### ANDREW BAY PROJECT

### Geochemical Report

on the

RIP 1,8; RIP 2,3,4; and RIP 5,6,7 Mineral Groups

OMINECA MINING DIVISION

NTS: 93E/15

LAT. 53° 50'N; LONG. 126° 44'W

Owner: KENNCO EXPLORATIONS, (WESTERN) LTD. Operator: SMD MINING COMPANY LTD. Consultant: R.W. BAMFORD

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By: R.W. Bamford R. Cann

May 1981





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#### INTRODUCTION

#### Location and Access

The RIP 1 to 8 mineral claims (Figures 1 and 2) are located 112 kilometres south-southeast of Smithers, in west-central B.C. (NTS: 93E/15). Access to the property is via logging roads from Houston or Burns Lake to Francois Lake and then to Ootsa Lake. Closest community is Wistaria, approximately 35 kilometres by road east of the property. A logging camp is situated at Andrew Bay, 10 kilometres east of the claims.

Physiographically, the property is situated on the west side of the Nechako Plateau in an area of rolling to hilly topography. Maximum elevation is 1235 m and maximum relief 300 metres.

The area is being actively logged at present. Vegetation consists primarily of pine, balsam and spruce.

#### Claim Definition

The RIP 1 and 2 claims were originally staked by Kennco Explorations (Western) Ltd. in 1975 to cover an I.P. anomaly discovered during a reconnaissance survey. In 1979, SMD Mining Company Ltd. entered into an option agreement with Kennco Explorations (Western) Ltd. That same year 6 new claims were added to the original 2, to total 8 claims as defined below. SMD Mining Company Ltd. is the current operator and Kennco Explorations (Western) Ltd. is the owner.

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| Claim | Units | Tag. No. | Record No. | Record Date       |
|-------|-------|----------|------------|-------------------|
| RIP 1 | 18    | 02517    | 110        | August 25, 1975   |
| RIP 2 | 18    | 02518    | 81         | August 25, 1975   |
| RIP 3 | 16    | 49603    | 2422       | November 29, 1979 |
| RIP 4 | 4     | 49604    | 2423       | November 29, 1979 |
| RIP 5 | 16    | 49605    | 2424       | November 29, 1979 |
| RIP 6 | 18    | 47726    | 2447       | November 29, 1979 |
| RIP 7 | 6     | 47727    | 2425       | November 29, 1979 |
| RIP 8 | 18    | 49608    | 2426       | November 29, 1979 |

# Summary of Work

Samples from 26 percussion drill holes located on the RIP 1, 2, 3 and 8 claims were analyzed for 15 elements to determine zoning patterns and possible drill targets.

All data processing, compilation and interpretation was by consultant R.W. Bamford, of Salt Lake City, Utah.

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#### ROCK GEOCHEMISTRY

This survey provides an independent determination of Mo-Cu resource targets within the claimed area. Samples for the survey are derived entirely from percussion hole drilling, since most of the claim block is blanketed by glacial till.

#### Survey Method

Geochemical zoning and gradients are determined by separation and analysis of a nonmagnetic +3.3 specific gravity (sp. gr.) fraction from composite rock samples. Interpretation of the geochemical results is based primarily on empirical multielement geochemical zoning models provided by proprietary studies of known porphyry copper and porphyry molybdenum deposits and their surroundings. The models incorporate an extensive and probably unique data base. They reflect consistent three-dimensional zoning relationships indicated by +3.3 sp. gr. and, in many cases, corresponding whole rock geochemical data for a variety of deposit types and environments.

The +3.3 sp. gr. fraction analyzed in this work provides large (threeto more than ten-fold) enhancements of hydrothermal trace element signatures relative to those of original rock. Heavy liquid separation procedures selectively concentrate hydrothermal sulfides and oxides (or their oxidation products), the principal hosts for the trace elements, in the +3.3 fraction. The predominant rock and alteration silicates in the orig-

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inal sample, which are relatively barren of hydrothermal trace elements, partition mainly into the light (-3.3 sp. gr.) fraction. General advantages of +3.3 sample geochemistry for exploring large sulfide systems include: (1) more effective detection of interpretable trace element signatures in the outer fringes of sulfide systems, (2) clearer definition of trace element zoning patterns and gradients related to ore, (3) minimization of rock type effects in the geochemical data, (4) elimination of pseudo-zoning indications caused by variations in total sulfide contents, and (5) improved utilization of Bi, Te, As, Sb, Sn, W, and Co data.

#### Sample Preparation and Analytical Procedures

Twenty-six composite chip samples, one from each of twenty-six percussion drill holes, are utilized in this work. Most of the composite samples represent the uppermost 30-meter (maximum) intercept of premineral rock encountered in each drill hole and incorporate several (commonly about 10) individual 3-meter-interval chip samples.

Samples are pulverized to -80 mesh and composited as needed. Eighty grams of each -80 mesh composite sample are used for preparation of a corresponding +3.3 sp. gr. fraction. A magnetic fraction consisting mostly of magnetite is separated from the +3.3 sp. gr. fraction using a hand magnet, leaving a sample ready for analysis. Total weights and percentages in original sample materials are recorded for both sample fractions.

The nonmagnetic +3.3 sp. gr. fractions were analyzed for Cu, Mo, Pb, Zn, Ag, Mn, Co, and Fe by atomic absorption spectrophotometry (AAS); for As and Sb by colorimetry; and for S by Leco induction furnace. This analytical work and the sample preparation were carried out by Rocky Mountain Geochemical Corporation, Salt Lake City, following specified procedures.

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Additional analyses for Bi, Te, Sn, and W were performed by COORS Spectro-Chemical Laboratory, Golden, Colorado, using optical emission spectrographic (OES) techniques. OES analyses were omitted for one drill hole because of insufficient sample. Omissions are indicated on the plots by the letters ND (no data).

#### Data Presentation

The geochemical results are presented in four forms: (1) a tabulation of original geochemical and sample fraction data (Appendix B), (2) tabulations and plots of various statistics for the geochemical data (Appendix A), (3) computer-generated contoured plan plots of the original geochemical and sample fraction data (Figures 1 thru 17), and (4) similar plan plots of geochemical parameters useful for interpretation and target selection in Cu-Mo sulfide systems (Figures 18 thru 20). A drill hole index map (Figure 21) is also included.

Statistics presented include simple statistics, Spearman rank correlation and cluster analysis, and Pearson product-moment correlation and cluster analysis. Correlation and cluster analysis by the Spearman rank method is free of underlying assumptions regarding type of data distribution and can often provide a more accurate indication of element associations than the Pearson product-moment method. Product-moment correlation assumes that data are normally distributed.

Plan plots are produced at two scales: approximately 1:20,000 scale for the bound reports and 1:10,000 scale for direct comparison with full scale geologic and geophysical maps. Minimum contour values on the plots are lowest meaningful values determined by inspection. Each successive contour value is double that of the neighboring smaller value. Circles on

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the plots symbolize percussion drill holes, stars indicate diamond drill holes, and a square indicates the location of a trench.

#### DISCUSSION

### Hydrothermal Element Zoning

A systematic large-scale zoning of hydrothermal elements, somewhat similar to that in the Whiting Creek sulfide system (Bamford, 1981), is defined at Andrew Bay (Figures 1-19 and Appendix A, Figures A-1 and A-2). Principal anomaly associations in the zoning are Cu-Mo-Sn and and Pb-Zn-As-Mn (see especially Appendix A, Table A-2 and Figure A-1). These associations are indicated to comprise relatively distinct element assemblages, actually two series of 2-, 3-, or 4-element assemblages, between which there is low distribution similarity. An Ag-Co-Bi association with distribution characteristics most like those of the Pb-Zn-As-Mn association is also tentatively distinguished.

Distribution maps for the elements show the Cu-Mo-Sn anomaly associations to be centrally zoned element assemblages (Figures 1, 2, 14, 15, and 18) and the Pb-Zn-As-Mn associations peripherally zoned assemblages (Figures 3, 4, 6, 8, and 19). Cu-Mo-Sn anomaly associations predominate in drill holes 12, 16, and 17 (Figures 18 and 21), defining a central zone with approximate dimensions of 600 meters E-W and 300 meters N-S in premineral rock just below the erosion surface. Pb-Zn-As-Mn anomaly associations predominate in most of the drill holes surrounding this central zone partly defining a conventional porphyry system halo zone. The halo zone is at least tentatively defined on all sides of the central zone except the northwest where samples are lacking. Definition is locally only fair to poor on the east and south-southeast of the central zone, due mainly to additional gaps in the sample distribution.

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### Sulfide and Magnetic Mineral Zoning

Concentrations of hydrothermal sulfide and oxide minerals in rock are indicated to be highest within or near the geochemically defined central zone of the system (cf. Figures 16, 17, 11, and 20 with, e.g., Figure 18). Thus no conventional pyrite halo is defined. Local association of high Cu and As concentrations, in drill hole 12 for example (cf. Figures 1, 6, and 21), suggests enargite or other sulfosalts may occur in the central zone.

