

86-686-15238

ASSESSMENT REPORT

1986 GEOCHEMICAL SAMPLING AND  
RECONNAISSANCE GEOLOGICAL MAPPING

on the

GOSSAN 1 - 4, 7 CLAIM GROUP

and

GOSSAN 14 - 17, 23 CLAIM GROUP

FILMED

NTS 104 B/10W, 104 B/11E

LIARD MINING DIVISION

owned by Western Canadian Mining (WCM) Ltd.

Operated by Cassiar Mining Corporation

Author: R.E. Meyers  
Date: November 1986  
NTS: 104 B/10W, 104 B/11E  
Commodities: Au, Ag, Zn, Pb  
Latitude: 56° ~~34'~~ North 31.9'  
Longitude: 130° ~~50'~~ West 48.2'

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

15,238

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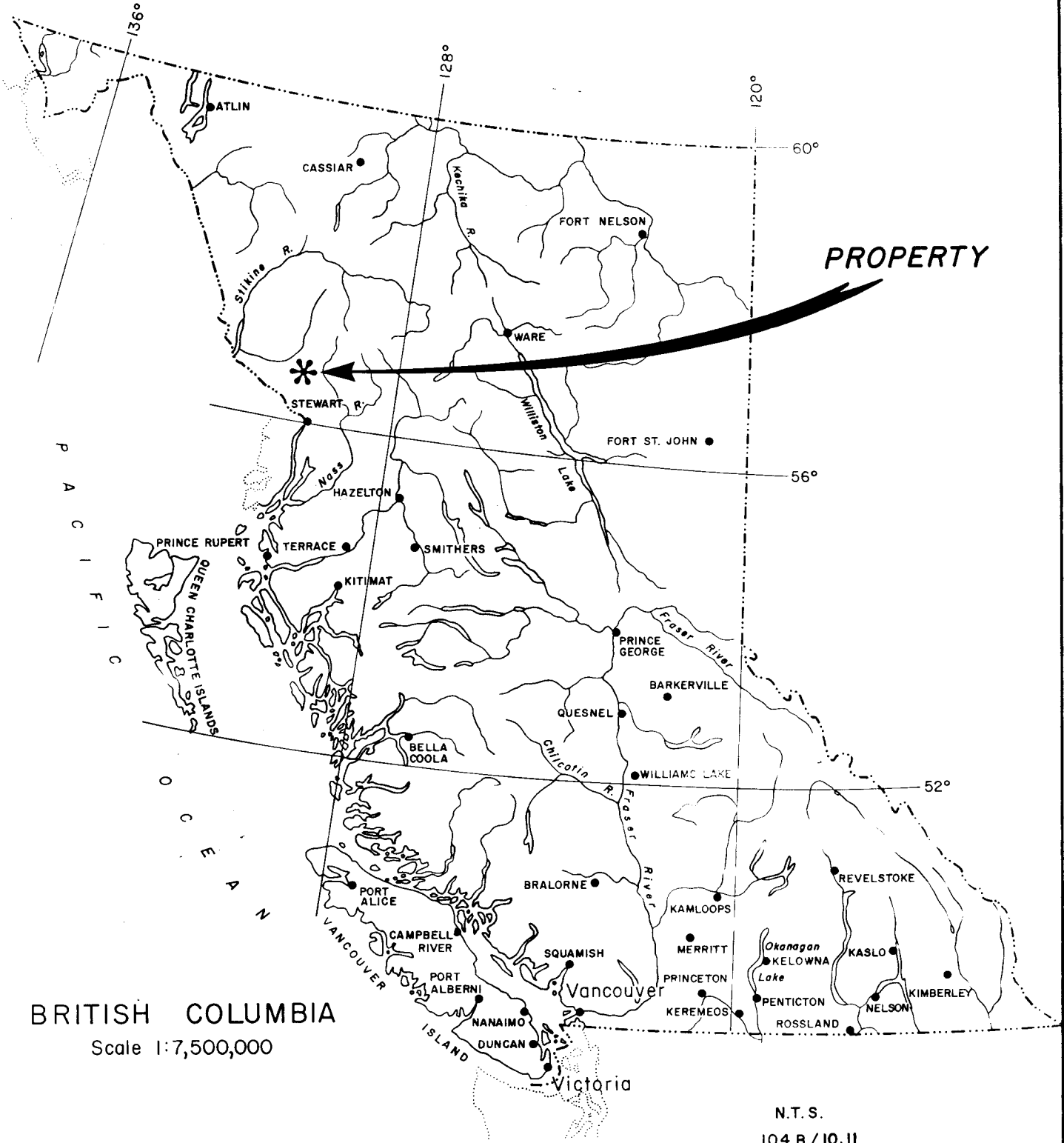
## SUMMARY

The 1986 exploration program on the GOSSAN 1-4, 7, and GOSSAN 14-17, 23 Claim Groups included follow-up geochemical sampling and reconnaissance geological mapping. Objectives were to outline precious metal targets and to determine whether or not the inferred economic potential of the claim groups warranted the planning and financing of future exploration programs.

## CONCLUSIONS AND RECOMMENDATIONS

In general, sampling results were not encouraging for most areas covered. Only a few one-, or two- sample anomalies were outlined. These anomalies are relatively weak and do not constitute high potential precious metal targets. Observed geological features, such as alteration and structure suggest that regional tectonic and associated hydrothermal processes were active and provided favourable environments for precious metals mineralization. However, on a local scale the results of geochemical sampling do not support this potential in the areas sampled.

No further work is recommended on the GOSSAN 1-4, 7 Claim Group. It is suggested that the GOSSAN 14-17, 23 Group be kept in good standing to protect the Wolverine Pb - Zn Showing. At some future time a limited, but detailed exploration program should be undertaken to properly evaluate the mineral potential of this showing.



BRITISH COLUMBIA  
Scale 1:7,500,000

N.T.S.  
104 B / 10, 11



WESTERN CANADIAN MINING LTD.			
GOSSAN CLAIMS			
LOCATION MAP			
DRAWN		DATE	FIGURE
		NOV. 1986	
Revised			I

## INTRODUCTION

### Location, Access and Terrain

The GOSSAN claims are situated in the Coast Ranges of the northern Cordillera, approximately 90 km northwest of Stewart, B.C. at 56° 34' north latitude and 130° 50' west longitude, in the Liard Mining Division (NTS 104B/10/11 Figure 1). The property lies 70 km west of the Stewart - Cassiar highway and about 55 km southwest of Bob Quinn Lake. Access can be gained by fixed wing aircraft to the Snippaker Creek airstrip, located near the southeast boundary of the claims and thence by helicopter to the property.

The claims lie in extremely steep mountainous country, south of the confluence of the Iskut River and Snippaker Creek. Elevations range from 600 metres to 2000 metres in steep alpine terrain, characterized by precipitous ridges, broad ice fields and valley glaciers. Tree line is at approximately 800 metres, below which spruce, fir, alder, and devils' club predominate.

### History

Interest in the area underlying the GOSSAN and surrounding claims dates back to 1907, when gold, silver, and galena bearing mineralization was discovered near Johnny Mountain by the Iskut Mining Company. Only scanty information is available covering subsequent activities until 1954-61, when Hudson's Bay Mining and Smelting carried out drilling programs in the same area. Since then the district has been explored for base and precious metals at both regional and property scales by various mining companies, including Skyline Exploration Ltd., Silver Standard Mines Ltd., Texasgulf Inc., Great Plains Developments, Cobre Explorations, Teck Corporation, and Dupont Canada Ltd.

In 1983 Lonestar Resources Ltd. commissioned Active Mineral Explorations Ltd. to carry out a reconnaissance geological mapping and geochemical sampling program (Bending, 1983). As a result of this program the GOSSAN claims were staked by Mr. C. Graf and a number of them were optioned to Brinco Mining Limited and subsequently transferred to Western Canadian Mining (WCM) Ltd. in 1986. Aggressive exploration has been continued in the immediate area of the GOSSAN claims, notably by Skyline Exploration Ltd. and by Cominco Ltd.

#### Claims Status (Figure 2)

The GOSSAN 3, 4, 7, 14, and 16 claims are 100% owned by Western Canadian Mining (WCM) Ltd. With the application of the 1986 assessment work all claims are in good standing until August 24, 1988.

CLAIM	RECORD #	UNITS	HECTARES	EXPIRY DATE
Gossan 3	2394	20	500	24/08/88
Gossan 4	2395	20	500	24/08/88
Gossan 7	2398	20	500	24/08/88
Gossan 14	2405	18	450	24/08/88
Gossan 16	2407	10	250	24/08/88

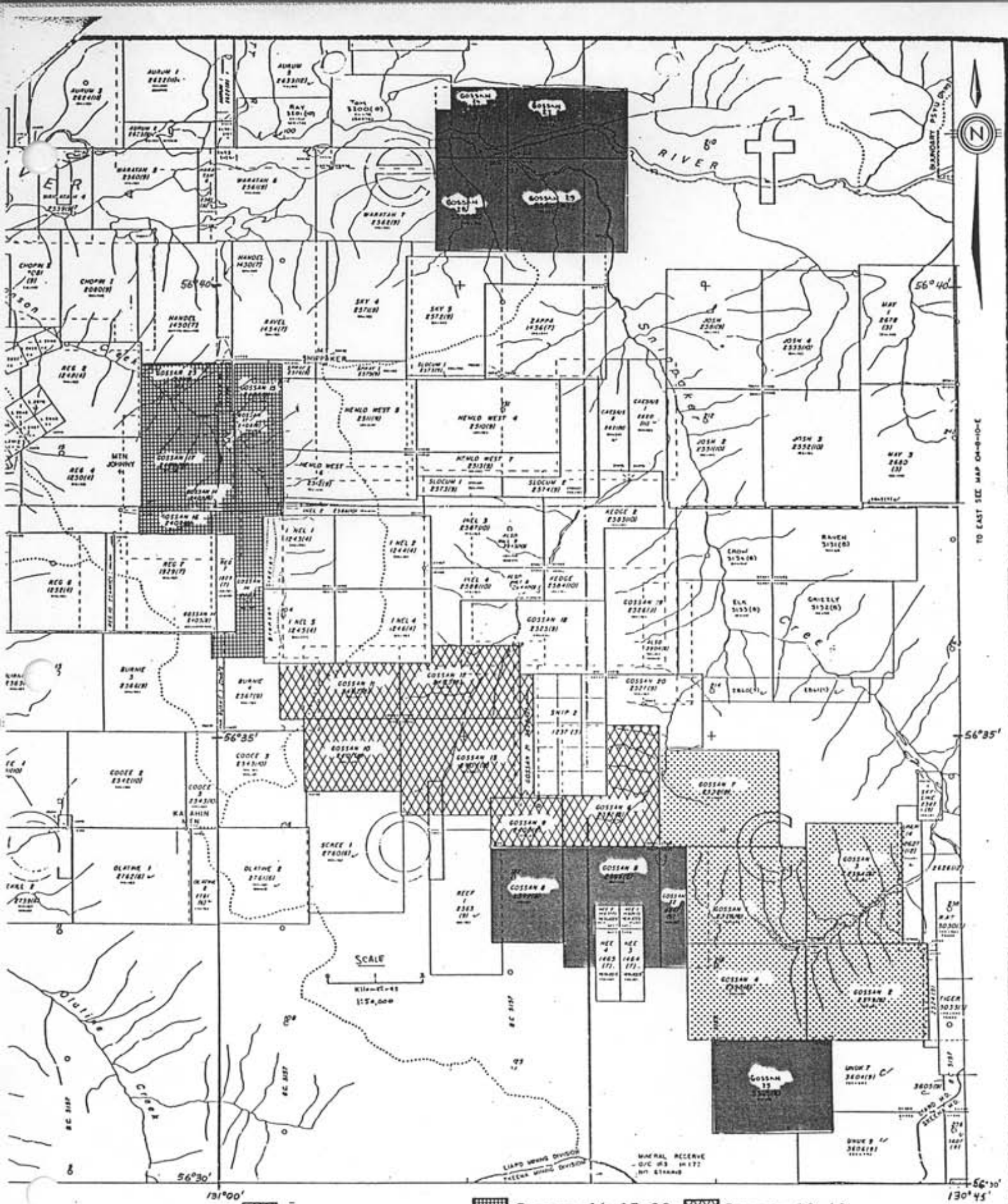
#### CLAIM GROUPINGS

GOSSAN 1-4, 7 GROUP  
GOSSAN 14-17, 23 GROUP

A statement of Costs for the 1986 exploration program may be found in Appendix 1.

#### 1986 Exploration Program

Exploration activities in 1986 on the GOSSAN 3, 4, 7, 14, and 16 claims consisted of follow up geochemical sampling in areas partially covered in 1983. The objectives of the 1986 work were to evaluate the precious metals potential of the claims and to determine whether



Liard M.D. - N.T.S. 104B/10W&11E

- Gossan 1-4,7
- Gossan 14-17,23
- Gossan 10-13
- Claims not Grouped.

GROUPS

Figure 2

Scale  
0 1 2 km

**Brinco**

LIMITED

Gossan Claims

May '86



additional work should be planned in light of their strategic proximity to known mineralization on other claims in the area.

#### REGIONAL GEOLOGY (Figure 3)

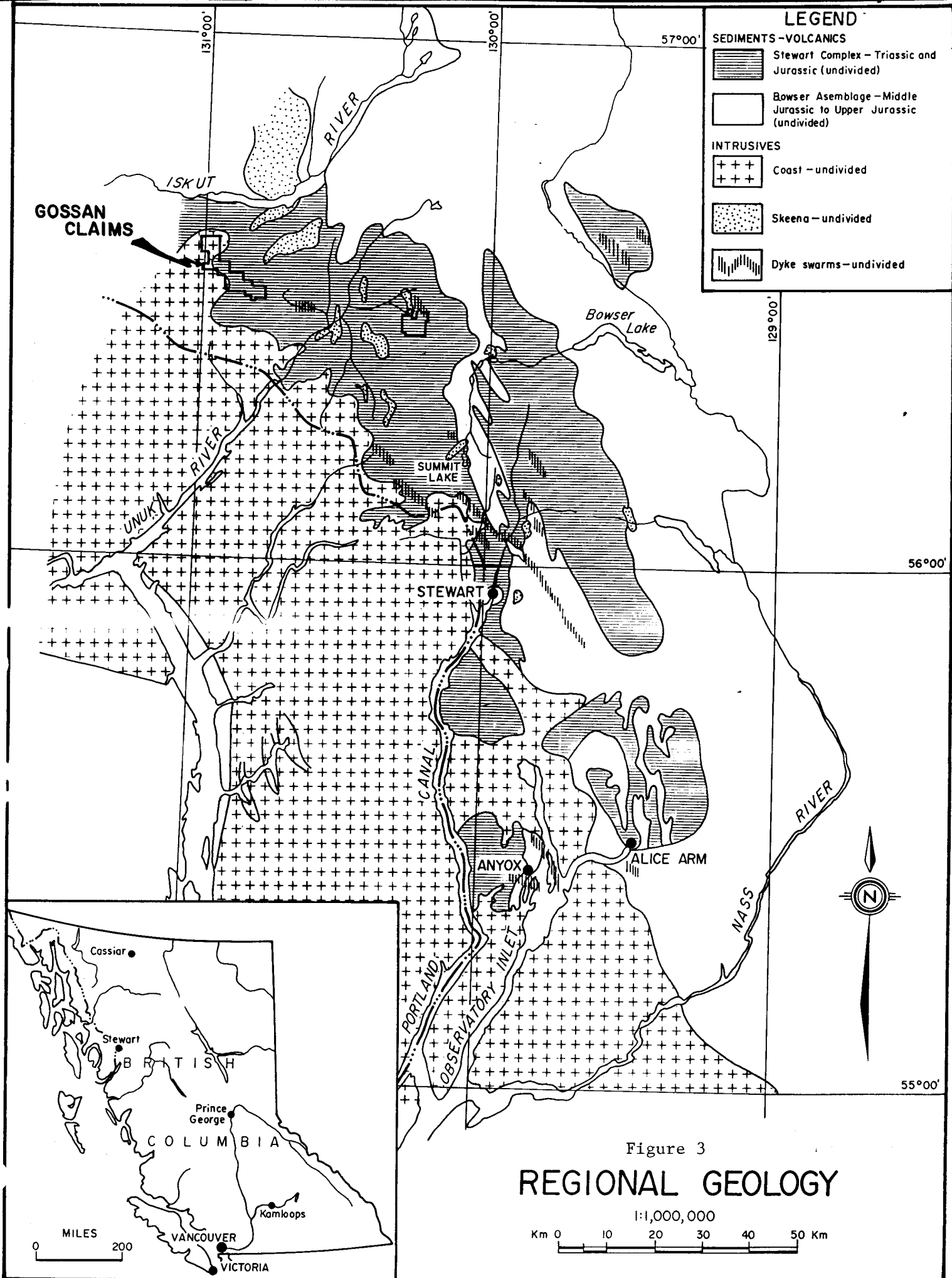
The GOSSAN property lies at the eastern edge of the Coast Plutonic Complex, near the western boundary of the Bowser Basin. The claims are at the northern end of a belt rocks described by Grove (1971) as the Stewart Complex. The complex consists of an undivided group of sedimentary and volcanic rocks of Upper Triassic and Jurassic age, which are intruded by middle Mesozoic marginal phases of the Coast Range intrusions.

