

86-388-14873

07/87

Alberni M.D.

NTS: 92 F2/E

49° 05'

124° 41'

ASSESSMENT REPORT  
ON  
SOIL GEOCHEMICAL SAMPLING  
OF THE  
T-2 GRID, TOBY 1 CLAIM  
C & R PROJECT  
BRITISH COLUMBIA  
BY  
A.M.S. CLARK  
GEOLOGIST  
IMPERIAL METALS CORPORATION  
DECEMBER 1985

FILMED

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

14,873

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SUMMARY

Soil sampling indicated localization of weak copper anomalies to the western and southern parts of the grid, but no localization of other metal anomalies.

The grid was not laid over the full planned extent because of weather problems, and should be extended to the southeast.

## INTRODUCTION

### Objectives

Contour soil sampling in 1984 (Clark, 1984a) of the adjacent Toby 2 claim indicated the north side of the boundary creek (a fault?) is anomalous in gold and copper. This has now been followed up with a grid and further soil sampling to give more definition to the soil anomalies. The original plan was to test the entire northern slope with a grid extending through the Toby 2 claim, but because of adverse weather the program had to be halted early.

### Location

The Toby 1 claim is situated between Museum and Corrigan Creeks, about 17 km south south-east of Port Alberni, and 11 kms due east of Alberni Inlet (Figures 1 & 2).

### Property

The property consists of the Toby 1 and Toby 2 claims of 16 + 16 units (Figure 3), record nos. 1824 and 1825, recorded on August 4th, 1983 and owned by Imperial Metals Corporation.

### Access

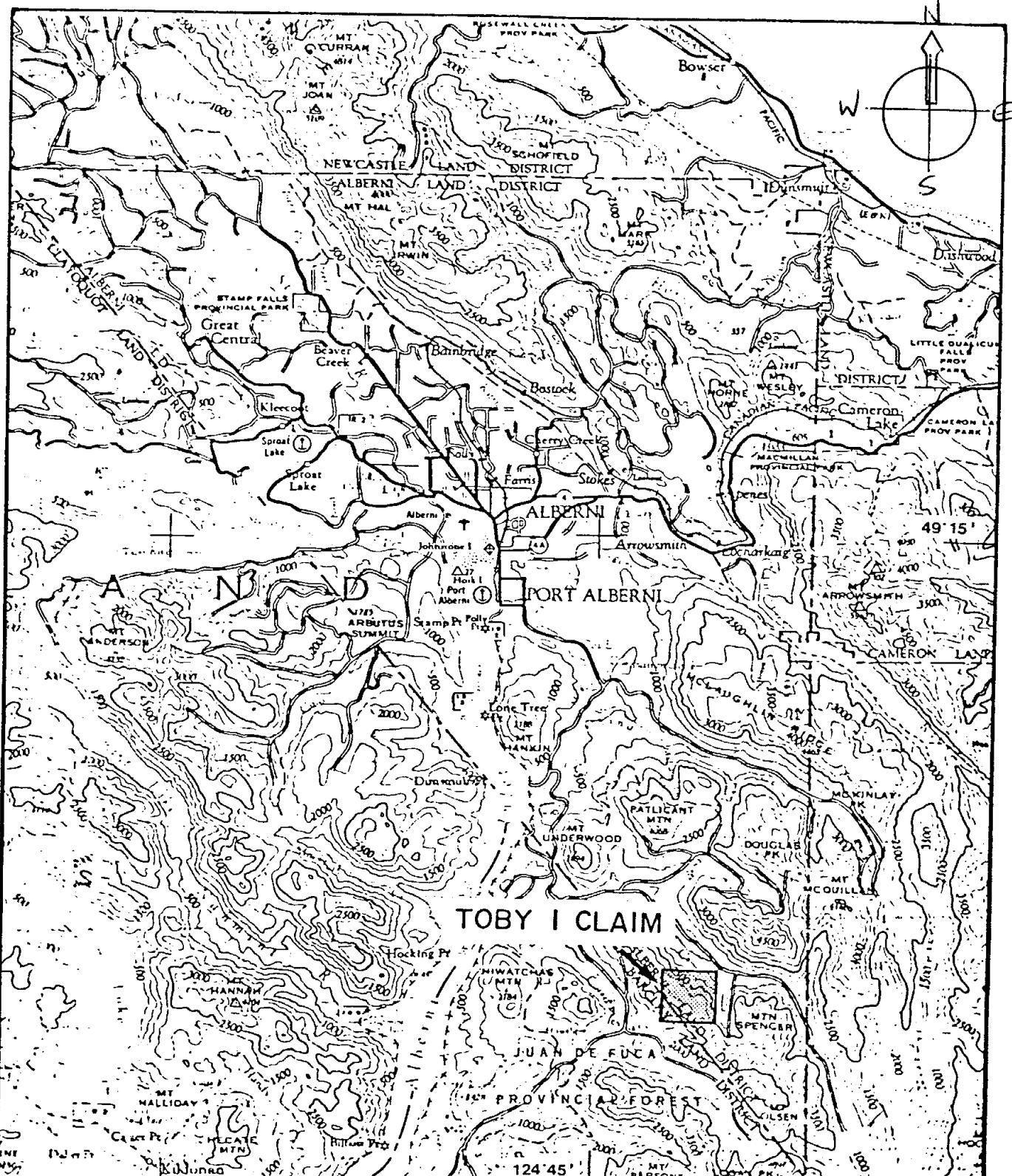
Access is by road south from Port Alberni along Corrigan Creek, then by logging road east of the Pool Creek Valley.

### Operations

Fieldwork was undertaken from Port Alberni, on November 10th to November 14th, 1985.

Physiography

Topography is steep and heavily wooded except where logging has been completed. The claims overlie the crest of a ridge and down both northeast and southwest flanks from 1040m down to 300m above sea level.



IMPERIAL METALS CORPORATION  
TOBY I

FIGURE 1

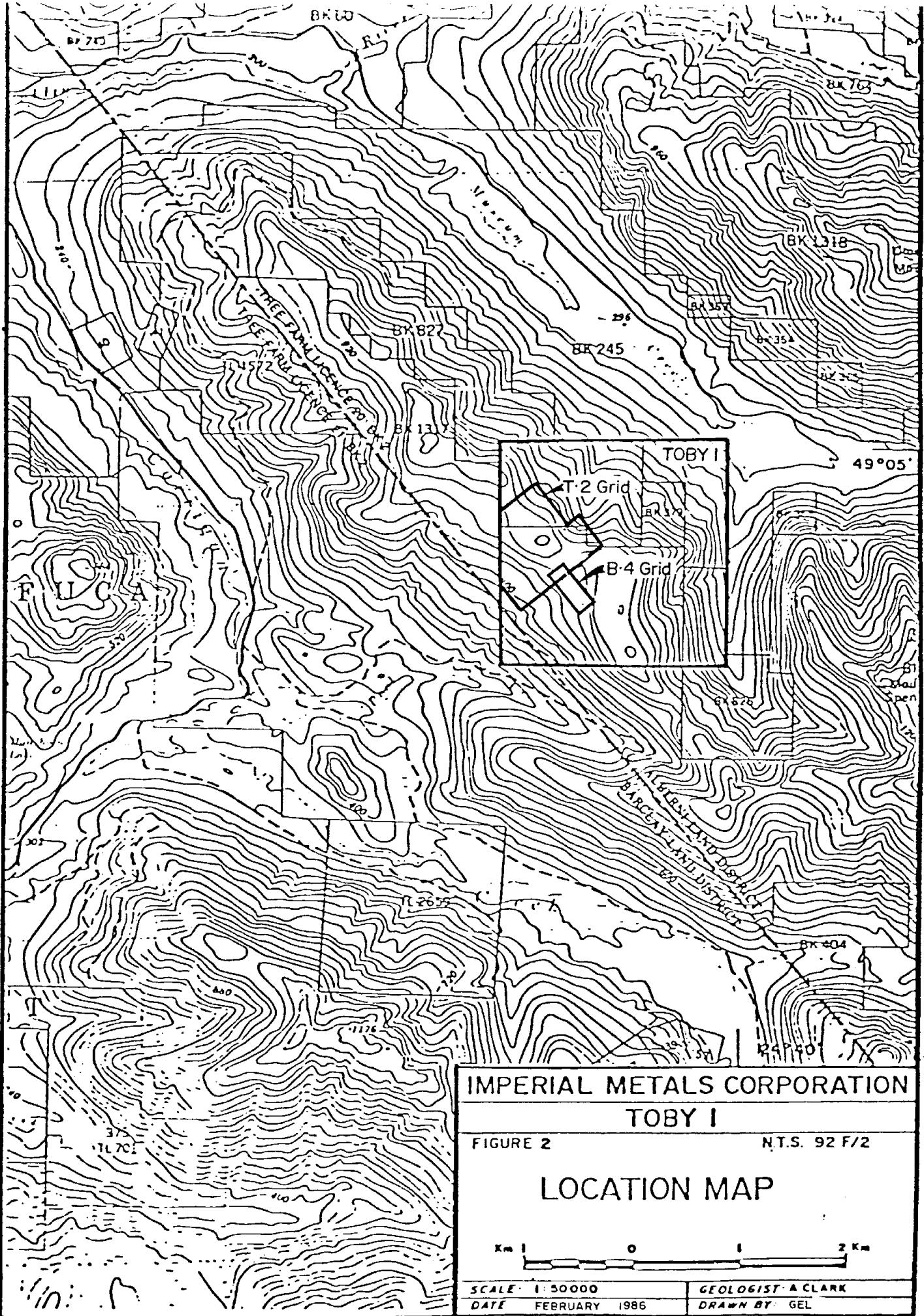
N.T.S. 92F

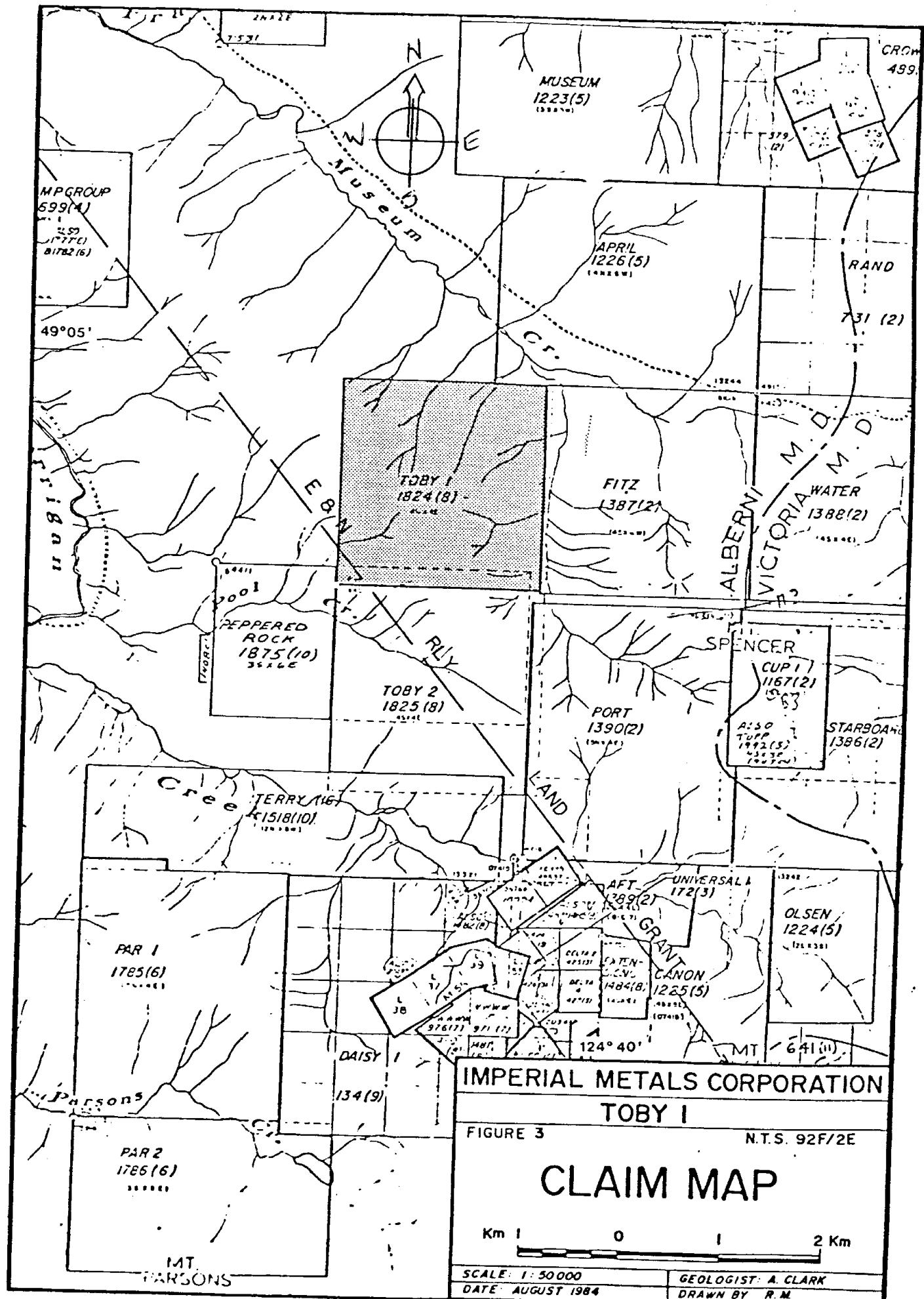
TOPOGRAPHIC MAP

Km 5 0 5 10 Km

SCALE: 1:250 000  
DATE AUGUST 1984

GEOLOGIST: A. CLARK  
DRAWN BY: R.M.





PREVIOUS WORK

Published

In 1968 Muller and Carson published a report on the geology and mineral deposits of Alberni map area, which includes the area of the Toby 1 claim.

Assessment

The only previous assessment work known is work by Imperial Metals in 1984 (Clark 1984a, 1984b & 1985) consisting of soil sampling, magnetometer survey and geological mapping of a small grid.

GEOLOGY

According to Muller and Carson (1968) the property is underlain by Upper Triassic Karmutsen basaltic volcanics intruded by the Jurassic Island intrusions of granodioritic to quartz dioritic composition.

