85-775-14164
10/86



# WAYSIDE, NEW DISCOVERY

Southwestern B.C. (92J/15W)

Geological, Geochemical and

Drilling Assessment Report of Work

Performed to July 28/1985

# GEOLOGICAL, GEOCHEMICAL AND

# REPORT ON DRILLING ON THE

# WAYSIDE CLAIMS

Lillooet Mining Division

N.T.S. Map - 92J/15W, Zone 10

Centered at Approximately - U.T.M. 5 635 500 N
512 000 E
765 m elevation

50° 53' - Latitude

122° 50' - Longitude

Owned By - Amazon Petroleum Corp. and
Carpenter Lake Res.

Operated By - Amazon Petroleum Corp.

Consultant - R.J. Morris
MORRIS GEOLOGICAL CO. LTD.

Author - R. J. Morris

Date - August 16, 1985

CONTENTS

# ENCLOSURES

## TABLES





## APPENDICES

SUMMARY -

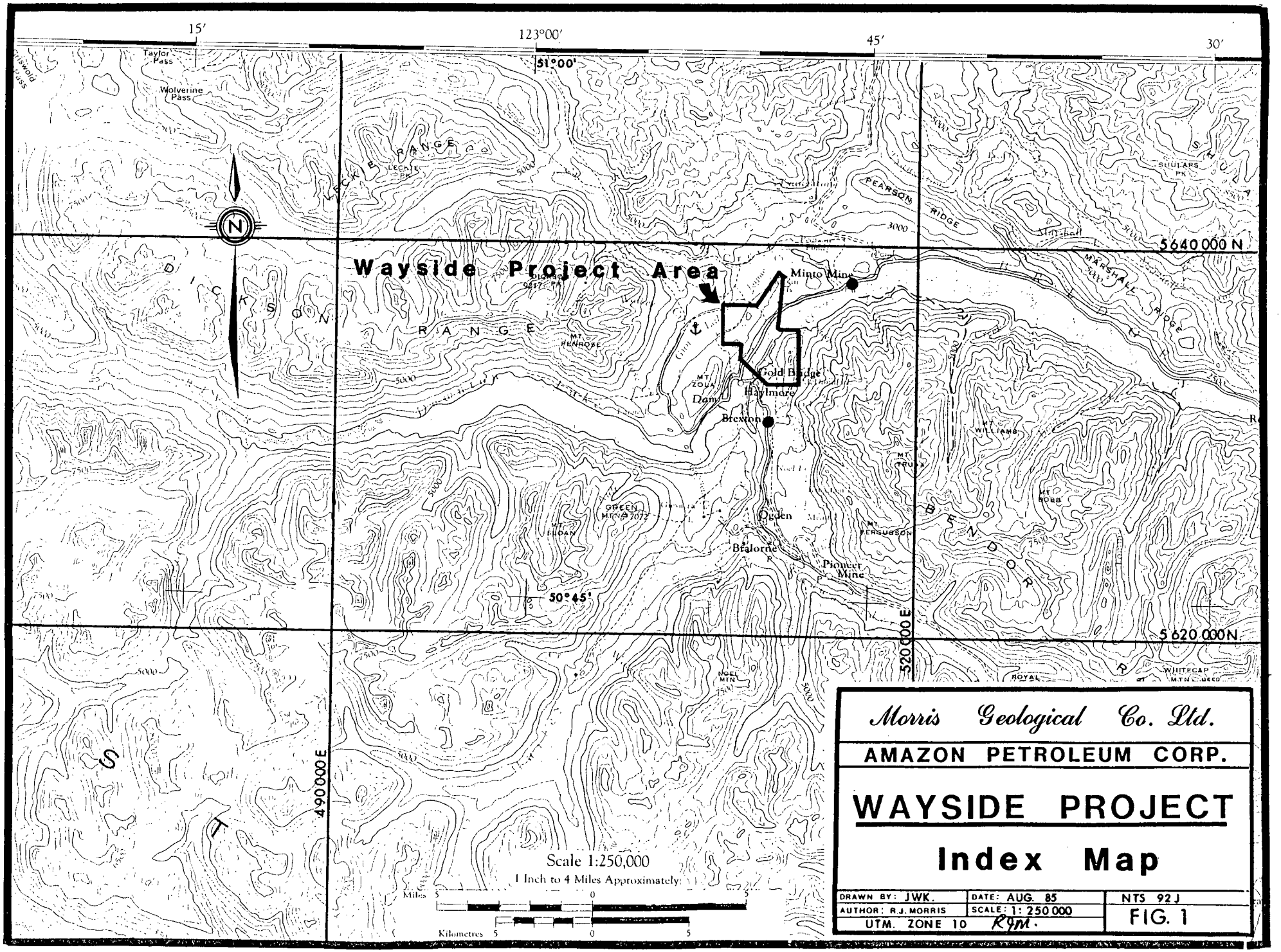
The discovery zone massive sulfide was located in the mid 70's during construction of the Lillooet - Gold Bridge highway. Since discovery 14 holes have been drilled to delineate 150,000 tonnes of copper-zinc mineralization with a minor precious metal content. The deposit is open to depth and along strike.

Work in 1985 was directed towards increasing the potential reserves of the main zone by testing its extension towards surface and to the north and south. A major EM conductor located in 1984 was also tested with diamond drilling as well as an I.P. anomaly delineated in 1981.

The Wayside property is within the Coast Plutonic Complex and comprises the Bridge River Group and the Bralorne Intrusives. The Bridge River Group is made up of volcanic and sedimentary rocks which strike north-south and dip steeply to the east. The Bralorne Intrusives are dominantly diorite which were probably emplaced as sills and may be the intrusive equivalent to the Bridge River Volcanics.

The property hosts at least two major strike - slip faults which strike east - west and appear to truncate the main ore horizon on the north and south. Combining geological mapping, geochemistry, I.P. and to an extent EM, the north and south extensions of the main ore zone appear to be displaced to the west, relatively.

It is recommended that diamond drilling be undertaken to test the present interpretation which leaves the down - dip extension and north and south ends of the deposit open.

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**AMAZON PETROLEUM CORP.**

# WAYSIDE PROJECT

## Index Map

| | | |
|---|---|---|
| DRAWN BY: JWK. | DATE: AUG. 85 | NTS 92 J |
| AUTHOR: R.J. MORRIS | SCALE: 1: 250 000 | FIG. 1 |
| UTM. ZONE 10 | RJM. | |

INTRODUCTION -

Location and Access:

The Wayside property is located 3.2 kilometers north of the town of Gold Bridge, adjacent to and covering the southwestern end of Carpenter Lake.

Access is via an all weather road westward from Lillooet approximately 112 kilometers. The highway goes through the claims and several good exploration and forestry roads allow access to various portions of the property.

Previous Work

- WAYSIDE MINE
  - produced 1914 - 37
  - 43,094 tons
  - 5,341 oz. gold
  - 842 oz. silver

  - active during 1946 - 53
  - no production figures

- 1934 - G.S.C. map 430A, "Gun Lake area"

- 1974 - Charles A.R. Lammle
  - preliminary report + map
  - 110 soil samples along highway analysed for gold.

  NOTE because of thick glacial debris soil sampling should be site specific.

  - ground magnetometer survey along highway.

  NOTE magnetometer results seem to map the diorite and Bridge River Group very well.

  - two sites noted for oxidized porphyritic rock, "New Discovery" and above D.D.H. 84.07.

  NOTE a boulder of massive pyrite in chert was located at

the second site (sample 59R).

- 1980, 1982 - J.P. Elwell - three reports coveryng diamond drilling + assays.
  - 8 holes in the "New Discovery"
  - total = 1995.8m (6548 ft.)

- 1981 - Geotronics - I.P. & S.P. survey
  - anomaly A correlates very well with the new discovery.

NOTE the new discovery is non-economical, massive pyrite;
a) surface sampling
b) holes 84 - 10, 11
c) holes 80 - S3, S2

- the north end of anomaly A is probably faulted (left lateral) to the 84-04 area.

NOTE anomaly A over 84-04 correlates with a conductor of Glen Whites.

- the south end of anomaly A is probably faulted (right lateral) to become anomaly B.

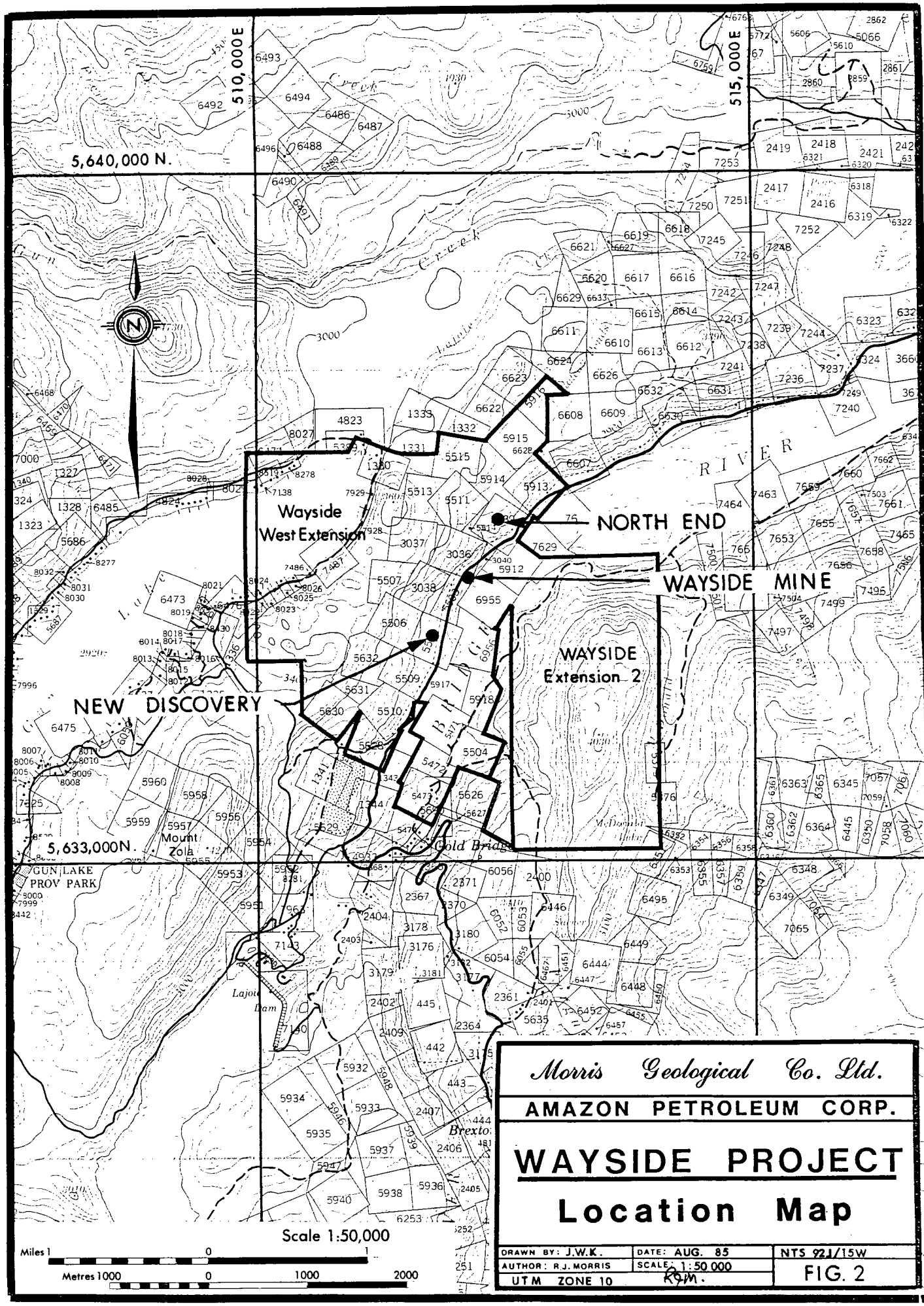
NOTE if anomaly A, over hole 84-04 and anomaly B are fault extensions of the main anomaly A, possibly they are merely massive pyrite also.

- 1983 - R.H. Seraphim - Geochemistry for gold over the Wayside diorite and onto Bridge River Group west of the diorite.

- 1984 - A. Halim Arik - Report on drilling, 1984
  - four holes on the New Discovery
  - total = 825.4m (2708 ft.)

- 1984 - Geotronics - EM and geochemistry.
  - North end and east of Wayside diorite.
  - good correlation of geochem and EM.

- 1984 - Glen White - Geophysical report for downhole and pulse EM.

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# WAYSIDE PROJECT

## Location Map

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG. 85 | NTS 92J/15W |
| AUTHOR: R.J. MORRIS | SCALE: 1:50 000 Rom. | FIG. 2 |
| UTM ZONE 10 | | |

SUMMARY OF 1985 EXPLORATION

- Geological mapping - North end, H. Arik east of base line
  R.J. Morris west of base line
  - South end, R.J. Morris
    - all roads
    - White's grid

- Chain and compass survey - 11 176m (36,666.7 ft = 6.9 mi.)
  - mostly roads

- Trenching - 453m (1,486.2 ft.)

- New road - 798m (2,618.1 ft.)

- Old trenching and adit - three old trenches were located.
  - one old adit was found

- Geochem - 324 soil and rock samples

- New sections, White's grid

- New detail on New Discovery

- Diamond drilling - 4 holes completed, number 5 in progress; 587.7m

- The present report describes work and interpretations by the author after field work from May 21 to August 29, 1985

## SUMMARY OF TRENCHES

TABLE 8

| TRENCH NO. | LENGTH | WIDTH | DEPTH | ACCESS | TO TEST FOR | SAMPLES | RECLAIMED |
|---|---|---|---|---|---|---|---|
| 41 | 24.5 | 1.0 | 2.5 | Edge of existing road | Au | 3 soils | ✓ |
| A34 | 20 | 0.5 | 0.5 | along skidder trail | Au | 1 soil | ✓ |
| A34E | 22 | 0.5 | 0.5 | " " " " | Au | 1 " " | ✓ |
| 34 | 21 | 0.5 | 0.5 | " " " " | Au | N/S | ✓ |
| 11 | 41 | 1.0 | 1.0 | new trail, length = 220m | Au | 5 soils | |
| 6N500W | 14 | 1.0 | 4.5 | along skidder trail | MS | 2 " " | ✓ |
| 103 | 55 | 1.0 | - | along road | MS | 15 rock chips | ✓ |
| 6N300W | 4 | 1.0 | - | new trail, length = 92m | MS | 1 soil | ✓ |
| 99 | 84 | 1.0 | 2.0 | re-opened old trench | Au | 4 soil, 3 rock | ✓ |
| 147 | 20 | 1.0 | 4.0 | along new trail to trench 11 | Au | 4 soils | ✓ |
| 81 | 20 | 1.0 | 1.5 | along old road | Au | 3 soils; 3 rock | |
| 118 | 15 | 2.0 | 1.5 | ditch of highway | MS | 3 soils; 12 rock | |
| 165 | 33 | 1.0 | 3.0 | new trail, length = 345m | MS | 2 soils | ✓ |
| 158 | 14 | 1.0 | 1.0 | new trail, length = 41m | MS | 3 soils | ✓ |
| 118A | 22 | 1.0 | 0.5 | along old road | MS | 17 rock | |
| 117 | 6 | 1.0 | 1.5 | along old road | MS | 5 rock, 3 soil | ✓ |
| 61 | 10 | 1.0 | 5.0 | re-opened old trench | MS | 1 soil | |
| 59 | 7.5 | 1.0 | 2.5 | " " " " | MS | 2 " " | |
| 900S | - | - | - | new trail, length = 100m | Au | N/S | ✓ |
| 600S320E | 15 | 1.5 | 3.0 | along old trail | Au | 1 soil, 1 rock | ✓ |
| PLA | 5 | 3.0 | 3.0 | re-opened old adit along old trail | Au | 3 rock | ✓ |

Total trenches = 453m
New road = 798m (for trenching)
New road = 777.5m (for drilling)
} 1575.5m

GEOLOGY -

Overview :

The Gold Bridge - Bralorne area is part of the Coast Geanticline tectonic element of the Canadian Cordillera. The area was subjected to a varied eugeosynclinal depositional regime including extensive and repeated volcanism in island arc environments and rapid changes in the distribution, thickness and character of the sediments, reflecting repeated deformation and uplift from late Devonian until the late Cenozoic.

The upper Paleozoic eugeosynclinal rocks were deposited in two relatively mobile volcanic arcs. The Coast Mountain arc is characterized by mixed volcanics: andesite, basalt, and rhyolite with abundant pyroclastics; clastics, partly terrigenous and partly volcanogenic.

The early Mesozoic witnessed extrusion of abundant andesitic and basaltic volcanics, in part from centres along island arcs, and, in part as submarine flows in adjacent troughs and basins. The basins also received thick accumulations of volcanogenic and terrigenous sediments from the arcs. Tectonic relief is recognized on the basis of gross changes in facies of volcanics and sediments.

The Tyaughton Trough successor basin was established following the mid-Jurassic tectonism. The trough received considerable granite debris from the east in late Jurassic and Early Cretaceous time. In early Late Cretaceous time much of the Cordilleran region was land - mainly mountains, though deposition continued in Tyaughton Trough.

The Coast Plutonic Complex is dominated by the Pacific Orogen. The structures are mainly steeply dipping reflecting the nearly vertical upward movement of blocks and plutonic material.

Detailed Geology :

Two formations are exposed on the Wayside Property, the older Bridge River Group which comprises sediments (argillite, sandstone and chert) and greenstones (andesite to gabbro), and the Bralorne Intrusives which are dominantly diorite.

The Bridge River Group is comprised of sediments and volcanics which strike north-south and are nearly vertical. Several tops determinations on the north end of the property indicate that younger strata is to the east. The depositional environment is submarine and generally low energy as indicated by up to 400m of chert and argillite at the north end of the property. Contradictory to this quiet environment are several locations of sandstone, conglomerate, agglomerates and pyroclastics. These occurrences indicate several periods of uplift and rapid deposition into paleo-basins.

The Bralorne Intrusives were probably emplaced as sills during eugeosynclinal basin development. The diorite is generally conformable, as indicated by numerous north-south contacts though drilling shows some cross cutting contacts. There does not appear to be much contact metamorphism though gradational lithology changes are evident where the diorite is in contact with greenstones. This gradation may indicate a near surface magma with the greenstones being volcanic equivalents.

Later stage structures include two east-west strike slip faults with up to 150m displacement. These faults are not reported on previous geological maps nor is the east-west slip component. As well as mapping, evidence to support this interpretation includes three silicic dikes, up to 6m thick, which strike east-west and could be interpreted as infilling zones of weakness, and an I.P. survey which shows identical displacement of a major anomaly.

A geological model for the accumulation of sediments and volcanics with the massive sulfide occurrence is proposed with sketches to aid interpretation.

During deposition of the Bridge River Group the sea floor level was very unstable with several high and low areas. The rapid transition from thick greenstone sequences to sediments indicates synvolcanic faulting. The fault zones acted as vents and supplied the volcanic flows which filled depressions and spilled out over lower areas. Continued movement along these fault zones would allow hydrothermal solutions and sulfide ore migration as well as later zones of weakness for faulting and shearing.

Hodgson and Lydon (1977) have presented two hydro-thermal systems which could be applicable to the Wayside property. The first, Fig.29 , shows development adjacent to a fault with volcanic flow, ore accumulation, the heat source would be the intruding Bralorne sills. Figure 30 shows several ore accumulation sites with sill emplacement. This model shows a favourable horizon for ore but also the exploration difficulties.

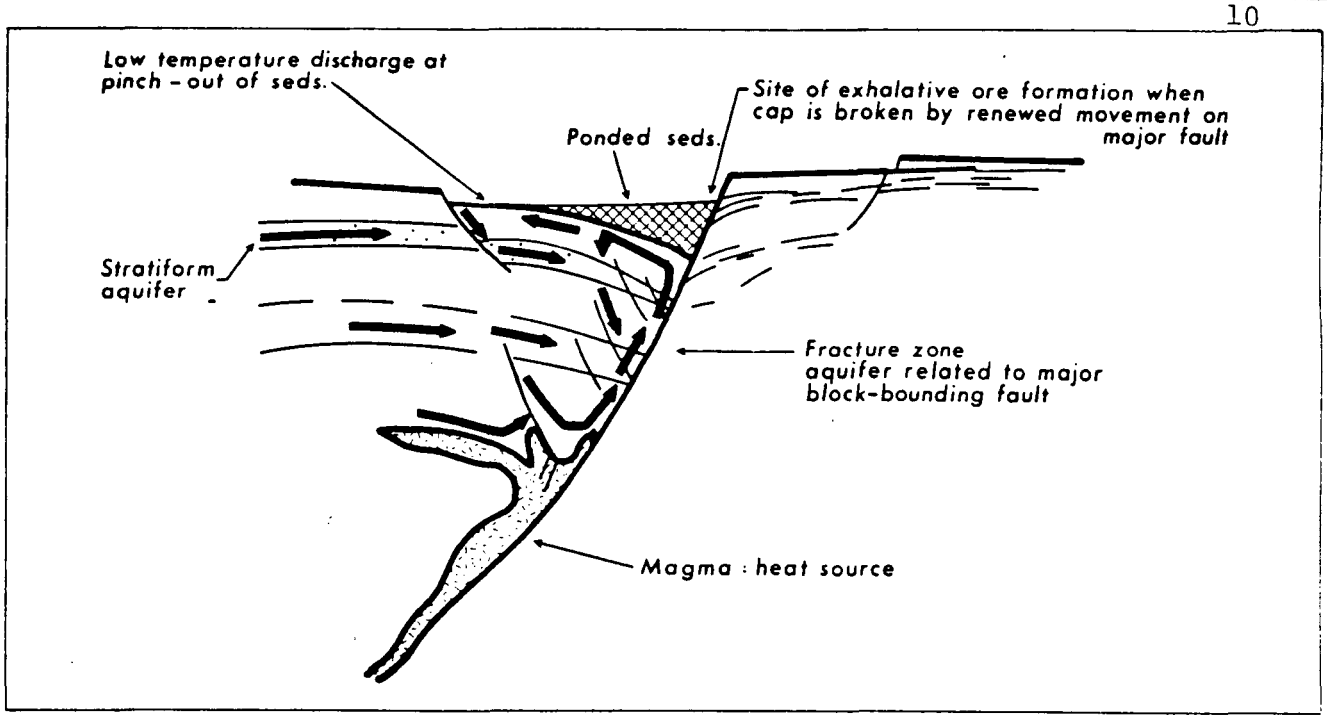


FIGURE 29 — Diagrammatic representation of a hydrothermal system developed in a fractured zone adjacent to the boundary fault of a tilted fault block.

(both from: Hodgson & Lydon, 1977)
R.G.M.

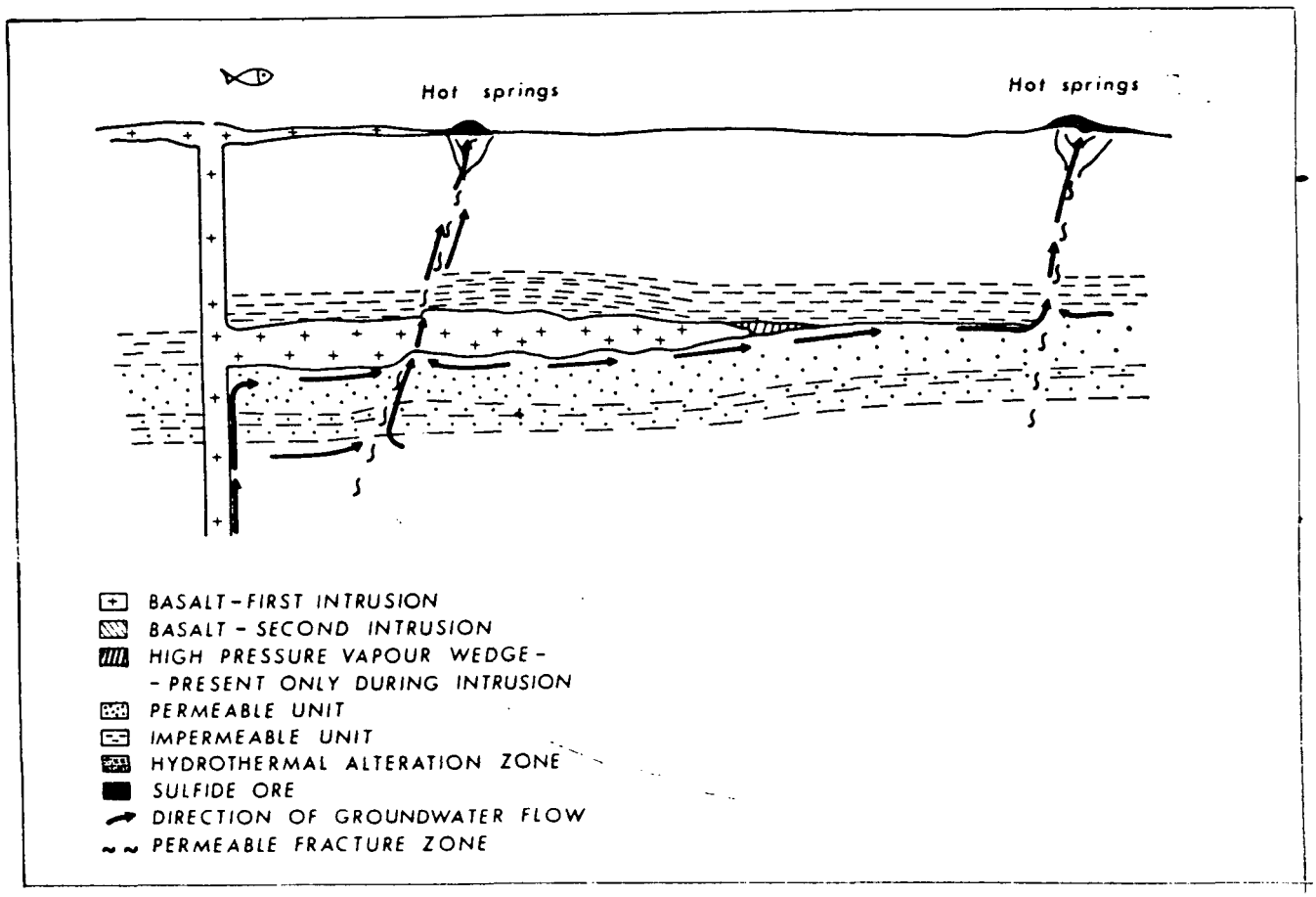


FIGURE 30 — Possible hydrothermal systems associated with sills: (a) sill emplaced beneath an impermeable layer below which the vapour wedge necessary for sill initiation and lateral expansion may form (c.f. Fig. 4), and which prevents the upward escape of groundwater heated by the sill, except where the layer is transected by permeable zones

DEPOSIT MODELLING -

The "New Discovery" is an example of a volcanogenic massive sulfide deposit. Since 1979 fourteen diamond drill holes have been completed to test a mineralized horizon approximately 140m long by 75m deep at a depth of 175 - 250m below surface. The mineralized horizon appears to be conformable with the volcanic strata. The best results include a 6.4m interval grading 1.76% Cu and 2.45% Zn (hole 79 - S6, 193.5 - 199.9m) 3.1m of 1.17% Cu and 3.03% Zn (hole 80 - S1, 206.3 - 209.4m) and 6.8m of 0.86% Cu and 2.03% Zn (hole 84 - 03, 203.5 - 210.3m).

Work in 1985 has been directed towards increasing the size of the occurrence using a volcanogenic massive sulfide deposit model. The following is a summary of characteristic features of the type deposit and observations from the New Discovery area.

| TYPE DEPOSIT FEATURES | NEW DISCOVERY |
|---|---|
| tectonic setting | - island arc, eugeosynclinal volcanic - sedimentary succession |
| age of host | - Triassic-Jurassic Bridge River Group |
| general form | - Stratabound, strata form lenses |
| deposit classification | - Cu - Zn type; minor lead; mafic footwall; Zn/Zn+Pb ratio 0.95. |
| host | - volcanic; adesitic to grabbroic (mafic greenstone), vesicular |
| submarine | - volcanics; pillows, vesicular<br>- cherts<br>- sediments; mostly argillites, some greywacke, siltstone |
| hanging wall | - sharp cut off of Cu - Zn mineralization, up to 20m above the ore is a massive |

| | |
|---|---|
| | pyrite horizon up to 100m thick. |
| footwall | - mafic volcanics; several zones of copper mineralization; pyrrhotite more common. |
| ore | - sections of massive sulfide; strata form thickness is much less than width ot length; Cu/Cu+Zn ratio is about 0.3 which approaches the typical 0.14 of massive ore |
| mineralogy | - dominantly pyrite, some chalcopyrite and sphalerite; very minor galena; some pyrrhotite |
| precious metals | - the highest values reported are from 84-03, 0.045 oz/ton Au and 1.7 oz/ton Ag. |
| gangue minerals | - quartz, chlorite, sericite. |
| alteration | - some chlorite alteration; pervasive sericite |
| structural controls | - preliminary mapping indicates rapid lithology changes, from thick volcanic sections to chert - argillite sections. |
| | - possibly synvolcanic faulting causing agglomerates and pyroclastics. |
| | - possibly thick volcanic sequences represent negative paleotopography while sediments represent paleo-highs and discharge areas. |

GENERAL FEATURES

- no oxide minerals (ex; magnetite, hematite) are obvious which may indicate shelf-basin paleotopography.

- barren sulfide horizons may be stratigraphic as well as genetic equivalents to ore horizons therefore geochemical studies may aid in deposit location.

- the deposit may be comprised of several individual ore lenses.

- no stringer ore zone has been identified; the 'footwall area' of hole 85 - 02 appeard copper rich and may represent a stringer zone.

- a heat source was near by as indicated by the Bralorne intrusives and various dikes in the immediate area.

GEOCHEMISTRY -

Sampling Procedure:

A total of 248 soil samples were collected, mostly from road cuts and trenches. The samples represent the B soil horizon where possible or the deepest soil from trenches. Road cuts provide ideal sample sites as the A soil horizon, the volcanic ash layer and the B soil horizon can be easily identified.

The sample numbering system used the road survey (chain and compass) control station numbers as a prefix and a distance from the station. The survey control stations are on all maps to aid in location of features.

A total of 76 rock samples were collected representing either channel samples or grab samples. The sample numbers correspond to survey control stations to aid in location.

LABORATORY TECHNIQUES:

Acme Analytical Lab. Ltd., of Vancouver did all of the geochem and assay work. The I.C.P. analysis report sheets include the sample preparation techniques. Appendix 1 includes the Laboratory Methodology for 1985.

Discussion of Results:

The property was divided into two projects, gold only, and massive sulfide. The gold only data is from the main Wayside diorite body and the north end, while the massive sulfide exploration was confined to volcanics and sediments between the Wayside diorite body and the southwest diorite body.

To aid in gold exploration, soil and rock samples were analysed

for 30 elements. Silver, arsenic and antimony appeared to be usefull indicator elements while cobalt, iron and vanadium showed false anomalies and occasionally failed to identify true anomalies. Figures 12, 13 and 14 show the distribution of values from soil sampling and the threshold value. Follow-up work included trenching and rock sampling where possible.

Table 1 summarizes the results of soil sampling for gold exploration with the anomalous results highlighted. Table 2 shows the results of rock sampling.

| Anomalous Sample | Description | Explanation |
|---|---|---|
| 74+00 | Wayside Shear near | on known shear zone |
| +20 | 150 Adit | no follow-up completed |
| 78+160 | Wayside Shear near | follow-up included |
| +180 | "O" Adit | channel sampling |
| +200 | | over 4m, see Table 3 and Figure 15. |
| PLA-3L | Power Line Adit, | follow-up included |
| 4L | east contact of Wayside | three rock samples, |
| | diorite | Table 2, PLA-5R, 6R, 7R. |

FOLLOW-UP

PLA-5R = chips from north wall of open cut, over +2m
PLA-6R = chips from quartz lens, 20 cm thick
PLA-7R = chips from gouge zone, argillite with quartz veinlets

| | | |
|---|---|---|
| 41 N | Trench 41, Figure 18 sample of soil debris over 5.5m | porphyry dike in black argillite |
| 11 W1 W2 N | Trench 11, Figure 16 | shear zone exposed by trenching. Grab sample 11 typifies the rock type. |

NOTE - sample 11 W1 has 0.058 oz/ton over 1.5m of soil debris above bedrock.

| | | |
|---|---|---|
| 31+240 | East contact of Wayside | Shear zone up to 5m |
| +260 | diorite. | of exposure (true thickness approx. 3m) |

FOLLOW-UP

| | |
|---|---|
| 31+256R | Calcite vein 70cm |
| 260R | random chips over 5m of shear |

Exploration for massive sulfide dominated the field program. Figures 9, 10 and 11 show the distribution of values from soil sampling and the threshold value. Follow-up work included mapping, trenching and diamond drilling. Tables 4 and 5 show the results of soil and rock sampling with the anomalous results highlighted.

| Anomalous Sample | Description | Explanation |
|---|---|---|
| | *NF means no follow-up in 1985 | |
| 103+5 | soil samples over pyroclastic | |
| 10 | with quartz and pyrite veins | |
| 15 | | |
| 70 | | |

FOLLOW-UP Trench 103, Figure 25
no economic mineralization located.

6N 490W Trench 6N 500W, Figure 26, still in overburden above big EM conductor.

98+10 NF along west contact scarp of Wayside diorite.

99+40 NF 40m from station 99 towards station 100, scree dominated sample.

100+20 NF

| Anomalous Sample | | Description Explanation contd |
|---|---|---|
| 102+25 | | Trench 103, Figure 25 |
| 30 | | over rusty gouge |
| 117+2L | | Trench 117, Figure 22 |
| 3L | | no economic mineralization located. |
| 59+00 | | |
| 59+2L | | Trench 59, soil sample over 3m, no bedrock exposed. |
| 158+30L | | Trench 158, Figure 27, no bedrock exposed. |
| 35L | | |
| HND+1L | | Trench 118, Figure 23, along highway massive sulfide exposure. |
| 117+120 | NF | Along road from 84-03 towards 84-04. |
| 140 | | Interpreted surface projection of ore |
| 180 | | horizon. |
| 200 | | |
| 220 | | |
| 240 | | |
| 260 | | |
| 340 | | |
| 420 | | |
| 129+80 | NF | Possible north extension of ore bearing strata. |
| 100 | | |
| 120 | | |
| 140 | | |
| 180 | | |
| 200 | | |
| 138+150 | NF | Possible north extension of ore bearing strata. |
| 142+15 | NF | " " " " " |

| Anomalous Sample | Description | Explanation contd |
|---|---|---|
| 31+20 | In black argillite | |
| 40 | | |
| 60 | | |
| 120 | | |

FOLLOW-UP Black argillite debris from road cut.

| | | |
|---|---|---|
| 31+100R | | |
| 32+20 | NF | Black argillite |
| 61+20 | NF | Possible north extension of ore bearing strata. |
| 40 | | |
| 60+40 | NF | Possible north extension of ore bearing strata. |

Rock sample 59R is from a piece of float located below station 59. The rock was massive pyrite in grey-black chert. It is suspected that the boulder may represent the north extension of the massive sulfide horizon. The sample is anomalous in its molybdenum content.

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WAYSIDE PROJECT

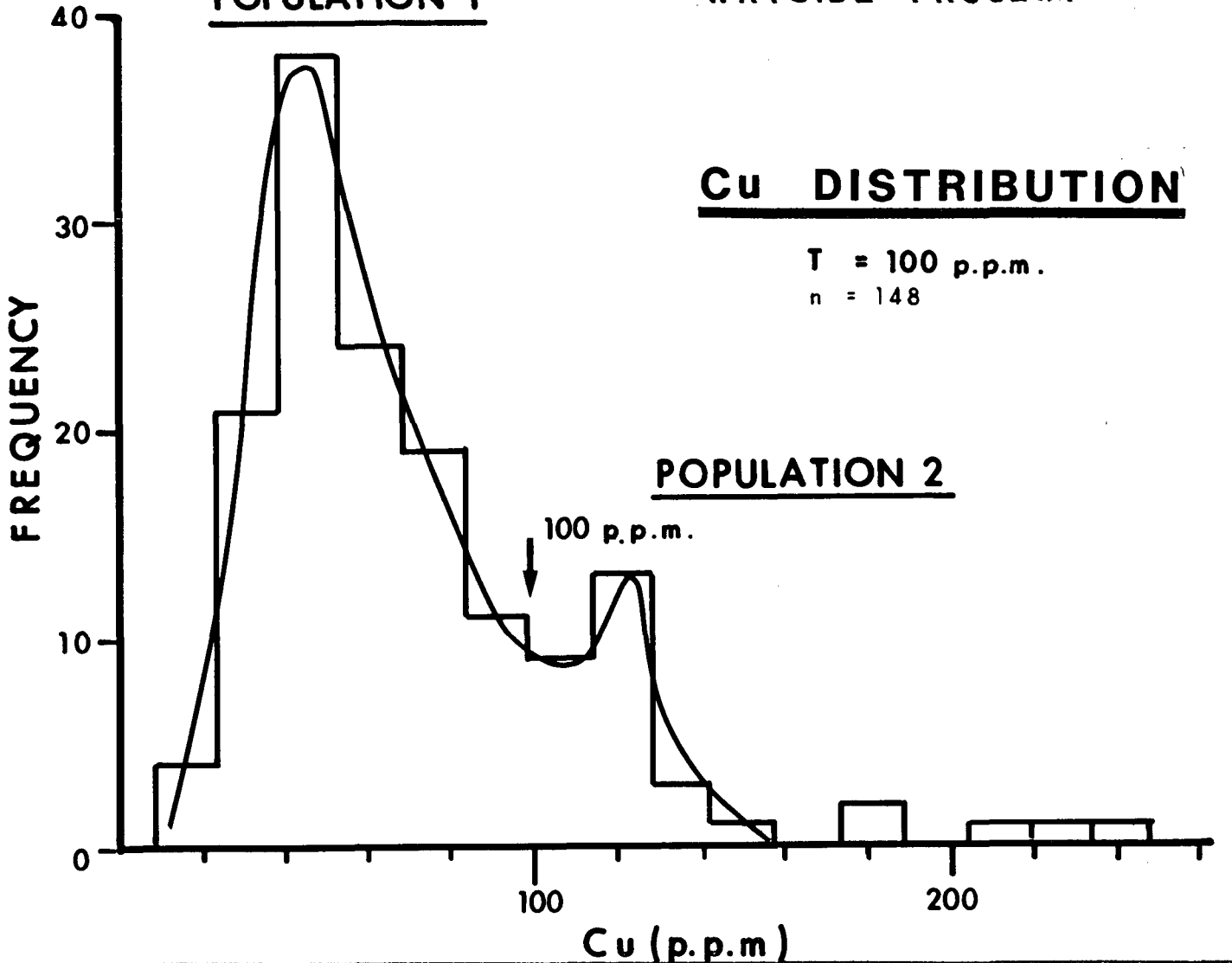


FIG 9

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## WAYSIDE PROJECT

## Pb DISTRIBUTION

T = 18 p.p.m.

n = 148

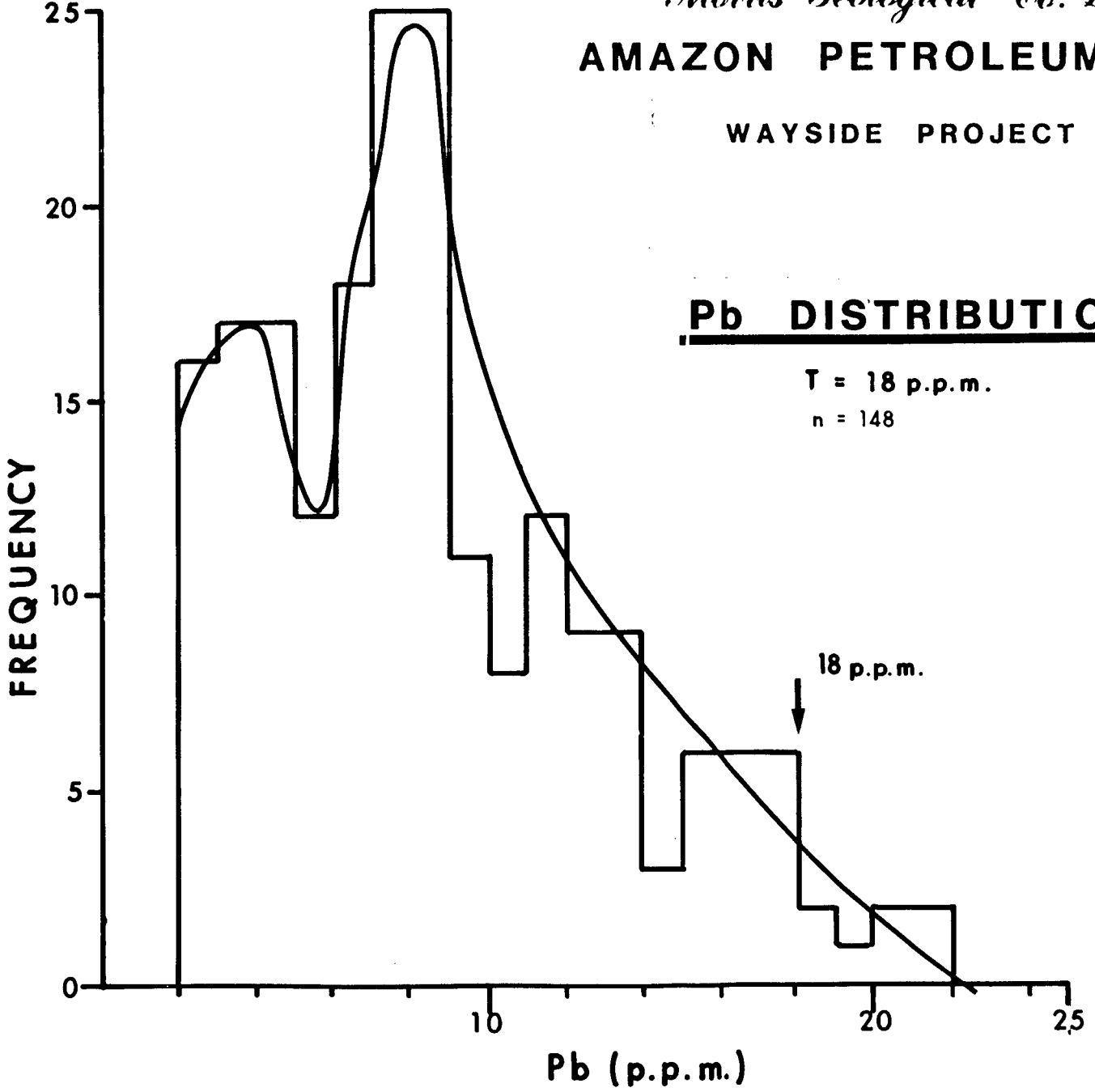


FIG. 10

R&M.

