GEOPHYSICAL AND GEOCHEMICAL REPORT ON THE MIR PROPERTY, TROUT LAKE, B.C.

MIR-1 TO MIR-6 MINERAL CLAIMS

ATLIN MINING DIVISION

N.T.S. MAP SHEET 104N/10W

LATITUDE 50° 40' N; LONGITUDE 132° 53' W

For

Union Oil Company of Canada Limited

By

D.G. Leighton and

R.R. Culbert, PhD., P.Eng.

D.G. Leighton & Associates Ltd.

Vancouver, B.C.

15 May 1978

part 1 of 2

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GEOPHYSICAL AND GEOCHEMICAL REPORT ON THE MIR-1 TO MIR-6 MINERAL CLAIMS TROUT LAKE, B.C.

INTRODUCTION

This report describes the results of follow-up exploration on parts of the MIR-1 to MIR-7 mineral claims during the 1977 field season. The descriptions are divided into two parts. The first refers to the "Radon Cirque" area where grid controlled radiometric - geochemical surveys and prospecting work was done. The second part of this report describes follow-up geochemistry and reconnaissance scintillometry along the western Trout Lake graben margin.

Work on the MIR property was done at intervals, being part of a larger program involving the Surprise Lake batholith and surrounding area.

The conclusions and recommendations set forth here are based entirely on the above work.

SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

1. The MIR property consists of nine unsurveyed mining claims (120 units) located west of Trout Lake and reached by helicopter from the town of Atlin, 50 km to the west.

2. The claims are almost entirely underlain by granite or quartz monzonite of the Surprise Lake batholith, and are on the margin graben in this body. The granite is banded with aplitic phases.

3. Geochemical anomalies in excess of 1000 ppm uranium have been found in silt or soil samples from several locations on the MIR property, and radioactive spring waters have given radon anomalies amongst the highest ever recorded.

4. Strong uranium anomalies are usually accompanied by high concentrations of other metals as well, including lead, zinc, silver, copper, arsenic and thorium. This assemblage likely indicates polymetallic veining or stockwork mineralization.

5. One important area, the "Radium Spring" sector of "Radon Cirque" has been studied in an attempt to interpret the geochemical anomalies. This work has included establishment of a four square kilometer grid to control a spectrometry survey, a geochemical survey and prospecting. Detailed studies here have included:

    - multi-element geochemistry,
    - uranium disequilibrium measurements,
    - Eh and pH determinations,
    - radon measurements on waters,
    - stable isotope analysis of waters, and
    - polished section study of mineralized samples.

6. The major conclusion of these studies has been that both the geochemical and radioactive anomalies result from water-borne elements, and their distribution is controlled almost entirely by proximity to spring waters and interaction of these waters with organic materials. The grid work has hence proved of limited value in tracing mineralization beyond the obvious spring mouths, and such grids are not recommended in the future.

7. Although there are some indications that mineralization is not distant from the Radium Springs, anomalies obtained there must be treated as transported, at present.

8. Mineralized float is found in patches on the property and mineralized bedrock was encountered in one trench. Lead, zinc and silver are present in these zones, which contain significant magnetite and could presumably be outlined by magnetometer. The arsenic, thorium and uranium components of the geochemical anomalies were not present in important amounts. Any uranium mineralization may, therefore, be separated spatially from that of lead, zinc and magnetite.

9. Recommendations:

   (a) Radium Springs Area

   In view of the transported nature of this anomaly, effort should be made to better delineate the radioactive deposit before drilling. This may not prove easy. Three surveys are recommended which may prove of use, in addition to more hand trenching:

   i) Radon gas measurements should be made along lineaments in this area before the groundwater has thawed. There is reason to hope that when the springs are not running, part of the large amounts of radon being produced will diffuse to the surface more directly, indicating the position of mineralization. Main lineaments have been marked with high flags to facilitate such a survey.

ii) A magnetometer survey will likely outline the lead-zinc-silver magnetite zones, and this may be useful in locating uranium mineralization.

iii) A VLF-EM survey could be used to better locate the fractures and fault zones with which the mineralization may be associated.

(b) Graben Margin

Follow-up work in this area is not developed to the point of drill targets, although hand trenching is indicated in the vicinity of Delta Pool. It is recommended that future work depend heavily on the prospecting of lineaments for radioactivity, especially in dry areas. This has proved the most successful method of finding and tracing new anomalies to date. High thorium/uranium and radium/ uranium ratios appear to be useful here in separating transported accumulations of uranium from those nearer to source - a more important distinction in the graben swamps and lineaments than in the Radon Cirque area.

The possibility of a uranium bog deposit should also be kept in mind, and deep (to 6 m) hand augering of some swamps with extendable augers is recommended.

Respectfully submitted,

D.G. Leighton

R.R. Culbert, PhD., P.Eng.

15 May 1978

GENERAL DESCRIPTIONS

Location and Access

The MIR claims are situated immediately west of Trout Lake, which in turn is located 30 miles east of Atlin townsite in northwestern British Columbia. The geodetic co-ordinates are 59^{o} 40' N, 132^{o} 45' W. Access is presently by helicopter from Atlin, or by floatplane to Trout Lake.

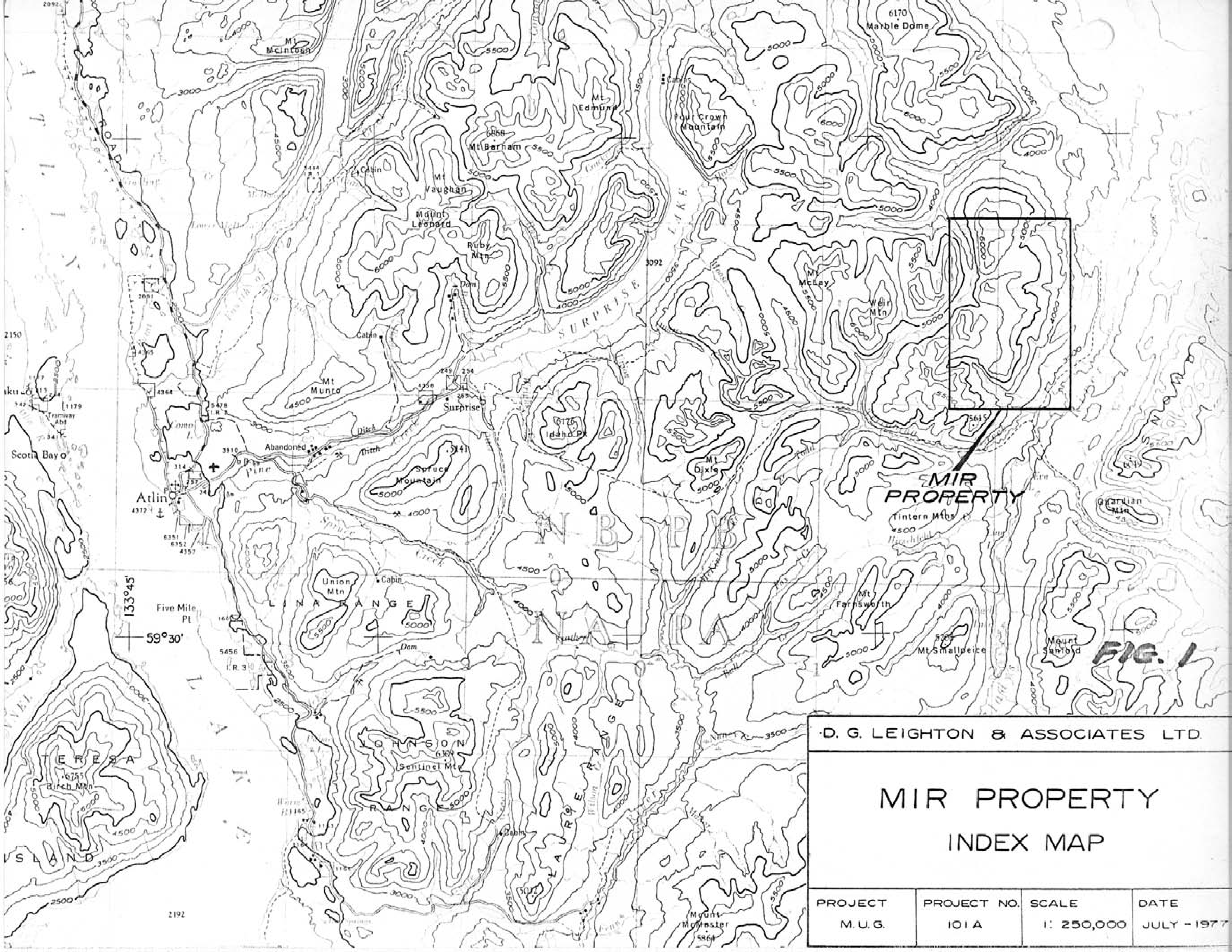
Topography

The claims cover the western flank of a major valley and adjacent barren ridges. The valley, which is structurally a graben, is forested, and contains Trout Lake and the Gladys River. Its topography is dominated by swamps and strong lineaments. The ridges reach altitudes of over 6000 feet, and are generally rounded, except where alpine glaciers have caused local cirques.

History

The MIR property was staked by Malabar Mines Ltd. (N.P.L.) in June 1976. Subsequent exploration was carried out under the Granville Square Joint Venture - M.U.G. Project.(Malabar, Union Oil and Getty Mines), currently managed by Union Oil.

There is no record of previous work on most of the area covered by the MIR claims apart from that done by Canadian Johns-Manville Co. Ltd. The Johns-Manville activities centered on the 1969-1971 interval and are described in a series of Assessment Reports. They deal with regional programs which largely concern the area to the west of the MIR property.



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MIR PROPERTY
INDEX MAP

PROJECT	PROJECT NO.	SCALE	DATE
M.U.G.	101 A	1: 250,000	JULY - 1977

Claims

The MIR property consists of the following mining claims held by Union Oil Company of Canada Limited:

Property	Claims	Units	Record No	Record Date	Group	Expiry
MIR	MIR 1	20	91	July 5, 1976)	MIR A	1978
	2	20	92	July 5, 1976)		1978
	MIR 3	20	93	July 5, 1976)	MIR B	1978
	4	20	94	July 5, 1976)		1978
	MIR 5	20	125	Sept. 17, 1971)	MIR C	1978
	6	20	126	Sept. 17, 1971)		1978
	MIR 7	20	127	Sept. 17, 1971	MIR D	1978
	MIR 8	20	160	Oct. 8, 1976)	MIR E	1978
	9	20	161	Oct. 8, 1976)		1978

The distribution of claims is shown on Figure 2.

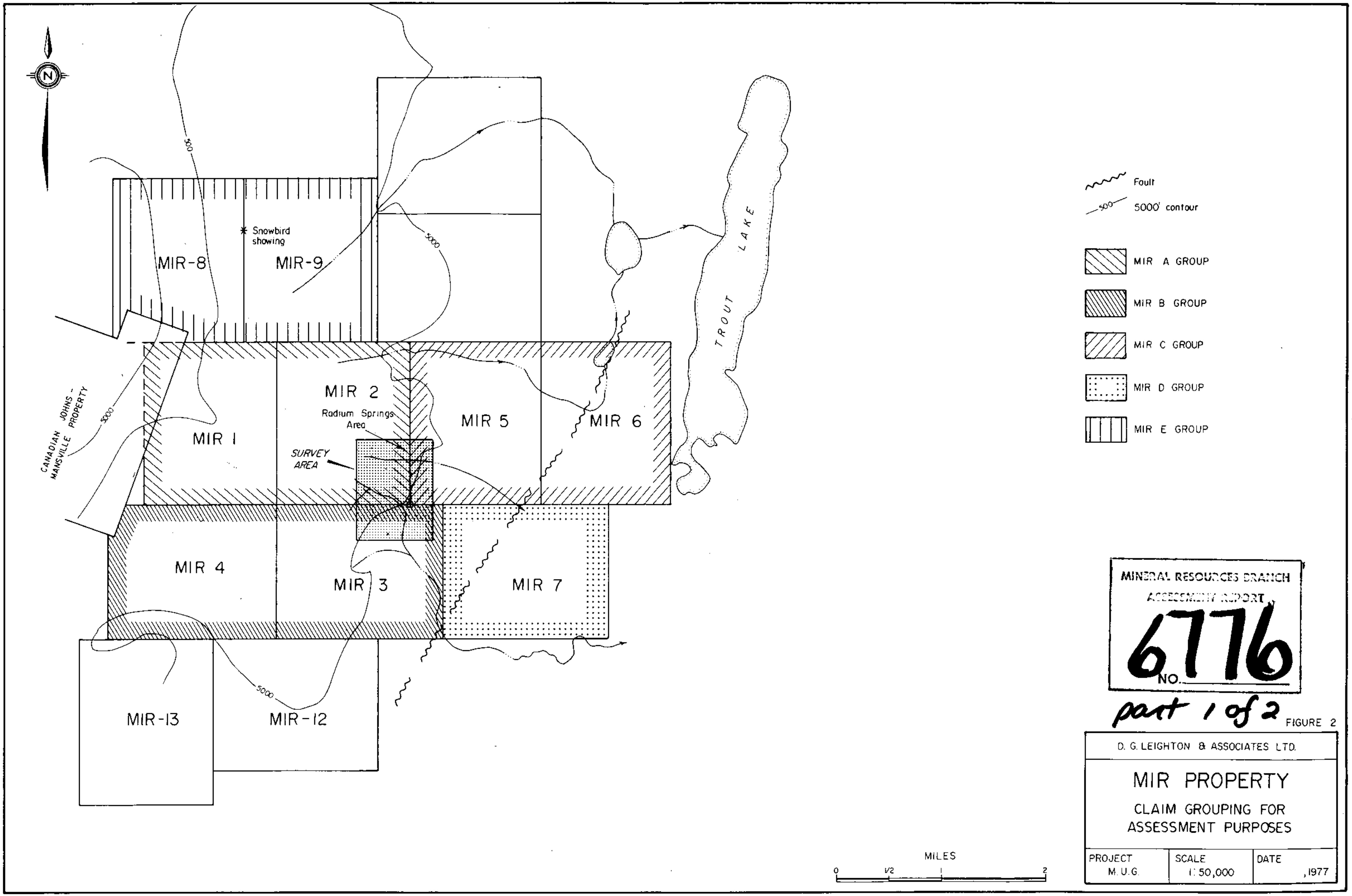

FIGURE 2

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MIR PROPERTY

CLAIM GROUPING FOR ASSESSMENT PURPOSES

PROJECT	SCALE	DATE
M.U.G.	1:50,000	,1977

GEOLOGY

Virtually the entire property is underlain by alaskitic quartz monzonite of the Surprise Lake batholith. This is considered to be of late Cretaceous or early Tertiary age, and forms a body roughly 55 km long a 40 km wide with elongation in the east-west direction. The intrusion is bisected by the "Trout Lake graben", a north-south trending feature which brings roof rocks down to valley level. The MIR claims lie on the western flank of this graben.

The rock is typically a two-mica granite or quartz monzonite, but in many areas there is an inter-layering of this with aplitic and pegmatitic phases. Commonly the aplitic phases are somewhat more radioactive, but this may be due to their greater resistance to surface weatherings. The G.S.C. collected a suite of fresh rock samples from the cirque rim west of Radium Springs on the MIR claims to find if there was any correlation between the granite phases and uranium content. No correlation was found (Bruce Ballyntine - personal communication).

Over most of the MIR property, the granite phases are found mixed in felsenmere. Above approximately the 4500 foot level, glacial action appears to have been strong only in the area of alpine cirque. Below this the valleys have been deepened by glaciation and are characterized by glacial features.

GEOCHEMISTRY

The average uranium content of the Surprise Lake granite is close to 17 ppm, and the mode for reconnaissance stream samples for this region in close to the same. Soil and silt samples in excess of 1000 ppm uranium have been encountered at several locations on the MIR property, and are usually accompanied by intense anomalies in other metals such as lead, silver, copper, arsenic or thorium. The geochemical analyses for uranium in this report are designed for routine tests where expected values lie in the 0 - 50 ppm range. For substantially higher values, the accuracy deteriorates in such a way that real values tend to be considerably higher than those reported. This has been demonstrated on the MIR property both by sending splits of some samples for delayed neutron activation analysis and by low energy gamma spectrometry. For geochemical exploration work, however, it is the relative rather than absolute values which are important, and the techniques used are sufficiently informative.

RADON

Radioactive springs and pools have been found scattered across much of the MIR property and in several other localities of the Atlin alaskite. Highly radioactive waters (as much as 3500 cps or 2 mR/h) have been encountered in a few places, usually associated with strong uranium geochemistry and anomalies in other metals.

In September of 1977, ten one liter bottles of water from radioactive springs and pools were shipped to Dr. W. Dyck of the Geological Survey of Canada in Ottawa for radon analyses. These were collected after a prolonged dry spell when radioactivity of the waters was low by comparison to earlier readings, but the results (Table I) ranged to as high as 82856 picocuries/liter, which Dr. Dyck suspects may be the highest ever recorded in natural waters. Furthermore, the less soluble helium which forms with radon (by alpha disintegration) had all escaped from these samples, suggesting that considerable degassing and radon loss had taken place before the waters were bottled.

Interpretation of radioactive springs is difficult. The most notable radioactive waters from the literature are either spatially associated with uranium deposits or involve hotsprings or mineral springs. The radioactivity in these latter cases results from the accumulation of radon's immediate parent element, radium, at or near the spring mouths. Radium is chemically similar to calcium and tends to accumulate, therefore, in some caliches. The radioactive waters of Atlin area, however, have been found to contain unusually little radium, and the associated sediments have less than required for equilibrium with the uranium present.

The short half life of radon (3.8 days) limits both the distance which this gas may travel in water from its source and the degree to which it may be geochemically concentrated. At this stage, therefore, radioactive waters may be interpreted only as transported anomalies, but as ones of considerable importance. Like other water-borne geochemical anomalies, radon can tell us little about the location of the uranium within the underground plumbing systems of the fractures along which the radioactive springs occur. It seems likely, however, that when these waters are immobilized by winter freezing, the large volumes of radon being produced would find their way to the surface much more directly than via waters in summer. For this reason we feel it is important to do a radon survey along the major fractures of the Radon Cirque area early in the spring of 1979, before melting has started. A system of numbered flags has been mounted here on poles and tree-tops to assist in identifying the important lineaments during the time of snow cover. A VLF-EM instrument could also be used to trace more accurately the fractures being tested for radon leakage.

At the site marked "LOC RB" of the Radium Springs (Map B), there is a deep, highly radioactive pool which does not have a correspondingly high radon content. It is possible that this anomaly is caused by a radioactive boulder below the pool.

TABLE I

RADON GAS (WATER) ANALYSES

Sample No.	Picocuries/liter Rn	μcc/l * He	Location
MIR A	56671	39.6	Radium Cold Springs
MIR B	48877	26.7	Radium Cold Springs
M 14	35587	36.4	Radium Cold Springs
M 16	64189	36.4	Radium Cold Springs
GAMMA	9951	33.1	Gamma Spring
DELTA	82856	42.8	Delta Pool
ZETA	13286	36.2	Zeta Pool
BOOM 2	75846	36.2	Boomerang Springs
ZAP 5	49151	29.8	Zapu Spring
RUBY	77572	29.8	Ruby Springs

* cm^3 x 10^6/liter water

NB: There was less helium in these waters than in water equilibrated with air (42.8 ucc/l) most likely because of degassing of CO_2 prior to bottling.

Addendum

A higher radon water value than recorded here has recently been announced from Finland, during a conference on radiation in Brazil.

A. RADON CIRQUE GRID

General

Intense uranium and radon anomalies were discovered in this region early in the 1976 program, especially in the area referred to as "Radium Cold Springs". Some soil and silt orientation work here in 1976 indicated strong multi-element anomalies, and defined them well enough to begin a grid at the beginning of the 1977 season. This grid was extended outward to eventually cover approximately four square kilometers, and was used as ground control for prospecting, soil sampling and a radiometric survey. Although both geochemical and radiometric anomalies were intense and widespread, analysis of the data indicates that it is the springs themselves which are the source of the anomalies.

Results of the grid controlled work are shown on six maps numbered H-M (see folder). These show geochemical and radiometric data plotted by computer and hand contoured.

A compilation map entitled "Spring Geochemistry - Structure" (see Map "B" in folder) shows the main structural features in relation to grid sample sites and the springs and creeks. Also shown are spring geochemical results, test pit locations, etc.

Radiometric Survey

A radiometric survey was carried out over most of the Radon Cirque grid using a McPhar Spectra 44 spectrometer. Results are given in maps G and H.

This has not proven to be an easy survey to interpret. Thorium was more common than expected, and may be involved in the uranium mineralization. The stripped uranium channel readings (i.e. after correcting for thorium's influence on this channel) are likely influenced by four major factors. These are:

1. Degree to which granite is covered by less radioactive overburden,

2. Rock type - the finer aplites being more radioactive in this area than coarse granite,

3. The degree to which uranium (or more specifically radium) has been concentrated in the surrounding soils. The correlation between radiometric and geochemical values for uranium over this grid is 0.48 which is surprisingly good in view of the fact that radium is not likely to closely follow uranium in water-transported anomalies. Furthermore, a radiometric reading averages conditions over a much larger area than a soil sample. The correlation between radiometric uranium and soil lead is almost the same as for soil uranium.

