85-804 – 14027

9/86

GEOCHEMICAL REPORT
ON THE SHEEP CREEK SOUTH GROUP
NELSON MINING DIVISION, B.C.

Latitude: 49°07'N
Longitude: 117°09'W

NTS 82F-3E

Mineral Claims: Yellowstone, Vixen, Independence 1

Reverted Crown Grants: Independence, Independence Fr., Buster Fr., Amco 35, Amco 36, Margaret, King #3, Lucky George, Amco 41 Fr., Amco 40 Fr., Gold Crown Fr., Amco 16 Fr.,

Crown Grants: Twilight Fr., Happy Jean, Fraction #1 Fr., Fractional #2 Fr., Peggy, Pat Fr., Success, Margaret Fr., Henry Fr., Alexandra, Placer Fr., Edward 7, Burlington Fr., Pat, Bullion, Bruhn #2, Vernon, Silver Tip Fr., Last Dollar Fr., Standard, Queen, Niagra, Lewiston, Struggle, Ore Hill #3, Ore Hill, Royal Ann Fr., Dixie, Royal Ann #1, Royal Ann, Queen Ann #1, Queen Ann Fr.,

Owner/Operator: Goldrich Resources Inc.
Vancouver, B.C.

Author: B. H. Meyer, P. Geol.

Date Submitted: October 23, 1985

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MAPS

GEOCHEMICAL REPORT
ON THE SHEEP CREEK SOUTH GROUP
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SUMMARY

The property is underlain by a succession of Lower Cambrian quartzitic, argillaceous, and calcareous sediments trending north-south, which are isoclinally folded and overturned. A series of auriferous pyrite-bearing quartz veins emplaced along northeast trending fissures are situated within the quartzitic members of the sediments. Northeast trending veins cutting limestone also contain galena-sphalerite mineralization. The property contains the underground workings of the former producing Sheep Creek gold mine, and the Sumit and Ore Hill mines.

Soil geochemistry has resulted in a significant gold-silver-lead-zinc anomaly situated at the western edge of the surveyed area. The anomaly is open to the south and west, and ties into a known anomaly of similar concentrations to the north. This zone reflects the location of mineralization present in the Ore Hill and Sumit mines.

A weak lead anomaly is situated near the base line at the south edge of the surveyed area. The zone appears to trend north-south near the quartzite-limestone contact.

A number of small weak lead anomalies are situated in the eastern part of the surveyed area near the headwaters of McArthur Creek. The area is underlain by quarzite.

Further exploratory work consisting of mapping and prospecting has been recommended for the area underlying the Independence 1 mineral claim. Mapping and sampling of the Ore Hill and Sumit mines plus the surrounding area, and in particular the headwaters of Bennett Creek, is also recommended.

BRITISH COLUMBIA

MINING DIVISIONS

Gold Commissioner's office–●

INDEX MAP

Figure 1

SHEEP CREEK SOUTH GROUP

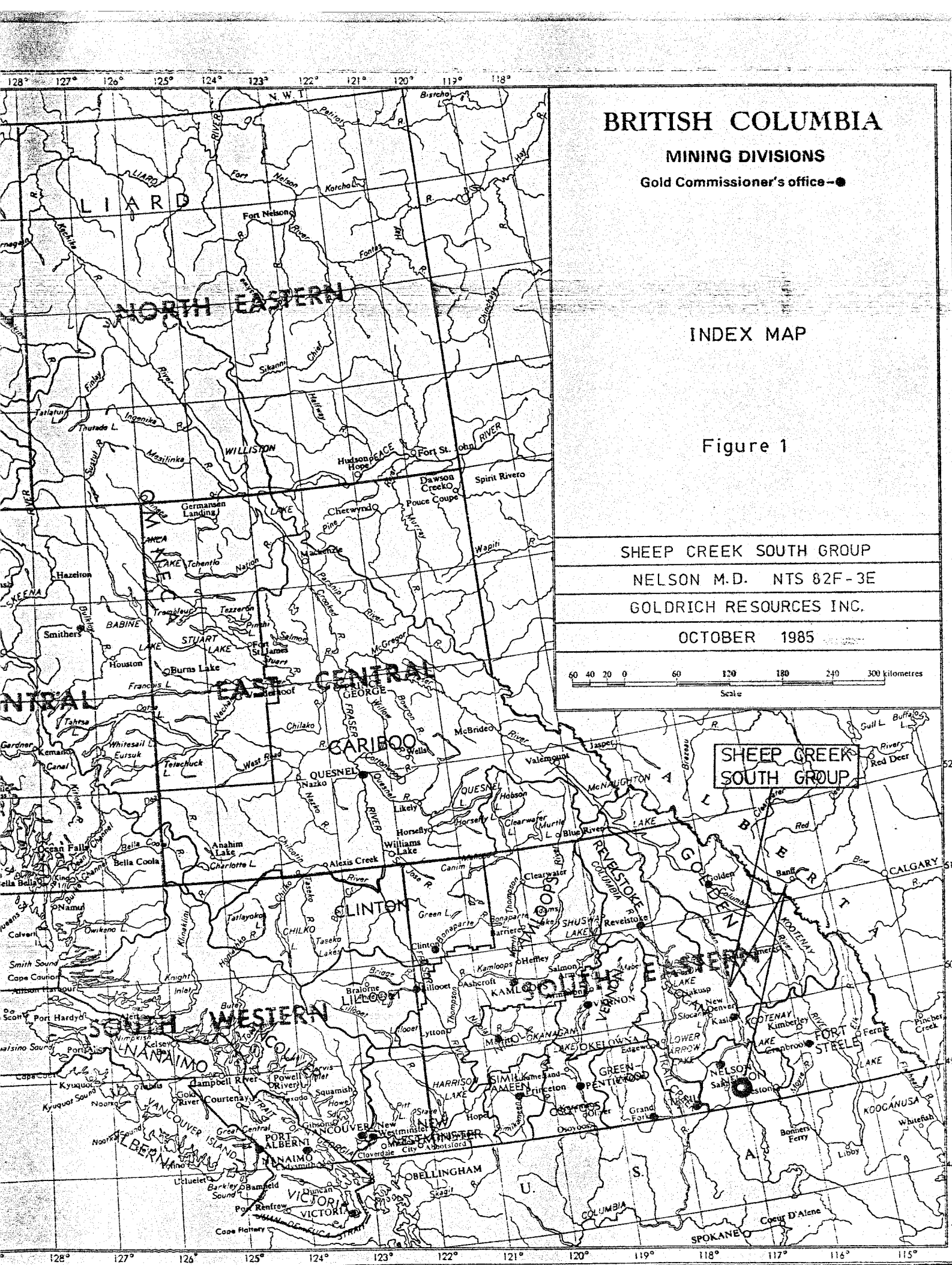
NELSON M.D. NTS 82F-3E

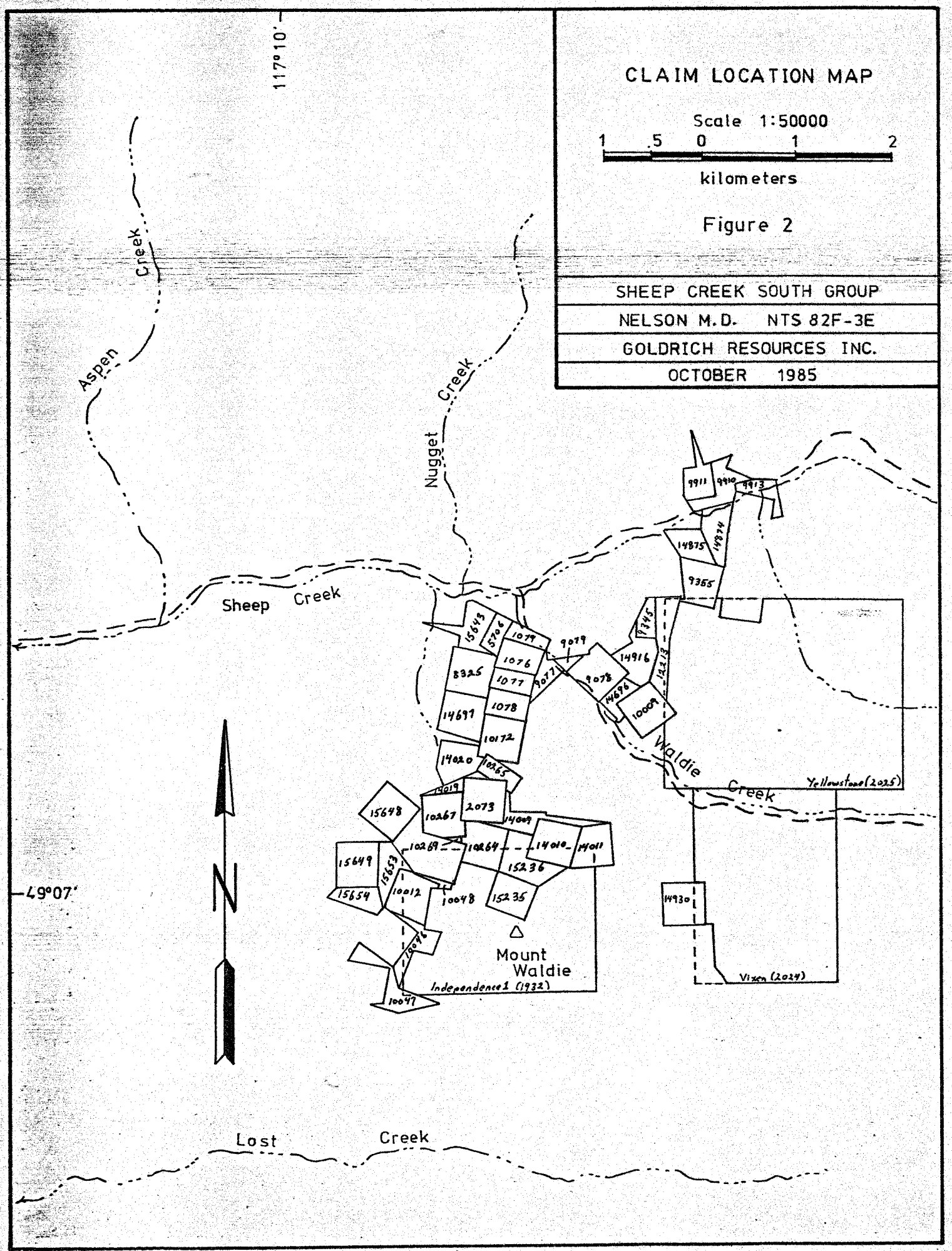
GOLDRICH RESOURCES INC.

OCTOBER 1985

60 40 20 0 60 120 180 240 300 kilometres

Scale




CLAIM LOCATION MAP
Scale 1:50000
1 .5 0 1 2
kilometers
Figure 2
SHEEP CREEK SOUTH GROUP
NELSON M.D. NTS 82F-3E
GOLDRICH RESOURCES INC.
OCTOBER 1985
117°10'
49°07'
N
Aspen Creek
Nugget Creek
Sheep Creek
Waldie Creek
Lost Creek
Mount Waldie
Independence 1 (1932)
Yellowstone (2025)
Vixen (2024)
9911
9910
9913
14874
14875
9355
9345
14916
14813
9078
9079
9077
14896
10009
15643
5706
1079
1076
8325
1077
1078
14697
10172
14020
10865
14019
15648
10267
2073
14009
15649
15653
10269
10264
14010
14011
15236
15654
10012
10048
15235
14930
10047

INTRODUCTION

An exploration program was conducted in the fall of 1985 in the vicinity of the former gold producing Sheep Creek and Ore Hill mines of the Sheep Creek gold camp. The program consisted of geochemical soil sampling along compassed and chained grid lines.

Location and Access (Latitude 49°07'N Longitude 117°09'W)

The property is situated in the Nelson Range of the Selkirk Mountains, 12 kilometers southeast of the town of Salmo. It occupies the top of Mount Waldie, extending north to Waldie Creek valley. Access from Salmo is along the old part of Hwy #3, 6 kilometers south to the mouth of Sheep Creek. The property, which 9 kilometers east, near the junction of Sheep and Waldie Creeks, can be reached by a good 2-wheel drive gravel road. A 4-wheel drive road connecting the Ore Hill mine, near the top of Mount Waldie, with the Sheep Creek mine below, is washed out and inaccessible. The property is approximately 55 road kilometers east of Trail.

Most of the property is situated on the steep north slope of Mount Waldie, with the vertical elevation increasing from 3200 feet(975 m.) to 7300 feet(2225 m.) elevation at the summit. At lower elevations, a thick cover of glacial drift is common, with few bedrock exposures. Near the summit, much of the area is covered by talus slopes and numerous small rock cliffs. Vegetation consists of a mature cedar, hemlock, and spruce forest which grades into scattered dwarf trees near Mount Waldie summit. The climate is cool temperate, with an average annual precipitation of 60 to 100 centimeters. There is a heavy accumulation of snow in the winter months.

Property and Ownership

The Sheep Creek South Group consists of the following mineral claims, reverted crown grants and crown grants, all of which are 100 percent owned by Goldrich Resources Inc. of Vancouver, B.C. Besides owning the mineral rights on the crown grants, Goldrich also owns the surface rights of the Queen and Burlington Fraction crown grants.

