GEOCHEMISTRY

OF THE

SB CLAIM

NANAIMO MINING DIVISION

N.T.S. 92 F/7E

Latitude 49°20'N Longitude 124°43'W

CLAIM OWNER AND OPERATOR

ASARCO EXPLORATION COMPANY OF CANADA LIMITED

JANUARY 26, 1983 D. M. FLETCHER

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SUMMARY

The SB Claim was staked to cover a sequence of Sicker Volcanics hosting antimony sulfide mineralization that may be auriferous.

A soil grid was established over the claim and approximately 275 samples were taken and analysed for 32 elements.

Geochemical response for pathfinder elements associated with gold mineralization is not overly encouraging, however detailed prospecting of the claim and mapping is warranted.

LOCATION AND ACCESS

The SB claim is situated on the south side of Horne Lake in the Alberni Land District. The property is positioned in the Nanaimo Mining Division (N.T.S. 92F/7E) and can be reached by logging roads extending from Port Alberni a distance of approximately 15.0 kilometers.

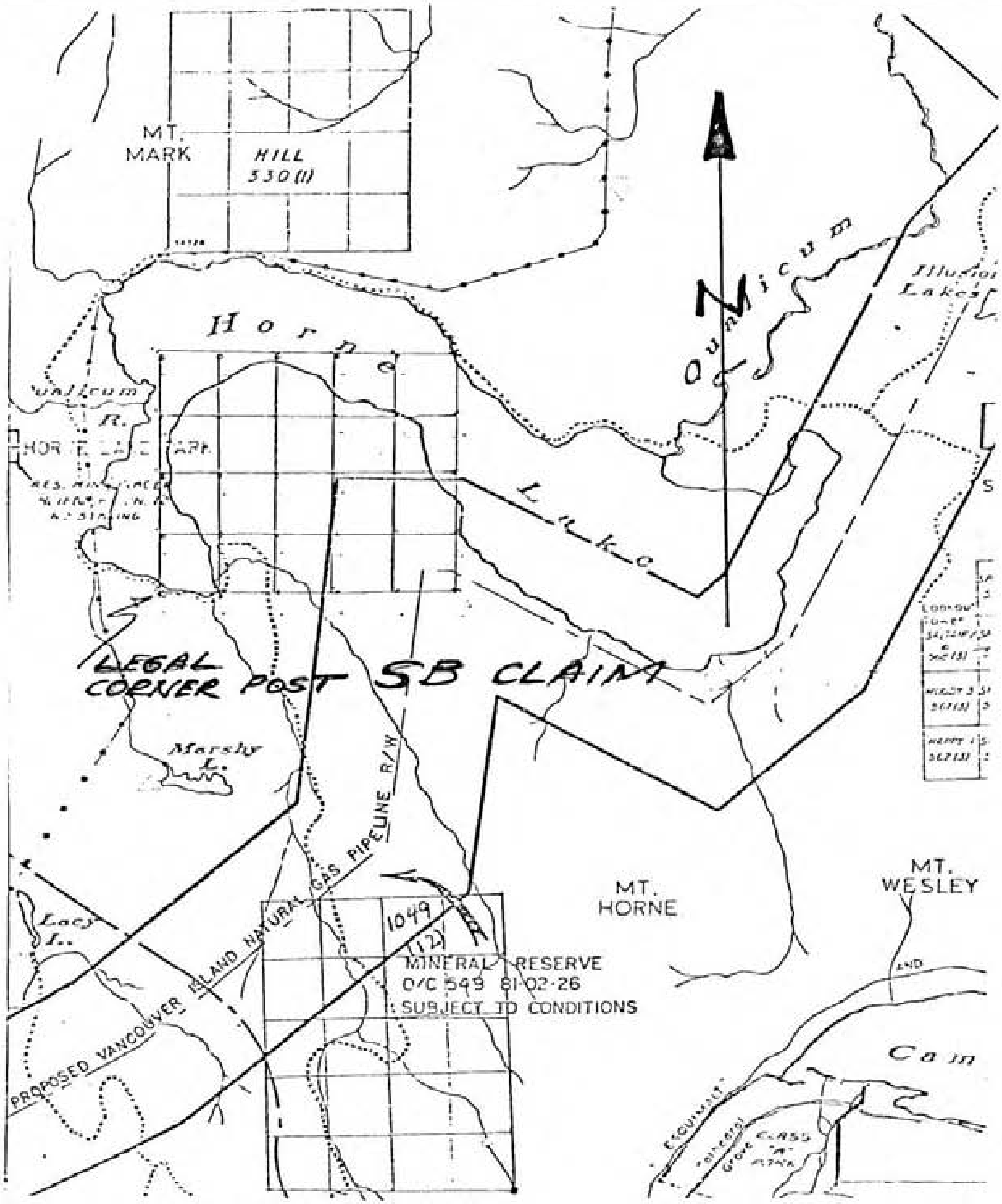
CLAIMS AND OWNERSHIP

The SB claim consisting of 20 units is held and operated by Asarco Exploration Company of Canada Limited. The claim was staked by Asarco on May 11, 1982 and is held under record number 1173 issued May 13, 1982. See Attachment "A".

GENERAL SETTING

The SB Property lies astride a sequence of Sicker volcanics consisting of volcanic breccia, tuff, argillite and andesite porphyry. Minor antimony mineralization is hosted within the Sicker volcanics.

ATTACHMENT A



ASARCO Vancouver

LOCATION
SB CLAIM

Drawn by	Date	N.T.S.	SCALE
D.M.F.	JAN '83	92F/7E	1:50,000

A major north-south trending fault bisects the claim. The claim encompasses a northwest trending knoll that rises approximately 400 feet above Horne Lake. The area was logged and is now covered with a veneer of debris interwoven with thick clustered salal.

HISTORY

Two stibnite-quartz veins with arsenopyrite were tested by a short adit driven in 1939. Minfile reports that small amounts of copper, lead, zinc, arsenic, gold and silver show in assay.

Asarco's geochemical sampling of the property was executed primarily to test for lateral extent of sulfide bodies carrying precious metal values by utilizing pathfinder geochemical elements normally associated with gold mineralization.

GEOCHEMICAL FIELD PROCEDURE

An enlargement at a scale of 1:10,000 was prepared utilizing a standard 1:50,000 topographic map with contour intervals at 100 foot elevations.

A soil survey grid was established by topo-chain and compass. Approximately 275 soil samples were taken at 50 meter intervals with variable line spacing up to 550 meters. See Attachment "B". Each soil sample was taken at a depth of 15-20 centimeters, bagged, packaged and dispatched to Acme Analytical Laboratories in Vancouver for analyses.

Sb Cu/AM

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS, VANCOUVER B.C. PH:253-3158 TELEX:04-53124

ICP GEOCHEMICAL ANALYSIS

A .500 GRAM SAMPLE IS DIGESTED WITH 3 ML OF 3:1:3 HCL TO HNO3 TO H2O AT 90 DEG.C. FOR 1 HOUR. THE SAMPLE IS DILUTED TO 10 MLS WITH WATER.
THIS LEACH IS PARTIAL FOR: Ca,P,Mg,Al,Ti,La,Na,K,W,Ba,Si,Sr,Cr AND B. Au DETECTION 3 ppm.
AU!! ANALYSIS FROM 10 GRAM FA+AA. AG! ANALYSIS BY AA. HG! ANALYSIS BY FLAMELESS AA FROM .500 GRAM SAMPLE. SAMPLE TYPE - SOIL

DATE RECEIVED AUG 30 1982 DATE REPORTS MAILED Sept 5/82 ASSAYER D. Toye DEAN TOYE, CERTIFIED B.C. ASSAYER

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SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au!! ppb	Hg! ppb	Ag! ppm
S2020E	1	66	6	38	.2	25	12	484	3.80	7	2	ND	2	13	1	2	2	118	.54	.04	6	52	.66	206	.25	4	3.00	.02	.04	2	1	110	.1
S2040E	1	69	3	42	.3	26	12	363	4.06	8	2	ND	2	10	1	2	2	128	.42	.03	5	56	.67	94	.29	4	3.15	.02	.03	2	2	55	.2
S2060E	1	60	5	39	.3	26	12	316	4.04	13	2	ND	2	10	1	2	2	126	.44	.03	6	53	.64	91	.26	4	3.21	.01	.03	2	1	90	.3
S2080E	1	73	8	33	.3	22	12	481	4.10	8	2	ND	2	16	1	2	2	105	.66	.03	9	66	.45	172	.21	4	3.31	.02	.03	2	1	55	.2
S2100E	1	61	6	39	.2	24	12	526	3.73	4	2	ND	2	11	1	2	2	114	.46	.05	6	50	.63	96	.23	3	3.19	.01	.03	2	5	50	.1
S2120E	1	61	7	44	.3	25	12	697	3.90	8	2	ND	2	11	1	2	2	118	.47	.07	5	51	.61	93	.23	4	3.21	.01	.04	2	3	60	.2
S2140E	1	38	7	40	.3	20	11	846	3.35	6	2	ND	2	11	1	2	2	100	.39	.05	4	46	.40	76	.21	2	2.92	.01	.03	2	2	65	.2
S2160E	1	61	7	36	.2	22	11	534	3.23	7	2	ND	2	15	1	2	2	99	.40	.05	5	43	.68	103	.20	4	2.34	.01	.04	2	3	55	.1
S2180E	1	61	8	39	.3	24	11	465	3.56	9	2	ND	2	12	1	2	2	110	.44	.05	5	50	.64	94	.27	3	3.23	.02	.05	2	2	100	.1
S2200E	1	42	8	49	.2	18	10	628	3.50	2	2	ND	2	8	1	2	2	98	.34	.06	3	43	.45	82	.14	3	2.79	.01	.03	2	1	40	.1
S2220E	1	26	13	59	.2	19	13	1975	3.96	3	2	ND	2	14	1	2	2	60	.78	.10	3	27	1.00	194	.01	3	2.45	.02	.06	2	2	55	.1
S2240E	1	27	9	48	.1	17	8	2211	2.96	3	2	ND	2	9	1	2	2	90	.35	.09	3	43	.35	114	.18	3	3.30	.01	.03	2	1	50	.1
S2260E	1	56	11	45	.3	26	12	709	3.68	6	2	ND	2	11	1	2	2	105	.44	.08	4	50	.77	85	.17	3	3.05	.01	.03	2	76	70	.2
S2280E	1	51	10	44	.2	24	11	606	3.65	5	2	ND	2	10	1	2	2	107	.42	.07	4	47	.66	86	.19	3	2.99	.01	.04	2	4	60	.1
S2300E	1	44	13	56	.1	18	11	2260	3.49	2	2	ND	2	10	1	2	2	94	.37	.09	4	41	.46	153	.13	2	3.16	.01	.04	2	1	60	.2
S2320E	1	27	10	50	.2	14	9	1439	3.04	2	2	ND	2	11	1	2	2	78	.34	.06	4	33	.47	145	.08	2	2.58	.01	.04	2	1	40	.3
S2340E	1	34	13	55	.2	35	13	1314	3.99	2	2	ND	2	17	1	2	2	96	.32	.05	5	50	.95	184	.06	3	3.11	.01	.05	2	1	65	.2
S2360E	1	291	18	58	.3	15	13	1436	5.77	8	2	ND	2	13	1	2	2	103	.26	.10	7	41	.82	151	.05	5	3.77	.01	.06	2	23	70	.4
S2380E	1	58	7	41	.2	27	12	262	3.97	10	2	ND	2	8	1	2	2	124	.33	.04	6	61	.64	85	.23	3	4.09	.01	.04	2	2	70	.2
S2400E	1	63	7	42	.2	29	13	384	3.92	6	2	ND	2	10	1	2	2	121	.37	.05	6	61	.71	119	.23	4	3.79	.01	.04	2	4	75	.3
S2420E	1	53	9	42	.2	26	12	410	3.67	8	2	ND	2	9	1	2	2	111	.38	.05	5	52	.64	98	.21	3	3.34	.01	.03	2	2	70	.2
S2440E	1	50	6	43	.3	25	11	472	3.60	11	2	ND	2	10	1	2	2	109	.37	.05	5	53	.59	105	.20	3	3.36	.01	.03	2	2	55	.1
S2460E	1	51	8	47	.2	26	12	579	3.61	9	2	ND	2	10	1	2	2	108	.35	.06	5	54	.58	116	.20	2	3.36	.01	.03	2	2	85	.2
S2480E	1	46	11	75	.2	19	16	1892	3.46	7	2	ND	2	12	1	2	2	79	.42	.13	5	42	.57	200	.12	2	2.93	.01	.04	2	2	60	.2
S2500E	1	63	10	50	.2	26	13	730	3.92	12	2	ND	2	14	1	2	2	107	.56	.09	6	52	.78	132	.18	3	3.52	.01	.04	2	3	140	.2
STD A-1	1	31	40	183	.5	35	12	994	2.83	12	2	ND	2	35	1	2	2	56	.66	.10	8	80	.78	281	.09	11	2.06	.02	.21	2	1	55	.2
S1400N	1	67	10	51	.2	33	12	353	4.55	9	2	ND	2	14	1	2	2	147	.40	.06	4	67	.54	112	.26	2	4.20	.01	.05	2	1	70	.2
S1420N	1	49	6	45	.2	27	13	570	4.07	3	2	ND	2	11	1	2	2	130	.44	.05	5	61	.57	88	.21	2	3.44	.01	.04	2	2	60	.1
S1440N	1	39	8	44	.2	22	11	927	3.30	5	2	ND	2	19	1	2	2	100	.61	.04	5	50	.55	108	.19	2	2.53	.02	.04	2	1	70	.2
S1460N	1	67	8	46	.2	26	14	620	3.99	8	2	ND	2	18	1	2	2	120	.69	.04	5	60	.73	111	.20	4	2.84	.02	.05	2	6	55	.1
S1480N	1	75	10	49	.2	29	16	774	4.30	9	2	ND	2	20	1	2	2	132	.72	.05	6	60	.79	131	.25	3	3.41	.02	.05	2	4	90	.3
S1500N	1	85	8	51	.2	31	17	720	4.43	11	2	ND	2	22	1	2	2	133	.99	.05	6	59	.89	157	.26	4	3.29	.02	.04	2	2	110	.2
S1520N	1	62	10	59	.2	31	14	734	4.50	7	2	ND	2	11	1	2	2	139	.42	.05	6	64	.53	113	.25	3	4.10	.01	.05	2	1	90	.1
S1540N	1	63	6	44	.2	27	14	551	4.06	5	2	ND	2	16	1	2	2	124	.54	.03	7	62	.72	208	.19	3	3.39	.01	.05	2	5	60	.1
S1560N	1	91	11	70	.3	26	15	2707	4.51	8	2	ND	2	27	1	2	2	111	.61	.12	8	57	.69	344	.15	2	3.81	.02	.06	2	10	95	.4
S1580N	1	123	11	46	.3	27	17	1103	5.17	15	2	ND	2	14	1	7	2	148	.64	.04	13	69	1.26	183	.05	5	3.33	.02	.05	2	15	95	.4
S1600N	1	77	12	36	.2	29	15	1419	4.85	4	2	ND	2	23	1	2	2	113	1.17	.03	8	79	.48	348	.19	4	3.55	.03	.04	2	2	65	.2
S1620N	1	132	9	32	.4	28	14	225	5.13	15	2	ND	2	10	1	2	2	172	.44	.03	7	75	.57	65	.31	3	4.09	.01	.04	2	8	100	.4

