

84-#484 - #12422
7/85

Geochemical Assessment Report

Specific Claims Involved:

St Teresa #1	13414
St Teresa #6	15531
MAC	1586 (10)
MC #1	1587 (10)
MC #2	1588 (10)
MC #3	1589 (10)

Mining Division: Clinton

Specific NTS Location: 92N/10/E

Latitude and Longitude: 51 44'N
124 38'W

Owner of Claims: Imperial Metals Corporation
and Don Rose

Author or Report: J.W. Morton

Date Submitted: July 12, 1984

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

12,422

TABLE OF CONTENTS

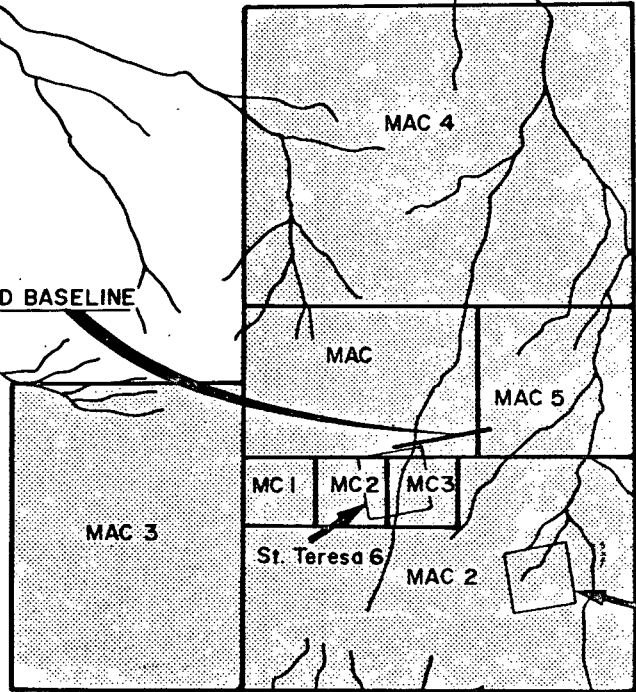
	<u>PAGE</u>
Claim Map	1
Introduction	2
Detailed Technical Data and Interpretations	3
Costs	4
Author Qualifications	5
MAP Soil Geochemistry Lead (Computer Plot)	6
MAP Soil Geochemistry Silver (Computer Plot)	7
MAP Soil Geochemistry Arsenic (Computer Plot)	8
MAP Soil Geochemistry Gold (Computer Plot)	9
MAP Soil Geochemistry Lead-Silver (Drafted Plot)	10
MAP Soil Geochemistry Arsenic-Gold (Drafted Plot)	11
Geochemical Certificates with Procedures	Appendix
Statistics	Appendix

124° 37'



51° 45'

GRID BASELINE



Valleau
Creek

IMPERIAL METALS CORPORATION	
MAC	
FIGURE 1	N.T.S. 92N/10E,15E
CLAIM MAP	
SCALE: 1:50000	GEOLOGIST: W. MORTON
DATE: JULY 1984	DRAWN BY: R. M.

INTRODUCTION

General Geographic and Physiographic Position

The MAC claim group is located within the Chilcotin region of British Columbia approximately 180 air miles west of the city of William's Lake. The claims are accessible via highway 20 from William's Lake to Tatla Lake village and then the Westbranch road to Bluff Lake. From Bluff Lake a truck road has been constructed to the center of the claim group. The claim group occurs on the edge of a mountain with elevations varying between 3500 feet and 7100 feet. Vegetation consists of open pine forest at lower elevations and alpine mosses and grasses at higher elevations.

Property Definition

The MAC claims cover a volcanic sedimentary sequence of probable Cretaceous age that has been intruded by a quartz diorite intrusive of probable late Cretaceous to early Tertiary age. An extensive area of volcanics display argillic and limonitic alteration. A strong vuggy quartz vein occurs within the alteration zone and has been exposed by hand trenching. The vein is up to 1.5 meters wide in surface exposure and is banded. A central core of white quartz (0.3m) contains 1 to 2% galena and contains 7 to 11 oz/ton silver and 0.060 to 0.120 oz/ton gold.

Summary of Work Completed

A detailed grid was established along the projected strike of the vein (078). The grid consists of a 650 meter baseline with crosslines running at 25 meter spacings in the central region of the grid and at 50 meter spacings on the ends. Sample spacing along the crosslines is 5m in the central region of the grid and 10m further out. A total of 250 soil samples were obtained and analysed by inductively coupled argon plasma analysis in the laboratory facilities of Acme Analytical Labs in Vancouver (gold determinations by atomic absorption methods).

Samples were collected with a sampling mattock and where possible were obtained from the Bm horizon.

Work completed occurs on the MC#2, MAC and St. Teresa #6 claim.

Detailed Technical Data and Interpretations

A lead-gold (silver, zinc, arsenic, molybdenum) anomaly corresponds to the known occurrence of the mineralized quartz vein. Similar anomalies occur along the eastward projected strike of the vein (078°). Westward from 0+00E, 0+00N the vein appears to be offset approximately 50 meters to the south.

Recommendations

A ^{dr}trenching program should be initiated to expose the quartz vein where it can be inferred from geochemical response. Initial trenching should be completed over the following intervals:

2+00E	0+10S to 2+00E	0+25S
2+50E	0+05N to 2+50E	0+25N
0+50E	0+05S to 0+50E	0+20N
0+25E	0+00N to 0+25E	0+10N
1+00W	0+40S to 1+00W	0+60S

Costs.

Grid Establishment and Geochemical Survey

June 12 , 15, 16 / 1984	Morton	3 days @ \$200/day	\$ 600.00
June 12, 14, 15, 16, 17, 20	MacKenzie	9 days @ \$100 day	900.00
June 21, 22, 23 / 1984	Wood	9 days @ \$75 day	675.00
Room & Board	21 man days @ \$50 day		1,050.00
Vehicle Costs	9 days @ \$50/day		450.00
Assay Costs	250 samples 30 element ICP analysis plus gold by A.A. @ \$11.85.		2,962.00
Report Prep and Drafting			<u>500.00</u>
		TOTAL	<u><u>\$ 7,137.00</u></u>

AUTHOR'S QUALIFICATIONS

I, JAMES W. MORTON, CERTIFY THE FOLLOWING:

I graduated from Carleton University in 1971 with a Bachelor of Science in Geology.

I graduated from the University of British Columbia in 1976 with a Master of Science in Soil Science.

I have worked for various mining and exploration companies since 1968.

I am presently a permanent staff geologist with Imperial Metals Corporation of Vancouver, B.C.

I supervised the work described in this report.



J.W. Morton,
Geologist

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-3 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SN, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: SOIL - PULVERIZING AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JUNE 27 1984 DATE REPORT MAILED: *July 3/84* ASSAYER: *A. J. P.* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT # MAE FILE # 84-1281

PAGE 1

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	ME	BA	TI	B	AL	NA	K	W	AU
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
1+50W 0+50N	1	12	8	27	.1	4	3	125	1.78	7	2	ND	2	11	1	2	2	50	.17	.04	2	8	.23	36	.04	3	1.09	.01	.02	2	5
1+50W 0+40N	2	14	8	44	.1	5	5	153	2.89	11	4	ND	2	8	1	2	2	56	.13	.04	2	11	.31	23	.03	3	1.70	.01	.03	2	5
1+50W 0+30N	2	19	8	43	.1	7	7	211	2.97	13	2	ND	2	9	1	2	2	69	.12	.04	2	14	.44	32	.04	3	1.63	.01	.03	2	10
1+50W 0+20N	2	41	8	53	.2	10	12	334	3.65	24	3	ND	2	8	1	2	2	85	.13	.05	2	20	.71	41	.04	3	2.52	.01	.03	2	5
1+50W 0+10N	2	26	8	50	.1	8	8	247	3.26	15	2	ND	2	7	1	2	2	74	.11	.03	2	18	.58	30	.04	5	2.07	.01	.02	2	5
1+50W 0+00S	2	11	6	22	.1	4	4	120	1.90	2	2	ND	2	10	1	2	2	62	.16	.03	2	9	.26	26	.05	2	1.20	.01	.02	2	5
1+50W 0+10S	2	17	6	37	.1	7	6	194	3.05	8	2	ND	2	7	1	2	3	75	.10	.04	2	15	.44	24	.05	3	1.90	.01	.03	2	5
1+50W 0+20S	2	16	6	32	.1	7	7	167	2.74	8	2	ND	2	6	1	2	2	73	.09	.02	2	14	.46	26	.05	4	1.78	.01	.02	2	10
1+50W 0+30S	2	24	7	47	.1	9	10	216	3.47	10	2	ND	2	6	1	2	2	78	.09	.04	2	20	.56	27	.06	4	2.48	.01	.02	2	5
1+50W 0+40S	2	29	8	41	.2	10	9	235	3.10	9	2	ND	2	8	1	2	3	70	.11	.03	2	18	.54	33	.05	4	2.13	.01	.02	2	5
1+50W 0+50S	3	21	157	823	.3	7	7	319	3.25	20	2	ND	2	8	2	2	2	64	.15	.04	3	14	.39	33	.02	4	1.93	.01	.04	2	25
1+00W 0+50N	2	32	40	127	.6	12	12	308	3.80	15	3	ND	2	9	2	2	2	74	.14	.03	2	21	.81	32	.04	5	2.49	.01	.03	2	5
1+00W 0+40N	3	17	13	65	.3	6	6	173	2.97	14	2	ND	2	10	1	2	2	76	.16	.03	2	12	.40	23	.02	5	1.80	.01	.03	2	5
1+00W 0+30N	3	22	19	43	.1	6	6	182	2.64	10	2	ND	2	8	1	2	2	65	.17	.03	2	11	.57	29	.02	4	1.59	.01	.04	2	5
1+00W 0+20N	3	13	13	29	.2	3	4	90	2.54	9	2	ND	2	8	1	2	2	70	.14	.02	2	10	.20	20	.02	3	1.66	.01	.03	2	5
1+00W 0+10N	2	14	12	25	.2	4	4	95	1.79	10	2	ND	2	9	1	2	2	58	.13	.02	2	8	.22	27	.05	3	1.21	.01	.03	2	5
1+00W 0+00S	2	18	12	34	.2	5	5	144	2.35	11	2	ND	2	6	1	2	2	64	.07	.02	2	11	.37	31	.04	4	1.47	.01	.03	2	5
1+00W 0+10S	2	20	5	37	.2	8	7	201	2.97	10	2	ND	2	6	1	2	2	75	.07	.03	2	17	.51	29	.05	5	1.87	.01	.02	2	5
1+00W 0+20S	2	28	17	80	.3	10	10	282	2.99	18	2	ND	2	10	1	2	2	57	.17	.03	2	18	.67	28	.03	3	2.24	.01	.03	2	5
1+00W 0+30S	3	35	85	94	.4	7	8	308	2.47	23	2	ND	2	18	1	2	2	46	.56	.06	2	13	.39	33	.01	5	1.75	.01	.03	2	5
1+00W 0+40S	1	23	7	32	.1	2	2	151	1.52	2	2	ND	2	9	1	2	8	29	.16	.07	2	3	.24	21	.01	2	1.09	.01	.01	2	5
1+00W 0+50S	5	92	78	121	1.0	7	21	1157	4.12	71	4	ND	2	23	2	2	2	57	.65	.04	2	7	.61	17	.01	5	2.33	.01	.05	2	55
0+50W 0+25N	2	47	9	61	.4	12	18	670	4.00	24	3	ND	2	20	2	3	2	77	.35	.04	2	24	1.04	33	.05	5	2.30	.01	.03	2	5
0+50W 0+20N	3	40	31	74	.3	12	15	497	3.94	34	2	ND	2	11	2	2	2	73	.19	.04	2	20	.86	28	.03	6	2.58	.01	.03	2	5
0+50W 0+15N	2	41	27	69	.3	11	14	525	3.85	35	2	ND	2	11	2	2	2	70	.20	.04	2	19	.86	29	.03	6	2.26	.02	.04	2	5
0+50W 0+10N	3	49	30	101	.3	12	19	921	4.14	68	2	ND	2	15	2	3	2	64	.34	.04	2	16	.81	31	.02	5	2.26	.01	.04	2	5
0+50W 0+05N	3	50	24	78	.3	12	17	724	4.06	38	2	ND	2	15	2	3	2	74	.28	.04	2	20	.92	31	.04	25	2.58	.02	.04	2	5
0+50W 0+05S	1	38	12	58	.2	11	14	525	3.38	21	2	ND	2	10	1	2	2	67	.15	.04	2	20	.80	32	.05	5	2.33	.01	.02	2	5
0+50W 0+10S	1	38	12	55	.2	12	14	485	3.54	19	2	ND	2	10	1	2	2	71	.12	.04	2	20	.81	38	.05	4	2.71	.01	.02	2	5
0+50W 0+15S	2	39	13	54	.1	12	14	446	3.54	22	2	ND	2	12	1	3	2	72	.14	.03	2	20	.85	34	.05	5	2.66	.01	.02	2	5
0+50W 0+20S	2	26	17	49	.3	9	10	248	3.37	21	2	ND	2	6	1	2	2	72	.08	.03	2	16	.56	29	.04	5	2.23	.01	.03	2	5
0+50W 0+25S	2	28	15.	50	.1	9	9	302	3.39	19	2	ND	2	6	1	2	2	74	.11	.03	3	16	.64	30	.04	4	2.08	.01	.03	2	5
0+00E 0+50N	4	65	17	56	.4	9	16	584	6.02	39	2	ND	2	29	2	2	2	50	.32	.09	3	11	.52	52	.07	8	2.09	.02	.07	2	15
0+00E 0+40N	7	65	56	127	.6	11	23	971	5.29	52	2	ND	2	37	2	2	2	58	.33	.06	4	15	.83	53	.02	7	2.31	.01	.05	2	5
0+00E 0+30N	7	66	39	121	.4	10	21	902	5.20	44	2	ND	2	51	2	3	2	52	.42	.06	2	14	.85	47	.02	6	2.36	.02	.06	2	5
0+00E 0+20N	3	72	33	203	.5	10	23	1538	5.36	84	2	ND	2	25	3	3	2	50	.53	.06	2	11	.80	41	.01	5	2.41	.01	.06	2	10
0+00E 0+10N	3	62	70	121	1.1	11	18	1281	4.06	57	4	ND	2	20	3	2	2	50	.68	.04	2	14	.74	42	.01	6	2.58	.01	.04	2	10
STD A-1/AU 0.5	2	30	39	186	.3	36	13	1019	2.79	9	2	ND	2	37	2	2	2	56	.62	.11	7	64	.63	255	.10	7	2.04	.02	.19	2	485