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## WAYSIDE PROJECT

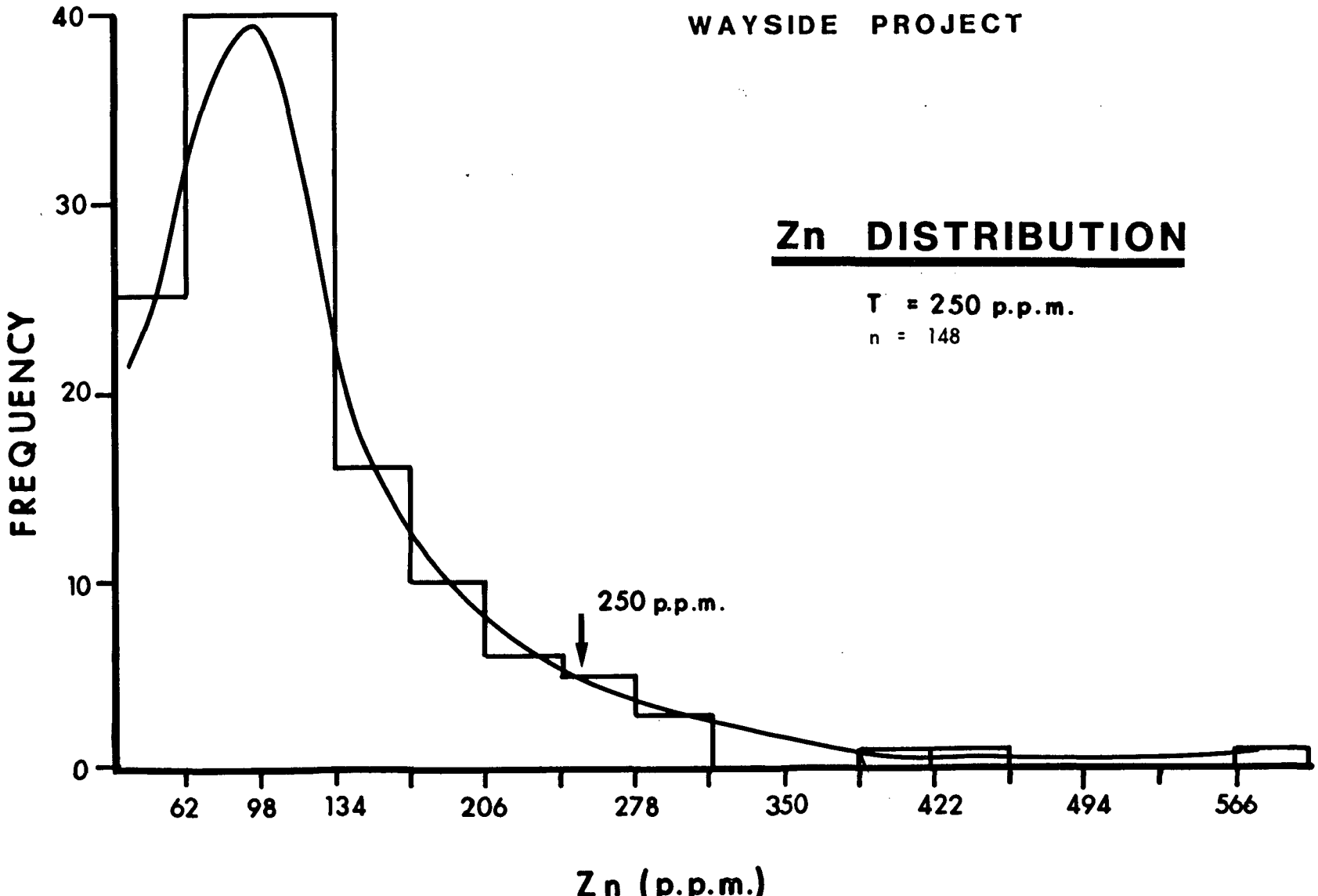


FIG. 11



RJM.

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## WAYSIDE PROJECT

## Ag DISTRIBUTION

T = 0.8 ppm
n = 98

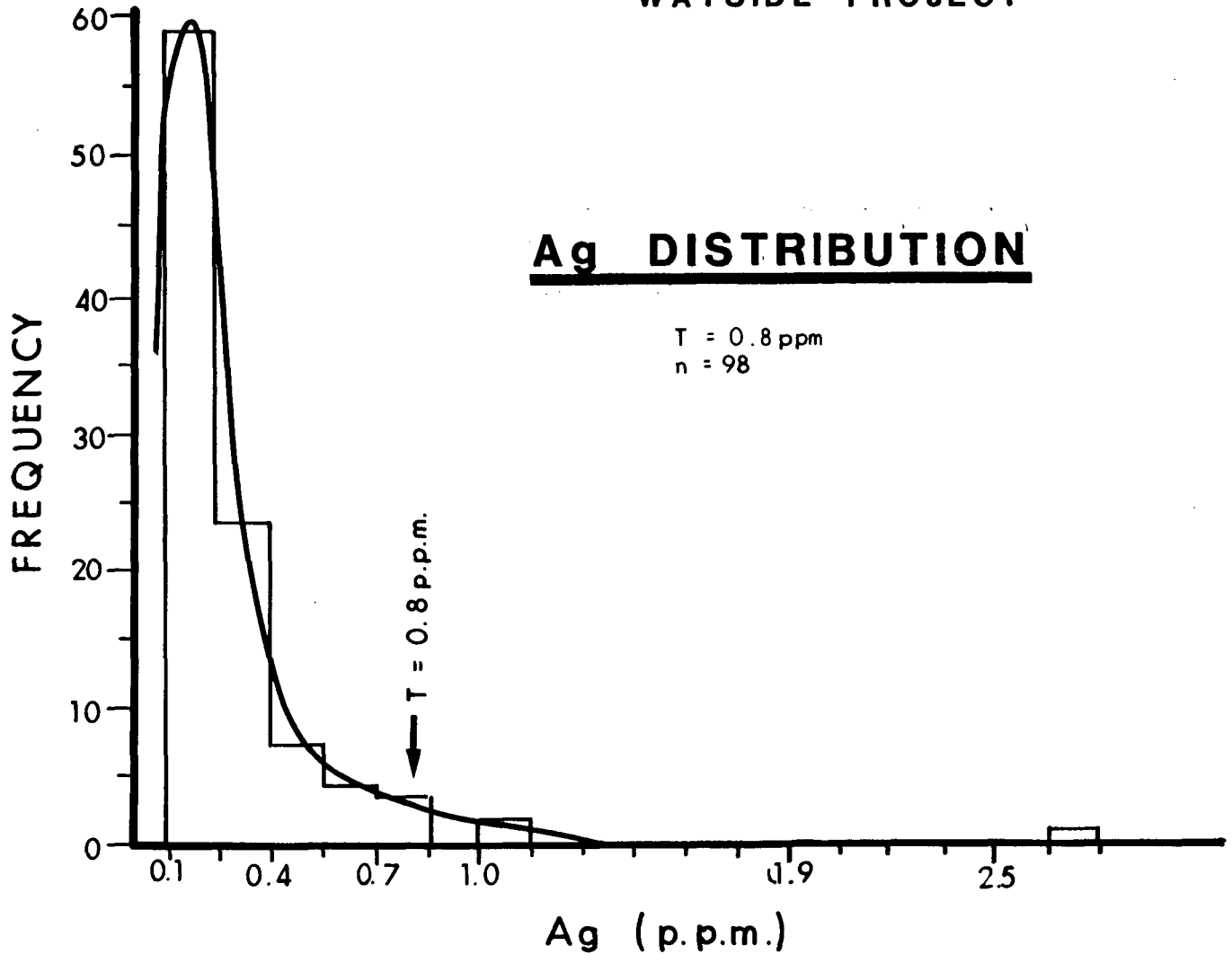


FIG. 12



RAM.

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## WAYSIDE PROJECT

## As DISTRIBUTION

T = 100 p.p.m.
n = 97

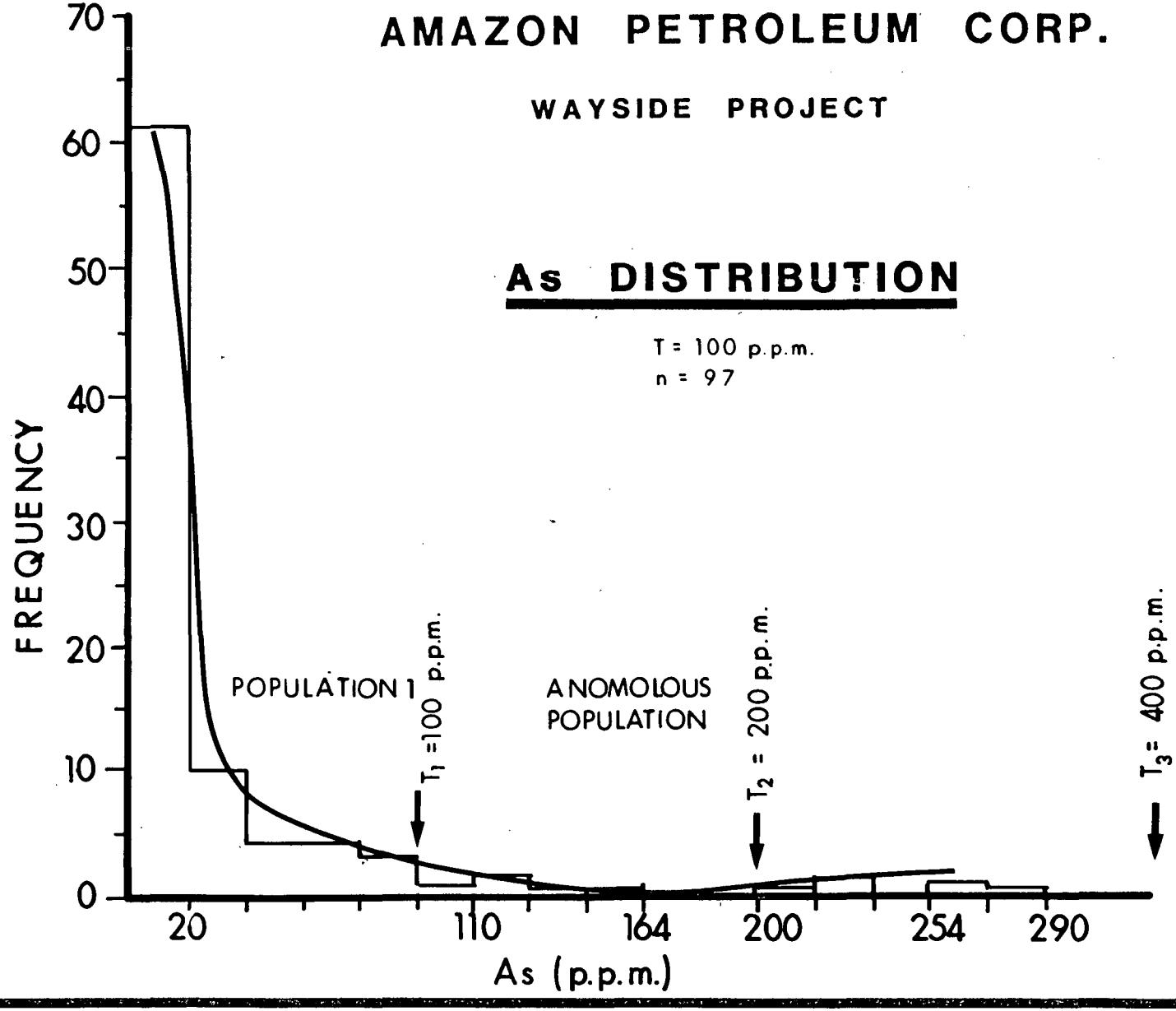


FIG. 13

RJM.

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## WAYSIDE PROJECT

## Sb DISTRIBUTION

T = 16 p.p.m.
n = 97

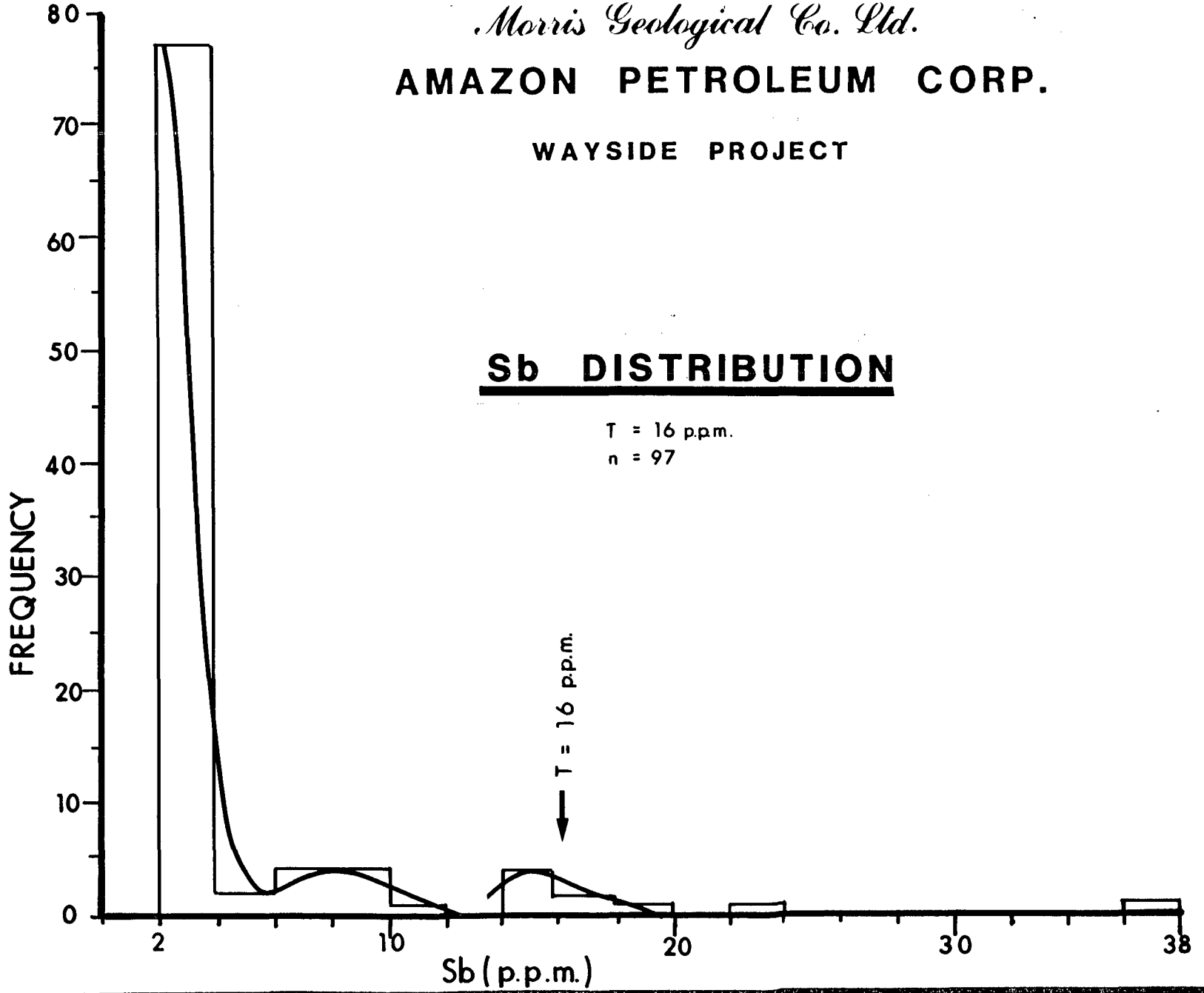


FIG. 14



RJM.

DIAMOND DRILLING -

SUMMARY:

The 1985 diamond drilling program started July 8 and by July 28 four and a half holes had been completed for a total of 587.7m. Hole 85-05 was in progress when the author completed his field contract.

Drill holes 85-01 and 85-02 were drilled to test the upward extension of the ore horizon from 84-03. Hole 85-01 was collared on the same site as 84-03 and drilled towards 260° at -70°. The hole was to intercept the ore horizon approximately 150m up dip from hole 84-03. Drill hole 85-02 was collared on the same site as 84-10, 11 and drilled towards 260° at -70°. The hole was to intercept the ore horizon approximately 60m up dip from 84-03.

Drill holes 85-03 and 85-04 were drilled to test an IP anomaly noted in 1981. Hole 85-03 was collared at the north end of the anomaly and drilled towards 270° at -45°. Hole 85-04 was collared in the south end of the anomaly and drilled towards 270° at -45°. Drill hole 85-05 was drilled to test a major EM conductor noted in 1984. It was collared east of the conductor and drilled towards 270° at -45°.

DISCUSSION OF RESULTS:

Drill hole 85-01 was in volcanic rock as projected though no ore horizon was intercepted. The footwall diorite was 23m above where it was projected and it may have truncated the ore horizon. The footwall diorite dips 80 - 85° east while the ore horizon dips 65° east, see Figure 8. Six drill core samples were taken, three quartz veins and three sulfide sections, the results are listed in Table 6.

| SAMPLE | DESCRIPTION |
|---|---|
| 2901 | 23.29m (0.18m), quartz vein with unknown silver mineral. |
| 2902 | 33.25m (0.25m), quartz vein with silver mineral. |
| 2903 | 33.38m (1.12m), breccia with abn. pyrite. |
| 2904 | 81.08m (0.18m), pyrite band. |
| 2905 | 91.20m (0.80m), disseminated pyrite. |
| 2906 | 147.37m (0.08m), quartz vein. |

Drill hole 85-02 was in volcanic rock as projected with abundant massive pyrite in the first 80m. Chalcopyrite first appeared at 77m while the first sign of sphalerite was at 135m. There was not an economic zone of massive sulfide intersected although a 3.9m section at 166m contained an appreciable amount of chalcopyrite, samples 2926 and 2927. This zone was very silicic and is precisely where the ore horizon porjects from hole 84-03. The footwall diorite was not intercepted. Twentythree core samples were collected, the results are listed in Table 6.

| SAMPLE | DESCRIPTION |
|---|---|
| 2907 | 3.05m (0.18m) massive pyrite |
| 2908 | 7.70m (0.44m) " " " |
| 2909 | 8.84m (0.46m) " " " |
| 2910 | 19.96m (0.55m) " " " |
| 2911 | 20.88m (0.46m) " " " |
| 2912 | 22.86m (0.76m) " " " |
| 2913 | 23.62M (0.31m) " " " |
| 2914 | 58.67m (1.10m) " " " |
| 2915 | 59.77m (0.89m) " " " |
| 2916 | 60.66m (1.21m) " " " |
| 2917 | 64.90m (0.91m) " " " |

| SAMPLE | | DESCRIPTION |
|---|---|---|
| 2918 | 66.90m (2.59m) | massive pyrite |
| 2919 | 76.20m (0.18m) | " " " |
| 2920 | 77.60m (2,78m) | " " ", some chalcopyrite |
| 2921 | 83.67m (2.98m) | " " " " " " " |
| 2922 | 86.65m (2.95m) | " " " " " " " |
| 2923 | 98.63m (3.33m) | chert lenses with pyrite |
| 2924 | 113.08m (0.61m) | chalcopyrite in vesicular volcanics |
| 2925 | 135.79m (0.18m) | quartz vein, breccia |
| 2926 | 166.30m (1.70m) | abn. Pyrite, some chalcopyrite, |
| 2927 | 168.00m (2.19m) | " " " " " sphalerite |
| 2928 | 191.50m (2.30m) | massive pyrite, some chalcopyrite |
| 2929 | 206.70m (1.50m) | chert bands, abn. chalcopyrite |
| 2930 | 211.10m (1.10m) | silicious breccia with pyrite |

Holes 85-01 and 85-02 showed that there is no obvious up-dip extension of the ore horizon from 84-03, the down-dip extension is still open. Drill hole 85-03 was in sediments including chert, siltstone and sandstone. No mineralization of economic significance was noted, six core samples were collected, the results are listed in Table 6.

| SAMPLE | | DESCRIPTION |
|---|---|---|
| 2931 | 3.05m (0.15m) | black mudstone with quartz veins |
| 2932 | 3.87m (0.31m) | white chert with black partings |
| 2933 | 14.02m (0.92m) | chert with black partings |
| 2934 | 25.80m (0.30m) | chert with black partings + chalcopyrite and pyrrhotite |
| 2935 | 38.20m (0.30m) | greywacke |
| 2936 | 42.76m (0.37m) | black, carbonaceous material |

Drill hole 85-04 was in sediments very similar to 85-03. The hole was abondoned at 26.82m after the core barrel parted from the rods and could not be retrieved. Three core samples were

taken, the results are listed in Table 6.

| SAMPLE | | DESCRIPTION |
|---|---|---|
| 2937 | 17.98m (0.31m) | chert with chalcopyrite |
| 2938 | 22.86m (0.15m) | black siltstone with chlorite alteration. |
| 2939 | 26.52m (0.30m) | Black siltstone, very carbonaceous |

Holes 85-03 and 85-04 tested an I.P. anomaly, no economic mineralization was located.

Drill hole 85-05 was to test a major EM conductor located in 1984. At 113m the rods were stuck and the hole was to be continued with BQ after reducing. Drilling was in progress July 28 when the author left the project. No core samples had been collected to 113m.

Drill cuttings were collected for hole 85-04 and 85-05, see Table 7. Drill hole 85-01 had no returns, hole 85-02 was in volcanics and massive sulfide and hole 85-03 was in blocky chert for the most part.

Drill core is stored in two buildings near the No. 5 adit of the old Wayside Mine.

TABLE 9

DRILL HOLE RESULTS

| Hole | From | To (m) | Thickness (m) | %Cu | %Zn | Thickness weighted combined Cu & Zn | $\frac{Cu}{Cu + Zn}$ | Intercept, see section |
|---|---|---|---|---|---|---|---|---|
| 79-S6 | 168.6 | 171.0 | 2.4 | 0.24 | 0.59 | 0.83% : 2.4m | 0.29 | a |
| | 188.4 | 191.4 | 3.0 | 0.12 | 0.69 | | 0.15 | b |
| | | 193.5 | 2.1 | 0.18 | 0.14 | | 0.56 | c |
| | | 195.7 | 2.2 | 2.56 | 1.48 | | 0.63 | d |
| | | 197.5 | 1.8 | 1.06 | 3.58 | 4.21% : 6.4m | 0.23 | e |
| | | 199.9 | 2.4 | 1.56 | 2.50 | | 0.38 | f |
| | | 202.1 | 2.2 | 0.29 | 0.48 | | 0.38 | g |
| | | 203.6 | 1.5 | 0.70 | 2.53 | | 0.22 | h |
| 80-S1 | 206.3 | 209.4 | 3.1 | 1.17 | 3.03 | 3.13% : 5.8m | 0.28 | a |
| | | 212.1 | 2.7 | 0.99 | 0.93 | | 0.52 | b |
| 80-S2 | 32.6 | 35.1 | 2.5 | 0.42 | 0.27 | 0.69% : 2.5m | 0.69 | a |
| 80-S3 | NO ORE | | | | | | | |
| 80-S4 | NO ORE | | | | | | | |
| 80-S5 | 220.1 | 223.1 | 3.0 | 0.56 | 2.32 | | 0.19 | e |
| | | 226.8 | 3.7 | 0.54 | 1.35 | 1.98% : 9.7m | 0.29 | f |
| | | 229.8 | 3.0 | 0.84 | 0.34 | | 0.71 | g |

Table 9 cont.

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 80-55 | 203.3 | 205.4 | 2.1 | 1.30 | 0.53 | 1.30% : 5.2m | 0.71 | a |
| | | 208.5 | 3.1 | 0.59 | 0.36 | | 0.62 | b |
| 80-S8 | 246.9 | 248.1 | 1.2 | 0.05 | 0.63 | 1.28% : 6.4m | 0.07 | a |
| | | 249.9 | 1.8 | 1.32 | 0.43 | | 0.75 | b |
| | | 251.8 | 1.9 | 0.69 | 0.04 | | 0.95 | c |
| | | 253.3 | 1.5 | 0.92 | 1.00 | | 0.48 | d |
| 84-03 | 176.0 | 177.4 | 1.04 | 0.14 | 0.90 | | | a |
| | 203.5 | 204.5 | 1.0 | 2.52 | 4.18 | 2.91% : 6.8m | 0.38 | b |
| | | 206.3 | 1.8 | 0.31 | 1.32 | | 0.19 | c |
| | | 207.9 | 1.6 | 0.71 | 2.36 | | 0.23 | d |
| | | 209.4 | 1.5 | 0.52 | 1.45 | | 0.26 | e |
| | | 210.3 | 0.9 | 0.98 | 1.53 | | 0.39 | f |
| | 211.2 | 212.8 | 1.6 | 0.56 | 1.73 | 2.73% : 1.9m | 0.24 | g |
| | 213.2 | 213.5 | 0.3 | 0.17 | 4.85 | | 0.01 | h |
| | 217.6 | 218.1 | 0.5 | 0.93 | 5.85 | 3.53% : 1.2m | 0.14 | i |
| | | 218.8 | 0.7 | 0.22 | 0.98 | | 0.18 | j |
| | 234.7 | 236.2 | 1.5 | 0.05 | 1.21 | | 0.04 | k |
| 84-05 | 265.9 | 266.4 | 0.5 | 1.51 | 0.24 | | | a |
| | 267.3 | 268.2 | 0.9 | 0.46 | 0.28 | | | b |

CONCLUSIONS -

The New Discovery occurrence typifies a volcanogenic massive sulfide deposit. Vesicular andesite - grabbo of the Triassic - Jurassic Bridge River Group is the host. To date 14 diamond drill holes indicate an ore horizon with a north-south strike length of 140m, and with an east dip (average of 65°) length of 75m. Potential reserves are estimated to be 150,000 tonnes(using a true thickness of 4.8m) with grades up to 1.76% Cu and 3.03% Zn and minor precious metal content.

Drilling in 1985 indicated that there is no near surface exposure of the ore horizon in the main zone (holes 85-01 and 85-02). The present interpretation shows that the down-dip extension is open and unexplored.

Drill holes 85-03 and 85-04 investigated IP anomalies which may be faulted southern extensions of the anomaly above the main zone. The holes encountered highly carbonaceous sediments which may have acted as the conductor.

Drill hole 85-05 was drilled into a major EM conductor which may have been caused by carbonaceous material and abundant water.

Geochemical studies conducted in 1985 attempted to identify the massive sulfide exposures and to locate additional target areas. Soil samples from the massive sulfide showing along the highway, at hole 85-02, are not anomalous in copper, lead or zinc though the iron content varies from 8.5 to 11.8%. Soil sampling stratigraphically below the massive pyrite showing yielded anomalous copper values (up to 2 times threshold). Anomalous zinc samples are erratic though there are four which correspond with anomalous copper areas and fit an interpreted north extension of the ore horizon. Lead shows a narrow range of values with no truly anomalous samples.

The gold only exploration was confined to the Wayside diorite and the north end of the property. On the Wayside diorite it was shown that geochemistry is an effective tool for locating anomalous areas. The main Wayside shear was identified twice as well as a smaller shear along the east contact and the Power Line adit.

On the north end of the property follow-up to 1984 sampling included detailed mapping and trenching. The anomalous geochemical samples seemed to be associated with a rhyolite dike and four trenches tested the contact zones, numbers 41, 34, 11 and 147. Trench 11 exposed a shear zone in black argillite with the highest gold value of 0.058 oz/ton (2 p.p.m) from a 1.5m sample of soil debris above bedrock.

RECOMMENDATIONS -

Several studies should be conducted to better understand the occurrence and to aid in further exploration.

1 - Detailed geological mapping to confirm the inferred structure and to better understand the lithological relationships. Initially confined to the grid area (White's grid).

2 - A geochemical soil sampling program covering from line 4S to line 6N (White's grid) from the highway west. The sample spacing would be every 20m east-west on 100m intervals north-south.

3 - A ground magnetometer survey (over White's grid) would assist the geological mapping. Lammle (1974) shows that the diorite can be mapped successfully and there is a possibility that the volcanic and sedimentary sequences could respond individually.

4 - Deep diamond drilling should be undertaken to explore the down-dip extension of the ore horizon in the main zone. The main zone is between holes 80-53 and 80-54. Drill hole 79-S6 has the nearest to surface ore intercept at 170m deep while the deepest intercept is 255m in hole 84-D5. To explore down dip from hole 84-03 a hole should be collared along line 0 approximately 200m east of hole 85-03 and drilled towards $270^{\circ}$ at $-60^{\circ}$. The ore zone would be intercepted 100m down dip from hole 84-03 with 200 meters of drilling. The hole should be drilled 400m in total which would project it vertically below hole 84-03. If ore is intercepted holes can be fanned out along line 0 to test various depths.

5 - Deep diamond drilling should be conducted to explore the north and south extensions of the main zone. Drilling to date indicates a deep ore horizon in the main zone so drilling north and south should attempt to locate ore at the same elevation; assuming no vertical displacement on the two east-west faults.

To test the north extension a hole should be collared 50m east of the highway along line 150N and drilled towards 270° at -60°. This hole would test strata due north of the main zone if no fault exists. Another hole would be collared along the baseline at 150N to test the proposed faulted north extension.

To test the south extension a hole should be collared 50m east of the highway along line 150S and drilled towards 270° at -60°. This hole would test strata due south of the main zone if no fault exists. Another hole should be collared on the west side of the highway at 250S and drilled towards 270° at -60°. This hole would test the proposed faulted south extension.

This proposed drilling will effectively test all potential strata for an extension of the known deposit.

6 - The Wayside diorite has produced gold and has been explored extensively diring the past decade. The limited mapping and soil sampling completed in 1985 indicates that there is potential for more shear zones and soil sampling could be used to locate them.

Typical shear zones are three to four meters wide and may carry up to 4830 p.p.b. gold (approx. 0.14 oz/ton), Fig. 15, Table 3.

7 - The north end of the property was explored briefly in 1985 and remains open to study. The moderately coincidental EM and arsenci anomalies should be tested further with deep trenching or drilling.

Trench 11, Fig. 16 exposed a shear zone with soil debris running up to 0.058 oz/ton gold (2 p.p.m.).

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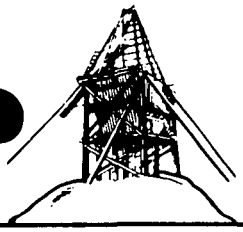

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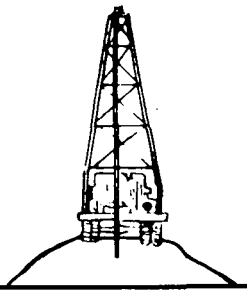

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STATEMENT TO CARPENTER LAKE RESOURCES LTD.
PERIOD: DECEMBER 1/84 to SEPTEMBER 30/85.

EXPENDITURES:

| | |
|---|---|
| Advertising & promotion | $4,200.00 |
| Geological & Engineering | 33,642.62 |
| I.C.B.C. | 759.00 |
| Mapping | 726.00 |
| Field wages & supervision | 10,500.00 |
| News releases & printing | 2,555.20 |
| Engineers reports | 737.56 |
| Assays | 3,698.40 |
| Dicks Mechanical Contracting | 5,353.25 |
| Gold Bridge Hotel | 4,099.52 |
| Legal fees | 1,500.00 |
| M & B Drilling | 63,770.57 |
| Labour | 4,142.00 |
| Secretarial | 1,000.00 |
| J & H Trucking | 217.00 |
| B. C. Telephone | 196.76 |
| Sub-Total | $137,097.88 |
| Over-run from Nov. 30/84 Statement | 10,745.76 |
| TOTAL to Sept. 30/85 | $147,843.64. |

Outstanding invoices for October will be submitted.

SIGNED: R. Schmick
AMAZON PETROLEUM CORP.

ACCEPTED BY: K. Dumont
CARPENTER LAKE RES.

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 64+0+00 | 1 | 53 | 4 | 67 | .3 | 115 | 12 | 345 | 3.35 | 9 | 5 | ND | 5 | 21 | 1 | 2 | 2 | 57 | .45 | .04 | 7 | 133 | 1.18 | 106 | .20 | 7 | 1.34 | .01 | .08 | 1 |
| 64+0+20 | 1 | 69 | 4 | 115 | .1 | 172 | 27 | 899 | 3.54 | 16 | 5 | ND | 3 | 47 | 1 | 3 | 2 | 53 | 1.26 | .09 | 7 | 134 | 2.07 | 65 | .13 | 17 | 1.60 | .03 | .09 | 1 |
| 64+0+20A | 2 | 66 | 10 | 107 | .3 | 93 | 13 | 409 | 4.26 | 14 | 5 | ND | 4 | 30 | 1 | 2 | 2 | 61 | .44 | .09 | 10 | 97 | 1.09 | 162 | .17 | 9 | 1.50 | .01 | .13 | 1 |
| 64+0+40 | 1 | 97 | 2 | 73 | .2 | 199 | 22 | 484 | 3.75 | 8 | 5 | ND | 3 | 18 | 1 | 2 | 2 | 59 | .45 | .05 | 5 | 227 | 2.28 | 128 | .12 | 10 | 2.52 | .01 | .05 | 1 |
| 64+0+60 | 1 | 85 | 5 | 76 | .1 | 143 | 24 | 512 | 4.22 | 4 | 5 | ND | 2 | 21 | 1 | 2 | 2 | 76 | .54 | .08 | 3 | 191 | 2.91 | 115 | .13 | 10 | 3.58 | .01 | .04 | 1 |
| 64+0+80 | 1 | 161 | 3 | 49 | .2 | 99 | 16 | 331 | 3.86 | 8 | 5 | ND | 3 | 40 | 1 | 2 | 3 | 109 | .44 | .04 | 4 | 101 | 1.54 | 72 | .13 | 9 | 2.25 | .01 | .03 | 1 |
| 64+1+00 | 1 | 106 | 10 | 112 | .1 | 139 | 20 | 527 | 3.07 | 18 | 5 | ND | 1 | 41 | 1 | 2 | 3 | 43 | .59 | .06 | 6 | 165 | 2.24 | 103 | .09 | 12 | 2.33 | .02 | .06 | 1 |
| 64+1+20 | 1 | 180 | 9 | 52 | .2 | 260 | 31 | 450 | 3.72 | 14 | 5 | ND | 2 | 23 | 1 | 2 | 2 | 41 | .65 | .03 | 2 | 251 | 3.93 | 35 | .06 | 16 | 3.25 | .01 | .03 | 1 |
| 64+1+40 | 1 | 98 | 5 | 151 | .3 | 165 | 22 | 814 | 2.89 | 11 | 5 | ND | 4 | 38 | 1 | 2 | 2 | 36 | .75 | .04 | 9 | 120 | 1.91 | 140 | .09 | 16 | 2.63 | .02 | .06 | 1 |
| 74+0+00 | 1 | 39 | 5 | 30 | .1 | 77 | 55 | 1160 | 3.52 | 258 | 14 | ND | 8 | 113 | 1 | 14 | 2 | 46 | 14.45 | .01 | 2 | 47 | .72 | 17 | .01 | 28 | .39 | .01 | .01 | 1 |
| 74+0+20 | 1 | 159 | 5 | 46 | .1 | 71 | 17 | 223 | 4.17 | 222 | 5 | ND | 2 | 15 | 1 | 8 | 2 | 66 | .31 | .04 | 2 | 105 | .65 | 46 | .03 | 23 | 1.19 | .01 | .06 | 1 |
| 74+0+40 | 1 | 75 | 3 | 55 | .3 | 67 | 9 | 219 | 2.91 | 18 | 5 | ND | 4 | 18 | 1 | 2 | 2 | 56 | .28 | .03 | 7 | 80 | .76 | 68 | .13 | 11 | 1.46 | .01 | .09 | 1 |
| 78+0+00 | 1 | 38 | 10 | 289 | .1 | 255 | 12 | 700 | 2.94 | 7 | 5 | ND | 4 | 32 | 1 | 2 | 2 | 52 | .38 | .07 | 8 | 51 | .95 | 126 | .19 | 15 | 1.99 | .01 | .17 | 1 |
| 78+0+20 | 1 | 35 | 2 | 76 | .3 | 85 | 11 | 345 | 3.03 | 5 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 55 | .32 | .04 | 7 | 80 | 1.00 | 83 | .15 | 10 | 1.74 | .01 | .11 | 1 |
| 78+0+40 | 1 | 18 | 9 | 49 | .1 | 25 | 8 | 193 | 2.57 | 11 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 65 | .21 | .32 | 8 | 27 | .63 | 41 | .20 | 7 | 1.65 | .02 | .02 | 1 |
| 78+0+60 | 1 | 35 | 5 | 67 | .4 | 66 | 11 | 427 | 2.73 | 9 | 5 | ND | 3 | 20 | 1 | 2 | 2 | 52 | .31 | .06 | 5 | 68 | .94 | 137 | .14 | 12 | 1.75 | .01 | .07 | 1 |
| 78+0+80 | 2 | 49 | 7 | 110 | .1 | 96 | 14 | 1257 | 2.88 | 13 | 5 | ND | 4 | 19 | 1 | 2 | 2 | 53 | .29 | .06 | 10 | 66 | .87 | 132 | .13 | 9 | 2.03 | .02 | .08 | 1 |
| 78+1+00 | 2 | 18 | 2 | 87 | .1 | 12 | 4 | 445 | 1.23 | 5 | 5 | ND | 1 | 19 | 1 | 2 | 3 | 28 | .21 | .19 | 4 | 7 | .21 | 140 | .09 | 10 | .67 | .02 | .05 | 1 |
| 78+1+20 | 1 | 137 | 4 | 50 | .1 | 68 | 9 | 290 | 2.68 | 22 | 5 | ND | 2 | 20 | 1 | 2 | 2 | 54 | .36 | .04 | 6 | 65 | .80 | 70 | .14 | 11 | 1.23 | .01 | .06 | 1 |
| 78+1+40 | 1 | 304 | 3 | 136 | .1 | 101 | 12 | 566 | 2.76 | 2 | 5 | ND | 3 | 49 | 1 | 2 | 2 | 43 | .84 | .04 | 10 | 128 | 1.20 | 134 | .11 | 28 | 1.81 | .02 | .08 | 1 |
| 78+1+60 | 1 | 151 | 7 | 69 | .4 | 70 | 20 | 562 | 3.45 | 118 | 5 | ND | 2 | 30 | 1 | 3 | 3 | 56 | .58 | .05 | 6 | 106 | 1.20 | 105 | .10 | 26 | 1.49 | .02 | .10 | 1 |
| 78+1+80 | 1 | 201 | 3 | 66 | .6 | 98 | 20 | 341 | 4.35 | 124 | 5 | ND | 1 | 20 | 1 | 11 | 2 | 80 | .41 | .07 | 2 | 268 | 1.46 | 81 | .03 | 20 | 1.78 | .01 | .07 | 1 |
| 78+2+00 | 1 | 275 | 9 | 44 | 2.7 | 76 | 27 | 731 | 7.28 | 1807 | 5 | 7 | 1 | 16 | 1 | 37 | 2 | 139 | .33 | .02 | 4 | 76 | .41 | 55 | .01 | 32 | 1.02 | .01 | .04 | 2 |
| PLA-1-L | 4 | 81 | 8 | 168 | .4 | 92 | 23 | 801 | 4.34 | 42 | 5 | ND | 5 | 61 | 1 | 7 | 2 | 47 | 2.53 | .11 | 11 | 62 | 1.18 | 95 | .07 | 23 | 1.28 | .03 | .07 | 1 |
| PLA-2-L | 3 | 73 | 7 | 150 | .3 | 81 | 21 | 708 | 4.11 | 56 | 5 | ND | 5 | 58 | 1 | 7 | 2 | 47 | 2.18 | .12 | 9 | 59 | 1.12 | 86 | .07 | 25 | 1.15 | .02 | .06 | 1 |
| PLA-3-L | 2 | 106 | 18 | 137 | .5 | 166 | 67 | 988 | 5.47 | 1661 | 5 | ND | 6 | 100 | 1 | 19 | 2 | 56 | 2.19 | .09 | 5 | 97 | 1.74 | 65 | .01 | 23 | 1.26 | .01 | .05 | 1 |
| PLA-4-L | 1 | 102 | 17 | 139 | .4 | 163 | 65 | 1013 | 5.33 | 1498 | 5 | ND | 3 | 103 | 1 | 16 | 2 | 55 | 2.30 | .09 | 4 | 91 | 1.77 | 68 | .01 | 23 | 1.26 | .01 | .04 | 1 |
| 41 S | 1 | 62 | 15 | 155 | .3 | 75 | 13 | 673 | 3.96 | 72 | 5 | ND | 3 | 24 | 1 | 5 | 6 | 50 | .35 | .12 | 14 | 60 | .72 | 93 | .10 | 13 | 1.49 | .01 | .06 | 1 |
| 41 N | 9 | 174 | 21 | 279 | 1.0 | 64 | 18 | 1343 | 8.27 | 59 | 5 | ND | 6 | 24 | 1 | 14 | 2 | 45 | .26 | .22 | 35 | 38 | .40 | 71 | .03 | 12 | 1.07 | .01 | .04 | 1 |
| 41 M | 1 | 40 | 8 | 79 | .1 | 70 | 10 | 622 | 3.25 | 42 | 5 | ND | 3 | 20 | 1 | 3 | 3 | 46 | .33 | .08 | 10 | 66 | .72 | 83 | .11 | 10 | 1.31 | .01 | .08 | 1 |
| A34E | 3 | 59 | 7 | 112 | .1 | 24 | 10 | 1025 | 6.87 | 14 | 5 | ND | 4 | 29 | 1 | 2 | 2 | 43 | .82 | .07 | 20 | 15 | .42 | 130 | .01 | 15 | 1.17 | .01 | .06 | 1 |
| 11 M1 | 1 | 79 | 6 | 93 | .8 | 796 | 47 | 1528 | 7.09 | 220 | 5 | 2 | 6 | 96 | 1 | 15 | 2 | 73 | .68 | .06 | 12 | 613 | 2.05 | 86 | .04 | 18 | 1.77 | .01 | .06 | 1 |
| 11 M2 | 1 | 84 | 9 | 132 | .8 | 773 | 51 | 993 | 7.56 | 257 | 5 | ND | 5 | 126 | 1 | 17 | 2 | 69 | .81 | .08 | 12 | 524 | 3.11 | 78 | .03 | 15 | 1.48 | .01 | .03 | 1 |
| 11 E | 1 | 42 | 8 | 93 | .1 | 109 | 11 | 418 | 3.21 | 31 | 5 | ND | 4 | 22 | 1 | 3 | 2 | 52 | .25 | .09 | 8 | 83 | .84 | 96 | .10 | 10 | 1.45 | .01 | .06 | 1 |
| 11 S | 1 | 62 | 2 | 76 | .1 | 468 | 34 | 851 | 4.46 | 50 | 5 | ND | 5 | 129 | 1 | 9 | 2 | 64 | 1.40 | .07 | 8 | 426 | 3.19 | 60 | .07 | 13 | 2.04 | .01 | .04 | 1 |
| 11 N | 10 | 125 | 15 | 130 | .3 | 479 | 31 | 2532 | 7.75 | 210 | 5 | ND | 4 | 91 | 1 | 23 | 2 | 103 | .68 | .08 | 13 | 289 | 1.62 | 116 | .03 | 14 | 1.84 | .01 | .04 | 1 |

