ASSESSMENT REPORT

EAGLE CLAIMS

BRITISH COLUMBIA

93J/1

MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
NO. 7388

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I. Property

Shell Canada Resources Limited has 9 contiguous mining claims consisting of 88 units. These claims are:

Eagle 1: Consisting of 12 units recorded on June 12, 1978.

Eagle 2: Consisting of 10 units recorded on June 12, 1978.

Eagle 3: Consisting of 12 units recorded on June 12, 1978.

Eagle 4: Consisting of 8 units recorded June 12, 1978.

Eagle 5: Consisting of 16 units recorded June 12, 1978. 58

Eagle 6: Consisting of 8 units recorded on June 12, 1978.

Eagle 7: Consisting of 6 units recorded on June 12, 1978.

Eagle 8: Consisting of 16 units recorded on July 17, 1978.

Eagle 9: Consisting of 4 units recorded on July 17, 1978.

Assessment credit applied for in this report is for the whole of the 88 units.

2. Location and Access

The Eagle Claims are located approximately 3 kilometres southeast of Giscome, British Columbia. The claims are accessed via abundant logging roads from Giscome.

Figure 1 shows the location of the Vama Claims with respect to Giscome.

3. Work Completed

The Eagle claims were worked intermittently from July 1, 1978 to August 27, 1978. The exploration target was volcanogenic massive sulphide type mineralization.

A 1:100,000 scale map is included in this report as Figure 1 showing regional geology, claim groups and grid locations.

The exploration activity on the Eagle claims was conducted as portion of a ground follow-up programme of EM anomalies generated by an airborne EM survey flown by Questor for Shell Canada Resources Limited in February of 1978. The programme conducted on the Eagle claims consisted of line cutting, grid controlled geological mapping, grid controlled geophysical surveys and grid controlled soil geochemical surveys.

Three grids were cut on the Eagle claims for a total of 74.7 line kilometres.

All grids were geologically mapped at a scale of 1 cm = 25 metres. The purpose of the mapping was to outline felsic volcanic horizons and to gather detailed stratigraphic and structural information. The geological grid maps are included in this report as Figures 2 to 4.

All grids were subjected to soil geochemical surveys. Samples were taken from the B_1 soil horizon at 50 metre intervals and analysed for copper, lead and zinc. 1,465 soil samples were taken. Contoured 1:2500 scale grid maps are included as Figures 5 to 13.

Crone Shootback EM surveys were run on all grids at 25 metre station intervals. The VLF-EM method was used to back up the Shootback EM system on grid 78-11 at 12.5 metre station intervals. Grids 78-10 and 78-11 were surveyed by a ground magnetometer at 12.5 metre station intervals. Shootback profiles are included as Figures 14 to 16. The VLF-EM contour map is included as Figure 17. Mag profile maps for Grids 78-10 and 78-11 are included as Figures 18 and 19.

4. Geology

4.1 General

The following geological summary is based on reconnaissance and detailed mapping during 1977 and 1978 by Shell personnel and on maps and reports from the Geological Survey of Canada (G.S.C. Report of Activities Paper 70-1, Part A; Campbell, et al, 1973) and the British Columbia Department of Mines (Southerland Brown 1977; Minister of Mines and Petroleum Resources Annual Report - 1967).

Contacts with the Slide Mountain where observed are high angle or thurst faults. The Group's basal formation rests with fault (?) contact on Cambrian Caribou Group metasediments, in the southeast and eastcentral areas and on Wolverine Complex metamorphic rocks east of Giscombe. A fault defines the western contact of the Slide Mountain's upper formation with Mesozoic sedimentary and volcanic rocks of the Eastern Group. Lower Jurassic felsic (Topley?) intrusions outcrop along the western contact and on the northeastern contact near Giscombe. A Table of Formations is presented as Table 1.

Slide Mountain Group rocks occupy the centre of the Black Stuart Synclinorium, a northwest to southeast trending structural trough situated roughly between Giscombe and Barkerville. The intervening area has a breadth of approximately 35 kilometres characterized by three northwest to southeast trending geomorphic features. From east to west they are: The Bowron River basin, a shallow broad basin underlain by sedimentary and minor volcanic rocks followed by a mountainous, mainly tholeiitic volcanic backbone rising sharply from the Bowron basin to maximum height of 1800 metres which falls off sharply into the Willow River Basin, another broad shallow basin underlain by volcanic rocks with intercalated sediments.

The Slide Mountain Group is divisible into two lithologic units; a lower mainly sedimentary unit, the Guyet Formation, and a dominantly tholeiitic volcanic upper unit, the Antler Formation. An average thickness for the Group is considered to be around 1400 metres (Table 2). Favourable felsic volcanic horizons are postulated to occur within middle sequences of the Antler Formation. The rocks are metamorphosed from zeolite lower greenschist facies.

Regional geology is plotted on a 1:100,000 scale compilation map included as Figure 1. Detailed geology is presented on 1:2,500 scale grid maps included as Figures 2 through 4.

TABLE 1
TABLE OF FORMATIONS

ERA	PERIOD	SERIES	FORMATION	LITHOLOGY	INTRUSIVES	ROCK UNITS WITH NO ASSIGNED TIME CLASSIFICAT
CENOZOIC	TERTIARY	MIOCENE	ENDAKO GROUP	BASALT, ANDESITE, RELATED TUFF AND BRECCIA; CONGLOMERATE; SANDSTONE, MUDSTONE, LIGNITE, DIATONINE	TOPLEY INTRUSIONS QUARTZ MONZONITE MONZONITE, GRANITE, MINOR DIORITE	WOLVERINE METAMORPHIC COMPLEX (FAULT CONTACT)
			FAULT CONTACT			
	CRETACEOUS OR TERTIARY		BOWRON RIVER COAL BEDS	CONGLOMERATE, BRECCIA SANDSTONE, SHALE, COAL		
			FAULT CONTACT (?)			
MESOZOIC	TRIASSIC AND/OR JURASSIC					
			FAULT CONTACT			
			EASTERN GROUP	ARGILLITE, GREYWACKE; GREEN, GREY, BLACK, AND PURPLE ANDESITE, BASALT AND RELATED TUFF AND BRECCIA; MINOR CONGLOMERATE AND LIMESTONE		
			FAULT CONTACT			
			TAKLA GROUP	ANDESITE TO BASALT TUFF BRECCIA AND FLOWS; MINOR CONGLOMERATE GREYWACKE ARGILLITE AND LIMESTONE		
			FAULT CONTACT			
PALEOZOIC	PENNSYLVANIAN		EASTERN ASSEMBLAGE SLIDE MOUNTAIN GROUP ANTLER FORMATION	BASALT AND ANDESITE, PILLOWS, TUFF, BRECCIA RHYOLITE, RHYODACITE, DACITE, BRECCIA AND PYROCLASTICS MINOR DIORITE AND GABBRO CHERT ARGILLITE AND LITHIC SANDSTONE		
			GUYET FORMATION	ARGILLITE, LITHIC, SANDSTONE CONGLOMERATE, MINOR, BASALT AND MINOR LIMESTONE		
			FAULT CONTACT			
	DEVONIAN		BLACK STUART FORMATION	BASALT; CHERT BRECCIA, DOLOMITE BRECCIA ARGILLITE LIMESTONE, SANDSTONE		
			UNCONFORMITY			
	CAMBRIAN AND EARLIER		CARIBOO GROUP	GREY MICACEOUS QUARTAITE, PHYLLITE, ARGILLITE		
			MURAL FORMATION	LIMESTONE, SHALE, PHYLLITE		
			UNCONFORMITY			
PROTEROZOIC			KAZA GROUP	FELDSPATHIC SANDSTONE		
			UNCONFORMITY			

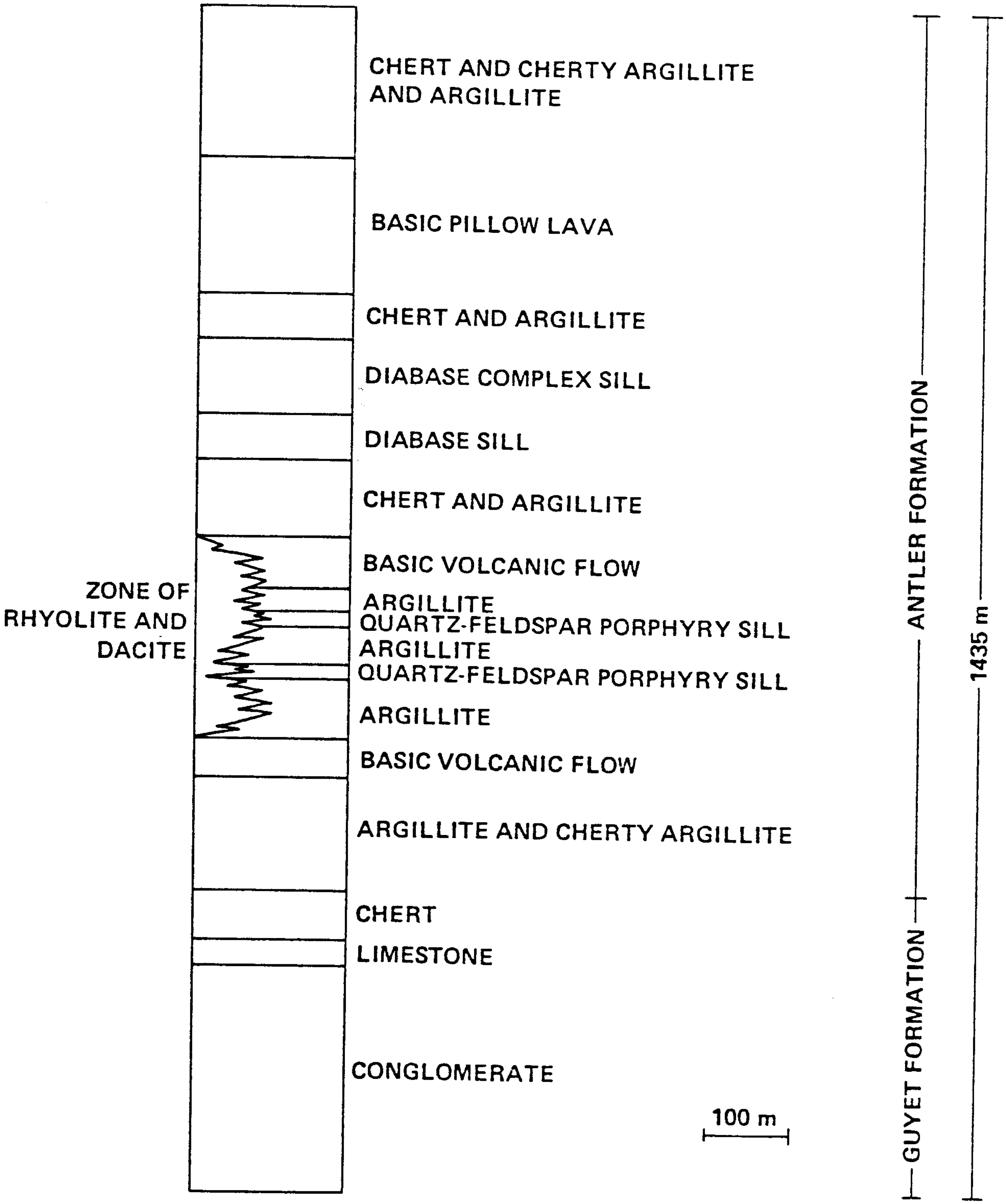


TABLE 2
SLIDE MOUNTAIN GROUP
PROPOSED STRATIGRAPHIC SECTION

4.2 Lithologies

4.2.1 Pre Upper Paleozoic Rocks

4.2.1.1 Kaza Group

Slide Mountain Group rocks unconformably overlie the Kaza Group directly east of Purden Lake and northwest of Barkerville.

The lithology is of a metamorphic character being mostly feldspathic sandstone, granule conglomerate ("grit"), argillite and minor limestone.

4.2.1.2 Cariboo Group

A profound unconformity exists between the Slide Mountain Group and rocks of the Cariboo Group, specifically Mural Formation carbonates. This is the case south of Purden Lake extending east along the Bowron River beyond Barkerville.

Cariboo Group rocks are a metamorphosed sedimentary sequence of pebble conglomerate, feldspathic and quartzose sandstone, argillite and carbonate rocks.

4.2.1.3 Black Stuart Formation

The Black Stuart Formation is limited in extent, outcropping north of Indian Lake and southeast of Wells near Barkerville.

Dark argillaceous rocks with minor carbonate and chert are characteristic of the Formation which is in fault contact with the Slide Mountain Group.

4.2.2 Upper Paleozoic Rocks

4.2.2.1 Slide Mountain Group

The Upper Paleozoic Slide Mountain Group outcrops within the axis of the Black Stuart Synclinorium. The Guyet Formation and the Antler Formation comprise the lower sedimentary and upper volcanic units, respectively, of the Group. Late Paleozoic thrusting is thought to be responsible for emplacing the Slide Mountain Group into its present position. The Group is metamorphosed from zeolite to greenschist grade. Internal structures and stratigraphy are not well known, especially within the project area. To the east the Guyet Formation lies with fault contact on either Lower Devonian carbonates of the Black Stuart Formation or on Lower Cambrian Metasedimentary shales of the Cariboo Group. On the western limit the Antler Formation is overlain by Upper Triassic volcanic and sedimentary rocks of the Eastern Group with a faulted contact.

4.2.2.2 Guyet Formation

The Guyet Formation is a dominantly sedimentary unit of greywacke suite rocks. A massive dark-grey to brown polymictic pebble and granule conglomerate is the main unit. Lesser chert, cherty argillite, and crinoidal limestone are included. Mississippian age crinoids have been found in the limestone member.

The upper contact is placed at the highest course clastic bed in the Slide Mountain Group. While the lower contact is not seen. (Campbell et al, 1973).

Locally the conglomerate grades from a normal conglomerate to one with a volcanic matrix, to agglomerate. The conglomerate is usually silicified to an almost uniform cherty rock. Quartz porphyry sills have been described within the conglomerate. Outcroppings of the Guyet Formation are described only in the Wells-Barkerville area, with an estimated thickness of the Formation there of from 300 to 400 metres (Southerland Brown 1957). The general strike of the Formation is northwest to southeast with a variable dip.

As the structural fabric of the area underlain by the Slide Mountain Group is poorly defined, it is likely that the Guyet Formation is more extensive than previously thought. Outcrops in the Bowron River Basin, for example, are mostly argillites, cherty argillites, and sandstone and may represent portions of the Guyet Formation.

The extent to which the Guyet Formation underlies the Willow River Basin is not known. Descriptions of Guyet Formation conglomerates do however bear striking resemblance to those rhyolites of a volcanoclastic nature found within the project area near Highway 16.

4.2.2.3 Antler Formation

The Antler Formation is a volcanic unit of Mississippian to pre-Upper Triassic island arc tholeiitic pillows, breccias, and pyroclastics with intercalated sediments. These rocks outcrop within the Willow River Basin and are the primary unit underlying the project area.

Argillite, cherty argillite, cherty siltstone, and chert constitute the sedimentary member. The cherts are banded to laminated sinuous masses often appearing within the volcanics. They range in colour from light grey or buff, to green, white and infrequently red. Argillaceous rocks are also finely banded to laminated. The cherty portions of the argillite occur as lenses or pods. Coarser sediments are absent in the Antler Formation. The sedimentary beds are highly folded, cleaved, and contorted.

Rhyolite occurs as a volcanoclastic rock with varying amounts of chert and argillite fragments and pieces and may be an epiclastic unit. Massive fine to medium grained quartz-feldspar porphyritic rocks also outcrop and may be sills. Some of the rhyolite is chloritic or limonitic.

As stated in the section on the Guyet Formation conglomerates, the rhyolites bear a striking resemblance to previously described silicified quartz-rich conglomerate. Quartz porphyritic sills have also been noted in the Guyet Formation. It is possible, then, that the rhyolites may be a portion of the Guyet Formation.

Intrusive rocks of the Slide Mountain Group are considered to belong to the Antler Formation. The most common type are diabase sills similar in composition to the basalts and only distinguished by their apparent granular texture. Within the project area gabbro and diorite bodies have been noted. Also, in the Giscome area serpentinized peridotite bodies occur along with some mafic intrusives.

4.2.3 Post Upper Paleozoic Rocks

4.2.3.1 Takla Group

The Takla Group outcrops in the proximity of Giscombe and extends northward. A high angle fault defines the contact between Takla Group and Slide Mountain Group rocks.

Takla Group rocks are composed of three units. A lower unit of crystal lithic tuff, argillite and minor carbonate. The middle unit is mainly an intermediate flow sequence with coarse grained augite and feldspar porphyries and lesser volcanic breccia. Agglomerate and breccia of an intermediate composition mark the upper sequence.

4.2.3.2 Eastern Group

Eastern Group rocks define the western boundary of the project area and is included within the project area as a downfaulted block east of Purden Lake.

Along the western boundary the Eastern Group consists mainly of argillite and greywacke with intercalated green, grey, black and purple flows, tuffs and breccias of a mafic to intermediate composition.

Eastern Group rocks west of Purden Lake are of a different lithological character with two main units, carbonate and mafic volcanic.

Carbonate rocks consist of white to grey-black massive crystalline limestone, finely banded sandy micritic limestone, fossiliferous limestone and carbonaceous limestone. Masses of Triassic pelecypods occur as pods within the limestone. The unit is extremely folded and sheared and cross-cut by multiple calcite filled joints and fractures.

The mafic volcanic rocks are mainly breccias. Most breccia pieces range in size from 3 to 8 cm, but larger block size pieces are not uncommon. The matrix material is a blue green very fine grained quartzfeldspathic material. Pillowed and pillow breccia sequences also occur along with some massive flows.

4.2.3.3 Topley Intrusions

Granodiorite, quartz diorite and quartz monzonite outcrop south-southwest of Prince George along the western contact of the Slide Mountain Group.

Outcropping in the Giscombe area, granodiorite, quartz diorite and rhyolite dykes may also belong to the Topley Intrusions.

4.2.3.4 Bowron River Coal Basin

The Bowron River Coal Basin is a mid-Tertiary successor basin of conglomerate, shale, and coal situated southwest of Purden Lake, west of the project area in the Bowron River Basin. The coal basin appears to be faulted against Slide Mountain Group Rocks.

4.2.4 Wolverine Metamorphic Complex

The Wolverine Complex is a high-grade metamorphic and intrusive terrain outcropping at the northeastern extreme of the project area east of Giscombe. The outcrops in the Giscombe area mark the southern terminus of the Complex which is a major feature extending hundreds of kilometres north of the project area.

Granodiorite, pegmatite, granite, granitoid gneiss, micaceous-garnetiferous-chloritic schists, and minor feldspathized quartzites comprise the lithologies of the Wolverine Complex.

4.3 Structure

The Slide Mountain Group occupies the center of the Black Stuart Synclinorium, a north-south trending structural basin.

The Slide Mountain Group is most widely believed to be an allocthonous sheet emplaced during the Cariboo Orogeny. This hypothesis is supported by the lack of source conduits for the Antler Formation volcanics in underlying Precambrian rocks and where contacts with the Antler Formation are observed they are faulted (Campbell et al, 1973).

Two major north-south trending strike dip faults crosscut all lithologies south of the Vama Claim block. These faults are characterized by broad limonitized zones with areas of carbonitization and propylitization. Extensions of these faults may continue for a large distance (north and south).

The degree of deformation within the Slide Mountain Group is reflected mainly in the highly sheared, cleaved and generally contorted argillite and chert beds. Volcanic rocks of the Group usually exhibit minor deformation structures such as complex joint patterns and minor slip surfaces.

Poor outcrop density and a lack of definite marker horizons within the Slide Mountain Group make the determination of stratigraphic and structural relationships within the Group at best difficult if not impossible.

Strike slip and downfaulting during the Columbia and Laramide orogenies produced the present map form. The downfaulting emplaced a block of Triassic volcanic and sedimentary rocks of the Eastern Group within the Slide Mountain Group southwest of Purden Lake.

The Guyet Formation since it contains a large volume of continental clastic material and minor crinoid beds has been thought to represent an orogenic sediment deposited in front of the allocthon which was subsequently overridden. However, the Guyet Formation grades into the Antler Formation wherever the contact is observed and is probably an original part of the allocthon.

5. GEOCHEMISTRY

5.1 Grid Controlled Geochemistry

5.1.1 Methodology

Geochemical samples of B_1 soil horizon were taken at fifty metre intervals along the cut lines of those geophysical grids deemed to be sufficiently close to outcrop to yield a useful expression of the geochemical environment.

All samples were dried, packaged, and shipped to Chemex Laboratories Limited and Loring Laboratories Limited, both in Calgary. Only complete grids were sent to either laboratory. A total of 1,465 samples were taken.

Geological mapping was carried out concomitantly with geochemical surveys. Slope direction and magnitude and the general geography of each grid was noted to aid in interpretation and control of the surveys.

1:2,500 scale contoured geochemical maps are included as Figures 4 to 13.

5.1.2 Anomaly Selection

Data processing of the grid geochemical results was necessary due to the large amount of data to be treated. Statistical manipulation of the data was employed to find a reasonable methodology for determining anomalous values. For a discussion of techniques used see Appendix II.

Below is a summary of the determination.

	Copper	Lead	Zinc
Background	35 ppm	20 ppm	150 ppm
3rd. order	35 ppm - 55 ppm	20 ppm - 35 ppm	150 ppm - 300 ppm
2nd order	55 ppm - 75 ppm	35 ppm - 45 ppm	300 ppm - 500 ppm
1st order	+75 ppm	+45 ppm	+500 ppm

All grids were computer contoured using ppm values. Criteria for the interpretation of the contoured maps was based on the magnitude of the anomalous value, whether the value was a single station or part of a trend, and whether the value was proximal to an EM conductor. In otherwords, a geochemical anomaly of high priority would be a high ppm value contained in an expressed geochemical trend proximal to an EM conductor. In addition, if all three elements, Cu, Pb, Zn, were of the same nature ie. coincident, then the total geochemical expression and EM conductor would be of the highest priority.

5.1.3.1 Grid 78-9 - Summary

No anomalous values for either copper, lead, or zinc were returned for grid 78-9. Lead anomalies on the southern stations of line 2+00E are considered to be the result of contamination as they occur on one line and are not continued laterally.

The poor geochemical results for Grid 78-9 may be in part due to extreme overburden thickness.

5.1.3.2 Grid 78-10

5.1.3.6.1 Copper

Grid 78-10 has a high copper geochemical relief. Two large anomalous copper zones are recognized.

Between lines 5+00 to 12+00 east is a broad zone of clustered first order anomalies separated by a narrow trough of below background values. This anomalous zone is underlain by mafic Paleozoic volcanic and intrusive rocks. The overburden cover is quite thin and it is felt that the copper anomalies reflect a high copper background in the mafic rocks. This is also true of another anomalous copper zone situated south of the baseline between lines 17+00 east through 20+00 east. Other single station anomalies are scattered throughout the grid.

5.1.3.6.2 Lead

A broad anomalous lead zone lies obliquely through lines 9+00 to 14+00 east on Grid 78-10. The zone contains several first order anomalies with a maximum value of 76 ppm, and is coincident with an anomalous copper zone.

5.1.3.6.3 Zinc

No significant zinc anomalies were obtained for Grid 78-10. The only anomalies obtained were second order single station values.

5.1.3.6.4 Summary

A broad copper-lead anomalous zone trends obliquely lines 9+00 through 14+00 east. The area is geologically complex with basic intrusives, serpentinite, argillaceous sediments and andesitic volcanics. No showings were discovered and it is not known whether the geochemical trend represents mineralization or high background copper and lead in the underlying lithologies.

5.1.3.3 Grid 78-11

5.1.3.7.1 Copper

Copper geochemistry on Grid 78-11 also has a high relief character with numerous singular highs distributed equally throughout the grid. Two anomalous terrains, however, can be discerned.

The first terrain is underlain by a band of andesitic volcanic rocks roughly situated in the centre portion of the grid. This zone is characterized by one station and some two station highs with an upper limit of 154 ppm. The anomalous values are thought to reflect a high copper background in the andesites with anomalous sample stations representing loci of positive enrichment of high copper backbround with the soil column.

A second anomalous copper terrain is underlain by the limestone unit and is roughly coincident with the anomalous zinc terrain. As in the case of the zinc anomalies, it is thought that the copper anomalies in this area reflect groundwater deposition of copper in a reducing (carbonaceous) limestone environment. Copper values in this area are generally higher with a highest value of 210 ppm.

A few isolated one station highs are thought to be the result of chemical and topographic dispersion.

5.1.3.7.2 Lead

Significant lead anomalies are confined to the northern region of the grid between lines 12+00E and 17+00E.

Between lines 12+00E and 17+00E there is a definite cluster of anomalies the highest of which reaches 100 ppm. The area surrounds the lead-zinc showing EG-11 and is underlain by the host rock extension of the original showing. These anomalies are thus thought to represent bedrock mineralization.

The anomalies on the northern portion of lines 19+00E to 24+00E do not define a definite zone as in the above. They are mostly one station highs, the highest being 220 ppm, and are not underlain by the favourable host rocks of the area. Thus it is felt that these anomalies represent dispersions of the bedrock mineralization on lines 12+00E to 17+00E.

5.1.3.7.3 Zinc

Grid 78-11 is considered to have a high relief with respect to zinc. A value of 2000 ppm was the highest recorded.

There exists a broad zone of zinc anomalies south and immediately north of the vaseline for the length of the grid, the highest value being 2000 ppm. The area is a topographic depression underlain by a nondescript sometimes carbonaceous limestone unit which is presumed to be a trap for groundwater transported zinc. Between the Northern extreme lines 12+00E and 17+00E is a cluster of zinc anomalies with values reaching 800 ppm. This anomalous area is considered to be a primary zone reflecting bedrock minerlization since it surrounds lead-zinc showing EG-11 and is underlain by the host rock extension of the original Giscome showing. Several displaced anomalies occur southeast of this area with a 400 ppm average and are thought to due to groundwater deposition.

Several erratic one station highs of from 300 to 500 ppm also occur on the grid. These are spurious values and are not considered as hard targets.

5.1.3.7.4 Summary

Copper and zinc exhibit a high relief throughout Grid 78-11 but are not considered to reflect significant accumulations of bedrock mineralization.

Anomalous lead distribution on Grid 78-11 appears to be a positive indicator of bedrock mineralization, specifically on the northern portion of lines 12+00E through 17+00E. Coincident zinc anomalies in this area may also indicate bedrock mineralization.

6. GEOPHYSICS

6.1 Terms of Reference

In March 1978, Questor Input airborne EM and magnetometer survey was carried out in the vicinity of Prince George, B.C. The purpose of the survey was to deliniate conductive zones of potential for sulfide mineralization and also to obtain magnetic and conductivity information which would contribute towards making geological interpretations within the survey area.

A total of nine kilometers of grid lines were cut in 3 separate grids over interesting looking Input EM anomalies for the purpose of doing geophysical and geochemical surveys, and geological mapping. Approximately 68.2 line kilometers of Shootback EM surveys were carried out over all grids. About 411 line kilometers on grids were surveyed using VLFEM method. Approximately 61.9 line kilometers of total field magnetometer surveys were completed over grid.

CEM Profiles are included as Figures 14 through 16. The VLF Contour Map is included as Figure 17, and Mag Contours are included as Figures 18 and 19.

6.2 Ground Geophysical Work

6.2.1 Methods Used

6.2.1.1 Shootback EM Method

Shootback EM method was used in ground followup of the airborne EM anomalies which seemed favourable. This method was chosen as a standard technique over other methods in this area because the effect of change in separation between the coils on measurements is minimal. Therefore, accurate distance measurements between the coils so the operation is rapid compared to other systems which require cable connection (e.g. Silingram).

The grids 789 through 7811 were surveyed using the Shootback EM method. Separation between the two coils was 100 meters and horizontal transmitter mode was used. Tilt angle (or inphase) measurements were taken every 25 meter intervals using the frequencies 390 Hz and 1830 Hz. Spacing between the lines was 100 meters.

