83-#759 - 11789

Report on

GEOCHEMICAL SURVEY AND RECONNAISSANCE MAPPING MONASHEE WEST GROUP NTS 82L/1W and L2E Lat. 50°6'N; Long. 118°30'W Vernon Mining Division

GEOLOGICAL BRANCH ASSESSMENT REPORT

11,789

NAKUSP RESOURCES LTD. (owner & operator)

by

U. SCHMIDT, B.Sc. I.M. WATSON, P.Eng. I.M. WATSON & ASSOCIATES LTD.

December 20, 1983

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83MW1B	Claim Map	1:50,000	Following P. 1
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8 3MW4	Reconnaissance Geochemistry As	1:5000	In Pocket
8 3MW 5	Reconnaissance Geochemistry Cu	1:5000	In Pocket
83MW6	Reconnaissance Geochemistry Pb	1:5000	In Pocket
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Fig. 83MW1 MONASHEE WEST GROUP Index Map

INTRODUCTION

The Monashee West Group of Nakusp Resources Ltd. is situated at Monashee Pass in the Monashee Mountain area of the Vernon Mining District, south-central B.C.

Reconnaissance geochemical sampling and geological mapping surveys were carried out by I.M. Watson & Associates Ltd. during the period August 28 to September 18, 1983. This work was part of a preliminary survey of the precious metal potential of an area which also includes the adjoining 'DAVID ONE' claim, immediately south and west of the Monashee West Group. (Schmidt & Watson, November 1983)

Interest in the area derives mainly from several gold-silver veins on the Withrow Crown Grant, which is centrally located within the Monashee West Group.

PROPERTY, LOCATION AND ACCESS

The Monashee West Group of Nakusp Resources Ltd. comprises twenty-six 2-post claims, four Crown grants and one fractional claim. All but the MW1 Fractional claim are held under option from J. Graves of Vernon, B.C. The MW1 claim was staked on 5th September 1983 by U. Schmidt on behalf of Nakusp Resources Limited. Details of the claims are listed below:

Claim Name	Record Number	Expiry Date
Phy1 1-2	1134-1135	October 5, 1983
Bud 1-2	1136-1137	October 5, 1983
Mort 1-2	1138-1139	October 5, 1983
John 1-4	1166-1169	November 3, 1983
Rob 1-4	1181-1184	December 4, 1983
Moonbeam 1-12	1314-1325	November 15, 1983
MW1 Fraction	1607	September 14, 1983
McIntyre Crown Grant	D.L. 194	July 2*
Riske Old Ledge		
Crown Grant	D.L. 192	July 2*
Vernon Crown Grant	D.L. 193	July 2*
Withrow Crown Grant	D.L. 306	July 2*

* Tax due date





The claims are situated just north of McIntyre Lake at Monashee Pass, approximately 20km. south of Cherryville, and 60 kms. east-southeast of Vernon. Highway 6 crosses the group near its western boundary; an older gravel surfaced section of the highway provides access to the south end of the property. Additional access is provided by a powerline road which cuts across the property and by a four-wheel drive road near the eastern claim boundary which connects to the St. Paul Mine on Monashee Mountain, 2km. to the northeast.

The claims straddle a south-westerly trending spur of Monashee Mountain which presents steep bluff topped slopes to the west and falls more gently to the east. The area is covered by thick evergreen forest of balsam and pine. A small tributary of the Kettle River drains the eastern area of the claim.

Elevations range from 1200m. along the highway on the west side to over 1550m. along the northern boundary of the claims.

HISTORY

Activity in the area dates back to 1886 when the Crown grants were staked. Periodic work on those claims included underground development and the operation of a mill on the Withrow Crown grant. The mill was dismantled in the 1940's and only the foundation remains. The underground workings are described in several of the Minister of Mines Annual Reports (1902; 1922; 1933 and 1934).

The most recent account of the underground workings (B.C. MMAR, 1934) describes four 'adit levels' between elevations 3900' and 4150'. Each level is reported to have been developed for several hundreds of feet, but description of the mineralised zone is limited to mention of 'lengths of quite high-grade ore'.

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The 1933 Annual Report refers to mineralised quartz veins in the #2 (middle) tunnel, containing minor pyrite, chalcopyrite and galena over a length of 185'. Average assays (calculated at the then gold price of \$20.00/oz) were reported to be the equivalent of \$7-\$8 per ton. Unfortunately, no elevations are recorded and discrepancies between descriptions of the adits, now caved and inaccessible, make identification on the ground difficult.

Two short north-westerly directed adits were found on the Moonbeam 5 and 6 claims, but there is no published record of these workings or of activity after 1940.

The claims were acquired by J.E. Graves of Vernon during 1981 and 1982, and were optioned to Nakusp Resources Limited in January 1983.

GEOLOGY

Mapping by the GSC (Jones, 1959; Okulitch and Campbell, 1979) shows the Monashee West Group to be underlain by Carboniferous and Permian Age metavolcanics and metasediments of the Thompson Assemblage, intruded on the south by a batholith of Late Jurassic granite-granodiorite.

The regional trend in the Monashee area is northwesterly with variable dips to the north-east and south-west. (Okulitch and Campbell, 1979)

U. Schmidt of I.M. Watson & Associates Ltd. spent five and a half days mapping the claim group on a reconnaissance basis, during the period 28th August to 18th September 1983. The work was done in conjunction with the reconnaissance soil sampling programme, using 1:5000 enlargements of the 1:50,000 topographic maps, air photos, chain, altimeter, and soil sample grid lines for control.

Outcrop is not abundant and most information has been obtained from roadcut and power line access road exposures in the eastern and central parts of the claim group. The greater part of the Monashee West Group is underlain by interdigitating lenses of fine grained altered volcanics (meta-andesites?) and metasediments (argillites and marbles). Attitudes in the sediments indicate west to north-westerly strikes and moderate to steep northerly dips. Sediments predominate in the northern part of the claim group, where grey to white, massive marble forms 50-metre cliffs along the crest of the ridge overlooking Highway 6.

The contact with the granitic rocks is poorly exposed except in road cuts on the DAVID ONE claim immediately west of the Moonbeam 7 and 9 claims. The intrusion is a leucocratic, medium to coarse grained, hornblende biotite granodiorite. The granitic rocks are generally fractured and locally heavily sheared and altered. Alteration (kaolinisation, chloritisation) is relative to the degree of deformation. Where the north-westerly trending contact is exposed, the granodiorite intrudes sheared, rusty, altered fine grained volcanics containing narrow sedimentary bands and lenses.

MINERALISATION

Pyrite is common as fine disseminations associated with fracturing in silicified and rusty metavolcanics and sediments, particularly along or near the contact with the granites. Finely pyritised rusty skarn at volcanic/marble contacts is exposed in roadside cuts on the Moonbeam 3 claim and on the Vernon Crown Grant (L193). The zones appear to be lensoid and limited to a few tens of feet in extent. Pyritic, rusty andesite sills were also noted in marble on the Vernon Crown Grant. Grab samples from both occurrences assayed less than a third of an ounce of silver/ton and 0.001 - 0.002 Au ozs/ton.

The adits on the Moonbeam 5 and 6 claims were driven on a strong northwesterly trending shear cutting highly silicified and carbonatised volcanics. Irregular quartz veins and pods within the shear are weakly to moderately pyritised, and contain rare chalcopyrite and galena. Chip and grab samples (Plan 82MW1) revealed low silver (0.67 - 3.85 ozs Ag/ton) and insignificant gold content (0.001 - 0.008 ozs Au/ton). Highest assays obtained from sampling of the dumps on the Withrow Crown Grant (L306) came from the workings at 1265 metres (4150') elevation. (Plan 83 MW1) A selected grab sample of quartz vein material containing disseminated pyrite, galena and chalcopyrite assayed as follows:

0.315% Cu; 0.71% Pb; 4.72 ozs/ton Ag; 0.726 ozs/ton Au

Samples of dump material from other adits above and below this elevation failed to produce assays of economic significance.

GEOCHEMISTRY

1. Sample Coverage

The reconnaissance soil sampling of the Monashee West Group was completed during the period September 3rd to September 18th, 1983 and involved a total of 23 man days work. The survey, in conjunction with the mapping and prospecting programme, was designed to provide a rapid preliminary evaluation of the Monashee West claims. The steep western half of the property was contour sampled at 100-metre intervals along lines spaced at 60-metre (200 foot) elevations. The same sampling density could not be maintained by contour sampling over the more gently sloping eastern half of the property, so a 100m. X 100m. sampling grid was established using the Moonbeam 1-12 claim line as a north-south base line. Flagged sample lines were controlled by hip-chain and compass.

Three small detail sampling grids (A-C) were established over specific areas of interest, using the Moonbeam grid as reference. <u>Grid 'A'</u> is situated in the north-east corner of the Moonbeam #1 claim, measures 250m. X 125m., and covers zones of pyritic skarn. The sample spacing is 25m. X 25m.

<u>Grid 'B'</u> covers the old workings on the Withrow Crown Grant (L306), and measures approximately 200m. X 250m. Samples were taken at 25-metre intervals along north-south lines 50 metres apart.

<u>Grid 'C'</u>, on claims Moonbeam 5 and 6, provides 25m. X 25m. sampling coverage of the shear zone and covers an area 200m. X 150m.

2. Methods and Analysis

Approximately .5 kg of 'B' horizon soil was placed in a standard gusseted soil sample bag at each site. An unique sample number was assigned to each sample and recorded on flagging tape at the site. In total, 459 soil and 3 rock samples were taken.

Analyses were done at Acme Analytical Laboratories Ltd. in Vancouver. A -80 mesh fraction of soil was analysed by the inductively coupled argon plasma method (ICP) and a separate analysis for gold was carried out by atomic absorption (A.A.).

The 30 elements reported by the ICP analysis method are as follows: Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K, W.

The sample is prepared by dissolving a .5 gram sample in hot aqua-regia (3:1:3 nitric acid to hydrochloric acid to water) at 90°C for 1 hour. This sample is diluted to 10 ml with water and converted to an aerosol.

A brief description of the ICP analysis is as follows: high frequency currents in a few turns of induction coil (powered by a high frequency generator) surround a plasma cell and generate a magnetic field. The cell consists of argon plasma enclosed between two concentric quartz tubes surrounding a glass sample injector. The plasma gas is seeded with electrons - resulting temperatures range from 7000 to 10,000°K. The sample, in the form of an aerosol, is injected into the centre of the cell and rises above into the doughnut-shaped plasma ring. The high temperatures vaporize the sample and dissociate molecular species. Spectral intensities of the excited sampled are then recorded and compared with standards by a direct-reading emission spectrometer in conjunction with a computer.

3. Discussion of Results

For the purposes of this reconnaissance survey, the anomalous level for each element was statistically established from the ICP analytical data as the mean plus two standard deviaitions. Five elements (Ag, As, Cu, Pb and Zn) were determined to be of geological significance. Results for these elements, as well as gold (A.A. analysis), are plotted on the accompanying plans. The format used is a series of six size-graded solid circles, each representing a different and equal range of values, the largest being anomalous. The readily visible density contrast patterns reveal not only statistically derived anomalies, but any significant trends of the individual elements. Analytical results for Mo, Ni, Co, Mn, Fe, U, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K and W are also appended to this report. These may be keyed to sample number locations provided on drawing no. 83MW8.

Plan 83MW3 shows the distributions of <u>gold</u> in soils. The most significant anomaly is on the Withrow Crown Grant (L306). Here the detailed grid sampling indicates a 150m.X 75m. anomalous area which includes the old adits and dumps. Analyses range from 25 to 985 ppb Au. Cu, Pb, Zn and Ag show a weak correlation with gold. It is not certain how much of the anomaly is caused by contamination from dump material; follow-up work will be needed to further evaluate the area, and to close off the anomaly, which is open to the east.

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Elsewhere, there is a cluster of weak (20 ppb - 60 ppb Au) anomalies on the Moonbeam 2 claim; an isolated high (370 ppb Au) on the southern boundary of the Moonbeam 1 claim; and a small cluster of anomalous samples around the workings on the Moonbeam 5 and 6 'C' grid, with correlating silver, arsenic and zinc anomalies.

<u>Silver</u> (Plan 83MW2) has an erratic trendless distribution over most of the property with the exception of the weak correlation with gold on the Withrow Crown Grant, mentioned above, and a stronger anomaly (1.0 - 2.5 ppm Ag) around the workings on Moonbeam 5 and 6 claims. There is an apparent slight enrichment of silver in the north eastern corner of grid 'A' on the Moonbeam 1 claims.

<u>Arsenic</u> in soils (Plan 83MW4) is most abundant in the area of the workings on the Moonbeam 5 and 6 claims (grid 'C'). Analyses range up to 115 ppm As. The soils in the north-western corner of grid 'A', on the Moonbeam 1 claim, show a weak but definite concentration of arsenic.

Soils over the workings in the grid 'B' and 'C' areas are also weakly anomalous in <u>lead</u>, <u>zinc</u>, and <u>copper</u> (Plans 83MW6; 83MW7; and 83MW5). Copper also shows an erratic distribution of 'one-spot' anomalies throughout the claim group.

SUMMARY

The purpose of the 1983 geochemical and geological reconnaissance of the Monashee West Group was to make a preliminary evaluation of the precious metal potential of the area.

The area of greatest geochemical interest includes the old adits on the Withrow Crown Grant (L306). Undoubtedly, some of this geochemical response is the result of contamination from the dumps, but follow-up prospecting, mapping, additional sampling and hand trenching will be required to fully evaluate the area. Old reports indicate that the adits were driven on an east-north-easterly striking vein or vein system of gold bearing quartz, but the extent and tenor of the mineralisation is not clear, and there is no surface exposure of the mineralised zones. Verification will require that the old adits be re-opened for mapping and sampling, if this is physically and economically feasible.

Sampling of the mineralised shear zone exposed in the old adits on the Moonbeam 5 and 6 claims failed to yield significant assays, but the correlating precious and base metal soil anomalies, although weak, merit a limited programme of follow-up prospecting, hand trenching and rock sampling.

CERTIFICATE OF QUALIFICATIONS

I, Ivor Moir Watson, of 584 East Braemar Road, North Vancouver, hereby certify that:

- I am a consulting geologist with offices at 410 675 West Hastings Street, Vancouver, B.C.
- I am a graduate of the University of St. Andrews, Scotland (B.Sc., Geology, 1955).
- 3. I have practiced my profession continuously since graduation.
- I am a member in good standing of the Association of the Professional Engineers of B.C., and a Fellow of the Geological Association of Canada.
- 5. Work on the Monashee West Group was carried out by the following people working under my supervision:
 - U. Schmidt, project geologist
 - L. Westervelt, geological assistant
 - R. Krawinkel, sampler
 - B. Dent, sampler
 - B. McDonald, sampler
 - D. Seaton, sampler

WATSON I. M. Natson, B.Sc.,

December 20, 1983 Vancouver

STATEMENT OF QUALIFICATIONS

I, Uwe Schmidt, with residential address in Port Moody, B.C. do hereby declare:

I am a 1971 graduate of the University of British Columbia with a B.Sc. degree in Geology.

Since graduation, I have been engaged in mineral exploration in Yukon Territory and British Columbia.

U. Schmidt, B.Sc.

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COST STATEMENT - MONASHEE WEST GROUP

Geological and geochemical surveys - 28th August - 18th September, 1983.

Salaries and Fees

a)	Field Work		
	U. Schmidt - project geologist 6 days @ \$200.00/day \$ 1 (28th August: 5-7, 12 & 18 September)	,200.00	
	L. Westervelt - geological asst. 1 day @ \$90.00/day (28 August)	90.00	
	R. Krawinkel - prospector 8 days @ \$100.00/day (31 August: 3, 5-9, 18 September)	800.00	
	B. Dent - prospector 8 days @ \$100.00/day	800.00	
	(31 August; 3, 5-9, 18 September)		
	D. McDonald - prospector 8 days @ \$100.00/day	800.00	
	(31 August; 3, 5-9, 18 September)		
	D. Seaton - prospector 1 day @ \$100.00/day (18 September)	100.00	4.1
	I. Watson - project manager 1 day @ \$400.00/day (12 September)	400.00	
b)	Report Preparation	1000	
	U. Schmidt 4 days @ \$200.00/day	800.00	1
	I. Watson 1 day @ \$400.00/day _	400.00 \$	5,390.00
Room	and Board *33 man days @ \$28.50/man/day		940.50
Tele	phone		45.00
Tran	sportation and Fuel		
1	*Two 4X4 trucks - 14 days @ \$35.00/day	490.00	
	Fuel - 765.7 1 @ 50.8¢/litre	388.98	878.98
Geoc	nemical Analyses		WAREAS I SHO
	30 element ICP + Au (A.A.) - 462 samples @ \$9.90/sample		4,573.80
Assa	ring		222.00
Equi	pment Purchase		
	12 rolls topo fil @ \$3.50 each	42.00	
	462 sample bags @ \$13.75/100	63.53	
	72 rolls flagging @ \$1.10	79.20	184.73
Equi	pment Rental		
	*5 hand held radios - 8 days @ \$2.50/day/unit	100.00	
	*2 mobile radios - 7½ days @ \$2.50/day/unit	37.50	137.50
Repr	oduction		342.67
Draf	ting		
	D. Phillips - 40 hours @ \$17.00/hr.	dellar	680.00
		10	13,395.18

* Pro rated costs

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Jones, A.G., Vernon Map Area, B.C. G.S.C. Memoir 296, 1959.

Okulitch, A.V. and Campbell, R.B. G.S.C. Open File 637, 1979.

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	1891
	1897
	1900
	1901
	1902
	1922
	1933
	1934
	1935
	1940

B.C. Dept. of Mines Bulletin 20, Part 3.



MIN-EN LABORATORIES LTD.

705 WEST 15TH STREET, NORTH VANCOUVER, B.C. V7M 1T2 PHONE: (604) 980-5814 OR (604) 988-4524

Certificate of Assay

	TM	TT - th	•	
TO:	L.M.	warson	¢.	ASSOC.

PROJECT No. Nakusp

P.O. Box 112,

Burton, B.C. VOG 1EO.

DATE: Aug. 12/83.

File No. 3-700

	Au	Ag	Zn %	РЬ %	Cu %	SAMPLE No.
	oz/ton	oz/t on				
				ple	no sam	19251
				ple	no san	52
· · ·	.726	4.72		.71	.315	55
	.070	.33				56
	.001	.01		**		57
	.001	.01	1	/ .	· · · · · · · · · · · · · · · · · · ·	58
	.001	.01				62
	.023	.42				63
	.138	.30				64
	.020	.01				65
	.412	1.70				66
	.160	.01				67
	.024	.08				68
	.032	.19				69
	.298	2.71				70
	.023	.01				71
	.260	.01				72
	.036	1.29	5.26	1.80		73
	.001	.38	.85	.48		74
	.010	.01				75
	2.525	12.05	10.25	15.10		76
	.706	1.80				77
	.011	.01				78
	.172	. 82				19279
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705 WEST 15TH STREET, NORTH VANCOUVER, B.C. V7M 1T2

PHONE: (604) 980-5814 OR (604) 988-4524

Certificate of Assay

i	TO:	I.M.	Watson	&	Assoc.,	
						_

Vancouver, B.C.

Nakusp PROJECT No. Monashee West DATE: Sept.21/83.

410-675 W. Hastings St.,

File No. 3-1024

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	.027	.027 .49	.027 .49 .03		

MIN-EN LABORATORIES LTD.

705 WEST 15TH STREET, NORTH VANCOUVER, B.C. V7M 1T2

PHONE: (604) 980-5814 OR (604) 988-4524

Certificate of Assay

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PROJECT No.

410-675 W. Hastings St.,

DATE: Sept. 20/83

Vancouver, B.C.