Property and Ownership Cont'd

Crown Grant	Lot Number	Hectares
Twilight Fr.	9910	13.66
Happy Jean	9911	11.87
Fraction #1 Fr.	14874	16.10
Fractional #2 Fr.	14875	15.23
Peggy	9355	18.13
Pat Fr.	12213	15.67
Success	10009	20.90
Margaret Fr.	14696	7.55
Henry Fr.	14916	15.30
Alexandra	9078	20.79
Placer Fr.	9079	3.13
Edward 7	9077	7.37
Burlington Fr.	1079	6.27
Pat	5706	7.85
Bullion	8325	20.53
Bruhn #2	14697	20.70
Vernon	14020	15.63
Silver Tip Fr.	14019	4.51
Last Dollar Fr.	10269	0.25
Standard	10267	18.63
Queen	1076	13.94
Niagra	1077	10.02
Lewiston	1078	12.58
Struggle	10172	20.25
Ore Hill #3	10265	8.70
Ore Hill	2073	20.90
Royal Ann Fr.	14009	12.47
Dixie	10264	18.45
Royal Ann #1	14011	16.75
Royal Ann	14010	20.90
Queen Ann #1	15235	17.38
Queen Ann Fr.	15236	20.86

Reverted Crown Grant	Lot Number	Record Number	Hectares	Expiry Date
Independence	10012	1761	19.00	June 19, 1987

Property and Ownership Cont'd

Reverted Crown Grant	Lot Number	Record Number	Hectares	Expiry Date
Independence Fr.	10048	1761	1.98	June 19, 1987
Buster Fr.	10046	1767	11.64	"
Amco 35	15648	2205	20.90	Mar. 13, 1987
Amco 36	15649	2204	20.90	Mar. 10, 1987
Margaret	9913	1922	9.06	Aug. 27, 1988
King #3	14930	2593	20.90	Feb. 17, 1987
Lucky George	9345	2592	6.77	Feb. 15, 1988
Amco 41 Fr.	15654	3388	11.28	Aug. 23, 1987
Amco 40 Fr.	15653	3388	12.15	"
Gold Crown Fr.	10047	3389	15.68	"
Amco 16 Fr.	15643	1781	14.79	June 24, 1987

Located Mineral Claim	Record Number	Hectares	Expiry Date
Yellowstone (20 units)	2025	500	Nov. 20, 1986
Vixen (12 units)	2024	300	"
Independence 1 (12 units)	1932	300	Sept 25, 1986

History

Gold mineralization was first discovered in the Sheep Creek gold camp in 1896 in the Yellowstone and Queen veins. In 1901, the Ore Hill and Sumit showings were discovered. By 1912, all the important producing veins known to date had been found, including the Kootenay Belle and Reno veins. A number of mines operated in the area until 1916, when rising costs resulted in temporary closures.

An increase in gold prices in 1932 resulted in a resurgence of mining activity in the area, and in the installation of milling operations at the Reno, Motherlode, Kootenay Belle and Sheep Creek mines. Mining activity continued in the Sheep Creek camp until the early 1940's when rising costs and the outbreak of war resulted in mine closures.

Production figures for individual mines situated within the Sheep Creek South Group are presented below. These figures are taken from Mathews(1953) and represent company estimates of tonnages and average grade of ore extracted from veins.

History Cont'd

	Ore(tons)	Gold(ozs)	Silver(ozs)	Lead(lbs)	Zinc(lbs)
Sheep Creek Mine	719,320	303,711	100,182	-----	-----
Ore Hill Mine	3,669	2,849	5,415	186,940	166,784
Sumit Mine	1,205	870	1,218	30,264	28,634

A 1970 report written by E. Thompson for J.A.C. Ross and Associates Ltd.(then owner of the Sheep Creek Mine claims), stated that an estimated 59,586 tons of proven and probable ore reserves grading 0.285 oz/ton gold exists within the Sheep Creek Mine workings.

A dewatering and mine rehabilitation program was carried out by Goldbelt Mines Inc. in 1980 at the Sheep Creek Mine. C. Sampson concluded in a report that further mine rehabilitation still necessary could not be justified at the time due to the high costs involved.

A geochemical and geological exploration program was carried out in 1983 by Springlake Resources Ltd. A continuation of the geochemical soil survey was recommended at this time, as there was a positive correlation of gold, silver, lead and zinc values to known mineral occurances.

Present Activity

A total of 4 days was spent conducting a geochemical exploration program on the property between September 3 and September 10, 1985. A 3-man fly camp was established near the old Ore Hill mine, with access provided by helicopter. Due to an early snowstorm, two trips into the property were necessary.

A reference grid was established, and consists of a partially cut base line, which is an extension of the base line established in 1983 by Springlake Resources. The base line starts at 5800 feet(1770 m.) elevation near the north edge of the Dixie crown grant, and extends south at 188° azimuth(subparallel to regional structural trend) for a chained length of 450 meters, ending near the south edge of Dixie 5750 feet(1750 m.) elevation. Flagged tie lines are situated normal to the base line at 90 meter intervals, and are chained to 30 meter station intervals. Tie lines range from 480 to 1530 meters length.

Present Activity Cont'd

A total of 9.2 line kilometers was established(flagged).

Geochemical soil sampling was conducted over the grid area at 30 meter station intervals. A total of 317 samples were collected.

The purpose of the program was to explore, by geochemical means, the southern part of the property, for possible mineralized veins associated with either the limestone hosted veins of the Ore Hill and Sumit mines, or the quartzite hosted veins of the Sheep Creek mine.

GEOLOGY

The Sheep Creek South Group is situated within the Kootenay Arc structural province, which is a belt of highly deformed volcanic and sedimentary rock extending from the Revelstoke area southwards along Kootenay Lake, and southwest into the United States. The suite of rocks within this belt represent a miogeosynclinal environment.

Locally, the claim area is underlain by Lower Cambrian quartzites of the Quartz Range Formation, which overlie Windermerian(?) sediments of the Three Sisters Formation. The Quartzite Range Formation comprises the lower Nugget Member, which consists of white quartzite, and the upper Navada Member, consisting of white to brownish-grey quartzite with argillaceous interbeds.

The Reno Formation conformably overlies the Quartzite Range Formation. It consists of brownish-grey argillaceous quartzite commonly with thin argillite interbeds.

The uppermost sedimentary unit is the Lower Cambrian Laib Group, which consists of alternating members of limestone and calcareous argillite. Occasionally, the argillite is schistose.

A quartz porphyry dyke trending north-south intrudes the sediments subparallel to bedding. This unit post-dates northeast-southwest trending faults.

Geology Cont'd

Structurally, the sediments are folded into a north-south trending isoclinal syncline with isoclinal anticlines overturned to the west, situated both east and west.

A series of ten gold-bearing quartz veins trending northeast-southwest and dipping steeply south constitute the economic significance of the Sheep Creek mine. These veins extend up to 1,000 meters in length. Mineralization consists of auriferous pyrite within veins cutting competent quartzite(Nugget and Navada members), and galena-sphalerite-pyrite in veins cutting limestone(Ore Hill and Sumit mines). Vein width is generally less than 1.2 meters.

The mineralized veins may be offset by north trending normal faults dipping east. A flat-lying post-vein fault is thought to be responsible for a 60 meter displacement in the Ore Hill mine.

GEOCHEMISTRY

A total of 317 soil samples were collected at 30 meter intervals along 8 tie lines spaced 90 meters apart. Tie lines are numbered 18+00S, 18+90S, and so on to 24+30S. Figure 3 shows sample locations with gold and lead values plotted, using a 1:5000 scale map.

All soil samples were analyzed by Vangeochem Lab Ltd. of Vancouver, B.C. for multi-element abundances. The detection method used was a hot acid extraction and ICAP(induction couple argon plasma) emission spectrometry with values recorded in parts per million or percentage. The gold detection method was by atomic absorption spectrometry, with values recorded in parts per billion. The particle size fraction used for analysis was minus 80 mesh.

The area sampled consists of a thick layer of overburden within creek valleys, and a thin layer on mountain slopes and ridges, where bedrock exposure is abundant and talus slopes common. Samples were collected from the B Horizon at a depth of approximately 18 centimeters. Occasionally, a combination of A and C Horizons have been sampled where

Geochemistry Cont'd

only a thin imature soil layer exists.

The geochemistry map shows gold concentrations in parts per billion with anomalous values being 30 ppb and greater. This threshold value was chosen arbitrarily and coincides with that used by Springlake Resources in their 1983 exploration program. Lead values are plotted in parts per million, with anomalous concentrations arbitrarily chosen to be 65 ppm and greater. This too is the same threshold value used by Springlake. Anomalous silver and zinc concentrations are associated with those of gold and lead, and have not been plotted on the map.

A significant gold-silver-lead-zinc anomaly situated between lines 20+70S and 23+40S at the western edge of the grid is open to the south and west, and ties into a predetermined anomaly to the north. This zone reflects the probable position of the Ore Hill and Sumit workings, although the area has not been mapped in detail yet. The highest gold value in this zone is 500 ppb. This zone is situated within the Laib Group limestone, which is a favorable host rock for argentiferous galena-sphalerite-auriferous pyrite mineralization within fissures.

A weak lead anomaly is situated on lines 23+40S to 24+30S just east of the base line, and is open to the south. The zone has a width of approximately 30 meters and appears to trend north-south. Geologically it is situated near the Reno(quartzite) and Laib(limestone) contact on the east limb of the syncline. Silver and zinc values are low.

A number of small weak lead anomalies are situated within the eastern part of the grid near the headwaters of McArthur Creek. Occasionally, weak anomalous silver values are associated. This area is underlain by the Quartzite Range Formation.

Other anomalies present within the sampled area are weak and scattered.

CONCLUSIONS AND RECOMMENDATIONS

The anomalous area near the Ore Hill and Sumit mines remains open to

Conclusions and Recommendations Cont'd

the southwest. Both underground and surface mapping and sampling should be carried out in this area. Also, geochemical soil sampling near the headwaters of Bennett Creek, which is southwest of the Ore Hill mine, should be conducted. The presence of near surface mineralized veins within the Laib limestone should be detectable by this method.

The lead anomalies near the base line and within the eastern part of the grid area are scattered and generally weak. The presence of minor scattered galena mineralization within veins in these areas would explain these anomalies. Prospecting and mapping of veins, with an emphasis on northeast-southwest trending fissures should be carried out in this area.

Prospecting and reconnaissance mapping of the Independence 1 mineral claim should be conducted, as Thompson reports that northeast trending veins are present on both the north and south slopes of Mount Waldie.

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A P P E N D I C E S

VANGEOCHEM LAB LIMITED

MAIN OFFICE
1521 PEMBERTON AVE.
NORTH VANCOUVER, B.C. V7P 2S3
(604) 986-5211 TELEX: 04-352578

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

REPORT NUMBER: 85-35-008 JOB NUMBER: 85405 **GOLDRICH RESOURCES INC.**

SAMPLE #	Au ppb
18+00S 5+40E	20
18+00S 5+70E	20
18+00S 6+00E	20
18+00S 6+30E	20
18+00S 6+60E	5
18+00S 6+90E	10
18+00S 7+20E	5
18+00S 7+50E	10
18+00S 7+80E	nd
18+00S 8+10E	nd
18+00S 8+40E	20
18+00S 8+70E	nd
18+00S 9+00E	nd
18+00S 9+30E	5
18+00S 9+60E	nd
18+00S 9+90E	5
18+00S 10+20E	5
18+90S 5+40E	10
18+90S 5+70E	10
18+90S 6+00E	10
18+90S 6+30E	15
18+90S 6+60E	10
18+90S 6+90E	nd
18+90S 7+20E	5
18+90S 7+50E	15
18+90S 7+80E	10
18+90S 8+10E	15
18+90S 8+40E	5
18+90S 8+70E	5
18+90S 9+00E	5
18+90S 9+30E	10
18+90S 9+60E	10
18+90S 9+90E	nd
18+90S 10+20E	nd
19+80S BL	10
19+80S 0+30E	5
19+80S 0+60E	20
19+80S 0+90E	10
19+80S 1+20E	nd
DETECTION LIMIT	5

nd = none detected — = not analysed is = insufficient sample

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SAMPLE #	Au ppb
19+80S 1+50E	5
19+80S 1+80E	10
19+80S 2+10E	15
19+80S 2+40E	10
19+80S 2+70E	nd
19+80S 3+00E	5
19+80S 3+30E	10
19+80S 3+60E	10
19+80S 3+90E	nd
19+80S 4+20E	nd
19+80S 4+50E	nd
19+80S 4+80E	20
19+80S 5+10E	30
19+80S 5+40E	nd
19+80S 5+70E	nd
19+80S 6+00E	5
19+80S 6+30E	5
19+80S 6+60E	nd
19+80S 6+90E	10
19+80S 7+20E	5
19+80S 7+50E	5
19+80S 7+80E	5
19+80S 8+10E	20
19+80S 8+40E	10
19+80S 8+70E	5
19+80S 9+00E	nd
19+80S 9+30E	nd
19+80S 9+60E	nd
19+80S 9+90E	nd
19+80S 10+20E	20
20+70S BL	10
20+70S 0+30E	5
20+70S 0+60E	nd
20+70S 0+90E	10
20+70S 1+20E	10
20+70S 1+50E	nd
20+70S 1+80E	10
20+70S 2+10E	10
20+70S 2+40E	nd
DETECTION LIMIT	5

