84-995-15493

ASSESSMENT REPORT

1986 GEOLOGICAL MAPPING, GEOCHEMICAL AND

GEOPHYSICAL SURVEYS

on the

KERR CLAIM GROUP #1866

NTS 104B/8W,8E

SKEENA MINING DIVISION

operated and owned by Western Canadian Mining (WCM) Ltd.

~~operated by Cassiar Mining Corporation~~

Author: R.E. Meyers
Date: December, 1986
NTS: 104B/8W,8E
Commodities: Au, Ag, Cu, Pb, Zn
Latitude: 56° 28' North
Longtitude: 130° 16' West
Report No: 962

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SUMMARY

Surface exploration was carried out in 1986 on the Kerr Claims to confirm and follow-up anomalous gold geochemical results delineated during the 1985 program.

Detailed geological mapping and geochemical sampling were carried out to investigate controls on alteration and mineralization and to establish new and more detailed gold targets. A total of 1,242 rock, talus and soil samples were systematically collected on east-west grid lines. The geological and geochemical activities were supplemented by preliminary magnetometer and VLF-EM surveys.

Results of the program generally confirmed the 1985 anomalies and outlined a new anomaly (Zone L). The best gold targets are on Zone A, with secondary targets on Zones B, L and F. Zone C was not explored in detail in 1986, but is still considered an important target to be re-examined in the future. Zone D results were not particularly encouraging, however, areas adjacent to this zone warrant investigation.

CONCLUSIONS

Important gold targets exist on the Kerr Claims that are worthy of additional surface follow-up work, as well as consideration for diamond drilling.

The results of detailed mapping and sampling indicate that much of the gold mineralization is concentrated in irregular and discontinuous quartz-sulphide veins and vein stockwork zones. At the property scale, mineralization is confined to a north-south trending zone of highly altered and intensely sheared volcanic, sedimentary and intrusive rocks, that have been metasomatized to form pyritic sericite schists.

On a larger scale, mineralization was likely concentrated as a result of hydrothermal activity in paleo-epithermal centres, which may have been deformed and possibly re-activated during regional tectonism.

RECOMMENDATIONS

A comprehensive surface follow-up program, combined with diamond drilling, is recommended for the Kerr Claims to effectively evaluate its precious metals potential. The required budget for this work is in the order of $400,000. The following items should be considered as an essential framework to the program:

A: Surface

1. Geochemical soil and talus grid sampling should be extended, at a minimum of 25 m spacing, in the area south of Zone L and possibly north and east of Zones C and D. Particular emphasis should be placed on covering the marginal areas of the sericite schist zone.

2. Detailed rock chip sampling* should be continued south and north of Zone A, and across Zone L. Closely spaced east-west rock chip sample lines are recommended.

3. Additional and more precise geophysical surveys should be considered and should include a detailed Proton Magnetometer survey (10 m spacing) and a Max-Min or Genie EM survey (100 m separation). The detailed mag survey may be useful in outlining unrecognized intrusive bodies and assist in delineating alteration intensities. A Genie EM survey would be useful in detecting appreciable near-surface sulphide concentrations (50 m penetration).

B: Diamond Drilling

A program of approximately 2000 m of diamond drilling is recommended for the Kerr Claims. Drilling should be initially concentrated

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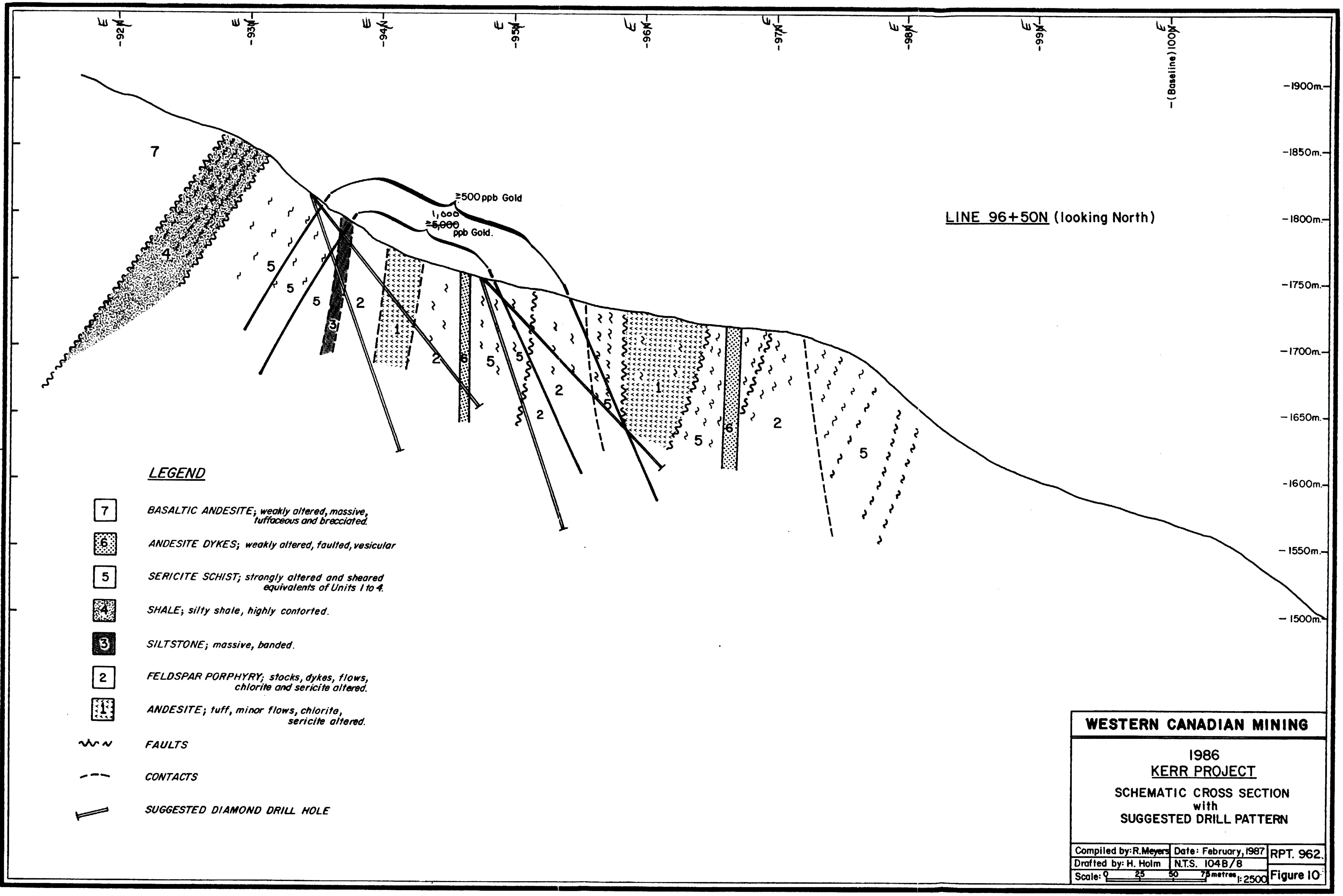
* Hand trenching in talus, of the type done in 1985, should be avoided as a sampling method wherever possible. Material obtained by this method is usually deeper talus, not outcrop, and should not be treated as outcrop. Gold values returned from such samples may be misleading and are difficult to assess.

in Zone A, where the best known gold targets presently occur and can be commenced concurrently with surface work in other areas.