ASARCO EXPLORATION PROJECT # SB PROSPECT FILE # 82-0984

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb	Hg* ppb	Ag* ppm
[illegible]	1	87	10	47	.2	32	15	2625	5.04	7	2	ND	2	14	1	2	2	119	.52	.03	13	68	.33	353	.22	4	3.83	.02	.04	2	2	90	.1
[illegible]	1	97	10	34	.2	35	19	402	6.68	11	2	ND	2	17	1	2	2	177	.44	.03	3	77	.46	205	.30	2	4.66	.02	.04	2	7	70	.1
[illegible]	1	48	9	36	.2	21	10	495	2.96	11	2	ND	2	13	1	2	2	85	.79	.03	3	39	.68	83	.18	4	2.16	.02	.02	2	2	60	.1
[illegible]	1	60	8	45	.2	21	11	838	3.82	13	2	ND	2	13	1	2	2	118	.63	.09	4	45	.62	90	.20	4	3.10	.02	.03	2	1	100	.1
[illegible]	1	60	10	45	.2	25	11	623	3.62	10	2	ND	2	12	1	2	2	118	.55	.05	4	50	.72	86	.22	5	2.83	.02	.03	2	4	85	.1
[illegible]	1	59	10	45	.2	24	12	558	4.01	7	2	ND	2	13	1	2	2	124	.61	.05	4	48	.76	84	.23	4	2.77	.02	.04	2	80	65	.1
[illegible]	1	56	9	44	.3	25	12	642	3.92	15	2	ND	2	12	1	2	2	122	.56	.05	5	50	.70	98	.23	4	3.17	.02	.04	2	2	90	.1
[illegible]	1	60	8	40	.2	22	11	601	3.62	11	2	ND	2	13	1	2	2	114	.53	.05	4	44	.64	102	.21	4	2.78	.01	.04	2	3	85	.1
[illegible]	1	65	8	43	.2	24	11	541	3.82	10	2	ND	2	12	1	2	2	119	.47	.05	5	48	.64	102	.23	4	2.97	.01	.04	2	1	75	.1
[illegible]	1	31	39	160	.5	34	12	933	2.90	12	2	ND	2	36	1	2	2	56	.65	.10	8	79	.78	281	.09	11	2.04	.02	.21	2	1	55	.4
[illegible]	1	46	11	43	.2	24	12	759	4.23	10	2	ND	2	14	1	2	2	122	.55	.04	6	55	.56	166	.21	3	3.28	.02	.03	2	1	50	.1
[illegible]	1	33	9	55	.1	20	9	440	4.55	4	2	ND	2	10	1	2	2	138	.40	.07	2	52	.38	111	.25	6	3.93	.01	.03	2	1	30	.1
[illegible]	1	13	11	72	.2	16	16	3124	3.62	2	2	ND	2	15	1	2	2	85	.50	.04	7	47	1.39	343	.01	6	2.72	.02	.07	2	1	80	.1
[illegible]	1	47	10	62	.1	15	13	1398	5.82	3	2	ND	2	13	1	2	2	99	.35	.09	8	34	.61	220	.02	4	2.21	.02	.05	2	4	50	.1
[illegible]	1	12	11	42	.2	11	11	3001	2.68	4	2	ND	2	14	1	2	2	84	.45	.04	4	31	.42	281	.03	4	1.77	.02	.04	2	1	60	.1
[illegible]	1	23	9	49	.1	20	10	501	4.34	8	2	ND	2	12	1	2	2	125	.40	.05	3	51	.51	166	.16	4	3.52	.01	.03	2	1	40	.1
[illegible]	1	6	7	43	.2	5	7	3155	2.58	2	2	ND	2	12	1	2	2	60	.31	.04	6	17	.33	212	.01	3	1.29	.01	.06	2	1	50	.1
[illegible]	1	59	8	46	.2	27	11	701	4.45	16	2	ND	2	12	1	2	2	133	.45	.11	4	60	.68	72	.23	8	4.23	.01	.05	2	2	80	.1
[illegible]	1	31	6	33	.1	13	6	573	4.14	7	2	ND	2	11	1	2	2	113	.31	.07	3	43	.34	55	.13	4	2.70	.01	.02	2	3	60	.1
[illegible]	1	9	13	66	.2	8	9	8000	3.27	3	2	ND	2	18	1	2	2	81	.27	.10	5	24	.54	237	.04	5	1.78	.01	.03	2	1	80	.1
[illegible]	1	72	10	72	.2	22	12	946	4.30	10	2	ND	2	10	1	2	2	102	.37	.18	4	46	.67	122	.12	4	2.97	.01	.04	2	4	80	.1
[illegible]	1	50	10	40	.1	15	7	610	4.92	14	2	ND	2	8	1	2	2	126	.30	.28	3	49	.50	68	.15	14	3.22	.01	.03	2	1	110	.1
[illegible]	1	54	8	76	.2	14	7	482	4.55	7	2	ND	2	8	1	2	2	114	.21	.19	4	45	.24	62	.15	4	3.13	.01	.03	2	1	60	.1
[illegible]	1	56	9	40	.2	22	11	521	3.72	12	2	ND	2	9	1	2	2	108	.39	.07	4	47	.65	73	.20	4	3.14	.01	.02	2	3	120	.1
[illegible]	1	62	11	46	.2	22	10	546	4.19	12	2	ND	2	10	1	2	2	120	.37	.09	4	55	.60	78	.21	4	3.65	.02	.03	2	1	100	.1

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS, VANCOUVER B.C. PH:253-3158 TELEX:04-53124

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THIS LEACH IS PARTIAL FOR: Ca,P,Mg,Al,Ti,La,Na,K,W,Ba,Si,Sr,Cr AND B. Au DETECTION 3 ppm.
AU** ANALYSIS FROM 10 GRAM FA+AA. AG* ANALYSIS BY AA. HG* ANALYSIS BY FLAMELESS AA FROM .500 GRAM SAMPLE. SAMPLE TYPE - SOIL

DATE RECEIVED OCT 1 1982 DATE REPORTS MAILED Oct 14/82 ASSAYER D. Toye DEAN TOYE, CERTIFIED B.C. ASSAYER

ASARCO EXPLORATION PROJECT # VILLALTA-GRID NO SB-LINE NO FILE # 82-1276 PAGE # 1

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb	Hg* ppb	Ag* ppm
SB1+0E	1	34	6	58	.1	31	15	2989	3.80	31	2	ND	2	25	1	2	2	107	.42	.04	6	51	.57	288	.10	2	2.36	.01	.04	2	2	120	.1
SB1+25E	1	37	2	55	.1	27	12	891	3.67	10	2	ND	2	21	2	2	2	108	.63	.05	5	42	.50	131	.24	2	3.01	.02	.03	2	1	85	.1
SB1+37.5E	1	40	4	51	.2	31	12	662	3.91	5	2	ND	2	14	2	3	2	126	.47	.03	4	56	.56	105	.27	2	3.16	.02	.02	2	2	60	.1
SB1+50E	1	22	5	59	.1	22	12	1660	4.13	3	2	ND	2	15	2	2	2	131	.50	.05	4	48	.37	110	.29	2	2.29	.02	.02	2	1	50	.1
SB1+62.5E	1	34	6	40	.2	28	13	637	4.00	2	2	ND	2	22	2	2	2	132	.65	.03	5	58	.47	128	.25	2	3.42	.02	.02	2	2	70	.1
SB1+75E	1	26	7	57	.1	23	13	3406	4.00	2	2	ND	2	29	2	2	2	120	.75	.05	5	45	.43	286	.22	2	2.08	.02	.02	2	1	80	.1
SB1+87.5E	1	38	5	55	.2	21	11	1185	3.82	33	2	ND	2	16	2	2	2	113	.45	.13	4	44	.31	164	.20	2	2.78	.01	.03	2	3	140	.1
SB1+100E	1	47	6	125	.3	24	16	5203	4.04	78	2	ND	2	23	2	4	2	94	.65	.22	8	40	.33	277	.20	2	2.93	.02	.03	2	2	100	.3
SB1+112.5E	1	58	3	52	.2	32	14	748	3.91	7	2	ND	2	12	2	10	2	120	.47	.07	6	53	.57	108	.24	2	3.89	.01	.03	2	54	120	.1
SB1+125E	1	35	6	85	.2	30	14	1870	4.57	16	2	ND	2	13	2	2	2	106	.43	.09	6	43	.37	376	.15	2	2.56	.01	.05	2	2	110	.3
SB1+137.5E	1	17	7	50	.2	26	14	4301	3.85	60	2	ND	2	19	1	2	2	99	.57	.05	6	39	.25	264	.17	2	1.74	.01	.03	2	1	130	.1
SB1+150E	1	39	3	29	.1	18	9	560	3.09	2	2	ND	2	15	1	2	2	103	.68	.04	5	30	.49	66	.24	2	2.47	.02	.02	2	1	60	.1
SB1+162.5E	1	49	5	29	.3	27	11	247	3.62	5	2	ND	2	16	2	2	2	124	.44	.02	6	63	.49	147	.29	2	3.98	.02	.03	2	2	100	.1
SB1+175E	1	15	4	33	.1	15	9	963	3.39	2	2	ND	2	20	1	2	2	107	.55	.02	4	32	.25	95	.22	2	1.57	.02	.02	2	1	50	.1
SB1+187.5E	1	30	5	60	.2	24	11	947	4.03	4	2	ND	2	17	2	2	2	126	.54	.04	4	37	.43	106	.28	2	2.39	.02	.03	2	1	70	.1
SB1+200E	1	26	6	47	.2	14	11	822	4.31	2	2	ND	2	12	2	2	2	141	.37	.03	5	34	.20	72	.30	2	1.86	.01	.02	2	1	60	.1
SB2+0W	1	39	4	25	.3	14	6	192	2.00	2	2	ND	2	25	1	2	2	68	1.03	.06	6	34	.49	92	.17	2	2.35	.02	.03	2	3	80	.1
SB2+50W	1	32	7	61	.1	16	11	505	3.99	2	2	ND	2	14	2	2	2	126	.43	.04	4	31	.42	179	.25	2	2.51	.01	.02	2	3	80	.1
SB2+100W	1	26	10	44	.2	34	14	3296	2.65	4	2	ND	2	30	1	2	2	59	1.16	.06	4	27	.71	384	.10	2	1.98	.02	.08	2	2	60	.1
SB2+150W	1	25	6	56	.1	15	11	1006	3.41	2	2	ND	2	12	1	2	2	97	.34	.10	4	33	.32	163	.18	2	2.38	.01	.03	2	1	50	.1
SB2+200W	1	10	9	16	.1	5	4	220	1.85	2	2	ND	2	19	1	2	2	62	.41	.05	4	10	.18	206	.04	2	1.62	.01	.07	2	1	50	.1
SB2+250W	1	13	8	41	.2	10	7	718	3.53	2	2	ND	2	16	1	2	2	112	.45	.05	4	28	.29	181	.16	2	2.03	.01	.03	2	2	60	.1
SB2+300W	1	42	8	80	.3	28	14	469	4.54	6	2	ND	2	15	2	2	2	116	.46	.07	7	47	.56	164	.25	2	3.80	.02	.04	2	2	130	.1
SB2+350W	1	65	12	55	.3	36	16	1064	5.65	38	2	ND	2	12	2	2	2	158	.39	.06	9	84	.82	172	.14	2	3.38	.01	.03	2	1	80	.1
SB2+400W	1	16	5	55	.1	10	11	1838	3.27	2	2	ND	2	17	1	2	2	91	.51	.06	7	23	.27	192	.09	2	1.70	.02	.05	2	2	70	.1
SB2+450W	1	53	7	497	.2	23	13	2420	3.98	3	2	ND	2	31	5	2	2	99	1.11	.06	12	39	.43	285	.20	2	3.08	.02	.03	2	9	360	.3
SB2+500W	1	33	8	71	.2	14	10	401	6.17	2	2	ND	2	14	2	2	2	156	.32	.17	4	36	.33	78	.23	2	3.44	.01	.02	2	6	70	.1
SB2+550W	1	26	8	73	.1	19	14	1646	2.86	2	2	ND	2	24	1	2	2	89	.46	.08	4	35	.55	171	.16	2	2.28	.01	.05	2	1	120	.1
SB2+600W	1	26	5	45	.2	18	10	782	3.57	2	2	ND	2	14	2	2	2	111	.38	.09	4	35	.33	113	.23	2	3.13	.01	.02	2	1	40	.1
SB2+650W	1	38	3	47	.1	22	10	684	3.69	2	2	ND	2	12	2	2	2	114	.41	.07	4	39	.41	118	.23	2	2.95	.01	.02	2	1	40	.1
SB2+700W	1	47	6	39	.2	24	13	884	4.74	2	2	ND	2	18	2	2	2	128	.48	.04	10	44	.44	202	.16	2	3.24	.01	.04	2	8	1600	.2
SB2+750W	1	46	4	57	.1	29	14	1129	4.56	2	3	ND	2	14	2	2	2	135	.47	.04	6	53	.46	158	.26	2	3.84	.01	.03	2	5	60	.1
SB2+800W	1	51	6	45	.3	28	15	480	4.83	2	2	ND	2	15	2	2	2	137	.50	.03	9	72	.41	131	.27	2	4.41	.02	.02	2	3	160	.2
SB2+850W	1	30	6	58	.2	22	14	1694	4.34	2	2	ND	2	25	2	5	2	139	.75	.04	6	42	.37	169	.25	2	2.60	.02	.03	2	2	110	.1
SB2+900W	1	42	3	56	.1	29	13	942	4.11	2	2	ND	2	16	2	2	2	131	.61	.05	5	47	.49	151	.26	2	3.66	.02	.03	2	2	65	.1
SB2+950W	1	18	3	48	.1	16	12	1233	3.90	2	2	ND	2	21	2	2	2	129	.59	.03	3	32	.26	98	.33	2	1.73	.02	.01	2	1	70	.1
SB2+1000W	1	36	5	43	.2	24	11	876	3.47	16	2	ND	2	15	1	2	2	112	.61	.04	4	34	.45	144	.25	2	2.62	.02	.02	2	2	110	.1
STD A-1	1	31	39	187	.4	36	13	1026	2.73	10	2	ND	2	34	2	2	2	55	.57	.10	8	72	.76	269	.08	4	1.91	.02	.20	2	1	55	.3