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SAMPLE #	Au ppb
20+70S 2+70E	nd
20+70S 3+00E	nd
20+70S 3+30E	10
20+70S 3+60E	15
20+70S 3+90E	10
20+70S 4+20E	5
20+70S 4+50E	5
20+70S 4+80E	5
20+70S 5+10E	5
20+70S 5+40E	10
20+70S 5+70E	10
20+70S 6+00E	10
20+70S 6+30E	10
20+70S 6+60E	5
20+70S 6+90E	5
20+70S 7+20E	10
20+70S 7+50E	5
20+70S 7+80E	5
20+70S 8+10E	nd
20+70S 8+40E	nd
20+70S 8+70E	nd
20+70S 9+00E	nd
20+70S 9+30E	nd
20+70S 9+60E	nd
20+70S 9+90E	nd
20+70S 10+20E	nd
20+70S 0+30W	nd
20+70S 0+60W	nd
20+70S 0+90W	5
20+70S 1+20W	nd
20+70S 1+50W	5
20+70S 1+80W	5
20+70S 2+10W	nd
20+70S 2+40W	nd
20+70S 2+70W	5
20+70S 3+00W	10
20+70S 3+30W	5
20+70S 3+60W	5
20+70S 3+90W	10
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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SAMPLE #	Au ppb
20+70S 4+20W	20
20+70S 4+50W	5
20+70S 4+80W	40
20+70S 5+10W	500
21+60S BL	nd
21+60S 0+30E	5
21+60S 0+60E	nd
21+60S 0+90E	20
21+60S 1+20E	5
21+60S 1+50E	nd
21+60S 1+80E	5
21+60S 2+10E	5
21+60S 2+40E	nd
21+60S 2+70E	nd
21+60S 3+00E	nd
21+60S 3+30E	nd
21+60S 3+60E	nd
21+60S 3+90E	nd
21+60S 4+20E	nd
21+60S 4+50E	nd
21+60S 4+80E	5
21+60S 5+10E	10
21+60S 5+40E	nd
21+60S 5+70E	5
21+60S 6+00E	5
21+60S 6+30E	nd
21+60S 6+60E	nd
21+60S 6+90E	nd
21+60S 7+20E	5
21+60S 7+50E	10
21+60S 7+80E	nd
21+60S 8+10E	5
21+60S 8+40E	20
21+60S 8+70E	nd
21+60S 9+00E	nd
21+60S 9+30E	10
21+60S 9+60E	5
21+60S 9+90E	nd
21+60S 0+30W	nd
DETECTION LIMIT	5

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SAMPLE #	Au ppb
21+60S 0+60W	nd
21+60S 0+90W	nd
21+60S 1+20W	nd
21+60S 1+50W	10
21+60S 1+80W	10
21+60S 2+10W	nd
21+60S 2+40W	nd
21+60S 2+70W	nd
21+60S 3+00W	30
21+60S 3+30W	15
21+60S 3+60W	nd
21+60S 3+90W	10
21+60S 4+20W	20
21+60S 4+50W	nd
21+60S 4+80W	10
21+60S 5+10W	10
22+50S BL	nd
22+50S 0+30E	5
22+50S 0+60E	nd
22+50S 0+90E	nd
22+50S 1+20E	10
22+50S 1+50E	5
22+50S 1+80E	5
22+50S 2+10E	10
22+50S 2+40E	5
22+50S 2+70E	nd
22+50S 3+00E	nd
22+50S 3+30E	nd
22+50S 3+60E	5
22+50S 3+90E	5
22+50S 4+20E	5
22+50S 4+50E	10
22+50S 4+80E	5
22+50S 5+10E	nd
22+50S 5+40E	nd
22+50S 5+70E	5
22+50S 6+00E	10
22+50S 6+30E	5
22+50S 6+60E	5
DETECTION LIMIT	5

nd = none detected — = not analysed is = insufficient sample

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SAMPLE #	Au ppb
22+50S 6+90E	nd
22+50S 7+20E	10
22+50S 7+50E	5
22+50S 7+80E	5
22+50S 8+10E	5
22+50S 8+40E	5
22+50S 8+70E	10
22+50S 9+00E	10
22+50S 9+30E	5
22+50S 9+60E	nd
22+50S 9+90E	nd
22+50S 0+30W	10
22+50S 0+60W	10
22+50S 0+90W	5
22+50S 1+20W	nd
22+50S 1+50W	10
22+50S 1+80W	20
22+50S 2+10W	nd
22+50S 2+40W	5
22+50S 2+70W	10
22+50S 3+00W	nd
22+50S 3+30W	nd
22+50S 3+60W	nd
22+50S 3+90W	nd
22+50S 4+20W	nd
22+50S 4+50W	15
22+50S 4+80W	nd
22+50S 5+10W	nd
23+40S BL	nd
23+40S 0+30E	nd
23+40S 0+60E	nd
23+40S 0+90E	10
23+40S 1+20E	nd
23+40S 1+50E	10
23+40S 1+80E	nd
23+40S 2+10E	10
23+40S 2+40E	10
23+40S 2+70E	10
23+40S 3+00E	5
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

VANGEOCHEM LAB LIMITED

MAIN OFFICE
1521 PEMBERTON AVE.
NORTH VANCOUVER, B.C. V7P 2S3
(604) 986-5211 TELEX: 04-352578

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Au ppb
23+40S 3+30E	5
23+40S 3+60E	10
23+40S 3+90E	10
23+40S 4+20E	nd
23+40S 4+50E	10
23+40S 4+80E	nd
23+40S 5+10E	5
23+40S 5+40E	10
23+40S 5+70E	5
23+40S 6+00E	5
23+40S 6+30E	5
23+40S 6+60E	20
23+40S 6+90E	nd
23+40S 7+20E	5
23+40S 7+50E	nd
23+40S 7+80E	nd
23+40S 8+10E	nd
23+40S 8+40E	10
23+40S 8+70E	5
23+40S 9+00E	nd
23+40S 9+30E	nd
23+40S 0+30W	nd
23+40S 0+60W	10
23+40S 0+90W	10
23+40S 1+20W	10
23+40S 1+50W	15
23+40S 1+80W	nd
23+40S 2+10W	10
23+40S 2+40W	10
23+40S 2+70W	10
23+40S 3+00W	10
23+40S 3+30W	5
23+40S 3+60W	nd
23+40S 3+90W	20
23+40S 4+20W	nd
23+40S 4+50W	10
23+40S 4+80W	10
23+40S 5+10W	20
24+30S BL	nd
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

REPORT NUMBER: 85-35-008 JOB NUMBER: 85405 GOLDRICH RESOURCES INC.

SAMPLE #	Au ppb
24+30S 0+30E	nd
24+30S 0+60E	5
24+30S 0+90E	nd
24+30S 1+20E	nd
24+30S 1+50E	nd
24+30S 1+80E	nd
24+30S 2+10E	nd
24+30S 2+40E	nd
24+30S 2+70E	5
24+30S 3+00E	nd
24+30S 3+30E	10
24+30S 3+60E	nd
24+30S 3+90E	nd
24+30S 4+20E	nd
24+30S 4+50E	nd
24+30S 4+80E	5
24+30S 5+10E	nd
24+30S 5+40E	nd
24+30S 5+70E	nd
24+30S 6+00E	nd
24+30S 6+30E	10
24+30S 6+60E	10
24+30S 6+90E	5
24+30S 7+20E	nd
24+30S 7+50E	10
24+30S 7+80E	nd
24+30S 8+10E	nd
24+30S 8+40E	nd
24+30S 8+70E	nd
24+30S 9+00E	10
24+30S 0+30W	nd
24+30S 0+60W	10
24+30S 0+90W	nd
24+30S 1+20W	nd
24+30S 1+50W	nd
24+30S 1+80W	nd
24+30S 2+10W	nd
24+30S 2+40W	nd
24+30S 2+70W	10
DETECTION LIMIT	5

nd = none detected — = not analysed is = insufficient sample

VANGEOCHEM LAB LIMITED

MAIN OFFICE
1521 PEMBERTON AVE.
NORTH VANCOUVER, B.C. V7P 2S3
(604) 986-5211 TELEX: 04-352578

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Au ppb
24+30S 3+00W	nd
24+30S 3+30W	nd
24+30S 3+60W	nd
24+30S 3+90W	nd
24+30S 4+20W	5

DETECTION LIMIT 5

nd = none detected -- = not analysed is = insufficient sample

VANGEOCHEM LAB LIMITED

MAIN OFFICE: 1521 PEMBERTON AVE. N.VANCOUVER B.C. V7P 2S3 PH:(604)986-5211 TELEX:04-352578
BRANCH OFFICE: 1630 PANDORA ST. VANCOUVER B.C. V5L 1L6 PH:(604)251-5656

ICAP GEOCHEMICAL ANALYSIS

A .5 GRAM SAMPLE IS DIGESTED WITH 5 ML OF 3:1:3 HCL TO HNO3 TO H2O AT 95 DEG. C FOR 90 MINUTES AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR SN,MN,FE,CA,P,CR,MG,BA,PD,AL,NA,K,W,PT AND SR. AU AND PD DETECTION IS 3 PPM.
IS= INSUFFICIENT SAMPLE, ND= NOT DETECTED, -= NOT ANALYZED

COMPANY: GOLDRICH RESOURCES LTD.
ATTENTION: MR. BILL DAY
PROJECT: SHEEP CREEK SOUTH

REPORT#: 85-35-008
JOB#: 85405
INVOICE#: 8986

DATE RECEIVED: 85/09/16
DATE COMPLETED: 85/09/20
COPY SENT TO: GEOSPHERE SERVICES LTD.

