EQUITY
SILVER MINES
LIMITED

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ASSESSMENT REPORT

FOR THE

1986 DIAMOND DRILLING

ON THE

SG 19, 20, 21, 22, 23, 24, AND 30

MINERAL CLAIMS

OMINECA MINING DIVISION

NTS 93 L/1W, 1E

LATITUDE 54° 11.4' N

LONGITUDE 126° 16.2' W

OWNED BY: EQUITY SILVER MINES LIMITED

WORK BY: EQUITY SILVER MINES LIMITED

REPORT BY: R. B. PEASE

DECEMBER 1986

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,379

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INTRODUCTION

(i) Location and Access

The Equity Silver minesite is located 40 km southeast of the town of Houston, British Columbia (see Figure 1). The minesite lies in the gentle, and occasionally steep, hills of the Nechako Plateau physiographic region. Access is gained to the property by an all-weather gravel road from Houston (see Figure 2). The drillholes discussed in this report are located in the general area south of the abandoned Southern Tail pit (see Figure 3). Access to the drillsites is via recently constructed 4 x 4 trails which run south from the Southern Tail pit and north from the old Buck Flats logging road (see Figure 4).

(ii) Claim Ownership and Status

The Equity minesite property consists of Certified Mining Lease # 1 and Mining Lease # 6 surrounded by a block of 289 two-post mineral claims, 7 fractional claims, and 3 modified grid claims (43 units). In addition, 19 two-post claims and one fraction are jointly held with Teck Corporation and Pioneer Metals Corporation.

The drilling was conducted on the SG 19, 20, 21, 22, 23, 24, and 30 mineral claims. All of these claims are wholly owned by Equity Silver Mines Limited and are not subject to any vendor agreements. Their boundaries are shown on Figure 4. For the purpose of recording assessment, several adjoining claims have been grouped to form the 86 -2 group.

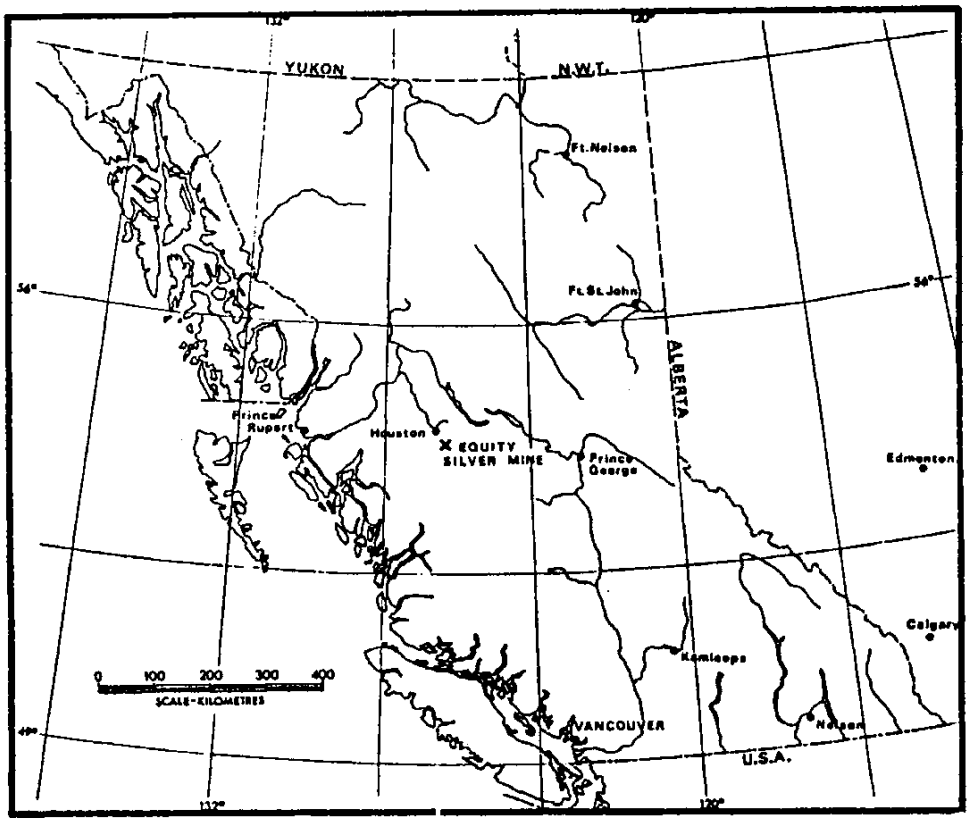

FIGURE 1 - MINESITE LOCATION

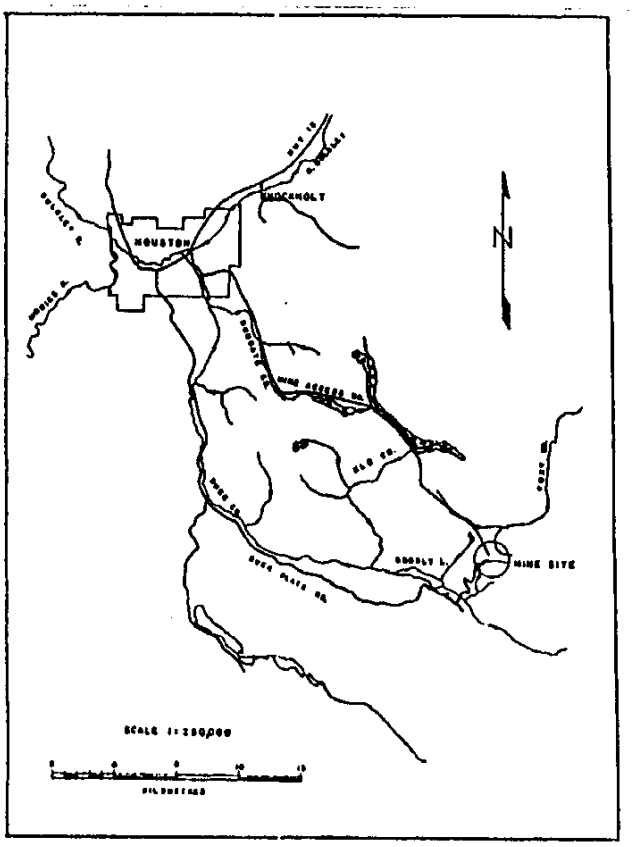

FIGURE 2 - MINESITE ACCESS

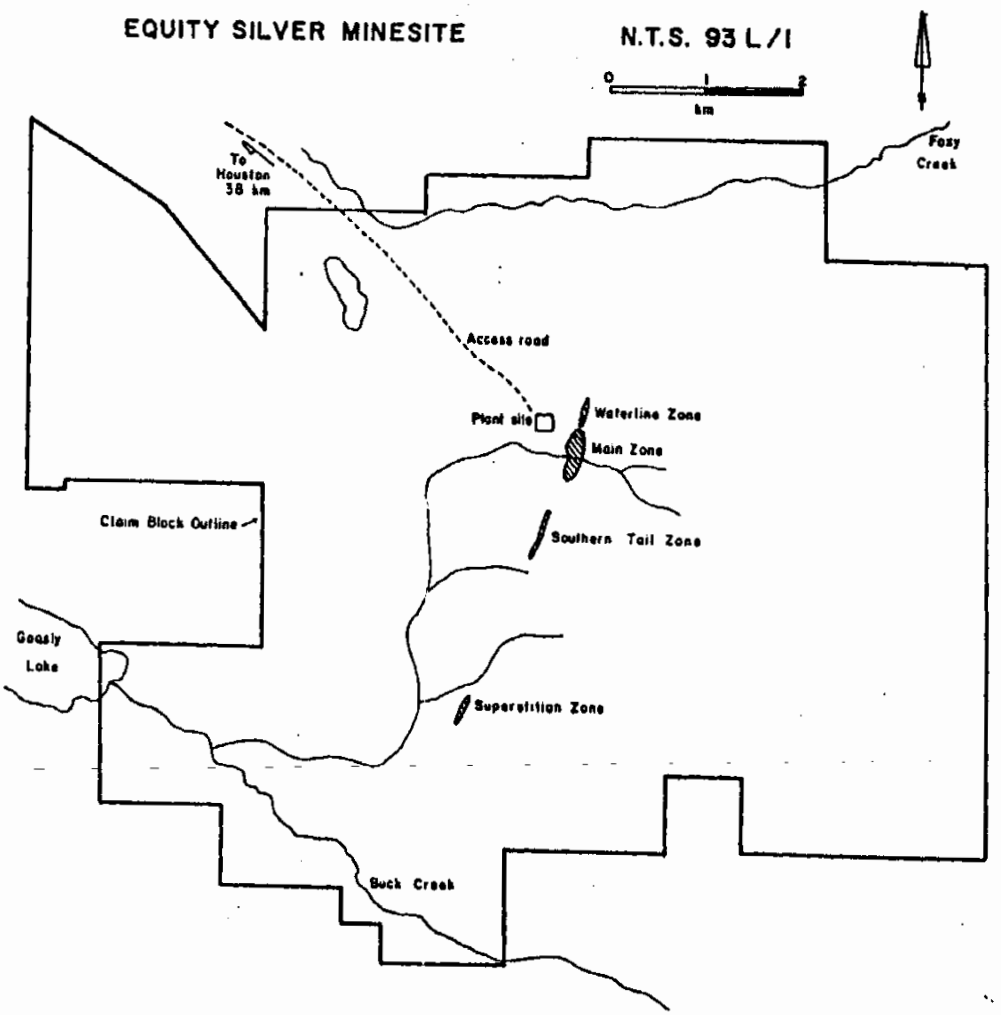

FIGURE 3 - PROPERTY LAYOUT

The company has been continuously operating a 5 500 tpd open pit mining and milling complex at this site since mid 1980. Production was increased to 10 000 tpd in mid 1986. Three ore deposits are known to occur on Certified Mining Lease # 1. The Southern Tail deposit has been mined out to the economic limit of an open pit. The Main Zone deposit is currently being mined by an open pit, and the Waterline deposit has yet to be developed. Proven ore reserves, as of January 1986, were approximately 17.8 million tonnes at a grade of 0.35% copper, 106 g/t silver, and 1.04 g/t gold.

(iii) Purpose

Eighteen NQ size diamond drillholes, totalling 3449.9 metres, were drilled to test possible mineralized structures. Ten holes were drilled north of Superstition Creek. Three holes had been drilled in previous years in this area, and some weakly mineralized structures were defined.

Eight holes were drilled south of Superstition Creek. Fourteen holes had been drilled in previous years in this area, and a low grade structure (termed the Superstition zone) was partially defined.

PROPERTY DESCRIPTION

(i) Geology

The geology of the Equity Silver property is briefly described below and illustrated on Figure 5. The reader is referenced to Cyr, et al. (1984) for a more detailed description.

The deposits occur in a homoclinal Upper Jurassic to Cretaceous inlier consisting of sedimentry, pyroclastic, and volcanic rocks flanked by intrusions and surrounded by younger, unconformable Tertiary andesitic to basaltic flows and flow breccias. Four stratigraphic conformable subdivisions, termed the Goosly Sequence, are recognized in the inlier and consist of a basal conglomerate and argillite (clastic division); intercalated sub-aerial tuffs and breccias (pyroclastic division); interbedded volcanic conglomerate, sandstone, and bedded tuff (sedimentry-volcanic division); and andesite and dacite flows (volcanic flow division). The Goosly sequence has an overall strike of 015 and dips generally to the west.

A quartz monzonite stock (58 m.y.) on the west, and a gabbro-monzonite complex (49 m.y.) to the east, intrude the Goosly sequence. Post-mineral andesite and quartz latite dykes (49 m.y.) crosscut the Goosly sequence and the gabbro-monzonite complex.

(ii) Mineralization

Economically significant Cu-Ag-Au mineralization occurs in three distinct zones designated the Main, Waterline, and Southern Tail orebodies (see Figure 5). Pyrite is the most abundant metallic

mineral throughout the Goosly sequence regionally, and within the zones of Cu-Ag-Au mineralization in particular. The principal silver mineral is tetrahedrite with minor values contributed by a variety of argentiferous minerals. Chalcopyrite is the principal copper mineral and a smaller but significant portion is in tetrahedrite.

The ore minerals are generally restricted to tabular zones subconcordant to host rock stratigraphy. They occur as disseminations, veins, fracture fillings, and locally as massive pods and matrix material in breccia zones. The primary ore control is structural, since "economic" sulphides tend to be best concentrated in zones of intense fracturing and brecciation.

It is believed the Cu-Ag-Au mineralization is epigenetic in origin. Intrusive activity resulted in the introduction of hydrothermal metal-rich solutions into the pyroclastic division of the Goosly sequence. Sulphides introduced into the more competent and permeable ash and lapilli tuffs of the Main and Waterline zones formed as stringers and disseminations which grade randomly into zones of massive sulphide. In the Southern Tail Zone, sulphides formed as veins, fracture fillings, and breccia zones in the brittle, less permeable fine grained dust tuff. Emplacement of postmineral dykes into all types of sulphide-rich pyroclastic rocks resulted in remobilization and concentration of sulphides adjacent intrusive contacts. Remobilization, concentration, and contact metamorphism of sulphides occurred in the Main and Waterline zones at the contact with the postmineral gabbro-monzonite complex.

(iii) Alteration

Alteration assemblages in the Goosly sequence are characterized by minerals rich in alumina, boron, and phosphorous. The distribution of various alteration zones is illustrated on Figure 6. Four types of alteration are recognized and briefly described below. The reader is referenced to Wojdak and Sinclair (1984) for a more detailed discussion.

1. Aluminous alteration is characterized by a suite of aluminous minerals including analusite, corrundum, pyrophyllite, and scorzalite. These alteration zones show a systematic spatial relationship to areas of mineral deposits.

2. Boron-bearing minerals consisting of tourmaline and dumortierite occur within the ore zones and in the hangingwall section of the Goosly sequence.

3. Phosphorous-bearing minerals including scorzalite, apatite, augelite, and svanbergite occur in the hangingwall zone, immediately above and intimately associated with sulphide minerals - particularly in the Main and Waterline zones.

4. Phyllic alteration is characterized by weak to pervasive sericite-quartz replacement. It appears to envelope zones of intense fracturing, with or without chalcopyrite/tetrahedrite occurences, particularly in Unit 2 dust tuffs.

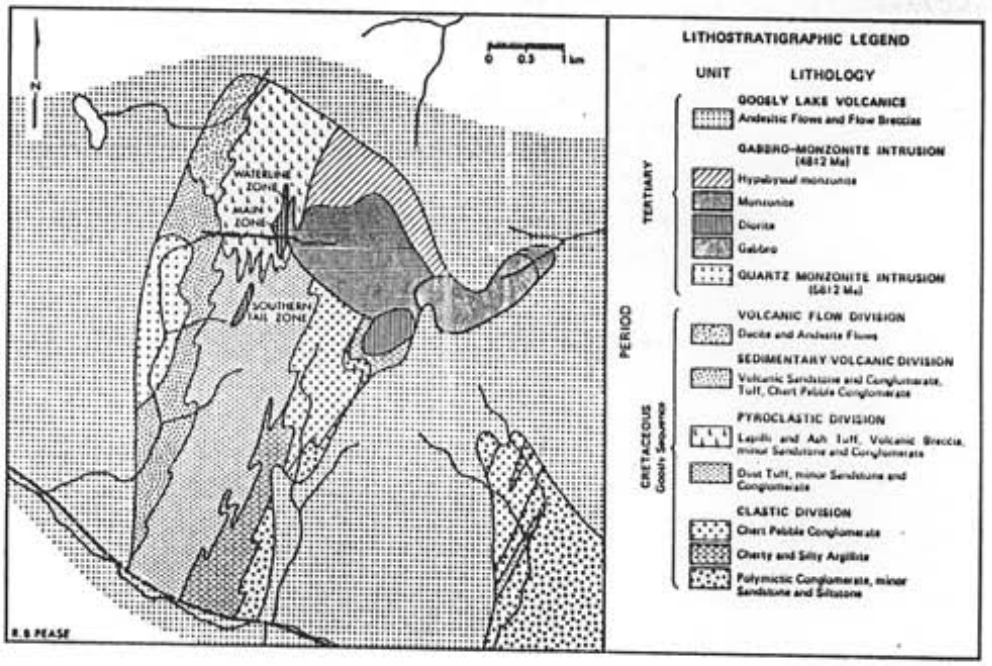

FIGURE 5 - PROPERTY GEOLOGY

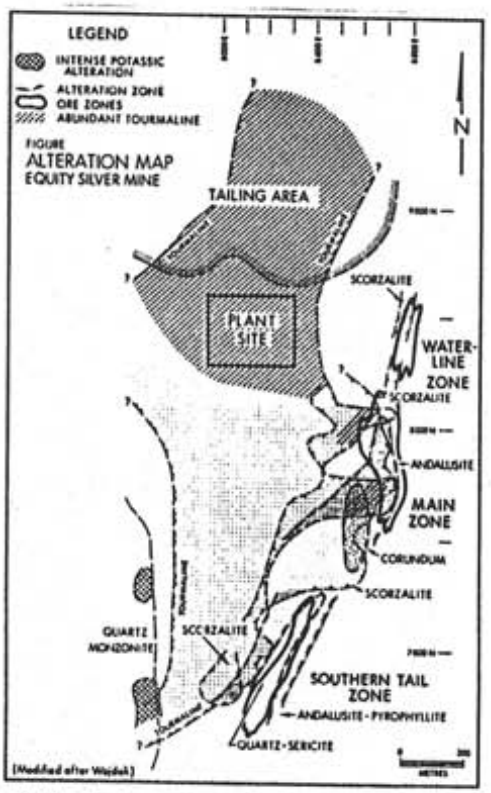

FIGURE 6 - PROPERTY ALTERATION

DRILLING PROGRAMME

The programme consisted of 3449.9 m of NQ wireline diamond drilling spread over eighteen (18) holes. The collar locations and surface projections of the drillholes are shown on Figure 4. All of the drillholes were inclined at angles from -45 to -70 degrees, and orientated in an easterly direction. This pattern was chosen to best intersect possible north-south, west dipping, mineralized structures striking through the general area.

The drill setup pads and access roads were constructed prior to drill mobilization by a contracted D8 tractor. The drilling contractor was G & D Diamond Drilling of Kamloops, B.C. A skid-mounted Longyear Super 38 wireline dig rig was utilized. The contractor supplied a tractor to move and assist the drill. The drilling of holes X86CH238, X86CH239, and X86CH240 commenced on March 20 and finished on March 29, 1986. The remaining drillholes, X86CH260 to X86CH274 were drilled sequentially from July 13 to August 26, 1986.

The core was transported to the logging facilities at the minesite immediately following hole completion. The core was logged by the author, Mr. Daryl Hanson and Mr. Ray Westendorf. Mr. Hanson, a geologist temporarily employed by Equity, has prevalent academic and practical training, holding a B.Sc. degree in geology and having over ten years experience in mineral exploration. Mr. Westendorf, a Carleton University geology student temporarily employed by Equity, logged three holes under the supervision of the author. The drillhole logs have been reproduced and are included in this report as

Appendix II. Assay results for the sampled intervals are recorded at the end of the logs. All assay results are recorded in percent, except silver and gold which are reported in grams/tonne.

A coded core logging system was utilized on this programme mainly to improve the measure of objectivity, consistency, measureability, and readability as compared to handwritten logs. The system allows geologic and assay data to be entered into formatted computer data files. These files can be accessed by programs which plot sections and plans, perform statistical analyses, and assist in reserve calculations. An explanation of the logging codes is provided in Appendix I.

The core was sampled top to bottom in approximately 3.0 metre intervals. Barren dyke intersections were generally omitted. Sampling was done by a hand operated core splitter. One half was placed in plastic sample bags and delivered to Equity's minesite laboratory for assay, and the other half was returned to the core box for permanent storage. The split core is stored in the facilities at the minesite.

The core samples were assayed for the metals Cu, Ag, Au, Sb, As, Fe, and Zn. In Equity's assay procedure, 1 gram of pulverized material is dissolved in 10 ml of nitric acid and 30 ml of hydrochloric acid. This solution is boiled for fifteen (15) minutes, after which 10 ml of 10% tartaric acid is added and the sample is returned to the hot plate for five (5) minutes. The solution is allowed to cool and quantitative analysis is done on an atomic absorption machine, except for Au which is fire assayed first.

RESULTS

(i) Overview

The geology of the drilling area is restricted to Unit 2 (Pyroclastic Division) and Unit 3 (Sedimentry - Volcanic Division) of the Goosly sequence. The Unit 2/Unit 3 contact is shown on Figure 4. The Unit 2 rocks intersected in the drilling consist mainly of massive, fine grained, green to tan dust tuffs. Some coarser grained ash and lapilli tuffs were also intersected. The Unit 3 rocks intersected in the drilling consist of interbedded chert pebble conglomerate, quartz sandstone, well-bedded dust and ash tuffs, and some volcanic conglomerate and sandstone. The chert pebble conglomerate and quartz sandstone tend to dominate the base of the unit, while the tuffs and sandstones are more common higher in the section. Both Unit 2 and 3 are cut by numerous andesite and quartz latite dykes.

The Units are believed to be steeply folded and have an overall strike of 017 degrees. The folding is apparent in Unit 3 rocks, but difficult to interpret in Unit 2 pyroclastics due to their massive nature and lack of well-preserved identifible bedding.

Unit 2 is considered the main target for hosting "economic" mineralization. The key guides to locating mineralization in this area are degree of fracturing, and alteration intensity. Low grade alteration (Propylitic) is characterized by chlorite lining fractures (microveins). Higher grade alteration is defined by increasing intensity of quartz-sericite (or phyllic) replacement. That is,

"economic" mineralization could be expected to occur in a zone of intense fracturing and pervasive phyllic alteration. The "economic" mineralization anticipated is chalcopyrite and/or tetrahedrite occurring in microveins. Accessory minerals could include sphalerite, arsenopyrite, and specular hematite. Pyrite occurring in microveins and disseminations is common throughout Unit 2 and 3. The distribution of lithology, fracture intensity, alteration, and Cu-Ag mineralization is summarized in the following hole by hole discussion. Descriptions of the frequent, post-mineralization dykes are generally omitted.

Some of the holes drilled north of Superstition Creek (see Figure 4) intersected a new mineralized structure which has been termed the Hope zone. The holes drilled in the Superstition zone lead to further definition of the zone. Both of these zones require further study and additional drilling to determine feasibility of mining. The Hope zone is poorly defined, and the grade of the Superstition zone appears to be below an economic level.

(ii) Hope Area

Holes X86CH238 and X86CH239 were drilled to intersect a possible southern extension of a weak structure previously defined to the north. The rock types intersected were Unit 2 dust tuffs, with minor ash units towards the end of the holes. Both holes display low fracture intensities, but rather pervasive quartz-sericite alteration. A few sporadic very low Ag assays were obtained, but they cannot be attributed to a significant structure.

Holes X86CH260 and X86CH261 were drilled on the same section as 238 and 239 but further to the east. This location tested a possible southern extension of the Southern Tail structure. Mainly Unit 2 dust tuffs were intersected, with some ash tuff near the top of 260 and a few intervals of lapilli tuff near the bottom of 261. The fracture intensity was relatively low throughout both holes. In hole 260, weak to moderate quartz-sericite alteration was observed above 61.0 metres, and only chlorite alteration occurs below. Hole 261 displays a very similiar alteration pattern with weak to moderate quartz-sericite above 101.0 metres, and chlorite below. Weak sporadic chalcopyrite in microveins was noted above 49.0 metres in hole 260. Two low grade intersections were found in hole 261, from 103.0 to 106.0 metres (0.38% Cu, 28 g/t Ag) and from 124.0 to 126.3 (0.24% Cu, 15 g/t Ag) metres.

Hole X86CH240 was drilled to test a possible up-dip extension of a small mineralized zone located by a hole drilled in 1970. Hole 240 intersected Unit 2 ash tuffs which displayed relatively high fracture intensity and moderate to pervasive quartz-sericite alteration. No significant mineralization was located. At a later date, hole X86CH262 was drilled on the same section but down-dip of the 1970 hole. A relatively good mineralized intersection was found, and termed the Hope zone. Hole X86CH273 was drilled further down-dip on the same section, and holes X86CH272 and X86CH274 were drilled approximately 100 metres to the south and north respectively, in an attempt to trace the zone.

All of these holes (262, 272, 273, 274) were collared in interleveled Unit 3 chert pebble conglomerates, quartz sandstones, and well-bedded ash and dust tuffs, and passed into Unit 2 dust tuffs to

the end of the hole. In hole X86CH262, the Unit 2 dust tuffs display medium to high fracture intensity and moderate to strong phyllic alteration down to approximately 270 metres. Below this point, the tuffs display only low to medium fracture intensity and chloritic alteration. Hole 262 contains a zone approximately 100 metres long of sporadic Cu-Ag mineralization broken by a few post-mineralization dykes. Two of the better intersections include; 167.0 to 194.0 metres averaging 0.57% Cu and 14 g/t Ag, and 235.0 to 256.3 metres averaging 0.39% Cu and 298 g/t Ag. These zones contained chalcopyrite and tetrahedrite in microveins.

The Unit 2 dust tuffs in hole X86CH273 displayed relatively high fracture intensity and pervasive quartz-sericite alteration to the end of the hole. However, only sporadic low grade mineralization was intersected. The interval from 228.0 to 267.3 metres averaged 0.23% Cu with a few low Ag assays. In hole X86CH274, the Unit 2 dust tuffs displayed the same fracture and alteration pattern as hole 273. Two sections of chalcopyrite and tetrahedrite occurring in microveins were located from 229.0 to 236.8 metres (0.50% Cu, 109 g/t Ag), and from 291.0 to 299.1 metres (0.26% Cu, 75 g/t Ag).

The Unit 2 portion of hole X86CH272 is dominantly dust tuff, but contains some interleveled ash tuff. The tuffs display a medium to high fracture intensity and moderation to pervasive phyllic alteration. Only low grade mineralization was intersected. A zone from 164.0 to 251.0 metres contains sporadic chalcopyrite in microveins with a few tetrahedrite occurences.

Farther to the south, hole X86CH263 was drilled up-section from a 1970 drillhole. Unit 2 dust tuffs were encountered throughout the

hole (except dykes). Down to 55.1 metres, only low fracture intensity and chloritic alteration was observed. From 55.1 metres to the end of the hole, medium fracture intensities and weak to moderate phyllic alteration was encountered. A zone from 57.0 to 119.0 metres contains sporadic chalcopyrite in microveins. A few patches of chalcopyrite, numerous occurences of tetrahedrite, and relatively high amounts of sphalerite, all occur in microveins from 159.0 to 186.2 metres.

(iii) Superstition Zone

Holes X86CH264 and X86CH265 were drilled to intersect the northerly trace of the Superstition zone structure. Hole 264 was collared in Unit 3 volcanic sandstone and chert pebble conglomerate, and passed into Unit 2 dust tuffs with minor ash tuff units to the end of the hole. Hole 265 intersected Unit 2 dust tuffs throughout, except for some ash tuff units towards the end of the hole. Both holes are cut by numerous dykes.

The Unit 2 portion of hole 264 from 89.0 to 130.0 metres, displays low fracture intensity and propylitic alteration, with a few sporadic chalcopyrite occurences in microveins. From 130.0 metres to the end of the hole, a medium to high fracture intensity was observed, with weak to moderate phyllic alteration. The zone from 133.0 to 145.0 metres contains numerous chalcopyrite and tetrahedrite in microveins, averaging 0.21% Cu and 40 g/t Ag. Hole 265 contains medium to high fracture intensity and moderate phyllic alteration throughout. The zone from 48.8 to 61.3 metres averaged 0.49% Cu with a low Ag grade of 9 g/t. Sphalerite occurences in microveins were found towards the end of both holes (particularly 265) with no associated chalcopyrite or tetrahedrite.

Hole X86CH266 was drilled down-section of a 1984 hole. Unit 2 dust tuffs were intersected throughout the hole. The zone from 101.0 to 203.0 metres displayed moderate to high fracture intensity with some brecciation, and pervasive phyllic alteration. The balance of the hole contained medium fracturing and weak to moderate phyllic alteration. Sporadic chalcopyrite with occasional tetrahedrite was found in microveins from 101.0 to 203.0 metres. The section from 188.0 to 203.0 metres averaged 0.32% Cu, and 37 g/t Ag.

Hole X86CH267 was located inbetween two previously drilled holes, but was prematurely terminated at 108.2 metres due to drilling problems. The hole should have continued to at least 150 metres to have properly tested the target. Unit 2 dust tuffs with considerable ash tuff interleveled were intersected. Down to 40.2 metres, the fracture intensity was low, and weak quartz-sericite alteration was observed. From 40.2 metres to the end of the hole, the fracture intensity increased and the phyllic alteration became pervasive. A few sporadic chalcopyrite occurences in microveins were encountered.

Hole X86CH269 was drilled up-section (albeit 30 m to the south), and holes X86CH268 and X86CH271 were drilled down-section of a previous hole. Hole 268 was abandoned in a fault zone at 72.9 metres, and hole 271 was drilled later at a steeper angle to test the same zone.

Hole 269 intersected Unit 2 dust tuffs. A medium fracture intensity and moderate to occasionally pervasive phyllic alteration was encountered down to 56.1 metres. Below this depth, only low fracturing and weak to moderate phyllic alteration were observed. A few chalcopyrite occurences in microveins were noted near the top of the hole. Hole 271 intersected Unit 2 dust tuffs with some

interleveled lapilli tuff towards the end of the hole. A low fracture intensity with generally only chloritic alteration was observed down to 88.0 metres. From 88.0 to 162.0 metres, a medium to high fracture intensity and moderate to pervasive phyllic alteration with a few silicified intervals was encountered. In the balance of the hole, a low fracture intensity and propylitic alteration was found. Hole 271 was essentially devoid of chalcopyrite/tetrahedrite mineralization.

Hole X86CH270 was drilled inbetween two previous holes. It was collared in Unit 2 ash tuff to 39.0 metres and passed into dust tuff to the end of the hole. Down to 54.8 metres, a low fracture intensity, and propylitic with some weak phyllic alteration was observed. In the zone from 54.8 to 98.0 metres, the fracture intensity increased and moderate phyllic alteration with a few intervals of silification was encountered. Below 98.0 metres, the fracture intensity was low and only propylitic alteration was noted. Sporadic, but some good grade, chalcopyrite and tetrahedrite mineralization was intersected in the zone from 54.8 to 98.0 metres. The section from 61.0 to 76.0 metres averaged 0.28% Cu and 28 g/t Ag, and the section from 82.0 to 88.0 metres averaged 0.35% Cu and 118 g/t Ag.

TABLE 1

STATEMENT OF EXPENDITURES

1.	Construction of Drillsites and Access Roads	
	D8 Tractor, 180 hours @ 117.50	$ 21 150.00
2.	Diamond Drilling	
	3449.9 metres @ 35.27/m	121 677.97
	Consumables	4 926.67
3.	Sample Assaying	
	998 samples @ 15.00/sample	14 970.00
4.	Salaries	
	R. Pease, logging and supervision	
	March 20, 21, 24	
	July 15, 16, 17, 22, 23, 24, 25, 29, 29, 30, 31	
	August 12, 13, 14, 15, 19, 20, 27, 28	
	22 days @ 185.00/day	4 070.00
	D. Hanson, logging and supervision	
	March 24, 25, 26, 27, 31, April 1	
	July 14, 15, 18, 21	
	August 5, 6, 7, 8, 11, 18	
	16 days @ 165.00/day	2 640.00
	G. Saretsky, splitting and sampling	
	March 20, 21, 24, 25, 26, 27, 31, April 1, 2	
	July 17, 22, 29, 31	
	August 5, 7, 11, 12, 13, 22, 25, 26, 27, 28, 29, Sept. 2	
	25 days @ 115.00/day	2 875.00
	R. Westendorf, splitting, sampling, and logging	
	July 16, 25, 30, 31	
	August 1, 7, 15, 19, 20, 21, 25, 26, 27, 28, 29	
	16 days @ 95.00/day	1 520.00
	R. Barnes, splitting and sampling	
	July 16, 23, 25, 28, 30	
	August 1, 6, 8, 14, 25, 26, 27, 28	
	13 days @ 95.00/day	1 235.00
	M. Meleski, splitting and sampling	
	July 17, August 6, 8, 15, 18, 29	
	6 days @ 100.00/day	600.00
5.	Vehicle Rental and Fuel	
	50 days @ 50.00/day	2 500.00
6.	Report Preparation	2 000.00
		$180 164.64

AUTHOR'S QUALIFICATIONS

I, Robert B. Pease, do hereby certify that:

1. I am a geologist residing at R. R. # 1, Kerr Road, Telkwa, British Columbia.

2. I am a 1981 graduate of the University of Waterloo, Waterloo, Ontario, with an Honours Bachelor of Science degree in Earth Sciences.

3. As a student, I spent some twenty (20) months employed in the mineral exploration field with several mining companies in various regions of Canada.

4. I was employed as an exploration geologist with Duval International Corporation in Vancouver from May 1981 to January 1982.

5. Since February of 1982, I have been continously employed as an exploration geologist with Equity Silver Mines Limited in Houston, British Columbia.

6. I am an Associate Member of the Geological Association of Canada, and a Member of the Canadian Institute of Mining and Metallurgy.

7. I personally supervised the work programmes as described in this report.

Respectfully submitted,

EQUITY SILVER MINES LIMITED

R. B. Pease, B.Sc.
Exploration Geologist

REFERENCES

Cyr, J. B.; Pease, R. B.; and Schroeter, T. G. (1984): Geology and Mineralization at Equity Silver Mine. Journal of Econ. Geol., Vol. 79, pp. 947-968.

Wojdak, P. J. and Sinclair, A. J. (1984): Equity Silver Ag-Cu-Au Deposit: Alteration and Fluid Inclusion Studies. Journal of Econ. Geol., Vol. 79, pp. 969-990.

APPENDIX I

Diamond Drillhole Logging Code Explanation

LOGGING CODE EXPLANATION

Column 1 is a key which indicates the type of data or information on each line.

I - Identity information/data
S - Survey data
/ - Upper tier geologic data
L - Lower tier geologic data
R - Free form remarks
A - Assay and analysis data

I DATA

Each drillhole has two I lines at the start.

The first line indicates:

Col. 17 to 24 - Drillhole Name
Col. 26 to 27 - Size of Core
Col. 29 to 35 - Day/Month/Year Logged
Col. 36 to 38 - Logger's Initials
Col. 39 to 41 - Helper's Initials (if any)
Col. 42 to 45 - Drilling Contractor
Col. 46 to 50 - Month/Year Hole Drilled
Col. 51 to 53 - Drill Rig Type
Col. 63 to 68 - Grid Azimuth (0.0 if True North)

The second line indicates:

Col. 5 to 45 - Company Name
Col. 46 to 80 - Zone and type of Geocode* used.

NOTE: * Equity uses two types of Geocodes, ST and MN. The ST geocode is used when a hole is drilled south of the Main Zone, and the MN geocode is used to the north of, and including, the Main Zone. This is done to reflect the differing host rock and style of mineralization/alteration between the northern and southern sections of the property.

S_DATA

The S000 line is the collar survey data. Subsequent S lines (S001, S002, etc.) are down-the-hole surveys.

Col. 5 to 10 - From (a decimal point is inferred between column 8 and 9)
Col. 11 to 16 - To (a decimal point is inferred between column 14 and 15)
Col. 17 to 18 - Units; MT (metres), FT (feet)
Col. 20 to 26 - Total Length
Col. 27 to 32 - Azimuth
Col. 33 to 38 - Dip
Col. 51 to 60 - Northing
Col. 61 to 70 - Easting
Col. 71 to 80 - Elevation

/_AND_L_DATA

Disregard the /SCL and LSCL lines, they are only for computer processing. Two lines are available to describe a geologic interval, the upper line (/) and the lower line (L). The /NAM line defines the mineral fields for the upper line, and the LNAM defines the lower line. These mineral fields change according to the type of Geocode (ST or MN) used.

ST Geocode - upper (/NAM) line

Col. 57, 58 MS - Muscovite (sericite)
Col. 59, 60 CL - Chlorite
Col. 61, 62 QZ - Quartz
Col. 63, 64 PY - Pyrite
Col. 65, 66 CP - Chalcopyrite
Col. 67, 68 TT - Tetrahedrite
Col. 69, 70 AS - Arsenopyrite
Col. 71, 72 PR - Pyrrhotite

- lower (LNAM) line

Col. 57, 58 CB - Carbonate
Col. 59, 60 GY - Gypsum
Col. 63, 64 MG - Magnetite
Col. 65, 66 HE - Hematite
Col. 67, 68 SL - Sphalerite
Col. 69, 70 GL - Galena
Col. 71, 72 MO - Molybdenum

MN Geocode - upper (/) line

Col. 57, 58 QZ - Quartz
Col. 59, 60 SZ - Scorzalite
Col. 61, 62 TO - Tourmaline
Col. 63 to 72 - Same as ST Geocode

- lower (L) line

Col. 57, 58 DM - Dumortierite
Col. 59, 60 CB - Carbonate
Col. 61, 62 CL - Chlorite
Col. 63 to 72 - Same as ST Geocode

Upper (/) Geologic Data

Col. 5 to 10 - From (decimal inferred between 8 and 9)
Col. 11 to 16 - To (decimal inferred between 14 and 15)
Col. 17 to 20 - Recovery in Metres (decimal inferred between 18 and 19)
Col. 24 to 27 - Rock Type Code - See Rock Type Chart
Col. 28 to 29 - Typifying Mineral 1 - see Mineral Chart
Col. 30 to 31 - Typifying Mineral 2 - see Mineral Chart
Col. 35 to 36 - Texture 1 - see Texture Chart
Col. 37 to 38 - Texture 2 - see Texture Chart
Col. 47 - Essentially always a "P" which stands for Principle Geologic Interval. If "D", it stands for Ditto Interval which means all of the above interval description applies, except as noted.
Col. 49 to 50 - Structure 1 - see Structure Chart
Col. 55 to 56 - Angle to Core Axis of Structure 1
Col. 57 - Mineral Field, Mode of Occurence - see How Chart
Col. 58 - Mineral Field, Amount of Occurence - see Amount Chart
Col. 59 to 72 - Mineral Fields, same pattern continues (ie. How, Amount) as in columns 57, 58.

Lower (L) Geologic Data

Col. 17 to 20 - RQD in Metres (decimal inferred between 18 and 19)
Col. 28 to 29 - Colour Code - see Colour Chart
Col. 35 to 36 - Typifying Mineral 3 - see Mineral Chart
Col. 37 to 38 - Typifying Mineral 4 - see Mineral Chart
Col. 43 - Count of Fractures at Steep Angle to Core Axis - See Amount Chart
Col. 44 - Count of Fractures at Medium Angle to Core Axis - See Amount Chart
Col. 45 - Count of Fractures at Low Angle to Core Axis - See Amount Chart
Col. 46 - Count of Total Fractures - See Amount Chart

NOTE: Columns 43 to 46 not always used

Col. 49 to 50 - Structure 2 - see Structure Chart
Col. 55 to 56 - Angle to Core Axis of Structure 2
Col. 57 to 72 - Mineral Fields, as in upper (/) Data

R_DATA

These are free form remarks written by the logger to further describe the gelogic interval. Note that Rock Type Codes (see Rock Type Charts) are often used.

A_DATA

This last type of data lists the assay information for the hole. Note that remarks are also used.

The first line, A001, defines a "set" of assay data. eg. A002 would define a different set, etc. The following lines describe and list the assay data.

ALAB Col. 17 to 80 - Define Laboratory
ATYP Col. 17 to 80 - Define Type of Determination
AMTH Col. 17 to 80 - Define Analytical Method
AUMM Col. 17 to 80 - Define Assay Fields
A001 Col. 5 to 10 - From (decimal inferred between 8 and 9)
Col. 11 to 16 - To (decimal inferred between 18 and 19)
Col. 23 to 26 - Sample Number
Col. 33 to 38 - Percent Copper
Col. 39 to 44 - Grams/Tonne Silver
Col. 45 to 50 - Grams/Tonne Gold
Col. 51 to 56 - Percent Antimony
Col. 57 to 62 - Percent Arsenic
Col. 63 to 68 - Percent Iron
Col. 69 to 74 - Percent Zinc

CHARTS

1. Rock Type Chart

A four digit code is used to describe rock types. The first and second digits are common to both ST and MN Geocodes. The first digit (number) defines stratigraphic unit, and the second digit (letter) defines a lithology unique to the stratigraphic unit. In the ST Geocode, the third digit (number) defines the intensity of fracturing

or brecciation, and the fourth digit (number) defines the type and intensity of alteration. In the MN Geocode, the third digit (number) defines the alteration, and the fourth digit (number) defines the mineralization.

One special code, OVBN, is used for overburden.