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb	Hg* ppb	Ag* ppm
SB2+1050W	1	57	7	65	.2	48	21	2530	6.20	55	3	ND	2	18	2	6	2	133	.22	.06	3	85	.53	300	.01	4	2.11	.01	.10	2	4	150	.1
SB2+1100W	1	31	8	35	.2	25	12	363	4.52	5	3	ND	2	13	2	7	2	121	.31	.04	5	45	.32	86	.20	3	3.00	.01	.02	2	1	80	.1
SB2+1150W	1	29	4	27	.2	17	8	184	2.14	10	2	ND	2	20	1	5	2	61	.79	.02	4	33	.70	73	.13	4	1.62	.02	.02	2	3	350	.1
SB3+0W	1	39	2	35	.2	22	11	271	2.51	3	2	ND	2	15	1	2	2	83	.73	.03	3	33	.85	78	.22	3	1.72	.02	.02	2	2	40	.1
SB3+50W	1	25	3	31	.2	19	8	229	2.49	2	2	ND	2	19	1	2	2	74	.88	.02	3	31	.76	74	.20	3	1.62	.04	.03	2	1	40	.1
SB3+100W	1	17	6	25	.2	14	8	195	3.71	2	3	ND	2	11	2	2	2	130	.35	.01	3	29	.35	106	.23	2	1.80	.01	.02	2	1	60	.1
SB3+150W	1	38	5	40	.2	21	11	653	3.74	2	2	ND	2	11	2	2	2	116	.42	.04	3	33	.49	99	.24	2	2.38	.01	.03	2	2	50	.1
SB3+200W	1	35	8	53	.2	24	11	838	3.45	2	3	ND	2	16	2	2	2	92	.83	.05	6	35	.75	164	.23	2	2.29	.02	.03	2	3	70	.1
SB3+250W	1	25	11	51	.3	17	10	1093	3.23	2	2	ND	2	15	1	2	2	94	.74	.04	4	29	.39	172	.18	2	2.18	.01	.02	2	1	60	.1
SB3+300W	1	25	22	131	.3	14	15	3213	3.23	2	3	ND	2	9	2	2	2	76	.36	.11	7	22	.26	254	.14	3	1.96	.01	.03	2	65	90	.1
SB3+350W	1	20	21	99	.4	13	12	1841	3.59	4	2	ND	2	13	2	2	2	103	.45	.05	5	30	.39	219	.15	3	1.94	.01	.03	2	1	65	.1
SB3+400W	1	30	20	238	.5	12	16	10235	2.22	3	2	ND	4	34	3	2	3	47	1.33	.08	9	15	.20	1157	.05	3	1.51	.01	.06	2	1	130	.4
SB3+450W	1	40	7	68	.2	19	11	998	3.74	4	2	ND	2	12	2	2	2	106	.43	.19	2	32	.45	171	.18	3	2.24	.01	.03	2	2	35	.1
SB3+500W	1	75	12	61	.3	19	13	5433	3.33	2	2	ND	2	32	2	2	2	81	1.40	.09	20	31	.38	417	.15	5	2.36	.01	.04	2	1	90	.4
SB3+550W	1	27	16	87	.2	13	15	6015	3.71	3	2	ND	2	14	1	2	2	84	.48	.12	8	26	.31	237	.12	2	1.90	.01	.04	2	1	60	.2
SB3+600W	1	13	6	64	.2	10	10	1944	3.41	7	2	ND	2	16	1	2	2	99	.39	.05	3	27	.28	162	.16	2	1.49	.01	.02	2	1	60	.1
SB3+650W	1	13	6	30	.2	8	4	205	2.63	2	2	ND	2	13	1	2	2	82	.33	.04	3	20	.22	60	.13	2	1.14	.01	.02	2	1	20	.1
SB3+700W	1	28	7	31	.1	12	6	423	3.80	2	2	ND	2	10	2	2	2	115	.30	.07	3	33	.32	65	.19	2	2.55	.01	.02	2	2	80	.1
SB3+750W	1	11	6	35	.1	5	5	631	2.04	3	2	ND	2	12	1	2	2	56	.32	.05	4	16	.16	61	.10	2	1.03	.01	.03	2	13	40	.1
SB3+800W	1	24	7	50	.1	14	8	377	3.53	2	3	ND	2	11	2	2	2	105	.34	.09	3	29	.36	88	.17	4	2.17	.01	.03	2	1	120	.1
SB3+850W	1	57	5	33	.2	22	9	560	2.93	2	2	ND	2	15	1	2	2	80	.68	.03	8	32	.62	102	.20	3	2.29	.02	.02	2	2	40	.1
SB3+900W	1	21	5	70	.1	15	9	1187	3.42	2	3	ND	2	11	1	2	2	86	.33	.14	4	29	.21	176	.20	2	2.02	.01	.02	2	2	60	.1
SB3+950W	1	12	7	38	.2	11	8	738	3.15	2	2	ND	2	13	1	2	2	88	.41	.07	3	24	.24	80	.20	2	1.36	.01	.02	2	1	40	.1
SB3+1000W	1	49	8	45	.2	21	11	1942	3.54	3	2	ND	2	15	2	2	2	89	.57	.06	6	33	.54	152	.20	3	2.57	.02	.03	2	35	180	.1
SB3+1050W	1	21	6	92	.2	16	13	2616	3.49	2	2	ND	2	16	1	2	2	78	.50	.10	7	46	.50	280	.05	3	2.29	.01	.04	2	2	75	.1
SB3+1100W	1	25	5	55	.2	9	9	914	3.45	2	2	ND	2	10	1	2	2	51	.14	.06	3	14	.20	254	.01	4	1.52	.02	.05	2	2	40	.1
SB3+1150W	1	38	7	39	.3	24	11	598	3.68	2	2	ND	2	11	2	2	2	118	.38	.03	4	40	.40	114	.24	2	3.13	.01	.02	2	1	60	.1
SB3+1200W	1	74	7	59	.1	29	14	1036	4.22	2	2	ND	2	12	2	2	2	126	.43	.09	6	47	.63	148	.21	3	3.82	.01	.04	2	3	80	.1
SB3+1250W	1	46	7	96	.1	25	12	1932	3.59	2	2	ND	2	11	1	2	2	97	.34	.23	3	37	.39	168	.19	2	2.98	.01	.03	2	2	45	.1
SB3+1300W	1	18	9	74	.1	27	23	4807	4.65	189	2	ND	2	25	2	29	2	59	.59	.10	6	27	.11	333	.01	4	1.01	.01	.11	2	1	180	.1
SB3+1350W	1	30	8	69	.1	22	12	1182	3.59	2	2	ND	2	15	1	2	2	94	.44	.15	4	36	.54	146	.14	2	2.48	.01	.04	2	1	40	.1
SB3+1400W	1	46	9	51	.2	28	11	1158	3.99	8	2	ND	2	18	2	2	2	112	.40	.12	5	41	.51	183	.19	3	2.92	.01	.04	2	1	55	.1
SB3+1450W	1	16	6	47	.2	17	9	389	2.95	2	2	ND	2	18	1	2	2	87	.41	.02	4	34	.42	97	.12	2	1.93	.01	.02	2	1	30	.1
SB3+1500W	1	54	6	34	.3	28	11	281	3.03	2	2	ND	2	34	1	2	2	95	1.07	.04	10	49	.79	108	.15	4	2.85	.02	.02	2	2	100	.1
SB4+0W	1	30	7	24	.1	17	7	175	1.79	2	2	ND	2	12	1	2	2	59	.44	.06	7	35	.55	40	.15	2	3.90	.02	.01	2	735	60	.1
SB4+50W	1	25	11	31	.1	10	10	235	4.98	2	3	2	2	14	2	2	2	129	.35	.03	4	32	.16	111	.20	2	4.07	.01	.02	2	3	60	.1
SB4+100W	1	25	8	56	.2	19	13	1285	3.54	3	2	ND	2	13	1	2	2	109	.45	.06	4	33	.37	168	.23	4	2.23	.01	.02	2	1	65	.1
STD A-1	1	31	40	182	.4	35	12	1013	2.70	9	2	ND	2	35	2	2	2	55	.56	.10	8	72	.76	275	.08	7	1.94	.01	.20	2	1	50	.3

ASARCO EXPLORATION PROJECT # VILLALTA-GRID NO SB-LINE NO FILE # 82-1276

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb	Hg* ppb	Ag* ppm
SE4+150M	1	16	9	76	.1	17	11	1022	4.55	5	2	ND	2	12	1	2	3	94	.39	.47	4	56	.38	104	.16	2	2.48	.01	.03	2	5	90	.3
SE4+200M	1	42	5	58	.1	27	13	682	4.40	7	2	ND	2	12	2	2	2	128	.50	.10	4	43	.50	85	.26	2	3.34	.01	.02	2	2	70	.1
SE4+250M	1	25	5	85	.1	25	15	1412	4.18	2	2	ND	2	16	1	2	3	116	.62	.08	4	43	.41	145	.25	2	2.87	.01	.03	2	2	70	.3
SE4+300M	1	44	7	55	.1	21	14	1793	3.92	3	2	ND	2	21	1	2	2	107	1.26	.05	9	42	.43	119	.20	2	2.79	.01	.02	2	1	80	.4
SE4+350M	1	33	7	63	.1	18	15	704	4.92	2	2	ND	2	14	1	2	3	130	.44	.04	7	58	.31	101	.27	2	3.14	.01	.01	2	1	80	.3
SE4+400M	1	20	12	51	.1	13	10	882	3.77	2	2	ND	2	16	1	2	2	102	.53	.06	5	33	.24	100	.23	2	1.74	.02	.02	2	1	40	.3
SE4+450M	1	48	6	53	.1	21	13	675	4.61	2	2	ND	2	13	1	2	2	134	.54	.09	7	39	.39	119	.27	2	3.07	.01	.03	2	1	80	.2
SE4+500M	1	12	8	36	.1	11	8	567	3.59	2	2	ND	2	14	1	2	2	108	.47	.05	4	27	.26	148	.18	2	1.61	.01	.03	2	11	30	.3
SE4+550M	1	67	8	53	.1	23	15	1203	4.46	4	4	ND	2	26	2	2	3	134	.80	.10	5	39	.54	318	.20	2	3.62	.01	.05	2	5	110	.2
SE4+600M	1	52	11	73	.1	21	25	2681	4.12	2	3	ND	2	18	2	2	3	88	.48	.16	11	27	.28	238	.19	2	3.56	.01	.04	2	7	120	.2
SE4+650M	1	6	5	14	.1	3	2	248	.87	2	2	ND	2	37	1	2	2	32	.50	.02	3	7	.09	99	.03	2	1.14	.01	.02	2	5	30	.2
SE4+700M	1	22	6	55	.1	8	14	4578	3.07	2	2	ND	2	22	1	2	2	66	.46	.13	6	24	.37	339	.09	2	1.76	.02	.05	2	4	140	.2
SE4+750M	1	42	6	44	.1	14	8	468	4.24	2	3	ND	2	14	1	2	2	127	.42	.10	4	33	.28	131	.21	2	2.35	.01	.02	2	5	60	.3
SE4+800M	1	9	7	55	.1	7	10	620	3.74	3	2	ND	2	7	1	2	2	53	.13	.05	17	10	1.00	125	.01	2	2.12	.02	.07	2	4	40	.2
SE4+850M	1	31	9	60	.1	19	22	545	5.91	2	2	ND	2	13	2	2	2	149	.45	.09	9	40	.40	212	.23	2	3.07	.01	.04	2	4	100	.3
SE4+900M	1	14	12	81	.1	8	13	2531	3.45	2	2	ND	2	18	1	2	2	54	.79	.07	27	8	.54	411	.01	2	2.32	.03	.09	2	3	75	.3
SE4+950M	1	34	13	58	.2	7	13	1928	2.96	2	2	ND	2	20	1	2	2	50	.68	.04	7	11	.65	667	.01	2	2.33	.02	.07	2	5	100	.2
SE4+1000M	1	26	8	45	.2	15	9	519	4.14	2	3	ND	2	12	1	2	2	122	.40	.08	4	32	.28	106	.22	2	2.11	.01	.02	2	2	60	.4
SE4+1050M	1	26	9	56	.1	21	10	888	4.49	2	3	ND	2	12	2	2	2	115	.41	.09	4	41	.42	99	.21	2	2.73	.01	.03	2	1	75	.3
SE4+1100M	1	10	8	45	.1	10	7	1583	4.24	2	2	ND	2	12	1	2	2	119	.39	.14	3	29	.25	106	.18	2	1.82	.01	.02	2	6	65	.1
SE4+1150M	1	32	10	65	.2	16	13	1558	4.16	6	3	ND	2	12	1	2	2	110	.42	.15	5	31	.33	161	.14	2	2.69	.01	.03	2	4	100	.3
SE4+1200M	1	13	8	50	.1	11	9	1483	2.87	2	2	ND	2	14	1	2	2	87	.44	.05	4	24	.30	111	.18	2	1.72	.02	.03	2	4	80	.1
SE4+1250M	1	48	10	77	.1	32	14	928	5.20	5	2	ND	2	13	2	2	2	128	.50	.17	5	53	.51	127	.23	2	3.73	.01	.03	2	1	85	.3
SE4+1300M	1	16	16	49	.1	8	9	5169	2.36	2	2	ND	2	12	1	2	3	68	.24	.08	7	19	.40	196	.01	2	1.68	.02	.05	2	1	90	.3
SE4+1350M	1	19	7	50	.1	15	11	1409	3.33	2	3	ND	2	17	1	2	2	93	.52	.06	6	31	.53	172	.04	2	2.17	.02	.05	2	2	55	.3
SE4+1400M	1	46	12	69	.1	25	11	3679	3.32	2	3	ND	2	34	1	2	2	76	1.53	.06	26	39	.41	277	.17	2	2.85	.02	.03	2	1	220	.4
SE4+1450M	1	8	7	34	.1	7	7	2374	2.03	2	2	ND	2	18	1	2	2	60	.48	.05	4	17	.27	110	.09	2	1.17	.01	.03	2	2	50	.1
SE4+1500M	1	19	6	46	.1	14	9	1547	2.77	2	2	ND	2	17	1	2	2	78	.54	.09	4	27	.49	98	.12	2	1.83	.02	.03	2	1	60	.1
SE4+1550M	1	38	12	70	.1	21	13	2898	4.53	2	2	ND	2	20	2	2	3	105	.46	.14	7	50	.50	258	.11	2	3.42	.01	.06	2	1	100	.1
SE4+1600M	1	49	6	80	.1	23	14	1380	4.78	2	3	ND	2	14	1	2	2	114	.48	.15	6	43	.32	136	.25	2	2.91	.02	.03	2	3	70	.4
SE4+1650M	1	68	4	89	.1	26	14	1413	4.15	2	3	ND	2	13	1	2	3	111	.48	.24	5	40	.45	121	.24	2	3.09	.01	.03	2	1	90	.2
SE4+1700M	1	34	7	107	.1	33	17	1719	4.63	4	3	ND	2	17	2	2	3	122	.47	.16	5	46	.39	151	.24	2	3.20	.02	.04	2	3	60	.1
SE4+1750M	1	57	2	75	.1	35	15	632	4.75	2	3	ND	2	14	2	2	2	150	.51	.12	4	53	.48	110	.33	2	4.56	.01	.03	2	1	45	.2
SE4+1800M	1	48	6	72	.1	28	16	2048	4.79	3	2	ND	2	16	2	2	3	147	.57	.20	4	46	.47	121	.29	2	3.97	.02	.02	2	2	65	.3
SE4+1850M	1	40	7	107	.1	28	16	2514	4.11	2	2	ND	2	14	1	3	3	117	.46	.18	6	48	.41	179	.24	2	3.59	.01	.03	2	1	60	.3
SE4+1900M	1	74	5	78	.1	31	16	1057	4.64	2	4	ND	2	11	2	2	3	148	.45	.19	5	50	.39	90	.31	2	4.73	.01	.02	2	3	75	.3
SE4+1950M	1	14	6	79	.1	12	12	3796	2.87	2	2	ND	2	20	1	2	2	79	.72	.18	4	25	.26	142	.22	2	1.60	.01	.03	2	1	60	.3
STD A-1	1	30	40	190	.3	36	13	1032	2.74	8	2	ND	2	32	2	2	2	55	.65	.11	8	74	.75	249	.08	3	1.89	.02	.19	2	1	55	.4