ANALYST W. Reeves

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
18+00S 5+40E	.1	2.37	ND	ND	77	ND	.02	.1	12	15	26	2.56	.06	.25	586	1	.04	16	.06	24	ND	ND	ND	ND	9	ND	ND	56
18+00S 5+70E	.2	.76	5	ND	72	ND	.06	.1	5	11	12	2.23	.05	.12	917	ND	.03	7	.05	22	ND	ND	ND	1	9	ND	ND	35
18+00S 6+00E	.2	3.24	ND	ND	146	ND	.09	.4	8	13	14	2.81	.05	.20	488	1	.08	15	.09	16	ND	ND	ND	1	11	ND	4	108
18+00S 6+30E	.4	1.94	ND	ND	71	ND	.02	.1	4	11	13	2.32	.05	.09	121	1	.04	7	.02	20	ND	ND	ND	1	4	ND	ND	39
18+00S 6+60E	.3	3.29	ND	ND	63	ND	.05	.2	4	12	11	2.76	.05	.10	202	1	.05	6	.05	23	ND	ND	ND	1	7	ND	ND	41
18+00S 6+90E	.1	1.04	ND	ND	91	ND	.05	.2	9	13	31	2.11	.05	.12	2455	1	.03	8	.07	26	ND	ND	ND	ND	8	ND	ND	43
18+00S 7+20E	.1	1.83	ND	ND	68	ND	.03	.2	10	13	26	2.36	.06	.20	1273	1	.04	12	.13	17	ND	ND	ND	ND	10	ND	ND	54
18+00S 7+50E	.5	1.05	7	ND	42	ND	.03	.3	4	9	9	2.39	.05	.07	91	1	.03	4	.03	32	ND	ND	ND	1	6	ND	ND	22
18+00S 7+80E	.3	.91	6	ND	36	ND	.04	.2	4	13	8	2.23	.06	.20	109	1	.03	8	.04	25	ND	ND	ND	1	6	ND	ND	31
18+00S 8+10E	.2	.94	ND	ND	43	ND	.04	.4	5	18	10	2.07	.06	.32	147	1	.03	13	.02	19	ND	ND	ND	ND	5	ND	ND	29
18+00S 8+40E	.4	1.18	6	ND	42	ND	.04	1.0	5	19	13	3.72	.07	.22	164	1	.08	8	.05	26	ND	ND	3	1	5	ND	ND	33
18+00S 8+70E	.4	4.61	ND	ND	37	ND	.03	.4	4	18	29	3.50	.06	.15	62	1	.07	7	.04	20	ND	ND	ND	1	4	ND	16	21
18+00S 9+00E	.4	.86	6	ND	31	ND	.02	.3	4	16	16	2.13	.05	.16	421	1	.04	7	.08	20	ND	ND	ND	1	4	ND	ND	30
18+00S 9+30E	.1	2.08	ND	ND	31	ND	.04	.3	12	11	40	1.35	.04	.10	267	1	.01	5	.06	21	ND	ND	ND	ND	5	ND	ND	25
18+00S 9+60E	.2	1.94	ND	ND	103	ND	.09	.4	14	9	16	1.49	.07	.10	347	1	.01	9	.03	18	ND	ND	ND	1	9	ND	ND	30
18+00S 9+90E	.6	.92	3	ND	58	ND	.12	.2	7	14	14	2.52	.07	.18	1119	1	.04	7	.07	17	ND	ND	ND	1	13	ND	ND	43
18+00S 10+20E	.1	.32	4	ND	37	ND	.01	.2	1	5	9	.45	.02	.02	28	1	.01	3	.06	28	ND	ND	ND	ND	4	ND	ND	11
18+90S 5+40E	.2	2.37	ND	ND	78	ND	.02	.2	11	16	31	2.66	.08	.30	300	1	.03	18	.06	21	ND	ND	ND	1	11	ND	ND	43
18+90S 5+70E	.2	.94	ND	ND	70	ND	.05	.1	6	10	18	2.23	.07	.08	676	ND	.01	7	.04	16	ND	ND	ND	1	9	ND	ND	28
18+90S 6+00E	.2	2.57	ND	ND	153	ND	.05	.2	12	12	25	2.86	.07	.21	1156	1	.06	16	.08	21	ND	ND	ND	1	10	ND	3	89
18+90S 6+30E	.1	.54	3	ND	303	ND	.09	.7	7	9	17	1.58	.05	.08	5195	1	.02	15	.05	43	ND	ND	ND	1	14	ND	ND	46
18+90S 6+60E	.3	1.30	ND	ND	115	ND	.05	.2	8	15	27	2.74	.07	.20	1432	1	.04	11	.10	24	ND	ND	ND	1	10	ND	ND	55
18+90S 6+90E	.3	.87	11	ND	242	ND	.20	2.3	4	10	17	1.40	.05	.13	1323	ND	.04	8	.06	63	ND	ND	ND	1	19	ND	ND	93
18+90S 7+20E	.2	1.10	5	ND	157	ND	.08	.9	11	13	15	1.92	.07	.18	1115	1	.02	10	.03	37	ND	ND	ND	ND	14	ND	ND	50
18+90S 7+50E	.4	1.26	6	ND	62	ND	.06	.6	4	12	17	1.86	.05	.14	1211	1	.03	7	.17	33	ND	ND	ND	1	8	ND	ND	47
18+90S 7+80E	.3	1.69	ND	ND	51	ND	.05	.3	7	16	15	2.86	.08	.28	421	1	.05	11	.04	30	ND	ND	ND	1	6	ND	ND	46
18+90S 8+10E	.3	1.44	3	ND	54	ND	.07	.8	7	15	12	4.02	.09	.25	242	1	.08	9	.06	44	ND	ND	ND	2	10	ND	ND	41
18+90S 8+40E	.5	.54	6	ND	110	ND	.15	.2	7	9	8	1.72	.06	.10	3105	1	.02	6	.03	22	ND	ND	ND	1	9	ND	ND	47
18+90S 8+70E	.3	1.11	8	ND	68	ND	.03	.5	6	12	12	1.51	.04	.12	882	ND	.02	7	.04	35	ND	ND	ND	1	6	ND	ND	36
18+90S 9+00E	.6	.60	4	ND	22	ND	.02	.1	3	8	6	1.77	.05	.04	67	1	.02	4	.01	16	ND	ND	ND	1	4	ND	ND	35
18+90S 9+30E	.2	.39	6	ND	35	ND	.04	.6	1	7	8	.68	.03	.04	86	ND	.01	3	.07	66	ND	ND	ND	ND	6	ND	ND	25
18+90S 9+60E	.3	1.73	ND	ND	19	ND	.03	.1	3	6	10	1.43	.03	.03	193	1	.02	2	.18	10	ND	ND	ND	1	3	ND	ND	14
18+90S 9+90E	.3	4.61	ND	ND	26	ND	.04	.2	4	9	13	1.72	.04	.08	106	1	.03	6	.09	10	ND	ND	ND	1	5	ND	17	24
18+90S 10+20E	.1	.56	4	ND	58	ND	.01	.1	1	4	7	.53	.01	.04	24	1	.01	2	.06	23	ND	ND	ND	ND	3	ND	ND	10
BL 19+80S	.4	3.55	ND	ND	97	5	1.93	.9	13	37	17	3.54	.16	2.27	2158	ND	.11	30	.16	73	ND	ND	ND	1	44	ND	24	96
18+90S 0+30E	.2	3.01	ND	ND	77	ND	.07	.1	9	25	13	3.08	.08	.51	638	1	.08	18	.07	29	ND	ND	ND	1	9	ND	10	90
18+90S 0+60E	.3	3.27	ND	ND	103	ND	.08	.1	12	26	13	3.20	.09	.59	1027	ND	.08	18	.06	36	ND	ND	ND	1	9	ND	12	99
18+90S 0+90E	.2	2.43	ND	ND	101	ND	.06	.2	9	18	11	2.84	.07	.36	888	1	.07	13	.09	32	ND	ND	ND	1	8	ND	7	88
18+90S 1+20E	.4	1.93	ND	ND	80	ND	.04	.1	7	22	12	2.97	.08	.33	988	ND	.07	14	.10	37	ND	ND	ND	1	7	ND	ND	90

CLIENT: GOLDRICH RESOURCES LTD. JOB#: 85405 PROJECT: SHEEP CREEK SOUTH REPORT: 85-35-008

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
19+80S 1+50E	.4	2.94	ND	ND	65	ND	.04	.4	8	22	13	3.26	.09	.39	356	1	.07	15	.08	29	ND	ND	ND	1	8	ND	ND	97
19+80S 1+80E	.5	1.08	8	ND	34	ND	.03	.1	4	13	7	2.38	.07	.15	337	1	.03	6	.05	28	ND	ND	4	1	5	ND	ND	42
19+80S 2+10E	.3	2.52	ND	ND	43	ND	.02	.1	5	22	12	3.87	.08	.27	245	1	.08	11	.07	29	ND	ND	ND	1	6	ND	ND	57
19+80S 2+40E	.4	2.05	5	ND	79	ND	.05	.5	13	21	22	3.00	.09	.43	428	1	.05	24	.07	31	ND	ND	ND	1	11	ND	ND	77
19+80S 2+70E	.6	1.28	6	ND	106	ND	.05	.2	6	18	11	2.91	.07	.29	209	1	.05	13	.06	30	ND	ND	3	2	10	ND	ND	56
19+80S 3+00E	.4	2.68	ND	ND	69	ND	.05	.1	8	13	14	2.47	.06	.18	795	1	.05	10	.09	23	ND	ND	ND	2	7	ND	ND	62
19+80S 3+30E	.4	2.97	ND	ND	63	ND	.05	.2	7	13	14	2.42	.06	.18	684	1	.05	10	.08	20	ND	ND	ND	2	7	ND	ND	60
19+80S 3+60E	.5	1.94	ND	ND	65	ND	.02	.2	4	22	15	4.36	.11	.30	189	2	.07	8	.05	97	ND	ND	ND	2	18	ND	ND	52
19+80S 3+90E	.3	2.11	ND	ND	70	ND	.02	.1	4	19	20	3.42	.09	.27	345	1	.06	9	.07	53	ND	ND	ND	1	14	ND	ND	55
19+80S 4+20E	.3	1.31	3	ND	62	ND	.02	.2	5	17	17	3.47	.09	.22	201	1	.05	10	.04	41	ND	ND	ND	1	12	ND	ND	41
19+80S 4+50E	.4	2.09	ND	ND	68	ND	.04	.3	9	20	24	3.41	.10	.28	633	1	.05	18	.05	35	ND	ND	ND	1	12	ND	3	62
19+80S 4+80E	.4	2.49	ND	ND	74	ND	.03	.2	10	22	28	3.74	.11	.33	365	1	.06	24	.06	39	ND	ND	ND	1	13	ND	5	71
19+80S 5+10E	.4	2.72	ND	ND	71	ND	.03	.2	9	24	28	3.66	.10	.32	250	1	.06	23	.06	37	ND	ND	ND	1	13	ND	7	68
19+80S 5+40E	.4	1.87	ND	ND	62	ND	.03	.1	5	15	13	2.50	.07	.20	257	1	.03	12	.03	21	ND	ND	ND	1	6	ND	ND	46
19+80S 5+70E	.4	1.43	ND	ND	59	ND	.02	.1	5	15	13	2.49	.07	.19	132	1	.03	12	.02	23	ND	ND	ND	1	7	ND	ND	34
19+80S 6+00E	.4	1.64	ND	ND	62	ND	.03	.2	10	15	33	2.60	.09	.23	517	1	.02	17	.05	20	ND	ND	ND	1	11	ND	ND	43
19+80S 6+30E	.6	1.99	3	ND	80	ND	.05	.4	7	13	15	2.89	.07	.16	810	1	.05	11	.05	22	ND	ND	ND	2	8	ND	ND	58
19+80S 6+60E	.4	2.65	ND	ND	63	ND	.04	.3	8	11	16	2.31	.06	.15	517	1	.04	9	.05	20	ND	ND	ND	1	7	ND	3	53
19+80S 6+90E	.4	3.64	ND	ND	40	ND	.04	.4	5	8	17	1.71	.05	.10	426	1	.03	6	.10	17	ND	ND	ND	1	5	ND	ND	44
19+80S 7+20E	.5	.79	5	ND	43	ND	.02	.1	3	9	9	1.43	.05	.07	91	1	.01	5	.02	23	ND	ND	3	1	6	ND	ND	25
19+80S 7+50E	.5	.45	5	ND	67	ND	.05	.4	3	8	17	.93	.04	.04	338	1	.01	9	.01	16	ND	ND	ND	1	9	ND	ND	30
19+80S 7+80E	.6	1.56	ND	ND	77	ND	.05	.6	2	6	16	1.19	.04	.04	53	1	.01	5	.04	31	ND	ND	ND	1	8	ND	ND	20
19+80S 8+10E	.5	1.48	ND	ND	52	ND	.04	.5	7	19	11	3.81	.09	.32	336	1	.07	12	.05	30	ND	ND	ND	2	7	ND	ND	53
19+80S 8+40E	.3	1.97	ND	ND	67	ND	.05	.7	9	19	21	2.38	.08	.43	338	1	.04	18	.05	27	ND	ND	ND	1	9	ND	ND	50
19+80S 8+70E	.6	1.42	4	ND	48	ND	.05	.3	6	16	12	2.27	.08	.45	332	1	.04	8	.04	33	ND	ND	ND	1	5	ND	ND	38
19+80S 9+00E	.3	1.62	ND	ND	35	ND	.02	.3	4	16	15	2.84	.06	.22	188	1	.05	8	.07	23	ND	ND	ND	1	6	ND	ND	35
19+80S 9+30E	.4	1.36	ND	ND	34	ND	.02	.1	4	15	17	2.56	.07	.20	117	1	.03	7	.05	26	ND	ND	ND	1	4	ND	ND	29
19+80S 9+60E	.5	.55	5	ND	49	ND	.04	.1	5	8	7	1.44	.05	.09	1040	1	.01	4	.03	14	ND	ND	3	1	5	ND	ND	27
19+80S 9+90E	.4	.20	3	ND	20	ND	.02	.3	1	5	5	.71	.03	.02	46	ND	.01	2	.01	20	ND	ND	ND	1	5	ND	ND	12
19+80S 10+20E	.2	.08	8	ND	18	ND	.01	.3	2	4	4	.47	.10	.01	28	1	.01	4	.01	16	ND	ND	ND	ND	2	ND	ND	8
BL 20+70S	.2	2.80	ND	ND	101	ND	.37	.4	19	30	27	3.71	.12	.81	4215	ND	.10	31	.17	45	ND	ND	ND	1	35	ND	11	110
20+70S 0+30E	.3	2.41	ND	ND	85	ND	.07	.3	11	25	12	3.07	.08	.54	772	ND	.07	19	.05	30	ND	ND	ND	1	8	ND	5	74
20+70S 0+60E	.4	2.48	ND	ND	90	ND	.06	.2	8	19	11	2.70	.08	.39	759	1	.06	17	.09	51	ND	ND	ND	1	7	ND	3	92
20+70S 0+90E	.3	1.62	ND	ND	87	ND	.04	.1	9	17	9	2.86	.08	.29	1337	ND	.06	13	.06	30	ND	ND	ND	ND	6	ND	ND	74
20+70S 1+20E	.3	1.84	ND	ND	80	ND	.04	.1	9	18	11	3.01	.09	.33	765	1	.06	15	.07	33	ND	ND	ND	ND	7	ND	ND	86
20+70S 1+50E	.4	2.18	ND	ND	67	ND	.03	.2	9	21	11	3.54	.09	.37	346	1	.06	13	.05	32	ND	ND	ND	1	7	ND	5	79
20+70S 1+80E	.5	2.28	ND	ND	76	ND	.03	.2	8	16	9	2.60	.07	.26	388	1	.05	12	.05	27	ND	ND	ND	1	6	ND	ND	64
20+70S 2+10E	.3	2.71	ND	ND	60	ND	.03	.3	7	18	11	2.55	.07	.30	277	1	.05	14	.07	28	ND	ND	ND	1	6	ND	3	69
20+70S 2+40E	.3	1.72	ND	ND	60	ND	.04	.2	6	20	11	3.61	.08	.30	326	1	.07	12	.05	28	ND	ND	ND	1	7	ND	8	58