ABOVE STA. 64

ABOVE STA. 74

FROM STA. 78

POWER LINE ADIT

TRENCH 41

TRENCH 34

TRENCH 11

TABLE 1

GOLD EXPLORATION SOIL

TABLE 1

GOLD EXPLORATION SOIL

| | SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 99+50L | 1 | 86 | 10 | 91 | .3 | 148 | 18 | 893 | 4.75 | 11 | 7 | ND | 4 | 28 | 1 | 2 | 2 | 64 | .53 | .08 | 22 | 128 | 1.35 | 227 | .20 | 10 | 1.69 | .02 | .11 | 1 |
| | 99+60L | 1 | 79 | 10 | 98 | .1 | 139 | 18 | 953 | 4.58 | 11 | 5 | ND | 6 | 33 | 1 | 2 | 2 | 61 | .58 | .09 | 24 | 128 | 1.45 | 304 | .18 | 14 | 1.65 | .03 | .12 | 1 |
| TRENCH 99 | 99+80L | 1 | 63 | 8 | 70 | .1 | 104 | 16 | 794 | 3.68 | 12 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 67 | .71 | .12 | 10 | 88 | 1.58 | 186 | .22 | 10 | 1.68 | .04 | .12 | 1 |
| | 99+90L | 1 | 77 | 10 | 75 | .2 | 138 | 19 | 744 | 4.52 | 11 | 5 | ND | 2 | 32 | 1 | 3 | 3 | 76 | .59 | .07 | 15 | 143 | 1.47 | 272 | .24 | 7 | 2.44 | .02 | .11 | 1 |
| NO. 31 FOLLOW UP | 31+260L | 1 | 166 | 16 | 77 | .4 | 111 | 31 | 698 | 5.93 | (1274) | 5 | ND | 1 | 45 | 1 | 6 | 2 | 76 | 1.75 | .05 | 5 | 152 | 1.86 | 51 | .03 | 9 | 2.62 | .01 | .08 | 3 |
| | 81+15L | 2 | 172 | 12 | 64 | .2 | 153 | 32 | 994 | 4.06 | 49 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 72 | 1.03 | .09 | 7 | 160 | 2.68 | 100 | .17 | 11 | 2.17 | .02 | .08 | 1 |
| TRENCH 81 | 81+20L | 1 | 192 | 5 | 70 | .3 | 105 | 20 | 845 | 4.15 | 68 | 5 | ND | 2 | 37 | 1 | 2 | 3 | 78 | .99 | .09 | 9 | 100 | 1.85 | 114 | .20 | 10 | 2.14 | .03 | .10 | 1 |
| | 81+25L | 1 | 196 | 10 | 67 | .2 | 135 | 22 | 800 | 4.20 | 44 | 5 | ND | 2 | 36 | 1 | 2 | 2 | 77 | .91 | .08 | 10 | 118 | 1.97 | 100 | .19 | 9 | 2.33 | .03 | .09 | 1 |
| | 147+4 | 2 | 67 | 15 | 117 | .2 | 62 | 13 | 931 | 4.38 | 18 | 5 | ND | 1 | 31 | 1 | 4 | 2 | 45 | .39 | .07 | 7 | 56 | .82 | 96 | .08 | 2 | 1.62 | .02 | .11 | 1 |
| | 147+7 | 1 | 56 | 13 | 89 | .2 | 76 | 13 | 806 | 3.73 | 20 | 5 | ND | 1 | 28 | 1 | 3 | 2 | 48 | .41 | .07 | 7 | 69 | .88 | 97 | .10 | 2 | 1.50 | .02 | .11 | 1 |
| TRENCH 147 | 147+9 | 1 | 58 | 15 | 94 | .1 | 86 | 14 | 697 | 3.94 | 15 | 5 | ND | 1 | 27 | 1 | 2 | 2 | 57 | .41 | .08 | 8 | 76 | .99 | 97 | .11 | 2 | 1.59 | .03 | .13 | 1 |
| | 147+12 | 1 | 59 | 12 | 78 | .2 | 88 | 13 | 961 | 4.14 | 35 | 5 | ND | 1 | 29 | 1 | 2 | 2 | 50 | .45 | .07 | 7 | 61 | 1.12 | 88 | .07 | 2 | 1.56 | .03 | .09 | 1 |
| STA. 156 | 156+37L | 1 | 73 | 9 | 67 | .2 | 52 | 13 | 485 | 3.92 | 66 | 5 | ND | 1 | 25 | 1 | 2 | 2 | 59 | .55 | .06 | 3 | 71 | .88 | 57 | .07 | 11 | 1.55 | .02 | .07 | 1 |
| | 23+0+40 | 1 | 36 | 7 | 114 | .1 | 72 | 11 | 359 | 2.86 | 2 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 49 | .41 | .06 | 3 | 91 | 1.27 | 89 | .09 | 15 | 1.96 | .02 | .08 | 1 |
| NEAR | 23+0+60 | 1 | 43 | 6 | 93 | .1 | 44 | 9 | 303 | 2.84 | 82 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 40 | .32 | .04 | 4 | 46 | .62 | 67 | .06 | 11 | 1.38 | .02 | .07 | 1 |
| STA. 23 | 23+0+80 | 1 | 83 | 7 | 143 | .3 | 75 | 20 | 777 | 4.54 | 78 | 5 | ND | 2 | 38 | 1 | 2 | 2 | 72 | .52 | .08 | 2 | 73 | 1.17 | 74 | .08 | 16 | 2.02 | .02 | .10 | 1 |
| | 23+1+00 | 1 | 49 | 6 | 66 | .2 | 75 | 12 | 298 | 2.86 | 15 | 5 | ND | 3 | 18 | 1 | 2 | 2 | 50 | .34 | .03 | 5 | 72 | .99 | 73 | .11 | 12 | 1.67 | .02 | .07 | 1 |
| | 23+1+20 | 1 | 53 | 3 | 54 | .1 | 65 | 10 | 249 | 2.84 | 7 | 5 | ND | 1 | 17 | 1 | 2 | 2 | 53 | .36 | .04 | 2 | 71 | 1.01 | 54 | .10 | 12 | 1.54 | .02 | .06 | 1 |
| | 31+1+60 | 1 | 125 | 7 | 155 | .3 | 124 | 31 | 714 | 5.53 | 21 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 109 | .59 | .04 | 2 | 241 | 3.72 | 70 | .06 | 18 | 4.15 | .01 | .05 | 1 |
| | 31+1+80 | 1 | 95 | 4 | 53 | .1 | 114 | 20 | 443 | 3.84 | 3 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 68 | .67 | .02 | 2 | 214 | 3.26 | 52 | .09 | 17 | 3.38 | .01 | .03 | 1 |
| NEAR STA. 31 | 31+2+00 | 1 | 119 | 10 | 109 | .1 | 149 | 29 | 563 | 5.38 | 68 | 5 | ND | 1 | 29 | 1 | 3 | 2 | 79 | .74 | .04 | 5 | 237 | 2.95 | 63 | .03 | 18 | 3.33 | .01 | .04 | 1 |
| | 31+2+20 | 1 | 99 | 6 | 66 | .2 | 115 | 22 | 524 | 4.58 | 88 | 5 | ND | 1 | 25 | 1 | 2 | 2 | 72 | .50 | .04 | 2 | 131 | 2.00 | 103 | .04 | 13 | 2.63 | .01 | .04 | 2 |
| | 31+2+40 | 1 | 69 | 8 | 69 | .2 | 91 | 19 | 545 | 3.83 | (145) | 5 | ND | 2 | 20 | 1 | 2 | 2 | 69 | .30 | .06 | 4 | 150 | 1.59 | 78 | .06 | 9 | 2.36 | .02 | .06 | 1 |
| | 31+2+60 | 1 | 110 | 7 | 66 | .3 | 168 | 25 | 376 | 4.75 | (280) | 5 | ND | 2 | 18 | 1 | 2 | 2 | 60 | .34 | .04 | 2 | 179 | 1.54 | 41 | .03 | 17 | 2.06 | .01 | .06 | 1 |
| | 52+0+00 | 1 | 41 | 4 | 50 | .1 | 102 | 12 | 379 | 3.03 | 6 | 5 | ND | 2 | 16 | 1 | 2 | 2 | 58 | .38 | .03 | 3 | 90 | 1.08 | 74 | .18 | 8 | 1.26 | .02 | .09 | 1 |
| NEAR STA. 52 | 52+0+20 | 1 | 43 | 9 | 100 | .1 | 113 | 14 | 582 | 3.49 | 9 | 5 | ND | 3 | 15 | 1 | 2 | 5 | 61 | .32 | .09 | 10 | 65 | 1.10 | 103 | .15 | 10 | 1.81 | .01 | .10 | 1 |
| | 52+0+40 | 1 | 53 | 10 | 107 | .1 | 71 | 15 | 768 | 4.19 | 6 | 5 | ND | 2 | 21 | 1 | 2 | 2 | 85 | .48 | .12 | 6 | 63 | 1.66 | 108 | .19 | 10 | 2.09 | .01 | .07 | 1 |
| | 52+0+60 | 1 | 28 | 8 | 195 | .4 | 59 | 13 | 1437 | 2.68 | 10 | 5 | ND | 3 | 14 | 1 | 3 | 2 | 51 | .26 | .07 | 5 | 50 | .65 | 162 | .14 | 9 | 1.43 | .01 | .09 | 1 |
| | 52+0+80 | 1 | 26 | 3 | 75 | .4 | 73 | 10 | 685 | 2.55 | 9 | 5 | ND | 3 | 14 | 1 | 2 | 2 | 46 | .27 | .03 | 8 | 59 | .64 | 143 | .14 | 10 | 1.42 | .01 | .09 | 1 |
| | 52+1+00 | 1 | 37 | 4 | 69 | .2 | 83 | 10 | 432 | 2.76 | 4 | 5 | ND | 1 | 13 | 1 | 3 | 3 | 45 | .33 | .04 | 8 | 82 | .80 | 133 | .15 | 7 | 1.41 | .01 | .09 | 1 |

| | SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| TRENCH 11 | 11 | 1 | 22 | 6 | 42 | .2 | 1224 | 59 | 775 | 5.13 | 77 | 5 | ND | 2 | 162 | 1 | 8 | 2 | 27 | 1.84 | .01 | 2 | 1108 | 5.27 | 30 | .01 | 10 | .88 | .01 | .01 | 1 |
| | A34E | 1 | 15 | 4 | 35 | .2 | 22 | 5 | 811 | 1.88 | 5 | 60 | ND | 1 | 212 | 1 | 2 | 2 | 18 | 24.66 | .06 | 2 | 18 | .82 | 43 | .01 | 8 | .33 | .01 | .04 | 2 |
| TRENCH 34 | 34 E | 1 | 35 | 2 | 53 | .1 | 87 | 12 | 439 | 3.35 | 163 | 5 | ND | 3 | 25 | 1 | 2 | 5 | 56 | .40 | .09 | 8 | 78 | .93 | 56 | .09 | 11 | 1.07 | .01 | .02 | 1 |
| TRENCH 99 | 99+9R | 9 | 107 | 9 | 119 | .1 | 248 | 24 | 1422 | 4.56 | 18 | 5 | ND | 4 | 151 | 1 | 2 | 5 | 80 | .18 | .05 | 9 | 143 | .38 | 157 | .03 | 15 | .75 | .01 | .06 | 1 |
| | 99+23R | 3 | 74 | 8 | 136 | .3 | 905 | 59 | 1678 | 8.94 | 71 | 5 | ND | 2 | 45 | 1 | 2 | 4 | 117 | 1.78 | .01 | 2 | 540 | .51 | 96 | .01 | 16 | .73 | .01 | .02 | 1 |
| | 99+60R | 3 | 80 | 11 | 74 | .1 | 52 | 14 | 783 | 4.69 | 6 | 5 | ND | 3 | 31 | 1 | 2 | 6 | 71 | .26 | .12 | 9 | 35 | .21 | 361 | .01 | 17 | .58 | .05 | .13 | 1 |
| FOLLOW-UP STA. 31 | 31+25GR | 1 | 20 | 4 | 16 | .1 | 6 | 4 | 967 | 1.44 | 38 | 5 | ND | 1 | 706 | 1 | 2 | 2 | 25 | 25.84 | .01 | 2 | 8 | .51 | 22 | .01 | 2 | .64 | .01 | .02 | 1 |
| | 31+26GR | 1 | 72 | 4 | 42 | .2 | 38 | 14 | 911 | 3.80 | 855 | 5 | ND | 2 | 275 | 1 | 2 | 2 | 30 | 9.10 | .02 | 3 | 52 | 2.03 | 17 | .01 | 2 | .88 | .01 | .05 | 1 |
| TRENCH 81 | 81+31R | 2 | 198 | 9 | 60 | .1 | 57 | 28 | 1106 | 6.17 | 221 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 121 | .68 | .02 | 4 | 75 | 5.04 | 25 | .01 | 11 | 4.77 | .01 | .05 | 1 |
| | 81+32R | 1 | 222 | 13 | 74 | .1 | 44 | 37 | 1141 | 9.27 | 129 | 5 | ND | 1 | 14 | 1 | 2 | 2 | 311 | .57 | .03 | 2 | 34 | 2.73 | 38 | .01 | 12 | 4.19 | .03 | .07 | 1 |
| | 81+35R | 1 | 442 | 3 | 44 | .1 | 131 | 32 | 850 | 4.31 | 18 | 5 | ND | 1 | 11 | 1 | 2 | 2 | 74 | .61 | .02 | 2 | 103 | 5.28 | 13 | .06 | 5 | 4.13 | .03 | .04 | 1 |
| STA. 156 | 156+37R | 1 | 65 | 11 | 38 | .1 | 82 | 25 | 1040 | 4.28 | 48 | 5 | ND | 1 | 158 | 1 | 2 | 2 | 82 | 5.95 | .01 | 2 | 197 | 2.69 | 23 | .01 | 7 | 2.14 | .03 | .04 | 1 |
| STA. 52 | 52 | 23 | 314 | 42 | 36 | 1.7 | 5 | 2 | 40 | 9.29 | 14 | 5 | ND | 2 | 3 | 1 | 3 | 2 | 32 | .07 | .01 | 3 | 14 | .09 | 46 | .04 | 11 | .14 | .01 | .02 | 1 |
| N. END TRENCH | 85+32OR | 2 | 26 | 10 | 41 | .1 | 15 | 4 | 420 | 1.39 | 2 | 5 | ND | 1 | 8 | 1 | 2 | 2 | 5 | .05 | .03 | 5 | 4 | .08 | 197 | .01 | 9 | .21 | .01 | .06 | 1 |
| POWER LINE ADIT | PLA-5R | 5 | 61 | 20 | 139 | .7 | 18 | 12 | 505 | 4.84 | 65 | 5 | ND | 1 | 39 | 1 | 10 | 2 | 14 | 1.18 | .08 | 6 | 5 | .15 | 86 | .01 | 18 | .59 | .03 | .11 | 1 |
| | PLA-6R | 1 | 18 | 4 | 15 | .1 | 37 | 9 | 810 | 2.47 | 170 | 6 | ND | 4 | 321 | 1 | 2 | 2 | 12 | 8.07 | .01 | 3 | 34 | 3.14 | 8 | .01 | 30 | .11 | .02 | .02 | 1 |
| | PLA-7R | 1 | 47 | 10 | 79 | .1 | 65 | 24 | 955 | 5.70 | 277 | 5 | ND | 2 | 121 | 1 | 2 | 2 | 120 | 4.37 | .05 | 7 | 58 | 2.51 | 19 | .01 | 21 | 2.07 | .03 | .05 | 1 |

TABLE 2

GOLD EXPLORATION ROCKS

TABLE 3

AMAZON PETROLEUM FILE # 85-0961 

| SAMPLE# | Ag PPM | As PPM | Sb PPM | Au* PPB |
|---|---|---|---|---|
| 76+13R | .1 | 76 | 3 | 45 |
| 76+14R | .5 | 39 | 5 | 27 |
| 76+15R | .4 | 276 | 8 | 13 |
| 76+16R | .3 | 498 | 11 | 155 |
| 76+17R | 2.1 | 1993 | 32 | 340 |
| 76+18R | .8 | 1329 | 14 | 4830 |
| STD C/AU-0.5 | 6.9 | 39 | 15 | 500 |

- see Figure 15 for sample description

| | SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| NEAR STA. 25 | 25+5 | 1 | 53 | 5 | 135 | .2 | 37 | 9 | 429 | 3.73 | 6 | 5 | ND | 4 | 25 | 1 | 2 | 2 | 41 | .30 | .06 | 11 | 41 | .58 | 67 | .04 | 12 | 1.77 | .01 | .06 | 1 |
| | 25+20 | 1 | 55 | 2 | 138 | .1 | 42 | 10 | 476 | 3.92 | 12 | 5 | ND | 4 | 25 | 1 | 2 | 2 | 44 | .28 | .07 | 10 | 44 | .60 | 76 | .05 | 13 | 1.82 | .01 | .08 | 1 |
| | 25+30 | 1 | 55 | 6 | 140 | .1 | 42 | 9 | 350 | 3.73 | 10 | 5 | ND | 4 | 23 | 1 | 2 | 2 | 43 | .26 | .07 | 9 | 45 | .54 | 66 | .05 | 13 | 1.49 | .01 | .06 | 1 |
| NEAR STA. 26 | 26+5 | 1 | 43 | 5 | 129 | .1 | 37 | 7 | 360 | 3.32 | 12 | 5 | ND | 3 | 20 | 1 | 2 | 4 | 37 | .23 | .05 | 9 | 37 | .42 | 71 | .06 | 11 | 1.13 | .01 | .10 | 1 |
| | 26+20 | 1 | 45 | 4 | 83 | .1 | 56 | 8 | 284 | 3.08 | 7 | 5 | ND | 2 | 19 | 1 | 2 | 3 | 48 | .28 | .04 | 9 | 53 | .59 | 54 | .09 | 10 | 1.12 | .01 | .09 | 1 |
| | 26+40 | 1 | 40 | 9 | 116 | .1 | 49 | 8 | 662 | 2.88 | 19 | 8 | ND | 3 | 25 | 1 | 4 | 2 | 42 | .34 | .09 | 10 | 46 | .47 | 90 | .08 | 13 | 1.09 | .01 | .12 | 1 |
| | 26+60 | 1 | 75 | 7 | 146 | .1 | 66 | 10 | 591 | 4.94 | 94 | 5 | ND | 4 | 31 | 1 | 8 | 2 | 35 | .37 | .09 | 11 | 27 | .33 | 125 | .02 | 17 | .84 | .01 | .09 | 1 |
| FROM STA. 31 | 31+0+00 | 5 | 39 | 6 | 185 | .3 | 36 | 7 | 547 | 3.33 | 19 | 5 | ND | 3 | 26 | 1 | 2 | 2 | 52 | .20 | .07 | 9 | 26 | .34 | 146 | .04 | 10 | 1.12 | .01 | .07 | 1 |
| | 31+0+20 | 2 | 46 | 5 | 276 | .2 | 38 | 9 | 1022 | 3.58 | 6 | 5 | ND | 2 | 27 | 1 | 2 | 2 | 44 | .30 | .06 | 14 | 34 | .57 | 178 | 06 | 9 | 2.07 | .02 | .10 | 1 |
| | 31+0+40 | 5 | 69 | 16 | 390 | .3 | 60 | 21 | 1246 | 5.37 | 15 | 5 | ND | 4 | 33 | 1 | 2 | 4 | 71 | .33 | .19 | 8 | 34 | .60 | 186 | .11 | 8 | 2.42 | .01 | .08 | 1 |
| | 31+0+60 | 4 | 57 | 7 | 223 | .3 | 69 | 14 | 954 | 3.88 | 6 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 51 | .30 | .07 | 12 | 49 | .75 | 146 | .06 | 9 | 2.25 | .01 | .06 | 1 |
| | 31+0+80 | 4 | 50 | 8 | 267 | .7 | 44 | 10 | 599 | 3.52 | 8 | 5 | ND | 3 | 24 | 1 | 2 | 2 | 44 | .22 | .06 | 10 | 33 | .55 | 98 | .03 | 8 | 1.99 | .02 | .05 | 1 |
| | 31+1+00 | 7 | 66 | 13 | 216 | 1.1 | 26 | 21 | 2142 | 5.22 | 12 | 7 | ND | 1 | 55 | 1 | 2 | 2 | 40 | 4.43 | .07 | 9 | 10 | .62 | 78 | .01 | 8 | 1.88 | .02 | .03 | 1 |
| | 31+1+20 | 4 | 59 | 11 | 264 | .2 | 48 | 11 | 884 | 3.66 | 9 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 44 | .38 | .07 | 10 | 36 | .54 | 157 | .07 | 10 | 2.00 | .02 | .11 | 1 |
| | 31+1+40 | 1 | 65 | 6 | 130 | .4 | 26 | 15 | 507 | 4.29 | 14 | 5 | ND | 2 | 25 | 1 | 3 | 2 | 47 | .42 | .04 | 9 | 26 | .65 | 108 | .05 | 10 | 2.24 | .02 | .09 | 1 |
| FROM STA. 32 | 32+0+00 | 2 | 58 | 7 | 179 | .1 | 76 | 17 | 1382 | 3.06 | 17 | 5 | ND | 5 | 25 | 1 | 3 | 2 | 50 | .35 | .12 | 11 | 53 | .76 | 146 | .10 | 9 | 2.16 | .01 | .09 | 1 |
| | 32+0+20 | 1 | 44 | 13 | 567 | .6 | 69 | 13 | 1107 | 2.86 | 4 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 41 | .43 | .03 | 11 | 49 | .66 | 87 | .12 | 16 | 1.71 | .02 | .08 | 1 |
| | 32+0+40 | 2 | 70 | 10 | 165 | .7 | 67 | 13 | 1415 | 4.50 | 13 | 5 | ND | 1 | 28 | 1 | 2 | 3 | 49 | .36 | .10 | 16 | 65 | .89 | 87 | .08 | 8 | 2.53 | .01 | .09 | 1 |
| | 32+0+60 | 2 | 37 | 8 | 172 | .2 | 61 | 10 | 1161 | 3.17 | 12 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 39 | .40 | .07 | 12 | 46 | .53 | 138 | .07 | 13 | 1.60 | .01 | .09 | 1 |
| | 32+0+80 | 3 | 51 | 15 | 186 | .1 | 66 | 13 | 817 | 4.78 | 19 | 5 | ND | 4 | 23 | 1 | 2 | 2 | 56 | .28 | .09 | 11 | 53 | .69 | 107 | .10 | 9 | 1.87 | .01 | .09 | 1 |
| | 32+1+00 | 1 | 46 | 9 | 131 | .7 | 41 | 9 | 404 | 4.63 | 15 | 5 | ND | 3 | 27 | 1 | 2 | 2 | 40 | .39 | .08 | 10 | 37 | .40 | 102 | .06 | 11 | 1.15 | .01 | .11 | 1 |
| | 32+1+20 | 1 | 33 | 9 | 119 | .2 | 40 | 8 | 344 | 3.76 | 11 | 5 | ND | 2 | 18 | 1 | 2 | 2 | 39 | .25 | .09 | 7 | 41 | .45 | 79 | .06 | 11 | 1.12 | .01 | .07 | 1 |
| | 32+1+40 | 1 | 44 | 6 | 100 | .1 | 55 | 9 | 354 | 3.93 | 31 | 5 | ND | 3 | 25 | 1 | 2 | 2 | 43 | .29 | .05 | 8 | 46 | .67 | 126 | .04 | 9 | 1.58 | .01 | .08 | 1 |
| | 32+1+60 | 1 | 35 | 5 | 89 | .3 | 56 | 9 | 303 | 3.45 | 59 | 5 | ND | 2 | 24 | 1 | 2 | 2 | 51 | .29 | .05 | 6 | 49 | .71 | 118 | .09 | 8 | 1.52 | .01 | .07 | 1 |
| FROM STA. 44 | 44+0+00 | 1 | 26 | 2 | 63 | .1 | 68 | 8 | 269 | 2.56 | 7 | 5 | ND | 3 | 15 | 1 | 2 | 2 | 45 | .31 | .04 | 6 | 71 | .74 | 92 | .14 | 7 | 1.12 | .02 | .07 | 1 |
| | 44+0+20 | 1 | 27 | 6 | 63 | .1 | 73 | 8 | 278 | 2.61 | 7 | 5 | ND | 3 | 14 | 1 | 2 | 2 | 45 | .31 | .04 | 5 | 74 | .76 | 87 | .14 | 9 | 1.14 | .01 | .09 | 1 |
| | 44+0+40 | 1 | 32 | 9 | 112 | .2 | 62 | 9 | 382 | 3.17 | 10 | 5 | ND | 3 | 35 | 1 | 2 | 2 | 42 | .46 | .40 | 7 | 34 | .51 | 274 | .08 | 11 | 1.71 | .01 | .08 | 1 |
| | 44+0+60 | 1 | 36 | 10 | 140 | .2 | 60 | 11 | 476 | 2.94 | 5 | 5 | ND | 2 | 27 | 1 | 2 | 2 | 37 | .49 | .03 | 11 | 77 | .74 | 141 | .14 | 11 | 1.76 | .02 | .08 | 1 |
| | 44+0+80 | 1 | 22 | 5 | 103 | .1 | 62 | 9 | 368 | 2.49 | 8 | 5 | ND | 2 | 15 | 1 | 2 | 2 | 43 | .29 | .03 | 7 | 61 | .73 | 104 | .16 | 9 | 1.27 | .01 | .09 | 1 |
| | 44+1+00 | 1 | 31 | 8 | 181 | .4 | 79 | 12 | 595 | 3.07 | 9 | 5 | ND | 2 | 15 | 1 | 2 | 2 | 50 | .25 | .06 | 7 | 65 | .80 | 114 | .15 | 9 | 1.68 | .01 | .09 | 1 |
| STA. 59 | 59+0+00 | 2 | 132 | 15 | 277 | .2 | 215 | 28 | 2213 | 6.93 | 22 | 5 | ND | 8 | 98 | 1 | 2 | 2 | 132 | .63 | .16 | 26 | 163 | 2.04 | 144 | .11 | 9 | 2.79 | .01 | .13 | 1 |
| | 59+0+20 | 6 | 72 | 7 | 121 | .3 | 138 | 15 | 485 | 5.05 | 28 | 5 | ND | 4 | 34 | 1 | 10 | 2 | 63 | .28 | .08 | 14 | 118 | 1.00 | 120 | .09 | 10 | 1.44 | .01 | .10 | 1 |
| | 59+0+40 | 4 | 91 | 6 | 102 | .4 | 161 | 20 | 693 | 6.56 | 35 | 5 | ND | 4 | 39 | 1 | 8 | 2 | 89 | .43 | .10 | 18 | 165 | 1.66 | 237 | .09 | 12 | 1.91 | .01 | .10 | 1 |
| | 59+0+60 | 4 | 89 | 11 | 100 | .3 | 115 | 19 | 932 | 5.50 | 25 | 5 | ND | 5 | 37 | 1 | 4 | 2 | 88 | .48 | .07 | 18 | 131 | 1.59 | 158 | .13 | 10 | 1.99 | .01 | .11 | 1 |
| STA. 61 | 61+0+00 | 2 | 72 | 17 | 134 | .2 | 74 | 10 | 362 | 3.50 | 22 | 5 | ND | 6 | 52 | 1 | 7 | 2 | 32 | .33 | .15 | 21 | 43 | .34 | 154 | .04 | 12 | .87 | .01 | .13 | 1 |
| | 61+0+20 | 2 | 66 | 13 | 302 | .4 | 82 | 14 | 950 | 3.19 | 15 | 5 | ND | 5 | 72 | 1 | 2 | 2 | 47 | .54 | .15 | 15 | 68 | .76 | 327 | .13 | 12 | 1.68 | .02 | .14 | 1 |
| | 61+0+40 | 1 | 35 | 12 | 270 | .1 | 96 | 9 | 860 | 4.70 | 23 | 19 | ND | 25 | 39 | 1 | 2 | 2 | 49 | .50 | .09 | 188 | 102 | 1.14 | 150 | .07 | 17 | 2.13 | .01 | .14 | 1 |
| | 61+0+60 | 3 | 69 | 10 | 171 | .4 | 139 | 15 | 551 | 4.22 | 16 | 5 | ND | 6 | 34 | 1 | 3 | 2 | 56 | .39 | .06 | 26 | 137 | 1.20 | 225 | .10 | 11 | 1.98 | .01 | .14 | 1 |
| HIGHWAY NEW DISCOVERY | MD-1-L | 1 | 38 | 4 | 55 | .1 | 138 | 17 | 628 | 3.06 | 17 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 44 | 1.01 | .11 | 6 | 138 | 2.31 | 68 | .13 | 15 | 1.23 | .01 | .07 | 1 |
| | MD-2-L | 1 | 44 | 5 | 59 | .2 | 128 | 17 | 674 | 3.08 | 12 | 5 | ND | 3 | 30 | 1 | 4 | 2 | 47 | .84 | .12 | 7 | 125 | 2.06 | 82 | .14 | 21 | 1.33 | .02 | .12 | 1 |
| | MD-3-L | 1 | 43 | 9 | 57 | .1 | 119 | 16 | 642 | 3.03 | 5 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 48 | .77 | .13 | 6 | 117 | 1.90 | 81 | .14 | 17 | 1.29 | .01 | .12 | 1 |
| | MD-4-L | 1 | 42 | 2 | 57 | .4 | 152 | 17 | 625 | 3.01 | 2 | 5 | ND | 4 | 32 | 1 | 2 | 2 | 48 | .85 | .11 | 8 | 139 | 2.18 | 63 | .14 | 26 | 1.33 | .02 | .09 | 1 |
| NEAR STA. 51 | 51 0+00 | 1 | 33 | 7 | 138 | .3 | 100 | 11 | 795 | 3.13 | 5 | 9 | ND | 6 | 20 | 1 | 3 | 2 | 55 | .34 | .06 | 15 | 86 | .92 | 143 | .17 | 6 | 1.71 | .02 | .15 | 1 |
| | 51 0+20 | 1 | 36 | 7 | 106 | .2 | 93 | 11 | 825 | 2.97 | 5 | 5 | ND | 3 | 20 | 1 | 2 | 2 | 52 | .34 | .04 | 18 | 76 | .80 | 147 | .17 | 4 | 1.65 | .02 | .11 | 1 |
| | 51 0+40 | 1 | 31 | 5 | 60 | .3 | 91 | 8 | 323 | 2.90 | 5 | 8 | ND | 4 | 17 | 1 | 2 | 2 | 53 | .36 | .03 | 13 | 87 | .85 | 93 | .19 | 3 | 1.41 | .02 | .10 | 1 |
| | 51 0+60 | 1 | 45 | 9 | 188 | .3 | 94 | 11 | 760 | 3.01 | 5 | 5 | ND | 5 | 19 | 1 | 3 | 2 | 50 | .34 | .06 | 16 | 72 | .90 | 162 | .16 | 2 | 1.58 | .02 | .12 | 1 |
| | 51 0+80 | 1 | 37 | 3 | 71 | .2 | 82 | 9 | 369 | 3.29 | 9 | 12 | ND | 4 | 16 | 1 | 3 | 2 | 56 | .34 | .04 | 16 | 79 | .85 | 122 | .21 | 5 | 1.34 | .01 | .11 | 1 |
| | 51 1+00 | 1 | 34 | 6 | 83 | .2 | 90 | 9 | 496 | 2.87 | 2 | 8 | ND | 2 | 17 | 1 | 3 | 2 | 50 | .32 | .04 | 15 | 82 | .86 | 110 | .18 | 2 | 1.39 | .01 | .10 | 1 |
| | 51 1+20 | 1 | 42 | 9 | 79 | .1 | 103 | 10 | 367 | 3.03 | 12 | 15 | ND | 4 | 18 | 1 | 4 | 2 | 52 | .36 | .06 | 12 | 91 | .93 | 111 | .17 | 2 | 1.53 | .02 | .10 | 1 |