1. Zone A: A fence-like cross-sectional drill pattern (Figure 10) should be utilized and should be completed on at least two sections. Holes can be staggered or offset, but should be placed to obtain complete cross-sectional information over the width of the +500 ppb gold anomaly. Holes should have a planned minimum depth of 200 m and should be laidout to intersect the anomalous zones at up to 150 m below surface. Eight 200 m holes are recommended in the pattern suggested in Figure 10 (four holes per section).

2. Zones L and C: As detailed surface information becomes available from these zones, a drill pattern can be designed to suit the anomalies. Holes should intersect the full width of the anomalies and penetrate the border zones of the sericite schist. At least 400 m of drilling should be considered for these zones.


92N-E
93N-E
94N-E
95N-E
96N-E
97N-E
98N-E
99N-E
100N-E
(Baseline)
1900m.
1850m.
1800m.
1750m.
1700m.
1650m.
1600m.
1550m.
1500m.
≥500 ppb Gold
1,000
≥5,000
ppb Gold.
LINE 96+50N (looking North)
LEGEND
7 BASALTIC ANDESITE; weakly altered, massive, tuffaceous and brecciated.
6 ANDESITE DYKES; weakly altered, faulted, vesicular
5 SERICITE SCHIST; strongly altered and sheared equivalents of Units 1 to 4.
4 SHALE; silty shale, highly contorted.
3 SILTSTONE; massive, banded.
2 FELDSPAR PORPHYRY; stocks, dykes, flows, chlorite and sericite altered.
1 ANDESITE; tuff, minor flows, chlorite, sericite altered.
FAULTS
CONTACTS
SUGGESTED DIAMOND DRILL HOLE
WESTERN CANADIAN MINING
1986
KERR PROJECT
SCHEMATIC CROSS SECTION
with
SUGGESTED DRILL PATTERN
Compiled by: R. Meyers
Date: February, 1987
RPT. 962.
Drafted by: H. Holm
N.T.S. 104B/8
Scale: 0 25 50 75 metres 1:2500
Figure 10
NCI-351

INTRODUCTION

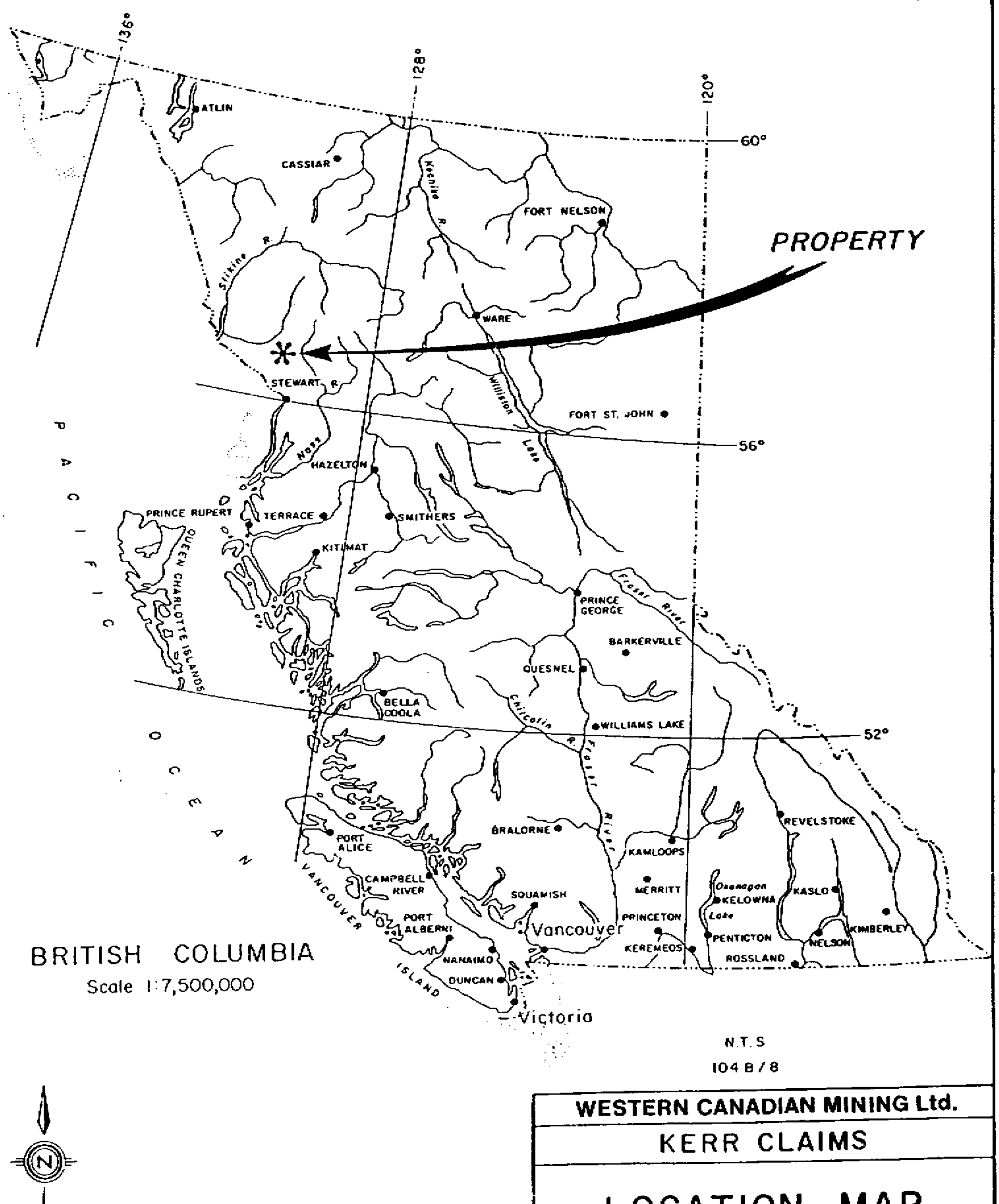
Location, Access and Terrain

The KERR claims are situated at the eastern edge of the northern Cordillera, approximately 65 km northwest of Stewart, B.C. at 56°28' north latitude and 130°16' west longtitude, in the Skeena Mining Division (NTS 104 B/8W, Figure 1). The property lies 45 km west of the Stewart Cassiar highway and about 55 km south of Bob Quinn Lake. Access to the claims is by fixed wing aircraft (scheduled flights in summer) to Snippaker Creek airstrip, south of the Iskut River and thence by helicopter to the claims.

The claims lie in extremely steep alpine-type mountainous terrain on the south side of Sulphurets Creek, east of the confluence of Sulphurets Creek and the Unuk River. The Sulphurets Glacier borders the property on the south, east and northeastern sides. Most of the property is above tree line, with elevations ranging from 900 metres to 1925 metres. Vegetation consists of alpine grasses, with dwarfed conifers, alder and willow.