### SAMPLE COLLECTION AND ANALYSIS

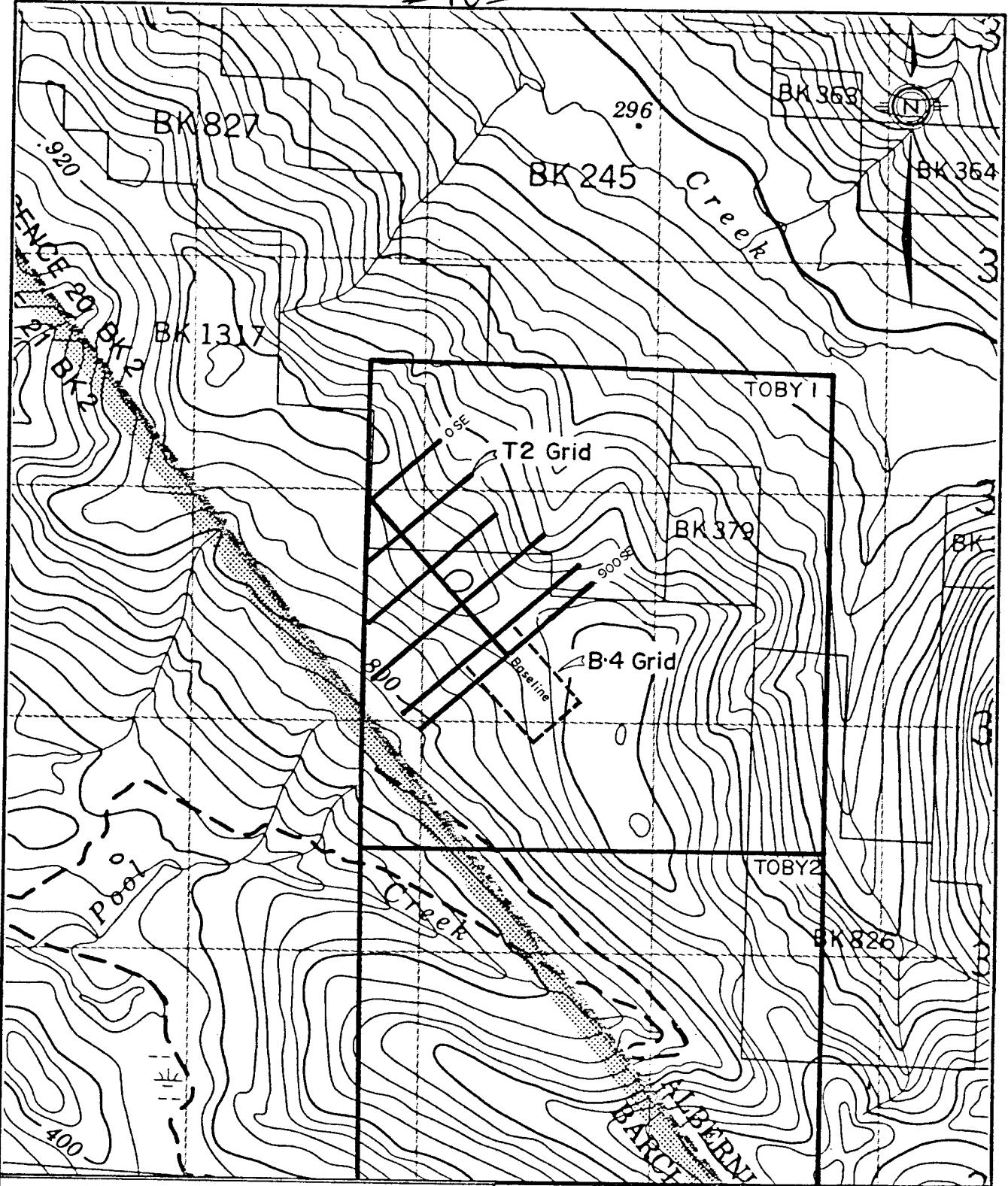
Samples of soil were collected from the B-horizon where this could be distinguished. The B-horizon was taken to be the first reddish soil horizon below the grey surficial horizon of soil. For the most part because of the steep terrain no soil horizons, as such, were developed, and soils had to be collected from "pore" spaces between boulders, at depths from surface (excluding the humic horizon) to about 40 cms depth.

Analysis was by induction coupled plasma method for 30 elements, and by atomic absorption for gold. The method employed by the laboratory and the elements and results are given in Appendix 1. The elements considered of significance in this program (with their assumed anomalous thresholds) are:

<u>Element</u>	<u>Threshold</u>
Copper	50 ppm
Zinc	100 ppm
Silver	1 ppm
Arsenic	12 ppm
Gold (AA)	25 ppb

The correlation, coefficients for all the elements, except for the positive correlation of arsenic and silver which is unusual in this instance as arsenic and gold do not correlate.

The T2-grid was originally intended to extend the previous B-4 grid (Clark, 1984b & 1985) over most of that hill-side (Figure 4). However, the old B-4 grid had been destroyed by logging, and onset of bad weather prevented the full extension of the T2 grid: the results of the sampling indicate weak anomalous copper values in the western and southern parts of the grid (Figure), but other elements show no localization of anomalous values.



IMPERIAL METALS CORPORATION

TOBY I

FIGURE

N.T.S. 92/F2

LOCATION MAP  
(T-2 Grid)

500 0 500 1000 metres

SCALE 1 : 25,000  
DATE FEBRUARY 1986

GEOLIST A. CLARK  
DRAWN BY GEL

CONCLUSION AND RECOMMENDATIONS

The grid should be extended to the southeast across the creek-gully, to overlie the previously located (weakly) anomalous base-metal soil values (north of the creek) and gold values (south of the creek). In addition further geological investigations and prospecting should be undertaken to determine the rock-types up-hill from the anomalous areas. The unusual Ag:As correlation without Au:As correlation should be checked where possible in rock samples.

REFERENCES

Muller, J.E. and Carson, D.J.T., 1968. Geology and Mineral Deposits of Alberni Map - Area, British Columbia (92F). Geol. Surv. Canada Paper, 68 - 50.

Clark, A.M.S., 1984a. Assessment Report on Soil Geochemical Sampling of the Toby 2 claim, C & R Project, B.C., B.C. Assessment Report Files.

Clark, A.M.S., 1984b. Assessment Report on Soil Geochemical Sampling of the B4-Grid, Toby 1 claim, C & R project, B.C. B.C. Assessment Report Files.

Clark, A.M.S., 1985. Geological Mapping and Magnetometer Survey of the B-4 Grid, Toby 1 claim, C & R Project, B.C. B.C. Assessment Report Files.

CERTIFICATE

I, Anthony Miles Stapleton Clark, geologist, residing at 2988 Fleet Street, in the Municipality of Coquitlam, Province of British Columbia, hereby certify that:

1. I received a Bachelor of Science degree in geology from the University of Cape Town, Cape Town, South Africa, in 1963, and a Doctor of Philosophy degree in geology from the Memorial University of Newfoundland, St. John's, Newfoundland in 1974.
2. I have been practising my profession as an exploration geologist since 1963.
3. I am a registered Professional Geologist of the Association of Professional Engineers, Geologists and Geophysicists of Alberta.
4. I am a Fellow of the Geological Association of Canada and a Member of the Society of Economic Geologists.
5. I am employed by Imperial Metals Corporation of 800 - 601 W . Hastings Street, in the city of Vancouver, Province of British Columbia.
6. The work described in this report was undertaken under my direct supervision.

\_\_\_\_ day of \_\_\_\_\_, 1986

Vancouver, British Columbia

A.M.S. Clark, Ph.D., FGAC, MSEG  
Geologist

APPENDIX 1  
Soil Sample Descriptions

CG 2  
a: Tz Soils

. list northeast,northwest,orthwest,soil

00001	-450	-50 medium brown silt
00002	-425	-50 medium brown silt
00003	-400	-50 medium brown silt
00004	-375	-50 dark brown silt, 30% humic
00005	-350	-50 medium brown silt
00006	-325	-50 medium brown silt
00007	-300	-50 medium brown silt
00008	-275	-50 medium brown silt
00009	-250	-50 medium brown silt
00010	-225	-50 red silt
00011	-200	-50 red silt
00012	-175	-50 red silt
00013	-150	-50 medium brown silt
00014	-125	-50 medium brown silt
00015	-100	-50 medium brown silt
00016	-75	-50 medium brown silt
00017	-50	-50 medium brown silt
00018	-25	-50 medium brown silt
00019	0	-50 medium brown silt
00020	-450	-25 medium brown silt
00021	-400	-25 medium brown silt
00022	-200	-25 medium brown silt
00023	0	-25 dark brown silt, 20% humic
00024	-800	0 medium brown silt, 10% humic
00025	-775	0 medium brown silt
00026	-750	0 medium brown silt
00027	-725	0 grey silt
00028	-700	0 medium brown silt
00029	-675	0 medium brown silt
00030	-650	0 medium brown silt
00031	-625	0 medium brown silt
00032	-600	0 medium brown silt
00033	-575	0 medium brown silt
00034	-550	0 medium brown silt, 5% humic
00035	-525	0 medium brown silt
00036	-500	0 medium brown silt
00037	-475	0 medium brown silt
00038	-450	0 medium brown silt
00039	-400	0 medium brown silt
00040	-200	0 medium brown silt
00041	0	0 dark brown silt, 10% humic
00042	-800	25 medium brown silt
00043	-600	25 medium brown silt
00044	-400	25 medium brown silt
00045	-200	25 medium brown silt
00046	0	25 medium brown silt
00047	-800	50 medium brown silt
00048	-600	50 medium brown silt
00049	-400	50 medium brown silt
00050	-200	50 medium brown silt
00051	0	50 medium brown silt
00052	-800	75 medium brown silt
00053	-600	75 medium brown silt
00054	-400	75 medium brown silt
00055	-200	75 red silt
00056	0	75 medium brown silt
00057	-800	100 medium brown silt
00058	-600	100 medium brown silt
00059	-400	100 no sample - lake
00060	-200	100 medium brown silt
00061	0	100 medium brown silt
00062	-800	125 medium brown silt

		125 medium brown silt
00064	-600	125 medium brown silt, 15% humic
00065	-400	125 medium brown silt
00066	-200	125 medium brown silt, 10% humic
00067	0	125 medium brown silt
00068	-800	150 dark brown silt, 20% humic
00069	-800	150 medium brown silt
00070	-600	150 medium brown silt
00071	-400	150 medium brown silt
00072	-200	150 medium brown silt
00073	0	150 medium brown silt
00074	-800	175 medium brown silt
00075	-800	175 red silt
00076	-600	175 medium brown silt
00077	-400	175 black 100% humic - swamp
00078	-200	175 medium brown silt
00079	0	175 medium brown silt
00080	-800	200 medium brown silt
00081	-600	200 medium brown silt
00082	-400	200 red silt
00083	-200	200 medium brown silt
00084	0	200 dark brown silt, 15% humic
00085	-800	225 medium brown silt
00086	-600	225 medium brown silt
00087	-400	225 medium brown clay
00088	-200	225 medium brown silt
00089	0	225 medium brown silt
00090	-800	250 medium brown silt, 10% humic
00091	-600	250 medium brown silt
00092	-400	250 medium brown silt
00093	-200	250 red silt
00094	0	250 medium brown silt
00095	-800	275 medium brown silt, 10% humic
00096	-600	275 medium brown silt
00097	-400	275 medium brown silt
00098	-200	275 medium brown silt
00099	0	275 medium brown silt
00100	-800	300 medium brown silt
00101	-600	300 medium brown silt
00102	-400	300 medium brown silt
00103	-200	300 medium brown silt
00104	0	300 red silt
00105	-800	325 medium brown silt
00106	-600	325 medium brown silt
00107	-400	325 medium brown silt
00108	-200	325 medium brown silt
00109	0	325 red silt
00110	-800	350 medium brown silt
00111	-600	350 medium brown silt
00112	-400	350 orange silt
00113	-200	350 dark brown silt, 15% humic
00114	0	350 red silt
00115	-800	375 medium brown silt
00116	-600	375 red silt
00117	-400	375 medium brown silt, 10% humic
00118	-200	375 drk brown silt, 10% humic
00119	0	375 medium brown silt
00120	-800	400 medium brown silt
00121	-600	400 medium brown silt
00122	-200	400 dark brown silt, 20% humic
00123	0	400 medium brown silt
00124	-800	425 medium brown silt
00125	-600	425 medium brown silt
00126	-200	425 red silt
00127	0	425 medium brown silt
00128	-800	450 medium brown silt

00130 -200 450 red silt  
00131 0 450 medium brown silt  
00132 -800 475 medium brown silt  
00133 -600 475 medium brown silt  
00134 -200 475 red silt  
00135 0 475 medium brown silt  
00136 -800 500 medium brown silt  
00137 -200 500 red silt  
00138 0 500 red silt  
• set print off

APPENDIX 2

Analytical Results

CER Project

Tob-Z Grid

ACME ANALYTICAL LABORATORIES LTD.

852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6

PHONE 253-3158 DATA LINE 251-1011

## GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR Mn,Fe,Ca,P,Cr,Mg,Ba,Ti,B,Al,Na,K,W,Si,Zr,CE,Sn,Y,Nb AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: SOIL Au ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 21 1985 DATE REPORT MAILED: Dec. 3/85 ASSAYER: *T. Saundry* DEAN TOYE OR TOM SAUNDRY. CERTIFIED B.C. ASSAYER

SAMPLE#	IMPERIAL METALS												PROJECT - 4202 FILE # 85-3163												PAGE 1						
	Mo	Cu	Pb	Zn	Aq	Mn	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	L4	Cr	Mg	Ba	Tl	B	Al	Na	K	N	Au
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	ND	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPB
T2 OSE 500NE	1	62	12	102	.7	22	17	307	1.96	2	5	ND	5	8	1	2	2	46	.21	.06	14	208	.23	21	.07	5	11.55	.01	.02	1	1
T2 OSE 475NE	1	19	5	30	.4	5	2	83	2.69	2	5	ND	1	13	1	4	2	129	.14	.04	9	13	.09	35	.15	3	1.60	.01	.02	2	1
T2 OSE 450NE	1	12	2	24	.3	3	1	115	4.18	2	5	ND	1	12	1	2	2	218	.15	.03	7	22	.15	11	.39	6	1.22	.01	.02	2	3
T2 OSE 425NE	1	8	9	38	.3	4	1	155	3.92	2	5	ND	1	14	1	2	2	167	.19	.05	7	18	.16	13	.24	6	.96	.01	.03	2	1
T2 OSE 400NE	1	10	2	34	.3	4	2	116	3.55	3	5	ND	2	15	1	3	2	215	.21	.03	6	17	.14	12	.37	6	.90	.02	.02	1	2
T2 OSE 375NE	1	10	7	30	.2	7	2	148	4.69	2	5	ND	1	20	1	2	2	176	.30	.05	7	21	.23	19	.36	5	1.09	.02	.03	1	2
T2 OSE 350NE	1	11	6	22	.1	4	1	112	5.09	2	5	ND	2	13	1	2	2	187	.15	.04	6	19	.21	10	.31	4	1.46	.01	.02	1	1
T2 OSE 325NE	1	11	11	30	.3	5	2	175	4.83	3	5	ND	2	16	1	2	2	204	.22	.07	9	24	.26	15	.27	6	1.40	.01	.02	3	5
T2 OSE 300NE	1	16	5	42	.3	10	5	351	5.45	2	7	ND	4	27	1	3	5	192	.26	.11	6	39	.53	27	.52	5	1.90	.01	.02	1	6
T2 OSE 275NE	1	5	5	31	.3	6	3	195	3.78	3	5	ND	2	23	1	2	2	158	.31	.07	4	21	.33	8	.34	3	.97	.02	.03	1	23
T2 OSE 250NE	1	20	9	22	.2	4	1	114	4.81	2	5	ND	2	16	1	3	2	172	.22	.06	5	21	.21	13	.29	2	1.45	.01	.02	1	14
T2 OSE 225NE	1	7	6	45	.2	6	3	180	1.78	3	5	ND	2	16	1	6	2	56	.26	.07	5	13	.25	20	.08	2	1.06	.02	.06	1	22
T2 OSE 200NE	1	7	8	50	.2	2	1	99	.48	2	5	ND	1	17	1	2	2	31	.46	.08	2	6	.08	27	.09	5	.28	.01	.07	1	44
T2 OSE 175NE	1	14	5	27	.2	7	2	208	5.84	2	5	ND	2	21	1	2	2	249	.37	.08	6	28	.27	15	.52	2	1.11	.02	.03	1	12
T2 OSE 150NE	1	10	8	41	.2	15	3	195	3.32	2	5	ND	1	29	1	2	2	177	.57	.06	4	28	.35	9	.45	4	.72	.04	.04	1	5
T2 OSE 125NE	1	13	10	54	.3	16	4	251	1.57	4	5	ND	1	25	1	2	2	54	.67	.05	3	50	.52	21	.24	5	.73	.03	.04	1	4
T2 OSE 100NE	1	27	9	47	.3	13	4	259	4.45	2	5	ND	2	20	1	3	2	138	.42	.12	4	49	.50	22	.24	5	1.38	.02	.04	2	6
T2 OSE 75NE	1	6	10	27	.2	3	1	95	1.79	2	5	ND	1	13	1	2	2	134	.22	.03	4	14	.09	8	.28	3	.40	.01	.02	1	9
T2 OSE 50NE	1	50	7	46	.3	13	5	190	3.71	2	5	ND	1	22	1	2	2	104	.27	.10	7	39	.38	31	.24	4	1.61	.01	.05	1	4
T2 OSE 25NE	1	7	10	24	.2	7	2	153	3.46	2	5	ND	1	14	1	3	3	222	.29	.06	4	29	.22	5	.49	4	.61	.01	.02	1	9
T2 OSE BLO	1	14	5	53	.2	43	13	322	5.85	2	5	ND	2	6	1	2	2	188	.07	.05	2	141	1.75	9	.02	3	3.15	.01	.02	1	7
T2 OSE 0SW	1	24	7	29	.2	5	2	106	1.18	2	5	ND	1	21	1	2	2	82	.25	.04	4	18	.08	24	.28	2	.67	.01	.03	2	6
T2 OSE 25SW	1	5	5	89	.2	3	1	432	.23	3	5	ND	1	7	1	2	2	6	.24	.11	2	5	.07	9	.01	4	.20	.02	.10	1	4
T2 25SE BLO 50SW	1	29	12	65	.4	21	7	581	2.41	2	5	ND	2	24	1	2	2	82	.47	.11	4	42	.60	23	.26	4	1.23	.02	.07	1	6
T2 50SE BLO 50SW	1	10	5	32	.2	6	2	165	3.21	3	5	ND	1	19	1	2	2	204	.32	.07	5	33	.28	8	.44	4	1.03	.01	.02	1	6
T2 100SE BLO 50SW	1	11	8	54	.1	45	13	457	5.64	2	5	ND	2	51	1	2	2	204	.58	.04	6	132	1.35	10	.60	4	1.86	.02	.02	1	2
T2 125SE BLO 50SW	1	9	8	48	.1	7	3	248	2.07	3	5	ND	1	34	1	2	2	176	.74	.03	4	31	.35	11	.46	2	.92	.03	.03	1	3
T2 150SE BLO	1	13	7	42	.3	5	2	165	4.23	3	5	ND	3	12	1	2	2	189	.19	.03	5	22	.25	13	.37	6	1.14	.01	.03	4	6
T2 175SE BLO 50SW	1	23	7	54	.2	32	9	360	4.80	3	8	ND	1	16	1	2	2	238	.58	.04	6	110	1.20	18	.64	4	1.73	.03	.03	1	11
T2 200SE 500NE	1	3	2	21	.2	1	1	50	1.27	2	5	ND	1	17	1	2	2	91	.14	.01	4	1	.07	14	.07	3	1.23	.01	.02	1	27
T2 200SE 475NE	1	18	4	42	.1	7	4	262	5.52	2	5	ND	4	18	1	2	2	102	.16	.03	9	21	.60	82	.15	5	2.65	.01	.04	1	10
T2 200SE 450NE	1	4	4	13	.2	2	1	86	2.33	3	5	ND	2	11	1	2	2	122	.07	.01	6	9	.05	13	.16	3	.91	.01	.01	1	4
T2 200SE 425NE	1	6	3	20	.2	2	1	95	3.66	3	5	ND	3	14	1	2	2	124	.12	.03	7	7	.17	14	.16	5	1.43	.01	.02	2	1
T2 200SE 400NE	1	7	4	26	.1	2	1	178	1.99	2	5	ND	1	16	1	2	2	120	.14	.03	4	23	.06	19	.21	4	.60	.01	.02	1	8
T2 200SE 375NE	1	13	4	29	.6	4	1	99	2.05	2	5	ND	1	13	1	2	2	112	.13	.05	7	13	.09	22	.24	3	1.15	.01	.03	2	3
T2 200SE 350NE	1	13	2	33	.4	6	2	167	3.17	3	5	ND	2	11	1	2	2	220	.20	.03	3	13	.12	14	.31	4	.77	.02	.02	1	7
STD Cu/Au-0.5	21	58	40	134	6.9	69	27	1149	3.96	40	16	8	32	46	18	15	20	59	.48	.15	38	58	.88	172	.07	39	1.72	.06	.10	14	510

## IMPERIAL METALS PROJECT - 4202 FILE # 85-3163

PAGE 2

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	B1	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#
	FPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	%	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	
T2 200SE 325NE	1	12	7	40	.3	10	2	228	4.81	3	5	ND	1	17	1	2	2	214	.41	.05	5	31	.28	19	.53	2	1.16	.02	.02	1	9
T2 200SE 300NE	2	37	17	89	.5	40	25	1584	8.21	6	5	ND	1	28	1	2	2	178	.32	.11	6	68	.59	29	.09	2	3.32	.02	.04	1	8
T2 200SE 275NE	1	38	20	83	.9	21	15	611	8.91	7	5	ND	1	5	1	5	2	204	.04	.11	7	48	.42	31	.01	2	2.80	.01	.04	1	5
T2 200SE 250NE	1	18	9	38	.4	2	4	163	6.51	5	5	ND	2	15	1	2	2	154	.13	.12	4	25	.26	66	.15	3	2.34	.01	.02	1	2
T2 200SE 225NE	1	6	2	17	.3	3	1	122	1.77	2	5	ND	1	9	1	2	2	103	.09	.02	4	13	.06	9	.14	2	.51	.01	.01	2	9
T2 200SE 200NE	1	38	5	30	.4	5	5	194	8.80	7	5	ND	2	15	1	2	6	247	.13	.14	3	41	.33	33	.35	2	1.95	.01	.02	1	4
T2 200SE 175NE	1	50	2	29	.2	3	3	184	9.38	5	5	ND	1	15	1	2	15	400	.18	.13	2	39	.15	15	.71	2	1.03	.01	.02	1	1
T2 200SE 150NE	1	19	6	43	.3	20	6	444	5.60	4	5	ND	2	15	1	2	2	169	.29	.07	3	37	.90	24	.28	6	1.50	.02	.03	1	2
T2 200SE 125NE	1	37	2	62	.2	25	9	483	4.20	5	5	ND	1	31	1	2	2	161	.85	.08	2	53	.97	10	.48	3	1.55	.04	.03	1	12
T2 200SE 100NE	1	95	4	55	.2	20	12	651	4.94	6	5	ND	1	49	1	2	7	165	1.01	.06	5	47	.78	9	.61	2	1.46	.04	.03	1	16
T2 200SE 75NE	1	62	2	57	.4	32	15	681	6.91	9	5	ND	1	25	1	2	4	256	.55	.05	2	72	1.39	13	.76	2	2.56	.02	.03	1	43
T2 200SE 50NE	1	28	5	42	.2	14	6	990	7.09	7	5	ND	1	21	1	2	2	218	.30	.19	2	50	.47	15	.39	2	1.75	.02	.02	1	4
T2 200SE 25NE	1	26	2	39	.2	28	6	320	3.84	3	5	ND	1	24	1	2	2	189	.87	.06	2	57	.85	12	.52	5	1.12	.06	.03	2	5
T2 200SE 0SW	1	47	5	44	.7	12	5	222	3.75	4	5	ND	1	20	1	2	2	135	.29	.05	3	31	.26	28	.30	3	1.70	.01	.02	2	4
T2 200SE 25SW	2	44	3	65	.3	46	15	497	6.39	10	5	ND	1	21	1	2	2	236	.61	.07	2	165	1.98	11	.61	2	2.50	.03	.02	1	14
T2 200SE BLO 50SW	1	186	10	71	.2	42	20	659	7.61	13	5	ND	1	13	1	2	2	218	.44	.07	2	150	1.69	16	.38	2	3.04	.03	.03	1	2
T2 200SE 75SW	1	46	3	45	.3	29	11	377	5.11	7	5	ND	1	14	1	2	4	255	.68	.04	2	88	1.19	10	.71	4	1.64	.04	.02	1	3
T2 200SE 100SW	1	21	2	39	.1	31	8	303	5.48	3	5	ND	1	16	1	2	2	197	.38	.05	4	82	.88	10	.32	2	1.57	.02	.01	2	2
T2 200SE 125SW	1	32	4	49	.3	17	6	182	4.49	4	5	ND	1	18	1	2	2	157	.29	.04	4	51	.53	24	.28	4	1.65	.02	.02	1	60
T2 200SE 150SW	2	75	2	63	.1	80	14	427	4.57	3	5	ND	1	19	1	2	2	155	.60	.03	5	108	1.74	10	.35	2	1.96	.04	.02	1	1
T2 200SE 175SW	2	32	2	62	.2	23	8	324	4.42	5	5	ND	1	18	1	2	2	167	.38	.04	3	62	.63	25	.34	4	1.82	.02	.02	1	3
T2 200SE 200SW	2	32	2	70	.2	37	12	433	4.59	4	5	ND	1	23	1	2	2	146	.88	.04	5	103	1.31	25	.43	3	2.15	.05	.02	1	1
T2 200SE 225SW	2	32	5	65	.2	21	9	377	5.93	3	5	ND	1	23	1	2	2	194	.60	.04	5	71	.83	23	.33	2	1.97	.03	.03	1	2
T2 200SE 250SW	3	114	7	153	.3	66	33	861	7.01	3	5	ND	1	12	1	3	2	165	.41	.05	6	177	2.35	32	.16	2	5.29	.02	.03	1	2
T2 225SE BLO 50SW	2	30	2	76	.2	45	15	464	6.17	6	5	ND	1	18	1	2	2	208	.58	.06	2	142	1.84	21	.38	3	2.52	.03	.04	1	1
T2 250SE BLO 50SW	2	70	2	75	.2	34	22	2226	6.15	7	5	ND	1	31	1	2	2	180	.64	.11	2	121	1.20	149	.42	2	2.66	.03	.04	1	3
T2 275SE BLO 50SW	1	18	5	36	.1	11	5	516	4.68	2	5	ND	1	25	1	2	2	160	.44	.06	6	42	.37	24	.27	2	1.52	.01	.02	2	3
T2 300SE BLO	2	89	6	66	.2	22	17	588	3.91	8	5	ND	1	16	1	4	2	80	.31	.15	6	67	.56	46	.16	3	5.23	.02	.03	1	2
T2 325SE BLO	2	20	2	68	.1	25	17	438	3.17	4	5	ND	1	16	1	2	2	100	.69	.06	4	79	.99	24	.37	2	1.74	.03	.03	1	1
T2 350SE BLO 50SW	2	7	5	36	.1	15	5	193	3.17	2	5	ND	1	13	1	2	2	123	.44	.04	3	37	.70	10	.24	2	.88	.03	.03	1	2
T2 375SE BLO 50SW	2	52	2	73	.4	21	15	432	2.45	6	5	ND	1	14	1	3	2	62	.43	.12	5	56	.57	18	.19	4	3.14	.02	.03	1	1
T2 400SE 375NE	1	8	2	18	.1	9	2	183	3.85	2	5	ND	1	14	1	2	2	250	.26	.02	6	41	.11	6	.45	2	.45	.02	.01	2	1
T2 400SE 350NE	1	29	3	34	.2	12	8	329	4.39	3	5	ND	3	11	1	3	2	139	.23	.05	10	37	.62	19	.14	3	2.22	.02	.02	1	1
T2 400SE 325NE	1	7	5	26	.1	6	3	146	3.68	4	5	ND	2	14	1	2	2	180	.17	.05	8	21	.14	11	.21	2	1.00	.01	.01	1	8
T2 400SE 300NE	1	5	2	27	.1	8	1	187	3.69	3	5	ND	2	32	1	2	3	182	.47	.06	4	33	.28	7	.52	2	1.01	.02	.02	1	4
T2 400SE 275NE	1	6	2	22	.1	4	1	133	2.18	2	5	ND	1	32	1	2	2	146	.52	.03	5	12	.11	7	.32	3	.61	.02	.01	2	1
STD C/AU-0.5	21	58	39	136	7.0	67	28	1121	3.96	38	18	7	32	45	17	15	22	56	.48	.15	36	55	.08	184	.07	30	1.72	.06	.11	14	500

