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INDUCED POLARIZATION SURVEY for

NEW WELLINGTON MINES LTD.

MENARD CREEK PROJECT

Induced Polarization Survey WARMOT GROUP 56 30-50"Ith:126°20-45"West G.A. Noutitsen, esq.

(Geofax Surveys Ltd).

NEW WELLINGTON MINES UTD. 21 Sept - 6 Oct. 1966.



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INDUCED POLARIZATION SURVEY for NEW WELLINGTON MINES LTD.

MENARD CREEK PROJECT

GEOFAX SURVEYS LTD.

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G. A. Mouritsen, Senior Geophysicist



October, 1966.

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TABLE OF CONTENTS

1

INTRODUCTION	1
CONCLUSIONS & RECOMMENDATIONS	1
RECOMMENDATIONS	2
PROPERTY LOCATION AND ACCESS	2
METHOD OF SURVEY and INSTRUMENT DATA	3
I.P. Instrument	3
I.P. Electrode Array	4
I.P. Data	5
DISCUSSION OF RESULTS	5

APPENDIX

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List of Personnel

POCKET ENCLOSURES

2 Plot of Chargeability & Resistivity Profiles

-Field Reports

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INTRODUCTION

During the dates of September 21st and October 6th, 1966, an induced polarization survey was carried out for New Wellington Mines Ltd. on their Menard Creek, B.C. property. The survey was contracted by Geofax Surveys Ltd. of Calgary, Alberta. In addition to the dates above, 8 days crew mobilization were required to get the crew to the property from Calgary, and from the property to Ft. St. James, B.C. (see Property Location & Access). The survey crew quartered in a camp supplied by New Wellington Mines Ltd. During the dates of actual survey operations given above, 4 operating days were lost due to camp move and 1 day was lost due to atmospherics. During the survey, 258 readings were attempted, of which 142 were reliable; the remainder were rendered unreliable by telluric currents, atmospherics and experimentation for proper electrode spacing.

CONCLUSIONS & RECOMMENDATIONS

Please see the plots of the Chargeability and Resistivity Profiles.

The induced polarization survey revealled 4 Primary Zones and 3 Secondary Zones described as follows (see Legend accompanying Profiles).

- 1. A Primary Zone on Line 1 lying near the 3200 W station and probably extending westward beyond control.
- 2. A Primary Zone on Line 1 lying near or between the 2900 W and the 3100W stations. This may be the east dipping counterpart of the Primary Zone described in (1) above.
- 3. A Primary Zone on Line 1 lying near or between the 150 E station and the 50W station. This anomaly is sparsely controlled, but appears to be dipping west.
- 4. A Primary Zone on Line 2 lying near or at the 3000 W station. This anomaly may be common to the Primary Zones lying at the west end of Line 1 as described above in (1) and (2).
- 5. A Secondary Zone (see Legend) extending from the 2250 W to the 2500 W station on Line 1. This zone is deeply buried (at least 600 feet) and may prove out as a target for the future.

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- 6. A narrow Secondary Zone at or near the 1100W station on Line 1. This minor anomaly requires further I.P. detail.
- 7. A secondary Zone extending west from the Primary Zone at the 3000 W station on Line 2. The mineralization here is also buried at least 600 feet deep and may not be economical as a prime target. More extensive I. P. control here may prove this theory wrong.
- 8. Minor mineralization on surface appears to be present along nearly the full extent of Line 2 except from the 1300 W to the 1700 W stations. This minor mineralization may be due to float or talus containing scattered minerals.

RECOMMENDATIONS

In the above conclusions, the zones of interest were described as lying near a certain distance. Where an anomalous condition is indicated on one line control only, the anomaly may lie to either side of the station or below it. Such anomalies require detail lines on either side to give lateral extent and a more fixed position. Integration of the surface geology with the I.P. survey results leaves the conclusions subject to change.

If further I.P. surveys are anticipated in the future, it is respectfully recommended that a line be placed between Line 1 and Line 2 from the 2200 W distance to at least the 3600 W distance. Electrode spacing of 400 and 600 feet should be used.

