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GEOLOGICAL BRANCH ASSESSMENT REPORT 11,670

HELICOPTER ELECTROMAGNETIC SURVEY

SELCO INC.

YMIR AREA, BRITISH COLUMBIA

PROJECT #24H59 FEBRUARY, 1983

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Questor Surveys Limited, 6380 Viscount Road, Mississauga, Ontario L4V 1H3

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INTRODUCTION

An airborne INPUT Helicopter Electromagnetic Survey, project number 24H59, was flown during the month of January, 1983, by Questor Surveys Limited for Selco Inc. The survey block is situated just west of Ymir in the Nelson Mining Division, British Columbia. An outline map of the survey area which was taken from National Topographical Series, sheet number 82F is provided in the Appendix. The operating base was Castlegar, British Columbia, situated approximately 25 kilometres west of the survey area.

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A total of 277 line kilometres were flown.

The principle products of the INPUT Helicopter Electromagnetic Survey are i) the total field magnetic contour map, and ii) the INPUT anomaly maps.

Questor Surveys Limited performed the airborne survey by a Bell 205A-1 Helicopter with Canadian Registration C-GLMC which was adapted for INPUT survey application. The 205A-1 combines substantial power, affordable space for equipment installation and service ceiling of 20,000 feet (unequipped). The INPUT installation consists of the following major additions:-

Equipment	Placement
Transmitter loop and frame	external
Transmitter	external, starboard
Receiver	internal
Recording system	internal
Magnetometer sensor	external, forward
Magnetometer	internal

Radar altimeter	external, starboard
Camera	external, starboard
Bird winch	internal
A.P.U.	external, port

A vertical axis coil was installed within the 'receiver bird' structure. During ferry flights, the 'receiver bird' is cradled beneath the airframe in the same manner as the fixedwing installation.

The equipped helicopter has a range of approximately four hours under optimum conditions. This figure is de-rated by temperature and altitude factors, plus an appropriate margin of reserve for safety, depending on the local setting of the particular survey.

The field personnel consisted of:

Pilot	-	в.	Masson
Navigator	-	н.	Sandau
Operator	-	D.	Borsoi
Engineer	-	J.	Caza
Data Technician	÷.	н.	Sandau

SURVEY PROCEDURE

During the survey, the helicopter maintained a terrain clearance as close to 122 metres as possible, with the E.M. bird at approximately 48 metres above the ground. In areas of substantial topographic relief, the helicopter height exceeds 122 metres for safety reasons. An East-West flight direction and a flight line spacing of 200 metres were established for this project, in order to optimize the electromagnetic coupling between the receiver and the conductive anomalies.

In addition to the flight lines, control lines were flown perpendicular to the flight lines to be used for computer levelling of the magnetic data. In addition, a ground magnetic base station was monitored daily for severe diurnal variations (magnetic storms).

The appropriate details of each flight are logged on the flight logs by the operator-technician. The logs include the flight times, line numbers and fiducial numbers as well as a record of equipment irregularities and atmospheric conditions. One can refer to these in order to relate the flight path film to the geophysical data.

The ground speed of the helicopter, when on line, is strongly under the control of topographic relief and aircraft performance limitations. This causes data to undergo a varying degree of compression and expansion when recorded in equal time increments. The accuracy of the data is determined by that of the flight path recovery.

The navigation was accomplished using airphotos supplied by the client.

MAP COMPILATION

The survey area is comprised of 6 cronaflex positive mosaics supplied by the client. The 6 photo base mosaics are at a scale of 1:5,000. Navigational and flight path recovery maps were produced from these mosaics.

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The navigational maps were used for the direct recovery of the flight path from the 35mm half-frame film negatives. This film is graduated into fiducials which are used in annotating points of similar topographic features. They are accurately plotted using at least one point per major fiducial.

The navigational maps cannot be employed for computer digitizing of the flight path because of shrinkage of the paper base. Therefore, Cronaflex maps with topographic details were utilized to trace the recovery from the navigation maps and for digitizing.

The Cronaflex with the flight path information has been combined photographically with the appropriate survey results to yield 6 INPUT maps and 6 magnetic contour mylars at a scale of 1:5,000. White prints of these are provided in the map pockets of this report.

INTERPRETATION

The most common types of bedrock conductors intercepted by the INPUT airborne system are those of massive sulphides, massive magnetite and graphite. In special circumstances, they produce strong and narrow INPUT responses of moderate to high conductivity proportional to the amount of sulphides, magnetite and/or graphite present. This is not always the case, since some sulphide deposits are known to produce poorer responses which may be attributed in part by the following circumstances:

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- 1. the conductor is sub horizontal;
- the mineralogy does not lend itself to be detected by electromagnetic methods;
- 3. the conductor is not massive but vein-like;
- there is a lack of continuity of individual veinlets;
- 5. the conductor width is small;

It should be noted that an INPUT response can also result over fault or shear zones containing conductive material. This material could be clay, saline or mineral alteration. Distinguishing these responses from genuine conductors, using only airborne data, is virtually impossible.

In areas of thin or nonconductive overburden, maximum penetration of INPUT system is likely and the masking effect of any underlying bedrock conductor would be minimal. In this instance, weaker responses in the order of two and three channels originating from the bedrock, would be indicative.

A number of targets have been selected and summarized. These were primarily chosen because they exhibit one or more of the following qualities:

- a) fair to excellent E.M. response character;
- b) bedrock origin;
- c) moderate to high conductivity-thickness values;
- d) magnetic association;
- e) favourable geological location as interpreted from the contoured magnetics.

The following summarizes the parameters and terms associated with each selected INPUT target:

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Final

Anomaly: An anomaly is designated by a flight line number and

a suffix letter, for example:

60010A

- 6 first digit signifies the block;
- 001 next three digits signifies the flight line number (900 series - tie lines);
 - 0 fifth digit signifies the number of reflys;
 - A a letter is assigned to each anomaly which relates to their sequential order along the flight line. QUESTOR'S alphabet is: ABCDEFGHJKLMNPRSTWYZ.

Anomaly Fiducial: The position in which the anomaly is located along the recovered flight path. A lag factor of a half subfiducial has been applied.

CHS : The number of channels displayed by the anomaly.
CH1.AMP : A computer estimate of channel 1 amplitude in units
of parts per million. For those amplitudes that
exceed the bottom of the analog record, a value of
6000 ppm is assumed.

CH2.AMP : A computer estimate of channel 2 amplitude in units of parts per million. A graduation on the analog record is equivalent to 30 ppm.

Siemens : The conductivity-thickness product in siemens. One siemen is equivalent to one mho.

Magnetic

Fiducial: The location of a correlating magnetic anomaly. These are flagged on the flight path. A lag factor of a half subfiducial has been applied.

Value : The magnitude of the magnetic anomaly, in gammas.

Alt. : The altitude of the aircraft above the ground surface, in feet.

RESULTS AND RECOMMENDATIONS

Three papers which had documented the INPUT responses of a vertical axis receiver coil over different geologic geometries were located and are listed at the back of this report.

Numerous INPUT anomalies were intercepted during the survey and all of them have been plotted on the maps.

H.W. Little (1960) suggested in his geologic report that a major syncline passes through the survey area in a North-South direction. With this assumption, it is probable that most conductors intercepted in this area are dipping conformably. However, the ability to discriminate a vertical conductor from a dipping conductor or a horizontal ribbon, or vice versa, was complicated by the interference between anomalies. Therefore, only an approximate strike location of the conductors could be interpreted. These interpreted conductors may dip vertically or at an angle, or lie in an horizontal position. Only in some instances, the dip direction was concluded because the INPUT responses exhibit the following characteristic: i) stagger of the INPUT peak

and ii) comparison of line to line responses with model curve (G.J. Palacky, 1974)

 Interpretation of magnetic responses gives extra information in some cases. Nevertheless; the direction of dip is not conclusive and ground geophysical and geological surveys are required for confirmation.

A large area of overburden has been outlined on map sheet number 1. An examination of the analogue records revealed that channels 1 to 4 responses observed are larger than the maximum response the system can record. The responses indicate that the conductors are either very conductive or surficial. The anomalous response of the later channels are also an indication of the presence of a thick conductive layer.

In some cases, when two conductors are dipping to each other as indicated on the interpretation map, it is probable that they may form one conductor. Most conductors in map sheet 1 are associated with surficial overburden except conductor 7 which may be formational and of graphitic origin.

