

84-#88-12282
2/85

ELECTROMAGNETIC

AND

GEOCHEMICAL

REPORT

ON

MAC CLAIM

OMENICA MINING DIVISION

56'55'N 126'30'W NTS 94D 15E

BY

J.W. MACLEOD

VANCOUVER, BRITISH COLUMBIA

FEBRUARY 14, 1984

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

12,282

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MAP

E.M. Profiles and Soil Sample Locations (In Pocket)

APPENDIX I

PHOENIX VLF-2 SPECIFICATIONS

APPENDIX II

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EXPENDITURE

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ENGINEERS CERTIFICATE

MAC CLAIM

INTRODUCTION

The following report on the Mac Claim, fiananced by Tenajon Silver Corp. and Sunena Resources, has been prepared to fulfill the requirements of the Mineral Act regarding the application of geophysical and geochemical surveys for assessment work.

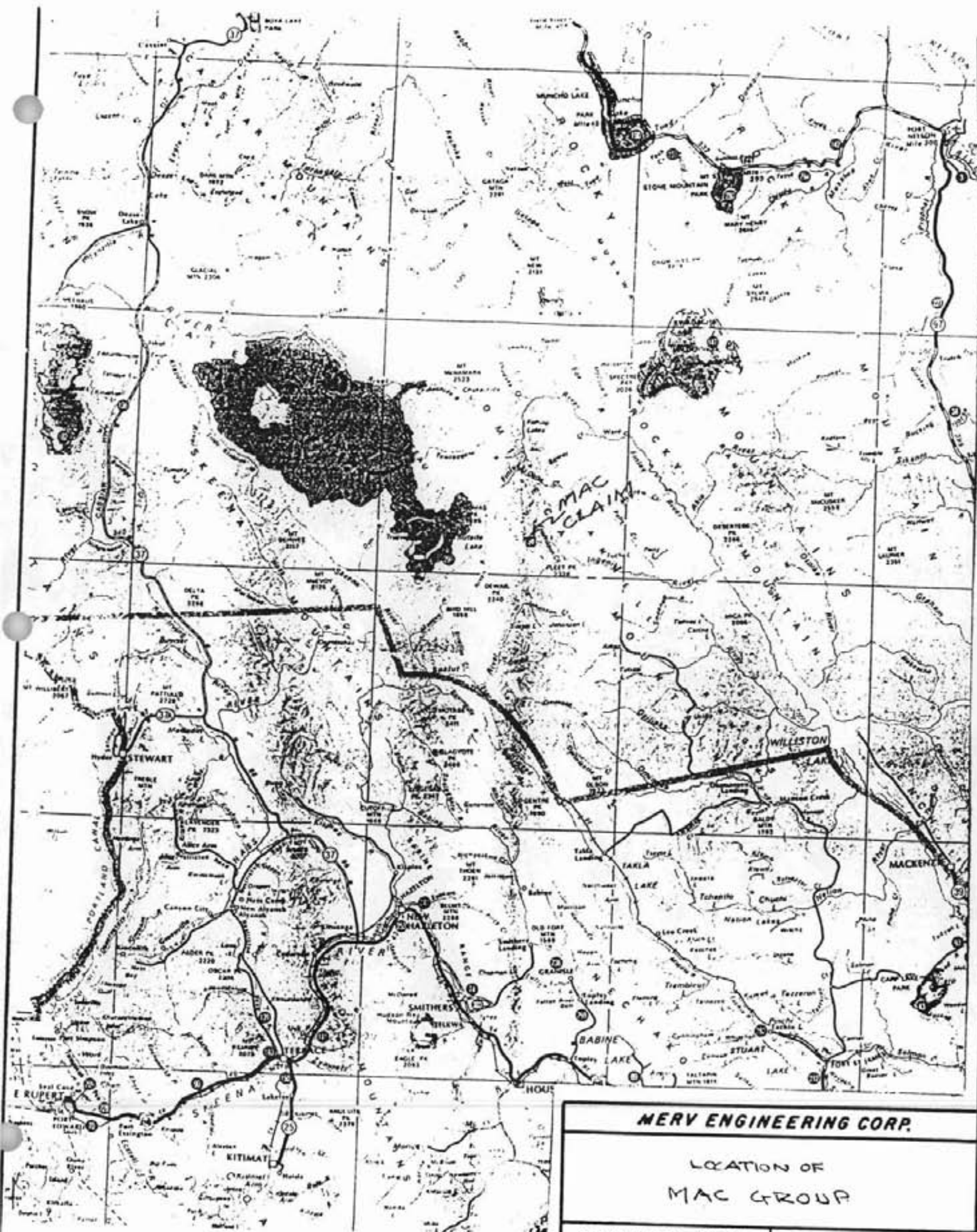
The surveys were carried out under the writer's direction by the following field crew:

Scott Angus; 12474 Crescent Road, Surrey, B.C.
Rex Brown; 473 Transit Road, Victoria, B.C.

Field work was carried out from September 12 to September 25, 1983.

PROPERTY

The property consists of the 16 unit Mac claim, Record No. 5095, recorded by Scott Angus on April 8, 1983 and transfered to Tenajon Silver Corp. on October 18, 1983.



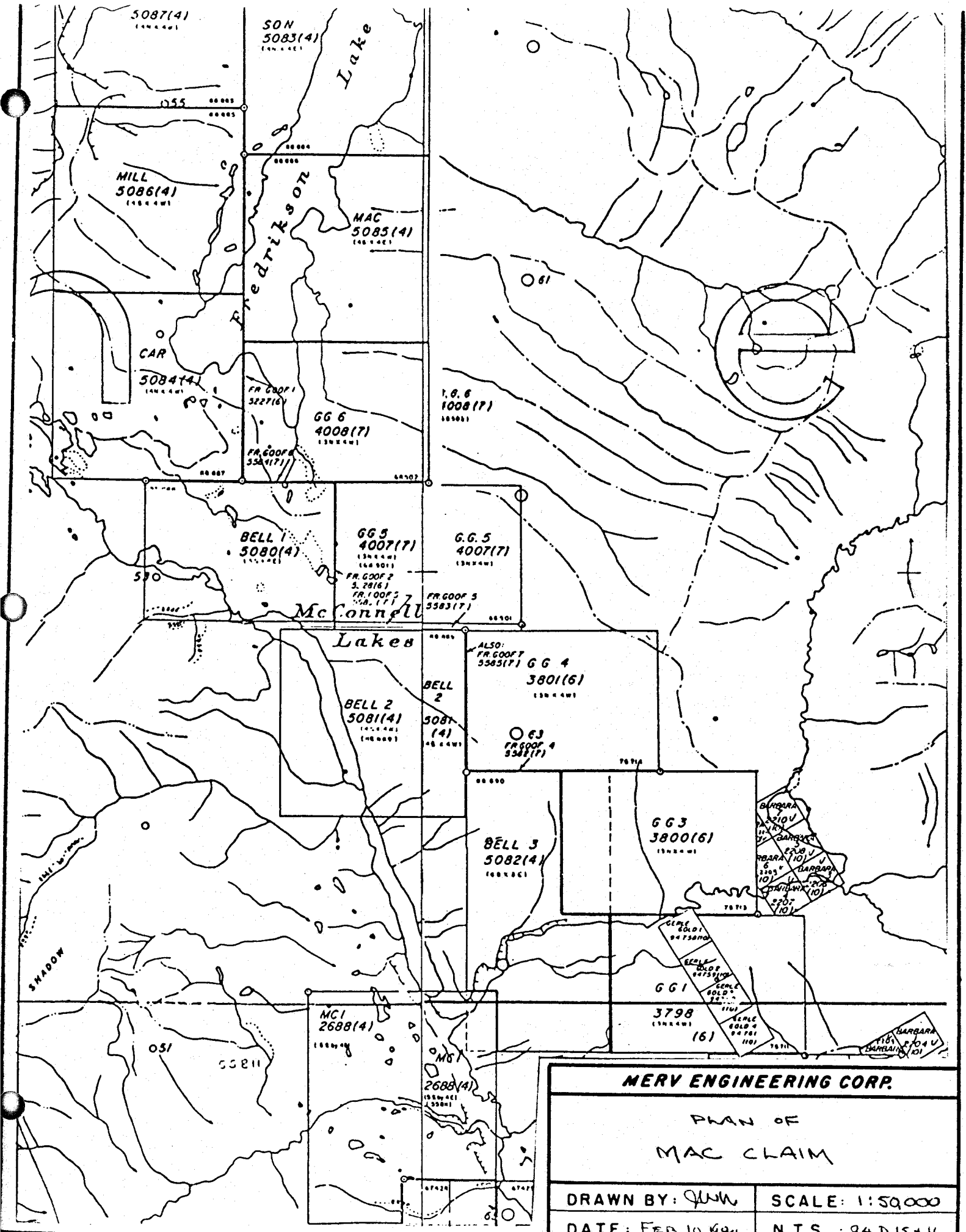
MERV ENGINEERING CORP.	
LOCATION OF MAC GROUP	
DRAWN BY: QJM	SCALE: 1:2,500,000
DATE: FEB 10, 1960	NTS: 24 D 1111

GENERAL

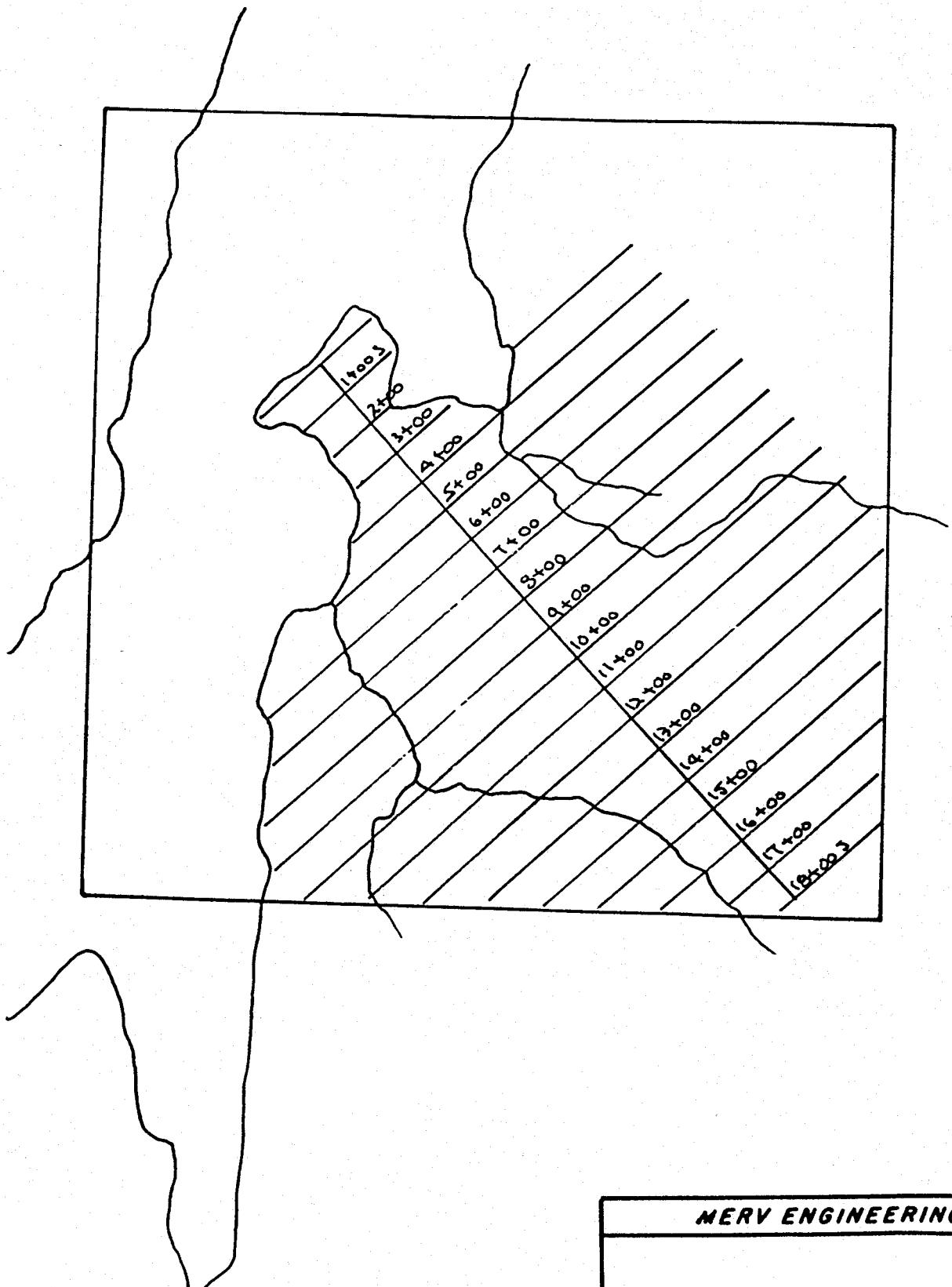
Interest in this area stems from the gold discovery in 1947 by Gerlitzky and Leontowich. Gerle Gold Mines acquired the original showing in 1982 and carried out a program which suggests considerable lateral extent to the original gold occurrences. Geophysical and geochemical surveys by Gerle suggest the favourable zone extends to the north and west. The Mac claim adjoins Gerle Gold Property to the north.

30% of the claim area is underlain by Fredrikson Lake and the rest is overburden cover with considerable muskeg. Elevation of the lake is 1300m and the ground rises gently to the west with a maximum relief of 200m on the claim.

The crew was mobilized by air out of Smithers 250 km to the south. Road access is not a serious problem since Gerle completed 4 x 4 road from the Department of Mines access road from Fort St. James to Moose Valley in 1983.



MERV ENGINEERING CORP.	
PLAN OF MAC CLAIM	
DRAWN BY: JUN	SCALE: 1:50000
DATE: FEB 10, 1984	N.T.S. : 94 DIS 16



MERV ENGINEERING CORP.

GRID LAYOUT

DRAWN BY: JMM

SCALE: 1:15,000

GEOLOGY

Most of the claim area is probably underlain by granodiorite but lenses of hornblende schist will occur and these are the host rocks for the gold veins found on the Gerle Gold ground to the southeast.

C.S. Lord, in G.S.C. Mem. 751, suggests the source of the placer gold in McConnell Creek was to the northwest but the Gerle gold showings were not known at the time he mapped this area.

E.M. SURVEY

Ground control for the surveys was a baseline bearing of N45W with flagged cross lines at 100m intervals.

Readings were taken with a Phoenix Model VLF2 electromagnetic unit at 50m stations. Seattle, frequency 24.8 KHz, bearing 160° was used and a west dip was plotted plus.

A series of anomalies referred to as "C" on the accompanying map could represent the northerly extension of the Gerle Gold structure. On the Gerle ground the trend is northwest but the schist exposed on the northwest side of Fredrikson Lake strike north-south which correlates with the trend of the C anomalies.

GEOCHEMICAL SURVEY

Soil samples were taken at the 50m stations of the "B"

horizon. At a number of stations the presence of deep muskeg prevented sample collection. The location of samples acquired is shown as a circle on the accompanying map.

Samples were analyzed by the aqua rigia method for gold content and 30 elements were determined by the Induction Couple Plasma Spectrometer (I.C.P.) method.

No anomalous values were obtained.

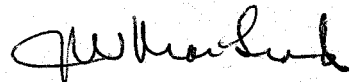
CONCLUSIONS AND RECOMMENDATIONS

The lack of geochemical response may be due to deep overburden.

The anomaly C conductor has the proper orientation but it is difficult to recommend further work without some geochemical confirmation of possible economic mineral.

It is recommended that the ground be maintained and the results of the Gerle Gold work to the south be monitored to determine the next phase of exploration of the Mac claim.

Respectfully submitted,



J.W. MacLeod, P.Eng.

Vancouver, B.C.

APPENDIX I

PHOENIX VLF - 2 SPECIFICATIONS

Specifications

- Parameters Measured** : Orientation and magnitude of the major and minor axes of the ellipse of polarization.
- Frequency Selection, Front Panel** : Dual channel, front panel selectable (F1 or F2) each with independent precision 10-turn dial gain control.
- Frequency Selection, Internal** : F1 and F2 can be selected by internal switches within the range 14.0 to 29.9 kHz in 100 Hz increments.
- Detection And Filtering** : Superheterodyne detection and digital filtering provide a much narrower bandwidth and thus greater rejection of interfering stations and 60 cycle noise than conventional receivers.
- Meter Display** : 2 ranges: 0 to 300 or 0 to 1000. Background is typically set at 100. Meter is also used as dip angle null indicator and battery test.
- Audio** : Crystal speaker. 2500 Hz used as null indicator.
- Clinometer** : $\pm 90^\circ$, $+0.5^\circ$ resolution. Normal locking, push button release.
- Battery** : One standard 9v transistor radio battery. Average life expectancy - 1 to 3 months (battery drain is 3 mA)
- Temperature Range** : -40° to $+60^\circ$ C.
- Dimensions** : 8 x 22 x 14 cm (3 x 9 x 6 inches).
- Weight** : 850 grams (1.9 pounds).

