84-1139-12947



# PLACER DEVELOPMENT LIMITED

#### GEOLOGIAL, GEOCHEMICAL AND GEOPHYSICAL REPORT

#### REN CLAIM GROUP

#### KAMLOOPS MINING DIVISION

### N.T.S. 921/15W 50°48'N, 120°52'W

Owner & Operator: Placer Development Ltd.

Work Performed:

26 April to 11 May and 29 and 30 September, 1984

Authors: R.A. Boyce R.W. Cannon, P. Eng.

21 November 1984

# GEOLOGICAL BRANCH

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#### 1. Introduction

Work performed on the Ren mineral claims in April and May of 1984 included geochemistry, geophysics, mapping and prospecting; principally on a grid covering the western two-thirds of the claims. Follow-up work in September included geochemistry and prospecting. Results were not encouraging. Further work is not contemplated at the present time.

The Ren property is located on the north shore of the west end of Kamloops Lake, in south-central B.C. The centre of the claims lies 40 kilometres west-northwest of Kamloops. Access to the southern edge of the claim block is provided by Trans-Canada Highway and C.N.R. mainline. Various dirt roads give good access to much of the claims area. A more detailed treatment of history and physical features may be found in the previous assessment report (#84-140-12057).

The Ren claims were located by Placer Development Ltd. in February 1983. The property includes six claims, totalling 80 units. It is bounded by other claims on the east and north, and Deadman Creek Indian Reserve on the west.

#### Regional Geology

The oldest rocks around the west end of Kamloops Lake are part of Upper Triassic Nicola Group. It is composed of basaltic fragmental rocks, flows, and minor associated sediments; generally younger toward the east. Triassic to Jurassic ultramafic rocks are exposed in Carabine Creek area. These are tentatively correlated with Iron Mask Batholith. These units are unconformably overlain by dominantly coarse clastic sediments of lower to Middle Jurassic Ashcroft Formation. The Eocene Kamloops Group is widespread in the area. It is dominantly basalts, with local more felsic volcanics and basal sediments. Mator northwest-trending faults were active during and after deposition of Kamloops Group strata. They were formed both from right-lateral transform and crustal extension movements. The result is a stepped horst-and-graben structure. Small Miocene intermediate intrusive bodies are mapped adjacent to these faults, especially within Ashcroft Formation. Northward, isolated remnants of Mio-Pliocene plateau basalts are exposed on ridgetops.

Numerous mineral occurrences have been recorded in the Kamloops Lake area. Placer gold deposits in Deadman River and Criss Creek were worked in the late 1800's. Several mercury occurrences, near Kamloops Lake and Criss Creek, were known since the 1930's. Some witnessed minor production. Minor copper showings are also known. Much work was done in the 1960's and 1970's in search for porphyry copper deposits similar to those related to Guichon and Iron Mask Batholiths.







REN CLAIMS

GRID LOCATION

### 3. Property Geology

Outcrop is common in most parts of the property. However, most outcrops are small, with the exception of the bluffs in the central and south-central part of the property. Hence, overburden covers 90% of the property, to an unknown depth. Fragments in soil contain local bedrock types, both rounded and angular; as well as locally common, rounded granitic rocks.

All bedrock encountered was assigned to Nicola Group. Grey shale and sandstone and interbedded tuff were found only in the northern third of the claims, mostly on higher ground. Clasts were largely volcanic origin. One outcrop contained conglomerate. Both conglomerate and limestone were noted in float.

Volcanic rock types encountered were dark green to maroon tuff, flows and agglomerate. Composition is basalt to andesite. Agglomerate is common in lowest slopes, but rare elsewhere. Flow rocks are frequently porphyritic but rarely amygdaloidal. Brecciation is locally common, and in some cases, especially when altered, makes the rock indistinguishable from agglomerate. Pyrite was the only sulphide noted. It generally occurs as disseminations or discrete crystals. Limonitization on weathered surfaces is common, but intense only near altered zones. Malachite and azurite were seen in two places.

No evidence was seen of Kamloops Group cap rocks or Tertiary intrusives.

Topography is largely structure-controlled. The large gully in the west is believed to be a fault trace, parallel to Deadman River Fault. Two smaller, parallel features are recognized in the northern part of the claims. A secondary set of fractures, striking approximately 125° is evident in the southeast. A third set runs about 050°.

Bedding was noted in sediment, most often dipping gently northward. Small-scale folding was seen in a few places. Jointing showed numerous attitudes, but the commonest strike is parallel to the secondary fracture set, dipping variably northeastward.

Carbonate veining is widespread on the property, usually occurring as thin calcite veinlets, stockworks, or fracture or breccia fillings. Quartz veining is less common, and often associated with silicification and epidote. Carbonate with quartz and/or chalcedony, or multi-stage quartz veining was rarely seen. They are most commonly associated with pervasive carbonate alteration. This alteration is linear to irregular in shape, and shear-related. It is usually about a metre wide, but varies from 2 centimetres to 7 metres. Composition is mainly ankerite, and limonitization of country rock is associated. Color is orange-brown to orange-pink and less often pale brown or off-white. Orientations vary, but the commonest noted were 100/steep, 100/gentle N, and 030/moderate SE. This alteration is believed indicative of epithermal activity. Mercury showings, dating from the 1930's (Davis showings) are located near the southeast margin of the claims. They are evident due to the bright-coloured carbonate alteration. A few small, hand-cut trenches and pits were found. Most alteration zones are low-angle or 100/90. No cinnabar was recognized.

Geology is plotted at a scale of 1:20,000 on Figure 2.

#### Geophysical Surveys

A magnetometer and a VLF-EM survey were run on the property grid. The purpose was to delineate structure and alteration pattern. A separate report may be found in Appendix A.

#### 5. Geochemical Sampling

All geochemical sample sites were located with reference to a grid set out by chain and compass. A 5200-metre base line was oriented at 345°, and perpendicular lines were set 400 metres apart. Grid location is shown on Figure 13.

Soil samples were collected 50 metres apart on lines, on the baseline, and on a parallel tie-line. Follow-up work included short, tight-spaced sampling near alteration zones. A base-of-slope contour line was also sampled at 30 meter spacing, in the southwest corner of the claims.

Soils in the area are dominantly immature regosols. They are alkaline and carbonate-rich, with caliche often seen as white to cream-coloured coatings on coarse particles. The principal parent material is glacial till, with considerable local colluvial movement on moderate to steep slopes which characterize much of the property. Soils developed on talus and bedrock were often encountered in the southeastern quarter of the grid, and locally elsewhere. Glaciofluvial silt, sand and gravel were observed in a few localities, notably along the southern claim boundary. A few, small meadows in upland depressions are underlain by lacustrine clay and silt.

About 500 grams of B1 or BC horizon was collected for each soil sample. Most samples were taken 15 to 20 centimetres deep. They were stored in kraft paper bags. A total of 787 samples was taken.

Rock samples were collected from outcrops encountered near grid lines, especially where altered. A few other samples were taken from traverses in the eastern and south western parts of the claims. Samples included 1 or 2 kilograms of chips collected in a plastic bag. 115 samples were collected.

Four bulk sediment samples were taken in the eastern area to test drainages not previously sampled. This was not successful, due to poor sample sites. Flowing water was found, but the sediment consisted mainly of organic-rich silt and clay. Bulk samples were taken by digging a hole vertically through the sediment profile, and running the material through a -20 mesh screen. The sediment collected in a pan was washed into a plastic bag. About 3 kilograms was taken.

Conventional sediment samples were collected from dry sediment in the major southeast-running gully. The intent was to subdivide the valley upstream from the anomalous heavy mineral sample.

All samples were taken to Placer Development Ltd. Research Centre Laboratory in Vancouver, for treatment and analysis. Soils from spring sampling were oven-dried and initially sieved to -10+80 mesh and -80 mesh. The coarse fraction was saved, and the fine analyzed. Fall samples were sieved to -80 only. Bulk sediment and conventional sediment was sieved to -80 mesh. Rock samples were pulverized. All samples were run for Cu, Zn, Pb, Ag, Au, As, Sb and Hg. Rocks from spring sampling and bulk sediments were also checked for Mo, and all rocks for Ba. Later, approximately one-third of soils had their coarse fraction pulverized and analyzed for Au content. Analytical procedures are listed in Appendix B.

#### 6. Analytical Results

Results were generally disappointing, with few elevated values in any metal except Hg. No Au was detected in rock samples. Only the area around the old showings displayed clusters of dectectable As and Sb. Analytical results are listed in Appendix C.

Simple statistics was applied to several elements in rock and soil to establish background and anomalous levels. Results are contained in Appendix D. Anomalous values were plotted to reveal patterns. Figures 6 through 19 show results on the grid plan at a scale of 1:10,000. Ag and Sb in soil were not plotted as the former had only one, and the later had no detectable values. Nor was coarse fraction Au, which showed only one detectable value. Similarliy in rock, only 3 As, one Sb and no Au analysis were above detection limit. Mo were all very low. Hence these four were not plotted. Bulk and conventional sediment sample analyses are plotted for Cu, Zn, Pb, and Hg in Figure 20. Values for Mo, Ag, Au, As and Sb are all at or below detection limit, so not plotted. Cu in soil highs are spotty, but strongly clustered in the northwest corner of the grid, and along the southern boundary. Zn in soil anomalies occur around the edges of sedimentary outcrop areas. Soil Hg highs are spotty, but weakly outline northwest and northeast-trend structures. As in soil shows a distinct linear pattern along the northern baseline, but otherwise is weak and scattered. Au shows only 5 soil values greater than detection limit. The highest is 1.2 ppm, and one is in the coarse fraction.

Cu in rock shows broad highs around all four corners of the grid. Zn in rock reveals a diffuse pattern, generally lower on the southwest. Pb in rock response was quite weak, but distinctly higher near the southern edge. Rock Hg shows sharp anomalies in the southeast (near old showings) and southwest corners, and a weaker high in the center grid centre. Ba was also weak, but locally higher north of the centre. Ag was weak and scattered, but possibly associated with northwest-trending structures.

Results from both bulk sediment and conventional sediment samples are all low, with the exception of moderate -level Hg.

The most promising area appears to be the southwest corner of the claims. Here there are coincident Au, Cu and Hg anomalies, common carbonate alteration, and quartz-carbonate veining. However, follow-up contour soil sampling reveals only one high As, and a few weak Hg highs. Also interesting is the area of Hg showings in the southeast. It hosts carbonate alteration, and the highest Hg, As and Sb on the property. Another possible area of interest is the north end of the baseline, which shows a linear As pattern. Most of this area is covered in till.

#### 7. Conclusions

Geochemical work has failed to delineate a source area for metal concentrations reported in heavy mineral samples. Anomalies are generally weak and scattered. No vertical zoning, as expected in an epithermal gold deposit, is evident. Distinct carbonate alteration zones, locally with quartz and chalcedony veins, generally fail to host high metal values other than Hg. No sulphide minerals were seen, except pyrite. The conclusion is made that soil geochemistry is unlikely to find precious metal indications.

The value of heavy mineral sample analyses may be called into question by these results. Soil, rock and sediment sampling has failed to support high values received from heavy minerals despite some replicated values. It is possible that the technique is too sensitive for interpretation of anomaly significance in this environment. Geophysical surveys have failed to identify targets for future work. A different orientation of survey lines would likely have better revealed the southeasterly-oriented fracture system. However, this might not produce any new information.

The possibility exists of precious metals deposits underlying the three areas noted above. Evaluation of these areas would require close-spaced outcrop sampling, mapping, basal till sampling in covered areas, and possibly drilling.

#### 8. Recommendation

It is recommended that no further work be done at this time due to discouraging results and high risk of next stage work.

R.A. Byen

R.A. Boyce

RAB/cs 11:13:84 Attachment

#### 9. References

B.C. Dept. of Mines and Petroleum Resources, Assessment Reports

#82 - 146 - 10223, R.A. Boyce, Xavona claim #84 - 140 - 12054, R.A. Boyce, Xavona claims #84 - 140 - 12057, R.A. Boyce, Ren claims

Canada Dept. of Mines and Resources - Map 886A - Geology, Nicola Map 887A - Mineral Localities, Nicola

Cockfield, W.E., 1948, <u>Geology and Mineral Deposits of Nicola Map</u> - Area, B.C., Geological Survey of Canada, Memoir 249.

Ewing, T.E., 1981 <u>Regional Stratigraphy and Structural Setting of</u> <u>Kamloops Group, South-Central B.C.</u>, C.J.E.S. v.18, No. 9, pp. 1464-1477.

Geological Survey of Canada, 1984, <u>Bedrock Geology of Ashcroft</u> (921) Map Area, Open File 980.

Stevensen, J.S., 1940. <u>Mercury Deposits of British Columbia</u>, B.C. Dept. of Mines, Bulletin 5.