History

Interest in the area around Sulphurets Creek dates back to the late 1800's and early 1900's when extensive placer prospecting was carried out by groups such as the Daily Syndicate, the Hammond Dredging Company and the Unuk River Gold Syndicate. In 1905 F.E. Wright of the USGS reported on the placer potential of Sulphurets Creek, as well as the presence of well mineralized veins bearing Au, Ag and Pb. In 1923,



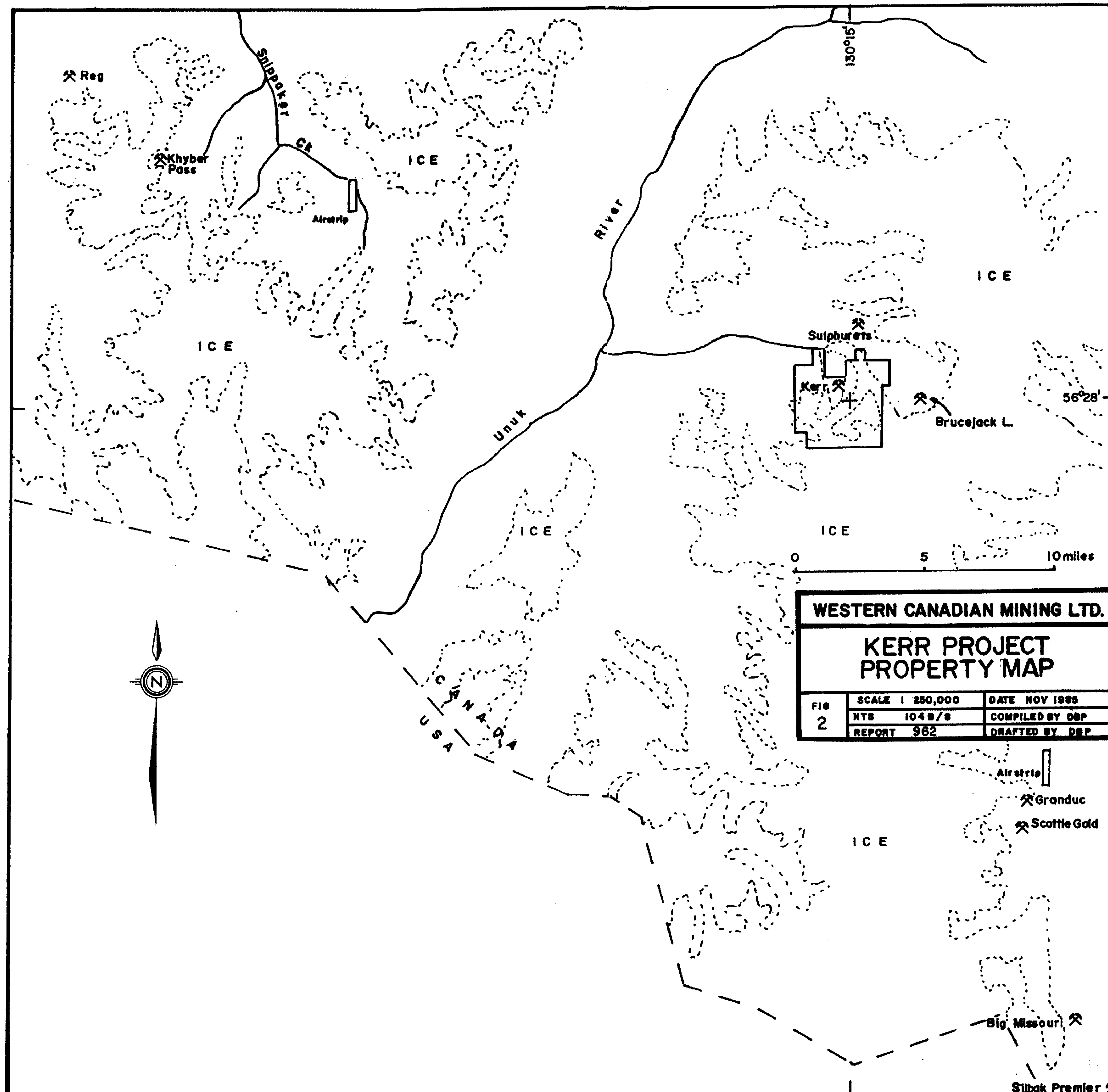
N.T.S
104 B / 8

WESTERN CANADIAN MINING Ltd.			
KERR CLAIMS			
LOCATION MAP			
DRAWN	WORK BY	DATE NOV. 1984	FIGURE 1
Revised			

G.E. King, while working for the International Boundary Survey, reported on the favourable intrusive and volcanic geology of the Sulphurets area. He suggested that it was on the same "contact" and held similar potential to the Premier gold camp near Stewart (King 1935). In the 1930's more placer activity was attempted, but prospectors were discouraged by the remoteness of the area, difficulty of access and short field season. In 1960 Newmont Mines carried out airborne and ground geophysical and geological surveys leading to the staking of the Sulphurets claims near Brucejack Lake for Granduc Mines Ltd. Newmont and Granduc carried on property work through the 1960's, along with other operators such as Phelps Dodge Corp. of Canada (1962) and the Meridian Syndicate (1965). The Sulphurets property was optioned to Esso Resources Canada Ltd. in 1979, who expended more than $2 million on precious metals exploration. In 1985 Newhawk Mines Ltd. and Lacana Mines Ltd. optioned the Sulphurets claims from Granduc and for the past two years have carried out an aggressive surface and underground (1986) exploration program. The most recently reported gold reserves are in the order of 1.5 M tonnes grading 0.34 oz/t Au.

The KERR claims (Figure 2) were originally staked by the Alpha Joint Venture in 1982 to a cover zone of alteration adjacent to the Sulphurets property. Anomalous gold geochemical values obtained in 1983 prompted Brinco Limited to option the property in 1984. In 1985 a comprehensive exploration program was funded, which included geological mapping, geochemical sampling, trenching and rock chip sampling, followed by the drilling of 3 short diamond drill holes.

The program was encouraging in that 4 notable gold geochemical talus/soil anomalies (>1000 ppb) were outlined and high grade gold



WESTERN CANADIAN MINING LTD.		
KERR PROJECT PROPERTY MAP		
FIG 2	SCALE 1:250,000	DATE NOV 1986
	NTS 104B/8	COMPILED BY DBP
	REPORT 962	DRAFTED BY DBP

values (e.g. 10,100 ppb and 5.76 oz/t Au) were obtained by trench sampling. Diamond drill results were somewhat less encouraging. Although drill results verified the gold anomalies, gold values were substantially lower than anticipated from trenching and geological results.

Claims Status

In 1986, 100% ownership in the KERR claims was transferred from Brinco Limited to Western Canadian Mining Corporation (WCM). With the application of the 1986 assessment work, all claims in the KERR Group #1866 are in good standing until 1993 (Kerr, 7,8,9,10,12,15,41) and KERR 99 claim is in good standing until 1989.

CLAIM	RECORD #	UNITS	HECTARES	EXPIRY DATE
Kerr 7	3662	6	150	17/12/93
Kerr 8	3663	16	400	17/12/93
Kerr 9	3664	10	250	17/12/93
Kerr 10	3665	9	225	17/12/93
Kerr 12	3666	20	500	17/12/93
Kerr 15	3669	16	400	17/12/93
Kerr 41	3697	20	500	20/12/93
Kerr 99	4690	20	500	30/10/89

CLAIM GROUPING

KERR 7,8,9,10,12,15,41 KERR GROUP # 1866

A Statement of Costs for the 1986 exploration program is found in Appendix 1.

1986 Exploration Program

The 1986 exploration program was carried out between July 11th and August 22nd. Objectives of the program were to verify and follow up the 1985 results; to establish new and more detailed gold targets; and to attempt to determine the geological controls on mineralization.

Activities were carried out initially with a crew of four, later reduced to three, from a camp located on the claims. A grid was established with a north-south baseline running along the eastern margin of the sericite schist zone (see property geology). East-west grid lines are spaced at 100 metre intervals along the baseline covering the essential parts of the schist zone, including the 1985 geochemical anomalies. Work consisted of geochemical rock, talus and soil sampling, geophysical surveys (VLF & Mag) and detailed geological mapping in selected gold anomalous areas.

REGIONAL GEOLOGY

The Kerr property lies adjacent to the eastern margin of the Coast Plutonic Complex, near the western edge of the Bowser Basin (Figure 3). The claims are at the northern end of a belt of rocks described by Grove (1971) as the Stewart Complex. The complex consists of an undivided group of sedimentary and volcanic rocks of Upper Triassic and Jurassic age, which are intruded by middle Mesozoic marginal phases of the Coast Range intrusions.