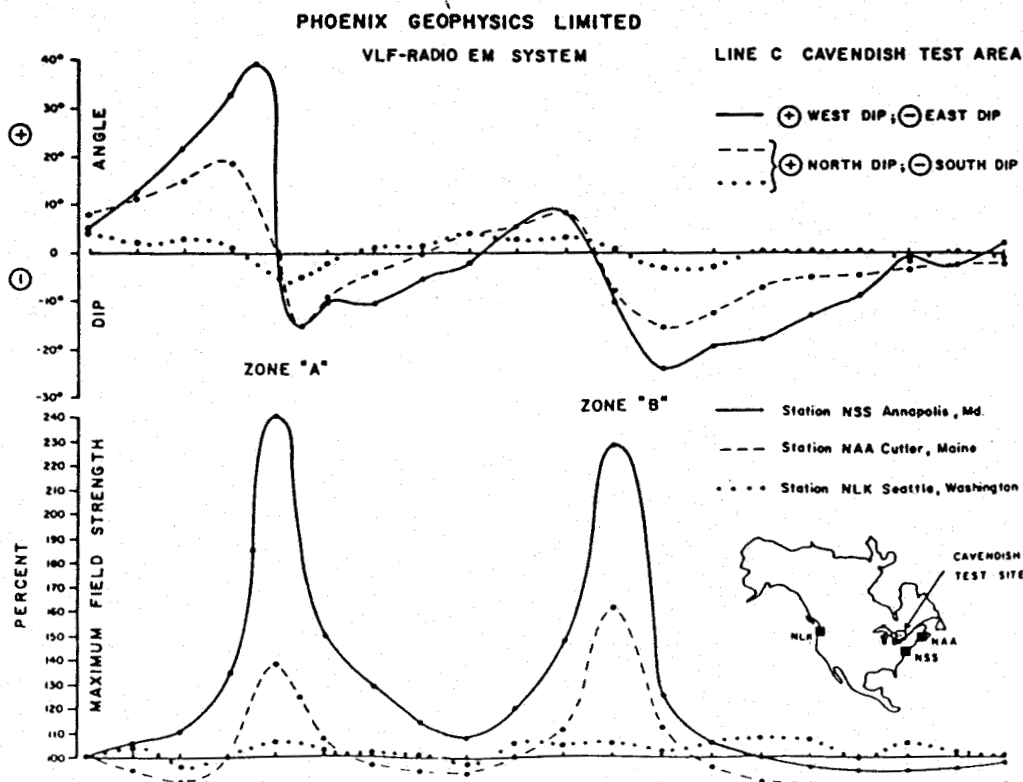
All of the established stations may be selected, or alternatively, a local VLF transmitter may be used which transmits at any frequency in the range 14.0 to 29.9 kHz.

VLF Station	Frequency (kHz)
Bordeaux, France	15.1
Odessa (Black Sea)	15.6
Rugby, U.K.	16.0
Moscow, U.S.S.R.	17.1
Yosamai, Japan	17.4
Hegaland, Norway	17.6
Cutler, Maine	17.8
24.8 Seattle, Washington	18.6
Malabar, Java	19.0
Oxford, U.K.	19.6
Paris, France	20.7
Annapolis, Maryland	21.4
Northwest Cape, Australia	22.3
Laulalei, Hawaii	23.4
Buenos Aires, Argentina	23.6
Rome, Italy	27.2

Field Data

The results below illustrate the need for using two orthogonal stations when the strike of the prospective conductor is not well-known. The dip angle and amplitude data measured using station NLK in Seattle, Washington, show only a very weak anomaly associated with the two conductive sulphide zones at Cavendish, Ontario.

The results obtained using Cutler, Maine reveal a more prominent anomaly, but the best response was obtained using Annapolis, Maryland since the station lies almost due south and the transmitted electromagnetic field is thus maximum-coupled with the North-South trending conductors.



APPENDIX II

GEOCHEMICAL ANALYTICAL PROCEDURES

ASSAYS

VANGEOCHEM LAB LTD.
1521 Pemberton Ave.
North Vancouver, B.C.
V7P 2S

TO: Tenagon Silver Mines
#1450 - 625 Howe Street
Vancouver, B.C. V6C 2T6

FROM: Vangeochem Lab Ltd.
1521 Pemberton Ave.
North Vancouver, B.C. V7P 2S3

SUBJECT: Analytical procedure used to determine elements in hot acid soluble by Induction Couple Plasma Spectrometer (ICP) analysis.

1. Method of Sample Preparation

- (a) Geochemical soil, silt or rock samples were received in the laboratory in wet-strength 4" x 6" Kraft paper bags or rock samples sometimes in 8" x 12" plastic bags.
- (b) The dried soil and silt samples were sifted by hand using a 8" diameter 80-mesh stainless steel sieve. The plus 80-mesh fraction was rejected and the minus 80-mesh fraction was transferred into a new bag for analysis later.
- (c) The dried rock samples were crushed by using a jaw crusher and pulverized to 100-mesh or finer by using a disc mill. The pulverized samples were then put in a new bag for later analysis.

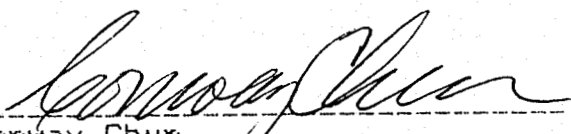
2. Method of Digestion

- (a) 0.500 gram of -80 mesh sample was used.
- (b) Samples were digested in a hot water bath with conc. HNO₃ and conc. HCl acids.
- (c) The digested samples were diluted to a fixed volume and shaken well.

3. Method of Analysis

The ICP analyses elements were determined by using Jarrel Ash, model 885. Direct reading emission spectrograph of a inductive coupled plasma excitation source. All major matrix and trace elements are interelement corrected to trace elements. All data is entered into Apple II plus, stored on floppy disks, and printed by Epson 100.

4. The analyses were supervised by Mr. Dean Toye and Mr. Conway Chun of Vangeochem Lab Ltd. and their staff.



Conway Chun
VANGEOCHEM LAB LTD.

VANGEOCHEM LAB LTD.
1521 Pemberton Ave.
North Vancouver, B.C.
V7P 2S3

TO: Tenison Silver Mines
#1450 - 625 Howe Street
Vancouver, B.C. V6C 2T6

FROM: Vangoechem Lab Ltd.
1521 Pemberton Ave.
North Vancouver, B.C. V7P 2S3

SUBJECT: Analytical procedure used to determine Aqua Regia
soluble gold in geochemical samples

1. Method of Sample Preparation

- (a) Geochemical soil, silt or rock samples were received in the laboratory in wet-strength 4" x 6" Kraft paper bags or rock samples sometimes in 8" x 12" elastic bags.
- (b) The dried soil and silt samples were sifted by hand using a 8" diameter 80-mesh stainless steel sieve. The plus 80-mesh fraction was rejected and the minus 80-mesh fraction was transferred into a new bag for analysis later.
- (c) The dried rock samples were crushed by using a jaw crusher and pulverized to 100-mesh or finer by using a disc mill. The pulverized samples were then put in a new bag for later analysis.

2. Method of Digestion

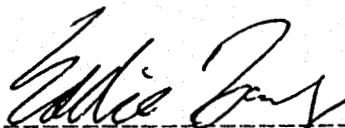
- (a) 5.00 - 10.00 grams of the minus 80-mesh samples were used. Samples were weighed out by using a top-loading balance into beakers.
- (b) 20 ml of Aqua Regia (3:1 HCl : HNO₃) were used to digest the samples over a hot plate vigorously.
- (c) The digested samples were filtered and the washed solids were discarded and the filtrate was reduced to about 5 ml.

- (d) The Au complex ions were extracted into diisobutyl ketone and thiourea medium. (Anion exchange liquids "Aliquot 336").
- (e) Separate Funnels were used to separate the organic layer.

3. Method_of_Detection

The gold analyses were detected by using a Techtron model AAS Atomic Absorption Spectrophotometer with a gold hollow cathode lamp. The results were read out on a strip chart recorder. A hydrogen lamp was used to correct any background interferences. The gold values in parts per billion were calculated by comparing them with a set of gold standards.

- 4. The analyses were supervised or determined by Mr. Conway Chun or Mr. Eddie Tang and his laboratory staff.



Eddie Tang
VANGEOCHEM LAB LTD.

VANGEOCHEM LAB LIMITED

=====

1521 Pemberton Ave.
North Vancouver B.C. V7P 2S3
(604)986-5211 Telex: 04-352578

GEOCHEMICAL ANALYTICAL REPORT

CLIENT: TENAJON SILVER CORP.
ADDRESS: 1450 - 625 Howe Street
: Vancouver, B.C.
: V6C 2T6

DATE: October 11 1983

REPORT#: 83-90-030

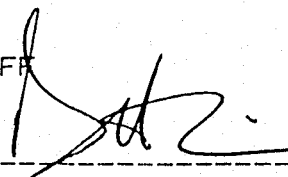
PROJECT#: MAC
COPY SENT TO: TENAJON SILVER CORP.
SAMPLES ARRIVED: September 27 1983
REPORT COMPLETED: October 11 1983
ANALYSED FOR: Au ICP

JOB#: 83369
INVOICE#: 7545
TOTAL SAMPLES: 358
SAMPLE TYPE: 358 Soil & Silt
REJECTS: DISCARDED

PREPARED FOR: TENAJON SILVER CORP.

ANALYSED BY: VGC STAFF

SIGNED: _____



GENERAL REMARK:

VANGEOCHEM LAB LIMITED
1521 Pemberton Avenue
North Vancouver B.C. V7P 2S3
(604) 986-5211 Telex: 04-352578

PREPARED FOR: TENAJON SILVER CORP.

NOTES: nd = none detected
: -- = not analysed
: is = insufficient sample

REPORT NUMBER: 83-90-030

JOB NUMBER: 83369

PAGE 1 OF 10

SAMPLE #	Au ppb
MAC SILT 1	nd
MAC SILT 2	10
MAC SILT 3	10
MAC SILT 4	15
MAC SILT 5	20
MAC SILT 6	nd
MAC SILT 7	5
MAC SILT 8	5
MAC SILT 9	10
MAC SILT 10	nd
MAC SILT 11	nd
MAC SILT 12	30
MAC SILT 13	nd
MAC SILT 14	nd
MAC SILT 15	nd
MAC SILT 16	nd
MAC SILT 17	10
MAC SILT 18	5
BL 0+00S	10
0+00S 0+50E	nd
0+00S 1+00E	10
0+00S 1+50E	nd
0+00S 0+50W	nd
0+00S 1+00W	nd
0+00S 1+50W	nd
0+00S 2+00W	nd
BL 1+00S	5
1+00S 0+50E	nd
1+00S 1+00E	10
1+00S 1+50E	nd
1+00S 4+50E	5
1+00S 5+00E	nd
1+00S 6+00E	5
1+00S 6+50E	nd
1+00S 7+00E	nd
1+00S 7+50E	nd
1+00S 8+00E	nd
1+00S 8+50E	nd
1+00S 9+00E	nd
DETECTION LIMIT	5

VANGEDICHEN LAB LIMITED
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North Vancouver B.C. V7P 2S3
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SAMPLE #	Au
	ppb
1+00S 9+50E	nd
1+00S 10+00E	nd
1+00S 0+50W	5
1+00S 1+00W	nd
1+00S 1+50W	10
BL 2+00S	5
2+00S 4+00E	nd
2+00S 4+50E	nd
2+00S 6+00E	10
2+00S 6+50E	nd
2+00S 7+00E	5
2+00S 7+50E	5
2+00S 8+00E	nd
2+00S 8+50E	15
2+00S 9+00E	nd
2+00S 9+50E	nd
2+00S 10+00E	nd
2+00S 0+50W	nd
2+00S 1+00W	nd
2+00S 1+50W	5
BL 3+00S	nd
0+00S 0+50E	10
3+00S 1+00E	nd
3+00S 1+50E	nd
3+00S 2+00E	nd
3+00S 4+00E	nd
3+00S 4+50E	nd
3+00S 5+00E	20
3+00S 5+50E	nd
3+00S 6+00E	nd
3+00S 6+50E	nd
3+00S 7+00E	nd
3+00S 7+50E	15
3+00S 8+00E	nd
3+00S 0+50W	35
3+00S 1+00W	10
3+00S 1+50W	10
BL 4+00S	20
4+00S 0+50E	5

DETECTION LIMIT

5

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SAMPLE #	Au
	oob
4+00S 1+00E	nd
4+00S 1+50E	10
4+00S 2+00E	nd
4+00S 5+00E	nd
4+00S 5+50E	nd
4+00S 6+00E	15
4+00S 6+50E	nd
4+00S 7+00E	nd
4+00S 8+00E	5
4+00S 0+50W	nd
4+00S 1+00W	5
4+00S 1+50W	30
4+00S 2+00W	10
4+00S 2+50W	5
BL 5+00S	10
5+00S 0+50E	5
5+00S 1+00E	5
5+00S 1+50E	10
5+00S 2+00E	nd
5+00S 2+00E (A)	nd
5+00S 2+50E	nd
5+00S 3+00E	20
5+00S 4+00E	nd
5+00S 4+50E	10
5+00S 5+00E	nd
5+00S 6+00E	nd
5+00S 0+50W	10
5+00S 1+00W	nd
5+00S 1+50W	15
5+00S 2+50W	nd
5+00S 3+00W	5
5+00S 3+50W	20
BL 6+00S	5
6+00S 0+50E	5
6+00S 1+50E	5
6+00S 2+50E	10
6+00S 3+00E	5
6+00S 4+50E	nd
6+00S 5+00E	10
DETECTION LIMIT	5

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PAGE 4 OF 10

SAMPLE #	Au ppb
6+00S 5+50E	5
6+00S 6+50E	nd
6+00S 7+00E	nd
6+00S 8+00E	10
6+00S 0+50W	5
6+00S 1+00W	10
6+00S 1+50W	5
6+00S 2+00W	5
6+00S 2+50W	5
6+00S 3+00W	10
6+00S 3+50W	5
6+00S 4+00W	5
6+00S 4+50W	10
6+00S 5+00W	nd
6+00S 5+50W	5
6+00S 6+00W	nd
6+00S 6+50W	nd
BL 7+00S	nd
7+00S 0+50E	5
7+00S 1+00E	nd
7+00S 2+00E	nd
7+00S 2+50E	nd
7+00S 3+50E	nd
7+00S 4+00E	nd
7+00S 7+00E	nd
7+00S 7+50E	5
7+00S 0+50W	nd
7+00S 2+50W	nd
7+00S 3+00W	5
7+00S 5+00W	nd
7+00S 5+50W	nd
7+00S 6+00W	nd
7+00S 6+50W	nd
7+00S 7+00W	nd
8+00S 1+00E	nd
8+00S 1+50E	nd
8+00S 2+00E	nd
8+00S 2+50E	20
8+00S 3+00E	nd
DETECTION LIMIT	5

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SAMPLE #	Au
	ppb
8+00S 3+50E	nd
8+00S 5+50E	nd
8+00S 7+50E	5
8+00S 0+50W	5
8+00S 1+50W	5
8+00S 2+00W	nd
8+00S 2+50W	nd
8+00S 3+00W	nd
8+00S 3+50W	15
8+00S 5+00W	nd
8+00S 5+50W	nd
8+00S 6+00W	5
8+00S 6+50W	nd
8+00S 7+00W	nd
8+00S 7+50W	nd
8+00S 9+00W	nd
BL 9+00S	nd
9+00S 0+50E	nd
9+00S 1+00E	15
9+00S 1+50E	nd
9+00S 3+50E	nd
9+00S 4+00E	nd
9+00S 4+50E	nd
9+00S 5+00E	nd
9+00S 5+50E	nd
9+00S 6+00E	nd
9+00S 6+50E	nd
9+00S 7+00E	5
9+00S 7+50E	nd
9+00S 8+00E	nd
9+00S 0+50W	nd
9+00S 1+00W	nd
9+00S 2+50W	nd
9+00S 3+00W	nd
9+00S 3+50W	nd
9+00S 5+00W	nd
9+00S 6+00W	nd
9+00S 6+50W	5
9+00S 7+00W	nd