TABLE 4

TABLE 4

| | SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| STA. 56 | 56+120 | 3 | 43 | 8 | 97 | .1 | 160 | 13 | 338 | 3.56 | 11 | 5 | ND | 1 | 23 | 1 | 2 | 5 | 63 | .42 | .04 | 8 | 155 | 1.28 | 120 | .21 | 6 | 1.51 | .01 | .11 | 1 |
| | 56+160 | 1 | 24 | 2 | 116 | .1 | 151 | 12 | 406 | 2.93 | 2 | 5 | ND | 1 | 25 | 1 | 2 | 5 | 49 | .40 | .04 | 9 | 106 | .88 | 119 | .20 | 7 | 1.46 | .01 | .13 | 1 |
| | 58+20 | 1 | 27 | 2 | 99 | .1 | 132 | 12 | 415 | 3.03 | 11 | 5 | ND | 1 | 25 | 1 | 2 | 6 | 51 | .41 | .04 | 11 | 102 | .92 | 108 | .22 | 5 | 1.42 | .01 | .13 | 1 |
| | 58+40 | 1 | 21 | 6 | 91 | .1 | 91 | 9 | 532 | 2.02 | 9 | 5 | ND | 1 | 47 | 1 | 2 | 3 | 40 | .47 | .24 | 8 | 75 | .64 | 186 | .10 | 4 | .88 | .03 | .06 | 1 |
| STA. 58 | 58+60 | 6 | 35 | 8 | 127 | .1 | 105 | 11 | 790 | 2.51 | 12 | 5 | ND | 1 | 47 | 1 | 2 | 2 | 37 | .40 | .19 | 12 | 73 | .55 | 245 | .07 | 5 | .89 | .03 | .09 | 1 |
| | 58+80 | 6 | 70 | 12 | 117 | .1 | 348 | 23 | 737 | 5.49 | 76 | 5 | ND | 1 | 48 | 1 | 10 | 3 | 80 | .41 | .08 | 14 | 272 | 1.70 | 88 | .07 | 7 | 1.73 | .01 | .08 | 1 |
| | 58+100 | 4 | 76 | 13 | 124 | .1 | 123 | 16 | 1032 | 5.10 | 51 | 5 | ND | 1 | 56 | 1 | 4 | 2 | 61 | .41 | .11 | 13 | 78 | .70 | 144 | .08 | 9 | 1.22 | .01 | .10 | 1 |
| | 60+20 | 2 | 47 | 5 | 130 | .1 | 92 | 18 | 903 | 4.58 | 7 | 5 | ND | 1 | 34 | 1 | 2 | 3 | 80 | .52 | .12 | 14 | 98 | 1.93 | 239 | .23 | 5 | 2.42 | .02 | .10 | 1 |
| STA. 60 | 60+40 | 2 | 53 | 9 | 320 | .1 | 111 | 14 | 1184 | 4.49 | 22 | 5 | ND | 1 | 35 | 1 | 2 | 2 | 55 | .37 | .14 | 22 | 89 | 1.08 | 299 | .12 | 7 | 1.78 | .01 | .14 | 1 |
| | 62+0 | 2 | 77 | 4 | 126 | .2 | 101 | 10 | 356 | 2.83 | 6 | 5 | ND | 2 | 23 | 1 | 2 | 4 | 53 | .29 | .06 | 7 | 82 | .82 | 264 | .12 | 4 | 1.31 | .01 | .08 | 1 |
| STA. 62 | 62+12 | 1 | 33 | 14 | 160 | .2 | 223 | 18 | 814 | 4.54 | 9 | 5 | ND | 1 | 46 | 1 | 2 | 4 | 60 | .59 | .09 | 14 | 224 | 1.89 | 149 | .21 | 12 | 2.35 | .01 | .20 | 1 |
| | 62+24 | 1 | 28 | 10 | 168 | .1 | 198 | 17 | 735 | 3.93 | 7 | 5 | ND | 1 | 44 | 1 | 2 | 2 | 55 | .52 | .12 | 14 | 198 | 1.60 | 159 | .19 | 13 | 2.05 | .02 | .19 | 1 |
| | 120+20 | 1 | 7 | 4 | 55 | .1 | 13 | 3 | 221 | 1.13 | 2 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 26 | .17 | .19 | 2 | 8 | .19 | 98 | .08 | 5 | .59 | .03 | .04 | 1 |
| | 120+40 | 1 | 21 | 2 | 72 | .1 | 55 | 6 | 332 | 1.90 | 5 | 5 | ND | 1 | 25 | 1 | 2 | 2 | 40 | .29 | .13 | 5 | 42 | .58 | 96 | .10 | 6 | 1.11 | .02 | .07 | 1 |
| | 120+60 | 1 | 8 | 8 | 76 | .1 | 16 | 3 | 228 | 1.18 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 28 | .21 | .17 | 3 | 10 | .21 | 72 | .08 | 3 | .61 | .03 | .04 | 1 |
| STA. 120 | 120+80 | 1 | 15 | 7 | 80 | .1 | 38 | 6 | 319 | 1.75 | 3 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 39 | .25 | .16 | 5 | 41 | .47 | 94 | .10 | 3 | .94 | .02 | .05 | 1 |
| | 120+100 | 1 | 36 | 2 | 90 | .2 | 98 | 10 | 317 | 2.61 | 4 | 5 | ND | 2 | 19 | 1 | 2 | 2 | 50 | .29 | .05 | 5 | 74 | .85 | 96 | .13 | 5 | 1.54 | .02 | .10 | 1 |
| | 120+120 | 2 | 48 | 6 | 108 | .3 | 133 | 15 | 715 | 3.29 | 11 | 5 | ND | 2 | 23 | 1 | 2 | 2 | 61 | .31 | .08 | 8 | 101 | 1.26 | 123 | .14 | 4 | 2.31 | .02 | .10 | 1 |
| | 123+60 | 1 | 5 | 2 | 62 | .1 | 16 | 3 | 170 | 1.16 | 2 | 5 | ND | 1 | 25 | 1 | 2 | 2 | 27 | .21 | .23 | 4 | 6 | .19 | 78 | .08 | 6 | .62 | .03 | .04 | 1 |
| | 123+80 | 1 | 51 | 2 | 117 | .2 | 169 | 14 | 698 | 3.40 | 10 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 52 | .41 | .15 | 8 | 135 | 1.34 | 170 | .14 | 4 | 1.92 | .01 | .10 | 1 |
| | 123+100 | 1 | 33 | 4 | 52 | .1 | 177 | 15 | 393 | 3.21 | 7 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 52 | .54 | .03 | 6 | 219 | 1.74 | 78 | .17 | 10 | 1.78 | .02 | .06 | 1 |
| | 123+120 | 1 | 37 | 2 | 45 | .3 | 116 | 11 | 298 | 3.06 | 4 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 54 | .40 | .03 | 5 | 107 | 1.09 | 57 | .17 | 2 | 1.24 | .01 | .09 | 1 |
| | 123+140 | 1 | 32 | 6 | 40 | .1 | 87 | 9 | 247 | 2.78 | 2 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 55 | .33 | .02 | 6 | 83 | .83 | 65 | .16 | 3 | 1.14 | .02 | .10 | 1 |
| STA. 123 | 123+160 | 1 | 31 | 9 | 100 | .2 | 154 | 14 | 457 | 3.11 | 8 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 56 | .33 | .10 | 4 | 99 | 1.00 | 117 | .15 | 6 | 1.58 | .02 | .09 | 1 |
| | 123+180 | 1 | 52 | 2 | 102 | .1 | 171 | 19 | 715 | 3.74 | 5 | 5 | ND | 1 | 26 | 1 | 2 | 2 | 56 | .44 | .05 | 13 | 133 | 1.34 | 138 | .17 | 7 | 1.93 | .02 | .13 | 1 |
| | 123+200 | 1 | 30 | 8 | 89 | .2 | 123 | 12 | 424 | 3.23 | 6 | 5 | ND | 2 | 20 | 1 | 2 | 2 | 58 | .35 | .05 | 8 | 96 | .90 | 104 | .16 | 3 | 1.64 | .01 | .12 | 1 |
| | 123+220 | 1 | 30 | 7 | 105 | .2 | 93 | 10 | 465 | 2.70 | 6 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 50 | .39 | .04 | 9 | 76 | .75 | 105 | .16 | 11 | 1.51 | .02 | .14 | 1 |
| | 123+240 | 1 | 19 | 10 | 99 | .2 | 100 | 10 | 362 | 2.55 | 2 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 49 | .31 | .03 | 6 | 68 | .72 | 81 | .16 | 5 | 1.51 | .02 | .12 | 1 |
| | 123+260 | 1 | 8 | 4 | 69 | .1 | 23 | 4 | 321 | 1.33 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 34 | .24 | .09 | 4 | 11 | .20 | 101 | .10 | 2 | .60 | .02 | .04 | 1 |
| STA. 166 | 166+20 | 1 | 36 | 10 | 57 | .1 | 115 | 14 | 386 | 2.96 | 8 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 58 | .37 | .03 | 6 | 110 | 1.23 | 82 | .13 | 6 | 2.03 | .02 | .08 | 1 |
| | 166+40 | 1 | 72 | 6 | 64 | .1 | 142 | 17 | 468 | 3.20 | 9 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 59 | .38 | .06 | 5 | 127 | 1.52 | 87 | .13 | 8 | 2.15 | .02 | .06 | 1 |
| OLD TRENCH | 4N 200W | 1 | 88 | 6 | 39 | .2 | 123 | 15 | 380 | 2.84 | 10 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 47 | .58 | .06 | 5 | 142 | 1.94 | 50 | .11 | 2 | 1.63 | .02 | .05 | 1 |
| OLD TRENCH | 5S 550W | 1 | 84 | 5 | 37 | .2 | 115 | 15 | 362 | 2.70 | 9 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 44 | .57 | .06 | 4 | 128 | 1.85 | 49 | .10 | 3 | 1.60 | .02 | .05 | 1 |
| N. END | 6S 320E | 5 | 154 | 20 | 144 | .2 | 52 | 9 | 490 | 3.26 | 15 | 5 | ND | 4 | 26 | 1 | 2 | 2 | 19 | .20 | .09 | 28 | 18 | .34 | 322 | .01 | 6 | .82 | .01 | .11 | 1 |
| TRENCH 117 | 117+1L | 2 | 84 | 7 | 96 | .1 | 82 | 17 | 371 | 3.05 | 5 | 5 | ND | 5 | 35 | 1 | 2 | 2 | 64 | .36 | .06 | 7 | 70 | 1.11 | 92 | .17 | 7 | 2.24 | .02 | .12 | 1 |
| | 117+2L | 2 | 187 | 12 | 69 | .1 | 63 | 12 | 488 | 3.37 | 6 | 5 | ND | 4 | 43 | 1 | 2 | 2 | 61 | .53 | .10 | 8 | 79 | 1.35 | 46 | .14 | 9 | 1.73 | .02 | .08 | 1 |
| | 117+3L | 4 | 179 | 11 | 78 | .1 | 63 | 15 | 604 | 4.49 | 8 | 5 | ND | 6 | 46 | 1 | 2 | 3 | 80 | .50 | .09 | 9 | 72 | 1.54 | 58 | .16 | 11 | 2.11 | .02 | .10 | 1 |
| TRENCH 59 | 59+1L | 8 | 79 | 12 | 126 | .1 | 648 | 52 | 1728 | 6.97 | 19 | 9 | ND | 6 | 131 | 1 | 2 | 2 | 79 | 3.51 | .13 | 12 | 569 | 5.16 | 98 | .04 | 33 | 2.56 | .01 | .13 | 1 |
| | 59+2L | 10 | 114 | 16 | 281 | .4 | 619 | 64 | 3182 | 7.60 | 46 | 7 | ND | 7 | 97 | 1 | 2 | 2 | 108 | 1.61 | .11 | 7 | 453 | 3.91 | 132 | .11 | 17 | 2.86 | .02 | .12 | 1 |
| TRENCH 61 | 61+1L | 1 | 62 | 8 | 68 | .1 | 132 | 17 | 581 | 3.77 | 8 | 5 | ND | 6 | 30 | 1 | 2 | 2 | 69 | .58 | .09 | 9 | 113 | 1.63 | 86 | .16 | 13 | 1.42 | .03 | .12 | 1 |
| | 158+30L | 1 | 119 | 8 | 61 | .1 | 151 | 18 | 467 | 3.42 | 9 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 61 | .46 | .06 | 3 | 138 | 1.74 | 84 | .13 | 2 | 2.19 | .02 | .07 | 1 |
| TRENCH 158 | 158+35L | 1 | 101 | 14 | 88 | .1 | 133 | 29 | 545 | 4.12 | 11 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 74 | .43 | .10 | 7 | 128 | 1.72 | 59 | .13 | 2 | 2.87 | .02 | .08 | 1 |
| | 158+40L | 1 | 84 | 6 | 52 | .1 | 126 | 15 | 446 | 3.28 | 2 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 60 | .48 | .06 | 5 | 123 | 1.57 | 72 | .12 | 6 | 1.91 | .03 | .07 | 1 |
| TRENCH 165 | 165+20L | 1 | 91 | 16 | 71 | .1 | 151 | 17 | 612 | 3.75 | 6 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 61 | .46 | .09 | 7 | 111 | 1.52 | 126 | .17 | 2 | 1.85 | .03 | .21 | 1 |
| | 165+30L | 1 | 65 | 11 | 71 | .1 | 135 | 17 | 625 | 3.51 | 4 | 7 | ND | 1 | 21 | 1 | 2 | 2 | 56 | .56 | .08 | 6 | 113 | 1.70 | 107 | .16 | 2 | 1.49 | .03 | .15 | 1 |
| HIGHWAY | HND-1L | 4 | 70 | 21 | 81 | .1 | 75 | 16 | 560 | 8.58 | 18 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 71 | .21 | .06 | 2 | 88 | .96 | 82 | .14 | 3 | 1.97 | .03 | .10 | 1 |
| | HND-2L | 6 | 56 | 16 | 60 | .3 | 45 | 11 | 262 | 11.84 | 10 | 5 | ND | 1 | 10 | 1 | 2 | 2 | 68 | .18 | .04 | 2 | 57 | .72 | 23 | .18 | 2 | 1.06 | .02 | .08 | 1 |
| NEW DISCOVERY | HND-3L | 6 | 37 | 14 | 41 | .1 | 31 | 7 | 200 | 9.65 | 6 | 5 | ND | 1 | 8 | 1 | 2 | 2 | 56 | .08 | .03 | 2 | 37 | .48 | 61 | .16 | 11 | .94 | .01 | .07 | 1 |

| | SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 103 | 1 | 124 | 13 | 110 | .2 | 97 | 25 | 1054 | 5.41 | 2 | 5 | ND | 3 | 28 | 1 | 2 | 2 | 116 | .52 | .12 | 8 | 121 | 1.71 | 85 | .22 | 5 | 2.45 | .02 | .08 | 1 |
| | 103+5 | 1 | 127 | 9 | 164 | .4 | 174 | 47 | 1833 | 7.22 | 8 | 5 | ND | 6 | 34 | 1 | 2 | 2 | 174 | .66 | .11 | 10 | 191 | 2.40 | 116 | .23 | 2 | 3.12 | .02 | .06 | 1 |
| ABOVE | 103+10 | 1 | 120 | 11 | 134 | .3 | 134 | 30 | 914 | 6.49 | 5 | 5 | ND | 4 | 27 | 1 | 2 | 2 | 134 | .44 | .06 | 3 | 150 | 2.03 | 72 | .25 | 2 | 2.66 | .02 | .05 | 1 |
| | 103+15 | 1 | 115 | 8 | 135 | .2 | 162 | 37 | 860 | 6.45 | 8 | 5 | ND | 3 | 35 | 1 | 2 | 2 | 94 | .52 | .06 | 4 | 112 | 1.91 | 50 | .25 | 2 | 2.79 | .01 | .07 | 1 |
| STATION | 103+20 | 1 | 65 | 4 | 94 | .1 | 209 | 25 | 766 | 4.86 | 7 | 5 | ND | 2 | 24 | 1 | 2 | 2 | 74 | .45 | .07 | 12 | 171 | 1.80 | 92 | .22 | 2 | 2.43 | .01 | .06 | 1 |
| 103 | 103+40 | 1 | 47 | 5 | 76 | .1 | 104 | 13 | 484 | 3.59 | 2 | 5 | ND | 4 | 18 | 1 | 2 | 2 | 60 | .32 | .05 | 13 | 94 | .92 | 103 | .18 | 2 | 1.63 | .01 | .07 | 1 |
| | 103+60 | 1 | 81 | 5 | 134 | .3 | 130 | 28 | 1028 | 5.58 | 11 | 5 | ND | 4 | 26 | 1 | 2 | 2 | 80 | .40 | .09 | 7 | 123 | 1.73 | 84 | .23 | 2 | 2.74 | .02 | .27 | 1 |
| | 103+70 | 1 | 107 | 6 | 187 | .1 | 187 | 40 | 1067 | 6.46 | 8 | 5 | ND | 4 | 26 | 1 | 2 | 2 | 85 | .35 | .09 | 5 | 132 | 1.64 | 135 | .20 | 2 | 2.87 | .01 | .29 | 1 |
| | 104 | 1 | 29 | 4 | 72 | .1 | 71 | 11 | 754 | 2.80 | 2 | 5 | ND | 5 | 24 | 1 | 2 | 2 | 49 | .34 | .11 | 7 | 66 | .82 | 128 | .15 | 2 | 1.78 | .01 | .06 | 1 |
| STA. 104 | 104+20 | 1 | 19 | 2 | 26 | .1 | 41 | 5 | 256 | 1.45 | 2 | 6 | ND | 3 | 8 | 1 | 2 | 2 | 21 | .13 | .03 | 5 | 42 | .38 | 47 | .07 | 2 | .60 | .01 | .04 | 1 |
| STA. 106 | 106+5 | 1 | 44 | 4 | 78 | .3 | 93 | 12 | 442 | 3.81 | 3 | 5 | ND | 4 | 21 | 1 | 2 | 2 | 57 | .36 | .06 | 17 | 85 | .77 | 115 | .17 | 2 | 1.61 | .01 | .10 | 1 |
| | 106+25 | 1 | 44 | 2 | 64 | .1 | 87 | 12 | 444 | 3.65 | 7 | 5 | ND | 3 | 19 | 1 | 2 | 2 | 60 | .38 | .07 | 13 | 78 | .91 | 99 | .23 | 2 | 1.39 | .01 | .10 | 1 |
| TRENCH | 6N 475W | 1 | 50 | 3 | 63 | .1 | 130 | 17 | 796 | 3.42 | 5 | 5 | ND | 4 | 18 | 1 | 3 | 2 | 47 | .51 | .12 | 11 | 101 | 1.42 | 97 | .16 | 4 | 1.20 | .02 | .08 | 1 |
| 6N 500 W. | 6N 490W | 2 | 116 | 6 | 118 | .2 | 194 | 27 | 1282 | 5.93 | 13 | 5 | ND | 7 | 29 | 1 | 2 | 2 | 92 | .72 | .10 | 12 | 208 | 2.42 | 216 | .41 | 2 | 2.82 | .01 | .20 | 1 |
| | 6N 300W | 1 | 46 | 3 | 57 | .1 | 124 | 17 | 739 | 3.26 | 3 | 5 | ND | 2 | 17 | 1 | 2 | 2 | 44 | .48 | .11 | 11 | 91 | 1.26 | 97 | .16 | 2 | 1.12 | .02 | .06 | 1 |
| | 98+10 | 3 | 106 | 14 | 208 | .2 | 175 | 36 | 1483 | 7.34 | 19 | 8 | ND | 8 | 50 | 1 | 2 | 2 | 121 | .44 | .11 | 30 | 193 | 2.33 | 184 | .16 | 11 | 3.11 | .02 | .15 | 1 |
| ABOVE | 98+20 | 1 | 68 | 10 | 98 | .3 | 125 | 18 | 647 | 4.88 | 14 | 5 | ND | 4 | 43 | 1 | 3 | 2 | 117 | .47 | .07 | 15 | 151 | 1.68 | 119 | .17 | 10 | 2.52 | .01 | .15 | 1 |
| STA. 98 | 98+40 | 1 | 50 | 8 | 108 | .3 | 87 | 13 | 524 | 4.18 | 12 | 5 | ND | 3 | 29 | 1 | 2 | 4 | 84 | .31 | .05 | 17 | 78 | .98 | 97 | .15 | 7 | 1.89 | .02 | .10 | 1 |
| | 98+60 | 1 | 43 | 10 | 170 | .5 | 95 | 14 | 1247 | 3.58 | 11 | 12 | ND | 6 | 24 | 1 | 4 | 2 | 64 | .32 | .13 | 18 | 78 | .79 | 111 | .14 | 9 | 2.12 | .02 | .11 | 1 |
| | 98+70 | 1 | 39 | 5 | 79 | .3 | 96 | 10 | 390 | 3.34 | 11 | 16 | ND | 6 | 21 | 1 | 4 | 2 | 61 | .28 | .05 | 16 | 87 | .97 | 105 | .17 | 2 | 1.68 | .01 | .11 | 1 |
| | 99 | 1 | 55 | 8 | 104 | .4 | 130 | 14 | 519 | 3.95 | 9 | 9 | ND | 5 | 23 | 1 | 3 | 2 | 61 | .46 | .04 | 18 | 136 | 1.32 | 149 | .21 | 15 | 1.71 | .02 | .13 | 1 |
| | 99+20 | 1 | 68 | 2 | 232 | .3 | 137 | 20 | 1408 | 4.34 | 8 | 5 | ND | 6 | 31 | 1 | 3 | 2 | 69 | .70 | .08 | 17 | 138 | 1.38 | 310 | .28 | 12 | 2.29 | .02 | .20 | 1 |
| ABOVE | 99+40 | 1 | 77 | 6 | 306 | .4 | 184 | 20 | 1837 | 4.36 | 8 | 9 | ND | 5 | 53 | 1 | 5 | 2 | 76 | .90 | .12 | 18 | 147 | 1.52 | 294 | .30 | 24 | 2.50 | .02 | .16 | 1 |
| | 99+60 | 1 | 79 | 6 | 131 | .2 | 181 | 21 | 1275 | 4.28 | 5 | 6 | ND | 4 | 41 | 1 | 2 | 2 | 74 | .99 | .06 | 16 | 232 | 1.64 | 300 | .26 | 14 | 2.39 | .03 | .14 | 1 |
| STA. 99 | 99+80 | 1 | 63 | 8 | 124 | .6 | 212 | 21 | 1000 | 4.75 | 10 | 13 | ND | 5 | 34 | 1 | 5 | 2 | 78 | 1.00 | .06 | 12 | 255 | 2.39 | 210 | .40 | 10 | 2.58 | .02 | .16 | 1 |
| | 99+100 | 1 | 45 | 6 | 99 | .2 | 102 | 12 | 481 | 3.96 | 6 | 10 | ND | 4 | 27 | 1 | 3 | 2 | 57 | .54 | .05 | 12 | 104 | 1.12 | 129 | .27 | 7 | 1.74 | .02 | .14 | 1 |
| | 99+120 | 1 | 71 | 8 | 126 | .2 | 174 | 18 | 637 | 4.58 | 10 | 5 | ND | 5 | 30 | 1 | 2 | 2 | 63 | .74 | .08 | 12 | 214 | 1.74 | 138 | .24 | 16 | 2.45 | .02 | .18 | 1 |
| | 100 | 1 | 49 | 8 | 91 | .2 | 134 | 12 | 481 | 3.62 | 10 | 9 | ND | 2 | 22 | 1 | 3 | 2 | 58 | .42 | .05 | 14 | 135 | 1.27 | 132 | .22 | 4 | 1.66 | .01 | .10 | 1 |
| ABOVE | 100+20 | 1 | 67 | 13 | 448 | .6 | 226 | 16 | 731 | 4.20 | 5 | 9 | ND | 7 | 35 | 1 | 3 | 2 | 64 | .45 | .06 | 16 | 121 | 1.20 | 230 | .20 | 12 | 2.28 | .02 | .14 | 1 |
| | 100+40 | 1 | 50 | 6 | 114 | .2 | 95 | 10 | 516 | 3.38 | 9 | 5 | ND | 3 | 21 | 1 | 4 | 2 | 61 | .27 | .09 | 14 | 57 | .82 | 169 | .16 | 6 | 1.69 | .02 | .10 | 1 |
| STA. 100 | 100+60 | 1 | 43 | 8 | 86 | .2 | 83 | 11 | 497 | 3.80 | 9 | 9 | ND | 5 | 24 | 1 | 2 | 2 | 65 | .37 | .05 | 18 | 75 | 1.01 | 136 | .22 | 6 | 1.58 | .02 | .14 | 1 |
| | 100+80 | 1 | 35 | 5 | 90 | .2 | 75 | 10 | 415 | 3.20 | 5 | 5 | ND | 4 | 22 | 1 | 2 | 2 | 54 | .31 | .04 | 14 | 69 | .90 | 138 | .23 | 9 | 1.39 | .02 | .10 | 1 |
| | 101 | 1 | 40 | 8 | 91 | .3 | 82 | 10 | 557 | 3.44 | 7 | 10 | ND | 6 | 31 | 1 | 3 | 2 | 58 | .43 | .07 | 14 | 80 | .86 | 133 | .20 | 6 | 1.55 | .02 | .13 | 1 |
| STA. 101 | 101+20 | 1 | 54 | 9 | 104 | .1 | 105 | 13 | 888 | 3.68 | 8 | 5 | ND | 4 | 22 | 1 | 2 | 2 | 59 | .28 | .11 | 13 | 86 | 1.01 | 140 | .16 | 2 | 2.23 | .01 | .11 | 1 |
| | 101+30 | 1 | 32 | 4 | 46 | .1 | 41 | 6 | 289 | 2.56 | 4 | 7 | ND | 3 | 26 | 1 | 3 | 2 | 52 | .29 | .03 | 10 | 44 | .60 | 106 | .15 | 5 | 1.10 | .02 | .07 | 1 |
| | 102+5 | 2 | 65 | 7 | 112 | .3 | 77 | 16 | 1034 | 4.93 | 12 | 7 | ND | 5 | 32 | 1 | 2 | 2 | 101 | .50 | .08 | 14 | 99 | 1.83 | 261 | .31 | 6 | 2.60 | .02 | .13 | 1 |
| | 102+10 | 2 | 89 | 10 | 118 | .3 | 99 | 18 | 1360 | 5.68 | 10 | 11 | ND | 3 | 28 | 1 | 3 | 2 | 113 | .51 | .10 | 18 | 139 | 2.45 | 258 | .34 | 9 | 3.08 | .02 | .16 | 1 |
| ABOVE | 102+15 | 1 | 85 | 12 | 121 | .3 | 120 | 23 | 1512 | 6.58 | 10 | 10 | ND | 7 | 38 | 1 | 2 | 2 | 148 | .74 | .11 | 14 | 184 | 3.39 | 246 | .42 | 4 | 4.05 | .02 | .14 | 1 |
| | 102+20 | 2 | 89 | 12 | 125 | .4 | 118 | 23 | 1629 | 5.89 | 13 | 9 | ND | 7 | 30 | 1 | 2 | 2 | 121 | .51 | .08 | 11 | 166 | 2.70 | 215 | .34 | 2 | 3.43 | .02 | .14 | 1 |
| STA. 102 | 102+25 | 2 | 439 | 17 | 139 | .2 | 119 | 34 | 1417 | 8.14 | 15 | 7 | ND | 6 | 31 | 1 | 3 | 2 | 143 | .40 | .15 | 13 | 134 | 3.08 | 379 | .36 | 6 | 4.25 | .01 | .32 | 1 |
| | 102+30 | 2 | 111 | 11 | 121 | .1 | 154 | 23 | 1523 | 5.94 | 7 | 5 | ND | 4 | 30 | 1 | 2 | 2 | 95 | .44 | .09 | 19 | 132 | 2.05 | 209 | .28 | 5 | 3.06 | .03 | .11 | 1 |
| | 102+35 | 2 | 87 | 7 | 112 | .3 | 134 | 20 | 822 | 5.44 | 7 | 7 | ND | 6 | 22 | 1 | 2 | 2 | 90 | .33 | .07 | 16 | 105 | 1.50 | 95 | .22 | 6 | 2.76 | .02 | .09 | 1 |

TABLE 4

MASSIVE SULFIDE SOILS

TABLE 4

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 117+00 | 1 | 55 | 5L | 33 | .2 | 94 | 11 | 362 | 2.37 | 11 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 44 | .58 | .07 | 5 | 91 | 1.40 | 47 | .11 | 4 | 1.31 | .03 | .04 | 1 |
| 117+40 | 2 | 56 | 9h | 149 | .2 | 79 | 17 | 820 | 3.40 | 14 | 5 | ND | 2 | 31 | 1 | 2 | 3 | 67 | .47 | .13 | 8 | 67 | 1.18 | 98 | .18 | 44 | 2.47 | .02 | .13 | 1 |
| 117+80 | 1 | 88 | 3L | 55 | .1 | 89 | 15 | 416 | 3.25 | 10 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 67 | .56 | .07 | 7 | 96 | 1.38 | 72 | .16 | 7 | 2.00 | .02 | .10 | 1 |
| 117+100 | 1 | 83L | 11h | 44 | .1 | 112 | 18 | 512 | 3.30 | 13 | 5 | ND | 1 | 26 | 1 | 2 | 2 | 65 | .63 | .07 | 4 | 119 | 1.85 | 50 | .12 | 2 | 1.88 | .02 | .05 | 1 |
| 117+120 | 1 | 120 | 7L | 49 | .3 | 103 | 20 | 517 | 3.59 | 18 | 5 | ND | 2 | 39 | 1 | 2 | 2 | 66 | 1.03 | .07 | 6 | 128 | 2.22 | 57 | .16 | 6 | 2.40 | .03 | .09 | 1 |
| 117+140 | 1 | 230 | 10h | 49 | .1 | 121 | 23 | 547 | 3.61 | 31 | 5 | ND | 2 | 45 | 1 | 2 | 2 | 61 | 1.04 | .07 | 4 | 129 | 2.34 | 61 | .15 | 9 | 2.29 | .04 | .08 | 1 |
| 117+160 | 1 | 85 | 7L | 43 | .1 | 109 | 17 | 507 | 3.00 | 36 | 5 | ND | 1 | 41 | 1 | 2 | 2 | 56 | .87 | .09 | 6 | 112 | 1.83 | 49 | .14 | 14 | 1.57 | .04 | .07 | 1 |
| 117+180 | 1 | 116 | 7h | 59 | .1 | 118 | 24 | 634 | 3.54 | 10 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 65 | .79 | .09 | 6 | 108 | 1.80 | 67 | .16 | 13 | 1.82 | .03 | .10 | 1 |
| 117+200 | 1 | 147 | 11L | 69 | .2 | 210 | 26 | 626 | 4.63 | 14 | 5 | ND | 2 | 54 | 1 | 2 | 3 | 89 | .77 | .08 | 8 | 199 | 2.23 | 119 | .21 | 4 | 3.27 | .02 | .25 | 1 |
| 117+220 | 1 | 115 | 6h | 62h | .1 | 149 | 22 | 614 | 4.02 | 13 | 5 | ND | 2 | 37 | 1 | 2 | 2 | 76 | .73 | .08 | 7 | 150 | 1.89 | 103 | .19 | 7 | 2.59 | .03 | .15 | 1 |
| 117+240 | 1 | 105 | 3L | 47 | .2 | 236 | 29 | 619 | 3.98 | 11 | 5 | ND | 2 | 39 | 1 | 2 | 2 | 69 | .86 | .07 | 7 | 245 | 3.03 | 71 | .16 | 10 | 2.60 | .03 | .06 | 1 |
| 117+260 | 1 | 123 | 4 | 40 | .1 | 128 | 24 | 508 | 3.89 | 11 | 5 | ND | 1 | 41 | 1 | 2 | 2 | 66 | .64 | .05 | 5 | 120 | 2.53 | 73 | .12 | 5 | 2.97 | .02 | .08 | 1 |
| 117+280 | 1 | 22 | 15h | 93 | .1 | 124 | 14 | 459 | 2.87 | 13 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 53 | .37 | .08 | 5 | 77 | .87 | 120 | .18 | 7 | 1.99 | .02 | .13 | 1 |
| 117+300 | 1 | 37 | 2 | 81 | .1 | 113 | 13 | 392 | 2.88 | 7 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 56 | .50 | .05 | 6 | 98 | 1.13 | 90 | .17 | 8 | 1.73 | .02 | .13 | 1 |
| 117+320 | 1 | 40 | 3L | 47 | .2 | 119 | 13 | 311 | 2.86 | 9 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 55 | .47 | .03 | 4 | 117 | 1.36 | 65 | .17 | 3 | 1.69 | .02 | .11 | 1 |
| 117+340 | 1 | 105 | 6h | 45 | .2 | 189 | 18 | 414 | 3.54 | 11 | 5 | ND | 2 | 21 | 1 | 2 | 2 | 56 | .56 | .05 | 7 | 194 | 2.17 | 60 | .15 | 6 | 2.17 | .01 | .08 | 1 |
| 117+360 | 1 | 46 | 6L | 79 | .2 | 131 | 15 | 505 | 3.53 | 3 | 6 | ND | 2 | 22 | 1 | 2 | 2 | 68 | .46 | .03 | 8 | 108 | 1.14 | 101 | .21 | 4 | 2.13 | .02 | .16 | 1 |
| 117+380 | 1 | 42 | 6h | 92 | .2 | 128 | 13 | 405 | 3.26 | 7 | 5 | ND | 2 | 22 | 1 | 2 | 3 | 62 | .43 | .06 | 9 | 107 | 1.14 | 104 | .19 | 8 | 2.02 | .02 | .16 | 1 |
| 117+400 | 1 | 50 | 2 | 96 | .1 | 155 | 17 | 537 | 3.50 | 11 | 5 | ND | 2 | 21 | 1 | 2 | 4 | 65 | .46 | .04 | 7 | 120 | 1.38 | 105 | .21 | 2 | 2.27 | .02 | .15 | 1 |
| 117+420 | 1 | 108 | 2 | 61 | .1 | 236 | 24 | 693 | 4.39 | 15 | 5 | ND | 2 | 23 | 1 | 2 | 2 | 63 | .63 | .07 | 10 | 221 | 2.65 | 94 | .20 | 11 | 2.25 | .02 | .09 | 1 |
| 117+440 | 1 | 72 | 5L | 59 | .2 | 180 | 17 | 443 | 3.94 | 9 | 5 | ND | 2 | 24 | 1 | 2 | 2 | 67 | .53 | .04 | 8 | 177 | 1.71 | 95 | .22 | 11 | 2.05 | .02 | .13 | 1 |
| 117+460 | 4 | 75 | 5h | 66 | .2 | 987 | 83 | 1003 | 5.20 | 16 | 5 | ND | 1 | 29 | 1 | 2 | 2 | 62 | .79 | .05 | 5 | 1767 | 9.15 | 38 | .20 | 14 | 3.39 | .01 | .02 | 1 |
| 117+480 | 1 | 71 | 8 | 53 | .1 | 188 | 18 | 479 | 3.48 | 10 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 57 | .56 | .07 | 10 | 199 | 2.13 | 67 | .19 | 3 | 1.74 | .02 | .11 | 1 |
| 129+00 | 2 | 33 | 11L | 99 | .2 | 79 | 13 | 439 | 3.41 | 7 | 5 | ND | 1 | 24 | 1 | 2 | 4 | 64 | .49 | .03 | 7 | 81 | .92 | 107 | .26 | 10 | 1.80 | .02 | .13 | 1 |
| 129+20 | 1 | 8 | 8 | 135 | .1 | 9 | 5 | 434 | 1.56 | 2 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 38 | .33 | .27 | 3 | 9 | .20 | 185 | .11 | 2 | .81 | .03 | .06 | 1 |
| 129+40 | 3 | 40 | 7h | 131 | .3 | 96 | 13 | 816 | 3.43 | 6 | 5 | ND | 2 | 26 | 1 | 2 | 5 | 62 | .44 | .06 | 10 | 93 | 1.01 | 158 | .22 | 6 | 1.87 | .02 | .13 | 1 |
| 129+80 | 9 | 99 | 19 | 163 | .3 | 180 | 26 | 1162 | 7.33 | 40 | 6 | ND | 4 | 33 | 1 | 4 | 2 | 99 | .33 | .09 | 25 | 147 | 1.14 | 82 | .07 | 4 | 1.80 | .01 | .13 | 1 |
| 129+100 | 8 | 108 | 20 | 253 | .2 | 128 | 24 | 1501 | 6.22 | 25 | 5 | ND | 3 | 32 | 1 | 2 | 2 | 107 | .35 | .14 | 27 | 111 | 1.20 | 184 | .08 | 8 | 2.43 | .01 | .15 | 1 |
| 129+120 | 2 | 117 | 17 | 169 | .1 | 83 | 17 | 3950 | 3.27 | 9 | 5 | ND | 1 | 48 | 1 | 2 | 2 | 47 | .68 | .19 | 21 | 31 | .48 | 207 | .11 | 7 | 1.42 | .02 | .13 | 1 |
| 129+140 | 5 | 137 | 16L | 225 | .2 | 84 | 17 | 3923 | 4.22 | 11 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 57 | .28 | .09 | 28 | 51 | .57 | 289 | .07 | 2 | 2.10 | .02 | .13 | 1 |
| 129+160 | 1 | 65 | 12h | 77 | .1 | 78 | 11 | 502 | 3.59 | 2 | 5 | ND | 1 | 28 | 1 | 2 | 3 | 61 | .32 | .05 | 12 | 69 | .78 | 128 | .15 | 2 | 1.74 | .02 | .10 | 1 |
| 129+180 | 2 | 209 | 14L | 198 | .1 | 82 | 21 | 4474 | 8.20 | 23 | 5 | ND | 1 | 32 | 1 | 2 | 2 | 139 | .38 | .15 | 16 | 77 | 1.03 | 133 | .07 | 2 | 1.70 | .01 | .14 | 1 |
| 129+200 | 1 | 118 | 11 | 94 | .1 | 102 | 14 | 1289 | 3.91 | 18 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 52 | .29 | .14 | 9 | 76 | .85 | 82 | .09 | 2 | 1.87 | .01 | .10 | 1 |
| 129+220 | 1 | 33 | 5 | 93 | .1 | 43 | 7 | 656 | 1.97 | 2 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 39 | .27 | .04 | 6 | 29 | .48 | 125 | .12 | 2 | 1.21 | .04 | .11 | 1 |
| 138+30 | 2 | 79 | 17 | 175 | .2 | 101 | 16 | 2349 | 3.64 | 13 | 5 | ND | 1 | 34 | 1 | 2 | 2 | 56 | .42 | .08 | 17 | 65 | .80 | 295 | .15 | 2 | 1.97 | .02 | .14 | 1 |
| 138+50 | 1 | 57 | 10 | 131 | .3 | 90 | 14 | 1518 | 3.44 | 11 | 5 | ND | 2 | 24 | 1 | 2 | 2 | 54 | .35 | .11 | 12 | 73 | .90 | 181 | .14 | 2 | 2.05 | .02 | .10 | 1 |
| 138+70 | 1 | 51 | 7L | 84 | .1 | 72 | 9 | 570 | 2.97 | 7 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 51 | .34 | .05 | 10 | 62 | .78 | 186 | .14 | 2 | 1.75 | .02 | .08 | 1 |
| 138+90 | 1 | 39 | 11h | 101 | .1 | 68 | 10 | 494 | 3.13 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 51 | .36 | .05 | 9 | 66 | .75 | 167 | .16 | 2 | 1.66 | .02 | .13 | 1 |
| 138+110 | 1 | 53 | 12L | 102 | .1 | 63 | 10 | 559 | 3.86 | 4 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 61 | .38 | .05 | 9 | 67 | .81 | 166 | .16 | 2 | 1.94 | .02 | .13 | 1 |
| 138+130 | 1 | 42 | 15h | 89 | .1 | 62 | 11 | 684 | 3.51 | 7 | 5 | ND | 1 | 26 | 1 | 2 | 2 | 62 | .39 | .09 | 8 | 64 | .92 | 160 | .16 | 3 | 2.12 | .01 | .11 | 1 |
| 138+150 | 1 | 138 | 20 | 107 | .1 | 90 | 26 | 2020 | 9.02 | 94 | 5 | ND | 1 | 23 | 1 | 6 | 2 | 88 | .31 | .15 | 15 | 67 | .89 | 123 | .05 | 7 | 1.68 | .01 | .13 | 1 |
| 142+15 | 1 | 71 | 18 | 111 | .1 | 222 | 21 | 926 | 4.26 | 6 | 7 | ND | 1 | 25 | 1 | 2 | 2 | 86 | .37 | .07 | 12 | 183 | 2.04 | 178 | .14 | 2 | 2.42 | .01 | .09 | 1 |
| 105L | 3 | 61 | 3L | 128 | .1 | 292 | 22 | 1304 | 7.47 | 514 | 5 | ND | 3 | 55 | 1 | 17 | 2 | 67 | .73 | .09 | 17 | 214 | 1.21 | 85 | .06 | 20 | 1.42 | .01 | .07 | 1 |