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10. Summary of Expenditures

# <u>Salaries:</u> <u>Field Work</u>:

R.A. Boyce, 14 1/2 days @ \$250. = R.W. Cannon, 5 days @ \$325 B.S. Ott, 5 days @ \$280 P. Pacor, 13 days @\$250 R.H. Pinsent, 1 1/2 days @\$350	\$ 3,625 1,625 1,400 3,250 525	
Office Work		
R.A. Boyce, 10 1/2 days @\$250 R.W. Cannon, 1 day @ \$325 M.T. Chan, 1/2 day @\$150 B.S. Ott, 1/2 day @\$280 P. Pacor, 1 day @\$250 I. Thomson, 1/2 day @ \$370	\$ 2,625 325 75 140 250 <u>185</u> \$14,025	\$14,025.00
Accommodation: Sage Brush Motel, Kamloops Meals: Groceries and supplies:		557.48 1,097.49 259.90
Geochemistry: 787 soils prep & analysis for Cu, Zn, Pb, Au, As, Sb, Hg @ \$22.35 =	Ag \$17,589.45	
302 soils prep. & analysis for Au (coarse fraction)@ \$8.00 -	2,416.00	
115 rocks prep. & analysis for Mo, Cu, Zn, Pb, Ag, Au As, Sb, Hg, Ba @ \$25.00	2,875.00	
4 bulk sediment prep & analysis for Cu, Zn, Pb, Ag, Au, As, Sb, Hg @ \$27.50	110.00	
8 sediment prep & analysis for Cu, Zn, Pb, Ag, Au, As, Sb, Hg @ \$22.35	178.80 \$23,169,25	\$23,169.25
Vehicles: Fuel 506. Operating expense $35/day \ge 20$ $\frac{700}{51,206}$	00 00 00	\$ 1,206,00

- 10 -			
Equipment Rental			
Geonics EM-16 VLF unit @ \$200/week	Ş	200.00	
Geometrics G-856 Proton Magnetometer \$750/2 week min.		750.00	
Scintrex MBS-2 Magnetic Base Station \$750/2 week min.	-	750.00	\$ 1,700.00
Report Preparation:			
Typing, draughting, duplicating, computer printout			1,050.00
TOTAL application for assessment credit on Ren Claims:			\$42,805.22

#### 11. Statement of Qualifications

I, R.A. Boyce, with business adress at Box 49330, Bentall Postal Station, Vancouver, B.C., V7X 1P1, do hereby certify that:

- I have personally supervised the field work, and have assessed and interpreted the data from this exploration program on the Ren claims, Kamloops Mining Division.
- I am a graduate of the University of British Columbia, Vancouver (B.Sc., Geological Sciences, 1977).
- 3. I am a member of the Canadian Institute of Mining and Metallurgy.
- I have engaged in the full-time practice of mineral exploration since graduation, in the Provinces of British Columbia and Saskatchewan, and Yukon and Northwest Territories.

Respectfully submitted,

PLACER DEVELOPMENT LIMITED

R.A. Bayer

R.A. Boyce

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#### APPENDIX A

#### Geophysical Surveys

A total of 35.2 line-kolometres of magnetometer and V.L.F.-E.M. surveys were conducted with readings taken every 25 meters along lines 400 meters apart.

#### Equipment Used

The magnetometer survey was conducted using a Geometrics G-856 Portable Proton Magnetometer. Instrument drift and diurnal corrections were made by use of the Scintrex MBS-2 Total Field Magnetic Base Station. The V.L.F.-E.M. Survey was conducted using a Geonics E.M.-16 and employing the Seattle transmitting station for the east-west lines and the Annapolis station for the north-south lines.

#### Results of the Geophysical Surveys

The corrected magnetometer readings were plotted as stacked profiles on a plan map at a scale of 1:10000 (see Fig. 3). The E.M.-16 results were presented as stacked In-phase and Quadrature profiles (Fig. 4) and as stacked Fraser-Filter profiles (Fig. 5) both at a scale of 1:10000. The E.M. -16 profiles were plotted as if the operator was facing east or north along the line and therefore, proper crossovers are from west to east and south to north. The Fraser filtered data was calculated by the method put forth by D.C. Fraser (1969, <u>Contouring of VLF-EM data</u>: Geophysics, v.34, p. 958-967). Principle conductor axes have been superimposed on the VLF profile plan.

#### Discussion of Results

#### Magnetometer Survey

The magnetometer survey revealed the area to be underlain by magnetic volcanic rocks south of line 20S. North of, and including 20S the magnetic results are quite flat and correspond to sedimentary rocks. In this area, there is some magnetic relief along and near the base line from 8S to 16S inclusive which is most likely due to a small section of volcanic rocks.

Two subtle magnetic lows, which correlate with major gullies in the area, may be due to alteration along the faults which controlled the formation of these gullies.

### VLF-EM Survey

Numerous northerly trending VLF conductors were detected. The more prominent of these correspond to known topographic linears and are most likely due to conductive faults.

R. W. Cannon P. Eng.

R.W. Cannon, P. Eng.

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F	ACER	DE	VELOP	MENT	LTD	( P E S	EARCH CENTRE)	(
~	GEOCHEMIC	AL DAT	A LISTING	: Carabine	soils			DATE: 84
	AREA:	lab da	ta file: CARAB	P40	240			
7	VENTURE GEOLOGI	T NO: ST:	92115 182 R. BO	NCE				
	LAB PRO	JECT N	0: 4040	TRUTE DESUI	TS TO.	P. DOVCE	S TENNANT B HONCOON	
	NE ANNO	AU2	ARE RESU	LTS FOR THE	COARSE	I. THOMSON SAMPLES AS	R. SHKLANKA REQUESTED.	
	STANDAR ALL RES	D ANAL	YSIS METH	AS INDICATE	PDL GE	OCHEM LAP A	RE LISTED BELOW: BELOW	
	REMARKS	: INT	ERNAL LAB	STANDARDS	HAVE BE	EN INCLUDED	FOR REFERENCE.	
	UNIT	SAM	ATTACK U	RS FOLLOWED	BY * A	RE DUPLICAT	E ANALYSES.	3
	MO PPM CU PPM	0.5	C HCL04/	HN03 HN03	4HRS 4HRS	1-1000	ATOMIC ABSORPTION	
	ZN PPM PE PPM	0.5	C HCL04/	HNO3 HNO3	4HRS 4HRS	2-3000	ATOMIC ABSORPTION A.A. BACKGROUND COR.	
ALU	CD PPM NI PPM	0.5	C HCL04/	HN03 HN03	4HRS 4HRS	C.2-200 2-2000	A.A. BACKGROUND COR. ATOMIC ABSORPTION	
NOTO NOTO	CO PPM AG1 PPM	0.5	C HCL04/	HN03 HN03	4HRS 4HRS	2-2000	ATOMIC ABSORPTION	
4	AU PPM U PPM	10.0	AQUA REG. DIL HN03	I A	3485 2465	0.02-2.00	A.A. SOLVENT EXTRACT. FLOURIMETRY SOLV. FX.	1
El .	V PPM W PPM	1.0	C HE/HCL	04/HN03/HCL 3/HCL/H2S04	6HRS 4HRS	5-1000	ATOMIC ABSORPTION A.A. SOLVENT EXTRACT.	
	AS PPM	0.25	NA2CO3/KI	NO3 FUSION	3CMIN 4HRS	40-4000	SPECIFIC ION ELECTODE	
	SE PPM BI PPM	0.5	C HCL04/1	HN03	4HRS 4HRS	2-1000	A.A. BACKGROUND COR.	
	MN PPM FF X	8.5	C HCLO4/H	INO3	4HRS	2-3000	ATOMIC ABSORPTION	
	HG PPP	0.25	DIL HNOS	HCL	ZHRS	5-2000PPB	A.A. COLD VAPOR GEN.	
1	NA 3	6.5	C HE/HCL	4/HN03/HCL	CHRS	0.2 -202	ATOMIC ABSORPTION	
	CA Z	0.5	C HE/HCL	4/HNO3/HCL	CHRS	0.02-20%	ATOMIC ABSORPTION	
	MG X	0.5	C HE/HCLO	ATHNOSTHEL	6HRS	0.2-20%	ATOMIC ABSORPTION	
	LOI X	1:0	ASH 600 i	DEG C	2HRS	0.02-99%	WEIGH RESDUE	

APPENDIX C

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GRI	D	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU2	
9211	5 W	RNX 1	4040	68	74	6	0.3	<0.02	45	83	<2	<0.02	
2211	5W-	RNX 2	4040	49	82		<0.2	<0.02		32	×2-	<0.03	
0211	5W	KNX S	2020	31	85	2	20.5	20.05	12	41	15	<0.02	
9211	5W	RNX 5	2020	44	95	ź	20.5	30.02	25	96	25	<0.02	
9211	50	RNX 6	4040	35	71	ė	<0.2	<0.02	- 12-		(2	<0.02	
9211	5 W	RNX 7	4040	56	62	5	<0.2	<0.02	<2	486	<2	0.02	
9211	5W	RNX 8	4040	50	56	4	<0.2	<0.05	<2	<5	<2	<0.02	
0511	2W	RNX 9	4040	40	21	2	20.5	10.04	25	82	25		
9211	54	RNX 11	2020	40	66	6	<0.2	<0.02	12	58	25	<0.02	
9211	5W	RNX 12	4040	41	68	5	<0.2	<0.02	<2	109	<2	<0.02	
9211	5W	RNX 13	4040	31	70	6	<0.2	<0.02	<2	54	<2	<0.02	
9211	2.	RNX 14	4040				50.2	<u> &lt;0.02</u> ·	<u> &lt;2</u>	125		<0.02	
0511	2 W 5 W	KNX 15 DNY 16	2040	27	62	0	20.5	20.02	25	239		<0.02	
9211	5.0	RNX 17	2020	69	73	6	20:5	20:05	25	301	25	20.02	
9211	5.	RNX 18	4040	53	93		<0.2	<0.02	<2		<2	0.03	
9211	5 W	<b>RNX 19</b>	4040	72	77	7	<0.2	<0.02	<2	198	<2	<0.02	
9211	5 W	RNX 20	4040	64	81	6	<0.2	<0.02	<2	42	<2	<0.02	
2211	2W	RNX 21	4040	51	63	ę	50.2	<0.02	\$2	123	~~	<0.02	
9211	5.4	RNY 23	4040	7.8	107	7	(0.2	<0.02	12	90	0	<0.02	
9211	50	RNX 24	4040	ŠŎ	114	8	<0.2	<0.02	<2	29	<2	<0.02	
9211	5 W	RNX 25	4040	25	155	5	<0.2	<0.02	<2	6	<2	<0.02	
9211	5 W	RNX 26	4040	20	62	- 4	<0.2	<0.02	<2	<u></u>	<2	<0.02	in and the second second
2311	2.	RNX 55.	4040	44	55	10	SU.3	<0.02	25	236	25		
9211	5.4	RNY 28	2020	20	20	12	20.3	<0.02	25	10	25		
9211	ŚW.	RNX 29	4040	23	25	.8	<0.2	<0.02	\$2	32	\$2		
9211	5 W	RNX 30	4040	19	38	7	<0.2	<0.02	<2	26	<2		
9211	SW	RNX 31	4040	25	80	6	<0.2	<0.02	<2	22	<2		
9211	2W	RNX 32	4040	20	23	5	<0.2	<0.02	<2	57	~~~		
0511	Sw	RNX 34	2020	52	20	0	20.5	20.02	- 25-	25	- 25	+-//	
9211	5.	RNX 35	4040	20	112	6	<0.2	<0.02	<2	<5	<2		
9211	5 W	RNX 36	4040	25	91	ž	<0.2	<0.02	<2	83	<2		
9211	54	RNX 36	4040	25	90	6	<0.2	NSS	<2_	77	<2		
9211	2W	RNX SI	4040	34	117	7	<0.2	<0.02	\$2	43	52	<0.02	
6511	5.	RNA JC	4040	10	71	9	20.5	20.05	25	14	25	20.02	
9211	ŚW	RNX 40	2020	49	57	5	20.2	20.02	<2	<5	<2	<0.02	
9211	5 W	RNX 41	4040	41	63	6	<0.2	<0.02	<2	27	<2	<0.02	
9211	5 W	RNX 42	4040	35	81	7	<0.2	<0.02	<2	20	<2	<0.02	
2511	2.	RNX 43	4040	49	15	6	<0.2	<0.02	<2	65	<2		
0211	54	PNY 45	4040	44	50		SU.2	20.02	- 25	85			
9211	5W	RNX 45	4040	45	50	7	20.5	10.02	<2	00	~		
9211	5 W	RNX 46	4040	34	69	ż	<0.2	<0.02	<2	85	<2		
9211	5 W	RNX 47	4040	29	60	6	<0.2	<0.02	<2	119	<2	Anorth (2.1.1)	
9211	2W	RNX 48	4040	35	70	7	<0.2	<0.02	<2	37	<2		
0211	2W	KNX 49	2020	470	66	3	S0.2	<0.02	22	41	22		
0211	E.	DNY 51	1010	20	07	6	10.2	10.02	14	14	14		

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•	GRID	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU2		0
•	92115W 92115W 92115W	- RNX 52 - RNX 53 - RNX 54	4040	27	72 65	897	<0.2	<0.02 <0.02	<22	34	<22 <22		-	
•	92115W 92115W 92115W	RNX 54* RNX 55 RNX 56	4040	2020	61 228 78	11	<0.2	<0.02	<22	54	<22			
	92115W 92115W 92115W	RNX 57 RNX 58 RNX 59	4040 4040 4040	2450	90970	7894	<0.22	<0.02 <0.02 <0.02	~~~~~	31 112 65	~~~~~			
	92115W 92115W 92115W	RNX 61 RNX 62 RNX 63	4040	26	108 138 26	67 11	<0.2	<0.02	~~~~	10 <5 41	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			
	92115W 92115W 92115W 92115W	RNX 65 RNX 65 RNX 66 RNX 67	4040 4040 4040 4040	21 23	76	767	<0.2	<0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	44 48 347	<2222		۹.	
•	92115W 92115W 92115W	RNX 63 RNX 69 RNX 70	4040	3556	15 70 114	8780	<0.2	<0.02 <0.02 <0.02	<2222	44	~~~~~	40.02	(*) <sup>******</sup> ***	
•	92115W	RNX 72 RNX 73	4040	400	70	86	<0.2	<0.02	<22	435	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02		
•	92115W 92115W 92115W	RNX 75 RNX 76 RNX 77	4040		70	67	×0.2	<0.02 <0.02	www.	218	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02 <0.02 <0.02		
AUTOVAL	92115W 92115W 92115W	RNX 78 RNX 79 RNX 80	4040 4040 4040	467 343	60 58 73	978	<0.2 <0.2 <0.2	<0.02 <0.02 <0.02	<22	37 75 61	<22 <22	<0.02 <0.02 <0.02		
-1	92115W 92115W 92115W 92115W	RNX 81* RNX 81* RNX 82 RNX 83	4040	41 402	608 565 62	1287	<0.2	<0.02 <0.02 <0.02	~~~~~	51 58 58	~~~~~	<0.02		
	92115W 92115W 92115W	RNX 84 RNX 85 RNX 86	4040	407	9723	977	<0.2	<0.02	~~~~	116	~~~~	<0.02 <0.02 <0.02		
	92115W 92115W 92115W 92115W	RNX 88 RNX 88 RNX 89 RNX 90	4040 4040 4040	467	67 61 53	10	<0.2	<0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	306	2000	<0.02 <0.02 <0.02		
-	92115W 92115W 92115W	RNX 91 RNX 92 RNX 93	4040	51	6665	~000~	<0.2 <0.2 <0.2	<0.02 <0.02 <0.02	<~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	44	<2222	<0.02 <0.02 <0.02	n a sana sa	
·	92115W 92115W 92115W	RNX 95 RNX 96 RNX 97	4040	61	79	11	<0.2	<0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	37	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02 <0.02		
*	92115W 92115W 92115W	RNX 98 RNX 99 RNX 99+	4040	4666	64 70	10	<0.22 <0.22	<0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	126 156	Novo			
¢	92115W 92115W 92115W	RNX100 RNX101 RNX102	4040 4040 4040	459	76 58 72	10 7 7	<0.2	<0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	37 <5 129	<22 <22			