The Shootback EM tilt angles were plotted in the form of stacked profiles for each grid. Scale along the lines was kept at 1/10,000 and along base lines at 1/5,000 in order to trim down the graphs to a manageable size.

6.2.1.2 VLF-EM Method

The VL-FEM method was used as a back up to the Shootback EM system to survey on grid 78-11. In surveying the grids either the VLF transmitting station NAA (18.6 KHz) or NLK (17.8 KHz) was used depending on the line orientation. A Geonics EM-16 instrument was used to measure inphase (percent tangent of tilt angle) and quadrature (percent of primary field) components at station of 12.5 meters. Inphase measurements were later filtered using a procedure devised by Frazer (1967), which transforms "crossovers" into peaks and rejects high frequency variations. The filtered inphase values are presented in the form of a contour map. High contour values correspond to locations of conductors detected by VLF-EM method.

6.2.1.3 Magnetometer Surveys

Some of the airborne EM Conductors chosen for ground follow-up happened to be within or in the vicinity of magnetic anomalies. Total field ground magnetometer surveys were done in order to resolve the relationship between magnetic features and EM conductors on grids 78-10 and 78-11 were surveyed using this method.

6.2.2 Grid 78-9

This grid covers the Southermost portion of a string of Input conductors which extend all the way to Giscome showing located about 6.5 kilometers Northwest of grid 78-9. The airborne EM response changes rapidly to East of the mentioned conductive zone becoming highly resistive compared to the area to West. This long Input conductor trend apparently marks the boundary between a resistive igneous and metamorphic complex (marked as Wolverine complex on Figure 2), and some younger volcanic and sedimentary rocks to the West. Aeromagnetic response is also quite active along the mentioned conductive border zone.

The Shootback EM results suggest that the grid is underlain by a series of poor conductors, however it is difficult to identify axis of individual conductors. A ground magnetometer survey on grid 78-9 would have aided interpretation. This grid also requires further exploration using some additional techniques as in grid 78-7.

6.2.3 Grid 78-10

This grid is located about 1.5 kilometers Northwest of grid 78-9 and the airborne EM and magnetic characteristics discussed under grid 78-9 also apply to this grid.

The Shootback EM surveys on this grid detected some weakly defined poor conductors with an approximate East-West trend as shown on the magnetic contour map.

The ground magnetometer survey results suggest that a highly magnetic body is located in the Southeast portion of the grid (see contour map). Some highly magnetic ultramafic rock outcrops were observed in field over the area of high magnetic response. The Northern part of the grid is characterized by moderately high and relatively quiet ground magnetic response. Some granitic rock outcrops were observed along the Northern edge of the grid over the area of moderate magnetic response. The areas which have low and noisy magnetic response are underlain by some sedimentary and volcanic rocks.

There is evidence in both Shootback EM and magnetic data that a fault might be crossing the grid as indicated on the magnetic contour map.

The Shootback EM conductors do not seem to indicate any correlation with the geochemical high spots of Pb, Zn and poorly conductive bedrock horizons. However, under the guidance of some previously done work on Giscome showing (Allen, 1973), the area between the EM conductors and granitic rocks to the North appears to be a favourable location for further exploration. Geological observations and geophysical evidence support the assumption that the EM conductor-mineralization-surrounding rock relationship as described by Allen for the Gisome showing in grid 78-11, persists along the grids 78-11, 78-10 and even 78-9.

6.2.4 Grid 78-11

This grid comprises the Northern part of the Input and aeromagnetic trend described under grid 78-9. Giscome showing, which is a Pb, Zn mineralization outlined as a result of extensive drilling in the past (Allen, 1973), is located at the Northern boundary of the grid. Previous reports indicate that a graphitic conductor is located just South of the mineralized zone and acts as a marker to the mentioned contact metamorphic zone.

The σ values estimated from the Input data for conductors in this grid range from 1 Mhos to 33 Mhos.

The Shootback EM survey detected a

well defined conductor which extends from the mentioned Pb, Zn mineralization near line 8W through line 14E along the Northern edge of the grid (marked as F on profiles). Previous drilling in the vicinity of lines 8W to 5W indicated that the conductor A is a graphitic argillite layer which constitutes the Southern boundary of a less than 100 meters wide skarn zone (Allen, 1973). The skarn zone is sandwiched between some gneissic (?) rocks to North and the graphitic argillite (A) and some intermediate to dark colored volcanic rocks to South. A map reproduced from Allen's report illustrates the geology in the vicinity of mineralization in detail.

The σ values of conductor A estimated from the Shootback EM data is highly variable over the conductor's two kilometer length in this grid. The typical σ values fall in the range of 10 - 37 Mhos.

A multiple conductive zone (marked as C on the map) extends Southeast along the base line starting from line 1E all the way to line 23E. Typical σ values estimated from the Shootback EM data for conductive zone C are usually 10 Mhos or less, which is in good agreement with values estimated from the Input data.

Axis of conductors inferred from the Shootback EM data are also plotted on the VLF-EM contour map. High contour values on the VLF-EM contour map correspond to VLF conductor locations. There is an excellent correlation between a VLF-EM low and the Shootback EM conductor A. VL-FEM high (or VLF-EM conductor axis) corresponding to the Shootback conductor axis A is displace about 50 - 75 meters North from the Shootback axis. This is expected since the conductor A is dipping to Southwest and VL-FEM responded to a shallower part of the conductor than the Shootback EM did. Therefore, the conductor axis indicated by the VLF-EM method appears displaced to North with respect to the Shootback conductor axis as a consequence of the conductor's Southerly dip.

The VLF-EM survey outlined in the full extend of the conductor A in this grid even at locations where it could not be detected by a Shootback EM method. The VLF-EM survey also detected several other conductors some of which are in Shootback conductor zone C and some others which have no expression on the Shootback EM data.

Ground magnetometer survey results are presented in the form of a contour map. Rocks in this grid can be grouped into three categories on the basis of their magnetic responses. Highly magnetic rocks are located in the Northeast part of the grid and they extend towards the center in a wedge form. The grid 78-11 is located about 1 kilometer Northwest of grid 78-10 along the trend of some highly magnetic ultramafic rocks which were observed in grid 78-10. Therefore it is reasonable to assume that the mentioned ultramafic rocks extend into grid 78-11 even though no such outcrops were observed in this grid. Aeromagnetic data also supports this argument.

Moderately magnetic response mostly exists along the Northern edge of the grid, which correlates well with the rocks of igneous and metamorphic origin observed in that area. Center of the grid along the base line is characterized by moderately high noisy magnetic response, which indicates the presence of possibly some volcanic rocks in these areas. A major part of the grid has background of below background magnetic response indicating that rocks of sedimentary origin underlie these areas.

Some geochemcial high spots of Zn, Pb, and Cu exist in the vicinity of conductor A along the lines 3E to 8E and 12E to 15E. There are no geochemcial values above background at Giscome showing even though Pn, Zn mineralization were encountered in previous drill holes.

7. Conclusions

Conclusions reached on the basis of work done to date on the Eagle Claims can be summarized as follows:

1) Eagle claims are underlain by graphitic sedimentary rocks to a large extent.

2) Shootback EM method was used successfully in detailing favourable Input anomalies on the ground. It was often possible to make predictions about conductor properties from the Shootback EM data, such as: depth to the top of conductor, conductivity-thickness products, dip and strike extent of conductor, multiple conductors, resistivity of host rocks.

3) Ground magnetometer surveys were used successfully in areas where rocks with different susceptibilities existed together. Ground magnetic data was helpful in interpreting EM survey results and in making geological interpretations.

4) VLF-EM method had limited usefulness in this project area due to the existence of a great number of bedrock conductors and the method responded indiscriminantly to all of them. It should not be employed routinely.

5) Ground geophysical surveys outlined several anomalous areas in favourable rock types and some with associated geochemical anomalies. Drilling is required to further investigate these "multi-anomalous" areas.

6) Trenching of geophysical and geochemical anomalies is not feasible due to thick overburden cover in the area.

It is recommended that EM conductors which are in a lithologically favourable environment and/or show correlation with geochemical anomalies of Pb, Zn or Cu, should be further investigated by means of drilling. See Figures 2 to 4 for proposed drill hole locations.

APPENDIX I

Qualifications of Author

I, Christopher J. C. Bloomer state that I am a geologist in Minerals Exploration of Shell Canada Resources Limited of Calgary, Alberta. I have obtained a B.Sc., '77 degree at the University of Toronto and have practiced my profession since graduation. I was directly involved with the work submitted here in this report.

C. J. C. Bloomer
Geologist
Minerals Exploration
Shell Canada Resources

PROFESSIONAL GEOPHYSICIST
SACIT SAYDAM
ALBERTA

A. S. Saydam, P. Geoph.
Geophysicist
Minerals Exploration
Shell Canada Resources Limited

APPENDIX II

GEOCHEMISTRY

General Statement

3,277 B_1 soil geochemical samples were taken over grids 78-3, 78-4, 78-5, 78-6, 78-9, 78-10, 78-11, 78-12 with partial coverage over grid 78-12. For the determination of background and anomalous values the data from all grids excepting 78-12 were considered as one population.

All zero values have been excluded and extreme values have been kept. Section II is a computer print out of the complete statistical analysis. A rigorous statistical examination of the data was not attempted as it is felt that it would not change the background and anomaly ranking to a significant degree.

Section III is a listing of all geochemical data.

Copper, lead, and zinc are plotted on cumulative curves (Figures A, B, and C) and relative frequency % vs. ppm (Figures D, E, and F). The graphs were compared with background and anomaly ranking as determined by standard formulas to select a final background and anomaly ranks for each element.

Calculations

The standard formula used is as below:

Background	$\bar{x} + s$
Third Order Anomaly	$\bar{x} + 5$ to $\bar{x} + 25$
Second Order Anomaly	$\bar{x} + 25$ to $\bar{x} + 35$
First Order	$+\bar{x} + 35$

Below are background and anomaly ranks determined by the standard formulas for copper, lead, and zinc:

	Copper	Lead	Zinc
Background (ppm)	39	16	241
Third Order (ppm)	39 to 60	16 to 25	241 to 387
Second Order (ppm)	60 to 81	25 to 34	387 to 537
First Order (ppm)	+81	+34	+537

Graphic Determination

A comparison of the calculated anomalies show a reasonable relationship to the population distribution as shown in the graphs. The final anomaly distribution is based on a comparison of the graphs and calculations with the final cut-offs being somewhat judgemental and arbitrary.

Copper and zinc have a similar population distribution and for both elements the top 10% of the population are considered anomlous. Lead is more positively skewed than copper and zinc and the top 5% of the lead population are considered anomalous.

Anomaly Ranking

The background values determined visually from the graphs compare closely with those calculated for copper and lead. The zinc background is lower due to a higher range of values and consequently a high standard deviation and a higher calculated background. A lower background for zinc is preferred when the population distribution is considered.

The final ranking of the anomalies is based on a comparison between the calculated ranks and the graphs to yield a reasonable distribution between the ranks:

The final background and anomaly ranks are as below:

	Copper	Lead	Zinc
Background (ppm)	35	20	150
Third Order (ppm)	35 to 55	20 to 35	150 to 300
Second Order (ppm)	55 to 75	35 to 45	300 to 500
First Order (ppm)	+75	+45	+500

Selection of background and anomalous ranks is for the most part subjective. By using the graphic and calculated methods together a reasonable ordering of the data can be achieved.

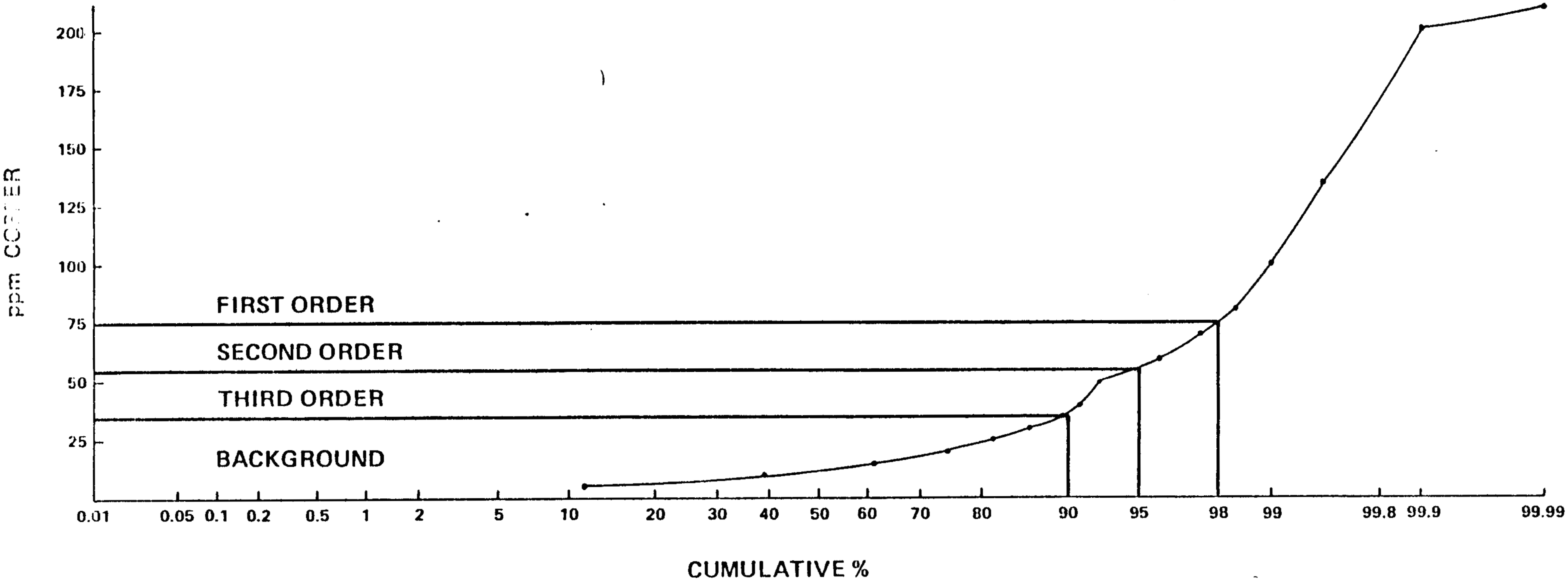
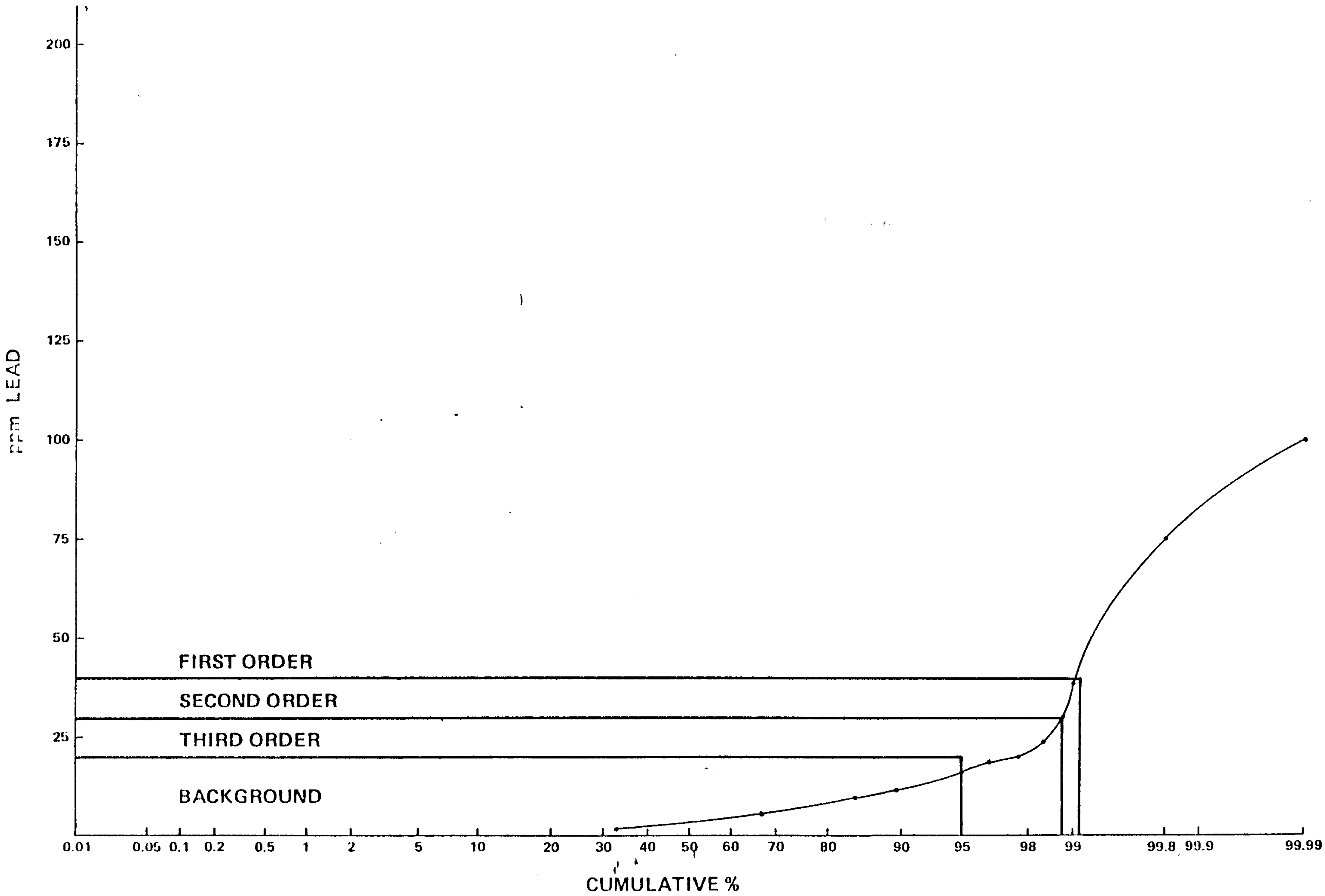

200
175
150
125
100
75
50
25
PPM COPPER
FIRST ORDER
SECOND ORDER
THIRD ORDER
BACKGROUND
0.01
0.05
0.1
0.2
0.5
1
2
5
10
20
30
40
50
60
70
80
90
95
98
99
99.8
99.9
99.99
CUMULATIVE %

FIGURE-A



ppm LEAD
200
175
150
125
100
75
50
25
FIRST ORDER
SECOND ORDER
THIRD ORDER
BACKGROUND
0.01
0.05
0.1
0.2
0.5
1
2
5
10
20
30
40
50
60
70
80
90
95
98
99
99.8
99.9
99.99
CUMULATIVE %

FIGURE - B

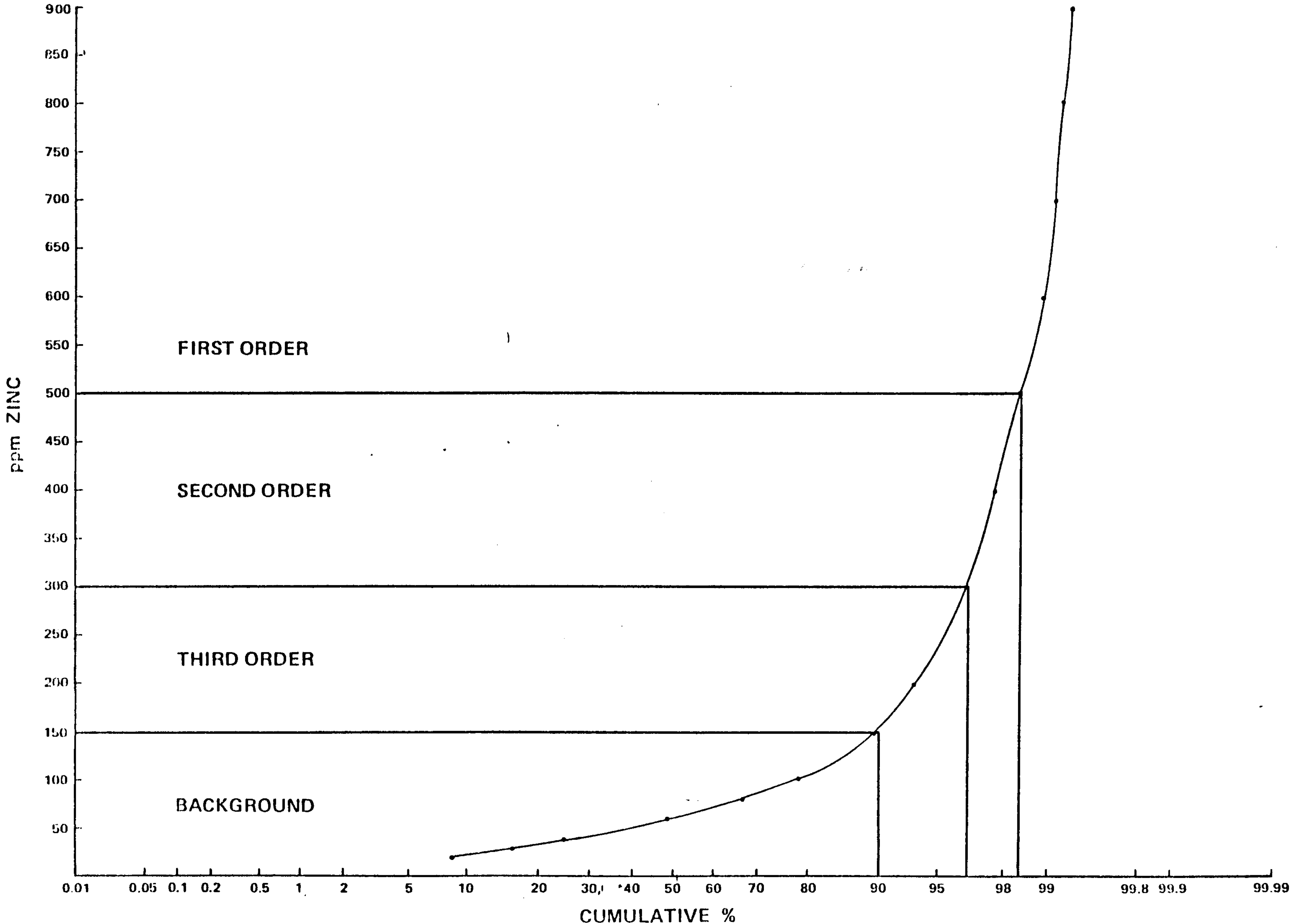

900
850
800
750
700
650
600
550
500
450
400
350
300
250
200
150
100
50
ppm ZINC
FIRST ORDER
SECOND ORDER
THIRD ORDER
BACKGROUND
0.01
0.05
0.1
0.2
0.5
1
2
5
10
20
30
40
50
60
70
80
90
95
98
99
99.8
99.9
99.99
CUMULATIVE %

FIGURE - C

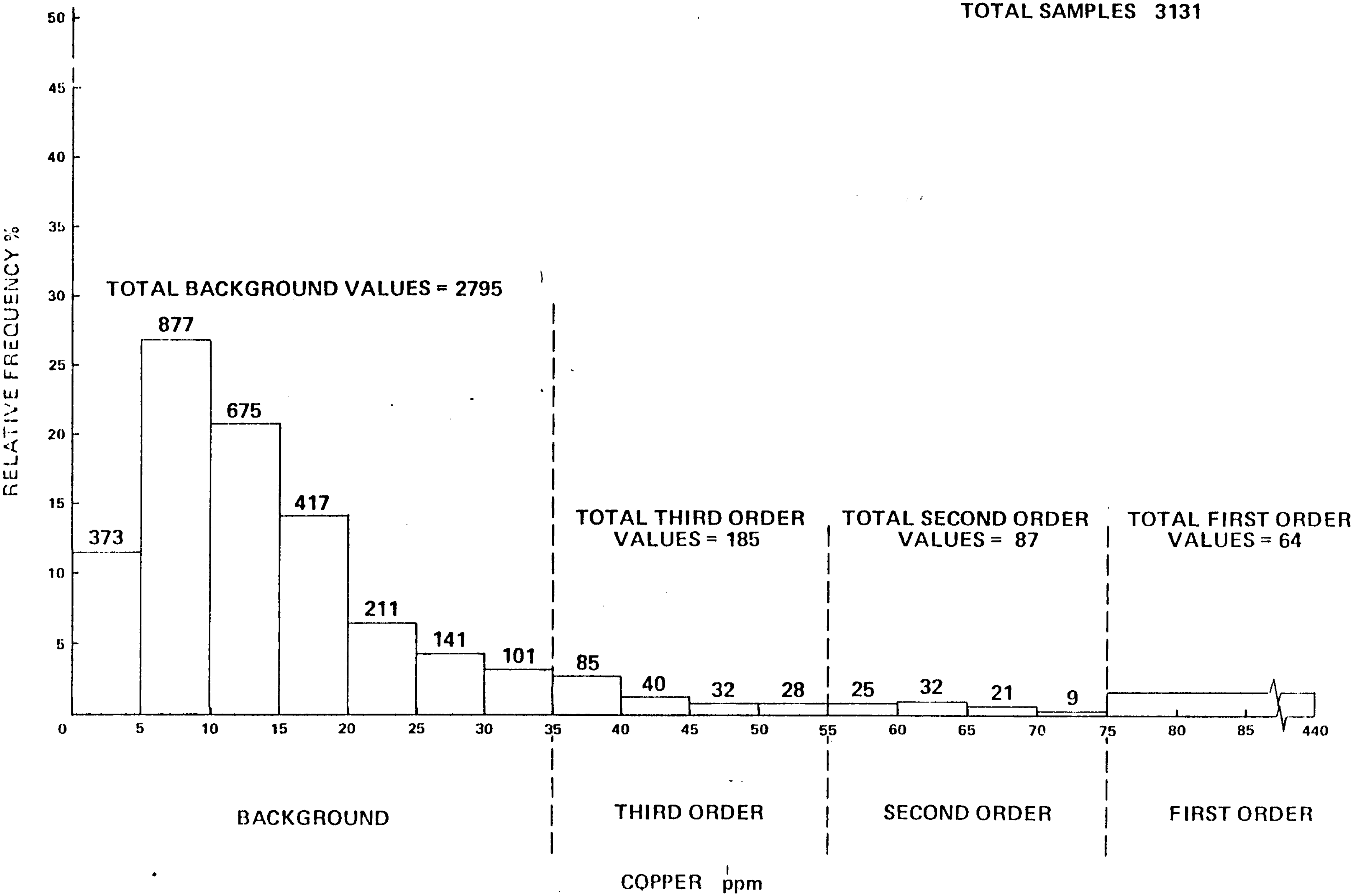

TOTAL SAMPLES 3131
TOTAL BACKGROUND VALUES = 2795
TOTAL THIRD ORDER VALUES = 185
TOTAL SECOND ORDER VALUES = 87
TOTAL FIRST ORDER VALUES = 64
RELATIVE FREQUENCY %
50
45
40
35
30
25
20
15
10
5
373
877
675
417
211
141
101
85
40
32
28
25
32
21
9
0
5
10
15
20
25
30
35
40
45
50
55
60
65
70
75
80
85
440
BACKGROUND
THIRD ORDER
SECOND ORDER
FIRST ORDER
COPPER ppm