4. Radioactivity over some springs is several times background, due to outgassing of radon. Although such places were avoided in taking readings, anomalous radioactivity occurs for a considerable distance around certain springs and over some spots where no spring in visible. Furthermore, the half-life of the radon isotope in the thorium decay sequence is so short that these radon sources have a strong effect on the U/Th ratio.

We conclude, therefore, that in this area even the radiometric anomalies are transported, and neither uranium nor uranium/

thorium statistics will be of direct use in isolating bedrock sources of uranium.

Disequilibrium Studies

Equilibrium in the uranium series was examined by low energy gamma spectrometry for 27 samples of silt and soil in the Radium Springs area and 29 from the graben region. This method determines the concentrations of the uranium daughter products, radium and Pb^{214}, as well as measuring uranium and thorium. The following observations may be made:

1. For the most part, the inorganic fraction of Radium Springs sediments have uranium and their daughter products near equilibrium, and in some cases there is a slight daughter excess.

2. Uranium in the organic fraction of sediments from these springs had considerably stronger disequilibria (less daughter products), and the bank samples were in even greater disequilibrium. Mosses absorbed only 10 - 25% of equilibrium radium.

3. Disequilibrium tends to increase away from springs, and is especially great in the uraniferous bogs of the graben.

4. Thorium and uranium anomalies are of the same order of magnitude in the Radium Springs sediments, but thorium tends to be less easily transported and its values drop off away from springs. Except for the Delta Pond area, thorium values are almost an order of magnitude lower in the graben samples.

5. Surprisingly, the dried mosses contained very high thorium content (up to 1600 ppm), and this is undoubtedly a partial explanation for their radioactivity.

The near equilibrium conditions of the inorganic fraction of spring sediments is the first real indication that uranium may be sufficiently close to the spring mouths to be transported in "silt" form to the surface. A conflicting explanation would be that this fraction is relatively more successful at scavenging radium from the water, but tests by the G.S.C. indicated that the radium content of this water was extremely low.

It would appear that in the MIR area uranium/radium and uranium/thorium ratios may be used to identify uranium accumulations which are significantly transported from their source springs.

Structure

The Radium Springs area (Radon Cirque grid) is one of high fracture density and structural complexity. Main elements in this system are shown on map B. A major fracture (which may be traced following the graben margin for several kilometers to the north) passes through the centre of the grid from north-northeast where it is flanked by two parallel "faults". This major lineament appears to terminate at the head of Radon Creek. A set of closely spaced fractures enters the springs area from east-northeast. In that direction this fracture system may be traced down to the Omega and Kappa anomalies of the north graben. This zone also appears to terminate at the grid site. The third important set of lineaments trend northwesterly and are clearest where they form Radium Creeks A, B and C east of the grid area.

Geochemistry

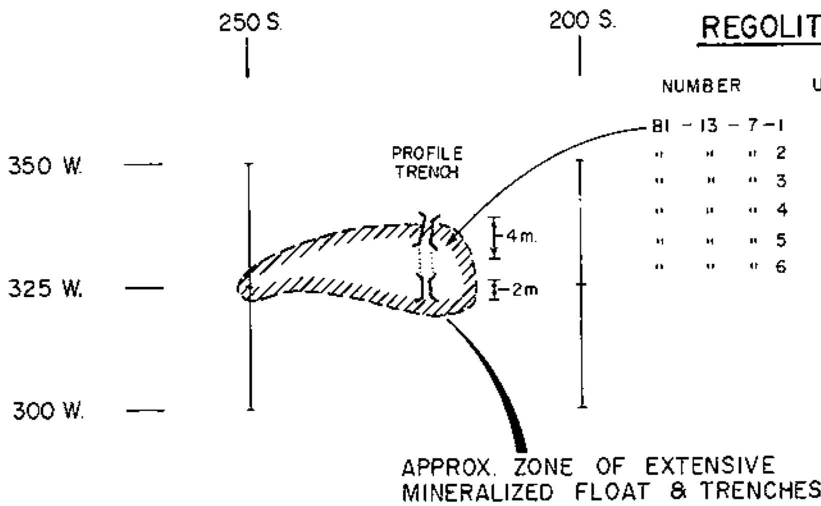
Soil and silt samples were analyzed for uranium, lead, silver and molybdenum. Molybdenum did not prove useful, and was dropped part way through the program. Results are given in accompanying maps (C, D, E, F) and show a fairly good correlation between lead, silver and uranium, each of which has strong anomalies. Results have been analyzed by computer in light of a detailed multi-element study done in the vicinity of four of the Radium Cold Springs located near the centre of the grid.

The results of the multi-element study are given in Appendix "E". Across the grid as a whole, the correlation between uranium and lead is substantially lower than in the detailed Radium Springs sampling, while the lead-to-silver correlation remains .85. This again points to the possible spatial separation of lead-silver mineralization from that of uranium, although both appear to be controlled by the same general structures.

The correlation between uranium and sample specific gravity is .61, which is somewhat better than for the springs alone. A four point scale for organic content by field observation was also available from the notes. Putting these two parameters together gives models explaining 46% of the variation in uranium or 40% of log uranium variation. The latter relationship is scatter-plotted in Figure 4, showing that control by organics in samples with greater than about 20 ppm uranium is strong, especially considering that the more potent measures of soil adsorption capacity (namely loss-on-ignition and exchangeable calcium) were not available in this model.

There is hence no reason to believe that uranium in the Radon grid sample group is controlled or distributed under principles differing from those governing the Radium Springs case. Another

TEST PIT "A" TRENCH



REGOLITH GRAB SAMPLES

NUMBER	U3O8%	Pb%	Zn %	Ag oz/ton
BI - 13 - 7 - 1	.003	.38	.62	.19
" " " 2	.002	.61	1.38	.20
" " " 3	.002	.12	.51	.29
" " " 4	.012	1.71	1.62	.59
" " " 5	.026	10.80	4.35	12.50
" " " 6	.065	12.30	3.10	15.50

TEST PIT "A" SOIL PROFILE

NUMBER	Mo	Pb	Ag	U (ppm.)
BI PP 1	4	300	1.3	49.5
BI PP 2	7	745	1.4	46.5
BI PP 3	3	860	1.7	50.0
BI PP 4	29	6500	22.0	170.0
BI PP 5	23	6200	22.5	165.0
BI PP 6	4	2550	14.5	100.0

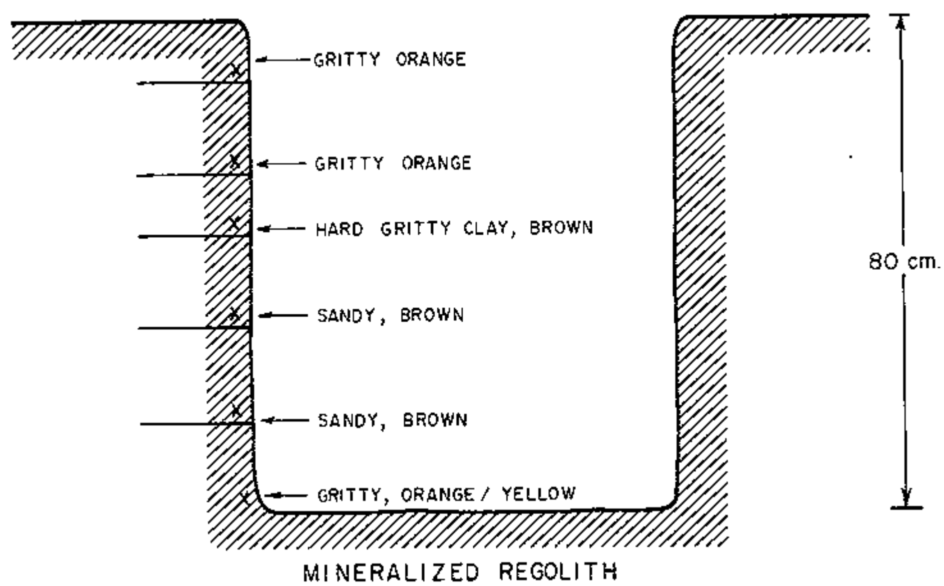


FIGURE 3

D. G. LEIGHTON & ASSOCIATES LTD.		
MIR PROPERTY RADON CIRQUE AREA TEST PIT "A" TRENCH		
PROJECT No. 101	SCALE AS SHOWN	DATE APRIL, 1978

RADON CIRQUE GRID SOILS

FILE NONAME (CREATION DATE = 11/12/77)
SCATTERGRAM OF (DOWN) LNUR (ACROSS) FLU

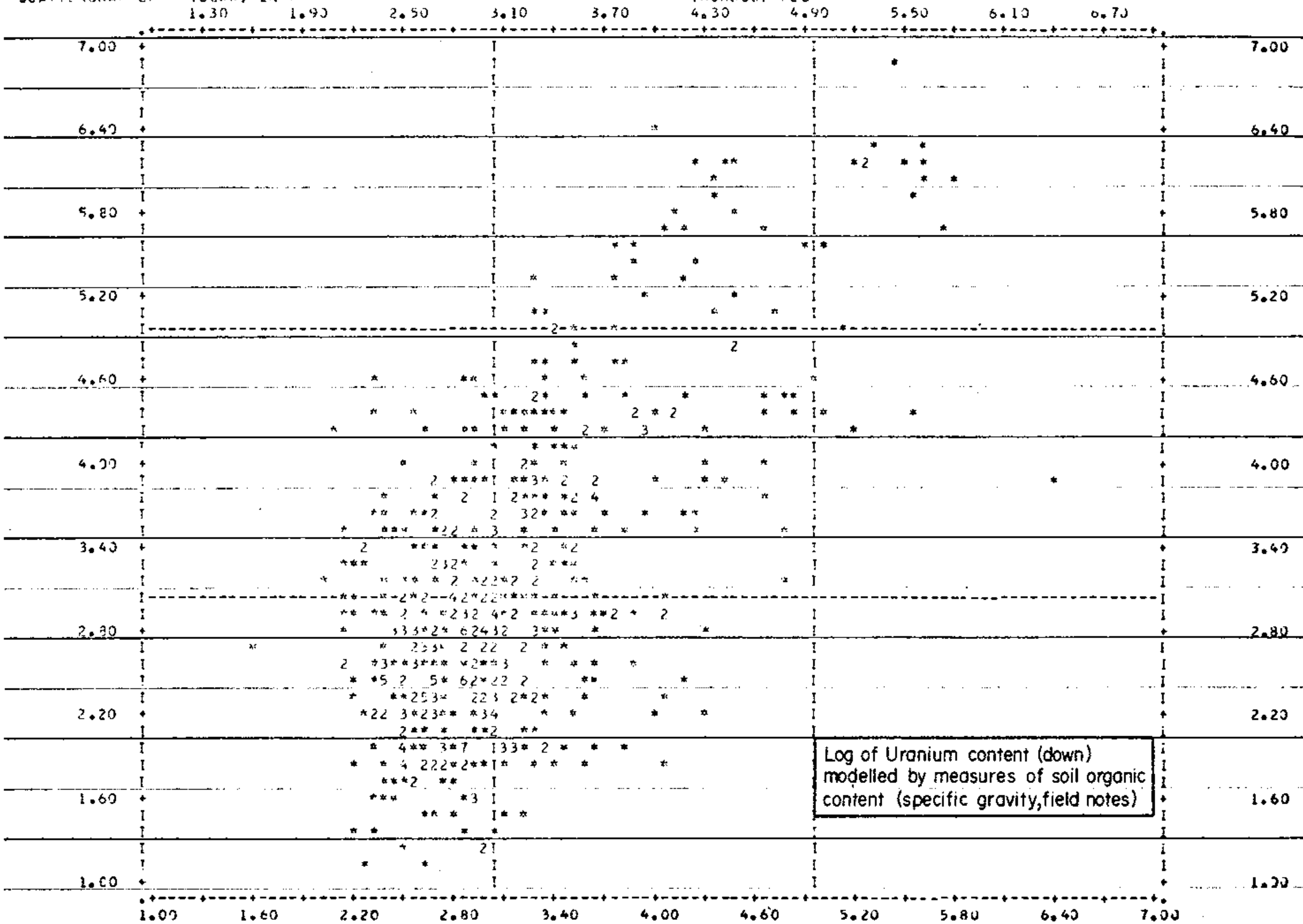


FIG. 4

way of examining this data, however, is to plot the difference between observed uranium in each soil sample and that which is expected for its specific gravity and organic field rating. These ratings have been calculated and plotted by the computer.

In view of the water-borne distribution of uranium and other elements involved in most major soil and sediment anomalies in this area, the uranium water geochemistry would appear to be a natural medium for exploration. Orientation work (mainly in 1976) showed that there were substantial water anomalies involved, but reproducibility of results was very poor. Even some of the most uraniferous springs were at certain times sufficiently low in water-borne uranium that they might be overlooked in reconnaissance. Sediments are therefore considered much more dependable in this area.

A few water samples collected from radioactive springs on the MIR property by the G.S.C. were subjected to stable isotope studies. The object was to determine whether the water involved was of deep-seated or shallow (meteoric) origin. A shallow origin was indicated (Bruce Ballantyne, personal communication). This interpretation is supported by short term change in discharge rates observed at the springs.

Mineralization

There is virtually no outcrop exposed in the Radium Springs area of the Radon Cirque grid. The area is covered by a thin mantle of glacial till. Prospecting here consisted of examining angular float (regolith) in the hope of defining source areas.

Mineralized rock takes the form of massive and disseminated galena-sphalerite with minor copper. Pyrargyrite (ruby silver) was noted at a trench which intersected this mineralization. Secondary manganese is commonly associated with base metal sulphides. Polished section work showed primary magnatite and hematite in association with the lead-zinc minerals. The location of mineralized float is noted on map B (see folder). Also shown on this map is the above mentioned trench, from which grab samples assayed up to 12.3% Pb, 4.35% Zn, 15.5 oz/ton Ag and 0.065% U_3O_8. The trench reached bedrock (see Figure 3).

Sulphide mineralization observed in the Radium Springs area is undoubtedly related to a series of poly-metallic veins. Beyond the general spacial relationship between base metals and uranium geochemical anomalies, nothing can be said about the place of uranium mineralization in this system

Further descriptions of sulphide mineralization as determined from polish and thin section studies of selected samples are provided in Appendix "D".

B. GRABEN MARGIN GEOCHEMISTRY

Geochemical work on the graben flank in 1977 was of a "follow-up" nature, as opposed to detailed grid work done to define drill targets in the adjacent Radon Cirque area. Answers were specifically sought to the following questions:

1. Distribution and extent of anomalies,
2. Relation of anomalies to structure,
3. Relation of geochemistry to radioactivity,
4. Relation of uranium anomalies to those of other elements,
5. Extent of environmental control, particularly the effect of organic materials and spring waters,
6. Possibility of economic uranium concentrations as secondary deposits.

The above points will now be discussed in order.

Anomaly Distribution

Silt and wet soil anomalies were found through the entire length of the graben margin examined (approximately 5 km) and apparently extend beyond in both directions. In addition, substantial anomalies were encountered on the valley flank west of the margin lineament, both in streams descending from Radon Cirque and from sediments or soils of apparent local derivation. Little work has been carried out to date east of the main lineament, but one radioactive and uraniferous area was discovered - the Delta Pool. Also, a major creek sampled in the northeast corner of the study area had high values in both uranium and arsenic.

In summary, a substantial portion of the water course sediments and water-affected soils in this area are highly anomalous in uranium.

Lineament Control

In the graben margin study (as at Radon Cirque itself), there is a strong correlation between geochemical (and radioactive) anomalies and prominent lineaments or lineament intersections. It is by no means clear, however, whether this relationship is due to fault controlled mineralization (the usual site for uranium deposits in granite), or whether it is due to lineament control of water routes, swampy ground and springs. Both relationships may well be involved.

The most prominent lineaments in this area are those trending in a north-east direction, paralleling the main graben margin fault. These are cut by lineaments on a northwest trend. In the MIR-6 area there is a chaotic pattern formed by intersections of three or more lineament sets, somewhat similar to that encountered in the Radon Cirque.

There is a disruption of the main graben margin fault in the vicinity of "Gamma Lake". This is also the area of the highest geochemistry, but unfortunately it also coincides with several large radioactive springs and with the main drainage from Radon Cirque. Hence, there is once again a question of whether structure or water transport are responsible.

Geochemistry vs. Radioactivity - Radon Anomalies

A variety of radioactive springs, swamps and soils were encountered, and to a large extent this governed the geochemical sampling, except for stream silts. The results, however (see maps in pocket), showed a rather poor correlation between the radioactivity of soils and uranium content. To some extent this is to be expected, due to separation of uranium from daughter products, notably radium, during surface transport, and due to the variable presence of thorium. Zones of intense radioactivity have usually, however, been due to the surfacing of radon.

Samples of radioactive waters were taken from various points in the Atlin region in September of 1977 and sent to the Geological Survey of Canada in Ottawa for analyses. One of the samples from MIR-7 (from Delta Pool) was, by a small margin, the richest in radon, 82,856 Picocuries per liter. This occurred despite the fact that the samples were taken after a prolonged dry spell when the waters were of unusually low radioactivity. Furthermore, virtually all of the associated (but less soluble) helium had escaped from these waters, suggesting that a major portion of the original radon had degassed prior to collection.

Radioactivity in swampy areas is sometimes increased dramatically by a floating moss which accumulates uranium, radon and thorium.

Other Elements

Uranium is known to occur with lead in the mineral casolite on the MIR property, and to be associated closely with lead, zinc and silver mineralization at Radon Cirque. At other locations in the Atlin granite it is found with arsenic and copper as zeunerite. Extensive analysis of silt and soil samples for lead, silver, copper and arsenic (see maps in pocket) was carried out in search of evidence of these mineral associations in terms of elements less mobile than uranium in surface waters.

Lead, silver and, to a less extent, copper have high background throughout the area examined. With respect to these backgrounds, there are certain anomalous areas for each element.

1. Lead

The two "Radium" creeks descending from Radon Cirque area carry high lead values in their sediments, as do the swamps into which they drain. A similar effect is observed for a drainage system in the centre of the MIR-5 claim, and for those swamps (above the main lineament) into which it drains. Omega lineament soils farther north are also lead rich. Strangely, Radon Creek itself does not have (by comparison) high lead values in its sediments, and the intense uranium anomalies in Gamma Lake and Alpha Springs are not accompanied by lead.

2. Silver

Silver variation in these soils and sediments is not as great as with the other elements. To a major extent it seems to follow lead, but with a greater tendency to accumulate near springs. An exception is the Alpha-Beta area, where silver values are high with respect to lead.

3. Copper

Copper forms fairly well defined anomalous areas, including the Alpha-Gamma region and an area encompassing the Zeta and Theta radioactive zones and lineament samples to south thereof. The Omega zone is also copper rich.

4. Arsenic

Arsenic values in soils and sediments are more erratic than the other elements tested, and are more difficult to categorize. High values are clearly associated with the Alpha Springs area, and the Omega zone is very anomalous. In general, the northeastern part of the study area (MIR-6) has a substantially higher arsenic background than the rest. Two single highs occur in the arsenic results, one from a swamp at base of "Radium A" creek, and the other from a large stream at the eastern edge of the MIR-6 claim.

Special mention should be made of the Delta Pool area. Like the Omega lineament, this area was anomalous in all 5 elements analyzed. The area of radioactivity and of strong geochemical anomalies was largely determined by ground in which soils were influenced by water. However, one sample (LIN-83) taken from a dry and only slightly radioactive lineament just above this pool had the following results: U = 1100 ppm, As = 480 ppm, Cu = 6200 ppm, Pb = 5400 ppm, Ag = 15.8 ppm. This sample very likely came from adjacent mineralization of a complex nature.

5. Environmental Control

The most obvious control of uranium in the geochemistry of this area is by organic material. Although the regional correlation between uranium and organic material in silt samples is poor, in localities where uranium is anomalously high the greatest values are almost always associated with the more organic samples. This is presumably due to the well-known ability of organic materials to adsorb uranium from water, especially where they create reducing conditions.

The underlying control in this pattern of distribution is the mobility of these elements in solution. This again is somewhat surprising, as neither lead nor silver are particularly mobile in waters of essentially neutral pH. Furthermore, tests run on the uranium content of these waters have shown them to be anomalous, but not highly so. Even the radioactive springs have seldom more than 10 ppb uranium.

Except, therefore, in areas affected by major creeks, these multi-element anomalies are likely transported indications of mineralization which is at no great distance. The exceptions will be where creeks or drainages of any size first encounter swamps. The forementioned example at Delta Pool strengthens this model of limited transport.

6. Springs and Bog Deposits

Some of the most intense geochemical anomalies occur near springs, where water-borne uranium first meets organic material (and reducing conditions). A somewhat similar condition may occur where rapidly descending creeks bearing some uranium abruptly encounter a swamp. On one hand, this causes interpretative problems, as such anomalies may have been transported considerable distance by creeks or from depth in the case of springs. On the other hand, in view of the intense accumulations of uranium in this area, it is conceivable that "bog-deposits" of economic size may be involved. This would be especially feasible where spring waters ascend below a marsh.