#### Sulfide System Model Concepts

Two principal system models can be suggested based on the geochemical results. The mineralization sampled is possibly located high in a porphyry sulfide system several hundred to more than a thousand meters above the principal Cu-Mo zone or it may simply represent part of the Cu-Mo zone itself in a small poorly developed porphyry-type system. Both models accommodate several of the principal system characteristics indicated by this work including: the conventional porphyry system zoning with central zone Cu-Mo-Sn anomaly associations surrounded by halo zone Zn-Pb-As-Mn anomaly associations (e.g., Figures 18 and 19), the maximum hydrothermal sulfide and oxide enrichment within or near the central zone rather than the halo zone (Figures 16 and 17), and, possibly, an important component of structural control of the mineralization (suggested by the north-northwesterly trend of Cu-Mo-Sn anomaly associations--Figure 18).

Geochemical characteristics which tend to support interpretation of the Andrew Bay mineralization as the top of a porphyry copper system include: unusually high As concentrations in most samples; local Cu-As associations which possibly indicate the occurrence of enargite or other sulfosalts (e.g., in drill hole 12; cf. Figures 1, 6, and 21); and unusually low W and

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Sn components in the Cu-Mo-Sn anomaly associations (cf. Figures 14 and 15 with Bamford, 1981, Figures 14 and 15). This geochemistry is not entirely unique to high level porphyry environments, but is less typical of deeper levels in porphyry system. Thus the alternate interpretion, that the drilled mineralization represents the main part of a small, poorly devel-oped porphyry-type system, is possibly less tenable. Limited mineralogic study to determine the nature of hydrothermal silicate and sulfide assemblages within the central zone could be helpful in further establishing the relative merits of the two models.

The results do not provide indications that the mineralization could be of a non-porphyry variety, although this possibility is not eliminated. The system could, however, be Au-bearing and it is recommended that a few of the more Cu-As-rich samples be analyzed for this element if not already done.

### Possible Ore Target

Only one potentially economic porphyry-type ore target is presently inferred from these results: higher grade porphyry Cu-Mo mineralization could be developed at depths of several hundred to more than a thousand meters beneath the sampled area. The probability of finding a large, highgrade orebody, especially at the shallower depths, is considered to be low due to the apparently limited size and relatively weak expression of the overall sulfide system.

Should drilling be carried out to test this target concept, design of the driling could be effectively based on the geochemical zoning plus structural information. Based on the zoning results alone, the drill test would probably best be sited within the central Cu-Mo-Sn zone and consist

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of a vertical hole with a maximum depth of 1000 meters. If reliable structural information is available and indicates either post-mineral tilting of the mineralized block or localization of the central-zone mineralization by non-vertical structures, then drilling should be offset to partially compensate for anticipated displacement of the target at depth. Geochemical logging of composite samples from a deep drill test of this type provides an effective means of evaluating and expanding or refining the target model and should be considered if drilling is undertaken.

### Recommended Follow-up Work

Near term discussions of the survey results are recommended to aid their integration with other data and to facilitate planning subsequent exploration activities. Also, limited XRD and/or polished section determinations of hydrothermal silicate and sulfide assemblages within the central zone would probably help better establish the relative merits of the two system models presented in this report. A deep drill test (above) is tentatively recommended contingent on the outcome of the survey results discussions, the mineralogic determinations, and an evaluation of target economic potential. A few Cu-As-rich samples should be analyzed for Au (if not already done), to test for possible economic concentrations of that element in the system.

# REFERENCES

Bamford, R. W., 1981, A multielement geochemical survey, Whiting Creek prospect area, British Columbia: Consulting report completed for Saskatchewan Mining Development Corporation.



































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# APPENDIX A

# Geochemical Data Statistics

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## TABLE A-1. SIMPLE STATISTICS FOR PERCUSSION-HOLE GEOCHEMICAL DATA

# ANDREW BAY PROSPECT BRITISH COLUMBIA

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| Rcd                             | # Description                | # Pts | Minimum    | Maximum    | Mean   | Variance                         | Std. Deviation |
|---------------------------------|------------------------------|-------|------------|------------|--------|----------------------------------|----------------|
| 9                               | COPPER (PPM)                 | 26    | 32.000     | 7200.0     | 1152.4 | .28995+007                       | 1702.8         |
| 10                              | MOLY BDENUM (PPM)            | 26    | 5.0000     | 6100.0     | 348.85 | .14614+007                       | 1208.9         |
| 11                              | LEAD'(PPM)                   | 26    | 40.000     | 3500.0     | 457.12 | <b>.</b> 78855 <del>,</del> +006 | 888.00         |
| 12                              | ZINC (PPM)                   | 26    | 145.00     | 19400.     | 3930.4 | •23397+008                       | 4837.0         |
| 13                              | SILVER (PPM)                 | 26    | 1.0000     | 21.000     | 7.7308 | 31.565                           | 5.6182         |
| 14                              | ARSENIC (PPM)                | 26    | 25.000     | 2700.0     | 650.38 | .57982+006                       | 761.46         |
| <sup>-3</sup> / <sub>4</sub> 15 | ANTIMONY (PPM)               | 26    | 1.0000     | 12.000     | 2.3077 | 7.8215                           | 2.7967         |
| 16                              | MANGANESE (PPM)              | 26    | 52.000     | .10400+006 | 5387.9 | •40556+009                       | 20139.         |
| 17                              | COBALT (PPM)                 | 26    | 25.000     | 630.00     | 270.38 | 34636.                           | 186.11         |
| 18                              | IRON (%)                     | 26    | 16.100     | 70.000     | 43.304 | 271.11                           | 16.465         |
| . 19                            | SULFUR (%)                   | 26    | 2.4000     | 42.000     | 24.496 | 151.12                           | 12.293         |
| 20                              | BISMUTH (PPM)                | 25    | .50000     | 20.000     | 4.3600 | 29.282                           | 5.4113         |
| 21                              | TELLURIUM (PPM) -            | 25    | 5.0000     | 15.000     | 5.8000 | 7.6667                           | 2.7689         |
| 22                              | TIN (PPM)                    | 25    | .50000     | 3.0000     | .76000 | .33583                           | .57951         |
| 23                              | TUNGSTEN (PPM)               | 25    | 5.0000     | 15.000     | 6.0800 | 7.0767                           | 2.6602         |
| 7                               | +3.3 SP. GR. FRACTION (WT.%) | 26    | .60000-001 | 10.500     | 1.3142 | 4.1834                           | 2.0453         |
| 8                               | % MAGNETIC FRACTION          | 26    | .10000-001 | .60000     | .11000 | .21688-001                       | .14727         |