CLIENT: GOLDRICH RESOURCES LTD. JOB#: 85405 PROJECT: SHEEP CREEK SOUTH REPORT: 85-35-008

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
20+70S 2+70E	.4	3.76	ND	ND	81	ND	.04	.1	7	18	14	2.42	.05	.24	277	1	.05	14	.13	24	ND	ND	ND	1	7	ND	4	57
20+70S 3+00E	.6	3.54	ND	ND	373	5	.18	.4	13	29	21	3.39	.10	.75	472	1	.06	47	.30	26	ND	ND	ND	2	35	ND	18	86
20+70S 3+30E	.2	3.10	6	ND	56	ND	.04	.1	5	17	14	2.56	.05	.21	487	1	.06	9	.11	23	ND	ND	ND	1	6	ND	4	59
20+70S 3+60E	.5	3.90	ND	ND	45	ND	.04	.1	4	14	14	2.84	.05	.16	133	1	.06	5	.07	51	ND	ND	ND	1	6	ND	11	52
20+70S 3+90E	.2	2.30	ND	ND	60	ND	.04	.1	8	21	20	3.02	.07	.33	656	1	.06	20	.05	25	ND	ND	ND	1	10	ND	ND	74
20+70S 4+20E	.3	1.24	5	ND	54	ND	.08	.4	5	11	17	2.12	.04	.13	587	1	.04	6	.04	24	ND	ND	ND	1	8	ND	ND	45
20+70S 4+50E	.1	2.78	ND	ND	56	ND	.02	.2	6	16	16	2.67	.06	.23	230	1	.04	12	.05	23	ND	ND	ND	1	7	ND	ND	41
20+70S 4+80E	.2	3.94	ND	ND	60	ND	.06	.1	7	13	17	2.04	.05	.22	317	1	.03	12	.08	24	ND	ND	ND	1	7	ND	10	41
20+70S 5+10E	.2	.71	4	ND	48	ND	.05	.1	3	13	9	1.93	.05	.11	140	1	.01	6	.03	26	ND	ND	ND	1	8	ND	ND	33
20+70S 5+40E	.2	1.49	ND	ND	92	ND	.02	.1	6	15	11	2.28	.06	.22	655	1	.02	11	.04	26	ND	ND	ND	1	8	ND	ND	39
20+70S 5+70E	.1	1.09	ND	ND	179	ND	.04	.4	9	13	23	2.45	.06	.11	9146	1	.03	11	.06	23	ND	ND	ND	1	9	ND	ND	63
20+70S 6+00E	.3	1.37	9	ND	67	ND	.07	.1	7	13	12	2.84	.06	.15	1395	1	.05	9	.06	24	ND	ND	3	1	8	ND	ND	58
20+70S 6+30E	.1	1.46	6	ND	135	ND	.13	.7	7	13	13	2.07	.05	.22	1748	1	.05	9	.06	43	ND	ND	ND	1	15	ND	ND	84
20+70S 6+60E	.1	.83	8	ND	92	ND	.14	1.4	4	12	17	1.30	.03	.19	511	ND	.05	9	.10	282	ND	ND	3	1	14	ND	ND	124
20+70S 6+90E	.1	2.05	3	ND	110	ND	.09	.5	4	13	18	1.94	.03	.20	632	1	.05	10	.10	27	ND	ND	ND	1	12	ND	ND	62
20+70S 7+20E	.2	1.71	6	ND	68	ND	.06	.4	5	14	12	2.72	.05	.18	217	1	.06	8	.03	31	ND	ND	ND	1	6	ND	ND	44
20+70S 7+50E	.1	.45	7	ND	115	ND	.29	.6	3	9	11	1.05	.04	.09	249	ND	.02	5	.04	39	ND	ND	ND	1	21	ND	ND	39
20+70S 7+80E	.9	.61	7	ND	74	ND	.03	.3	2	8	8	.89	.09	.08	65	ND	.01	5	.02	23	ND	ND	6	ND	6	ND	ND	21
20+70S 8+10E	.1	1.16	8	ND	88	ND	.10	.5	12	5	10	.69	.01	.10	348	ND	.01	6	.13	69	ND	ND	ND	ND	14	ND	ND	40
20+70S 8+40E	.1	2.45	ND	ND	40	ND	.09	.3	6	21	14	3.24	.08	.37	253	1	.06	16	.04	22	ND	ND	ND	1	8	ND	ND	57
20+70S 8+70E	.1	1.78	ND	ND	64	ND	.04	.2	6	17	63	2.32	.06	.45	217	1	.04	11	.03	18	ND	ND	ND	1	8	ND	ND	29
20+70S 9+00E	1.0	.75	10	ND	35	ND	.02	.8	2	10	67	1.41	.02	.09	67	1	.02	5	.06	25	ND	ND	ND	ND	4	ND	ND	24
20+70S 9+30E	.1	1.02	3	ND	73	ND	.07	.1	8	11	7	1.68	.05	.24	1184	ND	.03	8	.06	17	ND	ND	ND	ND	8	ND	ND	39
20+70S 9+60E	.2	1.35	3	ND	59	3	.12	.4	7	20	10	2.41	.06	.72	510	ND	.06	13	.07	12	ND	ND	ND	1	11	ND	ND	51
20+70S 9+90E	.1	.93	5	ND	39	ND	.06	.3	18	10	17	1.52	.03	.18	566	ND	.03	11	.10	29	ND	ND	ND	ND	8	ND	ND	27
20+70S 10+20E	.1	1.26	8	ND	39	ND	.02	.3	1	4	18	.53	.01	.05	47	1	.01	2	.15	24	ND	ND	ND	ND	4	ND	ND	14
20+70S 0+30W	.1	3.85	ND	ND	64	ND	.45	.6	15	37	15	3.86	.10	1.60	1431	ND	.12	33	.10	53	ND	ND	ND	1	17	ND	28	114
20+70S 0+60W	.1	4.19	ND	ND	99	ND	.19	.5	13	29	23	2.98	.07	1.07	363	ND	.09	28	.11	38	ND	ND	ND	1	12	ND	23	121
20+70S 0+90W	.1	2.15	ND	ND	99	ND	.20	.3	9	21	10	2.63	.05	.44	1211	ND	.07	14	.10	25	ND	ND	ND	1	13	ND	ND	94
20+70S 1+20W	.7	1.19	ND	ND	79	ND	.06	.1	6	14	6	1.73	.10	.27	527	1	.03	10	.05	26	ND	ND	6	ND	6	16	ND	57
20+70S 1+50W	.1	1.22	ND	ND	172	ND	.23	.5	7	14	14	1.81	.04	.19	3848	ND	.05	9	.09	28	ND	ND	ND	ND	12	ND	ND	80
20+70S 1+80W	.1	2.54	ND	ND	118	ND	.54	.4	11	25	15	2.69	.09	.60	1141	ND	.06	22	.07	25	ND	ND	ND	ND	22	ND	8	81
20+70S 2+10W	.1	2.57	ND	ND	57	ND	.53	.6	7	22	22	2.19	.08	.42	190	ND	.03	17	.07	30	ND	ND	ND	ND	19	ND	ND	72
20+70S 2+40W	.1	2.50	ND	ND	98	ND	.74	.4	10	27	19	2.80	.12	.79	1396	ND	.04	24	.16	37	ND	ND	ND	ND	28	ND	4	110
20+70S 2+70W	.1	2.09	ND	ND	106	ND	.22	.2	8	24	12	3.04	.08	.49	490	ND	.07	16	.06	46	ND	ND	ND	1	18	ND	ND	93
20+70S 3+00W	.1	1.90	ND	ND	84	ND	.08	.2	9	22	13	2.67	.09	.54	367	ND	.06	20	.05	37	ND	ND	ND	ND	14	ND	ND	85
20+70S 3+30W	.1	2.24	ND	ND	121	ND	.25	.5	19	21	14	4.09	.14	.45	1378	ND	.09	15	.10	26	ND	ND	ND	ND	21	ND	ND	75
20+70S 3+60W	.1	.88	ND	ND	92	ND	.09	.9	4	11	15	1.34	.02	.13	197	ND	.02	8	.06	26	ND	ND	ND	ND	11	ND	ND	48
20+70S 3+90W	.1	1.98	ND	ND	55	ND	.11	.1	8	18	10	3.12	.08	.32	204	ND	.05	14	.04	28	ND	ND	ND	1	13	ND	ND	51

CLIENT: GOLDRICH RESOURCES LTD. JOB#: 85405 PROJECT: SHEEP CREEK SOUTH REPORT: 85-35-008

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
20+70S 4+20W	.9	2.32	3	ND	60	ND	.41	1.2	9	20	13	2.43	.09	.39	1197	1	.08	14	.06	125	ND	ND	ND	1	16	ND	ND	191
20+70S 4+50W	1.0	2.53	5	ND	66	ND	.45	1.4	10	22	15	2.63	.11	.44	1200	1	.09	14	.06	146	ND	ND	ND	1	17	ND	ND	225
20+70S 4+80W	.6	3.49	ND	ND	126	ND	.25	1.7	13	34	18	3.29	.09	.83	1271	1	.16	23	.08	107	ND	ND	ND	1	13	ND	12	357
20+70S 5+10W	1.5	4.27	ND	ND	155	3	.52	5.0	18	49	31	4.01	.18	1.36	997	ND	.26	41	.10	446	ND	ND	ND	2	26	ND	20	747
21+60S BL	.4	2.04	ND	ND	83	ND	.04	.4	8	17	9	2.40	.08	.31	704	ND	.04	12	.07	28	ND	ND	ND	1	8	ND	ND	71
21+60S 0+30E	.5	2.75	ND	ND	112	ND	.07	.5	9	15	14	2.54	.07	.26	1495	1	.05	9	.13	31	ND	ND	ND	1	9	ND	ND	94
21+60S 0+60E	.5	1.72	ND	ND	111	ND	.12	.3	8	17	9	2.85	.10	.30	644	1	.05	13	.09	33	ND	ND	3	1	10	ND	ND	79
21+60S 0+90E	.3	1.69	3	ND	168	ND	.10	.4	12	20	15	2.92	.10	.34	2029	ND	.06	15	.09	47	ND	ND	ND	1	10	ND	ND	104
21+60S 1+20E	.4	2.10	ND	ND	96	ND	.05	.3	13	21	11	3.34	.10	.40	1090	1	.06	18	.07	40	ND	ND	ND	1	8	ND	ND	102
21+60S 1+50E	.5	2.33	3	ND	93	ND	.05	.2	6	35	21	2.10	3.48	.43	467	1	.02	18	.08	83	ND	ND	ND	1	8	ND	ND	92
21+60S 1+80E	.2	2.17	3	ND	110	ND	.05	.2	1	25	12	3.34	.32	.31	65	1	.01	11	.09	83	ND	ND	ND	ND	7	ND	ND	79
21+60S 2+10E	.3	3.16	ND	ND	87	ND	.03	.5	7	13	14	2.26	.06	.23	302	1	.04	12	.08	24	ND	ND	ND	1	7	ND	ND	70
21+60S 2+40E	.9	2.24	ND	ND	90	ND	.07	.2	8	13	10	2.42	.07	.15	1433	1	.05	10	.12	27	ND	ND	3	1	8	ND	ND	95
21+60S 2+70E	.3	4.45	ND	ND	51	ND	.04	.5	7	13	12	2.41	.06	.17	466	1	.05	11	.14	20	ND	ND	ND	1	5	ND	4	76
21+60S 3+00E	.5	1.57	ND	ND	65	ND	.03	.3	5	13	9	2.09	.06	.15	320	ND	.03	7	.03	21	ND	ND	3	1	4	ND	ND	43
21+60S 3+30E	.4	2.44	ND	ND	71	ND	.05	.4	7	18	15	2.73	.08	.29	332	1	.05	10	.09	31	ND	ND	ND	1	9	ND	ND	62
21+60S 3+60E	.8	3.20	ND	ND	67	ND	.06	.4	5	15	14	3.40	.08	.15	705	1	.07	7	.23	60	ND	ND	ND	2	6	ND	ND	64
21+60S 3+90E	.5	2.14	ND	ND	146	ND	.04	.3	10	24	20	3.59	.10	.47	571	1	.06	18	.08	34	ND	ND	ND	2	14	ND	ND	71
21+60S 4+20E	.3	2.50	ND	ND	381	ND	.08	.2	13	27	23	3.08	.12	.66	565	1	.04	33	.15	29	ND	ND	3	2	28	ND	ND	79
21+60S 4+50E	.3	.83	12	ND	64	ND	.19	.7	7	19	22	1.93	.27	.18	275	5	.01	78	.06	39	ND	ND	ND	1	8	ND	ND	39
21+60S 4+80E	.6	1.33	ND	ND	165	ND	.05	.1	7	22	12	2.83	.08	.31	243	1	.04	15	.05	45	ND	ND	4	1	14	ND	ND	59
21+60S 5+10E	.1	3.42	ND	ND	70	ND	.03	.4	6	17	12	2.50	.06	.25	259	1	.05	11	.06	28	ND	ND	ND	1	7	ND	ND	49
21+60S 5+40E	.1	1.09	4	ND	103	ND	.14	.3	7	13	11	2.11	.07	.23	2355	ND	.04	9	.05	48	ND	ND	3	1	14	ND	ND	65
21+60S 5+70E	.2	2.18	ND	ND	62	ND	.04	.2	6	14	10	2.41	.06	.22	666	ND	.04	9	.04	21	ND	ND	ND	1	6	ND	ND	54
21+60S 6+00E	.2	4.34	ND	ND	55	ND	.04	.2	7	9	12	1.87	.05	.13	384	1	.04	8	.07	15	ND	ND	ND	1	5	ND	ND	51
21+60S 6+30E	.4	.90	13	ND	50	ND	.08	2.0	2	10	7	.80	.04	.12	40	ND	.01	8	.09	37	ND	ND	3	ND	11	ND	ND	32
21+60S 6+60E	.2	.65	7	ND	36	ND	.03	.1	3	10	8	1.01	.04	.14	82	ND	.01	5	.03	17	ND	ND	4	ND	5	ND	ND	24
21+60S 6+90E	.3	.77	4	ND	35	ND	.02	.5	3	8	13	1.04	.04	.08	71	ND	.01	4	.03	19	ND	ND	4	ND	4	ND	ND	25
21+60S 7+20E	.3	1.17	7	ND	55	ND	.02	.7	6	13	15	2.58	.07	.18	333	1	.04	7	.05	36	ND	ND	5	1	5	ND	ND	38
21+60S 7+50E	.2	1.67	3	ND	37	ND	.09	.1	9	24	32	3.18	.22	.23	418	1	.01	18	.06	74	ND	ND	ND	1	12	ND	ND	49
21+60S 7+80E	.8	1.65	9	ND	27	ND	.03	1.2	13	16	17	3.05	.11	.30	400	1	.06	11	.07	26	ND	ND	8	1	4	ND	ND	45
21+60S 8+10E	.6	1.71	6	ND	33	ND	.03	.5	9	27	17	2.53	.09	.41	390	2	.05	15	.08	22	ND	ND	7	1	5	ND	ND	51
21+60S 8+40E	.9	.87	7	ND	43	ND	.03	.4	3	10	10	.91	.08	.17	164	1	.01	3	.01	69	ND	ND	5	1	3	ND	ND	20
21+60S 8+70E	.7	2.06	3	ND	50	3	.04	.5	9	25	89	3.05	.11	.91	1928	1	.09	11	.07	17	ND	ND	7	1	4	ND	3	58
21+60S 9+00E	.5	1.59	5	ND	59	ND	.04	.6	11	12	27	1.58	.08	.39	459	2	.02	8	.07	19	ND	ND	5	ND	6	ND	ND	34
21+60S 9+30E	.5	.81	5	ND	30	ND	.02	.2	4	9	5	1.44	.06	.18	153	1	.01	4	.02	15	ND	ND	5	ND	3	ND	ND	21
21+60S 9+60E	.6	2.08	4	ND	35	4	.04	.5	6	19	8	1.50	.06	1.45	783	1	.07	8	.01	14	ND	ND	4	1	3	ND	10	40
21+60S 9+90E	.5	.07	4	ND	15	ND	.01	.1	1	3	3	.43	.04	.01	33	ND	.01	1	.01	9	ND	ND	5	ND	2	ND	ND	8
21+60S 0+30W	.5	1.02	5	ND	56	ND	.06	.2	5	11	5	1.75	.08	.16	1044	ND	.03	6	.06	23	ND	ND	6	ND	6	ND	ND	43

