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11/85

# REPORT ON THE KALUM MINERAL CLAIM GROUP FOR BRADNER RESOURCES LTD. SKEENA MINING DIVISION BRITISH COLUMBIA

NTS 103I/10 and 15W
LAT. 54° 41'North, LONG. 128° 45'West

George Cavey
Diane Howe
November 19, 1984

## SUMMARY

The Kalum mineral claim group held in agreement by Bradner Resources Ltd. of Vancouver is located along the west shore of Kitsumkalum Lake approximately 32 kilometers north of Terrace, B.C.

The oldest rocks in the claim area are argillites and greywackes belonging to the Upper Jurrasic-Lower Cretaceous Age Bowser Group. Intrusive to the sediments are suites of granitoid rocks including granodiorite, diorite, monzonite and related rocks collectively termed the Coast Intrusions. Hybassal dikes believed related to the latter stages of the Coast Batholith also form a distinctive group within the claim area.

Exposed mineral showings on the Kalum property are the old "Portland" showings which consist of two separate quartz veins which contain appreciable values in gold and silver and are host in a quartz diorite stock.

The only recorded work on the Portland showing was in 1922-1923 when Kalum Mines Ltd. sunk two inclined shafts on the main vein, one to 30 feet and the other to 60 feet from which a drift was run westerly for 210 feet. Three hundred feet southeast of the shafts an adit had been driven for 85 feet to follow the second vein.

In late November 1983 and April 1984, the Kalum Lake Mining Group Ltd. did some hand trenching and blasting with follow up backhoe trenching on the area of

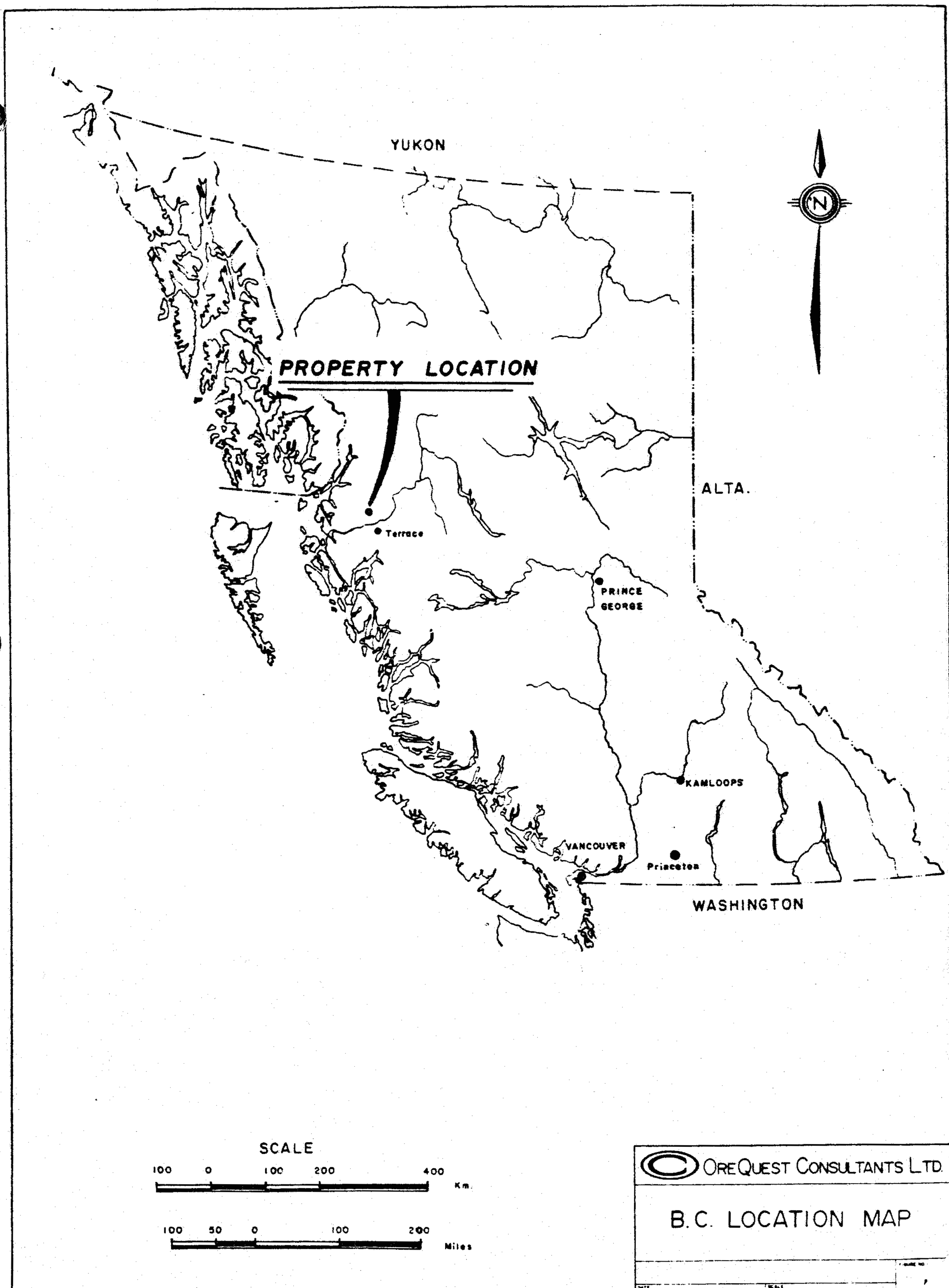
the old "Portland Group". The second vein was extended along strike for approximately 30 metres.

The Kalum Lake Mining Group also conducted some regional prospecting from which a third area of interest was discovered and subsequently staked.

The 1984 field program consisted of a soil geochemical survey over the third area (south showing) of which 576 soil and 17 rock samples were collected in an attempt to detect more auriferous quartz veins.

Results of this years program has produced favourable and encouraging results enough to recommend continuation of the work program.

Phase II should consist of linecutting (20 kilometers), detailed sampling, mapping and trenching. Phase III contingent on favourable results of Phase II should consist of 1,000 metres of overburden drilling or 375 metres of diamond drilling.


YUKON
PROPERTY LOCATION
Terrace
ALTA.
PRINCE GEORGE
KAMLOOPS
VANCOUVER
Princeton
WASHINGTON
N
SCALE
100 0 100 200 400
Km.
100 50 0 100 200
Miles
OREQUEST CONSULTANTS LTD.
B.C. LOCATION MAP

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# 1. INTRODUCTION

This report is a summary report on the soil geochemical survey conducted in late September of this year on a portion of the Kalum mineral claim group held in agreement by Bradner Resources of Vancouver.

This report briefly summarizes exploration done to date and presents recommendations for further work. Information contained in this report is from data collected during late September and early October of this year, the authors field examination in late September, as well as information obtained through various government and private publications listed in the bibliography.

## 1a. LOCATION and ACCESS

The Kalum mineral claim group is 32 kilometers north of the city of Terrace located in west-central B.C. The claim block is situated on the west shore and partly straddles Kitsumkalum Lake, and is centered at 54° 45' North Latitude and 128° 45' West Longitude on NTS map sheet 103I/10, 15W (Figure 1).

Easy access is provided to the claims by an all weather gravel road which leaves the Yellowhead #16 Highway approximately 5 kilometers west of Terrace and proceeds for 32 kilometers passing through the middle of the claim group.

The majority of the claim group is accessible by several old, 2 wheel drive logging roads which exit off the main access road.

Supporting infrastructure is well established with the main power transmission line which supplies power to the Nass Valley passing through the claim group, while the CNR Prince Rupert rail line which roughly follows the Yellowhead #16 Highway across B.C. is located 32 kilometers south of the property.

Pacific Western and Canadian Pacific Airlines have daily scheduled flights from Vancouver to Terrace daily.

1b. PHYSIOGRAPHY

The property is located at the divide of the Pacific Ranges of the Coast Mountains and the Hazelton Mountains of the Intermontane Physiographic Belt.

The Kitsumkalum Valley is typical of a wide glaciated valley with flat, gently rolling valley bottoms to steep, rugged mountain flanks. Elevations on the property vary from 500-1,500 feet ASL.

The area is well timbered with cedar, hemlock, fir and spruce with choking intergrowths of alder and willow.

The majority of the claims lie on the west shore of Kitsumkalum Lake which would provide enough water for any further exploration and development. The Nelson River, which crosscuts through the Burn 2 and 3 claims, would also provide adequate water for any drilling to be done. It should be noted at this point that the majority of the Trench claims are overlain by Kitsumkalum Lake.

Thick glacial depris consisting of clay, sand and till blanket at least 60% of the claim area.

## 1c. PROPERTY INFORMATION

The Kalum group of claims consist of 5 claim blocks totalling 87 units. All claims are owned by J. Apolzer of Terrace, B.C. and by agreement Bradner Resources Ltd. of Vancouver. The details of the agreement are beyond the scope of this report.

The following table summarizes pertinent data for the claim block:

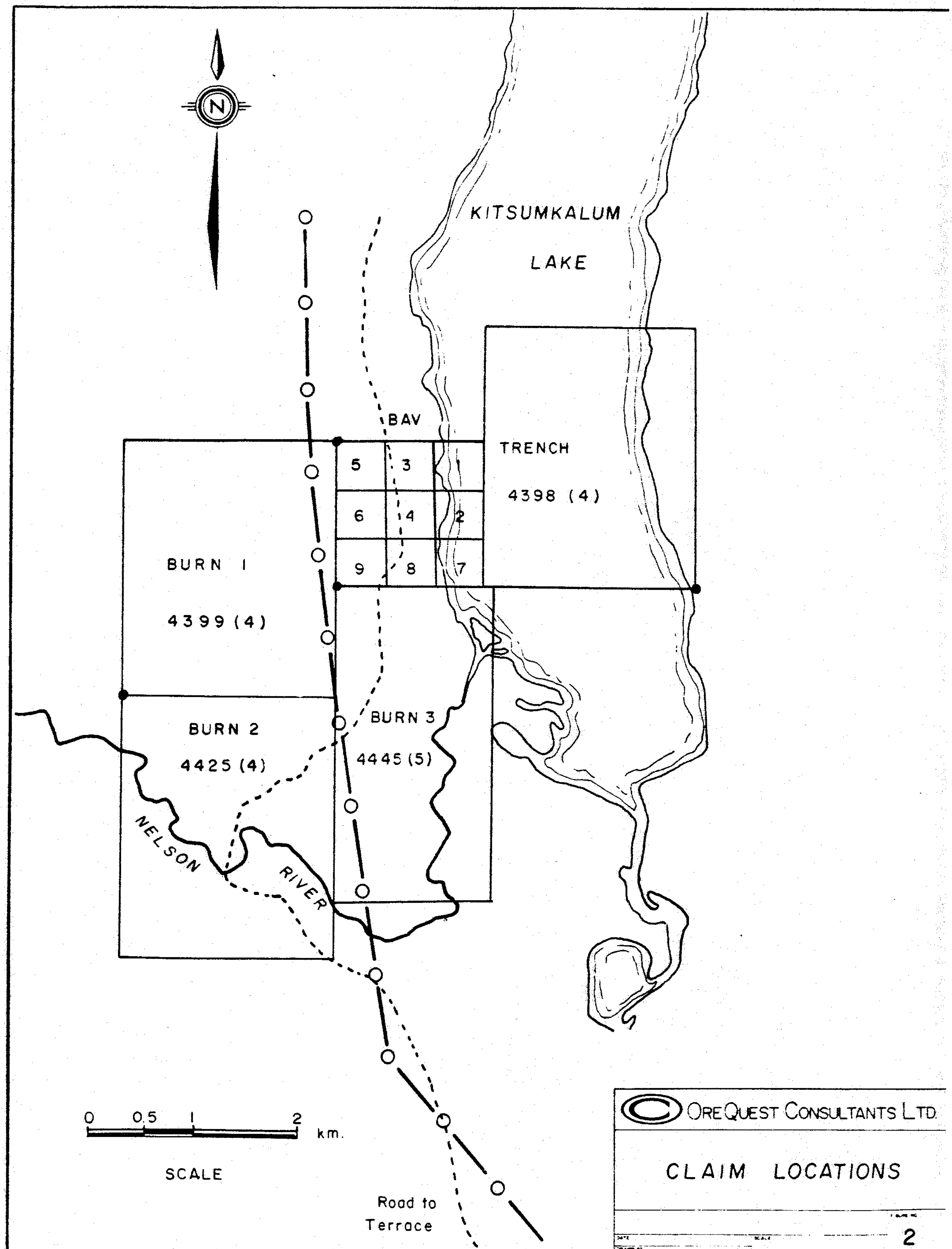
| Claim Name | Units | Record # | Anniversary Date | Year* |
|---|---|---|---|---|
| Bav 1-4 | 4 | 37397-37400 | July 21, 1990 | 1994 |
| Bav 5-9 | 5 | 4223-4227 | November 28, 1984 | 1994 |
| Trench 1 | 20 | 4398 | April 13, 1985 | 1988 |
| Burn 1 | 20 | 4399 | April 13, 1985 | 1987 |
| Burn 2 | 20 | 4425 | April 27, 1985 | 1987 |
| Burn 3 | 18 | 4445 | May 11, 1985 | 1987 |

*Pending approval of this years assessment.

All claims are located in the Skeena Mining Division of B.C. (see figure 2).

## 1d. HISTORY and PREVIOUS WORK

Earliest recorded activity on the Kalum property is 1919 when C.A. Smith of Terrace staked the original Lakeside claims, with the Portland and West Portland claims to follow in 1922. Between 1923 and 1925 the newly formed Kalum Mines Ltd. conducted considerable work on the property, which consisted of shaft sinking and drift development along the main vein discovered in 1919. Two shafts were sunk with the east shaft reaching 30 feet (9.1 metres) depth and the main or west shaft developed to 60 feet (18.2 metres) with 210 feet (64.0


N
KITSUMKALUM
LAKE
BAV
5
3
1
6
4
2
9
8
7
TRENCH
4398 (4)
BURN 1
4399 (4)
BURN 2
4425 (4)
BURN 3
4445 (5)
NELSON
RIVER
0
0.5
1
2
km.
SCALE
Road to
Terrace
OreQuest Consultants Ltd.
CLAIM LOCATIONS
2

metres) of drifting westerly along the vein. A selected grab sample collected in 1930 assayed 0.62 oz/t gold and 2.2 oz/t silver.

Approximately 300 feet southeast of the main vein, Kalum Mines Ltd. put in a third adit along a #2 vein extending 85 feet (25.91 metres). Assay values from this vein in 1937 contained only minor amounts of gold and silver.

In 1972, the original claims were restaked as the Bav 1-4 by J. Apolzer of Terrace, B.C. One drill hole totalling 374 feet was drilled in an attempt to intersect the main vein. Drill records indicate that the main vein was not intersected, but granodiorite with areas of quartz veining and minor alteration were intersected. Gold and silver values range from 0.002-0.011 oz/ton and 0.08-0.02 oz/ton respectively. From studying the drill hole plan, it appears that this drill hole was drilled almost parallel to the strike of the main vein.

In November of 1983, Kalum Lake Mining Group, of which Mr. Apolzer the present property vendor is a partner, trenched and sampled the Main and #2 veins. Values up to 7.328 oz/t gold and 6.58 oz/t silver were received in a few grab samples collected from the #2 vein extension. A total of five trenches were dug utilizing a traxcavator backhoe accompanied with blasting and hand trenching. Several of the trenches did not reach bedrock and were abandoned after the stability of the slopes became hazardous.

Just to the west of the Kalum Lake Mining claims, Campbell Resources Ltd. is presently conducting a drilling program on their Misty claims. Staked as a result of the release of the 1979 Silt Geochemistry Survey by the Government, Campbell Resources Ltd. has outlined areas of high gold interest by using soil geochemistry in what is felt to be the same type of environment as the Kalum mineral showings. No further work has been reported since 1982, but Campbell is still drilling on this property.

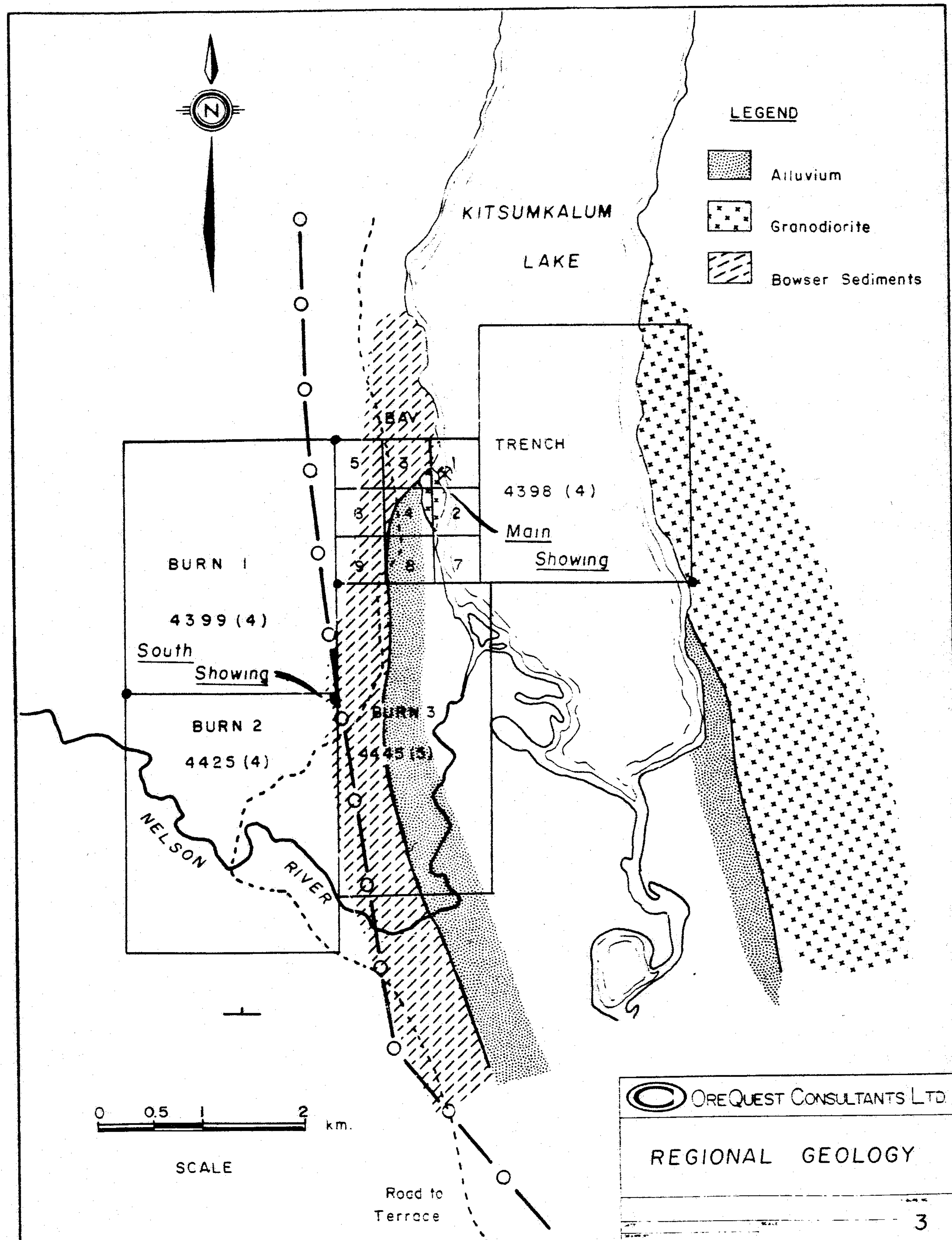
## 2. 1984 FIELD WORK

The 1984 field work was carried out by Mr. Ian Dow of Terrace under the guidance of Diane Howe, OreQuest Consultants Ltd. of Vancouver. The quality of work carried out by Mr. Dow and the efficient manner in which the work was completed has been excellent.

### 2a. GEOLOGY

Bedrock exposure along the valley bottom is sparse and is largely confined to the shore of Kitsumkalum Lake, streams, gulleys and old trenches on the property. A thick layer (up to 60 metres) of glacial alluvium masks at least 60% of the claim area. Towards the west edge of the Burn 1 and 2 claims outcrop exposure becomes more noticeable.

The oldest rocks underlying the claim area are Upper Jurassic-Lowwer Cretaceous dominantly greywackes, conglomerates and argillites belonging to the sedimentary package of Bowser Group. General strike in the claim area is east-west with dips 75° northerly. Intrusive to this sedimentary package are stocks of the Coast Intrusions which consist of granodiorite, diorite, quartz diorite and quartz monzonite of Upper Cretaceous or later age (Figure 3). Hybassal rocks in the form of dikes and sills varying between porphyrtic to



LEGEND
Alluvium
Granodiorite
Bowser Sediments
KITSUMKALUM
LAKE
TRENCH
4398 (4)
Main
Showing
BAV
5
3
1
6
4
2
9
8
7
BURN 1
4399 (4)
South
Showing
BURN 2
4425 (4)
BURN 3
4445 (5)
NELSON
RIVER
0
0.5
1
2
km.
SCALE
Road to
Terrace
OreQuest Consultants Ltd
REGIONAL GEOLOGY
3

aplitic to basaltic types intrude both the sediments and Coast granitoids.

Mineralization at the Kalum property is of the epigenetic vein type which typically consists of quartz gangue, pyrite, chalcopyrite and tetrahedrite with associated values in gold and silver. Lode vein deposits are common throughout the Terrace area with most deposits consisting of narrow quartz veins that have formed in faults, fractures, shear zones or along margins of dikes.

There are two good examples of vein mineralization exposed on the Kalum property and are host in a small granodiorite stock near waters edge.

The main vein, which was the locus for work in 1922-1923, is about 30 centimetres (1 foot) true width as exposed in the two shafts. Mineralization consists of pyrite, chalcopyrite, tetrahedrite and quartz gangue with associated gold and silver values. Selected assay samples collected from the dump between 1978-1984 have assay values ranging between trace to 5.62 oz/ton gold and 0.01-13.92 oz/t silver. Boths shaft were visited earlier this spring and fall and both were caved and probably flooded at depth.