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb	Hg* ppb	Ag* ppm
SB4+2000m	1	33	5	81	.2	20	12	911	3.52	2	2	ND	2	15	2	2	2	103	.59	.11	3	32	.39	53	.28	2	2.65	.01	.02	2	3	40	.4
SB4+2050m	1	39	6	100	.1	22	14	2295	3.72	2	2	ND	2	23	2	2	2	104	.60	.05	6	35	.37	120	.28	2	2.72	.01	.04	2	1	70	.3
SB4+2100m	1	25	6	47	.2	28	20	2102	5.72	18	2	ND	2	17	2	2	2	195	.62	.04	5	55	.42	128	.23	2	3.76	.01	.03	2	2	110	.3
SB4+2150m	1	28	2	37	.6	20	9	238	2.63	7	2	2	2	21	1	2	2	100	1.22	.02	4	31	.85	43	.31	2	2.16	.03	.01	2	3	50	.5
SB5+0m	1	26	2	33	.3	18	9	292	2.55	2	2	ND	2	21	1	2	2	83	1.10	.02	11	33	.80	58	.21	2	2.22	.01	.03	2	2	60	.2
SB5+50m	1	20	9	51	.1	12	12	4337	2.86	4	2	ND	2	28	1	2	2	87	.92	.04	7	25	.39	326	.16	2	1.94	.02	.03	2	1	80	.3
SB5+100m	1	38	3	68	.3	21	15	601	3.89	2	2	ND	2	15	2	2	2	118	.65	.06	7	39	.56	98	.23	2	3.19	.01	.03	2	1	95	.3
SB5+150m	1	47	7	77	.2	22	14	1551	3.78	2	2	ND	2	19	1	2	2	99	.73	.25	6	38	.44	289	.17	2	3.07	.01	.04	2	3	70	.2
SB5+200m	1	56	6	58	.2	23	13	1013	3.90	3	3	ND	2	15	2	2	2	116	.57	.13	6	39	.71	203	.19	2	3.48	.01	.04	2	3	120	.4
SB5+250m	1	10	15	68	.1	7	11	3308	1.77	2	2	ND	2	32	1	2	2	43	.92	.10	7	11	.36	509	.03	2	2.14	.01	.11	2	1	120	.2
SB5+300m	1	43	16	71	.2	12	16	3058	4.03	2	2	ND	2	27	2	2	2	88	.77	.13	8	16	.49	395	.04	2	3.21	.01	.13	2	1	130	.2
SB5+350m	1	51	6	60	.2	24	20	727	4.83	2	2	ND	2	13	2	2	2	135	.35	.13	13	44	.57	78	.22	2	4.60	.01	.03	2	7	170	.4
SB5+400m	1	57	6	51	.2	24	12	237	5.56	2	2	ND	2	16	2	2	2	158	.33	.06	5	52	.44	95	.19	2	4.32	.01	.03	2	2	100	.2
SB5+450m	1	78	9	71	.3	21	29	1855	5.00	5	2	ND	2	15	2	2	2	133	.30	.22	8	48	.43	107	.16	2	4.65	.01	.03	2	1	150	.4
SB5+500m	1	24	11	45	.2	20	13	549	4.97	2	3	ND	2	20	2	2	2	167	.38	.04	5	42	.35	137	.19	2	3.16	.01	.04	2	6	60	.3
SB5+550m	1	17	12	41	.3	9	6	646	4.03	2	2	ND	2	30	1	2	2	132	.77	.12	4	27	.38	92	.08	2	2.95	.01	.04	2	1	140	.3
SB5+600m	1	11	8	23	.3	5	3	237	2.29	2	2	ND	2	31	1	2	2	92	.58	.03	4	19	.23	30	.09	2	1.75	.01	.02	2	2	50	.1
SB5+650m	1	11	17	31	.2	4	4	672	1.90	2	2	ND	2	41	1	2	2	84	1.30	.06	4	11	.27	125	.06	2	2.87	.01	.05	2	1	60	.2
SB5+700m	1	54	10	55	.1	18	10	1139	4.72	2	2	ND	2	16	2	2	2	140	.43	.13	5	46	.51	91	.16	2	4.22	.01	.04	2	5	65	.4
SB5+750m	1	47	9	53	.2	19	11	1000	3.76	4	2	ND	2	17	1	2	2	110	.49	.10	5	50	.71	96	.14	2	3.47	.01	.04	2	1	130	.2
SB5+800m	1	68	12	62	.2	24	11	584	5.31	2	4	ND	2	14	2	2	2	159	.33	.11	5	61	.55	66	.23	2	5.60	.01	.02	2	4	80	.3
SB5+850m	1	59	9	48	.2	22	12	398	4.56	2	2	ND	2	14	2	2	2	140	.44	.09	5	52	.55	59	.21	2	4.49	.01	.02	2	2	90	.3
SB5+900m	1	47	9	57	.3	24	13	460	4.55	2	2	ND	2	13	2	2	2	130	.48	.07	6	44	.56	83	.22	2	3.96	.01	.02	2	1	80	.4
SB5+950m	1	53	13	49	.2	15	8	1262	3.92	2	2	ND	2	17	2	2	2	111	.45	.13	6	38	.39	94	.14	2	3.59	.01	.04	2	3	150	.3
SB5+1000m	1	55	7	56	.2	25	12	938	3.68	4	2	ND	2	13	1	2	2	113	.42	.07	5	43	.55	100	.20	2	3.93	.01	.03	2	2	90	.3
SB5+1050m	1	63	9	72	.1	34	15	396	5.03	2	2	ND	2	14	2	2	2	146	.46	.07	7	60	.62	108	.28	2	5.34	.01	.04	2	3	160	.2
SB5+1100m	1	74	9	54	.3	38	16	423	5.38	10	2	2	2	14	3	2	2	164	.43	.06	6	68	.62	138	.30	2	6.47	.02	.03	2	1	110	.5
SB5+1150m	1	39	9	48	.3	23	12	574	5.09	2	2	ND	2	14	2	2	2	158	.38	.05	5	54	.44	111	.25	2	3.46	.01	.02	2	2	60	.2
SB5+1200m	1	45	8	57	.2	26	13	614	4.08	2	2	ND	2	14	2	2	2	125	.47	.04	5	45	.51	99	.24	2	3.74	.01	.02	2	1	90	.3
SB5+1350m	1	28	9	45	.1	18	9	252	4.90	2	2	ND	2	19	2	2	2	162	.43	.04	5	43	.33	124	.24	2	3.01	.02	.03	2	2	50	.2
SB5+1400m	1	16	19	57	.1	7	10	6477	2.47	2	2	ND	3	41	1	2	2	60	.63	.09	6	17	.27	427	.02	2	2.41	.01	.09	2	1	120	.1
SB5+1450m	1	27	12	51	.2	17	16	1793	3.68	2	2	ND	2	20	2	2	2	111	.76	.09	7	29	.76	200	.11	2	2.40	.03	.09	2	1	55	.3
SB5+1500m	1	62	7	48	.2	27	12	799	3.50	2	2	ND	2	17	2	2	2	121	.56	.06	8	48	.66	149	.26	2	3.95	.02	.06	2	1	80	.4
SB5+1550m	1	28	12	82	.1	11	11	4392	3.77	2	2	ND	2	21	2	2	2	95	.51	.19	5	33	.19	204	.21	2	2.34	.01	.03	2	1	70	.5
SB5+1600m	1	53	10	43	.2	25	12	796	3.75	2	2	ND	2	18	2	2	2	117	.82	.07	8	46	.56	196	.22	2	3.54	.02	.03	2	1	70	.2
STD A-1	1	31	39	189	.4	36	13	1034	2.74	7	2	ND	2	34	2	2	2	56	.64	.10	9	74	.77	269	.08	3	2.20	.02	.20	2	1	55	.4

ASARCO EXPLORATION PROJECT # VILLALTA-GRID NO SB-LINE NO FILE # 82-1276

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb	Hg* ppb	Ag* ppm
SB5+1650M	1	53	5	31	.2	16	9	2276	3.03	2	2	ND	2	20	1	2	2	81	1.10	.05	13	34	.24	173	.15	2	2.39	.01	.02	2	1	90	.4
SB5+1700M	1	49	3	30	.2	18	10	522	3.03	2	2	ND	2	18	1	2	2	89	.91	.03	5	37	.39	149	.17	3	2.56	.01	.02	2	4	80	.1
SB5+1750M	1	43	2	37	.1	27	12	476	4.46	2	4	ND	2	11	2	2	2	131	.43	.05	8	61	.45	168	.27	2	3.74	.01	.03	2	3	70	.2
SB5+1800M	1	61	3	37	.1	22	11	239	3.87	2	3	ND	2	7	1	2	2	124	.26	.02	6	47	.44	72	.23	2	3.30	.01	.02	2	3	110	.2
SB5+1850M	1	50	3	32	.1	20	12	267	4.85	2	2	ND	2	8	2	2	2	147	.24	.02	5	44	.22	93	.26	2	3.33	.01	.01	2	4	70	.1
SB5+1900M	1	59	5	34	.1	25	10	419	3.64	2	3	ND	2	12	1	2	2	116	.42	.06	3	39	.49	61	.21	2	2.88	.01	.03	2	2	60	.2
SB5+1950M	1	56	18	86	.2	14	19	10273	3.43	7	2	ND	3	48	2	2	4	46	1.00	.11	11	18	.51	678	.02	3	1.88	.01	.08	2	1	280	.3
SB5+2000M	1	54	4	48	.1	23	12	897	3.14	2	2	ND	2	16	1	2	2	88	.47	.05	6	39	.65	124	.15	3	2.58	.01	.04	2	2	40	.1
SB5+2050M	1	22	5	45	.1	17	8	517	2.45	3	2	ND	2	12	1	2	2	70	.39	.05	3	26	.36	76	.16	2	1.87	.01	.03	2	5	50	.1
SB5+2100M	1	31	4	44	.1	24	11	420	3.20	2	2	ND	2	11	1	2	2	98	.33	.04	3	40	.49	101	.20	2	2.76	.01	.02	2	4	40	.1
SB5+2150M	1	32	1	48	.1	20	9	329	3.02	2	3	ND	2	8	1	2	2	95	.33	.05	4	32	.45	45	.22	3	2.41	.01	.02	2	3	45	.1
SB5+2200M	1	40	4	75	.1	27	12	1198	3.38	2	2	ND	2	15	1	2	2	96	.46	.11	3	42	.47	141	.17	3	3.18	.01	.03	2	1	65	.1
SB5+2300M	1	39	4	49	.1	30	12	268	4.42	3	3	ND	2	12	2	2	2	136	.35	.04	4	59	.43	113	.28	3	4.19	.01	.02	2	2	110	.1
SB5+2350M	1	18	1	40	.1	19	10	290	3.61	2	2	ND	2	10	1	2	2	117	.33	.03	2	35	.33	42	.28	2	2.13	.01	.02	2	1	55	.1
SB5+2400M	1	36	4	46	.1	21	10	220	3.37	2	3	ND	2	11	1	2	2	107	.35	.03	5	36	.46	87	.23	2	2.61	.01	.02	2	1	50	.1
SB6+0M	1	20	6	47	.1	12	11	1434	3.04	2	2	ND	2	14	1	2	2	80	.43	.10	3	26	.33	107	.23	2	1.55	.02	.02	2	4	60	.2
SB6+50M	1	21	3	34	.1	15	9	733	2.78	2	2	ND	2	12	1	2	2	83	.36	.04	3	25	.32	114	.18	3	1.96	.02	.02	2	3	60	.1
SB6+100M	1	24	24	44	.1	12	9	2225	3.24	2	3	ND	2	14	1	2	2	86	.34	.13	3	31	.35	119	.12	3	2.08	.01	.02	2	1	100	.1
SB6+150M	1	15	5	40	.1	9	8	1552	2.30	2	2	ND	2	11	1	2	2	60	.32	.13	3	21	.26	100	.08	2	1.41	.01	.02	2	5	60	.1
SB6+200M	1	58	9	36	.1	15	9	554	3.97	6	2	ND	2	11	2	2	2	114	.53	.05	4	57	.37	96	.16	3	2.42	.01	.02	2	1	85	.1
SB6+250M	1	32	5	25	.1	14	9	597	3.90	2	2	ND	2	11	1	2	2	119	.31	.03	9	64	.41	92	.16	3	2.08	.01	.02	2	1	90	.1
SB6+300M	1	35	8	56	.1	30	14	3576	3.32	2	2	ND	2	24	1	2	2	64	.53	.31	3	76	.80	408	.08	2	2.51	.01	.04	2	1	75	.2
SB6+350M	1	23	7	29	.1	12	11	1043	3.90	2	2	ND	2	10	1	2	2	104	.22	.09	3	31	.29	57	.13	2	2.17	.01	.02	2	1	70	.2
SB6+400M	1	20	7	42	.1	11	12	1332	2.92	2	2	ND	2	18	1	2	2	69	.45	.08	4	26	.28	255	.09	2	1.71	.02	.03	2	3	70	.1
SB6+450M	1	17	7	56	.1	16	12	1142	3.19	2	2	ND	2	14	1	2	2	69	.43	.23	3	28	.34	195	.11	2	2.66	.01	.03	2	1	80	.2
SB6+500M	1	28	11	91	.2	10	13	787	4.10	6	2	ND	2	13	1	2	2	66	.39	.17	4	20	.33	203	.07	3	1.98	.01	.06	2	1	100	.3
SB6+600M	1	41	6	29	.1	14	7	694	3.33	4	2	ND	2	6	1	2	2	89	.18	.14	6	39	.35	47	.14	3	4.78	.01	.02	2	3	300	.1
SB6+650M	1	9	7	43	.1	7	6	3453	1.90	2	2	ND	2	11	1	2	2	52	.29	.09	3	17	.19	168	.08	2	1.20	.01	.02	2	1	45	.1
SB6+700M	1	37	12	147	.3	15	19	13384	3.88	2	3	ND	5	18	2	2	4	77	.43	.23	4	38	.34	359	.06	2	2.96	.01	.02	2	1	220	.4
SB6+750M	1	41	4	36	.1	17	9	836	3.02	2	3	ND	2	7	1	2	2	91	.23	.06	5	33	.47	61	.17	2	3.17	.01	.02	2	1	180	.1
SB6+800M	1	17	8	33	.1	8	5	977	2.47	2	3	ND	2	9	1	2	2	70	.23	.06	3	22	.24	97	.10	2	1.45	.01	.02	2	1	65	.1
SB6+850M	1	10	7	57	.1	7	6	3894	2.58	2	2	ND	2	7	1	2	2	57	.22	.22	3	21	.17	135	.07	2	1.72	.01	.02	2	2	65	.1
SB6+900M	1	29	7	34	.1	15	7	305	3.05	2	3	ND	2	8	1	2	2	83	.20	.06	3	37	.38	97	.14	2	4.16	.01	.02	2	2	60	.1
SB6+950M	1	13	6	34	.2	8	7	616	2.08	2	2	ND	2	14	1	2	2	55	.28	.04	3	19	.36	98	.07	2	1.76	.01	.03	2	1	90	.1
SB6+1000M	1	39	8	42	.1	18	9	1184	3.02	2	2	ND	2	9	1	2	2	86	.24	.07	4	37	.47	129	.12	2	3.53	.01	.03	2	1	100	.1
STD A-1	1	29	35	176	.4	33	12	960	2.54	7	3	ND	2	32	2	2	2	51	.56	.10	8	69	.71	251	.08	7	1.90	.02	.19	2	1	55	.3

ASARCO EXPLORATION PROJECT # VILLALTA-GRID NO SB-LINE NO FILE # 82-1276

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb	Hg* ppb	Ag* ppm
SB6+1050W	1	14	5	31	.1	10	6	270	1.93	2	2	ND	2	6	-1	2	2	49	.18	.03	2	18	.27	63	.09	2	1.57	.01	.02	2	8	70	.1
SB6+1100W	1	15	8	40	.1	10	6	1592	2.06	2	2	ND	2	9	1	2	2	61	.28	.05	2	22	.29	138	.11	2	1.86	.01	.02	2	2	70	.1
SB6+1150W	1	17	7	33	.1	9	6	936	2.52	2	2	ND	2	7	1	2	2	67	.17	.16	3	18	.18	131	.06	2	1.93	.01	.02	2	1	50	.1
SB6+1200W	1	47	6	39	.2	22	11	790	3.66	5	3	ND	2	7	1	2	2	90	.28	.06	13	35	.51	123	.14	2	2.89	.01	.04	2	1	260	.1
SB6+1250W	1	16	9	57	.1	11	8	3875	2.28	2	2	ND	2	9	1	2	2	48	.26	.14	2	16	.30	223	.07	2	1.28	.01	.03	2	13	80	.1
SB6+1300W	1	18	4	31	.1	16	7	574	2.56	2	3	ND	2	7	1	2	2	70	.33	.03	3	30	.36	101	.12	2	1.82	.01	.02	2	1	40	.1
SB6+1350W	1	14	6	45	.1	15	9	1733	3.07	4	2	ND	2	8	1	2	2	82	.29	.05	3	25	.27	126	.15	2	1.60	.01	.01	2	1	50	.1
SB6+1400W	1	108	11	29	.4	21	11	2148	3.85	5	4	ND	2	26	2	2	2	88	1.43	.04	44	52	.36	376	.12	5	2.74	.01	.03	2	2	260	.5
SB6+1450W	1	31	6	22	.1	21	11	199	3.90	5	2	ND	2	9	1	2	2	104	.31	.01	7	56	.59	182	.10	2	2.70	.01	.01	2	6	60	.1
SB6+1500W	1	43	7	35	.1	26	10	748	3.43	3	2	ND	2	11	1	2	2	94	.42	.03	5	70	.76	200	.05	3	2.23	.01	.03	2	22	520	.1
SB6+1550W	1	28	6	33	.1	18	9	896	2.94	3	2	ND	2	9	1	2	2	83	.39	.03	4	39	.43	128	.14	2	1.95	.01	.02	2	2	120	.2
SB6+1600W	1	22	8	40	.1	17	9	1427	2.86	2	2	ND	2	12	1	2	2	82	.43	.04	3	31	.38	160	.16	2	1.83	.01	.02	2	1	70	.1
SB6+1650W	1	32	5	27	.1	15	8	363	2.52	2	2	ND	2	10	1	2	2	75	.46	.04	4	23	.55	52	.14	3	1.31	.02	.02	2	1	75	.3
SB6+1700W	1	32	6	36	.1	19	11	618	3.57	2	3	ND	2	8	1	2	2	108	.33	.04	3	36	.40	78	.22	2	2.22	.01	.02	2	1	70	.2
SB6+1750W	1	41	6	33	.1	19	12	574	3.06	5	3	ND	2	14	1	2	2	97	.41	.03	5	36	.55	241	.17	2	2.03	.02	.03	2	2	90	.1
SB6+1800W	1	36	6	34	.1	19	10	488	2.68	3	2	ND	2	11	1	2	2	81	.53	.05	4	33	.58	90	.15	2	1.71	.01	.02	2	1	65	.2
SB6+1850W	1	26	6	40	.1	21	9	438	2.97	2	2	ND	2	7	1	2	2	84	.29	.06	3	35	.40	56	.18	2	2.17	.01	.01	2	1	80	.1
SB6+1900W	1	33	4	29	.1	18	9	364	2.64	5	2	ND	2	8	1	2	2	78	.36	.04	4	27	.49	50	.16	2	1.92	.01	.01	2	2	60	.1
SB6+1950W	1	49	5	33	.1	19	9	419	2.87	3	2	ND	2	10	1	2	2	85	.47	.05	4	29	.56	73	.18	2	2.19	.01	.02	2	2	80	.1
SB6+2000W	1	41	3	34	.1	19	9	342	2.62	2	2	ND	2	5	1	2	2	80	.27	.06	2	27	.51	38	.17	2	2.34	.01	.01	2	1	50	.1
SB6+2050W	1	49	2	27	.1	17	8	365	2.35	6	2	ND	2	7	1	2	2	70	.36	.04	4	22	.59	46	.16	2	1.66	.02	.02	2	4	70	.1
SB6+2100W	1	40	4	32	.1	16	8	478	2.53	5	2	ND	2	8	1	2	2	76	.35	.08	3	25	.51	48	.15	2	1.99	.01	.02	2	2	90	.1
SB6+2150W	1	27	4	28	.1	15	10	400	2.69	5	3	ND	2	11	1	2	2	78	.41	.04	5	29	.52	70	.09	3	1.48	.02	.02	2	1	65	.1
STD A-1	1	29	42	188	.3	36	13	1045	2.78	12	2	ND	2	35	2	2	2	57	.58	.11	8	73	.77	278	.08	7	1.97	.02	.20	2	1	50	.3
[illegible]	1	40	12	44	.8	18	9	429	3.95	69	2	ND	2	7	1	2	3	93	.10	.06	3	43	.65	48	.13	2	3.42	.01	.03	2	10	80	1.0

ANALYTICAL PROCEDURES

All soil samples were dried at 75°C and sieved to minus 80 mesh. ICP geochemical analysis was determined by taking a .500 gram sample digested with 3 milliliters of 3:1:3 nitric acid to hydrochloric acid to water at 90°C for 1 hour. The sample was diluted to 10 milliliters with water. Results are reported in ppm except for: Fe, Ca, P, Ba, Ti Al, Na and K which are in percent. The leach is partial for Ca, P, Mg, Al, Ti, La, Na, K, Cl and Cr. IS = Internal Standard. ICP results reported are for the following elements, Mn, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, Al, Na and K. Au++ analysis was determined taking 10 - 30 gram samples subjected to fire assay preconcentration techniques to produce silver beads which are dissolved and Au is determined in solution by atomic absorption. Ag++ analysis is by atomic absorption. Hg++ analysis is determined by cold vapour AA using F. and J. Scientific Hg assembly. Au aliquot of the extract is added to a stannous chloride/hydrochloric acid solution. The reduced Hg is swept out of solution and passed into the Hg cell where is is measured by A.A.