IMPERIAL METALS PROJECT # MAR FILE # 84-1281

SAMPLE#	NO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
0+00E 0+00S	2	41	10	46	.4	9	15	534	3.50	70	5	ND	2	31	1	2	2	42	1.02	.02	2	9	.55	29	.02	3	2.51	.01	.03	2	10
0+00E 0+10S	2	42	30	59	.3	12	14	331	3.73	17	2	ND	2	12	1	2	2	73	.24	.02	2	22	.89	36	.04	5	2.34	.01	.03	2	5
0+00E 0+20S	2	49	17	62	.3	12	15	829	3.66	25	2	ND	2	18	1	2	2	64	.56	.02	3	16	.84	42	.03	4	2.54	.01	.03	2	5
0+00E 0+30S	2	53	17	65	.4	12	16	1122	3.79	27	3	ND	2	13	1	2	2	60	.57	.03	4	18	.86	40	.03	5	2.36	.01	.06	2	5
0+00E 0+40S	2	48	12	48	.3	9	11	558	3.02	21	2	ND	2	32	1	2	2	54	.93	.02	2	13	.61	97	.02	4	3.30	.01	.03	2	5
0+00E 0+50S	2	44	12	43	.3	8	10	836	2.63	27	2	ND	2	39	1	2	2	43	1.06	.03	3	11	.51	73	.02	4	2.88	.01	.04	2	5
0+25E 0+25N	2	41	25	95	1.2	15	15	447	4.00	25	6	ND	2	13	2	2	2	73	.23	.03	2	24	.96	41	.04	5	3.10	.01	.02	2	5
0+25E 0+20N	3	46	24	331	1.0	15	16	591	4.13	38	2	ND	2	16	3	2	2	72	.28	.03	2	22	.95	35	.04	5	2.93	.01	.04	2	5
0+25E 0+15N	3	57	47	182	1.0	11	16	994	4.64	30	3	ND	2	77	3	2	2	66	.36	.04	3	15	1.04	43	.01	6	2.17	.02	.04	2	5
0+25E 0+10N	4	69	425	782	9.0	11	15	1543	3.89	48	3	ND	2	14	6	7	2	54	.39	.04	4	14	.72	34	.01	6	2.18	.01	.04	2	45
0+25E 0+05N	4	62	30	123	.5	13	21	1009	5.32	94	6	ND	2	16	2	2	2	72	.31	.04	4	21	.97	32	.02	7	2.72	.01	.04	2	5
0+25E 0+00S	1	40	16	75	.2	13	16	587	3.68	20	2	ND	2	13	1	2	2	69	.23	.02	2	22	.95	30	.06	4	2.43	.01	.02	2	5
0+25E 0+05S	2	47	61	144	1.4	14	14	389	3.59	25	2	ND	2	11	1	2	3	65	.20	.03	2	21	.80	32	.04	6	2.63	.01	.03	2	5
0+25E 0+10S	2	26	19	75	.6	11	12	593	4.03	25	3	ND	2	11	2	2	2	82	.24	.04	2	19	.80	31	.03	6	2.29	.01	.03	2	5
0+25E 0+15S	2	39	19	109	.5	12	14	554	3.92	23	2	ND	2	10	2	2	2	73	.21	.04	2	19	.74	37	.02	6	2.52	.01	.03	2	5
0+25E 0+20S	3	22	19	68	.5	8	8	414	3.33	22	2	ND	2	11	1	2	2	69	.19	.03	2	13	.53	34	.02	7	1.98	.01	.03	2	5
0+25E 0+25S	3	48	32	134	.9	12	14	544	4.17	49	2	ND	2	9	2	2	2	63	.14	.04	3	17	.72	27	.02	8	2.59	.01	.03	2	5
0+50E 0+25N	2	30	53	113	.3	10	13	472	3.63	32	2	ND	2	14	2	2	2	57	.20	.03	2	15	.63	48	.01	7	2.07	.01	.04	2	5
0+50E 0+20N	2	24	36	123	.3	11	11	406	3.26	25	2	ND	2	15	2	2	2	61	.21	.02	2	15	.61	43	.01	6	2.10	.01	.03	2	5
0+50E 0+15N	3	36	622	399	8.5	9	14	1944	3.22	47	6	ND	2	20	4	4	2	49	.40	.04	2	11	.45	59	.01	7	1.95	.01	.05	2	5
0+50E 0+10N	3	20	196	406	1.2	8	11	478	3.33	45	2	ND	2	10	2	2	2	58	.19	.03	2	11	.45	43	.01	6	1.99	.01	.05	2	5
0+50E 0+05N	3	20	106	291	1.1	8	10	550	3.15	22	3	ND	2	12	2	2	2	66	.23	.03	2	11	.52	39	.01	6	2.13	.01	.04	2	5
0+50E 0+00S	3	89	910	1484	32.4	13	12	514	3.86	57	2	ND	2	8	4	17	2	58	.22	.03	2	19	.82	14	.03	7	2.44	.01	.02	2	135
0+50E 0+05S	2	60	62	159	2.1	15	15	444	4.07	35	2	ND	2	10	2	2	2	70	.16	.02	2	24	.94	33	.03	6	3.06	.01	.02	2	5
0+50E 0+10S	2	27	29	86	.9	10	13	708	3.71	27	4	ND	2	13	2	2	2	71	.21	.04	2	16	.61	44	.01	8	2.45	.01	.04	2	5
0+50E 0+15S	2	28	11	67	.3	11	13	740	3.57	24	2	ND	2	11	1	2	2	70	.18	.04	2	15	.65	47	.01	6	2.42	.01	.04	2	5
0+50E 0+20S	2	33	11	64	.2	11	12	426	3.73	30	2	ND	2	10	2	2	2	71	.22	.03	2	16	.68	39	.01	6	2.53	.01	.04	2	5
0+50E 0+25S	2	29	13	67	.3	11	14	777	3.61	23	4	ND	2	11	2	2	2	68	.17	.04	3	15	.64	43	.01	8	2.51	.01	.05	2	5
0+75E 0+25N	2	35	17	94	.4	14	15	312	3.99	30	3	ND	2	11	2	2	2	71	.12	.04	2	20	.73	37	.03	6	2.93	.01	.04	2	5
0+75E 0+20N	2	30	26	130	.3	12	13	347	3.63	29	2	ND	2	11	2	2	2	65	.13	.04	2	19	.71	35	.02	6	2.47	.01	.03	2	5
0+75E 0+15N	2	24	31	202	.8	11	11	278	3.62	30	2	ND	2	11	2	2	2	68	.15	.03	2	18	.56	36	.02	6	2.45	.01	.03	2	5
0+75E 0+10N	2	30	27	134	.4	16	12	298	3.78	32	2	ND	2	11	2	2	2	72	.14	.02	3	18	.70	37	.02	6	2.47	.01	.04	2	5
0+75E 0+05N	3	58	41	140	1.0	15	17	484	4.22	52	2	ND	2	9	2	2	2	69	.11	.02	3	24	.82	41	.02	7	2.83	.01	.03	2	5
0+75E 0+00S	2	43	34	149	1.1	14	15	349	4.04	41	2	ND	2	10	2	2	2	70	.14	.03	3	18	.76	38	.02	6	2.75	.01	.03	2	5
0+75E 0+05S	2	26	57	178	.9	10	13	483	3.74	28	2	ND	2	10	2	2	2	71	.18	.03	2	16	.56	37	.02	6	2.35	.01	.04	2	5
0+75E 0+10S	2	23	36	126	.7	11	13	487	3.66	26	2	ND	2	13	2	2	2	71	.23	.03	2	17	.61	35	.02	7	2.25	.01	.04	2	5
0+75E 0+15S	2	29	34	96	.7	10	13	583	3.72	26	2	ND	2	11	2	2	2	73	.28	.04	2	15	.64	43	.01	6	2.27	.01	.10	2	5
STD A-1/AU 0.5	2	30	40	188	.3	36	13	1039	2.82	9	2	ND	2	37	2	2	2	57	.63	.10	7	65	.64	258	.10	8	2.06	.02	.19	2	490

IMPERIAL METALS PROJECT # MAR FILE # 84-1281

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
0+75E 0+20S	2	49	18	83	.4	18	17	443	4.68	37	5	ND	2	15	2	2	3	93	.30	.04	2	27	.97	43	.04	5	3.33	.02	.06	2	5
0+75E 0+25S	2	24	19	75	.3	11	11	362	3.63	23	5	ND	2	17	1	2	2	82	.34	.04	2	19	.58	39	.03	3	2.79	.01	.06	2	5
1+00E 0+25N	2	31	14	76	.3	13	12	281	4.12	21	2	ND	2	13	2	2	3	90	.17	.03	2	24	.71	39	.06	6	3.08	.01	.03	2	5
1+00E 0+20N	2	38	17	80	.5	16	15	325	4.08	24	3	ND	2	14	2	2	2	82	.18	.03	2	26	.87	45	.07	5	3.44	.01	.03	2	5
1+00E 0+15N	2	27	12	103	.4	11	12	288	3.65	16	3	ND	2	15	2	2	2	79	.21	.04	2	20	.56	40	.07	5	2.60	.01	.04	2	5
1+00E 0+10N	2	21	9	98	.4	8	9	245	3.24	12	2	ND	2	16	2	2	2	77	.23	.03	2	17	.48	39	.06	5	2.37	.01	.04	2	5
1+00E 0+05N	2	19	9	91	.4	9	8	215	3.11	13	2	ND	2	21	2	2	2	76	.27	.03	2	17	.48	39	.06	6	2.42	.02	.04	2	5
1+00E 0+00S	2	22	9	73	.5	11	9	251	3.42	19	2	ND	2	13	2	2	2	81	.18	.03	2	17	.59	38	.05	7	2.76	.01	.04	2	5
1+00E 0+05S	2	20	6	53	.2	8	7	214	2.98	15	4	ND	2	13	1	2	2	73	.19	.03	2	14	.44	41	.03	5	2.24	.02	.05	2	5
1+00E 0+10S	2	26	9	60	.4	9	9	276	3.62	27	2	ND	2	15	2	2	2	78	.21	.04	2	15	.48	41	.03	5	2.57	.02	.06	2	5
1+00E 0+15S	3	30	9	62	.3	10	10	282	4.07	34	2	ND	2	13	2	2	2	83	.20	.04	3	18	.58	41	.03	7	2.72	.01	.05	2	5
1+00E 0+20S	3	28	9	69	.4	11	13	299	4.20	43	2	ND	2	12	2	2	2	77	.20	.04	3	18	.60	39	.03	6	3.08	.02	.06	2	5
1+00E 0+25S	4	67	13	66	.4	14	17	382	5.21	60	3	ND	2	10	2	2	2	77	.15	.04	3	20	.80	45	.04	7	3.50	.01	.03	2	10
1+25E 0+25N	2	28	10	63	.2	13	11	259	3.99	19	2	ND	2	11	2	2	2	90	.16	.03	2	24	.68	43	.06	6	3.11	.01	.03	2	5
1+25E 0+20N	2	29	10	70	.3	13	12	276	4.13	17	2	ND	2	13	2	2	2	93	.17	.03	2	25	.73	39	.06	5	3.20	.01	.03	2	5
1+25E 0+15N	2	45	10	66	.4	17	16	361	4.37	21	2	ND	2	12	2	2	2	88	.18	.03	3	30	.99	51	.09	5	3.69	.01	.03	2	5
1+25E 0+10N	2	48	9	76	.9	19	17	346	4.69	24	2	ND	2	15	2	2	2	92	.23	.04	3	32	.95	41	.09	7	3.67	.01	.03	2	5
1+25E 0+05N	2	32	10	65	.5	14	12	305	4.15	18	2	ND	2	16	2	2	2	94	.23	.03	2	25	.78	43	.08	6	3.00	.02	.04	2	5
1+25E 0+00S	2	20	6	54	.3	10	8	247	3.25	10	2	ND	2	13	1	2	2	85	.20	.03	3	21	.58	49	.07	6	2.29	.02	.04	2	5
1+25E 0+05S	2	22	7	50	.3	11	9	229	3.62	11	2	ND	2	14	2	2	2	87	.20	.03	2	22	.61	34	.07	5	2.73	.01	.03	2	5
1+25E 0+10S	2	20	6	43	.2	10	8	263	3.30	13	2	ND	2	18	1	2	2	85	.25	.03	2	21	.53	41	.07	6	2.25	.02	.04	2	5
1+25E 0+15S	2	22	9	57	.2	11	11	239	3.57	9	2	ND	2	15	1	2	2	82	.20	.03	2	22	.58	39	.07	5	2.82	.01	.03	2	5
1+25E 0+20S	2	32	9	68	.3	14	15	276	4.02	15	2	ND	2	12	2	2	2	87	.17	.03	4	26	.78	43	.09	6	3.32	.01	.03	2	15
1+25E 0+25S	2	26	8	54	.1	11	11	271	3.96	17	2	ND	2	18	2	2	2	92	.29	.04	3	24	.69	41	.07	7	2.55	.01	.04	2	5
1+50E 0+25N	2	28	9	55	.2	14	12	297	4.13	10	2	ND	2	14	1	2	2	100	.22	.04	2	26	.80	35	.10	7	2.96	.01	.03	2	5
1+50E 0+20N	1	20	6	47	.1	10	9	251	3.79	11	2	ND	2	17	1	2	2	98	.27	.04	4	20	.57	38	.07	5	2.51	.01	.04	2	5
1+50E 0+15N	2	22	6	53	.2	12	11	225	3.95	4	2	ND	2	14	2	2	2	100	.21	.03	3	25	.60	39	.08	6	3.01	.01	.03	2	5
1+50E 0+10N	2	21	3	47	.2	11	9	232	3.69	11	4	ND	2	16	2	2	2	93	.23	.03	3	23	.60	35	.08	7	2.71	.01	.04	2	5
1+50E 0+05N	2	27	6	58	.1	13	12	270	4.10	14	2	ND	2	12	2	2	2	99	.19	.04	4	28	.73	33	.09	6	3.12	.01	.03	2	5
1+50E 0+00S	2	40	8	62	.1	17	16	358	4.63	12	2	ND	2	13	2	2	2	104	.20	.04	4	35	1.10	45	.11	8	3.58	.01	.02	2	5
1+50E 0+05S	2	32	6	58	.2	14	13	299	4.05	14	2	ND	2	15	2	2	2	93	.21	.04	3	28	.86	41	.10	7	3.10	.01	.03	2	5
1+50E 0+10S	2	19	4	49	.2	11	9	230	3.43	7	2	ND	2	14	1	2	2	92	.20	.03	3	24	.63	35	.09	6	2.60	.01	.03	2	5
1+50E 0+15S	2	17	5	42	.1	9	8	200	3.16	3	2	ND	2	13	1	2	2	85	.18	.03	4	18	.53	33	.09	5	2.45	.01	.03	2	10
1+50E 0+20S	2	14	5	32	.1	8	6	165	2.56	2	2	ND	2	17	1	2	2	77	.22	.02	3	15	.45	34	.09	7	2.07	.01	.03	2	5
1+50E 0+25S	2	25	2	48	.2	13	11	233	3.37	9	2	ND	2	13	1	2	2	83	.16	.03	3	25	.74	41	.10	6	2.99	.01	.02	2	5
1+75E 0+50N	1	19	8	44	.2	9	8	211	3.29	14	2	ND	2	19	1	2	2	85	.21	.03	3	19	.53	33	.06	5	2.45	.01	.03	2	5
1+75E 0+40N	2	24	9	52	.3	12	11	242	4.11	21	2	ND	2	15	2	2	2	97	.19	.03	4	24	.62	38	.07	8	2.78	.02	.04	2	5
STD A-1/AU 0.5	2	29	39	184	.3	36	13	1008	2.76	9	2	ND	2	37	2	2	2	55	.61	.10	8	63	.62	252	.09	8	2.02	.02	.20	2	515

