ASSESSMENT REPORT

MAHON CLAIM GROUP

FORT STEELE MINING DIVISION

PERIOD JUNE 27, 1983 - DECEMBER, 1983

MOUNT MAHON AREA

N.T.S. 82G/4

LATITUDE 49°05'

LONGITUDE 115°58'

OWNER: ST. EUGENE MINING CORPORATION LTD.

OPERATOR: CHEVRON CANADA RESOURCES LIMITED

AUTHOR: LARRY DEKKER

DATE: APRIL 1984

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ILLUSTRATIONS

FIGURE 1

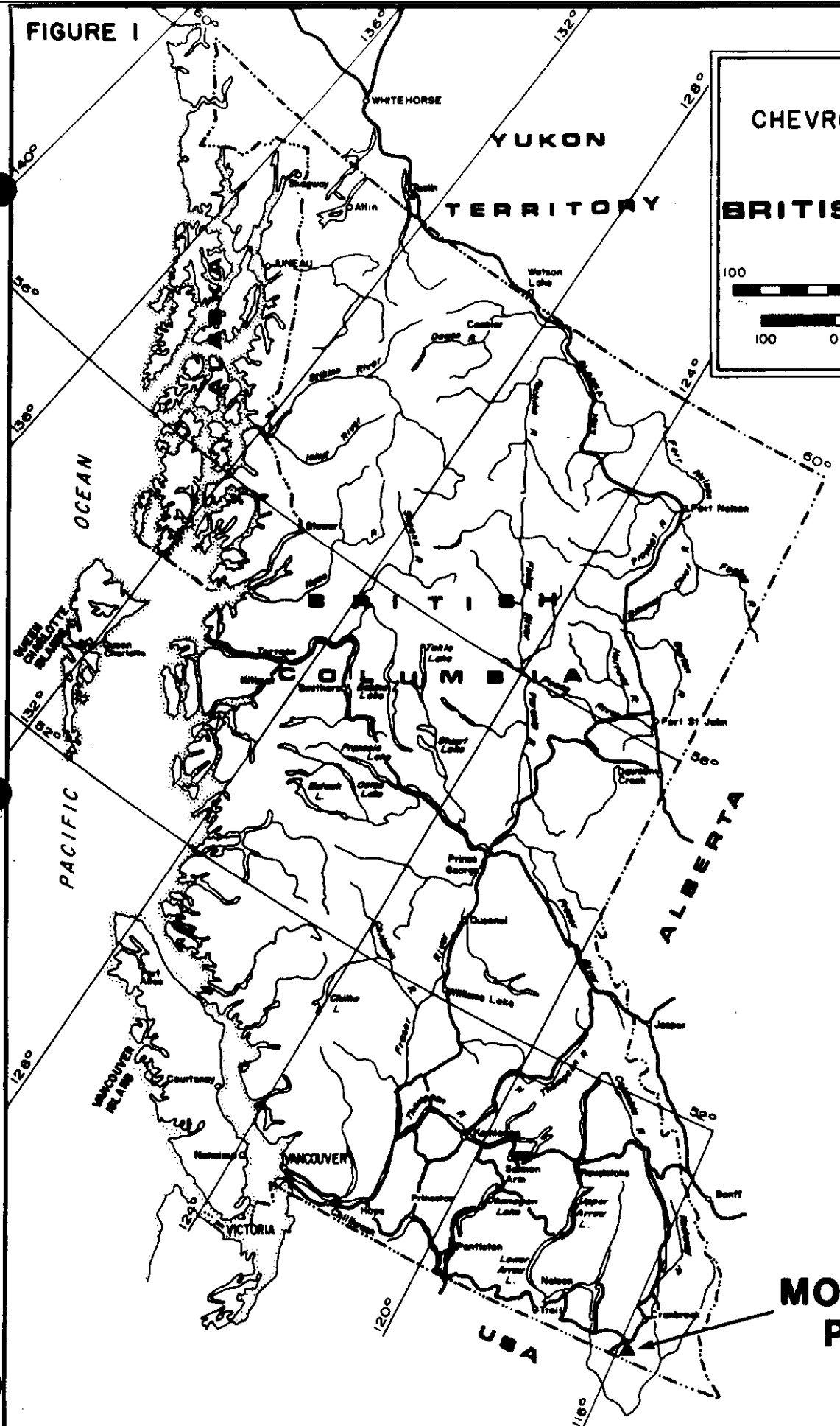


FIGURE 1

LOCATION MAP

MOUNT MAHON PROPERTY

1. INTRODUCTION

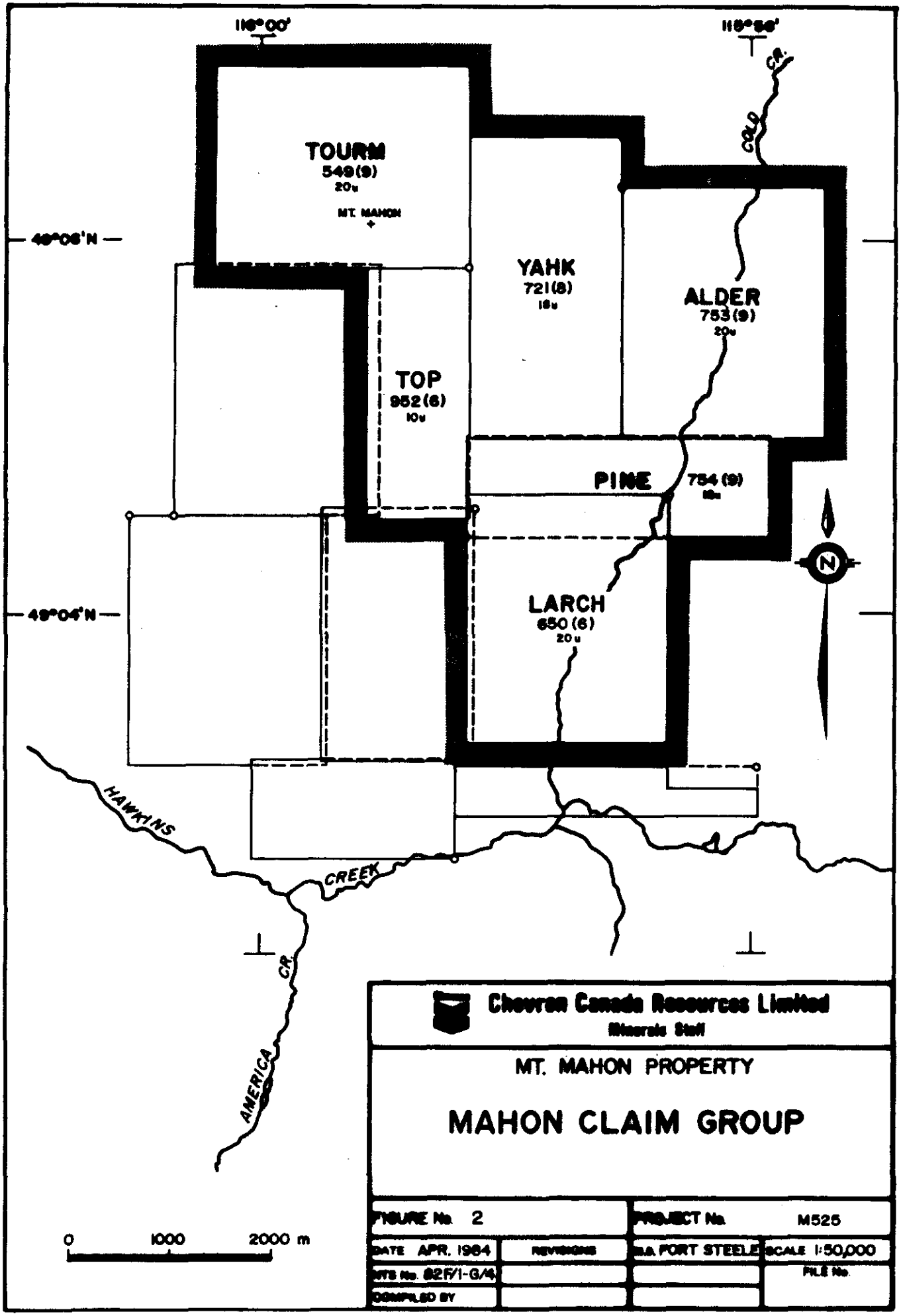
The Mount Mahon property is located in the Purcell Mountains in southwestern B.C., app. 8 km ENE of the town of Yahk and paved Highway #3 (Fig. 1). This area forms part of the interior rain belt with an average annual precipitation of 75 to 100 cm.

The property consists of a grouping of 100 units which are underlain by metasediments of the Proterozic Middle Aldridge Formation. On Mount Mahon several beds of tourmalinized siltstones and sandstones are present which were first described by Ethier and Campbell (1977). This tourmalinite suggests stratigraphic proximity to the Lower/Middle Aldridge contact, the level coeval with the Sullivan deposit.

Chevron Canada Resources optioned the property from St. Eugene Mining Corporation Ltd. in the fall of 1983 to further explore the possibility for Sullivan-type mineralization. This assessment report describes the results of the geological, geochemical and geophysical work carried out on the property by Chevron during the 1983/1984 field season. Each of these programs will be discussed separately in this report.

2. LOCATION AND ACCESS

The Mahon property is located in southeast British Columbia approximately 8 to 10 kms ENE of the town of Yahk (Fig. 1). Access is via Hawkins Creek road which joins Highway #3,via the turn off at kilometre 7 or the Cold Creek turn off near kilometre 12. The Cold Creek logging road parallels the eastern boundary of the claim block. Topographic elevation varies from 1895 m, the top of Mount Mahon,


116°00'
115°56'
49°08'N
49°04'N
TOURM
549(9)
20u
MT. MAHON
YAHK
721(8)
18u
ALDER
753(9)
20u
TOP
952(6)
10u
PINE
754(9)
LARCH
650(6)
20u
COLD CR.
HAWKINS CREEK
AMERICA CR.
N
0 1000 2000 m
Chevron Canada Resources Limited
Minerals Staff
MT. MAHON PROPERTY
MAHON CLAIM GROUP
FIGURE No. 2
PROJECT No. M525
DATE APR. 1984
REVISIONS
NTS No. 82F/1-G/4
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M.A. FORT STEELE
SCALE 1:50,000
FILE No.

to 906 m in Cold Creek Valley. Most of the claim group is located on the gently dipping eastern dip slope of Mount Mahon which has a gentle to moderate topographic relief. Vegetation is highly variable: from dense buckbrush and alder, which makes linecutting tedious and difficult, to more open areas with spruce, to bare patches at higher elevation along the ridge trending south of Mount Mahon summit. The property contains a myriad of old, mostly overgrown, logging roads, however, some of these are accessible with a 4 x 4. Water is scarce on the property.

3. CLAIMS

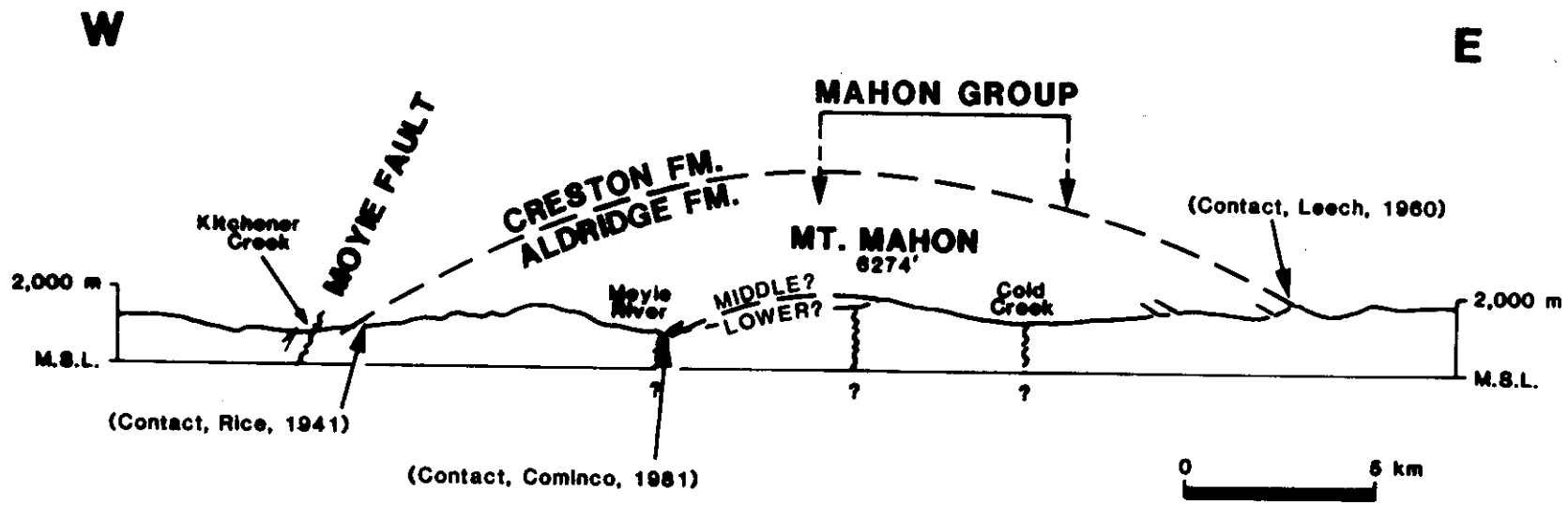
The Mahon claim (Fig. 2) consists of the following group of claims:

Claim Number	Record No.	Units	Date Recorded	Hectares	Expiry Date
TOURM	549	20	Sept.21/78	500.0	Sept.21/84
YAHK	721	18	Aug. 1/79	450.0	Aug. 1/84
TOP	952	10	Aug. 1/79	250.0	June 20/84
PINE	755	12	Sept.7/79	300.0	Sept. 7/85
ALDER	754	20	Sept.7/79	500.0	Sept. 7/84
LARCH	650	20	June 11/79	500.0	June 11/84
		Total 100 units			

These claims were staked by St. Eugene Mining Corporation Ltd. and optioned to Chevron Canada Resources Limited in 1983.

FIGURE 3

STRUCTURAL CROSS-SECTION
MOYIE ANTICLINE



M525

4. GEOLOGY

4.1 REGIONAL SETTING

The Mount Mahon area is located close to the hinge zone of the northeasterly plunging Moyie Anticline (Fig. 3). The strata exposed on and near the top of the mountain dip mainly at shallow 10° to 20° angles to the northeast, although strike varies locally by almost 40° from northwest to slightly south of west. Strata exposed on the ridge to the the west of Mount Mahon are dominantly flat lying but dip shallow to moderately west as well. These attitudes support the observation that Mount Mahon is located on the eastern edge of a broad hinge zone which includes locally some parasitic folds.

Strata exposed east of Cold Creek have shallow easterly dips as do those on the ridge extending south of Mount Mahon summit, thereby characterizing the east limb of the Moyie Anticline.

4.2 GEOLOGY OF THE CLAIM BLOCK

The claims are underlain by metasediments of the Middle Proterozoic (Helikian) Aldridge Formation of the Lower Purcell Super group. The claim area and the immediately surrounding area were mapped on a scale of 1:5000 (Figs. 4 and 5 in pocket Nos. 1 and 2).

The Aldridge Formation sediments within the claim block consist mainly of sandstone, but also include siltstone, argillite, and relatively minor amounts intraformational conglomerate. These rocks are partially tourmalinized over a substantial stratigraphic interval in the immediate vicinity of the summit

of Mount Mahon. Dioritic rocks are found mainly in the poorly exposed eastern portion of the claim block and also occur as two well exposed sills within Aldridge metasediments immediately east of the claim block. The rocks within the area have been recrystallized under upper greenschist facies metamorphic conditions, and the metasediments are characterized by a quartz-muscovite-biotite-garnet assemblage. Despite this metamorphism, the primary sedimentary structures within these Aldridge Formation rocks are very well preserved. Sulphide mineralization is restricted to a few exposures containing 1 to 2% disseminated pyrrhotite within both tourmalinized and non-tourmalinized metasediments.

The sandstones are generally fine to very fine grained. They weather typically light grey, are light to medium grey on fresh surface and are composed mainly of quartz (70 - 85%) along with biotite, muscovite and occasionally garnets. Beds range in thickness from a few cms to slightly more than a meter thick and are most commonly from 10 to 70 cm thick. These sandstone beds are for the most part massive, lacking internal structures. Commonly, they have graded tops and pass upward into 1 to 3 cm thick intervals of dark grey argillite. Load casts, flame structures, and rare flute casts are locally present on the bases of these graded beds. These beds are interpreted to represent A-E turbidites of the Bouma (1962) turbidite sequence. Intervals of parallel laminated, very fine grained sandstone to siltstone occasionally occur in the upper portions of these beds, and at one locality a thin zone of and crossbedded sandstone was observed at one locality (A-B, A-B-E, and a single A-B-C-E turbidite). The silty to

argillaceous tops of these beds are typically a darker colour, less quartzose, and correspondingly more micaeous than the massive lower portion of the beds. The micas are commonly aligned to define a weakly to moderately well developed cleavage.

Outcrop within the claim group is mainly restricted to two areas along its western boundary. The first of these comprises a 2.5 km^2 area of north-easterly to northerly, shallow dipping strata extending north, east and west from the top of Mount Mahon. These exposures represent approximately 300 meters of stratigraphic thickness. Tourmalinite occurs intermittently over a 70 meter stratigraphic interval on the southeast flank of Mount Mahon and also in two small isolated exposures on the southwest flank of the mountain. These latter exposures are approximately 100 meters lower in the section than the better exposed tourmalinized outcrops on the southeast flank. Rocks exposed east-northeast and northwest from the top of Mount Mahon cover the same stratigraphic interval as the tourmalinized outcrops but are <u>not</u> tourmalinized.

The second area of bedrock exposure occurs on the ridge which extends south from Mount Mahon. Outcrop along this ridge begins approximately 1.3 km from the summit of Mount Mahon and from there extends for almost 4 km southward. These strata dip shallowly to the east along most of the ridge, but the dip changes to east-southeast in the southernmost exposures. A rather thin stratigraphic interval of approximately 200? meters is exposed in this series of outcrops since they represent largely a dip slope.

Tourmalinite was not observed in place in this southern series of outcrops; however, abundant tourmalinite float occurs on and adjacent to the ridge top along the northernmost 1.5 km of these exposures and probably indicates tourmalinization at approximately this stratigraphic level. It is estimated that these exposures are approximately 250 meters lower in the section than the lowest tourmalinite exposed near the top of Mount Mahon.

Additional exposures within the actual claim block are restricted to two outcrops of dioritic rock approximately 3 km east-southeast of Mount Mahon summit. Included in the geological map (Fig. 4) are two areas of outcrop which were mapped to the immediate east and west of the claim block, respectively. These outlying exposures consist of Aldridge metasediments and of dioritic intrusions similar to those found within the claim block.

4.3 TOURMALINITE

Outcrops of tourmalinized sediments are restricted to the immediate vicinity of the summit of Mount Mahon. Tourmalinization occurs intermittently over a 70 meter stratigraphic interval on the southeast flank of the mountain, while two small tourmalinized outcrops on its southwest flank appear to be situated approximately 100 meters lower in the stratigraphic section (Figs. 4 and 6). Abundant tourmalinite float along the ridge south of Mount Mahon may represent tourmalinization at as yet a lower stratrigraphic level (Figs. 4 and 6).

The tourmalinite is most conspicuous as hard, "cherty", dark grey to black, black weathering beds which occur in the place of argillite at the tops of graded sandstone beds and within finely bedded laminated siltstone/tourmalinite couplets. These tourmalinite layers are typically only a few mm's to a few cm's thick but range up to several cm's thick in the upper portions of some sandstone beds. These tourmalinite horizons often appear graded changing upwards in colour from dark grey to black. Some of the thicker tourmalinized layers are internally laminated, also in shades of dark grey to black. The associated siltstone and sandstone layers within these tourmalinzed sections usually do not differ greatly in appearance from their counterparts within non-tourmalinized sections. Tourmalinite and/or tourmalinized argillite may extend as flame structures into overlying, essentially untourmalinized, sandstone, and tourmalinite beds may be broken and disrupted by overlying sandstone beds. Tourmalinite occurs also as flat rip-up clasts within otherwise untourmalinized sandstone-matrix of the conglomerates. As noted by Ethier and Campbell (1977), these relationships indicate clearly that boron enrichment was contemporaneous with sedimentation. In some instances, however, siltstone and sandstone beds are significantly tourmalinized, in which case they are black, dense, and very hard.

Thin Section observation reveals that the tourmalinite beds consist mainly of a fine felted mass of extremely small (0.01 mm long), greenish-brown tourmaline crystals. This tourmaline seems to comprise 40% to 60% of the typical black "cherty" "tourmalinite" rock in which it is accompanied mainly

by equally fine grained quartz and sericite (note, however, that the extremely fine grain size makes the determination of mineralogy and modal abundance very tenuous). Sphene and opaque grains (mainly Fe-Ti oxides?) are typically present as somewhat larger grains (together comprising 2% or less of a given layer), while euhedral garnet prophyroblasts of up to 0.1 mm in size are often present in minor (<1%) quantities. Ethier and Campbell (1977, p. 2352) indicate that microcline, biotite, and chlorite may also be present, although these minerals were not positively identified in the present study. Grading and/or laminations within these tourmalinite horizons are conspicuous in thin section as increasing tourmalinization leads to a denser, darker and more uniform appearance of the beds.

Thin section examination also shows that the sandstones and siltstones intercalated with the tourmalinite layers are, in fact, tourmalinized to some extent although this is generally not conspicuous in hand specimen. Extremely fine tourmaline crystals (<0.01 mm long) occur as single grains or small clusters of grains which comprise up to 25% of these rocks. Internal laminations, including cross-laminations, within these siltstones and sandstones are typically accentuated by variations in the proportion of tourmaline within the different layers. The heavily tourmalinized siltstone and sandstone beds, conspicuous by their hard, dense, black nature on the mesoscopic scale, consist of detrital quartz grains, which float in a matrix of densely concentrated, extremely fine-grained, felted tourmaline grains. The detrital character of the quartz grains is typically well preserved within these tourmalinized rocks.

The tourmalinite exposures on the southeast and southwest flanks of Mt. Mahon indicate that tourmalinization in this area occurs over a stratigraphic interval of at least 170 meters (Figs. 4 and 6). The lower limit of this tourmalinized section is defined only by the lack of exposure immediately south of Mount Mahon, and it possibly extends to even deeper levels. Tourmalinite float on the ridge farther south of Mount Mahon peak (Figs. 4 and 6) suggests, in fact, that tourmalinite does occur lower in the section. This float occurs on strata which are estimated to lie 250 meters lower stratigraphically than the lowest tourmalinite exposure on the southwest flank of Mount Mahon (Fig. 6). Tourmalinization may, therefore, occur over a stratigraphic interval of at least 400 meters. It appears, however, that the tourmalinite has rather limited lateral continuity. Exposures immediately to the north-northwest of Mount Mahon peak, and also 600 to 900 meters to the east-northeast of the mountain, appear to occupy the same stratigraphic interval as the Mount Mahon tourmalinites but show no sign of tourmalinization (Fig. 6).

5. MINERALIZATION

One of three drill holes on the east flank of Mount Mahon (No. YA-6, TD 124.1 m) did, at 23 m, intersected a 7 m thick zone of intensely chloritized sediments(?) with several up to 15 cm thick beds consisting of massive pyrrhotite/pyrite/marcasite with accessory chalcopyrite. The zone carries low, but anomalous values of Cu, Zn and Ag (1 oz/ton). The massive sulphide beds make up about 20% of this interval. Similar thin, chloritized zones (possible altered intrusive dykes) without sulphide mineralization occur near the bottom of this hole. No tourmalinite zones were found in the quartzwackes and siltstones which make

up the bulk of the drill intersection. No sulphide mineralization was found in holes Nos. YA-7 and YA-8 drilled several hundred meters away (see Figs. 4 and 11).

Correlation between the sulphide drill intersection and the tourmalinite outcrops near the top of Mount Mahon is not possible, but the shallow NE dips measured on the flank and the top of the mountain suggest that the tourmalinite and the sulphide occurence are positioned near the same stratigraphic level which closely follows the mountain slope (Fig. 6). Regional extrapolation suggests that this level approximates. The productive Lower/Middle Aldridge contact although, due to scarcity of outcrop and its gradational nature, this contact could not be positively identified.

6. GEOCHEMISTRY

6.1 GRID

A hand-cut grid was established on the East flank of Mount Mahon over the northern portion of the property to cover the tourmalinite outcrops on top of Mount Mahon and drill hole YA-6 containing the massive sulphide intersection (Fig. 7). Baseline 0+00 N was established so as to connect DDH's YA-6 (Station 0+00 E + N) and Y13-81 on top of Mount Mahon, which intersected several tourmalinite beds. This line runs WNW-ESE and approximates the regional strike direction. Baseline 0+00 E was established through DDH YA-6 as well and more or less coincides with the NNE regional plunge and dip direction. Sample lines were run parallel to baseline 0+00 N and spaced 200 m apart. Sample stations were established at 50 m intervals. The baselines were surveyed, the distances between sample stations tight chained and slope corrected. A total of 41.25 kms of line was cut.

6.2 GEOCHEMICAL SAMPLING

The grid area contains only a few, mostly dry creek beds. Silt samples were taken where grid lines crossed these creek beds, but, due to lack of run off, this method was not thought to be very effective. The grid area is largely covered by drift. The drift is virtually nil along the higher elevations on Mount Mahon and the west side of the grid where most of the bed rock outcrops. It increases in thickness to the east and the Cold Creek river valley near the east property boundary where it attains 39.6 m in DDH YA-8 near the south centre of the grid and 53.9 m in Y-10-81 just outside the SE corner of the grid. This thick drift cover together with the poor drainage will tend to adversely affect the effectiveness of a geochemical soil sampling program. Even so, it was felt that this geochemical technique had to be tested without too much emphasis to be placed on negative results as this might be due to other factors, such as overburden cover which could conceal a "blind" ore body not expressed in surface geochemistry. Soil Samples were taken on the grid at 50 m intervals from the "B" horizon which was well developed in most places at a depth of 5 to 25 cm. The samples were placed in conventional paper bags and dried in the field at room temperatures. A total of 828 soil samples and 16 silt samples were collected and analyzed with conventional analytical techniques by Chemex Labs Ltd. in North Vancouver.

6.3 GEOCHEMICAL RESULTS

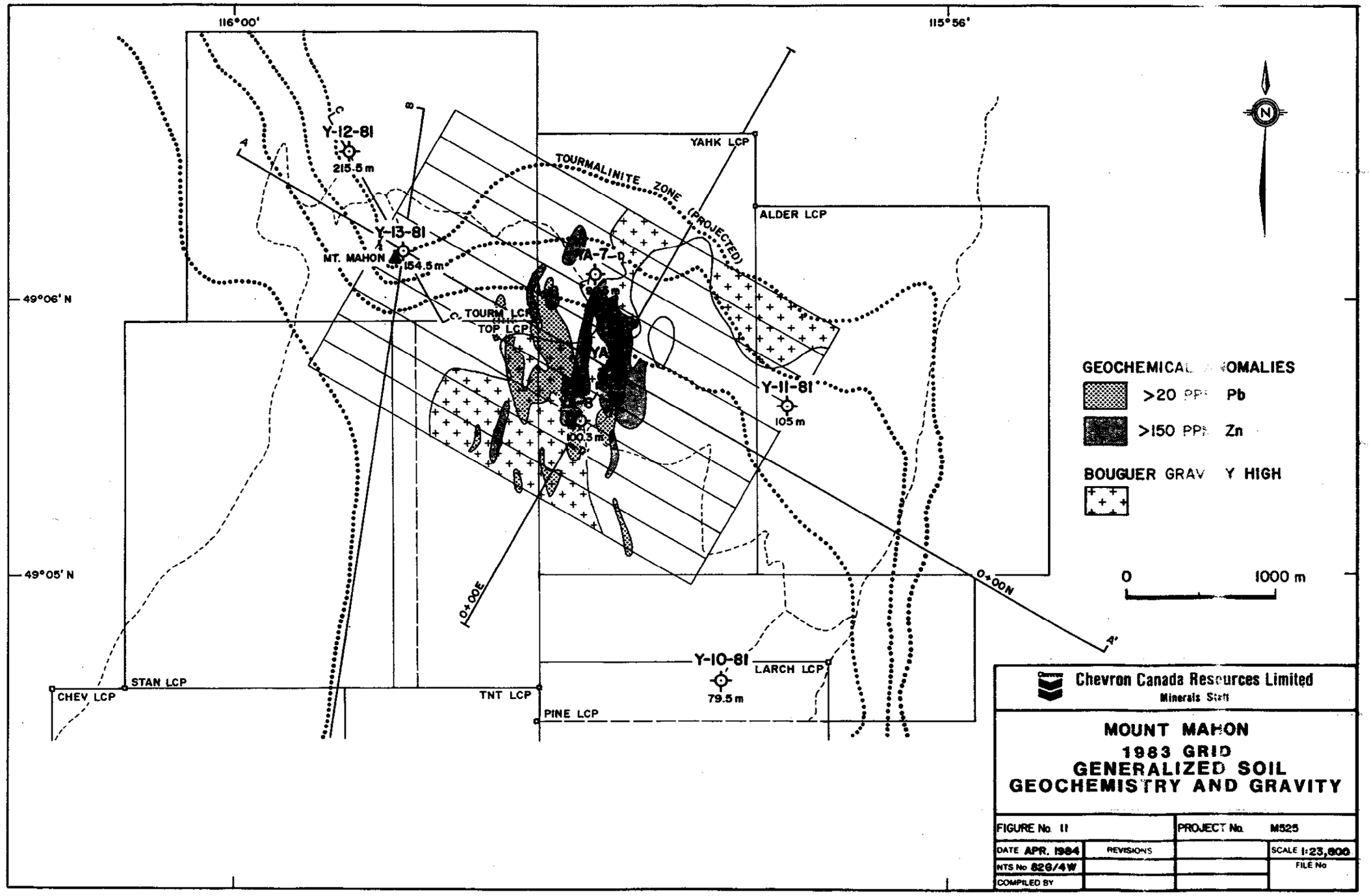
The soil samples were analyzed for Pb, Zn and Cu. The important statistical data of this population of 828 samples for these three elements are as follows:

	MEAN	MINIMUM	MAXIMUM	S.D.	C.I.
Pb	13	3	85	7	20
Zn	96	28	505	44.7	50 & 100
Cu	26	9	100	11	40 & 50

All numbers are in ppm.

The geochemical data have been plotted and contoured on individual 1:5000 scale maps (Figs. 8, 9 and 10; Pb, Zn and Cu respectively, in pockets). Pb and Zn are anomalous in the central portion of the grid in the vicinity of DDH YA-6 with two distinct elongated, approximately N-S trending anomalies (Fig. 8, 9 and 11). The most pronounced Pb and Zn anomalies are approximately 800 m long and 200 m wide, extend north and south of DDH YA-6 and might be related to the sulphides intersected in this hole. A second, broader and longer (approximately 500 m x 1200 m) anomaly extends north of DDH YA-8 and is most strongly expressed over 300 m directly upslope from this hole. There appears to be good correlation between Pb and Zn, with an expected slight downslope dispersion and shift of the Zn versus the Pb anomalies. Anomalous Pb and Zn were not found further east on the grid but, as mentioned previously, overburden could play a significant depressing role.