DETECTION LIMIT

5

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SAMPLE #	Au
	ppb
9+00S 7+50W	10
9+00S 8+00W	10
9+00S 8+50W	5
9+00S 9+00W	15
10+00S 0+50E	5
10+00S 1+50E	10
10+00S 2+00E	5
10+00S 2+50E	5
10+00S 3+00E	nd
10+00S 3+50E	10
10+00S 4+00E	10
10+00S 4+50E	10
10+00S 5+00E	15
10+00S 6+00E	nd
10+00S 6+50E	10
10+00S 7+00E	5
10+00S 7+50E	10
10+00S 8+00E	10
BL 10+00S	5
10+00S 0+50W	nd
10+00S 1+00W	5
10+00S 1+50W	nd
10+00S 3+50W	10
10+00S 4+00W	5
10+00S 4+50W	nd
10+00S 7+50W	10
10+00S 8+00W	nd
10+00S 8+50W	nd
10+00S 9+00W	20
10+00S 9+50W	15
BL 11+00S	nd
11+00S 0+50E	10
11+00S 1+00E	10
11+00S 1+50E	5
11+00S 2+00E	nd
11+00S 2+50E	10
11+00S 3+00E	nd
11+00S 3+50E	5
11+00S 4+00E	5
DETECTION LIMIT	5

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SAMPLE #	Au
	ppb
11+00S 5+00E	nd
11+00S 5+50E	nd
11+00S 6+00E	nd
11+00S 6+50E	nd
11+00S 7+00E	nd
11+00S 7+50E	5
11+00S 8+00E	5
11+00S 8+50E	nd
11+00S 9+00E	nd
11+00S 9+50E	5
11+00S 0+50W	nd
11+00S 1+00W	nd
11+00S 1+50W	5
11+00S 2+00W	15
BL 12+00S	15
12+00S 0+50E	10
12+00S 1+00E	5
12+00S 1+50E	30
12+00S 2+00E	nd
12+00S 2+50E	5
12+00S 4+00E	nd
12+00S 4+50E	5
12+00S 5+00E	5
12+00S 5+50E	5
12+00S 6+00E	5
12+00S 7+00E	10
12+00S 7+50E	10
12+00S 8+00E	nd
12+00S 8+50E	nd
12+00S 1+00W	5
12+00S 1+50W	nd
12+00S 2+00W	5
12+00S 2+50W	15
12+00S 3+00W	nd
12+00S 4+00W	5
12+00S 4+50W	nd
12+00S 5+00W	nd
12+00S 5+50W	nd
12+00S 6+50W	5

DETECTION LIMIT 5

VANGOCHEM LAB LIMITED

1521 Pemberton Avenue
 North Vancouver B.C. V7P 2S3
 (604) 986-5211 Telex: 04-352578

PREPARED FOR: TENAJON SILVER CORP.

NOTES: no = none detected
 : -- = not analysed
 : is = insufficient sample

REPORT NUMBER: 83-90-030

JOB NUMBER: 83359

PAGE 6 OF 12

SAMPLE #	Au
	ppb
13+00S 1+00E	nd
13+00S 1+50E	10
13+00S 2+00E	5
13+00S 3+50E	nd
13+00S 4+50E	nd
13+00S 5+00E	5
13+00S 5+50E	10
13+00S 6+00E	nd
13+00S 6+50E	nd
13+00S 7+00E	10
13+00S 7+50E	5
13+00S 0+50W	nd
13+00S 2+00W	20
13+00S 2+50W	10
13+00S 3+50W	5
13+00S 5+00W	10
13+00S 6+00W	15
BL 14+00S	5
14+00S 0+50E	nd
14+00S 1+00E	5
14+00S 1+50E	5
14+00S 2+50E	nd
14+00S 3+00E	15
14+00S 3+50E	nd
14+00S 4+00E	nd
14+00S 5+00E	5
14+00S 5+50E	5
14+00S 6+00E	nd
14+00S 6+50E	10
14+00S 0+50W	nd
14+00S 1+00W	nd
14+00S 1+50W	nd
14+00S 2+00W	5
14+00S 2+50W	nd
14+00S 3+50W	nd
14+00S 4+00W	5
14+00S 4+50W	nd
14+00S 5+00W	nd
BL 15+00S	nd

DETECTION LIMIT

5

VANGECHEM LAB LIMITED
1521 Pemberton Avenue
North Vancouver B.C. V7P 2S3
(604) 986-5211 Telex: 04-352578

PREPARED FOR: TENAJON SILVER CORP.

NOTES: nd = none detected
: -- = not analysed
: is = insufficient sample

REPORT NUMBER: 83-90-030

JOB NUMBER: 83369

PAGE 9 OF 10

SAMPLE #	Au
	ppb
15+00S 0+50E	nd
15+00S 2+00E	10
15+00S 2+50E	5
15+00S 3+00E	10
15+00S 3+50E	nd
15+00S 4+00E	5
15+00S 4+50E	nd
15+00S 5+00E	nd
15+00S 5+50E	nd
15+00S 0+50W	5
15+00S 1+50W	nd
15+00S 2+00W	10
15+00S 2+50W	nd
15+00S 3+00W	5
15+00S 3+50W	nd
15+00S 3+90W	10
BL 16+00S	nd
16+00S 1+00E	nd
16+00S 1+50E	nd
16+00S 2+00E	5
16+00S 2+50E	nd
16+00S 3+00E	5
16+00S 3+50E	5
16+00S 0+50W	nd
16+00S 1+00W	nd
16+00S 1+50W	nd
16+00S 2+00W	nd
16+00S 2+50W	nd
BL 17+00S	nd
17+00S 0+50E	nd
17+00S 1+00E	nd
17+00S 1+50E	nd
17+00S 2+50E	10
17+00S 3+00E	5
17+00S 3+50E	5
17+00S 0+50W	20
17+00S 1+00W	nd
17+00S 1+50W	nd
BL 18+00S	5

DETECTION LIMIT

5

VANGECHEM LAB LIMITED
1521 Pemberton Avenue
North Vancouver B.C. V7P 2S3
(604) 986-5211 Telex: 04-352578

PREPARED FOR: TENAJON SILVER CORP.

NOTES: no = none detected
: -- = not analysed
: is = insufficient sample

REPORT NUMBER: 83-90-030 JOB NUMBER: 83369

PAGE 10 OF 10

SAMPLE #	Au ppb
18+00S 0+50E	5
18+00S 1+00E	5
18+00S 1+50E	10
18+00S 2+00E	10
18+00S 2+50E	10
18+00S 3+00E	nd
18+00S 0+50W	5
DETECTION LIMIT	5

VANGEOCHEM LAB LIMITED
1521 PEMBERTON AVENUE
NORTH VANCOUVER, B.C. V7P 2S3

A .500 GRAM SAMPLE IS DIGESTED WITH 3 ML OF 3:1:3 HCL TO HMOS TO H2O AT 90 DEG.C. FOR 1 HOUR. THE SAMPLE IS DILUTED TO 10 MLS WITH WATER.
THIS LEACH IS PARTIAL FOR: Ca, P, Mg, Al, Ti, La, Na, K, W, Ba, Sr, Cr AND B. Au DETECTION 3 ppa.
SAMPLE TYPE - SOLUTION

INVOICE # 7545

DATE RECEIVED OCT 1983

DATE REPORTS MAILED Oct 11/83 ASSAYER A. J. Jones

DEAN TOYE, CERTIFIED B.C. ASSAYER

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM-MAC JOB # B3-369 FILE # B3-2423 PAGE # 1

SAMPLE #	Mo ppa	Cu ppa	Pb ppa	Zn ppa	Ag ppa	Ni ppa	Co ppa	Mn ppa	Fe %	As ppa	U ppa	Au ppa	Th ppa	Sr ppa	Cd ppa	Sb ppa	Bi ppa	V ppa	Ca %	P %	La ppa	Cr ppa	Hg %	Ba ppa	Ti %	B ppa	Al %	Na %	K %	W ppa
MAC SILT 1	1	22	4	82	.7	15	9	919	2.69	2	2	ND	2	104	1	2	2	62	.99	.12	13	26	.70	222	.05	2	2.24	.01	.13	2
MAC SILT 2	1	7	3	37	.2	7	6	479	1.96	2	2	ND	2	61	1	2	2	48	.58	.13	6	12	.42	66	.05	2	.90	.01	.09	2
MAC SILT 3	1	9	3	34	.2	7	5	312	2.24	2	2	ND	2	57	1	2	2	62	.65	.15	9	18	.37	62	.05	2	.84	.01	.08	2
MAC SILT 4	1	14	6	61	.3	13	7	480	2.33	3	2	ND	2	84	1	2	2	60	.86	.13	5	29	.71	125	.07	2	1.72	.01	.14	2
MAC SILT 5	1	9	4	33	.5	7	5	379	1.94	2	2	ND	2	53	1	2	2	51	.64	.15	8	15	.38	60	.06	2	.87	.01	.07	2
MAC SILT 6	1	6	1	37	.1	7	6	524	2.06	2	2	ND	2	56	1	2	2	48	.50	.12	6	13	.43	65	.05	2	.87	.01	.10	2
MAC SILT 7	1	11	7	59	.3	9	8	731	2.40	2	2	ND	2	59	1	2	2	55	.68	.14	8	13	.64	109	.07	2	1.24	.01	.17	2
MAC SILT 8	1	8	5	37	.2	7	6	741	1.91	3	2	ND	2	53	1	2	2	43	.54	.12	7	14	.43	77	.05	2	.93	.01	.08	2
MAC SILT 9	1	8	5	39	.2	8	6	1184	2.23	5	2	ND	2	54	1	2	2	47	.63	.14	8	13	.44	91	.05	2	.98	.01	.09	2
MAC SILT 10	1	6	3	39	.2	6	5	517	1.71	3	2	ND	2	53	1	2	2	43	.59	.14	5	11	.42	56	.04	2	.80	.01	.12	2
MAC SILT 11	1	7	1	31	.2	5	4	326	1.36	2	2	ND	2	46	1	2	2	32	.35	.08	3	6	.34	47	.04	2	.66	.01	.10	2
MAC SILT 12	1	8	4	39	.1	8	6	1335	2.25	4	2	ND	2	56	1	2	2	45	.62	.14	7	12	.47	97	.05	2	1.02	.01	.08	2
MAC SILT 13	1	6	4	43	.2	6	5	362	1.69	2	2	ND	2	75	1	2	2	39	.49	.11	4	9	.45	54	.05	2	.83	.02	.14	2
MAC SILT 14	1	8	1	41	.1	7	5	328	1.78	2	2	ND	2	77	1	2	2	45	.50	.09	5	13	.47	87	.05	2	1.07	.02	.09	2
MAC SILT 15	1	5	1	31	.2	5	4	487	1.65	2	2	ND	2	59	1	2	2	32	.41	.10	5	8	.35	61	.04	2	.67	.01	.10	2
MAC SILT 16	1	5	5	39	.1	6	7	2206	2.82	2	2	ND	2	63	1	2	2	57	.64	.15	7	12	.39	113	.05	2	.86	.01	.07	2
MAC SILT 17	1	6	4	31	.2	6	5	841	1.75	2	2	ND	2	46	1	2	2	38	.37	.08	4	7	.34	62	.04	2	.69	.01	.08	2
MAC SILT 18	1	7	3	36	.1	7	6	1010	2.12	3	2	ND	2	51	1	2	2	49	.53	.13	6	16	.42	69	.05	2	.90	.01	.06	2
BL 0+00S	1	17	5	44	.3	15	8	350	2.04	6	2	ND	2	41	1	2	2	57	.47	.05	6	30	.57	138	.06	2	1.72	.01	.03	2
0+00S 0+50E	1	16	3	44	.2	15	7	344	3.12	6	2	ND	2	23	1	2	2	75	.22	.09	5	32	.49	73	.07	2	1.69	.01	.02	2
STD	22	169	42	93	2.7	635	14	598	3.56	13	2	ND	3	25	1	8	2	50	1.69	.09	5	68	.63	27	.04	19	.89	.04	.20	2
0+00S 1+00E	1	16	6	57	.2	16	9	856	3.57	3	2	ND	2	26	1	2	2	86	.24	.12	7	30	.51	129	.08	2	2.12	.01	.03	2
0+00S 1+50E	1	15	8	38	.2	14	8	483	5.34	12	2	ND	2	25	1	2	2	155	.23	.12	5	43	.43	122	.16	2	1.80	.01	.02	2
0+00S 0+50W	1	29	3	52	.2	16	8	359	2.49	2	2	ND	2	39	1	2	2	65	.47	.05	6	33	.58	149	.05	2	1.83	.01	.03	2
0+00S 1+00W	1	21	5	49	.1	14	10	639	2.52	4	4	ND	2	36	1	2	2	67	.45	.05	5	33	.54	94	.07	2	1.40	.01	.03	2
0+00S 1+50W	1	14	5	17	.5	8	4	132	1.56	2	2	ND	2	27	1	2	2	44	.25	.04	4	24	.25	85	.05	2	1.40	.01	.01	2
0+00S 2+00W	1	24	3	33	.2	14	7	309	2.52	2	2	ND	2	47	1	2	2	68	.52	.05	5	33	.50	122	.06	2	1.62	.01	.02	2
BL 1+00S	1	11	7	38	.3	12	5	428	3.59	4	2	ND	2	20	1	2	2	93	.14	.09	8	44	.36	76	.12	2	1.61	.01	.03	2
1+00S 0+50E	1	6	6	22	.2	7	3	132	2.10	3	2	ND	2	18	1	2	2	60	.15	.06	5	20	.24	71	.08	2	1.25	.01	.02	2
1+00S 1+00E	1	11	7	32	.3	10	5	206	4.87	8	2	ND	2	17	1	2	2	122	.14	.13	8	28	.25	114	.20	2	2.19	.01	.02	2
1+00S 1+50E	1	8	2	25	.2	10	5	170	2.13	2	2	ND	2	26	1	2	2	60	.25	.06	5	24	.37	67	.08	2	1.29	.01	.02	2
1+00S 4+50E	1	10	8	33	.3	8	10	1255	3.00	9	2	ND	2	32	1	2	2	84	.27	.04	3	26	.40	64	.11	2	1.16	.01	.03	2
1+00S 5+00E	1	9	10	55	.1	10	6	358	4.29	4	2	ND	2	25	1	2	2	104	.16	.12	4	27	.54	81	.15	2	1.53	.01	.04	2
1+00S 6+00E	1	18	6	32	.3	13	7	243	2.86	4	2	ND	2	25	1	2	2	73	.21	.06	5	33	.48	73	.09	2	2.17	.01	.02	2
1+00S 6+50E	1	13	2	47	.2	12	7	285	3.29	4	2	ND	2	21	1	2	2	74	.20	.10	6	35	.45	85	.09	2	2.33	.01	.02	2
1+00S 7+00E	1	11	6	41	.3	10	5	327	4.00	4	2	ND	2	16	1	2	2	87	.13	.14	6	29	.31	64	.13	2	2.70	.01	.02	2
1+00S 7+50E	1	10	8	36	.2	11	5	240	3.71	3	2	ND	2	18	1	2	2	92	.17	.09	5	35	.38	68	.11	2	2.25	.01	.02	2
1+00S 8+00E	1	10	6	37	.1	13	6	298	3.53	5	3	ND	2	19	1	2	2	75	.17	.08	5	35	.41	63	.11	2	2.14	.01	.02	2
1+00S 8+50E	1	11	6	46	.2	11	6	270	3.37	7	2	ND	2	19	1	2	2	75	.18	.11	5	31	.41	65	.09	2	2.59	.01	.02	2
1+00S 9+00E	1	6	5	15	.1	4	3	208	2.05	2	2	ND	2	15	1	2	2	64	.11	.03	4	18	.12	63	.08	2	.91	.01	.01	2
STD A-1	1	30	38	183	.3	36	12	1000	2.83	10	2	ND	2	35	1	2	2	59	.61	.10	9	74	.72	278	.08	6	1.94	.02	.19	2

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM-MAC JOB # 83-369 FILE # 83-2423