ABOVE STATION 117

FROM STA. 129

FROM STA. 138

ABOVE STA. 105

TABLE 5

MASSIVE SULFIDE ROCKS

| | SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| TRENCH 103 | 103R | 1 | 90 | 8 | 24 | .1 | 20 | 11 | 355 | 3.37 | 4 | 5 | ND | 3 | 6 | 1 | 2 | 4 | 31 | .21 | .02 | 2 | 20 | .45 | 4 | .01 | 3 | .49 | .04 | .01 | 1 |
| | 103+3R | 3 | 59 | 5 | 97 | .2 | 76 | 27 | 2419 | 6.93 | 5 | 5 | ND | 4 | 26 | 1 | 2 | 3 | 201 | 1.22 | .14 | 2 | 128 | 5.18 | 207 | .73 | 8 | 3.81 | .08 | .22 | 1 |
| | 103+6R | 1 | 28 | 3 | 72 | .1 | 10 | 13 | 1064 | 4.88 | 3 | 5 | ND | 3 | 20 | 1 | 2 | 5 | 139 | .68 | .10 | 2 | 33 | 2.12 | 51 | .15 | 5 | 2.07 | .08 | .05 | 1 |
| | 103+13R | 2 | 57 | 2 | 82 | .1 | 55 | 24 | 1873 | 6.71 | 4 | 5 | ND | 2 | 35 | 1 | 2 | 2 | 179 | 1.23 | .14 | 2 | 134 | 4.93 | 218 | .69 | 5 | 4.02 | .13 | .35 | 1 |
| | 103+15R | 1 | 45 | 5 | 80 | .1 | 59 | 22 | 1740 | 6.44 | 2 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 189 | 1.19 | .14 | 2 | 153 | 4.90 | 105 | .70 | 5 | 3.85 | .12 | .32 | 1 |
| | 103+20R | 2 | 62 | 5 | 82 | .1 | 75 | 22 | 1049 | 6.32 | 6 | 5 | ND | 3 | 35 | 1 | 2 | 3 | 199 | 1.17 | .14 | 2 | 156 | 4.49 | 130 | .67 | 4 | 3.87 | .13 | .27 | 1 |
| | 103+20RA | 1 | 47 | 3 | 93 | .1 | 153 | 25 | 1428 | 6.69 | 2 | 5 | ND | 4 | 15 | 1 | 2 | 2 | 150 | .90 | .12 | 2 | 290 | 4.93 | 30 | .54 | 3 | 3.52 | .06 | .03 | 1 |
| | 103+25R | 1 | 62 | 4 | 75 | .1 | 58 | 21 | 1215 | 5.65 | 2 | 5 | ND | 4 | 24 | 1 | 2 | 3 | 185 | .66 | .09 | 2 | 123 | 3.32 | 42 | .38 | 3 | 2.61 | .07 | .06 | 1 |
| | 103+30R | 1 | 40 | 5 | 81 | .2 | 80 | 12 | 1163 | 4.38 | 7 | 5 | ND | 4 | 6 | 1 | 2 | 3 | 99 | .38 | .08 | 2 | 123 | 2.44 | 12 | .26 | 5 | 2.12 | .04 | .06 | 1 |
| | 103+30RA | 2 | 69 | 4 | 87 | .3 | 52 | 19 | 1235 | 5.95 | 5 | 5 | ND | 2 | 22 | 1 | 2 | 4 | 184 | .96 | .12 | 2 | 92 | 2.92 | 23 | .23 | 3 | 2.48 | .04 | .04 | 1 |
| | 103+35R | 4 | 56 | 5 | 55 | .1 | 46 | 13 | 773 | 3.58 | 2 | 5 | ND | 3 | 9 | 1 | 2 | 3 | 95 | .46 | .07 | 3 | 62 | 1.41 | 11 | .08 | 3 | 1.28 | .04 | .04 | 1 |
| | 103+40R | 2 | 72 | 4 | 75 | .2 | 54 | 19 | 1194 | 5.74 | 6 | 5 | ND | 4 | 52 | 1 | 2 | 2 | 188 | .86 | .10 | 2 | 89 | 2.71 | 50 | .37 | 9 | 2.54 | .16 | .11 | 1 |
| | 103+41R | 4 | 61 | 4 | 103 | .1 | 178 | 25 | 1336 | 5.79 | 5 | 5 | ND | 4 | 38 | 1 | 2 | 2 | 155 | .90 | .15 | 2 | 250 | 3.85 | 59 | .56 | 6 | 3.36 | .08 | .23 | 1 |
| | 103+45R | 2 | 62 | 5 | 71 | .1 | 140 | 21 | 1114 | 4.90 | 6 | 9 | ND | 4 | 13 | 1 | 2 | 2 | 121 | .45 | .10 | 3 | 194 | 2.95 | 26 | .28 | 6 | 2.18 | .04 | .06 | 1 |
| | 103+48R | 1 | 35 | 6 | 95 | .1 | 304 | 25 | 1201 | 5.31 | 13 | 5 | 2 | 3 | 10 | 1 | 2 | 2 | 112 | .54 | .11 | 3 | 401 | 5.04 | 25 | .39 | 7 | 3.27 | .02 | .03 | 1 |
| | 103+50R | 1 | 56 | 2 | 80 | .1 | 356 | 29 | 931 | 4.55 | 15 | 5 | ND | 3 | 16 | 1 | 2 | 3 | 106 | .64 | .08 | 2 | 476 | 4.80 | 44 | .36 | 5 | 2.90 | .03 | .06 | 1 |
| | 121R | 4 | 32 | 3 | 80 | .7 | 8 | 3 | 331 | 2.62 | 2 | 5 | ND | 3 | 8 | 1 | 2 | 7 | 56 | .03 | .02 | 2 | 16 | .84 | 171 | .03 | 2 | 1.07 | .03 | .11 | 1 |
| TRENCH 117 | 117+1R | 1 | 2 | 5 | 221 | .1 | 35 | 11 | 2209 | 5.79 | 2 | 5 | ND | 3 | 6 | 1 | 4 | 3 | 190 | .21 | .03 | 2 | 78 | 6.91 | 9 | .13 | 3 | 5.43 | .01 | .02 | 1 |
| | 117+2R | 12 | 6 | 6 | 38 | .1 | 7 | 6 | 377 | 4.16 | 2 | 8 | ND | 4 | 22 | 1 | 3 | 3 | 54 | .28 | .02 | 2 | 21 | 1.18 | 19 | .08 | 5 | 1.29 | .01 | .06 | 1 |
| | 117+3R | 9 | 62 | 11 | 167 | .1 | 35 | 32 | 2158 | 8.07 | 2 | 5 | ND | 2 | 17 | 1 | 2 | 2 | 195 | .33 | .03 | 2 | 60 | 5.24 | 43 | .13 | 9 | 4.42 | .02 | .03 | 1 |
| | 117+4R | 3 | 31 | 7 | 159 | .1 | 31 | 15 | 2036 | 6.01 | 2 | 5 | ND | 2 | 12 | 1 | 5 | 2 | 173 | .40 | .03 | 2 | 62 | 5.33 | 26 | .12 | 4 | 4.38 | .01 | .02 | 1 |
| | 117+5R | 1 | 153 | 12 | 159 | .1 | 30 | 27 | 2315 | 8.16 | 2 | 5 | ND | 2 | 11 | 1 | 2 | 2 | 180 | .65 | .03 | 2 | 55 | 4.68 | 35 | .11 | 3 | 4.22 | .02 | .03 | 1 |
| TRENCH 118 | 118+6 | 1 | 56 | 5 | 81 | .1 | 86 | 12 | 551 | 3.26 | 12 | 5 | ND | 2 | 28 | 1 | 5 | 3 | 59 | .64 | .07 | 4 | 66 | 1.30 | 53 | .09 | 8 | 1.58 | .05 | .10 | 1 |
| | 118+7 | 1 | 142 | 2 | 142 | .1 | 71 | 30 | 1114 | 6.62 | 8 | 5 | ND | 3 | 20 | 1 | 3 | 2 | 133 | .43 | .06 | 2 | 69 | 2.39 | 36 | .13 | 6 | 2.35 | .04 | .06 | 1 |
| | 118+8 | 3 | 241 | 10 | 184 | .1 | 20 | 27 | 2337 | 9.14 | 2 | 5 | ND | 3 | 10 | 1 | 5 | 2 | 198 | .40 | .05 | 2 | 26 | 3.79 | 13 | .16 | 6 | 3.75 | .02 | .02 | 1 |
| | 118+9 | 2 | 282 | 9 | 180 | .1 | 26 | 25 | 2223 | 8.81 | 2 | 5 | ND | 3 | 6 | 1 | 3 | 2 | 196 | .33 | .05 | 2 | 29 | 4.06 | 7 | .15 | 4 | 3.82 | .03 | .01 | 1 |
| | 118+10 | 3 | 158 | 5 | 144 | .1 | 93 | 26 | 1428 | 9.42 | 2 | 5 | ND | 4 | 8 | 1 | 7 | 2 | 155 | .23 | .04 | 2 | 109 | 3.66 | 23 | .19 | 4 | 3.41 | .02 | .06 | 1 |
| | 118+11 | 6 | 372 | 9 | 176 | .1 | 36 | 31 | 1653 | 10.32 | 2 | 5 | ND | 3 | 13 | 1 | 3 | 2 | 172 | .23 | .04 | 2 | 42 | 3.94 | 27 | .18 | 9 | 3.81 | .01 | .05 | 1 |
| | 118+12 | 3 | 380 | 11 | 160 | .1 | 53 | 37 | 1364 | 8.15 | 3 | 9 | ND | 4 | 23 | 1 | 7 | 2 | 108 | .44 | .06 | 2 | 63 | 2.40 | 48 | .13 | 13 | 2.56 | .02 | .08 | 1 |
| | 118+13 | 1 | 211 | 4 | 116 | .1 | 69 | 19 | 770 | 4.06 | 2 | 5 | ND | 4 | 36 | 1 | 2 | 2 | 61 | 1.18 | .06 | 3 | 99 | 1.87 | 36 | .12 | 14 | 2.38 | .05 | .08 | 1 |
| | 118+14 | 2 | 144 | 8 | 93 | .1 | 89 | 17 | 670 | 4.60 | 6 | 5 | ND | 4 | 32 | 1 | 5 | 2 | 65 | .89 | .07 | 2 | 95 | 1.72 | 34 | .13 | 12 | 2.00 | .04 | .07 | 1 |
| | 118+15 | 1 | 70 | 6 | 196 | .1 | 91 | 17 | 836 | 4.05 | 2 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 79 | .87 | .06 | 2 | 67 | 1.41 | 29 | .08 | 13 | 1.70 | .04 | .07 | 1 |
| | 118+16 | 2 | 107 | 2 | 156 | .1 | 96 | 18 | 839 | 3.75 | 15 | 5 | ND | 1 | 38 | 1 | 5 | 2 | 68 | 1.51 | .08 | 4 | 105 | 2.05 | 23 | .13 | 16 | 2.25 | .03 | .05 | 1 |
| | 118+17 | 2 | 170 | 10 | 87 | .1 | 211 | 23 | 902 | 8.08 | 2 | 9 | ND | 2 | 33 | 1 | 2 | 2 | 72 | .38 | .03 | 2 | 182 | 3.69 | 24 | .12 | 17 | 2.40 | .01 | .07 | 1 |
| | 118+18 | 5 | 224 | 8 | 207 | .1 | 168 | 31 | 1429 | 6.38 | 6 | 5 | ND | 1 | 17 | 1 | 4 | 2 | 86 | .37 | .04 | 3 | 105 | 2.86 | 29 | .09 | 22 | 2.50 | .02 | .06 | 1 |
| | 118+19 | 2 | 82 | 8 | 158 | .1 | 86 | 20 | 855 | 6.02 | 2 | 5 | ND | 2 | 15 | 1 | 5 | 2 | 71 | .81 | .04 | 2 | 69 | 2.19 | 26 | .09 | 13 | 2.60 | .02 | .04 | 1 |
| | 118+20 | 3 | 85 | 8 | 131 | .2 | 88 | 16 | 586 | 5.78 | 4 | 8 | ND | 3 | 13 | 1 | 3 | 2 | 50 | .42 | .03 | 2 | 139 | 1.31 | 33 | .07 | 9 | 1.41 | .03 | .06 | 1 |
| | 118+21 | 2 | 48 | 7 | 64 | .1 | 48 | 9 | 265 | 5.20 | 2 | 5 | ND | 1 | 15 | 1 | 4 | 2 | 58 | .33 | .02 | 2 | 67 | .64 | 35 | .11 | 13 | 1.00 | .05 | .08 | 1 |
| | 118+22 | 11 | 82 | 12 | 82 | .1 | 37 | 5 | 206 | 14.14 | 27 | 5 | ND | 4 | 35 | 1 | 5 | 2 | 85 | .12 | .02 | 2 | 27 | .45 | 70 | .15 | 30 | .89 | .06 | .13 | 1 |

TABLE 5

MASSIVE SULFIDE ROCKS

AMAZON PETROLEUM

HIGHWAY NEW DISCOVERY

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| HND-1R | 1 | 60 | 7 | 126 | .2 | 17 | 21 | 760 | 23.06 | 2 | 5 | ND | 2 | 7 | 1 | 2 | 2 | 126 | .08 | .06 | 2 | 77 | 1.32 | 30 | .15 | 13 | 2.53 | .01 | .05 | 1 |
| HND-2R | 3 | 42 | 15 | 102 | .1 | 16 | 13 | 844 | 14.55 | 10 | 5 | ND | 1 | 11 | 1 | 3 | 2 | 139 | .11 | .04 | 2 | 47 | 2.34 | 20 | .20 | 2 | 2.57 | .02 | .07 | 1 |
| HND-3R | 4 | 57 | 16 | 105 | .4 | 11 | 14 | 419 | 19.70 | 11 | 5 | ND | 2 | 9 | 1 | 10 | 2 | 162 | .03 | .04 | 2 | 40 | 1.22 | 26 | .15 | 6 | 1.92 | .01 | .11 | 1 |
| HND-4R | 1 | 33 | 15 | 128 | .1 | 14 | 18 | 1320 | 11.82 | 6 | 5 | ND | 1 | 5 | 1 | 2 | 2 | 156 | .02 | .02 | 2 | 37 | 3.43 | 28 | .27 | 2 | 3.43 | .01 | .09 | 1 |
| HND-5R | 1 | 38 | 14 | 27 | .2 | 2 | 5 | 69 | 11.36 | 8 | 5 | ND | 1 | 4 | 2 | 5 | 2 | 79 | .02 | .02 | 3 | 12 | .10 | 113 | .12 | 10 | .31 | .01 | .08 | 1 |
| HND-6R | 4 | 39 | 12 | 41 | .4 | 7 | 8 | 114 | 12.38 | 7 | 5 | ND | 1 | 8 | 1 | 3 | 2 | 96 | .05 | .03 | 2 | 15 | .17 | 38 | .24 | 7 | .68 | .01 | .09 | 1 |
| HND-7R | 2 | 16 | 6 | 30 | .2 | 8 | 8 | 269 | 8.84 | 2 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 94 | .04 | .02 | 2 | 20 | .86 | 72 | .24 | 13 | 1.02 | .02 | .17 | 1 |
| HND-8R | 1 | 18 | 13 | 31 | .1 | 8 | 9 | 254 | 13.98 | 8 | 5 | ND | 1 | 7 | 1 | 5 | 2 | 144 | .02 | .03 | 2 | 18 | .65 | 64 | .23 | 9 | .81 | .02 | .19 | 1 |
| HND-9R | 1 | 17 | 5 | 14 | .1 | 4 | 5 | 56 | 7.93 | 5 | 5 | ND | 1 | 2 | 1 | 3 | 2 | 47 | .03 | .02 | 2 | 9 | .07 | 25 | .30 | 7 | .24 | .01 | .08 | 1 |
| HND-10R | 5 | 38 | 8 | 70 | .2 | 9 | 7 | 591 | 7.33 | 9 | 5 | ND | 1 | 3 | 1 | 2 | 7 | 90 | .02 | .01 | 2 | 27 | 1.97 | 66 | .26 | 14 | 1.96 | .01 | .11 | 1 |
| HND-11R | 2 | 19 | 10 | 67 | .1 | 20 | 19 | 588 | 10.55 | 3 | 5 | ND | 1 | 5 | 1 | 2 | 3 | 102 | .02 | .02 | 2 | 32 | 2.01 | 9 | .27 | 3 | 2.12 | .01 | .08 | 1 |
| HND-12R | 5 | 35 | 20 | 109 | .2 | 12 | 12 | 785 | 15.46 | 36 | 5 | ND | 2 | 12 | 1 | 2 | 2 | 161 | .03 | .03 | 2 | 44 | 2.86 | 32 | .18 | 2 | 2.89 | .02 | .09 | 1 |
| 59R | 261 | 26 | 12 | 51 | .1 | 53 | 30 | 192 | 4.75 | 81 | 5 | ND | 1 | 7 | 1 | 9 | 2 | 40 | .07 | .01 | 2 | 11 | .37 | 17 | .01 | 2 | .34 | .01 | .04 | 1 |
| 31+00R | 7 | 63 | 12 | 160 | .5 | 22 | 10 | 682 | 5.40 | 8 | 5 | ND | 1 | 23 | 2 | 2 | 2 | 50 | .57 | .12 | 8 | 21 | .70 | 129 | .06 | 7 | 2.26 | .03 | .11 | 1 |

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

# ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: CORE AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

TABLE 6

DATE RECEIVED: JULY 19 1985 DATE REPORT MAILED: July 29/85 ASSAYER T. Saundry. DEAN TOYE OR TOM SAUNDRY. CERTIFIED B.C. ASSAYER

AMAZON PETROLEUM FILE # 85-1480 PAGE 1

| | SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB | Cu % | Zn % |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| D.D.H. 85-01 | 2901 | 1 | 6 | 9 | 26 | .4 | 78 | 11 | 525 | 2.19 | 510 | 8 | ND | 1 | 108 | 1 | 6 | 5 | 37 | 9.63 | .01 | 2 | 125 | 1.97 | 3 | .01 | 10 | 1.71 | .01 | .04 | 1 | 95 | - | - |
| | 2902 | 1 | 16 | 9 | 21 | .4 | 6 | 5 | 1164 | 2.67 | 3080 | 7 | ND | 1 | 226 | 1 | 5 | 4 | 41 | 11.08 | .01 | 2 | 3 | 1.82 | 4 | .01 | 7 | .92 | .02 | .03 | 1 | 745 | - | - |
| | 2903 | 1 | 113 | 9 | 77 | .2 | 78 | 35 | 1284 | 9.11 | 134 | 5 | ND | 2 | 39 | 1 | 4 | 3 | 184 | 2.24 | .04 | 2 | 102 | 4.11 | 3 | .01 | 8 | 3.47 | .03 | .04 | 1 | 13 | - | - |
| | 2904 | 1 | 8 | 13 | 96 | .2 | 18 | 45 | 1301 | 7.55 | 13 | 5 | ND | 1 | 31 | 1 | 3 | 2 | 215 | 1.03 | .05 | 2 | 30 | 4.58 | 2 | .27 | 9 | 3.46 | .04 | .01 | 1 | 6 | - | - |
| | 2905 | 1 | 71 | 9 | 76 | .3 | 88 | 22 | 1334 | 5.79 | 6 | 5 | ND | 1 | 35 | 1 | 4 | 2 | 158 | 2.09 | .03 | 2 | 145 | 5.00 | 3 | .14 | 12 | 3.49 | .08 | .01 | 1 | 1 | - | - |
| | 2906 | 1 | 13 | 2 | 6 | .3 | 9 | 3 | 288 | .78 | 7 | 5 | ND | 1 | 112 | 1 | 2 | 2 | 19 | 13.67 | .01 | 2 | 27 | .62 | 1 | .01 | 5 | .59 | .04 | .01 | 1 | 8 | - | - |
| D.D.H. 85-02 | 2907 | 2 | 30 | 22 | 117 | .1 | 18 | 17 | 541 | 16.39 | 17 | 5 | ND | 2 | 2 | 1 | 2 | 3 | 53 | .13 | .01 | 7 | 14 | 1.44 | 9 | .09 | 10 | 1.33 | .01 | .07 | 1 | 6 | .01 | .01 |
| | 2908 | 3 | 84 | 26 | 108 | .4 | 4 | 5 | 221 | 15.02 | 22 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 4 | 2.28 | .01 | 15 | 1 | .07 | 5 | .01 | 9 | .12 | .01 | .04 | 1 | 14 | .02 | .02 |
| | 2909 | 2 | 51 | 27 | 123 | .2 | 7 | 8 | 162 | 15.72 | 10 | 5 | ND | 2 | 7 | 1 | 2 | 3 | 18 | .52 | .01 | 14 | 3 | .45 | 8 | .02 | 13 | .48 | .01 | .07 | 1 | 2 | .01 | .02 |
| | 2910 | 6 | 34 | 26 | 152 | .2 | 3 | 14 | 148 | 15.95 | 10 | 5 | ND | 2 | 9 | 1 | 2 | 2 | 3 | .46 | .01 | 16 | 1 | .07 | 4 | .01 | 10 | .09 | .01 | .05 | 1 | 12 | .01 | .02 |
| | 2911 | 8 | 59 | 27 | 183 | .7 | 8 | 14 | 202 | 14.88 | 18 | 5 | ND | 2 | 19 | 1 | 2 | 2 | 5 | .81 | .01 | 9 | 1 | .13 | 3 | .01 | 10 | .14 | .02 | .06 | 1 | 16 | .01 | .03 |
| | 2912 | 5 | 23 | 21 | 197 | .1 | 18 | 36 | 837 | 16.99 | 5 | 5 | ND | 2 | 14 | 1 | 2 | 4 | 83 | .35 | .01 | 10 | 20 | 2.41 | 11 | .01 | 13 | 2.02 | .03 | .08 | 1 | 3 | .01 | .02 |
| | 2913 | 18 | 22 | 27 | 84 | .4 | 7 | 38 | 342 | 14.99 | 10 | 5 | ND | 2 | 17 | 1 | 2 | 3 | 7 | .47 | .01 | 16 | 1 | .28 | 8 | .01 | 10 | .17 | .02 | .07 | 1 | 15 | .01 | .01 |
| | 2914 | 4 | 167 | 14 | 199 | .2 | 23 | 21 | 1065 | 15.11 | 2 | 5 | ND | 2 | 10 | 1 | 2 | 2 | 155 | .33 | .02 | 9 | 29 | 4.21 | 22 | .20 | 19 | 3.83 | .04 | .07 | 1 | 5 | .02 | .02 |
| | 2915 | 11 | 68 | 27 | 129 | .3 | 11 | 8 | 276 | 16.56 | 5 | 5 | ND | 2 | 8 | 1 | 2 | 3 | 65 | .28 | .01 | 15 | 11 | 1.58 | 8 | .14 | 24 | 1.45 | .04 | .09 | 1 | 4 | .01 | .01 |
| | 2916 | 4 | 85 | 28 | 258 | .2 | 25 | 22 | 656 | 17.85 | 15 | 5 | ND | 3 | 12 | 2 | 2 | 5 | 158 | .28 | .01 | 11 | 33 | 4.46 | 15 | .19 | 31 | 4.00 | .05 | .07 | 1 | 8 | .01 | .03 |
| | 2917 | 11 | 39 | 25 | 262 | .4 | 22 | 18 | 851 | 17.43 | 17 | 5 | ND | 3 | 11 | 2 | 4 | 3 | 204 | .22 | .01 | 2 | 41 | 6.06 | 18 | .16 | 18 | 5.11 | .04 | .05 | 1 | 9 | .01 | .02 |
| | STD C/AU-0.5 | 20 | 60 | 43 | 134 | 7.4 | 72 | 27 | 1158 | 3.95 | 40 | 15 | 6 | 38 | 50 | 18 | 16 | 21 | 63 | .48 | .16 | 41 | 62 | .88 | 177 | .07 | 41 | 1.73 | .05 | .12 | 11 | 480 | - | - |

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

# ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: CORE AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

TABLE 6

DATE RECEIVED: JULY 24 1985 DATE REPORT MAILED: Aug 2/85 ASSAYER: T. Saundry. DEAN TOYE OR TOM SAUNDRY. CERTIFIED B.C. ASSAYER

AMAZON PETROLEUM FILE # 85-1550A



| | SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Cu % | Zn % | Au OZ/T |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| D.D.H. 85-02 | 2918 | 10 | 45 | 42 | 362 | .3 | 25 | 25 | 708 | 21.07 | 4 | 5 | ND | 2 | 14 | 1 | 3 | 2 | 153 | .43 | .01 | 25 | 31 | 4.33 | 8 | .21 | 15 | 3.94 | .06 | .01 | 1 | .01 | .05 | .001 |
| | 2919 | 2 | 323 | 19 | 228 | .1 | 19 | 23 | 648 | 19.41 | 6 | 5 | ND | 3 | 18 | 1 | 2 | 2 | 72 | .75 | .02 | 16 | 11 | 1.93 | 8 | .01 | 20 | 1.91 | .06 | .05 | 1 | .03 | .03 | .001 |
| | 2920 | 7 | 335 | 13 | 281 | .1 | 20 | 24 | 1560 | 15.49 | 2 | 5 | ND | 2 | 18 | 1 | 2 | 2 | 176 | .30 | .02 | 26 | 28 | 5.00 | 15 | .04 | 15 | 4.64 | .06 | .02 | 1 | .03 | .04 | .001 |
| | 2921 | 7 | 262 | 12 | 133 | .3 | 12 | 14 | 478 | 19.82 | 5 | 5 | ND | 3 | 15 | 1 | 2 | 3 | 48 | .53 | .01 | 5 | 7 | 1.28 | 4 | .01 | 14 | 1.22 | .04 | .04 | 1 | .03 | .02 | .001 |
| | 2922 | 11 | 267 | 14 | 129 | .2 | 21 | 20 | 291 | 17.35 | 4 | 5 | ND | 3 | 19 | 1 | 2 | 5 | 46 | .40 | .02 | 3 | 19 | .90 | 5 | .01 | 21 | 1.04 | .07 | .07 | 1 | .03 | .02 | .001 |
| | 2923 | 1 | 108 | 11 | 137 | .1 | 10 | 38 | 1117 | 14.83 | 2 | 5 | ND | 2 | 8 | 1 | 2 | 2 | 197 | .64 | .04 | 23 | 15 | 4.17 | 10 | .17 | 11 | 3.69 | .04 | .02 | 1 | .01 | .02 | .001 |
| | 2924 | 1 | 691 | 9 | 211 | .4 | 24 | 33 | 2005 | 11.53 | 6 | 5 | ND | 1 | 63 | 1 | 3 | 2 | 200 | .70 | .02 | 18 | 36 | 4.27 | 26 | .01 | 20 | 3.67 | .03 | .01 | 1 | .08 | .03 | .001 |
| | 2925 | 3 | 282 | 6 | 111 | .4 | 11 | 15 | 2421 | 5.95 | 21 | 5 | ND | 4 | 331 | 1 | 5 | 2 | 57 | 10.35 | .02 | 21 | 5 | 3.51 | 14 | .01 | 21 | .29 | .05 | .01 | 1 | .03 | .02 | .001 |
| | 2926 | 1 | 61 | 11 | 426 | .1 | 7 | 28 | 1193 | 7.69 | 3 | 5 | ND | 2 | 17 | 1 | 2 | 2 | 176 | .83 | .03 | 11 | 2 | 3.13 | 5 | .25 | 21 | 2.63 | .02 | .01 | 1 | .01 | .05 | .001 |
| | 2927 | 5 | 1181 | 11 | 915 | .5 | 6 | 34 | 910 | 9.33 | 270 | 5 | ND | 2 | 18 | 5 | 2 | 2 | 143 | .58 | .03 | 9 | 2 | 2.38 | 3 | .21 | 22 | 2.04 | .02 | .01 | 1 | .12 | .11 | .003 |
| | 2928 | 5 | 771 | 12 | 203 | .4 | 60 | 28 | 1214 | 13.75 | 3 | 5 | ND | 2 | 11 | 1 | 2 | 2 | 214 | .93 | .04 | 25 | 86 | 3.94 | 10 | .31 | 13 | 3.38 | .04 | .01 | 1 | .07 | .03 | .001 |
| | 2929 | 1 | 593 | 7 | 136 | .1 | 24 | 24 | 1778 | 7.60 | 4 | 5 | ND | 2 | 19 | 1 | 2 | 2 | 198 | .88 | .04 | 14 | 42 | 4.14 | 2 | .24 | 22 | 3.35 | .04 | .01 | 1 | .06 | .02 | .001 |
| | 2930 | 3 | 24 | 12 | 91 | .1 | 16 | 33 | 942 | 11.09 | 9 | 5 | ND | 2 | 14 | 1 | 3 | 2 | 118 | .52 | .02 | 17 | 23 | 3.83 | 1 | .14 | 20 | 2.37 | .02 | .01 | 1 | .01 | .01 | .001 |
| D.D.H. 85-03 | 2931 | 1 | 84 | 7 | 125 | .1 | 27 | 15 | 1722 | 5.60 | 8 | 5 | ND | 1 | 43 | 1 | 2 | 2 | 76 | .96 | .07 | 9 | 28 | 1.91 | 44 | .26 | 28 | 2.53 | .01 | .09 | 1 | .01 | .02 | .001 |
| | 2932 | 1 | 60 | 10 | 45 | .1 | 14 | 7 | 521 | 2.06 | 10 | 5 | ND | 1 | 39 | 1 | 2 | 2 | 17 | .69 | .03 | 3 | 7 | .53 | 33 | .07 | 16 | .64 | .01 | .10 | 1 | .01 | .01 | .001 |
| | 2933 | 7 | 93 | 16 | 70 | .1 | 30 | 12 | 616 | 2.51 | 16 | 5 | ND | 2 | 26 | 1 | 2 | 2 | 18 | .49 | .05 | 7 | 11 | .57 | 36 | .01 | 22 | .81 | .01 | .12 | 1 | .01 | .01 | .001 |
| | 2934 | 1 | 83 | 5 | 48 | .1 | 18 | 5 | 476 | 1.61 | 7 | 5 | ND | 4 | 16 | 1 | 2 | 2 | 10 | .44 | .03 | 10 | 7 | .42 | 18 | .01 | 16 | .66 | .01 | .13 | 1 | .01 | .01 | .001 |
| | 2935 | 1 | 41 | 8 | 71 | .1 | 17 | 10 | 1330 | 3.55 | 8 | 5 | ND | 2 | 142 | 1 | 2 | 2 | 51 | 2.90 | .05 | 11 | 30 | 1.16 | 19 | .01 | 24 | 1.63 | .03 | .09 | 1 | .01 | .01 | .001 |
| | 2936 | 51 | 106 | 9 | 305 | .7 | 92 | 12 | 370 | 2.46 | 39 | 5 | ND | 3 | 99 | 3 | 2 | 2 | 40 | 1.63 | .04 | 12 | 8 | .35 | 20 | .01 | 24 | .54 | .01 | .16 | 1 | .01 | .04 | .001 |
| D.D.H. 85-04 | 2937 | 1 | 305 | 9 | 54 | .2 | 38 | 6 | 2989 | 1.19 | 6 | 5 | ND | 2 | 15 | 1 | 2 | 2 | 11 | .47 | .01 | 5 | 6 | .38 | 35 | .01 | 13 | .20 | .01 | .04 | 1 | .03 | .01 | .001 |
| | 2938 | 1 | 73 | 5 | 122 | .2 | 332 | 40 | 3379 | 5.92 | 2 | 5 | ND | 3 | 170 | 1 | 3 | 2 | 51 | 4.01 | .02 | 21 | 462 | 4.91 | 60 | .01 | 29 | 3.59 | .01 | .10 | 1 | .01 | .02 | .001 |
| | 2939 | 2 | 88 | 3 | 97 | .4 | 313 | 30 | 2868 | 4.76 | 9 | 5 | ND | 4 | 164 | 1 | 2 | 2 | 64 | 5.63 | .05 | 19 | 390 | 3.56 | 85 | .01 | 26 | 2.59 | .01 | .06 | 1 | .01 | .01 | .001 |
| | STD C | 20 | 59 | 39 | 134 | 7.0 | 69 | 28 | 1167 | 4.00 | 39 | 17 | 8 | 39 | 53 | 16 | 15 | 21 | 62 | .48 | .15 | 38 | 59 | .08 | 179 | .08 | 41 | 1.72 | .06 | .10 | 12 | - | - | - |

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

# GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SLUDGE AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

TABLE 7

DATE RECEIVED: JULY 24 1985 DATE REPORT MAILED: Aug. 2/85 ASSAYER. V. Saundry. DEAN TOYE OR TOM SAUNDRY. CERTIFIED B.C. ASSAYER

AMAZON PETROLEUM FILE # 85-1550 PAGE 1

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| D.D.H. 85-04 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 85-04-20 | 3 | 177 | 165 | 153 | .4 | 88 | 12 | 911 | 3.47 | 5 | 5 | ND | 2 | 41 | 1 | 2 | 2 | 61 | 2.13 | .04 | 6 | 107 | 2.12 | 109 | .08 | 7 | 2.37 | .05 | .05 | 167 | 1 |
| 85-04-30 | 4 | 258 | 17 | 181 | .3 | 199 | 19 | 2790 | 3.76 | 3 | 5 | ND | 2 | 50 | 1 | 2 | 2 | 42 | 1.54 | .02 | 4 | 179 | 3.15 | 166 | .01 | 6 | 2.02 | .01 | .10 | 273 | 1 |
| 85-04-40 | 5 | 518 | 28 | 185 | .4 | 193 | 21 | 3863 | 4.72 | 5 | 5 | ND | 2 | 49 | 1 | 2 | 2 | 42 | 1.57 | .03 | 5 | 171 | 2.35 | 173 | .01 | 11 | 1.75 | .01 | .19 | 293 | 1 |
| 85-04-50 | 22 | 747 | 147 | 489 | .5 | 217 | 14 | 3802 | 12.37 | 15 | 5 | ND | 3 | 16 | 1 | 2 | 2 | 9 | .59 | .03 | 22 | 91 | .45 | 125 | .01 | 8 | .26 | .01 | .09 | 508 | 1 |
| 85-04-60 | 4 | 870 | 98 | 371 | .3 | 138 | 13 | 5001 | 3.06 | 4 | 5 | ND | 4 | 18 | 1 | 2 | 4 | 17 | .33 | .03 | 20 | 26 | .80 | 246 | .01 | 7 | .71 | .01 | .21 | 391 | 2 |
| 85-04-70 | 3 | 872 | 57 | 634 | .4 | 241 | 13 | 3375 | 1.98 | 2 | 5 | ND | 1 | 17 | 1 | 2 | 2 | 7 | .33 | .03 | 11 | 14 | .33 | 221 | .01 | 4 | .37 | .01 | .09 | 619 | 1 |
| 85-04-80 | 7 | 227 | 50 | 233 | .2 | 370 | 36 | 3798 | 6.63 | 40 | 5 | ND | 3 | 91 | 1 | 2 | 2 | 66 | 1.90 | .04 | 6 | 460 | 4.57 | 224 | .01 | 13 | 3.56 | .01 | .20 | 300 | 1 |
| D.D.H. 85-05 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 85-05-20 | 3 | 295 | 42 | 197 | 1.8 | 98 | 22 | 569 | 4.04 | 6 | 5 | ND | 1 | 20 | 47 | 2 | 2 | 94 | 5.88 | .01 | 4 | 195 | 2.14 | 17 | .08 | 21 | 4.42 | .03 | .01 | 509 | 1 |
| 85-05-30 | 6 | 222 | 78 | 105 | .8 | 78 | 29 | 720 | 7.80 | 2 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 445 | 3.45 | .01 | 2 | 85 | 2.20 | 19 | .40 | 17 | 3.76 | .02 | .02 | 106 | 2 |
| 85-05-40 | 5 | 216 | 68 | 71 | .7 | 73 | 25 | 648 | 6.32 | 2 | 5 | ND | 3 | 32 | 2 | 2 | 2 | 325 | 5.01 | .01 | 2 | 91 | 2.19 | 14 | .28 | 19 | 4.37 | .03 | .02 | 58 | 1 |
| 85-05-50 | 6 | 205 | 114 | 85 | .4 | 88 | 19 | 643 | 4.90 | 2 | 5 | ND | 1 | 36 | 2 | 2 | 2 | 136 | 4.89 | .01 | 2 | 116 | 2.37 | 13 | .14 | 23 | 4.17 | .04 | .01 | 70 | 2 |
| STD C/AU-0.5 | 20 | 60 | 38 | 138 | 7.1 | 69 | 25 | 1177 | 3.95 | 38 | 17 | 8 | 38 | 53 | 16 | 15 | 19 | 61 | .48 | .14 | 39 | 38 | .88 | 170 | .08 | 38 | 1.72 | .06 | .13 | 12 | 500 |

APPENDIX 1

**ACME ANALYTICAL LABORATORIES LTD.**
**Assaying & Trace Analysis**
852 E. Hastings St., Vancouver, B.C. V6A 1R6
**Telephone : 253 - 3158**

## GEOCHEMICAL LABORATORY METHODOLOGY - 1985

### Sample Preparation

1. Soil samples are dried at 60°C and sieved to -80 mesh.
2. Rock samples are pulverized to -100 mesh.

### Geochemical Analysis (AA and ICP)

0.5 gram samples are digested in hot dilute aqua regia in a boiling water bath and diluted to 10 ml with demineralized water. Extracted metals are determined by :

A. Atomic Absorption (AA)

Ag*, Bi*, Cd*, Co, Cu, Fe, Ga, In, Mn, Mo, Ni, Pb, Sb*, Tl, V, Zn
(* denotes with background correction.)

B. Inductively Coupled Argon Plasma (ICP)

Ag, Al, As, Au, B, Ba, Bi, Ca, Cd, Co, Cu, Cr, Fe, K, La, Mg, Mn, Mo, Na, Ni, P, Pb, Sb, Sr, Th, Ti, U, V, W, Zn.

### Geochemical Analysis for Au*

10.0 gram samples that have been ignited overnite at 600°C are digested with 30 mls hot dilute aqua regia, and 75 mls of clear solution obtained is extracted with 5 mls Methyl Isobutyl Ketone.

Au is determined in the MIBK extract by Atomic Absorption using background correction (Detection Limit = 1 ppb).

### Geochemical Analysis for Au**, Pd, Pt, Rh

10.0 - 30.0 gram samples are subjected to Fire Assay preconcentration techniques to produce silver beads.

The silver beads are dissolved and Au, Pd, Pt, and Rh are determined in the solution by graphite furnace Atomic Absorption. Detections - Au=1 ppb; Pd, Pt, Rh=5 ppb

### Geochemical Analysis for As

0.5 gram samples are digested with hot dilute aqua regia and diluted to 10 ml. As is determined in the solution by Graphite Furnace Atomic Absorption (AA) or by Inductively Coupled Argon Plasma (ICP).

### Geochemical Analysis for Barium

0.25 gram samples are digested with hot NaOH and EDTA solution, and diluted to 20 ml.

Ba is determined in the solution by ICP.

### Geochemical Analysis for Tungsten

0.25 gram samples are digested with hot NaOH and EDTA solution, and diluted to 20 ml. W in the solution determined by ICP with a detection of 1 ppm.

### Geochemical Analysis for Selenium

0.5 gram samples are digested with hot dilute aqua regia and dilute to 10 ml with $H_2O$. Se is determined with $NaBH_3$ with Flameless AA. Detection 0.1 ppm.

ACME ANALYTICAL LABORATORIES LTD.
Assaying & Trace Analysis
852 E. Hastings St., Vancouver, B.C. V6A 1R6
Telephone : 253 - 3158

Geochemical Analysis for Uranium

0.5 gram samples are digested with hot aqua regia and diluted to 10 ml.

Aliquots of the acid extract are solvent extracted using a salting agent and aliquots of the solvent extract are fused with NaF, $K_2CO_3$ and $Na_2CO_3$ flux in a platinum dish.

The fluorescence of the pellet is determined on the Jarrel Ash Fluorometer.

Geochemical Analysis for Fluorine

0.25 gram samples are fused with sodium hydroxide and leached with 10 ml water. The solution is neutralized, buffered, adjusted to pH 7.8 and diluted to 100 ml.

Fluorine is determined by Specific Ion Electrode using an Orion Model 404 meter.

Geochemical Analysis for Tin

1.0 gram samples are fused with ammonium iodide in a test tube. The sublimed iodine is leached with dilute hydrochloric acid.

The solution is extracted with MIBK and tin is determined in the extract by Atomic Absorption.

Geochemical Analysis for Chromium

0.1 gram samples are fused with $Na_2O_2$. The melt is leached with HCl and analysed by AA or ICP. Detection 1 ppm.

Geochemical Analysis for Hg

0.5 gram samples is digested with aqua regia and diluted with 20% HCl.

Hg in the solution is determined by cold vapour AA using a F & J scientific Hg assembly. An aliquot of the extract is added to a stannous chloride / hydrochloric acid solution. The reduced Hg is swept out of the solution and passed into the Hg cell where it is measured by AA.

Geochemical Analysis for Ga & Ge

0.5 gram samples are digested with hot aqua regia with HF in pressure bombs.

Ga and Ge in the solution are determined by graphite furnace AA. Detection 1 ppm.

Geochemical Analysis for Tl (Thallium)

0.5 gram samples are digested with 1:1 $HNO_3$. Tl is determined by graphite AA. Detection .1 ppm.

Geochemical Analysis for Te (Tellurium)

0.5 gram samples are digested with hot aqua regia. The Te extracted in MIBK is analysed by AA graphite furnace. Detection .1 ppm.

Geochemical Whole Rock

0.1 gram is fused with .6 gm $LiBO_2$ and dissolved in 50 mls 5% $HNO_3$. Analysis is by ICP or M.S. ICP gives excellent precision for major components. The M.S. can analyze for up to 50 elements.

D.D.H. - 85-01

STARTED - July 8/85
COMPLETED - July 12/85

T.D. = 149.96 (492 ft.)
Dip = -71°
Azim. = 263°

| FROM | TO | DESCRIPTION |
|---|---|---|
| 0 | 3.66 | overburden |
| | 4.42 | rubble, broken core |
| | 9.14 | volc., grn-grey, silicified, altered |
| | 12.80 | volc., dark grey, vfg, qz. por. (?)<br>- dis. Py throughout |
| | 19.51 | tuff - argl.; tuff, grn, massive, argl, blk.<br>layering = 40-50° |
| | 23.47 | diorite<br>FW contact = 18cm qz vein + brec<br>+ silver mineral (< 1%) |
| | 32.3 | volc., light grn, vfg, massive |
| | 35.2 | volc., massive, vfg, light grn-grey<br>33.25 = qz vein (5cm) + silver min<br>33.38-34.50 = brec + abn py |
| | 42.5 | volc., dark grey, minor Py<br>37.58 - some Po veins |
| | 50.9 | Volc., light grn |
| | 54.65 | Volc., grey - drk grey |
| | 65.07 | Volc., andesite, grn, mgr, generally massive<br>some Po, Py<br>65.07 - poss. fault zone, broken core |
| | 76.81 | Volc., dark grey matrix, lighter inclusions |
| | 105.31 | Volc., light grn, generally massive<br>some vesicals<br>- 87.8-89.06 = ves. volc.<br>+ minor Po, Py<br>- 92.0 = gouge zone (poss. fault) |
| | 114.21 | White dike - no meta-alt of HW volc.<br>- fragments of volc in wht<br>- vfg, poss. tuff<br>- colour gradation over +1m<br>from grn tint to white<br>109.6 = qz veins + brec (0.4m) |

RMM.

| FROM | TO | DESCRIPTION |
|---|---|---|
| | | 109.6 = qz veins + brec (0.4m) |
| | | - some maraposite |
| | | - bot 10cm is crumpled contact |
| | 149.96 | Diorite |
| | | - top 0.98m is altered |
| | | - 124.21 = grnst inclusion |

RAM.

D.D.H. - 85-02

STARTED - July 12/85
COMPLETED - July 17/85

T.D. =
Dip =
Azim. = 273°

| FROM | TO | DESCRIPTION |
|---|---|---|
| 3.05 | 35.48 | volc., light grey |
| | | - vesicular + Py + Qz |
| | | - abn chert (jasper) |
| | | layered |
| 3.05 | 3.23 | Detail mass Py + chert (jasper) |
| | -6.55 | sericitic, vesic. |
| | -7.62 | volc., andes, some sericite |
| | -7.70 | sericitic, vesicular + Py |
| | -8.14 | mass. Py |
| | -8.84 | ser. vesic, layered + Py |
| | -9.30 | mass. Py |
| | -19.96 | ser., vesic + Py layers |
| | -20.51 | massive Py |
| | -20.88 | seric. + Py bands |
| | -21.34 | mass. Py |
| | -22.86 | " " " |
| | -23.93 | " " " |
| 29.57 | 0.15m | brec. zone + qz veins + grn maraposite |
| 34.05 | 34.66 | brec. zone, some mass. Py fragments |
| 35.20 | 35.48 | brec. zone, up to 4cm |
| | | some maraposite alt |
| | | minor qz vein |
| | -58.58 | volc. vfg, light grn-grey |
| | -69.49 | volc.,grey abn. Py layers, vesic, sericitic |
| | | 58.67 = 0.37m mass Py |
| | | 59.34 = 0.21m " " " |
| | | 59.77 = 0.58m " " " |
| | | 60.66 = 1.21m " " " |
| | | 62.2 = Py layers to chert balls (jasper) |
| | | 66.1 = mass. Py, 0.3m |
| | | 66.9 = " " " 2.59m |

RJM.

| FROM | TO | DESCRIPTION D.D.H. 85-02 |
|---|---|---|
| 69.49 | 75.59 | volc., grn, mass. |
| | -80.16 | volc., blk to grey, very seric. + Py + chert |
| | | 77.6 = abn Py + Cp |
| | -83.27 | volc, grey-grn, vfg, massive |
| | -98.50 | volc, grey-wht, highly seric. |
| | | 83.7 = 0.3m mass Py + Cp |
| | | 84.3 = 0.8m " " " (Cp?) |
| | | 0.1m parting |
| | | 0.3m mass Py |
| | | 86.3m " " , +3.3m + Cp |
| | | 89.6 - 92.5 = volc, vesic, seric, some mass Py layers |
| | | 92.5 - 98.5 = mass Py + volc, seric |
| | | 94.9 = 0.7m brec + mass Py |
| | -102.02 | volc., dom. grn (dark), mgr |
| | -104.76 | volc, light grn |
| | | 103.9 = 12cm + Py + Sp(?) |
| | | 104.5 = 15cm " " " " |
| | -108.97 | volc., drk grn, mgr |
| | -113.66 | volc, m-cgr, vesic. |
| | | 112.3 = Py band 50° |
| | | some Cp in vesic 113.4m |
| | -120.55 | white dike alt. volc.? some qz veins |
| | -130.76 | volc. dark grn, grey |
| | | 121.16 - 125.6 = brec to abn Py |
| | | some Cp, Sp |
| | | 127.1 = gouge zone (fault?) |
| | | broken core, qz vein + maraposite |
| | -133.96 | volc. grn-light grn, massive |
| | | 133.2 = some Cp |
| | -138.4 | volc. grey, vfg |
| | | 135.1 = Sp parting in blk argl (?); 2mm th (red-yel) |
| | -221.59 | volc. light grn, large vesic (up to 1cm) |
| | | 148.13 = some Cp in veinlets |
| | | 166.3 = more silicic material (chert) |
| | | abn Py, some Cp + Sp |
| | | 0.97m |
| | | 0.73m grnst + Py |

RBM.

| FROM | TO | DESCRIPTION D.D.H. 85-02 |
|---|---|---|
| | 221.59 | continued |
| | | silic + Py, Cp (0.91m) |
| | | grnst + silic (1.28m) |
| | | 190.3 = Py band + Cp (0.15m) |
| | | 191.6 = sericite layers with mass Py, some Cp (2.3m) |
| | | 206.7 = chert band, abn Cp (5cm) |
| | | 211.1 = silic band + Py + Cp (?) (1.1m) |
| | | 219.1 = brec + Py + Cp (10cm) |

RJM.

D.D.H. - 85.03

STARTED - July 17
COMPLETED - July 19

T.D. = 76.20 (250ft)
Dip = - 45°
Azim. = 270°

| FROM | TO | DESCRIPTION |
|---|---|---|
| 0 | 1.22 | overburden |
| | -3.87 | Slsn, black, some fgr sasn |
| | -6.40 | chert banded wht + blk |
| | | some Po, Py, Cp? |
| | -10.21 | slsn + sasn; blk to grey interbeds |
| | -13.17 | chert dom wht |
| | | wht-grey argl partings |
| | -17.07 | chert with blk argl partings |
| | | 14.02 - partings are Py - Po (?) rich |
| | -21.24 | ~~asan~~ + slsn, abn qz veinlets |
| | -26.88 | chert, wht; with argl (seric) partings |
| | | some Po (?) |
| | | 25.0 = becomes very carb., blk partings |
| | | 25.8 = some Cp with Po along blk partings |
| | -29.47 | sasn, m-cgr, grey, greywacke |
| | -36.12 | slsn, blk + minor sasn |
| | 38.65 | sasn, m-cgr, grey |
| | -41.67 | ch + slsn, very carb partings |
| | -45.05 | slsn, some ch, some sasn |
| | -47.00 | ch with blk partings |
| | -53.04 | sasn with slsn, minor ch |
| | -55.47 | ch with carb partings |
| | -60.50 | blk matrix (mudst) with ch partings |
| | -69.65 | ch, dom wht with blk partings |
| | -70.41 | sasn + slsn |
| | -73.00 | ch, wht + blk partings |
| | | - some slsn interbeds |
| | -76.20 | slsn + sasn |

RAM

D.D.H. - 85.04

STARTED - July 19/1985
COMPLETED - July 22/1985

T.D. = 26.82m
Dip =
Azim. = 270° Vert = -45°

| FROM | TO | DESCRIPTION |
|---|---|---|
| 0 | 6.10 | O.B., some diorite |
| | 21.79 | broken core - black siltst + chert frag |
| | 22.71 | silt, blk, very carb |
| | 23.93 | " " " abn chl alt |
| | 26.82 | blk silt, very carb. |
| | | some wht ch fragments |
| | | some qz veins |

R4M.

D.D.H. - 85.05

STARTED - July 23/85
COMPLETED -

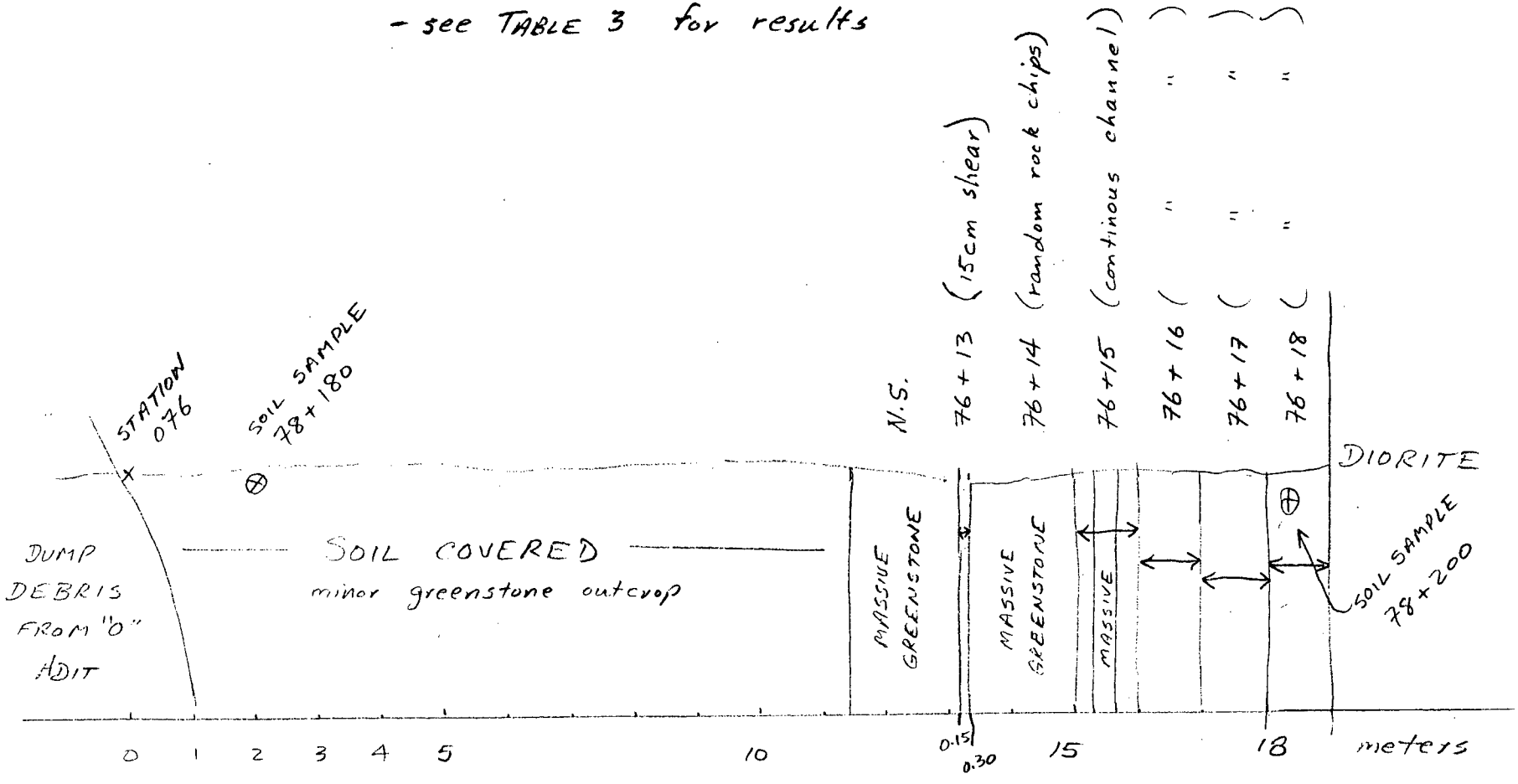
T.D. = in progress as of July 28
Dip =
Azim. = 270° Vert = -45°

| FROM | TO | DESCRIPTION |
|---|---|---|
| 0 | 2.44 | overburden |
| | -3.05 | broken diorite, rubble |
| | | Diorite |
| | -17.68 | Diorite?, very carb. |
| | | - some Cp at 8.23m; 9.30m (in Po veins) |
| | | 9.60m |
| | -19.05 | Volc. - Diorite contact zone, very black |
| | -26.40 | Volc. vfg, andes (?) |
| | -29.4 | Diorite black |
| | -34.69 | Volc, grn, some fgr, some cgr |
| | -35.72 | Diorite (?) |
| | -41.21 | Wht dike |
| | -42.98 | volc (?) dark grn, brec |
| | -60.84 | diorite (?) cgr, blk |
| | | 45.18 = some Cp + Po ( 10cm) |
| | -79.71 | Volc, grn, cataclastic text. gen. mgr, massive |
| | | 61.26 = some Cp (over 10cm) |
| | | 63.86 = some Sp with Py (Cp?) |
| | | 78.64 = some Cp ( 1%) |
| | -82.60 | Diorite, cgr, mass, some Ca veins |
| | -84.31 | grad. cont, (volc?) cataclastic |
| | -84.64 | ch, grey - wht |
| | -85.95 | blk, graph |
| | -94.79 | ch with clay lam., grey ( seric?) |
| | | - some tuff layers - grn grey |
| | -96.77 | grn rock - tuff? |
| | -97.23 | gouge, grey-blk |
| | | blk graph, cataclastic |

R4M.

# ROAD CUT, BELOW "0" ADIT

- see TABLE 3 for results




LOOKING WEST

"0" ADIT SHEAR (SECTION)

0 1 2 5

METERS

SCALE = 1 : 100

RJM 85.06.17

Fig. ...

# TRENCH No. 11 (PLAN)

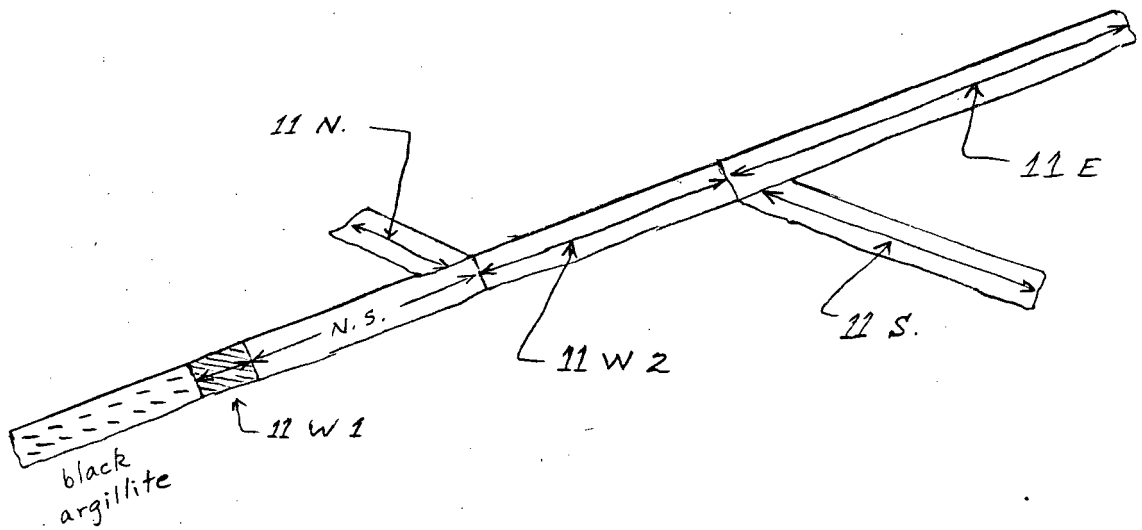
N.

- North End ; 11+00 S., 120 W.

SCALE = 1:200

0 5 10

METERS




N.S. = not sampled

= rust zone

N.D = no display

(p.p.m.)

| SAMPLE | Ag | Au | As | Sb | |
|---|---|---|---|---|---|
| 11 E | 0.1 | ND | 31 | 3 | soil debris over ~10 m |
| 11 S | 0.1 | ND | 50 | 9 | soil debris over 7 m |
| 11 N | 0.3 | ND | 210 | 23 | soil debris over 3 m |
| 11 W 1 | 0.8 | 2 | 220 | 15 | soil debris over 1.5 m |
| 11 W 2 | 0.8 | ND | 257 | 17 | soil debris over 7 m |

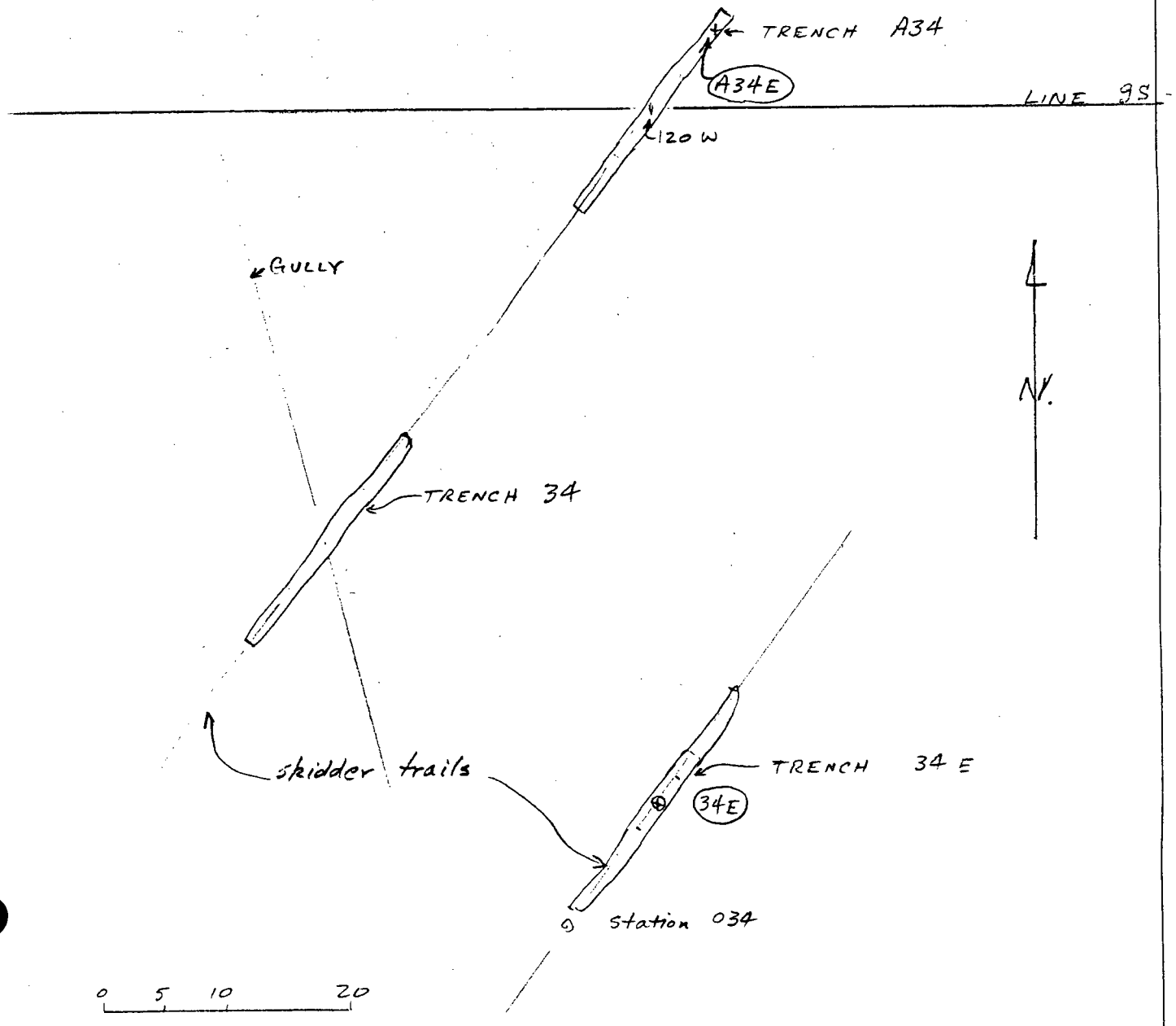
Fig. 16

85.06.12
RJM

# TRENCH No. 34 (PLAN)

- North End; between 8S and 9S approx. 120 W.

| SAMPLE | Ag | Au | As | Sb | |
|---|---|---|---|---|---|
| 34E | 0.1 | ND | 163 | 2 | soil from above rhyolite por. |
| A34E | 0.1 | ND | 14 | 2 | soil from rusty black argillite |




SCALE = 1:500

Fig. 1F

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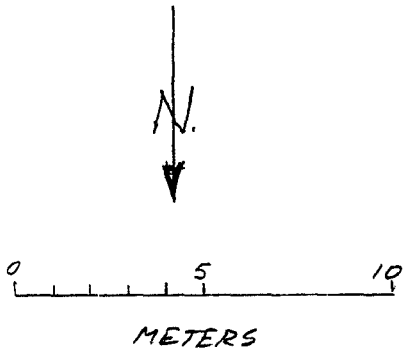
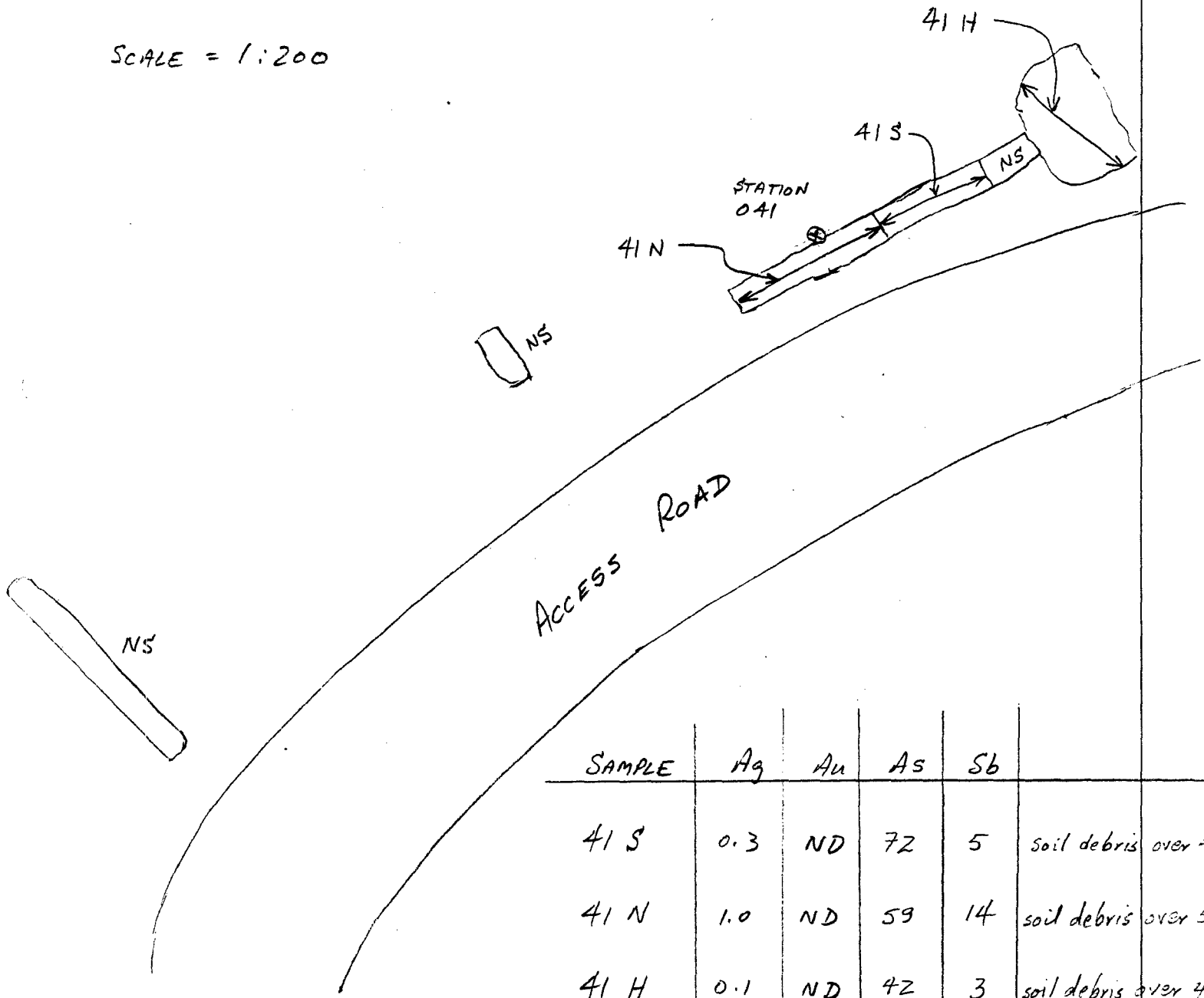
85·06·26

# TRENCH No. 41 (PLAN)

- North End;




SCALE = 1:200

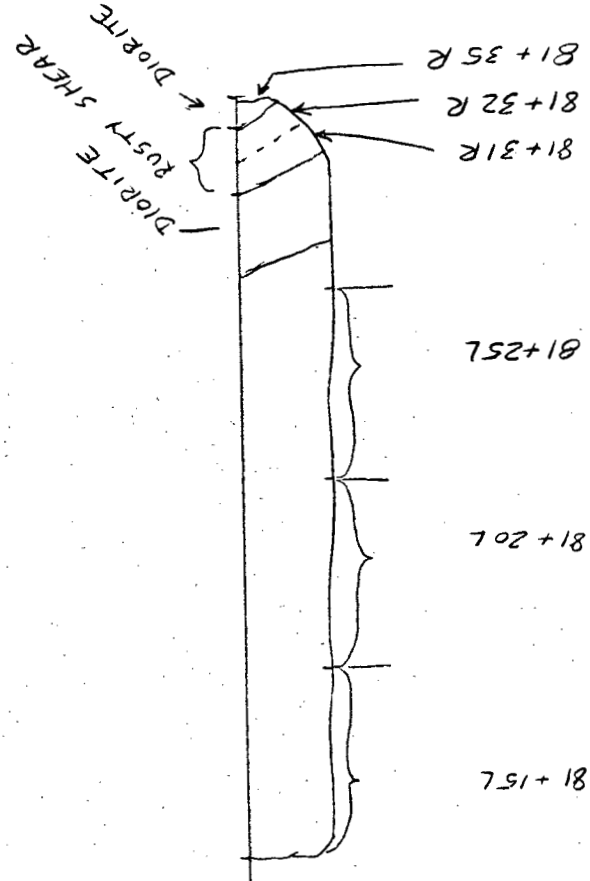



| SAMPLE | Ag | Au | As | Sb | |
|---|---|---|---|---|---|
| 41 S | 0.3 | ND | 72 | 5 | soil debris over 4 |
| 41 N | 1.0 | ND | 59 | 14 | soil debris over 5.5 |
| 41 H | 0.1 | ND | 42 | 3 | soil debris over 4 |

Fig. 18

RJM
85.06.13

# TRENCH 81 (SECTION)




| SAMPLE | Ag | Au | As | Sb | DESCRIPTION | |
|---|---|---|---|---|---|---|
| 81+15L | 0.2 | ND | 49 | 2 | soil over | 5 m |
| 81+20L | 0.3 | ND | 68 | 2 | " " | 5 m |
| 81+25L | 0.2 | ND | 44 | 2 | " " | 5 m |
| 81+31R | 0.1 | ND | 221 | 2 | rock chips over | 0.82 m |
| 81+32R | 0.1 | ND | 129 | 2 | " " " | 0.82 m |
| 81+35R | 0.1 | ND | 18 | 2 | " " " | 0.80 m |

Fig. 19

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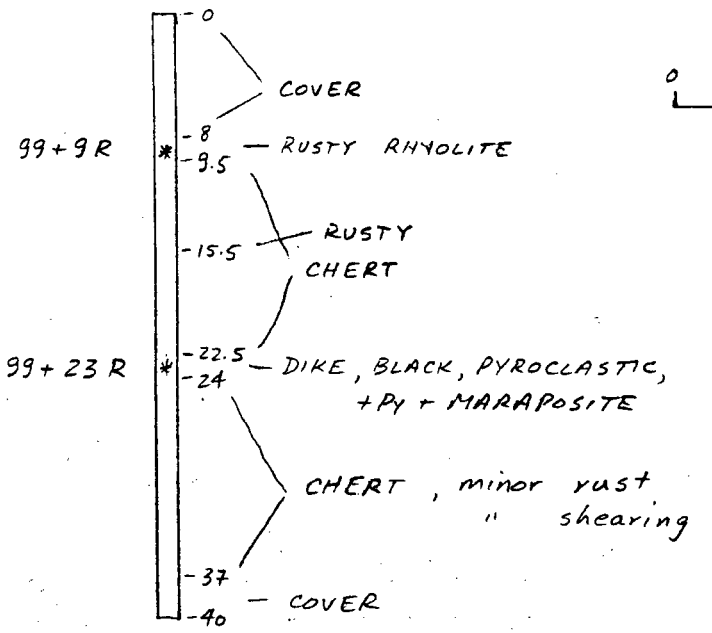
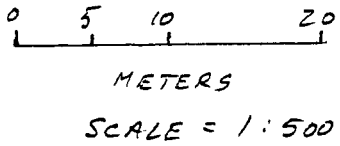
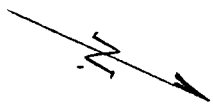
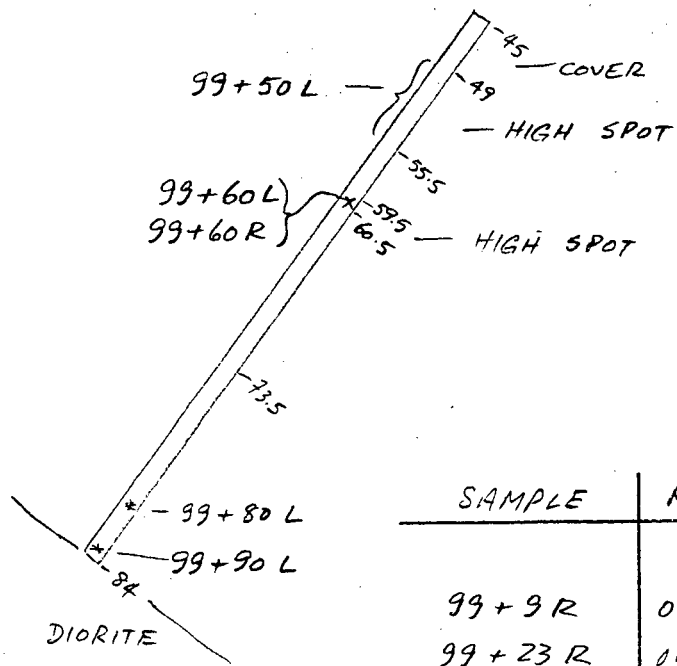
85.06.26

# TRENCH 99 (PLAN)



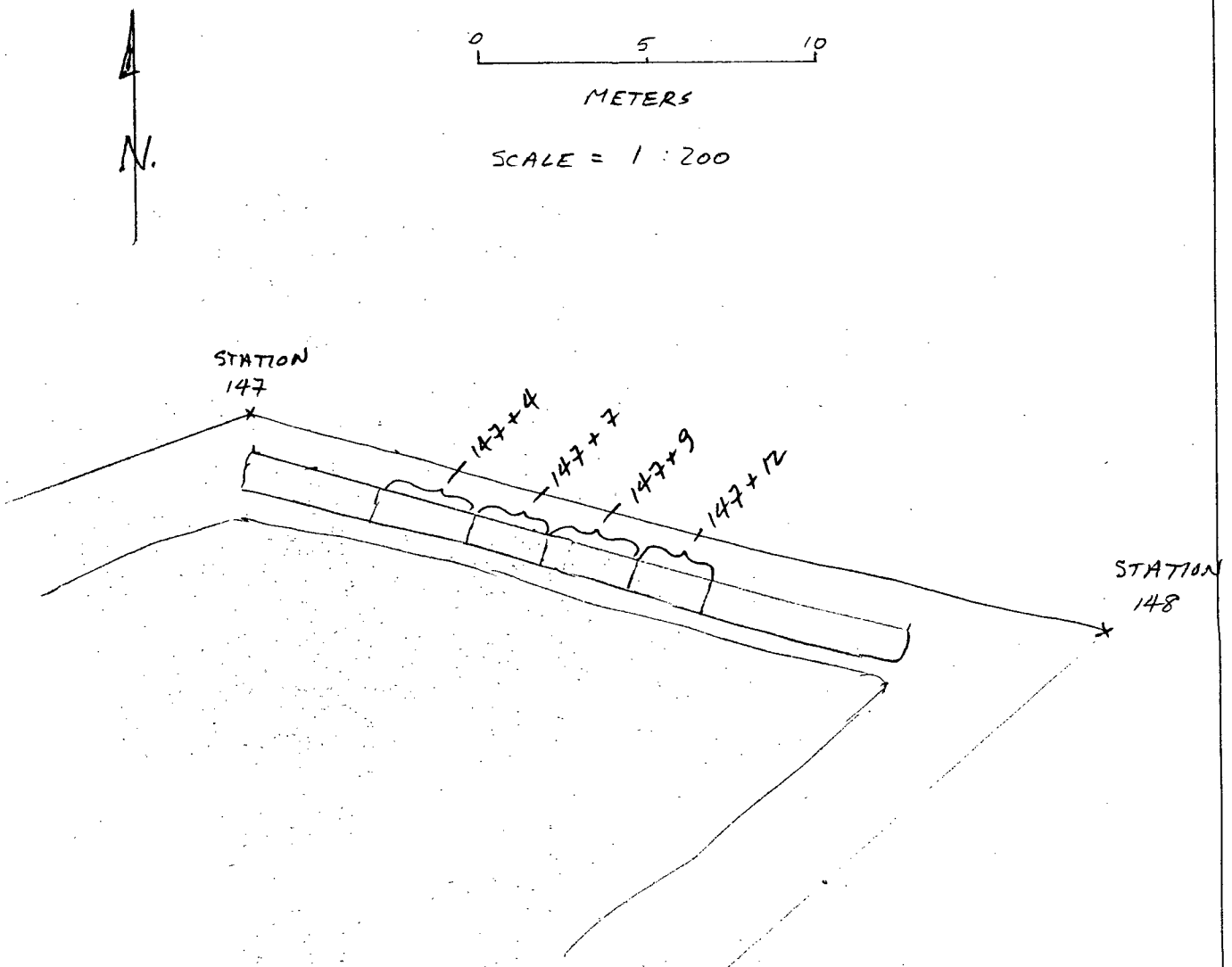

| SAMPLE | Ag | Au | As | Sb | DESCRITION |
|---|---|---|---|---|---|
| 99+9R | 0.1 | ND | 18 | 2 | rusty rock chips |
| 99+23R | 0.3 | ND | 71 | 2 | " " " |
| 99+60R | 0.1 | ND | 6 | 2 | rock chips |
| 99+50L | 0.3 | ND | 11 | 2 | soil over 6.5 m |
| 99+60L | 0.1 | ND | 11 | 2 | " " 1 m |
| 99+80L | 0.1 | ND | 12 | 2 | grab soil |
| 99+90L | 0.2 | ND | 11 | 3 | " " |

RJM

Fig. 20

85.06.26

# TRENCH 147 (PLAN)




| SAMPLE | Ag | Au | As | Sb |
|---|---|---|---|---|
| 147+4 | 0.2 | ND | 18 | 4 |
| 147+7 | 0.2 | ND | 20 | 3 |
| 147+9 | 0.1 | ND | 15 | 2 |
| 147+12 | 0.2 | ND | 35 | 2 |

Fig. 21

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85.06.26

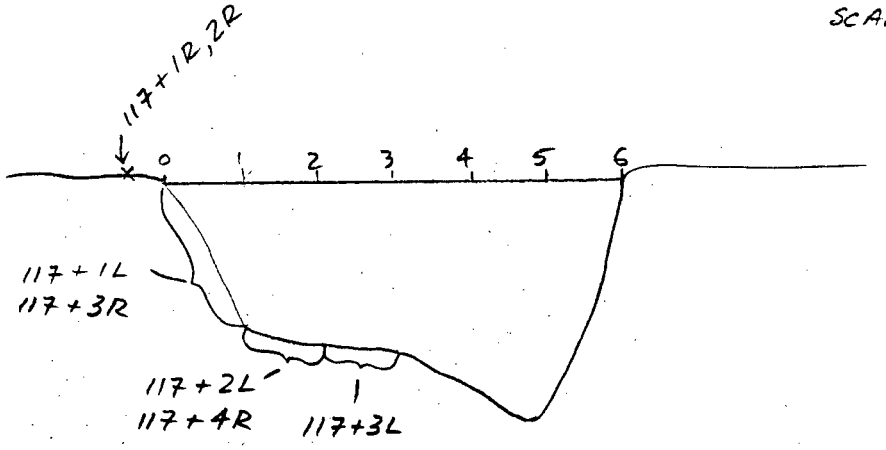
# TRENCH 117 (section)

LOOKING NORTHWEST

0 5

METERS

SCALE = 1: 100

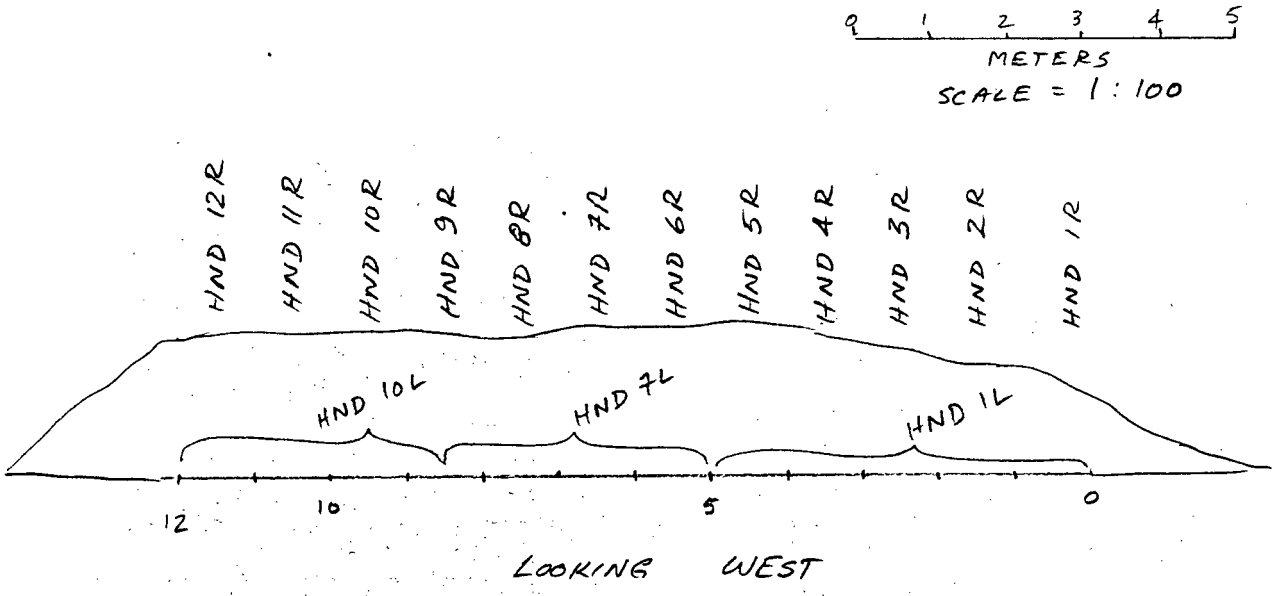



| SAMPLE | Cu | Pb | Zn | Fe % | Mo | | | DESCRIPTION |
|---|---|---|---|---|---|---|---|---|
| 117 + 1L | 84 | 7 | 86 | 3.1 | 2 | | | |
| 2L | 187 | 12 | 69 | 3.4 | 2 | | | |
| 3L | 179 | 11 | 78 | 4.5 | 4 | | | |
| 117 + 1R | 2 | 5 | 221 | 5.8 | 1 | | | |
| 2R | 6 | 6 | 38 | 4.2 | 12 | | | |
| 3R | 62 | 11 | 167 | 8.1 | 9 | | | |
| 4R | 31 | 7 | 159 | 6.0 | 3 | | | |
| 5R | 153 | 12 | 159 | 8.2 | 1 | | | |

Fig. 22

RJM
85.06.28

# TRENCH 118 (Highway New Discovery)
(SECTION)




| SAMPLE | Cu | Pb | Zn | Fe | Mo | DESCRIPTION | |
|---|---|---|---|---|---|---|---|
| HND 1L | 70 | 21 | 81 | 8.6 | 4 | soil over 5 m | |
| HND 7L | 56 | 16 | 60 | 11.8 | 6 | " " 3.5 m | |
| HND 10L | 37 | 14 | 41 | 9.7 | 6 | " " 3.5 m | |
| HND 1R | 60 | 7 | 126 | 23.1 | 1 | rock chips over 1m | (0-1 m) |
| 2R | 42 | 15 | 102 | 14.6 | 3 | " " " " | (1-2 m) |
| 3R | 57 | 16 | 105 | 19.7 | 4 | " " " " | (2-3 m) |
| 4R | 33 | 15 | 128 | 11.8 | 1 | " " " " | (3-4 m) |
| 5R | 38 | 14 | 27 | 11.4 | 1 | " " " " | (4-5 m) |
| 6R | 39 | 12 | 41 | 12.4 | 4 | " " " " | (5-6 m) |
| 7R | 16 | 6 | 30 | 8.8 | 2 | " " " " | (6-7 m) |
| 8R | 18 | 13 | 31 | 14.0 | 1 | " " " " | (7-8 m) |
| 9R | 17 | 5 | 14 | 7.9 | 1 | " " " " | (8-9 m) |
| 10R | 38 | 8 | 70 | 7.3 | 5 | " " " " | (9-10 m) |
| 11R | 19 | 10 | 67 | 10.6 | 2 | " " " " | (10-11 m) |
| 12R | 35 | 20 | 109 | 15.5 | 5 | " " " " | (11-12 m) |

Fig. 23

RJM
85.06.26

# TRENCH 118 A (section)

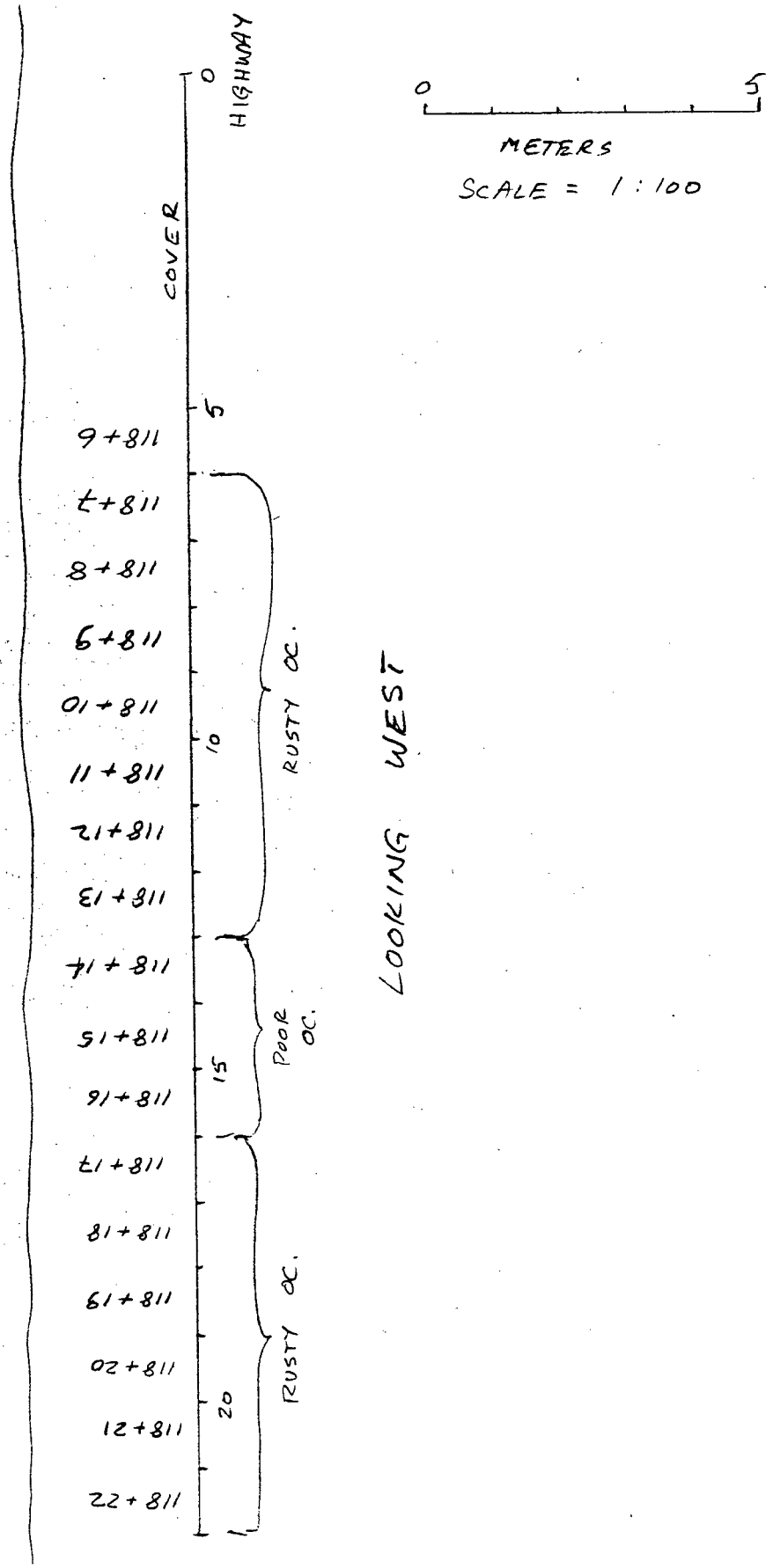
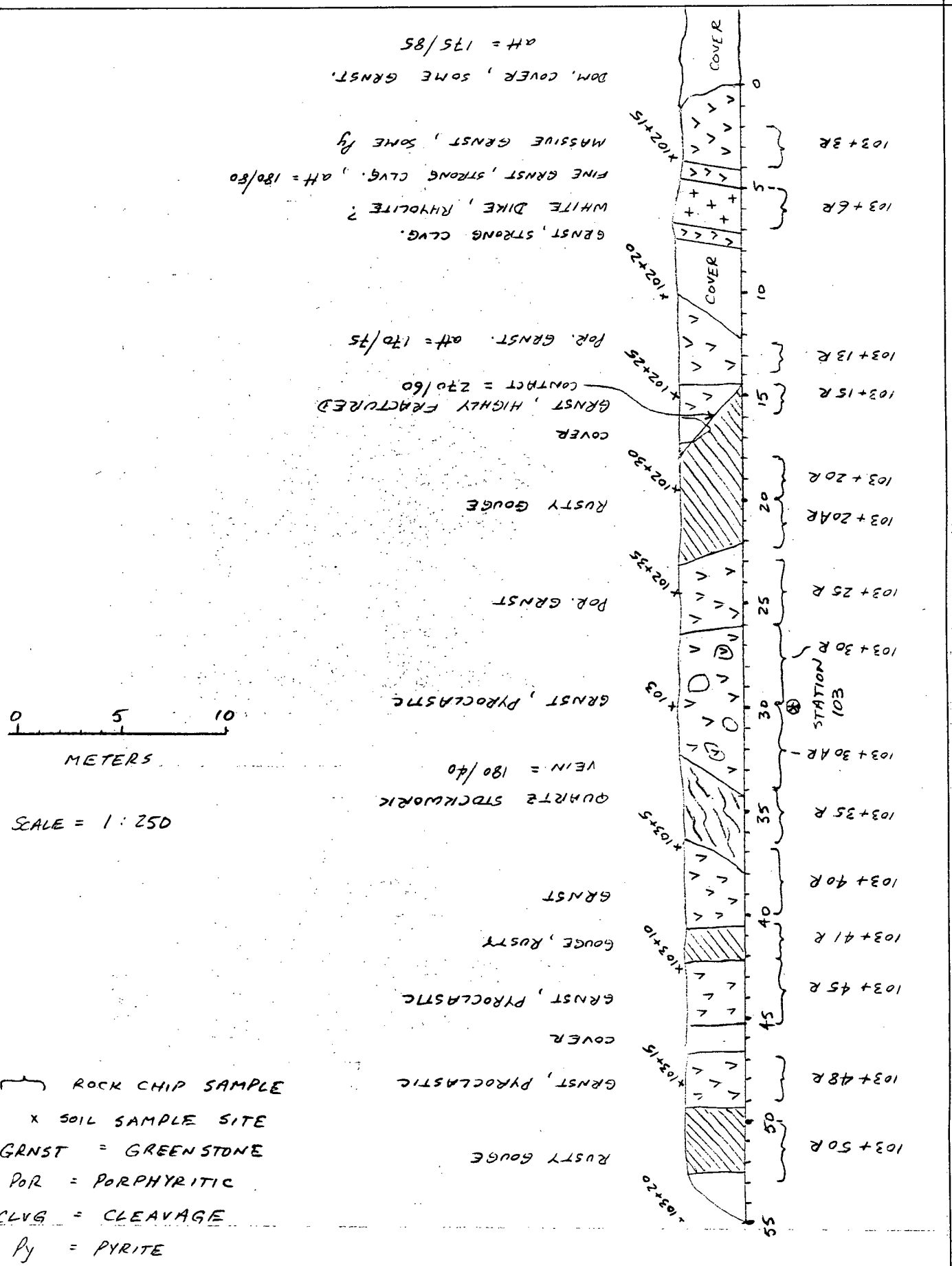



Fig. 24

RJM
85·06·28

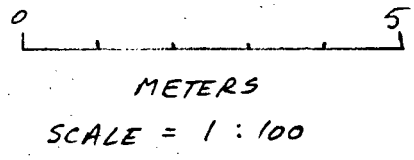
# TRENCH 103 (SECTION)

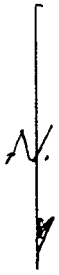


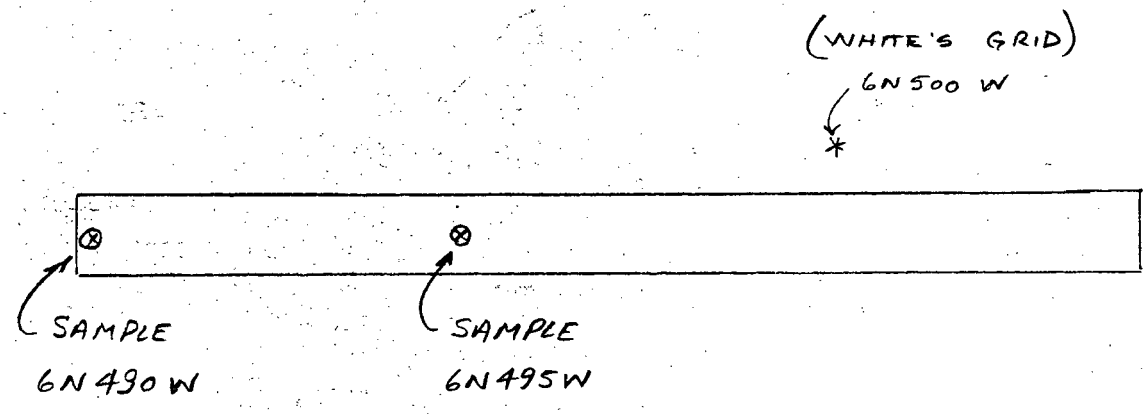

RJM
85·06·26

Fig. 25

# TRENCH 6N 500W (PLAN)



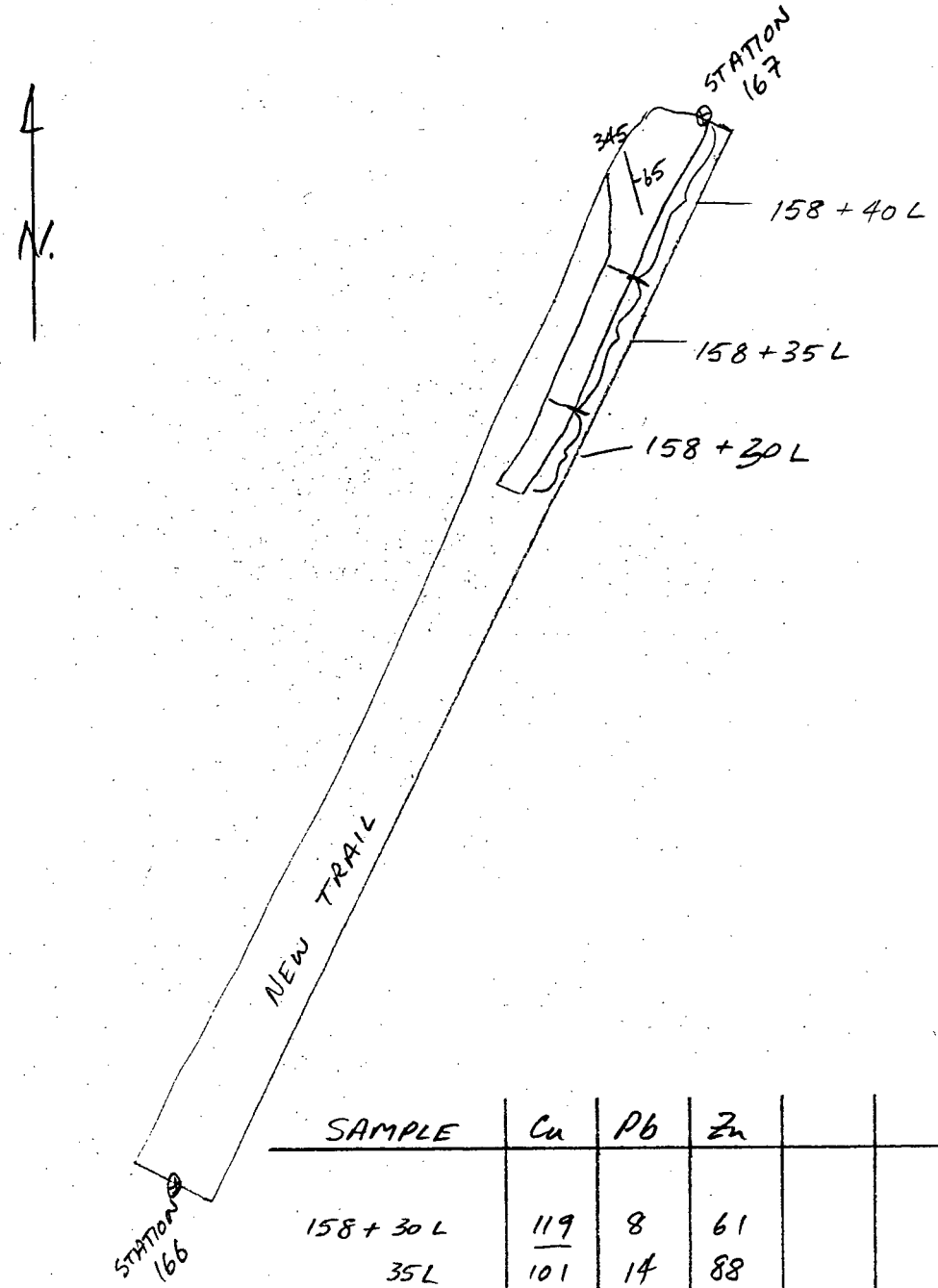

| SAMPLE | Cu | Pb | Zn | | DESCRIPTION |
|---|---|---|---|---|---|
| 6N 495 W | 50 | 3 | 63 | | SOIL FROM TILL, 4.5 m DEPTH |
| 6N 490 W | 116 | 6 | 118 | | SOIL FROM TILL, 5.5 m DEPTH |

Fig. 26

RJM
85.06.26

# TRENCH 158 (plan)

0 5 10
METERS
SCALE = 1:250




| SAMPLE | Cu | Pb | Zn | | | DESCRIPTION |
|---|---|---|---|---|---|---|
| 158 + 30 L | 119 | 8 | 61 | | | |
| 35 L | 101 | 14 | 88 | | | |
| 40 L | 84 | 6 | 52 | | | |

Fig. 27

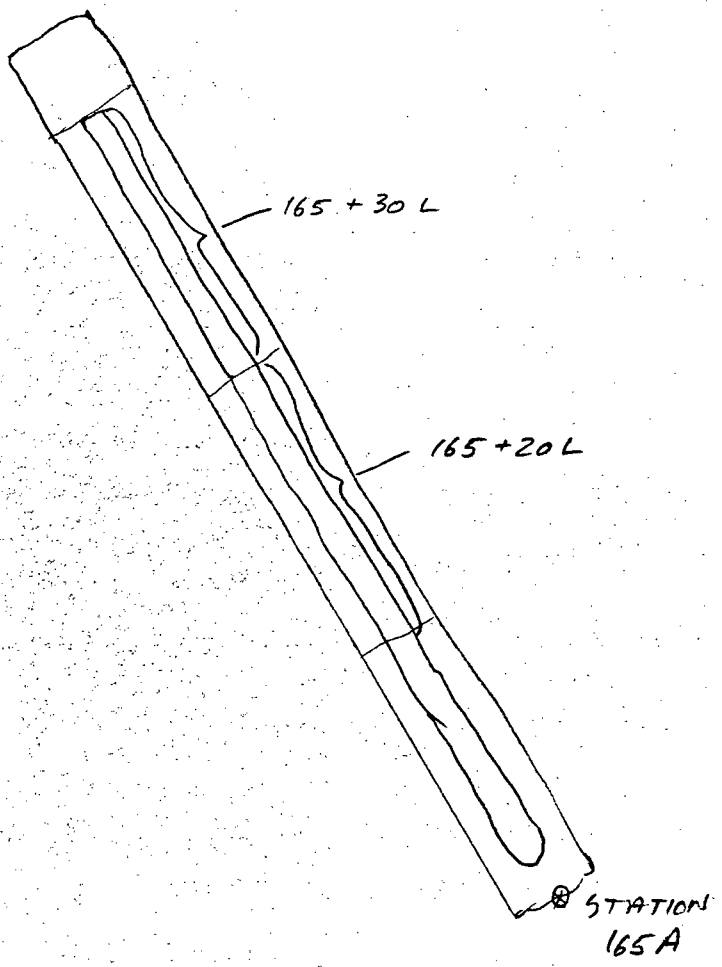
RTM
85·06·28

# TRENCH 165 (plan)

0 5 10

METERS

SCALE = 1:250




| SAMPLE | Cu | Pb | Zn | Fe | Mo | | | DESCRIPTION |
|---|---|---|---|---|---|---|---|---|
| 165 + 20 L | 91 | 16 | 71 | 3.75 | 1 | | | soil over 10 m |
| 165 + 30 L | 65 | 11 | 71 | 3.51 | 1 | | | " " " |

⊗ STATION 165

Fig. 28

RJM
85.06.25

400S
500S
600S
700S
800S
900S
1000S
1100S
1200S
BASELINE
500W
400W
300W
200W
100W
0
100E
200E
300E
400E
APPROX. CLAIM BDRY.
6628 FRACTION
UNIT 5913
As
EM
TRENCH 600S 320E
TRENCH 41
TRENCH 34
TRENCH 900S
NEW ROAD 1985
TRENCH 147
TRENCH 11
NEW ROAD 1985 station 144 - 148
LILLOOET - GOLD BRIDGE HWY
MATCH LINE SHEET A SHEET B
SEE SHEET 'B' FOR DETAILS IN THIS AREA
044
045
046
047
048
049
050
051
052
053
041
042
043
112
113
114
144
145
146
147
148
027
026
023
031
032
034
029
030

As ANOMOLY (MARK 1984)

EM VLF-EM CONDUCTOR (MARK 1984)

0 20 40 60 80 100 120
METERS
SCALE 1:1200

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

Morris Geological Co. Ltd.

AMAZON PETROLEUM CORP.

# WAYSIDE PROJECT

WAYSIDE MINE AREA

SUMMARY MAP OF PHYSICAL WORK

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG. '85 | SHEET 'A' |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | FIG. 3A |

TRENCH 99

TRENCH 103

TRENCH 81

TRENCH 6N 300W

TRENCH 6N 500N

'O' ADIT

No. 1 ADIT

No. 2 ADIT

No. 3 ADIT

No. 4 ADIT.

No. 5 ADIT

BASELINE

6N

5N

SPLICE LINE SHEET 'B'
SHEET 'C'

84 WS6

84 WS1

84 WS 2
84 WS2A

LEGEND:

⊗ SOIL SAMPLE SITE -(SERAPHIM 1983)

E.M. CONDUCTORS (WHITE 1984)

1985 ROAD

0 20 40 60 80 100 120
METERS
SCALE 1:1200

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ASSESSMENT REPORT

14,164

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AMAZON PETROLEUM CORP.

# WAYSIDE PROJECT

WAYSIDE MINE AREA

SUMMARY MAP OF PHYSICAL WORK

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG 85 | SHEET 3B |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | FIG. 3B |

4 N
3 N
2 N
1 N
0
1 S
2 S
3 S
4 S

BASELINE

TRENCH 59
TRENCH 61
TRENCH 165
TRENCH 158
TRENCH 117
TRENCH 118A
TRENCH 118

84-07
85-05
84-04
85-03
85-04
85-01
84-03
84-10,11
84-05
85-02
80-S1
80-S2
80-S3
80-S4
80-S5
80-S8
80-S9
79-S6
TD85-01 TD85-02

LEGEND:

- A — I.P. ANOMALIES (MARK, 1981)
- E.M. CONDUCTORS (WHITE, 1984)
- × SOIL SAMPLE SITE (ELWELL, 1980)
- 80-S1 — DRILL HOLE COLLAR & PROJECTION
- 171 — 1985 ROAD CONSTRUCTION
- 117 — PRE 1985 ROADS

SCALE 1:1200
0 20 40 60 80 100 120 METERS

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14,164

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# WAYSIDE PROJECT

WAYSIDE MINE AREA

SUMMARY MAP OF PHYSICAL WORK

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG. 85 | SHEET 0 |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | FIG. 3C |

400S

500S

600S

700S

800S

900S

1000S

1100S

1200S

500W 400W 300 W 200W 100W 0 100E 200E 300E 400E

BASELINE

ARG. CHERT

CHERT GRNST.

DIORITE CHERT

Rhy. Float.

Rhy. Dike Float

Rhy. Dike

Rhy. Dike

GULLY

GULLY

GULLY

TOP

MATCH LINE SHEET A SHEET B

SEE SHEET 'B' FOR DETAILS IN THIS AREA

LILLOOET - GOLD BRIDGE HWY.

LEGEND :

- ROAD OR TRAIL
- SURVEY STATION
- OUTCROP
- Ch ---- CHERT
- Arg ---- ARGILLITE
- Ss ---- SANDSTONE
- D ---- DIORITE GRNST. ---- GREENSTONE
- Rhy. ---- RHYOLITE
- Cong. ---- CONGLOMERATE
- 20 50 ---- BEDDING ATTITUDE
- 80 120 ---- JOINTING ATTITUDE
- SYNCLINE, ANTICLINE
- TOP ---- DIRECTION OF STRATIGRAPHIC TOP
- 50 90 ---- LINEAR FEATURE
- MAPPED CONTACT
- INFERRED CONTACT
- Flr. ---- FLOAT

* EAST SIDE GEOLOGY BY H.A.

0 20 40 60 80 100 120

METERS

SCALE 1:1200

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

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# WAYSIDE PROJECT

WAYSIDE MINE AREA

## GEOLOGY

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG. '85 | SHEET 'A' |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | FIG. 4A |

DIORITE

DIORITE

CHERT

MATCH LINE IS DIORITE CHERT CONTACT

MATCH LINE SHEET A
SHEET B

DIORITE

DIORITE

DIORITE

CHERT

CHERT

DIORITE

DIORITE

GRNST

GRNST

SWAMP (approx. loc.)

BASELINE

6N

5N

6N

5N

Major Gully 040°

Major Gully 05°

Major Gully 160°

Major Gully 0°

Minor Gully 080°

Ridge Gully

LANDING

Limestone

Paxton Adit

'O' ADIT

No. 1 ADIT

No. 2 ADIT

No. 3 ADIT

No. 4 ADIT

No. 5 ADIT

DUMP

Trench

White Int. Rhy.

White Rhy.

White Granite

Por. Grnst

blk. mafic

Grnst. Int.

Ch-Grnst. Int

Grnst Int

Grnst.

Gmst

Ch

Ch. Argl.

Chert

500W

400W

300W

200W

100W

SPLICE LINE SHEET 'B'
SHEET 'C'

0 20 40 60 80 100 120
METERS
SCALE 1 : 1200

LEGEND :

- ROAD OR TRAIL
- 017 SURVEY STATION
- OUTCROP
- Ch CHERT
- Arg ARGILLITE
- Ss SANDSTONE
- D DIORITE GRNST. GREENSTONE
- Rhy. RHYOLITE
- Cong. CONGLOMERATE
- 20/50 BEDDING ATTITUDE
- 80/120 JOINTING ATTITUDE
- SYNCLINE, ANTICLINE
- TOP DIRECTION OF STRATIGRAPHIC TOP
- 50→90 LINEAR FEATURE
- MAPPED CONTACT
- INFERRED CONTACT
- Flt. FLOAT

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

Morris Geological Co. Ltd.

AMAZON PETROLEUM CORP.

# WAYSIDE PROJECT

WAYSIDE MINE AREA

## GEOLOGY

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG. '85 | SHEET 'B' |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | FIG. 4B' |

CARPENTER LAKE

GRNST. POR.
GRNST. ?
GRNST.
Ch
Old Trench
CHERT
GRNST.
DIORITE
Gully 260°
Trench
84-C8
84-C9
Culvert
84-07
BASELINE
Massive Pyrite Float
Scattered Ch. Occ.
Ch Float?
Rhyolite Dike
Ch.
DIORITE
FW.
D
H.W.
DIORITE
Gully 010°
Gully 025°
RHYOLITE DIKE
White Rhyolite
HIGHWAY II
Culvert
84-04
80-S3
80-S8
80-S5
Grnst (brec)
80-S2
79-S6
HW. DIORITE
80-S9
84-05
Scattered Grnst Oc.
85-01
84-03
84-10,11
80-S1
D.Float
FW.
DIORITE
Grnst. Por.
80-S4
HW.
DIORITE
D. flt.?
Gully 020°
Gully 130°
FW.
D.Float?
Ch.
Old Trench

4 N
3 N
2 N
1 N
0
1 S
2 S
3 S
4 S

600W 500W 400W 300W 200W 100W 0

## LEGEND :

- ROAD OR TRAIL
- 017 SURVEY STATION
- OUTCROP
- Ch CHERT
- Arg ARGILLITE
- Ss SANDSTONE
- D DIORITE GRNST. GREENSTONE
- Rhy. RHYOLITE
- Cong. CONGLOMERATE
- 30/50 BEDDING ATTITUDE
- 80/120 JOINTING ATTITUDE
- SYNCLINE, ANTICLINE
- TOP DIRECTION OF STRATIGRAPHIC TOP
- 50 → 90 LINEAR FEATURE
- MAPPED CONTACT
- INFERRED CONTACT
- Flt. FLOAT

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

0 20 40 60 80 100 120
METERS
SCALE 1:1200

Morris Geological Co. Ltd.

AMAZON PETROLEUM CORP.

# WAYSIDE PROJECT

## WAYSIDE MINE AREA
## GEOLOGY

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG. 85 | SHEET 'C' |
| AUTHOR: R.J. MORRIS RJM | SCALE: 1:1200 | FIG. 4C |

400S

500S

600S

700S

800S

900S

1000S

1100S

1200S

BASELINE

× WS-85-A02

× WS-85-ECH 1

× WS-85-A01

600S 320R, L

TRENCH 600S 320E

× WS-85-A04

× WS-85-A03

TRENCH 41

TRENCH 900S

TRENCH 34

A34E

TRENCH 147

TRENCH 11

LILLOOET - GOLD BRIDGE HWY

MATCH LINE

SHEET A

SHEET B

SEE SHEET 'B' FOR DETAILS IN THIS AREA

● 108 SURVEY STATION

× 31+20 SOIL SAMPLE LOCATION & No.

X WS-85-A03 — H. ARIK SAMPLE

0 20 40 60 80 100 120

METERS

SCALE 1:1200

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14,164

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AMAZON PETROLEUM CORP.

# WAYSIDE PROJECT

WAYSIDE MINE AREA

## GEOCHEM SAMPLING

| | | |
|---|---|---|
| DRAWN BY: J.W.K | DATE: AUG. 85 | SHEET 'A' |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | FIG. 5A |

TRENCH 99

TRENCH 103

103+3R → 50R

See Detail Trench Sketch

TRENCH 81

TRENCH 6N300W, 6N300L

TRENCH 6N500W

6N495L , 6N490L

BASELINE

6N

5N

SPLICE LINE SHEET 'B'

SHEET 'C'

'0' ADIT

SEE: DETAIL AREA 78

No. 1 ADIT

No. 2 ADIT

No. 3 ADIT

No. 4 ADIT.

No. 5 ADIT

Power Line Adit

PLA 1-4

PLA 5,6,7 R

LILLOOET - GOLD BRIDGE HWY.

Thick Cover

× — SOIL SAMPLE

• SURVEY STATION

METERS

SCALE 1:1200

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

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# WAYSIDE PROJECT

WAYSIDE MINE AREA

## GEOCHEM SAMPLING

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG '85 | SHEET 'B' |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | FIG. 5B |

4 N

3 N

2 N

1 N

0

1 S

2 S

3 S

4 S

× 4 N 200 W.

× 55550W

BASELINE

LILLOOET - GOLD BRIDGE HWY.

TRENCH 61
61+1L

TRENCH 59
59+1, 2L × 59R.

TRENCH 158
84-04
120+120
158+40L
158+35L
158+30L
166+40
120+100
120+80
120+60
120+40
120+20

TRENCH 165
123+260
123+240
123+220
123+200
123+180
123+160
123+140
123+120
123+100
123+80
123+40
123+20

TRENCH 117
117R-5R
117 1L-3L
117+40
117+60
117+80
117+100
117+120
117+140
117+160
117+180
117+200
117+220
117+240
117+260
117+280
117+300
117+320
117+340
117+360
117+380
117+400
117+420
117+440
117+460
117+480
117+00
80-S3
80-S2
79-S6
80-S1
80-S4
80-S5
80-S8
80-S9
84-03
84-10,11
85-01
84-05

TRENCH 118A
118+6R-22R

HIGHWAY NEW DISCOVERY
HND 1-12R
HND 1,2 10L

56+160
56+120
58+20
58+40
58+60
58+80
58+100
61+60
61+40
61+20
60+20
60+40
59+60
59+40
59+20
59+00
62+24
62+12
62+0
84-07

LEGEND:

● 168 SURVEY STATION

× 120-60 SOIL SAMPLE LOCATION & No.

0 20 40 60 80 100 120
METERS
SCALE 1:1200

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

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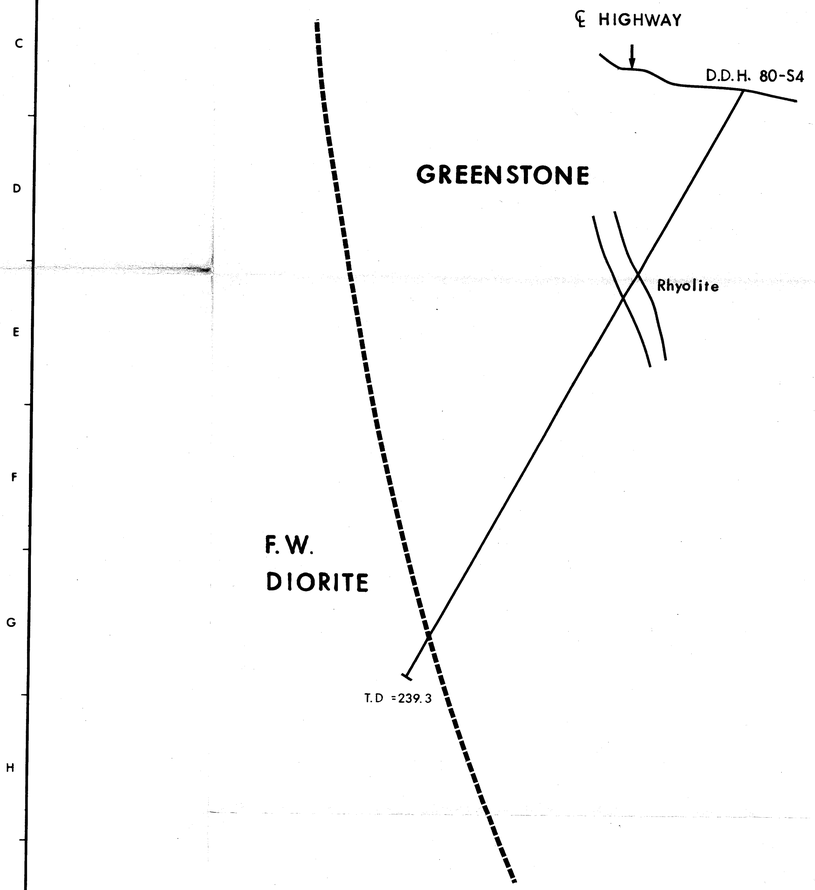
# WAYSIDE PROJECT

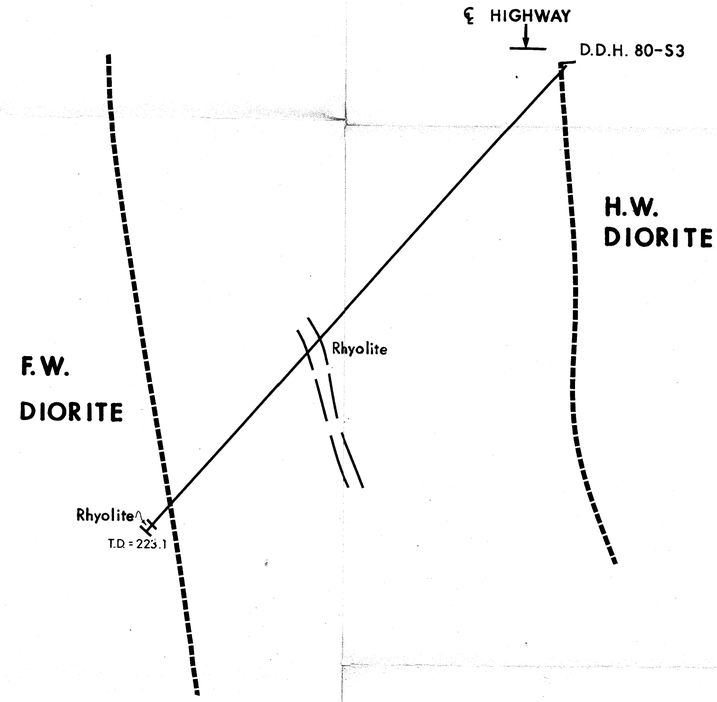
WAYSIDE MINE AREA

## GEOCHEM SAMPLING

| | | |
|---|---|---|
| DRAWN BY: J.W.K. | DATE: AUG. 85 | SHEET 'C' |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | FIG. 5C |




D.D.H. 80-S4




D.D.H. 80-S3



| NOTES | NUMBER | REFERENCE DRAWINGS |
|---|---|---|
| | | |

| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
|---|---|---|---|---|---|
| | | | | | |

| | ENG. IN CHARGE | PROJECT | DATE |
|---|---|---|---|
| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. 85
SCALE: 1:1000
DESIGN:
DRAWN: J.W.K.
CHECKED:
APPROVED:

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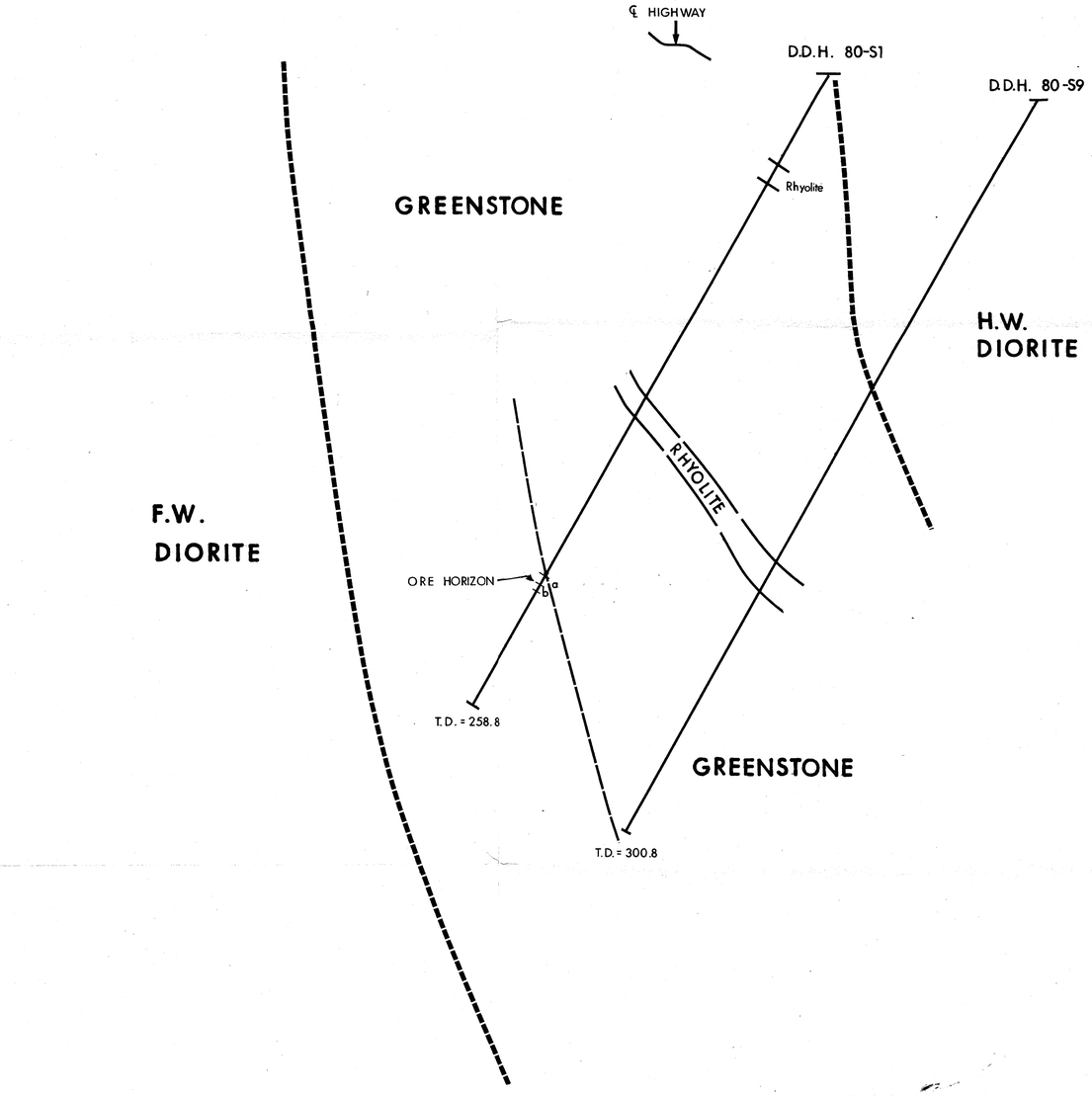
AMAZON PETROLEUM CORP

WAYSIDE PROJECT

DRILL HOLE SECTIONS-80-S3 & 80-S4
LOOKING NORTH

AUTO DRAFT | DRAWING NUMBER FIG. 6A | REV. △

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ASSESSMENT REPORT

14,164

| NOTES | NUMBER | REFERENCE DRAWINGS |
|---|---|---|
| | | |

| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
|---|---|---|---|---|---|
| | | | | | |

| | ENG. IN CHARGE | PROJECT | DATE |
|---|---|---|---|
| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. 85
SCALE: 1:1000
DESIGN:
DRAWN: J.W.K.
CHECKED:
APPROVED: RJM

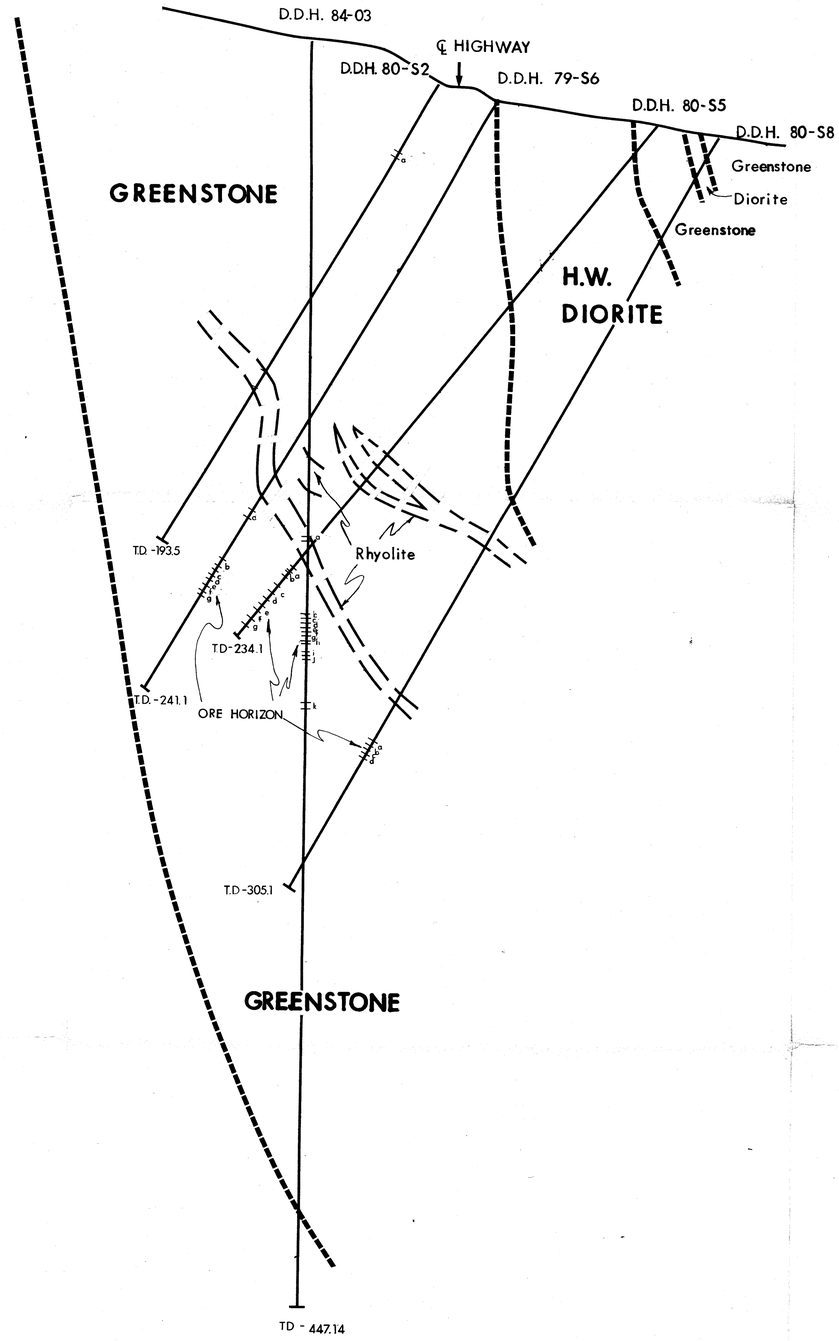
Morris Geological Co. Ltd.

