

GEOPHYSICAL REPORT

on

Priest Lake Group - Johnson Group  
Bowman Group - Hodges Group  
Severe Group - Mallette Group  
Averill Group

of mineral claims  
situated near Van Anda, Texada Island  
( 49° 124° NW ), British Columbia

by 92F/10E

D.F.Coolbaugh

March 26, 1956, to May 30, 1956

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GEOPHYSICAL REPORT

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Clark Claim Groups

Texada Island, British Columbia

by

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scale 1" equals 300'
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scale 1" equals 1000'

Report on Geophysical Survey and Examination on the Clark  
Claim Groups, Texada Island, British Columbia.

INTRODUCTION

After preliminary conferences and study of the known geologic features of the claim area, a geophysical survey was deemed advisable. Geologic considerations indicated that magnetic and electromagnetic techniques would yield the best information. Magnetite iron deposits on Texada Island indicated the probability of magnetite concentrations along fractures and fissures as well as in iron ore bodies. Although the magnetite bodies might, in themselves, be rather non-conductive any associated sulphide could make the body conductive as well as sulphide veins not associated with magnetite.

Field work commenced on the claim groups March 26, 1956 and was completed May 30, 1956.

Mr. Charles M. Mallette was geophysical observer and was in charge of the party. Mr. Gordon H. Johnson, surveyor-draftsman was employed on the survey for the full time. Mr. John A. Wolfe was employed part time as geologist-geophysicist. As many as five laborers at a time were employed on the project as rodmán, axman, and geophysicist helper. The writer was employed on the project from April 1, 1956 until its completion.

### LOCATION AND TERRAIN

The Clark Claims are located in the north central portion of Texada Island (  $49^{\circ} 12\frac{1}{2}^{\circ}$  NW ), British Columbia, Canada. The 46 claims extend roughly from Priest Lake on the northwest, which is 2 miles south of Van Anda, south nearly to the Strait of Georgia. Van Anda is 80 miles northwest of Vancouver, B.C. The claim locations are shown on Plate III.

The claims are in an area of rather low relief ranging from 250 to 800 feet in elevation. Small cliffs and some steep gullies are found throughout the area.

As Texada Island is nowhere more than 6 miles in width the streams are necessarily short and small. Most of the streams occupy shallow canyons or narrow rock-walled valleys. Typical glacial swamps, ponds, and streams are found in the area.

Texada Island is well forested with fir, spruce, hemlock, cedar, pine, and alder. While the forest is generally difficult to penetrate due to the second growth, swamps and shrub filled open areas do occur.

### GEOLOGY

The following geologic column is taken from Department of Mines, Geological Survey, Memoir 58, "Geology of Texada Island" by R. G. McConnell, 1914.

Quaternary

Recent.....Creek gravels, peat, etc.  
Glacial.....Boulder, Clays, sands, silts.

Mesozoic

Upper Cretaceous.... Sandstones, clays, shales.  
Lower Cretaceous or  
Upper Jurassic..... Diorites and diorite porphyrites  
in small stocks and dikes.  
Upper Jurassic (?)....Quartz diorites.  
Lower Jurassic (?)....Texada Group: porphyrites  
Triassic or Jurassic....Marble Bay Formation: limestones  
Triassic.....Anderson Bay Formation: Shists,  
tuffs, agglomerates, amygdaloids,  
and marbles.

The only distinguishable formations that are exposed in the claim area are the Marble Bay limestone, the Texada Group of porphyrites, the various fine-grained to porphyritic dikes that intrude both the limestone and the porphyrites and glacial till.

The Marble Bay formation consists entirely of relatively pure limestone ranging in color from white to blue to almost black. No continuous large siliceous or aluminous beds occur. The limestone ranges from very fine and compact to coarsely crystalline. The thickness of the formation has never been ascertained but the shaft of the Marble Bay Mine indicates a thickness of at least 1400 feet.

Texada Group of porphyrites varies widely in texture, from fine-grained and almost glassy to porphyritic with phenocrysts up to one-half inch. The color varies from white through green and grey to black. The composition ranges from

almost entirely feldspar to more than 50% ferromagnesian minerals, all with varying amounts of magnetite. The thickness of the formation is unknown and is believed to vary greatly. A few limestone blocks have been noted within the porphyrites.

The dikes vary widely in texture, color and composition. They are generally fine-grained and dark.

The glacial till is made up of fragments of porphyrites, dikes, iron stained sands and a large amount of granite. The granite is fine-to medium-grained. It is composed of approximately 75% feldspar, 10-20% quartz, 10-15% magnetite and a very minor amount of biotite.

The observed contacts between the limestone and the porphyrites are either marked by faults or are intrusive. There is a difference of opinion in the literature as to the age relationship between the limestone and porphyrites.

The dominant direction of faulting on the island strikes northwesterly. The glaciers appear to have moved across the island from this direction. A secondary system of faults is nearly at right angles to and is cut by the major set. Since there are no mappable lithologic horizons within the Marble Bay or Texada formations, it has been impossible to measure displacement on the faults, although it must be extensive. Faults are quite numerous and are characterized by stream valleys with cliffs on the sides.

Most of the dikes follow a trend of a few degrees west of north, intermediate between the two major fault directions. Several sills can be recognized.

The limestone is gently folded with the central portion of the area studied possibly being a syncline. Drag folding can be noted along some of the faults, indicating that the limestone has moved up in relation to the porphyrites.

The important mineral deposits near the claim area are to the north, in the vicinity of Van Anda, and to the south. Deposits in the vicinity of Van Anda, were mined for copper and gold. The ore bodies were small pipes or short veins of inconsistent grade. They were usually found in limestone at or near contacts with later dioritic intrusives. None of these mines is now active. To the south, Texada Mines Ltd. is mining irregular lenses of magnetite with associated pyrite and chalcopyrite. These iron-copper bodies are generally on or close to the contact of the limestone and quartz diorite intrusives. Texada Mines is presently producing about 1200 tons of ore per day and a large reserve is reported.

The Commodore shaft is located in the south-central portion of mining claim B 40854. It was sunk on the contact of the limestone and porphyrite. It is reported that the shaft is 140 feet deep and that drifts were run in a westerly direction for 750 feet and in an easterly direction for 250 feet from the foot of the shaft. Some pyrite, chalcopyrite and galena were reported, but no ore bodies of importance were found. The workings are presently inaccessible. Some prospect holes have been dug on mining claims B40853, B 40849, B 40868, and John. No ore bodies were reported.

Limestone quarries are operating at Blubber Bay, two miles south of Blubber Bay, Marble Bay and southeast of Van Anda. This stone is being produced from the Marble Bay formation.

#### GEOPHYSICAL SURVEYS

Base lines for the control grid were run roughly parallel to the limestone-porphyrite contact on the west side of the Clark claims. The limestone-porphyrite contact zone was felt to be the most likely location for mineral deposits, based upon the geologic characteristics and observed and known mineralization. Base lines A, F, G and H covered this zone. Base lines K, P and Z were placed parallel to any supposed mineral trend. On these seven base lines, stations were placed 400 feet apart and lines were run through these stations at right angles to the base line. Points were placed at 50 foot intervals from 1000 to 2000 feet on either side of the base line. Grid M was laid out to investigate the pyrite outcrop at M15N1. Lines L and N were laid out to investigate the northern part of the claim group. Relocated topographic traverse points were also used as geophysical stations. All 46 claims were investigated in some way by geophysical methods. Plate I (A and B) shows the location and numbers of all of the grid stations. Some of the stations shown were not used for geophysical readings.

Magnetic Survey: Askania vertical magnetometer No. 92998 was used to obtain the magnetic readings. The computed readings are compiled and presented as an appendix to this report. The results of the magnetic survey are plotted on Plate II

(A and B) and Plate III.

In calculating the station values, the Base Station B-1 was given a value of 1000 gammas and all readings in the survey were referred to this base reading. The correction for diurnal variation was made by securing base readings at various times throughout the day. Magnetograms from the Meanook Observatory in Alberta giving the Z readings, were secured for selected days. Some magnetic disturbances occurred during the time of the survey.

The magnetometer was temperature-compensated, so no correction for temperature was necessary. Because of the limited area covered by the survey, it was not necessary to correct for longitude and latitude.

Over 2000 magnetometer stations were read and recorded. In addition, comparison values were secured on the magnetometer work done by Texada Mines Ltd., thereby allowing their work to be correlated with the magnetic values obtained on this survey.

Nine type specimens were analyzed for magnetic susceptibility. The results of these tests follow:

<u>SAMPLE</u>	<u>TYPE</u>	<u>SUSCEPTIBILITY X 10<sup>6</sup></u>
1	Igneous porphyry from the Commodore Mine dump	2480
2	Limestone at volcanic contact	480
3	Glacial granite	2480
4	Limestone at volcanic contact iron stained B40854 claim	510
5	Volcanic porphyry B40849 claim	2740
6	Dike rock B40849 claim	1350
7	Limestone B40849 claim	30
8	Dike rock B40849 claim	920
9	Limestone B40854 claim	100

The susceptibility determinations were run by Mr. P.A. Rodgers of the Colorado School of Mines Research Foundation.

Calibration checks were run on the magnetometer at least twice a week. To calibrate, a Helmholtz coil,

manufactured by the Ruska Instrument Company, was employed. If the magnetometer case was opened, for any reason, a calibration check was run before any station values were read. The average gammas per scale division calibration was 39 gammas.

Electromagnetic Survey: A Sharpe, model SE-100 electromagnetic survey unit was employed on this survey. The results of the electromagnetic survey are plotted on Plate II (A and B). Forty-eight lines were run electromagnetically.

The same grid lines that were used in the magnetic survey were utilized in the electromagnetic survey. Generally the transmitter was set up on the base line station and the grid lines, 200 or 400 feet from this station, perpendicular to the base line, were read. Readings were usually taken on the even 100 foot stations, but some lines were run using the 50 foot stations where detail was needed.

Since there are no corrections to be made when recording electromagnetic values, only the correct-way crossovers are plotted. The thickness of the crossover symbol on Plate II indicates the strength of the crossover. The greater the thickness the stronger is the crossover.

#### GEOPHYSICAL INTERPRETATION

The magnetic survey easily delineated the contact between the Marble Bay limestone and the Texada formation porphyrites. The contact runs nearly parallel to the A base line starting at A14 through A12 N2, A10 N3, A8 and A6 S4. The limestone-porphyrite contact closely follows the 1000 gamma contour on the west F base line going through F12 W12

F9 W9, F6 W8 and F3 W6. A southeast-northwest contact runs roughly parallel to the G base line from G17 N $\frac{1}{2}$  on the east through G20, G23 N1, G26 N2 $\frac{1}{2}$ . The contact then turns southwest-northeast along the H base line crossing G27 1 $\frac{1}{2}$  through H8 E $\frac{1}{2}$  through H11 W1 $\frac{1}{2}$  and H14 W2. The contact becomes obscure, using the magnetic data, southeast of H15 W2. The large amount of intrusive material observed in this area probably accounts for the lack of a good limestone-porphyrite contact.

These contacts between the limestone and porphyrite are fault contacts. The A base contact is a steeply dipping fault but the direction of dip can not be ascertained from the magnetic data. The F base fault contact also dips very steeply. The magnetic information indicates that the porphyrite is not as deep along the F base as it is elsewhere along the contact.

The G base line fault contact dips steeply to the southeast. The H base line fault contact is vertical or dips quite steeply to the northeast. The magnetic information indicates that the porphyrite on the southwest side of the H base line fault is over 200 feet deep.

The northwest-southeast trending faults along the F and H base lines cut the northeast-southwest trending faults along the A and G base lines. The apparent drag along the southwest side of the A base line fault indicates the possibility that the A and G base line faults are the same, having been displaced by the F base line fault.

The porphyrite is found to the north and west of the contacts stated above. Nowhere else in the claim area is the porphyrite of the Texada formation found. Numerous intrusives, generally fine-grained narrow dikes and sills, are found in the limestone area. Although the magnetic susceptibility of these dikes is two to ten times higher than the surrounding limestone, they are not generally detected because of their limited mass. A magnetite rich vein of the same magnitude would, however, be easily detected. The plus 2000 gamma areas in the northeast four claims are due to dikes. Some solution activity associated with the dikes was observed.

Two magnetic highs were recorded at M15 N1 and Z10 N1. Neither of these highs proved to be more than very limited in extent. The M15 N1 anomaly was due to a massive pyrite body which was exposed by prospect pits. The Z10 N1 anomaly was covered by till.

In the limestone area the magnetic values indicate the depth of the limestone. The formation beneath the limestone is unknown, however, the change in magnetic values, the susceptibilities of the type samples and the known depths all indicate that the limestone is lying on an igneous basement. Some diamond drilling was done in the limestone in this area, in 1954 but of the numerous holes drilled none penetrated the limestone. The maximum vertical depth drilled was 400 feet.

The limestones in this area exceed 400 feet in depth and indications are that the depth could easily exceed 1000

feet. From Plate II and Plate III it is observed that the thickness of the limestone increases from the north and northeast toward the south and southeast. The surface topography is not the predominating influence and, therefore, the bottom of the limestone is assumed to be deeper in the south central and southeastern part of the area.

The highest magnetic values were over 4000 gammas and certainly indicated concentrations of magnetite. To check these anomalous areas, electromagnetic profiles were run to determine if the magnetite was associated with conductive bodies.

None of the electromagnetic crossovers was strong thereby indicating a large highly conductive body. Special profiles on 50 foot spacing were run on All $\frac{1}{2}$  and the M base line to evaluate exposed mineral bodies. The crossover at M15 between N $\frac{1}{2}$  and N1 was the strongest noted in the area and was over a massive pyrite body exposed by a pit approximately 6X6X10 feet. As noted on Plate II A, however, this crossover was not recorded on M14 or M16 which are only 100 feet from M15. This prospect is therefore just a local body with no lateral or vertical extent but deposited along a northwest-southeast trending fracture.

The fair crossover on All $\frac{1}{2}$  N3 $\frac{1}{2}$  was over a vein of massive pyrite and limonite which was exposed by a short adit. The local mineralization was strong as in M15 but again the crossover was not evident 200 feet along the strike in either direction.

The crossovers on All $\frac{1}{2}$ , A13, A12, A11, A10 and A9 lie in a fairly straight line and indicate a conductor. The half

lines of A11 $\frac{1}{2}$ , A10 $\frac{1}{2}$  and A9 $\frac{1}{2}$  did not show this crossover indicating that this conductor is discontinuous. It is possible that this conductor is along the fault contact between the limestone and porphyrite.

The high magnetic anomaly located just south of A9 $\frac{1}{2}$ , A10 and A10 $\frac{1}{2}$  showed no conductivity. This fact and the fact that there was no associated low with the high indicates a near surface effect which can be explained by the concentration of glacial granite at this place.

No crossovers were obtained on the F base line.

Only two crossovers of consequence were noted on the G base line. The fairly strong crossover at G17 $\frac{1}{2}$  is close to the limestone-porphyrite contact and probably indicates the zone explored by the Commodore Mine. A good crossover at G24 $\frac{1}{2}$  N6 $\frac{1}{2}$  corresponds to a magnetic high and indicates a conductive body at shallow depth. Since this crossover did not show up 200 feet east and west indicates that the body is not horizontally extensive.

No crossovers of consequence were recorded on the H base line. The crossover at G27 8 corresponds to a magnetic high. The crossovers at H13 E4 $\frac{1}{2}$  and H15 E4 are well within the limestone. These crossovers are only fair and can easily indicate better than average conductivity along a dike limestone contact.

A magnetic high encountered at Z10 N1 did not produce an electromagnetic crossover when run on 50 foot spacing.

RECOMMENDATIONS

1. Detailed geologic investigations should be carried out in the areas of porphyrite-limestone contact which has been delineated by the magnetic survey. Because of the talus slopes it may be necessary to dig pits in these contact areas.

