85-756-13555

GEOCHEMICAL REPORT

on the

WELL GROUP MINERAL CLAIMS

CRANBROOK AREA

FORT STEELE MINING DIVISION

BRITISH COLUMBIA

PROPERTY	WELL 3 and WELL 4 N.T.S. 82F/9E 49°33'N 116°07'W
OWNER	GEOTECH RESOURCES INC. /TUNSTALL RESOURCES INC. 319-470 GRANVILLE ST. VANCOUVER, B.C. V6C 1V5
OPERATOR	GEOTECH RESOURCES INC., 319-470 GRANVILLE STREET, VANCOUVER, B.C. V6C 1V5
AUTHOR	G.S. ARCHER, 319-470 GRANVILLE STREET VANCOUVER, B.C.
DATE	DECEM

13555
PART
2 of 2

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AUTHOR	G.S. ARCHER, 319-470 GRANVILLE STREET, VANCOUVER, B.C.
DATE	DECEMBER 12, 1984

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MAPS

APPENDIX

INTRODUCION

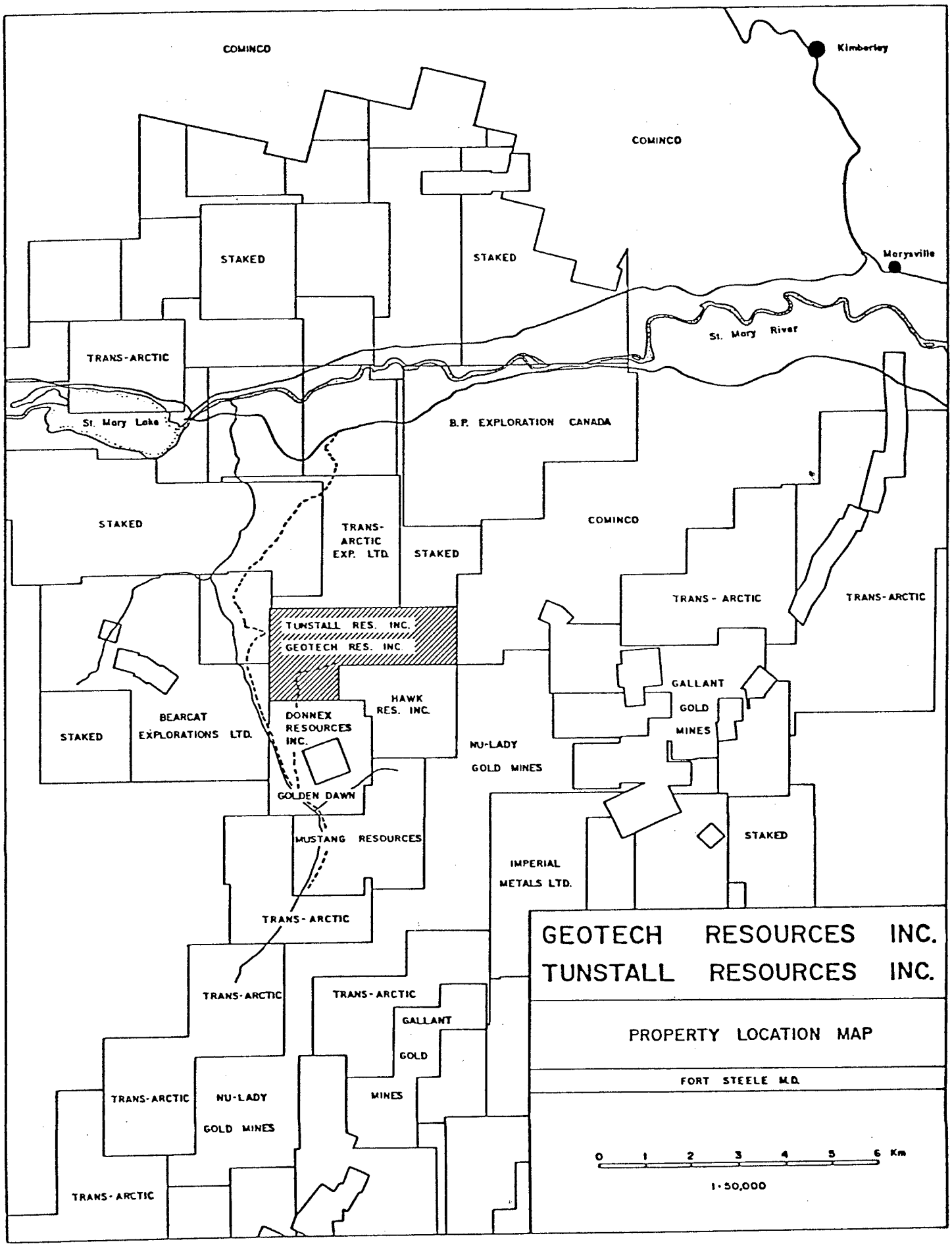
This report was written at the request of Geotech Resources Inc. and Tunstall Resources Inc. The report is based on geochemical data and observation made during the sampling process.

The Well mineral claim group is located 30 km. west of Cranbrook within one kilometer east of Angus Creek. Perry Creek is 4 km. to the east (see property location map). The property can be accessed from Cranbrook, north along Highway 95-A for 20 km. and west for 15 km. A main logging road is then followed south up the east side of Angus Creek where the Well group is located.

The property consists of two claims of 16 units each. The property was purchased from Trans-Arctic Ltd. with 50% interest in the claims held by Tunstall Resources Inc. Previous work has been filed on the property in July, 1984.

The geochemical survey that was carried out was designed to delineate any new anomalous zones and confirm the anomalous areas indicated by a recent VLF-EM survey. The gold and silver data correlated well with the VLF-EM survey. A total of 316 samples were collected with the sample lines spaced 100 metres apart and sample stations 40 metres apart, closing to 20 metres over the fault zone. The sample stations were the same locations as the VLF-EM stations. All samples were taken from the 'B' horizon.

Contoured sample location maps are located in the back pocket.


COMINCO
Kimberley
COMINCO
STAKED
STAKED
Marysville
St. Mary River
TRANS-ARCTIC
St. Mary Lake
B.P. EXPLORATION CANADA
STAKED
TRANS-ARCTIC EXP. LTD.
STAKED
COMINCO
TRANS-ARCTIC
TRANS-ARCTIC
TUNSTALL RES. INC.
GEOTECH RES. INC.
GALLANT GOLD MINES
HAWK RES. INC.
STAKED
BEARCAT EXPLORATIONS LTD.
DONNEX RESOURCES INC.
NU-LADY GOLD MINES
GOLDEN DAWN
MUSTANG RESOURCES
STAKED
IMPERIAL METALS LTD.
TRANS-ARCTIC
TRANS-ARCTIC
TRANS-ARCTIC
GALLANT GOLD MINES
TRANS-ARCTIC
NU-LADY GOLD MINES
TRANS-ARCTIC
GEOTECH RESOURCES INC.
TUNSTALL RESOURCES INC.
PROPERTY LOCATION MAP
FORT STEELE M.D.
0 1 2 3 4 5 6 Km
1:50,000

GEOLOGY

The general geologic setting of the property consists of three formations. The basal Aldridge Formation, the oldest formation occuring in the region as well as the property consists primarily of weathered argillite and argillaceous quartzite. The Creston Formation, which is transitional from the Aldridge Formation consists of argillaceous quartzites and argillites. This formation is host to gold quartz veins on Perry Creek situated to the east. The Moyie Intrusions, which are interbedded with the Aldridge Formation, consists of meta-diorite and meta-quartz diorite.

The following is quoted from L. Sookochoff's June 5, 1984 report on the Well claim group.

"The general structure of the area is of a broad, northerly striking anticline exposing the core of the Proterozoic rocks with younger rocks to the west and east. The regional St. Mary's Fault trends east northeast through the property area and creates a fault contact with the Aldridge and Creston Formations.

Faults extending from the south generally terminate or trend into the St. Mary's fault and commonly indicate contacts between the Creston and Kitchener Formations.

The property predominantly covers the basal Aldridge Formation in a northeasterly trending contact with the Creston Formation to the southeast. The two Formations are partly in fault contact by the east northeasterly trending St. Mary's fault."

Locally, the property has few outcrops although the St. Mary's fault zone is easily located due to the distinctive gossans over the fault area. Several deep trenches were also observed over the fault zone. The western end of the fault appeared to be very siliceous with diseminated pyrite throughout the outcrop. The outcrop on the eastern end of the fault zone was bleached with a boxwork pattern left after the iron sulphides had been removed by oxidation. The fault itself strikes 270^{o}(M), and dips steeply. The general position of the fault zone is marked on the contoured sample location maps located in the back pocket.

SAMPLING AND LABORATORY METHODOLOGY

A total of 316 samples were taken with sample lines spaced 100 metres apart. Sample stations were usually 40 metres apart, closing to 20 metres over the fault zone. The sample locations were the same locations as the VLF-EM stations. All samples were taken from the 'B' soil horizon which was usually found less than 6 cm. below the surface. The sample stations were originally located during the VLF-EM survey using compass and 'hip chain'. All soil samples were placed in Kraft paper bags, using the same numbering system as the VLF-EM stations.

The samples were analyzed by Acme Analytical Laboratories Ltd., Vancouver, B.C. The samples were tested for 30 elements using Inductively Coupled Argon Plasma (ICP). The rock samples were pulverized to -100 mesh and dried. A 0.5 gram sample was digested in hot diluted aqua regia (3 ml) in boiling water bath (90°C) and diluted to 10 ml with demineralized water. Gold was determined from Atomic Absorption (10 gram sample).

CONCLUSIONS

The results for gold and silver tended to correlate positively with each other as well as with the VLF-EM survey that had been completed prior to the soil sampling. It appears that additional soil sampling and possibly some trenching is warranted over the anomalous areas delineated by the geochemical survey.

ITEMIZED COST STATEMENT

A) Wages - Sept. 13-17, 1984		
Geologist	@115/day	$ 575.00
Assistant	@100/day	$ 500.00
B) Transportion		
Truck		$ 254.17
Air fair		$ 357.93
C) Food and Accomadation		$ 485.03
D) Misc.		$ 130.20
E) Geochemical Analysis (see Appendix B)		$3351.74

		$5654.07

GORDON S. ARCHER - QUALIFICATIONS

1) I am a graduate of the University of Victoria with a Bachelor of Science Degree (1980 - Physical Geography).

2) I have subsequently completed the Geology Program at the University of British Columbia.

3) Geology Work Experience :
   - Assistant Geologist with the B.C. Ministry of Energy, Mines and Petroleum Resources, Project Geology Dept. 1980-1981.

   - Intermediate Field Geologist with Petro Canada (Coal Division) - 1982.

   - Self-employed - worked for several Vancouver based resource companies and with various geological engineers throughout the season - 1983.

   - Currently employed by Geotech Resources Inc. as a Geologist and Computer Programmer.

4) I am currently a shareholder of Geotech Resources Inc.

Gordon Archer

APPENDIX A

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-3 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS AND ROCKS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: SEPT 20 1984 DATE REPORT MAILED: Sept 25/84 ASSAYER. D. Toye ...DEAN TOYE. CERTIFIED B.C. ASSAYER

GEOTECH RES (PROJECT # WELL GROUP-84) FILE # 84-2711 PAGE 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
7W 2+00N	1	12	12	42	.3	16	7	273	1.74	2	5	ND	4	18	1	3	2	23	.19	.11	10	15	.40	91	.07	4	1.63	.01	.08	2	5
7W 1+60N	2	13	11	39	.1	26	10	137	1.96	4	5	ND	3	13	1	2	3	24	.10	.07	10	14	.35	107	.08	4	2.09	.01	.06	2	5
7W 1+20N	1	16	7	25	.1	15	7	131	1.86	2	5	ND	5	9	1	3	3	26	.11	.05	13	20	.49	48	.05	3	.92	.01	.05	2	5
7W 0+80N	1	17	8	24	.2	15	8	149	1.93	2	9	ND	5	10	1	2	2	28	.14	.06	12	26	.57	41	.05	2	.93	.01	.09	2	5
7W 0+40N	1	18	16	36	.2	16	7	265	1.89	4	6	ND	3	14	1	2	3	27	.13	.09	11	17	.45	85	.07	5	1.31	.01	.08	2	5
7W 0+00N	1	11	9	19	.2	11	3	104	1.09	2	5	ND	2	12	1	2	2	20	.18	.01	9	15	.33	34	.05	6	.65	.01	.06	2	5
7W 0+40S	1	22	10	35	.1	14	6	137	1.73	5	5	ND	5	14	1	2	2	26	.11	.07	12	12	.40	81	.09	6	1.83	.02	.09	2	5
7W 0+60S	1	26	16	36	.1	26	7	167	2.08	4	5	ND	5	15	1	2	2	30	.15	.06	11	17	.48	128	.11	5	2.44	.02	.14	2	5
7W 0+80S	1	15	14	29	.1	13	7	172	1.63	4	6	ND	4	14	1	2	2	24	.17	.06	15	15	.51	56	.06	2	1.03	.01	.13	2	5
7W 1+00S	1	17	13	51	.2	19	7	130	1.69	2	5	ND	5	15	1	2	2	22	.11	.07	11	11	.34	101	.08	4	1.84	.01	.07	2	5
7W 1+20S	1	11	14	50	.2	13	6	220	1.60	2	5	ND	4	14	1	2	2	23	.10	.09	9	11	.25	89	.07	2	1.45	.01	.06	2	65
7W 1+60S	1	12	18	40	.2	13	6	181	1.47	5	5	ND	5	10	1	4	2	18	.08	.03	12	11	.41	57	.05	3	1.02	.01	.07	2	5
7W 2+00S	1	20	32	65	.3	18	7	190	1.60	3	5	ND	6	12	1	2	2	22	.08	.09	11	10	.27	103	.09	4	2.20	.02	.09	2	5
7W 2+40S	1	10	19	60	.3	12	5	235	1.39	4	5	ND	5	13	1	4	2	21	.09	.06	11	10	.31	72	.07	3	1.06	.01	.06	2	5
7W 2+80S	1	17	15	92	.2	20	7	342	1.85	4	5	ND	5	17	1	2	2	24	.13	.12	9	12	.39	98	.11	2	2.25	.02	.09	2	5
7W 3+20S	1	24	15	69	.1	19	10	618	1.73	9	5	ND	4	20	1	2	2	23	.12	.16	9	9	.23	143	.11	3	2.29	.02	.05	2	5
7W 3+40S	1	16	11	58	.3	18	7	296	1.60	3	5	ND	5	16	1	2	2	24	.13	.12	10	11	.31	90	.09	4	1.95	.02	.07	2	5
7W 3+80S	1	15	10	54	.2	14	7	140	1.80	4	5	ND	5	16	1	2	2	26	.09	.08	10	12	.35	88	.09	2	1.78	.01	.06	2	5
7W 4+20S	1	14	10	52	.1	14	6	370	1.76	4	5	ND	4	12	1	2	2	26	.10	.12	9	11	.38	87	.10	3	1.97	.01	.06	2	5
7W 4+60S	1	19	13	50	.3	14	6	392	2.13	2	6	ND	5	14	1	2	3	34	.15	.08	10	14	.52	85	.09	4	1.69	.01	.07	2	5
7W 4+80S	1	17	10	36	.2	11	5	294	1.67	5	5	ND	5	13	1	2	2	27	.13	.09	12	12	.38	66	.07	6	1.27	.01	.07	2	5
6W 2+00N	1	12	14	52	.1	24	10	598	2.23	2	5	ND	4	17	1	2	3	29	.14	.08	9	17	.34	91	.10	3	2.02	.02	.06	2	5
6W 1+60N	1	13	13	57	.1	36	13	514	2.27	3	5	ND	4	17	1	2	2	30	.13	.07	8	13	.25	126	.14	5	2.05	.02	.06	2	5
6W 1+20N	2	14	13	47	.1	44	11	573	2.11	4	5	ND	3	14	1	2	3	28	.12	.06	8	21	.36	112	.12	3	2.40	.02	.06	2	5
6W 0+80N	1	10	11	41	.1	35	10	346	1.96	4	5	ND	3	12	1	2	2	28	.13	.04	7	21	.32	78	.10	2	1.82	.02	.05	2	5
6W 0+40N	1	11	13	35	.1	22	9	363	1.75	2	5	ND	4	16	1	2	2	28	.15	.04	11	24	.53	94	.08	3	1.40	.01	.07	2	5
6W 0+00N	2	81	21	40	.1	95	20	285	3.30	4	12	ND	11	17	1	2	2	45	.24	.02	130	82	1.01	83	.08	3	2.58	.01	.11	2	5
6W 0+40S	1	8	10	28	.2	14	4	122	1.40	2	5	ND	5	13	1	2	2	23	.11	.04	14	12	.40	63	.07	2	1.14	.01	.07	2	5
6W 0+60S	1	11	13	31	.2	23	8	164	1.68	2	5	ND	4	14	1	2	2	27	.18	.05	11	17	.37	60	.09	3	1.66	.01	.09	2	5
6W 0+80S	1	11	11	27	.2	21	7	143	1.76	3	5	ND	4	12	1	2	2	30	.17	.04	9	16	.39	59	.08	3	1.61	.02	.09	2	35
6W 1+00S	1	11	13	28	.2	15	7	150	1.74	2	5	ND	4	11	1	3	2	30	.16	.01	10	18	.63	43	.08	3	1.18	.02	.10	2	75
6W 1+20S	1	13	27	38	.3	14	6	238	1.69	2	5	ND	4	11	1	3	2	32	.15	.06	11	18	.49	70	.08	3	1.21	.01	.08	2	5
6W 1+60S	1	12	11	28	.3	10	4	183	1.40	3	5	ND	5	15	1	3	2	26	.13	.05	13	12	.51	66	.07	4	1.00	.01	.10	2	5
6W 2+00S	1	13	11	41	.3	13	6	258	1.59	6	5	ND	4	11	1	2	2	30	.12	.13	9	14	.37	89	.08	4	1.29	.01	.07	2	5
6W 2+40S	1	18	11	59	.2	15	7	231	1.72	2	5	ND	5	12	1	2	2	33	.13	.07	11	18	.44	76	.09	3	1.45	.01	.06	2	5
6W 2+80S	1	17	11	35	.2	12	5	160	1.45	3	5	ND	5	15	1	5	2	28	.14	.02	14	17	.48	48	.07	2	1.01	.01	.08	2	5
6W 3+20S	1	11	16	47	.2	13	6	255	1.52	4	5	ND	4	13	1	2	2	25	.11	.07	11	14	.32	114	.08	2	1.36	.01	.07	2	5
STD C/AU-0.5	19	58	39	124	7.0	70	27	1083	3.82	40	17	7	35	49	16	15	19	59	.44	.14	36	58	.88	181	.07	38	1.64	.06	.13	14	500

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
6W 3+60S	1	13	15	37	.1	9	4	159	1.26	5	5	ND	4	11	1	2	2	18	.08	.05	12	10	.33	58	.05	3	1.09	.01	.06	2	5
6W 4+00S	1	9	11	37	.2	9	4	180	1.41	3	5	ND	3	11	1	2	2	21	.08	.13	11	9	.27	87	.06	2	1.36	.01	.05	2	5
6W 4+40S	1	16	10	37	.1	10	5	212	1.44	3	5	ND	4	13	1	2	2	23	.12	.06	13	13	.40	65	.05	3	1.02	.01	.07	2	5
6W 4+80S	1	11	10	32	.1	8	4	148	1.54	2	5	ND	2	12	1	3	2	25	.08	.10	11	12	.27	74	.06	3	1.05	.01	.05	2	5
5W 2+00N	1	21	18	79	.1	31	19	1058	2.90	6	5	ND	6	11	1	2	3	22	.12	.05	12	16	.44	96	.07	4	1.49	.01	.08	2	5
5W 1+60N	1	19	14	77	.1	38	20	646	2.84	8	5	ND	6	15	1	2	2	26	.12	.06	11	15	.43	129	.10	3	2.37	.02	.07	2	5
5W 1+20N	1	18	15	82	.1	66	30	810	2.83	5	5	ND	5	11	1	2	3	29	.09	.04	16	16	.36	96	.09	3	2.13	.01	.06	2	5
5W 0+80N	1	21	9	41	.1	24	10	160	2.46	8	5	ND	7	13	1	2	3	25	.07	.06	11	13	.37	108	.11	2	2.82	.02	.04	2	5
5W 0+40N	1	66	8	37	.1	26	16	253	3.53	8	5	ND	5	10	1	2	3	38	.10	.03	14	31	.91	48	.07	5	1.83	.01	.04	2	5
5W 0+00N	1	15	9	42	.1	21	12	366	2.13	4	5	ND	4	15	1	2	4	27	.11	.12	8	12	.26	98	.13	2	2.68	.02	.05	2	5
5W 0+40S	1	9	14	29	.1	17	10	130	1.56	2	5	ND	3	8	1	2	4	21	.09	.05	10	11	.43	54	.07	2	1.52	.01	.06	2	5
5W 0+60S	1	9	12	32	.1	38	43	151	2.98	2	5	ND	4	16	1	2	4	40	.26	.04	11	25	.45	54	.10	2	2.34	.02	.05	2	5
5W 0+80S	1	10	13	26	.1	20	17	139	2.12	6	5	ND	3	6	1	2	4	30	.10	.02	12	24	.60	42	.06	2	1.60	.01	.07	2	5
5W 1+00S	1	7	16	28	.1	14	6	118	1.61	2	5	ND	3	8	1	2	3	24	.09	.03	11	12	.36	56	.07	2	1.40	.01	.06	2	355
5W 1+20S	1	6	14	27	.1	12	5	234	1.28	3	5	ND	3	12	1	2	2	18	.11	.08	11	11	.33	79	.05	2	1.00	.01	.07	2	5
5W 1+60S	1	9	9	27	.1	18	8	387	1.58	4	5	ND	3	12	1	2	3	22	.11	.08	8	11	.25	93	.08	2	1.75	.01	.06	2	5
5W 2+00S	1	9	8	24	.1	11	5	141	1.38	2	5	ND	4	8	1	2	2	19	.09	.03	13	11	.42	60	.05	2	.97	.01	.05	2	5
5W 2+40S	1	6	16	38	.1	11	5	235	1.39	3	5	ND	3	9	1	2	2	21	.09	.06	10	10	.32	93	.07	2	1.23	.01	.07	2	25
5W 2+80S	1	9	14	38	.2	12	5	229	1.51	4	5	ND	3	11	1	2	2	22	.10	.06	12	13	.51	63	.07	2	1.23	.01	.08	2	5
5W 3+20S	1	19	16	36	.2	13	6	177	1.88	4	5	ND	5	12	1	2	2	29	.10	.04	13	19	.60	67	.07	2	1.35	.01	.07	2	5
5W 3+60S	1	14	16	51	.2	14	6	142	1.72	5	5	ND	4	11	1	2	2	27	.11	.08	10	14	.38	63	.08	2	1.59	.02	.07	2	25
5W 4+00S	1	18	22	47	.2	12	5	200	1.83	2	5	ND	6	13	1	3	2	28	.11	.04	15	14	.80	102	.08	2	1.45	.01	.14	2	5
5W 4+40S	1	23	15	63	.3	16	7	268	1.94	4	5	ND	4	17	1	2	2	36	.18	.12	11	22	.54	95	.08	2	1.61	.02	.11	2	5
5W 4+80S	1	20	11	58	.3	16	6	170	1.81	2	5	ND	3	12	1	2	2	33	.15	.11	11	19	.48	85	.08	2	1.54	.01	.08	2	5
4W 2+00N	1	20	18	80	.2	40	14	251	2.73	8	5	ND	6	13	1	2	2	29	.09	.07	10	17	.41	104	.13	2	2.87	.02	.06	2	5
4W 1+60N	1	26	14	68	.2	33	14	276	2.71	9	5	ND	9	15	1	2	4	27	.15	.09	11	12	.37	105	.14	2	3.62	.02	.06	2	5
4W 1+20N	1	22	17	70	.1	29	13	1044	3.45	8	5	ND	6	12	1	2	2	32	.09	.10	12	16	.37	118	.11	2	2.68	.02	.06	2	5
4W 0+80N	1	22	20	54	.1	23	12	594	3.80	11	5	ND	6	11	1	2	2	33	.08	.09	13	19	.50	94	.08	2	2.01	.01	.05	2	5
4W 0+40N	1	21	14	62	.3	27	12	238	3.16	11	5	ND	7	17	1	2	2	30	.11	.06	12	15	.38	122	.11	3	2.69	.02	.06	2	5
4W 0+00N	1	17	12	55	.1	32	20	882	2.85	19	5	ND	6	14	1	2	2	26	.14	.10	13	16	.47	103	.08	2	2.11	.01	.09	2	5
4W 0+20S	1	10	12	39	.1	26	14	662	2.24	9	5	ND	2	13	1	2	4	27	.14	.12	12	15	.35	84	.06	2	1.26	.01	.07	2	5
4W 0+40S	1	7	10	33	.2	19	9	503	1.64	4	5	ND	3	12	1	2	3	18	.14	.31	9	10	.24	109	.06	2	1.23	.01	.06	2	5
4W 0+60S	1	7	11	29	.1	22	9	221	1.64	2	5	ND	3	9	1	2	3	19	.07	.10	11	13	.37	53	.05	2	1.18	.01	.04	2	5
4W 0+80S	1	6	13	26	.1	22	11	217	1.51	5	5	ND	3	7	1	2	2	20	.06	.03	10	9	.39	60	.05	2	1.20	.01	.05	2	5
4W 1+00S	1	8	10	30	.1	18	11	148	1.90	3	5	ND	3	9	1	2	2	22	.07	.04	12	11	.33	75	.06	2	1.61	.01	.05	2	5
4W 1+20S	1	6	20	32	.1	13	8	556	1.61	4	5	ND	3	11	1	2	2	24	.11	.03	10	12	.41	91	.07	2	1.34	.01	.06	2	5
4W 1+60S	1	10	18	35	.1	13	5	217	1.40	6	5	ND	5	11	1	3	2	19	.13	.04	13	11	.50	68	.05	2	1.04	.01	.07	2	85
STD C/AU 0.5	19	58	39	124	7.2	69	27	1109	3.82	40	17	7	35	49	15	14	18	58	.44	.13	37	57	.88	181	.07	40	1.64	.06	.13	12	495

GEOTECH RES PROJECT # WELL GROUP-84 FILE # 84-2711

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
4W 2+00S	1	9	18	37	.1	16	7	138	1.49	3	5	ND	3	8	1	2	4	22	.07	.05	10	19	.40	68	.06	2	1.30	.01	.05	2	5
4W 2+40S	2	14	17	57	.1	22	9	218	3.86	8	5	ND	7	8	1	2	4	43	.04	.12	14	27	.49	88	.10	3	2.56	.01	.06	2	5
4W 2+80S	1	8	23	33	.1	12	4	112	1.33	2	5	ND	5	6	1	2	2	18	.07	.03	14	13	.65	44	.07	4	1.27	.01	.07	2	5
4W 3+20S	1	6	20	32	.1	10	4	166	1.27	5	5	ND	2	8	1	2	2	20	.08	.15	11	10	.36	82	.07	2	1.08	.01	.07	2	5
4W 3+60S	1	11	29	36	.1	8	3	170	1.16	2	5	ND	5	13	1	3	4	18	.17	.04	15	10	.68	74	.07	2	.97	.01	.11	2	20
4W 4+00S	1	20	20	40	.2	22	6	199	1.41	2	5	ND	5	12	1	2	2	21	.13	.02	17	14	.61	67	.07	2	1.47	.01	.07	2	5
4W 4+40S	1	15	16	33	.1	10	3	198	1.23	3	5	ND	5	19	1	3	2	20	.22	.05	19	12	.69	71	.07	3	1.01	.01	.13	2	5
4W 4+80S	1	10	18	40	.2	10	4	181	1.33	3	5	ND	4	9	1	2	2	21	.10	.08	12	11	.45	72	.07	3	1.26	.01	.07	2	5
3W 0+00S	1	10	22	44	.1	16	5	331	1.39	7	5	ND	3	10	1	2	2	20	.09	.04	11	14	.43	112	.07	3	1.55	.01	.05	2	5
3W 0+20S	2	14	13	31	.2	26	10	167	4.68	10	6	ND	9	20	1	2	2	74	.05	.10	14	50	.98	68	.06	2	1.93	.01	.08	2	5
3W 0+40S	1	9	10	34	.3	27	14	237	4.14	9	5	ND	4	17	1	2	2	71	.13	.07	10	39	.71	53	.08	3	1.86	.01	.04	2	5
3W 0+60S	1	9	10	30	.2	18	15	364	2.56	8	5	ND	2	12	1	3	2	36	.07	.06	11	26	.46	64	.06	4	1.39	.01	.04	2	5
3W 0+80S	1	7	11	26	.1	13	8	170	1.48	8	5	ND	3	13	1	2	2	23	.10	.05	9	12	.27	67	.07	4	1.43	.01	.05	2	5
3W 1+20S	2	7	14	33	.2	17	8	140	1.47	5	5	ND	3	7	1	3	2	20	.07	.08	8	13	.28	62	.06	2	1.59	.01	.04	2	5
3W 1+60S	1	8	16	35	.1	15	6	106	1.45	4	5	ND	2	13	1	3	2	18	.11	.08	10	10	.42	62	.05	2	1.52	.01	.03	2	5
3W 2+00S	1	8	13	37	.1	14	5	99	1.45	3	5	ND	4	7	1	3	2	17	.07	.09	15	14	.33	38	.05	3	1.25	.01	.06	2	5
3W 2+40S	1	5	12	26	.1	8	3	222	1.08	4	5	ND	3	9	1	2	2	15	.07	.09	10	8	.31	60	.04	2	.96	.01	.04	2	5
3W 2+80S	2	8	14	29	.1	12	4	97	1.54	4	5	ND	2	7	1	2	2	23	.06	.09	8	9	.21	53	.08	2	1.98	.01	.04	2	5
3W 3+60S	1	8	11	32	.2	12	4	98	1.66	6	5	ND	3	10	1	2	3	25	.07	.10	9	10	.21	61	.08	3	1.37	.01	.05	2	5
3W 4+00S	1	20	28	37	.1	19	5	233	1.49	2	5	ND	3	17	1	2	3	22	.18	.04	20	12	.60	74	.06	2	1.55	.01	.06	2	5
3W 4+40S	1	6	20	44	.1	11	4	178	1.70	2	5	ND	2	7	1	2	2	26	.08	.11	8	10	.35	51	.09	2	1.84	.01	.03	2	5
3W 4+80S	1	10	16	38	.1	12	4	111	1.27	2	5	ND	4	15	1	2	3	18	.15	.04	15	9	.64	64	.06	2	1.35	.01	.05	2	5
2W 1+20N	1	7	13	33	.1	19	9	245	1.59	4	5	ND	2	9	1	2	3	26	.09	.05	8	27	.33	62	.07	2	1.34	.01	.04	2	5
2W 0+80N	1	10	12	40	.1	18	8	202	1.81	3	5	ND	3	7	1	3	4	28	.08	.04	9	36	.61	54	.08	3	1.73	.01	.04	2	5
2W 0+40N	1	21	18	59	.2	40	13	472	2.91	5	5	ND	2	9	1	2	4	46	.08	.08	6	60	.52	117	.14	4	3.34	.01	.06	2	5
2W 0+00N	1	9	11	50	.2	24	15	640	2.74	7	5	ND	3	7	1	2	2	43	.05	.07	7	46	.48	69	.10	2	2.13	.01	.04	2	5
2W 0+20S	1	10	15	32	.2	16	8	155	2.46	28	5	ND	4	10	1	2	2	33	.07	.09	7	18	.24	71	.12	2	2.65	.02	.04	2	5
2W 0+40S	2	9	13	36	.3	18	12	420	2.76	9	5	ND	5	11	1	2	2	43	.07	.09	8	26	.32	75	.10	4	1.78	.01	.05	2	5
2W 0+80S	1	10	14	49	.3	28	8	155	2.40	10	5	ND	5	11	1	2	2	31	.11	.13	10	24	.50	70	.08	2	2.34	.01	.05	2	5
2W 1+20S	1	5	22	35	.1	14	5	131	1.38	2	5	ND	3	7	1	2	2	21	.08	.05	9	13	.45	56	.06	2	1.53	.01	.06	2	5
2W 1+60S	1	10	11	25	.1	12	4	75	1.41	2	5	ND	6	5	1	2	2	15	.04	.08	24	10	.17	51	.04	2	1.24	.01	.02	2	5
2W 2+00S	1	13	16	31	.3	21	9	105	1.81	9	5	ND	4	13	1	3	2	24	.11	.09	9	23	.32	79	.07	2	2.05	.01	.06	2	5
2W 2+40S	1	8	19	28	.2	10	4	97	1.31	7	5	ND	4	10	1	5	2	21	.10	.04	12	12	.60	36	.06	2	1.19	.01	.05	2	5
2W 2+80S	1	4	12	24	.1	6	3	82	1.01	5	5	ND	2	8	1	4	2	17	.07	.04	9	9	.23	41	.05	2	.84	.01	.04	2	5
2W 3+60S	1	10	21	53	.2	18	6	151	1.66	6	5	ND	4	17	1	3	2	23	.19	.18	11	10	.49	65	.07	2	1.80	.01	.07	2	5
2W 4+00S	1	10	30	51	.2	15	6	209	1.87	7	5	ND	5	10	1	2	2	26	.10	.15	11	14	.55	70	.08	2	2.06	.01	.06	2	5
2W 4+40S	1	8	22	38	.1	13	4	112	1.70	9	5	ND	3	9	1	2	3	23	.09	.19	8	10	.35	60	.08	2	2.44	.01	.03	2	5
2W 4+80S	1	7	22	38	.3	11	5	77	1.50	4	8	ND	5	7	1	2	2	20	.07	.18	10	6	.38	48	.06	2	1.70	.01	.06	2	5
STD C/AU 0.5	21	59	39	125	7.0	70	27	1063	3.82	40	17	7	35	49	17	15	22	59	.44	.15	36	58	.88	182	.07	37	1.65	.06	.13	12	510

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
1W 2+00N	1	16	13	50	.2	26	8	312	2.18	5	5	ND	4	8	1	2	2	32	.08	.09	5	30	.48	72	.11	4	3.05	.01	.05	2	5
1W 1+60N	1	9	11	49	.1	21	8	199	1.92	2	5	ND	2	7	1	2	2	28	.08	.09	9	40	.70	56	.07	6	1.80	.01	.05	2	5
1W 1+20N	1	15	14	54	.1	21	10	500	2.15	4	5	ND	2	9	1	2	2	34	.11	.08	4	28	.40	69	.13	5	2.68	.01	.06	2	5
1W 0+80N	1	29	13	70	.1	29	8	1451	2.14	4	5	ND	2	9	1	2	2	33	.08	.09	5	18	.19	86	.14	4	2.96	.02	.05	2	5
1W 0+40N	1	21	18	52	.1	36	12	440	2.63	6	5	ND	4	8	1	2	3	39	.06	.12	6	39	.51	66	.15	4	3.82	.01	.06	2	5
1W 0+20N	1	12	10	38	.2	25	11	316	2.17	2	5	ND	2	7	1	2	3	35	.08	.06	5	54	.59	44	.09	3	2.01	.01	.05	2	5
1W 0+00N	1	8	11	49	.1	24	13	639	2.20	2	5	ND	2	9	1	2	4	38	.13	.04	7	40	.65	68	.09	5	1.80	.01	.06	2	5
1W 0+40S	1	9	11	38	.3	19	16	170	2.34	5	5	ND	2	5	1	2	3	38	.05	.05	7	45	.48	58	.07	2	1.71	.01	.04	2	5
1W 0+80S	1	14	7	35	.2	22	11	156	2.09	5	9	ND	4	5	1	2	2	28	.05	.03	13	53	.73	40	.05	4	1.27	.01	.04	2	5
1W 1+20S	1	12	8	36	.1	11	4	108	1.40	2	8	ND	3	9	1	2	2	17	.13	.02	16	16	1.15	44	.08	3	1.51	.01	.07	2	5
1W 1+60S	1	11	10	30	.1	12	4	94	1.20	5	5	ND	3	12	1	2	2	17	.11	.01	16	15	.68	50	.07	4	1.41	.01	.05	2	5
1W 1+80S	1	10	19	52	.2	13	5	127	1.92	4	5	ND	4	8	1	2	2	23	.10	.21	8	12	.56	59	.09	3	2.26	.01	.06	2	5
1W 2+00S	1	11	14	47	.3	12	4	103	1.72	2	7	ND	4	8	1	2	2	22	.10	.10	10	14	.75	58	.08	6	2.01	.01	.08	2	5
1W 2+40S	1	13	12	41	.1	14	4	135	1.38	6	5	ND	4	12	1	2	2	19	.17	.03	15	17	.99	53	.07	3	1.40	.01	.06	2	5
1W 2+80S	1	11	10	35	.1	12	3	115	1.18	6	5	ND	4	10	1	2	2	15	.14	.02	14	15	.89	37	.06	2	1.15	.01	.06	2	5
1W 3+20S	1	15	27	34	.1	15	4	93	1.88	8	5	ND	5	12	1	2	2	25	.12	.22	8	12	.36	60	.11	3	3.25	.02	.05	2	5
1W 3+60S	1	10	20	33	.2	11	4	118	1.35	4	5	ND	5	8	1	2	2	16	.11	.05	13	11	.74	52	.06	2	1.36	.01	.08	2	5
1W 4+00S	1	10	26	37	.3	11	4	92	1.61	3	5	ND	4	7	1	2	2	22	.07	.10	10	13	.43	52	.07	3	1.70	.01	.07	2	35
1W 4+40S	1	6	14	30	.1	7	2	86	.88	4	5	ND	2	15	1	2	2	12	.16	.04	14	10	.60	46	.06	5	1.00	.01	.06	2	5
1W 4+80S	1	11	19	32	.2	8	3	170	1.36	3	5	ND	5	18	1	2	2	21	.25	.05	15	11	.86	48	.07	9	1.01	.01	.16	2	5
1W 5+20S	1	7	21	38	.3	6	3	113	1.24	3	5	ND	3	9	1	2	3	18	.12	.15	11	8	.40	55	.06	5	1.12	.01	.07	2	15
0W 2+00N	1	7	9	43	.4	7	2	327	1.17	4	5	ND	2	5	1	2	3	24	.06	.07	5	20	.15	51	.07	2	.99	.01	.04	2	5
0W 1+60N	1	19	10	35	.1	14	6	169	1.73	5	5	ND	3	8	1	2	3	27	.05	.12	9	17	.23	69	.12	3	2.95	.02	.04	2	5
0W 1+20N	1	17	10	47	.1	22	7	579	1.83	6	5	ND	2	10	1	2	4	29	.08	.10	7	27	.45	95	.13	2	2.85	.02	.05	2	5
0W 0+80N	1	23	9	57	.3	46	12	463	2.79	6	11	ND	3	8	1	2	4	44	.08	.06	8	88	.99	57	.09	2	2.45	.01	.06	2	5
0W 0+40N	1	15	11	79	.2	52	23	912	2.65	5	6	ND	2	10	1	2	4	44	.11	.05	7	90	.76	59	.10	2	2.35	.01	.05	2	5
0W 0+00N	1	11	10	60	.2	42	24	693	3.55	2	6	ND	2	6	1	2	4	68	.06	.04	10	97	.97	39	.08	4	2.02	.01	.05	2	15
0W 0+80S	1	20	12	35	.2	27	16	244	2.42	4	5	ND	3	11	1	2	3	40	.12	.02	16	83	1.00	48	.06	2	1.41	.01	.05	2	5
0W 1+20S	1	18	17	38	.3	22	29	125	1.74	4	6	ND	3	12	1	2	2	27	.09	.03	13	29	.51	70	.06	2	1.70	.01	.06	2	5
0W 1+40S	1	15	9	37	.2	26	11	174	2.08	3	5	ND	2	7	1	2	2	33	.06	.04	6	38	.44	54	.08	3	1.79	.01	.04	2	5
0W 1+60S	1	16	14	56	.2	21	6	140	1.95	3	5	ND	5	10	1	2	2	26	.10	.07	11	18	.80	95	.09	2	2.45	.01	.08	2	5
0W 2+00S	1	8	6	37	.2	11	3	109	1.22	3	6	ND	5	14	1	2	2	17	.15	.04	14	14	.90	31	.07	3	1.29	.01	.08	2	35
0W 2+40S	1	12	11	41	.2	12	5	492	1.24	5	5	ND	5	24	1	2	2	18	.22	.05	15	14	.83	66	.07	2	1.32	.01	.08	2	5
0W 2+80S	1	6	7	34	.1	7	2	95	1.01	4	5	ND	3	10	1	2	2	17	.11	.03	12	11	.64	39	.07	2	1.06	.01	.05	2	5
0W 3+20S	1	11	11	40	.2	9	3	134	1.27	5	7	ND	5	16	1	2	2	19	.15	.02	13	11	.87	51	.08	3	1.31	.01	.09	2	5
0W 3+60S	1	10	17	39	.1	8	3	194	1.15	2	6	ND	4	19	1	2	2	18	.17	.04	13	10	.67	59	.07	2	1.20	.01	.12	2	5
0W 4+00S	1	17	17	46	.2	13	5	361	1.56	2	8	ND	4	29	1	2	3	21	.29	.05	24	14	.90	96	.07	2	1.72	.01	.10	2	5
STD C/AU-0.5	19	58	40	125	7.3	70	27	1151	3.82	42	20	7	35	49	17	15	19	59	.44	.15	39	58	.88	181	.07	39	1.65	.06	.14	12	490

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
0W 4+40S	1	19	30	73	.1	17	6	161	2.48	6	5	ND	7	14	1	2	3	31	.12	.17	11	17	.72	97	.11	3	3.21	.01	.09	2	5
0W 4+80S	1	16	25	57	.1	14	4	438	1.54	2	5	ND	4	29	1	2	3	19	.27	.04	21	14	.80	143	.08	3	1.95	.02	.13	2	5
1E 2+00N	1	11	10	69	.1	19	8	307	2.13	2	5	ND	2	9	1	2	4	30	.08	.18	5	37	.40	63	.09	3	2.76	.01	.05	2	5
1E 1+60N	1	11	14	41	.1	17	6	209	2.01	5	5	ND	2	6	1	2	3	33	.05	.10	6	46	.47	63	.09	4	2.29	.01	.04	2	5
1E 1+20N	1	14	9	38	.1	20	4	325	1.87	6	5	ND	3	6	1	3	4	26	.05	.14	3	19	.13	42	.13	4	4.26	.02	.03	2	5
1E 0+80N	1	13	11	53	.1	18	7	641	2.03	4	5	ND	2	7	1	2	3	37	.07	.07	5	50	.43	58	.10	3	2.17	.01	.05	2	5
1E 0+40N	1	10	8	46	.1	19	5	334	2.20	7	5	ND	2	7	1	2	3	41	.06	.06	6	44	.36	53	.12	4	2.51	.02	.03	2	5
1E 0+00N	2	16	11	36	.2	15	11	73	1.76	11	5	ND	4	5	1	2	4	25	.03	.05	6	12	.27	60	.07	2	2.79	.01	.03	2	5
1E 0+20S	1	11	11	38	.2	13	5	249	1.52	3	5	ND	2	6	1	2	3	27	.06	.08	6	18	.30	49	.09	4	1.56	.01	.04	2	5
1E 0+40S	1	21	10	37	.2	22	11	188	1.81	6	5	ND	4	8	1	2	2	26	.06	.13	8	17	.22	57	.12	4	3.46	.02	.03	2	5
1E 0+60S	1	39	11	38	.1	37	17	136	2.42	11	5	ND	10	9	1	3	2	33	.05	.10	11	30	.24	68	.14	3	4.42	.02	.04	2	5
1E 0+80S	1	19	10	40	.2	21	7	154	1.88	4	5	ND	3	6	1	2	2	31	.06	.03	9	42	.76	37	.07	2	1.61	.01	.04	2	5
1E 1+00S	2	17	7	36	.1	19	5	125	1.93	6	5	ND	3	7	1	2	2	30	.07	.02	11	38	.66	39	.07	4	1.40	.01	.03	2	5
1E 1+20S	1	23	15	45	.1	24	10	143	1.95	5	5	ND	4	9	1	2	2	30	.07	.09	8	30	.41	54	.09	4	2.03	.01	.04	2	5
1E 1+60S	1	13	13	25	.1	13	4	73	1.13	4	5	ND	2	8	1	2	2	20	.06	.02	8	19	.32	46	.07	2	1.20	.02	.03	2	5
1E 2+00S	1	6	9	19	.1	8	2	68	.76	2	5	ND	2	12	1	2	2	13	.07	.02	11	9	.30	38	.05	3	.86	.01	.03	2	5
1E 2+40S	1	10	15	35	.1	10	3	108	1.22	2	5	ND	4	16	1	2	2	16	.10	.03	15	10	.42	63	.06	4	1.44	.01	.06	2	5
1E 2+80S	1	11	11	32	.1	8	3	207	1.28	2	5	ND	6	27	1	2	2	21	.22	.06	19	11	.63	64	.07	5	1.09	.01	.16	2	5
1E 3+20S	1	8	8	38	.1	10	3	110	1.19	2	5	ND	4	18	1	2	2	17	.14	.03	14	12	.69	62	.07	4	1.38	.01	.05	2	5
1E 3+60S	1	4	8	35	.1	7	2	84	.96	2	5	ND	4	12	1	2	2	16	.13	.02	12	10	.58	30	.08	3	1.09	.01	.04	2	5
1E 4+00S	1	8	13	61	.1	10	4	121	1.58	3	5	ND	4	9	1	3	3	21	.10	.13	10	12	.62	59	.07	2	1.62	.01	.04	2	5
1E 4+40S	1	7	10	41	.1	7	3	110	1.11	3	5	ND	4	16	1	2	2	19	.15	.04	13	10	.59	47	.08	3	1.19	.01	.05	2	5
1E 4+80S	1	10	12	45	.1	8	3	129	1.28	3	5	ND	3	20	1	2	3	22	.18	.02	13	13	.80	62	.08	3	1.42	.02	.05	2	5
2E 2+00N	1	15	18	25	.2	8	3	64	2.98	7	5	ND	7	5	1	4	3	29	.03	.18	9	23	.17	40	.07	2	4.00	.01	.03	2	5
2E 1+60N	1	8	13	26	.1	9	3	93	1.91	3	5	ND	3	4	1	2	3	23	.02	.05	14	18	.21	43	.05	3	1.39	.01	.04	2	5
2E 1+20N	1	12	8	22	.4	6	2	42	2.53	4	5	ND	4	6	1	4	3	39	.03	.19	4	10	.07	26	.13	2	4.55	.02	.03	2	5
2E 0+80N	1	14	6	22	.2	7	3	60	2.00	4	5	ND	4	6	1	2	2	29	.03	.17	3	11	.06	38	.13	4	4.33	.02	.01	2	5
2E 0+40N	1	12	8	25	.1	7	4	80	1.99	7	5	ND	5	6	1	2	2	28	.03	.14	6	13	.13	46	.10	3	2.80	.01	.02	2	5
2E 0+20N	1	16	15	49	.2	13	6	120	1.72	3	5	ND	4	6	1	3	2	22	.05	.11	10	18	.45	58	.08	3	1.87	.01	.04	2	5
2E 0+00N	1	14	7	35	.2	13	9	107	1.69	7	5	ND	4	7	1	2	2	22	.05	.20	7	9	.12	55	.10	2	3.18	.02	.03	2	5
2E 0+20S	1	13	11	29	.1	11	4	68	2.33	7	5	ND	4	6	1	3	2	32	.03	.16	9	10	.16	71	.09	2	2.59	.01	.03	2	5
2E 0+40S	1	14	15	28	.2	11	3	85	2.62	6	5	ND	5	6	1	3	2	36	.04	.14	9	12	.21	71	.09	2	2.30	.01	.03	2	5
2E 0+80S	2	27	13	47	.2	13	4	181	2.16	8	5	ND	5	5	1	2	2	32	.04	.13	11	12	.30	63	.10	3	2.30	.01	.03	2	5
2E 1+20S	1	10	8	70	.3	13	6	840	1.81	4	5	ND	4	7	1	2	2	24	.05	.18	8	9	.24	72	.09	3	2.42	.01	.03	2	5
2E 1+60S	1	6	9	25	.1	7	2	88	1.07	3	5	ND	4	6	1	2	2	15	.03	.04	11	7	.17	49	.05	2	1.04	.01	.03	2	5
2E 2+00S	1	10	12	29	.2	10	3	95	.98	3	5	ND	3	13	1	2	2	14	.08	.02	11	9	.31	83	.06	3	1.25	.02	.05	2	5
2E 2+40S	1	10	12	66	.2	15	4	169	2.39	4	5	ND	5	9	1	2	2	29	.05	.33	14	12	.18	82	.08	3	2.49	.01	.04	2	5
STD C/AU-0.5	19	58	39	124	6.9	69	27	1079	3.82	39	18	7	35	49	16	15	18	59	.44	.14	38	58	.88	182	.07	37	1.65	.06	.13	13	500

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
2E 2+80S	1	6	10	24	.1	8	2	97	.86	2	5	ND	2	12	1	2	3	11	.07	.02	13	7	.32	63	.04	4	.87	.01	.04	2	5
2E 3+20S	1	11	11	33	.1	11	4	158	1.16	5	6	ND	2	18	1	3	3	15	.12	.02	17	11	.54	85	.05	4	1.42	.01	.06	2	5
2E 3+60S	1	10	9	65	.1	15	4	139	1.42	2	5	ND	3	14	1	2	3	20	.15	.02	13	17	.94	62	.09	5	1.77	.01	.05	2	5
2E 4+00S	1	9	11	41	.1	11	4	100	1.39	2	5	ND	4	10	1	2	3	18	.09	.04	14	11	.73	68	.07	3	1.63	.01	.06	2	5
2E 4+40S	1	8	9	34	.1	9	3	99	1.31	2	5	ND	4	14	1	2	3	20	.15	.03	12	12	.78	45	.07	4	1.21	.01	.04	2	10
2E 4+80S	1	16	19	66	.1	18	6	276	2.09	2	5	ND	4	15	1	2	4	28	.12	.10	12	15	.60	112	.09	4	2.73	.01	.09	2	5
3E 2+00N	1	7	10	19	.1	6	2	71	.91	2	5	ND	3	7	1	2	3	17	.06	.01	10	16	.24	59	.05	2	.65	.01	.05	2	5
3E 1+60N	1	8	8	25	.1	7	3	67	1.20	2	5	ND	4	4	1	2	3	13	.03	.06	12	9	.21	36	.04	3	1.30	.01	.04	2	5
3E 1+20N	1	8	10	33	.1	9	3	83	2.63	2	7	ND	4	4	1	2	4	34	.03	.10	7	46	.32	35	.06	4	1.75	.01	.04	2	5
3E 0+80N	1	10	12	26	.1	6	2	54	2.44	6	5	ND	4	4	1	2	4	36	.02	.21	4	23	.06	34	.12	3	4.07	.01	.03	2	5
3E 0+40N	1	6	10	22	.1	6	3	67	1.46	2	5	ND	4	5	1	2	2	17	.04	.05	12	10	.18	29	.03	3	.88	.01	.03	2	5
3E 0+00N	2	10	12	39	.1	7	3	216	1.78	4	5	ND	3	5	1	2	2	25	.04	.17	6	8	.11	46	.10	4	2.54	.01	.03	2	5
3E 0+20S	1	13	11	27	.2	9	9	134	1.75	7	5	ND	5	7	1	2	2	22	.04	.13	6	8	.14	52	.09	3	2.51	.02	.03	2	5
3E 0+40S	1	10	13	35	.1	9	4	107	2.22	4	5	ND	5	5	1	2	2	30	.03	.22	9	10	.11	53	.09	4	2.85	.01	.04	2	5
3E 0+60S	1	10	10	38	.2	7	4	360	1.95	4	5	ND	3	5	1	2	2	30	.03	.17	4	8	.09	48	.10	3	2.71	.01	.02	2	5
3E 0+80S	1	15	12	57	.2	11	4	171	2.04	6	5	ND	3	8	1	2	2	30	.05	.17	4	7	.10	72	.13	5	3.04	.01	.02	2	5
3E 1+20S	1	10	14	57	.2	11	4	173	1.67	2	5	ND	4	5	1	2	2	22	.04	.22	6	9	.16	61	.08	3	2.06	.01	.04	2	5
3E 1+60S	1	9	13	27	.1	11	3	63	1.04	2	5	ND	2	7	1	2	2	15	.04	.02	10	8	.22	50	.06	3	1.23	.01	.03	2	5
3E 2+00S	1	6	8	29	.1	8	3	82	1.24	2	5	ND	4	4	1	2	2	14	.03	.03	15	8	.24	44	.04	3	.95	.01	.03	2	5
3E 2+40S	1	8	13	18	.2	10	3	57	.78	2	5	ND	2	12	1	2	2	11	.08	.01	10	8	.21	94	.06	2	1.20	.02	.04	2	5
3E 2+80S	1	7	9	32	.1	10	4	68	1.49	2	5	ND	4	6	1	2	2	16	.05	.15	12	7	.16	56	.05	3	1.78	.01	.04	2	5
3E 3+20S	1	6	9	60	.1	8	3	96	1.54	3	5	ND	5	5	1	2	3	19	.04	.16	11	10	.27	45	.06	3	1.56	.01	.04	2	5
3E 3+60S	2	7	9	59	.1	10	4	126	1.82	2	5	ND	4	6	1	2	2	23	.05	.26	7	10	.26	57	.09	2	2.55	.02	.04	2	15
3E 4+00S	1	4	4	21	.1	5	2	73	.92	2	5	ND	4	12	1	2	3	13	.08	.03	14	7	.32	35	.05	3	.72	.01	.03	2	5
3E 4+40S	1	5	8	30	.1	7	2	81	.92	2	5	ND	3	9	1	2	2	14	.08	.02	10	10	.41	39	.06	2	.91	.01	.04	2	5
3E 4+80S	1	10	11	50	.1	11	4	122	1.60	2	5	ND	4	12	1	2	3	22	.11	.06	10	12	.65	70	.08	2	1.80	.01	.05	2	5
4E 2+00N	1	5	8	14	.1	5	2	51	.98	2	5	ND	4	2	1	2	3	8	.01	.02	14	7	.19	19	.02	2	.63	.01	.02	2	5
4E 1+60N	1	9	12	22	.1	9	5	80	2.53	2	6	ND	7	2	1	2	2	20	.01	.07	14	21	.40	17	.02	2	1.08	.01	.02	2	5
4E 1+20N	1	14	7	30	.2	7	5	57	2.72	8	6	ND	6	6	1	4	3	31	.04	.34	8	16	.15	38	.11	2	4.58	.02	.03	2	5
4E 0+80N	1	5	6	22	.1	7	3	78	.91	2	5	ND	4	6	1	2	2	10	.04	.02	14	8	.27	41	.04	2	.93	.01	.04	2	5
4E 0+40N	1	10	12	23	.2	6	3	51	2.67	10	5	ND	4	7	1	3	2	39	.04	.29	4	11	.08	50	.15	2	4.61	.02	.02	2	5
4E 0+00N	1	7	8	21	.3	4	2	255	1.18	5	5	ND	2	6	1	2	2	22	.05	.11	5	6	.06	37	.08	3	1.59	.01	.03	2	5
4E 0+20S	1	9	10	71	.3	8	4	608	2.69	7	5	ND	4	10	1	4	2	35	.06	.25	4	9	.07	128	.15	3	4.96	.02	.02	2	5
4E 0+40S	1	12	8	39	.3	7	4	295	1.86	7	5	ND	5	7	1	5	2	25	.04	.29	4	8	.07	41	.13	4	4.34	.02	.03	2	5
4E 0+80S	1	9	11	32	.3	7	3	163	1.69	7	5	ND	3	7	1	3	2	25	.05	.19	6	6	.07	52	.11	3	3.27	.02	.04	2	5
4E 1+00S	1	13	13	60	.2	12	8	152	2.21	2	5	ND	6	7	1	4	2	23	.04	.16	12	11	.15	68	.09	3	3.49	.02	.03	2	5
4E 1+20S	1	12	10	21	.2	8	2	69	2.03	4	5	ND	4	7	1	5	2	28	.04	.42	3	6	.06	22	.13	3	4.79	.02	.03	2	5
STD C/AU-0.5	20	58	39	124	7.2	69	27	1064	3.82	42	20	7	35	49	16	14	18	59	.44	.14	37	57	.88	181	.07	37	1.65	.06	.13	14	490

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
4E 1+40S	2	12	15	68	.1	9	3	659	2.25	10	5	ND	4	10	1	2	4	35	.06	.34	5	6	.13	127	.17	4	2.55	.02	.04	2	5
4E 1+60S	1	10	10	65	.1	14	5	116	2.00	5	5	ND	5	8	1	3	2	24	.05	.15	9	10	.19	56	.11	5	3.02	.02	.05	2	5
4E 2+00S	1	8	5	38	.1	10	4	119	1.33	2	5	ND	5	5	1	3	2	15	.04	.06	12	8	.28	47	.04	4	1.39	.01	.04	2	5
4E 2+40S	2	15	15	97	.1	18	10	505	2.48	9	5	ND	6	8	1	3	2	30	.06	.22	18	13	.27	107	.11	5	2.86	.01	.04	3	5
4E 2+60S	2	9	16	72	.1	11	4	131	2.24	4	5	ND	4	6	1	2	2	29	.05	.17	16	11	.28	74	.10	6	1.90	.01	.04	2	5
4E 3+20S	1	8	13	34	.1	11	3	100	1.00	2	5	ND	3	11	1	2	2	14	.08	.01	13	9	.36	70	.07	4	1.17	.01	.04	2	5
4E 3+60S	1	7	7	30	.1	9	3	124	.89	3	5	ND	4	7	1	2	2	10	.07	.01	17	7	.35	54	.05	4	.95	.01	.03	2	5
4E 4+00S	1	4	7	15	.1	4	1	45	.55	2	5	ND	3	6	1	2	2	8	.05	.01	13	6	.17	39	.03	4	.49	.01	.02	2	5
4E 4+40S	1	8	8	30	.1	9	3	102	1.06	2	5	ND	4	8	1	2	2	13	.05	.02	15	8	.27	51	.05	3	.98	.01	.04	2	5
4E 4+80S	1	11	13	53	.1	17	5	149	1.33	2	5	ND	6	12	1	2	2	17	.10	.02	16	13	.51	76	.06	2	1.48	.01	.06	2	5
5E 2+00N	1	11	14	39	.2	11	4	77	2.20	5	5	ND	5	11	1	2	2	27	.09	.27	8	11	.18	58	.09	4	3.36	.01	.03	2	5
5E 1+60N	1	10	12	37	.2	9	4	65	1.76	2	5	ND	6	4	1	2	2	17	.03	.08	13	8	.19	46	.05	3	1.70	.01	.04	2	5
5E 1+20N	1	5	8	17	.1	4	1	76	1.17	2	5	ND	3	3	1	2	2	18	.02	.03	10	7	.16	31	.04	3	.88	.01	.03	2	5
5E 0+80N	1	14	12	35	.1	12	5	88	1.87	6	5	ND	5	5	1	3	2	21	.04	.12	12	14	.31	51	.06	4	2.54	.01	.04	2	5
5E 0+40N	1	15	8	24	.2	7	4	51	1.87	6	5	ND	4	6	1	7	4	24	.03	.19	4	8	.12	32	.11	4	4.19	.02	.02	2	5
5E 0+20N	1	11	8	19	.1	6	2	99	2.19	13	5	ND	3	6	1	7	4	29	.04	.25	3	8	.06	24	.13	4	5.28	.02	.01	2	5
5E 0+00N	1	9	18	48	.2	8	3	253	2.30	8	5	ND	4	7	1	2	4	37	.07	.27	8	11	.16	60	.14	4	2.21	.01	.04	2	5
5E 0+20S	1	11	7	26	.1	5	1	61	1.92	5	5	ND	3	5	1	5	3	31	.03	.27	3	9	.06	26	.13	4	4.30	.02	.02	2	5
5E 0+40S	1	12	12	24	.2	5	1	170	2.39	9	5	ND	3	5	1	3	2	37	.03	.32	4	9	.05	30	.14	4	4.45	.02	.01	2	5
5E 0+80S	1	10	14	41	.2	6	2	107	1.88	7	5	ND	3	5	1	2	2	27	.04	.20	6	9	.08	53	.10	5	2.35	.02	.03	2	5
5E 1+20S	1	14	12	39	.1	9	3	145	1.90	6	5	ND	4	6	1	6	2	27	.05	.20	5	8	.08	46	.12	5	4.33	.02	.03	2	5
5E 1+60S	1	8	13	29	.1	9	3	125	1.10	2	5	ND	3	9	1	2	2	17	.08	.04	12	10	.25	68	.06	3	1.38	.01	.04	2	5
5E 2+00S	2	12	10	53	.1	12	5	158	1.91	5	5	ND	4	8	1	6	2	24	.05	.20	6	8	.12	61	.12	3	3.94	.02	.02	2	5
5E 2+40S	1	6	8	30	.2	9	3	78	.95	2	5	ND	4	7	1	4	2	12	.04	.02	14	7	.25	62	.05	3	1.07	.01	.03	2	5
5E 2+80S	1	9	13	46	.3	11	3	122	2.41	3	5	ND	5	7	1	2	2	32	.04	.16	9	11	.18	60	.09	5	2.52	.01	.03	2	5
5E 3+20S	1	9	9	27	.2	7	1	84	2.40	6	5	ND	4	9	1	2	2	38	.11	.35	5	8	.07	46	.15	4	3.90	.02	.03	2	5
5E 3+60S	1	6	7	28	.3	6	2	60	1.14	2	5	ND	4	5	1	3	2	17	.05	.07	12	6	.16	49	.06	3	1.05	.01	.03	2	5
5E 4+00S	1	10	16	41	.3	11	4	122	1.40	5	5	ND	3	7	1	3	2	20	.05	.05	14	10	.26	60	.07	3	1.34	.01	.04	2	5
5E 4+40S	1	11	11	58	.2	17	5	168	1.22	4	5	ND	4	9	1	4	2	17	.07	.02	15	10	.41	91	.07	4	1.52	.01	.04	2	5
5E 4+80S	1	7	10	78	.3	11	4	141	1.69	3	5	ND	5	5	1	3	2	19	.05	.25	12	9	.27	57	.07	2	1.83	.01	.04	2	5
6E 2+00N	1	12	9	71	.3	11	6	122	1.86	3	7	ND	7	5	1	4	2	20	.04	.09	15	18	.40	54	.04	3	1.51	.01	.04	2	5
6E 1+60N	1	7	7	20	.1	5	2	46	1.48	2	5	ND	5	5	1	3	2	17	.03	.07	11	9	.15	37	.03	3	1.21	.01	.02	2	5
6E 1+20N	1	11	6	20	.1	5	1	32	1.39	3	5	ND	2	4	1	2	3	19	.02	.12	4	7	.04	33	.09	3	2.51	.01	.02	2	5
6E 0+80N	1	8	9	29	.3	7	3	137	1.52	2	6	ND	4	5	1	2	2	20	.04	.09	11	10	.23	45	.06	3	1.52	.01	.04	2	5
6E 0+40N	1	8	5	23	.2	4	1	112	1.16	2	5	ND	3	6	1	3	3	18	.05	.17	6	6	.07	37	.07	2	1.94	.01	.03	2	5
6E 0+20N	1	10	5	32	.3	8	4	74	1.67	2	5	ND	4	5	1	5	2	20	.03	.15	10	9	.17	52	.06	2	2.64	.01	.04	2	5
6E 0+00N	1	10	6	31	.3	9	4	128	2.04	11	5	ND	6	9	1	6	2	25	.06	.29	6	8	.11	37	.11	2	4.12	.02	.03	2	5
STD C/AU-0.5	19	58	39	124	7.0	69	27	1090	3.82	38	18	7	35	49	16	15	19	59	.44	.14	36	57	.88	182	.07	38	1.66	.06	.12	13	510

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
6E 0+20S	1	10	10	44	.3	5	2	75	1.45	3	5	ND	3	7	1	2	2	20	.05	.20	7	6	.09	61	.06	2	2.30	.01	.03	2	5
6E 0+40S	1	9	11	40	.1	8	2	75	2.09	2	5	ND	5	17	1	2	2	25	.11	.12	17	8	.18	82	.09	3	1.64	.01	.04	2	5
6E 0+60S	1	5	9	22	.1	5	2	94	.85	4	5	ND	2	5	1	2	3	15	.04	.02	15	6	.13	73	.06	2	.64	.01	.03	2	5
6E 0+80S	1	10	4	23	.1	7	3	115	1.68	8	5	ND	4	8	1	2	2	23	.06	.21	3	7	.07	33	.13	2	3.84	.03	.02	2	5
6E 1+00S	1	10	7	50	.1	10	4	86	1.77	5	5	ND	4	9	1	2	3	21	.07	.13	11	9	.21	77	.08	3	2.46	.01	.04	2	5
6E 1+20S	1	7	8	53	.1	7	3	226	1.60	4	5	ND	4	6	1	2	2	21	.05	.19	15	7	.20	70	.08	2	1.80	.01	.04	2	5
6E 1+60S	1	15	7	45	.1	9	5	139	1.70	10	5	ND	4	8	1	2	2	23	.05	.17	10	9	.17	72	.11	7	3.14	.02	.02	2	5
6E 2+00S	1	9	11	47	.2	7	3	106	1.52	3	5	ND	4	5	1	2	2	22	.04	.10	9	10	.17	44	.07	4	1.98	.01	.03	2	5
6E 2+40S	1	11	9	40	.3	6	3	110	1.96	7	5	ND	3	6	1	2	2	30	.04	.20	5	8	.08	42	.13	5	3.42	.02	.02	2	5
6E 2+80S	1	9	9	46	.2	12	4	80	1.83	4	5	ND	5	6	1	2	2	21	.04	.14	11	9	.15	62	.08	3	2.66	.01	.03	2	5
6E 3+20S	1	12	11	47	.2	9	4	261	1.78	7	5	ND	3	7	1	2	2	26	.07	.20	4	8	.08	62	.11	3	2.99	.02	.02	2	5
6E 3+60S	1	9	14	37	.2	9	3	70	1.24	4	5	ND	2	8	1	2	2	17	.08	.05	9	6	.17	61	.08	3	1.36	.01	.04	2	5
6E 4+00S	1	5	6	37	.2	8	2	75	.78	2	5	ND	4	5	1	5	2	9	.05	.01	15	8	.36	34	.04	3	.85	.01	.03	2	5
6E 4+40S	1	9	7	58	.1	12	4	123	1.37	5	5	ND	3	6	1	2	2	19	.06	.07	11	10	.38	52	.07	3	1.54	.01	.03	2	5
6E 4+80S	1	7	11	67	.4	9	4	155	1.69	5	5	ND	4	5	1	2	2	20	.04	.09	11	8	.22	54	.07	2	1.44	.01	.03	2	5
7E 2+00N	1	6	5	34	.2	11	4	128	1.67	3	5	ND	3	6	1	3	2	29	.08	.02	11	41	.59	22	.06	3	1.06	.01	.03	2	5
7E 1+60N	1	9	9	21	.1	9	10	62	1.06	4	5	ND	2	12	1	2	2	20	.10	.02	4	10	.26	68	.08	3	1.25	.03	.03	2	5
7E 1+20N	1	11	14	21	.2	7	3	66	2.55	7	5	ND	3	9	1	2	3	33	.09	.11	9	11	.19	64	.11	4	2.40	.01	.03	2	5
7E 0+80N	1	6	12	16	.2	4	2	45	1.61	3	5	ND	3	6	1	2	2	21	.04	.06	11	6	.10	51	.06	3	1.10	.01	.03	2	5
7E 0+60N	1	7	15	17	.1	9	3	63	.96	4	5	ND	2	12	1	2	2	13	.12	.02	8	7	.18	71	.07	2	1.18	.02	.03	2	5
7E 0+40N	1	6	15	19	.1	5	2	56	1.48	2	5	ND	4	9	1	2	2	16	.07	.07	15	8	.16	58	.03	3	.78	.01	.03	2	5
7E 0+20N	1	9	12	38	.1	8	4	78	1.58	2	5	ND	6	7	1	2	2	15	.05	.10	16	10	.23	43	.04	3	1.24	.01	.04	2	5
7E 0+00N	1	5	8	21	.1	6	2	63	.88	2	5	ND	3	8	1	2	2	10	.08	.02	13	7	.18	74	.03	2	.80	.01	.03	2	5
7E 0+40S	1	7	12	37	.1	7	3	75	2.03	3	5	ND	6	4	1	2	2	19	.03	.06	19	10	.29	32	.05	2	1.31	.01	.03	2	5
7E 0+80S	1	8	10	46	.1	7	2	91	1.77	2	5	ND	4	4	1	2	2	21	.03	.07	11	9	.16	56	.06	3	1.93	.01	.03	2	5
7E 1+20S	1	8	10	50	.1	8	3	98	1.42	2	5	ND	5	5	1	2	2	16	.03	.07	14	9	.21	52	.06	2	1.79	.01	.03	2	5
7E 1+60S	1	8	12	45	.1	8	3	81	2.17	2	5	ND	8	4	1	3	2	20	.03	.10	17	10	.25	38	.05	2	1.53	.01	.04	2	5
7E 2+00S	1	7	15	26	.1	5	1	73	1.57	3	5	ND	3	6	1	2	2	25	.04	.09	9	8	.09	43	.10	2	2.01	.01	.02	2	5
7E 2+40S	2	9	11	40	.2	5	2	105	2.14	8	5	ND	4	4	1	2	2	28	.02	.16	9	8	.17	42	.11	3	2.33	.01	.01	2	5
7E 2+80S	1	10	10	28	.3	5	1	99	2.14	3	5	ND	2	9	1	2	2	34	.07	.37	3	7	.07	38	.14	2	3.22	.02	.01	2	5
7E 3+20S	1	10	12	50	.1	7	2	93	2.01	8	5	ND	5	5	1	2	2	26	.03	.30	4	9	.08	44	.12	4	3.74	.02	.02	2	5
7E 3+60S	1	5	7	34	.1	6	2	86	.84	2	5	ND	3	7	1	2	2	10	.09	.02	14	7	.27	58	.04	2	.86	.01	.02	2	5
7E 4+00S	1	5	10	25	.1	6	2	74	.74	2	5	ND	4	5	1	4	2	9	.05	.01	15	6	.26	31	.04	2	.74	.01	.03	2	5
7E 4+40S	1	10	14	61	.4	10	3	101	2.43	4	5	ND	5	4	1	2	2	29	.03	.28	12	11	.18	55	.11	5	2.21	.01	.04	2	5
7E 4+80S	1	4	9	31	.1	6	3	82	.76	3	5	ND	2	8	1	3	2	10	.12	.02	12	7	.20	52	.05	3	.83	.01	.03	2	5
8E 2+00N	1	6	10	9	.2	2	1	15	.99	5	5	ND	2	5	1	2	2	15	.04	.02	4	6	.03	38	.08	2	2.22	.02	.02	2	5
8E 1+60N	1	8	15	24	.1	9	9	62	1.48	3	5	ND	2	9	1	2	2	29	.09	.02	10	13	.20	54	.13	4	1.50	.02	.02	2	5
STD C/AU-0.5	20	58	39	124	7.2	70	27	1080	3.82	39	18	7	34	49	17	15	20	59	.44	.14	37	58	.88	181	.07	40	1.65	.06	.11	13	490

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
BE 1+20N	1	10	6	30	.2	7	6	94	2.46	6	5	ND	3	6	1	2	3	40	.04	.06	8	9	.23	37	.10	5	2.68	.02	.02	2	5
BE 0+40N	1	8	14	15	.6	4	2	36	1.53	6	5	ND	5	5	1	3	3	20	.04	.06	8	7	.07	40	.07	4	1.80	.01	.03	2	5
BE 0+20N	1	11	10	26	.2	8	2	93	2.03	3	5	ND	5	6	1	2	3	26	.05	.36	10	8	.13	50	.10	3	2.77	.01	.05	2	5
BE 0+00N	1	12	11	43	.1	7	2	66	2.07	5	5	ND	4	4	1	2	3	21	.03	.24	11	10	.14	47	.06	4	2.75	.01	.03	2	5
BE 0+20S	1	11	6	28	.1	5	2	52	1.38	6	5	ND	3	4	1	3	2	20	.02	.20	8	6	.09	49	.06	3	2.23	.01	.03	2	5
BE 0+40S	1	5	8	15	.2	2	1	54	.72	2	5	ND	2	2	1	2	2	14	.01	.06	4	3	.03	35	.07	3	.80	.01	.03	2	5
BE 0+60S	1	13	11	29	.1	5	2	87	2.02	9	5	ND	4	4	1	2	4	27	.02	.39	6	9	.07	33	.12	4	4.06	.01	.02	2	5
BE 0+80S	1	4	11	18	.1	3	1	62	1.26	4	5	ND	3	4	1	3	4	19	.03	.08	9	6	.09	26	.05	2	1.28	.01	.03	2	5
BE 1+00S	1	8	10	23	.1	4	1	46	1.88	8	5	ND	3	3	1	2	3	30	.02	.22	7	7	.08	28	.10	4	1.95	.01	.02	2	5
BE 1+60S	1	5	8	25	.1	4	1	42	1.20	5	5	ND	3	3	1	3	2	16	.01	.05	12	8	.11	26	.04	3	.87	.01	.03	2	5
BE 2+00S	1	9	10	25	.1	5	1	72	1.84	7	5	ND	3	5	1	4	4	28	.03	.24	6	6	.07	38	.09	3	2.92	.01	.03	2	5
BE 2+40S	1	8	14	20	.1	4	1	41	2.08	5	5	ND	3	3	1	2	5	27	.02	.20	6	6	.07	30	.11	3	2.43	.01	.03	2	5
BE 2+80S	1	14	9	33	.1	7	3	75	1.88	10	5	ND	4	6	1	2	4	25	.04	.27	5	7	.09	38	.13	2	4.14	.02	.02	2	5
BE 3+20S	1	14	9	30	.1	6	3	133	2.15	7	5	ND	3	5	1	3	3	31	.03	.34	5	7	.07	31	.14	4	4.66	.02	.01	2	5
BE 3+60S	1	8	11	35	.1	6	2	63	1.47	4	5	ND	4	3	1	3	2	18	.02	.14	9	8	.13	43	.06	3	1.95	.01	.02	2	5
BE 4+00S	1	9	8	21	.1	4	1	39	2.25	6	5	ND	4	4	1	2	3	28	.03	.41	7	8	.08	41	.09	3	3.79	.01	.02	2	5
BE 4+40S	1	8	13	11	.1	4	1	22	2.34	9	5	ND	3	6	1	2	2	30	.05	.22	8	7	.07	59	.12	3	3.09	.01	.02	2	5
BE 4+80S	1	3	10	12	.1	3	1	41	.63	3	5	ND	2	4	1	3	2	10	.03	.02	7	3	.06	40	.05	2	.64	.01	.03	2	5
3W 0+60S-B ROCK	1	15	12	9	.2	14	19	122	2.71	7	5	ND	38	2	1	4	2	7	.01	.04	14	7	.11	6	.01	3	.23	.01	.05	2	5
STD C/AU-0.5	19	58	39	124	6.9	69	27	1082	3.82	40	17	7	35	49	16	15	20	59	.44	.14	39	58	.88	181	.07	40	1.65	.06	.14	12	500

APPENDIX B

ACME ANALYTICAL LABORATORIES LTD.

PHONE: 253-3158 852 East Hastings St., Vancouver, B.C. V6A 1R6

File: 84-2711

Date: SEPT 25 1984

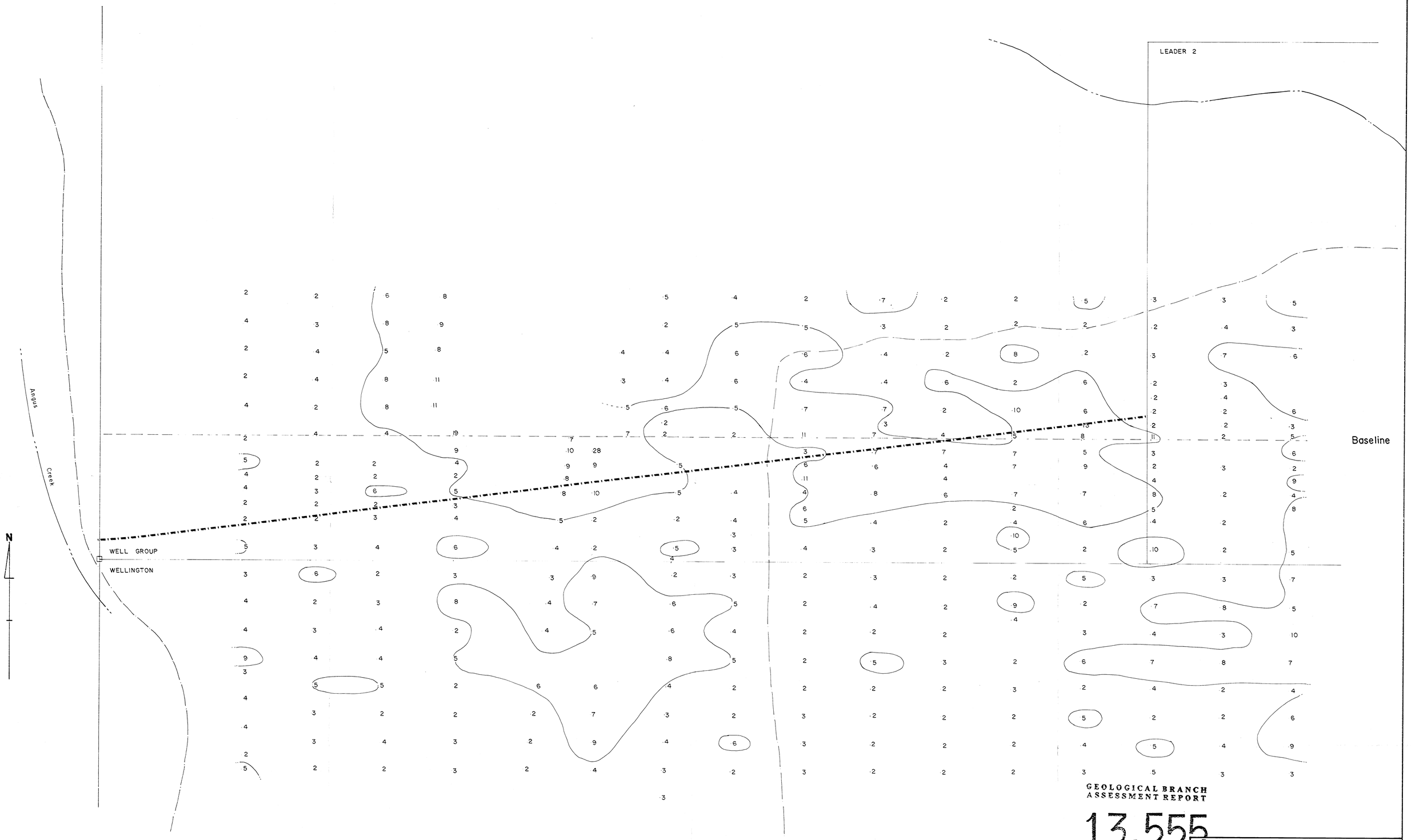
GEOTECH RESOURCES INC.
319 - 470 GRANVILLE ST
VANCOUVER B.C.
ATTN G.S. ARCHER

TERMS:
NET TWO WEEKS
2% PER MONTH CHARGED ON
OVERDUE ACCOUNTS.

NUMBER	ASSAY	PRICE	AMOUNT
	PROJECT : WELL GROUP-84		
316	ICP ANALYSIS @	6.00	1896.00
316	GEOCHEM AU ASSAY @	4.00	1264.00
315	SOIL SAMPLE PREPARATION @	.60	189.00
1	ROCK SAMPLE PREPARATION @	2.75	2.75
	TOTAL		3351.75

pd 1675.88 pd Geotech chq #276 Oct 18/84
1675.87 " Timetau 238 " "

PLEASE PAY LAST AMOUNT



GEOLOGICAL BRANCH
ASSESSMENT REPORT

13,555
PART
2 OF 2

LEGEND

CREEK

ROAD

CLAIM BOUNDARY

SAMPLE STATION 5.2 VALUE (P.P.M.)

APPROX. LOCATION OF FAULT

100 0 100 200 METRES

SCALE 1:2000

N.T.S. 82 F/9E

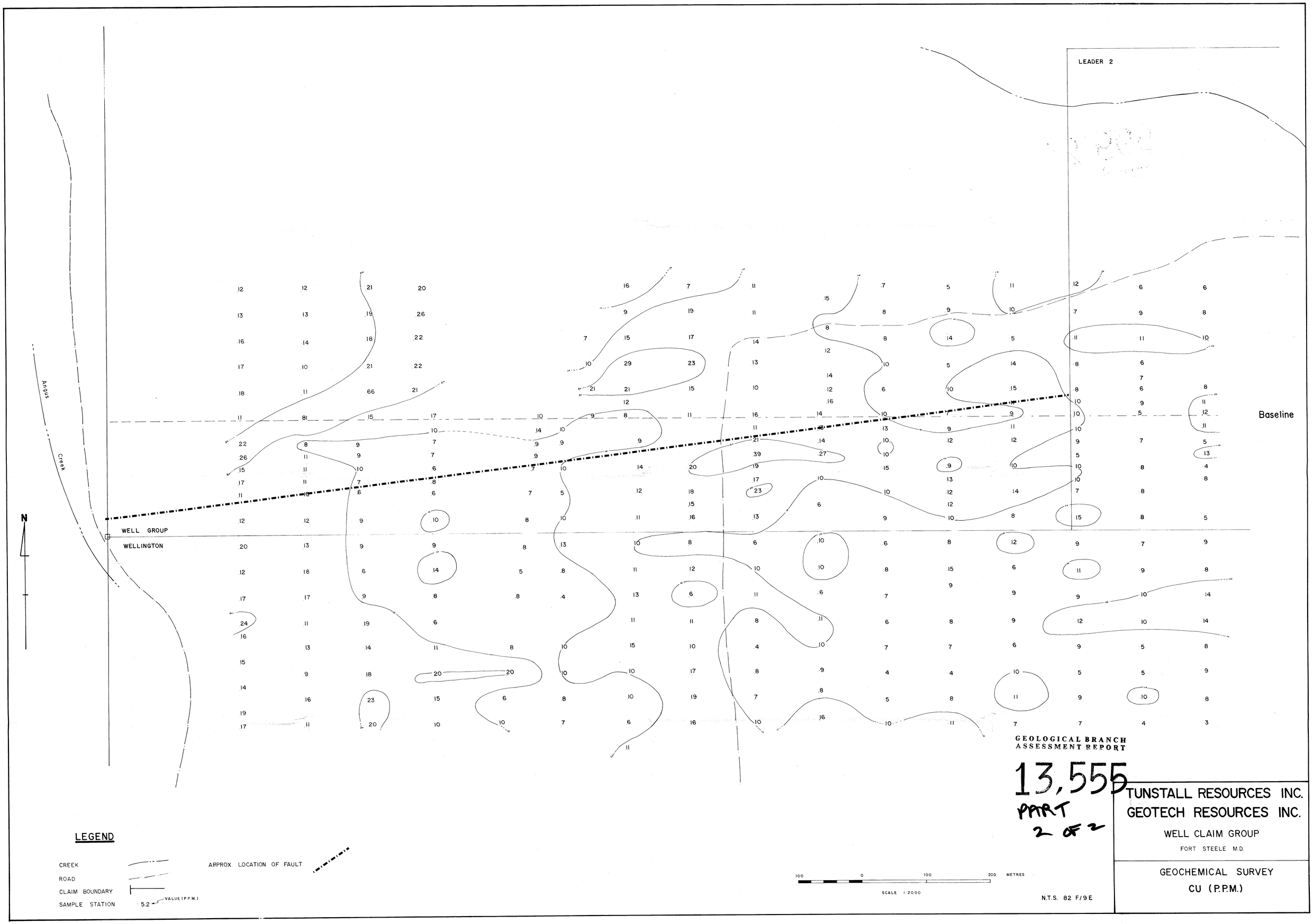
TUNSTALL RESOURCES INC.
GEOTECH RESOURCES INC.

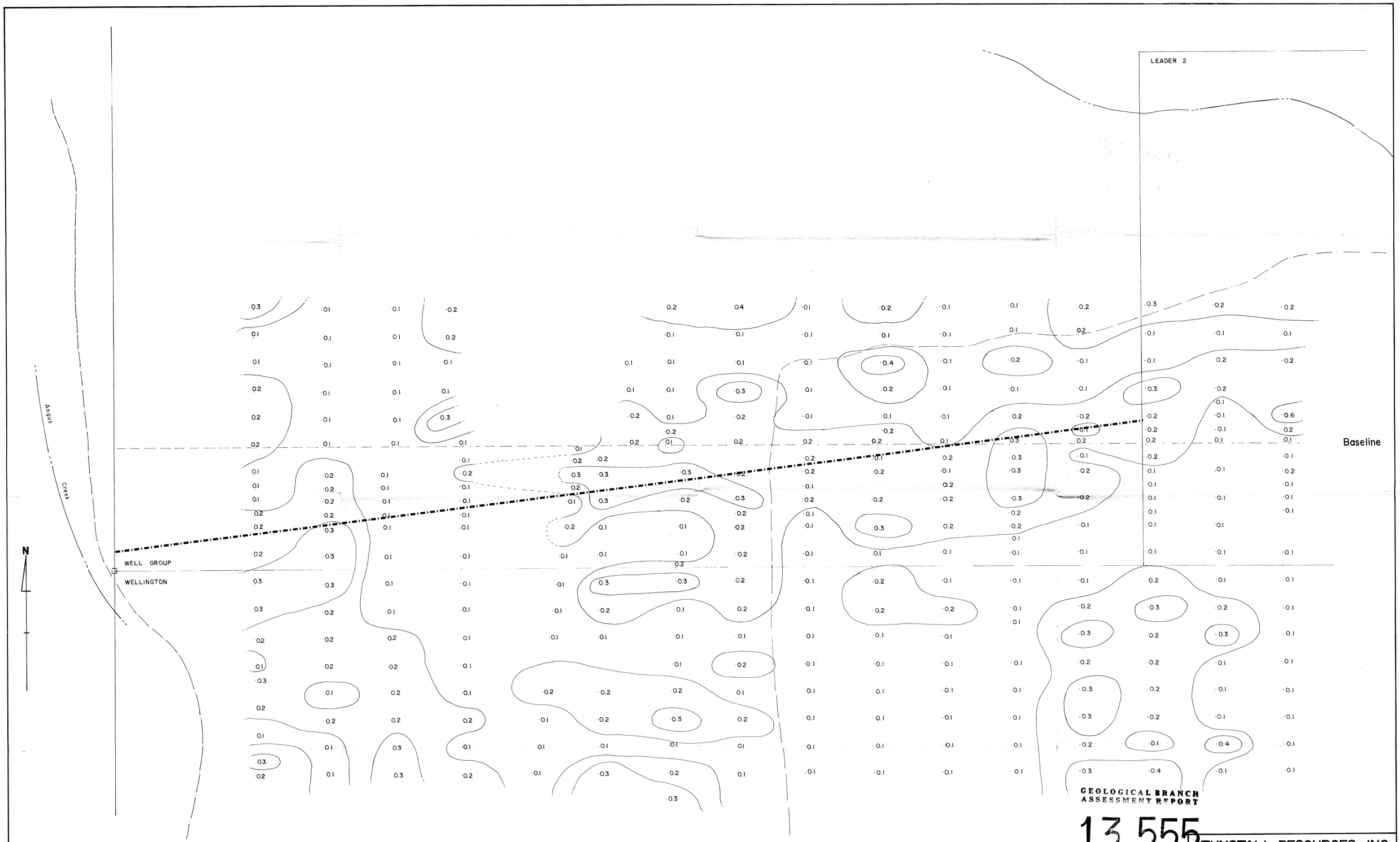
WELL CLAIM GROUP

FORT STEELE M.D.

GEOCHEMICAL SURVEY

AS (P.P.M.)


LEADER 2
Baseline
Angus Creek
N
WELL GROUP
WELLINGTON
LEGEND
CREEK
ROAD
CLAIM BOUNDARY
SAMPLE STATION
5.2
VALUE (P.P.M.)
APPROX. LOCATION OF FAULT
100 0 100 200 METRES
SCALE 1:2000
N.T.S. 82 F/9E
GEOLOGICAL BRANCH
ASSESSMENT REPORT
13,555
PART
2 OF 2
TUNSTALL RESOURCES INC.
GEOTECH RESOURCES INC.
WELL CLAIM GROUP
FORT STEELE M.D.
GEOCHEMICAL SURVEY
CU (P.P.M.)



GEOLOGICAL BRANCH
ASSESSMENT REPORT

13,555
PART 2 OF 2

TUNSTALL RESOURCES INC.
GEOTECH RESOURCES INC.

WELL CLAIM GROUP

FORT STEELE M.D.

GEOCHEMICAL SURVEY

AG (P.P.M.)

LEGEND

CREEK

ROAD

CLAIM BOUNDARY

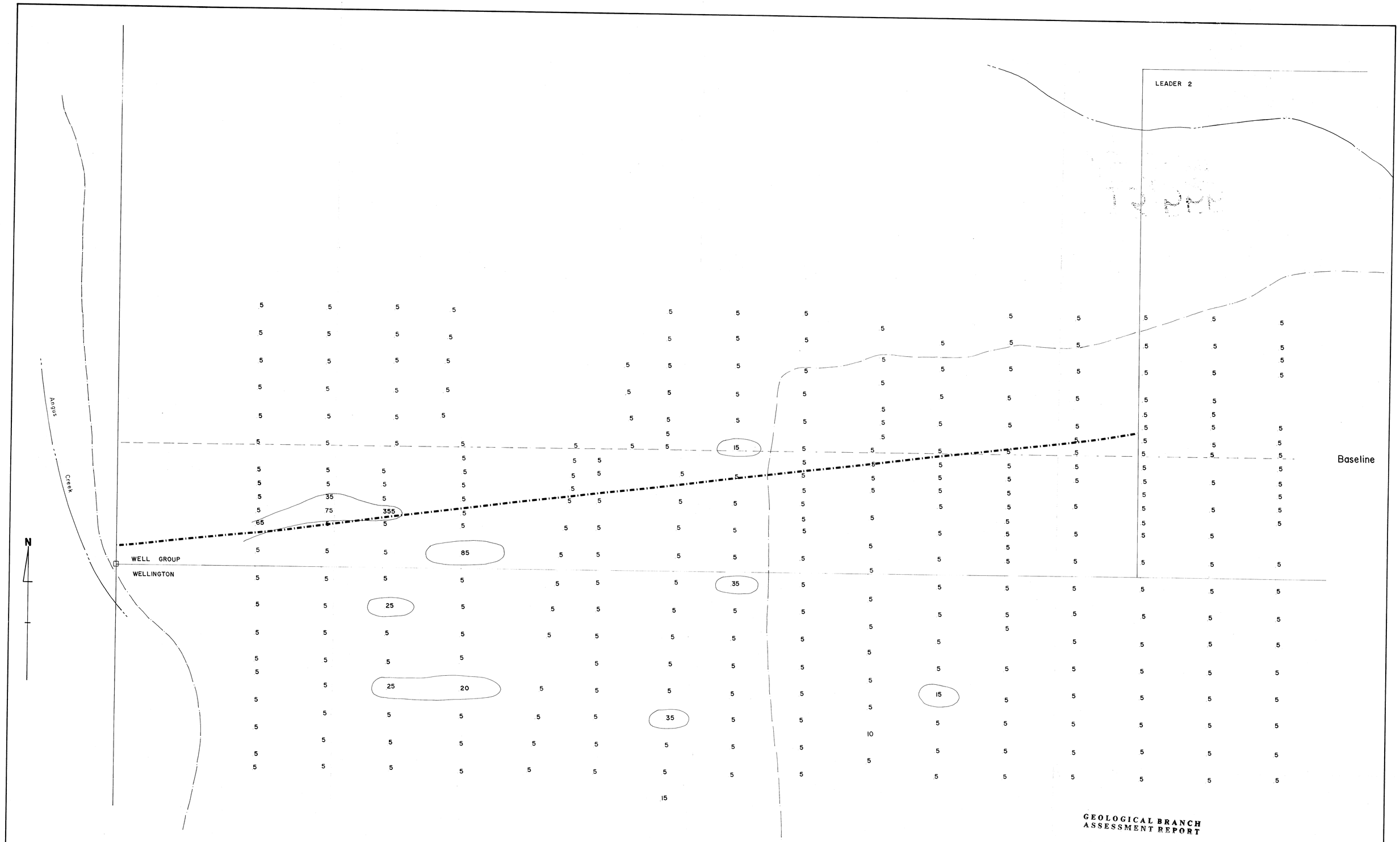
SAMPLE STATION ·5.2 VALUE (P.P.M.)

APPROX. LOCATION OF FAULT

100 0 100 200 METRES

SCALE 1:2000

N.T.S. 82 F/9E



GEOLOGICAL BRANCH
ASSESSMENT REPORT

13,555
PART 2 OF 2

LEGEND

CREEK
ROAD
CLAIM BOUNDARY
SAMPLE STATION 5.2 VALUE (P.P.M.)
APPROX. LOCATION OF FAULT

100 0 100 200 METRES
SCALE 1:2000

N.T.S. 82 F/9E

TUNSTALL RESOURCES INC.
GEOTECH RESOURCES INC.

WELL CLAIM GROUP

FORT STEELE M.D.

GEOCHEMICAL SURVEY
AU (P.P.B.)