## IMPERIAL METALS PROJECT - 4202 FILE # 85-3163

PAGE 3

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	B1 PPM	V PPM	Ca %	P PPM	La PPM	Cr PPM	Mg PPM	Ba PPM	Ti %	B PPM	Al %	Na %	K PPM	W PPB	Hf PPB
I2 400SE 250NE	1	2	8	20	.1	3	1	118	1.50	3	5	ND	1	33	1	2	2	98	.38	.03	3	21	.09	7	.28	2	.41	.02	.01	1	8
I2 400SE 225NE	3	7	11	22	.1	135	4	141	4.36	5	5	ND	1	9	1	2	2	262	.19	.04	5	63	.10	7	.50	4	.49	.02	.02	1	110
I2 400SE 200NE	4	9	17	48	.1	58	14	524	8.08	2	5	ND	1	21	1	2	4	243	.34	.08	3	72	.98	22	.23	2	2.35	.03	.03	1	32
I2 400SE 175NE	1	62	12	30	.2	6	3	84	.84	2	5	ND	1	10	1	2	2	46	.11	.33	9	31	.07	22	.13	2	2.78	.01	.02	1	2
I2 400SE 150NE	1	9	4	29	.1	8	5	174	6.11	2	5	ND	1	21	1	2	2	267	.34	.04	3	38	.25	9	.62	4	1.05	.02	.02	1	1
I2 400SE 125NE	1	5	9	51	.2	14	7	214	7.45	2	5	ND	1	9	1	2	2	270	.16	.13	3	71	.57	6	.20	6	2.08	.01	.03	1	1
I2 400SE 75NE	3	25	5	61	.1	352	27	438	5.13	2	9	ND	1	5	1	2	2	101	.30	.06	2	326	4.23	5	.24	2	3.00	.02	.01	1	1
I2 400SE 50NE	1	12	11	22	.1	15	5	170	7.45	3	5	ND	1	17	1	3	2	257	.26	.08	6	56	.34	7	.54	2	1.50	.02	.02	1	2
I2 400SE 25NW	1	74	5	53	.1	24	11	351	4.19	4	5	ND	1	30	1	2	2	143	.51	.05	3	78	.69	23	.35	4	1.76	.03	.03	1	41
I2 400SE 25NE	1	6	8	16	.1	10	4	152	3.16	5	5	ND	1	20	1	2	2	174	.33	.03	5	28	.26	7	.36	3	.83	.02	.01	1	14
I2 400SE 0NW	1	75	6	57	.2	15	12	357	5.83	2	5	ND	2	16	1	2	2	112	.25	.16	2	76	.21	20	.25	2	6.23	.02	.02	1	7
I2 400SE BLO 50SW	1	100	8	57	.1	46	17	657	4.37	7	7	ND	1	44	1	2	2	177	1.50	.05	2	135	1.74	30	.59	6	2.54	.03	.02	1	10
I2 400SE 75SW	2	92	2	61	.1	32	17	365	5.87	2	5	ND	1	22	1	2	2	183	.33	.06	3	92	1.03	25	.34	2	3.60	.02	.02	1	8
I2 400SE 100SW	1	23	2	42	.1	26	10	438	3.98	3	5	ND	1	31	1	2	2	159	.73	.03	2	87	1.02	11	.49	2	1.45	.03	.02	1	1
I2 400SE 125SW	2	90	16	211	.2	32	49	1143	6.57	2	5	ND	1	17	1	2	2	149	.39	.07	3	97	.63	52	.30	2	4.14	.02	.04	1	2
I2 400SE 150SW	1	21	6	45	.1	22	8	503	3.21	3	5	ND	1	15	1	2	2	93	.41	.04	4	56	.74	35	.25	2	1.87	.03	.04	1	1
I2 400SE 175SW	2	48	9	84	.1	13	20	3169	2.94	2	5	ND	1	23	1	2	2	72	.78	.06	4	30	.52	70	.12	2	2.01	.02	.05	1	5
I2 400SE 200SW	1	23	7	54	.1	14	9	891	3.35	2	5	ND	1	19	1	2	2	99	.42	.05	3	36	.57	38	.17	2	1.79	.02	.05	1	3
I2 400SE 225SW	2	42	7	59	.1	21	10	321	5.71	3	5	ND	1	23	1	2	2	202	.46	.03	2	75	.68	29	.45	2	2.26	.02	.03	1	1
I2 400SE 250SW	2	39	2	54	.1	22	12	359	5.35	7	5	ND	1	24	1	2	2	186	.64	.03	2	74	.81	24	.49	2	2.20	.03	.03	1	130
I2 400SE 275SW	2	38	7	61	.1	18	12	308	3.20	2	5	ND	1	16	1	2	2	96	.36	.03	5	40	.49	42	.14	5	2.57	.01	.02	1	1
I2 400SE 300SW	1	11	5	25	.1	5	3	116	3.01	2	5	ND	1	19	1	2	2	136	.28	.02	3	28	.16	21	.35	2	.88	.01	.01	1	1
I2 400SE 325SW	2	71	7	74	.1	29	16	1221	4.26	4	5	ND	1	23	1	2	2	112	.62	.06	5	49	.94	62	.22	2	3.00	.02	.02	1	3
I2 400SE 350SW	3	80	7	77	.2	30	18	1524	4.29	2	5	ND	1	23	1	2	2	116	.56	.06	5	56	.81	59	.22	2	3.05	.01	.02	1	3
I2 400SE 375SW	2	85	4	68	.1	33	18	596	5.60	7	5	ND	1	23	1	2	4	188	.70	.03	4	79	1.55	40	.55	2	2.54	.03	.03	1	2
I2 400SE 400SW	1	24	9	54	.2	23	11	326	4.67	2	5	ND	1	21	1	3	2	162	.58	.04	4	76	.59	19	.30	2	1.42	.01	.02	1	6
I2 400SE 425SW	2	71	2	74	.1	40	20	568	4.92	2	5	ND	1	19	1	2	2	139	.66	.04	2	93	1.56	29	.35	2	3.84	.04	.03	1	1
I2 400SE 450SW	2	54	6	66	.1	34	16	580	5.00	3	5	ND	1	18	1	2	2	154	.62	.04	2	82	1.18	33	.34	6	2.87	.02	.03	1	2
I2 425SE BLO	3	30	2	73	.1	62	16	2055	3.89	2	5	ND	1	26	1	2	2	136	1.29	.06	2	114	1.24	32	.45	2	1.85	.04	.03	1	6
I2 450SE BLO	2	23	7	51	.1	20	10	688	4.86	6	5	ND	1	51	1	2	5	223	.88	.07	2	48	.93	8	.78	3	1.36	.04	.03	1	1
I2 450SE 50SW	3	120	5	86	.2	34	79	1470	4.11	2	5	ND	1	24	1	2	2	116	.51	.06	10	64	.60	39	.26	2	3.81	.02	.02	1	1
I2 475SE BLO	1	15	2	34	.1	11	5	244	2.87	2	5	ND	1	33	1	2	2	165	.50	.05	2	28	.34	9	.62	2	.83	.03	.02	1	2
I2 500SE BLO	2	56	4	117	.2	22	36	1110	4.92	3	5	ND	1	36	1	2	2	132	.59	.07	5	46	.69	28	.40	4	2.40	.03	.03	1	1
I2 525SE BLO	1	11	4	25	.1	9	3	158	2.74	5	5	ND	1	21	1	2	2	143	.35	.02	4	39	.25	29	.45	2	1.03	.02	.01	1	20
I2 550SE BLO	2	13	8	79	.1	37	8	322	1.97	2	5	ND	1	23	1	2	2	75	.38	.08	2	84	.74	11	.24	2	.78	.02	.07	1	4
I2 575SE BLO	1	57	4	79	.1	34	18	662	7.71	5	5	ND	1	21	1	2	5	263	.47	.07	2	83	1.18	22	.61	2	2.13	.02	.02	1	2
STD C/AU-0.5	20	61	39	137	6.9	69	29	1185	3.94	40	18	8	33	48	18	16	21	59	.48	.15	37	59	.88	174	.08	38	1.72	.06	.11	13	505

## IMPERIAL METALS PROJECT - 4202 FILE # 85-3163

PAGE 4

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V %	Ca %	P PPM	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K PPM	W PPB	Aut
T2 600SE 475NE	1	4	3	34	.2	4	2	81	2.09	4	5	ND	3	9	1	2	2	84	.10	.02	8	9	.12	46	.02	3	1.99	.01	.02	2	3
T2 600SE 450NE	1	8	4	31	.1	1	3	75	3.04	2	5	ND	2	10	1	2	2	132	.10	.04	5	7	.13	39	.08	5	1.40	.01	.02	1	2
T2 600SE 425NE	1	5	8	34	.1	1	2	63	1.95	2	5	ND	1	11	1	2	2	107	.14	.04	4	5	.11	24	.04	4	.98	.01	.02	1	2
T2 600SE 400NE	1	8	6	40	.1	1	5	182	5.62	4	5	ND	3	13	1	2	2	109	.09	.06	7	11	.33	35	.07	7	2.09	.01	.02	1	4
T2 600SE 375NE	1	5	3	31	.1	1	1	66	1.89	2	5	ND	2	13	1	2	2	88	.09	.02	4	4	.11	18	.08	3	1.20	.01	.01	1	1
T2 600SE 350NE	1	21	10	53	.3	13	8	245	5.18	3	5	ND	1	6	1	2	2	195	.13	.06	4	48	.48	22	.09	2	1.63	.01	.02	1	5
T2 600SE 325NE	1	17	7	48	.4	9	7	177	5.99	6	5	ND	1	7	1	2	2	160	.07	.10	4	40	.38	18	.02	6	2.29	.01	.03	1	2
T2 600SE 300NE	1	22	2	43	.4	2	6	184	5.82	2	5	ND	2	5	1	2	2	90	.05	.07	8	22	.26	36	.01	5	3.14	.01	.01	1	3
T2 600SE 275NE	1	11	3	26	.2	2	3	204	1.59	2	5	ND	1	6	1	2	2	51	.08	.04	5	8	.16	22	.03	4	1.04	.01	.02	1	1
T2 600SE 250NE	1	7	8	30	.1	10	4	220	1.60	2	5	ND	1	16	1	2	2	56	.14	.05	5	20	.24	11	.06	3	.82	.01	.02	1	12
T2 600SE 225NE	1	6	9	35	.2	12	4	209	3.10	2	5	ND	1	11	1	2	2	145	.27	.06	4	45	.26	15	.27	3	1.11	.02	.02	1	2
T2 600SE 200NE	1	8	5	36	.2	1	2	223	1.98	2	5	ND	2	14	1	2	2	56	.18	.04	3	7	.15	64	.08	2	.92	.01	.02	1	1
T2 600SE 175NE	1	3	2	25	.2	3	2	105	1.46	2	5	ND	2	12	1	2	2	68	.16	.02	4	10	.15	13	.14	2	.62	.02	.01	2	1
T2 600SE 150NE	1	9	2	62	.1	31	10	406	4.12	2	5	ND	1	29	1	2	2	198	.49	.06	2	88	.99	12	.53	2	1.30	.02	.02	1	16
T2 600SE 125NE	1	4	4	44	.5	2	2	88	1.77	2	5	ND	1	10	1	2	2	56	.15	.04	2	6	.09	8	.06	3	.35	.03	.03	2	26
T2 600SE 100NE	1	3	3	18	.2	3	2	94	2.11	2	5	ND	2	14	1	2	2	97	.15	.03	4	13	.16	8	.12	2	.94	.01	.01	1	12
T2 600SE 75NE	1	24	10	55	1.1	8	4	146	2.37	2	5	ND	1	15	1	2	2	53	.14	.08	5	16	.17	54	.03	3	2.24	.01	.03	1	2
T2 600SE 50NE	1	1	2	22	.2	1	1	68	1.10	2	5	ND	1	10	1	2	2	50	.12	.02	3	7	.06	9	.08	2	.56	.02	.01	1	3
T2 600SE 25NE	1	8	2	41	.1	7	4	111	2.91	2	5	ND	2	11	1	2	2	97	.10	.03	3	17	.21	21	.09	2	1.39	.01	.01	1	17
T2 600SE 60	1	6	2	65	.1	10	8	199	5.72	2	5	ND	2	19	1	2	2	168	.33	.04	3	46	.21	30	.40	5	2.99	.02	.01	1	1
T2 600SE 25SW	1	94	4	75	.4	29	20	614	7.30	5	5	ND	2	13	1	2	2	196	.25	.06	2	60	1.19	37	.07	3	3.40	.01	.03	1	6
T2 600SE 50SW	1	22	4	66	.1	20	11	460	3.85	2	5	ND	2	26	1	2	2	129	.35	.04	6	78	.65	41	.31	5	1.91	.01	.02	1	3
T2 600SE 75SW	1	9	2	36	.1	13	4	244	2.38	2	5	ND	1	28	1	2	3	110	.42	.02	2	54	.50	17	.39	2	1.04	.02	.01	1	4
T2 600SE 100SW	1	56	5	52	.2	17	10	266	4.38	2	5	ND	1	16	1	2	2	108	.26	.08	2	68	.59	30	.24	3	4.21	.02	.02	1	1
T2 600SE 125SW	1	6	2	36	.2	6	3	216	1.46	2	5	ND	1	18	1	2	2	59	.35	.03	3	19	.25	44	.14	2	.71	.02	.02	1	3
T2 600SE 150SW	1	19	4	48	.1	16	7	302	3.36	2	5	ND	1	33	1	2	2	120	.41	.03	3	62	.66	34	.34	4	1.68	.02	.01	1	2
T2 600SE 175SW	1	36	8	62	.1	11	25	775	3.19	2	5	ND	2	12	1	2	2	62	.14	.05	6	26	.46	72	.02	3	3.24	.01	.04	1	46
T2 600SE 200SW	2	85	6	70	.2	24	22	1173	5.05	2	5	ND	1	16	1	2	2	145	.23	.08	3	91	.96	42	.14	4	2.98	.01	.03	1	8
T2 600SE 225SW	6	86	7	47	.4	11	10	171	7.04	19	5	ND	5	6	1	21	2	137	.11	.15	7	152	.28	24	.22	7	8.86	.01	.02	1	5
T2 600SE 250SW	4	111	8	79	.1	20	18	911	4.90	6	5	ND	1	25	1	2	2	128	.57	.07	8	50	.90	66	.14	6	4.04	.01	.03	1	9
T2 600SE 275SW	1	12	2	20	.1	3	3	96	1.61	2	5	ND	1	8	1	2	2	64	.10	.02	6	12	.13	25	.03	2	.99	.01	.01	1	1
T2 600SE 300SW	3	45	11	102	.1	28	22	562	6.40	2	5	ND	1	15	1	2	2	174	.20	.05	2	72	1.17	38	.11	2	2.78	.01	.02	1	3
T2 600SE 325SW	3	47	5	113	.1	25	23	2990	4.86	2	5	ND	1	19	1	2	2	111	.71	.10	8	62	.67	69	.10	4	3.24	.01	.03	1	4
T2 600SE 350SW	2	44	9	88	.1	38	19	737	5.70	3	5	ND	1	16	1	3	2	142	.36	.05	5	95	1.91	45	.13	4	3.13	.01	.02	1	3
T2 600SE 375SW	3	35	2	96	.1	33	17	407	6.67	2	5	ND	1	10	1	2	2	193	.20	.05	4	127	1.30	30	.09	2	3.24	.01	.02	1	2
T2 600SE 400SW	3	72	14	107	.4	21	25	2462	6.66	2	5	ND	2	16	1	2	3	169	.45	.07	10	61	.69	55	.18	2	3.54	.01	.03	1	47
STD C/AU-0.5	21	59	41	138	6.9	65	29	1189	3.95	39	19	7	33	47	17	14	21	59	.48	.16	37	59	.88	172	.08	39	1.72	.06	.10	13	495

