85-844
14048
8/86

MIN-EX RESOURCE CONSULTANTS

806 - 402 West Pender Street
Vancouver, B.C. V6B 1T6
Phone: (604) 669-7033

GEOCHEMICAL SURVEY
WHIPSAW CREEK PROPERTY
(MIKE, KERRY 1, KERRY 2 CLAIMS)
SIMILKAMEEN M.D.
NTS 92H/7E
49°16'N, 120°43'W

Owner and Operator:

WORLD WIDE MINERALS LTD.
807 - 402 West Pender Street
Vancouver, B.C. V6B 1T6

Report Prepared by:

R.C. Heim, Ph.D., P.Eng.

September 12, 1985

GEOLOGICAL BRANCH
ASSESSMENT REPORT
14,048

WHIPSAW CREEK PROPERTY
GEOCHEMICAL SURVEY REPORT

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1. INTRODUCTION

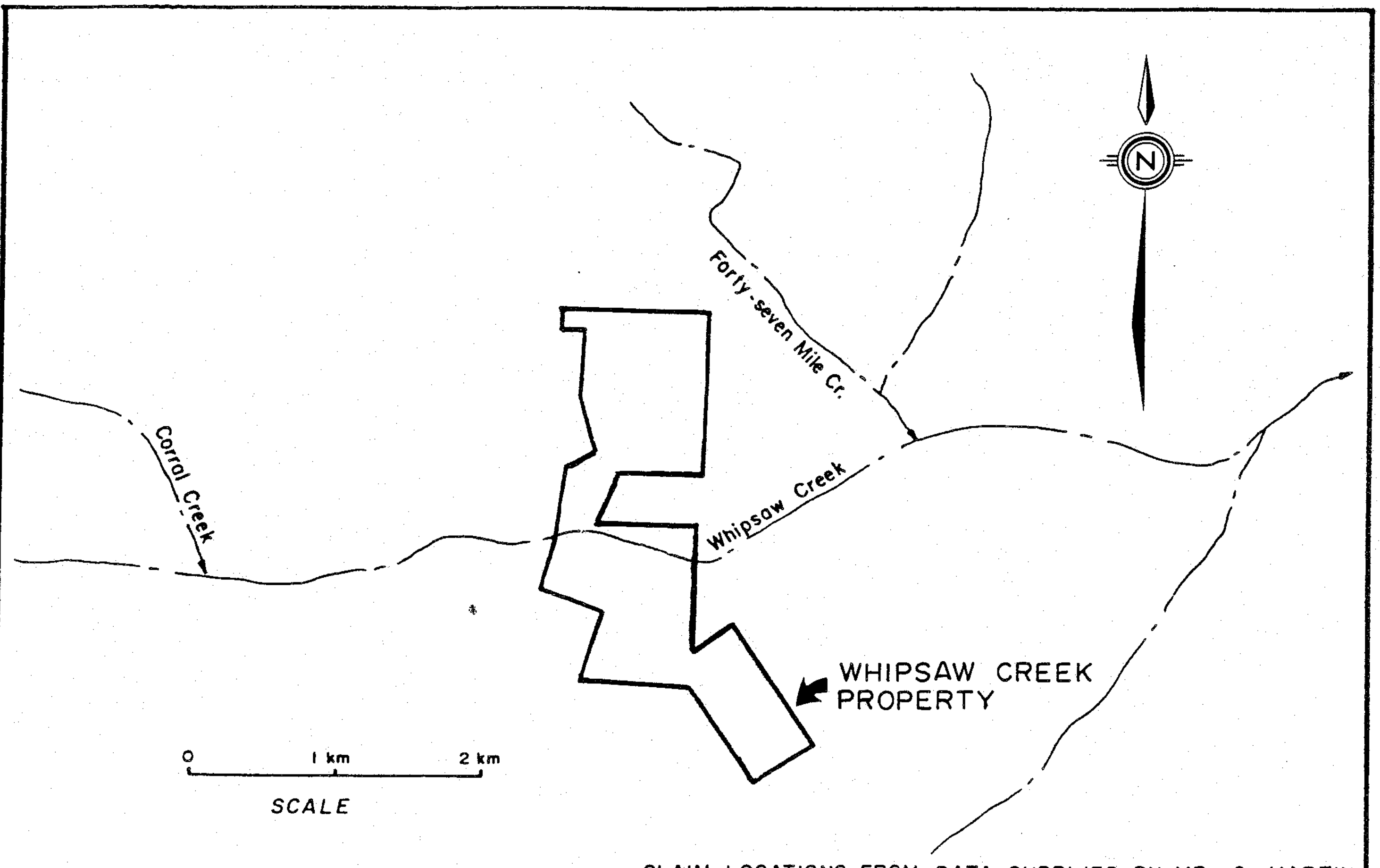
The Whipsaw Creek property of World Wide Minerals Ltd. is located 26 kilometres southwest of Princeton (see Figure 1). The property consists of the Mike, Kerry 1 and Kerry 2 claims which are accessed by secondary logging roads from the Hope-Princeton Highway. In wet weather the use of four wheel drive vehicles is recommended. The topographic relief is gentle, except for the deeply incised valley of Whipsaw Creek, which bisects the property (Figure 2). Elevations on the property range from 1385 to 1660 metres.

The property is underlain by hornblende-biotite schists and amphibolites, derived from Upper Triassic, Nicola Group volcanic and sedimentary rocks. Immediately to the southwest of the property, this rock sequence was intruded by the Eagle granodiorite, part of the Coast Range Intrusive. A number of shear zones and breccia zones are present on the property and near the intrusive contact there are swarms of feldspar porphyry dikes.

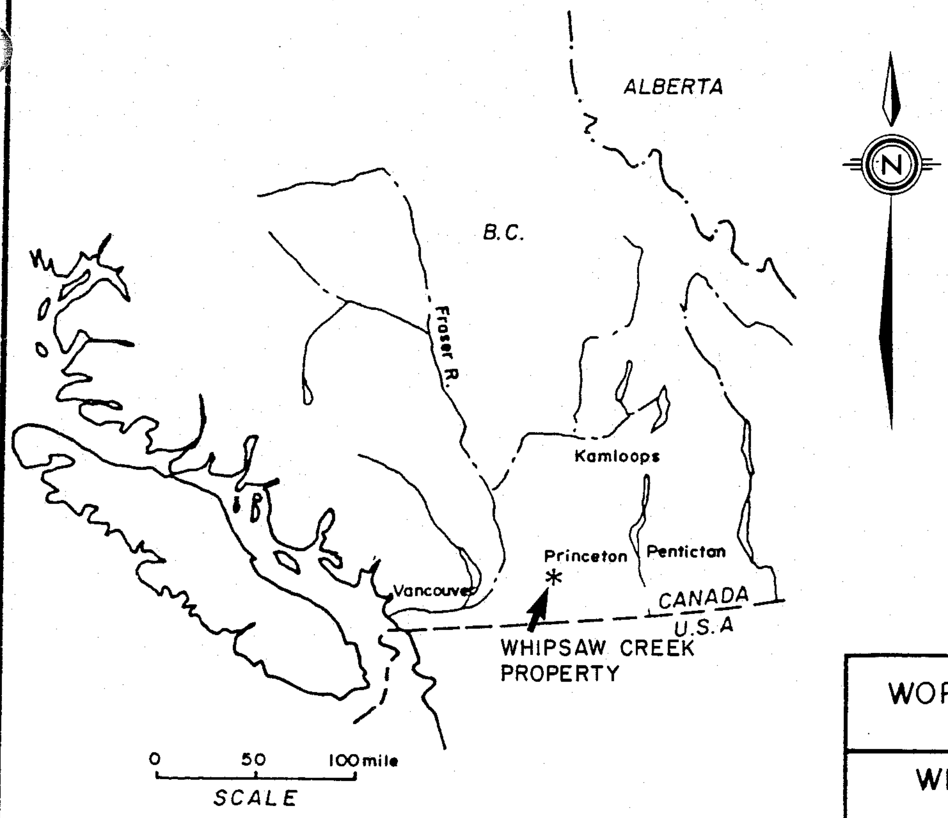
Mineralization took place in three stages: (i) widespread, finely disseminated pyrite, (ii) stockworks of pyrite, sphalerite, chalcopyrite and galena, (iii) coarse pyrite and other sulphides in quartz-carbonate veins.

Previous exploration dates back to 1915. It has included geological mapping, geochemical and geophysical surveys, trenching and diamond drilling. Most efforts were directed at the base metals potential, concentrating on the copper-zinc-lead mineralization in the southern part of the property, and on the porphyry-type copper-molybdenum potential in the northern part. Until recently, relatively little attention was paid to the possible gold and silver components of the mineralization.