The anomaly at the 00 to 100 E station on Line 1 should be detailed with a line parallel to and north of Line 1 from the 500 W to the 400 E stations. Electrode spacings of 200 and 400 or possibly 600 should be used to determine dip. If the detail lines fail to pick up the anomalies, new lines should be placed closer to the existing lines.

PROPERTY LOCATION AND ACCESS

The property is located approximately 220 miles NNW

- 2 -

of Fort St James in the Omineca Mining Division of B C. The survey crew travelled from Calgary to Fort St. James via Wagoneer Jeep Wagon, from Fort St. James to McConnell Lake by plane on the third day, from McConnell Lake to McConnell Creek by bulldozer on the fourth day, from McConnell Creek to Grant's field by bulldozer on the fifth day and from Grant's field to Menard Creek camp by bulldozer on the sixth day.

Transportation from camp to the survey site was by bulldozer daily, requiring two hours up to the site and 1-3/4 hours return in the evening. To alleviate this extensive travel time, the camp was moved to a new location during operations. This move required 4 days.

Demobilization from the property required two days, the first spent moving from Menard Creek to Moose Valley by bulldozer. The second day the crew was taken from Moose Valley by helicopter to Thorn Lake to Takla Landing, and thence by plane to Fort St. James, B.C.

METHOD OF SURVEY and INSTRUMENT DATA

I.P. Instrument

The instrument used was a new Huntec pulse-type system capable of delivering 2500 watts to the ground. The system is composed of 3 sub-systems: a generator, a transmitter and a receiver. The generator provides the source of prime power for the transmitter which produces a rectangular current pulse to the ground. The cycling rate is 1.5 seconds "current on" and 0.5 seconds "current off"; succeeding pulses are of opposite polarity. The receiver operates remotely and is triggered by the decay of the transmitter current. The readings for the primary potential Vp and secondary potential Vs are taken by the null balance method with the input

- 3 -

signal balanced over a period of time to reduce noise effects. The main advantages of the pulse type system over the variable frequency type system are, 1. Any electrode spacing may be used, whereas the spacings used on variable frequency systems are restricted, due to inductive coupling between transmitter and receiver circuits. 2. Less time is required to take each reading as no average is required.

I.P. Electrode Array

Please see the Legend accompanying the Chargeability and Resistivity Profiles.

The lines were surveyed using a normal and a special 3-array electrode spacing. The arrays consist of one current electrode (C_1) and two potential electrodes $(P_1 \& P_2)$ which are moved together down the line. The fourth electrode (C_2) is placed at an "infinite" distance from the other three electrodes (where infinity = 7 to 10a). The electrode distance C_1 to P_1 (a) is determined by the depth to which penetration is required. For example, if the mineralized zone was believed to lie at a depth of 175 to 200 feet below surface with normal ground moisture, a normal 200 foot electrode spacing would be used. If the anticipated depth of burial was 500 to 600 feet and only reconnaissance was required, or the dip of a known anomaly was to be checked, a normal 600 foot electrode spacing would be used. The special 3-array is used when ground conditions are too wet due to rain or snow cover, or the ground is extremely dry so that voltages cannot be compensated or the automatic tripping signal is too weak.

On this project, electrode spacings of 200, 300, 400 and 600 feet normal and special 3-array were used to compensate for changing surface conditions due to float or talus or wet conditions. The varied spacings are differentiated by width of line on the plotted profiles.