As a preliminary investigation of these uraniferous organic areas, a series of deep auger samples were taken along the main lineament. Results were mixed, with some sites increasing in uranium downwards, and some decreasing. The situation is hence likely to be complex, and exploration will be made more difficult by the fact that several of the highest geochemical results were returned from swamp of low radioactivity. On the other hand, augering showed that the organic material along much of the west marginal lineament was not very deep.

BREAKDOWN OF COSTS - MIR PROPERTY (1977)

Approximately $68,880 was spent on the MIR property and surrounding area in 1977 to carry out geophysical-geochemical surveys and prospecting. This was distributed approximately as follows:

Wages and salaries	$31,800.00	
Benefits	3,816.00	$35,616.00
Meals and accommodation		2,500.00
Mobilization - mainly helicopter charges		13,500.00
Assay costs		11,500.00
Miscellaneous; includes base map preparation, drafting and report preparation, geophysical equipment rental, etc.		4,664.00
TOTAL		$68,880.00

Of this total, approximately $21,100 was spent up to July 5, 1977 and the balance, $47,780, thereafter.

Of the $47,780 balance, $10,000 was filed to maintain the MIR-5 - MIR-9 claims in good standing, leaving $37,780 available for assessment credit.

PROJECT PERSONNEL

The following individuals were involved with field work on the MIR property:

R.R. Culbert	Geologist
D.G. Leighton	Geologist
J.W. Davis (Union Oil)	Geologist
R.J. Bilquist	Prospector
D.T. Kenning	Field Technician
L.O. Allen	Field Technician

CERTIFICATION

I, R.R. Culbert, do hereby certify that:

1. I am a practicing Professional Geological Engineer with offices at 3152 West 10th Avenue, Vancouver, B.C.

2. I am a graduate of the University of British Columbia, BASc. (1964), PhD. (1971).

3. I have practiced mining exploration for fifteen years, most of which were based in British Columbia.

4. I am a member, in good standing, of the Association of Professional Engineers of the Province of British Columbia.

5. I have personally visited the MIR property and supervised exploration work carried out there.

Respectfully submitted,

R.R. Culbert, PhD., P.Eng.

15 May 1978

APPENDIX "A"

MIR PROPERTY

RADON CIRQUE GRID

GEOCHEMICAL AND RADIOMETRIC DATA

CLAIM	CO-ORDS	SM	CL	URAN PPM	LEAD PPM	AG	MO	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
MIR 5	1000N 00E	A	B	85.0	53	.6	3	2.28	18436	1216	514	370	296
MIR 5	1000N 50E	A	B	35.0	44	.7	2	2.33	12816	752	322	262	168
MIR 5	1000N 100E	A	B	8.0	18	.8	3	2.82	12642	808	290	236	151
MIR 5	1000N 150E	A	G	9.5	10	.6	1	2.66	8846	512	184	180	78
MIR 5	1000N 200E	A	B	19.5	50	.4	2	2.93	10898	790	230	186	120
MIR 5	1000N 250E	A	B	70.0	57	1.1	3	2.05	13484	896	334	254	184
MIR 5	950N 250E	A	G	6.0	32	1.0	2	2.58	11172	720	268	250	121
MIR 5	900N 00E	A	G	4.5	18	.6	4	2.51	10576	696	274	226	141
MIR 5	900N 50E	A	B	17.0	34	.7	4	2.54	13344	884	290	346	86
MIR 5	900N 100E	A	B	75.0	87	1.0	6	2.41	16790	914	436	314	251
MIR 5	900N 150E	A	B	65.0	69	1.0	3	2.56	13862	812	330	288	160
MIR 5	900N 200E	A	R	11.0	52	.7	4	2.78	10376	850	210	168	111
MIR 5	900N 250E	A	B	13.0	59	.7	4	2.70	17848	1392	438	388	210
MIR 5	850N 250E	A	G	2.5	47	.8	4	2.67	12328	850	268	246	123
MIR 5	800N 00E	A	B	65.0	48	1.0	4	1.20	11740	660	306	248	160
MIR 5	800N 50E	A	G	4.5	17	.6	3	2.64	7776	458	186	140	103
MIR 5	800N 100E	A	G	8.0	23	.7	4	2.80	8470	640	182	160	88
MIR 5	800N 150E	A	B	16.0	220	1.0	5	2.57	14798	1140	314	238	174
MIR 5	800N 200E	A	B	4.5	44	.9	4	2.94	11656	812	278	222	147
MIR 5	800N 250E	A	O	6.5	50	1.2	4	2.70	9488	752	240	194	126
MIR 5	750N 250E	A	B	6.5	33	.9	3	2.85	13208	956	308	258	156
MIR 5	700N 00E	A	G	2.0	16	.4	3	2.85	13908	850	352	278	188
MIR 5	700N 50E	A	B	7.5	33	.4	2	2.43	10676	716	246	244	102
MIR 5	700N 100E	A	G	12.5	38	.6	2	2.70	11018	726	252	178	147
MIR 5	700N 150E	A	G	4.0	31	.9	3	2.82	8506	586	208	158	115
MIR 5	700N 200E	A	B	11.0	46	.5	2	2.57	10968	800	238	208	115
MIR 5	700N 250E	A	B	7.0	35	.8	2	2.77	12246	1090	260	172	159
MIR 5	650N 250E	A	B	6.0	39	.8	2	2.40	12322	874	246	282	80
MIR 5	600N 00E	A	G	7.5	26	.6	4	2.56	7720	522	166	116	97
MIR 5	600N 50E	A	G	4.0	55	.5	3	2.78	9042	606	190	138	108
MIR 5	600N 100E	A	B	5.5	36	.3	2	2.49	13674	956	326	278	162
MIR 5	600N 150E	A	B	5.5	39	.4	3	2.66	7768	544	202	136	122
MIR 5	600N 200E	A	Y	14.5	38	.6	4	2.43	17290	1176	474	334	277
MIR 5	600N 250E	A	B	6.5	56	.7	1	2.58	12892	976	332	202	213
MIR 5	550N 250E	A	B						11662	842	274	222	143
MIR 5	500N 00E	A	G	30.0	55	.5	3	2.64	8250	458	182	168	83
MIR 5	500N 50E	A	B	13.5	72	.4	3	2.43	13656	740	382	264	227
MIR 5	500N 100E	A	O	7.5	59	.5	3	2.65	16116	1124	394	334	197
MIR 5	500N 150E	A	B	75.0	240	1.0	5	1.65	15454	1096	392	292	220
MIR 5	500N 200E	A	B	9.5	75	.6	2	2.72	12748	968	288	208	165
MIR 5	500N 250E	A	B	8.0	53	.9	2	2.98	11044	802	212	184	103
MIR 5	400N 00E	A	Y	9.5	82	.6	2	2.91	14472	1032	360	324	169
MIR 5	400N 50E	A	B	6.0	86	.6	4	1.99	18556	1302	426	408	186
MIR 5	400N 100E	A	B	23.0	97	.8	3	2.35	12172	772	262	226	129
MIR 5	400N 150E	A	B	13.0	92	.4	1	2.55	15170	972	314	296	140
MIR 5	400N 200E	A	Y	10.0	79	.6	4	2.78	11864	866	274	218	146
MIR 3	400N 250E	A	B	30.5	197	1.1	3	2.52	13662	818	352	272	192
MIR 3	350N 250E	A	B	6.0	64	.7	2	2.66	14150	846	312	312	128
MIR 5	300N 00E	A	B	4.5	32	.4	2	2.78	13200	780	340	250	193
MIR 5	300N 50E	A	B	5.0	73	.8	4	1.68	16240	1056	338	360	126

CLAIM		CO-ORDS		S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
MIR	5	300N	100E	A	B	20.5	135	.9	3	2.27	15460	964	396	316	210
MIR	5	300N	150E	A	B	52.5	60	1.4	4	1.92	12040	824	322	224	190
MIR	5	300N	200E	A	B	6.5	295	2.1	6	1.88	15538	982	398	348	193
MIR	3	300N	250E	A	B	55.0	267	1.4	4	2.32	14654	862	356	274	195
MIR	3	250N	250E	A	B	10.5	71	.8	3	2.82	13718	914	368	278	204
MIR	3	200N	00W	A	B	75.0	185	1.2	2	1.26	17120	1004	384	374	164
MIR	3	200N	50E	A	B	15.0	63	.8	3	2.80	13316	908	306	276	143
MIR	3	200N	100E	A	B	22.5	75	.8	4	2.63	12928	932	326	242	183
MIR	3	200N	150E	A	B	18.5	121	1.0	8	2.42	13580	960	268	250	121
MIR	3	200N	200E	A	B	11.5	75	.9	6	2.20	13800	920	360	300	183
MIR	3	200N	250E	A	B	17.5	83	.8	3	2.38	14380	876	358	314	173
MIR	3	150N	600W	A	B	7.5	107	.5	4	2.50	16294	1000	376	330	182
MIR	3	150N	550W	A	B	6.0	42	.6	3	2.57	10818	714	270	238	130
MIR	3	150N	500W	A	B	29.0	70	.8	4	2.58	14870	976	338	302	160
MIR	3	150N	450W	A	B	23.0	39	.5	2	2.85	11410	652	306	244	162
MIR	3	150N	400W	A	B	23.5	47	.7	3	2.45	8698	522	214	164	117
MIR	3	150N	350W	A	B	15.0	44	.6	3	2.41	10284	676	234	242	91
MIR	3	150N	300W	A	G	10.5	43	.7	5	2.40	9236	644	242	156	150
MIR	3	150N	250W	A	G	16.0	39	.6	4	2.32	11426	836	246	224	114
MIR	3	150N	200W	A	B	7.0	42	.7	5	2.49	14982	1032	368	328	175
MIR	3	150N	150W	A	O	13.5	138	1.7	9	2.58	9784	620	248	178	143
MIR	3	150N	100W	A	B	16.5	50	.7	4	2.26	12726	786	320	218	192
MIR	3	150N	50W	A	G	19.5	44	.4	2	2.60	11822	736	232	232	95
MIR	5	150N	00E	A	R						12162	822	280	236	141
MIR	5	150N	50E	A	B						10240	722	282	186	172
MIR	5	150N	100E	A	B						16644	1068	428	346	224
MIR	5	150N	150E	A	B						15876	1016	406	284	239
MIR	5	150N	200E	A	R						15368	1190	400	330	206
MIR	5	150N	250E	A	B						13598	978	326	254	176
MIR	3	100N	600W	A	B	20.0	52	.4	4	2.78	14320	964	308	240	167
MIR	3	100N	550W	A	B	24.0	49	.6	3	2.27	14978	906	332	302	154
MIR	3	100N	500W	A	B	11.0	36	.4	5	2.70	12140	880	280	224	148
MIR	3	100N	450W	A	B	9.5	28	.5	4	2.47	12458	902	276	234	138
MIR	2	100N	400W	A	B	18.5	50	.6	2	2.44	19206	864	582	348	377
MIR	2	100N	375W	A	B	6.5	32	.6	2	2.39	14898	2130	330	324	139
MIR	2	100N	350W	A	B	6.0	66	.6	3	2.64	13944	870	348	318	161
MIR	2	100N	325W	A	Y	4.0	41	.8	3	2.37	19794	552	156	138	74
MIR	2	100N	300W	A	B	3.5	104	.8	3	2.40	10752	876	276	168	177
MIR	2	100N	275W	A		5.0	44	.8	2	2.65	13212	1002	360	270	201
MIR	2	100N	250W	A	B	13.5	96	.9	2	2.80	14058	870	372	270	213
MIR	2	100N	225W	A	Y	6.5	38	1.6	3	2.79	7038	504	156	150	67
MIR	2	100N	200W	A	B	5.0	47	.9	1	2.58	7446	528	150	132	72
MIR	2	100N	175W	A	B	15.0	26	.9	2	2.78	8160	636	228	186	118
MIR	2	100N	150W	A	R	10.5	52	.8	2	2.80	11724	858	270	210	146
MIR	2	100N	125W	A	B	9.0	87	1.8	5	1.75	10014	738	270	180	164
MIR	2	100N	100W	A	B	26.5	100	1.0	2	2.18	13128	798	288	234	150
MIR	2	100N	75W	A	B	12.0	68	.7	2	2.79	13704	870	288	234	150
MIR	2	100N	50W	A	B	13.0	106	.9	4	2.29	11838	822	270	222	139
MIR	2	100N	25W	A	B	9.5	164	1.6	2	2.34	13662	936	312	276	149
MIR	2	100N	0W	A	B	75.0	440	2.4	3	1.74	10950	708	264	216	137

CLAIM		CO-ORDS		S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	PCT CHN	URN CHN	TH CHN	URAN STRP
MIR	5	100N	25E	A	B	30.0	89	.6	3	3.02	12552	696	324	258	172
MIR	5	100N	50E	A	B	18.0	148	1.1	4	2.45	13830	1020	312	276	149
MIR	5	100N	75E	A	B	25.5	174	.8	5	2.65	15990	1218	360	342	159
MIR	5	100N	100E	A	B	11.0	84	.9	3	2.72	17292	996	474	330	280
MIR	5	100N	125E	A	B	20.0	45	.6	2	2.44	13716	942	342	270	183
MIR	5	100N	150E	A	B	9.5	67	.5	5	2.28	17262	1128	426	378	204
MIR	5	100N	175E	A	B	305.0	570	2.9	12	1.93	36702	1602	1218	816	739
MIR	5	100N	200E	A	B	17.5	64	.8	2	2.18	13152	972	294	252	146
MIR	5	100N	225E	A	B	115.0	215	1.2	4	2.20	14796	948	384	294	211
MIR	5	100N	250E	A	B						12330	864	312	258	160
MIR	3	50N	600W	A	B	9.0	53	.6	5	2.45	10202	698	226	198	109
MIR	3	50N	550W	A	B	195.0	630	2.2	6	1.60	23124	1212	630	596	280
MIR	3	50N	500W	A	B	6.0	30	.4	3	2.36	12242	878	280	206	159
MIR	3	50N	450W	A	B	65.0	80	.8	2	1.80	13424	842	336	296	162
MIR	2	50N	400W	A	B	15.0	67	1.1	3	2.23	9318	408	312	228	178
MIR	2	50N	375W	A	B	40.5	186	1.5	5	2.02	15504	972	330	288	160
MIR	2	50N	350W	A	B	6.5	68	.9	4	2.59	9768	606	204	114	137
MIR	2	50N	325W	A	B	21.0	190	.9	3	2.01	15984	942	354	330	160
MIR	2	50N	300W	A	R	3.5	59	.6	2	2.59	11430	912	252	246	107
MIR	2	50N	275W	A	B	6.0	126	.5	2	2.37	12114	696	216	198	99
MIR	2	50N	250W	A	B	3.0	58	.2	2	2.55	10236	708	258	168	159
MIR	2	50N	225W	A	B	5.0	29	.4	1	2.71	9270	684	288	210	164
MIR	2	50N	200W	A	B	5.0	40	.1	1	2.70	11652	714	318	150	229
MIR	2	50N	175W	A	B	6.0	75	.8	1	2.12	11094	750	264	168	165
MIR	2	50N	150W	A		10.5	40	.5	2	2.29	13554	912	330	228	196
MIR	2	50N	125W	A	G	12.5	85	.6	5	2.26	8190	468	186	120	115
MIR	2	50N	100W	A	B	65.0	136	.9	5	2.16	16314	732	462	252	314
MIR	2	50N	75W	A		275.0	990	4.2	9	1.13	13674	564	420	288	250
MIR	2	50N	50W	A	B	34.5	255	.9	5	2.17	17070	978	486	294	313
MIR	2	50N	25W	A	B	5.0	107	1.0	4	2.83	13014	888	336	204	216
MIR	2	50N	0W	A	B	2.0	37	1.4	3	2.73	5324	330	120	66	81
MIR	5	50N	25E	A	B	20.5	127	1.3	5	2.59	11796	816	312	270	153
MIR	5	50N	50E	A	B						21346	1248	576	576	237
MIR	5	50N	75E	A	B	455.0	2850	7.6	8	1.82	17004	888	474	306	294
MIR	5	50N	100E	A	B	465.0	885	2.6	9	1.30	14778	1050	378	270	219
MIR	5	50N	125E	A	B	16.5	64	.8	3	2.84	13860	942	306	276	143
MIR	5	50N	150E	A	B	15.5	73	1.1	2	2.76	16494	1038	432	324	241
MIR	5	50N	175E	A	R	17.0	52	.5	3	1.96	14160	990	342	288	172
MIR	5	50N	200E	A	B	105.0	330	.6	5	1.90	14196	942	396	246	251
MIR	5	50N	225E	A	B	135.0	116	1.2	4	2.08	17820	1182	396	348	191
MIR	5	50N	250E	A	B	5.0	146	1.2	6	2.05	14310	924	384	264	229
MIR	3	0N	800W	A	B	90.0	202	1.0	2	1.90	13754	840	386	264	231
MIR	3	0N	750W	A	B	10.0	82	.8	3	2.59	16870	1098	398	322	208
MIR	3	0N	700W	A	B	17.5	52	.8	4	2.57	13280	856	336	276	173
MIR	3	0N	650W	A	B	11.0	64	1.2	2	2.58	12848	946	354	250	207
MIR	3	0N	600W	A	B	12.5	52	.9	4	3.10	12708	768	316	294	143
MIR	3	0N	550W	A	B	15.0	56	1.6	3	2.87	12214	868	250	238	110
MIR	3	0N	500W	A	B	15.5	84	1.4	5	2.57	10082	650	246	196	130
MIR	3	0N	450W	A	B	12.0	46	1.1	3	2.77	11886	958	240	226	107
MIR	2	0N	400W	A	B	14.5	106	.4	4	2.27	6420	402	264	84	214

CLAIM		CO-ORDS		S M	C L	URAN PPM	LEAD PPM	A G	M C	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
MIR	2	CN	375W	A	B	4.0	52	.4	4	2.59	7608	504	180	102	120
MIR	2	CN	350W	A	B	6.5	56	.3	1	2.81	10896	708	186	192	73
MIR	2	CN	325W	A	B	16.0	89	1.0	2	2.43	12414	762	330	258	178
MIR	2	CN	300W	A		75.0	275	2.5	2	1.77	13266	732	276	204	156
MIR	2	CN	275W	A	G	4.5	52	.7	2	2.72	9474	552	180	150	91
MIR	2	CN	250W	A	G	5.0	32	.6	1	2.57	7302	480	156	120	85
MIR	2	ON	225W	A	B	10.0	131	.9	3	2.31	9714	624	270	132	192
MIR	2	CN	200W	A	R	2.5	32	1.9	4	2.32	8718	516	162	132	84
MIR	2	CN	175W	A	G	5.5	161	1.1	2	2.52	8166	534	186	138	104
MIR	2	CN	150W	A		135.0	1760	6.7	8	1.27	16152	906	450	330	256
MIR	2	CN	125W	A	B	35.5	195	.7	5	2.94	14634	798	438	198	321
MIR	2	ON	100W	A	B	45.5	705	1.2	6	1.74	11814	648	282	168	183
MIR	2	CN	75W	A	R	4.0	89	.5	3	2.72	13878	768	276	258	124
MIR	2	CN	50W	A	B	75.0	640	2.1	9	1.65	11670	660	264	144	179
MIR	2	ON	25W	A	B	33.5	160	.4	6	2.53	18114	1008	462	342	261
MIR	2	ON	0W	A		22.5	900	3.2	11	1.82	23616	1194	798	318	611
MIR	3	CS	25E	A	B	44.5	60	.8	4	1.99	16626	1014	468	300	291
MIR	3	CS	50E	A	R	55.0	265	1.4	3	2.16	15234	1134	366	306	186
MIR	3	CS	75E	A	B	435.0	1690	4.3	100	1.21	18438	1146	498	426	247
MIR	3	CS	100E	A	B	550.0	755	4.9	6	.89	15858	924	402	336	204
MIR	3	CS	125E	A	B	19.5	54	.9	2	2.61	13542	1140	348	264	193
MIR	3	CS	150E	A	R	15.5	53	.8	4	2.55	14544	978	336	246	191
MIR	3	CS	175E	A	B	17.5	62	.9	6	2.19	15102	1140	342	324	151
MIR	3	0S	200E	A	B	14.5	40	.8	2	2.51	15174	1176	330	282	164
MIR	3	CS	225E	A	B	9.0	37	.6	3	2.47	15738	1170	354	324	163
MIR	3	CS	250E	A	B	26.0	47	.9	4	2.26	13188	864	312	276	149
MIR	3	5CS	900W	A	B	8.5	22	.7		2.94	0	0	0	0	0
MIR	3	5CS	850W	A	B	18.0	30	.8		2.60	0	0	0	0	0
MIR	3	50S	800W	A	B	255.0	290	1.8	11	1.75	19814	978	582	454	315
MIR	3	5CS	775W	A	B	41.0	183	1.3		2.28	0	0	0	0	0
MIR	3	50S	750W	A	B	20.5	36	.9		2.42	0	0	0	0	0
MIR	3	5CS	725W	A	R	46.0	46	1.0		2.31	0	0	0	0	0
MIR	3	5CS	700W	A		9.5	31	0.8		2.61	0	0	0	0	0
MIR	3	5CS	675W	A	B	14.0	66	1.0		2.47	0	0	0	0	0
MIR	3	5CS	650W	A	B	10.5	29	.7		2.72	0	0	0	0	0
MIR	3	5CS	625W	A	B	43.0	75	1.2		2.90	0	0	0	0	0
MIR	3	5CS	600W	A	B	37.5	98	.8	2	2.23	11456	754	250	230	114
MIR	3	5CS	575W	A	B	12.0	40	.8		2.90	0	0	0	0	0
MIR	3	50S	550W	A	B	16.0	40	.7	2	2.45	14072	876	362	294	189
MIR	3	50S	525W	A	B	88.5	74	1.2		1.80	0	0	0	0	0
MIR	3	5CS	500W	A	B	50.0	79	.8	1	2.30	10634	630	290	248	144
MIR	3	50S	475W	A	B	8.0	17	.8		2.48	0	0	0	0	0
MIR	3	50S	450W	A	B	14.5	19	.6	3	2.85	11396	786	240	206	119
MIR	3	50S	425W	A	W	12.5	13	.5		2.54	0	0	0	0	0
MIR	2	5CS	400W	A	B	5.0	36	.3	3	2.63	7158	468	156	162	60
MIR	2	5CS	375W	A	B	15.0	62	.2	1	2.51	9396	552	198	144	113
MIR	2	5CS	350W	A	B	9.5	49	.2	4	2.54	16056	924	432	270	273
MIR	2	50S	325W	A	B	6.0	71	.2	4	2.61	10812	702	192	294	19
MIR	2	5CS	300W	A	B	11.0	76	.4	1	2.58	13326	696	282	270	123
MIR	2	5CS	275W	A	R	3.0	68	.1	4	2.80	12186	864	294	174	191