In this respect, the previous work in the BZ showing area is of particular interest. The BZ showing is on the west side of a small, north-south flowing creek, about 450 metres north of its termination at Whipsaw Creek. Some years ago, this



CLAIM LOCATIONS FROM DATA SUPPLIED BY MR. C. MARTIN



KEY MAP

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
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WHIPSAW CREEK PROPERTY

PROPERTY LOCATION MAP

FIG NO: 1

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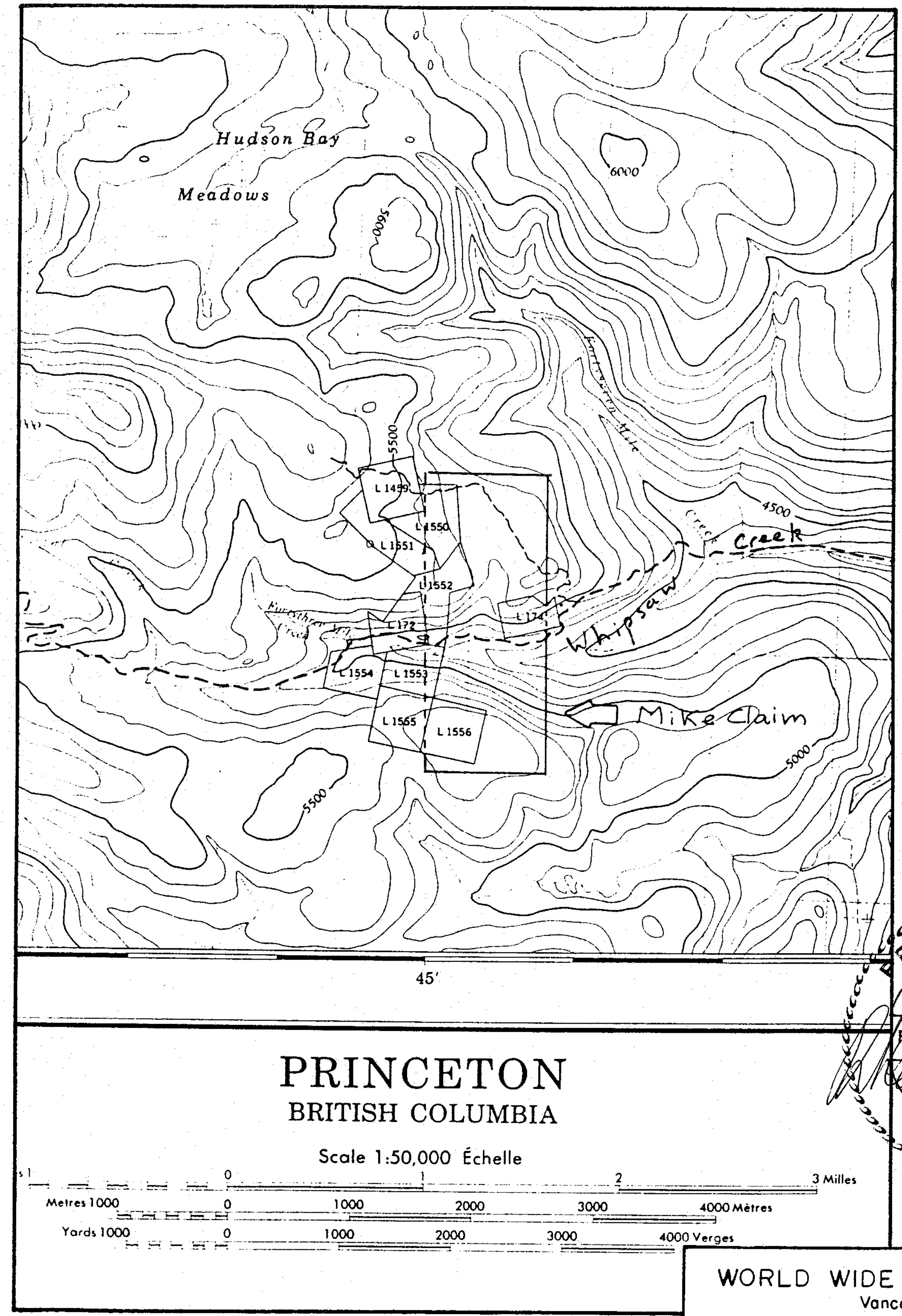
DRAWN BY: RCH	DATE: 20 AUG 1985



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WHIPSAW CREEK PROPERTY

CLAIM & TOPOGRAPHIC MAP

NTS 92 H/7 FIG NO: 2

MIN-EX RESOURCE CONSULTANTS

PREPARED BY: RCH	SCALE: AS SHOWN
DRAWN BY: RCH	DATE: 20 AUG 1985

mineralized zone was discovered by soil geochemistry, which outlined an elongate copper soil anomaly (see Section 3.0). These soils, however, were not analyzed for gold or silver. Four trenches across the anomaly revealed copper-zinc mineralization in the bedrock with gold and silver values. Two of the samples assayed 0.167 oz/ton gold and 0.339 oz/ton gold, with 6.12 oz/ton silver and 5.40 oz/ton silver, respectively, over a width of 0.7 metres.

The precious metals potential in the general area of the BZ showing should be further investigated. To this end, as a first step, a reconnaissance soil sampling program was carried out.

2. SOIL SURVEY

2.1 Sampling Method

Five east-west soil sampling lines were laid out, centered around the BZ trenches. The lines are 340 metres long and 180 metres apart. Along these lines soil samples were collected at 20 metre intervals and a total of 90 soil samples were taken. The samples were collected in "High West Strength" Kraft bags and sent to Acme Analytical Laboratories Ltd., Vancouver, for assay. The analytical procedures are described on the assay sheets (Appendix A).

As a result of the semi-arid climate, soil development is poor. The thickness of the A-horizon is 4 centimetres or less and the B-horizon is usually less than 5 centimetres thick, and often poorly defined. In the current survey, the soil samples were collected from the C-horizon, at depths varying from 20 to 30 centimetres. By taking the soil samples from the C-horizon, precious metals values are considered to reflect more accurately the content of the underlying bedrock. At 2-20 W on line ON, one sample was taken from the B-horizon and another one was taken from the C-horizon, from a depth of about 1.3 metres. The assay printout shows that the gold value in the deeper sample (C-horizon) is greater than that reported for the more shallow (B-horizon) sample.

2.2 Anomalous Values

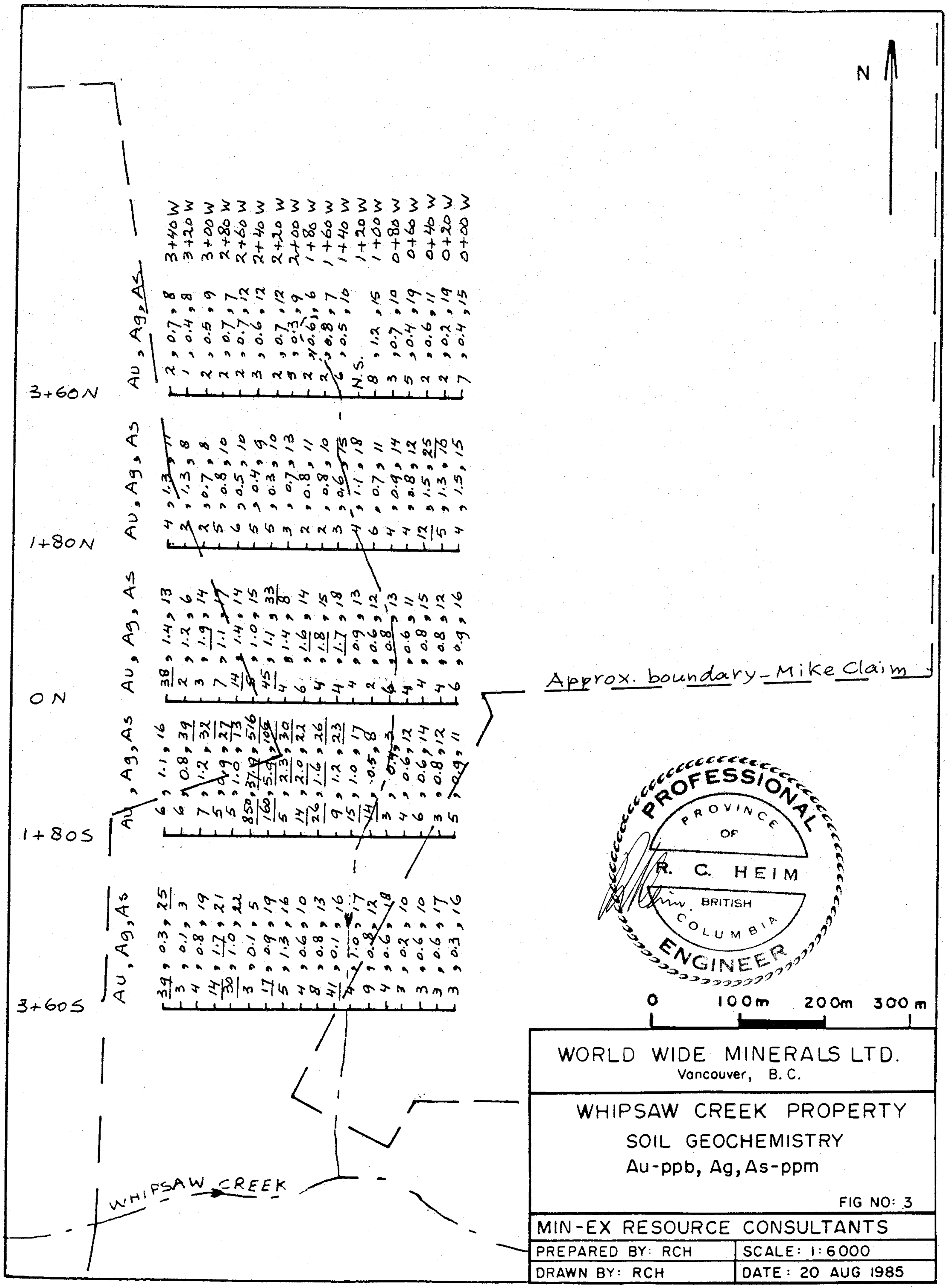
Anomalous values were determined for copper, lead, zinc, gold, silver and arsenic by calculating the mean and standard deviation of the visually estimated background scatter. First order anomalous is from mean + 2 SD to mean + 8 SD; second order anomalous is from mean + 8 SD to mean + 16 SD; third order anomalous is mean + 16 SD and higher. The values calculated for these elements are presented in Table 2.1. Histograms illustrating the frequency of the reported values for copper, lead, zinc, silver and gold are presented in Appendix B.