# TABLE A-2. SPEARMAN RANK CORRELATION MATRIX FOR PERCUSSION-HOLE GEOCHEMICAL DATA

ANDREW BAY PROSPECT BRITISE COLUMBIA

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| Element     | Cu                   | Mo                   | Pb                    | 2 B                  | Åg                   | A S                  | 56                   | Mo                  | Co                    | 7e                   | \$                   | Bi                   | Te                   | Sn            | ¥                    | R 7                  | R 8                  |
|-------------|----------------------|----------------------|-----------------------|----------------------|----------------------|----------------------|----------------------|---------------------|-----------------------|----------------------|----------------------|----------------------|----------------------|---------------|----------------------|----------------------|----------------------|
| Cu          | 1.000                | .627                 | .013                  | .102                 | .231                 | .054                 | .170                 | 123                 | .598                  | 011                  | .285                 | .284                 | .123                 | .179          | .107                 | .002                 | .336                 |
|             | ( 0)                 | (26)                 | (26)                  | (26)                 | (26)                 | (26)                 | (26)                 | (26)                | (26)                  | ( 26)                | (26)                 | (25)                 | (25)                 | (25)          | (25)                 | (26)                 | (26)                 |
|             | .000                 | .000                 | .473                  | .312                 | .128                 | .394                 | .295                 | .279                | .001                  | .479                 | .073                 | .083                 | .283                 | .302          | .309                 | .495                 | .945                 |
| Mo          | .627                 | 1.000                | 194                   | 174                  | 199                  | 330                  | 223                  | 270                 | .197                  | .174                 | .292                 | 317                  | 354                  | .315          | .330                 | 110                  | •193                 |
|             | (26)                 | (0)                  | (26)                  | (26)                 | (26)                 | (26)                 | (26)                 | (26)                | (26)                  | (26)                 | (26)                 | (25)                 | (25)                 | (25)          | (25)                 | ( 26)                | (26)                 |
|             | .000                 | .000                 | .328                  | .300                 | .335                 | .048                 | .137                 | .089                | .332                  | .300                 | .872                 | .059                 | .040                 | .061          | .052                 | .299                 | •327                 |
| Pb          | .913                 | 194                  | 1.000                 | .795                 | .569                 | .588                 | .381                 | .466                | .116                  | 676                  | 394                  | .458                 | .041                 | 427           | 050                  | 453                  | 274                  |
|             | (26)                 | (26)                 | ( 0)                  | (26)                 | (26)                 | (26)                 | (26)                 | ( 26 )              | (26)                  | (26)                 | (26)                 | (25)                 | (25)                 | (25)          | (25)                 | ( 26)                | (26)                 |
|             | .473                 | .328                 | .000                  | .860                 | .001                 | .901                 | .026                 | .008                | .290                  | .000                 | .022                 | .010                 | .420                 | .016          | .386                 | .010                 | .087                 |
| 21          | .1#2                 | 174                  | .795                  | 1.000                | .416                 | .589                 | .247                 | .499                | .119                  | 697                  | 314                  | .340                 | 102                  | 209           | 167                  | 437                  | 140                  |
|             | (26)                 | ( 26)                | (26)                  | ( 8)                 | (26)                 | (26)                 | (26)                 | (26)                | (26)                  | (26)                 | ( 26)                | (25)                 | ( 25)                | (25)          | ( 25)                | ( 26)                | (26)                 |
|             | .312                 | .300                 | .000                  | .002                 | .016                 | .001                 | .111                 | .005                | .284                  | .998                 | .057                 | .046                 | .316                 | .159          | .285                 | .012                 | .251                 |
| Ag          | .231                 | 199                  | .569                  | .416                 | 1.800                | .317                 | .440                 | .094                | .548                  | 316                  | .031                 | .652                 | .291                 | 269           | 194                  | 046                  | 224                  |
|             | (26)                 | (26)                 | (26)                  | (26)                 | ( 0)                 | (26)                 | (26)                 | (26)                | (26)                  | (26)                 | ( 26)                | (25)                 | (25)                 | (25)          | (25)                 | ( 26)                | (26)                 |
|             | .128                 | .335                 | .001                  | .016                 | .000                 | .055                 | .012                 | .326                | .092                  | .056                 | .438                 | .000                 | .077                 | .095          | .322                 | .409                 | .135                 |
| <b>A</b> s  | .054                 | 330                  | .588                  | .589                 | .317                 | 1.000                | .319                 | .533                | .193                  | 500                  | 475                  | .486                 | 031                  | 116           | 263                  | 308                  | .113                 |
|             | (26)                 | (26)                 | (26)                  | (26)                 | (26)                 | ( 0)                 | (26)                 | (26)                | (26)                  | (26)                 | ( 26)                | (25)                 | (25)                 | (25)          | ( 25)                | (26)                 | (26)                 |
|             | .394                 | .048                 | .001                  | .001                 | .055                 | .000                 | .054                 | .002                | .318                  | .995                 | .807                 | .007                 | .440                 | .293          | .101                 | .061                 | .294                 |
| 56          | .178                 | 223                  | .381                  | .247                 | .440                 | .319                 | 1.000                | .256                | .383                  | ~.₽7€                | 101                  | .428                 | .155                 | 141           | .008                 | 048                  | .18E                 |
|             | (26)                 | (26)                 | (26)                  | (26)                 | (26)                 | (26)                 | ( 0)                 | (26)                | (26)                  | (26)                 | ( 26)                | (25)                 | (25)                 | (25)          | (25)                 | (26)                 | (26)                 |
|             | .295                 | .137                 | .026                  | .111                 | .012                 | .054                 | .000                 | .182                | .964                  | .35€                 | .315                 | .016                 | .267                 | -254          | .463                 | .405                 | .320                 |
| Mn          | 123                  | 270                  | .466                  | .499                 | .094                 | .533                 | .256                 | 1.000               | 191                   | 794                  | 759                  | .115                 | 102                  | 217           | .140                 | 548                  | .622                 |
|             | (26)                 | (26)                 | ( 26)                 | (26)                 | (26)                 | (26)                 | (26)                 | ( 0)                | (26)                  | (26)                 | ( 26)                | (25)                 | (25)                 | (25)          | (25)                 | (26)                 | (26)                 |
|             | .279                 | .089                 | .008                  | .005                 | .326                 | .092                 | .102                 | .000                | .323                  | .999                 | .000                 | .295                 | .316                 | .148          | .256                 | .002                 | .456                 |
| Co          | .598<br>(26)<br>.001 | .197<br>(26)<br>.332 | .116<br>( 26)<br>.290 | .119<br>(26)<br>.284 | .540<br>(26)<br>.002 | .103<br>(26)<br>.310 | .303<br>(26)<br>.054 | 191<br>(26)<br>.323 | 1.000<br>( 8)<br>.000 | .133<br>(26)<br>.263 | .470<br>(26)<br>.007 | .668<br>(25)<br>.000 | .143<br>(25)<br>.251 | ( 25)<br>.349 | .113<br>(25)<br>.299 | .139<br>(26)<br>.252 | .317<br>(26)<br>.056 |
| Ye          | 011                  | -174                 | 676                   | 697                  | 316                  | 500                  | 076                  | 704                 | .133                  | 1.000                | .621                 | 184                  | .092                 | .292          | .072                 | .686                 | .255                 |
|             | (26)                 | (26)                 | (26)                  | (26)                 | (26)                 | (26)                 | (26)                 | (26)                | (26)                  | ( B)                 | (26)                 | ( 25)                | (25)                 | (25)          | (25)                 | (26)                 | (26)                 |
|             | .479                 | -389                 | .000                  | .000                 | .056                 | .005                 | .356                 | .000                | .263                  | .000                 | .000                 | .309                 | .332                 | .076          | .365                 | .000                 | .103                 |
| S           | .285                 | .292                 | 394                   | 314                  | .931                 | 478                  | 101                  | 758                 | .470                  | .621                 | 1.090                | .124                 | .143                 | 037           | 004                  | -654                 | .095                 |
|             | (26)                 | (26)                 | (26)                  | (26)                 | (26)                 | (26)                 | (26)                 | (26)                | (26)                  | (26)                 | ( 0)                 | (25)                 | (25)                 | (25)          | (25)                 | (26)                 | (26)                 |
|             | .Ø78                 | .Ø72                 | .022                  | .057                 | .438                 | .007                 | .315                 | .000                | .007                  | .000                 | .000                 | .280                 | .251                 | .428          | .492                 | -099                 | .322                 |
| <b>B1</b> · | .284                 | 317                  | .458                  | .340                 | .652                 | .486                 | .428                 | .115                | .668                  | 184                  | .124                 | 1.000                | .435                 | 317           | 068                  | .846                 | .187                 |
|             | (25)                 | { 25)                | (25)                  | (25)                 | (25)                 | (25)                 | (25)                 | (25)                | (25)                  | (25)                 | (25)                 | ( 0)                 | (25)                 | (25)          | (25)                 | (25)                 | (25)                 |
|             | .883                 | .059                 | .010                  | .046                 | .000                 | .007                 | .016                 | .295                | .000                  | .309                 | .290                 | .000                 | .014                 | .059          | .373                 | .411                 | .314                 |
| Te          | .123                 | 354                  | .041                  | 102                  | .291                 | 031                  | .155                 | 102                 | .143                  | .092                 | .143                 | .435                 | 1.000                | 182           | 128                  | .246                 | 052                  |
|             | (25)                 | (25)                 | (25)                  | (25)                 | (25)                 | (25)                 | (25)                 | (25)                | (25)                  | (25)                 | (25)                 | (25)                 | ( 0)                 | (25)          | (25)                 | (25)                 | (25)                 |
|             | .283                 | .040                 | .420                  | .316                 | .077                 | .449                 | .267                 | .316                | .251                  | .332                 | .251                 | .014                 | .000                 | .306          | .274                 | .118                 | .401                 |
| Sn          | .179                 | .315                 | 427                   | 209                  | 269                  | 116                  | 141                  | 217                 | 083                   | .292                 | 037                  | 317                  | 182                  | 1.000         | .190                 | 016                  | .501                 |
|             | ( 25)                | (25)                 | ( 25)                 | (25)                 | (25)                 | (25)                 | (25)                 | (25)                | (25)                  | (25)                 | (25)                 | (25)                 | (25)                 | ( 0)          | (25)                 | (25)                 | (25)                 |
|             | .302                 | .061                 | .016                  | .159                 | .095                 | .293                 | .254                 | .14B                | .348                  | .Ø76                 | .428                 | .059                 | .306                 | .000          | .317                 | .469                 | .005                 |
| ۷           | .107                 | .330                 | 969                   | 167                  | 194                  | 263                  | .008                 | .140                | .113                  | .072                 | 004                  | 068                  | 128                  | -190          | 1.000                | 024                  | .318                 |
|             | (25)                 | (25)                 | (25)                  | (25)                 | (25)                 | (25)                 | (25)                 | (25)                | (25)                  | (25)                 | (25)                 | (25)                 | (25)                 | (25)          | ( 0)                 | (25)                 | (25)                 |
|             | .309                 | .052                 | .386                  | .285                 | .322                 | .101                 | .483                 | .256                | .298                  | .365                 | .492                 | .373                 | .274                 | -317          | .000                 | .452                 | .059                 |
| B 7         | .082                 | 110                  | 453                   | 437                  | 946                  | 308                  | 948                  | 548                 | .139                  | -686                 | -654                 | .046                 | .246                 | 016           | 024                  | 1.000                | .179                 |
|             | (26)                 | (26)                 | (26)                  | (26)                 | (26)                 | (26)                 | (26)                 | ( 26)               | (26)                  | (26)                 | ( 26)                | (25)                 | (25)                 | (25)          | (25)                 | ( 0)                 | (26)                 |
|             | .495                 | .299                 | .010                  | .012                 | .499                 | .061                 | .405                 | -002                | .252                  | .989                 | -000                 | .411                 | .118                 | .469          | .452                 | .452                 | .307                 |
| 11 8        | .336                 | .193                 | 274                   | 148                  | 224                  | .113                 | .198                 | .022                | .317                  | .255                 | .095                 | .187                 | 052                  | .501          | .318                 | .179                 | 1.090                |
|             | (26)                 | (26)                 | (26)                  | (26)                 | (26)                 | ( 26)                | (26)                 | (26)                | (26)                  | (26)                 | (26)                 | (25)                 | (25)                 | (25)          | (25)                 | (26)                 | ( 0)                 |
|             | .945                 | .327                 | .087                  | .251                 | .135                 | .294                 | .320                 | .455                | .056                  | .103                 | .322                 | .314                 | .401                 | .005          | .059                 | .307                 | .301                 |