FIGURE - 2

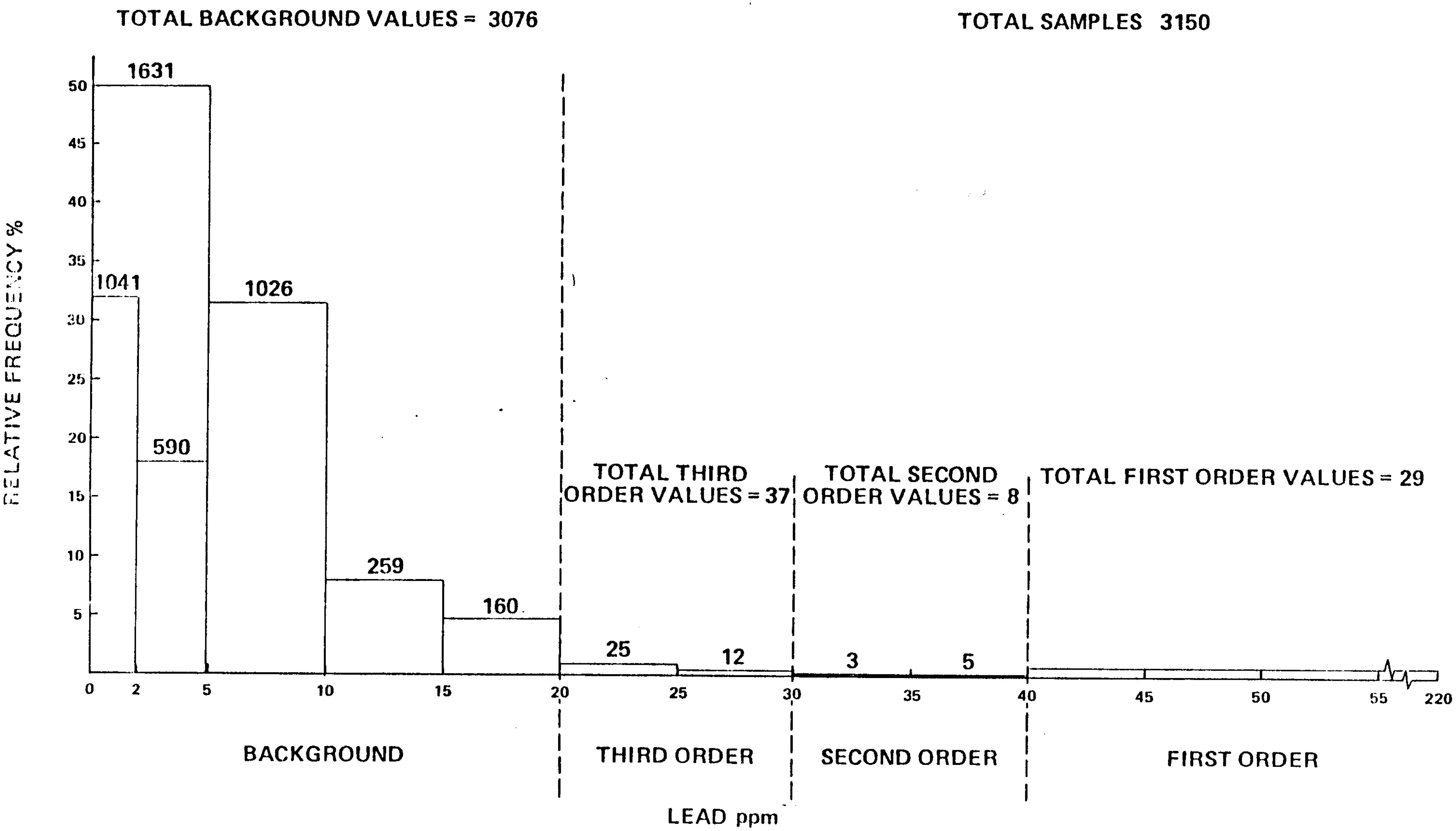

TOTAL BACKGROUND VALUES = 3076
TOTAL SAMPLES 3150
RELATIVE FREQUENCY %
50
45
40
35
30
25
20
15
10
5
1631
1041
590
1026
259
160
25
12
3
5
TOTAL THIRD ORDER VALUES = 37
TOTAL SECOND ORDER VALUES = 8
TOTAL FIRST ORDER VALUES = 29
0
2
5
10
15
20
25
30
35
40
45
50
55
220
BACKGROUND
THIRD ORDER
SECOND ORDER
FIRST ORDER
LEAD ppm

FIGURE -E

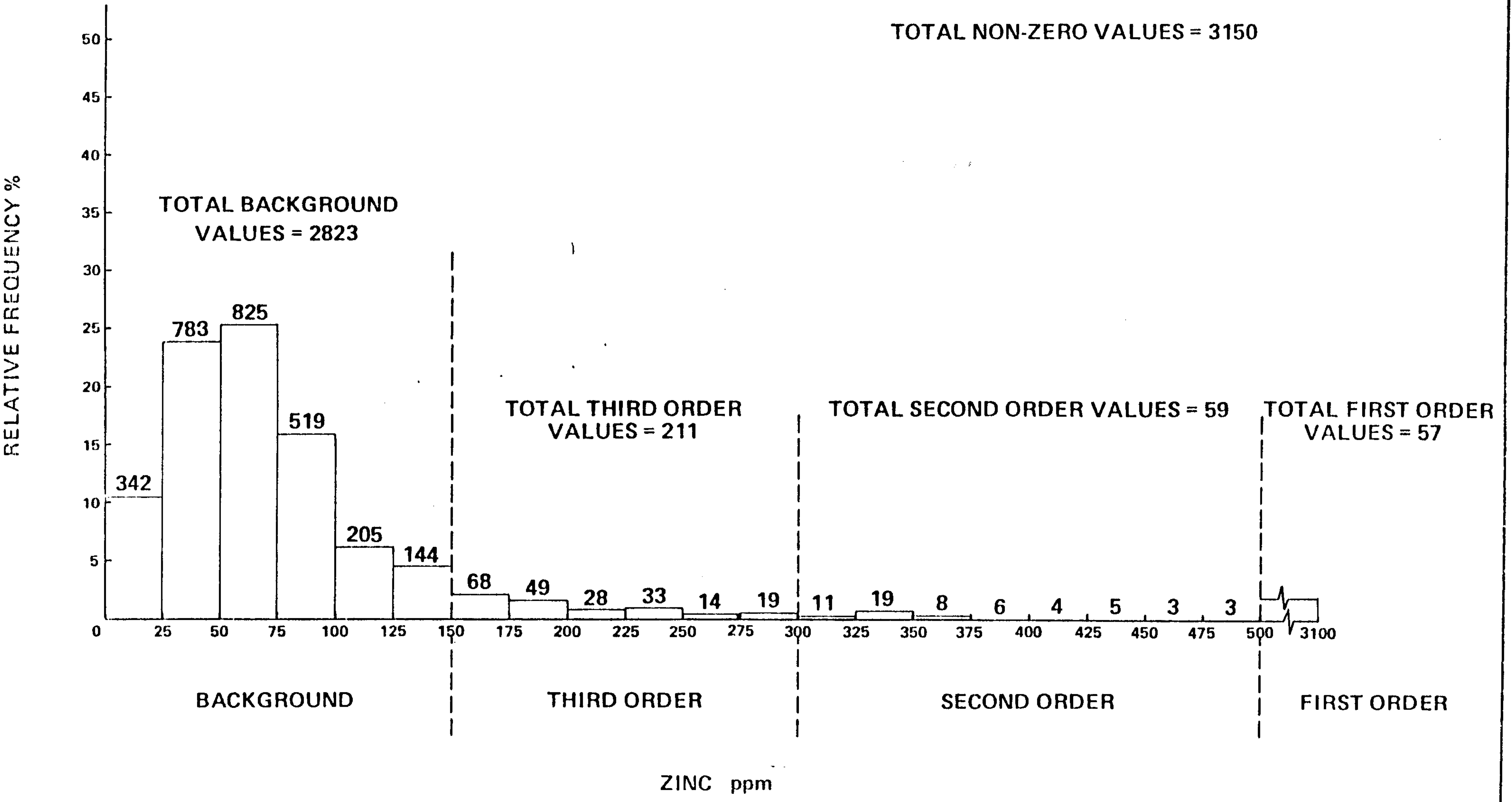

TOTAL NON-ZERO VALUES = 3150
TOTAL BACKGROUND VALUES = 2823
TOTAL THIRD ORDER VALUES = 211
TOTAL SECOND ORDER VALUES = 59
TOTAL FIRST ORDER VALUES = 57
RELATIVE FREQUENCY %
50
45
40
35
30
25
20
15
10
5
342
783
825
519
205
144
68
49
28
33
14
19
11
19
8
6
4
5
3
3
0
25
50
75
100
125
150
175
200
225
250
275
300
325
350
375
400
425
450
475
500
3100
BACKGROUND
THIRD ORDER
SECOND ORDER
FIRST ORDER
ZINC ppm

FIGURE-F

APPENDIX II

SECTION I

```
DESCRIPTIVE STATISTICS OF CU, PB, ZN DATA                                        29 NOV 78         PAGE     3

FILE    GEOCHEM  (CREATION DATE = 29 NOV 78)    CU PB ZN DATA COLLETED BY C. BLOOMER

VARIABLE   CU          COPPER PPM

MEAN          18.41584                   STD ERROR     .3741729                      STD DEV       20.93697
VARIANCE      438.3567                   KURTOSIS      68.34733                      SKEWNESS      5.729993
RANGE         439.0000                   MINIMUM       1.000000                      MAXIMUM       440.0000

VALID OBSERVATIONS -     3131                      MISSING OBSERVATIONS -      146

- - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -

VARIABLE   PB          LEAD PPM

MEAN          6.751111                   STD ERROR     .1583423                      STD DEV       8.886941
VARIANCE      78.97773                   KURTOSIS      163.3729                      SKEWNESS      9.453066
RANGE         219.0000                   MINIMUM       1.000000                      MAXIMUM       220.0000

VALID OBSERVATIONS -     3150                      MISSING OBSERVATIONS -      127

- - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -

VARIABLE   ZN          ZINC PPM

MEAN          93.22857                   STD ERROR     2.634997                      STD DEV       147.8888
VARIANCE      21871.10                   KURTOSIS      109.8708                      SKEWNESS      8.623178
RANGE         3098.000                   MINIMUM       2.000000                      MAXIMUM       3100.000

VALID OBSERVATIONS -     3150                      MISSING OBSERVATIONS -      127

- - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -

VARIABLE   LOGCU       LOG TO BASE 10 OF CU PPM

MEAN          1.114234                   STD ERROR     .6218292-02                   STD DEV       .3479467
VARIANCE      .1210669                   KURTOSIS      .5197068                      SKEWNESS      .2191577
RANGE         2.643453                   MINIMUM       .0000000                      MAXIMUM       2.643453

VALID OBSERVATIONS -     3131                      MISSING OBSERVATIONS -      146

- - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -

VARIABLE   LOGPB       LOG TO BASE 10 OF PB PPM

MEAN          .6514123                   STD ERROR     .6922468-02                   STD DEV       .3885225
VARIANCE      .1509498                   KURTOSIS     -.3287153                      SKEWNESS      .7336540-01
RANGE         2.342423                   MINIMUM       .0000000                      MAXIMUM       2.342423

VALID OBSERVATIONS -     3150                      MISSING OBSERVATIONS -      127
```

```
VARIABLE  LOGZN      LOG TO BASE 10 OF ZN PPM

MEAN          1.794495                STD ERROR    .6440463-02                STD DEV      .3614701
VARIANCE       .1306606               KURTOSIS    2.179999                    SKEWNESS     .1077197
RANGE         3.190332                MINIMUM      .3010300                   MAXIMUM     3.491362

VALID OBSERVATIONS -     3150                   MISSING OBSERVATIONS -      127
```

```
          DATA TRANSFORMATION DONE UP TO THIS POINT..

                 NO OF TRANSFORMATIONS               9
                 NO OF RECODE VALUES                 0
                 NO OF ARITHM. OR LOG. OPERATIONS    9
          THE AMOUNT OF TRANSPACE REQUIRED IS     270 WORDS

            24.     FREQUENCIES    GENERAL=ALL
            25.     STATISTICS     ALL

GIVEN WORKSPACE ALLOWS FOR   4373 TOTAL VALUES AND    437 LABELED VALUES PER VARIABLE FOR 'FREQUENCIES'
```

```
FILE   GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER

CU         COPPER PPM
                                                    RELATIVE  ADJUSTED    CUM
                                         ABSOLUTE     FREQ      FREQ      FREQ
CATEGORY LABEL                     CODE    FREQ      (PCT)     (PCT)     (PCT)

                                     1.      10        .3        .3       .30
                                     2.      45       1.4       1.4      1.80
                                     3.      76       2.3       2.4      4.20
                                     4.     167       5.1       5.3      9.50
                                     5.      75       2.3       2.4     11.90
                                     6.     192       5.9       6.1     18.00
                                     7.     142       4.3       4.5     22.60
                                     8.     241       7.4       7.7     30.30
                                     9.      64       2.0       2.0     32.30
                                    10.     238       7.3       7.6     39.90
                                    11.      76       2.3       2.4     42.40
                                    12.     228       7.0       7.3     49.60
                                    13.     133       4.1       4.2     53.90
                                    14.     193       5.9       6.2     60.00
                                    15.      45       1.4       1.4     61.50
                                    16.     151       4.6       4.8     66.30
                                    17.      31        .9       1.0     67.30
                                    18.     115       3.5       3.7     71.00
                                    19.      16        .5        .5     71.50
                                    20.     104       3.2       3.3     74.80
```

```
                          21.      45       1.4       1.4      76.20
                          22.      66       2.0       2.1      78.30
                          23.      25        .8        .8      79.10
                          24.      61       1.9       1.9      81.10
                          25.      14        .4        .4      81.50
                          26.      48       1.5       1.5      83.10
                          27.      13        .4        .4      83.50
                          28.      40       1.2       1.3      84.80
                          29.       3        .1        .1      84.90
                          30.      37       1.1       1.2      86.00
                          31.      21        .6        .7      86.70
                          32.      27        .8        .9      87.60
                          33.      19        .6        .6      88.20
                          34.      28        .9        .9      89.10
                          35.       6        .2        .2      89.30
                          36.      24        .7        .8      90.00
                          37.       4        .1        .1      90.20
                          38.      27        .8        .9      91.00
                          39.       2        .1        .1      91.10
                          40.      28        .9        .9      92.00
                          41.       7        .2        .2      92.20
                          42.      13        .4        .4      92.60
                          43.       3        .1        .1      92.70
                          44.      12        .4        .4      93.10
```

```
                              45.        5         .2         .2      93.30
                              46.        8         .2         .3      93.50
                              47.        3         .1         .1      93.60
                              48.       10         .3         .3      93.90
                              49.        1         .0         .0      94.00
                              50.       10         .3         .3      94.30
                              51.        2         .1         .1      94.30
                              52.        9         .3         .3      94.60
                              53.        1         .0         .0      94.70
                              54.       13         .4         .4      95.10
                              55.        3         .1         .1      95.20
                              56.        7         .2         .2      95.40
                              58.        7         .2         .2      95.60
                              59.        2         .1         .1      95.70
                              60.        9         .3         .3      96.00
                              61.        1         .0         .0      96.00
                              62.       12         .4         .4      96.40
                              63.        5         .2         .2      96.60
                              64.       10         .3         .3      96.90
                              65.        4         .1         .1      97.00
                              66.        8         .2         .3      97.30
                              67.        1         .0         .0      97.30
                              68.        5         .2         .2      97.40
                              70.        7         .2         .2      97.70
```

```
                        72.       4        .1        .1      97.80
                        73.       1        .0        .0      97.80
                        74.       4        .1        .1      98.00
                        76.       2        .1        .1      98.00
                        78.       2        .1        .1      98.10
                        80.       5        .2        .2      98.20
                        82.       1        .0        .0      98.30
                        84.       3        .1        .1      98.40
                        85.       1        .0        .0      98.40
                        86.       2        .1        .1      98.50
                        88.       1        .0        .0      98.50
                        90.       4        .1        .1      98.60
                        92.       2        .1        .1      98.70
                        94.       3        .1        .1      98.80
                        96.       2        .1        .1      98.90
                        98.       1        .0        .0      98.90
                       100.       3        .1        .1      99.00 ✓
                       104.       1        .0        .0      99.00
                       107.       1        .0        .0      99.00
                       108.       1        .0        .0      99.10
                       110.       1        .0        .0      99.10
                       112.       2        .1        .1      99.20
                       114.       1        .0        .0      99.20
                       116.       2        .1        .1      99.30
```

```
                                    118.        1        .0        .0     99.30

                                    120.        1        .0        .0     99.30

                                    124.        1        .0        .0     99.40

                                    130.        1        .0        .0     99.40

                                    135.        3        .1        .1     99.50

                                    136.        2        .1        .1     99.60

                                    140.        1        .0        .0     99.60

                                    148.        1        .0        .0     99.60

                                    154.        1        .0        .0     99.60

                                    160.        2        .1        .1     99.70

                                    164.        1        .0        .0     99.70

                                    170.        1        .0        .0     99.80

                                    174.        1        .0        .0     99.80

                                    175.        1        .0        .0     99.80

                                    180.        1        .0        .0     99.90

                                    195.        1        .0        .0     99.90

                                    200.        1        .0        .0     99.90

                                    210.        1        .0        .0    100.00

                                    440.        1        .0        .0    100.00

                                      0.      146       4.5   MISSING    100.0
                                           ------    ------    ------
                                   TOTAL     3277     100.0     100.0
```

```
DESCRIPTIVE STATISTICS OF CU, PB, ZN DATA                                                      29 NOV 78        PAGE   11

FILE    GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER


MEAN           18.416      STD ERR          .374      MEDIAN        12.586
MODE            8.000      STD DEV        20.937      VARIANCE     438.357
KURTOSIS       68.302      SKEWNESS        5.727      RANGE        439.000
MINIMUM         1.000      MAXIMUM       440.000

VALID CASES     3131       MISSING CASES    146
```

```
PB          LEAD PPM
                                               RELATIVE   ADJUSTED    CUM
                                    ABSOLUTE     FREQ       FREQ      FREQ
CATEGORY LABEL                CODE     FREQ     (PCT)      (PCT)     (PCT)

                                1.      370      11.3       11.7     11.70

                                2.      671      20.5       21.3     33.00

                                3.        1        .0         .0     33.10

                                4.      589      18.0       18.7     51.80

                                6.      461      14.1       14.6     66.40

                                8.      310       9.5        9.8     76.30

                               10.      255       7.8        8.1     84.30

                               12.      161       4.9        5.1     89.50

                               14.       98       3.0        3.1     92.60

                               16.       76       2.3        2.4     95.00

                               18.       47       1.4        1.5     96.50

                               20.       37       1.1        1.2     97.70

                               22.       19        .6         .6     98.30

                               24.        6        .2         .2     98.40

                               26.        7        .2         .2     98.70

                               28.        1        .0         .0     98.70

                               30.        4        .1         .1     98.80

                               32.        3        .1         .1     98.90

                               36.        2        .1         .1     99.00

                               38.        1        .0         .0     99.00
```

```
          40.       2       .1        .1     99.10
          42.       2       .1        .1     99.10
          44.       1       .0        .0     99.20
          46.       1       .0        .0     99.20
          48.       3       .1        .1     99.30
          55.       1       .0        .0     99.30
          56.       1       .0        .0     99.40
          60.       2       .1        .1     99.40
          62.       3       .1        .1     99.50
          64.       1       .0        .0     99.60
          67.       1       .0        .0     99.60
          70.       1       .0        .0     99.60
          72.       3       .1        .1     99.70
          74.       2       .1        .1     99.80
          76.       2       .1        .1     99.80
          82.       1       .0        .0     99.90
          87.       1       .0        .0     99.90
         100.       1       .0        .0     99.90
         174.       1       .0        .0    100.00
         220.       1       .0        .0    100.00
           0.     127      3.9    MISSING   100.0
                -------  ------   ------
       TOTAL     3277    100.0     100.0
```

```
FILE    GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER


MEAN              6.751      STD ERR            .158      MEDIAN          4.405
MODE              2.000      STD DEV           8.887      VARIANCE       78.978
KURTOSIS        163.267      SKEWNESS          9.449      RANGE         219.000
MINIMUM           1.000      MAXIMUM         220.000

VALID CASES      3150        MISSING CASES   127
```

```
DESCRIPTIVE STATISTICS OF CU, PB, ZN DATA                                         29 NOV 78        PAGE   15

FILE   GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER

ZN         ZINC PPM
                                                      RELATIVE  ADJUSTED    CUM
                                            ABSOLUTE    FREQ      FREQ      FREQ
CATEGORY LABEL                      CODE      FREQ      (PCT)     (PCT)     (PCT)

                                      2.         4        .1        .1       .10

                                      4.        17        .5        .5       .70

                                      6.        21        .6        .7      1.30

                                      8.        19        .6        .6      1.90

                                     10.        21        .6        .7      2.60

                                     12.        22        .7        .7      3.30

                                     14.        27        .8        .9      4.20

                                     16.        46       1.4       1.5      5.60

                                     17.         4        .1        .1      5.70

                                     18.        28        .9        .9      6.60

                                     19.        15        .5        .5      7.10

                                     20.        33       1.0       1.0      8.20

                                     21.        11        .3        .3      8.50

                                     22.        36       1.1       1.1      9.70

                                     24.        38       1.2       1.2     10.90

                                     26.        60       1.8       1.9     12.80

                                     28.        49       1.5       1.6     14.30

                                     30.        52       1.6       1.7     16.00

                                     31.         1        .0        .0     16.00

                                     32.        33       1.0       1.0     17.00
```

```
                        33.        7        .2        .2     17.30

                        34.       39       1.2       1.2     18.50

                        35.       11        .3        .3     18.90

                        36.       48       1.5       1.5     20.40

                        37.       11        .3        .3     20.70

                        38.       46       1.4       1.5     22.20

                        39.        1        .0        .0     22.20

                        40.       93       2.8       3.0     25.20

                        41.        1        .0        .0     25.20

                        42.       65       2.0       2.1     27.30

                        44.       58       1.8       1.8     29.10

                        45.        1        .0        .0     29.10

                        46.       76       2.3       2.4     31.60

                        48.       62       1.9       2.0     33.50

                        49.       18        .5        .6     34.10

                        50.       56       1.7       1.8     35.90

                        52.       94       2.9       3.0     38.90

                        54.       68       2.1       2.2     41.00

                        56.       79       2.4       2.5     43.50

                        57.        2        .1        .1     43.60

                        58.       86       2.6       2.7     46.30

                        60.       90       2.7       2.9     49.20

                        62.       50       1.5       1.6     50.80

                        63.       13        .4        .4     51.20
```

```
                         64.      60      1.8      1.9     53.10
                         65.      17       .5       .5     53.60
                         66.      35      1.1      1.1     54.70
                         67.       5       .2       .2     54.90
                         68.      60      1.8      1.9     56.80
                         69.       6       .2       .2     57.00
                         70.      60      1.8      1.9     58.90
                         71.       2       .1       .1     59.00
                         72.      60      1.8      1.9     60.90
                         73.       3       .1       .1     61.00
                         74.      22       .7       .7     61.70
                         75.      13       .4       .4     62.10
                         76.      40      1.2      1.3     63.30
                         77.      17       .5       .5     63.90
                         78.      42      1.3      1.3     65.20
                         79.       1       .0       .0     65.20
                         80.      52      1.6      1.7     66.90
                         82.      33      1.0      1.0     67.90
                         83.      14       .4       .4     68.40
                         84.      29       .9       .9     69.30
                         85.      25       .8       .8     70.10
                         86.      26       .8       .8     70.90
                         87.      15       .5       .5     71.40
                         88.      27       .8       .9     72.30
```

```
             89.         5        .2          .2       72.40
             90.        36       1.1         1.1       73.60
             91.        13        .4          .4       74.00
             92.        22        .7          .7       74.70
             93.         8        .2          .3       74.90
             94.        21        .6          .7       75.60
             95.        11        .3          .3       75.90
             96.        20        .6          .6       76.60
             97.        17        .5          .5       77.10
             98.        12        .4          .4       77.50
            100.        33       1.0         1.0       78.50
            102.        22        .7          .7       79.20
            103.         7        .2          .2       79.50
            104.         4        .1          .1       79.60
            105.        12        .4          .4       80.00
            106.         7        .2          .2       80.20
            107.        10        .3          .3       80.50
            108.         5        .2          .2       80.70
            110.        28        .9          .9       81.60
            112.        11        .3          .3       81.90
            113.         1        .0          .0       81.90
            114.         5        .2          .2       82.10
            115.        13        .4          .4       82.50
            116.        21        .6          .7       83.20
```

```
          117.       3        .1        .1      83.30
          118.       9        .3        .3      83.60
          120.      19        .6        .6      84.20
          122.       9        .3        .3      84.40
          123.       6        .2        .2      84.60
          124.       6        .2        .2      84.80
          125.       7        .2        .2      85.00
          126.      16        .5        .5      85.60
          127.       1        .0        .0      85.60
          128.      10        .3        .3      85.90
          129.       1        .0        .0      85.90
          130.      17        .5        .5      86.50
          132.       9        .3        .3      86.80
          133.       5        .2        .2      86.90
          134.       2        .1        .1      87.00
          135.       5        .2        .2      87.10
          136.      11        .3        .3      87.50
          137.       2        .1        .1      87.60
          138.       7        .2        .2      87.80
          140.      19        .6        .6      88.40
          142.       4        .1        .1      88.50
          144.       8        .2        .3      88.80
          145.       9        .3        .3      89.00
          146.       6        .2        .2      89.20
```

```
                                        148.         3           .1           .1        89.30

                                        150.         9           .3           .3        89.60

                                        153.         1           .0           .0        89.70

                                        154.         3           .1           .1        89.70

                                        155.         7           .2           .2        90.00

                                        156.         3           .1           .1        90.10

                                        157.         1           .0           .0        90.10

                                        158.         6           .2           .2        90.30

                                        160.        10           .3           .3        90.60

                                        162.         5           .2           .2        90.80

                                        163.         2           .1           .1        90.80

                                        164.         1           .0           .0        90.90

                                        165.         5           .2           .2        91.00

                                        166.         5           .2           .2        91.20

                                        170.        10           .3           .3        91.50

                                        172.         3           .1           .1        91.60

                                        174.         4           .1           .1        91.70

                                        175.         2           .1           .1        91.80

                                        176.         1           .0           .0        91.80

                                        178.         2           .1           .1        91.90

                                        180.         5           .2           .2        92.00

                                        182.         1           .0           .0        92.10

                                        184.         3           .1           .1        92.20

                                        185.         3           .1           .1        92.30
```

```
                                   188.         1          .0          .0      92.30
                                   190.         9          .3          .3      92.60
                                   194.         2          .1          .1      92.60
                                   195.         2          .1          .1      92.70
                                   200.        20          .6          .6      93.30
                                   201.         1          .0          .0      93.40
                                   205.         1          .0          .0      93.40
                                   210.        10          .3          .3      93.70
                                   215.         1          .0          .0      93.70
                                   220.        12          .4          .4      94.10
                                   225.         3          .1          .1      94.20
                                   230.         8          .2          .3      94.50
                                   235.         5          .2          .2      94.60
                                   240.         4          .1          .1      94.80
                                   245.         4          .1          .1      94.90
                                   250.        12          .4          .4      95.30
                                   255.         5          .2          .2      95.40
                                   260.         4          .1          .1      95.60
                                   266.         1          .0          .0      95.60
                                   270.         4          .1          .1      95.70
                                   280.         5          .2          .2      95.90
                                   285.         3          .1          .1      96.00
                                   290.         3          .1          .1      96.10
                                   300.         8          .2          .3      96.30
```

```
                    310.       3        .1        .1       96.40
                    318.       1        .0        .0       96.40
                    320.       6        .2        .2       96.60
                    325.       1        .0        .0       96.70
                    330.       8        .2        .3       96.90
                    335.       4        .1        .1       97.00
                    340.       3        .1        .1       97.10
                    345.       2        .1        .1       97.20
                    350.       2        .1        .1       97.30
                    360.       2        .1        .1       97.30
                    365.       2        .1        .1       97.40
                    370.       2        .1        .1       97.50
                    375.       2        .1        .1       97.50
                    380.       1        .0        .0       97.60
                    390.       1        .0        .0       97.60
                    400.       4        .1        .1       97.70
                    410.       3        .1        .1       97.80
                    425.       1        .0        .0       97.80
                    430.       1        .0        .0       97.90
                    440.       2        .1        .1       97.90
                    450.       2        .1        .1       98.00
                    460.       1        .0        .0       98.00
                    470.       1        .0        .0       98.10
                    475.       1        .0        .0       98.10
```

```
                              490.        2         .1         .1       98.20
                              500.        1         .0         .0       98.20
                              510.        2         .1         .1       98.30
                              520.        2         .1         .1       98.30
                              550.        3         .1         .1       98.40
                              560.        2         .1         .1       98.50
                              570.        3         .1         .1       98.60
                              580.        3         .1         .1       98.70
                              590.        4         .1         .1       98.80
                              600.        1         .0         .0       98.80
                              620.        2         .1         .1       98.90
                              640.        2         .1         .1       99.00
                              650.        2         .1         .1       99.00
                              660.        1         .0         .0       99.00
                              670.        1         .0         .0       99.10
                              700.        1         .0         .0       99.10
                              740.        1         .0         .0       99.10
                              750.        2         .1         .1       99.20
                              800.        1         .0         .0       99.20
                              855.        1         .0         .0       99.30
                              900.        2         .1         .1       99.30
                             1000.        2         .1         .1       99.40
                             1050.        2         .1         .1       99.50
                             1100.        3         .1         .1       99.60
```

```
                             1150.        2        .1         .1      99.60

                             1200.        1        .0         .0      99.70

                             1300.        2        .1         .1      99.70

                             1350.        1        .0         .0      99.70

                             1400.        1        .0         .0      99.80

                             1550.        1        .0         .0      99.80

                             1700.        1        .0         .0      99.80

                             2000.        4        .1         .1     100.00

                             3100.        1        .0         .0     100.00

                                0.      127       3.9    MISSING     100.0
                                      ------    ------    ------
                             TOTAL     3277     100.0      100.0


MEAN           93.229      STD ERR        2.635      MEDIAN         62.020
MODE           52.000      STD DEV      147.889      VARIANCE    21871.101
KURTOSIS      109.799      SKEWNESS       8.619      RANGE        3098.000
MINIMUM         2.000      MAXIMUM     3100.000

VALID CASES      3150      MISSING CASES     127
```

```
FILE    GEOCHEM   (CREATION DATE = 29 NOV 78)    CU PB ZN DATA COLLETED BY C. BLOOMER

LOGCU      LOG TO BASE 10 OF CU PPM
                                                  RELATIVE  ADJUSTED    CUM
                                        ABSOLUTE    FREQ      FREQ      FREQ
CATEGORY LABEL                    CODE    FREQ     (PCT)     (PCT)     (PCT)

                                 .0000      10        .3        .3       .30

                                 .3010      45       1.4       1.4      1.80

                                 .4771      76       2.3       2.4      4.20

                                 .6021     167       5.1       5.3      9.50

                                 .6990      75       2.3       2.4     11.90

                                 .7782     192       5.9       6.1     18.00

                                 .8451     142       4.3       4.5     22.60

                                 .9031     241       7.4       7.7     30.30

                                 .9542      64       2.0       2.0     32.30

                                1.0000     238       7.3       7.6     39.90

                                1.0414      76       2.3       2.4     42.40

                                1.0792     228       7.0       7.3     49.60

                                1.1139     133       4.1       4.2     53.90

                                1.1461     193       5.9       6.2     60.00

                                1.1761      45       1.4       1.4     61.50

                                1.2041     151       4.6       4.8     66.30

                                1.2304      31        .9       1.0     67.30

                                1.2553     115       3.5       3.7     71.00

                                1.2788      16        .5        .5     71.50

                                1.3010     104       3.2       3.3     74.80
```

```
                              1.3222       45         1.4         1.4       76.20
                              1.3424       66         2.0         2.1       78.30
                              1.3617       25          .8          .8       79.10
                              1.3802       61         1.9         1.9       81.10
                              1.3979       14          .4          .4       81.50
                              1.4150       48         1.5         1.5       83.10
                              1.4314       13          .4          .4       83.50
                              1.4472       40         1.2         1.3       84.80
                              1.4624        3          .1          .1       84.90
                              1.4771       37         1.1         1.2       86.00
                              1.4914       21          .6          .7       86.70
                              1.5051       27          .8          .9       87.60
                              1.5185       19          .6          .6       88.20
                              1.5315       28          .9          .9       89.10
                              1.5441        6          .2          .2       89.30
                              1.5563       24          .7          .8       90.00
                              1.5682        4          .1          .1       90.20
                              1.5798       27          .8          .9       91.00
                              1.5911        2          .1          .1       91.10
                              1.6021       28          .9          .9       92.00
                              1.6128        7          .2          .2       92.20
                              1.6232       13          .4          .4       92.60
                              1.6335        3          .1          .1       92.70
                              1.6435       12          .4          .4       93.10
```

```
        1.6532        5         .2          .2      93.30
        1.6628        8         .2          .3      93.50
        1.6721        3         .1          .1      93.60
        1.6812       10         .3          .3      93.90
        1.6902        1         .0          .0      94.00
        1.6990       10         .3          .3      94.30
        1.7076        2         .1          .1      94.30
        1.7160        9         .3          .3      94.60
        1.7243        1         .0          .0      94.70
        1.7324       13         .4          .4      95.10
        1.7404        3         .1          .1      95.20
        1.7482        7         .2          .2      95.40
        1.7634        7         .2          .2      95.60
        1.7709        2         .1          .1      95.70
        1.7782        9         .3          .3      96.00
        1.7853        1         .0          .0      96.00
        1.7924       12         .4          .4      96.40
        1.7993        5         .2          .2      96.60
        1.8062       10         .3          .3      96.90
        1.8129        4         .1          .1      97.00
        1.8195        8         .2          .3      97.30
        1.8261        1         .0          .0      97.30
        1.8325        5         .2          .2      97.40
        1.8451        7         .2          .2      97.70
```

```
                                   1.8573       4          .1          .1       97.80
                                   1.8633       1          .0          .0       97.80
                                   1.8692       4          .1          .1       98.00
                                   1.8808       2          .1          .1       98.00
                                   1.8921       2          .1          .1       98.10
                                   1.9031       5          .2          .2       98.20
                                   1.9138       1          .0          .0       98.30
                                   1.9243       3          .1          .1       98.40
                                   1.9294       1          .0          .0       98.40
                                   1.9345       2          .1          .1       98.50
                                   1.9445       1          .0          .0       98.50
                                   1.9542       4          .1          .1       98.60
                                   1.9638       2          .1          .1       98.70
                                   1.9731       3          .1          .1       98.80
                                   1.9823       2          .1          .1       98.90
                                   1.9912       1          .0          .0       98.90
                                   2.0000       3          .1          .1       99.00
                                   2.0170       1          .0          .0       99.00
                                   2.0294       1          .0          .0       99.00
                                   2.0334       1          .0          .0       99.10
                                   2.0414       1          .0          .0       99.10
                                   2.0492       2          .1          .1       99.20
                                   2.0569       1          .0          .0       99.20
                                   2.0645       2          .1          .1       99.30
```

```
FILE   GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER

                          2.0719      1         .0         .0      99.30
                          2.0792      1         .0         .0      99.30
                          2.0934      1         .0         .0      99.40
                          2.1139      1         .0         .0      99.40
                          2.1303      3         .1         .1      99.50
                          2.1335      2         .1         .1      99.60
                          2.1461      1         .0         .0      99.60
                          2.1703      1         .0         .0      99.60
                          2.1875      1         .0         .0      99.60
                          2.2041      2         .1         .1      99.70
                          2.2148      1         .0         .0      99.70
                          2.2304      1         .0         .0      99.80
                          2.2405      1         .0         .0      99.80
                          2.2430      1         .0         .0      99.80
                          2.2553      1         .0         .0      99.90
                          2.2900      1         .0         .0      99.90
                          2.3010      1         .0         .0      99.90
                          2.3222      1         .0         .0     100.00
                          2.6435      1         .0         .0     100.00
                       -100.0000    146        4.5    MISSING     100.0
                                  ------     ------     ------
                             TOTAL  3277      100.0      100.0
```

```
DESCRIPTIVE STATISTICS OF CU, PB, ZN DATA                                           29 NOV 78        PAGE   30

FILE    GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER


MEAN            1.114      STD ERR          .006      MEDIAN         1.113
MODE             .903      STD DEV          .348      VARIANCE        .121
KURTOSIS         .517      SKEWNESS         .219      RANGE          2.643
MINIMUM          .000      MAXIMUM         2.643

VALID CASES     3131       MISSING CASES    146
```

```
LOGPB      LOG TO BASE 10 OF PB PPM
                                                RELATIVE  ADJUSTED    CUM
                                      ABSOLUTE    FREQ      FREQ      FREQ
CATEGORY LABEL                 CODE     FREQ     (PCT)     (PCT)     (PCT)

                              .0000      370      11.3      11.7     11.70

                              .3010      671      20.5      21.3     33.00

                              .4771        1        .0        .0     33.10

                              .6021      589      18.0      18.7     51.80

                              .7782      461      14.1      14.6     66.40

                              .9031      310       9.5       9.8     76.30

                             1.0000      255       7.8       8.1     84.30

                             1.0792      161       4.9       5.1     89.50

                             1.1461       98       3.0       3.1     92.60

                             1.2041       76       2.3       2.4     95.00

                             1.2553       47       1.4       1.5     96.50

                             1.3010       37       1.1       1.2     97.70

                             1.3424       19        .6        .6     98.30

                             1.3802        6        .2        .2     98.40

                             1.4150        7        .2        .2     98.70

                             1.4472        1        .0        .0     98.70

                             1.4771        4        .1        .1     98.80

                             1.5051        3        .1        .1     98.90

                             1.5563        2        .1        .1     99.00

                             1.5798        1        .0        .0     99.00
```

```
                     1.6021       2         .1         .1      99.10
                     1.6232       2         .1         .1      99.10
                     1.6435       1         .0         .0      99.20
                     1.6628       1         .0         .0      99.20
                     1.6812       3         .1         .1      99.30
                     1.7404       1         .0         .0      99.30
                     1.7482       1         .0         .0      99.40
                     1.7782       2         .1         .1      99.40
                     1.7924       3         .1         .1      99.50
                     1.8062       1         .0         .0      99.60
                     1.8261       1         .0         .0      99.60
                     1.8451       1         .0         .0      99.60
                     1.8573       3         .1         .1      99.70
                     1.8692       2         .1         .1      99.80
                     1.8808       2         .1         .1      99.80
                     1.9138       1         .0         .0      99.90
                     1.9395       1         .0         .0      99.90
                     2.0000       1         .0         .0      99.90
                     2.2405       1         .0         .0     100.00
                     2.3424       1         .0         .0     100.00
                  -100.0000     127        3.9    MISSING     100.0
                             ------     ------     ------
                      TOTAL    3277      100.0      100.0
```