The #2 vein, which is believed to be the vein which was followed by the adit in 1923, has been trenched and exposed on surface for about 30 metres (100 feet) along strike. This vein similar to the main vein in mineralogy, varies between 15 to 60 centimetres (6 to 24 inches) true width. In reports by the B.C. Ministry of Mines, there is mention of another vein approximately 10 centimetres wide which comes in along the north wall of the old adit and comes to within 5 centimetres of the second vein.

Selected assay samples taken from the adit in 1937 indicate only minor amounts of gold and silver. Surface trench samples taken from the same vein in 1983-1984 have yielded values up to 7.328 oz/ton gold and 6.58 oz/ton silver.

Both the main and #2 veins strike parallel at 037° northeast with the main vein dipping approximately 45° southwest and the #2 vein dipping approximately 65° southwest.

Not all quartz veins crosscutting the granodiorite carry mineralization. Most quartz veins observed are generally a barren, milky coloured quartz which strike obique to the two main auriferous veins. It is felt that the masses of barren quartz are older in age than the auriferous veins, but this is uncertain at this time.

Both basaltic and porphyritic type dikes are observed within the old workings. In review of the old drill core left on the property, both types appear fairly common, but their relationships to the mineralization at this time is uncertain. A 12 cm wide basaltic dike was observed as the footwall in the main vein adit. It is possible that the open spaces developed along the borders of the dikes formed conducts or dilant zones for mineral deposition.

Aplitic dikes are frequently observed crosscutting the barren quartz veins. The relationship again to the other rocks observed is uncertain.

A second area of interest located approximated 2.25 kilometers southwest of the main showing has been discovered by the owners while doing some regional prospecting. Tentatively labeled the south showing, the granodiorite here is similar to the main showing and indicates some alteration to the original rock with associated quartz veins and stringers. Pyrite and chalcopyrite have been observed and selected grab samples from a trench have yielded values up to 0.49 oz/t gold and 7.06 oz/t silver.

## 2b. SOIL GEOCHEMICAL SURVEY

Most exploration and mining personal believe that soil geochemistry is an effective tool in areas of little or no glacial overburden. Exploration geochemistry is based on the feature that economic mineral deposits constitute an "anomalous" concentration of one or more metals relative to surrounding country host rock. During the process of surface and near surface weathering, these anomalous concentrations of metals become incorporated in the weathering products and through natural processes of chemical and mechanical breakdown spread outwards from the ore deposit giving a "dispersion halo", which provides a considerably larger exploration target than the ore deposit itself.

Based on the abovementioned theory, a systematic grid was established over the Burn 1 and 2 claims where glacial overburden was believed minimal and mineralization has been observed.

A total of 576 soil and 17 rock samples were collected along grid lines 100 metres apart with 100 metre interval stations. A four kilometer cut line base was used for control while grid lines were established using a compass and chain.

Soil samples of the B horizon were collected where possible and sent to Vangeochem Labs in Vancouver for anaylsis in gold, silver, copper, lead, zinc, arsenic and molybdenum. A summary of their techniques and copies of the lab report sheets are given in Appendix I.

From results returned, threshold, anomalous and very anomalous values were determined by standard statistical techniques.

| | Threshold | Anomalous | Very Anomalous |
|---|---|---|---|
| Gold (ppb) | 29 | 52 | 95 |
| Silver (ppm) | 1.4 | 2.5 | 4.6 |
| Arsenic (ppm) | 23 | 53 | 121 |
| Zinc (ppm) | 222 | 449 | 909 |
| Lead (ppm) | 43 | 70 | 114 |
| Copper (ppm) | 36 | 64 | 112 |

Results of the survey are encouraging.

Most of the anomalies in all elements are isolated occurrences, but based on the large grid dimensions the individual anomalies are expected. An area stretching between Lines 2+00S and 7+00N and stations 0+00N (baseline) to 20+00N should be considered for further detailed evaluation.

Gold values returned are extremely encouraging with isolated anomalous values reaching 9,400 ppb. Most of the anomalous values are confined between Lines 2+00S to 7+00N and stations 0+00 (baseline) to 6+00 West. This area partly overlies the south showing and is believed underlain by the altered granodiorite. A large swamp passes through the middle of the anomalous area indicating that overburden may vary in thickness through this area.

One other very anomalous isolated gold value (120 ppb) is located outside the area of interest on Line 12+00S at Station 15+00W. This small area should also be resampled.

High silver values are primarily confined to the main area of interest. Silver values range between "0" to 3.1 ppm. The higher anomalous silver values are located on Lines 1+00S at station 1+00W, 1+00W at station 14+00W and 5+00W at station 14+00W. Elevated silver values are generally dispersed, but noteably confined to the area of interest. Arsenic is the same as with silver values. Isolated arsenic anomalies are noteably confined to the area of interest. There are also scattered isolated anomalies in zinc, copper and lead which either may or may not be coincident with one other element.

## 3. CONCLUSIONS and RECOMMENDATIONS

Phase I has been successfully completed and consisted of a soil geochemical survey and a preliminary geological survey over the Burn 1 and 2 mineral claims of the Kalum group.

Due to a thick glacial overburden cover on most of the Bav, Trench and Burn 3 claims, the entire Phase I program was designed to concentrate on areas where the overburden cover is not as excessive.

Results of the Phase I program were extremely encouraging and continuation of the exploration program is recommended.

Phase II should concentrate in the area outlined in Phase I and consist of linecutting, detail soil and rock sampling and geological mapping. Pending results, trenching may also be required.

Pending successful completion and encouraging results of Phase II, diamond drilling and/or overburden drilling will be recommended.

## ITEMIZED COST ESTIMATE

### PHYSICAL

| | |
|---|---|
| Cat Trenching, blasting, explosives, copco rock drill, etc. (done in April 1984 - Kalum Lake Mining Group) | $12,017.00 |

### SOIL SAMPLING

| | |
|---|---|
| J. Holland - 12 days @ $125/day | 1,500.00 |
| J. Dow - 20 days @ $100/day | 2,000.00 |
| - 3 days @ $150/day | 450.00 |
| (Mapping) - 10 days @ $200/day | 2,000.00 |
| D. Howe (Supervision) - 2 days @ $200/day | 400.00 |
| Report Writing and Drafting | 2,000.00 |

### DISBURSEMENTS

| | |
|---|---|
| Truck Rental | 525.00 |
| Gas | 315.00 |
| Freight | 58.80 |
| Kanata Travel | 295.00 |
| D. Howe - (Expense) | 107.89 |
| Neville Crosby | 115.86 |
| B.C. Telephone | 50.74 |
| Assays | 8,701.43 |
| Maps | 20.00 |
| | **$18,540.62** |

## QUALIFICATIONS

I, George Cavey, of 6891 Wiltshire Street, Vancouver, British Columbia hereby certify:

1. I am a graduate of the University of British Columbia (1976) and hold a BSc. degree in geology.
2. I am presently employed as a consulting geologist with OreQuest Consultants Ltd. of 404-595 Howe Street, Vancouver, British Columbia.
3. I have been employed in my profession by various mining companies for the past nine years.
4. I am a Fellow of the Geological Association of Canada.
5. I am a member of the Canadian Institute of Mining and Metallurgy.
6. The information contained in this report was obtained during the completion of the field work program supervised by OreQuest Consultants Ltd. in 1984.
7. Neither OreQuest Consultants Ltd. nor myself have direct or indirect interest in the property nor in the securities of Bradner Resources Ltd.
8. This report may be used by Bradner Resources Ltd. for all corporate purposes and including any public financing.

George Cavey
Consulting Geologist

DATED at Vancouver, British Columbia, this 19th day of November, 1984.

# QUALIFICATIONS

I, Diane Howe, of 21394-126th Avenue, Maple Ridge, British Columbia hereby certify:

1. I am a graduate of the University of British Columbia (1980) and hold a BSc. degree in geology.
2. I am presently employed as a project geologist with OreQuest Consultants Ltd. of 404-595 Howe Street, Vancouver, British Columbia.
3. I have been employed in my profession by various mining companies for the past five years.
4. I am a member of the Canadian Institute of Mining.
5. The information contained in this report was obtained from data personally collected during the field program in April and September of 1984 and from the reports and files listed in the Bibliography.
6. Neither OreQuest Consultants Ltd. nor myself have direct or indirect interest in the property described nor in the securities of Bradner Resources Ltd.
7. This report may be used by Bradner Resources Ltd. for all corporate purposes and including any public financing.

Diane Howe
Project Geologist

DATED at Vancouver, British Columbia, this 19th day of November, 1984.

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Geology of the Terrace Map Area, B.C. Memo 329; 1964, 117 pp.

G.S.C. PAPER
1956: 36-17-22

APPENDIX A

BRADNER

| SAMPLE # | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|---|
| 0S 0W | 3 | 15 | 24 | 115 | 1.3 | 45 | 4 |
| 0S 1W | 5 | 31 | 27 | 140 | .8 | 20 | 2 |
| 0S 2W | 3 | 24 | 40 | 119 | 1.2 | 50 | 10 |
| 0S 3W | 2 | 31 | 59 | 80 | 1.6 | 9400 | 20 |
| 0S 4W | 2 | 14 | 25 | 24 | .4 | 5 | 2 |
| 0S 5W | 2 | 9 | 20 | 49 | .3 | 15 | 2 |
| 0S 6W | 2 | 10 | 24 | 64 | .8 | 5 | 2 |
| 0S 7W | 2 | 29 | 25 | 94 | .6 | 10 | 10 |
| 0S 8W | 2 | 37 | 24 | 91 | .4 | 5 | 4 |
| 0S 9W | 1 | 5 | 19 | 75 | .4 | nd | 2 |
| 0S 10W | 1 | 10 | 10 | 35 | .2 | 10 | nd |
| 0S 11W | 2 | 6 | 16 | 20 | .4 | 20 | 2 |
| 0S 12W | 2 | 14 | 25 | 66 | .7 | 15 | 4 |
| 0S 13W | 3 | 17 | 50 | 174 | 1.0 | 5 | 4 |
| 0S 14W | 2 | 15 | 33 | 80 | 1.2 | 10 | nd |
| 0S 15W | 3 | 18 | 24 | 113 | 1.6 | 15 | 10 |
| 0S 16W | 2 | 10 | 15 | 40 | .9 | 40 | 10 |
| 0S 17W | 1 | 9 | 12 | 25 | .6 | 50 | nd |
| 0S 18W | 2 | 4 | 16 | 41 | .4 | 10 | 4 |
| 0S 19W | 1 | 2 | 9 | 9 | .2 | 10 | nd |
| 0S 20W | 1 | 7 | 14 | 13 | .7 | 5 | 2 |
| 1S 00W | 2 | 24 | 20 | 220 | .8 | 25 | 30 |
| 1S 01W | 4 | 44 | 31 | 600 | 2.6 | 5 | 35 |
| 1S 02W | 7 | 74 | 25 | 98 | 1.1 | 60 | 50 |
| 1S 03W | 2 | 16 | 19 | 85 | .7 | 20 | 2 |
| 1S 04W | 7 | 25 | 20 | 143 | .8 | 10 | 4 |
| 1S 05W | 2 | 24 | 16 | 122 | .8 | 15 | 2 |
| 1S 06W | 2 | 12 | 15 | 49 | .5 | 5 | 2 |
| 1S 07W | 1 | 11 | 15 | 53 | .7 | 20 | 4 |
| 1S 08W | 2 | 25 | 20 | 70 | 1.0 | nd | 4 |
| 1S 09W | 2 | 15 | 16 | 96 | .2 | 5 | 10 |
| 1S 10W | 2 | 14 | 19 | 55 | .2 | 5 | 4 |
| 1S 320mW | 2 | nd | 16 | 15 | .3 | 15 | 2 |
| 1S - 11W | 5 | 95 | 23 | 166 | nd | 5 | 1.4 |
| 1S - 12W | 3 | 21 | 27 | 144 | 20 | 5 | .9 |
| 1S - 13W | 3 | 20 | 26 | 105 | 10 | 10 | 1.0 |
| 1S - 14W | nd | 9 | 15 | 19 | 2 | 10 | .6 |
| 1S - 15W | 2 | 15 | 15 | 26 | 4 | 5 | .6 |
| 1S - 16W | 4 | 19 | 23 | 70 | 15 | 10 | .1 |
| 1S - 17W | 3 | 10 | 14 | 74 | 2 | 15 | .6 |
| 1S - 18W | 2 | 11 | 15 | 27 | 4 | 5 | .3 |
| 1S - 19W | 1 | 12 | 13 | 54 | 4 | 5 | .5 |
| | | | | | As | | Ag |

| | Mo ppm | Cu ppm | Pb ppm | Zn ppm | As ppm | Au ppb | Ag ppm |
|---|---|---|---|---|---|---|---|
| 2S - 0W | 2 | 22 | 20 | 102 | 40 | nd | .4 |
| 2S - 1W | 3 | 24 | 25 | 160 | 20 | 20 | .6 |
| 2S - 2W | 2 | 35 | 21 | 97 | 30 | 10 | .8 |
| 2S - 3W | 4 | 24 | 20 | 111 | 20 | nd | .4 |
| 2S - 4W | 3 | 20 | 25 | 226 | 10 | nd | .4 |
| 2S - 5W | 2 | 25 | 23 | 99 | 4 | 15 | .2 |
| 2S - 6W | 2 | 25 | 30 | 110 | 10 | 5 | .3 |
| 2S - 7W | 2 | 18 | 26 | 123 | 15 | nd | .4 |
| 2S - 8W | 2 | 13 | 18 | 100 | 10 | 5 | .5 |
| 2S - 9W | 3 | 27 | 18 | 150 | 10 | nd | .3 |
| 2S - 10W | 1 | 9 | 13 | 44 | 4 | 5 | .2 |
| 2S - 11W | 2 | 16 | 24 | 95 | 15 | 10 | .3 |
| 2S - 12W | 3 | 14 | 26 | 84 | 10 | 10 | .6 |
| 2S - 13W | 4 | 26 | 27 | 156 | 20 | 5 | .5 |
| 2S - 14W | 2 | 15 | 17 | 100 | 10 | 10 | .7 |
| 2S - 15W | 3 | 18 | 20 | 108 | 15 | 10 | .4 |
| 2S - 16W | 3 | 11 | 22 | 75 | 10 | 5 | .5 |
| 2S - 17W | 3 | 26 | 28 | 49 | 4 | 15 | .1 |
| 2S - 18W | 2 | 15 | 29 | 41 | 4 | 15 | .2 |
| 2S - 19W | 2 | 32 | 20 | 127 | 15 | 10 | .5 |
| 0020 | | | | | | | |
| L3S - 0W | 3 | 15 | 21 | 165 | 35 | 5 | .4 |
| L3S - 1W | 2 | 23 | 20 | 147 | 30 | 5 | .3 |
| L3S - 2W | 1 | 7 | 9 | 35 | 2 | 10 | .2 |
| L3S - 3W | 2 | 14 | 15 | 44 | nd | 10 | .4 |
| L3S - 4W | 2 | 16 | 18 | 59 | 30 | 30 | .6 |
| L3S - 5W | 1 | 9 | 18 | 27 | 10 | 10 | .3 |
| L3S - 6W | 2 | 15 | 20 | 55 | 2 | 5 | .7 |
| L3S - 7W | 5 | 72 | 31 | 95 | 50 | 10 | 1.6 |
| L3S - 8W | 17 | 18 | 15 | 75 | 20 | nd | .3 |
| L3S - 9W | 3 | 14 | 24 | 108 | 10 | 10 | .5 |
| L3S - 10W | 3 | 19 | 20 | 97 | 40 | 10 | .6 |
| L3S - 11W | 2 | 22 | 17 | 73 | 30 | 10 | .4 |
| L3S - 12W | 2 | 16 | 24 | 143 | 25 | 5 | .1 |
| L3S - 13W | 2 | 17 | 21 | 87 | 20 | 5 | .4 |
| L3S - 14W | 2 | 17 | 20 | 99 | 20 | 10 | .4 |
| L3S - 15W | 2 | 10 | 23 | 166 | 15 | 10 | .2 |
| DETECTION LIMIT | 1 | 1 | 2 | 1 | 2 | 5 | |

| | Cu | Pb | Zn. | As | Au | As |
|---|---|---|---|---|---|---|
| L3S 16W | 15 | 19 | 87 | .5 | nd | 2 |
| L3S 17W | 9 | 20 | 75 | .4 | nd | 2 |
| L3S 18W | 11 | 16 | 55 | .4 | 10 | 2 |
| L3S 19W | 13 | 15 | 49 | .4 | nd | 2 |
| L3S 20W | 11 | 13 | 36 | .4 | 5 | 4 |

| | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|
| L4S 0W | 5 | 17 | 110 | .2 | nd | nd |
| L4S 1W | 20 | 15 | 78 | .4 | 15 | 4 |
| L4S 2W | 16 | 15 | 95 | .5 | nd | 4 |
| L4S 3W | 40 | 41 | 205 | .6 | 5 | nd |
| L4S 4W | 16 | 14 | 72 | .6 | nd | 4 |
| L4S 5W | 17 | 15 | 90 | .3 | nd | 2 |
| L4S 6W | 9 | 11 | 34 | .2 | nd | nd |
| L4S 7W | 14 | 14 | 53 | nd | nd | 2 |
| L4S 8W | 9 | 12 | 60 | .6 | nd | 4 |
| L4S 9W | 10 | 18 | 59 | .6 | nd | 2 |
| L4S 10W | 15 | 16 | 71 | .3 | 5 | 4 |
| L4S 11W | 11 | 27 | 116 | 1.1 | 5 | 15 |
| L4S 12W | 14 | 15 | 101 | .5 | nd | 2 |
| L4S 13W | 12 | 11 | 49 | .3 | nd | 2 |
| L4S 14W | 26 | 10 | 75 | .6 | nd | 10 |
| L4S 15W | 12 | 11 | 64 | .4 | nd | 4 |
| L4S 16W | 14 | 14 | 40 | .4 | nd | 10 |
| L4S 17W | 15 | 16 | 45 | .4 | 5 | 20 |
| L4S 18W | 10 | 12 | 50 | .2 | nd | 4 |
| L4S 19W | 25 | 15 | 116 | .4 | nd | 4 |
| L4S 20W | 7 | 12 | 30 | .1 | 5 | 4 |
| L5S 0W | 12 | 22 | 114 | .2 | nd | 2 |
| L5S 1W | 15 | 16 | 151 | .5 | nd | 4 |
| L5S 2W | 35 | 18 | 136 | .7 | 10 | 10 |
| L5S 3W | 20 | 20 | 120 | .6 | 25 | 4 |
| L5S 4W | 24 | 15 | 77 | .5 | nd | 4 |
| L5S 5W | 12 | 21 | 116 | .7 | 5 | 2 |
| L5S 6W | 9 | 14 | 41 | .2 | 5 | 2 |
| L5S 7W | 16 | 15 | 55 | .4 | 10 | 10 |
| L5S 8W | 17 | 23 | 95 | .3 | 5 | 15 |
| L5S 9W | 15 | 16 | 100 | .5 | nd | 4 |
| L5S 10W | 21 | 21 | 144 | .3 | nd | 4 |
| L5S 11W | 16 | 21 | 86 | .3 | 10 | 20 |
| L5S 12W | 15 | 24 | 75 | .6 | 10 | 2 |
| L5S 13W | 12 | 21 | 99 | .6 | nd | 2 |
| L5S 14W | 15 | 17 | 86 | .4 | 5 | 4 |
| L5S 15W | 20 | 15 | 86 | .7 | 10 | 4 |
| L5S 16W | 15 | 21 | 39 | .1 | nd | 4 |
| L5S 17W | 14 | 9 | 66 | .3 | nd | 4 |
| L5S 18W | 11 | 21 | 71 | .4 | 10 | 2 |
| L5S 19W | 12 | 15 | 60 | .5 | 10 | 2 |
| L5S 20W | 22 | 17 | 123 | .3 | 10 | 2 |

| | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|
| L6S 0W | 10 | 17 | 84 | .3 | nd | 4 |
| L6S 1W | 10 | 20 | 90 | .3 | nd | 4 |
| L6S 2W | 10 | 5 | 18 | .6 | 10 | 2 |
| L6S 3W | 10 | 21 | 53 | .7 | 10 | 4 |
| L6S 4W | 8 | 15 | 45 | .3 | 5 | 4 |
| L6S 5W | 17 | 21 | 95 | .3 | 10 | 4 |
| L6S 6W | 12 | 15 | 54 | .5 | 5 | 2 |
| L6S 7W | 10 | 17 | 55 | .5 | 5 | 2 |
| L6S 8W | 12 | 19 | 130 | .3 | nd | 2 |
| L6S 9W | 11 | 12 | 78 | .2 | nd | 2 |
| L6S 10W | 10 | 20 | 140 | .6 | 15 | 4 |
| L6S 11W | 8 | 13 | 46 | .4 | 5 | 2 |
| L6S 12W | 15 | 8 | 90 | .8 | nd | 2 |
| L6S 13W | 36 | 4 | 130 | .7 | 15 | 4 |
| L6S 14W | 21 | 20 | 123 | .4 | 10 | 10 |
| L6S 15W | 10 | 25 | 53 | .6 | 15 | 2 |
| L6S 16W | 9 | 15 | 60 | .5 | 10 | 4 |
| L6S 17W | 14 | 20 | 40 | .4 | 5 | 10 |
| L6S 18W | 14 | 19 | 55 | .5 | 5 | 4 |
| L6S 19W | 10 | 20 | 46 | .5 | nd | 2 |
| L6S 20W | 9 | 16 | 39 | .3 | nd | 4 |
| L7S 0W | 5 | 4 | 18 | .2 | nd | 2 |
| L7S 1W | 4 | 14 | 20 | .1 | 5 | 2 |
| L7S 3AW | 12 | 21 | 75 | .4 | 15 | 4 |
| L7S 3BW | 5 | 8 | 20 | .2 | 10 | 2 |
| L7S 4W | 21 | 17 | 56 | nd | 5 | 4 |
| L7S 5W | 6 | 25 | 65 | .8 | 5 | 4 |
| L7S 6W | 24 | 20 | 135 | .5 | 5 | 10 |
| L7S 7W | 12 | 20 | 105 | .7 | 10 | 4 |
| L7S 8W | 12 | 19 | 75 | .5 | 5 | 4 |
| L7S 9W | 11 | 25 | 106 | .2 | 5 | 4 |
| L7S 10W | 13 | 24 | 99 | .6 | 5 | 4 |
| L7S 11W | 14 | 17 | 100 | .2 | nd | 4 |
| L7S 12W | 10 | 19 | 42 | .3 | nd | 15 |
| L7S 13W | 9 | 19 | 115 | nd | nd | 10 |
| L7S 14W | 11 | 24 | 60 | .4 | 10 | 15 |
| L7S 15W | 14 | 17 | 105 | .4 | nd | 4 |
| L7S 16W | 6 | 14 | 35 | .2 | 5 | 2 |
| L7S 17W | 10 | 15 | 55 | .1 | 10 | 2 |
| L7S 18W | 15 | 15 | 39 | nd | 10 | 4 |
| L7S 19W | 20 | 14 | 50 | .5 | 50 | 4 |
| L7S 20W | 21 | 15 | 56 | .2 | nd | 10 |