\*\*\* Correlation Coefficient / (# of data points) / Significance

R 7 = +3.3 SP. GR. FRACTION (WT.X)

R B - T MAGNETIC FRACTION

# TABLE A-3. PEARSON PRODUCT-MOMENT CORRELATION MATRIX FOR PERCUSSION-HOLE GEOCHEMICAL DATA

ANDREW BAY PROSPECT BRITISE COLUMBIA

| Bitment         Cu         Pa         Ta         Ag         A         Sb         Pa         Co         Pa         S         Bit         Te         Sit         V         Bit           Gu         1.888         .666         .113         .1231         .681         .261         .281         .284         .335         .285         .385         .286         .385         .285         .286         .385         .285 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>•</th> <th></th>  |            |                       |                         |                       |                       |                       |                       | •                     |                       |                       |                        |                       |                       |                       |                       |                       |                       |                              |
|---|------------|-----------------------|-------------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------------|
| Cu       1.000       .066       -114       -1162       .001       .000       .004       .100       .200       .201  | Element    | Cu                    | Mo                      | Pb                    | 2 n                   | 46                    | A s                   | Sb                    | Ħв                    | Co                    | Te                     | S                     | Bi                    | Te                    | Sn                    | ¥                     | B 7                   | R 8                          |
| mo  | Cu         | 1.000<br>( 0)<br>.000 | .666<br>(26)<br>.000    | 174<br>( 26)<br>.309  | 162<br>(26)<br>.283   | .951<br>( 26)<br>.490 | 016<br>(26)<br>.468   | 087<br>(26)<br>.337   | 090<br>(26)<br>.332   | •484<br>(26)<br>•996  | .188<br>(26)<br>.320   | .294<br>(26)<br>.978  | 030<br>( 25)<br>.440  | 076<br>(25)<br>.359   | .781<br>( 25)<br>.000 | .150<br>(25)<br>.259  | .010<br>(26)<br>.481  | .478<br>(26)<br>.806         |
| Pb      174      115       1.000       .651       .251       .251       .252       .251       .251       .252       .251   | Mo         | .665<br>(26)<br>.899  | 1.000<br>( 0)<br>.000   | 115<br>( 26)<br>.291  | 148<br>(26)<br>.261   | .895<br>(26)<br>.324  | 887<br>(26)<br>.338   | +.963<br>(26)<br>.378 | 873<br>(26)<br>.362   | .327<br>(26)<br>.049  | .185<br>(26)<br>.317   | .260<br>(26)<br>.099  | 011<br>( 25)<br>.479  | 086<br>( 25)<br>.342  | •889<br>(25)<br>•990  | 038<br>(25)<br>.426   | 057<br>(26)<br>.390   | .704<br>(26)<br>.000         |
| 2a      162      162       .164       .653       .261       .263       .261       .263       .261       .263       .261       .251       .251  | Pb         | 174<br>( 26)<br>.300  | 115<br>(26)<br>.291     | 1.000<br>( 0)<br>.000 | .651<br>(26)<br>.000  | .501<br>( 26)<br>.004 | .261<br>(26)<br>.897  | .102<br>(26)<br>.313  | .649<br>(26)<br>.009  | 139<br>(26)<br>.253   | 298<br>(26)<br>.154    | 091<br>(26)<br>.331   | 031<br>(25)<br>.439   | 058<br>(25)<br>.389   | 185<br>(25)<br>.310   | 120<br>( 25)<br>.288  | 060<br>(26)<br>.385   | +.206<br>(26)<br>.156        |
| A6  | 2.n        | 162<br>(26)<br>.283   | 148<br>( 26)<br>.261    | .651<br>(26)<br>.900  | 1.800<br>( 6)<br>.900 | .550<br>(26)<br>.002  | .486<br>(26)<br>.896  | .846<br>(26)<br>.410  | .663<br>(26)<br>.899  | .898<br>(26)<br>.328  | 486<br>(26)<br>.819    | 182<br>(26)<br>.312   | .318<br>(25)<br>.059  | 086<br>(25)<br>.343   | 199<br>(25)<br>.329   | 120<br>(25)<br>.287   | 176<br>( 26)<br>.303  | 241<br>(26)<br>.117          |
| As      816      807       .2261       .486       .415       1.808       .804       .432       .967      395      335       .555       .603       .304       .181      226       .226       (22)       .222       .445       .597       .333      146       .444       .444       .444       .444       .444       .444       .444       .444       .444       .466       .226       .2267       .594       .229       .225 <td><b>A</b>g</td> <td>.051<br/>(26)<br/>.400</td> <td>.095<br/>(26)<br/>.324</td> <td>-501<br/>(26)<br/>-894</td> <td>.559<br/>(26)<br/>.992</td> <td>1.899<br/>( 9)<br/>.999</td> <td>.415<br/>(26)<br/>.017</td> <td>.230<br/>(26)<br/>.129</td> <td>.480<br/>(26)<br/>.995</td> <td>.360<br/>(26)<br/>.834</td> <td>311<br/>(26)<br/>.059</td> <td>.016<br/>(26)<br/>.467</td> <td>.588<br/>(25)<br/>.001</td> <td>.236<br/>(25)<br/>.127</td> <td>008<br/>(25)<br/>.484</td> <td>220<br/>(25)<br/>.146</td> <td>119<br/>( 26)<br/>.285</td> <td>099<br/>(26)<br/>.318</td>               | <b>A</b> g | .051<br>(26)<br>.400  | .095<br>(26)<br>.324    | -501<br>(26)<br>-894  | .559<br>(26)<br>.992  | 1.899<br>( 9)<br>.999 | .415<br>(26)<br>.017  | .230<br>(26)<br>.129  | .480<br>(26)<br>.995  | .360<br>(26)<br>.834  | 311<br>(26)<br>.059    | .016<br>(26)<br>.467  | .588<br>(25)<br>.001  | .236<br>(25)<br>.127  | 008<br>(25)<br>.484   | 220<br>(25)<br>.146   | 119<br>( 26)<br>.285  | 099<br>(26)<br>.318          |
| Sb      087      063       .192       .046       .238       .094       1.086       .141       .165       .954      166       .377       .333      146       .444       .444         .337       .377       .373       .313       .141       .122       .449       .449       .251       .251       (.25  | <b>A</b> s | 016<br>(26)<br>.468   | 087<br>(26)<br>.338     | .261<br>( 26)<br>.097 | .486<br>(26)<br>.005  | .415<br>(26)<br>.917  | 1.000<br>(            | .004<br>(26)<br>.498  | .432<br>(26)<br>.913  | .967<br>(26)<br>.372  | 395<br>(26)<br>.822    | 335<br>(26)<br>.945   | .355<br>(25)<br>.639  | 083<br>(25)<br>.347   | 181<br>( 25)<br>.394  | 256<br>(25)<br>.107   | 210<br>(26)<br>.152   | 076<br>( 26)<br>-356         |
| Ma      099      073       .649       .663       .480       .432       .141       1.090      146      299      280       .044      0655      118      064       .125         .332       .552       .562       .090       .690       .261       (26)       (26)       (25) <td>52</td> <td>087<br/>(26)<br/>.337</td> <td>963<br/>(26)<br/>.378</td> <td>.102<br/>(26)<br/>.313</td> <td>.946<br/>(26)<br/>.419</td> <td>.230<br/>(26)<br/>.129</td> <td>.004<br/>(26)<br/>.490</td> <td>1.000<br/>( 0)<br/>.000</td> <td>.141<br/>(26)<br/>.250</td> <td>.165<br/>(26)<br/>.287</td> <td>.854<br/>(26)<br/>.394</td> <td>165<br/>(26)<br/>.289</td> <td>.377<br/>(25)<br/>.030</td> <td>.333<br/>(25)<br/>.050</td> <td>148<br/>(25)<br/>.256</td> <td>.494<br/>(25)<br/>.822</td> <td>081<br/>(26)<br/>.349</td> <td>.312<br/>(26)<br/>.059</td>                                     | 52         | 087<br>(26)<br>.337   | 963<br>(26)<br>.378     | .102<br>(26)<br>.313  | .946<br>(26)<br>.419  | .230<br>(26)<br>.129  | .004<br>(26)<br>.490  | 1.000<br>( 0)<br>.000 | .141<br>(26)<br>.250  | .165<br>(26)<br>.287  | .854<br>(26)<br>.394   | 165<br>(26)<br>.289   | .377<br>(25)<br>.030  | .333<br>(25)<br>.050  | 148<br>(25)<br>.256   | .494<br>(25)<br>.822  | 081<br>(26)<br>.349   | .312<br>(26)<br>.059         |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$   | Ms         | 090<br>(26)<br>.332   | +.073<br>(26)<br>.362   | .649<br>(26)<br>.800  | .663<br>(26)<br>.998  | .480<br>(26)<br>.006  | .432<br>( 26)<br>.013 | .141<br>(26)<br>.250  | 1.000<br>( 0)<br>.000 | 146<br>(26)<br>.258   | 289<br>(26)<br>.074    | 209<br>(26)<br>.153   | 044<br>(25)<br>.415   | 065<br>(25)<br>.376   | 110<br>(25)<br>.303   | 064<br>(25)<br>.379   | .039<br>(26)<br>.422  | . <b>894</b><br>(26)<br>.325 |