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DESCRIPTIVE STATISTICS OF CU, PB, ZN DATA                                                29 NOV 78          PAGE    33

FILE     GEOCHEM   (CREATION DATE = 29 NOV 78)    CU PB ZN DATA COLLETED BY C. BLOOMER


MEAN              .651      STD ERR           .007      MEDIAN            .605
MODE              .301      STD DEV           .389      VARIANCE          .151
KURTOSIS         -.330      SKEWNESS          .073      RANGE            2.342
MINIMUM           .000      MAXIMUM          2.342

VALID CASES       3150      MISSING CASES     127
```

```
LOGZN      LOG TO BASE 10 OF ZN PPM
                                                  RELATIVE  ADJUSTED    CUM
                                        ABSOLUTE    FREQ      FREQ      FREQ
CATEGORY LABEL                   CODE     FREQ     (PCT)     (PCT)     (PCT)

                                .3010        4        .1        .1       .10

                                .6021       17        .5        .5       .70

                                .7782       21        .6        .7      1.30

                                .9031       19        .6        .6      1.90

                               1.0000       21        .6        .7      2.60

                               1.0792       22        .7        .7      3.30

                               1.1461       27        .8        .9      4.20

                               1.2041       46       1.4       1.5      5.60

                               1.2304        4        .1        .1      5.70

                               1.2553       28        .9        .9      6.60

                               1.2788       15        .5        .5      7.10

                               1.3010       33       1.0       1.0      8.20

                               1.3222       11        .3        .3      8.50

                               1.3424       36       1.1       1.1      9.70

                               1.3802       38       1.2       1.2     10.90

                               1.4150       60       1.8       1.9     12.80

                               1.4472       49       1.5       1.6     14.30

                               1.4771       52       1.6       1.7     16.00

                               1.4914        1        .0        .0     16.00

                               1.5051       33       1.0       1.0     17.00
```

```
                                 1.5185        7          .2          .2       17.30
                                 1.5315       39         1.2         1.2       18.50
                                 1.5441       11          .3          .3       18.90
                                 1.5563       48         1.5         1.5       20.40
                                 1.5682       11          .3          .3       20.70
                                 1.5798       46         1.4         1.5       22.20
                                 1.5911        1          .0          .0       22.20
                                 1.6021       93         2.8         3.0       25.20
                                 1.6128        1          .0          .0       25.20
                                 1.6232       65         2.0         2.1       27.30
                                 1.6435       58         1.8         1.8       29.10
                                 1.6532        1          .0          .0       29.10
                                 1.6628       76         2.3         2.4       31.60
                                 1.6812       62         1.9         2.0       33.50
                                 1.6902       18          .5          .6       34.10
                                 1.6990       56         1.7         1.8       35.90
                                 1.7160       94         2.9         3.0       38.90
                                 1.7324       68         2.1         2.2       41.00
                                 1.7482       79         2.4         2.5       43.50
                                 1.7559        2          .1          .1       43.60
                                 1.7634       86         2.6         2.7       46.30
                                 1.7782       90         2.7         2.9       49.20
                                 1.7924       50         1.5         1.6       50.80
                                 1.7993       13          .4          .4       51.20
```

```
                            1.8062       60        1.8         1.9      53.10
                            1.8129       17         .5          .5      53.60
                            1.8195       35        1.1         1.1      54.70
                            1.8261        5         .2          .2      54.90
                            1.8325       60        1.8         1.9      56.80
                            1.8388        6         .2          .2      57.00
                            1.8451       60        1.8         1.9      58.90
                            1.8513        2         .1          .1      59.00
                            1.8573       60        1.8         1.9      60.90
                            1.8633        3         .1          .1      61.00
                            1.8692       22         .7          .7      61.70
                            1.8751       13         .4          .4      62.10
                            1.8808       40        1.2         1.3      63.30
                            1.8865       17         .5          .5      63.90
                            1.8921       42        1.3         1.3      65.20
                            1.8976        1         .0          .0      65.20
                            1.9031       52        1.6         1.7      66.90
                            1.9138       33        1.0         1.0      67.90
                            1.9191       14         .4          .4      68.40
                            1.9243       29         .9          .9      69.30
                            1.9294       25         .8          .8      70.10
                            1.9345       26         .8          .8      70.90
                            1.9395       15         .5          .5      71.40
                            1.9445       27         .8          .9      72.30
```

```
                              1.9494        5          .2          .2      72.40
                              1.9542       36         1.1         1.1      73.60
                              1.9590       13          .4          .4      74.00
                              1.9638       22          .7          .7      74.70
                              1.9685        8          .2          .3      74.90
                              1.9731       21          .6          .7      75.60
                              1.9777       11          .3          .3      75.90
                              1.9823       20          .6          .6      76.60
                              1.9868       17          .5          .5      77.10
                              1.9912       12          .4          .4      77.50
                              2.0000       33         1.0         1.0      78.50
                              2.0086       22          .7          .7      79.20
                              2.0128        7          .2          .2      79.50
                              2.0170        4          .1          .1      79.60
                              2.0212       12          .4          .4      80.00
                              2.0253        7          .2          .2      80.20
                              2.0294       10          .3          .3      80.50
                              2.0334        5          .2          .2      80.70
                              2.0414       28          .9          .9      81.60
                              2.0492       11          .3          .3      81.90
                              2.0531        1          .0          .0      81.90
                              2.0569        5          .2          .2      82.10
                              2.0607       13          .4          .4      82.50
                              2.0645       21          .6          .7      83.20
```

```
                    2.0682      3      .1      .1     83.30
                    2.0719      9      .3      .3     83.60
                    2.0792     19      .6      .6     84.20
                    2.0864      9      .3      .3     84.40
                    2.0899      6      .2      .2     84.60
                    2.0934      6      .2      .2     84.80
                    2.0969      7      .2      .2     85.00
                    2.1004     16      .5      .5     85.60
                    2.1038      1      .0      .0     85.60
                    2.1072     10      .3      .3     85.90
                    2.1106      1      .0      .0     85.90
                    2.1139     17      .5      .5     86.50
                    2.1206      9      .3      .3     86.80
                    2.1239      5      .2      .2     86.90
                    2.1271      2      .1      .1     87.00
                    2.1303      5      .2      .2     87.10
                    2.1335     11      .3      .3     87.50
                    2.1367      2      .1      .1     87.60
                    2.1399      7      .2      .2     87.80
                    2.1461     19      .6      .6     88.40
                    2.1523      4      .1      .1     88.50
                    2.1584      8      .2      .3     88.80
                    2.1614      9      .3      .3     89.00
                    2.1644      6      .2      .2     89.20
```

```
                    2.1703       3        .1         .1      89.30
                    2.1761       9        .3         .3      89.60
                    2.1847       1        .0         .0      89.70
                    2.1875       3        .1         .1      89.70
                    2.1903       7        .2         .2      90.00
                    2.1931       3        .1         .1      90.10
                    2.1959       1        .0         .0      90.10
                    2.1987       6        .2         .2      90.30
                    2.2041      10        .3         .3      90.60
                    2.2095       5        .2         .2      90.80
                    2.2122       2        .1         .1      90.80
                    2.2148       1        .0         .0      90.90
                    2.2175       5        .2         .2      91.00
                    2.2201       5        .2         .2      91.20
                    2.2304      10        .3         .3      91.50
                    2.2355       3        .1         .1      91.60
                    2.2405       4        .1         .1      91.70
                    2.2430       2        .1         .1      91.80
                    2.2455       1        .0         .0      91.80
                    2.2504       2        .1         .1      91.90
                    2.2553       5        .2         .2      92.00
                    2.2601       1        .0         .0      92.10
                    2.2648       3        .1         .1      92.20
                    2.2672       3        .1         .1      92.30
```

```
2.2742     1     .0     .0    92.30
2.2788     9     .3     .3    92.60
2.2878     2     .1     .1    92.60
2.2900     2     .1     .1    92.70
2.3010    20     .6     .6    93.30
2.3032     1     .0     .0    93.40
2.3118     1     .0     .0    93.40
2.3222    10     .3     .3    93.70
2.3324     1     .0     .0    93.70
2.3424    12     .4     .4    94.10
2.3522     3     .1     .1    94.20
2.3617     8     .2     .3    94.50
2.3711     5     .2     .2    94.60
2.3802     4     .1     .1    94.80
2.3892     4     .1     .1    94.90
2.3979    12     .4     .4    95.30
2.4065     5     .2     .2    95.40
2.4150     4     .1     .1    95.60
2.4249     1     .0     .0    95.60
2.4314     4     .1     .1    95.70
2.4472     5     .2     .2    95.90
2.4548     3     .1     .1    96.00
2.4624     3     .1     .1    96.10
2.4771     8     .2     .3    96.30
```

```
                    2.4914      3       .1       .1      96.40
                    2.5024      1       .0       .0      96.40
                    2.5051      6       .2       .2      96.60
                    2.5119      1       .0       .0      96.70
                    2.5185      8       .2       .3      96.90
                    2.5250      4       .1       .1      97.00
                    2.5315      3       .1       .1      97.10
                    2.5378      2       .1       .1      97.20
                    2.5441      2       .1       .1      97.30
                    2.5563      2       .1       .1      97.30
                    2.5623      2       .1       .1      97.40
                    2.5682      2       .1       .1      97.50
                    2.5740      2       .1       .1      97.50
                    2.5798      1       .0       .0      97.60
                    2.5911      1       .0       .0      97.60
                    2.6021      4       .1       .1      97.70
                    2.6128      3       .1       .1      97.80
                    2.6284      1       .0       .0      97.80
                    2.6335      1       .0       .0      97.90
                    2.6435      2       .1       .1      97.90
                    2.6532      2       .1       .1      98.00
                    2.6628      1       .0       .0      98.00
                    2.6721      1       .0       .0      98.10
                    2.6767      1       .0       .0      98.10
```

```
                         2.6902        2         .1         .1       98.20
                         2.6990        1         .0         .0       98.20
                         2.7076        2         .1         .1       98.30
                         2.7160        2         .1         .1       98.30
                         2.7404        3         .1         .1       98.40
                         2.7482        2         .1         .1       98.50
                         2.7559        3         .1         .1       98.60
                         2.7634        3         .1         .1       98.70
                         2.7709        4         .1         .1       98.80
                         2.7782        1         .0         .0       98.80
                         2.7924        2         .1         .1       98.90
                         2.8062        2         .1         .1       99.00
                         2.8129        2         .1         .1       99.00
                         2.8195        1         .0         .0       99.00
                         2.8261        1         .0         .0       99.10
                         2.8451        1         .0         .0       99.10
                         2.8692        1         .0         .0       99.10
                         2.8751        2         .1         .1       99.20
                         2.9031        1         .0         .0       99.20
                         2.9320        1         .0         .0       99.30
                         2.9542        2         .1         .1       99.30
                         3.0000        2         .1         .1       99.40
                         3.0212        2         .1         .1       99.50
                         3.0414        3         .1         .1       99.60
```

```
FILE    GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER

                         3.0607       2        .1        .1     99.60

                         3.0792       1        .0        .0     99.70

                         3.1139       2        .1        .1     99.70

                         3.1303       1        .0        .0     99.70

                         3.1461       1        .0        .0     99.80

                         3.1903       1        .0        .0     99.80

                         3.2304       1        .0        .0     99.80

                         3.3010       4        .1        .1    100.00

                         3.4914       1        .0        .0    100.00

                      -100.0000     127       3.9   MISSING   100.0
                                 ------    ------    ------
                          TOTAL    3277     100.0     100.0

MEAN          1.794      STD ERR          .006      MEDIAN         1.792
MODE          1.716      STD DEV          .361      VARIANCE        .131
KURTOSIS      2.177      SKEWNESS         .108      RANGE          3.190
MINIMUM        .301      MAXIMUM         3.491

VALID CASES    3150      MISSING CASES    127
```

```
            26.      SCATTERGRAM    CU,PB,ZN
            27.      STATISTICS     ALL

**** GIVEN WORKSPACE ALLOWS FOR   3279 CASES FOR SCATTERGRAM PROBLEM *****
```

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DESCRIPTIVE STATISTICS OF CU, PB, ZN DATA                                           29 NOV 78        PAGE   45

FILE   GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER
SCATTERGRAM OF   (DOWN) CU       COPPER PPM                        (ACROSS) PB       LEAD PPM
                11.95     33.85     55.75     77.65     99.55    121.45    143.35    165.25    187.15    209.05
            .+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+.
    440.00  +   *                              I                               I                                  +      440.00
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    396.10  +                                  I                               I                                  +      396.10
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    352.20  +                                  I                               I                                  +      352.20
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    308.30  +                                  I                               I                                  +      308.30
            I                                  I                               I                                  I
            I-----------------------------------------------------------------------------------------------------I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    264.40  +                                  I                               I                                  +      264.40
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    220.50  +                                  I                               I                                  +      220.50
            I                                  I                               I                                  I
            I*                                 I                               I                                  I
            I**                                I                               I                                  I
            I                                  I                               I                                  I
    176.60  + *                                I                               I                                  +      176.60
            I 2  *                             I                               I                                  I
            I*    **                           I                               I                                  I
            I-*---------------------------------------------------------------------------------------------------I
            I             *                    I                               I                                  I
    132.70  +2* 2  *                           I                               I                                  +      132.70
            I* *                               I                               I                                  I
            I*2       *                        I                               I                                  I
            I* ** **    *                      I                               I                                  I
            I* ****                            I                               I                                  I
     88.80  +5*  2  * *                        *                               I                                  +       88.80
            I3** **    *                       I                               I                                  I
            I4*334 *  *           *            I                               I                                  I
            I9834223 * 2*  *  * *              I                               I                                  I
            I79959  3 **2                      I          *                    I                                  I
     44.90  +9959*2***3 *                     **                               I                                  +       44.90
            I9898933534*2*      *     *        I                               I                                  I
            I99999939774* *    2               I                               I            *                     I
            I999999999483    *   **        * 2 I                               I                                 *I
            I999999999922 22 *    2      2   2 I  * *                          I                                  I
      1.00  +9999999774                 **     I                               I                                  +        1.00
            .+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+.
            1.00     22.90     44.80     66.70     88.60    110.50    132.40    154.30    176.20    198.10    220.00
```

```
STATISTICS..

  CORRELATION (R)-          .12079       R SQUARED       -          .01459       SIGNIFICANCE   -          .00001
  STD ERR OF EST -        20.78699       INTERCEPT (A)   -        16.46408       SLOPE (B)      -          .29162

  PLOTTED VALUES -      3131             EXCLUDED VALUES-            0           MISSING VALUES -       146

                              '********' IS PRINTED IF A COEFFICIENT CANNOT BE COMPUTED.
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DESCRIPTIVE STATISTICS OF CU, PB, ZN DATA                                          29 NOV 78        PAGE   47

FILE   GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER
SCATTERGRAM OF    (DOWN) CU      COPPER PPM                        (ACROSS) ZN       ZINC PPM
               156.90    466.70    776.50   1086.30   1396.10   1705.90   2015.70   2325.50   2635.30   2945.10
            .+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+.
    440.00  +*                                 I                               I                                  +      440.00
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    396.10  +                                  I                               I                                  +      396.10
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    352.20  +                                  I                               I                                  +      352.20
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    308.30  +                                  I                               I                                  +      308.30
            I                                  I                               I                                  I
            I-----------------------------------------------------------------------------------------------------I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    264.40  +                                  I                               I                                  +      264.40
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    220.50  +                                  I                               I                                  +      220.50
            I                                  I                               I                                  I
            I   *                              I                               I                                  I
            I                   *    *         I                               I                                  I
            I                                  I                               I                                  I
    176.60  +    *                             I                               I                                  +      176.60
            I  * *                             I                    *          I                                  I
            I *  *   *                         I                               I                                  I
            I--*--------------------------------------------------------------------------------------------------I
            I             *                    I                               I                                  I
    132.70  + *** *     *            *         I                               I                                  +      132.70
            I* *                               I                               I                                  I
            I   3     *                        I                               I                                  I
            I** 2                              *                               I                                 *I
            I *3*                              I                               I                                  I
     88.80  +*2  2**2    **                    I                               I                                  +       88.80
            I*2* 3*                            I                               I                                  I
            I 5253*    *       *               I                               I                                  I
            I*9477**3 **  *    *          *    I                               I                                  I
            I 5996*3*22       *   *            I                               I                                  I
     44.90  +*89867   2 *  *        *          I                               I                                  +       44.90
            I39999 *3* 22**   ***              I                               I                                  I
            I999995824*32 ** * *     *         I  *      *                     I                                  I
            I999999575**3**23*  4 *    *     * I*                            3 I                                  I
            I9999999996856*2 2 3*23      **  * *2 * *  2  *    *             * I                                  I
      1.00  +999999954235 *  * **  *           I                               I                                  +        1.00
            .+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+.
            2.00    311.80    621.60    931.40   1241.20   1551.00   1860.80   2170.60   2480.40   2790.20   3100.00
```

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STATISTICS..