All conductors on map sheets 2 and 4 are interpreted as surficial overburden.

Map sheets 3, 5 and 6 represent a more resisitive area of this survey block. Many conductors of these three map sheets are probably structural, associated with the anticline-syncline system which passes through this area. Conductors are striking in a NNW-SSE direction at the southern half of map sheet 3. On the northern half of map sheet 3, the strike direction changes into a NNE-SSW direction. In map sheet 5, the conductors are

- 8 -

striking in an approximate north-south direction except Conductor 9.

Four Conductors 1,2,3 and 8 were selected in map sheet 3 because of thin short strike length and an association with a probable intrusive, suggested by magnetic response. However, the relatively low conductance, 5 siemens for Conductor 1 and 3, degrade their priority. Because of the better decay response and conductance value of conductors 2 and 8, a medium priority is designated. The north-south trending conductors found in map sheet 5 and 6 appear to be formational. Downwarp, upwarp are apparent from the magnetic responses of these two map sheets. Also, an intrusive exits at the northwest corner of map sheet 5.

Four Conductors 4,5,6 and 9 are selected in map sheet 5 because of their short strike length and apparent association with magnetics. Conductor 4 is a poor priority because of the poor decay response and low conductance value. Conductors 5 and 6 exhibit good decay response and fair conductance value. Conductor 9 is given a higher priority because of its sharp response, high conductance value and good decay response. The magnetic association suggests pyrrhotite may be the source material.

> Respectfully submitted, QUESTOR SURVEYS LIMITED

S. Wor

S. Wong, Geophysicist.

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APPENDIX

EQUIPMENT

The helicopter is equipped with a Mark VI INPUT ^(R) E.M. system and Sonotek P.M.H. 5010 Proton Magnetometer. Radar altimeters are used for vertical control. The outputs of these instruments together with fiducial timing marks are recorded by means of galvanometer type recorders using light sensitive paper. Thirty-five millimeter half frame cameras are used to record the actual flight path.

BARRINGER/QUESTOR MARK VI INPUT (R) SYSTEM

The Induced Pulse Transient (INPUT) system is particularly well suited to the problems of overburden penetration. Currents are induced into the ground by means of a pulsed primary electromagnetic field which is generated in a transmitting loop around the helicopter. By using half sine wave current pulses and a loop of large turns-area, the high output power needed for deep penetration is achieved.

The induced current in a conductor produces a secondary electromagnetic field which is detected and measured after the termination of each primary pulse. Detection is accomplished by means of a receiving coil towed behind the helicopter on two hundred and fifty feet of cable, and the received signal is processed and recorded by equipment in the helicopter. Since the measurements are in the time domain rather than the frequency domain common to continuous wave systems, interference effects of the primary transmitted field are eliminated. The secondary field is in the form of a decaying voltage transient originating in time at the termination of the transmitted pulse. The amplitude of the transient is, of course, proportional to the amount of current induced into the conductor and, in turn, this current is proportional to the dimensions, the conductivity and the depth beneath the helicopter.

The rate of decay of the transient is inversely proportional to conductivity. By sampling the decay curve at six different time intervals, and recording the amplitude of each sample, an estimate of the relative conductivity can be obtained. By this means, it is possible to discriminate between the effects due to conductive near-surface materials such as swamps and lake bottom silts, and those due to genuine bedrock sources. The transients due to strong conductors such as sulphides exhibit long decay curves and are therefore commonly recorded on all six channels. Sheetlike surface materials, on the other hand, have short decay curves and will normally only show a response in the first two or three channels.

The samples or gates are positioned at 340, 540, 840, 1240, 1740 and 2340 micro-seconds after the cessation of the pulse. The widths of the gates are 200, 200, 400, 400, 600 and 600 micro-seconds respectively.

For homogeneous conditions, the transient decay will be exponential and the time constant of decay is equal to the time difference at two successive sampling points divided

(ii)

by the log ratio of the amplitudes at these points.

SONOTEK P.M.H. 5010 PROTON MAGNETOMETER

The magnetometers which measure the total magnetic field have a sensitivity of 1 gamma and a range from 20,000 gammas to 100,000 gammas.

Because of the high intensity field produced by the INPUT transmitter, the magnetometer results are recorded on a timesharing basis. The magnetometer head is energized while the transmitter is on, but the read-out is obtained during a short period when the transmitter is off. The precession frequency is being recorded and converted to gammas during the 0.2 second interval when there is no power in the transmitter loop.

For this survey, a lag factor has been applied to the data. Magnetic data recorded on the analogue records at fiducial 10.00 for example would be plotted at fiducial 9.95 on the mosaics.

The magnetometer has two scales, a coarse and a fine scale. The fine scale indicates a 10 gamma change for a 1 cm. change in amplitude. The coarse scale moves 2 mm. (or 1 division) for a 100 gamma change with gamma range with 1 gamma sensitivity.

DATA PRESENTATION

The symbols used to designate the anomalies are shown in the legend on each map sheet and the anomalies on each line are lettered in alphabetical order in the direction of

(iii)

flight. Their locations are plotted with reference to the fiducial numbers on the analog record.

A sample record is included to indicate the method used for correcting the position of the E.M. Bird and to identify the parameters that are recorded.

All the anomaly locations, magnetic correlations, conductivity-thickness values and the amplitudes of channel number 2 are listed on the data sheets accompanying the final maps.

GENERAL INTERPRETATION

The INPUT system will respond to conductive overburden and near-surface horizontal conducting layers in addition to bedrock conductors. Differentiation is based on the rate of transient decay, magnetic correlation and the anomaly shape together with the conductor pattern and topography.

Power lines sometimes produce spurious anomalies but these can be identified by reference to the monitor channel.

Railroad and pipeline responses are recognized by studying the film strips.

Graphite or carbonaceous material exhibits a wide range of conductivity. When long conductors without magnetic correlation are located on or parallel to known faults or photographic linears, graphite is most likely the cause. Contact zones can often be predicted when anomaly trends coincide with the lines of maximum gradient along a flanking magnetic anomaly. It is unfortunate that graphite can also occur as relatively short conductors and produce attractive looking anomalies. With no other information than the airborne results, these must be examined on the ground.

Serpentinized peridotites often produce anomalies with a character that is fairly easy to recognize. The conductivity which is probably caused in part by magnetite, is fairly low so that the anomalies often have fairly large response on channel # 1, they decay rapidly and they have strong magnetic correlation. INPUT E.M. anomalies over massive magnetites show a relationship to the total Fe content. Below 25-30%, very little or no response at all is obtained but as the percentage increases the anomalies become quite strong with a characteristic rate of decay which is usually greater than that produced by massive sulphides.

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Commercial sulphide ore bodies are rare and those that respond to helicopter survey methods usually have medium to high conductivity. Limited lateral dimensions are to be expected and many have magnetic correlation caused by magnetite or pyrrhotite. Provided that the ore bodies do not occur within formational conductive zones as mentioned above, the anomalies caused by them will usually be recognized on an E.M. map as priority targets.

(v)



Representative INPUT Magnetometer and Altimeter Recording

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CTHAL	ANOHALY					MAGNETTO		
FINAL	ANUMALY		-	CUO AND	OTENEND	FIDURIAL	HALINE	4
ANOMALY	FIDUCIAL	CHS	CH1+AMP	CH2.AMP	STEMENS	FIDUCIAL	VALUE	A
100100	11,862	6	6394	3210	37	-	-	4
10010B	12.904	6	6394	3210	45		-	4
100100	14.152	6	6394	3209	53	-	-	4
100100	14.643	6	6394	3209	52	+	8	4
10010E	15.298	6	6394	3209	39	15.10	2	4
10010F	16.047	6	3635	2414	28	-	-	4
100106	17,272	6	6395	3209	51	100		4
10010H	18,003	6	6395	3209	NC	100	-	9
10010J	18,297	6	6395	3209	NC			4
10010K	19.947	6	6395	3208	33	19.80	12	4
10010L	20.367	5	6395	3208	32	20.55	47	4
10010M	21,281	6	6395	3208	NC	-	**	4
10010N	21.448	6	6395	3208	NC	21.40	15	4
10010P	21.683	6	6395	3208	NC	-	-	4
10010R	21.881	6	6395	3208	NC	21.80	67	4
100105	22.147	6	6395	3208	64	22.20	82	4
100101	23.614	6	580	412	45	-	-	4
10010₩	23.925	6	5658	3207	57	-	-	4
10020A	25.679	6	180	140	27	-		2
10020B	25.999	6	6395	3207	NC	-	-	4
10020C	26.328	6	6395	3207	NC	26.40	15	1
100200	27,100	6	4530	2625	15	-	-	1
10020E	28.325	6	6396	3205	57	-	-	- 2
10020F	29.322	6	6396	3206	NC	-	-	1
10020G	29.747	6	6396	3205	54	-	4	
10020H	30,216	6	6396	3205	51	0.000		1
10020J	30.509	6	6396	3206	45		-	
10020K	30.936	6	6396	3206	68	31.00	52	1
10020L	31.315	5	6221	3206	57	-	-	5
10020M	32.028	6	6396	3205	37	-	9	
10020N	32.745	6	6396	3205	39	-	-	
10020F	34.049	6	6396	3205	NC		-	1
10020R	34.394	6	6396	3205	HC	-	-	
100205	34.900	6	5109	3205	40	-	-	
100306	40.245	4	3215	2107	26	-	-	3
100308	41, 299	4	6397	3203	42	-	-	
100300	42,080	6	6397	3203	NC	-	-	1
100300	42.499	Å	5484	3203	49	-	_	1
10030E	43,048	6	6397	3203	33		241	1
10030F	43,722	6	6397	3203	64	4		
100306	44,173	6	6397	3203	NC	-	-	
10030H	45,249	6	3903	2621	NC	-	-	
10030J	46.147	6	6397	3202	NC	0.441	-	3
10030K	46.797	6	6175	3202	45	-	-	
10030L	47,519	6	6397	3202	65		200	
10030H	47.848	6	6397	3202	59	-	-	-
10030N	48.695	6	6397	3202	70	-74	-	
10030P	49.146	6	6397	3201	69	49.05	1	4
100308	49.547	6	6397	3201	58	-		

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FINAL	ANUMALY FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	MAGNETIC FIDUCIAL	VALUE
100305	49.949	4	6397	3201	45		
100303	50.499	6	6397	3201	43	50.55	53
100304	50,842	6	6398	3201	39	50155	00
100300	51.494	6	6378	3201	NC	21	
100707	50 740	5	770	470	25	-	-
100302	52+747	2	/100	432	25		
1003000	54 135	6	4700	3200	At		
1003088	54+125	0	0370	3200	91		
1003000	54,450	0	0378	3200	ni.	-	-
100406	55.595	6	1417	903	24	55.45	6
10040B	56.199	8	6.398	3200	NE	-	
100400	56.546	5	6398	3200	50	-	_
100400	57,110	4	4799	1200	51	-	_
10040E	58.089	Ă	6398	3199	61	_	-
10040F	58.444	6	6399	3199	NC	-	-
100406	50.044	4	4700	3100	21	50 05	20
100400	59.004	0	4700	7100	21	30.73	20
100401	60 000	0	4700	3199	NC		-
100405	00.776	0	6376	7100	Et	(1	70
100406	01+344	0	6398	3199	51	51,40	70
10040L	61.916	6	6398	3198	NL		-
100400	62.4/1	0	6399	3198	NIC:	100	-
10040N	53.446	6	6180	3198	87	-	
10040P	63,897	6	6336	3198	80	64.00	64
10040R	64.748	6	6399	3198	NC	-	-
100405	65.194	6	6399	3198	NC	-	-
10040T	65.596	6	6399	3198	29	140	-
10040W	66.043	6	4905	2804	19	-	-
10040Y	66.643	6	4499	2418	15	-	-
10040Z	67,491	6	6399	3197	33	67.35	5
1004000	68.289	6	6399	3197	NC	68.25	91
10040BB	68.671	6	6399	3197	46	-	-
10040CC	69.195	6	6399	3197	38	68.95	-47
10040DD	69.619	6	5859	3197	29	69.20	6
10040EE	70.174	6	6399	3197	25	+	4
10040FF	70,598	6	3302	2051	25	-	Ť
		4					
100504	74.039	0	4936	2989	20	74 01	
100508	/4./4/	0	6400	2149	39	74.80	34
100500	75.090	6	6400	3195	.313	1.00	175
100500	75.257	6	6400	3195	37	+	-
10050E	75+946	5	6400	3195	NC	-	
10050F	76.622	6	6400	3195	23	76.45	41
10050G	77.046	6	4309	2348	16	1.44	-
10050H	78,197	6	6400	3195	NC	-	-
10050J	78.994	6	6400	3195	NC	78.90	60
10050K	80,194	6	6400	3194	NC	-	-
10050L	80.744	6	6400	3194	NC		-
10050H	81.922	6	6400	3194	NC	-	-
10050N	82.728	5	6228	3194	52	100	-
10050P	82.971	6	6400	3194	43	-	-
10050R	83,269	6	6400	3194	52	83.15	37
100500	84.198	6	6400	3193	NC		-
100303							

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FINAL ANDMALY	ANDMALY FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	MAGNETIC FIDUCIAL	VALUE	6
						the lot, day any the rol and an		1
100500	80.679	0	6401	3173	NU	05 05	3	
100501	85.943	0	8401	3193	28	82.43	1	
100502	86.331	6	6401	3193	51	01 50		1000
10050AA	86,466	6	6401	3193	54	86.00	36	1
10060A	87.495	6	6401	3193	38	-	-	
10060B	89.070	6	6401	3192	34		-	1
10060C	89.497	6	6401	3192	39		15	
10050D	90.593	6	6401	3192	NC	-	-	
10060E	90.792	6	6401	3192	NC	-	-	
10050F	91.243	6	5401	3192	43	-	-	3
100606	92.262	6	6401	3191	42	92.15	49	
10060H	92.798	5	5401	3191	61	-1	-	
10060J	93,222	6	6401	3191	54	-	1	
10060K	93.515	6	6401	3191	NC	-	÷-	9
10060L	94.043	6	6401	3191	38	94.15	15	3
10060M	94.792	6	5576	3191	58		-	
100501	95.554	6	6401	3191	NC	-	-	
10060P	96.337	6	6402	3191	34		-	
10060R	97.267	6	6402	3190	NC	-	-	
100605	97.592	6	6402	3190	39	-	1	
100601	97.867	6	6402	3190	47	-	2	
100600	98.097	6	3642	2481	29		-	
10060Y	98.719	4	420	281	21	98.85	275	
	10703.01	50 1	101	2014-1	20		1.1	
10061A	99.549	6	6402	3190	NC			
10061B	101.371	3	60	30	4	101.35	191	
10061C	101.994	2	60	30	NC		-	
10061D	102.265	2	60	30	NC	-	-	
100704	106.197	4	2690	1952	47		_	
100708	100.177	2	4707	7100	57	1.00	-	
100705	106, 340	0	4/8/	3100	33	-	-	
100700	107 275	0	4070	2024	52	-		
100705	107.233	4	4971	7100	17			
100705	100 074	6	40/1	3100	50			
100706	100.030	2	6407	7100	JO			
100708	100,300	4	6403	7100	NC	1.4		
100701	107.303	°,	6403	3100	NC	-		
100703	109.040	0	6403	3187	NC		2	
100706	110,436	0	0403	3107	52	-	-	
10070L	111+522	0	6403	318/	13	-	-	
100708	112,398	2	1600	1117	36	112.25	17	
100700	113.186	0	6403	318/	5/	-	-	
10070P	113.556	6	6403	3187	45		-	
10070R	113.868	6	6403	3186	NC	113.90	28	
100705	114.795	6	6403	3188	42	-	-	
10070T	115.043	6	6403	3186	NC	115.25	45	
10070W	116.095	6	6228	3186	37	-		
100804	116.993	6	6403	3186	11	1	2	
10080B	118,094	6	6403	3186	NC	-	-	
	*******			an al parts				