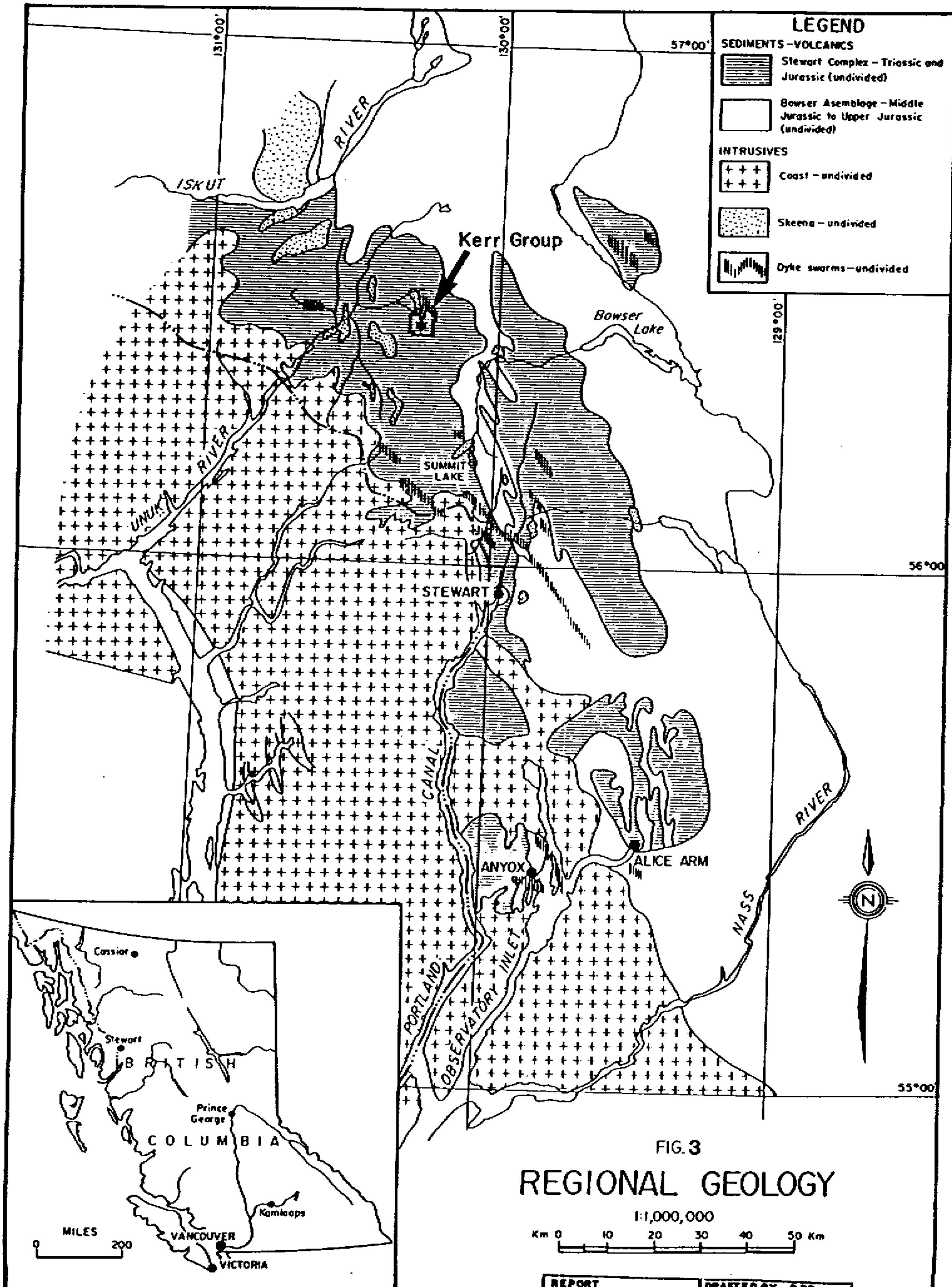


FIG. 3

REGIONAL GEOLOGY

Regionally, the Stewart Complex dips beneath the Middle to Upper Jurassic Bowser Group and forms an integral part of the Bowser Basin. The stratified rocks are composed of submarine and subaerial fragmental volcanic rocks that are interlayered with sequences of argillite, siltstone, greywacke, conglomerate and minor impure limestone, most of which are believed to be correlative with the Lower Jurassic Hazelton Group. Some of the lowermost members may correspond to the Upper Triassic Stuhini and King Salmon Groups, which also occur in the region.

The stratigraphy is intruded by subvolcanic intrusives and by mid to late Mesozoic and Cenozoic plutonic rocks. These include stocks and dykes of granodiorite, quartz monzonite, syenodiorite and feldspar porphyry, as well as late Tertiary dykes and plugs of basalt and diorite.

PROPERTY GEOLOGY

General

Property wide geological mapping at 1:5000 scale was carried out on the KERR claims in 1985 (Figure 4). On the basis of that mapping and the 1985 geochemical results, selected areas were mapped at 1:2500 (Figure 5). The prime purpose of this was to establish geological controls on gold mineralization. In most cases lithological units have been reinterpreted with respect to rock type, alteration and origin.

The areas mapped in 1986 lie entirely within the "tectonized shear zone" outlined in 1985. This zone contains all of the significant gold anomalies known to date on the property. It covers an elongate northerly trending area, averaging 800-900 metres in width, at least 2 km in length and transects the central part of the KERR property. The most continuous cross-sectional exposure of the zone is in the central area covering geochemical anomalies A to C.

Borders of the zone are sharp to gradational and are poorly exposed due to widespread talus, felsenmeer and overburder cover. The zone is flanked by comparatively unaltered or weakly altered, fine grained, brownish green clastic sediments and submarine volcanic rocks on the east, and by a thick unit of basaltic andesite on the west.

The tectonized zone is typically composed of moderately to strongly altered and sheared rocks interpreted to be of volcanic and subvolcanic or plutonic origin. About 75-80% of the zone is best described as a sericite schist. However, isolated blocks enclosed within the schist are disoriented, but notably less altered and deformed to the extent that primary lithologies are recognized. They include andesite tuff and flows, and feldspar porphyry stocks, dykes and possibly flows. A later formed "swarm" of fine grained, weakly altered andesite dykes cross-cuts the schistosity. The dykes have subsequently been dissected and offset by later faults which post-date schist development. Minor sections of silty shale and siltstone occur on the western margin of the zone and are likely to be part of the same stratigraphic package that occurs on the eastern side of the zone.

Lithology

Rock units mapped within the schist zone are listed below and their distribution shown in Figure 5. Relative ages are interpreted from observed geological relationships and the inferred sequence of alteration.

Table of Lithologies

Unit 7	Basaltic Andesite
Unit 6	Andesite Dykes
Unit 5	Sericite Schist
Unit 4	Shale
Unit 3	Siltstone
Unit 2	Feldspar Porphyry
Unit 1	Andesite

Unit 1 Andesite

Rocks in this unit are predominantly medium yellow-green to dark green, fine to medium grained tuffs. Massive, non-fragmented sections comprise a much smaller proportion of the unit. Most fragmental rocks are non-layered, ranging from ashy tuffs (fragments < 4 mm), to ash-lapilli tuffs (fragments > 4 mm). Lamellar tuffaceous layering (< 1 cm) is present at a few localities, with fragments oriented in the plane of layering. In areas where minor brecciation has occurred, tuffaceous textures are visible in some breccia fragments. Massive andesite is generally fine grained, moderately to well jointed, making up less than 30% of the unit. Typically, massive andesites are interlayered with tuffs, have poorly defined contacts and usually grade laterally and vertically into fragmental sections.