IMPERIAL METALS PROJECT # MAR FILE # B4-1281

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU1 PPB
1+75E 0+30N	2	19	7	42	.3	10	8	207	3.45	12	3	ND	2	14	1	2	2	92	.19	.03	2	21	.56	36	.08	8	2.52	.01	.03	2	5
1+75E 0+20N	2	29	2	50	.2	13	12	253	3.78	17	2	ND	2	13	1	2	2	90	.17	.03	2	24	.73	41	.10	10	3.14	.01	.03	2	5
1+75E 0+10N	1	18	3	41	.2	9	7	196	3.26	10	2	ND	2	13	1	2	2	88	.18	.03	2	20	.48	31	.08	6	2.28	.02	.04	2	5
1+75E 0+00S	2	22	5	47	.1	11	8	223	3.37	11	2	ND	2	15	1	2	2	86	.21	.03	2	23	.59	40	.09	7	2.56	.01	.04	2	5
1+75E 0+10S	2	26	4	55	.3	12	10	222	3.45	15	2	ND	2	15	2	2	2	83	.17	.03	2	25	.65	41	.09	9	3.06	.01	.03	2	5
1+75E 0+20S	2	27	3	52	.2	11	9	225	3.57	19	2	ND	2	12	2	2	2	82	.15	.03	2	21	.57	39	.07	7	2.95	.01	.03	2	5
1+75E 0+30S	2	27	2	48	.2	10	8	243	3.59	29	3	ND	2	14	1	2	2	87	.19	.03	2	21	.56	34	.06	7	2.61	.02	.03	2	5
1+75E 0+40S	2	28	1	45	.1	11	9	254	3.57	26	3	ND	2	15	2	2	2	85	.20	.03	2	20	.59	40	.06	10	2.78	.01	.03	2	5
1+75E 0+50S	2	26	4	48	.2	11	9	243	3.44	23	2	ND	2	15	1	2	2	80	.20	.04	2	21	.62	35	.07	7	2.84	.01	.03	2	5
2+00E 0+25N	2	29	3	54	.1	12	12	259	3.74	11	4	ND	2	14	2	2	2	90	.17	.03	2	24	.72	36	.10	9	3.17	.01	.03	2	5
2+00E 0+20N	1	22	1	51	.2	11	9	219	3.70	14	3	ND	2	15	1	2	2	94	.19	.03	2	22	.53	34	.09	9	2.82	.02	.04	2	5
2+00E 0+15N	3	28	5	59	.2	13	12	284	4.06	22	2	ND	2	18	2	2	2	100	.21	.03	2	26	.73	33	.10	8	3.00	.02	.03	2	5
2+00E 0+10N	2	33	4	66	.4	15	12	305	4.47	19	3	ND	2	13	2	2	2	102	.17	.04	2	29	.82	44	.10	9	3.17	.01	.03	2	5
2+00E 0+05N	2	25	14	79	.7	11	10	245	4.07	32	6	ND	2	14	2	2	2	90	.16	.04	2	22	.56	38	.07	8	2.91	.01	.04	2	20
2+00E 0+00S	3	21	14	67	.4	10	8	236	3.50	29	2	ND	2	12	2	2	2	88	.16	.03	3	21	.50	36	.06	9	2.56	.01	.04	2	5
2+00E 0+05S	3	32	20	121	.5	12	12	293	4.00	39	3	ND	2	10	2	2	2	83	.15	.04	2	23	.63	42	.06	8	3.22	.01	.05	2	5
2+00E 0+10S	3	27	19	79	.7	10	9	255	3.75	35	4	ND	2	12	2	2	2	89	.14	.03	2	19	.52	35	.04	8	2.57	.02	.04	2	5
2+00E 0+15S	5	44	30	124	1.4	10	11	344	4.79	80	8	ND	2	10	2	2	3	91	.11	.04	2	19	.53	39	.03	8	2.50	.01	.05	2	5
2+00E 0+20S	3	28	5	82	.9	9	10	284	3.93	39	2	ND	2	11	2	2	3	86	.14	.04	2	15	.47	31	.05	7	2.47	.01	.05	2	205
2+00E 0+25S	3	19	10	57	1.1	7	6	213	3.04	28	2	ND	2	12	1	2	2	77	.15	.03	2	15	.37	30	.03	6	2.29	.01	.05	2	225
2+25E 0+50N	2	27	5	53	.1	12	12	353	3.89	12	2	ND	2	13	1	2	2	96	.17	.03	2	24	.67	39	.10	10	2.85	.01	.03	2	5
2+25E 0+40N	2	18	6	44	.1	8	7	182	3.04	11	2	ND	2	14	1	2	2	79	.16	.03	2	20	.46	33	.09	9	2.52	.01	.03	2	85
2+25E 0+30N	2	19	4	37	.1	8	6	178	3.06	12	2	ND	2	14	1	2	3	84	.16	.03	2	18	.43	34	.07	8	2.40	.01	.03	2	5
2+25E 0+20N	2	31	5	60	.2	13	12	281	4.04	9	2	ND	2	14	2	2	2	96	.18	.03	2	26	.72	38	.09	6	3.25	.01	.03	2	5
2+25E 0+10N	2	32	2	58	.2	14	12	289	3.99	14	2	ND	2	10	1	2	2	93	.14	.04	2	28	.76	37	.10	9	3.24	.01	.03	2	5
2+25E 0+00S	2	22	5	54	.1	10	8	234	3.31	17	2	ND	2	14	1	2	2	85	.16	.02	2	21	.57	39	.08	8	2.67	.02	.03	2	5
2+25E 0+10S	3	34	11	99	.3	13	11	326	4.55	36	2	ND	2	12	2	2	2	98	.22	.04	2	23	.72	35	.07	10	2.84	.02	.05	2	10
2+25E 0+20S	3	22	6	47	.2	9	8	231	3.65	37	2	ND	2	13	2	2	2	93	.16	.03	2	19	.51	32	.05	8	2.48	.02	.04	2	25
2+25E 0+30S	3	48	9	61	.3	13	13	359	4.32	54	5	ND	2	14	2	2	2	85	.18	.04	2	22	.74	49	.06	11	2.96	.02	.04	2	5
2+25E 0+40S	2	24	4	45	.1	10	8	250	3.53	21	2	ND	2	11	1	2	2	87	.13	.02	2	21	.59	34	.06	7	2.57	.02	.03	2	5
2+25E 0+50S	3	53	13	61	.1	13	13	340	4.94	58	2	ND	2	12	2	2	2	83	.15	.04	2	22	.83	33	.02	9	2.93	.01	.05	2	5
2+25E 0+60S	2	33	4	54	.7	15	14	293	4.03	18	2	ND	2	12	2	2	2	93	.16	.03	2	27	.85	39	.10	10	3.42	.02	.03	2	5
2+25E 0+70S	2	25	3	44	.2	11	9	235	3.45	18	2	ND	2	13	1	2	2	85	.18	.04	2	23	.64	34	.09	9	2.85	.01	.03	2	5
2+25E 0+80S	2	20	5	44	.1	9	8	226	3.63	31	2	ND	2	14	1	2	2	94	.18	.04	2	21	.49	35	.08	9	2.55	.02	.04	2	5
2+25E 0+85S	2	33	1	51	.1	14	13	280	3.61	57	2	ND	2	14	1	2	2	78	.19	.04	2	26	.76	52	.10	9	3.43	.01	.03	2	5
2+25E 0+90S	2	35	2	56	.2	14	15	299	3.91	65	2	ND	2	12	2	2	2	81	.18	.04	2	26	.80	46	.11	7	3.54	.01	.03	2	5
2+25E 0+95S	2	22	4	45	.2	11	8	339	3.31	27	2	ND	2	18	1	2	2	84	.24	.04	2	21	.56	42	.09	8	2.49	.02	.04	2	5
STD A-1/AU 0.5	2	30	39	186	.3	36	13	1029	2.79	9	2	ND	2	37	2	2	2	56	.62	.10	7	64	.63	255	.10	8	2.05	.02	.20	2	485

IMPERIAL METALS PROJECT # MAR FILE # 84-1281

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
2+25E 1+00S	1	22	2	57	.3	10	10	284	3.39	24	2	ND	2	17	1	2	2	84	.25	.04	2	26	.54	39	.11	5	3.15	.02	.04	2	35
2+25E 1+05S	1	27	2	61	.2	12	11	310	3.77	37	3	ND	2	16	1	2	2	88	.23	.03	5	27	.73	51	.13	6	3.36	.01	.03	2	60
2+50E 0+25N	1	36	44	151	1.0	14	14	320	4.45	23	4	ND	2	14	2	2	2	97	.26	.03	2	29	.77	39	.09	6	3.70	.01	.04	2	95
2+50E 0+20N	2	28	80	374	.6	12	13	457	4.28	37	4	ND	2	13	2	2	2	94	.39	.03	4	24	.66	39	.04	6	3.21	.01	.06	2	25
2+50E 0+15N	3	33	128	814	1.1	11	14	678	4.53	56	3	ND	2	12	3	2	2	88	.40	.03	3	24	.66	35	.02	7	3.17	.01	.07	2	285
2+50E 0+10N	2	26	110	677	1.0	10	13	604	4.47	46	4	ND	2	13	2	2	2	93	.36	.03	3	20	.59	38	.03	7	2.89	.02	.08	2	40
2+50E 0+05N	2	36	58	514	1.2	13	13	409	4.88	44	4	ND	2	12	2	2	2	104	.30	.04	5	26	.76	41	.05	9	3.50	.01	.05	2	15
2+50E 0+00S	1	38	14	205	.5	15	17	346	4.58	21	3	ND	2	13	2	2	2	99	.22	.03	4	24	.75	39	.06	7	3.77	.01	.04	2	5
2+50E 0+05S	1	28	15	180	.6	13	13	392	4.41	26	3	ND	2	15	2	2	2	107	.33	.03	5	25	.71	40	.05	7	3.26	.01	.07	2	5
2+50E 0+10S	1	42	12	170	.5	15	14	428	5.61	51	4	ND	2	14	2	2	2	113	.30	.04	5	26	.84	42	.06	5	3.59	.02	.05	2	5
2+50E 0+15S	3	25	24	83	.5	11	9	246	4.02	21	3	ND	2	14	2	2	2	101	.23	.03	5	25	.57	37	.06	7	2.92	.01	.04	2	5
2+50E 0+20S	2	20	5	59	.4	8	7	218	3.47	18	2	ND	2	15	2	2	2	87	.22	.04	4	19	.45	33	.08	6	2.83	.02	.04	2	5
2+50E 0+25S	1	27	8	56	.4	11	9	285	4.00	29	3	ND	2	16	1	2	2	98	.24	.05	3	27	.57	38	.08	7	2.90	.01	.06	2	5
2+50E 0+30S	2	29	5	64	.4	13	13	268	4.11	11	2	ND	2	16	2	2	2	92	.23	.03	4	26	.69	40	.10	6	3.47	.01	.04	2	5
2+75E 0+50N	1	45	7	65	.4	15	15	336	4.78	7	4	ND	2	19	1	2	2	103	.28	.04	2	31	.88	45	.12	9	3.66	.01	.04	2	95
2+75E 0+40N	1	39	3	65	.1	15	16	327	4.58	4	4	ND	2	20	1	2	2	106	.29	.03	3	30	.94	44	.14	6	3.65	.01	.04	2	5
2+75E 0+30N	1	41	4	63	.1	17	17	325	4.64	8	3	ND	2	17	2	2	2	101	.24	.04	2	30	.96	40	.13	5	3.72	.01	.03	2	5
2+75E 0+20N	1	22	2	54	.1	12	11	349	4.03	3	3	ND	2	20	1	2	2	100	.28	.04	3	25	.66	52	.11	5	2.96	.01	.07	2	55
2+75E 0+10N	1	27	5	60	.2	14	13	388	4.28	4	3	ND	2	18	1	2	2	104	.24	.03	3	29	.75	45	.12	4	3.19	.01	.04	2	5
2+75E 0+00S	1	36	3	67	.1	13	15	402	4.66	18	3	ND	2	18	1	2	2	104	.24	.04	4	25	.78	51	.12	5	3.57	.01	.06	2	5
2+75E 0+10S	1	29	9	67	.3	13	13	325	4.40	9	2	ND	2	18	1	2	2	99	.23	.03	2	27	.72	42	.09	5	3.29	.01	.05	2	5
2+75E 0+20S	1	37	7	72	.3	15	15	346	4.64	17	3	ND	2	20	1	2	2	96	.24	.04	3	29	.79	39	.09	5	3.53	.01	.05	2	5
2+75E 0+40S	2	30	4	58	.1	12	13	306	4.11	19	2	ND	2	19	1	2	2	89	.27	.04	5	26	.69	40	.09	6	3.16	.01	.04	2	5
3+00E 0+25N	1	33	4	62	.3	14	14	269	4.43	3	3	ND	2	18	1	2	2	107	.26	.04	2	30	.70	38	.11	7	3.71	.01	.05	2	5
3+00E 0+20N	1	40	4	64	.2	16	15	312	4.59	2	3	ND	2	17	1	2	2	109	.24	.03	2	35	.95	39	.13	7	3.68	.01	.04	2	5
3+00E 0+15N	1	44	5	64	.2	16	16	343	4.64	7	3	ND	2	18	1	2	2	105	.25	.04	3	31	.98	51	.13	6	3.85	.01	.03	2	5
3+00E 0+10N	1	23	3	58	.3	12	11	266	4.01	2	3	ND	2	17	1	2	2	100	.23	.04	2	25	.67	32	.11	7	2.94	.01	.04	2	5
3+00E 0+05N	1	31	1	56	.2	13	12	271	4.27	2	3	ND	2	16	1	2	2	107	.21	.03	4	28	.78	35	.13	6	3.51	.01	.03	2	5
3+00E 0+00S	1	18	4	46	.1	10	9	237	3.62	2	2	ND	2	19	1	2	2	99	.26	.03	6	27	.57	41	.12	9	2.67	.01	.03	2	10
3+00E 0+05S	2	17	2	35	.2	9	8	195	3.34	5	2	ND	2	19	1	2	2	94	.25	.02	5	21	.48	40	.11	7	2.42	.01	.03	2	5
3+00E 0+10S	1	22	4	45	.1	12	10	272	3.80	4	2	ND	2	20	1	2	2	100	.28	.03	2	26	.67	52	.11	5	2.75	.01	.04	2	10
3+00E 0+15S	1	29	2	55	.2	13	13	272	3.98	8	2	ND	2	20	1	2	2	96	.27	.04	6	27	.66	41	.12	7	3.57	.01	.04	2	5
3+00E 0+20S	2	21	3	46	.2	11	10	246	3.80	5	2	ND	2	19	1	2	2	101	.25	.03	5	28	.62	40	.11	7	3.04	.01	.02	2	5
3+00E 0+25S	1	37	1	63	.2	16	16	481	4.55	2	2	ND	2	19	2	2	2	108	.27	.03	4	33	.99	41	.14	6	3.62	.02	.04	2	5
3+50E 0+50N	2	51	50	93	.3	14	12	341	6.18	27	2	ND	2	16	1	2	2	98	.13	.05	8	22	.64	45	.08	6	3.65	.01	.05	2	5
3+50E 0+40N	1	61	21	78	.4	13	13	410	5.92	23	2	ND	2	22	2	2	2	99	.15	.05	6	19	.70	52	.11	4	3.94	.01	.06	2	10
3+50E 0+30N	2	60	21	86	.4	13	11	431	6.47	21	3	ND	2	16	2	2	2	105	.16	.06	5	23	.70	57	.10	5	4.09	.01	.07	2	5
STD A-1/AU 0.5	2	31	40	188	.3	36	13	1029	2.82	9	2	ND	2	37	2	2	2	57	.63	.10	7	65	.64	258	.11	8	2.07	.02	.21	2	495