						2		
FINAL	ANOMALY					MAGNETIC		
ANOMALY	FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	FIDUCIAL	VALUE	ALT
100800	118,670		6403	3185	NC	-		197
100800	119,143	6	6404	3185	NC	-	4	332
10080E	119,888	6	6404	3185	NC	119.85	4	366
10080F	120,768	6	1322	963	49	-	-	376
10080G	121.291	6	6404	3102	11	-	-	440
10080H	121.745	6	2551	1667	29		***	452
10080J	122.196	6	6404	3185	NC	-	-	404
10080K	122,692	6	6404	3184	53	122.85	26	500
10080L	123.545	6	6276	3184	57		-	427
10080M	124.316	6	6404	3184	47	1221	2	392
10080N	124.912	6	4598	3089	· NC	-	-	422
10080P	125.398	6	2901	1976	38	-	-	419
10080R	127.324	3	60	30	2	127.45	223	443
						175 10	-	
10090A	135.675	6	6405	3181	NC	135.60	29	410
100908	136.018	6	6386	3181	65	-	-	448
100900	136,541	0	6405	3181	36	-		452
100900	138.947	6	5549	3181	35	136+85	13	400
10090E	137.642	0	2952	1893	36	12.1	-	422
10090F	137.944	6	32/4	1922	26	32	1	502
100906	138,544	0	6405	3181	12	•	-	411
10090H	138,998	6	4080	2632	NC	-	-	451
10090J	139.549	6	6405	3181	NG	139.60	13	400
100906	140.433	0	4/18	2880	NL	-	-	400
10090L	141.944	6	6406	3180	15	142.05	7	427
10090M	143.147	6	6406	3180	34		-	399
10090N	143.743	6	6406	3180	27	143.60	38	357
10090P	144.013	5	6390	3180	20	-	-	440
10090R	144,492	6	6303	3179	19	-	÷	416
10091A	16.692	3	60	30	10	-	-	434
10091B	19.420	2	60	30	NC	-	<u>_</u>	334
10091C	20.435	6	2572	1749	37	-	-	467
10091D	20.891	6	6147	3193	43	21.00	22	402
10091E	21.541	6	5897	3193	36	-	-	416
10091F	22.393	6	6388	3193	58	-	-	424
100916	22.739	6	6388	3193	55	1 	-	460
10091H	23.506	6	6388	3193	NC	-	-	360
10091J	24.444	6	6388	3193	NC	-	-	427
10091K	25.518	6	6388	3194	NC	-	-	406
10091L	26.067	6	5388	3194	NC	-		403
10091M	27.163	6	3644	2423	23		-	383
10091N	28.016	5	5822	2756	12	-		419
10091P	29.773	6	6388	3194	35	-	-	408
10091R	30.468	6	6388	3194	NC	-	-	351
100915	30.942	6	6388	3194	NC	-	-	408
10091T	31.420	6	6388	3194	39	31.60	52	458
10091W	32,210	Б	3906	1968	13		-	498
101014	24.447	- 14	10	16				510
101010	39:16/	3	150	30	12	74.05	0	010
101010	76 144	3	2221	1.41272	12	04400	1	474
101010	33.104	2	3/31	24435	0		-	422

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FINAL	ANOMALY FIDUCIAL	CHS	CH1.AMP	CH2.AMP	STEMENS	MAGNETIC FIDUCIAL	VALUE
10101D	36.191	6	6388	3194	162	36.05	9
10101E	36.416	6	4388	3194	NC		-
10101F	36.682	6	6388	3194	NC.		***
101016	37.264	6	5388	3194	NC	-	-
10101H	38,068	6	6388	3195	NC	38.00	8
10101J	38.912	5	1200	868	51	38,75	75
10101K	39,690	5	6388	3195	NC		-
10101L	40.421	6	6384	3195	38	-	
10101M	40.696	6	5081	3195	44	-	-
10101N	42,122	6	6388	3195	33	1	100
10101P	42.397	6	6388	3195	29		-
10101R	43.045	6	6388	3195	56	-	-
101015	45.919	2	60	30	NC	~	-
10101T	46.373	2	60	30	NC	-	-
10101W	48.597	1	30	-	NC	-	-
10101Y	50.197	2	60	30	NC	-	-
10101Z	50.540	1	30	-	NC	-	+
10101AA	51.239	2	60	30	NC	-	-
101100	54 700	i.	70		NC		
101108	40.414	Å	4799	7194	50	-	-
101106	41 344	4	4700	3170	37		
101100	01.240	0	6306	3176	71		
101100	61+343	0	6388	3196	31		- 2
TOTTOE	61.940	0	0300	3170	34		
101106	02+322	5	1030	007	10	-	
101100	02+940	4	1731	1007	12	17 48	10
101101	03+411	0	3784	1723	13	03.40	12
101103	04+278	0	6388	3197	01	-	
101108	64,921	6	6388	3197	39	-	-
TOTTOL	031240	0	0388	3197	33		~
10110M	65.746	5	3119	1912	22		
10110N	66,148	6	3025	1986	29	66.10	24
10111A	66.869	6	1416	931	33	67.00	46
10111B	67.140	6	6388	3197	NC	-	-
10111C	57.645	4	2128	1155	13	-	+
10111D	68.195	6	4000	2909	NC	68.05	76
10111E	68.543	6	5675	3197	54	68.55	12
10111F	69.003	6	6388	3197	NC	-	-
101116	69.666	6	6219	3197	23		-
10111H	69.941	5	2050	1300	22	-	
101111	71.194	2	513	99	NC	-	-
10111K	71,636	2	103	32	NC	71.55	52
10120A	74.447	2	60	33	NC		-
10120B	75.498	6	328	234	36		-
101200	76+245	6	6388	3198	22		-
101208	76.895	6	6388	3198	22	**	
10120E	77.964	5	1688	859	16	100	-
10120F	78.790	6	6388	3198	55		-
101206	78.948	6	6388	3198	45	-	17
10120H	79.496	6	3275	1959	21		-

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						VIOUETTO		
FINAL	ANUMALY	ene		CUT: AND	OTHER	MAGNETIC		
ANUMALT	FILULIAL	CHS	CH1.AMP	CH2+APP	STEMENS	FIDUCIAL	VALUE	ALI
101201	79.947	4	1751	1823	19			452
101206	80.796	7	2175	889	10	-	-	351
101201	81.941	6	1338	775	35	-	**	432
10120M	82.320	6	6388	3198	32	-	-	383
10120N	82.847	6	6388	3198	42	-	-	490
		Charles .		10.001.00	1.14725			1000
10121A	88.396	2	60	30	NC	-		507
101306	99.747	2	60	30	NC		-	454
10130B	103,891	6	6388	3200	32	-	-	448
10130C	104.147	6	6388	3200	28	1	14	435
101300	104.995	6	6388	3200	NC	104.90	S	414
10130E	105.897	6	1759	1061	16	_	_	472
10130F	106.425	6	1528	959	17	-	·	431
10130G	106.750	6	5988	3200	17	40	-	459
10130H	107.169	6	5509	3200	29	-	-	415
10130J	107.948	6	5681	3200	46	**		508
10130K	108.169	6	6103	3200	45	-	-	408
101301	109.193	4	950	688	28	-		443
10130M	110.493	6	4363	2885	NC	-	-	428
10130N	110.897	6	5909	3200	51	-	-	356
10130P	111.538	6	4378	2488	17	-	-	394
10140A	117.671	4	256	187	14	2	**	366
10140B	118.244	6	3150	1704	20	-		390
10140C	120.296	6	3350	2300	37	**	-	467
10140B	120.689	6	6388	3201	38	-	+	362
10140E	121.720	6	6388	3201	11	-	-	424
10140F	122.492	6	3266	1622	10	-	-	434
10140G	123.141	6	6388	3201	18			440
10140H	123,593	6	6388	3201	27	7	75	488
10140J	127.074	2	60	30	NC	-	-	474
101504	177 407		.7	70	2			
101500	141 004	4	4041	2007	2	-		4/2
101500	142,270	6	5959	3205	15	-	-	430
101500	142,892	4	4972	2105	7	3.1	-	766
101505	147.099	4	2484	1101	0		-	000
10150F	143.691	6	3366	1520	13	-	-	472
101506	143.944	6	3941	2298	21	-	-	490
10150H	144.273	6	3297	2198	37	2		504
10150J	144.783	6	1469	837	32	-	2	432
10150K	145.417	3	875	541	21	145.30	5	360
101501	145.744	6	4375	2575	22	-	-	383
10150M	146.996	6	1919	985	14	-	-	384
10150N	149.480	2	75	43	NC	-	-	368
1000000			1.2	115	0.5			1000
10150A	153.765	5	328	188	17	-	-	448
10160B	154.217	6	2156	1226	19		-	394
10160C	155.216	4	1313	738	19	-	-	408