First Digit	Stratigraphic Unit	Second Digit	Lithology
1	Clastic Division	A	Polymictic Conglomerate
		B	Cherty or Silty Conglomerate
		C	Chert Pebble Conglomerate
		D	Quartz Sandstone
		E	Cherty Argillite
		F	Silty Argillite
2	Pyroclastic Division	A	Flow Breccia
		B	Ash Flow
		C	Dust Tuff
		D	Ash Tuff
		E	Lapilli Tuff
		F	Volcanic Breccia
		G	Volcanic Sandstone
		H	Volcanic Conglomerate
		I	Welded tuff
		J	Interbedded Dust and Ash Tuff
		K	Lahar
		L	Tuffaceous Siltsone
		M	Claystone
3	Sedimentry - Volcanic Division	A	Chert Pebble Conglomerate
		B	Quartz Sandstone
		C	Laminated Dust Tuff
		D	Volcanic Conglomerate
		E	Volcanic Sandstone
		F	Dust Tuff
		G	Ash Tuff
		H	Lapilli Tuff
		I	Volcanic Siltstone
		J	Interbedded Dust and Ash Tuff
		K	Silty Argillite
4	Volcanic Flow Division	A	Andesite Flow
		B	Dacite Flow
6	Quartz Monzonite	A	Fresh Quartz Monzonite
		B	Altered (Potassic) Quartz Monzonite

7	Gabbro-Monzonite Complex	A	Gabbro
		B	Diorite
		C	Monzonite
		D	Hypabyssal Monzonite Prophyry
		E	Gabbro - Monzonite Transition Phase
8	Property Dykes	A	Andesite
		B	Trachyandesite
		C	Quartz Latite
9	Tertiary Volcanics (Goosly Lake Fm)	A	Trachyandesite Flow
		B	Amygdaloidal Andesite Flow
		C	Flow Breccia
		D	Reddish-Purple Flow
		E	Massive Andesite Flow
		F	Quartz-eye Porphyry (Latite)
		G	Tuffaceous Sandstone/Siltstone

ST - Geocode

Third Digit	Intensity of Fracturing or Brecciation
0	No Fracturing
1	Weak Fracturing
2	Moderate Fracturing
3	Mod to Strong Fracturing
4	Strong Fracturing
5	Weak Brecciation
6	Weak to Mod Brecciation
7	Moderate Brecciation
8	Mod to Strong Brecciation
9	Strong Brecciation

Fourth Digit	Type and Intensity of Alteration
0	Unaltered
1	Weak Propylitic (CHL - CLAY)
2	Strong Propylitic
3	Weak Phyllic (QTZ - SER.)
4	Moderate Phyllic
5	Pervasive Phyllic
6	Advanced Argillic
7	Weak Potassic
8	Strong Potassic
9	Silicic (QTZ)

MN - Geocode

Third Digit	Alteration
0	Unaltered
1	Propylitic
2	Scorzalite Bearing/Argillic
3	Andalusite Bearing/Argillic
4	Moderate Silicification
5	Strong Silicification
6	Biotite Hornfels
7	Pyrite Porphyroblast Bearing
8	Phyllic (Quartz-Sericite)
9	Quartz - Tourmaline

Fourth Digit	Sulphide Mineralization
0	None
1	Disseminated Pyrite +/- Chalcopyrite
2	Pyrite - Magnetite Intergrowths
3	Sulphide Bearing (CP+/-PY+/-SL) Stringers
4	Sulphide Bearing (CP+/-PY) Patches
5	Massive Sulphide (CP+/-PY+/-TT+/-PO+/-SL) Replacements or Remobilized
6	Grey, "Dusty" Sulphides (fine grained mixture of sulphides and quartz)
7	Sulphides in Breccia Matrix (CP+/-PY+/-TT+/-SL)

2. Mineral Chart (ie. Mineral short-forms)

QZ	Quartz
CL	Chlorite
CY	Clay
CB	Carbonate
PY	Pyrite
MS	Muscovite
CP	Chalcopyrite
TT	Tetrahedrite
AS	Arsenopyrite
PR	Pyrrhotite
MG	Magnetite
HE	Hematite
SL	Sphalerite
GL	Galena
MO	Molybdenite
GY	Gypsum
EP	Epidote
FL	Feldspar
BI	Biotite

3. Texture Chart (ie. Texture Short-Forms)

<<	Micro Veins
MX	Massive
BR	Brecciated
P*	Porphyritic
A*	Amygdaloidal
TC	Trachytic
WP	Wispy
VU	Vugs
AD	Adherring/Pyroclastic
RC	Chilled Rind/Pyroclastic

4. Structure Chart (ie. Structure Short-Forms)

C/	Contact
BD	Bedding
V/	Vein
F/	Fault
BN	Banding
FB	Flow Banding
CU	Upper Contact
CL	Lower Contact
SH	Shear

5. How Chart

Symbol	Most Dominant Mode of Occurence
A	Amygdaloids, cavity fillings
B	Blebs
#	Breccia fillings
C	Coatings & encrustations
*	Clasts
D	Disseminations & scat.x'ls
E	Envelopes
F	Framework crystals
G	Gouge
H	Halos
I	Eyes, augen
J	Interstitial
K	Stockwork
L	Laminated/bedded
M	Massive
N	Nodules
O	Spots
Q	Patches, as in quilts
R	Rosettes & x'tls clusters
S	Selvages
$	Sheeting
T	Stainings, as in tarnish
U	Euhedral crystals

V	Veins
>	Macroveins
<	Microveins
W	Boxwork
X	Massive and/or laminated/bedding
Y	Dalmationite
Z	Fresh, primary rock
+	Flooding

6. Amount Chart

Code	Assigned Value	Range
X	100	100
9	90	85 to 99
8	80	75 to <85
7	70	65 to <75
6	60	55 to <65
5	50	45 to <55
4	40	35 to <45
3	30	25 to <35
2	20	15 to <25
1	10	7 to <15
=	5	4 to < 7
+	3	2 to < 4
)	1	.5 to < 2
*	.3	.2 to <.5
(	.1	.05 to <.2
-	.03	.02 to <.05
.	.01	Trace = <.02
0	0	Nil, Absent
/	.07	Present: Estimate impossible
?	0	Possibly Present

7. Colour Chart

The colour chart can be used in two ways. A lightness can be combined with a colour, or two colours can be combined.

eg. 3U - Dark Brown

or

RU - Reddish Brown

Lightness		Colour	
Symbol	Value	Symbol	Colour
9	palest	R	Red

8	pale
7	light
6	lighter
5	medium
4	darker
3	dark
2	very dark
1	darkest

U	brown (Umber)
O	Orange
T	Tan (khaki)
Y	Yellow
L	Lime (Y-G)
G	Green
Q	Aqua (B-P)
B	Blue
V	Violet (B-P)
P	Purple
M	Mauve (P-R)
W	White
A	Gray
N	Black (Noir)

APPENDIX II

Diamond Drillhole Geologic Logs

and

Assay Data

NOTE: All Drillholes were logged using ST Geocode

```
IDEN6B0201      X86CH238 NQ 20MAR86RBP   G&D MAR86S38          0.0
IPRJ          EQUITY SILVER MINES LTD        SOUTH OF S.T. - ST GEOCODE
S000   00   419 MT  157.3 090.0 -45.0              6227.50   7677.82   1281.18
S001  419  1206     157.3 090.0 -42.0
S002 1206  1573     157.3 090.0 -44.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                      MSCLQZPYCPTTASPR
LNAM                                                      CBGY  MGHESLGLMO
/      00   152        OVBN                    P
L
R               CASED TO 15.2 M. NO OXIDE IN FIRST CORE. SUSPECT CASING WELL
R               INTO BEDROCK. ACTUAL BEDROCK DEPTH LIKELY 2 TO 3 M.
/     152   184  20    2C13MS     <<           P           <)<(<*
L                  00        5T
R               CORE IS VERY BROKEN. NO OXIDE ZONE.
/     184   244  54    2C12CL     <<           P           <+  <(
L                  06        TG
R               CORE STILL VERY BROKEN.
/     244   293  35    2C13MS     <<           P           E)<(<*
L                  05        5T
R               CORE STILL VERY BROKEN. GOOD TYPICAL 2C13.
/     293   315  21    2C34MS     <<           P           E(<)<+<(
L                  13        6T            ++=1           <-
/     315   332  16    2C45MS     <<           P             <(<*
L                  09        7T            +1=2                <(
/     331   332                               D F/
/     332   389  54    2C34MS     <<BR         P           E(<)<)
L                  15        6T            12=4                <(
R               SPOT OF OXIDE AT 35.9 M.
/     389   408  09    2C45MS     <<           P           D)  D)
L                  00        7T
/     398   408                               D F/
R               RUMBLE FROM 39.8 TO 40.8, VERY LOW RECOVERY, LIKELY FAULT
R               ZONE.
/     408   439  11    2C34MS     <<BR         P           E(++D)<.
L                  00        6T
/     420   439                               D F/
R               RUMBLE FROM 42.0 TO 43.9, VERY LOW RECOVERY, LIKELY FAULT
R               ZONE.
/     439   497  55    2C23MS     <<           P           E*<)<+
L                  13        5T            ++23
R               MINOR 2D AT 47.6 M.
/     497   503  16    2C75MSQZ   BF<<         P             #1#+
L                  13        6T            ))+=
R               NICE STRUTURE, BUT WHERE'S THE BEEF!
/     503   532  27    2C13MS     <<           P             <*<)
L                  19        TA            =1+2
R               CONSIDERABLE DISSEMINATED PYRITE IN THIS INTERVAL.
/     532   566  32    2C14MS     <<           P             <*<)
L                  11        5T            =2=3
/     566   590  22    2C55MSQZ   BR<<         P           <(#=#+
L                  09        5T            +==1
/     590   674  77    2C24MS     <<           P           E)<*<)
L                  19        6T            1214
```

```
R                CHLORITE GIVES BLUE COLOUR TO <<'S. CORE QUITE BROKEN, BUT
R                UNIFORM.
/     674   689  15    2C13      <<          P          <)<(<*
L                  13       TG            )1+2
/     689   725  26    2C24MS    <<BR        P          <*V)V+
L                  00       6T
R                MINOR BRECCIATION. CORE QUITE BROKEN, POOR RECOVERY.
/     725   813  80    2C14MS    <<          P          <)V*<)
L                  21       6T            11+3
/     813   820  07    2C55MS    BR<<        P          <)#+#=
L                  03       TA
R                BLUE TARNISH ON SOME PYRITE GRAINS.
/     820   831  10    2C23      <<          P          <)<)<)
L                  00       5T            1102
/     831   856  23    2C13      <<BR        P          <)V*V+
L                  06       AT            11=3
R                MINOR BRECCIATION.
/     856   912  51    2C24MS    <<          P          E)Q)Q+
L                  03       AT            12=4
R                CORE QUITE BROKEN, DISRUPTED. IE. MINOR DISPLACEMENT ON <<'S.
/     912   942  29    2C14MS    <<          P          E)<)<)
L                  03       5T            11+3
/     942  1001  56    2C24MS    <<BR        P          E)V+Q=
L                  11       AT      VU    12=4
R                CORE VERY BROKEN. VERY SIMILIAR TO 85.6 TO 91.2 M.
/    1001  1073  55    2C14MS    <<          P          E)<)<+<?
L                  03       5T                                 <.
R                CORE VERY BROKEN, POOR RECOVERY.
/    1073  1099  25    2C13      <<WP        P          <*V*<)
L                  11       5T            +1+2
/    1099  1137  37    2C12CL    <<          P V/   68  <)V(<(D.D?
L                  31       4A            ==+2                V.
R                SPOT OF ASH TUFF AT 112.0 M.
/    1137  1146  09    2C29QZ    <<BR        P          <)+1Q+  D?
L                  06       AW            +=)1
R                MINOR BRECCIATION - DISRUPTION.
/    1146  1161  15    8B10      TC          P CU   75    <*
L                  13       3G            +=)1  CL   73
/    1161  1198  37    8A10      MX          P CU   73    <*D.
L                  29       BG            +=)1  F/   73
R                CONTACT BETWEEN DYKES IS FAULTED.
/    1198  1226  27    2C33      <<BR        P          <)+=Q+
L                  23       BT            11=3
R                SLIGHTLY BRECCIATED NEAR LOWER CONTACT. UNIT MAYBE XENOLITH.
/    1226  1252  24    8C11      VUMX        P CU   70     D-
L                  16       YW
R                SMALL XENOLITH OF DUST TUFF AT 125.0 M.
/    1252  1287  34    8A00      MX          P F/   68    <(D.
L                  27       GB
/    1287  1293  06    8C10      MX          P             D-
L                  06       AW
R                CONTACT BETWEEN TWO ABOVE DYKES GRADATIONAL.
/    1293  1304  11    2C55MS    BR          P            #=#+
L                  06       5T            )))+
/    1304  1332  26    2C24MS    <<BR        P          E*<)<+
```

```
L                09        5T              =1+2
R                MINOR BRECCIATION.
/    1332  1344  11    2C13       <<VU         P            E*<+<+
L                03        5T              +=+1
R                VUGS HAVE COARSE GRAINED PYRITE CRYSTALS (EUHEDRAL).
/    1344  1354  10    2D13       <<           P              <)<)
L                03        7A              )))+
/    1354  1389  33    2C14       <<           P            E*<)<)
L                09        5T              =1+2
/    1389  1409  19    2C23       <<BR         P              <)<+
L                03        AT              =1+2                  <-
R                MINOR BRECCIATION.
/    1409  1438  27    2C13       <<           P            E*<*<)
L                03        5T              =1=2
/    1438  1450  11    2D13       <<           P            E(<)<+
L                03        AT              )++1
/    1450  1488  34    2C23       <<           P            E(<*<)
L                03        5T                5
R                CORE VERY BROKEN. HARD TO ESTIMATE FRACTURES.
/    1488  1515  25    2C34MS     <<ER         P V/    10   <(@)<+
L                06        5T              1214
R                MINOR BRECCIATION.
/    1515  1540  23    2C24MS     <<           P            E*<*<)
L                05        4T              1124
R                MINOR EUHEDRAL PYRITE IN <<'S.
/    1540  1573  32    2C13       <<           P V/    48   E*<(<)
L                11        AT              11+2                  <.
R                PATCH OF ASH TUFF AT 156.3 M., AND AT VERY END OF HOLE,
R                157.3 M.
R                END OF HOLE.
A001
ALAB             EQUITY MINESITE LABORATORY
ATYP             ASSAY
AMTH             WET EXTRACTION A.A. -- AU FIRE ASSAYED FIRST
AUMM             RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
A001  152   180        5288        0.005   0.5 0.020 0.005 0.005 2.010 0.005
A001  180   210        5289        0.005   0.5 0.020 0.005 0.005 3.240 0.005
A001  210   240        5290        0.010   0.5 0.080 0.005 0.005 4.300 0.005
A001  240   270        5291        0.020   0.5 0.050 0.005 0.005 3.360 0.005
A001  270   300        5292        0.040   0.5 0.240 0.005 0.005 4.120 0.005
A001  300   330        5293        0.210   0.5 0.070 0.005 0.005 3.950 0.005
A001  330   360        5294        0.020   0.5 0.080 0.005 0.005 2.940 0.005
A001  360   390        5295        0.040   0.5 0.120 0.005 0.005 2.980 0.005
A001  390   440        5296        0.020   0.5 0.050 0.005 0.005 5.010 0.005
A001  440   470        5297        0.010   0.5 0.030 0.005 0.005 2.870 0.005
A001  470   500        5298        0.005   0.5 0.030 0.005 0.005 6.500 0.005
A001  500   530        5299        0.005   0.5 0.030 0.005 0.005 6.540 0.005
A001  530   560        5300        0.005   0.5 0.050 0.005 0.005 4.330 0.005
A001  560   590        5301        0.005   0.5 0.040 0.005 0.005 7.760 0.005
A001  590   620        5302        0.005   0.5 0.040 0.005 0.005 3.660 0.005
A001  620   650        5303        0.005   0.5 0.040 0.005 0.005 4.310 0.005
A001  650   680        5304        0.020   0.5 0.070 0.005 0.005 4.140 0.005
A001  680   720        5305        0.010   0.5 0.050 0.005 0.005 7.050 0.005
A001  720   750        5306        0.005   0.5 0.040 0.005 0.005 4.130 0.005
A001  750   780        5307        0.005   0.5 0.070 0.005 0.005 3.800 0.005
```

A001	780	810	5308	0.020	0.5	0.040	0.005	0.005	3.490	0.005
A001	810	840	5309	0.005	0.5	0.050	0.005	0.005	7.160	0.005
A001	840	870	5310	0.010	0.5	0.040	0.005	0.005	3.470	0.005
A001	870	900	5311	0.005	0.5	0.080	0.005	0.005	3.150	0.005
A001	900	930	5312	0.005	0.5	0.050	0.005	0.005	4.580	0.005
A001	930	950	5313	0.020	0.5	0.060	0.005	0.005	9.150	0.010
A001	950	980	5314	0.005	5.0	0.080	0.005	0.005	6.000	0.005
A001	980	1010	5315	0.005	3.0	0.060	0.005	0.005	7.360	0.005
A001	1010	1040	5316	0.005	2.0	0.060	0.005	0.005	4.120	0.005
A001	1040	1070	5317	0.005	2.0	0.020	0.005	0.005	4.570	0.020
A001	1070	1100	5318	0.005	3.0	0.040	0.005	0.005	4.940	0.005
A001	1100	1125	5319	0.015	11.0	0.050	0.010	0.060	5.670	0.150
A001	1125	1146	5320	0.022	11.0	0.070	0.010	0.005	4.220	0.090
A001	1198	1226	5321	0.005	4.0	0.080	0.005	0.020	5.210	0.005
A001	1293	1320	5322	0.005	3.0	0.080	0.005	0.005	5.360	0.005
A001	1320	1350	5323	0.005	5.0	0.230	0.005	0.005	8.130	0.010
A001	1350	1380	5324	0.005	3.0	0.070	0.005	0.005	6.910	0.005
A001	1380	1410	5325	0.005	9.0	0.060	0.010	0.005	7.030	0.005
A001	1410	1440	5326	0.005	4.0	0.050	0.005	0.005	6.200	0.005
A001	1440	1470	5327	0.005	4.0	0.040	0.005	0.005	6.610	0.010
A001	1470	1500	5328	0.005	2.0	0.040	0.005	0.005	3.200	0.010
A001	1500	1530	5329	0.005	4.0	0.030	0.010	0.010	4.680	0.010
A001	1530	1573	5330	0.005	3.0	0.020	0.005	0.005	4.530	0.010
R			END OF ASSAYS - END OF LOG							

```
IDEN6B0201      X86CH239 NQ 24MAR86DJH   G&D MAR8653B            0.0
IPRJ          EQUITY SILVER MINES LTD        SOUTH OF S.T. - ST GEOCODE
S000   00   457 MT  245.7 090.0 -45.0                6224.65   7591.57   1264.62
S001  457  1350     245.7 090.0 -44.0
S002 1350  2112     245.7 090.0 -46.0
S003 2112  2457     245.7 090.0 -44.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                      MSCLQZPYCPTTASPR
LNAM                                                      CBGY  MGHESLGLMO
/      00    46         OVBN                    P
R                 :TRICONED - NO CORE
/      46    79   30    2C24MSCL   <<           P            E)<*<)
L                 00         GT
R                 :HEAVILY BROKEN UP CORE W/ FE OXIDES ON FRACTURES :TO 2C12 LOC.
/      79   110   30    2C23CLMS   <<           P          E.E*<.<*
L                 02         TG                                  D*
R                 : TO 2C12 AND 2C24 LOC : MINOR FE OXIDES ON FRACTS. : HEAVILY
R                    BROKEN UP CORE
/     110   140   18    2C13CLMS   <<           P            <*<.<*
L                 00         TG
R                 :NO FE OXIDES :TO 2C12 AND 2C15 LOC.
/     140   170   28    2C12CL     <<           P            <*<.<*
L                 18         5G                           <.
R                 : TO 2C25 LOC. W/ 5T COLOR
/     170   200   28    2C23CLMS   <<           P            <*<*<*
L                 11         TG                           <.
R                 : TO 2C25 LOC. W/ 5T COLOR
/     200   230   29    2C24CLMS   <<           P            <*  <*<.
L                 24         TG                           <.
R                 : TO 2C25 LOC. W/ 5T COLOR
/     230   260   30    2C34MSCL   <<           P            <*<)<=
L                 26         GT
R                 : TO 2C35 LOC.
/     260   290   29    2C12CL     <<           P            <*<.<*
L                 09         5G
R                 : TO 2C23 LOC.
/     290   320   28    2C13CLMS   <<           P            <.  <(
L                 02         TG                           <.
R                 : HEAVILY BROKEN CORE W/ MINOR GOUGE : TO 2C12 LOC.
/     320   350   28    2C13CLMS   <<           P            <(<(<*
L                 08         5G                           <.
R                 : TO 2C25 LOC.
/     350   380   28    2C12CL     <<           P            <.<.<(
L                 05         5G                           <.
R                 : TO 2C13 AND 2C25 LOC.
/     380   410   28    2C24CLMS   <<           P            <*<.<*
L                 04         TG                           <.
R                 : TO 2C25 TOWARDS EOI
/     390   390         X                      D F/   060
R                 : 1 CM CLAY GOUGE
/     410   440   29    2C24MSCL   <<           P            <.<*<*
L                 15         GT                           <.
R                 : TO 2C25 AND 2C23 LOC.
/     440   470   28    2C13CLMS   <<           P            <*<(<+
```

```
L                19          TG
R              : LOCAL CL SPOTS (2D?)
/      470   500  30    2C24CLMS   <<          P           <(<.<(
L                23          TG
R              : TO 2C13 LOC. : TO 2C25 TOWARDS EOI
/      500   530  29    2C13CLMS   <<          P           <(<.<(
L                16          6G
R              : LOCAL CL SPOTTING
/      502   502       X          VU          D4V/   030    V4V6
/      530   560  27    2C25MS     <<          P           <.V*V+
L                03          5T
R              : TO 2C13 TOWARDS EOI : NUMEROUS THIN QZ+PY VEINS
/      560   590  29    2C14CLMS   <<          P           <.<.<*
L                13          GT
R              : 20% 2C25
/      590   620  27    2C25MS     <<          P           <.<(<+
L                03          6T
R              : TO 2C13 LOC. : NUMEROUS QZ+PY VEINS :CL IN 2C13 MICRO VEINS
/      620   650  29    2C25MS     <<          P             <(<+<.
L                07          6T
R              : TO 2C33 TOWARDS EOI W/ CL IN << + TR. CP
/      634   634       X                      D3V/   035    V2V8
/      650   680  30    2C33CLMS   <<          P           <*<.<.
L                24          5G
/      676   676       X                      D3V/   040    V7V3
/      680   710  29    2C33CLMS   <<          P           <*<.<*
L                21          TG
R              : TO 2C35 LOC. W/ 5T COLOR
/      710   740  28    2C23CLMS   <<          P           <*<.<)
L                19          TG
R              : TO 2C35 LOC. W/ 5T COLOR
/      740   770  29    2C24MSCL   <<          P           <*<.<(
L                24          GT
/      770   800  29    2C24MSCL   <<          P           <*<.<(
L                23          GT
R              : TO 2C12 TOWARDS EOI
/      800   830  27    2C25MS     <<          P             <(<)
L                18          6T
R              : TO 2C12 AT SOI
/      830   860  29    2C25MS     <<          P           <.<(<)
L                07          6T
R              : TO 2C24 LOC.
/      857   857       X                      D2V/   030    V2V8
/      860   890  28    2C24MSCL   <<          P           <(<(<)
L                19          GT
/      890   920  28    2C34MSCL   <<          P           <(<(<)
L                21          GT
/      920   950  26    2C24MSCL   <<          P           <(<(<)
L                05          GT
R              : HEAVILY BROKEN CORE W/ CLAY (GOUGE?) AND LOST CORE 94.0-94.9
R              : TO 2C15 LOC. W/O CL ON <<
/      923   923       X                      D2V/   035    V6V4
/      950   980  27    2C35MS     <<          P           <.<(
L                05          6T
R              : TO 2C55 97.0-98.0 M W/ MINOR CY
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```
/     980  1010  29    2C25MS     <<          P            <(((
L                 05       6T
R                : TO 2C35 LOC.
/    1010  1040  29    2C24MSCL   <<          P          <((<.<*
L                 11       GT
/    1040  1070  29    2C24MSCL   <<          P          <((<.<*
L                 09       GT
R                : TO 2C25 AND 2C12 LOC.
/    1070  1100  29    2C13CLMS   <<          P          <((<.<*
L                 03       TG
/    1100  1130  28    2C13CLMS   <<          P          <((<*<)
L                 10       TG
R                : TO 2C25 TOWARDS EOI
/    1130  1160  29    2C25MS     <<          P            <*<+
L                 04       5T
R                : NOTE ABSENCE OF CL.
/    1160  1190  25    2C25MS     <<          P            <((+
L                 02       5T
R                : HEAVILY BROKEN AND LOST CORE 117.0-117.7 M : QZ+PY ENVELOPES
/    1190  1220  28    2C25MS     <<          P            <((*
L                 00       5T
R                : FAULT ZONE 121-122 M (NO ATTITUDE) CLAY GOUGE
/    1220  1250  15    2C25MS     <<          P            <((*
L                 00       5T
R                : HEAVILY BROKEN CORE W/ NUMEROUS ZONES CLAY GOUGE
/    1250  1280  25    2C25MS     <<          P            <((*
L                 00       5T
R                : HEAVILY BROKEN CORE W/ NUMEROUS ZONES OF CLAY GOUGE
/    1280  1310  28    2C25MS     <<          P            <((*
L                 05       5T
R                : HEAVILY BROKEN CORE W/ LOCAL CLAY GOUGE
/    1310  1340  29    2C25MS  CL <<          P          +((((*
L                 04       5T
R                : V. MINOR CL AS FLOODING :NO CL IN MICROVEINS
/    1340  1370  29    2C25MS     <<          P            <((*
L                 00       5T
R                : MOD. BROKEN CORE W/O GOUGE
/    1370  1400  28    2C25MS  CL <<          P          +((((*
L                 03       5T
R                :PY ALSO AS SPOTS TO 0.5 MM : LOOKS LIKE 2D LOC. : TR CL LOC.
/    1400  1430  29    2C25MS     <<          P            <((*  <.
L                 04       5T
R                : TR. SHINEY GREY SDE. MINERAL W/ QZ (TT?)
/    1430  1460  19    2C25MS     <<          P            <(((
L                 00       5T
R                : HEAVILY BROKEN CORE
/    1460  1490  13    2C25MS  CL <<          P          +.<(((
L                 00       5T
R                : LOST AND BROKEN CORE W/ CLAY GOUGE 146.0-147.8 M (0.2 M CORE)
R                : MINOR LOCAL CL ALT'N
/    1490  1520  20    2C25MS     <<          P            <(((
L                 00       5T
R                : LOC'LLY PY SPOTTED : HEAVILY BROKEN CORE W/O GOUGE
/    1520  1550  28    2C25MS     <<          P            <(((
L                 04       5T
```

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R                  : HEAVILY BROKEN CORE : LOC. PY SPOTTING
/    1550  1580  29    2C25MS     <<          P              <)<+
L                  00        5T
R                  : TO 2C35 LOC. : HEAVILY BROKEN CORE : MINOR TECTONIC BXIA W/
R                     CLAY GOUGE
/    1580  1610  27    2C25MS     <<          P              <(<(
L                  00        5T
R                  : LIGHT GREY QZ. RICH ENVELOPES
/    1585  1585        X                      D3V/   062    V7V3
/    1610  1640  29    2C25MS     <<          P              <(<)
L                  04        5T
R                  : STILL NO CL ON MICROVEINS
/    1640  1670  25    2C25MS     <<          P              <(<(
L                  02        5T
R                  : TO 2D TOWARDS EOI
/    1670  1700  25    2C25MS     <<          P              <(<)
L                  00        5T
R                  : HEAVILY BROKEN CORE W/O GOUGE
/    1700  1728  26    2C25MS     <<          P              <(<(
L                  00        5T
R                  : HEAVILY BROKEN CORE W/ PATCHES GOUGE
/    1728  1767  34    2C45MS  QZ <<          P              <(<+
L                  25        4T
R                  : NOTE STRANGE COLOR- UNLIKE TYPICAL 2C : TO 2D45 LOC. : TR.
R                     TO? W/ SDES. :LIGHT GREY QZ RICH ENVELOPES
/    1750  1750        X                      D F/   050
/    1767  1786  16    8A02CL     P*          P CU   045
L                  08        5G
R                  : 20% PLAG PHENOS TO 10 MM : LOWER CNT. NOT OBSERVED
/    1786  1798  11    8A06CY                 P
L                  00        7T
R                  : TOTALLY ALTERED TO CLAY : 8A? : CNTS NOT OBSERVED
/    1798  1820  21    2C45MS  QZ <<BR        P          <*  <.<)
L                  16        4T
R                  : TO 2C55 AT SOI : UT COLOR LOCALLY : TR TO? IN SDE PATCHES
R                  :LIGHT GREY QZ RICH ENVELOPES
/    1820  1844  24    2C45MS  QZ <<          P          <.  <.<)
L                  20        4T
R                  : TO 2C35 LOC. : UT COLOR LOC. : TO 2D LOC. : NOTE SAME
R                     STRANGE COLOR AS ABOVE  : LIGHT GREY QZ RICH ENVELOPES
/    1844  1919  73    8C03MS     P*          P CU   060
L                  51        7C
R                  : 10% PLAG PHENOS TO 3 MM : 7G COLOR LOC. : LOWER CNT. NOT
R                      OBSERVED DUE TO BROKEN CORE
/    1919  1950  29    2C25MS  QZ <<          P          <.<+<+
L                  06        4T
R                  : TO 5T COLOR TOWARDS EOI : NOTE TR CL
/    1950  1980  29    2C25MS     <<          P <<   045    <*<+
L                  02        5T
/    1980  2010  28    2C25MS     <<          P <<   060    <*<+
L                  03        5T
/    2010  2040  29    2C15MS     <<          P BD   060    <(<(
L                  02        5T
R                  : 10% INTERLEVED 1D : LIGHT GREY QZ RICH ENVELOPES
/    2040  2064  23    2C25MS     <<          P              <*<+
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```
L                00        5T
R              : MINOR 1D INTERLEVED
/    2064  2079  14    8A02CL     A*          P CU   070    A(
L                14        4G                           A(
R              : LOWER CNT. NOT EXPOSED
/    2079  2110  30    2C25MS     <<          P             <*<+
L                03        5T
R              : LIGHT GREY QZ RICH ENVELOPES
/    2110  2140  30    2C35MS     <<          P             <*<=
L                05        5T
R              : TO 2C25 LOC. : LIGHT GREY QZ RICH ENVELOPES
/    2140  2170  28    2C35MS     <<BR        P             <*<=
L                07        5T
R              : 2C85 LAST 0.2 M OF INT.
/    2166  2166        X                      D F/
R              : CLAY GOUGE - NO ATTITUDE
/    2170  2179  09    8A02CL     A*          P CU   065
L                07        4G                  CL   055A=
R              : GOOD CHILLED INTRUSIVE CNTS.
/    2179  2184  04    2C85MS     BR          P             #=#=
L                02        5T
/    2184  2246  61    8A02CL     A*P*        P CU   039
L                57        4G                  CL   051      D.
R              : TO 8A06 W/ 8G COLOR AT SOI AND EOI
/    2246  2270  22    2C35MS     <<BR        P             <)<=
L                05        5T
R              : 2C85 (TECTONIC BXIA) AT SOI
/    2270  2300  28    2C25MS     <<          P <<   061    <(<)
L                04        5T
R              : TR DARK GREY SDE? MINERAL (TT?)
/    2300  2330  28    2C25MS     <<          P <<   048    <(<)
L                02        5T
R              : 2D? (PHYLLIC ALT'N MAY MAKE IT DIFFICULT TO DETERMINE
R                    ORIGINAL TEXTURE!!)
/    2330  2360  29    2C15MS     <<          P             <(<)
L                00        5T
R              : TR DARK GREY SDE? AS ABOVE 227-230 M : TO 2D LOC.
/    2360  2390  28    2C15MS     <<          P             <(<)
L                00        5T                                    <.
R              : TR DARK GREY SDE? AS ABOVE : 2D?
/    2390  2420  28    2D25MS     <<          P <<   060    <)<+
L                05        5T
R              : TO 2C LOC. : TO 2D15 LOC.
/    2420  2457  32    2D15MS     <<          P <<   047    <(<)
L                00        5T
R              : TO 2C LOC.
R              END OF HOLE.
A001
ALAB           EQUITY MINESITE LABORATORY
ATYP           ASSAY
AMTH           WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM           RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
A001   46   79      5331       0.036   1.0 0.010 0.005 0.005 4.370 0.005
A001   79  110      5332       0.022   1.0 0.060 0.005 0.005 3.430 0.005
A001  110  140      5333       0.023   2.0 0.070 0.005 0.005 3.910 0.005
```

A001	140	170	5334	0.010	0.5	0.080	0.005	0.005	4.170	0.005
A001	170	200	5335	0.010	0.5	0.120	0.005	0.005	4.330	0.005
A001	200	230	5336	0.020	0.5	0.060	0.005	0.005	4.440	0.005
A001	230	260	5337	0.020	0.5	0.060	0.005	0.005	7.630	0.005
A001	260	290	5338	0.030	0.5	0.100	0.005	0.005	4.260	0.005
A001	290	320	5339	0.020	0.5	0.090	0.005	0.005	2.850	0.005
A001	320	350	5340	0.020	0.5	0.050	0.005	0.005	4.250	0.005
A001	350	380	5341	0.010	0.5	0.060	0.005	0.005	3.830	0.005
A001	380	410	5342	0.020	0.5	0.050	0.005	0.005	3.960	0.005
A001	410	440	5343	0.010	0.5	0.080	0.005	0.005	3.950	0.005
A001	440	470	5344	0.020	0.5	0.080	0.005	0.005	4.160	0.005
A001	470	500	5345	0.020	0.5	0.070	0.005	0.005	4.290	0.005
A001	500	530	5346	0.040	2.0	0.040	0.010	0.005	5.500	0.005
A001	530	560	5347	0.020	1.0	0.070	0.005	0.005	4.640	0.005
A001	560	590	5348	0.010	0.5	0.020	0.005	0.005	3.930	0.005
A001	590	620	5349	0.020	2.0	0.040	0.005	0.005	4.430	0.005
A001	620	650	5350	0.020	1.0	0.060	0.005	0.005	4.200	0.005
A001	650	680	5351	0.030	0.5	0.060	0.005	0.005	4.970	0.005
A001	680	710	5352	0.020	1.0	0.060	0.005	0.005	4.880	0.100
A001	710	740	5353	0.060	3.0	0.050	0.005	0.005	5.600	0.020
A001	740	770	5354	0.050	0.5	0.040	0.005	0.005	4.150	0.005
A001	770	800	5355	0.030	0.5	0.060	0.005	0.005	4.000	0.005
A001	800	830	5356	0.010	0.5	0.050	0.005	0.005	3.620	0.005
A001	830	860	5357	0.040	0.5	0.040	0.005	0.005	4.070	0.005
A001	860	890	5358	0.030	7.0	0.210	0.010	0.005	3.980	0.005
A001	890	920	5359	0.020	5.0	0.060	0.010	0.005	4.640	0.005
A001	920	950	5360	0.020	4.0	0.050	0.005	0.005	3.770	0.005
A001	950	980	5361	0.005	0.5	0.040	0.005	0.005	4.780	0.005
A001	980	1010	5362	0.010	1.0	0.080	0.005	0.005	3.340	0.005
A001	1010	1040	5363	0.040	12.0	0.050	0.020	0.005	4.600	0.005
A001	1040	1070	5364	0.020	1.0	0.070	0.005	0.005	3.790	0.005
A001	1070	1100	5365	0.005	1.0	0.070	0.005	0.005	4.880	0.005
A001	1100	1130	5366	0.010	3.0	0.040	0.005	0.005	4.380	0.005
A001	1130	1160	5367	0.005	1.0	0.050	0.005	0.005	5.110	0.005
A001	1160	1190	5368	0.005	1.0	0.040	0.005	0.005	4.080	0.030
A001	1190	1220	5369	0.010	2.0	0.040	0.005	0.005	4.290	0.005
A001	1220	1250	5370	0.020	3.0	0.030	0.010	0.005	5.240	0.005
A001	1250	1280	5371	0.020	2.0	0.060	0.010	0.005	5.550	0.005
A001	1280	1310	5372	0.005	3.0	0.040	0.005	0.005	4.710	0.005
A001	1310	1340	5373	0.020	3.0	0.050	0.010	0.010	4.730	0.005
A001	1340	1370	5374	0.030	1.0	0.050	0.005	0.005	4.640	0.005
A001	1370	1400	5375	0.010	2.0	0.060	0.005	0.020	3.440	0.005
A001	1400	1430	5376	0.010	3.0	0.050	0.010	0.010	5.570	0.005
A001	1430	1460	5377	0.005	2.0	0.040	0.010	0.005	5.600	0.005
A001	1460	1490	5378	0.010	2.0	0.040	0.005	0.005	2.720	0.005
A001	1490	1520	5379	0.020	3.0	0.050	0.005	0.005	3.560	0.005
A001	1520	1550	5380	0.005	4.0	0.070	0.005	0.030	3.720	0.005
A001	1550	1580	5381	0.005	1.0	0.050	0.005	0.005	4.240	0.005
A001	1580	1610	5382	0.005	3.0	0.050	0.005	0.005	3.290	0.005
A001	1610	1640	5383	0.005	2.0	0.050	0.005	0.005	3.590	0.005
A001	1640	1670	5384	0.020	7.0	0.040	0.010	0.005	4.770	0.005
A001	1670	1700	5385	0.005	2.0	0.060	0.005	0.005	3.860	0.005
A001	1700	1730	5386	0.005	0.5	0.040	0.005	0.005	3.250	0.010
A001	1730	1767	5387	0.005	0.5	0.040	0.005	0.005	5.760	0.060
A001	1798	1820	5388	0.005	0.5	0.040	0.005	0.005	7.320	0.005

A001	1820	1844	5389							
A001	1919	1950	5390	0.005	0.5	0.040	0.005	0.005	3.200	0.005
A001	1950	1980	5391	0.005	0.5	0.010	0.005	0.005	2.730	0.005
A001	1980	2010	5392	0.005	0.5	0.020	0.005	0.005	4.390	0.005
A001	2010	2040	5393	0.005	0.5	0.070	0.005	0.005	3.700	0.005
A001	2040	2064	5394	0.005	0.5	0.030	0.005	0.005	2.540	0.005
A001	2079	2110	5395	0.005	0.5	0.020	0.005	0.005	4.890	0.005
A001	2110	2140	5396	0.005	0.5	0.010	0.005	0.005	4.810	0.005
A001	2140	2170	5397	0.030	16.0	0.030	0.005	0.005	8.050	0.120
A001	2170	2184	5398	0.030	11.0	0.040	0.005	0.005	5.170	0.050
A001	2246	2270	5399	0.005	0.5	0.020	0.005	0.005	8.670	0.050
A001	2270	2300	5400	0.005	0.5	0.010	0.005	0.005	5.520	0.060
A001	2300	2330	5401	0.005	0.5	0.040	0.005	0.005	5.370	0.005
A001	2330	2360	5402	0.005	0.5	0.070	0.005	0.005	3.580	0.005
A001	2360	2390	5403	0.005	0.5	0.010	0.005	0.005	3.900	0.030
A001	2390	2420	5404	0.005	0.5	0.020	0.005	0.005	5.300	0.005
A001	2420	2457	5405	0.005	0.5	0.010	0.005	0.005	2.510	0.005
R			END OF ASSAYS - END OF LOG							

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IDEN6B0201      X86CH240 NQ 27MAR86DJH   G&D MAR86S38          0.0
IPRJ          EQUITY SILVER MINES LTD        SOUTH OF S.T. - ST GEOCODE
S000   00   457 MT  148.1 090.0 -45.0              6029.20   7648.38   1258.98
S001  457  1198     148.1 090.0 -44.0
S002 1198  1481     148.1 090.0 -46.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                    MSCLQZPYCPTTASPR
LNAM                                                    CBGY  MGHESLGLMO
/      00   280        OVBN                    P
R                : TRICONED AND CASED - NO CORE
/     280   302  11    2C25MS     <<           P              <*<)
L                  00        5T
R                : HEAVILY BROKEN CORE : NO FE OXIDES : CLAY GOUGE? ZONES
R                : NO CL ON MICROVEINS
/     302   332  21    2C35MS     <<           P              <*<)
L                  00        5T
R                : HEAVILY BROKEN UP CORE W/O CLAY ZONES  : TO 2C55 LOC.
/     332   360  20    2C55MS     <<BR         P              <)<=  <.
L                  02        5T
R                : MOD.-STRONGLY BROKEN UP CORE W/O GOUGE : TO 2C45 LOC.
R                : NOTE TR. GREY SDE. (TT?)
/     360   390  22    2C45MS     <<           P              <*<)  <.
L                  00        5T
R                : MOD. BROKEN UP CORE W/O GOUGE : TR GREY SDE (TT?)
/     390   418  21    2C45MS     <<           P              <*<)
L                  00        5T
R                : MOD. BROKEN UP CORE W/O GOUGE
/     418   445  06    2C25MS     <<           P              <*<)
L                  00        5T
R                : HEAVILY BROKEN AND LOST CORE W/O GOUGE : 1 QZ+PY VEIN > 50 MM
R                  - NO ATTITUDE POSSIBLE
/     445   466  10    2C45MS     <<           P              <*<=
L                  00        5T
R                : MOD. BROKEN UP CORE W/O GOUGE : LOST CORE
/     466   485  11    2C45MS     <<BR         P              <*<=  <.
L                  00        5T
R                : MOD. BROKEN CORE W/O GOUGE : LOST CORE : TO 2C55 LOC. : TR
R                  GREY SDE? (TT?)
/     485   506  05    2C45MS     <<BR         P              <*<=  <.
L                  00        5T
R                : MOD. BROKEN UP CORE W/O GOUGE : LOST CORE : TO 2C55 LOC. :TR
R                  GREY SDE? AS ABOVE
/     506   530  17    2C45MS     <<BR         P              <*<=  <.
L                  02        5T
R                : MOD. BROKEN UP CORE W/O CLAY GOUGE : LOST CORE : TO 2C55 LOC.
R                : TR GREY SDE? (TT?)
/     530   560  25    2C45MS     <<           P              <*<=  <.
L                  04        5T
R                : MOD. BROKEN UP CORE - W/O GOUGE : TO 2C55 LOC. : TR TT?
/     560   590  29    2C45MS     <<           P              <*<=  <.
L                  04        5T
R                : LESS BROKEN UP THAN ABOVE INTS. : TO 2C85 LOC. : TR TT?
/     590   620  29    2C35MS     <<           P              <*<=  <.
L                  02        5T
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```
R                  : TR TT?
/      620   650   24    2C35MS     <<          P              <*<)  <.
L                  04        5T
R                  : TR TT?
/      642   642         X                     D F/
R                  : CLAY GOUGE (FAULT?) - NO ATTITUDE POSSIBLE
/      650   680   18    2C35MS     <<          P              <*<)  <.
L                  02        5T
R                  : HEAVILY BROKEN UP CORE : LOST CORE 66.2-68.0 M : TR TT?
/      680   701   17    2C45MS     <<          P              <*<)  <.
L                  00        5T
R                  : HEAVILY BROKEN CORE W/O GOUGE : LOST CORE : TR. TT?
/      701   735   17    2C45MS     <<          P              <*<)
L                  02        5T
R                  : HEAVILY BROKEN UP CORE W/ MINOR CLAY GOUGE : LOST CORE : TO
R                    2C55 LOC.
/      735   760   24    2C45MS     <<          P              >)<=  <.
L                  14        5T
R                  : TR TT?
/      760   790   28    2C35MS     <<          P              <)<=  <.
L                  09        5T
R                  : HEAVILY BROKEN UP LOCALLY : TR TT?
/      790   823   24    2C45MS     <<BR        P              <)<=  <.
L                  02        5T
R                  : HEAVILY BROKEN UP LOCALLY W/ SOME GOUGE : TO 2C55 LOC.: TR
R                    TT?
/      823   892   61    8A01CL     P*          P
L                  45        4G                                  D.
R                  : CNTS OBSCURRED IN BROKEN CORE : 5% ALTERED, UNALIGNED PLAG
R                    PHENOS TO 10*2 MM : POST-MIN DYKE
/      892   917   20    2C45MS     <<BR        P              <*<)  <.
L                  00        5T
R                  : TR TT? : 8A 91.1-91.4 M W/ MG
/      917   950   32    8A02CL     A*          P CU   052    A)
L                  28        4G                   CL   085A)
R                  : 5% AMYGDS. W/ CB+QZ INFILLING
/      950   972   16    2C45MS     <<          P              <*<)  <.
L                  05        5T
R                  : TR TT? : HEAVILY BROKEN UP CORE EXCEPT FOR DYKE 95.4-95.9 M
/      972   997   12    2C25MS     <<          P              <*<)  <.
L                  00        5T
R                  : V. MINOR 2D INTERLEVED : TR. TT? : HEAVILY BROKEN UP CORE
/      997  1027   25    2C25MS     <<          P              <(<*  <.
L                  00        5T
R                  : MOD.-STRONGLY BROKEN UP CORE : TR TT?
/     1027  1061   26    2C15MS     <<          P              <(<*  <.
L                  00        5T
R                  : TR TT?
/     1061  1090   27    2C25MS     <<          P              <*<)  <.
L                  02        5T
R                  : HEAVILY BROKEN UP CORE : TR. TT?
/     1090  1120   27    2C25MS     <<          P              <*<)  <.
L                  00        5T
R                  : HEAVILY BROKEN UP CORE LOCALLY : TR. TT?
/     1120  1150   27    2C25MS     <<          P              <*<)  <.
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L                 03         5T                                  <.
R                : HEAVILY BROKEN UP CORE TO 114.0 M : TR. TT?
/     1123  1123        X                          D4V/   025     V5V5
/     1150  1180  28    2C13CLMS   <<              P              <.<(<)
L                 07         TG                                <(      <.
R                : TO 2C15 LOC.
/     1180  1210  25    2C15MS     <<              P              <.<(<*
L                 02         5T                                <.
R                : TO 2C13 TOWARDS EOI
/     1210  1231  20    2C13CLMS   <<              P              <.<(<*
L                 00         TG
R                : MOD. BROKEN UP CORE : TO 2C15 LOC.
/     1231  1243  11    8A02CL     A*              P FB   050     A(
L                 10         6G                    CL   080A(
R                : POST-MIN DYKE : UPPER CNT. IRREG.-NO ATTITUDE
/     1243  1254  11    2C23CL     <<              P              <(<(<*
L                 10         5G                                       <.
R                : TO 2C25 @ EOI
/     1254  1274  12    2C25MS     <<              P              <.<(<*
L                 00         5T
/     1274  1302  25    2C25MS     <<              P                <(<)  <.
L                 02         5T                                <(
R                : TR. TT?
/     1302  1332  29    1D20QZ     <<              P                <(<)  <.
L                 13         AW                                <(
R                : TR. TT? : MINOR 2C INTERLEVED AT SOI & EOI
/     1332  1360  27    2D25MSCL   <<              P <<   045    <(<(<+
L                 22         5T
R                : TO 2D23 & 2C LOC.
/     1360  1390  29    2C23CLMS   <<              P              <(<(<+
L                 14         TG
R                : TO 2C25 & 2D LOC.
/     1390  1420  30    2C24CLMS   <:              P              <(<(<)
L                 12         TG                                <.
/     1420  1450  29    2C13CLMS   <:              P              <(<(<)
L                 00         TG
R                : TO 2C12 & 2C15 LOC.
/     1450  1481  28    2C24CLMS   <<              P              <)<)<)
L                 05         TG
R                : MINOR 2D INTERLEVED
R                :END OF HOLE @ 148.1 M
A001
ALAB              EQUITY MINESITE LABORATORY
ATYP              ASSAY
AMTH              WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM              RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
A001  280   302       5406       0.005   0.5 0.200 0.005 0.005 2.660 0.005
A001  302   332       5407       0.005   0.5 0.010 0.010 0.005 2.590 0.005
A001  332   360       5408       0.010   0.5 0.100 0.010 0.005 3.990 0.005
A001  360   390       5409       0.005   2.0 0.030 0.010 0.005 6.140 0.010
A001  390   418       5410       0.005   0.1 0.005 0.005 0.005 5.500 0.010
A001  418   445       5411       0.005   0.1 0.010 0.005 0.005 4.600 0.010
A001  445   466       5412       0.005   0.1 0.010 0.005 0.005 4.420 0.010
A001  466   506       5413       0.001   0.1 0.020 0.005 0.005 5.640 0.010
A001  506   530       5415       0.001   0.1 0.020 0.005 0.005 3.330 0.005
```