Chlorite is the dominant alteration in andesite, with variable amounts of sericite and local silicified sections. As the extent and intensity of alteration increases, chlorite gives way to sericite and the schistosity becomes more pronounced. Ultimately, the altered volcanic grades into sericite schist.

Unit 2 Feldspar Porphyry

This unit is intermediate in composition and chemically it is likely quite similar to the andesitic rocks. Textures range from medium grained, subequigranular to porphyritic. The coarser grained equigranular sections are hornblende-bearing, have a distinct intrusive character and predominate in the central part of the schist zone as irregular stock-like masses. In other areas, coarse plagioclase phenocrysts occur in a medium to dark green, fine grained andesitic matrix. Phenocrysts are < 4 mm to > 1.5 cm in length and, at some localities, are aligned in a preferred orientation parallel to contacts, suggesting a flow orientation mechanism.

As with the andesites, alteration in this unit is variable, with increased sericite content as alteration and deformation increase. Contacts are commonly gradational with sericite schist.

Unit 3 Siltstone

A narrow band (± 10 m) of weakly laminated siltstone occurs near the western margin of the schist zone, in the area of zone A. The unit is discontinuous and outcrops with relatively poor exposure. Banding is diffuse, but ranges from < 1 cm to > 3 cm. Graded bedding is indistinct at this locality. At zone F, to the south, a relatively thick section of impure brownish grey silty sediments lies west of the schist zone boundary. Only very minor portions of this unit display weak evidence of bedding and in general, the unit is quite massive. Alteration is generally weak throughout.

Unit 4 Shale

This unit was observed at only one locality, in the footwall of the thrust fault west of zone A. The section is somewhat contorted, but foliation trends subparallel to the fault plane. The shale is fine grained, dark grey-brown, weakly phyllitic, with a silty or gritty texture. As is typical of many shale deposits, a talus bank is formed at the base of the unit, concealing the location and character of its lower contact. The upper contact is the west-dipping thrust plane.

Unit 5 Sericite Schist

As described earlier, sericite schist occupies most of the tectonized zone. It is a metasomatic "alteration unit" derived from the volcano-sedimentary assemblage. The unit is composed of rusty weathering, yellow-orange to yellow-green, moderately to strongly foliated rock with up to 5% finely disseminated pyrite. Chlorite, quartz, residual feldspar, minor carbonate and talc (apophyllite?) are accessory minerals. The unit has sharp to gradational contacts with less altered rocks. At some localities, shear offsets have juxtaposed the schist into contact with comparatively fresh andesitic rocks. In other areas, where schistosity is weak, primary volcanic textures and relict minerals (feldspar, hornblende) are visible in spite of intense alteration.

Unit 6 Andesite Dykes

Several weakly altered, chloritic andesite dykes occur as crosscutting features within the schist zone. They are fine grained, dark green, well fractured and some display crudely developed columnar jointing. Some dykes have well displayed vesicular zones and weakly chilled margins. Most are segmented and offset by post-schist faulting. The fact that they are only weakly altered, cross-cut highly altered and schistose rocks, and are subsequently offset by later structures, rules out the likelihood that they are andesite feeders to the immediate volcanic stratigraphy.

Unit 7 Basaltic Andesite

This unit was mapped in 1985 as the dominant volcanic member of the "upper sequence" (Figure 4) and was not remapped in detail in 1986. The unit lies to the west of the schist zone and forms the hanging wall of the west dipping thrust fault. The lower part of the unit, above the fault is tuffaceous, with 1 mm to 3 cm lapilli oriented parallel to weakly developed layering or foliation. Fragments are buff coloured in a slightly sheared chloritic matrix. Overlying the tuffaceous rocks are massive and brecciated sections of similar lithology.

Structure

The main foliation trends within the schist zone strike northwesterly to east-west. True bedding orientations were rarely observed. Of these, the majority have a northerly strike, the exception being east-west striking tuff beds near the eastern margin of the schist zone. To the east, the volcano-sedimentary sequence strikes northeasterly and is oriented obliquely to the main trend of the shear zone. This may reflect a fault truncation, although well defined offsets, or abrupt termination of units has not been observed. To the west, the basaltic andesite rests unconformably on a northwest trending thrust fault, which dips moderately to the west. Some textures observed in the tuffaceous hanging wall rocks may be cataclastic in origin. A possible extension of the thrust fault was mapped by Kirkham (1963; personal communication 1986) on the north side of Sulphurets Creek.

Within and adjacent to the boundaries of the schist zone, minor faults and offsets are in evidence at several localities. The dislocation of andesite dykes and the juxtapositioning of highly altered and deformed schists against relatively unaltered volcanic and intrusive rocks have resulted from late fault movements post-dating schist development. Schistosity orientations at some localities contrast noticeably with orientations in adjacent areas. This, along with contortions and minor folds in the foliation, suggest that entire blocks of altered and deformed rock were differentially sheared and rotated as a result of late stage shear stresses which were active after the main schistosity had developed.

Mineralization

Mineralization takes the form of quartz-sulphide veins, stockworks and disseminated sulphides. Veining has accompanied the development of sericitization and silicification to the extent that disseminated and vein material are an integral part of the alteration assemblage. Veins range in width from a few millimetres to several centimetres and may be cross-cutting or intrafolial. One exceptional pyrite vein (4 m width) occurs in a shear zone at zone D (L 102 N, 95 + 75 E). Unfortunately, chip samples from this vein returned fairly low, unencouraging gold values. In many cases the quartz-sulphide veins are strongly leached of their sulphide content, leaving only a rusty quartz-rich boxwork and an array of cubic pyrite casts in the wall rock. Pyrite is the most common and abundant sulphide and is ubiquitious within the schist zone. It occurs as widespread disseminations and localized vein-stockwork zones. Chalcopyrite occurs with pyrite at a few localities in small quartz-pyrite stockworks. Minor malachite is visible at the margins of some chalcopyrite-bearing veins. Where stockwork veining is intense, whole-sale silicification of the wall rock is common. Clay alteration also occurs adjacent to some larger quartz-pyrite veins (> 2 cm). The clay minerals (kaolinite, illite?) are cream-white with a yellowish tinge and appear to be intergrown with sericite ± chlorite. Calcite occurs with a few veins, but is generally not a common alteration mineral at the Kerr.

Sphalerite, galena and hematite were reported in polished thin section descriptions in 1985 (Epp, 1985). These minerals were not observed macroscopically in 1986, although minor anomalous values in lead and zinc are present (Appendix 1).

Gold mineralization on the Kerr property is primarily associated with quartz-pyrite veins. Many such veins are intrafolial and sub-conformable to schistosity, although some veins are cross-cutting and associated with shears and localized stockworks. At surface, most veins are strongly weathered and leached and it is apparent that gold is residual during the leaching process. It should also be noted that gold may conceivably become concentrated during weathering, therefore, caution should be exercised in evaluating surface gold values from these veins.

The distribution of gold from detailed rock chips and talus/soil sampling is discussed in the next section under Geochemistry.

GEOCHEMISTRY

Procedures

Geochemical sampling was carried out in 1986 to confirm and follow up the anomalies outlined in 1985. A total of 1242 samples were collected, including 649 rock chips and 593 soil and talus samples (Figures 6a-c, 7a-c, 8a-c). Soil and talus samples were collected along grid lines at 25 metre intervals over the entire grid. Detailed rock chip samples were taken along continuous lines (where possible) at 3 metre intervals on zones A/E, F and D, and a detailed soil grid was extended over zone F. During geological mapping, selected vein samples were collected to compare with data from the rock chip sample results.