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FINAL	ANDMALY	200	-	010 400	ATTUTUO	MAGNETIC			
ANDMALY	FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	FIDUCIAL	VALUE	ALI	
101200	154 400	4	4700	7204	A7			506	
101600	157 120	4	4904	3204	37		-	476	
101602	157.120	2	4000	2204	17			409	
101606	159.071	2	7070	1974	12	**	1	408	
101806	150.021	0	3770	1507	7			400	
10160H	150.040	3	4704	1307	15	150 00	27	479	
101603	158,964	6	5104	3204	15	130.90	21	492	
101600	1371373	0	3108	2200	20			507	
10180L	159./49	0	4671	2789	20	-		303	
101800	163.3/4	1	50	-	NL	-	-	404	
10170A	174.419	2	84	43	NC	191	**	415	
10170B	175,838	5	1203	640	12	-	-	443	
10170C	176.470	6	2578	1529	15	-	-	371	
101700	176.722	6	2816	1274	14	176.65	179	382	
10170E	176.998	5	2106	928	13	-1	-	400	
10170F	177.556	6	1797	904	21	4	-	365	
101706	178.318	6	3422	1842	15	178.40	7	366	
10170H	178,570	6	4247	2311	15	-	-	378	
10170J	179.247	6	6388	3206	NC	179.10	86	386	
	200000	2	2222		1.100	1201022	20		
			75		110				
101814	11.144	1	35		NU	-	-	38/	
101818	12.844	1	826	7101	NC	17.00		505	
101810	13.244	6	63/2	3181	NC	13.20	47	394	
101910	13+944	6	4147	2399	15	-	7	382	
10181E	14.241	6	3563	1759	13	14.15	4	411	
10131F	14.745	6	5/13	2339	10	-	-	446	
101816	15.241	4	1657	872	10	-	**	510	
10181H	15,742	4	701	384	14	-	-	526	
10185A	104.598	1	144	-	NC	÷	-	472	
10185B	107.880	3	195	90	7	-	-	393	
10185C	109.283	6	1126	571	20	-	-	488	
101850	109.918	6	6386	3190	41	-	-	507	
10185E	110.464	6	2414	1488	19	-	**	452	
10185F	110.716	6	3167	1579	13	-	-	452	
10185G	111.366	6	6139	2658	9		-	484	
10185H	111,871	5	2129	1087	10	-	-	510	
10185J	112.417	5	998	530	14	- 1	-	520	
10185K	115.330	3	117	30	4	**	**	442	
10185L	115.713	3	114	34	3	-	-	456	
10190A	189,322	3	163	55	11	-		350	
10190B	191.672	6	6388	3207	NC	191.60	96	370	
101900	192.352	6	3581	2112	18	-	2	387	
101900	193.795	6	2850	1130	17	-	-	432	
10190E	194.039	6	2959	1141	13	194.10	146	442	
10190F	194.445	6	2916	1568	13	+	-	474	
101906	195.244	4	1472	732	11			504	
10190H	198,621	2	60	30	NC	-	-	464	
10190.1	199,156	2	60	30	NC	-	-	411	
10190K	199,522	ĩ	38		NC	-	-	482	
			19. A. V.		20.00				
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FINAL	FINAL ANOMALY DMALY FIDUCIAL		NAL ANOMALY ALY FIDUCIAL CHS		CH1,AMP CH2,AMP		SIEMENS	MAGNETIC FIDUCIAL VALUE		ALT
101901	100.010	2	40	30	NC		_	442		
101904	202 700		50		NC		-	500		
101900	202,377	1	27		NC	1		309		
10200A	29.997	5	480	237	12	-	-	387		
10200B	30.444	5	639	303	13	-	-	422		
10200C	31,120	6	2836	1789	24	-	-	394		
102000	31.890	5	2761	1419	12	31.85	24	400		
10205A	93.896	3	281	122	9	-	-	512		
10205B	94.492	5	947	455	11	94.55	59	484		
10205C	95.114	6	1466	684	16	95.05	20	376		
10205D	95.489	6	1297	681	21	-	-	459		
10205E	96.344	6	2735	1538	21	96.50	21	464		
10205F	96.994	6	1838	1088	18		-	442		
102056	98.063	4	513	236	11	98.15	24	392		
102120	44,465	3	325	139	14	-	2	432		
102128	44.944	6	2390	1286	15	-	-	425		
102120	45.323	6	2769	1655	22	-	-	464		
102120	46.043	4	475	222	12		-	440		
10212E	46,595	3	45	30	1			440		
10213A	53.624	1	72	-	NC	-		427		
10220A	56.495	5	1351	660	8	-	-	504		
10220B	56.820	4	691	232	5	56.80	17	483		
10220C	66.716	1	61	-	NC	-	-	428		
10220D	67.948	3	430	160	6	-	-	398		
10220E	68.397	3	380	158	7	-		383		
10220F	68.798	2	223	108	NC	-	17	363		
102206	69.768	6	505	294	21	-	-	371		
10220H	69.994	6	755	458	19	-	-	395		
10220J	70.414	6	1093	611	14	-	-	408		
10231A	84.277	6	1671	894	14	84.20	32	435		
10231B	84.651	6	1384	810	23	-	-	478		
102310	91.289	2	241	30	- NC			484		
102310	92.119	2	128	41	NC	-	-	506		
10231E	93,768	1	60		NC	-	-	386		
10236A	76.264	6	2074	1138	16		-	458		
10236B	76.638	6	3252	1976	24	-	-	475		
10236C	77.346	6	783	368	12	-	-	504		
102360	77,762	3	233	113	10	-	-	506		
10236E	80.025	2	60	30	NC		-	382		
10236F	83.519	2	60	30	NC	*	-	448		
102356	83.930	3	109	36	7		-	476		
10236H	84.638	2	60	30	NC		-	467		