  CORRELATION (R)-           .18784     R SQUARED        -          .03528     SIGNIFICANCE    -            .00001

  STD ERR OF EST -         20.56759     INTERCEPT (A)    -        15.93744     SLOPE (B)       -            .02652

  PLOTTED VALUES -       3131           EXCLUDED VALUES-           0           MISSING VALUES -         146

                              '********' IS PRINTED IF A COEFFICIENT CANNOT BE COMPUTED.
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DESCRIPTIVE STATISTICS OF CU, PB, ZN DATA                                           29 NOV 78        PAGE   49

FILE   GEOCHEM  (CREATION DATE = 29 NOV 78)   CU PB ZN DATA COLLETED BY C. BLOOMER
SCATTERGRAM OF   (DOWN) PB       LEAD PPM                          (ACROSS) ZN       ZINC PPM
               156.90    466.70    776.50   1086.30   1396.10   1705.90   2015.70   2325.50   2635.30   2945.10
            .+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+.
    220.00  +               *                  I                               I                                  +      220.00
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    198.10  +                                  I                               I                                  +      198.10
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    176.20  +                                  I                               I                                  +      176.20
            I   *                              I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    154.30  +                                  I                               I                                  +      154.30
            I                                  I                               I                                  I
            I-----------------------------------------------------------------------------------------------------I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    132.40  +                                  I                               I                                  +      132.40
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                                  I                               I                                  I
    110.50  +                                  I                               I                                  +      110.50
            I                                  I                               I                                  I
            I                                  I                               I                                  I
            I                     *            I                               I                                  I
            I                                  I                               I                                  I
     88.60  +                                  I                               I                                  +       88.60
            I*                                 I                               I                                  I
            I*                                 I                               I                                  I
            I---------*--*----------------------------------------------------------------------------------------I
            I3    *   *                        I                               I                                  I
     66.70  +2                                 I                               I                                  +       66.70
            I*                                 I                               I                                  I
            I3 *   *                           I                               I                                  I
            I*          *                      I                               I                                  I
            I                                  I                               I                                  I
     44.80  + *   * *             *            I                               I                                  +       44.80
            I   2         *                    I                               I                                  I
            I         **  *                    I                               I                                  I
            I* *      **  *                    I                               I                                  I
            I **  2       *                    I                               I                                  I
     22.90  + **3 *** *     * * 2              I                               I                                  +       22.90
            I*39964*22*  2*                    I                             * I                                  I
            I*89992333 * 2*       *            I*                            * I                                  I
            I99999992445*2 * 2 *2**    * **    **      2 **    *               I                                  I
            I999999979368* 2   3** * *    *  * I* 2 *                        * I                                 *I
      1.00  +993999999359*23*3*43 * *2       * *                    *        * I                                  +        1.00
            .+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+----+.
            2.00    311.80    621.60    931.40   1241.20   1551.00   1860.80   2170.60   2480.40   2790.20   3100.00
```

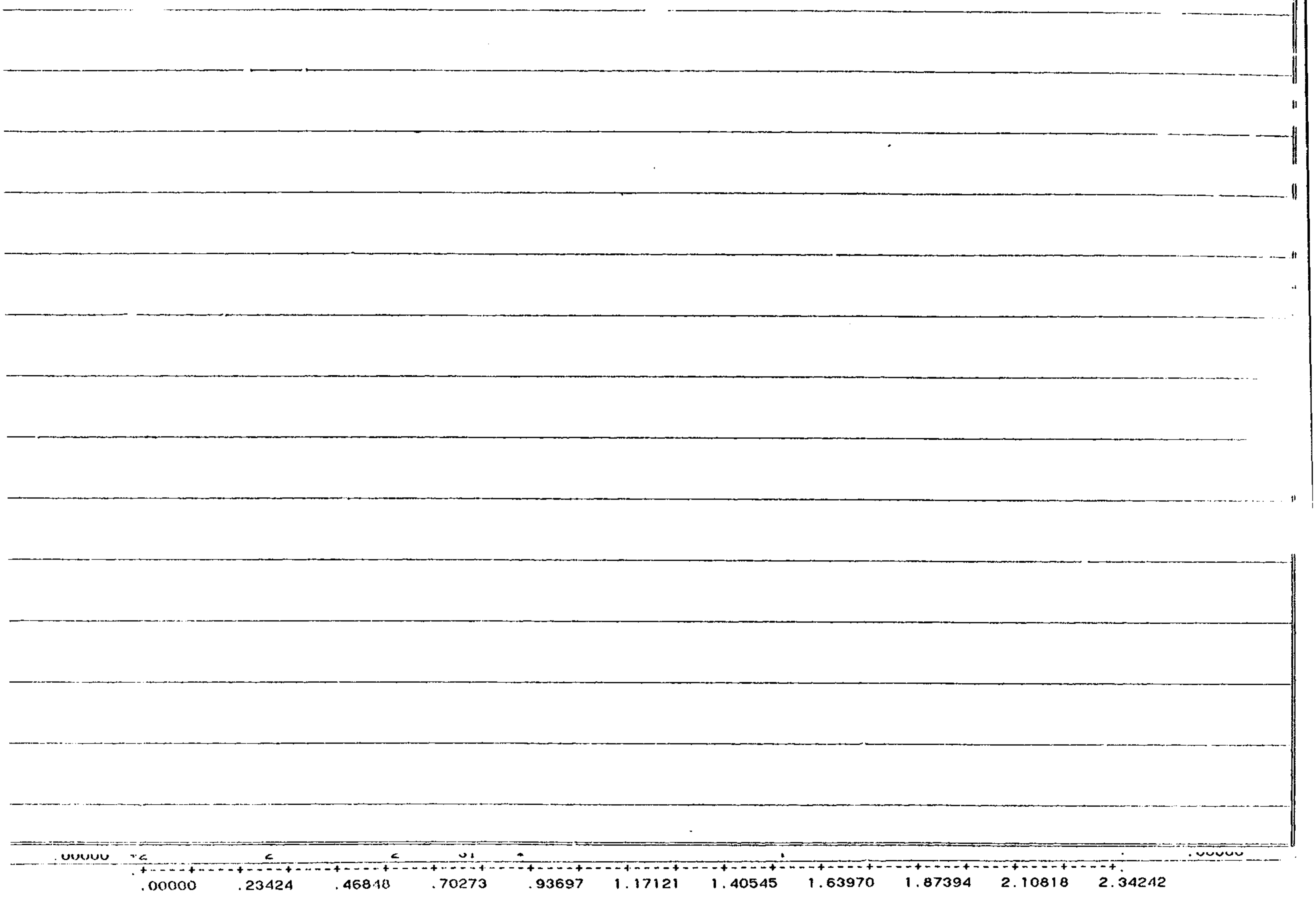
```
STATISTICS..

  CORRELATION (R)-         .12064      R SQUARED       -        .01455     SIGNIFICANCE    -          .00001
  STD ERR OF EST -        8.82344      INTERCEPT (A)   -       6.07526     SLOPE (B)       -          .00725