## IMPERIAL METALS PROJECT - 4202 FILE # 85-3163

PAGE 5

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca PPM	P PPM	La PPM	Cr PPM	Mg PPM	Ba PPM	Ti PPM	B PPM	Al PPM	Na PPM	K PPM	W PPB	
T2 600SE 425SW	1	58	11	57	.1	12	10	398	5.95	12	5	ND	1	22	1	2	2	172	.21	.11	8	.47	.72	22	.28	2	3.47	.01	.02	1	8
T2 600SE 450SW	1	70	13	57	.2	14	10	294	5.23	9	5	ND	1	20	1	2	2	157	.20	.07	7	.39	.66	21	.24	2	2.93	.01	.02	1	10
T2 600SE 475SW	2	151	3	88	.4	29	29	670	5.10	22	5	ND	1	14	1	3	2	130	.19	.11	12	.67	.80	31	.21	3	6.73	.01	.02	1	4
T2 600SE 500SW	2	141	14	87	.5	27	26	588	5.04	21	5	ND	1	14	1	3	2	131	.19	.10	8	.64	.77	32	.21	4	6.35	.01	.02	1	2
T2 625SE BLO	1	10	13	43	.2	6	7	194	3.74	7	5	ND	1	15	1	2	2	117	.33	.03	7	.11	.59	29	.02	2	2.64	.02	.03	1	11
T2 650SE BLO	3	27	14	108	1.3	9	25	411	3.67	13	5	ND	1	16	1	3	2	83	.43	.07	17	.25	.27	41	.05	2	6.70	.01	.02	1	2
T2 675SE BLO	1	2	4	17	.1	1	1	57	1.10	3	5	ND	1	20	1	2	3	66	.20	.01	5	.4	.06	10	.15	2	.54	.02	.01	1	1
T2 700SE BLO	1	3	3	19	.2	2	1	102	1.68	2	5	ND	1	32	1	2	2	87	.31	.02	5	.5	.12	13	.15	2	.85	.02	.01	1	5
T2 725SE BLO	1	2	2	17	.1	3	1	84	1.45	3	5	ND	1	34	1	2	2	107	.39	.01	5	.8	.13	8	.24	3	.67	.02	.01	1	2
T2 750SE BLO	1	7	3	51	.4	5	6	305	3.63	6	5	ND	1	34	1	3	2	132	.44	.06	10	.12	.31	39	.14	2	2.11	.01	.03	1	6
T2 755SE BLO 50SW	1	15	6	36	.1	13	4	282	3.82	8	5	ND	1	23	1	2	2	185	.46	.05	9	.46	.48	8	.52	2	1.20	.02	.02	1	5
T2 775SE BLO	1	5	7	22	.1	4	2	218	2.06	4	5	ND	1	28	1	2	2	113	.42	.03	7	.12	.19	6	.30	2	.60	.03	.01	1	3
T2 800SE 500NE	2	1	8	57	.1	1	2	141	2.25	2	5	ND	1	21	1	3	2	61	1.05	.04	9	3	.17	598	.01	2	2.49	.01	.02	1	2
T2 800SE 475NE	3	3	4	33	.1	1	3	2024	1.27	2	5	ND	1	20	1	2	2	46	.53	.03	11	5	.16	357	.03	2	1.28	.01	.02	1	7
T2 800SE 450NE	4	9	13	32	.2	3	4	97	4.43	2	5	ND	1	9	1	2	2	121	.07	.04	14	6	.13	46	.04	2	2.62	.01	.03	1	5
T2 800SE 425NE	1	1	7	33	.1	2	1	43	1.39	2	5	ND	1	9	1	2	2	66	.11	.02	6	.4	.04	19	.02	2	.73	.01	.03	1	9
T2 800SE 400NE	1	1	5	33	.1	1	3	120	1.19	2	5	ND	1	12	1	2	2	33	.07	.04	7	2	.30	37	.01	2	1.66	.01	.05	1	17
T2 800SE 375NE	1	4	4	18	.1	1	1	57	1.84	2	5	ND	1	9	1	2	2	91	.07	.02	6	4	.06	12	.04	4	1.09	.01	.01	1	6
T2 800SE 350NE	7	15	13	53	.5	4	10	446	8.56	13	5	ND	3	6	2	5	6	56	.08	.18	28	11	.10	43	.06	2	5.14	.01	.03	1	2
T2 800SE 325NE	3	7	14	43	.2	3	6	249	5.96	3	5	ND	3	11	1	5	2	106	.08	.06	18	10	.45	36	.06	3	3.04	.01	.02	1	1
T2 800SE 300NE	2	9	9	32	.1	1	2	94	3.50	2	5	ND	1	9	1	2	2	130	.07	.05	9	6	.13	42	.06	3	1.68	.01	.02	1	4
T2 800SE 275NE	1	3	5	18	.1	1	1	47	1.79	2	5	ND	1	7	1	2	2	83	.06	.03	6	9	.04	8	.03	3	.60	.01	.02	1	3
T2 800SE 250NE	1	10	5	19	.2	2	3	72	3.10	2	5	ND	1	16	1	2	2	112	.09	.04	10	6	.08	16	.04	2	1.06	.01	.02	1	24
T2 800SE 225NE	5	48	26	82	2.2	11	26	1463	4.78	28	5	ND	3	9	1	2	2	96	.16	.12	18	35	.29	44	.04	2	6.97	.01	.02	1	5
T2 800SE 200NE	1	18	6	49	.4	4	4	131	4.07	6	5	ND	1	10	1	3	2	97	.08	.12	14	12	.27	30	.02	2	3.29	.01	.03	1	7
T2 800SE 175NE	1	11	9	45	.3	3	5	182	7.04	6	5	ND	1	14	1	2	3	167	.16	.15	12	.24	.25	19	.18	2	2.26	.01	.02	1	13
T2 800SE 150NE	1	8	5	42	.4	5	3	229	1.92	2	5	ND	1	19	1	2	2	84	.38	.06	5	10	.27	24	.14	2	.73	.03	.02	1	23
T2 800SE 125NE	1	7	4	20	.2	7	3	195	3.43	3	5	ND	1	12	1	2	2	219	.21	.03	10	37	.15	8	.29	2	.62	.02	.01	1	2
T2 800SE 100NE	1	55	8	48	.3	16	9	314	8.67	26	5	ND	1	17	1	3	16	275	.22	.10	13	66	.65	18	.49	2	3.16	.02	.03	1	1
T2 800SE 75NE	1	56	20	56	.2	21	13	467	5.55	26	5	ND	1	19	1	2	2	153	.35	.08	11	50	1.00	33	.16	4	3.55	.03	.03	1	4
T2 800SE 25NE	2	51	15	126	.8	35	30	387	4.87	77	5	ND	1	16	1	4	2	118	.49	.07	13	50	.57	39	.12	2	6.12	.02	.02	1	2
T2 800SE BLO	1	15	9	56	.1	8	4	236	3.67	30	5	ND	1	26	1	2	2	161	.49	.04	7	27	.29	15	.26	3	1.32	.02	.01	1	3
T2 800SE 25SW	1	22	3	52	.2	11	9	378	2.40	4	5	ND	1	34	1	2	2	78	.07	.06	6	19	.80	25	.14	2	1.07	.02	.03	1	19
T2 800SE 50SW	2	26	7	182	1.6	23	24	3172	2.54	45	5	ND	1	27	1	4	2	53	1.60	.12	18	35	.24	77	.06	6	5.93	.01	.02	1	1
T2 800SE 75SW	1	28	19	49	.4	9	9	349	4.39	17	5	ND	2	17	1	3	2	129	.25	.06	9	22	.36	66	.07	2	2.99	.01	.02	1	2
T2 800SE 100SW	1	19	16	38	.4	8	7	239	4.10	15	5	ND	1	17	1	2	2	137	.21	.04	10	20	.32	61	.07	2	2.40	.01	.02	1	17
STD C/AU-0.5	21	58	40	137	7.2	64	29	1197	3.87	40	18	7	30	48	17	14	17	59	.48	.15	40	55	.87	177	.08	36	1.70	.06	.11	13	505