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	F INAL ANDHAL Y	ANOMALY FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	MAGNETIC FIDUCIAL	VALUE	ALT
	102320	119.344	1	61		NE			491
	102378	122.695	2	268	30	NC	-		466
	102370	126.442	2	109	39	NE	4.	1	437
	102370	127.722	3	131	47	6	-	-	430
	102375	129 340	7	194	57	5	20	<i>a</i> .	454
	102376	100 004	7	240	94	4	2	2	442
	102376	120.544	7	280	122	7	-		418
	102370	127 010	5	1225	577	0		-	440
	102378	132.017	3	1223	000	7	-		440
	102373	132.937		781	207	0		10	420
	102376	122+737	4	101	307	0		-	4.30
	10237L	133,893	3	162	55	0		172	440
	1023/M	134+618	3	112	42	5		-	502
	102406	98.523	1	135	4	NC	÷.	2	430
	10240B	98,875	1	135	-	NC	-		474
	10240C	103.699	1	176	-	NC	-	-	479
	102400	104.244	2	201	78	NC	-		460
	10240E	104.614	3	217	105	9	-	-	358
	10240F	106.670	5	1054	477	10	-	-	448
	10240G	107.117	3	623	211	7		-	414
	10240H	107.392	4	714	269	8	-	-	400
	10240J	108.741	2	117	43	NC	-	-	422
	10251A	116.844	4	461	208	9	-	-	392
	10251B	117.047	4	455	224	10	-	-	434
	102510	117.720	5	1011	458	5		-	376
	102510	117,990	4	1189	427	7		*	354
	102524	118,537	4	274	124	9	-	-	498
	10252B	118,794	4	318	138	8	-	-	415
	10252C	119.344	5	311	171	16		**	467
	10252D	122,370	2	255	63	NC	(# ²)	-	406
	102600	132.747	3	184	93	13	-		414
	102408	134.644	4	322	127	Q	-		444
	102600	135,299	6	6263	3196	13	135.30	36	484
	102600	134,849	5	710	315	9		-	424
	102600	177 174	-	1075	100	11	100		414
	102000	177 046	7	522	177	4	177 05	00	427
	102000	170 247	5	307	25	MC	101.00	00	420
	102600	170 040	4	1000	228	7	170 15	102	720
	102604	140 244	1	140	140	MC	137,13	102	414
	102005	140.244	1	107		NC	-		414
	102801	140.9/1	I	13/		NO		-	450
	10260L	141+280	1	144	-	NC	-	-	447
	102604	142+640	1	91	~	NL	-	20	400
	10271A	152.891	4	636	233	8	-	4	402
	10271B	153.234	6	1111	528	13	153.20	124	431
	102710	153.441	6	1442	670	11	-	-	470
e	10271D	154.744	6	6383	3199	15	-	-	507
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FINAL	FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	FIDUCIAL	VALUE	AL
							******	77
10280A	161.310	3	143	62	9		-	46
102808	162.221	5	477	250	15	162.25	153	35
102800	163.218	6	2221	1217	19		-	45
102800	163.692	6	4105	2089	14	-	<u></u>	50
10280E	164.093	6	4618	2783	19	-	-	45
10280F	154.895	6	4821	2498	13	164.95	16	4
102806	165.296	6	1724	906	17	-	-	48
10280H	165.815	6	1955	9.67	15		-	30
10280J	166,884	8	2199	1102	16	57.0	-	40
10280K	167.056	6	2065	1008	17	-	-	38
10280L	167,665	6	2712	1588	23	167,75	162	37
10280M	168.647	4	818	336	8	-	-	42
10280N	168,795	4	721	301	8	-	-	4:
10280P	170,050	2	137	66	NC	-	-	42
10280R	170.776	2	178	79	NC	170.75	45	4
102805	171.218	2	159	63	NC	-	+	4
102801	171,799	2	108	48	NC	-	-	4
10285A	58.631	6	3897	2610	NC		4	5
10285B	59.127	6	2419	1275	18	1.00	100	4
102850	59,840	6	1213	611	17	-	2	4
102850	60.115	6	2241	1308	22	60.20	164	4
10285E	60.810	4	2613	977	8	-		4
10285F	61.301	6	2541	1383	15	(14)	1.00	4
102856	61.518	6	2351	1533	33	0+10	-	4
10285H	61.843	6	6382	3188	52	61.70	61	5
102904	15,053	4	1071	618	20			4
102908	15.789	6	6377	3185	37	15.60	54	4
102900	16.217	6	2774	1777	26	-	-	4
10290B	16.443	6	3636	1967	15		-	3
10290F	16.840	4	3739	1405	8	-	-	3
10290F	17.249	6	1517	786	16		-	4
102906	17,804	6	1820	876	15	-	-	4
10290H	18,137	5	1786	917	16	-	-	4
10290J	19.157	6	1248	623	14	-		5
10290K	19.951	6	3917	2234	15	-	-	4
10290L	20.852	5	4926	2381	11	-	-	4
10290M	21.650	6	1795	988	19	-	-	3
103000	26,983	6	578	284	17			٨
103008	27.347	Å	1325	629	12	-		
103000	27, 499	6	2014	1231	23	-	2	-
10300B	28,270	6	6375	3182	40	-		0
10300F	28,717	6	4375	3192	22	-		
103005	20.000	4	6100	3100	20			5
103006	20,700	6	7400	2150	10	-	-	
103000	30.364	4	907	551	34			
103001	70 744	0	013	ACC	14	2.0		
103005	71.745	X	A774	3182	0		1	1
TABAAN	51.705	0	00/4	0102	1		107.2	1.1