Soil and talus samples (0.5 kg) were collected in wet-strength Kraft paper sample envelopes. Rock samples (1.5 - 2.0 kg) were collected in heavy plastic sample bags. Each sample was dried and shipped to Acme Laboratories in Vancouver. Soil/talus samples were seived to -80 mesh and rock samples were pulverized prior to analysis. All samples were geochemically analysed for gold and by Inductively Coupled Plasma (ICP) for 30 elements. Rock samples returning >1000 ppb gold were fire assayed. All analytical data are tabled in Appendix II.

Results

Systematic talus and soil grid sampling carried out in 1986 generally confirmed the 1985 +1000 ppb gold anomalies and as well, outlined a new anomaly (Figure 6b). Zone "A" now encompasses the two 1985 zones A and E. Zone B is considered a northeastern extension of zone A and sampling results from zone D are less encouraging than the 1985 results from that area. Zone "L", the new anomaly, is a southern continuation of zone C and lies along the eastern margin of the schist zone.

It should be recognized, however, that almost the entire schist zone is a +100 ppb gold talus geochemical anomaly and that the +1000 ppb zones described here are exceptionally higher grade portions of the anomaly. The 500 ppb gold contours shown in Figure 6b illustrate the continuity of the anomalies and indicate their relationship to the northerly trending structural trends within the schist zone. As noted previously (Epp 1985), many of the higher gold values are concentrated in the border areas of the schist.

Detailed sampling results are shown in Figures 7a-c and 8a-c. The best gold targets known to date are in zone A, with secondary targets on zones L, B and F. Zone C was not explored in detail this year due to time and budget constraints, however, this zone is still considered an important target to be reexamined in the future.

Zone A (Figure 7a, b, c)

Analysis of rock chip samples from this zone returned twenty-one samples having gold values >1000 ppb, of which five are >10,000 ppb [i.e. (K86R-001 = 85,000 ppb), (K86R-009 = 33,200 ppb), (K86R-028 = 11,000 ppb), (K86R-1463 = 43,000 ppb), (K86R-1785 = 15,500 ppb)]. Several "high grade" samples were collected near L95+50N, 93+75E, from a 30 metre long quartz-sulphide vein structure, 100 metres southwest of DDH KE85-1. This structure contains 2-4 cm veins of massive pyrite and chalcopyrite (K86R-028). Other high gold values are from similar veins, most of which are conformable to the main schistisity (e.g. K86R-009). Individual rock chip anomalies >500 ppb in zones A and B are outlined as northerly trending structures (Figure 7b). The frequency of the structures reflects the extent and intensity of the vein system. At zone B it is apparent that the system is weaker in the number of gold-bearing structures, although a few of the 1985 trench samples are notably anomalous.

Zone F

A detailed soil grid was extended over zone F to cover the 1985 reconnaissance gold anomaly (Figure 6a-c). Results indicate that this anomaly is more restricted in extent than other zones, however, this may be due, in part, to the widespread overburden cover. Exposed sections of the sericite schist in this area are narrow and likely to be branching offshoots from the western margin of the main schist zone. Detailed sampling of one such structure near L87+50N, 94+25E returned a value of 11,300 ppb (K86R-006) and a 1985 rock sample taken nearby returned 46,000 ppb (KE85-4317).

Zone D (Figure 8a-c)

Sampling in this zone was hampered by permanent snow and ice cover. Detailed rock chip samples were collected over four lines spaced

50 metres apart. Most analytical results were in the 100-500 ppb range, with only one rock sample and a few scattered talus samples returning >500 ppb.

Zone L (Figure 6b)

Zone L is a +500 ppb talus/soil anomaly extending along the baseline from L96N to L101N and is at the eastern margin of the sericite schist zone. Detailed rock sampling was not extended to this area due to delays in receiving analytical data and to time constraints. However, follow-up rock sampling should be completed here in the future.

GEOPHYSICS

VLF and magnetometer surveys (Figure 9a,b) were completed over most of the central part of the schist zone, from L90N TO L100N. The surveys covered zones A,B and L. Attempts to continue the work on zones F and D were restricted by inclement weather.

Instruments used for the surveys were a Geonics EM16 VLF-EM unit (using the Seattle, Washington NLK transmitting station) and a McPhar M700 Vertical Field Fluxgate Magnetometer.

The VLF data indicate weak crossovers in the area northeast of zone A, trending northeasterly from L97N to L100N. There is also a weak trend on L90N and L91N near 99+00E. The trends may be due to faults, or possibly sulphide bearing structures, however, the inferred northeast orientations are not consistent with observed structural trends.

The magnetometer survey results show more coherent and well defined data. A small, but high contrast +300 gamma anomaly corresponds well with zone B and also has a weak northeasterly trend. The northeast orientation of the zone B gold geochemical anomaly may be reflected here. A weaker +100 gamma anomaly corresponds to the southern part of zone A. In the south central area on L90N there is a broad multiple anomaly with peak values of 359 and 299 gammas. Corresponding geological information is scant in this area due to relatively poor outcrop. In any case the geochemical values for gold and silver are not particularly encouraging.

DISCUSSION

The geological and geochemical data collected on the KERR property indicates that the area has undergone a complex geological history involving submarine volcanism and sedimentation, subvolcanic and plutonic intrusion and large scale regional deformation, followed by later stage volcanism and regional thrust tectonics. To establish the exact order of events and timing of mineralization will require more precise evaluation at both the regional and local scales and is generally beyond the scope of the present stage of property exploration. However, from the data accumulated to date, two general possibilities are suggested for the genesis of precious metals mineralization on the property.

The first, attributes mineralization to an epithermal process during the very late stages, or soon after volcanism. Metals are precipitated in vein and breccia stockworks by the circulation of hydrothermal fluids, while the wall rocks are converted to sericite, chlorite and associated alteration minerals (Buchanan, 1979).

The second scenario would be to relate mineralization to much later hydrothermal activity accompanying regional shear deformation. In this case, the sericite schist post-dates all primary volcanic or plutonic processes and could perhaps place the schist development with late Mesozoic regional tectonics, which might be associated with the current "terrane" concepts.

Either case closely relates mineralization to the formation of the sericite schist zone, regardless of the timing of the event. The emplacement of the relatively unaltered andesite dykes obviously post-dates mineralization, but can be included in either model (1) as recurring andesite volcanism in an active epithermal centre or, (2) as fault-related dyking in a regional tensional regime.

At Brucejack Lake gold mineralization occurs in sericite schists which represent intensely altered feldspar and hornblende bearing syenitic rocks (Schroeter, 1982). Kirkham (1963) concluded that a broad porphyry copper system existed in the Sulphurets region, which led to the genesis of the copper and molybdenum occurrences on the north side of Sulphurets Creek. He compared the widespread sericitic alteration (i.e. Kerr, Brucejack Lake) to the alteration zones surrounding porphyry deposits of the southwestern United States and South America and inferred that altering and mineralizing fluids were contained by an overlying, impermeable volcanic "cap" or "trap" rock. Grove (1971) emphasized that the major precious metals deposits of the Stewart area, to the south, occur in highly altered and deformed volcanic derived epiclastic rocks. The majority of these occurrences are tabular quartz-breccia veins, which formed as fissure fillings, with gradations to sulphide replacement deposits, features consistent with the epithermal model. More recently Panteleyev and Schroeter (1985) placed the Stewart and sulphurets (Brucejack Lake) deposits at the lowermost zone of the "boiling level" of their B.C. epithermal model.

Kerr mineralization is perhaps more compatible with the epithermal model. The development of intense shearing in the sericite zones, with closely associated quartz-sulphide veins, may actually post-date initial alteration and mineralization and result from the deformation and remobilization of a previously formed epithermal centre, whereby regional stresses took the path of least resistance in acting on the less competent altered rocks.

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Panteleyev, A. and Schroeter, T.G. 1985. British Columbia Epithermal Model. British Columbia Department of Energy, Mines and Petroleum Resources, Poster Issue.

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APPENDIX I

STATEMENT OF COSTS

STATEMENT OF COSTS

KERR CLAIM GROUP #1866*

and

KERR 99 CLAIM

FIELD LABOUR COSTS

Project Geologist, R.E. Meyers, 38 days @ $170 (July 8 - August 19)	$ 6,460.00		
Junior Geologist, S. Casselman, 47 days @ $95 (July 8 - August 23)	4,465.00		
Student Assistant, T. McIntyre, 47 days @ $75 (July 8 - August 23)	3,525.00		
Field Assistant, E. Alionis,	18 days @ $125	2,250.00	
TOTAL	150 man-days		
TOTAL LABOUR			$ 16,700.00

GEOCHEMICAL COSTS

593 Soil/Talus sample prep. @ $ 0.75		$ 444.75	
649 Rock sample prep. @	3.00	1,947.00	
1,242 Total Au & ICP Analysis @ $10.00		12,420.00	
TOTAL ANALYTICAL COSTS:			$ 14,811.75

SHIPPING CHARGES

Freightways (4 shipments)	$ 470.00

AIR CHARTERS

Fixed Wing (Trans Provincial)	$ 8,262.47	
Helicopter (Northern Mountain) 26.2 hrs @ $547.50 (incl. fuel)	14,344.50	
		$ 22,606.97

CAMP COSTS

4-man crew, totalling 150 man-days @ $60/man-day (includes food, accommodation, camp & gear, fuel, communications)		$ 9,000.00

TRAVEL EXPENSES

Truck Rentals (Mob-Demob)	$ 1,924.00	
Fuel	600.00	
Hotels, meals, 4 men, 4 nights @ $60	960.00	
2 Vancouver-Terrace Airfares @ $345	690.00	
APPORTIONMENT 50%	$ 4,174.00	$ 2,087.00

REPORT PREPARATION

R. Meyers, 5 days @ $170	$ 850.00	
Drafting 20 hrs @ $20	400.00	
Maps & Materials	200.00	
TOTAL		$ 1,450.00
TOTAL ASSESSMENT COSTS*		$ 67,125.72

* APPORTIONMENT OF COSTS:

KERR GROUP #1866	75%	$ 50,344.29
KERR 99 CLAIM	25%	16,781.43

APPENDIX II

TABLE OF GEOCHEMICAL DATA

ASSAYS

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS, VANCOUVER B.C.
PH: (604)253-3158 COMPUTER LINE:251-1011

DATE RECEIVED AUG 6 1986
DATE REPORTS MAILED Aug 11/86

ASSAY CERTIFICATE

SAMPLE TYPE : PULP
AU** BY FIRE ASSAY

ASSAYER _D Toye_ DEAN TOYE . CERTIFIED B.C. ASSAYER

CASSIAR MINING PROJECT 7506 FILE# 86-1776 PAGE# 1

SAMPLE	Au** oz/t
KB6T 1173	.046
KB6T 1613	.176
KB6R 001	2.430
KB6R 1610	.041

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS, VANCOUVER B.C.
PH: (604)253-3158 COMPUTER LINE:251-1011

DATE RECEIVED AUG 9 1986
DATE REPORTS MAILED Aug 12/86

ASSAY CERTIFICATE

SAMPLE TYPE : PULP
AU** BY FIRE ASSAY

ASSAYER D. Toye DEAN TOYE , CERTIFIED B.C. ASSAYER

CASSIAR MINING PROJECT 7506 FILE# 86-1868 R PAGE# 1

SAMPLE	Au** oz/t
K86S 1230	.057
K86S 1233	.420
K86T 1742	.082
K86R 004	.032
K86R 006	.312
K86R 009	.990
K86R 1300	.069
K86R 1313	.099
K86R 1321	.037
K86R 1730	.050
K86R 1731	.088

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS, VANCOUVER B.C.
PH: (604) 253-3158 COMPUTER LINE: 251-1011

DATE RECEIVED AUG 26 1986

DATE REPORTS MAILED Aug 29/86

ASSAY CERTIFICATE

SAMPLE TYPE : PULP
AU** BY FIRE ASSAY

ASSAYER D. Toye DEAN TOYE , CERTIFIED B.C. ASSAYER

CASSIAR MINING PROJECT 7506 FILE# 86-2114 R PAGE# 1

SAMPLE	Au** oz/t
K86R-577	.059
K86R-1355	.081
K86R-1392	.039
K86R-1404	.044
K86R-1422	.043
K86R-1463	1.120
K86R-1488	.068
K86R-1493	.039
K86R-1785	.415
K86R-1789	.058
K86R-1840	.085
K86T-552	.131
K86T-1357	.071
K86T-1361	.122
K86T-1870	.038
K86T-1874	.030

File - Ker

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS, VANCOUVER B.C.
PH:(604)253-3158 COMPUTER LINE:251-1011

DATE RECEIVED SEPT 5 1986
DATE REPORTS MAILED Sept. 10/86

ASSAY CERTIFICATE

SAMPLE TYPE : PULP
AU** BY FIRE ASSAY

ASSAYER ___D Toye___ DEAN TOYE , CERTIFIED B.C. ASSAYER

CASSIAR MINING PROJECT 7506 FILE# 86-2303 R PAGE# 1

SAMPLE	Au** oz/t
K86R-010	.134
K86R-011	.218
K86R-012	.057
K86R-014	.148
K86R-015	.302
K86R-016	.058
K86R-017	.160
K86R-028	.322
K86R-1892	.108
K86T-654	.112
K86T-742	.036
K86T-1897	.063