The mean Pb value on the property is 13 ppm. Work on 863 soil samples collected in a regular network across the U.S. at a depth of about 20 cm gave


116°00'
115°56'
49°06' N
49°05' N
Y-12-81
215.5 m
Y-13-81
MT. MAHON
154.5 m
TOURMALINITE ZONE (PROJECTED)
YAHK LCP
ALDER LCP
A-7-
TOURM LCP
TOP LCP
YA
Y-11-81
105 m
100.3 m
0+00E
0+00N
A
A'
Y-10-81
79.5 m
LARCH LCP
STAN LCP
CHEV LCP
TNT LCP
PINE LCP
GEOCHEMICAL ANOMALIES
>20 PPM Pb
>150 PPM Zn
BOUGUER GRAVITY HIGH
0
1000 m
Chevron Canada Resources Limited
Minerals Staff
MOUNT MAHON
1983 GRID
GENERALIZED SOIL
GEOCHEMISTRY AND GRAVITY
FIGURE No. 11
PROJECT No. M525
DATE APR. 1984
REVISIONS
SCALE 1:23,600
NTS No 82G/4W
FILE No
COMPILED BY

a geometric mean of 16 ppm (Shacklette et al. 1971). Mean values for similar populations for sandstones and shales vary from 10 ppm to 21.6 ppm (Source: Handbook of Geochemistry). The 13 ppm Pb mean on the property is well within this range. Thus, values of 2 Standard Deviations and higher ($\geq$27 ppm Pb), even through low in absolute terms, should be taken seriously and deserve further field investigation.

The geochemical pattern of Cu is inconspicuous and spurious with numerous small anomalies being present. There is absolutely no correlation between Cu and either Pb or Zn. The origin of the Cu may be sought in the diorite intrusives that outcrop in a few places on the property and is commonly found as float.

7. GRAVITY

7.1 PROCEDURE

In the fall of 1983 a gravity survey was completed over the same grid used for the geochemical survey. Station intervals were at 100 meters on lines 200 meters apart. The two baselines were extended beyond the central portion of the grid to enable establishing regional response and background. Measurements were taken at 413 stations. Gravity obervations were made using a La Coste and Romberg Model G gravity meter.

7.2 RESULTS

A gravity high trends across the grid in a NNE-SSW direction, 200 to 400 meters W of baseline 0+00 E (Figs. 11 and 12). This feature can be explained

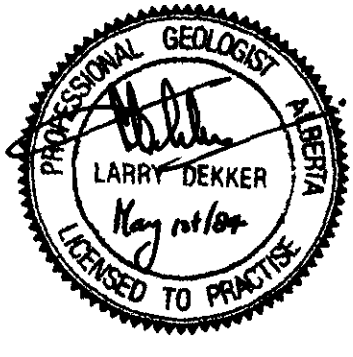
by possible changes in lithology (sill versus clastics) and/or topographic changes. If so, it does not seem to represent significant sulphide mineralization. It should be noted, though, that the elongate Pb/Zn geochemical anomalies in the central portion of the grid do to some degree coincide with this anomaly. Due to the lack of outcrop one can only guess at a possible explanation and drill testing is necessary to evaluate the significance of the anomaly.

In the northeastern portion of the grid a gravity low, indicative of stream sediments, can be observed at line 10 north, 200 east trending south along the existing stream. This low separates, and accentuates a gravity high on lines 8 and 10 north. Observation of gravity profiles at various different density factors indicates that this feature is not related to topography. The feature is not closed off to the northeast in the direction of the Cold Creek Valley where one would intuitively expect more alluvial valley fill of lesser density and thus a relatively negative gravity response.

No anomalous geochemical response was obtained in this area. This, however, could be attributed to possible significant overburden masking any possible sulphide mineralization. As the positive gravity feature is not closed off to the northeast, further expansion of the gravity coverage is needed to further define this gravity high. If it persists, a drill test is required to determine its nature. A complete and detailed report discussing the gravity survey is found in Pocket #10.

8. CONCLUSIONS

The geological mapping confirmed the presence and extent of at least four stratiform tourmalinite zones on the Mount Mahon property and, most likely, stratigraphic proximity to the Lower/Middle Aldridge contact, the productive level for Sullivan Type mineralization. The zones seem not to be laterally continuous but this is difficult to ascertain due to lack of outcrop. The geochemical work indicated the presence of two pronounced elongated anomalies near the central portion of the grid in proximity, and coincidental with, the sulphide mineralization in DDH YA-6. Thick overburden on the east portion of the grid may suppress anomalous Pb and Zn response and the negative results here should be viewed accordingly. The gravity survey shows two positive gravity anomalies, one of which roughly coincides with the anomalous geochemical patterns of Pb and Zn. This one is fairly weak and may be explained by lithology and/or topography variation or else, weak sulphide mineralization. The other positive gravity anomaly is present on the NE corner of the grid. This anomaly is roughly 500 m x 1000 m and is open to the northeast. There is no favourable geochemical response associated with this high. In view of the favourable geologic environment, this anomaly could reflect stratiform shale-hosted sulphide mineralization and its significance must be further tested.



L. Dekker

April 1984

REFERENCE

Ethier, V. G. and Campbell, F. A. 1977.

Tourmaline concentrations in Proterozoic sediments of the southern Cordillera of Canada and their economic significance. Can. J. Earth Sci. vol. 14, pp. 2348-2363.

APPENDIX I

EXPENDITURE STATEMENT

MAHON CLAIM GROUP
FORT STEELE MINING DIVISION

1) GEOLOGICAL MAPPING, PROSPECTING, CREW SUPERVISION, REPORT COMPILATION

Labour	Position	Period	Days	Amount
Larry Dekker	Sr. Geologist	8/8-22/12/83	74 @ $242/day	$17,908.00
A. Paul Schiarizza	Geologist	15/8-18/11/83	55 @ $120/day	6,600.00

2) GEOCHEMISTRY

Line Cutting (41.25 km) + soil and silt sampling (Bema Industries)	$37,168.00
Sample preparation and analysis - Pb, Zn, Cu. (Chemex Labs) (828 soils, 16 silts)	6,058.00

3) GRAVITY

413 Stations (Ager, Berretta, Ellis)	$25,650.00

4) OTHER EXPENSES

Travel (incl. truck), gas, etc.	$ 1,211.29
Camp Supplies	191.57
Equipment	823.10
Food and lodging (Ambleside Park, Yahk)	1,609.39
Drafting	4,003.00
Report Preparation	2,000.00
	$103,222.35
Add PAC	16,777.65
	$120,000.00

APPENDIX II

CHEVRON PERSONNEL EMPLOYED ON THE MAHON CLAIM GROUP

Larry Dekker,
850 Cardero Street,
Vancouver, B. C.
V6G 2G5

Paul Schiarizza,
c/o B.C. Ministry of Energy, Mines and Resources,
Geological Branch,
Mineral Resources Division,
Parliament Buildings,
Victoria, B. C.
V8V 1X4

APPENDIX III

STATEMENT OF QUALIFICATIONS

L. DEKKER

I, Larry Dekker, have worked as a geologist since graduation from the University of Amsterdam, the Netherlands, with a B.Sc. Degree in Geology (1965) and a M.Sc. Degree in Stratigraphy and Sedimentology (1969).

I am a licensee (P.Eng.) of the Association of Professional Engineers, Geologists and Geophysicists of the Province of Alberta, a Fellow of the Geological Association of Canada, a member of the American Association of Petroleum Geologists and a member of the Canadian Society of Petroleum Geologists.

I am currently employed as a senior geologist by Chevron Canada Resources Limited, 1900 - 1055 West Hastings Street, Vancouver, B. C., V6E 2E9 and have been with this company for 15 years.

The exploration program on the Mahon claim group was performed under my direction and supervision.

APPENDIX IV

STATEMENT OF QUALIFICATIONS

A. PAUL SCHIARIZZA

A. Paul Schiarizza holds a B.Sc. (Honours) Degree in Geology (1975) from Queen's University, Kingston, Ontario.

He has been employed as a research assistant at Queen's University (1974 and 1975), by Cominco (1978) and as a senior field assistant to Dr. V. A. Preto of the B.C. Ministry of Energy, Mines and Petroleum Resources (1978, 1979 and 1983). During the 1983 field season he worked as a senior field assistant for Chevron Canada Resources, Minerals Staff.

APPENDIX V

SOIL GEOCHEMICAL DATA WITH STATISTICAL ANALYSIS

CHEMEX LABS LTD.

212 BROOKSBANK AVE.
NORTH VANCOUVER, B.C.
CANADA V7J 2C1

TELEPHONE: (604) 984-0221
TELEX: 043-52597

• ANALYTICAL CHEMISTS • GEOCHEMISTS • REGISTERED ASSAYERS

CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-001-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L0+00N 0+50E	214	19	265	--	--	--	--
L0+00N 1+00E	214	36	285	--	--	--	--
L0+00N 1+50E	214	18	173	--	--	--	--
L0+00N 2+00E	214	14	190	--	--	--	--
L0+00N 2+50E	214	32	173	--	--	--	--
L0+00N 3+00E	214	20	118	--	--	--	--
L0+00N 3+50E	214	26	98	--	--	--	--
L0+00N 4+00E	214	18	50	--	--	--	--
L0+00N 4+50E	214	49	120	--	--	--	--
L0+00N 5+00E	214	34	110	--	--	--	--
L0+00N 5+50E	214	31	112	--	--	--	--
L0+00N 6+00E	214	22	95	--	--	--	--
L0+00N 6+50E	214	43	108	--	--	--	--
L0+00N 7+00E	214	30	105	--	--	--	--
L0+00N 7+50E	214	31	92	--	--	--	--
L0+00N 8+00E	214	26	65	--	--	--	--
L0+00N 8+50E	214	24	100	--	--	--	--
L0+00N 9+00E	214	25	115	--	--	--	--
L0+00N 9+50E	214	29	100	--	--	--	--
L0+00N 10+00E	214	14	60	--	--	--	--
L0+00N 10+50E	214	22	55	--	--	--	--
L0+00N 10+55E	214	48	68	--	--	--	--
L0+00N 11+00E	214	16	65	--	--	--	--
L0+00N 11+50E	214	23	100	--	--	--	--
L0+00N 12+00E	214	26	58	--	--	--	--
L0+00N 12+50E	214	24	73	--	--	--	--
L0+00N 13+00E	214	25	68	--	--	--	--
L0+00N 13+50E	214	31	80	--	--	--	--
L0+00N 14+00E	214	21	50	--	--	--	--
L0+00N 14+50E	214	31	63	--	--	--	--
L0+00N 15+00E	214	16	47	--	--	--	--
L0+00N 15+50E	214	23	38	--	--	--	--
L0+00N 16+00E	214	22	72	--	--	--	--
L0+00N 16+50E	214	24	57	--	--	--	--
L0+00N 17+00E	214	44	72	--	--	--	--
L0+00N 17+50E	214	19	55	--	--	--	--
L0+00N 18+00E	214	75	63	--	--	--	--
L0+00N 18+50E	214	61	38	--	--	--	--
L0+00N 19+00E	214	22	52	--	--	--	--
L0+00N 19+50E	214	95	52	--	--	--	--

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Certified by Hart Richler

CHEMEX LABS LTD.

212 BROOKSBANK AVE.
NORTH VANCOUVER, B.C.
CANADA V7J 2C1

TELEPHONE: (604) 984-0221
TELEX: 043-52597

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CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-002-A
INVOICE # : 18316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L0+00N 19+80E	214	28	62	--	--	--	--
L0+00N 20+00E	214	28	57	--	--	--	--
L0+00N 20+50E	214	26	57	--	--	--	--
L0+00N 21+00E	214	36	70	--	--	--	--
L0+00N 21+50E	214	29	60	--	--	--	--
L0+00N 22+00E	214	28	54	--	--	--	--
L0+00E 19+25N	214	21	51	--	--	--	--
L0+00N 0+50W	214	10	119	--	--	--	--
L0+00N 1+00W	214	10	102	--	--	--	--
L0+00N 1+50W	214	10	65	--	--	--	--
L0+00N 2+00W	214	15	178	--	--	--	--
L0+00N 2+50W	214	16	195	--	--	--	--
L0+00N 3+00W	214	19	92	--	--	--	--
L0+00N 3+50W	214	32	140	--	--	--	--
L0+00N 4+00W	214	32	130	--	--	--	--
L0+00N 4+50W	214	26	90	--	--	--	--
L0+00N 5+00W	214	37	128	--	--	--	--
L0+00N 5+50W	214	22	135	--	--	--	--
L0+00N 6+00W	214	33	140	--	--	--	--
L0+00N 6+50W	214	16	148	--	--	--	--
L0+00N 7+00W	214	18	100	--	--	--	--
L0+00N 7+50W	214	26	120	--	--	--	--
L0+00N 8+00W	214	21	55	--	--	--	--
L0+00N 8+50W	214	37	107	--	--	--	--
L0+00N 9+00W	214	32	120	--	--	--	--
L0+00N 9+50W	214	23	78	--	--	--	--
L0+00N 10+00W	214	19	72	--	--	--	--
L0+00N 10+50W	214	20	75	--	--	--	--
L0+00N 11+00W	214	15	110	--	--	--	--
L0+00N 11+50W	214	12	81	--	--	--	--
L0+00N 12+00W	214	24	86	--	--	--	--
L0+00N 12+50W	214	15	78	--	--	--	--
L0+00N 13+00W	214	14	82	--	--	--	--
L0+00N 13+50W	214	17	98	--	--	--	--
L0+00N 14+00W	214	30	230	--	--	--	--
L0+00N 14+50W	214	21	130	--	--	--	--
L0+00N 15+00W	214	23	95	--	--	--	--
L0+00N 15+50W	214	20	104	--	--	--	--
L0+00N 16+00W	214	20	96	--	--	--	--
L0+00N 16+50W	214	24	88	--	--	--	--

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TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

ATTN: LARRY DEKKER

CERT. # : A8316943-003-
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

Sample description	Prep code	Cu ppm	Zn ppm				
L0+00N 17+00W	214	14	57	--	--	--	--
L0+00N 17+50W	214	21	75	--	--	--	--
L0+00N 18+00W	214	16	66	--	--	--	--
L0+00N 18+50W	214	14	73	--	--	--	--
L0+00N 19+00W	214	15	72	--	--	--	--
L0+00N 19+50W	214	18	85	--	--	--	--
L0+00N 20+00W	214	13	80	--	--	--	--
L0+00N 20+50W	214	20	143	--	--	--	--
L0+00N 21+00W	214	15	57	--	--	--	--
L0+00N 21+50W	214	18	57	--	--	--	--
L0+00N 22+00W	214	30	75	--	--	--	--
L0+00N 22+50W	214	33	85	--	--	--	--
L0+00N 23+00W	214	19	75	--	--	--	--
L0+00N 23+50W	214	21	65	--	--	--	--
L0+00N 24+00W	214	16	68	--	--	--	--
L0+00N 24+50W	214	16	70	--	--	--	--
L0+00N 25+00W	214	10	63	--	--	--	--
L0+00N 25+50W	214	14	73	--	--	--	--
L0+00N 26+00W	214	19	132	--	--	--	--
L0+00N 26+50W	214	17	75	--	--	--	--
L0+00N 27+00W	214	22	70	--	--	--	--
0+00N 27+50W	214	12	62	--	--	--	--
L0+00N 28+00W	214	14	75	--	--	--	--
L2+00N 0+50E	214	16	159	--	--	--	--
L2+00N 1+00E	214	20	90	--	--	--	--
L2+00N 1+50E	214	28	110	--	--	--	--
L2+00N 2+00E	214	31	105	--	--	--	--
L2+00N 2+50E	214	28	97	--	--	--	--
L2+00N 3+00E	214	18	85	--	--	--	--
L2+00N 3+50E	214	23	82	--	--	--	--
L2+00N 4+00E	214	30	93	--	--	--	--
L2+00N 4+50E	214	12	60	--	--	--	--
L2+00N 5+00E	214	30	100	--	--	--	--
L2+00N 5+50E	214	28	93	--	--	--	--
L2+00N 6+00E	214	30	98	--	--	--	--
L2+00N 6+50E	214	31	168	--	--	--	--
L2+00N 7+00E	214	25	112	--	--	--	--
L2+00N 7+50E	214	18	44	--	--	--	--
L2+00N 8+00E	214	18	94	--	--	--	--
L2+00N 8+50E	214	26	142	--	--	--	--

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VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-004-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L2+00N 9+00E	214	25	103	--	--	--	--
L2+00N 9+22E	214	40	77	--	--	--	--
L2+00N 9+50E	214	18	63	--	--	--	--
L2+00N 10+00E	214	21	92	--	--	--	--
L2+00N 10+50E	214	23	88	--	--	--	--
L2+00N 11+00E	214	27	95	--	--	--	--
L2+00N 11+50E	214	24	80	--	--	--	--
L2+00N 12+00E	214	21	80	--	--	--	--
L2+00N 0+00W	214	20	193	--	--	--	--
L2+00N 0+50W	214	16	410	--	--	--	--
L2+00N 1+00W	214	14	215	--	--	--	--
L2+00N 1+50W	214	17	165	--	--	--	--
L2+00N 2+00W	214	17	180	--	--	--	--
L2+00N 2+50W	214	15	125	--	--	--	--
L2+00N 3+00W	214	15	200	--	--	--	--
L2+00N 3+50W	214	21	120	--	--	--	--
L2+00N 4+00W	214	18	114	--	--	--	--
L2+00N 4+50W	214	18	117	--	--	--	--
L2+00N 5+00W	214	18	160	--	--	--	--
L2+00N 5+50W	214	18	158	--	--	--	--
L2+00N 6+00W	214	28	155	--	--	--	--
L2+00N 6+50W	214	21	130	--	--	--	--
L2+00N 7+00W	214	50	108	--	--	--	--
L2+00N 7+50W	214	22	165	--	--	--	--
L2+00N 8+00W	214	29	95	--	--	--	--
L2+00N 8+50W	214	30	77	--	--	--	--
L2+00N 9+00W	214	31	57	--	--	--	--
L2+00N 9+50W	214	27	55	--	--	--	--
L2+00N 10+00W	214	16	82	--	--	--	--
L2+00N 10+50W	214	17	82	--	--	--	--
L2+00N 11+00W	214	26	105	--	--	--	--
L2+00N 11+50W	214	18	77	--	--	--	--
L2+00N 12+00W	214	19	72	--	--	--	--
L2+00N 12+50W	214	26	75	--	--	--	--
L2+00N 13+00W	214	24	79	--	--	--	--
L2+00N 13+50W	214	24	80	--	--	--	--
L2+00N 14+00W	214	30	90	--	--	--	--
L2+00N 14+50W	214	27	82	--	--	--	--
L2+00N 15+00W	214	21	72	--	--	--	--
L2+00N 15+50W	214	15	65	--	--	--	--

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V6E 2E9

CERT. # : A8316943-005-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L2+00N 16+00W	214	17	68	--	--	--	--
L2+00N 16+50W	214	22	70	--	--	--	--
L2+00N 17+00W	214	18	67	--	--	--	--
L2+00N 17+50W	214	26	78	--	--	--	--
L2+00N 18+00W	214	27	78	--	--	--	--
L2+00N 18+50W	214	20	74	--	--	--	--
L2+00S 0+00E	214	26	125	--	--	--	--
L2+00S 0+50E	214	10	190	--	--	--	--
L2+00S 1+00E	214	18	360	--	--	--	--
L2+00S 1+50E	214	22	155	--	--	--	--
L2+00S 2+00E	214	18	233	--	--	--	--
L2+00S 2+50E	214	23	225	--	--	--	--
L2+00S 3+00E	214	33	303	--	--	--	--
L2+00S 3+50E	214	24	235	--	--	--	--
L2+00S 4+00E	214	22	130	--	--	--	--
L2+00S 4+50E	214	40	138	--	--	--	--
L2+00S 5+00E	214	23	107	--	--	--	--
L2+00S 5+50E	214	31	112	--	--	--	--
L2+00S 6+00E	214	33	138	--	--	--	--
L2+00S 6+50E	214	29	152	--	--	--	--
L2+00S 7+00E	214	27	88	--	--	--	--
L2+00S 7+50E	214	25	78	--	--	--	--
L2+00S 8+00E	214	42	95	--	--	--	--
L2+00S 8+50E	214	27	78	--	--	--	--
L2+00S 9+00E	214	29	75	--	--	--	--
L2+00S 9+50E	214	28	92	--	--	--	--
L2+00S 10+00E	214	41	75	--	--	--	--
L2+00S 10+50E	214	17	53	--	--	--	--
L2+00S 11+00E	214	17	56	--	--	--	--
L2+00S 11+50E	214	20	36	--	--	--	--
L2+00S 12+00E	214	15	58	--	--	--	--
L2+00S 0+50W	214	14	150	--	--	--	--
L2+00S 1+00W	214	20	192	--	--	--	--
L2+00S 1+50W	214	29	183	--	--	--	--
L2+00S 1+80W	214	21	223	--	--	--	--
L2+00S 2+00W	214	21	124	--	--	--	--
L2+00S 2+50W	214	40	150	--	--	--	--
L2+00S 3+00W	214	18	115	--	--	--	--
L2+00S 3+50W	214	28	105	--	--	--	--
L2+00S 4+00W	214	12	77	--	--	--	--

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VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-006-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L2+00S 4+50W	214	21	130	--	--	--	--
L2+00S 5+00W	214	18	113	--	--	--	--
L2+00S 5+50W	214	25	75	--	--	--	--
L2+00S 6+00W	214	31	98	--	--	--	--
L2+00S 6+50W	214	31	143	--	--	--	--
L2+00S 7+00W	214	43	130	--	--	--	--
L2+00S 7+50W	214	29	142	--	--	--	--
L2+00S 8+00W	214	17	125	--	--	--	--
L2+00S 8+50W	214	29	130	--	--	--	--
L2+00S 9+00W	214	35	85	--	--	--	--
L2+00S 9+50W	214	37	76	--	--	--	--
L2+00S 10+00W	214	31	61	--	--	--	--
L2+00S 10+50W	214	32	120	--	--	--	--
L2+00S 11+00W	214	27	103	--	--	--	--
L2+00S 11+50W	214	19	58	--	--	--	--
L2+00S 12+00W	214	14	119	--	--	--	--
L2+00S 12+50W	214	22	100	--	--	--	--
L2+00S 13+00W	214	21	82	--	--	--	--
L2+00S 13+50W	214	15	72	--	--	--	--
L2+00S 14+00W	214	22	105	--	--	--	--
L2+00S 14+50W	214	51	100	--	--	--	--
L2+00S 15+00W	214	15	84	--	--	--	--
L2+00S 15+50W	214	20	93	--	--	--	--
L2+00S 16+00W	214	24	100	--	--	--	--
L2+00S 16+50W	214	22	96	--	--	--	--
L2+00S 17+00W	214	11	60	--	--	--	--
L2+00S 17+50W	214	13	66	--	--	--	--
L2+00S 18+00W	214	17	84	--	--	--	--
L4+00N 0+00E	214	19	75	--	--	--	--
L4+00N 0+50E	214	27	95	--	--	--	--
L4+00N 1+00E	214	31	108	--	--	--	--
L4+00N 1+50E	214	40	92	--	--	--	--
L4+00N 2+00E	214	32	92	--	--	--	--
L4+00N 2+50E	214	29	75	--	--	--	--
L4+00N 3+00E	214	58	95	--	--	--	--
L4+00N 3+50E	214	34	103	--	--	--	--
L4+00N 4+00E	214	34	130	--	--	--	--
L4+00N 4+50E	214	22	80	--	--	--	--
L4+00N 5+00E	214	27	102	--	--	--	--
L4+00N 5+50E	214	37	90	--	--	--	--

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TO : CHEVRON CANADA RESOURCES LTD.
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1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-007-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L4+00N 6+00E	214	22	90	--	--	--	--
L4+00N 6+50E	214	42	80	--	--	--	--
L4+00N 7+00E	214	18	90	--	--	--	--
L4+00N 7+50E	214	15	60	--	--	--	--
L4+00N 8+00E	214	22	115	--	--	--	--
L4+00N 8+50E	214	30	105	--	--	--	--
L4+00N 9+00E	214	22	113	--	--	--	--
L4+00N 9+50E	214	15	97	--	--	--	--
L4+00N 10+00E	214	19	112	--	--	--	--
L4+00N 10+50E	214	22	103	--	--	--	--
L4+00N 11+00E	214	32	93	--	--	--	--
L4+00N 11+50E	214	17	59	--	--	--	--
L4+00N 12+00E	214	23	57	--	--	--	--
L4+00N 0+50W	214	41	97	--	--	--	--
L4+00N 1+00W	214	28	103	--	--	--	--
L4+00N 1+50W	214	23	108	--	--	--	--
L4+00N 2+00W	214	30	170	--	--	--	--
L4+00N 2+50W	214	26	150	--	--	--	--
L4+00N 3+00W	214	18	165	--	--	--	--
L4+00N 3+50W	214	28	155	--	--	--	--
L4+00N 4+00W	214	75	82	--	--	--	--
L4+00N 4+50W	214	31	98	--	--	--	--
L4+00N 5+00W	214	37	100	--	--	--	--
L4+00N 5+50W	214	25	96	--	--	--	--
L4+00N 6+00W	214	24	118	--	--	--	--
L4+00N 6+50W	214	20	110	--	--	--	--
L4+00N 7+00W	214	21	108	--	--	--	--
L4+00N 7+50W	214	33	150	--	--	--	--
L4+00N 8+00W	214	18	125	--	--	--	--
L4+00N 8+50W	214	11	70	--	--	--	--
L4+00N 9+00W	214	18	56	--	--	--	--
L4+00N 9+50W	214	10	60	--	--	--	--
L4+00N 10+00W	214	23	80	--	--	--	--
L4+00N 10+50W	214	18	95	--	--	--	--
L4+00N 11+00W	214	18	72	--	--	--	--
L4+00N 11+50W	214	20	70	--	--	--	--
L4+00N 12+00W	214	20	67	--	--	--	--
L4+00N 12+50W	214	16	88	--	--	--	--
L4+00N 13+00W	214	23	105	--	--	--	--
L4+00N 13+50W	214	21	102	--	--	--	--

CTA MEMBER CANADIAN TESTING ASSOCIATION

Certified by Hart Bichler

CHEMEX LABS LTD.

212 BROOKSBANK AVE.
NORTH VANCOUVER, B.C.
CANADA V7J 2C1

TELEPHONE: (604) 984-0221
TELEX: 043-52597

• ANALYTICAL CHEMISTS • GEOCHEMISTS • REGISTERED ASSAYERS

CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

ATTN: LARRY DEKKER

CERT. # : A8316943-008-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

Sample description	Prep code	Cu ppm	Zn ppm				
L4+00N 14+00W	214	18	85	--	--	--	--
L4+00N 14+50W	214	18	120	--	--	--	--
L4+00N 15+00W	214	17	56	--	--	--	--
L4+00N 15+50W	214	20	69	--	--	--	--
L4+00N 16+00W	214	16	46	--	--	--	--
L4+00N 16+50W	214	15	52	--	--	--	--
L4+00N 17+00W	214	15	63	--	--	--	--
L4+00N 17+50W	214	22	68	--	--	--	--
L4+00N 18+00W	214	18	63	--	--	--	--
L4+00N 18+50W	214	17	62	--	--	--	--
L4+00N 19+00W	214	14	66	--	--	--	--
L4+00N 19+50W	214	17	80	--	--	--	--
L4+00N 20+00W	214	19	64	--	--	--	--
L4+00N 20+50W	214	16	77	--	--	--	--
L4+00N 21+00W	214	17	80	--	--	--	--
L4+00N 21+50W	214	22	57	--	--	--	--
L4+00N 22+00W	214	24	80	--	--	--	--
L4+00N 22+50W	214	21	65	--	--	--	--
L4+00N 23+00W	214	30	61	--	--	--	--
L4+00S 0+00E	214	20	165	--	--	--	--
L4+00S 0+50W	214	27	505	--	--	--	--
L4+00S 1+00W	214	19	225	--	--	--	--
L4+00S 1+50W	214	16	210	--	--	--	--
L4+00S 2+00W	214	15	84	--	--	--	--
L4+00S 2+50W	214	20	98	--	--	--	--
L4+00S 3+00W	214	28	210	--	--	--	--
L4+00S 3+50W	214	20	193	--	--	--	--
L4+00S 4+00WSILT	214	9	152	--	--	--	--
L4+00S 4+00W	214	14	223	--	--	--	--
L4+00S 4+50W	214	14	135	--	--	--	--
L4+00S 5+00W	214	13	145	--	--	--	--
L4+00S 5+50W	214	43	125	--	--	--	--
L4+00S 6+00W	214	17	120	--	--	--	--
L4+00S 6+50W	214	36	103	--	--	--	--
L4+00S 7+00W	214	38	70	--	--	--	--
L4+00S 7+50W	214	29	108	--	--	--	--
L4+00S 8+00W	214	21	68	--	--	--	--
L4+00S 8+50W	214	24	93	--	--	--	--
L4+00S 9+00W	214	17	82	--	--	--	--
L4+00S 9+50W	214	31	80	--	--	--	--

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212 BROOKSBANK AVE.
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CANADA V7J 2C1

TELEPHONE: (604) 984-0221
TELEX: 043-52597

• ANALYTICAL CHEMISTS • GEOCHEMISTS • REGISTERED ASSAYERS

CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-009-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L4+00S 10+00W	214	23	58	--	--	--	--
L4+00S 10+50W	214	17	135	--	--	--	--
L4+00S 11+00W	214	23	105	--	--	--	--
L4+00S 11+50W	214	28	115	--	--	--	--
L4+00S 12+00W	214	25	125	--	--	--	--
L4+00S 12+50W	214	23	77	--	--	--	--
L4+00S 13+00W	214	33	115	--	--	--	--
L4+00S 13+50W	214	25	110	--	--	--	--
L4+00S 14+00W	214	28	92	--	--	--	--
L4+00S 14+50W	214	20	75	--	--	--	--
L4+00S 15+00W	214	20	80	--	--	--	--
L4+00S 15+50W	214	21	79	--	--	--	--
L4+00S 16+00W	214	22	95	--	--	--	--
L4+00S 16+50W	214	18	88	--	--	--	--
L4+00S 17+00W	214	17	88	--	--	--	--
L4+00S 17+50W	214	15	75	--	--	--	--
L4+00S 18+00W	214	16	80	--	--	--	--
L6+00N 0+00E	214	35	185	--	--	--	--
L6+00N 0+50E	214	42	105	--	--	--	--
L6+00N 1+00E	214	17	60	--	--	--	--
L6+00N 1+50E	214	17	65	--	--	--	--
L6+00N 2+00E	214	24	67	--	--	--	--
L6+00N 2+50E	214	30	88	--	--	--	--
L6+00N 3+00E	214	29	103	--	--	--	--
L6+00N 3+50E	214	30	58	--	--	--	--
L6+00N 4+00E	214	80	117	--	--	--	--
L6+00N 4+10E	214	32	74	--	--	--	--
L6+00N 4+50E	214	21	66	--	--	--	--
L6+00N 5+00E	214	18	74	--	--	--	--
L6+00N 5+50E	214	23	70	--	--	--	--
L6+00N 6+00E	214	26	83	--	--	--	--
L6+00N 6+50E	214	45	140	--	--	--	--
L6+00N 7+00E	214	39	98	--	--	--	--
L6+00N 7+50E	214	45	98	--	--	--	--
L6+00N 8+00E	214	19	98	--	--	--	--
L6+00N 8+50E	214	22	85	--	--	--	--
L6+00N 9+00E	214	25	93	--	--	--	--
L6+00N 9+50E	214	17	120	--	--	--	--
L6+00N 10+00E	214	29	120	--	--	--	--
L6+00N 10+50E	214	21	92	--	--	--	--

Certified by Hart Bichler

CTA MEMBER CANADIAN TESTING ASSOCIATION

CHEMEX LABS LTD.