SAMPLE #	No	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Ti	B	Al	Na	K	M
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm
1+00S 9+50E	1	11	10	49	.4	10	5	287	4.24	5	4	ND	2	14	1	9	2	91	.12	.12	11	32	.26	62	.16	2	3.14	.01	.03	2
1+00S 10+00E	1	11	5	31	.2	8	4	185	2.70	2	2	ND	2	19	1	2	2	72	.16	.06	4	30	.29	55	.10	2	2.32	.01	.02	2
1+00S 0+50W	1	8	6	25	.2	8	4	174	2.40	5	2	ND	2	20	1	2	2	73	.16	.10	5	22	.30	64	.09	2	1.49	.01	.01	2
1+00S 1+00W	1	7	13	47	.2	8	4	420	4.51	5	2	ND	2	15	1	4	2	89	.12	.21	12	26	.21	104	.15	2	1.83	.01	.04	2
1+00S 1+50W	1	25	4	40	.1	15	8	310	2.40	2	2	ND	2	43	1	2	2	64	.49	.06	6	28	.52	110	.10	2	1.67	.01	.03	2
BL 2+00S	1	20	2	31	.1	13	6	238	1.81	2	2	ND	2	37	1	2	2	55	.45	.06	7	31	.51	81	.10	2	1.46	.01	.03	2
2+00S 4+00E	1	24	3	35	.2	13	9	298	2.83	6	2	ND	2	42	1	3	2	75	.52	.07	6	35	.47	93	.10	2	1.30	.01	.03	2
2+00S 4+50E	1	6	11	36	.4	9	5	231	3.97	2	3	ND	2	24	1	2	2	99	.20	.22	6	31	.41	112	.15	2	1.88	.01	.04	2
2+00S 6+00E	1	8	5	19	.3	9	4	170	2.75	3	2	ND	2	25	1	3	2	88	.24	.04	5	33	.31	55	.12	2	1.03	.01	.04	2
2+00S 6+50E	1	10	5	34	.2	11	6	309	3.40	3	4	ND	2	17	1	3	2	73	.19	.17	6	31	.36	57	.09	2	2.16	.01	.02	2
2+00S 7+00E	1	15	6	40	.4	13	7	301	3.06	2	3	ND	2	22	1	4	2	70	.20	.09	6	35	.47	78	.11	2	2.32	.01	.03	2
2+00S 7+50E	1	10	6	31	.3	10	5	312	2.76	2	2	ND	2	20	1	2	2	71	.19	.08	5	30	.35	52	.10	2	1.60	.01	.03	2
2+00S 8+00E	1	10	3	40	.3	11	6	273	3.64	4	2	ND	2	22	1	4	2	85	.22	.10	6	36	.40	73	.11	2	2.64	.01	.03	2
2+00S 8+50E	1	10	4	42	.3	10	5	297	3.42	3	3	ND	2	22	1	2	2	81	.21	.14	5	32	.34	54	.10	2	2.52	.01	.03	2
2+00S 9+00E	1	10	10	32	.5	8	4	226	3.37	5	4	ND	2	19	1	3	2	79	.14	.08	7	28	.22	60	.13	2	1.67	.01	.03	2
2+00S 9+50E	1	17	2	29	.3	12	7	250	2.58	5	2	ND	2	28	1	2	2	72	.32	.06	5	31	.42	63	.09	2	1.69	.01	.02	2
2+00S 10+00E	1	9	11	58	.5	12	6	298	4.76	4	7	ND	2	17	1	7	2	83	.15	.15	8	32	.35	66	.14	2	2.63	.01	.03	2
2+00S 0+50W	1	11	7	29	.3	11	6	229	2.79	6	3	ND	2	23	1	3	2	78	.22	.04	5	28	.38	69	.10	2	1.71	.01	.02	2
2+00S 1+00W	1	11	12	37	.5	12	7	582	3.99	4	4	ND	2	18	1	2	2	100	.20	.20	6	37	.42	66	.12	2	1.86	.01	.04	2
2+00S 1+50W	1	21	5	26	.3	12	6	279	2.34	5	2	ND	2	29	1	2	2	65	.34	.05	6	31	.46	80	.08	2	1.78	.01	.02	2
STD	23	168	42	92	2.8	636	14	611	3.52	16	5	ND	3	25	1	10	2	50	1.72	.10	5	72	.62	27	.04	20	.95	.04	.22	2
BL 3+00S	1	16	4	30	.3	14	6	229	1.93	2	3	ND	2	32	1	3	2	54	.39	.05	6	25	.48	102	.08	2	1.47	.01	.03	2
3+00S 0+50E	1	18	3	29	.1	12	7	379	2.10	5	2	ND	2	40	1	2	2	61	.54	.06	6	28	.46	91	.10	2	1.24	.01	.03	2
3+00S 1+00E	1	16	4	21	.3	10	5	196	1.94	2	2	ND	2	31	1	2	2	56	.39	.06	5	28	.35	72	.08	2	1.50	.01	.02	2
3+00S 1+50E	1	12	4	36	.2	11	7	318	2.88	3	5	ND	2	36	1	2	2	68	.28	.04	4	18	.62	74	.12	2	1.50	.02	.04	2
3+00S 2+00E	1	8	7	20	.2	5	3	141	1.85	2	2	ND	2	25	1	2	2	58	.16	.04	3	20	.29	46	.07	2	1.34	.01	.03	2
3+00S 4+00E	1	16	5	28	.2	10	5	208	2.05	5	2	ND	2	32	1	2	2	56	.34	.04	5	25	.46	73	.08	2	1.56	.01	.02	2
3+00S 4+50E	1	9	7	42	.3	9	6	455	3.21	2	2	ND	2	26	1	2	2	67	.25	.11	4	26	.42	62	.09	3	1.96	.01	.04	2
3+00S 5+00E	1	8	9	59	.2	7	6	748	2.77	2	3	ND	2	27	1	2	2	65	.24	.18	4	13	.60	103	.09	4	1.56	.01	.16	2
3+00S 5+50E	1	8	3	41	.4	9	6	293	3.53	6	2	ND	2	28	1	2	2	88	.19	.07	4	26	.45	48	.11	2	2.03	.01	.03	2
3+00S 6+00E	1	8	3	29	.2	7	4	231	2.07	2	3	ND	2	55	1	2	2	62	.38	.04	4	17	.35	68	.06	2	1.15	.01	.04	2
3+00S 6+50E	1	13	2	35	.2	13	7	283	2.51	3	2	ND	2	24	1	4	2	61	.22	.05	5	29	.45	59	.09	2	1.94	.01	.03	2
3+00S 7+00E	1	10	5	32	.3	10	5	282	3.33	4	6	ND	2	20	1	4	2	76	.17	.07	6	31	.33	62	.10	2	2.18	.01	.02	2
3+00S 7+50E	1	16	6	30	.3	13	6	277	2.69	2	2	ND	2	25	1	2	2	71	.25	.07	6	31	.42	62	.10	2	1.94	.01	.03	2
3+00S 8+00E	1	12	6	36	.2	11	7	366	2.85	6	2	ND	2	24	1	2	2	93	.25	.12	5	30	.38	95	.09	2	2.05	.01	.03	2
3+00S 0+50W	1	15	6	65	.5	13	7	333	3.90	7	2	ND	2	26	1	2	2	94	.22	.10	6	41	.45	82	.10	2	2.56	.01	.03	2
3+00S 1+00W	1	14	4	30	.4	11	7	529	4.08	4	4	ND	2	20	1	2	2	104	.23	.16	6	48	.32	58	.08	2	2.84	.01	.02	2
3+00S 1+50W	1	22	1	37	.2	15	7	338	2.39	3	2	ND	2	34	1	2	2	58	.41	.07	4	23	.62	77	.08	2	2.15	.02	.04	2
BL 4+00S	1	15	14	48	.6	14	6	283	3.97	5	5	ND	2	18	1	4	2	71	.13	.08	10	34	.38	81	.17	2	2.93	.01	.03	2
4+00S 0+50E	1	19	3	28	.2	12	6	237	2.45	2	4	ND	2	29	1	2	2	70	.37	.06	5	32	.44	72	.09	2	1.61	.01	.02	2
STD A-1	1	30	39	180	.3	35	12	1016	2.80	11	2	ND	2	36	1	2	2	58	.61	.10	7	33	.71	278	.08	6	2.05	.02	.20	2

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM-MAC JOB # 83-369 FILE # 83-2423

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	M ppm
4+00S 1+00E	1	22	9	32	.4	11	5	355	4.25	9	3	ND	2	18	1	2	2	96	.16	.14	5	30	.28	73	.12	2	3.06	.01	.02	2
4+00S 1+50E	1	12	4	29	.2	12	5	226	2.87	7	2	ND	2	21	1	3	2	71	.22	.08	4	29	.41	55	.09	2	1.62	.01	.02	2
4+00S 2+00E	1	10	6	44	.3	10	6	374	3.94	2	2	ND	2	24	1	5	2	79	.20	.17	6	27	.45	71	.12	2	3.36	.01	.04	2
4+00S 5+00E	1	16	6	52	.2	12	8	435	2.58	6	5	ND	2	33	1	3	3	58	.37	.11	5	24	.64	82	.07	2	1.73	.01	.10	2
4+00S 5+50E	1	12	5	32	.2	12	6	285	3.81	2	2	ND	2	25	1	2	2	99	.25	.14	5	39	.41	103	.09	4	2.07	.01	.02	2
4+00S 6+00E	1	10	1	33	.5	10	5	259	2.42	3	4	ND	2	22	1	4	2	55	.17	.04	5	24	.39	62	.08	5	1.55	.01	.03	2
4+00S 6+50E	1	12	5	65	.4	12	6	392	4.14	4	2	ND	2	20	1	3	2	79	.16	.13	7	32	.41	76	.11	6	2.79	.01	.03	2
4+00S 7+00E	1	11	1	43	.3	11	6	283	3.16	9	3	ND	2	25	1	2	2	73	.21	.07	4	35	.43	70	.10	6	2.17	.01	.02	2
4+00S 8+00E	1	10	2	41	.2	10	6	316	3.02	7	2	ND	2	22	1	2	2	59	.16	.09	5	25	.39	71	.09	5	2.68	.01	.02	2
4+00S 0+50W	1	12	7	41	.2	11	6	260	3.53	7	2	ND	2	19	1	2	2	83	.20	.09	5	30	.38	81	.09	5	2.30	.01	.02	2
4+00S 1+00W	1	11	5	36	.3	11	5	298	3.25	3	4	ND	2	20	1	2	2	80	.17	.09	6	29	.35	65	.10	2	1.63	.01	.02	2
4+00S 1+50W	1	14	5	37	.1	12	6	356	3.07	4	2	ND	2	23	1	2	2	71	.26	.13	5	33	.40	75	.07	2	2.59	.01	.02	2
4+00S 2+00W	1	12	7	25	.2	10	5	212	3.16	5	2	ND	2	25	1	2	2	89	.20	.04	5	33	.36	75	.10	2	1.44	.01	.02	2
4+00S 2+50W	1	15	4	38	.2	12	10	791	3.79	6	2	ND	2	43	1	3	2	79	.45	.09	8	32	.53	122	.05	2	1.48	.01	.03	2
BL 5+00S	1	13	4	62	.2	13	6	379	3.81	5	2	ND	2	20	1	2	2	80	.17	.09	6	37	.38	120	.12	2	2.67	.01	.03	2
5+00S 0+50E	1	6	10	30	.3	7	3	248	2.96	3	2	ND	2	14	1	2	2	73	.12	.07	6	21	.21	54	.11	4	1.26	.01	.02	2
5+00S 1+00E	1	10	9	40	.4	10	5	250	4.30	8	2	ND	2	16	1	2	2	87	.14	.17	6	28	.32	63	.12	5	2.17	.01	.02	2
5+00S 1+50E	1	11	9	41	.3	12	5	434	3.76	6	2	ND	2	19	1	2	2	79	.18	.12	6	30	.36	68	.11	4	1.90	.01	.02	2
5+00S 2+00E	1	12	7	43	.3	13	7	276	3.18	5	2	ND	2	24	1	2	2	67	.26	.11	6	33	.44	87	.09	6	2.63	.01	.02	2
5+00S 2+00E(1)	1	17	9	57	.5	17	10	469	4.15	8	2	ND	2	30	1	4	2	101	.40	.13	7	39	1.01	127	.13	6	2.58	.01	.25	2
STD	21	173	44	97	2.8	662	14	654	3.64	16	4	ND	3	25	1	10	2	50	1.76	.10	5	69	.63	29	.04	19	.95	.04	.22	2
5+00S 2+50E	1	6	8	33	.2	10	5	302	3.38	2	2	ND	2	18	1	2	2	78	.13	.15	4	20	.37	69	.10	2	1.29	.01	.04	2
5+00S 3+00E	1	7	6	15	.2	5	3	187	2.42	9	2	ND	2	18	1	2	2	72	.08	.05	3	19	.10	72	.10	2	.80	.01	.02	2
5+00S 4+00E	1	7	8	39	.2	7	5	276	2.91	8	2	ND	2	34	1	4	2	90	.18	.03	3	18	.45	68	.20	2	1.07	.01	.07	2
5+00S 4+50E	1	11	7	29	.2	12	6	259	3.36	3	5	ND	2	23	1	2	2	82	.24	.09	4	30	.42	66	.09	2	1.58	.01	.03	2
5+00S 5+00E	1	12	6	40	.2	12	7	320	3.40	7	2	ND	2	22	1	2	2	77	.20	.09	4	32	.45	100	.09	2	1.93	.01	.02	2
5+00S 6+00E	1	8	4	24	.3	8	4	172	1.92	5	2	ND	2	24	1	2	2	58	.22	.04	5	23	.34	67	.10	4	1.26	.01	.02	2
5+00S 0+50W	1	15	3	39	.4	14	6	264	3.31	7	3	ND	2	25	1	2	2	75	.18	.08	6	34	.46	72	.09	5	1.95	.01	.02	2
5+00S 1+00W	1	11	8	32	.2	10	5	214	3.27	9	2	ND	2	22	1	2	2	76	.18	.12	6	33	.35	100	.10	2	1.63	.01	.02	2
5+00S 1+50W	1	5	9	31	.4	5	3	195	2.43	5	2	ND	2	10	1	3	2	54	.08	.08	6	22	.14	58	.09	2	1.42	.01	.02	2
5+00S 2+50W	1	5	12	17	.2	3	1	81	1.26	3	2	ND	2	13	1	2	2	38	.08	.03	8	15	.08	67	.08	2	.92	.01	.02	2
5+00S 3+00W	1	10	5	41	.1	11	6	261	3.00	5	2	ND	2	17	1	2	2	73	.14	.09	5	30	.32	85	.08	2	1.74	.01	.02	2
5+00S 3+50W	1	9	4	24	.1	8	5	289	2.59	6	2	ND	2	17	1	2	2	71	.18	.07	4	25	.25	61	.07	2	1.38	.01	.02	2
BL 6+00S	1	8	7	30	.3	9	4	238	3.45	7	2	ND	2	19	1	2	2	83	.15	.11	4	28	.27	86	.11	2	1.31	.01	.02	2
6+00S 0+50E	1	10	7	31	.4	9	4	309	2.97	2	2	ND	2	22	1	2	2	75	.18	.05	5	28	.28	76	.09	4	1.67	.01	.03	2
6+00S 1+50E	1	9	7	39	.4	10	5	407	3.57	2	3	ND	2	18	1	4	2	77	.16	.08	5	31	.32	86	.09	5	1.85	.01	.02	2
6+00S 2+50E	1	5	8	38	.2	7	3	204	1.75	2	2	ND	2	30	1	4	2	50	.18	.02	4	13	.55	77	.14	4	1.14	.01	.11	2
6+00S 3+00E	1	11	1	44	.1	9	6	455	2.05	5	2	ND	2	59	1	2	2	50	.41	.09	5	19	.58	110	.07	2	1.31	.01	.07	2
6+00S 4+50E	1	8	7	33	.2	8	4	255	3.28	3	2	ND	2	18	1	2	2	74	.14	.10	6	24	.28	85	.11	4	1.93	.01	.03	2
6+00S 5+00E	1	9	8	34	.2	9	5	232	2.96	3	2	ND	2	31	1	2	2	65	.14	.09	5	21	.35	104	.09	3	1.78	.01	.03	2
STD A-1	1	29	38	182	.3	35	12	1025	2.80	10	2	ND	2	35	1	2	2	57	.60	.10	7	73	.70	283	.08	6	1.96	.02	.19	2

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM-MAC JOB # 83-369 FILE # 83-2423