A001	530	560	5416	0.005	0.1	0.020	0.005	0.005	3.830	0.060
A001	560	590	5417	0.005	0.1	0.010	0.005	0.005	10.040	0.005
A001	590	620	5418	0.005	0.1	0.020	0.005	0.005	5.580	0.005
A001	620	650	5419	0.001	0.1	0.030	0.005	0.005	2.840	0.005
A001	650	680	5420	0.001	0.1	0.090	0.005	0.005	3.690	0.005
A001	680	701	5421	0.001	0.1	0.040	0.005	0.005	1.770	0.005
A001	701	735	5422	0.005	2.0	0.030	0.010	0.005	5.140	0.005
A001	735	760	5423	0.005	1.0	0.040	0.010	0.005	8.560	0.005
A001	760	790	5424	0.005	0.1	0.030	0.005	0.005	7.980	0.005
A001	790	823	5425	0.005	0.1	0.050	0.005	0.005	2.930	0.005
A001	892	917	5426	0.005	1.0	0.040	0.010	0.005	5.070	0.005
A001	950	972	5427	0.005	0.1	0.020	0.010	0.005	2.280	0.005
A001	972	997	5428	0.005	0.1	0.020	0.010	0.005	4.100	0.005
A001	997	1027	5429	0.005	1.0	0.020	0.005	0.005	4.240	0.005
A001	1027	1061	5430	0.005	1.0	0.010	0.005	0.005	5.420	0.005
A001	1061	1090	5431	0.005	0.1	0.030	0.005	0.005	5.420	0.005
A001	1090	1120	5432	0.005	1.0	0.050	0.010	0.001	5.080	0.005
A001	1120	1150	5433	0.010	0.5	0.060	0.010	0.001	6.430	0.005
A001	1150	1180	5434	0.030	0.5	0.060	0.005	0.005	4.170	0.005
A001	1180	1210	5435	0.005	3.0	0.080	0.005	0.005	4.240	0.005
A001	1210	1231	5436	0.005	1.0	0.060	0.010	0.010	4.090	0.005
A001	1243	1274	5437	0.040	4.0	0.090	0.010	0.005	5.680	0.020
A001	1274	1302	5438	0.005	18.0	0.120	0.005	0.001	3.280	0.010
A001	1302	1332	5439	0.005	3.0	0.100	0.010	0.005	5.890	0.005
A001	1332	1360	5440	0.005	2.0	0.050	0.005	0.005	4.100	0.005
A001	1360	1390	5441	0.005	1.0	0.050	0.005	0.005	4.060	0.005
A001	1390	1420	5442	0.005	2.0	0.070	0.005	0.005	3.540	0.005
A001	1420	1450	5443	0.005	5.0	0.050	0.010	0.005	5.320	0.005
A001	1450	1481	5444	0.010	1.0	0.060	0.005	0.005	5.220	0.005
R			END OF ASSAYS - END OF LOG							

```
IDEN6B0201      X86CH260 NQ   JUL86DJH   G&D JUL86S38          0.0
IPRJ          EQUITY SILVER MINES LTD        SOUTH OF S. TAIL - ST GEOCODE
S000   00   555 MT  116.1 090.0 -45.0              6252.31   7919.61   1312.56
S001  555  1161     116.1 090.0 -43.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                    MSCLQZPYCPTTASPR
LNAM                                                    CBGY  MGHESLGLMO
/      00   152        OVBN                  P
R                :TRICONED - NQ CORE
/     152   212  34    2C25MSQZ   <<         P             <(<+<.
L                00        5T
R                :LIMONITE ON FRACTURES FROM 20.1 - 21.2
/     212   225  12    8A02CLCB   A*         P             A)
L                06        4G                        A(
R                :1-2% AMYGDS :CNTS NOT OBSERVED (GOUGE @ UPPER CNT)
/     225   250  25    2C24MSCL   <<         P           <)  <+
L                00        GT
R                :10% 2D INTERLEVED :LIMONITE ON FRACTS
/     250   280  28    2D24MSCL   <<         P           <.<(<)
L                00        GT
R                :LIMONITE ON FRACTS
/     280   310  29    2D23CLMS   <<         P           <.<(<)<.
L                00        TG
/     310   340  26    2D23CLMS   <<         P           <(<(<)
L                00        TG
R                :10% 2C INTERLEVED
/     340   370  27    2D23CLMS   <<         P           <(  <)<(
L                00        TG
R                :10% 1A INTERLEVED (20% CHERT CLASTS)
/     370   400  30    2C24MSCL   <<         P           <*<(<)<.
L                06        GT
/     400   430  29    2C23CLMS   <<         P BD   045  <(<.<)
L                18        TG
R                :~25% 2D INTERLEVED
/     430   446  15    2C24MSCL   <<         P           <(<.<)<.
L                09        GT                  CL   047
R                :LOWER CNT V SHARP
/     446   462  15    1C10QZ     <<         P             <(<(
L                12        5A                  CL   049
R                :LOWER CNT V SHARP
/     462   490  27    2C24MSCL   <<         P           <)<(<+<(
L                13        GT
/     490   520  29    2C23CLMS   <<         P           <+<(<)<.
L                24        TG
/     520   550  29    2C23CLMS   <<         P           <+<(<=
L                20        TG
R                :TO STRONG << TEXT LOC
/     550   580  27    2C23CLMS   <<         P           <*<(<)<.  <.
L                20        TG
R                :TO STRONG << TEXT LOC
/     580   609  29    2C23CLMS   <<         P           <)<(<(<.
L                11        TG
R                :TO 2C15 LOC
/     609   614  05    8A20CLCB   A*         P CU   060
```

```
L                04          4G                    CL   060
R               :LOWER CNT IRREGULAR
/     614   637  22    2C22CL      <<          P           <)<.<(
L                10          6G
/     637   673  36    8A20CLCB    P*          P
L                311         4G                    CL   070      D)
R               :UPPER CNT IRREG W/ MINOR BXIA :LOWER CNT WEAKLY IRREGULAR
/     673   700  26    2C22CL      <<          P           <)<.<(
L                18          5G
R               :TO 2C25 LOC :10% 1D INTERLEVED
/     700   730  30    2C22CL      <<          P           <)<(<(
L                19          5G
R               :TO 2C25 LOC  :10% 1D INTERLEVED :V IRREGULAR GREEN/TAN COLOR
R               :BANDING
/     730   760  30    2C22CL      <<          P           <)<(<(
L                16          5G
R               :AS ABOVE W/ 2C25 LOC AND TAN/GREEN COLOR BANDING
/     760   790  27    2C22CL      <<          P BD  071   <)<(<(
L                20          5G                                <.
R               :5% 1D INTERBEDDED
/     790   820  29    2C22CL      <<          P           <)<*<(
L                19          5G                              <.
/     820   846  26    2C22CL      <<          P           <)<*<*
L                07          5G                            <.
R               :LOWER CNT FAIRLY SHARP BUT IRREGULAR (NO ATTITUDE
/     846   857  10    1D12CL      <<          P           <.<.
L                03          AG
R               :TUFFACEOUS MATRIX? :V WEAK << TEXT :30% 1C (EOI)
/     857   880  23    2C21CL      <<          P           <)<(<(
L                18          GA                              <(
/     880   910  28    2C23CLMS    <<          P           <)<(<(
L                19          TG
R               :10% 2D INTERLEVED
/     910   940  30    2C10        <<          P           <(<(<(
L                21          4M
R               :PROPYLITIC ALT'N CNV ON << :TO 2C22 @ START OF INT
/     940   970  29    2C10        <<          P           <(<(<(
L                14          4M
R               :TO 2C22 LOC
/     970  1000  29    2C22CL      <<          P           <)<(<*
L                23          AG
R               :LOCAL IRREGULAR GREEN/BUFF COLOR BANDING
/    1000  1030  28    2C22CL      <<          P           <)<(<*
L                19          AG
R               :PY ALSO IN PATCHES
/    1030  1060  30    2C21CL      <<          P           <)<(<(
L                21          GM
/    1060  1084  24    2C21CL      <<          P           <)<.<.
L                07          6M                              <.
/    1084  1096  12    8A02CLCB    A*          P
L                08          AG
R               :CNTS NOT OBSERVED
/    1096  1125  27    2C22CL      <<          P           <)<.<.
L                14          5G
R               :MINOR BXIA @ 112.5 M
```

/	1125	1132	07	8A12CLCB	<<		P CU	045					
L			02	5G			CL	053<)					
/	1132	1161	29	2C22CL	<<		P		<)<(<(				
L			02	5G					<.				
R			:MINOR BXIA @ 113.2 M :ID 115.8 - 116.1										
R			:EOH @ 116.1 M										
R			END OF HOLE.										
A001													
ALAB			EQUITY MINESITE LABORATORY										
ATYP			ASSAY										
AMTH			WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST										
AUMM			RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN		
R	00	152	:OVBN - NO CORE (TRICONED)										
A001	152	186	6782		0.100	3.0	0.20	0.001	0.13	3.10	0.005		
A001	186	212	6783		0.11	5.0	0.23	0.001	0.06	4.37	0.005		
R			:DYKE - NO SAMPLE										
A001	225	250	6784		0.19	8.0	0.18	0.001	0.005	4.80	0.05		
A001	250	280	6785		0.08	3.0	0.18	0.005	0.05	5.65	0.02		
A001	280	310	6786		0.22	7.0	0.18	0.020	0.04	5.42	0.005		
A001	310	340	6787		0.07	2.0	0.09	0.005	0.04	4.96	0.005		
A001	340	370	6788		0.17	4.0	0.04	0.005	0.001	6.04	0.005		
A001	370	400	6789		0.08	4.0	0.14	0.001	0.070	4.58	0.005		
A001	400	430	6790		0.03	2.0	0.03	0.005	0.001	4.85	0.005		
A001	430	460	6791		0.09	3.0	0.08	0.005	0.030	4.80	0.005		
A001	460	490	6792		0.19	3.0	0.08	0.030	0.020	4.73	0.005		
A001	490	520	6793		0.05	2.0	0.04	0.005	0.001	5.35	0.005		
A001	520	550	6794		0.03	2.0	0.02	0.005	0.001	7.15	0.005		
A001	550	580	6795		0.04	4.0	0.10	0.005	0.350	5.30	0.005		
A001	580	610	6796		0.02	2.0	0.05	0.005	0.001	3.10	0.005		
A001	610	637	6797		0.02	6.0	0.01	0.005	0.001	2.77	0.001		
R			:DYKE - NO SAMPLE										
A001	673	700	6798		0.005	0.5	0.050	0.005	0.001	3.95	0.001		
A001	700	730	6799		0.02	0.5	0.04	0.005	0.001	3.94	0.02		
A001	730	760	6800		0.02	0.5	0.03	0.005	0.001	4.67	0.001		
A001	760	790	6801		0.02	0.5	0.02	0.005	0.001	3.47	0.001		
A001	790	820	6802		0.02	0.5	0.02	0.005	0.001	4.10	0.001		
A001	820	850	6803		0.005	0.5	0.01	0.005	0.001	3.20	0.001		
A001	850	880	6804		0.005	0.5	0.02	0.005	0.001	2.98	0.001		
A001	880	910	6805		0.03	0.5	0.01	0.005	0.001	3.19	0.001		
A001	910	940	6806		0.005	0.5	0.01	0.005	0.001	4.02	0.001		
A001	940	970	6807		0.005	0.5	0.01	0.005	0.001	3.75	0.001		
A001	970	1000	6808		0.005	0.5	0.02	0.005	0.03	5.22	0.06		
A001	1000	1030	6809		0.005	0.5	0.01	0.005	0.001	4.92	0.001		
A001	1030	1060	6810		0.005	0.5	0.01	0.005	0.001	3.76	0.001		
A001	1060	1084	6811		0.005	0.5	0.01	0.005	0.001	4.28	0.001		
R	1084	1096	:DYKE - NO SAMPLE										
A001	1096	1125	6812		0.005	0.5	0.01	0.005	0.001	4.04	0.001		
R	1125	1132	:DYKE - NO SAMPLE										
A001	1132	1161	6813		0.001	0.5	0.01	0.005	0.001	3.61	0.001		
R			:EOH @ 116.1 M										
R			END OF ASSAYS - END OF LOG										

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IDEN6B0201      X86CH261 NQ   JUL86RBP   G&D JUL86S38            0.0
IPRJ          EQUITY SILVER MINES LTD        SOUTH OF S. TAIL - ST GEOCODE
S000   00   534 MT  139.3 090.0 -45.0                  6223.63   7813.25   1299.72
S001  534  1393     139.3 090.0 -42.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                    MSCLQZPYCPTTASPR
LNAM                                                    CBGY  MGHESLGLMO
/      00   183        OVBN                    P
R                 CASING TO 18.3 , HOLE IS LIKELY WELL INTO BEDROCK.
/     183   210  20    2C14QZMS   <<           P           <+  <)
L                  00        6T
R                 CORE IS VERY BROKEN.
/     210   240  26    2C24QZMS   <<           P           <+  <+
L                  00        6T
R                 CORE VERY BROKEN. WEATHERING (FE-STAIN) ON FRACTURES TO 22.9.
/     240   270  27    2C54QZMS   <<BR         P           <+<)#+
L                  02        6T
R                 BR'X MOST INTENSE FROM 24.0 TO 25.0. BR'X TYPICAL OF 2C.
/     270   300  20    2C24QZMS   <<           P V/    50  <+<(<+
L                  00        6T
R                 POSSIBLE SS ON FRACTURE.
/     300   330  29    2C13QZMS   <<           P           <)  <+
L                  00        6T
R                 PYRITE OCCURS IN SMALL WISPS AS WELL. CORE STILL VERY BROKEN.
/     330   360  22    2C33QZMS   <<BR         P           <)<)<+
L                  00        7T
/     360   390  11    2C24QZMS   <<           P           <*  <)
L                  00        6T
R                 VERY BROKEN CORE, VERY POOR RECOVERY. NO CLAY GOUGE, I SEE NO
R                 REASON FOR BROKEN AND POOR RECOVERY.
/     390   440  20    2C33QZMS   <<VU         P               <)
L                  00        6T
R                 VERY BROKEN POOR RECOVERY.
/     440   480  30    2C13       <<           P           <)<*<*
L                  00        6T
R                 CORE STILL VERY BROKEN.
/     480   510  28    2C23QZMS   <<BR         P           <)<)<+
L                  05        6T     VU
R                 CORE GETTING MORE SOLID. MINOR BRECCIATION.
/     510   540  29    2C14QZMS   <<           P           <)<*<)
L                  05        6T
R                 MINOR DISPLACEMENT OF SOME <<.
/     540   570  20    2C13QZMS   <<           P           <+<)<)  #-
L                  03        5T
R                 LOST CORE FROM 55.9 TO 56.7. SMALL BR'X AT 55.0 WITH TT/PY/QZ.
/     570   600  28    2C13       <<           P           <)<*<)
L                  00        AT
R                 PATCH OF 2D AT 58.0
/     600   630  29    2C13       <<           P           <+  <*
L                  03        6T
/     630   660  29    2C13       <<           P           <+<)<*
L                  11        GT
/     660   690  29    2C13       <<           P           <+  <*
L                  03        GT                        <(
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```
R                TYPICAL 2C13.
/     690   720  29    2C14       <<          P           <)  <*
L                08       AT
/     720   754  33    2C13       <<WP        P           <)  <(
L                09       GT
/     754   763  09    8C00       P*          P FB    40      D.
L                05       8A
R                FAULT GOUGE ON UPPER CONTACT, LOWER CONTACT NOT PRESERVED.
/     763   788  24    2C54MSQZ   BR<<        P           <)  <)Q-
L                08       AT                                      Q.
R                ZONE WEAKLY BX'D.
/     788   802  13    8A00       MS          P             I=
L                09       2A
/     802   830  27    2C14       <<          P           <)<+<)<.
L                09       AT
R                PATCH OF 1C AT 80.4
/     830   860  29    2C13       <<          P           <)<)<+
L                09       7A
R                PATCH OF 1C AT 85.2.
/     860   895  34    2C23       <<BR        P           <)<+<)
L                06       7A
R                CONTAIINS OCCASIONAL CLASTS OF QZ PEBBLES.
/     895   917  21    1C11       <<          P CU    55  <(  <*
L                07       AW                                  D.
R                LOWER CONTACT GRADATIONAL INTO 2C.
/     917   950  32    2C13       <<          P V/    35  <)<+<)
L                11       AT
R                PATCH OF 1C AT 93.2. OCCASIONAL QZ CLASTS
/     950   980  29    2C13       <<          P V/    45  <)V+V+
L                11       5A
R                PATCH OF 1C AT 95.8 AND 98.0.
/     980  1010  29    2C23       <<BR        P           <+<)<+
L                09       5A
R                CLASTS OF QTZ IN 2C. SLIGHTLY BX'D.
/    1010  1040  28    2C22       <<BR        P           <+  <+B(
L                00       5A
R                PATCH OF 1C AT 102.7.
/    1040  1070  28    2C22       <<          P           <=  <*B(
L                00       6A
R                CORE VERY BROKEN. SOME CP IN << AS WELL.
/    1070  1100  29    2C22CL     <<          P           <1<)<+B.
L                06       GT
/    1100  1123  22    2C22CL     <<          P           <1<*<+B.
L                03       GT
/    1123  1140  17    2E12       <<          P CU    85  <*  D+
L                07       2A
/    1140  1160  20    2C29       <<          P           <(<)<+<)<-
L                06       5A                                  <(
R                CP BLEBS AS WELL, GOOD INTERVAL.
/    1160  1190  29    2C19       <<          P           <*B*V+B(
L                09       5A
R                OCCASIONAL LAPILLI.
/    1190  1209  19    2E12       <<          P             V)V)
L                05       AG
R                SOME LAPILLI SILICIFIED.
```

```
/    1209  1240  30    2C12      <<          P           <+<*<+
L                  17       AG                                <.
R                  ROCK CONTAINS OCCASIONAL LAPILLI.
/    1240  1263  23    2C22      <<          P BN    55  <+  <)<.
L                  05       AG
/    1247  1248        X                     D               B2B+D(B1
L                                                             B)
/    1263  1290  27    8B01FL    TC          P CU    55  E=<-
L                  21       GA                 CL    65      D*
/    1290  1320  30    2C12      <<BR        P           <+  <+<)
L                  05       AG
R                  SOME LAPILLI, DISRUPTION, BX'D. SMALL 8< 131.0 TO 131.1.
/    1320  1350  29    2C22      <<          P BN    55  <+B*<
L                  06       GA
R                  OCCASIONAL LAPILLI.
/    1350  1381  30    2C29      <<          P           <+B(B)<.
L                  11       GA
R                  STILL CONTAINS OCCASIONAL LAPILLI.
/    1381  1388  07    8A00      MS          P CU    75    <-
L                  07       1A                 CL    40      D)
/    1388  1393  05    2C22      <<          P           <+  B)
L                  02       GA
R                  END OF HOLE.
A001
ALAB               EQUITY MINESITE LABORATORY
ATYP               ASSAY
AMTH               WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM               RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
A001  183   210        6841        0.001   0.5 0.005 0.005 0.001 2.60  0.001
A001  210   240        6842        0.001   0.5 0.005 0.005 0.001 5.14  0.001
A001  240   270        6843        0.001   0.5 0.07  0.005 0.001 5.09  0.001
A001  270   300        6844        0.001   0.5 0.005 0.005 0.001 4.76  0.001
A001  300   330        6845        0.005   0.5 0.03  0.005 0.001 2.31  0.001
A001  330   360        6846        0.02    0.5 0.31  0.005 0.04  5.13  0.001
A001  360   390        6847        0.001   0.5 0.03  0.005 0.001 1.64  0.001
A001  390   440        6848        0.001   0.1 0.01  0.001 0.001 0.72  0.001
A001  440   480        6849        0.001   0.5 0.03  0.005 0.001 2.21  0.001
A001  480   510        6850        0.001   0.5 0.02  0.005 0.001 5.19  0.001
A001  510   540        6851        0.001   0.5 0.06  0.005 0.03  3.24  0.001
A001  540   570        6852        0.001   0.5 0.08  0.005 0.03  2.31  0.001
A001  570   600        6853        0.001   0.5 0.04  0.005 0.001 3.11  0.001
A001  600   630        6854        0.005   0.5 0.03  0.005 0.001 3.44  0.001
A001  630   660        6855        0.005   0.5 0.03  0.005 0.001 5.27  0.001
A001  660   690        6856        0.02    0.5 0.05  0.005 0.001 5.00  0.001
A001  690   720        6857        0.005   0.5 0.03  0.005 0.001 4.26  0.001
A001  720   750        6858        0.005   0.5 0.03  0.005 0.001 4.60  0.001
A001  750   788        6859        0.040   0.5 0.05  0.005 0.001 2.95  0.001
A001  802   830        6860        0.050   3.0 0.22  0.020 0.050 5.45  0.020
A001  830   860        6861        0.020   0.5 0.13  0.005 0.040 3.73  0.001
A001  860   890        6862        0.020   0.5 0.05  0.020 0.005 3.09  0.001
A001  890   920        6863        0.030   3.0 0.12  0.020 0.050 2.46  0.001
A001  920   950        6864        0.005   0.5 0.12  0.020 0.050 4.55  0.001
A001  950   980        6865        0.001   0.1 0.03  0.005 0.001 3.60  0.001
A001  980  1010        6866        0.020   0.1 0.03  0.005 0.001 3.03  0.001
A001 1010  1040        6867        0.080   0.1 0.03  0.005 0.001 2.55  0.001
```

A001	1040	1070	6868	0.130	2.0	0.03	0.005	0.001	1.79	0.001
A001	1070	1100	6869	0.070	3.0	0.04	0.005	0.001	3.49	0.001
A001	1100	1130	6870	0.005	3.0	0.06	0.005	0.001	3.70	0.140
A001	1130	1160	6871	0.380	28.0	0.05	0.005	0.001	5.36	0.030
A001	1160	1190	6872	0.080	4.0	0.05	0.005	0.020	5.64	0.030
A001	1190	1220	6873	0.030	4.0	0.05	0.005	0.020	7.41	0.020
A001	1220	1240	6874	0.060	4.0	0.04	0.005	0.010	4.41	0.020
A001	1240	1263	6875	0.240	15.0	0.16	0.005	0.610	6.82	0.170
A001	1290	1320	6876	0.050	3.0	0.03	0.005	0.001	4.36	0.020
A001	1320	1350	6877	0.030	2.0	0.05	0.005	0.030	3.49	0.010
A001	1350	1370	6878	0.080	5.0	0.04	0.005	0.010	4.27	0.020
A001	1370	1393	6879	0.010	1.0	0.03	0.005	0.005	4.17	0.005
R			END OF ASSAYS - END OF LOG							

```
IDEN6B0201      X86CH262 NQ   JUL86DJHRBPG&D JUL86S38          0.0
IPRJ          EQUITY SILVER MINES LTD         SOUTH OF S. TAIL - ST GEOCODE
S000   00   457 MT  312.7 090.0 -45.0                6033.06   7496.15   1213.20
S001  457  1372     312.7 090.0 -44.0
S002 1372  2478     312.7 090.0 -44.0
S003 2478  3127     312.7 090.0 -44.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                        MSCLQZPYCPTTASPR
LNAM                                                        CBGY  MGHESLGLMO
/      00   244         OVBN                    P
R                  :TRICONED - NO CORE
/     244   270  20     3A10QZ      <<VU        P              <(<(
L                  00         AN
R                  :FE OXIDE STAINS ON FRACTS :VUGS MAY BE CAUSED BY DISSOLUTION
R                  OF PY.
/     270   300  30     3A20QZ      <<          P              <)<)
L                  06         AN
R                  :FE OXIDE STAINS ON FRACTS.
/     300   330  18     3A10QZ      <<          P              <(<*
L                  00         AN
R                  :TO 3A20/OC :FE OXIDE STAIN ON SOME FRACTS :NOTE -CHERT CLASTS
R                  ARE LOCALLY INDISTINCT (SILICIFICATION?).
/     330   372  22     3A10QZ      <<          P              <(<(
L                  10         AN                    CL   070
R                  :AS ABOVE 300 TO 330 :MINOR FE OXIDE STAIN ON FRACTS :CORE
R                  HEAVILY BROKEN TO 34.1 M.
R                  :MOST OF CORE LOSS FROM 33-34.1 M. :LOWER CNT SHARP AND REG.
R                  :TO 3B LOCALLY :AGAIN THERE SEEMS TO BE A SILICA OVERPRINT ON
R                  THE CLASTS.
/     372   409  24     3G12CL      <<          P            <(<+<)
L                  07         5G
R                  :TO 3F LOC. :MINOR OXIDE STAINS ON FRACTS. :LOWER CNT NOT
R                  OBSERVED.
/     409   437  21     3A10QZ      <<          P              <(<+
L                  09         AN                        <(
R                  :AS ABOVE 33.0-37.2 M :LOWER CNT GRADATIONAL :TR FE OXIDES ON
R                  FRACTS.
/     437   450  13     3B10QZ      <<          P              <(<(
L                  05         AN                        <(
R                  :W/10% 1C INTERLEVED :LOWER CNT SHARP BUT VERY IRREGULAR.
/     450   480  29     3G12CL      <<          P          <(<(<)<)
L                  04         5G
R                  :TO AG LOCALLY :TO MOD FRACT LOCALLY.
/     480   510  29     3G12CL      <<          P            <)<(<(
L                  06         5G                        <(
R                  :REMARKS AS ABOVE.
/     510   540  30     3G12CL      <<          P            <*<*<*
L                  05         5G
R                  :REMARKS AS ABOVE.
/     540   570  30     3G12CL      <<          P            <*<(<(
L                  11         5G                        <(
R                  :REMARKS AS ABOVE :NOTE-FINE ASH
/     570   600  29     3G12CL      <<          P            <)<(<(
L                                    5G
```

```
R                  :REMARKS AS ABOVE.
/      600   628   28    3G12CL     <<          P           <+<)<)
L                  22       5G                          <(
R                  :REMARKS AS ABOVE :LOWER CNT NOT OBSERVED.
/      628   660   32    3A10QZ     <<          P           <(<+
L                  27       AN
R                  :DISTINCT CLASTS TO 20 MM. (WHITE AND GREY)
/      660   690   30    3A10QZ     <<          P           <(<+
L                  13       AN
R                  :REMARKS AS ABOVE.
/      690   720   30    3A12QZ     <<          P           <.<.
L                  10       AN
R                  :VERY WEAK << TEXT :OTHER REMARKS AS ABOVE.
/      720   750   30    3A10QZ     <<          P           <.<.
L                  06       AN
R                  :REMARKS AS ABOVE
/      750   785   25    3A10QZ     <<          P           <(<*
L                  04       AN
R                  :MOD << TEXT LOC.
/      797   797         X                      D F/   010
R                  :CLAY GOUGE.
/      785   830   30    3G22CL     <<BR        P           <*<)<)
I                  18       AG
R                  :LOCAL ZONES OF BRECCIA BETWEEN 78.5 & 80.2 M. (50%) W/ QZ +
R                  PY MATRIX.
R                  :CL ALSO IN << ENVELOPES :FAULT @ 80.2 M.
/      830   851   20    3G22CL     <<BR        P           <*<)<)
L                  14       AG
R                  :LOCAL BRECCIA ZONES 84.4-85.1 M W/ QZ + PY MATRIX. :CL ALSO
R                  IN << ENVELOPES.
/      851   860   09    8A02CL     A*          P CU   075
L                  08       AG                    CL   060
R                  :LOWER CNT SLIGHTLY IRREGULAR :AMYGDS CONCENTRATED NEAR CNTS.
/      860   890   28    3G22CL     <<          P           <)<)<)
L                  15       5G
R                  :CL ALSO IN << ENVELOPES
/      890   920   30    3G22CL     <<          P           <)<*<*
L                  25       5G                         <*
R                  :TO WEAK << TEXT LOC. :CL << ENVELOPES.
/      920   941   20    3G12CL     <<          P           <)  <*
L                  15       5G                    CL   054
R                  :CL ALSO IN << ENVELOPES.
/      941   980   37    3A10QZ     <<          P BD   058    <(<(<.
L                  33       AN
R                  :CP AT TOP OF INT ONLY :0.1 M. 3G INTERBEDDED @94.6 M.
/      980  1020   34    3A10QZ     <<          P           <(<.
L                  16       AN
R                  :VERY WEAK << TEXT :NOTE-NO CORE 100.9-101.5 (TUBE DIDN'T LOCK)
R                  :LOWER CONTACT NOT OBSERVED
/     1020  1040   19    3F22CL     <<          P         <(<)<.<(
L                  14       5G
/     1040  1070   30    3F23CLMS   <<          P           <)<(<)
L                  22       TG
R                  :POSSIBLY 2C : TO 3F34 LAC : CL ALSO IN << ENVELOPES
/     1070  1100   30    3F23CLMS   <<          P           <)<)<)
```

```
L                16        TG                                  <(
R               :CL ALSO IN << ENVELOPES
/    1100  1130  29    3F35MS     <<          P            <.<)<)<*<.
L                12        5T
R               :TO 3F23 LOC.
/    1130  1160  30    3F25MS     <<          P              <)<)<.
L                03        5T
R               :TO 3F13 LOC.
/    1160  1190  29    3G24CLMS   <<          P            <(<)<)<)
L                18        TG
R               :TO 3F25 LOC. : 3F/3G CONTACT IS ARBITRARY(V.GRADATIONAL)
/    1190  1216  26    3G24CLMS   <<          P            <.<)<)<*
L                15        TG                  CL   025
R               :TO 2F25 LOC.
/    1216  1250  34    3A30QZ     <<          P              <)<=
L                29        AW
/    1250  1280  29    3A20QZ     <<VU        P              <)<+
L                14        AW
/    1280  1310  29    3A20QZ     <<          P              <)<+
L                13        AW                                    <.
/    1310  1340  30    3A20QZ     <<          P              <(<*
L                23        AW                                  <.
/    1340  1370  30    3A20QZ     <<          P              <(<)<.<.
L                24        AW
R               :TR. TT?
/    1370  1400  30    3A20QZ     <<          P              <(<)
L                26        AW
/    1400  1430  30    3A20QZ     <<          P              <(<)
L                25        AW
/    1430  1472  42    3A20QZ     <<          P              <(<)
L                25        AW                  CL   035
R               :VL @ LOWER CNT. THEREFORE NOT NECESSARILY BEDDING
/    1472  1503  31    3B20QZ     <<          P              <+<+
L                18        AW
R               :LOWER CNT. NOT OBSERVED
/    1503  1536  33    3A20QZ     <<          P              <)<+
L                22        AW                  CL   022
R               :<< RUNS RIGHT ALONG LOWER CONTACT
/    1536  1580  44    2C23CLMS   <<          P            <)<)<+<.
L                36        TG
/    1580  1610  30    2C25MS     <<          P            <(<=<=
L                26        5T
R               :TO 2C23 LOC :UPPER CNT GRADATIONAL
/    1610  1658  30    2C24MSCL   <<          P            <)<*<+
L                15        GT                                    <.
R               :10-15% 3B INTERLEVED
/    1658  1686  28    2D13       <<          P            <(<)<+<-
L                21        AG
R               :LOC 2C INTERBEDDED, NO SHARP CONTACT
/    1686  1730  42    2C24MSCL   <<          P            <(<+<+<*
L                      GT
R               :LOC 2C44, GOOD CP MINERALIZATION
/    1730  1760  30    2C24MSCL   <<          P            <(<+<)<(
L                21        GT
/    1760  1790  30    2C34MSCL   <<          P            <-<)<+<*
```

```
L                17        GT
R               :LOC 2D34 INTERBEDDED. SOFT, GREEN, GREASY MINERAL IN <<
/    1790  1820  29    2C34MSCL   <<          P          <-<)<)<*<-
L                21        GT
R               :MINOR TT OCCURING WITH CP IN <<
/    1820  1850  29    2C44MSCL   <<BR        P          <-<)<=<*<-
L                17        GT                                  <-
R               :MINOR BRECCIA
/    1850  1880  30    2C34MSCL   <<BR        P          <-<*<=<-
L                21        GT
/    1880  1910  29    2C44MSCL   <<          P          <-<)<+<(
L                11        GT
/    1910  1940  30    2C34MSCL   <<          P          <(<)<+<(
L                21        GT
/    1940  1970  30    2C23MSCL   <<          P          <+<*<)<.<.
L                19        TG                                  <.
R               :TT AND SL IN << AT 196.6
/    1970  2000  30    2C34MSCL   <<BR        P          <-<(<)<.<(
L                20        AT                                  <-
R               :MINOR BX'D. GOOD TT IN <<
/    2000  2030  30    2C34MSCL   <<          P          <-<)<+<.<-
L                15        GT
R               :ROCK BECOMING SILICIOUS TOWARDS BOTTOM OF INTERVAL
/    2030  2057  26    2C44MSCL   <<BR        P          <(<+<+<(
L                11        GT
R               :MINOR BR'X
/    2057  2062  05    8C00       MXCM        P CL   40
L                02        9T
/    2062  2082  20    8B01       TCCM        P CL   55
L                16        AG                                  D(
/    2082  2110  27    2C43MSCL   <<BR        P F/   35  <(<)<)B.
L                06        GT
R               :CLAY RICH FAULT GOUGE
/    2110  2140  28    2C53MSCL   <<BR        P  '       <(<)<)<.
L                09        GTCY
/    2140  2160  19    2C53MSCL   <<BR        P          <(<*<*<-
L                03        GTCL
/    2160  2185  24    2C44MSCL   <<BR        P          <(<+<=<-<-
L                06        GT
/    2185  2194  09    8C01FL     P*          P CU   50
L                06        GY                  CL   60
/    2194  2230  34    2C44MSCL   <<BR        P          <(<(<)
L                03        GTCY
R               :BR'X ON UPPER CONTACT WITH DYKE
/    2230  2260  29    2C44MSCL   <<          P          <*<(<)
L                06        GT                           <(    <-
/    2260  2290  30    2C24MSCL   <<          P          <)<*<+
L                09        6T                           <-
/    2290  2320  29    2C25MSCL   <<          P          <(<(<)
L                08        6T
R               :BX FILLING FY AT 229.1
/    2320  2350  29    2C25MSCL   <<          P          <(<)<+
L                06        5T                                <-
R               :CLASSIC 2C25 !
/    2350  2380  29    2C24MSCL   <<          P          <(<)<)<.<-
```

L			05	GT						<-
R			:VERY FINE TT IN WITH HE IN <<'S							
/	2380	2410	29	2C24MSCL	<<	P				<(<*<)<-<-
L			02	GT						
/	2410	2440	29	2C34MSCL	<<	P				<(<*<+<(<(
L			11	GT						<(
R			:TT, HE IN <<'S							
/	2440	2470	30	2C55MSCL	<<BR	P				<(<*<+<-<*
L			19	GT						<.
R			:GOOD LOOKING ROCK!!							
/	2470	2500	29	2C34MSCL	<<	P				<(<)<)
L			05	GT						<-
/	2500	2530	30	2C34MSCL	<<	P				<(<)<+<.<.
L			11	GT						<-
/	2530	2563	33	2C34MSCL	<<BR	P				<(<+<+ <.
L			09	GT						<-
R			:MINOR BR'X AT CONTACT WITH DYKE BELOW							
/	2563	2582	19	8A00	CM	P	CU	45		<(
L			11	BG			CL	60		D(
/	2582	2600	18	8C00	CMP*	P				<(
L			06	9T			CL	60		
/	2600	2617	17	8A00	CM	P				<(
L			11	BG						D(
R			:LOWER CONTACT IRREGULAR							
/	2617	2636	19	2C55MSCL	BR<<	P				#+#=
L			15	5T						<-
R			:COULD BE XENOLITH							
/	2636	2663	26	8A00	MSCM	P	CU	60		<)<-
L			17				CL	50		D(
/	2663	2669	06	2C55MSCL	BR<<	P				#=#=
L			03	5T						#.
/	2669	2675	06	8A00	MS	P	CU	70		
L			04	2B			CL	50		D(
/	2675	2700	23	2C35MSCL	<<BR	P	F/			<*<*<+
L			11	5T						
R			:MINOR BR'X UNDER DYKE. FAULT GOUGE 268.3 TO 268.5							
/	2700	2723	23	2C24MSCL	<<	P				<*<*<)
L			06	GT						
/	2723	2760	36	2C12CL	<<	P				<)<-<)
L			06	4G						
R			:BANG! GREEN ROCK, FASTEST TRANSITION I'VE SEEN!							
/	2760	2790	28	2C24MSCL	<<	P				<*<)<)
L			00	GT						
R			:CORE VERY BROKEN							
/	2790	2820	28	2C24MSCL	<<	P				<(<+<+
L			00	GT						
/	2820	2850	30	2C12CL	<<	P				<)<-<*
L			11	TG						
/	2850	2880	30	2C12CL	<<	P				<)<+<+<.
L			17	TG						
/	2880	2910	30	2C12CL	<<	P				<+<-<)
L			13	5G						
/	2910	2940	30	2C12CL	<<	P				<+<-<*
L			11	5G						
/	2940	2968	27	2C23CLMS	<<	P				<*<(<+

```
L                   06        GT
/    2968   2997    29    8B01        <<P*          P CL    25    <-
L                   19        BG      CM                          D(
/    2997   3031    33    2C23CLMS    <<            P           <+<*<+<.
L                   08        GT                                  <-
/    3031   3044    13    1C12CL      <<            P           <-<(<(
L                   03        5G
/    3044   3127    81    2C12CL      <<            P           <+<(<*<.
L                   36        TG
R                   :CONTAINS TO SMALL (0.1 M) INTERVALS OF 1C. TUFF ALSO CONTAINS
R                   :OCCASIONAL CHERT PEBBLES.
R                   :END OF HOLE AT 312.7 M
A001
ALAB                EQUITY MINESITE LABORATORY
ATYP                ASSAY
AMTH                WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM                RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R                   :TRICONED - NO CORE
A001   244    270        6814        0.04    0.5 0.07  0.005 0.005 1.10  0.001
A001   270    300        6815        0.04    0.5 0.05  0.010 0.001 1.88  0.005
A001   300    330        6816        0.09    1.0 0.05  0.020 0.010 1.86  0.010
A001   330    360        6817        0.10    0.5 0.05  0.005 0.010 1.14  0.005
A001   360    390        6818        0.14    0.5 0.09  0.005 0.010 2.30  0.005
A001   390    420        6819        0.09    0.5 0.07  0.005 0.005 2.86  0.005
A001   420    450        6820        0.15    0.5 0.08  0.005 0.001 1.86  0.005
A001   450    480        6821        0.11    0.5 0.08  0.001 0.005 3.46  0.005
A001   480    510        6822        0.13    1.0 0.07  0.001 0.001 4.26  0.005
A001   510    540        6823        0.04    0.5 0.05  0.005 0.001 4.54  0.005
A001   540    570        6824        0.03    0.5 0.03  0.005 0.001 3.87  0.005
A001   570    600        6825        0.03    1.0 0.04  0.005 0.001 4.37  0.005
A001   600    630        6826        0.07    1.0 0.03  0.001 0.010 4.55  0.005
A001   630    660        6827        0.06    1.0 0.05  0.005 0.001 1.46  0.001
A001   660    690        6828        0.06    0.5 0.04  0.010 0.001 1.10  0.005
A001   690    720        6829        0.02    0.5 0.04  0.010 0.010 0.90  0.005
A001   720    750        6830        0.05    0.5 0.05  0.005 0.001 1.14  0.010
A001   750    780        6831        0.08    1.0 0.07  0.010 0.001 2.07  0.010
A001   780    810        6832        0.11    4.0 0.08  0.040 0.005 3.18  0.020
A001   810    830        6833        0.02    0.5 0.04  0.005 0.001 2.69  0.005
A001   830    851        6834        0.06    2.0 0.07  0.010 0.020 3.45  0.005
R      851    860 :DYKE-NO SAMPLE
A001   860    890        6835        0.03    1.0 0.05  0.005 0.001 4.29  0.005
A001   890    920        6836        0.05    1.0 0.09  0.001 0.001 4.08  0.005
A001   920    950        6837        0.10    0.5 0.07  0.005 0.001 3.01  0.005
A001   950    980        6838        0.05    1.0 0.03  0.005 0.001 0.89  0.005
A001   980   1009        6839        0.08    1.0 0.04  0.005 0.001 1.33  0.010
R     1009   1015 :NO CORE-TUBE DIDN'T LOCK
A001  1015   1040        6840        0.05    0.5 0.05  0.005 0.001 2.17  0.005
A001  1040   1070        6880        0.07    1.0 0.06  0.010 0.005 3.82  0.010
A001  1070   1100        6881        0.04    0.5 0.03  0.005 0.005 3.37  0.010
A001  1100   1130        6882        0.19    9.0 0.05  0.050 0.010 4.89  0.020
A001  1130   1160        6883        0.14    3.0 0.05  0.010 0.001 4.54  0.040
A001  1160   1190        6884        0.31    5.0 0.05  0.005 0.010 4.85  0.005
A001  1190   1220        6885        0.15    5.0 0.04  0.010 0.001 4.56  0.050
A001  1220   1250        6886        0.03    2.0 0.05  0.010 0.010 4.73  0.010
A001  1250   1280        6887        0.03    2.0 0.04  0.010 0.020 2.01  0.005
```

A001	1280	1310	6888	0.05	2.0	0.03	0.100	0.020	2.66	0.030
A001	1310	1340	6889	0.04	2.0	0.04	0.010	0.010	2.44	0.020
A001	1340	1370	6890	0.05	2.0	0.04	0.010	0.005	2.58	0.005
A001	1370	1400	6891	0.02	2.0	0.03	0.010	0.010	4.22	0.005
A001	1400	1430	6892	0.02	1.0	0.03	0.010	0.005	2.71	0.005
A001	1430	1460	6893	0.03	1.0	0.02	0.005	0.005	2.18	0.010
A001	1460	1490	6894	0.05	3.0	0.04	0.020	0.020	4.71	0.020
A001	1490	1520	6895	0.01	1.0	0.03	0.005	0.010	4.83	0.005
A001	1520	1550	6896	0.04	1.0	0.12	0.005	0.010	3.93	0.005
A001	1550	1580	6897	0.04	2.0	0.09	0.005	0.020	5.33	0.030
A001	1580	1610	6898	0.03	1.0	0.02	0.005	0.010	5.74	0.005
A001	1610	1640	6899	0.05	3.0	0.06	0.005	0.010	5.02	0.040
A001	1640	1670	6900	0.09	2.0	0.04	0.010	0.001	4.54	0.005
A001	1670	1700	6901	0.30	4.0	0.04	0.010	0.020	4.34	0.005
A001	1700	1730	6902	1.48	26.0	0.08	0.010	0.010	6.49	0.010
A001	1730	1760	6903	0.86	11.0	0.04	0.005	0.005	5.04	0.005
A001	1760	1790	6904	0.32	9.0	0.03	0.005	0.010	4.96	0.001
A001	1790	1820	6905	0.97	26.0	0.08	0.010	0.020	5.57	0.005
A001	1820	1850	6906	0.41	22.0	0.13	0.010	0.030	7.76	0.010
A001	1850	1880	6907	0.16	11.0	0.11	0.010	0.020	10.35	0.020
A001	1880	1910	6908	0.23	5.0	0.04	0.010	0.005	6.42	0.001
A001	1910	1940	6909	0.44	8.0	0.04	0.005	0.005	6.85	0.005
A001	1940	1970	6910	0.11	3.0	0.05	0.005	0.001	4.70	0.140
A001	1970	2000	6911	0.16	16.0	0.10	0.005	0.020	5.48	0.260
A001	2000	2030	6912	0.52	25.0	0.06	0.030	0.080	5.17	0.460
A001	2030	2057	6913	0.18	18.0	0.09	0.001	0.100	5.93	0.020
R	2057	2082	:DYKE-NO SAMPLE							
A001	2082	2110	6914	0.27	22.0	0.07	0.001	0.001	4.62	0.005
A001	2110	2140	6915	0.23	9.0	0.04	0.020	0.001	4.11	0.005
A001	2140	2160	6916	0.14	8.0	0.05	0.020	0.005	3.48	0.005
A001	2160	2185	6917	0.19	12.0	0.07	0.040	0.020	6.35	0.005
R	2185	2194	:DYKE-NO SAMPLE							
A001	2194	2230	6918	0.03	3.0	0.04	0.001	0.001	3.95	0.001
A001	2230	2260	6919	0.03	10.0	0.04	0.005	0.001	4.39	0.001
A001	2260	2290	6920	0.03	22.0	0.06	0.020	0.001	8.57	0.001
A001	2290	2320	6921	0.02	2.0	0.05	0.005	0.001	8.50	0.001
A001	2320	2350	6922	0.07	16.0	0.08	0.020	0.001	4.88	0.005
A001	2350	2380	6923	0.08	34.0	0.07	0.020	0.001	3.95	0.005
A001	2380	2410	6924	0.14	83.0	0.08	0.005	0.020	3.85	0.020
A001	2410	2440	6925	0.83	234.0	0.13	0.130	0.100	4.08	0.070
A001	2440	2470	6926	0.91	1030.0	0.19	0.480	0.070	5.25	0.170
A001	2470	2500	6927	0.22	173.0	0.10	0.080	0.020	4.75	0.040
A001	2500	2530	6928	0.51	511.0	0.14	0.240	0.050	5.79	0.080
A001	2530	2563	6929	0.03	24.0	0.07	0.005	0.005	4.66	0.001
R	2563	2617	:DYKE-NO SAMPLE							
A001	2617	2636	6930	0.07	47.0	0.12	0.020	0.001	4.86	0.005
R	2636	2663	:DYKE-NO SAMPLE							
A001	2663	2669	6931	0.03	23.0	0.12	0.005	0.001	8.50	0.001
R	2669	2675	:DYKE-NO SAMPLE							
A001	2675	2700	6932	0.03	31.0	0.05	0.005	0.001	9.40	0.005
A001	2700	2730	6933	0.005	0.1	0.06	0.001	0.001	5.07	0.001
A001	2730	2760	6934	0.005	0.5	0.05	0.001	0.001	4.39	0.001
A001	2760	2790	6935	0.005	0.1	0.04	0.001	0.001	3.66	0.001
A001	2790	2820	6936	0.005	0.1	0.03	0.001	0.001	5.47	0.001
A001	2820	2850	6937	0.02	0.1	0.07	0.001	0.001	4.67	0.001

A001	2850	2880	6938	0.07	0.1	0.06	0.001	0.001	5.39	0.001
A001	2880	2910	6939	0.02	0.1	0.08	0.001	0.001	4.03	0.001
A001	2910	2940	6940	0.02	0.1	0.04	0.001	0.001	4.12	0.001
A001	2940	2968	6941	0.03	2.0	0.03	0.001	0.001	3.25	0.001
R	2968	2997	:DYKE-NO SAMPLE							
A001	2997	3030	6942	0.10	0.5	0.04	0.001	0.001	2.65	0.001
A001	3030	3060	6943	0.03	0.5	0.05	0.001	0.001	3.17	0.001
A001	3060	3090	6944	0.02	0.5	0.07	0.001	0.001	3.59	0.001
A001	3090	3127	6945	0.03	0.5	0.03	0.001	0.001	4.22	0.001
R			END OF ASSAYS - END OF LOG							

```
IDEN6B0201      X86CH263 NQ   JUL86RBP   G&D JUL86S38          0.0
IPRJ          EQUITY SILVER MINES LTD        SOUTH OF S. TAIL - ST GEOCODE
S000   00   552 MT  195.7 062.0 -45.0                5793.69   7548.10   1194.91
S001  552  1515     195.7 062.0 -44.0
S002 1515  1957     195.7 062.0 -44.5
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                        MSCLQZPYCPTTASPR
LNAM                                                        CBGY  MGHESLGLMO
/      00    37        OVBN                    P
R                  :TRICONED - NO CORE
/      37    61  20    2C12CL     <<           P           <((<-<)
L                  00       6G
/      61    85  15    2C12CL     <<           P           <(  <-
L                  00       6G
R                  :CORE BROKEN, FE STAIN
/      85   140  00    NREC                    P
L                  00
R                  :TRICONED AGAIN DOWN TO 14.0 -  NO CORE
/     140   170  22    2C12CL     <<           P           <*<(<)
L                  00       TG                           <-
/     170   198  23    2C22CL     <<           P           <*<-<)
L                  03       5G
R                  :FRACTURES STILL RUSTY
/     198   238  32    8C00       P*           P BN    40
L                  09       9G                               D.
/     238   270  27    2C12CL     <<           P           <*  <)
L                  00       6G
/     270   300  28    2C12CL     <<           P           <*<)<*
L                  05       6G
/     300   330  28    2C12CL     <<           P           <*  <*
L                  09       AG
R                  :FRACTURES STILL RUSTY
/     330   360  29    2C12CL     <<           P           <*<-<)
L                  00       AG
/     360   390  29    2C12CL     <<           P           <*<(<)
L                  00       AG
/     390   420  28    2C12CL     <<           P           <*<-<)
L                  00       AG
R                  :SOME BLEACHING ON <<'S
/     420   450  26    2C12CL     <<           P           <(  <*
L                  00       AG
R                  :RUSTY FRACTURES END IN THIS INTERVAL. CORE VERY BROKEN.
/     450   546  30    2C12CL     <<           P           <*  <*<.
L                  00       AG
R                  :CP IN << AT 53.7 CORE IS RUMBLE, NO FAULT GOUGE THOUGH.
/     546   551  04    8B01FL     P*CM         P
L                  00       6A     <<VU
/     551   570  18    2C24MS     <<           P           <*<-<)
L                  00       GT
R                  :UPPER CONTACT WITH DYKE IRREGULAR
/     570   600  29    2C23MS     <<           P           <*<(<)
L                  05       GT
/     589   590       X                       D V/    50     V5V2  V=V=
L                                                                  V1
```

```
/     600   637   35    2C13MS     <<          P          <*<(<)
L                 03       AG
/     637   652   15    8B01       P*TC        P CU   45    <-
L                 09       4A                   CL   50      D-
/     652   680   27    2C23MS     <<          P          <)<-<)
L                 00       GT
R                 :CORE VERY BROKEN
/     680   710   29    2C34MS     <<          P          <)<)<+<(
L                 02       GT
/     710   740   29    2C34MS     <<BR        P          <)<=<+
L                 00       GT
/     740   770   25    2C23MS     <<          P          <)<)<=<-
L                 00       GT
R                 :MASSIVE CG. PYRITE SEAM AT 75.3, BUT POOR RECOVERY
/     770   800   26    2C23MS     <<          P          <)<)<)
L                 00       GT
/     800   830   29    2C22       <<          P          <)<+<+<.
L                 00       GA
/     830   860   29    2C24MS     <<          P          <*<+<+<-
L                 03       AT                                 <-
/     860   890   28    2C34MS     <<          P          <(<+<=<(<?
L                 03       6T                                 <-<-
/     890   944   43    2C35M6     <<BR        P          <(<+<+<-
L                 03       6T
R                 :POOR RECOVERY
/     944   961   17    8B00       TCCM        P CU   30    <(
L                 08       2A                   CL   25      D-
/     961   986   24    2C65       <<          P          <-#1#2#(
L                 09                                         #-
R                 :MINOR 8B AT 96.7
/     986   1038        8B00       CMTC        P CU   20    <(
L                       3A                      CL   35      D-
/     1038  1052  14    2C44MS     <<          P          <*<)<+<(
L                 00
/     1052  1100  47    8B01FL     CM          P            <)D.
L                 21       5A                               D-
R                 :CONTACTS NOT PRESERVED
/     1100  1130  29    2C44MS     <<          P          <*<+<=<-  <-
L                 09       GT                                 <-
R                 :LOTS OF DISSEM PY AS WELL
/     1130  1160  27    2C44MS     <<BR        P          <(<)<+<(
L                 00       AT                                 <-
/     1160  1190  29    2C33MS     <<          P          <(<+<+<-
L                 00       AT                                 <(
/     1190  1199  09    8A00       MS<<        P CL   65    <(
L                 06       GA       CM                      D-
/     1199  1209  09    2C95MSQZ   BR<<        P            #=
L                 03       6T
/     1209  1262  52    8A00       MS          P            <(
L                 26       GA                               D-0-
R                 :CONTACTS NOT PRESERVED
/     1262  1304  40    2C34MS     <<BR        P          <-<+<+<.<?
L                 08       AT
/     1304  1316  12    8A00       CM<<        P CU   65    <-
L                 08       GB                   CL   35      D-
```

```
/    1316  1350  33    2C24MS     <<BR        P            <)<)<+
L                  09       AT
/    1350  1380  29    2C34MS     <<BR        P            <)<+<+
L                  06       AT
/    1380  1410  30    2C34MS     <<BR        P            <(<+<+
L                  15       AT
/    1410  1440  30    2C34MS     <<            V/    65   <*<=<+
L                  17       AT
/    1440  1470  30    2C34MS     <<          P V/    70   <)<=<+
L                  05       AT
R                 :BIG VEINS IN LAST TWO INTERVALS ARE QZ-PY, 5 CM WIDE
/    1470  1500  30    2C24MS     <<          P            <(<)<+
L                  07       AT
/    1500  1530  29    2C24MS     <<          P V/    65   <-<)<+<.
L                  05       AT
R                 :VEIN IS PY-QZ, 5 CM WIDE
/    1530  1560  29    2C34MS     <<          P            <(<+<+
L                  05       6T
/    1560  1590  30    2C34MS     <<          P            <-<+<+  <.
L                  09       AT
/    1590  1620  30    2C34MS     <<BR        P            <-<+<+<.<*
L                  11       6T                                    <(
R                 :GOOD TT, IN << AND ANGULAR BX AT 161.3
/    1620  1650  30    2C55MSQZ   <<BR        P            <.<=<+  <(
L                  16       AT                                    <(
R                 :BX WEAK., TT IN <<
/    1650  1680  30    2C34MS     <<BR        P            <(<+<+  <(
L                  09       AT                                    <-
/    1680  1710  30    2C33MSCL   <<          P            <*<(<*
L                  15       GT
/    1710  1740  28    2C34MS     <<BR        P            <(<(<)  <(
L                  03       AT
R                 :MINOR BX'D
/    1740  1770  28    2C34MS     <<          P            <*<+<+  <-
L                  00       AT                                    <(
/    1770  1800  29    2C33MS     <<          P            <*<+<+  <.
L                  05       AT                                    <.
R                 :<< WITH TT-SL AT 178.6, ONLY OCCURRANCE
/    1800  1830  30    2C23MSCL   <<          P            <)<)<)
L                  09       GT
R                 :ROCK TURNING GREEN!
/    1830  1862  31    2C33MS     <<          P            <*<+<+<.<(
L                  00       GT                                  <-<-
R                 :ESSENTIALLY ALL TT, SL, CP OCCUR FROM 185.8 TO 186.1
/    1862  1890  28    2C34MS     <<          P            <(<=<+
L                  09       AT                                  <-
/    1890  1923  32    2C33MSCL   <<          P            <*<+<+<.
L                  09       GT                                  <(
/    1923  1957  33    2C23MSCL   <<          P            <*<)<)
L                  12       AT
R                 :END OF HOLE
A001
ALAB              EQUITY MINESITE LABORATORY
ATYP              ASSAY
AMTH              WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
```

AUMM			RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	37	:TRICONED - NO CORE								
A001	37	61	6946		0.03	2.0	0.01	0.005	0.010	4.17	0.010
A001	61	85	6947		0.02	0.5	0.02	0.005	0.001	2.76	0.005
R	85	140	:TRICONED - NO CORE								
A001	140	170	6948		0.03	1.0	0.02	0.001	0.001	3.75	0.005
A001	170	198	6949		0.02	0.5	0.06	0.001	0.020	3.50	0.005
R	198	238	:DYKE - NO SAMPLE								
A001	238	270	6950		0.04	1.0	0.02	0.005	0.001	3.22	0.005
A001	270	300	6951		0.05	0.5	0.03	0.005	0.005	3.88	0.005
A001	300	330	6952		0.03	0.5	0.04	0.005	0.010	2.91	0.005
A001	330	360	6953		0.03	0.5	0.01	0.001	0.030	3.14	0.005
A001	360	390	6954		0.04	0.5	0.02	0.001	0.010	2.54	0.005
A001	390	420	6955		0.06	1.0	0.02	0.005	0.005	3.80	0.005
A001	420	450	6956		0.09	2.0	0.01	0.005	0.001	3.38	0.010
A001	450	540	6957		0.06	1.0	0.02	0.005	0.005	3.05	0.030
A001	540	570	6958		0.06	1.0	0.04	0.001	0.010	3.58	0.030
A001	570	600	6959		0.11	2.0	0.11	0.001	0.140	3.85	0.170
A001	600	639	6960		0.03	0.5	0.02	0.010	0.010	3.99	0.010
R	639	652	:DYKE - NO SAMPLE								
A001	652	680	6961		0.05	3.0	0.03	0.005	0.030	3.08	0.210
A001	680	710	6962		0.39	6.0	0.04	0.005	0.001	3.55	0.005
A001	710	740	6963		0.03	1.0	0.03	0.005	0.020	3.50	0.005
A001	740	770	6964		0.14	2.0	0.02	0.005	0.001	6.20	0.005
A001	770	800	6965		0.11	4.0	0.02	0.005	0.001	3.44	0.005
A001	800	830	6966		0.06	1.0	0.03	0.005	0.005	3.69	0.005
A001	830	860	6967		0.08	2.0	0.03	0.005	0.010	2.47	0.020
A001	860	890	6968		0.29	12.0	0.03	0.010	0.030	3.62	0.300
A001	890	944	6969		0.19	10.0	0.02	0.005	0.005	2.34	0.010
R	944	961	:DYKE - NO SAMPLE								
A001	961	986	6970		0.16	10.0	0.12	0.005	0.030	7.09	0.010
R	986	1038	:DYKE - NO SAMPLE								
A001	1038	1052	6971		0.47	14.0	0.03	0.005	0.010	2.84	0.010
R	1052	1100	:DYKE - NO SAMPLE								
A001	1100	1130	6972		0.38	11.0	0.04	0.001	0.010	5.47	0.005
A001	1130	1160	6973		0.51	20.0	0.04	0.070	0.010	5.24	0.030
A001	1160	1190	6974		0.14	8.0	0.04	0.060	0.001	5.36	0.030
R	1190	1199	:DYKE - NO SAMPLE								
A001	1199	1209	6975		0.02	1.0	0.03	0.005	0.001	2.46	0.005
R	1209	1262	:DYKE - NO SAMPLE								
A001	1262	1283	6976		0.03	2.0	0.05	0.005	0.010	3.78	0.005
A001	1283	1304	6977		0.05	4.0	0.07	0.005	0.001	4.18	0.005
R	1304	1316	:DYKE - NO SAMPLE								
A001	1316	1350	6978		0.07	4.0	0.04	0.005	0.010	3.69	0.005
A001	1350	1380	6979		0.08	3.0	0.07	0.005	0.001	3.96	0.005
A001	1380	1410	6980		0.04	3.0	0.06	0.010	0.010	5.94	0.005
A001	1410	1440	6981		0.02	1.0	0.08	0.010	0.001	6.87	0.005
A001	1440	1470	6982		0.02	1.0	0.03	0.005	0.001	4.85	0.005
A001	1470	1500	6983		0.01	1.0	0.03	0.005	0.001	4.04	0.005
A001	1500	1530	6984		0.01	3.0	0.04	0.005	0.020	4.72	0.005
A001	1530	1560	6985		0.04	2.0	0.04	0.020	0.010	4.32	0.010
A001	1560	1590	6986		0.03	3.0	0.03	0.010	0.001	4.28	0.090
A001	1590	1620	6987		0.19	38.0	0.11	0.080	0.010	3.44	5.140
A001	1620	1650	6988		0.08	10.0	0.07	0.040	0.020	4.41	0.940
A001	1650	1680	6989		0.02	10.0	0.03	0.010	0.030	3.87	0.360

A001	1680	1710	6990	0.04	5.0	0.08	0.010	0.001	3.61	0.380
A001	1710	1740	6991	0.04	13.0	0.04	0.020	0.020	4.00	0.430
A001	1740	1770	6992	0.01	2.0	0.03	0.010	0.010	4.42	0.160
A001	1770	1800	6993	0.005	2.0	0.02	0.010	0.020	4.42	0.010
A001	1800	1830	6994	0.02	3.0	0.04	0.010	0.005	5.13	0.005
A001	1830	1862	6995	0.25	99.0	0.06	0.110	0.005	5.24	0.810
A001	1862	1890	6996	0.02	5.0	0.02	0.020	0.005	6.48	0.010
A001	1890	1923	6997	0.09	0.5	0.06	0.040	0.005	4.99	0.010
A001	1923	1957	6998	0.01	0.5	0.02	0.005	0.005	4.20	0.005
R			:END OF ASSAYS - END OF HOLE							
R			END OF ASSAYS - END OF LOG							

```
IDEN6B0201      X86CH264 NQ   JUL86RBP   G&D JUL86S38          0.0
IPRJ          EQUITY SILVER MINES LTD        SUPERSTITION ZONE - ST GEOCODE
S000   00   488 MT  251.5 090.0 -45.0              5611.87   7435.93   1107.05
/SCL        MT.2MT.1
LSCL            MT.2
/NAM                                                    MSCLQZPYCPTTASPR
LNAM                                                    CBGY  MGHESLGLMO
/      00   104        OVBN                  P
R                 :TRICONED - NO CORE
/      104  130  26    3F11CL     <<         P          <)<+<*
L                 05        GA
R                 :VERY LITTLE RUST ON <<
/      130  160  30    3F11CL     <<         P          <+<)<*
L                 19        AG
/      160  190  30    3F13CLMS   <<         P          <)<)<*
L                 15        GA
R                 :MINOR MS-QZ ALT'N ENVELOPE ON <<
/      190  220  30    3F12CL     <<         P          <+<(<(
L                 17        GA
/      220  247  27    3F13CLMS   <<         P          <)<+<(
L                 09        TG
/      247  280  33    3A11QZ     <<         P          <(<+<*
L                 12        AW
R                 :TYPICAL, VERY SILICOUS, CHERT PEBBLE CONGLOMERATE
/      280  310  30    3A21QZ     <<         P          <(<+<*
L                 14        AW
/      310  340  30    3A21QZ     <<         P V/   25  <(<=<+    <.
L                 10        AW
R                 :NOT SURE ABOUT ARSENO, VERY SMALL OCCURRANCE WITH QZ-PY
/      340  370  30    3A21QZ     <<         P          <(<+<)
L                 09        AW
/      370  397  27    8C02CY     P*CM       P CU   45      <-
L                 09        WT                 CL   45
/      397  430  33    3A11QZ     <<         P          <(<)<*
L                 15        AW
/      430  460  29    3A21QZ     <<         P          <(<+<)
L                 09        AW
/      460  499  38    3A21QZ     <<         P          <(<+<)
L                 08        AW
/      499  505  06    3E11       <<         P BD   50  <(<(<*
L                 04        TG                 CL   50
R                 :TOP CONTACT GRADATIONAL, BOTTOM SHARP!
/      505  569  53    3A11QZ     <<         P          <(<*<)<.
L                 18        AW
R                 :MINOR CP IN << AT 53.1
/      569  616  46    3B11QZ     <<         P BD   50  <*<)<)<.
L                 21        AG                 CL   90
R                 :TOP CONTACT GRADATIONAL, BOTTOM SHARP. MINOR CP AT 58.5
R                 :BOTTOM CONTACT IRREGULAR
/      616  670  52    3A11QZ     <<         P          <(<)<*
L                 14        AW                              <(
/      670  700  29    3A11QZ     <<         P          <.<+<(
L                 06        AW                              <-
R                 :RUST ON FRACTURES (MINOR)
/      700  729  28    3A21QZ     <<         P          <.<+<*
```

```
L                 11        AW
R                :LOWER CONTACT IS SHARP, BUT IRREGULAR
/      729   760  31    3F12CL     <<          P           <)<+<(<.
L                 19        AG
R                :SMALL (0.1 M) 3B AT TOP OF INTERVAL. STRAT COULD BE UNIT 2?
/      760   790  30    3F22CL     <<          P           <+<+<(<.
L                 17        AG
/      790   820  30    3F22CL     <<          P V/    40  <(<+<*<.
L                 15        AG
R                :TUFF CONTAINS ABUNDANT BLACK SHARDS. MINOR QZ-SER ALT'N ON
R                :SOME <<
/      820   846  26    3F23CLMS   <<          P           <*<)<(<.
L                 09        TG
/      846   858  11    3B12CL     <<          P           <(<)<(<.
L                 03        AG
R                :UPPER CONTACT IS GRADATIONAL OVER 0.3 M
/      858   864  05    8A01       <<          P             <*
L                 02        7G                  CL    70  <*<)<-
/      864   873  09    3B12CL     <<          P BD  70
L                 03        AG
R                :LOWER CONTACT GRADATIONAL, CONTAINS 0.2 CM WIDE 2C. TO BEDDING
/      873   890  17    3J12CL     <<          P BD  70  <(<)<(
L                 09        AG
R                :INTERBEDS ARE JUST OVER 1.0 CM WIDE
/      890   940  49    2C23CL     <<          P           <(<+<*<-
L                 20        TG
R                :SLIGHT QZ-SER ALT'N ON <<. THIS IS LIKELY THE ACTUAL
R                :TRANSITION INTO UNIT 2
/      940   970  30    2C22CL     <<          P           <+<)<)
L                 11        AG
/      970  1000  30    2C23CLMS   <<          P           <*<+<+<(
L                 19        AT
R                :MINOR 2D INTERBED
/     1000  1030  30    2C22CL     <<          P           <*<(<)<-
L                 21        AG
R                :MOST OF CP AT 100.4
/     1030  1060  30    2C12CL     <<          P           <)<)<*
L                 11        AG
R                :MINOR 2D
/     1060  1090  30    2C12CL     <<          P           <)<)<*#-  #?
L                 09        AG
R                :MOST CP IN SMALL BX AT 107.7 M. MAYBE SOME ARSENO TOO
/     1090  1120  28    2C13CLMS   <<          P           <+<)<)<-
L                 06        TG
/     1120  1150  30    2C12CL     <<          P           <+<)<(<.
L                 14        AG
/     1150  1180  29    2C22CL     <<          P           <+<)<)<-<-
L                 16        AG                            <-      <(
R                :MINOR QZ-SER ALT'N AT 117.6, WITH TT, SL, CP
/     1180  1210  30    2C22CL     <<          P           <)<+<)<.
L                 19        AG
R                :AGAIN, MINOR QZ-SER ALT'N
/     1210  1240  30    2C23CLMS   <<          P           <)<)<*
L                 19        AG
/     1240  1270  30    2C23CLMS   <<          P           <)<+<*<-
```

```
L                  17        TG
/    1270  1300    30    2C22CL      <<          P              <+<)<*<.
L                  17        AG
/    1300  1330    29    2C32CL      <<          P              <+<+<*
L                  12        AG
/    1330  1376    44    2C45MSQZ    <<BR        P                #+<+B(
L                  18        6T
/    1376  1386    08    8B01CY      <<F*        P CU    40
L                  00        7A                  CL    35
/    1386  1420    31    2C45MSQZ    BR<<        P                #1#+#(
L                  17        AT
R                  :NO VISIBLE TT BUT COULD BE LOW GRADE AG
/    1420  1450    30    2C54MSQZ    <<BR        P V/    65       <1#+#*
L                  12        AT
/    1450  1480    29    2C34MSQZ    <<BR        P V/    60       <=<+<-
L                  05        AT
/    1480  1500    20    2C44MSQZ    <<BR        P                <+<)<-<?
L                  06        AT
/    1500  1571    70    8B01CY      <<F*        P CU    50         D(
L                  36        GA      CM            CL    65         D-
R                  :CL-CY REPLACE FL LATHS
/    1571  1588    17    2C64MSQZ    <<BR        P                #1#+B-
L                  06        AT
/    1588  1594    06    8A02CL      <<CM        P CU    55       <=
L                  03        6G                    CL    60
R                  :PERSAVSIVE CL ALT'N
/    1594  1619    23    2C64MSQZ    BR<<        P                +1#=B-B(
L                  06        6T
R                  :0.1 M OF 8C AT 160.4. BOTTOM 0.4 M CY RICH BX; LIKELY FAULT
R                  :GOUGE
/    1619  1623    04    8C12CY      <<          P CU    50
L                  00                            CL    60
/    1623  1643    20    2C54MSQZ    BR<<        P                <=#)B.
L                  03        AT
/    1643  1653    10    8A10        <<CM        P CU    65       A=
L                  10        4G                    CL    65A*
R                  :0.1 M 8C MARGINS. SOLID PIECE OF CORE
/    1653  1680    27    2C43MSQZ    <<BR        P                #=Q=B(B(
L                  14        AT                                       B-
/    1680  1710    29    2C34MSQZ    <<          P              <)<1<=<-<-
L                  13        AT                                       <-
/    1710  1740    30    2C34MS      <<          P              <)<+<+<.<-
L                  21        AT                                       <*
/    1740  1770    30    2C34MS      <<          P              <)<=<+<-<-B?
L                  17        AT                                       <*
/    1770  1800    30    2C34MS      <<          P              <)<+<)<*<-
L                  11        AT                                       <(
R                  :TT OCCURS IN << WITH SL, IDENTIFICATION DIFFICULT
/    1800  1830    29    2C33MS      <<          P              <*<=<+<(<*
L                  08        AT                                       <)
R                  :MOST SL, TT, CP OCCURS IN TOP HALF OF INTERVAL
/    1830  1860    30    2C33MS      <<          P V/    65     <*<)<+<-<.
L                  17        AT                                       <)
/    1860  1890    30    2C23MS      <<          P              <*<+<+<-
L                  11        AT
```

```
/    1890  1920  30    2C23CLMS   <<          P          <+<)<+<.
L                 14       GT
/    1920  1950  29    2C23CLMS   <<          P          <+<+<)<-
L                 07       GT                                  <.
/    1950  1980  30    2C33CLMS   <<          P          <)<)<+<-<?
L                 09       GT                                  <-
R                :MINOR 2D
/    1980  2010  30    2C43CLMS   <<          P          <)<+<=<(<?
L                 09       TG                                  <(
R                :GENERAL REMARK: MOST OF ABOVE SL, CP, TT OCCURS IN IRREGULAR
R                :GASHES, ALL THE WAY BACK TO 168.0
/    2010  2040  30    2C43CLMS   <<          P          <*<=<+<-
L                 18       GT
/    2040  2078  37    2C43CLMS   <<BR        P          <*<+<+<)<-
L                 16       TA                                  <*
R                :MINOR BX, NOT NOT AT DYKE CONTACT
/    2078  2096  18    8C00FL     P*CM        P            A)
L                 16       9G                 CL    70
/    2096  2130  32    2C44MSQZ   <<          P            <+<+<(<*
L                 06       AT                                  <-
/    2130  2160  30    2C43CLMS   <<          P          <)<+<1<)<*
L                 12       TA                                  <*
R                :MINOR 2D, SPOTTY STRONG DISSEM. PY
/    2160  2190  30    2C43MS     <<BR        P          <)<+<=<)<?
L                 13       AT
R                :VERY FINE GRAINED GRAY-BLUE IN << WITH CP, TT ?
/    2190  2220  30    2C33CLMS   <<          P          <+<*<+<-<?
L                 15       AT                                  <.
R                :AS ABOVE
/    2220  2250  30    2C33CLMS   <<          P          <+<)<+<(<-
L                 21       AT                                  <-
/    2250  2280  30    2C33CLMS   <<BR        P          <+<*<+<-
L                 12       AT
R                :CP OCCURS ONLY AT 227.0
/    2280  2310  30    2C33CLMS   <<BR        P          <+<+<=<(
L                 15       AT
/    2310  2340        2C33CLMS   <<          P          <+<=<=<(<?
L                 15       AT                                  #+
R                :MINOR 2D. LOTS OF SL, NO POSITIVE ID OF TT, BUT SUSPECT SOME
R                :IN WITH THE SL
/    2340  2370  30    2D23CLMS   <<          P          <+<=<+  <?
L                 12       TA                                  <-
R                :SOME INTERBEDDED 2C. SL OCCURS ONLY IN FIRST 0.2 M OF INTERVAL
/    2370  2399  28    2C23CLMS   <<          P          <=<+<+
L                 05       TA
/    2399  2408  09    8A11CL     <<P*        P          D+<+D)
L                 09       7G
R                :CONTACTS SHARP, BUT IRREGULAR
/    2408  2440  31    2D22CL     <<          P BD   60  <=<*<)
L                 09       TA                                  <.
R                :INTERBEDDED 2C
/    2440  2462  22    2C44CLMS   <<          P          <=<*<)  <?
L                 12       AT                                  <*
R                :NO POSITIVE ID ON TT, BUT SUSPECT IN WITH SL
/    2462  2484  22    2C44MSCL   <<          P          <=<*<*  <?
```

```
L                 05          GT                                          <>
R                :AS ABOVE, SL OCCURS ONLY IN TWO <<'S
/    2484   2515  31     8A10        <<A*          P CU     40     A=<-
L                 28          BA                                    D+
R                :QTZ ALSO OCCURS IN <<'S. HOLE ENDS IN DYKE
R                :HOLE LIKELY SHOULD HAVE BEEN CONTINUED. I SHUT IT DOWN BECAUSE
R                :OF THE INCREASE OF CL IN <<'S
R                :END OF HOLE
A001
ALAB             EQUITY MINESITE LABORATORY
ATYP             ASSAY
AMTH             WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM             RCOVSAMPLE    RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R       00   104 :TRICONED - NO CORE
A001   104   130        6999        0.05    0.5 0.02  0.005 0.005 3.27  0.010
A001   130   160        7000        0.04    0.5 0.02  0.005 0.005 3.64  0.005
A001   160   190        7001        0.04    0.5 0.02  0.005 0.005 4.18  0.005
A001   190   220        7002        0.04    0.5 0.04  0.005 0.005 4.45  0.005
A001   220   250        7003        0.03    0.5 0.01  0.005 0.005 3.35  0.005
A001   250   280        7004        0.04    0.5 0.02  0.005 0.005 0.78  0.005
A001   280   310        7005        0.05    3.0 0.03  0.01  0.005 1.31  0.04
A001   310   340        7006        0.02    2.0 0.02  0.005 0.005 6.01  0.005
A001   340   370        7007        0.06    0.5 0.01  0.005 0.005 1.15  0.005
R      370   397 :DYKE - NO SAMPLE
A001   397   430        7008        0.06    0.5 0.005 0.005 0.005 0.88  0.005
A001   430   460        7009        0.10    0.5 0.01  0.005 0.005 1.36  0.005
A001   460   490        7010        0.05    0.5 0.005 0.005 0.005 0.58  0.005
A001   490   520        7011        0.05    0.5 0.005 0.005 0.005 2.20  0.005
A001   520   550        7012        0.10    0.5 0.005 0.005 0.005 0.69  0.005
A001   550   580        7013        0.07    0.5 0.07  0.005 0.005 1.06  0.005
A001   580   610        7014        0.14    2.0 0.02  0.005 0.005 1.84  0.005
A001   610   640        7015        0.07    0.5 0.02  0.005 0.005 2.02  0.005
A001   640   670        7016        0.05    0.5 0.03  0.005 0.005 1.48  0.02
A001   670   700        7017        0.06    0.5 0.03  0.005 0.005 0.98  0.005
A001   700   730        7018        0.09    3.0 0.04  0.001 0.001 0.82  0.005
A001   730   760        7019        0.06    2.0 0.04  0.001 0.001 4.04  0.001
A001   760   790        7020        0.09    2.0 0.07  0.001 0.001 2.80  0.001
A001   790   820        7021        0.06    0.5 0.06  0.001 0.001 2.73  0.001
A001   820   850        7022        0.13    2.0 0.06  0.001 0.001 3.10  0.001
A001   850   880        7023        0.10    2.0 0.04  0.001 0.001 2.89  0.001
A001   880   910        7024        0.11    2.0 0.05  0.001 0.001 4.27  0.001
A001   910   940        7025        0.07    0.5 0.04  0.001 0.001 4.01  0.001
A001   940   970        7026        0.09    2.0 0.07  0.001 0.001 3.70  0.001
A001   970  1000        7027        0.26   13.0 0.06  0.001 0.001 3.57  0.001
A001  1000  1030        7028        0.13    4.0 0.03  0.001 0.001 4.07  0.001
A001  1030  1060        7029        0.05    0.1 0.03  0.001 0.001 2.37  0.001
A001  1060  1090        7030        0.13    3.0 0.06  0.001 0.001 3.70  0.001
A001  1090  1120        7031        0.09    3.0 0.02  0.001 0.001 2.52  0.03
A001  1120  1150        7032        0.07    2.0 0.04  0.001 0.001 2.99  0.001
A001  1150  1180        7033        0.11    4.0 0.04  0.001 0.001 2.30  0.12
A001  1180  1210        7034        0.11    3.0 0.03  0.001 0.001 2.42  0.005
A001  1210  1240        7035        0.09    4.0 0.04  0.001 0.001 2.77  0.02
A001  1240  1270        7036        0.08    4.0 0.01  0.001 0.001 3.01  0.005
A001  1270  1300        7037        0.11    6.0 0.05  0.001 0.001 3.64  0.02
A001  1300  1330        7038        0.12    9.0 0.02  0.001 0.001 2.76  0.03
```

A001	1330	1360		7039	0.28	27.0	0.18	0.005	0.04	2.96	0.05
A001	1360	1390		7040	0.14	28.0	0.18	0.005	0.005	3.84	0.001
A001	1390	1420		7041	0.19	46.0	0.07	0.005	0.001	3.03	0.001
A001	1420	1450		7042	0.22	57.0	0.04	0.005	0.001	4.08	0.001
A001	1450	1480		7043	0.07	8.0	0.04	0.001	0.001	3.56	0.005
A001	1480	1500		7044	0.06	5.0	0.04	0.001	0.001	2.87	0.005
R	1500	1571	:DYKE - NO SAMPLE								
A001	1571	1588		7045	0.33	14.0	0.04	0.02	0.001	3.33	0.21
R	1588	1594	:DYKE - NO SAMPLE								
A001	1594	1619		7046	0.29	7.0	0.04	0.001	0.001	3.01	0.09
R	1619	1623	:DYKE - NO SAMPLE								
A001	1623	1643		7047	0.04	3.0	0.04	0.005	0.001	3.84	0.005
R	1643	1653	:DYKE - NO SAMPLE								
A001	1653	1680		7048	0.33	11.0	0.05	0.005	0.001	4.43	0.09
A001	1680	1710		7049	0.17	6.0	0.03	0.001	0.001	4.34	0.08
A001	1710	1740		7050	0.06	3.0	0.03	0.001	0.001	3.08	0.02
A001	1740	1770		7051	0.05	3.0	0.03	0.001	0.001	2.35	0.02
A001	1770	1800		7052	0.04	3.0	0.03	0.001	0.001	2.48	0.37
A001	1800	1830		7053	0.12	7.0	0.03	0.001	0.001	6.78	0.41
A001	1830	1860		7054	0.13	3.0	0.03	0.001	0.001	5.01	0.005
A001	1860	1890		7055	0.16	0.5	0.03	0.001	0.001	4.54	0.001
A001	1890	1920		7056	0.12	3.0	0.04	0.001	0.001	4.75	0.005
A001	1920	1950		7057	0.10	0.5	0.02	0.04	0.005	3.77	0.03
A001	1950	1980		7058	0.12	0.5	0.02	0.03	0.005	4.11	0.02
A001	1980	2010		7059	0.17	0.5	0.03	0.06	0.005	5.52	0.03
A001	2010	2040		7060	0.08	0.5	0.03	0.01	0.005	4.35	0.02
A001	2040	2078		7061	0.10	0.5	0.03	0.06	0.005	4.15	0.03
R	2078	2096	:DYKE - NO SAMPLE								
A001	2096	2130		7062	0.09	0.5	0.02	0.04	0.005	3.30	0.08
A001	2130	2160		7063	0.26	0.5	0.03	0.09	0.01	5.55	0.06
A001	2160	2190		7064	0.18	0.5	0.03	0.04	0.005	4.46	0.005
A001	2190	2220		7065	0.07	0.5	0.01	0.005	0.005	4.16	0.005
A001	2220	2250		7066	0.08	0.5	0.02	0.005	0.005	3.56	0.11
A001	2250	2280		7067	0.07	0.5	0.02	0.005	0.005	4.95	0.005
A001	2280	2310		7068	0.08	0.5	0.02	0.005	0.005	4.13	0.01
A001	2310	2340		7069	0.10	0.5	0.02	0.01	0.005	5.10	0.54
A001	2340	2370		7070	0.06	0.5	0.02	0.01	0.005	3.07	0.05
A001	2370	2399		7071	0.06	0.5	0.02	0.01	0.005	3.67	0.07
R	2399	2408	:DYKE - NO SAMPLE								
A001	2408	2440		7072	0.04	0.5	0.02	0.01	0.005	3.42	0.02
A001	2440	2462		7073	0.04	0.5	0.04	0.01	0.01	3.45	0.51
A001	2462	2484		7074	0.05	0.5	0.05	0.005	0.01	3.12	0.50
R	2484	2515	:DYKE - NO SAMPLE								
R			:END OF HOLE - END OF LOG								
R			END OF ASSAYS - END OF LOG								

```
IDEN6B0201      X86CH265 NQ   JUL86RWW   G&D JUL86S38          0.0
IPRJ          EQUITY SILVER MINES LTD        SUPERSTITION ZONE - ST GEOCODE
S000   00   457 MT  168.9 090.0 -45.0              5612.14   7537.21   1135.33
S001  457  1302     168.9 090.0 -44.5
S002 1302  1689     168.9 090.0 -42.5
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                    MSCLQZPYCPTTASPR
LNAM                                                    CBGY  MGHESLGLMO
/      00   488        OVBN                  P
R                :TRICONED - NO CORE
/     488   520  29    2C34MS      <<BR      P <<    60  <(<+<=B.
L                  08        AT
R                :SOME INTERBEDDED 2D
/     520   549  27    2D44CL      <<BR      P           <(<=<=B.
L                  09        6A
R                :SOME INTERBEDDED 2C
/     549   552  03    8C11        <<        P CU    65      <.
L                  00        YT      VU
/     552   579  25    2C44MS      <<BR      P           <(<=<=<-<.
L                  08        AT
R                :SOME INTERBEDDED 2D. :SOME FE STAINING
/     579   613  31    2C34MS      <<BR      P           <(<+<=Q*<.
L                  15        AT
R                :SOME INTERBEDDED 2D
/     613   623  09    8B13MS      <<AA      P
L                  08        5T                      <(
R                :MORE MAFIC COMPOSITION FROM 61.8 TO 62.2 M. FELDSPAR INFILLING
R                :AMYGDS
/     623   653  27    2C44MS      <<BR      P           <*<+<=B.
L                  11        AT
R                :SOME CP IN <<
/     653   690  37    2C44MS      <<BR      P           <(<=<=P-
L                  11        AT
/     680   690       X                     D             +4
R                :QTZ FLOODING CONTAINS PATCHY PY
/     690   715  25    2C44MS      <<BR      P <<    60  <(<=<=
L                  08        AT
R                :.1 M OF PATCH FELDSPAR FROM 71.3 TO 71.4 M
R                :POSSIBLE GL BUT MAY BE TARNISHED PY
/     715   745  28    2D44CL      <<BR      P             <+<=
L                  03        TA
R                :SOME FE STAINING. :SOME INTERBEDDED 2C. SOME PY STAINED BLUE
R                :SIMILAR FELDS TO ABOVE
/     745   772  24    2D44CL      <<BR      P             <+<=
L                  06        TA
R                :SOME PATCHY PY. :STILL SOME FE STAINING
/     772   803  28    2D44CL      <<BR      P             <+Q=
L                  08        TA
R                :SOME PY QUITE MASSIVE. :SOME INTERBEDDED 2C
/     803   833  26    2C44MS      <<BR      P           <-<+Q=
L                  03        AT
/     803   805       X                     D V1    60
R                :QTZ-PY VEIN FROM 80.3 TO 80.5
/     833   863  28    2C34MS      <<BR      P           <(<+<=B.
```

```
L                06        AT
R               :SOME FE STAINING. :AGAIN SOME STRANGE FELDSPARS AS BEFORE
/      863   893  25    2C34MS     <<          P           <(<+<+
L                00        AT
/      864   865       X                      D V1    55
R               :.1 M OF QTZ-PY VEIN FROM 86.4 TO 86.5 M
/      893   923  26    2C45MS     <<BR        P           <(<+<+<.
L                02        AT
R               :SOME PATCHY PYRITE. :IDENTIFIED BLUE-GRAY MIN. (CHLORITE?)
R               :ROCK CONTAINS FINE GLASS SHARDS. :ALSO SOME FE STAINING.
R               :SOME VEINS OF ALTERED FELDSPAR(?)
/      923   953  27    2C44MS     <<BR        P           <(<+<=<-
L                02        AT
R               :SLIGHT FE STAINS. :AGAIN FELDSPAR AS ABOVE. :SOME PY PATCHY
/      953   983  28    2C44MS     <<          P           <*<+<+
L                02        AT
R               :SOME MASSIVE PY AND SOME MINOR QTZ FLOODING. :SOME FE STAINS
/      983  1013  29    2C34MS     <<BR        P WP    35  <(<+<+  <.
L                06        6T                          Q-
R               :SOME FE STAINING. :SOME CARONATE AGAIN FELDSPAR TOO
R               :TT ONLY AT 99.2 M
/     1013  1043  27    2C44MS     <<BR        P           <(<+<+
L                00        AT
R               :AGAIN ALT. FELDSPAR. :FE STAIN AT BEGINNING OF INT
/     1043  1073  29    2C44MS     <<BR        P           <(<+<+  B.
L                00        AT                        Q.
R               :MINOR FE STAINS :TT ONLY AT 105.9 M :QTZ-PY VEIN FOR 0.1 M
R               :FROM 107.4 - 107.5 M
/     1073  1103  29    2C44MS     <<BR        P           <(<+<=
L                05        AT
R               :GOOD BRECCIATION FROM 107.5 - 107.7 M
/     1103  1133  28    2C43MSCL   <<BR        P             <+<+<.
L                03        ATAG
R               :0.1 M OF QTZ-PY VEIN FROM 112.9 - 113.0 M :AGAIN FELDS PATCHES
R               :SOME INTERBEDDED 2D :GOOD BR'N AT START OF INT
/     1133  1163  29    2C44MS     <<BR        P           <(<+<=<-
L                05        AT                                  <.<.
R               :SOME FE STAINING :SL MAYBE QUESTIONABLE
/     1163  1193  28    2C44MS     <<BR        P           <*<+<=
L                03        AT
R               :SOME FE STAINING
/     1193  1223  29    2C43MS     <<          P           <*<+<+
L                02        AT                        B.
R               :SOME FELDSPAR BLEBS. FE STAINS
/     1223  1253  28    2C44MS     <<ER        P           <(<+<+<.
L                03        AT                        Q.
R               :CP ONLY FROM 124.0 - 124.1 M :MINOR FE STAINS :LAST METER
R               :MAINLY ASH :QTZ-PY VEIN .1 M - CANNOT DETERMINE C1
/     1253  1283  27    2C43MS     <<BR        P           <*<+<+<.
L                00        AT                                  <.B.
R               :SP & GL ONLY AT 127.8 M
/     1283  1313  28    2C44MS     <<BR        P           <(<+<=
L                00        AT                            <*
R               :GY FROM 129.8 - 130.5 M
/     1313  1336  26    2C44MS     <<          P           <(<+<=Q(<.
```

```
L                 08        AT                                          <(
R                :GREY-BLUE HIGH LUSTRE MIN - UNIDENTIFIED TT(?)
/    1336  1360   23    2C44MS     <<BR        P            <(<+<+<(<.
L                 03        AT                                        <.
/    1360  1379   19    8A11CL     <<FB        P              <.<.
L                 11        AG     A*
/    1379  1389   09    2C44MS     <<BR        P CU    50   <+<+<+<.<)
L                 06        AT                                    <.<*
R                :STRONGLY BRECCIATED AT BEGINNING OF INT
/    1389  1415   25    8A11CL     <<          P CL    45       <(
L                 21        AG                                  <.<.
R                :CARBONATE AMYGDS :INTERIOR 8A DYKE WITH SLIGHTLY DIFF. TEXT.
/    1415  1445   28    2C44MS     <<BR        P            <+<+<=
L                 03        AT                                    <.Q(
R                :HE ONLY AT 144.6 M :PY-QZ VEIN (.2 M) FROM 143.7 - 143.9 M
/    1445  1475   29    2C44MS     <<          P            <)<+<+
L                 08        AT
R                :SOME INTERBEDDED 2D
/    1475  1505   29    2C44MS     <<BR        P            <(<+<=
L                 05        AT                                      <)
R                :SOME SL IN PATCHES
/    1505  1535   29    2C44MS     <<BR        P            <(<+<=<.<.
L                 08        AT                                      <(
R                :HE MAY BE MIXED WITH SL :CP ONLY IN 2 PLACES (IN <<)
/    1535  1550   14    2C44MS     <<BR        P <<    55   <(<+<+<.<.
L                 06        AT                                  <?<(
R                :BLUISH GRAY MIN WITH SL << - MAYBE SPECULARITE - CAN'T TELL!
/    1550  1558   07    8A11CL     <<          P
L                 06        5G
R                :CARBONATE AMYGDS :CONTACTS NOT MEAS. DUE TO BROKEN CORE
/    1558  1589   29    2C44MS     <<BR        P            <(<+<=<.<.
L                 08        AT                                      <.
R                :BRITTLE PURPLE-BLUE MIN. AGAIN(?) :3 CM PY-QZ VEIN AT 158.6 M
/    1589  1621   31    2C44MS     <<BR        P            <(<+=<*<-
L                 09        AT                                  <?<)
R                :AGAIN BLUE GRAY MIN WITH SL - COULD BE SPECULARITE
R                :0.4 M OF STRONGLY BRECCIATED CORE WITH GOOD TT, CP, SL
R                :FROM 161.6 M
/    1621  1653   31    2C44MS     <<BR        P <<    50   <(<+<+Q-<-
L                 14        AT                          Q.      <?<(
R                :SOME GOOD FRACTURING :ROCK STARTING TO TURN GREENER AT END
R                :OF INTERVAL
/    1653  1671   17    2C33MS     <<          P            <)<+<)  <.
L                 06        AT                                  <?<-
R                :TT AT 165.7 M
/    1671  1689   16    2C43MS     <<BR        P            <)<+<)<.<.
L                 00        GT                                  <.<.
R                :0.1 M QZ-PY VEIN AT 167.5 M :TUFF ASH HAS GREEN COLORATION
R                :END OF LOG
A001
ALAB             EQUITY MINESITE LABORATORY
ATYP             ASSAY
AMTH             WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM             RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R      00   488 :TRICONED - NO CORE
```

A001	488	520	7081	0.31	0.5	0.02	0.06	0.03	4.87	0.005
A001	520	550	7082	0.44	11.0	0.04	0.09	0.04	7.50	0.02
A001	550	579	7083	0.35	10.0	0.04	0.10	0.04	6.31	0.005
A001	579	613	7084	0.85	15.0	0.03	0.16	0.06	7.64	0.005
R	613	623	:DYKE - NO SAMPLE							
A001	623	653	7085	0.10	0.5	0.02	0.005	0.005	3.70	0.005
A001	653	683	7086	0.22	0.5	0.07	0.03	0.01	6.01	0.005
A001	683	712	7087	0.02	0.5	0.11	0.005	0.005	7.41	0.005
A001	712	742	7088	0.01	0.5	0.04	0.005	0.005	11.54	0.005
A001	742	772	7089	0.01	0.5	0.04	0.005	0.005	7.49	0.005
A001	772	803	7090	0.02	0.5	0.03	0.005	0.005	8.23	0.005
A001	803	833	7091	0.02	0.5	0.03	0.005	0.005	6.04	0.005
A001	833	863	7092	0.04	0.5	0.03	0.005	0.005	3.82	0.02
A001	863	893	7093	0.03	0.5	0.03	0.005	0.005	5.21	0.005
A001	893	923	7094	0.08	0.5	0.04	0.005	0.005	3.96	0.01
A001	923	953	7095	0.12	0.5	0.03	0.005	0.005	4.37	0.005
A001	953	983	7096	0.06	0.5	0.03	0.02	0.005	4.83	0.005
A001	983	1013	7097	0.03	0.5	0.02	0.01	0.005	2.12	0.005
A001	1013	1043	7098	0.03	0.5	0.02	0.01	0.005	3.41	0.005
A001	1043	1073	7099	0.02	0.5	0.02	0.01	0.005	5.72	0.005
A001	1073	1103	7100	0.03	0.5	0.02	0.01	0.005	5.03	0.005
A001	1103	1133	7101	0.05	0.5	0.03	0.01	0.005	4.32	0.005
A001	1133	1163	7102	0.04	0.5	0.02	0.005	0.005	3.82	0.005
A001	1163	1193	7103	0.04	0.5	0.02	0.005	0.005	3.54	0.005
A001	1193	1223	7104	0.04	0.5	0.02	0.005	0.005	4.71	0.005
A001	1223	1253	7105	0.06	0.5	0.02	0.005	0.005	3.87	0.005
A001	1253	1283	7106	0.11	0.5	0.02	0.04	0.01	3.50	0.02
A001	1283	1313	7107	0.03	0.5	0.03	0.005	0.01	4.72	0.05
A001	1313	1336	7108	0.28	18.0	0.07	0.05	0.01	4.13	0.28
A001	1336	1360	7109	0.06	0.5	0.11	0.01	0.01	4.18	0.25
R	1360	1379	:DYKE - NO SAMPLE							
A001	1379	1389	7110	0.05	0.5	0.03	0.005	0.005	2.73	0.53
R	1389	1415	:DYKE - NO SAMPLE							
A001	1415	1445	7111	0.02	0.5	0.06	0.005	0.005	5.83	0.18
A001	1445	1475	7112	0.05	0.5	0.02	0.005	0.005	4.04	0.05
A001	1475	1505	7113	0.01	0.5	0.04	0.005	0.005	5.80	0.17
A001	1505	1535	7114	0.06	0.5	0.12	0.005	0.005	5.04	0.36
A001	1535	1550	7115	0.09	0.5	0.08	0.005	0.005	2.56	1.00
R	1550	1558	:DYKE - NO SAMPLE							
A001	1558	1589	7116	0.07	0.5	0.12	0.005	0.005	6.00	0.03
A001	1589	1621	7117	0.27	26.0	0.14	0.02	0.04	7.00	1.68
A001	1621	1653	7118	0.10	9.0	0.05	0.005	0.01	5.00	0.74
A001	1653	1671	7119	0.04	1.0	0.01	0.005	0.001	2.31	0.12
A001	1671	1689	7120	0.03	2.0	0.02	0.005	0.005	3.77	0.05
R			:END OF HOLE - END OF LOG AT 168.9 M							
R			END OF ASSAYS - END OF LOG							

```
IDEN6B0201       X86CH266 NQ   AUG86DJH   G&D AUG86S38            0.0
IPRJ          EQUITY SILVER MINES LTD          SUPERSTITION ZONE - ST GEOCODE
S000   00   457 MT  230.4 090.0 -45.0                  5523.54   7452.69   1128.68
S001  457  1470     230.4 090.0 -43.0
S002 1470  2304     230.4 090.0 -45.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                        MSCLQZPYCPTTASPR
LNAM                                                        CBGY  MGHESLGLMO
/      00   100        OVBN                      P
R                :TRICONED  0 - 9.8 M NO CORE :CORED A FEW BOULDERS 9.8 - 10.0 M
/     100   130  25    2C24MSCL   <<            P              <)<)<.
L                  00        GT
R                :LI ON FRACTS :TO 2D LOC
/     130   160  29    2C23CLMS   <<            P <<   028     <)<)<.
L                  00        TG
R                :ONLY MINOR LI PAST 13.7 M :2C24 13.0-13.7 M (GRADATIONAL CNT)
R                :10% MS AS << ENVELOPES
/     160   190  26    2C23CLMS   <<            P <<   024   <+<)<)
L                  09        TG                             <(
R                :10% MS AS << ENVELOPES :5% CL AS << ENVELOPES
/     190   212  20    2C23CLMS   <<            P <<   036   <+<)<+
L                  05        TG                             <(
R                :5% MS AS << ENVELOPES :10% CL AS << ENVELOPES
/     212   240  22    8C05MSCL   P*            P
L                  18        GT
R                :TYPICAL POST-MIN LATITE DYKE :CNTS NOT OBSERVED DUE TO
R                :BROKEN CORE
/     240   270  29    2C23CLMS   <<            P            <(<)<+<.<.
L                  00        TG
R                :5% MS AS << ENVELOPES :TT?
/     270   300  28    2C23CLMS   <<            P            <(<)<+<.
L                  02        TG
R                :TO 2C15 LOC :10% MS AS << ENVELOPES
/     300   330  30    2C23CLMS   <<            P              <)<+<(
L                  05        TG
R                :10% MS AS << ENVELOPES
/     330   360  20    2C24MSCL   <<            P              <)<)<.
L                  00        GT
R                :HEAVILY BROKEN UP INTERVAL :60% MS
/     360   390  25    2C24CLMS   <<            P            <(<)<)<(
L                  04        TG
R                :TO 2D LOC :30% MS
/     390   420  30    2C24CLMS   <<            P            <(<)<)
L                  15        TG
R                :30% MS
/     420   450  28    2C23CLMS   <<            P <<   025   <(<)<)
L                  12        TG
R                :5% MS AS << ENVELOPES :1% CL AS << ENVELOPES
/     450   480  30    2C23CLMS   <<            P            <(<)<)<.
L                  09        TG                             <+
R                :5% MS AS << ENVELOPES :2% CL AS << ENVELOPES :TO 2C23 LOC
/     480   510  26    2C23CLMS   <<            P            <(<)<+<.
L                  12        TG
R                :TO 2C15 @ END OF INTERVAL :10% MS AS << ENVELOPES
```

```
/     510   540  29    2C23CLMS   <<          P          <(<)<+
L                05       TG
R               :TO 2C15 @ START OF INTERVAL :10% MS AS << ENVELOPES
/     540   563  23    2C44MSCL   <<BR        P            <)<+<+
L                08       GT                            <(
R               :TO 8A FROM 54.6 - 55.1 M
/     563   598  35    8A11CLCY   <<P*        P CU   020  <(
L                30       GA                   CL   015<(
R               :PLAG PHENOS TO 15 X 3 MM (ALTERED TO MONT)
/     598   611  13    2C34MSCL   <<          P          <(<+<+
L                05       GT                            <(
/     611   624  13    8A11CLCY   <<P*        P CU   025    <(
L                00       GA                            <(
R               :SIMILAR TO 56.3 - 59.8 EXCEPT LOCALLY BLEACHED WHITE
R               :LOWER CNT NOT OBSERVED DUE TO GROUND CORE
/     624   650  24    2C24CLMS   <<          P            <+<)<+
L                04       TG                            <(
R               :2% CL AS << ENVELOPES
/     650   680  28    2C24CLMS   <<          P            <(<)<+<.
L                02       TG                            <+
/     680   710  29    2C34MSCL   <<          P            <(<)<)
L                13       GT                            <+
R               :TO 2C54 LOC
/     710   740  28    2C34MSCL   <<          P              <+<)<.
L                05       GT                             <(
R               :TO 2C12 LOC (EOI)
/     740   770  29    2C24MSCL   <<          P              <)<)<.
L                06       GT
R               :TO 2C12 LOC (SOI)
/     770   800  28    2C25MS     <<          P              <*<)
L                00       5T
R               :5% QZ AS << ENVELOPES
/     800   812  11    2C25MS     <<          P              <*<)<.
L                00       5T
R               :AS ABOVE 77.0 - 80.0 M
/     812   822  10    8A01CY     P*          P CU   070
L                04       5A
R               :LOWER CNT NOT OBSERVED DUE TO BROKEN CORE
/     822   860  36    2C25MS     <<                         <*<)<.<?
L                02       5T
R               :MINOR GOUUGE @ 83.5 M :5% QZ AS << ENVELOPES
/     860   890  28    2C24MSCL   <<          P              <*<)<(<?
L                19       GT
R               :BROKEN CORE AND GOUGE 88.8 - 89.0 M :TO 2C34 LOC
/     890   915  24    2C24MSCL   <<          P              <*<)<(
L                03       GT
R               :TO 2C35LOC
/     915   925  09    8A01CY     P*CM        P CU   048
L                06       AU                   CL   045      D(
R               :GOOD INTRUSIVE CNTS W/ CHILLED MARGINS :.1 M XENOLITH @
R               :UPPER CNT
/     925   950  23    2C24CLMS   <<          P            <*<)<)<.
L                03       TG
R               :TO 2C45LOC
/     950   980  25    2C34CLMS   <<          P            <(<+<)<(
```

```
L                 06         TG                                <(
/    980   1010   18     2C24MSCL                P              <(<+<)<.
L                 00         GT
R                :POOR REC - SMALL CHIPS OF CORE - NO GOUGE
/   1010   1045   40     2C45MS      <<          P                <)<)
L                 05         AT
R                :GOUGE @ 103.6
/   1024   1024           X                      D F/    080
R                :2 CMS GOUGE
/   1045   1101   56     8A11CLCY    P*A*        P CU    070     <*
L                 42         AG      <<                          <*
R                :GOUGE & BXIA 109.6 - 110.1 M :NOTE 2 TYPES OF ANDESITE DYKE
R                :(AMYGDALOIDAL ONE CUTS PORPHYRITIC ONE)
R                :UNALIGNED PLAG PHENOS (15 X 2 MM) ALTERED TO SAUSS
R                :LOWER CNT OBBSCURRED IN GOUGE :.08 M XENOLITH @ 109.6 M
/   1101   1130   27     2C55MS      BR<<        P               #+#+<(
L                 13         AT
R                :TO 2C35 LOC
/   1130   1160   30     2C55MS      BR<<        P               #+#=#)#(
L                 09         AT
/   1160   1190   27     2C35MS      <<          P               <+<+<(<(
L                 17         5T
/   1190   1220   28     2C35MS      <<          P               <)<)
L                 02         5T
R                :8A FROM 115.1 - 115.4 (PREVIOUS INTERVAL)
/   1220   1250   25     2C35MS      <<          P <<    068     <+<)<.<.
L                 08         5T
/   1250   1280   30     2C35MS      <<          P <<    060     <)<)<.
L                 05         5T
/   1280   1310   30     2C35MS      <<          P <<    060     <)<)<.<(
L                 03         5T
R                :TO 2D LOC :OCC PY + QZ V/
/   1310   1340   29     2C35MS      <<BR        P               <)<)<(<.
L                 05         5T
/   1331   1331           X                      D F/    015
/   1340   1370   27     2C35MS      <<          P               <)<)<(<(
L                 06         5T
R                :8A FROM 134.2 - 134.8 M
/   1370   1400   30     2C35MS      <<          P               <)<)<*<(
L                 10         5T
/   1400   1416   16     2C35MS      <<          P               <)<)<(
L                 00         5T
R                :TO 2C45 LOC :TO 2D LOC
/   1416   1428   12     8A02CLCB    P*A*        P CU    060
L                 10         5G                    CL    085
/   1428   1460   32     2C25MS      <<          P <<    060     <)<)<(<.
L                 03         5T
R                :TO 2D LOC
/   1460   1490   30     2C25MS      <<          P V/    050     <+<+<(<.
L                 04         5T
R                :4 - V/ QZ + PY 2 - 4 CMS WIDE
/   1490   1520   30     2C35MS      <<BR        P               <)<)<*<?
L                 13         5T
R                :TO 2C55 LOC
/   1520   1550   29     2C55MS      BR<<        P               #)#+  <?
```

```
L                14        5T                                          <?<*
R               :TT POSSIBLY IN W/ SL - DIFFICULT TO IDENTIFY POSITIVELY
R               :TO 2C35 LOC :POSSIBLY HE (HS) IN W/ SL
/    1550  1580   30    2C65MS     BR<<        P              #+#+#.#?
L                04        5T                              Q(    #?
R               :TO 2C35 LOC :APPEARS TO BE TECTONIC BXIA W/ SOME GOUGE
/    1580  1610   29    2C35MS     <<          P <<   040    <)<)<(
L                07        5T                                  <?<(
/    1610  1640   29    2C55MS     BR<<        P              #+#+
L                22        5T
R               :TO 2C35 TOWARDS EOI
/    1640  1670   29    2C35MS     <<          P <<   070    <)<)<(<.
L                16        5T
/    1670  1700   30    2C35MS     <<          P <<   050    <)<)Q(
L                12        5T
/    1700  1730   30    2C35MS     <<          P <<   052    <)<)<(
L                15        5T
/    1730  1760   29    2C35MS     <<          P <<   060    <)<)
L                04        5T
/    1760  1790   26    2C55MS     <<          P              #)#+  #?
L                02        5T
R               :GOUGE @ 177.3 M
/    1790  1820   30    2C35MS     <<          P              <)<)
L                04        5T
/    1820  1850   28    2C45MS     <<          P              <)<+
L                08        5T
/    1850  1880   30    2C55MS     <<          P              #)#)  ##
L                19        5T
/    1880  1910   27    2C45MS     <<          P              <*<)<.#(
L                02        5T
R               :TO 2C55 LOC
/    1910  1940   26    2C45MS     <<          P              <)<)<(<)
L                20        5T
R               :TO 2C55 LOC :TT OBSERVED TO CROSS-CUT PY :LOST CORE @ 191.1 M
/    1940  1953   13    2C45MS     <<          P              <)<)<*
L                07        5T                                  <.
/    1953  1965   12    8A02CL     A*          P CU   042
L                09        5G                    CL   045      D(
/    1965  2000   33    2C45MS     <<<<        P              <)<+<*
L                17        5T                                     <(
/    2000  2030   30    2C45MS     <<          P              <)<+<*
L                04        5T
/    2030  2060   30    2C24CLMS   <<          P             <*<*<*<(
L                09        TG
R               :2C25 TO 204.2 :8A 203.7 - 203.9 M :CP ONLY TO 204.2
/    2060  2090   30    2C24CLMS   <<          P             <*<*<*<.<?
L                22        TG                                     <.
R               :GREY UNIDENTIFIED MINERAL W/ SL :NOTE COLOR CHANGE @ 204.2 M
/    2090  2120   29    2C24CLMS   <<          P             <*<*<*<.
L                04        TG
/    2120  2150   29    2C24CLMS   <<          P             <(<*<*
L                05        TG
R               :TO 2C25 LOC
/    2150  2170   20    2C24CLMS   <<          P             <(<*<*
L                08        TG                                     <.
```

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R                    :TO 2C25 LOC
/     2170   2195    20     2C24MSCL    <<          P           <.<*<*
L                    12         GT                                    <*
/     2195   2225    30     8A02CLCB    A*<<        P
L                    29         4G                    CL    050<.
R                    :V WEAK << TEXT W/ CB :UPPER CNT NOT OBSERVED
/     2225   2255    30     2C24CLMS    <<          P           <(<*<*<.
L                    03         TG
R                    :TO 2C25 @ END OF INTERVAL
/     2255   2285    30     2C24MSCL    <<          P           <(<*<)
L                    02         GT
R                    :TO 2C25 LOC :TO 2D LOC
/     2285   2304    19     2C24CLMS    <<          P           <(<*<)
L                    03         TG
R                    :EOH @ 230.4
A001
ALAB                 EQUITY MINESITE LABORATORY
ATYP                 ASSAY
AMTH                 WET EXTRACTION A.A. -- AU FIRE ASSAYED FIRST
AUMM                 RCOVSAMPLE    RQD % CU   G/TAG G/TAU % SB   % AS   % FE   % ZN
R       00    100    :OVBN - NO CORE
A001    100   130          7161        0.13     0.5 0.03  0.02   0.005  2.13   0.001
A001    130   160          7162        0.09     0.5 0.02  0.01   0.005  2.46   0.001
A001    160   190          7163        0.05     0.5 0.03  0.005  0.005  2.61   0.001
A001    190   212          7164        0.06     0.5 0.04  0.005  0.005  2.88   0.001
R       212   240    :DYKE - NO SAMPLE
A001    240   270          7165        0.05     0.5 0.02  0.005  0.005  3.17   0.001
A001    270   300          7166        0.08     0.5 0.02  0.005  0.005  2.44   0.001
A001    300   330          7167        0.07     0.5 0.02  0.005  0.005  2.01   0.001
A001    330   360          7168        0.09     0.5 0.02  0.005  0.005  1.75   0.001
A001    360   390          7169        0.06     0.5 0.02  0.005  0.005  2.980  0.001
A001    390   420          7170        0.12     0.5 0.02  0.02   0.005  2.41   0.001
A001    420   450          7171        0.11     0.5 0.03  0.02   0.005  3.52   0.001
A001    450   480          7172        0.04     0.5 0.03  0.005  0.005  5.31   0.001
A001    480   510          7173        0.07     0.5 0.01  0.01   0.005  2.35   0.001
A001    510   540          7174        0.09     0.5 0.02  0.01   0.005  2.01   0.001
A001    540   563          7175        0.05     0.5 0.02  0.01   0.005  2.74   0.001
R       563   598    :DYKE - NO SAMPLES
A001    598   622          7176        0.06     0.5 0.02  0.01   0.005  3.12   0.001
A001    622   650          7177        0.10     0.5 0.02  0.03   0.005  2.64   0.001
A001    650   680          7178        0.07     0.5 0.02  0.005  0.005  2.99   0.001
A001    680   710          7179        0.18     1.0 0.04  0.005  0.001  4.02   0.005
A001    710   740          7180        0.09     1.0 0.01  0.005  0.001  2.51   0.005
A001    740   770          7181        0.07     0.5 0.01  0.001  0.01   2.55   0.005
A001    770   800          7182        0.14     1.0 0.01  0.005  0.005  2.58   0.005
A001    800   812          7183        0.12     1.0 0.01  0.005  0.005  2.80   0.005
A001    822   860          7184        0.07     0.5 0.01  0.005  0.005  2.84   0.005
A001    860   890          7185        0.07     0.5 0.05  0.005  0.001  3.29   0.005
A001    890   915          7186        0.14     0.5 0.02  0.005  0.001  3.23   0.005
R       915   925    :DYKE - NO SAMPLE
A001    925   950          7187        0.12     2.0 0.01  0.005  0.01   2.48   0.005
A001    950   980          7188        0.17     2.0 0.01  0.005  0.001  2.87   0.005
A001    980   1010         7189        0.07     1.0 0.01  0.005  0.005  1.65   0.005
A001    1010  1045         7190        0.03     1.0 0.02  0.005  0.02   3.39   0.005
R       1045  1101   :DYKE - NO SAMPLES
```

A001	1101	1130		7191	0.19	7.0	0.05	0.01	0.03	6.22	0.02
A001	1130	1160		7192	0.78	20.0	0.03	0.005	0.01	5.58	0.01
A001	1160	1190		7193	0.13	6.0	0.01	0.02	0.005	3.64	0.09
A001	1190	1220		7194	0.08	3.0	0.01	0.01	0.001	1.65	0.02
A001	1220	1250		7195	0.04	8.0	0.02	0.01	0.005	2.44	0.06
A001	1250	1280		7196	0.13	4.0	0.01	0.01	0.001	4.48	0.01
A001	1280	1310		7197	0.19	8.0	0.07	0.02	0.02	5.58	0.01
A001	1310	1340		7198	0.18	6.0	0.04	0.005	0.01	2.85	0.06
A001	1340	1370		7199	0.06	3.0	0.04	0.001	0.001	3.22	0.06
A001	1370	1400		7200	0.14	4.0	0.01	0.005	0.005	4.41	0.01
A001	1400	1416		7201	0.10	3.0	0.03	0.005	0.001	2.16	0.01
R	1416	1428	:DYKE - NO SAMPLE								
A001	1428	1460		7202	0.37	15.0	0.03	0.005	0.005	3.37	0.03
A001	1460	1490		7203	0.06	12.0	0.03	0.01	0.005	4.95	0.03
A001	1490	1520		7204	0.16	16.0	0.14	0.01	0.01	4.23	0.01
A001	1520	1550		7205	0.05	8.0	0.24	0.005	0.01	6.68	0.44
A001	1550	1580		7206	0.14	33.0	0.79	0.01	0.10	9.46	0.10
A001	1580	1610		7207	0.12	6.0	0.04	0.005	0.01	3.73	0.10
A001	1610	1640		7208	0.02	3.0	0.22	0.005	0.01	5.98	0.005
A001	1640	1670		7209	0.12	14.0	0.03	0.01	0.01	5.12	0.005
A001	1670	1700		7210	0.05	14.0	0.38	0.005	0.02	6.16	0.005
A001	1700	1730		7211	0.20	33.0	0.29	0.01	0.005	5.34	0.01
A001	1730	1760		7212	0.02	5.0	0.11	0.005	0.005	5.25	0.03
A001	1760	1790		7213	0.02	7.0	0.11	0.005	0.001	7.24	0.02
A001	1790	1820		7214	0.02	6.0	0.04	0.005	0.01	6.00	0.005
A001	1820	1850		7215	0.04	4.0	0.52	0.005	0.01	3.15	0.005
A001	1850	1880		7216	0.02	7.0	0.13	0.005	0.17	6.15	0.005
A001	1880	1910		7217	0.12	52.0	0.31	0.03	0.26	4.94	0.02
A001	1910	1940		7218	0.27	42.0	0.33	0.05	0.63	8.53	0.01
A001	1940	1953		7219	0.43	28.0	0.07	0.01	0.03	4.21	0.005
R	1953	1965	:DYKE - NO SAMPLE								
A001	1965	2000		7220	0.32	22.0	0.06	0.01	0.001	4.78	0.30
A001	2000	2030		7221	0.37	20.0	0.09	0.005	0.005	5.00	0.06
A001	2030	2060		7222	0.04	3.0	0.01	0.001	0.005	3.97	0.02
A001	2060	2090		7223	0.15	10.0	0.04	0.01	0.005	3.65	0.07
A001	2090	2120		7224	0.04	4.0	0.04	0.001	0.005	2.74	0.07
A001	2120	2150		7225	0.03	5.0	0.03	0.005	0.01	3.16	0.09
A001	2150	2170		7226	0.03	2.0	0.01	0.001	0.01	4.51	0.02
A001	2170	2195		7227	0.01	2.0	0.02	0.001	0.005	4.99	0.98
R	2195	2225	:DYKE - NO SAMPLE								
A001	2225	2255		7228	0.03	2.0	0.02	0.005	0.01	5.81	0.005
A001	2255	2285		7229	0.02	1.0	0.01	0.001	0.001	5.00	0.005
A001	2285	2304		7230	0.02	1.0	0.02	0.005	0.001	7.11	0.005
R			:EOH @ 230.4 M								
R			END OF ASSAYS - END OF LOG								

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IDEN6B0201      X86CH267 NQ   AUG86DJH   G&D AUG86S38           0.0
IPRJ          EQUITY SILVER MINES LTD        SUPERSTITION ZONE - ST GEOCODE
S000   00   434 MT  108.2 090.0 -45.0                5421.68   7507.98   1131.07
S001  434  1082     108.2 090.0 -44.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                      MSCLQZFYCPTTASPR
LNAM                                                      CBGY  MGHESLGLMO
/      00    52        OVBN                    P
R                :TRICONED - NO CORE
/      52    80  26    2C13CLMS   <<           P           <.<(<*<.
L                00        TG
R                :FE OXIDE ON FRACTS :MS AS << ENVELOPES
/      80   110  29    2C13CLMS   <<           P           <(<(<*
L                00        TG
R                :FE OXIDES ON FRACTS :MS AS << ENVELOPES
/     110   140  29    2C13CLMS   <<           P           <(<(<*
L                12        TG
R                :MINOR FE OXIDES :MS AS << ENVELOPES
/     140   170  27    2C13CLMS   <<           P           <(<(<*<.
L                11        TG
R                :MS ON << ENVELOPES
/     170   200  29    2C13CLMS   <<           P           <(<(<*<.
L                07        TG
R                :MS ON << ENVELOPES
/     200   230  28    2C13CLMS   <<           P           <(<(<*<.
L                02        TG
R                :MS AS << ENVELOPES
/     230   260  28    2C13CLMS   <<           P           <(<(<*<.
L                09        TG
R                :MS AS << ENVELOPES
/     260   290  29    2C13CLMS   <<           P           <(<(<*
L                04        TG
R                :MS AS << ENVELOPES
/     290   320  28    2C13CLMS   <<           P           <(<(<*<.
L                04        TG
R                :MS AS << ENVELOPES
/     320   350  28    2C13CLMS   <<           P           <(<*<*<.
L                18        TG
R                :MS AS << ENVELOPES
/     350   380  28    2C13CLMS   <<           P           <(<*<*<.
L                05        TG
R                :MS AS << ENVELOPES
/     380   402  12    2C13CLMS   <<           P           <(<*<*<.
L                00        TG
R                :8A 38.0 - 38.4 M :V RUBBLY INTERVAL :DIFFICULT TO TELL RX TYPE
/     402   428  19    2C65MSQZ   BR           P             #=##
L                00        5A
R                :FAULT ZONE - GOUGE RX TYPE UNCERTAIN :TECTONIC BXIA
/     428   474  42    8A02CLCB   P*           P
L                18        5G                                 D(
R                :NO CNTS OBSERVED DUE TO BADLY BROKEN CORE
/     474   500  25    2C35MSQZ   <<           P           <.<(<*<.
L                03        5T
R                :BADLY BROKEN UP
```

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/     500   530  29    2C25MSQZ   <<          P              0+0+
L                 09        5T
R                :PY + QZ ALSO IN << - STRANGE RX TYPE - POSSIBLE 2C55?
R                :MINOR GOUGE ZONES
/     530   560  30    2C35MSQZ   <<          P              <)<)
L                 22        5A
R                :TO 2D LOC
/     560   593  31    2C35MSQZ   <<          P              <)<)<.
L                 19        5T
R                :TO 2D LOC
/     593   626  32    VEINQZPY               P              V8V2
L                 24        AW
R                :A FEW SHORT SECTIONS OF 2C35 :NO CNT ATTITUDES POSSIBLE
/     626   650  23    2C35MSQZ   <<BR        P              <=<=
L                 12        5A
R                :TO 2C75 LOC
/     650   680  29    2C25MSQZ   <<          P            <.<)<)
L                 14        5A
R                :TO 2D LOC
/     680   710  29    2D25MSQZ   <<          P              <)<+
L                 21        5A
R                :TO 2C LOC
/     710   740  29    2D25MSQZ   <<          P              <)<)
L                 13        5A
R                :TO 2C65
/     740   770  27    2D25MSQZ   <<          P              <)<)
L                 15        5A
/     770   800  29    2D25MSQZ   <<          P              <)<)
L                 07        5A
/     800   820  18    2D25MSQZ   <<          P              <+<+
L                 10        5A
R                :TO 2D55 LOC
/     820   840  17    2C25MSQZ   <<          P              <)<)
L                 03        5T
/     840   858  15    8A02CL     A*          P CU   064     A(
L                 12        6G                 CL   075         A.
R                :CL AS A* ENVELOPES
/     858   889  31    2C25MSQZ   <<          P            <(<)<)
L                 04        5T
R                :TO 2C22 @ END OF INTERVAL W/ CL ON <<
/     889   937  45    8B02CLCB   P*A*        P TC   044
L                 38        4G                          A.       A.
R                :NO CNTS OBSERVED BUT PROBABLY // TO TC
/     937   970  31    2C25MSQZ   <<          P            <(<)<)<.
L                 14        5T
R                :TO 2C22 @ START OF INT :TO 2D LOC
/     970  1000  25    2C25MSQZ   <<          P              <)<)
L                 00        5T
R                :CORE HEAVILY BROKEN UP
/    1000  1033  31    2C25MSQZ   <<          P              <)<)
L                 04        5T
R                :V BROKEN UP CORE :TO 2C23 LOC
/    1033  1060  27    1D10QZ     <<          P              <*<*<.
L                 19        5A
/    1060  1082  20    2D25QZMS   <<          P              <)<)<.
```

L			08	5A							
R			:UPPER CNT GRADATIONAL OVER 0.2 M - ENTIRE INT MAY HAVE								
R			:QZ GRAINS (IE - COMFORMABLE TRANSITION ZONE)								
R			:EOH @ 108.2 :RODS STRUCK WHILE TRIPPING OUT OF HOLE -								
R			:BLASTED OFF								
R			:COLLAR LOCATION LOST WHILE MOVING DRILL (RE-POSITIONED								
R			:WITHIN 0.5 M RADIUS)								
A001											
ALAB			EQUITY MINESITE LABORATORY								
ATYP			ASSAY								
AMTH			WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST								
AUMM			RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	52	:TRICONED - NO CORE								
A001	52	80		7231		0.11	0.5	0.03	0.005	0.001	2.56	0.005
A001	80	110		7232		0.10	1.0	0.02	0.005	0.001	3.40	0.005
A001	110	140		7233		0.06	1.0	0.04	0.005	0.001	3.47	0.005
A001	140	170		7234		0.07	1.0	0.04	0.005	0.001	3.04	0.005
A001	170	200		7235		0.13	1.0	0.03	0.005	0.001	3.71	0.005
A001	200	230		7236		0.13	1.0	0.03	0.005	0.001	3.28	0.005
A001	230	260		7237		0.15	1.0	0.03	0.001	0.005	3.93	0.005
A001	260	290		7238		0.05	0.5	0.01	0.005	0.005	4.10	0.005
A001	290	320		7239		0.09	1.0	0.02	0.005	0.005	3.79	0.005
A001	320	350		7240		0.07	1.0	0.01	0.005	0.005	3.43	0.005
A001	350	380		7241		0.16	1.0	0.01	0.005	0.005	2.89	0.005
A001	380	402		7242		0.11	4.0	0.06	0.01	0.001	3.82	0.04
A001	402	428		7243		0.16	5.0	0.05	0.005	0.001	3.05	0.005
R	428	474	:DYKE - NO ASSAYS									
A001	474	500		7244		0.05	1.0	0.14	0.005	0.001	2.21	0.005
A001	500	530		7245		0.01	1.0	0.05	0.01	0.001	3.70	0.005
A001	530	560		7246		0.005	1.0	0.04	0.01	0.001	4.69	0.005
A001	560	590		7247		0.02	1.0	0.05	0.01	0.001	5.71	0.005
A001	590	620		7248		0.01	3.0	0.33	0.02	0.02	12.40	0.005
A001	620	650		7249		0.02	8.0	0.26	0.03	0.01	18.50	0.005
A001	650	680		7250		0.04	2.0	0.16	0.01	0.001	4.43	0.005
A001	680	710		7251		0.01	2.0	0.04	0.02	0.01	7.14	0.005
A001	710	740		7252		0.02	2.0	0.25	0.02	0.02	7.59	0.005
A001	740	770		7253		0.01	2.0	0.05	0.01	0.01	6.11	0.005
A001	770	800		7254		0.005	2.0	0.02	0.02	0.01	8.13	0.005
A001	800	820		7255		0.005	2.0	0.09	0.01	0.01	8.08	0.005
A001	820	840		7256		0.005	2.0	0.02	0.01	0.001	7.16	0.005
R	840	858	:DYKE - NO SAMPLE									
A001	858	889		7257		0.06	16.0	0.02	0.01	0.04	6.21	0.005
R	889	937	:DYKE - NO SAMPLE									
A001	937	970		7258		0.11	8.0	0.04	0.01	0.01	4.71	0.01
A001	970	1000		7259		0.05	2.0	0.04	0.01	0.001	5.25	0.005
A001	1000	1030		7260		0.07	2.0	0.06	0.005	0.01	2.89	0.02
A001	1030	1060		7261		0.19	1.0	0.01	0.005	0.001	1.73	0.005
A001	1060	1082		7262		0.08	3.0	0.03	0.005	0.001	2.67	0.005
R			:END OF ASSAYS - END OF HOLE									
R			:HOLE TERMINATED DUE TO STUCK RODS - BLASTED OFF @ 200 FT									
R			END OF ASSAYS - END OF LOG									

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IDEN6B0201      X86CH268 NQ   AUG86DJH   G&D AUG86S38          0.0
IPRJ          EQUITY SILVER MINES LTD       SUPERSTITION ZONE - ST GEOCODE
S000   00   729 MT   72.9 090.0 -45.0              5340.99   7399.62   1108.48
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                    MSCLQZPYCPTTASPR
LNAM                                                    CBGY  MGHESLGLMO
/      00   183        OVBN                  P
R                :TRICONED - NO CORE
/     183   210  22    2D13CLMS   <<         P           <.<*<*
L                  12       TG                        <.
R                :MS AS << ENVELOPES
/     210   240  28    2C13CLMS   <<         P           <(<*<*
L                  08       TG                        <.
R                :TO 2D LOC
/     240   270  25    2C13CLMS   <<         P           <.<(<(.
L                  05       TG                        <.
R                :HEAVILY BROKEN 25.3 - 27.0 M :TO 2C12 LOC :TO 2D LOC
/     270   300  15    2C12CL     <<         P           <.<.<.
L                  00       5G
R                :V HEAVILY BROKEN UP CORE :TO 2C13 LOC
/     300   323  10    2C12CL     <<         P           <(<(<(<(
L                  00       5G
R                :HEAVILY BROKEN UP CORE :TO 2C13 LOC :CP IN ONE SMALL VEINLET
R                :TO 2D LOC
/     323   351  07    2C24CLMS   <<         P             <.<.
L                  00       TG                        <(
R                :HEAVILY BROKEN UP INT :SAND SEAM REPORTED BY DRILLERS @ 34.1
/     351   374  21    2C24CLMS   <<         P           <(<*<*<(
L                  05       TG
R                :TO 2C12 LOC
/     374   393  19    8A02CLCB   A*         P
L                  10       4G                    A*
R                :NO CNTS OBSERVED :XENOLITH 2C23 W/ MINOR CP 38.3 - 38.6 M
/     393   420  22    2C12CL     <<         P           <(<*<*<(
L                  00       5G
R                :TO 2C13 LOC
/     420   450  24    2C12CL     <<         P           <(<(<(.
L                  00       5G
R                :TO 2C24 LOC
/     450   480  29    2C13CLMS   <<         P           <(<*<*<(
L                  02       TG
R                :ONE QZ + PY + CP VEIN
/     480   510  27    2C13CLMS   <<         P           <.<(<(.
L                  00       TG
R                :TO 2D LOC :TO 2C14 LOC
/     510   540  28    2C13CLMS   <<         P           <.<(<(.
L                  08       TG                        <(
R                :TO 2D LOC
/     540   570  29    2C13CLMS   <<         P           <(<(<(.
L                  06       TG                        <(
R                :TO 2C14 LOC
/     570   600  27    2C13CLMS   <<         P           <(<(<(.
L                  06       TG
R                :TO 2D LOC
```

```
/      600    632   29     2C23CLMS    <<          P            <(<(<(<.
L                   13         TG
R                  :TO 2C34 LOC
/      632    669   36     8A01CL      P*          P CU    060
L                   32         6G                  CL    075
R                  :POSSIBLY LATITE
/      669    700   31     2C13CLMS    <<          P            <(<*<(<.
L                   17         TG
R                  :TO 2C55 @ DYKE CNT
/      700    729   25     2C13CLMS    <<          P            <(<(<(
L                   02         TG
R                  :CLAY GOUGE & HEAVILY BROKEN CORE  72.4 - 72.9
R                  :EOH @ 72.9 M - COULDN'T GET THROUGH FAULT ZONE
A001
ALAB               EQUITY MINESITE LABORATORY
ATYP               ASSAY
AMTH               WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM               RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R       00   183  :TRICONED - NO CORE
A001    183  210        7075        0.05    1.0 0.03  0.01  0.001 2.83  0.005
A001    210  240        7076        0.06    1.0 0.02  0.01  0.001 3.04  0.005
A001    240  270        7077        0.07    1.0 0.02  0.01  0.001 3.34  0.005
A001    270  300        7078        0.07    1.0 0.04  0.01  0.001 3.90  0.005
A001    300  323        7079        0.14    6.0 0.06  0.02  0.01  6.65  0.01
A001    323  351        7080        0.04    0.5 0.06  0.005 0.001 2.12  0.005
A001    351  374        7121        0.13    1.0 0.01  0.005 0.001 2.85  0.005
R       374  393  :DYKE - NO SAMPLE
A001    393  420        7122        0.12    1.0 0.04  0.01  0.001 4.67  0.02
A001    420  450        7123        0.13    2.0 0.03  0.01  0.001 4.06  0.005
A001    450  480        7124        0.13    1.0 0.03  0.01  0.001 3.28  0.005
A001    480  510        7125        0.08    1.0 0.03  0.005 0.001 2.80  0.005
A001    510  540        7126        0.09    1.0 0.04  0.01  0.001 2.87  0.005
A001    540  570        7127        0.04    1.0 0.02  0.01  0.001 2.50  0.01
A001    570  600        7128        0.10    1.0 0.04  0.01  0.001 3.31  0.005
A001    600  632        7129        0.03    0.5 0.01  0.01  0.001 2.30  0.005
R       632  669  :DYKE - NO SAMPLE
A001    669  700        7130        0.03    1.0 0.01  0.01  0.001 3.31  0.005
A001    700  729        7131        0.03    1.0 0.05  0.01  0.001 2.80  0.005
R                  :END OF HOLE - COULDN'T GET THROUGH SAND SEAM
R                  END OF ASSAYS - END OF LOG
```

```
IDEN6B0201      X86CH269 NQ   AUG86DJH   G&D AUG86S38          0.0
IPRJ          EQUITY SILVER MINES LTD        SUPERSTITION ZONE - ST GEOCODE
S000   00   364 MT   72.9 090.0 -45.0              5309.99   7554.41   1137.79
S001  364   729      72.9 090.0 -42.0
/SCL        MT.2MT.1
LSCL            MT.2
/NAM                                                      MSCLQZPYCPTTASPR
LNAM                                                      CBGY  MGHESLGLMO
/      00   152        OVBN                    P
R                :TRICONED - NO CORE
/     152   180  26    2C24MSCL   <<           P           <.<*<*<.
L                  09        GT                          <(
R                :TO 2D LOC
/     180   210  29    2C24MSCL   <<           P           <.<)<)<.
L                  02        GT                          <*
R                :TO 2C45 LOC :TO 2D LOC
/     210   240  30    2C24MSCL   <<           P           <.<+<+
L                  04        GT
R                :TO 2D LOC :NUMEROUS QZ + PY VEINLETS :LOOKS LIKE A TRACE OF
R                :NATIVE CU? ON FRACTS
/     240   270  30    2C24MSCL   <<           P           <.<+<+
L                  16        GT                          <*
R                :TO 2C25 LOC
/     270   297  26    2C24MSCL   <<           P           <.<)<)<.
L                  06        GT
/     297   317  19    2C24MSCL   <<           P           <.<*<*
L                  04        GT
R                :TO 2D LOCALLY :QZ + FY VEIN 29.7 - 30.2
/     317   348  27    2C24MSCL   <<           P           <.<)<)
L                  02        GT
R                :TUBE DIDN'T LOOK @ 33.5 M
/     348   380  30    2C24MSCL   <<           P           <.<*<*<.
L                  06        GT
/     380   410  27    2C55MS     BR<<         P             #)#+
L                  18        5T
R                :2C24 TO 39.0 M :PY + QZ V/ 40.8 - 41.0 (CONT'D NEXT INT)
/     410   430  18    2C35MSQZ   <<           P             <)<)
L                  04        5A
R                :TO 2C55 LOC :30% QZ + PY - VEINS? PODS?
/     430   460  07    2C35MSQZ   <<           P             <)<)
L                  00        5T
R                :TUBE DIDN'T LOOK @ 46.0 M :HEAVILY BROKEN UP CORE
R                :60% QZ + PY VEINS?/PODS?
/     460   490  28    2C24MSCL   <<           P           <.<(<(
L                  07        GT
R                :TO 2C23 LOC
/     490   520  30    2C13CLMS   <<           P           <(<(<(
L                  11        TG
/     520   550  28    2C34MSCL   <<           P           <(<)<)<.
L                  12        GT
R                :TO 2C33 LOC
/     550   561  10    2C24MSCL   <<           P           <.<*<*
L                  00        GT
/     561   578  16    BA02CL     A*FB         P FB   025
L                  14        5G
```

R			:NO CNTS OBSERVED									
/	578	600	20	2C14CLMS	<<		P		<.<*<*			
L			00	TG								
/	600	630	28	2C14CLMS	<<		P		<.<*<(			
L			03	TG								
/	630	660	29	2C13CLMS	<<		P		<(<*<(<.			
L			05	TG								
/	660	690	25	2C13CLMS	<<		P		<(<(<(			
L			03	TG								
/	690	729	23	2C14CLMS	<<		P		<(<(<*			
L			02	TG								
R			:TO 2C24 LOC									
R			:EOH @ 72.9 M									
A001												
ALAB			EQUITY MINESITE LABORATORY									
ATYP			ASSAY									
AMTH			WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST									
AUMM			RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN	
R	00	152	:TRICONED - NO CORE									
A001	152	180		7132	0.15	1.0	0.01	0.005	0.001	2.00	0.005	
A001	180	210		7133	0.10	2.0	0.03	0.01	0.001	3.46	0.005	
A001	210	240		7134	0.03	3.0	0.04	0.02	0.001	14.50	0.02	
A001	240	270		7135	0.08	5.0	0.04	0.02	0.001	6.80	0.25	
A001	270	297		7136	0.11	2.0	0.02	0.005	0.001	3.13	0.01	
A001	297	317		7137	0.07	4.0	0.10	0.005	0.001	14.90	0.005	
A001	317	348		7138	0.03	2.0	0.02	0.001	0.001	2.52	0.005	
A001	348	380		7139	0.02	2.0	0.01	0.001	0.001	6.69	0.005	
A001	380	410		7140	0.001	0.1	0.02	0.001	0.001	5.63	0.001	
A001	410	430		7141	0.001	0.5	0.03	0.005	0.001	11.95	0.001	
A001	430	460		7142	0.005	5.0	0.20	0.005	0.001	18.30	0.001	
A001	460	490		7143	0.07	0.5	0.02	0.005	0.001	2.13	0.001	
A001	490	520		7144	0.05	0.5	0.02	0.001	0.001	2.87	0.001	
A001	520	550		7145	0.07	0.5	0.01	0.001	0.001	2.80	0.005	
A001	550	561		7146	0.03	0.5	0.01	0.001	0.001	3.30	0.005	
R	561	578	:DYKE - NO SAMPLE									
A001	578	600		7147	0.03	0.5	0.01	0.001	0.001	3.96	0.005	
A001	600	630		7148	0.06	0.5	0.01	0.001	0.001	1.63	0.005	
A001	630	660		7149	0.02	0.5	0.01	0.001	0.001	2.96	0.005	
A001	660	690		7150	0.03	0.5	0.01	0.001	0.001	3.18	0.005	
A001	690	729		7151	0.03	0.5	0.01	0.001	0.001	1.86	0.005	
R			:EOH @ 72.9 M									
R			END OF ASSAYS - END OF LOG									

```
IDEN6B0201      X86CH270 NQ   AUG86DJHRBPG&D AUG86S38          0.0
IPRJ         EQUITY SILVER MINES LTD         SUPERSTITION ZONE - ST GEOCODE
S000   00   535 MT  119.5 090.0 -45.0              5186.05   7440.19   1110.85
S001  535  1195     119.5 090.0 -43.0
/SCL        MT.2MT.1
LSCL            MT.2
/NAM                                                    MSCLQZPYCPTTASPR
LNAM                                                    CBGY  MGHESLGLMO
/      00   122        OVBN                    P
R                :TRICONED - NO CORE
/     122   150  23    2D13CLMS   <<           P          <(<(<*
L                  00        TG
R                :MINOR MS SERICITE ALT'N :TO 2C LOC
/     150   180  28    2D13CLMS   <<           P          <(<(<*
L                  05        TG
R                :V WEAK MS ALT'N :TO 2D12 LOC
/     180   210  26    2D13CLMS   <<           P          <(<(<*
L                  02        TG                       <.
R                :V WEAK MS ALT'N TO 2D12 LOC
/     210   240  29    2D13CLMS   <<           P          <.<.<(
L                  09        TG
R                :V WEAK MS ALT'N AS << ENVELOPES :AMYGDALOIDAL 8C  22.0 - 22.4
R                :AND 23.3 - 23.8 M W/ DISS MG
/     240   270  30    2D13CLMS   <<           P          <.<(<*
L                  04        TG
R                :V WEAK MS ALT'N AS << ENVELOPES :TO 2C LOC
/     270   300  27    2D13CLMS   <<           P          <.<(<*
L                  03        TG
R                :TO 2C LOC :TUBE DIDN'T LOOK @ 27.4 M
/     300   330  29    2D12CL     <<           P          <.<(<*
L                  03        4G
R                :TO 2D13 LOC :BORDERLINE CALL BETWEEN 2C & 2D
/     330   360  27    2D13CLMS   <<           P          <.<(<*
L                  00        TG
R                :TO 2D25 LOC
/     360   390  24    2D12CL     <<           P          <.<.<(
L                  00        4G                       <.
R                :TO 2D13 LOC
/     390   420  24    2C12CL     <<           P          <.<(<*
L                  00        4G                       <.
R                :TO 2C13LOC
/     420   450  23    2C12CL     <<           P          <.<.<.
L                  00        4G                       <.
/     450   475  20    2C13CLMS   <<           P          <.<.<.
L                  00        TG
R                :MINOR 8B FROM 46.6 - 47.5 M :TO 2C15 LOC
/     475   506  22    8C11CLCY   P*<<         P                <.
L                  00        9G                    <.
R                :NO CNT ATTITUDES OBSERVED
/     506   548  42    8A12CL     P*<<         P
L                  05        AG                    <.     D.
R                :V WEAK << TEXT
/     548   580  30    2C34CLMS   <<           P             <=<(<.
L                  07        TG
/     580   610  27    2C24CLMS   <<           P             <(<(
```

```
L                 03        TG
R                :TO 2C25 LOC
/      610   640  26    2C24CLMS   <<          P              <+<(<.<.
L                 00        TG                                  <)<-
R                :NO POS ID ON TT, BUT SUSPECT IN << WITH HE
/      640   670  20    2C24CLMS   <<          P              <=<+<-<-
L                 00        TG
R                :POOR RECOV FROM 64.3 TO 65.5
/      670   700  27    2C39QZ     <<BR        P              <)<)<-<(
L                 03        TA                                    <(
R                :MINOR BR'X.  ,LOC 2C24
/      700   730  27    2C59QZ     BR<<        P              <)<)<-<*
L                 04        TA                                    <)
R                :TT-SL BR'X AT 71.0
/      730   760  29    2C44MSCL   <<          P              <*<+<.<(
L                 00        AT                                    <*
/      760   790  26    2C34MSCL   <<BR        P              <*<+<-<-
L                 00        AT                          <-        <.
R                :MINOR BR'X
/      790   820  15    2C34MSCL   <<          P              <*<+<.<-
L                 00        AT                          <-        <-
R                :POOR RECOV
/      820   850  14    2C34MSCL   <<BR        P              <)<)<.<.
L                 00        AT                                    <.
R                :POOR RECOV
/      850   880  29    2C59QZ     <<BR        P              +1+=  #+<-
L                 09        TA                                    #)
/      850   850       X                                      #1  #4
L                                                                  #2
R                :TT-PY-SL BR'X FROM 85.0 TO 85.2, TT ALSO OCCURS IN << IN
R                :REST OF INTERVAL
/      880   920  11    2C23CL     <<          P              V+<)
L                 00        AG
R                :TERRIBLE RECOVERY
/      920   950  27    2C45       <<BR        P              V+#+  ###-
L                 03                                               ##
R                :TT-PY-QZ BR'X AT 94.8
/      950   980  29    2C33CLMS   <<          P              <)<)  <.
L                 11        GT                          <-        <.
/      980  1010  30    2C22CL     <<          P            <(<(<*
L                 15        TG                          <-
/     1010  1040  29    2C12CL     <<          P            <*<*<*
L                 09        TG
/     1040  1070  11    2C23CLMS   <<          P            <*<)<*
L                 03        GT
R                :TERRIBLE RECOV
/     1070  1100  29    2C22CL     <<          P            <(<(<*
L                 08        AG
/     1100  1130  29    2C12CL     <<          P            <(<*<(
L                 03        AG
R                :LOC 2C33
/     1130  1160  29    2C12CL     <<          P            <(<(<(
L                 09        AG
R                :MINOR 2D AT 114.8
/     1160  1195  33    2C22CLMS   <<          P            <(<*<*
```

L			03	AG							
R			:LOC 2C23								
R			:END OF HOLE AT 119.5								
A001											
ALAB			EQUITY MINESITE LABORATORY								
ATYP			ASSAY								
AMTH			WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST								
AUMM			RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	122	:TRICONED - NO CORE								
A001	122	150	7152	0.02	0.5	0.01	0.001	0.001	4.03	0.005	
A001	150	180	7153	0.02	0.5	0.01	0.001	0.001	3.61	0.005	
A001	180	210	7154	0.02	0.5	0.02	0.005	0.001	4.09	0.005	
A001	210	240	7155	0.005	0.5	0.01	0.005	0.001	3.80	0.005	
A001	240	270	7156	0.005	0.5	0.01	0.001	0.001	3.22	0.005	
A001	270	300	7157	0.02	0.5	0.01	0.001	0.001	3.51	0.005	
A001	300	330	7158	0.02	0.1	0.01	0.001	0.001	4.35	0.005	
A001	330	360	7159	0.02	0.1	0.01	0.001	0.001	3.84	0.005	
A001	360	390	7160	0.005	0.1	0.03	0.001	0.001	4.71	0.005	
A001	390	420	7263	0.02	0.1	0.02	0.001	0.001	4.77	0.001	
A001	420	450	7264	0.02	0.1	0.04	0.001	0.001	4.13	0.001	
A001	450	475	7265	0.005	0.5	0.02	0.001	0.001	3.52	0.001	
R	475	548	:DYKE - NO SAMPLES								
A001	548	580	7266	0.03	4.0	0.03	0.001	0.09	5.69	0.001	
A001	580	610	7267	0.04	0.1	0.02	0.001	0.005	3.81	0.02	
A001	610	640	7268	0.43	15.0	0.03	0.03	0.06	4.57	0.13	
A001	640	670	7269	0.10	3.0	0.03	0.001	0.005	6.17	0.03	
A001	670	700	7270	0.12	11.0	0.03	0.005	0.005	3.74	0.08	
A001	700	730	7271	0.39	88.0	0.34	0.13	0.34	5.01	0.62	
A001	730	760	7272	0.35	24.0	0.08	0.07	0.04	4.32	0.40	
A001	760	790	7273	0.10	2.0	0.06	0.005	0.005	2.94	0.10	
A001	790	820	7274	0.07	2.0	0.12	0.005	0.02	4.76	0.08	
A001	820	850	7275	0.32	69.0	0.19	0.09	0.07	5.61	0.37	
A001	850	880	7276	0.38	167.0	0.32	0.15	0.60	10.13	3.00	
A001	880	920	7277	0.005	0.1	0.08	0.001	0.10	5.71	0.001	
A001	920	950	7278	0.11	19.0	0.25	0.14	0.37	10.58	0.52	
A001	950	980	7279	0.02	0.5	0.02	0.001	0.001	5.47	0.005	
A001	980	1010	7280	0.07	0.5	0.04	0.001	0.001	3.82	0.03	
A001	1010	1040	7281	0.05	0.1	0.03	0.001	0.001	4.92	0.001	
A001	1040	1070	7282	0.03	0.1	0.01	0.001	0.001	3.48	0.001	
A001	1070	1100	7283	0.05	0.1	0.01	0.001	0.001	4.62	0.001	
A001	1100	1130	7284	0.03	0.1	0.01	0.001	0.001	2.81	0.001	
A001	1130	1160	7285	0.05	0.1	0.01	0.001	0.001	3.06	0.001	
A001	1160	1195	7286	0.05	0.1	0.05	0.001	0.001	3.16	0.001	
R			:END OF HOLE - END OF ASSAYS								
R			END OF ASSAYS - END OF LOG								

```
IDEN6B0201       X86CH271 NQ   AUG86RBP   G&D AUG86S3B            0.0
IPRJ          EQUITY SILVER MINES LTD        SUPERSTITION ZONE - ST GEOCODE
S000   00   514 MT  189.9 090.0 -75.0                5339.84   7431.17   1113.81
S001  514  1347     189.9 090.0 -78.0
S002 1347  1899     189.9 090.0 -74.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                          MSCLQZPYCPTTASPR
LNAM                                                          CBGY  MGHESLGLMO
/      00    91         OVBN                    P
R                 :TRICONED - NO CORE
/      91   140  28     2C11CL      <<          P            <(<*<(<.
L                 00         AG
R                 :POOR RECOVERY, VERY BROKEN.
/     140   170  27     2C13CL      <<          P            <.<*<(<.
L                 02         AG
R                 :VERY MINOR QTZ-SER ALT-N.
/     170   200  20     2C13CL      <<          P            <(<-<*
L                 00         TG
R                 :VERY BROKEN
/     200   230  28     2C23CLMS    <<          P            <(<(<*<-
L                 05         TG
R                 :LOC 2C33
/     230   270  28     2C23GLMS    <<          P            <*<(<(<.
L                 00         TG
R                 :POOR RECOVERY
/     270   300  29     2C12CL      <<          P            <(<-<(
L                 00         AG
/     300   330  27     2C12CL      <<          P            <(<(<-
L                 00         AG
R                 :LOC 2C23
/     330   380  24     2C22CL      <<          P              <(<-
L                 00         GA
R                 :SOME CORE VERY FRACTURED, ALL BROKEN, SUSPECT FAULT ZONE
R                 :BUT NO CLAY GOUGE.
/     380   410  28     2C12CL      <<          P            <*<)<(<.
L                 03         AG
R                 :LOC 2C13
/     410   440  29     2C12CL      <<          P            <*<(<-
L                 00
R                 :ABUNDANT SHARDS
/     440   470  29     2C12CL      <<          P            <*<(<-
L                 05         GA                          <-
R                 :LOC 2C13
/     470   500  29     2C12CL      <<          P            <(<*<(<-<.
L                 08         GA
R                 :LOC 2C13. LOW ALT'N AND FRACTURING, BUT A BIT OF MINERAL
/     500   513  12     2C12CL      <<BR        P            <*<-<(
L                 03         GA
R                 :QTZ-PY BR'X FROM 51.1 TO 51.3
/     513   541  27     8C00FL      P*CM        P CU    50
L                 17         TW                  CL    80
/     541   570  27     2C23CLMS    <<          P              <)<+<=
L                 00         TG                          <-
R                 :LOC 2C25
```

```
/     570   600   25    2C22CL     <<          P          <+<(<(
L                 00       AG                          <*
/     600   640   25    2C22CL     <<          P          <=<(<(
L                 00       AG
/     640   670   27    2C12CL     <<          P          <)<*<(
L                 00       AG                          <-
/     670   700   29    2C12CLMS   <<          P          <-<)<)
L                 09       AG
R                :LOC 2C13
/     700   730   30    2C12CLMS   <<          P          <-<)<*<.
L                 21       AG
R                :LOC 2C13. FIRST REASONABLY SOLID CORE INTERVAL. TRACE CP
/     730   760   30    2C22CLMS   <<          P          <-<*<*<.
L                 12       AG
R                :LOC 2C23
/     760   790   30    2C22CLMS   <<          P          <-<)<*<.
L                 12       TG
R                :LOC 2C23, CLOSER TO BOTTOM OF INTERVAL
/     790   820   27    2C22CLMS   <<          P          <-<*<(
L                 09       AG
R                :LOC 2C23
/     820   850   30    2C22CL     <<          P          <(<)<(<-
L                 11       AG
R                :LOC 2C23
/     850   880   30    2C22CLMS   <<          P BD   50  <-<(<-<.
L                 17       AG
R                :LOC 2C32 AND 2C23
/     880   910   30    2C29QZ     <<          P            <*<(  <.
L                 06       7A
R                :TT IN ONE << AT 89.4
/     910   929   19    2C33CLMS   <<          P          <-<+<)
L                 03       GT
/     929   953   24    2C89QZPY   BR          P            #5#2
L                 07       AW
R                :QTZ-PY-2C BR'X
/     953   960   07    8C11FL     <<CM        P            <*
L                 05       GW                   CL   60
/     960   961   01    2C89QZPY   BR          P            #8#1
L                 01       AW
/     961   969   08    8B11FL     <<P*        P CU   60    <*
L                 05       AG     CM             CL   40
/     969  1000   31    2C54MS     BR<<        P            #1#=
L                 18       TA
R                :BR'X LESS INTENSE TOWARDS BOTTOM OF INTERVAL
/    1000  1030   30    2C54MS     BR<<        P            #=#=
L                 13       TA
R                :QTZ-PY IN << AS WELL
/    1030  1060   30    2C54MS     BR<<        P            #+#+
L                 06       TA
/    1060  1090   30    2C55MS     BR<<        P            #1#+  #?
L                 00       TA
/    1090  1120   29    2C44MS     <<BR        P            <*<)
L                 00       TA
R                :MINOR BR'X, LOC 2D
/    1120  1150   28    2C45MS     <<BR        P            <)<)
```

```
L                 03        AT
/    1150  1190   31    2C35MS      <<          P              B+<)
L                 03        3T
/    1190  1224   32    2C39QZ      <<          P              <*<)<-<.
L                 14        6A
R                :TT OCCURS AROUND 121.0
/    1224  1263   39    8B11CL      <<TC        P              <*
L                 28        2A      CM            CL    70
/    1263  1290   25    2C39QZ      <<BR        P              <+<)
L                 00        6A
R                :SMALL BR'X UNDER DYKE. GRADES INTO 2C34
/    1290  1320   25    2C34MS      <<          P              <)<)<.<-
L                 00        AT                                    <-
R                :TT-SL IN ONE << AT 130.0
/    1320  1350   28    2C34MS      <<          P              <)<*<(
L                 00        AT
/    1350  1380   29    2C33CLMS    <<          P              <)<(<(
L                 06        AT
/    1380  1405   23    2C22MSCL    <<          P              <)<(
L                 09        AT
R                :LOC 2C33
/    1405  1440   27    2C23MSCL    <<          P              <)<(  <-
L                 00        AT                                    <.
/    1440  1470   27    2C22CL      <<          P              <)<*  <?
L                 00        TA                                    <-
/    1470  1496   20    2C22CLCY    <<          P              <*<(
L                 00        TA
R                :CLAY RICH FAULT GOUGE
/    1496  1530   33    2E26MS      <<          P                B=  D(
L                 11        AW                                     D(
R                :STRANGE ROCK. COULD BE FLOW INTENSELY ALT'D TO SERICITE
/    1530  1560   29    2E26MS      <<          P              <*B=<-D-
L                 17        AW                                     D(
R                :AS ABOVE
/    1560  1590   30    2E26MS      <<          P                D=  D(
L                 15        AW                                   D-D-
R                :AS ABOVE
/    1590  1620   30    2E26MSCL    <<          P                D=D.D.
L                 21        AW                                   D(D.
R                :AS ABOVE, SOME CL RIMS ON LAPILLI
/    1620  1643   23    2E12CL      <<          P                D*
L                 13        GW
R                :ALT'N ?
/    1643  1650   07    8B01FL      P*          P CU    75
L                 03        TA                  CL    75
/    1650  1662   12    2E12CL      <<          P                D*
L                 06        GW
/    1662  1725   20    2C22CLCY    <<          P F/             D*
L                 00        GA
R                :FAULT ZONE, POOR RECOVERY
/    1725  1750   24    2C12CL      <<          P              <*<(
L                 03        TA
R                :LOC 2C23
/    1750  1780   28    2C22CL      <<          P              <+<(<-
L                 00        TA
```

```
/     1780   1800   19     2C22CL      <<          P              <+<(
L                   00        TA
/     1800   1829   28     2C22CL      <<          P              <+<(<.
L                   00        TA
/     1829   1840   11     8B01CL      <<TC        P CU     70    <(
L                   04        5G      CM            CL     75      D-
/     1840   1870   28     2C42CLMS    <<BR        P              <+<*<-
L                   00        TA
R                  :LOC 2C43, MINOR BR'X
/     1870   1899   27     2C32CL      <<          P              <*<(
L                   00        TA
R                  :END OF HOLE AT 189.9. WOULD HAVE LIKED TO DRILL INTO GREENER
R                  :ROCK, BUT WE WERE PAST THE TARGET
A001
ALAB               EQUITY MINESITE LABORATORY
ATYP               ASSAY
AMTH               WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM               RCOVSAMPLE   ROD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R       00     91  :TRICONED - NO CORE
A001    91    140        7287        0.100    1.0 0.020 0.005 0.001 3.060 0.005
A001   140    170        7288        0.07     0.5 0.03  0.001 0.001 2.54  0.005
A001   170    210        7289        0.11     1.0 0.02  0.005 0.001 3.60  0.01
A001   210    240        7290        0.12     1.0 0.01  0.005 0.001 3.16  0.01
A001   240    270        7291        0.05     0.1 0.02  0.005 0.001 2.67  0.005
A001   270    300        7292        0.12     0.5 0.02  0.005 0.001 3.23  0.005
A001   300    330        7293        0.14     0.5 0.04  0.001 0.001 4.41  0.005
A001   330    380        7294        0.09     1.0 0.02  0.005 0.001 3.26  0.005
A001   380    410        7295        0.07     1.0 0.04  0.001 0.001 2.82  0.03
A001   410    440        7296        0.04     1.0 0.03  0.005 0.001 2.85  0.01
A001   440    470        7297        0.04     0.5 0.02  0.005 0.001 2.70  0.005
A001   470    500        7298        0.08     1.0 0.02  0.005 0.001 3.02  0.01
A001   500    513        7299        0.05     1.0 0.03  0.001 0.001 3.36  0.01
R      513    541  :DYKE - NO SAMPLE
A001   541    570        7300        0.06     1.0 0.05  0.001 0.001 4.14  0.005
A001   570    600        7301        0.05     1.0 0.02  0.005 0.001 3.33  0.005
A001   600    640        7302        0.04     1.0 0.02  0.005 0.001 2.92  0.005
A001   640    670        7303        0.06     1.0 0.01  0.01  0.001 2.69  0.005
A001   670    700        7304        0.07     0.5 0.02  0.005 0.001 2.47  0.01
A001   700    730        7305        0.09     0.5 0.02  0.005 0.001 2.40  0.001
A001   730    760        7306        0.06     0.5 0.02  0.001 0.001 2.65  0.005
A001   760    790        7307        0.07     0.5 0.02  0.005 0.001 1.96  0.001
A001   790    820        7308        0.04     1.0 0.02  0.005 0.005 3.24  0.005
A001   820    850        7309        0.10     0.5 0.02  0.005 0.001 2.56  0.005
A001   850    880        7310        0.09     0.5 0.02  0.005 0.005 2.55  0.001
A001   880    910        7311        0.07     0.5 0.01  0.005 0.001 1.09  0.005
A001   910    929        7312        0.05     1.0 0.01  0.005 0.001 3.04  0.02
A001   929    953        7313        0.001    3.0 0.11  0.005 0.01 13.88  0.005
R      953    969  :DYKE - NO SAMPLE
A001   969   1000        7314        0.03     5.0 0.07  0.01  0.001 4.17  0.02
A001  1000   1030        7315        0.005    2.0 0.06  0.005 0.001 5.52  0.005
A001  1030   1060        7316        0.005    0.5 0.03  0.005 0.001 2.27  0.001
A001  1060   1090        7317        0.005    0.5 0.02  0.005 0.001 2.57  0.001
A001  1090   1120        7318        0.005    1.0 0.02  0.001 0.001 2.48  0.001
A001  1120   1150        7319        0.02     3.0 0.02  0.005 0.001 2.97  0.001
A001  1150   1190        7320        0.01     0.5 0.03  0.01  0.01  3.05  0.001
```

A001	1190	1224		7321	0.13	15.0	0.05	0.03	0.02	3.92	0.01
R	1224	1263	:DYKE - NO SAMPLE								
A001	1263	1290		7322	0.09	4.0	0.02	0.005	0.01	3.12	0.005
A001	1290	1320		7323	0.05	3.0	0.12	0.001	0.05	2.06	0.22
A001	1320	1350		7324	0.12	5.0	0.02	0.005	0.01	1.73	0.07
A001	1350	1380		7325	0.09	4.0	0.02	0.01	0.01	1.96	0.04
A001	1380	1405		7326	0.05	3.0	0.02	0.005	0.01	1.66	0.03
A001	1405	1440		7327	0.06	2.0	0.06	0.01	0.08	1.68	0.42
A001	1440	1470		7328	0.03	1.0	0.02	0.001	0.01	1.32	0.07
A001	1470	1500		7329	0.04	3.0	0.02	0.005	0.01	2.48	0.06
A001	1500	1530		7330	0.02	6.0	0.16	0.005	0.03	3.99	0.47
A001	1530	1560		7331	0.08	8.0	0.11	0.005	0.08	5.34	0.35
A001	1560	1590		7332	0.08	7.0	0.17	0.005	0.15	5.80	0.73
A001	1590	1620		7333	0.04	1.0	0.03	0.001	0.01	3.66	0.01
A001	1620	1643		7334	0.001	0.5	0.01	0.001	0.001	2.12	0.005
R	1643	1650	:DYKE - NO SAMPLE								
A001	1650	1673		7335	0.001	0.5	0.03	0.01	0.01	3.13	0.005
A001	1673	1716		7336	0.02	1.0	0.07	0.005	0.04	5.89	0.005
A001	1716	1750		7337	0.04	1.0	0.03	0.005	0.01	1.85	0.06
A001	1750	1780		7338	0.06	2.0	0.03	0.01	0.01	1.76	0.18
A001	1780	1800		7339	0.04	1.0	0.05	0.001	0.01	2.05	0.19
A001	1800	1829		7340	0.09	3.0	0.07	0.005	0.001	1.81	0.01
R	1829	1840	:DYKE - NO SAMPLE								
A001	1840	1870		7341	0.03	2.0	0.01	0.005	0.02	2.27	0.01
A001	1870	1899		7342	0.02	2.0	0.03	0.005	0.01	2.48	0.01
R			:END OF HOLE - END OF SAMPLES								
R			END OF ASSAYS - END OF LOG								

```
IDEN6B0201      X86CH272 NQ   AUG86RBPDJHG&D AUG86S38          0.0
IPRJ          EQUITY SILVER MINES LTD         SOUTH OF S. TAIL - ST GEOCODE
S000   00   914 MT  266.7 090.0 -45.0                5939.73   7480.12   1201.18
S001  914  1713     266.7 090.0 -45.0
S002 1713  2667     266.7 090.0 -45.0
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                        MSCLQZPYCPTTASPR
LNAM                                                        CBGY  MGHESLGLMO
/      00   122        OVBN                    P
R                 :TRICONED - NO CORE
/     122   186  20    3G11CL     <<           P              <(<-
L                 00        AG
R                 :VERY BROKEN, RUSTY. NO RECOVERY AT ALL FROM 13.6 TO 14.2
/     186   220  20    3G11CL     <<           P C/    70     <(<*
L                 00        AG                  BD    70
R                 :LOC 3D, POOR RECOV
/     220   293  25    3H11CL     <<
L                 00        AG                 P              <(<)
R                 :POOR RECOV, LOC 3G
/     293   332  23    3G11CL     <<           P              <-<*
L                 00        AG
R                 :POOR RECOV, VERY BROKEN, SUSPECT CHIPS FROM FARTHER UP HOLE
/     332   367  20    3H11CL     <<BR         P              <-<*
L                 00        AG
R                 :SOME 3H MAYBE BRECCIA. RUST ON FRACTURES ENDS
/     367   395  27    8C11FL     <<P*         P              <(
L                 13        GW
R                 :CONTACTS NOT PRESERVED
/     395   431  23    3H11CL     <<           P                <*
L                 00        AG
R                 :FAULT GOUGE AT 41.0. LOC 3H21
/     431   463  29    3A21QZPY   <<           P           <-  <*
L                 03        AW
/     463   492  29    3B11QZ     <<           P           <-<(<*
L                 13        AW
R                 :OCCASIONAL CHERT CLAST
/     492   540  33    3A21QZ     <<           P           <-<-<*
L                 06        AW
R                 :TYPICAL 3A, CLASTS UP TO 2.0 CM, SOMETIMES CLAST BORDERS
R                 :INDISTINCT. 3A-3B CONTACT GRADATIONAL
/     540   553  11    3B11QZ     <<           P
L                 03        GA
/     553   580  25    3A11QZ     <<           P           <-<-<(<.
L                 15        AW
R                 :CLASTS SOMETIMES INDISTINCT, ONE TINY SPOT OF CP IN <<
/     580   610  28    3A11QZ     <<           P           <-<(<*
L                 13        AW
R                 :LOC 3B AND 3F INTERBEDDED. BLACK TARNISH ON SOME PY
/     610   640  28    3A21QZ     <<           P           <-<*<)
L                 09        AW
/     640   670  28    3A21QZ     <<           P           <-<-<)  <?
L                 08        AW
R                 :POSSIBLE TT IN <<
/     670   719  41    3A11QZ     <<           P           <-<-<)<.<.
```

```
L                09        AW
R               :8A FROM 68.0 TO 68.2. LOWER CONTACT GRADATIONAL OVER 0.3 M
/     719   760  39    2C22CLMS   <<          P          <*<(<*
L                09        TG
R               :LOC 2C23
/     760   790  30    2C22CLMS   <<          P          <*<)<)
L                14        TG
R               :LOC 2C23, 2C24
/     790   820  30    2C12CLMS   <<          P          <*<)<)<.<-
L                18        TG
R               :LOC 2C23
/     820   850  30    2C22CLMS   <<          P          <(<)<*<(
L                14        TG
R               :LOC 2C23, 2C24. CP IN ONE << AT 82.6
/     850   880  29    2C33CLMS   <<          P          <-<*<=<-<.
L                09        GT
R               :LOC 2C22
/     880   910  30    2C23MSCL   <<          P          <(<)<+
L                11        GT
R               :LOC 2C22
/     910   938  28    2C23MSCL   <<          P          <-<)<)<-<?
L                06        GT                                  <.
R               :LOC 2C22, 2C24. TT IN <<, COULD BE SPECULARITE
/     938   976  38    3A20QZ     <<          P            <*<)<-
L                05        AW                                  <.
R               :LOWER CNT NOT OBSERVED DUE TO BROKEN UP CORE
/     976  1000  22    2C23CLMS   <<          P          <(<)<)<-
L                11        TG
R               :TO 2C24 LOC :CL ALSO AS << ENVELOPES
/    1000  1030  30    2C24MSCL   <<          P          <-<)<)<*
L                06        GT                       <-
R               :TO 2C34 LOC :TO 2D LOC
/    1030  1060  29    2C34MSCL   <<          P          <(<*<*<*
L                10        GT                                  <.
R               :SPEC. HE
/    1060  1090  30    2C24MSCL   <<          P          <(<*<*<-
L                16        GT
R               :TO 2C12 LOC
/    1090  1120  30    2C24CLMS   <<          P          <(<*<*<-
L                05        TG                                  <-<.
R               :TT OR SPEC HE (BLUISH GREY COLOR W/ METALLIC LUSTER
R               :TO 2C22 LOC :TO 2D LOC
/    1120  1161  41    2C23CLMS   <<          P CL   035  <-<*<*<.
L                22        TG                       <-
R               :TO 2C22 LOC :CB << X-CUTS QZ + PY <<
/    1161  1180  19    3A20QZ     <<          P          <.<*<*
L                05        AW
R               :SOME << ARE VUGGY
/    1180  1216  36    3A20QZ     <<          P          <.<)<)
L                09        AW                                  <.
R               :SPEC. HE? OR TT
/    1216  1224  08    8A12CLCY   <<P*        P
L                07        TG
R               :MICRO-PORPHYRITIC TEXT :NO CNTS OBSERVED
/    1224  1250  25    3A20QZ     <<VU        P            <*<*
```

```
L                  11        AW
/    1250  1280    29    3A20QZ      <<          P              <*<*<-
L                  05        AW
/    1280  1310    28    3A10QZ      <<          P              <(<(
L                  22        AW
/    1310  1340    30    3A20QZ      <<          P              <)<)
L                  25        AW
/    1340  1358    18    3A20QZ      <<          P              <(<(
L                  12        AW
R                  :LOWER CNT GRADATIONAL OVER 0.3 M
/    1358  1387    28    3B20QZ      <<          P              <*<*<(
L                  10        AW
R                  :2C FROM 138.3 - 138.7 M. W/ CL ON << :LOWER CNT IRREGULAR
R                  :(NO ATTITUDE) - 2C/3A CNT
/    1387  1397    10    3A20QZ      <<          P              <(<(
L                  09        AW                                    <.
R                  :LOWER CNT GRADATIONAL OVER 0.2 M
/    1397  1410    13    3B10QZ      <<BD        P BD   060     <(<(
L                  05        AW                    CL   040
R                  :OCC. CHERT PEBBLES
/    1410  1430    16    3A10QZ      <<          P              <(<(
L                  05        AW
/    1430  1460    30    3A20QZ      <<          P              <(<*
L                  24        AW
/    1460  1490    30    3A20QZ      <<          P              <*<*
L                  15        AW
/    1490  1528    37    3A30QZ      <<          P              <*<)
L                  18        AW
R                  :LOC 3A20
/    1528  1550    21    2D23MS      <<          P              <(<*<-<-
L                  04        TA                                    <.
R                  :UPPER CONTACT SHARP, BUT IRREGULAR
/    1550  1580    30    2D23MS      <<          P              <(<*<-
L                  08        TA
/    1580  1610    29    2D24MSCL    <<          P            <(<*<*
L                  12        TA
/    1610  1640    30    2D12CLMS    <<          P V/    40   <-<*<*<.
L                  11        TA
R                  :LOC 2C23
/    1640  1670    30    2D13MSCL    <<BR        P V/    45   <(<*<*<.<.
L                  12        TA
R                  :LOC 2C23, MINOR BRECCIA
/    1670  1700    30    2C23MSCL    <<          P            <-<(<*<(<-
L                  18        TA                                  <?
/    1700  1730    30    2C34MSCL    <<          P            <-<(<*<.
L                  21        AT
/    1730  1754    24    2C34MSCL    <<          P            <.<(<)<-<.
L                  12        AT
/    1754  1790    36    2D23MSCL    <<          P              <*<*<.<.
L                  23        TA                                    <.
R                  :LOC 2C23
/    1790  1820    30    2C34MS      <<          P              <(<*<(<.
L                  11        AT
/    1820  1850    29    2D23MSCL    <<          P              <(<*<-<.
L                  14        AT
```

```
R                  :CLAY RICH FAULT BX AT 184.6
/    1850   1880   29    2C34MSCL   <<          P              <(<()<(<.
L                   09        AT
R                  :CLAY RICH FAULT BX AT 197.1
/    1880   1910   30    2C45MS     <<          P              <+<=<(<?
L                   11        AT                                  <(
/    1910   1940   30    2C45MS     <<          P              <+<=<(<?
L                   12        AT                                  <*
R                  :FINE HE IN <<, COULD BE TT AS WELL
/    1940   1970   30    2C55MS     <<BR        P              <+<=<-<?
L                   15        AT                                  <-
/    1970   2000   28    2C44MS     <<          P            <.<(<+<.<.
L                   09        AT
/    2000   2030   29    2C44MS     <<BR        P              <(<)<.<.
L                   13        AT                                  <-
R                  :MINOR BR'X
/    2030   2060   30    2C55MS     <<BR        P              <*<)<-<-
L                   15        AT                                     <.
/    2060   2090   30    2C55MSCL   <<BR        P            <(<(<)<-<-
L                   11        AT                                     <-
/    2090   2120   27    2C35MSCL   <<          P            <-<(<)<.<-
L                   03        AT                                     <.
R                  :LOST CORE AT 211.2 SUSPECT MORE TT THAN VISIBLE IN THIS
R                  :INTERVAL AND THE FEW ABOVE. TT COULD BE IN SMALL << WITH
R                  :BLUEIISH TINGE
/    2120   2150   29    2C34MS     <<          P              <*<)<.<-
L                   12        AT
/    2150   2181   31    2C35MSCL   <<BR        P              <*<+<-<(
L                   18        AT                                  <.
R                  :MINOR BR'X
/    2181   2209   28    8B10FL     <<CM        P CU    30     <(
L                   21        5G                  CL    30
/    2209   2236   21    2C65MS     <<BR        P              #)#+#.#-
L                   03        AT                                  <-
R                  :SANDY FAULT ZONE FROM 222.9 - 223.6
/    2236   2286   50    8B10FL     <<CM        P              <(
L                   31        5G                  CL    40
/    2286   2310   23    2C55MS     <<BR        P              <(<)<(<*
L                   13        AT                                  <-
R                  :MINOR BR'X. 8A FROM 230.4 TO 230.5
/    2310   2335   15    2C65MS     BR<<        P              #)#=#.#.
L                   03        AT
/    2335   2358   23    2C55MS     <<BR        P              <(<+<-<-
L                   17        AT
R                  :MINOR BR'X
/    2358   2375   17    8A10       <<CM        P CU    30     <(
L                   13        AG                  CL    65
/    2375   2377   02    2C55MSCL   <<BR        P            <)#+<=<.<.<.
L                   02        AT                                  <.
R                  :MINOR BR'X
/    2377   2394   17    8A10       <<CM        P CU    50     <(D(
L                   11        6G                  CL    65
/    2394   2410   16    2C65MSCL   <<BR        P            <)#=#+#-#.
L                   09        AT                                  #.#-
R                  :LESS BR'X TOWARDS BOTTOM OF INTERVAL
```

```
/    2410  2448  38    8B10FL     <<TC        P CU    35    <(
L                  25       4G     CM            CL    50      D-
/    2448  2480  30    2C45MSCL   <<BR        P             <*<*<+  <?
L                  05       AT                                 <(
R                 :LOTS OF << HE, MAYBE MINOR TT IN WITH HE
/    2480  2510  29    2434MSCL   <<          P             <)<)<+<.<?
L                  00       AT                                 <-
R                 :AS ABOVE CONCERNING HE
/    2510  2540  29    2C35MSCL   <<BR        P             <)<*<=  <?
L                  11       AT                                 <-
R                 :LOC 2C55, BUT MINOR. AS ABOVE CONCERNING HE
/    2540  2570  30    2C23MSCL   <<          P BD    50    <)<(<*  <?
L                  06       AT                                 <-
R                 :GRADES INTO 2C12, MINOR 2D - BEDDING CONTACT
/    2570  2600  30    2C24MSCL   <<          P             <)<(<(
L                  05       AT                                   <.
/    2600  2630  30    2C23MSCL   <<          P             <+<-<-
L                  00       GT
R                 :GREEN ROCK, VERY LITTLE PY, NO HE
/    2630  2667  37    2C23MSCL   <<          P             <+<(<(
L                  03       GT
R                 :GRADES INTO 2C12 AT END OF HOLE - LAST 0.5 M
R                 :END OF HOLE @ 266.7
A001
ALAB              EQUITY MINESITE LABORATORY
ATYP              ASSAY
AMTH              WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM              RCOVSAMPLE   ROD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R      00    122 :TRICONED - NO CORE
A001   122   186       7343       0.05    1.0 0.02  0.001 0.001 3.86  0.005
A001   186   220       7344       0.08    1.0 0.02  0.001 0.001 3.61  0.005
A001   220   293       7345       0.16    0.5 0.05  0.001 0.005 3.51  0.01
A001   293   332       7346       0.12    0.5 0.06  0.001 0.001 3.50  0.005
A001   332   367       7347       0.05    0.5 0.01  0.001 0.001 3.86  0.005
R                 END OF ASSAYS - END OF LOG
R      367   395 :DYKE - NO SAMPLE
A001   395   430       7348       0.12    0.5 0.03  0.001 0.001 4.24  0.005
A001   430   460       7349       0.03    0.5 0.04  0.001 0.005 1.16  0.001
A001   460   490       7350       0.05    1.0 0.02  0.001 0.001 2.11  0.001
A001   490   520       7351       0.07    0.5 0.02  0.005 0.001 1.25  0.005
A001   520   550       7352       0.09    0.5 0.06  0.005 0.001 1.77  0.001
A001   550   580       7353       0.06    2.0 0.05  0.001 0.01  1.76  0.005
A001   580   610       7354       0.11    0.5 0.03  0.001 0.005 2.94  0.005
A001   610   640       7355       0.04    0.5 0.02  0.005 0.001 1.34  0.005
A001   640   670       7356       0.06    0.5 0.04  0.001 0.001 1.29  0.005
A001   670   700       7357       0.05    0.5 0.07  0.005 0.01  2.15  0.005
A001   700   730       7358       0.06    0.5 0.04  0.001 0.001 2.91  0.001
A001   730   760       7359       0.09    0.5 0.06  0.005 0.001 4.10  0.001
A001   760   790       7360       0.08    0.5 0.04  0.005 0.001 4.35  0.001
A001   790   820       7361       0.05    0.5 0.04  0.005 0.001 4.66  0.005
A001   820   850       7362       0.20    1.0 0.03  0.001 0.001 4.97  0.005
A001   850   880       7363       0.09    4.0 0.06  0.01  0.001 5.22  0.01
A001   880   910       7364       0.04    0.5 0.03  0.005 0.001 3.06  0.005
A001   910   940       7365       0.06    2.0 0.05  0.005 0.001 4.67  0.01
A001   940   970       7366       0.03    2.0 0.05  0.005 0.005 2.24  0.05
```

A001	970	1000		7367	0.08	1.0	0.07	0.005	0.001	4.83	0.05
A001	1000	1030		7368	0.24	10.0	0.04	0.005	0.001	5.41	0.005
A001	1030	1060		7369	0.24	10.0	0.07	0.01	0.005	4.72	0.005
A001	1060	1090		7370	0.10	2.0	0.04	0.005	0.001	3.92	0.005
A001	1090	1120		7371	0.14	4.0	0.03	0.005	0.005	4.04	0.01
A001	1120	1150		7372	0.14	3.0	0.04	0.005	0.005	4.26	0.005
A001	1150	1180		7373	0.03	0.5	0.02	0.005	0.005	3.24	0.005
A001	1180	1200		7374	0.03	2.0	0.02	0.01	0.005	1.68	0.02
A001	1200	1216		7375	0.01	0.5	0.001	0.005	0.005	4.45	0.01
R	1216	1224	:DYKE - NO SAMPLE								
A001	1224	1250		7376	0.02	0.5	0.001	0.005	0.005	2.94	0.005
A001	1250	1280		7377	0.08	0.5	0.01	0.005	0.005	1.85	0.005
A001	1280	1310		7378	0.04	0.5	0.01	0.005	0.001	1.20	0.005
A001	1310	1340		7379	0.06	1.0	0.001	0.005	0.005	2.37	0.005
A001	1340	1370		7380	0.08	2.0	0.01	0.005	0.005	1.83	0.005
A001	1370	1400		7381	0.23	3.0	0.01	0.005	0.005	2.74	0.005
A001	1400	1430		7382	0.03	0.5	0.02	0.005	0.005	1.19	0.005
A001	1430	1460		7383	0.03	0.5	0.01	0.005	0.005	2.16	0.005
A001	1460	1490		7384	0.03	0.5	0.01	0.005	0.001	1.03	0.005
A001	1490	1520		7385	0.02	0.5	0.01	0.01	0.005	2.90	0.01
A001	1520	1550		7386	0.14	5.0	0.02	0.02	0.005	5.04	0.005
A001	1550	1580		7387	0.05	0.5	0.01	0.005	0.005	4.74	0.005
A001	1580	1610		7388	0.04	0.5	0.02	0.005	0.005	3.28	0.005
A001	1610	1640		7389	0.09	0.5	0.01	0.005	0.005	6.33	0.005
A001	1640	1670		7390	0.10	2.0	0.01	0.005	0.001	4.48	0.005
A001	1670	1700		7391	0.14	8.0	0.005	0.01	0.005	4.11	0.02
A001	1700	1730		7392	0.07	0.5	0.005	0.01	0.005	5.16	0.005
A001	1730	1760		7393	0.13	4.0	0.005	0.005	0.005	3.83	0.005
A001	1760	1790		7394	0.17	2.0	0.005	0.01	0.005	3.60	0.03
A001	1790	1820		7395	0.17	2.0	0.005	0.01	0.005	6.31	0.005
A001	1820	1850		7396	0.06	0.5	0.005	0.005	0.005	3.50	0.005
A001	1850	1880		7397	0.28	13.0	0.05	0.01	0.005	5.82	0.005
A001	1880	1910		7398	0.13	6.0	0.005	0.03	0.005	8.36	0.005
A001	1910	1940		7399	0.20	7.0	0.24	0.04	0.01	6.53	0.01
A001	1940	1970		7400	0.09	4.0	0.01	0.03	0.02	8.82	0.005
A001	1970	2000		7401	0.04	2.0	0.005	0.02	0.02	7.84	0.005
A001	2000	2030		7402	0.14	8.0	0.005	0.04	0.02	5.02	0.02
A001	2030	2060		7403	0.11	5.0	0.005	0.03	0.01	4.97	0.07
A001	2060	2090		7404	0.10	3.0	0.005	0.005	0.01	3.10	0.14
A001	2090	2120		7405	0.07	2.0	0.005	0.005	0.005	2.38	0.10
A001	2120	2150		7406	0.08	2.0	0.005	0.005	0.005	3.01	0.01
A001	2150	2181		7407	0.13	7.0	0.005	0.01	0.01	4.14	0.07
R	2181	2209	:DYKE - NO SAMPLE								
A001	2209	2236		7408	0.20	52.0	0.02	0.05	0.02	5.12	0.07
R	2236	2286	:DYKE - NO SAMPLE								
A001	2286	2310		7409	0.15	20.0	0.005	0.04	0.02	6.02	0.44
A001	2310	2335		7410	0.01	0.5	0.005	0.01	0.005	4.50	0.005
A001	2335	2358		7411	0.06	9.0	0.005	0.01	0.005	5.89	0.08
R	2358	2375	:DYKE - NO SAMPLE								
A001	2375	2377		7412	0.02	6.0	0.005	0.01	0.005	4.30	0.11
R	2377	2394	:DYKE - NO SAMPLE								
A001	2394	2410		7413	0.03	12.0	0.005	0.01	0.01	5.29	0.26
R	2410	2448	:DYKE - NO SAMPLE								
A001	2448	2480		7414	0.06	19.0	0.005	0.02	0.02	5.33	0.01
A001	2480	2510		7415	0.06	11.0	0.05	0.03	0.03	3.74	0.005

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A001 2510  2540       7416       0.02    7.0 0.09  0.005 0.001 5.53  0.001
A001 2540  2570       7417       0.03    5.0 0.03  0.005 0.001 4.92  0.02
A001 2570  2600       7418       0.02    0.5 0.02  0.005 0.001 3.47  0.001
A001 2600  2630       7419       0.005   0.5 0.01  0.001 0.001 2.61  0.001
A001 2630  2667       7420       0.001   0.1 0.01  0.005 0.001 3.65  0.001
R                 :END OF HOLE - END OF SAMPLES
```

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IDEN6B0201      X86CH273 NQ   AUG86RWW   G&D AUG86S38          0.0
IPRJ          EQUITY SILVER MINES LTD        SOUTH OF S. TAIL - ST GEOCODE
S000   00   541 MT  343.2 092.0 -45.0              6030.84   7429.97   1193.26
S001  541  1584     343.2 092.0 -44.0
S002 1584  2759     343.2 092.0 -43.5
S003 2759  3432     343.2 092.0 -43.5
/SCL         MT.2MT.1
LSCL             MT.2
/NAM                                                      MSCLQZPYCPTTASPR
LNAM                                                      CBGY  MGHESLGLMO
/      00   213        OVBN                    P
R                  :TRICONED - NO CORE, CASING TO 21.3
/     213   243  25    3A20QZ     CT<<         P              <)<*B.
L                  02        7A
R                  :MAINLY BOULDERS AT BEGINNING OF INTERVAL  :SOME FRACTURES CON-
R                  TAIN CLAY
/     243   270  29    3A30QZ     CT<<         P              <)<(  B.
L                  06        7A
R                  :SOME THIN INTERBEDDED 3F AND 3B  :CLAY PRESENT AGAIN
/     270   300  28    3A30QZ     CT<<         P              <)<*B.
L                  00        7A
R                  :AGAIN SOME CLAY FILLING FRACTURES  :CP ONLY AT 27.2M
R                  :SMALL ZONE OF 3G AT END ON INT.
/     300   330  29    3A10QZ     CT<<         P              <*<*P.
L                  11        7A
R                  :CP ONLY AT 31.9M  :AGAIN SOME INTERBEDDED 3F AND 3B.
/     330   360  29    3A20QZ     CT<<         P              <)<*<.
L                  06        7A     BR
R                  :AGAIN SOME INTERBEDDED 3B  :SMALL BR'N IN VEIN AT 35.6M.
/     360   390  29    3A20QZ     CT<<         P              <+<*
L                  14        7A
R                  :AS ABOVE
/     390   420  28    3A21QZ     CT<<         P           <-<+<*B>
L                  05        6A
R                  :AS ABOVE  :CL ALSO PRESENT  :SMALL ZONE OF 3F FROM 39.8 TO
R                  40.2
R                  :CP ONLY AT 40.5 M  :.3M OF 8C HEAVILY ALTERED TO CY AT 41.7M.
/     420   450  29    3B21QZ     CT<<         P              <-<+<(<.
L                  09        6A
R                  :SOME CHERTY PEBBLES SCATTERED THROUGHOUT INT.
/     450   480  28    3B21QZ     CT<<         P              <-<+<(<.
L                  11        7A
R                  :SOME INTERBEDDED 2C  :ALSO MUCH 3A.
/     480   518  36    3B21QZ     CT<<         P              <.<+<*<.
L                  11        7A
R                  :CP ONLY AT 49.3M  :AGAIN INTERBEDDED 3A.
/     518   540  21    8A00
L                  08
R                  :CLAY PHENOS PRESENT  :CONTACTS NOT MEAS. DUE TO BROKEN CORE.
/     540   570  28    3B11QZ     CT<<         P              <.<)<*B
L                  05        6A
R                  :CP ONLY AT 56.8M  :AGAIN INTERBEDDED 3A
/     570   600  29    3A21QZ     CT<<         P              <*<(*<.
L                  08        7A
R                  :SOME INTERBEDDED 3F
```

```
/     600   630  27    3A11QZ     CT<<        P            <.<(<*<.
L                03        7A
R               :AS ABOVE
/     630   660  28    3A20QZ     CT<<        P              <+<*  B.
R               :TT ONLY AT 63.2 M
/     660   690  28    3A20QZ     CT<<        P              <+<*  B?
L                05        7A
R               :BLUE TARNISH ON PY.
/     690   720  29    3A11QZ     CT<<        P            <.<+<(<.
L                06        7A
R               :STARTING TO GET 2D MIXED IN WITH 3A.
/     720   750  28    2C33MS
L                02        GT     <<          P            <)<+<*<.
R               :MAINLY 2D AT BEGINNING OF INTERVAL.
/     750   780  28    2C32MS     <<          P <<     25  <)<+<)<.B.
L                08        TG                            <.
/     780   810  29    2C32CL     <<          P            <)<+<)<.
L                09        TG                           <.
/     810   840  28    2C21CL     <<          P            <)<+<*
L                03        GA
R               :SOME INTERBEDDED 2D
/     840   870  29    2C33MS     <<          P            <)<=<+<.
L                05        GT                                 B.
/     870   900  28    2C22CL     <<          P            <+<=<)<.
L                03        TG                          Q)       U-<.
R               :HE IN NEEDLES - MAYBE SOME TT MIXED IN.
/     900   930  29    2C32CL     <<          P            <+<=<=B.B.
L                05        TG                          <-       U.
R               :HE AS ABOVE  :CP AND TT MAINLY IN LARGE QUARTZ <<
/     930   960  29    2C22CL     <<          P <<     25  <+<=<)<.
L                08        TG                          Q        <.
/     960   990  29    2C32CL     <<          P            <+<=<)<.<?
L                14        TG                          <)       <-
R               :HE AS ABOVE, SOME IN PATCHES.
/     990  1020  29    2C21CL     <<          P            <(<+<)<.
L                14        GA                                 <(
/    1020  1050  29    2C22CL     <<          P            <)<=<+
L                08        TG                                 <.
R               :SOME MS ALTERATION.
/    1050  1080  29    2C21CL     <<          P C1     62  <(<)<*
L                09        AG
R               :CONTACT MEASURED BTWN A2C AND G2C WHERE 62C HAS STRONGER ALT.
/    1080  1110  29    2C21CL     <<          P            <(<+<)<-
L                09        TG                          <(    B.<.
R               :HE IN CE-CB VEIN  :PART OF INT MAGNETIC
/    1110  1140  29    2C22CL     <<          P            <)<+<)<.
L                15        TG                               B)B.
R               :SOME CORE QUITE MAGNETIC
/    1140  1170  29    2C22CL     <<          P            <+<+<)<.
L                11        TG                          <.    B(<.
R               :AS ABOVE (MAG NOT AS STRONG).
/    1170  1200  29    2C21CL     <<          P            <(<+<*
L                04        TA                          <-    B-Q.
R               :MG AS ABOVE
/    1200  1230  28    2C23MS     <<          P            <(<+<)<-
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L                09        GT                                    <.
R               :MG FOUND WITH PY-QTZ VEIN.
/    1230  1260  28    2C22CL     <<          P            <)<+<)
L                02        TG                                   B-<.
R               :AGAIN CORE SLIGHTLY MAGNETIC
/    1260  1290  30    2C22CL     <<          P            <)<+<)<.
L                14        TG                                   B.<-
R               :AS ABOVE
/    1290  1320  29    2C23CL     <<          P            <+<+<)<.
L                11        TG                                   B-<.
R               :AS ABOVE
/    1320  1350  28    2C33CL     <<          P            <)<+<+Q-<?
L                06        TG                              <.   B.<-
R               :AS ABOVE  :HE SUSPICIOUS - MAY BE SOME TT IN IT
/    1350  1380  28    2C44MS     <<          P            <*<=<)B.<?
L                04        AT                                   <.
R               :AGAIN HE MAY CONTAIN TT
/    1380  1410  28    2C44MS     <<          P            <+<=<)<.<
L                04        GT                                   <.<.
R               :SL ONLY AT 139.0M
/    1410  1440  29    2C44MS     <<          P            <)<=<+<.
L                14        GT                                   B.<.
R               :STARTING TO GET GOOD MS ALT'N. :CORE SLIGHTLY MAG AGAIN
/    1440  1470  28    2C44MS     <<BR        P            <)<=<+<.<.
L                06        GT
R               :.1M BRECCIATION AT 146.9
/    1470  1500  28    2C33MS     <<          P CL     75  <)<+<*<.B.
L                11        TG
R               :.3M BC FROM 148.2M. :TT ONLY AT 148.6M
/    1500  1530  29    2C44MS     <<          P CU     35  <+<=<+<.B.
L                17        AT                                   Q.
R               :UPPER CONTACT IRREGULAR  :.7M OF BC FROM 153.7M
/    1530  1560  29    3A41QZ     <<CT        P            <*<+<=<*
L                14        6A
R               :BEGINNING 1M MAINLY 2C WITH ALT'N 4  :GRAD'NAL CNT BTWN 2C & 3A
/    1560  1590  28    2A30QZ     <<CT        P              <+<)
L                11        7A
/    1590  1620  26    3A30QZ     <<CT        P              <+<(
L                02        71
/    1620  1650  28    3A30QZ     <<CT        P              <=<+  Q.
L                08        6A                                   Q.
R               :TT 7 SL ONLY AT 163.9M
/    1650  1680  28    3A30QZ     <<CT        P              <=<+
L                11        6A
/    1680  1710  29    3A30QZ     <<CT        P              <+<+  B.
L                12        7A                                  B-
R               :HE MORE COMMON THAN TT BUT HE MAY CONTAIN TT (CAN'T TELL)
/    1710  1740  29    3A20QZ     <<CT        P              <+<(  <.
L                09        7A                            <.
R               :SOME INTERBEDDED 3B. :ALSO SOME 2C FRAGMENTS. :TT ONLY AT
R               173.5M.
/    1740  1770  28    3A31QZ     <<CT        P            <-<+<)<.
L                11        7A                          <.
R               :TT IN SMALL CB'TIZED VEINS
/    1770  1800  28    3A31QZ     <<CT        P            <.<+<+  <.
```

```
L                  04        7A                                          <.
/    1800  1830  28    3A310Z     <<CT       P            <-<+<=
R                :SOME INTERBEDDED 2D AND SOME 2C FRAGS.
/    1830  1860  29    3A300Z     <<CT       P            <.<+<=  B.
L                  08        8A
R                :SOME TINY SILVER SPECS BUT CANNOT TELL WHAT?
/    1860  1890  29    3A320Z     <<CT       P            <-<+<=<.
L                  11        7A     BR
R                :FINAL 1.1M OF INT 2C WITH CP AND ACT'N 3 :GOOD .1M BRECCIATION
R                AT BEGINNING OF 2C
/    1890  1920  30    2C43MS     <<         P            <+<+<*<)<.
L                  18        GT                                        <.
R                :TT MAY BE MOSTLY HE BUT GAVE A DULL GRAY STREAK (V. GRANULAR)
/    1920  1950  28    2C34MS     <<         P            <+<=<)<.
L                  08        AT                                        <.
/    1950  1980  28    2033MS     <<         P            <+<=<+<.
L                  11        TA
R                :SOME INTERBEDDED 2C  :FIRST PART OF INT 2C,LAST 2/3RDS 2D
/    1980  2010  29    2C44MS     <<BR       P            <*<+<)<-
L                  15        GT                                  <-    B.B.
R                :BIG PATCH OF CP AT 200.8M  :CORE SLIGHTLY MAGNETIC
/    2010  2040  29    2033MS     <<         P            <-<+<)<.
L                  15        TA
R                :INTERBEDDED 2C AND 2D
/    2040  2070  28    2C44MS     <<         P            <)<(<(<.<.
L                  09        GT                                        <.
R                :LARGE QTZ-PY VEIN AT END OF INT. QZ PART CONTAINS GRAY-BLUE
R                FLECKS-MAY BE TT BUT TOO SMALL TO TELL
/    2070  2100  28    2C45MS     <<         P            <)<=<)<*
L                  09        AT                                     B.<.
R                :THIS TIME HE AS BLUE-GRAY PATCHES IN QTZ-VEIN
/    2100  2130  29    2C45MS     <<BR       P            <.<+<=<-<.
L                  14        AT                                     B.<.
R                :ALONG WITH << PY ALSO FINELY DISSEMINATED PY.
/    2130  2160  29    2C34MS     <<         P            <+<=<)<.
L                  05        TA
/    2160  2190  28    2C44MS     <<BR       P            <)<=<+
L                  05        AT
R                :LARGE TQZ-PY VEIN WITH 2C FRAGS AT 216.7M ALONG WITH BRECCIA.
/    2190  2220  28    2C43MS     <<         P            <*<+<)<-
L                  04        TA
/    2220  2250  29    2C33MS     <<         P            <+<=<+  B.
L                  08        TG                                        B-
R                :TT LOOKED LIKE IT HAD HE BUT DIN'T GIVE RED STREAK
/    2250  2280  30    2C44MS     <<         P            <)<=<+Q)
L                  18        GT                                        <(
R                :SOME CP ALSO AS <<.
/    2280  2310  30    2C44MS     <<         P            <)<=<)<)B.
L                  11        AT                                  <-
R                :CP AS PATCHES & BLEBS AS WELL
/    2310  2340  29    2C33MS     <<         P            <)<=<)<.
L                  09        TA                                        <.
/    2340  2370  30    2C22MS     <<         P            <)<+<)<)
L                  15        TG
/    2370  2400  27    2C44MS     <<BR       P            <+<+<+<*
```

```
L                  15          AT
R                 :BIG PATCH OF CP AT 237.5M.
/     2400   2430  30    2C44MS      <<          P              <)<=<+<(
L                  09          AT
R                 :SOME INTERBEDDED 2D.
/     2430   2460  29    2C44MS      <<BR        P              <(<=<=<)<-
L                  06          AT
R                 :STRONG << AND BRECCIATION THROUGHOUT INTERVAL
/     2460   2490  29    2C45MS      <<BR        P              <.<=<=<)<(
L                  06          AT                                    <-
R                 :SOME TT MAY CONTAIN HE AND VISA-VERSA - NICE CORE!
/     2490   2520  29    2C45MS      <<          P              <)<+<=<(<-
L                  14          AT
R                 :MOST TT AT BEGINNING OF INTERVAL
/     2520   2550  30    2C44MS      <<BR        P              <)<+<=<-<.B?
L                  17          AT                                    B-
R                 :MOST BLUE-GRAY LOGGED AS HE
/     2550   2580  29    2C45MS      <<B4        P              <=<=<.<-
L                  12          5T                                  <-
R                 :HARD TO GELL IF HE OR TT - BURGUNDY STK.
/     2580   2610  29    2C44MS      <<BR                       <.<+<+<.<.
L                  12          AT                                    <-
R                 :AS ABOVE
/     2610   2640  28    2C44MT      <<          P              <.<=<)<.<-
L                  12          AT
/     2640   2673  30    2C44MS      <<BR        P              <.<=<+B.<.
L                  06          AT
R                 :CP ALSO IN <<
/     2673   2705  31    8A20CL      <<BR        P CU     70
L                  21          5G
R                 :FELDSPAR PHENOS  :BR OF 2C INTO PART OF DYKE
/     2705   2740  33    2C44MS      <<BR        P              <.<=<+  <.
L                  17          AT                                    <-
R                 :SOME 8A IN SAMPLE AT START OF INTERVAL
/     2740   2770  26    2C44MS      <<BR        P              <.<=<+  <.
L                  03          AT                                    <.
/     2770   2800  28    2C44MS      <<BR        P              <.<=<+<.<.
L                  05          AT                                    <-
/     2800   2830  29    2C44MS      <<BR        P              <.<=<=0.0.
L                  14          AT                                    <.
R                 :SOME BLUE-GRAY HARD TO TELL BTWN HE & TT
/     2830   2860  29    2C44MS      <<BR        P              <.<=<=B-B.
L                  11          AT                                    B.
/     2860   2890  28    2C44MS      <<BR        P              <.<=<+<.<.
L                  00          AT
/     2890   2920  29    2C44MS      <<BR        P              <.<=<=B.B.
L                  05          AT                                    B.
/     2920   2950  29    2C44MS      <<BR        P              <.<+<=
L                  06          AT
R                 :GOOD ALT'N BUT ONLY PY MINERALIZATION
/     2950   2980  29    2C44MS      <<BR        P              <.<=<+
L                  09          AT
R                 :2 PY-QTZ VEINS ABOUT 2CM WIDE - NO MINERALIZATION
/     2980   3010  29    2C44MS      <<BR        P                <=<=  B.
L                  06          AT                                    B.
```

```
/    3010  3040  28    2C44MS     <<BR       P            <.<=<=
L                  11       AT                                B.
/    3040  3070  29    2C44MS     <<BR       P            <.<+<=
L                  04       AT                                B.
/    3070  3102  29    2C44MS     <<BR       P            <.<+<+
L                  06       AT
/    3102  3136  33    8A10CL     <<A*       P CL    50      <-
L                  18       TG                          <.
R                 :UPPER CONTACT NOT MEASURED DUE TO BROKEN CORE :FELDSPAR AMYGDS
/    3136  3165  25    2C44MS     <<BR       P            <.<=<+
L                  09       6T                         <-
R                 :SOME CB PRESENT IN <<
/    3165  3180  14    8C10CL     <<A*       P              <)
L                  08       TG                          <.    B.
R                 :CL AMYGDS  :BANDS OF DARK GREEN (ANDESITE)
/    3180  3185  05    2C44MS    <<BR        P              <=<=
L                  03       6T                                <?
R                 :SHORT SAMPLE SINCE ENCASED BY DYKE ON TOP & BOTTOM
/    3185  3224  37    8A10CL     <<A*       P              <)<.
L                  15       5G                          <.    B(
R                 :CL & HE AMYGDS  :SOME TYPE OF SOFT RED MINERAL (?)
/    3224  3250  24    2C45MS     <<BR       P              <+<+
L                  06       6T
/    3250  3280  27    2C34M3     <<         P            <-<+<+
L                  05       7T
R                 :CORE STARTING TO LOSE FRACTURING
/    3280  3310  29    2C33MS     <<         P            <)<+<)B.
L                  09       TG                          <.
R                 :SOME CLY PRESENT  :ROCK TURNING QUITE GREEN
/    3310  3326  15    2C22MS     <<         P            <+<=<)<.
L                  03       TG
/    3326  3349  22    8A10CL     <<         P              <-
L                  12       4G
R                 :CL PHENOS
/    3349  3380  29    2C32MS     <<         P            <+<+<)
L                  08       TG                          <.
/    3380  3410  27    2C32MS     <<BR       P              <+<+<*B.
L                  02       TG                          <-
R                 :SOMETHING CAUSING A PURPLE COLOR (UNIDENTIFIABLE MINERAL)
/    3410  3432  21    2C21CL     <<         P            <+<+<*Q-
L                  06       AG
R                 :CP BECOMING MORE PROMINENT
R                 :END OF HOLE - END OF LOG

A001
ALAB              EQUITY MINESITE LABORATORY
ATYP              ASSAY
AMTH              WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM              RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R                 :TRICONED - NO CORE TO 21.3
A001  213   243       7441       0.050    0.1 0.010 0.005 0.001 1.270 0.001
A001  243   270       7442       0.10     0.5 0.02  0.005 0.001 1.57  0.001
A001  270   300       7443       0.06     0.5 0.03  0.005 0.001 1.57  0.001
A001  300   330       7444       0.06     0.1 0.01  0.005 0.001 1.24  0.001
A001  330   360       7445       0.04     0.1 0.01  0.005 0.001 1.09  0.001
```

A001	360	390	7446	0.04	0.5	0.01	0.005	0.001	1.15	0.001
A001	390	420	7447	0.07	0.5	0.03	0.005	0.001	2.06	0.001
A001	420	450	7448	0.04	0.5	0.01	0.005	0.001	2.09	0.001
A001	450	480	7449	0.08	0.5	0.01	0.005	0.001	2.05	0.001
A001	480	518	7450	0.05	0.5	0.01	0.005	0.001	1.15	0.001
R	518	540	:DYKE - NO SAMPLE							
A001	540	570	7451	0.06	0.5	0.03	0.005	0.001	2.13	0.001
A001	570	600	7452	0.06	0.1	0.03	0.005	0.001	1.53	0.001
A001	600	630	7453	0.04	0.1	0.01	0.005	0.001	1.21	0.001
A001	630	660	7454	0.03	0.5	0.01	0.005	0.001	1.69	0.001
A001	660	690	7455	0.05	0.5	0.05	0.005	0.001	1.60	0.001
A001	690	720	7456	0.04	1.0	0.01	0.005	0.005	1.12	0.005
A001	720	750	7557	0.10	1.0	0.04	0.005	0.005	3.56	0.005
A001	750	780	7458	0.12	1.0	0.05	0.005	0.005	4.39	0.005
A001	780	810	7459	0.04	0.5	0.03	0.005	0.005	3.53	0.005
A001	810	840	7460	0.07	1.0	0.01	0.005	0.01	3.71	0.005
A001	840	870	7461	0.06	1.0	0.01	0.005	0.005	3.54	0.005
A001	870	900	7462	0.04	1.0	0.01	0.005	0.005	4.96	0.005
A001	900	930	7463	0.08	1.0	0.01	0.005	0.005	4.78	0.005
A001	930	960	7464	0.05	1.0	0.01	0.005	0.005	4.16	0.005
A001	960	990	7465	0.03	1.0	0.01	0.005	0.005	4.05	0.005
A001	990	1020	7466	0.04	1.0	0.01	0.005	0.005	5.65	0.005
A001	1020	1050	7467	0.04	1.0	0.01	0.005	0.005	4.73	0.005
A001	1050	1080	7468	0.03	1.0	0.01	0.005	0.005	3.81	0.005
A001	1080	1110	7469	0.07	1.0	0.02	0.005	0.005	3.14	0.005
A001	1110	1140	7470	0.05	1.0	0.01	0.005	0.005	4.41	0.005
A001	1140	1170	7471	0.03	1.0	0.01	0.005	0.005	3.89	0.005
A001	1170	1200	7472	0.07	1.0	0.03	0.005	0.005	4.15	0.005
A001	1200	1230	7473	0.18	1.0	0.01	0.01	0.01	4.20	0.01
A001	1230	1260	7474	0.05	1.0	0.01	0.01	0.005	4.81	0.005
A001	1260	1290	7475	0.02	0.5	0.01	0.005	0.005	4.19	0.005
A001	1290	1320	7476	0.06	1.0	0.02	0.005	0.005	4.28	0.005
A001	1320	1350	7477	0.15	2.0	0.03	0.03	0.005	4.48	0.01
A001	1350	1380	7478	0.08	5.0	0.03	0.03	0.02	4.26	0.03
A001	1380	1410	7479	0.14	3.0	0.01	0.05	0.01	4.66	0.07
A001	1410	1440	7480	0.03	1.0	0.02	0.01	0.01	4.62	0.03
A001	1440	1470	7481	0.04	1.0	0.02	0.01	0.01	4.65	0.04
A001	1470	1500	7482	0.06	2.0	0.11	0.01	0.01	5.10	0.04
A001	1500	1530	7483	0.06	3.0	0.05	0.02	0.005	3.94	0.07
A001	1530	1560	7484	0.09	3.0	0.01	0.01	0.005	5.12	0.01
A001	1560	1590	7485	0.02	2.0	0.01	0.01	0.01	2.32	0.005
A001	1590	1620	7486	0.09	2.0	0.01	0.04	0.01	1.59	0.01
A001	1620	1650	7487	0.05	4.0	0.12	0.02	0.02	2.97	0.01
A001	1650	1680	7488	0.02	2.0	0.04	0.01	0.005	4.29	0.01
A001	1680	1710	7489	0.05	2.0	0.01	0.02	0.01	3.33	0.05
A001	1710	1740	7490	0.06	2.0	0.01	0.02	0.005	1.82	0.01
A001	1740	1770	7471	0.08	2.0	0.01	0.01	0.005	1.95	0.04
A001	1770	1800	7492	0.01	1.0	0.01	0.01	0.005	4.26	0.02
A001	1800	1830	7493	0.02	2.0	0.01	0.01	0.005	6.10	0.005
A001	1830	1860	7494	0.01	1.0	0.01	0.005	0.005	3.34	0.005
A001	1860	1890	7495	0.26	1.0	0.01	0.005	0.005	2.83	0.005
A001	1890	1920	7496	0.45	4.0	0.02	0.02	0.005	3.48	0.01
A001	1920	1950	7497	0.07	1.0	0.01	0.005	0.005	3.75	0.005
A001	1950	1980	7498	0.08	0.5	0.08	0.005	0.005	3.37	0.005
A001	1980	2010	7499	0.10	0.5	0.08	0.01	0.005	3.41	0.005

A001	2010	2040	7500	0.13	0.5	0.03	0.02	0.005	4.26	0.005
A001	2040	2070	7501	0.06	0.5	0.04	0.02	0.005	6.77	0.005
A001	2070	2100	7502	0.15	0.5	0.03	0.01	0.005	2.73	0.005
A001	2100	2130	7503	0.09	0.5	0.01	0.02	0.005	6.15	0.005
A001	2130	2160	7504	0.04	0.5	0.01	0.02	0.005	3.76	0.005
A001	2160	2190	7505	0.01	0.5	0.01	0.02	0.005	5.60	0.005
A001	2190	2220	7506	0.09	0.5	0.03	0.005	0.005	3.67	0.005
A001	2220	2250	7507	0.05	0.5	0.04	0.005	0.005	4.15	0.005
A001	2250	2280	7508	0.10	0.5	0.02	0.005	0.005	4.30	0.005
A001	2280	2310	7509	0.34	0.5	0.03	0.005	0.005	3.84	0.005
A001	2310	2340	7510	0.11	0.5	0.03	0.02	0.005	4.47	0.005
A001	2340	2370	7511	0.17	0.5	0.02	0.01	0.005	4.08	0.005
A001	2370	2400	7512	0.22	0.5	0.01	0.02	0.005	3.53	0.005
A001	2400	2430	7513	0.30	0.5	0.01	0.005	0.005	4.32	0.005
A001	2430	2460	7514	0.61	24.0	0.07	0.03	0.01	7.68	0.005
A001	2460	2490	7515	0.43	18.0	0.05	0.09	0.02	5.92	0.03
A001	2490	2520	7516	0.13	0.5	0.07	0.04	0.005	6.37	0.005
A001	2520	2550	7517	0.14	10.0	0.07	0.03	0.005	4.97	0.005
A001	2550	2580	7518	0.12	12.0	0.22	0.05	0.005	6.89	0.19
A001	2580	2610	7519	0.14	0.5	0.06	0.04	0.005	4.12	0.02
A001	2610	2640	7520	0.16	0.5	0.01	0.05	0.005	4.10	0.01
A001	2640	2673	7521	0.16	0.5	0.02	0.04	0.005	3.99	0.005
R	2673	2705	:DYKE - NO SAMPLE							
A001	2705	2740	7522	0.05	0.5	0.03	0.03	0.005	5.16	0.005
A001	2740	2770	7523	0.04	0.5	0.01	0.03	0.005	6.02	0.005
A001	2770	2800	7524	0.05	0.5	0.03	0.03	0.005	4.68	0.005
A001	2800	2830	7525	0.07	0.5	0.07	0.04	0.005	4.79	0.005
A001	2830	2860	7526	0.08	0.5	0.04	0.02	0.005	4.49	0.005
A001	2860	2890	7527	0.07	0.5	0.02	0.02	0.005	3.68	0.005
A001	2890	2920	7528	0.12	0.5	0.03	0.03	0.005	6.16	0.005
A001	2920	2950	7529	0.02	0.5	0.02	0.02	0.005	6.05	0.005
A001	2950	2980	7530	0.02	0.5	0.02	0.03	0.005	4.48	0.005
A001	2980	3010	7531	0.04	13.0	0.04	0.005	0.005	5.11	0.02
A001	3010	3040	7532	0.005	0.5	0.02	0.005	0.005	5.98	0.001
A001	3040	3070	7533	0.01	0.5	0.02	0.02	0.005	5.10	0.005
A001	3070	3102	7534	0.03	20.0	0.05	0.04	0.005	6.15	0.005
R	3102	3136	:DYKE - NO SAMPLE							
A001	3136	3165	7535	0.005	0.5	0.04	0.02	0.005	4.06	0.005
R	3165	3180	:DYKE - NO SAMPLE							
A001	3180	3185	7536	0.01	0.5	0.11	0.01	0.005	4.52	0.005
R	3185	3224	:DYKE - NO SAMPLE							
A001	3224	3250	7537	0.01	0.5	0.02	0.005	0.005	4.46	0.001
A001	3250	3280	7538	0.005	0.5	0.01	0.005	0.005	3.30	0.001
A001	3280	3310	7539	0.02	0.5	0.02	0.01	0.005	4.62	0.001
A001	3310	3326	7540	0.02	0.5	0.03	0.005	0.005	3.93	0.005
R	3326	3349	:DYKE - NO SAMPLE							
A001	3349	3380	7421	0.01	0.5	0.03	0.005	0.005	4.20	0.005
A001	3380	3410	7422	0.02	0.5	0.02	0.01	0.005	4.61	0.005
A001	3410	3432	7423	0.02	0.5	0.02	0.005	0.005	4.93	0.005
R			END OF ASSAYS - END OF LOG							

```
IDEN6B0201      X86CH274 NQ   AUG86RWWRBPG&D AUG86S38          0.0
IPRJ         EQUITY SILVER MINES LTD         SOUTH OF S. TAIL - ST GEOCODE
S000   00   375 MT  310.9 090.0 -45.0              6131.61   7484.28   1224.09
S001  375  1276     310.9 090.0 -44.0
S002 1276  2373     310.9 090.0 -42.0
S003 2373  3109     310.9 090.0 -42.0
/SCL         MT.2MT.2
LSCL             MT.2
/NAM                                                      MSCLQZPYCPTTASPR
LNAM                                                      CBGY  MGHESLGLMO
/      00    61         OVBN                    P
R                :TRICONED - NO CORE
/      61   105  24     3F10QZ      <<          P              <)<*
L                00         SA
R                :FE STAINING ALONG FRACTURES, SOME MANGANESE OXIDATION
/     105   127  20     3F10QZ      <<          P              <+<)
L                02         SA                          <-
R                :AS ABOVE
/     127   140         NREC                    P
R     127   140 :MISLATCH - NO CORE  :SOME QZ PEBBLES
/     140   170  25     3F10QZ      <<BR        P              <+<)
L                00         SA
R                :SOME FE STAINING ON FRACIS  :ALSO SOME 3D
/     170   200  25     3F10QZ      <<          P              <)<*
L                02         SA
R                :AS ABOVE
/     200   230  27     3F10QZ      <<          P  FB   50     <+<)
L                03         4A
R                :FE STAIN HAS JUST ABOUT DISAPPEARED :SOME LARGER FRAGMENTS
/     230   260  28     3F10QZ      <<          P              <+<)
L                05         SA                          <-
R                :BEGINNING OF INT FE STAINED, SOME AT END :MANY CLASTS TOWARD
R                END OF INT.
/     260   290  27     3F11CL      <<CL        P            *=<+<(
L                00         AG                          <(    B.*.
R                :AGAIN SOME 3D MIXED IN :CORE SLIGHTLY MAGNETIC
/     290   320  27     3F21CL      <<CL        P            <)<+<)
L                03         AG
R                :FE STAINING ALONG FRACTURES
/     320   350  27     3F21CL      <<          P            <)<+<*
L                03         3A
R                :MINOR FE STAINING
/     350   380  28     3F32CL      <<          P            <+<+<.
L                06         TA
R                :AS ABOVE
/     380   410  28     3F43MS                  P            <)<+<)B.B.
L                05         AT
R                :AS ABOVE :GRAY SULPHIDE - MAYBE TT
/     410   440  27     3F42CL      <<          P            <+<=<)
L                05         TG                          <-
R                :AS ABOVE
/     440   470  28     3F33MS      <<BR        P            <)<=<*
L                05         TG                          <-
R                :AS ABOVE
/     470   500  27     3F33MS      <<          P            <+<+<)B.
```

```
L                 02        GT                                  <(
R                :AS ABOVE
/      500   530  27    3F32MS     <<          P                 <)<+<*B.B.
L                 05        GT                                  <(
/      530   560  27    3F34MS     <<          P                   <(<+<-
L                 00        GT
/      560   590  29    3F33MS     <<          P FB     30       <+<+<*
L                 00        TG                                        <.
/      590   620  28    3F33MS     <<          P                   <=<+<)<.B.
L                 00        TG                                  <-
R                :TT QUESTIONABLE - VERY TINY SILVER-GRAY BLEBS
/      620   650  26    3F33MS     <<          P                   <=<+<)B.
L                 05        TG                                        B.
/      650   680  29    3F32CL     <<          P                   <+<=<*B.
L                 05                                            <(
R                :CORE QUITE GREEN
/      680   710  28    3F32CL     <<          P                   <)<=<*<.B?
L                 03        TG                                  <)     B.
/      710   740  27    3F32CL     <<          P                   <+<+<*B.
L                 03        5G                                  <(       <-
R                :HE ONLY AT 71.7M
/      740   770  29    3F43MS     <<          P                   <+<=<+B.B.
L                 12        TG                                  <(
/      770   790  18    3F33MS     <<BR        P
L                 03        TA
/      790   801  10    8F00                   P
L                 00
R                :CONTACTS SOMEWHAT IRREGULAR
/      801   830  28    3F32CL     <<BR        P                   <)<+<*
L                 06        TG                                        8.<.
/      830   860  28    3E32CL     <<          P                   <)<=<*B.
L                 02        AG
R                :SOME CLAY FILLING FRACTURES
/      860   890  29    3B31QZ     <<          P                   <.<=<*<.
L                 06        6A
R                :INTERVAL STARTS AS 3C GOES TO 3B THEN 3D AND FINALLY INTO 3A
R                :GRADATIONAL CONTACTS  :CLAY FILLING SOME FRAC'S.
/      890   920  28    3A10QZ     <<BR        P                     <+<)<.
L                 05        6A     CL
R                :ONE BAND OF 3C AT 90.6M
/      920   950  28    3A10QZ     <<CL        P                     <+<)B.
L                 06        7A                                  <)
R                :SOME CLASTS OF ARGILLITE  :SOME CLAY INFILLING FRAC'S.
/      950   980  28    3A21QZ     <<CL        P                     <+<(
L                 12        GA                                  <)
R                :SOME CARB INFILLING FRAC'S  :ALSO SOME 3B AT END OF INTERVAL
/      980  1010  28    3A20QZ     <<CL        P                     <=<(<.
L                 12        6A                                  <.U-
/     1010  1040  27    3A10QZ     <<CL        P                   <.<+<(
L                 11        6A                                  <-
R                :FIRST .7M IS 3C
/     1040  1070  30    3A21CL     <<CL        P CU     100      <-<+<(
L                 15        5A                                  <)
R                :2 BANDS OF 3C-UPPER ONE MEASURED  :SOME FE STAINING
/     1070  1100  29    3A10QZ     <<CL        P                     <)<+
```

```
                  11        6A                                  <.
R                :CL PRESENT BUT NOT IN FRAC'S
/    1100  1130  29    3A10QZ     <<CL        P                 <)<)
L                11        6A
/    1130  1160  29    3A20QZ     <<CL        P                 <*<)
L                09        6A
/    1160  1190  28    3G10QZ     <<CL        P                 <)<)B.B.
L                09        5A                                  <.
R                :FIRST .7M 3A - CONTACT GRADATIONAL  :LAST .1M 3F.
/    1190  1220  29    3F32CL     <<          P                 <)<)<)Q-
L                17        4G                                  <.    B.E-
R                :SOME INTERBEDDED 3G
/    1220  1250  28    3F22CL     <<          P                 <)<)<)<.
L                09        TG                                        <-
/    1250  1280  30    3F22CL     <<BR        P                 <)<+<*<-
L                11        TG                                        <.
/    1280  1310  29    3F11CL     <<          P                 <(<)<*<-
L                11        TA
R                :SOME INTERBEDDED 3G - PERHAPS A LITTLE 3E
/    1310  1340  28    3F22CL     <<          P                 <)<+<)<.
L                14        TG                                  <.    B-
R                :AS ABOVE - NO 3E
/    1340  1370  30    3E21CL     <<          P                 <)<+<)B.<.
L                21        AG                                  <-
R                :SOME 3F MIXED IN
/    1370  1400  28    3E32CL     <<          P                 <)<(<+<.B.
L                05        TG                                  <-    B-<.
R                :AS ABOVE
/    1400  1430  28    3F33MS     <<          P                 <)<+<)  B.
L                05        AT
R                :SOME 3E MIXED IN
/    1430  1460  28    3E22CL     <<          P                 <)<)<*B.
L                09        TA                                  <-
/    1460  1490  27    3E33MS     <<BR        P                 <-<+<+  B.
L                08        AT                                  <.
R                :SOME 3F MIXED IN
/    1490  1520  28    3E34MS     <<          P                 <.<)<+Q.<-
L                06        AT
/    1520  1550  29    3E33MS     <<          P                 <(<)<(B.<.
L                12        TG                                        <.
R                :HE GIVING OFF A BURGUNDY STREAK
/    1550  1580  29    3E32CL     <<          P                 <(<)<)<-<.
L                18        TG                                      <?
R                :TT GIVING OFF REDDISH-GRAY STREAK
/    1580  1610  27    3E48MS     <<          P                 <.<+<)Q-<.
L                06        TA                                  <.    <.
R                :HUGE PATCH OF CP AT 158.05M
/    1610  1640  29    3A30QZ     <<CL        P                   <)<=  B?
L                14        7A                                        B-
R                :SOME INTERBEDDED 3E  :HE MAY CONTAIN TT
/    1640  1670  28    3A30QZ     <<CL        P                   <)<=  Q-
L                17        7A                                        Q.
/    1670  1700  28    3A31QZ     <<CL        P                 <.<)<+  B.
L                08        6A
R                :FINAL METRE OF INT GRADATIONALLY GOES TO 2E
```

```
/    1700  1730  28    3A20QZ     <<CL        P            <)<+  <*
L                02        7A                                <.<-
R                :INTERBEDDED 3E
/    1730  1760  26    2G20QZ     <<          P            <)<+  <.
L                03        4A
R                :MAY BE HARD 2C
/    1760  1790  30    2C21QZ     <<          P          <.<*<+
L                05        AT
R                :ROCK SEEMS TO HAVE CHANGED FROM HARD 2G TO SOFTER 2C
/    1790  1820  28    2C22QZ     <<          P            <)<)B.<.
L                05        AT                           <.
/    1820  1850  28    2C44MS     <<BR        P            <.<+<=<.
L                03        AT                              <.
/    1850  1880  28    2C44MS     <<BR        P            <.<+<+  <.
L                06        AT                              <.
/    1880  1910  28    2C44MS     <<          P            <.<+<+
L                05        AT                         <.
/    1910  1940  28    2C43MS     <<          P            <.<)<+  Q.
L                14        AT                         <.      <.
R                :TT ONLY AT 192.0M
/    1940  1970  28    2C33MS     <<          P            <.<)<+<.
L                09        AT                              <.
/    1970  2000  29    2C43MS     <<          P            <.<+<=Q.
L                06        AT                         <.      <.
R                :GOOD CP AT END OF INTERVAL  :HE MAY CONTAIN TT
/    2000  2030  29    2C33MS     <<          P            <.<+<+<.<?
L                06        AT                              <.
/    2030  2060  29    2C44MS     <<          P            <.<+<+  <-
L                09        AT                              <.
/    2060  2090  28    2C45MS     <<          P            <.<=<+  <.
L                09        6T                                 <.
R                :HE MAY CONTAIN TT
/    2090  2110  19    2C44MS     <<BR        P            <.<=<+Q.<.
L                06        AT                           <.
/    2110  2140  28    2C45MS     <<BR        P            <.<+<+<)<(
L                06        AT                           <.
/    2110  2140  28    2C45MS     <<BR        P            <.<+<+<)<(
L                06        5T                              <.
R                :EXCELLENT CP AT START OF INT & TT IN MIDDLE OF INT.
/    2140  2170  29    2C34MS     <<          P            <.<+<+<<.
L                14        AT                              <.
/    2170  2200  28    2C44MS     <<          P            <.<+<)Q<.
L                03        AT                           <       <.
R                :HUGE PATCH OF CD AT 217.6M
/    2200  2230  30    2C44MS     <<          P            <.<)<+<<.
L                12        AT
R                :GOOD CD THROUGHOUT INTERVAL
/    2230  2260  29    2C45MS     <<BR        P            <.<+<=<.<.
L                06        AT
/    2260  2290  28    2C45MS     <<BR        P            <.<=<+<.<.
L                00        7T
/    2290  2320  26    2C55MS     <<BR        P              <+<=  <
L                03        6T                                 <.
R                :WELL BRECCIATED ROCK WITH GOOD TT
/    2320  2350  30    2C55MS     <<BR        P              <)<=  <)
```

```
L                21        ST                                  <.    <)
R               :MAY BE MORE TT THAN HE BUT DON'T WANT TO OVERESTIMATE
R               :.7M OF BC AT 229.6M WITH CB-QTZ AMYGDS
/    2350  2368  16    2C45MS     <<BR        P                <)<=<.<.
L                02        5T                                  <.    <.
/    2368  2432  51    8A10                   P CU    65       <)
L                18                                            <.    B.
R               :DYKE CHANGES ATO BC AT 240.0 WITH ALTERED FELDSPAR PHENOS
R               :FIRST PART OF DYKE CONTAINS SOME CL WITH MAINLY FELDSPAR
R               :PHENOS UP TO 1CM IN LENGTH
/    2432  2460  26    2C55MS     <<BR        P                <(<2  <.
L                17        5T                                      <-
R               :HE MAY CARRY TT
/    2460  2490  29    2C45MS     <<BR        P                <+<(
L                14        5T
/    2490  2520  29    2C45MS     <<BR        P                <+<+  <.
L                09        5T
/    2520  2550  28    2C34MS     <<BR        P                <+<+  <-
L                06        6T                                      <.<?
R               :SOME TYPE OF COATING ON TT-SOME LOOKS LIKE SL
/    2550  2580  29    2C34MS     <<BR        P                <)<* <?
L                12        6T                                      <?
R               :AS ABOVE
/    2580  2610  28    2C45MS     <<          P                <+<+  <.
L                06        6T                                      <?
R               :AS ABOVE-GIVES BROWNISH-BEIGE STREAK!
/    2610  2640  29    2C44MS     <<          P                <+<+
L                08        5T
/    2640  2670  28    2C44MS     <<          P                <+<+  <.
L                08        AT                                      <.
R               :AS ABOVE
/    2670  2700  27    2C34MS     <<          P                <)<+  <.
L                09        7T
/    2700  2730  28    2C44MS     <<          P                <)<)  <.
L                05        7T
/    2730  2760  29    2C24MS     <<          P                <)Q*<.<)
L                09        7T                                      <.
R               :EXCELLENT INTERVAL OF TT - CONTAINS LITTLE HE.
/    2760  2790  28    2C34MS     <<          P                <)<)B><-
L                05        8T
/    2790  2820  29    2C44MS     <<          P  <<   20  <(<*<+B.<.
L                20        AT
R               :CP & TT ONLY AT 281.1 M
/    2820  2850  29    2C45MS     <<BR        P              <.<)<+  <-
L                12        7T                           <.       <.
/    2850  2880  29    2C44MS     <<BR        P              <.<)<+<.<.
L                14        AT                           <.
R               :CP ONLY AT 287.9 M
/    2880  2910  29    2C45MS     <<BR        P                 <)<=  <-
L                08        6T                           <.
/    2910  2940  29    2C45MS     <<BR        P                 <+<+Q-<(
L                09        AT                           <.
R               :GOOD TT & CP IN MIDDLE OF INTERVAL
/    2940  2965  24    2C45MS     <<BR        P              <.<+<+  <.
L                14        7T
```

```
R                    :STRONGLY ALTERED ROCK AT END OF INTERVAL
/    2965   2991     24     2C55MS      <<BR          P            <.<)<)  Q.
L                     10          4T                                    Q-
R                    :EXTREME BRECCIATION & ALT'N
/    2991   3039     47     8A10QZ      <<            P  CU          <)
L                     26          6G                          <.
R                    :DYKE CONTAINS MAINLY QTZ - CL PHENOS
R                    :FROM 299.6M 8A CONTAINS BLEACHED 8C FOR 1.9M - 8C CONTAINS
R                    SOME FRAGMENTS OF 2C AND THE UPPER CONTACT IS IRREGULAR - COLOR
R                    IS CREAMY TO 6G - LOWER CONTACT ALSO GRADATIONAL WITH SLIGHT ALT
/    3039   3042     03     2C55MS      <<BR          P  CU   140   <.<+<=
L                     00          6T                          <.
R                    :SMALL SAMPLE BECAUSE BTWN 2 DYKES
/    3042   3057     14     8C21QZ      <<            P  CU    55     <-<.
L                     03          9T
R                    :BOTTOM CONTACT NOT MEASURED DUE TO BROKEN CORE
/    3057   3072     10     2C45MS      <<            P              <)<+
L                     00          6T
R                    :CORE VERY BROKEN - SOME 8C MIXED IN
/    3072   3101     29     8C10QZ      <<            P              <)Q.
L                     15                                      <.
R                    :QZ AND CB AMYGDS  :COLOR FROM CREAM TO GRAY TO PALE GREEN
R                    :MANY CB AMYGDS WEATHERED OUT
/    3101   3109     07     2C45MS      <<BR          P            <.<)<)  <.
L                     02          6T                          <.
R                    :HOLE ENDED ON DRILLER'S CONVENIENCE - STILL HIGH ALT & VISIBLE
R                    TT
R                    :END OF HOLE AT 310.9M - END OF LOG - BACK TO SCHOOL!
A001
ALAB                 EQUITY MINESITE LABORATORY
ATYP                 ASSAY
AMTH                 WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM                 RCOVSAMPLE   ROD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R       00     61    :TRICONED - NO CORE
A001    61    105          7424        0.070    0.5 0.120 0.01  0.005 3.710 0.010
A001   105    127          7425        0.11     0.5 0.08  0.01  0.005 3.35  0.005
R      127    140    :MISLATCH - NO RECOVERY
A001   140    170          7426        0.13     0.5 0.08  0.005 0.005 3.33  0.005
A001   170    200          7427        0.07     0.5 0.03  0.01  0.005 3.44  0.005
A001   200    230          7428        0.06     0.5 0.03  0.005 0.005 3.72  0.005
A001   230    260          7429        0.06     0.5 0.02  0.005 0.005 2.51  0.005
A001   260    290          7430        0.04     0.5 0.02  0.005 0.005 2.29  0.005
A001   290    320          7431        0.03     0.5 0.03  0.005 0.005 3.49  0.005
A001   320    350          7432        0.15     0.5 0.09  0.005 0.005 3.18  0.005
A001   350    380          7433        0.09     0.5 0.04  0.005 0.005 3.02  0.005
A001   380    410          7434        0.07     0.5 0.04  0.005 0.005 3.38  0.03
A001   410    440          7435        0.07     0.5 0.04  0.01  0.005 3.53  0.005
A001   440    470          7436        0.06     0.5 0.04  0.01  0.005 3.09  0.005
A001   470    500          7437        0.14     0.5 0.09  0.005 0.005 3.48  0.005
A001   500    530          7438        0.17     0.5 0.07  0.01  0.005 4.87  0.005
A001   530    560          7439        0.09     0.5 0.04  0.005 0.005 3.53  0.005
A001   560    590          7440        0.05     0.5 0.02  0.005 0.005 3.39  0.005
A001   590    620          7541        0.07     0.5 0.01  0.005 0.005 3.62  0.005
A001   620    650          7542        0.05     0.5 0.005 0.005 0.005 4.20  0.005
A001   650    680          7543        0.04     0.5 0.005 0.005 0.005 3.18  0.005
```

A001	680	710	7544	0.04	0.5	0.005	0.005	0.005	3.37	0.005
A001	710	740	7545	0.04	0.5	0.005	0.005	0.005	3.44	0.005
A001	740	770	7546	0.17	0.5	0.01	0.01	0.005	3.75	0.005
A001	770	790	7547	0.13	0.5	0.02	0.01	0.005	3.94	0.005
R	790	801	:DYKE - NO SAMPLE							
A001	801	830	7548	0.13	0.5	0.03	0.01	0.005	3.79	0.005
A001	830	860	7549	0.10	0.5	0.05	0.005	0.005	4.37	0.005
A001	860	890	7550	0.09	0.5	0.03	0.01	0.005	3.62	0.005
A001	890	920	7551	0.09	0.5	0.07	0.005	0.005	1.55	0.005
A001	920	950	7552	0.07	0.5	0.02	0.005	0.005	1.90	0.005
A001	950	980	7553	0.06	0.5	0.03	0.005	0.005	1.93	0.01
A001	980	1010	7554	0.11	0.5	0.005	0.005	0.005	1.67	0.005
A001	1010	1040	7555	0.05	0.5	0.01	0.005	0.005	1.87	0.01
A001	1040	1070	7556	0.04	0.5	0.01	0.005	0.005	2.11	0.005
A001	1070	1100	7557	0.04	0.1	0.02	0.005	0.001	1.17	0.005
A001	1100	1130	7558	0.05	0.1	0.02	0.005	0.001	1.60	0.005
A001	1130	1160	7559	0.03	0.1	0.01	0.005	0.001	1.01	0.005
A001	1160	1190	7560	0.12	0.1	0.03	0.02	0.001	1.61	0.005
A001	1190	1220	7561	0.12	0.1	0.09	0.005	0.001	2.87	0.005
A001	1220	1250	7562	0.29	0.1	0.08	0.03	0.001	3.66	0.005
A001	1250	1280	7563	0.07	0.1	0.03	0.001	0.001	3.16	0.005
A001	1280	1310	7564	0.16	0.1	0.04	0.005	0.001	2.63	0.005
A001	1310	1340	7565	0.05	0.1	0.04	0.005	0.001	2.81	0.001
A001	1340	1370	7566	0.04	0.1	0.03	0.005	0.001	3.65	0.001
A001	1370	1400	7567	0.13	0.1	0.06	0.005	0.001	3.40	0.005
A001	1400	1430	7568	0.04	0.1	0.02	0.005	0.001	3.16	0.02
A001	1430	1460	7569	0.08	0.1	0.06	0.005	0.001	3.46	0.005
A001	1460	1490	7570	0.08	0.5	0.04	0.005	0.001	4.50	0.005
A001	1490	1520	7571	0.08	0.5	0.02	0.03	0.001	3.67	0.005
A001	1520	1550	7572	0.05	0.5	0.03	0.005	0.001	2.51	0.005
A001	1550	1580	7573	0.13	3.0	0.04	0.02	0.001	3.57	0.005
A001	1580	1610	7574	0.14	4.0	0.02	0.02	0.001	4.31	0.005
A001	1610	1640	7575	0.05	10.0	0.05	0.03	0.001	3.86	0.005
A001	1640	1670	7576	0.02	0.5	0.01	0.005	0.001	3.62	0.005
A001	1670	1700	7577	0.05	3.0	0.03	0.03	0.001	5.54	0.005
A001	1700	1730	7578	0.16	36.0	0.08	0.09	0.005	5.80	0.40
A001	1730	1760	7579	0.06	4.0	0.03	0.03	0.001	4.00	0.005
A001	1760	1790	7580	0.02	0.5	0.02	0.005	0.001	5.55	0.005
A001	1790	1820	7581	0.16	8.0	0.16	0.05	0.02	3.76	0.02
A001	1820	1850	7582	0.16	10.0	0.17	0.06	0.02	5.79	0.02
A001	1850	1880	7583	0.15	6.0	0.21	0.05	0.01	5.03	0.02
A001	1880	1910	7584	0.02	0.5	0.06	0.02	0.005	5.39	0.005
A001	1910	1940	7585	0.05	4.0	0.05	0.02	0.005	4.38	0.005
A001	1940	1970	7586	0.08	4.0	0.04	0.02	0.005	3.57	0.005
A001	1970	2000	7587	0.08	5.0	0.04	0.03	0.005	9.12	0.005
A001	2000	2030	7588	0.07	3.0	0.03	0.02	0.005	5.60	0.005
A001	2030	2060	7589	0.10	10.0	0.05	0.04	0.01	5.29	0.04
A001	2060	2090	7590	0.10	5.0	0.04	0.03	0.01	5.03	0.02
A001	2090	2110	7591	0.13	4.0	0.03	0.01	0.005	4.42	0.005
A001	2110	2140	7592	2.89	49.0	0.13	0.04	0.08	5.68	0.04
A001	2140	2170	7593	0.21	13.0	0.04	0.01	0.005	4.03	0.005
A001	2170	2200	7594	0.13	9.0	0.05	0.005	0.01	3.66	0.01
A001	2200	2230	7595	0.31	9.0	0.06	0.01	0.005	4.35	0.005
A001	2230	2260	7596	0.09	7.0	0.17	0.01	0.005	7.59	0.005
A001	2260	2290	7597	0.15	9.0	0.05	0.02	0.01	3.78	0.005

A001	2290	2320		7598	0.23	126.0	0.19	0.10	0.04	7.18	0.07
A001	2320	2350		7599	0.95	139.0	0.18	0.37	0.19	6.64	0.16
A001	2350	2368		7600	0.45	62.0	0.22	0.09	0.05	9.71	0.04
4	2368	2432	:DYKE - NO SAMPLE								
A001	2432	2460		7601	0.13	38.0	0.43	0.08	0.06	16.90	0.05
A001	2460	2490		7602	0.01	4.0	0.12	0.01	0.005	7.51	0.02
A001	2490	2520		7603	0.05	2.0	0.07	0.01	0.005	4.40	0.03
A001	2520	2550		7604	0.03	4.0	0.03	0.02	0.001	5.00	0.37
A001	2550	2580		7605	0.03	7.0	0.04	0.02	0.005	2.99	0.50
A001	2580	2610		7606	0.02	3.0	0.03	0.005	0.001	4.24	0.33
A001	2610	2640		7607	0.001	0.5	0.04	0.005	0.001	6.19	0.005
A001	2640	2670		7608	0.005	0.5	0.01	0.005	0.001	5.02	0.09
A001	2670	2700		7609	0.005	0.5	0.02	0.005	0.001	4.35	0.05
A001	2700	2730		7610	0.02	8.0	0.01	0.005	0.001	2.83	0.005
A001	2730	2760		7611	0.33	62.0	0.02	0.10	0.05	0.96	0.06
A001	2760	2790		7612	0.06	2.0	0.03	0.20	0.001	2,81	0.005
A001	2790	2820		7613	0.02	0.5	0.11	0.005	0.005	4.38	0.005
A001	2820	2850		7614	0.24	18.0	0.08	0.09	0.03	3.20	0.03
A001	2850	2880		7615	0.04	2.0	0.08	0.02	0.005	4.33	0.005
A001	2880	2910		7616	0.04	7.0	0.03	0.02	0.001	4.36	0.005
A001	2910	2940		7617	0.39	97.0	0.11	0.13	0.05	4.83	0.04
A001	2940	2965		7618	0.11	63.0	0.09	0.06	0.001	5.28	0.02
A001	2965	2991		7619	0.29	64.0	0.12	0.15	0.02	9.57	0.06
R	2991	3039	:DYKE - NO SAMPLE								
A001	3039	3042		7620	0.005	8.0	0.06	0.005	0.005	5.48	0.005
R	3042	3057	:DYKE - NO SAMPLE								
A001	3057	3072		7621	0.005	2.0	0.11	0.02	0.02	5.33	0.005
R	3072	3101	:DYKE - NO SAMPLE								
A001	3101	3109		7622	0.001	3.0	0.17	0.005	0.001	3.58	0.005
R			:END OF HOLE - END OF ASSAYS								
R			END OF ASSAYS - END OF LOG								

To Southern Tail Pit

X86CH239
X86CH238
X86CH261
X86CH260
X86CH274
X86CH273
X86CH262
X86CH240
X86CH272
X86CH263
X86CH264
X86CH265
X86CH266
X86CH267
X86CH268
X86CH271
X86CH269
X86CH270

1200 m
1250 m
1300 m
1150 m
1100 m
1200m
1300 m
250 m

6200 N
6000
5800
5600
5400
5200 N

SG 20
SG 19
SG 30
SG 22
SG 21
SG 32
SG 24
SG 23
SG 34

UNIT 3
UNIT 2

Superstition Creek

To Buck Creek

7400 E
7600
7800
8000 E

0 100 200
METRES

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,379

FIGURE 4. DIAMOND DRILLHOLE LOCATIONS

EQUITY SILVER MINES LIMITED
MINESITE PROPERTY
GROUP 86-2 ASSESSMENT REPORT