1	GRID	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU2		
	92115W	RNX103	4040	38	52	5	<0.2	<0.02	<2	122	<2			
	92115W	RNX104 RNX105	4040	49	50	6	<0.2	<0.02	<2	-170	<2		an a	-
	92115W	RNX106	4040	44	5 Ó	7	<0.2	<0.02	<2	258	<2			
5	92115W	RNX107 RNX108	4040	40	68	6	<0.2	<0.02	<2	54	<2			
(	92115W	RNX109	4040	53	68	6	<0.2	<0.02	<2	81	<2			
	92115W	RNX111	2628	57	66	9	20:2	<0.02	25	249	22			
	92115W	RNX112	4040	59	62	10	<0.2	<0.02	<2	137	<2	and the second second		
	92115W	RNX114	4040	42	59	10	<0.2	<0.02	22	214	<2			
	92115W	RNX115	4040	45	62	8	<0.3	<0.02	<2	53	<2			
Γ	92115W	RNX117	4040	43	67	. 8	<0.2	<0.02	<2	95	<2	100 Part 100 Part 100		ternite we see
	92115W 92115W	RNX118 RNX119	4040	57	67	10	<0.2	<0.02	<2	<u>91</u>	<2			
	92115W	RNX120	4040	36	64	ž	<0.2	<0.02	<2	112	<2	<0.02		
	921150	RNX121 RNX122	4040	41	<u>67</u>	10	<0.2	<0.02	<2	42	<2	<0.02		
	92115W	RNX123	4040	34	85	8	<0.2	<0.02	<2	<5	<2	<0.02		
F	92115W	RNX125	4040	55	69	10	<0.2	<0.02	<2	46	<2	<0.02		
	92115W	RNX126	4040	46	76	7	<0.2	<0.02	<2	39	<2	<0.02		
	92115W	RNX120*	4040	35	81	8	<0.2	<0.02	<2	144	<2	<0.02		
	92115W	RNX128	4040	47	72	7	<0.2	<0.02	<2	110	<2	<0.02		
	92115W	RNX130	4040	64	69	9	<0.2	<0.02	<2	14	<2			
-	92115W	RNX131	4040		70	8	<0.2	<0.02	<2	18	<2			
	92115W	RNX133	2020	58	62	10	20.2	<0.02	<2	25	22			
	92115W	RNX134 RNX135	4040	57	84	87	<0.2	<0.02	<2	53	<2			
1	92115W	RNX136	4040	41	63	8	<0.2	<0.02	<2	11	<2			
	92115W	RNX137 RNX13R	4040	35	77	10	<0.2	<0.02	<2	11	<2			
-	<u>92115</u>		4040	48	<u>71</u>		<0.2	<0.02	<2	<u>ž1</u>	<2			
	92115W	RNX140	4040	22	23	10	<0.2	<0.02	<22	35	<2			
	92115W	RNX142	4240	63	64	9	<0.2	<0.02	<2	98	<2			
	92115W	RNX144	4646	42	64	9	20.2	<0.02	<2	133	22			
	92115W	RNX 144*	4848	49	66	9	<0.2	<0.02	<2		<2			
	92115W	RNX146	4040	48	73	7	<0.2	<0.02	<2	22	<2		and the second second second	1000
	92115W	RNX147	4040	48	62	6	<0.2	<0.02	<2	<5	<2			
	92115W	RNX 149	2020	57	76	10	20:2	<0.02	22	42	<2			
	92115W	RNX150	4040	63	54	2	\$0.2	<0.02	<2	96	<2	10 02		
	92115	RNX152	2020	64	56	6	2:0>	20.02	22	326	22	<0.02		
	92115w	RNX153	4040	46	64	5	<0.2	<0.02	<2	64	<2	<0.02		

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		AU2	SB	HG	AS	AU	AG	PB	ZN	CU	PROJECT	SAMPLE	GRID
		<0.02	<2	<5	<2	<0.02	<0.2	9	78	56	4040	RNX155	92115W
		<0.02	<2	106	<2	<0.02	<0.2	8	65	46	4040	- ENX156	92115W
		20:02	22	<5	22	<0.02	20.5	10	55	28	4040	RNX158	92115W
		<0.02	<2	77	<2	<0.02	<0.2	6	112	29	4949	RNX159	92115W
and a second		<0.02	22	141	22	<0.02	<0.2	12	125	133	4040	RNX161	92115W
		<0.02	<2	74	<2	<0.02	<0.2	9	105	81	4040	RNX162	92115W
			3	33	~~	<0.02	20.2	11	104	69	4040	RNX162*	92115W
		Charles and the second s	<2	51	<2	<0.02	<0.2	9	83	39	4040	RNX164	92115W
			<2	51	<2	<0.02	<0.2	7	113	35	4040	RNX165	92115W
			<2	90_	<2	<0.02	<0.2	11		33	2020	RNX167	92115W
			<2	42	<2	<0.02	<0.3	10	74	34	4040	RNX168	92115W
			22	53	22	20.02	20.2	19	63	36	4040	RNX170	92115W
	ىر ئېمورىي، دىكىسورىق		<2	86	<2	<0.02	<0.2	6	58	37	4040	_RNX171_	92115W
			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	74	3	<0.02	<0.2	2	32	51	4040	RNX171*	92115W
			<2	138	<2	<0.02	<0.2	10	77	ŹŚ	4040	RNX173	92115W
			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	38	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02	20.2	9	60	- 25	4040	RNX174	92115W
			<2	45	<2	<0.02	<0.2	8	58	45	4040	RNX176	92115W
			<2	115	<2	<0.02	<0.2	3	52	39	4949	RNX177	92115W
			22	~5	22	20:02	20.2	10	67	25	2020	RNX179	92115W
			<2	32	<2	<0.02	<0.2	10	76	30	4040	RNX180	92115W
			<2	<5	<2	<0.02	<0.2	2	72	37	4040	RNX182	92115W
	and a second		<2	<5	<2	<0.02	<0.2	7	69	24	4040	RNX 183	92115W
			<2	56	22	<0.02	20.2	8	64	29	4040	RNX185	92115W
			<2	125	<2	<0.02	<0.2	8	45	- 21	4040	RNX186	92115W
			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	SU SS	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02	<0.2	10	20	15	4040	RNX 187	92115W
			<2	<5	<2	<0.02	<0.2	8	54	29	4040	RNX189	92115W
		status cantilation	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	- 17-	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02	<0.2	- 8	132	<u> </u>	- 2828-	RNX189*	82115W
			<2	132	<2	<0.02	<0.2	8	73	48	4040	RNX 191	92115W
			<2	10	<2	<0.02	<0.2	8	69	32	4949	RNX192	92115W
			22	17	22	20:02	20:2	9	90	39	2828	RNX194	92115W
			<2	13	<2	<0.02	<0.2	18	102	51	4040	RNX195	92115W
			22	<5	<2	<0.02	<0.2	10	72	35	4040	RNX197	92115W
			<2	<5	<2	<0.02	<0.2	8	97	36	4040	RNX198	92115W
			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	45	3	<0.02	<0.2	10	32	28	4040	RNX199	92115W
			<2	96	<2	<0.02	<0.2	9	71	è Ó	4040	PNX201	92115W
			<2	281	<2	<0.02	<0.2	8	57	50	4040	RNX202	92115W
			<2	23	<2	<0.02	<0.2	7	60	44	4040	RNX204	921150
			<2	<5	<2	<0.02	<0.2	9	52	48	4040	RNX205	92115W

		AUZ	SB	HG	AS	AU	AG	PB	ZN	CU	PROJECT	SAMPLE	GRID	1
			<2	<5	53	<0.02	<0.2	18	69	45	4248	RNX206	22115W	] [
+-+	an ear an	the provide theories in power backtory a	<2	79	<2	<0.02	20.2	9	61	45	4040	RNX208	92115W	1
			<2	20	<2 <2	<0.02 <0.02	<0.2	84	59	43	4040	RNX2U9 RNX210	92115W 92115W	
		<u></u>	- (2	- 76	<2	<0.02	<0.2			58	4040	RNX211 RNX212	92115W	2
			<2	10	<2	<0.02	<0.2	8	78	197	4040	RNX213	92115W	
	en les enerses de la companya en la	<0.02	~2	20	<2	<0.02	<0.2	11	83	43	4040	RNX215	92115W	
		<0.02	<2	20	<2	<0.02	<0.2	10	114	56	4040	RNX216 RNX216*	92115W 92115W	
		<0.02	<2	.7	<2	<0.02	<0.2	5	66	49	4040	RNX217	92115W	
		<0.02	<2	50	<2	<0.02	<0.2	6	65	51	4040	RNX219	92115W	T
	A		<2	56	<2	<0.02	<0.2	4	67 58	46	4040	RNX220 RNX221	92115W	
95	The start		<2	56	<2	<0.02	<0.2	-6	67	63	4040	RNX222	92115w	
			22	33	<2	<0.02	<0.2	7	87	56	4040	RNX224	92115W	
			<22	46	<22	<0.02	<0.2	10	87	59	4040	RNX225 RNX226	92115W 92115W	
100			<2	205	<2	<0.02	<0.2	6	74	89	4040	RNX227	92115W	
			22	30	22	<0.02	20.2	ž	65	45	4040	RNX229	92115W	
			<2	43	<2	<0.02	<0.2	6	62	55	4040	RNX230 RNX231	92115W 92115W	
			<2	36	<2	<0.02	<0.2	10	93	38	4040	RNX232	92115W	
			~2	69	22	<0.02	20.2	?	61	64	4040	RNX234	921156	
			<22	188	<2	<0.02	<0.2	11	67	58	4040	RNX235 RNX236	92115W 92115W	
			<2	59	<2	<0.02	<0.2	8	61	44	4040	RNX237	92115W	
	a parameter of the second		<2	59	<2	<0.02	<0.2	8	76	45	4040	RNX239	92115W	
			<2	119	<2	<0.02	<0.2	89	247	52	4040	RNX241	92115W	
			<2	<5	<2	<0.02	<0.2	8	64	47	4040	RNX242 RNX243	92115W	-
			<2	57	<2	10.02	<0.2	6	75	46	4040	RNX243*	82115W	
			<2	36	<2	<0.02	<0.2	°7.	69	53	4040	RNX245	92115W	
		<0.02	<2	17	<2	<0.02	<0.2	7	73	31	4040	RNX246 RNX247	92115W 92115W	
		<0.02	<2	3	<2	<0.02	<0.2	.9	67	45	4040	RNX248	92115W	
	1.1	<0.02	<2	63	66	<0.02	<0.2	7	88	54	4040	RNX250	92115W	T
		<0.02	<2	83	10	<0.02	<0.2	9	92	29	4040	RNX251 RNX252	92115W	
	a second	20.00	52	50	<2	\$0.02	\$0.2	. ě	70	29	4040	RNX252*	92115W	-
		<0.02	<2	75	<2	20.02	2:0>	27	59	38	4040	RNX254	92115W	
		<0.02	<2	31	<2	<0.02	<0.2	10	117	42	2040	RNX255 RNX256	92115W	