PAGE # 1

SAMPLE #	Mo ppa	Cu ppa	Pb ppa	Zn ppa	Ag ppa	Ni ppa	Co ppa	Mn ppa	Fe %	As ppa	U ppa	Au ppa	Th ppa	Sr ppa	Cd ppa	Sb ppa	Bi ppa	V ppa	Ca %	P %	La ppa	Cr ppa	Mg %	Ba ppa	Ti %	B ppa	Al %	Na %	K %	M ppa
6+00S 5+50E	1	8	9	60	.3	10	6	555	4.11	7	2	ND	2	41	1	2	2	90	.32	.15	5	26	.78	78	.15	3	2.23	.01	.06	2
6+00S 6+50E	1	9	1	57	.3	14	6	448	4.00	2	2	ND	2	41	1	2	2	88	.28	.09	5	35	.92	61	.15	3	2.61	.01	.05	2
6+00S 7+00E	1	8	6	32	.2	8	4	267	3.13	3	2	ND	2	36	1	2	2	76	.26	.09	6	27	.41	55	.13	3	1.53	.01	.03	2
6+00S 8+00E	1	6	1	35	.2	5	3	242	1.52	2	2	ND	2	73	1	2	2	47	.53	.07	5	10	.48	70	.10	2	1.06	.01	.05	2
6+00S 0+50M	1	20	2	61	.4	15	7	445	3.50	2	2	ND	2	37	1	3	2	80	.33	.08	9	38	.53	90	.12	3	2.78	.01	.04	2
6+00S 1+00M	1	15	3	47	.1	11	6	297	3.27	3	2	ND	2	29	1	2	2	71	.26	.07	7	38	.41	69	.12	2	2.27	.01	.03	2
6+00S 1+50M	1	15	3	51	.3	12	6	309	3.85	4	2	ND	2	30	1	2	2	91	.28	.10	7	39	.42	87	.14	3	2.66	.01	.03	2
6+00S 2+00M	1	13	4	68	.4	11	6	283	3.86	2	2	ND	2	28	1	2	2	89	.24	.08	7	40	.36	94	.15	2	2.61	.01	.03	2
6+00S 2+50M	1	15	2	37	.3	13	7	307	3.19	5	2	ND	2	32	1	2	2	77	.30	.07	7	38	.48	83	.13	3	2.45	.01	.03	2
6+00S 3+00M	1	19	2	30	.1	11	6	247	2.31	2	3	ND	2	34	1	2	2	64	.40	.06	6	32	.43	84	.10	2	1.55	.01	.03	2
6+00S 3+50M	1	13	1	43	.3	13	7	300	3.26	3	2	ND	2	32	1	2	2	79	.31	.07	8	39	.47	75	.13	3	2.25	.01	.03	2
6+00S 4+00M	1	15	5	34	.3	9	5	347	3.47	9	2	ND	2	31	1	2	2	82	.30	.07	8	33	.33	91	.13	3	1.81	.01	.03	2
6+00S 4+50M	1	15	2	30	.3	12	6	281	3.13	4	2	ND	2	41	1	2	2	86	.49	.06	7	42	.47	78	.13	3	1.63	.01	.03	2
6+00S 5+00M	1	8	9	31	.1	8	4	269	3.05	4	2	ND	2	28	1	3	2	80	.27	.11	8	30	.34	65	.14	2	1.64	.01	.03	2
6+00S 5+50M	1	10	9	39	.2	10	5	496	3.72	4	2	ND	2	29	1	2	2	84	.27	.14	8	31	.38	87	.16	3	1.92	.01	.03	2
6+00S 6+00M	1	11	2	49	.4	12	6	378	3.82	3	2	ND	2	31	1	3	2	92	.30	.13	6	41	.47	95	.14	6	2.45	.01	.03	2
6+00S 6+50M	1	20	2	37	.1	17	9	358	3.39	6	2	ND	2	50	1	2	2	91	.58	.06	8	44	.66	112	.15	3	2.07	.01	.03	2
BL 7+00S	1	15	4	37	.3	13	7	367	3.37	4	3	ND	2	49	1	2	2	87	.59	.04	6	38	.52	85	.14	9	1.45	.01	.04	2
7+00S 0+50E	1	9	3	32	.3	10	5	317	3.72	2	2	ND	2	25	1	2	2	91	.21	.06	6	34	.30	63	.13	5	1.78	.01	.03	2
7+00S 1+00E	1	9	1	40	.1	10	5	267	3.43	5	2	ND	2	27	1	2	2	82	.25	.10	5	36	.35	79	.11	2	1.85	.01	.03	2
STD	23	179	50	96	2.8	663	14	671	3.98	15	2	ND	3	27	1	8	2	56	1.74	.10	6	107	.67	26	.05	25	1.09	.04	.23	2
7+00S 2+00E	1	7	2	23	.3	8	4	200	3.29	2	2	ND	2	31	1	2	2	89	.22	.05	5	26	.28	47	.14	2	1.82	.01	.03	2
7+00S 2+50E	1	4	1	31	.1	6	4	256	1.88	2	3	ND	2	51	1	2	2	46	.33	.05	5	12	.40	48	.11	3	1.24	.01	.06	2
7+00S 3+50E	1	8	5	39	.5	9	5	413	3.53	2	2	ND	2	41	1	2	2	84	.27	.09	5	25	.49	104	.14	3	2.13	.01	.04	2
7+00S 4+50E	1	17	2	31	.3	9	5	246	2.75	3	2	ND	2	42	1	2	2	74	.33	.06	6	29	.44	79	.13	3	2.11	.01	.04	2
7+00S 7+00E	1	7	1	34	.2	5	4	274	1.79	2	2	ND	2	65	1	2	2	52	.38	.03	4	11	.38	67	.11	2	1.14	.01	.10	2
7+00S 7+50E	1	8	1	33	.1	8	5	314	2.75	4	4	ND	2	42	1	2	2	68	.28	.05	5	21	.46	59	.12	3	1.72	.01	.04	2
7+00S 0+50M	1	9	5	24	.3	9	4	326	3.90	8	2	ND	2	29	1	2	2	119	.23	.05	6	39	.24	94	.16	3	1.42	.01	.04	2
7+00S 2+50M	1	11	1	29	.1	10	5	235	1.31	3	2	ND	2	40	1	2	2	40	.49	.05	7	23	.49	91	.13	2	1.60	.01	.04	2
7+00S 3+00M	1	22	1	34	.2	14	8	408	2.55	5	2	ND	2	45	1	2	2	68	.56	.06	8	31	.54	117	.11	2	1.62	.01	.03	2
7+00S 5+00M	1	21	2	36	.1	13	7	318	2.42	4	2	ND	2	54	1	2	2	68	.71	.06	9	32	.56	108	.14	3	1.57	.01	.03	2
7+00S 5+50M	1	15	2	35	.3	12	6	306	2.60	4	2	ND	2	35	1	2	2	71	.41	.06	6	33	.48	81	.12	10	1.70	.01	.03	2
7+00S 6+00M	1	12	3	34	.4	11	5	222	2.66	6	2	ND	2	34	1	2	2	68	.40	.06	9	33	.42	84	.13	3	2.35	.01	.03	2
7+00S 6+50M	1	8	5	30	.1	10	5	213	3.10	3	2	ND	2	31	1	2	2	81	.30	.10	6	33	.35	82	.13	2	2.11	.01	.03	2
7+00S 7+00M	1	20	1	34	.2	15	8	370	2.90	6	2	ND	2	51	1	2	2	81	.60	.06	7	38	.59	108	.14	3	1.85	.01	.03	2
8+00S 1+00E	1	18	1	30	.2	11	6	268	2.50	6	2	ND	2	38	1	3	2	67	.40	.07	7	30	.46	89	.11	2	2.17	.01	.03	2
8+00S 1+50E	1	16	1	33	.2	13	7	286	2.88	4	2	ND	2	38	1	2	2	71	.34	.05	6	33	.51	96	.13	2	2.13	.01	.03	2
8+00S 2+00E	1	12	1	44	.1	10	7	422	2.41	7	2	ND	2	48	1	2	3	64	.46	.07	7	23	.58	92	.11	2	1.65	.01	.08	2
8+00S 2+50E	1	12	2	35	.1	10	6	270	2.43	5	2	ND	2	42	1	2	2	64	.35	.04	6	21	.57	77	.12	2	1.68	.01	.07	2
8+00S 3+00E	1	12	1	43	.1	8	5	331	2.12	2	2	ND	2	75	1	2	2	59	.66	.12	8	22	.58	103	.10	2	1.44	.02	.10	2
STD A-1	1	29	39	181	.3	35	12	1069	2.93	12	2	ND	2	34	1	2	2	57	.60	.10	7	73	.73	281	.08	6	2.04	.02	.20	2

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM JOB# B3-369 FILE # 83-2420

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe ppm	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm
B+00S 3+50E	1	8	7	40	.1	10	5	296	3.65	2	3	ND	2	38	1	2	2	71	.26	.14	6	24	.49	138	.12	2	2.06	.01	.03	2
B+00S 5+50E	1	5	4	28	.1	6	4	285	1.25	2	2	ND	2	73	1	2	3	39	.51	.08	5	11	.37	61	.08	2	.92	.01	.05	2
B+00S 7+50E	1	7	4	42	.3	9	4	234	2.15	4	3	ND	2	52	1	2	2	57	.31	.04	6	19	.46	61	.14	2	1.69	.01	.04	2
B+00S 0+50W	1	14	4	45	.1	12	7	358	2.34	2	2	ND	2	77	1	2	2	63	.70	.07	8	25	.61	86	.12	2	1.43	.01	.06	2
B+00S 1+50W	1	16	3	33	.2	13	8	421	2.64	5	2	ND	2	50	1	2	2	87	.64	.06	7	39	.50	98	.14	2	1.42	.01	.03	2
B+00S 2+00W	1	8	7	40	.3	9	4	233	2.72	3	2	ND	2	35	1	2	2	74	.29	.07	9	30	.36	58	.16	2	1.83	.01	.03	2
B+00S 2+50W	1	6	3	16	.2	5	2	172	2.08	2	3	ND	2	35	1	2	2	68	.29	.02	5	28	.14	89	.12	2	.82	.01	.03	2
B+00S 3+00W	1	11	2	34	.3	12	6	284	2.99	4	2	ND	2	42	1	2	2	81	.43	.10	7	28	.50	87	.12	3	2.04	.01	.04	2
B+00S 3+50W	1	21	4	52	.1	15	8	434	2.68	3	2	ND	2	53	1	2	2	77	.64	.06	9	35	.56	128	.12	2	1.79	.01	.03	2
B+00S 5+00W	1	20	7	52	.2	14	7	386	2.51	4	2	ND	2	56	1	2	2	74	.64	.05	9	36	.51	109	.15	2	1.48	.01	.03	2
B+00S 5+50W	1	21	5	36	.2	15	7	297	2.75	4	2	ND	2	43	1	2	2	77	.46	.05	7	37	.55	88	.14	2	1.89	.01	.03	2
B+00S 6+00W	1	13	5	58	.1	15	8	347	3.25	6	2	ND	2	32	1	2	2	81	.30	.07	6	43	.49	93	.15	2	2.48	.01	.03	2
B+00S 6+50W	1	23	4	44	.4	18	8	341	3.24	7	2	ND	2	38	1	2	2	84	.36	.04	7	44	.61	94	.15	2	2.63	.01	.02	2
B+00S 7+00W	1	17	5	42	.2	16	8	339	3.44	4	2	ND	2	38	1	2	2	92	.37	.06	7	44	.53	91	.14	2	2.59	.01	.03	2
B+00S 7+50W	1	21	6	38	.2	16	9	423	3.07	5	3	ND	2	65	1	2	2	95	.82	.06	9	46	.60	114	.17	2	1.57	.01	.03	2
B+00S 9+00W	1	23	6	53	.3	16	9	439	2.81	2	2	ND	2	64	1	2	2	84	.82	.07	9	41	.64	155	.12	3	2.12	.01	.04	2
BL 9+00S	1	25	5	43	.1	18	7	283	3.63	2	2	ND	2	36	1	2	2	84	.30	.09	8	39	.48	81	.16	2	2.90	.01	.03	2
9+00S 0+50E	1	15	6	47	.3	16	7	331	3.72	7	2	ND	2	37	1	2	2	81	.32	.09	8	41	.52	111	.15	4	3.35	.01	.03	2
9+00S 1+00E	1	11	4	32	.2	11	6	250	3.49	5	2	ND	2	51	1	2	2	90	.42	.04	7	35	.38	122	.16	3	1.60	.01	.02	2
9+00S 1+50E	1	17	2	49	.1	14	7	280	2.62	2	3	ND	2	37	1	2	2	68	.34	.06	6	31	.49	75	.12	2	1.95	.01	.03	2
STD	25	184	45	99	3.1	680	15	665	3.92	16	2	ND	3	28	1	7	2	57	1.77	.09	6	104	.67	37	.05	27	1.09	.04	.23	2
9+00S 3+50E	1	13	6	44	.1	14	7	332	2.99	5	3	ND	2	38	1	2	2	72	.29	.08	6	29	.53	98	.12	2	2.44	.01	.03	2
9+00S 4+00E	1	11	3	48	.1	12	8	508	3.25	2	2	ND	2	89	1	2	2	66	.63	.10	6	22	.64	100	.09	2	1.54	.01	.09	2
9+00S 4+50E	1	11	3	55	.1	11	7	411	2.92	2	2	ND	2	80	1	2	2	77	.53	.10	6	23	.62	55	.10	3	1.66	.01	.10	2
9+00S 5+00E	1	9	2	40	.1	9	6	389	2.45	3	3	ND	2	79	1	2	2	67	.76	.14	6	22	.48	55	.06	2	1.10	.01	.10	2
9+00S 5+50E	1	7	4	46	.1	9	6	349	2.51	2	2	ND	2	98	1	2	2	70	.72	.15	6	23	.56	71	.09	2	1.20	.01	.14	2
9+00S 6+00E	1	9	4	41	.1	8	6	328	2.39	2	2	ND	2	76	1	2	2	67	.59	.10	6	21	.48	71	.09	3	1.07	.01	.10	2
9+00S 6+50E	1	12	3	53	.2	11	6	368	2.08	4	2	ND	2	74	1	2	2	58	.63	.07	7	22	.71	99	.14	2	1.57	.01	.07	2
9+00S 7+00E	1	11	4	43	.2	10	6	327	2.57	2	3	ND	2	48	1	2	2	65	.38	.05	7	22	.53	85	.14	3	1.65	.01	.05	2
9+00S 7+50E	1	7	3	51	.1	9	5	309	1.55	2	3	ND	2	59	1	2	3	42	.46	.07	7	17	.61	89	.10	2	1.48	.01	.08	2
9+00S 8+00E	1	8	5	41	.2	9	5	270	3.26	3	4	ND	2	41	1	2	2	79	.22	.08	4	16	.46	55	.15	2	1.59	.01	.05	2
9+00S 0+50W	1	20	9	32	.3	13	6	271	4.25	6	2	ND	2	32	1	2	2	98	.27	.11	6	36	.41	72	.14	3	3.04	.01	.03	2
9+00S 1+00W	1	17	7	45	.4	15	10	405	3.01	2	2	ND	2	46	1	2	2	83	.50	.09	8	34	.79	99	.11	3	2.14	.01	.14	2
9+00S 2+50W	1	21	3	31	.2	13	6	236	2.21	4	4	ND	2	39	1	2	2	65	.41	.04	8	33	.48	113	.10	2	2.04	.01	.03	2
9+00S 3+00W	1	17	3	51	.4	17	8	396	3.25	7	2	ND	2	45	1	2	2	86	.48	.05	8	39	.64	122	.15	3	2.37	.01	.04	2
9+00S 3+50W	1	20	6	48	.4	17	8	323	3.55	6	2	ND	2	38	1	2	2	90	.38	.07	8	38	.61	97	.15	4	2.66	.01	.04	2
9+00S 5+00W	1	15	5	28	.2	14	6	261	3.14	6	2	ND	2	41	1	2	2	84	.44	.05	8	41	.46	84	.14	3	2.12	.01	.02	2
9+00S 6+00W	1	20	5	36	.3	14	7	277	2.05	5	2	ND	2	55	1	2	2	66	.70	.05	8	36	.56	127	.15	3	1.65	.01	.02	2
9+00S 6+50W	1	12	5	28	.1	10	4	545	1.35	2	2	ND	2	40	1	2	2	47	.37	.03	6	27	.29	189	.08	2	1.66	.01	.03	2
9+00S 7+00W	1	14	7	24	.2	10	4	193	1.80	2	2	ND	2	38	1	2	2	57	.40	.03	6	24	.37	86	.11	2	1.32	.01	.02	2
STD A-1	1	30	38	180	.3	36	12	1030	2.82	11	2	ND	2	36	1	2	2	57	.60	.09	8	74	.73	285	.08	6	2.07	.01	.19	2