TO:

File No. 3-1030

SAMPLE No	PD	Zn	Ag	Au	
SAMPLE NO.	%	%	oz/ton	oz/ton	
0872			1.14	002	
9872			1.14	.002	
9873			.88	.002	
9874			.67	.001	
9875	-		.29	.001	
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I.M. WATSONS & ASSOCIATES PROJECT # NAKUSP FILE # 83-2468

1

SAMPLE #	Ho ppa	Cu ppe	Pb ppe	Zn ppe	Ag	Ni pps	Co pps	Mn ppa	fe	As ppa	U ppm	Au pps	Th ppa	Sr ppa	Cd pp=	Sb pp=	Bi pp=	V pp=	Ca Z	P Z	La ppa	Cr ppe	Mg	Ba ppe	Ti Z	B ppe	Al Z	Na Z	ĸ	H ppe	Aut ppb
USS-33119	1	40	8	100	.1	16	15 .	771	5.34	6	2	ND	2	31	1	2	2	110	.66	.06	4	17	1.57	206	.14	7	2.B4	.04	.41	2	10

I.M. WATSON & ASSOCIATES PROJECT # NAKUSP FILE # 83-2358

SAMPLE I	No	Cu	Pb	Zn pp=	Ag ppe	Ki PP#	Co	Mn pps	Fe	As	U	Au	Th	Sr	Cd ppe	Sb pp .	Bi pp=	V pps	Ca	PI	La ppe	Cr	Mg	Ba	Ti Z	8 ppa	A1 Z	Na Z	ĸ	N pps	Aut
BDB-38390	1	20	29	65	.1	8	7	975	2.51	3	2	ND	5	23	1	2	2	55	. 38	.08	6	15	π.	90	.12	3	1.24	.02	.09	2	5
000-70701		127	,	74		154	74	800	1.17	15	7	ND	2	102		2	2	117	74	17	7	140	1 94	105	15		2 71	70	70	,	
DDD-30371		123		101		130	17	1123	4 50	10	2	ND		47	:	2	2	07		17		20	1 14	70	.15	-	2.07	.03		2	5
500-30312 500-70707		47	10	PO		20	1.5	377	1. 31		2	ND	7	20		2	2	72	.01	.17	1	27	1.14	01	.00		1.0/	.07		2	75
000-30313	:	24	10	110		40	10	950	TTD	2	î	M		TO	:	-	2	75		10	5	17	.00	114	. 12		TAT	07	10	-	5
B0B-38395	1	30	8	102	.1	116	10	329	2.58	25	2	ND	2	18	i	ź	2	47	.25	.28	3	72	.79	196	.11	3	3.44	.02	.06	2	5
BDB-38396	1	59	11	100	.2	19	14	596	3.67	10	5	ND	2	34	1	2	2	93	.34	.10	4	22	1.05	212	.16	4	3.27	.03	.23	2	5
808-38397	1	70	12	85	.2	13	13	782	3.51	13	2	ND	2	24	1	2	2	102	.38	.10	4	13	. 91	162	.17	4	2.89	.02	.23	2	5
808-38398	1	75	11	95	.7	16	13	613	4.21	14	2	ND	2	25	1	2	2	172	.24	.08	4	17	.95	204	.17	5	3.06	.02	.26	2	5
808-38399	1	82	9	115	.2	14	20	747	5.09	4	5	ND	2	65	1	2	2	163	.34	.05	2	18	1.78	165	.19	4	3.66	.03	.79	2	5
BDB-38400	13	73	37	119	.2	15	29	2009	6.49	18	2	ND	2	35	2	2	2	120	.78	.11	7	19	1.33	195	.10	7	2.43	.02	.40	2	15
BDB-38401	1	19	11	81	.1	18	8	414	2.33	10	2	ND	2	23	1	2	2	45	.47	. 08	4	20	.52	180	.10	4	3.42	.03	.16	2	5
BDB-38402	1	19	10	85	.2	15	9	693	2.78	12	2	ND	2	17	1	2	2	51	.25	.14	4	16	.53	217	.09	4	3.44	.02	.11	2	5
BDB-38403	2	25	11	96	.1	16	11	1454	2.98	10	2	ND	2	43	1	2	2	45	. 86	. 06	2	10	.47	137	.04	3	2.43	.02	.23	2	5
BDB-38404	1	29	12	71	.1	13	10	799	2.97	7	4	ND	2	24	1	2	2	57	.37	.04	4	16	. 66	148	.10	4	3.34	.03	.14	2	5
BDB-38405	1	50	15	102	.1	14	13	1425	3.29	B	2	ND	2	43	1	2	2	68	.74	. 06	4	14	.73	231	.05	4	2.71	.02	.16	2	15
BDB-38406	2	42	9	89	.1	18	14	968	4.35	13	2	ND	2	82	1	2	2	75	.40	.04	4	13	.81	226	.07	4	3.63	.02	.39	2	5
BDB-38407	1	46	8	85	.1	14	12	591	3.31	7	2	ND	2	42	1	2	2	72	.35	.09	6	15	.74	227	.11	4	3.69	.03	.25	2	5
STD A-1/AU 0.5	1	30	39	178	.3	36	12	1006	2.83	11	2	ND	2	35	1	2	2	60	.62	.10	8	73	.72	279	.08	7	2.07	.02	.21	2	510
BDB-38408	1	58	. 2	93	.4	19	14	819	4.77	9	4	ND	2	94	1	2	2	79	1.05	.06	6	25	1.35	161	.05	6	3.88	.06	.43	2	5
BDB-38409	1	25	2	125	.1	15	15	971	3.57	2	2	ND	2	39	1	2	2	65	.24	. 14	2	17	.80	226	.07	5	3.30	.01	.12	2	5
BDB-38410	1	29	7	95	.2	11	11	504	3.81	2	6	ND	2	24	1	2	2	101	. 38	.04	2	17	1.49	177	.05	4	3.92	.01	.29	2	5
BOB-38411	1	107	1	68	.2	21	22	351	5.61	2	10	ND	2	29	1	2	2	197	.40	.04	2	22	2.58	289	.11	7	4.31	.02	.17	2	5
9D D -38412	1	74	11	108	.1	14	17	1201	4.52	2	2	ND	2	22	1	2	2	123	.40	.08	3	16	1.35	235	.09	6	3.51	.02	.15	2	5
BDB-38413	1	66	23	112	.2	13	17	1293	4.27	2	4	ND	2	25	1	2	2	110	.50	.09	2	16	1.17	226	.07	7	3.21	.01	.15	2	5
BDB-38414	1	80	2	79	.4	60	21	701	4.73	8	2	ND	2	55	1	2	2	128	.64	.07	11	65	1.51	180	.14	6	2.72	.02	. 32	2	5
BDB-38415	1	73	4	81	.3	72	20	768	4.62	11	2	ND	2	65	1	2	2	111	.67	.07	12	84	1.59	170	.11	6	2.80	.02	.24	2	5
BDB-38416	1	39	5	87	.3	30	14	622	3.64	2	2	ND	2	42	1	2	2	86	.42	.04	5	36	1.12	212	.11	5	2.81	.02	.15	2	5
BDB-38417	1	34	1	93	.3	30	13	724	3.44	3	2	ND	2	44	1	2	2	78	.49	.05	4	36	.98	218	.10	6	2.72	.02	.13	2	5
BDD-38418	1	23	6	103	.3	30	13	676	3.50	6	2	ND	2	36	1	2	2	79	.34	.06	4	37	.93	211	.10	5	2.81	.02	.11	2	5
BDB-38419	1	47	1	73	.3	30	15	392	3.92	2	2	ND	2	43	1	2	2	98	.38	.03	5	39	1.37	194	.13	5	2.92	.02	.19	2	5

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I.M. WATSON & ASSOCIATES PROJECT # NAKUSP FILE # 83-2358