and the second second second

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0.10		PROJECT	CU	7 N	PR	AG	AU	AS	HG	SB	A112	
02115W	DNY257	4040	53	72	6	<0.2	<0.02	<2	31	(2		
92115W	· RNX258	2020	59	81	10	<0.2	<0.02	<2	54	<2		a second to a subsection of the second second
921-15W	RNX259 RNX260	4040	60 54	96	11	<0.2	<0.02	<2	54	~2		
92115W	RNX261	4040	37	75	8	<0.2	<0.02	<2	34	<2		
92115	<u>RNX261*</u>	2020	42			<0.2	<0.02	- 2	37	- 23		
92115W	RNX263	4040	33	35	12	<0.2	<0.02	<2	109	<2		
92115W	RNX264	4040	45	<u>65</u>	ş	<0.2	<0.02	<2	75	<2		
92115W	RNX266	4040	36	75	5	<0.2	20.02	<2	.7	<2	a na sa	and the second se
92115W	RNX267	4040	32	65	Ę	<0.2	<0.02	<2	112	<2		
92115W	RNX269	4040	57	60	5	<0.2	<0.02	<2	44	<2	and the second sec	
92115W	RNX270	4040	73	62	4	<0.2	<0.02	<2	65	<2	3	
92115W	RNX271	4040	66	62	3	20:2	<0.02	22	292	22		
92115W	RNX272	4848	59	70	<u> </u>	<0.2	<u>&lt;0.03</u>	<2	102	< <u>&lt;</u>	ورور المراجع والمراجع والمراجع والمراجع والمراجع والمراجع	
92115W	RNX274	4040	35	74	8	<0.2	<0.02	<2	31	22		
92115W	RNX275	4040	33	63	5	<0.2	<0.02	<2	<5	<2		
92115W	RNX277	4040	24	- 22	- 3	<0.2	<0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	3	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
92115W	RNX278	4040	38	66	7	<0.2	<0.02	<2	<5	<2		
92115W	RNX279 RNX280	4040	42	63	6	<0.2	<0.02	<2	~5	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
92115W	RNX281	4040	38	66	5	<0.2	<0.02	<2	<5	<2	and the second secon	a yan da barkan dan sama di sasta da sa sa sa sa
92115W	RNX282 PNX283	4040	34	62	7	<0.2	<0.02	<2	119	~~~		
92115W	RNX284	4040	25	58	6	<0.2	<0.02	<2	zó	<2		
92115W	RNX285	4040	39	77	67	<0.2	<0.02	<2	41	<2		
92115W	RNX287	4040	21	89	. 5	<0.2	<0.02	<2	37	<2		
92115W	RNX288	4040	27	21	5	<0.2	<0.02	<2 <u></u>	<u> 10</u>	<2 .	<0.02	
92115W	RNX289	4040	35	62	10	<0.5	<0.02	<2	20	22	0.02	
92115W	RNX291	4040	25	101	8	<0.2	<0.02	<2	<5	<2 •	<0.02	
921150	RNX292	4040	28	47	12	<0.2	<0.02	- 3	- 22	- 2	0.02	
92115W	RNX294	4040	32	115	. 5	<0.2	<0.02	<2	126	<2 .	0.02	
92115W	RNX295	4040	50	102	10	<0.2	<0.02	10	286	3	C • U 2	
92115W	RNX297	2020	38	136	10	<0.2	<0.02	22	×5	22 .	0.02	
92115W	RNX297*	4040	36	133	2	<0.2	<0.02	<2	34	<2	0 02	
92115W	RNX299	4040	40	42	13	20.2	20.02	22	°Ę	22	0.02	
92115W	RNX 300	4040	21	41	- 7	<0.2	<0.02	<2	14	<2		
92115W	RNX302	4040	24	63	7	<0.2	<0.02	<2	17	<2		
22115W	RNX 303	4040	29	71	8	<0.2	<0.02	<2	<5	<2 .	0.02	
92115W	RNX304 *	4040	55	00	10	<0.2	<0.02	<2	1	<2	0.02	
92115W	RNX305	4040	41	66	11	<0.2	<0.02	<2	27	<2 .	0.02	
	WW         SS         WW         SS         WW         SS         WW         SS         WW         SS         SS         WW         SS         SS	92115W RNX260 92115W RNX260 92115W RNX260 92115W RNX266 92115W RNX266 92115W RNX266 92115W RNX266 92115W RNX266 92115W RNX2266 922115W RNX2266 922115W RNX2266 922115W RNX2266 922115W RNX2270 922115W RNX2277 922115W RNX2278 922115W RNX2288 922115W RNX22997 922115W RNX22991 922115W RNX23004 922115W RNX3005 922115W RNX3005 922115W RNX3005 922115W RNX3005 922115W RNX3005 922115W RNX3005 922115W RNX3005 922115W	92115W       RNX260       4040         92115W       RNX261*       4040         92115W       RNX262       4040         92115W       RNX265       4040         92115W       RNX266       4040         92115W       RNX2669       4040         92115W       RNX270*       4040         92115W       RNX2770*       4040         92115W       RNX2771*       4040         92115W       RNX2775       4040         92115W       RNX2775       4040         92115W       RNX2780       4040         92115W       RNX2780       4040         92115W       RNX2883       4040         92115W<	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	92115W       RNX2601       4040       37       75         92115W       RNX2661       4040       37       73         92115W       RNX2661       4040       42       71         92115W       RNX2662       4040       42       71         92115W       RNX2663       4040       45       65         92115W       RNX2664       4040       36       75         92115W       RNX2666       4040       36       75         92115W       RNX2666       4040       73       63         92115W       RNX2669       4040       73       63         92115W       RNX2770       4040       73       63         92115W       RNX2771       4040       59       70         92115W       RNX2774       4040       35       74         92115W       RNX2775       4040       38       66         92115W       RNX2776       4040       38       66         92115W       RNX2776       4040       38       66         92115W       RNX27884       4040       38       66         92115W       RNX22881       4040       36       51	92115W       RNX260       4040       54       97       8         92115W       RNX261       4040       35       73       9         92115W       RNX261       4040       35       73       9         92115W       RNX2662       4040       35       65       8         92115W       RNX2664       4040       35       65       5         92115W       RNX2664       4040       32       65       5         92115W       RNX2667       4040       32       65       5         92115W       RNX2667       4040       73       62       4         92115W       RNX270*       4040       73       62       4         92115W       RNX270*       4040       73       62       4         92115W       RNX2770*       4040       59       70       6         92115W       RNX2774       4040       35       5       5         92115W       RNX2776       4040       38       66       7         92115W       RNX2777       4040       38       66       7         92115W       RNX278       4040       36       55	92115w       RNX260       4040       37       75       8       <0.2	92115W       RNX260       4040       54       97       8       <00.2	92115W       RNX260       4040       54       97       8       CO.2       CO.02       C2         92115W       RNX261       4040       35       73       9       CO.2       CO.02       C2         92115W       RNX263       4040       35       73       9       CO.2       CO.02       C2         92115W       RNX263       4040       42       71       5       CO.2       CO.02       C2         92115W       RNX263       4040       42       76       5       5       CO.02       C2         92115W       RNX266       4040       49       70       5       CO.2       CO.02       C2         92115W       RNX266       4040       76       65       5       CO.2       CO.02       C2         92115W       RNX267       4040       73       62       4       CO.2       C0.02       C2         92115W       RNX270*       4040       73       62       4       CO.2       C2       C2	92115W       RNX260       4040       54       97       8       <0.2	92115 **       RNX260       4040       54       97       8       C0-2       C002       C2       34       C2         92116 **       RNX261       4040       75       75       9       C0-2       C002       C2       37       C2         92116 **       RNX261       4040       75       75       9       C002       C2       37       C2         92116 **       RNX263       4040       75       75       9       C002       C2       77       C2       C002       C2       37       C2         92116 **       RNX263       4040       75       35       12       C002       C2       112       C2       <	02115       RNX260       4040       37       75       8       C0-2       C9.02       C2       34       C2         02115       RNX261       4040       37       75       8       C0-2       C0.02       C2       34       C2         02115       RNX264       4040       42       75       9       C0-2       C0-02       C2       75       C2         02115       RNX264       4040       42       75       5       C0-2       C0-02       C2       75       C2         02115       RNX264       4040       36       70       5       C0-2       C0-02       C2       82       C2       75       C2       27       C2       82       C2       75       C2

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GR	ID	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU 2	
0.2.7	1511	0.0.7	(0(0	20	47	4	10.2	<0.02	12	0.2	12	<0.02	
921	150	RNX308	4040	32	68	4	<0.2	<0.02	<2	-10	42	<0.02	
921	15W	RNX309	4040	29	68	3	<0.2	<0.02	<2	65	<2	<0.02	
921	154	RNX310	4040	39	68	8	<0.2	<0.02	<2	14	<2	<0.02	
621	15W_	RNX312	4040	38	77	ŝ	20.2	<0.02	2	68	22	20.02	
921	15W	RNX313	4040	23	58	4	<0.2	<0.02	<2	27	<2	<0.02	
921	15W	RNX 514	4040	24	63	2	<0.2	<0.02	<2	31	<2	<0.02	
921	150	RNX315*	4040	36	100	9	<0.2	10.02	22	37	<2	<b>U</b> .02	
921	15W	RNX316	4040	37	76	7	<0.2	<0.02	<2	27	<2	<0.02	
921	154	RNX317	4040	57	75	5	<0.2	<0.02	<2	61	<2	<0.02	
921	154	RNX319	2020	45	93	4	20.5	20.02	32	61	32	10.02	
921	15w	RNX320	4040	30	92	6	<0.2	<0.02	<2	<5	<2		
821	15W	RNX321	4040	46	131	8	<0.2	<0.02	<2	<5	52		
921	154	RNX323	2020	20	73	7	20.5	<0.02	62	17	3		
921	15W	RNX324	4040	25	93	8	<0.2	<0.02	<2	14	<2		
921	15W	RNX325	4040	32	71	6	<0.2	<0.02	2	20	<2		
851	120	RNX359	2020	31	21	ğ	20.3	20.02	3	22	3		
921	15W	RNX328	4040	39	66	7	<0.2	<0.02	<2	30	<2	a second and a second	
921	15W	RNX329	4040	34	61	7	<0.2	<0.02	<2	46	<2	5	
921	15W	RNX33U	4040	32	86	11	20.2	<0.02	25	50	12		
921	15W	RNX332	4040	26	58	7	<0.2	<0.02	<2	53	<2	a difference al lines and the second	
921	15W	RNX333	4040	20	44	5	<0.2	<0.02	<2	43	<2		
921	15W	RNX 334	4040	45	95	3	<0.2	<0.02	3	267	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
921	15W	RNX336	4040	22	. 50	5	<0.2	<0.02	<2	7	<2		
921	15W	RNX337	4040	61	77	6	<0.2	<0.03	<2	36	<2		
921	150	RNX 330	4040	20	01	6	<0.2	<0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	27	3		
921	150	RNX340	4040	66	66	6	<0.2	<0.02	<2	102	<2		
921	15 W	RNX341	4040	34	97	7	<0.2	<0.02	<2	112	<2	<0.02	
921	120	RNX342	4040	39	79	é	<0.2	<0.02	<2	119	~2	<0.02	
921	15w	RNX343	4040	50	100	5	<0.2	<0.02	28	112	<2	<0.02	
921	15.	RNX344	4040	46	79	7	<0.2	<0.02	<2	76	<2	<0.02	
921	15W	RNX345	4040	51	15	2	<0.2	<0.02	22	50	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02	
921	150	RNX347	4040	65	63	6	<0.2	<0.02	<2	129	22	<0.02	
921	15 W	RNX348	4040	37	71	5	<0.2	<0.02	< Ž	79	<2	<0.02	
921	15W	RNX349	4040	33	72	5	<0.2	<0.02	<2	40	<2	<0.02	
921	15W	RNX351	4040	69	61	5	<0.2	20.02	<2	347	22	NUAUZ	
921	15w	RNX352	4040	28	119	8	<0.2	<0.02	<2	50	<2		
921	154	RNX353	4040	57	87	5	<0.2	<0.02	<2	79	<2		
831	154	KNX 224	2625	20	24	2	20.5	20.02	3	100	- 25	· · · · · · · · · · · · · · · · · · ·	
921	150	RNX356	4040	58	99	5	<0.2	<0.02	<2	56	<2		
921	15W	RNX357	4040	30	60	5	<0.2	<0.02	<2	23	<2		
751	124	KNX335	4040		105		CU.2	50.02	52	0.5	<2		

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1	GRID	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU2		
	92115w	RNX359	4040	38	75	4	<0.2	<0.02	<2	69	<2			
	92115W	· RNX360	4040	22	78	5	<0.2	<0.02	<2		<2		$(a_1,a_2,a_3,a_4,a_4,a_4,a_4,a_4,a_4,a_4,a_4,a_4,a_4$	-
	92115W	RNX361	2828	34	76	5	20.2	<0.02	<2	45	<2			
	92115W	RNX362	4040	36	70	5	<0.2	<0.02	<2	45	<2	<0.02		
2	92115W	RNX364	4040	55	66	4	<0.2	<0.02		87	<2	<0.02		
	92115W	RNX 365	4040	65	67	6	<0.2	<0.02	6	14	<2	<0.02		
1	92115W	RNX366	4040	40	77	5	<0 Z	<0.02	<2	~5	\$3	<0.02		
1	92115W	RNX368	4040	54	80	5	<0.2	<0.02	2	25	22	<0.02		1
	92115W	RNX369	4040	35	75	4	<0.2	<0.02	<2	34	<2	<0.02		
	92115W	RNX 370	4040	62	54	4	<0.2	<0.02	<2	123	<2	<0.02		
F	92115W	RNX372	4040	45	66	9	<0.2	<0.02	<2	84	<2	<0.02		
1	92115W	RNX373	4040	26	68	6	<0.2	<0.02	<2	<5	<2	<0.02		
	921150	RNX 574	4040	40	60	6	20.3	<0.02	<2	35	23	<0.02		
1	92115W	RNX376	4040	41	47	6	<0.2	<0.02	<2	53	<2	<0.02		-
	92115W	RNX377	4040	31	63	6	<0.2	<0.02	<2	14	2	<0.02		
	92115W	RNX 378	4040	23	20	2	20.3	<0.02	~~	44	<2	<0.02		
t	92115W	RNX379	2020	39	70	8	<0.2	<0.02	<2	14	<2			-
	92115W	RNX380	4040	43	74	5	<0.2	<0.02	<2	<5	2			
	92115W	RNX 381	4040	43	62	9	<0.2	<0.02	<2	177	22			
5	92115W	RNX383	2020	69	66	7	<0.2	20:02	22	165	<2	and a second		
F	92115W	RNX384	4040	45	70	6	<0.2	<0.02	<2	59	<2			
ē	92115W	RNX 385	4040	20	64	6	20.2	<0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	17	22			
	92115W	RNX387	4040	- 77	ĕŎ	6	<0.2	<0.02	<2	56	<2			-
	92115W	RNX387*	4040	44	58	5	<0.2		<2					
0	92112W	RNX389	2020	51	61	05	20.5	<0.02	25	33	3			
	92115W	RNX390	4040	44	61	ž	<0.2	<0.02	<2	17	~22	and the second	Energy and an energy of the second	
	92115W	RNX391	4040	42	66	5	<0.2	<0.02	<2	<5	<2			
	921150	RNX392	2040	36	55	2	20.2	<0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	104	3			
T	92115W	RNX394	4040	47	59	Š	<0.2	<0.02	<2	17	<2		and the second second second	-
1	92115W	RNX395	4040	38	63	6	<0.2	<0.02	<2	53	<2			
	92115W	RNX397	2020	27	57	25	20.2	<0.02	3	56	3			
1	92115W	RNX398	4040	4C	54	6	<0.2	<0.02	2	13	<2	Harristen and Second		
	92115W	RNX399	4040	182	54	5	<0.3	<0.02	<2	33	<2			
	92115W	RNX401	4040	42	72	8	<0.2	<0.02	22	69	22			
Γ	92115W	RNX402	4040	48	61	6	<0.2	<0.02	<2	NSS	<2	1. M. P. C. M. P.		-
	92115W	RNX403	4040	37	65	7	<0.2	<0.02	<2	NSS	<2			
	92115W	RNX405	4040	28	85	5	20:2	20:02	22	NSS	22			
1	92115W	RNX405*	4040	29	87	?	<0.2		<2	NSS	·	(1) and (1) (1) (1) (1) (2) second (1) (2) (2) (3)	nu⊶) an 2000 - Contra - Contr	69
	921154	RNX4U6	4040	58	240	9	20.2	<0.02	<2	<5 7 A	\$2			
	02115	PNYLOR	2020	25	68	Ś	20.5	20.05	25	26	25			