STATISTICAL EVALUATION OF RESULTS

Gold - Please refer to ATTACHMENT "C" depicting gold values plotted in parts per billion at grid sites. The highest gold response in soils was 735 ppb postioned at SB4,0W. The attached probability plot for gold suggests the following anomalous parameters,

$>$ 16 ppb GOLD = anomalous

9 - 16 ppb GOLD = possibly anomalous

$<$ 9 ppb GOLD = background

Silver - Please see ATTACHMENT "D" indicating soil response for silver. The highest silver response was 0.5 ppm located at grid coordinates SB4,2150W; SB5,1100W; and SB6,1400W. Probability plot for silver indicates the following anomalous parameters,

> 0.4 ppm SILVER = anomalous

0.3 - 0.4 ppm SILVER = possibly anomalous

< 0.3 ppm SILVER = background

Mercury - Soil response for mercury is depicted in ATTACHMENT "E". The suggested geochemical response parameters using a probability plot are:

> 240 ppb MERCURY = anomalous

110 - 240 ppb MERCURY = possibly anomalous

< 110 ppb MERCURY = background

Antimony - Geochemical response for antimony in soils is plotted on ATTACHMENT "F". The probability plot suggests,

> 30 ppm ANTIMONY = anomalous

4 - 30 ppm ANTIMONY = possibly anomalous

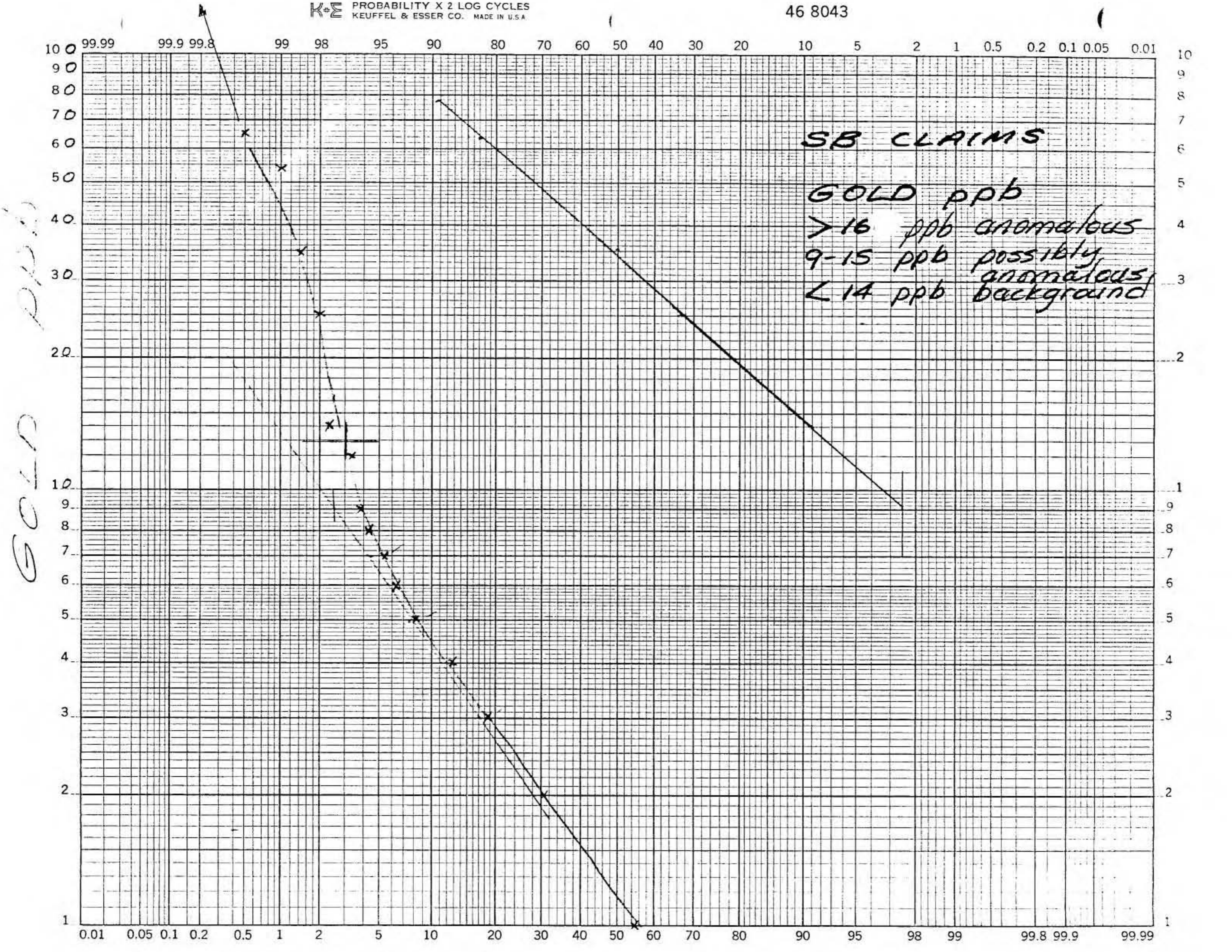
< 4 ppm ANTIMONY = background

Arsenic - Please refer to ATTACHMENT "G" depicting arsenic geochemical response obtained from soil. Probability plot of these values suggests,

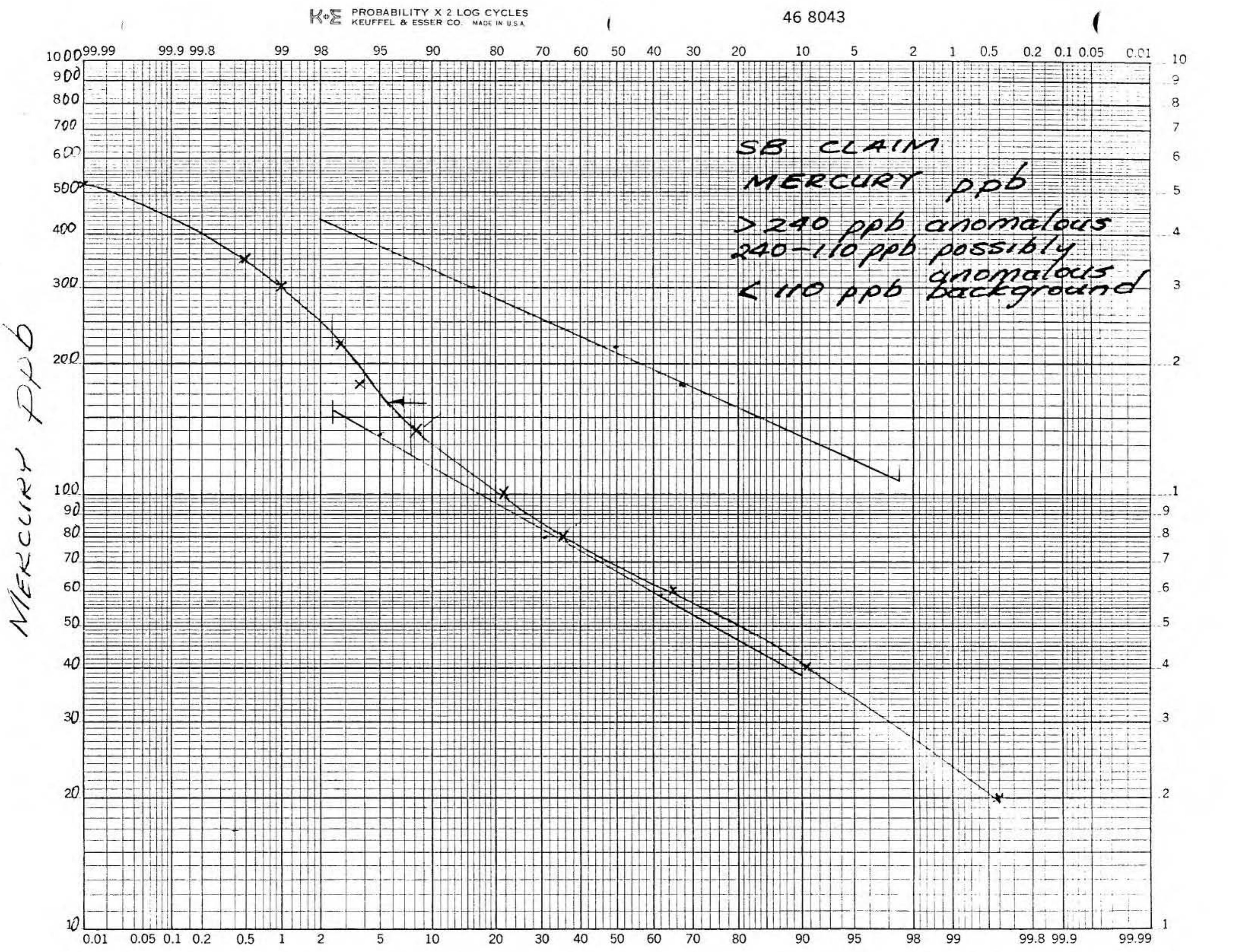
> 55 ppm ARSENIC = anomalous

20 - 55 ppm ARSENIC = possibly anomalous

< 20 ppm ARSENIC = background

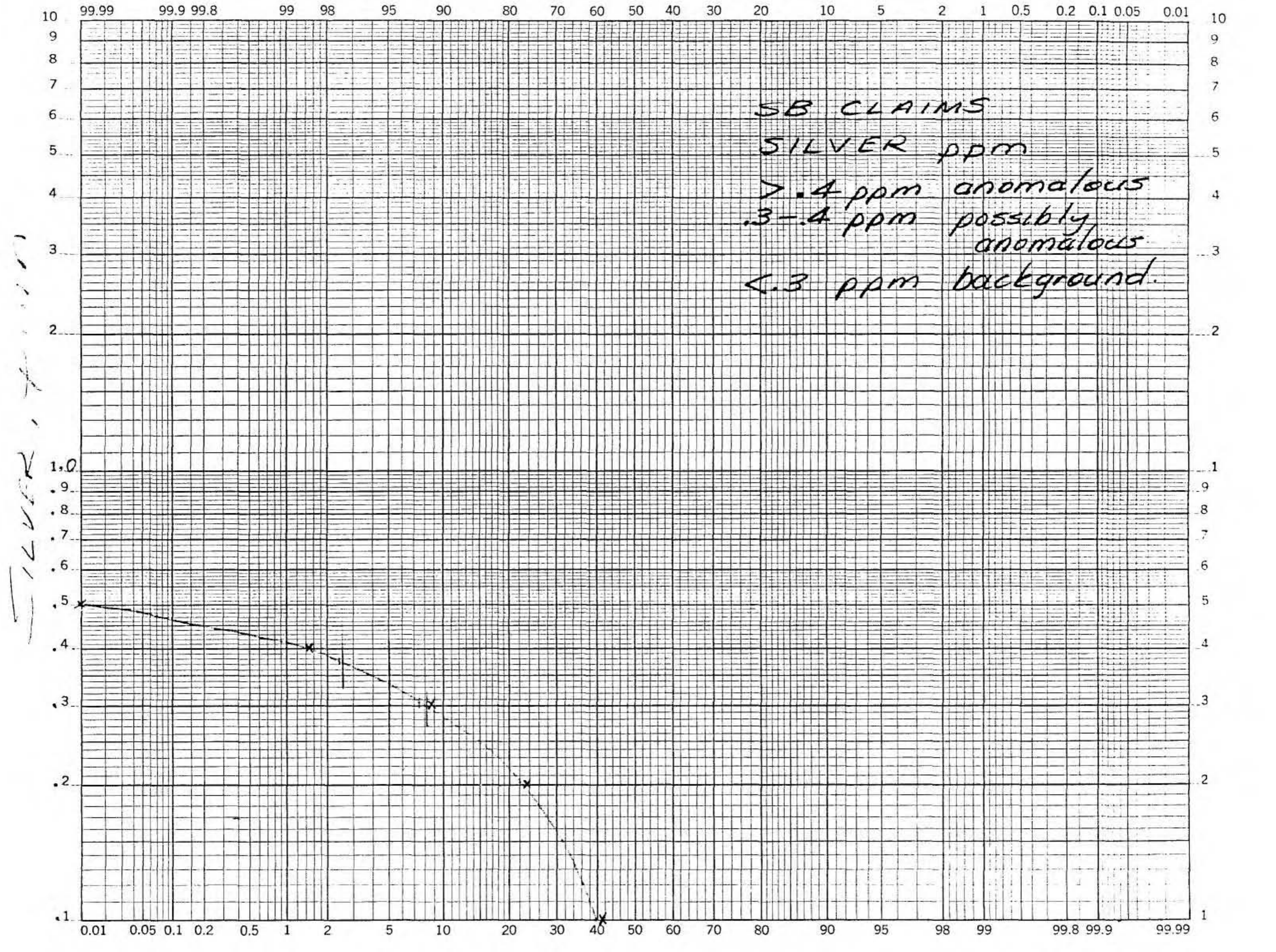


K+E PROBABILITY X 2 LOG CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.
46 8043
SB CLAIMS
GOLD ppb
>16 ppb anomalous
9-15 ppb possibly anomalous
<14 ppb background
GOLD ppb


K+E PROBABILITY X 2 LOG CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.
46 8043
SB CLAIM
MERCURY ppb
>240 ppb anomalous
240-110 ppb possibly anomalous
<110 ppb background
MERCURY ppb

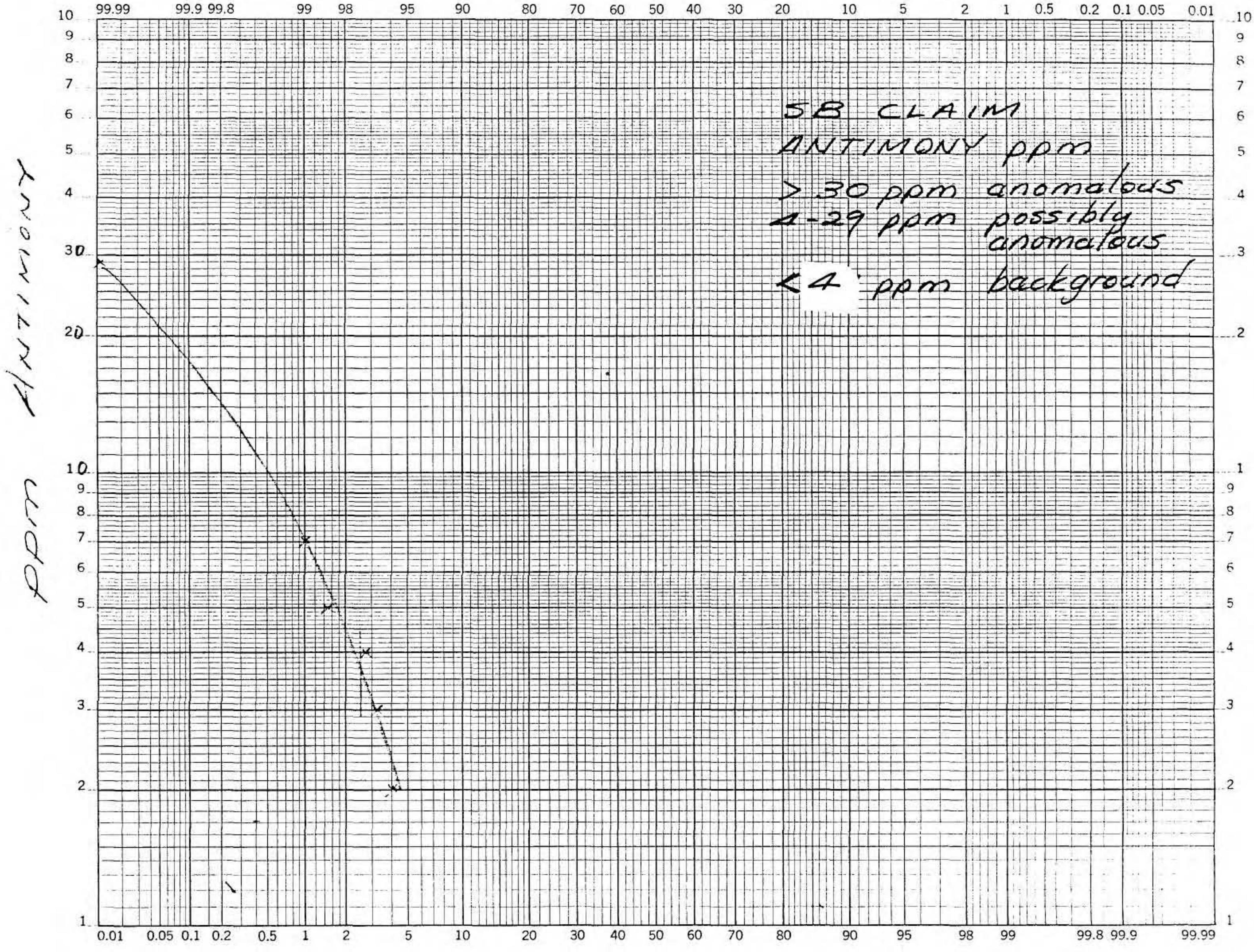
K+E PROBABILITY X 2 LOG CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.