212 BROOKSBANK AVE.
NORTH VANCOUVER, B.C.
CANADA V7J 2C1

TELEPHONE: (604) 984-0221
TELEX: 043-52597

• ANALYTICAL CHEMISTS • GEOCHEMISTS • REGISTERED ASSAYERS

CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-011-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L8+00N 0+50E	214	24	64	--	--	--	--
L8+00N 1+00E	214	17	52	--	--	--	--
L8+00N 1+50E	214	13	56	--	--	--	--
L8+00N 2+00E	214	25	83	--	--	--	--
L8+00N 2+50E	214	18	81	--	--	--	--
L8+00N 2+59E	214	31	60	--	--	--	--
L8+00N 3+00E	214	14	52	--	--	--	--
L8+00N 3+50E	214	21	81	--	--	--	--
L8+00N 4+00E	214	18	75	--	--	--	--
L8+00N 4+50E	214	17	66	--	--	--	--
L8+00N 5+00E	214	23	75	--	--	--	--
L8+00N 5+50E	214	20	90	--	--	--	--
L8+00N 6+00E	214	33	76	--	--	--	--
L8+00N 6+50E	214	33	85	--	--	--	--
L8+00N 7+00E	214	26	70	--	--	--	--
L8+00N 7+50E	214	40	63	--	--	--	--
L8+00N 8+00E	214	46	66	--	--	--	--
L8+00N 8+50E	214	19	77	--	--	--	--
L8+00N 9+00E	214	29	89	--	--	--	--
L8+00N 9+50E	214	25	95	--	--	--	--
L8+00N 10+00E	214	20	84	--	--	--	--
L8+00N 10+50E	214	20	74	--	--	--	--
L8+00N 11+00E	214	20	64	--	--	--	--
L8+00N 11+50E	214	16	58	--	--	--	--
L8+00N 12+00E	214	37	120	--	--	--	--
L8+00N 0+50W	214	32	109	--	--	--	--
L8+00N 1+00W	214	25	58	--	--	--	--
L8+00N 1+50W	214	32	87	--	--	--	--
L8+00N 2+00W	214	57	95	--	--	--	--
L8+00N 2+50W	214	41	70	--	--	--	--
L8+00N 3+00W	214	52	82	--	--	--	--
L8+00N 3+50W	214	100	88	--	--	--	--
L8+00N 4+00W	214	25	53	--	--	--	--
L8+00N 4+50W	214	26	88	--	--	--	--
L8+00N 5+00W	214	23	60	--	--	--	--
L8+00N 5+50W	214	28	58	--	--	--	--
L8+00N 6+00W	214	33	56	--	--	--	--
L8+00N 6+50W	214	41	72	--	--	--	--
L8+00N 7+00W	214	26	75	--	--	--	--
L8+00N 7+50W	214	20	55	--	--	--	--

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TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-012-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L8+00N 8+00W	214	35	48	--	--	--	--
L8+00N 8+50W	214	22	110	--	--	--	--
L8+00N 9+00W	214	29	85	--	--	--	--
L8+00N 9+50W	214	17	68	--	--	--	--
L8+00N 10+00W	214	30	45	--	--	--	--
L8+00N 10+50W	214	22	68	--	--	--	--
L8+00N 11+00W	214	24	95	--	--	--	--
L8+00N 11+50W	214	22	72	--	--	--	--
L8+00N 12+00W	214	26	114	--	--	--	--
L8+00N 12+50W	214	27	85	--	--	--	--
L8+00N 13+00W	214	22	78	--	--	--	--
L8+00N 13+50W	214	15	72	--	--	--	--
L8+00N 14+00W	214	21	78	--	--	--	--
L8+00N 14+50W	214	17	62	--	--	--	--
L8+00N 15+00W	214	23	70	--	--	--	--
L8+00N 15+50W	214	20	75	--	--	--	--
L8+00N 16+00W	214	15	63	--	--	--	--
L8+00N 16+50W	214	16	66	--	--	--	--
L8+00N 17+00W	214	13	55	--	--	--	--
L8+00N 17+50W	214	14	57	--	--	--	--
L8+00N 18+00W	214	12	51	--	--	--	--
L10+00N 0+00E	214	26	73	--	--	--	--
L10+00N 0+35E	214	32	77	--	--	--	--
L10+00N 0+50E	214	16	40	--	--	--	--
L10+00N 0+71E	214	25	56	--	--	--	--
L10+00N 1+00E	214	13	80	--	--	--	--
L10+00N 1+50E	214	23	52	--	--	--	--
L10+00N 2+00E	214	13	43	--	--	--	--
L10+00N 2+50E	214	19	48	--	--	--	--
L10+00N 3+00E	214	18	84	--	--	--	--
L10+00N 3+50E	214	26	71	--	--	--	--
L10+00N 4+00E	214	48	115	--	--	--	--
L10+00N 4+50E	214	22	100	--	--	--	--
L10+00N 5+00E	214	55	85	--	--	--	--
L10+00N 5+50E	214	25	80	--	--	--	--
L10+00N 6+00E	214	49	80	--	--	--	--
L10+00N 6+50E	214	33	98	--	--	--	--
L10+00N 7+00E	214	29	90	--	--	--	--
L10+00N 7+50E	214	48	130	--	--	--	--
L10+00N 8+00E	214	33	98	--	--	--	--

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CANADA V7J 2C1

TELEPHONE: (604) 984-0221
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TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-013-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L10+00N 8+50E	214	25	89	--	--	--	--
L10+00N 9+00E	214	30	77	--	--	--	--
L10+00N 9+50E	214	25	85	--	--	--	--
L10+00N 10+00E	214	22	60	--	--	--	--
L10+00N 10+50E	214	20	65	--	--	--	--
L10+00N 11+00E	214	22	55	--	--	--	--
L10+00N 11+50E	214	16	53	--	--	--	--
L10+00N 12+00E	214	25	70	--	--	--	--
L10+00N 0+50W	214	36	100	--	--	--	--
L10+00N 1+00W	214	38	104	--	--	--	--
L10+00N 1+50W	214	22	83	--	--	--	--
L10+00N 2+00W	214	40	77	--	--	--	--
L10+00N 2+11W	214	18	53	--	--	--	--
L10+00N 2+50W	214	21	74	--	--	--	--
L10+00N 3+00W	214	25	79	--	--	--	--
L10+00N 3+50W	214	25	71	--	--	--	--
L10+00N 4+00W	214	45	90	--	--	--	--
L10+00N 4+50W	214	33	70	--	--	--	--
L10+00N 5+00W	214	42	52	--	--	--	--
L10+00N 5+50W	214	83	80	--	--	--	--
L10+00N 6+00W	214	24	73	--	--	--	--
L10+00N 6+50W	214	27	112	--	--	--	--
L10+00N 7+00W	214	19	74	--	--	--	--
L10+00N 7+50W	214	21	35	--	--	--	--
L10+00N 7+62.5W	214	48	52	--	--	--	--
L10+00N 8+00W	214	25	78	--	--	--	--
L10+00N 8+50W	214	54	77	--	--	--	--
L10+00N 9+00W	214	22	46	--	--	--	--
L10+00N 9+50W	214	23	44	--	--	--	--
L10+00N 10+00W	214	40	43	--	--	--	--
L10+00N 10+50W	214	35	60	--	--	--	--
L10+00N 11+00W	214	38	74	--	--	--	--
L10+00N 11+50W	214	28	64	--	--	--	--
L10+00N 12+00W	214	27	68	--	--	--	--
L10+00N 12+50W	214	24	72	--	--	--	--
L10+00N 13+00W	214	24	74	--	--	--	--
L10+00N 13+50W	214	15	44	--	--	--	--
L10+00N 14+00W	214	45	80	--	--	--	--
L10+00N 14+50W	214	26	54	--	--	--	--
L10+00N 14+93W	214	15	32	--	--	--	--

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TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

ATTN: LARRY DEKKER

CERT. # : A8316943-014-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

Sample description	Prep code	Cu ppm	Zn ppm				
L10+00N 15+00W	214	26	71	--	--	--	--
L10+00N 15+50W	214	21	77	--	--	--	--
L10+00N 16+00W	214	21	61	--	--	--	--
L10+00N 16+50W	214	12	46	--	--	--	--
L10+00N 17+00W	214	22	62	--	--	--	--
L10+00N 17+50W	214	21	72	--	--	--	--
L10+00N 18+00W	214	15	65	--	--	--	--
A	214	55	80	--	--	--	--
B	214	22	78	--	--	--	--
C	214	23	130	--	--	--	--
D	214	28	96	--	--	--	--
E	214	30	102	--	--	--	--
F	214	17	76	--	--	--	--
G	214	13	83	--	--	--	--
H	214	52	130	--	--	--	--
#LD83-135	214	26	68	--	--	--	--
LON STN 22+50E	214	27	60	--	--	--	--
LON STN 23+00E	214	22	60	--	--	--	--
LON STN 23+50E	214	24	51	--	--	--	--
LON STN 24+00E	214	21	55	--	--	--	--
LON STN 24+50E	214	44	40	--	--	--	--
LON STN 25+00E	214	18	69	--	--	--	--
LON STN 25+50E	214	15	53	--	--	--	--
LON STN 26+00E	214	17	54	--	--	--	--
LON STN 26+50E	214	14	60	--	--	--	--
LON STN 27+00E	214	25	74	--	--	--	--
LON STN 27+50E	214	16	50	--	--	--	--
LON STN 28+00E	214	20	64	--	--	--	--
LON STN 28+50E	214	21	58	--	--	--	--
LON STN 29+00E	214	9	57	--	--	--	--
LON STN 29+50E	214	15	67	--	--	--	--
LON STN 30+00E	214	22	98	--	--	--	--
LON STN 30+50E	214	25	82	--	--	--	--
LON STN 31+00E	214	14	81	--	--	--	--
LON STN 31+50E	214	28	93	--	--	--	--
OE STN 0+50N	214	15	385	--	--	--	--
OE STN 1+00N	214	21	238	--	--	--	--
OE STN 1+50N	214	17	320	--	--	--	--
OE STN 2+50N	214	27	170	--	--	--	--
OE STN 3+00N	214	28	149	--	--	--	--

Certified by Hart Bichler

CHEMEX LABS LTD.

212 BROOKSBANK AVE.
NORTH VANCOUVER, B.C.
CANADA V7J 2C1

TELEPHONE: (604) 984-0221
TELEX: 043-52597

• ANALYTICAL CHEMISTS • GEOCHEMISTS • REGISTERED ASSAYERS

CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-015-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
OE STN 3+50N	214	26	180	--	--	--	--
OE STN 4+50N	214	53	118	--	--	--	--
OE STN 5+00N	214	28	92	--	--	--	--
OE STN 5+50N	214	23	137	--	--	--	--
OE STN 6+50N	214	17	57	--	--	--	--
OE STN 7+00N	214	22	147	--	--	--	--
OE STN 7+50N	214	24	90	--	--	--	--
OE STN 8+50N	214	25	110	--	--	--	--
OE STN 9+00N	214	26	136	--	--	--	--
OE STN 9+50N	214	42	134	--	--	--	--
OE STN 10+50N	214	23	54	--	--	--	--
OE STN 11+00N	214	51	112	--	--	--	--
OE STN 11+50N	214	21	90	--	--	--	--
OE STN 12+00N	214	16	60	--	--	--	--
OE STN 12+50N	214	24	90	--	--	--	--
OE STN 13+00N	214	27	82	--	--	--	--
OE STN 13+50N	214	27	66	--	--	--	--
OE STN 14+00N	214	24	95	--	--	--	--
OE STN 14+50N	214	18	120	--	--	--	--
OE STN 15+00N	214	30	123	--	--	--	--
OE STN 15+50N	214	13	57	--	--	--	--
OE STN 16+00N	214	34	105	--	--	--	--
OE STN 16+50N	214	80	68	--	--	--	--
OE STN 17+00N	214	43	80	--	--	--	--
OE STN 17+50N	214	22	74	--	--	--	--
OE STN 18+00N	214	24	50	--	--	--	--
OE STN 18+50N	214	28	66	--	--	--	--
OE STN 19+00N	214	18	90	--	--	--	--
OE STN 19+50N	214	30	70	--	--	--	--
OE STN 20+00N	214	18	70	--	--	--	--
OE STN 20+50N	214	15	85	--	--	--	--
OE STN 21+00N	214	24	50	--	--	--	--
OE STN 21+50N	214	20	110	--	--	--	--
OE STN 22+00N	214	34	92	--	--	--	--
OE STN 22+50N	214	21	50	--	--	--	--
OE STN 23+00N	214	40	99	--	--	--	--
OE STN 23+50N	214	25	66	--	--	--	--
OE STN 24+00N	214	23	91	--	--	--	--
OE STN 24+50N	214	26	86	--	--	--	--
OE STN 25+00N	214	36	97	--	--	--	--

Certified by Stewart Buchler

CHEMEX LABS LTD.

212 BROOKSBANK AVE.
NORTH VANCOUVER, B.C.
CANADA V7J 2C1

TELEPHONE: (604) 984-0221
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CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-016-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
OE STN 0+50S	214	26	224	--	--	--	--
OE STN 1+00S	214	37	270	--	--	--	--
OE STN 1+50S	214	15	140	--	--	--	--
OE STN 2+00S	214	19	138	--	--	--	--
OE STN 2+50S	214	26	124	--	--	--	--
OE STN 3+00S	214	18	82	--	--	--	--
OE STN 3+50S	214	24	150	--	--	--	--
OE STN 4+00S	214	20	158	--	--	--	--
OE STN 4+50S	214	24	95	--	--	--	--
OE STN 5+00S	214	28	140	--	--	--	--
OE STN 5+50S	214	24	133	--	--	--	--
OE STN 6+00S	214	40	98	--	--	--	--
OE STN 6+50S	214	25	68	--	--	--	--
OE STN 7+00S	214	20	54	--	--	--	--
OE STN 7+50S	214	26	78	--	--	--	--
OE STN 8+00S	214	22	75	--	--	--	--
OE STN 8+50S	214	60	115	--	--	--	--
OE STN 9+00S	214	37	145	--	--	--	--
OE STN 9+50S	214	30	100	--	--	--	--
OE STN 10+00S	214	23	90	--	--	--	--
OE STN 10+50S	214	32	120	--	--	--	--
OE STN 11+00S	214	18	50	--	--	--	--
OE STN 11+50S	214	17	93	--	--	--	--
OE STN 12+00S	214	38	150	--	--	--	--
OE STN 12+50S	214	23	260	--	--	--	--
OE STN 13+00S	214	47	190	--	--	--	--
OE STN 13+50S	214	35	175	--	--	--	--
OE STN 14+00S	214	21	118	--	--	--	--
OE STN 14+50S	214	21	93	--	--	--	--
OE STN 15+00S	214	28	80	--	--	--	--
OE STN 15+50S	214	25	123	--	--	--	--
OE STN 16+00S	214	23	28	--	--	--	--
OE STN 16+50S	214	25	90	--	--	--	--
OE STN 17+00S	214	25	134	--	--	--	--
OE STN 17+50S	214	23	125	--	--	--	--
OE STN 18+00S	214	35	115	--	--	--	--
OE STN 18+50S	214	28	155	--	--	--	--
OE STN 19+00S	214	38	155	--	--	--	--
OE STN 19+50S	214	37	135	--	--	--	--
OE STN 20+00S	214	23	125	--	--	--	--

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TO : CHEVRON CANADA RESOURCES LTD.
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1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-017-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L0E STN 5+92S	214	22	80	--	--	--	--
L4S STN 0+50E	214	24	110	--	--	--	--
L4S STN 1+00E	214	24	103	--	--	--	--
L4S STN 1+50E	214	43	136	--	--	--	--
L4S STN 2+00E	214	24	105	--	--	--	--
L4S STN 2+50E	214	22	170	--	--	--	--
L4S STN 3+00E	214	28	106	--	--	--	--
L4S STN 3+50E	214	28	92	--	--	--	--
L4S STN 4+00E	214	26	96	--	--	--	--
L4S STN 4+50E	214	28	94	--	--	--	--
L4S STN 5+00E	214	24	140	--	--	--	--
L4S STN 5+50E	214	24	82	--	--	--	--
L4S STN 6+00E	214	27	105	--	--	--	--
L4S STN 6+50E	214	27	79	--	--	--	--
L4S STN 7+00E	214	30	78	--	--	--	--
L4S STN 7+50E	214	24	76	--	--	--	--
L4S STN 8+00E	214	26	78	--	--	--	--
L4S STN 8+50E	214	29	80	--	--	--	--
L4S STN 9+00E	214	33	62	--	--	--	--
L4S STN 9+50E	214	27	68	--	--	--	--
L4S STN 10+00E	214	30	72	--	--	--	--
L4S STN 10+50E	214	35	50	--	--	--	--
L4S STN 11+00E	214	26	52	--	--	--	--
L4S STN 11+50E	214	28	60	--	--	--	--
L4S STN 12+00E	214	24	155	--	--	--	--
L6S STN 0+50E	214	26	87	--	--	--	--
L6S STN 1+00E	214	38	80	--	--	--	--
L6S STN 1+50E	214	26	68	--	--	--	--
L6S STN 2+00E	214	25	78	--	--	--	--
L6S STN 2+50E	214	35	85	--	--	--	--
L6S STN 3+00E	214	23	90	--	--	--	--
L6S STN 3+50E	214	35	163	--	--	--	--
L6S STN 4+00E	214	33	76	--	--	--	--
L6S STN 4+50E	214	27	79	--	--	--	--
L6S STN 5+00E	214	42	90	--	--	--	--
L6S STN 5+50E	214	55	80	--	--	--	--
L6S STN 6+00E	214	32	102	--	--	--	--
L6S STN 6+50E	214	34	88	--	--	--	--
L6S STN 7+00E	214	22	95	--	--	--	--
L6S STN 7+50E	214	32	80	--	--	--	--

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CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-018-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L6S STN 8+00E	214	19	104	--	--	--	--
L6S STN 8+50E	214	25	79	--	--	--	--
L6S STN 9+00E	214	52	107	--	--	--	--
L6S STN 9+50E	214	32	87	--	--	--	--
L6S STN 10+00E	214	47	77	--	--	--	--
L6S STN 10+50E	214	25	59	--	--	--	--
L6S STN 11+00E	214	34	71	--	--	--	--
L6S STN 11+50E	214	29	67	--	--	--	--
L6S STN 12+00E	214	33	71	--	--	--	--
L6S STN 0+50W	214	22	85	--	--	--	--
L6S STN 1+00W	214	25	125	--	--	--	--
L6S STN 1+50W	214	17	68	--	--	--	--
L6S STN 2+00W	214	21	100	--	--	--	--
L6S STN 2+50W	214	23	120	--	--	--	--
L6S STN 3+00W	214	23	65	--	--	--	--
L6S STN 3+50W	214	25	135	--	--	--	--
L6S STN 4+00W	214	23	117	--	--	--	--
L6S STN 4+50W	214	19	70	--	--	--	--
L6S STN 5+00W	214	20	200	--	--	--	--
L6S STN 5+50W	214	50	109	--	--	--	--
L6S STN 6+00W	214	22	95	--	--	--	--
L6S STN 6+50W	214	24	85	--	--	--	--
L6S STN 7+00W	214	38	96	--	--	--	--
L6S STN 7+50W	214	42	110	--	--	--	--
L6S STN 8+00W	214	45	88	--	--	--	--
L6S STN 8+50W	214	65	103	--	--	--	--
L6S STN 9+00W	214	48	86	--	--	--	--
L6S STN 9+50W	214	37	125	--	--	--	--
L6S STN 10+00W	214	33	96	--	--	--	--
L6S STN 10+50W	214	40	105	--	--	--	--
L6S STN 11+00W	214	40	115	--	--	--	--
L6S STN 11+50W	214	28	128	--	--	--	--
L6S STN 12+00W	214	33	130	--	--	--	--
L6S STN 12+50W	214	25	105	--	--	--	--
L6S STN 13+00W	214	21	130	--	--	--	--
L6S STN 13+50W	214	23	106	--	--	--	--
L6S STN 14+00W	214	20	140	--	--	--	--
L6S STN 14+50W	214	17	70	--	--	--	--
L6S STN 15+00W	214	21	80	--	--	--	--
L6S STN 15+50W	214	22	89	--	--	--	--

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TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

ATTN: LARRY DEKKER

CERT. # : A8316943-019-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

Sample description	Prep code	Cu ppm	Zn ppm				
L6S STN 16+00W	214	21	82	--	--	--	--
L6S STN 16+50W	214	22	80	--	--	--	--
L6S STN 17+00W	214	19	64	--	--	--	--
L6S STN 17+50W	214	20	83	--	--	--	--
L6S STN 18+00W	214	24	70	--	--	--	--
L8S STN 0+50E	214	45	93	--	--	--	--
L8S STN 1+00E	214	19	63	--	--	--	--
L8S STN 1+50E	214	15	50	--	--	--	--
L8S STN 2+00E	214	18	63	--	--	--	--
L8S STN 2+50E	214	32	100	--	--	--	--
L8S STN 3+00E	214	23	74	--	--	--	--
L8S STN 3+50E	214	42	138	--	--	--	--
L8S STN 4+00E	214	22	100	--	--	--	--
L8S STN 4+50E	214	41	100	--	--	--	--
L8S STN 5+00E	214	90	100	--	--	--	--
L8S STN 5+50E	214	22	65	--	--	--	--
L8S STN 6+00E	214	28	62	--	--	--	--
L8S STN 6+50E	214	36	70	--	--	--	--
L8S STN 7+00E	214	32	73	--	--	--	--
L8S STN 7+50E	214	28	100	--	--	--	--
L8S STN 8+00E	214	29	74	--	--	--	--
L8S STN 8+50E	214	20	72	--	--	--	--
L8S STN 9+00E	214	19	54	--	--	--	--
L8S STN 9+50E	214	18	52	--	--	--	--
L8S STN 10+00E	214	21	64	--	--	--	--
L8S STN 10+50E	214	23	80	--	--	--	--
L8S STN 11+00E	214	25	81	--	--	--	--
L8S STN 11+50E	214	18	83	--	--	--	--
L8S STN 12+00E	214	22	73	--	--	--	--
L8S STN 3+04E	214	30	95	--	--	--	--
L8S STN 0+50W	214	21	72	--	--	--	--
L8S STN 1+00W	214	25	79	--	--	--	--
L8S STN 1+50W	214	21	62	--	--	--	--
L8S STN 2+00W	214	18	63	--	--	--	--
L8S STN 2+50W	214	25	90	--	--	--	--
L8S STN 3+00W	214	31	87	--	--	--	--
L8S STN 3+50W	214	22	82	--	--	--	--
L8S STN 4+00W	214	45	120	--	--	--	--
L8S STN 4+50W	214	66	190	--	--	--	--
L8S STN 5+00W	214	42	140	--	--	--	--

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TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-020-A
INVOICE # : 18316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L8S STN 5+50W	214	43	131	--	--	--	--
L8S STN 6+00W	214	42	118	--	--	--	--
L8S STN 6+50W	214	23	72	--	--	--	--
L8S STN 7+00W	214	44	155	--	--	--	--
L8S STN 7+50W	214	27	68	--	--	--	--
L8S STN 8+00W	214	42	140	--	--	--	--
L8S STN 8+50W	214	45	104	--	--	--	--
L8S STN 9+00W	214	32	113	--	--	--	--
L8S STN 9+50W	214	41	96	--	--	--	--
L8S STN 10+00W	214	61	115	--	--	--	--
L8S STN 10+50W	214	58	120	--	--	--	--
L8S STN 11+00W	214	44	134	--	--	--	--
L8S STN 11+50W	214	32	105	--	--	--	--
L8S STN 12+00W	214	33	92	--	--	--	--
L8S STN 12+50W	214	21	57	--	--	--	--
L8S STN 13+00W	214	22	106	--	--	--	--
L8S STN 13+50W	214	25	108	--	--	--	--
L8S STN 14+00W	214	14	91	--	--	--	--
L8S STN 14+50W	214	21	98	--	--	--	--
L8S STN 15+00W	214	21	82	--	--	--	--
L8S STN 15+50W	214	22	80	--	--	--	--
L8S STN 16+00W	214	19	82	--	--	--	--
L8S STN 16+50W	214	19	71	--	--	--	--
L8S STN 17+00W	214	17	51	--	--	--	--
L8S STN 17+50W	214	19	74	--	--	--	--
L8S STN 18+00W	214	18	78	--	--	--	--
L10S STN 0+50E	214	32	90	--	--	--	--
L10S STN 1+00E	214	19	67	--	--	--	--
L10S STN 1+50E	214	34	100	--	--	--	--
L10S STN 2+00E	214	28	88	--	--	--	--
L10S STN 2+50E	214	35	98	--	--	--	--
L10S STN 3+00E	214	25	58	--	--	--	--
L10S STN 3+50E	214	36	115	--	--	--	--
L10S STN 4+00E	214	28	84	--	--	--	--
L10S STN 4+50E	214	49	119	--	--	--	--
L10S STN 5+00E	214	22	138	--	--	--	--
L10S STN 5+50E	214	25	90	--	--	--	--
L10S STN 6+00E	214	45	82	--	--	--	--
L10S STN 6+50E	214	28	77	--	--	--	--
L10S STN 7+00E	214	63	91	--	--	--	--

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TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

ATTN: LARRY DEKKER

CERT. # : A8316943-021-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

Sample description	Prep code	Cu ppm	Zn ppm				
L10S STN 7+50E	214	20	74	--	--	--	--
L10S STN 8+00E	214	23	68	--	--	--	--
L10S STN 8+50E	214	22	66	--	--	--	--
L10S STN 9+00E	214	50	107	--	--	--	--
L10S STN 9+50E	214	21	106	--	--	--	--
L10S STN 10+00E	214	35	60	--	--	--	--
L10S STN 10+50E	214	20	90	--	--	--	--
L10S STN 11+00E	214	32	60	--	--	--	--
L10S STN 11+50E	214	23	69	--	--	--	--
L10S STN 12+00E	214	31	80	--	--	--	--
L10S STN 5+32E	214	25	28	--	--	--	--
L10S STN 0+50W	214	22	71	--	--	--	--
L10S STN 1+00W	214	21	70	--	--	--	--
L10S STN 1+50W	214	72	170	--	--	--	--
L10S STN 2+00W	214	40	128	--	--	--	--
L10S STN 2+50W	214	28	85	--	--	--	--
L10S STN 3+00W	214	25	105	--	--	--	--
L10S STN 3+50W	214	35	146	--	--	--	--
L10S STN 4+00W	214	27	98	--	--	--	--
L10S STN 4+50W	214	37	116	--	--	--	--
L10S STN 5+00W	214	17	71	--	--	--	--
L10S STN 5+50W	214	19	77	--	--	--	--
L10S STN 6+00W	214	43	115	--	--	--	--
L10S STN 6+50W	214	20	60	--	--	--	--
L10S STN 7+00W	214	30	123	--	--	--	--
L10S STN 7+50W	214	20	70	--	--	--	--
L10S STN 8+00W	214	49	140	--	--	--	--
L10S STN 8+50W	214	45	119	--	--	--	--
L10S STN 9+00W	214	41	150	--	--	--	--
L10S STN 9+50W	214	34	110	--	--	--	--
L10S STN 10+00W	214	17	52	--	--	--	--
L10S STN 10+50W	214	33	99	--	--	--	--
L10S STN 11+00W	214	34	150	--	--	--	--
L10S STN 11+50W	214	34	130	--	--	--	--
L10S STN 12+00W	214	22	132	--	--	--	--
L10S STN 12+50W	214	22	130	--	--	--	--
L10S STN 13+00W	214	22	87	--	--	--	--
L10S STN 13+50W	214	22	80	--	--	--	--
L10S STN 14+00W	214	20	53	--	--	--	--
L10S STN 14+50W	214	17	50	--	--	--	--

Certified by Hart Bichler

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NORTH VANCOUVER, B.C.
CANADA V7J 2C1

TELEPHONE: (604) 984-0221
TELEX: 043-52597

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CERTIFICATE OF ANALYSIS

TO : CHEVRON CANADA RESOURCES LTD.
MINERALS STAFF
1900 - 1055 W. HASTINGS ST.
VANCOUVER, B.C.
V6E 2E9

CERT. # : A8316943-022-A
INVOICE # : I8316943
DATE : 23-DEC-83
P.O. # : NONE
M525

ATTN: LARRY DEKKER

Sample description	Prep code	Cu ppm	Zn ppm				
L10S STN 15+00W	214	17	66	--	--	--	--
L10S STN 15+50W	214	28	46	--	--	--	--
L10S STN 16+00W	214	19	80	--	--	--	--
L10S STN 16+50W	214	19	67	--	--	--	--
L10S STN 17+00W	214	25	63	--	--	--	--
L10S STN 17+50W	214	33	55	--	--	--	--
L10S STN 18+00W	214	25	74	--	--	--	--
L10S STN 18+50W	214	21	55	--	--	--	--
L10S STN 19+00W	214	50	90	--	--	--	--
L10S STN 19+50W	214	22	72	--	--	--	--
L10S STN 20+00W	214	37	90	--	--	--	--