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM JOB# 83-369 FILE # 83-2423

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	M ppm
9+00S 7+50W	1	21	3	33	.1	14	8	367	2.51	8	2	ND	2	57	1	2	2	75	.67	.06	10	36	.52	105	.15	2	1.44	.01	.02	?
9+00S 8+00W	1	31	2	47	.2	19	9	426	2.98	9	2	ND	2	64	1	2	2	83	.92	.06	9	41	.66	139	.14	6	1.84	.02	.05	2
9+00S 8+50W	1	19	3	38	.2	16	8	346	2.63	4	2	ND	2	58	1	2	2	79	.75	.06	8	37	.65	115	.15	2	1.78	.01	.02	2
9+00S 9+00W	1	20	5	46	.1	17	9	524	2.71	3	2	ND	2	57	1	2	2	79	.85	.05	8	41	.59	125	.13	3	1.69	.02	.03	2
10+00S 0+50E	1	12	4	31	.3	10	4	208	2.12	7	3	ND	2	38	1	2	2	58	.40	.05	7	27	.36	88	.11	2	1.49	.01	.03	2
10+00S 1+50E	1	9	4	43	.4	10	5	304	3.07	4	2	ND	2	29	1	2	2	75	.24	.12	8	27	.40	72	.14	2	2.13	.01	.03	2
10+00S 2+00E	1	8	1	34	.4	11	5	251	3.73	7	2	ND	2	28	1	2	2	89	.22	.13	6	26	.40	67	.14	2	1.92	.01	.02	2
10+00S 2+50E	1	14	4	54	.5	14	7	351	3.87	8	2	ND	2	31	1	2	2	78	.23	.13	7	27	.50	83	.15	2	2.96	.01	.03	2
10+00S 3+00E	1	8	6	39	.3	10	5	226	3.18	13	2	ND	2	28	1	2	2	71	.17	.07	8	25	.35	80	.14	2	2.61	.01	.02	2
10+00S 3+50E	1	8	1	57	.2	13	9	431	3.54	8	2	ND	2	48	1	2	2	88	.38	.11	6	27	.75	76	.12	2	2.35	.01	.09	2
10+00S 4+00E	1	4	5	28	.3	5	3	172	1.84	2	2	ND	2	31	1	3	2	51	.15	.06	6	13	.28	44	.14	2	1.25	.01	.02	2
10+00S 4+50E	1	6	3	74	.4	32	12	521	3.69	10	2	ND	2	26	1	2	2	108	.18	.04	3	55	1.81	50	.28	2	3.07	.01	.09	2
10+00S 5+00E	1	9	1	39	.2	11	6	281	3.32	5	2	ND	2	33	1	2	2	75	.25	.14	5	25	.47	68	.11	2	2.52	.01	.03	2
10+00S 6+00E	1	7	1	33	.1	8	6	266	2.10	2	5	ND	2	62	1	2	2	60	.53	.12	7	18	.42	62	.08	2	1.02	.01	.10	2
10+00S 6+50E	1	10	4	42	.1	11	6	275	2.68	6	3	ND	2	44	1	2	2	69	.30	.04	6	24	.50	74	.13	2	1.93	.01	.06	2
10+00S 7+00E	1	11	3	39	.4	11	5	287	3.82	8	5	ND	2	39	1	2	2	95	.24	.12	6	24	.45	100	.16	6	1.99	.01	.03	2
10+00S 7+50E	1	10	6	61	.2	12	7	475	3.11	2	2	ND	2	60	1	2	2	92	.30	.04	6	24	.68	116	.11	2	2.30	.01	.07	2
10+00S 8+00E	1	10	1	43	.2	12	6	293	3.33	2	3	ND	2	40	1	2	2	75	.27	.06	6	25	.50	70	.12	11	1.99	.01	.03	2
BL 10+00S	1	7	6	62	.4	10	6	481	4.18	3	2	ND	2	22	1	2	2	83	.19	.19	10	27	.46	69	.15	2	2.13	.01	.06	2
10+00S 0+50W	1	8	7	60	.4	14	7	498	3.94	9	2	ND	2	55	1	2	2	108	.61	.04	8	30	1.01	139	.22	2	2.04	.01	.09	2
STD	25	182	42	97	4.2	695	15	650	3.81	13	4	ND	2	28	1	9	2	56	1.76	.10	6	90	.64	35	.04	26	1.05	.04	.26	2
10+00S 1+00W	1	8	4	60	.3	13	6	244	3.11	5	3	ND	2	37	1	2	2	101	.33	.03	6	32	.45	110	.17	2	1.45	.01	.05	2
10+00S 1+50W	1	23	6	47	.3	17	8	356	3.15	6	3	ND	2	52	1	2	2	81	.62	.06	8	33	.75	132	.13	2	2.24	.01	.09	2
10+00S 3+50W	1	15	4	63	.4	20	12	644	4.01	13	2	ND	2	62	1	2	2	101	.65	.16	12	39	1.31	148	.16	2	2.71	.01	.50	2
10+00S 4+00W	1	8	3	37	.5	14	8	452	3.84	5	2	ND	2	43	1	2	2	91	.45	.16	6	30	.67	62	.13	2	1.74	.01	.14	2
10+00S 4+50W	1	11	4	42	.3	13	7	416	2.58	7	2	ND	2	55	1	2	2	70	.59	.11	7	26	.87	105	.12	2	1.76	.01	.28	2
10+00S 7+50W	1	17	1	32	.1	16	7	312	3.00	4	4	ND	2	46	1	2	2	90	.54	.06	8	42	.46	87	.14	2	1.62	.01	.02	2
10+00S 8+00W	1	10	7	37	.4	13	6	414	3.60	6	2	ND	2	26	1	2	2	84	.23	.13	10	29	.38	77	.13	3	1.99	.01	.03	2
10+00S 8+50W	1	31	5	45	.4	18	8	495	3.01	3	2	ND	2	41	1	2	2	78	.51	.07	8	39	.52	223	.05	2	2.90	.01	.05	2
10+00S 9+00W	1	20	2	38	.2	18	9	372	2.97	6	5	ND	2	54	1	2	2	84	.56	.05	8	39	.65	117	.15	3	1.99	.01	.02	2
10+00S 9+50W	1	42	9	59	.4	28	21	2446	5.51	6	2	ND	2	58	1	2	2	130	.93	.08	9	54	.88	282	.06	4	3.37	.01	.06	2
BL 11+00S	1	13	7	146	.3	15	9	1133	3.95	8	2	ND	2	41	1	2	2	97	.33	.18	6	34	.93	145	.17	2	2.19	.01	.09	2
11+00S 0+50E	1	8	5	56	.2	8	5	290	3.20	4	3	ND	2	48	1	2	2	81	.19	.13	4	18	.52	45	.16	2	1.47	.01	.05	2
11+00S 1+00E	1	11	1	35	.4	10	5	244	2.92	2	3	ND	2	37	1	2	2	77	.25	.07	5	26	.41	62	.14	2	1.86	.01	.03	2
11+00S 1+50E	1	8	4	42	.2	9	9	1050	2.49	2	3	ND	2	60	1	2	2	72	.51	.04	6	22	.49	70	.14	2	1.33	.01	.05	2
11+00S 2+00E	1	5	3	74	.2	8	5	325	2.82	2	3	ND	2	55	1	2	2	64	.20	.13	4	11	.56	57	.15	2	1.72	.01	.06	2
11+00S 2+50E	1	4	2	38	.3	7	4	245	2.88	5	5	ND	2	44	1	2	3	81	.18	.05	5	17	.34	53	.17	2	1.50	.01	.03	2
11+00S 3+00E	1	9	1	32	.1	10	5	243	2.82	4	6	ND	2	40	1	2	2	75	.31	.07	5	22	.43	63	.14	2	1.41	.01	.05	2
11+00S 3+50E	1	14	4	38	.4	10	6	402	2.19	3	3	ND	2	112	1	2	2	84	1.06	.10	11	22	.49	139	.06	2	1.68	.01	.07	2
11+00S 4+00E	1	10	4	52	.2	10	7	555	2.46	2	2	ND	2	77	1	2	2	77	.69	.14	8	20	.65	129	.07	2	1.80	.01	.07	2
STD A-1	1	30	36	182	.3	37	12	1026	2.81	11	2	ND	2	36	1	2	2	58	.60	.10	8	70	.69	274	.08	6	2.06	.02	.21	2

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM JOB# 83-369 FILE # 83-2423

SAMPLE #	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	N
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	I	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	I	I	ppm	ppm	I	ppm	I	ppm	I	I	I	ppm
11+005 5+00E	1	8	5	68	.1	14	9	446	4.07	2	6	ND	2	53	1	2	2	109	.30	.08	4	31	1.03	51	.20	3	2.08	.01	.07	2
11+005 5+50E	1	4	8	42	.3	4	3	234	2.17	6	2	ND	2	38	1	3	3	72	.16	.04	8	10	.39	41	.23	2	1.11	.01	.07	2
11+005 6+00E	1	8	3	36	.2	6	4	302	1.58	2	2	ND	2	98	1	2	2	47	.70	.04	5	13	.45	82	.08	3	1.26	.01	.07	2
11+005 6+50E	1	7	5	48	.2	8	5	365	2.48	2	2	ND	2	67	1	2	3	77	.43	.09	6	17	.67	90	.14	3	1.69	.01	.08	2
11+005 7+00E	1	7	5	36	.3	9	5	248	3.14	4	6	ND	2	43	1	2	2	80	.27	.11	6	25	.42	69	.13	4	2.53	.01	.05	2
11+005 7+50E	1	6	4	40	.2	6	8	416	2.10	3	2	ND	2	88	1	2	2	60	.47	.10	5	18	.43	79	.07	3	1.13	.01	.12	2
11+005 8+00E	1	14	3	70	.4	13	8	437	2.81	2	3	ND	2	84	1	2	2	85	.54	.08	7	28	.81	143	.12	3	2.47	.01	.10	2
11+005 8+50E	1	10	1	54	.2	9	7	440	2.52	2	3	ND	2	73	1	2	2	67	.41	.07	6	19	.69	113	.12	3	1.96	.01	.14	2
11+005 9+00E	1	9	4	47	.2	10	5	270	2.99	2	4	ND	2	41	1	2	2	71	.26	.08	6	24	.44	89	.12	3	2.73	.01	.05	2
11+005 9+50E	1	5	1	33	.1	5	4	238	1.80	2	3	ND	2	51	1	2	2	51	.27	.05	4	11	.40	39	.10	2	1.18	.01	.07	2
11+005 0+50W	1	8	6	33	.2	6	4	227	2.23	4	2	ND	2	54	1	2	2	77	.33	.03	7	25	.36	73	.20	3	1.00	.01	.07	2
11+005 1+00W	1	13	10	47	.3	12	7	509	3.24	2	2	ND	2	68	1	2	2	93	.72	.06	12	32	.67	111	.19	4	1.48	.01	.11	2
11+005 1+50W	1	9	7	88	.1	19	9	536	5.37	2	5	ND	2	33	1	2	2	139	.31	.13	7	40	1.36	128	.24	4	3.02	.01	.19	2
11+005 2+00W	1	10	10	54	.6	13	7	411	4.80	2	2	ND	2	36	1	2	2	120	.24	.06	12	33	.65	77	.25	5	2.36	.01	.10	2
BL 12+00S	1	32	6	75	.5	15	10	807	3.48	2	2	ND	2	100	1	2	2	89	1.07	.14	19	33	.96	154	.10	3	2.23	.01	.20	2
12+005 0+50E	1	15	6	40	.2	13	6	287	2.43	2	2	ND	2	54	1	2	3	74	.59	.09	8	33	.60	103	.14	3	1.62	.01	.08	2
12+005 1+00E	1	15	1	40	.1	13	7	297	3.18	2	2	ND	2	42	1	2	2	81	.35	.07	7	32	.58	85	.14	3	2.15	.01	.05	2
12+005 1+50E	1	16	5	41	.1	13	7	320	3.08	4	3	ND	2	38	1	2	3	77	.26	.03	8	35	.52	93	.15	3	2.52	.01	.05	2
12+005 2+00E	1	7	6	68	.1	8	6	392	3.14	2	3	ND	2	54	1	4	2	90	.28	.05	4	14	.68	95	.19	3	1.56	.01	.14	2
12+005 2+50E	1	11	3	49	.1	10	8	350	2.38	2	2	ND	2	56	1	2	2	65	.53	.05	6	18	.67	93	.13	3	1.53	.01	.09	2
STD	25	177	36	95	3.0	670	14	654	3.79	13	4	ND	3	28	1	9	2	56	1.77	.10	6	99	.66	35	.05	29	1.09	.04	.25	2
12+005 4+00E	1	10	7	49	.2	13	6	331	2.59	2	2	ND	2	54	1	2	2	71	.42	.05	6	25	.63	77	.13	3	1.98	.01	.06	2
12+005 4+50E	1	6	7	34	.2	8	4	236	2.66	2	2	ND	2	44	1	2	2	93	.26	.03	5	19	.45	39	.19	3	1.40	.01	.05	2
12+005 5+00E	1	11	3	73	.2	11	10	1085	3.09	2	2	ND	2	100	1	2	2	95	1.07	.16	7	18	1.15	122	.13	4	2.14	.02	.22	2
12+005 5+50E	1	13	3	46	.4	7	6	768	1.85	2	2	ND	2	187	1	2	2	51	2.00	.16	12	13	.53	106	.05	3	1.21	.01	.12	2
12+005 6+00E	1	5	2	62	.2	8	6	560	2.68	4	2	ND	2	62	1	2	2	85	.60	.14	5	14	.82	65	.13	8	1.69	.02	.14	2
12+005 7+00E	1	9	9	59	.3	13	6	343	2.48	4	2	ND	2	78	1	3	2	83	.45	.04	5	27	.68	96	.14	4	2.10	.01	.11	2
12+005 7+50E	1	17	7	63	.4	13	10	680	3.01	2	2	ND	2	95	1	2	2	87	.60	.12	8	31	.75	183	.07	3	2.72	.01	.11	2
12+005 8+00E	1	16	12	64	.3	15	8	522	3.79	3	3	ND	2	55	1	2	2	104	.35	.09	7	35	.79	138	.11	3	3.24	.01	.10	2
12+005 8+50E	1	8	4	33	.2	7	4	287	1.64	3	2	ND	2	63	1	2	2	57	.25	.05	4	21	.36	79	.07	2	1.52	.01	.07	2
12+005 1+00W	1	10	3	52	.2	32	7	385	2.28	7	2	ND	2	54	1	2	2	70	.62	.05	4	68	1.05	97	.16	2	1.56	.01	.24	2
12+005 1+50W	1	32	3	7	.3	8	4	624	1.19	2	2	ND	2	212	1	2	2	27	3.95	.09	4	5	.13	233	.01	3	.62	.01	.03	2
12+005 2+00W	1	11	9	71	.2	16	12	705	4.19	4	2	ND	2	64	1	2	2	101	.88	.14	7	33	1.32	125	.16	2	2.66	.01	.39	2
12+005 2+50W	1	15	5	55	.1	14	9	572	3.03	3	2	ND	2	63	1	2	2	78	.81	.15	9	28	1.01	113	.15	2	1.93	.01	.37	2
12+005 3+00W	1	23	8	74	.4	20	14	2903	4.34	4	4	ND	2	88	1	4	2	98	1.02	.13	9	44	1.43	242	.14	4	2.88	.02	.46	2
12+005 4+00W	1	6	4	48	.3	10	6	771	4.55	2	2	ND	2	84	1	2	2	67	.80	.16	7	16	.62	83	.09	3	1.46	.01	.10	2
12+005 4+50W	1	10	1	47	.2	10	7	633	2.20	2	2	ND	2	64	1	2	2	52	.56	.10	6	19	.67	91	.08	2	1.59	.01	.14	2
12+005 5+00W	1	16	11	70	.4	20	12	785	4.24	2	4	ND	2	61	1	2	2	103	.73	.13	8	36	1.38	122	.17	3	2.83	.01	.44	2
12+005 5+50W	1	12	2	50	.2	9	7	873	2.24	2	2	ND	2	81	1	2	2	53	.63	.11	10	16	.60	112	.07	2	1.55	.01	.10	2
12+005 6+50W	1	28	5	65	.4	15	27	1909	3.17	2	2	ND	2	91	1	2	3	82	.65	.08	12	27	.83	166	.11	3	2.39	.02	.16	2
STD A-1	1	29	38	180	.3	36	12	1036	2.82	11	2	ND	2	35	1	2	2	59	.60	.10	8	74	.73	277	.09	6	2.07	.02	.21	2