CLIENT: GOLDRICH RESOURCES LTD. JOB#: 85405 PROJECT: SHEEP CREEK SOUTH REPORT: 85-35-008

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
21+60S 0+60W	.6	1.23	4	ND	47	ND	.04	.2	4	12	50	1.78	.05	.16	283	1	.03	5	.05	22	ND	ND	ND	1	5	ND	ND	47
21+60S 0+90W	.6	2.45	ND	ND	96	ND	.04	.2	7	15	9	2.09	.05	.26	487	1	.05	9	.12	20	ND	ND	ND	1	7	ND	3	83
21+60S 1+20W	.3	2.26	ND	ND	120	ND	.05	.5	8	16	11	2.22	.06	.22	1361	1	.04	9	.07	21	ND	ND	ND	1	7	ND	ND	79
21+60S 1+50W	.3	2.43	ND	ND	99	ND	.09	.3	8	21	10	2.80	.09	.44	341	1	.05	16	.05	28	ND	ND	ND	1	10	ND	ND	74
21+60S 1+80W	.4	1.73	ND	ND	65	ND	.46	.2	9	15	10	2.07	.10	.32	884	ND	.03	11	.08	27	ND	ND	ND	ND	17	ND	ND	61
21+60S 2+10W	.3	1.96	ND	ND	80	ND	1.31	.6	7	17	11	1.93	.12	.41	1344	ND	.04	14	.15	26	ND	ND	ND	1	37	ND	ND	97
21+60S 2+40W	.2	2.49	ND	ND	107	ND	.22	.8	10	25	11	2.92	.11	.66	1869	ND	.07	18	.17	40	ND	ND	ND	1	15	ND	8	121
21+60S 2+70W	.3	1.60	3	ND	159	ND	.18	.4	9	18	10	2.42	.09	.38	1234	ND	.05	13	.06	44	ND	ND	ND	1	16	ND	ND	82
21+60S 3+00W	.5	2.87	ND	ND	61	ND	.39	.1	8	19	8	2.15	.10	.37	280	ND	.03	16	.09	31	ND	ND	ND	1	25	ND	3	67
21+60S 3+30W	.5	2.85	ND	ND	127	ND	.10	.4	12	26	11	3.82	.12	.49	1184	ND	.09	16	.12	26	ND	ND	ND	1	13	ND	6	119
21+60S 3+60W	.6	4.09	ND	ND	199	ND	.11	.4	13	16	10	2.98	.08	.25	277	ND	.07	13	.78	26	ND	ND	ND	2	15	ND	5	93
21+60S 3+90W	.7	3.40	ND	ND	95	ND	.08	.2	15	21	16	3.63	.10	.42	948	1	.08	13	.19	25	ND	ND	ND	1	10	ND	9	93
21+60S 4+20W	.5	1.83	ND	ND	66	ND	.09	.7	12	19	6	2.91	.12	.54	982	ND	.04	7	.12	34	ND	ND	ND	1	10	ND	ND	58
21+60S 4+50W	.7	2.22	ND	ND	134	ND	.17	.5	15	25	10	3.30	.12	.41	1276	ND	.08	18	.05	54	ND	ND	ND	1	18	ND	ND	145
21+60S 4+80W	.8	2.45	ND	ND	135	ND	.48	2.9	10	23	21	2.62	.12	.55	2952	ND	.22	19	.14	168	ND	ND	ND	1	35	ND	7	654
21+60S 5+10W	.7	3.15	ND	ND	77	4	.16	.8	12	45	12	3.66	.12	.84	1651	ND	.08	19	.08	39	ND	ND	ND	2	11	ND	16	124
22+50S BL	.5	1.83	ND	ND	347	ND	.52	1.0	22	19	14	2.61	.14	.38	2405	ND	.01	19	.10	49	ND	ND	ND	1	41	ND	ND	154
22+50S 0+30E	.7	2.22	3	ND	144	3	.09	.3	15	28	12	3.71	.14	.53	594	ND	.06	25	.12	42	ND	ND	ND	1	15	ND	7	141
22+50S 0+60E	.6	2.33	3	ND	288	ND	.33	.7	53	27	18	3.78	.15	.56	2516	ND	.09	32	.11	49	ND	ND	ND	1	39	ND	7	193
22+50S 0+90E	.4	2.70	ND	ND	126	ND	.11	.6	13	20	14	3.07	.09	.37	809	1	.07	25	.28	32	ND	ND	ND	1	16	ND	ND	126
22+50S 1+20E	.5	1.94	4	ND	131	ND	.30	.6	15	22	15	3.45	.13	.47	888	ND	.08	22	.19	38	ND	ND	ND	1	40	ND	5	136
22+50S 1+50E	.5	2.53	3	ND	172	5	.16	.5	29	24	15	3.81	.13	.53	2009	ND	.11	25	.13	49	ND	ND	ND	2	22	ND	9	221
22+50S 1+80E	.7	3.37	ND	ND	93	3	.05	.5	15	28	15	3.85	.13	.49	452	1	.07	25	.06	44	ND	ND	ND	2	10	ND	10	124
22+50S 2+10E	.6	2.10	4	ND	55	ND	.06	.2	8	26	12	4.65	.12	.39	289	1	.07	18	.09	33	ND	ND	ND	2	10	ND	4	61
22+50S 2+40E	.5	2.20	9	ND	63	3	.03	.3	16	27	22	3.60	.12	.47	1102	1	.06	27	.08	45	ND	ND	ND	1	9	ND	7	100
22+50S 2+70E	.5	2.02	8	ND	69	ND	.05	.5	12	24	20	3.18	.10	.42	1018	1	.04	23	.07	40	ND	ND	ND	1	12	ND	ND	79
22+50S 3+00E	.6	2.31	ND	ND	88	ND	.05	.6	20	23	24	3.01	.11	.36	1746	1	.02	27	.07	48	ND	ND	ND	1	12	ND	ND	74
22+50S 3+30E	.6	1.30	3	ND	69	ND	.04	.3	4	17	8	2.76	.08	.20	141	1	.03	10	.03	28	ND	ND	3	1	9	ND	ND	37
22+50S 3+60E	.5	1.97	ND	ND	88	ND	.09	.4	7	16	13	2.25	.07	.27	893	1	.04	12	.12	28	ND	ND	ND	1	13	ND	ND	70
22+50S 3+90E	.9	1.10	ND	ND	50	ND	.04	.3	5	12	8	2.08	.06	.11	112	1	.02	6	.03	29	ND	ND	3	2	6	ND	ND	42
22+50S 4+20E	.6	1.95	ND	ND	76	ND	.04	.4	5	17	11	2.67	.08	.21	491	1	.04	9	.05	43	ND	ND	ND	1	10	ND	ND	59
22+50S 4+50E	.7	1.63	ND	ND	47	ND	.04	.3	5	21	10	3.01	.09	.25	173	2	.04	10	.04	34	ND	ND	ND	1	10	ND	ND	49
22+50S 4+80E	.8	3.30	ND	ND	86	ND	.05	.4	9	19	17	2.88	.08	.32	565	1	.06	15	.07	31	ND	ND	ND	2	9	ND	ND	107
22+50S 5+10E	.6	3.04	ND	ND	139	ND	.07	.5	9	15	16	2.57	.07	.27	1895	1	.06	13	.08	23	ND	ND	ND	2	11	ND	6	101
22+50S 5+40E	.7	2.67	ND	ND	52	ND	.03	.4	6	19	12	3.33	.08	.29	180	2	.06	9	.05	26	ND	ND	ND	2	7	ND	ND	45
22+50S 5+70E	.5	.64	ND	ND	55	ND	.13	2.3	2	8	7	.61	.04	.09	67	1	.01	3	.05	51	ND	ND	ND	1	16	ND	ND	48
22+50S 6+00E	.7	2.50	ND	ND	78	ND	.07	.5	4	14	12	1.86	.07	.20	114	2	.01	8	.06	18	ND	ND	ND	1	11	ND	ND	26
22+50S 6+30E	1.7	1.71	ND	3	422	9	.11	.7	12	35	13	3.68	.12	.69	311	1	.04	25	.16	26	ND	ND	4	3	36	ND	ND	77
22+50S 6+60E	.8	1.16	ND	ND	195	4	.05	.5	7	19	12	2.32	.07	.30	321	2	.03	12	.05	63	ND	ND	ND	2	15	ND	ND	51