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L	PLACER	GEOCHEM A	SSAY SYST	EM: DAT	A FROM	1 Cara	bine	soils							DA
1	GRID	SAMPLE	PROJECT	сu	ZN	PB	AG	AU	AS	HG	SB	AU2	- San Sec.		
G	92115W 92115W 92115W	RNX409 RNX410 RNX411	4040 4040 4040	328	730	105	<0.2 <00.2	<0.02 <0.02 <0.02	<>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	310	~~~~~	· · · · · ·			
c	92115W	RNX412 RNX413 RNX414	4040	21	43	154	<0.2	<0.02	<2	\$5	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~				
•	92115W 92115W 92115W 92115W 92115W 92115W	RNX415 RNX416 RNX416 RNX417 RNX418 RNX419	4040 4040 4040 4040 4040	360527	81 57 631 71	66566	<00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2 <00.2	<0.02 <0.02 <0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	30 <5 149 20 17	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	te ye her for family			
c	92115W	RNX420 RNX421	4040	2360	59	6	<0.2	<0.02	<22	33	<2				
L	92115W 92115W 92115W 92115W 92115W	RNX423 RNX423 RNX424 RNX425 RNX426	4040 4040 4040 4040	202044	59676	00400	<0.2 <0.2 <0.2 <0.2 <0.2	<0.02 <0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	97662	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	en ann an Stainer I		_	
C	92115W 92115W 92115W 92115W	RNX427 RNX428 RNX429 RNX429	4040 4040 4040 4040	27 39 31 14	65 68 77 35	67.64	<0.22 <00.22 <00.22	<0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	59 20 45	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~				
ALU C	921155W 9221155W 99221155W 99221155W 99221155W	RNX432 RNX432 RNX433 RNX433 RNX435	4040 4040 4040 4040 4040 4040	2991	20889 2798 1182	11 11 867	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02 <0.02 <0.02 <0.02		30 15 <5 <5	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	11			
CUTO	92115W 92115W	RNX436 RNX437	4040	20	98	10	<0.2	<0.02	2	21	<2			And the second second	
, a	92115W 92115W 92115W 92115W 92115W 92115W 92115W	RNX438 RNX439 RNX440 RNX441 RNX442 RNX443	4040 4040 4040 4040 4040 4040 4040	2223254	70 60 75 71 62	887676	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02 <0.02 <0.02 <0.02 <0.02 <0.02	NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN	692 171 545	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~				
-	92115W 92115W	RNX444 RNX445	4040	<u> </u>	72		<0.2	<0.02	<22	<5 66	<22	<0.02			
C	92115W 92115W 92115W 92115W	RNX446 RNX447 RNX448 RNX448	4040 4040 4040 4040	345	86 92 72	686	<0.2	<0.02 <0.02 <0.02	<2 <2 12	30 <5 48	<22	<0.02 <0.02 <0.02 <0.02			
ç	92115W 92115W 92115W 92115W	RNX449 RNX450 RNX451 RNX452	4040 4040 4040 4040	363 31 51	65 67 895	7777	<0.2	<0.02 <0.02 <0.02 <0.02	*** ***	<5 <52 79	<22 <22 <22	<0.02 <0.02 <0.02 <0.02			
L	92115W 92115W 92115W 92115W 92115W	RNX453 RNX454 RNX455 RNX456 RNX457	4040 4040 4040 4040	402123	805485 685	78878	<0.2 <0.2 <0.2 <0.2 <0.2	<0.02 <0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<5 60 57 102	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02 <0.02 <0.02 <0.02 <0.02	1) 10 (10) - 100 <sup>-10</sup> - 10		
C	92115W 92115W 92115W	RNX458 RNX459 RNX459 *	4040 4040 4040	73 52 53	60 69 70	7 8 7	<0.2 <0.2 <0.2	<0.02 <0.02	<2 <2 <2	105 72	<2 <2 <2	<0.02 <0.02			

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F	PLACER	GEOCHEM A	SSAY SYST	EM: DAT	A FROM	1 Cara	bine	soils						C	DA
1	GRID	SAMPLE	PROJECT	cu	ZN	PB	AG	AU	AS	HG	\$B	AUZ			
9	92115W	RNX460	4040	55	73	8	<0.2	<0.02	<2	.9	<2	<0.02			
2	92115W	· RNX461	4040	25	68	9	<0.2	<0.02	<2	1043	- 52	<0.02			
2	921-10W	KNX402	2020	26	48	à	20.5	20.05	25	1002	15	20.05			
ć	92115W	RNX464	2020	42	60	6	20.5	20.02	25	57	25	20.02			
5	92115W	RNX465	4040	44	75	6	<0.2	<0.02	<2	96	<2	<0.02			
5	92115W	RNX466	4040	42	73	7	<0.2	<0.02	<2	36	<2	<0.02			
9	92115W	RNX467	4040	61	68	7	<0.2	<0.02	<2	93	<2	<0.02			
5	92115W	RNX468	4040	51	65	6	<0.2	<0.02	<2	72	<2				
1	92115W	RNX469	4040	46	67	<u> </u>	.<0.2	<0.02		20	<u>&lt;2</u>				
1	92112W	RNX470	4040	43	03	3	<0.2	<0.02	4	<5	52				
2	YZIIZW	KNX471	4040	22	94	4	50.3	20.02	53	44	55				
6	05115W	DN Y / 73	2020	57	68	é	20.3	20.05	25	25	25				
0	921154	RNX474	2020	- 22	58	8	20.5	20.05	25	05	- 25	the second second			-
ć	921150	RNX475	2020	62	54	ă	20.2	<0.02	22	66	(2		4		
C	92115W	RNX476	4040	45	56	ğ	<0.2	<0.02	<2	<5	<2				
4	92115W	RNX477	4040	53	60	Ź	<0.2	<0.02	\$2	27	<2				
\$	92115W	RNX477*	4040	56	62	8	<0.2		<2						
9	92115W	RNX478	4040	36	50	7	<0.2	<0.02	<2	< 5	<2			<i>4</i> :	
5	92115W	RNX479	4040	43	78	9	<0.2	<0.02	2	< 5	<2				
_	92115W		4040	41	63	8	<0.2	<0.02	<2	34	<2	<0.02	and the second		
2	92112W	RNX481	4040	28	40	10	<0.2	<0.02	<2	53	<2	<0.02			
2	Y LI LOW	KNX484	4040	23	02	2	50.2	<0.02	22	44	54	20.02			
2	92112W	KNA405	4040	44	29	9	20.3	20.03	25	15	25	20.03			
ć	05115W	PNYZ85	2020	- 21	25		20.5	20:05				20:05			
ć	921150	RNXL86	2020	43	66	8	20.2	<0.02	12	44	25	<0.02			
ć	92115W	RNX487	4040	50	64	7	<0.2	<0.02	<2	37	<2	<0.02			
(	92115W	RNX487*	4040	20	<b>C</b> +					5.		<0.02			
9	92115W	RNX488	4040	51	64	7	<0.2	<0.02	<2	<5	<2	<0.02			
9	92115W	RNX489	4040	52	58	7	<0.2	<0.02	<2	< 5	<2	<0.05			
5	92115W	RNX490	4040	45	61	5	<0.2	<0.02	<2	< 5	<2	<0.02			
5	92115W	RNX491	4040	67	51	6	<0.2	<0.02	<2	82	<2	<0.02			-
2	24112W	RNX494	4040	40	23	9	<0.2	0.04	53	<b>\$5</b>	<2	<0.02			
2	92115W	RNX493	4040	22	21	2	20.5	20.05	25	10	25	20.05			
ć	02115W	PNYLOS	2020	13	60	2	20.5	20.05	25	25	25	20.02			
(	92115W	RNX496	4040	13	62	10	<0.2	20:05	25		25	20.02			
¢	92115W	RNX496*	4040		01	10	-0-2					<0.02			
9	92115W	RNX497	4040	51	66	8	<0.2	<0.02	<2	< 5	2	<0.02			
5	92115W	RNX498	4040	51	47	8	<0.2	<0.02	<2	170	<2	<0.02			
5	92115W	RNX499	4040	32	40	6	<0.2	<0.02	<2	150	<2	<0.02			
1	92115W	RNX500	4040	38	53	7	<0.2	<0.02	<2	31	<2	<0.02			
2	92115W	RNX501	4040	49	05	1	<0.2	<0.02	<2	21	<2				
	X5+12W	KNX2US				9	50.2	50.02		- 77	- 52				
2	021150	PNYSOL	4040	20	49	04	20.5	20.02	25	10	15				
0	021150	RNY504	2020	21	54	05	20.5	20.05	25	25	25				
c	921150	RNX505	2020	54	62	2	20.5	20.05	25	11	25				
é	921150	RNX506	2020	ĩõ	46	11	20.5	20:05	- 25-	22	- 25	·····		were written at the s	- 10 miles
ć	921150	RNX507	4020	48	64	0	<0.5	20.05	25	20	3				
4	92115W	RNX508	4040	45	62	9	<0.2	<0.02	<2	187	<2				
c	92115W	RNX509	4040	48	60	6	<0.2	<0.02	<2	95	<2				

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يوية ( <sup>عر</sup> مية) المحمولية،		ىرىكى بىر يەرىسەيەر «ھەرمەر بەر بەر بەر بەر بەر بەر بەر بەر بەر ب	an a	antiki ishin ju wanag		يىنىرەدى، مېراھى			ويغلونه والمعاديات		*****	بریسود موجود از در اف	an she water the state of the s	-
•	PLACER	GEOCHEM A	SSAY SYST	EM: DAT	A FROM	Cara	bine s	oils						C
**	GRID	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU2		
3	92115W 92115W 92115W	RNX510 RNX511 RNX512	4040	6030	462	11	<0.2 <0.2 <0.2	<0.02 <0.02 <0.02	<22	116	<22 <22		- 1)	
c	92115w 92115w 92115w	RNX513 RNX514 RNX515	4040 4040 4040	50 37 35	57 49 59	878	<0.2	<0.02 <0.02 <0.02	<22	41 48 27	<2			
c	92115W 92115W 92115W 92115W 92115W	RNX516 RNX517 RNX518 RNX519	4040 4040 4040 4040	451	6500 6500	6778	<0.2	<0.02 <0.02 <0.02 <0.02	~~~~~	231	~~~~			
L	92115W 92115W 92115W 92115W	RNX52U RNX521 RNX522 RNX523	4040 4040 4040 4040	43927	58 61 64	877	<0.2	<0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	485 45 41 82	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			
L	92115W 92115W 92115W 92115W 92115W 92115W	RN X 524 RN X 525 RN X 526 RN X 527 RN X 528	4040 4040 4040 4040	55558	62 61 51 50	54865	<0.2 <0.2 <0.2 <0.2 <0.2	<0.02 <0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<pre></pre>	<22 <22 <22 <22	<0.02 <0.02 <0.02 <0.02 <0.02	а. •	
s.	92115W 92115W 92115W	RNX528 * RNX529 RNX530	4040	33	62	4	<0.2	<0.02	<2	34	<2	<0.02 <0.02 <0.02		
ر د	92115W 92115W 92115W 92115W 92115W 92115W	RNX531 RNX531 * RNX532 RNX533 RNX534	4040 4040 4040 4040 4040	4962 728	62 60 68 56 81	50545	<<<<<<<<<<<<<<<<<<<<<<<<<<>>	<0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	51 20 31 24 <5	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<0.02 <0.02 <0.02 <0.02 <0.02	a na ana ana ana a	
LTOVAL	92115W 92115W 92115W	RNX535 RNX536 RNX537	4040 4040 4040	45 40 42	63 60 56	454	<0.2 <0.2 <0.2	<0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	82 51 71	<22 <22	<0.02 <0.02 <0.02		
F.	92115W 92115W 92115W 92115W 92115W 92115W	RNX538 RNX539 RNX540 RNX540* RNX541 RNX542	4040 4040 4040 4040 4040 4040	5379072 45072	61 58 60 62 56	645685	<0.22×0.22×0.22×0.22×0.22×0.22×0.22×0.22	<0.02 <0.02 <0.02 <0.02	<>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	150 58 109	<<<<<>>><<<<>><<<<>><<<<>><<<<>><<<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><<>><>><<>><<>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>><>>	art-angé = 301		a marte a second
C	92115W	RNX543 RNX544	4040	45	58 70	55	<0.2	<0.02	<22 <22	112	<22 <22			
2	92115W 92115W 92115W 92115W 92115W	R N X 5 4 5 R N X 5 4 6 R N X 5 4 7 R N X 5 4 7 R N X 5 4 9	4040 4040 4040 4040	44445	696620 7620	35574	<0.2 <0.2 <0.2	<0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	132	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		(1 · + +) · (1 · 1)	
C	92115W 92115W 92115W	RNX550 RNX551 RNX552	4040	46337	55	542	<0.2	<0.02	~~~~	8630	2222			
Ļ	92115W 92115W 92115W 92115W 92115W 92115W	RNX553 RNX554 RNX555 RNX555 RNX557	4040 4040 4040 4040 4040	41 480 443 44	559 587 587 58	NUNUN NUNUN	<0.22 <0.22 <0.22 <0.22 <0.22	<0.02 <0.02 <0.02 <0.02 <0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	30 79 96 218 59	<<<<<>><<<<<>><<<<>><<<<>><<<<>><<<<>><<<<			
c	92115W 92115W 92115W	RNX 558 RNX 558 * RNX 559	4040 4040 4040	444	61 61 74	<222	<0.2 <0.2 <0.2	<0.02 <0.02	<2 <2 <2	83 79 26	<22 <22			