The assay values for gold, silver and arsenic are plotted on Figure 3, the values for copper, lead and zinc are plotted on Figure 4. The anomalous values are underlined.

TABLE 2.1

Anomalous Assay Values for Cu, Pb, Zn, Au, Ag and As

	Cu (ppm)	Pb (ppm)	Zn (ppm)	Au (ppb)	Ag (ppm)	As (ppm)
1st Order Anomalous	490-730	40-60	520-790	10-15	1.6-2.8	23-35
2nd Order Anomalous	730-1220	60-100	790-1330	15-26	2.8-5.2	35-59
3rd Order Anomalous	1220	100	1320	26	5.2	59



	3+60S	1+80S	0N	1+80N	3+60N
	Au, Ag, As	Au, Ag, As	Au, Ag, As	Au, Ag, As	Au, Ag, As
3+40W	39, 0.3, 25	6, 1.1, 16	38, 1.4, 13	4, 1.3, 11	2, 0.7, 8
3+20W	3, 0.1, 3	6, 0.8, 39	2, 1.2, 6	3, 1.3, 8	1, 0.4, 8
3+00W	4, 0.8, 19	7, 1.2, 32	3, 1.9, 14	2, 0.7, 8	2, 0.5, 9
2+80W	14, 1.7, 21	5, 0.9, 27	7, 1.1, 17	5, 0.8, 10	2, 0.7, 7
2+60W	30, 1.0, 22	5, 1.0, 13	14, 1.4, 14	6, 0.5, 10	2, 0.7, 12
2+40W	3, 0.1, 5	850, 37.9, 516	5, 1.0, 15	5, 0.4, 9	3, 0.6, 12
2+20W	17, 0.9, 19	160, 5.9, 106	45, 1.1, 33	5, 0.3, 10	2, 0.7, 12
2+00W	5, 1.3, 16	5, 2.3, 30	4, 1.4, 8	3, 0.7, 13	3, 0.3, 9
1+80W	4, 0.6, 10	14, 2.0, 22	6, 1.6, 14	2, 0.8, 11	2, (0.6), 6
1+60W	8, 0.8, 13	26, 1.6, 26	4, 1.8, 15	2, 0.8, 10	2, 0.8, 7
1+40W	41, 0.1, 16	9, 1.2, 23	4, 1.7, 18	3, 0.6, 15	6, 0.5, 10
1+20W	4, 1.0, 17	15, 1.0, 17	4, 0.9, 13	4, 1.1, 18	N.S.
1+00W	9, 0.8, 12	14, 0.5, 8	2, 0.6, 12	6, 0.7, 11	8, 1.2, 15
0+80W	4, 0.6, 18	3, 0.4, 3	6, 0.8, 13	4, 0.9, 14	3, 0.7, 10
0+60W	3, 0.2, 10	4, 0.6, 12	4, 0.6, 11	4, 0.8, 12	5, 0.4, 19
0+40W	3, 0.6, 10	6, 0.6, 14	4, 0.8, 15	12, 1.5, 25	2, 0.6, 11
0+20W	3, 0.6, 17	3, 0.8, 12	4, 0.8, 12	5, 1.3, 16	2, 0.2, 19
0+00W	3, 0.3, 16	5, 0.9, 11	6, 0.9, 16	4, 1.5, 15	7, 0.4, 15

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WHIPSAW CREEK PROPERTY
SOIL GEOCHEMISTRY
Au-ppb, Ag, As-ppm

FIG NO: 3

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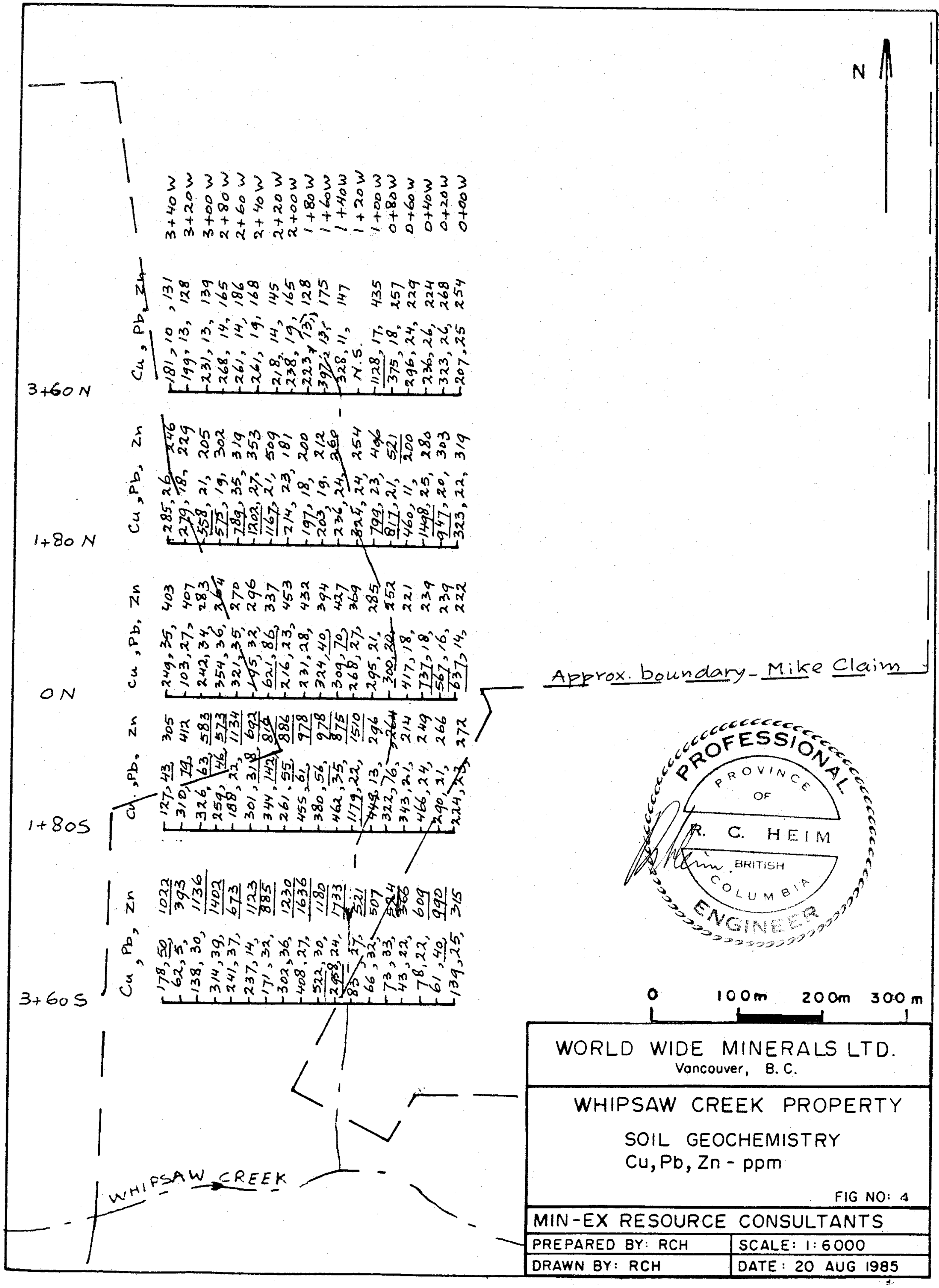

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SOIL GEOCHEMISTRY
Cu, Pb, Zn - ppm