  PLOTTED VALUES -      3150           EXCLUDED VALUES-        0           MISSING VALUES -       127

                          '********' IS PRINTED IF A COEFFICIENT CANNOT BE COMPUTED.
```

```
**** GIVEN WORKSPACE ALLOWS FOR   3279 CASES FOR SCATTERGRAM PROBLEM *****
```



APPENDIX II

SECTION III

GRID GEOCHEMISTRY RESULTS

GRID 78-9

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DATE 4-OCT-78

PROJECT NO. 716-1-1049

GEOCHEMICAL ANALYSIS

PAGE: 11 OF 36

SAMPLE NUMBER GRID 78-9	CU PPM	ZN PPM	PB PPM
L1E			
3+50S		64	4
3+00S		66	2
2+50S		54	2
2+00S		74	4
1+50S		44	6
1+00S		84	6
0+50S		96	8
0+00BL		100	<1
0+50N		36	<1
1+00N		72	10
1+50N		80	4
2+00N		94	4
2+50N		74	2
3+00N		40	2
3+50N		72	<1
L2E			
3+50S		56	4
3+00S		60	2
2+50S		74	8
2+00S		64	8
1+50S	20	72	10
1+00S	16	62	6
0+50S	14	72	4
0+00BL	8	66	<1
0+50N	12	70	4
1+00N	18	60	4
1+50N	26	50	6
2+00N	13	56	2
2+50N	13	70	4
3+00N	12	70	2
3+50N	20	90	4
L3E			
3+50S	12	64	4
3+00S	8	50	4
2+50S	8	46	2
2+00S	10	36	<1
1+50S	8	72	2
1+00S	10	60	8
0+50S	13	102	2

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GEOCHEMICAL ANALYSIS

PAGE: 12 OF 36

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-9			
0+00BL	13	82	2
0+50N	12	84	2
1+00N	14	68	2
1+50N	13	90	4
2+00N	14	95	2
2+50N	18	102	8
3+00N	30	115	6
3+50N	12	54	2
L4E			
3+50S	20	48	<1
3+00S	14	64	2
2+50S	12	54	2
2+00S	16	58	4
1+50S	13	40	2
1+00S	10	50	4
0+50S	34	70	4
0+00BL	10	66	2
0+50N	8	90	2
1+00N	6	97	2
1+50N	8	97	2
2+00N	12	102	4
2+50N	16	95	<1
3+00N	13	73	<1
3+50N	20	100	4
L5E			1
3+50S	7	42	<1
3+00S	41	14	<1
2+50S	13	46	2
2+00S	13	170	2
1+50S	8	40	2
1+00S	7	66	<1
0+50S	18	16	<1
0+00BL	28	110	4
0+50N	14	70	2
1+00N	12	95	8
1+50N	8	68	4
2+00N	12	64	6
2+50N	13	78	.4
3+00N	10	82	4
3+50N	8	60	4

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SAMPLE NUMBER GRID 78-9	CU PPM	ZN PPM	PB PPM
L6E			
3+50S	10	78	<1
3+00S	3	70	4
2+50S	3	98	<1
2+00S	3	44	2
1+50S	12	58	2
1+00S	7	50	2
0+50S	14	36	2
2+00BL	14	70	4
0+50N	8	68	6
1+00N	7	40	<1
1+50N	14	70	6
2+00N	14	60	2
2+50N	6	58	2
3+00N	8	58	<1
3+50N	12	56	<1
L7E			
3+50S	13	90	2
3+00S	22	150	2
2+50S	8	95	<1
2+00S	7	78	2
1+50S	6	28	<1
1+00S	10	10	2
0+50S	14	58	<1
0+00BL	12	64	2
0+50N	10	56	2
1+00N	12	52	4
1+50N	10	64	6
2+00N	6	58	6
2+50N	8	170	2
3+00N	10	62	2
3+50N	10	60	4
L8E			
3+50S	10	60	4
3+00S	7	40	6
2+50S	10	46	2
2+00S	10	60	2
1+50S	13	80	2
1+00S	10	42	2
0+50S	8	50	2

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GEOCHEMICAL ANALYSIS

PAGE: 14 OF 36

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-9			
0+00BL	8	78	<1
0+50N	7	50	2
1+00N	8	48	<1
1+50N	3	44	<1
2+00N	10	60	<1
2+50N	8	56	4
3+00N	12	48	4
3+50N	14	84	2
L9E			
3+50S	18	64	<1
3+00S	31	110	2
2+50S	12	70	<1
2+00S	10	122	<1
1+50S	8	58	<1
1+00S	10	82	4
0+50S	13	82	2
0+00BL	12	108	2
0+50N	7	46	<1
1+00N *	NSS	NSS	NSS
1+50N *	NSS	NSS	NSS
2+00N *	NSS	NSS	NSS
2+50N	8	28	2
3+00N	16	54	6
3+50N	14	80	2
L1+50E 00+0BL	14	70	<1
L2+50E 00+0BL	7	70	2
3+80E 00+0BL	10	42	<1
4+50E 00+0BL	13	92	2
5+50E 00+0BL	31	56	<1
6+50E 0+00BL	7	78	<1
7+50E 0+00BL	13	48	2
8+50E 0+00BL	4	46	2

*NOT ENOUGH SAMPLE

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GEOCHEMICAL ANALYSIS

PAGE: 15 OF 36

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
L7E			
4+00S	10	64	2
3+50S	16	124	14
3+00S	12	124	4
2+50S	20	64	4
2+00S	20	80	2
1+50S	30	84	6
1+00S	18	66	4
0+50S	18	66	2
BL0+00	24	66	2
0+50N	31	64	2
1+00N	20	91	2
1+50N	20	62	<1
2+00N	20	90	4
2+50N	16	68	2
3+00N	12	58	2
3+50N	21	68	<1
4+00N	13	56	2
L2E			
4+00S	12	48	2
3+50S	30	318	40
3+00S	18	235	18
2+50S	41	115	2
2+00S	8	90	2
1+50S	8	72	2
1+00S	12	91	2
0+50S	33	72	6
BL0+00	NSS*	NSS	NSS
0+50N	16	64	4
1+00N	8	56	4
1+50N	8	62	2
2+00N	10	70	2
2+50N	20	78	2
3+00N	30	60	4
3+50N	12	52	2
4+00N	6	54	2
L3E			
4+00S	4	200	4
3+50S	8	50	4
3+00S	13	162	4

*NOT SUFFICIENT SAMPLE

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
2+50S	12	70	2
2+00S	20	95	4
1+50S	13	142	2
1+00S	16	102	2
0+50S	14	98	2
0+00BL	12	82	2
0+50N	26	64	4
1+00N	16	58	2
1+50N	14	68	4
2+00N	12	72	2
2+50N	7	52	2
3+00N	16	78	4
3+50N	20	62	2
4+00N	22	60	4
L4E			
4+00S	21	34	2
3+50S	13	46	2
3+00S	16	56	2
2+50S	14	72	2
2+00S	14	95	4
1+50S	26	130	2
1+00S	14	82	4
0+50S	10	95	2
BL0+00	18	90	<1
0+50N	16	80	2
1+00N	10	62	4
1+50N	16	68	<1
2+00N	16	48	2
2+50N	21	72	4
3+00N	24	66	4
3+50N	13	78	2
4+00N	18	62	4
L5E			
4+00S	54	78	4
3+50S	136	58	4
3+00S	62	72	2
2+50S	38	93	10
2+00S	66	56	2
1+50S	50	70	6
1+00S	13	52	2

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GRID 78-10

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GEOCHEMICAL ANALYSIS

PAGE: 17 OF 36

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
0+50S	12	70	2
0+00BL	14	120	4
0+50N	20	68	2
1+00N	14	52	4
1+50N	13	56	6
2+00N	14	28	<1
2+50N	12	40	<1
3+00N	13	44	4
3+50N	21	60	2
4+00N	16	50	4
L6E			
4+00S	16	80	6
3+50S	28	78	6
3+00S	84	48	<1
2+50S	24	66	8
2+00S	40	300	10
1+50S	20	90	<1
1+00S	22	64	6
0+50S	21	100	<1
BL0+00	41	76	4
0+50N	60	76	4
1+00N	20	80	6
1+50N	6	56	<1
2+00N	8	115	6
2+50N	10	44	2
3+00N	16	70	4
3+50N	16	44	4
4+00N	31	58	8
L7E			
4+00S	10	150	2
3+50S	16	76	4
3+00S	21	48	2
2+50S	28	56	6
2+00S	20	58	2
1+50S	24	94	6
1+00S	13	74	20
0+50S	MISSING SAMPLE	MISSING SAMPLE	
BL0+00	30	115	6
0+50N	26	125	2
1+00N	24	160	6

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GEOCHEMICAL ANALYSIS

PAGE: 18 OF 36

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
1+50N	22	270	22
2+00N	16	115	20
2+50N	10	100	2
3+00N	13	96	2
3+50N	62	76	4
4+00N	13	60	2
L8E			
4+00S	31	76	2
3+50S	31	62	4
3+00S	16	60	<1
2+50S	112	12	2
2+00S	84	12	<1
1+50S	21	130	6
1+00S	MISSING SAMPLE		
0+50S	18	145	10
BL0+00	13	98	8
0+50N	51	150	8
0+00N	18	145	6
1+50N	12	98	2
2+00N	8	140	6
2+50N	52	89	12
3+00N	8	48	2
3+50N	10	120	2
4+00N	12	130	10
L9E			
4+00S	98	64	6
3+50S	24	105	2
3+00S	16	120	2
2+50S	7	66	<1
2+00S	70	266	38
1+50S	34	107	14
1+00S	13	145	4
0+50S	16	118	2
BL0+00	54	200	10
0+50N	31	78	6
1+00N	16	135	10
1+50N	12	105	4
2+00N	8	107	<1
2+50N	26	105	10
3+00N	8	78	4

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PAGE: 19 OF 36

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
3+50N	12	102	2
4+00N	7	68	<1
L10E			
4+00S	48	430	2
3+50S	20	86	2
3+00S	31	102	6
2+50S	18	125	4
2+00S	4	26	<1
1+50S	14	145	14
1+00S	36	76	6
0+50S	MISSING SAMPLE		
BL0+00	MISSING SAMPLE		
0+50N	13	60	2
1+00N	66	40	4
1+50N	7	44	<1
2+00N	72	145	48
2+50N	18	62	4
3+00N	7	58	2
3+50N	8	60	<1
4+00N	16	74	4
L11E			
4+00S	30	120	2
3+50S	56	210	6
3+00S	80	125	2
2+50S	20	72	10
2+00S	21	120	8
1+50S	21	92	4
1+00S	33	66	4
0+50S	63	140	12
BL0+00	8	110	<1
0+50N	22	60	4
1+00N	94	365	76
1+50N	12	60	4
2+00N	40	210	16
2+50N	10	155	4
3+00N	21	165	72
3+50N	8	110	8
4+00N	MISSING SAMPLE		
L12E			
4+00S	41	58	2

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
3+50S	7	200	2
3+00S	21	80	4
2+50S	92	205	2
2+00S	76	320	6
1+50S	31	195	<1
1+00S	14	225	4
0+50S	12	86	2
BL0+00	6	60	<1
0+50N	4	50	<1
1+00N	36	38	4
1+50N	4	18	<1
2+00N	22	230	46
2+50N	12	115	8
3+00N	6	74	6
3+50N	MISSING SAMPLE		
4+00N	3	34	<1
L13E			
4+00S	62	255	4
3+50S	13	76	2
3+00S	12	52	2
2+50S	13	32	2
2+00S	22	210	6
1+50S	18	120	4
1+00S	8	42	4
0+50S	12	68	8
BL0+00	13	48	2
0+50N	4	30	<1
1+00N	14	40	4
1+50N	26	155	16
2+00N	12	310	32
2+50N	NOT SUFFICIENT SAMPLE		
3+00N	34	62	14
3+50N	6	105	<1
4+00N	50	270	74
L14E			
4+00S	46	130	2
3+50S	18	130	2
3+00S	28	195	2
2+50S	14	52	2
2+00S	14	105	<1

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
1+50S	22	103	2
1+00S	12	34	<1
0+50S	13	66	2
BL0+00	13	105	2
0+50N	18	64	4
1+00N	13	48	2
1+50N	44	86	12
2+00N	14	92	4
2+50N	8	97	14
3+00N	3	24	<1
3+50N	10	58	2
4+00N	33	107	8
L15E			
4+00S	6	60	<1
3+50S	22	180	2
3+00S	14	80	2
2+50S	24	126	<1
2+00S	20	64	<1
1+50S	4	26	<1
1+00S	3	52	2
0+50S	16	86	4
BL0+00	4	30	<1
0+50N	7	110	8
1+00N	4	48	<1
1+50N	7	76	4
2+00N	14	50	<1
2+50N	31	54	2
3+00N	12	50	2
3+50N	8	95	2
4+00N	20	72	6
L16E			
4+00S	8	140	2
3+50S	12	62	4
3+00S	13	76	<1
2+50S	22	145	2
2+00S	13	54	2
1+50S	10	58	2
1+00S	12	52	<1
0+50S	6	38	<1
BL0+00	7	44	<1

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DATE 4-OCT-78

PROJECT NO. 716-1-1049

GEOCHEMICAL ANALYSIS

PAGE: 22 OF 36

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
0+50N	10	64	2
1+00N	10	62	4
1+50N	8	66	<1
2+00N	7	100	4
2+50N	3	64	<1
3+00N	10	85	2
3+50N	10	70	2
4+00N	7	62	<1
L17E			
4+00S	64	26	2
3+50S	62	54	6
3+00S	160	135	12
2+50S	18	92	2
2+00S	33	100	10
1+50S	21	475	24
1+00S	22	365	12
0+50S	22	230	4
BL0+00	18	185	<1
0+50N	13	62	2
1+00N	33	72	4
1+50N	14	40	2
2+00N	4	46	<1
2+50N	10	105	14
3+00N	6	60	4
3+50N	12	80	2
4+00N	8	72	4
L18E			
4+00S	7	30	<1
3+50S	10	92	2
3+00S	100	26	2
2+50S	18	72	6
2+00S	68	52	4
1+50S	21	60	6
1+00S	26	34	<1
0+50S	31	200	16
BL0+00	10	160	6
0+50N	10	50	<1
1+00N	34	52	6
1+50N	38	58	6
2+00N	38	72	10

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GEOCHEMICAL ANALYSIS

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
2+50N	16	60	6
3+00N	21	62	8
3+50N	24	74	8
4+00N	20	68	4
L19E			
4+00S	48	76	4
3+50S	22	92	4
3+00S	42	130	8
2+50S	72	38	<1
2+00S	52	56	6
1+50S	24	52	8
1+00S	12	48	8
0+50S	38	52	6
BL0+00	24	97	8
0+50N	4	46	2
1+00N	1	16	<1
1+50N	3	14	<1
2+00N	10	107	4
2+50N	13	50	4
3+00N	174	75	4
3+50N	14	80	6
4+00N	10	85	2
L20E			
4+00S	14	97	2
3+50S	7	58	<1
3+00S	34	132	6
2+50S	10	42	<1
2+00S	36	28	2
1+50S	21	66	2
1+00S	20	92	6
0+50S	8	54	2
BL0+00	8	48	4
0+50N	62	85	10
1+00N	28	68	6
1+50N	13	64	4
2+00N	6	85	8
2+50N	34	245	14
3+00N	6	74	<1
3+50N	10	58	4
4+00N	8	85	<1

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GEOCHEMICAL ANALYSIS

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
L21E			
4+00S	18	60	<1
3+50S	21	36	2
3+00S	13	40	<1
2+50S	14	40	<1
2+00S	8	30	<1
1+50S	13	30	2
1+00S	13	84	6
0+50S	13	112	14
BL0+00	7	42	<1
1+00N	4	26	<1
0+50N	7	42	2
1+50N	8	32	4
2+00N	8	26	2
2+50N	7	56	<1
3+00N	18	105	2
3+50N	20	123	2
4+00N	13	120	6
L22E			
4+00S	16	50	6
3+50S	8	50	2
3+00S	24	88	8
2+50S	14	64	6
2+00S	12	46	4
1+50S	7	32	2
1+00S	7	22	<1
0+50S	6	22	<1
BL0+00	12	44	4
0+50N	14	74	6
1+00N	21	58	6
1+50N	7	44	<1
2+00N	8	52	<1
2+50N	7	68	4
3+00N	10	110	4
3+50N	7	40	2
4+00N	14	86	6
L23E			
4+00S	12	32	2
3+50S	8	40	2
3+00S	18	84	8

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
2+50S	30	48	2
2+00S	16	82	8
1+50S	26	64	6
1+00S	50	58	8
0+50S	38	88	16
BL0+00	41	130	12
0+50N	18	60	4
1+00N	16	58	6
1+50N	12	54	2
2+00N	20	58	4
2+50N	12	30	2
3+00N	14	58	2
3+50N	8	52	<1
4+00N	14	54	6
L24E 4+00S	36	26	2
3+50S	24	26	4
3+00S	21	40	<1
2+50S	12	38	4
2+00S	13	36	2
1+50S	18	40	2
1+00S	24	34	4
0+50S	20	74	4
BL0+00A	10 } 16	28 } 39	<1 } 2
BL0+00B	22	50	4
0+50N	16	42	6
1+00N	16	62	6
1+50N	13	40	4
2+00N	14	58	2
2+50N	18	68	4
3+00N	16	62	2
3+50N	20	60	2
4+00N	20	70	2
L25E			
4+00S	13	40	<1
3+50S	16	30	<1
3+00S	7	32	2
2+50S	8	34	4
2+00S	13	28	4
1+50S	24	40	<1
1+00S	28	36	2

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-10			
0+50S	31	22	<1
BL0+00	28	32	<1
0+50N	14	28	<1
1+00N	16	28	<1
1+50N	8	42	<1
2+00N	7	72	<1
2+50N	46	80	8
3+00N	21	92	4
3+50N	22	102	6
4+00N	33	92	8
L26E			
4+00S	8	52	<1
3+50S	7	50	2
3+00S	10	40	2
2+50S	38	38	6
2+00S	21	22	4
1+50S	12	36	<1
1+00S	30	18	<1
0+50S	18	18	2
BL0+00	16	22	2
0+50N	8	36	2
1+00N	10	42	4
1+50N	10	54	2
2+00N	7	34	2
2+50N	12	28	<1
3+00N	34	44	4
3+50N	13	50	4
4+00N	12	54	4
L1+50E BL0+00	22	72	2
L2+50E	24	72	4
L3+50E	12	95	2
L4+50E	14	72	2
L5+50E	80	98	2
L6+50E	22	140	10
L7+50E	6	36	<1
L8+50E	30	64	20
L9+50E	4	18	<1
L10+50E	44	100	42
L11+50E	3	22	<1
L12+50E	8	34	2

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PAGE: 27 OF 36

SAMPLE NUMBER GRID 78-10	CU PPM	ZN PPM	PB PPM
L13+50BL0+00	7	92	2
L14+50BL0+00	10	58	2
L15+50BL0+00	8	54	10
L16+50BL0+00	40	83	10
L17+50BL0+00	21	117	4
L18+50BL0+00	31	190	24
L19+50BL0+00	12	48	10
L20+50BL0+00	7	56	<1
L21+50BL0+00	36	89	10
L22+50BL0+00	30	110	10
L23+50BL0+00	14	54	2
L24+50BL0+00	63	42	2
L25+50BL0+00	6	26	2

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GRID 78-11

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GEOCHEMICAL ANALYSIS

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
L0+00			
0+00BL	7	70	<1
0+50N	12	68	4
1+00N	4	36	2
1+50N	7	54	2
2+00N	3	28	2
2+50N	7	72	2
3+00N	14	52	8
3+50N	41	82	10
4+00N	90	120	20
4+50N	16	155	26
5+00N	10	125	2
5+50N	1	44	6
6+00N	16	120	6
6+50N	6	40	2
7+00N	16	153	6
7+50N	21	80	4
8+00N	7	107	6
8+50N	12	145	10
9+00N	6	83	6
9+50N	7	103	6
10+00N	13	120	8
L1W			
0+00BL	4	42	4
0+50N	3	52	4
1+00N	12	66	4
1+50N	10	130	6
2+00N	8	64	6
2+50N	6	64	6
3+00N	18	58	6
3+50N	20	62	4
4+00N	6	34	4
4+50N	3	22	4
5+00N	7	52	10
5+50N	52	48	8
6+00N	54	70	16
6+50N	12	110	8
7+00N	26	145	4
7+50N	21	115	2
8+00N	2	28	4

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GEOCHEMICAL ANALYSIS

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
8+50N	7	58	6
9+00N	10	77	6
9+50N	8	110	6
10+00N	18	130	10
L2W			
0+00BL	12	77	16
0+50N	10	85	10
1+00N	20	130	18
1+50N	7	56	8
2+00N	20	46	10
2+50N	13	52	14
3+00N	12	30	8
3+50NA	16	64	8
3+50NB	26	90	8
4+50N	22	50	6
5+00N	10	48	6
5+50N	14	54	12
6+00N	8	142	4
6+50N	24	97	4
7+00N	26	135	4
7+50N	7	103	6
8+00N	14	550	14
8+50N	13	85	6
9+00N	10	120	8
9+50N	18	46	10
10+00N	21	60	8
L3W			
0+00BL	16	58	<1
0+50N	8	34	2
1+00N	10	54	2
1+50N	56	60	10
2+00N	26	14	2
2+50N	24	14	<1
3+00N	54	123	6
3+50N	33	113	10
4+00N	36	155	22
4+50N	154	50	4
5+00N	13	48	<1
5+50N	24	80	4
6+00N	21	157	2

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GEOCHEMICAL ANALYSIS

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
6+50N	13	137	<1
7+00N	13	72	4
7+50N	7	125	16
8+00N	24	600	24
8+50N	10	52	2
9+00N	13	46	2
9+50N	14	145	6
10+00N	33	290	8
L4W			
0+00BL	8	48	<1
0+50N	12	85	2
1+00N	6	58	2
1+50N	8	85	<1
2+00N	31	14	<1
2+50N	44	34	<1
3+00N	16	44	2
3+50N	16	56	2
4+00N	14	66	2
4+50N	16	48	6
5+00N	30	185	10
5+50N	26	64	18
6+00N	4	16	<1
6+50N	MISSING SAMPLE		
7+00N	3	18	<1
7+50N	7	54	4
8+00N	14	220	18
8+50N	12	165	2
9+00N	7	140	2
9+50N	18	80	4
10+00N	8	80	4
L5W			
0+00BL	12	70	2
0+50N	13	54	2
1+00N	7	60	<1
1+50N	16	72	4
2+00N	18	52	<1
2+50N	12	58	<1
3+00N	12	80	2
3+50N	20	60	2
4+00N	14	56	4

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
4+50N	10	80	2
5+00N	7	52	<1
5+50N	10	64	30
6+00N	12	40	<1
6+50N	104	64	10
7+00N	22	58	2
7+50N	30	100	6
8+00N	10	102	2
8+50N	16	180	12
9+00N	175	123	10
9+50N	7	92	<1
10+00N	4	68	<1
L6W			
0+00BL	8	56	2
0+50N	7	56	<1
1+00N	10	90	<1
1+50N	7	70	2
2+00N	8	126	4
2+50N	8	120	<1
3+00N	20	62	2
3+50N	8	90	4
4+00N	10	107	<1
4+50N	7	115	<1
5+00N	8	80	2
5+50N	12	70	<1
6+00N	6	50	<1
6+50N	18	48	4
7+00N	42	46	<1
7+50N	36	155	2
8+00N	13	48	<1
8+50N	12	46	2
9+00N	10	100	<1
9+50N	10	83	<1
10+00N	14	70	4
L7W			
0+00BL	6	230	<1
0+50N	6	92	2
1+00N	6	44	<1
1+50N	4	58	<1
2+00N	6	83	2

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
2+50N	20	86	6
3+00N	12	52	4
3+50N	7	130	2
4+00N	13	90	2
4+50N	7	130	<1
5+00N	13	56	6
5+50N	8	70	4
6+00N	8	97	4
6+50N	7	60	6
7+00N	8	54	2
7+50N	6	64	<1
8+00N	18	38	<1
8+50N	6	36	2
9+00N	8	220	<1
9+50N	7	93	6
10+00N	4	42	<1
LBW			
0+00BL	4	42	<1