CLAIM		CO-ORDS	S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
MIR	2	50S 250W	A	B	3.5	105	.6	4	2.31	12462	888	204	180	98
MIR	2	50S 225W	A	G	8.0	54	.4	4	2.62	15096	888	420	330	226
MIR	2	50S 200W	A	B	13.5	235	1.0	1	2.24	13284	834	312	228	178
MIR	3	50S 175W	A	B	26.5	880	1.7	8	2.68	17742	1182	474	246	329
MIR	3	50S 150W	A	B	13.5	196	.6	5	2.76	13992	936	372	222	241
MIR	3	50S 125W	A	G	185.0	1050	2.4	9	1.63	22344	1038	696	276	533
MIR	3	50S 100W	A	B	31.5	162	.4	4	2.44	15198	774	408	300	231
MIR	3	50S 75W	A	B	21.0	575	.3	5	2.18	10974	786	234	168	135
MIR	3	50S 50W	A	B	19.0	210	.9	7	2.52	14106	858	348	180	242
MIR	3	50S 25W	A	B	6.0	220	1.4	6	2.41	11910	870	144	138	62
MIR	3	50S 00W	A	B	7.0	50	.5	7	2.52	15516	1176	366	282	200
MIR	3	50S 25E	A	B	450.0	440	1.9	5	1.94	19752	996	600	324	409
MIR	3	50S 50E	A	B	43.5	118	.8	4	2.11	13986	894	348	264	193
MIR	3	50S 75E	A	B	235.0	1150	2.1	9	1.82	19110	1014	540	330	346
MIR	3	50S 100E	A	B	17.5	171	.6	4	2.36	14790	948	306	294	133
MIR	3	50S 125E	A	R	10.0	89	.8	3	2.54	15342	1134	342	300	165
MIR	3	50S 150E	A	B	8.0	37	.8	2	2.65	14622	1098	354	258	202
MIR	3	50S 175E	A	B	6.0	28	.4	3	2.59	16044	1140	408	264	253
MIR	3	50S 200E	A	R	23.0	165	1.0	7	2.28	12324	840	294	186	184
MIR	3	50S 225E	A	B	16.0	64	1.0	6	2.16	12420	816	330	222	199
MIR	3	50S 250E	A	B	16.5	48	.8	4	2.40	13644	894	306	288	136
MIR	3	100S 900W	A	B	36.5	42	1.0		2.15	0	0	0	0	0
MIR	3	100S 800W	A	W	12.5	17	.4	3	2.80	15776	1096	352	382	127
MIR	3	100S 850W	A	B	16.0	29	.9		2.50	0	0	0	0	0
MIR	3	100S 750W	A	B	75.5	117	1.4		2.02	0	0	0	0	0
MIR	3	100S 725W	A	B	90.0	370	1.3		1.81	0	0	0	0	0
MIR	3	100S 700W	A	W	14.0	24	.7		2.77	0	0	0	0	0
MIR	3	100S 675W	A	P	9.5	22	1.5		2.86	0	0	0	0	0
MIR	3	100S 650W	A	B	38.5	59	.7		2.25	0	0	0	0	0
MIR	3	100S 625W	A	W	8.5	23	1.2		2.76	0	0	0	0	0
MIR	3	100S 600W	A	G	135.0	161	1.2	5	1.77	16248	1030	432	372	213
MIR	3	100S 575W	A	W	9.0	23	.7		2.60	0	0	0	0	0
MIR	3	100S 550W	A	G	280.0	215	2.0	7	1.43	15252	730	498	388	270
MIR	3	100S 525W	A	B	18.5	60	.8		2.43	0	0	0	0	0
MIR	3	100S 500W	A	B	11.0	35	.5	2	2.44	12204	856	250	256	99
MIR	3	100S 475W	A	B	26.0	38	.9		3.06	0	0	0	0	0
MIR	3	100S 450W	A	B	440.0	260	2.6	6	1.47	15770	790	458	322	268
MIR	3	100S 425W	A	B	140.0	101	.7		2.85	0	0	0	0	0
MIR	3	100S 400W	A	G	125.0	146	2.1	5	1.95	14250	714	492	204	372
MIR	3	100S 375W	A	B	95.0	240	3.2	6	1.72	14220	588	300	282	134
MIR	3	100S 350W	A	B	6.0	36	.8	3	2.56	11868	726	354	138	272
MIR	3	100S 325W	A	B	38.5	205	1.5	6	2.08	11982	780	288	186	178
MIR	3	100S 300W	A	B	4.0	21	.6	6	2.53	15402	1008	300	264	145
MIR	3	100S 275W	A	B	5.0	94	.8	4	2.91	9870	696	168	132	90
MIR	3	100S 250W	A	B	21.0	129	.8	1	2.56	20670	1062	582	444	321
MIR	3	100S 225W	A	B	14.5	205	1.3	2	2.50	6856	480	186	96	129
MIR	3	100S 200W	A	G	10.0	310	1.3	3	2.55	9282	612	264	150	175
MIR	3	100S 175W	A	B	13.5	255	2.1	2	2.68	14226	720	390	276	227
MIR	3	100S 150W	A	B	95.0	535	2.1	1	2.58	26616	1644	774	390	545
MIR	3	100S 125W	A	W	185.0	1210	4.1	7	1.79	19356	1092	546	354	338

CLAIM	CO-ORDS	S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
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MIR 3	100S 100W	A	B	30.5	155	.8	2	2.74	13404	660	312	192	199
MIR 3	100S 75W	A	B	33.5	250	1.0	2	2.42	14154	888	450	198	333
MIR 3	100S 50W	A	D	11.5	114	1.0	5	2.58	12540	822	312	246	167
MIR 3	100S 25W	A	B	13.5	190	.6	6	2.31	18570	816	588	270	429
MIR 3	100S 00W	A	B	9.0	44	.2	5	2.75	14208	1008	300	282	134
MIR 3	100S 25E	A	B	28.5	78	.7	2	2.69	15396	1062	402	312	218
MIR 3	100S 50E	A	B	24.0	43	.7	4	2.69	12420	942	306	186	196
MIR 3	100S 75E	A	R	18.5	65	.8	4	2.70	13536	954	306	312	122
MIR 3	100S 100E	A	B	46.5	255	1.2	6	2.12	18828	1260	486	342	285
MIR 3	100S 125E	A	B	31.0	76	.9	3	2.68	13920	942	294	258	142
MIR 3	100S 150E	A	B	35.0	184	1.1	7	1.95	12060	924	264	210	140
MIR 3	100S 175E	A	B	25.5	55	.8	4	2.09	12726	984	348	258	196
MIR 3	100S 200E	A	B	16.0	31	.7	3	2.49	17508	1062	432	306	252
MIR 3	100S 225E	A	B	47.5	71	.9	3	2.62	26364	1596	666	522	359
MIR 3	100S 250E	A	B	35.0	41	.8	5	1.55	19470	1302	444	468	169
MIR 3	150S 900W	A	B	55.5	70	1.1		2.12	0	0	0	0	0
MIR 3	150S 850W	A	B	37.0	40	.9		1.77	0	0	0	0	0
MIR 3	150S 525W	A	B	54.0	27	1.0		2.16	0	0	0	0	0
MIR 3	150S 800W	A	B	14.5	20	.6	3	2.84	13836	866	320	304	141
MIR 3	150S 600W	A	B	22.0	62	.9	1	2.25	13458	834	350	246	205
MIR 3	150S 550W	A	B	9.0	13	.5	2	2.70	12112	844	242	232	105
MIR 3	150S 500W	A	B	120.0	71	1.3	2	2.05	14526	844	372	302	194
MIR 3	150S 475W	A		6.0	23	0.6		2.43	0	0	0	0	0
MIR 3	150S 450W	A	B	32.0	46	1.0	4	1.82	10200	686	240	240	99
MIR 3	150S 425W	A		33.5	87	0.8		2.76	0	0	0	0	0
MIR 3	150S 400W	A	B	155.0	380	2.8	4	1.88	15654	1152	324	420	77
MIR 3	150S 375W	A	B	16.0	59	.4	2	2.85	19944	1284	534	450	269
MIR 3	150S 350W	A	R	25.5	72	.7	4	2.50	18312	1254	456	474	177
MIR 3	150S 325W	A	B	39.0	140	.7	1	2.80	19032	1140	588	402	352
MIR 3	150S 300W	A	B	31.5	272	1.6	2	1.55	17970	1074	492	312	308
MIR 3	150S 275W	A	B	10.5	190	1.1	3	2.92	14184	750	354	300	177
MIR 3	150S 250W	A	B	26.5	170	.6	1	3.10	17454	1050	366	408	126
MIR 3	150S 225W	A	B	95.0	1395	6.2	2	2.03	15498	744	366	300	189
MIR 3	150S 200W	A	B	20.0	905	3.2	3	2.37	13326	714	288	198	171
MIR 3	150S 175W	A	B	8.0	258	.9	2	2.75	16044	1116	318	426	67
MIR 3	150S 150W	A	R	21.5	118	.6	3	2.35	16236	918	396	324	205
MIR 3	150S 125W	A	B	50.0	652	1.8	3	2.55	13674	1254	528	426	277
MIR 3	150S 100W	A	B	34.5	620	1.8	4	1.85	15006	738	402	330	208
MIR 3	150S 75W	A	B	40.5	270	1.2	2	2.20	14406	948	336	282	170
MIR 3	150S 50W	A	B	13.5	89	.7	2	2.80	14784	780	330	264	175
MIR 3	150S 25W	A	B	17.5	75	1.2	3	2.08	14484	966	360	270	201
MIR 3	150S 0W	A	B	60.0	260	1.1	4	2.08	18744	1056	456	348	251
MIR 3	150S 25E	A	B	60.0	250	1.6	3	2.13	15786	870	522	300	345
MIR 3	150S 50E	A	B	21.0	50	.6	4	2.63	15588	1092	354	234	216
MIR 3	150S 75E	A	B	925.0	1270	3.4	7	1.05	17628	978	432	318	245
MIR 3	150S 100E	A	B	15.0	29	.6	4	2.55	16266	1044	492	312	308
MIR 3	150S 125E	A	B	475.0	1250	3.3	6	1.48	18954	1056	618	312	434
MIR 3	150S 150E	A	B	35.0	305	1.0	4	2.71	15006	1032	342	258	190
MIR 3	150S 175E	A	B	44.5	84	.7	4	2.37	16836	1008	444	342	243
MIR 3	150S 200E	A	B	21.5	44	1.4	2	2.36	12882	900	306	198	189

CLAIM	CO-ORDS	S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
MIR 3	150S 225E	A	B	18.5	80	.9	2	1.92	16980	960	396	330	202
MIR 3	150S 250E	A	B	9.5	53	.6	4	2.35	14232	912	408	282	242
MIR 3	200S 900W	A	B	74.0	35	.9		2.27	0	0	0	0	0
MIR 3	200S 850W	A	B	30.0	41	.9		2.26	0	0	0	0	0
MIR 3	200S 800W	A	B	46.5	47	1.3	3	1.84	14416	1018	320	300	143
MIR 3	200S 600W	A	B	16.0	26	.8	3	2.68	11454	690	246	210	122
MIR 3	200S 550W	A	B	14.0	53	.9	1	2.71	15024	1064	374	248	228
MIR 3	200S 525W	A		11.5	60	1.1		2.78	0	0	0	0	0
MIR 3	200S 500W	A	W	18.5	57	.6	2	2.43	6636	364	186	108	122
MIR 3	200S 475W	A		12.0	45	0.8		2.93	0	0	0	0	0
MIR 3	200S 450W	A	B	48.5	190	1.2	2	2.70	14230	764	354	352	147
MIR 3	200S 425W	A	B	83.0	220	1.8		1.86	0	0	0	0	0
MIR 3	200S 400W	A	B	110.0	568	3.3	6	1.87	16884	882	528	372	309
MIR 3	200S 375W	A	R	30.0	102	.5	2	2.87	18030	1140	396	384	170
MIR 3	200S 350W	A		355.0	990	3.3	7	1.24	19434	1152	582	306	402
MIR 3	200S 325W	A	B	34.5	472	2.1	3	2.62	10200	594	198	216	71
MIR 3	200S 300W	A	B	75.0	895	2.5	6	1.83	9876	660	192	198	75
MIR 3	200S 275W	A	B	75.0	1440	3.4	2	2.96	48294	1998	1626	1020	1027
MIR 3	200S 250W	A	G	55.0	360	3.2	3	2.67	18774	960	480	336	282
MIR 3	200S 225W	A	B	18.5	245	1.1	1	3.04	11502	858	276	210	152
MIR 3	200S 200W	A	B	6.5	102	1.3	2	2.85	11502	792	480	342	279
MIR 3	200S 175W	A	C	80.0	995	4.7	1	1.08	19134	1128	498	360	285
MIR 3	200S 150W	A	B	600.0	920	4.5	3	1.73	15516	966	384	306	204
MIR 3	200S 125W	A	B	20.5	126	.7	4	2.38	20256	1206	606	444	345
MIR 3	200S 100W	A		465.0	820	3.8	3	.90	15066	678	366	270	207
MIR 3	200S 75W	A	B	450.0	1040	4.4	9	1.38	19428	1080	486	450	221
MIR 3	200S 50W	A	B	300.0	545	3.1	6	1.68	16086	888	474	336	276
MIR 3	200S 25W	A	R	12.0	185	.8	1	2.65	17784	1308	468	282	302
MIR 3	200S 00W	A	R	95.0	1225	2.2	10	2.36	18126	834	564	486	278
MIR 3	200S 25E	A	C	24.0	262	1.8	6	3.04	17394	1176	372	312	188
MIR 3	200S 50E	A	B	20.0	133	1.0	2	3.05	16488	966	462	348	257
MIR 3	200S 75E	A	B	19.0	64	.7	4	2.74	20244	1146	564	366	349
MIR 3	200S 100E	A	B	75.0	530	1.2	5	2.35	19056	1134	552	306	372
MIR 3	200S 125E	A	B	42.0	134	.7	2	2.56	18696	1158	528	354	320
MIR 3	200S 150E	A	B	255.0	265	2.9	5	1.93	16716	858	582	282	416
MIR 3	200S 175E	A	B	27.0	71	.6	3	2.70	14712	1122	318	264	163
MIR 3	200S 200E	A	B	34.0	59	.5	2	2.86	17964	1242	456	372	237
MIR 3	200S 225E	A	B	33.0	220	.5	1	2.85	21378	1278	516	420	269
MIR 3	200S 250E	A	B	27.0	81	.4	2	2.99	21918	1404	498	486	212
MIR 3	250S 900W	A	W	8.0	40	.8		2.47	0	0	0	0	0
MIR 3	250S 850W	A	B	44.5	52	.8		2.30	0	0	0	0	0
MIR 3	250S 525W	A	B	19.5	61	.7		3.10	0	0	0	0	0
MIR 3	250S 425W	A	B	470.0	960	3.5		1.20	0	0	0	0	0
MIR 3	250S 800W	A	B	18.5	18	.5	2	2.73	13486	866	308	204	188
MIR 3	250S 750W	A	B	115.0	35	.7	4	2.07	14812	848	376	264	221
MIR 3	250S 700W	A	B	18.5	22	.7	1	2.08	13222	910	318	284	151
MIR 3	250S 650W	A	B	32.0	27	.6	2	2.42	11974	878	270	236	131
MIR 3	250S 600W	A	B	16.5	36	.8	1	2.10	9142	618	186	160	92
MIR 3	250S 550W	A	B	7.0	24	.6	2	2.65	10856	738	236	226	103
MIR 3	250S 500W	A	B	65.0	104	.8	1	2.40	21790	1298	628	412	336

CLAIM		CO-ORDS		S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
MIR	3	250S	475W	A		335.0	1750	3.0		1.23	0	0	0	0	0
MIR	3	250S	450W	A	B	155.0	275	1.2	1	2.24	18732	1128	472	446	210
MIR	3	250S	400W	A	B	230.0	545	2.5	4	1.58	24330	1548	696	426	445
MIR	3	250S	375W	A	B	45.0	315	1.6	2	2.53	16290	918	468	336	270
MIR	3	250S	350W	A	B	38.0	222	1.1	4	2.95	12390	924	282	186	172
MIR	3	250S	325W	A	B	13.0	102	.5	1	3.48	17076	1164	378	330	184
MIR	3	250S	300W	A	B	49.0	565	1.8	3		13614	930	438	252	290
MIR	3	250S	275W	A	B	36.0	980	2.7	1	2.65	12648	804	252	300	75
MIR	3	250S	250W	A	B	15.5	520	2.5	3	2.25	11538	840	234	222	103
MIR	3	250S	225W	A	B	10.0	118	.8	2	2.58	17910	1248	546	240	405
MIR	3	250S	200W	A	B	44.0	652	4.8	3	1.98	19896	1482	420	348	215
MIR	3	250S	175W	A		440.0	4075	9.6	7	1.07	17160	1002	474	384	248
MIR	3	250S	150W	A	B	17.5	378	1.2	3	2.55	14454	1182	342	276	179
MIR	3	250S	125W	A	G	5.0	56	1.2	3	2.58	14226	1092	444	276	281
MIR	3	250S	100W	A	R	14.0	39	1.1	3	2.57	13140	996	288	258	136
MIR	3	250S	75W	A	R	7.5	41	1.2	4	2.87	12906	966	282	216	155
MIR	3	250S	50W	A	B	15.0	41	1.1	3	2.87	13236	1032	378	222	247
MIR	3	250S	25W	A	R	16.0	57	.8	2	2.65	14616	954	288	312	104
MIR	3	250S	00W	A	B	150.0	540	2.4	8	2.18	14820	780	330	264	175
MIR	3	250S	25E	A		490.0	1330	6.1	10	1.49	19572	1170	570	354	362
MIR	3	250S	50E	A	R	10.5	30	1.0	2	2.75	17844	1170	366	420	119
MIR	3	250S	75E	A	B	15.0	29	1.2	2	2.89	15534	1038	384	300	207
MIR	3	250S	100E	A	B	9.5	30	1.0	3	2.74	15342	1104	324	348	119
MIR	3	250S	125E	A	B	15.5	56	1.2	1	2.55	16962	1104	480	312	296
MIR	3	250S	150E	A	B	49.0	316	1.8	4	2.25	14742	930	390	294	217
MIR	3	250S	175E	A	B	50.0	148	1.2	2	2.14	16512	1056	396	324	205
MIR	3	250S	200E	A	B	165.0	462	2.0	6	2.25	18990	1122	468	288	298
MIR	3	250S	225E	A	R	26.5	252	1.4	3	2.55	20982	1488	540	312	356
MIR	3	250S	250E	A	R	22.0	277	1.4	3	2.48	19248	1212	450	402	214
MIR	3	300S	900W	A	W	4.5	20	.6		2.70	0	0	0	0	0
MIR	3	300S	850W	A	W	5.5	21	.6		2.70	0	0	0	0	0
MIR	3	300S	800W	A	B	22.0	26	.9	1	2.90	15794	1074	440	366	225
MIR	3	300S	750W	A	B	40.5	22	.4	3	2.35	20448	1302	554	400	319
MIR	3	300S	700W	A	B	65.0	30	.4	2	2.54	14696	900	342	280	177
MIR	3	300S	650W	A	B	14.0	22	.5	4	2.44	15726	1032	432	336	234
MIR	3	300S	600W	A	B	27.5	50	.6	4	2.30	12376	770	278	242	135
MIR	3	300S	550W	A	B	28.0	24	.7	3	2.45	12006	800	290	240	149
MIR	3	300S	525W	A	B	4.0	29	.8		2.52	0	0	0	0	0
MIR	3	300S	500W	A	B	34.0	92	.8	3	2.02	8970	550	204	148	117
MIR	3	300S	475W	A		83.0	240	1.4		2.10	0	0	0	0	0
MIR	3	300S	450W	A	B	390.0	255	3.8	2	1.47	13548	736	376	270	217
MIR	3	300S	425W	A	W	32.0	51	.6		2.96	0	0	0	0	0
MIR	3	300S	400W	A	B	31.0	145	1.0	3	2.68	16890	972	402	336	204
MIR	3	300S	375W	A	B	65.0	76	1.0	2	2.75	20310	1254	606	402	370
MIR	3	300S	350W	A	B	65.0	53	.8	2	3.15	15180	978	336	366	121
MIR	3	300S	325W	A	G	5.5	75	.8	4	2.70	17514	1134	450	312	266
MIR	3	300S	300W	A	B	17.5	388	1.4	2	3.10	11658	726	198	234	60
MIR	3	300S	275W	A	B	17.0	121	.8	3	2.92	20370	1146	510	408	270
MIR	3	300S	250W	A	B	55.0	430	2.0	4	2.53	17970	1116	378	348	173
MIR	3	300S	225W	A	G	10.5	104	.9	2	2.75	13104	750	342	222	211