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
22+50S 6+90E	.1	.41	6	ND	42	ND	.06	.1	3	7	11	1.11	.01	.59	90	1	.01	12	.02	15	ND	ND	ND	2	5	4	3	31
22+50S 7+20E	.2	1.04	ND	ND	34	ND	.02	.1	4	14	26	2.50	.06	.23	114	ND	.04	7	.03	19	ND	ND	ND	1	4	ND	ND	27
22+50S 7+50E	.4	1.77	ND	ND	73	ND	.05	.5	7	25	16	4.51	.10	.40	236	1	.09	13	.08	23	ND	ND	ND	1	10	ND	ND	50
22+50S 7+80E	.1	1.26	ND	ND	44	ND	.04	.2	1	7	13	.69	.02	.12	52	ND	.01	4	.10	44	ND	ND	ND	ND	7	ND	ND	19
22+50S 8+10E	.1	1.32	7	ND	68	ND	.04	.5	15	10	13	1.48	.05	.20	391	1	.02	7	.08	96	ND	ND	ND	1	9	ND	ND	38
22+50S 8+40E	.4	.88	ND	ND	56	ND	.16	.5	3	12	4	.99	.06	.55	99	ND	.01	8	.01	20	ND	ND	ND	1	12	ND	ND	20
22+50S 8+70E	.1	3.26	ND	ND	73	5	.10	.9	10	32	226	4.64	.14	1.52	1419	ND	.14	16	.10	19	ND	ND	ND	2	12	ND	16	61
22+50S 9+00E	.4	2.07	ND	ND	51	ND	.04	.3	5	15	16	2.95	.08	.23	141	1	.05	8	.04	21	ND	ND	ND	1	8	ND	ND	36
22+50S 9+30E	.2	3.50	ND	ND	51	ND	.04	.3	4	11	17	1.69	.05	.16	114	ND	.02	6	.06	16	ND	ND	ND	1	7	ND	ND	22
22+50S 9+60E	.3	.37	ND	ND	23	ND	.02	.4	2	6	5	.83	.04	.03	56	ND	.01	3	.01	13	ND	ND	ND	ND	4	ND	ND	17
22+50S 9+90E	.3	.93	5	ND	41	ND	.03	.5	3	11	12	1.94	.05	.18	179	1	.03	5	.03	14	ND	ND	ND	ND	6	ND	ND	26
22+50S 0+30W	.1	1.47	ND	ND	324	ND	.28	1.0	19	19	22	2.98	.14	.37	4897	ND	.08	21	.11	50	ND	ND	ND	1	23	ND	ND	159
22+50S 0+60W	.2	1.57	ND	ND	92	ND	.06	.3	7	17	10	2.48	.10	.29	631	ND	.04	12	.10	31	ND	ND	ND	1	9	ND	ND	72
22+50S 0+90W	.2	1.12	3	ND	49	ND	.04	.5	5	13	8	2.06	.08	.23	302	ND	.03	8	.06	29	ND	ND	ND	ND	7	ND	ND	41
22+50S 1+20W	.1	2.32	ND	ND	90	ND	.13	.7	10	22	11	2.71	.12	.51	1186	ND	.06	18	.12	37	ND	ND	ND	1	13	ND	ND	116
22+50S 1+50W	.2	2.74	ND	ND	70	ND	.09	.8	9	26	10	2.96	.12	.74	455	ND	.06	19	.11	39	ND	ND	ND	1	11	ND	3	97
22+50S 1+80W	.1	2.89	ND	ND	96	ND	.26	.9	24	30	23	4.12	.17	.93	1656	ND	.10	35	.10	47	ND	ND	ND	1	20	ND	11	111
22+50S 2+10W	.3	3.42	ND	ND	69	ND	.44	.9	14	38	15	3.42	.16	.95	871	ND	.08	21	.09	39	ND	ND	ND	1	19	ND	9	128
22+50S 2+40W	.1	2.94	ND	ND	116	ND	.45	.9	14	27	17	4.37	.20	.81	4285	ND	.11	21	.32	137	ND	ND	ND	1	15	ND	5	130
22+50S 2+70W	.6	1.86	ND	ND	94	ND	.23	.5	9	16	9	3.35	.11	.26	523	ND	.08	11	.06	32	ND	ND	ND	1	14	ND	ND	96
22+50S 3+00W	.4	2.60	ND	ND	132	ND	.23	.8	12	18	13	3.39	.15	.39	1039	ND	.08	20	.13	34	ND	ND	ND	1	18	ND	ND	111
22+50S 3+30W	.3	2.25	ND	ND	211	ND	.13	.9	13	17	12	3.51	.13	.27	4392	ND	.09	12	.20	36	ND	ND	ND	1	14	ND	ND	112
22+50S 3+60W	.4	2.56	ND	ND	76	ND	.08	.5	15	20	17	4.28	.17	.53	916	ND	.09	15	.08	29	ND	ND	ND	1	13	ND	4	79
22+50S 3+90W	.4	2.59	ND	ND	79	3	.09	.3	10	24	16	3.45	.15	.52	636	1	.07	15	.10	70	ND	ND	ND	1	12	ND	ND	89
22+50S 4+20W	.7	2.27	ND	ND	70	3	.09	.9	14	17	14	2.73	.13	.33	557	ND	.05	13	.09	92	ND	ND	ND	1	12	ND	ND	84
22+50S 4+50W	.7	2.31	ND	ND	82	ND	.30	1.3	19	23	21	2.49	.18	.38	2561	ND	.05	26	.17	127	ND	ND	ND	1	32	ND	ND	183
22+50S 4+80W	.7	3.24	ND	ND	151	ND	.30	1.8	15	28	36	3.34	.17	.62	2551	ND	.26	24	.19	995	ND	ND	ND	1	20	ND	12	740
22+50S 5+10W	.3	3.32	ND	ND	209	5	.38	2.4	15	43	23	3.67	.19	.88	5271	ND	.14	30	.21	142	ND	ND	ND	1	18	ND	5	316
23+40S BL	.2	1.85	ND	ND	170	ND	.12	.6	12	23	13	3.21	.14	.49	2373	1	.08	16	.07	43	ND	ND	ND	1	13	ND	ND	108
23+40S 0+30E	.3	1.41	3	ND	130	ND	.42	.9	10	13	39	2.11	.14	.29	2082	ND	.04	11	.06	71	ND	ND	3	ND	22	6	ND	96
23+40S 0+60E	.3	2.51	ND	ND	92	3	.08	.7	10	23	14	3.71	.16	.45	416	ND	.08	17	.06	60	ND	ND	ND	1	11	ND	ND	110
23+40S 0+90E	.3	1.82	5	ND	121	ND	.26	.5	14	24	15	3.69	.20	.51	617	ND	.08	22	.09	58	ND	ND	4	1	26	4	ND	104
23+40S 1+20E	.1	1.47	7	ND	95	ND	.34	1.0	101	11	10	2.32	.17	.31	1228	1	.01	15	.07	87	ND	ND	3	1	37	4	ND	55
23+40S 1+50E	.3	1.76	10	ND	132	ND	.18	1.1	34	20	21	2.79	.15	.42	749	ND	.05	22	.07	111	ND	ND	4	1	20	ND	ND	104
23+40S 1+80E	.1	2.00	ND	ND	101	ND	.08	.7	56	19	59	2.66	.04	.35	706	1	.03	24	.07	54	ND	ND	ND	1	13	ND	ND	75
23+40S 2+10E	.1	2.31	5	ND	96	ND	.07	.6	17	30	27	4.13	.09	.59	638	1	.08	30	.06	46	ND	ND	ND	1	14	ND	ND	120
23+40S 2+40E	.1	1.87	6	ND	82	ND	.07	.6	20	25	28	3.44	.08	.44	1827	1	.05	25	.09	70	ND	ND	ND	1	11	ND	ND	97
23+40S 2+70E	.1	3.25	ND	ND	47	ND	.03	.3	9	26	31	3.63	.05	.42	301	1	.06	24	.06	36	ND	ND	ND	1	8	ND	6	78
23+40S 3+00E	.1	1.00	3	ND	41	ND	.04	.5	4	16	16	2.33	.01	.18	337	1	.02	10	.04	41	ND	ND	ND	ND	8	ND	ND	45

CLIENT: GOLDRICH RESOURCES LTD. JOB#: 85405 PROJECT: SHEEP CREEK SOUTH REPORT: 85-35-008

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
23+40S 3+30E	.1	1.47	ND	ND	57	ND	.03	.2	3	13	11	2.05	.01	.15	151	1	.02	7	.03	27	ND	ND	ND	1	6	ND	ND	29
23+40S 3+60E	.1	2.42	ND	ND	73	ND	.03	.3	5	17	19	2.54	.01	.28	390	1	.04	9	.08	31	ND	ND	ND	1	7	ND	ND	53
23+40S 3+90E	.1	2.00	ND	ND	78	ND	.03	.4	6	15	18	2.48	.01	.23	327	1	.04	9	.04	35	ND	ND	ND	1	8	ND	ND	58
23+40S 4+20E	.1	.66	ND	ND	70	ND	.06	.9	3	9	16	1.27	.01	.08	668	1	.02	6	.02	50	ND	ND	3	1	10	ND	ND	52
23+40S 4+50E	.1	2.49	ND	ND	65	ND	.04	.4	6	17	18	2.62	.02	.27	340	1	.05	11	.05	39	ND	ND	ND	2	8	ND	ND	82
23+40S 4+80E	.3	1.51	12	ND	38	ND	.05	.4	5	13	16	2.83	.01	.15	158	1	.05	7	.06	50	ND	ND	3	2	7	ND	ND	56
23+40S 5+10E	.1	2.70	ND	ND	67	ND	.04	.6	4	12	17	2.48	.01	.11	224	1	.04	5	.05	34	ND	ND	ND	2	6	ND	ND	36
23+40S 5+40E	.1	.94	ND	ND	52	ND	.03	.3	4	12	15	1.75	.01	.11	116	1	.01	6	.02	20	ND	ND	ND	1	6	ND	ND	38
23+40S 5+70E	.1	1.98	ND	ND	56	ND	.03	.2	3	12	13	2.01	.01	.12	182	1	.03	4	.03	19	ND	ND	ND	1	5	ND	ND	30
23+40S 6+00E	.1	2.27	ND	ND	38	ND	.04	.4	2	11	21	1.22	.01	.16	69	ND	.01	6	.05	33	ND	ND	ND	1	6	ND	ND	25
23+40S 6+30E	.1	.85	ND	ND	41	ND	.03	.3	2	10	7	1.02	.01	.11	72	ND	.01	3	.02	27	ND	ND	ND	1	7	ND	ND	28
23+40S 6+60E	.1	.83	3	ND	113	ND	.06	.5	5	15	15	1.93	.01	.14	325	1	.02	9	.04	44	ND	ND	3	1	10	ND	ND	54
23+40S 6+90E	1.4	2.31	ND	ND	792	16	.34	.9	22	64	27	4.62	.18	1.39	1068	1	.07	53	.17	38	ND	ND	3	4	68	ND	17	125
23+40S 7+20E	.1	.90	ND	ND	150	ND	.09	.7	5	9	13	1.20	.01	.11	93	1	.01	8	.04	131	ND	ND	3	1	15	ND	ND	40
23+40S 7+50E	.1	1.59	ND	ND	114	ND	.17	1.1	18	12	14	1.54	.01	.24	2044	3	.02	9	.12	41	ND	ND	ND	1	29	ND	ND	48
23+40S 7+80E	.1	2.25	ND	ND	64	ND	.05	.8	6	16	19	2.57	.01	.24	237	1	.04	11	.06	27	ND	ND	ND	1	11	ND	ND	44
23+40S 8+10E	.1	1.64	ND	ND	55	ND	.03	.8	3	13	16	1.98	.01	.19	105	1	.02	8	.09	24	ND	ND	ND	1	7	ND	ND	26
23+40S 8+40E	.1	1.51	ND	ND	44	ND	.03	.2	4	17	13	2.15	.01	.42	341	ND	.04	8	.06	16	ND	ND	ND	1	5	ND	ND	39
23+40S 8+70E	.1	1.61	6	ND	38	ND	.04	.5	5	18	13	2.73	.01	.34	179	1	.05	11	.04	20	ND	ND	ND	1	8	ND	ND	44
23+40S 9+00E	.1	2.92	ND	ND	47	ND	.04	.3	2	9	17	1.31	.01	.12	92	ND	.01	11	.08	12	ND	ND	ND	1	5	ND	ND	18
23+40S 9+30E	.1	4.73	ND	ND	45	ND	.06	.3	5	8	13	1.96	.01	.13	220	ND	.04	8	.07	14	ND	ND	ND	2	6	ND	8	41
23+40S 0+30W	.1	1.77	5	ND	144	ND	.18	1.2	12	22	19	2.71	.05	.45	2274	ND	.06	15	.12	56	ND	ND	ND	1	16	ND	ND	110
23+40S 0+60W	.1	1.99	ND	ND	59	ND	.06	.2	8	18	13	2.47	.02	.37	1481	ND	.05	11	.16	28	ND	ND	ND	1	7	ND	ND	66
23+40S 0+90W	.1	2.73	ND	ND	66	ND	.34	.5	11	25	13	2.85	.09	.68	1404	ND	.05	19	.11	34	ND	ND	ND	1	14	ND	ND	98
23+40S 1+20W	.1	2.35	ND	ND	66	ND	.09	.3	9	24	13	3.03	.06	.59	759	ND	.06	18	.10	33	ND	ND	ND	1	10	ND	ND	84
23+40S 1+50W	.1	3.09	ND	ND	89	ND	.06	.7	14	26	14	3.04	.08	.61	606	ND	.05	22	.06	32	ND	ND	ND	1	11	ND	5	87
23+40S 1+80W	.1	2.32	ND	ND	101	ND	.23	.6	12	29	11	3.17	.07	.67	1218	ND	.07	20	.07	33	ND	ND	ND	1	13	ND	ND	107
23+40S 2+10W	.1	2.67	ND	ND	64	ND	6.09	.6	10	28	14	2.59	.22	1.39	1401	ND	.07	22	.19	44	ND	ND	ND	1	71	ND	4	102
23+40S 2+40W	.1	3.82	ND	ND	71	ND	.34	.5	17	47	16	4.19	.14	1.08	1206	ND	.09	28	.11	42	ND	ND	ND	2	17	ND	17	119
23+40S 2+70W	.1	1.97	ND	ND	145	ND	1.17	1.0	9	21	23	2.65	.12	.52	4496	ND	.05	14	.13	50	ND	ND	ND	1	37	7	ND	85
23+40S 3+00W	.1	2.00	ND	ND	162	ND	.10	.6	9	17	14	2.93	.06	.37	2447	ND	.08	13	.19	34	ND	ND	ND	1	11	ND	ND	132
23+40S 3+30W	.1	2.39	ND	ND	74	ND	.09	.5	9	20	16	3.88	.09	.38	498	ND	.08	12	.09	22	ND	ND	ND	1	10	ND	ND	74
23+40S 3+60W	.1	1.43	ND	ND	89	ND	.09	.5	7	19	12	3.80	.06	.27	642	ND	.07	10	.07	25	ND	ND	ND	1	11	ND	ND	52
23+40S 3+90W	.1	2.23	ND	ND	75	ND	.11	.4	10	20	12	3.58	.07	.46	883	ND	.07	13	.07	42	ND	ND	ND	1	11	ND	3	79
23+40S 4+20W	.1	2.61	ND	ND	85	ND	.09	.3	13	22	15	3.27	.09	.46	651	ND	.07	19	.08	49	ND	ND	ND	1	12	ND	3	107
23+40S 4+50W	.1	2.66	ND	ND	93	ND	.09	.5	10	21	17	3.08	.09	.42	707	ND	.05	17	.12	51	ND	ND	ND	1	11	ND	ND	90
23+40S 4+80W	.1	2.30	ND	ND	226	3	.17	.6	11	23	18	3.15	.07	.42	2538	ND	.10	17	.18	57	ND	ND	ND	1	13	ND	ND	207
23+40S 5+10W	.1	2.49	ND	ND	205	ND	1.86	1.2	10	24	16	3.25	.18	.63	5114	ND	.08	18	.19	69	ND	ND	ND	1	38	ND	ND	149
24+30S BL	.1	1.93	ND	ND	125	3	.29	.6	10	22	14	2.68	.07	.50	492	ND	.03	17	.04	33	ND	ND	ND	1	22	ND	ND	74