check #2 no 2

| SAMPLE # | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|---|
| 8S 1W | 5 | 5 | 7 | 8 | 1.0 | 10 | 2 |
| 8S 2W | 3 | 27 | 16 | 57 | 1.3 | 5 | 15 |
| 8S 3W | 3 | 14 | 24 | 124 | 1.1 | 5 | 4 |
| 8S 4W | 2 | 14 | 20 | 65 | .5 | 5 | 10 |
| 8S 5W | 2 | 15 | 27 | 125 | .6 | 10 | 4 |
| 8S 6W | 2 | 5 | 29 | 40 | .5 | 10 | 2 |
| 8S 7W | 1 | 15 | 25 | 130 | .3 | 10 | 4 |
| 8S 8W | 3 | 9 | 17 | 61 | .6 | 10 | 10 |
| 8S 9W | 1 | 5 | 11 | 35 | .2 | 5 | 2 |
| L8S 12W | | 4 | 3 | 20 | .1 | 10 | nd |
| L8S 13W | | 12 | 35 | 95 | .5 | nd | 4 |
| L8S 14W | | 6 | 10 | 75 | .2 | nd | 2 |
| L8S 15W | | 15 | 22 | 120 | .4 | nd | 15 |
| L8S 16W | | 10 | 19 | 76 | .7 | 5 | 2 |
| L8S 17W | | 9 | 21 | 54 | .7 | nd | 4 |
| L8S 18W | | 19 | 22 | 44 | .4 | nd | 2 |
| L8S 19W | | 8 | 12 | 37 | .1 | nd | 2 |
| L8S 20W | | 16 | 15 | 40 | .2 | nd | 2 |
| 9S 1W | 3 | 19 | 16 | 100 | .4 | 10 | 10 |
| 9S 2W | 2 | 13 | 24 | 105 | .6 | 10 | 4 |
| 9S 3W | 2 | 21 | 25 | 125 | .7 | 10 | 10 |
| 9S 4W | 1 | 5 | 20 | 40 | .3 | 20 | 2 |
| 9S 5W | 2 | 12 | 21 | 110 | .6 | nd | 4 |
| 9S 6W | 2 | 9 | 20 | 84 | .3 | 20 | 4 |
| 9S 7W | 1 | 5 | 18 | 60 | .3 | 15 | 2 |
| 9S 8W | 2 | 10 | 15 | 50 | .2 | 10 | 2 |
| 9S 9W | 1 | 10 | 49 | 55 | .7 | 15 | 4 |
| L9S 12W | | 24 | 5 | 18 | .6 | nd | 2 |
| L9S 13W | | 4 | 14 | 28 | .4 | 10 | 2 |
| L9S 14W | | 5 | 15 | 44 | .3 | nd | 4 |
| L9S 15W | | 10 | 15 | 46 | .2 | 5 | 15 |
| L9S 16W | | 14 | 16 | 93 | .2 | 5 | 4 |
| L9S 17W | | 7 | 19 | 36 | .4 | 10 | 4 |
| L9S 18W | | 15 | 14 | 71 | .3 | nd | 2 |
| L9S 19W | | 6 | 5 | 35 | .3 | 5 | 2 |
| L9S 20W | | 9 | 13 | 66 | nd | 20 | 2 |

| Sample | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm | Notes |
|---|---|---|---|---|---|---|---|---|
| 10S 1W | 3 | 15 | 15 | 90 | .5 | 5 | 4 | |
| 10S 2W | 3 | 16 | 20 | 99 | .9 | 10 | 4 | |
| 10S 3W | 3 | 18 | 19 | 87 | .5 | 10 | 4 | |
| 10S 4W | 2 | 13 | 21 | 71 | .7 | 5 | 4 | |
| 10S 5W | 2 | 10 | 15 | 64 | .2 | nd | 4 | |
| 10S 6W | 3 | 11 | 21 | 115 | .6 | 5 | 2 | |
| 10S 7W | 3 | 9 | 20 | 75 | .6 | nd | 4 | |
| 10S 12W | 4 | 10 | 23 | 109 | .8 | 5 | 4 | |
| 10S 13W | 4 | 10 | 26 | 94 | .6 | 10 | 10 | |
| 10S 14W | 2 | 15 | 20 | 95 | .6 | nd | 2 | |
| L10S 16W | | 10 | 14 | 51 | .6 | 10 | 4 | check no #15 |
| L10S 17W | | 13 | 23 | 102 | .2 | nd | 10 | |
| L10S 18W | | 6 | 19 | 40 | .2 | 5 | 2 | |
| L10S 1850W | | 21 | 10 | 54 | .1 | nd | 10 | 18.5 |
| L10S 19W | | 6 | 7 | 27 | .2 | 10 | nd | |
| L10S 20W | | 10 | 10 | 34 | .3 | 5 | 4 | |
| 11S 1W | 2 | 6 | 21 | 65 | .5 | nd | 2 | |
| 11S 2W | 2 | 16 | 22 | 85 | .4 | nd | 10 | |
| 11S 3W | 2 | 10 | 16 | 85 | .5 | 5 | 4 | |
| 11S 4W | 3 | 8 | 21 | 100 | .4 | nd | 2 | |
| 11S 5W | 3 | 10 | 25 | 177 | .5 | nd | 4 | |
| L11S 13W | | 13 | 12 | 79 | .3 | 5 | 4 | |
| L11S 14W | | 9 | 9 | 34 | .4 | nd | 10 | |
| L11S 15W | | 16 | 15 | 71 | .2 | nd | 4 | |
| L11S 16W | | 15 | 13 | 51 | .6 | nd | 4 | |
| L11S 17W | | 15 | 15 | 71 | .4 | 5 | 4 | |
| L11S 18W | | 13 | 15 | 79 | .6 | nd | 2 | check 18A,B |
| L11S 1800W | | 21 | 14 | 60 | .4 | 5 | 15 | |
| L11S 19W | | 7 | 5 | 33 | .3 | nd | 2 | |
| L11S 20W | | 4 | 9 | 25 | .2 | nd | 2 | |
| 12S 1W | 2 | 16 | 19 | 69 | .1 | 15 | 4 | |
| 12S 2W | 2 | 9 | 24 | 75 | .3 | 5 | 10 | |
| 12S 3W | 2 | 9 | 10 | 61 | .4 | 5 | 2 | |
| 12S 4W | 3 | 15 | 14 | 75 | .4 | 5 | 4 | |
| 12S 5W | 2 | 7 | 19 | 94 | .6 | 15 | 2 | |
| L12S 13W | | 9 | 10 | 25 | .3 | 5 | 4 | |
| L12S 14W | | 23 | 19 | 150 | .2 | nd | 15 | |
| L12S 15W | | 10 | 12 | 99 | .6 | 120 | 2 | |
| L12S 16W | | 15 | 19 | 81 | .1 | 5 | 4 | |
| L12S 17W | | 5 | 11 | 20 | .4 | nd | nd | |
| L12S 18W | | 4 | 6 | 15 | .5 | nd | 2 | |
| L12S 19W | | 9 | 19 | 35 | .3 | 5 | 2 | |
| L12S 20W | | 25 | 12 | 50 | .1 | 5 | 10 | |

| | Mo (ppm) | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|---|
| 13S 1W | 1 | 2 | 5 | 10 | .4 | 5 | 2 |
| 13S 2W | 1 | 9 | 15 | 62 | .5 | nd | 10 |
| 13S 3W | 5 | 14 | 19 | 142 | .4 | nd | 4 |
| 13S 4W | 2 | 14 | 16 | 67 | .5 | 5 | 4 |
| 13S 13W | 3 | 15 | 22 | 50 | .6 | 5 | 15 |
| 13S 14W | 3 | 5 | 19 | 46 | .8 | 5 | 2 |
| 13S 15W | 2 | 11 | 40 | 49 | 1.0 | 5 | 4 |
| 13S 16W | 5 | 10 | 26 | 37 | .6 | 5 | 2 |
| 13S 17W | 2 | 8 | 21 | 94 | .6 | nd | 2 |
| 14S 1W | 3 | 26 | 25 | 127 | 1.0 | 5 | 10 |
| 14S 2W | 2 | 10 | 15 | 47 | .4 | 5 | 2 |
| 14S 3W | 3 | 25 | 24 | 98 | .6 | 5 | 10 |
| 14S 4W | 2 | 9 | 21 | 65 | .4 | 5 | 2 |
| 14S 10W | 3 | 12 | 24 | 45 | .4 | 10 | 10 |
| 14S 11W | 3 | 15 | 14 | 34 | .3 | 5 | 4 |
| 14S 12W | 3 | 8 | 19 | 58 | .4 | nd | 2 |
| 14S 13W | 3 | 13 | 21 | 55 | .1 | 10 | 20 |
| 14S 14W | 3 | 6 | 21 | 46 | 1.4 | 10 | 2 |
| 14S 15W | 3 | 6 | 16 | 53 | .4 | nd | 2 |
| 14S 16W | 3 | 10 | 25 | 198 | .7 | 10 | 4 |
| 14S 17W | 3 | 10 | 20 | 88 | .7 | 10 | 2 |
| 15S 1W | 2 | 5 | 20 | 65 | .3 | 5 | 4 |
| 15S 2W | 2 | 15 | 21 | 103 | .3 | nd | 4 |
| 15S 3W | 3 | 6 | 10 | 67 | .2 | nd | 2 |
| 15S 10W | 2 | 9 | 19 | 30 | .5 | 10 | 4 |
| 15S 11W | 2 | 4 | 10 | 16 | .6 | 5 | 2 |
| 15S 12W | 2 | 5 | 19 | 80 | .4 | 5 | 2 |
| 15S 13W | 4 | 7 | 18 | 25 | .4 | 5 | 4 |
| 15S 14W | 2 | 7 | 25 | 30 | .4 | 5 | 4 |

| | Mo | Cu | Pb | Zn | Ag | Au | As |
|---|---|---|---|---|---|---|---|
| 16S 0W | 3 | 14 | 18 | 79 | .6 | nd | 4 |
| 16S 1W | 3 | 11 | 22 | 75 | .6 | 10 | 2 |
| 16S 2W | 7 | 10 | 18 | 100 | .4 | 5 | 4 |
| 16S 3W | 7 | 9 | 23 | 114 | .5 | nd | 4 |
| 16S 8W | 3 | 14 | 25 | 44 | .5 | nd | 4 |
| 16S 9W | 4 | 12 | 30 | 51 | .7 | 15 | 2 |
| 16S 10W | 4 | 16 | 18 | 64 | .3 | 10 | 4 |
| 16S 11W | 2 | 10 | 16 | 49 | .8 | 10 | 4 |
| 16S 12W | 4 | 6 | 21 | 104 | .4 | 5 | 10 |
| 16S 13W | 4 | 10 | 23 | 69 | .6 | 5 | 4 |
| 16S 14W | 3 | 10 | 25 | 80 | .4 | 10 | 10 |
| 17S 0W | 1 | 6 | 10 | 69 | .5 | 10 | 2 |
| 17S 1W | 5 | 14 | 20 | 103 | .5 | 10 | 10 |
| 17S 2W | 3 | 10 | 25 | 134 | .6 | 10 | 4 |
| 17S 3W | 4 | 16 | 35 | 145 | .4 | 5 | 4 |
| 17S 7W | 2 | 7 | 17 | 30 | .4 | 5 | 2 |
| 17S 8W | 3 | 11 | 22 | 50 | .4 | 5 | 2 |
| 17S 9W | 3 | 10 | 15 | 31 | .6 | 5 | 10 |
| 17S 10W | 3 | 14 | 15 | 33 | .3 | 5 | 20 |
| 17S 11W | 2 | 5 | 15 | 25 | .7 | 15 | 4 |
| 18S 0W | 2 | 13 | 13 | 137 | .7 | 5 | 2 |
| 18S 1W | 1 | 24 | 14 | 75 | .2 | nd | 4 |
| 18S 2W | 2 | 10 | 20 | 149 | .6 | 5 | 2 |
| 18S 3W | 2 | 7 | 14 | 108 | .3 | nd | 4 |
| 18S 8W | 3 | 14 | 21 | 53 | .5 | 10 | 10 |
| 18S 9W | 3 | 10 | 19 | 49 | .4 | 5 | 4 |
| 18S 10W | 2 | 11 | 14 | 46 | .3 | 5 | 4 |
| 18S 11W | 4 | 14 | 21 | 70 | .3 | nd | 4 |

| | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|---|
| 1N 0W | 20 | 21 | 30 | 124 | .4 | 10 | 2 |
| 1N 1W | 8 | 34 | 29 | 80 | .5 | 40 | 4 |
| 1N 2W | 19 | 14 | 31 | 56 | .4 | nd | 2 |
| 1N 3W | 3 | 15 | 30 | 78 | .7 | 10 | 4 |
| 1N 5W | 2 | 35 | 19 | 35 | .2 | 5 | nd |
| 1N 6W | 2 | 10 | 31 | 149 | .4 | 10 | 2 |
| 1N 7W | 2 | 14 | 27 | 39 | .6 | 35 | 4 |
| 1N 8W | 3 | 15 | 25 | 60 | .4 | 10 | 4 |
| 1N 9W | 2 | 25 | 30 | 95 | .7 | 5 | 10 |
| 1N 10W | 2 | 14 | 36 | 39 | .5 | 10 | 4 |
| 1N 11W | 2 | 28 | 30 | 88 | .4 | 15 | 15 |
| 1N 12W | 2 | 10 | 30 | 75 | .8 | 15 | 10 |
| 1N 13W | 4 | 7 | 21 | 37 | .4 | 10 | 2 |
| 1N 14W | 3 | 39 | 40 | 144 | 3.1 | 20 | 10 |
| 1N 15W | 2 | 20 | 32 | 80 | .6 | 10 | 10 |
| 1N 16W | 3 | 10 | 39 | 99 | .6 | 5 | 15 |
| 1N 17W | 2 | 14 | 24 | 35 | .6 | 5 | 4 |
| 1N 18W | 1 | 4 | 16 | 11 | .4 | 5 | nd |
| 1N 19W | 1 | 4 | 7 | 5 | .1 | nd | nd |
| 1N 20W | 1 | 5 | 7 | 10 | .8 | 10 | 2 |
| 2N 0W | 18 | 9 | 14 | 58 | .3 | nd | nd |
| 2N 1W | 9 | 25 | 20 | 135 | .8 | nd | 4 |
| 2N 2W | 2 | 12 | 25 | 140 | .7 | 5 | 15 |
| 2N 3W | 1 | 15 | 17 | 75 | 1.0 | 10 | 2 |
| 2N 4W | 2 | 5 | 2 | 9 | .5 | nd | 4 |
| 2N 5W | 1 | 6 | 16 | 69 | .3 | 5 | 2 |
| 2N 6W | 2 | 17 | 20 | 75 | .4 | 150 | 15 |
| 2N 7W | 2 | 20 | 25 | 85 | .2 | 5 | 4 |
| 2N 8W | 1 | 5 | 10 | 35 | .3 | nd | nd |
| 2N 9W | 1 | 10 | 5 | 25 | .7 | 5 | 4 |
| 2N 10W | 2 | 26 | 25 | 229 | 2.0 | nd | 10 |
| 2N 11W | 2 | 15 | 24 | 177 | .5 | nd | 4 |
| 2N 12W | 3 | 15 | 18 | 55 | 1.2 | nd | 4 |
| 2N 13W | 2 | 31 | 16 | 419 | nd | nd | 80 |
| 2N 14W | 2 | 15 | 10 | 25 | .2 | nd | 2 |
| 2N 15W | 2 | 9 | 22 | 29 | .9 | nd | 4 |
| 2N 16W | 2 | 21 | 15 | 34 | .3 | nd | 10 |
| 2N 17W | 2 | 10 | 15 | 30 | .1 | 15 | 4 |
| 2N 18W | 3 | 15 | 19 | 41 | .7 | 5 | 2 |
| 2N 19W | 2 | 10 | 16 | 9 | .6 | 10 | nd |
| 2N 20W | 2 | 25 | 22 | 56 | .5 | 10 | 10 |

| | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|---|
| 3N 00W | 1 | 15 | 15 | 75 | .5 | 15 | 4 |
| 3N 01W | 1 | 20 | 15 | 130 | .1 | 10 | 15 |
| 3N 02W | 2 | 10 | 15 | 50 | .3 | 5 | 2 |
| 3N 03W | 2 | 26 | 19 | 75 | .4 | nd | 15 |
| 3N 04W | 2 | 5 | 11 | 45 | 1.0 | 10 | 4 |
| 3N 05W | nd | 3 | 5 | 15 | .1 | 15 | 2 |
| 3N 06W | 2 | 27 | 15 | 90 | nd | 20 | 10 |
| 3N 07W | 1 | 13 | 13 | 60 | .5 | 20 | 4 |
| 3N 08W | 3 | 16 | 45 | 130 | .7 | 35 | 10 |
| 3N 09W | 1 | 10 | 9 | 24 | .7 | 10 | nd |
| 3N 10W | 2 | 11 | 10 | 23 | .2 | 10 | nd |
| 3N 11W | 2 | 8 | 9 | 29 | .2 | 80 | 4 |
| 3N 12W | 3 | 14 | 14 | 50 | .5 | 10 | 10 |
| 3N 13W | 3 | 14 | 14 | 85 | .3 | 20 | 15 |
| 3N 14W | nd | 5 | 5 | 17 | .2 | nd | 2 |
| 3N 15W | 1 | 2 | 2 | 5 | .2 | 10 | 2 |
| 3N 16W | nd | 10 | 11 | 39 | nd | 10 | 10 |
| 3N 17W | nd | 8 | 6 | 13 | nd | 25 | 10 |
| 3N 18W | nd | 3 | 1 | 9 | nd | 5 | 2 |
| 3N 19W | 2 | 10 | 13 | 35 | .7 | 5 | 4 |
| 3N 20W | 2 | 8 | 18 | 54 | .3 | nd | 15 |
| 4N 00W | 2 | 8 | 14 | 64 | .2 | nd | 10 |
| 4N 01W | 1 | 10 | 14 | 61 | .3 | nd | 4 |
| 4N 02W | 1 | 6 | 6 | 21 | .4 | 5 | 2 |
| 4N 03W | 2 | 7 | 8 | 59 | .3 | 10 | 2 |
| 4N 04W | 1 | 10 | 5 | 52 | .3 | nd | nd |
| 4N 05W | 1 | 5 | 10 | 14 | .4 | 10 | 2 |
| 4N 06W | 1 | 14 | 15 | 80 | .6 | 105 | 10 |
| 4N 07W | nd | 2 | 15 | 20 | .4 | 10 | 2 |
| 4N 08W | 2 | 24 | 25 | 220 | 1.1 | 10 | 4 |
| 4N 09W | 1 | 30 | 40 | 38 | 1.3 | 10 | nd |
| 4N 10W | 2 | 10 | 16 | 77 | 1.0 | 10 | 4 |
| 4N 11W | 1 | 5 | 6 | 20 | .4 | 5 | nd |
| 4N 12W | 1 | 4 | 3 | 12 | .2 | 15 | nd |
| 4N 13W | 2 | 11 | 11 | 39 | .2 | 10 | 2 |
| 4N 14W | 2 | 14 | 23 | 50 | .7 | 5 | 15 |
| 4N 15W | 2 | 13 | 10 | 35 | 1.5 | nd | 2 |
| 4N 16W | 4 | 20 | 18 | 45 | 1.3 | 5 | 4 |
| 4N 17W | 7 | 12 | 30 | 38 | .3 | 25 | 15 |
| 4N 18W | 1 | 6 | 9 | 15 | .2 | nd | 2 |
| 4N 19W | 1 | nd | 5 | 5 | .4 | 10 | 2 |
| 4N 20W | 2 | 14 | 13 | 28 | .2 | nd | 4 |

| | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm | Note |
|---|---|---|---|---|---|---|---|---|
| 5N 00W | 1 | 5 | 10 | 110 | .5 | 50 | 20 | |
| 5N 01W | 2 | 8 | 11 | 1 | .8 | 20 | 4 | |
| 5N 02W | 1 | 10 | 14 | 84 | .5 | 10 | 4 | |
| 5N 03W | 1 | 23 | 24 | 114 | 1.4 | 5 | 10 | |
| 5N 04W | 1 | 13 | 24 | 100 | 1.2 | nd | 10 | |
| 5N 06W | 2 | 5 | 9 | 25 | .3 | nd | 2 | |
| 5N 07W | 1 | 15 | 16 | 90 | .5 | nd | 4 | |
| 5N 08W | 1 | 4 | 5 | 10 | .2 | 60 | nd | |
| 5N 09W | nd | 14 | 14 | 55 | 1.2 | 15 | 15 | |
| 5N 10W | 1 | 35 | 96 | 200 | 1.1 | 5 | 2 | |
| 5N 11W | 4 | 25 | 25 | 90 | .7 | 5 | 40 | |
| 5N 12W | 1 | 3 | nd | 5 | nd | 5 | 2 | |
| 5N 13W | 1 | 6 | 10 | 35 | .1 | nd | 2 | |
| 5N 14W | 2 | 15 | 15 | 62 | 2.1 | nd | 4 | |
| 5N 15W | 4 | 15 | 33 | 96 | 1.0 | nd | 30 | |
| 5N 16W | 3 | 15 | 24 | 42 | .6 | nd | 4 | |
| 5N 17W | 2 | 8 | 9 | 25 | .3 | nd | 2 | |
| 5N 18W | 7 | 14 | 20 | 53 | .6 | 10 | 2 | |
| 5N 19W | 3 | 19 | 15 | 55 | .3 | nd | 4 | |
| 5N 20W | 2 | 8 | 11 | 25 | .3 | 20 | 4 | |
| 6N 00W | 1 | 5 | 9 | 33 | .3 | 5 | nd | |
| 6N 01W | 2 | 19 | 19 | 95 | .7 | nd | 2 | |
| 6N 02W | 2 | 10 | 20 | 80 | .5 | nd | 4 | |
| 6N 03AW | 3 | 31 | 20 | 144 | .2 | 80 | 10 | check |
| 6N 03BW | 3 | 13 | 20 | 104 | .3 | nd | 4 | check |
| 6N 04W | 1 | 10 | 14 | 55 | .6 | 320 | 10 | |
| 6N 05W | 4 | 30 | 160 | 286 | 1.5 | 100 | 50 | |
| 6N 06W | 1 | 11 | 14 | 70 | .6 | 10 | 10 | |
| 6N 07W | 1 | 5 | 10 | 30 | .3 | nd | 2 | |
| 6N 08W | 1 | 15 | 15 | 59 | .5 | 5 | 4 | |
| 6N 09W | 2 | 14 | 20 | 133 | .2 | 15 | 2 | |
| 6N 10W | 2 | 15 | 15 | 58 | .4 | nd | 4 | |
| 6N 11W | 3 | 23 | 15 | 70 | .6 | nd | 2 | |
| 6N 12W | 1 | 16 | 15 | 75 | .5 | nd | 2 | |
| 6N 13AW | 2 | 10 | 15 | 50 | .4 | nd | 10 | check |
| 6N 13BW | 3 | 30 | 17 | 159 | .9 | nd | 2 | check |
| 6N 15W | 3 | 10 | 19 | 80 | .6 | nd | 2 | |
| 6N 16W | 2 | 15 | 15 | 55 | .4 | nd | 4 | |
| 6N 17W | 6 | 24 | 19 | 66 | .5 | 5 | 4 | |
| 6N 18W | 2 | 10 | 14 | 24 | .3 | 15 | 2 | |
| 6N 19W | 3 | 15 | 15 | 36 | .6 | 10 | 10 | |
| 6N 20W | 4 | 17 | 16 | 40 | .3 | nd | 15 | |

| SAMPLE # | Mo | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|---|
| L7N 0W | | 5 | 5 | 28 | .3 | 5 | nd |
| L7N 1W | | 8 | 16 | 114 | .3 | nd | 4 |
| L7N 2W | | 14 | 24 | 93 | .4 | nd | 2 |
| L7N 3W | | 18 | 24 | 59 | .4 | nd | 4 |
| L7N 4W | | 14 | 19 | 39 | .6 | nd | 2 |
| L7N 5W | | 15 | 15 | 91 | .8 | 10 | 4 |
| L7N 6W | | 5 | 10 | 35 | .5 | 5 | nd |
| L7N 7W | | 4 | 11 | 20 | .2 | nd | 2 |
| L7N 8W | | 25 | 15 | 63 | .3 | 45 | 10 |
| L7N 9W | | 5 | 10 | 20 | .2 | nd | nd |
| L7N 10W | | 25 | 44 | 190 | .7 | 10 | 2 |
| L7N 11W | | 4 | 5 | 20 | .2 | 10 | 2 |
| L7N 12W | | 4 | 20 | 12 | .2 | 5 | nd |
| L7N 13W | | 13 | 10 | 46 | .6 | 20 | 2 |
| L7N 14W | | 14 | 8 | 41 | .6 | 5 | 2 |
| 7N 15W | 2 | 15 | 15 | 39 | .4 | 5 | 2 |
| 7N 16W | nd | 7 | 7 | 16 | .3 | 10 | 2 |
| 7N 17W | 3 | 30 | 20 | 60 | 1.0 | nd | 4 |
| 7N 18W | 5 | 13 | 12 | 42 | .3 | 5 | 10 |
| 7N 19W | 5 | 10 | 10 | 41 | .3 | nd | 10 |
| 7N 20W | 4 | 10 | 9 | 30 | .3 | 10 | 4 |
| L8N 0W | | 12 | 12 | 55 | .4 | nd | 4 |
| L8N 1W | | 20 | 18 | 45 | .5 | nd | 2 |
| L8N 2W | | 20 | 19 | 120 | .5 | 10 | 10 |
| L8N 3W | | 6 | 14 | 66 | .3 | nd | nd |
| L8N 4W | | 21 | 35 | 91 | .5 | nd | 10 |
| L8N 5W | | 10 | 15 | 70 | .5 | 10 | 4 |
| L8N 6W | | 8 | 9 | 40 | .5 | nd | 2 |
| L8N 7W | | 4 | 2 | 15 | .4 | nd | nd |
| L8N 8W | | 3 | 6 | 15 | .4 | nd | 2 |
| L8N 9W | | 12 | 15 | 93 | 1.1 | nd | 4 |
| L8N 10W | | 9 | 24 | 25 | .7 | 5 | 2 |
| L8N 11W | | 10 | 10 | 31 | .4 | nd | 2 |
| L8N 12W | | 15 | 25 | 69 | .5 | nd | 10 |
| L8N 13W | | 11 | 19 | 34 | 1.0 | nd | 2 |
| L8N 14W | | 10 | 9 | 24 | .6 | nd | nd |
| L8N 15W | | 7 | 5 | 11 | .8 | 5 | 2 |
| L8N 16W | | 10 | 15 | 35 | .1 | 5 | 4 |
| L8N 17W | | 10 | 15 | 33 | .2 | nd | 4 |
| L8N 18W | | 9 | 13 | 24 | .1 | 5 | 2 |
| L8N 19W | | 21 | 20 | 73 | .4 | nd | 15 |
| L8N 20W | | 17 | 15 | 42 | .8 | 35 | 2 |

| | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|
| L9N 0W | 10 | 10 | 61 | .7 | 5 | 2 |
| L9N 1W | 11 | 7 | 48 | .5 | nd | 2 |
| L9N 2W | 12 | 11 | 65 | .4 | nd | 2 |
| L9N 5W | 11 | 10 | 40 | .2 | 30 | 10 |
| L9N 6W | 9 | 12 | 25 | nd | 10 | 2 |
| L9N 7W | 25 | 16 | 70 | .4 | nd | 10 |
| L9N 8W | 24 | 7 | 8 | .5 | nd | nd |
| L9N 9W | 13 | 12 | 75 | .6 | 25 | 2 |
| L9N 10W | 20 | 20 | 71 | 1.0 | nd | 4 |
| L9N 11W | 14 | 11 | 44 | .4 | 5 | 4 |
| L9N 12W | 19 | 14 | 97 | .4 | nd | 4 |
| L9N 13W | 15 | 17 | 50 | .2 | nd | 2 |
| L9N 14W | 10 | 18 | 24 | .1 | nd | 10 |
| L9N 15W | 4 | 6 | 7 | .3 | nd | nd |
| L9N 16W | 3 | 5 | 4 | .2 | nd | nd |
| L9N 17W | 18 | 10 | 33 | .3 | nd | 2 |
| L9N 18W | 27 | 12 | 55 | nd | 5 | 4 |
| L9N 19W | 49 | 26 | 71 | 1.3 | nd | 4 |
| L9N 20W | 6 | 2 | 10 | .2 | nd | nd |

| | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|---|
| 10N 1W | 2 | 9 | 20 | 39 | 1.0 | 15 | 4 |
| 10N 2W | 2 | 10 | 15 | 90 | .1 | 5 | 4 |
| 10N 3W | 2 | 8 | 18 | 44 | 1.0 | nd | 4 |
| 10N 4W | 5 | 25 | 22 | 65 | 2.1 | nd | 2 |
| 10N 5W | 3 | 16 | 15 | 52 | .4 | 5 | 4 |
| 10N 6W | 3 | 12 | 15 | 74 | .7 | 10 | 2 |
| 10N 7W | 1 | 9 | 14 | 45 | .3 | 10 | 4 |
| 10N 8W | 2 | 16 | 15 | 57 | .3 | 10 | 4 |
| 10N 9W | 3 | 7 | 17 | 52 | .3 | 10 | 2 |
| 10N 10W | 1 | 9 | 14 | 45 | .4 | 20 | 2 |
| 10N 11W | 2 | 15 | 21 | 41 | .4 | 5 | 4 |
| 10N 12W | 3 | 24 | 16 | 68 | .3 | 20 | 20 |
| 10N 13W | 2 | 10 | 14 | 85 | .6 | 10 | 2 |
| 10N 14W | 4 | 11 | 19 | 71 | .7 | 10 | 4 |
| 10N 15W | 3 | 10 | 16 | 53 | .8 | 5 | 4 |
| 10N 16W | 4 | 10 | 21 | 89 | .4 | 20 | 2 |
| 10N 17W | 3 | 13 | 15 | 89 | .7 | 15 | 4 |
| 10N 18W | 3 | 10 | 15 | 50 | .4 | 5 | 4 |
| 10N 19W | 4 | 10 | 16 | 71 | .2 | 20 | 4 |
| 10N 20W | 4 | 10 | 19 | 29 | .7 | 5 | 2 |

| | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm |
|---|---|---|---|---|---|---|---|
| 12N 2W | 2 | 5 | 15 | 43 | .4 | 25 | 2 |
| 12N 3W | 2 | 13 | 14 | 50 | .6 | 5 | 4 |
| 12N 4W | 3 | 9 | 20 | 45 | 1.2 | nd | 2 |
| 12N 5W | 3 | 11 | 20 | 49 | .4 | 5 | 4 |
| 12N 6W | 2 | 14 | 15 | 65 | .2 | 5 | 4 |
| 12N 7W | 4 | 8 | 19 | 56 | .2 | 5 | nd |
| 12N 8W | 1 | 6 | 9 | 34 | .3 | 5 | 2 |
| 12N 9W | 5 | 37 | 31 | 134 | .7 | 5 | 10 |
| 12N 10W | 2 | 6 | 15 | 70 | .6 | 5 | 2 |
| 12N 11W | 3 | 10 | 18 | 50 | .4 | 10 | 4 |
| 12N 11.50W | 3 | 14 | 16 | 100 | 1.1 | nd | 4 |
| 12N 12W | 3 | 9 | 20 | 45 | .2 | nd | 10 |
| 12N 13W | 4 | 13 | 20 | 36 | .4 | nd | 2 |
| 12N 14W | 3 | 10 | 18 | 47 | .2 | 5 | 4 |
| 12N 15W | 3 | 10 | 17 | 63 | .5 | 5 | 4 |
| 12N 16W | 6 | 16 | 15 | 39 | .8 | 5 | 10 |
| 12N 17W | 5 | 36 | 19 | 45 | .6 | 5 | 4 |
| 12N 18W | 2 | 11 | 12 | 50 | .1 | 5 | 4 |
| 12N 19W | 6 | 17 | 12 | 45 | .5 | 10 | 4 |
| 12N 20W | 7 | 14 | 15 | 50 | .6 | 10 | 10 |
| 14N 13W | 3 | 5 | 6 | 15 | .3 | nd | nd |
| 14N 13.50W | 3 | 5 | 7 | 28 | .4 | 10 | 2 |
| 14N 14W | 2 | 2 | 16 | 14 | .2 | nd | 2 |
| 14N 14.50W | 3 | 9 | 18 | 25 | .7 | 5 | 4 |
| 14N 15W | 3 | 9 | 16 | 53 | .8 | 5 | 2 |
| 14N 15.50W | 3 | 9 | 20 | 35 | .8 | 5 | 4 |
| 14N 16W | 3 | 10 | 15 | 41 | .6 | 5 | 2 |
| 14N 16.50W | 3 | 8 | 15 | 30 | 1.4 | 5 | 2 |
| 14N 17W | 3 | 6 | 14 | 17 | .5 | 10 | 2 |
| 14N 17.50W | 4 | 26 | 21 | 74 | .9 | nd | 10 |
| 14N 18W | 4 | 20 | 16 | 41 | .8 | 10 | 4 |
| 14N 18.50W | 2 | 15 | 14 | 27 | .4 | nd | 4 |
| 14N 19W | 3 | 9 | 14 | 60 | .3 | nd | 4 |
| 14N 19.50W | 4 | 14 | 17 | 53 | .5 | 10 | 4 |
| 14N 20W | 4 | 15 | 15 | 55 | .4 | 10 | 4 |
| 16N 13.50W | 2 | 5 | 15 | 24 | .4 | 5 | nd |
| 16N 14W | 1 | 10 | 11 | 22 | .4 | nd | 2 |
| 16N 14.50W | 2 | 6 | 15 | 24 | .2 | 10 | 4 |
| 16N 15W | 1 | 11 | 22 | 47 | .8 | 10 | 10 |
| 16N 15.50W | 2 | 10 | 23 | 54 | .7 | 10 | 4 |
| 16N 15.60W | 4 | 14 | 20 | 50 | .2 | 5 | 10 |
| 16N 16W | 2 | 5 | 17 | 35 | .3 | 10 | 4 |
| 16N 16.50W | 3 | 7 | 20 | 42 | .4 | nd | 4 |
| 16N 17W | 3 | 6 | 15 | 27 | .5 | 10 | 2 |
| 16N 17.50W | 3 | 15 | 13 | 45 | .7 | 10 | 2 |
| 16N 18W | 4 | 8 | 25 | 25 | .5 | 5 | 10 |
| 16N 18.50W | 3 | 15 | 15 | 55 | .4 | 5 | 4 |
| 16N 19W | 4 | 10 | 21 | 51 | .7 | 10 | 4 |
| 16N 19.30W | 2 | 14 | 10 | 50 | .3 | 5 | 50 |
| 16N 19.50W | 3 | 15 | 16 | 92 | .5 | 10 | nd |

| | Mo | Cu | Pb | ZN | Ag | Au | As. |
|---|---|---|---|---|---|---|---|
| 18N 13W | 2 | 8 | 6 | 17 | .3 | 10 | 2 |
| 18N 13.50W | 3 | 15 | 15 | 55 | .4 | 15 | 4 |
| 18N 14W | 3 | 14 | 16 | 40 | .3 | 10 | 4 |
| 18N 14.50W | 3 | 16 | 12 | 33 | .5 | 5 | 2 |
| 18N 15W | 2 | 54 | 16 | 79 | .2 | 5 | 15 |
| 18N 15.50W | 1 | 9 | 17 | 40 | .3 | 5 | 2 |
| 18N 16W | 2 | 8 | 12 | 19 | .2 | 20 | 30 |
| 18N 16.50W | 3 | 10 | 14 | 25 | .5 | 5 | 50 |
| 18N 17W | 1 | 11 | 14 | 25 | .4 | nd | 60 |
| 18N 17.50W | 2 | 14 | 11 | 37 | .4 | nd | 4 |
| 18N 18W | 4 | 12 | 14 | 46 | .6 | 5 | 2 |
| 18N 18.50W | 1 | 7 | 9 | 25 | .1 | 10 | 30 |
| 18N 19W | 2 | 10 | 11 | 79 | .1 | 10 | 35 |
| 18N 19.50W | 4 | 25 | 26 | 64 | .3 | 10 | 40 |
| 18N 20W | 4 | 36 | 22 | 80 | .3 | nd | 30 |
| 20N 13W | 3 | 12 | 6 | 14 | .5 | 5 | 2 |

ROCKS

| SAMPLE # | Mo ppm | Cu ppm | Pb ppm | Zn ppm | As ppm | Au ppb | Ag ppm | Sample Location |
|---|---|---|---|---|---|---|---|---|
| KALUM 1 | 1 | 24 | 10 | 78 | 10 | 5 | .5 | 70 m N of 2+00S, 20+00W |
| KALUM 2 | 2 | 45 | 17 | 123 | 60 | nd | .6 | 1+00S, 11+00 W |
| KALUM 3 | 1 | 11 | 12 | 61 | 20 | 5 | .4 | 1+00S, 18+80W |
| DETECTION LIMIT | 1 | 1 | 2 | 1 | 2 | 5 | 0.1 | |

| SAMPLE # | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm | Sample Location |
|---|---|---|---|---|---|---|---|
| C - 1 | 600 | 65 | 14 | 8.0 | 640 | 50 | QZ - SOUTH SHOWING. |
| C - 2 | 5800 | 1500 | 115 | 80.1 | 16700 | 100 | #1 VEIN - DUMP (BAN) |
| C - 3 | 69 | 29 | 39 | 4.2 | 70 | 4 | 1+00S, 3+10W (QZ) |
| C - 4 | 10 | 5 | 71 | .5 | 5 | nd | 4+00N, 4+30W (ARG) QZ |
| C - 5 | 6 | nd | 35 | .7 | nd | 4 | 4+00S, 8+50W (" ) QZ |
| C - 6 | 39 | 26 | 124 | .6 | 15 | 2 | 0+00, 7+00W (") |
| C - 7 | 65 | 15 | 32 | .8 | 5 | nd | 2+00N, 10+50W (RHY?) |
| C - 8 | 12 | 13 | 71 | .4 | 5 | nd | 0+00, 9+00W (ARG) QZ |
| C - 9 | 22 | 9 | 74 | .5 | nd | 10 | 1+00N, 15+30W (" ) |
| C - 10 | 10 | 4 | 53 | .2 | 5 | 10 | 3+00N, 13+00W (" ) QZ |
| C - 11 | 13 | 10 | 67 | .4 | nd | 10 | 5+00N, 15+50W (" ) QZ. |
| C - 13 | 127 | 430 | 19 | 89.2 | 1575 | 2 | BAN #2 |
| C - 14 | 1520 | 850 | 2 | 199.2 | 6580 | 15 | " |

| | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb | As ppm | |
|---|---|---|---|---|---|---|---|---|
| 0C 1N 1450W (ROCK) | 1 | 35 | 13 | 84 | .2 | nd | 10 | 1+00N, 14+50W. |

File B:BRADNER.VGC Threshold/Anomaly Statistics
GOLD

| B:BRADNER.VGC / col 7 | Normal | Log-xform | Un-xform |
|---|---|---|---|
| No. Samples | 387 | | |
| Min | 5.00 | | |
| Max | 100.00 | | |
| Mean | 10.84 | 0.93 | 8.59 |
| Standard Deviation | 10.73 | 0.26 | 1.83 |
| Threshold | 32.29 | 1.46 | 28.64 |
| Anomalous | 43.02 | 1.72 | 52.29 |
| Very Anomalous | 53.74 | 1.98 | 95.47 |
| Upper Discard Limit | 100.00 | | |

Listing of threshold & anomalous values:

| Sample | Raw Value | | Log10(Value) | |
|---|---|---|---|---|
| ( 1 ) | 45.00 | ** ANOM | 1.65 | * thresh |
| ( 3 ) | 50.00 | ** ANOM | 1.70 | * thresh |
| ( 15 ) | 40.00 | * thresh | 1.60 | * thresh |
| ( 16 ) | 50.00 | ** ANOM | 1.70 | * thresh |
| ( 21 ) | 40.00 | * thresh | 1.60 | * thresh |
| ( 25 ) | 35.00 | * thresh | 1.54 | * thresh |
| ( 40 ) | 60.00 | *** V ANOM | 1.78 | ** ANOM |
| ( 65 ) | 35.00 | * thresh | 1.54 | * thresh |
| ( 68 ) | 80.00 | *** V ANOM | 1.90 | ** ANOM |
| ( 90 ) | 50.00 | ** ANOM | 1.70 | * thresh |
| ( 94 ) | 60.00 | *** V ANOM | 1.78 | ** ANOM |
| ( 102 ) | 80.00 | *** V ANOM | 1.90 | ** ANOM |
| ( 103 ) | 100.00 | *** V ANOM | 2.00 | *** V ANOM |
| ( 261 ) | 45.00 | ** ANOM | 1.65 | * thresh |
| ( 273 ) | 35.00 | * thresh | 1.54 | * thresh |
| ( 275 ) | 30.00 | | 1.48 | * thresh |
| ( 329 ) | 50.00 | ** ANOM | 1.70 | * thresh |
| ( 377 ) | 30.00 | | 1.48 | * thresh |

Note: 10 value(s) not included ( exceed limit of 100 )

```
Class % vs. Log10(PPM): B:BRADNER.VGC
   GOLD

   upper                      F R E Q U E N C Y   ( % )
   Log10 Class%   Cum% +----:----1----:----2----:----3----:----4----:----5
    0.03   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.13   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.23   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.33   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.43   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.53   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.63   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.73  44.44  44.44 :********************************************.    :
    0.83   0.00  44.44 :    .    :    .    :    .    :    .    :    .    :
    0.93   0.00  44.44 M    .    :    .    :    .    :    .    :    .    :
    1.03  35.92  80.36 :************************************    :    .    :
    1.13   0.00  80.36 :    .    :    .    :    .    :    .    :    .    :
    1.23   8.27  88.63 :********:    .    :    .    :    .    :    .    :
    1.33   5.17  93.80 :*****   :    .    :    .    :    .    :    .    :
    1.43   1.55  95.35 T**  .    :    .    :    .    :    .    :    .    :
    1.53   0.52  95.87 :*   .    :    .    :    .    :    .    :    .    :
    1.63   1.29  97.16 A*   .    :    .    :    .    :    .    :    .    :
    1.73   1.55  98.71 :**  .    :    .    :    .    :    .    :    .    :
    1.83   0.52  99.22 :*   .    :    .    :    .    :    .    :    .    :
    1.93   0.52  99.74 V*   .    :    .    :    .    :    .    :    .    :
    2.03   0.26 100.00 :    .    :    .    :    .    :    .    :    .    :
                       +----:----1----:----2----:----3----:----4----:----5
```

```
Cumulative Percent vs. Log(PPM): B:BRADNER.VGC
   GOLD

        upper                     P R O B A B I L I T Y   ( C U M % )
   PPM  Log10    Cum%  .01 .1 .5  2     10    30  50% 70    90    98 99 999 9999
   4.3  0.63     0.00   :   :  :  :      :     :   |   :     :     :  :   :   :
   5.4  0.73    44.44   :   :  :  :      :     : + |   :     :     :  :   :   :
   6.8  0.83    44.44   :   :  :  :      :     :   |   :     :     :  :   :   :
   8.5  0.93    44.44   :   :  :  :      :     :   |   :     :     :  :   :   :
    11  1.03    80.36   :   :  :  :      :     :   |   : +   :     :  :   :   :
    13  1.13    80.36   :   :  :  :      :     :   |   :     :     :  :   :   :
    17  1.23    88.63   :   :  :  :      :     :   |   :    +:     :  :   :   :
    21  1.33    93.80   :   :  :  :      :     :   |   :     : +   :  :   :   :
    27  1.43    95.35   :   :  :  :      :     :   |   :     : +   :  :   :   :
    34  1.53    95.87   :   :  :  :      :     :   |   :     :  +  :  :   :   :
    43  1.63    97.16   :   :  :  :      :     :   |   :     :   + :  :   :   :
    54  1.73    98.71   :   :  :  :      :     :   |   :     :     +  :   :   :
    68  1.83    99.22   :   :  :  :      :     :   |   :     :     : +:   :   :
    85  1.93    99.74   :   :  :  :      :     :   |   :     :     :  :+  :   :
   107  2.03   100.00   :   :  :  :      :     :   |   :     :     :  :   :   :+
                       .01 .1 .5  2     10    30  50% 70    90    98 99 999 9999
```