Certified by Hart Bichler

CTA MEMBER CANADIAN TESTING ASSOCIATION

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L0+00N 0+50E	19	84	265		******)+ 2 std dev.	******)+ 2 std dev.
L0+00N 1+00E	36	75	285		******)+ 2 std dev.	******)+ 2 std dev.
L0+00N 1+50E	18	11	173			** + 1 std dev.
L0+00N 2+00E	14	10	190	** - 1 std dev.		**** + 2 std dev.
L0+00N 2+50E	32	14	173			** + 1 std dev.
L0+00N 3+00E	20	9	118			
L0+00N 3+50E	26	9	98			
L0+00N 4+00E	18	6	50			** - 1 std dev.
L0+00N 4+50E	49	15	120	**** + 2 std dev.		
L0+00N 5+00E	34	14	110			
L0+00N 5+50E	31	14	112			
L0+00N 6+00E	22	10	95			
L0+00N 6+50E	43	14	100	** + 1 std dev.		
L0+00N 7+00E	30	14	105			
L0+00N 7+50E	31	12	92			
L0+00N 8+00E	26	12	65			
L0+00N 8+50E	24	12	100			
L0+00N 9+00E	25	12	115			
L0+00N 9+50E	29	11	100			
L0+00N 10+00E	14	7	60	** - 1 std dev.		
L0+00N 10+50E	22	9	55			
L0+00N 10+55E	48	17	68	** + 1 std dev.		
L0+00N 11+00E	16	6	65			
L0+00N 11+50E	23	10	100			
L0+00N 12+00E	26	8	58			
L0+00N 12+50E	24	7	73			
L0+00N 13+00E	25	9	68			
L0+00N 13+50E	31	8	80			
L0+00N 14+00E	21	6	50			** - 1 std dev.
L0+00N 14+50E	31	9	63			
L0+00N 15+00E	16	7	47			** - 1 std dev.
L0+00N 15+50E	23	6	38			** - 1 std dev.
L0+00N 16+00E	22	8	72			
L0+00N 16+50E	24	7	57			
L0+00N 17+00E	44	10	72	** + 1 std dev.		
L0+00N 17+50E	19	8	55			
L0+00N 18+00E	75	10	63	******)+ 2 std dev.		
L0+00N 18+50E	61	9	38	******)+ 2 std dev.		** - 1 std dev.
L0+00N 19+00E	22	6	52			
L0+00N 19+50E	95	10	52	******)+ 2 std dev.		
L0+00N 20+00E	28	11	57			
L0+00N 20+50E	26	12	57			
L0+00N 21+00E	36	15	70			
L0+00N 21+50E	29	10	60			
L0+00N 22+00E	28	12	54			
L0+00N 0+50W	10	10	119	** - 1 std dev.		
L0+00N 1+00W	10	16	102	** - 1 std dev.		
L0+00N 1+50W	10	8	65	** - 1 std dev.		
L0+00N 2+00W	15	10	178	** - 1 std dev.		** + 1 std dev.
L0+00N 2+50W	16	18	195			**** + 2 std dev.
L0+00N 3+00W	19	12	92			

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu		Pb		Zn	
L0+00N 3+50W	32	36	140			******	)+ 2 std dev.		
L0+00N 4+00W	32	36	130			******	)+ 2 std dev.		
L0+00N 4+50W	26	22	90			**	+ 1 std dev.		
L0+00N 5+00W	37	30	128			****	+ 2 std dev.		
L0+00N 5+50W	22	19	135						
L0+00N 6+00W	33	21	140			**	+ 1 std dev.		
L0+00N 6+50W	16	10	148					**	+ 1 std dev.
L0+00N 7+00W	18	19	100						
L0+00N 7+50W	26	20	120						
L0+00N 8+00W	21	12	55						
L0+00N 8+50W	37	22	107			**	+ 1 std dev.		
L0+00N 9+00W	32	20	120						
L0+00N 9+50W	23	13	78						
L0+00N 10+00W	19	9	72						
L0+00N 10+50W	20	12	75						
L0+00N 11+00W	15	18	110	**	- 1 std dev.				
L0+00N 11+50W	12	23	81	**	- 1 std dev.	**	+ 1 std dev.		
L0+00N 12+00W	24	14	86						
L0+00N 12+50W	15	11	78	**	- 1 std dev.				
L0+00N 13+00W	14	11	82	**	- 1 std dev.				
L0+00N 13+50W	17	13	98						
L0+00N 14+00W	30	15	230					******	)+ 2 std dev.
L0+00N 14+50W	21	17	130						
L0+00N 15+00W	23	17	95						
L0+00N 15+50W	20	16	104						
L0+00N 16+00W	20	17	96						
L0+00N 16+50W	24	13	88						
L0+00N 17+00W	14	11	57	**	- 1 std dev.				
L0+00N 17+50W	21	12	75						
L0+00N 18+00W	16	14	66						
L0+00N 18+50W	14	13	73	**	- 1 std dev.				
L0+00N 19+00W	15	12	72	**	- 1 std dev.				
L0+00N 19+50W	18	11	85						
L0+00N 20+00W	13	18	80	**	- 1 std dev.				
L0+00N 20+50W	20	16	143					**	+ 1 std dev.
L0+00N 21+00W	15	11	57	**	- 1 std dev.				
L0+00N 21+50W	18	9	57						
L0+00N 22+00W	30	23	75			**	+ 1 std dev.		
L0+00N 22+50W	33	16	85						
L0+00N 23+00W	19	10	75						
L0+00N 23+50W	21	11	65						
L0+00N 24+00W	16	12	68						
L0+00N 24+50W	16	13	70						
L0+00N 25+00W	10	14	63	**	- 1 std dev.				
L0+00N 25+50W	14	10	73	**	- 1 std dev.				
L0+00N 26+00W	19	29	132			****	+ 2 std dev.		
L0+00N 26+50W	17	11	75						
L0+00N 27+00W	22	20	70						
L0+00N 27+50W	12	12	62	**	- 1 std dev.				
L0+00N 28+00W	14	12	75	**	- 1 std dev.				
L2+00N 0+50E	16	8	159					**	+ 1 std dev.

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L2+00N 1+00E	20	10	90			
L2+00N 1+50E	28	13	110			
L2+00N 2+00E	31	15	105			
L2+00N 2+50E	28	14	97			
L2+00N 3+00E	18	8	85			
L2+00N 3+50E	23	10	82			
L2+00N 4+00E	30	11	93			
L2+00N 4+50E	12	7	60	** - 1 std dev.		
L2+00N 5+00E	30	11	100			
L2+00N 5+50E	28	10	93			
L2+00N 6+00E	30	11	98			
L2+00N 6+50E	31	12	168			** + 1 std dev.
L2+00N 7+00E	25	12	112			
L2+00N 7+50E	18	6	44			** - 1 std dev.
L2+00N 8+00E	18	8	94			
L2+00N 8+50E	26	9	142			** + 1 std dev.
L2+00N 9+00E	25	8	103			
L2+00N 9+50E	18	7	63			
L2+00N 10+00E	21	8	92			
L2+00N 10+50E	23	10	88			
L2+00N 11+00E	27	11	95			
L2+00N 11+50E	24	10	80			
L2+00N 12+00E	21	11	80			
L2+00N 0+00W	20	20	193			**** + 2 std dev.
L2+00N 0+50W	16	29	410		**** + 2 std dev.	******)+ 2 std dev.
L2+00N 1+00W	14	12	215	** - 1 std dev.		**** + 2 std dev.
L2+00N 1+50W	17	14	165			** + 1 std dev.
L2+00N 2+00W	17	12	180			** + 1 std dev.
L2+00N 2+50W	15	11	125	** - 1 std dev.		
L2+00N 3+00W	15	11	200	** - 1 std dev.		**** + 2 std dev.
L2+00N 3+50W	21	16	120			
L2+00N 4+00W	18	8	114			
L2+00N 4+50W	18	12	117			
L2+00N 5+00W	18	11	160			** + 1 std dev.
L2+00N 5+50W	18	8	158			** + 1 std dev.
L2+00N 6+00W	28	26	155		** + 1 std dev.	** + 1 std dev.
L2+00N 6+50W	21	18	130			
L2+00N 7+00W	50	53	188	**** + 2 std dev.	******)+ 2 std dev.	
L2+00N 7+50W	22	13	165			** + 1 std dev.
L2+00N 8+00W	29	10	95			
L2+00N 8+50W	30	9	77			
L2+00N 9+00W	31	11	57			
L2+00N 9+50W	27	10	55			
L2+00N 10+00W	16	8	82			
L2+00N 10+50W	17	10	82			
L2+00N 11+00W	26	10	105			
L2+00N 11+50W	18	13	77			
L2+00N 12+00W	19	10	72			
L2+00N 12+50W	26	11	75			
L2+00N 13+00W	24	13	79			
L2+00N 13+50W	24	13	80			

Samole description	Cu ppm	Pb ppm	Zn ppm		Cu		Pb		Zn
L2+00N 14+00W	30	14	90						
L2+00N 14+50W	27	14	82						
L2+00N 15+00W	21	13	72						
L2+00N 15+50W	15	12	65	**	- 1 std dev.				
L2+00N 16+00W	17	15	68						
L2+00N 16+50W	22	17	70						
L2+00N 17+00W	18	14	67						
L2+00N 17+50W	26	14	78						
L2+00N 18+00W	27	14	78						
L2+00N 18+50W	20	12	74						
L2+00S 0+00E	26	15	125						
L2+00S 0+50E	10	16	190	**	- 1 std dev.			****	+ 2 std dev.
L2+00S 1+00E	18	18	360					******	)+ 2 std dev.
L2+00S 1+50E	22	22	155			**	+ 1 std dev.	**	+ 1 std dev.
L2+00S 2+00E	18	20	233					******	)+ 2 std dev.
L2+00S 2+50E	23	12	225					****	+ 2 std dev.
L2+00S 3+00E	33	17	303					******	)+ 2 std dev.
L2+00S 3+50E	24	10	235					******	)+ 2 std dev.
L2+00S 4+00E	22	8	130						
L2+00S 4+50E	40	12	138	**	+ 1 std dev.				
L2+00S 5+00E	23	11	107						
L2+00S 5+50E	31	11	112						
L2+00S 6+00E	33	10	138						
L2+00S 6+50E	29	12	152					**	+ 1 std dev.
L2+00S 7+00E	27	9	88						
L2+00S 7+50E	25	9	78						
L2+00S 8+00E	42	10	95	**	+ 1 std dev.				
L2+00S 8+50E	27	9	78						
L2+00S 9+00E	29	8	75						
L2+00S 9+50E	28	9	92						
L2+00S 10+00E	41	13	75	**	+ 1 std dev.				
L2+00S 10+50E	17	6	53						
L2+00S 11+00E	17	7	56						
L2+00S 11+50E	20	2	36			**	- 1 std dev.	**	- 1 std dev.
L2+00S 12+00E	15	5	58	**	- 1 std dev.	**	- 1 std dev.		
L2+00S 0+50W	14	9	150	**	- 1 std dev.			**	+ 1 std dev.
L2+00S 1+00W	20	22	192			**	+ 1 std dev.	****	+ 2 std dev.
L2+00S 1+50W	29	40	183			******	)+ 2 std dev.	**	+ 1 std dev.
L2+00S 2+00W	21	14	124						
L2+00S 2+50W	40	40	150	**	+ 1 std dev.	******	)+ 2 std dev.	**	+ 1 std dev.
L2+00S 3+00W	18	17	115						
L2+00S 3+50W	28	32	105			****	+ 2 std dev.		
L2+00S 4+00W	12	14	77	**	- 1 std dev.				
L2+00S 4+50W	21	17	130						
L2+00S 5+00W	18	10	113						
L2+00S 5+50W	25	12	75						
L2+00S 6+00W	31	20	98						
L2+00S 6+50W	31	20	143					**	+ 1 std dev.
L2+00S 7+00W	43	21	130	**	+ 1 std dev.	**	+ 1 std dev.		
L2+00S 7+50W	29	15	142					**	+ 1 std dev.
L2+00S 8+00W	17	22	125			**	+ 1 std dev.		

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L2+00S 8+50W	29	14	130			
L2+00S 9+00W	35	16	85			
L2+00S 9+50W	37	20	76			
L2+00S 10+00W	31	11	61			
L2+00S 10+50W	32	14	120			
L2+00S 11+00W	27	18	103			
L2+00S 11+50W	19	18	58			
L2+00S 12+00W	14	12	119	** - 1 std dev.		
L2+00S 12+50W	22	12	100			
L2+00S 13+00W	21	11	82			
L2+00S 13+50W	15	11	72	** - 1 std dev.		
L2+00S 14+00W	22	13	105			
L2+00S 14+50W	51	36	100	**** + 2 std dev.	******)+ 2 std dev.	
L2+00S 15+00W	15	15	84	** - 1 std dev.		
L2+00S 15+50W	20	20	93			
L2+00S 16+00W	24	24	100		** + 1 std dev.	
L2+00S 16+50W	22	41	96		******)+ 2 std dev.	
L2+00S 17+00W	11	13	60	** - 1 std dev.		
L2+00S 17+50W	13	15	66	** - 1 std dev.		
L2+00S 18+00W	17	11	84			
L4+00N 0+00E	19	9	75			
L4+00N 0+50E	27	11	95			
L4+00N 1+00E	31	12	108			
L4+00N 1+50E	40	15	92	** + 1 std dev.		
L4+00N 2+00E	32	16	92			
L4+00N 2+50E	29	10	75			
L4+00N 3+00E	58	21	95	**** + 2 std dev.	** + 1 std dev.	
L4+00N 3+50E	34	13	103			
L4+00N 4+00E	34	16	130			
L4+00N 4+50E	22	12	80			
L4+00N 5+00E	27	14	102			
L4+00N 5+50E	37	15	90			
L4+00N 6+00E	22	10	90			
L4+00N 6+50E	42	13	80	** + 1 std dev.		
L4+00N 7+00E	18	11	90			
L4+00N 7+50E	15	7	60	** - 1 std dev.		
L4+00N 8+00E	22	11	115			
L4+00N 8+50E	30	16	105			
L4+00N 9+00E	22	11	113			
L4+00N 9+50E	15	10	97	** - 1 std dev.		
L4+00N 10+00E	19	11	112			
L4+00N 10+50E	22	11	103			
L4+00N 11+00E	32	12	93			
L4+00N 11+50E	17	8	59			
L4+00N 12+00E	23	9	57			
L4+00N 0+50W	41	15	97	** + 1 std dev.		
L4+00N 1+00W	28	11	103			
L4+00N 1+50W	23	11	108			
L4+00N 2+00W	30	17	170			** + 1 std dev.
L4+00N 2+50W	26	13	150			** + 1 std dev.
L4+00N 3+00W	18	16	165			** + 1 std dev.

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L4+00N 3+50W	28	14	155			** + 1 std dev.
L4+00N 4+00W	75	20	82	******)+ 2 std dev.		
L4+00N 4+50W	31	17	98			
L4+00N 5+00W	37	17	100			
L4+00N 5+50W	25	12	96			
L4+00N 6+00W	24	13	118			
L4+00N 6+50W	20	19	110			
L4+00N 7+00W	21	13	108			
L4+00N 7+50W	33	15	150			** + 1 std dev.
L4+00N 8+00W	18	12	125			
L4+00N 8+50W	11	9	70	** - 1 std dev.		
L4+00N 9+00W	18	11	56			
L4+00N 9+50W	10	8	60	** - 1 std dev.		
L4+00N 10+00W	23	12	80			
L4+00N 10+50W	18	11	95			
L4+00N 11+00W	18	12	72			
L4+00N 11+50W	20	8	70			
L4+00N 12+00W	20	8	67			
L4+00N 12+50W	16	12	88			
L4+00N 13+00W	23	12	105			
L4+00N 13+50W	21	20	102			
L4+00N 14+00W	18	17	85			
L4+00N 14+50W	18	14	120			
L4+00N 15+00W	17	9	56			
L4+00N 15+50W	20	18	69			
L4+00N 16+00W	16	14	46			** - 1 std dev.
L4+00N 16+50W	15	15	52	** - 1 std dev.		
L4+00N 17+00W	15	14	63	** - 1 std dev.		
L4+00N 17+50W	22	11	68			
L4+00N 18+00W	18	10	63			
L4+00N 18+50W	17	14	62			
L4+00N 19+00W	14	16	66	** - 1 std dev.		
L4+00N 19+50W	17	13	80			
L4+00N 20+00W	19	14	64			
L4+00N 20+50W	16	12	77			
L4+00N 21+00W	17	11	80			
L4+00N 21+50W	22	13	57			
L4+00N 22+00W	24	14	80			
L4+00N 22+50W	21	13	65			
L4+00N 23+00W	30	17	61			
L4+00S 0+00E	20	14	165			** + 1 std dev.
L4+00S 0+50W	27	33	505		**** + 2 std dev.	******)+ 2 std dev.
L4+00S 1+00W	19	44	225		******)+ 2 std dev.	**** + 2 std dev.
L4+00S 1+50W	16	19	210			**** + 2 std dev.
L4+00S 2+00W	15	16	84	** - 1 std dev.		
L4+00S 2+50W	20	16	98			
L4+00S 3+00W	28	26	210		** + 1 std dev.	**** + 2 std dev.
L4+00S 3+50W	20	28	193		**** + 2 std dev.	**** + 2 std dev.
L4+00S 4+00WSILT	9	18	152	** - 1 std dev.		** + 1 std dev.
L4+00S 4+00W	14	40	223	** - 1 std dev.	******)+ 2 std dev.	**** + 2 std dev.
L4+00S 4+50W	14	11	135	** - 1 std dev.		

Sample description	Cu ppm	Pb ppm	Zn ppm		Cu		Pb		Zn
L4+00S 5+00W	13	26	145	**	- 1 std dev.	**	+ 1 std dev.	**	+ 1 std dev.
L4+00S 5+50W	43	27	125	**	+ 1 std dev.	**	+ 1 std dev.		
L4+00S 6+00W	17	11	120						
L4+00S 6+50W	36	17	103						
L4+00S 7+00W	38	12	70	**	+ 1 std dev.				
L4+00S 7+50W	29	13	100						
L4+00S 8+00W	21	11	60						
L4+00S 8+50W	24	14	93						
L4+00S 9+00W	17	11	82						
L4+00S 9+50W	31	11	80						
L4+00S 10+00W	23	14	58						
L4+00S 10+50W	17	8	135						
L4+00S 11+00W	23	20	105						
L4+00S 11+50W	28	17	115						
L4+00S 12+00W	25	17	125						
L4+00S 12+50W	23	13	77						
L4+00S 13+00W	33	19	115						
L4+00S 13+50W	25	8	110						
L4+00S 14+00W	28	13	92						
L4+00S 14+50W	20	9	75						
L4+00S 15+00W	20	11	80						
L4+00S 15+50W	21	10	79						
L4+00S 16+00W	22	14	95						
L4+00S 16+50W	18	16	80						
L4+00S 17+00W	17	9	80						
L4+00S 17+50W	15	11	75	**	- 1 std dev.				
L4+00S 18+00W	16	11	80						
L6+00N 0+00E	35	16	185					**	+ 1 std dev.
L6+00N 0+50E	42	14	105	**	+ 1 std dev.				
L6+00N 1+00E	17	7	60						
L6+00N 1+50E	17	5	65			**	- 1 std dev.		
L6+00N 2+00E	24	7	67						
L6+00N 2+50E	30	11	80						
L6+00N 3+00E	29	11	103						
L6+00N 3+50E	30	6	58						
L6+00N 4+00E	80	18	117	******	)+ 2 std dev.				
L6+00N 4+50E	21	8	66						
L6+00N 5+00E	18	7	74						
L6+00N 5+50E	23	9	70						
L6+00N 6+00E	26	11	83						
L6+00N 6+50E	45	14	140	**	+ 1 std dev.				
L6+00N 7+00E	39	13	98	**	+ 1 std dev.				
L6+00N 7+50E	45	9	98	**	+ 1 std dev.				
L6+00N 8+00E	19	6	98						
L6+00N 8+50E	22	11	85						
L6+00N 9+00E	25	7	93						
L6+00N 9+50E	17	8	120						
L6+00N 10+00E	29	10	120						
L6+00N 10+50E	21	8	92						
L6+00N 11+00E	22	9	70						
L6+00N 11+50E	24	8	71						

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L6+00N 12+00E	27	7	61			
L6+00N 0+50W	25	9	67			
L6+00N 1+00W	34	15	61			
L6+00N 1+50W	38	13	92	** + 1 std dev.		
L6+00N 2+00W	20	12	96			
L6+00N 2+50W	34	14	103			
L6+00N 3+00W	24	8	80			
L6+00N 3+50W	17	8	120			
L6+00N 4+00W	21	5	72		** - 1 std dev.	
L6+00N 4+50W	28	9	75			
L6+00N 5+00W	25	8	80			
L6+00N 5+50W	25	12	145			** + 1 std dev.
L6+00N 6+00W	34	27	250		** + 1 std dev.	******)+ 2 std dev.
L6+00N 6+50W	15	17	220	** - 1 std dev.		**** + 2 std dev.
L6+00N 7+00W	20	6	62			
L6+00N 7+50W	21	7	73			
L6+00N 8+00W	12	7	53	** - 1 std dev.		
L6+00N 8+50W	21	9	56			
L6+00N 9+00W	20	8	58			
L6+00N 9+50W	23	7	69			
L6+00N 10+00W	15	10	76	** - 1 std dev.		
L6+00N 10+50W	18	9	78			
L6+00N 11+00W	17	7	78			
L6+00N 11+50W	20	10	73			
L6+00N 12+00W	27	10	70			
L6+00N 12+50W	20	9	82			
L6+00N 13+00W	24	12	81			
L6+00N 13+50W	20	8	79			
L6+00N 14+00W	15	7	52	** - 1 std dev.		
L6+00N 14+50W	18	13	64			
L6+00N 15+00W	23	10	72			
L6+00N 15+50W	16	8	56			
L6+00N 16+00W	17	10	50			** - 1 std dev.
L6+00N 16+50W	24	10	56			
L6+00N 17+00W	19	15	68			
L6+00N 17+50W	16	9	68			
L6+00N 18+00W	23	10	60			
L8+00N 0+00E	37	10	96			
L8+00N 0+50E	24	8	64			
L8+00N 1+00E	17	5	52		** - 1 std dev.	
L8+00N 1+50E	13	5	56	** - 1 std dev.	** - 1 std dev.	
L8+00N 2+00E	25	14	83			
L8+00N 2+50E	18	13	81			
L8+00N 3+00E	14	7	52	** - 1 std dev.		
L8+00N 3+50E	21	8	81			
L8+00N 4+00E	18	7	75			
L8+00N 4+50E	17	8	66			
L8+00N 5+00E	23	10	75			
L8+00N 5+50E	20	9	90			
L8+00N 6+00E	33	11	76			
L8+00N 6+50E	33	10	85			

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L8+00N 7+00E	26	9	70			
L8+00N 7+50E	40	6	63	** + 1 std dev.		
L8+00N 8+00E	46	9	66	** + 1 std dev.		
L8+00N 8+50E	19	8	77			
L8+00N 9+00E	29	12	89			
L8+00N 9+50E	25	10	95			
L8+00N 10+00E	20	10	84			
L8+00N 10+50E	20	19	74			
L8+00N 11+00E	20	7	64			
L8+00N 11+50E	16	8	58			
L8+00N 12+00E	37	13	120			
L8+00N 0+50W	32	14	109			
L8+00N 1+00W	25	9	58			
L8+00N 1+50W	32	7	87			
L8+00N 2+00W	57	15	95	**** + 2 std dev.		
L8+00N 2+50W	41	13	70	** + 1 std dev.		
L8+00N 3+00W	52	16	82	**** + 2 std dev.		
L8+00N 3+50W	100	17	88	******)+ 2 std dev.		
L8+00N 4+00W	25	7	53			
L8+00N 4+50W	26	13	88			
L8+00N 5+00W	23	16	60			
L8+00N 5+50W	28	13	58			
L8+00N 6+00W	33	15	56			
L8+00N 6+50W	41	15	72	** + 1 std dev.		
L8+00N 7+00W	26	11	75			
L8+00N 7+50W	20	10	55			
L8+00N 8+00W	35	14	48			** - 1 std dev.
L8+00N 8+50W	22	13	110			
L8+00N 9+00W	29	14	85			
L8+00N 9+50W	17	8	68			
L8+00N 10+00W	30	7	45			** - 1 std dev.
L8+00N 10+50W	22	8	68			
L8+00N 11+00W	24	9	95			
L8+00N 11+50W	22	7	72			
L8+00N 12+00W	26	14	114			
L8+00N 12+50W	27	11	85			
L8+00N 13+00W	22	25	78		** + 1 std dev.	
L8+00N 13+50W	15	12	72	** - 1 std dev.		
L8+00N 14+00W	21	10	78			
L8+00N 14+50W	17	11	62			
L8+00N 15+00W	23	17	70			
L8+00N 15+50W	20	13	75			
L8+00N 16+00W	15	12	63	** - 1 std dev.		
L8+00N 16+50W	16	14	66			
L8+00N 17+00W	13	9	55	** - 1 std dev.		
L8+00N 17+50W	14	9	57	** - 1 std dev.		
L8+00N 18+00W	12	5	51	** - 1 std dev.	** - 1 std dev.	
L10+00N 0+00E	26	8	73			
L10+00N 0+50E	16	5	40		** - 1 std dev.	** - 1 std dev.
L10+00N 1+00E	13	5	80	** - 1 std dev.	** - 1 std dev.	
L10+00N 1+50E	23	4	52		** - 1 std dev.	

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu		Pb		Zn	
L10+00N 2+00E	13	9	43	**	- 1 std dev.			**	- 1 std dev.
L10+00N 2+50E	19	9	48					**	- 1 std dev.
L10+00N 3+00E	18	7	84						
L10+00N 3+50E	26	9	71						
L10+00N 4+00E	48	16	115	**	+ 1 std dev.				
L10+00N 4+50E	22	8	100						
L10+00N 5+00E	55	14	85	****	+ 2 std dev.				
L10+00N 5+50E	25	9	80						
L10+00N 6+00E	49	12	80	****	+ 2 std dev.				
L10+00N 6+50E	33	12	98						
L10+00N 7+00E	29	13	90						
L10+00N 7+50E	48	15	130	**	+ 1 std dev.				
L10+00N 8+00E	33	11	98						
L10+00N 8+50E	25	11	89						
L10+00N 9+00E	30	10	77						
L10+00N 9+50E	25	11	85						
L10+00N 10+00E	22	29	60			****	+ 2 std dev.		
L10+00N 10+50E	20	8	65						
L10+00N 11+00E	22	6	55						
L10+00N 11+50E	16	4	53			**	- 1 std dev.		
L10+00N 12+00E	25	11	70						
L10+00N 0+50W	36	14	100						
L10+00N 1+00W	38	12	104	**	+ 1 std dev.				
L10+00N 1+50W	22	9	83						
L10+00N 2+00W	40	16	77	**	+ 1 std dev.				
L10+00N 2+50W	21	16	74						
L10+00N 3+00W	25	9	79						
L10+00N 3+50W	25	10	71						
L10+00N 4+00W	45	15	90	**	+ 1 std dev.				
L10+00N 4+50W	33	8	70						
L10+00N 5+00W	42	13	52	**	+ 1 std dev.				
L10+00N 5+50W	83	17	80	******	)+ 2 std dev.				
L10+00N 6+00W	24	8	73						
L10+00N 6+50W	27	11	112						
L10+00N 7+00W	19	8	74						
L10+00N 7+50W	21	5	35			**	- 1 std dev.	**	- 1 std dev.
L10+00N 8+00W	25	7	78						
L10+00N 8+50W	54	15	77	****	+ 2 std dev.				
L10+00N 9+00W	22	6	46					**	- 1 std dev.
L10+00N 9+50W	23	7	44					**	- 1 std dev.
L10+00N 10+00W	40	13	43	**	+ 1 std dev.			**	- 1 std dev.
L10+00N 10+50W	35	10	60						
L10+00N 11+00W	38	14	74	**	+ 1 std dev.				
L10+00N 11+50W	28	11	64						
L10+00N 12+00W	27	13	68						
L10+00N 12+50W	24	7	72						
L10+00N 13+00W	24	5	74			**	- 1 std dev.		
L10+00N 13+50W	15	9	44	**	- 1 std dev.			**	- 1 std dev.
L10+00N 14+00W	45	13	80	**	+ 1 std dev.				
L10+00N 14+50W	26	12	54						
L10+00N 15+00W	26	15	71						

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
[illegible]+00N 15+50W	21	11	77			
L10+00N 16+00W	21	12	61			
L10+00N 16+50W	12	12	46	** - 1 std dev.		** - 1 std dev.
L10+00N 17+00W	22	13	62			
L10+00N 17+50W	21	17	72			
L10+00N 18+00W	15	12	65	** - 1 std dev.		
L0N STN 22+50E	27	11	60			
L0N STN 23+00E	22	5	60		** - 1 std dev.	
L0N STN 23+50E	24	8	51			
L0N STN 24+00E	21	7	55			
L0N STN 24+50E	44	14	40	** + 1 std dev.		** - 1 std dev.
L0N STN 25+00E	18	10	69			
L0N STN 25+50E	15	10	53	** - 1 std dev.		
L0N STN 26+00E	17	9	54			
L0N STN 26+50E	14	8	60	** - 1 std dev.		
L0N STN 27+00E	25	8	74			
L0N STN 27+50E	16	15	50			** - 1 std dev.
L0N STN 28+00E	20	9	64			
L0N STN 28+50E	21	7	58			
L0N STN 29+00E	9	7	57	** - 1 std dev.		
L0N STN 29+50E	15	7	67	** - 1 std dev.		
L0N STN 30+00E	22	7	98			
L0N STN 30+50E	25	10	82			
L0N STN 31+00E	14	8	81	** - 1 std dev.		
L0N STN 31+50E	28	8	93			
0E STN 0+50N	15	31	385	** - 1 std dev.	**** + 2 std dev.	******)+ 2 std dev.
[illegible]STN 1+00N	21	78	238		******)+ 2 std dev.	******)+ 2 std dev.
0E STN 1+50N	17	15	320			******)+ 2 std dev.
0E STN 2+50N	27	18	170			** + 1 std dev.
0E STN 3+00N	28	17	149			** + 1 std dev.
0E STN 3+50N	26	18	180			** + 1 std dev.
0E STN 4+50N	53	19	118	**** + 2 std dev.		
0E STN 5+00N	28	12	92			
0E STN 5+50N	23	14	137			
0E STN 6+50N	17	11	57			
0E STN 7+00N	22	13	147			** + 1 std dev.
0E STN 7+50N	24	12	90			
0E STN 8+50N	25	13	110			
0E STN 9+00N	26	16	136			
0E STN 9+50N	42	19	134	** + 1 std dev.		
0E STN 10+50N	23	9	54			
0E STN 11+00N	51	17	112	**** + 2 std dev.		
0E STN 11+50N	21	9	90			
0E STN 12+00N	16	9	60			
0E STN 12+50N	24	13	90			
0E STN 13+00N	27	10	82			
0E STN 13+50N	27	10	66			
0E STN 14+00N	24	13	95			
0E STN 14+50N	18	10	120			
0E STN 15+00N	30	18	123			
0E STN 15+50N	13	6	57	** - 1 std dev.		