## IMPERIAL METALS PROJECT - 4202 FILE # 85-3163

PAGE 6

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca PPM	P PPM	La PPM	Cr PPM	Mn PPM	Ba PPM	Ti PPM	B PPM	Al %	Na %	K PPM	W PPB	
T2 800SE 125SW	1	25	9	.99	.9	13	12	1197	3.15	23	5	ND	1	23	1	3	2	72	1.50	.06	10	24	.30	71	.06	4	3.51	.01	.02	1	8
T2 800SE 150SW	4	35	10	.61	.4	57	17	501	7.20	3	5	ND	1	12	1	2	2	173	.29	.07	2	114	.83	34	.16	2	3.05	.01	.02	1	1
T2 800SE 175SW	1	18	11	.35	.2	12	7	152	5.99	5	5	ND	1	11	1	2	2	178	.16	.05	3	48	.32	24	.16	3	1.95	.01	.02	1	11
T2 800SE 200SW	1	22	4	.56	.3	11	9	910	3.08	2	5	ND	1	25	1	2	2	84	.93	.04	5	23	.34	76	.07	2	1.66	.01	.02	1	1
T2 800SE 225SW	1	41	8	.50	.1	16	11	491	4.01	5	5	ND	2	16	1	2	2	94	.39	.09	5	28	.95	57	.13	4	2.13	.01	.02	1	7
T2 800SE 250SW	1	167	7	.69	.2	21	19	914	5.42	10	5	ND	1	21	1	2	2	124	.35	.07	5	41	.74	67	.14	2	3.26	.01	.02	1	6
T2 800SE 275SW	1	102	4	.92	.1	47	23	1039	6.24	3	6	ND	1	17	1	2	6	149	.98	.08	4	81	2.48	43	.31	8	2.78	.01	.04	1	4
T2 800SE 300SW	1	67	11	.70	.2	21	12	950	3.61	4	5	ND	1	18	1	2	2	114	.69	.08	2	40	1.09	57	.22	3	1.73	.01	.03	1	5
T2 800SE 325SW	1	134	6	.61	.2	19	16	353	5.05	4	5	ND	2	16	1	2	2	116	.44	.08	3	42	.75	57	.16	2	4.99	.01	.03	1	9
T2 800SE 350SW	1	131	5	.58	.2	20	16	347	4.56	6	5	ND	2	16	1	2	2	104	.44	.08	7	44	.80	57	.16	4	5.00	.01	.02	1	12
T2 800SE 375SW	1	62	6	.60	.4	12	10	234	5.33	5	5	ND	1	14	1	2	2	139	.22	.05	2	31	.50	61	.18	2	2.59	.01	.02	1	3
T2 800SE 400SW	1	61	10	.53	.2	13	11	275	5.38	2	5	ND	1	15	1	2	2	141	.24	.06	2	30	.55	60	.18	3	2.42	.01	.02	1	1
T2 800SE 425SW	1	69	8	.39	.2	15	11	291	4.60	3	5	ND	1	13	1	2	2	139	.24	.03	2	46	.58	34	.19	2	1.94	.01	.01	1	8
T2 800SE 450SW	1	57	4	.39	.1	13	10	284	4.73	2	5	ND	1	14	1	2	2	149	.26	.03	2	48	.55	37	.21	3	1.81	.01	.02	1	5
T2 800SE 475SW	1	99	10	.101	.7	31	41	3589	5.21	13	5	ND	1	23	1	3	2	114	1.00	.08	9	57	.61	93	.16	2	4.78	.01	.03	1	1
T2 800SE 500SW	1	79	3	101	.4	47	21	1114	6.01	2	7	ND	1	19	1	2	5	143	1.00	.05	2	85	2.19	36	.24	3	5.25	.02	.03	1	1
T2 825SE 8L	1	16	4	.79	.1	37	15	930	4.51	2	5	ND	1	21	1	2	7	161	.51	.09	2	99	1.49	14	.34	3	1.49	.02	.03	1	2
T2 850SE 8L	1	7	7	.30	.1	5	2	110	1.47	2	5	ND	1	17	1	2	5	99	.36	.04	2	40	.16	11	.34	2	.51	.02	.02	1	1
T2 875SE 8L	1	11	12	124	.4	9	13	1180	2.36	4	5	ND	1	22	1	2	2	55	1.11	.06	7	14	.20	91	.05	2	2.00	.01	.03	1	3
T2 900SE 500NE	16	14	11	.68	.5	3	15	11631	1.70	10	32	ND	1	8	1	3	2	41	.17	.23	19	16	.08	74	.01	4	5.48	.01	.02	1	1
T2 900SE 475NE	1	10	6	.70	.5	3	2	63	.37	2	5	ND	1	23	1	2	2	7	.17	.13	11	6	.08	114	.01	3	1.70	.01	.04	1	1
T2 900SE 450NE	2	14	4	.56	.2	2	5	276	3.37	2	5	ND	2	7	1	2	2	42	.06	.10	9	3	.44	85	.01	4	2.84	.01	.03	1	2
T2 900SE 425NE	1	4	4	.23	.1	1	1	68	1.77	2	5	ND	1	5	1	2	2	76	.04	.03	6	3	.08	30	.02	3	1.40	.01	.02	1	3
T2 900SE 400NE	1	4	6	.29	.1	1	2	119	1.93	3	5	ND	1	8	1	2	2	55	.06	.04	6	1	.11	28	.01	2	1.84	.01	.02	1	7
T2 900SE 375NE	1	3	2	.34	.1	1	2	242	1.13	2	5	ND	2	6	1	2	2	37	.06	.07	4	2	.20	37	.01	4	1.70	.01	.04	1	5
T2 900SE 350NE	2	4	7	.20	.2	1	2	109	1.59	2	5	ND	1	62	1	2	2	48	.33	.04	3	1	.13	94	.03	2	1.81	.01	.03	1	1
T2 900SE 325NE	1	1	2	.23	.1	1	1	36	.88	3	5	ND	1	8	1	2	2	42	.07	.02	6	2	.05	13	.02	7	.57	.01	.02	1	1
T2 900SE 300NE	1	1	3	.30	.1	1	1	58	1.18	2	5	ND	1	15	1	2	2	39	.14	.03	2	1	.16	8	.01	2	1.04	.01	.02	1	1
T2 900SE 275NE	1	1	6	.19	.1	1	1	22	.75	3	5	ND	1	8	1	2	2	26	.09	.02	2	2	.02	9	.01	2	.57	.01	.01	1	31
T2 900SE 250NE	1	4	5	.27	.2	3	2	46	1.32	2	5	ND	1	8	1	2	2	51	.10	.03	2	4	.07	24	.04	4	.36	.01	.02	1	34
T2 900SE 225NE	1	3	2	.15	.1	1	2	32	1.48	2	5	ND	1	11	1	2	2	73	.08	.02	3	2	.05	33	.04	3	.73	.01	.01	1	8
T2 900SE 200NE	1	4	3	.20	.1	1	2	59	2.36	2	5	ND	1	8	1	2	2	77	.07	.02	3	1	.10	36	.04	2	1.13	.01	.01	1	4
T2 900SE 175NE	2	11	12	.40	.1	3	5	193	6.65	2	5	ND	1	11	1	2	2	168	.09	.08	2	18	.43	44	.08	6	2.53	.01	.02	1	3
T2 900SE 150NE	2	14	6	.59	.2	4	14	214	3.56	2	5	ND	2	15	1	2	2	79	.28	.04	7	10	.32	110	.03	2	3.64	.01	.02	1	3
T2 900SE 125NE	1	26	6	.67	.2	20	26	1056	4.95	2	5	ND	2	18	1	2	3	111	.35	.10	6	39	1.08	78	.15	3	4.23	.02	.03	1	1
T2 900SE 100NE	1	45	2	.61	.2	9	11	588	3.96	14	5	ND	3	14	1	2	2	81	.32	.11	10	21	.99	54	.11	5	3.77	.01	.02	1	1
STD C/AU-0.5	20	59	39	138	6.9	65	27	1130	4.00	41	18	9	36	47	19	15	22	58	.48	.17	37	58	.88	172	.08	40	1.72	.06	.11	14	480

## IMPERIAL METALS PROJECT - 4202 FILE # 85-3163

PAGE 7

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn %	Fe PPM	As %	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	F PPM	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K PPM	N %	Au# PPB
T2 900SE 75NE	2	9	61	141	.5	9	6	136	4.02	16	5	ND	1	25	1	2	2	126	.25	.03	4	21	.32	24	.09	2	2.67	.01	.02	1	10
T2 900SE 50NE	1	8	4	19	.2	6	3	186	1.95	2	5	ND	1	33	1	4	2	112	.42	.04	3	15	.18	9	.30	5	.59	.03	.02	1	5
T2 900SE 25NE	2	15	12	55	.3	6	6	203	5.44	6	5	ND	1	23	1	2	2	132	.22	.08	2	35	.45	31	.21	2	2.44	.01	.03	1	35
T2 900SE BL	1	5	2	40	.3	3	3	114	1.48	2	5	ND	1	15	1	3	2	51	.26	.05	6	10	.12	37	.05	5	1.09	.01	.03	1	4
T2 900SE 25SW	1	21	2	47	.1	9	7	361	4.09	2	5	ND	1	27	1	2	2	117	.35	.08	5	26	.5v	75	.17	5	2.29	.02	.03	1	3
T2 900SE 50SW	1	6	2	19	.2	3	2	125	1.97	2	5	ND	1	31	1	3	2	101	.34	.03	4	11	.14	24	.19	2	.92	.02	.02	1	27
T2 900SE 75SW	1	18	3	57	.1	3	6	226	7.63	3	5	ND	1	3	1	2	2	163	.04	.06	2	4	.27	24	.01	5	2.75	.01	.03	1	1
T2 900SE 100SW	1	25	4	55	.1	5	9	221	6.05	2	5	ND	2	4	1	4	2	151	.06	.05	6	7	.28	25	.01	7	2.78	.01	.02	1	14
T2 900SE 125SW	3	28	6	102	.5	8	9	219	3.99	20	5	ND	2	12	1	2	2	87	.16	.04	7	28	.45	60	.07	7	5.78	.01	.02	1	16
T2 900SE 150SW	3	24	6	88	.4	8	8	210	4.41	15	5	ND	3	18	1	2	2	109	.20	.03	5	25	.50	66	.08	2	4.35	.01	.03	1	8
T2 900SE 175SW	1	15	5	27	.1	5	4	85	1.99	2	5	ND	1	7	1	2	2	90	.09	.02	6	14	.18	17	.05	5	1.18	.01	.02	1	4
T2 900SE 200SW	3	86	13	84	.4	18	14	623	5.54	9	5	ND	1	21	1	2	3	147	.52	.05	7	47	.89	79	.18	5	3.20	.01	.04	1	12
T2 900SE 225SW	2	78	19	76	.1	21	13	591	5.02	3	5	ND	1	21	1	2	2	133	.50	.04	3	43	.89	76	.17	2	2.89	.01	.04	1	9
T2 900SE 250SW	1	25	4	63	.3	11	7	219	3.28	2	5	ND	1	19	1	2	2	102	.18	.04	5	27	.49	51	.08	4	2.20	.01	.05	1	39
T2 900SE 275SW	2	131	2	94	.3	38	22	1145	5.21	7	5	ND	1	34	1	2	5	132	.89	.06	9	77	1.98	76	.29	4	3.17	.01	.04	1	2
T2 900SE 300SW	3	79	11	110	.1	69	30	1246	6.08	7	10	ND	1	31	1	2	2	152	.78	.07	6	184	3.08	45	.31	4	4.06	.01	.02	1	1
T2 900SE 325SW	2	87	3	98	.1	72	30	1165	5.96	12	5	ND	1	46	1	2	7	154	.82	.06	6	194	3.26	38	.34	4	4.02	.01	.02	1	16
T2 900SE 350SW	4	35	6	49	.1	14	9	238	5.21	5	5	ND	1	21	1	2	2	145	.22	.02	6	64	.68	50	.19	2	2.60	.01	.02	1	11
T2 900SE 375SW	2	6	11	26	.1	11	5	152	2.86	2	5	ND	1	12	1	2	2	129	.15	.02	3	41	.47	15	.12	2	1.28	.01	.02	1	75
T2 900SE 400SW	2	25	7	67	.1	34	15	435	5.69	2	5	ND	1	10	1	2	2	174	.10	.04	3	133	1.63	11	.13	2	2.38	.01	.01	1	22
T2 900SE 425SW	1	34	2	161	.1	38	19	632	8.19	7	5	ND	1	7	1	2	11	245	.20	.06	6	94	1.72	30	.30	3	3.66	.01	.04	1	8
T2 900SE 450SW	2	33	6	59	.2	9	8	242	5.52	4	5	ND	2	19	1	2	2	150	.20	.09	6	37	.55	40	.18	3	3.29	.01	.02	1	7
T2 900SE 475SW	1	26	10	42	.2	9	9	246	5.25	2	5	ND	1	19	1	2	2	164	.22	.08	4	38	.58	31	.26	2	2.21	.01	.02	1	24
T2 900SE 500SW	2	21	12	36	.2	11	7	224	4.92	2	5	ND	1	19	1	2	2	167	.22	.05	7	34	.51	26	.27	2	1.95	.01	.01	1	3
NO NAME	2	33	8	74	.3	46	16	672	5.47	2	5	ND	1	46	1	2	9	157	1.02	.08	3	107	1.51	24	.51	7	2.08	.04	.03	1	4
STD C/AU-0.5	21	58	39	138	7.2	66	26	1122	3.93	38	18	8	33	46	17	13	19	56	.48	.15	36	56	.88	172	.07	37	1.72	.06	.10	13	515

APPENDIX 3  
Correlation Co-efficients

. display structure

STRUCTURE FOR FILE: A\*T2CHEM .DBF

NUMBER OF RECORDS: 00274

DATE OF LAST UPDATE: 04/18/86

PRIMARY USE DATABASE

FLD	NAME	TYPE	WIDTH	DEC
001	MOPPM	N	005	
002	CUPPM	N	005	
003	PBPPM	N	005	
004	ZNPPM	N	005	
005	AGPPM	N	005	001
006	NIPPM	N	005	
007	COPPM	N	005	
008	MNPPM	N	006	
009	FEPCT	N	005	002
010	ASPPM	N	005	
011	UPPM	N	005	
012	AUPPM	N	005	
013	THPPM	N	005	
014	SRPPM	N	005	
015	CDPPM	N	005	
016	SBPPM	N	005	
017	BIPPM	N	005	
018	VPPM	N	005	
019	CAPCT	N	005	002
020	PPCT	N	005	002
021	LAPPM	N	005	
022	CRPPM	N	005	
023	MGPCT	N	005	002
024	BAPPM	N	005	
025	TIPCT	N	005	002
026	EPPM	N	005	
027	ALPCT	N	006	002
028	NAPCT	N	005	002
029	KPCT	N	005	002
030	WPPM	N	005	
031	AUPPB	N	005	
** TOTAL **			00158	

. set print off

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
1	1.520833	1.287038	2	5.950955	.1371834
			3	1.467969	.211886
			4	10.16632	.2680121
			5	5.920106E-02	.1996915
			6	5.984982	.1705053
			7	3.632291	.3004872
			8	619.7037	.7111764
			9	.3626261	.1555311
			10	1.630642	.1764695
			11	1.662674	.7166316
			12	0	1.701412E+38
			13	6.423616E-02	7.458002E-02
			14	-.8747387	-7.712628E-02
			15	2.282989E-02	.2759462
			16	.4732638	.2744188
			17	-1.467037E-02	-7.177663E-03
			18	-6.485596	-8.470289E-02
			19	6.587804E-03	1.879778E-02
			20	1.627342E-02	.3305218
			21	1.911632	.4163467
			22	10.06432	.1824898
			23	9.466827E-02	.1249437
			24	10.40139	.1692654
			25	-2.751723E-02	-.1234897
			26	-1.076412E-02	-6.062047E-03
			27	.8522129	.4260211
			28	-6.084442E-04	-5.403129E-02
			29	2.1962B2E-04	1.477936E-02
			30	-.0477432	-.1088637
			31	.2365456	1.271857E-02
2	31.65417	33.84596	3	13.53297	7.427852E-02
			4	516.6991	.5179799
			5	.7932563	.1017486
			6	264.4556	.286492
			7	218.4931	.6873338
			8	6915.823	.228165
			9	29.34282	.4535543
			10	60.21425	.2477964
			11	-.204102E-02	-1.508534E-03
			12	0	1.701412E+38
			13	-.8738212	-3.857893E-02
			14	41.48029	.1390754
			15	-6.938935E-02	-3.189319E-02
			16	4.564652	.1006475
			17	7.610604	.1415943
			18	334.2617	.1660044
			19	2.920784	.3169202
			20	.3620807	.2796476
			21	.6369061	.5.440501E-03
			22	695.471	.4795319
			23	10.20074	.5119484
			24	126.9745	7.857385E-02
			25	.9258175	.1579924

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			26	4.034424E-02	.8.639861E-04
			27	31.16199	.5923696
			28	1.927239E-02	.6.507958E-02
			29	4.970813E-02	.1271978
			30	-1.597469	-.1365124
			31	-25.9054	-.5.296613E-02
3	6.6375	5.405507	4	50.21271	.3151804
			5	.4363961	.3504822
			6	1.142555	.0077501
			7	7.579796	.1492993
			8	473.8882	9.789295E-02
			9	1.864037	.1804065
			10	11.98557	.3088339
			11	.5153122	.0528828
			12	0	1.701412E+38
			13	2.729225E-02	7.544619E-03
			14	-1.601608	-.3.362271E-02
			15	2.651119E-02	7.629655E-02
			16	.4735422	.6.537691E-02
			17	-.6201563	-.7.224339E-02
			18	1.440125	.0044782
			19	-9.063721E-02	-.6.157826E-02
			20	3.916294E-02	.1893875
			21	4.951771	.2567831
			22	-2.353379	-.1.016194E-02
			23	-.1221826	-.3.839497E-02
			24	16.61583	.6.438045E-02
			25	-.178607	-.1908445
			26	-.774374	-.1038356
			27	2.22309	.2646032
			28	-8.915946E-03	-.1885155
			29	6.532863E-03	.1046709
			30	-.1459374	-.7.923065E-02
			31	2.967037	3.798406E-02
4	52.81667	29.59588	5	2.434113	.3570516
			6	248.3446	.3076735
			7	208.5908	.7504136
			8	493195476	.3922332
			10	83.3262	.3921606
			11	3.56015	.6.672945E-02
			12	0	1.701412E+38
			13	-.9377747	-.047348
			14	29.27442	.1122464
			15	7.667542E-04	4.030296E-04
			16	1.785278	4.501703E-02
			17	5.261597	.1119489
			18	14.69287	8.344786E-03
			19	3.567925	.4427328
			20	.2913077	.2572962
			21	16.84766	.1595698
			22	580.7898	.4579658
			23	8.536812	.4899659