FIG NO: 4

MIN-EX RESOURCE CONSULTANTS

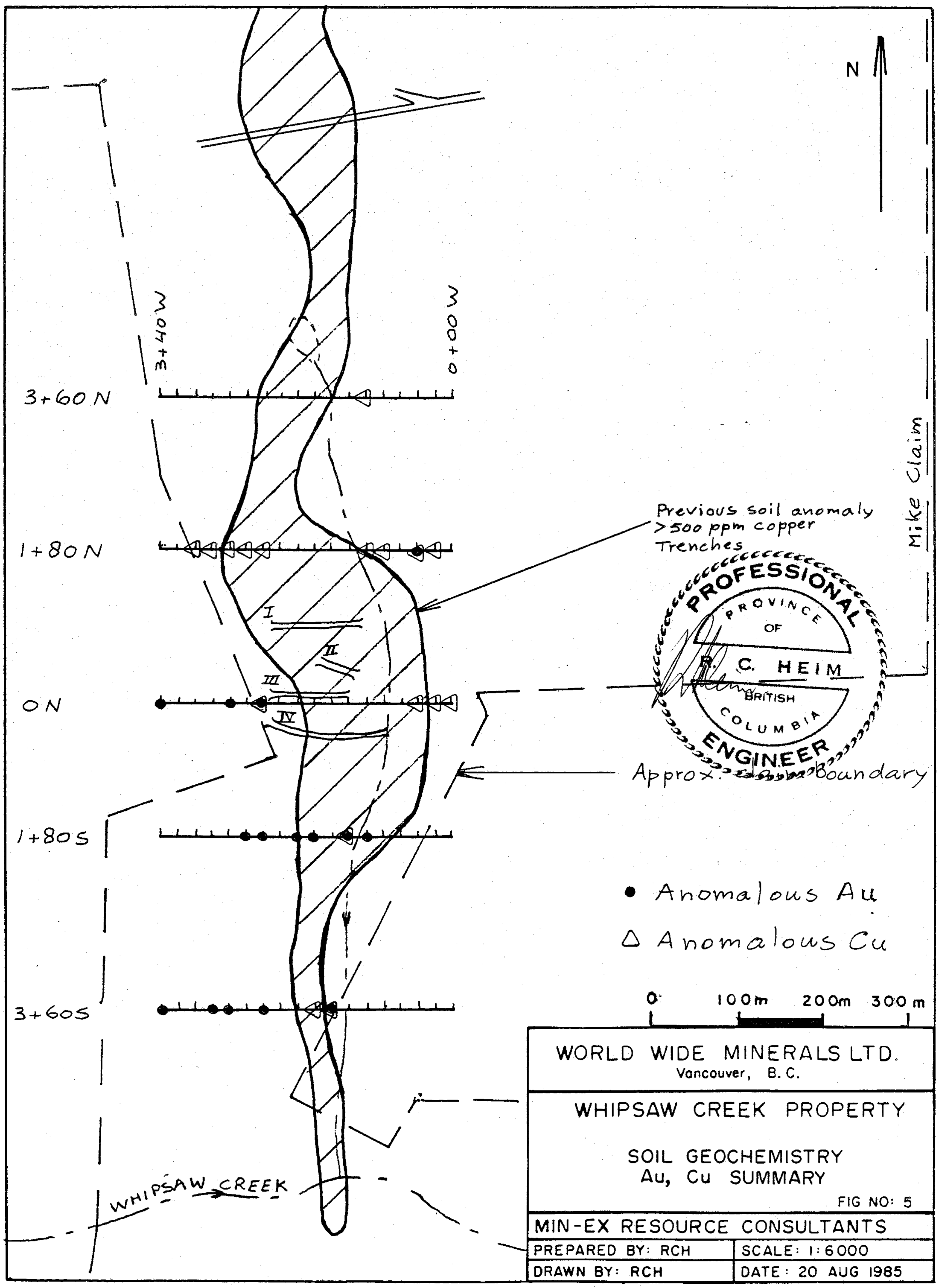
PREPARED BY: RCH	SCALE: 1:6000
DRAWN BY: RCH	DATE: 20 AUG 1985

3. DISCUSSION OF RESULTS

The orientation soil survey found a number of clearly anomalous gold values. It should be noted that the higher gold values tend to concentrate in the southern part of the grid and that they are generally found up-slope from the previously indicated copper soil anomaly. The spatial relationship between the established copper soil anomaly and the gold values reported in this study can be seen in Figure 5. Because the samples were taken from the C-horizon, the anomalous gold values probably reflect mineralization in the bedrock directly underlying the soil samples.

The extremely high copper background represents a confirmation and expansion of the previously indicated copper soil anomaly as previous work has established that the regional copper background is around 40 ppm, a fairly normal figure. This anomaly is elongated in a north-south direction and is 3,000 metres long and 1,000 metres wide (Figure 5) with copper values of more than 500 ppm and peaks of more than 1,000 ppm.

In the present survey, only the values in excess of 490 ppm were designated as being anomalous. This very high anomalous value is valid only for the present population of 90 samples. It indicates that the soil sampling lines are entirely contained within a large copper soil anomaly. Similarly, the very high nickel and chromium backgrounds (see assay sheets) are probably indicative of large nickel and chromium anomalies.



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SOIL GEOCHEMISTRY
Au, Cu SUMMARY

FIG NO: 5

MIN-EX RESOURCE CONSULTANTS

PREPARED BY: RCH	SCALE: 1:6000
DRAWN BY: RCH	DATE: 20 AUG 1985

4. RECOMMENDATIONS

A systematic compilation of all recorded previous work should be carried out.

Intermediate soil lines should be established between line 1+80 N and 3+60 S and the grid should be expanded to the south. All soil samples should be taken from the C-horizon, at depths of at least 30 centimetres. The samples should be assayed by the ICP method, with additional AA analyses for gold. Gold anomalies should be trenched or drilled.

The bedrock in the "Texas Gulf" trench, situated to the north of the present soil grid, should be sampled and assayed for precious metals.

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BRITISH COLUMBIA
ENGINEER

5. ITEMIZED COST STATEMENT

Soil Sampling; 90 samples, 3 man-days @ $100	$ 300.00
Report	343.00
Assays; 90 assays @ $10.60	954.00
Histograms	32.00
Transportation; truck rental, gasoline, taxi	270.94
Room & Board; 2 men, 2 days and 2 nights	171.00
Materials; 90 soil bags, topo maps, topofil, flagging	36.28
Total	$ 2,107.22

6. AUTHOR'S QUALIFICATIONS

I, Robert C. Heim, of North Vancouver, B.C., hereby certify the following:

1. I am a Senior Associate Geologist of Min-Ex Resource Consultants, the offices of which are located at 806 - 402 West Pender Street, Vancouver, B.C.

2. I have a Ph.D. (1952) degree in Geology from the University of Utrecht, Holland.

3. I have practised my profession since 1952, and have been an independent consultant since 1984.

4. I am a member of the Association of Professional Engineers of British Columbia and Ontario.

5. This report is based on the geochemical survey that I have carried out with Mr. John H. Perry, P.Geol., on August 12th and 13th, 1985.

Dated at Vancouver, B.C., this 12th day of September 1985.

R. C. HEIM

R.C. Heim, Ph.D., P.Eng.

APPENDICES

APPENDIX A

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS -80 MESH AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 14 1985 DATE REPORT MAILED: Aug 16/85 ASSAYER. T. Saundry .DEAN TOYE OR TOM SAUNDRY. CERTIFIED B.C. ASSAYER