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
0E STN 16+00N	34	17	105			
0E STN 16+50N	80	18	68	******)+ 2 std dev.		
0E STN 17+00N	43	14	80	** + 1 std dev.		
0E STN 17+50N	22	16	74			
0E STN 18+00N	24	11	50			** - 1 std dev.
0E STN 18+50N	28	10	66			
0E STN 19+00N	18	12	90			
0E STN 19+50N	30	14	70			
0E STN 20+00N	18	9	70			
0E STN 20+50N	15	12	85	** - 1 std dev.		
0E STN 21+00N	24	14	50			** - 1 std dev.
0E STN 21+50N	20	12	110			
0E STN 22+00N	34	19	92			
0E STN 22+50N	21	14	50			** - 1 std dev.
0E STN 23+00N	40	12	99	** + 1 std dev.		
0E STN 23+50N	25	16	66			
0E STN 24+00N	23	20	91			
0E STN 24+50N	26	14	86			
0E STN 25+00N	36	23	97		** + 1 std dev.	
0E STN 0+50S	26	40	224		******)+ 2 std dev.	**** + 2 std dev.
0E STN 1+00S	37	66	270		******)+ 2 std dev.	******)+ 2 std dev.
0E STN 1+50S	15	12	140	** - 1 std dev.		
0E STN 2+00S	19	15	138			
0E STN 2+50S	26	13	124			
0E STN 3+00S	18	14	82			
0E STN 3+50S	24	16	150			** + 1 std dev.
0E STN 4+00S	20	15	158			** + 1 std dev.
0E STN 4+50S	24	17	95			
0E STN 5+00S	28	26	140		** + 1 std dev.	
0E STN 5+50S	24	20	133			
0E STN 6+00S	40	27	98	** + 1 std dev.	** + 1 std dev.	
0E STN 6+50S	25	16	68			
0E STN 7+00S	20	12	54			
0E STN 7+50S	26	17	78			
0E STN 8+00S	22	12	75			
0E STN 8+50S	60	33	115	******)+ 2 std dev.	**** + 2 std dev.	
0E STN 9+00S	37	20	145			** + 1 std dev.
0E STN 9+50S	30	17	100			
0E STN 10+00S	23	11	90			
0E STN 10+50S	32	17	120			
0E STN 11+00S	18	8	50			** - 1 std dev.
0E STN 11+50S	17	14	93			
0E STN 12+00S	38	24	150	** + 1 std dev.	** + 1 std dev.	** + 1 std dev.
0E STN 12+50S	23	19	260			******)+ 2 std dev.
0E STN 13+00S	47	27	190	** + 1 std dev.	** + 1 std dev.	**** + 2 std dev.
0E STN 13+50S	35	18	175			** + 1 std dev.
0E STN 14+00S	21	13	118			
0E STN 14+50S	21	14	93			
0E STN 15+00S	28	16	80			
0E STN 15+50S	25	20	123			
0E STN 16+00S	23	15	28			** - 1 std dev.

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu		Pb		Zn	
0E STN 16+50S	25	13	90						
0E STN 17+00S	25	19	134						
0E STN 17+50S	23	17	125						
0E STN 18+00S	35	20	115						
0E STN 18+50S	28	18	155					**	+ 1 std dev.
0E STN 19+00S	38	24	155	**	+ 1 std dev.	**	+ 1 std dev.	**	+ 1 std dev.
0E STN 19+50S	37	22	135			**	+ 1 std dev.		
0E STN 20+00S	23	19	125						
L4S STN 0+50E	24	19	110						
L4S STN 1+00E	24	14	103						
L4S STN 1+50E	43	23	136	**	+ 1 std dev.	**	+ 1 std dev.		
L4S STN 2+00E	24	22	105			**	+ 1 std dev.		
L4S STN 2+50E	22	20	170					**	+ 1 std dev.
L4S STN 3+00E	28	12	106						
L4S STN 3+50E	28	11	92						
L4S STN 4+00E	26	12	96						
L4S STN 4+50E	28	12	94						
L4S STN 5+00E	24	11	140						
L4S STN 5+50E	24	12	82						
L4S STN 6+00E	27	11	105						
L4S STN 6+50E	27	14	79						
L4S STN 7+00E	30	11	78						
L4S STN 7+50E	24	14	76						
L4S STN 8+00E	26	11	78						
L4S STN 8+50E	29	11	80						
L4S STN 9+00E	33	11	62						
L4S STN 9+50E	27	10	68						
L4S STN 10+00E	30	10	72						
L4S STN 10+50E	35	8	50					**	- 1 std dev.
L4S STN 11+00E	26	5	52			**	- 1 std dev.		
L4S STN 11+50E	28	8	60						
L4S STN 12+00E	24	5	155			**	- 1 std dev.	**	+ 1 std dev.
L6S STN 0+50E	26	22	87			**	+ 1 std dev.		
L6S STN 1+00E	38	20	80	**	+ 1 std dev.				
L6S STN 1+50E	26	12	68						
L6S STN 2+00E	25	15	78						
L6S STN 2+50E	35	12	85						
L6S STN 3+00E	23	11	90						
L6S STN 3+50E	35	15	163					**	+ 1 std dev.
L6S STN 4+00E	33	11	76						
L6S STN 4+50E	27	7	79						
L6S STN 5+00E	42	9	90	**	+ 1 std dev.				
L6S STN 5+50E	55	12	80	****	+ 2 std dev.				
L6S STN 6+00E	32	9	102						
L6S STN 6+50E	34	12	88						
L6S STN 7+00E	22	8	95						
L6S STN 7+50E	32	11	80						
L6S STN 8+00E	19	7	104						
L6S STN 8+50E	25	9	79						
L6S STN 9+00E	52	10	107	****	+ 2 std dev.				
L6S STN 9+50E	32	9	87						

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L6S STN 10+00E	47	8	77	** + 1 std dev.		
L6S STN 10+50E	25	7	59			
L6S STN 11+00E	34	8	71			
L6S STN 11+50E	29	6	67			
L6S STN 12+00E	33	8	71			
L6S STN 0+50W	22	11	85			
L6S STN 1+00W	25	12	125			
L6S STN 1+50W	17	10	68			
L6S STN 2+00W	21	17	100			
L6S STN 2+50W	23	16	120			
L6S STN 3+00W	23	13	65			
L6S STN 3+50W	25	23	135		** + 1 std dev.	
L6S STN 4+00W	23	15	117			
L6S STN 4+50W	19	10	70			
L6S STN 5+00W	20	12	200			**** + 2 std dev.
L6S STN 5+50W	50	14	109	**** + 2 std dev.		
L6S STN 6+00W	22	8	95			
L6S STN 6+50W	24	12	85			
L6S STN 7+00W	38	10	96	** + 1 std dev.		
L6S STN 7+50W	42	8	110	** + 1 std dev.		
L6S STN 8+00W	45	11	88	** + 1 std dev.		
L6S STN 8+50W	65	17	103	******)+ 2 std dev.		
L6S STN 9+00W	48	13	86	** + 1 std dev.		
L6S STN 9+50W	37	16	125			
L6S STN 10+00W	33	16	96			
L6S STN 10+50W	40	12	105	** + 1 std dev.		
L6S STN 11+00W	40	12	115	** + 1 std dev.		
L6S STN 11+50W	28	11	128			
L6S STN 12+00W	33	16	130			
L6S STN 12+50W	25	9	105			
L6S STN 13+00W	21	12	130			
L6S STN 13+50W	23	11	106			
L6S STN 14+00W	20	7	140			
L6S STN 14+50W	17	6	70			
L6S STN 15+00W	21	8	80			
L6S STN 15+50W	22	6	89			
L6S STN 16+00W	21	6	82			
L6S STN 16+50W	22	12	80			
L6S STN 17+00W	19	9	64			
L6S STN 17+50W	20	6	83			
L6S STN 18+00W	24	11	70			
L8S STN 0+50E	45	22	93	** + 1 std dev.	** + 1 std dev.	
L8S STN 1+00E	19	10	63			
L8S STN 1+50E	15	3	50	** - 1 std dev.	** - 1 std dev.	** - 1 std dev.
L8S STN 2+00E	18	7	63			
L8S STN 2+50E	32	17	100			
L8S STN 3+00E	23	13	74			
L8S STN 3+50E	42	16	138	** + 1 std dev.		
L8S STN 4+00E	22	8	100			
L8S STN 4+50E	41	8	100	** + 1 std dev.		
L8S STN 5+00E	90	21	100	******)+ 2 std dev.	** + 1 std dev.	

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L8S STN 5+50E	22	7	65			
L8S STN 6+00E	28	10	62			
L8S STN 6+50E	36	11	70			
L8S STN 7+00E	32	11	73			
L8S STN 7+50E	28	7	100			
L8S STN 8+00E	29	8	74			
L8S STN 8+50E	20	9	72			
L8S STN 9+00E	19	7	54			
L8S STN 9+50E	18	6	52			
L8S STN 10+00E	21	8	64			
L8S STN 10+50E	23	7	80			
L8S STN 11+00E	25	3	81		** - 1 std dev.	
L8S STN 11+50E	18	4	83		** - 1 std dev.	
L8S STN 12+00E	22	6	73			
L8S STN 0+50W	21	10	72			
L8S STN 1+00W	25	20	79			
L8S STN 1+50W	21	15	62			
L8S STN 2+00W	18	9	63			
L8S STN 2+50W	25	14	90			
L8S STN 3+00W	31	16	87			
L8S STN 3+50W	22	10	82			
L8S STN 4+00W	45	20	120	** + 1 std dev.		
L8S STN 4+50W	66	20	190	******)+ 2 std dev.		**** + 2 std dev.
L8S STN 5+00W	42	17	140	** + 1 std dev.		
L8S STN 5+50W	43	16	131	** + 1 std dev.		
L8S STN 6+00W	42	20	118	** + 1 std dev.		
L8S STN 6+50W	23	6	72			
L8S STN 7+00W	44	19	155	** + 1 std dev.		** + 1 std dev.
L8S STN 7+50W	27	11	68			
L8S STN 8+00W	42	16	140	** + 1 std dev.		
L8S STN 8+50W	45	18	104	** + 1 std dev.		
L8S STN 9+00W	32	14	113			
L8S STN 9+50W	41	14	96	** + 1 std dev.		
L8S STN 10+00W	61	17	115	******)+ 2 std dev.		
L8S STN 10+50W	58	20	120	**** + 2 std dev.		
L8S STN 11+00W	44	19	134	** + 1 std dev.		
L8S STN 11+50W	32	13	105			
L8S STN 12+00W	33	12	92			
L8S STN 12+50W	21	6	57			
L8S STN 13+00W	22	9	106			
L8S STN 13+50W	25	10	108			
L8S STN 14+00W	14	8	91	** - 1 std dev.		
L8S STN 14+50W	21	7	98			
L8S STN 15+00W	21	7	82			
L8S STN 15+50W	22	6	80			
L8S STN 16+00W	19	6	82			
L8S STN 16+50W	19	10	71			
L8S STN 17+00W	17	9	51			
L8S STN 17+50W	19	12	74			
L8S STN 18+00W	18	12	78			
L10S STN 0+50E	32	15	90			

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L10S STN 1+00E	19	7	67			
L10S STN 1+50E	34	14	100			
L10S STN 2+00E	28	11	88			
L10S STN 2+50E	35	19	98			
L10S STN 3+00E	25	8	58			
L10S STN 3+50E	36	17	115			
L10S STN 4+00E	28	12	84			
L10S STN 4+50E	49	18	119	**** + 2 std dev.		
L10S STN 5+00E	22	13	138			
L10S STN 5+50E	25	13	90			
L10S STN 6+00E	45	11	82	** + 1 std dev.		
L10S STN 6+50E	28	10	77			
L10S STN 7+00E	63	28	91	******)+ 2 std dev.	**** + 2 std dev.	
L10S STN 7+50E	20	9	74			
L10S STN 8+00E	23	10	68			
L10S STN 8+50E	22	9	66			
L10S STN 9+00E	50	12	107	**** + 2 std dev.		
L10S STN 9+50E	21	8	106			
L10S STN 10+00E	35	6	60			
L10S STN 10+50E	20	8	90			
L10S STN 11+00E	32	7	60			
L10S STN 11+50E	23	8	69			
L10S STN 12+00E	31	6	80			
L10S STN 0+50W	22	11	71			
L10S STN 1+00W	21	11	70			
L10S STN 1+50W	72	29	170	******)+ 2 std dev.	**** + 2 std dev.	** + 1 std dev.
L10S STN 2+00W	40	19	128	** + 1 std dev.		
L10S STN 2+50W	28	11	85			
L10S STN 3+00W	25	11	105			
L10S STN 3+50W	35	15	146			** + 1 std dev.
L10S STN 4+00W	27	13	98			
L10S STN 4+50W	37	15	116			
L10S STN 5+00W	17	9	71			
L10S STN 5+50W	19	16	77			
L10S STN 6+00W	43	19	115	** + 1 std dev.		
L10S STN 6+50W	20	7	60			
L10S STN 7+00W	30	16	123			
L10S STN 7+50W	20	7	70			
L10S STN 8+00W	49	25	140	**** + 2 std dev.	** + 1 std dev.	
L10S STN 8+50W	45	17	119	** + 1 std dev.		
L10S STN 9+00W	41	18	150	** + 1 std dev.		** + 1 std dev.
L10S STN 9+50W	34	15	110			
L10S STN 10+00W	17	10	52			
L10S STN 10+50W	33	14	99			
L10S STN 11+00W	34	19	150			** + 1 std dev.
L10S STN 11+50W	34	16	130			
L10S STN 12+00W	22	9	132			
L10S STN 12+50W	22	12	130			
L10S STN 13+00W	22	13	87			
L10S STN 13+50W	22	12	80			
L10S STN 14+00W	20	7	53			

Sample description	Cu ppm	Pb ppm	Zn ppm	Cu	Pb	Zn
L10S STN 14+50W	17	6	50		**	- 1 std dev.
L10S STN 15+00W	17	11	66			
L10S STN 15+50W	28	11	46		**	- 1 std dev.
L10S STN 16+00W	19	9	80			
L10S STN 16+50W	19	12	67			
L10S STN 17+00W	25	15	63			
L10S STN 17+50W	33	10	55			
L10S STN 18+00W	25	11	74			
L10S STN 18+50W	21	7	55			
L10S STN 19+00W	50	17	90	**** + 2 std dev.		
L10S STN 19+50W	22	11	72			
L10S STN 20+00W	37	16	90			

date of this run : 3-JAN-84

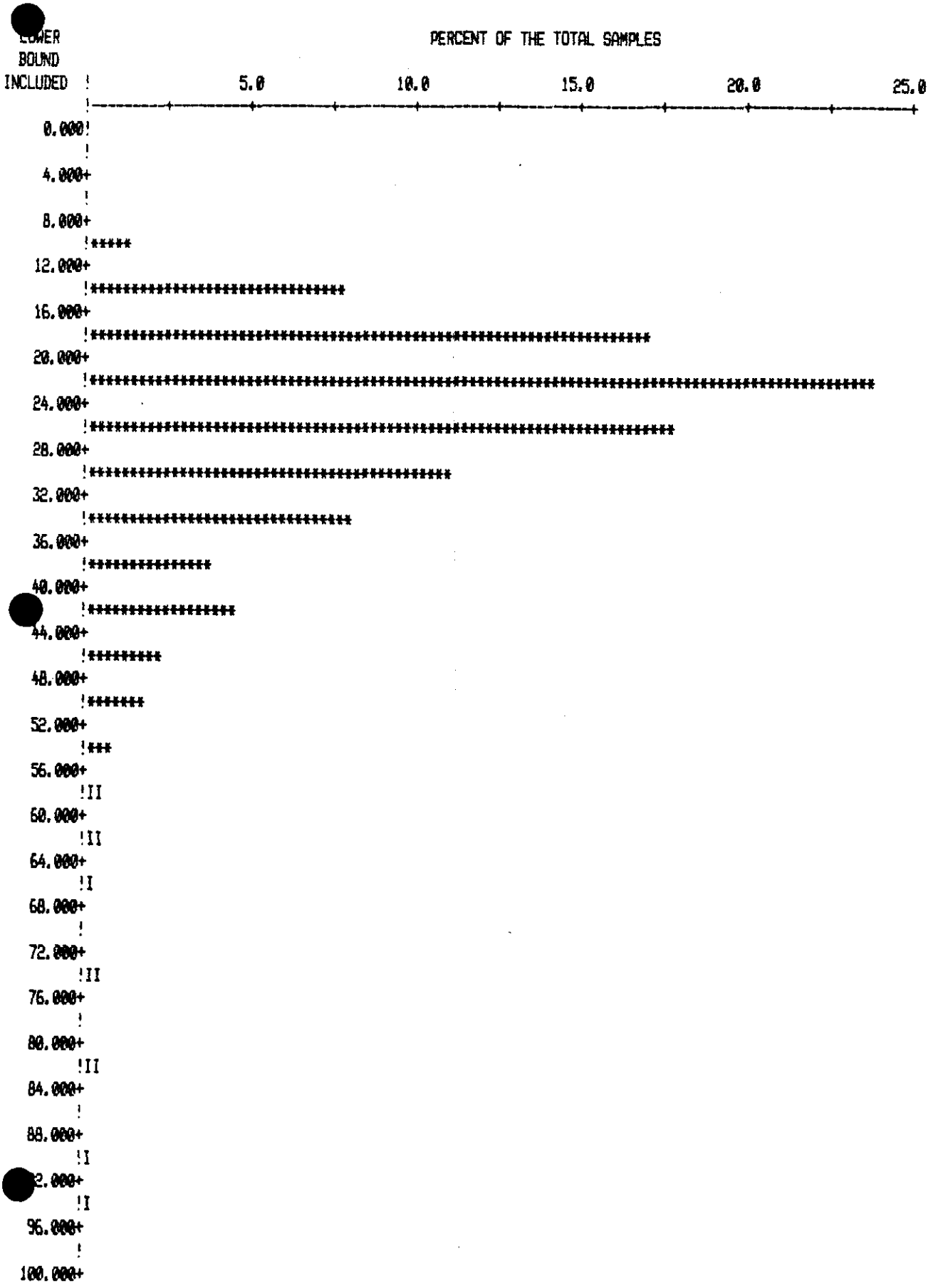
DATA TITLE: CHEVRON -- Larry Dekker project M525

THE FOLLOWING VARIABLES ARE IN THE DATA SET:

Cu	Pb	Zn	logCu	logPb	logZn

DATA TITLE : CHEVRON -- Larry Dekker project M525

VARIABLE : Cu



VARIABLE: Cu

NUMBER OF OBSERVATIONS:	828
MINIMUM:	9.000
MAXIMUM:	100.000
MEAN:	26.266
STANDARD ERROR OF MEAN:	0.387
STANDARD DEVIATION:	11.126
COEFFICIENT OF VARIATION:	42.358
SKEWNESS:	2.202
KURTOSIS:	8.028

CHI-SQUARE TEST FOR "GOODNESS OF FIT" WITH A NORMAL DISTRIBUTION

VARIABLE : Cu

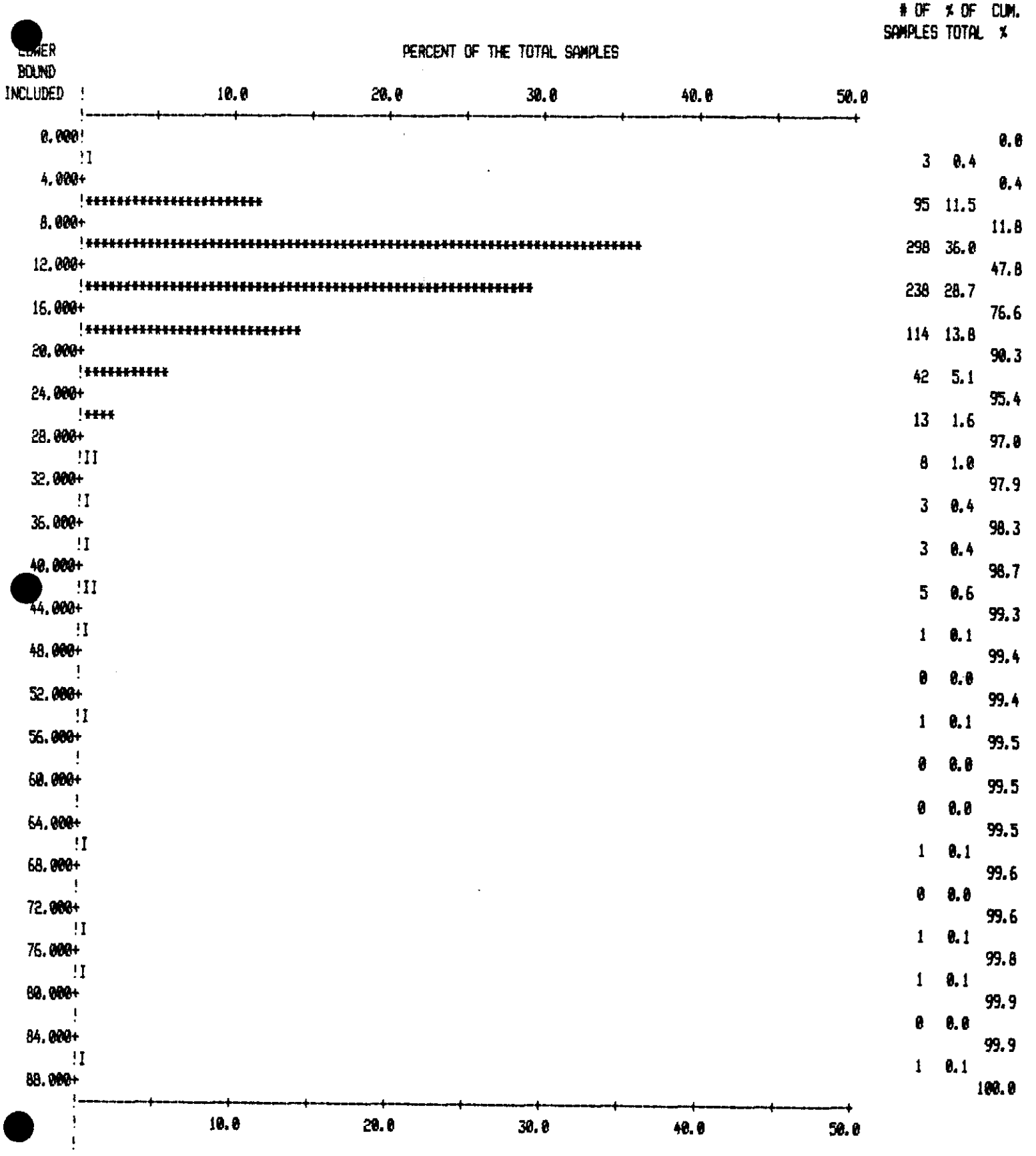
CLASS BOUNDS			OBSERVED	EXPECTED	(OBS-EXP)	[(OBS.-EXP.)**2 / EXP.]
-INFINITY	TO	12.007	17	82.8	-65.8	52.290
12.007	TO	16.902	79	82.8	-3.8	0.174
16.902	TO	20.431	162	82.8	79.2	75.757
20.431	TO	23.448	150	82.8	67.2	54.539
23.448	TO	26.266	120	82.8	37.2	16.713
26.266	TO	29.084	78	82.8	-4.8	0.278
29.084	TO	32.100	56	82.8	-26.8	8.674
32.100	TO	35.629	46	82.8	-36.8	16.356
35.629	TO	40.524	40	82.8	-42.8	22.124
40.524	TO	+INFINITY	80	82.8	-2.8	0.095

CHI-SQUARED VALUE IS 247.00. DEGREES OF FREEDOM ARE 7.

SIGNIFICANCE LEVEL	CHI-SQUARE VALUE
0.500	6.35
0.750	9.04
0.900	12.00
0.950	14.10
0.975	16.00
0.990	18.50
0.995	20.30

DATA TITLE : CHEVRON -- Larry Dekker project M525

VARIABLE : Pb



VARIABLE: Pb

NUMBER OF OBSERVATIONS:	828
MINIMUM:	2.000
MAXIMUM:	84.000
MEAN:	13.087
STANDARD ERROR OF MEAN:	0.249
STANDARD DEVIATION:	7.172
COEFFICIENT OF VARIATION:	54.803
SKEWNESS:	4.280
KURTOSIS:	30.974

CHI-SQUARE TEST FOR "GOODNESS OF FIT" WITH A NORMAL DISTRIBUTION

VARIABLE : Pb

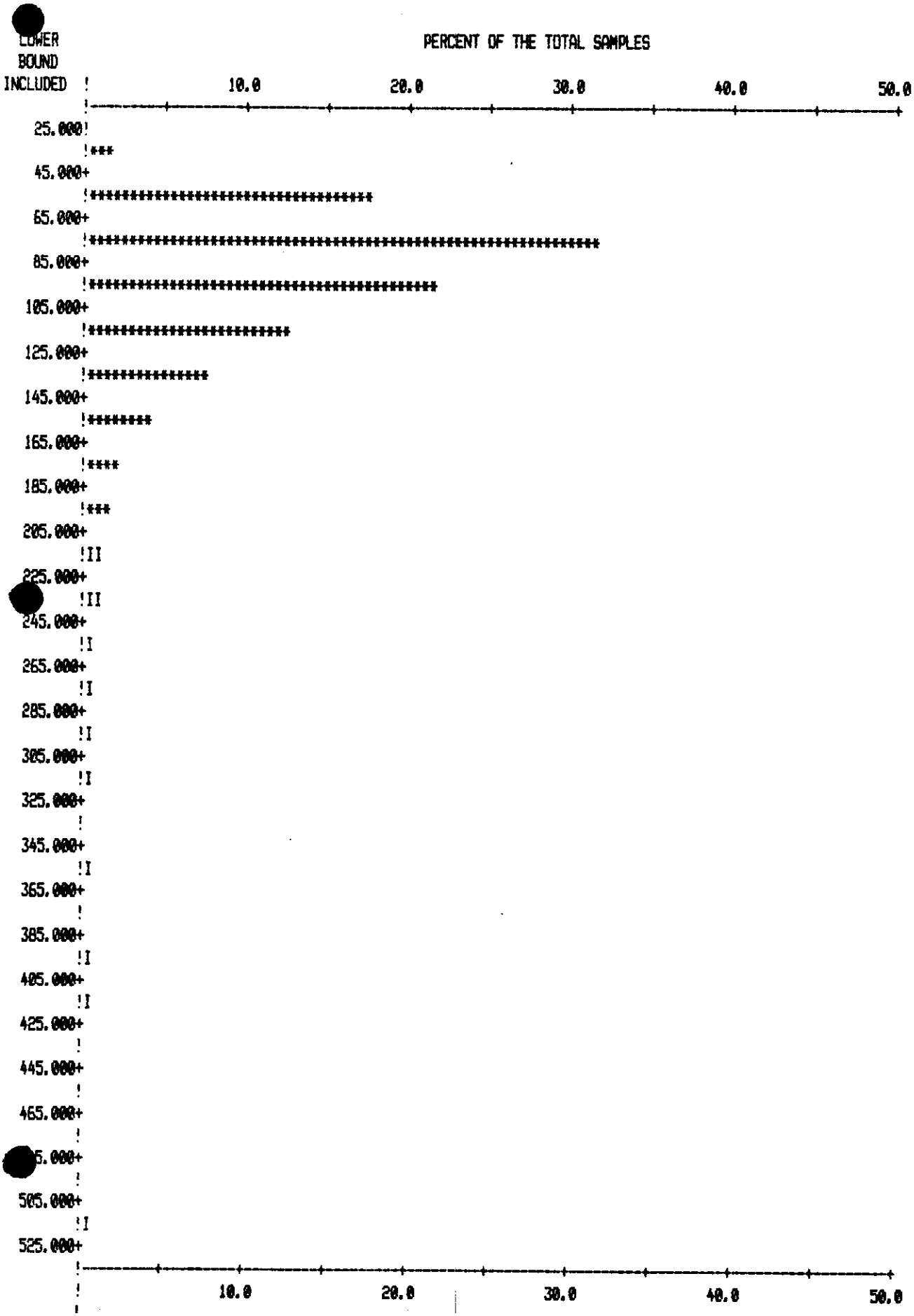
CLASS BOUNDS			OBSERVED	EXPECTED	(OBS-EXP)	[(OBS.-EXP.)**2 / EXP.]
-INFINITY	TO	3.895	3	82.8	-79.8	76.909
3.895	TO	7.051	95	82.8	12.2	1.798
7.051	TO	9.326	133	82.8	50.2	30.435
9.326	TO	11.270	165	82.8	82.2	81.604
11.270	TO	13.087	139	82.8	56.2	38.145
13.087	TO	14.904	62	82.8	-20.8	5.225
14.904	TO	16.848	76	82.8	-6.8	0.558
16.848	TO	19.123	75	82.8	-7.8	0.735
19.123	TO	22.279	37	82.8	-45.8	25.334
22.279	TO	+INFINITY	43	82.8	-39.8	19.131

CHI-SQUARED VALUE IS 279.87. DEGREES OF FREEDOM ARE 7.

SIGNIFICANCE LEVEL	CHI-SQUARE VALUE
0.500	6.35
0.750	9.04
0.900	12.00
0.950	14.10
0.975	16.00
0.990	18.50
0.995	20.30

DATA TITLE : CHEVRON -- Larry Dekker project M525

VARIABLE : Zn



VARIABLE: Zn

NUMBER OF OBSERVATIONS:	828
MINIMUM:	28.000
MAXIMUM:	505.000
MEAN:	95.653
STANDARD ERROR OF MEAN:	1.555
STANDARD DEVIATION:	44.736
COEFFICIENT OF VARIATION:	46.769
SKEWNESS:	3.050
KURTOSIS:	16.404

CHI-SQUARE TEST FOR "GOODNESS OF FIT" WITH A NORMAL DISTRIBUTION

VARIABLE : Zn

CLASS BOUNDS			OBSERVED	EXPECTED	(OBS-EXP)	[(OBS.-EXP.)**2 / EXP.]
-INFINITY	TO	38.320	5	82.8	-77.8	73.102
38.320	TO	58.004	95	82.8	12.2	1.798
58.004	TO	72.194	159	82.8	76.2	70.126
72.194	TO	84.322	155	82.8	72.2	62.957
84.322	TO	95.653	106	82.8	23.2	6.500
95.653	TO	106.985	88	82.8	5.2	0.327
106.985	TO	119.113	60	82.8	-22.8	6.278
119.113	TO	133.303	51	82.8	-31.8	12.213
133.303	TO	152.987	47	82.8	-35.8	15.479
152.987	TO	+INFINITY	62	82.8	-20.8	5.225

CHI-SQUARED VALUE IS 254.00. DEGREES OF FREEDOM ARE 7.