IMPERIAL METALS PROJECT # MAR FILE # 84-1281

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	M PPM	AU# PPB
3+50E 0+20N	2	40	11	78	.3	11	11	316	4.68	22	2	ND	2	16	1	2	2	93	.19	.05	2	23	.58	43	.06	7	3.01	.01	.06	2	5
3+50E 0+10N	1	34	3	70	.2	15	13	350	4.37	14	2	ND	2	14	1	2	2	99	.21	.04	2	25	.83	44	.09	8	3.46	.01	.05	2	5
3+50E 0+00S	1	27	7	68	.1	14	14	276	4.06	7	2	ND	2	14	1	2	2	98	.20	.03	2	29	.81	37	.10	8	3.54	.01	.06	2	5
3+50E 0+10S	1	26	2	62	.1	14	13	278	4.10	6	2	ND	2	15	1	2	2	98	.23	.04	2	28	.82	35	.10	7	3.50	.01	.04	2	5
3+50E 0+20S	2	27	1	61	.1	15	13	275	4.06	7	2	ND	2	17	1	2	2	100	.26	.05	2	31	.84	38	.12	8	3.49	.01	.07	2	5
3+50E 0+30S	1	30	1	66	.1	15	14	305	4.48	2	2	ND	2	17	2	2	2	110	.27	.04	2	30	.96	36	.14	6	3.66	.01	.05	2	10
3+50E 0+40S	1	25	1	65	.3	13	11	272	3.72	4	2	ND	2	18	1	2	2	91	.27	.05	2	27	.73	38	.12	7	3.41	.01	.05	2	5
3+50E 0+50S	2	20	1	61	.1	12	10	297	3.66	4	2	ND	2	16	1	2	2	90	.27	.09	2	23	.68	36	.10	7	3.22	.01	.05	2	5
4+00E 0+50N	1	50	13	97	.3	12	11	353	4.86	22	2	ND	2	14	1	2	2	88	.13	.05	2	19	.59	41	.08	5	3.66	.01	.06	2	15
4+00E 0+40N	2	29	17	66	.3	9	8	263	4.16	17	2	ND	2	16	1	2	2	89	.18	.04	2	16	.48	51	.06	9	3.00	.01	.07	2	5
4+00E 0+30N	2	33	13	81	.5	9	10	272	4.09	19	2	ND	2	14	1	2	2	82	.15	.04	2	17	.44	46	.05	8	3.04	.01	.06	2	5
4+00E 0+20N	2	29	20	86	.3	9	9	303	4.29	22	3	ND	2	14	1	2	2	90	.16	.04	2	17	.47	43	.05	7	2.92	.01	.06	2	5
4+00E 0+10N	2	39	11	94	.5	13	13	308	4.24	16	2	ND	2	15	1	2	2	87	.18	.04	2	24	.63	39	.06	5	3.21	.01	.06	2	5
4+00E 0+00S	2	44	28	156	1.4	9	11	287	4.93	40	5	ND	2	12	2	2	2	77	.11	.06	2	15	.47	51	.02	7	3.12	.01	.08	2	5
4+00E 0+10S	3	48	28	93	2.3	10	12	250	5.36	44	2	ND	2	11	1	2	2	81	.10	.06	2	18	.50	39	.02	7	2.94	.01	.07	2	5
4+00E 0+20S	1	39	6	71	.5	14	14	374	4.64	17	3	ND	2	14	1	2	2	94	.22	.06	2	26	.73	44	.05	7	3.36	.01	.09	2	5
4+00E 0+30S	2	42	1	69	.1	18	16	373	4.72	15	3	ND	2	18	1	2	2	100	.26	.06	2	35	.93	48	.07	6	3.93	.01	.07	2	80
4+00E 0+40S	2	31	5	61	.1	12	13	349	4.29	13	2	ND	2	17	1	2	2	93	.23	.04	2	23	.72	41	.06	5	3.21	.01	.06	2	5
4+00E 0+50S	1	33	1	64	.1	16	15	299	4.42	10	2	ND	2	15	1	2	2	102	.21	.04	2	27	.88	32	.09	4	3.62	.01	.05	2	5
4+27E 0+50N	3	64	23	85	.4	14	13	360	5.98	25	2	ND	2	16	1	2	2	99	.15	.06	2	21	.69	52	.08	7	3.66	.01	.06	2	10
4+27E 0+45N	2	72	27	76	.3	12	10	368	7.52	24	2	ND	2	17	1	2	2	109	.14	.07	2	21	.61	51	.15	5	3.66	.01	.06	2	5
4+27E 0+40N	2	37	39	150	.3	9	9	269	4.70	18	3	ND	2	16	1	2	2	94	.18	.05	2	19	.51	50	.07	7	3.03	.01	.07	2	5
4+27E 0+35N	3	47	11	92	.3	13	12	369	4.87	15	2	ND	2	16	2	2	2	88	.18	.05	2	23	.57	49	.09	8	3.65	.01	.07	2	5
4+27E 0+30N	2	45	10	74	.1	15	14	336	4.78	15	3	ND	2	15	1	2	2	88	.17	.05	2	24	.68	41	.10	7	3.51	.01	.06	2	5
4+50E 0+50N	2	25	15	54	.2	7	7	205	3.92	12	6	ND	2	15	1	2	2	83	.18	.05	2	17	.39	39	.04	6	2.66	.01	.06	2	5
4+50E 0+40N	3	59	15	74	.2	12	11	362	5.60	23	2	ND	2	13	1	2	2	98	.14	.06	2	24	.59	47	.08	7	3.52	.01	.06	2	5
4+50E 0+30N	2	45	12	64	.2	12	12	317	5.46	26	2	ND	2	14	1	2	2	103	.17	.05	2	23	.54	45	.07	7	3.52	.01	.06	2	5
4+50E 0+20N	2	17	7	48	.1	10	8	225	3.25	2	4	ND	2	16	1	2	2	85	.22	.03	2	20	.53	35	.07	6	2.63	.01	.05	2	5
4+50E 0+10N	2	43	5	76	.2	14	14	324	4.61	17	2	ND	2	16	1	2	2	99	.19	.05	2	27	.74	42	.08	7	3.57	.01	.05	2	5
4+50E 0+00S	1	27	9	207	1.3	14	15	259	3.65	7	4	ND	2	15	1	2	2	75	.20	.08	2	26	.54	48	.09	9	3.65	.01	.07	2	5
4+50E 0+10S	2	45	6	75	.2	15	16	320	4.96	17	2	ND	2	14	1	2	2	105	.16	.05	2	28	.76	42	.10	6	3.63	.01	.04	2	10
4+50E 0+20S	2	45	4	77	.1	23	19	376	5.31	3	2	ND	2	14	2	2	2	123	.20	.03	2	41	1.18	55	.16	8	4.33	.01	.04	2	5
4+50E 0+30S	2	31	6	65	.1	14	13	310	4.17	10	3	ND	2	14	1	2	2	95	.20	.04	2	28	.72	41	.09	7	3.39	.01	.05	2	5
4+50E 0+40S	2	26	7	64	.3	12	12	299	4.09	17	2	ND	2	16	1	2	2	90	.22	.05	2	22	.58	49	.07	9	3.17	.01	.05	2	5
4+50E 0+50S	2	24	6	67	.2	12	11	252	3.51	14	2	ND	2	15	1	2	2	79	.21	.05	2	22	.56	39	.07	6	3.40	.01	.05	2	5
5+00E 0+50N	2	60	91	96	1.0	13	11	356	5.71	31	6	ND	2	12	1	2	2	98	.12	.07	2	23	.65	59	.07	6	3.62	.01	.06	2	5
5+00E 0+40N	2	55	15	78	.9	13	12	313	4.94	21	2	ND	2	14	2	2	2	89	.14	.06	3	22	.55	48	.07	10	3.70	.01	.06	2	5
STD A-1/AU 0.5	2	30	39	186	.3	36	13	1029	2.79	9	2	ND	2	37	2	2	2	56	.62	.11	7	64	.63	255	.10	7	2.05	.02	.20	2	495

IMPERIAL METALS PROJECT # MAR FILE # 84-1281

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
5+00E 0+30N	3	35	9	67	.4	9	10	291	3.88	20	3	ND	2	10	1	2	2	69	.10	.05	3	17	.53	39	.04	8	3.01	.01	.04	2	5
5+00E 0+20N	2	35	11	63	.6	6	6	298	4.42	16	5	ND	2	8	1	2	2	72	.08	.06	3	13	.44	49	.02	8	2.85	.01	.06	2	5
5+00E 0+10N	3	40	10	66	1.0	8	9	262	4.58	19	3	ND	2	8	1	2	2	78	.09	.06	5	18	.43	36	.03	10	2.72	.01	.05	2	5
5+00E 0+00S	3	44	7	59	.8	9	9	301	4.92	35	2	ND	2	8	2	2	2	82	.08	.07	5	19	.53	43	.04	10	2.79	.01	.04	2	5
5+00E 0+10S	2	44	8	69	.6	12	12	291	4.35	20	2	ND	2	9	2	2	2	77	.09	.06	5	20	.57	40	.06	9	3.17	.01	.05	2	5
5+00E 0+20S	2	27	5	54	.5	13	11	329	3.88	15	2	ND	2	15	1	2	2	83	.20	.04	4	26	.73	55	.05	8	2.57	.01	.04	2	40
5+00E 0+30S	2	39	6	52	.6	13	12	293	4.29	20	2	ND	2	8	1	2	2	85	.11	.04	3	25	.65	44	.06	8	2.89	.01	.04	2	5
5+00E 0+40S	2	21	8	47	1.2	8	8	211	3.22	15	2	ND	2	10	1	2	2	70	.12	.04	3	20	.45	38	.04	6	2.64	.01	.04	2	5
5+00E 0+50S	1	22	10	43	.4	8	8	198	3.46	14	3	ND	2	9	1	2	2	72	.12	.04	4	16	.43	44	.04	7	2.71	.01	.04	2	5
13T-M-1	2	69	3	56	.2	142	27	518	3.99	4	2	ND	2	33	2	3	2	106	1.59	.04	5	241	2.86	25	.15	13	3.38	.01	.02	2	5
13T-M-1S	2	49	2	53	.1	105	23	435	3.89	8	2	ND	2	18	2	2	2	102	1.03	.03	4	178	2.17	23	.12	9	3.02	.01	.03	2	5
STD A-1	2	30	38	184	.3	36	13	1039	2.76	9	2	ND	2	37	2	2	2	55	.61	.10	7	63	.62	252	.10	8	2.03	.01	.20	2	-

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-3 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SN, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: P1-P3 SOIL P4 ROCK AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

Soils - 80 pulverized

DATE RECEIVED: JUNE 28 1984 DATE REPORT MAILED: *June 30/84* ASSAYER: *D. J. J.* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT # MAC FILE # 84-1312