BBB-LSS01 1 50 8 P2 2 14 15 0.0 2.77 41 2 100 2 2 6.7 7.0 6.0 2 6.0 2 15 1.0 2 6.0 1.0 2 2.0 7.0 7.0 6.0 2 6.0 2 2 7.0 7.0 6.0 2 6.0 2 2 6.0 2 2 6.0 1.0 2 2 6.0 1.0 7.0 6.0 1.0 7.0<	SAMPLE I	No Jpm	Cu	Pb pps	Zn ppa	49 994	Ni pps	Co pp=	m pp=	Fe	As ppm	U ppe	Au ppe	Th pp=	Sr ppe	Cd ppa	Sb pps	Bi ppe	V ppe	1	PI	La pps	Cr pps	No X	8a ppa	Ti T	B pp=	Al I	Na I	E X	¥ ppm	Au1 ppb	
bss-stort 1 54 9 71 .3 64 16 47 2 10 2 2 44 1 2 2 77 .4 .06 11 5 1.44 1.4 1.5 1.44 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 <th1.7< th=""> <th1.7< th=""> <th1.7< th=""></th1.7<></th1.7<></th1.7<>	058-36501	1	30	8	82	.2	147	15	470	2.77	41	2	ND	2	156	1	4	2	62	.30	.10	2	66	1.72	229	.11	1	2.79	.02	.14	2	15	
DSB-BASS 1 41 9 H 4 24 45 3.13 9 5 9 5 9 5 9 5 9 1 1 2 2 85 .11 67 5 24 1.41 1.44 1.44 5 3.16 .02 1.03 2 9 1 2 2 44 .45 1.13 1.12 8 2 1.03 1.01 1 1.14 1.44 <th1.44< th=""> <th1.44< th=""> <th1.44< td="" th<=""><td>DSB-36507</td><td>1</td><td>54</td><td>9</td><td>71</td><td>.3</td><td>84</td><td>18</td><td>942</td><td>3.82</td><td>16</td><td>2</td><td>ND</td><td>2</td><td>64</td><td>1</td><td>2</td><td>2</td><td>97</td><td>.47</td><td>.08</td><td>•</td><td>56</td><td>1.35</td><td>144</td><td>.11</td><td>5</td><td>2.54</td><td>.02</td><td>.21</td><td>2</td><td>5</td><td></td></th1.44<></th1.44<></th1.44<>	DSB-36507	1	54	9	71	.3	84	18	942	3.82	16	2	ND	2	64	1	2	2	97	.47	.08	•	56	1.35	144	.11	5	2.54	.02	.21	2	5	
BEB-MASO 1 23 8 77 14 14 8 72 14 7 14 7	058-38503	1	41	9	84	.4	24	12	485	3.35	9	3	ND	2	29	1	2	2	83	.31	.07	5	26	1.14	144	.14	5	3.48	.02	.12	2	5	
DSB-MSOS 1 16 1 16 1 16 1 17 18 13 2 4 31 2 10 2 19 1 2 2 11 17 4 1.01 6 4 4 7 7 7 11 7 4 1.01 6 4 1.4 7 1 12 2 11 7 1 1 1 7 1 1 1 2 1 1 1 2 10 2 11 1 1 2 10 1 2 2 11 11 10 4 1.0 2 10 11 10 10 2 10 11 10 10 10 11 10 11 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 <th< td=""><td>058-34504</td><td>1</td><td>23</td><td></td><td>77</td><td>.1</td><td>14</td><td>8</td><td>821</td><td>2.64</td><td>7</td><td>2</td><td>KD.</td><td>2</td><td>19</td><td>1</td><td>2</td><td>2</td><td>44</td><td>.65</td><td>.12</td><td>7</td><td>14</td><td>. 34</td><td>172</td><td>.07</td><td>- 4</td><td>3.13</td><td>.02</td><td>.07</td><td>2</td><td>5</td><td></td></th<>	058-34504	1	23		77	.1	14	8	821	2.64	7	2	KD.	2	19	1	2	2	44	.65	.12	7	14	. 34	172	.07	- 4	3.13	.02	.07	2	5	
bis-bis-bis-bis 1 13 6 4 4 9 5 7.50 7.01 7 2 NO 2 19 1 2 2 31 .24 17 4 12 7.25 15 1 2 2 31 .24 17 4 12 2 31 .24 17 4 12 12 7.75 .16 5 1.4 4.51 20 7.7 .22 13 .24 16 5 1.4 4.51 10 5 2.77 .22 11 2 2 77 .42 .02 5 31 .47 .05 .23 .12 2 18 .14 18 14 18 14 18 14 18 14 18 14 18 14 18 14 18 14 18 14 18 14 18 14 18 14 18 18 11 18 <td>058-36505</td> <td>1</td> <td>16</td> <td>11</td> <td>60</td> <td>.1</td> <td>12</td> <td>4</td> <td>351</td> <td>2.33</td> <td>8</td> <td>2</td> <td>ND.</td> <td>2</td> <td>19</td> <td>1</td> <td>2</td> <td>2</td> <td>41</td> <td>.22</td> <td>.06</td> <td>4</td> <td>14</td> <td>. 34</td> <td>142</td> <td>.05</td> <td>4</td> <td>3.29</td> <td>. 22</td> <td>.10</td> <td>2</td> <td>.5</td> <td></td>	058-36505	1	16	11	60	.1	12	4	351	2.33	8	2	ND.	2	19	1	2	2	41	.22	.06	4	14	. 34	142	.05	4	3.29	. 22	.10	2	.5	
DSB-36507 1 S2 11 74 .1 11 9 S24 2.89 4 2 38 1 7 2 53 .18 .06 5 14 .51 207 .65 5 2.77 .02 1.13 2 5 DSB-36507 1 43 7 8 .1 25 2.07 6 5 1.4 .55 1.63 .57 1.72 .66 5 .3.4 .63 .12 2 1.63 .16 1.44 1.63 1.64 1.63 1.77 1.72 .66 5 .14 .15 .2 1.74 .2 2 7.75 .13 .14 1.2 .12 .14 1.33 .14 1.33 .14 1.4 1.2 .16 1.33 .2 1.33 .34 .17 .13 .14 .14 .14 1.2 .14 1.2 .14 1.2 .14 1.2 .14 1.2 .14 .14 .14 .14 .14 .14 .14 .14 .12<	058-36506	1	13		64	.4	9	5	750	2.01	7	2	ND	2	19	1	2	2	31	.24	.17	4	12	.26	177	.10	4	4.01	.03	30.	2	5	
PSB-34306 1 25 7 58 .1 25 9 22 3.0 6 3 M0 2 64 1 2 2 7 2.6 5 3.1 .75 172 .66 5 3.1.4 .61 1.12 2 2 77 2.68 .64 3 18 1.16 182 2.00 5 3.11 .75 172 .66 5 3.13 .63 1.16 2.2 2 77 2.68 .64 3 18 1.16 182 2.00 3.33 1.65 1.6 2 2.15 1.4 2 2.16 2 2.2 2.2 2.2 3.33 1.64 3 1.16 1.16 2.2 2.16 3.33 1.65 1.16 2.33 1.16 2.33 1.16 3.33 1.16 1.16 2.33 1.16 2.33 1.16 2.33 1.16 1.33 1.16 1.33 1.16 1.17 1.16 1.16 1.17 1.16 1.16 1.17 <th1.16< th=""> 1.16 <th1.17< td=""><td>058-36507</td><td>1</td><td>32</td><td>11</td><td>74</td><td>.1</td><td>11</td><td>9</td><td>526</td><td>2.89</td><td>4</td><td>2</td><td>ND</td><td>2</td><td>38</td><td>1</td><td>2</td><td>2</td><td>22</td><td>.18</td><td>.06</td><td>5</td><td>14</td><td>.51</td><td>207</td><td>.05</td><td>5</td><td>2.79</td><td>.92</td><td>.13</td><td>2</td><td>5</td><td></td></th1.17<></th1.16<>	058-36507	1	32	11	74	.1	11	9	526	2.89	4	2	ND	2	38	1	2	2	22	.18	.06	5	14	.51	207	.05	5	2.79	.92	.13	2	5	
Span-MaxBorn 1 Q3 B 70 -2 14 16 555 577 18 N0 2 20 77 2.68 .68 3 18 1.16 162 .68 5 7.12 2 77 2.68 .68 5 1.16 152 5.13 .44 235 .60 15 3.55 .66 45 3.77 .62 2 N0 2 2.77 1 2 2 1.33 1.55 .60 45 3.77 .62 .51 .33 1.54 .60 45 3.77 .62 .24 1 2 2 .65 .77 .61 42 .55 .66 45 .77 .64 .25 .77 .66 44 .71 .60 2 .44 .72 .55 .44 .67 .66 44 .71 .60 .21 .44 .66 47 .71 .60 .71 .75 .61 .77 .65 .11 .75 .67 .74 .67 .74 .67	058-36506	1	25	7	58	.1	25	9	292	3.07	6	3	ND	2	64	1	2	2	79	.43	.02	5	31	.75	172	.06	5	3.34	.63	.12	2	10	
DSB-34510 1 20 9 86 .7 17 6 477 2.64 13 2 27 1 2 2 41 125 .07 5 13 .44 235 .00 5 .13 .44 235 .00 5 .13 .44 23 .00 5 .13 .44 23 .00 5 .13 .44 23 .00 5 .13 .44 25 .00 2 .44 1 2 2 24 1 .22 2 24 1 .22 2 45 .72 .00 5 .13 .44 201 .00 2 24 1 22 2 45 .20 7 3 3 35 .66 4 17 1.00 25 .07 5 .13 .44 .03 .26 24 1 22 2 45 3 12 46 47 .26 25 35 35 35 .21 .46 17 100 25 <	058-34509	1	43	8	70	.2	14	16	222	3.97	18	5	ND.	2	60	1	2	2	77	2.68	.05	2	18	1.15	182	.08	5	2.12	.95	.32	2	5	
DSB-MASLI 2 28 10 83 .2 21 8 45 3.7 1 2 2 38 .33 1.54 .06 4 4.5 7.7 .03 7 14 .00 201 .06 5 .76 .65 .24 2 15 14 .00 25 .76 .65 .24 2 15 14 .00 25 .76 .65 .24 2 15 14 .00 25 .76 .65 .24 2 15 .14 .00 25 .76 .65 .24 2 .15 .14 .00 .25 .07 .26 .00 2 .44 1 2 2 .44 1 .25 .44 .25 .24 .45 .25 .21 .2 .26 .44 .15 .24 .46 .25 .24 .46 .25 .41 .25 .24 .46 .25 .24 .45 .25 .24 .45 .25 .24 .46 .25 .24	DSB-36510	1	20	5	88	.2	17	8	497	2.66	13	2	KD	2	27	1	2	2	41	.25	.07	5	13	.44	238	. 10	5	3.55	.02	.19	2	5	
bgs-34512 1 63 16 76 .4 14 12 607 3.45 12 2 40 2 44 1 2 2 65 .72 .03 7 14 .60 201 .66 5 .76 .42 1 2 2 65 .72 .03 7 14 .60 201 .66 5 .76 .72 .17 1.00 275 .09 5 .49 .62 .11 2 10 2 64 1 3 2 81 .29 .03 8 12 .46 174 .67 5 .44 .62 .15 13 73 14 .60 73 .44 .62 .15 13 .61 .13 .14 .11 .15 .14 .11 .13 .14 .11 .14 .12 .24 .24 .14 .22 .14 .22 .24 .13 .201 .15 .13 .201 .15 .291 .02 .11 .25 .291	059-36511	2	28	10	83	.2	21	8	445	3.39	6	2	ND	2	25	1	2	2	38	. 35	.04	5	13	*22	156	.06	4	2.21	.07	.14	2	5	
DSB-34513 1 73 8 128 .7 15 14 120 3.70 11 2 ND 2 64 1 3 2 81 .29 .66 4 17 1.00 275 .09 5 2.49 .62 .21 2 84 .104 .10 .11 .10 .10 .10 .10 .10 .10 .10 .10 .10 .10 .11 .10 .1	058-36512	1	63	10	75	.4	14	12	607	3.45	12	2	ND	2	64	1	2	2	65	.72	.03	7	14	.80	201	.06	5	2.95	.05	.26	2	15	
958-34514 1 154 4 101 44 17 10 545 3,20 4 2 N0 2 57 1 2 1 2 2 46 64 .05 6 11.2 .05 5.137 282 .11 13 51.4 .11 13 51.4 .11 4.17 4 3 N0 2 37 1 2 2 112 .33 .08 3 15 1.47 .05 5 .44 .07 5 7.47 .03 .15 5 3.44 .07 .34 .25 .15 .13 282 .13 282 .13 29 .14 2 2 101 .15 5 .14 .07 .15 .15 .14 .07 .15 .15 .14 .02 .14 .15 .15 .14 .15 .15 .11 .15 .15 .11 .15 .11 .16 .11 .15 .12 .12 .13 .21 .21 .23 .23 .23	058-36513	1	33	8	125	.2	15	14	1290	3.70	11	2	ND	2	64	1	3	2	81	.29	.08	4	17	1.00	275	.09	5	3.49	.92	.31	2	5	
958-36315 1 37 9 117 1 13 514 4.17 4 3 800 2 37 1 2 2 112 333 .000 3 15 1.57 282 1.15 5 4.14 .02 .333 .000 2 37 1 2 2 11 .333 .000 4 1.5 1.6 4.14 .02 .333 .000 2 24 1.15 24 1.02 .33 .000 4 2.14 .15 5 3.14 .02 .13 2.14 .02 .11 2 2 10 2 2 10 2 2 11 2 2 11 2 2 11 2 2 11 2 2 11 2 2 11 2 2 11 2 2 11 2 2 13 3 2 13 3 3 3 3 3 3 3 3 3 3 10 11 10 11	058-36514	1	36		104	.4	17	10	545	3.20	4	2	ND	2	59	1	2	2	46	.84	.05	8	12	.46	174	.07	- 5	2,42	.62	-17	2	5	
DSB-34516 1 50 10 79 .2 14 14 712 4.21 2 2 ND 2 84 1 2 2 91 .42 .06 2 24 1.36 24 .07 5 3.44 .03 .34 2 5 5 30 17 2 2 10 2 2 66 .23 .05 5 33 .99 80 .06 4 2.47 .35 13 2 .11 15 16 613 4.47 7 6 N0 2 53 .17 2 13 20 13 20 .11 15 5 3.44 .03 .14 2 2 13 .05 5 .33 .90 .06 4 2.47 .11 2 2 13 2 13 2 13 .05 1.11 5 3.14 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10	358-36515	1	37	7	117	.1	13	13	514	4.17	4	2	ND	2	37	1	2	2	112	.73	.08	2	15	1.37	282	.13	5	4.14	.02	. 35	2	5	
DSB-34517 1 44 6 54 .7 21 12 368 3.13 ? 2 MB 2 30 1 2 2 66 .73 .97 60 .06 4 7.47 .02 .11 2 5 33 .97 60 .06 4 7.47 .02 .11 2 5 33 .97 60 .06 4 7.47 .02 .11 2 5 33 .97 60 .06 4 7.47 .02 .11 2 5 33 .97 60 .06 4 7.47 .02 .11 2 5 33 .97 60 .06 4 7.47 .02 .11 2 5 33 .97 60 .06 4 7.47 .02 .11 2 5 33 .97 60 .06 4 7.47 .02 .11 2 5 .13 101 .11 .11 .11 .11 .11 .11 .11 .22 .11 <	DSB-36516	1	50	10	79	.2	16	14	712	4.21	2	2	ND	2	84	1	2	2	91	.42	.06	2	24	1.36	249	.07	5	3.44	.03	.34	2	5	
DSB-34518 1 36 10 96 .1 15 16 613 4.47 7 6 NB 2 54 1 2 2 135 .41 .04 2 15 1.31 201 .15 5 2.91 .02 .14 2 5 1 1 2 2 135 .41 .04 2 15 1.31 201 .15 5 2.91 .02 .17 9 9 .2 7 9 712 2.54 6 2 ND 2 63 1 2 2 133 .37 .06 3 6 .77 181 .02 3 .15 12 2 5 .99 .333 .37 .06 3 6 .77 181 .02 3 .15 1.5	058-36517	1	44	ò	54	.7	21	12	368	5.13	5	2	ND	2	30	1	2	2	66	.23	.05	5	22	.99	80	.06	4	2.47	.92	.11	2	5	
DSB-36519 1 24 10 81 .3 12 12 432 3.16 2 4 N0 2 39 1 3 2 78 .22 .12 2 13 .67 209 .11 5 3.59 .07 .17 2 5 DSB-36521 1 53 10 74 18 .2 7 9 712 2.54 6 2 N0 2 78 1 2 2 33 .37 .06 3 6 .77 181 .02 3 .55 .15 12 12 12 12 2 13 .64 10 .77 181 .02 3 .5 .15 1 .15 12 126 .15 .15 .15 .15 .16 .10 .15 .17 .15 .11 .10 .11 .10 .11 .10 .11 .10 .11 .10 .11 .10 .11 .11 .11 .11 .11 .11 .11 .11 <td>058-36518</td> <td>1</td> <td>36</td> <td>10</td> <td>96</td> <td>.1</td> <td>15</td> <td>16</td> <td>613</td> <td>4.47</td> <td>7</td> <td>6</td> <td>ND</td> <td>2</td> <td>54</td> <td>1</td> <td>2</td> <td>2</td> <td>135</td> <td>.41</td> <td>.04</td> <td>2</td> <td>15</td> <td>1.31</td> <td>201</td> <td>.15</td> <td>5</td> <td>2.91</td> <td>.02</td> <td>.14</td> <td>2</td> <td>2</td> <td></td>	058-36518	1	36	10	96	.1	15	16	613	4.47	7	6	ND	2	54	1	2	2	135	.41	.04	2	15	1.31	201	.15	5	2.91	.02	.14	2	2	
DSB-34520 1 17 9 98 .2 7 9 712 2.54 6 2 N0 2 63 1 2 2 33 .37 .06 3 6 .77 181 .02 3 2.55 .01 .15 2 2.55 .01 .15 2 2.55 .01 .16 4 10 .37 242 .03 5 7.7 9 7.12 2.54 5 ND 2 65 1 2 2 51 .91 .16 4 10 .37 242 .03 5 7.7 9 7.12 2.54 6 2 ND 2 65 1 2 2 95 .34 .05 2 16 1.30 246 .13 5 7.790 .04 .33 25 1.17 22 2.06 .13 35 .02 .01 2 2 10 .01 .02 37 1 2 2 95 .34 .05 2 16 .13	058-36519	1	24	10	31	.3	12	12	432	3.16	2	4	ND	2	39	1	2	2	78	.22	.12	2	13	.87	209	.11	5	1.59	.07	.17	3	5	
DSB-36521 i 53 10 94 .1 15 12 1263 3.06 11 2 N0 2 78 1 2 2 51 .91 .16 4 10 .37 242 .03 5 2.43 .02 .15 5 .04 .37 2 2 5 .34 .05 2 16 1.30 242 .03 5 2.43 .02 .15 5 .04 .37 2 2 .05 .34 .05 2 16 1.30 242 .03 5 2.43 .02 .04 .37 2 16 .03 13 5 ND 2 80 1 2 2 95 .34 .05 2 16 1.30 242 .03 5 7.43 .04 3 73 .04 3 73 .04 3 10 .45 .02 .01 .13 2 .02 .01 2 2 50 .13 10 2 .00 2 .11<	DS8-36520	1	17	9	98	.2	7	9	712	2.54	6	2	ND	2	63	1	2	2	22	.37	.06	2	6	.77	181	.02	2	2.55	+01	.17	2	5	
DSB-34522 1 61 11 121 .7 16 14 1105 4.03 13 5 MD 2 65 1 2 2 95 .34 .05 2 16 1.30 246 .13 5 7.90 .04 .33 2 2 95 .34 .05 2 16 1.30 246 .13 5 7.90 .04 .33 2 2.65 1 2 2 95 .34 .05 2 16 1.30 246 .13 5 7.90 .04 .33 177 222 .06 4 3.42 .02 .06 2 .06 4 3.42 .02 .06 2 .01 3 10 .01 <td>058-36521</td> <td>1</td> <td>53</td> <td>10</td> <td>74</td> <td>.1</td> <td>15</td> <td>12</td> <td>1263</td> <td>3.06</td> <td>11</td> <td>2</td> <td>ND</td> <td>2</td> <td>78</td> <td>1</td> <td>2</td> <td>2</td> <td>51</td> <td>.91</td> <td>.16</td> <td>4</td> <td>10</td> <td>. 37</td> <td>242</td> <td>.03</td> <td>5</td> <td>2,43</td> <td>.92</td> <td>.12</td> <td>2</td> <td>5</td> <td></td>	058-36521	1	53	10	74	.1	15	12	1263	3.06	11	2	ND	2	78	1	2	2	51	.91	.16	4	10	. 37	242	.03	5	2,43	.92	.12	2	5	
DSB-36523 5 272 13 73 .2 26 23 356 6.20 45 7 N0 2 90 1 2 2 199 .73 .04 3 251 1.77 222 .06 4 3.42 .52 .06 2 .10 2 1 2 2 199 .73 .04 3 251 1.77 222 .06 4 3.42 .52 .05 .13 2 2 10 2 2 10 2 2 10 2 2 10 3 10 .49 185 .07 4 3.29 .02 .13 2 2 50 .04 3 10 .49 10 2 .00 2 20 17 1 2 2 50 .01 4 3.29 .02 .13 2 2 50 .05 3 10 .49 10 2 .02 .01 11 2 .01 2 .01 .02 .02 .21	058-36522	1	61	11	121	.2	16	14	1105	4.03	13	5	ND	2	65	1	2	2	95	.34	.05	2	16	1.30	246	.15	5	2.90	.04	.32	2	5	
DSB-36524 2 27 11 72 .5 15 11 620 2.81 6 2 ND 2 22 1 2 2 52 .23 .10 3 10 .49 185 .09 4 3.29 .02 .13 2 25 570 A-1/AU 0.5 1 31 38 181 .3 36 12 10022 2.84 11 2 ND 2 37 1 2 2 60 .61 .09 8 73 .74 252 .06 8 2.08 .02 .21 2 250 9.92 .05 3 19 .65 77 .03 3 1.58 .02 .24 2 50 53 19 .65 77 .03 3 1.58 .02 .24 2 50 53 14 40 3.35 4 2 ND 2 12 12 90 153 .16 41 2.79 .02 .17 2 5 53	058-36523	5	272	13	73	.7	25	23	396	6.20	45	7	ND	2	90	1	z	2	199	.73	.04	3	75	1.77	722	.08		3.42	.52	.06	2	10	
STD A-1/AU 0.5 1 31 38 181 .3 36 12 1022 2.84 11 2 ND 2 37 1 2 2 60 .61 .09 8 73 .74 252 .06 8 2.08 .92 .21 2 510 DSB-34525 1 59 6 43 .7 13 10 348 2.31 10 2 54 1 2 2 50 9.92 .05 3 19 .65 77 .03 3 1.58 .02 .24 2 5 DSB-34526 1 54 12 95 .5 11 12 440 3.35 4 2 ND 2 17 1 2 2 99 .24 .10 2 153 .16 4 2.97 .02 .17 2 5 DSB-34527 1 149 9 81 .2 20 17 37 13 10 3 ND 2 12	DSB-36524	2	27	11	72	.5	15	11	620	2.81		2	ND	2	22	1	2	2	52	.23	.10	3	10	.49	185	.05	4	3.29	.02	.13	2	25	
DSB-34525 1 59 6 43 .7 13 10 348 2.31 10 2 N0 2 54 1 2 2 50 9.92 .05 3 19 .65 77 .03 3 1.58 .02 .24 2 5 5 11 12 440 3.35 4 2 ND 2 17 1 2 2 99 .24 .10 2 12 .80 153 .16 4 2.97 .02 .17 2 5 5 11 12 440 3.35 4 2 ND 2 17 1 2 2 99 .24 .10 2 12 .80 153 .16 4 2.97 .02 .17 4 3.35 .02 .24 2 12 .24 .10 2 12 .24 .10 2 12 .25 .11 2 .24 .21 .11 2 .24 .21 .11 2 .24 .21	STD A-1/AU 0.5	1	31	38	181	.3	36	12	1022	2.84	11	2	ND	2	37	1	2	2	60	.61	.07	8	73	.74	252	.06	3	2.08	. 92	.21	2	510	
DSB-34526 1 54 12 55 15 12 440 3.35 4 2 ND 2 17 1 2 2 99 .16 17 100 51 100 51 100 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11	058-14575	1	59	4	43	7	17	10	149	2.31	10	2	ND.	2	54		2	2	50	0 02	05		10	25	77	10		1 50	67	24			
DSB-34527 1 14 17 17 17 17 17 11	059-14524		54	12	95	5	11	12	440	27.7		;	ND	-	17		-	;	00	24		-		.00	157	.04	ĩ	2 07	.02		-		
SSB-34520 1 77 7 98 .1 16 15 454 4.07 19 2 10 2 10 2 12 12 12 12 11 138 .11 3 3.33 .02 .22 2 10 1 2 12 12 12 11 10 1 3 .133 .02 .22 2 10 1 10 3 .133 .02 .22 2 121 .19 .06 3 19 .97 169 .20 3 2.89 .02 .22 10 10 .9 .11 3 .33 .02 .22 2 10 17 .99 .01 .22 2 121 .19 .97 169 .20 3 2.99 .02 .22 2 10 .9 .11 2 2 86 .26 .05 3 16 .16 16 16 17 .9 .11 2 2 85 .26 .05 3 16 .16 <td>059-14527</td> <td></td> <td>149</td> <td></td> <td>21</td> <td>2</td> <td>20</td> <td>17</td> <td>171</td> <td>4 14</td> <td>-</td> <td>÷</td> <td>NO.</td> <td>2</td> <td>27</td> <td></td> <td>5</td> <td>5</td> <td>177</td> <td>24</td> <td></td> <td>:</td> <td>74</td> <td>1.12</td> <td>181</td> <td>.10</td> <td></td> <td>7 18</td> <td>.02</td> <td>.11</td> <td>-</td> <td></td> <td></td>	059-14527		149		21	2	20	17	171	4 14	-	÷	NO.	2	27		5	5	177	24		:	74	1.12	181	.10		7 18	.02	.11	-		
Solution 1 1 10 13	BCB_ 14570	:		2	00		14	15	151	4.07	10	2	-	-	14				124	10	.00	- 2	1	1.12	100	.17		5.33	.92	.20	-		
DSB-34530 1 45 9 84 .3 20 13 697 3.59 5 2 HD 2 32 1 2 2 83 .34 .08 5 30 1.04 160 .10 4 2.76 .03 .29 2 5 DSB-34531 1 62 8 52 .4 171 21 530 3.77 9 2 NO 2 51 1 2 2 87 .62 .07 4 97 1.74 165 .12 4 2.63 .03 .34 2 5 DSB-34532 1 19 14 67 .4 103 9 250 2.89 6 2 10 7 17 10 3 42 .58 104 .13 4 3.99 .03 .07 2 5 .17 10 3 40 .5 .07 2 <td< td=""><td>059-36529</td><td>i</td><td>32</td><td>á</td><td>73</td><td>.4</td><td>14</td><td>12</td><td>529</td><td>3.20</td><td>7</td><td>5</td><td>xo</td><td>2</td><td>19</td><td>i</td><td>ź</td><td>2</td><td>86</td><td>.26</td><td>.05</td><td>3</td><td>16</td><td>.78</td><td>176</td><td>.15</td><td>3</td><td>2.74</td><td>.02</td><td>.15</td><td>2</td><td>10</td><td></td></td<>	059-36529	i	32	á	73	.4	14	12	529	3.20	7	5	xo	2	19	i	ź	2	86	.26	.05	3	16	.78	176	.15	3	2.74	.02	.15	2	10	
958-34531 1 62 8 52 .4 171 21 530 3.77 9 2 NO 2 51 1 2 2 87 .62 .07 4 97 1.74 165 .12 4 2.63 .03 .34 2 5 958-34532 1 1 9 14 67 .4 103 9 250 2.69 6 10 7 10 3 42 .58 104 .13 4 3.98 .03 .07 2 50 .19 1 2 2 56 .17 .10 3 42 .58 104 .13 4 3.98 .03 .07 2 5 .27 .24 10 3 42 .58 104 .13 4 3.98 .03 .07 2 5 .27 .24 10 3 80 .07 2 5 .27 <	058-36530	1	45	9	84	.3	20	13	697	1.59	5	7	ND	7	37	,	7	,	78	u	0.9		-	1.04	160	10		7 74	76	20			
DSB-34532 1 19 14 67 .4 103 9 250 2.89 5 2 ND 2 19 1 2 2 58 .17 .10 3 42 .58 104 .13 4 3.98 .03 .07 2 5 DSB-34533 3 29 11 210 .2 133 14 441 3.30 10 2 ND 2 22 1 2 2 72 .24 10 3 80 73 125 11 4 3.98 .03 .07 2 5	17245-1820	1	62		52		171	21	510	3.77		2	NO	2	51	- 1	5	5	87	47	.07		07	1.74	145	.10	- 1	2 43	.03		- 5	:	
658-34533 3 29 11 210 .2 133 14 441 3.30 10 2 10 2 27 1 2 27 27 4 10 3 80 17 19 11 4 3.10 10 7 2 5	059-34532	1	19	14	67	4	103	9	250	2.99		;	ND	-	10	1.5	-		50	17	107	-	12	50	103	.17	- 1	7 00	.03		-		
	TT24T-820	3	29	11	210	3	571	14	441	3.30	10	2	ND.	2	22	1	5	2	72	24	10		94		195			2.10	.03	.07		2	

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I.M. WATSON & ASSOCIATES PROJECT # NAKUSP FILE # 83-2358

SAMPLE #	Mo pps	Cu ppa	Pb pps	Zn ppa	Ag ppa	Ni ppe	Co ppe	Mn ppe	Fe	As ppa	U pps	Au ppe	Th pp=	Sr ppn	Cd ppa	Sb ppm	Bi ppn	V pps	Ca Z	P Z	La ppa	Cr ppa	Ng	Ba ppa	Ti Z	B ppe	Al I	Na Z	ĸ	W ppa	Aut ppb
30N 27+50E	3	53	17	75	.3	16	16	363	5.99	27	2	ND	2	55	1	2	2	82	.43	.03	2	17	1.03	152	.03	5	3.69	. 02	.04	2	5
30N 27+75E	1	64	17	123	.2	18	20	1367	5.86	42	2	ND	2	30	1	2	2	75	.24	.11	2	14	.72	217	.04	6	3.92	.01	.05	2	•
30N 28E	1	32	13	91	.3	18	12	760	3.92	25	3	ND	2	25	1	2	2	54	. 16	.08	4	72	.65	151	.04	4	2 82	01	05	-	š
30N 28+25E	1	42	18	108	.3	19	14	1667	4.22	20	3	ND	2	45	1	2	2	54	.74	.13	3	17	.57	201	.04	5	3 25	01	05	5	5
30N 28+50E	2	28	18	92	.3	18	11	1048	4.15	19	3	ND	2	21	1	2	2	58		.08	4	77	.77	172	04	5	3 17	01	04	-	5
30N 28+75E	3	23	18	123	.5	21	10	2437	3.68	29	4	ND	2	15	2	2	2	39	.42	.16	ì	19	.54	166	.05	5	3.60	.01	.03	2	5
30N 28+95E	2	23	13	94	.5	17	10	748	3.30	22	2	ND	2	19	1	2	2	46	.11	.11	4	19	. 46	140	.04	4	7.77	01	. 05	7	5
30N 29+25E	2	24	13	85	.5	17	10	805	3.21	16	3	ND	2	21	1	2	2	47	.22	.11	3	23	. 50	157	.05	4	7.94	.01	.04	5	Ę
30N 29+50E	3	28	17	110	.5	16	9	753	3.26	20	2	ND	2	19	1	2	2	44	.12	.08	6	25	.51	126	.06	4	1.75	.01	.05	-	5
30N 29+75E	5	27	15	86	.4	20	10	601	3.84	13	4	ND	2	20	1	2	2	56	.10	.06	4	11	. 67	145	05	4	7 88	01	04	-	ĩ
29+75N 27+50E	i	33	13	102	.3	16	13	904	4.24	25	2	ND	2	37	i	2	2	61	.23	.05	3	19	.86	173	.03	5	3.29	.01	.05	ž	25
29+75N 27+75E	1	40	17	97	.5	18	13	B47	3.82	18	2	ND	2	30	1	2	2	54	.22	.08	4	18	. 67	156	.04	5	3.00	.01	.06	2	5
29+75N 28E	1	35	14	91	.2	16	13	608	4.35	26	6	ND	2	33	1	2	2	60	.17	.09	3	13	.61	169	.04	5	3.12	.01	06	-	5
29+75N 28+25E	2	54	15	87	.4	24	13	682	3.81	16	3	ND	2	83	1	2	2	59	. 19	.12	3	74	.71	161	05	4	3 42	07	07	-	5
29+75N 28+50E	3	30	14	226	.3	16	12	1182	3.95	14	2	ND	7	27	3	2	2	56	.77	.07	i.	25	83	170	05		3 28	01	05	÷	ŝ
29+75N 28+75E	1	28	14	83	.5	24	10	436	3.22	14	4	ND	2	17	- 1	2	2	46	.11	.08	6	29	. 59	144	.05	4	2.87	.01	.05	2	5
29+75N 29E	2	26	15	78	.6	21	9	658	3.74	26	4	ND	2	17	1	3	2	50	. 12	.07	7	29	.59	153	. 05	4	7.78	. 01	.05	2	5
29+75N 29+25E	2	23	15	70	.5	19	9	404	3.39	16	3	ND	2	19	1	2	2	51	.15	.10	5	28	.51	112	.04	4	7.76	.01	.05	2	š
29+75N 29+50E	2	62	16	84	.9	17	7	1172	2.62	15	5	ND	2	42	2	2	2	37	1.31	.11	11	24	.44	97	.04	4	3.60	.07	64	-	5
29+75N 29+75E	5	52	15	131	.7	20	15	1791	5.07	12	6	ND	2	36	2	2	2	45	.93	.12	11	22	.52	110	.05	6	7.89	.02	04	5	5
29+75N 30E	4	77	14	89	1.0	25	10	1081	3,18	12	4	ND	2	36	2	2	- 2	42	1.18	.08	12	37	.64	75	.04	5	3.54	.02	.05	ž	5
29+50N 27+50E	2	38	15	95	.3	18	.13	620	4.14	21	3	ND	2	50	1	3	2	62	. 28	.05	4	22	.90	152	.04	5	97.79	.01	.0ė	2	5
29+50N 27+75E	2	39	17	97	.3	15	14	788	4.29	22	4	ND	-7	47	1	3	2	64	.21	.08	3	18	.78	173	.04	5	7. 77	.07	.06	2	5
29+50H 28E	2	50	18	84	.4	16	13	332	4.85	22	6	ND	2	41	1	2	2	69	. 26	.05	4	16	. 69	139	.05	5	7.97	.07	.06	2	•
29+50N 28+25E	1	31	13	108	.2	13	11	484	4.46	12	2	ND	2	54	1	2	2	58	. 31	.04	2	19	1.25	184	.11	5	4.77	.03	05	2	ŝ
29+50N 28+45E	2	30	14	73	.5	14	9	413	3.86	19	4	ND	2	24	1	2	2	59	.08	.05	4	20	.59	138	. 05	5	2.89	.02	.05	2	5
29+50N 28+75E	2	37	13	95	.5	20	11	570	3.43	15	2	ND	2	27	1	2	2	50	.13	.07	6	25	.56	150	.06	4	3.39	. 02	.05	2	5
29+50N 29E	1	21	15	108	.3	17	9	2567	3.21	15	2	ND	2	18	1	2	2	51	.23	.07	4	27	. 56	244	.05	4	2.47	.01	.05	2	5
29+50N 29+25E	1	24	16	85	.7	15	7	259	3.06	9	4	ND	2	14	1	4	2	46	.17	.17	5	24	.43	166	.05	4	7.51	.01	.04	2	5
29+50N 29+50E	1	33	13	87	.5	26	11	453	3.42	12	2	ND	2	17	1	3	2	53	.16	.05	B	39	.72	158	.05		2.71	.07	07	-	5
29+50N 29+75E	1	22	12	102	.1	17	8	420	3,02	3	2	ND	2	11	1	3	2	46	.05	.07	6	28	.50	150	.06	4	2.56	.01	.05	2	5
29+50N 30E	3	75	13	98	1.2	20	9	1103	3.32	12	4	ND	2	27	1	4	2	62	.55	.06	13	28	. 63	105	.05	5	3.09	.07	.06	2	5
STD A-1/AU 0.5	1	30	38	162	.3	35	12	1041	2.85	11	2	ND	2	37	1	2	2	58	. 58	.09	7	73	.72	279	.08	8	2.07	.07	.19	2	510