2. In areas of high magnetization detailed geology and possibly geochemistry should be undertaken.

3. Investigation by drilling would be recommended at the following locations:

- a. A11<sub>4</sub>
- b. A10 N2<sub>2</sub><sup>1</sup>
- c. G21<sub>4</sub><sup>1</sup> N6<sub>2</sub><sup>1</sup>

May 30, 1956.

Respectfully submitted,

  
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MAGNETIC SURVEY EQUIPMENT AND PROCEDURE

The magnetic exploration method is one of the oldest of the applied geophysical methods. It utilizes a natural field of force, that is, the Earth's magnetic field, and is applicable economically in regions where the magnetic properties of the rocks have some known relationship to the economic geology.

Interpretation of magnetic data is based on the fact that the Earth's normal magnetic field is uniform over areas of magnetically homogeneous composition but is distorted in certain regions of inhomogeneous composition. The amount of distortion depends upon the relative magnetic susceptibilities of the subsurface materials and the relative masses and configurations of these component materials. Most magnetic anomalies are due to igneous rocks, iron ores, and those sedimentary deposits which contain magnetite derived from igneous rocks. Magnetic methods, therefore, are directly applicable where the mineral sought is itself magnetic, or is associated in its occurrence with magnetic minerals.

On this magnetic survey a vertical Askania magnetometer was used. This magnetometer measures the vertical component of the Earth's magnetic field by recording the bar magnet needle position. This needle is acted upon by two opposing torques; that due to gravity and that due to the vertical component of the Earth's field. When reading the magnetometer the bar magnet needle is oriented perpendicular to the Earth's magnetic field. In this position the horizontal component of the Earth's field passes through the axis of rotation and will

exert zero torque on the system, while the vertical magnetic component exerts maximum torque.

The reading procedure at a station is as follows:

1. Set up tripod and level using the single level bubble in the tripod head.
2. Orient head of tripod magnetically east-west, using compass.
3. Place and lock magnetometer on tripod head and level.
4. Orient magnetometer with its north pole to the east.
5. Release the system by lowering magnet onto quartz knife edges and read scale. Repeat by lifting and replacing until check readings are obtained.
6. Orient magnetometer with its north pole to the west and repeat reading.

The magnetometer must be oriented east-west within a degree or two and must be carefully leveled. Taking readings with the north pole to the east and to the west compensates for errors in orientation and leveling. The reading used for calculation is the mean of the north to east and north to west readings.

In computing station values in gammas it is first necessary to determine the number of gammas for each scale division of deflection. A Helmholtz coil was employed for the above determination and a calibration was carried out at least twice a week. The average value of gammas per scale

division was 39.

Corrections for temperature were not necessary, as the magnetometer used was temperature compensated. No correction for latitude or longitude was made since the survey was confined to an area of less than three miles square.

Corrections were made for auxiliary magnets and for the diurnal variation. The diurnal variation correction was made by using multiple readings of a base station during each day that the magnetic survey was carried out. Some magnetic disturbances were noted but most of these were of small magnitude and were corrected.

A station value was assigned to one station and all of the other readings were made relative to that base.

ELECTROMAGNETIC SURVEY EQUIPMENT AND PROCEDURE

Exploration for base metals has shown that one geophysical method is not always sufficient to determine likely locations for these deposits.

In the case of massive sulphide deposits, some of these, as at Sudbury, Ontario, are sufficiently magnetic to be detected in a magnetometer survey, but these same magnetic anomalies could equally well arise from other and uneconomical sources such as ultra basic rocks or iron formations. In other cases the deposits do not produce marked magnetic anomalies and, therefore, could be missed by magnetic methods. These massive sulphide deposits do, however, act as very good conductors of electricity, and electromagnetic methods have been used to advantage in the search for these deposits.

The electromagnetic method has been one of the fundamental methods of geophysics for many years. The principle of operation is that if an electric current is caused to flow in a coil of wire, small concentric magnetic fields are set up about this wire in planes at right angles to the coil. An alternating or varying electromagnetic field due to one loop will cause an oppositely-directed electromagnetic field in a nearby loop.

The principle of all electromagnetic methods is that an energizing coil will induce current in a conductive body which can be measured on the surface and used to locate the deposit.

A grid is chosen and surveyed so that the direction of the base line is parallel to the strike of the geology.

Parallel grid lines are then run at right angles to this base line.

The survey method employed is to set up a transmitter, consisting of a three-foot square loop of 50 turns of wire, at a central point in the prepared grid. Generally the size of the area which is to be explored is not more than 2000 feet square for each transmitter location. The transmitting coil is then energized by means of a small portable gasoline motor driven generator. The coil is beamed or pointed in turn at each individual station and readings are taken with the receiver coil. The receiver consists of a nine inch diameter closely-wound coil which is mounted on a staff along with the amplifier and clinometer.

At each station where readings are taken the transmitter coil must be pointed at the receiver and the receiver tilted to right or left, a certain position will be found where no, or greatly reduced, sound is heard in the earphones. If the clinometer needle is read at the null point, its deviation from zero will measure the angle of the resultant magnetic field from the horizontal. Where successive readings are taken in this manner at equal spacing along a profile over a conducting body it will be found that the receiver will always tilt away from the conductor. For example, if a conductor strikes east-west, on the west side of the line the receiver coil will tilt toward the west, while on the east side of the conductor it will tilt toward the east. At that place where the tilt of the receiver changes from west to east we have a correct-way crossover which marks the electrical axis of the

conductor.

The equipment employed on this survey was a Sharpe Model SE-100 Electromagnetic Survey Unit, manufactured by Sharpe Instruments Ltd., Toronto.

**APPENDIX**

STATION	VALUE	STATION	VALUE	STATION	VALUE
B 1	1000	A 14 S 9 $\frac{1}{2}$	1839	A 13 S 2	2559
A 10 0	2910	A 14 S 10	1849	A 13 S 2 $\frac{1}{2}$	2054
A 5	1412	A 14 S 10 $\frac{1}{2}$	1983	A 13 S 3	1957
A 6	1464	A 14 S 11	1616	A 13 S 3 $\frac{1}{2}$	1949
A 7	1481	A 14 S 11 $\frac{1}{2}$	1602	A 13 S 4	1915
A 8	1335	A 14 S 12	2297	A 13 S 4 $\frac{1}{2}$	1837
A 9	1256	A 14 S 12 $\frac{1}{2}$	1673	A 13 S 5	1774
A 10	1170	A 14 S 13	1631	A 13 S 5 $\frac{1}{2}$	1731
A 11	1224	A 14 S 13 $\frac{1}{2}$	1670	A 13 S 6	1707
B 1	1000	A 14 S 14	1548	A 13 S 6 $\frac{1}{2}$	1686
A 10 0	2942	A 14 S 14 $\frac{1}{2}$	1522	A 13 S 7	1745
A 14 S 1	2444	A 14 S 15	1545	A 13 S 7 $\frac{1}{2}$	1798
A 14 S 1 $\frac{1}{2}$	2697	A 10 0	2857	A 13 S 8	1661
A 14 S 2	2447	B 1	1000	A 13 S 8 $\frac{1}{2}$	1675
A 14 S 2 $\frac{1}{2}$	2294	A 10 0	2860	A 13 S 9	1632
A 14 S 3	2300	A 13 N 4	3335	A 13 S 9 $\frac{1}{2}$	1624
A 14 S 3 $\frac{1}{2}$	2342	A 13 N 3 $\frac{1}{2}$	3385	A 13 S 10	1631
A 14 S 4	2258	A 13 N 3		A 13 S 10 $\frac{1}{2}$	1616
A 14 S 4 $\frac{1}{2}$	2210	A 13 N 2 $\frac{1}{2}$	3748	A 13 S 11	1605
A 14 S 5	2214	A 13 N 2	4118	A 13 S 11 $\frac{1}{2}$	1607
A 14 S 5 $\frac{1}{2}$	2534	A 13 N 1 $\frac{1}{2}$	3982	A 13 S 12	1580
A 14 S 6	2633	A 13 N 1	3277	A 13 S 12 $\frac{1}{2}$	1575
A 14 S 7	2530	A 13 N $\frac{1}{2}$	2583	A 10	2860
A 14 S 7 $\frac{1}{2}$	1910	A 13	2534	A 13 N 2 $\frac{1}{2}$	3757
A 14 S 8	2063	A 13 S $\frac{1}{2}$	2397	A 13 N 3	4610
A 14 S 8 $\frac{1}{2}$	1942	A 13 S 1	2217	A 12 N 3	4216
A 14 S 9	1817	A 13 S 1 $\frac{1}{2}$	2090	A 12 N 2 $\frac{1}{2}$	2979
				A 12 N 2	2579

STATION	VALUE	STATION	VALUE	STATION	VALUE
A 12 N 1 $\frac{1}{2}$	2285	A 12 S 12 $\frac{1}{2}$	1488	A 11 S 9 $\frac{1}{2}$	1600
A 12 N 1	2281	A 12 S 13	1571	A 11 S 10	1611
A 12 N $\frac{1}{2}$	2576	A 12 S 13 $\frac{1}{2}$	1491	A 11 S 11	1588
A 12	1917	A 12 S 14	1452	A 11 S 11 $\frac{1}{2}$	1551
A 12 S $\frac{1}{2}$	1968	A 12 S 14 $\frac{1}{2}$	1414	A 11 S 12	1582
A 12 S 1	1926	A 12 S 15	1440	A 11 S 12 $\frac{1}{2}$	1613
A 12 S 1 $\frac{1}{2}$	1891	A 10	2860	A 11 S 13	1587
A 12 S 2	1859	B 1	1000	A 11 S 13 $\frac{1}{2}$	1678
A 12 S 2 $\frac{1}{2}$	1894	A 10	2860	A 11 S 14	1639
A 12 S 3	1933	A 11	2159	A 11 S 14 $\frac{1}{2}$	1787
A 12 S 3 $\frac{1}{2}$	1769	A 11 S $\frac{1}{2}$	2167	A 11 S 15	1639
A 12 S 4	1798	A 11 S 1	1973	A 11 N $\frac{1}{2}$	2311
A 12 S 4 $\frac{1}{2}$	1753	A 11 S 1 $\frac{1}{2}$	1937	A 11 N 1	2363
A 12 S 5	1785	A 11 S 2	1888	A 11 N 1 $\frac{1}{2}$	3131
A 12 S 5 $\frac{1}{2}$	1766	A 11 S 2 $\frac{1}{2}$	1866	A 11 N 2	2937
A 12 S 6	1715	A 11 S 3	1829	A 11 N 2 $\frac{1}{2}$	2521
A 12 S 6 $\frac{1}{2}$	1664	A 11 S 3 $\frac{1}{2}$	1843	A 11 N 3	2816
A 12 S 7	1683	A 11 S 4	1857	A 11 N 3 $\frac{1}{2}$	3203
A 12 S 7 $\frac{1}{2}$	1613	A 11 S 4 $\frac{1}{2}$	1809	A 11 N 4	3083
A 12 S 8	1571	A 11 S 5	1836	A 11 N 4 $\frac{1}{2}$	2741
A 12 S 8 $\frac{1}{2}$	1597	A 11 S 5 $\frac{1}{2}$	1788	A 10 N 6 $\frac{1}{2}$	2560
A 12 S 9	1609	A 11 S 6	1786	A 10 N 6	2627
A 12 S 9 $\frac{1}{2}$	1542	A 11 S 6 $\frac{1}{2}$	1738	A 10 N 5 $\frac{1}{2}$	2753
A 12 S 10	1542	A 11 S 7	1720	A 10 N 5	2775
A 12 S 10 $\frac{1}{2}$	1552	A 11 S 7 $\frac{1}{2}$	1681	A 10 N 4 $\frac{1}{2}$	2683
A 12 S 11	1526	A 11 S 8	1638	A 10 N 4	2741
A 12 S 11 $\frac{1}{2}$	1510	A 11 S 8 $\frac{1}{2}$	1631	A 10 N 3 $\frac{1}{2}$	2652
A 12 S 12	1507	A 11 S 9	1789	A 10 N 3	2749

STATION	VALUE	STATION	VALUE	STATION	VALUE
A 10 N 2½	2745	A 10 S 12	1413	A 9 S 2	1898
A 10 N 2	2780	A 10 S 12½	1386	A 9 S 2½	1794
A 10 N 1½	2712	A 10 S 13	1387	A 9 S 3	1766
A 10 N 1	2737	A 10 S 13½	1353	A 9 S 3½	1738
A 10 N ½	2681	A 10 S 14	1416	A 9 S 4	1704
A 10 S ½	3220	A 10 S 14½	1441	A 9 S 4½	1522
A 10 S 1	3189	A 10 S 15	1438	A 9 S 5	1522
A 10 S 1½	3360	A 9	2197	A 9 S 5½	1555
A 10 S 2	3505	A 9 N ½	2334	A 9 S 6	1513
A 10 S 2½	3478	A 9 N 1	2621	A 9 S 6½	1526
A 10 S 3	3226	A 9 N 1½	2750	A 9 S 7	1517
A 10 S 3½	3369	A 9 N 2	2930	A 9 S 7½	1758
A 10 S 4	2389	A 9 N 2½	3032	A 9 S 8	1461
A 10 S 4½	2033	A 9 N 3	3003	A 9 S 8½	1448
A 10 S 5	2291	A 9 N 3½	2849	A 9 S 9	1430
A 10 S 5½	2025	A 9 N 4	2696	A 9 S 9½	1479
A 10 S 6	1789	A 9 N 4½	2556	A 9 S 10	1435
A 10 S 6½	1637	A 9 N 5	2360	A 9 S 10½	1914
A 10 S 7	1590	A 9 N 5½	2217	A 9 S 11	1613
A 10 S 7½	1554	A 9 N 6	2592	A 9 S 11½	1408
A 10 S 8	1549	A 9 N 6½	2519	A 9 S 12	1418
A 10 S 8½	1516	A 9 N 7	2743	A 9 S 12½	1423
A 10 S 9	1465	A 9 N 7½	2786	A 9 S 13	1370
A 10 S 9½	1442	A 9 N 8	2877	A 9 S 13½	1444
A 10 S 10	1443	A 9 N 8½	2825	A 9 S 14	1298
A 10 S 10½	1434	A 9 S ½	2105	A 9 S 14½	1382
A 10 S 11	1456	A 9 S 1	1983	A 9 S 15	1295
A 10 S 11½	1478	A 9 S 1½	1930	A 8	2614

STATION	VALUE	STATION	VALUE	STATION	VALUE
A 8 S ½	2389	A 8 S 14	1306	A 7 N ½	1648
A 8 S 1	2128	A 8 S 14½	1311	A 7 N 1	1577
A 8 S 1½	1898	A 8 S 15	1291	A 7 N 1½	2009
A 8 S 2	1802	A 8 N ½	2716	A 7 N 2	1633
A 8 S 2½	1709	A 8 N 1	2908	A 7 N 2½	1408
A 8 S 3	1647	A 8 N 1½	2961	A 7 N 3	1318
A 8 S 3½	1645	A 8 N 2	3078	A 7 N 3½	1630
A 8 S 4	1552	A 8 N 2½	3453	A 7 N 4	2181
A 8 S 4½	1522	A 8 N 3	3046	A 7 N 4½	4069
A 8 S 5	1559	A 8 N 3½	4011	A 7 N 5	2517
A 8 S 5½	1519	A 8 N 4	3947	A 7 N 5½	3349
A 8 S 6	1427	A 8 N 4½	3787	A 7 N 6	1978
A 8 S 6½	1433	A 8 N 5	3287	A 7 N 6½	2383
A 8 S 7	1331	A 8 N 5½	3745	A 7 N 7	2267
A 8 S 7½	1347	A 8 N 6	3574	A 7 N 7½	2014
A 8 S 8	1364	A 8 N 6½	3931	A 7 N 8	1667
A 8 S 8½	1351	A 8 N 7	4110	A 7 N 8½	1579
A 8 S 9	1384	A 8 N 7½	2493	A 7 N 9	2265
A 8 S 9½	1332	A 8 N 8	2262	A 7 N 9½	1636
A 8 S 10	1329	A 8 N 8½	2401	A 7 N 10	1760
A 8 S 10½	1292	A 8 N 9	2245	A 7 N 10½	2160
A 8 S 11	1287	A 8 N 9½	2267	A 7 N 11	2496
A 8 S 11½	1203	A 8 N 10	1971	A 7 N 11½	2416
A 8 S 12	1244	A 8 N 10½	1751	A 7 N 12	2398
A 8 S 12½	1343	A 8 N 11	1930	A 7 N 12½	2926
A 8 S 13	1295	A 8 N 11½	1774	A 7 N 13	2229
A 8 S 13½	1286	A 7	1818	A 7 N 13½	2953