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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	FINAL ANOMALY	ANDMALY FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	MAGNETIC FIDUCIAL	VALUE
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	103001	32.289	 5	 &1.74	3104			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	103001	77 775		4474	3177	9	175-6	10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	103000	33+333	*	4474	2135	10	74.05	50
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10300N	34+17/	0	4290	2210	17	24+23	20
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	103000	34,470	0	3021	2///	17		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10300R	34./10	0	3311	2092	29		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	103005	35.066	6	63/4	3181	150	34.90	120
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	103001	36.347	3	60	30	7	36.20	54
10300Y $38,989$ 2 60 30 NC - 10310A 43,342 2 60 30 NC 43,30 5 10310B 45,425 6 6372 3179 NC 45,35 5 10310D 46,219 6 3928 2134 16 - - 10310F 47,671 5 3969 2117 10 - - 103106 48,076 5 5912 3173 9 - - 10320B 51,765 4 4943 2005 6 51.80 22 - 10320B 51,765 4 4943 2005 6 51.80 22 - 10320D 52,541 5 3180 1475 12 - - 10320F 53,010 4 2933 1128 10 52,95 1 10320F 53,147 6 6370 3178 NC - - 10320H 54,546 6370 3178 NC	10300W	38.443	2	60	30	NC	-	-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10300Y	38,989	2	60	30	NC	-	ĩ
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10310A	43.342	2	60	30	NC	43.30	51
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10310B	45.425	6	5372	3179	NC	45.35	53
103100 46.219 6 3928 2134 16 - - 10310E 46.864 6 3894 2106 12 - - 10310F 47.71 5 3969 2117 10 - - 10310F 47.71 5 3969 2117 10 - - 10310F 47.751 5 5912 3173 9 - - 10310H 49.136 6 2809 1685 22 - - 10320E 51.765 4 4943 2005 6 51.80 22 10320E 52.045 6 4940 2425 11 - - - 10320E 53.010 4 2393 1128 10 52.95 1 10320F 53.349 4 1944 1011 12 53.30 - 10320G 54.035 6 6370 3178 NC - - 10320H 55.436 6 6370 3178	103100	45.993	6	4641	2650	19	45.95	32
103100 46.864 6 3728 2104 16 - 103106 46.864 6 3894 2106 12 - 103106 48.076 5 5912 3173 9 - 103104 49.136 6 2809 1685 22 - 103208 51.765 4 4943 2005 6 51.80 22 103200 52.045 6 4940 2425 11 - - 103200 52.541 5 3160 1475 12 - - 103206 53.010 4 2393 1128 10 52.95 1 103206 54.035 6 2505 1422 19 - - 103204 54.549 6 6371 3178 NC - - 103204 55.833 6 6370 3178 NC - - 103204 <td< td=""><td>107100</td><td>46.219</td><td></td><td>1011</td><td>2174</td><td>14</td><td>45175</td><td>24</td></td<>	107100	46.219		1011	2174	14	45175	24
Norve Norve <t< td=""><td>103105</td><td>40.217</td><td>6</td><td>7004</td><td>2104</td><td>10</td><td></td><td>1</td></t<>	103105	40.217	6	7004	2104	10		1
103106 48.076 5 5912 3173 9 - 103108 49.136 6 2809 1685 22 - 103208 51.765 4 4943 2005 6 51.80 22 103208 51.765 4 4943 2005 6 51.80 22 103208 51.765 4 4943 2005 6 51.80 22 103200 52.045 6 4940 2425 11 - - 103200 52.045 6 4940 2425 11 - - - 103200 52.045 6 4740 2178 10 52.95 1 103206 53.010 4 2393 1128 10 52.95 1 103204 54.035 6 2505 1422 19 - - 103204 55.433 6 6370 3178 NC - - 103204 55.833 6 6370 3178 NC -	103102	40+004	o c	70/0	2100	10		12
103100 48.076 5 5712 3173 9 - 103104 49.136 6 2809 1685 22 - 103208 51.765 4 4943 2005 6 51.80 22 103208 51.765 4 4943 2005 6 51.80 22 103200 52.045 6 4940 2425 11 - - 103201 52.541 5 3180 1475 12 - - 103206 54.035 6 2505 1422 19 - - 103206 54.035 6 2505 1422 19 - - 103204 55.437 6 6371 3178 NC - - 103204 55.438 6 6370 3178 NC - - 103204 59.576 2 60 30 NC - -	103105	47+6/1	5	3767	2117	10	-	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10310G	48.078	5	2809	1685	22	-	-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					192203051351			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10320A	49+994	6	4024	2613	ć.		-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10320B	51.765	4	4943	2005	6	51.80	225
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	103200	52.045	6	4940	2425	11	-	-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10320D	52,541	5	3180	1475	12	-	-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10320E	53.010	4	2393	1128	10	52,95	18
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10320F	53.349	4	1964	1011	12	53.30	7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	103206	54.035	6	2505	1422	19		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10320H	54.549	6	6371	3178	6	-	**
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10320J	55.147	6	6008	3178	NC	55.05	123
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10320K	55.436	6	6370	3178	NC	-	-
10320h 57.958 2 64 30 NC $-$ 10320N 59.576 2 60 30 NC $-$ 10320P 60.271 2 60 30 NC $-$ 10320R 60.622 1 35 $-$ NC $-$ 10330A 68.037 6 6368 3176 NC $-$ 10330B 68.495 6 4478 2679 20 68.45 6 10330C 68.942 6 5678 2935 14 $ -$ 10330D 70.038 5 3937 2002 11 $ -$ 10330F 71.660 6 3896 2308 23 71.65 5 10340A 72.293 6 4958 3175 6 $ -$ 10340B 73.006 5 1214 703 20 $ -$ 10340D 76.347 6 3745 2040 $ -$ 10340D	10320	55,833	6	6370	3178	NC		
10320N 59.576 2 60 30 NC $ 10320P$ 60.271 2 60 30 NC $ 10320R$ 60.622 1 35 $ NC$ $ 10330A$ 68.037 6 6368 3176 NC $ 10330B$ 68.495 6 4478 2679 20 68.45 6 $10330C$ 68.942 6 5678 2935 14 $ 10330D$ 70.038 5 3937 2002 11 $ 10330E$ 70.534 6 6368 3175 11 $ 10330F$ 71.660 6 3896 2308 23 71.65 5 $10340A$ 72.293 6 4958 3175 6 $ 10340B$ 73.006 5 1214 703 20 $ 10340C$ 75.293 6 4317 2281 13 $ 10340D$ 76.347 6 3745 2040 14 $ 10340E$ 76.654 6 2992 1824 20 76.80 16 $10340F$ 77.493 6 6367 3174 10 $-$	103206	57,958	2	64	30	NC	-	-
10320P 60.271 2 60 30 NC $ 10320R$ 60.622 1 35 $ NC$ $ 10330R$ 68.037 6 6368 3176 NC $ 10330B$ 68.495 6 4478 2679 20 68.45 6 $10330C$ 68.942 6 5678 2935 14 $ 10330D$ 70.038 5 3937 2002 11 $ 10330E$ 70.534 6 6368 3175 11 $ 10330F$ 71.660 6 3896 2308 23 71.65 5 $10340A$ 72.293 6 4958 3175 6 $ 10340B$ 73.006 5 1214 703 20 $ 10340C$ 75.293 6 4317 2281 13 $ 10340D$ 76.347 6 3745 2040 14 $ 10340E$ 76.54 6 2992 1824 20 76.80 16 $10340F$ 77.493 6 6367 3174 10 $-$	10320N	59.576	2	60	30	NC	1	-
10320R 60.622 1 35 $ NC$ $ 10330A$ 68.037 6 6368 3176 NC $ 10330B$ 68.495 6 4478 2679 20 68.45 6 $10330C$ 68.942 6 5678 2935 14 $ 10330D$ 70.038 5 3937 2002 11 $ 10330E$ 70.534 6 6368 3175 11 $ 10330F$ 71.660 6 3896 2308 23 71.65 5 $10340A$ 72.293 6 4958 3175 6 $ 10340B$ 73.006 5 1214 703 20 $ 10340C$ 75.293 6 4317 2281 13 $ 10340D$ 76.347 6 3745 2040 14 $ 10340E$ 76.654 6 2992 1824 20 76.80 16	10320P	60.271	2	60	30	NC	1.000	-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10320R	60.622	1	35	-	NC	-	-
10330A 35.037 6 6368 3176 MC - 10330B 68.495 6 4478 2679 20 68.45 6 10330C 68.942 6 5678 2935 14 - - 10330D 70.038 5 3937 2002 11 - - 10330E 70.534 6 6368 3175 11 - - 10330F 71.660 6 3896 2308 23 71.65 5 10340A 72.293 6 4958 3175 6 - - 10340B 73.006 5 1214 703 20 - - 10340C 75.293 6 4317 2281 13 - - 10340D 76.347 6 3745 2040 14 - - 10340D 76.454 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 -	107704	10.077	,	17/0	717/			
103300 68.942 6 5678 2935 14 - 103300 70.038 5 3937 2002 11 - 10330E 70.534 6 6368 3175 11 - 10330F 71.660 6 3896 2308 23 71.65 5 10340A 72.293 6 4958 3175 6 - - 10340B 73.006 5 1214 703 20 - - 10340C 75.293 6 4317 2281 13 - - 10340D 76.347 6 3745 2040 14 - - 10340D 76.347 6 3745 2040 14 - - 10340D 76.347 6 3745 2040 14 - - - 10340E 76.654 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 - - <td>103308</td> <td>40 405</td> <td>2</td> <td>4470</td> <td>2470</td> <td>20</td> <td>49.45</td> <td>40</td>	103308	40 405	2	4470	2470	20	49.45	40
103300 70.038 5 3937 2002 11 - 103301 70.038 5 3937 2002 11 - 103302 70.534 6 6368 3175 11 - 103305 71.660 6 3896 2308 23 71.65 5 10340A 72.293 6 4958 3175 6 - - 10340B 73.006 5 1214 703 20 - - 10340C 75.293 6 4317 2281 13 - - 10340D 76.347 6 3745 2040 14 - - 10340D 76.454 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 - -	103306	00+473	0	5(70	2077	1.4	00+40	00
103300 70.038 5 3737 2002 11 - 10330E 70.534 6 6368 3175 11 - 10330F 71.660 6 3896 2308 23 71.65 5 10340A 72.293 6 4958 3175 6 - - 10340B 73.006 5 1214 703 20 - - 10340C 75.293 6 4317 2281 13 - - 10340D 76.347 6 3745 2040 14 - - 10340E 76.654 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 - -	103300	00:742	0	30/8	2733	1.4	1272	-
10330E 70,334 6 6368 5175 11 - 10330F 71,660 6 3896 2308 23 71,65 5 10340A 72,293 6 4958 3175 6 - - 10340B 73,006 5 1214 703 20 - - 10340C 75,293 6 4317 2281 13 - - 10340D 76,347 6 3745 2040 14 - - 10340E 76,654 6 2992 1824 20 76,80 16 10340F 77,493 6 6367 3174 10 -	103300	70.038	5	373/	2002	11	12	-
10330F 71,680 6 3898 2308 23 71,65 5 10340A 72.293 6 4958 3175 6 - - 10340B 73.006 5 1214 703 20 - - 10340C 75.293 6 4317 2281 13 - - 10340D 76.347 6 3745 2040 14 - - 10340E 76.654 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 -	10330E	70+004	0	0368	0700	11		
10340A 72.293 6 4958 3175 6 - 10340B 73.006 5 1214 703 20 - 10340C 75.293 6 4317 2281 13 - 10340D 76.347 6 3745 2040 14 - 10340E 76.654 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 -	103301	/1.650	6	3848	2308	23	/1,65	5/
10340B 73,006 5 1214 703 20 - 10340C 75,293 6 4317 2281 13 - 10340D 76,347 6 3745 2040 14 - 10340E 76,654 6 2992 1824 20 76,80 16 10340F 77,493 6 6367 3174 10 -	10340A	72.293	6	4958	3175	6	-	-
10340C 75.293 6 4317 2281 13 - 10340D 76.347 6 3745 2040 14 - 10340E 76.654 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 -	10340B	73.006	5	1214	703	20	-	-
10340D 76.347 6 3745 2040 14 - 10340E 76.654 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 -	10340C	75.293	6	4317	2281	13	-	-
10340E 76.654 6 2992 1824 20 76.80 16 10340F 77.493 6 6367 3174 10 -	103400	76.347	6	3745	2040	14	-	-
10340F 77.493 6 6367 3174 10 -	10340E	16.654	6	2992	1824	20	76.80	161
AAMINI LILIN M MAME MALL AV	10340F	77.493	6	6367	3174	10		
103406 77.935 & 5695 3174 MC 79.00 7	103400	77.975	4	5495	3174	MC	79.00	25
10740H 79,000 4 4407 0747 00	107400	70.330	4	4627	0747	10	70100	CI.
10340J 78.639 6 3795 2400 22 78.65 8	10340J	78.639	6	3795	2400	22	78.65	84