AMAZON PETROLEUM CORP

WAYSIDE PROJECT

Drill Hole Section 80-S1 → 80-S9
LOOKING NORTH

AUTO DRAFT | DRAWING NUMBER FIG. 6B | REV. △




GEOLOGICAL BRANCH
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14,164

| NOTES | NUMBER | REFERENCE DRAWINGS |
|---|---|---|
| | | |

| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
|---|---|---|---|---|---|
| | | | | | |

| | ENG. IN CHARGE | PROJECT | DATE |
|---|---|---|---|
| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. 85
SCALE: 1:1000
DESIGN:
DRAWN: J.W.K.
CHECKED:
APPROVED: RAM

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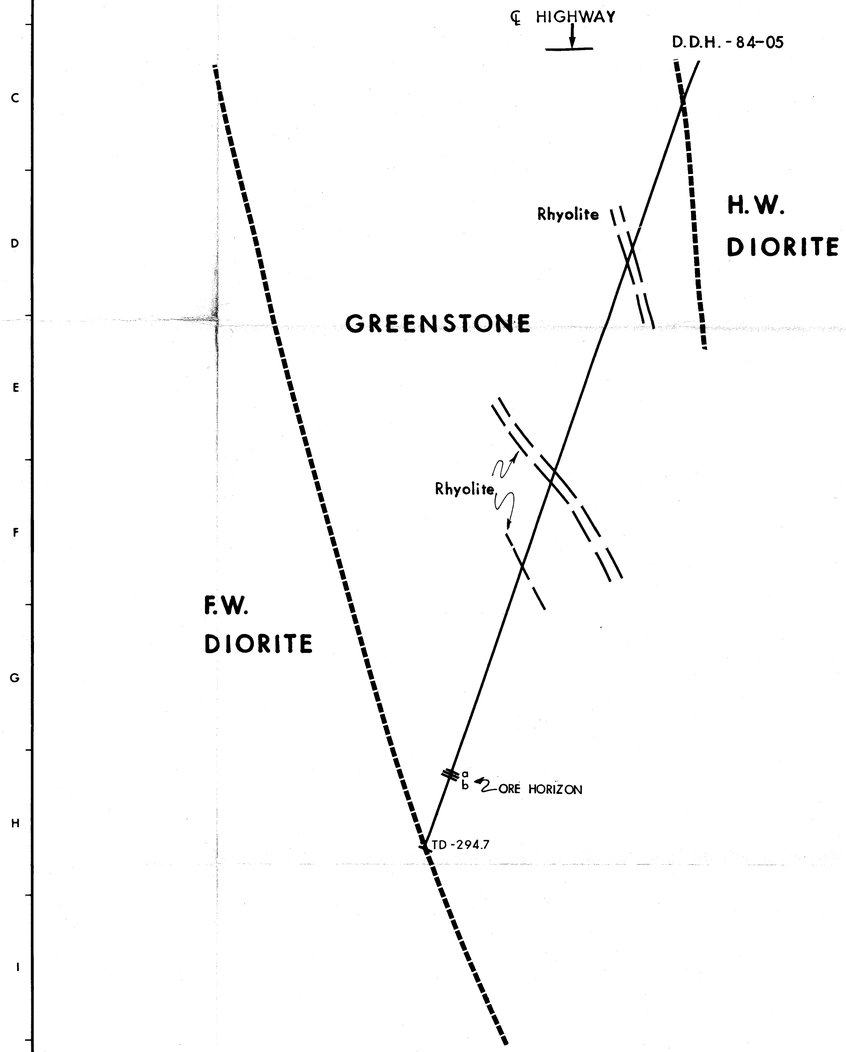
AMAZON PETROLEUM CORP

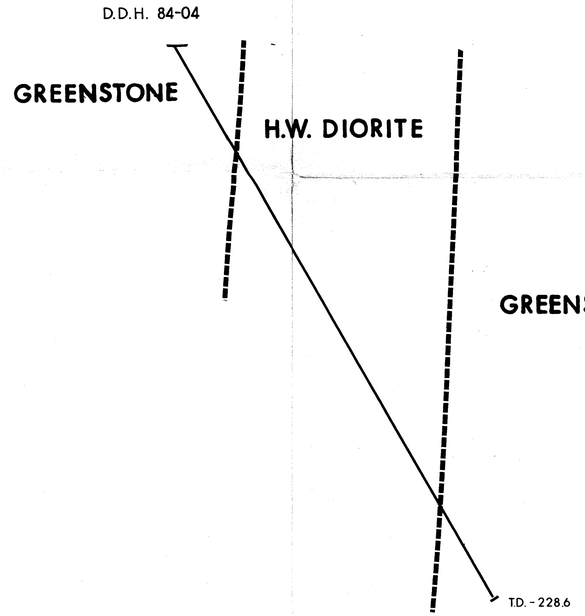
WAYSIDE PROJECT

DRILL HOLE SECTION 84-03 → 80-S8

AUTO DRAFT | DRAWING NUMBER FIG. 6C | REV. △




D.D.H. 84-05




D.D.H. 84-04

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

| NOTES | NUMBER | REFERENCE DRAWINGS | No. | REVISIONS | DATE | BY | CH'D. | APP'D |
|---|---|---|---|---|---|---|---|---|
| | | | | | | | | |

| | ENG. IN CHARGE | PROJECT | DATE |
|---|---|---|---|
| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. 85
SCALE: 1:1000
DESIGN:
DRAWN: J.W.K.
CHECKED:
APPROVED: RJM

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AMAZON PETROLEUM CORP

WAYSIDE PROJECT

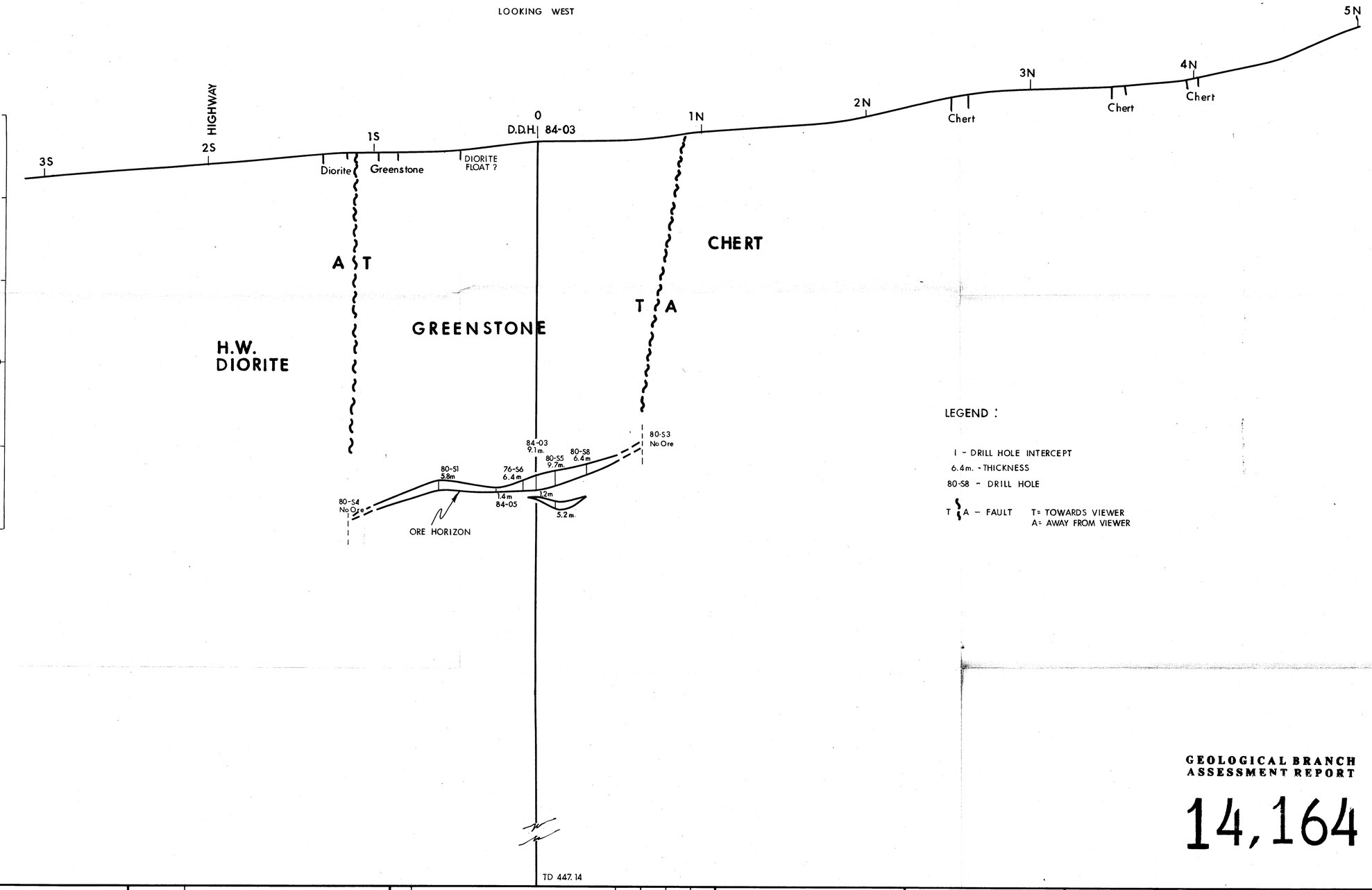
DRILL HOLE SECTIONS 84-05 & 84-04

LOOKING NORTH

AUTO DRAFT | DRAWING NUMBER FIG. 6D | REV. △

# LONGITUDINAL SECTION ALONG BASELINE

LOOKING WEST




LEGEND :

I - DRILL HOLE INTERCEPT
6.4m. - THICKNESS
80-S8 - DRILL HOLE

T ⟆ A – FAULT T= TOWARDS VIEWER
A= AWAY FROM VIEWER

GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

| NOTES | NUMBER | REFERENCE DRAWINGS |
|---|---|---|
| | | |

| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
|---|---|---|---|---|---|
| | | | | | |

| | ENG. IN CHARGE | PROJECT | DATE |
|---|---|---|---|
| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. 85
SCALE: 1: 1200
DESIGN:
DRAWN: J.W.K.,
CHECKED:
APPROVED: RAM

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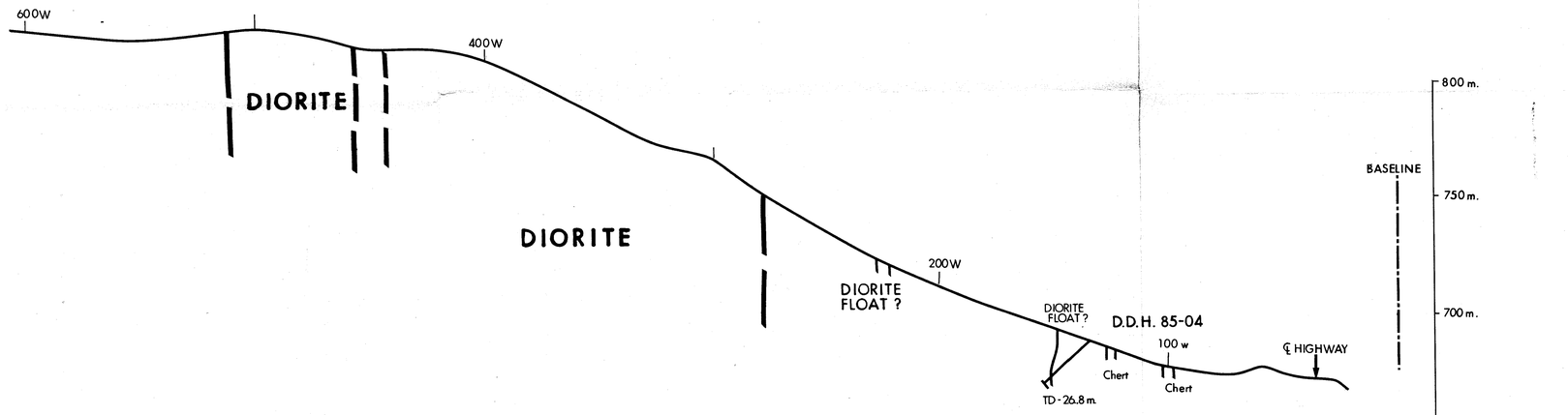
AMAZON PETROLEUM CORP

WAYSIDE PROJECT

LONGITUDINAL SECTION
LOOKING WEST ALONG BASELINE

AUTO DRAFT | DRAWING NUMBER FIG. 7A | REV. △

# SECTION 3S







GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

| NOTES | NUMBER | REFERENCE DRAWINGS |
|---|---|---|
| | | |

| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
|---|---|---|---|---|---|
| | | | | | |

| | ENG. IN CHARGE | PROJECT | DATE |
|---|---|---|---|
| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. 85
SCALE: 1:1200
DESIGN:
DRAWN: J.W.K.
CHECKED:
APPROVED:

Morris Geological Co. Ltd.

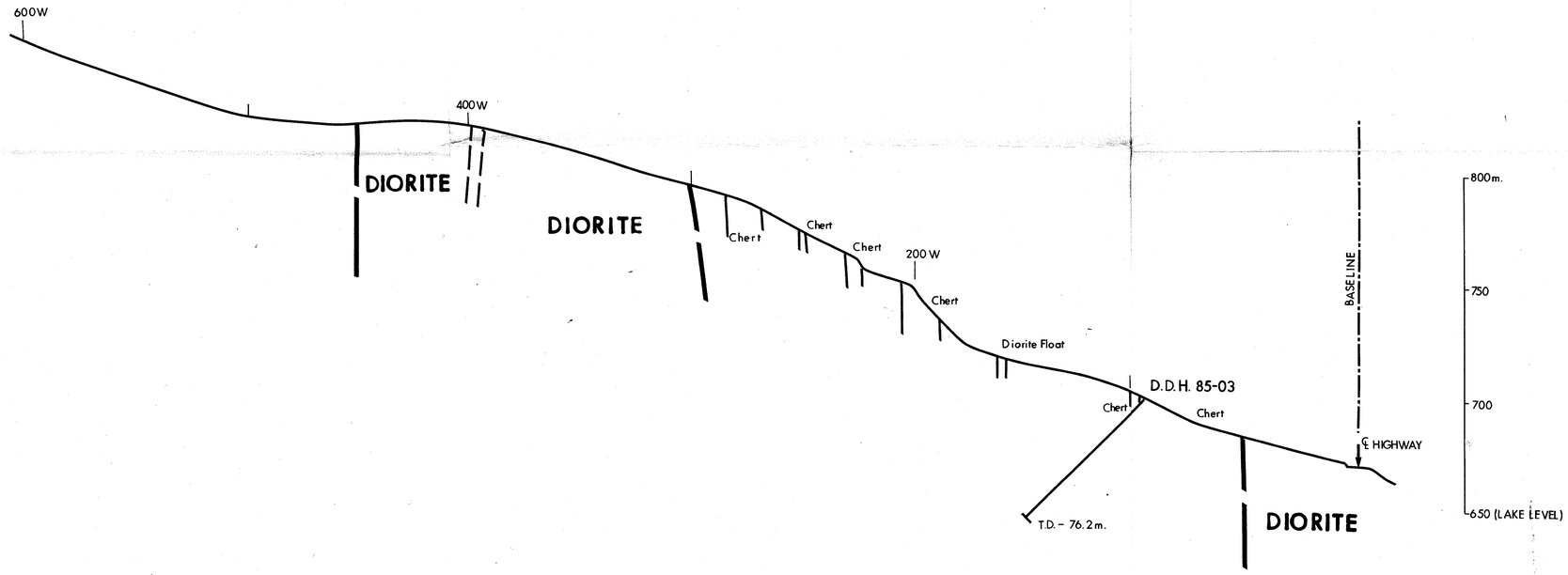
AMAZON PETROLEUM CORP

WAYSIDE PROJECT

SECTION 3S

AUTO DRAFT | DRAWING NUMBER FIG. 7B | REV. △

# SECTION 2S




GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

| NOTES | NUMBER | REFERENCE DRAWINGS |
|---|---|---|
| | | |

| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
|---|---|---|---|---|---|
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| | ENG. IN CHARGE | PROJECT | DATE |
|---|---|---|---|
| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. 85
SCALE: 1:1200
DESIGN:
DRAWN: J.W.K.
CHECKED:
APPROVED:

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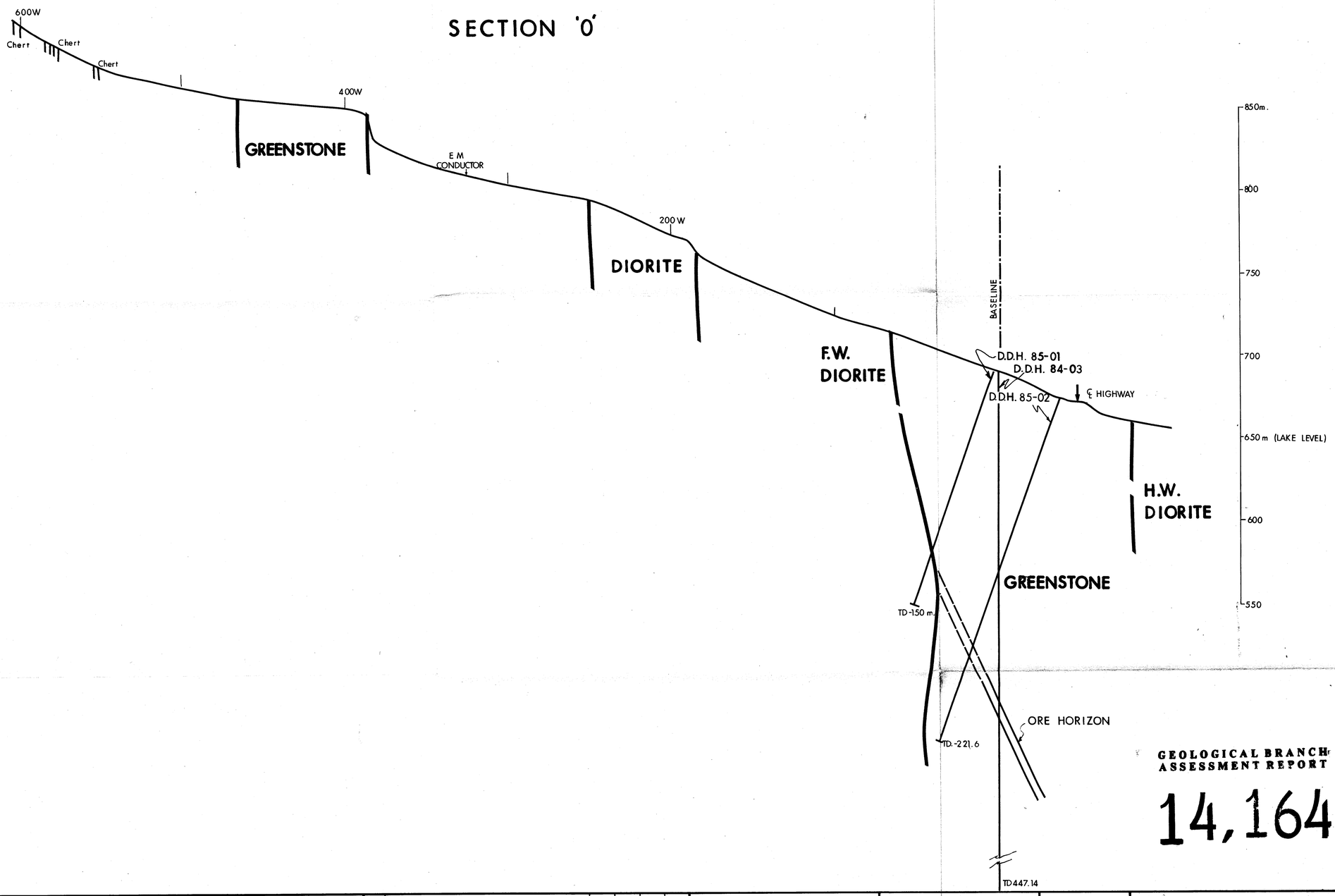
AMAZON PETROLEUM CORP

WAYSIDE PROJECT

SECTION 2S

AUTO DRAFT | DRAWING NUMBER FIG. 7C | REV. △

# SECTION '0'




GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

| NOTES | NUMBER | REFERENCE DRAWINGS |
|---|---|---|
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| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
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| FABRICATION | | | |
| CONSTRUCTION | | | |

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DRAWN: J.W.K.
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AMAZON PETROLEUM CORP

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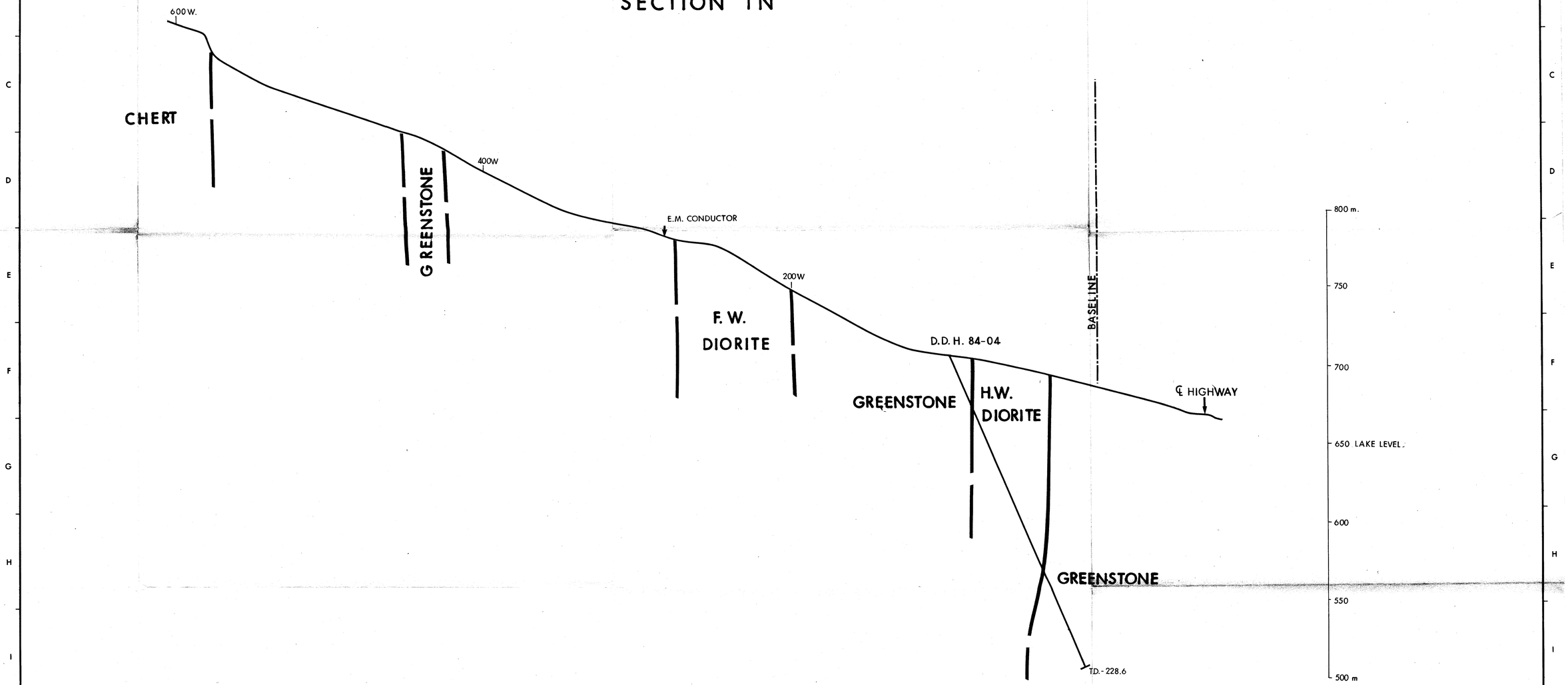
SECTION '0'

AUTO DRAFT | DRAWING NUMBER FIG. 7D | REV.

# SECTION 1N




GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

| NOTES | NUMBER | REFERENCE DRAWINGS |
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| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
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| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. 85
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DRAWN: JWK
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APPROVED: RJM

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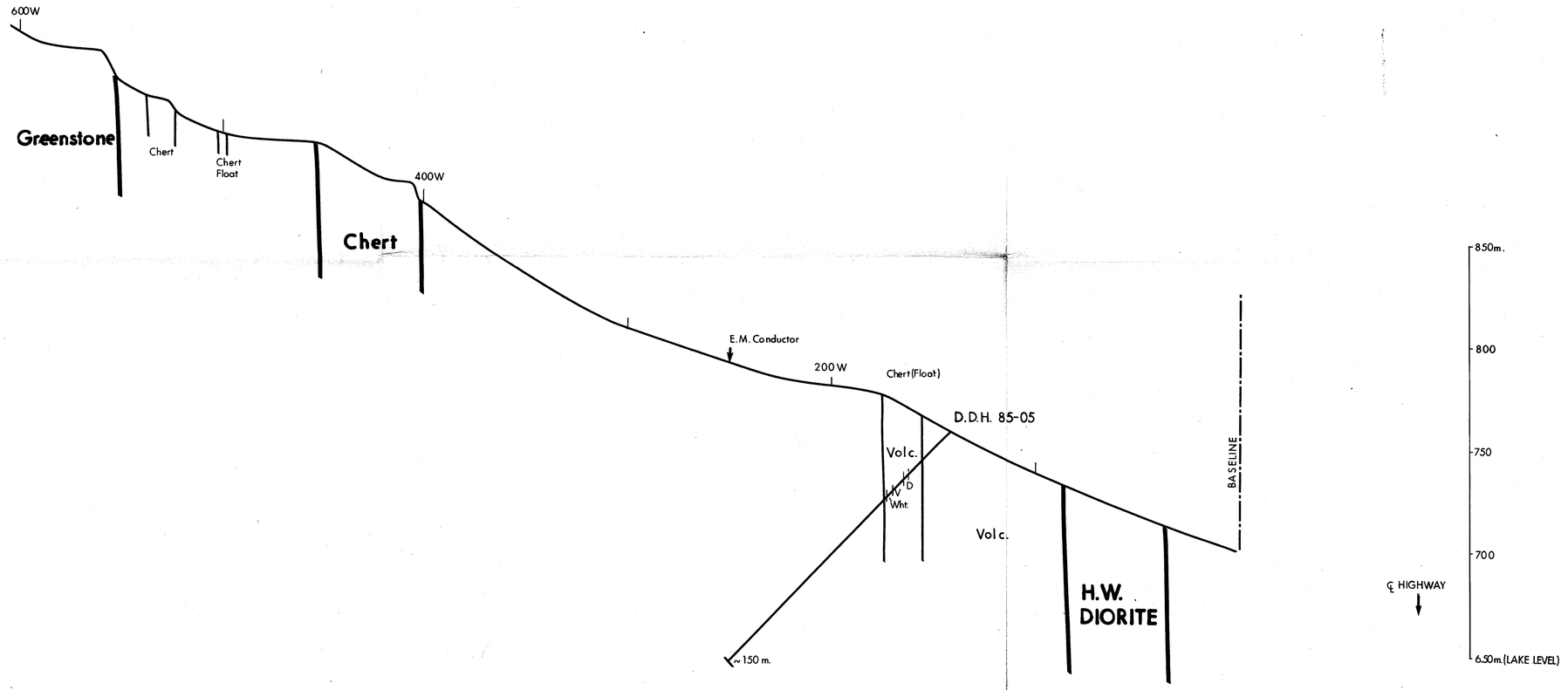
AMAZON PETROLEUM CORP

WAYSIDE PROJECT

SECTION 1N

AUTO DRAFT | DRAWING NUMBER FIG. 7E | REV. △

# SECTION 2N




GEOLOGICAL BRANCH
ASSESSMENT REPORT

14,164

| NOTES | NUMBER | REFERENCE DRAWINGS | No. | REVISIONS | DATE | BY | CH'D. | APP'D |
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| | ENG. IN CHARGE | PROJECT | DATE |
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| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

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DESIGN:
DRAWN: J.W.K.
CHECKED:
APPROVED: RAM.

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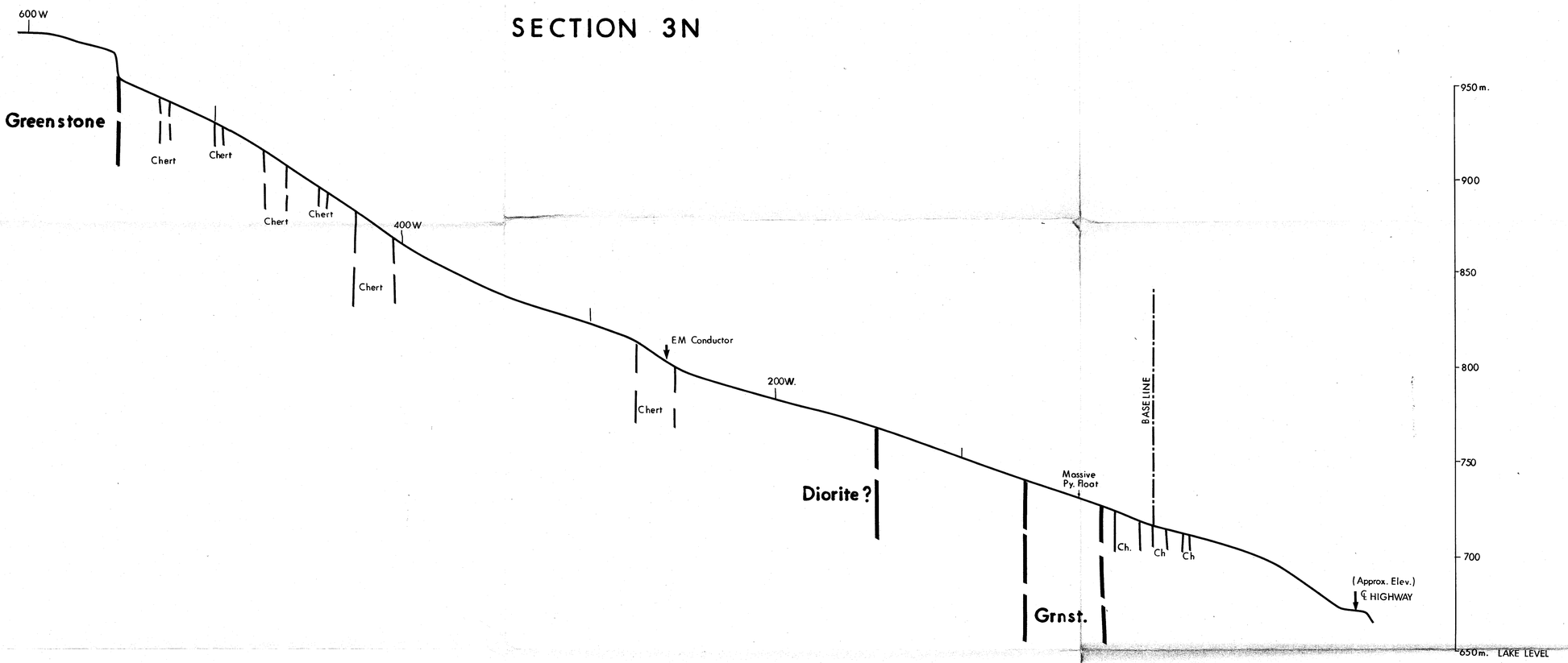
AMAZON PETROLEUM CORP.

WAYSIDE PROJECT

SECTION 2N

AUTO DRAFT | DRAWING NUMBER FIG. 7F | REV. △

# SECTION 3N






| NOTES | NUMBER | REFERENCE DRAWINGS |
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| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
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| | ENG. IN CHARGE | PROJECT | DATE |
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| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG. '85
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DRAWN: J.W.K.
CHECKED:
APPROVED: Rgm.

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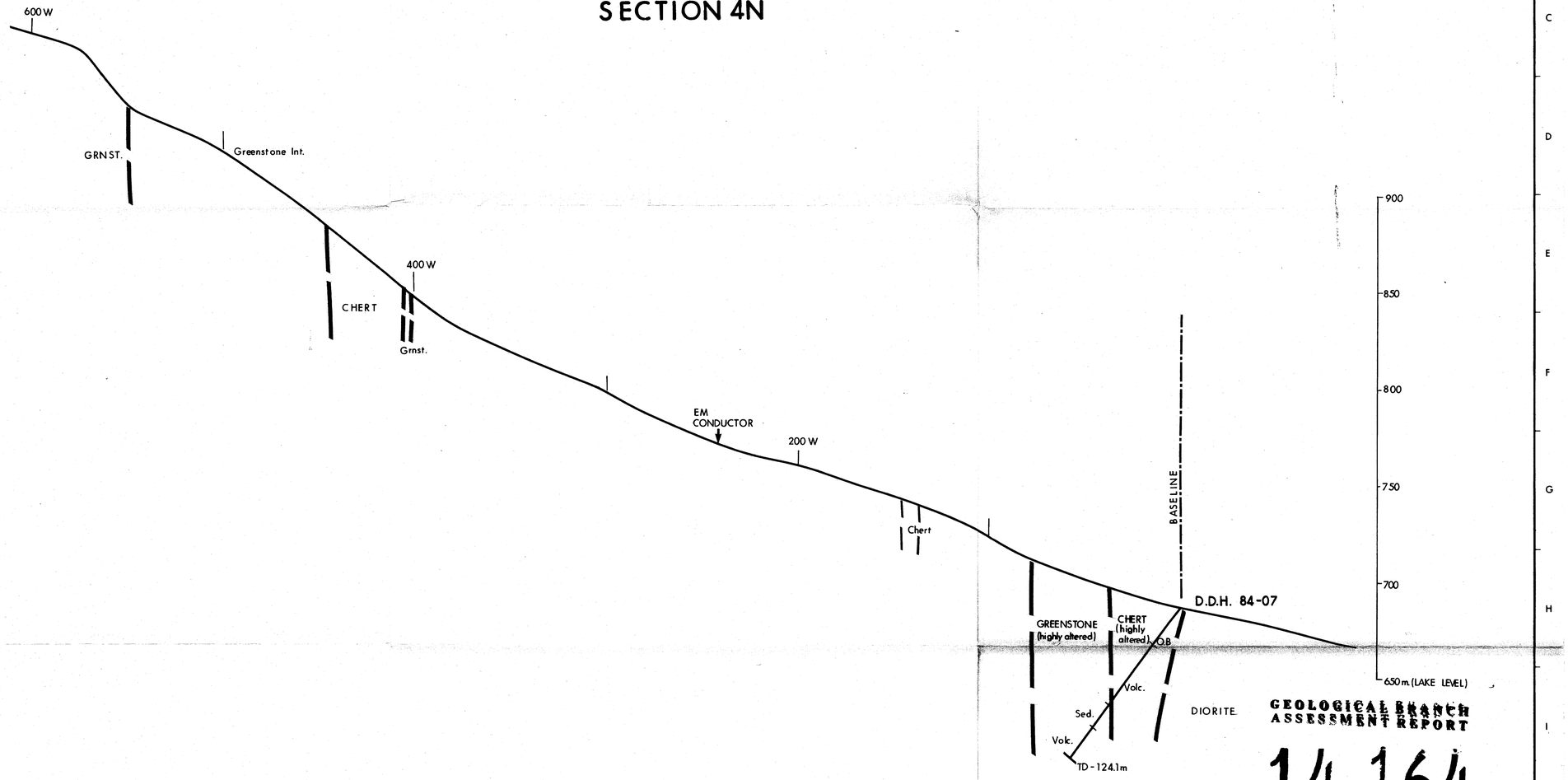
AMAZON PETROLEUM CORP

WAYSIDE PROJECT

SECTION 3N

AUTO DRAFT | DRAWING NUMBER FIG. 7G | REV. △

# SECTION 4N






| NOTES | NUMBER | REFERENCE DRAWINGS |
|---|---|---|
| | | |

| No. | REVISIONS | DATE | BY | CH'D. | APP'D |
|---|---|---|---|---|---|
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METRIC

THIRD ANGLE PROJECTION

ALL DIMENSIONS SHOWN ON THIS DRAWING ARE IN _____ UNLESS OTHERWISE SPECIFIED

| RELEASED ONLY FOR | | | |
|---|---|---|---|
| | ENG. IN CHARGE | PROJECT ENG. | DATE |
| CHECKING | | | |
| PRELIMINARY | | | |
| BIDDING | | | |
| FABRICATION | | | |
| CONSTRUCTION | | | |

DATE: AUG '85
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DESIGN:
DRAWN: J.W.K.
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APPROVED:

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AMAZON PETROLEUM CORP

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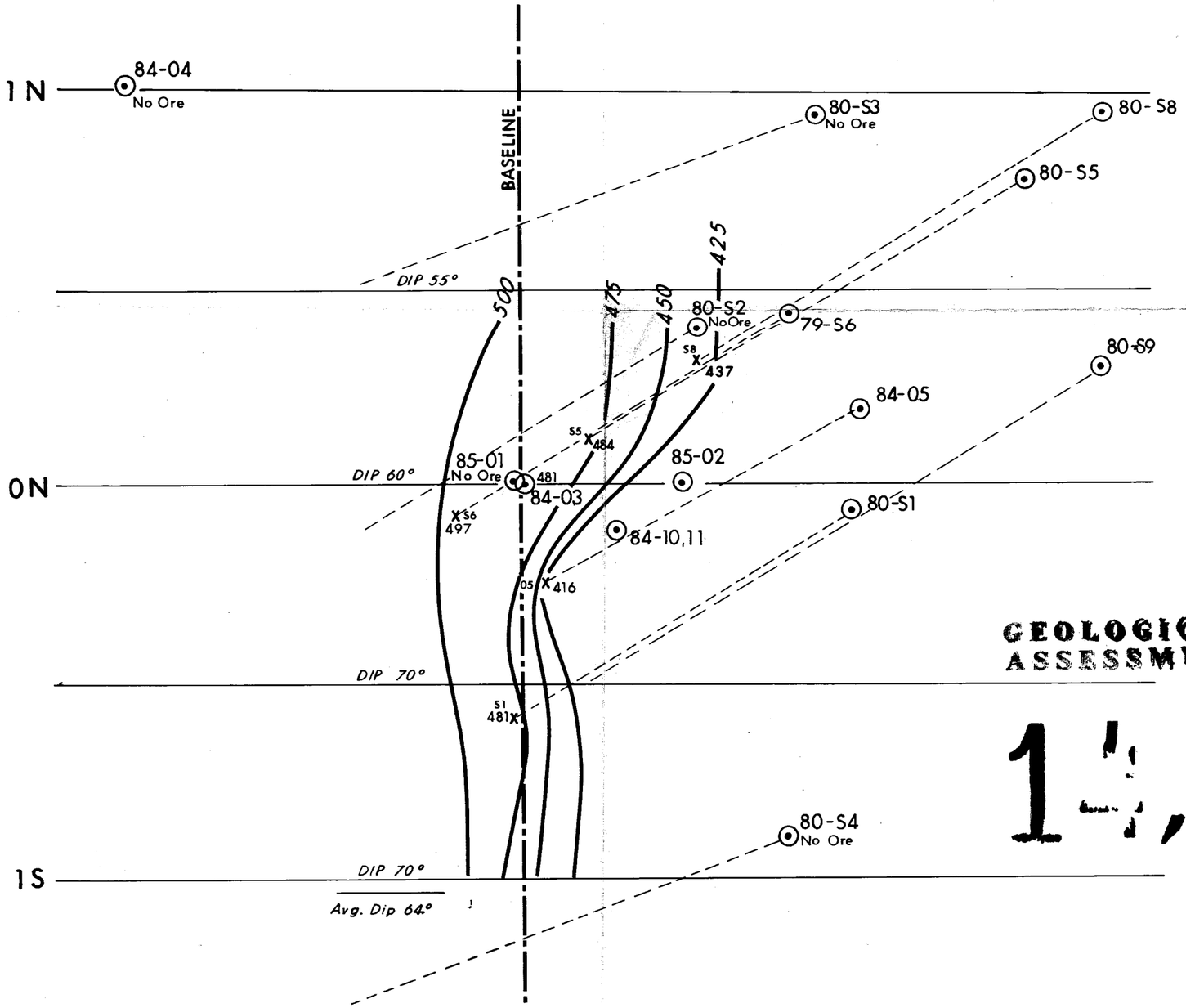
SECTION 4N

AUTO DRAFT | DRAWING NUMBER FIG. 7H | REV. △




LEGEND:

80 - S8 — DRILL HOLE COLLAR

S8 X 416 — HOLE NO. / INTERCEPT / ELEVATION

500 — STRUCTURE CONTOURS, METERS ABOVE SEA LEVEL

LAKE LEVEL IS 650 m



Morris Geological Co. Ltd.

AMAZON PETROLEUM CORP.

# WAYSIDE PROJECT

## STRUCTURE CONTOURS ORE HORIZON

| | | |
|---|---|---|
| DRAWN BY: JWK | DATE: AUG. '85 | FIG. 8 |
| AUTHOR: R.J. MORRIS | SCALE: 1:1200 | |
| RJM | | |