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Mi ppm	Co ppm	Mn ppm	Fe I	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca I	P I	La ppm	Cr ppm	Mg I	Ba ppm	Ti I	B ppm	Al I	Na I	K I	M ppm
13+00S 1+00E	1	9	5	44	.1	10	5	243	2.90	2	4	ND	2	32	1	2	2	70	.23	.06	5	28	.42	75	.13	9	2.01	.01	.04	2
13+00S 1+50E	1	7	6	13	.3	4	2	97	.93	2	2	ND	2	86	1	2	2	31	.76	.03	4	8	.16	60	.08	7	.57	.01	.04	2
13+00S 2+00E	2	24	8	69	.5	14	11	1740	4.92	2	2	ND	2	98	1	2	2	101	.85	.12	16	29	.71	197	.06	10	2.46	.02	.09	2
13+00S 3+50E	1	7	9	40	.3	7	5	251	2.55	7	2	ND	2	39	1	2	2	74	.24	.07	6	21	.44	61	.16	6	1.56	.01	.04	2
13+00S 4+50E	1	4	5	23	.1	4	3	153	1.84	2	2	ND	2	44	1	2	2	51	.14	.04	4	9	.16	53	.09	8	1.09	.01	.02	2
13+00S 5+00E	1	3	6	10	.2	1	1	87	.94	2	2	ND	2	54	1	2	2	35	.14	.01	3	3	.05	48	.05	8	.68	.01	.02	2
13+00S 5+50E	1	5	8	33	.3	5	3	218	2.13	2	2	ND	2	61	1	2	3	65	.21	.03	6	9	.31	51	.14	8	1.04	.01	.05	2
13+00S 6+00E	1	3	5	13	.2	2	2	95	.98	2	2	ND	2	46	1	2	2	28	.13	.01	3	2	.08	30	.05	7	.46	.01	.02	2
13+00S 6+50E	1	5	5	42	.2	5	3	220	1.28	3	2	ND	2	106	1	2	2	35	.67	.06	3	6	.34	67	.06	11	.94	.02	.08	2
13+00S 7+00E	1	6	8	35	.1	7	4	273	1.48	3	2	ND	2	62	1	2	2	49	.45	.05	5	15	.43	68	.13	6	1.05	.01	.09	2
13+00S 7+50E	1	7	6	40	.2	8	5	272	2.09	2	2	ND	2	51	1	2	2	57	.32	.09	5	17	.48	74	.08	11	1.44	.02	.05	2
13+00S 0+50W	1	23	9	60	.3	20	9	379	2.78	5	2	ND	2	42	1	2	2	79	.49	.10	6	38	1.09	129	.15	8	1.92	.01	.34	2
13+00S 2+00W	1	12	7	36	.3	10	7	286	2.49	2	2	ND	2	37	1	2	2	66	.39	.09	6	23	.56	83	.13	12	1.60	.01	.07	2
13+00S 2+50W	1	11	9	45	.2	10	10	1234	2.57	5	2	ND	2	72	1	2	3	57	.61	.12	7	18	.60	96	.09	14	1.51	.02	.13	2
13+00S 3+50W	1	10	6	44	.3	9	6	332	1.90	2	2	ND	2	76	1	2	2	54	.65	.10	6	17	.57	98	.09	11	1.50	.02	.12	2
13+00S 5+00W	1	11	6	51	.4	9	6	360	2.24	2	2	ND	2	77	1	2	2	52	.56	.12	6	13	.65	97	.09	15	1.49	.02	.18	2
13+00S 6+00W	1	10	5	46	.2	8	6	384	2.57	2	4	ND	2	99	1	2	2	69	.79	.14	7	20	.52	83	.07	14	1.18	.02	.15	2
BL 14+00S	1	6	8	53	.4	8	5	337	2.78	4	2	ND	2	49	1	2	3	76	.35	.03	5	17	.84	71	.21	11	1.68	.01	.13	2
14+00S 0+50E	1	11	10	15	.4	3	1	87	.92	2	2	ND	2	54	1	2	2	30	.42	.03	11	9	.13	103	.10	6	.88	.01	.06	2
14+00S 1+00E	1	30	11	75	1.1	17	11	1637	3.61	2	7	ND	2	98	1	2	2	88	.93	.14	23	31	.79	233	.05	11	2.99	.02	.11	2
STD	27	181	44	99	2.9	666	15	660	3.81	15	3	ND	2	29	1	9	2	57	1.78	.10	6	98	.67	33	.05	34	1.10	.04	.25	2
14+00S 1+50E	1	5	7	50	.2	9	5	441	3.03	5	5	ND	2	46	1	2	2	88	.24	.09	4	18	.58	100	.15	10	1.32	.01	.07	2
14+00S 2+50E	1	22	6	80	.6	15	9	807	3.06	2	3	ND	2	90	1	2	2	90	.80	.13	8	27	.81	169	.08	12	2.43	.02	.14	2
14+00S 3+00E	1	10	6	58	.2	7	5	267	1.75	3	2	ND	2	80	1	2	3	52	.41	.04	3	16	.65	63	.16	11	1.16	.01	.11	2
14+00S 3+50E	1	7	11	44	.2	7	3	274	2.92	2	7	ND	2	29	1	3	2	65	.16	.07	10	20	.23	74	.17	8	1.41	.01	.05	2
14+00S 4+00E	1	3	7	13	.3	1	1	71	.73	2	2	ND	2	68	1	2	2	28	.23	.02	6	4	.07	74	.07	9	.80	.01	.04	2
14+00S 6+00E	1	10	4	64	.4	9	7	427	2.48	9	2	ND	2	81	1	2	2	69	.66	.08	6	17	.85	101	.15	12	1.84	.02	.12	2
14+00S 5+50E	1	13	7	60	.3	11	8	569	2.65	2	2	ND	2	97	1	2	2	80	.83	.14	7	24	.79	133	.08	11	2.27	.02	.09	2
14+00S 6+00E	1	5	4	52	.2	5	5	304	1.81	2	2	ND	2	59	1	2	2	51	.38	.09	4	9	.61	58	.10	13	1.51	.01	.06	2
14+00S 6+50E	1	9	5	63	.3	10	7	486	2.47	4	2	ND	2	61	1	3	2	68	.45	.08	7	15	.87	111	.13	13	1.90	.01	.16	2
14+00S 0+50W	1	9	7	57	.4	9	6	394	2.61	5	2	ND	2	65	1	2	2	66	.75	.08	7	20	.95	159	.16	12	1.67	.02	.39	2
14+00S 1+00W	1	11	9	46	.2	11	9	380	3.20	3	2	ND	2	62	1	2	2	96	.67	.13	5	30	.66	97	.09	14	1.55	.01	.14	2
14+00S 1+50W	1	12	5	53	.3	9	7	431	2.17	2	2	ND	2	82	1	2	2	55	.71	.12	7	17	.63	109	.09	13	1.53	.02	.14	2
14+00S 2+00W	1	10	8	52	.3	13	9	615	3.61	2	2	ND	2	70	1	2	2	69	.63	.09	6	24	.76	98	.12	14	1.85	.01	.13	2
14+00S 2+50W	1	8	14	53	.3	14	8	413	4.12	7	4	ND	2	43	1	2	2	119	.31	.07	5	31	1.05	76	.21	13	2.66	.02	.18	2
14+00S 3+50W	1	10	5	47	.3	9	6	379	2.80	3	4	ND	2	72	1	2	2	82	.59	.13	7	23	.52	87	.09	15	1.42	.02	.09	2
14+00S 4+00W	1	11	5	42	.3	9	6	338	2.02	2	2	ND	2	67	1	2	2	57	.48	.09	6	17	.51	91	.09	12	1.46	.02	.09	2
14+00S 4+50W	1	12	7	44	.3	10	7	403	2.85	2	2	ND	2	81	1	2	2	80	.72	.15	7	25	.54	72	.09	10	1.41	.02	.11	2
14+00S 5+00W	1	12	6	47	.2	9	10	606	1.99	4	2	ND	2	80	1	2	2	54	.61	.13	7	18	.57	95	.09	11	1.38	.02	.14	2
BL 15+00S	1	8	6	49	.2	9	5	258	2.83	6	3	ND	2	37	1	2	3	84	.23	.12	6	26	.44	70	.19	8	1.64	.01	.04	2
STD A-1	1	30	39	182	.3	35	12	1018	2.77	9	2	ND	2	36	1	2	2	58	.60	.11	8	74	.72	278	.09	7	2.07	.02	.21	2

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM JOB# 83-369 FILE # 83-2423

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe I	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca I	P I	La ppm	Cr ppm	Hg I	Ba ppm	Ti I	B ppm	Al I	Na I	K I	M ppm
15+00S 0+50E	1	8	5	49	.3	7	5	281	3.41	5	2	ND	2	57	1	4	2	89	.25	.11	4	17	.51	58	.18	3	1.79	.01	.05	2
15+00S 2+00E	1	6	7	34	.1	5	4	217	2.56	2	3	ND	2	42	1	3	2	89	.22	.05	5	20	.30	69	.17	3	1.05	.01	.05	2
15+00S 2+50E	1	6	9	27	.1	5	3	169	2.38	2	2	ND	2	48	1	2	2	69	.21	.06	6	15	.18	49	.15	3	.89	.01	.05	2
15+00S 3+00E	1	4	5	31	.2	6	3	208	1.90	5	2	ND	2	45	1	2	2	48	.32	.13	5	16	.27	49	.07	2	1.29	.01	.04	2
15+00S 3+50E	1	27	7	89	.1	15	10	726	2.96	2	2	ND	2	97	1	2	2	80	.67	.10	9	29	.78	206	.09	3	2.68	.01	.13	2
15+00S 4+00E	1	3	7	11	.2	1	1	61	.77	2	2	ND	2	42	1	2	3	38	.21	.02	3	7	.04	39	.14	2	.47	.01	.02	2
15+00S 4+50E	1	16	4	46	.2	10	6	420	2.18	4	3	ND	2	100	1	2	2	62	.84	.12	7	21	.55	114	.07	3	1.76	.01	.11	2
15+00S 5+00E	1	11	8	61	.3	11	7	514	4.61	5	2	ND	2	47	1	3	2	129	.26	.07	7	28	.58	76	.21	3	2.07	.01	.08	2
15+00S 5+50E	1	15	8	69	.3	13	8	477	2.76	5	2	ND	2	71	1	3	2	68	.44	.10	7	26	.89	120	.14	3	2.24	.01	.16	2
15+00S 0+50W	1	9	4	43	.1	10	6	247	2.98	2	9	ND	2	31	1	2	3	72	.23	.05	4	23	.54	63	.14	2	1.85	.01	.05	2
15+00S 1+50W	1	13	7	50	.1	10	6	353	1.84	6	4	ND	2	80	1	3	2	63	.60	.09	7	21	.61	100	.10	2	1.74	.01	.11	2
15+00S 2+00W	1	12	9	44	.3	12	7	290	2.88	2	2	ND	2	40	1	2	2	70	.30	.07	7	28	.56	75	.15	3	2.20	.01	.07	2
15+00S 2+50W	1	10	2	46	.3	10	5	333	2.46	2	2	ND	2	73	1	2	2	65	.42	.10	6	18	.57	81	.12	3	1.91	.01	.07	2
15+00S 3+00W	1	10	8	45	.3	12	6	285	3.15	6	2	ND	2	43	1	2	2	80	.28	.05	5	26	.68	61	.16	4	1.82	.01	.08	2
15+00S 3+50W	1	8	7	57	.1	7	6	434	2.68	2	2	ND	2	89	1	2	2	73	.51	.07	4	16	.59	82	.11	3	1.47	.01	.24	2
15+00S 3+90W	1	7	12	38	.2	11	6	311	2.70	4	6	ND	2	60	1	3	2	89	.49	.05	7	23	.72	75	.22	3	1.73	.01	.11	2
BL 16+00S	1	3	6	11	.1	2	1	95	.90	4	2	ND	2	53	1	2	2	30	.24	.01	5	8	.10	53	.11	2	.56	.01	.04	2
16+00S 1+00E	1	9	10	50	.2	7	4	302	2.11	6	3	ND	2	62	1	2	2	65	.42	.04	10	21	.46	90	.20	2	1.27	.03	.13	2
16+00S 1+50E	1	13	8	45	.2	9	5	272	2.53	7	4	ND	2	42	1	4	2	71	.24	.04	9	28	.43	78	.14	3	1.76	.02	.06	2
16+00S 2+00E	1	5	5	40	.1	3	3	211	1.47	3	2	ND	2	65	1	2	2	41	.24	.03	3	7	.39	54	.14	2	.95	.01	.12	2
STD	25	183	45	100	2.8	674	15	660	3.95	16	2	ND	3	29	1	11	2	57	1.79	.11	6	109	.66	30	.05	30	1.14	.04	.26	2
16+00S 2+50E	1	3	6	19	.3	3	2	129	1.27	2	2	ND	2	52	1	2	2	38	.22	.02	4	6	.13	37	.12	2	.58	.01	.05	2
16+00S 3+00E	1	6	7	41	.2	5	4	278	2.50	3	3	ND	2	64	1	2	2	72	.25	.06	5	12	.33	60	.17	2	1.05	.01	.05	2
16+00S 3+50E	1	7	6	50	.2	7	5	314	2.65	2	2	ND	2	52	1	2	3	70	.40	.10	5	16	.63	55	.16	2	1.75	.01	.05	2
16+00S 0+50W	1	7	7	39	.2	7	4	258	3.98	4	3	ND	2	49	1	2	2	98	.21	.06	5	18	.37	50	.17	3	1.93	.01	.05	2
16+00S 1+00W	1	6	7	61	.1	8	6	415	3.78	3	2	ND	2	57	1	2	2	101	.23	.10	5	17	.63	47	.21	4	1.88	.01	.06	2
16+00S 1+50W	1	13	9	48	.1	10	7	419	2.23	3	2	ND	2	78	1	2	2	57	.53	.12	7	20	.59	79	.10	2	1.59	.01	.12	2
16+00S 2+00W	1	13	6	55	.1	11	6	394	2.59	6	2	ND	2	90	1	2	2	70	.41	.05	6	22	.60	118	.13	3	2.15	.02	.08	2
16+00S 2+50W	1	12	4	49	.2	10	6	355	2.26	2	2	ND	2	89	1	2	2	60	.49	.06	8	19	.61	108	.11	2	1.98	.01	.08	2
BL 17+00S	1	10	6	39	.1	8	4	316	1.70	4	2	ND	2	82	1	2	2	47	.59	.10	7	19	.51	86	.09	2	1.33	.01	.07	2
17+00S 0+50E	1	8	14	41	.1	7	3	229	2.89	9	4	ND	2	61	1	2	2	94	.25	.06	7	24	.24	91	.21	3	1.28	.01	.06	2
17+00S 1+00E	2	17	9	90	.2	14	9	908	3.83	6	5	ND	2	82	1	2	2	108	.58	.07	9	34	.75	151	.14	3	2.29	.01	.09	2
17+00S 1+50E	1	6	9	41	.1	7	4	233	2.19	2	2	ND	2	55	1	2	2	71	.25	.06	5	15	.42	56	.20	3	1.39	.01	.05	2
17+00S 2+50E	1	31	11	61	.7	14	9	796	2.36	2	2	ND	2	186	1	2	2	55	1.83	.16	27	22	.62	239	.03	4	2.44	.02	.11	2
17+00S 3+00E	1	16	6	82	.1	11	7	462	2.60	2	2	ND	2	94	1	2	2	74	.67	.05	6	19	1.03	114	.18	5	2.07	.01	.16	2
17+00S 3+50E	1	10	3	51	.1	10	7	396	2.55	6	3	ND	2	77	1	2	2	61	.67	.10	7	19	.64	92	.13	2	1.49	.01	.14	2
17+00S 0+50W	1	4	8	33	.1	5	4	239	2.18	4	2	ND	2	51	1	2	2	65	.19	.06	4	10	.35	42	.16	2	1.33	.01	.04	2
17+00S 1+00W	1	4	8	19	.2	4	3	157	2.47	3	3	ND	2	37	1	2	2	104	.18	.03	4	18	.20	36	.18	2	1.01	.01	.04	2
17+00S 1+50W	1	14	9	49	.1	13	7	317	3.91	8	2	ND	2	41	1	3	2	108	.29	.06	7	32	.59	102	.18	3	2.13	.01	.05	2
BL 18+00S	1	6	6	25	.2	5	4	187	2.08	4	4	ND	2	61	1	2	2	71	.21	.03	5	12	.24	61	.17	3	.86	.01	.06	2
STD A-1	1	30	38	183	.3	34	12	1019	2.82	12	2	ND	2	36	1	2	2	57	.60	.11	8	72	.72	278	.09	6	2.07	.02	.21	2