CLIENT: GOLDRICH RESOURCES LTD. JOB#: 85405 PROJECT: SHEEP CREEK SOUTH REPORT: 85-35-008

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
24+30S 0+30E	.2	2.11	ND	ND	54	ND	.05	.5	5	13	14	2.59	.05	.20	495	1	.05	7	.07	33	ND	ND	ND	1	6	ND	ND	45
24+30S 0+60E	.3	1.23	8	ND	138	ND	.18	.6	10	17	17	2.81	.09	.32	1373	1	.05	14	.06	49	ND	ND	3	1	19	ND	ND	84
24+30S 0+90E	.2	1.76	3	ND	128	ND	.31	1.1	67	12	23	2.40	.08	.21	3241	2	.04	11	.11	119	ND	ND	ND	1	30	ND	ND	64
24+30S 1+20E	.1	2.29	ND	ND	98	ND	.14	1.0	51	20	33	2.93	.10	.35	3083	1	.06	22	.15	86	ND	ND	ND	1	16	ND	ND	105
24+30S 1+50E	.2	1.21	ND	ND	77	ND	.08	.3	6	15	10	1.71	.06	.19	208	1	.01	8	.03	42	ND	ND	ND	1	10	ND	ND	41
24+30S 1+80E	.1	1.23	3	ND	68	ND	.03	.6	6	20	19	2.94	.09	.37	249	1	.03	14	.04	41	ND	ND	3	1	11	ND	ND	47
24+30S 2+10E	.1	2.27	3	ND	71	ND	.05	.4	21	25	22	3.51	.10	.49	1628	1	.07	23	.09	41	ND	ND	ND	1	9	ND	ND	110
24+30S 2+40E	.1	2.85	3	ND	70	ND	.03	.4	14	28	28	3.96	.11	.53	597	1	.07	28	.06	52	ND	ND	ND	1	9	ND	14	118
24+30S 2+70E	.1	1.60	4	ND	75	ND	.06	.5	14	23	24	3.31	.10	.39	1020	1	.05	20	.07	29	ND	ND	ND	1	12	ND	ND	84
24+30S 3+00E	.1	1.49	3	ND	57	ND	.04	.3	11	18	22	2.78	.09	.33	1246	1	.03	14	.10	39	ND	ND	ND	1	8	ND	ND	56
24+30S 3+30E	.1	2.07	ND	ND	40	ND	.04	.3	7	13	19	2.12	.05	.25	1505	1	.04	9	.09	48	ND	ND	ND	1	7	ND	ND	63
24+30S 3+60E	.4	2.91	ND	ND	59	ND	.05	.4	9	23	21	3.69	.09	.38	409	1	.08	16	.07	95	ND	ND	ND	1	9	ND	8	96
24+30S 3+90E	.6	3.89	ND	ND	68	ND	.04	.3	8	18	23	2.98	.07	.23	470	1	.06	11	.05	45	ND	ND	ND	2	8	ND	9	83
24+30S 4+20E	.2	2.47	ND	ND	74	ND	.06	.4	8	19	21	3.04	.08	.32	770	1	.07	15	.06	49	ND	ND	ND	1	10	ND	ND	118
24+30S 4+50E	.2	2.46	ND	ND	88	ND	.05	.5	9	13	14	2.48	.06	.23	2627	1	.06	11	.07	36	ND	ND	ND	1	7	ND	ND	109
24+30S 4+80E	1.4	1.65	ND	ND	151	ND	.13	2.2	10	13	24	2.52	.07	.19	3082	1	.07	12	.06	115	ND	ND	ND	1	15	ND	ND	149
24+30S 5+10E	.3	1.19	7	ND	48	ND	.05	.5	5	15	20	2.23	.05	.16	271	1	.04	7	.05	246	ND	ND	3	1	11	ND	ND	65
24+30S 5+40E	.1	2.70	ND	ND	24	ND	.03	.5	1	6	15	1.76	.02	.03	36	1	.02	2	.04	29	ND	ND	ND	1	4	ND	ND	11
24+30S 5+70E	.2	1.19	5	ND	40	ND	.05	.1	4	15	22	2.48	.05	.18	269	1	.04	6	.09	22	ND	ND	ND	1	7	ND	ND	37
24+30S 6+00E	.1	1.26	ND	ND	33	ND	.03	.3	4	13	29	2.03	.04	.17	203	1	.03	7	.07	24	ND	ND	ND	1	6	ND	ND	33
24+30S 6+30E	.6	1.74	ND	ND	28	ND	.05	.3	5	16	15	3.96	.07	.16	98	2	.08	13	.04	23	ND	ND	ND	1	7	ND	ND	29
24+30S 6+60E	.1	1.23	6	ND	34	ND	.02	.5	3	13	12	1.81	.04	.19	131	1	.03	8	.08	21	ND	ND	ND	ND	4	ND	ND	39
24+30S 6+90E	.2	1.64	ND	ND	36	ND	.03	.3	5	15	13	2.39	.05	.29	179	1	.04	9	.06	21	ND	ND	ND	1	6	ND	ND	43
24+30S 7+20E	.1	2.39	ND	ND	47	ND	.06	.3	7	20	20	2.47	.06	.49	278	1	.05	15	.11	18	ND	ND	ND	1	9	ND	ND	56
24+30S 7+50E	.5	1.95	ND	ND	35	ND	.03	.6	5	7	20	1.31	.02	.08	317	ND	.01	4	.08	20	ND	ND	ND	1	3	ND	ND	18
24+30S 7+80E	.1	1.41	ND	ND	92	ND	.06	.5	12	10	12	1.61	.03	.19	438	1	.03	9	.08	35	ND	ND	ND	1	11	ND	ND	36
24+30S 8+10E	.1	2.86	ND	ND	30	ND	.15	.3	6	17	13	1.44	.05	.92	172	ND	.04	12	.09	14	ND	ND	ND	1	11	ND	6	46
24+30S 8+40E	.2	1.83	ND	ND	59	ND	.06	.2	12	19	15	2.58	.07	.58	1230	2	.06	9	.04	17	ND	ND	ND	1	7	ND	ND	44
24+30S 8+70E	.2	1.02	ND	ND	27	ND	.05	.4	3	12	19	2.20	.05	.20	154	1	.04	6	.04	17	ND	ND	ND	1	5	ND	ND	26
24+30S 9+00E	.1	1.49	ND	ND	49	ND	.03	.3	3	13	18	1.53	.03	.20	161	1	.02	6	.06	18	ND	ND	ND	1	6	ND	ND	31
24+30S 0+30W	.1	2.63	ND	ND	62	ND	.21	.3	7	13	18	1.90	.07	.26	863	ND	.01	12	.15	32	ND	ND	ND	1	16	ND	ND	68
24+30S 0+60W	.1	1.89	ND	ND	77	ND	.10	.3	8	16	12	2.17	.07	.36	892	1	.05	10	.14	35	ND	ND	ND	ND	10	ND	ND	84
24+30S 0+90W	.1	1.65	ND	ND	49	ND	.07	.4	10	19	14	2.32	.07	.38	1044	ND	.05	15	.15	30	ND	ND	ND	1	8	ND	ND	64
24+30S 1+20W	.1	1.36	ND	ND	58	ND	.17	.3	9	22	9	2.39	.08	.43	2149	1	.05	12	.08	61	ND	ND	ND	ND	11	ND	ND	65
24+30S 1+50W	.1	2.34	5	ND	72	ND	1.27	.7	10	24	13	3.27	.15	1.05	2207	1	.09	20	.24	38	ND	ND	ND	1	29	ND	11	142
24+30S 1+80W	.1	2.49	ND	ND	83	ND	.59	.5	10	22	10	2.60	.11	.73	1413	ND	.06	19	.14	38	ND	ND	ND	1	16	ND	5	99
24+30S 2+10W	.5	2.21	ND	ND	51	ND	2.56	.9	9	24	9	2.24	.17	1.52	1239	ND	.08	20	.22	53	ND	ND	ND	1	34	5	8	107
24+30S 2+40W	.4	2.15	ND	ND	53	ND	.77	.6	11	21	11	2.26	.12	.59	1238	1	.05	21	.11	31	ND	ND	ND	1	22	5	ND	78
24+30S 2+70W	.5	2.34	ND	ND	59	ND	.24	.4	10	29	9	2.67	.10	.77	832	1	.07	18	.08	35	ND	ND	ND	1	13	ND	5	98
24+30S 3+00W	.4	2.03	ND	ND	66	ND	.17	.4	8	19	28	2.32	.09	.58	1237	1	.05	14	.09	38	ND	ND	4	1	6	ND	ND	62
24+30S 3+30W	.3	1.34	ND	ND	177	ND	.66	.5	7	12	11	2.28	.11	.40	3251	ND	.06	7	.09	61	ND	ND	3	ND	21	ND	ND	68
24+30S 3+60W	.5	1.46	ND	ND	96	ND	.12	.3	10	17	11	2.91	.10	.37	621	1	.07	14	.05	33	ND	ND	5	1	7	ND	4	66
24+30S 3+90W	.2	2.10	ND	ND	81	ND	.03	.2	12	17	13	2.93	.08	.36	813	1	.08	13	.05	30	ND	ND	ND	1	8	ND	5	83
24+30S 4+20W	.3	2.21	ND	ND	64	ND	.02	.2	8	17	13	2.86	.08	.34	273	ND	.07	11	.04	28	ND	ND	ND	1	4	ND	4	58

Itemized Cost Statement

Sheep Creek South Group

Period: September 3 to September 10, 1985

PERSONNEL (Field)

Brian Meyer	Geologist	4 Days	@ $200	$ 800.00
Bill Day	Geologist	2 Days	@ $200	$ 400.00
Jeff Murray	Assistant	3 Days	@ $150	$ 450.00
Doug Murray	Assistant	3 Days	@ $150	$ 450.00
Vehicle		4 Days	@ $ 40	$ 160.00
Food				$ 113.27
Fuel, Ect.				$ 79.34
Helicopter				$ 446.40

PERSONNEL (Office)

Brian Meyer	Geologist	2 Days	@ $150	$ 300.00

Analyses		$3835.70
Map Preparation		$ 800.00
Shipping		$ 23.80
	TOTAL	$7858.51

APPENDIX II

STATEMENT OF QUALIFICATIONS

I, Brian H. Meyer, Professional Geologist, of the City of Nelson, B.C. do hereby certify as follows:

1. I am a Professional Geologist registered in the Province of Alberta.

2. I am a graduate of the University of Alberta, year 1979, and have been practicing my profession since that time.

3. I have received no interest either directly or indirectly, nor do I expect to receive any interest in this property.

4. The foregoing report on the SHEEP CREEK SOUTH GROUP is based on field work carried out under my direction and my personal examination of the property, visited between September 3 and September 10, 1985, and from previous related reports, and published material available from government geological departments.

Brian H. Meyer, P. Geol.

October 23, 1985

Billings Creek

Bennett Creek

McArthur Creek

Weasel Creek

King Lake

Abandoned

Mount Waldie

Qtz Porphyry

Reno Fmtn.

Qtz Range Fmtn.

Laib Group

INDEPENDENCE #1 1932 (9)

LEGEND

- Gold Value (ppb)
- Sample Location
- Lead Value (ppm)

Note: nd denotes "not detectable"

- Gold Anomaly (30 ppb and greater)
- Lead Anomaly (65 ppm and greater)
- Approximate Geological Contact

100 0 100 200 300 m

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,027

GOLDFIELD RESOURCES INC.

SHEEP CREEK SOUTH GROUP W1/2

SOIL GEOCHEMISTRY (GOLD)

NELSON MINING DIVISION, B.C.

Scale: 1:5000	NTS: 82F3E
Date: October, 1985	Dwg. No.: