85-910-14062

REPORT ON

GRID CONSTRUCTION, GEOCHEMISTRY AND GEOPHYSICS

ON THE

P.D.L. MINERAL CLAIM

OSOYOOS MINING DIVISION

N.T.S. 82 E 5

LATITUDE 49° 22' N LONGITUDE 119° 48' W

OWNER OF CLAIM

PLACER DEVELOPMENT LIMITED

OPERATOR

PLACER DEVELOPMENT LIMITED

R.J. YOUNG GEOLOGICAL BRANCH VEMBER 1985 ASSESSMENT REPORT

14,062

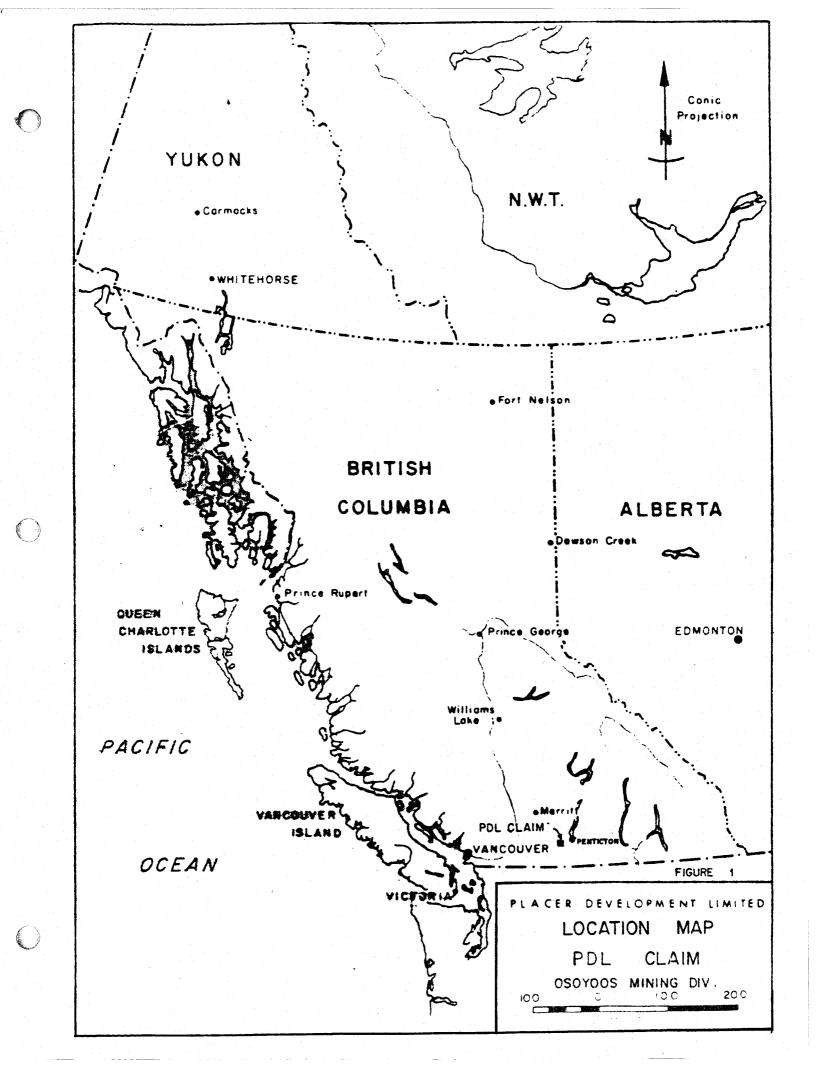


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1. INTRODUCTION

Placer Development Limited carried out an exploration program on the P.D.L. claim, in the Osoyoos Mining Division, consisting of grid construction, soil geochemistry, and geophysics. This report describes the work carried out and the results of that program.

2. SUMMARY

A grid consisting of 1.7 km of baseline and 13.05 km of sideline was constructed.

244 soil samples were collected from the grid. These were analysed for Au, As, Cu, Mo and W.

Magnetometer and V.L.F. - EM surveys were conducted over 5.32 line km# of the grid lines.

The grid plan is presented on a 1:10,000 scale plan, the geochemical and geophysical results are presented on 1:5000 scale plans.

Significant geocehmical response for Au and As is confined to the eastern portion of the grid (east wall of valley). Cu response is high (+100 ppm) over almost the entire grid. Mo and W response is minimal.

No significant magnetic response was detected.

Four V.L.F. conductors were noted. These appear to be due to topographic effect.

Cost for the work totalled \$13,944.70.

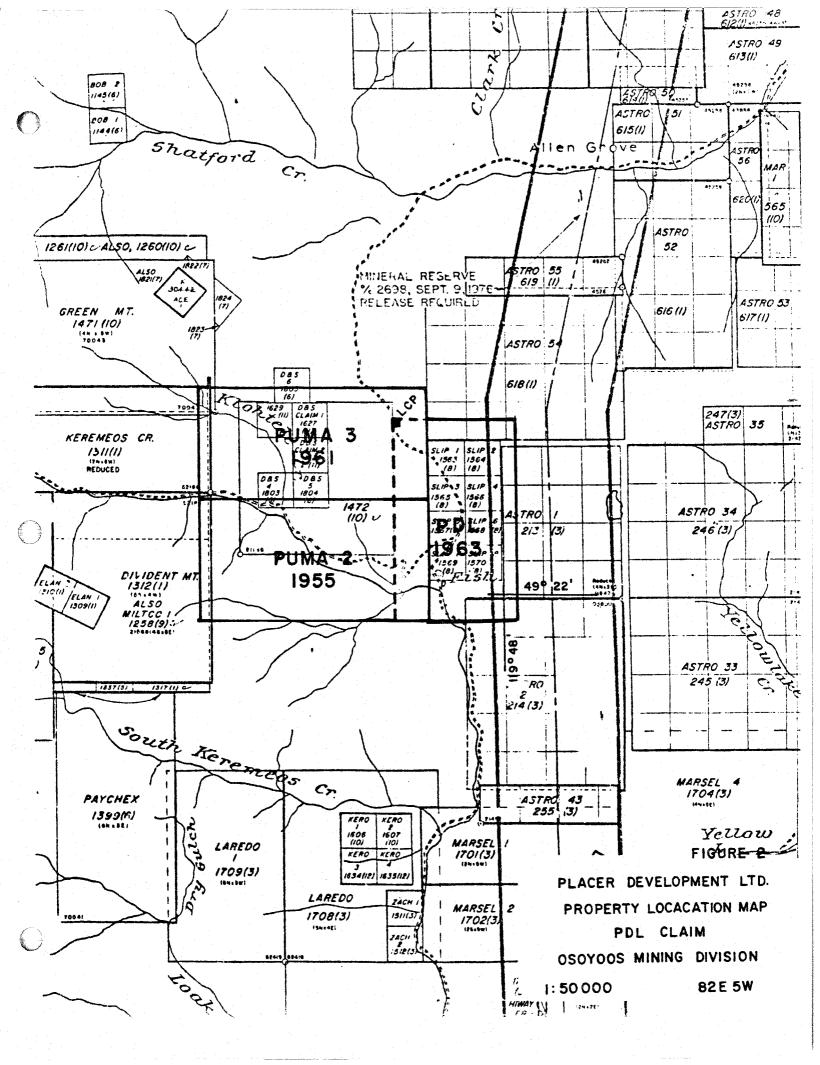
Geologic mapping, trenching and diamond drilling are recommended.

3. PROPERTY DEFINITION

The property consists of the 15 unit P.D.L. Claim. Record No. is 1963 and the anniversary date is December 23. The claim location is shown in Figs. 1 and 2.

4. TOPOGRAPHY, COVER AND ACCESS

The claim covers the valley bottom and adjacent slopes of a 2.5 km portion of Keremeos Creek. The valley bottom is relatively narrow. The adjacent slopes are steep and rugged with numerous talus slopes and rock bluffs.



The area is moderately well forested with fir and/or pine. There is only a moderate amount of underbrush.

Access is extremely easy. The Green Mountain road, a good gravel road in this section, is located within the westerly side of the claims. It can be accessed from a point approximately 6 km northerly from Keremeos on Highway 3A, or from a point approximately 20 km westerly from Penticton on the Apex Alpine ski resort access road.

5. ECONOMIC ASSESSMENT

No economic mineralization is known to exist on the property.

Two small massive sulphide showings are known. They consist of "massive" pyrrhotite and/or pyrite plus minor chalcopyrite. Minor Au values accompany the massive sulphides. However, the geochemical results suggest that sources other than the known mineralization are responsible for the anomalous results. Thus other showings are likely to be uncovered by further work.

6. WORK DONE

The work done was carried out from June to September 1985.