| Pe       .188       .186      286      486      311      395       .854      289       .235       1.888       .493      815       .143       .256       .894       .2         .326       .317       .154       .019       .659       .622       .394       .674       .123       .696       .695       .476       .145       .256       .251       (.25) <td>Co</td> <td>.484<br/>(26)<br/>.996</td> <td>.327<br/>(26)<br/>.049</td> <td>139<br/>(26)<br/>.253</td> <td>.098<br/>(26)<br/>.320</td> <td>-360<br/>(26)<br/>-034</td> <td>.867<br/>(26)<br/>.372</td> <td>.165<br/>(26)<br/>.287</td> <td>146<br/>( 26)<br/>.258</td> <td>1.000<br/>( 0)<br/>.000</td> <td>.235<br/>(26)<br/>.123</td> <td>.429<br/>(26)<br/>.014</td> <td>.481<br/>(25)<br/>.007</td> <td>.064<br/>(25)<br/>.380</td> <td>.277<br/>(25)<br/>.089</td> <td>.141<br/>(25)<br/>.254</td> <td>090<br/>(26)<br/>.333</td> <td>.424<br/>(26)<br/>.015</td> | Co         | .484<br>(26)<br>.996  | .327<br>(26)<br>.049    | 139<br>(26)<br>.253   | .098<br>(26)<br>.320  | -360<br>(26)<br>-034  | .867<br>(26)<br>.372  | .165<br>(26)<br>.287  | 146<br>( 26)<br>.258  | 1.000<br>( 0)<br>.000 | .235<br>(26)<br>.123   | .429<br>(26)<br>.014  | .481<br>(25)<br>.007  | .064<br>(25)<br>.380  | .277<br>(25)<br>.089  | .141<br>(25)<br>.254  | 090<br>(26)<br>.333   | .424<br>(26)<br>.015         |
| S       .264       .266      091      182       .016      335      166      289       .429       .493       1.000       .116       .167       .166      129       .         S       (26)       (25) <t< td=""><td>Je</td><td>.188<br/>(26)<br/>.320</td><td>.186<br/>(26)<br/>.317</td><td>208<br/>(26)<br/>.154</td><td>406<br/>(26)<br/>.019</td><td>311<br/>(26)<br/>.#59</td><td>395<br/>(26)<br/>.822</td><td>.054<br/>(26)<br/>.394</td><td>289<br/>(26)<br/>.074</td><td>.235<br/>(26)<br/>.123</td><td>1.000<br/>( 0)<br/>.000</td><td>.493<br/>(26)<br/>.885</td><td>015<br/>(25)<br/>.478</td><td>.143<br/>(25)<br/>.251</td><td>.258<br/>(25)<br/>.195</td><td>.894<br/>(25)<br/>.329</td><td>.395<br/>(26)<br/>.022</td><td>.267<br/>(26)<br/>.092</td></t<>  | Je         | .188<br>(26)<br>.320  | .186<br>(26)<br>.317    | 208<br>(26)<br>.154   | 406<br>(26)<br>.019   | 311<br>(26)<br>.#59   | 395<br>(26)<br>.822   | .054<br>(26)<br>.394  | 289<br>(26)<br>.074   | .235<br>(26)<br>.123  | 1.000<br>( 0)<br>.000  | .493<br>(26)<br>.885  | 015<br>(25)<br>.478   | .143<br>(25)<br>.251  | .258<br>(25)<br>.195  | .894<br>(25)<br>.329  | .395<br>(26)<br>.022  | .267<br>(26)<br>.092         |
| B1      030      011      031       .318       .588       .355       .377      044       .481      015       .116       1.000       .592      144      127          (25)  | S          | .294<br>(26)<br>.078  | .260<br>(26)<br>.099    | 091<br>(26)<br>.331   | 182<br>(26)<br>.312   | .016<br>(26)<br>.467  | 335<br>(26)<br>.045   | 166<br>(26)<br>.289   | 209<br>(26)<br>.153   | .429<br>(26)<br>.014  | •493<br>(26)<br>•005   | 1.000<br>( 0)<br>.000 | .116<br>(25)<br>.294  | .167<br>(25)<br>.285  | .166<br>(25)<br>.283  | 129<br>(25)<br>.273   | .479<br>(26)<br>.006  | .061<br>(26)<br>.362         |
| Te      076      086      086       .236      083       .333      066       .064       .143       .167       .592       1.000      135      122       .         (25)   | Bi         | 030<br>(25)<br>.440   | 011<br>(25)<br>.479     | 031<br>(25)<br>.439   | .318<br>(25)<br>.659  | .588<br>(25)<br>.001  | .355<br>(25)<br>.039  | .377<br>(25)<br>.838  | 844<br>(25)<br>.415   | .481<br>(25)<br>.007  | +.015<br>( 25)<br>.470 | .116<br>(25)<br>.294  | 1.090<br>( 0)<br>.990 | .592<br>(25)<br>.001  | 144<br>(25)<br>.251   | 127<br>(25)<br>.277   | 111<br>( 25)<br>.301  | .834<br>(25)<br>.434         |
| Sb       .781       .889      185      199      000      148      110       .277       .250       .166      144      135       1.000       .001       .251       (25)   | Te         | 076<br>(25)<br>.359   | 086<br>( 25)<br>.342    | 058<br>(25)<br>.389   | 086<br>(25)<br>.343   | .236<br>(25)<br>.127  | 083<br>(25)<br>.347   | .333<br>(25)<br>.050  | 066<br>(25)<br>.375   | .064<br>(25)<br>.380  | .143<br>(25)<br>.251   | .167<br>(25)<br>.285  | .592<br>(25)<br>.001  | 1.000<br>( 0)<br>.000 | 135<br>(25)<br>.263   | 122<br>(25)<br>.284   | .824<br>(25)<br>.453  | 119<br>(25)<br>.288          |
| Y       .150838120120220256 .404064 .141 .094129127122 .091 1.000         (25)       (26)   | So         | .781<br>( 25)<br>.000 | .889<br>(25)<br>.000    | 185<br>(25)<br>.310   | 199<br>(25)<br>.329   | 00e<br>( 25)<br>.484  | 181<br>(25)<br>.304   | 148<br>(25)<br>.256   | 110<br>( 25)<br>.303  | .277<br>(25)<br>.089  | .258<br>(25)<br>.105   | .166<br>(25)<br>.283  | 144<br>(25)<br>.251   | 135<br>(25)<br>.263   | 1.000<br>( 0)<br>.000 | .081<br>(25)<br>.352  | 075<br>(25)<br>.361   | .623<br>(25)<br>.000         |
| B 7       .010057068176119218081 .039090 .395 .479111 .624075091 1.         (26) (26) (26) (26) (26) (26) (26) (26)   | v          | .150<br>(25)<br>.259  | 038<br>(25)<br>.426     | 120<br>(25)<br>.288   | 128<br>(25)<br>.287   | 220<br>(25)<br>.146   | 256<br>(25)<br>.107   | .494<br>(25)<br>.022  | 864<br>(25)<br>.379   | .141<br>(25)<br>.254  | .994<br>(25)<br>.329   | 129<br>(25)<br>.273   | 127<br>(25)<br>.277   | 122<br>(25)<br>.284   | .081<br>(25)<br>.352  | 1.000<br>( 0)<br>.000 | 091<br>(25)<br>.334   | .326<br>(25)<br>.054         |
| B 8 .478 .704285241099076 .312094 .424 .267 .061 .034119 .623 .326<br>{ (26) (26) (26) (26) (26) (26) (26) (26)   | 11 7       | .010<br>(26)<br>.481  | ~.057<br>(26)<br>.390   | 060<br>(26)<br>.385   | 176<br>(26)<br>.383   | 119<br>(26)<br>.285   | 210<br>(26)<br>.152   | 081<br>(26)<br>.348   | .#39<br>(26)<br>.422  | 090<br>(26)<br>.333   | .395<br>(26)<br>.022   | .479<br>(26)<br>.906  | 111<br>(25)<br>.301   | .624<br>(25)<br>.453  | 075<br>(25)<br>.361   | 091<br>(25)<br>.334   | 1.000<br>( 0)<br>.334 | 152<br>(26)<br>.267          |
|   | B 8        | .478<br>(26)<br>.006  | · .784<br>( 26)<br>.888 | 206<br>(26)<br>.156   | 241<br>(26)<br>.117   | 099<br>(26)<br>.318   | 076<br>(26)<br>.356   | .312<br>(26)<br>.059  | 094<br>(26)<br>.325   | .424<br>(26)<br>.015  | .267<br>(26)<br>.092   | .961<br>(26)<br>.382  | .034<br>(25)<br>.434  | 119<br>(25)<br>.288   | .623<br>(25)<br>.000  | .326<br>(25)<br>.054  | 152<br>(26)<br>.267   | 1.800<br>( 0)<br>.267        |