PAGE 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
1+50W 0+80N	3	20	8	57	.2	9	7	227	3.57	16	3	ND	2	17	1	2	2	87	.24	.05	2	19	.47	36	.11	8	2.60	.01	.04	2	5
1+50W 0+70N	3	24	3	49	.2	9	9	221	3.77	14	4	ND	2	15	1	2	2	91	.25	.05	2	17	.45	35	.11	6	3.10	.01	.04	2	5
1+50W 0+60N	3	32	7	60	.4	11	11	266	4.10	21	2	ND	2	13	1	2	2	91	.22	.05	2	21	.64	37	.10	9	3.26	.01	.03	2	5
1+00W 0+80N	3	23	7	79	.1	9	11	536	3.58	17	2	ND	2	16	1	2	2	77	.24	.06	2	17	.45	41	.09	6	2.52	.01	.05	2	5
1+00W 0+70N	2	14	7	65	.1	7	6	197	2.64	13	3	ND	2	18	1	2	2	72	.24	.03	2	12	.38	44	.07	7	2.07	.01	.04	2	10
1+00W 0+60N	2	18	10	64	.1	7	7	213	2.83	11	2	ND	2	15	1	2	2	74	.22	.03	2	15	.42	39	.08	5	2.05	.01	.05	2	25
2+50E 0+35S	2	26	4	54	.2	11	10	245	4.52	28	2	ND	2	14	1	2	2	102	.20	.05	2	21	.58	33	.10	6	3.19	.01	.03	2	5
2+50E 0+45S	3	24	5	50	.2	11	10	235	4.09	23	3	ND	2	19	1	2	2	92	.25	.04	2	20	.58	39	.10	7	2.90	.01	.04	2	5
2+50E 0+55S	3	30	4	50	.2	13	10	260	3.74	22	2	ND	2	17	1	2	2	86	.23	.05	2	22	.64	34	.09	5	2.99	.01	.05	2	45
2+50E 0+65S	3	25	1	48	.1	12	10	245	3.71	22	2	ND	2	16	1	2	2	85	.23	.04	2	22	.63	33	.11	7	3.12	.01	.03	2	80
2+50E 0+75S	2	26	4	53	.1	12	10	259	4.16	49	3	ND	2	15	1	2	2	90	.22	.05	2	22	.58	35	.11	7	3.11	.01	.03	2	5
2+50E 0+85S	2	26	1	43	.1	12	9	225	3.41	17	4	ND	2	15	1	2	2	84	.21	.03	3	22	.59	39	.11	7	2.83	.01	.03	2	5
2+50E 0+95S	2	24	4	45	.1	12	11	211	3.39	13	2	ND	2	15	1	2	2	85	.23	.03	3	23	.66	33	.12	7	3.29	.01	.02	2	10
2+50E 1+05S	2	35	3	55	.2	16	15	270	4.06	26	2	ND	2	14	1	2	2	89	.21	.03	2	27	.84	50	.12	8	3.71	.01	.02	2	25
2+36E 0+80S	2	35	2	53	.2	15	14	314	3.98	27	2	ND	2	16	1	2	2	88	.23	.03	2	29	.82	47	.13	6	3.44	.01	.03	2	5
2+36E 0+85S	2	23	1	44	.1	11	10	229	3.20	18	2	ND	2	16	1	2	2	81	.23	.03	2	19	.60	39	.12	5	3.10	.01	.03	2	5
2+36E 0+90S	2	28	2	51	.2	14	13	259	3.73	17	2	ND	2	16	1	2	2	91	.24	.03	2	27	.77	42	.13	9	3.69	.01	.03	2	5
2+36E 0+95S	1	25	3	46	.3	12	12	225	3.41	16	2	ND	2	14	1	2	2	85	.23	.03	3	23	.66	36	.12	8	3.50	.01	.03	2	5
2+36E 1+00S	3	26	5	50	.1	11	10	273	4.00	39	2	ND	2	18	1	2	2	95	.27	.04	3	21	.59	42	.13	8	2.93	.01	.04	2	5
MR-0	10	477	9849	2877	300.6	14	18	4504	5.96	182	2	ND	2	17	28	60	2	67	.39	.04	9	17	.75	27	.05	7	2.72	.01	.04	2	2100
MR-1	7	81	224	336	5.4	15	18	722	6.32	66	2	ND	2	26	3	7	2	62	.25	.05	12	16	.71	41	.04	9	2.60	.02	.05	2	10
MR-2	3	65	73	266	2.0	14	24	1137	4.90	72	3	ND	2	59	3	3	3	70	.49	.04	5	16	.82	48	.07	8	2.64	.02	.05	2	190
MR-3	3	59	38	118	.3	18	24	949	5.26	56	3	ND	2	35	2	2	2	81	.39	.05	3	25	.94	45	.12	6	3.07	.02	.04	2	5
MR-4	3	57	27	99	.4	17	19	781	4.90	54	2	ND	2	32	2	2	2	86	.31	.04	6	24	.94	53	.08	11	3.90	.01	.03	2	5
MR-5	3	59	50	95	1.4	17	20	1094	4.86	53	2	ND	2	25	2	2	2	83	.30	.04	5	23	1.01	48	.07	8	3.39	.01	.04	2	20
MR-6	2	28	3	58	.6	13	13	270	4.01	17	2	ND	2	16	1	2	2	98	.23	.02	2	26	.69	44	.11	9	3.48	.01	.04	2	10
MR-7	1	52	7	70	.5	21	19	643	5.26	15	2	ND	2	29	1	2	2	110	.39	.03	2	40	1.37	48	.13	7	4.38	.01	.03	2	5
MR-8	3	48	5	60	.5	17	16	362	4.45	17	5	ND	2	16	2	2	2	97	.23	.03	4	31	.96	65	.14	11	4.20	.01	.02	2	5
MR-9	2	49	13	72	.5	17	17	533	4.72	38	2	ND	2	25	2	2	2	96	.28	.03	3	27	.97	58	.14	11	3.92	.01	.02	2	5
MR-10	2	55	21	105	.4	15	17	755	4.98	48	2	ND	2	31	2	2	2	92	.32	.03	4	26	.86	57	.12	8	2.96	.02	.04	2	25
MR-11	4	54	20	98	.5	15	19	692	5.29	44	2	ND	2	20	2	2	2	95	.30	.04	5	22	.81	54	.14	10	4.01	.01	.04	2	70
MR-12	2	51	15	70	.3	16	15	506	4.61	20	2	ND	2	24	1	2	2	88	.22	.03	5	28	.93	47	.13	9	3.27	.01	.04	2	5
MR-13	3	68	42	149	.3	16	18	657	5.77	35	2	ND	2	42	2	2	2	92	.22	.04	6	23	.75	56	.14	10	3.66	.02	.05	2	5
MR-14	1	111	87	216	.7	13	22	757	10.76	41	2	ND	2	26	2	2	2	155	.15	.08	7	23	.66	35	.14	6	3.55	.02	.04	2	5
MR-15	1	170	146	245	.7	6	10	429	15.27	54	2	ND	2	13	1	2	2	89	.06	.09	4	22	.44	14	.02	2	2.17	.01	.05	2	5
MR-16	2	96	35	92	.4	13	14	558	9.06	43	2	ND	2	41	1	2	2	112	.30	.08	7	27	.80	54	.21	9	4.64	.02	.04	2	5
MR-17	2	66	12	69	.2	14	12	428	6.42	19	2	ND	2	17	2	2	2	100	.11	.07	4	26	.76	46	.07	10	3.72	.01	.05	2	5
STD A-1/AU 0.5	2	30	39	188	.3	36	13	1029	2.82	9	2	ND	2	37	2	2	2	57	.63	.10	7	65	.64	258	.10	8	2.07	.02	.20	2	510

IMPERIAL METALS PROJECT # MAC FILE # 84-1312

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU1 PPB
MR-18	2	85	16	189	.1	24	61	3750	7.21	38	4	ND	2	38	2	2	2	101	.29	.06	2	22	.93	44	.10	2	3.34	.02	.04	2	5
MR-19	2	77	6	48	.2	7	7	319	8.62	38	2	ND	2	12	1	2	2	75	.10	.10	2	16	.52	32	.03	2	2.83	.01	.04	2	5
MR-20	4	78	33	72	.2	10	9	321	6.84	39	3	ND	2	14	1	2	2	59	.05	.08	3	16	.58	46	.01	3	2.99	.01	.03	2	5
MR-21	2	90	19	63	.7	8	8	312	9.06	38	2	ND	2	14	1	2	2	69	.08	.10	2	17	.60	35	.02	2	3.06	.01	.04	2	5
MR-22	2	60	15	81	.1	13	14	529	5.20	29	2	ND	2	17	1	2	2	73	.22	.05	2	20	.67	61	.04	4	3.21	.01	.06	2	5
MR-23	3	83	33	69	.3	11	9	309	7.70	38	2	ND	2	17	2	2	2	58	.16	.09	2	19	.63	37	.02	2	2.92	.01	.04	2	5
MR-24	3	58	16	59	.3	7	7	314	6.88	34	2	ND	2	11	1	2	2	65	.12	.08	2	15	.54	29	.03	4	2.52	.01	.04	2	5
MR-25	2	56	38	72	.2	10	10	405	4.89	29	2	ND	2	22	2	2	2	63	.20	.04	2	17	.51	34	.08	4	1.97	.02	.04	2	5
MR-26	2	65	22	66	.1	10	8	351	5.19	31	4	ND	2	21	2	2	2	56	.26	.05	2	15	.70	44	.02	2	2.63	.01	.04	2	5
MR-27	5	88	8	172	.2	29	52	1279	4.88	33	2	ND	2	49	3	5	2	79	.52	.05	6	19	.67	253	.11	4	5.00	.01	.08	3	5
MR-28	2	57	8	60	.1	12	12	470	4.90	28	2	ND	2	21	2	2	2	73	.29	.04	3	20	.75	38	.09	4	2.42	.02	.04	2	5
MR-29	3	47	12	181	.3	21	34	2048	4.39	16	5	ND	2	38	2	3	2	50	1.01	.04	3	11	.80	67	.01	4	4.53	.01	.03	2	5
MR-30	2	59	16	67	.2	11	15	628	5.50	23	2	ND	2	23	1	2	2	74	.25	.05	3	20	.66	41	.08	4	2.45	.02	.05	2	5
MR-31	2	42	10	89	.2	11	10	316	5.35	26	3	ND	2	15	2	2	2	77	.17	.14	2	19	.55	51	.05	5	3.07	.02	.08	2	10
MR-32	2	29	10	71	.2	9	9	270	4.08	22	2	ND	2	19	1	2	2	72	.23	.07	4	16	.49	43	.06	6	2.16	.02	.06	2	5
MR-33	1	44	4	52	.1	12	11	347	4.40	27	2	ND	2	21	1	2	2	75	.23	.04	2	21	.70	42	.08	4	2.38	.02	.03	2	5
MR-34	2	101	12	83	.2	7	7	424	6.10	21	2	ND	2	24	2	2	2	86	.29	.06	4	25	.42	29	.20	6	2.62	.01	.05	2	5
MR-35	1	126	2	89	.3	9	20	925	12.23	23	2	ND	2	40	1	2	2	136	.52	.13	2	25	.37	44	.26	2	4.26	.02	.02	2	10
MR-36	2	66	26	237	.3	12	15	666	4.30	38	2	ND	2	16	2	2	2	72	.31	.04	5	18	.70	45	.10	7	2.88	.01	.06	2	10
MR-37	2	66	14	90	.4	10	15	626	3.92	36	2	ND	2	21	2	2	2	71	.42	.03	3	15	.71	42	.14	6	3.06	.01	.04	2	5
MR-38	2	61	14	83	.4	15	23	925	4.29	37	3	ND	2	14	2	2	2	55	.65	.04	11	15	.56	71	.03	6	2.90	.01	.06	2	15
MR-39	2	68	10	71	.1	11	17	879	4.77	76	2	ND	2	21	2	2	2	80	.53	.03	5	15	.79	53	.12	7	3.01	.01	.06	2	10
MR-40	1	64	9	66	.1	10	14	621	4.36	83	2	ND	2	22	1	2	2	79	.48	.03	4	16	.76	48	.12	7	2.87	.01	.04	2	5
MR-41	2	53	7	57	.1	11	13	531	4.37	40	2	ND	2	20	1	2	2	68	.36	.02	4	20	.78	53	.08	5	2.57	.01	.03	2	5
MR-42	2	64	13	74	.1	11	15	695	4.54	50	2	ND	2	24	2	2	2	81	.52	.04	5	15	.71	43	.14	9	2.91	.01	.05	2	5
MR-43	2	60	6	65	.1	11	13	787	4.73	44	2	ND	2	19	2	2	2	78	.54	.04	4	13	.62	49	.11	6	2.55	.02	.06	2	5
MR-44	3	53	6	53	.1	11	13	653	4.27	40	2	ND	2	16	1	2	2	67	.52	.03	5	19	.72	48	.08	6	2.51	.02	.05	2	5
MR-45	2	49	9	51	.1	10	12	578	4.09	40	2	ND	2	17	1	2	2	66	.46	.03	5	15	.67	56	.06	7	2.57	.01	.04	2	5
MR-46	2	59	16	69	.1	10	15	801	4.31	48	2	ND	2	24	2	2	3	77	.66	.04	4	16	.69	48	.15	6	2.71	.02	.06	2	5
MR-47	2	52	8	52	.1	8	15	916	3.84	29	2	ND	2	22	1	2	2	60	.48	.03	4	12	.50	55	.09	5	2.13	.01	.06	2	5
MR-48	2	54	13	69	.2	9	15	677	4.36	39	2	ND	2	18	2	2	2	74	.45	.03	3	14	.58	47	.12	5	2.52	.01	.06	2	5
MR-49	2	59	9	58	.1	9	13	526	4.61	43	2	ND	2	16	2	2	3	71	.38	.03	3	13	.62	40	.10	6	2.55	.01	.05	2	5
MR-50	2	38	7	59	.1	9	12	460	3.92	28	4	ND	2	16	1	2	2	67	.36	.03	3	14	.56	36	.09	8	2.25	.01	.05	2	5
MR-51	1	94	16	50	.1	19	14	465	9.95	67	2	ND	2	14	1	3	3	68	.13	.11	2	17	.60	45	.13	3	3.02	.01	.04	2	5
MR-52	1	58	16	59	.1	9	13	569	4.66	50	2	ND	2	21	1	2	2	72	.36	.04	3	14	.68	46	.14	8	2.86	.01	.05	2	15
MR-53	2	64	15	65	.1	9	13	613	4.80	54	2	ND	2	26	2	2	2	75	.41	.04	4	16	.73	57	.16	10	3.16	.02	.04	2	5
MR-54	3	51	12	74	.1	12	15	479	4.58	50	2	ND	2	20	2	2	2	73	.33	.04	4	16	.65	67	.14	7	3.22	.02	.04	2	5
STD A-1/AU 0.5	2	30	39	184	.3	36	13	1008	2.76	9	2	ND	2	37	2	2	2	55	.61	.10	7	63	.62	252	.10	7	2.03	.02	.18	2	500