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			24	268.5802	.1900689
			25	-.2119532	-.4.136435E-02
			26	1.425568	.3.491312E-02
			27	28.93048	.628925
			28	6.180704E-03	2.386837E-02
			29	.1138998	.3333118
			30	-1.837364	-.182191
			31	-36.76656	-.0860147
5	.2383333	.2313086	6	-.3284664	-.5.206739E-02
			7	.4656675	.2143487
			8	43.70258	.2109732
			9	2.877754E-02	6.508728E-02
			10	.8592992	.5174343
			11	2.390278E-02	5.732407E-02
			12	0	1.701412E+38
			13	2.494422E-02	.1611434
			14	-.2008553	-.9.853872E-02
			15	1.090288E-03	7.332661E-02
			16	5.247188E-02	.1692922
			17	-7.993162E-03	-2.176007E-02
			18	-1.723406	-.1252379
			19	5.470492E-03	8.685442E-02
			20	2.600621E-03	.2938988
			21	.3939027	.4773529
			22	-.4629765	-.4.671029E-02
			23	-.1.599437E-02	-.1174564
			24	.7110596	.0643847
			25	-.8.420281E-03	-.210258
			26	1.094419E-02	3.429445E-02
			27	.1651689	.4594211
			28	-.3.338202E-04	-.1649442
			29	1.582559E-04	5.925529E-02
			30	4.402757E-03	5.585934E-02
			31	-.2195057	-.5.567027E-02
6	17.22083	27.38715	7	112.909	.4389535
			8	2800.089	.1141661
			9	15.5356	.2967669
			10	10.81439	.0549994
			11	5.795174	.1173816
			12	0	1.701412E+38
			13	-.2.349095	-.1281705
			14	14.60986	6.053616E-02
			15	-.5.508614E-02	-.129015E-02
			16	-.1.233399	-.3.360925E-02
			17	2.752415	6.328496E-02
			18	322.5606	.1979723
			19	1.939362	.2600575
			20	4.210973E-02	.0401928
			21	-.14.3542	-.1470202
			22	898.2098	.7653787
			23	11.99016	.7436689
			24	-.86.48272	-.066138
			25	1.08795	.2294457

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			26	-2.213261	-5.857576E-02
			27	8.601818	.2020775
			28	5.712909E-02	.2384112
			29	4.72337E-03	1.493703E-02
7	9.45	9.431409	30	-1.6785762	-9.414464E-02
			31	37.38614	9.446669E-02
			8	3517.399	.4164444
			9	7.862789	.4361485
			10	19.15355	.2828624
			11	1.517918	8.927958E-02
			12	0	1.701412E+38
			13	-.434166	-6.878815E-02
			14	11.63147	.1399502
			15	2.292633E-03	3.781552E-03
			16	.460001	3.639858E-02
			17	1.184792	7.910407E-02
			18	53.81885	9.591746E-02
			19	.9767201	.3803215
			20	7.959753E-02	.2206153
			21	4.447087	.1321726
			22	223.7569	.5536626
			23	3.198013	.575977
			24	50.25336	.1115981
			25	.1073003	6.571159E-02
			26	-.8608303	-6.615659E-02
			27	9.077232	.6192291
			28	7.873073E-03	9.540778E-02
			29	1.432708E-02	.1315649
8	483.9209	899.2933	30	-.6329165	-.1969395
			31	-8.00145	-5.870931E-02
			9	131.3206	7.639512E-02
			10	1067.886	.1653964
			11	1275.507	.7867955
			12	0	1.701412E+38
			13	-.48.20825	-8.010404E-02
			14	660.5821	8.335677E-02
			15	-.157959	-2.732468E-03
			16	31.94751	2.651171E-02
			17	-4560.4862	-8.597991E-02
			18	75.0603	.3065253
			20	12.55892	.3650594
			21	922.5474	.2875608
			22	5430.723	.1409294
			23	87.59091	.1654471
			24	8931.401	.2080111
			25	-.7.564392	-4.858367E-02
			26	4.4552	3.590856E-03
			27	453.7844	.3246554
			28	3.740978E-02	4.754446E-03
			29	1.155468	.1112796
			30	-.28.40112	-9.268236E-02
			31	-755.3516	-5.812495E-02

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
9	4.092875	1.91946	10	2.544041	.1846068
			11	-.1631393	-.4.714766E-02
			12	0	1.701412E+38
			13	.1388369	.1080837
			14	-.0486908	-.2.878613E-03
			15	1.861382E-02	.150858
			16	.3358107	.1305622
			17	1.124671	.3689605
			18	82.73193	.7244926
			19	3.513312E-02	6.721946E-02
			20	2.375694E-02	.323537
			21	.1523514	2.224896E-02
			22	39.94841	.4856974
			23	.5505846	.4872439
			24	-.4.504822	-.4.915492E-02
			25	.1129264	.3398083
			26	4.887104E-02	.0184546
			27	1.250224	.4190668
			28	8.151084E-04	4.853471E-02
			29	4.487857E-04	2.024971E-02
			30	-.6.122351E-02	-.9.360564E-02
			31	-.3853684	-.0138935
10	5.029167	7.209593	11	.4819107	3.707971E-02
			12	0	1.701412E+38
			13	.1990976	4.126575E-02
			14	2.480782	.0390475
			15	3.321219E-02	7.166363E-02
			16	2.358402	.2441234
			17	1.446546	.1263441
			18	9.958496	.0232179
			19	.3845279	.195873
			20	5.929521E-02	.2149916
			21	10.99129	.4273466
			22	22.8288	7.389544E-02
			23	.2720258	6.409156E-02
			24	16.17445	4.698804E-02
			25	-.4.899168E-02	-.9.24906E-02
			26	.2299309	2.311632E-02
			27	5.280258	.4712148
			28	-.8.89197E-04	-.1.409624E-02
			29	-.3.87995E-03	-.4.660948E-02
			30	-.2193403	-.8.928339E-02
			31	-.4.030918	-.3.869083E-02
11	5.191667	1.810226	12	0	1.701412E+38
			13	-.3.569365E-02	-.2.946405E-02
			14	-.8167648	-.5.120114E-02
			15	-.7.982254E-04	-.6.859694E-03
			16	6.652832E-02	2.742685E-02
			17	-.1.079941E-02	-.3.756648E-03
			18	-.8.494079	-.7.887209E-02
			19	6.707311E-03	1.360733E-02
			20	1.944035E-02	.2807268
			21	1.427849	.2211016

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			22	.310105	8.134841E-02
			23	.9.463215E-02	8.879882E-02
			24	.3.867783	4.475047E-02
			25	-.1.135182E-02	-3.622016E-02
			26	.1693056	6.779085E-02
			27	.4420672	.1571194
			28	-.5.233139E-04	-3.304041E-02
			29	-.7.295609E-04	-.034905
			30	-.1.756954E-02	-2.848331E-02
			31	-.1.153782	-4.410681E-02
12	0	0	13	0	1.701412E+38
			14	0	1.701412E+38
			15	0	1.701412E+38
			16	0	1.701412E+38
			17	0	1.701412E+38
			18	0	1.701412E+38
			19	0	1.701412E+38
			20	0	1.701412E+38
			21	0	1.701412E+38
			22	0	1.701412E+38
			23	0	1.701412E+38
			24	0	1.701412E+38
			25	0	1.701412E+38
			26	0	1.701412E+38
			27	0	1.701412E+38
			28	0	1.701412E+38
			29	0	1.701412E+38
			30	0	1.701412E+38
			31	0	1.701412E+38
13	1.316667	.672015	14	-.1.202707	-.2030937
			15	.7.014036E-03	.1623683
			16	.3394446	.3769573
			17	-.2.798581E-02	-2.622361E-02
			18	-.3.111786	-7.783423E-02
			19	-.4.664231E-02	-.2548933
			20	.3.331244E-03	.1295806
			21	.6851392	.2857869
			22	-.2081223	-7.227448E-03
			23	-.5.177379E-02	-.1308677
			24	-.2427798	.7.56659E-03
			25	-.1.566392E-02	-.1346292
			26	.2630558	.2837273
			27	.3649752	.349429
			28	-.1.299262E-03	-.2209703
			29	-.2.868027E-04	-3.696265E-02
			30	.2.930558E-02	.1279777
			31	-.6428461	-.0661977
14	18.0875	.8.849074	15	-.5.036354E-02	-.8.853816E-02
			16	-.1.424789	-.1201586
			17	.1.289639	.9.177059E-02
			18	.70.02564	.1330145
			19	.1.505668	.6248686
			20	-.2.307379E-02	-.8.816065E-02

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			21	-5.046974	-.1598732
			22	57.97394	.1528905
			23	1.193037	.2290116
			24	27.10254	6.414762E-02
			25	.7549441	.492757
			26	-1.364372	-.111755
			27	-1.413029	-.1027372
			28	3.170726E-02	.4095217
			29	7.151336E-03	6.999197E-02
			30	-.2163544	-.7.175145E-02
			31	.4114227	3.217401E-03
15	1.004167	6.455075E-02	16	.0113194	.1308652
			17	.0149827	.1461579
			18	-.3279419	-.0853956
			19	-1.144946E-03	-6.513898E-02
			20	5.005226E-04	.2026913
			21	9.399366E-02	.4081687
			22	-.141716	-.5.123456E-02
			23	-2.007902E-03	-5.283754E-02
			24	3.444672E-02	1.117674E-02
			25	-6.951392E-04	-6.219968E-02
			26	-.0046525	-.0522417
			27	1.222158E-02	.1218149
			28	-2.586655E-05	-4.579873E-02
			29	2.309121E-05	3.098164E-02
			30	-3.819466E-04	-1.736458E-02
			31	-2.643967E-02	-2.834455E-02
16	2.283333	1.345585	17	1.048613E-02	4.90724E-03
			18	-2.775696	-3.467373E-02
			19	-1.902413E-02	-5.192196E-02
			20	1.220211E-02	.2370481
			21	1.054029	.2195754
			22	6.22979	.1080457
			23	-5.695987E-02	-.7.190502E-02
			24	1.413055	2.199462E-02
			25	-1.622778E-02	-6.965713E-02
			26	.3211117	.1729725
			27	.7187419	.3436657
			28	-9.256415E-04	-7.862266E-02
			29	2.368353E-04	1.524383E-02
			30	-1.347208E-02	-2.938234E-02
			31	-.7979851	-4.103916E-02
17	2.404167	1.594703	18	35.87622	.3781522
			19	3.435516E-02	7.911693E-02
			20	1.080053E-02	.1770425
			21	.333993	5.870835E-02
			22	6.499112	.1273035
			23	.1853083	.1973861
			24	-3.713059	-4.876635E-02
			25	8.632174E-02	.3198935
			26	-.1221523	-5.552058E-02
			27	.1183806	4.776117E-02
			28	4.908853E-04	3.518164E-02

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
18	134.7063	59.74114	29	1.281433E-03	.959449E-02
			30	-3.704658E-02	-6.817961E-02
			31	-.8772736	-.806887E-02
			19	1.420784	.733974E-02
			20	7.070732E-02	.0309388
			21	-47.33362	-.222095
			22	936.4829	.3658236
			23	10.30196	.2929193
			24	-720.336	-.2525399
			25	7.471125	.7223209
			26	-.4284363	-.198103E-03
			27	-5.102265	-.494952E-02
			28	.1352699	.2587878
			29	-9.382462E-02	-.1360198
			30	1.53923	.561241E-02
			31	63.31763	.834423E-02
19	.3547916	.2734362	20	1.225807E-05	1.171868E-03
			21	-7.407451E-02	-7.593731E-02
			22	3.956946	.3377143
			23	6.910128E-02	.4292709
			24	3.059906	.23438
			25	1.947892E-02	.4114589
			26	-9.75728E-04	-2.586455E-03
			27	4.797572E-02	.112886
			28	1.163592E-03	.4863631
			29	5.215481E-04	.1651951
			30	-8.897543E-03	-.549419E-02
			31	-.1273232	-.222302E-02
20	5.987504E-02	3.841499E-02	21	4.272169E-02	.3117383
			22	.2077076	.1261819
			23	1.338124E-03	.0591694
			24	.0929234	.066322E-02
			25	-.1.312411E-04	-.0197327
			26	3.264591E-03	6.159709E-02
			27	.0254828	.4267966
			28	-2.589013E-05	-7.702816E-02
			29	1.159731E-04	.261466
			30	-1.488544E-03	-.1137166
			31	-6.837377E-02	-.1231696
21	5.441667	3.582374	32	=29.166817	=1949278
			24	36.46779	.2132097
			25	-.1985601	-.3201391
			26	.219307	4.437247E-02
			27	2.460409	.4418867
			28	-9.241886E-03	-.2948532
			29	-2.344027E-03	-.666967E-02
			30	9.513855E-03	7.793787E-03
			31	-6.386071	-.1233609
22	45.0125	43.02967	23	21.11084	.8333721
			24	-206.5259	-.1005252
			25	2.872163	.3855305
			26	-1.172287	-.974686E-02