STATION	VALUE	STATION	VALUE	STATION	VALUE
A 7 N 14	3155	A 6 N 9 $\frac{1}{2}$	1970	A 5 N 8	1791
A 7 N 14 $\frac{1}{2}$	2601	A 6 N 10	1805	A 5 N 8 $\frac{1}{2}$	1614
A 7 N 15	2015	A 6 N 10 $\frac{1}{2}$	1591	A 5 N 9	1500
A 14 N 3 $\frac{1}{2}$	2739	A 6 N 11	1760	A 7 S $\frac{1}{2}$	2229
A 14 N 4	3295	A 6 N 11 $\frac{1}{2}$	1765	A 7 S 1	2272
A 14 N 4 $\frac{1}{2}$	2646	A 6 N 12	1407	A 7 S 1 $\frac{1}{2}$	2223
A 14 N 5	4161	A 6 N 12 $\frac{1}{2}$	1151	A 7 S 2	1632
A 14 N 5 $\frac{1}{2}$	2914	A 6 N 13	1619	A 7 S 2 $\frac{1}{2}$	1646
A 14 N 6	3721	A 6 N 13 $\frac{1}{2}$	2414	A 7 S 3	1568
A 6	1433	A 6 N 14	2042	A 7 S 3 $\frac{1}{2}$	1510
A 6 N $\frac{1}{2}$	1210	A 6 N 14 $\frac{1}{2}$	2063	A 7 S 4	1460
A 6 N 1	1022	A 6 N 15	1922	A 7 S 4 $\frac{1}{2}$	1416
A 6 N 1 $\frac{1}{2}$	1039	A 5	1775	A 7 S 5	1379
A 6 N 2	1247	A 5 N $\frac{1}{2}$	1847	A 7 S 5 $\frac{1}{2}$	1349
A 6 N 2 $\frac{1}{2}$	1492	A 5 N 1	1749	A 7 S 6	1326
A 6 N 3	1915	A 5 N 1 $\frac{1}{2}$	1333	A 7 S 6 $\frac{1}{2}$	1350
A 6 N 3 $\frac{1}{2}$	1647	A 5 N 2	940	A 7 S 7	1248
A 6 N 4	1734	A 5 N 2 $\frac{1}{2}$	1293	A 7 S 7 $\frac{1}{2}$	1264
A 6 N 4 $\frac{1}{2}$	1398	A 5 N 3	1531	A 7 S 8	1246
A 6 N 5	1040	A 5 N 3 $\frac{1}{2}$	1635	A 7 S 8 $\frac{1}{2}$	1247
A 6 N 5 $\frac{1}{2}$	1457	A 5 N 4	1639	A 7 S 9	1248
A 6 N 6	1683	A 5 N 4 $\frac{1}{2}$	1838	A 7 S 9 $\frac{1}{2}$	1177
A 6 N 6 $\frac{1}{2}$	1701	A 5 N 5	1715	A 7 S 10	1146
A 6 N 7	1927	A 5 N 5 $\frac{1}{2}$	1971	A 7 S 10 $\frac{1}{2}$	1189
A 6 N 7 $\frac{1}{2}$	1752	A 5 N 6	1662	A 7 S 11	1183
A 6 N 8	1779	A 5 N 6 $\frac{1}{2}$	1710	A 7 S 11 $\frac{1}{2}$	1179
A 6 N 8 $\frac{1}{2}$	1548	A 5 N 7	1738	A 7 S 12	1240
A 6 N 9	1698	A 5 N 7 $\frac{1}{2}$	1822	A 7 S 12 $\frac{1}{2}$	1216

STATION	VALUE	STATION	VALUE	STATION	VALUE
A 7 S 13	1216	A 6 S 12	1155	A 5 S 11	1144
A 7 S 13 $\frac{1}{2}$	1172	A 6 S 12 $\frac{1}{2}$	1172	A 5 S 11 $\frac{1}{2}$	1103
A 7 S 14	1094	A 6 S 13	1089	A 5 S 12	1140
A 7 S 14 $\frac{1}{2}$	1087	A 6 S 13 $\frac{1}{2}$	1088	A 5 S 12 $\frac{1}{2}$	1182
A 7 S 15	1089	A 6 S 14	1150	A 5 S 13	993
A 6 S $\frac{1}{2}$	1599	A 6 S 14 $\frac{1}{2}$	1039	A 5 S 13 $\frac{1}{2}$	1055
A 6 S 1	2061	A 6 S 15	1110	A 5 S 14	911
A 6 S 1 $\frac{1}{2}$	2213	A 5 S $\frac{1}{2}$	1160	A 5 S 14 $\frac{1}{2}$	933
A 6 S 2	2671	A 5 S 1	1197	A 5 S 15	972
A 6 S 2 $\frac{1}{2}$	2619	A 5 S 1 $\frac{1}{2}$	1626	A 10 $\frac{1}{2}$	2867
A 6 S 3	2526	A 5 S 2	1756	A 10 $\frac{1}{2}$ N $\frac{1}{2}$	2920
A 6 S 3 $\frac{1}{2}$	2923	A 5 S 2 $\frac{1}{2}$	1683	A 10 $\frac{1}{2}$ N 1	2779
A 6 S 4	2051	A 5 S 3	1471	A 10 $\frac{1}{2}$ N 1 $\frac{1}{2}$	2803
A 6 S 4 $\frac{1}{2}$	1855	A 5 S 3 $\frac{1}{2}$	1515	A 10 $\frac{1}{2}$ N 2	2917
A 6 S 5	1560	A 5 S 4	1912	A 10 $\frac{1}{2}$ N 2 $\frac{1}{2}$	3028
A 6 S 5 $\frac{1}{2}$	1452	A 5 S 4 $\frac{1}{2}$	1875	A 10 $\frac{1}{2}$ N 3	2934
A 6 S 6	1190	A 5 S 5	2825	A 10 $\frac{1}{2}$ N 3 $\frac{1}{2}$	2711
A 6 S 6 $\frac{1}{2}$	1294	A 5 S 5 $\frac{1}{2}$	2480	A 10 $\frac{1}{2}$ N 4	2462
A 6 S 7	1243	A 5 S 6	1742	A 10 $\frac{1}{2}$ N 4 $\frac{1}{2}$	2487
A 6 S 7 $\frac{1}{2}$	1242	A 5 S 6 $\frac{1}{2}$	1521	A 10 $\frac{1}{2}$ N 5	2437
A 6 S 8	1163	A 5 S 7	1430	A 10 $\frac{1}{2}$ N 5 $\frac{1}{2}$	2347
A 6 S 8 $\frac{1}{2}$	1361	A 5 S 7 $\frac{1}{2}$	1368	A 10 $\frac{1}{2}$ N 6	2401
A 6 S 9	1225	A 5 S 8	1341	A 10 $\frac{1}{2}$ S $\frac{1}{2}$	2894
A 6 S 9 $\frac{1}{2}$	1117	A 5 S 8 $\frac{1}{2}$	1246	A 10 $\frac{1}{2}$ S 1	3242
A 6 S 10	1124	A 5 S 9	1237	A 10 $\frac{1}{2}$ S 1 $\frac{1}{2}$	3555
A 6 S 10 $\frac{1}{2}$	1124	A 5 S 9 $\frac{1}{2}$	1171	A 10 $\frac{1}{2}$ S 2	3224
A 6 S 11	1132	A 5 S 10	1155	A 10 $\frac{1}{2}$ S 2 $\frac{1}{2}$	3036
A 6 S 11 $\frac{1}{2}$	1078	A 5 S 10 $\frac{1}{2}$	1072	A 10 $\frac{1}{2}$ S 3	1784

STATION	VALUE	STATION	VALUE	STATION	VALUE
A 10½ S 3½	1779	A 11½ S 4½	1591	A 9½ S 1	3704
A 10½ S 4	1713	A 11½ S 5	1554	A 9½ S 1½	3619
A 10½ S 4½	1683	A 11½ S 5½	1524	A 9½ S 2	3607
A 10½ S 5	1632	A 11½ S 6	1499	A 9½ S 2½	3369
A 10½ S 5½	1628	A 11½ S 6½	1592	A 9½ S 3	2341
A 10½ S 6	1627	A 11½ S 7	1551	A 9½ S 3½	1844
A 10½ S 6½	1588	A 11½ S 7½	1536	A 9½ S 4	3620
A 10½ S 7	1562	A 11½ S 8	1520	A 9½ S 4½	2965
A 10½ S 7½	1562	A 11½ S 8½	1439	A 9½ S 5	1385
A 10½ S 8	1553	A 11½ S 9	1401	A 9½ S 5½	1685
A 10½ S 8½	1579	A 11½ S 9½	1382	A 9½ S 6	1955
A 10½ S 9	1545	A 11½ S 10	1363	A 9½ S 6½	2014
A 10½ S 9½	1488	A 11½ S 3½	1516	A 9½ S 7	2061
A 10½ S 10	1479	A 11½ S 4	1486	A 9½ S 7½	2120
A 11½	1821	A 9½ N 6	2452	A 9½ S 8	2555
A 11½ N ½	1831	A 9½ N 5½	2746	A 9½ S 8½	1845
A 11½ N 1	1910	A 9½ N 5	2619	A 9½ S 9	1959
A 11½ N 1½	2017	A 9½ N 4½	2549	A 9½ S 9½	1637
A 11½ N 2	2110	A 9½ N 4	2724	A 9½ S 10	1364
A 11½ N 2½	2270	A 9½ N 3½	2986	F 3	661
A 11½ N 3	2593	A 9½ N 3	2958	F 3 W ½	664
A 11½ N 3½	3765	A 9½ N 2½	2499	F 3 W 1	737
A 11½ N 4	2989	A 9½ N 2	2551	F 3 W 1½	799
A 11½ S ½	1710	A 9½ N 1½	2692	F 3 W 2	752
A 11½ S 1	1675	A 9½ N 1	2748	F 3 W 2½	843
A 11½ S 1½	1628	A 9½ N ½	2671	F 3 W 3	796
A 11½ S 2	1581	A 9½	3128	F 3 W 3½	843
A 11½ S 2½	1574	A 9½ S ½	3415	F 3 W 4	905

STATION	VALUE	STATION	VALUE	STATION	VALUE
F 3 W 4½	865	F 3 E 8½	725	F 4 W 2	895
F 3 W 5	766	F 3 E 9	935	F 4 W 2½	835
F 3 W 5½	825	F 3 E 9½	905	F 4 W 3	837
F 3 W 6	1496	F 3 E 10	894	F 4 W 3½	858
F 3 W 6½	1871	F 4 E 10	839	F 4 W 4	858
F 3 W 7	1621	F 4 E 9½	874	F 4 W 4½	843
F 3 W 7½	2930	F 4 E 9	904	F 4 W 5	857
F 3 W 8	1098	F 4 E 8½	938	F 4 W 5½	788
F 3 W 8½	2436	F 4 E 8	997	F 4 W 6	619
F 3 W 9	2245	F 4 E 7½	1089	F 4 W 6½	644
F 3 W 9½	2384	F 4 E 7	1260	F 4 W 7	1171
F 3 W 10	2782	F 4 E 6½	1063	F 4 W 7½	1290
F 3 E ½	815	F 4 E 6	1050	F 4 W 8	1436
F 3 E 1	829	F 4 E 5½	1048	F 4 W 8½	1376
F 3 E 1½	799	F 4 E 5	992	F 4 W 9	1643
F 3 E 2	809	F 4 E 4½	1030	F 4 W 9½	2017
F 3 E 2½	829	F 4 E 4	1046	F 4 W 10	2509
F 3 E 3	774	F 4 E 3½	976	F 4 W 10½	2494
F 3 E 3½	856	F 4 E 3	912	F 5 W 10	1885
F 3 E 4	754	F 4 E 2½	860	F 5 W 9½	1428
F 3 E 4½	813	F 4 E 2	869	F 5 W 9	1756
F 3 E 5	918	F 4 E 1½	766	F 5 W 8½	1524
F 3 E 5½	971	F 4 E 1	832	F 5 W 8	1577
F 3 E 6	1118	F 4 E ½	856	F 5 W 7½	690
F 3 E 6½	1052	F 4	889	F 5 W 7	927
F 3 E 7	914	F 4 W ½	871	F 5 W 6½	1018
F 3 E 7½	981	F 4 W 1	911	F 5 W 6	1057
F 3 E 8	991	F 4 W 1½	930	F 5 W 5½	1229

STATION	VALUE	STATION	VALUE	STATION	VALUE
F 5 W 5	1110	F 5 E 8½	755	F 6 E 3½	810
F 5 W 1½	1199	F 5 E 9	801	F 6 E 3	758
F 5 W 4	1120	F 5 E 9½	763	F 6 E 2½	584
F 5 W 3½	1092	F 5 E 10	761	F 6 E 2	699
F 5 W 3	964	F 5 E 10½	745	F 6 E 1½	658
F 5 W 2½	933	F 5 E 11	838	F 6 E 1	609
F 5 W 2	892	F 5 E 11½	747	F 6 E ½	668
F 5 W 1½	759	F 5 E 12	802	F 6	570
F 5 W 1	740	F 5 E 12½	780	F 6 W ½	624
F 5 W ½	611	F 5 E 13	663	F 6 W 1	582
F 5	650	F 5 E 13½	721	F 6 W 1½	583
F 5 E ½	566	F 5 E 14	813	F 6 W 2	602
F 5 E 1	722	F 5 E 14½	833	F 6 W 2½	693
F 5 E 1½	696	F 5 E 15	773	F 6 W 3	904
F 5 E 2	605	F 6 E 10	763	F 6 W 3½	1098
F 5 E 2½	712	F 6 E 9½	794	F 6 W 4	1126
F 5 E 3	678	F 6 E 9	822	F 6 W 4½	1025
F 5 E 3½	614	F 6 E 8½	1033	F 6 W 5	1067
F 5 E 4	652	F 6 E 8	1120	F 6 W 5½	1062
F 5 E 4½	718	F 6 E 7½	890	F 6 W 6	916
F 5 E 5	775	F 6 E 7	914	F 6 W 6½	1111
F 5 E 5½	805	F 6 E 6½	819	F 6 W 7	1219
F 5 E 6	806	F 6 E 6	809	F 6 W 7½	841
F 5 E 6½	806	F 6 E 5½	879	F 6 W 8	843
F 5 E 7	838	F 6 E 5	925	F 6 W 8½	509
F 5 E 7½	959	F 6 E 4½	854	F 6 W 9	595
F 5 E 8	1052	F 6 E 4	821	F 6 W 9½	611

STATION	VALUE	STATION	VALUE	STATION	VALUE
F 6 W 10	574	F 7 E 4 $\frac{1}{2}$	801	F 7 W 9 $\frac{1}{2}$	1120
100 B	1656	F 7 E 4	968	F 7 W 10	1219
A Base	1102	F 7 E 3 $\frac{1}{2}$	993	F 8 W 10	1212
F 7 E 17	1056	F 7 E 3	907	F 8 W 9 $\frac{1}{2}$	1009
F 7 E 16 $\frac{1}{2}$	963	F 7 E 2 $\frac{1}{2}$	806	F 8 W 9	1075
F 7 E 16	1031	F 7 E 2	723	F 8 W 8 $\frac{1}{2}$	1388
F 7 E 15 $\frac{1}{2}$	978	F 7 E 1 $\frac{1}{2}$	756	F 8 W 8	1388
F 7 E 15	993	F 7 E 1	657	F 8 W 7 $\frac{1}{2}$	1014
F 7 E 14 $\frac{1}{2}$	971	F 7 E $\frac{1}{2}$	484	F 8 W 7	946
F 7 E 14	826	F 7	896	F 8 W 6 $\frac{1}{2}$	988
F 7 E 13 $\frac{1}{2}$	887	F 7 W $\frac{1}{2}$	1646	F 8 W 6	751
F 7 E 13	899	F 7 W 1	5236	F 8 W 5 $\frac{1}{2}$	790
F 7 E 12 $\frac{1}{2}$	906	F 7 W 1 $\frac{1}{2}$	1152	F 8 W 5	473
F 7 E 12	900	F 7 W 2	825	F 8 W 4 $\frac{1}{2}$	599
F 7 E 11 $\frac{1}{2}$	1045	F 7 W 2 $\frac{1}{2}$	799	F 8 W 4	650
F 7 E 11	949	F 7 W 3	750	F 8 W 3 $\frac{1}{2}$	581
F 7 E 10 $\frac{1}{2}$	991	F 7 W 3 $\frac{1}{2}$	750	F 8 W 3	490
F 7 E 10	988	F 7 W 4	834	F 8 W 2 $\frac{1}{2}$	610
F 7 E 9 $\frac{1}{2}$	1016	F 7 W 4 $\frac{1}{2}$	624	F 8 W 2	611
F 7 E 9	1234	F 7 W 5	762	F 8 W 1 $\frac{1}{2}$	616
F 7 E 8 $\frac{1}{2}$	1005	F 7 W 5 $\frac{1}{2}$	736	F 8 W 1	617
F 7 E 8	902	F 7 W 6	873	F 8 W $\frac{1}{2}$	690
F 7 E 7 $\frac{1}{2}$	890	F 7 W 6 $\frac{1}{2}$	778	F 8	699
F 7 E 7	910	F 7 W 7	713	F 8 E $\frac{1}{2}$	696
F 7 E 6 $\frac{1}{2}$	815	F 7 W 7 $\frac{1}{2}$	1252	F 8 E 1	666
F 7 E 6	876	F 7 W 8	897	F 8 E 1 $\frac{1}{2}$	958
F 7 E 5 $\frac{1}{2}$	937	F 7 W 8 $\frac{1}{2}$	619	F 8 E 2	936
F 7 E 5	857	F 7 W 9	1069	F 8 E 2 $\frac{1}{2}$	975

STATION	VALUE	STATION	VALUE	STATION	VALUE
F 8 E 3	924	F 9 E 4	1034	F 9 W 9½	1431
F 8 E 3½	914	F 9 E 3½	975	F 9 W 10	1273
F 8 E 4	943	F 9 E 3	937	F 10 W 10	1457
F 8 E 4½	953	F 9 E 2½	938	F 10 W 9½	861
F 8 E 5	1012	F 9 E 2	800	F 10 W 9	735
F 8 E 5½	942	F 9 E 1½	761	F 10 W 8½	403
F 8 E 6	932	F 9 E 1	671	F 10 W 8	436
F 8 E 6½	919	F 9 E ½	763	F 10 W 7½	552
F 8 E 7	829	F 9	780	F 10 W 7	553
F 8 E 7½	906	F 9 W ½	726	F 10 W 6½	427
F 8 E 8	881	F 9 W 1	719	F 10 W 6	495
F 8 E 8½	962	F 9 W 1½	704	F 10 W 5½	639
F 8 E 9	992	F 9 W 2	618	F 10 W 5	620
F 8 E 9½	1032	F 9 W 2½	643	F 10 W 4½	601
F 8 E 10	1077	F 9 W 3	596	F 10 W 4	662
F 9 E 10	995	F 9 W 3½	656	F 10 W 3½	706
F 9 E 9½	928	F 9 W 4	718	F 10 W 3	730
F 9 E 9	902	F 9 W 4½	653	F 10 W 2½	656
F 9 E 8½	926	F 9 W 5	639	F 10 W 2	719
F 9 E 8	963	F 9 W 5½	550	F 10 W 1½	794
F 9 E 7½	968	F 9 W 6	514	F 10 W 1	974
F 9 E 7	941	F 9 W 6½	665	F 10 W ½	795
F 9 E 6½	1010	F 9 W 7	734	F 10	728
F 9 E 6	1078	F 9 W 7½	581	F 10 E ½	763
F 9 E 5½	1067	F 9 W 8	1063	F 10 E 1	735
F 9 E 5	997	F 9 W 8½	1183	F 10 E 1½	900
F 9 E 4½	1033	F 9 W 9	1054	F 10 E 2	1030

STATION	VALUE	STATION	VALUE	STATION	VALUE
F 10 E 2½	954	F 11 E 5	939	F 11 W 9	-25
F 10 E 3	941	F 11 E 4½	984	F 11 W 9½	1049
F 10 E 3½	1003	F 11 E 4	986	F 11 W 10	1850
F 10 E 4	1014	F 11 E 3½	1040	F 11 W 10½	763
F 10 E 4½	974	F 11 E 3	982	F 11 W 11	946
F 10 E 5	968	F 11 E 2½	976	F 11 W 11½	1043
F 10 E 5½	986	F 11 E 2	934	F 11 W 12	1226
F 10 E 6	864	F 11 E 1	924	F 11 W 12½	1026
F 10 E 6½	1009	F 11 E ½	922	F 11 W 13	863
F 10 E 7	993	F 11	869	F 11 W 13½	1038
F 10 E 7½	934	F 11 W ½	863	F 11 W 14	1160
F 10 E 8	889	F 11 W 1	865	F 11 W 14½	1573
F 10 E 8½	957	F 11 W 1½	831	F 11 W 15	1321
F 10 E 9	941	F 11 W 2	829	F 11 W 15½	1412
F 10 E 9½	965	F 11 W 2½	751	F 11 W 16	1658
F 10 E 10	1023	F 11 W 3	785	F 11 W 16½	1470
F 10 E 10½	1023	F 11 W 3½	727	F 11 W 17	1095
F 11 E 10	991	F 11 W 4	729	F 11 W 17½	1030
F 11 E 9½	1067	F 11 W 4½	863	F 11 W 18	1128
F 11 E 9	1050	F 11 W 5	674	F 11 W 18½	1195
F 11 E 8½	1014	F 11 W 5½	676	F 11 W 19	1226
F 11 E 8	1133	F 11 W 6	594	F 11 W 19½	1229
F 11 E 7½	1010	F 11 W 6½	624	F 11 W 20	1248
F 11 E 7	1017	F 11 W 7	542	F 12 W 17	1386
F 11 E 6½	1013	F 11 W 7½	508	F 12 W 16	1333
F 11 E 6	1037	F 11 W 8	318	F 12 W 15	1197
F 11 E 5½	1084	F 11 W 8½	315	F 12 W 14	1467

STATION	VALUE	STATION	VALUE	STATION	VALUE
F 12 W 13	1151	F 12 E 8	1099	G 27-8 $\frac{1}{2}$	2291
F 12 W 12	1011	F 12 E 7	1216	G 27-9	3046
F 12 W 11 $\frac{1}{2}$	584	F 12 E 6	1020	G 27-9 $\frac{1}{2}$	3105
F 12 W 11	312	F 12 E 5	1053	G 27-10	1834
F 12 W 10 $\frac{1}{2}$	367	F 12 E 4 $\frac{1}{2}$	1061	G 27-10 $\frac{1}{2}$	2105
F 12 W 10	179	F 12 E 4	1023	G 27-11	1812
F 12 W 9 $\frac{1}{2}$	341	F 12 E 3	945	G 17	1692
F 12 W 9	310	F 12 E 2	966	G 17 S $\frac{1}{2}$	1450
F 12 W 8 $\frac{1}{2}$	404	F 12 E 1	1000	G 17 S 1	1190
F 12 W 8	532	F 12	1024	G 17 S 1 $\frac{1}{2}$	1358
F 12 W 7 $\frac{1}{2}$	590	G 27	1173	G 17 S 2	1372
F 12 W 7	596	G 27- $\frac{1}{2}$	1063	G 17 S 2 $\frac{1}{2}$	1404
F 12 W 6 $\frac{1}{2}$	761	G 27-1	643	G 17 S 3	1329
F 12 W 6	683	G 27-1 $\frac{1}{2}$	1847	G 17 S 3 $\frac{1}{2}$	1280
F 12 W 5 $\frac{1}{2}$	785	G 27-2	566	G 17 S 4	1269
F 12 W 5	799	G 27-2 $\frac{1}{2}$	1116	G 17 S 4 $\frac{1}{2}$	1240
F 12 W 4 $\frac{1}{2}$	809	G 27-3	2330	G 17 S 5	1225
F 12 W 4	847	G 27-3 $\frac{1}{2}$	2103	G 17 S 5 $\frac{1}{2}$	1253
F 12 W 3 $\frac{1}{2}$	857	G 27-4	1108	G 17 S 6	1200
F 12 W 3	883	G 27-4 $\frac{1}{2}$	1921	G 17 S 6 $\frac{1}{2}$	1170
F 12 W 2 $\frac{1}{2}$	902	G 27-5	1368	G 17 S 7	1186
F 12 W 2	961	G 27-5 $\frac{1}{2}$	841	G 17 S 7 $\frac{1}{2}$	1115
F 12 W 1 $\frac{1}{2}$	1079	G 27-6	1051	G 17 S 8	1149
F 12 W 1	832	G 27-6 $\frac{1}{2}$	1927	G 17 S 8 $\frac{1}{2}$	1122
F 12 W $\frac{1}{2}$	982	G 27-7	2651	G 17 S 9	1160
F 12 E 10	1230	G 27-7 $\frac{1}{2}$	2626	G 17 S 9 $\frac{1}{2}$	1141
F 12 E 9	1263	G 27-8	3584	G 17 S 10	1137

STATION	VALUE	STATION	VALUE	STATION	VALUE
G 17 S 11	1119	G 18 N 9	1539	G 18 S 3	1612
G 17 S 12	1144	G 18 N 9½	1864	G 18 S 3½	1503
G 17 S 13	1166	G 18 N 10	1476	G 18 S 4	1434
G 17 S 14	1173	G 17 N 10	831	G 18 S 4½	1415
G 17 S 15	1180	G 17 N 9½	1008	G 18 S 5	1358
G 17 S 16	1175	G 17 N 9	1670	G 18 S 6	1255
G 17 S 17	1178	G 17 N 8½	964	G 18 S 7	1229
G 17 S 18	1184	G 17 N 8	1110	G 18 S 8	1245
G 17 S 19	1235	G 17 N 7½	1138	G 18 S 9	1192
G 17 S 20	1290	G 17 N 7	1059	G 18 S 10	1190
G 18	2105	G 17 N 6½	915	G 19 S 10	1214
G 18 N ½	3460	G 17 N 6	904	G 19 S 9	1218
G 18 N 1	2872	G 17 N 5½	802	G 19 S 8	1242
G 18 N 1½	2852	G 17 N 5	979	G 19 S 7	1255
G 18 N 2	2922	G 17 N 4½	964	G 19 S 6	1298
G 18 N 2½	2477	G 17 N 4	893	G 19 S 5	1344
G 18 N 3	2156	G 17 N 3½	1222	G 19 S 4½	1329
G 18 N 3½	2429	G 17 N 3	1571	G 19 S 4	1402
G 18 N 4	2855	G 17 N 2½	1190	G 19 S 3½	1440
G 18 N 4½	2620	G 17 N 2	1202	G 19 S 3	1483
G 18 N 5	1954	G 17 N 1½	2525	G 19 S 2½	1590
G 18 N 5½	2953	G 17 N 1	3535	G 19 S 2	1575
G 18 N 6	1683	G 17 N ½	2336	G 19 S 1½	1983
G 18 N 6½	1860	G 18 S ½	1770	G 19 S 1	1667
G 18 N 7	2144	G 18 S 1	1752	G 19 S ½	1896
G 18 N 7½	2053	G 18 S 1½	1657	G 19	1903
G 18 N 8	1772	G 18 S 2	1638	G 19 N ½	2036
G 18 N 8½	1590	G 18 S 2½	1982	G 19 N 1	1906

STATION	VALUE	STATION	VALUE	STATION	VALUE
G 19 N 1 $\frac{1}{2}$	1684	G 20 N 5 $\frac{1}{2}$	2466	G 21 S 9	1171
G 19 N 2	1454	G 20 N 5	2732	G 21 S 8	1145
G 19 N 2 $\frac{1}{2}$	2221	G 20 N 4 $\frac{1}{2}$	2634	G 21 S 7 $\frac{1}{2}$	1123
G 19 N 3	2092	G 20 N 4	3120	G 21 S 7	1129
G 19 N 3 $\frac{1}{2}$	2523	G 20 N 3 $\frac{1}{2}$	3090	G 21 S 6	1267
G 19 N 4	2046	G 20 N 3	2940	G 21 S 5	1389
G 19 N 4 $\frac{1}{2}$	2241	G 20 N 2 $\frac{1}{2}$	3588	G 21 S 4	1431
G 19 N 5	2140	G 20 N 2	3562	G 21 S 3	1537
G 19 N 5 $\frac{1}{2}$	2015	G 20 N 1 $\frac{1}{2}$	2260	G 21 S 2 $\frac{1}{2}$	1675
G 19 N 6	2277	G 20 N 1	2547	G 21 S 2	1874
G 19 N 6 $\frac{1}{2}$	2032	G 20 N $\frac{1}{2}$	2326	G 21 S 1 $\frac{1}{2}$	1781
G 19 N 7	1630	G 20	1785	G 21 S 1	1952
G 19 N 7 $\frac{1}{2}$	1808	G 20 S $\frac{1}{2}$	1808	G 21 S $\frac{1}{2}$	2675
G 19 N 8	1862	G 20 S 1	1614	G 21	2934
G 19 N 8 $\frac{1}{2}$	1924	G 20 S 1 $\frac{1}{2}$	1640	G 21 S 11	1103
G 19 N 9	2382	G 20 S 2	1594	G 21 S 12	1115
G 19 N 9 $\frac{1}{2}$	2404	G 20 S 2 $\frac{1}{2}$	1512	G 21 S 13	1172
G 19 N 10	1826	G 20 S 3	1422	G 21 S 14	1156
G 20 N 10	1436	G 20 S 3 $\frac{1}{2}$	1372	G 21 S 15	1160
G 20 N 9 $\frac{1}{2}$	2474	G 20 S 4	1372	G 21 S 16	1241
G 20 N 9	2108	G 20 S 5	1274	G 21 S 17	1208
G 20 N 8 $\frac{1}{2}$	1942	G 20 S 6	1220	G 21 S 18	1285
G 20 N 8	3032	G 20 S 7	1342	G 21 S 19	1309
G 20 N 7 $\frac{1}{2}$	1750	G 20 S 8	1276	G 21 S 20	1285
G 20 N 7	2168	G 20 S 9	1122	G 22 S 10	1039
G 20 N 6 $\frac{1}{2}$	2274	G 20 S 10	1120	G 22 S 9	1067
G 20 N 6	2484	G 21 S 10	1134	G 22 S 8	1096

STATION	VALUE	STATION	VALUE	STATION	VALUE
G 22 S 7	1391	G 22 N 7	2726	G 23 S 9½	1026
G 22 S 6	1445	G 22 N 7½	2806	G 23 S 8½	1079
G 22 S 5½	1361	G 22 N 8	2211	G 23 S 7½	1115
G 22 S 5	1687	G 22 N 8½	2396	G 23 S 6½	1099
G 22 S 4½	1366	G 22 N 9	2333	G 23 S 5½	1200
G 22 S 4	1481	G 22 N 9½	2250	G 23 S 4½	1220
G 22 S 3½	1531	G 22 N 10	2551	G 23 S 3½	1341
G 22 S 3	1804	G 21 N 10	2283	G 23 S 2½	1510
G 22 S 2½	1919	G 21 N 9½	2224	G 23 S 2	1595
G 22 S 2	1751	G 21 N 9	2295	G 23 S 1½	1735
G 22 S 1½	1806	G 21 N 8½	2374	G 23 S 1	1628
G 22 S 1	1820	G 21 N 8	2675	G 23 S ½	2033
G 22 S ½	1947	G 21 N 7½	1905	G 23	2267
G 22	2240	G 21 N 7	3390	G 24 S 10	1029
G 22 N ½	2066	G 21 N 6½	2463	G 24 S 9	1043
G 22 N 1	2430	G 21 N 6	2743	G 24 S 8	1090
G 22 N 1½	3523	G 21 N 5½	1934	G 24 S 7	1680
G 22 N 2	3312	G 21 N 5	2002	G 24 S 6	1245
G 22 N 2½	2071	G 21 N 4½	1997	G 24 S 5½	1186
G 22 N 3	2427	G 21 N 4	2271	G 24 S 5	1530
G 22 N 3½	1927	G 21 N 3½	3199	G 24 S 4½	1284
G 22 N 4	2793	G 21 N 3	4677	G 24 S 4	1277
G 22 N 4½	2919	G 21 N 2½	2736	G 24 S 3½	1336
G 22 N 5	3368	G 21 N 2	2073	G 24 S 3	1336
G 22 N 5½	3103	G 21 N 1½	2697	G 24 S 2½	1651
G 22 N 6	2651	G 21 N 1	2558	G 24 S 2	1648
G 22 N 6½	2939	G 21 N ½	2806	G 24 S 1½	1655

STATION	VALUE	STATION	VALUE	STATION	VALUE
G 24 S 1	1726	G 23 N 8 $\frac{1}{2}$	3370	G 25 N 5	2262
G 24 S $\frac{1}{2}$	1761	G 23 N 8	4001	G 25 N 5 $\frac{1}{2}$	1863
G 24	1889	G 23 N 7 $\frac{1}{2}$	2829	G 25 N 6	3028
G 24 N $\frac{1}{2}$	1928	G 23 N 7	3256	G 25 N 6 $\frac{1}{2}$	3202
G 24 N 1	2162	G 23 N 6 $\frac{1}{2}$	1542	G 25 N 7	3226
G 24 N 1 $\frac{1}{2}$	2638	G 23 N 6	2242	G 25 N 7 $\frac{1}{2}$	2738
G 24 N 2	2342	G 23 N 5 $\frac{1}{2}$	1154	G 25 N 8	2746
G 24 N 2 $\frac{1}{2}$	2674	G 23 N 5	2320	G 25 N 8 $\frac{1}{2}$	3382
G 24 N 3	1623	G 23 N 4 $\frac{1}{2}$	1511	G 25 N 9	3405
G 24 N 3 $\frac{1}{2}$	2525	G 23 N 4	2281	G 25 N 9 $\frac{1}{2}$	2667
G 24 N 4	2012	G 23 N 3 $\frac{1}{2}$	2239	G 25 N 10	2245
G 24 N 4 $\frac{1}{2}$	2053	G 23 N 3	2981	G 26 N 10	3377
G 24 N 5	2409	G 23 N 2 $\frac{1}{2}$	1972	G 26 N 9 $\frac{1}{2}$	2572
G 24 N 5 $\frac{1}{2}$	3995	G 23 N 2	2730	G 26 N 9	2613
G 24 N 6	5505	G 23 N 1 $\frac{1}{2}$	2713	G 26 N 8 $\frac{1}{2}$	1915
G 24 N 6 $\frac{1}{2}$	3201	G 23 N 1	2659	G 26 N 8	3642
G 24 N 7	2450	G 23 N $\frac{1}{2}$	2446	G 26 N 7 $\frac{1}{2}$	1697
G 24 N 7 $\frac{1}{2}$	2595	G 25	1486	G 26 N 7	1974
G 24 N 8	2152	G 25 N $\frac{1}{2}$	1587	G 26 N 6 $\frac{1}{2}$	3050
G 24 N 8 $\frac{1}{2}$	2215	G 25 N 1	1667	G 26 N 6	2896
G 24 N 9	1883	G 25 N 1 $\frac{1}{2}$	1800	G 26 N 5 $\frac{1}{2}$	2417
G 24 N 9 $\frac{1}{2}$	1832	G 25 N 2	1880	G 26 N 5	2210
G 24 N 10	1459	G 25 N 2 $\frac{1}{2}$	2322	G 26 N 4 $\frac{1}{2}$	3193
G 23 N 10 $\frac{1}{2}$	4288	G 25 N 3	3047	G 26 N 4	3096
G 23 N 10	3156	G 25 N 3 $\frac{1}{2}$	3253	G 26 N 3 $\frac{1}{2}$	5025
G 23 N 9 $\frac{1}{2}$	3472	G 25 N 4	2255	G 26 N 3	2508
G 23 N 9	3160	G 25 N 4 $\frac{1}{2}$	2790	G 26 N 2 $\frac{1}{2}$	1988

STATION	VALUE	STATION	VALUE	STATION	VALUE
G 26 N 2	1719	G 25 S 2	1289	G 27 S 0 $\frac{1}{2}$	369
G 26 N 1 $\frac{1}{2}$	1713	G 25 S 3	1217	G 27 S 9	381
G 26 N 1	1572	G 25 S 4	1121	G 27 S 9 $\frac{1}{2}$	446
G 26 N $\frac{1}{2}$	1466	G 25 S 5	1064	G 27 S 10	477
G 26	1389	G 25 S 6	1061	H Paso	1067
G 27	1122	G 25 S 7	1029	H 8	869
G 27 N $\frac{1}{2}$	1219	G 25 S 8	1022	H 8 N $\frac{1}{2}$	1256
G 27 N 1	1418	G 25 S 9	1043	H 8 N 1	1667
G 27 N 1 $\frac{1}{2}$	1801	G 25 S 10	1028	H 8 N 1 $\frac{1}{2}$	1623
G 27 N 2	2114	G 26 S 10	957	H 8 N 2	1657
G 27 N 2 $\frac{1}{2}$	1959	G 26 S 9	951	H 8 N 2 $\frac{1}{2}$	1519
G 27 N 3	1948	G 26 S 8	965	H 8 N 3	15
G 27 N 3 $\frac{1}{2}$	1928	G 26 S 7	971	H 8 N 3 $\frac{1}{2}$	2204
G 27 N 4	1903	G 26 S 6	1079	H 8 N 4	3325
G 27 N 4 $\frac{1}{2}$	1848	G 26 S 5	1016	H 8 N 4 $\frac{1}{2}$	3363
G 27 N 5	1892	G 26 S 4	1095	H 8 N 5	3283
G 27 N 5 $\frac{1}{2}$	1904	G 26 S 3	1121	H 8 N 5 $\frac{1}{2}$	1444
G 27 N 6	2517	G 26 S 2	1317	H 8 N 6	-555
G 27 N 6 $\frac{1}{2}$	1617	G 26 S 1	1310	H 8 N 6 $\frac{1}{2}$	3514
G 27 N 7	1691	G 27 S 1	926	H 8 N 7	2105
G 27 N 7 $\frac{1}{2}$	1829	G 27 S 2	767	H 8 N 7 $\frac{1}{2}$	2564
G 27 N 8	2630	G 27 S 3	792	H 8 N 8	2708
G 27 N 8 $\frac{1}{2}$	2801	G 27 S 4	613	H 8 N 8 $\frac{1}{2}$	4046
G 27 N 9	1669	G 27 S 5	483	H 8 N 9	2558
G 27 N 9 $\frac{1}{2}$	1884	G 27 S 6	402	H 8 N 9 $\frac{1}{2}$	2576
G 27 N 10	1751	G 27 S 7	333	H 8 N 10	1605
G 25 S 1	1373	G 27 S 8	341	H 9 N 10	4833

STATION	VALUE	STATION	VALUE	STATION	VALUE
H 9 W 9½	1564	H 8 E 5½	890	H 10 W 4	1376
H 9 W 9	2276	H 8 E 6½	950	H 10 W 4½	1000
H 9 W 8½	2192	H 8 E 7½	1088	H 10 W 5	2216
H 9 W 8	1635	H 8 E 8½	973	H 10 W 5½	2246
H 9 W 7½	2537	H 8 E 9½	1038	H 10 W 6	3174
H 9 W 7	2284	H 8 E 10	1025	H 10 W 6½	829
H 9 W 6½	2367	H 9 E 10	1029	H 10 W 7	645
H 9 W 6	3148	H 9 E 9	1012	H 10 W 7½	1041
H 9 W 5½	2537	H 9 E 8	999	H 10 W 8	2240
H 9 W 5	-806	H 9 E 7	990	H 10 W 8½	1024
H 9 W 4½	2691	H 9 E 6	966	H 10 W 9	2001
H 9 W 4	3380	H 9 E 5	977	H 10 W 9½	3533
H 9 W 3½	3653	H 9 E 4	932	H 10 W 10	1305
H 9 W 3	2229	H 9 E 3	879	H 11 W 10	1144
H 9 W 2½	1718	H 9 E 2½	802	H 11 W 9½	693
H 9 W 2	2174	H 9 E 2	581	H 11 W 9	419
H 9 W 1½	1729	H 9 E 1½	296	H 11 W 8½	1435
H 9 W 1	1233	H 9 E 1	909	H 11 W 8	1621
H 9 W ½	2874	H 9 E ½	2850	H 11 W 7½	1193
H 9	1955	H 10	1035	H 11 W 7	970
H 8 E ½	2159	H 10 W ½	1764	H 11 W 6½	1491
H 8 E 1	787	H 10 W 1	2407	H 11 W 6	2089
H 8 E 1½	599	H 10 W 1½	1289	H 11 W 5½	1810
H 8 E 2	376	H 10 W 2	3122	H 11 W 5	2497
H 8 E 2½	387	H 10 W 2½	2174	H 11 W 4½	3942
H 8 E 3½	781	H 10 W 3	3402	H 11 W 4	3431
H 8 E 4½	853	H 10 W 3½	1991	H 11 W 3½	1387

STATION	VALUE	STATION	VALUE	STATION	VALUE
H 11 W 3	2147	H 11 E 2	1171	H 12 W 1	1230
H 11 W 2½	2677	H 11 E 1½	1119	H 12 W 1½	1413
H 11 W 2	3085	H 11 E 1	1114	H 12 W 2	1500
H 11 W 1½	1926	H 11 E ½	1065	H 12 W 2½	3332
H 11 W 1	1316	H 12	1044	H 12 W 3	2529
H 11 W ½	1002	H 12 E 1	1173	H 12 W 3½	2361
H 11	1395	H 12 E 2	1324	H 12 W 4	2138
H 10 E ¾	917	H 12 E 3	1319	H 12 W 4½	1202
H 10 E 1	961	H 12 E 4	1364	H 12 W 5	3107
H 10 E 1½	1021	H 12 E 5	1336	H 12 W 5½	2275
H 10 E 2	1097	H 12 E 6	1344	H 12 W 6	2872
H 10 E 3	1104	H 12 E 7	1344	H 12 W 6½	1996
H 10 E 4	1103	H 12 E 8	1697	H 12 W 7	2773
H 10 E 5	1138	H 12 E 9	1311	H 12 W 7½	189
H 10 E 6	1117	H 12 E 10	1336	H 12 W 8	2602
H 10 E 7	1128	H 13 E 10	1376	H 12 W 8½	1202
H 10 E 8	1168	H 13 E 9	1384	H 12 W 9	1119
H 10 E 9	1106	H 13 E 8	1445	H 12 W 9½	2175
H 10 E 10	1121	H 13 E 7	1709	H 12 W 10	1896
H 11 E 10	1242	H 13 E 6	1502	H 13 W 10	1316
H 11 E 9	1351	H 13 E 5	1531	H 13 W 9½	1545
H 11 E 8	1208	H 13 E 4	1661	H 13 W 9	1089
H 11 E 7	1247	H 13 E 3	1518	H 13 W 8½	2190
H 11 E 6	1380	H 13 E 2	1490	H 13 W 8	1686
H 11 E 5	1253	H 13 E 1	1458	H 13 W 7½	1963
H 11 E 4	1256	H 13	1425	H 13 W 7	2648
H 11 E 3	1238	H 12 W ½	1168	H 13 W 6½	1528

STATION	VALUE	STATION	VALUE	STATION	VALUE
H 13 W 6	1905	H 14 W 7 $\frac{1}{2}$	977	H 15 E 1 $\frac{1}{2}$	1386
H 13 W 5 $\frac{1}{2}$	4313	H 14 W 8	1566	H 15	1434
H 13 W 5	2510	H 14 W 8 $\frac{1}{2}$	1211	H 15 W 1	1611
H 13 W 4 $\frac{1}{2}$	2410	H 14 W 9	796	H 15 W 1 $\frac{1}{2}$	542
H 13 W 4	823	H 14 W 9 $\frac{1}{2}$	902	H 15 W 2	900
H 13 W 3 $\frac{1}{2}$	3279	H 14 W 10	948	H 15 W 2 $\frac{1}{2}$	697
H 13 W 3	2252	H 14 E 1	1334	H 15 W 3	3627
H 13 W 2 $\frac{1}{2}$	1776	H 14 E 2	1668	H 15 W 3 $\frac{1}{2}$	2158
H 13 W 2	1821	H 14 E 3	1762	H 15 W 4	1103
H 13 W 1 $\frac{1}{2}$	1369	H 14 E 4	1684	H 15 W 4 $\frac{1}{2}$	1135
H 13 W 1	1266	H 14 E 5	2226	H 15 W 5	689
H 13 W $\frac{1}{2}$	1234	H 14 E 6	1832	H 15 W 5 $\frac{1}{2}$	1553
H 14	1526	H 14 E 7	1937	H 15 W 6	754
H 14 W $\frac{1}{2}$	1416	H 14 E 8	1602	H 15 W 6 $\frac{1}{2}$	778
H 14 W 1	1662	H 14 E 9	1965	H 15 W 7	1254
H 14 W 1 $\frac{1}{2}$	828	H 14 E 10	1600	H 15 W 7 $\frac{1}{2}$	890
H 14 W 2	1930	H 15 E 10	1591	H 15 W 8	911
H 14 W 2 $\frac{1}{2}$	3668	H 15 E 9	1918	H 15 W 8 $\frac{1}{2}$	363
H 14 W 3	1711	H 15 E 8	1946	H 15 W 9	1109
H 14 W 3 $\frac{1}{2}$	1390	H 15 E 7	1861	H 15 W 9 $\frac{1}{2}$	569
H 14 W 4	2489	H 15 E 6	1717	H 15 W 10	907
H 14 W 4 $\frac{1}{2}$	1628	H 15 E 5	2228	H 16 W 10	1206
H 14 W 5	1975	H 15 E 4 $\frac{1}{2}$	1603	H 16 W 9 $\frac{1}{2}$	1375
H 14 W 5 $\frac{1}{2}$	926	H 15 E 4	1563	H 16 W 9	1255
H 14 W 6	873	H 15 E 3	1814	H 16 W 8 $\frac{1}{2}$	1323
H 14 W 6 $\frac{1}{2}$	936	H 15 E 2	1944	H 16 W 8	1504
H 14 W 7	1203	H 15 E 1	1404	H 16 W 7 $\frac{1}{2}$	1234

STATION	VALUE	STATION	VALUE	STATION	VALUE
H 16 W 7	1071	H 17 E 9	1736	H 17 W 9	2810
H 16 W 6½	2283	H 17 E 8	1676	H 17 W 9½	1950
H 16 W 6	2892	H 17 E 7	1687	H 17 W 10	1757
H 16 W 5½	2110	H 17 E 6	1729	C 9	1041
H 16 W 5	2219	H 17 E 5	1599	C 10	1089
H 16 W 4½	1331	H 17 E 4	1547	C 11	1126
H 16 W 4	1963	H 17 E 3	1522	C 13	1198
H 16 W 3½	415	H 17 E 2	1713	C 14	1230
H 16 W 3	823	H 17 E ½	2010	C 15	1201
H 16 W 2½	911	H 17	1684	C 16	1212
H 16 W 2	1455	H 17 W ½	2443	C 17	1229
H 16 W 1½	2767	H 17 W 1	2588	C 18	1268
H 16 W 1	2492	H 17 W 1½	3551	C 19	1276
H 16 W ½	2518	H 17 W 2	1731	C 20	1263
H 16	3098	H 17 W 2½	2777	C 21	1312
H 16 E ½	1752	H 17 W 3	2054	C 22	1267
H 16 E 1	1571	H 17 W 3½	1504	C 23	1262
H 16 E 2	1480	H 17 W 4	968	C 24	1311
H 16 E 3	1526	H 17 W 4½	1142	C 25	1351
H 16 E 4	1713	H 17 W 5	1190	C 26	1488
H 16 E 5	1547	H 17 W 5½	1038	C 27	1497
H 16 E 6	1597	H 17 W 6	1035	C 28	1354
H 16 E 7	1600	H 17 W 6½	2514	C 29	1646
H 16 E 8	1575	H 17 W 7	519	C 30	1402
H 16 E 9	1606	H 17 W 7½	1943	C 31	1503
H 16 E 10	1589	H 17 W 8	1744	C 32	1417
H 17 E 10	1792	H 17 W 8½	2094	C 33	1416

STATION	VALUE	STATION	VALUE	STATION	VALUE
C 34	1518	C 61	1339	K 22 E 6 $\frac{1}{2}$	1452
C 35	1516	C 62	1336	K 22 E 7	1482
C 36	1464	C 63	1363	K 22 E 7 $\frac{1}{2}$	1464
C 37	1488	C 64	1336	K 22 E 8	1474
C 38	1480	C 65	1384	K 22 E 8 $\frac{1}{2}$	1524
C 39	1464	C 66	1384	K 22 E 9	1642
C 40	1473	C 67	1432	K 22 E 9 $\frac{1}{2}$	1528
C 41	1431	C 68	1436	K 22 E 10	1518
C 42	1349	C 69	1460	K 23 E 10	1504
C 43	1435	C 70	1464	K 23 E 9 $\frac{1}{2}$	1506
C 44	1347	C 71	1492	K 23 E 9	1504
C 45	1131	C 72	1484	K 23 E 8 $\frac{1}{2}$	1506
C 46	1164	C 73	1600	K 23 E 8	1492
C 47	1111	C 74	1548	K 23 E 7 $\frac{1}{2}$	1474
C 48	1320	K 22	1540	K 23 E 7	1520
C 49	1234	K 22 E $\frac{1}{2}$	1378	K 23 E 6 $\frac{1}{2}$	1483
C 50	1181	K 22 E 1	1447	K 23 E 6	1494
C 51	1226	K 22 E 1 $\frac{1}{2}$	1344	K 23 E 5 $\frac{1}{2}$	1497
C 52	1125	K 22 E 2	1409	K 23 E 5	1452
C 53	1174	K 22 E 2 $\frac{1}{2}$	1410	K 23 E 4 $\frac{1}{2}$	1459
C 54	1150	K 22 E 3	1523	K 23 E 4	1466
C 55	1162	K 22 E 3 $\frac{1}{2}$	1500	K 23 E 3 $\frac{1}{2}$	1464
C 56	1144	K 22 E 4	1493	K 23 E 3	1457
C 57	1166	K 22 E 4 $\frac{1}{2}$	1430	K 23 E 2 $\frac{1}{2}$	1450
C 58	1237	K 22 E 5	1427	K 23 E 2	1433
C 59	1247	K 22 E 5 $\frac{1}{2}$	1536	K 23 E 1 $\frac{1}{2}$	1504
C 60	1269	K 22 E 6	1574	K 23 E 1	1507

STATION	VALUE	STATION	VALUE	STATION	VALUE
K 23 E ½	1518	K 25 E 8	1571	K 26 E 4	1668
K 23	1525	K 25 E 7½	1579	K 26 E 4½	1669
K 24	1502	K 25 E 7	1631	K 26 E 5	1889
K 24 E ½	1500	K 25 E 6½	1627	K 26 E 5½	1909
K 24 E 1	1494	K 25 E 6	1607	K 26 E 6	1977
K 24 E 1½	1484	K 25 E 5½	1554	K 26 E 6½	2064
K 24 E 2	1554	K 25 E 5	1534	K 26 E 7	1599
K 24 E 2½	2040	K 25 E 4½	1510	K 26 E 7½	1640
K 24 E 3	1518	K 25 E 4	1506	K 26 E 8	1660
K 24 E 3½	1513	K 25 E 3½	1514	K 26 E 8½	1669
K 24 E 4	1512	K 25 E 3	1537	K 26 E 9	1674
K 24 E 4½	1487	K 25 E 2½	1617	K 26 E 9½	1679
K 24 E 5	1494	K 25 E 2	1509	K 26 E 10	1700
K 24 E 5½	1485	K 25 E 1½	1501	K 27 E 10	1761
K 24 E 6	1528	K 25 E 1	2205	K 27 E 9½	1747
K 24 E 6½	1931	K 25 E ½	2268	K 27 E 9	1706
K 24 E 7	1814	K 25	1640	K 27 E 8½	1657
K 24 E 7½	1494	K 26	1530	K 27 E 8	1620
K 24 E 8	1505	K 26 W ½	1592	K 27 E 7½	1618
K 24 E 8½	1537	K 26 W 1	1625	K 27 E 7	1961
K 24 E 9	1521	K 26 E ½	1704	K 27 E 6½	1810
K 24 E 9½	1525	K 26 E 1	1615	K 27 E 6	1816
K 24 E 10	1516	K 26 E 1½	1569	K 27 E 5½	1763
K 25 E 10	1600	K 26 E 2	1597	K 27 E 5	1707
K 25 E 9½	1608	K 26 E 2½	1606	K 27 E 4½	2131
K 25 E 9	1654	K 26 E 3	1662	K 27 E 4	1592
K 25 E 8½	1568	K 26 E 3½	1659	K 27 E 3½	1744

STATION	VALUE	STATION	VALUE	STATION	VALUE
K 27 E 3	1738	K 21 E 1 $\frac{1}{2}$	1419	N 10-E	1521
K 27 E 2 $\frac{1}{2}$	1744	K 21 E 2	1375	N 10-9	1507
K 27 E 2	1750	K 21 E 2 $\frac{1}{2}$	1405	N 10-10	1552
K 27 E 1 $\frac{1}{2}$	1756	K 21 E 3	1342	N 10-11	1589
K 27 E 1	1773	K 21 E 3 $\frac{1}{2}$	1349	N 10-12	1604
K 27 E $\frac{1}{2}$	1729	K 21 E 4	1371	N 10-13	1654
K 27	1715	K 21 E 4 $\frac{1}{2}$	1401	N 10-14	1684
K 27 W $\frac{1}{2}$	1705	K 21 E 5	1369	N 10-15	1690
K 27 W 1	1692	K 21 E 5 $\frac{1}{2}$	1325	L 10-15	1516
K 27 W 1 $\frac{1}{2}$	1755	L 21 E 6	1351	L 10-14	1521
K 27 W 2	1752	K 21 E 6 $\frac{1}{2}$	1393	L 10-13	1508
K 27 W 2 $\frac{1}{2}$	1724	K 21 E 7	1412	L 10-12	1487
K 27 W 3	1640	K 21 E 7 $\frac{1}{2}$	1458	L 10-11	1473
K 27 W 3 $\frac{1}{2}$	1634	K 21 E 8 $\frac{1}{2}$	1476	L 10-10	1490
K 27 W 4	1627	K 21 E 9 $\frac{1}{2}$	1487	L 10-9	1506
K 27 W 4 $\frac{1}{2}$	1620	K 21 E 10	1475	L 10-8	1442
K 27 W 5	1617	N 10	1452	L 10-7	1561
K 27 W 5 $\frac{1}{2}$	1598	N 10- $\frac{1}{2}$	1488	L 10-6	1485
K 27 W 6	1564	N 10-1	1516	L 10-5	1432
K 27 W 7	1687	N 10-1 $\frac{1}{2}$	1498	L 10-4	1446
K 27 W 7 $\frac{1}{2}$	1654	N 10-2	1585	L 10-3	1432
K 27 W 8	1636	N 10-2 $\frac{1}{2}$	1491	L 10-2	1450
K 27 W 8 $\frac{1}{2}$	1584	N 10-3	1442	L 10-1	1461
K 27 W 9	1582	N 10-3 $\frac{1}{2}$	1455	L 10	1452
K 27 W 10	1570	N 10-4	1480	N 17 S 5	878
K 21	1406	N 10-5	1513	N 17 S 4 $\frac{1}{2}$	871
K 21 E $\frac{1}{2}$	1726	N 10-6	1532	N 17 S 4	892
K 21 E 1	1686	N 10-7	1519	N 17 S 3 $\frac{1}{2}$	893

STATION	VALUE	STATION	VALUE	STATION	VALUE
M 17 S 3	992	M 16	1131	M 15 N 3	1048
M 17 S 2½	871	M 16 S ½	1058	M 15 N 3½	1056
M 17 S 2	927	M 16 S 1	1001	M 15 N 4	1055
M 17 S 1½	936	M 16 S 1½	979	M 15 N 4½	1055
M 17 S 1	933	M 16 S 2	927	M 15 N 5	1047
M 17 S ½	1052	M 16 S 2½	922	M 14 N 5	1066
M 17	892	M 16 S 3	929	M 14 N 4½	1086
M 17 N ½	940	M 16 S 3½	994	M 14 N 4	1039
M 17 N 1	953	M 16 S 4	1036	M 14 N 3½	1062
M 17 N 1½	997	M 16 S 4½	870	M 14 N 3	1066
M 17 N 2	1029	M 16 S 5	903	M 14 N 2½	1043
M 17 N 2½	1152	M 15 S 5	960	M 14 N 2	1023
M 17 N 3	1071	M 15 S 4½	943	M 14 N 1½	1011
M 17 N 3½	1005	M 15 S 4	954	M 14 N 1	894
M 17 N 4	1116	M 15 S 3½	945	M 14 N ½	1106
M 17 N 4½	1105	M 15 S 3	901	M 14	988
M 17 N 5	1047	M 15 S 2½	920	M 14 S ½	906
M 16 N 5	1048	M 15 S 2	934	M 14 S 1	1015
M 16 N 4½	1073	M 15 S 1½	972	M 14 S 1½	960
M 16 N 4	1109	M 15 S 1	983	M 14 S 2	960
M 16 N 3½	1063	M 15 S ½	1100	M 14 S 2½	910
M 16 N 3	1060	M 15	1024	M 14 S 3	898
M 16 N 2½	1082	M 15 N ½	1278	M 14 S 3½	933
M 16 N 2	993	M 15 N 1	31	M 14 S 4	941
M 16 N 1½	971	M 15 N 1½	928	M 14 S 4½	880
M 16 N 1	1007	M 15 N 2	1010	M 14 S 5	980
M 16 N ½	979	M 15 N 2½	993	M 13 S 5	933

STATION	VALUE	STATION	VALUE	STATION	VALUE
M 13 S 4 $\frac{1}{2}$	937	M 11 N 1 $\frac{1}{2}$	1048	M 10 N 2	1103
M 13 S 4	964	M 11 N 1	1044	M 10 N 2 $\frac{1}{2}$	1142
M 13 S 3 $\frac{1}{2}$	988	M 11 N $\frac{1}{2}$	1032	M 10 N 3	1114
M 13 S 3	1015	M 11	1071	M 10 N 3 $\frac{1}{2}$	1102
M 13 S 2 $\frac{1}{2}$	991	M 11 S $\frac{1}{2}$	956	M 10 N 4	1148
M 13 S 2	959	M 11 S 1	968	M 10 N 4 $\frac{1}{2}$	1145
M 13 S 1 $\frac{1}{2}$	1018	M 11 S 1 $\frac{1}{2}$	968	M 10 N 5	1147
M 13 S 1	956	M 11 S 2	992	P 14	1046
M 13 S $\frac{1}{2}$	963	M 11 S 2 $\frac{1}{2}$	988	P 15	992
M 13	1046	M 11 S 3	980	P 15 W 1	943
M 13 N $\frac{1}{2}$	975	M 11 S 3 $\frac{1}{2}$	967	P 15 W 2	933
M 13 N 1	1018	M 11 S 4 $\frac{1}{2}$	936	P 15 W 3	891
M 13 N 1 $\frac{1}{2}$	1030	M 11 S 5	955	P 15 W 4	869
M 13 N 2	995	M 10 S 5	939	P 15 W 5	936
M 13 N 2 $\frac{1}{2}$	1081	M 10 S 4 $\frac{1}{2}$	935	P 15 W 6	852
M 13 N 3	1064	M 10 S 4	929	P 15 W 7	876
M 13 N 3 $\frac{1}{2}$	1041	M 10 S 3 $\frac{1}{2}$	1030	P 15 W 8	877
M 13 N 4	1053	M 10 S 3	969	P 15 W 9	886
M 13 N 4 $\frac{1}{2}$	1064	M 10 S 2 $\frac{1}{2}$	1027	P 15 W 10	1022
M 13 N 5	1049	M 10 S 2	1005	P 14 W 10	861
M 11 N 5	1076	M 10 S 1 $\frac{1}{2}$	1016	P 14 W 9	921
M 11 N 4 $\frac{1}{2}$	1119	M 10 S 1	1025	P 14 W 8	859
M 11 N 4	1123	M 10 S $\frac{1}{2}$	1017	P 14 W 7	935
M 11 N 3 $\frac{1}{2}$	1104	M 10	1096	P 14 W 6	908
M 11 N 3	1075	M 10 N $\frac{1}{2}$	1013	P 14 W 5	957
M 11 N 2 $\frac{1}{2}$	1067	M 10 N 1	1064	P 14 W 4	1045
M 11 N 2	1063	M 10 N 1 $\frac{1}{2}$	1080	P 14 W 3	1002

STATION	VALUE	STATION	VALUE	STATION	VALUE
F 14 E 2	1067	G 23½ N 2	3183	G 23½ N 15½	1739
F 14 W 1	1072	G 23½ N 2½	3675	G 23½ N 16	1563
F 14	1038	G 23½ N 3	2514	G 23½ N 16½	1672
F 14 E 1	1219	G 23½ N 3½	2347	G 23½ N 17	1725
F 14 E 2	1146	G 23½ N 4	2235	G 23½ N 17½	1805
F 14 E 3	1150	G 23½ N 4½	2926	G 23½ N 18	1914
F 14 E 4	1256	G 23½ N 5	2798	G 23½ N 18½	2117
F 14 E 5	1186	G 23½ N 5½	3454	G 23½ N 19	2178
F 14 E 6	1236	G 23½ N 6	2818	G 23½ N 19½	1943
F 14 E 7	1344	G 23½ N 6½	1851	G 23½ N 20	2111
F 14 E 8	1147	G 23½ N 7	1552	G 24½ N 10	2341
F 14 E 9	1302	G 23½ N 7½	1061	G 24½ N 9½	2536
F 14 E 9½	1327	G 23½ N 8	1575	G 24½ N 9	2144
F 15 E 10	1209	G 23½ N 8½	1321	G 24½ N 8½	2438
F 15 E 9	1162	G 23½ N 9	1138	G 24½ N 8	2369
F 15 E 8	1247	G 23½ N 9½	1335	G 24½ N 7½	2879
F 15 E 7	1117	G 23½ N 10	1759	G 24½ N 7	3608
F 15 E 6	1142	G 23½ N 10½	1993	G 24½ N 6½	2354
F 15 E 5	1092	G 23½ N 11	2042	G 24½ N 6	2084
F 15 E 4	1118	G 23½ N 11½	2052	G 24½ N 5½	2460
F 15 E 3	1109	G 23½ N 12	1558	G 24½ N 5	2489
F 15 E 2	1048	G 23½ N 12½	1792	G 24½ N 4½	1757
F 15 E 1	1047	G 23½ N 13	1837	G 24½ N 4	2359
G 23½	2163	G 23½ N 13½	2217	G 24½ N 3½	2795
G 23½ N ½	2189	G 23½ N 14	2562	G 24½ N 3	2806
G 23½ N 1	2270	G 23½ N 14½	2202	G 24½ N 2½	1808
G 23½ N 1½	2606	G 23½ N 15	1839	G 24½ N 2	1853

STATION	VALUE	STATION	VALUE	STATION	VALUE
G 24½ N 1½	1853	G 18½ N 9½	2121	G 17½ N 10½	1303
G 24½ N 1	1825	G 18½ N 10	2033	G 17½ N 10	1303
G 24½ N ½	1753	G 19 N 10	1723	G 17½ N 9½	1567
G 24½	1606	G 19 N 10½	2306	G 17½ N 9	1624
G 18½	1938	G 19 N 11	1778	G 17½ N 8½	1446
G 18½ S ½	1909	G 19 N 11½	1511	G 17½ N 8	2004
G 18½ S 1	1768	G 19 N 12	1692	G 17½ N 7½	1305
G 18½ S 1½	1641	G 19 N 12½	1678	G 17½ N 7	1685
G 18½ S 2	1582	G 19 N 13	1268	G 17½ N 6½	1471
G 18½ N ½	2583	G 19 N 13½	1584	G 17½ N 6	1485
G 18½ N 1	3480	G 19 N 14	1770	G 17½ N 5½	1448
G 18½ N 1½	2789	G 19 N 14½	1733	G 17½ N 5	1555
G 18½ N 2	2745	G 19 N 15	1668	G 17½ N 4½	1785
G 18½ N 2½	2972	F 6 W 14½	1600	G 17½ N 4	2304
G 18½ N 3	2069	F 6 W 14	1527	G 17½ N 3½	2600
G 18½ N 3½	2534	F 6 W 13½	1556	G 17½ N 3	2386
G 18½ N 4	2075	F 6 W 13	1374	G 17½ N 2½	2455
G 18½ N 4½	2399	F 6 W 12½	1164	G 17½ N 2	2978
G 18½ N 5	2667	F 6 W 12	1111	G 17½ N 1½	3579
G 18½ N 5½	2042	F 6 W 11½	1258	G 17½ N 1	3691
G 18½ N 6	1300	F 6 W 11	1323	G 17½ N ½	2325
G 18½ N 6½	1494	F 6 W 10½	1415	G 17½	2021
G 18½ N 7	1504	F 6 W 10	1619	G 17½ S ½	1610
G 18½ N 7½	1569	G 17½ N 12½	1470	G 17½ S 1	1449
G 18½ N 8	2124	G 17½ N 12	1613	G 17½ S 1½	1408
G 18½ N 8½	2862	G 17½ N 11½	1572	G 17½ S 2	1363
G 18½ N 9	2386	G 17½ N 11	1460	G 17½ S 2½	1325

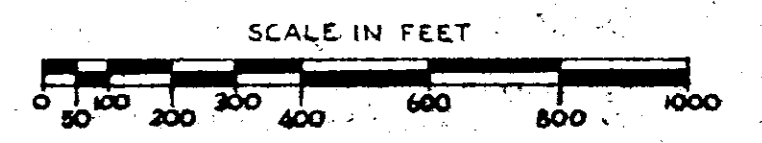
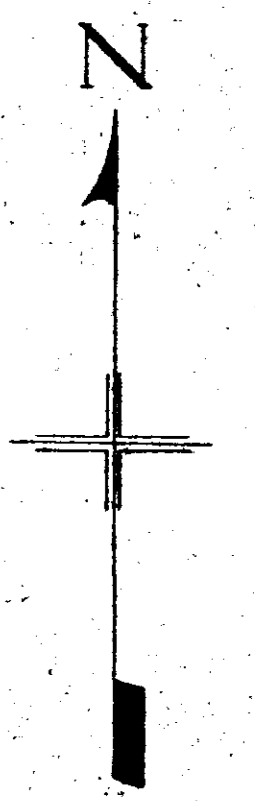
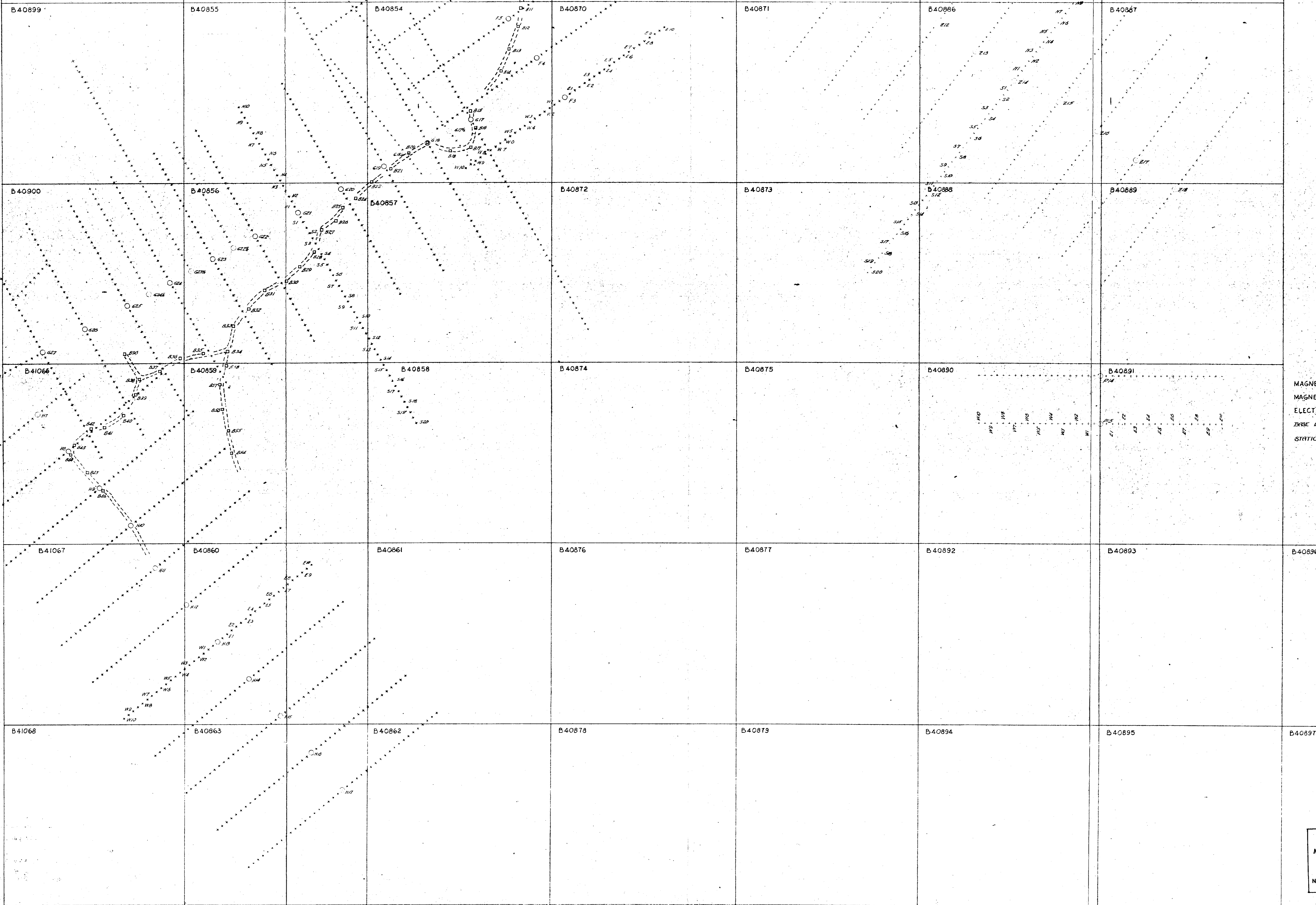
STATION	VALUE	STATION	VALUE	STATION	VALUE
Z 17 1/2 S 3	2304	Z 10 S 3	933	Z 12 N 7	1163
Z 10 N 1	-304	Z 10 S 4	931	Z 12 N 8	1325
Z 10 N 1 1/2	778	Z 10 S 5	1019	Z 12 N 9	1338
Z 10 N 2	1043	Z 10 S 6	935	Z 12 N 10	1217
Z 10 N 3	986	Z 10 S 7	866	Z 13 N 10	1238
Z 10 N 4	1133	Z 10 S 8	888	Z 13 N 9	1184
Z 10 N 5	1119	Z 10 S 9	792	Z 13 N 8	1197
Z 10 N 6	1148	Z 10 S 10	793	Z 13 N 7	1206
Z 10 N 7	1150	Z 11 S 10	831	Z 13 N 6	1207
Z 10 N 8	1202	Z 11 S 9	806	Z 13 N 5	1189
Z 10 N 9	1319	Z 11 S 8	856	Z 13 N 4	1203
Z 10 N 10	1200	Z 11 S 7	819	Z 13 N 3	1119
Z 11 N 10	1258	Z 11 S 6	888	Z 13 N 2	1161
Z 11 N 9	1222	Z 11 S 5	1038	Z 13 N 1	1138
Z 11 N 8	1205	Z 11 S 4	939	Z 13	1168
Z 11 N 7	1176	Z 11 S 3	931	Z 12 S 1	983
Z 11 N 6	1140	Z 11 S 2	1016	Z 12 S 2	922
Z 11 N 5	1166	Z 11 S 1	995	Z 12 S 3	987
Z 11 N 4	1087	Z 11	943	Z 12 S 4	974
Z 11 N 3	1070	Z 11 N 1/2	1005	Z 12 S 5	958
Z 11 N 2	1030	Z 12	1039	Z 12 S 6	960
Z 11 N 1	1036	Z 12 N 1	1228	Z 12 S 7	895
Z 10 N 1/2	885	Z 12 N 2	1123	Z 12 S 8	928
Z 10 N 3/4	9317	Z 12 N 3	1112	Z 12 S 9	852
Z 10	911	Z 12 N 4	1129	Z 12 S 10	838
Z 10 S 1	956	Z 12 N 5	1114	Z 13 S 10	852
Z 10 S 2	982	Z 12 N 6	1151	Z 13 S 9	873

STATION	VALUE	STATION	VALUE	STATION	VALUE
Z 13 S 9	906	Z 14 S 4	1100	Z 16 S 9	1156
Z 13 S 7	972	Z 14 S 4 $\frac{1}{2}$	1118	Z 16 S 10	1081
Z 13 S 6	1042	Z 14 S 5	1138	Z 15 S 10	966
Z 13 S 5	958	Z 14 S 6	1059	Z 15 S 9	1040
Z 13 S 4	996	Z 14 S 7	1010	Z 15 S 8	1010
Z 13 S 3	1011	Z 14 S 8	965	Z 15 S 7	1054
Z 13 S 2	1045	Z 14 S 9	956	Z 15 S 6	1016
Z 13 S 1	970	Z 14 S 10	925	Z 15 S 5	1063
Z 14	1143	Z 14 S 11	917	Z 15 S 4	1092
Z 14 N 1	1120	Z 14 S 12	893	Z 15 S 3	1175
Z 14 N 2	1192	Z 14 S 13	875	Z 15 S 2	1105
Z 14 N 3	1201	Z 14 S 14	763	Z 15 S 1	1147
Z 14 N 4	1229	Z 14 S 15	801	Z 15	1116
Z 14 N 4 $\frac{1}{2}$	1297	Z 14 S 16	810	Z 15 S $\frac{1}{2}$	1173
Z 14 N 5	1222	Z 14 S 17	777	Z 15 N 1	1073
Z 14 N 5 $\frac{1}{2}$	1211	Z 14 S 18	740	Z 15 N 2	1110
Z 14 N 6	1103	Z 14 S 19	730	Z 15 N 3	1148
Z 14 N 7	1308	Z 14 S 20	733	Z 15 N 4	1139
Z 14 N 8	1177	Z 16	1156	Z 15 N 5	1113
Z 14 N 7 $\frac{1}{2}$	1226	Z 16 S 1	1365	Z 15 S 6	1233
Z 14 N 8 $\frac{1}{2}$	1321	Z 16 S 2	1173	Z 15 N 7	1184
Z 14 N 9	1127	Z 16 S 3	1174	Z 15 N 8	1065
Z 14 N 9 $\frac{1}{2}$	1211	Z 16 S 4	1267	Z 15 N 9	1137
Z 14 N 10	1174	Z 16 S 5	1155	Z 15 N 10	1166
Z 14 S 1	1118	Z 16 S 6	1165	Z 16 N 1	1104
Z 14 S 2	1198	Z 16 S 7	1135	Z 16 N 2	1114
Z 14 S 3	1102	Z 16 S 8	1118	Z 16 N 3	1163

STATION	VALUE	STATION	VALUE	STATION	VALUE
Z 16 N 4	1098	Z 16	1195	G 27 x 4	3166
Z 16 N 5	1104	Z 18 S 1	1171	G 27 x 4 <sub>2</sub>	1996
Z 16 N 6	1164	Z 18 S 2	1250	H 7 S1	974
Z 16 N 7	1202	Z 18 S 3	1216	H 7 S 1 $\frac{1}{2}$	3128
Z 16 N 8	1200	Z 18 S 4	1268	H 7 S 2	-220
Z 16 N 9	1178	Z 18 S 5	1270	H 7 S 2 $\frac{1}{2}$	-80
Z 16 N 10	1141	Z 18 S 6	1280	H 7 S 3	420
Z 17	1122	Z 18 S 7	1277	H 7 S 3 $\frac{1}{2}$	658
Z 17 N 1	1126	Z 18 S 8	1247	H 7 S 4	720
Z 17 N 2	1176	Z 18 S 9	1212	H 7 S 4 $\frac{1}{2}$	844
Z 17 N 3	1132	Z 18 S 10	1217	H 7 S 5	906
Z 17 N 4	1190	Z 17 S 10	1105	H 7 S $\frac{1}{2}$	2748
Z 17 N 5	1155	Z 17 S 9	1172	H 7	1033
Z 17 N 6	1133	Z 17 S 8	1173	H 7 S $\frac{1}{4}$	817
Z 17 N 7	1177	Z 17 S 7	1190	H 7 W 1	636
Z 17 N 8	1190	Z 17 S 6	1148	H 7 W 1 $\frac{1}{2}$	3638
Z 17 N 9 $\frac{1}{2}$	1199	Z 17 S 5	1161	H 7 W 2	2712
Z 17 N 10	1612	Z 17 S 4	1162	H 7 W 2 $\frac{1}{2}$	778
Z 18 N 10	1228	Z 17 S 3	1218	H 7 W 3	1884
Z 18 N 9	1246	Z 17 S 2	1152	Z 17 S 3 $\frac{1}{2}$	3745
Z 18 N 8	1198	Z 17 S 1	1181	H 7 W 4	1148
Z 18 N 7	1167	G 27 x 2	2100	H 7 W 4 $\frac{1}{2}$	1987
Z 18 N 6	1103	G 27 x 1	2023	H 7 W 5	2003
Z 18 N 5	1089	G 27 x 1 $\frac{1}{2}$	2928	A 14 N 1 $\frac{1}{2}$	3553
Z 18 N 4	1115	G 27 x 2	2476	A 14 N 1	3722
Z 18 S 3	1279	G 27 x 2 $\frac{1}{2}$	1910	A 14 N 3/4	4292
Z 18 S 2	1211	G 27 x 3	2239	A 14 N $\frac{1}{2}$	3751
Z 18 S 1	1181	G 27 x 3 $\frac{1}{2}$	3004	A 14	

STATION	VALUE	STATION	VALUE	STATION	VALUE
A 14 S 2	2418	B 44	1581		
B 10	802	B 45	2360		
B 11	667				
B 12	673				
B 13	798				
B 14	823				
B 15	1739				
B 16	1604				
B 17	1463				
B 18	1598				
B 19	2219				
B 20	2164				
B 22	1861				
B 23	1733				
B 25	1622				
B 26	1718				
B 27	1515				
B 29	1822				
B 30	1364				
B 33	1127				
B 35	1205				
B 37	1095				
B 38	1022				
B 39	1067				
B 40	895				
B 41	748				
B 42	512				
B 43	1545				



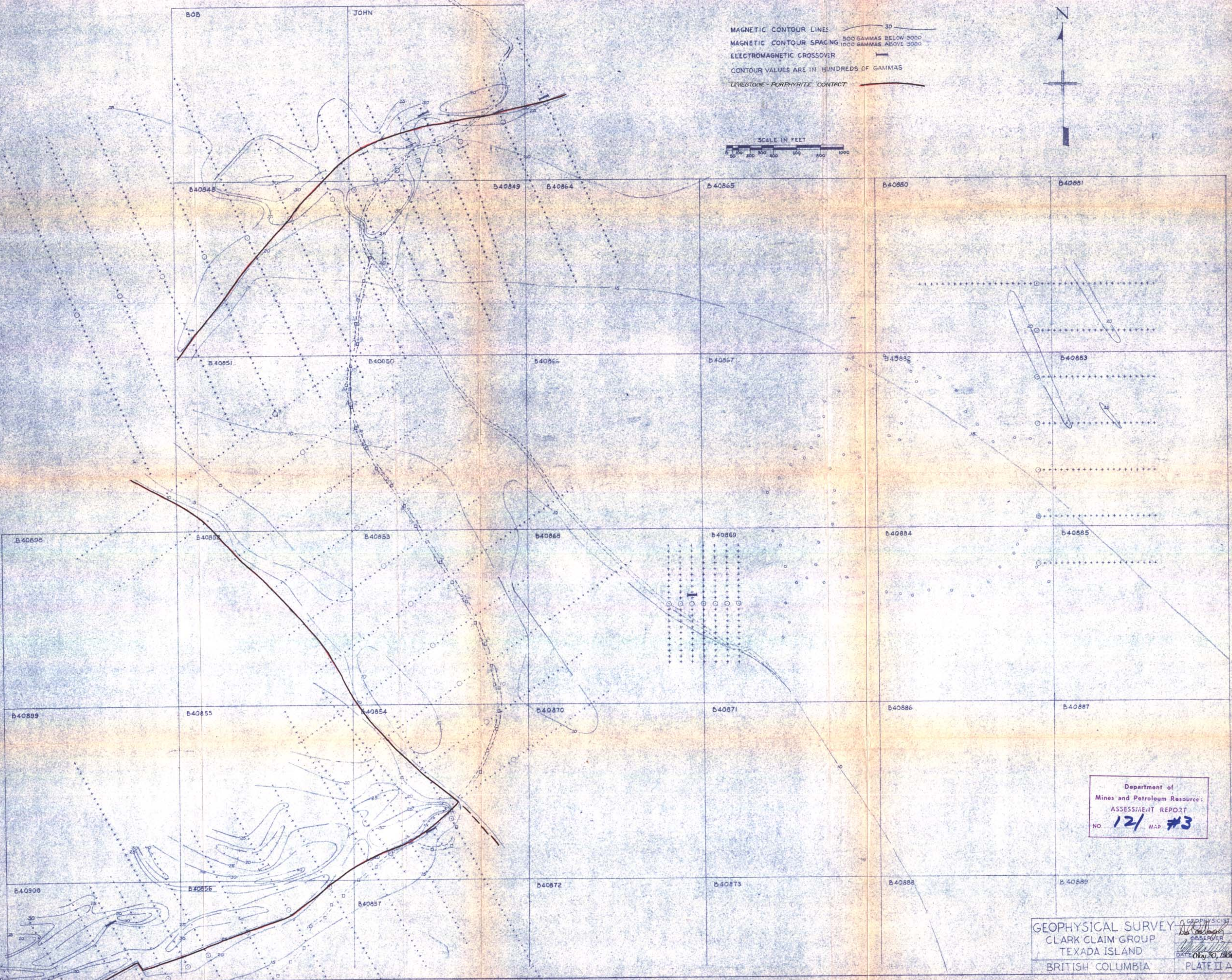


MAGNETIC CONTOUR LINES } SEE PLATE II  
 MAGNETIC CONTOUR SPACING }  
 ELECTROMAGNETIC CROSSOVER }  
 BORE HOLE STATIONS    O  
 STATIONS                    +

Department of  
 Mines and Petroleum Resources  
 ASSESSMENT REPORT  
 NO. 121 MAP #2

GEOPHYSICAL SURVEY  
 CLARK CLAIM GROUPS  
 TEXADA ISLAND  
 BRITISH COLUMBIA

GEOPHYSICIST  
 OBSERVER  
 DATE July 30, 1956  
 PLATE I B



MAGNETIC CONTOUR LINES 30  
 MAGNETIC CONTOUR SPACING 500 GAMMAS BELOW 3000  
 1000 GAMMAS ABOVE 3000  
 ELECTROMAGNETIC CROSSOVER  
 CONTOUR VALUES ARE IN HUNDREDS OF GAMMAS  
 LIMESTONE-PORPHYRITE CONTACT

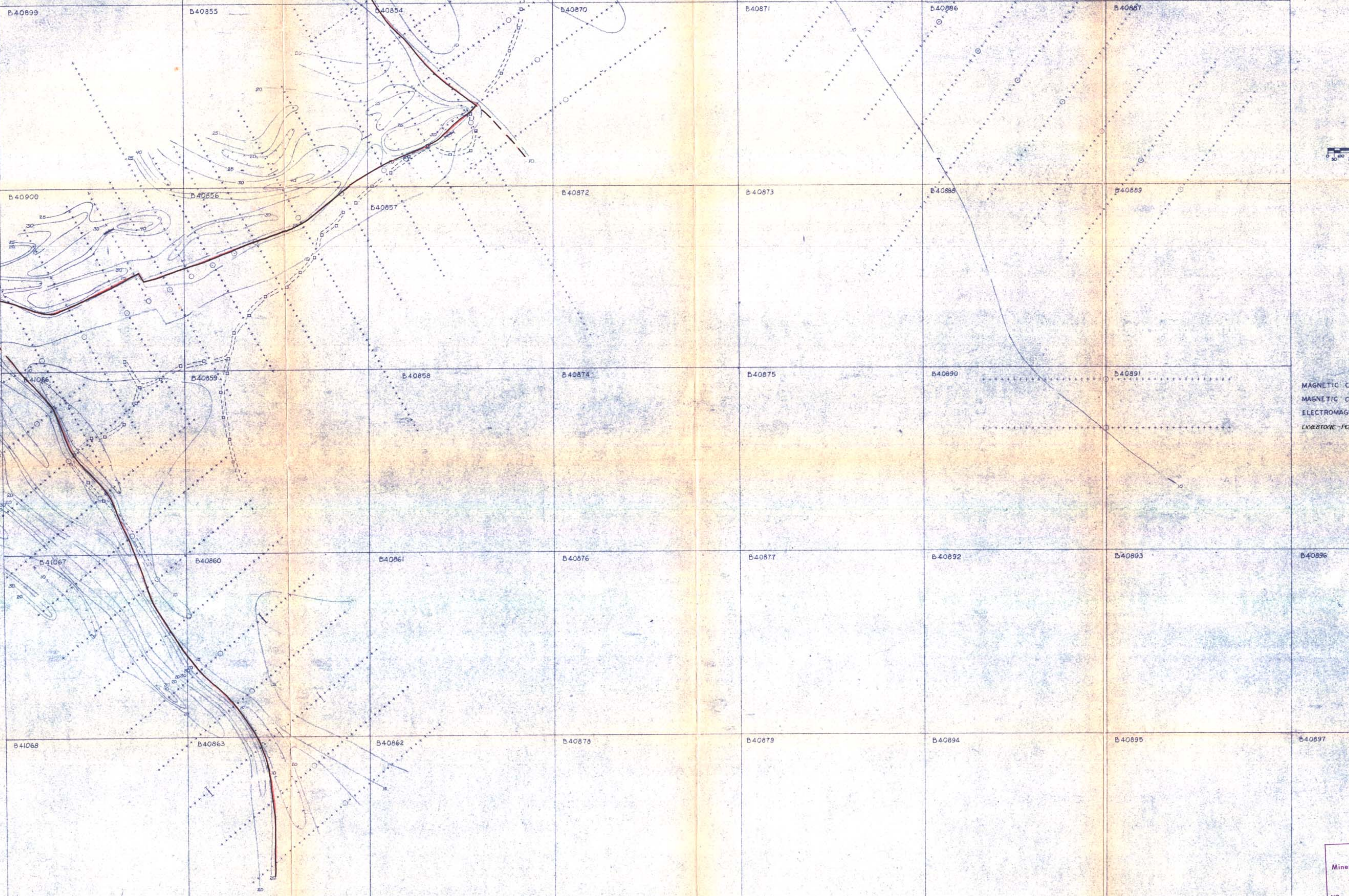
SCALE IN FEET  
 0 100 200 300 400 500 600 700 800 900 1000



Department of  
 Mines and Petroleum Resources  
 ASSESSMENT REPORT  
 NO. 121 MAP #3

GEOPHYSICAL SURVEY  
 CLARK CLAIM GROUP  
 TEXADA ISLAND  
 BRITISH COLUMBIA

GEOPHYSICIST  
 OBSERVER  
 DATE (May 20, 1966)  
 PLATE II A

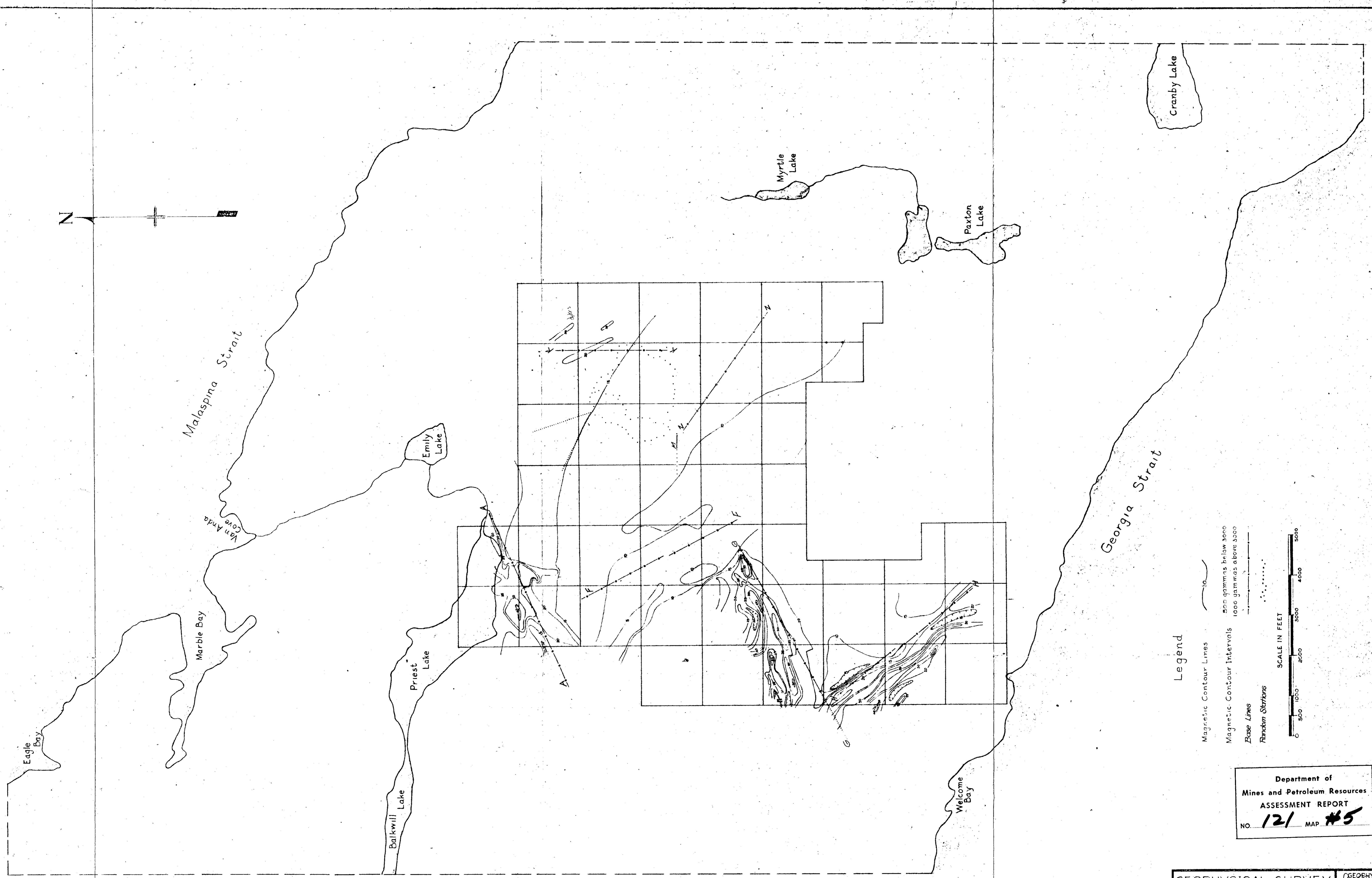


MAGNETIC CONTOUR LINES 30  
MAGNETIC CONTOUR SPACING 300 GAUSS BELOW 3000,  
1000 GAUSS ABOVE 3000  
ELECTROMAGNETIC CROSSOVER  
LIMESTONE-PORPHYRITE CONTACT

Department of  
Mines and Petroleum Resources  
ASSESSMENT REPORT  
NO. 121 MAP #4

GEOPHYSICAL SURVEY  
CLARK CLAIM GROUPS  
TEXADA ISLAND  
BRITISH COLUMBIA

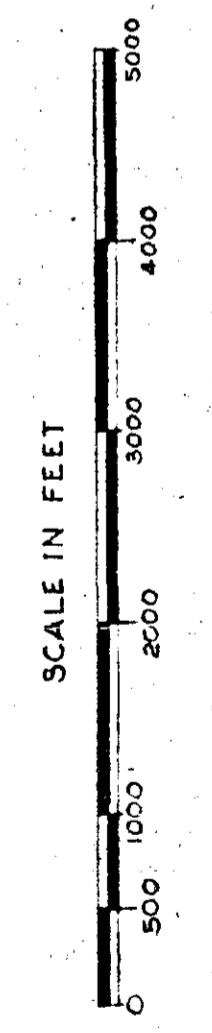
GEOPHYSICIST  
OBSERVER  
DATE May 30, 1966  
PLATE II B



Legend

- Magnetic Contour Lines —
- Magnetic Contour Intervals - - -
- Base Lines — · — · — ·
- Random Striations · · · · ·

500 gammas below 3000  
1000 gammas above 3000



Department of  
Mines and Petroleum Resources  
ASSESSMENT REPORT  
NO. 121 MAP #5

GEOPHYSICAL SURVEY  
CLARK CLAIM GROUPS  
TEXADA ISLAND  
BRITISH COLUMBIA

GEOPHYSICIST  
OBSERVER  
DATE May 31, 1958  
PLATE III