MIN-EX CONSULTING LTD PROJECT - 85-WS FILE # 85-1866 PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
3+60N 3+40W	3	181	10	131	.7	34	11	305	3.09	8	5	ND	2	13	1	2	2	67	.13	.10	2	64	1.04	57	.10	3	2.01	.02	.03	1	2
3+60N 3+20W	3	199	13	128	.4	38	12	318	3.22	8	5	ND	1	13	1	2	2	69	.13	.08	2	72	1.20	62	.10	2	2.11	.02	.03	1	1
3+60N 3+00W	3	231	13	139	.5	38	11	275	3.26	9	5	ND	2	16	1	2	2	69	.16	.09	3	65	1.07	80	.11	3	2.26	.02	.02	1	2
3+60N 2+80W	4	268	14	165	.7	35	12	490	2.91	7	5	ND	1	19	1	2	2	62	.19	.07	3	65	1.02	82	.11	3	2.19	.02	.03	1	2
3+60N 2+60W	5	261	14	186	.7	35	12	284	3.35	12	7	ND	2	15	1	2	2	69	.15	.10	3	61	.94	72	.12	3	2.26	.01	.04	1	2
3+60N 2+40W	5	261	19	168	.6	41	14	349	3.57	12	5	ND	3	15	1	2	2	74	.14	.12	4	74	1.18	66	.12	2	2.49	.02	.03	1	3
3+60N 2+20W	4	218	14	145	.7	32	10	287	3.26	12	5	ND	2	13	1	2	2	66	.13	.12	2	61	.92	53	.11	3	2.08	.02	.03	1	2
3+60N 2+00W	4	238	19	165	.3	39	13	423	3.47	9	5	ND	2	17	1	2	2	69	.15	.13	3	75	1.16	66	.11	2	2.24	.02	.04	1	5
3+60N 1+80W	4	223	13	128	.6	26	6	222	2.83	6	5	ND	1	11	1	2	2	61	.10	.11	3	53	.71	49	.14	3	1.96	.01	.01	1	2
3+60N 1+60W	15	397	13	175	.8	41	7	244	4.60	7	16	ND	4	26	1	2	4	104	.12	.13	5	118	1.41	157	.20	2	3.28	.02	.07	1	2
3+60N 1+40W	17	328	11	147	.5	31	5	229	4.22	10	5	ND	2	11	1	2	2	98	.08	.10	2	95	1.20	80	.17	2	2.36	.02	.04	1	6
3+60N 1+00W	6	1128	17	435	1.2	66	18	362	3.97	15	5	ND	1	25	1	5	2	89	.46	.04	6	104	1.65	83	.14	2	2.51	.02	.05	1	8
3+60N 0+80W	2	375	18	257	.7	42	11	329	3.29	10	5	ND	2	22	1	2	3	72	.33	.08	3	68	1.13	96	.13	3	2.14	.01	.05	1	3
3+60N 0+60W	5	296	24	229	.4	57	14	475	4.18	19	5	ND	1	29	1	2	2	85	.46	.07	4	100	1.81	87	.12	2	2.26	.02	.06	1	5
3+60N 0+40W	2	236	26	224	.6	44	9	241	2.91	11	5	ND	1	20	1	2	2	62	.31	.05	4	54	.97	70	.12	2	1.81	.02	.04	1	2
3+60N 0+20W	6	323	26	268	.2	57	13	363	3.79	19	5	ND	1	24	1	2	2	81	.37	.06	5	90	1.59	88	.13	3	2.12	.02	.09	1	2
3+60N 0+00W	3	207	25	254	.4	47	10	291	3.21	15	5	ND	2	21	1	2	2	72	.30	.06	3	74	1.36	60	.12	2	1.95	.02	.04	1	7
1+80N 3+40W	7	285	26	246	1.3	44	12	256	3.45	11	5	ND	2	15	1	2	4	72	.14	.08	3	80	1.13	69	.13	2	2.29	.02	.03	1	4
1+80N 3+20W	9	279	18	229	1.3	45	12	259	3.12	8	5	ND	2	14	1	2	2	69	.14	.09	3	101	1.24	81	.13	2	2.28	.02	.02	1	2
1+80N 3+00W	10	558	21	205	.7	47	13	256	3.70	8	5	ND	3	16	1	2	2	74	.12	.07	3	76	1.05	84	.14	3	2.57	.01	.03	1	2
1+80N 2+80W	17	575	19	302	.8	45	7	164	3.28	10	5	ND	2	15	1	2	4	63	.14	.07	3	71	.72	56	.13	2	2.25	.02	.03	1	5
1+80N 2+60W	26	789	35	319	.5	41	8	184	4.02	10	5	ND	2	22	1	4	2	75	.19	.05	3	65	.93	65	.08	2	1.71	.02	.06	1	6
1+80N 2+40W	19	1202	27	353	.4	76	18	323	3.86	9	5	ND	2	31	1	2	2	70	.32	.04	4	106	1.32	73	.12	3	2.56	.01	.06	1	5
1+80N 2+20W	8	1167	21	509	.3	86	13	283	3.19	10	5	ND	3	27	1	2	2	66	.31	.04	3	86	1.37	56	.12	3	2.31	.02	.09	1	5
1+80N 2+00W	5	214	23	181	.7	37	11	225	3.08	13	5	ND	1	15	1	2	2	67	.14	.08	4	63	.94	59	.12	2	2.10	.01	.02	1	3
1+80N 1+80W	3	197	18	200	.8	43	13	270	3.27	11	5	ND	2	16	1	2	2	69	.14	.10	2	74	1.11	60	.11	2	2.15	.01	.04	1	2
1+80N 1+60W	2	203	19	212	.8	43	13	323	3.21	10	5	ND	3	16	1	2	2	67	.15	.11	5	71	1.09	75	.11	2	2.21	.01	.03	1	2
1+80N 1+40W	3	236	24	260	.6	44	13	316	3.26	15	5	ND	1	15	1	2	2	67	.14	.11	2	74	1.02	68	.11	2	2.21	.01	.03	1	3
1+80N 1+20W	5	324	24	254	1.1	43	13	322	3.57	18	5	ND	2	17	1	2	2	75	.16	.13	2	78	1.05	76	.12	2	2.30	.01	.04	1	4
1+80N 1+00W	10	799	23	496	.7	60	25	477	3.50	11	5	ND	3	17	1	2	2	74	.18	.07	3	84	1.27	52	.11	2	2.40	.01	.03	1	6
1+80N 0+80W	5	817	21	521	.9	63	17	340	3.18	14	5	ND	2	14	1	2	2	62	.13	.08	3	61	.81	70	.13	2	2.53	.02	.03	1	4
1+80N 0+60W	6	460	11	200	.8	33	9	229	3.51	12	5	ND	2	11	1	2	5	76	.09	.12	3	72	.90	71	.16	2	2.88	.02	.02	1	4
1+80N 0+40W	36	1498	25	250	1.5	62	14	391	6.26	25	5	ND	3	35	1	2	2	145	.19	.09	5	183	2.68	185	.21	3	3.46	.02	.16	1	12
1+80N 0+20W	10	947	20	303	1.3	53	13	281	3.82	16	5	ND	3	15	1	2	2	86	.14	.06	4	96	1.31	71	.15	2	2.66	.01	.04	1	5
1+80N 0+00W	5	323	22	319	1.5	54	10	238	3.40	15	5	ND	2	22	1	2	2	73	.26	.06	4	72	1.10	94	.12	2	2.47	.01	.06	1	4
0+00N 3+40W	3	249	35	403	1.4	46	13	370	3.45	13	5	ND	1	19	1	2	2	71	.21	.09	4	87	1.35	72	.11	3	2.15	.01	.04	1	38
STD C/AU-0.5	20	58	39	133	7.0	68	26	1161	3.97	38	17	8	36	51	16	15	22	59	.48	.13	37	55	.87	174	.07	41	1.55	.06	.09	12	480

MIN-EX CONSULTING LTD PROJECT - 85-WS FILE # 85-1866

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
0+00N 3+20W	2	103	27	407	1.2	31	9	367	2.90	6	5	ND	2	14	1	2	2	62	.16	.09	5	56	.86	102	.12	2	1.97	.01	.05	1	2
0+00N 3+00W	3	242	34	283	1.9	47	15	419	3.64	14	5	ND	2	18	1	2	2	75	.17	.11	8	81	1.22	77	.13	2	2.85	.01	.04	1	3
0+00N 2+80W	5	354	36	264	1.1	46	14	633	3.86	17	5	ND	2	20	1	2	2	76	.19	.11	6	85	1.16	87	.11	2	2.70	.01	.08	1	7
0+00N 2+60W	5	321	35	270	1.4	46	15	416	3.56	14	5	ND	2	19	1	2	4	71	.18	.09	6	82	1.13	84	.12	2	2.49	.01	.04	1	14
0+00N 2+40W	3	195	32	296	1.0	41	12	472	3.08	15	5	ND	2	17	1	2	2	63	.17	.08	6	66	.92	85	.11	2	2.31	.01	.05	1	5
0+00N 2+20W-C	23	621	86	337	1.1	52	10	495	5.50	33	5	ND	3	78	1	3	3	100	.33	.08	10	163	1.78	152	.13	3	2.73	.01	.21	1	45
0+00N 2+20W-B	3	212	27	438	1.4	39	12	358	3.03	13	5	ND	2	20	1	2	4	63	.20	.07	5	65	.84	70	.11	2	2.19	.01	.05	1	3
0+00N 2+00W	3	216	23	453	1.4	42	12	294	2.99	8	5	ND	2	15	1	2	2	62	.15	.08	7	69	.91	80	.12	2	2.34	.01	.05	1	4
0+00N 1+80W	5	231	28	432	1.6	40	12	327	3.04	14	5	ND	3	14	1	4	5	64	.16	.09	5	66	.88	70	.10	2	2.22	.01	.06	1	6
0+00N 1+60W	5	324	40	394	1.8	43	13	432	3.66	15	5	ND	2	20	1	2	3	73	.20	.09	5	74	.98	87	.12	2	2.45	.02	.06	1	4
0+00N 1+40W	5	309	70	427	1.7	35	12	401	3.74	18	5	ND	3	29	1	2	3	70	.15	.12	8	68	.84	112	.12	2	2.53	.01	.07	1	4
0+00N 1+20W	3	268	27	369	.9	37	13	415	2.99	13	5	ND	3	21	1	2	2	59	.20	.11	5	56	.74	66	.11	2	2.19	.01	.06	1	2
0+00N 1+00W	4	295	21	285	.6	37	13	346	3.15	12	5	ND	2	20	1	2	2	64	.16	.09	5	63	.92	67	.11	2	2.14	.01	.04	1	2
0+00N 0+80W	6	300	20	252	.8	28	9	295	2.96	13	5	ND	2	11	1	2	2	59	.10	.11	6	47	.54	43	.12	2	2.42	.02	.04	1	8
0+00N 0+60W	5	417	18	221	.6	32	10	239	3.11	11	5	ND	3	11	1	2	2	70	.11	.13	6	60	.81	56	.14	2	2.61	.01	.03	1	4
0+0CN 0+40W	8	737	18	239	.8	44	14	309	3.79	15	5	ND	3	16	1	2	2	84	.14	.07	6	87	1.20	82	.15	2	2.79	.01	.04	1	4
0+00N 0+20W	6	567	16	239	.8	38	12	349	3.23	12	5	ND	2	14	1	2	2	73	.13	.10	7	73	.97	60	.13	2	2.76	.01	.04	1	4
0+00N 0+00W	8	637	14	222	.9	42	13	304	3.63	16	5	ND	2	15	1	2	2	81	.13	.06	6	80	1.11	70	.15	2	2.78	.02	.04	1	6
1+80S 3+40W	1	127	43	305	1.1	23	9	568	3.41	16	5	ND	2	11	1	2	2	77	.16	.11	4	46	.73	41	.12	2	1.89	.01	.03	1	6
1+80S 3+20W	6	310	79	412	.8	30	14	849	3.87	39	5	ND	2	21	1	2	2	83	.23	.09	6	52	1.02	115	.11	2	2.50	.01	.06	1	6
1+80S 3+00W	5	326	63	583	1.2	34	14	563	3.67	32	5	ND	2	21	1	2	2	77	.27	.10	8	59	.99	117	.12	3	2.48	.01	.06	1	7
1+80S 2+80W	4	259	46	573	.9	41	13	480	3.27	27	5	ND	2	21	1	3	2	71	.25	.08	5	75	.95	86	.12	2	2.25	.01	.06	1	5
1+80S 2+60W	1	188	22	1134	1.0	48	10	596	2.93	13	5	ND	2	18	1	2	2	70	.29	.05	4	89	1.10	53	.17	2	2.15	.01	.03	1	5
1+80S 2+40W	5	301	318	692	37.9	32	8	468	5.21	516	5	ND	3	13	2	31	40	59	.15	.09	4	70	.74	68	.08	2	1.73	.01	.09	1	856
1+80S 2+20W	4	344	142	816	5.9	46	14	461	4.16	106	5	ND	3	18	1	2	6	73	.19	.08	4	95	1.13	94	.11	2	2.33	.01	.06	1	160
1+80S 2+00W	3	261	55	886	2.3	49	15	468	3.47	30	5	ND	2	18	1	2	2	71	.23	.08	5	86	1.10	78	.12	2	2.30	.01	.06	1	5
1+80S 1+80W	5	455	61	978	2.0	60	17	520	3.87	22	5	ND	2	16	1	2	2	76	.24	.10	7	96	1.22	65	.12	2	2.47	.01	.05	1	14
1+80S 1+60W	4	380	56	978	1.6	55	16	551	3.47	26	5	ND	3	14	1	2	2	67	.18	.09	6	96	1.13	73	.12	2	2.23	.01	.05	1	26
1+80S 1+40W	5	462	35	875	1.2	51	16	540	3.57	23	5	ND	2	17	1	2	2	74	.21	.10	5	80	1.05	78	.13	2	2.29	.01	.05	1	9
1+80S 1+20W	8	1179	22	1510	1.0	70	15	318	3.72	17	5	ND	3	12	1	2	2	77	.15	.08	6	88	1.14	48	.13	2	2.52	.01	.04	1	15
1+80S 1+00W	6	449	13	296	.5	52	14	348	3.32	8	5	ND	3	30	1	2	2	75	.33	.07	6	95	1.48	79	.12	2	2.08	.02	.06	1	14
1+80S 0+80W	2	322	16	264	.4	42	12	341	2.64	3	5	ND	2	27	1	2	2	58	.28	.06	5	74	1.09	77	.10	2	1.98	.01	.04	1	3
1+80S 0+60W	5	343	21	214	.6	43	12	274	3.08	12	5	ND	2	21	1	2	2	65	.19	.10	5	73	1.04	81	.10	2	2.27	.01	.05	1	4
1+80S 0+40W	6	466	24	249	.6	48	15	326	3.38	14	5	ND	2	20	1	2	2	72	.21	.10	6	86	1.22	89	.11	2	2.34	.01	.06	1	6
1+8CS 0+20W	3	290	21	266	.8	41	12	285	3.00	12	5	ND	2	17	1	2	2	65	.16	.09	5	70	.94	82	.11	2	2.28	.01	.05	1	3
1+80S 0+00W	3	224	23	272	.9	39	12	288	2.96	11	5	ND	2	18	1	2	2	64	.17	.08	6	66	.96	76	.11	2	2.22	.01	.04	1	5
STD C/AU 0.5	21	59	41	137	7.0	71	26	1184	3.99	39	19	8	38	52	16	15	20	60	.48	.13	37	59	.88	177	.07	41	1.72	.06	.10	12	495