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			27	28.48571	.4289254
			28	.1103813	.2931861
			29	1.373494E-02	2.764507E-02
			30	-1.805317	-1.1231256
			31	-6.816803	-1.096295E-02
23	.5819169	.5911694	24	-.4568299	-1.625579E-02
			25	3.057259E-02	.2987019
			26	4.425049E-04	5.425482E-04
			27	.2878412	.3132676
			28	1.426857E-03	.2758574
			29	9.264445E-04	.1210767
			30	-3.038401E-02	-1.1508329
			31	-.3141227	-3.677072E-02
24	34.73333	47.94518	25	-2.199054	-.2649163
			26	-3.531387	-5.338663E-02
			27	14.06318	.1887179
			28	-7.996899E-02	-1.1906307
			29	3.931308E-02	7.101515E-02
			30	-1.629726	-9.975454E-02
			31	-48.29111	-6.970068E-02
25	.2268334	.1738584	26	-1.092213E-02	-4.553485E-02
			27	-.0494037	-.1828261
			28	9.046602E-04	.5947108
			29	-9.422004E-05	-4.693605E-02
			30	3.748581E-03	6.327528E-02
			31	.1678453	6.680795E-02
26	3.116667	1.385419	27	.2127891	9.881948E-02
			28	-.1.390893E-03	-.1147436
			29	1.813255E-03	.113354
			30	.0768056	.1626951
			31	-1.369511	-6.840676E-02
27	2.206792	1.56077	28	-2.277136E-03	-.1667501
			29	5.11352E-04	2.837527E-02
			30	-9.783078E-02	-.1839499
			31	-2.575681	-.1142005
28	1.620832E-02	8.786123E-03	29	1.398879E-05	.1378928
			30	-6.908178E-05	-2.307434E-02
			31	4.103109E-03	3.231697E-02
29	2.445835E-02	1.159456E-02	30	-2.003424E-04	-5.070857E-02
			31	1.474989E-02	8.803371E-02
30	1.091667	.3421767	31	-.3567009	-7.213875E-02
31	8.345833	14.51104			

# OF ROWS = 240

APPENDIX 4  
Frequency Histograms

--> FREHIST (att2temp.dst): C & R Project Toby Claims Soil Samples ( program PAGE 1

0	
15	
30	
45	
60	
75	
90	
105	
120	
135	

----> FREHIST (a:t2temp.dat);

PAGE 1

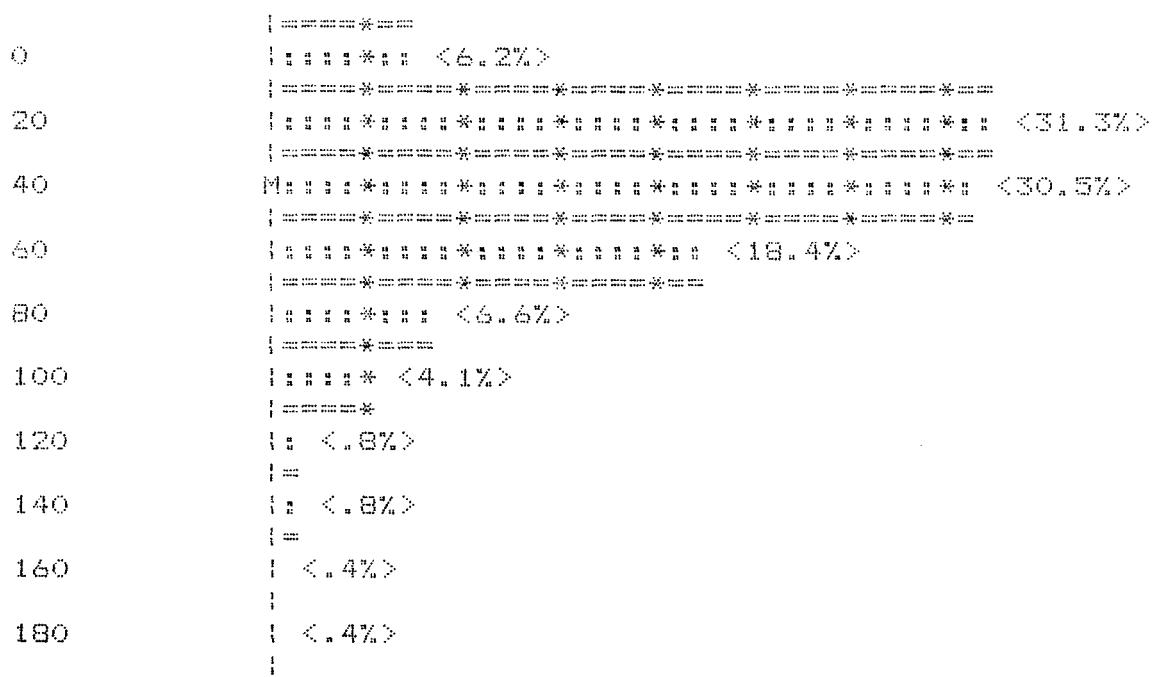
FROM	TO BELOW	FREQ	%	CUMUL	%	
0	15	103	43.4	103	43.4	
15	30	54	22.7	157	66.2	*MEDIAN*
30	45	22	9.2	179	75.5	
45	60	19	8	198	83.5	
60	75	13	5.4	211	89	
75	90	12	5	223	94	
90	105	7	2.9	230	97	
105	120	2	.8	232	97.8	
120	135	4	1.6	236	99.5	
135	150	1	.4	237	100	

MEAN: 30.53798 S-SQUARED: 900.8972 S: 30.01495 SKEWNESS: 1.484601  
S.D. OF MEAN: 1.937457

Low Outliers = 0  
High Outliers = 3

--> FREHIST (at2temp.dat) : C & R Project Toby Claims Soil Samples Zt  
rogram PAGE 4

LOW LIMIT C DX = 20 SCALE = 2:1 3



----> FREHIST (a:t2temp.dat):

PAGE 1

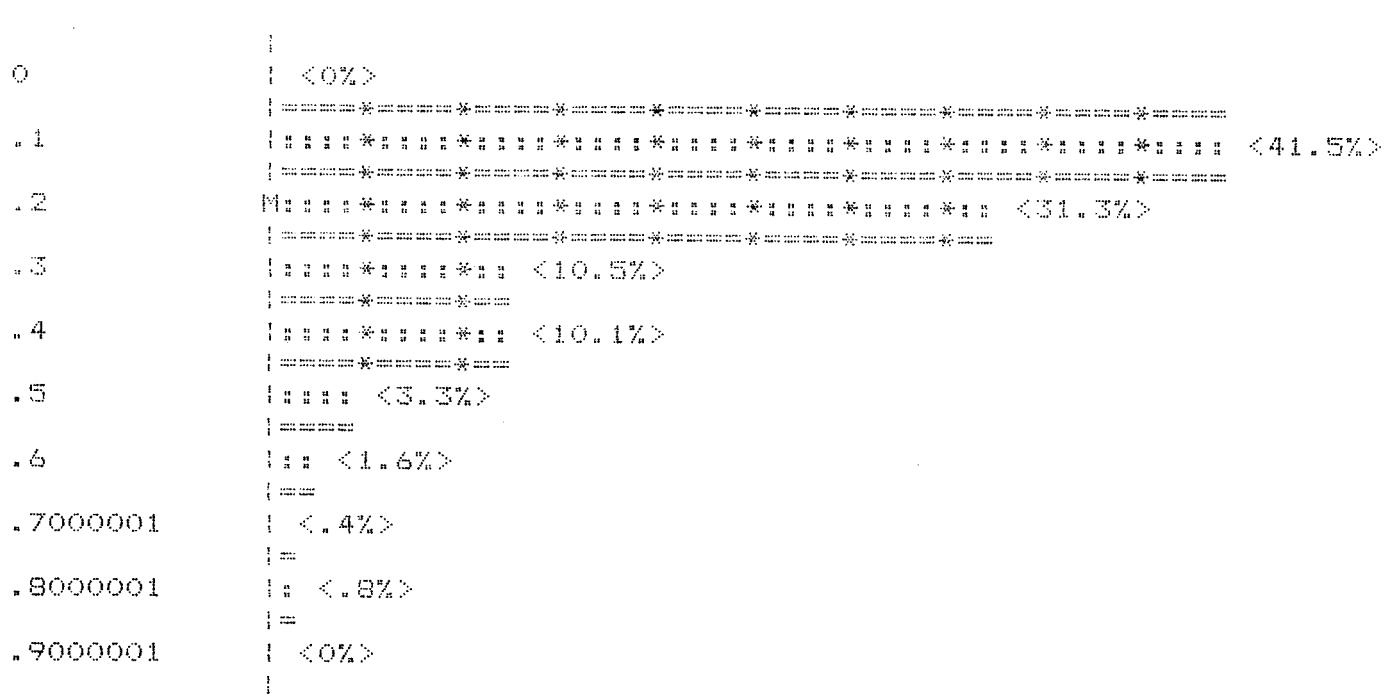
FROM	TO BELOW	FREQ	%	CUMUL	%
0	20	15	6.2	15	6.2
20	40	75	31.3	90	37.6
40	60	73	30.5	163	68.2
60	80	44	18.4	207	86.6
80	100	16	6.6	223	93.3
100	120	10	4.1	233	97.4
120	140	2	.8	235	98.3
140	160	2	.8	237	99.1
160	180	1	.4	238	99.5
180	200	1	.4	239	100

MEAN: 52.67783 S-SQUARED: 829.6492 S: 28.80363 SKEWNESS: 1.378741  
S.D. OF MEAN: 1.859266

Low Outliers = 0

High Outliers = 1

---> FREHIST (at:temp.dat) : C & R Project Toby Claims Soil Samples Ag RH  
ram PAGE 1



----> FREHIST (a:t2temp.dat):

PAGE 1

FROM	TO BELOW	FREQ	%	CUMUL	%
0	.1	0	0	0	0
.1	.2	98	41.5	98	41.5
.2	.3	74	31.3	172	72.8
.3	.4	25	10.5	197	83.4
.4	.5	24	10.1	221	93.6
.5	.6	8	3.3	229	97
.6	.7000001	4	1.6	233	98.7
.7000001	.8000001	1	.4	234	99.1
.8000001	.9000001	2	.8	236	100
.9000001	1	0	0	236	100

MEAN: .2635593 S-SQUARED: .0189687 S: .1377269 SKEWNESS: 1.565664  
S.D. OF MEAN: 8.890234E-03

Low Outliers = 0  
High Outliers = 4

---> FREIGHT (att2temp.dat); C & R Project Toby Claims Soil Samples As  
ocean PAGE 4

(+) LOW LIMIT < DX = 3 SCALE = 4:1 3

----> FREHIST (art2temp.dat):

PAGE 1

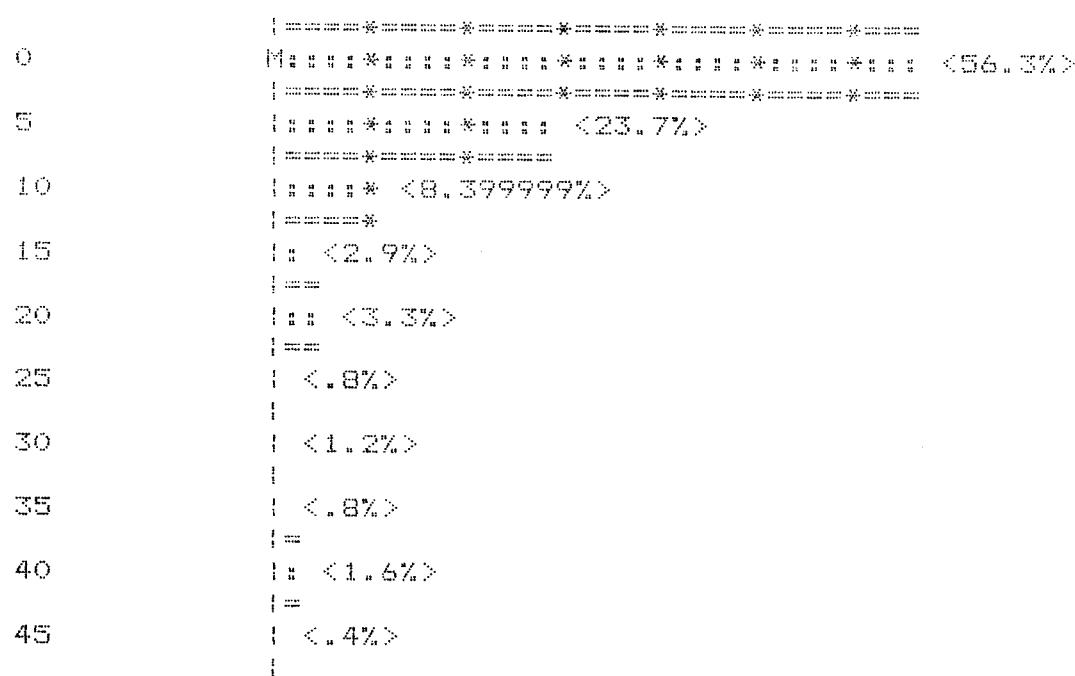
FROM	TO BELOW	FREQ	%	CUMUL	%	
0	3	115	48.5	115	48.5	
3	6	71	29.9	186	78.4	*MEDIAN*
6	9	26	10.9	212	89.4	
9	12	6	2.5	218	91.9	
12	15	7	2.9	225	94.9	
15	18	4	1.6	229	96.6	
18	21	2	.8	231	97.4	
21	24	3	1.2	234	98.7	
24	27	2	.8	236	99.5	
27	30	1	.4	237	100	

MEAN: 4.626582 S-SQUARED: 23.22448 S: 4.819179 SKEWNESS: 2.465882  
S.D. OF MEAN: .3110762

Low Outliers = 0  
High Outliers = 3

----> PREHIST (at2temp.dat) : C & R Project Toby Clime Soil Samples Act PAGE 1

LOW LIMIT = C DX = 5 SCALE = 4.13



----> FREHIST (a:t2temp.dat):

PAGE 1

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	5	133	56.3	133	56.3	*MEDIAN*
5	10	56	23.7	189	80	
10	15	20	8.399999	209	88.5	
15	20	7	2.9	216	91.5	
20	25	8	3.3	224	94.9	
25	30	2	.8	226	95.7	
30	35	3	1.2	229	97	
35	40	2	.8	231	97.8	
40	45	4	1.6	235	99.5	
45	50	1	.4	236	100	

MEAN: 7.415254 S-SQUARED: 73.29791 S: 8.561421 SKEWNESS: 2.543233  
S.D. OF MEAN: .5526373

Low Outliers = 0  
High Outliers = 4