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GRID	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU2	ald a real and a stand by	
2115W	RNX 560	4040	30	53	<2	<0.2	<0.02	<2	122	<2			
2112W	RNX561	4040	- 29	56		20.3	20.02		70	- 22	<0.02		****** ** • ******** ** •
21150	RNX563	4040	46	68	š	<0.2	<0.02	<2	<b>&lt;</b> 5	<2	<0.02		
2115W	RNX564	4040	43	64	5	<0.2	<0.02	<2	26	<2	<0.02		
21150	RNX565	4040	60	63		×0.2	<u>&lt;0.02</u>		45		<u>&lt;0.02</u>		
21150	RNX567	2020	69	66	4	<0.2	<0.02	<2	13	<2	<0.02		
2115W	RNX568	4040	64	52	9	<0.2	<0.02	<2	320	<2	<0.02		
2115W	RNX569	4040	76	68	4	<0.2	<0.02	\$2	122	<u> &lt;2</u>	<0.02	in the second second relation being the second s	
2112W	RNX57U	2020	161	68	5	20.5	<0.02	25	508	25	<0.02		
21150	RNX572	2020	86	64	4	<0.2	<0.02	<2	17	<2	<0.02		
2115W	RNX573	4040	65	61	3	<0.2	<0.02	<2	63	<2	<0.02		
2115W	RNX574	4040	22	61	<2	<0.2	<0.02	<2	224	<2	<0.02	•	
2115W	RNX576	2020	64	68	Ę	20.5	<0.02	25	43	25	20:05		
2115W	RNX576*	4040	60	65	Ž	<0.2		<2	69	<2			• • • • • • • • • • • • • • • • • • •
2115W	RNX577	4040	45	58	5	<0.2	<0.02	<2	155	<2	<0.02		
STIEW	RNX278	4040	30	50	Ę	20.3	20.03	25	129		20.05		
21150	RNX580	4040	53	57	ž	<0.2	<0.02	<2	121	<2	<0.02		
2115W	RNX581	4040	59	64	4	<0.2	<0.02	<2	43	<2	<0.02	14779-	
2115W	RNX582	4040	45	41	6	<0.2	<0.02	<2	121	<2	<0.02		
ZIIZW	RNX585	4040	24	00	2	20.3	<0.02	25	23		<0.02		
21150	RNX 585	4040	62	62	5	<0.2	<0.02	<2	40	₹2	and the lines of the section of the line of the section of		and the second second second
2115W	RNX586	4040	53	63	4	<0.2	<0.02	<2	< 5	<2	<0.02		
2115W	RNX587	4040	47	64	6	<0.2	<0.02	<2	31	22			
21154	RNX589	2020		66		10.2	20:05	- 25	12	<2			
21150	RNX590	4040	73	60	4	<0.2	<0.02	<2	34	<2			
2115W	RNX591	4040	57	60	2	<0.2	<0.02	<2	102	<2			
STILW -	- RNX294	2828	41	- 20		50.5		- 25	15-	- 25			(17) * (7) (#1)
21150	RNX594	4040	44	57	T.	<0.2	<0.02	<2	<5	<2			
2115W	RNX594*	4040	44	57	ž	<0.2		<2	22				
2115W	<u>RNX595</u>	4040	41	51		<0.2	<0.02	<2		<2			
21150	RNX 390	4040	20	53	2 R	20.2	<0.02	62	68	3			
21150	RNX598	4040	64	46	6	<0.2	<0.02	<2	118	<2			
2115W	RNX599	4040	48	53	5	<0.2	<0.02	<2	16	<2		-	
2115W	RNX600	4040	51	50	5	<0.2	<0.02	<2	105	<2	10 02		
51150	RNX601	2020	71	22	Ę	20.5	20.05	25	78	25	20.02		
2115%	RNX603	4040	57	62	ž	<0.2	<0.02	<2	53	<2	<0.02		
2115W	RNX603*	4040	58	63	4	<0.2		<2	19	<2			
2115W	RNX604	4040	50	50	5	<0.2	<0.02	<2	198	\$2	<0.02		
21150	RNX606	2020	55	61	2	20.2	20.05	25	96	25	20.02		
2115W	RNX607	4040	44	67	3	<0.2	<0.02	<2	4Ŏ	<2	<0.02		
2115W	RNX608	4040	48	62	Z	<0.2	<0.02	<2	22	<2	<0.02		
2115W	RNX609	4040	02	28	3	<0.2	<0.02	<2	08	<2	<0.02		

GRID	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU2	
92115W	ENX611 ENX612	2020	58	55	Nr.	<0.2	<0.02	<2	\$5	<2	<0.02	
92115W	RNX613	4040	50	67	6	<0.2	<0.02	<2	44	<2	<0.02	
92115W	RNX614 RNX614*	4040	87	70	4	<0.2	<0.02	<2	17	<2	<0.02	
92115W	RNX615	4040	65	62	- 6	<0.2	<0.02	<2	75	<2	<0.02	
92115W	RNX617	4040	38	93	5	<0.2	<0.02	22	14	<2	10.02	
92115W	RNX618 RNX619	2040	42	26	4	<0.2	<0.02	<2	194	<2		
92115W	RNX620	4040	37	73	3	<0.2	<0.02	<2	58	<2		
92115w	RNX621*	4040	59	20	4	<0.2	<b>KU.</b> 02	22	112	<2		
92115W	RNX622	4040	58	75	_ <2_	<0.2	<0.02	<2	- 44	<2		
92115W	RNX624	4040	39	86	22	<0.2	<0.02	<2	NSS	NSS		
92115W	RNX625 RNX626	4040	40	81	<2	<0.2	<0.02	<2	. 10	<2	<0.02	
92115W	RNX627	4848	65	68	3	<0.2	<0.02	<2	143	<2	<0.02	
92115W	RNX629	4040	48	65	<2	<0.2	<0.02	22	78	<2	<0.02	
92115W	RNX630	4040	35	63	<2	<0.2	<0.02	<2	20	<2	<u>&lt;0.02</u> <0.02	
92115W	RNX631*	4040	70	71	7	<0.2	10.02	12	1/	12	<0.02	
92115W	RNX633	4040	40	66	ŝ	<0.2	<0.02	<2	99	<2	<0.02	
92115W	RNX634	4040	26	56	6	<0.2	<0.02	<2	NSS	NSS	<0.02	
92115W	RNX636	4040	40	69	4	<0.2	<0.02	<2	<5	<2	<0.02	
92115W	RNX637	4040	40	71	6	<0.2	<0.02	<2	24	<2	<0.02	
92115W	RNX639	4040	38	63	3	<0.2	<0.02	<2	44	<2		
92115W	RNX641	4040	45	71	- 4	<0.2	<0.02	<2	<5			
92115W 92115W	RNX642 RNX643	4040	35	47	< 2	<0.2	<0.02	<2	422	<2		
92115W	RNX644	4040	36	67	3	<0.2	<0.02	<2	78	<2		
92115W	RNX646	4040	38	65	<2	<0.2	<0.02	<2	139	<2		
92115W	RNX647 RNX648	4040	39	58	<2	<0.3	<0.02	<3	<5 12	~3		
92115W	RNX648*	4040	32	82	<2	<q.2< td=""><td>20.00</td><td>&lt;ż.</td><td>····</td><td></td><td>an an a</td><td></td></q.2<>	20.00	<ż.	····		an a	
92115W	RNX650	4040	44	56	2	<0.2	<0.02	<2	432	<2		
92115W	RNX651	4040	56	60	< 2	<0.2	<0.02	<2	25	<2		
92115W	RNX653	4040	53	71	3	<0.2	<0.02	<2	48	<2		
92115W	RNX654 RNX655	4040	55	66	5	<0.2	<0.02	<2	88	<2		
92115W	RNX656	4040	63	51	3	\$0.2	<0.02	<2	139	<2	promptones (company)	inter a series and
92115W	RNX658	4040	19	59	3	<0.2	<0.02	<2	<5	22	1.5.1	
92115W 92115W	RNX659 RNX660	4040	43	60	32	<0.2	<0.02	<2	71	<2	<0.02	
							- SULE LEL					

GRI				EM: DAI	A FROM	1 Carat	oine :	soils						DA
	D	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AUZ		
9211	5 W	RNX661	4040	49	76	4	<0.2	<0.02	8	54	<2	<0.02		
9211	5 W .	RNX662	4040	57	59	4	<0.2	<0.02	<2	173	<2	<0.02		-
21.1	SW	RNX663	4040	46	72	3	<0.2	<0.02	<2	<5	<2	<0.02		
211	2W	RNX664	4040	24	41	3	<0.2	<0.02	<2	\$5	<2	<0.02		
0511	SW SW	RNXODD	4040	40	ón	4	20.5	<0.02	25	19	15	<0.02		
9211	54	RNX667	2020	12	71	3	20.5	20.05	3	201	3	20.02		1.50
7211	5 W	RNX668	4040	49	68	3	<0.2	<0.02	10	~ < 5	<2	<0.02		
9211	5 W	RNX669	4040	60	58	2	<0.2	<0.02	<2	170	<2	<0.02		
211	5W.	RNX670	4040	50	37		<0.2	<0.02	<2	<5	<2	<0.02		
511	2.	RNX0/1	4040	42	20	< 2	50.5	20.02	22	< 3	55	S0.03		
5511	5W	RNX673	2626	57	71	3	20:5	20:05	25	102	25	20.05		
9211	5.	RNX674	4040	58	76	3	<0.2	<0.02	<2	99	<2	<0.02		
9211	5 W	RNX675	4040	71	71	3	<0.2	<0.02	<2	51	<2	<0.02		
9211	5 W	RNX675*	4040	70	70	4	<0.2	6124 82-33	<2	9.47				
9211	5.	RNX676	4040	57	63.	2	<0.2	<0.02	<2	<5	<2	<0.02		
2511	20	RNXC//	4040	46.	94-		50.2	50.02	<u> </u>		- 52		<del></del>	
6511	SW	PNX679	2020	50	65	45	20:5	20.05	25	14	25			
9211	50	RNX680	4040	47	64	ž	<0.2	<0.02	<2	25	25			
9211	5W	RNX681	4040	50	66	3	<0.2	<0.02	<2	20	<2			
9211	5 W	RNX682	4040	61	65	4	<0.2	<0.02	<2	<5	<2			
8211	2W	RNX683	4040	20	62	3	<0.2	<0.02	<2	48	<2			
0211	2W	RNX004	4040	20	20	5	20.5	20.02	25	20	25			
9211	5.	RNX685	2020	53	68	3	20.5	20:05	- 25-	115	- 25	<0.02	a de la compania de l	1
9211	5W	RNX686	4040	37	58	ž	<0.2	<0.02	<2	35	<2	COLOR		
9211	5 W	RNX687	4040	42	56	2	<0.2	<0.02	<2	125	<2			
9211	5W	RNX701	4040	47	62	5	<0.2	<0.02	<2	83	<2		and the second	
9211	2W	RNXTUZ	4040	01	63	3	<0.2	<0.02	<2	67	<2	10.00		
0511	SW SW	PNY704	2020	62	67	42	20.5	20.05	25	12	25	20.02		
9211	5.4	RNX705	2020	74	71	5	20.5	20.02	25	67	3	<0.02		
9211	5W	RNX706	4040	68	66	<2	<0.2	<0.02	<2	38	<2	<0.02		at an infairmere
9211	5 W	RNX706*	4040	66	66	<2	<0.2		<2					
9211	2W	RNX/U/	4040	61	67	2	<0.2	<0.02	<2	19	<2	<0.02		
8511	24	PNY 700	- 2020	- 72	-26		58.5	58.85	4	347		50.05		
9211	50	RNX710	2020	55	57	5	20.5	20.05	<2	50	25	20.02		
9211	5W	RNX711	4040	58	57	2	<0.2	<0.02	<2	58	<2	<0.02		
9211	5W	RNX712	4040	82	68	4	<0.2	<0.02	<2	90	<2	<0.02		
9211	5W	RNX713	4040	121	62	2	<0.2	<0.02	6	58	<2	0.07		
9211	2W	RNX 14	4040	18	69	<2	<0.2	<0.02	<2	20	<2	<0.02		
0211	2W	RNX715	4040	54	47	4	20.2	<0.02	25	151	<2	<0.02		
9211	5.0	RNX716	2020	- 66-			20:5	<0.02	- 25	147	<2	<0.02		-
9211	5W	RNX717	4040	58	63	<2	<0.2	<0.02	<2	83	<2	<0.02		
9211	5W	RNX718	4040	70	57	<2	<0.2	<0.02	<2	77	<2	<0.02		
9211	5W	RNX719	4040	60	58	<2	<0.2	<0.02	<2	10	<2	<0.02		
9211	2W	RNX720	4040	66	56	<2	<0.2	<0.02	<2	19	<2	<0.02		
9211	2W	RNX (21	4040	64	60	<2	<0.2	<0.02	<2	16	<2	<0.02		
0211	5.4	ENY753	4040	200	60	2	20.5	20.05	25	50	25	20.02		

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(	GRID	SAMPLE	PROJECT	CU	ZN	PB	AG	AU	AS	HG	SB	AU2		
	92115W	RNX724	4040	48	52	<2	<0.2	<0.02	<2	80	<2	<0.02		
	test	STD G	4040	47	53	108	<0.2	<0.02	<2	< 5	<2	<0.02	a service a service se	
	test	STD G	4040	95	72	102	0.8		66					
>	test	STD G	4040	90	70	105	0.8		64					
	test	STD G	4040	92	76	110	0.9		70					
	test	STD G	4040	92	20	104	0.8		64					
	test	STD G	4040	90	70	102	0.9		70					
	test	STD G	4040	94	71	108	0.8		66					
	test	STD G	4040	88	70	110	0.9		64					
	test	STD G	4040	90	73	109	0.8		62	-	1	10000		
	test	STD G	4040	20	71	108	Ŭ.8		60				*	
	test	STD G	4040	92	29	102	0.9		64					
	test	STD G	4040	ē ģ	66	104	0.8		64		and the second sec		CONTRACTOR SAL	
	test	STD G	4040	81	72	110	0.8		70					
	test	SID G	4040	10 <u>ģ</u>	- 70	110	0.8		66					
	test	STD G	4040	91	72	100	1.0		68					
	test	STD G	4040	85	72	105	0.7		64					
	test	STD G	4040	89	20	105	0.8		66	· · · · · · · · · · · · · ·			(and a second se	
	test	STD G	4040	96	72	104	0.8		66					
	test	STD G	4040	26	72	105	0.8		64					
	test	STD G	4040	90	67	101	0.8		72					esteration de
	test	STD G	4040	91	20	107	0.8		<u>68</u> 70					
	test	STD G	4040	89	66	100	0.8		64					
	test	STD G	4040	88	21	100	0.7		66					
	test	STD G	4040	89	70	108	0.8		66					
	test	STD G	4040	92	69	108	0.7		68					
	test	STD SB	4040	22.5	-		0.0		00		124			
	test	STD SB	4040								124			
	test	STD SB	4040					an a sama sana tana tana sa kana jina	and the second	1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917	124			
	test	STD SB	4040								129			
	test	STD SB	4040								126			
	test	STD SB	4040								134			
	test	STD SB	4040								136			
	test	STD SB	4040								126	••••••••••••••••••••••••••••••••••••••	and the second second	
	test	STD SB	4040								124			
	test	STD SB	4040								126			

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									DOGICOT	CANOL C	COIN
	SB	НG	AS	ΑU	AG	PB	ZN	ιu	PROJECT	SAMPLE	GEID
	<2	74	<2	<0.02	<0.2	11	74	51	4233	0 Q 1	R N X
	\$2	190	<2	50.02	<0.Z	20	64	21	4322	204	RNX RNX
	12	110	15	10.02	20.5	7	22	12	4200	202	NX
	25	>2000	25	<0.02	<0.5	\$	65	42	4527	805	NX
	<2	430	<2	<c.c2< td=""><td>&lt;0.2</td><td>10</td><td>73</td><td>29</td><td>4203</td><td>806</td><td>R N X</td></c.c2<>	<0.2	10	73	29	4203	806	R N X
		120	- <ž-	<0.02	<0.2	9	70	39	4283	807	RNX
	<2	290	<2	<0.02	<0.2	2	65	36	4203	308	R N X
	53	350	~~	<0.02	20.2	00	70	47	4202	210	
	25	1120	25	20.05	20.5	ž	21	57	752+	811	XX
	<2	150	<2	<0.02	<0.2	ž	76	48	4283	812	NX
	<2	230	<2	<0.02	<0.2	8	77	46	4267	813	INX
	<2	210	<2	<0.05	<0.2	6	69	45	4203	814	NX
1991 - Constant Constant (1997 - 2007) (1978 - 2007)		360	2	\$0.02	50.2	-11-	60	70	428	815	NX
	12	220	3	20.02	21.5	7	8.0	40	22947	×17	NX
	67	280	<2	<0.02	6.2	ċ,	96	43	4283	618	NX
	<2	210	<2	<0.02	<0.2	10	78	5 Č	4283	819	NX
	<2	230	<2	<0.05	<0.2	Č,	80	52	4283	320	NX
	<2	400	<2	<0.02	<0.2	19	1/1	e s	4 3 3 4	021	NX
	~~	100		KU.L2	50.5		1.0		4:0-	893	N A
	3	600	3	20:05	20.2	13	75	¢7	4283	824	NX
	16	>zóŏŏ	<2	<0.02	<0.2	15	24	111	4287	825	NX
	20	>2000	<2	<0.02	<6.2	17	95	107	4283	826	NX
	<2	68	<2	<0.02	<0.2	9	66	75	4283	827	NX
	<2	40	<2	<0.02	<0.2	8	52	10	4537	0278	IN X
	25	24	19	20.02	20.5	2	72	164	2587	222	NX
		- 53		C.P2-	20.2	- 6	77-	-102-	4221	-936	NX
	<2	34	<2	<0.02	<0.2	7	60	56	4203	871	NX
	<2	34	<2	<0.02	<c.2< td=""><td>7</td><td>27</td><td>82</td><td>4283</td><td>832</td><td>h.X</td></c.2<>	7	27	82	4283	832	h.X
	<2	25	<2	< <u>0.02</u>	<0.2	2	11	57	4281	635	NX
	22	40	25	20.02	20.5	C x	67	21	4201	875	NX
	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	65	22	20.05	20.2	00	72	79	2223	836	NX
	<2	43	<2	<0.02	<0.2	8	70	76	4283	536×	NX
		160	- <2-	<0.02	<0.2	3			4283	837	NX
	<2	47	<2	<n. n2<="" td=""><td>&lt;0.2</td><td>ć</td><td>64</td><td>64</td><td>4203</td><td>010</td><td>N X</td></n.>	<0.2	ć	64	64	4203	010	N X
	22	54	24	CU.U2	20.2	0	CU A/	21	4201	224	N A
	15	21	25	20.05	20:5	2	61	73	1552	241	NX
	<2	37	<2	<0.02	<0.2	7	66	64	4233	842	NX
	<2	74	<2	<0.02	<0.2	9	FÜ	71	4283	843	N X
	<2	47	<2	<0.05	<0.2	9	f 4	52	4783	844	NX
-	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	74		10.05	0.5	2	22	40	423	846	NX
	25	12	25	20.05	20.5	7	67	24	2523	647	NX
	22	19	<2	<0.02	20.2	è	64	ĒŠ	4233	248	NX
	<2	40	<2	<0.02	<0.2	7	61	45	4263	849	NX
	<2	124	<2	<0.02	<0.2	.9	51	42	4283	850	NX
	<2	81	<2	<0.05	<0.2	10	50	53	4283	621	NX

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PLACER	GEOCHEM /	ASSAY SYSTE	M: DAT	A FROI	M Cara	bine	R. Boy	се					ſ	DATE
GRID	SAMPLE	PROJECT	CU	ZN	PB	AG	UA	AS	HG	SB				
RNX	853	4263	57	65	7	<0.2	<0.02	<4	10	<2				
RNX	824	4283	44	20	2	20.3	20.05	23	20	25				
RNX	855	2587	52	62	6	20.5	20.05	<2	<5	<2				
RNX	856	4233	47	63	7	<0.2	<0.02	<2	19	<2				
RNX	857	4203	41	60	6	<0.2	<0.02	<2	53	<2	1			
RNX	858	4283	43	52	9	<0.2	<0.05	<2	68	<2				
RNX	859	4283	42	28	10	<u.2< td=""><td>&lt;0.02</td><td>25</td><td>24</td><td>25</td><td></td><td></td><td></td><td></td></u.2<>	<0.02	25	24	25				
RNX	864	1582	44	22	1 L	20.5	20.05	25	45	25				
RNY	862	2582	45	53	12	20.5	<0.02	25	16	<2				
RNX	863	4283	57	63	ģ	<0.2	<0.02	<2	105	<2				
RINX	864	4283	43	62	10	<0.2	<0.02	<2	22	<2				
RNX	865	4287	50	64	8	<0.2	<0.02	<2	34	<2				
RNX	866	4283	10	25	10	<0.2	<0.02	~~~	120	~~~				
RNA	6001	1583	40	65	10	20.2	20.02	25	50	25		9		
RNX	375	2283	54	80	ģ	<0.2	<0.02	<2	43	<2				
RNX	870	4283	45	72	9	<0.2	<0.02	<2	310	<2				
RNX	871	4283	48	72	8	<0.2	<0.02	<2	50	<2				
RNX	872	4283	41	70	9	<0.2	<0.05	<2	56	<2				
RNX	872*	423	41	/0	Š	<0.2	<0.02	<2	43	<2				
RIX	543	4502	40	100	Ş	10.2		.5	81					
RNX	875	2223	77	65	6	20.2	20.02	25	67					
RNX	875*	4283	39	65	ĕ	<0.2		<2						
test	STD G	4233	90	76	112	0.7		60						
test	STD G	4283	29	76	110	Q.7		64						
test	STD G	4284	91		110	2.5		00						
test	SID U	420:	. C	- 4	110	0.1		cu_		150				
test	STD SP	1583								146				
test	STO SE	2383								160				
test	STD AU	4283					0.65			2 7 T				
test	STD AU	4283					0.70							
test	STD AU	4283					0.62							
test	STD AU	4235					0.00		205					
test	SID HG	4203		-					- 200	وبالريقية المعالمة			and a million	
test	STD HG	2524							320					
test	STD HG	4203							290					
3 2 5 5		A												

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END OF LISTING - 95 RECORDS PRINTED GCLIST RUN AT: 09:42:57

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		- a la constante de la competencia				موريح مريد المراجع	(					مرود و سرو بومرود	ىرىدى مۇممۇر مۇمىيۇ سى	-(
	PLACER	GEOCHEM	ASSAY SYSTE	M: DATA	FROM	Carab	ine	R. BO	yce					
	GRID	SAMPLE	PROJECT		€ <del>∪</del> —	- Z N-		AG		AS	HG	BA		
5	92115W 92115W	75801	4038	22	35	64	07	<0.2	<0.02	<22	\$25	0.04	~~~~	
	92115W	75804	4038	220	51	73	777	<0.2	<0.02	<22	155	0.03	~~~~	
	92115W	75806	4038	122	56	564	1ģ	<0.2	<0.02	22	25	0.06	<22	
	92115W 92115W	75808	4038	222	49	59	9	<0.2	<0.02	<22	<5	0.05	<22	
	92115W 92115W	75809* 75810	4038	22	41	63	7	<0.2	<0.02	<22	32	0.03	<2	
	92115W 92115W	75811 75812	4038	23	35	67	68	<0.2 <0.2	<0.02	<22	<5 14	0.05	<22	
	92115W 92115W	75813	4038	~~~~~	50 31	63	6	<0.2	<0.02	<2	25	0.03	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	
	92115W 92115W	75816	4038	1	55	71	4	<0.2	<0.02	< 22 22	50	0.03	~~~	
	92115W	75818	4038	20	41	597	4	<0.2	<0.02	<22	14	0.02	<22	
	92115W	75819	4038	1	64	69	6	<0.2	<0.02	~~~	22	0.02	<22	
	92115W	75821	4038		37	58		<0.2	<0.02		230	0.03		
	92115W 92115W	75823	4038	1	45	59	56	<0.2	<0.02	<22	14	0.02	<2 <2	
. 3	92115W 92115W	75825 75826	4038	52	22	31 68	117	<0.2 <0.2	<0.02	<2	40 <5	<0.02 <0.02	<2 <2	
TOVAL	92115W 92115W	75827 75828	4038	2	31	56	57	<0.2	<0.02	<22	<5 40	<0.02	<2	
AU	92115W	75820	4038	2	22	49	4	<0.2	<0.02	<2	<5	<0.02	<2	
	92115W	75832	4038	2	84	53	10	<0.2	<0.02	~~~~	50	0.02	<2	
	92115W	75834	4038	סויזר	22	60	056	<0.2	<0.02	~~~	79	<0.02	<22	
	92115W	75836	4038	1	65	697	58	<0.2	<0.02	<22	58	0.03	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	
	92115W	75838	4038	1	63	60	77	<0.2	<0.02	<2	14	0.02	<2	
	92115W 92115W	75840	4038	2	80 50	49	10	<0.2	<0.02	<22 <22	25	0.02	<22	
	92115W 92115W	75842 75843	4038	1	51	71	10	<0.2	<0.02	<2	182	0.03	<2	
	92115W 92115W	75844	4038		67	60	77	<0.2	<0.02	<2	<5 35	<0.02	<2 <2	
	92115W 92115W	75846	4038	<1	63	70	9	<0.2	<c.d2 &lt;0.02</c.d2 	<2 <2	133	0.03	<2	
	92115W 92115W	75848	4038	1	34	64	87	<0.2	<0.02	<2	25	0.04	<22	
	92115W 92115W	75850	4038	1	64	66	87	<0.2	<0.02	<2	175	0.04	<2	
	92115W	75852	4038	2	60	72	8	<0.2	<0.02	<2	<5	0.02	<2	

PLALER	GEUCHEM A	SSAY SYSTE	M: DATA	FROM	Carab	ine	R. BO	yce				· ·	
GRID	SAMPLE	PROJECT	MO	_ cu	Z N	PB	AG	AU	AS	HG	BA	SB	
92115W 92115W 92115W	75853 75854 75855	4038 4038 4038	1 2	67 39 79	74 48 61	8000	<0.2 <0.2 <0.2	<0.02 <0.02 <0.02	<22	<5 425	0.03	<22	
92115W 92115W 92115W	75856 75857 75858	4038 4038 4038	211	55 62 57	79 63 66	10	<0.2 <0.2 <0.2	<0.02 <0.02 <0.02	<22	<5 <5 <5	<0.02 0.03 0.03	<22	
92115W 92115W	75859	4038	2	<u>81</u> 38	58	8	<0.2	<0.02 <0.02	<2	25	0.02	<2	
92115W 92115W	75861 75862	4038	1	52	60	66	<0.2	<0.02	<2 <2	32	<0.02	<22	
92115W	75863*	4038	1	40	61	70	<0.2	<0.02	<22	<5	0.02	<22	
92115W	75865	4038	1	64	53	10	<0.2	<0.02	<22	84	<0.02	~~~	
92115W 92115W	75867 75868	4038	1 2	50	56	11	<0.2	<0.02	<2	39	0.02	<22	
92115W 92115W	75869 75870	4038	1	33	54	11	<0.2	<0.02	<2 <2	39 <5	0.03	<2 <2	
92115W 92115W	75871	4038	1	31	63	10	<0.2	<0.02	<2 >	4000	0.02	222	
92115W	75873	4038		154	47	2	<0.2	<0.02	~~~ >	4000	<0.02	52	
92115W 92115W	75875	4038	<1	50	66 68	66	<0.2	<0.02	<22	91 112	0.02	<22	
92115W 92115W	75877 75878	4038	<1	48 26	53	10	<0.2	<0.02	<22 <2	14	0.05	<22	
92115W 92115W	75879	4038	<1	70	79	96	0.4	<0.02	<22	126	0.04	<2<	
92115W	75881*	4038	<1	34	53	10	0.2	<0.02	<2	- <5_	0.02	<2	
92115W	75883	4038	2	23	65	67	<0.2	<0.02	<22	28	0.03	<22	
92115W 92115W	75885 75886	4038	NN.	38	54	79	0.2	<0.02	<22	112	0.02	<22	
92115W 92115W	75887	4038	2	47	53	7	0.3	<0.02 <0.02	<2	77	<0.02	<2 <2	
92115W	75890	4038	1	79	45	87	<0.2	<0.02	<22	168	<0.02	<22	
92115W	75892	4038	21	84	65	11	0.3	<0.02	<22 >	4000	<0.02	<22	
92115W 92115W	75894 75895	4038	1	28	56	97	<0.2	<0.02	<22	<5	0.02	~~~	
92115W 92115W	75896 75897	4038	2	33 41	69	7	<0.2	<0.02	<2	<5	<0.02	<2	
92115W 92115W	75898	4038	1	47	59	77	0.3	<0.02	<22 <22	81	0.02	×22	
92115W	75901	4038	1	3301	69	057	<0.2	<0.02	~~~	18	<0.02	<22	
92115W	75903	4038	1	32	62	6	<0.2	<0.02	<2	14	0.02	<2	

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GRID	SAMPLE	PROJECT	- *0		2 N		- AG	AU	A 5-	HG			
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test test test test test test	STD G STD G STD SB STD SB STD SB STD SB STD SB	14444444444444444444444444444444444444	13	98 95	73	110	0.8		62			126 120 132 132	
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test test test test test test test	STD BA STD BA STD BA STD HG STD HG STD HG STD HG	14444444444444444444444444444444444444						1.95		403 410 361 473 385	0:54		
test END OF GCLIST	STD HG LISTING - RUN AT: 16	4038 140 RECO	ORDS PR	INTED						417			
										-			

GRID	SAMPLE	PROJECT		ZN	PB	AG	AU	AS	нg	BA	SB			
2115w 2115w 2115w 2115w 2115w 2115w 2115w	RNR1 ENR2 RNR3 RNR45 RNR5 RNR5	5555555 2122222 44444 4444	7420764	45095300	586 1146			104	140 < 660 < 840 < 140 2000 <	0.02				
2115W 2115W 2115W est est est	KNRB KNRO STD G STD SB STD HG	42223855	677 94	5806G	10 106	<0.2 <0 <0.2 <0 0.7	02	<22 72	110 590 < 310	0.02	<2 <2 140			
ND OF I	LISTING - Run at: Ca	12 REC( :34:44	OPDS PR	INTED								•	et samtat, no estande e	
a		- Walan ang ang ang ang ang ang ang ang ang a	• • • • • • • • • • • • • • • • • • •	CHICKE SPECIFIC SECTION			- Maria Managara da Maria da M							<b>() - 1</b> () () () () () () () () () () () () ()
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PLACER GEOCHEM ASSAY SYSTEM: DATA FROM Carabine R. Boyce 6 1.00 GRID SAMPLE PROJECT MO CU ZN PB AG AU AS HG SB 4039 4039 4039 4039 4039 <0.2 <C.02 <0.2 <C.02 <0.2 <0.02 <0.2 <0.02 <0.2 <0.02 <0.2 <0.02 <0.2 <0.02 <0.02 <0.02 <0.02</pre> 92115W 92115W 92115W 92115W 92115W 152 112 267 87 105 Ę. 127 91 5555557 RNB1 <1 35338 RNB2 RNB3 -1 RNB4 888 RNB4\* ٩\_ 4039 STD G 13 110 test 132 test STD SB 4039 STD HG 301 test 1.93 STD AU test 1 GCLIST RUN AT: 13:09:17 1 63 3 14 2.11 AUTOVALU 4 3 . 6 . And the second s



APPENDIX D

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HISTO: REN SOIL RUN ON 84:06:05 Field name: CU LOG = O File: EXPL\*RNX. k ----14.0000 MAXIMUM: STD. DEV.: STATISTICS: MINIMUM: 133.000 MEAN: Sec. 712 VALUES PLOTTED ( O OUTSIDE RANGE O NULLS) SCALE OF HISTOGRAM IS 2.00 COUNTS/PRINT POSTIION MIDPOINT PERCENT O 20 60 40 80 -1-- 1 ---16:995 :28 Ī\*\* I\* 2.81 1\*\*\*\*\*\*\* 15 19.950 2030 22.925 \*\*\*\*\* \*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\* n 2564 31.850 3.93 -33 34 825 37 800 40 775 8.9 0 75 63 59 41 43.750 10. \*\*\*\*\*\*\*\* 46.725 8.8 \*\*\*\*\* 5. \*\*\*\* 55.650 58.625 61.600 64.575 403125 \*\*\*\*\*\*\* 5.62 AUTOVALU 4.3 \*\*\*\*\*\*\*\*\* 3.51 -12 67.550 1.69 1\*\*\*\*\* 70 525 73 500 76 475 .84 .56 6 1\*\*\* -I \* \* I \* \* .70 I\*\*\* 79.450 5 82 425 85 400 88 375 •28 I\* - 84 •14 I\* •42 I\*\* 91.350 94.325 97.300 100.27 .14 I\* :14 I\* I .14 1\* 20 103.25 .00 T 106.22 .00 n I :00 ň ī 12.00 Π 115.15 .00 Т 118.12 121.10 124.07 .00 0 I 1 \* 0 .00 1 127.05 0 .00 I .00 I 1 \* I -712 20 40 60 80 Ū

HISTO:		1.700-1.100	REN SOIL			f	UN ON 84:06:05
File; E	XPL*RNX.		Field name:	ZN LO	G = 0	4	
STATIST	162:	MINIMUM: MEAN:	15.0000 68.0449	MAXIMUM: STD. DEV.:	164.000		
712 V	ALUES PL	OTTED (	O OUTSIDE RANGE	O NULLS	,		
SCALE	OF HIST	OGRAM IS	4.00 COUNTS/PRIM	T POSTIION			
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1	15.000	·14 1			1		
	18.725	•28 I* •14 I		Drive	<u> </u>	····· .	and Artennia
6	26.175	.56 I*			· · · · · · · · · · · · · · · · · · ·		
4	33.625	•56 I*		······································	260 <b>- 1</b>		
40	41.075	.56 1			1		
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100	59.700	14.04 14	**************	********	** 1		
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61	74.600	8.57 1	***********		į		
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14	89.500	1.97 1	***	2	i		
13	93.225	1.83 1*	**		I.	بركيب الجاهرية الشامر ووجع بمعمو وسوية للتربي	
52	100.67	.70 1			Į		
3	108.12	.42 1*	<u>← 110</u>		i	->	
6	115.57	.84 1*	*		1		•
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	126.75	:12 1	$ \mathbf{x}_{i}  \leq 1 \leq 1$ , for the product of the product of the H state $\mathbf{x}_{i}$ and $\mathbf{y}_{i}$	artin dae waar na di na mad shareen ar a shara a s	i	an a	and a second state of the
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1	156.55	.00 1			<b>I</b>		- المحمد الم
9	160.27	:00 1			Į		
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	HISTO:		REN SO	11		,	RUN ON 84:06:05
]	File: EXPL*RNX	•	Field n	ame: PB	L06 = 0		
	STATISTICS:	MINIMUM: MEAN:	1.00000 6.18680	MAX STD.	IMUM: 13.00 DEV.: 2.381	00 41	
$\sim$	712 VALUES P	LOTTED (	O OUTSIDE R	ANGE O	NULLSY	•	
	SCALE OF HIS	TOGRAM IS	4.00 COUNTS/	PRINT POST	IION		
	N MIDPOINT	PERCENT C	40	80	120	160	
		3.93 1	******			I	
	30 1.9000 0 2.2000	4.21 I 4.21 I .00 I	******			I	÷
	0 2.8000 43 3.1000 0 3.4000	6.04 I 6.04 I	**********			İ	(me)
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AU (M		17.98 I	******	********	****	İ	7
a l	0 7.3000 0 7.6000 103 7.9000 0 8.2000 0 8.5000	.00 I .00 I 14.47 I .00 I .00 I	*****	*****	***		na na seconda e e e e e e e e e e e e e e e e e e e
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	36 10.000	5.060 1	*****			1	
	15 10.900	2.11 1	****			<u> </u>	
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	0 12.700 2 13.000	.00 1 .28 1	*	1		1 <sup>1</sup>	
-	712	ĉ	40	8Ô	120	160	

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HISTO:	REN LITHO	EOCHEM	•	RUN ON 84:06:0
File: EXPL*RNR	• Field r	ame: CU LOG	= 0	
STATISTICS:	MINIMUM: 6.00000 MEAN: 49.7830	STD. DEV.:	154.000	
106 VALUES P	LOTTED ( O OUTSIDE I	ANGE O NULLS)		na an an an an an an an an an an an an a
SCALE OF HIS	TOGRAM IS .33 COUNTS,	PRINT POSTIION		
N MIDPOINT 1 6.0000 0 9.7000	PERCENT 0 3 II .94 I*** .00 I	10 10	13 1 I	
0 17.100 3 20.800 5 24.500	.94 1*** .00 1 2.83 1******** 4.72 1*********	** 30	Ì	
12 28.200 12 31.900 11 35.600 11 39.300	1.89 I****** 11.32 I************ 10.38 I************ 10.38 I*************		******	
2 43.000 6 46.700 13 50.400 1 54.100	1.89 1***** 5.66 1***********************************	***** - 45 ************************************	******	
5 57 800 7 61 500 8 65 200 2 68 900	4.72 I************************************	************		
2 72.600 3 76.300 5 80.000 3 83.700	1.89 I****** 2.83 I******** 4.72 I********* 2.83 I********	**	I I I	
0 91.100 0 94.800 0 98.500	•00 I •00 I •00 I •00 I			
0 102.20 0 105.90 0 109.60 0 113.30	•00 I •00 I •00 I	4	I	
0 120.70 0 124.40 0 128.10	.00 I .00 I .00 I			
0 131-80 0 135-50 0 139-20 0 142-90 0 146-60	00 I 00 I 00 I 00 I 00 I			
1 154.00	.94 I*** II 0 3	I	<sup>1</sup> 13	





•	HISTO	:		REN LITHOGEOCHEM	RUN ON 84:06:0
	File:	EXPL*RN	R •	Field name: AG LOG = 0	r.
	STAT	STICS:	MINIMUM: MEAN:	:100000+000 STD. DEV.: :585617-00	
	100	VALUES	PLOTTED (	O OUTSIDE RANGE O NULLS)	
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	ğ	.39250	:00		I
-	1	•40000	.94		1

6 HISTO: REN LITHOGEOCHEM RUN ON 84:06:05 A File: EXPL\*RNR. Field name: BA LOG = 0C .100000-001 .700000-001 STATISTICS: MINIMUM: MAXIMUM: MEAN: .250943-001 STD. DEV .: 6 106 VALUES PLOTTED **O OUTSIDE RANGE** O NULLS) C SCALE OF HISTOGRAM IS 1.00 COUNTS/PRINT POSTIION N MIDPOINT PERCENT D 10 30 20 40 . -1------!-.10000-001 25.47 I\* 27 Ô .11500-001 .00 •13000-001 •14500-001 •16000-001 .00 .00 Ū ğ .17500-001 19000-001 20500-001 .22000-001 .00 33.96 00 3ĕ 1 \* \* \*\*\*\*\*\*\*\*\*\*\*\*\*\* 1 õ .23500-001 .00 •25000-001 •26500-001 •28000-001 000 .00 .00 1 L 22 .29500-001 20.75 1\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* 000 •31000-001 •32500-001 •34000-001 AUTOVALU 1 Õ .00 .35500-001 1 •37000-001 •38500-001 •40000-001 -00 7-55 O Т 5 Ī 1 \*\*\*\*\*\*\* Ř 1 .41500-001 .00 0 1 :00 Ō .43000-001 .44500-001 1 T - 0.5 Õ .46000-001 .00 1 .00 0 .47500-001 5 1 9.43 1\*\*\*\*\*\*\*\* D 10 .52000-001 .00 0 1 L Ô .53500-001 .00 I .55000-001 .00 0 .56500-001 0 1 Õ .58000-001 .00 I 1 .59500-001 1.89 I\*\* .00 .61000-001 :22000-001 .65500-001 .00 0 I .00 .00 .94 .67000-001 .68500-001 .70000-001 0 I Ĩ I\* 6 106 10 20 30 40 . 3



















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