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I.M. WATSON & ASSOCIATES PROJECT # NAKUSP FILE # 83-2358

SAMPLE #	Mo ppe	Cu ppe	Pb ppe	Zn pp s	Ag pps	Ni ppa	Co pps	Ko ppe	Fe	As ppm	U ppa	Au ppa	Th pp=	Sr ppm	Cd pp m	Sb pp a	Bi pps	V pp∎	Ca X	P 2	La ppm	Cr ppe	Ng X	Ba pp e	Ti I	B pp=	Al X	Na Z	ĸ	N ppe	Au1 ppb
						-					4			75	2	-	•		07			74	70	150	07	5	7 50	61		•	
29+25N 27+50E	3	36	15	105	• 2	20	14	1215	9, 30	14	2	UN	4	34	-	4	4	00	. 00	.04	5	70	./0	110	.05	5	7 00	.01	.05	4	
29+25N 27+75E	2	42	14	87	.2	20	14	142	3.43	10	2	NU	2	30	1	2	2	00	.21	.05	3	20	./3	107	.05	-	3.07	.02	.04	-	10
29+25N 28E	2	22	13	75	.2	19	12	544	3.68	15		ND	2	31	1	4	4	51	.17	.04		28	.14	137	.05	0	2.8/	.01	.07	4	2
29+25N 28+25E	1	23	13	100	.2	16	12	381	3.83	13	2	ND	2	38	1	3	2	61	.13	.09	5	22	. 64	149	.0/	3	3.62	.01	.05	2	5
29+25N 28+50E	2	30	11	66	.4	19	10	292	3.45	16	2	ND	2	23	1	2	2	22	. 15	.04	2	22	. 69	m	.05	•	2.68	.02	.05	2	2
29+25N 28+75E	2	24	12	84	.4	18	8	459	3.11	12	2	ND	2	16	1	2	2	49	.11	. 07	6	28	. 55	137	.05	4	2.48	.01	.05	2	5
29+25N 29E	1	20	15	70	.2	16	7	517	3.07	10	2	ND	2	15	1	2	2	50	.11	.05	6	26	. 48	120	.07	5	2.71	.02	.05	2	5
29+25N 29+25E	2	24	10	73	.6	18	8	306	2.95	11	2	ND	2	13	1	2	2	50	.11	.05	5	30	. 54	117	.07	5	2.69	.01	.05	2	5
29+25N. 29+50E	1	35	16	76	.9	24	8	546	3.25	10	2	ND	2	18	1	2	2	52	.25	.04	9	33	.47	138	.08	4	3.33	.02	. 06	2	5
29+25N 29+75E	2	30	13	77	.3	21	9	355	3.13	5	2	ND	2	19	1	2	2	52	.23	.04	7	32	. 54	119	.07	4	2.67	.02	.05	2	5
	i	22	10	95		18	7	351	3.08	12	7	NO	2	11	1	2	. 7	46	. 09	.08	6	31	.46	113	.07	4	2.69	.07	.05	2	5
20N 274505	5	70	14	140	2	19	14	2043	4 40	12	2	ND	2	77	2	5	2	67	.62	10	7	40	. 93	144	.03	5	4.30	.01	.03	2	5
201 27.300	ĩ			00		70	14	101	1 05	11	ŝ	ND	-	40	ĩ	7	2	85	76	04	4	50	1 78	161	09	4	4.13	.04	.07	2	5
20N 20F	÷.	70		07		20	17	704	7 07	14	2	ND	2	20	i	2	;	45	13	05	5	28	77	177	.06	4	77.7	.07	.07	2	5
ZYN ZBE	4	34	19	11		20	13	179	3.02	17	4	ND	-	21	-	-	-	75	10	.03	i	20		140		5	4 40	.02	09	-	š
24N 28+25E	1	28	15	43		18	10	212	3.8/	15	4	NU.	4	51	1	4	*	13	.17	.01		20	.74	107		2	4.41	.05	.00	-	-
29N 28+50E	2	21	12	69	.4	17	9	317	3.30	14	2	ND	2	14	1	2	2	49	. 08	.05	5	27	.45	121	.06	4	3.08	.01	.04	2	10
29N 28+75E	1	19	13	79	.4	15	7	875	2.84	8	4	ND	2	16	1	2	2	47	.16	.07	6	25	. 44	130	.06	4	2.36	.01	.05	2	5
29N 29E	2	32	12	73	.4	22	10	594	3.18	14	2	ND	2	17	1	5	2	54	.14	.05	8	38	.71	117	.06	5	2.55	.01	.07	2	5
29N 29+25E	1	20	11	64	.4	14	6	292	2.86	9	4	ND	2	11	1	2	2	47	.07	.05	4	27	.42	102	.05	4	2.12	.01	.04	2	10
29N 29+50E	2	31	17	59	.7	21	9	1495	3.18	13	3	ND	2	18	1	2	2	54	.39	.06	8	30	. 48	144	.07	5	3.21	.02	.05	2	5
29N 29+75F	1	28	13	61		20	8	666	2.82	10	3	ND	2	14	1	2	2 -	47	.15	.07	- 6	33	.53	165	.06	5	2.27	.01	.05	2	5
28+75N 27+50F	2	38	14	BT	.7	25	14	501	3.61	13	2	ND	2	29	1	3	2	69	.12	.04	4	42	1.04	116	.07	5	3.27	.02	.06	2	5
28+75N 27+75F	- T	77	11	99	3	20	13	665	3.78	9	2	ND	2	11	1	7	2	79	.17	.08	4	28	1.14	142	.09	5	3.37	.02	.06	2	5
201751 200	2	12	12	77		27	11	504	TAI		÷	ND	-	19	i	2	2	56	09	.05	7	74	.72	136	.07	4	3.28	.07	.06	2	5
20175H 200-255	-	71	14	70	.4	23		570	7 77	17	2	ND	-	21		2	2	55		07		17	4.8	137	.04	5	1 25	.07	.06	2	5
28+134 28+236	2	21	12	/6		25	11	3/4	3.31	15	-	U.N.	4	21	•	-	•	55				52		101			5.25				
28+75N 28+50E	2	24	13	66	.4	19	9	445	3.22	12	2	ND	2	19	1	2	2	53	.13	.05	6	30	.59	109	.06	4	2.82	.02	.05	2	5
28+75N 28+75E	1	22	9	83	.4	17	9	758	3.13	12	2	ND	2	16	1	4	2	52	.09	.08	6	27	. 51	130	.06		2.88	.01	.05	2	2
28+75N 29E	1	20	14	80	.6	18	8	671	3.00	14	3	ND	2	13	1	2	2	49	.11	.07	6	31	.50	125	.07	4	2.84	.02	.05	2	5
28+75N 29+25E	1	23	12	85	.3	22	9	747	3.01	23	2	ND	2	15	1	2	2	51	.15	.08	6	36	.55	148	.07	5	2.62	.02	.06	2	5
28+75N 29+50E	1	16	13	64	.5	15	6	457	2.77	12	2	ND	2	14	1	3	2	45	.12	.09	5	27	. 37	111	.07	4	2.26	.02	.04	2	5
28+75N 29+75E	2	22	13	81	.4	21	10	451	3.17	13	2	ND	2	11	1	2	2	50	.07	.08	6	35	. 49	123	.08	5	3.19	.02	.05	2	5
28+75N 30E	1	18	13	71	.4	18	7	315	3.07	11	2	ND	2	11	1	2	2	53	.07	.12	6	36	.46	113	.05	4	2.52	.02	.05	2	5

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and the second state of the construction of the

I.M. WATSON FILE # 83-2151 PROJECT # NAKUSP

SAMPLE #	No pos	Cu ppe	Pb	In ppe	Ag ppa	Ni PD#	Co pos	Mn	Fe	As post	U	Au	Th ppe	Sr	Cd	50	Bi	V	C.	P	La	Cr	Mg	Ba	Ti	3	AL	Ha	ĸ		Aul
						-		1470			-					-	-			-		~		154			2 54	- 12			
KS-32233		14	10	194		-	14	14/0	3.33	10	-	nu	3	17	- 20	- 1	4	01	.10			23		130		- 2	1.00				
RX8-32256	1	zs	1	139	.2	31	17	244	4.20	19	2	ND	2	75	1	2	2	110	.16	.17	3	52	.54	117	.17	2	3.11	.92	.05	2	,
PXB-32257	1	64	4	109	.2	129	16	440	4.13	15	2	ND	2	28	1	2	2	93	.40	.09	4	67	.93	170	.14	2	2.85	.02	.21	2	5
FXB-37258	- i -	43	7	69	.4	143	20	973	3.81	8	2	ND	2	26	1	2	2	101	. 48	.05	4	182	1.78	213	.19	2	2.98	.01	.30	2	5
PTR-17259	i	40	17	103		. 44	15	1015	4.34	74	2	ND		20	1	2	2	107	.18	.06	3	37	.97	157	.12	2	2.90	.01	.14	2	5
PYR-12210		12		105		24	14	404	1 77	17	-	NO.	5	11		2	5	01	37	67	Ť	27	04	175	14		1 47	20	12		5
DVD-32290		40		100		20	17	101	4 10					27				07			1	-	1 21	107			1.41	07	21		÷
ND-32202	1	40	1.	100	.,	"	15	901	4.10	1.	*	nu	1	23		4	4	83	. 33	.04		12	1.21	112	.1.0	•	3.01			•	
RKB-32263	1	51	15	214	.2	23	20	2138	5.15	27	2	ND	2	25	2	2	2	96	1.61	.09	7	22	1.53	322	.14	3	2.64	.02	.35	2	10
PXB-32264	1	54	11	118	.1	15	17	1288	4.81	13	5	ND	2	32	2	2	2	145	1.38	.04	3	17	1.52	228	.20	2	2.70	.02	.55	2	5
RKB-32265	1	56	5	91	.2	23	14	554	4.69	15	2	MD	2	41	2	2	2	101	.86	.03	5	36	2.07	86	.23	2	3.48	.05	.09	2	5
8XB-37766	7	21	19	69		17		584	3.65	16	4	ND	7	40	2	2	2	56	5.89	.04	6	41	7.77	79	.04	6	2:93	.07	.07	2	5
BYB-17747	1	13	10	141			2	1414	3 42	14		ND	5	78	5	5	2	59	1.04	05	10	50	2 70	172	.08		1.15	. 67	.08	2	4
NUR STERN	10			100				1.131					•		•	•	•													•	
FXB-32268	3	17	10	52	.3	11	5	526	1.92	22	2	ND	2	84	2	2	2	16	12.06	.04	3	15	.93	72	.01	6	1.47	.01	.04	2	5
RXB-32269	1	69	7	110	.3	11	16	615	4.87	15	-4	ND	2	18	1	2	2	197	.41	.05	2	10	1.83	187	.25	2	3.27	.01	.35	2	10
STD A-1/AU 0.5	1	30	38	177	.3	36	12	1045	2.80	9	2	ND	2	37	1	2	2	58	.59	.10	1	71	.71	273	.08	9	2.08	.02	.21	2	530
														-				-	~											114	
KKB-322/0 +		24		41		18	14	333	4.03	10	- 5	AU .	4	20		4	4	44	.28	.04		11	. 11	130	.18	4	3.20	.02	. 15		
RX3-32271	1	82	11	74	.2	18	16	441	4.31	12	- 2	ND	2	41	1	2	2	116	и.	.06	2	28	1.32	128	.18	2	3.34	.02	.77	2	2
RKB-32272		76	9	62	.2	474	17	992	2.81	12		N2	2	45	1	2	2	104	.42	.05	4	41	1.23	119	.21	2	2.91	.02	.16	2	5
RXB-32273	1	37	- 5	112	.3	368	14	821	3,97	11	4	ND	2	29	1	2	2	86	.30	.06	4	- 54	.98	182	.15	2	3.27	.02	.18	2	5
forB-32274	1	58	7	90	.3	202	14	676	3.07	14	3	XD.	2	42	1	2	2	74	.56	.05	6	51	.95	117	.14	3	7.50	.03	.13	2	5
RKB-32276	1	26	10	81	а	17	8	600	2.94	12	4	ND	2	16	1	2	2	64	.19	.11	1	15	.48	117	.13	4	3.19	.02	.07	2	5
US8-33102	1	20	14	97		76	11	900	3.47		2	10		745		2	,	80	1.20	0.9	14	11	1.29	114	20	2	1.54	.08	.77		56
USB-33103	1	74	13	77	1	71	11	877	1 10	7	-	10	÷	169	i	-	-	74	79	04	19	TO	1.00	84	11	-	7.90	04			20
USB-33104		74	20	85			1	1001	2.57	5	-	NO.		107	1	-		10	.74		20	17	1.10	60	.15	:	7 71			-	120
20177-821	1	74	15	07				013	2.03	-	-	No.	-	130		-	4	34	.75	.00	2V	13		01	.04	:	2.71		***	- 2	10
278 A.LINIA -	- 21	20	15	6/		11		142	1.89	1	4	NO	2	81	1	2	1	22	.43	.08	15	23	.36	172	.10	2	2. 20	.00	-16	1	10
310 H-1/HU 0.5	4	20	36	182		22	13	1010	2.79	11	2	ND	2	35	1	2	2	59	.59	.10	7	74	.71	275	.08		Z.05	.02	.21	- 2	216

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SAMPLE .	No ppe	Cu ppe	Pb ppe	Zn ppe	Ag pp=	Ni PP=	Co pp=	Mn ppm	Fe	As pp=	U ppm	Au pp=	Th ppa	Sr ppm	Cd ppm	Sb ppm	Bi pps	V pp=	Ca Z	PI	La ppm	Cr pp=	Mg	Ba ppm	Ti Z	B pp=	A1 7.	Na T	K Z	W ppa	Aut ppb
USB-33106	1	29	19	84	. 6	11	8	1195	2.82	5	4	ND	4	135	1	2	2	38	. 64	.04	25	15	.57	79	.03		2.51	.02	.29	2	45
USB-33107	i	37	70	91	.8	18	8	1232	3. 71	12	17	ND		115	1	2	2	57	.64	.04	27	74	.65	104	.07	5	3.11	.03	.75	7	20
USB-11108	1	74	17	78	4	9		\$20	7.44		3	ND	5	137	i	5	5	70	1.05	04	25	17	52	40	05	ĭ	2 94	10	75	-	10
1058-TT109	i	14	10	77	1	7	5	937	7. 17	5	ĩ	ND	5	135	i	2	2	37	92	06	18	11	52	41	05	4	7 44	07	27	-	5
USB-33110	ĩ	25	16	83	.4	11	6	1106	2.64	4	3	ND	4	164	i	2	2	45	. 86	.05	21	15	.58	97	.06	ţ	2.99	.03	.23	2	5
JSB-33111	1	17	14	61	.4	8	4	660	2.08	3	3	ND	4	121	1	2	2	35	. 65	.07	17	11	.42	78	.08	4	2.89	.04	.20	2	5
US6-33112	3	172	25	104	.2	20	30	858	8.11	38	5	ND	2	65	2	2	2	113	.74	.04	4	20	1.63	113	.08	3	5.37	.02	.14	2	15
USC-33113	4	115	23	94	1.1	72	25	769	4.90	61	ó	ND	2	219	2	2	2	30	3.94	.10	2	40	1.99	82	.01	5	1.32	.01	.30	2	25
30N 26E	1	89	15	119	.2	21	18	656	4.18	22	5	ND	2	70	1	2	2	92	.18	.04	4	25	.90	196	.10	5	4.28	.03	.22	2	20
JON 27E	1	56	13	137	.2	13	27	1283	5.35	17	4	ND	2	119	1	2	2	110	.65	.13	3	14	1.19	178	.08	6	3.39	.03	.25	2	5
30N 28E	5	38	19	60	.5	20	15	907	4.53	22	5	ND	2	39	2	2	2	53	5.36	.04	4	31	2.57	41	.02	7	3.20	.01	.07	2	5
30N 29E	7	33	18	94	.3	28	13	779	4.03	25	6	ND	2	23	1	2	2	64	. 39	.06	9	45	.88	149	.09	6	3.90	.02	.09	2	5
30N 31E	5	20	23	208	.2	25	8	2845	5.57	29	4	ND	2	19	5	2	2	76	1.55	.08	15	101	1.33	159	.06	6	3.31	.01	.08	2	5
30N 32E	1	18	22	131	.3	23	10	1303	3.74	29	5	ND	2	24	2	2	2	72	.91	.07	13	36	.67	160	.10	8	4.25	.03	.09	2	5
30N. 33E	3	34	63	122	.3	25	10	715	2.73	20	2	ND	2	25	1	2	2	50	. 39	.07	7	27	.54	122	.10	5	3.14	.03	.09	2	20
JON 34E	1	43	18	129	.1	30	17	1410	3.39	19	5	ND	2	26	1	2	2	81	.33	.10	7	37	.81	190	.11	5	3.39	.05	.17	2	15
29N 26E	1	44	13	94	.3	17	13	497	3.78	11	4	ND	2	41	1	2	2	87	.33	.05	ó	24	1.10	150	.12	5	3.54	.03	.14	2	5
29N 27E	2	54	16	132	.2	23	16	1124	4.34	17	3	ND	2	35	1	2	2	77	.47	.05	8	28	1.09	157	.10	5	4.00	.03	.14	2	10
29N 28E	1	49	15	99	.3	37	20	813	4.01	9	5	ND	2	50	1	2	2	99	. 36	.05	5	62	1.63	160	.12	4	4.99	.07	.09	2	5
29N 29E	2	22	14	75	.5	17	8	558	3.26	15	5	ND	2	16	1	2	2	61	.12	.06	9	30	.57	117	.05		2.71	.03	.08	2	5
29N 31E	1	54	14	119	.2	15	13	763	4.13	7	6	ND	Z	37	1	2	2	119	.27	-09	4	23	1.02	136	.11	4	3.64	.03	.08	2	60
29N 32E	-1	79	11	103	.3	32	22	565	4.18	13	8	ND	2	34	1	2	2	122	. 23	.06	7	60	1.39	116	.18	4	4.09	.03	.12	2	10
29N JJE	2	28	15	120	.3	27	15	925	3.72	23	5	ND	2	37	1	2	2	67	. 35	.08	á	31	.75	156	.11	5	3.51	.03	.13	2	5
29N 34E	1	28	13	97	.3	19	11	954	2.71	4	4	ND	2	56	1	2	2	58	.44	.14	7	26	.64	210	.10	4	3.31	.03	.12	2	5
28W 26E	1	12	13	33	.5	10	á	565	2.07	3	4	ND	2	52	1	2	2	38	7.49	.02	6	23	4.65	71	.05	3	2.29	.02	.04	2	5
28N 27E	1	71	8	91	.2	31	22	402	4.41	9	5	ND	2	34	1	2	2	110	. 37	.05	5	48	1.50	90	.19	5	3.65	.07	.09	2	5
28N 28E	2	35	14	105	.5	27	12	726	3.59	16	6	ND	2	23	1	3	2	65	.35	.07	11	41	.80	148	. 10	4	3.63	.03	.12	2	5
28N 29E	1	21	15	86	.3	22	9	919	2.94	9	5	ND	2	20	1	2	2	55	.21	.08	9	34	.63	141	.09	5	2.96	. 93	.09	2	5
28N 31E	1	32	15	101	.2	28	13	810	3.58	10	4	ND	2	18	1	2	2	79	.23	.10	9	43	.92	153	.11	5	2.98	.02	.10	2	10
28M 32E	1	56	17	87	.2	39	20	968	4.51	12	4	ND	2	21	1	2	2	103	.27	.06	6	48	1.62	131	.13	5	3, 51	.94	.09	2	35
28W 33E	1	71	19	128	.4	23	17	935	3.86	11	4	ND	2	34	1	2	Z	98	. 32	.14	5	26	.72	137	.15	5	3.81	.04	.13	2	10
28N 34E	1	42	12	78	.4	28	15	726	3.77	13	4	ND	2	54	1	3	2	83	.43	.07	7	56	1.35	149	.13	4	3.14	.04	.17	2	5
27N 26E	1	35	14	58	.2	23	13	1048	4.31	12	3	ND	2	28	1	2	2	82	1.06	.04	6	35	1.74	95	.11	5	3.78	.03	.08	2	5
27N 27E	2	54	15	103	.3	38	14	902	3.48	13	3	ND	2	27	1	2	2	76	.73	.06	10	43	. 99	118	.15	4	3.76	.04	.10.	2	5
27N 28E	2	22	18	93	.3	31	12	901	3.41	19	5	ND	3	20	1	3	2	63	.24	.0?	13	45	.81	172	.09	4	3.19	.02	.09	2	5
STD A-1/AU 0.5	1	30	40	180	.3	35	12	1026	2.79	9	2	ND	2	35	1	2	2	58	.59	.09	8	71	.71	278	.08	10	2.05	.02	. 21	2	540