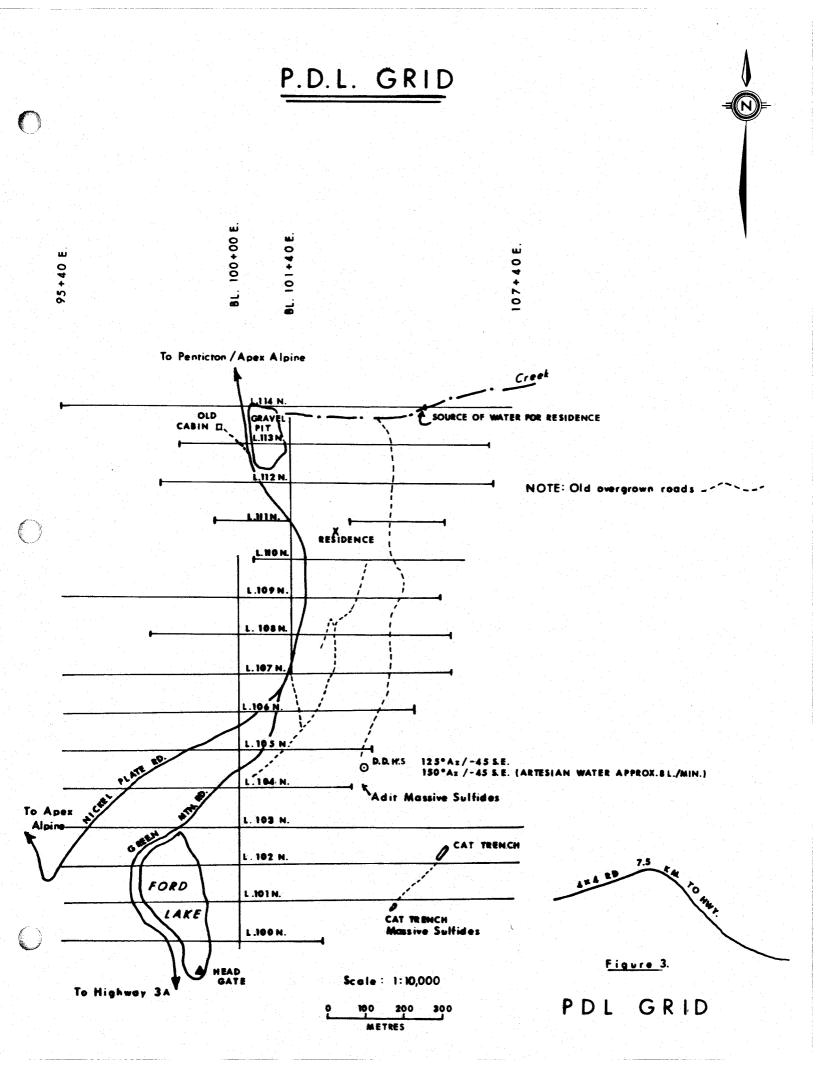
6:1 <u>GRID</u> A grid consisting of 1,700 meters of baselines and 13,050 m of sidelines was constructed under contract by Leo Reichert of Keremeos. The baselines runs north-south. The rugged topography caused some duplication and offsetting of the baseline. Lines were set at 100 m intervals along the baseline(s). Stations were set at 20 m intervals along the lines. Only a few lines were constructed to the planned limit - most were terminated by the topography. The grid is shown on Fig. 3.

6:2 <u>SOIL GEOCHEMICAL SURVEY</u> Samples were collected at 40 m intervals on all sidelines except where the lines traverse valley till.

A total of 244 samples was collected.

The B soil horizon was sampled. In some locations only talus was available and where necessary, fines from this material was collected.

All samples were analysed for Au, As, Cu, Mo and W.



Plans showing the posted values were prepared. These were hand contoured.

6:2:1 SAMPLE PREPARATION AND ANALYTICAL PROCEDURES

All samples for this program were prepared and assayed by Placer Development Limited Geochemical Laboratory in Vancouver, B.C.

i) Analysis for Cu, Mo and As

All samples are dried in a hot-air dryer. The soil samples are then sifted in -80 mesh nylon seives.

Following the drying and sieving process, a 0.50 gm portion of -80 mesh fraction of soil is weighed with a precision torsion balance. Samples were digested in hot solution of HNO3 and HC104 for three and a half hours, then cooled, diluted and prepared for analysis on Perkin-Elmer 603 Atomic Absorption Spectophotometer for Cu, Mo and As.

Detection limits and ranges are listed below:

Metal	Detection Limit & Range
Copper	2 - 4,000 ppm
Molybdenum	1 - 1,000 ppm
Arsenic	2 - 1,000 ppm

ii) Analysis for Au

Following the drying and seiving process, a 10.0 gm portion of -80 mesh fraction of soil talus-fine or conventional sediment of -150 mesh fraction of the bulk sediments of rock is mixed with aqua regia and heated at 600° celsius for three hours, the HBr solution is added and allowed to stand overnight. Water and MIBr solution are added, shaken, contrifuged and then 1% HBr in water is added to the top organic layer seperate. Solution is shaken prior to analysis for Au by atomic absorption. Detection limit and range are 0.02 ppm and 4.00 ppm respectively.

iii) Analysis for W

Following the seiving and drying process a 0.5 gm. sample is put in a 16 x 150 mm test tube and 3 ml of mixed acid (1:2 H₃ PO₄ - HC1O₄) is added. Digestion is at 250° celsius fuming for 1 hour. The mixture is then cooled, 4 ml of 1:1 HCl is added, the tube is swirled to loosen caked solids and the mixture is heated at 100° celsuis for 30 minutes. It is cooled, 8 ml of 2500 ug/ml Li buffer solution is added and the tube capped and shook. Results are read on a Direct Coupled Plasma unit using matrix matched standards. Detection limit and range are 2.5 ppm to 1000 ppm. 6:2:2 RESULTS

All values are displayed on the accompanying plans.

i) Au: Fig. 4

Values range from below detection limit to 1.08 ppm. There is considerable response on the east half of the grid, (east side of the valley) particularily in the central portion of the grid.

> ii) As: Fig. 5 Values range from 0.5 (detection limit) to 620 ppm.

Response is much greater on the east side of the grid which covers the east side of the valley. On the western side of the valley (and grid) not one sample is in excess of 25 ppm.

Again the strongest response is in the central portion of the east side of the grid.

> iii) Cu: Fig. 6 Values range from 15 to 408 ppm.

A large part of the grid has a response between 100 and 200 ppm. A broad zone of slightly higher i.e. 200 - 300 ppm response lies in the eastern portion of the grid from 10 300N to 10 700N. The one result of over 400 ppm (408 ppm) is a point high on the western portion of line 10 500N.

> iv) Mo: Fig. 7 Values range from 1 to 16 ppm.

No strongly anomalous areas are present. Small areas of plus 10 ppm exist near the south end of the grid, as shown on the accompanying plan.

v) W: Fig. 8

Values range from below detection limit (2.5 ppm) to 14 ppm. The only area above 10 ppm is in the northwesterly portion of the grid.

6:2:3 DISCUSSION OF RESULTS

The geochemical results indicate that the eastern side of the valley is the only portion of the claim area where significant Au mineralization is, possibly, present. The mineralization responsible for the anomalous Au values may exist within the grid and on the bluff against which most of the lines terminate.

Arsenic bearing mineralization like Au, appears to be confined the the eastern side of the valley.

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The general background for Cu is high throughout almost the entire grid. The higher Cu values in the eastern half of the grid are partially coincident with anomalous Au and As areas and may represent minor Cu mineralization accompanying Au, As mineralization.

The molybdenum values suggest that no significant Mo mineralization is present anywhere within the grid. The slightly higher Mo values in the eastern portion of the grid are coincident with the Au, As, Cu response and probably reflect a slight increase in Mo accompanying other mineralization.

The distribution of W values demonstrate that there is no coincidence of W with other the elements analysed for. Values also suggest that no significant W mineralization is present within the grid area.

6:3 Geophysical Surveys

VLF-EM and magnetometer surveys were conducted along 5.32 kms of line.

The VLF survey was carried out using the Seattle transmitting station NLK (24.8 kHz) with readings being taken, at 20 m stations.

Magnetometer readings were taken at 10 m intervals and corrections for drift and diurnal changes were made by use of a base station recording magnetometer.

6:3:1 Equipment Used

The magnetometer survey was conducted using two Geometrics G-856A portable proton magnetometers (memory mags). One was used in the field mode (Ser. No. 27383) while the other was used in a base station mode (Ser. No. 27382). The internal clocks were synchronized before commencement of the survey and subsequent daily readings were dumped out to floppy disc in a Kaypro II portable computer. The data from the two magnetometers was merged and corrected for diurnal drift from an established base station value. The corrected results were plotted as field profiles and also stored on disc for eventual transfer to a Univac 1108 for final plotting.

The VLF-EM survey employed a Geonics EM-16 (Ser. No. 25) which used the Seattle transmitting station. VLF readings were also entered onto floppy disc in a Kaypro II computer and field profiles of In-Phase, Quadrature and Fraser Filter data were plotted. The stored data was transferred to a Univac 1108 for final processing and plotting.

6:3:2 Survey Results

The magnetometer survey results were plotted as plan maps of stacked profiles at a scale of 1:5000 (see plate in folder at back of report).

The VLF-EM survey results were plotted as stacked In-Phase, Quadrature and positive Fraser filter profiles on plan maps at a scale of 1:5000. The Fraser filter data was calculated as per the method put forth by D.C. Fraser (1969, Contouring of VLF-EM data: Geophysics, v. 34, P. 958-967). See plate in the folder at the back of report.

6:3:3 Discussion of Results

i) Magnetic Survey

No significant magnetic anomalies or trends were detected with the magnetometer survey.

ii) VLF-EM Survey

Four major conductors of limited strike length were detected by the VLF survey. These anomalies appear to be due to the extreme topographic changes which occur on the PDL claim. None of the above conductors seem to relate to geologic contacts or obvious fault zones. - 7 -

7. STATEMENT OF EXPENDITURES

Days Worked in Field (Placer Per	connel)	
R. Young 6, 7, 8, 10, 11		6.0 days
T. Koecher 6, 7, 8, 10, 11		6.0 days
B. Ott $4, 5(1/2 \text{ day}),$	18(1/2 day)	0.0 days
20(1/2 day) Sep		2.5 days
R. Boyce $4, 5(1/2 \text{ day})$ Sep		1.5 days
· · · ·		
\mathbf{R} . Cannon 10(1/2 day), 20	(1/2 day) Septemb TOTAL	er <u>1.0 day</u> 17.0 days
	IOTAL	17.0 days
Data Interpretation and Report W	Iriting	
R. Cannon 2 days		
R. Young 2 days		
		14 ····
Salaries and Benefits		
R. Young $8 \times 400.00 =$	\$3200.00	
T. Koecher $6 \times 150.00 =$	900.00	and the second second
R. Cannon $3 \times 350.00 =$	1050.00	
B. Ott $2.5 \times 250.00 =$	625.00	
R. Boyce 1.5 x 275.00	412.50	
	\$6187.50	\$ 6187.50
Camp Cost @ \$30.00/day/man	\$ 510.00	\$ 510.00
Grid Construction		
By contract to Leo Reichert	\$1744.00	\$1744.00
Faui-mant Obanaa		
Equipment Charges		*
2-G856 magnetometers		
@ \$400/wh x 1/2	\$ 200.00	
l Kaypro computer		
@ \$100/wh x 1/2	50.00	
1 Geonics EM 16		
@ \$200/wh x 1/2	100.00	
	350.00	\$ 350.00
Transportation		
1 3/4 ton Chev pickup for		
6 days @ \$50/day	\$ 300.00	
1 3/4 ton Chev Suburban for		
2.5 days @ \$50/day	125.00	
Fuel		
	$\frac{200.00}{625.00}$	\$ 625 00
	023.00	\$ 625.00
Analyses		
Analyses	62/00 00	
244 samples @ \$14.05/sample	\$3428.20	\$3428.20
Plotting, Drafting and Computer	Work	
3 days @ \$250/day	\$ 750.00	\$ 750.00
J days e y2JU/day	γ / συ • συ	\$ /JU.UU
Report Preparation		
1 day @ \$350.00	\$350.000	\$ 350.00
	AL COSTS= \$	<u>\$ 350.00</u> 13,944.70
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CONCLUSIONS 8.

Significant Au mineralization may exist within either the grid area in the east side of the valley (grid) and/or the bluffs just to the east of the grid.

Magnetometer and V.L.F. surveys are of little use in evaluating the mineral potential of the P.D.L. claim.

9. RECOMMENDATIONS

i) That geologic mapping and where indicated, rock sampling be carried out over the east side of the present grid and that the work be extended as required up onto the rock bluffs to the east of the present grid.

ii) That backhoe trenching be done to evaluate presently known anomalies and any other targets identified by further work.

iii) That targets identified by the mapping, trenching and other means be diamond drilled, if warrented.

Robert J. Young P

RJY/stm 11.18.85

APPENDIX I

STATEMENT OF QUALIFICATIONS

I, Robert J. Young of Placer Development Limited do hereby certify that:

- 1. I am a Geological Engineer.
- 2. I am a graduate of the University of British Columbia with a B.A.Sc in Geological Engineering 1962.
- 3. I am a member, in good standing at the Association of Professional Engineers of British Columbia.
- 4. From 1957 until the present, I have been engaged in exploration and mining geology (open pit and underground) in British Columbia and in Chile, S.A.
- 5. I personally supervised and participated in the field work and have compiled, reviewed and assessed the data resulting from the work.

RMJ.J

Robert J. Young P. Eng.

RJY/stm 11.19.85

STATEMENT OF QUALIFICATIONS

I, Richard W. Cannon, of the City of Vancouver, Province of British Columbia, hereby certify as follows:

- I am a graduate of the University of British Columbia where I 1. received a B.A.Sc. in Geological Engineering (Geophysics Option) in May 1966.
- 2. I am a member of the Association of Professional Engineers of British Columbia and have been so since 1968. Registration No. 6742.
- 3. I am a member of the Canadian Institute of Mining and Metallurgy, Society of Exploration Geophysicists, and B.C. Geophysical Society.
- I have practised my profession since 1966. 4.

R.W. Cannon, P. Eng

RWC/stm 11.19.85

APPENDIX III

Geochemical Assay Listing for Soil Samples.

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Fol	Lowing	elements	needed som	e values ac	justed:		-	
EL	EMENT	NSS L	OW HI	% BLNK	NVAL			
	AU	0 1	39 D 13 D		244			
·	AS	0	13 0 10 0	0 0	244			
	44 rec	ords skip	ped: tests.	duplicate	analyses			
na i statu i	2 - Carlon -				unaty ses			
SUM	MARY O	F GEOCHEM	DATA: PD	L		•		
ITE	M #		MISSING	MINIMUM	MAXIMUM	AVERAGE	STD. DEV.	
G R S A	MP	244	0 0	82E5 100N	82E5 10260N			• • 1917 -
PR	0 J	244	Ő	100N 5050	10260N 5050			
A A C	S U	244	0	.50	620.00	73.34	99.50	
C M W	0	244	0 0 0	15.00 1.00 2.50	408.00 16.00 14.00	149.86 4.56 5.08	09 62.06 2.48 2.87	
W		244	0	2.50	14.00	5.08	2.87	
					· · · · · · · · · · · · · · · · · · ·			
END	OF GC	HSCAN:	DATE: 25-	06-24 tim	ie: 11-29-37	244 R	ECORDS PRO	CESSI
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GRID	SAMPLE	P	ROJECT	MO	CU	AU	W	AS	
82E5 822E5 822E5 822E5 822E5 822E5 822E5	100N 100N 100N 100N 100N 100N	9980E 10020E 10060E 10100E 10140E	5050 5050 5050 5050 5050 5050	32323234	136 45 70 44 151		<5 <55 <55 <55	29 41 41 35 60 121	
82E5 82E5 82E5	100N 100N 101N STD AU	10200E	5050 5050 5050 5050	3 4 6	151 198 205 219 167	0 02	<5 <5 <5	180 248 81	
test 82E5 82E5 82E5 82E5 82E5	101N 101N 101N 101N	10000E 10040E 10080E 10120E	2020 5050	6587	154 205 180 177	0.02	<5 <5 <5	77 165 120 115	
82E5 82E5 82E5 82E5 82E5 82E5	101N 101N 101N 101N 101N	10160E 10200E 10240E 10280E 10280E 10320E	5050 5050 5050 5050 5050 5050 5050	7 7 7 8 9	169 199 186 160 184	<0.02	<5 <5 <5 <5	128 110 110 125 120	
test 82E5 82E5 82E5	STD AU 101N 101N	10360E	5050 5050 5050 5050	12	206	0.04	~5	148	
822E5 822E5 822E5 822E5 822E5 822E5 822E5 822E5 822E5 822E5	101N 101N 101N 101N 101N 101N 101N 101N	10440E 10480E 10520E 10560E 10600E 10640E 10680E 10680E *	5050 5050 5050 5050 5050 5050 5050	321122	005592787	<pre>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>></pre>	7 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5557 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <5757 <57577 <5757 <5777 <57577 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <5777 <57777 <57777 <57777 <57777 <57777 <57777 <577777 <577777 <577777777	31 11 16 11 17 9 35	
82E5 82E5 822E5 822E5 822E5 822E5 822E5 822E5 822E5 822E5	101N 102N 102N 102N 102N 102N 102N 102N	10720E 9540E 9960E 10000E 10040E 10080E 10120E 10160E	5050 5050 5050 5050 5050 5050 5050	~~~	105 106 100 109 120 140	<pre>< 0.02 C.02 < 0.02 < 0.02 < 0.02 C.02 C.02 C.02 C.02 C.02 C.02 C.02</pre>	<57 <55 <55 <7 11	13 6 28 25 37 47 60	
022E55 825 825 825 825 825 825 825 825 825 8	102N 102N 102N 102N 102N 102N 102N 102N	10200E 10200E 10240E 10280E 10320E 10360E 10360E 10400E 10440E	50550 5500550 5500550 5500550	5 5 4 10 5 5 3	140 156 137 129 1650 1855 28355 125	C.D5 NSS6 D.D3 C.04 C.04 C.04 C.04 C.04 C.04 C.04 C.04	8855555555555555555555555555555555555	57 57 524 88 86 59	
B2E5 B2E5 Lest	102N 102N 102N STD AU	10480E 10520E 10560E	5050 5050 5050	322	54 109 35	<0.02 <0.02 <0.02	<5 <5 <5	31 14	
2E5 2E5 2E5 2E5	STD AU 102N 102N 102N 102N	10600E 10640E 10680E 10720E	50500 50500 50500 50500 50500 50500 500500	4222	238 27 31 80	<pre><</pre>			
22E5 22E5 22E5 22E5 22E5 22E5 22E5 22E5	10260N 10260N 10260N 10260N 103N 103N	10600E 10640E 10680E 10720E 10200E 10240E 10280E 10280E 9560E 9560E *	5050 5050 5050 5050 5050 5050 5050 505	9 7 5 5 6 6	219 357 216 110 95 95	<pre><0.02 0.08 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02</pre>	<5 <55 <55 <75 <55 <55 <55	50 13 10 18 159 74 45 28 45 28 10	

PLACER GEOCHEM ASSAY SYSTEM: DATA FROM POL

ALTOVALU

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GRID	SAN	IPLE		ROJECT	MO	CU	AU	W	AS	
822E5 8822E5 8825 882		103N 103N 103N 103N 103N 103N	9600E 9640E 9680E 9720E 9960E 10000E	5050 5050 5050 5050 5050	6 65 M 5 N	160	<pre></pre>	5555 555 555	38 12 15 71 25	
82E5 82E5 82E5 82E5 test	STD	103N 103N AU	10040E 10080E 10120E	5050 5050 5050	NNW	68 69 134	<0.02 <0.02 <0.02	<5 <5 <5	25 28 47 151	
82E5 82E5 82E5 82E5		103N 103N 103N 103N 103N	10160E 10200E 10360E 10400E	5050 5050 5050 5050 5050	11 6 2	63 184 230 98	<0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0	<5 <5 <5	170 85 84 49	
82255 8255 82555 855555 855555 855555 855555 855555 855555 855555 8555555		103N 103N 103N 103N	10440E 10480E 10520E 10560E 10600E	5050 5050 5050 5050 5050	1	118	0.02	<5 <5 <5	40 79 18 10 7	
82E5 82E5 82E5 82E5		103N 103N 103N 103N	10600E* 10640E 10680E	5050 5050 5050 5050 5050	1	31 32 15 52	<0.02 <0.02 <0.02 <0.02	<5 <5 <5	12	
822E5 822E5 822E5 822E5 822E5 822E5 822E5 822E5 822E5		104N 104N 104N 104N	9560E 9600E 9640E 9680E	5050 5050 5050 5050 5050	8 7 3 10	165 4	<pre> 0 • 02 0</pre>	<55 <55 <55 <55	<27	
+ +	· · · · · ·	104N 104N AU 104N	9720E 9760E	5050 5050 5050 5050 5050	65 	96	C 02 C 02 C 75 C 02 C 75 C 02 C 75 C 02 C 02 C 02 C 02 C 02 C 02 C 02 C 02	<5 <5 <5	<2 10 8 73	
82255 8255 8555 8		104N 104N	10040E 10080E 10120E 10160E 10200E 10220E 102280E 102280E 102295E	5050 5050 5050 5050 5050 5050 5050	98 64 14 129	260 < 236	0.03 0.05 0.05 0.15 0.14	<5 <57 68 60 10 6	94 168 147 129 140 127	
822E5 822E5 822E5 822E5 822E5 822E5 822E5 822E5 82E5 8		105N 1055N 1055N 1055N 1055N	9560E 9560E* 9600E 9640E 9680E 9720E 9760E	5050 5050 5050 5050 5050 5050 5050	12 11 6655 12	220 < 219 < 149 < 120 < 142 < 142 < 1428 < 1428 < 1428 <	0.02	55	N242050	
0 2 2 2 2 2 2 2 2 2 2 2 2 2		105N 105N 105N 105N 105N 105N 105N 105N	9800E 9840E 10120E 10160E 102200E 102280E 102280E 102280E 95600E 9640E 9680E 9680E	50500 500500 50055000 50055000 50055000 50055000 50055000000	4 097 768	123 < 167 2290 187 2097 1987 2094 1987 2488 499 10638 78		6555557565656555565 < < < < < < < < < < < < < < < < < < <	<2 11 135 127 254 162 112 4 202 112 4 202 4 202 8 202 8 202 8 202 8 202 8 202 202	
 22255 22555 22255 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 22555 25555 25555 25555 25555 25555 25555 25555 25555 25555 255555 255555 255555 255555 255555 255555 255555 255555 255555 255555 255555 255555 255555 2555555		05N 05N 06N 06N 06N	9560E 9560E 9600E	5000 500500 500500 550500	6 87 10 10 16 6 4 3	172 < 228 < 198 < 109 < 163 <	02 02 02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	<55 55 55 6	202 112 193 <2 <2 <2 <2	

PLACER GEOCHEM ASSAY SYSTEM. **T** A . _

PLA GR			PROJECT	MO	CU	AU		AS		
82EE 82EE 82EE 82EE 82EE		06N 9720E	5050	532			7 7	7		
825	5	06N 9800E	SOSO	- 5 0 0	158	<0.02	8 6	24		
82E	5	06N 9880E	5050	4	153	<0.02 <0.02 >0.02	<5	10		
×2E	5 1	DAN QQADE	5050		139	<0.02	< 5	1	· · · · · · · · · · · · · · · · · · ·	
82E 82E 82E 82E	5 1	06N 10160E 06N 10200E 06N 10200E	* 5050 * 5050 * 5050 * 5050	5	139 210 209 237 260 305 271	<0.02 0.09 0.08 0.10 0.10	<56 <57	260 2550 3300 4300 22500		
82E	5	06N 10200E 06N 10240E	* 5050	6	209		<57	250	•	
82E 82E 82E	5 1	06N 10280E	5050	4	260	0.19	7	430		
82E	5 1	06N 10320E	5050 5050	<u> </u>	271	0.09 0.08 0.10 0.10 0.10 0.10 0.10 0.10 0.10	8 <u> </u>	240		. <u> </u>
82E 82E 82E 82E 82E	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 7 7 1 1 1 1	06N 10400E 06N 10440E	5050	5	226 225 204 96 180	0.10	5	221 232 225 <2		
82E	3	06N 10480E 07N 9560E	5050 5050	54	204	<0.02	<5	223		
82E	5 1 t STD A	107N 9600E	5050	9 1	180	<0.02				
tes 82E 82E	5 1	07N 9640E 07N 9680E	5050	4	120	<0.02	5	2		
822EE 822EE 822EE 822EE 822EE 822EE 822EE	5 1	07N 97201	- <u>5050</u> -	35	95	<0.02 <0.02 <0.02	<5	11		
825	5 1	07N 9800E	5050	- 4	103	<0.02	6	<23 5		
82E	5 1	07N 98401 07N 98801	5 5 1 5 1	6	145 158	<0.02	<5 <5	4		
82E	5 1 5 1	07N 99201 07N 99601	5050 5050 5050	22	158 119 141	<pre>< < <</pre>	<5	16		
tes 82F	t STD A 5 1	U 07N 100408	<u> </u>	2	107	<u>0.68</u> <0.02	<5	8		
82E	5 1	07N 100801 07N 102401	5050 5050 5050 5050 5050	23	130	<0.02 <0.02 0.12 0.19 0.13 0.11	105	460		
82E	5	07N 10280 07N 10320	5050		210	0.19	5.	406		
825	5 1	107N 103601	5050 5050 5050	2233332	219	0.11 0.10 0.25	67	410		
12222222222222222222222222222222222222	5	07N 104401	5050		1121214529744577 1121214529744577		< 5	19 460 400 400 400 320 328 3328 3325		
82E	5 1 5 1	07N 104801 07N 104801 07N 105201	5050 * 5050 5050	4	290	0.26	<5	328		
82E 82E	5 1 5 1	ID8N 9800	5050 5050	57	374	<0.09	<57	380		
82E	5 1 5 1	03N 98401 03N 98801	5050	5	143	<0.02	8	12		
	5	03N 98801 08N 99201 08N 99601	5050 5050 5050	4	173	<0.02 <0.02	57	12 10 13 8		
826	5	08N 10000 08N 10040 08N 10080 08N 10080 08N 10080 08N 10200 08N 10200 08N 10240 08N 10240 08N 10280	5050	5		<u><0.02</u>				
82E	5	08N 10080	5050	2222	11687 1677 17767 17767 17787		05555555555555555555555555555555555555	17		
82E 82E	5 1	108N 10120	5050	24	156	<0.02	<5	13		
82E	5 1 5 1	108N 10200 108N 10240	5050. 5050.	5	177 224 187	0.15	<5	230		
88888888888888888888888888888888888888	5 1	<u>088 10280</u> 088 10320	*	<u> </u>	187	<pre>< 0.02 < 0.02 <</pre>		11 12 17 130 1400 14308 174 40 158		· · · · · · · · · · · · · · · · · · ·
825	5	08N 10360	<u> </u>	4	153	<0.02	5 7 7	41 40		
82E	5	C8N 10440	Į	4000	186 153 150 114 157	<0.02	7	15		
82E 82E	2 5 1	08N 10000 08N 10040 08N 10080 08N 10080 08N 10080 08N 100240 08N 10080 08N 100240 08N 102200 08N 102240 08N 102240 08N 102240 08N 102400 08N 102400 08N 102400 08N 102400 08N 103400 08N 104400 08N 104480 08N 104480 08N 10480 08N 10480	* <u>5050</u>	3.	127		C	120		

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GRID S	AMPLE	PROJ	ECT MO	CU	AU	W	AS	
82E5 82EE5 82EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822EE5 822E5	109N 9 109N 9 109N 9	580E 50 620E 50 680E 50 720E 51	050 870 050 60 050 50 050 33 050 33 050 55 050 55 050 55 0550 55	142 102 124 97	0.31 0.24 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02 <0.02	< < < 556565 56577 7	141 1649 115 1037	
822E5 822E5 822E5 822E5 822E5 822E5	109N 9 109N 9 109N 9 109N 10	800E* 50 840E 50 880E 50 920E 50 960E 50 000E 51	050 5 050 3 050 2 050 4 050 4	117 172 146 117	<0.02 <0.02 <0.02 <0.02 <0.02	8 6 7 9 7	10 8 16 4	
82E5 82E5 82E5 82E5 82E5 82E5 82E5 82E5	109N 10 109N 10 109N 10 109N 10 W 109N 10 109N 10	120E 5 280E 5 320E 5 360E 5	050 4 050 4 050 4 050 6 050 6 050 5 050 5 050 5	177 169 157 161	<0.02 <0.02 <0.02 0.03 0.10 0.04	68 < 5 38 7 8	<pre> </pre>	
82E5 82E5 82E5 82E5 82E5 82E5 82E5 82E5	110N 10 110N 10 110N 10 110N 10	120E 50 120E 50	050 6 050 7 050 6 050 6 050 3 050 3 050 3 050 3 050 3 050 3 050 3	1522 1551 1553 1667	0.10 <0.02 0.11 0.02 <0.02 <0.02 0.02 <0.02 0.04 NSS	10893 1323 123 123	19 23 21 10 11 8	
822 822 822 822 822 822 822 822	110N 10 110N 10 110N 10 110N 10 110N 10 110N 10 110N 10	360E 50 600E 50 44400E 50 44800E 50 5560E 50	050 4 050 4 050 4 050 4 050 5 050 5 050 6 050 6 050 6 050 2	1482 1428 1483 1485 108	NSS 0.05 0.057 0.075 0.02 0.02 0.02 0.02	0 6 8 9 6 8 7 9	111 114 130 139 337 9	
8265	111N 9 111N 10 111N 10 111N 10 111N 10 111N 10	400E 20	C550 4 C550 5 C550 5 C500 5 C500 5 C500 5 C500 5 C500 5 C500 5 C5	183 177 168 170 160 150	<pre>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>></pre>	9 8 11 12 11 9 11 9	23 24 11 86 55 55 315	
82E5 82E5 82E5 82E5 82E5 82E5 82E5 82E5	N 3.4	440E 51 480E 51 520E 51 800E 51 840E 51 880E 51 880E 51 920E 51		158 217	0.14	7771 1443 10	02357777560 12177560 116665 22475	
82E5 82E5 82E5 82E5 82E5 82E5 test STE	112N 9 112N 9 112N 9 112N 9 112N 9 112N 10 112N 10 112N 10 112N 10 112N 10	800E 55 840E 55 880E 55 920E 55 950E 55 000E 55 400E 55 440E 55	2000 2000 2000 2000 2000 2000 2000 200		<pre></pre>	11 5 7 8 33	211 246 276 135	

PLACER GEOCHEM ASSAY SYSTEM: DATA FROM POL

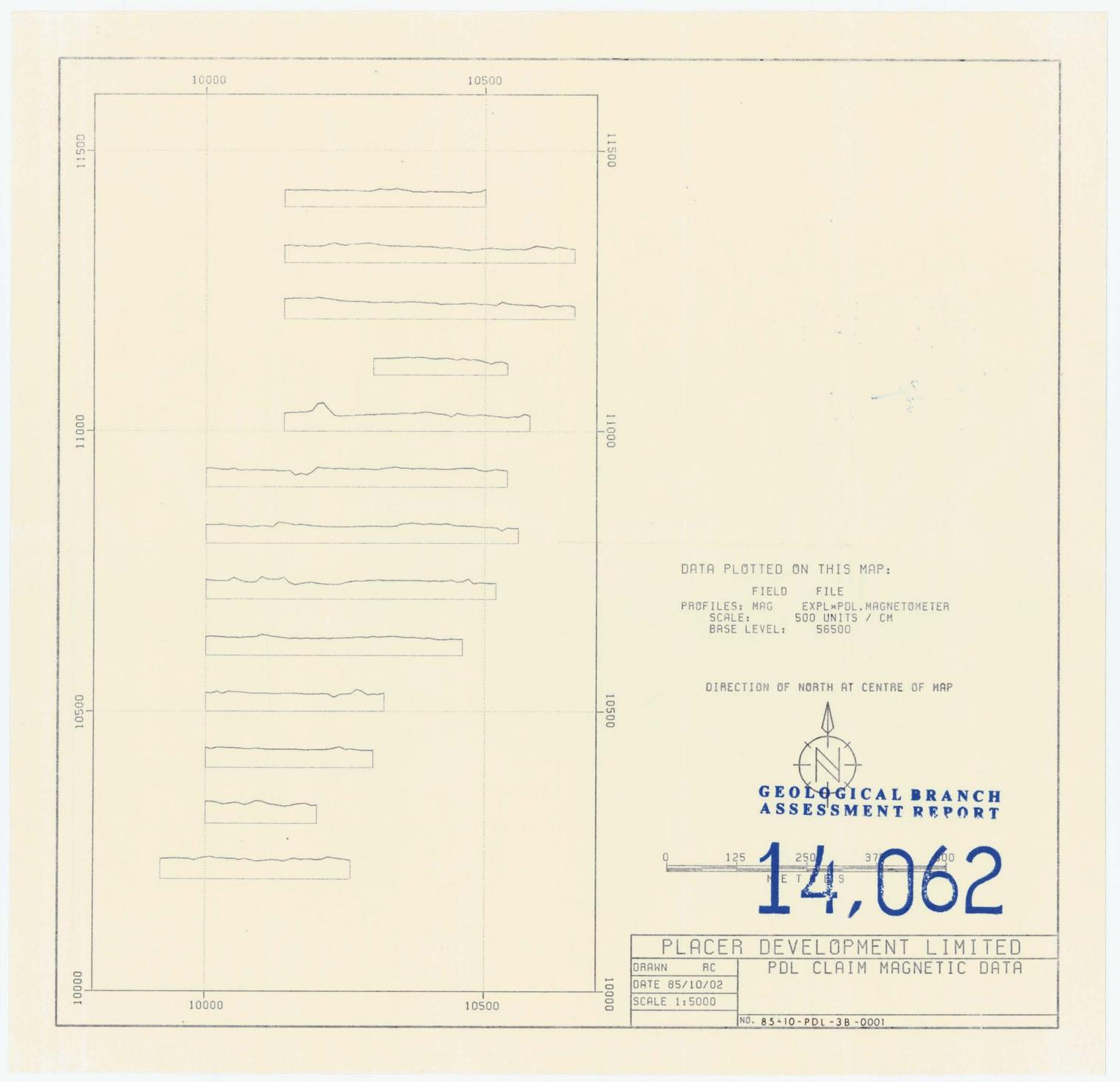
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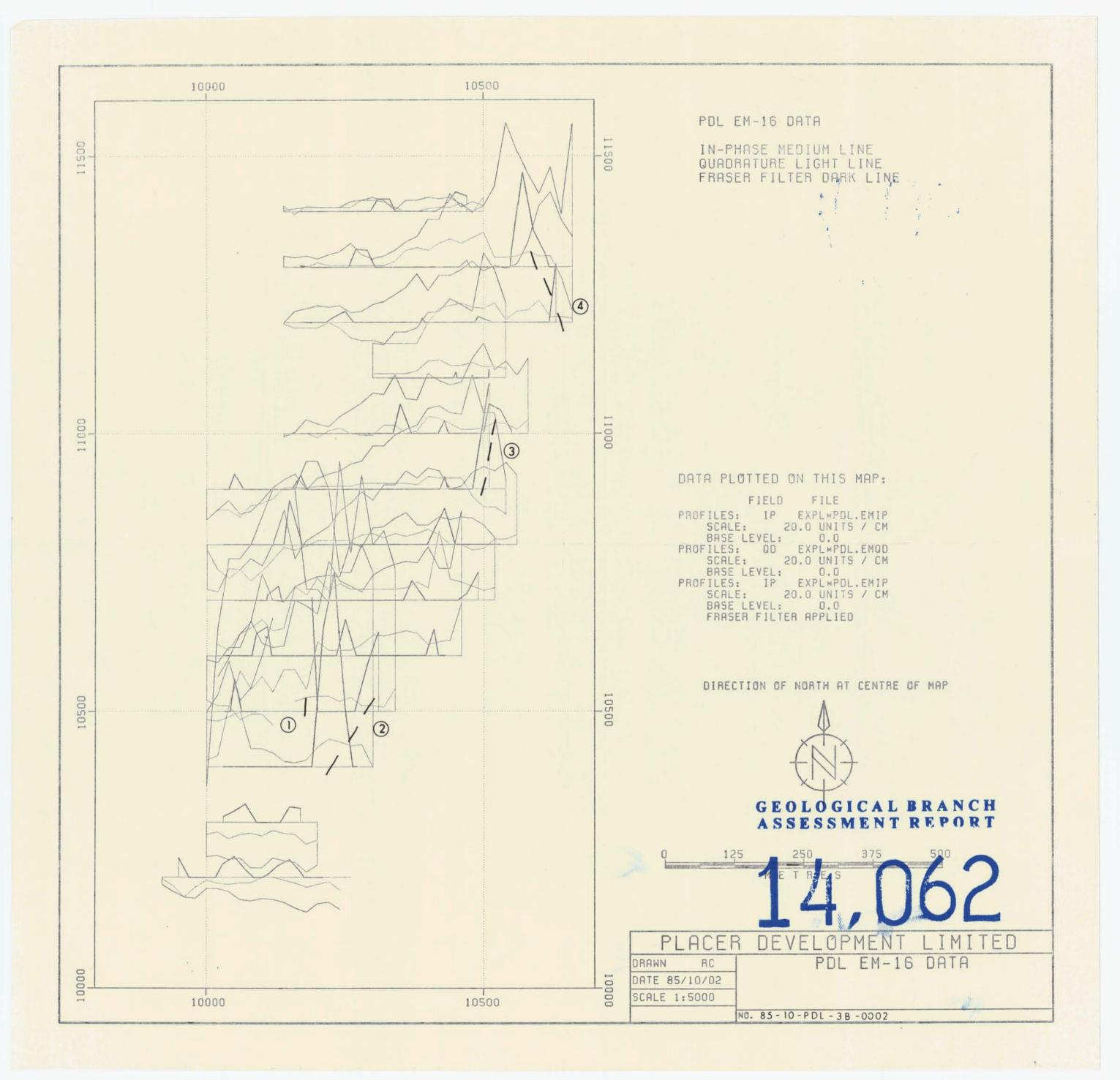
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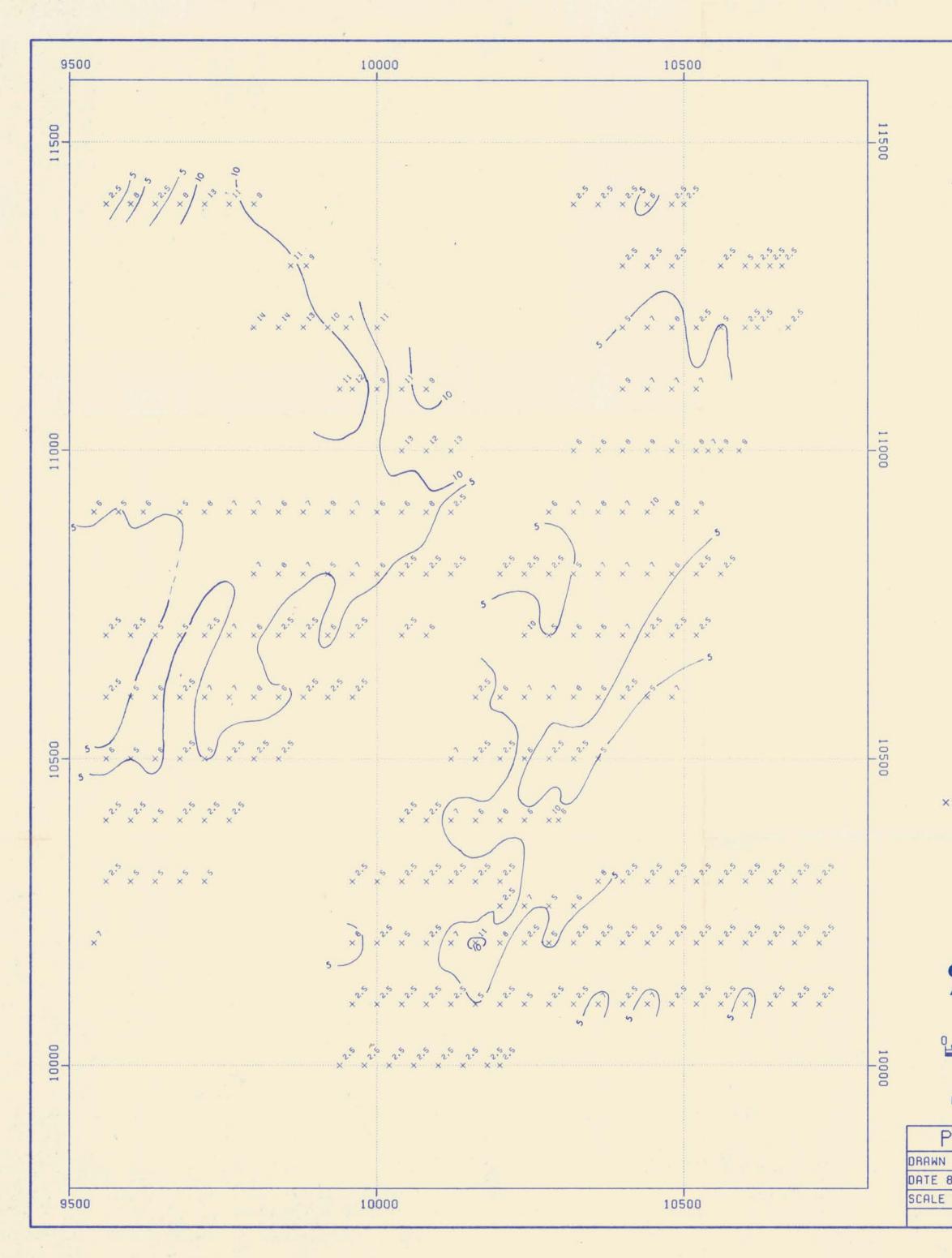
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255 112N 10520E 5050 3 120 0.071 55 558 862255 112N 10520E 5050 3 125 0.03 553 862255 112N 10520E 5050 3 126 0.03 553 862255 112N 10600E 5050 3 124 0.010 553 862255 112N 10600E 5050 2 1220 0.024 553 862255 113N 106400E 50500 2 1220 0.044 521 144 862255 113N 104400E 50500 2 141 0.02 570 2202 141 0.02 570 2202 141 0.02 570 2202 141 0.02 570 2202 141 0.02 570 2202 141 0.02 570 2202 141 0.02 570 2202 141 0.02 570 2202 141 0.02 570 2202 141 0.02 570 2202 127 0.02 570 200 200 200 200	B2EES 113N 10460E 5650 2 202 0.44 4 45 145 B2EES 113N 10440E 5650 2 141 45 145 B2EES 113N 10440E 5650 2 141 45 145 B2EES 113N 10480E 5650 2 141 45 145 B2EES 113N 10480E 5650 2 141 45 143 B2EES 113N 10480E 5650 2 141 45 443 B2EES 113N 10640E 5650 3 115 0079 45 77 B2EES 113N 10640E 50500 3 115 0079 45 107 B2EES 114N 9660E 50500 3 100 128 13 10 B2EES 114N 9680E 50500 2 127 0.02 13 10 B2EES 114N 9680E 50500 2 127 0.02 13	B 22E5 113N 98856 5050 2 202 0.04 4 4 45 145 B 22E5 113N 10440E 5050 2 142 0.04 5 145 B 22E5 113N 10440E 5050 2 141 4 6.02 5 24 B 22E5 113N 10480E 5050 2 141 6 52 143 B 22E5 113N 10640E 5050 2 141 6 50 50 50 50 B 22E5 113N 10640E 5050 3 1150 00002 5 57 B 22E5 113N 10640E 5050 3 1150 0002 5 126 B 22E5 114N 9640E 5050 3 127 0.02 30 128 B 22E5 114N 9640E 5050 2 127 0.02 30 128 B 22E5 114N 9640E 5050 2 127 0.02 13 10 B 22E5 114N 10360E 5050 2 262 0.02 <td< th=""><th>GRID</th><th>SAMPLE</th><th>PROJECT</th><th>MO CU</th><th>AU</th><th>W</th><th>AS</th><th></th></td<>	GRID	SAMPLE	PROJECT	MO CU	AU	W	AS	
82E5 113N 10640E 5050 3 1138 0.02 <5 92 82E5 114N 9660E 5050 2 129 <0.02 <5 107 82E5 114N 9660E 5050 2 129 <0.02 <5 107 82E5 114N 9660E 5050 2 129 <0.02 <5 107 82E5 114N 9660E 5050 2 129 <0.02 <5 107 82E5 114N 9680E 5050 2 127 <0.02 8 113 82E5 114N 9720E 5050 2 127 <0.02 9 17 82E5 114N 9720E 5050 2 68 <0.02 9 17 82E5 114N 10320E 5050 2 68 <0.02 5 31 82E5 114N 10440E 5050 2 78 0.006 5 56 82E5 114N 10440E 5050 2 120 103 5 56 82E5 114N 10460E* 5050	82E5 113N 10640E 5050 3 113C 0.02 <5 92 82E5 114N 9660E 5050 2 130 40.02 <5 107 82E5 114N 9660E 5050 2 129 40.02 <5 167 82E5 114N 9640E 5050 2 129 40.02 <5 167 82E5 114N 9640E 5050 2 129 40.02 30 128 82E5 114N 9640E 5050 2 127 40.02 8 130 82E5 114N 970E 5050 2 200 128 113 82E5 114N 9760E 5050 2 260 00.2 9 17 82E5 114N 10320E 5050 2 68 00.02 9 17 82E5 114N 10440E 5050 2 78 0.02 6142 142 82E5 114N 10440E 5050 2 124 0.008 55 56 82E5 114N 10440E 5050 2 124 0.008 55 56 82E5 114N 10500E	82255 113N 10640E 5050 3 113N 002 5 92 82255 114N 9640E 5050 2 138 0.02 5 26 82255 114N 9640E 5050 2 129 0.02 8 15 82255 114N 9640E 5050 2 129 0.02 8 15 82255 114N 9640E 5050 2 127 0.02 8 17 82255 114N 9640E 5050 2 127 0.02 30 128 82255 114N 9700E 50500 2 167 0.02 13 10 82255 114N 9700E 50500 2 268 0.02 9 10 82255 114N 10320E 50500 2 92 0.02 5 20 82255 114N 10440E 50500 2 92 0.02 142 142 82255 114N 10480E 50500 2 124 0.03 556 3 82255 114N 10480E 50500 3 90 0.04 5 556 82255 114N 10500E 50500 </th <th>82E5 82E5 82E5</th> <th>112N 1 112N 1 112N 1 112N 1 113N 113N 1 113N 1 113N 1 113N 1 113N 1</th> <th>0620E 5050 0670E 5050 9860E 5050 9885E 5050 0400E 5050 0440E 5050 0440E 5050</th> <th>3 126 3 154 4 141 4 180 2 202 3 123 4 142</th> <th>0.02 0.04 0.04 0.10</th> <th>11</th> <th>252 308 53 58 17 145 145 143</th> <th></th>	82E5 82E5 82E5	112N 1 112N 1 112N 1 112N 1 113N 113N 1 113N 1 113N 1 113N 1 113N 1	0620E 5050 0670E 5050 9860E 5050 9885E 5050 0400E 5050 0440E 5050 0440E 5050	3 126 3 154 4 141 4 180 2 202 3 123 4 142	0.02 0.04 0.04 0.10	11	252 308 53 58 17 145 145 143	
test STD W 9680E 5050 2 127 0.02 13 10 82E5 114N 9720E 5050 4 260 0.02 13 10 92E5 114N 9760E 5050 4 260 0.02 11 10 92E5 114N 9760E 5050 4 260 0.02 11 10 92E5 114N 10320E 5050 4 260 0.02 9 17 82E5 114N 10320E 5050 2 92 0.02 4 4 82E5 114N 10340E 5050 2 92 0.02 4 4 82E5 114N 10440E 5050 2 124 0.08 4 4 82E5 114N 10480E 5050 2 124 0.08 4 4 82E5 114N 10480E 5050 3 90 0.04 4 5 56 82E5 114N 10480E 5050 <td>test STD W 9680E \$050 2 127 0.02 13 10 \$2255 114N 9720E \$050 4 260 0.02 13 10 \$2255 114N 9760E \$050 4 260 0.02 11 10 \$2255 114N 9760E \$050 4 260 0.02 19 17 \$2255 114N 10320E \$050 2 920 0.02 9 17 \$2255 114N 10400E \$050 2 92 0.02 47 10 \$2255 114N 10400E \$050 2 78 0.02 47 142 \$2255 114N 104480E \$050 2 124 0.08 \$5 56 \$2255 114N 10480E \$050 3 90 0.05 \$5 60 \$2255 114N 10480E \$050 3 90 0.05 \$5 60 \$2455 114N 10480E \$050</td> <td>test STD W 9680E 5050 2 127 0.02 8 13 10 s2E5 114N 9720E 5050 4 2600 0.02 13 10 s2E5 114N 9760E 5050 4 2600 0.02 11 10 s2E5 114N 9760E 5050 4 2600 0.02 19 10 s2E5 114N 10320E 5050 2 922 0.02 9 17 s2E5 114N 10320E 5050 2 922 0.06 <5</td> 20 s2E5 114N 10400E 5050 2 76 0.02 4 47 s2E5 114N 10480E 5050 2 124 0.08 <5	test STD W 9680E \$050 2 127 0.02 13 10 \$2255 114N 9720E \$050 4 260 0.02 13 10 \$2255 114N 9760E \$050 4 260 0.02 11 10 \$2255 114N 9760E \$050 4 260 0.02 19 17 \$2255 114N 10320E \$050 2 920 0.02 9 17 \$2255 114N 10400E \$050 2 92 0.02 47 10 \$2255 114N 10400E \$050 2 78 0.02 47 142 \$2255 114N 104480E \$050 2 124 0.08 \$5 56 \$2255 114N 10480E \$050 3 90 0.05 \$5 60 \$2255 114N 10480E \$050 3 90 0.05 \$5 60 \$2455 114N 10480E \$050	test STD W 9680E 5050 2 127 0.02 8 13 10 s2E5 114N 9720E 5050 4 2600 0.02 13 10 s2E5 114N 9760E 5050 4 2600 0.02 11 10 s2E5 114N 9760E 5050 4 2600 0.02 19 10 s2E5 114N 10320E 5050 2 922 0.02 9 17 s2E5 114N 10320E 5050 2 922 0.06 <5	82E5 82E5 82E5 82E5	113N 11 113N 11 113N 11 113N 11 113N 11 113N 11 114N 114N	U480E 5050 0620E 5050 0600E 5050 0640E 5050 0640E 5050 0660E 5050 9560E 5050 9560E 5050	3 135 2 80 4 115 3 115		<5 <5 <5 8	92 107 26 15	
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SYSTEM: DATA FROM PDL



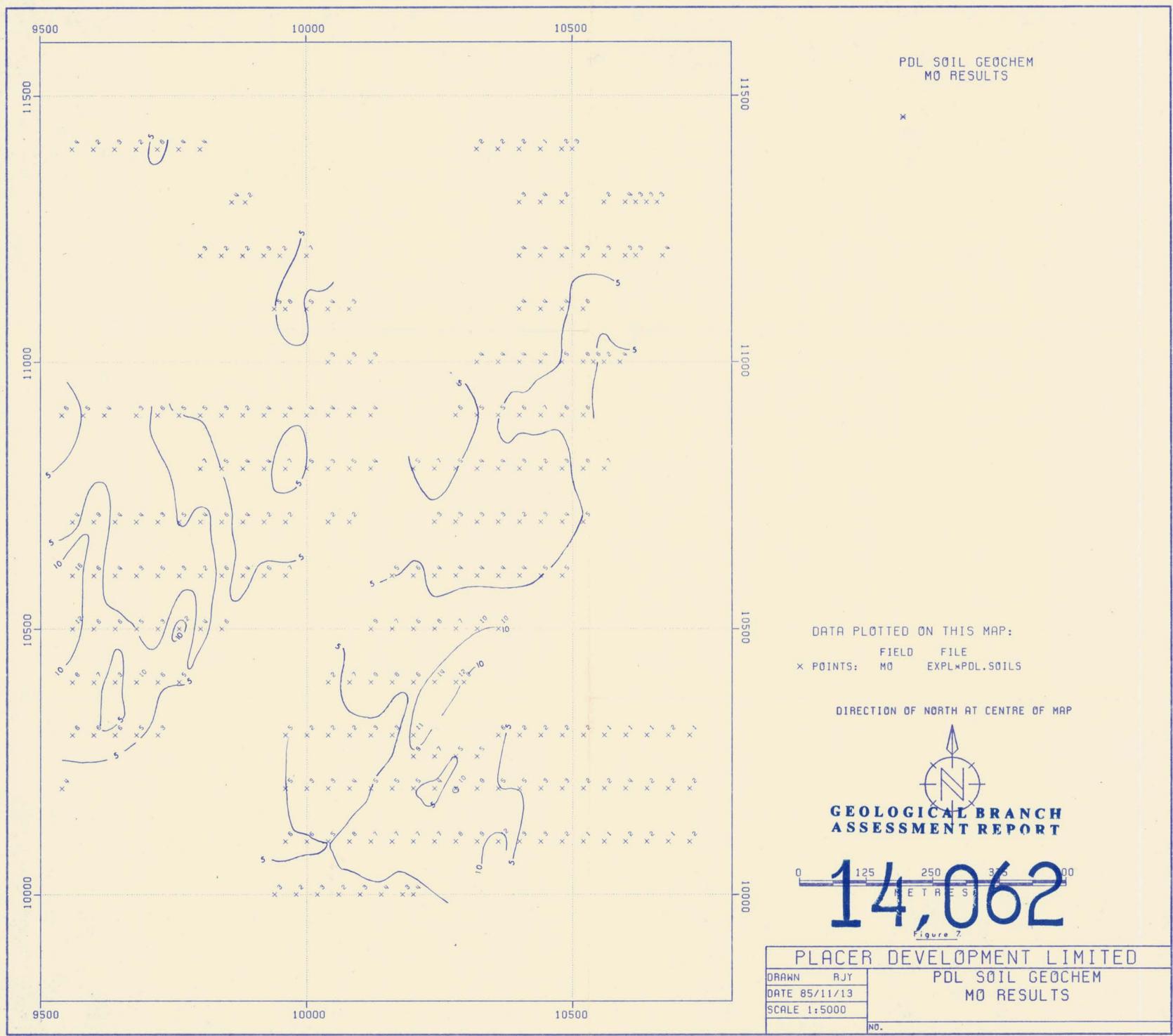


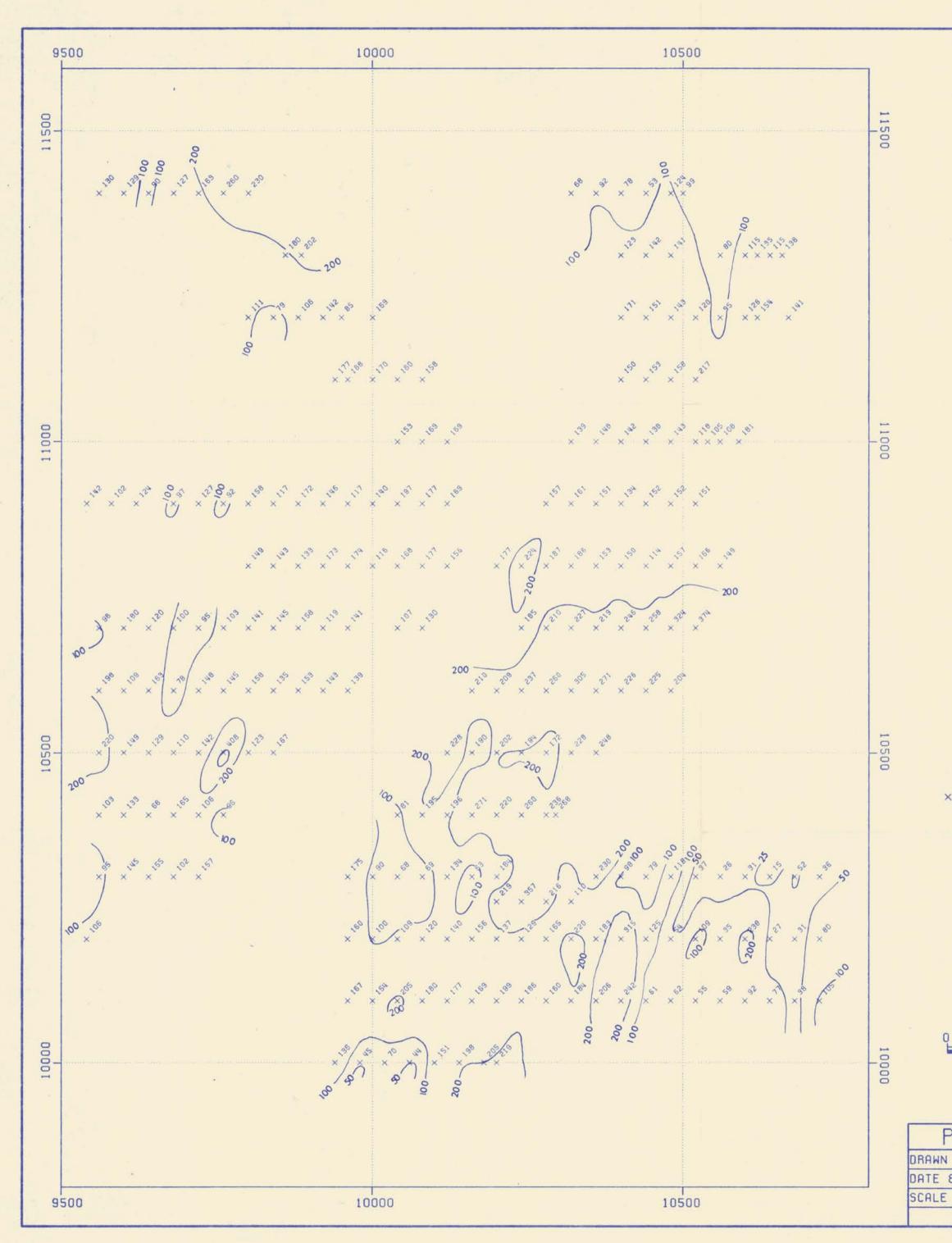


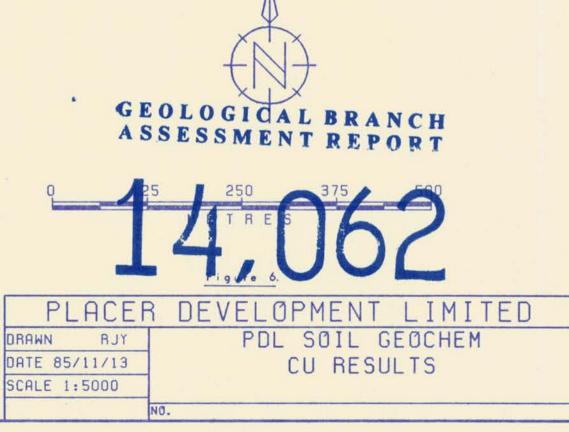


DATA PLOTTED ON THIS MAP: FIELD FILE EXPL*PDL.S0ILS × POINTS: W

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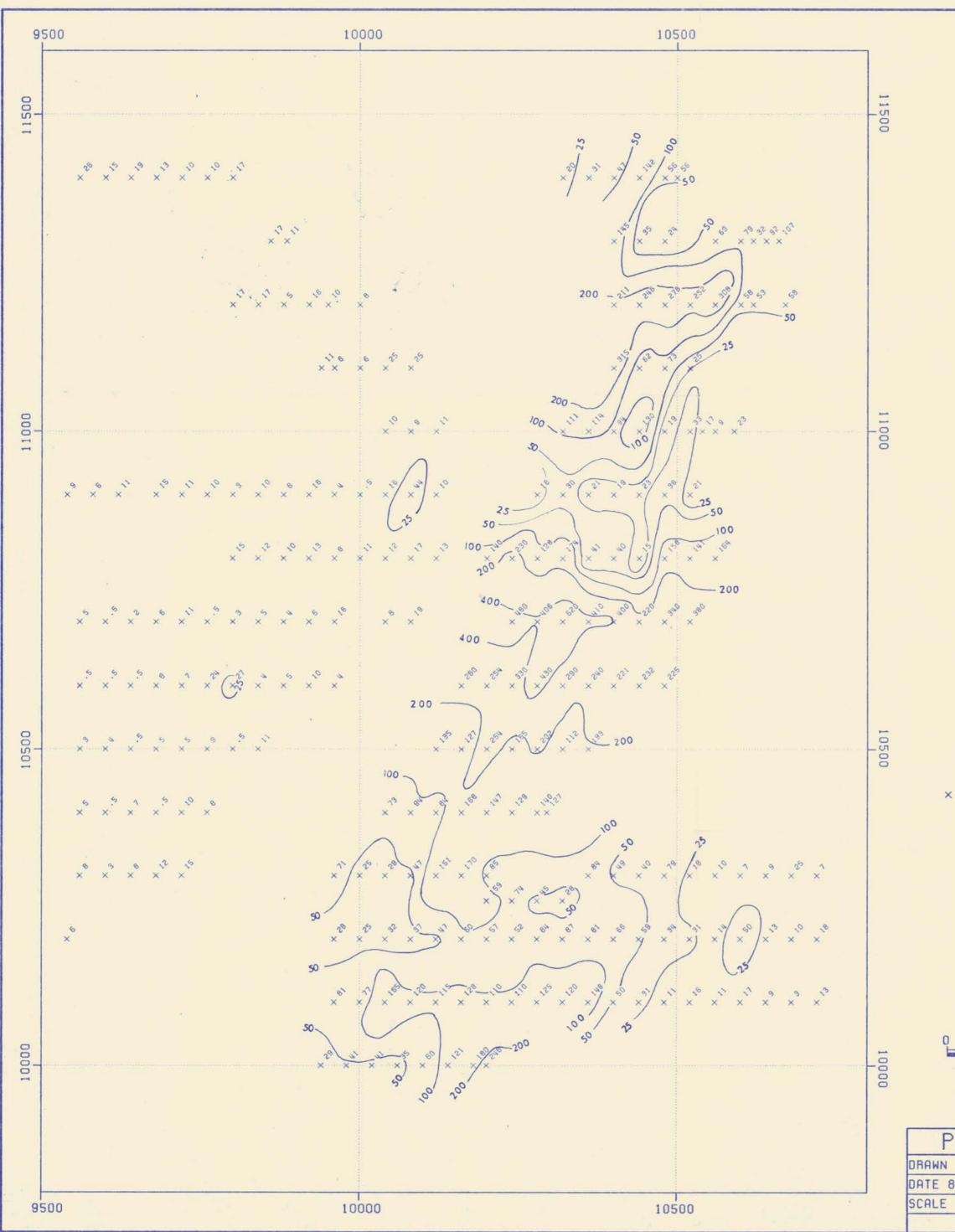


DIRECTION OF NORTH AT CENTRE OF MAP

DATA PLOTTED ON THIS MAP: FIELD FILE × POINTS: CU EXPL*PDL.SOILS

PDL SØIL GEØCHEM CU RESULTS