IMPERIAL METALS PROJECT # MAC FILE # 84-1312

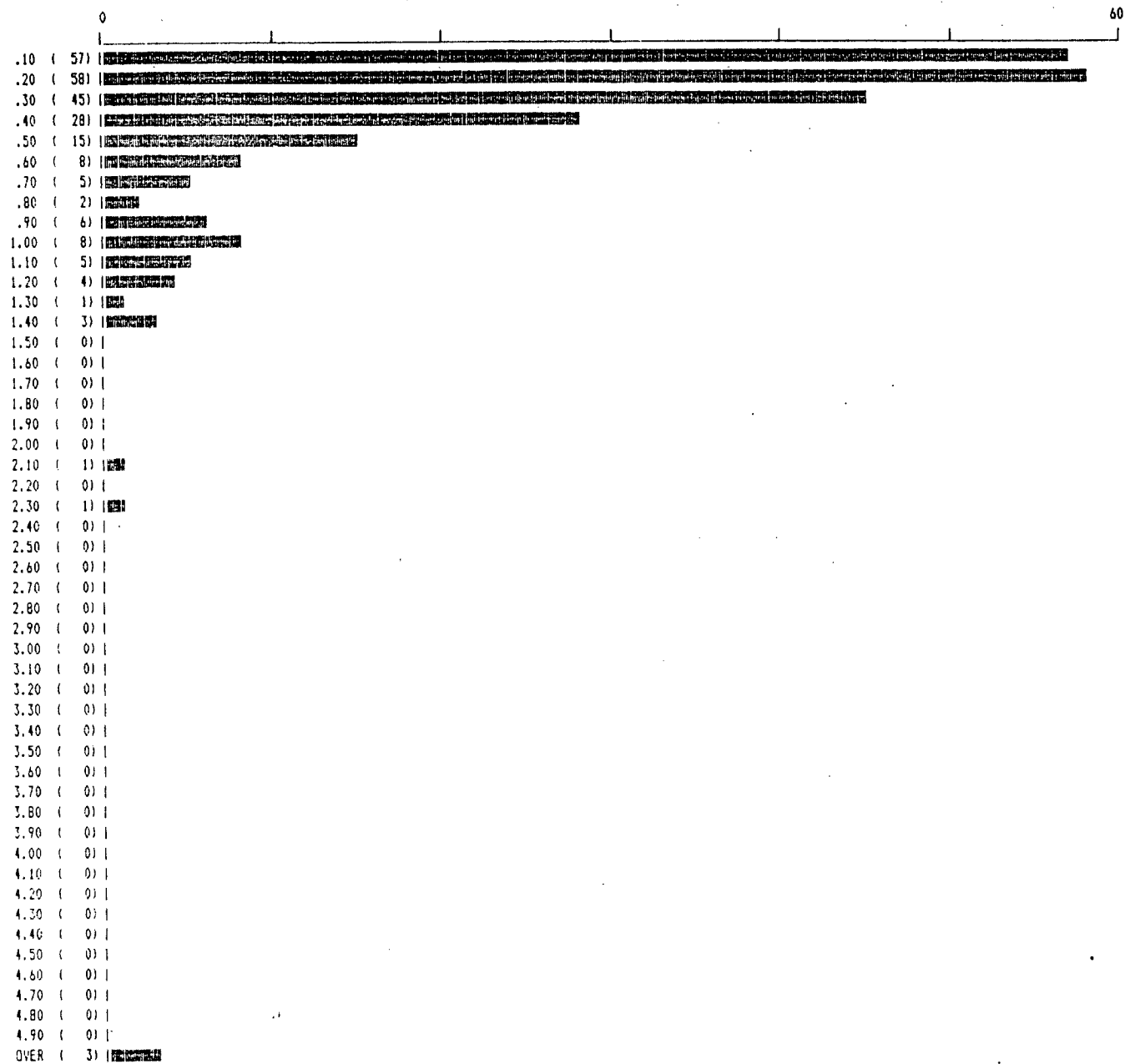
PAGE 3

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUX
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
HR-55	2	47	9	55	.2	10	12	573	3.81	41	2	ND	2	23	1	2	2	64	.35	.03	2	17	.71	51	.13	8	2.65	.02	.05	2	5
HR-56	2	51	11	54	.2	11	11	494	4.24	39	4	ND	2	21	1	2	2	65	.51	.04	3	19	.65	67	.12	10	2.43	.02	.05	2	5

IMPERIAL METALS PROJECT # MAC FILE # 84-1312

PAGE 4

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AUT PPB
TR-1	1	9	4	5	.4	1	1	44	1.51	20	2	ND	2	4	1	2	3	18	.03	.02	2	1	.13	29	.02	10	.56	.02	.17	2	5
TR-2	3	26	6	62	.1	7	6	559	4.35	177	2	ND	2	13	2	3	6	106	.51	.05	2	28	2.35	102	.25	6	2.83	.03	.08	2	5
TR-3	4	86	17	112	.6	10	16	731	5.16	372	4	ND	2	14	2	2	5	122	.90	.07	2	20	1.12	42	.24	11	2.42	.06	.15	2	50
TR-4	4	98	8	60	.3	11	17	460	4.53	91	2	ND	2	14	1	2	5	105	1.83	.06	2	21	1.02	20	.19	10	2.86	.06	.08	2	5
TR-5	4	7	28	88	1.0	6	9	791	1.69	45	4	ND	2	7	2	2	2	6	1.03	.03	2	1	.09	11	.01	5	.43	.01	.12	2	20
TR-6	8	11	31	242	2.2	7	9	1624	2.82	108	2	ND	2	33	2	2	2	9	5.76	.04	2	3	.15	18	.01	9	.64	.01	.15	2	25
TR-7	3	20	24	125	1.2	11	12	985	2.81	82	4	ND	2	8	2	2	2	14	.98	.04	3	3	.27	17	.01	6	.69	.01	.10	2	5
TR-8	3	95	43	996	.3	19	13	1608	3.71	34	2	ND	2	8	9	2	2	55	.79	.06	8	12	1.38	36	.01	8	2.28	.01	.16	3	5
TR-9	3	40	30	580	.8	15	14	1643	4.43	50	2	ND	2	9	5	5	3	63	.97	.06	12	14	1.57	42	.01	11	2.61	.01	.13	2	5
STD A-1/AU 0.5	2	30	39	186	.3	36	13	1019	2.79	9	2	ND	2	37	2	2	2	56	.62	.10	7	64	.63	255	.10	7	2.05	.02	.19	2	520



SAMPLE SIZE : 250 MAX : 32.4 MIN : .1 MEDIAN : .3
 MEAN : .57 S.D. : 2.18

Time	Count	Description
2.00	(10)	[REDACTED]
4.00	(10)	[REDACTED]
6.00	(3)	[REDACTED]
8.00	(11)	[REDACTED]
10.00	(15)	[REDACTED]
12.00	(16)	[REDACTED]
14.00	(16)	[REDACTED]
16.00	(15)	[REDACTED]
18.00	(22)	[REDACTED]
20.00	(14)	[REDACTED]
22.00	(21)	[REDACTED]
24.00	(16)	[REDACTED]
26.00	(12)	[REDACTED]
28.00	(10)	[REDACTED]
30.00	(8)	[REDACTED]
32.00	(5)	[REDACTED]
34.00	(2)	[REDACTED]
36.00	(5)	[REDACTED]
38.00	(6)	[REDACTED]
40.00	(5)	[REDACTED]
42.00	(1)	[REDACTED]
44.00	(4)	[REDACTED]
46.00	(2)	[REDACTED]
48.00	(2)	[REDACTED]
50.00	(2)	[REDACTED]
52.00	(3)	[REDACTED]
54.00	(1)	[REDACTED]
56.00	(1)	[REDACTED]
58.00	(4)	[REDACTED]
60.00	(1)	[REDACTED]
62.00	(0)	[REDACTED]
64.00	(0)	[REDACTED]
66.00	(1)	[REDACTED]
68.00	(1)	[REDACTED]
70.00	(1)	[REDACTED]
72.00	(1)	[REDACTED]
74.00	(0)	[REDACTED]
76.00	(0)	[REDACTED]
78.00	(0)	[REDACTED]
80.00	(1)	[REDACTED]
82.00	(0)	[REDACTED]
84.00	(1)	[REDACTED]
86.00	(0)	[REDACTED]
88.00	(0)	[REDACTED]
90.00	(0)	[REDACTED]
92.00	(0)	[REDACTED]
94.00	(1)	[REDACTED]
96.00	(0)	[REDACTED]
98.00	(0)	[REDACTED]
OVER	(0)	[REDACTED]

SAMPLE SIZE : 250 MAX : 94 MIN : 2 MEDIAN : 19
 MEAN : 22.51 S.D. : 15.6

0

300

5.00	(207)	
10.00	(16)	
15.00	(4)	
20.00	(1)	
25.00	(5)	
30.00	(0)	
35.00	(1)	
40.00	(2)	
45.00	(2)	
50.00	(0)	
55.00	(2)	
60.00	(1)	
65.00	(0)	
70.00	(0)	
75.00	(0)	
80.00	(2)	
85.00	(1)	
90.00	(0)	
95.00	(2)	
100.00	(0)	
105.00	(0)	
110.00	(0)	
115.00	(0)	
120.00	(0)	
125.00	(0)	
130.00	(0)	
135.00	(1)	
140.00	(0)	
145.00	(0)	
150.00	(0)	
155.00	(0)	
160.00	(0)	
165.00	(0)	
170.00	(0)	
175.00	(0)	
180.00	(0)	
185.00	(0)	
190.00	(0)	
195.00	(0)	
200.00	(0)	
205.00	(1)	
210.00	(0)	
215.00	(0)	
220.00	(0)	
225.00	(1)	
230.00	(0)	
235.00	(0)	
240.00	(0)	
245.00	(0)	
OVER	(1)	

SAMPLE SIZE : 250 MAX : 285 MIN : 5 MEDIAN : 5
 MEAN : 12.24 S.D. : 29.8

0

200

10.00	(147)	[REDACTED]
20.00	(51)	[REDACTED]
30.00	(18)	[REDACTED]
40.00	(11)	[REDACTED]
50.00	(4)	[REDACTED]
60.00	(4)	[REDACTED]
70.00	(3)	[REDACTED]
80.00	(2)	[REDACTED]
90.00	(1)	[REDACTED]
100.00	(1)	[REDACTED]
110.00	(2)	[REDACTED]
120.00	(0)	[REDACTED]
130.00	(1)	[REDACTED]
140.00	(0)	[REDACTED]
150.00	(0)	[REDACTED]
160.00	(1)	[REDACTED]
170.00	(0)	[REDACTED]
180.00	(0)	[REDACTED]
190.00	(0)	[REDACTED]
200.00	(1)	[REDACTED]
210.00	(0)	[REDACTED]
220.00	(0)	[REDACTED]
230.00	(0)	[REDACTED]
240.00	(0)	[REDACTED]
250.00	(0)	[REDACTED]
260.00	(0)	[REDACTED]
270.00	(0)	[REDACTED]
280.00	(0)	[REDACTED]
290.00	(0)	[REDACTED]
300.00	(0)	[REDACTED]
310.00	(0)	[REDACTED]
320.00	(0)	[REDACTED]
330.00	(0)	[REDACTED]
340.00	(0)	[REDACTED]
350.00	(0)	[REDACTED]
360.00	(0)	[REDACTED]
370.00	(0)	[REDACTED]
380.00	(0)	[REDACTED]
390.00	(0)	[REDACTED]
400.00	(0)	[REDACTED]
410.00	(0)	[REDACTED]
420.00	(0)	[REDACTED]
430.00	(1)	[REDACTED]
440.00	(0)	[REDACTED]
450.00	(0)	[REDACTED]
460.00	(0)	[REDACTED]
470.00	(0)	[REDACTED]
480.00	(0)	[REDACTED]
490.00	(0)	[REDACTED]
OVER	(2)	[REDACTED]

SAMPLE SIZE : 250 MAX : 910 MIN : 1 MEDIAN : 9
MEAN : 23.9 S.D. : 76.37



.10	(57)	
.20	(58)	
.30	(45)	
.40	(28)	
.50	(15)	
.60	(8)	
.70	(5)	
.80	(2)	
.90	(6)	
1.00	(8)	
1.10	(5)	
1.20	(4)	
1.30	(1)	
1.40	(3)	
1.50	(0)	
1.60	(0)	
1.70	(0)	
1.80	(0)	
1.90	(0)	
2.00	(0)	
2.10	(1)	
2.20	(0)	
2.30	(1)	
2.40	(0)	
2.50	(0)	
2.60	(0)	
2.70	(0)	
2.80	(0)	
2.90	(0)	
3.00	(0)	
3.10	(0)	
3.20	(0)	
3.30	(0)	
3.40	(0)	
3.50	(0)	
3.60	(0)	
3.70	(0)	
3.80	(0)	
3.90	(0)	
4.00	(0)	
4.10	(0)	
4.20	(0)	
4.30	(0)	
4.40	(0)	
4.50	(0)	
4.60	(0)	
4.70	(0)	
4.80	(0)	
4.90	(0)	
OVER	(3)	

SAMPLE SIZE : 250 MAX : 32.4 MIN : .1 MEDIAN : .3
 MEAN : .57 S.D. : 2.18

0

30

2.00	(10)	
4.00	(10)	
6.00	(3)	
8.00	(11)	
10.00	(15)	
12.00	(16)	
14.00	(16)	
16.00	(15)	
18.00	(22)	
20.00	(14)	
22.00	(21)	
24.00	(16)	
26.00	(12)	
28.00	(10)	
30.00	(8)	
32.00	(5)	
34.00	(2)	
36.00	(5)	
38.00	(6)	
40.00	(5)	
42.00	(1)	
44.00	(4)	
46.00	(2)	
48.00	(2)	
50.00	(2)	
52.00	(3)	
54.00	(1)	
56.00	(1)	
58.00	(4)	
60.00	(1)	
62.00	(0)	
64.00	(0)	
66.00	(1)	
68.00	(1)	
70.00	(1)	
72.00	(1)	
74.00	(0)	
76.00	(0)	
78.00	(0)	
80.00	(1)	
82.00	(0)	
84.00	(1)	
86.00	(0)	
88.00	(0)	
90.00	(0)	
92.00	(0)	
94.00	(1)	
96.00	(0)	
98.00	(0)	
OVER	(0)	

SAMPLE SIZE : 250 MAX : 94 MIN : 2 MEDIAN : 19
 MEAN : 22.51 S.D. : 15.6



5.00	(207)	
10.00	(16)	
15.00	(4)	
20.00	(1)	
25.00	(5)	
30.00	(0)	
35.00	(1)	
40.00	(2)	
45.00	(2)	
50.00	(0)	
55.00	(2)	
60.00	(1)	
65.00	(0)	
70.00	(0)	
75.00	(0)	
80.00	(2)	
85.00	(1)	
90.00	(0)	
95.00	(2)	
100.00	(0)	
105.00	(0)	
110.00	(0)	
115.00	(0)	
120.00	(0)	
125.00	(0)	
130.00	(0)	
135.00	(1)	
140.00	(0)	
145.00	(0)	
150.00	(0)	
155.00	(0)	
160.00	(0)	
165.00	(0)	
170.00	(0)	
175.00	(0)	
180.00	(0)	
185.00	(0)	
190.00	(0)	
195.00	(0)	
200.00	(0)	
205.00	(1)	
210.00	(0)	
215.00	(0)	
220.00	(0)	
225.00	(1)	
230.00	(0)	
235.00	(0)	
240.00	(0)	
245.00	(0)	
OVER	(1)	