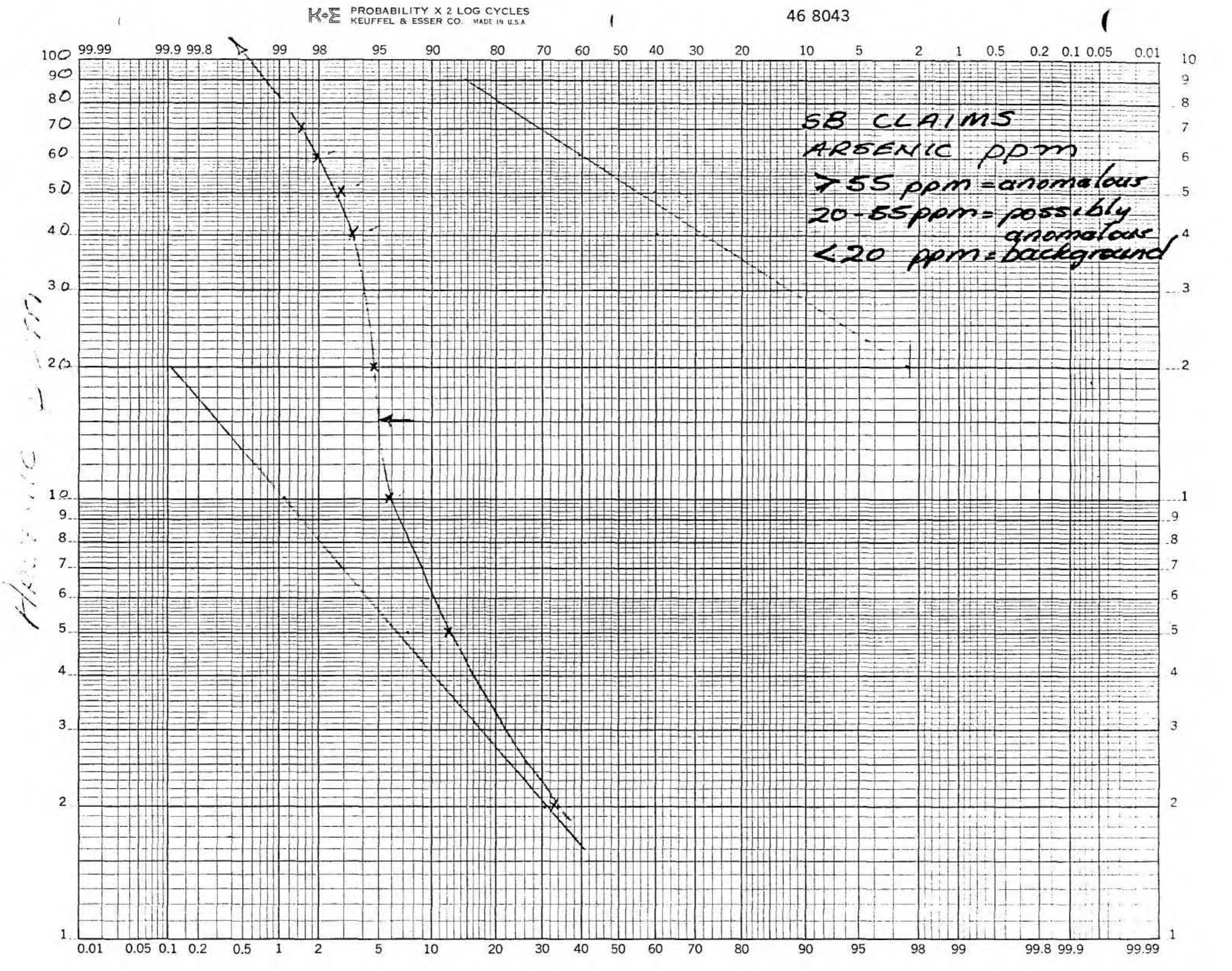
46 8043

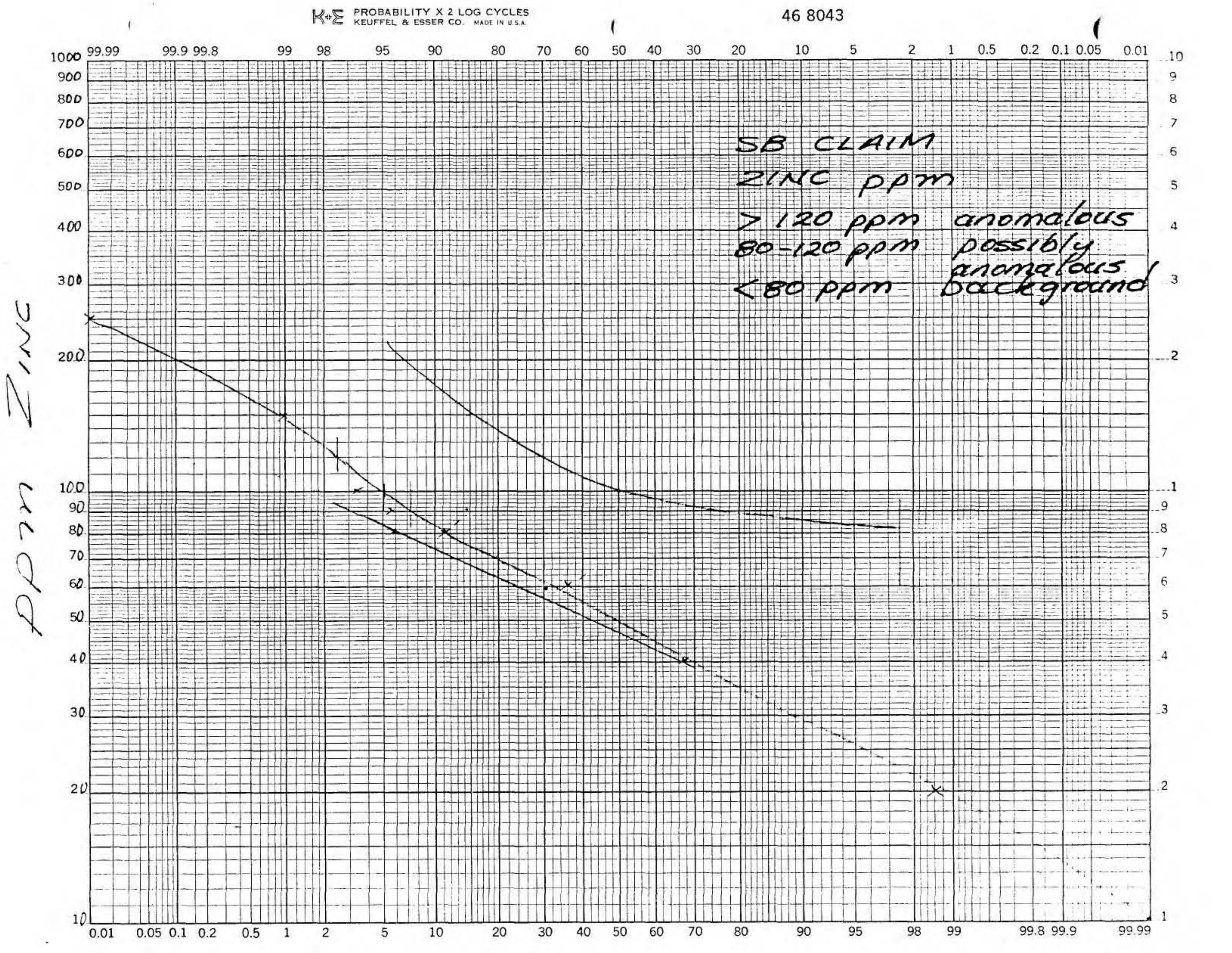


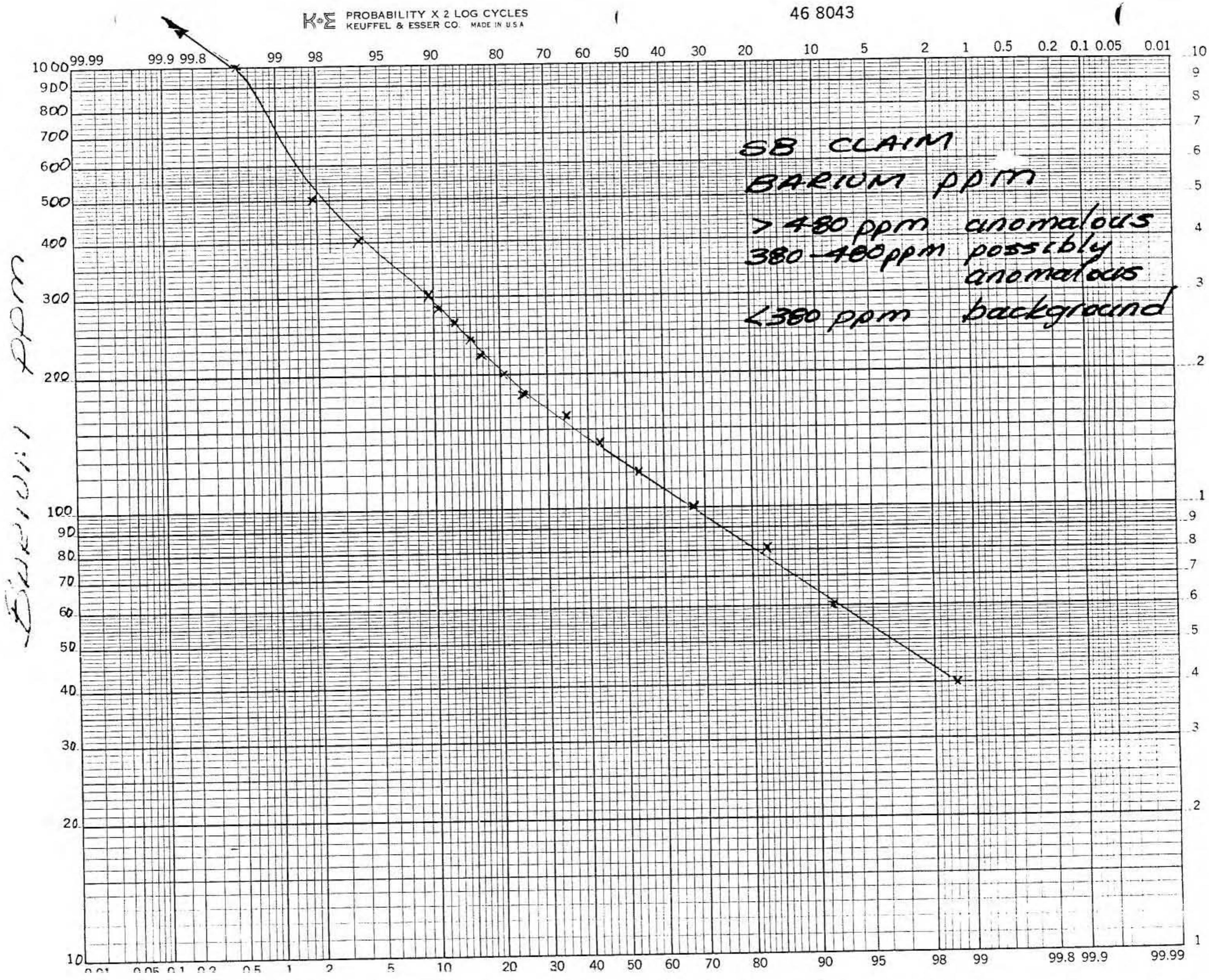
K+E PROBABILITY X 2 LOG CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.

46 8043




K+E PROBABILITY X 2 LOG CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.
46 8043
SB CLAIMS
ARSENIC ppm
>55 ppm = anomalous
20-55 ppm = possibly anomalous
<20 ppm = background


K+E PROBABILITY X 2 LOG CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.
46 8043
SB CLAIM
ZINC ppm
> 120 ppm anomalous
80-120 ppm possibly anomalous
< 80 ppm background
PPM ZINC


K+E PROBABILITY X 2 LOG CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.
46 8043
SB CLAIM
BARIUM ppm
> 480 ppm anomalous
380-480 ppm possibly anomalous
<380 ppm background
BARIUM ppm

Zinc - Soil response for zinc is plotted on ATTACHMENT "H". The appended probability plot suggests:

$>$ 120 ppm ZINC = anomalous

80 - 120 ppm ZINC = possibly anomalous

$<$ 80 ppm ZINC = background

Barium - See attached geochemical and probability plots. See ATTACHMENT "I".

CONCLUSION

Detailed prospecting of the claim and geologic mapping at a scale of 1:10,000 is recommended.

D. M. Fletcher

APPENDIX 1

STATEMENT OF EXPENDITURES

1st AUGUST - 15th SEPTEMBER 1982

1.	SALARIES		
	P. Conroy $78/day x 2 days =	$156.00	
	M. Specogna $44/day x 2 days =	88.00	
	R. Wahl $72/day x 6 days =	432.00	
	A. Hamilton $56/day x 6 days =	336.00	$ 1012.00
2.	ACCOMMODATION, SUPPLIES & EQUIPMENT		820.00
3.	GEOCHEMICAL SAMPLING		
	Invoice # 1276 =	$3100.00	
	Invoice # 0984 =	828.91	3928.91
4.	VEHICLE EXPENSE, MOBILIZATION ETC.		260.00
	TOTAL EXPENDITURES		$ 6020.91

APPENDIX 2

STATEMENT OF QUALIFICATIONS

I, David McLean Fletcher of Vancouver, British Columbia, Canada, certify that,

1. I am a graduate in Geological Engineering (B.Ap.Sc. 1956) of the University of British Columbia.

2. I have practised my profession as an exploration geologist continuously for the past 27 years.

3. I am a registered Professional Engineer in the Provinces of British Columbia and Ontario, Canada.

4. I supervised the geological and geochemical work accomplished at the SB Claim from August 1982 through September 1982.