0+50N	3	64	<1
1+00N	6	70	<1
1+50N	8	60	2
2+00N	12	54	8
2+50N	13	80	6
3+00N	18	62	4
3+50N	10	137	4
4+00N	8	150	4
4+50N	6	190	4
5+00N	4	100	2
5+50N	7	64	<1
6+00N	7	110	2
6+50N	6	92	4
7+00N	1	20	<1
7+50N	1	16	2
8+00N	20	56	4
8+50N	8	42	2
9+00N	3	36	2
9+50N	62	54	8
10+00N	12	40	6

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- GAS
- WATER
- OIL
- SOILS
- VEGETATION
- ENVIRONMENTAL ANALYSIS

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BOX 100
CALGARY, ALBERTA

DATE 29-AUG-78

PROJECT NO. 716-1-784

GEOCHEMICAL ANALYSIS

PAGE: 1 OF 7

GRID 78-11

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
BL0+00 L11+00E	12	580	14
L12+00E	18	58	4
L16+00E	10	132	4
L1+00E 0+00BL	18	69	4
1+00S	4	71	4
0+50S	4	24	6
0+50N	4	52	4
1+00N	28	34	4
1+50N	4	20	4
1+50S	14	78	6
2+00S	2	71	<1
2+00N	8	60	4
2+50S	14	330	2
2+50N	2	28	4
3+00S	8	200	6
3+00N	10	66	2
3+50S	16	1000	8
3+50N	2	44	2
4+00S	8	240	2
4+50S	2	24	2
4+50N	120	98	4
5+00S	8	87	<1
5+00N	6	48	4
5+50N	8	330	6
6+00N	4	66	6
6+50N	100	64	8
7+00N	4	140	6
7+50N	6	100	4
8+00N	6	118	2
8+50N	22	66	8
9+00N	14	50	6
9+50N	34	100	12
L2+00E-0+00BL	6	82	4
0+50N	8	66	4
0+50S	4	54	2
1+00S	4	48	2
1+00N	78	20	<1
1+50N	28	140	6
1+50S	4	56	2
2+00N	4	69	<1

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PROJECT NO. 716-1-784

GEOCHEMICAL ANALYSIS

PAGE: 2 OF 7

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
L2+00E-2+00S	6	87	4
2+50S	6	300	10
2+50N	18	58	<1
3+00N	12	104	2
3+00S	4	62	2
3+50N	6	116	<1
3+50S	6	100	6
4+00S	16	240	6
4+00N	6	110	6
4+50S	2	32	2
4+50N	12	48	2
5+00S	2	24	2
5+00N	16	48	4
5+50N	12	62	6
6+00N	2	36	2
6+50N	4	76	10
7+00N	10	76	4
7+50N	14	250	6
8+00N	8	76	8
8+50N	8	142	6
9+00N	12	90	10
9+50N	14	174	10
10+00N	14	56	8
L3+00E-0+00N	16	107	6
0+50S	12	120	4
0+50N	2	48	4
1+00N	30	93	2
1+00S	14	118	2
1+50N	12	132	2
1+50S	10	118	4
2+00N	18	200	4
2+00S	12	140	8
2+50N	6	84	4
2+50S	8	580	6
3+00N	12	140	<1
3+00S	12	87	2
3+50N	14	87	2
3+50S	4	44	2
4+00S	4	48	4
4+00N	54	107	4

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PROJECT NO. 716-1-784

GEOCHEMICAL ANALYSIS

PAGE: 3 OF 7

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
4+50S	14	87	4
5+00S	16	160	4
L4+00E-0+00BL	34	82	6
0+50N	6	78	2
1+00S	14	93	2
1+00N	10	90	4
1+50S	12	96	4
2+00N	14	64	4
2+00S	10	93	6
2+50N	2	52	2
2+50S	10	380	20
3+00N	10	110	6
3+00S	40	110	10
3+50N	20	96	6
3+50S	28	38	6
4+00N	24	163	8
L1+00E-4+00N	22	140	8
L4+00E-4+00S	12	80	6
4+50S	4	90	6
4+50N	30	100	10
5+00S	2	20	4
10+50N	12	300	6
L7+00E-2+50N	18	62	2
3+00N	12	107	4
3+50N	4	44	2
4+00N	4	34	2
4+50N	4	16	6
5+00N	12	87	2
5+50N	20	56	2
6+00N	4	32	6
6+50N	24	135	4
7+00N	18	160	2
7+50N	14	166	6
8+00N	6	50	6
8+50N	14	163	14
9+00N	20	800	12
9+50N	60	640	100
10+00N	6	260	20
L8+00E-0+50S	10	107	4
2+50N	20	107	4

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GEOCHEMICAL ANALYSIS

PAGE: 4 OF 7

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
L8+00E-3+00N	4	87	8
3+50N	8	44	8
4+00N	4	30	4
4+50N	4	54	4
5+00N	8	78	4
5+50N	46	38	4
6+00N	84	116	12
6+50N	64	220	24
7+00N	14	87	10
7+50N	18	98	22
8+00N	44	590	26
8+50N	10	38	10
9+00N	6	120	14
9+50N	14	250	10
10+00N	64	390	32
L9+00E-2 +50N	94	200	10
3+00N	60	280	10
3_50N	66	140	6
4+00N	8	76	4
4+50N	32	440	6
5+00N	12	74	2
5+50N	64	44	2
6+00N	38	520	26
6+50N	24	230	10
7+00N	22	128	8
7+50N	24	180	10
8+00N	14	142	14
8+50N	12	87	14
9+00N	26	300	16
9+50N	24	230	22
10+00N	20	220	22
L10+00E-1+50N	10	107	4
3+00N	10	156	4
3+50N	40	140	10
4+00N	4	42	4
4+50N	14	78	6
5+00N	18	66	2
5+50N	16	87	2
6+00N	20	250	2
6+50N	94	116	16

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GEOCHEMICAL ANALYSIS

PAGE: 5 OF 7

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
L10+00E-7+00N	64	87	42
7+50N	10	80	2
8+00N	34	132	8
8+50N	16	96	6
9+00N	6	90	2
10+00N	22	62	4
L11+00E-0+50N	18	146	6
1+00N	16	69	4
1+50N	12	110	2
2+00N	16	140	2
2+50N	18	96	<1
3+00N	18	135	2
L12+00E-0+50N	16	150	6
1+00N	14	124	6
1+50N	12	90	2
2+00N	20	50	2
2+50N	12	114	6
3+00N	23	100	4
L13+003-0+00N	26	59	2
50N	9	158	2
1+00N	19	94	4
1+50N	14	106	2
2+00N	12	128	4
2+50N	19	97	6
3+00N	20	80	6
3+50N	38	102	8
L13+00E-4+00N	10	42	<1
L15+003E-8+50N	8	59	2
L13+00E-4+50N	7	68	2
5+00N	4	26	4
5+50N	10	69	<1
6+00N	10	57	<1
6+50N	7	37	<1
7+00N	3	68	4
8+00N	27	470	220
8+50N	7	285	4
9+00N	16	44	8
9+50N	5	85	4
10+00N	16	140	16
L14+00E-UNNUMBERED	31	75	8

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PROJECT NO. 716-1-784

GEOCHEMICAL ANALYSIS

PAGE: 6 OF 7

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
L14+00E-4+50N	12	31	2
5+00N	23	72	4
5+50N	11	72	4
6+00N	7	40	2
6+50N	11	52	4
7+00N	11	60	2
7+50N	10	70	4
8+50N	10	37	2
9+00N	23	45	8
9+50N	11	54	4
10+00N	10	120	6
L15+00E-0+00BL	14	245	4
0+50N	10	68	6
1+00N	9	78	4
1+50N	13	124	4
2+00N	12	114	4
2+50N	20	68	2
3+00N	12	140	<1
3+50N	23	60	2
4+00N	16	52	2
4+50N	42	91	6
5+00N	16	66	4
5+50N	8	52	4
6+00N	7	52	2
6+50N	8	42	2
7+00N	14	70	2
7+5N	11	85	2
8+50N	42	85	8
9+00N	12	114	2
9+50N	8	56	60
10+00N	12	46	6
L16+00E-0+50N	14	60	6
1+00N	12	167	4
1+50N	17	167	6
L13+00E-3+50N	4	24	4
SAMPLE X*	18	56	8
L17+00E-10+00N	11	30	4
9+50N	13	100	4
9+00N	15	52	2
8+50N	11	58	4

* SAMPLE X NO SAMPLE NUMBER

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DATE 29-AUG-78

PROJECT NO 716-1-784

GEOCHEMICAL ANALYSIS

PAGE: 7 OF 7

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
L17+00E-8+00N	16	106	6
7+50N	11	54	<1
7+00N	18	97	4
6+50N	13	40	2
6+00N	68	94	8
5+50N	10	21	2
L16+00E-10+00N	29	91	22
9+50N	13	52	4
9+00N	6	75	4
8+50N	3	21	4
8+00N	7	60	6
7+50N	5	16	6
7+00N	14	46	6
6+50N	14	37	4
6+00N	12	60	8
5+50N	10	57	6
5+00N	22	83	6
4+50N	14	94	4
4+00N	15	56	6
3+50N	11	144	8
3+00N	15	100	6
2+50N	16	108	6
2+00N	16	127	6
L15+00E-8+00N	8	58	2

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1=10 3=12
2=11

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CERTIFICATE OF ANALYSIS

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CALGARY, ALBERTA

DATE 14-SEP-78

PROJECT NO. 716-1-851

GEOCHEMICAL ANALYSIS

PAGE: 13 OF 24

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-5			
2+00S	14	82	6
2+50S	18	87	4
3+00S	18	62	8
3+50S	4	18	2
4+00S	12	36	4
L23E 4+50S	16	70	2
5+00S	22	67	2
L24E 5+00N	10	50	2
4+50N	14	620	6
4+00N	26	1000	4
3+50N	32	1150	8
3+00N	20	590	2
2+50N	22	138	2
2+00N	38	40	2
1+50N	34	90	4
1+00N	24	90	2
0+50N	66	105	8
BL0+00	18	67	2
0+50S	42	115	6
1+00S	107	1050	12
1+50S	24	93	6
2+00S	36	80	4
2+50S	16	67	2
3+00S	32	80	4
3+50S	12	46	4
4+00S	28	80	6
4+50S	20	72	<1
5+00S	14	48	4
12 GRID78-11-L3E 4+50N	8	74	2
5+00N	18	60	6
5+50N	14	270	32
6+00N	14	96	8
6+50N	8	220	2
7+00N	8	112	<1
7+50N	28	340	<1
8+00N	66	310	8
8+50N	28	400	40
9+00N	14	280	26
9+50N	12	200	8
10+00N	48	280	76

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GEOCHEMICAL ANALYSIS

PAGE: 14 OF 24

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
13 L4E 5+00N	6	58	6
5+50N	30	146	4
6+00N	8	30	2
6+50N	10	105	2
7+00N	16	200	2
13 L4E 7+50N	8	112	2
8+00N	8	122	18
8+50N	16	650	48
9+00N	6	82	6
9+50N	24	400	44
10+00N	22	190	16
14 L5E 10+00N	14	190	18
9+50N	8	130	4
9+00N	10	160	8
8+50N	6	174	62
8+00N	32	240	8
7+50N	34	220	4
7+00N	8	58	4
6+50N	6	85	2
6+00N	72	42	6
5+50N	12	32	2
5+00N	62	60	8
4+50N	130	58	6
4+00N	4	46	6
3+50N	14	138	4
3+00N	12	115	6
2+50N	18	60	6
2+00N	10	134	4
1+50N	14	82	4
1+00N	8	90	8
0+50N	34	115	6
BL	10	77	4
0+50S	34	112	8
1+00S	4	22	6
1+50S	46	82	4
2+00S	20	126	10
2+50S	18	80	4
3+00S	6	20	2
3+50S	12	30	<1
4+00S	6	16	2

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DATE 14-SEP-78
PROJECT NO. 716-1-851

GEOCHEMICAL ANALYSIS

PAGE: 15 OF 24

SAMPLE NUMBER GRID 78-11	CU PPM	ZN PPM	PB PPM
4+50S	22	16	4
5+00S	164	20	2
15 L6E 5+00S	12	46	2
4+50~~E~~S	12	320	14
4+00~~E~~S	86	22	<1
3+50S	10	26	<1
3+00S	16	46	6
2+50S	10	134	12
2+00S	14	82	6
1+50S	8	110	18
1+00S	16	52	4
0+50S	12	138	4
0+00BL	14	105	2
0+50N	6	44	4
1+00N	16	62	6
1+50N	16	52	4
2+00N	10	70	4
2+50N	8	44	4
3+00N	4	24	2
3+50N	4	46	2
15 L6E 4+00N	14	103	4
4+50N	10	200	4
5+00N	10	86	2
5+50N	18	194	4
6+00N	12	166	6
6+50N	10	158	4
7+00N	9	91	4
7+50N	16	250	6
8+00N	16	235	6
8+50N	14	235	4
9+00N	17	58	6
9+50N	14	182	8
10+00N	7	60	10
? 5+00S L6E	13	103	10
4+50S	8	54	4
4+00S	68	28	2
16 L7E 3+00S	14	28	<1
2+50S	56	97	<1
1+50S	8	34	2
1+00S	9	76	2

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DATE 14-SEP-78

PROJECT NO. 716-1-851

GEOCHEMICAL ANALYSIS

PAGE: 16 OF 24

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
16 L7E 0+50S	38	210	2
3+50S	32	16	<1
2+00S	9	40	2
0+50N	10	166	<1
0+00BL	37	48	<1
1+00N	10	110	2
1+50N	22	69	4
2+00N	14	78	2
17 L8E 5+00S	12	44	2
4+50S	4	36	12
4+00S	100	106	12
3+50S	13	73	4
3+00S	12	64	<1
2+50S	13	129	4
2+00S	10	97	<1
1+50S	21	116	4
1+00S	8	103	<1
0+50S	10	123	4
2+00N	13	133	2
1+00N	42	133	6
1+50N	34	64	4
0+50N	22	77	2
0+00BL	12	133	6
18 L9E 5+00S	64	86	8
4+50S	58	46	<1
4+00S	200	740	<1
3+50S	14	620	14
3+00S	12	76	4
2+50S	38	320	2
2+00S	20	172	6
1+50S	11	67	2
1+00S	13	86	4
0+50S	14	370	6
0+00BL	12	91	2
0+50N	32	560	4
1+00N	12	210	4
2+00N	26	158	2
19 L10E 2+50N	19	176	2
2+00N	50	148	<1
1+50N	31	148	<1

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TELEPHONE (403) 465-9877 TELEX 037-41596

CERTIFICATE OF ANALYSIS

• MINERAL • GAS • WATER • OIL • SOILS • VEGETATION • ENVIRONMENTAL ANALYSIS

SHELL CANADA RESOURCES LTD
P. O. BOX 100
CALGARY, ALBERTA

DATE 14-SEP-78

PROJECT NO. 716-1-851

GEOCHEMICAL ANALYSIS

PAGE: 17 OF 24

	SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
	GRID 78-11			
20	L10E 1+00N	20	210	<1
	0+50N	11	660	4
	BL0+00	13	400	4
	0+50S	21	2000	4
	1+00S	16	1100	6
	1+50S	28	1350	14
	2+00S	45	158	4
	2+50S	66	570	4
	3+00S	18	290	12
	3+50S	90	210	4
	4+00S	23	590	4
	4+50S	13	89	4
	5+00S	38	136	<1
20	L11E 10+00N	12	123	4
	9+50N	6	62	2
	9+00N	14	60	12
	8+50N	18	210	10
	8+00N	14	133	2
	7+50N	23	133	4
	7+00N	18	148	4
20	L11E 6+50N	20	123	2
	6+00N	140	350	2
	5+50N	40	360	<1
	5+00N	10	56	2
	4+50N	40	42	4
	4+00N	15	40	<1
	3+50N	8	89	4
	0+50S	12	1050	4
	1+00S	12	490	2
	1+50S	14	640	2
	2+00S	13	94	2
	2+50S	12	86	2
	3+00S	210	94	<1
	3+50S	11	280	2
	4+00S	33	106	<1
	4+50S	18	58	6
	5+00S	42	91	4
21	L12E 10+00N	6	56	6
	9+50N	3	36	2
	9+00N	15	172	16

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GEOCHEMICAL ANALYSIS

PAGE: 18 OF 24

	SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
	GRID 78-11			
21	L12E 8+50N	18	172	30
	8+00N	42	330	55
	7+50N	14	350	8
	7+00N	5	28	<1
	6+50N	10	235	16
	6+00N	53	146	4
	5+50N	44	330	6
	5+00N	11	190	4
	4+50N	4	21	4
	4+00N	15	136	4
	0+50S	27	450	4
	1+00S	10	144	4
	1+50S	16	230	<1
	2+00S	9	56	<1
	2+50S	10	54	<1
	3+00S	16	49	2
	3+50S	11	49	6
	4+00S	8	240	18
	4+50S	3	24	6
	5+00S	12	54	4
22	L13E 5+00S	26	118	<1
	4+50S	4	26	<1
	4+00S	11	1150	14
	3+50S	29	63	2
	3+00S	14	72	<1
	2+50S	16	26	<1
	2+00S	14	52	<1
	1+50S	20	215	<1
	1+00S	68	136	2
	0+50S	11	200	4
	4+00N	34	116	2
	3+50N	24	85	<1
	3+00N	23	75	2
	2+50N	11	74	2
	2+00N	33	250	<1
	1+50N	8	72	6
	1+00N	12	70	2
	0+50N	14	200	<1
23	L14E 0+00BL	25	335	4
	0+50S	20	235	6

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GEOCHEMICAL ANALYSIS

PAGE: 19 OF 24

	SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
	GRID 78-11			
23	L14E1+00S	20	94	4
	1+50S	12	72	4
	2+00S	20	100	6
	2+50S	16	100	4
	3+00S	10	72	4
	3+50S	10	88	4
	4+00S	11	44	4
	4+50S	10	56	<1
	5+00S	16	52	8
24	L15E 5+00S	58	19	2
	L15E 4+00S	14	158	10
	3+50S	5	83	6
	3+00S	8	94	10
	2+50S	6	63	4
	2+00S	9	570	4
	1+50S	23	440	12
	1+00S	12	1400	12
	0+50S	10	68	4
25	L16E 0+50S	10	154	4
	1+00S	10	72	2
	1+50S	10	72	6
	2+00S	21	162	4
	2+50S	15	375	20
	3+00S	8	40	2
	3+50S	11	1150	8
	4+00S	8	80	8
	4+50S	26	52	2
	5+00S	6	60	2
26	L17E 5+00S	13	49	6
	4+50S	10	40	6
	4+00S	16	68	4
	3+50S	7	72	6
	3+00S	7	26	2
	2+50S	12	78	6
	2+00S	6	28	<1
	1+50S	14	94	4
	1+00S	8	52	4
	0+50S	11	190	4
	0+00BL	18	122	6
	0+50N	22	200	2

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DATE 14-SEP-78

PROJECT NO. 716-1-851

GEOCHEMICAL ANALYSIS

PAGE: 20 OF 24

SAMPLE NUMBER GRID 78-11	CU PPM	ZN PPM	PB PPM
L17E 1+00N	70	210	<1
1+50N	24	102	<1
2+00N	8	190	2
2+50N	20	2000	8
3+00N	22	94	4
3+50N	NOT ENOUGH SAMPLE		
4+00N	13	178	4
4+50N	16	200	<1
5+00N	14	220	6
L18E 10+00N	10	97	8
9+50N	12	88	8
8+50N	26	97	6
8+00N	80	136	10
7+50N	20	112	6
7+00N	13	132	8
6+50N	25	88	8
6+00N	12	245	2
5+50N	11	184	6
5+00N	18	65	<1
4+50N	15	310	4
4+00N	4	72	4
3+50N	14	116	4
3+00N	18	94	2
2+50N	12	110	2
1+00N	18	78	4
1+50N	14	75	6
2+00N	13	60	2
0+50N	12	590	10
BLO +00	10	78	2
0+50S	8	37	4
1+00S	10	72	6
1+50S	10	65	2
2+00S	10	60	2
2+50S	6	33	2
3+00S	14	102	10
3+50S	10	370	10
4+00S	8	30	<1
4+50S	18	144	6
5+00S	14	72	4
L19E 10+00N	8	60	6

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DATE 14-SEP-78

PROJECT NO. 716-1-851

GEOCHEMICAL ANALYSIS

PAGE: 21 OF 24

SAMPLE NUMBER GRID 78-11	CU PPM	ZN PPM	PB PPM
L19E 9+50N	14	80	6
9+00N	14	70	4
8+50N	8	63	<1
8+00N	13	94	6
7+50N	33	100	12
7+00N	32	83	8
6+50N	13	170	2
6+00N	22	91	4
5+00N	22	78	4
5.50 4+50N	25	132	4
4+00N	12	215	4
3+50N	14	65	2
3+00N	4	28	2
2+50N	18	136	4
2+00N	32	335	8
1+50N	6	72	6
1+00N	9	78	4
0+00N	14	40	4
BL0+00	59	70	4
0+50S	15	245	6
1+00S	8	132	2
1+50S	19	150	4
2+00S	8	94	8
2+50S	13	170	6
3+00S	64	174	14
3+50S	5	60	2
4+00S	4	49	<1
4+50S	16	375	18
5+00S	5	35	<1
29 L20E 4+00N	15	83	2
3+50N	16	190	2
3+00N	12	184	4
2+50N	10	110	2
2+00N	14	166	6
1+50N	17	116	2
1+00N	12	210	4
0+50N	15	46	2
BL0+00	8	30	2
0+50S	26	85	6
1+00S	135	97	8

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SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
L20E 1+50S	10	65	4
2+00S	14	140	4
2+50S	16	1300	12
3+00S	24	2000	22
3+50S	5	46	8
4+00S	9	37	2
L21E 4+00N	16	70	2
3+50N	74	91	8
3+00N	3	12	4
2+50N	8	88	8
2+00N	14	42	6
1+50N	11	2000	18
1+00N	28	132	6
0+50N	19	75	6
0+00BL	18	42	4
0+50S	68	42	4
1+00S	45	128	8
1+50S	12	560	8
2+00S	14	170	8
2+50S	16	170	6
3+00S	6	94	4
3+50S	18	360	16
4+00S	36	200	6
4+50S	8	140	4
5+00S	36	750	6
4+00N	20	30	4 ?
3+50N	32	72	2
L22E 3+00N	24	19	2
2+50N	27	68	4
2+00N	26	63	6
1+50N	30	60	<1
1+00N	18	56	<1
0+50N	12	52	<1
0+00BL	34	116	4
0+50S	10	49	2
1+00S	13	116	2
1+50S	8	46	6
2+00S	58	91	6
2+50S	180	133	4
3+00S	32	110	12

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DATE 14-SEP-78
PROJECT NO. 716-1-851

GEOCHEMICAL ANALYSIS

PAGE: 23 OF 24

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
L22E 3+50S	13	94	<1
4+00S	17	194	6
4+50S	90	30	2
5+00S	14	78	2
~~L23E~~ 10+00W	~~12~~	~~104~~	~~6~~
4+00N	22	335	6
3+50N	11	150	4
3+00N	26	128	2
2+50N	40	60	<1
2+00N	8	44	<1
1+50N	48	128	2
1+00N	11	126	2
0+50N	13	100	6
0+00BL	13	72	2
0+50S	40	126	4
1+00S	20	63	4
1+50S	22	650	10
2+00S	58	58	4
2+50S	6	78	6
3+00S	13	335	12
3+50S	6	26	2
4+00S	27	580	10
4+50S	15	106	6
5+00S	12	78	<1
L23E BL0+00 ✓	7	85	6
5+00N ✓	10	97	6
ok L22E 5+00N ✓	51	184	6
ok L20E 4+50S ✓	9	40	<1
ok 5+00S	16	42	2
? L21E 50S	16	100	4
? 0+50S ok	74	550	8
L13E 1+00S	58	126	6
1+50S	16	65	2
? 2+00S	12	56	2
2+50S	10	52	<1
3+00S	60	200	4
3+50S	10	1550	10
4+00S	6	40	2
4+50S	11	58	4
5+00S	12	128	<1