SAMPLE SIZE : 250 MAX : 285 MIN : 5 MEDIAN : 5
 MEAN : 12.24 S.D. : 29.8

IMPERIAL METALS PROJECT # MAC FILE # 84-1281 & 84-1312

PB (PPM)

PROJECT # MAC FILE # 84-1281 & 1312

PB (PPM)

PROJECT # MAC FILE # 84-1281 & 1312

PB (PPM)

02W

01W

00

01E

02E

03E

04E

05E

06E

07E

01N

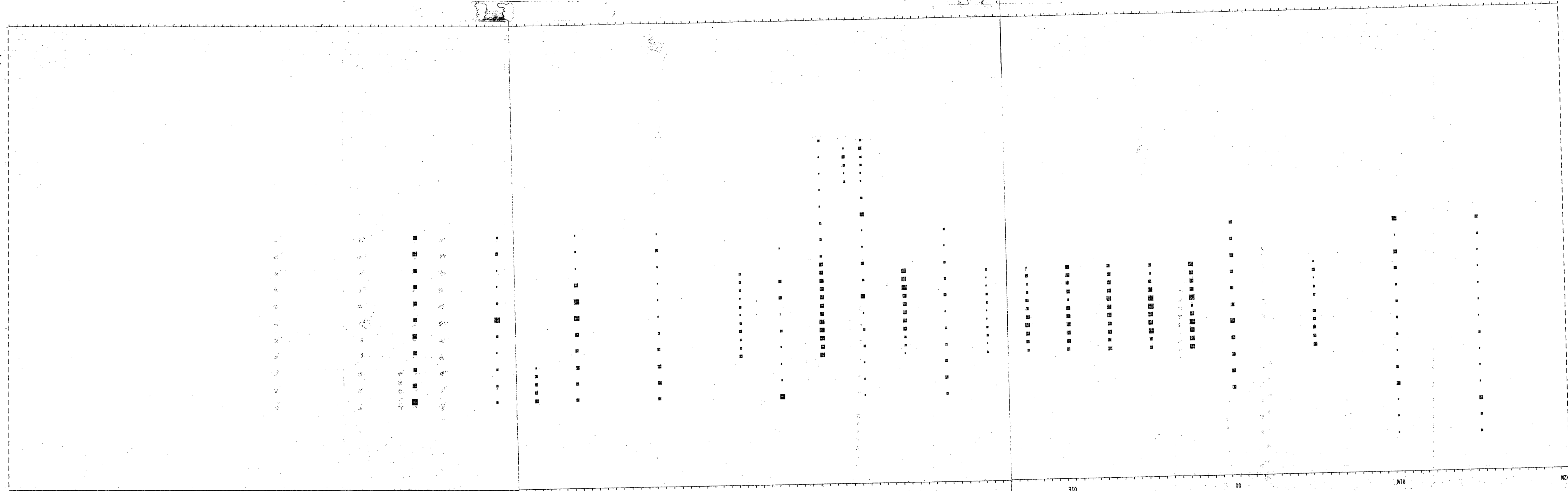
00

01S

OVER 91 34 17 10 5 UNDER

12,422
Pg 6

OVER 1.3
0.9
0.4
0.3
0.2
UNDER



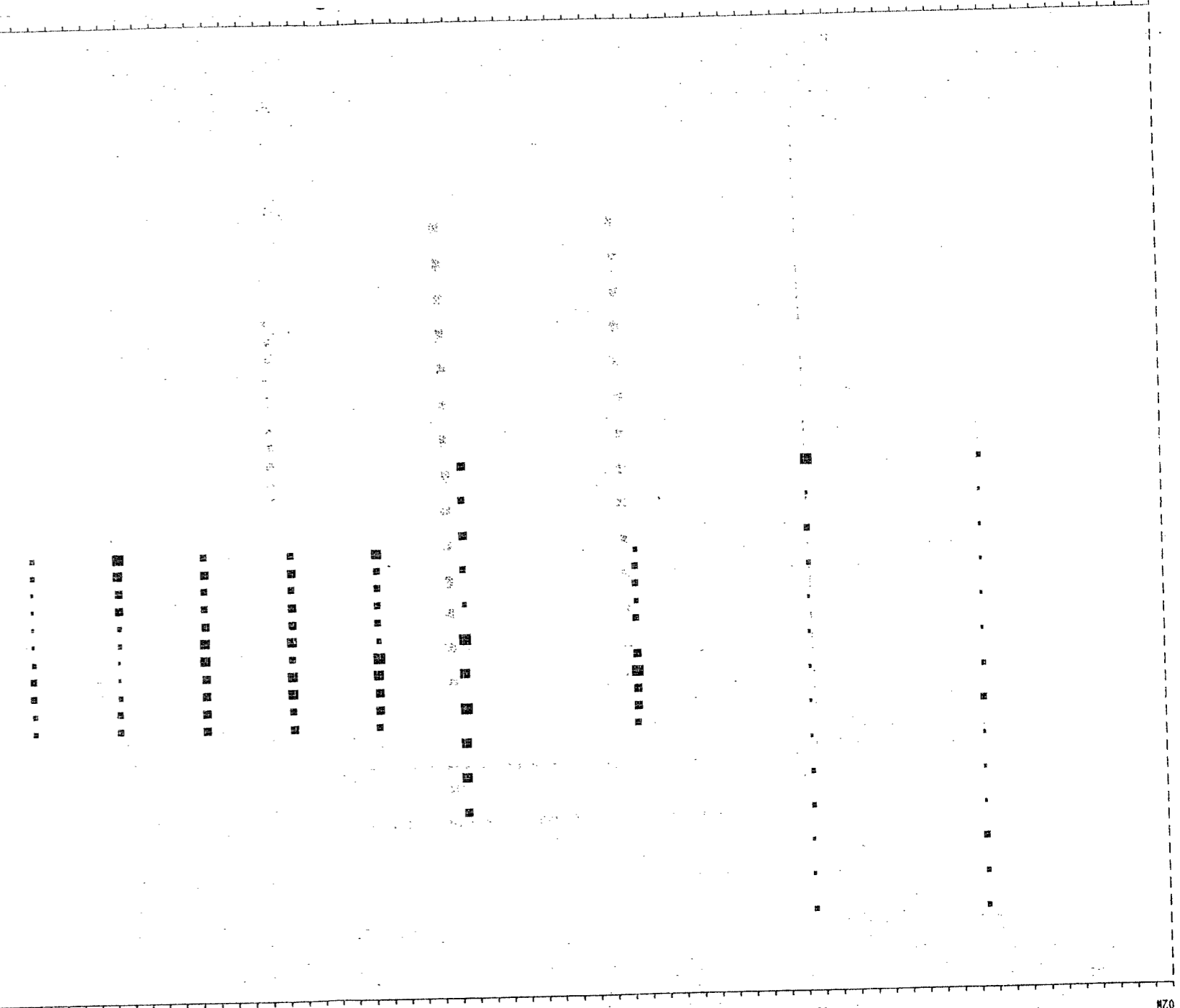
02H
IMPERIAL METALS PROJECT # MAC FILE # 84-1281 & 1312
01H
00
AG (PFM)
01E

PROJECT # MAC FILE # 84-1281 & 84-1312
02E
AG (PFM)
04E
03E

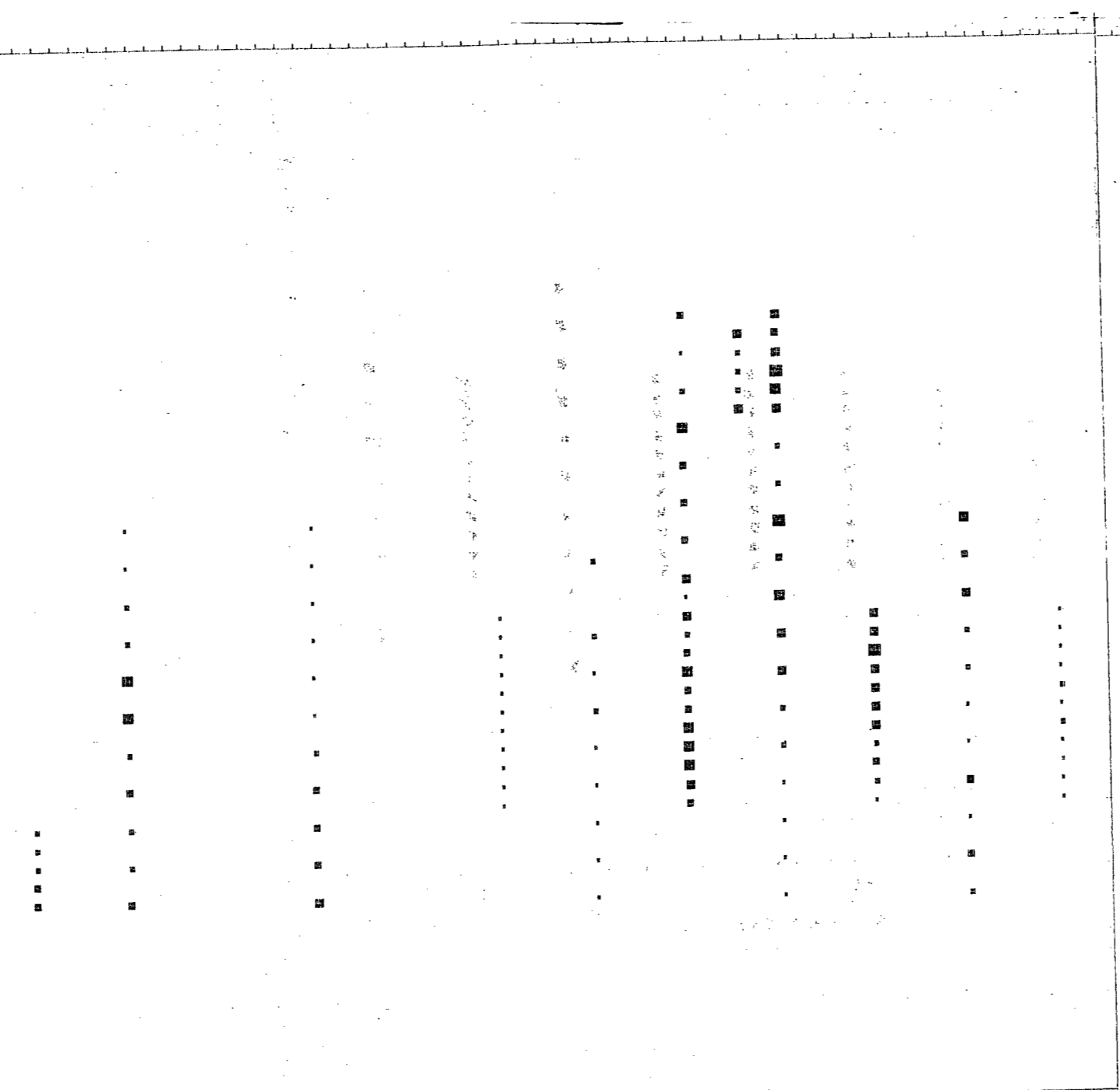
PROJECT # MAC FILE # 84-1281 & 84-1312
05E
AG (PFM)
06E
07E