CLAIM		CC-CRDS		S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	PCT CHN	URN CHN	TH CHN	URAN STRP
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MIR	3	300S	200W	A	B	39.0	114	1.0	2	2.45	16962	816	456	336	258
MIR	3	300S	175W	A	B	20.5	143	.8	1	2.83	14346	912	342	342	141
MIR	3	300S	150W	A	B	10.5	48	1.5	3	2.84	14028	1194	354	294	181
MIR	3	300S	125W	A	B	9.5	62	1.3	2	2.27	12870	798	240	234	102
MIR	3	300S	100W	A	B	250.0	508	3.2	5	1.83	16830	786	462	246	317
MIR	3	300S	75E	A	B	16.5	48	1.0	4	1.68	12384	1044	258	246	113
MIR	3	300S	50W	A	B	9.5	69	1.2	1	2.53	15294	1080	450	258	298
MIR	3	300S	25W	A	B	12.0	31	1.4	4	2.74	14682	1206	282	318	95
MIR	3	300S	00W	A	B	10.0	23	.8	2	2.50	11982	912	252	204	132
MIR	3	300S	25E	A	B	11.5	28	.9	3	2.28	13758	996	258	210	134
MIR	3	300S	50E	A	B	38.5	39	.8	2	2.32	13890	918	324	300	147
MIR	3	300S	75E	A	B	16.5	48	1.0	4	1.68	12384	1044	258	246	113
MIR	3	300S	100E	A	B	80.0	102	1.5	4	1.84	14994	882	390	216	263
MIR	3	300S	125E	A	B	20.5	22	.8	2	2.62	14010	912	294	276	131
MIR	3	300S	150E	A	B	195.0	620	3.9	3	1.90	21612	1386	618	540	301
MIR	3	300S	175E	A	B	25.0	102	.9	2	2.42	21252	1272	450	462	178
MIR	3	300S	200E	A	B	32.0	136	1.0	2	2.48	23076	1476	630	504	334
MIR	3	300S	225E	A	B	80.0	293	2.2	7	2.16	23652	1452	600	372	381
MIR	3	300S	250E	A	B	31.0	118	1.6	4	2.53	23670	1704	546	630	176
MIR	3	350S	900W	A	B	20.0	56	1.2		2.48	0	0	0	0	0
MIR	3	350S	850W	A	W	6.5	22	.6		2.40	0	0	0	0	0
MIR	3	350S	800W	A	B	15.0	21	.8	3	2.70	15586	1022	482	316	296
MIR	3	350S	750W	A	B	5.0	12	.4	2	3.04	8478	618	210	144	125
MIR	3	350S	725W	A	B	12.5	14	.5	4	2.51	12846	906	318	252	170
MIR	3	350S	700W	A	B	65.0	41	.9	6	1.80	13410	834	318	276	155
MIR	3	350S	675W	A	B	42.0	33	.6	2	2.15	16806	1152	414	354	206
MIR	3	350S	650W	A	B	41.5	24	.6	5	2.07	13602	966	336	270	177
MIR	3	350S	625W	A	B	34.5	20	.4	2	2.30	13842	846	348	246	203
MIR	3	350S	600W	A	B	49.0	53	.6	6	2.20	12246	858	312	240	171
MIR	3	350S	575W	A	B	3.5	13	.6	4	2.62	12078	756	294	210	170
MIR	3	350S	550W	A	B	10.0	38	.8	2	2.02	12846	966	300	246	155
MIR	3	350S	525W	A	B	16.5	42	.8	2	2.23	10038	606	246	138	164
MIR	3	350S	500W	A	B	11.0	18	.6	1	2.33	8196	564	174	144	89
MIR	3	350S	475W	A	B	65.0	132	1.7	3	1.97	13026	642	354	270	195
MIR	3	350S	450W	A	B	525.0	335	4.8	5	1.45	12624	726	312	222	181
MIR	3	350S	425W	A	B	7.0	17	.4	2	2.83	10560	678	222	210	98
MIR	3	350S	400W	A	B	13.5	49	.9	3	2.47	7980	570	210	126	136
MIR	3	350S	375W	A		5.5	42	0.7		2.41	0	0	0	0	0
MIR	3	350S	325W	A		3.5	59	0.9		2.53	0	0	0	0	0
MIR	3	350S	275W	A	B	7.0	200	1.4		2.26	0	0	0	0	0
MIR	3	350S	225W	A		60.0	123	1.1		2.30	0	0	0	0	0
MIR	3	350S	350W	A	B	7.5	18	.7	1	2.75	12204	666	294	238	154
MIR	3	350S	300W	A	B	50.0	410	1.2	1	2.72	13424	856	290	296	116
MIR	3	350S	250W	A	B	43.0	660	1.3	1	2.72	9832	688	228	158	135
MIR	3	350S	200W	A	B	21.0	38	.6	3	2.47	8914	540	250	166	152
MIR	3	350S	175W	A	B	8.0	45	.9		2.24	0	0	0	0	0
MIR	3	350S	150W	A	G	3.0	16	.4	3	2.88	8584	632	192	148	105
MIR	3	350S	100W	A	B	12.0	30	.6	3	1.98	15460	1030	336	290	165
MIR	3	350S	50W	A	B	95.0	39	.5	3	2.98	14640	854	364	274	203
MIR	3	350S	00W	A	B	6.5	28	.5	2	2.21	15616	1150	334	282	168

CLAIM		CO-ORDS		S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
MIR	3	350S	50E	K	B	9.0	32	.8		1.70	0	0	0	0	0
MIR	3	350S	100E	K	B	7.0	28	.6		2.73	0	0	0	0	0
MIR	3	350S	150E	K	B	11.5	59	.8		2.40	0	0	0	0	0
MIR	3	350S	200E	K	B	11.0	98	.8		2.54	0	0	0	0	0
MIR	3	350S	250E	K	B	5.5	109	.8		2.18	0	0	0	0	0
MIR	3	350S	300E	K	B	18.0	105	.8		2.60	0	0	0	0	0
MIR	3	350S	350E	K	B	8.5	81	.9		2.70	0	0	0	0	0
MIR	3	400S	900W	A	B	15.0	26	.7		2.28	0	0	0	0	0
MIR	3	400S	800W	A	Y	15.0	29	.9	4	2.92	14250	876	292	292	120
MIR	3	400S	750W	A	B	265.0	210	1.7	15	1.66	20400	1032	678	372	459
MIR		400S	725W	A							19146	966	528	312	344
MIR	3	400S	700W	A	B	80.0	34	.6	3	2.80	14526	840	354	264	199
MIR	3	400S	675W	A	B	50.0	44	1.1	4	2.00	18186	1128	480	378	258
MIR	3	400S	650W	A	B	80.0	37	.9	2	2.33	15852	984	408	330	214
MIR	3	400S	625W	A	B	14.5	18	.6	5	2.40	10518	720	240	192	127
MIR	3	400S	600W	A	B	5.5	21	.8	4	2.52	8646	576	210	144	125
MIR	3	400S	575W	A	B	27.0	38	.9	3	2.25	13062	900	300	294	127
MIR	3	400S	550W	A	B	10.5	36	.7	3	2.54	14790	1080	294	324	103
MIR	3	400S	525W	A	B	30.5	47	1.0	3	2.14	10950	672	246	204	126
MIR	3	400S	500W	A	B	40.0	49	1.4	3	1.98	8052	522	174	138	92
MIR	3	400S	475W	A	B	90.0	53	.8	2	2.44	9822	516	252	180	146
MIR	3	400S	450W	A	B	85.0	127	1.1	4	2.21	16830	954	444	282	278
MIR	3	400S	425W	A	B	35.0	72	.9	5	2.73	8100	552	156	120	85
MIR	3	400S	400W	A	B	3.0	20	.4	2	2.45	6504	486	102	102	42
MIR	3	400S	375W	A	B	6.5	40	.7		2.82	0	0	0	0	0
MIR	3	400S	325W	A	B	45.0	230	1.8		2.25	0	0	0	0	0
MIR	3	400S	275W	A	B	20.0	85	.8		2.83	0	0	0	0	0
MIR	3	400S	350W	A	B	16.5	38	.6	2	2.50	9210	532	246	174	143
MIR	3	400S	300W	A	B	14.5	129	.8	2	2.20	20704	1244	562	438	304
MIR	3	400S	250W	A	B	25.0	30	.6	2	2.60	9904	456	262	134	183
MIR	3	400S	200W	A	B	11.0	21	.6	3	3.06	12474	954	296	240	155
MIR	3	400S	150W	A	B	14.0	28	.7	2	2.70	17188	1146	390	318	203
MIR	3	400S	100W	A	B	2.5	26	.6	4	2.50	12466	794	298	246	153
MIR	3	400S	50W	A	B	5.5	21	.8	3	2.85	11048	684	208	198	91
MIR	3	400S	00W	A	B	9.0	26	.8	4	2.80	10202	766	226	158	133
MIR	3	400S	175W	A		9.0	38	1.0		2.52	0	0	0	0	0
MIR	3	400S	225W	A		7.5	46	0.7		1.35	0	0	0	0	0
MIR	3	400S	50E	K	B	24.0	54	.9		2.50	0	0	0	0	0
MIR	3	400S	100E	K	B	63.0	187	1.9		2.25	0	0	0	0	0
MIR	3	400S	150E	K	R	35.5	101	1.6		2.27	0	0	0	0	0
MIR	3	400S	200E	K	B	9.5	47	.9		2.30	0	0	0	0	0
MIR	3	400S	250E	K	R	100.0	490	2.8		2.08	0	0	0	0	0
MIR	3	400S	350E	K	R	22.5	375	1.0		2.65	0	0	0	0	0
MIR	3	400S	300E	K	B	26.0	150	1.2		2.60	0	0	0	0	0
MIR	3	450S	900W	A	B	35.0	39	.7		2.32	0	0	0	0	0
MIR	3	450S	850W	A	B	90.0	97	1.6		2.00	0	0	0	0	0
MIR	3	450S	800W	A	O	16.5	26	1.5	2	2.80	10394	688	270	196	154
MIR	3	450S	750W	A	B	19.0	32	.6	3	2.32	12120	732	306	246	161
MIR	3	450S	725W	A	W	8.0	11	.4	1	2.55	13254	852	264	282	98
MIR	3	450S	700W	A	B	7.0	12	.5	2	2.85	10358	804	192	204	72

CLAIM	CO-ORDS	SM	CL	URAN PPM	LEAD PPM	AG	MO	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
MIR 3	450S 675W	A	W	8.0	16	.4	4	2.68	14178	972	348	258	196
MIR 3	450S 650W	A	B	30.5	32	.9	7	2.07	9294	660	246	198	129
MIR 3	450S 625W	A	B	65.0	24	.8	6	2.32	8658	546	174	114	107
MIR 3	450S 600W	A	B	75.0	39	.9	5	2.20	13008	768	348	246	203
MIR 3	450S 575W	A	B	75.0	32	1.1	2	2.15	11742	792	318	192	205
MIR 3	450S 550W	A	B	45.5	27	.9	4	2.02	9396	606	216	156	124
MIR 3	450S 525W	A	C	22.0	31	.9	3	2.25	12888	870	288	258	136
MIR 3	450S 500W	A	B	21.5	27	.6	1	2.07	12414	876	252	216	125
MIR 3	450S 475W	A	B	16.5	36	.7	3	1.97	11316	738	246	204	126
MIR 3	450S 450W	A	B	30.0	30	1.3	7	2.28	8558	564	186	144	101
MIR 3	450S 425W	A	B	37.0	35	.7	5	2.70	9048	672	210	126	136
MIR 3	450S 400W	A	B	65.0	56	1.4	8	2.04	6750	432	156	84	106
MIR 3	450S 375W	A	B	9.5	29	1.0		2.21	0	0	0	0	0
MIR 3	450S 350W	A	B	7.5	31	.6	6	2.42	6700	502	158	126	84
MIR 3	450S 325W	A		6.0	19	0.7		2.52	0	0	0	0	0
MIR 3	450S 300W	A	B	315.0	790	2.5	6	1.66	16848	834	486	196	370
MIR 3	450S 275W	A	W	22.0	86	.7		2.32	0	0	0	0	0
MIR 3	450S 250W	A	W	210.0	370	1.3	3	2.10	19836	1054	566	342	365
MIR 3	450S 225W	A		7.5	38	1.0		2.30	0	0	0	0	0
MIR 3	450S 200W	A	B	8.0	26	1.0	2	2.50	9476	298	218	170	118
MIR 3	450S 175W	A	B	9.5	53	.9		2.45	0	0	0	0	0
MIR 3	450S 150W	A	B	10.5	42	1.0	1	2.42	14526	1048	298	242	155
MIR 3	450S 100W	A	B	7.0	25	.6	2	2.43	11282	910	258	194	144
MIR 3	450S 50W	A	B	115.0	255	1.6	5	2.25	14208	1042	276	264	121
MIR 3	450S 00W	A	B	15.0	33	.6	5	2.00	14406	980	364	276	201
MIR 3	450S 50E	K	B	10.5	44	.8		2.05	0	0	0	0	0
MIR 3	450S 100E	K	B	14.0	235	1.1		2.15	0	0	0	0	0
MIR 3	450S 150E	K	B	12.0	27	.7		2.50	0	0	0	0	0
MIR 3	450S 200E	K	B	11.5	29	.6		2.90	0	0	0	0	0
MIR 3	450S 250E	K	B	68.0	205	1.1		1.90	0	0	0	0	0
MIR 3	450S 300E	K	B	12.0	27	.4		2.52	0	0	0	0	0
MIR 3	450S 350E	K	B	57.0	280	1.6		2.18	0	0	0	0	0
MIR 3	500S 900W	A	B	28.5	56	.9		2.10	0	0	0	0	0
MIR 3	500S 850W	A	B	84.5	69	1.0		2.03	0	0	0	0	0
MIR 3	500S 800W	A	B	12.0	30	1.0	3	2.40	13118	830	352	218	224
MIR 3	500S 750W	A	B	50.0	50	1.1	4	1.53	11976	654	288	228	154
MIR 3	500S 725W	A	B	14.0	22	.5	2	2.56	14430	1008	318	300	141
MIR 3	500S 700W	A	B	10.5	20	.5	3	2.68	12570	738	306	264	151
MIR 3	500S 675W	A	B	6.5	19	.6	3	2.21	10062	720	186	168	87
MIR 3	500S 650W	A	W	9.0	18	.4	3	2.55	11124	840	264	198	147
MIR 3	500S 625W	A	B	12.5	48	1.0	4	1.83	12078	822	282	252	134
MIR 3	500S 600W	A	B	8.0	20	.4	2	2.45	12558	918	306	276	143
MIR 3	500S 575W	A	B	12.0	22	.6	6	2.55	9138	450	222	168	123
MIR 3	500S 550W	A	B	50.0	20	.6	3	2.36	7482	510	138	126	64
MIR 3	500S 525W	A	B	17.5	14	.4	2	2.67	8514	648	150	102	90
MIR 3	500S 500W	A	B	65.0	36	.7	3	1.80	12786	720	324	270	165
MIR 3	500S 475W	A	B	24.0	20	.6	4	2.05	12012	1176	276	252	128
MIR 3	500S 450W	A	B	50.0	28	.8	3	2.25	15270	942	360	288	190
MIR 3	500S 425W	A	B	25.5	26	.4	9	2.13	14922	960	432	276	269
MIR 3	500S 400W	A	B	17.0	16	.5	4	2.53	9822	630	240	138	158

CLAIM	CO-ORDS	S M	C L	URAN PPM	LEAD PPM	A G	M O	SPEC GRAV	TOT CNT	POT CHN	URN CHN	TH CHN	URAN STRP
******	-----*-----*	*	*	-----*****		---***		-----	*****	-----	*****	-----	*****
MIR 3	500S 350W	A	B	19.0	43	1.6	4	1.68	7060	468	148	116	79
MIR 3	500S 300W	A	G	4.5	24	.8	2	2.45	6220	426	118	96	61
MIR 3	500S 250W	A	B	5.5	26	.6	2	2.39	9604	612	230	150	141
MIR 3	500S 200W	A	B	9.5	22	.9	3	2.73	13000	826	296	232	159
MIR 3	500S 150W	A	B	8.0	32	.6	7	2.08	14212	1068	330	262	176
MIR 3	500S 100W	A	B	6.0	30	.7	8	2.33	13184	874	348	246	203
MIR 3	500S 50W	A	B	18.0	24	.6	4	1.90	15754	1096	408	350	202
MIR 3	500S 00W	A	B	125.0	98	1.2	5	1.38	17786	1098	444	288	274
MIR 3	500S 50E	A	B	35.5	94	1.2		1.60	0	0	0	0	0
MIR 3	500S 100E	A	B	7.0	43	.8		2.30	0	0	0	0	0
MIR 3	500S 150E	A	B	16.0	54	1.2		2.44	0	0	0	0	0
MIR 3	500S 200E	A	R	10.0	59	.8		2.23	0	0	0	0	0
MIR 3	500S 250E	A	B	6.5	36	.8		2.35	0	0	0	0	0
MIR 3	500S 300E	A	R	54.0	162	2.0		2.12	0	0	0	0	0
MIR 3	500S 350E	A	B	9.0	54	.8		2.28	0	0	0	0	0

Appendix "B"

SPECTRA 44

SPECIFICATIONS - Console

Analyzers:	One integral channel for total count (T/C) (energy above 0.4 MeV) Three differential channels individually continuous variable from 0.0 MeV to 6.62 MeV for both threshold (E) and window width (ΔE). From the factory set as follows: K-40, peak 1.46 MeV, window width 200 keV. Bi-214, peak 1.76 MeV, window width 200 keV. Tl-208, peak 2.62 MeV, window width 400 keV.
Calibration Source:	Cesium-137 (approx. 1 micro curie)
Calibration:	Separate calibration channel with analogue readout adjusted with lockable potentiometer.
Sample times:	1, 2, 4, 6, 8, 10, 20 and 30 seconds or minutes, selected by switches on front panel.
Functions:	Operate, battery test, calibration and lamp test.
Display:	One 4-digit numerical sequential readout for all four channels (display time 8 sec.).
Sequences:	Start up, sampling, ready, display, automatic switch off.
Batteries:	Twelve replaceable "D" size (1.5 volt) cells contained within the console. Alkaline type is recommended because of the extended life (approx. 40 hours of continuous sampling).
Dimensions:	$3\frac{1}{2}$" x 7" x $10\frac{1}{2}$" (9 x 18 x 27 cm)
Weight:	Console empty: $4\frac{1}{2}$ lbs. (2.0 Kg) Console with 12 alkaline "D" cells - 8 lbs. (3.7 Kg)

SPECIFICATIONS - Detector

The standard detector used is a 3" diameter x 3" thick NaI (Tl) crystal. The crystal is coupled to a high gain photomultiplier tube as a hermetically sealed unit. The complete detector has the preamplifier and high voltage power supply built into a sealed, sturdy aluminum housing. This assembly connects to the instrument console by a plug-on (replaceable) coiled rubber cable.

INVENTORY INSPECTION

When received from the manufacturer, the Spectra 44 should include the following items:

1 Spectra 44 Console	1 each
2 Xtal 33 Detector	1 each
3 Interconnect cable	1 each
4 Recorder cable	1 each
5 Adjustable Console harness and pouch	1 each
6 Detector pouch	1 each
7 Batteries "D" type Alkaline	12 each
8 Calibration Source - C_s 137	1 each
9 Transit Case	1 each

PHONE 980-5814

MIN-EN Laboratories Ltd.
Specialists in Mineral Environments
Corner 15th Street and Bewicke
705 WEST 15th STREET
NORTH VANCOUVER, B.C.
CANADA

ANALYTICAL PROCEDURE REPORTS FOR ASSESSMENT WORK

Procedure for Uranium Analysis:

Rock, soil and silt samples are dried at 110°C and then rocks are crushed and pulverized to -80 mesh.