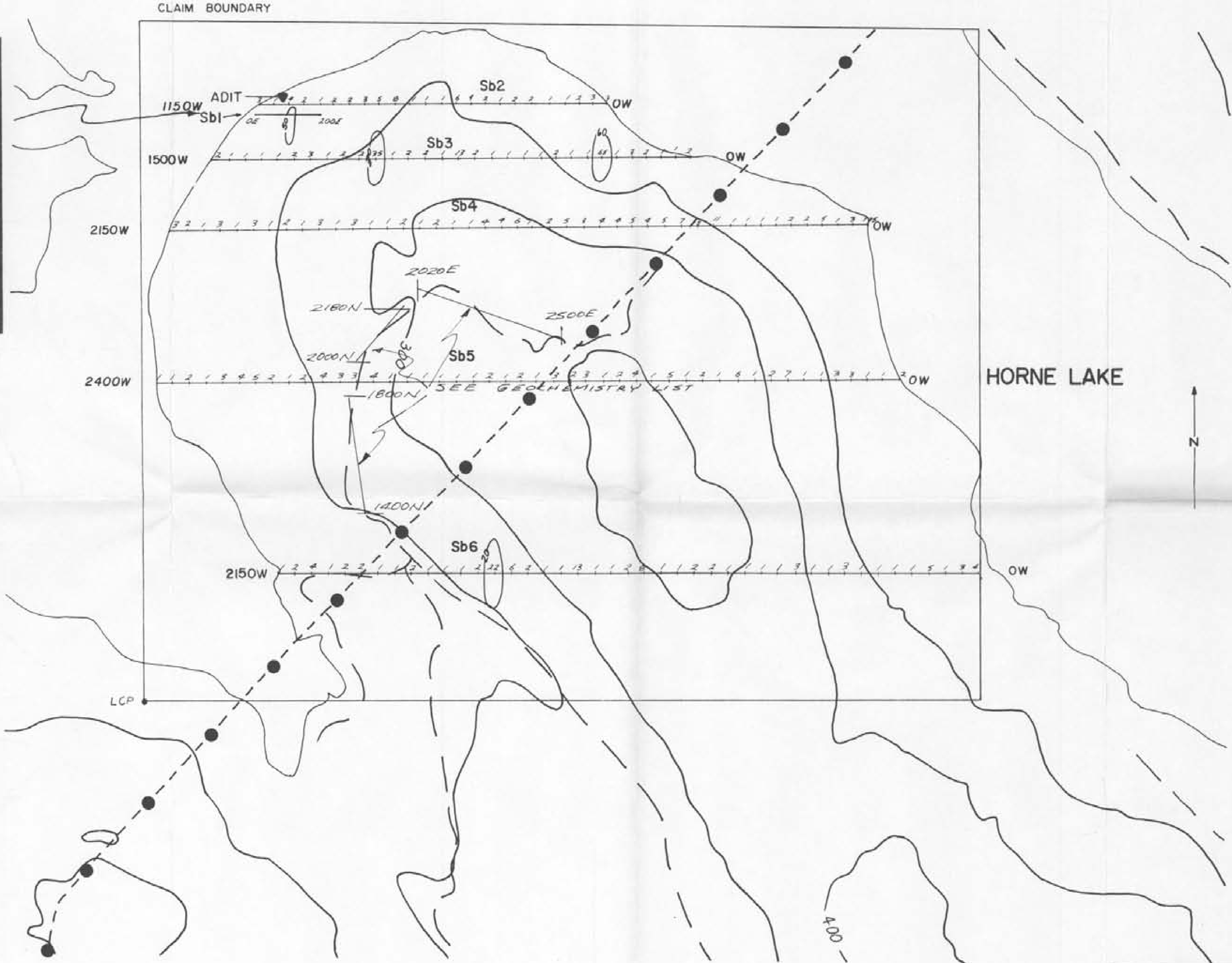
D. M. Fletcher
January 26, 1983

ATTACHMENT "C"

GEOLOGICAL BRANCH
ASSESSMENT REPORT

11,02[illegible]

[redacted]



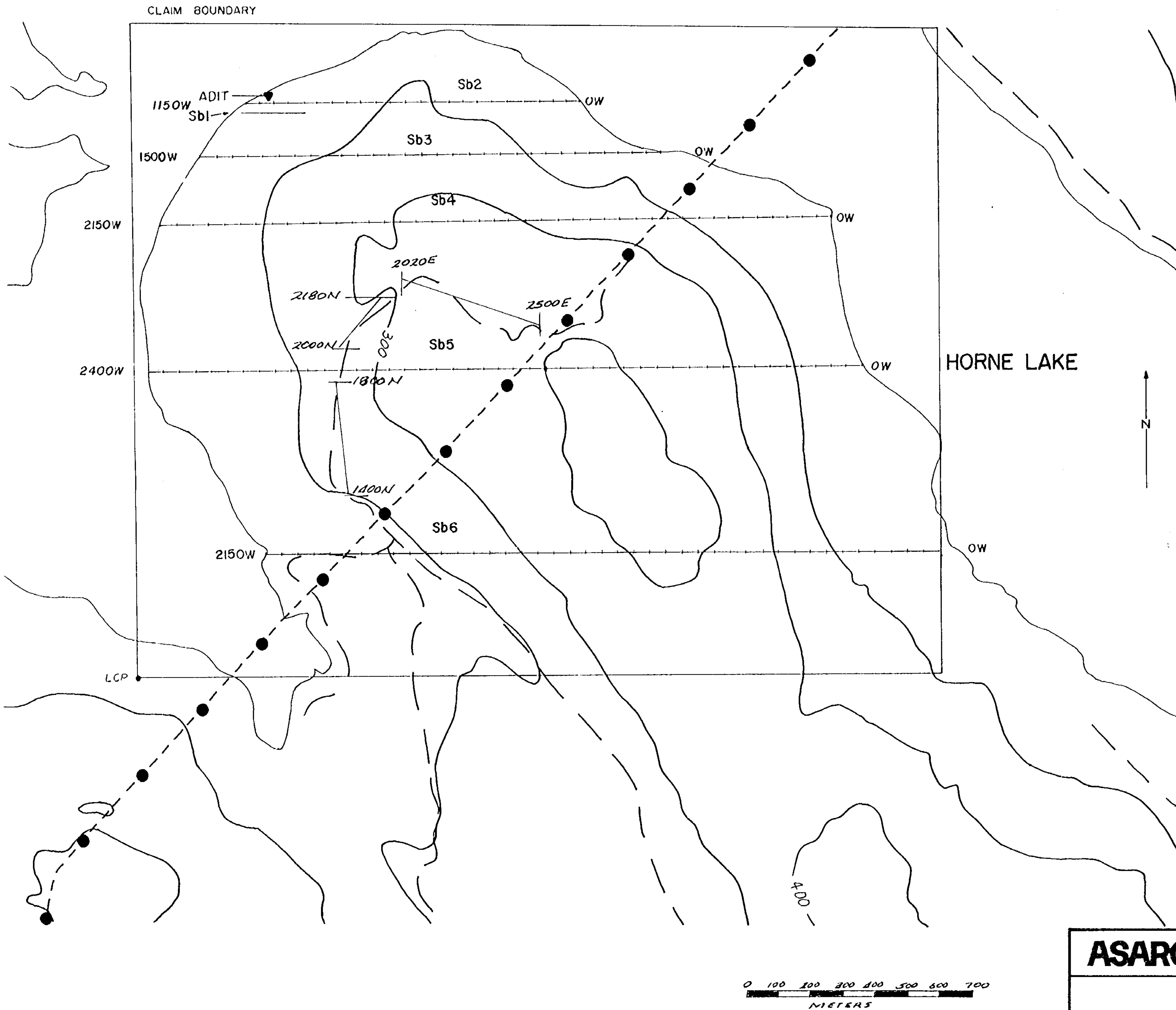
D. M. FLETCHER
BRITISH COLUMBIA
ENGINEER

ASARCO		Vancouver	
Sb CLAIMS GEOCHEM GRID GOLD (ppb)			
Drawn by	Date	N.T.S.	SCALE
A P H	NOV 82	92 F/7	1:10,000

ATTACHMENT "B"

GEOLOGICAL BRANCH
ASSESSMENT REPORT

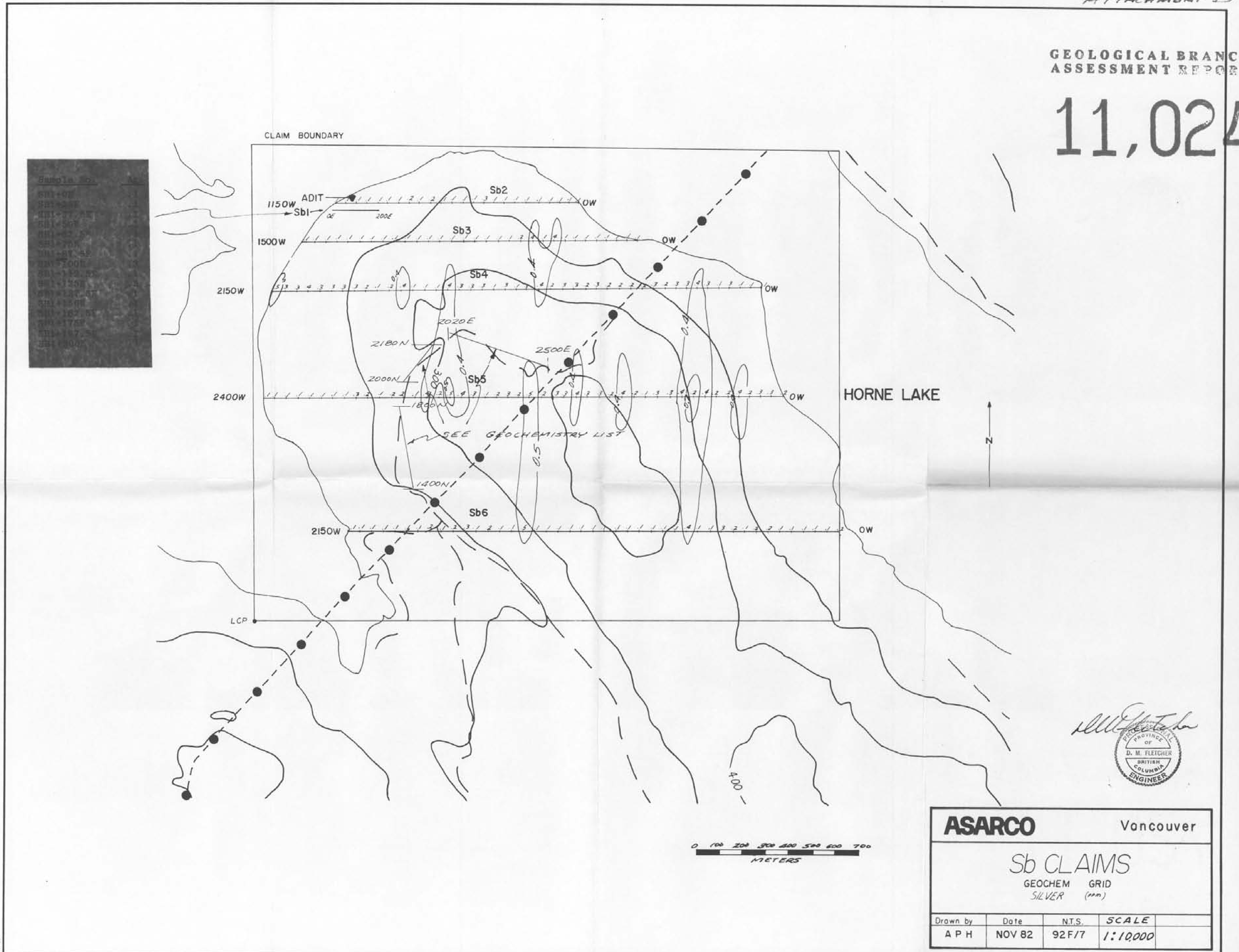
11,024



D. M. FLETCHER
PROVINCE OF BRITISH COLUMBIA
ENGINEER

ASARCO		Vancouver	
Sb CLAIMS GEOCHEM GRID			
Drawn by	Date	N.T.S.	SCALE
A P H	NOV 82	92F/7	1:10,000

ATTACHMENT "D"

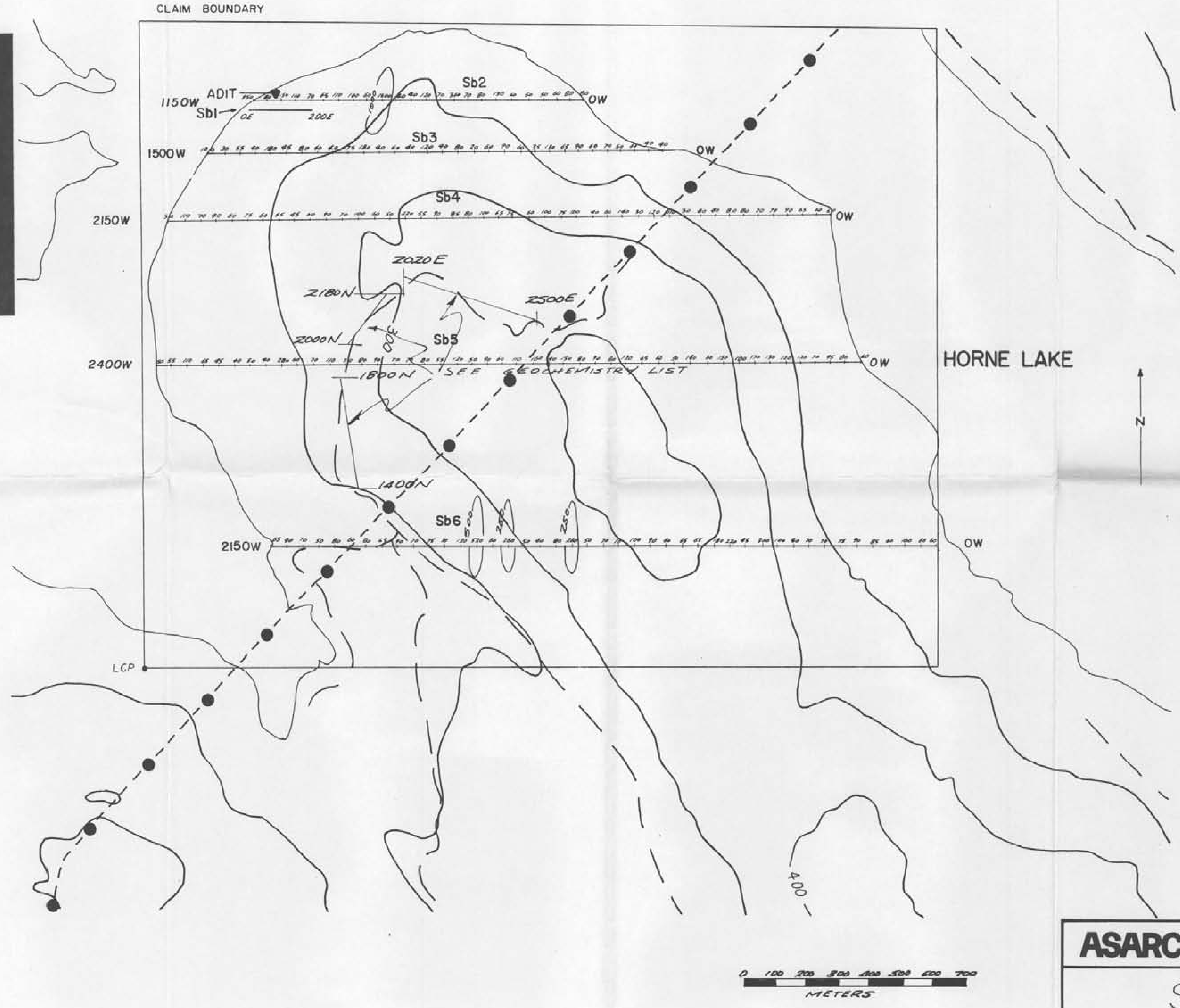


ATTACHMENT "E"

GEOLOGICAL BRANCH
ASSESSMENT REPORT

11,024

[redacted]



ASARCO Vancouver

Sb CLAIMS

GEOCHEM GRID
MERCURY (PPB)