\*\*\* Correlation Coefficient / (# of data points) / Significance

E 7 = +3.3 SP. GR. FRACTION (WT.%)

R 8 = % MAGNETIC FRACTION

# FIGURE A-1. SPEARMAN RANK CLUSTER ANALYSIS FOR PERCUSSION-HOLE GEOCHEMICAL DATA

\*\*\* Spearman Rank Cluster Analysis \*\*\*

#### ANDREW BAY PROSPECT BRITISH COLUMBIA



| Cu | Mo         | .62680 |
|----|------------|--------|
| Pb | Zn         | .79500 |
| Co | Bi         | .66790 |
| Fe | R 7        | .68642 |
| Sn | R 8        | .50143 |
| Pb | As         | .58873 |
| Åg | Co         | .59613 |
| Ĩĕ | S          | .63715 |
| Cu | Sn         | .25587 |
| Pb | Mn         | .50811 |
| Mg | Sb         | .40277 |
| Cũ | W          | .23592 |
| Pb | ٨g         | .23531 |
| Fe | Te         | .15607 |
| Cu | <b>F</b> e | 02666  |
| Cu | Pb         | 07874  |

Columns 1 and 2 - Observations combined into clusters Column 3 - Similarity level of clustering

DENEROGRAM - VALUES ALONG X-AXIS ARE SIMILARITIES

R 7 = +3.3 SP. GR. FRACTION (WT.%)

R = % MAGNETIC FRACTION

## FIGURE A-2. PEARSON PRODUCT-MOMENT CLUSTER ANALYSIS FOR PERCUSSION-HOLE GEOCHEMICAL DATA

\*\*\* Pearson Product-Moment Cluster Analysis \*\*\*

#### ANDREW BAY PROSPECT BRITISH COLUMBIA



R = +3.3 SP. GR. FRACTION (WT.%)

R = % MAGNETIC FRACTION

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# APPENDIX B

Original Geochemical Data



# ROCKY MOUNTAIN CEOCHEMICAL CORP.

W. 7900 SOUTH • WEST JORDAN, UTAH 84084

PHONE: (801) 255-3558

# Certificate of Analysis

|      |   |    | 6 |
|------|---|----|---|
| Page | 1 | of |   |

 Date:
 January 5, 1981
 RMGC Numbers:

 Local Job No.:
 B0-35-36-SL

 Client:
 Robert W. Bamford
 Foreign Job No.:

 1138 Gilmer Drive
 Invoice NoM 102703

Client Order No.:

none

Report On: 26 Composite Samples

Submitted by: Robert W. Bamford

Date Received: 10/31/80

Analysis: Heavy Mineral Separation, Sulfur, Copper, Lead, Zinc, Cobalt, Molybdenum, Manganese, Iron, Silver, Antimony and Arsenic.

Analytical Methods: Sulfur determined by leco induction furnace. Arsenic determined colormetrically. Remaining elements determined by atomic absorption.

#### Remarks:

CC:

enc. file (2) GJC/lw

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All values are reported in parts per million unless specified otherwise. A minus sign (—) is to be read "less than" and a plus sign (+) "greater than." Values in parenthesis are estimates. This analytical report is the confidential property of the above mentioned client and for the protection of this client and ourselves we reserve the right to forbid publication or reproduction of this report or any part thereof without written permission. ND — None Detected 1 ppm = 0.0001% 1 Troy oz./ton = 34.286 ppm 1 ppm = 0.0292 Troy oz./ton

| ClientRob  | ert W. Bamfor | đ              |              | <u>l</u> | RMGC Job No. 80 | -35-36-SI |
|------------|---------------|----------------|--------------|----------|-----------------|-----------|
| •          |               |                |              |          | Page 2          | of6       |
|            | MRG-1         |                | SY-2         |          | GRLD            | -105      |
|            | Lit Value     | Found          | Lit Value    | Found    | Lit Value       | Found     |
| COPPER     | 135           | 118            | 5            | 6        | 0.726%          | 0.721%    |
| LEAD       | 10            | 40             | 80           | 100      | 37              | 40        |
| ZINC       | 190           | 134            | 250          | 185      | 48              | 38        |
| MOLYBDENUM | -1            | -1             | 3            | -1       | 344             | 280       |
| MANGANESE  | 0.131%        | 0.149%         | 0.248%       | 0.240%   | 105             | 100       |
| IRON       | 12.4%         | 11.0%          | 4:39%        | 4.01%    | 2.90%           | 2.71%     |
| COBALT     | 86            | 90             | 11           | 15       | 24              | 15        |
| SILVER     | -1            | -2             | - <b>-</b> 1 | -2       | 3               | 4         |
| ANTIMONY   | -1            | -1             | -1           | -1       | -1              | -1        |
| ARSENIC    | -1            | <del>-</del> 5 | 18           | 20       | 26              | 35        |



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| Client | Robert | W. | Bamford |
|--------|--------|----|---------|
| Cuent  |        |    |         |

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Date 1/5/81 RMGC Job No. 80-35-36-SI

| Sample No.      | Wt<br><u>+3.3 gr</u> . | Wt %<br>+3.3 | Wt Mag. | Wt %<br>Mag. | Page <u>3 of 6</u><br>Sample Wt<br>Separated gr. |
|-----------------|------------------------|--------------|---------|--------------|--|
| ABPH- 1/115-210 | 1.56                   | 1.95         | 0.03    | 0.04         | 80   |
| 2/130-230       | 1.45                   | 1.81         | 0.07    | 0.09         | 80   |
| 5/230-282       | 1.97                   | 2.46         | 0.11    | 0.14         | 80   |
| 7/190-290       | 0.31                   | 0.39         | 0.13    | 0.16         | 80   |
| 9/ 70-170       | 0.11                   | 0.14         | 0.02    | 0.02         | 80   |
| 10/172-270      | 0.16                   | 0.20         | 0.05    | 0.06         | 80   |
| 11/190-200      | 0.51                   | 0.93         | 0.09    | 0.16         | 55   |
| 12/250-270      | 0.53                   | 0.66         | 0.17    | 0.21         | 80   |
| 13/153-250      | 0.65                   | 0.81         | 0.27    | 0.34         | 80   |
| 14/ 60-160      | 0.30                   | 0.38         | 0.36    | 0.45         | 80   |
| 15/165-260      | 0.80                   | 1.00         | 0.05    | 0.06         | 80   |
| 16/ 9-110       | 0.40                   | 0.50         | 0.48    | <b>0.</b> 60 | 80   |
| ¥7/ 88-190      | 1.68                   | 2.10         | 0.12    | 0.15         | 80   |
| 18/ 57-160      | 0.60                   | - 0.75       | 0.02    | 0.02         | 80   |
| 19/ 63-160      | 2.76                   | 3.45         | 0.01    | 0.01         | 80   |
| 20/137-240      | 8.42                   | 10.5         | 0.02    | 0.02         | 80   |
| 22/ 77-180      | 0.15                   | 0.19         | 0.01    | 0.01         | 80   |
| 23/ 20-120      | 0.74                   | 0.92         | 0.03    | 0.04         | 8.0  |
| 25/ 41-140      | 1.00                   | 1.25         | 0.02    | 0.02         | 80   |
| 26/ 37-140      | 0.42                   | 0.52         | 0.02    | 0.02         | , 80   |
| 27/ 42-140      | 0.57                   | 0.71         | 0.09    | 0.11         | 80   |
| 28/ 57-160      | 0.16                   | 0.20         | 0.01    | 0.01         | 80   |
| 29/ 75-170      | 0.16                   | 0.20         | 0.01    | 0.01         | 80   |
| 30/ 20-120      | 0.59                   | 0.74         | 0.01    | 0.01         | 80   |
| 32/ 74-170      | 0.05                   | 0.06         | -0.01   | -0.01        | 80   |
| ABPH-36/180-230 | 1.08                   | 1.35         | 0.07    | 0.09         | 80   |