Soils and silts are sieved and the minus 80 mesh fraction is retained for analysis.

1.000 g. sub-sample is weighed and digested for eight hours with HNO_3 and $HClO_4$.

Then the uranium is separated chemically from other possible interfering ions as Mn,Fe, etc.

After preparation a suitable aliquote is taken and fluxed to form a 1.5 inch diameter discs in platinum dishes.

These salt discs then are compared and measured along with suitable standard with a Jarrell Ash Fluorometer.

The results are calculated accordingly to the sample aliquotes used from standard graphs.

GEOCHEMICAL ANALYSIS BY MIN-EN LABORATORIES LTD.

Samples are processed by Min-En Laboratories Ltd. at 705 W. 15th St., North Vancouver Laboratory employing the following procedures.

After drying the samples at 95°C soil and stream sediment samples are screened by 80 mesh sieve to obtain the minus 80 mesh fraction for analysis. The rock samples are crushed by jaw crusher and pulverized by ceramic plated pulverizer.

1.0 gram of the samples are digested for 6 hours with HNO_3 and $HClO_4$ mixture.

After cooling samples are diluted to standard volume. The solutions are analysed by Atomic Absorption Spectrophotometers.

Copper, lead, zinc, silver, cadmium, cobalt, nickel and manganese are analysed using the CH_2H_2-Air flame combination but the molybdenum determination is carried out by C_2H_2-N_2O gas mixture directly or indirectly (depending on the sensitivity and detection limit required) on these sample solutions.

For Arsenic analysis a suitable aliquote is taken from the above 1 gram sample solution and the test is carried out by Gutzit method using Ag CS_2 N $(C_2H_5)_2$ as a reagent. The detection limit obtained is 1. ppm.

Fluorine analysis is carried out on a 200 miligram sample. After fusion and suitable dilutions the fluoride ion concentration in rocks or soils samples are measured quantitatively by using fluorine specific ion electrode. Detection limit of this test is 10 ppm F.

APPENDIX "D"

PETROGRAPHY

INTRODUCTION

Several mineralized samples were selected from the MIR property for polished/thin section work. This was a preliminary study, and results are tentative. Time did not permit an exhaustive examination, and the sample suite was not adequate for the determination of ambiguous relations. The petrography was done by Dr. K.I. Lu using a Nikon POH microscope.

RESULTS

Abbreviations used:

Crystal Form

- E - enhedral
- S - subhedral
- A - anhedral

Size denotes any number

n = from 1 - 9

Relationship (single)

- * - some
- ** - very common

Mineral

- Sp - Sphalerite
- Mt - Magnetite
- Hm - Hematite
- Cp - Chalcopyrite
- Gl - Galena
- Py - Pyrite

MPA - MIR TRENCH

Opaque mineral approx. 25 vol. %

	Vol. %	Shape	Size (mm)	Relation	Paragenesis
Sp	40+	S-A	0.1-1.2		————————
Mt	40-	E-A	0.0n-0.7	*	- ———————
Gl	13	S-A	0.0n-0.5		————
Hm	5+	S-A	0.0n		—?——
Py	1	E-S	0.0n	*	?
Cp	1-	A	0.00n		- - - - - - - - - - - -
Needle - lathe shaped Goethite	Some	?			- - - - - - -

Note:

1) Although Mt - Sp frequently occur in contact, some Sp are surrounded by Mt, and also Gl rims Mt - Sp grain. (It seems Mt - Sp formed earlier and Gl later.)

2) Needle - lathe shaped Goethite: probably needle - lathe shaped Hm formed first and later altered and converted to Goethite.

3) Hm frequently occurs as a) rim of Mt grain, b) interstices of Mt grains boundaries, c) Mt crystal form.

Also suggested Mt $\xrightarrow[\text{and/or converted}]{\text{alter}}$ Hm

4) In thin section opaque mineral accompanied with dusty quartz (about 30 vol. % in thin section) and carbonate (5 - 10 vol. %).

MIR BL

Opaque mineral approx. 5 vol. %

	Vol. %	Shape	Size (mm)	Relation	Paragenesis
Sp	50	S-A	0.5-1.2+	*	———————
Gl	20	S-A	0.n	*	--------———————
Py	15	E-A	0.n-1+	*	------------------
Hm	10	S-A	0.0n-0.5 aggregates	**	-----------
Mt	5	E-A	"	**	———
Cp	Some	A	0.04	*	----------

Note:

1) Cp mostly occurs as exsolution product in Sp xstal
2) One place shown Mt rimmed by Hm. (Mt converted Hm?)
3) Red spots in polished section are Hm and Hm rimmed by Fe(OH)n (limonite).

Thin section

Holocrystalline (up to 0.6 mm across)

Consisting	35 vol. %	Plagioclase
	40+ vol. %	Orthoclase
	10- vol. %	Quartz
	5 vol. %	Sericite
	5 vol. %	Sphalerite and other opaque mineral
	5 vol. %	Unknown mineral (X)

Unknown mineral (X) has characteristics of strong pleochroism (yellow-brown) and associated with oz. sericite and sphalerite. Requires X-ray identification.

B1/13/7 - MIR TRENCH
(1)

Opaque mineral = 30 vol. % +

	Vol. %	Shape	Size (mm)	Relation	Paragenesis
Mt	29	E-A	0.1-0.8	**	———
Sp	7	A	0.05-0.1	*	—

Note:

With the exception of one grain of Sp, all Sp grains are trapped or surrounded by Mt.

Mt often shows enhedral cube crystal dispersed in the polished section or anhedral aggregate scattered.

Thin section

There are 30 vol. % + fine grain (0.03-0.1 mm) green hornblende-like mineral - similar to Hastingsite - Fe-rich if alkali rich rock, then possibly barkevikite.

BI/13/7 - MIR FLOAT
(4)

Opaque minerals approx. 20 vol. %

	Vol. %	Shape	Size (mm)	Relation	Paragenesis
Sp	35	E-S	0.n-1.0+	*	———— -
Mt	45	E-S	0.0n-0.6±	*	———
Hm	5	E-A	0.0n		——
Gl	15	S-A	0.0n-1.0+	*	—— ----

Note:

Sp as pale greenish-brown containing Gl round grain inclusion, often surrounded by Mt.

A larger number of enhedral hexagonal shaped zonal structured Mt found. Lathe-shaped crystals (probably originally phenocryst replaced by Mt) are also recognized. Several Mt mafic grains contain many minute grained Gl.

Hm occurs as enhedral crystal grain (0.1 mm length) in some, but mostly occurs as rim or fill-in crack (or interstices) of Mt grain (refer to BI/10/7 (1)) in thin section.

Plageoclase (- 60 vol. %) crystals are 60-80% or more altered or decomposed to sericite and carbonate, showing dusty feature; difficult to identify original composition.

Qz (- 15 vol. %) and calcite (- 15 vol. %) show fill-in or replacing textured occurrences. Few chalcedonic (?) quartz grains are recognized.

BI/10/7 - MIR FLOAT
(I)

Opaque mineral approx. 15 vol. %

	Vol. %	Shape	Size (mm)	Relation	Paragenesis
Gl	10-	S	0.0n-0.4±	*	---- ------
Sp	4-	S-A	up to 0.6		--------
Mt	4+	E-A	up to 0.6		- -------
Hm	6+	E-A	0.0n-0.n		--------
Cp	One grain		0.08	*	?

Note:

Large number of hexagonal-shaped zonal structured Mt crystals are found which probably formed by Mt replaced or converted (?) from hexagonal-shaped crystals (Hm?). Hexagonal-shaped Mt again, in turn, converted to Hm from rim (or outer zone) or crack toward the core of crystal. Most are 1/3 of outer zone converted to Hm but some are wholly converted to Hm (made of occurrence similar to BI/13/7 (4) but that section has much less conversion).

CONCLUSIONS

The main conclusions from the petrographic work are:

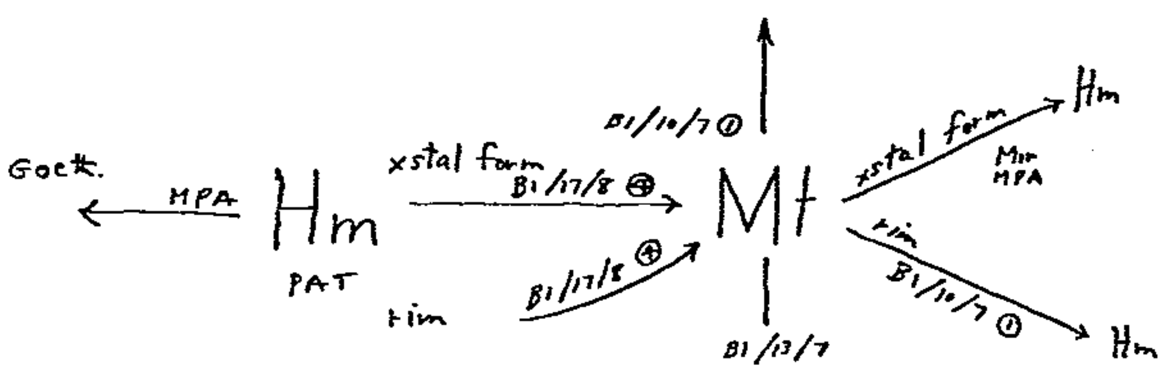
1) That sulphide mineralization is characteristic of polymetallic hydrothermal veins.

2) That mineralization is of the telethermal type. Closest analogy is Wölsendorf uranium deposit located in Germany.

3) That the hydrothermal mineralization sequence involved first deposition of hematite under high PO_2 conditions followed by magnetite under low PO_2 and finally by hematite.

4) That quartz is intimately involved in the mineralization sequence.

Paragenetic relationships are summarized in the diagram below:



APPENDIX "E"

MIR PROPERTY

RADON CIRQUE GRID

MULTI-ELEMENT DATA

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$COPY VIEWANCCC(1,,2)
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LISTING OF MULTI-ELEMENT ANALYSES

********* FIRST OF TWO PARTS *********

SAMPLE	MO	CU	PB	ZN	NI	CO	AG FE	TH	AS	MN	PH	BI	CD	F
A1WT14	3	15	29	130	12	9	0624000	47	9	150	5.5	16	0.8	500
C1SLA1	7	37	11	160	11	9	0917000	27	6	190	5.5	21	0.3	47
A1ET15	6	14	7	42	16	12	0612500	14.5	4	200	6.7	18	0.3	530
SHEER	4	6	49	59	14	7	0410000	42.0	4	160				
DIXORG	7	65	130	370	16	15	1036000	69.0	166	425				
DIX SH	2	91	83	615	12	13	0725000	89.5	460	105				
DIX LK	13	114	33	125	15	12	0921000	29.0	40	110				
DIXMOS	7	52	94	335	16	17	0733000	80.0	140	400				
IDAHC4	5	84	21	100	10	10	1217000	24.0	6	230				
ASWP15	3	22	36	118	14	13	0927000	73	13	260	4.5	27	0.1	490
CIND11	42	143	19	120	67	14	1217000	19	4	210		36	0.3	69
K1J1	12	28	16	55	20	13	1317000	31	3	260	6.2	38	0.5	730
K13E1S	8	205	66	510	37	14	4032000	81	17	680	5.1	47	2.4	2110
**** ZAPU CLAIMS AREA ****														
C1ELB6	13	15	80	330	14	8	1816000	97	42	220	5.9	22	1.0	2390
C1EL6B	52	30	205	220	11	10	2826500	126	81	340	5.1	33	0.1	302
B1SF15	6	124	270	390	50	14	4122000	110	230	220	5.4	34	2.5	2115
CZAP15	20	114	500	250	260	26	5034000	73	108	720		40	4.9	1130
C1ZAP6	8	27	230	245	32	14	2221000	100	69	400	5.2	28	2.3	232
P20	3	7	14	52	30	11	0411500	40	20	180	6.7	23	0.7	1100
**** SLA ANOMALY AREA ****														
CSLA10	5	44	21	92	106	19	1030500	37	8	510	5.4	37	0.5	750
CSLA11	5	86	16	80	140	18	2022000	34	6	560	4.9	35	1.2	1060
SLA12B	4	63	25	82	190	22	1724500	31	10	550	5.4	38	0.8	64
CSLA13	3	40	9	60	120	21	1222500	16	9	460	5.6	33	1.0	335
**** TUPA ANOMALIES ****														
C1TUP3	3	17	22	65	21	12	1020500	31	5	250	4.4	25	0.2	505
T66S80	6	11	29	155	16	10	0920000	84	4	550		30	0.4	555
CTUP11	6	36	23	65	68	11	1015000	21	13	540	5.6	27	0.3	75
CTUP35	6	132	47	320	91	24	2842000	14.5	9	980	5.4	59	1.4	1750
CTUP33	7	24	14	75	34	13	1124000	126	2	400	4.5	30	0.1	660
**** ZENAZIE CREEK (MIR 8) REGION ****														
A1MZ83	15	27	37	185	20	21	1827500		4	400		36	1.4	
K1MZ20	6	41	56	165	12	10	1524000	365	28	290	5.1	31	0.2	152
CZEN5A	12	127	260	1700	20	17	2535000	152	270	1780	4.3	49	20.3	2055
**** NORTHERN GRABEN ****														
CLIN44	18	102	52	470	48	24	2844000	50	34	2200		52	5.4	
CLIN21	18	186	162	540	64	30	3645000	134	338	1080		53	2.0	
CLIN32	8	41	57	260	34	13	1824000	50	28	250	4.9	35	0.5	166
MGS32	11	60	72	750	39	21	1736000	31	33	1420	5.1	46	3.7	2640
Z074	7	124	98	335	44	18	2925500	40	24	260		36	4.0	1370
**** SOUTHERN GRABEN ****														
B1GRB1	10	340	350	2900	49	16	7633000	97	14	490		47	12.1	1975
LIN5	5	72	52	360	17	19	0825500	32.5	10	380				

LIN4B	8	90	27	108	15	16	3017000	40.0	10	285				
CLIN40	15	108	320	720	42	18	10226000	74	10	1860		42	29.0	
GAMMA	11	134	65	295	71	25	2331000	42	13	380	5.0	52	1.2	188
CLIN77	7	178	39	210	32	12	1415000	37	6	140		26	5.1	1610
[illegible]N72A	14	206	32	110	48	18	3430000	29	8	320		48	3.4	
[illegible]HT	6	172	68	320	36	24	2830400	25	8	300		35	4.6	
CLIN10	36	520	48	190	38	20	4826000	67	38	280		48	3.2	
CLIN74	44	500	86	290	62	28	5848000	134	59	740		49	0.4	
CLIN83	12	2650	4900	280	26	24	17345000	63	600	380	4.5	56	1.6	363[illegible]
LIN84A	9	280	290	910	30	12	7317500	200	6	130		37	9.9	
CLIN96	17	275	134	605	27	17	12826000	110	23	640	4.5	33	7.2	1560

**** RADON CIRQUE AREA ****

AMR192	10	275	1280	660	47	21	5535000	19	23	1080		44	7.9	1950
AMR128	9	195	4600	2600	24	17	12634000	21	33	1040		46	11.9	
KIMR74	9	100	520	355	14	12	2022000	137	64	195	4.6	28	0.4	2005
1600N	6	58	1400	1150	13	10	2120500	45.5	5	200				
NO NBR	13	70	1250	1560	20	18	2238500	78.0	58	580				
M14AUG	7	26	108	160	19	15	1020000	11.5	6	300				
M SOIL	41	100	1500	2300	8	11	2519000	87.5	34	860				
M 13	4	78	4300	800	18	21	3918000	107.5	14	160				
M13AUG	7	115	7200	920	19	24	3429500	100.0	34	200				
M14-2W	5	108	2400	1000	17	18	3930000	91.0	62	460				

**** DETAILED STUDY DATA-- RADIUM COLD SPRINGS ****

AC 0	5	126	1480	840	36	20	5342000	182	34	680		37		5.3
AC 5	6	59	610	830	26	11	2836000	165	34	470		41		2.[illegible]
AC 10	3	34	355	525	15	9	1727000	89	10	260		31		1.7
AC 15	7	76	635	1100	32	18	3954000	160	37	650		51		3.9
AC 25	6	80	500	1210	31	15	3547000	117	24	480		45		3.[illegible]
[illegible]35	6	74	765	1080	29	12	2137000	146	20	210		44		2.6
[illegible]	4	32	540	490	18	5	1915000	115	20	165		26		1.0
BC 15	7	46	435	1010	29	12	1926000	132	41	440		32		1.[illegible]
BC 45	8	22	285	405	12	8	1218000	77	15	270		28		0.9
BC 65	6	50	645	1210	26	11	2827000	150	47	400		39		2.6
BC 20	6	24	475	380	13	10	1319000	112	25	660		34		1.[illegible]
CC 0	5	116	2200	1010	20	10	5533000	205	62	460		44		10.1
CC 8	18	100	870	2500	13	9	2817000	167	28	150		35		2.3
CC 15	10	102	2400	1880	35	18	5737000	245	110	1280		52		6.[illegible]
AD 0	11	74	700	630	29	16	2442000	120	30	700		42		2.7
AD 4	5	30	340	390	18	8	1521000	100	20	360		38		0.9
AD 10	3	27	350	380	20	9	1325000	97	22	420		28		0.[illegible]
AD 25	7	88	540	1050	39	21	3250000	100	27	680		49		3.4
BD 0	5	36	670	600	20	18	2315500	148	33	220		32		1.2
BD 15	4	28	355	750	22	12	1625000	117	36	480		31		1.[illegible]
BD 45	4	52	765	935	24	12	3330000	155	44	460		32		2.3
BD 65	3	51	740	1250	19	17	2728000	155	53	520		32		2.0
CD 0	4	36	480	560	11	10	2118000	173	46	230		27		1.
CD 8	76	91	1200	1690	19	11	2819500	177	47	380		44		1.9
AH-1		95	482	515			47			420				
BH-1		36	565	285			22			125				
CH-1		118	1820	820			36			560				
BD-1		26	340	605			12			200				
CD-1		68	955	870			30			350				
AH		94	680	670			40			530				
AH 4		82	630	880			44			980				
5		90	930	1290			44			1640				
AH 16		73	620	910			38			770				
AH 25		104	730	925			38			630				
AH 35		110	745	1270			53			400				

BH 15		57	495	795			20			530
BH 45		63	1240	670			34			900
BH 65		53	685	790			34			340
CH 15		102	1790	1860			60			1450

* 1976 SOIL ORIENTATION-- RADON CIRQUE ****

SOIL 1	2	12	205	3700	5	6	07 6000	40.0	4	72
SOIL 2	6	35	600	400	14	18	1331000	22.0	10	1500
KM 1	4	38	82	380	28	10	0732500	51.0	50	220
KM 2	5	24	50	230	22	11	0827500	43.5	36	220
KM 3	5	55	1050	1300	12	9	2334000	36.0	54	1680
KM 4	4	26	104	182	30	12	0830000	17.0	61	550
KM 6	4	15	41	76	29	8	0719000	8.0	26	330
KM 7	4	31	80	190	19	10	0823000	42.0	62	290
KM 8	5	21	45	106	18	9	0822500	25.5	44	210
KM 9	6	19	44	118	36	10	0725000	22.0	30	240
KM 10	6	49	96	440	210	16	1029500	15.5	18	1020
KM 11	7	16	39	107	25	8	0724000	20.5	12	380
KM 12	11	98	114	400	32	12	1736000	51.0	72	400
KM 13	7	21	50	120	24	9	0823500	15.5	17	420
KM 14	7	19	68	132	20	10	1027000	24.0	14	250
KM 15	8	54	66	166	28	10	1026500	22.0	16	840
KM 16	10	20	46	132	36	9	0721500	25.5	12	260
KM 17	10	20	62	136	22	11	0826000	25.5	14	360
KM 18	10	16	98	194	26	12	1031000	24.0	14	460
KM 19	11	12	100	192	18	10	1027000	22.0	21	270
KM 20	9	20	87	126	25	11	0826500	13.5	11	300
KM 21	8	32	172	162	44	10	1025500	11.0	10	490
KM 22	6	44	220	168	34	13	1139000	15.5	8	600
KM 23	11	98	1300	580	24	12	2440000	42.0	27	770
24	4	28	360	440	15	9	1541000	61.5	36	220
25	6	32	410	710	16	10	1330000	43.5	33	340
KM 26	4	26	320	740	24	10	1428000	42.0	20	330
KM 27	10	49	580	1270	28	15	2054000	36.0	26	860
KM 28	4	16	148	260	16	10	0927500	43.5	15	270
KM 29	4	16	210	300	12	11	0819000	49.5	11	190
KM 30	7	35	560	890	42	14	1247500	54.5	40	640
KM 31	6	14	34	200	20	10	0831000	29.5	8	240
KM 32	4	23	29	114	18	9	0718500	47.0	8	320
KM 33	3	11	20	88	14	8	0621200	31.0	8	420
KM 34	4	11	56	94	27	10	0829300	33.0	10	230
B0+00	4	28	29	65	26	10	0928000	22.0	8	240
B 1N	4	45	21	58	18	9	0622000	17.0	3	160
B 2N	5	27	32	64	23	13	0739000	20.5	3	350
B 3N	5	32	24	69	16	9	0621500	20.5	8	180
B 4N	4	32	37	99	27	10	0723000	38.5	6	280
B 5N	5	44	33	88	24	10	0626000	34.5	3	230
B 6N	4	24	24	55	17	11	0825000	15.5	4	240
B 7N	6	54	29	85	18	10	0524500	29.5	10	210
B 8N	6	36	50	127	16	13	0831000	27.5	10	350
B 9N	4	42	32	94	26	9	0419000	33.0	10	230
B 10N	7	64	28	81	19	9	1023500	27.5	45	260
B 11N	8	30	24	73	26	12	0825500	18.5	33	290
B 12N	8	60	33	124	24	10	0927000	27.5	10	240
B 13N	7	21	20	86	12	9	0715500	36.0	11	120
B 14N	4	31	30	72	31	12	0826500	18.5	8	290
5N	9	32	34	92	46	18	0845000	25.5	10	490
B 16N	8	40	35	90	44	15	0938000	22.0	10	380
B 17N	9	32	56	200	60	14	1037500	34.5	20	420
B 18N	5	30	28	87	43	10	0926000	10.0	8	490