File B:BRADNER.VGC Threshold/Anomaly Statistics
SILVER

| B:BRADNER.VGC / col 6 | Normal | Log-xform | Un-xform |
|---|---|---|---|
| No. Samples | 563 | | |
| Min | 0.10 | | |
| Max | 3.10 | | |
| Mean | 0.51 | -0.37 | 0.43 |
| Standard Deviation | 0.33 | 0.26 | 1.82 |
| Threshold | 1.16 | 0.15 | 1.41 |
| Anomalous | 1.49 | 0.41 | 2.56 |
| Very Anomalous | 1.82 | 0.67 | 4.65 |

Listing of threshold & anomalous values:

| Sample | Raw Value | | Log10(Value) | |
|---|---|---|---|---|
| ( 1 ) | 1.30 | * thresh | 0.11 | |
| ( 3 ) | 1.20 | * thresh | 0.08 | |
| ( 4 ) | 1.60 | ** ANOM | 0.20 | * thresh |
| ( 15 ) | 1.20 | * thresh | 0.08 | |
| ( 16 ) | 1.60 | ** ANOM | 0.20 | * thresh |
| ( 35 ) | 3.10 | *** V ANOM | 0.49 | ** ANOM |
| ( 43 ) | 2.60 | *** V ANOM | 0.41 | ** ANOM |
| ( 64 ) | 2.00 | *** V ANOM | 0.30 | * thresh |
| ( 66 ) | 1.20 | * thresh | 0.08 | |
| ( 100 ) | 1.30 | * thresh | 0.11 | |
| ( 106 ) | 1.50 | ** ANOM | 0.18 | * thresh |
| ( 107 ) | 1.30 | * thresh | 0.11 | |
| ( 115 ) | 1.40 | * thresh | 0.15 | |
| ( 116 ) | 1.20 | * thresh | 0.08 | |
| ( 120 ) | 1.20 | * thresh | 0.08 | |
| ( 124 ) | 2.10 | *** V ANOM | 0.32 | * thresh |
| ( 137 ) | 1.60 | ** ANOM | 0.20 | * thresh |
| ( 161 ) | 1.30 | * thresh | 0.11 | |
| ( 181 ) | 2.10 | *** V ANOM | 0.32 | * thresh |
| ( 215 ) | 1.20 | * thresh | 0.08 | |
| ( 254 ) | 1.40 | * thresh | 0.15 | |
| ( 270 ) | 1.40 | * thresh | 0.15 | |
| ( 393 ) | 1.30 | * thresh | 0.11 | |
| ( 520 ) | 1.40 | * thresh | 0.15 | |
| ( 556 ) | 1.60 | ** ANOM | 0.20 | * thresh |

```
Class % vs. Log10(PPM):  B:BRADNER.VGC
   SILVER

   upper                           F R E Q U E N C Y   ( % )
   Log10  Class%   Cum%  +----:----1----:----2----:----3----:----4----:----5
    0.03   94.32   94.32 :*********************************************>> :
    0.13    3.20   97.51 T***  .    :    .    :    .    :    .    :    .    :
    0.23    1.60   99.11 :**   .    :    .    :    .    :    .    :    .    :
    0.33    0.53   99.64 A*    .    :    .    :    .    :    .    :    .    :
    0.43    0.18   99.82 :     .    :    .    :    .    :    .    :    .    :
    0.53    0.18  100.00 :     .    :    .    :    .    :    .    :    .    :
                         +----:----1----:----2----:----3----:----4----:----5
```

```
Cumulative Percent vs. Log(PPM):  B:BRADNER.VGC
   SILVER

        upper                       P R O B A B I L I T Y   ( C U M % )
   PPM  Log10    Cum%   .01 .1 .5  2     10   30  50% 70    90    98 99 999 9999
   1.1  0.03    94.32    :   :  :  :      :    :   ¦   :     : +   :  :  :    :
   1.3  0.13    97.51    :   :  :  :      :    :   ¦   :     :   + :  :  :    :
   1.7  0.23    99.11    :   :  :  :      :    :   ¦   :     :     :+ :  :    :
   2.1  0.33    99.64    :   :  :  :      :    :   ¦   :     :     :  + :    :
   2.7  0.43    99.82    :   :  :  :      :    :   ¦   :     :     :  : +:    :
   3.4  0.53   100.00    :   :  :  :      :    :   ¦   :     :     :  :  :   :+
                        .01 .1 .5  2     10   30  50% 70    90    98 99 999 9999
```

File B:BRADNER.VGC Threshold/Anomaly Statistics
ARSENIC

| B:BRADNER.VGC / col 8 | Normal | Log-xform | Un-xform |
|---|---|---|---|
| No. Samples | 536 | | |
| Min | 2.00 | | |
| Max | 80.00 | | |
| Mean | 6.88 | 0.66 | 4.52 |
| Standard Deviation | 8.71 | 0.36 | 2.27 |
| Threshold | 24.29 | 1.37 | 23.40 |
| Anomalous | 33.00 | 1.73 | 53.21 |
| Very Anomalous | 41.71 | 2.08 | 120.99 |

Listing of threshold & anomalous values:

| Sample | Raw Value | | | Log10(Value) | | |
|---|---|---|---|---|---|---|
| ( 35 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 36 ) | 35.00 | ** | ANOM | 1.54 | * | thresh |
| ( 37 ) | 50.00 | *** | V ANOM | 1.70 | * | thresh |
| ( 58 ) | 80.00 | *** | V ANOM | 1.90 | ** | ANOM |
| ( 110 ) | 40.00 | ** | ANOM | 1.60 | * | thresh |
| ( 114 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 125 ) | 50.00 | *** | V ANOM | 1.70 | * | thresh |
| ( 280 ) | 50.00 | *** | V ANOM | 1.70 | * | thresh |
| ( 308 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 309 ) | 50.00 | *** | V ANOM | 1.70 | * | thresh |
| ( 310 ) | 60.00 | *** | V ANOM | 1.78 | ** | ANOM |
| ( 313 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 314 ) | 35.00 | ** | ANOM | 1.54 | * | thresh |
| ( 315 ) | 40.00 | ** | ANOM | 1.60 | * | thresh |
| ( 316 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 502 ) | 40.00 | ** | ANOM | 1.60 | * | thresh |
| ( 504 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 522 ) | 35.00 | ** | ANOM | 1.54 | * | thresh |
| ( 523 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 525 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 528 ) | 50.00 | *** | V ANOM | 1.70 | * | thresh |
| ( 531 ) | 40.00 | ** | ANOM | 1.60 | * | thresh |
| ( 532 ) | 30.00 | * | thresh | 1.48 | * | thresh |
| ( 533 ) | 25.00 | * | thresh | 1.40 | * | thresh |

```
Class % vs. Log10(PPM): B:BRADNER.VGC
   ARSENIC

   upper                              F R E Q U E N C Y   ( % )
   Log10  Class%    Cum% +----:----1----:----2----:----3----:----4----:----5
    0.03    0.00    0.00 :    .    :    .    :    .    :    .    :    .    :
    0.13    0.00    0.00 :    .    :    .    :    .    :    .    :    .    :
    0.23    0.00    0.00 :    .    :    .    :    .    :    .    :    .    :
    0.33   33.96   33.96 :**********************************.   :    .    :
    0.43    0.00   33.96 :    .    :    .    :    .    :    .    :    .    :
    0.53    0.00   33.96 :    .    :    .    :    .    :    .    :    .    :
    0.63   37.87   71.83 M**************************************:    .    :
    0.73    0.00   71.83 :    .    :    .    :    .    :    .    :    .    :
    0.83    0.00   71.83 :    .    :    .    :    .    :    .    :    .    :
    0.93    0.00   71.83 :    .    :    .    :    .    :    .    :    .    :
    1.03   15.49   87.31 :***************    :    .    :    .    :    .    :
    1.13    0.00   87.31 :    .    :    .    :    .    :    .    :    .    :
    1.23    5.60   92.91 :******   :    .    :    .    :    .    :    .    :
    1.33    2.61   95.52 T***.    :    .    :    .    :    .    :    .    :
    1.43    0.19   95.71 :    .    :    .    :    .    :    .    :    .    :
    1.53    1.68   97.39 :**  .    :    .    :    .    :    .    :    .    :
    1.63    1.31   98.69 A*   .    :    .    :    .    :    .    :    .    :
    1.73    0.93   99.63 :*   .    :    .    :    .    :    .    :    .    :
    1.83    0.19   99.81 :    .    :    .    :    .    :    .    :    .    :
    1.93    0.19  100.00 :    .    :    .    :    .    :    .    :    .    :
                         +----:----1----:----2----:----3----:----4----:----5
```

```
Cumulative Percent vs. Log(PPM): B:BRADNER.VGC
   ARSENIC

       upper                      P R O B A B I L I T Y   ( C U M % )
  PPM  Log10    Cum%   .01 .1 .5  2     10    30  50% 70    90     98 99 999 9999
  1.7  0.23     0.00    :   :  :  :      :     :   |   :     :      :  :  :    :
  2.1  0.33    33.96    :   :  :  :      :     +   |   :     :      :  :  :    :
  2.7  0.43    33.96    :   :  :  :      :     :   |   :     :      :  :  :    :
  3.4  0.53    33.96    :   :  :  :      :     :   |   :     :      :  :  :    :
  4.3  0.63    71.83    :   :  :  :      :     :   |   +     :      :  :  :    :
  5.4  0.73    71.83    :   :  :  :      :     :   |   :     :      :  :  :    :
  6.8  0.83    71.83    :   :  :  :      :     :   |   :     :      :  :  :    :
  8.5  0.93    71.83    :   :  :  :      :     :   |   :     :      :  :  :    :
   11  1.03    87.31    :   :  :  :      :     :   |   :    +:      :  :  :    :
   13  1.13    87.31    :   :  :  :      :     :   |   :     :      :  :  :    :
   17  1.23    92.91    :   :  :  :      :     :   |   :     :+     :  :  :    :
   21  1.33    95.52    :   :  :  :      :     :   |   :     :  +   :  :  :    :
   27  1.43    95.71    :   :  :  :      :     :   |   :     :  +   :  :  :    :
   34  1.53    97.39    :   :  :  :      :     :   |   :     :   +  :  :  :    :
   43  1.63    98.69    :   :  :  :      :     :   |   :     :      +  :  :    :
   54  1.73    99.63    :   :  :  :      :     :   |   :     :      :  +  :    :
   68  1.83    99.81    :   :  :  :      :     :   |   :     :      :  : +:    :
   85  1.93   100.00    :   :  :  :      :     :   |   :     :      :  :  :   :+
                       .01 .1 .5  2     10    30  50% 70    90     98 99 999 9999
```

File B:BRADNER.VGC Threshold/Anomaly Statistics
ZINC

| B:BRADNER.VGC / col 5 | Normal | Log-xform | Un-xform |
|---|---|---|---|
| No. Samples | 576 | | |
| Min | 1.00 | | |
| Max | 286.00 | | |
| Mean | 66.81 | 1.74 | 54.33 |
| Standard Deviation | 41.04 | 0.31 | 2.02 |
| Threshold | 148.89 | 2.35 | 222.19 |
| Anomalous | 189.93 | 2.65 | 449.33 |
| Very Anomalous | 230.97 | 2.96 | 908.69 |
| Upper Discard Limit | 500.00 | | |

Listing of threshold & anomalous values:

| Sample | Raw Value | | | Log10(Value) | | |
|---|---|---|---|---|---|---|
| ( 14 ) | 174.00 | * | thresh | 2.24 | | |
| ( 27 ) | 149.00 | * | thresh | 2.17 | | |
| ( 42 ) | 220.00 | ** | ANOM | 2.34 | | |
| ( 63 ) | 229.00 | ** | ANOM | 2.36 | * | thresh |
| ( 64 ) | 177.00 | * | thresh | 2.25 | | |
| ( 103 ) | 220.00 | ** | ANOM | 2.34 | | |
| ( 125 ) | 200.00 | ** | ANOM | 2.30 | | |
| ( 140 ) | 184.00 | * | thresh | 2.26 | | |
| ( 142 ) | 286.00 | *** | V ANOM | 2.46 | * | thresh |
| ( 151 ) | 159.00 | * | thresh | 2.20 | | |
| ( 217 ) | 177.00 | * | thresh | 2.25 | | |
| ( 277 ) | 198.00 | ** | ANOM | 2.30 | | |
| ( 340 ) | 149.00 | * | thresh | 2.17 | | |
| ( 357 ) | 190.00 | ** | ANOM | 2.28 | | |
| ( 410 ) | 205.00 | ** | ANOM | 2.31 | | |
| ( 429 ) | 151.00 | * | thresh | 2.18 | | |
| ( 525 ) | 150.00 | * | thresh | 2.18 | | |
| ( 532 ) | 166.00 | * | thresh | 2.22 | | |
| ( 542 ) | 160.00 | * | thresh | 2.20 | | |
| ( 545 ) | 226.00 | ** | ANOM | 2.35 | * | thresh |
| ( 550 ) | 150.00 | * | thresh | 2.18 | | |
| ( 554 ) | 156.00 | * | thresh | 2.19 | | |
| ( 561 ) | 165.00 | * | thresh | 2.22 | | |
| ( 576 ) | 166.00 | * | thresh | 2.22 | | |

Note: 2 value(s) not included ( exceed limit of 500 )

Class % vs. Log10(PPM): B:BRADNER.VGC
ZINC

```
upper                              F R E Q U E N C Y   ( % )
Log10  Class%   Cum%  +----:----1----:----2----:----3----:----4----:----5
 0.03   0.17    0.17  :    .    :    .    :    .    :    .    :    .    :
 0.13   0.00    0.17  :    .    :    .    :    .    :    .    :    .    :
 0.23   0.00    0.17  :    .    :    .    :    .    :    .    :    .    :
 0.33   0.00    0.17  :    .    :    .    :    .    :    .    :    .    :
 0.43   0.00    0.17  :    .    :    .    :    .    :    .    :    .    :
 0.53   0.00    0.17  :    .    :    .    :    .    :    .    :    .    :
 0.63   0.17    0.35  :    .    :    .    :    .    :    .    :    .    :
 0.73   0.69    1.04  :*   .    :    .    :    .    :    .    :    .    :
 0.83   0.00    1.04  :    .    :    .    :    .    :    .    :    .    :
 0.93   0.52    1.56  :*   .    :    .    :    .    :    .    :    .    :
 1.03   1.39    2.95  :*   .    :    .    :    .    :    .    :    .    :
 1.13   1.04    3.99  :*   .    :    .    :    .    :    .    :    .    :
 1.23   2.08    6.08  :**  .    :    .    :    .    :    .    :    .    :
 1.33   3.30    9.38  :*** .    :    .    :    .    :    .    :    .    :
 1.43   4.86   14.24  :*****    :    .    :    .    :    .    :    .    :
 1.53   4.69   18.92  :*****    :    .    :    .    :    .    :    .    :
 1.63  11.98   30.90  :************  .    :    .    :    .    :    .    :
 1.73  13.72   44.62  M**************.    :    .    :    .    :    .    :
 1.83  13.89   58.51  :**************.    :    .    :    .    :    .    :
 1.93  14.41   72.92  :**************.    :    .    :    .    :    .    :
 2.03  12.67   85.59  :************* .    :    .    :    .    :    .    :
 2.13   7.47   93.06  :*******  :    .    :    .    :    .    :    .    :
 2.23   4.69   97.74  :*****    :    .    :    .    :    .    :    .    :
 2.33   1.39   99.13  T*   .    :    .    :    .    :    .    :    .    :
 2.43   0.69   99.83  :*   .    :    .    :    .    :    .    :    .    :
 2.53   0.17  100.00  :    .    :    .    :    .    :    .    :    .    :
                      +----:----1----:----2----:----3----:----4----:----5
```

Cumulative Percent vs. Log(PPM): B:BRADNER.VGC

ZINC

```
          upper                   P R O B A B I L I T Y   ( C U M % )
 PPM  Log10    Cum%  .01 .1 .5  2    10   30  50% 70   90    98 99 999 9999
 1.1   0.03    0.17   :   +  :  :     :    :   |   :    :     :  :  :   :
 1.3   0.13    0.17   :   :  :  :     :    :   |   :    :     :  :  :   :
 1.7   0.23    0.17   :   :  :  :     :    :   |   :    :     :  :  :   :
 2.1   0.33    0.17   :   :  :  :     :    :   |   :    :     :  :  :   :
 2.7   0.43    0.17   :   :  :  :     :    :   |   :    :     :  :  :   :
 3.4   0.53    0.17   :   :  :  :     :    :   |   :    :     :  :  :   :
 4.3   0.63    0.35   :   : +:  :     :    :   |   :    :     :  :  :   :
 5.4   0.73    1.04   :   :  :+ :     :    :   |   :    :     :  :  :   :
 6.8   0.83    1.04   :   :  :  :     :    :   |   :    :     :  :  :   :
 8.5   0.93    1.56   :   :  : +:     :    :   |   :    :     :  :  :   :
  11   1.03    2.95   :   :  :  :+    :    :   |   :    :     :  :  :   :
  13   1.13    3.99   :   :  :  :  +  :    :   |   :    :     :  :  :   :
  17   1.23    6.08   :   :  :  :   + :    :   |   :    :     :  :  :   :
  21   1.33    9.38   :   :  :  :    +:    :   |   :    :     :  :  :   :
  27   1.43   14.24   :   :  :  :     :+   :   |   :    :     :  :  :   :
  34   1.53   18.92   :   :  :  :     :  + :   |   :    :     :  :  :   :
  43   1.63   30.90   :   :  :  :     :    +   |   :    :     :  :  :   :
  54   1.73   44.62   :   :  :  :     :    :  +|   :    :     :  :  :   :
  68   1.83   58.51   :   :  :  :     :    :   |+  :    :     :  :  :   :
  85   1.93   72.92   :   :  :  :     :    :   |   +    :     :  :  :   :
 107   2.03   85.59   :   :  :  :     :    :   |   :  + :     :  :  :   :
 135   2.13   93.06   :   :  :  :     :    :   |   :    :+    :  :  :   :
 170   2.23   97.74   :   :  :  :     :    :   |   :    :    +:  :  :   :
 214   2.33   99.13   :   :  :  :     :    :   |   :    :     :+ :  :   :
 269   2.43   99.83   :   :  :  :     :    :   |   :    :     :  : +:   :
 339   2.53  100.00   :   :  :  :     :    :   |   :    :     :  :  :   :+
                     .01 .1 .5  2    10   30  50% 70   90    98 99 999 9999
```

File B:BRADNER.VGC Threshold/Anomaly Statistics
LEAD

| B:BRADNER.VGC / col 4 | Normal | Log-xform | Un-xform |
|---|---|---|---|
| No. Samples | 576 | | |
| Min | 1.00 | | |
| Max | 160.00 | | |
| Mean | 17.78 | 1.20 | 15.91 |
| Standard Deviation | 9.90 | 0.21 | 1.64 |
| Threshold | 37.59 | 1.63 | 42.64 |
| Anomalous | 47.49 | 1.84 | 69.82 |
| Very Anomalous | 57.39 | 2.06 | 114.30 |

Listing of threshold & anomalous values:

| Sample | Raw Value | | | Log10(Value) | | |
|---|---|---|---|---|---|---|
| ( 3 ) | 40.00 | * | thresh | 1.60 | | |
| ( 4 ) | 59.00 | *** | V ANOM | 1.77 | * | thresh |
| ( 14 ) | 50.00 | ** | ANOM | 1.70 | * | thresh |
| ( 35 ) | 40.00 | * | thresh | 1.60 | | |
| ( 37 ) | 39.00 | * | thresh | 1.59 | | |
| ( 83 ) | 45.00 | * | thresh | 1.65 | * | thresh |
| ( 105 ) | 40.00 | * | thresh | 1.60 | | |
| ( 126 ) | 96.00 | *** | V ANOM | 1.98 | ** | ANOM |
| ( 142 ) | 160.00 | *** | V ANOM | 2.20 | *** | V ANOM |
| ( 182 ) | 49.00 | ** | ANOM | 1.69 | * | thresh |
| ( 249 ) | 40.00 | * | thresh | 1.60 | | |
| ( 357 ) | 44.00 | * | thresh | 1.64 | * | thresh |
| ( 410 ) | 41.00 | * | thresh | 1.61 | | |