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GEO	LOGICAL BRANCH ESSMENT REPORT
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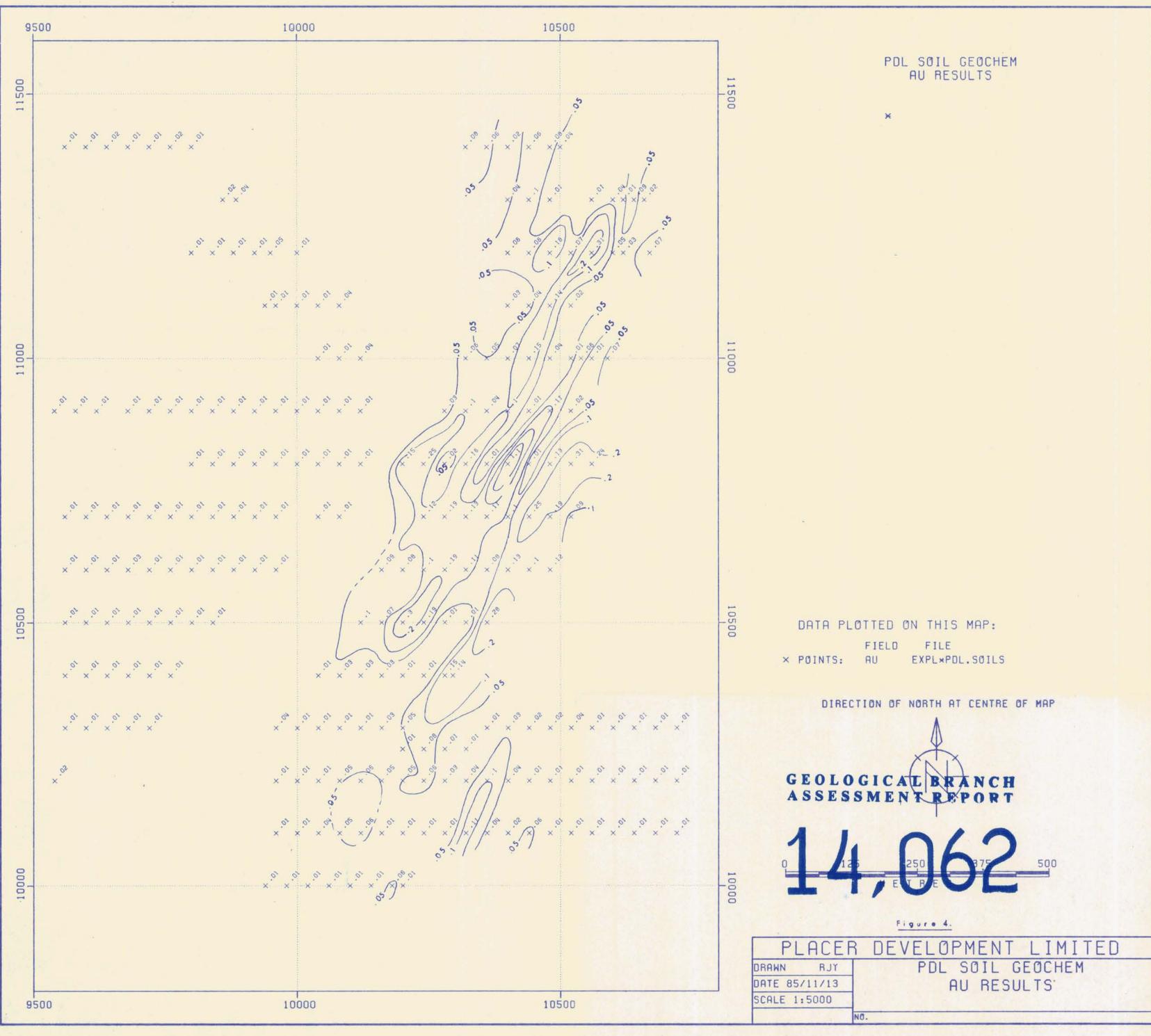
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FIELD FILE × POINTS: AS EXPL*PDL.SOILS

DATA PLOTTED ON THIS MAP: FIELD FILE

PDL SØIL GEØCHEM AS RESULTS



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