B 19N	6	30	42	175	88	12	0735000	18.5	8	580				
B 20N	4	23	40	225	81	13	0621000	25.5	11	310				
B 21N	6	30	180	900	56	11	0833000	56.5	23	420				
B 22N	7	28	200	570	47	13	1029000	34.5	17	300				
B 23N	6	24	198	460	37	11	0824500	22.0	17	280				
[illegible]N	7	20	430	350	51	12	1025000	25.5	17	520				
B 25N	6	15	90	340	26	10	0617000	27.5	8	260				
B 26N	9	11	90	300	46	7	0618000	40.0	10	240				
B27N	8	94	1120	1700	49	20	2059000	61.5	29	840				
B28N	6	21	210	220	27	12	1429000	17.0	6	580				
B29N	4	12	205	186	56	7	0619000	40.0	10	260				
B30N	4	19	120	167	26	8	0821500	18.5	6	220				
B31N	4	14	90	230	34	7	0710500	29.5	11	180				
B32N	6	16	88	320	31	9	0724000	33.0	6	320				
B33N	6	39	230	188	44	13	1136000	18.5	6	570				
B34N	6	25	150	148	68	12	1033000	13.5	3	300				
B35N	4	18	120	240	59	11	0926000	18.5	8	310				
B36N	3	24	124	215	35	9	0924500	27.5	6	240				
B37N	5	32	250	225	60	10	0831500	33.0	12	320				
B38N	2	16	98	200	51	7	0721000	17.0	8	210				
B39N	7	106	250	620	62	12	2135500	63.5	18	320				
B40N	4	50	210	370	28	10	0831500	25.5	15	240				
**** RCCKS ANC MINERAL SPECIMENS ****														
IRA TR	4	900	104	1620	16	22	4047500	46	4	480	5.5	89	1.8	6400
SNOB20	12	172	170	138	12	12	4022000	65	1450	260		83	3.1	
SNOB21	3	18	410	325	13	11	2057000	46	24	600		31	0.8	
SNOB21	2	5	111	420	11	9	1141000	70	4	1300		22	4.1	
SNOB22	4	48	70	640	21	20	2298000	42	1	1400		66	0.7	
SNOB23	1	10	240010400		12	10	4521000	70	1	1200		19	63.5	
[illegible]LT	3	20	420	107	10	6	18 8500	72	5	380		13	0.7	
[illegible]	3	391740012900			19	17	4251000	70	1	7800		20	78.5	
MPC 2	2	2551520012800			11	11	4432000	58	2	8500		16	81.5	
B11376	16	480675001870			32	28	645099999	132	124400			460	68.0	
B1-117	5	99	3700	1700	7	8	5023000	40	4	440	5.4	22	4.1	660
SNOWBD	130	84	3500	1550	6	7	2033000	46	32	2500	5.4	31	4.7	10[illegible]
LBOCM1	12	142	3500	230	8	5	220 4900	70	23	60	5.0	31	1.9	1710
BPATC2	21	195	700	140	6	6	57 9600	46	1700	100	5.1	16	27.8	1160
B1IRA1	12	715	1240	2550	19	22	5147000	27	11	600	5.4	96	6.9	166[illegible]
C1HUS1	23	57	154	820	41	31	2042000	640	2311200		6.7	62	2.9	595

$SIG

$COPY VIEWANOCC(2,,2)

LISTING OF MULTI-ELEMENT ANALYSES

********* SECOND OF TWO PARTS *********

SAMPLE	U	U3O8	CXU	CXPB	CXCA	LOI	S.G.		RADON	HE	LOCATION
A1 WT 14	5.5	30	10.5	2	1500	7.2	2.58		2		MIR II CREEK
C1 SLA 1	42.5	40	37	3	2500	19	1.81		2		HORSE CR AREA
A1 ET 15	3.0	10	3.5	2	1900	5.1	2.71		2		MPLA CREEK
SHEER	18.5						2.555	1	5		
DIXORG	100								2		DIXIE LK CR
DIX SH	50								4		DIXIE SHEAR SOIL
DIX LK	40								1		DIXIE LK SED
DIXMOSS	80								2		DIXIE CR BELOW MO
IDAHC4	160								3		IDAHO SPRING
A1 SWP 15	42.5	60	26	2	200	15.5			2		SWAPC CR
C1 IND 11	265	350	210	3	16000	39.5	1.30		1		INDIAN LIN LAKE
K1 J1	105	540	425	4	8500	33	1.82		1		JEN ANOMALY
K1 3E1S	600	650	400	8	2000	25	1.64	6	4		IRA LIN SOIL
**** ZAPL CLAIMS AREA ****											
C1 ELB 6	58	90	50	9	3500	5	2.6	9	2		LITTLE ELBOW CR
C1 ELB 6B	215	360	270	14	5500	7.2	1.93	9	375846	36.2	BOCM SPRINGS
B1 SNF 15	530	590	455	52	4500	14.5	1.77	9	377572	29.8	RUBY SPRINGS
C1 ZAP 15	610	830	500	48	6000	49	2.20	9	4		RUBY AREA LIN.
C1 ZAP 6	140	150	260	60	6000	13.2	2.14	9	349151	29.8	N ZAPU SPRINGS
C1 ZAP 20	9	20	8.5	3	2000	5.1	2.60	9	2		RUBY TRIB
**** SLA ANOMALY AREA ****											
C1 SLA 10	1050	1180	950	3	5500	12.5	2.34	8	2		SLA NORTH SPR
C1 SLA 11	4500	4480	3350	14	6000	63.1	0.94	8	3		SLA CENTER SPR
C1 SLA 12B	4050	3540	2550	8	7500	39.5	1.45	8	3		SLA SOUTH SPR
C1 SLA 13	680	460	470	4	7600	20	1.98	8	2		CRK FARTHER SOUTH
**** TUPA ANOMALIES ****											
C1 TUP 3	7.5	20	8.5	2	2000	5.1	2.22	5	3		E TUPA SPRING
T66 S80E	13.5	50	17.5	4	150	11.5	1.93	5	2		E TUPA CR
C1 TUP 11	730	1950	1300	4	8500	32	1.15	5	3		TUPA SPRINGS
C1 TUP 35	1200	1880	1200	5	7000	19.2	1.68	5	4		TUP LIN SOIL
C1 TUP 33C	305	360	215	2	2800	4.1	3.01	5	4		TUP LIN SAND
**** ZENAZIE CREEK (MIR 8) REGION ****											
A1 MZ 83	105						0.40	4	2		ZENAZIE CAMP CR
K1 MZ 20	490	590	380	9	4200	8.5	2.07	4	2		ZENAZIE SPRING
C1 ZEN 5A	300	310	150	100	4000	21.5	1.42	4	4		ZENAZIE R/A SOIL
**** NORTHERN GRABEN ****											
C1 LIN 44	930	1050	600	5	8000		0.72	3	1		TRIFLE LKS
C1 LIN 21	840	890	370	4	6500		1.47	3	4		OMEGA LINEAMENT
C1 LIN 32	300	210	180	9	3700	17.5	1.77	3	2		SIGMA SWAMP CR
MGS 32	350	350	140	2	4000	20.1	1.57	3	4		LOWER GRABEN SOIL
ZC 74	370	400	310	13	6500	38.5	1.95	3	113286	36.2	ZETA R/A POOL
**** SOUTHERN GRABEN ****											
B1 GRB 1	1150	1470	1150	102	8500	36.5	1.40	2	4		ABOVE GAMMA LK
LIN5	410							2	3		GAMMA TRENCH

LIN4B	700							2	4			GAMMA TRENCH
C1 LIN 40	580	630					0.72	2	3			GRABEN SPRING
GAMMA	1000	2180	840	8	6000	32.2	1.68	2	3	9951	33.1	GAMMA LK BY SPRIN
C1 LIN 77	1650	1880	1650	10	8000		0.88	2	1			BETA LK
C1 LIN 72A	2450		2600		1214000		1.37	2	4			S OF BETA LK
750 MHT	2850	2490	2100	32	4700		0.70	2	4			RADON CR SOIL
C1 LIN 10	1850	2120	1800	18	5200			2	3			ALPHA SPRINGS
C1 LIN 74	1650		1600		1510000		0.90	2	6			ALPHA SPR WASH
C1 LIN 83	1100	1360	260	860	1200	27.5	1.08	2	4			DELTA LIN SOIL
C1 LIN 84A	1150	1640	1000		16010100		0.90	2		182856	42.8	DELTA POOL
C1 LIN 96	1200	1770	850		2812000	60.1	1.23	2	5			DELTA SOIL

**** RADON CIRQUE AREA ****

A1 MR 192	925	1020	500	205	3500		1.05	1	5			RADON GRID SOIL
A1 MR 128	440	710	380	2800	5200		1.07	1	5			RADON GRID SOIL
K1 MR 74	800	820	950	198	1700	10	1.82	1	3			350S 200E RADON G
1600N	295							1	3			N OF SPRING 'D'
NC NBR	260							1	2			SPRING 'C' CRK
M14AUGER	12							1	2			AUGER BY 'C' SPRI
M SOIL	170							1	4			MIR AREA SOIL
M 13	800							1	2			RADON GRD 100SW
M13AUGER	1080							1	4			M13 AUGER SAMPLE
M13 2W	1150							1	3			SPRING IN SW RADO

**** DETAILED STUDY DATA-- RADIUM COLD SPRINGS ****

AC 0	600		200	90	3800	35	1.50	1		356671	39.6	RADON SPRING 'A'
AC 5	200		100	72	2600	15	1.41	1	2			CREEK BELOW
AC 10	155		58	45	2050	17	1.06	1	2			
AC 15	425		145	86	3200	22	1.14	1	2			
AC 25	290		78	76	2900	26	1.35	1	2			
AC 35	225		63	126	2000	30	0.85	1	2			
BC 0	120		73	89	1700	12	1.90	1		348877	26.7	RADON SPRING 'B'
BC 15	68		34.5	76	1300	17	1.54	1	2			CREEK BELOW
BC 45	50		20.5	49	800	6	1.63	1	2			
BC 65	135		50	122	1400	17	1.71	1	2			
BC 20	115		60	88	1000	6	2.46	1	2			
CC 0	830		235	350	2200	21	1.63	1	3			
CC 8	205		68	160	1900	8	1.74	1	2			
CC 15	275		116	570	4000	15		1	2			
AD 0	235		93	47	1900	12	2.21	1		335587	36.4	RADON SPRING 'C'
AD 4	70		41.5	26	1000	5	2.31	1	2			CREEK BELOW
AC 10	70		24.5	38	1000	5	2.36	1	2			
AD 25	195		50	58	2200	16	2.05	1	2			
BD 0	245		70	124	1500	10	1.86	1	3			
BD 15	68		31	66	1000	8	2.12	1	2			
BD 45	140		63	132	1800	15	1.58	1	2			
BD 65	125		40.5	134	1200	16	1.79	1	2			
CD 0	175		68	66	1000	6	2.23	1		364169	36.4	RADON SPRING 'D'
CD 8	215		60	154	1500	7	1.88	1	2			CREEK BELOW
AH 1	78		14	49	1300	32	1.38	1	3			RADIUM SPR BANK S
BH 1	225		70	144	2500	29	1.64	1	3			
CH 1	940		250	405	2400	20	1.70	1	3			
BD 1	63		26.5	63	1600	12	2.08	1	3			
CD 1	310		225	220	2300	19	2.21	1	3			
AH	1060		365	122	6000	52	1.32	1	3			
AH 4	530		98	117	7000	59	0.95	1	4			
AH 15	315		110	123	3700	29	1.60	1	4			
AH 16	270		60	82	5600	43	1.20	1	4			
AH 25	110		37.5	96	3300	32	1.63	1	4			
AH 35	325		83	120	4000	30	1.36	1	4			

BH 15	90	44.5	78	1800	15	1.41	1 4
BH 45	215	53	220	3200	23	1.82	1 4
BH 65	100	50	140	2600	21	1.75	1 4
CH 15	330	105	540	4300	38	1.12	1 4

**** 1976 SOIL ORIENTATION-- RADON CIRQUE ****

SOIL 1	35.5		1 5	MIR AREA SOIL
SOIL 2	50		1 5	MIR AREA SOIL
KM 1	15	1.900	1 5	1976 RADON CIRQ S
KM 2	9	2.150	1 5	
KM 3	40.5	2.352	1 5	
KM 4	8.5	2.100	1 5	
KM 6	7.5	2.050	1 5	
KM 7	15	3.100	1 5	
KM 8	10	2.602	1 5	
KM 9	14	2.350	1 5	
KM 10	30	1.850	1 5	
KM 11	10	2.300	1 5	
KM 12	44.5	2.250	1 5	
KM 13	15	2.900	1 5	
KM 14	13.5	2.200	1 5	
KM 15	15.5	2.352	1 5	
KM 16	16	2.950	1 5	
KM 17	13.5	3.100	1 5	
KM 18	12.5	1.750	1 5	
KM 19	9	2.605	1 5	
KM 20	9.5	2.200	1 5	
KM 21	37	2.050	1 5	
KM 22	31.5	2.300	1 5	
KM 23	150	1.802	1 5	
KM 24	80	2.550	1 5	
KM 25	60	2.355	1 5	
KM 26	90	2.900	1 5	
KM 27	230	2.100	1 5	
KM 28	49	2.850	1 5	
KM 29	70	2.305	1 5	
KM 30	135	2.300	1 5	
KM 31	15	2.100	1 5	
KM 32	18.5	2.900	1 5	
KM 33	13.5	2.400	1 5	
KM 34	15	2.350	1 5	
B0+00	13	2.150	1 5	1976 RADON CIRQ S
B 1N	15	2.550	1 5	
B 2N	10	2.450	1 5	
B 3N	21.5	2.605	1 5	
B 4N	23	2.200	1 5	
B 5N	19.5	2.902	1 5	
B 6N	10.5	2.750	1 5	
B 7N	19.5	2.550	1 5	
B 8N	26.5	2.300	1 5	
B 9N	23.5	2.200	1 5	
B 10N	26.5	2.600	1 5	
B 11N	18.5	2.500	1 5	
B 12N	15	2.500	1 5	
B 13N	18.5	2.550	1 5	
B 14N	11.5	2.700	1 5	
B 15N	9	2.200	1 5	
B 16N	33	2.300	1 5	
B 17N	18.5	1.900	1 5	
B 18N	7.5	2.050	1 5	

B 19N	22.5						2.350	1	5	
B 20N	23						2.500	1	5	
B 21N	47.5						1.950	1	5	
B 22N	60						2.100	1	5	
B 23N	25						1.805	1	5	
B 24N	12.5						2.050	1	5	
B 25N	11.5						3.000	1	5	
B 26N	18.5						2.600	1	5	
B 27N	125						2.250	1	5	
B 28N	12.5						2.055	1	5	
B 29N	22.5						3.000	1	5	
B 30N	9						2.950	1	5	
B 31N	17						2.500	1	5	
B 32N	13						2.400	1	5	
B 33N	27.5						2.050	1	5	
B 34N	10						2.200	1	5	
B 35N	15						2.550	1	5	
B 36N	10						2.650	1	5	
B 37N	12.5						2.500	1	5	
B 38N	9						2.300	1	5	
B 39N	32.5						2.000	1	5	
B 40N	12.5						2.455	1	5	

**** ROCKS AND MINERAL SPECIMENS ****

IRA TRENCH	365	510	26.5	13	2500	4.2	2.15	6	9	MIN SAMPLE
SNOB20	70							4	8	SNOWB ZEUN SHOW
SNOB21	31.5							4	8	SOUTH OF SNOB
SNOB21A	15							4	8	
SNOB22	5							4	8	
SNOB23	15.5							4	8	NW OF RADON
MP BALT	17.5							1	9	RADON GRID PITS
MPC	23.5							1	9	RADON GRID PITS
MPC 2	16.5							1	9	RADON GRID PITS
B1 13 76	83							1	9	RADON GRID PITS
B1-11-7-1	14.5	30	3.5	1600	1000	1		1	9	MAIN MIR TRENCH
SNOWBIRD	1400	2890	95	560	4000	3.1		4	9	MIN SAMPLE
L1 BOOM 1	110	110	6.5	270	700	2.5		9	8	ALT ROCK N OF ZAP
B1 PATO 2	1000	1090	140	48	200	1.1	2.61	7	9	NEW PATO SHOW
B1 IRA 1	410	410	43.5	154	3200	4.4		6	8	IRA TRENCH ROCK
C1 HUS 1	18	40	5.5	61	1000	41.2			8	HUSSELBE PROP ROC

$SIG

6776

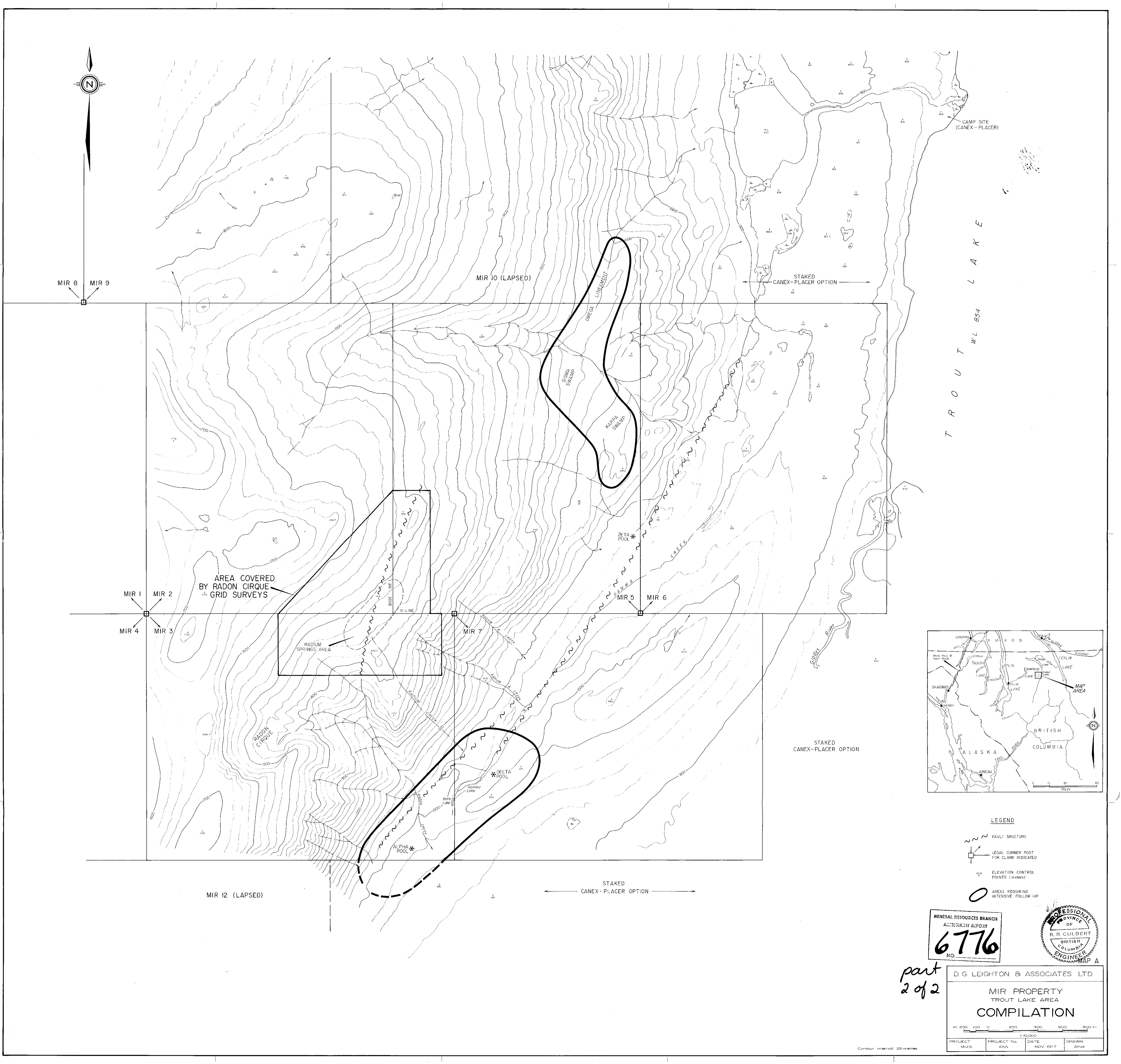
PARTS 1+ 2 of 2

'78-#180-#6776

MAPS TO ACCOMPANY REPORT
ON THE MIR PROPERTY

By
D.G. Leighton and
R.R. Culbert, PhD., P.Eng.