SAMPLE I	Mo ppa	Cu ppz	Pb pps	In pps	Ag pps	Ni ppm	Co ppe	Mn ppe	Fe	As ppa	U PP=	Au ppe	Th pps	Sr ppa	Cd pps	Sb pp=	Bi pp=	y ppa	Ca I	FZ	La ppe	Cr pps	Mg	Ba ppe	Ti I	B ppa	AL	Na Z	ĸ	W ppe	Au 8 ppb
27N 29E	1	24	12	74	.4	22	8	270	2.73	3	2	ND	2	13	1	2	2	47	.12	.05	ę	35	.56	131	.06	2	2.63	.02	. 07	2	5
27N 31E	1	99	12	83	.1	16	14	334	4.25	2	3	ND	2	18	1	2	2	137	.20	.03	3	24	1.36	90	.22	2	3.59	.02	.13	2	5
27N 37E	1	41	14	99	.1	20	13	1322	3.38	6	2	ND	2	48	1	2	2	78	.34	. 06	4	24	.93	151	.11	3	3.16	.02	.13	2	75
27H TTF	1	84	16	120	3	16	19	2004	3.50	i	2	ND	2	112	1	2	2	RR	.64	.08	2	19	.77	777	.11	2	3.46	.04	.18	2	40
27N 34E	i	34	13	Π	.1	34	10	341	2.67	10	2	ND	2	21	i	2	2	45	.15	.06	10	40	.72	117	.05	2	1.92	.02	.09	2	5
26N 26E	1	26	15	103	.1	20	9	937	3.26	30	2	ND	2	26	1	2	2	52	.36	.09	7	32	.92	138	.06	2	3.28	.02	.07	2	5
26N 27E	1	42	15	125	.2	24	20	3186	3.29	2	2	ND	2	22	1	2	2	70	.18	.12	5	34	.71	262	.08	3	2.50	.03	. 08	2	5
26M 28E	1	40	16	82	.3	26	12	956	3.32	5	2	ND	2	25	1	2	2	60	.27	.07	9	38	.83	168	.07	2	3.21	.02	.08	2	370
36N 29E	2	28	16	86	.1	23	10	700	3.26	10	2	ND	2	15	1	2	2	60	.18	.07	7	38	.70	164	.08	2	3.20	.02	.06	2	5
26N 31E	2	23	15	128	.2	32	11	2039	3.24	6	2	ND	2	21	2	2	2	57	.41	.10	8	45	.54	191	.05	2	3.14	.01	.06	2	5
76N 32E	1	28	15	99	.1	21	12	1190	3.20	8	2	ND	2	27	1	2	2	66	.29	.07	5	31	. 82	148	. 10	3	3.36	.03	. 07	2	10
26N TTE	1	41	11	77	.7	77	11	560	3.17	2	2	ND	2	32	1	2	2	67	.17	. 06	6	31	.86	111	.09	2	2.95	.03	.11	2	10
TAN TAF	i	31	14	77	1	20	11	523	3.12	7	2	ND	2	31	1	-	-	60	.78	.10	4	31	.73	140	.07	2	3.16	.02	.07	7	70
75N 745	- 1	27	15	107	.,	19	9	1097	7 79	Å	2	ND	2	41	i	5	5	41	. 76	.12	6	78	.93	171	.05	3	4.09	.07	.06	2	5
25N 27E	i	23	15	75	.3	20	9	720	2.70	8	2	ND	2	17	1	3	2	52	.20	.05	6	31	. 69	128	.08	2	2.73	.02	.07	2	10
25N 28E	2	28	17	118	.3	26	10	1049	3.13	16	2	ND	2	18	1	2	2	54	.90	.07	9	48	.77	134	.07	2	3.45	.02	.06	2	10
25N 29E	1	46	14	79	.2	26	15	627	3.80	6	3	ND	2	25	1	2	2	83	.21	.09	5	45	1.17	136	.11	2	3.73	.03	.08	2	5
75W 31E	1	73	12	95	.1	25	15	653	3.71	6	2	ND	2	18	1	2	2	90	.77	.09	6	37	1.06	146	.12	2	3.38	.02	.09	2	10
25H 32E	i	40	14	109		25	15	639	3.42	10	2	ND	2	25	î	2	2	82	.74	.07	4	39	1.21	112	. 15	2	3. 18	.02	.08	2	10
25N 33E	i	63	14	102	.3	25	18	795	3.46	7	2	ND	2	37	i	3	2	84	.24	.08	4	43	1.11	124	.14	2	3.19	.03	.11	2	25
25N 34E	1	23	13	75	.5	21	10	352	2.77	6	2	ND	2	29	1	2	2	57	.31	.11	5	29	. 66	145	.09	5	3.35	.03	.11	2	10
24N 26E	1	111	13	117	. 6	23	10	1388	3.46	22	2	ND	2	58	2	2	2	53	1.75	.05	8	23	.99	71	.10	3	4.24	.09	.07	Z	10
24N 27E	2	32	13	82	.4	21	11	359	3.02	11	2	ND	2	17	1	2	2	63	.20	.06	5	28	.58	87	.10	2	2.95	.02	.06	2	15
24N 28E	1	38	13	90	.4	25	11	663	2.96	8	3	ND	2	17	1	2	2	60	. 18	.06	7	35	.70	129	.09	Z	3.03	.02	.07	2	10
24N 29E	1	34	14	109	.2	24	17	1264	3.58	8	2	ND	2	24	1	2	2	92	.27	.11	4	48	1.25	159	.14	2	3.67	.03	.09	2	15
24N 31E	1	81	23	85	.5	31	10	647	2.82	10	2	ND	2	26	1	2	2	50	.75	.05	7	29	.52	79	.09	2	3.64	.03	.07	2	15
24N 32E	1	34	15	83	.2	23	11	672	2.74	8	3	ND	2	22	1	3	2	54	.29	.07	7	32	.70	102	.08	2	2.72	.02	.06	2	15
24N 33E	1	32	22	99	.3	19	11	902	3.03	2	2	ND	2	16	1	2	2	61	. 1ó	.10	6	28	.58	144	.09	2	2.79	.02	.09	2	10
24N 34E	1	144	16	132	.5	21	14	1463	3.77	8	2	ND	2	33	2	2	2	100	. 56	.05	6	24	1.02	122	.13	2	3.13	.03	.14	2	15
23N 26E	1	32	11	86	.2	16	11	455	3.65	7	2	ND	2	21	1	2	2	73	.15	.05	5	28	.76	152	.07	2	3.38	.02	.08	2	5
23N 27E	2	36	14	73	.3	21	9	359	2.98	5	2	ND	2	21	1	.2	2	60	.41	.04	7	32	. 50	102	.09	2	2.92	.03	.08	2	5
23N 28E	1	33	11	90	.3	20	10	587	3.01	4	3	ND	2	19	1	2	2	63	.23	.09	7	30	.71	137	. 09	2	2.80	.07	.12	7	10
23N 29E	1	108	14	110	1.4	21	6	527	2.45	11	7	ND	2	32	2	2	2	54	. 88	.09	14	25	.46	109	.09	2	3.98	.04	.11	2	5
23N 31E	1	54	10	111		10	11	739	3.48	1	4	ND	2	18	1	2	2	81	47	.06	8	78	.83	117	.15	2	3.76	.03	.08	2	5
23N 32E	î	73	14	161	.1	19	17	679	4.36	6	6	ND	2	21	i	2	2	157	.29	.04	3	23	1.27	177	.28	2	3.63	.02	.26	2	5
23N 33E	1	29	15	103	.2	19	9	357	3.53	4	2	ND	2	39	1	2	2	71	.16	.08	5	31	.77	140	.13	2	3.30	.02	.07	2	5
STD A-1/AU 0.5	1	31	40	184	.3	35	13	1017	2.82	10	2	ND	2	36	1	2	2	60	.60	.10	7	71	.72	284	.08	9	2.07	.07	.20	2	530

SAMPLE I	Mo ppm	Cu ppa	Pb pp=	In ppn	Ag pps	Ni ppe	Co ppe	Min ppe	Fe Z	As ppm	. U ppm	Au ppe	Th pp=	Sr ppe	Cd pp=	Sb pps	Bi pp=	V ppa	Ca I	۶ ۲	La pp=	Cr ppe	Ng Z	Ba ppa	Ti 1	B ppm	Al	Na I	ĸ	W pps	Aut ppb	
	7	70	17	171	.1	76	16	1017	4.40	13	7	ND	7	70	1	7	2	100	.22	.08	5	28	.92	162	.11	2	2.44	.02	.17	2	5	
201 312	•	77	10	70		21	15	775	4 45	11	1	NB	2	21		7	2	125	22	04	4	29	1.71	95	19	2	ET T	.03	17	2	5	
228 20E	1		10	00	.4	21	13	710	1.13	11	-	10	-	10		ĩ	-	07	27	07		21	41	74	15		2 50	07		-	-	
22N 2/E	4	20	12	82	-4	10	14	307	9.41	10	4	NU	1	10	- 31	- 2	-	75	.20	.05	- 2	20	.01	107		-	2.00	.00	.00	-	-	
22N 28E	1	33	11	90	• • •	14	4	409	3.31	1	2	ND	1	13	1	2	4	12	.15	.08	2	23	. 36	103	.11	4	2.69	.02	.08	4	3	
22N 29E	1	29	10	88	.2	17	•	513	3.25	3	2	ND	2	14	1	2	2	74	.13	.10	2	29	./4	103	.09	2	2.11	.03	.08	2	2	
22N 31E	1	34	8	85	.6	29	12	405	3.53	8	2	ND	2	15	1	2	2	73	.17	.13	4	45	.70	112	.11	2	3.04	.02	.09	2	5	
22W 32E	1	51	14	96	. 6	271	13	976	3.26	17	2	ND	2	28	1	2	2	64	.48	.07	7	42	. 68	97	. 14	3	3.81	.05	.09	2	. 5	
77N TTE	1	14	12	46	4	14	5	280	7 77	7	2	ND	2	15	1	2	2	57	.17	.04	5	23	.34	86	.11	2	2.73	.03	.05	2	5	
TTH JJL		70		75		10	10	100	7 04		-	NTL.	2	24	1.25	-	-	40	14	00	5	20	54	105	00	2	2 92	07	07	2	10	
12N 34E	1	50	12	:2		17	10	400	3.04	0	4	NU	4	21	1	-	-	00	.10	.00		20	1 05	103		-	7 30	.03	.07	-	10	
21N 26E	4	51	1/	79	.3	104	14	1104	5.22	16		ND	2	41	1	2	4	67	.12	.07	10	74	1.03	117	.11	1	3.78	.03	.08	4	3	
21N 27E	2	20	12	51	.3	20	7	538	2.63	10	2	ND	2	15	1	2	2	51	.17	.07	4	30	. 47	114	.10	4	2.84	.02	.05	2	5	
21N 28E	1	27	11	83	.4	24	11	672	3.24	8	2	ND	2	18	1	2	2	66	.20	.07	4	45	.80	118	.10	2	3.25	.02	.09	2	5	
21N 200	1	49	15	84		108	11	7814	7.43	74	2	ND	2	88	7	7	2	47	1.21	.07	10	39	.52	158	.09	4	3.69	.03	.07	2	5	
218 20.355		24	17	00		77	11	1007	7.11	7	7	MD	2	77	1	2	2	67	22	07	5	R	.87	166	.09	2	2.78	.03	.09	2	5	
218 277236	1	24	13	100		20		1007	7.00		-	10		22	:	-	-	70		05	-	17	20	107	10	-	2 11	02		-	10	
21N 29+50E	-1	13	7	108	.1	20	12	127/	3.00	8	4	NU	2	21	1	4	-	14		.05		31	. 07	117	.10	•	2. 51			-	19	
21N 29+75E	1	76	12	99	.1	95	31	879	5.62	8	3	ND	2	42	1	4	2	163	.52	.08	4	253	2.91	450	.16	• 2	4.02	.02	.52	2	5	
21N 30+25E	3	28	14	65	.4	62	15	822	3.34	38	2	ND	2	20	1	2	2	54	.20	.10	8	58	. 41	141	.09	3	3.46	.03	. 07	2	5	
71N 30+50E	7	31	9	99	.3	53	16	1641	3.95	13	3	D	2	21	1	2	2	90	.23	.11	4	73	.77	240	.07	2	2.55	.02	.10	2	5	
TIN 30+75F		58	14	83		101	74	778	4.85	17	2	ND	2	25	1	2	2	108	.24	.06	6	244	1.61	243	.12	2	4.03	.02	.14	2	5	
DIN TIE	-	74	15	01		57	17	527	7 55	18	-	ND	5	16		2		75	77	06	5	61	94	115	11	2	3.31	.02	.09	7	5	
214 316	-	30	13			32	15	921	3.33	10	-	ne		10																-		
21N 32E	1	26	11	69	.4	23	9	199	3.34	18	2	ND	2	11	1	2	2	59	.10	.05	5	36	. 47	115	.09	2	3.61	.02	.05	2	10	
21N 33E	-1	32	13	72	.2	16	5	331	3.40	7	3	ND	2	11	1	2	2	73	.11	.15	5	25	.84	220	.16	2	3.01	.04	.10	2	5	
21N 34E	2	31		99	.2	22	11	317	3.57	13	3	ND	2	18	1	2	2	73	.22	.10	6	33	. 66	118	.11	2	3.33	.02	.08	2	5	
20+758 295	1	76	12	95	.3	33	17	856	3.77	7	2	ND	2	20	1	2	2	67	.24	.12	5	67	.94	186	.10	2	3.16	.03	.10	2	5	
204754 204255		27		25		23	11	947	2 91	17	2	ND	7	23	÷	2	2	59	.76	.09	5	40	.79	1.60	.08	3	7.45	.02	.12	2	5	
204734 274236		25		03	•*	23		142	2.01	12	-	nu		23		•	•	51	.20					100								
20+75N 29+50E	1	30	9	87	.2	26	13	552	3.27	2	2	ND	2	21	1	2	2	76	.24	.07	6	40	.93	155	.11	2	2.65	.02	.14	2	5	
20+75N 29+75E	1	48	11	100	.1	BO	21	439	4.49	11	2	ND	2	30	1	2	2	68	. 39	.08	5	186	1.69	198	.10	2	3.41	.02	.13	2	5	
20+75N 30+25E	1	27	15	134	. 6	41	16	797	3.48	9	2	ND	2	25	1	4	2	69	.25	.19	2	48	.71	165	.09	2	2.91	.02	.09	2	5	
10+75N 10+50F		18	12	87	4	55	10	661	7 79	77	3	ND	7	17	1	7	2	45	.21	.14	4	40	.41	131	.09	2	3.25	.03	.07	2	5	
20475N 704755		71	12	04		77	10	580	4 07	10	2	ND		21		2	2	91	20	.05	7	114	1.05	148	12	2	1.49	.03	.09	7	5	
20+738 30+736	•	20	12	74		15	10	379	4.0/	10	2	NU	4	21		4	4	n	. 20	.05		***	1.05	144		•	2. 11			•		
20+75N 31E	1	70	14	86	.6	69	11	1484	2.57	12	2	ND	2	81	2	2	2	52	1.27	.06	9	42	.54	153	.08	4	3.59	.03	. 07	2	5	
20+50N 29E	1	35	8	94	.2	36	15	943	3.31	10	2	ND	2	24	1	3	2	71	.33	.07	6	73	1.09	187	.09	3	2.82	.02	.12	2	5	
20+50N 29+25E	1	34	11	89	.1	34	14	1220	3.22	9	2	ND	2	28	1	3	2	70	.36	.07	6	70	1.11	181	.09	2	2.73	.02	. 14	2	5	
20+50H 29+50F		54	17	113	1	RR	IR	1042	4.09	48	2	ND	7	21	1	2	2	72	.29	.06	7	55	. 72	137	.08	3	2.88	.02	.13	2	10	
COLEAN 20. TEL	-	50	74	140		17	20	011	4 70	70	-	ND	-	10		-	2	77	18	08	5	57	70	117	OR	1	3.01	.07	.09	2	5	
10420W 244/2F	3	24	21	140		0/	22	716	9.27	28	1	RO	2	10	1	2	-	13	. 10	.00	5	37	•17	102	.00				• • •	•		
20+50N 30+25E	6	62	24	188	2.5	159	20	1156	3.99	115	2	ND	2	19	1	2	2	70	.26	.07	5	61	.81	131	.06	2	2.45	.02	.10	2	5	
STD A-1/AU 0.5	1	30	38	183	.3	36	13	1014	2.81	10	2	ND	2	36	1	2	2	50	.60	.10	8	74	.71	281	.08	10	2.06	.02	.21	2	210	