SUCT LARE CITY, UTAM REPORTED AND ARIZONA

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| Client Robert W. I | Bamford                      | Date1/        | 5/81        |             | Job No. 80-35-36-SL              |
|--------------------|------------------------------|---------------|-------------|-------------|----------------------------------|
| ample No.          | gr.<br>Sample Wt<br>Analyzed | ppm<br>Copper | ppm<br>Lead | ppm<br>Zinc | Page 4 of 6<br>ppm<br>Molybdenum |
| ABPH- 1/115-210    | 0.2000                       | 500           | 0.33%       | 1.94%       | -5                               |
| 2/130-230          | 0.2000                       | 915           | 490         | 0.49%       | -5                               |
| 6/230-282          | 0.2000                       | 32            | 40          | 325         | <del>-</del> 5                   |
| 7/190-290          | 0.2000                       | 455           | 65          | 0.12%       | 10                               |
| 9/ 70-170          | 0.0800                       | 470           | 190         | 0.56%       | 25                               |
| 10/172-270         | 0.1000                       | 580           | 290         | 1.08%       | 20                               |
| 11/190-200         | 0.2000                       | 415           | 125         | 0.25%       | -5                               |
| 12/250-270         | 0.2000                       | 0.44%         | 170         | 0.20%       | <b>9</b> 85                      |
| 13/153-250         | 0.2000                       | 0.11%         | 85          | 0.14%       | 160                              |
| 14/ 60-160         | 0.2000                       | 725           | 320         | 0.10%       | 20                               |
| 15/165-260         | 0.2000                       | 610           | 165         | 960         | 15                               |
| 16/ 9-110          | 0.2000                       | 0.51%         | 100         | 0.15%       | 0.61%                            |
| 17/ 88-190         | 0.2000                       | 0.72%         | 40          | 670         | 0.12%                            |
| 18/ 57-160         | 0.2000                       | 0.14%         | <b>48</b> 5 | 1.13%       | <b>4</b> 0                       |
| 19/ 63-160         | 0.2000                       | 525           | 40          | 325         | 15                               |
| 20/137-240         | 0.2000                       | 860           | 70          | 145         | 170                              |
| 22/ 77-180         | 0.1000                       | 780           | 120         | 0.20%       | 50                               |
| 23/ 20-120         | 0.2000                       | 310           | 7 0         | 165         | 10                               |
| 25/ 41-140         | 0.2000                       | 540           | 70          | 190         | -5                               |
| 26/ 37-140         | 0.2000                       | 570           | 160         | 0.68%       | 10                               |
| 27/ 42-140         | 0.2000                       | 630           | 335         | 1.22%       | -5                               |
| 28/ 57-160         | 0.1000                       | 365           | 860         | 0.37%       | -10                              |
| 29/ 75-170         | 0.1000                       | 170           | 220         | 0.14%       | -10                              |
| 30/ 20-120         | 0.2000                       | 200           | 0.35%       | 0.81%       | 20                               |
| , 32/ 74-170       | 0.0400                       | 840           | 500         | 0.34%       | 125                              |
| BPH-36/180-230     | 0.2000                       | 270           | 75          | 210         | 55                               |



TUCSON ARIZONA

| Client Robert W. Bamford |                  | Date1/    | 5/81          | RMGC Job No           | 36-SL       |          |
|--------------------------|------------------|-----------|---------------|-----------------------|-------------|----------|
| Sample No.               | ppm<br>Manganese | ۶<br>Iron | ppm<br>Cobalt | Page<br>ppm<br>Silver | <u>5</u> of | <u> </u> |
| BPH- 1/115-210           | 10.4%            | 21.9      | 140           | 21                    |             |          |
| 2/130-230                | 0.12%            | 48.8      | 285           | 14                    |             |          |
| 6/230-282                | 240              | 57.5      | 170           | 4                     |             |          |
| 7/190-290                | 0.26%            | 50.0      | 75            | 4                     |             |          |
| 9/ 70-170                | 0.23%            | 19.2      | 40            | -4                    |             |          |
| 10/172-270               | 0.22%            | 27.0      | 100           | -3                    |             |          |
| 11/190-200               | 0.14%            | 24.2      | 135           | 4                     |             |          |
| 12/250-270               | 0.22%            | 43.8      | 220           | 4                     |             |          |
| 13/153-250               | 655              | 53.8      | 560           | 4                     |             |          |
| 14/ 60-160               | 0.40%            | 48.8      | 420           | 5                     |             |          |
| 15/165-260               | 530              | 53.8      | 255           | 6                     |             |          |
| 16/ 9-110                | 135              | 56.2      | 510           | 11                    |             |          |
| 17/ 88-190               | 210              | 53.8      | 620           | 8                     |             |          |
| 18/ 57-160               | 0.22%            | 47.5      | 495           | 14                    |             |          |
| 19/ 63-160               | 52               | . 61.2    | 130           | 4                     |             |          |
| 20/137-240               | 58               | 61.2      | 185           | 4                     |             |          |
| 22/ 77-180               | 0.26%            | 17.4      | 130           | 5                     |             |          |
| 23/ 20-120               | 835              | 70.0      | 25            | 2                     |             |          |
| 25/ 41-140               | 910              | 55.0      | 340           | 9                     |             |          |
| 26/ 37-140               | 0.15%            | 50.0      | 520           | 5                     |             |          |
| 27/ 42-140               | 0.24%            | 38.8      | 630           | 16                    |             |          |
| 28/ 57-160               | 0.20%            | 24.7      | 370           | 17                    |             |          |
| 29/ 75-170               | 0.23%            | 16.6      | 110           | 7                     |             |          |
| 30/ 20-120               | 460              | 51.2      | 165           | 9                     |             |          |
| 32/ 74-170               | 0.11%            | 16.1      | 220           | 18                    |             |          |
| ABPH-36/180-230          | 0.20%            | 57.4      | 180           | 4                     |             |          |



| Client Robert W. Ban | lford          | _ Date1/5/81    | RMGC Job No. 80-35-36-SL |
|----------------------|----------------|-----------------|--------------------------|
| ample No.            | ppm<br>Arsenic | ppm<br>Antimony | Page6of_6<br>§<br>Sulfur |
| ABPH- 1/115-210      | 0.22%          | <u>4</u>        | 14.0                     |
| 2/130-230            | 0.078%         | 10              | 30.8                     |
| 6/230-282            | 25             | -1              | 33.2                     |
| 7/190-290            | <b>29</b> 5    | 2               | 4.00                     |
| 9/ 70-170            | 160            | -2              | 16.5                     |
| 10/172-270           | 0.040%         | -2              | 15.2                     |
| 11/190-200           | 0.065%         | -1              | 22.4                     |
| 12/250-270           | 0.20%          | -1              | 20.0                     |
| 13/153-250           | 0.078%         | -1              | 36.0                     |
| X4/ 60-160           | 250            | 12              | 4.80                     |
| 15/165-260           | 240            | 5               | 36.0                     |
| 16/ <b>9-</b> 110    | 255            | 2               | 37.6                     |
| 17/ 88-190           | 55             | -1              | 39.6                     |
| 18/ 57-160           | 0.13%          | 2               | 26.4                     |
| 19/ 63-160           | 55             | -1              | 42.0                     |
| 20/137-240           | 35             | -1              | 42.0                     |
| 22/ 77-180           | 170            | -2.             | 14.0                     |
| 23/ 20-120           | 0.065%         | - 1             | 2.40                     |
| 25/ 41-140           | 130            | -1              | 32.8                     |
| 26/ 37-140           | 0.032%         | 2               | 29.2                     |
| 27/ 42-140           | 0.20%          | -1              | 26.0                     |
| 28/ 57-160           | 0.095%         | 4               | 25.6                     |
| 29/ 75-170           | 0.27%          | -2              | 8.00                     |
| 30/ 20-120           | 215            | -1              | 30.4                     |
| 32/ 74-170           | 200.           | -5              | 12.0                     |
| EPH-36/180-230       | 95             | -1              | 36.0                     |



| BOGEXY         | MOUNTAIN | Geochemical | 1 <b>60</b> 37. |
|----------------|----------|-------------|-----------------|
| SALT LANS CITS | /T.1     |             | TUCSON ADIZONI  |

adua By\_ Jim Cardwell

TRO-CHEMICAL LABORATORY DIVISION OF COORS PORCELAIN COMPANY Coois/SPEC

GOLDEN, COLORADO, U.S.A.