12,422
7

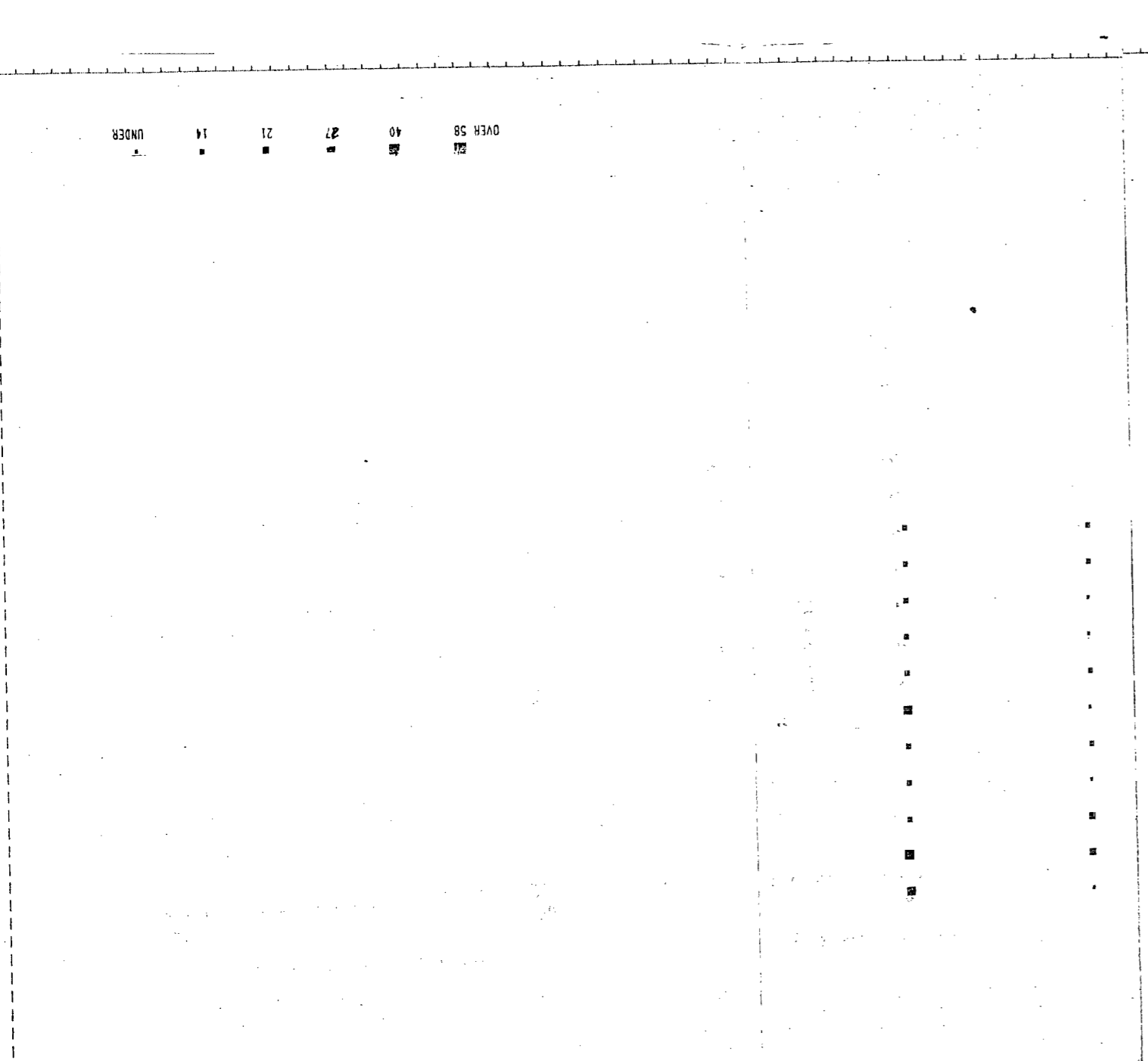
510
00
10IN
02N



IMPERIAL METALS PROJECT # MAC FILE # 84-1281 & 1312
 01N
 00
 AS (PFM)
 01E



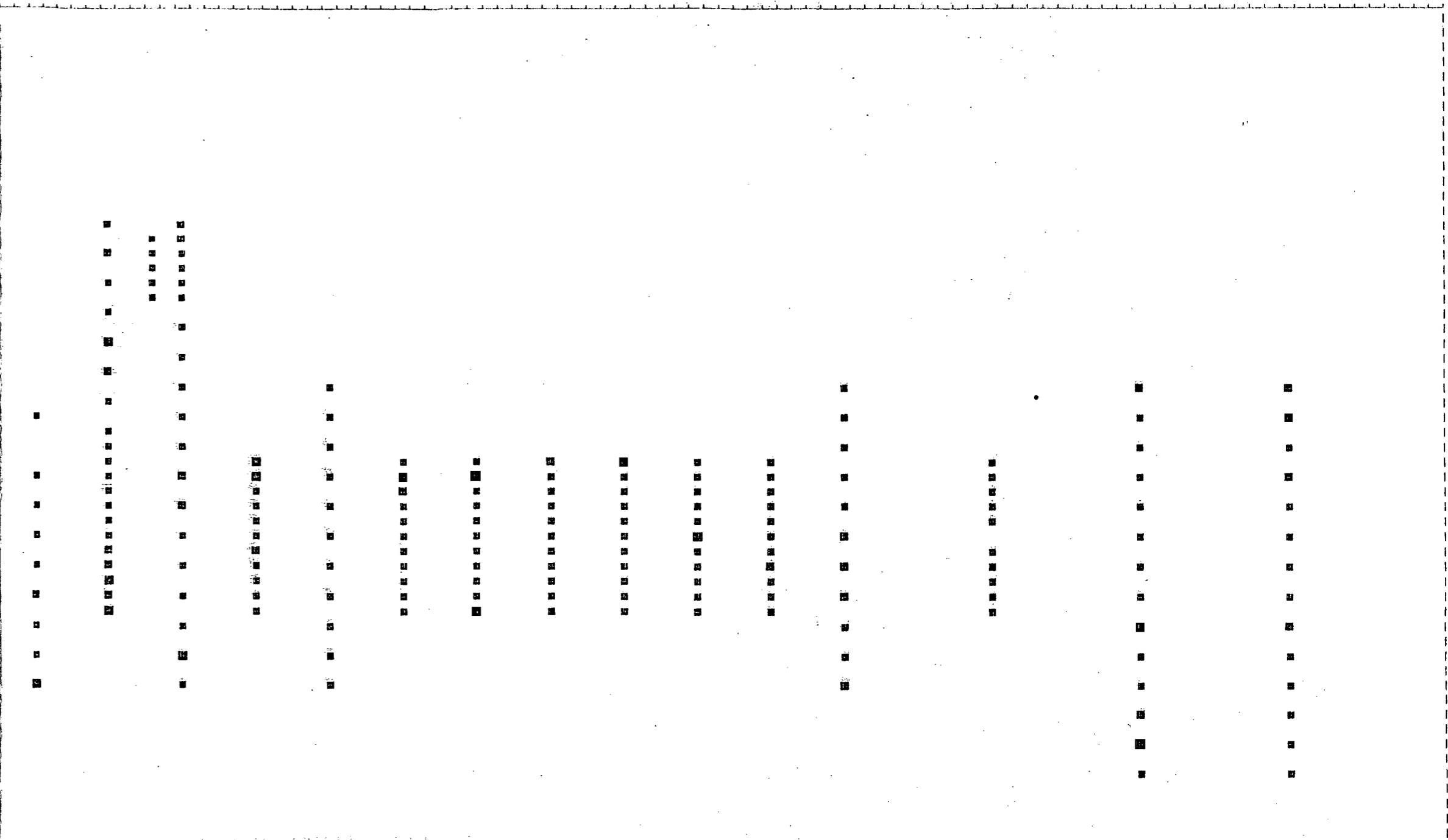
PROJECT # MAC FILE # 84-1281 & 84-1312
 02E
 03E
 04E
 AS (PFM)



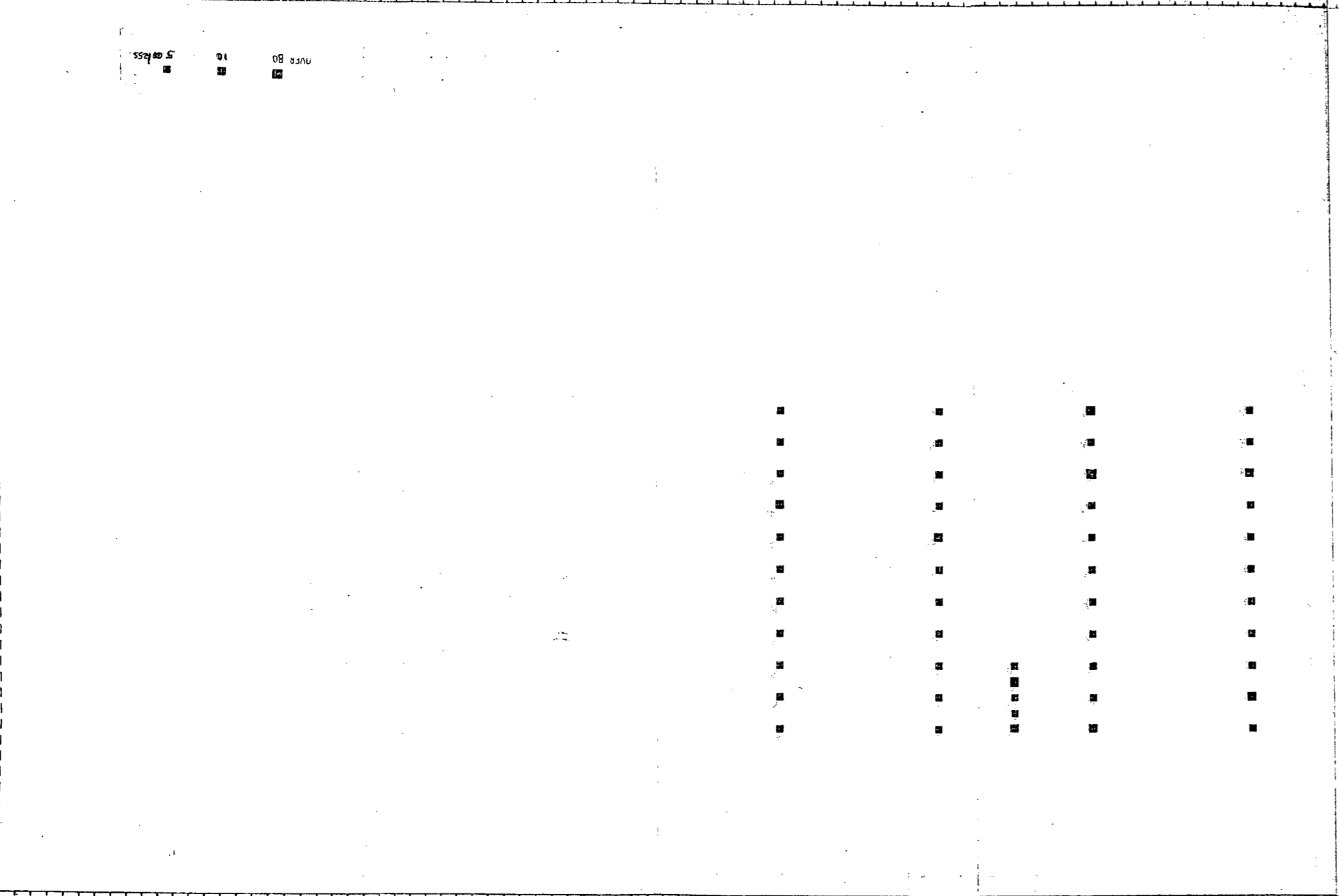
PROJECT # MAC FILE # 84-1281 & 84-1312
 05E
 06E
 AS (PFM)
 07E

22
 40
 27
 21
 14
 UNDER

12,422
 8



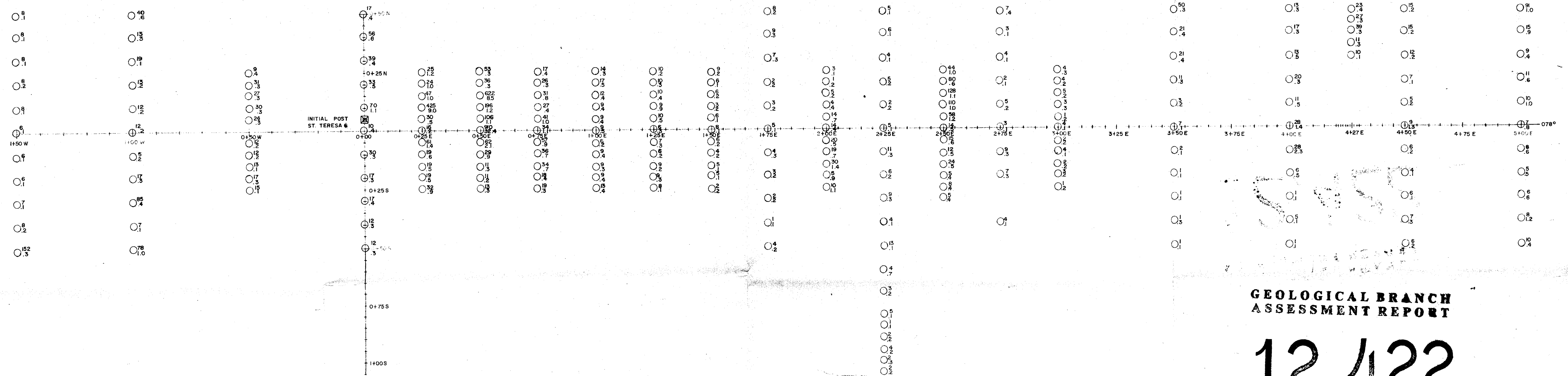
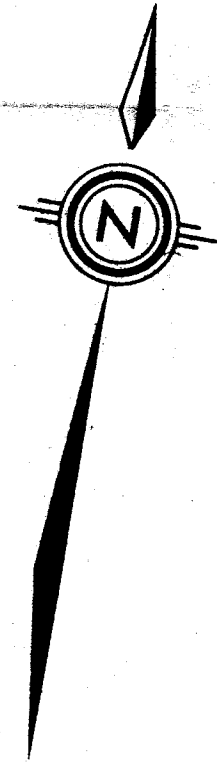
IMPERIAL METALS PROJECT # MAC FILE # 84-1281 & 1312
 AU* (FPB)
 PROJECT # MAC FILE # 84-1281 & 84-1312



AU* (FPB)
 PROJECT # MAC FILE # 84-1281 & 84-1312
 AU* (FPB)

020 010 515

9 12,422



**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

12,422

IMPERIAL METALS CORPORATION

MAC

**SOIL GRID "A"
LEAD & SILVER**

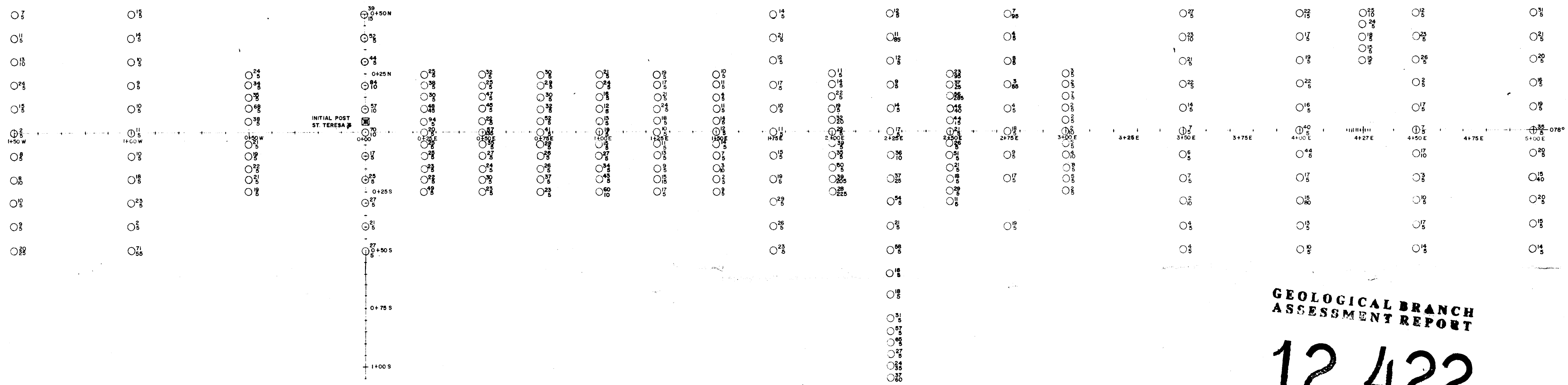
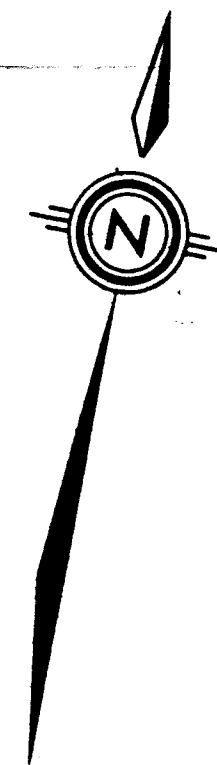
Pb ppm.
Ag ppm.



Page 10

DATE	JULY 1984	GEOLOGIST	W. MORTON
DRAWN BY	M. FERGUSON		

From -80 mesh Fraction



**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

12,422

IMPERIAL METALS CORPORATION

MAC

SOIL GRID "A"

ARSENIC & GOLD

As ppm
Au ppb



Page 11

SCALE	1:500	GEOLOGIST	W. WORTON
DATE	JULY 1984	DRAWN BY	M. FERGUSON

From - 80 Mesh Fraction