SAMPLE I	No ppe	Cu ppe	Pb ppa	In pps	Ag pp.	Ki ppa	Co pps	Mn ppe	Fe 1	As pps	U ppe	Au ppn	Th ppe	Sr ppa	Cd pp=	50 pp=	Bi pp=	V ppe	Ca 1	PI	La ppa	Cr pps	Ng	Ba pps	Ti 1	B ppe	Al I	Na 1	K 1	¥ pps	Au3 ppb
20+50N 30+50E	3	30	21	176	1.1	64	13	704	3.09	17	2	ND	2	13	1	2	2	52	.14	.15	3	40	. 48	107	.09	2	2.99	.02	.07	2	270
70+50N 30+75E	2	22	7	90	.2	25	10	576	3.11	8	2	ND	2	17	1	2	7	71	.20	.08	3	38	.71	94	.09	2	2.63	.03	.09	2	10
70+50H 31E	ĩ	23	10	99	.3	41	10	733	2.77	12	2	ND	2	55	1	2	2	55	. 68	.08	7	12	.62	112	.11	3	3.78	.03	.07	2	5
20+25W 29F	1	77	12	77	.1	51	16	776	3.62	10	2	ND	2	28	i.	2	2	87	.43	.07		88	1.40	153	.09	3	2.63	.03	.21	2	5
20+25W 29+25E	2	60	14	119	.1	316	27	706	4.11	17	3	ND	ž	20	i	2	2	75	.29	.06	i	119	1.60	127	.08	2	3.39	.02	.10	2	ŝ
20+25M 29+50E	1	39	5	82	.1	95	16	518	3.16	4	3	ND	2	15	1	2	2	64	.23	.05		58	1.00	123	.09	2	3.09	.02	.11	2	5
20+254 29+75E	2	22	5	125	.1	178	17	781	3.37	7	3	ND	2	14	1	2	2	66	.29	.07	3	75	1.00	107	.09	2	2.90	.02	.06	2	5
20+25N 30+25E	2	24	17	134	.5	65	13	861	2.79	53	2	ND	2	16	1	2	2	54	.22	.07	3	42	.53	128	.0å	2	2.18	.02	.08	2	5
20+25N 30+50E	2	28	18	204	.3	143	14	673	3.32	110	4	ND	2	14	1	2	2	60	.19	.09	3	60	.70	167	.06	2	2.69	.02	.06	2	5
20+25H 30+75E	2	24	10	90	.5	54	12	340	2.91	28	2	ND	2	16	1	2	2	57	.17	.07	4	50	.58	105	.10	2	3.46	.03	.06	2	5
20+25H 31E	2	25	13	128	.2	31	11	265	3.25	17	2	ND	2	30	1	2	2	77	.33	.08	4	37	.78	106	.11	2	3.17	.03	.06	2	5
20W 26E	1	13	8	54	-3	17	8	281	2.44	10	2	ND	2	16	1	2	2	45	.17	.10	4	29	. 41	66	-08	2	2.83	.02	.04	2	5
20N 27E	2	25	8	100	.1	20	12	1048	3.02	4	2	NO	2	17	1	2	2	68	-18	.07	4	48	.96	220	-10	2	2.76	-02	.09	2	5
20M 28E	1	34	11	101	.2	45	15	1300	3.21	8	2	ND	2	24	1	2	2	74	.32	.09	4	85	1.13	225	.05	4	2.74	.02	.13	2	5
20N 29E -	2	44		97	.7	129	16	618	3.57	5	2	NO	2	20	1	2	2	68	.28	.06		79	1.09	119	.10	2	3.36	.02	.10	2	5
20# 29+255	2	30	8	78	.3	85	13	577	2.79	12	2	ND	2	16	1	2	2	56	.20	.06		47	.73	178	.07	3	2.62	.03	.03	2	5
29N 29+50E	1	37	8	102	.1	136	18	808	3.35	6	2	ND	2	23	1	2	2	65	.41	.09	4	79	1.03	145	.08	3	2.92	.02	.10	2	5
208 29+75E	3	39	12	172	.1	159	20	651	3.48	12	2	ND	2	19	1	2	2	66	. 38	.07	4	71	. 96	138	. 10	3	3.26	.02	.09	2	5
20N 30+25E	3	59	13	119	.3	43	16	728	3.87	21	2	ND.	2	18	1	2	2	76	.16	.07	6	47	.92	147	.06	2	2.78	.02	.16	2	20
20H 30+50E	2	22	19	142	.5	48	17	1048	3.67	16	4	ND	2	27	2	2	2	76	.28	.08	6	66	.89	94	.11	2	3.28	.02	.08	2	5
20N 30+75E	2	39	18	115	1.3	41	12	520	3.21	16	2	N	2	18	1	2	2	62	.14	.07	7	40	.61	172	.11	2	3.79	.03	.08	2	5
20N 31E	4	56	14	125	2.3	63	12	969	3.31	12	2	ND	2	57	2	2	2	69	.60	.05	9	42	.78	132	.11	2	3.69	.03	.05	2	5
20N 32E	1	15		84	.5	15	8	395	2.59	10	2	ND	2	13	1	2	2	52	.14	.13	2	22	.38	100	.11	2	2.91	.03	.06	2	5
20W 33E	4	85	15	112	1.0	89	15	1514	4.46	28	2	ND	2	35	2	2	2	84	.67	.05	16	67	.78	265	.06	2	4.02	.02	.10	2	5
20M 34E	1	32	6	74	-1	18	7	268	3.46	14	3	ND	2	10	1	2	2	72	.09	.18	5	27	.83	190	.16	2	3.21	.03	.08	2	5
19+75N 29E	1	32	9	86	.2	58	15	584	3.24	7	2	ND	2	22	1	2	2	75	.35	.05	5	113	1.35	170	.10	3	2.98	.05	.14	2	5
19+75K 29+25E	2	24	. 8	103	.2	127	16	577	2.87	10	2	ND	2	17	1	2	2	58	.38	.07	2	82	.96	136	.08	2	2.47	.01	.09	2	5
19+75# 29+50E	1	36	5	90	.3	100	15	373	3.17	10	2	ND	2	18	1	2	2	65	.24	.09	4	73	1.00	162	.09	2	3.15	.02	.08	2	5
19+75H 29+75E	2	39	6	83	.1	28	13	731	3.50	14	2	ND	2	18	1	2	2	87	.24	.07	3	38	1.04	163	.11	2	3.00	.03	.14	2	5
19+75# 30+25E	2	32	7	83	.2	38	12	445	3.32	8	4	ND	2	25	1	2	2	73	.36	.06	8	43	.78	145	.13	2	4.23	.03	.07	2	5
19+75H 30+50E	2	45	19	100	.2	38	16	483	4.20	19	2	ND	2	46	1	2	2	97	.65	.06	5	52	1.12	63	.12	3	3.63	.02	.07	2	5
19+75H 30+75E	2	49	21	85	.3	38	16	394	4.17	19	3	ND	2	47	1	2	2	98	.63	.05	6	52	1.17	91	.12	3	3.66	.03	.07	2	5
19+75N 31E	3	46	26	106	.5	54	16	650	3.60	22	3	ND	2	27	1	2	2	80	.28	.07	6	52	1.02	133	.10	2	7.94	.02	.15	2	5
19+50H 29E	2	32	11	89	.1	80	15	594	3.40	7	2	ND	2	18	1	2	2	74	-26	.08	4	96	1.22	149	.08	2	3.20	.02	.10	2	5
19+50W 29+25E	1	34	13	109	.1	109	17	1211	3.24	8	2	ND	2	27	1	2	2	75	.43	.04	5	111	1.25	236	.10	2	2.96	.02	.10	2	5
10.500 20.505			10	143		130	10	534		24		NP.							20									-			
STD 4-1/4/ 4 5	:	74	10	102	.4	128	17	1077	2.82	10	-	ND	-	10	1	-	-	6/	-20	-14	;	73	1.20	774	.00	3	2.04	.02	-11	-	510
10 H 11 H V.J			- 27			-943		1041	4.04	14		~		33				90				14		4/9				- 94			280

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2010/20

in taking the

SAMPLE I	Na pp=	Cu ppe	Pb pp=	Za ppe	Ag ppa	Ni ppa	Co ppe	in ppe	Fe 1	As ppe	U pp=	Au ppa	Th pp=	Sr ppe	Cd pp=	Sb pp=	Bi pp.	V pps	4	F I	La ppe	Cr pp=	Ng	Ba pps	Ti T	8 998	Al I	Na Z	K I	¥ ppe	Aut ppb
19+50N 29+75E 19+50N 30+25E 19+50N 30+50E 19+50N 30+75E	1 1 2	38 27 29 42	10 10 11	88 91 91 69	.3 .1 .2	26 21 21 23	13 12 11	501 1144 401 541	3.57 3.23 3.48 7.81	10 10 8 17	3232	ND N	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	25 23 20	1 1 1	2222	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	77 72 77 54	.37	.07	5 5 5 12	34 33 33	.93 .76 .75 .58	168 148 143 85	-12 -12 -13		3.56 3.18 3.54 4.48	.03 .03	.13 .09 .09	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5 5 5 5 5
19+50N 31E	3	50	11	98	.1	32	15	366	4.15	16	ž	ND	2	39	i	ž	2	103	.37	.03	10	53	1.33	112	.15	4	3.33	.03	.10	ž	5
19N 26E 19N 27E 19N 28E 19N 28E 19N 25E	3 1 1 2 1	25 34 31 41	10 13 13 13	133 100 92 113	.4 .1 .1 .2 .	65 39 79 62	14 12 14 15	904 369 422 495	3.19 3.50 3.36 3.58	19 9 14 15		22225	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	21 18 20 20	1 1 1 1	22222	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	57 72 69 79	.29 .21 .34 .28	.09 .08 .05 .07	67470	53 37 51 82	.59 1.00 .96 1.15	177 139 161 157	.09 .13 .14 .14		J.19 J.87 4.00 J.63	.03	.09	2	10 5 5 5 5
178 316				114		**		007		10	•	nu		n	•	*		er	1.31	.va			. 10	1.51		•	3.14			•	
19N 32E 19N 33E 19N 34E 18N 26E 18N 27E	1 1 3 3	46 42 55 31 42	20 15 15 14 16	123 115 105 132 138	1.0 .4 .1 .4 .2	46 35 31 59 64	15 14 18 16 17	832 505 906 881 1068	4.24 3.87 7.59 3.61 3.99	16 14 23 21 17	35733	55855	22422	30 27 29 24 49	1 1 1 1	22222	222222	86 93 180 72 80	.68 .37 .93 .32 .45	.05 .12 .36 .09	9 5 15 6	50 41 40 56 45	.77 1.05 2.33 .72 .91	195 179 153 161 178	.11 .14 .20 .11		3.75 3.31 5.45 3.41 3.27	.02 .02 .01 .03 .02	.14 .14 .31 .07 .15	22272	2225
18N 28E 18N 29E 18N 31E 18N 32E 18N 33E	2 4 1 1 1	37 31 51 27 50	10 12 12 16	96 114 89 124 131	.1 .2 .1 .5 .3	37 70 50 27 60	15 11 15 12 20	645 740 287 1224 1132	2.88 2.22 2.50 2.20 2.20	13 11 10 12 22	2 2 5 2 5	5 5 5 5 5 5	22223	26 18 23 18 38	1 1 1 1	27272	222222	80 71 89 69 94	.26 .20 .28 .19 .35	.06 .06 .05 .19 .11	4 5 6 5 8	51 38 61 43	1.11 .75 1.10 .71 .99	151 148 163 185 148	.14 .14 .14 .11 .15	4 5 3 4	3.49 3.82 3.66 3.30 3.53	.03 .03 .02 .03 .02	.11 .07 .11 .10 .11	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
18N 34E 17N 28E 17N 29E 17N 31E 17N 31E	1 19 1	29 31 11 20 28	14 13 10 14 14	106 80 14 79	.1 .1 .2 .5 .4	80 24 12 24 35	14 9 1 13	778 214 56 307 1203	5.03 3.81 .34 2.69 3.28	44 15 2 7 10	22822	85555	2 2 2 2 2 2 2	27 25 102 19 24	1 1 1 1 1 1	22222	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	67 83 25 58 75	.31 .30 5.24 .27 .38	.06 .03 .07 .09 .12	8 2 5 5	46 35 4 29 43	.76 .68 .11 .60 .81	198 97 23 104 197	.13 .13 .01 .12 .12	431144	2.88 3.25 .22 2.93 3.38	.03 .02 .01 .03 .03	.10 .07 .02 .09 .10	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
17N 33E 17N 34E 16M 28E 16N 29E 16N 31E	1 1 15 1	51 79 22 80 42	12 21 10 7 13	102 137 60 23 153	.1	27 35 24 71 20	14 23 10 7 13	1188 1595 329 1850 2583	2.93 3.73 3.33 1.67 2.97	16 15 14 6	22372	10 10 10 10 10 10 10 10 10 10 10 10 10 1	22222	44 51 21 89 33	1	222222	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	63 79 73 45 64	.29 .33 .26 2.85 .27	.13 .14 .09 .11 .14	5 4 7 5	29 42 35 16 23	.61 .81 .68 .33 .64	153 201 95 132 195	.11 .10 .13 .03 .11	*5*3*	2.98 3.23 3.61 2.05 3.22	.03 .02 .03 .02 .03	.10 .15 .09 .05 .10	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5 70 5 5
16N 32E 16N 33E 16N 34E 15N 28E 15N 29E	1 1 1 2	58 41 41 41 25	18 12 10 9	124 128 102 70 74	.1 .1 .1 .1	29 42 41 35 25	14 14 15 13	1107 732 430 427 401	3.80 3.38 3.63 3.71 3.67	9 15 13 18 20	32233	88888	222222	41 29 25 35 21	1 1 1 1		122222	82 71 81 91 84	.41 .33 .24 .41 .24	.12 .08 .11 .05 .06	75564	36 34 45 43 35	.96 .65 .95 1.20 .68	183 123 164 144 107	.13 .13 .13 .13 .13		4.24 1.39 3.62 1.08 2.87	.02 .03 .03 .02 .03	.16 .11 .13 .15 .07	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	55555
STD A-1/AU 0.5	1	30	40	183	.3	36	13	1012	2.80	9	2	ND	2	35	1	2	2	60	. 61	- 10	8	71	.71	276	.08	9	2.0?	.02	.21	2	540

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THE REAL OF LEVEL 1

SAMPLE 1	No 204	Du ppe	Pb ppa	Zn pps	Aq pps	Ri ppe	Co ppe	Ppe	Fe	As ppe	U ppa	Au 998	Th pps	Sr ppa	Cd pps	50 ppn	Bi ppm	pp=	1	PI	La ppe	Cr pps	Nq I	Ba ppa	71	B ppe	Al I	1	z	Ppa	Auli
15W 31E	1	78	11	100	.3	56	17	842	4.23	9	2	80	2	37	1	2	2	94	.28	.07	3	51	.79	121	.09	4	3.03	.02	.07	2	5
15N 32E	i	42	8	75	.3	43	12	344	2.99	8	4	ND	2	24	1	2	2	63	.19	.07	3	30	.66	104	.10	4	3.30	.02	.08	2	5
15N 33E	1	22	9	90	.2	24	11	934	2.86	7	2	ND	2	15	1	2	2	65	.18	.09	4	30	.71	126	.09	4	2.68	.02	.09	2	5
15N 34E	1	26	9	76	.2	30	10	237	2.78	9	6	ND	2	20	1	2	7	59	.22	.06	3	30	.58	120	.11	4	3.48	.03	.09	2	5
14K 28E	1	19	12	61	.3	16	6	345	2.58	8	4	ND	2	14	1	2	2	59	.19	.11	3	22	.37	66	.11	2	3.36	.02	.05	2	5
14H 29E	1	15	7	63	.4	17	7	599	2.27	5	2	ND	2	13	1	2	2	47	.14	.05	4	23	.36	119	.09	2	2.40	.02	.05	2	5
14N 31E	1	20	9	84	.2	26	12	441	2.86	11	2	ND	2	24	1	2	2	64	.29	.09	4	30	.71	149	.09	4	2.86	.02	.07	2	15
14N 32E	1	38	8	63	.4	26	13	349	3.34	13	2	ND	2	29	1	2	2	81	.33	.04	5	28	1.07	101	.10	4	2,65	-02	-13	2	5
14M 33E	1	29	10	82	.2	24	13	348	3.41	13	2	ND	2	25	1	2	2	78	.25	. 07	4	29	.84	85	.10	4	3.10	.02	.10	2	5
14N 34E	1	43	11	73	.8	38	10	378	2.93	10	2	ND	2	30	1	2	2	55	.78	.06	9	42	.64	67	.13	•	3.74	-03	-07	2	32
13N 28E	2	26	8	61	.3	27	11	254	3.28	9	3	MD	2	22	1	2	2	85	.24	.03	5	39	.90	102	.12	3	2.47	.02	.10	2	15
13W 29E	1	23	9	98	.3	22	9	574	3.32	10	2	ND	2	29	1	2	2	78	.23	*0B		30	+92	114	.11	1	3.17	.02	.08	2	10
13M 31E	1	34	2	60	.1	22	10	429	2.66	n	3	ND	2	19	1	2	2	61	. 16	.06	4	34	.69	122	.10	3	2.84	.07	.11		2
13W 32E	2	38	9	60	-	61	15	284	3.56	26	3	ND	Z	19	- 1	Z	2	84	.18	.07	3	45	.29	24	.10	3	2.01	.02	.9/	-	
13M 33E	1	26	12	112		48	12	410	2.42	31	•	MD	2	22	1	2	-	63	-10	.12	,	28	.21	152	.04	,	3.09	-02	.00	-	10
13H 34E	1	22	9	73	.5	26	9	597	2.52	12	2	ND	2	23	1	2	2	55	.16	.07	6	28	.35	98	- 10	3	3.03	.02	.05	2	5
12W 28E	1	ш		62	.5	17	6	209	2.17	5	2	ND	2	13	1	2	2		-13	-11	3	20	.31	83	.12	2	3.19	.03	.90	2	3
12N 29E	1	21	11	87	.1	31	10	260	2.66	20	1	10	7	28	1	7	2	20		.07	3	20	. 48	112	.09		3.81	.02	.0/	-	
12M 31E	2	16	10	/1	1	18	4	4/5	2.20		-	ND	-	13	1	-	-	10	-14	-11	2		. 30	70	. 10	2	3.80	.03	.00	:	2
124 326	•	24	15	124	.,	82	15	1366	4.20	22	•		-	21		1	1	80		.08	٥	•1	.01	155	.01		3.11	.02	.00	-	
12N 33E	1	34	8	82	.4	36	11	438	3.17	12	5	ND	2	23	1	2	2	70	.33	.07	5	39	.64	140	.09	2	3.71	.02	.09	2	5
12N 34E	1	37	7	86	.7	30	11	426	3.25	14	2	ND	2	18	1	2	2	70	.20	.05	4	36	.75	168	.11	2	3.36	.02	.08		5
11N 28E	1	16	1	57	.4	20	8	288	2.37	5	2	ND	2	19	- 1	2	2	53	.23	.0?	4	32	.52	91	*08	2	2.38	.02	.07	2	5
11N 29E	1	28	13	78	.2	31	9	657	2.80	10	2	ND	2	12	- 1	- 2	2	60	.13	.10	7	46	-68	140	.09	2	2.24	.02	.10	- 7	5
11N 31E	1	14	10	82	.2	31	9	443	2.49	8	2	ND	2	18	1	2	2	54	.22	.10	4	78	.49	111	.10	2	2.91	.02	.07	2	5
11N 32E	2	38	8	58	.2	44	11	296	3.58	72	2	ND	2	21	1	2	2	75	.25	.08	5	46	.85	75	.07	2	2.65	.01	.08	2	5
11M 33E	1	12	10	64	.1	15	7	360	2.24	9	2	ND	2	15	1	2	z	45	.17	.17	3	25	.30	116	.06	2	2.65	.02	-05	2	5
IIN JAE	- 1	19	6	60	.3	18	8	191	2.86	9	3	ND	2	12	1	2	2	59	-12	.13		31	- 51	92	.10	2	3. 37	.03	.06	7	2
ION ZEE	1	24	. 1	90	2	22	11	326	2.82	11		ND	2	17	1	2	2	60	.17	.09	1	22	- 62	115	.10	3	3.40	.07	80,	2	3
ION 29E	1	3	11	98	.3	34	10	204	2.72	1	•	ND	2	16	1	2	2	61	.16	.06		36	.70	89	.10	3	3.19	.02	.09	2	,
ION SIE	3	40		72	.3	36	10	682	3.13	- 16	1	ND	2	32	1	2	2	69	.38	.04	8	45	.85	203	.09	3	3.32	.03	.11	2	5
TON STE	2	28	12	141	.9	22	17	435	3,00	11	2	ND	1	10	2	1	1	64	-14	-14		31	+22	106	.10	1	3.79	+02	.07		2
300 332	1	16		60	.4	19		201	2.58		2	ND	-	15	1	2	2	63	-15	.11	3	34	.61	00	.08	3	1.66	.02	.08	-	3
STR A-L/ML A S		10	Te	194	1	29	17	1077	2.01	10	3	ND ND	-	20		-		13	. 40	.05	2	43	. 70	278	.07	5	2.01	102	.07	5	510
212 HTL/HU U.3		- 30	20	105				10.37		10				- 36				0.0						2.76	- UG		2.198	- 112			410