303-278-4000 Ext. 2302

Mailing Address: P.O. Box 500 Golden, Colorado 80401

Analytical Report

TO: . Robert W, Bamford 1138 Gilmer Drive . Salt Lake City, UT 84105

| LABORATORY<br>NUMBER  | 96309  |  |
|-----------------------|--------|--|
| DATE                  | 2-5-81 |  |
| CUSTOMER<br>ORDER NO. |        |  |

ABPH Con's

Sample No. Bismuth Tin Tellurium Tungsten (mqq) (ppm) (ppm) (mag) < 10 < 10 1 3 < 1 2 20 < 1 15 < 10 6 < 10 1 l < 10 < 10 < 10 7 1 l < < 10 9 < 1 1 < 10 < 1 < 10 10 10 l < 10 < 10 5 < 1 11 4 < 10 12 1 < 10 < 10 13 2 < 1 < 10 14 5 < 10 15 < 1 < 10 15 2 < 1 < 10 16 5 3 < 10 < 10 10 2 < 10 17 1 < 10 < 10 18 10 < l < 10 < 10 19 l < l < < 10 < 10 20 1 1 < 10 22 < < 1 < 10 1 < 10 ٢ 1 < 10 23 1 < = Less than < 10 25 10 < 1 15 < 10 < 10 26 < 1 5 < 10 27 20 < l < 10 < 10 28 5 < 1 < 10 < 10 3 < 10 29 < l < 10 1 < l < 10 30 12 2 1 < 10 36 < Coors / SPECTRO-CHEMICAL LABORATORY This report is rendered upon the conditions that it is not to be reproduced wholly or in part for advertising or other purposes over our signature or in connection with our name without special permission in writing. BY LABORATORY MANAGER -46-

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# ITEMIZED COST STATEMENT

Β.

A. Consultants Expenditures (January 6, 1981 - April 8, 1981)

| Consulting, Report Writing<br>Geological Assistant<br>Data Processing, Computer Ch<br>Miscellaneous<br>Analyses | 5.44 days @ \$479/day<br>3.73 days @ \$210/day<br>arges | \$<br>2,176<br>782<br>1,714<br>215<br>2,151 |
|---|---|---|
| Allalyses   | SUBTOTAL  | \$<br>7,038                                 |
| Company Expenditures  |   |   |
| 1 day writing and typing (Ma  | v 8)  | \$<br>120                                   |

TOTAL

\$ 7,158

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# SYSTEMATIC · COST-EFFECTIVE · RESOURCE DISCOVERY Applications and Technique Development

|                   | Rol   | bert W. Bam   | ford  |  |   |
|-------------------|---|---|---|--|---|
|                   |   | Geologist/Geochem   | ISL   | ى دەرىپ ئۆتۈكۈنىدۇ.<br>1993- يېرىكى ئېچىلىرى ئېزىكى ئېچىكى ئېچىكى ئېچىكى ئېچىكى ئېچىكى ئېچىكى ئېچىكى ئېچىكى ئېچىكى<br>1994- يېرىكى ئېچىكى   | ا مېرې د د و ويونو و او  |
|                   |   | المراجعين والج  |   |  |   |
|                   |   |   |   |  |   |
| Consulting (hours | worked per day)   | ) for SMDC on   | Whiting Creek   | and Andrew Bay   | geochemical   |
| surveys.          |   | an an an Article and Articl<br>Article and Article and Artic<br>Article and Article and Artic |   |  |   |
| Data              |   | Whiting Cre   | ook   | Andrey Bay   |   |
|                   |   | MILLING UI  |   |  |   |
| Nov. 20, 1980     |   | 1.0 hrs.  |   |  |   |
| Dec. 4            |   | 2.3   |   |  |   |
| Dec. 10<br>Ian 6  |   |   |   | 2-0  |   |
| Feb. 5            |   |   |   | 1.0  |   |
| Feb. 9            |   |   |   | =1.0   |   |
| Feb. 10           |   |   |   | 2.0  |   |
| Feb. 11           |   | 1.5   | and a second second<br>Second second   |  |   |
| Feb. 23           |   | -0.5  |   |  |   |
| Mar. 5            |   | 1.5   |   |  |   |
| Mar. 6            |   | 2.0   |   |  |   |
| Mar. 6 invoice    | ≥ (#131)  | 10.0 hrs.   | . = 1.25 days   | 6.5 hrs.   | = 0.81 days   |
| Mar. 9            |   | 4.0 hrs.  |   |  |   |
| Mar. 10           |   | 5.0   |   |  |   |
| Mar. 11           |   | 4.5   |   |  |   |
| Mar. 12           |   | 5.0   | <ul> <li>A second se</li></ul> |  |   |
| Mar. 13           |   | 6.5   |   |  |   |
| Mar. 14           |   | 2.0   |   |  |   |
| Mar. 16           |   | 4.0 共成的   |   |  |   |
| Mar. 17           | in the second | 4.0   |   |  |   |
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| Mar. 20           |   | 8.0   |   | - A set of the set |   |
| Mar. 23           |   | 6.0   |   |  |   |
| Mar. 24           | n far an  | 6.5   |   |  |   |
| Mar. 25           |   | 11.0  |   |  |   |
| Mar. 26           |   | 3.5   |   | are di <b>C.I</b> . Addeles u.<br>Merako en esta   |   |
| Mar. 27           |   | 8.0   |   | 0.5  |   |
| Mar 20            |   | 4 5   |   |  |   |
| Mar 30            |   | 8.0   |   | 1.0  |   |
|                   |   |   | 40 40 1   |  | - 0 20 3  |
| Mar. 31 invoice   | e (#132)  | 105.0 hrs.  | • = 13.13 days  | J.U Nrs.   | = 0.38 days.  |
|                   |   | (charged  | TO.JO UAYSI   | · · · ·  |   |
| Apr. 1            |   |   | • •   | 6.5 hrs.   |   |
| Apr. 2            |   |   |   | 7.0  |   |
| Apr. 3            |   | jt, ⊁ž  |   | 4.0  | an an an the second and a second s<br>A second secon   |
| Apr. 4            |   |   |   | 5 n  |   |
| Apr. b            |   | •   |   | 20   |   |
| Apr. /            |   |   | en de la companya de<br>La companya de la comp<br>La companya de la comp  | 2.5  |   |
| API. O            |   |   |   |  |   |
| Apr. 8 invoice    | e (#135)  |   |   | 34.0 hrs.  | = 4.25 days   |
|                   |   | aa<br>Seetaat gaa   |   |  |   |
|                   |   |   |   |  |   |

1138 Gilmer Drive, Salt Lake City, Utah 84105 / Telephone (801) 583-3366

## **Robert W. Bamford**

1138 Gilmer Drive, Salt Lake City, Utah 84105

Ph.D., Geology (Economic Geology and Geochemistry), Stanford University, 1970, and B.Sc., Chemical Engineering, University of Washington, 1959.

Consultant in resource exploration, 1977 through present.

Project Manager, Geochemical Research, Earth Science Laboratory, University of Utah Research Institute, 1977 through 1979.

Project Manager, Sulfide System Research, Kennecott Exploration Services, 1974 through 1976.

Technical advisor to Kennecott's exploration programs in the Southwest Pacific area, 1972 and 1973.

Chief Site Geologist, Kennecott (Australia) Ok Tedi Project, Papua New Guinea, 1971 Exploration/research geologist, Kennecott Exploration Services, 1970

Member SEG, GRC, AEG, GSA, MSA, and AIME



I, ROBERT M. CANN, of the City of Vancouver, Province of British Columbia, hereby certify:

- 1. That I am a geologist residing at 4647 W. 15th Avenue, Vancouver, B.C.
- 2. That I am a graduate of the University of British Columbia with a B.Sc. degree in Geology in 1976 and a M.Sc. degree in Geology in 1979.
- 3. That I have practised my profession for six field seasons.
- That I personally supervised the rock sampling on the WHIT Claims.

Signed

Date May 9, 1981