SIGNIFICANCE LEVEL	CHI-SQUARE VALUE
0.500	6.35
0.750	9.04
0.900	12.00
0.950	14.10
0.975	16.00
0.990	18.50
0.995	20.30

DATA TITLE : CHEVRON -- Larry Dekker project M525

VARIABLE : logCu

LOWER BOUND INCLUDED	PERCENT OF THE TOTAL SAMPLES	# OF SAMPLES	% OF TOTAL	CUM. %
0.900				0.0
		0	0.0	
0.950				0.0
	I	2	0.2	
1.000				0.2
	****	8	1.0	
1.050				1.2
	****	7	0.8	
1.100				2.1
	**********	26	3.1	
1.150				5.2
	**********	30	3.6	
1.200				8.8
	**********	63	7.6	
1.250				16.4
	**********	76	9.2	
1.300				25.6
	**********	154	18.6	
1.350				44.2
	**********	130	15.7	
1.400				59.9
	**********	92	11.1	
1.450				71.0
	**********	55	6.6	
1.500				77.7
	**********	65	7.9	
1.550				85.5
	**********	29	3.5	
1.600				89.0
	**********	40	4.8	
1.650				93.8
	**********	25	3.0	
1.700				96.9
	****	8	1.0	
1.750				97.8
	****	7	0.8	
1.800				98.7
	I	2	0.2	
1.850				98.9
	II	3	0.4	
1.900				99.3
	II	3	0.4	
1.950				99.6
	I	2	0.2	
2.000				99.9

PERCENT OF THE TOTAL SAMPLES

VARIABLE: logCu

NUMBER OF OBSERVATIONS:	828
MINIMUM:	0.954
MAXIMUM:	2.000
MEAN:	1.389
STANDARD ERROR OF MEAN:	0.005
STANDARD DEVIATION:	0.158
COEFFICIENT OF VARIATION:	11.386
SKEWNESS:	0.511
KURTOSIS:	0.777

CHI-SQUARE TEST FOR "GOODNESS OF FIT" WITH A NORMAL DISTRIBUTION

VARIABLE : logCu

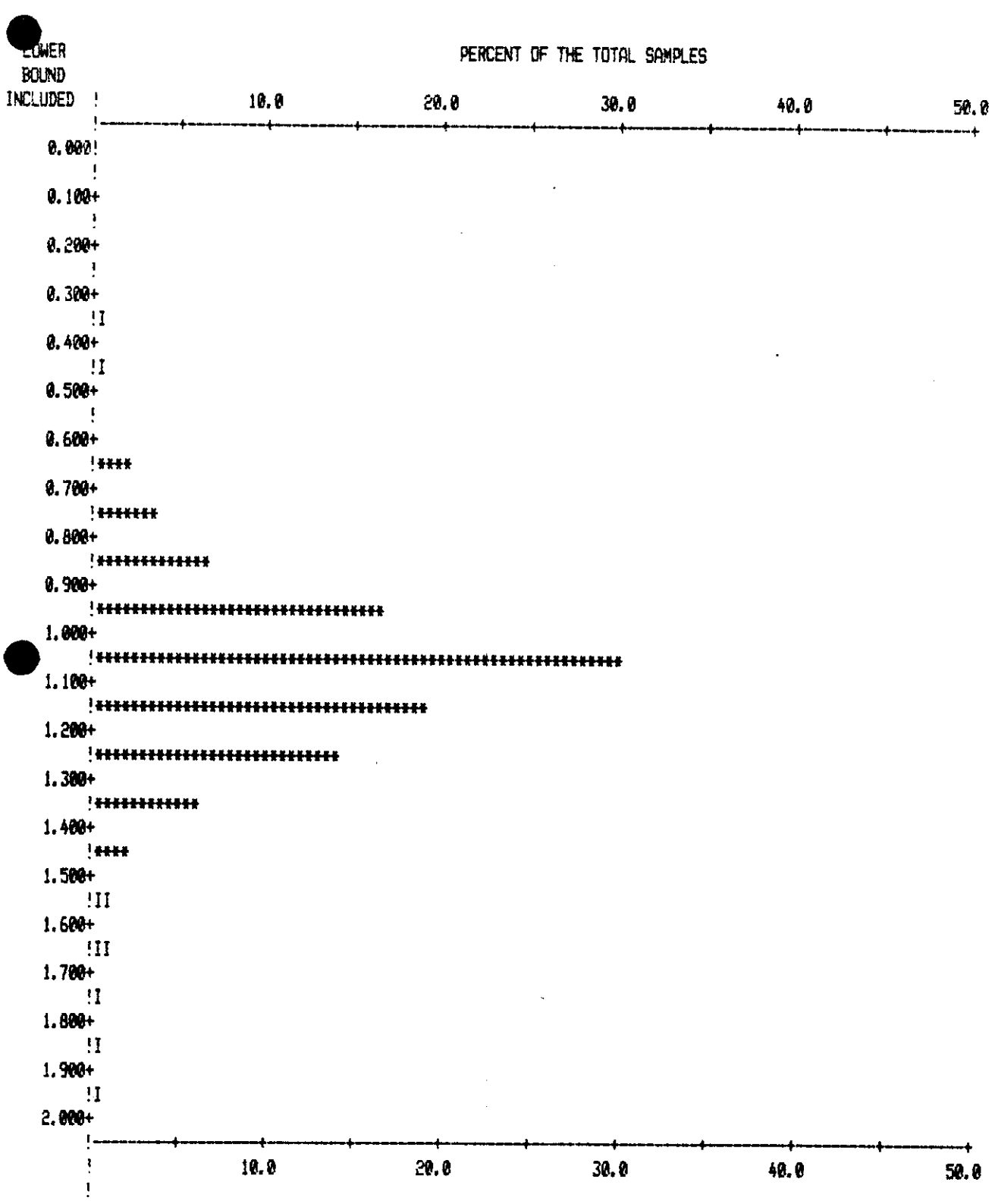
CLASS BOUNDS			OBSERVED	EXPECTED	(OBS-EXP)	[(OBS.-EXP.)**2 / EXP.]
-INFINITY	TO	1.186	73	82.8	-9.8	1.160
1.186	TO	1.256	109	82.8	26.2	8.290
1.256	TO	1.306	76	82.8	-6.8	0.558
1.306	TO	1.349	108	82.8	25.2	7.670
1.349	TO	1.389	83	82.8	0.2	0.000
1.389	TO	1.429	79	82.8	-3.8	0.174
1.429	TO	1.472	78	82.8	-4.8	0.278
1.472	TO	1.522	76	82.8	-6.8	0.558
1.522	TO	1.591	55	82.8	-27.8	9.334
1.591	TO	+INFINITY	91	82.8	8.2	0.812

CHI-SQUARED VALUE IS 28.84. DEGREES OF FREEDOM ARE 7.

SIGNIFICANCE LEVEL	CHI-SQUARE VALUE
0.500	6.35
0.750	9.04
0.900	12.00
0.950	14.10
0.975	16.00
0.990	18.50
0.995	20.30

DATA TITLE : CHEVRON -- Larry Dekker project M525

VARIABLE : logPb



# OF SAMPLES	% OF TOTAL	CUM. %
		0.0
0	0.0	
		0.0
0	0.0	
		0.0
0	0.0	
		0.0
1	0.1	
		0.1
2	0.2	
		0.4
0	0.0	
		0.4
16	1.9	
		2.3
28	3.4	
		5.7
51	6.2	
		11.8
133	16.1	
		27.9
248	30.0	
		57.9
155	18.7	
		76.6
114	13.8	
		90.3
47	5.7	
		96.0
16	1.9	
		97.9
6	0.7	
		98.7
6	0.7	
		99.4
1	0.1	
		99.5
3	0.4	
		99.9
1	0.1	
		100.0

VARIABLE: logPb

NUMBER OF OBSERVATIONS:	828
MINIMUM:	0.301
MAXIMUM:	1.924
MEAN:	1.075
STANDARD ERROR OF MEAN:	0.006
STANDARD DEVIATION:	0.182
COEFFICIENT OF VARIATION:	16.927
SKEWNESS:	0.457
KURTOSIS:	2.167

CHI-SQUARE TEST FOR "GOODNESS OF FIT" WITH A NORMAL DISTRIBUTION

VARIABLE : logPb

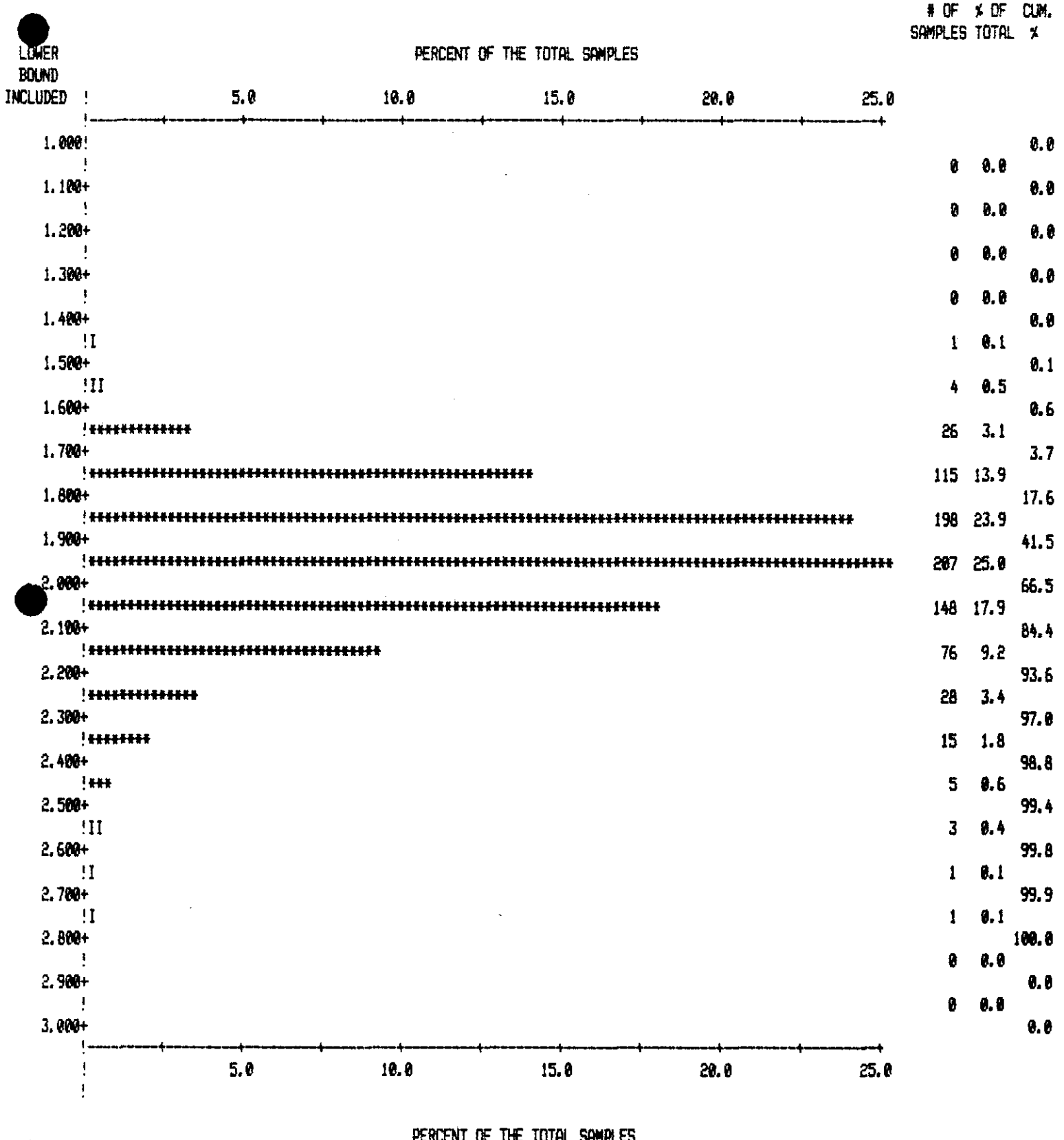
CLASS BOUNDS			OBSERVED	EXPECTED	(OBS-EXP)	[(OBS.-EXP.)**2 / EXP.]
-INFINITY	TO	0.842	47	82.8	-35.8	15.479
0.842	TO	0.922	119	82.8	36.2	15.827
0.922	TO	0.980	65	82.8	-17.8	3.827
0.980	TO	1.029	72	82.8	-10.8	1.409
1.029	TO	1.075	93	82.8	10.2	1.257
1.075	TO	1.121	139	82.8	56.2	38.145
1.121	TO	1.170	62	82.8	-20.8	5.225
1.170	TO	1.228	76	82.8	-6.8	0.558
1.228	TO	1.300	99	82.8	16.2	3.170
1.300	TO	+INFINITY	56	82.8	-26.8	8.674

CHI-SQUARED VALUE IS 93.57. DEGREES OF FREEDOM ARE 7.

SIGNIFICANCE LEVEL	CHI-SQUARE VALUE
0.500	6.35
0.750	9.04
0.900	12.00
0.950	14.10
0.975	16.00
0.990	18.50
0.995	20.30

DATA TITLE : CHEVRON -- Larry Dekker project M525

VARIABLE : logZn



VARIABLE: logZn

NUMBER OF OBSERVATIONS:	828
MINIMUM:	1.447
MAXIMUM:	2.703
MEAN:	1.947
STANDARD ERROR OF MEAN:	0.006
STANDARD DEVIATION:	0.163
COEFFICIENT OF VARIATION:	8.356
SKEWNESS:	0.738
KURTOSIS:	1.327

CHI-SQUARE TEST FOR "GOODNESS OF FIT" WITH A NORMAL DISTRIBUTION

VARIABLE : logZn

CLASS BOUNDS			OBSERVED	EXPECTED	(OBS-EXP)	[(OBS.-EXP.)**2 / EXP.]
-INFINITY	TO	1.738	57	82.8	-25.8	8.039
1.738	TO	1.810	97	82.8	14.2	2.435
1.810	TO	1.862	105	82.8	22.2	5.952
1.862	TO	1.906	119	82.8	36.2	15.827
1.906	TO	1.947	72	82.8	-10.8	1.409
1.947	TO	1.988	83	82.8	0.2	0.000
1.988	TO	2.032	79	82.8	-3.8	0.174
2.032	TO	2.084	72	82.8	-10.8	1.409
2.084	TO	2.155	65	82.8	-17.8	3.827
2.155	TO	+INFINITY	79	82.8	-3.8	0.174

CHI-SQUARED VALUE IS 39.25. DEGREES OF FREEDOM ARE 7.

SIGNIFICANCE LEVEL	CHI-SQUARE VALUE
0.500	6.35
0.750	9.04
0.900	12.00
0.950	14.10
0.975	16.00
0.990	18.50
0.995	20.30

$ C80
?31

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X - Y P L O T program V3.2 mar/1980 4-JAN-84

DATA TITLE: CHEVRON -- Larry Dekker project M525

THE FOLLOWING VARIABLES ARE IN THE DATA SET:

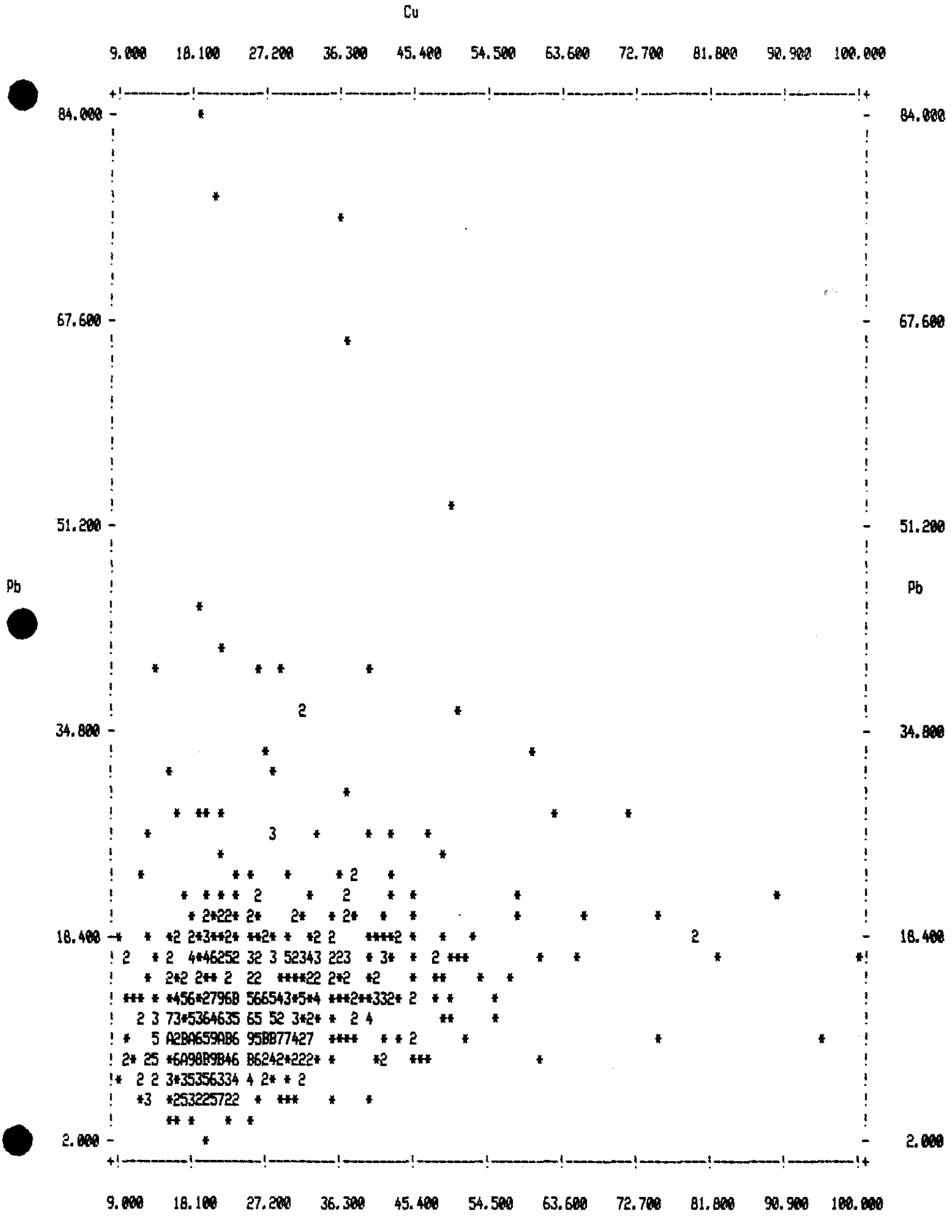
Cu	Pb	Zn	logCu	logPb	logZn

CORRELATION MATRIX: (99.0 INDICATES COEFFICIENT COULD NOT BE CALCULATED)

	Cu	Pb	Zn	logCu	logPb	logZn
Cu	1.000	0.249	0.091	0.955	0.319	0.154
Pb	0.249	1.000	0.543	0.248	0.897	0.524
Zn	0.091	0.543	1.000	0.103	0.530	0.940
logCu	0.955	0.248	0.103	1.000	0.321	0.179
logPb	0.319	0.897	0.530	0.321	1.000	0.561
logZn	0.154	0.524	0.940	0.179	0.561	1.000

NUMBER OF SAMPLES PER VARIABLE PAIR

	Cu	Pb	Zn	logCu	logPb	logZn
Cu	828	828	828	828	828	828
Pb	828	828	828	828	828	828
Zn	828	828	828	828	828	828
logCu	828	828	828	828	828	828
logPb	828	828	828	828	828	828
logZn	828	828	828	828	828	828



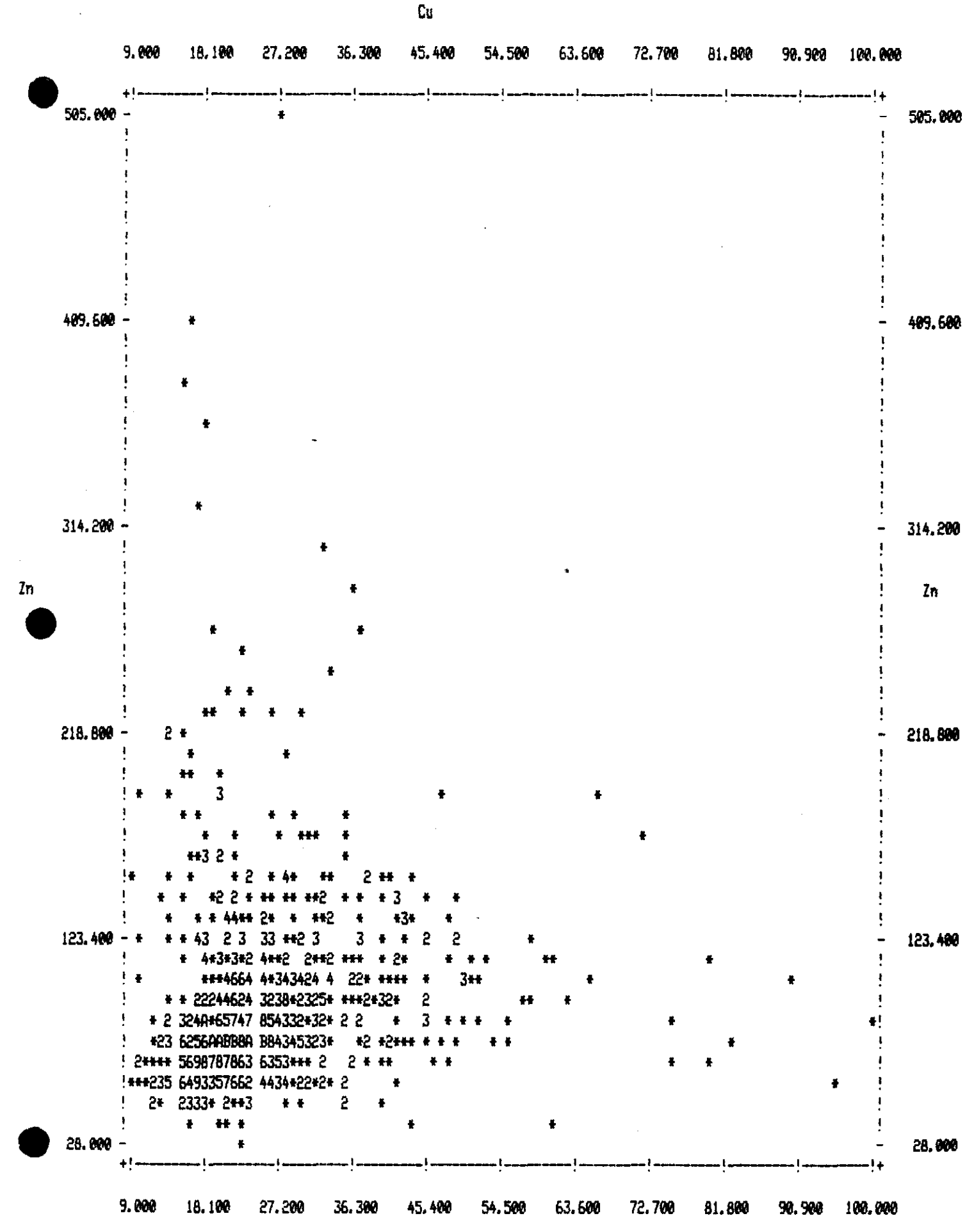
0 POINTS OUT OF RANGE

STATISTICS FOR VARIABLES:	Cu	Pb
NUMBER OF OBSERVATIONS:	828	828
MINIMUM:	9.00	2.00
MAXIMUM:	100.00	84.00
MEAN:	26.27	13.09
STANDARD ERROR OF MEAN:	0.39	0.25
STANDARD DEVIATION:	11.13	7.17
COEFFICIENT OF VARIATION:	42.36	54.80
SKEWNESS:	2.20	4.28
KURTOSIS:	8.03	30.97
CORRELATION COEFFICIENT:	0.2489	

****

WE WILL NOW MAKE ANOTHER PASS THROUGH THE DATA.

THE SAME TRANSFORMATIONS AND SELECTIONS AS LAST RUN WILL BE USED IN THIS RUN.



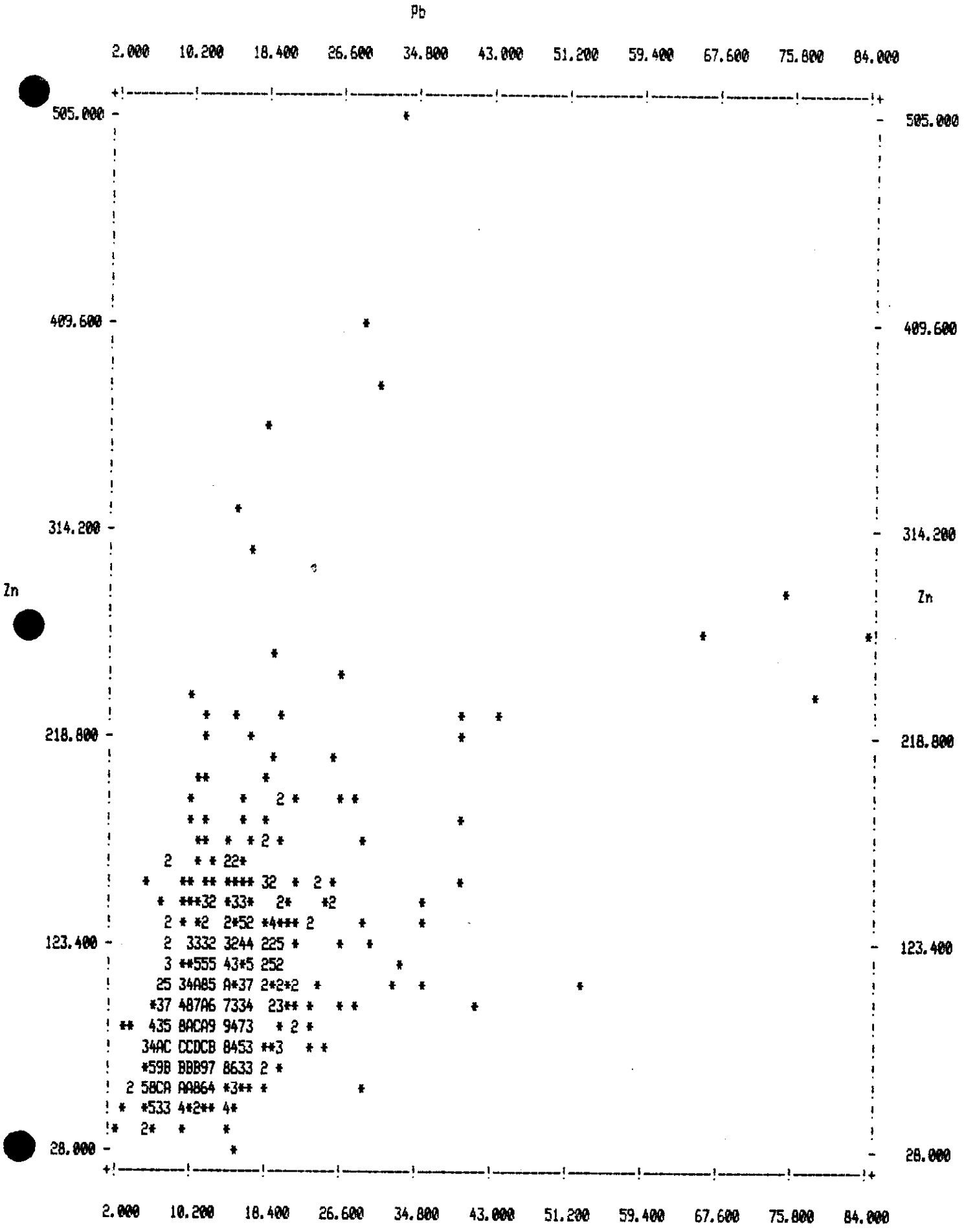
0 POINTS OUT OF RANGE

STATISTICS FOR VARIABLES:	Cu	Zn
NUMBER OF OBSERVATIONS:	828	828
MINIMUM:	9.00	28.00
MAXIMUM:	100.00	505.00
MEAN:	26.27	95.65
STANDARD ERROR OF MEAN:	0.39	1.55
STANDARD DEVIATION:	11.13	44.74
COEFFICIENT OF VARIATION:	42.36	46.77
SKEWNESS:	2.20	3.05
KURTOSIS:	8.03	16.40
CORRELATION COEFFICIENT:	0.0905	

****

WE WILL NOW MAKE ANOTHER PASS THROUGH THE DATA.

THE SAME TRANSFORMATIONS AND SELECTIONS AS LAST RUN WILL BE USED IN THIS RUN.



0 POINTS OUT OF RANGE

STATISTICS FOR VARIABLES:	Pb	Zn
NUMBER OF OBSERVATIONS:	828	828
MINIMUM:	2.00	28.00
MAXIMUM:	84.00	505.00
MEAN:	13.09	95.65
STANDARD ERROR OF MEAN:	0.25	1.55
STANDARD DEVIATION:	7.17	44.74
COEFFICIENT OF VARIATION:	54.80	46.77
SKEWNESS:	4.28	3.05
KURTOSIS:	30.97	16.40

CORRELATION COEFFICIENT: 0.5429

Symbol	Number of samples at that point
*	1
2	2
3	3
4	4
5	5
6	6
7	7
8	8
9	9
A	10-11
B	12-15
C	16-20
D	21-30
E	31-50
F	) 50

Relationship between X-Y plot symbols
and number of samples

MOUNT MAHON PROJECT

YAHK, B. C.

CHEVRON CANADA RESOURCES LIMITED

GRAVITY SURVEY 1983

Ager, Berretta & Ellis
#606 - 595 Howe Street
Vancouver, B. C.

AGER, BERRETTA & ELLIS INC.

Telephone: (604) 669-7748
CONSULTING
GEOPHYSICISTS
606 - 595 Howe Street
Vancouver, B.C., Canada
V6C 2T5

SUMMARY

A gravity survey was completed over Chevron's Mount Mahon project, Yahk, B. C. during the fall of 1983. Station interval was 100 metres on lines 200 metres apart. The purpose was to investigate the potential for extensive massive sulphides. Data analysis indicates that most variations in the gravitational field can be explained by lithological variations or topography. One significant potential target remains in the north east corner of the grid.

Respectfully submitted,

Gregory Paquin

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LIST OF FIGURES

MOUNT MAHON PROJECT, YAHK, B. C.
GRAVITY SURVEY

At the request of Chevron Standard Limited, Minerals Division, Ager, Berretta & Ellis Inc. completed a gravity survey on the Mount Mahon Grid near Yahk, B.C.(Figure 1). The purpose of the work was to assist in the search for massive sulphides.

SURVEY PROCEDURE

The ABE crew stayed in a hotel in Yahk and used a truck for transportation to and from the job site. The gravity base for the survey was established at line 0 stn. 0, next to the drill hole(Y-6).

Gravity observations were made using a LaCoste & Romberg model G gravity meter(#618) with a reading accuracy of +0.01 milligals. Instrument and diurnal drift were accounted for by tying to the base station and to temporary base stations on the grid and drifting the data accordingly.

Elevations were determined by the use of an electronic level developed by ABE. Standard survey closure methods were used and station elevations were calculated to within a relative accuracy of ±0.03 meters.

Field results were calculated and plotted in the field. Final data preparation was completed in the Vancouver office.

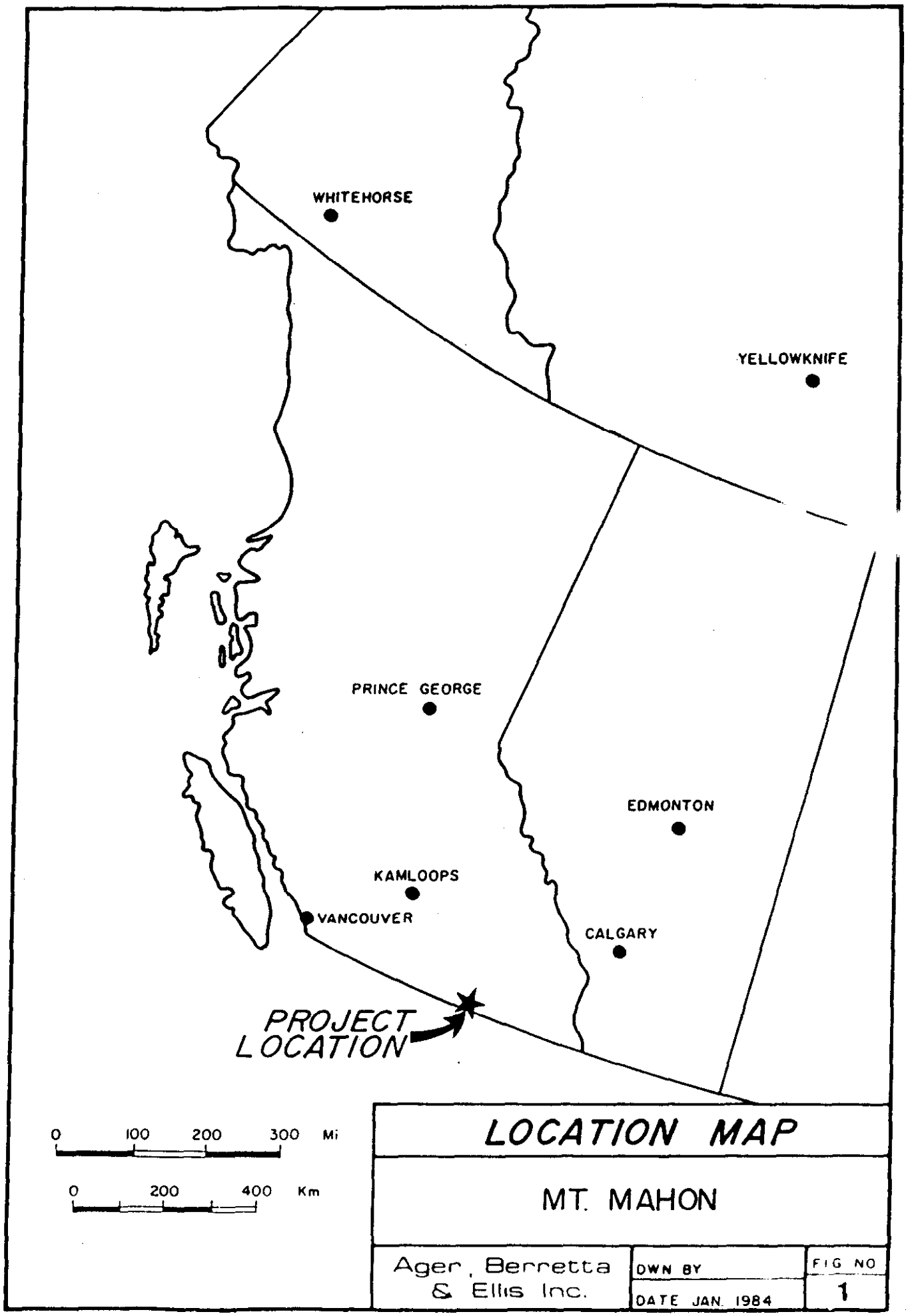
GEOLOGY

The survey area lies on the eastern flank of a gently folded anticline, with Mount Mahon very near the axis. The formation is plunging to the north. The area contains sandstone, siltstone, argillites and some conglomerates of the Aldridge Formation. A more complete description of the geology can be found in "Geology of Mount Mahon Area (Yahk Claim Group)" as completed by Larry Decker of Chevron Canada Resources Limited.

DATA REDUCTION

A brief outline of gravity fundamentals is included as Appendix I.

The survey area crossed several statigraphic layers of varying densities. From correlation of gravity values Elevation Density Factors for different rock units were determined. For the higher elevation area of Mount Mahon



LOCATION MAP

MT. MAHON

Ager, Berretta & Ellis Inc.	DWN BY	FIG NO
	DATE JAN. 1984	1

(above 1700 meters) a density of 2.10 grams per cc was derived. The remaining portion of the grid was evaluated at 2.67 grams per cc yielding an overall average elevation density factor of 2.45 grams per cc.

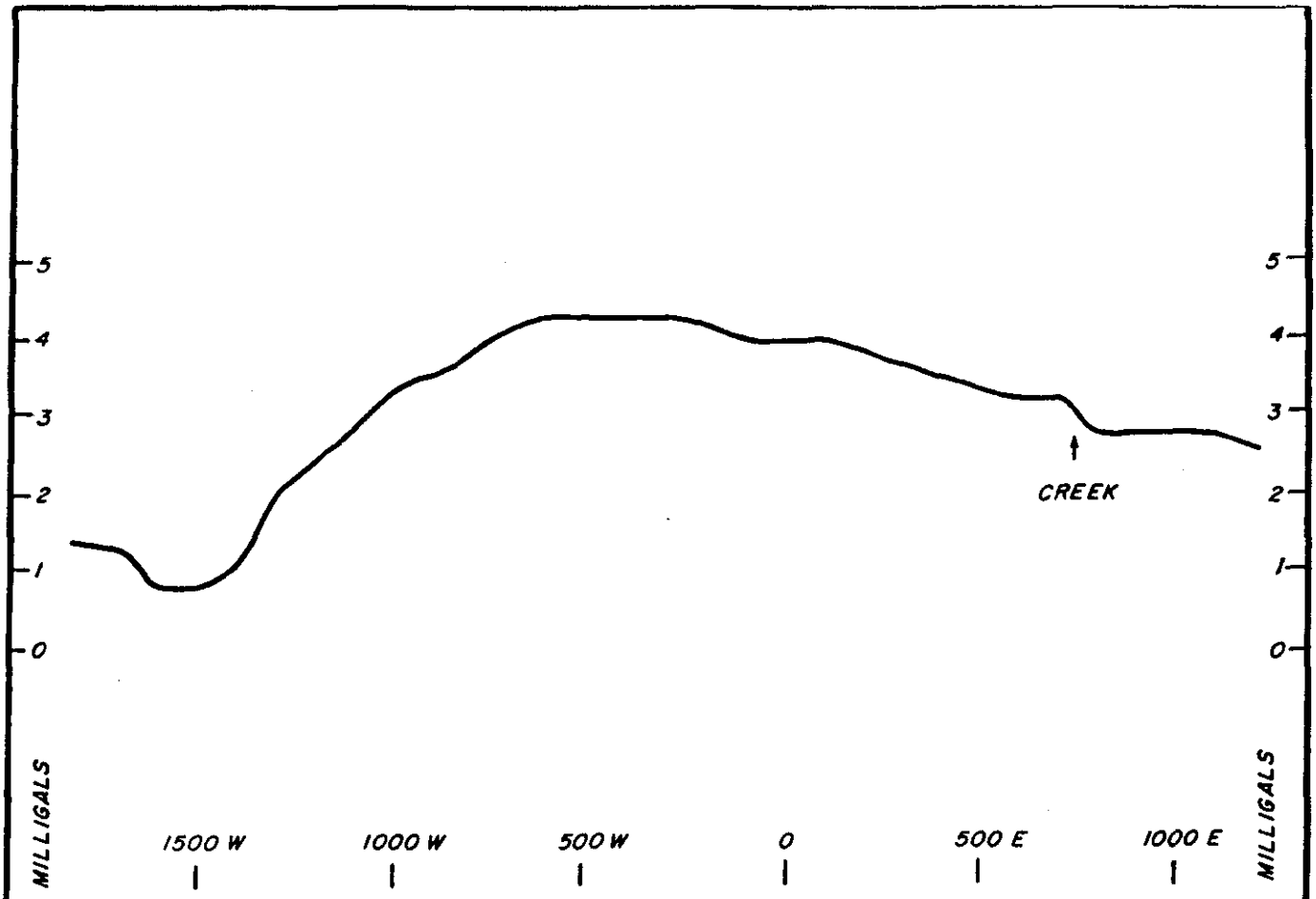
A density of 2.67 grams per cc was used for terrain correction calculations. The resulting Complete Bouguer Gravity Map is given as Figure 7.

INTEPRETATION

Several features can be observed from the Complete Bouguer Gravity Map.

A gravity high trends across the grid 200 to 400 meters west of the base line. This feature shifts to the west if the elevation density factor is lowered slightly and becomes only a gradient at an elevation correction factor of 2.1 grams per cc (see Figures 2, 3, & 4). Using geological information supplied by Chevron, line 0 has been modelled. As can be been on Figure 6, variations in gravitational fields can be explained by changes in local geology.

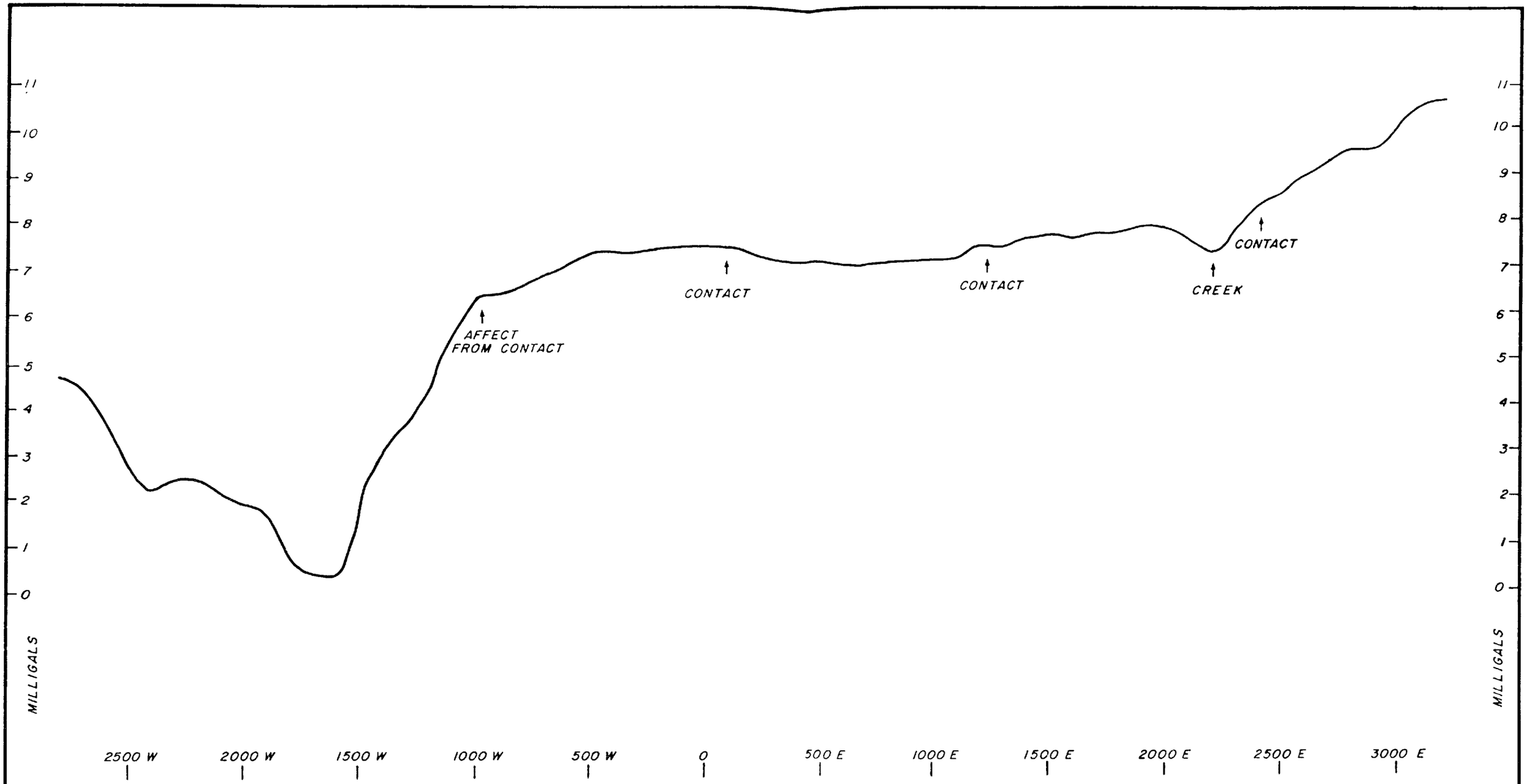
In the eastern portion of the grid a gravity low, indicative of stream sediments, can be observed at line 10 north, 200 east trending south along the existing stream. This low separates, and accentuates a gravity high on lines 8 and 10 north. Observation of gravity profiles at various different density factors indicates that this feature is not topographically related. The feature is not closed off to the north east. If this area is geologically favourable, further investigations are warranted.



GRAVITY PROFILE LINE 8 S

CHEVRON CANADA RESOURCES LTD.
YAHK, B.C.

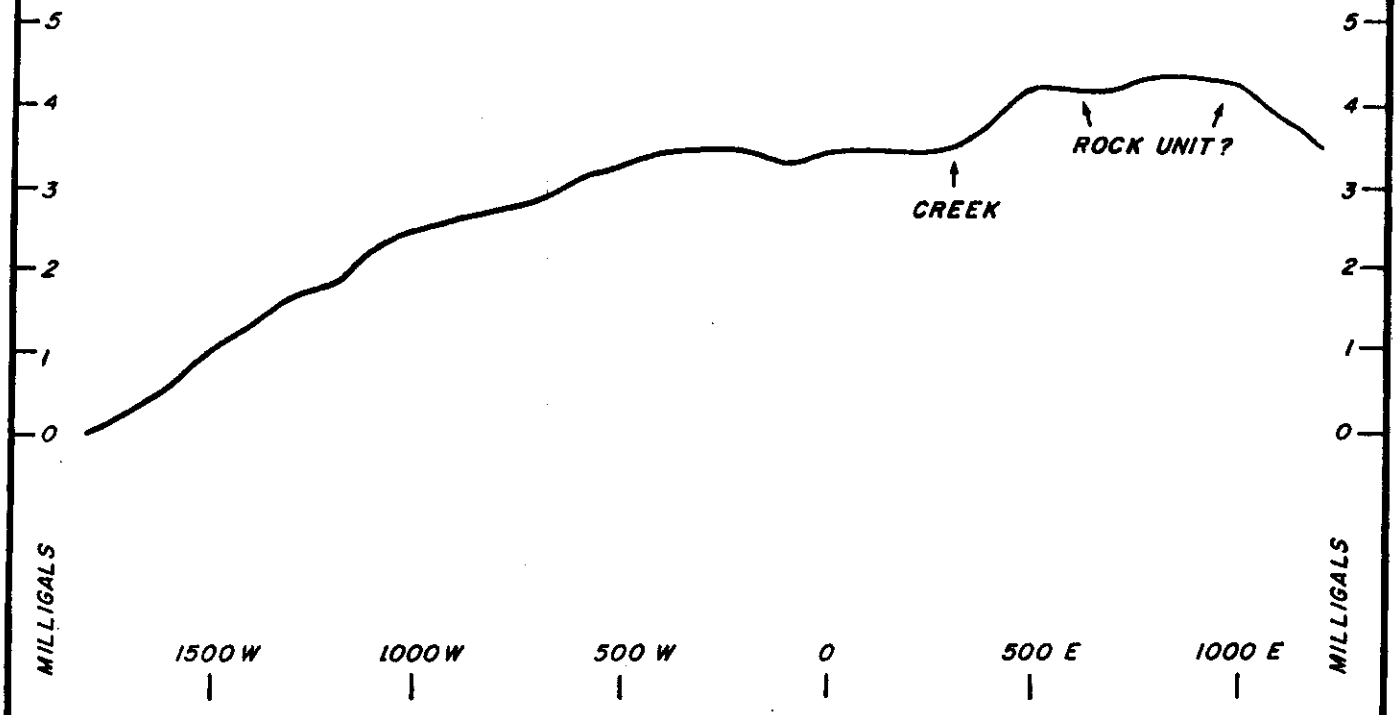
Ager, Berretta & Ellis Inc.	DWN. BY: B.J.C.	FIG. NO.
	DATE: JAN. 1984	2



GRAVITY PROFILE LINE 0

CHEVRON CANADA RESOURCES LTD.
YAHK, B.C.

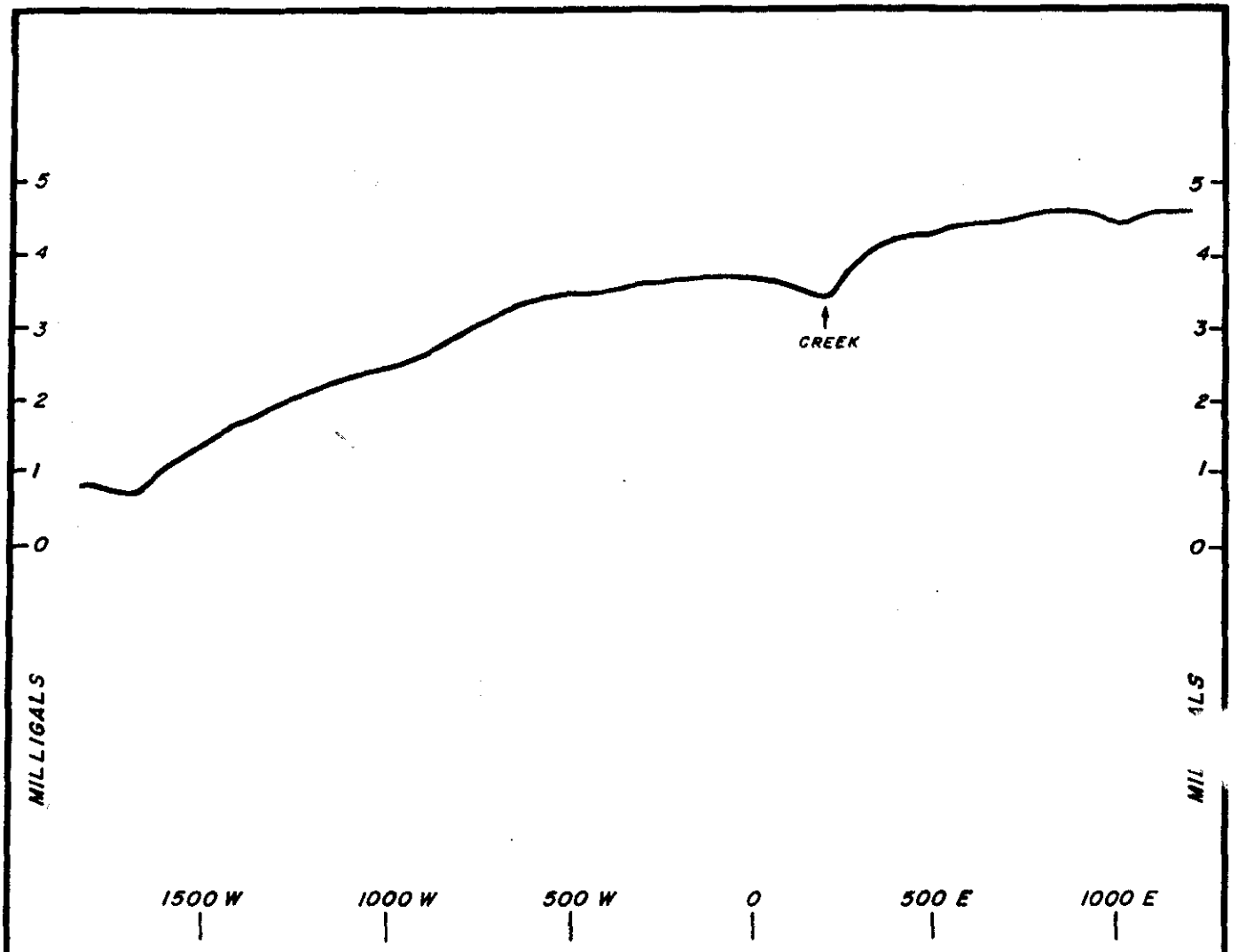
Ager, Berretta & Ellis Inc.	DWN. BY: B.J.C.	FIG. NO. 3
	DATE: JAN. 1984	



GRAVITY PROFILE LINE 8 N

CHEVRON CANADA RESOURCES LTD.
YAHK, B.C.

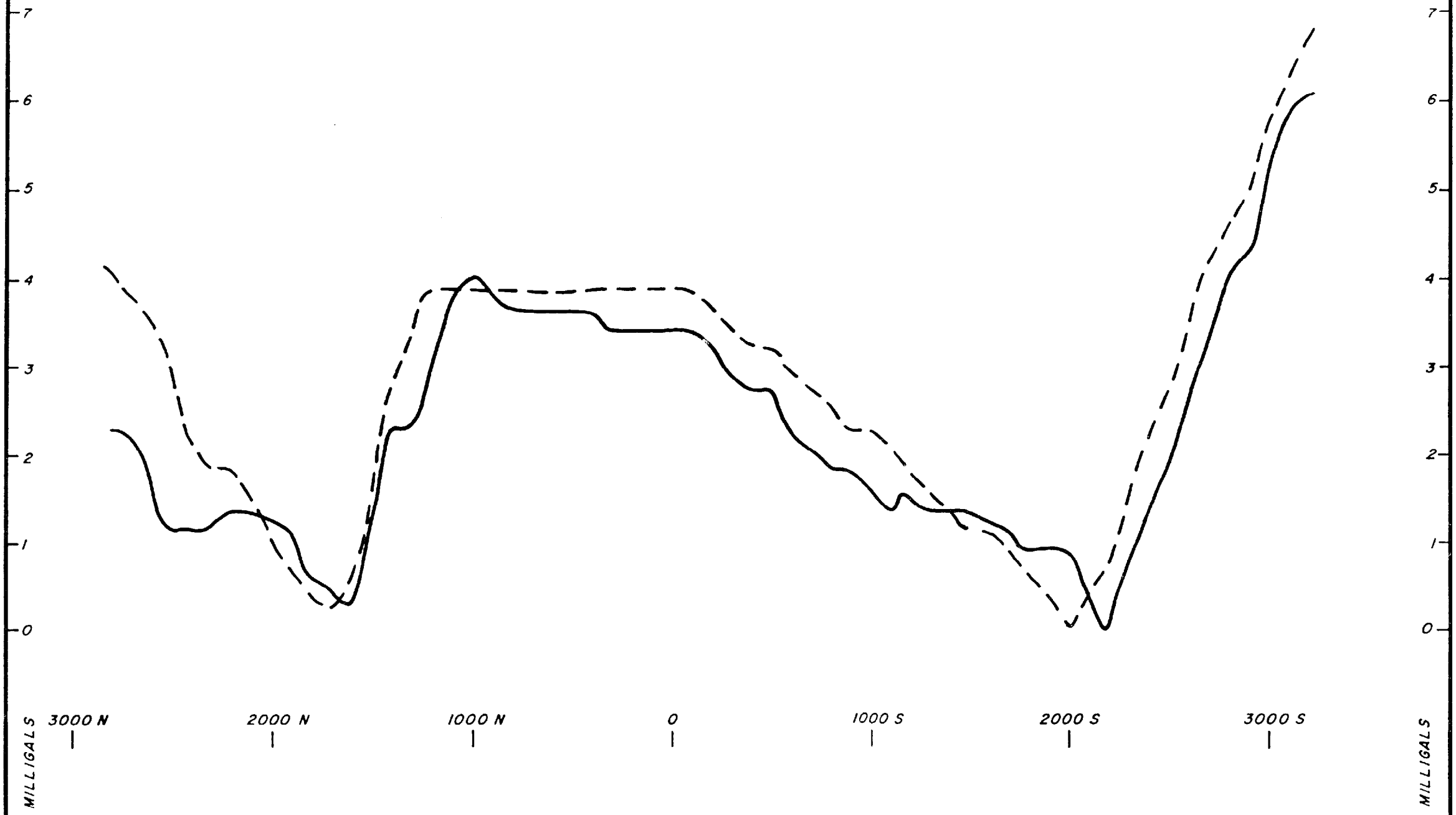
Ager, Berretta & Ellis Inc.	DWN. BY: B.J.C.	FIG. NO.
	DATE: JAN. 1984	4



GRAVITY PROFILE LINE 10 N

CHEVRON CANADA RESOURCES LTD.
YAHK, B.C.

Ager, Berretta & Ellis Inc.	DWN. BY: B.J.C.	FIG. NO.
	DATE: JAN. 1984	5



GRAVITY MODEL LINE 0

CHEVRON CANADA RESOURCES LTD.
YAHK, B.C.

Ager, Berretta & Ellis Inc.	DWN. BY: B.J.C.	FIG. NO.
	DATE: JAN. 1984	6

APPENDIX I

GRAVITY FUNDAMENTALS

There are a number of steps required in order to obtain meaningful, relative gravity values from raw field data. The final values are referred to as Complete Bouguer Gravity and are derived from the following components:

g_o = observed gravity = field observations corrected for drift and adjusted to primary base station gravity datum.

g_{fa} = free air effect = correction for the relative distance of the gravity station from the mass of the earth (point source mass). This calculation assumes a normal free air and corrects for relative differences in distance from the elevation datum.

g_{bs} = Bouguer slab effect = correction for the relative differences in thickness of rock material between gravity stations and the elevation datum. This calculation requires that a mean density for rock types between the lowest and highest grid elevations be established. All stations are then corrected for the gravity effect caused by this assumed slab of the derived density above the elevation datum.

g_l = latitude effect = correction for change of observed gravity with change in latitude - due primarily to the difference in the earth's radius between the poles and equator.

g_t = terrain effect = correction for variations caused by local terrain. The vertical component of the gravitational effect exerted by nearby hills, or not exerted by valleys or gullies, will affect the net reading obtained at any one station. The overall effect on a given line profile or grid area will be a function of the station spacing relative to the frequency of the terrain correction.

Accurate and appropriate application of the above corrections yields Complete Bouguer Gravity values which are, in theory, free from all effects except those caused by relative changes in density within rock units below the survey area.

$$G_{cb} = g_o - (g_{fa} + g_{bs} + g_l + g_t) = \text{Complete Bouguer Gravity.}$$

Changes in relative gravity values which may result in "anomalies" are a function of:

- the difference in densities between rock units;
- the sizes of rock units relative to each other and relative to the grid spacing or "target" size;
- the distance from the area of density contrast to the observation points.

For example: Steeply dipping, near surface massive sulphide deposits or coal seams will give sharp featured gravity anomalies, the former greater than background, the latter less than background. Density contrasts at depth, such as slopes or changes in basement stratigraphy, will result in very low frequency changes, often referred to as gradients.

APPENDIX II

GRAVITY LISTING

Elevation density factor : 2.10 grams per cc above 1700 meters
2.67 grams pre cc below 1700 meters
Gravity datum as printed : arbitrary
Elevation datum : 1524 meters at line 0 station 0
Grid spacing : 100 meter stations on lines offset 200 meters, see Figure X

GRAVITY

Base station at line 0 station 0 : 4158.50 milligals

Field work : 2 October to 14 October 1983

Meter Counter Reading : 4000.00

Pertinent Meter Factor : 1.02681

CREW

Gregory Paquin	Project Geophysicist/ Gravity Observer
Larry Carlson	Surveyor
Tom Roney	Field Assistant

LINE 10S

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLETI BOUGUE
1000S	20.W	1607.46	5273.81	123.33	2.60	3.02	445.14
1000S	19.W	1631.68	5353.28	118.53	2.64	2.92	445.04
1000S	18.W	1659.35	5444.07	112.86	2.68	2.78	444.71
1000S	17.W	1687.75	5537.25	107.18	2.72	2.62	444.50
1000S	16.W	1713.23	5620.83	101.90	2.76	2.51	444.48
1000S	15.W	1732.04	5682.55	97.91	2.80	2.52	444.69
1000S	14.W	1739.53	5707.11	96.37	2.84	2.49	444.81
1000S	13.W	1728.33	5670.37	98.79	2.88	2.39	444.70
1000S	12.W	1703.43	5588.68	104.26	2.92	2.20	444.53
1000S	11.W	1675.62	5497.45	110.25	2.96	2.16	444.96
1000S	10.W	1652.92	5422.98	114.91	3.00	2.18	445.22
1000S	9.W	1630.40	5349.09	119.50	3.04	2.22	445.46
1000S	8.W	1603.77	5261.70	124.80	3.08	2.25	445.59
1000S	7.W	1578.24	5177.95	129.92	3.12	2.24	445.72
1000S	6.W	1554.25	5099.23	134.76	3.16	2.22	445.86
1000S	5.W	1530.63	5021.75	139.62	3.20	2.15	446.05
1000S	4.W	1505.63	4939.72	144.66	3.24	2.04	446.10
1000S	3.W	1485.34	4873.15	148.80	3.28	1.92	446.17
1000S	2.W	1466.18	4810.30	152.71	3.32	1.78	446.21
1000S	1.W	1452.27	4764.66	155.44	3.36	1.70	446.16
1000S	0.	1436.41	4712.64	158.46	3.40	1.57	445.97
1000S	1.E	1417.78	4651.51	162.17	3.44	1.49	445.98
1000S	2.E	1401.12	4596.86	165.46	3.48	1.38	445.92
1000S	3.E	1385.63	4546.03	168.50	3.52	1.23	445.86
1000S	4.E	1370.81	4497.41	171.26	3.56	1.16	445.62
1000S	5.E	1362.48	4470.07	172.84	3.60	1.08	445.52
1000S	6.E	1354.33	4443.33	174.29	3.64	1.00	445.33
1000S	7.E	1346.21	4416.71	175.84	3.68	.98	445.30
1000S	8.E	1342.03	4402.99	176.41	3.72	.95	445.06
1000S	9.E	1331.28	4367.72	178.28	3.76	.92	444.82
1000S	10.E	1313.41	4309.10	181.51	3.80	.88	444.54
1000S	11.E	1314.60	4313.00	181.42	3.84	.82	444.66
1000S	12.E	1317.56	4322.71	180.80	3.88	.84	444.68

LINE 8S

800S	18.W	1719.58	5641.68	99.93	2.54	2.95	444.13
800S	17.W	1739.09	5705.69	95.90	2.58	2.88	444.37
800S	16.W	1758.18	5768.32	91.77	2.62	2.82	444.43
800S	15.W	1760.65	5776.42	91.36	2.66	2.68	444.47
800S	14.W	1740.56	5710.49	95.74	2.70	2.50	444.28
800S	13.W	1711.81	5616.18	102.25	2.74	2.46	444.45
800S	12.W	1683.11	5522.03	108.45	2.78	2.28	444.58
800S	11.W	1655.84	5432.54	114.29	2.82	2.28	445.09
800S	10.W	1632.55	5356.15	119.14	2.86	2.35	445.47

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLETE BOUGUER
800S	9.W	1608.09	5275.88	123.94	2.90	2.38	445.53
800S	8.W	1580.96	5186.88	129.52	2.94	2.39	445.83
800S	7.W	1556.81	5107.63	134.52	2.98	2.35	446.08
800S	6.W	1533.67	5031.72	139.26	3.02	2.22	446.17
800S	5.W	1512.46	4962.15	143.56	3.06	2.09	446.21
800S	4.W	1495.33	4905.94	147.04	3.10	1.98	446.25
800S	3.W	1479.18	4852.96	150.21	3.14	1.88	446.19
800S	2.W	1461.56	4795.15	153.56	3.18	1.78	446.01
800S	1.W	1445.36	4742.01	156.65	3.22	1.70	445.87
800S	0.	1422.54	4667.13	161.09	3.26	1.60	445.76
800S	1.E	1408.61	4621.44	163.91	3.30	1.47	445.75
800S	2.E	1393.70	4572.49	166.83	3.34	1.31	445.62
800S	3.E	1383.36	4538.57	168.78	3.38	1.20	445.47
800S	4.E	1381.44	4532.29	169.10	3.42	1.06	445.31
800S	5.E	1380.06	4527.75	169.18	3.46	.98	445.08
800S	6.E	1377.90	4520.67	169.51	3.50	.97	445.01
800S	7.E	1376.23	4515.21	169.66	3.54	1.00	444.90
800S	8.E	1362.52	4470.20	172.02	3.58	.96	444.57
800S	9.E	1343.31	4407.20	175.70	3.62	.90	444.45
800S	10.E	1349.60	4427.82	174.50	3.66	.80	444.43
800S	11.E	1340.54	4398.08	176.40	3.70	.67	444.45
800S	12.E	1336.24	4383.99	177.27	3.74	.55	444.40
LINE 6S.							
600S	18.W	1769.53	5805.55	88.95	2.40	3.15	444.23
600S	17.W	1784.95	5856.13	85.68	2.44	3.15	444.40
600S	16.W	1789.51	5871.11	84.78	2.48	3.10	444.50
600S	15.W	1768.94	5803.61	89.57	2.52	2.79	444.48
600S	14.W	1738.61	5704.11	96.36	2.56	2.67	444.50
600S	13.W	1708.49	5605.29	102.96	2.60	2.63	444.45
600S	12.W	1676.70	5500.99	109.65	2.64	2.61	444.71
600S	11.W	1646.82	5402.95	115.90	2.68	2.62	445.13
600S	10.W	1618.57	5310.26	121.71	2.72	2.64	445.44
600S	9.W	1587.92	5209.72	127.94	2.76	2.68	445.72
600S	8.W	1559.20	5115.47	133.79	2.80	2.65	445.94
600S	7.W	1535.92	5039.10	138.68	2.84	2.54	446.18
600S	6.W	1517.02	4977.09	142.48	2.88	2.32	446.08
600S	5.W	1501.60	4926.52	145.73	2.92	2.15	446.17
600S	4.W	1485.84	4874.81	148.97	2.96	2.02	446.22
600S	3.W	1469.86	4822.36	152.04	3.00	1.95	446.11
600S	2.W	1449.04	4754.07	156.03	3.04	1.90	446.0(
600S	1.W	1429.32	4689.36	159.94	3.08	1.83	446.0(
600S	0.	1413.65	4637.96	163.04	3.12	1.74	445.9(
600S	1.E	1408.06	4619.61	164.10	3.16	1.56	445.7(
600S	2.E	1406.13	4613.30	164.27	3.20	1.30	445.3(
600S	3.E	1408.93	4622.48	163.54	3.24	1.17	445.0(

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLET BOUGUE
600S	4.E	1411.75	4631.72	163.07	3.28	1.08	445.12
600S	5.E	1411.60	4631.25	162.92	3.32	1.02	444.92
600S	6.E	1405.52	4611.30	164.37	3.36	1.04	445.24
600S	7.E	1402.21	4600.44	164.73	3.40	1.07	445.02
600S	8.E	1388.33	4554.90	167.48	3.44	1.02	445.02
600S	9.E	1374.47	4509.41	170.24	3.48	.95	445.03
600S	10.E	1361.89	4468.14	172.73	3.52	.90	445.03
600S	11.E	1349.86	4428.67	175.10	3.56	.84	445.02
600S	12.E	1339.71	4395.36	177.04	3.60	.82	444.98
LINE 4S							
400S	18.W	1820.45	5972.60	77.45	2.26	3.70	444.37
400S	17.W	1830.68	6006.17	75.25	2.30	3.80	444.57
400S	16.W	1828.97	6000.57	75.71	2.34	3.85	444.74
400S	15.W	1804.04	5918.77	81.38	2.38	3.60	444.70
400S	14.W	1765.56	5792.53	89.89	2.42	3.30	444.46
400S	13.W	1732.24	5683.19	97.33	2.46	3.06	444.35
400S	12.W	1697.75	5570.05	104.77	2.50	2.95	444.17
400S	11.W	1663.72	5458.39	111.85	2.54	2.87	444.51
400S	10.W	1632.83	5357.05	118.34	2.58	2.80	444.90
400S	9.W	1601.89	5255.53	124.68	2.62	2.75	445.14
400S	8.W	1572.78	5160.04	130.53	2.66	2.68	445.24
400S	7.W	1546.47	5073.72	135.87	2.70	2.61	445.37
400S	6.W	1524.96	5003.15	140.33	2.74	2.45	445.48
400S	5.W	1505.04	4937.80	144.38	2.78	2.33	445.53
400S	4.W	1484.27	4869.65	148.57	2.82	2.24	445.59
400S	3.W	1464.27	4804.04	152.74	2.86	2.04	445.66
400S	2.W	1459.33	4787.82	153.92	2.90	1.73	445.60
400S	1.W	1455.26	4774.49	154.90	2.94	1.58	445.67
400S	0.	1452.02	4763.86	155.44	2.98	1.46	445.49
400S	1.E	1450.50	4758.85	155.61	3.02	1.37	445.31
400S	2.E	1455.69	4775.88	154.54	3.06	1.30	445.23
400S	3.E	1450.90	4760.18	155.59	3.10	1.20	445.28
400S	4.E	1444.58	4739.44	156.83	3.14	1.18	445.30
400S	5.E	1435.43	4709.42	158.64	3.18	1.16	445.33
400S	6.E	1424.88	4674.79	160.65	3.22	1.13	445.27
400S	7.E	1412.03	4632.63	163.06	3.26	1.10	445.17
400S	8.E	1395.75	4579.22	166.27	3.30	1.06	445.17
400S	9.E	1380.71	4529.90	169.09	3.34	1.01	445.03
400S	10.E	1366.43	4483.04	171.84	3.38	.99	444.99
400S	11.E	1352.63	4437.77	174.56	3.42	.98	445.02
400S	12.E	1338.63	4391.83	177.25	3.46	.95	444.97

LINE 2S

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLETI BOUGUE
200S	18.W	1870.35	6136.32	65.85	2.12	4.70	444.64
200S	17.W	1890.14	6201.25	60.53	2.16	5.10	444.12
200S	16.W	1871.45	6139.93	65.00	2.20	4.44	443.85
200S	15.W	1829.51	6002.32	75.13	2.24	3.90	444.23
200S	14.W	1790.77	5875.24	83.97	2.28	3.60	444.26
200S	13.W	1755.44	5759.33	92.10	2.32	3.35	444.39
200S	12.W	1717.53	5634.93	100.42	2.36	3.15	444.19
200S	11.W	1682.84	5521.11	108.01	2.40	2.92	444.35
200S	10.W	1651.41	5418.02	114.83	2.44	2.74	444.84
200S	9.W	1626.35	5335.81	120.02	2.48	2.62	445.02
200S	8.W	1603.13	5259.61	124.95	2.52	2.53	445.34
200S	7.W	1577.88	5176.77	130.30	2.56	2.42	445.65
200S	6.W	1554.53	5100.16	135.06	2.60	2.28	445.72
200S	5.W	1531.05	5023.12	139.89	2.64	2.05	445.74
200S	4.W	1513.39	4965.20	143.51	2.68	1.82	445.69
200S	3.W	1505.87	4940.52	145.27	2.72	1.63	445.83
200S	2.W	1493.22	4899.02	147.77	2.76	1.48	445.73
200S	1.W	1490.04	4888.60	148.38	2.80	1.38	445.65
200S	0.	1493.11	4898.66	147.69	2.84	1.34	445.57
200S	1.E	1493.29	4899.26	147.66	2.88	1.30	445.57
200S	2.E	1490.52	4890.17	148.18	2.92	1.27	445.56
200S	3.E	1480.83	4858.37	149.99	2.96	1.24	445.47
200S	4.E	1468.28	4817.18	152.29	3.00	1.22	445.32
200S	5.E	1454.50	4771.98	154.94	3.04	1.23	445.31
200S	6.E	1441.43	4729.09	157.55	3.08	1.22	445.38
200S	7.E	1423.00	4668.64	161.11	3.12	1.19	445.32
200S	8.E	1404.31	4607.31	164.86	3.16	1.15	445.4C
200S	9.E	1388.48	4555.39	167.94	3.20	1.12	445.37
200S	10.E	1372.12	4501.70	171.20	3.24	1.08	445.42
200S	11.E	1356.06	4449.02	174.20	3.28	1.04	445.26
200S	12.E	1331.26	4367.65	178.90	3.32	1.02	445.1C

BASE LINE NORTH-SOUTH

0	-28.W	1669.07	5475.95	109.62	1.58	3.45	442.9(
0	-27.W	1702.93	5587.04	102.64	1.62	3.39	442.6(
0	-26.W	1738.23	5702.85	95.06	1.66	3.30	442.8
0	-25.W	1769.91	5806.79	88.01	1.70	3.10	442.6
0	-24.W	1796.66	5894.55	82.47	1.74	2.98	442.9(
0	-23.W	1797.58	5897.58	82.94	1.78	2.50	443.1
0	-22.W	1804.85	5921.42	81.46	1.82	2.48	443.2
0	-21.W	1822.66	5979.86	77.49	1.86	2.73	443.5
0	-20.W	1846.61	6058.42	71.91	1.90	3.20	443.7
0	-19.W	1867.20	6126.00	67.07	1.94	3.85	444.1
0	-18.W	1896.19	6221.10	59.67	1.98	4.65	443.9
0	-17.W	1908.06	6260.04	56.51	2.02	5.10	443.9
0	-16.W	1900.21	6234.28	58.10	2.06	5.00	443.7

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLETI BOUGUEI
0	-15.W	1861.78	6108.19	67.53	2.10	4.35	444.06
0	-14.W	1821.41	5975.74	77.18	2.14	3.90	444.39
0	-13.W	1787.64	5864.97	84.60	2.18	3.60	444.10
0	-12.W	1744.89	5724.72	94.12	2.22	3.25	443.88
0	-11.W	1702.68	5586.21	103.88	2.26	2.92	444.04
0	-10.W	1671.39	5483.56	111.04	2.30	2.62	444.72
0	-9.W	1649.46	5411.63	115.39	2.34	2.48	444.66
0	-8.W	1621.90	5321.18	121.09	2.38	2.38	444.88
0	-7.W	1595.41	5234.29	126.64	2.42	2.23	445.11
0	-6.W	1575.06	5167.53	130.89	2.46	2.08	445.24
0	-5.W	1552.04	5092.01	135.78	2.50	1.86	445.43
0	-4.W	1537.21	5043.34	138.93	2.54	1.62	445.46
0	-3.W	1529.19	5017.04	140.71	2.58	1.43	445.51
0	-2.W	1520.14	4987.35	142.55	2.62	1.36	445.54
0	-1.W	1525.70	5005.57	141.42	2.66	1.33	445.52
0	0.	1524.00	5000.00	141.78	2.70	1.30	445.55
0	1.E	1517.82	4979.73	142.97	2.74	1.28	445.55
0	2.E	1509.33	4951.87	144.46	2.78	1.27	445.40
0	3.E	1494.51	4903.25	147.26	2.82	1.26	445.31
0	4.E	1477.65	4847.94	150.50	2.86	1.25	445.26
0	5.E	1462.42	4797.95	153.46	2.90	1.24	445.26
0	6.E	1445.30	4741.81	156.65	2.94	1.23	445.11
0	7.E	1423.89	4671.54	160.79	2.98	1.22	445.07
0	8.E	1405.51	4611.26	164.40	3.02	1.21	445.09
0	9.E	1387.71	4552.87	167.94	3.06	1.18	445.14
0	10.E	1362.44	4469.95	172.90	3.10	1.12	445.11
0	11.E	1351.32	4433.46	175.08	3.14	1.08	445.11
0	12.E	1337.81	4389.13	177.94	3.18	1.05	445.32
0	13.E	1324.57	4345.69	180.60	3.22	1.00	445.36
0	14.E	1304.21	4278.91	184.67	3.26	.94	445.41
0	15.E	1289.28	4229.93	187.78	3.30	.87	445.55
0	16.E	1279.15	4196.70	190.00	3.04	.84	445.49
0	17.E	1266.86	4156.38	192.43	3.08	.87	445.57
0	18.E	1246.47	4089.48	196.29	3.12	.89	445.48
0	19.E	1235.85	4054.62	198.47	3.16	.92	445.64
0	20.E	1221.69	4008.16	201.15	3.20	1.04	445.70
0	21.E	1222.02	4009.26	200.55	3.24	1.22	445.38
0	22.E	1221.65	4008.04	200.12	3.28	1.30	445.00
0	23.E	1258.51	4128.98	193.26	3.32	1.37	445.50
0	24.E	1264.74	4149.41	192.39	3.36	1.60	446.12
0	25.E	1273.38	4177.76	190.54	3.40	1.88	446.29
0	26.E	1308.37	4292.56	183.90	3.44	2.07	446.77
0	27.E	1334.21	4377.34	178.92	3.48	2.24	447.08
0	28.E	1363.75	4474.26	173.26	3.52	2.48	447.51
0	29.E	1393.36	4571.39	167.39	3.56	2.55	447.57
0	30.E	1427.92	4684.79	160.93	3.60	2.62	448.02
0	31.E	1457.25	4780.99	155.56	3.64	2.62	448.46
0	32.E	1461.69	4795.56	155.04	3.66	2.52	448.73

LINE 2N

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLETE BOUGUE
200N	18.W	1894.48	6215.50	60.30	1.84	4.08	443.51
200N	17.W	1886.98	6190.89	62.19	1.88	4.10	443.81
200N	16.W	1879.16	6165.22	63.82	1.92	4.12	443.77
200N	15.W	1862.87	6111.79	67.91	1.96	4.00	444.19
200N	14.W	1831.02	6007.29	75.38	2.00	3.65	444.32
200N	13.W	1801.32	5909.84	82.11	2.04	3.30	444.19
200N	12.W	1763.82	5786.82	90.56	2.08	3.05	444.16
200N	11.W	1726.23	5663.48	99.13	2.12	2.72	444.15
200N	10.W	1689.69	5543.61	107.38	2.16	2.47	444.37
200N	9.W	1664.68	5461.55	112.86	2.20	2.25	444.75
200N	8.W	1645.99	5400.24	116.79	2.24	2.14	444.94
200N	7.W	1621.88	5321.13	121.81	2.28	2.00	445.11
200N	6.W	1595.07	5233.17	127.40	2.32	1.80	445.27
200N	5.W	1579.04	5180.59	130.73	2.36	1.60	445.29
200N	4.W	1564.12	5131.62	133.80	2.40	1.46	445.32
200N	3.W	1550.64	5087.39	136.57	2.44	1.37	445.39
200N	2.W	1551.89	5091.49	136.43	2.48	1.34	445.51
200N	1.W	1547.28	5076.37	137.31	2.52	1.30	445.48
200N	0.W	1535.27	5036.96	139.69	2.56	1.25	445.49
200NE	1.	1523.08	4996.97	142.03	2.60	1.27	445.49
200NE	2.	1508.16	4948.03	144.87	2.64	1.31	445.48
200NE	3.	1491.55	4893.53	148.12	2.68	1.32	445.51
200NE	4.	1476.77	4845.05	150.87	2.72	1.30	445.37
200NE	5.	1457.36	4781.35	154.60	2.76	1.26	445.28
200NE	6.	1438.18	4718.43	158.33	2.80	1.23	445.25
200NE	7.	1416.39	4646.94	162.60	2.84	1.20	445.24
200NE	8.	1393.96	4573.35	166.97	2.88	1.20	445.24
200NE	9.	1373.41	4505.95	171.00	2.92	1.17	445.24
200NE	10.	1372.54	4503.10	171.14	2.96	1.14	445.22
200NE	11.	1363.83	4474.50	172.71	3.00	1.12	445.10
200NE	12.	1345.81	4415.40	176.32	3.04	1.10	445.18

LINE 4N

400NW	23.	1841.52	6041.73	71.74	1.50	4.20	443.05
400NW	22.	1842.36	6044.49	72.07	1.54	3.40	442.80
400NW	21.	1834.48	6018.63	74.62	1.58	2.92	443.18
400NW	20.	1838.61	6032.20	73.81	1.62	2.86	443.26
400NW	19.	1839.18	6034.05	73.88	1.66	2.82	443.4
400NW	18.	1832.76	6012.98	75.65	1.70	2.58	443.61
400NW	17.	1829.15	6001.16	76.54	1.74	2.58	443.74
400NW	16.	1818.63	5966.64	79.12	1.78	2.55	444.01
400NW	15.	1805.84	5924.67	82.04	1.82	2.55	444.1
400NW	14.	1791.97	5879.17	85.18	1.86	2.58	444.3
400NW	13.	1773.66	5819.10	89.25	1.90	2.50	444.2
400NW	12.	1748.00	5734.91	95.13	1.94	2.38	444.4
400NW	11.	1725.82	5662.15	100.09	1.98	2.24	444.4

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLET BOUGUE
400NW	10.	1697.96	5570.74	106.23	2.04	2.12	444.38
400NW	9.	1677.81	5504.62	110.45	2.06	2.00	444.54
400NW	8.	1652.05	5420.12	115.89	2.10	1.89	444.84
400NW	7.	1631.94	5354.15	120.15	2.14	1.77	445.06
400NW	6.	1607.66	5274.48	125.47	2.18	1.58	445.46
400NW	5.	1596.59	5238.15	127.71	2.22	1.43	445.41
400NW	4.	1581.69	5189.27	130.85	2.26	1.36	445.59
400NW	3.	1572.73	5159.87	132.57	2.30	1.33	445.56
400NW	2.	1561.55	5123.18	134.79	2.34	1.29	445.58
400NW	1.	1549.33	5083.10	137.14	2.38	1.27	445.54
400N	0.	1533.13	5029.95	140.23	2.42	1.28	445.5C
400NE	1.	1515.87	4973.34	143.56	2.46	1.30	445.49
400NE	2.	1499.44	4919.42	146.84	2.50	1.40	445.6E
400NE	3.	1482.99	4865.44	149.81	2.54	1.44	445.49
400NE	4.	1457.76	4782.69	154.74	2.58	1.30	445.36
400NE	5.	1435.82	4710.70	158.98	2.62	1.22	445.25
400NE	6.	1411.12	4629.67	163.89	2.66	1.22	445.34
400NE	7.	1398.56	4588.45	166.29	2.70	1.18	445.27
400NE	8.	1399.43	4591.32	166.06	2.74	1.15	445.22
400NE	9.	1399.82	4592.59	165.81	2.78	1.19	445.12
400NE	10.	1384.83	4543.41	168.64	2.82	1.21	445.07
400NE	11.	1362.08	4468.77	173.27	2.86	1.20	445.25
400NE	12.	1344.80	4412.09	176.70	2.90	1.18	445.3C
LINE 6N							
600NW	18.	1786.82	5862.27	86.53	1.56	1.96	443.5
600NW	17.	1786.95	5862.69	86.69	1.60	2.00	443.8
600NW	16.	1780.46	5841.41	88.21	1.64	1.94	443.9
600NW	15.	1762.48	5782.42	92.26	1.68	1.88	443.9
600NW	14.	1750.52	5743.16	95.01	1.72	1.86	444.1
600NW	13.	1735.18	5692.84	98.44	1.76	1.84	444.1
600NW	12.	1718.83	5639.21	102.20	1.80	1.79	444.3
600NW	11.	1704.07	5590.78	105.41	1.84	1.78	444.3
600NW	10.	1692.36	5552.36	107.89	1.88	1.78	444.4
600NW	9.	1673.60	5490.80	111.80	1.92	1.78	444.7
600NW	8.	1655.19	5430.41	115.46	1.96	1.72	444.7
600NW	7.	1630.55	5349.56	120.65	2.00	1.60	444.9
600NW	6.	1608.71	5277.91	125.29	2.04	1.45	445.2
600NW	5.	1598.03	5242.88	127.47	2.08	1.37	445.2
600NW	4.	1584.03	5196.95	130.41	2.12	1.33	445.4
600NW	3.	1571.08	5154.47	132.91	2.16	1.29	445.3
600NW	2.	1555.87	5104.56	136.01	2.20	1.27	445.5
600NW	1.	1541.38	5057.01	138.77	2.24	1.25	445.4
600N	0.	1520.90	4989.83	142.67	2.28	1.27	445.3
600NE	1.	1501.85	4927.32	146.31	2.32	1.29	445.3
600NE	2.	1483.27	4866.37	149.77	2.36	1.35	445.2

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLETI BOUGUEI
600NE	3.	1456.97	4780.08	154.91	2.40	1.40	445.30
600NE	4.	1426.49	4680.07	160.71	2.44	1.29	445.03
600NE	5.	1430.75	4694.07	160.16	2.48	.96	445.03
600NE	6.	1432.19	4698.79	160.14	2.52	1.05	445.42
600NE	7.	1424.07	4672.13	161.85	2.56	1.12	445.64
600NE	8.	1412.99	4635.81	164.09	2.60	1.17	445.80
600NE	9.	1405.25	4610.41	165.45	2.64	1.21	445.71
600NE	10.	1386.18	4547.83	169.02	2.68	1.24	445.60
600NE	11.	1366.43	4483.03	172.62	2.72	1.24	445.36
600NE	12.	1343.18	4406.77	177.24	2.76	1.21	445.41
LINE 8N							
800NW	18.	1744.74	5724.22	96.31	1.42	1.40	443.39
800NW	17.	1741.73	5714.35	97.23	1.46	1.36	443.65
800NW	16.	1731.24	5679.93	99.47	1.50	1.35	443.60
800NW	15.	1719.99	5643.03	102.13	1.54	1.36	443.83
800NW	14.	1709.41	5608.29	104.35	1.58	1.37	443.77
800NW	13.	1695.96	5564.16	107.38	1.62	1.37	443.97
800NW	12.	1688.63	5540.14	108.84	1.66	1.38	444.03
800NW	11.	1673.35	5490.00	112.17	1.70	1.38	444.40
800NW	10.	1664.02	5459.39	114.21	1.74	1.41	444.67
800NW	9.	1655.06	5429.99	115.94	1.78	1.49	444.76
800NW	8.	1637.38	5371.98	119.44	1.82	1.52	444.85
800NW	7.	1615.74	5300.99	123.87	1.86	1.46	445.01
800NW	6.	1597.65	5241.64	127.77	1.90	1.38	445.31
800NW	5.	1584.63	5198.91	130.45	1.94	1.34	445.43
800NW	4.	1568.99	5147.59	133.69	1.98	1.29	445.58
800NW	3.	1555.45	5103.18	136.32	2.02	1.27	445.57
800NW	2.	1542.81	5061.72	138.79	2.06	1.25	445.57
800NW	1.	1530.50	5021.34	141.01	2.10	1.23	445.39
800N	0.	1506.78	4943.52	145.74	2.14	1.22	445.48
800NE	1.	1484.19	4869.39	150.10	2.18	1.21	445.43
800NE	2.	1459.16	4787.27	154.97	2.22	1.14	445.35
800NE	3.	1454.16	4770.85	156.10	2.26	1.02	445.41
800NE	4.	1458.71	4785.81	155.39	2.30	1.05	445.67
800NE	5.	1451.98	4763.71	156.99	2.34	1.18	446.11
800NE	6.	1440.50	4726.06	159.21	2.38	1.13	446.07
800NE	7.	1429.43	4689.73	161.42	2.42	1.17	446.1[illegible]
800NE	8.	1418.30	4653.21	163.67	2.46	1.21	446.3[illegible]
800NE	9.	1404.40	4607.60	166.18	2.50	1.25	446.1[illegible]
800NE	10.	1385.93	4547.00	169.61	2.54	1.27	446.0[illegible]
800NE	11.	1366.50	4483.26	172.94	2.58	1.23	445.5[illegible]
800NE	12.	1343.58	4408.06	177.22	2.62	1.19	445.31

LINE 10N

	STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLETI BOUGUEI
1000NW	18.	1722.07	5649.84	101.80	1.28	1.17	443.51
1000NW	17.	1721.95	5649.46	101.83	1.32	1.06	443.44
1000NW	16.	1714.14	5623.81	103.67	1.36	1.03	443.57
1000NW	15.	1701.02	5580.78	106.54	1.40	1.04	443.60
1000NW	14.	1688.96	5541.21	109.12	1.44	1.07	443.85
1000NW	13.	1678.99	5508.48	111.20	1.48	1.10	444.04
1000NW	12.	1666.95	5469.00	113.75	1.52	1.14	444.30
1000NW	11.	1658.45	5441.10	115.50	1.56	1.18	444.46
1000NW	10.	1650.06	5413.58	117.20	1.60	1.23	444.60
1000NW	9.	1640.05	5380.74	119.15	1.64	1.30	444.69
1000NW	8.	1621.91	5321.23	122.95	1.68	1.36	445.02
1000NW	7.	1606.41	5270.37	126.21	1.72	1.35	445.26
1000NW	6.	1585.37	5201.33	130.47	1.76	1.28	445.35
1000NW	5.	1567.84	5143.84	134.05	1.80	1.24	445.48
1000NW	4.	1553.53	5096.88	136.89	1.84	1.20	445.51
1000NW	3.	1539.20	5049.88	139.76	1.88	1.19	445.59
1000NW	2.	1524.95	5003.13	142.50	1.92	1.19	445.57
1000NW	1.	1503.88	4933.99	146.62	1.96	1.18	445.57
1000N	0.	1489.63	4887.25	149.37	2.00	1.15	445.53
1000 N	1. E	1481.15	4859.42	150.97	2.04	1.08	445.43
1000 N	2. E	1457.41	4781.53	155.53	2.08	1.00	445.28
1000 N	3. E	1470.71	4825.18	153.47	2.12	1.00	445.88
1000 N	4. E	1466.19	4810.32	154.50	2.16	1.07	446.13
1000 N	5. E	1455.04	4773.74	156.54	2.20	1.13	446.08
1000 N	6. E	1443.69	4736.52	158.81	2.24	1.16	446.18
1000 N	7. E	1429.28	4689.23	161.64	2.28	1.20	446.26
1000 N	8. E	1414.78	4641.66	164.55	2.32	1.22	446.38
1000 N	9. E	1400.22	4593.90	167.28	2.36	1.28	446.34
1000 N	10. E	1380.84	4530.33	170.93	2.40	1.28	446.22
1000 N	11. E	1365.85	4481.13	174.06	2.44	1.22	446.38
1000 N	12. E	1339.60	4395.02	179.09	2.48	1.20	446.27

BASE LINE WEST-EAST

0 W	20. S	1473.66	4834.83	149.77	4.10	2.55	446.29
0 W	19. S	1461.92	4796.31	152.21	4.03	2.51	446.31
0 W	18. S	1451.41	4761.86	154.33	3.96	2.44	446.22
0 W	17. S	1439.16	4721.67	156.86	3.89	2.39	446.22
0 W	16. S	1430.74	4694.03	158.58	3.82	2.28	446.11
0 W	15. S	1428.16	4685.58	159.13	3.75	2.17	445.97
0 W	14. S	1431.77	4697.40	158.80	3.68	2.00	446.11
0 W	13. S	1433.18	4702.02	158.68	3.61	1.86	446.06
0 W	12. S	1434.91	4707.70	158.62	3.54	1.77	446.18
0 W	11. S	1435.73	4710.40	158.58	3.47	1.68	446.14
0 W	10. S	1436.41	4712.64	158.46	3.40	1.57	445.97

STN. NO.	ELEV. METRES	ELEV. FEET	OBSERVED GRAVITY	LATITUDE COR.	TERRAIN COR.	COMPLET BOUGUE
0 W 9. S	1431.32	4695.93	159.45	3.33	1.58	445.90
0 W 8. S	1422.54	4667.13	161.08	3.26	1.60	445.75
0 W 7. S	1418.71	4654.56	162.01	3.19	1.68	445.94
0 W 6. S	1413.65	4637.96	163.03	3.12	1.74	445.96
0 W 5. S	1431.52	4696.59	159.60	3.05	1.61	445.84
0 W 4. S	1452.02	4763.86	155.42	2.98	1.46	445.47
0 W 3. S	1474.02	4836.01	151.17	2.91	1.37	445.39
0 W 2. S	1493.11	4898.66	147.69	2.84	1.34	445.57
0 W 1. S	1508.26	4948.36	144.93	2.77	1.32	445.70
0 W 0.	1524.00	5000.00	141.79	2.70	1.30	445.56
0 W 1. N	1533.96	5029.37	140.18	2.63	1.28	445.82
0 W 2. N	1535.27	5036.96	139.69	2.56	1.25	445.49
0 W 3. N	1533.77	5032.04	140.12	2.49	1.26	445.56
0 W 4. N	1533.13	5029.95	140.20	2.42	1.27	445.46
0 W 5. N	1528.10	5013.46	141.23	2.35	1.28	445.44
0 W 6. N	1520.90	4989.83	142.67	2.28	1.27	445.38
0 W 7. N	1516.62	4975.79	143.64	2.21	1.25	445.42
0 W 8. N	1506.78	4943.52	145.74	2.14	1.22	445.48
0 W 9. N	1498.14	4915.17	147.54	2.07	1.19	445.48
0 W 10. N	1489.63	4887.25	149.37	2.00	1.15	445.53
0 W 11. N	1494.25	4902.39	148.64	1.93	1.15	445.64
0 W 12. N	1500.41	4922.61	147.60	1.86	1.18	445.77
0 W 13. N	1506.26	4941.80	146.95	1.79	1.22	446.24
0 W 14. N	1506.44	4942.39	147.14	1.72	1.24	446.42
0 W 15. N	1487.77	4881.14	150.82	1.65	1.23	446.34
0 W 16. N	1474.06	4836.16	153.73	1.58	1.19	446.45
0 W 17. N	1461.49	4794.91	156.47	1.51	1.17	446.63
0 W 18. N	1456.90	4779.87	157.32	1.44	1.16	446.49
0 W 19. N	1450.00	4757.23	158.64	1.37	1.15	446.38
0 W 20. N	1439.23	4721.87	160.76	1.30	1.14	446.30
0 W 21. N	1437.13	4714.98	161.43	1.23	1.13	446.47
0 W 22. N	1440.77	4726.94	160.91	1.16	1.12	446.59
0 W 23. N	1439.72	4723.48	161.49	1.09	1.11	446.88
0 W 24. N	1437.55	4716.38	162.24	1.02	1.11	447.14
0 W 25. N	1432.61	4700.15	163.25	.95	1.10	447.09