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execution is special amount

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SAMPLE #	No ppe	Cu ppa	Pb ppm	Zn pps	Ag ppe	Ni ppm	Co ppe	Min pp#	Fe %	As pp=	U ppø	Au pps	Th ppa	Sr ppa	Cd pp=	Sb pp =	Bi ppm	V pp=	Ca I	PI	La ppe	Cr ppm	Ng Z	Ba pps	Ti Z	B ppa	Al Z	Na Z	K Z	N pps	Au t ppb
9N 28E 9N 29E 9N 31E	1 1 1	43 22 54	4 8 7	138 86 260	.1 .4 .5	81 35 42	13 8 21	442 408 2745	3.84 2.36 3.38	19 7 15	2 2 2	ND ND ND	2 2 2 2	30 12 35	1 1 4	2 2 2 2	2 2 2 2	52 46 76	.33 .14 .37	.09 .08 .16	344	66 28 34	1.21 .41 .44	116 172 323	.07 .11 .10	323	2.91 3.10 1.94	.02 .03 .03	.09 .08 .10	2 2 2 2 2	5 5 5
9N 32E 9N 33E	1	30 20	4	62 127	.1	26 23	10 10	416 1307	2.68	87	2 2	ND ND	2 2	16	1 2	2	2 2	61 55	.18	.11	4	30 27	.56	117	.08	2	1,95	.03	.07	2 2	25
9N 34E	1	16	8	116	.•	28	8	337	2.35	4	2	ND	2	24	2	2	2	51	.28	.09	3	23	. 32	84	.08	2	2.26	.03	.06	2	5
BN ZBE	1	17	3	22		23	1	170	2.21	0	2	ND	2	10	-	2	2	94	.10	.07	-	20		75	.00	2	1 45	.02	.07	2	5
DN TIE	- 1	11		12		15	4	475	2 00	1	2	ND	2	13	-	5	2	10	17	10	1	21	.30	99	.07	2	1.97	.02	.08	5	5
BN 32E	i	16	7	58	.4	22	7	201	2.69	10	2	ND	2	11	i	3	2	54	.15	.10	4	30	.40	73	. 07	3	2.72	.02	.08	2	ŝ
BN JJE	2	47	10	70	.5	33	11	1080	3.03	6	2	ND	2	25	1	2	2	64	.35	.04	11	44	.86	126	.08	3	2.44	.03	.13	2	5
BN 34E	1	8	9	59	.3	10	5	533	1.87	3	2	ND	2	10	1	2	2	33	.15	.13		17	.13	III	.09	3	2.59	.02	.05	2	2
7N 28E	1	16	10	65		17	6	1250	2.52	12	2	ND	4	23	1	2	2	40	.15	.11		14	.41	174	.10	7	3.38	.02	.07	2	10
78 275	1	14	8	50	1.1	17	7	1001	2.15	3	2	ND	2	13	-	2	2	49	.71	.06	5	26	.37	111	.07	ž	1.90	.02	.08	2	5
IN SIL						• ·	c								•	-	-	14.44							1 1 March 1				* 8 3.		075
7N 32E	1	14	9	67	.4	23	7	271	2.10	3	7	ND	2	11	1	2	2	38	.13	.10	5	24	.41	?6	.09	3	2.79	.03	.08	2	5
7N 33E	1	13	7	62	.3.	21	7	280	2.29	6	2	ND	2	12	1	2	2	38	.18	.11	ò	28	. 40	86	.07	3	2.43	.02	.08	2	5
7N 34E	1	23	5	51	.2	24	8	213	2.37	7	2	ND	2	14	1	2	2	49	.16	.04	7	35	.65	103	.07	3	1.97	.02	.08	2	5
6N 27E	2	57	11	122	.3	65	12	904	3.38	20	2	ND	2	35	1	2	2	73	.55	.07	5	50	. 86	155	.11	3	3.57	.03	.09	2	5
6N 28E	1	15	10	51	.4	15	5	174	2.35	11	2	ND	2	15	1	2	- 2	45	.23	.15	4	21	.23	88	. 10	2	3.55	.03	.06	2	5
6N 29E	1	9	9	46	.4	10	4	397	1.48	2	2	ND	2	9	1	2	2	25	.08	. 10	6	17	. 18	80	.06	2	1.97	.03	.06	2	5
6N 31E	- 1	12	8	39	.3	15	5	242	2.22	12	2	ND	2	13	1	. 2	2	48	.18	.05	- 4	22	.29	93	.09	3	2.47	.03	.06	2	5
6N 32E	1	17	5	72	.2	24	8	342	2.39	11	2	ND	2	12	1	2	2	39	.12	.09	9	32	. 46	114	.06	3	2.12	.02	.09	2	5
AN 33E	1	25	6	55	.1	25	8	229	2.54	7	2	ND	2	15	1	2	2	54	.16	.04	7	37	.72	106	.07	3	2.02	.02	.10	2	5
6N 34E	. 1	28	7	54	.1	26	9	224	2.63	6	2	ND	2	16	1	2	2	55	.17	.05	1	38	.73	119	.08	3	2.19	.02	.10	2	2
26+75N 18E	1	25	7	114	.3	17	10	303	3.01	2	2	ND	2	23	1	7	2	62	.17	.06	4	22	.81	230	.08	3	3.06	.02	.15	2	5
26+50N 18E	1	20	8	110	.4	15	9	303	2.96	2	2	ND	2	19	1	2	2	59	.17	.09	4	22	.70	234	.09	3	3.33	.03	.15	2	5
26+25N 18E	1	24	5	111	.4	16	10	302	3.17	4	2	ND	2	20	1	2	2	65	.18	. 08	4	23	.82	257	.09	2	3.31	.03	.16	2	5
26N 18E	1	13	6	102	- 4	11	7	265	2.43	2	2	ND	2	13	1	3	2	44	.13	.13	1	18	.41	159	.10	. 3	4.01	.03	.08	2	2
27+75N 18+50E	1	53	6	71	.1	17	12	567	3. 78	•	2	ND	2	28	1	2	2	14	. 28	.05	2	23	1.22	124	,10	3	3.01	.04	. 40	2	2
27+50N 18+50E	1	30	6	102	.3	16	10	422	3.14	3.	2	ND	2	24	1	2	2	63	.20	.07	5	23	.84	210	.09	3	3.28	.03	.21	2	5
27+25N 18+50E	1	34	7	103	.3	17	11	459	3.42	8	2	ND	2	27	1	2	2	70	.20	. 08	4	25	.97	217	.09	3	3.19	.02	.23	2	5
27N 18+50E	1	38	6	98	.1	16	11	543	3.39	4	2	ND	2	30	1	2	2	69	. 24	.08	é	25	.96	193	.09	4	3.17	.03	.25	2	2
26+25N 18+50E	1	29	11	77	.1	15	9	303	2.85	3	2	ND	2	24	1	2	2	56	.24	.07	1	19	. 59	167	.10	3	3.13	.03	.16	2	15
26N 18+50E	1	50	9	80	.1	16	12	358	5.59	10	2	ND	2	42	1	2	2	82	.24	.04	5	20	1.00	141	.10	2	3.16	-05	.20	2	13
STD A-1/AU 0.5	1	31	39	186	.3	36	13	1023	2.83	10	2	ND	2	35	1	2	2	59	. 59	.10	7	73	.75	283	.08	9	2.05	.02	.21	2	490

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生産 感情 第二十二十一十

19219-6"-S.L

SAMPLE 1	No pp=	Cu ppe	Pb ppa	ln ppm	Ag pp=	Ni ppa	Co pps	Kn ppe	Fe Z	As ppm	U ppa	Au ppm	Th pp=	Sr ppe	Cd pp=	Sb ppe	Bi ppm	V ppm	Ca I	P I	La ppe	Cr ppe	Kg I	Ba pps	Ti Z	B ppe	Al Z	Na Z	K Z	¥ ppe	Aut ppb
25W 19E	1	21	10	87	.2	14	10	559	2.94	8	2	ND	2	40	1	2	2	53	.29	.05	4	22	.70	202	.07	3	2.91	.02	.21	2	5
27+75H 19E	2	62	20	138	.1	25	15	558	4.48	14	2	ND	2	196	1	2	2	51	.36	.10	3	16	.65	194	.03	3	3.58	.02	.16	2	5
27+50N 19E	1	24	14	115	.1	13	10	1562	2.70	6	3	ND	2	32	1	2	2	48	.24	.12	4	20		230	.06	2	2.80	.02	.15	2	5
27+25# 19E	1	25	6	82	.1	14	8	460	2.61	14	2	ND	2	28	1	2	2	50	.21	.09	3	19	.57	185	.08	2	3.40	.02	.18	2	5
27N 19E	1	31	5	62	.1	10	9	381	3.51	9	3	ND	2	32	1	2	2	75	.25	.02	3	19	1.10	165	.13	2	2.82	.02	.57	2	5
26+75N 19E	1	17	33	137	1.0	12	6	777	2.02	6	2	ND	2	20	2	2	2	36	.23	.19	3	19	.37	164	.08	3	3.25	.02	.11	2	15
26+50N 19E	1	76	229	266	3.0	15	10	449	3.17	11	2	ND	2	27	3	2	2	66	. 34	.06	3	36	1.03	182	.10	2	3.63	.02	.29	2	985
26+25N 19E	1	38	30	122	.1	15	11	593	3.61	12	3	ND	2	40	2	2	2	81	.31	.11	2	23	.97	276	.12	2	4.12	.02	.35	2	10
26N 19E	1	93	13	118	.2	12	16	1196	4.46	7	5	ND	2	25	2	2	2	153	.34	.06	2	20	1.45	188	.13	2	3.35	.02	.19	2	5
28N 19+50E	1	25	10	72	.1	14	9	568	2.58	8	2	ND	2	23	1	2	2	49	.26	.04	2	21	.63	178	.08	3	3.09	.02	.18	2	5
27+75N 19+50E	1	22	10	76	.1	15	10	652	2.75	5	2	ND	2	27	1	2	2	53	.35	.04	3	21	.76	177	.08	4	2.98	.02	.27	2	5
27+50N 19+50E	1	32	9	92	.1	19	10	469	3.22	13	3	ND	2	26	1	2	• 2	60	. 22	.20	4	26	.89	209	.09	3	3.23	.02	.24	2	5
27+25N 19+50E	1	47	24	95	.4	16	12	710	3.67	7	2	ND	2	40	2	2	2	BO	.59	.05	5	30	1.18	154	.09	3	3.05	.03	.27	2	70
27N 19+50E	4	47	44	116	1.0	18	13	648	3.94	9	3	ND	2	40	2	2	2	76	.29	.07	4	31	1.07	144	.09	2	3.18	.02	.46	2	215
26+75N 19+50E	1	24	16	114	.3	14	10	627	2.23	7	2	ND	2	26	1	2	2	70	.35	.06	4	21	.87	149	.10	2	3.23	.01	.24	2	10
24-50N 19+50E	4	46	19	106	.2	20	13	403	4.02	3	2	ND	2	24	1	2	2	58	.36	.04	3	21	.79	85	.05	2	3.14	.01	.15	2	35
26+25N 19+50E	1	60	65	146	.3	17	14	1014	3.81	11	2	ND	2	55	2	2	2	78	.28	.06	3	35	. 98	176	.09	2	3.66	.02	.25	2	20
26H 19+50E	1	58	11	99	.4	12	14	867	3.52	9	5	ND	2	23	1	2	2	105	.28	.09	2	15	.83	145	.11	2	2.77	.02	.13	2	5
28N 20E	1	27	8	101	.1	14	11	1363	3.56	4	2	ND	2	31	1	2	2	75	. 38	.06	3	22	. 98	272	.10	3	3.12	.02	.29	2	5
27+75N 20E	2	39	13	91	.3	14	9	1176	4.02	10	3	ND	2	58	1	2	2	68	.57	.05	7	20	. 92	162	.06	3	3.02	.02	.36	2	5
27+50N 20E	1	57	7	72	.8	16	12	611	4.25	12	3	ND	2	36	1	2	2	99	.54	.04	7	30	1.46	181	.14	2	2.97	.04	.73	2	55
27+25N 20E	1	34	17	89	.1	13	11	1019	3.34	12	4	ND	2	25	1	-3	2	68	.29	.08	4	23	1.02	210	.10	3	2.33	.02	.34	2	25
27N 20E	1	14	15	71	.3	12	6	825	2.17	9	2	ND	2	19	1	2	2	35	. 30	.21	4	14	.32	155	.10	2	3.95	.03	.09	2	5
26+75N 20E	2	79	24	96	.3	36	25	881	5.55	24	5	ND	2	36	2	2	2	112	1.57	.08	2	89	2.30	74	.02	2	3.52	.02	.33	2	115
26+50N 20E	2	22	9	85	.1	17	10	1133	3.37	10	2	ND	2	21	1	2	2	69	.47	.05	2	21	.84	153	.09	3	2.94	.02	.11	2	5
26+25H 20E	1	23	11	84	.3	15	9	320	2.81	7	2	ND	2	17	1	2	2	58	.18	. 06	3	23	.64	112	.10	3	2.98	.02	.09	2	5
26N 20E	1	45	7	81	.3	13	10	524	3.06	2	2	ND	2	16	1	2	2	80	.22	.11	2	16	.75	141	.13	2	3.29	.02	.16	2	5
28N 20+50E	1	23	10	124	.1	12	13	2299	3.13	8	2	ND	2	23	1	2	2	71	.20	.12	3	20	.79	414	.11	3	2.71	.02	.26	2	5
27+75N 20+50E	1	23	8	106	.1	12	12	1122	4.12	10	5	ND	2	16	1	2	2	112	.19	.03	2	25	1.52	410	.23	2	3.25	.02	.59	2	5
27+50N 20+50E	1	26	16	114	.1	12	13	1108	3.23	8	2	ND	2	46	1	2	2	55	.45	.09	2	14	.70	296	.08	3	2.79	.02	.29	2	5
27+25N 20+50E	1	30	7	72	.3	13	9	459	2.68	5	2	ND	2	23	1	2	2	57	.24	.08	5	14	. 59	215	.14	3	3.63	.03	.22	2	5
27N 20+50E	1	30	10	110	.3	14	11	1309	3.16	5	2	ND	2	45	2	2	2	61	.54	.08	4	19	.87	307	.09	4	2.74	.02	.31	2	40
26+75N 20+50E	3	43	11	79	.9	16	12	449	4.03	9	5	2	2	24	1	2	2	94	.22	.03	3	27	1.44	214	.13	3	2.94	.02	.45	2	200
26+50N 20+50E	1	32	7	84	.1	17	12	753	3.57	8	2	ND	2	23	1	2	2	77	.57	.09	5	23	.99	184	.11	4	2.75	.02	.33	2	5
26+25N 20+50E	1	25	10	103	.2	15	11	741	3.21	12	2	ND	2	18	1	2	2	58	.17	.09	3	20	. 59	136	.10	3	3.62	.03	.13	2	5
26N 20+50E	1	33	10	86	.2	18	11	448	3.39	6	3	ND	2	27	1	2	2	77	.23	.05	2	29	1.11	110	.11	3	3.49	.02	.14	2	5
STD A-1/AU 0.5	1	30	38	178	.3	36	12	1019	2.87	9	2	ND	2	37	i	2	2	57	. 59	.10	7	75	.73	282	.08	8	2.07	.07	.21	2	500

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San Carlos

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SAMPLE 1	No pp=	Cu ppe	Pb pps	Zn ppa	Ag ppa	Ni pp=	Co ppe	Kn pps	Fe Z	As ppa	U ppe	Au pps	Th pp=	Sr ppn	Cd pp=	Sb ppm	Bi ppæ	V ppm	Ca 1	P X	La pp#	Cr ppe	Hg 1	Ba ppa	Ti Z	B ppm	Al Z	Na Z	ĸ	¥ ppe	Aut ppb
JON JOE	5	37	17	114	.2	24	10	1860	5.31	18	2	ND	7	17	2	7	2	05	.20	10	15	57	81	178	07	2	7 57	07	-	2	5
29N 30E	1	19	11	78	.3	21	8	374	3.22	12	2	ND	2	11	ī	2	5	54	09	07		40	57	105	.09	2	2 07	07	.00	2	2
ZEN JOE	1	27	15	87	. 6	25	9	445	3.09	R	2	ND	2	17	i	2	2	50	10	.05	0	41	17	140	.00	2	7.54	.02	.00	4	3
27N 30E	1	24	12	107	.3	25	10	612	2.97	7	ĩ	ND	2	14	i	5	2	57	14	17	8	70	50	144		-	7 50	.02	.00	2	2
26N 30E	1	29	12	82	.4	25	11	407	3.00	11	2	ND	ž	15	i	2	2	54	.14	.06	9	41	. 62	126	.09	Ă	3.05	.02	.09	2	5
25N 30E	1	30	13	104	.3	25	12	1087	3.13	12	2	ND	2	20	t	2	2	63	.19	10		47	84	149		*	7.44		00	2	
24N 30E	1	38	13	101	.3	29	13	667	3.18	15	2	ND	7	73	1	2	2	44	71		7	47	.00	177		Ť	7 14	.03	.00	2	-
23N 30E	1	20	10	70	.3	16	8	464	7.70	9	2	ND	2	17	i	2	7	59	17	.06	5	78	54	104	17	2	2 PA	.02	.07	2	5
271 30E	i	24	13	94		19	11	599	3.12	13	2	ND	2	27	i	-	2	74	TL	.00	5	20		170	.12	-	7.04	.02	.0/	2	3
21N 30E	1	36	8	119	.4	72	17	692	3.54	15	2	ND	2	21	î	2	2	82	.26	.09	4	185	1.38	214	.12	2	3.66	.03	.10	2	5
20+75N 30E	1	32	12	134	.3	50	15	1110	7 41	19	2	ND	2	74	Ť.	2	2	70		17		51	20	217				03		-	
20+50H 30F	2	46	64	229	2 3	57	14	LOL	3 72	10	i.	ND	2	24		-	2	20		.15	1	57	.00	151	.11	2	3.20	.02	-11	4	2
20425N 30F	-	20	54	104	1.0	10	10	1410	2 71	17	2	ND	-	71	4	-	2	50	. 21	.00	1	32	. 84	134	.13	4	3.61	.03	.09	2	20
TOT THE SUC	-	17		104	1.0	57	13	1410	4. /0	.00	4	ND	4		3	4	2	26	. 54	.08	1	43	. 56	152	.09	2	2002	.02	.09	2	5
104 TEN TOP		33	17	123		33	15	133	3.40	25	4	ND	2	14		4	4	64	.18	.07		50	.70	141	.13	2	3.59	.02	.08	2	5
17773N 30C		24	10	68	.1	13	11	828	3.18	14	2	ND	2	21	1	2	2	76	.24	.07	3	35	. 86	139	.13	2	3.43	.03	.08	2	5
19+50W 30E	1	32	10	84	.1	23	12	718	3.10	12	2	ND	2	24	1	2	2	73	. 30	.11	3	39	.97	198	.12	2	3.16	.03	.15	2	5
19+25N 30E	1	31	10	69	.3	24	11	449	3.07	11	2	ND	2	16	1	2	2	70	.19	.05	5	40	.81	131	.12	-	1.4	07	09	5	5
19N 30E	1	28	8	76	.2	22	10	663	2.99	17	2	ND	2	17	1	2	2	68	.19	12	2	74	76	117	12	2	3 18	70	09	2	5
18N 30E	1	34	9	84	.1	22	10	468	3.27	13	2	ND	2	15	1	2	2	BO	21	13	2	74	77	104	12	2	3.10	.03	07	-	5
17N 30E	8	39	12	84	1.3	27	7	1570	2.51	16	2	ND	2	32	2	z	2	49	.71	.07	9	32	.44	96	.13	2	4.80	.05	.08	2	5
16N JOE	1	76	14	103	.6	63	12	512	3.44	25	2	ND	2	71	2	2	2	AR	.78	.06	5	18	74	157	13	2	5 14	70	00	2	5
15N 30E	1	36	10	73	.1	32	10	295	3.11	11	2	ND	2	28	ī	. 2	2	72	29	07		10	50	177	11	5	7 77	.03	10	5	5
14N 30E	3	51	9	63	.1	66	11	270	3. 26	18	2	ND	2	16	i	2	2	78	18	09	2	54	17	01	17	2	3.01	05	07	2	5
13N 3OF	1	24	10	147	.3	29	8	817	2.43	17	2	ND	2	13	;	2	5	50	12		ĩ	27	50	190	.14	2	7 70	.03	.07	2	5
12N 30E	i	45	13	108	.6	29	10	452	3.66	14	2	ND	2	13	i	2	2	81	.13	.12	5	42	.88	114	.13	2	3.79	.05	.13	2	5
11N 30E	1	11	12	82	.4	15	5	677	1.88	17	2	ND	2	14	1	2	2	78	15	15		74	27	111	10	7	7 47	05	04	2	5
10N 30E	1	18	9	69		29	8	145	2.45	0	2	ND	2	14	i	2	-	51	14	09	÷	11	54	170	10	-	1 75	.03	00	2	š
AN TOP	i	22	8	67		76	8	746	2 43	13	2	MA	5	15		2	2	57	.15	.07	5	70	50	1.1	.10	-	7.50	.03	.00	2	5
BN JOF	i	25	11	67		77		245	2.43	14	2	ND	-	19	1	-	-	55	.13	.00	1	30		102	. 12	-	3.37	.03	.00	2	5
TN SOE	i	20	9	66	.2	26	8	491	2.45	9	2	ND	2	20	i	2	2	54	.25	.05	ŝ	22	.56	102	.10	2	2.52	.02	.08	2	5
AN JOF		15	8	54	7	14		790	1.94	10	2	ND	2	17		2	2	74	12			74	71	05	00	-			07	2	•
STD A-1/AU 0.5	i	30	40	183	.3	36	12	1002	2.80	9	2	ND	2	36	1	2	ź	58	.57	.10	6	74	.71	282	.08	7	2.07	.02	.21	ź	530
PKS- 12761	ĩ	16	5	a		5	1	17	70		2	MD	2	70		2			17 71	01	-		74	10			10		03	-	
PYC-19975	1	57		10		14	10	401	7 20	15	2	ND ND	2	12	1	2	2		1 10	.01	4	71	1 01	17	.01	2	. 77	.01	.02	4	2
221 245		111	11	07		20	10	000	1.50	20	4	ND	4	12	1	2	2	140	1.00	.08	2	31	1.01	83	.10	2	1.75	.05	.18	2	3
STD A-1	i	30	39	182	.3	35	12	1017	2.84	11	2	ND	2	36	1	2	2	58	. 58	.10	7	74	.75	279	.08	8	2.03	.04	. 60	2	2
USR-90601	1	10	9	59	.2	5		594	2.23	6	2	ND	5	204		,	,	70	1.51	07	14		40	70	00		24		24		
USR-90602	1	6	12	57	.1	3		712	2.26	2	2	ND	5	15		5	5	20	53	00	21	0	. 10	57	.00	3	2.00	.04	.24	2	2
USR-90603	1	7	5	44	.1	X	1	578	1.78	2	7	ND		177	1	5	5	14	2 41	.01	21		.03	0/	.01	4	1.74	.02	. 40	1	2
USR-90701	1	197	3	AR	P	71	70	201	6 00	14		MD	-	77	-	-	2	110	1.70	.00	11	1	.13	3/	.01	1	1.05	.04	. 30	2	3
					.0		47	201	0.71	14	7	NU	4	13	2	4	2	118	3.51	.11	2	9	.18	34	.35	2	3.89	. 28	.16	2	5