Class % vs. Log10(PPM): B:BRADNER.VGC
LEAD

```
 upper                            F R E Q U E N C Y   ( % )
 Log10  Class%    Cum% +----:----1----:----2----:----3----:----4----:----5
  0.03    0.17    0.17 :    .    :    .    :    .    :    .    :    .    :
  0.13    0.00    0.17 :    .    :    .    :    .    :    .    :    .    :
  0.23    0.00    0.17 :    .    :    .    :    .    :    .    :    .    :
  0.33    0.69    0.87 :*   .    :    .    :    .    :    .    :    .    :
  0.43    0.00    0.87 :    .    :    .    :    .    :    .    :    .    :
  0.53    0.35    1.22 :    .    :    .    :    .    :    .    :    .    :
  0.63    0.35    1.56 :    .    :    .    :    .    :    .    :    .    :
  0.73    2.60    4.17 :*** .    :    .    :    .    :    .    :    .    :
  0.83    1.56    5.73 :**  .    :    .    :    .    :    .    :    .    :
  0.93    2.08    7.81 :**  .    :    .    :    .    :    .    :    .    :
  1.03    7.64   15.45 :******** :    .    :    .    :    .    :    .    :
  1.13    8.16   23.61 M******** :    .    :    .    :    .    :    .    :
  1.23   27.78   51.39 :**************************** :    .    :    .    :
  1.33   27.08   78.47 :***************************  :    .    :    .    :
  1.43   13.89   92.36 :**************.    :    .    :    .    :    .    :
  1.53    4.69   97.05 T*****    :    .    :    .    :    .    :    .    :
  1.63    1.74   98.78 :**  .    :    .    :    .    :    .    :    .    :
  1.73    0.69   99.48 :*   .    :    .    :    .    :    .    :    .    :
  1.83    0.17   99.65 A    .    :    .    :    .    :    .    :    .    :
  1.93    0.00   99.65 :    .    :    .    :    .    :    .    :    .    :
  2.03    0.17   99.83 V    .    :    .    :    .    :    .    :    .    :
  2.13    0.00   99.83 :    .    :    .    :    .    :    .    :    .    :
  2.23    0.17  100.00 :    .    :    .    :    .    :    .    :    .    :
                       +----:----1----:----2----:----3----:----4----:----5
```

Cumulative Percent vs. Log(PPM): B:BRADNER.VGC
LEAD

```
      upper                     P R O B A B I L I T Y   ( C U M % )
 PPM  Log10     Cum%   .01 .1 .5  2     10   30  50% 70   90    98 99 999 9999
 1.1   0.03     0.17   :   +  :  :     :    :   |   :    :     :  :  :   :
 1.3   0.13     0.17   :   :  :  :     :    :   |   :    :     :  :  :   :
 1.7   0.23     0.17   :   :  :  :     :    :   |   :    :     :  :  :   :
 2.1   0.33     0.87   :   :  :+ :     :    :   |   :    :     :  :  :   :
 2.7   0.43     0.87   :   :  :  :     :    :   |   :    :     :  :  :   :
 3.4   0.53     1.22   :   :  : +:     :    :   |   :    :     :  :  :   :
 4.3   0.63     1.56   :   :  : +:     :    :   |   :    :     :  :  :   :
 5.4   0.73     4.17   :   :  :  : +   :    :   |   :    :     :  :  :   :
 6.8   0.83     5.73   :   :  :  :  +  :    :   |   :    :     :  :  :   :
 8.5   0.93     7.81   :   :  :  :   + :    :   |   :    :     :  :  :   :
  11   1.03    15.45   :   :  :  :     :+   :   |   :    :     :  :  :   :
  13   1.13    23.61   :   :  :  :     :  + :   |   :    :     :  :  :   :
  17   1.23    51.39   :   :  :  :     :    :   +   :    :     :  :  :   :
  21   1.33    78.47   :   :  :  :     :    :   |   :+   :     :  :  :   :
  27   1.43    92.36   :   :  :  :     :    :   |   :    :+    :  :  :   :
  34   1.53    97.05   :   :  :  :     :    :   |   :    :   + :  :  :   :
  43   1.63    98.78   :   :  :  :     :    :   |   :    :     +  :  :   :
  54   1.73    99.48   :   :  :  :     :    :   |   :    :     : +:  :   :
  68   1.83    99.65   :   :  :  :     :    :   |   :    :     :  +  :   :
  85   1.93    99.65   :   :  :  :     :    :   |   :    :     :  :  :   :
 107   2.03    99.83   :   :  :  :     :    :   |   :    :     :  : +:   :
 135   2.13    99.83   :   :  :  :     :    :   |   :    :     :  :  :   :
 170   2.23   100.00   :   :  :  :     :    :   |   :    :     :  :  :   :+
                       .01 .1 .5  2     10   30  50% 70   90    98 99 999 9999
```

File B:BRADNER.VGC Threshold/Anomaly Statistics
COPPER

| B:BRADNER.VGC / col 3 | Normal | Log-xform | Un-xform |
|---|---|---|---|
| No. Samples | 575 | | |
| Min | 2.00 | | |
| Max | 95.00 | | |
| Mean | 13.87 | 1.07 | 11.85 |
| Standard Deviation | 8.87 | 0.24 | 1.75 |
| Threshold | 31.62 | 1.56 | 36.46 |
| Anomalous | 40.49 | 1.81 | 63.94 |
| Very Anomalous | 49.37 | 2.05 | 112.15 |

Listing of threshold & anomalous values:

| Sample | Raw Value | | | Log10(Value) | | |
|---|---|---|---|---|---|---|
| ( 9 ) | 37.00 | * | thresh | 1.57 | * | thresh |
| ( 23 ) | 34.00 | * | thresh | 1.53 | | |
| ( 26 ) | 35.00 | * | thresh | 1.54 | | |
| ( 35 ) | 39.00 | * | thresh | 1.59 | * | thresh |
| ( 43 ) | 44.00 | ** | ANOM | 1.64 | * | thresh |
| ( 44 ) | 74.00 | *** | V ANOM | 1.87 | ** | ANOM |
| ( 124 ) | 35.00 | * | thresh | 1.54 | | |
| ( 163 ) | 35.00 | * | thresh | 1.54 | | |
| ( 224 ) | 37.00 | * | thresh | 1.57 | * | thresh |
| ( 233 ) | 36.00 | * | thresh | 1.56 | | |
| ( 326 ) | 54.00 | *** | V ANOM | 1.73 | * | thresh |
| ( 336 ) | 36.00 | * | thresh | 1.56 | | |
| ( 399 ) | 49.00 | ** | ANOM | 1.69 | * | thresh |
| ( 409 ) | 40.00 | * | thresh | 1.60 | * | thresh |
| ( 429 ) | 35.00 | * | thresh | 1.54 | | |
| ( 461 ) | 36.00 | * | thresh | 1.56 | | |
| ( 531 ) | 95.00 | *** | V ANOM | 1.98 | ** | ANOM |
| ( 542 ) | 35.00 | * | thresh | 1.54 | | |
| ( 559 ) | 32.00 | * | thresh | 1.51 | | |
| ( 567 ) | 72.00 | *** | V ANOM | 1.86 | ** | ANOM |

```
Class % vs. Log10(PPM): B:BRADNER.VGC
   COPPER

   upper                          F R E Q U E N C Y   ( % )
   Log10 Class%   Cum% +----:----1----:----2----:----3----:----4----:----5
    0.03   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.13   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.23   0.00   0.00 :    .    :    .    :    .    :    .    :    .    :
    0.33   0.87   0.87 :*   .    :    .    :    .    :    .    :    .    :
    0.43   0.00   0.87 :    .    :    .    :    .    :    .    :    .    :
    0.53   0.87   1.74 :*   .    :    .    :    .    :    .    :    .    :
    0.63   2.78   4.52 :*** .    :    .    :    .    :    .    :    .    :
    0.73   5.91  10.43 :******   :    .    :    .    :    .    :    .    :
    0.83   4.17  14.61 :****.    :    .    :    .    :    .    :    .    :
    0.93   6.78  21.39 :*******  :    .    :    .    :    .    :    .    :
    1.03  21.74  43.13 M**********************  .    :    .    :    .    :
    1.13  12.35  55.48 :************    .    :    .    :    .    :    .    :
    1.23  22.26  77.74 :**********************  .    :    .    :    .    :
    1.33   8.87  86.61 :*********:    .    :    .    :    .    :    .    :
    1.43   7.48  94.09 :*******  :    .    :    .    :    .    :    .    :
    1.53   2.61  96.70 T*** .    :    .    :    .    :    .    :    .    :
    1.63   2.26  98.96 :**  .    :    .    :    .    :    .    :    .    :
    1.73   0.35  99.30 A    .    :    .    :    .    :    .    :    .    :
    1.83   0.17  99.48 :    .    :    .    :    .    :    .    :    .    :
    1.93   0.35  99.83 :    .    :    .    :    .    :    .    :    .    :
    2.03   0.17 100.00 V    .    :    .    :    .    :    .    :    .    :
                       +----:----1----:----2----:----3----:----4----:----5
```

```
Cumulative Percent vs. Log(PPM): B:BRADNER.VGC
   COPPER

        upper               P R O B A B I L I T Y   ( C U M % )
   PPM  Log10    Cum%  .01 .1 .5  2     10   30  50% 70   90     98 99 999 9999
   1.7  0.23     0.00   :   :  :  :      :    :   |   :    :      :  :  :    :
   2.1  0.33     0.87   :   :  :+ :      :    :   |   :    :      :  :  :    :
   2.7  0.43     0.87   :   :  :  :      :    :   |   :    :      :  :  :    :
   3.4  0.53     1.74   :   :  :  +      :    :   |   :    :      :  :  :    :
   4.3  0.63     4.52   :   :  :  : +    :    :   |   :    :      :  :  :    :
   5.4  0.73    10.43   :   :  :  :     +:    :   |   :    :      :  :  :    :
   6.8  0.83    14.61   :   :  :  :      :+   :   |   :    :      :  :  :    :
   8.5  0.93    21.39   :   :  :  :      :   +:   |   :    :      :  :  :    :
    11  1.03    43.13   :   :  :  :      :    : + |   :    :      :  :  :    :
    13  1.13    55.48   :   :  :  :      :    :   |+  :    :      :  :  :    :
    17  1.23    77.74   :   :  :  :      :    :   |   :+   :      :  :  :    :
    21  1.33    86.61   :   :  :  :      :    :   |   :  + :      :  :  :    :
    27  1.43    94.09   :   :  :  :      :    :   |   :    :   +  :  :  :    :
    34  1.53    96.70   :   :  :  :      :    :   |   :    :     +:  :  :    :
    43  1.63    98.96   :   :  :  :      :    :   |   :    :      :+ :  :    :
    54  1.73    99.30   :   :  :  :      :    :   |   :    :      : +:  :    :
    68  1.83    99.48   :   :  :  :      :    :   |   :    :      : +:  :    :
    85  1.93    99.83   :   :  :  :      :    :   |   :    :      :  : +:    :
   107  2.03   100.00   :   :  :  :      :    :   |   :    :      :  :  :   :+
                       .01 .1 .5  2     10   30  50% 70   90     98 99 999 9999
```

File B:BRADNER.VGC Threshold/Anomaly Statistics
MOLYBDENUM

| B:BRADNER.VGC / col 2 | Normal | Log-xform | Un-xform |
|---|---|---|---|
| No. Samples | 383 | | |
| Min | 1.00 | | |
| Max | 20.00 | | |
| Mean | 2.71 | 0.37 | 2.32 |
| Standard Deviation | 2.06 | 0.23 | 1.69 |
| Threshold | 6.84 | 0.82 | 6.65 |
| Anomalous | 8.91 | 1.05 | 11.25 |
| Very Anomalous | 10.97 | 1.28 | 19.05 |

Listing of threshold & anomalous values:

| Sample | Raw Value | | Log10(Value) | |
|---|---|---|---|---|
| ( 22 ) | 20.00 | *** V ANOM | 1.30 | *** V ANOM |
| ( 23 ) | 8.00 | * thresh | 0.90 | * thresh |
| ( 24 ) | 19.00 | *** V ANOM | 1.28 | ** ANOM |
| ( 44 ) | 7.00 | * thresh | 0.85 | * thresh |
| ( 46 ) | 7.00 | * thresh | 0.85 | * thresh |
| ( 54 ) | 18.00 | *** V ANOM | 1.26 | ** ANOM |
| ( 55 ) | 9.00 | ** ANOM | 0.95 | * thresh |
| ( 107 ) | 7.00 | * thresh | 0.85 | * thresh |
| ( 127 ) | 7.00 | * thresh | 0.85 | * thresh |
| ( 230 ) | 7.00 | * thresh | 0.85 | * thresh |
| ( 298 ) | 7.00 | * thresh | 0.85 | * thresh |
| ( 299 ) | 7.00 | * thresh | 0.85 | * thresh |
| ( 376 ) | 17.00 | *** V ANOM | 1.23 | ** ANOM |

Class % vs. Log10(PPM): B:BRADNER.VGC
MOLYBDENUM

```
upper                             F R E Q U E N C Y   ( % )
Log10  Class%   Cum%  +----:----1----:----2----:----3----:----4----:----5
 0.03   16.97  16.97  :*****************  :    .    :    .    :    .    :
 0.13    0.00  16.97  :    .    :    .    :    .    :    .    :    .    :
 0.23    0.00  16.97  :    .    :    .    :    .    :    .    :    .    :
 0.33   39.16  56.14  M***************************************:    .    :
 0.43    0.00  56.14  :    .    :    .    :    .    :    .    :    .    :
 0.53   27.15  83.29  :***************************  :    .    :    .    :
 0.63    9.40  92.69  :*********:    .    :    .    :    .    :    .    :
 0.73    3.13  95.82  T***.    :    .    :    .    :    .    :    .    :
 0.83    0.78  96.61  :*   .    :    .    :    .    :    .    :    .    :
 0.93    2.09  98.69  :**  .    :    .    :    .    :    .    :    .    :
 1.03    0.26  98.96  A    .    :    .    :    .    :    .    :    .    :
 1.13    0.00  98.96  :    .    :    .    :    .    :    .    :    .    :
 1.23    0.00  98.96  V    .    :    .    :    .    :    .    :    .    :
 1.33    1.04 100.00  :*   .    :    .    :    .    :    .    :    .    :
                      +----:----1----:----2----:----3----:----4----:----5
```

Cumulative Percent vs. Log(PPM): B:BRADNER.VGC
MOLYBDENUM

```
      upper                        P R O B A B I L I T Y   ( C U M % )
 PPM  Log10    Cum%  .01 .1 .5  2    10   30  50% 70   90    98 99 999 9999
 1.1  0.03    16.97   :   :  :  :     : +  :   |   :    :     :  :  :   :
 1.3  0.13    16.97   :   :  :  :     :    :   |   :    :     :  :  :   :
 1.7  0.23    16.97   :   :  :  :     :    :   |   :    :     :  :  :   :
 2.1  0.33    56.14   :   :  :  :     :    :   |+  :    :     :  :  :   :
 2.7  0.43    56.14   :   :  :  :     :    :   |   :    :     :  :  :   :
 3.4  0.53    83.29   :   :  :  :     :    :   |   : +  :     :  :  :   :
 4.3  0.63    92.69   :   :  :  :     :    :   |   :    :+    :  :  :   :
 5.4  0.73    95.82   :   :  :  :     :    :   |   :    :  +  :  :  :   :
 6.8  0.83    96.61   :   :  :  :     :    :   |   :    :  +  :  :  :   :
 8.5  0.93    98.69   :   :  :  :     :    :   |   :    :     +  :  :   :
  11  1.03    98.96   :   :  :  :     :    :   |   :    :     :+ :  :   :
  13  1.13    98.96   :   :  :  :     :    :   |   :    :     :  :  :   :
  17  1.23    98.96   :   :  :  :     :    :   |   :    :     :  :  :   :
  21  1.33   100.00   :   :  :  :     :    :   |   :    :     :  :  :   :+
                     .01 .1 .5  2    10   30  50% 70   90    98 99 999 9999
```

VGC

VANGEOCHEM LAB LTD. 1521 PEMBERTON AVE., NORTH VANCOUVER, B.C., CANADA V7P 2S3 604-986-5211

Nov. 8 1983

TO: Orequest Consultants
#404 - 595 Howe St.
Vancouver, B C V6C 2T5

FROM: Vangeochem Lab Ltd.
1521 Pemberton Ave.
North V ncouver, B.C. V7P 2S3

SUBJECT: Analytical procedure used to determine hot acid soluble arsenic in geochemical silt, soil, lake sediments and rock samples.

for geochem soil humus , rock samples

1. Sample Preparation

(a) Geochemical soil, silt, lake sediments or rock samples were received in the laboratory in wet-strength 3½ x 6½ Kraft paper bags and rock samples in 4" x 6" Kraft paper bags.

(b) The wet samples were dried in a ventilated oven.

(c) The dried soil and silt samples were sifted by hands using a 8" diameter 80-mesh stainless steel sieves. The plus 80-mesh fraction was rejected and the minus 80-mesh fraction was transferred into a nwq bag for analysis later.

(d) The dried rock samples were crushed by using a jaw crusher and pulverized to 100-mesh or finer by using a disc mill. The pulverized samples were then put in a new bag for later analysis.

2. Method of Digestion

(a) 0.25 gram of the minus 80-mesh sample was used. Samples were weighed out by using a top-loading balance.

(b) Samples were heated in a sand bath with concentrated perchloric acid (70 - 72% $HClO_4$ by weight) at a medium heat for four hours.

(c) The digested samples were diluted with demineralized water.

...2

3. <u>Method of Analysis</u>

(a) Potassium iodide and stannous chloride in HCL were added to the digested samples.

(b) Zinc metal was introduced and the arsenic in solution was gassed off as arsene through a glass wool scrubber plug saturated with lead acetate and into a solution of silver diethyldithiocarbamate in chloroform with l-ephedrine, forming a red complex with the silver diethyldithiocarbamate.

(c) The concentration of the arsenic was determined colorimetrically by comparing the intensity of the color of the red complex with a set of known standards prepared in a similar fashion as the samples.

4. The analyses were supervised or determined by Mr. Eddie Tang or Mr. Conway Chun and their laboratory staff.

Eddie Tang
VANGEOCHEM LAB LTD.

VANGEOCHEM LAB LTD. 1521 PEMBERTON AVE., NORTH VANCOUVER, B.C. CANADA 604-xxxxxxxx 986-5211
V7P 2S3

Nov.8, 1983

To: Orequest Consultants
#404 - 595 Howe St.
Vancouver, B C V6C 2T5

From: Vangeochem Lab Ltd.
1521 Pemberton Avunue
North Vancouver, B.C. V7P 2S3

Subject: Analytical procedure used to determine hot acid soluble Mo, Cu,Pb,Zn, Ag in geochemical silt, soil and rock samples.

1983 samples

1. Sample Preparation

(a) Geochemical soil, silt or rock samples were received in the laboratory in wet-strength 3½ x 6½ Kraft paper bags and rock samples in 4" x 6" Kraft paper bags.

(b) The wet samples were dried in a ventilated oven.

(c) The dried soil and silt samples were sifted by hands using a 8" diameter 80-mesh stainless steel sieves. The plus 80-mesh fraction was rejected and the minus 80-mesh fraction was transferred into a new bag for analysis later.

(d) The dried rock samples were crushed by using a jaw crusher and pulverized to 100-mesh or finer by using a disc mill. The pulverized samples were then put in a new bag for later analysis.

2. Methods of Digestion

(a) 0.50 gram of the minus 80-mesh samples was used. Samples were weighed out by using a top-loading balance.

(b) Samples were heated in a sand bath with nitric and perchloric acids (15% to 85% by volume of the concentrated acids respectively).

.....2

(C) The digested samples were diluted with demineralized water to a fixed volume and shaken.

3. Method of Analysis

Mo, Cu, Pb, Zn, Ag analyses were determined by using a Techtron Atomic Absorption Spectrophotometer Model AA4 or Model AA5 with their respective hollow cathode lamps. The digested samples were aspirated directly into an air and acetylene flame, but Mo digestion were aspirated into an acetylene and nitrous flame. The results, in parts per million, were calculated by comparing a set of standards to calibrate the atomic absorption unit and displayed in a strip chart recorder.

4. The analyses were supervised or determined by Mr. Conway Chun or Mr. Eddie Tang and the labroatory staff.

5. Back Ground Correction

A Hydrongen continunnm lamp is used to correct the silver groung interferencesa.

Eddie Tang
VANGEOCHEM LAB LTD.

ET:jl

VANGEOCHEM LAB LTD. 1521 PEMBERTON AVE., NORTH VANCOUVER, B.C., CANADA 604-986-5211
V7P 2S3

Nov.8, 1983

To: Orequest Consultants
#404 - 595 Howe St.
Vancouver, B C V6C 2T5

From: Vangeochem Lab Ltd.
1521 Pemberton Ave.
North Vancouver, B.C. V7P 2S3

Subject: Analytical procedure used to determine Aqua Regia soluble gold in geochemical samples.

For soil and humus samples

1. Method of Sample Preparation

(a) Geochemical soil, silt or rock samples were received in the laboratory in wet-strength 4 x 6 Kraft paper bags or rock samples sometimes in 8" x 12" plastic bags.

(b) The dried soil and silt samples were sifted by hands using a 8" diameter 80-mesh stainless steel sieve, The plus 80-mesh fraction was rejected and the minus 80-mesh fraction was tracsferred into a new bag for analysis later.

(c) The dried rock samples were crushed by using a jaw crusher and pulverized to 100-mesh or finer by using a disc mill. The pulverized samples were then put in a new bag for later analysis.

2. Method of Digestion

(a) 5.00 - 10.00 grams of the minus 80-mesh samples were used. Samples were wrighed out by using a top-loading balance into beakers.

(b) 20 ml of Aqua Regia (3:1 $HCl:HNO_3$) were used to digest the samples over a hot plate vigorously.

(c) The digested samples were filtered and the washed pulps were discarded and the filtrate was reduced to about 5 ml.

(d) The Au comples ions were extracted into diisobutyl ketone and thiourea medium. (Anion exchange liquids "Aliquot 336").

... 2

(e) Separate Funnels were used to separate the organic layer.

3. Method of Detection

The gold analyses were detected by using a Techtron model AA5 Atomic Absorption Spectrophotometer with a gold hollow cathode Lamp. The results were read out on a strip chart recorder. A hydrogen lamp was used to correct any background interferences. The gold values in parts per billion were calculated by comparing them with a set of gold standards.

4. The analyses were supervised or determined by Mr. Conway Chun or Mr. Eddie Tang and his laboratory staff.

Eddie Tang
VANGEOCHEM LAB LTD.

ET: jl

VGC
**VANGEOCHEM LAB LTD.**
1521 PEMBERTON AVE., NORTH VANCOUVER, B.C., CANADA V7P 2S3 (604) 986-5211

Nov.8 1983

To: Orequest Consultants
#404 - 595 Howe St.
Vancouver, B C V6C 2T5

From: Vangeochem Lab Ltd.
1521 Pemberton Avenue
North Vancouver, B.C. V7P 2S3

Subject: Analytical procedure used to determine gold by fire-assay method and detected by atomic absorption spec. in geological samples.