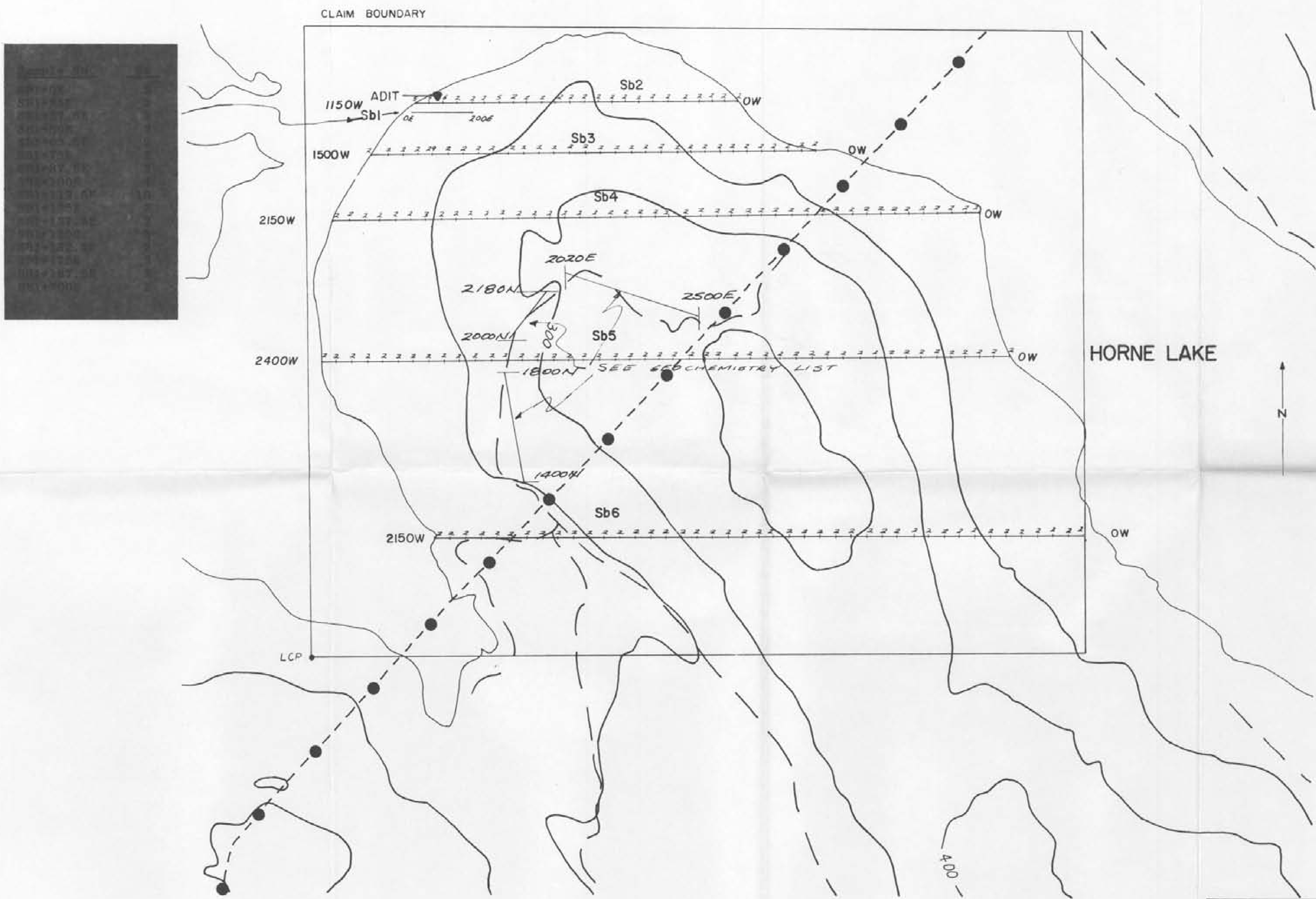
Drawn by	Date	N.T.S.	SCALE
A P H	NOV 82	92 F/7	1:10,000

D. M. FLETCHER
PROVINCE OF BRITISH COLUMBIA
ENGINEER

ATTACHMENT "F"

GEOLOGICAL BRANCH
ASSESSMENT REPORT

11,024



ASARCO Vancouver

Sb CLAIMS

GEOCHEM GRID

ANTIMONY (PPM)

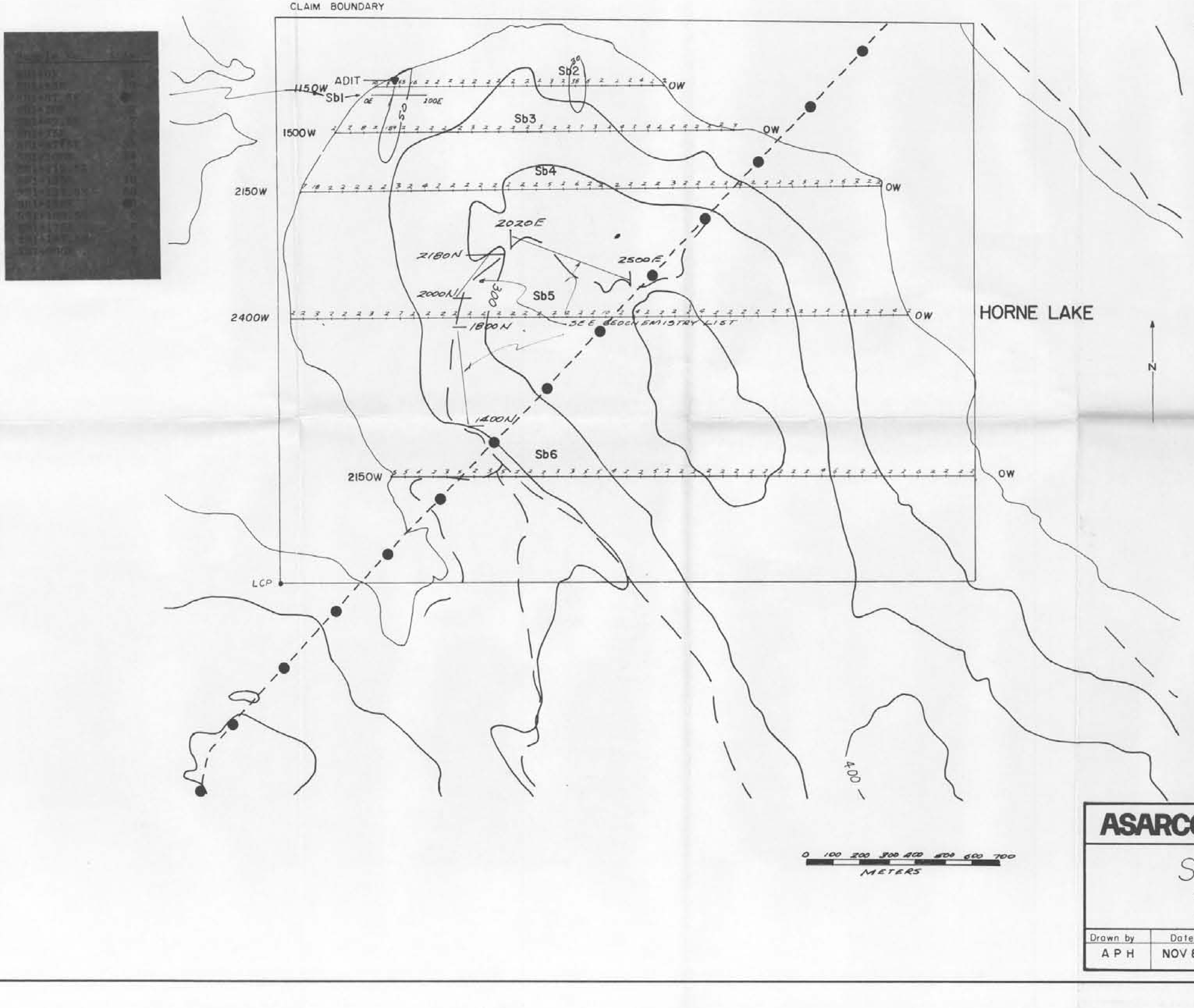
Drawn by	Date	N.T.S.	SCALE
A P H	NOV 82	92 F/7	1:10,000

PROVINCE OF BRITISH COLUMBIA
D. M. FLETCHER
ENGINEER

ATTACHMENT "G"

GEOLOGICAL BRANCH
ASSESSMENT REPORT

11,024



PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
D. M. FLETCHER

ASARCO Vancouver

Sb CLAIMS

GEOCHEM GRID

ARSENIC (ppm)

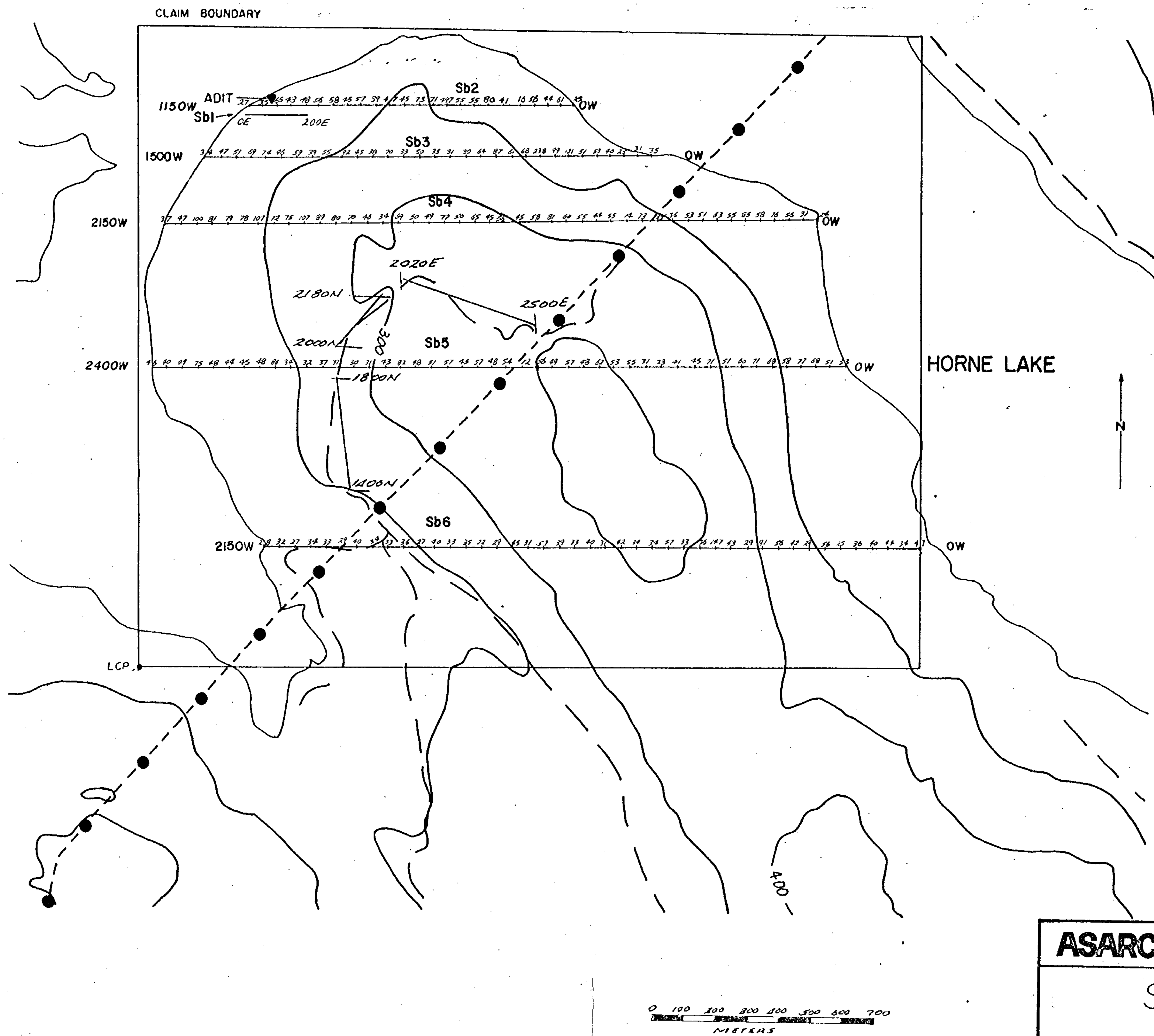
Drawn by	Date	N.T.S.	SCALE
A P H	NOV 82	92 F/7	1:10,000

Attachment "H"

GEOLOGICAL BRANCH
ASSESSMENT REPORT

11,024

Sample No.	Zn
SB1+0E	58
SB1+25E	55
SB1+37.5E	51
SB1+50E	59
SB1+62.5E	40
SB1+75E	57
SB1+87.5E	55
SB1+100E	125
SB1+112.5E	52
SB1+125E	85
SB1+137.5E	50
SB1+150E	29
SB1+162.5E	29
SB1+175E	33
SB1+187.5E	60
SB1+200E	47



D. M. Fletcher

PROVINCE OF BRITISH COLUMBIA
D. M. FLETCHER
ENGINEER

ASARCO Vancouver

Sb CLAIMS

GEOCHEM GRID

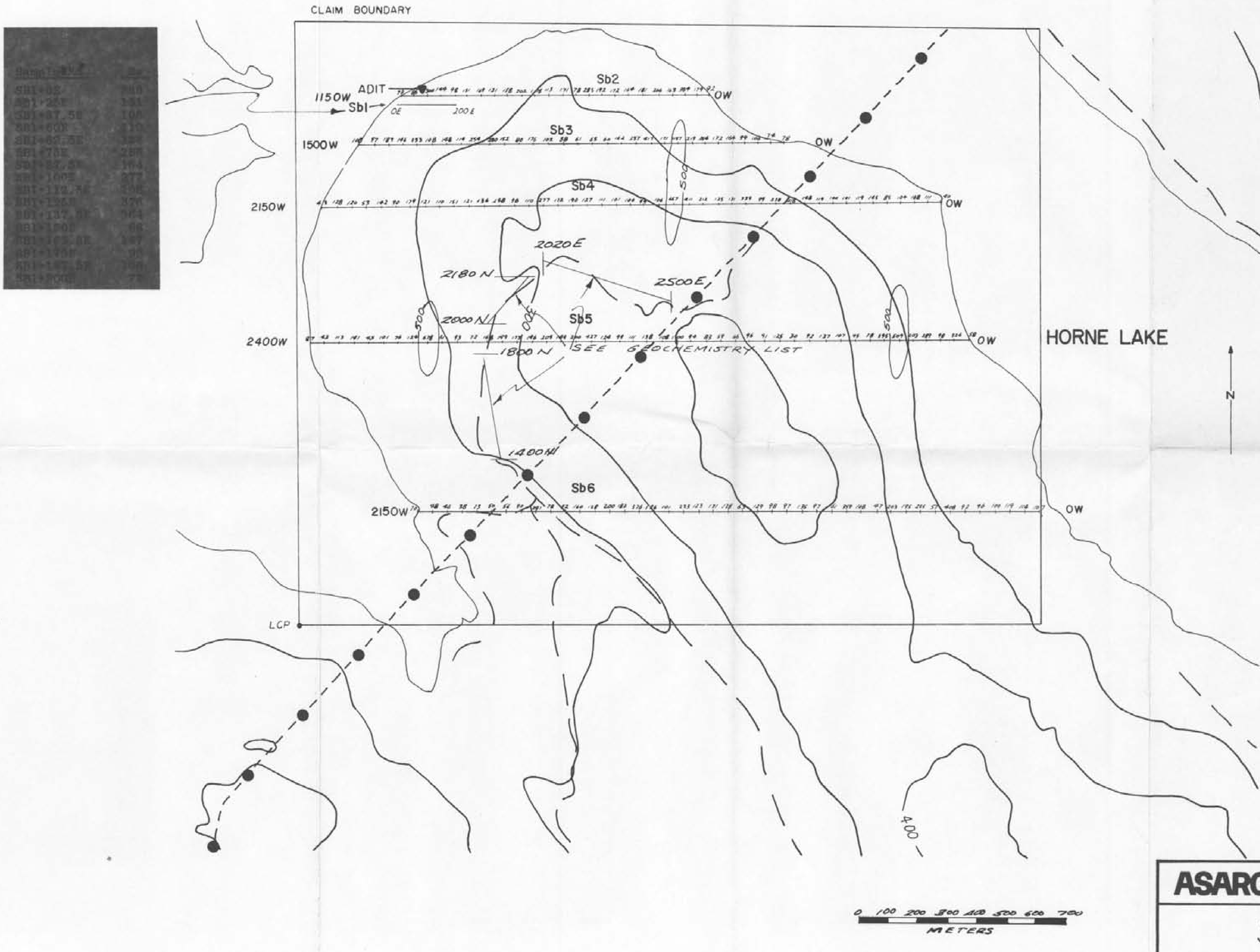
ZINC (PPM)

Drawn by	Date	N.T.S.	SCALE
A P H	NOV 82	92 F/7	1:10,000

ATTACHMENT "I"

GEOLOGICAL BRANCH
ASSESSMENT REPORT

11,024



ASARCO Vancouver

Sb CLAIMS

GEOCHEM GRID

BARIUM (ppm)

Drawn by	Date	N.T.S.	SCALE
A P H	NOV 82	92 F/7	1:10,000