TENAJON SILVER PROJECT # SOLUTION FROM VANGEOCHEM JOB# 83-369 FILE # 83-2423

PAGE # 10

SAMPLE #	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm
18+005 0+50E	1	10	10	97	.2	13	7	505	3.64	3	2	ND	2	50	1	5	2	82	.34	.07	8	25	.87	95	.17	3	2.11	.01	.08	2
18+005 1+00E	2	34	13	144	.1	18	12	1280	4.51	3	5	ND	2	80	1	2	2	99	.58	.07	15	37	.75	237	.11	4	3.07	.01	.11	2
18+005 1+50E	1	6	9	39	.1	8	2	168	1.51	2	2	ND	2	59	1	2	2	51	.27	.02	6	17	.26	82	.13	2	1.20	.01	.05	2
18+005 2+00E	1	8	6	36	.1	8	4	197	2.70	6	2	ND	2	48	1	2	2	99	.30	.03	4	32	.30	55	.18	2	.95	.01	.07	2
18+005 2+50E	1	29	7	59	.6	13	7	583	2.11	3	2	ND	2	210	1	2	2	46	1.99	.12	24	19	.64	230	.04	5	2.11	.01	.14	2
18+005 3+00E	1	6	10	45	.2	6	3	242	2.04	7	3	ND	2	57	1	5	2	62	.24	.05	9	13	.48	58	.26	2	1.35	.01	.07	2
18+005 0+50N	1	8	5	53	.1	8	6	517	2.12	3	2	ND	2	80	1	2	2	60	.53	.09	5	17	.58	67	.10	2	1.42	.02	.06	2
STD A-1	1	30	39	184	.3	36	12	1026	2.82	11	2	ND	2	37	1	2	2	58	.60	.11	7	75	.72	285	.09	6	2.07	.02	.21	2

APPENDIX III

EXPENDITURE

EXPENDITURE

Central Mountain Air	675.40
Scott Angus - groceries and supplies	1,096.74
Scott Angus - wages	1,207.09
Rex Brown - wages	767.83
Phoenix Geophysics	420.00
Central Mountain Air	675.40
Mern Engineering - Truck Rental	325.00
Vancouver Geochem	4,009.60
	<hr/>
	\$9,377.06
	=====

**CENTRAL MOUNTAIN
AIR SERVICES LTD.**

Box 998 Phone: 847-4780 or 847-4548
Smithers, B.C. V0J 2N0

INVOICE
N^o 1331

DATE: SEPT 12 1983 AIC: BEAVER C-FGON

NAME: TENAJON SILVER

ADDRESS: 1450 - 625 HOWE ST
VANCOUVER

FROM	MILES	HOURS	CARGO	PASSENGER/REMARKS
<u>McCLURE</u>				
TO <u>FREDRICKSON</u>	<u>155</u>			<u>* SCOTT ANGUS</u>
<u>McCLURE</u>	<u>155</u>			<u>* ?</u>

SPECIAL INSTRUCTIONS	@	PER HOUR		
<u>2 pass in</u>	<u>310</u>	<u>@ 21.70</u>	PER MILE	<u>527 00</u>
WAIT TIME	@	PER HOUR		
FUEL <u>56</u>	<u>@ 2.65</u>	PER LITRE		<u>148 40</u>
OTHER				
2% per month (24% per annum) charged on accounts over 30 days.				<u>675 40</u>

PILOT'S SIGNATURE: [Signature] P/O, CONTRACT: [Signature] CHARTERER'S AUTHORIZATION: [Signature]

White - Office Copy/Original
Blue - Customer Copy
Yellow - Office Copy/Records
Green - Base Copy (Not Perforated - Stays in Book)

SEE MOORE PRINT SMITHERS

Thank You  PAY LAST AMOUNT IN THIS COLUMN

MIRV ENGINEERING CORP.
 1450 - 625 Howe Street,
 Vancouver, B.C. V6C 2T6

Date

EXPENSE ACCOUNT

In account with SCOTT E Angus
 (Name and Address)

Expenses incurred SEPT 9 TO SEPT 24 1983 (MAC Group)
 (Description and date)

STATEMENT OF ACCOUNT

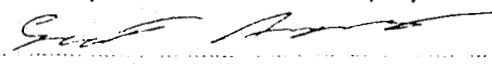
Cash on hand last account \$
 Advances received \$
 Expenses as per this account
 Cash on hand \$

Note: If space provided below is insufficient, please use supplementary page and bring totals forward.

Date	Details (attach receipts)	Trans- portation	Hotel & Meals	Supplies	Other	Acct./ Job No.
	Totals from supplementary page(s)	162 00	381 47	506 27		
9.24.	meals		8 45			
	995	38 55				
	NRM 255.78 ✓ KASHO					
	TJS 383.73 ✓ HORN.					
	CMA 180.00 ✓ SUMMIT					
	TJS 103.57 ✓ TIDE		3095.16			
	NHG 103.57 ✓ TIDE		1500.00	ADVANCE		
	NRM 23.01 ✓ TIDE					
	TJS 474.38 ✓ HORN.		1395.16		CK 590.	
	TJS 213.47 ✓ TIDE					
	NHG 213.47 ✓ TIDE					
	NRM 47.44 ✓ TIDE					
	TJS 548.37 ✓ MAC					
	SNU 548.37 ✓ MAC	1096.74				
Charge acct. No.	<u>\$ 3095.16</u>	Column totals	200 55	389 92	506 27	

MAC - TJS - 548.37
 SNU - 548.37
1096.74

Total expenses 1096.74

This is my account for expenses incurred on Company business

 Employee's Signature

Approved

590

MERV ENGINEERING CORP.
1450 - 625 HOWE STREET,
VANCOUVER, B.C. V6C 2T6

Invoice # 635

TELEPHONE: (604) 689-8325

Oct. 5, 1983

Tenajon Silver Corp.,
1450 625 Howe St.,
Vancouver, B.C.

To invoice you per disbursement of salaries:

Scott Angus:	Sept. 16th to 30th		
15 days @	\$ 95.00 per day		
	1,425.00		
CPP	24.28		
UIC	19.19		
WCB	49.00		
Hol. Pay	<u>57.00</u>	1,574.47	
Plus 15%		<u>236.17</u>	\$ <u>1,810.64</u>

Respectfully submitted,

J. W. MacLeod, P. Eng.

4,1207.09

SEPT 16-25 MAC $10/15 \times 1810.64 = 1207.09$ - TJS 603.55
SEPT 26-30 KASHO $5/15 \times 1810.64 = 603.55$ SNV 603.54
NRM 603.55

MERV ENGINEERING CORP.
1450 - 625 HOWE STREET,
VANCOUVER, B.C. V6C 2T6

TELEPHONE: (604) 689-8325

Oct. 5, 1983

Invoice # 636

Tenajon Silver Corp.,
1450 625 Howe St.,
Vancouver, B. C.

To invoice you per: Disbursement of salaries.

Rex Brown:	Sept. 16th to 30th.		
	900.00 15 days @ \$ 60.00 per day	
CPP	14.83		
UIC	19.19		
WCB	31.50		
Hol. Pay	<u>36.00</u>	1,001.52	
Plus 15%		<u>150.23</u>	\$ <u>1,151.75</u>

Respectfully submitted,

J.W. MacLeod, P. Eng.

92
Sept 16 - 25 - Mac. — $\frac{10}{15} \times 1,151.75 = 767.83$ — TJS 383.92
SNV 383.91
Sept 26 - 30 - Kasuo. — $\frac{5}{15} \times 1,151.75 = 383.92$ — NRM 383.92
1151.75



PHOENIX Geophysics Limited

200 YORKLAND BLVD., WILLOWDALE, ONTARIO, CANADA M2J 1R5

TELEPHONE (416) 493-6350
Telex: 06-986856
Cable: PHEXCO TORONTO

INVOICE

INVOICE No. 3815
DATE: September 21, 1983.

Tenajon Silver Corp.,
1480 - 625 Howe Street
Vancouver, B.C.
V6C 2T6

RENTAL

1 VLF-2 Serial No. L1048

RENTAL PERIOD:
September 6 - October 5, 1983
30 days @ \$21.00/day

\$630.00

1/3 NORANDA - 210.00 - K. L. H. S.
1/3 TENAJON - 210.00
1/3 SISEVA - 210.00 } *MAC GR.*

*CK \$79
597*

PHOENIX GEOPHYSICS LIMITED



VANGEOCHEM LAB LTD. (604) 986-5211
1521 PEMBERTON AVE., NORTH VANCOUVER, B. C.
CANADA V7P 2S3

IN ACCOUNT WITH:
Tenajon Silver Corp.
1450 - 825 Howe St.
Vancouver, B.C.
V6C 2T6

INVOICE: 7545
DATE: October 11, 1983
TERMS: NET 21 DAYS

FOR REPORT 83-90-030

PROJECT: MAC

ORDER NO. 83-369

358 Soil & Silt samples for preparation	@ \$0.70	\$ 250.60
358 Trace analyses for Au	@ \$4.50	\$1,611.00
358 I C P analyses	@ \$6.00	\$2,148.00
Total this invoice		<u>\$4,009.60</u>

CK 612

PLEASE PAY BY INVOICE
NO STATEMENT WILL BE ISSUED

APPENDIX IV

ENGINEERS CERTIFICATE

CERTIFICATE

I, James W. MacLeod, of 1220 Arbutus Street, in the city of Vancouver, in the Province of British Columbia,

DO HEREBY CERTIFY:

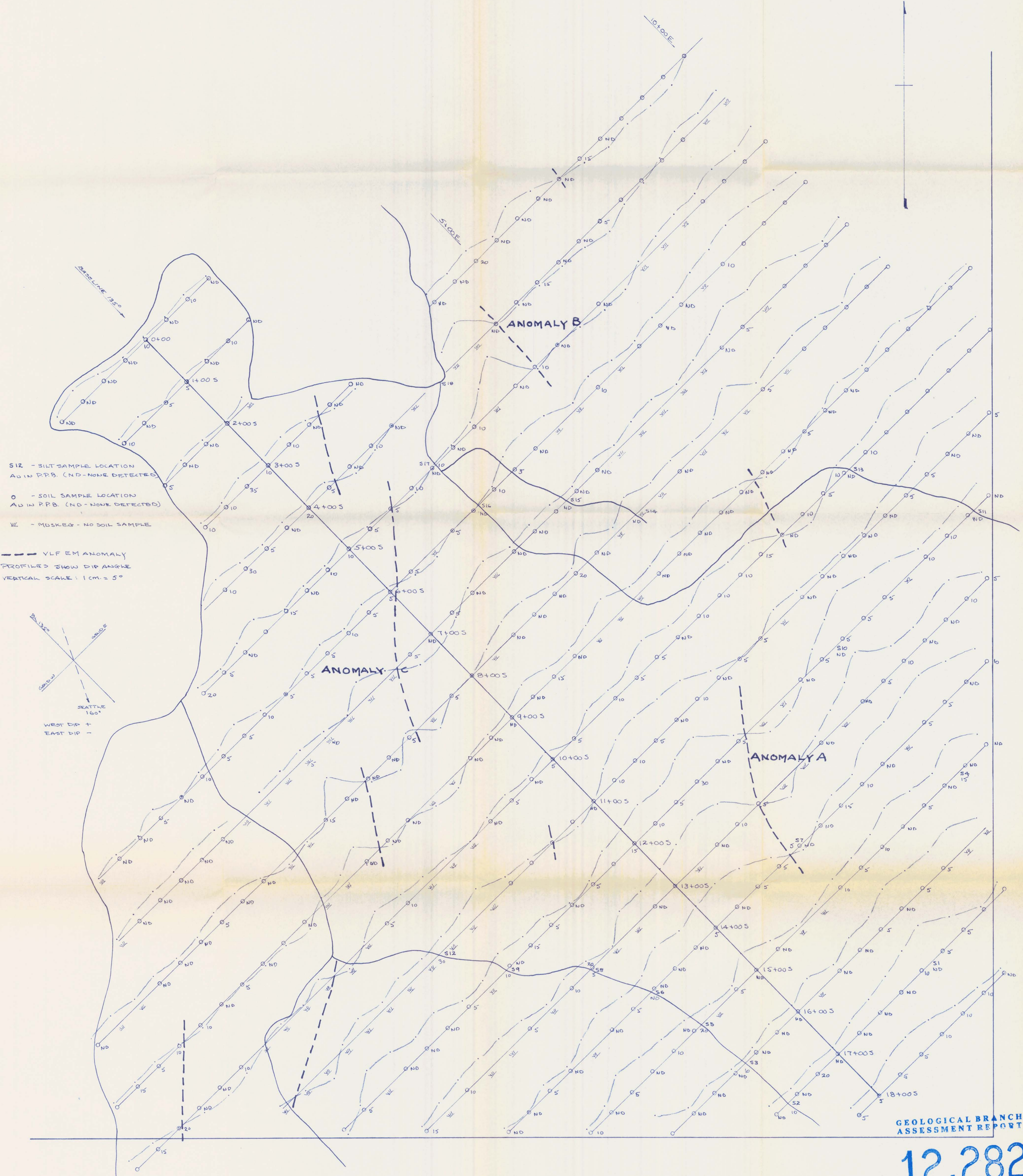
1. That I am a Consulting Engineer, with a business address at #1450-625 Howe Street in the City of Vancouver, in the Province of B.C.
2. That I am a graduate of the University of Alberta with the degree of B.Sc. in Mining Engineering.
3. That I have actively practiced my profession in mineral exploration since graduation in 1946.
4. That I am a registered Professional Engineer in the Province of British Columbia.
5. That I directed the program of geochemical and geophysical work carried out on the Mac Claim during the 1983 field season.



J.W. Macleod, B.Sc.,

P.Eng.

Dated at the City of Vancouver,
Province of British Columbia,
this 14th day of February, 1984.

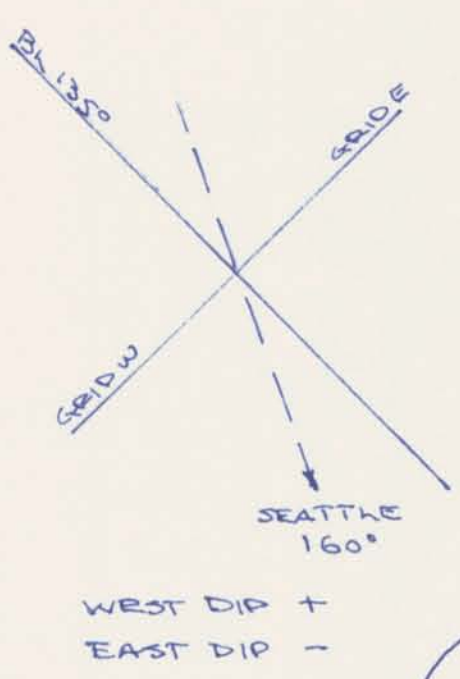


S12 - SILT SAMPLE LOCATION
 AS IN P.P.B. (ND - NONE DETECTED)

○ - SOIL SAMPLE LOCATION
 AS IN P.P.B. (ND - NONE DETECTED)

⊥ - MUSKEG - NO SOIL SAMPLE

--- VLF EM ANOMALY
 PROFILED SHOW DIP ANGLE
 VERTICAL SCALE: 1 CM. = 5°



GEOLOGICAL BRANCH
 ASSESSMENT REPORT

12,282

TENISON SILVER CORP	
SCALE 1:2500	DRAWN BY: J.W.H.
DATE FEB 78A	NTS: 94 D 15-16
VLF EM SURVEY	
MAC CLAIM - FREDRICKSON LAKE	

CROSS LINES FOR THIS SURVEY TOTALS 22.15 KM.

TO ACCOMPANY REPORT ON THE MAC CLAIM BY: J.W.H. FEB 12, 1984