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GEOCHEMICAL ANALYSIS

PAGE: 24 OF 24

SAMPLE NUMBER	CU PPM	ZN PPM	PB PPM
GRID 78-11			
L14E 0+00N	42	1150	10
0+50N	25	1475	4
1+50N	7	68	4
2+00N	5	28	6
2+50N	4	14	4
3+00N	2	17	2
3+50N	12	140	4
4+00N	16	56	4
4+50N	13	40	<1
5+00N	7	35	2
L11E XX .	7	270	2
ok L9E 2+50N	11	17	<1
? L7E 2+00S	20	70	6
004	10	50	6
L1E 1+50S	22	162	10
L1E 2+50S	10	<1	<1
L2E 4+00S	[illegible]	21	<1
GRID 78-5			

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APPENDIX III

Table 4

Grid #	Line Kilometres Cut	# of Soil Samples Taken
78-9	7.1	143
78-10	23.3	466
78-11	44.3	856
TOTAL:	747	1465

Cost: 74.7 line kilometres, cut and chained at $140.63 per line kilometre = $10,505.06.

1,465 soil samples analyzed for copper, lead and zinc at $3.05 each = $4,468.25.

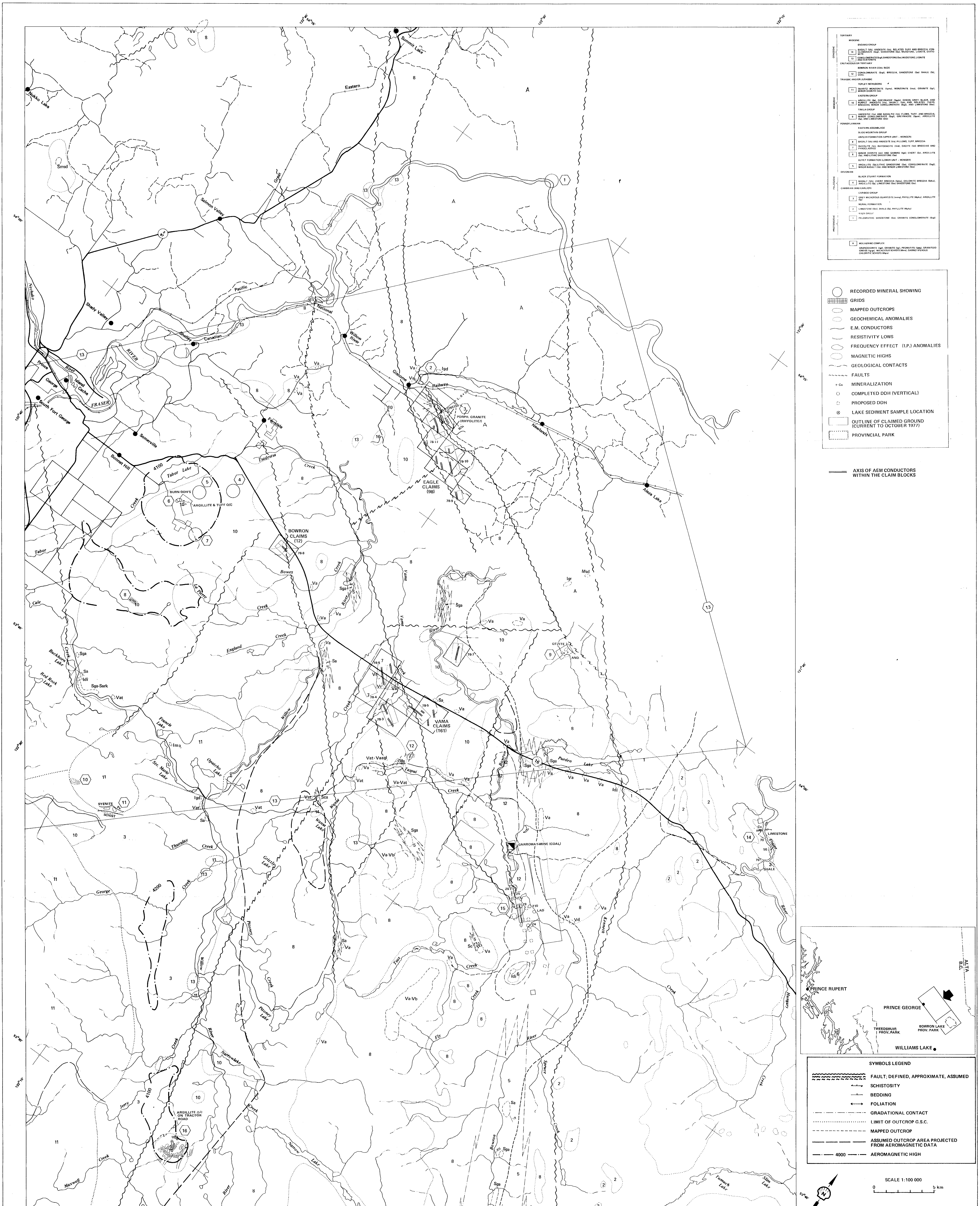
Table 5

Labour	$13,125.00
Line Cutting	$10,505.06
Geochemistry	$ 4,568.25
TOTAL:	$28,098.31

	JULY																															AUGUST																															TOTAL MAN DAYS PER PERSON
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	
BLOOMER C.	X							X	X				X		X						X									X		X	X						X					X	X						X							X					14
GALLAGHER F.								X	X		X	X	X	X	X	X	X		X	X	X	X									X	X	X					X	X	X		X	X	X	X			X										X					25
GEORGE P.		X	X											X			X		X	X	X	X	X	X							X									X		X	X	X	X							X			X			X					19
CARLETON B.													X	X	X	X	X		X	X	X	X									X	X								X		X	X	X	X										X								17
M^c^GILL M.												X	X	X	X	X	X		X	X	X	X	X								X	X	X					X	X	X		X	X	X	X			X							X								23
OLNEY A.																			X	X	X	X	X	X		X	X													X		X	X	X	X		X	X			X	X			X			X					18
HENDRICK P.																			X	X	X	X	X	X		X	X													X		X	X	X	X		X	X			X	X											19
WIERZBICKI R.											X	X	X	X			X		X	X	X	X	X	X		X	X																																				13
MAIZE A.	X	X	X					X	X			X	X			X	X		X	X	X	X	X								X	X							X	X		X	X	X	X		X				X	X			X			X					27
TOTAL MAN DAYS PER DAY	2	2	2					3	3		2	4	6	5	4	4	6		8	8	9	8	6	4		3	3			1	5	5	3					2	4	7		7	7	8	8		3	4			4	4			6			5					175 TOTAL MAN DAYS SPENT ON EAGLE CLAIM GROUP

LABOUR COST: 175 MAN DAYS @ $75.00 PER MAN DAY = $13,125.00
(LABOUR COSTS COVER GEOCHEMICAL SAMPLING, GEOPHYSICAL SURVEYS AND GEOLOGICAL MAPPING. THE DAILY RATE IS AN AVERAGE OF THE TOTAL WAGES PAID).

TABLE 3



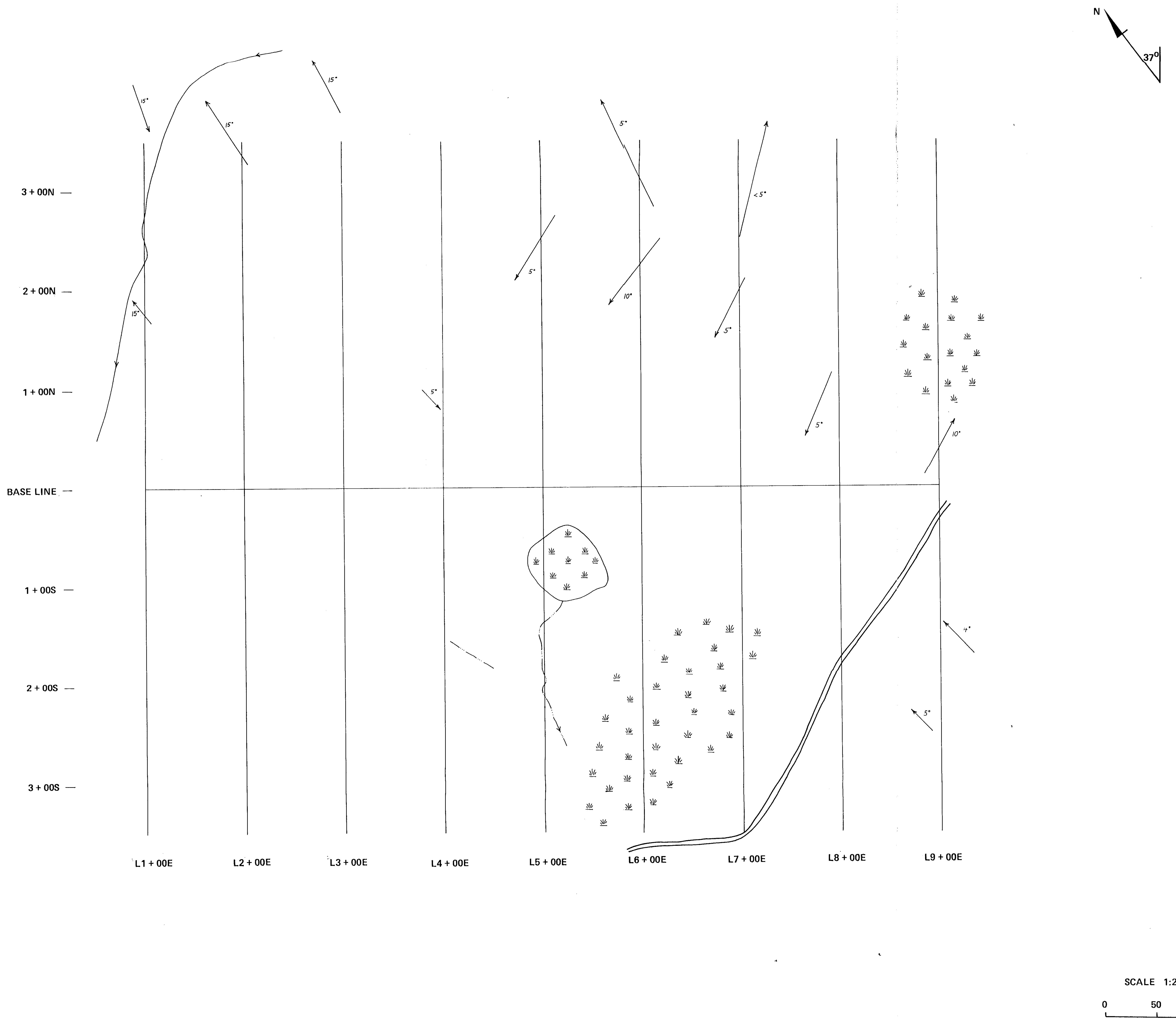
SHELL CANADA RESOURCES LIMITED
MINERALS DEPARTMENT

PRINCE GEORGE PROJECT – B.C.
3891D

PRINCE GEORGE
MAP SHEET A
PREVIOUS WORK
AND
CURRENT CLAIM OWNERSHIP

AUTHOR: W.A. MACLEOD	SCALE: 1:100 000	DRAWING No.: VG 39
DATE: NOV.'77	REVISED:	ENCLOSURE No.: FIG. 1
To Accompany		

MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
7388



☐	Vr	Rhyolite	agl	agglomerate
☐	Vrd	Rhyodacite	t	tuff
☐	Vd	Dacite	bx	breccia
☐	Va	Andesite	p	pillows
☐	Vb	Basalt	Serp	Serpentinized
☐	Vtr	Trachyte		

☐	Sa	Argillite
☐	Sca	Cherty Argillite
☐	Sga	Graphitic Argillite
☐	Sark	Arkose
☐	Sgwk	Greywacke
☐	Slst	Limestone
☐	Sc	Chert
☐	Scgl	Conglomerate
☐	Sss	Sandstone

☐	Igr	Granite
☐	Igd	Granodiorite
☐	Idi	Diorite
☐	Isy	Syenite
☐	Imz	Monzonite
☐	Igb	Gabbro
☐	Iub	Ultrabasic
☐	Ifd	Felsic dyke

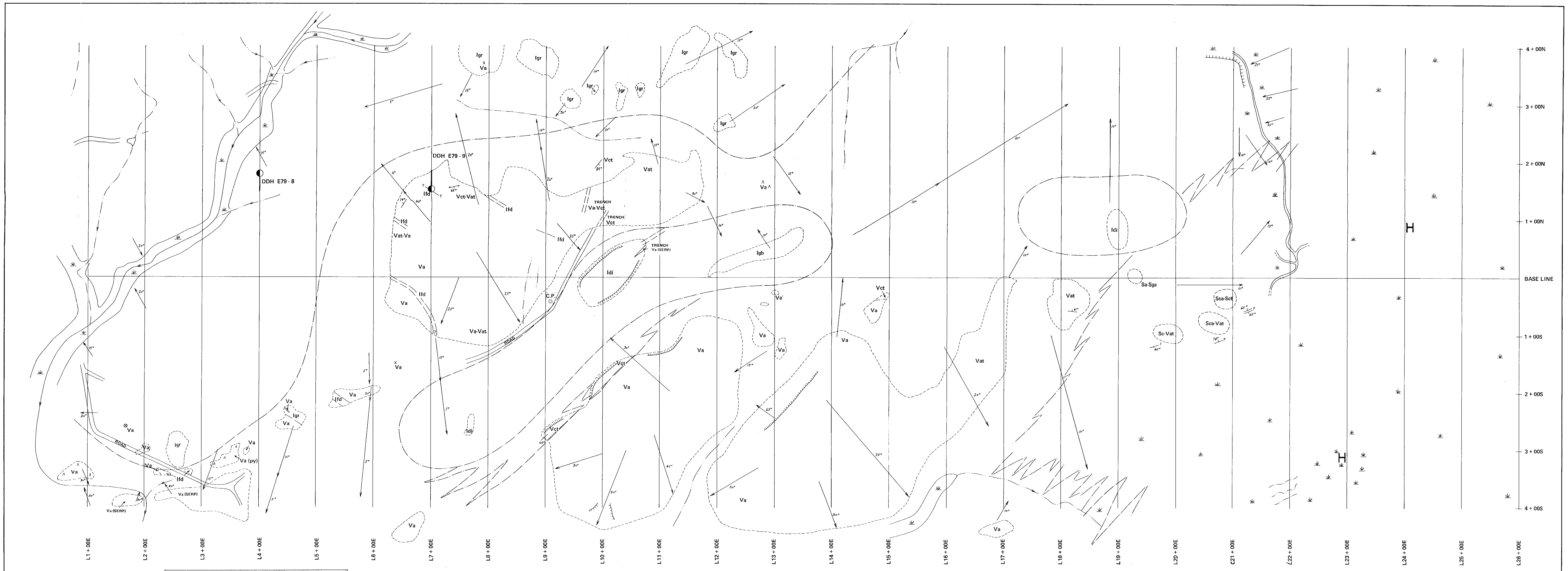
☐	Mgrgn	Granitoid Gneiss
☐	Ms	Schist
☐	Mgms	Quartz-mica Schist
☐	Mcss	Chlorite-Sericite Schist
☐	Mbs	Biotite Schist
☐	Mgs	Garentiferous Schist
☐	Mhbds	Hornblende Schist
☐	Mq	Quartzite
☐	Msd	Meta-Sediment
☐	Msgn	Meta-Sediment - Gneiss

	AREA OF OUTCROP
× , ∧ , ⊗	SINGLE OUTCROP, POSSIBLE OUTCROP, BOULDERS
30°	STRIKE AND DIP
30°	SCHISTOSITY
〰	POSSIBLE FAULT
— · — · —	GEOLOGICAL CONTACT (PROBABLE)
↔	TREND OF GLACIAL STRIA
↔	FOLIATION
	LARGE CREEK WITH FLOW DIRECTION
	STREAM WITH FLOW DIRECTION
	INTERMITTENT STREAM WITH FLOW DIRECTION
	ESCARPMENT, CUT BANK, STEEP SLOPE
→ 20°	DOWNSLOPE DIRECTION WITH ESTIMATED MAGNITUDE
	SWAMP
	TILL, SAND, GRAVEL
	EDGE OF LOGGING CUT WITH DIRECTION TOWARD CUT AREA
ROAD	ROAD
	ACTUAL LOCATION OF CUT LINE WHERE DEVIATION IS NOTED
— — —	CUT LINES PLANNED BUT NOT COMPLETED
☐ C.P.	CLAIM POST
☐ L.C.P.	LEGAL CLAIM POST
H	HELICOPTER LANDING SITE

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT
GEOLOGICAL BASE MAP
GRID 78 - 9

AUTHOR: C.J. BLOOMER	SCALE: 1:2500	DRAWING No.: VD052-B
DATE: NOV. 78	REVISED:	ENCLOSURE No.: FIGURE-2
To Accompany		

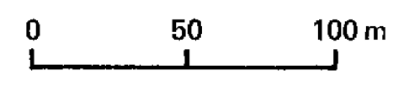


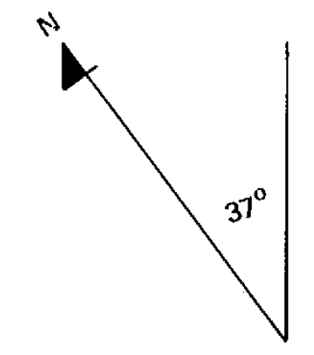
Vr	Rhyolite		agl	agglomerate
Vrd	Rhyodacite		t	tuff
Vd	Dacite		bx	breccia
Va	Andesite		p	pillows
Vb	Basalt		Serp	Serpentinized
Vtr	Trachyte			
Sa	Argillite			
Sca	Cherty Argillite			
Sga	Graphitic Argillite			
Sark	Arkose			
Sgwk	Greywacke			
Slst	Limestone			
Sc	Chert			
Scgl	Conglomerate			
Sss	Sandstone			
Igr	Granite			
Igd	Granodiorite			
Idi	Diorite			
Isy	Syenite			
Imz	Monzonite			
Igb	Gabbro			
Iub	Ultrabasic			
Ifd	Felsic dyke			
Mgrgn	Granitoid Gneiss			
Ms	Schist			
Mgms	Quartz-mica Schist			
Mcss	Chlorite-Sericite Schist			
Mbs	Biotite Schist			
Mgs	Garentiferous Schist			
Mhbds	Hornblende Schist			
Mq	Quartzite			
Msd	Meta-Sediment			
Msgn	Meta-Sediment - Gneiss			

◐ PROPOSED DDH

AREA OF OUTCROP
×, ∧, ⊗ SINGLE OUTCROP, POSSIBLE OUTCROP, BOULDERS
30° STRIKE AND DIP
30° SCHISTOSITY
POSSIBLE FAULT
GEOLOGICAL CONTACT (PROBABLE)
TREND OF GLACIAL STRIA
FOLIATION
LARGE CREEK WITH FLOW DIRECTION
STREAM WITH FLOW DIRECTION
INTERMITTENT STREAM WITH FLOW DIRECTION
ESCARPMENT, CUT BANK, STEEP SLOPE
20° DOWNSLOPE DIRECTION WITH ESTIMATED MAGNITUDE
SWAMP
TILL, SAND, GRAVEL
EDGE OF LOGGING CUT WITH DIRECTION TOWARD CUT AREA
ROAD ROAD
ACTUAL LOCATION OF CUT LINE WHERE DEVIATION IS NOTED
CUT LINES PLANNED BUT NOT COMPLETED
☐ C.P. CLAIM POST
☐ L.C.P. LEGAL CLAIM POST
H HELICOPTER LANDING SITE

SCALE 1:2500





S H E L L C A N A D A R E S O U R C E S L I M I T E D
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT
GEOLOGICAL BASE MAP
GRID 78-10

AUTHOR: C.J. BLOOMER	SCALE: 1:2500	DRAWING No.: VD052-C
DATE: NOV 78	REVISED:	ENCLOSURE No.: FIGURE 3
To Accompany		

N

31°

◐ PROPOSED DDH

☐	Vr	Rhyolite		
☐	Vrd	Rhyodacite	agl	agglomerate
☐	Vd	Dacite	t	tuff
☐	Va	Andesite	bx	breccia
☐	Vb	Basalt	p	pillows
☐	Vtr	Trachyte	Serp	Serpentinized
☐	Sa	Argillite		
☐	Sca	Cherty Argillite		
☐	Sga	Graphitic Argillite		
☐	Sark	Arkose		
☐	Sgwk	Greywacke		
☐	Slst	Limestone		
☐	Sc	Chert		
☐	Scgl	Conglomerate		
☐	Sss	Sandstone		
☐	Igr	Granite		
☐	Igd	Granodiorite		
☐	Idi	Diorite		
☐	Isy	Syenite		
☐	Imz	Monzonite		
☐	Igb	Gabbro		
☐	Iub	Ultrabasic		
☐	Ifd	Felsic dyke		
☐	Mgrgn	Granitoid Gneiss		
☐	Ms	Schist		
☐	Mgms	Quartz-mica Schist		
☐	Mcss	Chlorite-Sericite Schist		
☐	Mbs	Biotite Schist		
☐	Mgs	Garentiferous Schist		
☐	Mhbds	Hornblende Schist		
☐	Mq	Quartzite		
☐	Msd	Meta-Sediment		
☐	Msgn	Meta-Sediment - Gneiss		

AREA OF OUTCROP
×, ∧, ⊗ SINGLE OUTCROP, POSSIBLE OUTCROP, BOULDERS
30° STRIKE AND DIP
30° SCHISTOSITY
POSSIBLE FAULT
GEOLOGICAL CONTACT (PROBABLE)
TREND OF GLACIAL STRIA
FOLIATION
LARGE CREEK WITH FLOW DIRECTION
STREAM WITH FLOW DIRECTION
INTERMITTENT STREAM WITH FLOW DIRECTION
ESCARPMENT, CUT BANK, STEEP SLOPE
20° DOWNSLOPE DIRECTION WITH ESTIMATED MAGNITUDE
SWAMP
TILL, SAND, GRAVEL
EDGE OF LOGGING CUT WITH DIRECTION TOWARD CUT AREA
ROAD ROAD
ACTUAL LOCATION OF CUT LINE WHERE DEVIATION IS NOTED
CUT LINES PLANNED BUT NOT COMPLETED
☐ C.P. CLAIM POST
☐ L.C.P. LEGAL CLAIM POST
H HELICOPTER LANDING SITE

SCALE 1:2500

0 50 100 m

MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
NO. 7388

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT – B.C.
GEOLOGICAL BASE MAP
GRID 78-11

AUTHOR: C. BLOOMER	SCALE: 1:2500	DRAWING No.: VD052-D	
DATE: NOV. 78	REVISED:	ENCLOSURE No.: FIGURE-4	
To Accompany			

CONTOUR OF ZINC CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1

7388

Zinc

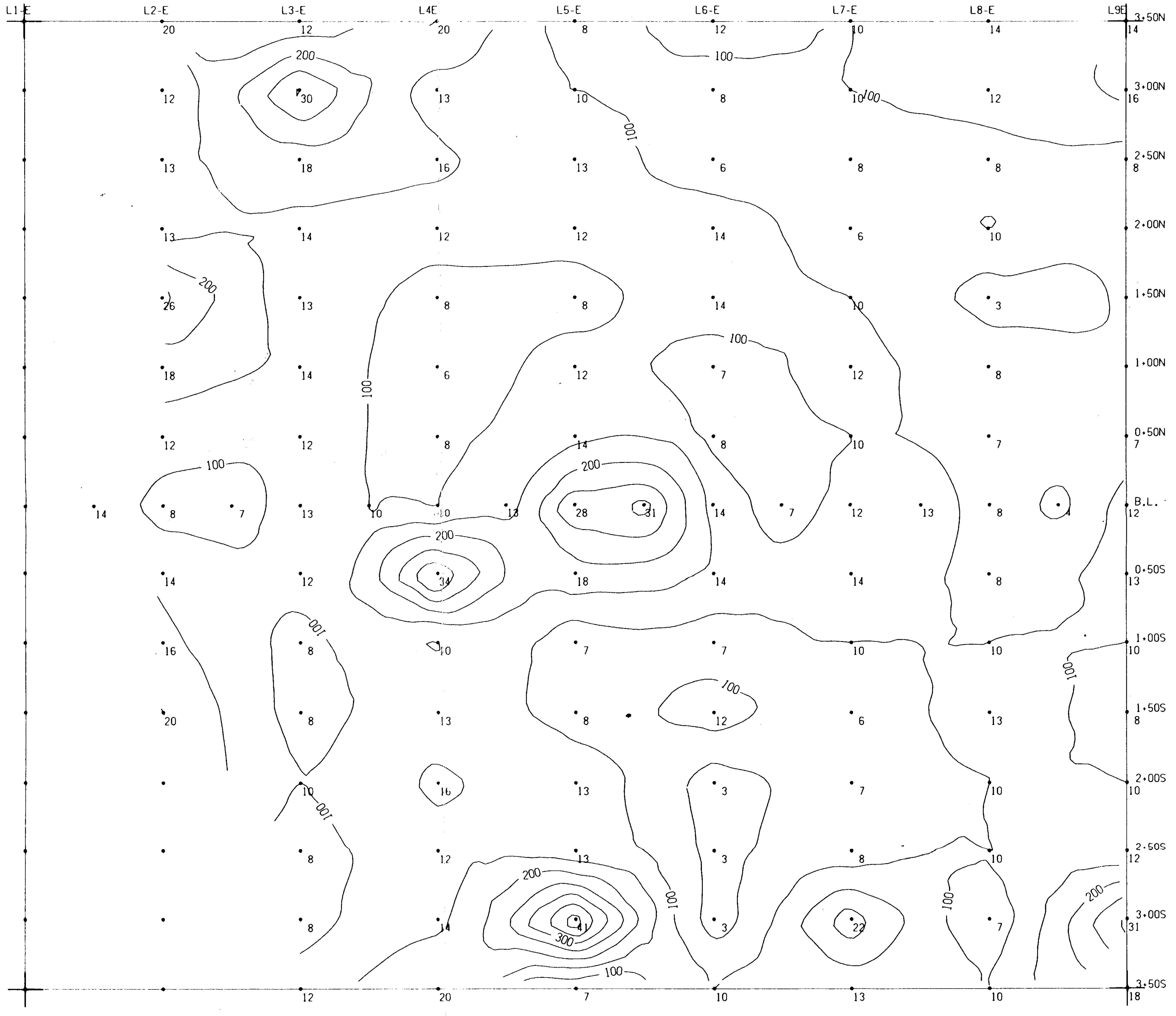
Background	150 ppm
3rd order	150 ppm - 300 ppm
2nd order	300 ppm - 500 ppm
1st order	+500 ppm

ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

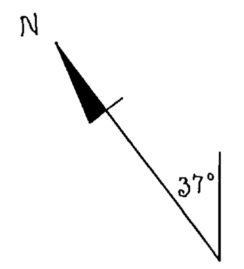
SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78-11
CONTOUR OF B-1 SOIL GEOCHEMISTRY
ZINC

AUTHOR: C.J. BLOOMER	SCALE: 1:2500	DRAWING No.: VJ51-D
DATE: JAN. 79	REVISED:	ENCLOSURE No.:
To Accompany		



CONTOUR OF COPPER CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1



Copper

Background	35 ppm
3rd order	35 ppm - 55 ppm
2nd order	55 ppm - 75 ppm
1st order	+75 ppm

ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78 - 9
CONTOUR OF B-1 SOIL GEOCHEMISTRY
COPPER

AUTHOR: C.J. BLOOMER
SCALE: 1:2500
DRAWING No.: VI 51-E
DATE: JAN. 79
REVISED:
ENCLOSURE No.: FIGURE 5
To Accompany

CONTOUR OF COPPER CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1

7388

	Copper
Background	35 ppm
3rd order	35 ppm - 55 ppm
2nd order	55 ppm - 75 ppm
1st order	+75 ppm

ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78 - 10
CONTOUR OF B-1 SOIL GEOCHEMISTRY
COPPER

AUTHOR: C.J. BLOOMER
SCALE: 1:2500
DRAWING No.: VJ 51-B
DATE: JAN. 79
REVISED:
ENCLOSURE No.: FIGURE 6
To Accompany

CONTOUR OF COPPER CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1

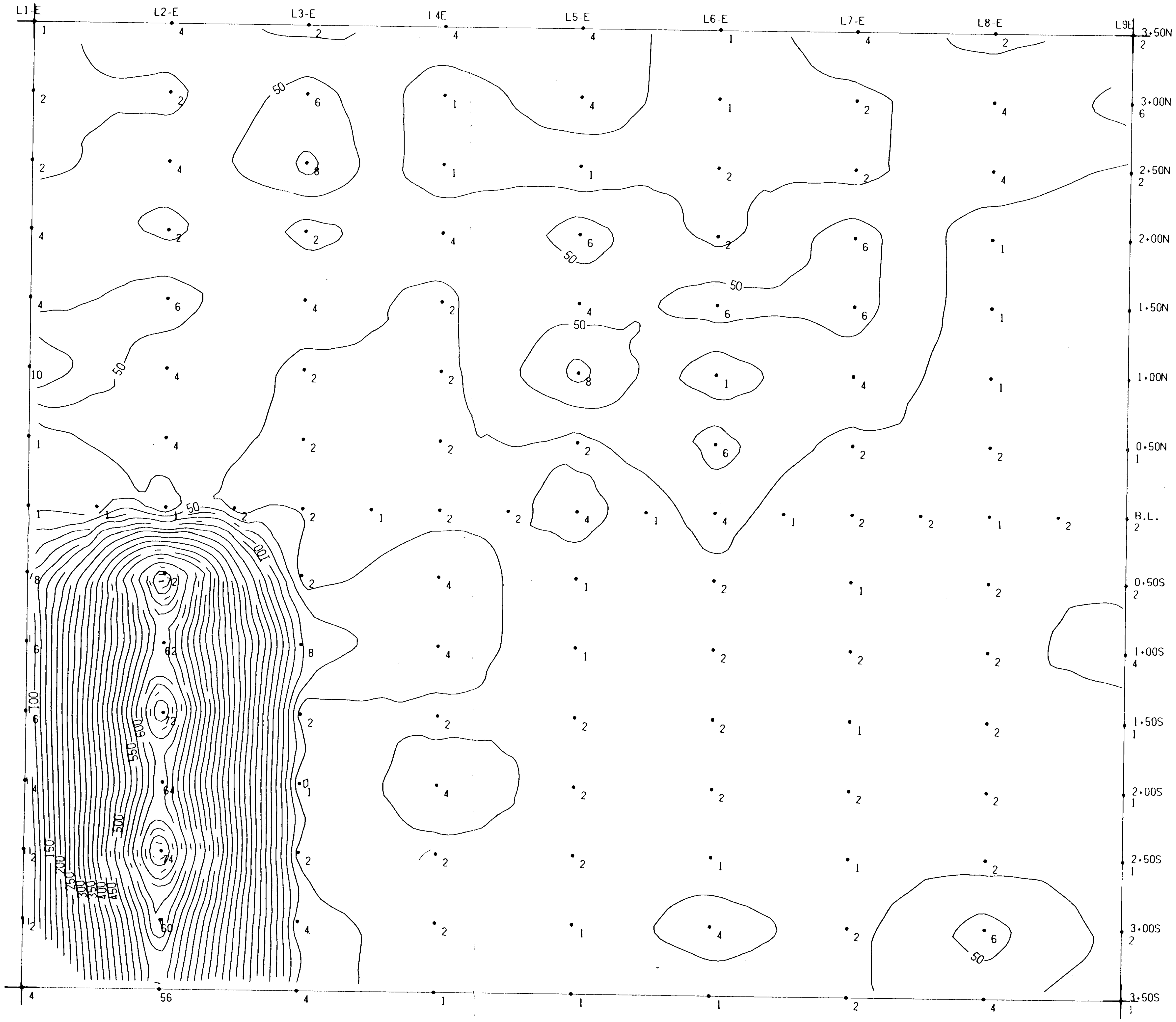
	Copper
Background	35 ppm
3rd order	35 ppm - 55 ppm
2nd order	55 ppm - 75 ppm
1st order	+75 ppm

ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

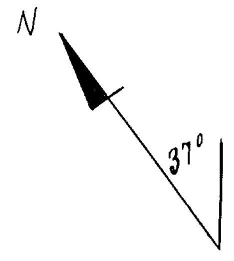
SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78-11
CONTOUR OF B-1 SOIL GEOCHEMISTRY
COPPER

AUTHOR: C.J. BLOOMER
SCALE: 1:2500
DRAWING No.: VJ 51-E
DATE: JAN. 79
REVISED:
ENCLOSURE No.: FIGURE 9
To Accompany



CONTOUR OF LEAD CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1



Lead

Background	20 ppm
3rd order	20 ppm - 35 ppm
2nd order	35 ppm - 45 ppm
1st order	+45 ppm

ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78 - 9
CONTOUR OF B-1 SOIL GEOCHEMISTRY
LEAD

AUTHOR: C.J. BLOOMER	SCALE: 1:2500	DRAWING No.: V151-C	
DATE: JAN. 79	REVISED:	ENCLOSURE No.: FIGURE 8	
To Accompany			

MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
7388
NO.

CONTOUR OF LEAD CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1

Lead

Background	20 ppm
3rd order	20 ppm - 35 ppm
2nd order	35 ppm - 45 ppm
1st order	+45 ppm

ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78 - 10
CONTOUR OF B-1 SOIL GEOCHEMISTRY
LEAD

AUTHOR: C.J. BLOOMER | SCALE: 1:2500 | DRAWING No.: VJ 51
DATE: JAN. 79 | REVISED: | ENCLOSURE No.: FIGURE 9
To Accompany

MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
7388
NO.

CONTOUR OF LEAD CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1

Lead

Background	20 ppm
3rd order	20 ppm - 35 ppm
2nd order	35 ppm - 45 ppm
1st order	+45 ppm

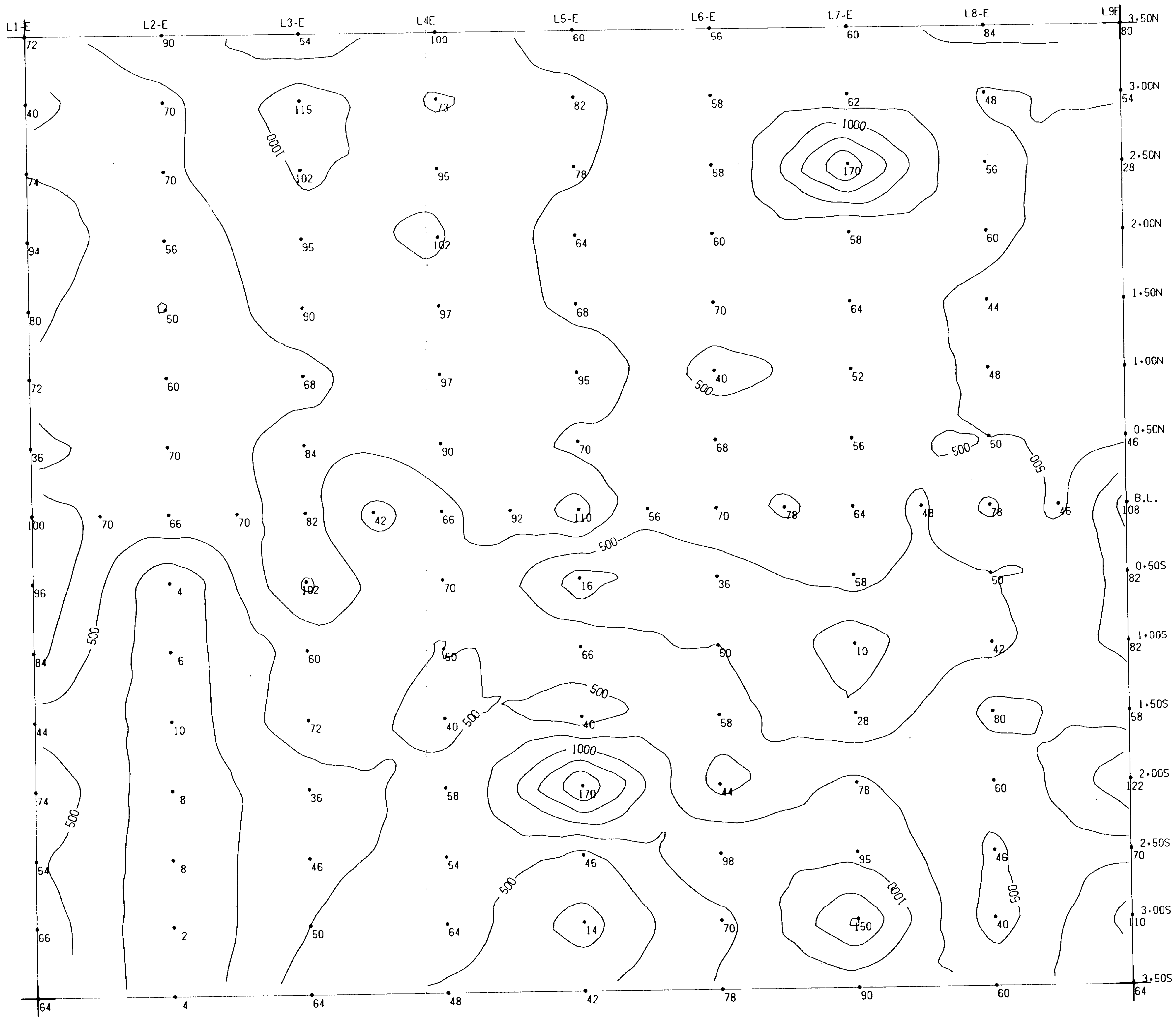
ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

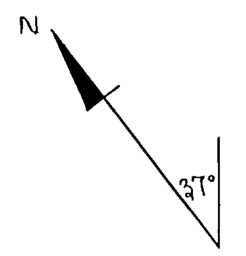
PRINCE GEORGE PROJECT, B.C.
GRID 78 - 11
CONTOUR OF B-1 SOIL GEOCHEMISTRY
LEAD

AUTHOR: C.J. BLOOMER
SCALE: 1:2500
DRAWING No.: VJ 51-C
DATE: JAN. 79
REVISED:
ENCLOSURE No.: FIGURE 10
To Accompany

MINERAL RESOURCES
ASSESSMENT REPORT
NO. 7388



CONTOUR OF ZINC CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1



Zinc

Background	150 ppm
3rd order	150 ppm - 300 ppm
2nd order	300 ppm - 500 ppm
1st order	+500 ppm

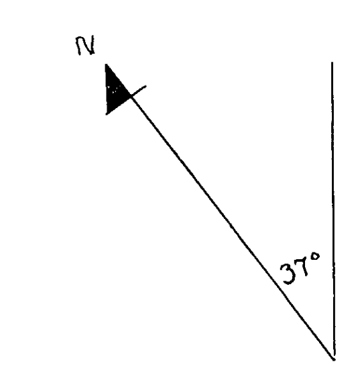
ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78 - 9
CONTOUR OF B-1 SOIL GEOCHEMISTRY
ZINC

AUTHOR: C.J. BLOOMER
SCALE: 1:2500
DRAWING No.: VI 51-D
DATE: JAN. 79
REVISED:
ENCLOSURE No.: FIGURE 11
To Accompany

CONTOUR OF ZINC CONCENTRATION . SCALE : 1 : 2500 . VALUES X .1



Zinc

Background	150 ppm
3rd order	150 ppm - 300 ppm
2nd order	300 ppm - 500 ppm
1st order	+500 ppm

ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78 - 10
CONTOUR OF B-1 SOIL GEOCHEMISTRY
ZINC

AUTHOR: C.J. BLOOMER
SCALE: 1:2500
DRAWING No.: VJ 51-A
DATE: JAN. 79
REVISED:
ENCLOSURE No.: FIGURE 12
To Accompany

MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
7388
NO.

CONTOUR OF ZINC CONCENTRATION . SCALE = 1 : 2500 . VALUES X .1

Zinc

Background	150 ppm
3rd order	150 ppm - 300 ppm
2nd order	300 ppm - 500 ppm
1st order	+500 ppm

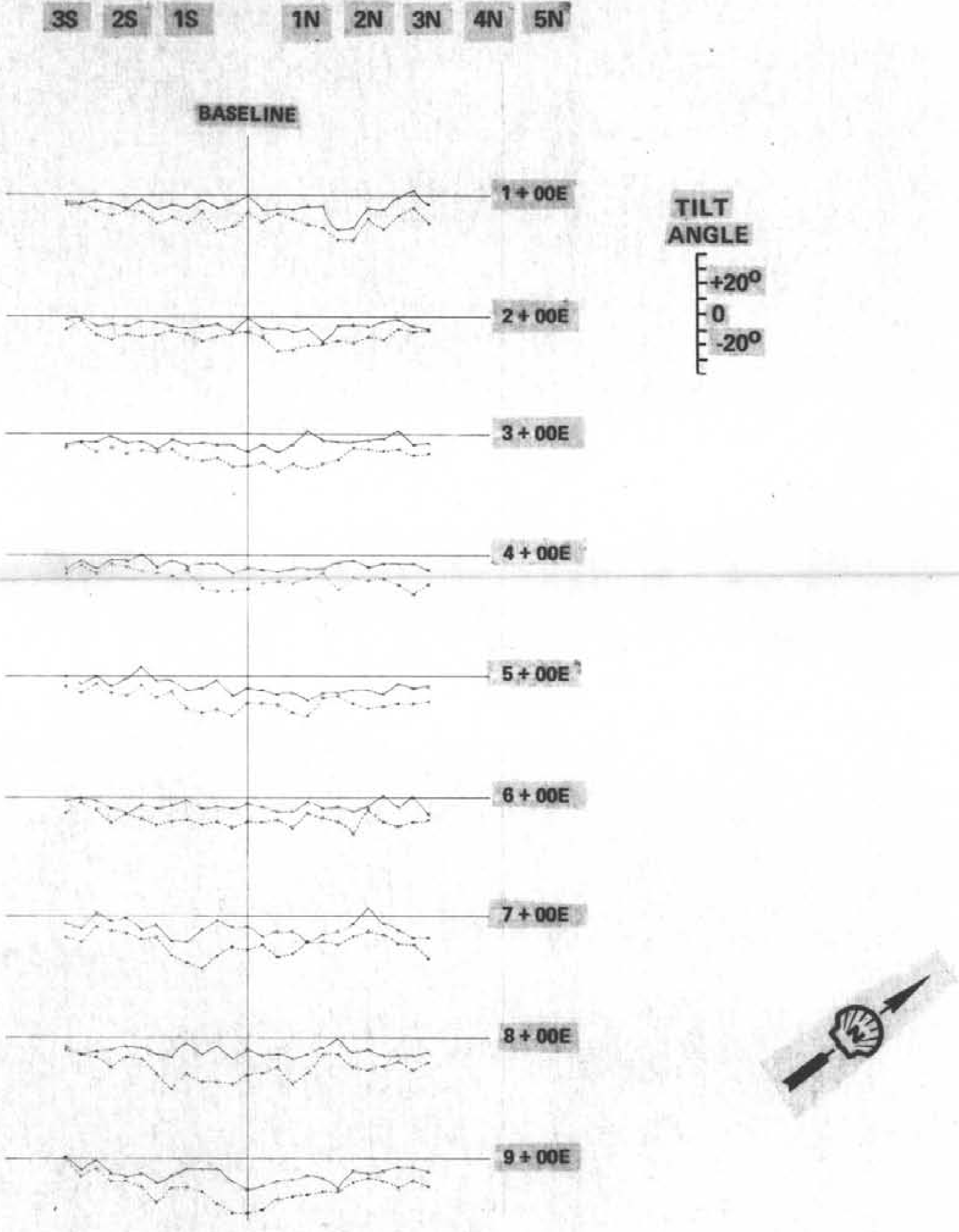
ACTUAL CONTOUR INTERVALS ARE
0.1 x THE VALUE SHOWN.
STATION VALUES ARE IN PARTS PER MILLION

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT, B.C.
GRID 78-11
CONTOUR OF B-1 SOIL GEOCHEMISTRY
ZINC

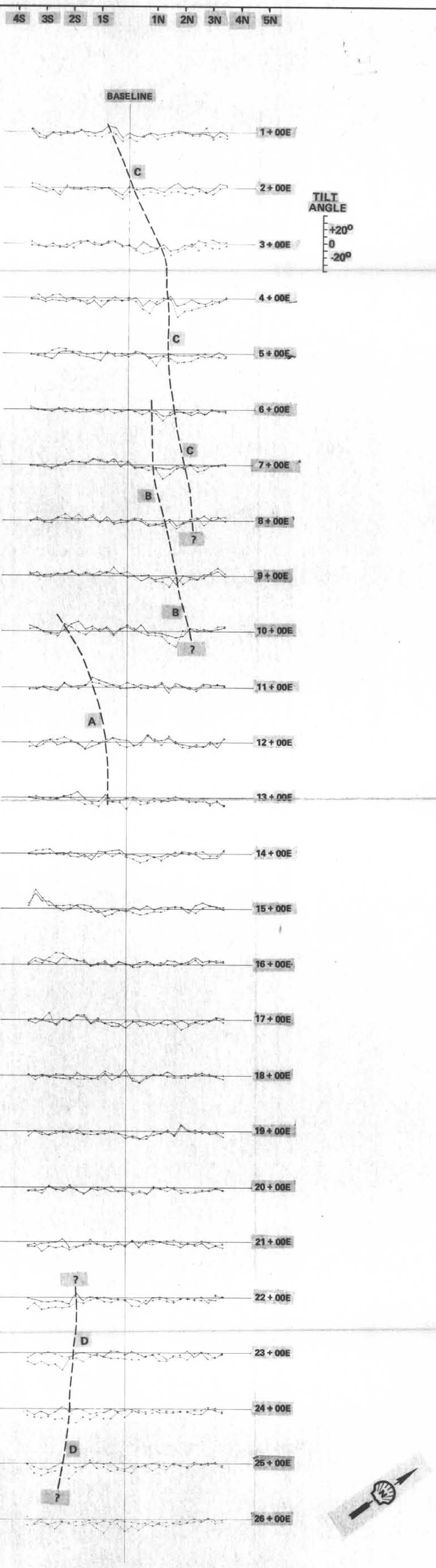
AUTHOR: C.J. BLOOMER
SCALE: 1:2500
DRAWING No.: VJ51-D
DATE: JAN. 79
REVISED:
ENCLOSURE No.: FIGURE 13
To Accompany

7388



PRINCE GEORGE PROJECT
GRID 78 - 9
SHOOTBACK EM RESULTANT
TILT ANGLE PROFILES
SCALE ALONG B.L. = 1:5000
SCALE ALONG LINES = 1:10 000

FIGURE 14
VG 40-G



×——× 390 Hz
•------• 1830 Hz
A AXIS OF SHOOTBACK EM CONDUCTOR

MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
NO. 7388

PRINCE GEORGE PROJECT
GRID 78 -10
SHOOTBACK EM RESULTANT
TILT ANGLE PROFILES
SCALE ALONG B.L. = 1:5000
SCALE ALONG LINES = 1:10 000

FIGURE 15

VG 40-H

x——x 390 Hz

o- - -o 1830 Hz

A — AXIS OF SHOOTBACK EM CONDUCTOR

EXTENT OF CONDUCTIVE ZONE

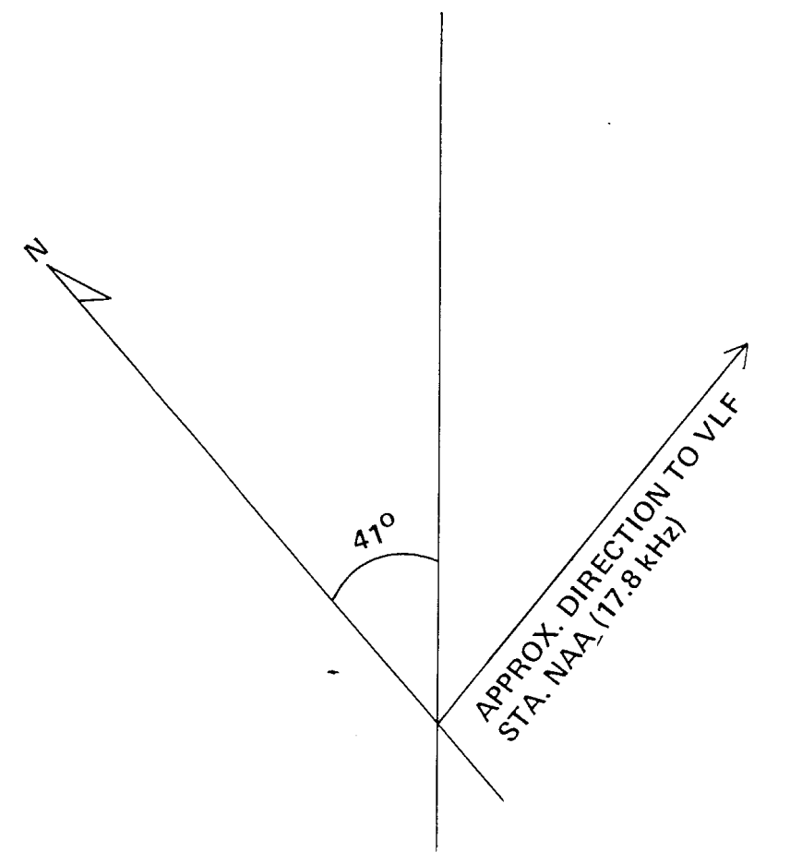
MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
NO. 7388

PRINCE GEORGE PROJECT
GRID 78 -11
SHOOTBACK EM RESULTANT
TILT ANGLE PROFILES
SCALE ALONG B.L. = 1:5000
SCALE ALONG LINES = 1:10 000

FIGURE 16

4640-I

GRID 78-11 VLF CONTOUR MAP SCALE 1/2500 NO UNIT



LEGEND

A	AXIS OF SHOOTBACK EM CONDUCTOR
∿ ∿ ∿ ∿	INFERRED FAULT
▲	Pb, Zn MINERALIZATION (Allen, 1973)

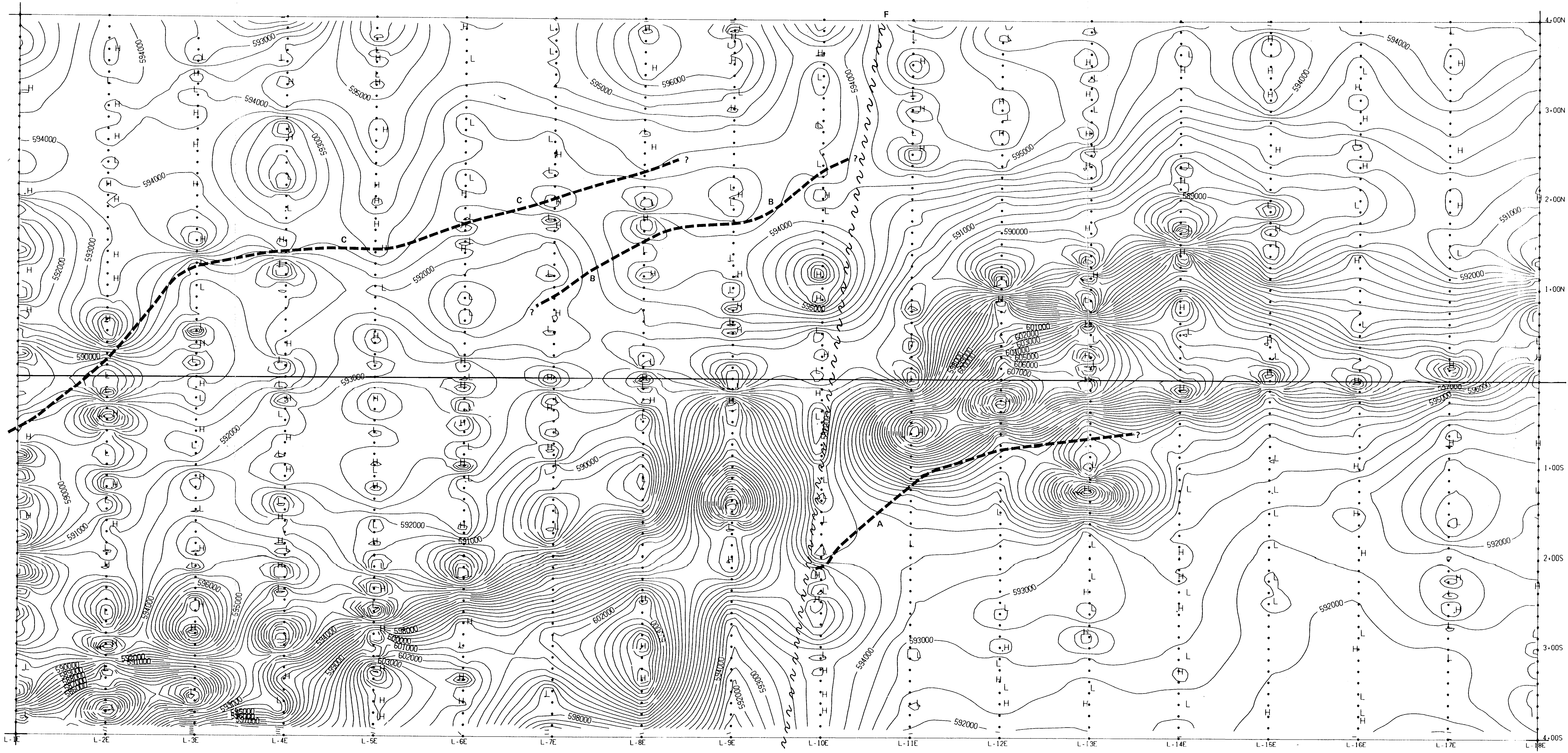
SCALE 1:2500

0 50 100 150 m

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT
GRID 78-11
VLF-EM
CONTOUR MAP OF FRAZER
FILTERED TILT ANGLE VALUES
CONTOUR VALUES: ACTUAL VALUES x 100

AUTHOR: A.S. SAYDAM
SCALE: 1:2500
DRAWING No.: V651-E
DATE: DEC. 1978
REVISED:
ENCLOSURE No.: FIGURE 17
To Accompany



GRID 78-10 MAG CONTOUR MAP. SCALE 1/2500 . CONT.LEVEL•10(-1) GAMMAS

LEGEND

A ▬ ▬ ▬	AXIS OF SHOOTBACK EM CONDUCTOR
∿ ∿ ∿ ∿	INFERRED FAULT

SCALE 1:2500

0 50 100 150 m

S H E L L   C A N A D A   R E S O U R C E S   L I M I T E D

EXPLORATION – MINERALS

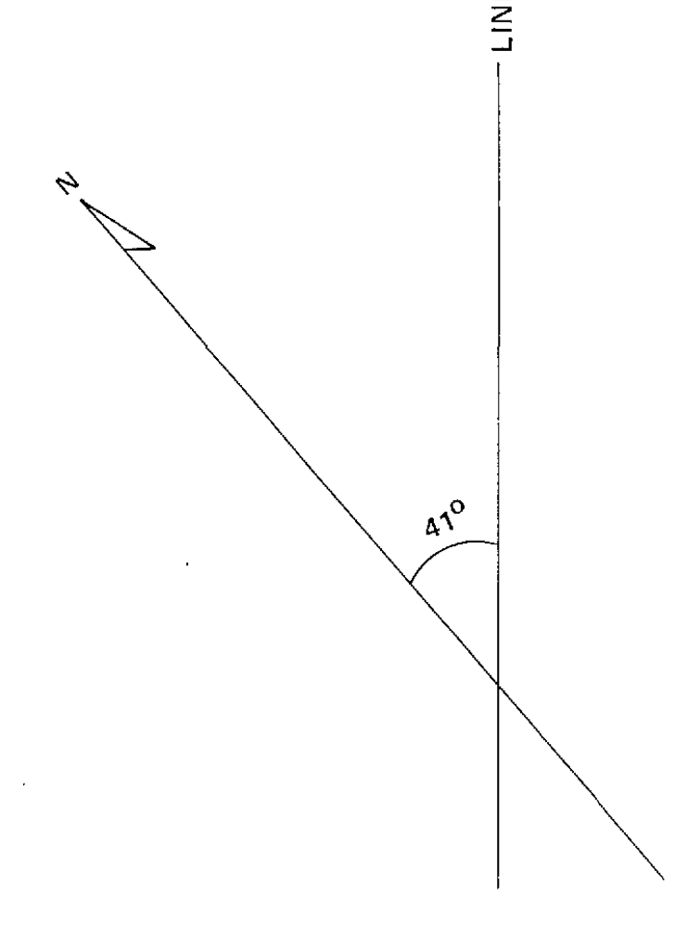
PRINCE GEORGE PROJECT
GRID 78-10
CONTOUR MAP OF TOTAL MAGNETIC FIELD
CONTOUR INTERVAL: 50 GAMMAS
ACTUAL VALUES: 10^{-1} OF CONTOUR VALUES

AUTHOR: A.S. SAYDAM	SCALE: 1:2500	DRAWING No.: V451-D
DATE: DEC. 1978	REVISED:	ENCLOSURE No.: FIGURE 18

To Accompany

MINERAL RESOURCES BRANCH
ASSESSMENT REPORT
NO. 7388

GRID 78-11 MAG CONTOUR MAP SCALE 1/2500 IN GAMMAS



LEGEND

A — — —	AXIS OF SHOOTBACK EM CONDUCTOR
∿ ∿ ∿ ∿	INFERRED FAULT
▲	Pb, Zn MINERALIZATION (Allen, 1973)

SCALE 1:2500

0 50 100 150 m

SHELL CANADA RESOURCES LIMITED
EXPLORATION – MINERALS

PRINCE GEORGE PROJECT
GRID 78-11
CONTOUR MAP OF TOTAL MAGNETIC FIELD
CONTOUR INTERVAL: 50 GAMMAS
ACTUAL VALUES: 10^{-1} OF CONTOUR VALUES

AUTHOR: A.S. SAYDAM	SCALE: 1:2500	DRAWING No.: V651-F
DATE: DEC. 1978	REVISED:	ENCLOSURE No.: FIGURE 19
To Accompany		