FINAL		ANDHALY FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	MAGNETIC FIDUCIAL	VALUE	ALT
	10340K	79.088	6	6367	3174	9	2	-	382
	10340L	79.287	6	6366	3174	NC	-		394
	10340M	80.068	6	5223	2481	11	-	-	342
	10340N	81.060	2	194	75	NC	#5	-	437
	10340P	82.583	1	44	-	NC	-	3 - 27	411
	10340R	83.513	1	35	-	NC	-	-	419
	10340S	84.027	1	41		NC	-	-	420
	10340T	84.780	3	75	30	8	-	-	491
	10350A	86.277	1	30	-	NC	2	(<u>a</u>)	400
	10350B	86.787	1	30	-	NC	-	-	466
	10350C	89.867	1	49	-	NC	-	-	392
	10350B	91.437	2	161	67	NC	-	-	488
	10350E	92.041	4	414	171	11	-	-	355
	10350F	92.249	4	452	184	10	-		354
	103514	93,592	6	589	251	15	-	**	363
	103518	94.747	6	6364	3171	8	-	-	412
	103510	94.945	6	6364	3171	NC	-	-	446
	103510	95.388	6	2904	1786	22	**	-	472
	10351E	95.681	6	2873	1750	23	-		428
	10351F	95.988	6	4939	3158	6	1000	-	484
	103516	97.588	6	5448	2261	7	97.55	224	416
	10360A	98.793	5	485	211	14	2	-	419
	10360B	99.073	3	369	158	10		-	442
	103600	99.694	4	541	248	14	-	140	396
	103500	100.019	4	619	334	14	-	-	387
	10360E	100.456	5	2032	857	9	-	-	339
	10350F	100.939	5	2972	1204	9	-	-	371
	10360G	101,408	6	4150	2171	12	-	-	358
	10360H	101.841	4	3747	1399	9	101.85	32	344
	10360J	102.653	6	4010	2273	16	-	-	427
	10360K	103.432	6	6363	3169	7	-		356
	10360L	103.631	6	6362	3169	NC	-		390
	10360M	104.037	6	6362	3169	NC	-	-	326
	10360N	104.240	6	6362	3169	NC	104.15	247	342
	10360P	104.474	6	6256	3169	NC	-	-	374
	10360R	105.011	5	3219	1663	12	-	-	412
	103605	105.345	6	2284	1377	24	-		498
	10360T	105.742	6	6362	3169	6	105.70	107	410
	10360W	106.999	4	1468	553	6	-	-	364
	10360Y	107.333	4	653	237	7	-	-	410
	10360Z	108.154	2	60	30	NC	-	-	418
	10360AA	108.858	2	60	30	NC	-	-	383
	10360BB	109.758	2	60	30	NC	100	-	400
		and the second							
	10370A	112.656	2	60	30	NC	-	-	446
	10370B	113.057	2	60	30	NC	-		418
	103700	113.412	2	60	30	NC	-	-	408
	103700	114.653	2	60	30	NC	-	-	402

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FINAL	ANDMALY					MAGNETIC		1.000	
ANOMALY	FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	FIDUCIAL	VALUE	ALT	
103705	116.374		60	30	NC			YAF.	
103705	114.025	5	40	30	NC	-	-	155	
103700	117 444	2	177	45	ALC:	1.12	195	770	
107700	119 125	Ā	4094	1523	5	1	3	370	
103701	110,120	1	1024	1004	17			502	
103703	110.770	4	1020	2101	20		2	452	
103706	119.779	4	3247	2745	27		_	462	
107708	110 041	4	2202	2345	20			407	
103700	127.741	4	3/02	2070	17	-		44.0	
103708	120.270	7	2714	1080	10			374	
103700	101.514	4	2010	2039	24			370	
107700	171 705	2	1710	7144	22	1.000		115	
103705	122.044	4	4750	3166	44	-	-	302	
103704	100 475	4	1750	3100	75			700	
103700	122.033	0	4012	3100	33		5	427	
103707	120+340	0	4012	1700	17	-		927	
103702	123,892	0	2475	1300	1.5	-	-	407	
103800	124.871	4	284	139	20	-	-	440	
103808	125.625	5	806	423	15	~	-	403	
103800	126.094	6	2703	1283	10	-	-	368	
103800	126.674	6	2706	1517	15		-	408	
10380E	127.355	6	4102	2281	17	-		360	
10380F	127.784	6	6359	3165	34	-	-	392	
10380G	128.619	6	6327	3165	33	128.60	28	340	
10380H	128,989	6	5074	3165	20		-	399	
10380J	129.794	6	4558	2496	17	-	-	452	
10380K	130.440	4	2021	1012	12	-	-	504	
10380L	130.670	6	1874	1118	23		-	514	
10380M	130.945	4	1921	1094	15	-	-	507	
10380N	131.198	6	1986	1130	19	131.15	55	440	
10380P	132.046	6	1777	888	11	-	-	513	
10380R	133.167	1	108	-	NC	-	-	408	
103805	135.134	4	95	30	54	-	-	360	
103801	135.617	2	79	.30	NC	-		392	
		-	6.6	1022.					
10390A	138.020	2	60	30	NC	-	-	323	
10390B	138.471	2	60	30	NC	-	-	322	
		2						144	
10391A	141.487	6	2038	994	10	-	10	483	
103918	142.644	0	2040	11//	20	-	5	490	
103910	143.091	0	2872	1687	18	-	-	490	
103910	144,363	6	2025	11/3	25	-		392	
103924	145,420	6	1846	1048	22	1	-	451	
10392B	145,862	6	5709	3160	14	-	-	438	
103920	146,947	4	6355	3147	28	-		PAT	
103920	147.543	6	2868	1519	15	147.45	173	417	
10392E	148.044	6	2696	1469	15			402	
10392F	148,391	6	2352	1165	11	-	-	418	
103926	148, 694	5	889	446	14	-	-	402	
100710	TIMUTA	0	007	110				101	

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	FINAL	ANOMALY FIDUCIAL	CHS	CH1.AMP	CH2.AMP	SIEMENS	MAGNETIC	VALUE	ALT	
-	10400A	150.619	5	705	358	14	-	-	430	
1	10400B	151.242	6	2239	1072	10	151.00	155	415	
1	10400C	151.648	6	2361	1230	14	-	-	441	
1	0400D	152.139	6	1642	966	20	-	-	513	
1	10400E	152.843	6	3611	1962	14	-	-	513	
1	10400F	153.333	6	2339	1297	15	-	-	507	
1	10400G	153.721	4	1739	917	13	-	-	465	
1	L0400H	154.272	6	1535	809	17	-	12	498	
1	10400J	154.732	6	2501	1390	20	-	-	512	
1	10400K	155.395	6	6354	3160	39	-	-	366	
1	10400L	155.923	6	6354	3160	14	-	-	396	
	10400AX	149.200	6	2649	1514	11			440	
1	19010A	11.493	6	3813	2202	17	-	-	472	
1	19010B	11.890	6	4163	2470	23	-		490	
1	19010C	12.283	6	4547	2933	24	-	-	500	
1	19010D	12.946	5	2219	1252	15	-	-	512	
1	19010E	13.591	2	1085	602	NC	13.55	8	530	
1	19010F	15.868	4	335	143	9	-	-	486	
	00110	17 /75		100	17					
1	19011H	17:030	2	129	4/	NC	10 10	-	510	
	190110	10.33/		388	125	8	18.60	21	4/2	
1	00110	20,110	-	142	-	NC	-	-	419	
	90115	22./81	ĉ	4/9	200	26		-	450	
1	00115	23.430	0	03/7	3187	24	-	-	440	
	190116	24.217	3	1998	1057	13	-		499	
	190116	24.012	5	4//6	2469	11	24.45	13	4/0	
	170114	20.200	2	03/7	3187	39	-	-	428	
	190115	25.495	0	63/9	318/	35	-		449	
	190116	26,312	0	3286	2180	3/	26.20	11	504	
	19011L	20./93	0	2030	1//1	40	-		512	
	190118	27.952	0	4998	28/0	19	-	-	444	
	19011N	28.313	6	4098	2/91	6	-	-	452	
1	19020A	29.997	6	5384	3187	36	-	-	515	
-	19020B	30.841	6	6380	3187	62	-	12	452	
ŝ	190200	31.574	~	5394	3187	43	-	-	400	
	190200	33.040	1	177	-	NC	141		522	
1	19020F	33.418	1	108	-	NC	-	-	472	
	19020F	45.282	Å	1740	917	15	120	124	520	
	190206	44. 257	4	1154	600	20			507	
1	190208	46.920	7	704	323	11	-	-	103	
		101720	5	100	525	11	-53		474	

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