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• 25 • 25 •4 5 • 9 • 1 5 • 75 • 2 5 • 2 • 10 • 2 10 45 € 15 3 • -2 5 2 20 • · 5 25 MOONBEAM 1 • 2 5 • 1 5 • ²/₇ • ³/₁₃ • ³/₂₃ • ·7 5 -3 5 ● 11 ·2 I¤ ● 17 • 2,10 • 10 • ·2 ·35 /●·S_5 18 ● 3_5 • 5 5 • 2 5 9 • 15 • 125 ● 35 ● 45 2 • 25 12 • <u>2</u> 5 6 • 3 370 • 1 5 • 0 • 1 5 .45 8 ● 2 25 MOONBEAM 4 MOONBEAM 3 • 5 5 4 • 1 20 7 • 2 5 • 3 10 • 6 8 • 2 5 2 • 3 5 • 2 0 6 10 / '3 5 🍯 ● 1 5 ● 1 5 ● 3 ● 6 • 2 5 • 4 • 1 5 ● ³ 5 5 2 5 ivIV/ • • 3 5 PACTION • 4 5 7 8 25 • 10 • 6 5 12 $\begin{array}{ccc} 3 & 5 \\ \bullet & 7 \end{array} \qquad \begin{array}{c} 2 & 5 \\ \bullet & 3 \end{array}$ ·25 • ·3 5 2 GRID C 10 ↓ 5 2 5 ♦ 4 ♥ B ·3 5 • 2 5 J 13 • J 35 13^{-1} 10^{-5} 10^{-5} 10^{-3} 10^{-3} 10^{-1} 10^{-5} 10^{-5} 10^{-3} 10^{-5} $10^{$ 0 1 5 23 WIGONBEZAN PIPODNBEZATS 3 50 ·3 5 4 10 5 15 ·2 70 14 • 1 5 • 1 5 • 1 5 • 3 5 • 3 5 • 2 5 • 2 5 • 18 • 20 • 11 • 9 • 8 • 7 • 9 '45 ● 17 • 13 5 ·2 5 2 45 45 **•** 10 -35 7 35 777 2 5 MOONBEAM ? MOONBEAM 17 25 4 - 15 - 12• 4 5 • 9 25 12 • 25 39 25 9 • • • • • 3 5 / • 3 5 i2 • 35 7 MI TMOONBEAM 12 • ·3 10 / ·3 $35 \bullet 8 \bullet 145 \bullet 35 \bullet 145 \bullet 55 \bullet 35$ +1 5 ● 12 • 4 5 12 • $\frac{1}{3}$ • $\frac{5}{12}$ • $\frac{1}{9}$ • $\frac{2}{3}$ • $\frac{2}{3}$ • $\frac{4}{3}$ • $\frac{3}{6}$ • $\frac{5}{7}$ • $\frac{2}{7}$ e 2 5 14 2 S 0 || $\bullet_{20}^{35} \bullet_{11}^{45} \bullet_{2}^{45} \bullet_{10}^{35} \bullet_{12}^{35} \bullet_{12}^{25} \bullet_{11}^{15} \bullet_{6}^{15}$ _ . __b_ - ______ 1 4 5 . 3 5 2 5 DAVID ONE × 10 5 ۲ -55 11 3 10





A,B,C Grid Scale 1:2500

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	• 45 • 25 22 • 12	• • • 5 5 19 ● • 5 5	⁵ ● ⁻³ 5 ● ⁻⁷ 15 ● ⁹	⁵ ● ⁻⁵ ⁵ ● ¹²	·4 5 1·2 5	
-2 15 -2 15 -2 15 -2 10 -2 10 -2 15 -2 10 -2 10 -2 10 -2 10 -2 10 -2 10 -2 10 -2 10 -2 10 -2 10 	° ● ^{·2} 5 ● ·2 5 ● ·6 ● ·13	● ⁻⁴ 5 ● ⁻⁴ 5 16 ● 12	5 • ⁻² 5 • 6	5 9 5 •	3 5 • 4 5 5 • 12	
• 12 • 12 • 12 • 11	• 15 • 14 5 14 • 13	• 410 • 45 14 • 8		10 7 5 •	4.5 ● 3.5 10 ● 12	
• ^{-2 5} 1 ³³ ● ^{3 5} 27+50E	• ² ⁵ • ³ ⁵ 13	• ⁴⁵ • 45	• ⁶⁵ • ³ 14 • ²	5 • 5 5 •	30+00E	<u> </u>
		• 2 5 8	• ¹ 5 8	• ¹ 5 4	• (5 • 8	28+
	• 4	• 15 ● 14	• ⁻¹⁵ 5	• ·3 5 10	• ·) 5 10	
	• ³⁵ 3	• 45 4	• 15 • 13	• *8 55 12	• 15 • 15	
	• 35 8	• 15 14	• ·4 70 7	• 125 • 12	• ³⁵ / ₅	
	-15 • 4	• g	1:0 2:5 9	• 35 9	• 3 10 • 5	
• 3 5 z		1.0 15 4	• ⁻³ io 7	• 5 115 • 24	•9 Zoo 9	
• 4 5 z		3.0 985 N	• ·2 35 • 3	• 10	• ¹⁵	
• 4 5 • 4	• ¹ 5 3	 1 10 12 	• ·3 20	• ³⁵ 7	● ⁻² 5 2	
● 2 5 1 18+00E	● 10 10	• 25	• 4 5 9	• ³⁵ 2	• 8 5 20+50E	26+
● ⁻⁶ 5 ·1 5 34 ● 7	-210 -15 ● 9 ● 8	● ¹ 4 5 • 1 5 15 ● 38	● ³ 35 ● ³ 5 13 ● 17	•4 5 ● 18		2 +
● ³ 5 25 ● 7 ● 12	-25 -15 ● 2 ● 11	• ³⁵ • ⁴⁵ 19 • 9	● 4 5 · 1 5 ● 23 ● 18	• ⁴ 5		
25 IS ● 10 ● 9	• 14 10 • 4 5 18 • 38	2.3 20 2.5 5	1.1 270 -2 (17 ● 8	° ● ³ 5 32		
• 15 • 15 • 10 • 17	• 4 • 7	30^{10} • 55_{53}^{15}	• ³ 5 • 5 5 110 • 26	2.5 ● 17		
• ² ₅ • ³ ₁₂	• 1 5 • 1 5 • 6 • 12	• $35 - 320$ • $23 - 21$	• 5 5 13 S	5 2.3 5		
• 25 • 25 • 7 • 10	• 35 • 15 10 • 14	• 15 · 25 • 14 • 8	• ² 5 • 3 5 19 • 19	• ⁵ 5 22		
● 7 ● 8 29+00E	• 25 • 35 • 24 ● 10	• 12 • 15 • 12 • 10	• ² 5 10 5 8 12	5 • 15 +00E		— 9+
		- 11				

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Soil sample location Silt " " Geochemical results Cu (ppm) Pb (ppm) Zn (ppm) 36 8 75 Pb ≥34 ppm GEOLOGICAL BRANCH ASSESSMENT REPORT 2**7-33** ppm 21-**26 p**pm 14-20 ppm 7-13 ppm ≤6 ppm

Rock sample location

• ³¹ 10 A,B,C Grid Scale 1:2500

13 6 102 102 102	٠	50 9 80	93 13 1ì8	58 II 99	●45 7 81	● 33 10 86 20+50E	
49 (5 86	2 1 i3 z ● 90 ● i	5 9 76 12 108 • 99	368 28 14 119 ● 65	³¹ ⁹ 5 8 1 99 8 8	4 36 15 ₿1		
● 26 IZ 95	23 7 3. ● ⁸⁵ ●	o 9 48 ⊔ 87 ● too ●	32 12 27 15 134 134	18 12 36 12 82 ● 94	. 70 (4 ● 88		
35 B ● 94	³⁴ 11 5 ⁴ ● ⁸⁹ ●	6 13 59 31 113 140	16 64 62 24 229 ● ¹⁸⁸	30 21 22 7 126 ● 90	23 10 99		
53 12 • 77		9 S 33 5 82 125	29 56 24 17 184 134	28 18 24 10 204 • 90	25 13 ● (28		
4 1 6 • 97	30 8 37 ● 78 ● 1	7 g ³⁴ ³⁹ ³⁹ ¹² 122	33 14 59 13 123 • 119	33 19 39 18 142 115	● 56 14 125		
32 9 ● 86	24 8 30 ● 103 ●	90 3 96 90 8 3	29 10 35 7 88 • 83	⁴⁵ 19 4 9 2 100 85	46 26		
32 († ● 89	34 13 5 ● 109 ● 1	10 38 10 162 88	32 10 27 10 84 91	2911 4219 91 69	● 98		
29+00E			31.00	31	+00E		

I					1	
		21 i0 ● 87	25 10 ● 72	● ²⁷ 8	● 23 io 12 4	28+
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	30 6 • 102	• ²⁴ 14 115	● 32 9 92	• 57 7 72	• 26 16 114	
	● 34 7 103	25 6 ₿2	• 47 24 95	• 34 17 89	• 30 7 72	
25 7	• 38 6 98	● 31 5 ● 62	47 +4 (16	● 14 15 71	• 30 10 110	
• •		17 33	• 24 16 114	• 79 24 96	• 43 11 79	
20 B 110		76 229 264	• 46 19 106	• 22 9 85	• 32 7 84	
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27+50 E

 $\begin{array}{c} \bullet & 162 \\ \bullet & 97 \\ \bullet & 97 \\ \end{array} \begin{array}{c} \bullet & 535 \\ 91 \\ \bullet & 87 \\ \end{array} \begin{array}{c} 54 \\ 0 \\ 5226 \\ \end{array} \begin{array}{c} 50 \\ 226 \\ 0 \\ 226 \\ \end{array} \begin{array}{c} 28 \\ 83 \\ 0 \\ 78 \\ \end{array} \begin{array}{c} 26 \\ 78 \\ 78 \\ 78 \\ \end{array} \begin{array}{c} 23 \\ 77 \\ 0 \\ 84 \\ 0 \\ 131 \\ \end{array} \begin{array}{c} 52 \\ 15 \\ 89 \\ \end{array} \begin{array}{c} 77 \\ 14 \\ 89 \\ \end{array}$ $\begin{array}{c} 3^{36} {}^{15} \\ 9^{37} \\ 9^{7} \\ 9^{7} \\ 9^{7} \\ 8^{4} \\ 9^{17} \\ 8^{4} \\ 9^{10} \\ 8^{11} \\ 9$ $\overset{36}{\bullet} \overset{14}{\bullet} \overset{33}{\bullet} \overset{11}{\bullet} \overset{31}{\bullet} \overset{12}{\bullet} \overset{31}{\bullet} \overset{13}{\bullet} \overset{24}{\bullet} \overset{13}{\bullet} \overset{22}{\bullet} \overset{9}{\bullet} \overset{26}{\bullet} \overset{14}{\bullet} \overset{23}{\bullet} \overset{12}{\bullet} \overset{16}{\bullet} \overset{13}{\bullet} \overset{22}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{22}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{22}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{22}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset{23}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{23}{\bullet} \overset$ 30+00E

 $\bigcirc ^{75} \bigcirc ^{123} \bigcirc ^{91} \bigcirc ^{106} \bigcirc ^{92} \bigcirc ^{23} \bigcirc ^{123} \bigcirc ^{94} \bigcirc ^{23} \bigcirc ^{13} \bigcirc ^{26} \bigcirc ^{17} \bigcirc ^{27} \bigcirc ^{15} \bigcirc ^{37} \bigcirc ^{17}$

LEGEND

AGE UNKNOWN

Lamprophyre dykes dark green to brown, weakly calcareous.

LATE JURASSIC

Valhalla Plutonic Rocks Coarse grained hornblende-biotite granodiorite, minor aplite and pegmatite. LJgd

CARBONIFEROUS AND PERMIAN

	Thompson Assemblage (Cache Creek r quivalent)
CPtav	Pale red brown weathering altered metavolcanics chlorite schist, minor phyllite, and biotite schist.
CPtac	Massive, crystalline white and grey limestone and marble.
Symbols	

Limit of outcrop Float × Geological Boundary: Defined, approximate, assumed. Bedding, Inclined Foliation, Inclined 🗡 🥖 👘 Joints: Verti al, Inclined Fault: Defined, Approximate Adit and Waste Dump Claim Post: Located by hip-chain, compass and altimeter survey Paved Highway

SCALE

1:5060

82 L/I 82 L/2 83 MW 9

Rock sample location

Soil sample location

-3 5 2 5 3 5 3 5 5 5 5 5 5 4 5 2 5 ● 27 ● 42 ● 25 ● 20 ● 19 ● 29 ● 22 ● 16 ● 20 ● 13 ● 18 ----- 30+00N 27+50E • ²⁵ • ¹⁵ • ¹⁵ • ¹⁵ • ¹⁵ • ^{28+00N} • 35 • 15 • (5 3 • 4 • 13 r6 55 • ·1 5 • 35 8 • 1 • 1 5 • 35 z • 4 5 2 • 15 • 15 • 10 • 8 • ¹/₂⁵ ● ¹/₁₀⁵ • ²/₇⁵ • ¹/₉⁵ • ²/₂⁵ • ²/₈⁵ --- 26+00 N IB+00E 20+50E 20+50E 65 15 210 15 45 45 35 35 4534 \bullet 7 \bullet 8 \bullet 8 \bullet 15 \bullet 38 \bullet 13 \bullet 17 \bullet 18---- 21+00N 35 25 25 15 35 65 45 15 65 • 7 • 12 • 2 • 11 • 19 • 9 • 23 • 18 • 12 • $\frac{125}{7}$ • $\frac{125}{10}$ • $\frac{135}{10}$ • $\frac{15}{14}$ • $\frac{15}{14}$ • $\frac{125}{19}$ • $\frac{25}{19}$ • $\frac{35}{19}$ • $\frac{55}{22}$ • $7 \cdot 8 \cdot 25 \cdot 35 \cdot 15 \cdot 15 \cdot 25 \cdot 105 \cdot 15$ • $7 \cdot 8 \cdot 24 \cdot 10 \cdot 12 \cdot 10 \cdot 8 \cdot 12 \cdot 16$ ---- 19+50N 29+00E 31+00E ● ³5

A, B,C Grid Scale 1:2500

Z n ≥ 151 µ	nqq	×			
33-	150ppm				
115-	132 "				
97-	114 "				
• 79-	96 "				
• ≤78p	p m	GFO	TOCI	~	
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SCALE		BY	N.T.S. No.	DWG No.	
1:5000	Huy. 03	ULF	82L/I 82L/2	83MW 7	
	_			L	i

Scale 0 100 200 metres

Rock sample location

Soil sample location

Geochemical results Cu (ppm) Pb (ppm)

Silt "

36 8

		€ 87	25 10 ● 72	● ²⁷ 8	2 3 10 12.4	28
	536 71	62 20 138	• 22 10 76	• 39 13 91	• ²³ 8	
	● ³⁰ 6 102	24 14 115	• ³² 9 92	• 57 7 72	• 26 16 114	
	● ³⁴ 7 103	• ²⁵ 4 82	• 47 24 95	• 3+ 17 89	• 30 7 72	
25 7	• 38 6 98	● 31 5 ● 62	• 47 +4 116	• 14 i5 71	• 30 10 110	
		17 33	• 24 16	• 79 24 96	• 43 11 79	
● ²⁰ 8 110		76 229 26 4	• 46 19 106	● 22 9 85	• 32 7 84	
• 24 5 111	29 ii • 77	38 30 122	60 65 146	● 23 // 84	● 25 10 103	
13 6 102	● ⁵⁰ 9 80	93 I3 116	• 56 11 99	● 45 7 81	• 33 10 86	26
18 TOUL					20+50E	

N

Scale O

100 200 metres

•LWB 34130 Soil sample location and number

GEOLOGICAL BRANCH ASSESSMENT REPORT

11,789

NAKUSP RESOURCES LTD. MONASHEE WEST **RECONNAISSANCE GEOCHEMISTRY** SAMPLE LOCATION I.M.WATSON & ASSOCIATES LTD. <u>SCALE DATE BY N.T.S. No. DWG No.</u> 1: 5000 AJJ. 83 DLP 82 L/1 82 L/2 83 MW 8

A,B,C Grid Scale 1:2500

			30 102		• ²⁴ 14	ŀ	• 32 92	9	• 57 7:	, <i>7</i> 2	•	26 16 14	
			34 103	7	• ²⁵ 6 82		• 47 95	24	• 34 89	+ 17 9	• =	80 7 72	
	-		38 6 98		● 31 5 62		• 47 116	44	• 14 71	15	•	80 10 110	
(25 7 314				17 33 • 137	3	• 24 114	16	7 9 96	24	• 4 7	3 II 19	
(208 110				76 2 264	29	• 46 106	19	• 22 85	9	• 3: 8	27 14	
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18+	13 6 102 00E		50 80	9	93	13	• 58 99	н	•45 81	7	● 84 20+50)E	26
	49 15 86	2+ 13 90	25 9 108	76 12 99	● ^{36 8}	28 14 65	● ³¹ 99	58 i 4 88	• 36	15			21
•	26 12 95	• ^{23 -7}	30 9 87	48 II	32 12 134	27 15 • 134	18 12 ● 82	36 12 94	1 70 88	(4 3			
	35 B 94	³⁴ "	56 13 113	59 31 140	46 64 229	62 24 188	30 ZI ● 126	22 7 ● 90	• ^{2 5} 99	10			,
	53 12 77	60 (4) ⁹	39 S 82	33 5	29 56 184 (24 17 134	28 18 204	● 24 10 ● 90	• ²⁵	13 B			
	4+ 6 97	³⁰ 8 78	37 8 ЮZ	39 12 122	33 14 123	59 13 119	33 19 • 142	39 IB	• 56 129	(4			
	32 9 86	24 B • 103	36 5 90	³ 7 € 83	2 9 ID 88	35 7 83	15 / 9 100	492 85	46 2 106	6			
(32 ≀I ● 89	34 iB 109	51 10 162	38 (Ő	32 (0 84	27 10 91	• 29 11 91	42 19 69	• ⁵ °	8			19
29	9+00 E I				• ³¹ 10			31	+00E				

 $\overset{30}{\bullet} \overset{16}{\bullet} \overset{46}{\bullet} \overset{8}{\bullet} \overset{34}{\bullet} \overset{14}{\bullet} \overset{28}{\bullet} \overset{15}{\bullet} \overset{21}{\bullet} \overset{12}{\bullet} \overset{19}{\bullet} \overset{13}{\bullet} \overset{32}{\bullet} \overset{12}{\bullet} \overset{20}{\bullet} \overset{11}{\bullet} \overset{31}{\bullet} \overset{17}{\bullet} \overset{28}{\bullet} \overset{13}{\bullet} \overset{19}{\bullet} \overset{11}{\bullet} \overset{16}{\bullet} \overset{90}{\bullet} \overset{90}{\bullet} \overset{97}{\bullet} \overset{95}{\bullet} \overset{69}{\bullet} \overset{67}{\bullet} \overset{97}{\bullet} \overset{9}{\bullet} \overset{73}{\bullet} \overset{64}{\bullet} \overset{94}{\bullet} \overset{96}{\bullet} \overset{91}{\bullet} \overset{91}{\bullet} \overset{91}{\bullet} \overset{78}{\bullet} \overset{19}{\bullet} \overset{11}{\bullet} \overset{17}{\bullet} \overset{28}{\bullet} \overset{13}{\bullet} \overset{19}{\bullet} \overset{11}{\bullet} \overset{16}{\bullet} \overset{90}{\bullet} \overset{90}{\bullet} \overset{97}{\bullet} \overset{95}{\bullet} \overset{69}{\bullet} \overset{67}{\bullet} \overset{9}{\bullet} \overset{79}{\bullet} \overset{73}{\bullet} \overset{64}{\bullet} \overset{94}{\bullet} \overset{96}{\bullet} \overset{91}{\bullet} \overset{91}{\bullet} \overset{91}{\bullet} \overset{19}{\bullet} \overset{11}{\bullet} \overset{17}{\bullet} \overset{28}{\bullet} \overset{13}{\bullet} \overset{19}{\bullet} \overset{11}{\bullet} \overset{17}{\bullet} \overset{18}{\bullet} \overset{18}{\bullet} \overset{1$ 27+50 E 30+00E

 $\begin{array}{c} 36 \\ 95 \\ 97 \\ 97 \\ 84 \\ 108 \\ 95 \\ 108 \\ 95 \\ 108 \\ 95 \\ 108 \\$

 $\overset{53}{\bullet} \overset{17}{\bullet} \overset{64}{\bullet} \overset{17}{\bullet} \overset{32}{\bullet} \overset{13}{\bullet} \overset{12}{\bullet} \overset{16}{\bullet} \overset{28}{\bullet} \overset{16}{\bullet} \overset{23}{\bullet} \overset{18}{\bullet} \overset{23}{\bullet} \overset{13}{\bullet} \overset{24}{\bullet} \overset{13}{\bullet} \overset{28}{\bullet} \overset{17}{\bullet} \overset{27}{\bullet} \overset{15}{\bullet} \overset{37}{\bullet} \overset{17}{\bullet} \overset{---}{--} 30+00 N$ $\overset{33}{\bullet} \overset{15}{\bullet} \overset{4\circ}{\bullet} \overset{17}{\bullet} \overset{35}{\bullet} \overset{14}{\bullet} \overset{54}{\bullet} \overset{15}{\bullet} \overset{3\circ}{\bullet} \overset{14}{\bullet} \overset{28}{\bullet} \overset{14}{\bullet} \overset{26}{\bullet} \overset{15}{\bullet} \overset{23}{\bullet} \overset{15}{\bullet} \overset{62}{\bullet} \overset{16}{\bullet} \overset{52}{\bullet} \overset{15}{\bullet} \overset{52}{\bullet} \overset{15}{\bullet} \overset{77}{\bullet} \overset{14}{\bullet} \overset{15}{\bullet} \overset{17}{\bullet} \overset{17}{\bullet}$