The stratified rocks are composed of submarine and subaerial fragmental volcanic rocks that are interlayered with sequences of argillite, banded siltstone, greywacke, conglomerate and minor impure limestone, most of which are believed correlative with the Lower Jurassic Hazelton Group. Some of the lowermost members may correspond to the Upper Triassic Stuhini and King Salmon Groups, which also occur in the region.

The stratigraphy is intruded by subvolcanic intrusives and by mid to late Mesozoic and Cenozoic plutonic rocks. These include stocks and dykes of granodiorite, quartz monzonite, syenodiorite and feldspar porphyry, as well as late Tertiary dykes and plugs of basalt and diorite.

#### PROPERTY GEOLOGY

Several reconnaissance geological "prospecting" traverses were carried out in conjunction with the geochemical sampling program. Major lithological units were mapped and rock samples were collected wherever warranted by alteration or mineralization. Geological observations are described below by claim area and in the sequence they were mapped.



GOSSAN 3, GOSSAN 4, GOSSAN 7 Area (Figure 4b)

In the southwestern corner of Gossan 3 claim most bedrock exposures lie above 725 metre elevation, where andesitic volcanic rocks are overlain by a tuffaceous and argillaceous sedimentary sequence. The andesites are at least 100 metres thick and consist of massive flows and interlayered tuff. The massive lavas are fine to medium grained, generally non-porphyrific, with moderate fracturing and jointing. They are medium grey-green, chloritic, with a locally developed schistosity. Tuffaceous sections usually display diffuse banding or layering subparallel to contacts. Fragment size is generally less than 2 mm, but a few narrow bands of lapilli tuff ( $>4$ mm) are also present.

The volcanic rocks are overlain in this area by a unit of massive to weakly banded siltstone. The lower contact is poorly exposed, but the unit is probably 150-200 metres thick. Massive sections are light greenish grey, brown weathering and weakly calcareous. Banded siltstone has alternating 1 to 4 cm light and dark grey brown layers. Weakly graded beds and soft-sediment slumping suggest that tops are right-side up.

A thick unit of black argillite overlies the siltstone. The argillite is massive, highly fractured, with a blocky appearance and tends to form steep irregular cliffs. Texturally, it is fine grained, slightly phyllitic, with poor but definite bedding/cleavage development. On Gossan 3 the unit is locally "shot through" with fine, irregular calcite stringers and veinlets. Minor pyrite content ( $<1\%$ ) has resulted in a mottled, orange-brown, somewhat "baked" weathered surface.

Two kilometres to the southwest, the southern half of Gossan 4 claim is underlain by altered, bright orange "rusty" exposures of granodiorite to diorite intrusive rocks. They are likely related to the Coast Range intrusive complex. In this area

the rocks are medium to coarse grained, well jointed and quite strongly sheared and altered in places. Much of the outcrop is decomposed, with clay, sericite and minor epidote alteration, resulting from the breakdown of feldspars. Mafic minerals are chloritized and there is about 5 to 15% residual quartz. Veining is generally weak, with scattered quartz-carbonate stringers. Sulphide content is typically low (<1%)

The central part of Gossan 7 claim is underlain by granodiorite and diorite intrusives of similar character to those described above. A broad, northwest trending shear and fracture zone cross-cuts the intrusive and is displayed as a bright rusty alteration zone. Pyrite content is sporadic, locally up to 5%. Minor malachite and traces of chalcopyrite occur near the eastern edge of the altered shear zone. To the west and down slope from the zone an ice rafted boulder of fragmental andesite (2m) contains bands or layers of semi-massive pyrite with minor chalcopyrite. Further down slope a narrow, iron stained fault zone has bluish-green malachite and azurite copper staining.

#### GOSSAN 14, GOSSAN 16 Area (Figure 5b)

Work in the area was limited to three traverses on the western side of Bronson Glacier. The stratigraphy consists of a lowermost unit of grey and brown banded siltstone which strikes northwesterly, dips moderately to the west and is conformably overlain by comparatively narrow units of basalt, andesite, argillite and tuffaceous greywacke.

The siltstone is a competent, massive, well banded calcareous sedimentary unit of about 300 to 400 metres thickness. It contains local concentrations of disseminated pyrite with minor occurrences of galena and sphalerite. Oxidation has caused much of this unit to weather orange brown which, in places, masks the rhythmic, 1 to 3 cm thick layering. A notable lead-zinc occurrence, known as the Wolverine showing (Figure 5b), was previously reported by Bending (1983).

A narrow 30 to 50 metre section of fine grained, very dark greenish black basalt locally overlies the siltstone and is partially interlayered with a well fractured and moderately sheared black argillite. The argillaceous rocks are weakly calcareous and similar to the argillite described on Gossan 3 claim.

Andesitic volcanic rocks overlie the argillite and basalt and include massive, fine grained flow rocks and medium to coarse tuff and breccia. They are typically greyish green, moderately chloritized and contain ~10% feldspar phenocrysts. The fragmental rocks consist of weakly stratified lapilli ash tuff, containing silicic and feldspathic fragments (<1cm), a coarser lapilli tuff (>1cm) and a section of agglomeratic block breccia. Neither the andesites, nor basalts display any obvious features of mineralization, as is reflected in geochemical sampling results.

The uppermost unit encountered in this area overlies the andesites and is a rusty weathering, grey tuffaceous greywacke. This rock contains about 60% quartz and 25% feldspar fragments, with up to 5% disseminated pyrite. The unit is highly fractured and has a crudely developed cleavage. Sampling results for precious metals in this unit are equally low.

## GEOCHEMICAL SAMPLING

### Procedures

A total of 418 geochemical samples were collected, including 310 soil/talus samples, 12 silt samples and 96 rock samples. Samples were collected in areas warranted by geological reconnaissance. Most soil and talus sample lines were placed parallel to topographic contours at 100 metre spacing, with sample sites spaced at 50 metres apart. Silt samples were collected wherever active streams were encountered. Wherever possible, the B soil horizon was sampled.

Rock samples were collected randomly where warranted by alteration, or mineralization. In some areas, detailed rock chip sample lines were placed over areas displaying widespread alteration.

Soil, silt, and talus samples were collected in wet-strength kraft paper sample envelopes. Each sample was dried and shipped to Acme Analytical Laboratories in Vancouver. Samples were then seived and the -80 mesh fraction was analysed. Rock samples were pulverized prior to analysis. All samples were geochemical analysed for gold and by Inductively Coupled Plasma (ICP) for 30 elements. Analytical results are tabled in Appendix 2.

#### Results

In general, the analytical results for precious metals were not encouraging. In the southeastern area of Gossan 3, there were only 4 soil samples with Au  $> 100$ ppb. Two of these were adjacent (115, 250 ppb), while the other two were single sample anomalies and widely separated.

There were no significant precious metals anomalies on Gossan 4, and only one single sample anomaly on Gossan 7. Two rock samples collected from this claim were marginally encouraging. All other sample results from this claim group were generally erratic.

Precious metals results on Gossan 14 and 16 were equally low, with no significant anomalies.

REFERENCES

- Bending, D.A. 1983. Summary Report of the 1983 Field Program.  
GOSSAN CLAIMS 1 - 23, SNIP 2 CLAIM.  
Snippaker Creek Area, B.C.  
Unpublished Report for Lonestar Resources Ltd.
- Grove, E.W. 1971. Geology and Mineral Deposits of the Stewart  
Area, British Columbia. B.C. Department of Mines and  
Petroleum Resources, Bulletin No. 58.

APPENDIX 1

STATEMENT OF COSTS



STATEMENT OF COSTS

GOSSAN 1-4, 7 CLAIM GROUP

GOSSAN 14-17, 23 CLAIM GROUP

FIELD LABOUR COSTS

Project Geologist, R.E. Meyers - 15 days @ \$170 =	\$2550.00
(June 23 - July 7)	
Field Assistant, E. Alionis - 14 days @ \$125 =	1750.00
(June 23 - July 6)	
Junior Geologist, S. Casselman - 15 days @ \$95 =	1425.00
(June 23 - July 7)	
Student Assistant, T. McIntyre - 15 days @ \$75 =	1125.00
(June 23 - July 7)	
TOTAL LABOUR	<u>\$6850.00</u>

GEOCHEMICAL COSTS

95 Rock sample prep. @ 3.00 =	\$ 285.00
<u>337</u> Soil/talus prep. @ .75 =	252.75
Total <u>432</u> Au + ICP Analysis @10.00 =	4320.00
TOTAL ANALYTICAL COSTS	4857.75

SHIPPING CHARGES

Bus Express \$66.70	
Freightways 67.85	
TOTAL SHIPPING	134.55

AIR CHARTERS

Fixed Wing (Trans Provincial) 50% of \$5912 =	\$2956.00
Helicopter (Northern Mt.) 7.1 hrs. @ \$547.50 =	3887.25
TOTAL AIR CHARTERS	6843.25

CAMP COSTS

5-man crew (including pilot), 15 days @ \$60/man-day (includes food, accommodation, camp gear, fuel, communications, expediting)	4500.00
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TRAVEL EXPENSES

Truck Rental, Vancouver-Terrace	\$ 668.00
Fuel	250.00
Hotel, meals, 2 nights @ \$60, 4 men	480.00
2 Van.-Terrace rtn. airfares @ \$345	<u>690.00</u>
TOTAL TRAVEL (50% apportionment) of	\$2088.00 = 1044.00

REPORT PREPARATION

R. Meyers, 3 days @ \$170	\$510	
Drafting, 10 hrs. @ \$20	200	
Maps and materials	<u>100</u>	
TOTAL		<u>810.00</u>

TOTAL ASSESSMENT COSTS		<u><u>\$25,039.55</u></u>
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APPORTIONMENT OF COSTS

GOSSAN 1-4, 7 Group, 68%	\$17,026.89
GOSSAN 14-17, 23 Group 32%	8,012.66

APPENDIX 2

TABLE OF GEOCHEMICAL DATA

GOSIAN  
ASSESSMENT 1986

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SN, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.  
SAMPLE TYPE: P1-7 SOILS -BOMESH PG-9 ROCKS AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JULY 10 1986 DATE REPORT MAILED: July 15/86 ASSAYER: D. J. DEAN TOYE. CERTIFIED B.C. ASSAYER.

CASSIAR MINING PROJECT - 8310 FILE # 86-1409

PAGE 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPB
686S 501	4	41	19	81	.1	20	15	707	6.35	7	7	ND	1	29	1	2	2	125	.44	.092	7	44	1.10	38	.41	7	2.51	.05	.05	1	3
686S 502	3	56	15	90	.5	24	16	810	7.12	17	8	ND	1	34	1	2	2	118	.51	.104	5	49	1.42	29	.31	6	2.64	.11	.10	1	4
686S 503	2	40	8	44	2.9	16	11	329	6.49	11	7	ND	1	21	1	2	2	97	.35	.120	7	30	.36	26	.47	6	1.60	.04	.04	1	8
686S 504	2	50	15	44	.4	13	10	249	6.13	13	5	ND	1	16	1	2	2	130	.22	.115	7	44	.31	29	.38	4	1.15	.03	.04	2	9
686S 505	2	57	10	55	.8	16	9	230	4.17	14	5	ND	1	19	1	2	2	58	.26	.168	8	33	.41	39	.17	6	1.42	.04	.04	1	9
686S 506	2	44	16	114	.3	33	28	1377	6.20	26	8	ND	1	110	1	2	2	105	1.46	.112	8	31	1.99	68	.46	4	2.57	.55	.22	1	7
686L 507	3	78	19	163	.5	51	31	1481	6.71	47	5	ND	1	47	1	2	2	96	.80	.135	10	49	2.05	49	.16	7	2.31	.08	.08	1	16
686S 508	2	32	11	60	.1	20	12	353	7.39	20	7	ND	2	23	1	3	2	138	.31	.271	5	37	.82	35	.51	4	1.45	.07	.05	1	4
686S 509	2	37	15	93	.2	23	15	1015	7.02	33	5	ND	1	42	1	3	3	100	1.04	.311	4	49	1.18	58	.15	7	1.82	.08	.12	1	5
686S 510	2	34	16	116	.1	30	24	1810	5.60	21	5	ND	1	55	1	3	2	102	.99	.155	8	43	1.81	61	.26	3	2.25	.19	.11	1	9
686S 511	4	59	26	149	.4	40	33	2492	6.80	41	5	ND	1	19	1	3	2	85	.35	.129	13	47	1.62	41	.11	3	2.25	.02	.06	1	110
686S 512	3	47	22	124	.2	33	29	2181	6.14	27	5	ND	1	43	1	2	2	88	.59	.195	11	41	1.65	40	.24	2	2.14	.17	.10	1	8
686S 513	3	66	39	135	.7	24	32	3408	6.97	28	5	ND	1	22	1	2	2	51	.26	.108	19	24	.89	40	.11	3	2.03	.08	.07	1	34
686S 514	4	92	38	185	1.0	42	46	4095	8.10	39	5	ND	1	27	1	2	2	60	.38	.184	24	22	1.05	47	.09	3	2.24	.07	.07	1	70
686S 515	3	86	34	173	1.9	41	42	3845	7.30	39	5	ND	1	22	1	2	2	54	.28	.180	21	21	1.09	39	.12	3	2.28	.07	.07	1	61
686S 516	6	146	37	271	.9	68	44	3738	8.58	47	5	ND	1	48	1	2	2	44	.77	.158	26	21	.95	99	.08	4	1.94	.04	.08	1	45
686S 517	5	131	31	252	.4	55	46	3173	8.23	33	5	ND	1	54	2	2	2	55	.70	.140	24	23	1.08	84	.13	3	2.04	.11	.10	1	50
686L 518	5	82	19	171	.2	43	25	1667	4.98	14	5	ND	1	76	1	2	2	49	1.15	.139	14	22	1.06	72	.18	4	1.56	.15	.11	1	12
686L 519	5	66	15	135	.2	32	22	1233	4.08	13	13	ND	1	126	1	2	2	60	2.29	.118	9	20	1.03	93	.31	8	1.55	.31	.16	1	44
686S 520	5	55	16	91	.1	24	18	1041	3.57	14	5	ND	1	55	1	2	3	54	.73	.156	10	31	.96	75	.11	2	1.35	.05	.13	1	32
686S 521	4	66	13	158	.3	41	33	2298	6.24	19	7	ND	1	132	1	2	2	93	1.67	.131	15	29	1.67	119	.49	3	2.61	.58	.27	1	16
686S 522	5	75	22	169	.3	45	32	2414	6.50	28	5	ND	1	92	1	2	2	74	1.11	.133	15	28	1.44	121	.34	5	2.28	.36	.17	1	17
686S 523	5	118	31	246	.4	67	44	3872	7.99	32	5	ND	1	36	1	3	2	53	.54	.132	21	24	1.18	75	.09	5	2.27	.06	.07	1	20
686S 524	7	112	28	233	.6	58	44	3396	7.77	39	5	ND	1	40	1	2	2	49	.59	.148	18	28	1.10	71	.09	9	2.08	.05	.08	1	27
686T 525	3	81	20	184	.1	44	28	3490	6.05	18	9	ND	1	84	1	3	2	27	2.88	.128	11	12	.81	47	.05	2	1.62	.03	.09	1	12
686S 526	1	287	12	111	.6	73	74	2548	8.30	55	11	ND	1	93	1	2	2	136	3.70	.082	5	32	2.08	53	.28	3	3.00	.28	.11	1	7
686L 527	7	240	38	386	.5	140	61	5021	9.95	32	13	ND	2	78	1	2	3	23	3.46	.141	16	10	.76	63	.04	6	1.54	.01	.05	1	24
686S 528	7	270	46	387	.8	154	63	5658	10.82	45	9	ND	1	76	1	3	5	32	2.51	.131	28	13	.81	104	.08	7	1.66	.06	.06	1	37
686T 529	5	163	36	286	.3	89	45	3699	8.26	28	10	ND	1	110	1	2	2	29	4.76	.130	16	10	.84	56	.11	5	1.50	.09	.07	1	31
686S 530	8	276	49	405	.8	155	80	6689	12.08	50	6	ND	1	59	2	3	8	39	1.30	.163	38	14	.96	93	.04	8	1.99	.04	.04	1	21
686S 531	3	49	16	144	.2	28	26	1630	5.20	4	10	ND	1	135	1	2	2	71	2.51	.123	16	7	1.02	65	.43	2	2.01	.47	.17	1	1
686S 532	6	220	42	321	.9	118	62	5950	9.93	34	5	ND	1	58	1	2	2	36	.97	.150	37	17	.83	115	.04	4	1.86	.01	.06	1	47
686L 533	5	116	33	229	.7	55	34	2471	7.43	40	6	ND	1	57	1	4	2	32	1.49	.147	20	16	.77	100	.04	2	1.66	.03	.10	1	43
686S 534	7	170	53	238	1.3	74	59	5728	9.99	59	5	ND	1	14	1	2	5	37	.18	.149	35	15	.91	83	.01	6	2.21	.01	.05	1	70
686S 535	2	66	32	178	.9	38	38	3692	6.40	26	5	ND	1	60	1	2	2	60	1.54	.120	18	20	1.11	58	.23	5	1.69	.16	.09	1	35
686T 536	5	125	74	223	2.2	60	57	7784	8.63	48	5	ND	1	8	1	3	2	40	.07	.167	26	20	.79	47	.04	6	3.00	.01	.05	1	115
STD C/AU-0.5	21	56	38	131	7.1	68	30	1108	3.96	39	18	7	33	49	18	17	20	63	.48	.100	37	62	.88	181	.08	39	1.72	.07	.14	15	480

R. Meyers

CASSIAR MINING PROJECT - 8310 FILE # 86-1409

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
686S 537	2	65	54	202	.6	39	40	4214	7.04	26	5	ND	1	99	1	2	2	80	1.67	.134	20	30	1.45	88	.34	2	2.24	.39	.17	1	250
686S 538	26	137	53	609	.9	103	53	3465	10.95	47	5	ND	1	22	6	3	5	61	.38	.174	34	35	1.24	64	.08	2	2.30	.02	.09	1	12
686S 539	23	65	34	248	.5	37	26	1932	8.53	25	5	ND	1	26	1	2	2	65	.36	.219	23	35	.95	32	.13	2	1.82	.07	.08	1	9
686S 540	21	35	23	159	.1	19	10	501	7.09	18	5	ND	1	12	1	2	2	98	.16	.419	16	19	.26	32	.21	3	.82	.03	.10	1	4
686S 541	1	25	6	108	.1	24	27	1229	5.88	8	5	ND	1	163	1	2	2	122	2.03	.111	18	27	2.01	87	.74	2	2.65	.86	.31	1	5
686S 542	2	53	20	134	.3	33	36	1999	6.43	24	5	ND	1	102	1	2	2	106	1.50	.143	20	38	1.87	83	.41	2	2.42	.43	.18	1	8
686S 543	2	45	11	126	.1	29	30	1324	6.52	11	5	ND	1	100	1	2	2	118	1.51	.113	17	40	2.04	58	.46	2	2.58	.44	.19	1	5
686S 544	5	21	16	70	.1	5	9	615	6.30	9	5	ND	2	45	1	6	2	88	.34	.070	22	29	.46	51	.26	2	2.07	.07	.07	1	3
686S 545	2	17	16	72	.1	5	9	500	7.15	4	5	ND	3	32	1	2	2	174	.32	.122	16	27	.46	73	.96	2	2.03	.08	.06	1	9
686S 546	6	25	20	80	1.7	7	10	1544	10.39	6	5	ND	3	24	1	2	2	132	.26	.213	23	32	.29	39	.46	2	1.80	.04	.06	1	7
686S 547	4	34	17	96	.4	5	13	1738	7.69	7	5	ND	2	14	1	2	2	93	.16	.241	22	24	.34	35	.40	2	3.03	.05	.06	1	5
686S 548	4	29	16	87	1.0	8	9	704	7.48	9	5	ND	2	26	1	2	2	170	.31	.265	11	24	.24	37	.48	2	1.00	.04	.09	1	3
686S 549	7	38	15	85	.3	6	10	1026	7.78	14	5	ND	2	21	1	4	2	104	.17	.274	22	30	.30	29	.26	2	1.61	.05	.07	1	11
686L 550	4	60	32	198	.5	35	27	4740	5.59	19	5	ND	1	44	1	2	2	40	.60	.132	28	14	.63	128	.06	2	1.82	.07	.13	1	17
686S 551	2	128	14	77	.3	17	24	1594	9.60	15	5	ND	1	30	1	2	2	272	.31	.120	9	78	.60	53	.49	4	1.68	.05	.04	1	9
686S 552	5	35	25	103	.1	7	15	3007	6.48	17	5	ND	1	29	1	3	2	88	.24	.128	18	22	.36	72	.27	2	2.47	.05	.06	1	2
686L 553	8	32	36	111	.3	6	13	2520	4.31	4	5	ND	1	68	1	2	2	77	.63	.137	27	13	.59	247	.24	2	2.33	.11	.10	1	4
686S 554	3	28	35	66	.1	3	9	524	3.85	2	5	ND	2	65	1	2	2	109	.48	.088	11	12	.53	106	.36	2	1.92	.10	.07	1	1
686S 555	2	27	16	102	.1	8	15	2014	4.15	2	5	ND	1	95	1	2	2	102	1.16	.118	10	15	.86	213	.33	4	1.91	.22	.12	1	1
686S 556	4	22	12	72	.1	5	11	734	6.01	4	5	ND	4	46	1	3	2	109	.45	.084	18	21	.58	55	.62	5	3.79	.09	.07	1	1
686S 557	4	39	28	103	.1	5	12	2730	4.80	3	5	ND	2	93	1	2	2	108	.67	.141	12	15	.63	189	.23	4	2.17	.09	.11	1	1
686S 558	10	29	53	60	.3	2	7	672	4.40	3	5	ND	6	61	1	2	2	150	.32	.063	15	15	.28	97	.70	3	1.43	.05	.06	1	3
686S 559	12	50	30	87	.4	2	9	834	4.89	3	14	ND	3	114	1	2	4	107	1.52	.083	13	23	.75	322	.25	4	2.01	.10	.14	1	3
686L 560	3	51	43	101	.1	1	9	1694	2.62	2	5	ND	2	139	1	2	2	55	1.01	.160	18	7	.82	155	.16	2	1.79	.07	.08	1	2
686S 561	3	25	6	68	1.0	11	17	1470	4.62	2	5	ND	1	117	1	2	2	104	1.18	.128	11	15	1.48	62	.71	4	1.92	.57	.20	1	1
686S 562	4	44	25	64	.3	1	7	659	5.42	5	5	ND	6	55	1	5	2	74	.37	.091	21	9	.27	78	.30	5	1.89	.07	.07	1	2
686S 563	5	58	22	45	1.9	5	8	279	3.65	2	5	ND	1	43	1	2	2	57	.35	.121	22	12	.39	35	.27	2	2.92	.14	.07	2	2
686S 564	16	30	15	73	.2	4	10	2287	3.32	2	7	ND	1	136	1	2	2	68	1.75	.111	14	8	.58	195	.25	2	1.51	.13	.09	2	1
686S 565	4	18	4	78	.4	15	14	517	4.38	2	5	ND	1	113	1	2	2	84	1.20	.137	14	13	1.19	68	.54	2	2.43	.54	.20	1	1
686S 566	4	149	18	132	.2	24	26	1848	4.51	8	5	ND	4	80	1	2	2	91	1.00	.165	9	64	1.68	255	.21	2	2.17	.05	.29	1	10
686S 567	15	211	14	120	.3	21	70	4429	6.15	11	5	ND	6	71	1	2	2	67	.52	.200	13	46	1.39	194	.12	2	3.10	.02	.20	1	14
686T 568	26	198	18	105	.1	14	92	4560	7.99	10	5	ND	11	70	1	2	2	59	.30	.266	11	31	1.20	182	.11	5	3.15	.01	.12	1	12
686S 569	10	155	12	120	.1	27	43	2050	5.58	11	5	ND	4	60	1	2	3	86	.62	.180	7	65	1.59	164	.19	3	2.76	.03	.27	1	3
686T 570	1	155	10	142	.1	32	27	1267	4.66	13	5	ND	2	70	1	2	2	116	1.13	.160	5	80	2.08	249	.25	2	2.46	.06	.46	1	2
686T 571	6	149	9	117	.1	26	38	3305	3.89	7	5	ND	5	62	1	2	2	65	.72	.167	19	47	1.39	286	.11	3	2.40	.02	.17	1	5
686T 572	5	174	12	143	.2	38	38	2787	3.95	7	5	ND	5	84	1	2	2	79	.90	.145	12	88	1.80	254	.16	2	2.79	.02	.31	1	4
STD C/AU-0.5	20	59	41	138	7.0	74	29	1168	3.94	42	19	7	35	50	18	15	19	67	.47	.108	37	68	.87	187	.09	35	1.72	.07	.15	14	485

CASSIAR MINING PROJECT - B310 FILE # 86-1409

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	R PPM	Al %	Na %	K %	W PPM	Au PPB
686T 573	6	192	13	153	.4	55	45	1672	4.96	17	5	ND	2	69	1	2	2	96	.98	.144	14	123	2.37	163	.20	8	2.86	.05	.28	1	4
686T 574	16	186	18	128	.4	28	51	3610	4.35	8	5	ND	5	84	1	2	2	66	.95	.170	20	59	1.54	544	.11	2	3.15	.02	.22	1	2
686T 575	17	219	19	165	.4	31	46	3770	3.42	6	5	ND	6	132	2	2	3	59	1.19	.143	24	48	1.50	261	.12	2	2.74	.02	.26	1	5
686T 576	8	133	20	135	.4	34	32	1556	4.51	12	5	ND	3	69	1	2	2	85	1.02	.160	12	81	1.84	159	.17	2	2.56	.04	.29	1	6
686T 577	13	159	21	148	.4	34	34	1597	5.51	15	5	ND	3	68	1	2	2	88	.96	.176	11	78	1.85	157	.18	2	2.59	.04	.28	1	10
686T 578	9	140	22	144	.3	36	31	1377	5.32	15	5	ND	3	87	1	2	2	83	1.01	.196	15	80	1.79	303	.19	2	2.25	.03	.28	1	8
686T 579	7	133	18	108	.1	22	23	957	4.02	12	5	ND	4	60	1	2	4	53	.82	.141	9	49	1.27	85	.12	2	1.56	.02	.19	1	7
686T 580	11	220	20	127	.4	21	35	1484	4.12	16	5	ND	3	68	1	2	2	51	.79	.153	12	43	1.20	110	.11	2	1.85	.02	.16	1	5
686T 581	8	176	24	151	.4	24	29	1372	5.20	21	5	ND	3	49	1	2	2	67	.59	.141	10	56	1.43	89	.13	4	2.06	.02	.17	2	7
686T 582	7	151	23	149	.4	26	31	1566	4.78	19	5	ND	3	60	1	2	2	65	.65	.165	9	60	1.47	95	.14	5	2.07	.03	.19	1	11
686T 583	36	220	25	143	.6	26	64	6467	4.32	10	5	ND	9	121	1	2	2	67	.78	.158	23	52	1.78	236	.13	3	3.31	.03	.20	1	6
686T 584	31	94	25	89	.3	8	43	1678	7.39	5	5	ND	12	50	1	2	3	41	.41	.217	5	22	1.27	69	.06	2	1.72	.01	.05	1	8
686T 585	13	168	30	187	.6	42	52	2622	7.17	22	5	ND	4	57	1	2	2	89	.48	.186	8	95	1.86	162	.17	4	3.08	.03	.19	1	16
686T 586	10	108	34	154	.5	32	51	1892	7.54	16	5	ND	6	109	1	2	2	79	.39	.272	18	49	1.51	413	.20	3	2.67	.02	.26	1	9
686T 587	12	138	22	107	.6	22	65	2699	8.53	14	5	ND	8	94	1	2	7	65	.38	.259	10	38	1.31	297	.17	4	2.61	.02	.20	1	13
686T 588	9	79	32	115	.4	22	33	1169	8.17	16	5	ND	8	80	1	2	4	80	.27	.234	11	47	1.27	267	.20	3	2.52	.02	.20	1	11
686T 589	12	124	25	132	.4	35	60	2980	7.15	20	5	ND	5	103	1	2	2	68	.36	.250	16	42	1.37	329	.17	3	2.64	.02	.19	1	12
686T 590	17	85	18	79	.4	18	46	1816	8.29	7	10	ND	9	82	1	2	5	47	.26	.304	7	16	1.15	197	.10	3	2.22	.02	.10	1	14
686T 591	12	100	12	76	.2	21	41	1392	7.25	5	6	ND	8	99	1	2	4	51	.22	.293	9	24	1.08	215	.12	2	2.79	.01	.09	1	10
686T 592	15	383	17	138	.6	36	111	6953	6.59	11	7	ND	11	39	1	2	9	26	.26	.166	39	21	.99	482	.03	2	3.00	.01	.07	1	17
686T 593	15	559	23	148	.7	42	107	4638	6.32	11	5	ND	3	46	1	2	3	69	.57	.163	16	84	1.61	200	.13	2	6.78	.02	.22	1	7
686T 594	9	266	18	79	.5	11	94	4046	13.63	4	5	ND	15	18	1	2	4	44	.18	.388	2	22	1.14	112	.03	2	2.49	.01	.09	1	11
686T 595	5	124	21	88	.4	18	78	3750	8.02	5	5	ND	8	39	1	2	4	33	.52	.193	9	33	.85	358	.02	6	1.38	.02	.09	1	5
686T 596	22	246	16	119	.3	29	33	942	9.84	17	5	ND	7	38	1	2	3	84	.25	.271	6	75	1.76	130	.12	2	2.63	.02	.16	1	13
686T 597	22	277	26	129	.4	64	146	4219	11.14	13	7	ND	10	104	1	2	2	113	.32	.434	31	60	1.68	901	.31	3	3.61	.02	.33	1	6
686T 598	19	185	15	70	.2	21	44	1292	10.01	9	5	ND	13	54	1	2	3	80	.17	.290	4	29	.97	462	.17	8	2.46	.01	.10	1	5
686S 1001	2	33	11	55	.6	11	11	306	7.40	3	6	ND	2	21	1	2	2	143	.36	.232	6	30	.69	33	.70	2	1.93	.08	.06	1	8
686S 1002	2	45	10	50	.6	11	9	251	4.29	10	5	ND	1	27	1	2	2	63	.39	.178	4	28	.39	22	.14	6	1.33	.08	.05	1	4
686S 1003	2	38	15	99	.5	21	27	1200	5.01	15	5	ND	1	66	1	2	2	95	.84	.107	14	35	1.29	76	.24	5	2.24	.25	.11	1	5
686S 1004	3	72	15	131	.4	39	29	1271	6.43	26	5	ND	1	24	1	3	2	110	.34	.128	13	59	1.87	58	.18	2	3.04	.05	.07	1	6
686S 1005	2	51	15	79	.7	22	14	712	5.52	19	5	ND	1	42	1	4	2	94	.74	.147	9	39	1.20	41	.24	3	2.01	.15	.08	1	2
686S 1006	2	43	14	97	.5	22	19	902	5.72	24	5	ND	1	59	1	4	2	103	1.90	.146	10	37	1.44	46	.28	3	2.08	.22	.11	1	4
686L 1007	3	73	23	156	.5	50	28	1713	6.53	39	5	ND	1	42	1	4	2	94	.91	.136	13	54	2.09	59	.16	2	2.30	.06	.09	1	6
686S 1008	3	64	26	163	.7	39	30	1548	6.62	48	5	ND	1	21	1	5	2	101	.43	.161	13	49	1.82	38	.13	7	2.41	.02	.08	1	5
686S 1009	1	43	8	80	.2	31	18	808	4.97	37	5	ND	1	44	1	5	2	77	.45	.095	8	31	1.01	38	.18	2	1.24	.15	.08	1	2
686S 1010	3	55	21	150	.4	39	30	1628	6.34	32	5	ND	1	31	1	3	2	92	.62	.140	14	45	1.81	45	.18	3	2.30	.07	.07	1	10
STD C/AU-0.5	21	56	39	133	7.0	69	30	1123	3.97	38	18	7	34	49	17	15	18	64	.48	.104	38	63	.88	184	.09	40	1.72	.07	.13	14	485

## CASSIAR MINING PROJECT - 8310 FILE # 86-1409

PAGE 4

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
686S 1011	1	112	44	194	1.6	42	33	2702	6.94	35	6	ND	1	28	1	4	2	34	.62	.134	9	28	1.01	54	.04	6	1.44	.01	.07	1	21
686S 1012	1	120	45	217	1.1	54	38	4113	7.42	29	5	ND	1	23	1	2	2	38	.46	.156	16	25	1.07	35	.04	5	1.88	.01	.09	1	18
686S 1013	1	76	25	190	.5	34	37	2814	7.44	16	10	ND	1	143	1	2	2	101	1.99	.153	10	28	1.81	97	.54	2	2.68	.75	.26	1	23
686S 1014	1	102	40	216	1.0	44	44	4441	7.43	29	5	ND	1	40	1	2	2	58	.56	.172	14	26	1.18	68	.13	2	2.10	.13	.10	1	42
686S 1015	1	71	27	141	1.3	26	26	2235	6.95	33	5	ND	1	33	1	2	2	60	.39	.184	10	28	.84	47	.12	2	1.98	.10	.07	1	26
686S 1016	5	125	37	243	.6	42	43	3436	10.69	38	5	ND	1	58	1	3	5	51	1.02	.183	23	33	.91	80	.06	9	1.89	.02	.08	1	33
686S 1017	4	117	34	190	.7	26	31	2213	9.15	28	5	ND	1	27	1	3	5	47	.30	.243	33	22	.73	32	.15	2	2.15	.09	.07	1	3
686L 1018	1	37	19	93	.2	16	15	937	7.98	8	11	ND	2	39	1	2	2	102	.42	.353	8	25	.64	32	.46	2	1.39	.15	.08	1	2
686S 1019	5	109	40	261	.4	54	56	7595	9.62	26	6	ND	1	33	1	3	3	36	.53	.201	24	23	.84	73	.05	8	2.07	.04	.07	1	12
686S 1020	2	42	21	86	.1	11	12	1269	7.74	14	5	ND	2	16	1	2	3	102	.23	.500	4	29	.58	19	.24	3	1.32	.02	.06	1	2
686S 1021	2	32	19	97	.1	11	13	3348	8.51	8	5	ND	1	18	1	2	2	95	.23	.198	2	29	.89	46	.27	9	1.82	.02	.05	1	5
686S 1022	2	69	38	113	.6	16	15	797	10.19	22	6	ND	1	30	1	2	2	87	.35	.193	11	32	.66	26	.34	5	1.48	.09	.08	1	3
686S 1023	1	97	19	184	.5	35	41	3426	6.91	29	15	ND	2	173	1	2	2	107	4.45	.109	7	38	1.82	50	.12	8	2.67	.10	.07	1	6
686S 1024	6	110	36	219	.6	49	38	3577	7.68	43	5	ND	1	32	1	3	3	57	.37	.189	16	48	1.34	95	.04	3	2.33	.02	.10	1	21
686S 1025	6	95	36	203	.6	48	33	2947	6.67	48	5	ND	1	41	1	3	5	46	.91	.162	16	41	1.13	86	.04	7	1.97	.02	.10	2	18
686S 1026	5	72	34	189	.2	43	35	3512	6.97	38	5	ND	1	35	1	2	3	68	.45	.190	11	57	1.51	66	.14	2	2.27	.08	.09	1	24
686S 1027	1	60	12	121	.2	17	26	1185	5.45	7	5	ND	1	126	1	2	2	98	1.32	.147	7	32	1.53	96	.54	2	2.52	.60	.26	1	8
686S 1028	3	88	16	120	.1	18	24	1252	4.75	12	5	ND	2	59	1	2	4	74	.58	.158	8	44	1.27	73	.22	2	1.92	.15	.16	1	5
686S 1029	18	232	60	205	.4	37	48	2027	6.85	33	5	ND	4	35	1	2	2	56	.23	.180	17	57	1.13	119	.09	3	2.21	.03	.10	1	23
686L 1030	11	181	45	206	.5	38	39	1677	5.26	23	5	ND	2	68	2	2	2	46	.68	.155	12	50	1.03	132	.10	5	1.75	.07	.09	1	42
686S 1031	18	255	58	217	.6	47	56	2602	6.41	37	5	ND	4	43	2	2	5	47	.34	.173	17	53	1.01	194	.07	2	1.93	.02	.09	2	22
686S 1032	15	230	53	199	.7	45	47	2228	6.03	27	5	ND	4	40	1	2	2	52	.37	.173	17	66	1.19	176	.08	5	1.99	.02	.10	1	20
686L 1033	15	240	44	209	.5	38	44	1861	6.11	31	5	ND	3	53	2	2	2	41	.39	.161	16	48	.97	161	.06	6	1.81	.03	.09	1	22
686S 1034	10	179	42	159	.6	35	38	1550	5.54	24	5	ND	2	47	1	2	4	60	.40	.135	15	56	1.18	141	.18	2	2.07	.12	.10	1	48
686S 1035	1	31	11	65	.3	86	21	565	4.08	3	5	ND	1	25	1	2	2	88	.40	.113	2	103	2.42	32	.42	5	1.98	.07	.06	1	5
686S 1036	2	41	20	65	.4	27	12	389	5.06	7	5	ND	1	24	1	2	3	87	.22	.428	4	128	.69	28	.24	3	1.08	.03	.07	1	3
686S 1037	5	61	30	89	1.0	10	9	412	5.05	17	5	ND	1	28	1	2	2	59	.18	.195	13	50	.33	30	.03	3	1.17	.02	.06	1	9
686S 1038	1	18	11	29	.1	13	4	227	1.47	8	5	ND	1	9	1	3	2	18	.07	.055	8	12	.22	8	.01	3	.39	.01	.02	4	14
686L 1039	8	98	34	199	.4	47	28	2353	6.94	57	5	ND	1	49	1	3	3	46	.97	.161	16	48	1.16	76	.05	2	1.84	.04	.09	2	26
686S 1040	2	37	15	84	.6	8	11	378	7.03	8	5	ND	1	41	1	2	2	125	.38	.210	8	23	.42	39	.57	4	1.49	.10	.06	1	10
686S 1041	3	149	35	302	.7	76	52	4514	8.71	35	5	ND	1	65	1	2	6	51	1.65	.161	24	26	1.16	90	.08	6	2.30	.05	.08	1	17
686S 1042	6	54	45	154	.1	14	79	15211	9.47	24	5	ND	1	27	1	2	8	47	.31	.726	17	22	.74	55	.07	6	1.97	.05	.09	1	18
686S 1043	4	45	19	73	.6	8	12	621	6.09	19	5	ND	2	52	1	2	2	113	.37	.119	7	30	.79	43	.35	2	1.53	.08	.06	1	11
686S 1044	4	44	23	61	.6	8	10	406	6.14	18	5	ND	2	32	1	2	2	130	.25	.215	6	44	.70	44	.43	2	1.60	.02	.05	1	6
686S 1045	12	36	16	69	.9	6	10	345	10.92	8	5	ND	4	29	1	2	4	116	.22	.095	20	29	.29	41	.62	6	1.71	.07	.06	1	1
686S 1046	3	63	27	133	.7	12	19	1496	6.02	22	5	ND	1	35	1	2	2	108	.27	.108	8	73	1.27	54	.27	2	2.95	.04	.08	2	5
STD C/AU-0.5	21	59	41	135	7.0	68	31	1153	3.94	42	19	7	35	51	19	15	19	66	.48	.112	38	67	.87	189	.09	37	1.72	.07	.13	13	510

## CASSIAR MINING PROJECT -- 8310 FILE # 86-1409

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	AuI PPB
686S 1047	2	22	12	58	.5	8	9	195	5.42	2	5	ND	1	41	1	3	2	110	.30	.130	10	25	.47	51	.59	6	4.30	.05	.03	2	1
686S 1048	17	47	20	70	.5	3	14	1585	8.73	4	5	ND	5	99	1	2	2	64	.15	.211	14	27	.80	106	.13	9	2.27	.05	.09	1	50
686S 1049	5	77	16	95	.8	18	13	463	8.63	22	5	ND	2	30	1	2	2	146	.20	.080	10	59	.84	45	.43	5	3.53	.02	.07	1	7
686S 1050	14	105	24	125	.8	16	19	762	7.54	13	5	ND	4	42	1	2	2	89	.21	.123	10	55	1.30	91	.15	6	3.10	.04	.10	1	8
686S 1051	14	196	22	108	.2	9	33	1600	10.50	17	5	ND	3	97	1	2	4	92	.25	.227	12	21	1.43	140	.15	7	2.95	.06	.05	1	18
686T 1052	5	213	28	182	.5	29	37	1966	5.86	11	5	ND	4	95	1	2	2	100	1.09	.181	11	68	2.01	197	.21	5	2.55	.05	.27	1	10
686T 1053	4	166	18	154	.1	42	31	1516	5.12	11	5	ND	2	86	1	2	3	107	1.57	.169	9	93	2.17	203	.20	5	2.51	.04	.37	1	9
686T 1054	3	177	19	177	.2	38	33	1528	5.45	12	5	ND	2	82	1	2	2	115	1.35	.171	11	85	2.19	220	.21	6	2.68	.06	.43	1	7
686T 1055	2	161	17	157	.1	38	31	1238	5.20	13	5	ND	1	78	1	2	2	120	1.77	.163	9	89	2.27	200	.22	5	2.65	.06	.43	1	16
686T 1056	2	180	14	175	.2	43	33	1452	5.79	13	5	ND	1	78	1	2	2	136	1.39	.178	11	99	2.49	254	.25	3	2.95	.06	.51	1	7
686T 1057	3	180	25	173	.3	39	31	1340	5.53	15	5	ND	2	85	1	2	2	128	1.58	.189	11	87	2.22	250	.24	8	2.77	.08	.48	1	8
686T 1058	5	203	30	225	.3	39	40	2270	6.47	13	5	ND	4	84	1	2	2	125	1.15	.188	15	86	2.37	233	.23	6	3.04	.05	.40	1	4
686T 1059	9	158	50	208	.3	25	30	2645	5.19	8	5	ND	7	77	1	2	5	76	.89	.181	21	55	1.60	324	.14	9	2.23	.02	.22	1	170
686T 1060	5	107	31	167	.2	21	23	2092	4.29	12	5	ND	5	95	1	2	2	81	1.11	.192	15	49	1.59	205	.15	3	2.10	.04	.27	1	18
686T 1061	6	88	26	136	.1	17	23	2227	3.74	8	5	ND	4	107	1	2	2	67	1.50	.179	13	39	1.30	324	.14	5	1.79	.04	.25	1	16
686S 1501	2	51	22	65	.2	16	12	550	9.17	6	5	ND	2	26	1	3	2	123	.36	.134	17	27	.65	23	.64	10	1.85	.07	.05	1	8
686S 1502	2	50	13	54	.4	8	13	677	7.83	9	7	ND	2	21	1	3	2	122	.30	.193	22	27	.57	21	.64	5	4.06	.06	.05	1	7
686S 1503	5	184	38	332	.3	103	66	7037	9.37	21	5	ND	2	136	1	2	2	67	2.54	.143	28	15	1.20	103	.32	6	2.22	.40	.14	1	16
686S 1504	9	154	67	373	.7	127	74	10508	12.42	47	5	ND	1	36	1	3	4	29	.81	.196	51	15	.82	94	.02	8	2.04	.02	.05	1	30
686S 1505	7	180	49	387	.5	94	77	5985	10.03	33	8	ND	1	104	2	2	2	40	2.59	.191	38	11	.72	99	.13	11	1.86	.18	.08	1	10
686S 1506	8	161	48	328	.7	72	86	6368	13.16	41	5	ND	1	13	2	4	9	41	.10	.254	48	17	.86	54	.02	8	2.80	.02	.05	1	12
686S 1507	4	102	30	229	1.0	52	50	4208	8.24	37	5	ND	1	126	1	2	2	74	2.22	.151	23	17	1.23	90	.32	3	2.32	.46	.17	1	36
686S 1508	2	82	32	220	.9	46	40	3581	6.76	30	8	ND	1	102	1	2	2	76	2.53	.135	16	19	1.36	94	.30	6	2.12	.37	.16	1	37
686S 1509	3	68	53	193	1.0	31	39	4748	7.97	27	5	ND	1	53	1	5	2	56	.64	.176	18	19	1.12	65	.18	5	1.91	.20	.12	1	26
686S 1510	2	40	24	141	.3	26	34	2355	6.68	11	10	ND	2	178	1	2	2	107	3.02	.117	14	21	1.84	100	.57	6	2.71	.87	.30	1	14
686S 1511	1	37	14	128	.4	25	36	2146	6.38	13	11	ND	1	174	1	2	2	116	2.57	.138	12	21	2.00	99	.65	5	2.82	.95	.32	1	10
686S 1512	4	24	9	121	.2	20	27	1149	6.36	3	5	ND	1	166	1	2	2	119	2.17	.132	12	22	2.01	83	.68	7	2.52	.92	.31	1	4
686S 1513	3	36	16	109	.1	25	24	1185	5.57	29	5	ND	1	55	1	3	2	90	.74	.122	11	35	1.58	45	.26	2	2.02	.18	.10	1	7
686L 1514	2	58	23	132	.6	42	24	1597	6.03	31	5	ND	2	65	1	4	2	86	1.67	.135	13	48	2.00	54	.15	8	2.19	.06	.12	1	7
686S 1515	1	34	14	130	.1	20	34	1589	6.56	11	5	ND	1	162	1	2	2	122	2.22	.142	13	23	2.06	86	.56	6	2.96	.85	.29	1	7
686S 1516	2	59	11	84	.7	16	21	822	5.61	17	5	ND	1	58	1	2	2	97	.81	.148	14	33	.97	50	.21	2	2.05	.20	.10	1	1
686S 1517	7	47	32	81	.2	7	29	3992	11.47	14	6	ND	1	20	1	6	5	73	.17	.165	19	27	.44	33	.13	9	2.42	.09	.08	1	10
686S 1518	10	31	25	75	.8	3	7	467	10.28	14	6	ND	10	18	1	2	2	62	.19	.110	28	21	.15	36	.40	11	2.57	.04	.05	2	5
686S 1519	5	38	26	87	.4	8	22	4345	7.83	17	5	ND	1	33	1	3	2	64	.20	.157	25	17	.47	52	.09	5	3.05	.05	.06	1	7
686S 1520	3	31	12	73	1.6	5	13	1074	7.72	7	5	ND	3	28	1	3	2	152	.34	.091	16	26	.57	41	.69	5	4.16	.09	.06	1	3
686S 1521	6	18	21	67	.2	3	8	512	7.24	11	8	ND	4	30	1	7	2	63	.19	.062	24	17	.32	29	.30	8	2.43	.03	.05	1	11
STD C/AU 0.5	22	58	36	134	7.0	73	31	1135	3.93	40	16	7	34	51	18	15	18	66	.48	.103	39	65	.88	188	.08	36	1.72	.07	.13	14	510



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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au1 PPB
686S 1522	2	37	18	74	.1	14	13	665	4.31	4	5	ND	3	84	1	2	3	68	.50	.072	12	16	.83	65	.20	4	1.98	.06	.08	2	1
686L 1523	2	29	22	114	.9	13	27	2281	4.34	3	5	ND	1	80	1	2	2	73	.80	.143	39	16	.75	138	.28	11	3.42	.24	.13	1	1
686S 1524	3	29	24	80	.4	20	18	1293	5.51	7	5	ND	2	115	1	2	2	119	1.15	.116	11	23	1.10	132	.49	5	1.95	.42	.19	1	1
686S 1525	3	17	18	37	.1	4	7	202	4.95	2	5	ND	2	57	1	2	2	100	.30	.051	5	14	.20	41	.44	2	1.62	.04	.04	1	4
686L 1526	1	19	9	107	.1	10	14	1426	3.51	6	5	ND	6	124	1	2	2	72	.63	.081	15	13	1.00	102	.15	2	2.01	.05	.08	1	1
686S 1527	2	27	13	65	.3	7	15	2291	4.96	2	5	ND	1	81	1	2	2	107	.67	.150	9	16	.65	87	.41	2	1.82	.21	.11	1	1
686S 1528	2	22	3	48	.6	8	12	490	7.03	2	5	ND	2	26	1	2	6	138	.32	.087	13	22	.60	28	.93	3	3.62	.07	.04	1	1
686S 1529	3	12	14	38	.3	6	8	310	3.96	2	5	ND	1	51	1	2	2	89	.22	.072	7	13	.25	49	.33	5	1.54	.03	.03	1	24
686S 1530	3	30	14	49	.3	7	6	258	3.19	2	5	ND	2	49	1	2	2	82	.26	.062	16	10	.14	49	.48	6	.84	.03	.04	1	2
686S 1531	2	8	11	38	.2	4	6	414	3.11	2	5	ND	1	125	1	2	2	88	.52	.140	3	12	.24	80	.49	4	1.06	.06	.04	1	1
686S 1532	1	14	18	77	.3	18	21	781	5.13	5	5	ND	3	162	1	2	2	115	1.63	.118	6	19	1.63	90	.72	4	2.21	.69	.24	1	1
686S 1533	1	19	8	71	.2	16	17	502	4.02	3	5	ND	1	120	1	2	2	91	1.24	.082	5	18	1.17	112	.54	2	1.86	.43	.16	1	1
686S 1534	2	15	13	75	.2	13	17	544	4.16	3	5	ND	1	148	1	2	6	96	1.36	.084	7	12	1.26	80	.54	2	2.05	.59	.21	1	1
686S 1535	10	8	22	58	.3	5	6	400	7.83	7	5	ND	3	13	1	2	4	51	.11	.056	19	15	.09	24	.29	6	2.65	.04	.05	1	1
686S 1536	2	11	14	54	.2	7	9	482	3.86	2	5	ND	4	87	1	2	2	96	.59	.075	5	13	.59	71	.64	2	1.73	.20	.09	1	1
686S 1537	4	7	13	38	.1	2	6	309	2.89	3	5	ND	1	55	1	2	2	58	.35	.057	5	7	.37	38	.26	2	1.42	.13	.06	1	1
686S 1538	5	19	6	67	.6	7	9	963	5.45	2	8	ND	4	55	1	2	3	89	.26	.108	6	15	.39	44	.41	4	2.69	.04	.04	1	1
686S 1539	12	15	9	44	.2	3	7	399	5.31	2	5	ND	1	42	1	3	2	68	.20	.085	8	13	.25	46	.22	4	2.16	.02	.05	1	1
686S 1540	10	18	18	37	.3	4	4	155	4.72	4	5	ND	3	23	1	5	2	102	.13	.055	12	14	.14	45	.46	2	1.44	.02	.03	1	1
686T 1541	3	153	16	136	.2	36	28	1370	4.75	11	5	ND	2	76	1	2	2	91	1.07	.164	5	72	1.78	180	.20	6	2.24	.05	.32	1	3
686T 1542	5	118	15	123	.3	24	24	1671	4.07	10	5	ND	5	76	1	2	2	68	.94	.169	9	47	1.30	178	.13	6	1.80	.03	.21	1	3
686T 1543	4	192	18	155	.5	45	36	1462	5.36	18	5	ND	2	57	1	2	4	95	.69	.155	6	90	1.96	151	.20	3	2.71	.03	.32	1	23
686T 1544	7	221	15	192	.4	47	49	3288	4.63	11	5	ND	5	89	2	2	2	91	.91	.140	22	78	1.83	234	.17	12	3.33	.03	.34	1	6
686T 1545	27	213	14	113	.2	30	96	4292	8.84	12	5	ND	12	89	1	2	10	75	.30	.306	12	45	1.43	189	.14	4	3.81	.01	.19	1	8
686S 1546	6	157	7	121	.1	47	43	2200	4.51	8	5	ND	2	55	1	2	2	85	.64	.143	3	98	1.77	172	.14	2	2.98	.02	.23	1	2
686S 1547	8	149	19	126	.3	41	43	4336	4.57	5	5	ND	5	58	1	2	3	68	.71	.163	15	73	1.70	289	.10	2	2.63	.03	.21	1	7
686S 1548	10	155	15	117	.2	54	40	1954	4.85	11	5	ND	2	74	1	2	2	83	.82	.159	11	109	1.86	184	.13	2	2.88	.02	.23	1	4
686T 1549	1	116	10	116	.1	51	25	1430	3.90	12	5	ND	1	49	1	2	2	101	.81	.120	6	125	2.14	175	.21	2	2.20	.03	.36	1	1
686T 1550	1	138	13	172	.2	100	32	1184	5.18	21	5	ND	1	52	1	3	2	120	.98	.149	5	230	3.26	169	.24	2	2.91	.04	.35	1	6
686S 1551	1	126	28	455	.3	139	34	1177	5.59	19	5	ND	1	58	1	3	2	133	1.63	.136	5	324	3.98	165	.24	2	3.30	.02	.46	1	2
686T 1552	1	135	10	179	.1	118	34	1220	5.35	19	5	ND	1	42	1	3	2	128	1.01	.138	5	279	3.76	167	.25	2	3.23	.04	.37	1	6
686S 1553	1	130	12	165	.1	105	30	1056	4.48	17	5	ND	1	38	1	3	2	101	.77	.142	5	232	3.07	123	.20	4	2.61	.01	.31	1	6
686S 1554	1	425	4	184	.9	39	63	2335	11.36	31	5	ND	2	65	1	2	4	287	1.77	.203	9	88	3.14	333	.46	2	4.73	.17	1.82	1	50
686S 1555	3	161	10	138	.2	77	42	1526	6.55	16	5	ND	2	57	1	2	3	122	.75	.175	7	186	2.76	185	.22	2	2.98	.02	.33	1	7
686S 1556	8	124	22	95	.3	13	21	981	7.25	18	5	ND	3	65	1	3	3	82	.24	.175	9	34	1.20	75	.16	2	2.19	.03	.07	1	12
686S 1557	8	104	13	92	.4	18	15	550	6.03	17	5	ND	2	39	1	2	2	91	.19	.115	8	59	1.12	71	.16	3	2.44	.02	.11	1	6
STD C/AU-0.5	21	57	39	135	7.0	70	30	1141	3.97	40	17	7	34	50	18	16	19	66	.48	.107	39	62	.88	186	.09	38	1.72	.07	.13	14	510

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
686S 1558	4	114	22	125	1.0	21	18	853	5.35	22	6	ND	2	31	1	2	2	93	.18	.075	6	73	1.37	69	.18	2	2.80	.02	.14	1	1
686S 1559	7	122	18	81	.6	8	33	1252	7.61	15	5	ND	2	88	1	2	2	81	.60	.171	6	21	1.35	89	.31	4	2.18	.28	.11	1	7
686T 1560	10	191	19	121	.5	39	65	2103	9.20	18	5	ND	6	76	1	2	4	102	.21	.348	11	44	1.70	377	.23	6	3.31	.02	.20	1	11
686T 1561	15	126	16	116	.6	57	99	4950	7.33	12	8	ND	8	164	1	2	3	72	.56	.354	36	47	1.58	995	.29	2	2.94	.03	.41	1	6
STD C/AU-0.5	20	57	38	130	7.1	71	30	1083	3.97	40	18	7	33	46	16	16	19	63	.47	.103	35	63	.86	179	.08	37	1.72	.07	.14	14	500

CASSIAR MINING PROJECT - 8310 FILE # 86-1409

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
686R 001	1	37	7	63	.2	32	18	1183	4.75	5	5	ND	3	39	1	2	2	144	5.57	.141	9	49	2.99	24	.47	3	2.96	.05	.04	1	1
686R 002	1	59	2	67	.1	24	18	861	4.67	2	5	ND	2	33	1	2	2	167	2.99	.175	9	19	3.07	27	.58	9	2.54	.06	.04	1	1
686R 003	2	7	7	87	.1	2	5	1052	2.14	2	5	ND	2	74	1	2	2	24	4.31	.052	10	7	.99	67	.01	8	1.14	.02	.15	1	1
686R 004	1	35	2	41	.1	12	7	669	1.96	6	5	ND	1	6	1	2	2	26	.18	.041	2	10	.61	33	.01	3	.90	.04	.07	1	1
686R 005	1	123	9	56	.8	47	36	1721	7.36	8	5	ND	1	56	1	2	2	256	4.27	.027	2	90	2.63	61	.59	2	3.36	.12	.17	1	1
686R 006	1	34	6	838	.3	21	13	2138	4.27	6	5	ND	3	105	1	2	2	66	7.44	.099	12	23	1.01	39	.05	2	1.33	.05	.09	1	1
686R 007	1	8	2	13	.1	4	3	1978	1.69	11	7	ND	1	1683	1	2	3	8	29.88	.022	2	3	.34	1376	.01	4	.27	.01	.09	1	1
686R 008	1	6	2	17	.1	4	2	471	.42	2	5	ND	14	51	1	2	2	5	1.72	.019	7	4	.16	64	.01	2	.50	.03	.18	1	1
686R 009	4	19	2	26	.1	1	3	672	2.94	2	5	ND	3	237	1	3	2	32	1.45	.093	7	4	.52	122	.10	4	1.66	.01	.16	1	1
686R 010	11	15	4	37	.1	1	12	865	2.99	5	5	ND	6	145	1	2	2	28	.82	.075	8	1	1.05	12	.08	2	1.55	.04	.06	2	3
686R 011	3	9	6	48	.1	1	12	527	2.28	3	5	ND	4	116	1	2	2	36	.83	.110	8	5	1.04	22	.11	2	1.28	.05	.05	1	1
686R 012	7	12	9	55	.1	4	13	497	3.11	2	5	ND	6	113	1	2	2	31	.98	.108	6	6	1.20	25	.09	3	1.54	.04	.15	1	2
686R 013	6	18	5	33	.1	1	14	466	3.07	2	5	ND	6	116	1	2	2	40	.86	.129	8	3	1.03	37	.12	2	1.43	.09	.10	2	9
686R 014	1	8	2	9	.1	3	2	118	2.18	2	5	ND	5	174	1	2	2	64	1.15	.072	7	3	.25	32	.14	2	1.25	.04	.09	1	1
686R 015	2	25	2	26	.1	1	4	208	3.53	2	5	ND	5	57	1	2	2	31	.30	.118	10	3	.98	75	.01	4	1.37	.08	.14	1	2
686R 599	1	15	7	104	.1	16	21	1999	10.62	10	5	ND	2	180	1	2	2	149	1.20	.260	11	31	3.86	23	.33	2	3.88	.02	.05	1	5
686R 600	2	13	2	23	.1	1	13	373	3.32	2	5	ND	4	103	1	2	2	36	.81	.125	12	3	1.04	34	.01	2	1.50	.11	.08	1	1
686R 601	2	13	2	21	.1	1	10	231	2.34	2	5	ND	3	153	1	2	2	47	1.03	.097	10	4	.84	29	.11	3	1.52	.10	.07	1	1
686R 602	2	24	2	27	.1	4	7	256	1.43	3	5	ND	6	92	1	3	5	51	.71	.103	8	2	.95	25	.12	2	1.30	.08	.03	1	1
686R 603	26	221	2	31	.2	1	17	339	3.80	2	5	ND	5	43	1	2	2	28	.33	.098	9	3	.85	61	.03	2	1.32	.07	.15	2	7
686R 604	4	19	2	14	.2	1	13	50	3.53	2	5	ND	2	33	1	3	2	12	.20	.084	8	2	.22	28	.01	3	.67	.07	.19	1	2
686R 605	4	33	3	15	.1	5	16	76	4.98	4	5	ND	2	35	1	2	2	13	.24	.093	7	3	.22	12	.01	2	.72	.07	.20	1	1
686R 606	1	28	2	31	.1	1	3	75	1.50	2	5	ND	6	45	1	4	2	17	.28	.107	17	2	.39	162	.01	2	1.04	.08	.16	1	1
686R 607	10	205	5	35	.1	2	12	280	1.18	2	5	ND	7	69	1	6	5	22	.68	.094	12	2	.72	47	.01	2	1.05	.08	.13	1	2
686R 1062	78	703	9	3	7.7	3	71	66	6.35	6	5	ND	1	9	1	2	8	5	.03	.013	2	5	.03	6	.01	2	.19	.01	.08	1	115
686R 1063	25	160	8	7	4.5	1	28	69	5.46	10	5	ND	1	9	1	2	9	7	.04	.025	2	6	.07	20	.01	2	.24	.01	.09	31	130
686R 1064	16	378	5	9	2.0	5	23	64	5.09	7	5	ND	1	6	1	2	5	10	.03	.023	2	5	.10	36	.01	2	.27	.01	.07	3	250
686R 1065	29	30	3	22	.6	1	13	246	5.45	7	5	ND	1	8	1	2	2	13	.24	.046	2	9	.23	16	.01	2	.40	.01	.07	11	44
686R 1066	16	70	6	13	.7	1	10	101	6.27	5	5	ND	4	9	1	2	2	10	.06	.077	9	4	.13	164	.01	3	.46	.01	.16	1	30
686R 1067	8	71	6	18	1.0	3	15	291	6.03	5	5	ND	2	22	1	2	2	11	.54	.049	5	6	.19	31	.01	2	.42	.01	.15	1	31
686R 1068	1	62	2	41	.2	33	9	462	2.61	16	5	ND	2	80	1	2	2	87	1.19	.154	11	53	1.19	34	.32	2	1.35	.06	.08	1	2
686R 1069	9	16	3	24	.3	4	15	728	4.71	3	5	ND	5	47	1	2	2	8	1.87	.087	6	2	.41	31	.01	3	.64	.02	.23	1	38
STD C/AU 0.5	20	56	38	130	7.1	71	29	1091	3.95	38	20	8	33	48	16	15	18	62	.48	.102	36	61	.88	177	.08	41	1.72	.07	.13	14	500

## CASSIAR MINING PROJECT - 8310 FILE # 86-1409

PAGE 9

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
686R 1562	1	8	3	15	.1	4	3	216	1.25	2	5	ND	3	174	1	2	2	28	1.15	.087	7	5	.58	25	.07	2	1.23	.05	.03	1	1
686R 1563	4	71	4	49	.1	5	16	565	2.88	2	5	ND	4	56	1	2	2	59	.42	.132	6	3	1.60	29	.07	2	2.15	.07	.03	1	2
686R 1564	1	10	3	31	.1	2	9	378	2.04	2	5	ND	3	83	1	2	5	30	.59	.104	7	4	1.03	23	.08	3	1.25	.04	.04	1	1
686R 1565	6	16	2	30	.1	3	7	305	3.44	2	5	ND	5	39	1	2	2	25	.25	.108	7	4	1.08	24	.02	2	1.47	.04	.07	1	3
686R 1566	2	6	2	12	.1	2	6	179	2.24	2	5	ND	5	76	1	2	2	22	.48	.093	6	3	.63	35	.03	2	.99	.08	.09	2	1
686R 1567	3	6	4	13	.1	2	5	156	1.78	2	5	ND	2	48	1	2	4	29	.36	.063	6	4	.58	24	.06	2	.70	.04	.07	1	1
686R 1568	3	5	2	17	.1	2	5	170	2.24	2	5	ND	2	80	1	2	3	34	.54	.068	6	4	.92	67	.11	5	1.11	.06	.04	1	1
686R 1569	4	7	2	12	.1	4	11	132	5.02	2	5	ND	3	52	1	2	3	32	.21	.063	9	4	.51	74	.10	2	.71	.03	.09	1	16
686R 1570	3	11	2	15	.1	2	6	175	2.59	2	5	ND	2	74	1	2	2	32	.47	.080	7	3	.81	71	.10	2	.91	.07	.06	1	3
686R 1571	2	15	2	35	.1	2	4	304	4.27	2	5	ND	5	105	1	2	2	40	.71	.157	8	5	1.40	41	.08	2	1.74	.03	.07	1	1
STD C/AU 0.5	19	58	36	128	7.3	70	29	1085	3.93	36	18	7	32	46	16	16	18	61	.47	.099	36	59	.88	173	.08	36	1.72	.06	.13	14	500

GLOSSAN  
ASSESSMENT 1986

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE 253-3158

DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SN, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.  
- SAMPLE TYPE: SOILS -BOMESH AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.  
PS & L RECKS

DATE RECEIVED: JULY 9 1986 DATE REPORT MAILED: July 14/86 ASSAYER: D. [Signature] DEAN TOYE. CERTIFIED B.C. ASSAYER.

CASSIAR MINING PROJECT - 8310 FILE # 86-1379

PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
686-S-608	66	8	26	76	.3	7	6	457	6.04	3	6	ND	2	31	1	3	2	79	.27	.160	12	20	.29	115	.33	2	1.65	.03	.07	1	15
686-S-609	3	7	12	63	.2	4	8	1788	2.76	3	5	ND	1	60	1	2	2	49	.39	.103	8	8	.55	76	.13	2	1.41	.06	.11	2	2
686-S-610	10	8	17	37	.1	1	2	99	1.44	3	5	ND	1	23	1	7	2	34	.13	.037	25	6	.06	53	.27	3	.77	.02	.04	2	5
686-S-611	12	15	10	42	.4	4	4	172	4.10	12	5	ND	1	35	1	4	2	63	.17	.071	8	9	.13	39	.14	2	.74	.01	.04	2	5
686-L-612	18	50	17	91	.4	5	8	1251	2.56	2	6	ND	1	73	1	2	2	42	.54	.138	11	7	.44	161	.07	4	1.82	.03	.10	1	1
686-S-613	15	20	14	59	.1	3	7	355	3.86	10	5	ND	1	49	1	2	2	46	.33	.084	8	10	.47	66	.12	2	1.71	.02	.05	1	3
686-S-614	4	9	4	76	.2	4	5	294	1.23	2	6	ND	1	68	1	2	2	23	1.29	.074	2	6	.24	40	.16	6	.59	.06	.06	1	1
686-S-615	85	12	2	52	.2	7	6	246	1.30	2	8	ND	1	267	1	2	2	28	4.16	.069	3	7	.41	159	.16	3	.70	.13	.07	1	1
686-S-616	130	31	19	116	.7	9	14	9202	2.86	2	14	ND	1	132	1	2	2	45	1.75	.126	40	15	.32	239	.15	3	2.21	.03	.05	1	2
686-S-617	3	6	21	53	.1	3	7	1115	2.52	2	5	ND	1	39	1	2	2	77	.28	.108	8	9	.29	61	.25	3	.91	.02	.06	1	2
686-S-618	4	19	31	50	.4	5	18	2753	1.46	2	5	ND	1	36	1	2	2	38	.27	.160	14	6	.24	51	.08	5	1.94	.04	.07	1	4
686-S-619	75	23	15	218	.6	9	24	6665	4.41	7	14	ND	1	218	1	2	2	36	2.51	.123	47	10	.27	246	.09	5	2.19	.04	.05	1	2
686-S-620	23	4	21	34	.2	1	4	109	3.78	5	5	ND	2	18	1	2	2	69	.14	.037	20	8	.09	48	.36	2	.85	.03	.04	1	4
686-S-621	4	7	9	65	.1	14	15	467	4.56	2	5	ND	1	76	1	3	2	90	.79	.075	10	17	1.16	53	.61	4	1.50	.33	.12	1	1
686-S-622	1	8	9	76	.1	21	22	671	5.27	2	5	ND	1	116	1	2	2	112	1.37	.083	6	20	1.99	61	.76	2	1.84	.62	.21	1	3
686-S-623	9	14	18	40	.5	3	4	123	4.02	4	5	ND	1	13	1	6	2	54	.09	.052	23	11	.12	28	.31	2	1.43	.04	.06	1	3
686-S-624	4	8	7	32	.1	5	6	163	2.54	6	5	ND	1	50	1	3	2	86	.30	.045	6	8	.33	31	.20	4	1.06	.07	.04	2	1
686-S-625	4	14	25	42	.3	3	6	261	5.13	15	5	ND	3	54	1	4	2	62	.25	.124	6	12	.38	28	.18	2	1.24	.01	.04	4	12
686-T-626	62	551	32	94	.4	5	38	4223	7.34	8	5	ND	3	22	1	2	6	37	.13	.179	29	7	.48	105	.07	2	1.70	.02	.07	1	18
686-S-627	15	25	40	60	.2	2	9	387	12.27	23	5	ND	15	16	1	2	9	76	.09	.271	27	15	.15	80	.32	2	2.33	.04	.08	3	4
686-S-628	3	42	67	91	.2	1	10	645	2.23	3	5	ND	4	85	1	2	2	40	.80	.158	12	3	.64	160	.06	2	1.05	.01	.06	1	16
686-S-629	2	37	29	92	.3	4	9	632	2.14	5	5	ND	2	78	1	2	2	33	.77	.184	12	4	.63	106	.07	3	.92	.02	.05	1	19
686-L-630	22	276	27	152	.4	6	25	1551	4.07	6	8	ND	4	117	1	2	2	39	.93	.178	19	8	.90	578	.10	2	1.49	.06	.09	1	14
686-S-648	3	76	176	624	1.2	66	21	2524	5.81	88	5	ND	1	24	3	2	2	105	.36	.098	17	77	1.48	454	.19	2	2.36	.02	.73	1	3
686-S-649	4	120	47	262	2.5	197	32	5679	5.61	165	5	ND	1	29	2	6	2	77	.63	.117	23	118	2.03	286	.22	2	2.47	.01	.83	1	5
686-S-650	3	98	57	313	1.5	122	29	2765	6.24	123	5	ND	1	36	1	3	2	178	.55	.114	18	136	2.75	492	.29	2	3.54	.02	1.13	1	4
686-S-651	2	67	44	175	1.1	41	17	1785	5.33	48	5	ND	1	29	1	2	2	154	.43	.099	13	64	1.66	414	.23	2	2.78	.03	.37	1	12
686-S-652	1	99	51	219	.9	46	20	2231	5.92	41	5	ND	1	28	1	2	2	158	.37	.106	18	65	2.12	420	.30	2	3.64	.02	.66	1	5
686-S-653	1	89	46	221	.4	52	18	1595	5.71	19	5	ND	2	20	1	2	2	143	.20	.075	12	77	2.01	327	.32	2	3.69	.02	.58	1	6
686-S-654	1	193	52	186	.4	99	30	2792	6.34	7	5	ND	2	39	1	2	2	202	.41	.136	10	154	3.59	685	.38	2	4.31	.02	.84	1	4
686-S-655	1	144	31	173	.1	37	25	3383	5.86	9	5	ND	1	34	1	2	2	208	.68	.132	11	56	2.31	527	.29	2	3.34	.03	.82	1	2
686-S-656	1	194	177	575	1.0	39	30	4508	6.79	8	5	ND	2	33	1	2	2	200	.46	.086	12	43	2.37	472	.36	2	3.91	.02	.82	1	8
686-S-657	1	130	147	310	.5	73	24	3817	5.69	14	5	ND	1	28	1	2	2	152	.30	.077	9	83	2.27	385	.31	2	3.85	.02	.73	1	5
686-S-658	2	144	169	475	1.3	65	24	3852	5.61	10	5	ND	2	51	2	2	2	157	.65	.092	11	81	2.52	851	.33	2	3.12	.02	1.08	1	4
686-S-659	3	84	89	301	.4	44	20	3370	5.15	7	5	ND	1	35	1	2	2	120	.49	.089	7	57	1.49	499	.24	5	2.60	.03	.49	1	3
686-S-660	2	109	122	472	1.3	46	24	3361	5.32	9	5	ND	1	50	4	2	2	132	1.04	.148	10	57	2.01	406	.31	2	2.63	.06	.88	1	10
STD C/AU-0.5	20	56	36	132	7.0	65	30	1110	3.95	40	16	7	33	49	18	15	19	64	.48	.105	38	60	.88	182	.08	38	1.71	.07	.13	14	480

copy 1/16

## CASSIAR MINING PROJECT - 8310 FILE # 86-1379

PAGE 2

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Ri PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
686-S-661	2	152	152	562	2.4	56	29	3363	6.61	12	5	ND	3	50	3	2	2	160	.98	.160	11	59	2.18	404	.36	2	2.95	.05	1.09	2	12
686-S-662	7	390	160	322	3.7	107	71	6167	14.50	199	10	ND	3	17	2	2	10	38	.06	.202	29	18	.55	132	.02	2	1.66	.02	.11	7	15
686-S-663	5	50	70	131	1.0	19	15	1520	6.22	79	9	ND	1	18	1	2	2	58	.10	.138	14	11	.22	89	.04	2	.77	.01	.08	4	3
686-S-664	7	38	222	200	.8	17	23	8968	5.60	39	12	ND	1	53	1	2	2	41	.25	.104	30	12	.32	2168	.04	2	1.69	.01	.09	1	32
686-S-665	1	135	34	172	2.1	28	28	2597	9.32	45	8	ND	2	20	1	2	7	119	.19	.207	19	12	1.62	208	.08	2	2.47	.01	.23	2	5
686-S-666	1	126	39	136	2.8	18	28	1960	8.96	33	9	ND	1	17	1	2	6	198	.15	.102	11	17	1.60	254	.12	2	3.09	.02	.26	1	1
686-S-667	1	169	48	152	5.7	29	34	2310	9.06	20	10	ND	2	34	1	2	2	255	.29	.084	9	17	2.65	374	.28	2	4.66	.03	.59	1	6
686-S-668	1	122	23	118	.9	38	30	2186	7.16	19	5	ND	1	46	1	2	2	192	.42	.111	8	18	2.10	370	.25	2	3.73	.04	.55	4	2
686-T-669	1	272	68	186	2.4	18	45	3633	7.40	42	8	ND	3	38	1	2	5	191	.39	.154	6	19	1.61	501	.29	2	3.95	.05	1.06	1	9
686-S-670	1	166	90	190	1.1	38	27	1682	7.34	19	8	ND	1	39	1	2	8	226	.23	.085	6	49	2.26	293	.25	2	4.35	.04	.49	1	4
686-S-671	1	150	62	159	2.0	41	30	2167	6.63	19	9	ND	1	53	1	2	2	209	.37	.103	9	55	2.22	329	.25	2	4.19	.07	.44	2	6
686-T-672	2	139	41	139	1.1	35	27	1927	6.54	20	9	ND	1	40	1	2	10	221	.32	.134	8	54	2.45	346	.21	2	3.64	.04	.46	3	3
686-T-673	2	252	47	206	1.0	44	39	4119	7.50	19	5	ND	1	32	1	2	2	191	.24	.070	9	50	2.13	341	.27	2	4.57	.09	.59	4	6
686-S-674	2	151	93	232	2.4	39	29	3056	6.06	16	5	ND	1	51	1	2	4	185	.34	.095	4	55	1.85	242	.23	2	4.13	.12	.51	1	3
686-S-675	2	129	139	273	.8	35	18	1337	5.68	90	5	ND	1	18	1	4	2	134	.15	.071	7	41	1.42	137	.20	2	4.92	.03	.38	5	15
686-T-676	2	64	57	181	1.1	19	21	2010	5.70	36	5	ND	1	52	1	2	2	60	.75	.213	9	15	1.08	184	.13	2	1.50	.04	.35	1	7
686-S-1070	6	46	37	99	1.7	2	9	429	5.12	51	6	ND	2	47	1	3	2	48	.20	.124	8	16	.55	43	.08	2	1.83	.01	.05	5	10
686-S-1071	46	19	24	35	.9	7	3	116	2.23	10	16	ND	1	25	1	2	2	76	.19	.081	5	11	.14	42	.50	2	.67	.01	.04	3	1
686-L-1072	9	16	21	123	.5	24	23	1094	4.97	10	139	ND	2	256	1	2	2	108	3.31	.120	16	23	1.90	274	.57	2	2.83	.81	.29	3	6
686-S-1073	10	23	35	77	4.9	8	18	2232	4.16	8	5	ND	1	33	1	2	2	82	.23	.120	11	16	.43	42	.32	2	2.21	.06	.07	2	6
686-S-1074	31	16	48	50	2.0	4	4	149	7.53	21	12	ND	5	29	1	2	2	69	.13	.050	21	10	.11	64	.31	2	1.48	.04	.07	2	2
686-S-1075	22	15	49	69	1.2	5	5	267	6.26	19	11	ND	6	15	1	2	5	29	.11	.067	37	11	.16	22	.20	2	4.16	.07	.08	1	4
686-S-1076	2	3	25	56	.3	10	6	518	2.15	2	5	ND	1	46	1	2	5	49	.42	.117	10	8	.54	55	.13	2	1.17	.10	.08	1	1
686-S-1077	10	13	29	83	.9	2	9	344	10.83	6	12	ND	5	37	1	5	2	96	.31	.077	16	13	.63	41	.50	2	1.45	.08	.07	1	1
686-S-1078	92	4	10	51	.1	2	1	85	.56	5	76	ND	3	450	1	4	2	49	7.49	.080	2	2	.11	174	.03	3	.26	.03	.04	5	1
686-S-1079	35	17	33	154	1.0	14	10	670	4.26	39	172	ND	2	150	1	5	2	77	1.29	.213	46	23	.53	218	.19	3	4.41	.04	.08	9	6
686-S-1080	4	1	24	25	.1	1	1	79	.54	3	6	ND	1	32	1	2	2	29	.18	.039	8	2	.05	29	.12	2	.62	.01	.03	1	36
686-S-1081	8	5	34	41	1.0	2	4	107	6.68	12	11	ND	3	21	1	2	2	81	.08	.041	17	10	.11	70	.41	2	1.19	.01	.05	2	1
686-S-1082	4	2	29	35	1.1	1	3	135	2.42	8	6	ND	2	23	1	3	2	121	.22	.068	5	10	.11	43	.86	2	.42	.02	.05	1	1
686-S-1083	13	11	40	73	1.9	5	5	387	9.23	16	17	ND	6	11	1	2	2	36	.10	.070	33	14	.12	31	.29	2	3.25	.04	.07	3	2
686-S-1084	73	11	24	110	.9	6	7	964	7.05	12	17	ND	2	43	1	3	2	71	.35	.076	24	17	.38	60	.29	2	2.41	.07	.08	2	1
686-S-1085	24	50	42	102	.4	5	16	893	4.93	36	15	ND	4	54	1	2	2	40	.38	.169	16	9	.63	38	.11	2	1.65	.01	.05	2	13
686-S-1086	13	12	25	101	.1	5	12	2655	2.76	5	8	ND	1	58	1	2	2	55	.59	.199	9	8	.83	82	.11	2	1.28	.11	.11	1	3
686-S-1087	7	57	29	54	.5	2	13	832	2.50	3	5	ND	5	75	1	2	8	37	.67	.191	13	1	.64	290	.06	2	.96	.01	.05	1	8
686-S-1088	6	14	35	47	.5	5	5	174	2.13	10	5	ND	2	32	1	2	2	111	.16	.041	6	6	.21	34	.35	2	.75	.02	.03	2	6
686-S-1089	7	41	50	90	.3	5	14	1214	3.01	12	5	ND	1	60	1	2	4	38	.50	.157	14	3	.64	104	.06	2	1.25	.02	.05	3	9
STD. C/AU-0.5	20	57	39	139	7.0	75	32	1048	3.98	40	21	8	38	54	18	16	21	71	.48	.111	41	63	.86	186	.09	39	1.72	.07	.15	14	490

CASSIAR MINING PROJECT - 8310 FILE # 86-1379

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
686-S-1090	3	45	22	59	.2	4	11	613	2.58	2	5	ND	1	63	1	2	2	36	.61	.117	10	9	.65	134	.06	3	.99	.04	.06	1	30
686-L-1091	4	148	22	98	.2	19	23	860	4.72	2	18	ND	3	136	1	2	2	80	1.47	.111	10	25	1.71	226	.50	7	1.62	.46	.16	1	4
686-S-1092	24	378	20	97	.4	1	25	1341	3.88	5	11	ND	4	63	1	2	2	33	.65	.176	16	6	.84	227	.09	2	1.34	.04	.07	1	5
686-S-1093	63	37	35	77	.1	5	8	414	7.01	10	6	ND	5	50	1	3	4	57	.24	.061	12	20	.57	98	.20	2	2.93	.01	.08	1	2
686-S-1094	78	18	25	62	.4	4	6	416	5.77	4	6	ND	1	31	1	3	2	64	.19	.063	25	23	.34	52	.23	2	1.97	.03	.05	1	3
686-S-1095	28	13	19	47	.2	3	3	219	2.25	3	5	ND	1	48	1	2	2	44	.27	.056	11	13	.27	101	.09	2	1.50	.02	.04	1	1
686-S-1096	51	7	26	59	.2	3	6	436	6.88	6	5	ND	2	24	1	6	2	87	.24	.044	24	15	.17	72	.49	2	1.16	.03	.06	3	1
686-S-1097	79	5	19	106	.2	5	7	1622	3.36	19	154	ND	1	127	1	2	2	85	1.08	.082	21	14	.22	119	.27	2	1.75	.03	.05	1	1
686-S-1098	4	1	18	30	.2	1	2	118	1.35	2	5	ND	1	65	1	2	2	58	.32	.052	7	6	.18	83	.26	2	1.25	.02	.04	1	1
686-L-1099	7	21	22	113	.1	6	8	980	2.21	8	5	ND	1	117	1	2	2	34	.95	.132	14	7	.75	99	.10	4	1.35	.05	.06	1	12
686-S-1100	13	17	18	92	.1	4	8	819	2.32	7	29	ND	1	135	1	2	2	42	1.17	.120	15	9	.73	92	.18	3	1.48	.13	.08	1	2
686-S-1101	51	50	28	111	.3	7	17	3002	4.25	16	15	ND	1	77	1	2	2	70	.66	.115	36	14	.66	169	.19	3	1.81	.03	.05	1	22
686-L-1102	12	16	9	100	.2	18	10	1158	2.43	4	15	ND	1	138	1	2	2	47	1.27	.112	18	11	.90	134	.15	2	1.65	.08	.09	1	2
686-S-1103	38	14	33	60	.2	6	7	349	9.25	15	5	ND	3	33	1	2	9	64	.19	.054	21	12	.24	68	.37	2	1.14	.03	.04	1	1
686-L-1104	14	19	12	83	.6	6	9	1214	2.27	3	7	ND	1	107	1	2	2	37	1.07	.105	21	10	.56	146	.14	4	1.82	.09	.07	1	1
686-S-1105	26	11	24	68	.3	1	6	411	8.40	10	5	ND	2	26	1	2	2	49	.25	.059	22	14	.17	100	.25	5	1.47	.03	.06	1	1
686-L-1106	14	28	18	94	.2	2	9	1085	2.31	11	23	ND	1	108	1	2	2	36	.94	.154	16	7	.78	120	.09	2	1.35	.04	.07	1	1
686-L-1107	2	20	25	77	.1	1	8	468	1.79	4	5	ND	2	64	1	2	2	23	1.22	.189	11	1	.52	94	.05	2	.63	.03	.03	1	3
686-S-1107	6	3	12	31	.1	1	4	179	2.51	6	5	ND	1	44	1	2	2	46	.27	.048	8	4	.23	59	.06	2	1.15	.02	.08	2	3
686-L-1572	10	20	50	220	.5	3	11	2236	2.29	6	5	ND	3	81	5	2	2	33	1.04	.169	14	10	.93	341	.07	2	1.29	.02	.12	1	3
686-S-1573	32	17	24	94	1.0	1	6	495	6.59	12	12	ND	1	32	1	2	2	28	.42	.097	42	10	.14	102	.12	2	1.95	.04	.06	1	1
686-S-1574	3	10	9	34	.1	1	4	158	1.33	5	5	ND	1	46	1	2	2	24	.28	.049	5	5	.14	54	.05	3	.53	.01	.04	2	1
686-L-1575	3	26	18	77	.1	4	8	894	2.10	8	10	ND	3	115	1	2	2	36	.84	.135	11	7	.85	173	.10	2	1.21	.06	.09	1	2
686-S-1576	18	32	15	119	.4	6	9	452	4.06	8	7	ND	1	38	1	2	2	34	.26	.115	16	14	.45	62	.08	2	4.37	.01	.05	1	1
686-S-1577	21	5	18	37	.1	1	4	201	3.98	6	5	ND	1	32	1	4	2	67	.15	.071	14	10	.17	46	.30	3	1.19	.01	.04	2	4
686-S-1578	54	16	28	100	.4	3	6	411	5.60	8	7	ND	1	46	1	3	2	51	.38	.061	30	13	.25	101	.14	2	2.22	.02	.05	1	8
686-S-1579	58	37	14	61	1.1	7	15	3507	3.73	2	43	ND	1	96	1	2	2	82	1.08	.083	91	14	.48	111	.42	3	1.83	.12	.08	1	5
686-S-1580	6	10	14	56	.7	6	17	1155	4.69	2	5	ND	1	39	1	2	2	107	.39	.065	13	15	.58	39	.62	2	1.67	.15	.09	1	2
686-S-1581	97	10	21	64	.5	2	6	477	5.77	4	9	ND	2	34	1	3	2	60	.29	.053	18	14	.24	48	.30	2	1.70	.02	.05	1	1
686-S-1582	33	6	18	46	.2	2	4	224	4.18	8	5	ND	1	26	1	5	2	50	.21	.038	18	8	.25	34	.23	4	1.36	.02	.04	1	1
686-S-1583	6	20	16	37	.4	1	4	147	3.22	5	5	ND	1	16	1	4	2	47	.09	.052	19	11	.13	23	.21	2	1.86	.01	.04	1	4
686-S-1584	3	12	15	45	.3	5	7	209	4.93	3	5	ND	1	17	1	2	2	80	.21	.065	14	18	.40	26	.40	2	2.55	.05	.08	1	2
686-S-1585	6	3	21	32	.1	1	2	120	1.92	5	5	ND	1	25	1	3	2	64	.14	.042	11	9	.17	31	.33	2	1.00	.02	.05	1	5
686-S-1586	7	3	21	26	.2	1	3	129	1.30	4	5	ND	1	23	1	3	3	52	.14	.051	17	9	.11	32	.42	3	.82	.02	.03	2	7
686-S-1587	9	26	24	50	.9	1	8	217	5.77	18	5	ND	3	33	1	4	2	72	.18	.119	8	9	.21	34	.18	7	.99	.01	.03	2	4
686-S-1588	47	564	30	63	1.4	1	43	2272	7.04	6	5	ND	7	21	1	2	4	27	.24	.171	20	5	.58	202	.06	5	3.25	.01	.04	1	30
STD C/AU-0.5	20	57	38	130	7.1	65	29	1091	3.92	39	15	7	33	46	17	15	19	63	.48	.104	35	58	.88	178	.08	38	1.71	.06	.13	13	490

CASSIAR MINING PROJECT - 8310 FILE # 86-1379

PAGE 4

SAMPLE#	Mg	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
686-S-1589	8	248	61	84	.1	5	28	1346	6.45	11	5	ND	5	79	1	2	2	55	.67	.153	15	7	.98	96	.14	4	1.50	.09	.09	1	80
686-S-1590	4	318	78	304	.5	14	43	1486	8.55	93	5	ND	4	81	2	2	5	56	.52	.359	14	18	1.06	112	.10	2	1.50	.01	.04	4	210
686-S-1614	2	24	24	103	.1	4	16	1625	7.58	13	5	ND	2	53	1	2	3	50	.13	.180	8	6	.79	101	.16	3	1.92	.02	.17	1	2
686-S-1615	2	22	21	131	.1	4	15	1838	5.56	16	5	ND	2	49	1	2	2	55	.15	.154	15	6	1.05	127	.15	2	2.47	.03	.26	1	2
686-S-1616	4	42	38	251	.3	8	15	2245	5.26	29	5	ND	2	23	1	2	2	59	.15	.102	42	9	.92	108	.16	7	3.08	.05	.19	1	3
686-S-1617	4	14	20	131	.2	6	6	1277	4.29	16	5	ND	2	8	1	10	2	18	.07	.071	37	8	.21	78	.10	3	2.91	.08	.09	1	9
686-S-1618	6	20	19	206	.2	2	28	5239	5.19	10	5	ND	1	57	1	2	2	47	.27	.174	18	3	.87	502	.14	2	2.30	.02	.43	1	2
686-S-1619	1	10	15	107	.1	3	10	631	4.97	12	5	ND	1	49	1	4	2	43	.15	.118	16	6	.56	52	.10	4	1.70	.02	.17	1	1
686-S-1620	1	182	29	149	.1	18	30	1331	7.35	17	5	ND	3	54	1	2	2	273	.49	.208	21	13	2.50	410	.26	8	4.94	.05	.99	1	24
STD C/AU-0.5	21	62	39	139	7.0	70	32	1091	3.95	41	17	8	34	49	17	15	18	67	.48	.109	37	63	.88	183	.08	36	1.72	.07	.14	15	510



CASSIAR MINING PROJECT - B010 FILE # 86-1079

SAMPLE#	Mo	Cu	Pb	Zn	Ag	As	Co	Mn	Fe	Al	S	Si	Ti	Cr	Ca	F	La	Er	Mo	Ba	Li	Sr	K	Na	Cl	Mg	Al		
PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM		
686-R-016	15	24	110	11	1.1	1	90	270	5.07	5	5	NO	7	70	1	1	1	1	15	104	100	15	17	100	100	100	1	20	
686-R-017	1	10	6	28	.1	1	4	454	1.21	1	5	NO	6	51	1	1	1	1	3	4.27	100	17	1	100	104	101	19	17	
686-R-018	8	156	11	25	.1	1	17	360	1.71	6	6	NO	1	47	1	1	1	1	7	1.41	145	6	1	104	141	107	24	107	
686-R-019	5	66	7	77	.1	1	6	515	2.26	5	5	NO	4	25	1	1	1	1	4	67	124	171	6	1	100	107	104	27	107
686-R-020	17	88	17	37	.1	1	6	484	2.67	4	5	NO	7	47	1	1	1	1	4	55	147	107	7	1	100	115	109	22	101
686-R-021	18	77	8	26	.1	5	10	8401	3.64	6	5	NO	4	101	1	1	1	1	5	4.25	1010	6	1	105	107	101	14	115	
686-R-022	4	57	6	26	.4	1	7	365	2.26	4	6	NO	6	67	1	1	1	1	1	45	163	110	6	1	109	100	114	24	117
686-R-023	5	104	13	32	.1	1	12	762	2.36	5	4	NO	4	76	1	1	1	1	5	51	177	121	4	1	105	91	112	21	114
686-R-024	9	156	7	69	.3	5	18	2029	3.01	1	5	NO	6	120	1	1	1	1	4	24	12.81	1057	12	1	170	43	101	21	102
686-R-025	8	22	8	14	.1	4	6	159	1.69	2	5	NO	10	27	1	1	1	1	1	24	114	1072	4	1	107	120	105	25	102
686-R-026	107	16	225	19	8.1	1	255	44	18.78	2	5	NO	1	4	1	2	13	4	6	1.02	1001	4	1	105	6	101	15	105	
686-R-027	10	119	19	18	.3	3	11	235	1.96	3	5	NO	6	24	1	2	2	2	11	26	1064	12	4	130	100	101	28	104	
686-R-028	14	106	23	37	.6	4	8	532	2.95	2	5	NO	6	68	1	2	3	3	56	47	144	6	2	104	235	113	22	110	
686-R-029	1	3	10	24	.1	2	1	639	1.44	6	11	NO	5	317	1	2	2	2	11	5.52	1077	7	2	103	29	104	17	122	
686-R-030	12	30	27	19	2.8	26	131	376	18.16	33	5	NO	2	33	1	2	25	28	28	21	1031	9	15	109	4	108	23	172	
686-R-031	2	511	4	71	.1	2	10	1456	2.27	4	5	NO	2	150	1	2	4	24	1.38	1105	7	2	126	79	110	25	160		
686-R-032	1	5	11	30	.1	1	8	232	4.79	11	5	NO	2	48	1	2	2	2	17	45	1169	8	1	133	27	111	23	104	
686-R-033	1	6	16	49	.1	1	6	496	4.25	11	5	NO	1	71	1	2	2	2	31	58	1156	7	2	145	54	125	30	176	
686-R-034	1	5	31	54	.1	1	6	821	3.44	12	6	NO	1	49	1	2	2	2	16	1.46	1119	6	2	121	25	119	2	147	
686-R-035	1	4	14	5	.1	1	5	49	4.29	13	5	NO	2	43	1	2	2	2	11	23	1131	6	1	105	31	120	24	135	
686-R-036	1	4	5	4	.1	4	1	333	1.41	4	5	NO	1	144	1	2	4	7	36	1013	2	3	102	10	102	28	120		
686-R-037	1	3	16	47	.1	1	5	613	3.13	9	5	NO	2	81	1	2	2	2	29	43	1136	7	2	163	154	123	2	190	
686-R-038	1	105	12	101	.5	17	25	1516	6.53	10	5	NO	4	164	1	2	2	2	289	6.02	1247	11	27	239	1129	130	2	333	
686-R-039	2	78	22	69	1.1	21	11	635	4.09	6	7	NO	1	56	1	5	2	2	16	53	1191	9	24	103	92	107	9	127	
686-R-031	1	51	4	27	.2	4	11	487	3.23	4	6	NO	6	57	1	2	4	4	20	125	1147	7	3	170	44	101	2	142	
686-R-433	5	28	5	31	.1	5	59	424	6.33	6	6	NO	4	58	1	2	2	2	33	112	1089	7	2	171	31	101	2	135	
686-R-435	9	76	9	25	.3	7	23	333	10.68	6	5	NO	5	29	1	2	6	31	109	1087	8	6	156	27	101	2	108		
686-R-437	32	78	4	47	.3	4	14	661	4.47	5	5	NO	2	48	1	2	2	2	9	127	1049	5	3	176	57	102	5	144	
686-R-439	17	39	8	31	.1	3	9	310	3.22	2	5	NO	4	41	1	2	2	2	23	132	1106	5	3	182	73	104	2	105	
686-R-441	13	127	9	28	.3	4	13	191	3.45	4	5	NO	5	38	1	2	2	2	27	128	1120	4	3	187	51	101	5	106	
686-R-443	15	14	9	39	.4	5	10	330	2.12	3	5	NO	4	95	1	2	2	2	41	149	1111	9	4	193	34	109	2	110	
686-R-445	3	27	6	25	.1	6	17	193	2.75	2	5	NO	3	92	1	2	2	2	34	181	1108	5	4	178	21	106	2	109	
686-R-447	2	13	3	22	.1	4	17	562	3.01	3	5	NO	5	99	1	2	2	2	25	258	1113	4	5	162	41	106	2	107	
686-R-1108	2	13	5	50	.3	3	5	670	1.93	2	12	NO	6	33	1	2	3	3	23	1.47	1064	10	3	154	144	109	2	101	
686-R-1109	1	21	10	30	.2	6	3	553	1.15	2	5	NO	4	18	1	2	2	2	4	156	1041	13	3	108	105	101	25	132	
686-R-1110	1	23	7	24	.3	6	3	578	1.19	5	5	NO	4	17	1	2	2	2	4	155	1042	14	3	101	105	101	2	127	
STD CHU 0.5	22	58	43	138	7.3	71	31	1099	3.99	42	17	8	36	51	17	15	19	67	148	1109	39	61	188	185	109	36	172		