For samples requested for Fireassays- AAS finished

1. Method of Sample Preparation

(a) Geochemical soil, silt or rock samples were received in the laboratory in wet-strength 4" x 6" Kraft paper bags or rock samples sometimes in 8" x 12" plastic bags.

(b) The dried soil and silt samples were sifted by hands using a 8" diameter 80-mesh stainless steel sieve. The plus 80-mesh fraction was rejected and the minus 80-mesh fraction was transferred into a new bag for analysis later.

(c) The dried rock samples were crushed by using a jaw crusher and pulverized to 100-mesh or finer by using a disc mill. The pulverized samples were then put in a new bag for later analysis.

2. Method of Extraction

(a) 20.0 - 30.0 grams of the pulp samples were used. Samples were weighed out by using a top-loading balance into a fusion pot.

(b) A Flux of litharge, soda ash, silica, borax, flour, or potassium nitrite is added, then fused at 1900°F and a lead button is formed.

(c) The gold is extract by cupellation and part with diluted nitric acid.

(d) The gold bead is saved or measurement later.

... 2

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3. Method of Detection

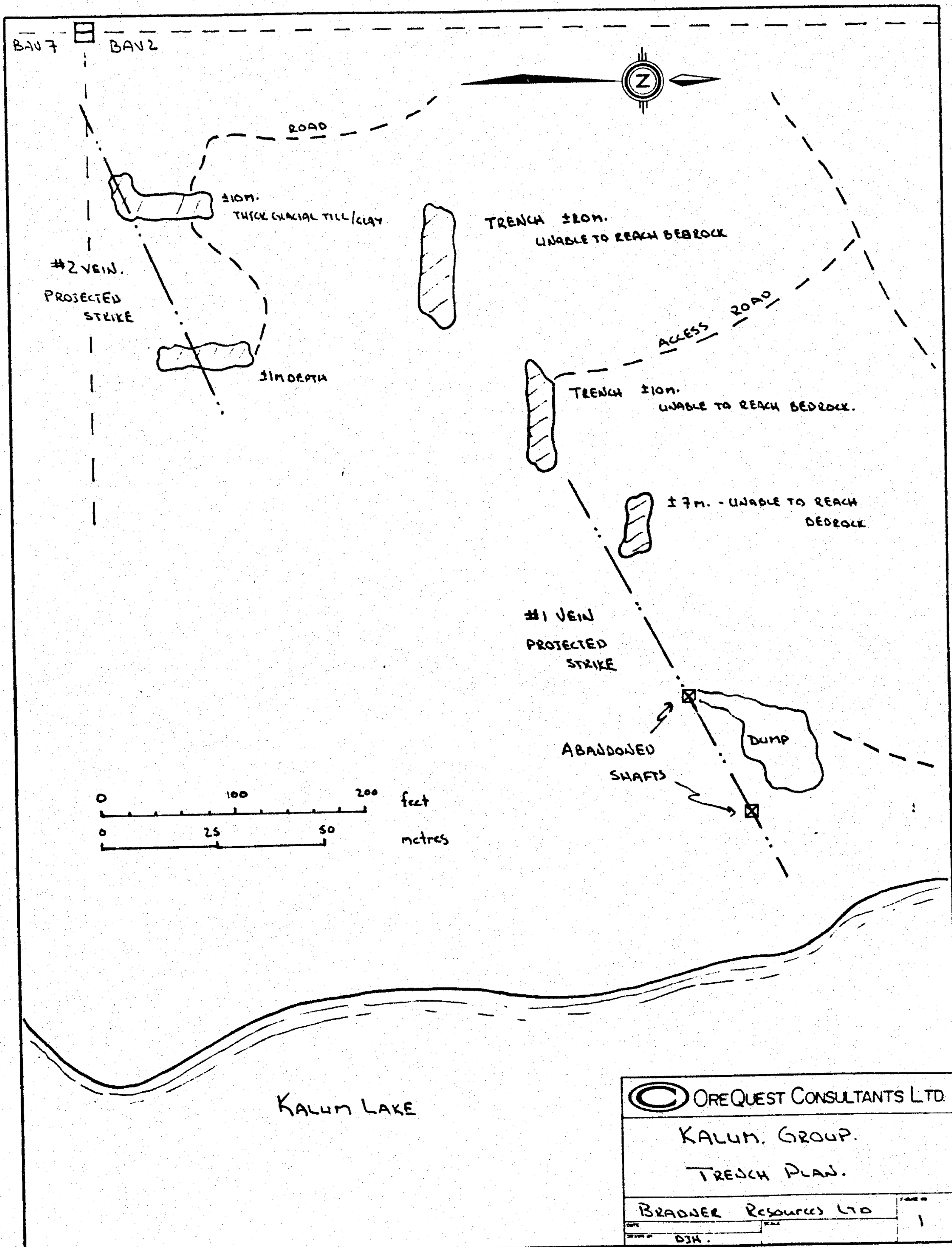
(a) The gold bead is disolved by boiling with sodium cyanide, hydrogen peroxide and amonium hydroxide.

(b) The gold analyses were detected by using a Techtron model AA5 Atomic Absorption Spectrophotometer with a gold hollow cathode lamp. The results were read out on a strip chart recorder. The gold values in parts per billion were calculated by comparing them with a set of gold standards.

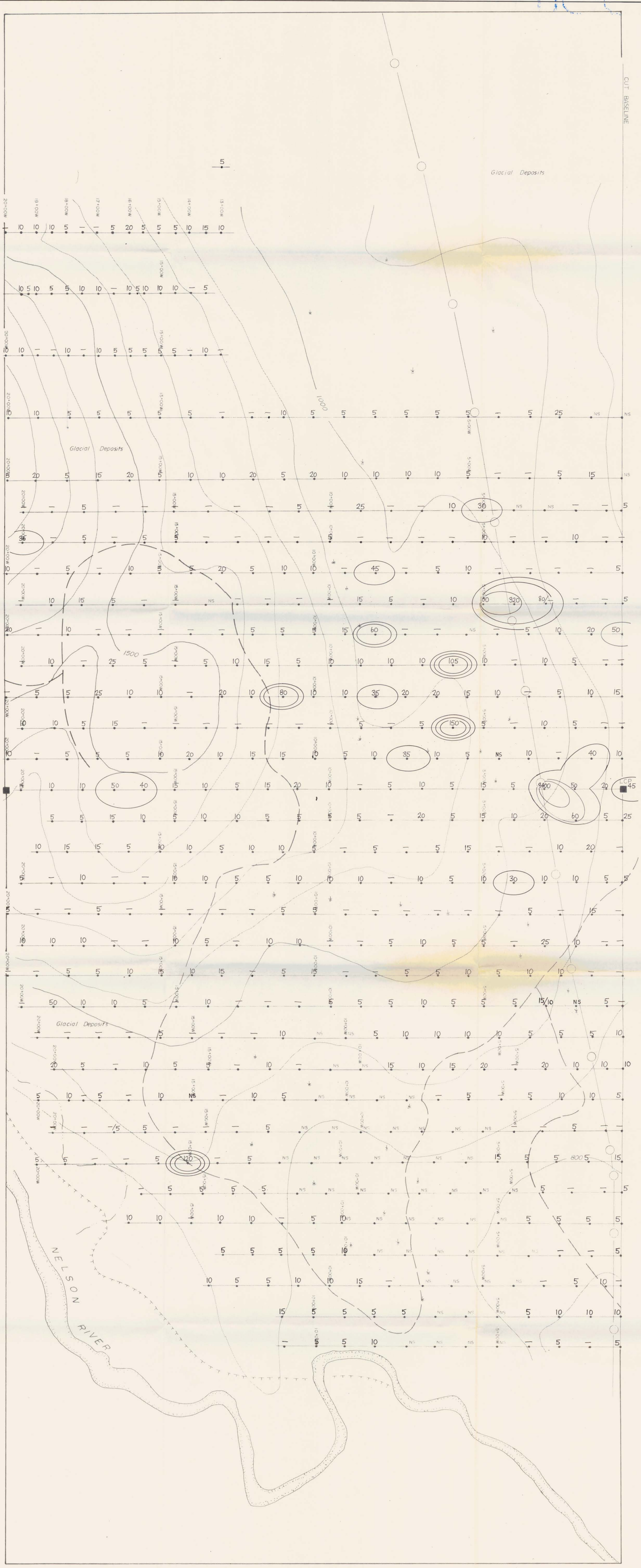
4. The analyses were supervised or determined by Mr. Conway Chun or Mr. David Chiu and his laboratory staff.

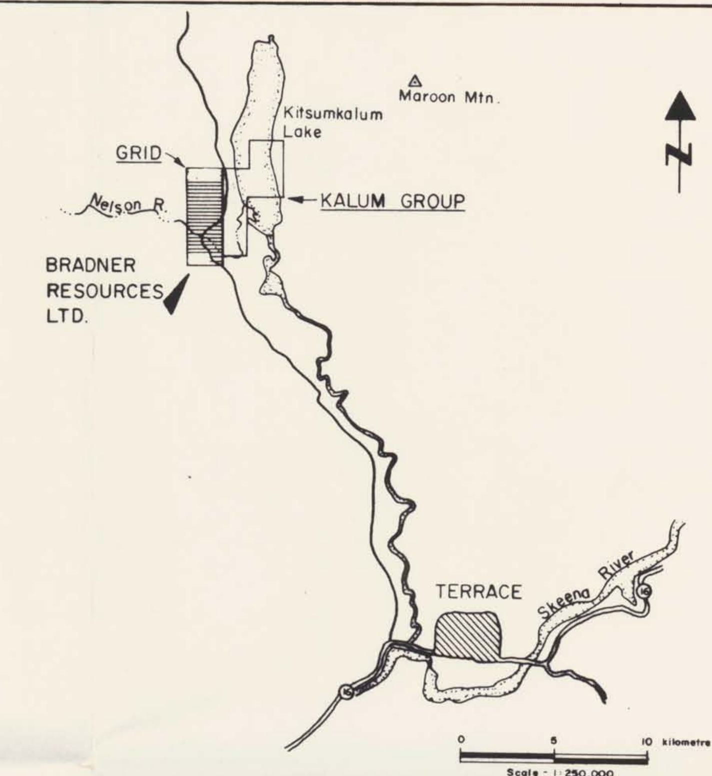
David Chiu
VANGEOCHEM LAB LTD.

DC:jl



BAV 7
BAV 2
Z
ROAD
±10m.
THICK GLACIAL TILL/CLAY
TRENCH ±20m.
UNABLE TO REACH BEDROCK
#2 VEIN.
PROJECTED
STRIKE
ACCESS ROAD
±1m DEPTH
TRENCH ±10m.
UNABLE TO REACH BEDROCK.
± 7m. - UNABLE TO REACH
BEDROCK
#1 VEIN
PROJECTED
STRIKE
ABANDONED
SHAFTS
DUMP
0
100
200
feet
0
25
50
metres
KALUM LAKE
OREQUEST CONSULTANTS LTD.
KALUM. GROUP.
TRENCH PLAN.
BRADNER RESOURCES LTD
DJH.
1




LOCATION MAP
BRADNER RESOURCES LTD.

## LEGEND

- Very Anomalous ≥ 95 ppb
- Anomalous ≥ 52 ppb
- Threshold ≥ 29 ppb
- Claim post & Claim outline
- Gravel Road
- B.C. Hydro & Transmission line
- Slope
- Stream
- Swamp
- Grid line & Soil sample location
- NS No sample taken

0 100 200 400 metres
Scale - 1: 5,000

GEOLOGICAL BRANCH
ASSESSMENT REPORT

13,303

**OREQUEST CONSULTANTS LTD.**

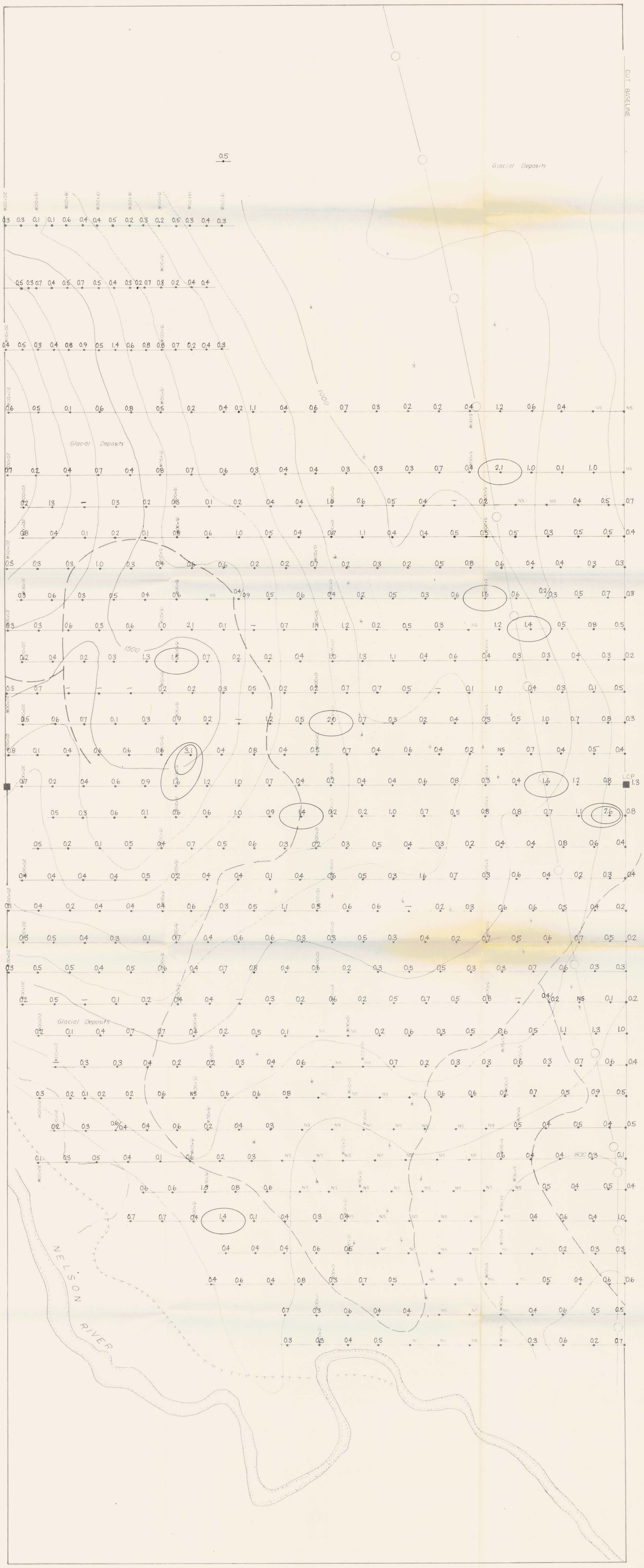
SOIL GEOCHEMISTRY

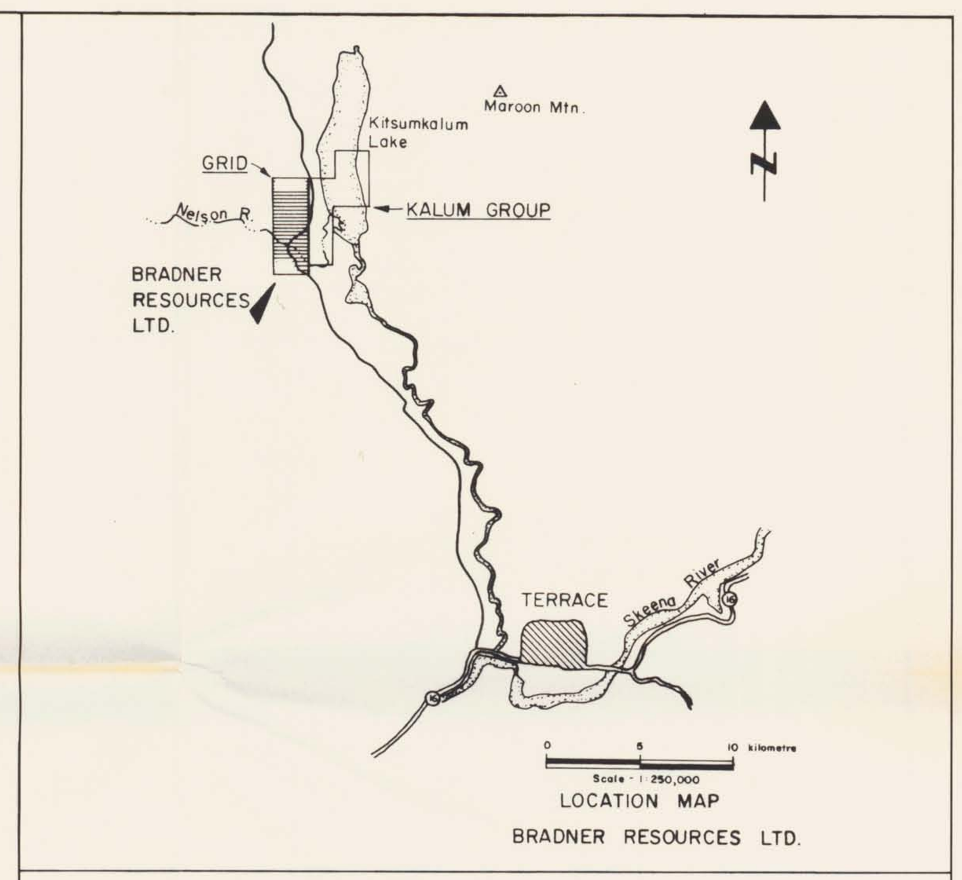
Au (ppb)

Skeena Mining Division, NTS 103I/10 and 15W

BRADNER RESOURCES LTD.

| DATE: NOV/1984 | SCALE: 1:5,000 | FIGURE NO. 4 |
|---|---|---|
| DRAWN BY: PY | | |




## LEGEND

- Very Anomalous ≥ 4.6 ppm
- Anomalous ≥ 2.5 ppm
- Threshold ≥ 1.4 ppm

- Claim post & Claim outline
- Gravel Road
- B.C. Hydro & Transmission line
- Slope
- Stream
- Swamp
- Grid line & Soil sample location
- NS No sample taken

Scale - 1:5,000



OreQuest Consultants Ltd.

SOIL GEOCHEMISTRY

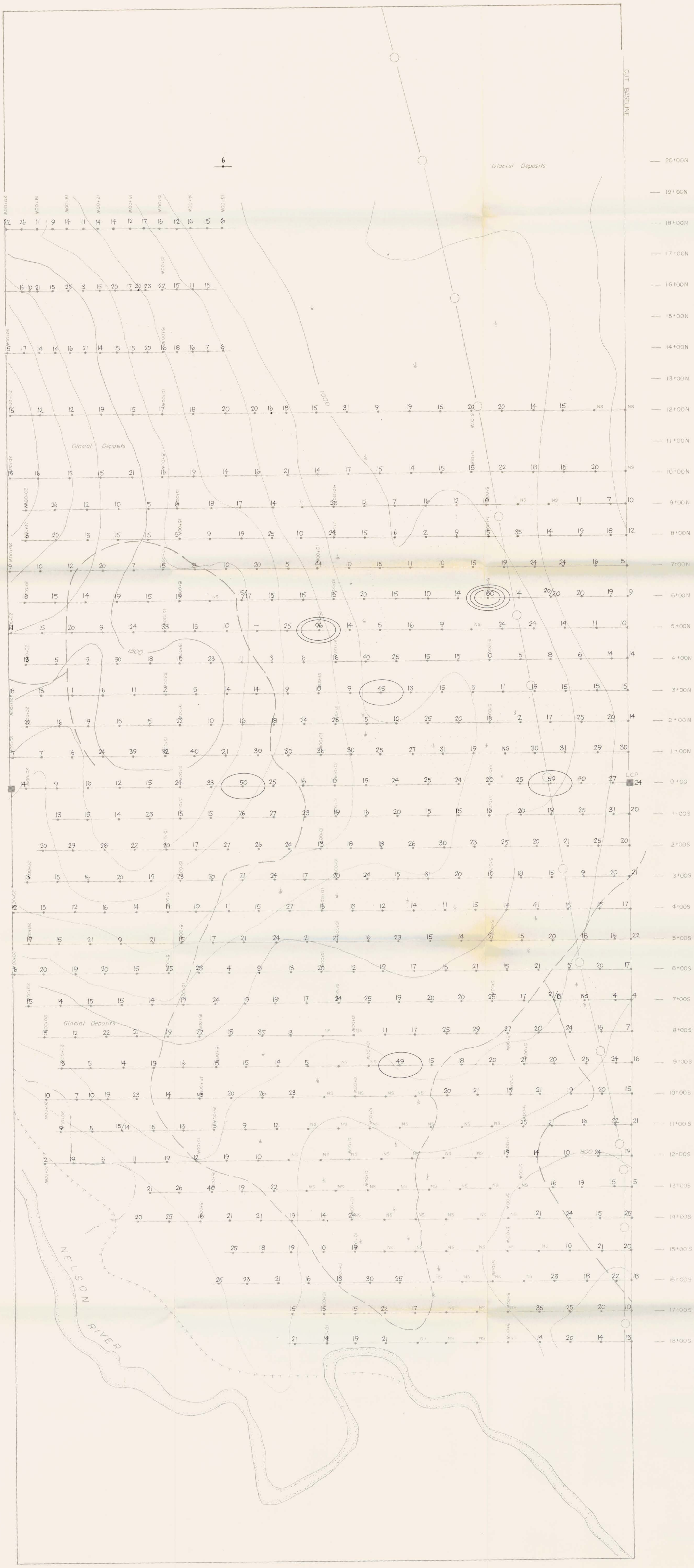
Ag (ppm)

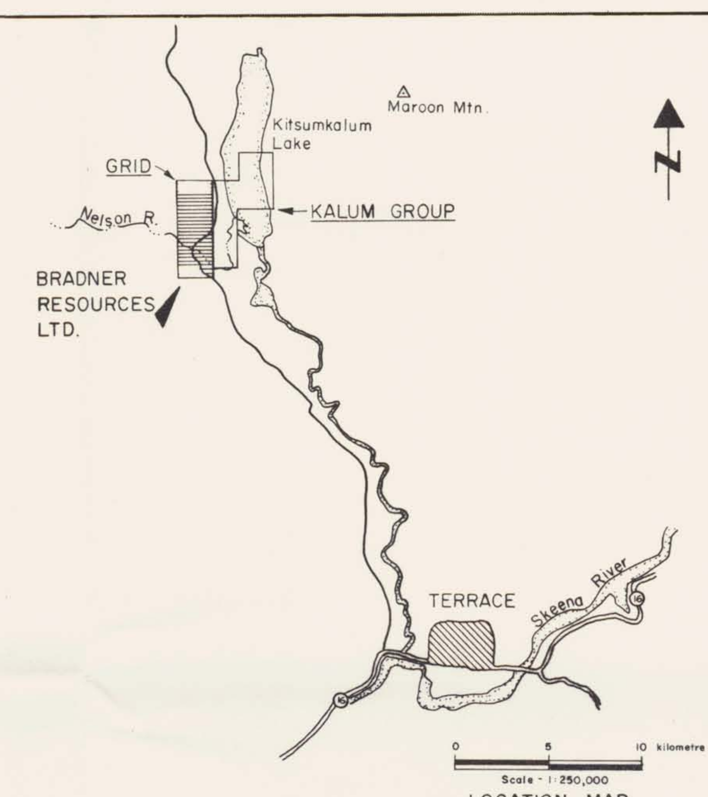
Skeena Mining Division , NTS 103I/10 and 15W

BRADNER RESOURCES LTD.

| DATE | SCALE | FIGURE NO. |
|---|---|---|
| NOV/1984 | 1:5,000 | 5 |
| DRAWN BY: P.Y. | | |

CUT BASELINE
Glacial Deposits
NELSON RIVER
20+00N
19+00N
18+00N
17+00N
16+00N
15+00N
14+00N
13+00N
12+00N
11+00N
10+00N
9+00N
8+00N
7+00N
6+00N
5+00N
4+00N
3+00N
2+00N
1+00N
0+00
1+00S
2+00S
3+00S
4+00S
5+00S
6+00S
7+00S
8+00S
9+00S
10+00S
11+00S
12+00S
13+00S
14+00S
15+00S
16+00S
17+00S
18+00S
LCP
NS
Maroon Mtn.
Kitsumkalum Lake
GRID
KALUM GROUP
Nelson R.
BRADNER RESOURCES LTD.
TERRACE
Skeena River
Scale - 1:250,000
LOCATION MAP
BRADNER RESOURCES LTD.
LEGEND
Very Anomalous ≥ 121 ppm
Anomalous ≥ 53 ppm
Threshold ≥ 23 ppm
Claim post & Claim outline
Gravel Road
B.C. Hydro & Transmission line
Slope
Stream
Swamp
Grid line & Soil sample location
NS No sample taken
GEOLOGICAL BRANCH
ASSESSMENT REPORT
13,303
0 100 200 400 metre
Scale - 1:5,000
OREQUEST CONSULTANTS LTD.
SOIL GEOCHEMISTRY
As(ppm)
Skeena Mining Division, NTS 103I/10 and 15W
BRADNER RESOURCES LTD.
DATE NOV/1984
DRAWN BY PY
SCALE 1:5,000
FIGURE NO. 6




LOCATION MAP

BRADNER RESOURCES LTD.