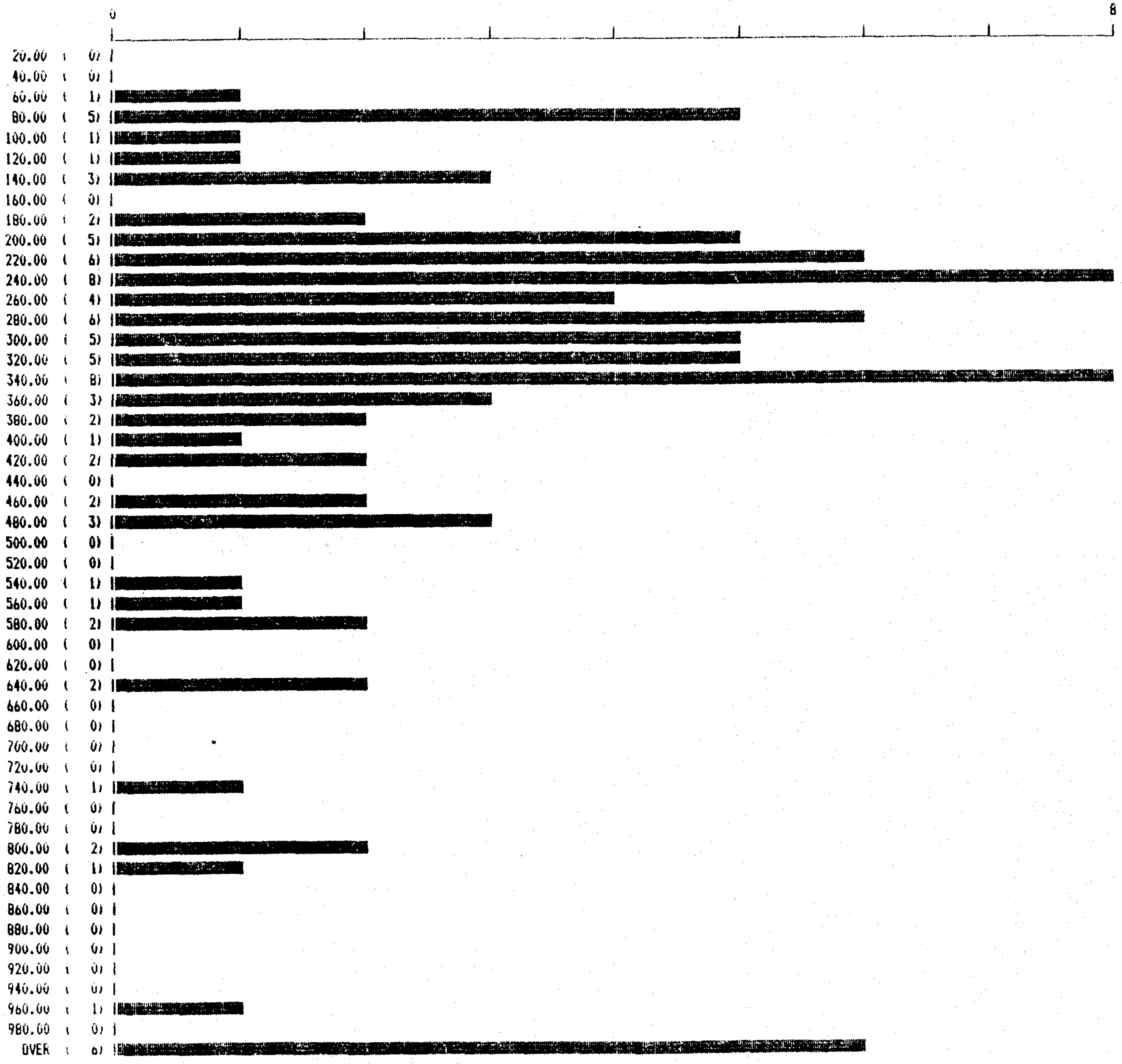
MIN-EX CONSULTING LTD PROJECT - 85-WS FILE # 85-1866