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I. P. Data

All I.P. data has been plotted planimetrically on a scale of 1 inch equals 100 feet. The scales for Chargeability (Ma) and Resistivity (Ra) are located at each end of the lines. In the Legend accompanying the profiles, "Background" refers to the lowest average chargeabilities and represents rock which is barren of any disseminated sulphide mineralization. A "Primary Zone" is an anomaly which displays chargeabilities equal to or greater than three times the chargeabilities of the barren rock. A "Secondary Zone'' is an anomaly which displays chargeabilities equal to or greater than two times the background. On the two lines surveyed at Menard Creek, the background chargeabilities average 1 / .4 milliseconds. A Primary Zone, then is represented by chargeabilities of 4 milliseconds or greater and a secondary zone by 2 milliseconds or greater. When designating either type of zone, the increase in chargeability should be corroborated by a rapid decrease in the resistivity. Extreme changes in topography have no bearing whatsoever on the chargeabilities and only a minor relative effect on the resistivities. Topography only affects the chained distances. This could be compensated for by broken chaining or step-chaining.

DISCUSSION OF RESULTS

Please see again the plots of the Chargeability and Resistivity Profiles.

The positions of the Primary and Secondary zones were described under "Conclusions" and need not be reiterated here. The anomalies are fairly well defined and stand out quite clearly above the background. The highest chargeability of 6.9 milliseconds occurred at station 3000 W Line 2 on

- 5 -

the 400 foot spacing. A chargeability of 6.3 milliseconds is noted at the 3250W station on Line 1 on the 300 foot spacing and 6.0 milliseconds at the 100 E station on Line 1. The high readings of 6.9 and 6.3 milliseconds, although on different lines, may represent a common vein or narrow zone of disseminated sulphides. The anomaly on the west end of Line 1 appears to be dipping eastward, as indicated by a relatively fast drop off of readings on the 300 foot spacing but a continuation of relatively high readings on the 600 foot spacing, extending east to the 2700W station. This would indicate the mineralization to be at a depth of approximately 300 feet at the 3250 W station and broadening but dipping to the 600 foot depth at the 2700 station. A rapid decrease in resistivity over the anomaly with a good increase beyond the edge to the east, corroborates the rise in chargeabilities. No increase in resistivity is noted at the extreme west end of the line, suggesting that the I.P. control was not extended far enough west to fully delineate the west edge of the anomaly, where the chargeabilities remain relatively high.

Only one spacing control exists over the Primary Zone at the 100 F to 50 W stations on Line 1. Further detailing with parallel lines are recommended here to further outline this interesting feature.

The Secondary Zones indicated along the lines may prove to be of a lower grade mineralization but may also become Prime Zones after detailing. For the present they should be treated as future or secondary targets to be explored after the Prime Zones. It is noted that the chargeabilities from approximately station 1700 W to 2600 W show a relatively high smooth chargeability plot. This could occur if the line crossed talus or float containing scattered disseminated minerals. True background chargeabilities can be seen at stations 1300 W & 1400 W, Line 2, between stations 500 W & 1000 W and 1200 W and 1700 W on Line 1. The high background resistivities existing

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generally over the central portion of both lines could be the results of talus and float allowing poor electrode to ground contact.

Due to the fine cooperation of the personnel from New Wellington Mines Ltd., reliable results were obtained from a rather difficult survey.

> Respectfully submitted, GEOFAX SURVEYS LTD, 910. Mouritain G. A. Mouritsen, Senior Geophysicist.

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APPENDIX

The following personnel were employed on the survey at Menard Creek:

G. A. Mouritsen	Senior Geophysicist
P.L. Brooks	Party Chief and Chief Operator
T. Lefebure	Operator

and two helpers supplied by New Wellington Mines Ltd.

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Client Representative on the property was Mr. W. D. Savage.

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0400	2	225 *	Mag										
												12.0	
1+00W	0.00	3+001	VIteo	30001	20 K	500	.02	33.5	-3	19.0	-5	22.2	132=
2+000	3	-			IOK	300	2	51.0	-3	25.5	- 5*	20:04	28.80
3 +00W	2				s k	300	. 05	57.0	-3	22.0	-5	15.4	13 (8)
0+00		020 0	723										1
+ ODE	oteo	2400 K	3+00 8		15 k	500	104	127.5	-4	19.0	-5	59.6	366
7+0 0 E					20.6	300	.01	20.0	-3	11.0	-5	24-0	230
3400 E					20 k		. 01	165	-3	8.0	-5		190 190
3400 E					200	300		16.2		010			
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PAGE 182