CASSIAR MINING PROJECT - 8310 FILE # 86-1379

PAGE 6

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	S	Al	Ti	Cr	Ce	Sr	Sc	V	Ca	P	La	Er	Mo	Sa	Bi	B	Fl	Na	K	Rb	Ba#	
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	1	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	1	1	PPM	PPM	1	PPM	1	PPM	1	1	1	1	PPM	PPM
886-R-1111	1	55	4	127	.2	8	14	350	4.40	1	5	NO	1	178	1	2	2	121	3.15	.289	34	19	1.77	245	.36	3	1.91	.28	.18	1	2	
886-R-1112	1	67	58	200	.7	45	17	2051	5.48	1	5	NO	1	45	1	2	2	197	1.72	.178	17	24	2.61	583	.45	8	3.27	.78	3.51	1	1	
886-R-1117	1	13	18	43	.4	7	4	847	1.43	14	8	NO	1	104	1	2	2	3	3.88	.038	14	3	1.99	177	.01	3	.38	.02	.25	1	1	
886-R-1114	1	7	5	19	.1	1	1	941	.48	1	5	NO	4	137	1	1	3	1	1.37	.019	28	2	1.03	488	.01	2	.24	.63	.23	1	1	
886-R-1115	1	9	7	23	.1	2	3	382	1.25	19	5	NO	1	78	1	2	3	2	.86	.024	24	3	1.03	1851	.01	4	.42	.02	.28	1	4	
886-R-1114	1	129	16	44	1.0	10	24	1402	8.28	4	5	NO	4	276	1	2	2	188	6.89	.247	8	6	1.85	54	.98	12	1.69	.02	1.09	1	2	
886-R-1591	1	36	2	118	.1	12	14	1662	8.64	1	5	NO	2	91	1	2	2	147	.55	.247	13	44	4.49	32	.23	10	3.91	.01	.02	1	4	
886-R-1593	1	12	7	41	.1	6	5	717	2.08	1	5	NO	5	44	1	2	5	35	.27	.099	11	3	1.10	70	.09	8	1.42	.04	.69	1	1	
886-R-1595	4	11	2	35	.1	4	7	632	2.03	1	5	NO	5	105	1	2	5	22	.58	.095	11	3	.71	186	.67	2	1.23	.04	.18	1	1	
886-R-1597	2	5	2	18	.1	3	4	400	.84	1	5	NO	1	74	1	2	4	8	.25	.029	4	4	.45	24	.03	3	.58	.03	.05	1	1	
886-R-1599	4	22	5	26	.1	3	23	349	5.86	2	5	NO	4	54	1	2	3	15	.40	.094	5	3	.73	17	.02	2	1.82	.04	.11	1	15	
886-R-1601	20	31	4	17	.1	1	9	267	2.98	2	5	NO	4	101	1	2	2	40	.71	.113	5	3	.82	24	.09	2	1.86	.06	.86	1	1	
886-R-1603	45	13	7	18	.2	3	63	148	7.13	2	5	NO	3	40	1	2	2	17	.47	.076	5	3	.38	20	.08	6	.63	.05	.11	1	3	
886-R-1605	225	29	6	30	.2	4	8	745	1.37	2	5	NO	5	132	1	2	4	19	1.02	.082	11	2	.86	14	.04	2	1.21	.03	.07	1	4	
886-R-1607	4	9	4	34	.1	2	4	894	1.26	2	5	NO	4	83	1	2	3	19	.82	.096	8	6	.78	31	.97	2	1.88	.03	.12	1	1	
886-R-1609	4	9	3	42	.1	2	4	656	1.66	2	5	NO	3	146	1	2	2	28	1.03	.128	8	4	.83	27	.11	3	1.28	.03	.18	2	1	
886-R-1611	6	3	2	55	.1	2	13	881	1.62	2	8	NO	6	82	1	3	4	19	.61	.113	10	4	.83	47	.62	2	1.29	.03	.14	1	3	
886-R-1613	1	2	2	62	.1	4	2	511	.77	2	5	NO	3	130	1	3	5	22	1.89	.114	10	5	.83	14	.09	4	1.12	.04	.08	1	1	
STD C/AH-0.5	21	60	40	136	7.1	69	31	1136	4.80	40	19	8	35	50	17	16	20	65	.48	.189	37	61	.88	184	.98	36	1.72	.07	.14	14	490	

APPENDIX 3

STATEMENT OF QUALIFICATIONS

STATEMENT OF QUALIFICATIONS

RICHARD E. MEYERS

B.Sc. Geology - Carleton University, Ottawa, 1974

M.Sc. Economic Geology - McGill University, Montreal, 1980

I have practised my profession continuously since graduation in 1974, including three years as a mining and evaluation geologist (1974-77), two years in economic geology research (1977-79) and seven years as an exploration geologist.

A handwritten signature in black ink, appearing to read 'R. E. Meyers', with a stylized flourish at the end.



6272000 N

6272000 N

6270000 N

6268000 N

6266000 N

384000 E

386000 E

388000 E

390000 E

West

Sericite

Glacier

Lake Glacier

Nee Glacier

North Pins Glacier

South Pins Glacier

GOSSAN 6

GOSSAN 7

LCP

GOSSAN 5

GOSSAN 22

GOSSAN 1

GOSSAN 3

LCP

GOSSAN 4

GOSSAN 2

**LEGEND**

- 523H Soil(S) or talus(T) sample location & number.
- △ L1533 Stream sediment(L) sample location & number.
- 4002 Rock(R) sample location & number.

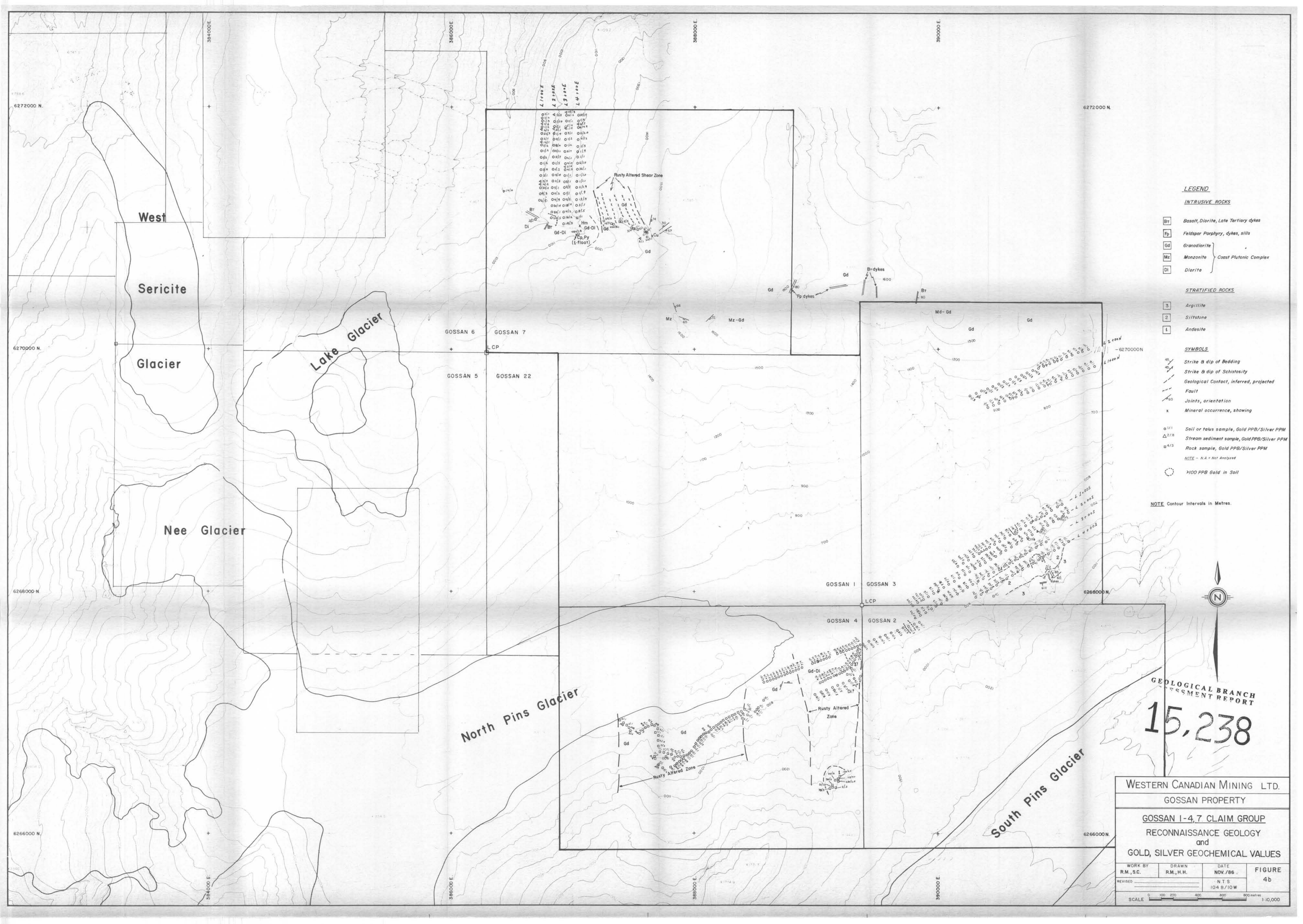
NOTE: Contour intervals in Metres.



GEOLOGICAL BRANCH  
ASSESSMENT REPORT

**15,238**

WESTERN CANADIAN MINING LTD.			
GOSSAN PROPERTY			
GOSSAN 1-4,7 CLAIM GROUP			
1986			
SAMPLE LOCATIONS			
WORK BY R.M., S.C.	DRAWN R.M., H.H.	DATE NOV./86	FIGURE 4a
REVISED	N.T.S. 104 B/10W		
SCALE 0 100 200 400 600 800 metres			1:10,000



**LEGEND**

**INTRUSIVE ROCKS**

- [BT] Basalt, Diorite, Late Tertiary dykes
  - [Fp] Feldspar Porphyry, dykes, sills
  - [Gd] Granodiorite
  - [Mz] Monzonite
  - [Di] Diorite
- } Coast Plutonic Complex

**STRATIFIED ROCKS**

- [3] Argillite
- [2] Siltstone
- [1] Andesite

**SYMBOLS**

- ↘ Strike & dip of Bedding
- ↘ Strike & dip of Schistosity
- Geological Contact, inferred, projected
- - - Fault
- ↘ Joints, orientation
- x Mineral occurrence, showing
- 1/1 Soil or talus sample, Gold PPB/Silver PPM
- △ 2/8 Stream sediment sample, Gold PPB/Silver PPM
- 4/3 Rock sample, Gold PPB/Silver PPM
- NOTE - N.A. = Not Analyzed
- >100 PPB Gold in Soil

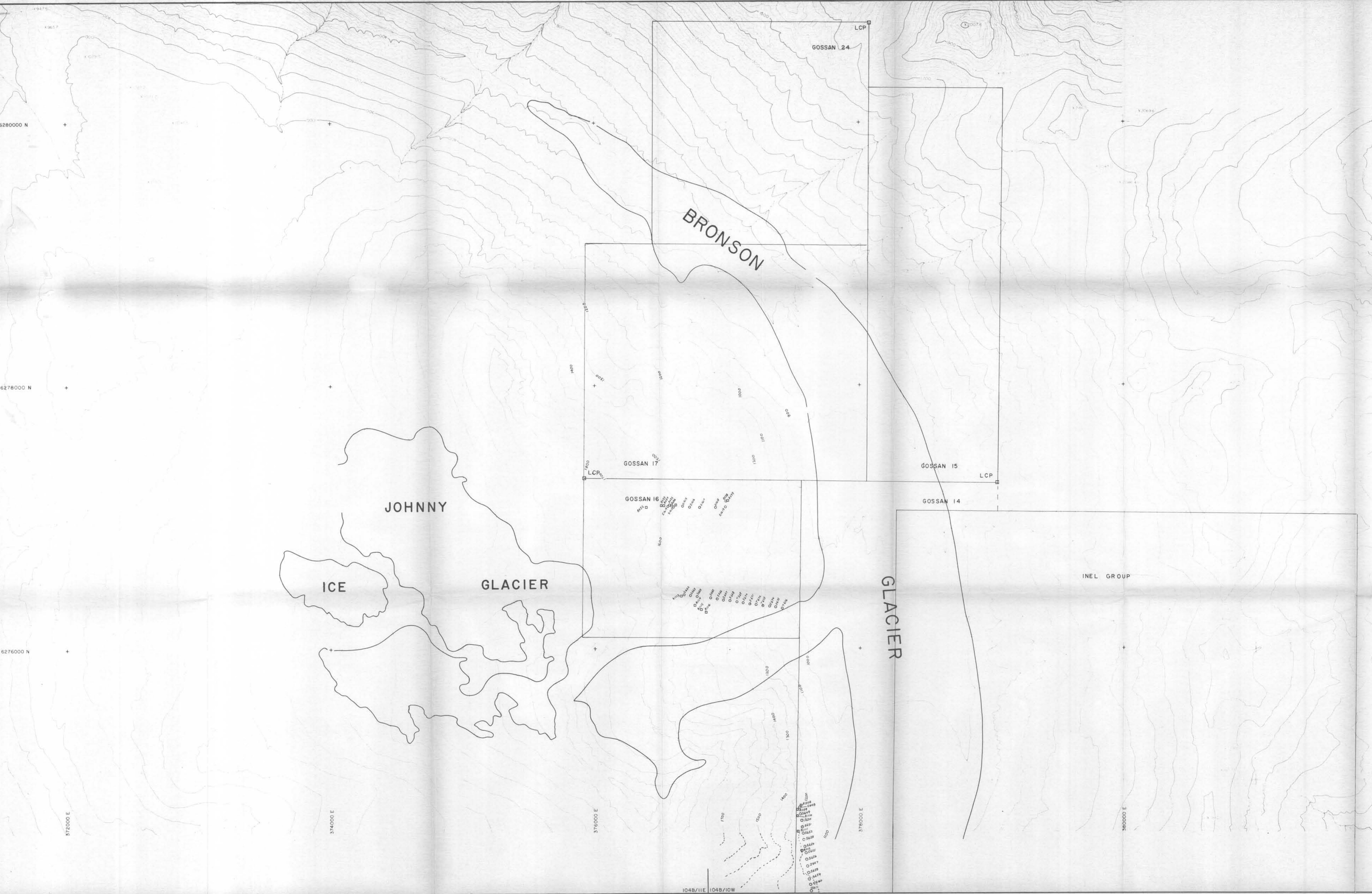
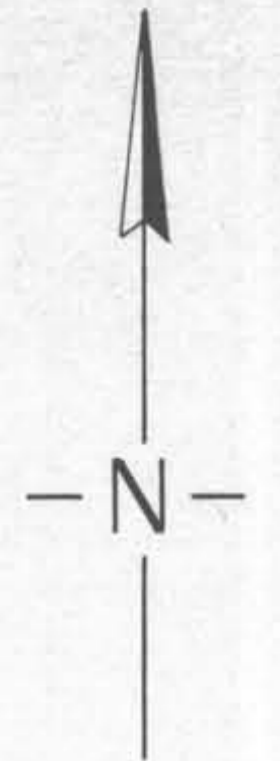
NOTE Contour Intervals in Metres.



GEOLOGICAL BRANCH  
ASSESSMENT REPORT

15,238

WESTERN CANADIAN MINING LTD.			
GOSSAN PROPERTY			
GOSSAN 1-4.7 CLAIM GROUP			
RECONNAISSANCE GEOLOGY and GOLD, SILVER GEOCHEMICAL VALUES			
WORK BY R.M., S.C.	DRAWN R.M., H.H.	DATE NOV./86	FIGURE 4b
REVISED		N.T.S. 104 B/10W	
SCALE 0 100 200 400 600 800 metres 1:10,000			



**LEGEND**

- <sub>S</sub> Soil (S) or talus (T) sample location & number.
- <sub>R</sub> Rock (R) sample location & number.

NOTE: Contour Intervals in Metres.

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

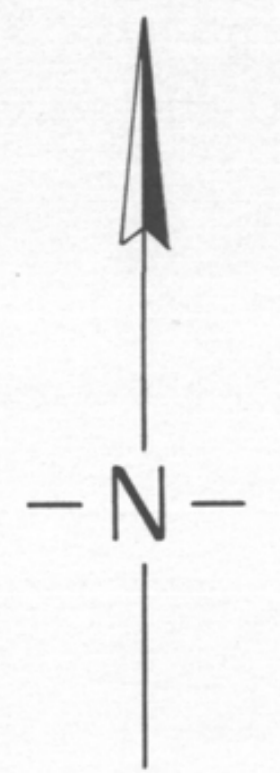
**15,238**

WESTERN CANADIAN MINING LTD.

GOSSAN PROPERTY  
GOSSAN 14-17, 23 CLAIM GROUP  
1986  
SAMPLE LOCATIONS

DATE: NOVEMBER, 1986	COMPILED BY: R.M.	FIGURE No.
N.T.S. 104B/10W-11E	DRAFTED BY: H.H.	5a
SCALE: 0 100 200 300 400 500 metres 1:10,000 RPT. No.		

104B/11E 104B/10W



**LEGEND**

**INTRUSIVE ROCKS**

Gd **Granodiorite**

**STRATIFIED ROCKS**

- 5 **Greywacke, tuffaceous, pyritic**
- 4 **Andesite, flow, tuff, breccia**
- 3 **Argillite**
- 2 **Basalt, massive**
- 1 **Siltstone, banded, pyritic**

**SYMBOLS**

- ↗ **Strike & dip of Bedding**
- ↗ **Strike & dip of Schistosity**
- - - **Geological Contact, inferred, projected.**
- — — **Fault**
- ↗ **Joints, orientation.**
- x **Mineral occurrence, showing.**
- <sup>2/10</sup> **Soil or talus sample, Gold PPB/Silver PPM.**
- <sup>2/10</sup> **Rock sample, Gold PPB/Silver PPM.**

NOTE: Contour Intervals in Metres.

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT  
15,238**

**WESTERN CANADIAN MINING LTD.**

**GOSSAN PROPERTY  
GOSSAN 14-17, 23 CLAIM GROUP  
RECONNAISSANCE GEOLOGY  
and  
GOLD, SILVER GEOCHEMICAL VALUES**

DATE: NOVEMBER, 1986	COMPILED BY: R.M.	FIGURE No.
NTS: 104B/10W-11E	DRAFTED BY: H.H.	5b
SCALE: 0 100 200 300 400 500 metres		1:10,000 RPT. No.