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
3+60S 3+40W	2	178	50	1022	.3	45	14	736	3.17	25	5	ND	1	17	1	2	2	68	.27	.09	2	88	1.05	79	.13	3	2.34	.01	.08	1	39
3+60S 3+20W	1	62	5	393	.1	27	11	680	2.77	3	5	ND	1	13	2	2	2	70	.34	.10	2	52	.96	87	.17	4	1.52	.02	.12	1	3
3+60S 3+00W	1	138	30	1136	.8	44	13	356	3.19	19	5	ND	2	18	2	2	2	65	.25	.09	2	65	.95	94	.14	3	2.52	.02	.08	1	4
3+60S 2+80W	2	314	39	1402	1.7	48	12	305	3.26	21	5	ND	1	16	1	2	2	69	.28	.06	2	77	.99	66	.13	3	2.35	.02	.06	1	14
3+60S 2+60W	2	241	37	673	1.0	42	12	341	3.17	22	5	ND	2	18	1	2	3	67	.26	.06	2	76	1.01	95	.12	5	2.26	.01	.08	1	30
3+60S 2+40W	1	237	14	1123	.1	76	15	489	3.16	5	8	ND	1	19	1	2	4	69	.42	.05	2	160	2.23	54	.21	2	2.67	.01	.04	1	3
3+60S 2+20W	1	171	32	885	.9	47	13	502	3.44	19	8	ND	1	22	2	2	3	72	.30	.06	2	80	1.19	114	.13	5	2.54	.02	.07	1	17
3+60S 2+00W	1	302	36	1230	1.3	58	14	540	3.59	16	6	ND	2	19	2	2	6	73	.29	.08	2	103	1.34	117	.15	2	2.76	.02	.09	1	5
3+60S 1+80W	2	408	27	1636	.6	57	15	536	3.58	10	5	ND	1	24	2	2	3	75	.38	.09	2	85	1.29	62	.12	2	2.52	.02	.06	1	4
3+60S 1+60W	4	522	30	1180	.8	56	19	545	3.48	13	5	ND	1	20	1	2	2	74	.28	.06	2	87	1.15	72	.13	2	2.47	.01	.06	1	8
3+60S 1+40W	6	2958	24	1733	.1	174	47	467	3.49	16	5	ND	1	22	1	2	2	68	.25	.05	2	80	1.21	109	.10	4	2.78	.02	.05	1	41
3+60S 1+20W	1	83	27	521	1.0	46	11	311	3.09	17	5	ND	1	19	1	2	2	67	.20	.07	2	74	1.06	77	.13	3	2.24	.01	.07	1	4
3+60S 1+00W	1	66	32	507	.8	41	11	438	3.07	12	5	ND	1	15	1	2	2	70	.19	.07	2	65	1.03	72	.14	2	2.17	.01	.06	1	9
3+60S 0+80W	1	73	33	524	.6	44	12	415	3.61	18	5	ND	1	18	1	5	2	79	.29	.03	2	91	1.51	60	.12	2	2.23	.02	.10	1	4
3+60S 0+60W	1	43	22	366	.2	41	11	681	3.16	10	5	ND	1	25	1	2	2	68	.31	.06	2	72	1.29	63	.11	3	2.11	.01	.09	1	3
3+60S 0+40W	1	78	22	609	.6	39	11	542	3.03	10	5	ND	1	22	1	2	2	63	.25	.09	2	64	1.09	90	.12	2	2.20	.01	.05	1	3
3+60S 0+20W	1	61	40	990	.6	35	11	814	3.08	17	5	ND	2	18	2	2	2	66	.23	.10	2	54	.82	97	.14	2	2.17	.02	.07	1	3
3+60S 0+00W	1	139	25	315	.3	51	15	530	3.86	16	5	ND	1	20	1	2	2	83	.31	.05	2	99	1.74	92	.13	3	2.35	.01	.20	1	3
STD C/AU-0.5	21	53	40	134	7.0	71	25	1172	3.98	39	15	8	36	51	16	15	21	59	.48	.13	37	57	.88	173	.07	40	1.72	.06	.11	11	480

APPENDIX B

MIN-EX CONSULTING LTD PROJECT - 85-WS FILE # 85-1866

CU (PPM)