15 May 1978



MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
NO. 6776

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
R. R. CULBERT

part 2 of 2

MAP A

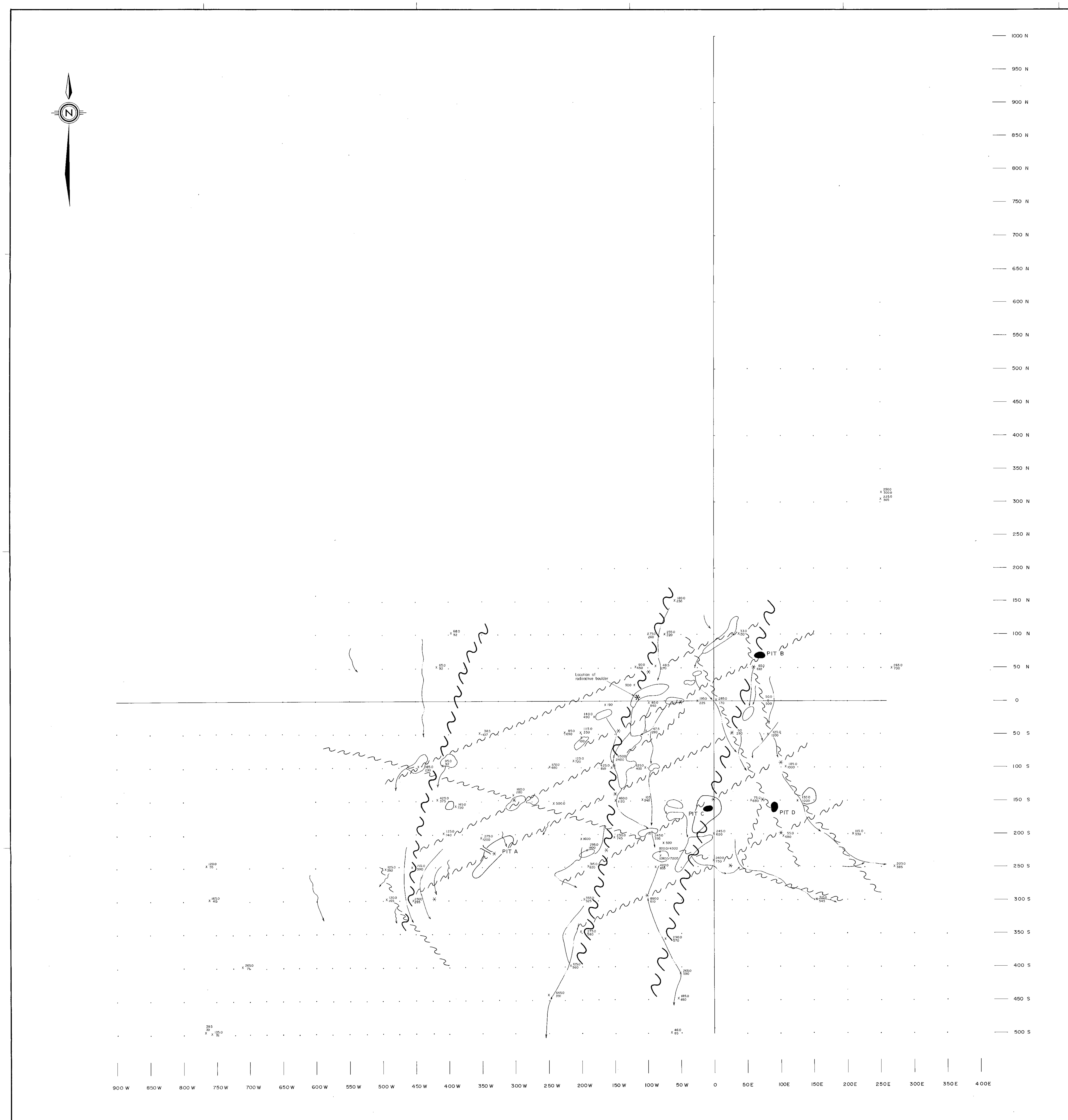
D.G. LEIGHTON & ASSOCIATES LTD.

MIR PROPERTY
TROUT LAKE AREA

COMPILATION

m. 200 100 0 200 400 600 800 m.
1:10,000

PROJECT	PROJECT No.	DATE	DRAWN
M.U.G.	101A	NOV. 1977	Altair



LEGEND

- GRID STATION
- ✳ LINEAMENT MARKERS
- SPRING SEDIMENT (p.p.m.) — URANIUM 115.0 x LEAD 330
- SPRING (WET AREA)
- PRIMARY LINEAMENT
- SECONDARY LINEAMENT
- AREA OF ABUNDANT MINERALIZED FLOAT (Pb, Zn, Mn)
- TEST PITS

part 2 of 2

PROFESSIONAL ENGINEER — PROVINCE OF BRITISH COLUMBIA — R. R. CULBERT

4B

D. G. LEIGHTON & ASSOCIATES LTD.

MIR PROPERTY
RADON CIRQUE AREA
SPRING GEOCHEMISTRY
(STRUCTURE)

SCALE IN METRES
50 0 50 100 150
1:20

PROJECT	PROJECT No.	DATE	DRAWN
MUG	101 A	DEC. 1977	Altair

MAP C
D. G. LEIGHTON & ASSOCIATES LTD.
MIR PROPERTY
RADON CIRQUE GRID
SOIL URANIUM
METRES 50 0 50 100 METRES
1:2000
PROJECT M.U.G.
PROJECT No. 101A
DATE DEC. 1977
DRAWN Altair
LEGEND
x135 SOIL URANIUM IN PPM.
HUNDREDS OF METERS WEST
HUNDREDS OF METERS EAST
HUNDREDS OF METERS NORTH
HUNDREDS OF METERS SOUTH
BASE LINE
"O" LINE
MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
6776
NO.
part 2 of 2
PROFESSIONAL
PROVINCE OF
R. R. CULBERT
BRITISH COLUMBIA
ENGINEER


HUNDREDS OF METERS WEST
HUNDREDS OF METERS EAST
HUNDREDS OF METERS NORTH
HUNDREDS OF METERS SOUTH
BASE LINE
"0" LINE
MAP D
D. G. LEIGHTON & ASSOCIATES LTD.
MIR PROPERTY
RADON CIRQUE GRID
RESIDUAL SOIL URANIUM
METRES 50 0 50 100 METRES
1:2000
PROJECT M.U.G.
PROJECT No. 101A
DATE DEC 1977
DRAWN Altair
LEGEND
RESIDUAL URANIUM AFTER THAT PREDICTED BY ORGANICS REMOVED
MINERAL RESOURCES BRANCH ASSESSMENT REPORT
NO. 6776
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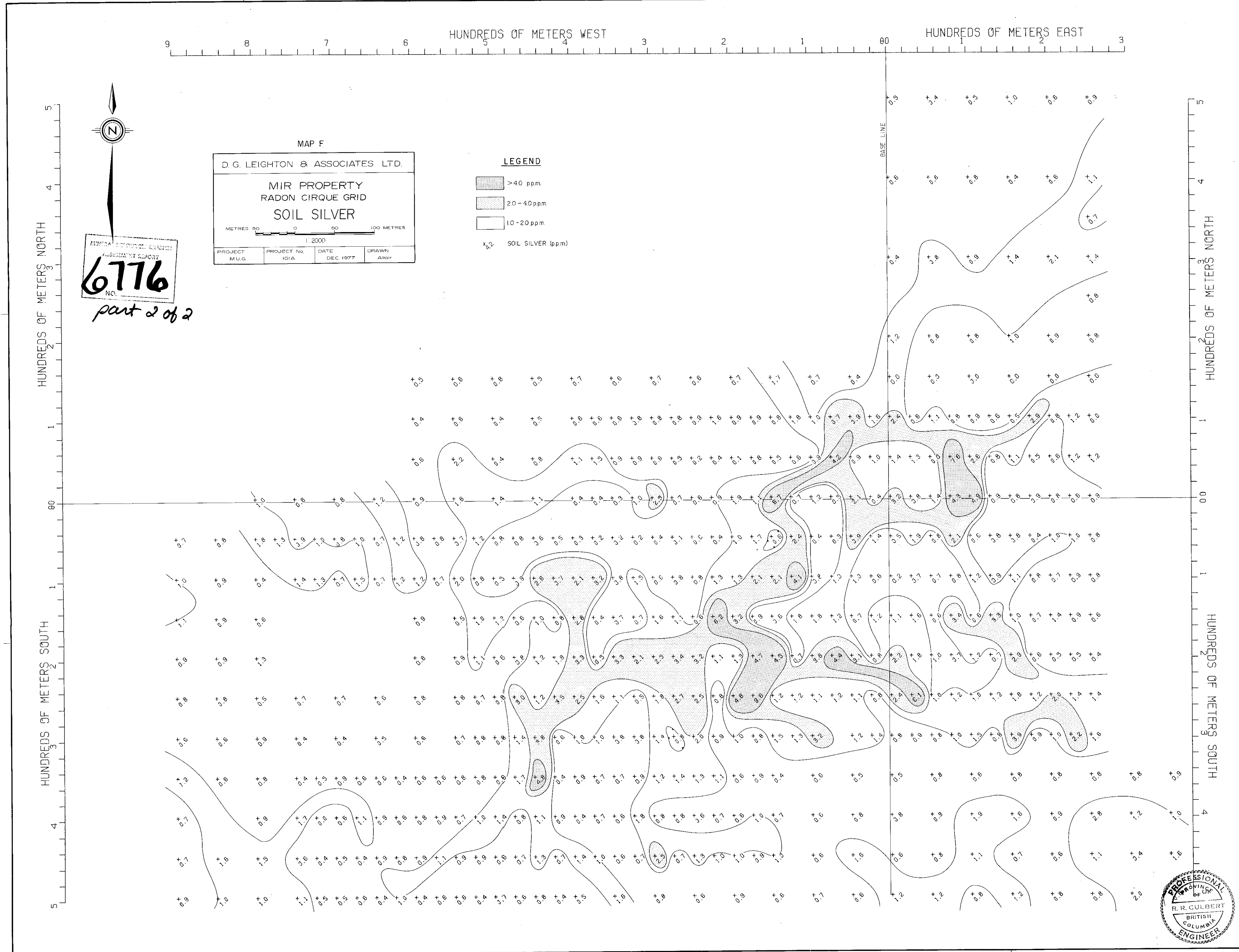
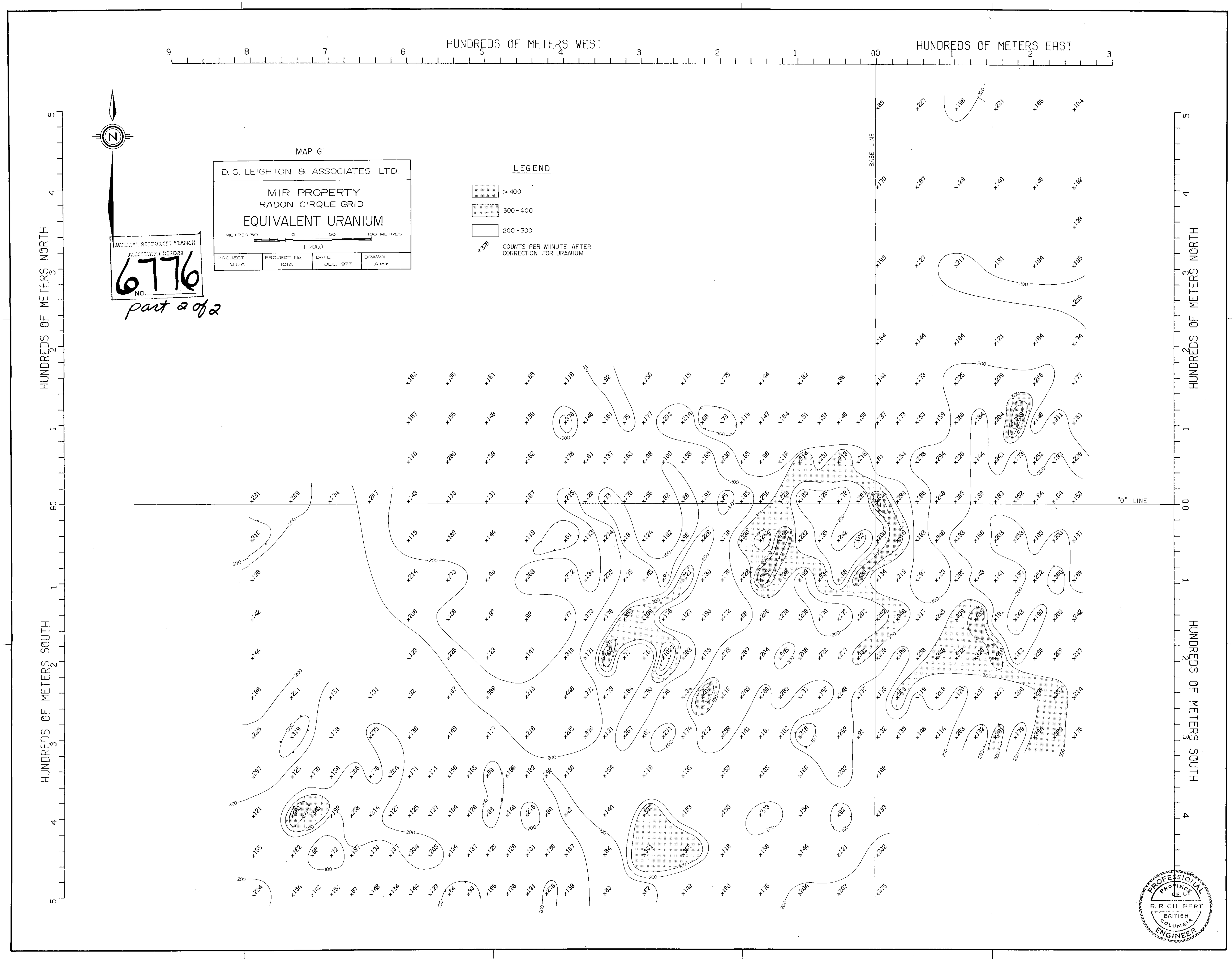
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
R. R. CULBERT

HUNDREDS OF METERS WEST
HUNDREDS OF METERS EAST
HUNDREDS OF METERS NORTH
HUNDREDS OF METERS SOUTH
BASE LINE
"O" LINE
MAP E
D. G. LEIGHTON & ASSOCIATES LTD.
MIR PROPERTY
RADON CIRQUE GRID
SOIL LEAD
METRES 50 0 50 100 METRES
1: 2000
PROJECT M.U.G.
PROJECT No. 101A
DATE DEC. 1977
DRAWN Altair
LEGEND
>2000 p.p.m.
1000 - 2000 p.p.m.
500 - 1000 p.p.m.
100 - 500 p.p.m.
SOIL LEAD (p.p.m.)
ASSESSMENT REPORT
6776
part 2 of 2
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
R. R. CULBERT


MAP F
D. G. LEIGHTON & ASSOCIATES LTD.
MIR PROPERTY
RADON CIRQUE GRID
SOIL SILVER
METRES 50 0 50 100 METRES
1: 2000
PROJECT M.U.G.
PROJECT No. 101A
DATE DEC. 1977
DRAWN Altair
LEGEND
>4.0 p.p.m.
2.0 - 4.0 p.p.m.
1.0 - 2.0 p.p.m.
x 4.2 SOIL SILVER (p.p.m.)
HUNDREDS OF METERS WEST
HUNDREDS OF METERS EAST
HUNDREDS OF METERS NORTH
HUNDREDS OF METERS SOUTH
BASE LINE
N
MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
6776
NO.
part 2 of 2
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
R. R. CULBERT



MAP G
D. G. LEIGHTON & ASSOCIATES LTD.
MIR PROPERTY
RADON CIRQUE GRID
EQUIVALENT URANIUM
METRES 50 0 50 100 METRES
1: 2000
PROJECT M.U.G.
PROJECT No. 101A
DATE DEC 1977
DRAWN Altair
LEGEND
> 400
300 - 400
200 - 300
x 378 COUNTS PER MINUTE AFTER CORRECTION FOR URANIUM
HUNDREDS OF METERS WEST
HUNDREDS OF METERS EAST
HUNDREDS OF METERS NORTH
HUNDREDS OF METERS SOUTH
BASE LINE
"O" LINE
MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
6776
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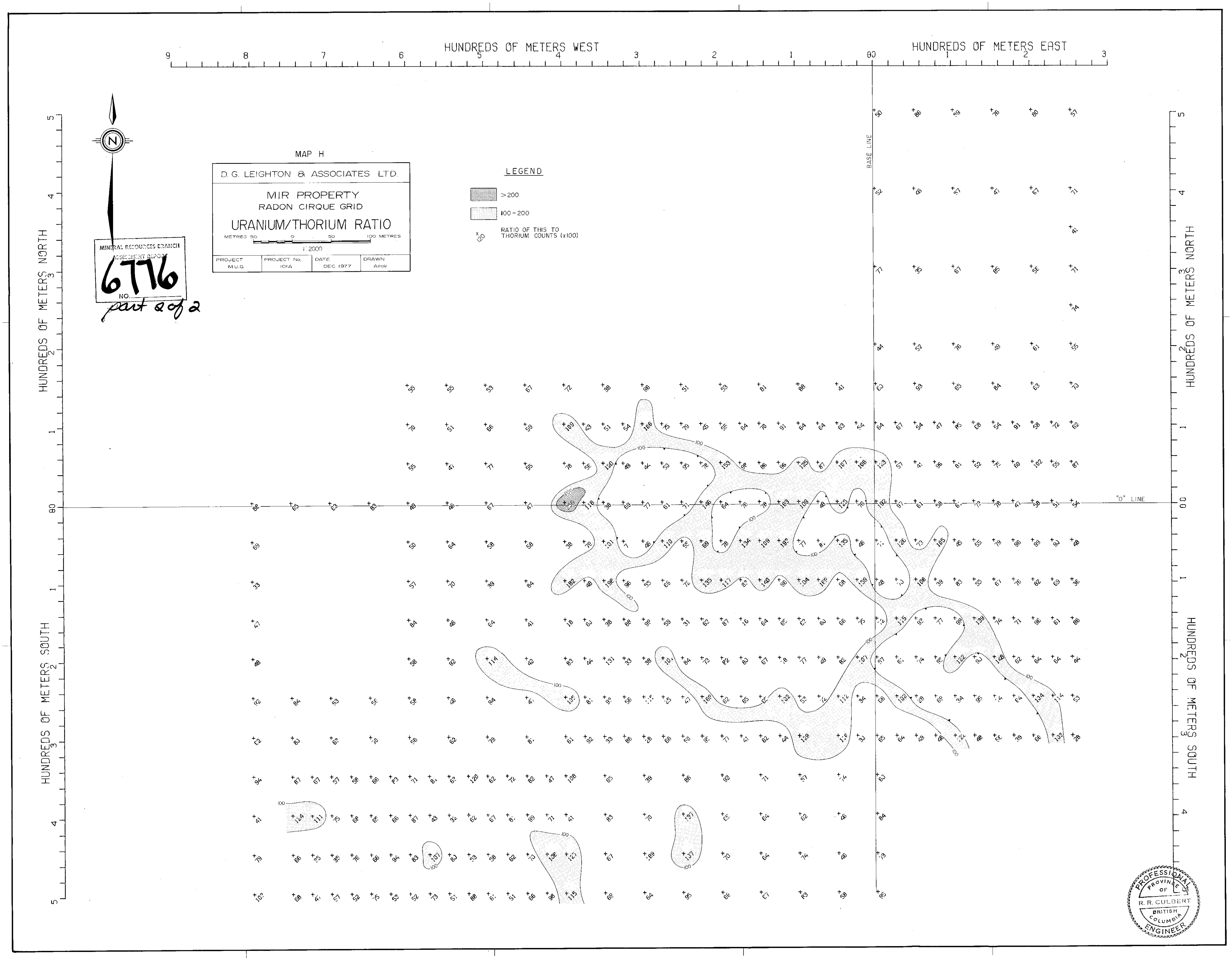
PROFESSIONAL ENGINEER
PROVINCE OF
R. R. CULBERT
BRITISH COLUMBIA



HUNDREDS OF METERS WEST
HUNDREDS OF METERS EAST
HUNDREDS OF METERS NORTH
HUNDREDS OF METERS SOUTH
BASE LINE
"O" LINE
MAP H
D. G. LEIGHTON & ASSOCIATES LTD.
MIR PROPERTY
RADON CIRQUE GRID
URANIUM/THORIUM RATIO
METRES 50 0 50 100 METRES
1:2000
PROJECT M.U.G.
PROJECT No. 101A
DATE DEC. 1977
DRAWN Altair
LEGEND
>200
100-200
RATIO OF THIS TO THORIUM COUNTS (x100)
MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
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ENGINEER