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3+00E	->				10 K	500	.07	27	-3				
					<u> </u>	300	.04	40	-3				
						300	.02	234	-4	-			
~	cha	to	40	a' a	st.								
3+00 E	->				20K	300	.02						
						500	. 04						-39
						875	.06						
						1250	-1a -11	695	-3	48	-5	27.6	1435 1750
2 700 E					15K	875	.06	4.5	-3				
						875	.08	48.5	-3	37	-5	30.4	11952
1+00E					IOK	875	-#						
						1250	.2		+				
					7K	1750	.34						
		-			IOK	1250	.13						
						1750	.2	168	-3				
0+00					BK	875	18	59	-3	39	-5	26.4	7554
1+00 W					7.5 R	875	.13						
						1250	-22	71	-3	38	- 5	2/.+	6801
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PAGE 342

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STN.	C1	PI	P2	C2	L.R.	TAP, V.	IG	VP	s	Vs	s	MA	RA
0+000	*				20 K	875	.05	41	-3	36	- a	35.1	9401
1+00W					12.K	500	·05						
	6					875	.1						l
						300	.02						19
						500	.07	95	-3	37	- స్	15.5	15400
2700W					5K	300	.08	115	-3	62	-5	21.6.	16501
3700W					4.5 K	300	.09						
					3.9K	200	.15						
					4.5K	875	.25	130	-3	68	5	20.9	598V
4+00W					1K	1250	.20	149	-3	57	-5	15.31	855 V
Stoow			1		IOK	1250	.14	132.5	-3	34	-5	10.5	1085 V
Gtoow					7K	875	.11						
					1	1250	.16	165	-3	28	-5	6197	11850
7+00 W					ZK	1250	.2	262	-3	63	5	9.6	1505 V
8 toow					4.5K	1250	.3						
						875	.25						
						500	.17	218	-3	54	-5	9.9	1475 √
9+00W					15K	1750	.16		43				
						2500	+23	214- 226	-3	53	- 5	9.4	1000
10+00					/3K	2500	.26						

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10+00	w	et.			4K	500	.15						
	-					875	.28	162	3	26	5	6.4	865V
11+20					6.5K	875	121	270	3	13	5	19.3	14800
12338					4K	875	.27						
					3K	500	.2					-	
					1	300	.12	251	PN.	43	5	6.7.	24161
13+00					20 K	1750	. 7/	195	3	44	5	9.1	20.400
14/100					4.5K	500	./4	151	3	3/	5	8.4	12.400
5+00					IOK.	875	13	174	3	57	5	13.1-	15400
16100					15K	1250	.13	216	3	79	5	14.6	1925V
17100					6K	875	18				×		
						500	.14						
						875	.22						
						300	.08			-			
18400					10K	875	+11	1					
		0	bg :	ti	3	05' N	amal.						
17.50				-	61	275	.2						1.15
3 						500	.14	312	3	158	5	20.4	25601
18+50			-		Isk	875		264	3	144	5	21.9	27601
19150		34 			INK.	-875	/3	279	3	153	5	22.1	2,4.70)

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STN.	CI	Pi	P2	C2	L.R.	TAP. V.	la	VP	S	Vs	S	Ma	RA
20150	W	est			14K	1250	•//	120	3	87	2	19.31	18831
21150					8 K.	875	.15		1				
						500	de	205	3	103	5	20.2	2140
22150					ZOK	1750	.11	216	3	106	5	19.6'	22601
23+50					12K	1250	.12	188	3	90	5	19.2	1805/
24450					17K	1750	,13	172	3	69	5	16.10	15200
25+50					12K	1250	.12	159	3	74	5	18.6	1525V
26+50					12K	1250	.13	136	3	63	5	18.50	
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	Line	1	300	HOR	nn2	CALGAR	r, ALBERT	A					
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27+50	Wes	<i>t</i>		_	8K	875	.12						
						500	.08						
				_		1230	18						<u> </u>
						875	.14		1	Tellur	ie e		
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STN.	Ct	Pi	P2	C2	L.R.	TAP. V.	19	VP	5	Vs	5	Ma	RA
27+50	W	ist		÷	IR	500	.04						
					·	875	.18	74	3	39	5	21,3	475 475p
28+50					4.15	500	.16	70	101	24	5	13.74	502.0
29150					3K	300	.12	35	3	13	1.1	14.8	3350
30+50					88	875	++3- ,14						
						500	.09	0					
						875	.14	10	3	11	\boldsymbol{v}_{1}^{i}	4.41	82,0
314 50					7K	875	.16	12	3	10	¢,	3.3	859
32+50					11.K	875	. 08						19
						1250	.12	51	4	8	5	6.3	4890
33+50					15 K	1250	:11			_			
				4 		1750	.15						
						1250	.12						d.
						1750	.17	56	4	.6	5	4.30	
34+50					4.5K	500	.14				_	23.9	3
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	0.02		i cir		1					<u>1766</u>	-		
35700	M	est			12K	875	11	-					
						1250	.16		_				V. 150
						875	12						
						1750	.24	66	4	6	5	3.64	3160
34+00					IK	1750	,20						
						2500	.33	65	ų	9	5	15.52	33.70 -
				200'	No	emal					4	4	X= 96"
344.00					IK		.19	60	4	5	5	3.33	2410
33400					11.15	1250	. 14	75	4	8	ν_1	4.26	\$100
32100					9K	875	.12	107	3	4	5	14.9	6822
31+00					12K	1250	.15				3		
						1750	.20						
					-	875	.16	95	4	6.5	10	2.74	4550
30+00		5		10	6R	500	- 11						
		1				300	.07	57	3	21	4	14.8	6220
29400					4.5K	300	.10						
						500	.17	5	e A	uric	t		
				600	51	Creston	al						
30+00					5K	875	.21	91	4	8.5	5	3.74	1490
31+00					6K	1	-20	1	1/	uRics			

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PAGE R. 42

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STN.	Cı	<u>1</u> Pi	P2	C2	L.R.	TAP. V.	IG	VP	s	Vs	s	Ма	RA
31+00					7K	875	.70	63	4	7	5	4.44	1085
29+00					10K	275	.1						
						500	. 38						
						1750	126						- 115
						2500	-38	76	4	8	5	4.21	645
28+00					2K	1250	.20	93	4	9	5	3.8%	16 40
27400					15K	1750	.18	23	3	19	5	33.1	4415
26+00					15K	1750	.16						
						1250	.14	34	3	14	5	16.5	8370
25+00		_			16K	1250	~17°						
						1750	.16	70	5	41	5	23.4	15050
24+00					15K	1250	.12	73	3	42	5	23.0	1190
23+00					8K	875	+14	68	3	56	12	32.9	14700
22100					16K	1750	14						
				-		1250	,11	Tel	weig	s a h	the	spheric	1
			-	3					A	6 Vr.		·	
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STN.	Cı	Pt	P2	C2	L.R.	TAP. V.	la	VP	s	Vs	\$	Ma	RA
22100					Rok	1750		64	36	18	57	10.9	16:00
21+00					W.K.	1260	.19						
					8.5K	875	.14	71	3	24	5	12.3	B/60
20100					έĶ	825	 	117	3	59	5	22.2	1075
19+00					12K	1250	116	124	h	53	5	18.8	7439
gun.					75 K	1756	.25	185	5	84	5	18.2	2420
18420					żźk	1752	-#	72	Na	37	1	19.2	3041
				1 12	1 1	Aswal							
here.			_	_	28	875	14						
						500				-	4		6
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171.5					68	275	117	2.44	5	Er.	5	12.3	5.9.30
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						875	.07	- K			1-1		
					1	1750	1.14	2					
						12.50	.1	×.					
	Reve	ic.l	BANK	Test		1250	.1	1					2
				A CARE		1750	14	1					
					N		41.7						
		1	600		2/21	ormal					1		
stin.		L		<u> </u>	8 K.	875	114	1					
						1250	. 5/	~					
			20	2 11	ali	simal							
144.00					92	875-	1/5						
						825	-45 -18	522	3	64	4	11.5	14-1
20710					POK	1250	.1	2					
						875	.08	1					
			ine	# 2		200'	alm	/	3				
			one	~				emas		·			1
331 ap			1		ZK	300	.17	13	7.			33.9	15
						500	.28	140	-4	.11	5	31.40	559
						375	.64	26	3	12	5	18.5	4270

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CALGARY, ALE king # 1 200' Normal

-	itd. Ita				PA	GE 2/3	t.
3	Vp	s	Vs	s	Ma	RA	
-		-		-	San and San IV	1 100	-

STN.	Cı	Pi	P2	C2	L.R.	TAP. V.	la	VP	s	Vs	s	MA	RA
33100					1.4 R	500	.45	27 263.5	1 10	17	5	25.2 25. B.	4247
32+00					MR	500	-78-	:					
						300	.57	198	4	14	5	28.2	260
3/4 00					44	500	.23	321	4	13	10	23.5	-92
30400						500	-14			1.5			
2						875	172						
					3.2K	300	.18						
					£K.	1250	.2						
-					SK.	875	.2				•		
					-	1750	A					1	
	1				6K	875	.27	138	3	79	5	22.8	3910
22+10					1.3K	300	-20-						
					7R	500	.12	Wet	5	new	to	W. ME	ed in
					2.8 K	300	.12	N	6	2 m pe	al red	tion	
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STN.	C1	Pi	P2	C2	L.R.	TAP. V.	IG	VP	s	Vs	s	MA	Ra
5100					2.8K	200	12	19	11	2	5	4.21	5458
						510	.25	49	4	6	5	1.87	5650
(b + co					1ĸ	200	.43	74.5	4	7.5	5	4.02	5 590
1474					10K	1250	.16	Hot	S	tabe			1.22
_					9K	1250	.17	32	4	2	5	a2.5-)0	Kug.s.
						1750	.27	45	4	6	5	the state of the s	\$750
30+10					20K	1750	2.	heating	e.	Nortio	1	2 × 2	states
						2500	.17						
						3500	.26	26	4	3	5	3.3.3	4750
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	V	Kint	#2		610	1	Y, ALBER					P	AGE
STN.	Cı	P۱	P2	C2	L.R.	TAP. V.	IG	VP	s	Vs	S	Ma	RA
29+H					13K	300	-24						1.1
						500	.12						1
						875	.74	142	4	10	5	2.82	6630
284.00					4.5K	1250	-38-	35	3	22	5	25.2	3000
27413					S	1250	.58	61	3				322
						275	.43	50	141				
						500	-28	34	3				1.120
						875	144	52	44	33	5	25.4.	4080
5640					.8K	300	-34-	80	50				478.
					IN	500	19R	141	3	69	14	1944	5291
25110					IOR	1250	18						
					NE	1750	-28						
						2510	144	71	3	42	5	23.71	5240
24110					17.4	2500	-26 -30	77	3	48	5	24.9- 25.9	885
221.00					2.15	574	- 3/						
					13.8	875	-55	204	U.I	111	5	21.81	2940
22+10				8	1.8K	1250	121	122	3	74	5	24,21	14100
3/1 A					-758K 1-2510	12:00	.2	105	M	58	5	221	18100
20430					164. 954	2500	-26-	165	3				
					1.50	2500	34	180	3	102	5	62.64	18351

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PAGE 242

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STN.	CI	Pi	P2	C2	L.R.	TAP. V.	la	VP	s	Vs	5	MA	RA
10					145年 学习大	2500	-27-	143.5		20		29.3 V	10-50
19+00					7.81.		12	167	3	95	5		
18+00					TESS	200	-62	244.5	3	117	5	1210	1300
17400					2. 8 化	5 en.	.25						
					2.14 K	875	.41	105	5	38	5	14,60	8825
6+00					44 21000	815	34	39	3	13	5	13,3 0	355
15+00					12	300	+ 42						
					7.4.K 473.K	30	. 4 3						
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STN.	CI	Pi	P2	C2	L.R.	TAP. V.	la	VP	S	Vs	5	Ма	RA
15tw					-64 7.6K	300	.52						
4.113-87.L						50	.87	197	14	46	5	9.35	780
14+50					2.K	500	.34						Į
						875	.68	150	3	48	10	12 8	761V
				4	1001	at	1 تى						
13+00					7K	1250	-1-8- - 2.6						
						1750	.28	125	3	20	5	64	1030
14+00					7K	1750	.3/	711	3	10	5	3.6 V	8.2.2
15+00		<u></u>			6K	1750	-48/.53	189	3	58	5	12.31	886
16+00	2				.7K	500	.78 ,81	302	5	93	5	12.30	869
17:00					281	875	.52	37	2	162	5	17.7	1680
18+00					3K	875	137	-41	2	180	5	17.9	2090
19+00					1.2K	500	.57	45	2	200	5	.17.8	1820
20+00					HR	875	.26	22	2	104	5	18.9	1940
21+00					10K	1750	.22	173	3	93	5	21.5	1820.
22+00				_	IOK.	1750	130	204	3	94	5	1.8.1	1470
23+00					8 K	1250	122	105	3	56	6	27.4	1100
24400					20K	2500	.20	72	3	27	5	15.0	830
25700					15K	1750	.19	49	3	26	5	21.20	59a

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STN.	Ct	Pi	P2	C2	L.R.	TAP. V.	la	VP	S	Vs	S	Ma	RA
26+00					15K	1750	-26 -30	95	3	37	5	15.6	1620 728
27400					1.5K	500	.42	100	3	52	5	20.8	549
28+00					3K	875	-36 -42	87	3	50	50	23.0	476
29+00					2K	500	132						
						875	.54	84	Ξ	44	5	20.9	358
30400					.9K	300						69.1	
						500	-62.6K	110	4	19	5	-6.8	3720
3/100					.5K	300	1.3			_			31
					1.7K.	300							
					1.5K	500	.76						
						875	.9						1
						500	1.08	169	4	7	5	406	36,00
32100	2				2.8 K	875	- 3 8 - 18 - 5	1				16.5	
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Following is a resume of the qualifications of the active partners of Geofax Surveys Ltd., and the personnel employed on the induced polarization survey on the Marmot Group of Mineral Claims:

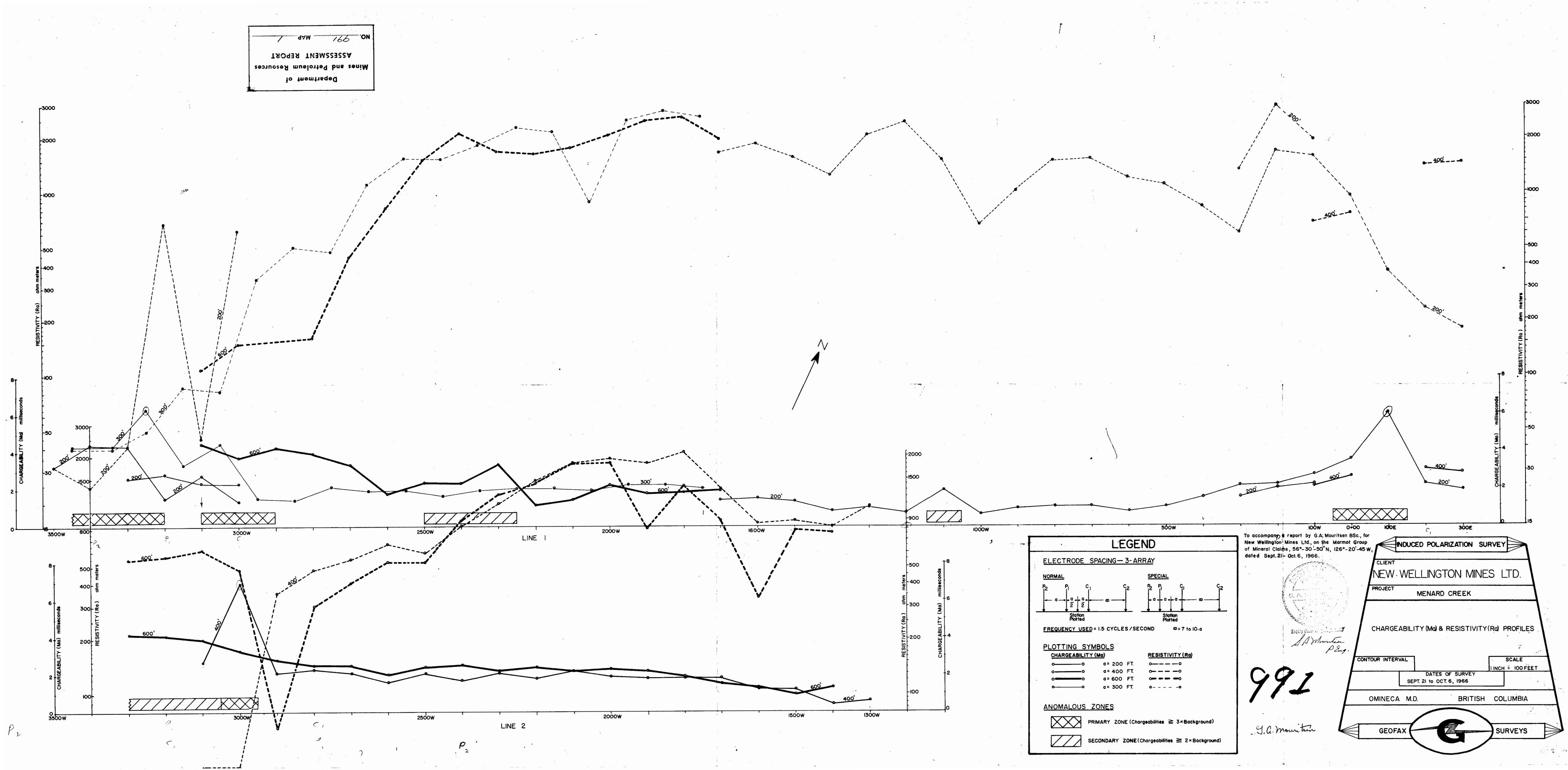
- S. A. Mouritsen-B.Sc., P. Eng. B. C. and Alberta, Geophysical and Geological Consultant for 20 years.
- W. Clemis- B.Sc., P. Eng., Former Exploration Manager of Canadian Fina Oil, now Geological Consultant, 20 years experience.
- J. V. Millar- M. Sc., P. Eng., B.C. and Alta., 15 years Mining Engineering Consultant.

G. A. Mouritsen- B.Sc., 18 years Geophysical experience.

The following personnel carried out the survey in the field:

- P. L. Brooks- B.Sc., 15 years Forestry in B.C., Alta and Sask. 9 months I.P.experience. Party Chief and Chief Operator.
- T. Lefebure- 14 years as Electronics Instructor(R.C.A.F), 2 years Mining Electronics Instructor. Assistant Operator.

In addition, two helpers were supplied by New Wellington Mines Ltd.





TO ACCOMPANY J. P. SURVEY BY J. S. MOURITSEN (GEOFAX SURVEYS LTD) OF MARMOT GROUP MENARD CREEK, OMINECA M.D. V DATED, OCTOBER, 1966.

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\bigtriangledown	GEOLOGICAL CONTACT
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R	ATTITUDE OF LAYERS
	FAULT FISSURE
tanks .	VOLCANIC
	INTRUSIVE
-000-	I.P. ANAMOLIES
211304	SAMPLE - COLLECTED BY SAVAGE
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