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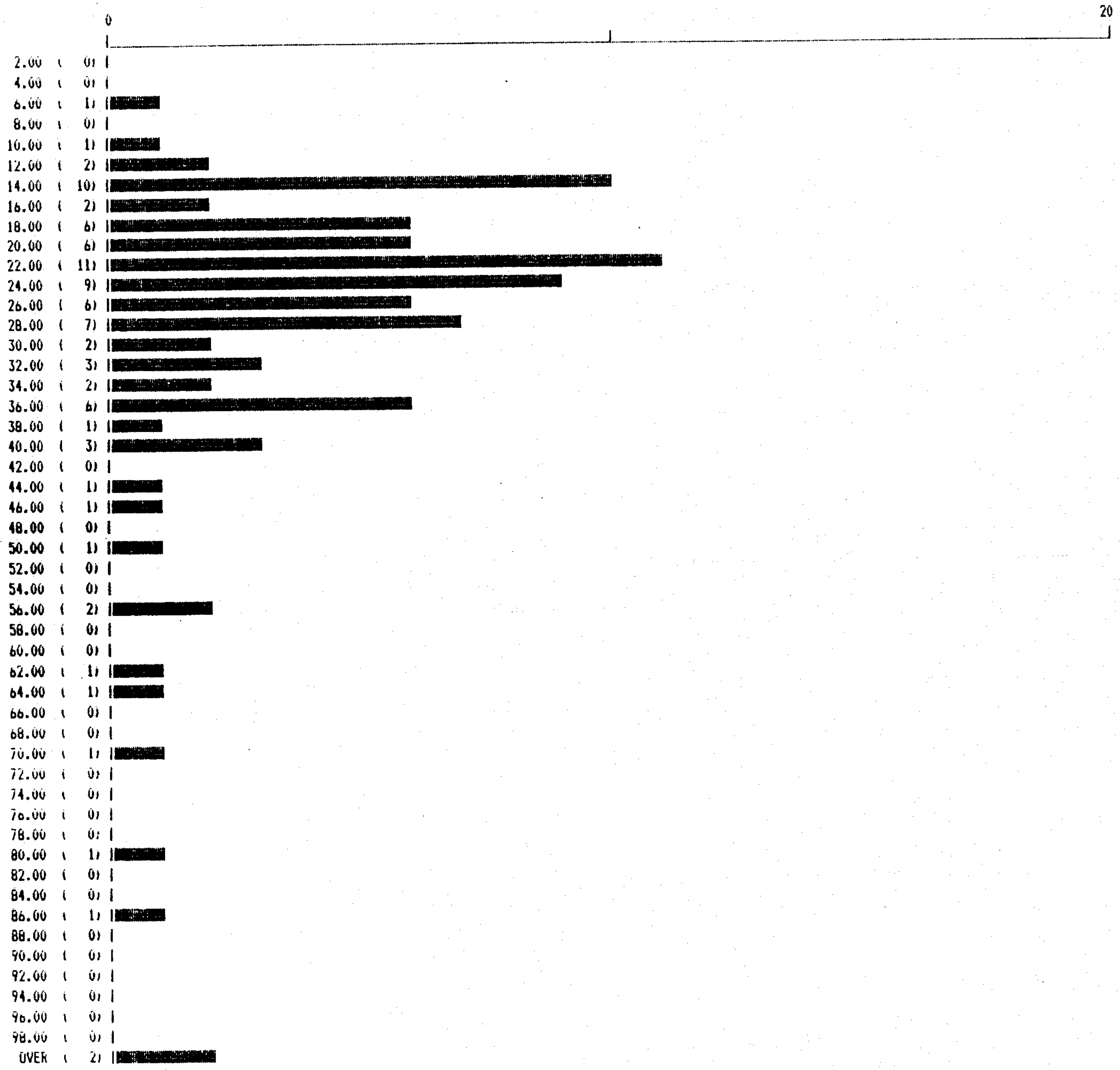
SAMPLE SIZE :    90    MAX :    2958    MIN :      43    MEDIAN  : 295
                       MEAN :  395.79   S.D. :  386.28
```

MIN-EX CONSULTING LTD PROJECT - 85-WS FILE # 85-1866

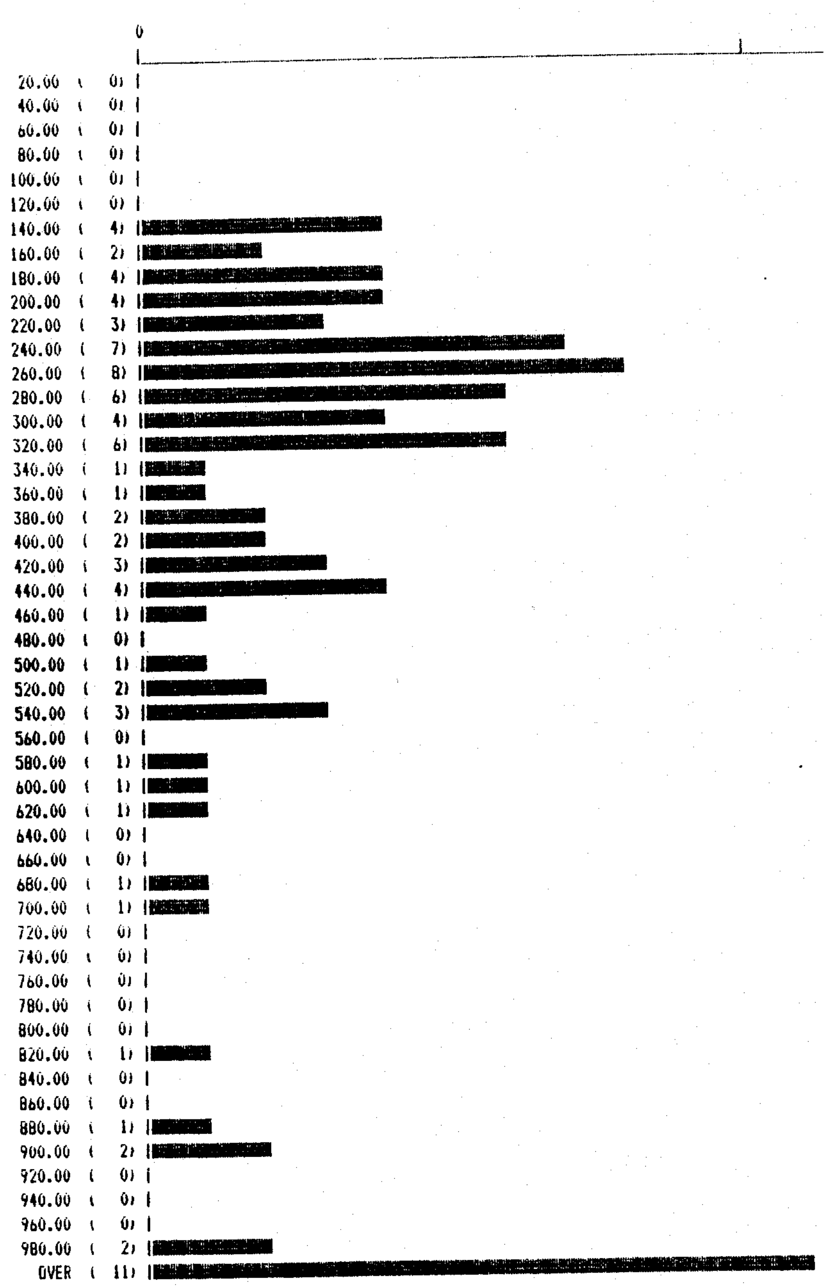
PB (PPM)



SAMPLE SIZE : 90 MAX : 318 MIN : 5 MEDIAN : 24
MEAN : 31.98 S.D. : 35.71

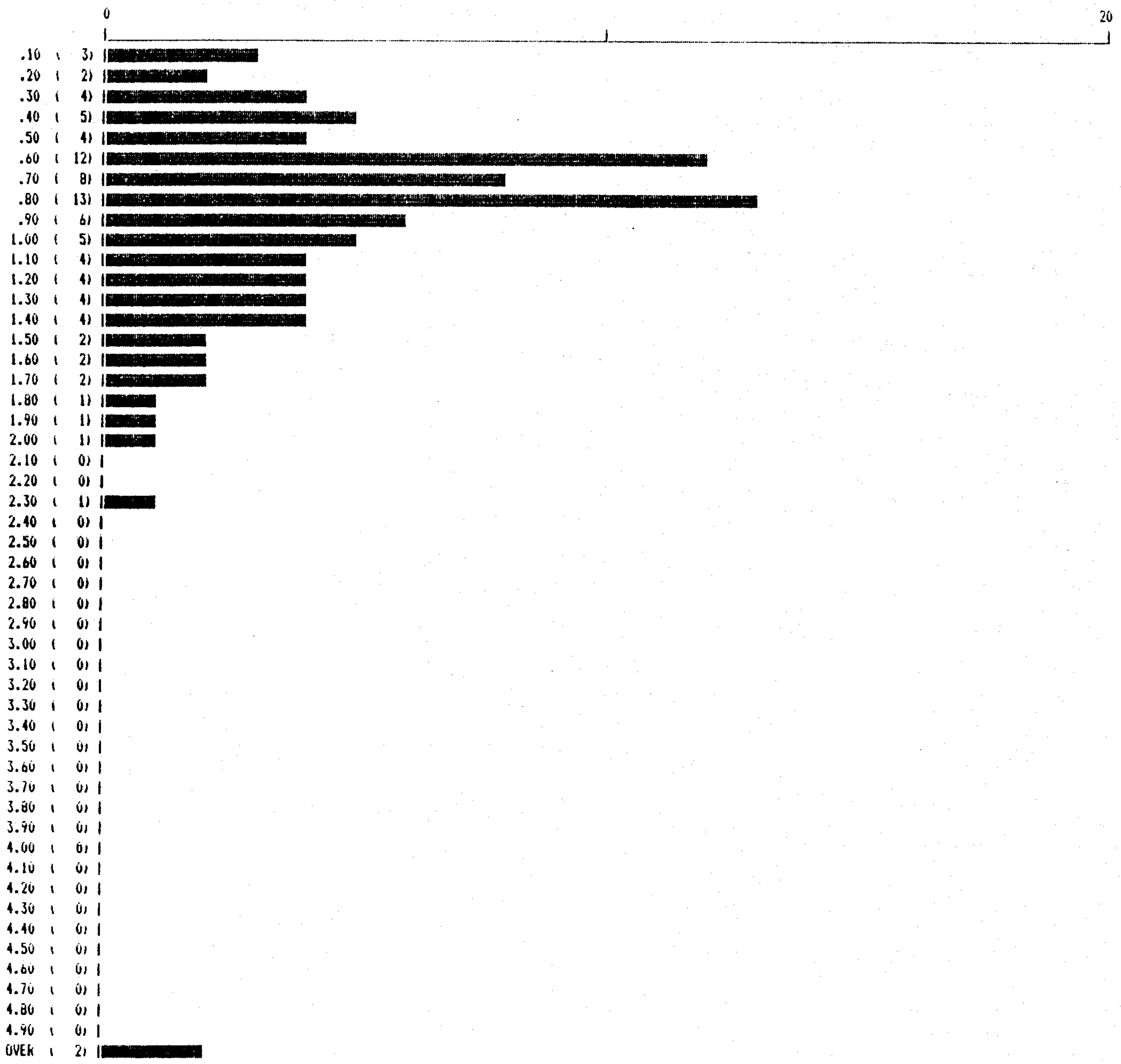
MIN-EX CONSULTING LTD PROJECT - 85-WS FILE # 85-1866

ZN (PPM)



SAMPLE SIZE : 90 MAX : 1733 MIN : 128 MEDIAN : 305
MEAN : 472.02 S.D. : 366.71

MIN-Ex CONSULTING LTD PROJECT - 85-WS FILE # 85-1866 AG (PPM)



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SAMPLE SIZE :     90     MAX  :     37.9     MIN  :        .1     MEDIAN  : .6
                         MEAN :     1.34     S.D. :     3.94
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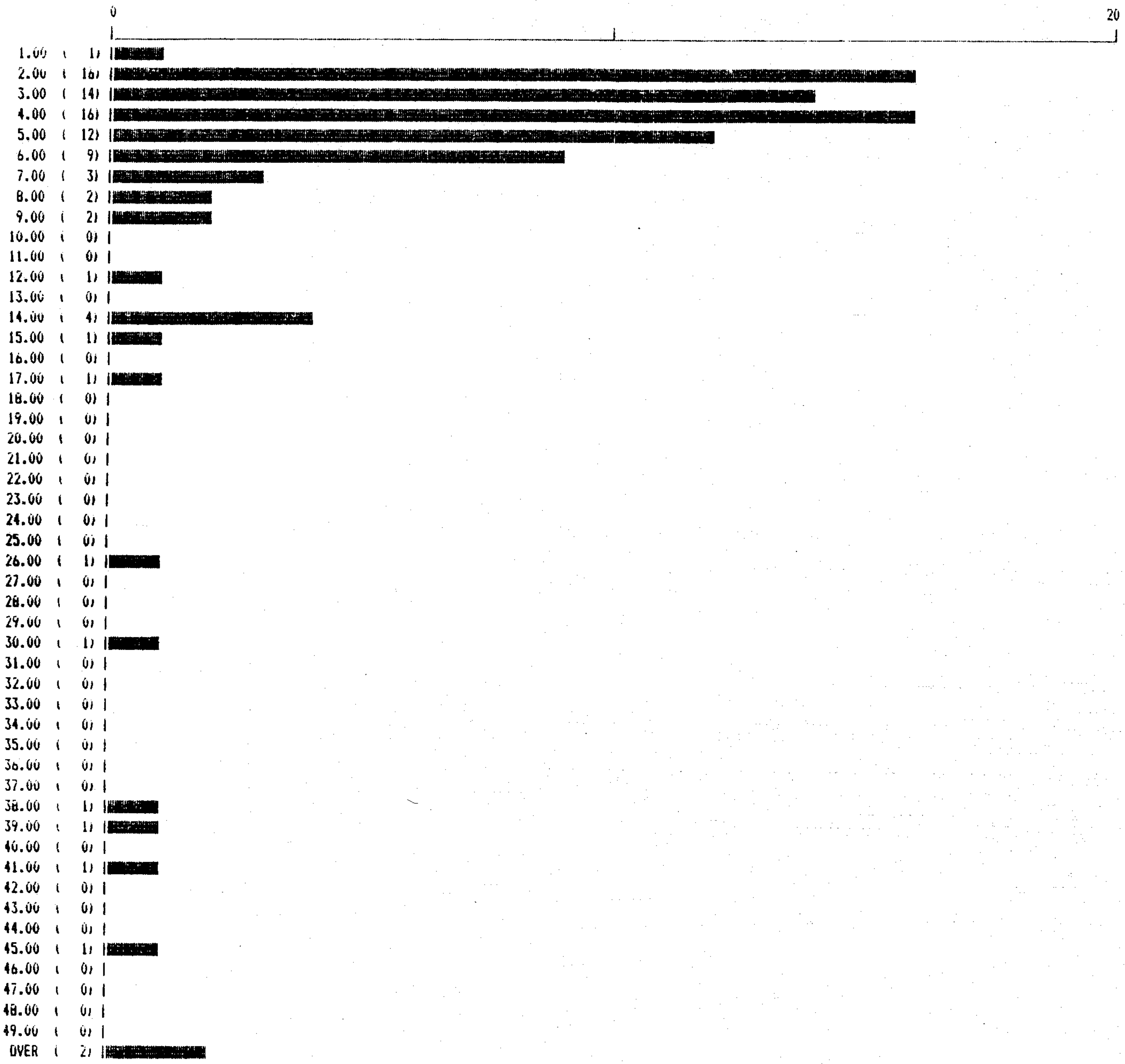
MIN-EX CONSULTING LTD PROJECT - 85-WS FILE # 85-1866 AU* (PPB)



SAMPLE SIZE : 90 MAX : 850 MIN : 1 MEDIAN : 4
MEAN : 18.19 S.D. : 90.03