## LEGEND

- Very Anomalous ≥ 114 ppm
- Anomalous ≥ 70 ppm
- Threshold ≥ 43 ppm

- Claim post & Claim outline
- Gravel Road
- B.C. Hydro & Transmission line
- Slope
- Stream
- Swamp
- Grid line & Soil sample location
- NS No sample taken



Scale - 1:5,000

OREQUEST CONSULTANTS LTD.

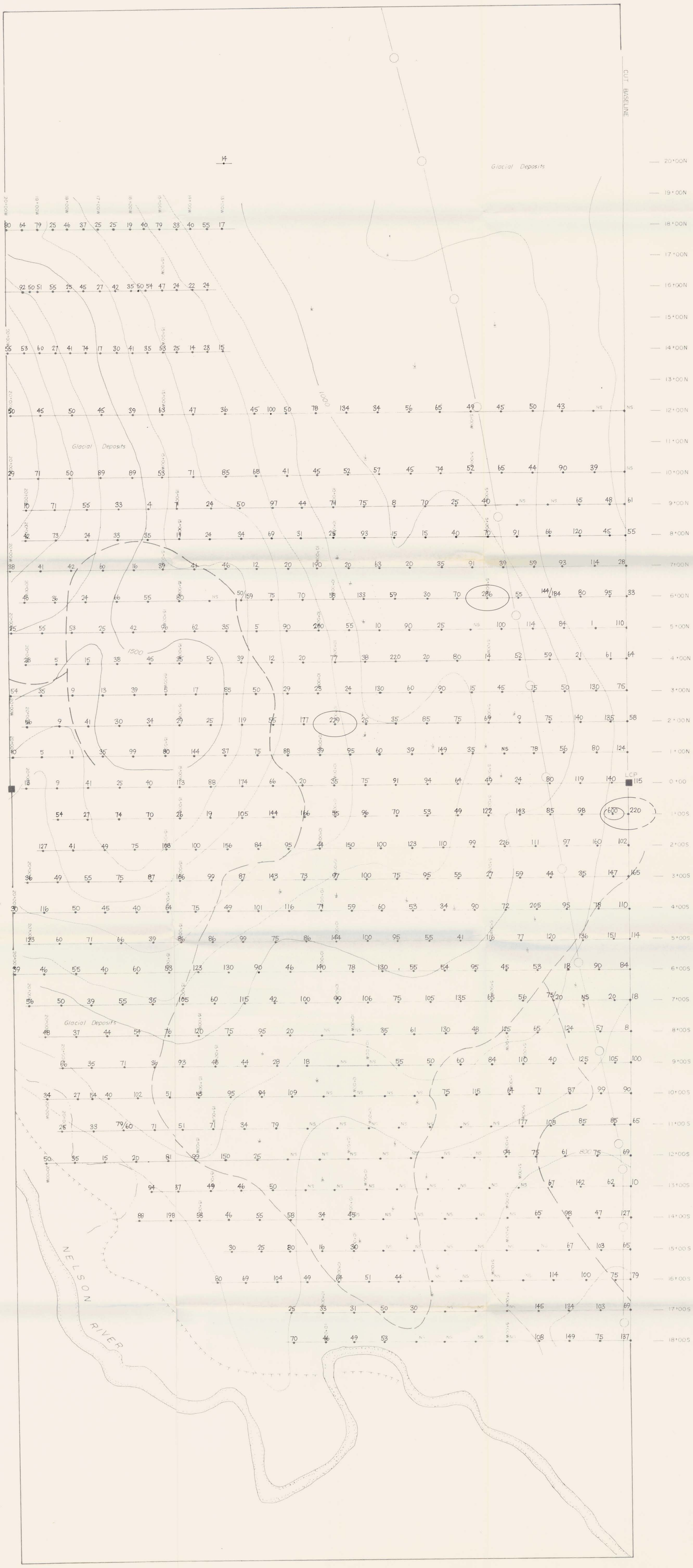
SOIL GEOCHEMISTRY

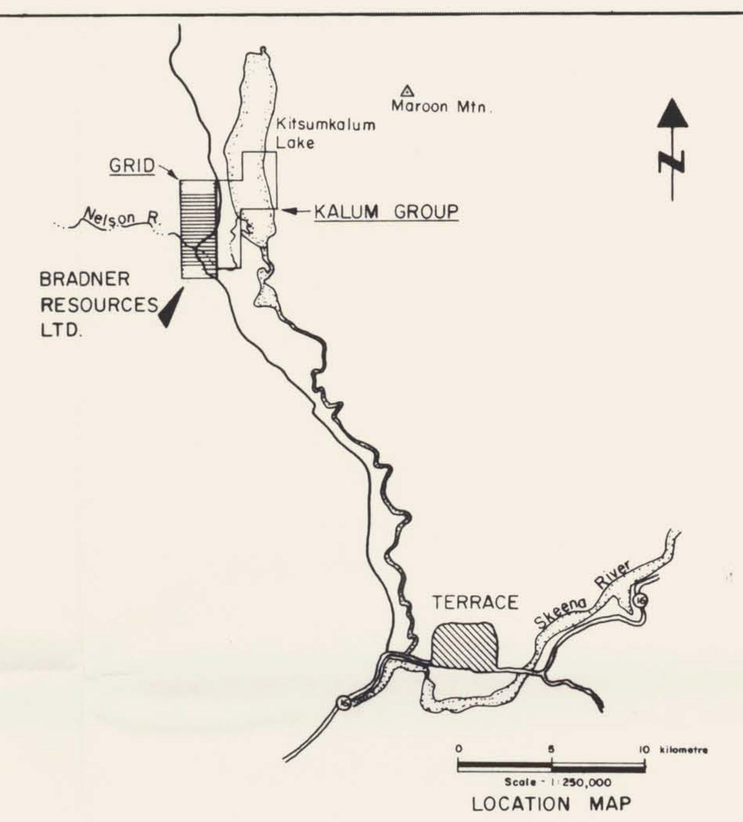
Pb (ppm)

Skeena Mining Division, NTS 103I/10 and 15W

BRADNER RESOURCES LTD.

| | | | |
|---|---|---|---|
| DATE NOV/1984 | SCALE 1:5,000 | FIGURE NO. 7 | |
| DRAWN BY PY | | | |




LOCATION MAP

BRADNER RESOURCES LTD.

## LEGEND

○ Very Anomalous ≥ 909 ppm

○ Anomalous ≥ 449 ppm

○ Threshold ≥ 222 ppm

Claim post & Claim outline

Gravel Road

B.C. Hydro & Transmission line

Slope

Stream

Swamp

Grid line & Soil sample location

NS No sample taken



0 100 200 400 metres

Scale - 1:5,000

OreQuest Consultants Ltd.

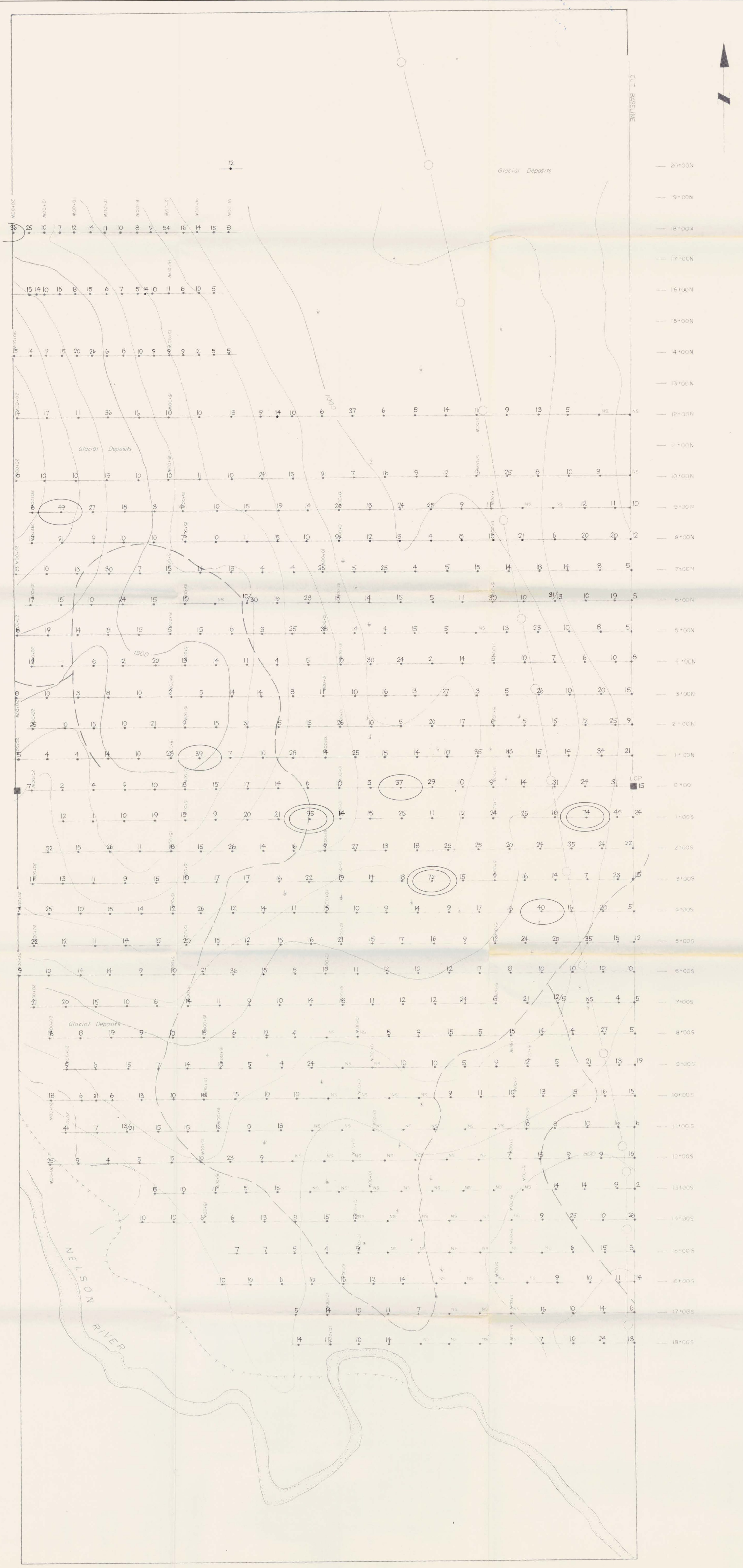
# SOIL GEOCHEMISTRY

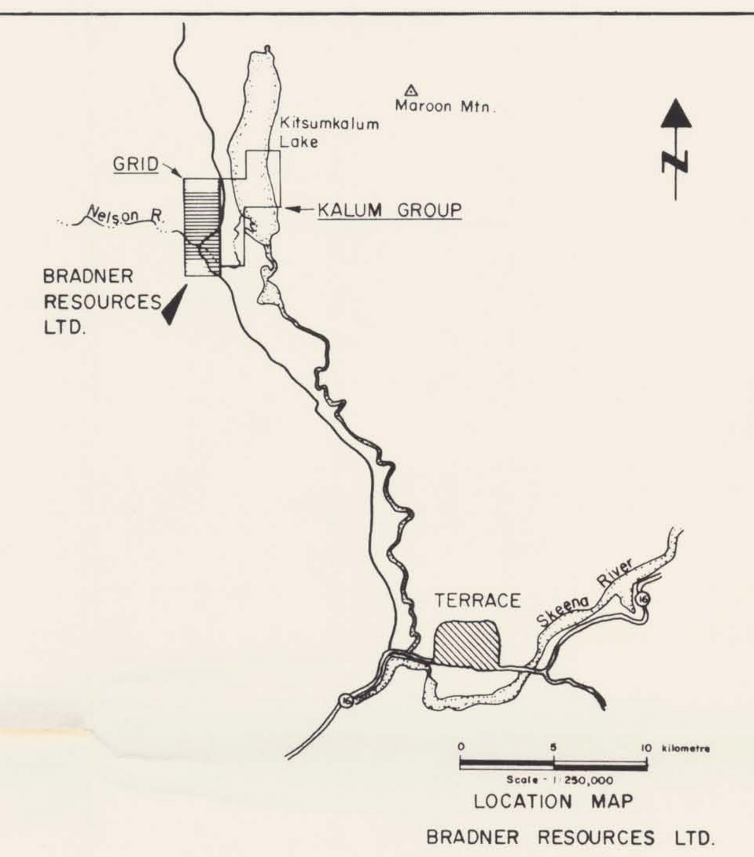
## Zn (ppm)

Skeena Mining Division, NTS 103I/10 and 15W

BRADNER RESOURCES LTD.

| DATE | SCALE | FIGURE NO. |
|---|---|---|
| NOV/1984 | 1:5,000 | 8 |
| DRAWN BY PY | | |




## LEGEND

- Very Anomalous ≥ 112 ppm
- Anomalous ≥ 64 ppm
- Threshold ≥ 36 ppm

- Claim post & Claim outline
- Gravel Road
- B.C. Hydro & Transmission line
- Slope
- Stream
- Swamp
- Grid line & Soil sample location
- NS No sample taken



0 100 200 400 metres
Scale - 1:5,000

**OREQUEST CONSULTANTS LTD.**

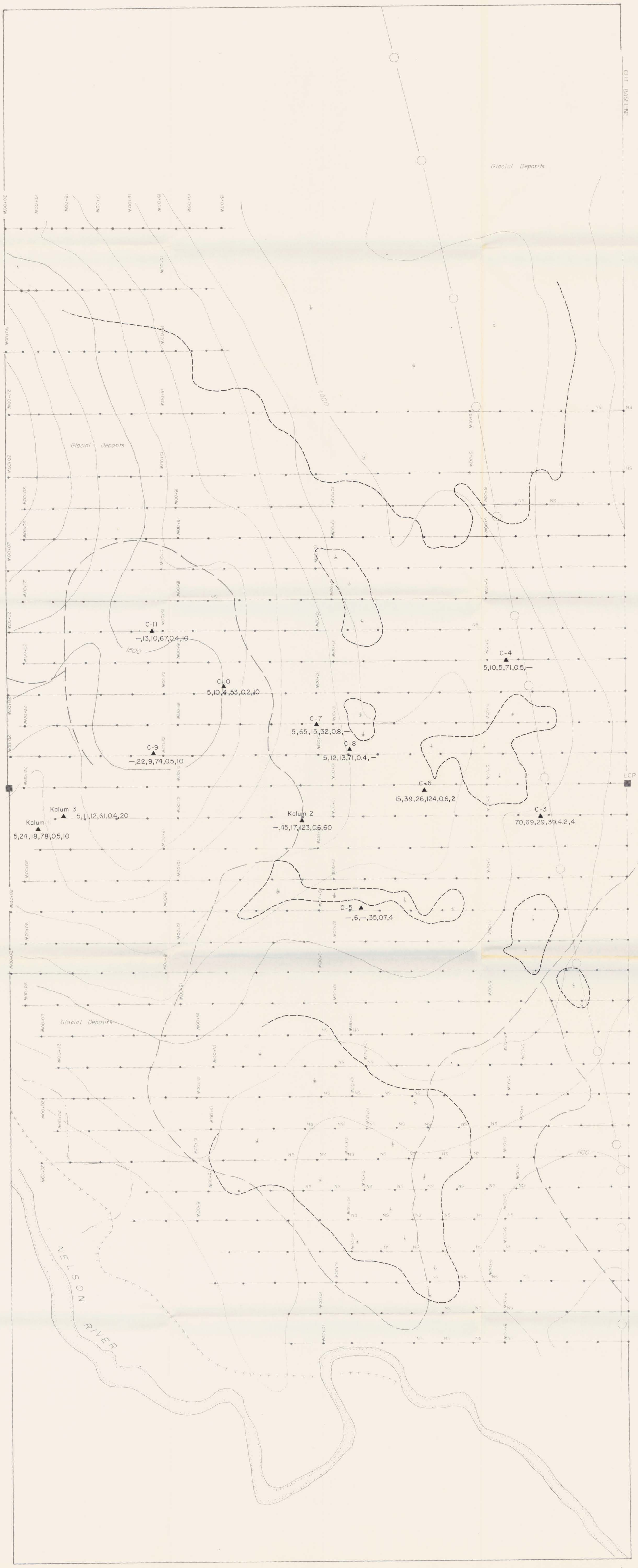
# SOIL GEOCHEMISTRY

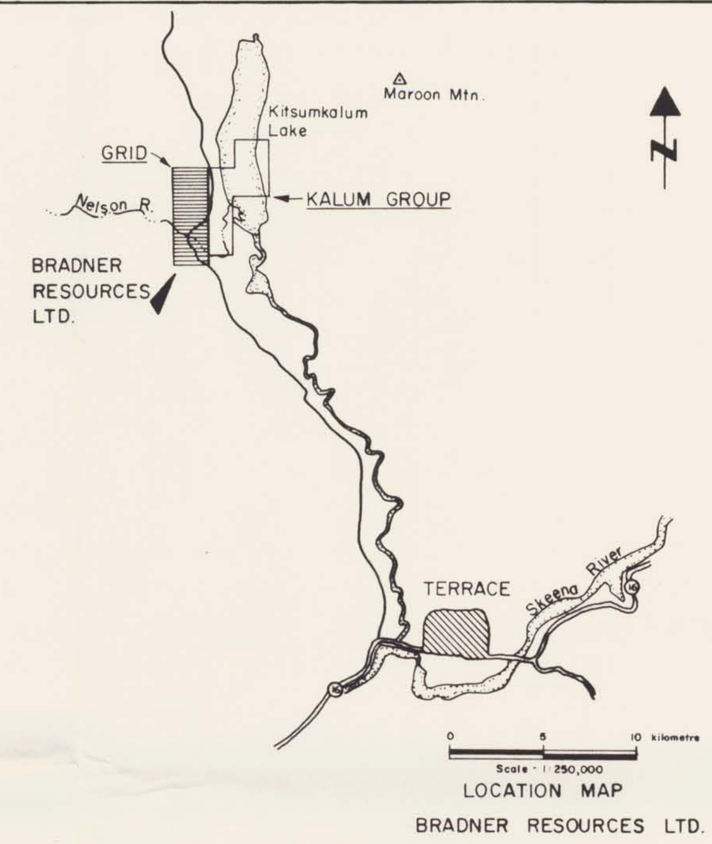
## Cu (ppm)

Skeena Mining Division, NTS 103I/10 and 15W

BRADNER RESOURCES LTD.

| | | |
|---|---|---|
| DATE NOV/1984 | SCALE 1:5,000 | FIGURE NO. 9 |
| DRAWN BY P.Y. | | |




## LEGEND

- Claim post & Claim outline
- Gravel Road
- B.C. Hydro & Transmission line
- Slope
- Stream
- Swamp
- Grid line & Soil sample location
- NS No sample taken
- ▲ Rock sample Au (ppb), Cu, Pb, Zn, Ag, As (ppm)

0 100 200 400 m

Scale - 1:5,000



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# ROCK SAMPLE LOCATION

Skeena Mining Division, NTS 103I/10 and 15W

BRADNER RESOURCES LTD.

| DATE | SCALE | FIGURE NO. |
|---|---|---|
| NOV/1984 | 1:5,000 | 10 |
| DRAWN BY: PY | | |