R

Rocks

CASSIAR MINING PROJECT - 7506 FILE # 86-1776

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
* K86R 001	95	500	113	81	136.4✓	3	2	277	5.49	234	7	113	2	5	1	19	7	71	.04	.086	14	5	.09	110	.04	17	.32	.01	.18	1	85000 ✓
K86R 1153	1	93	37	139	7.1	7	11	2104	4.23	22	5	ND	1	47	1	2	2	80	1.49	.100	9	21	1.23	188	.07	6	1.53	.05	.14	1	310
K86R 1154	1	175	58	121	1.4	9	10	1617	4.15	23	5	ND	1	20	1	2	2	83	.64	.111	10	23	1.29	128	.10	7	1.53	.05	.15	1	200
K86R 1155	1	145	43	142	.7	7	12	1804	4.41	23	5	ND	1	30	1	3	2	90	.90	.107	11	22	1.38	118	.09	7	1.64	.05	.12	2	115
K86R 1156	2	182	93	214	.8	8	13	2023	4.44	43	5	ND	1	33	2	4	2	85	1.28	.103	11	22	1.31	100	.08	8	1.60	.05	.13	3	130
K86R 1157	8	138	40	138	1.3	6	12	3325	7.15	120	5	ND	1	23	1	2	2	77	.89	.125	14	15	1.17	53	.10	8	1.79	.05	.14	3	235
K86R 1158	1	85	7	95	.2	6	12	2218	4.40	7	5	ND	1	18	1	2	2	78	.54	.130	14	9	2.40	620	.08	8	2.34	.04	.15	2	8
K86R 1159	1	74	2	107	.2	6	16	3183	5.45	13	5	ND	2	62	1	2	2	89	1.01	.152	14	7	3.36	1591	.08	8	2.92	.05	.12	1	25
K86R 1160	1	70	6	118	.2	7	17	4288	6.51	13	5	ND	2	48	1	2	2	103	.53	.157	15	10	4.02	1530	.05	8	3.43	.05	.10	2	7
K86R 1161	1	67	5	98	.5	8	19	3045	5.47	5	5	ND	1	78	1	2	2	98	1.36	.144	15	14	2.90	1524	.11	9	2.73	.05	.13	3	105
K86R 1162	1	461	17	163	.5	7	28	2637	5.79	15	5	ND	1	53	1	2	2	105	1.17	.153	17	10	3.23	641	.12	7	2.83	.05	.10	2	505
K86R 1163	1	97	5	128	.2	8	18	2371	5.64	6	5	ND	1	65	1	2	2	99	.99	.151	16	11	3.01	1455	.12	7	2.82	.05	.12	1	28
K86R 1164	1	54	5	106	.1	9	16	2319	5.51	9	5	ND	1	135	1	2	2	98	1.71	.156	19	15	2.14	268	.12	13	2.42	.06	.11	1	4
K86R 1165	1	312	11	164	1.4	6	22	1609	4.87	22	5	ND	2	15	1	2	2	77	.37	.152	13	8	1.54	188	.03	6	1.95	.04	.16	2	415
K86R 1166	2	382	42	68	2.8	2	3	310	3.98	37	5	ND	1	7	1	2	4	23	.09	.117	11	3	.18	139	.01	5	.57	.02	.21	1	475
K86R 1167	7	428	41	97	1.2	3	7	807	5.86	33	5	ND	2	8	1	2	3	36	.19	.174	7	1	.39	90	.01	8	.98	.02	.24	1	450
K86R 1168	1	196	27	85	.7	2	6	954	4.00	36	5	ND	2	6	1	2	3	32	.18	.149	8	2	.42	158	.01	6	.97	.02	.26	1	135
K86R 1169	1	208	7	128	.5	3	10	1350	5.96	34	8	ND	2	6	1	2	2	39	.23	.182	12	2	.64	115	.01	9	1.36	.03	.29	1	26
K86R 1170	3	228	10	121	.6	2	12	907	5.05	43	5	ND	1	5	1	2	2	25	.21	.161	9	3	.31	96	.01	7	.96	.02	.30	1	85
K86R 1171	3	262	46	126	1.1	2	6	1271	5.02	52	5	ND	2	7	1	2	2	37	.24	.193	11	2	.58	163	.01	8	1.41	.03	.35	1	90
K86R 1172	3	150	36	107	.4	3	5	885	3.60	57	5	ND	2	6	1	2	2	29	.22	.183	8	2	.48	184	.01	6	1.12	.02	.31	1	135
K86R 1174	4	491	4	263	.1	4	17	2196	10.21	21	5	ND	2	17	1	2	2	157	.50	.150	24	2	1.54	190	.36	6	2.77	.05	.09	1	11
K86R 1175	5	84	25	44	1.3	1	2	449	2.26	31	5	ND	1	18	1	2	2	20	.07	.098	8	4	.28	99	.02	4	.54	.01	.17	2	85
K86R 1176	52	117	27	43	1.3	1	1	350	2.74	29	5	ND	1	9	1	3	2	9	.01	.074	7	1	.02	288	.01	4	.23	.01	.28	2	175
K86R 1606	19	380	21	8	.8	10	10	16	3.46	4	5	ND	1	6	1	3	3	6	.01	.010	5	4	.02	9	.01	9	.18	.01	.14	1	315
K86R 1607	43	316	20	8	.6	9	8	14	2.63	9	6	ND	1	10	1	5	2	6	.01	.023	4	5	.02	14	.01	4	.19	.01	.14	1	440
K86R 1608	23	1138	15	164	.6	12	22	1293	8.67	41	5	ND	2	10	1	2	2	30	.27	.190	11	2	.24	17	.01	8	.89	.02	.27	1	95
K86R 1609	40	1521	45	500	.9	12	30	2825	19.15	43	5	ND	2	22	2	2	2	62	.34	.252	17	7	.48	15	.01	8	1.89	.04	.15	1	125
K86R 1610	5	264	483	441	7.2	28	9	919	3.74	49	5	2	1	48	3	13	2	72	1.42	.126	13	27	1.10	111	.12	9	1.32	.04	.19	5	1490
K86R 1611	4	205	17	68	.4	43	11	1393	4.26	31	5	ND	2	93	1	2	2	142	2.18	.128	11	36	1.10	102	.14	6	1.32	.05	.17	1	90
K86R 1612	1	127	9	81	.4	30	11	1313	3.78	60	5	ND	1	108	1	2	2	132	2.89	.162	12	48	1.19	108	.15	5	1.42	.06	.12	1	85
K86R 1614	9	58	18	41	.3	9	2	429	2.79	556	6	ND	3	7	1	4	4	48	.27	.143	7	12	.45	152	.08	4	1.01	.02	.25	2	155
K86R 1616	1	87	8	24	.2	14	8	396	1.31	56	5	ND	2	10	1	2	3	14	.32	.149	7	5	.32	155	.02	4	.69	.02	.25	2	30
K86R 1617	4	141	7	14	.2	6	5	189	1.47	47	5	ND	1	10	1	2	2	17	.18	.101	4	5	.07	198	.02	6	.39	.01	.24	3	75
K86R 1618	8	529	23	42	1.3	6	7	501	2.46	30	5	ND	1	20	1	2	3	27	.36	.130	6	9	.26	187	.08	6	.63	.02	.24	3	150
K86R 1619	3	346	12	55	.2	11	7	637	2.34	44	5	ND	1	9	1	2	2	36	.34	.147	7	11	.43	179	.06	6	.93	.03	.24	2	65
STD C/AU-0.5	20	61	40	136	7.3	74	30	1149	3.98	42	17	7	34	50	19	15	22	65	.48	.108	41	61	.89	189	.09	37	1.73	.09	.13	15	480

✓ Assay required for correct result

R

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R 1620	4	390	20	78	.8	5	7	831	3.26	38	5	ND	1	7	1	6	3	61	.26	.138	4	7	.84	146	.09	6	1.23	.03	.20	3	95
K86R 1621	2	562	10	103	.5	6	12	1536	3.13	12	5	ND	1	82	1	5	2	62	.82	.138	7	6	1.17	1292	.11	7	1.45	.05	.16	2	32
K86R 1624	16	179	32	62	1.4	2	2	345	3.75	85	5	ND	2	11	1	4	3	23	.19	.177	6	1	.23	250	.01	7	.67	.02	.25	1	85
K86R 1625	28	152	26	51	.8	2	4	363	4.55	156	5	ND	2	10	1	3	4	25	.18	.177	5	2	.21	223	.01	6	.66	.02	.25	1	160
K86R 1626	12	64	46	20	.7	1	1	97	3.01	293	5	ND	2	5	1	8	3	14	.05	.126	4	1	.06	183	.01	6	.35	.01	.24	1	690
K86R 1627	7	90	67	74	.7	2	1	542	3.95	178	5	ND	2	7	1	6	3	26	.14	.176	7	1	.28	161	.01	6	.76	.01	.24	1	205
K86R 1628	1	73	44	127	.5	5	3	636	4.00	70	5	ND	1	7	1	2	3	32	.16	.140	5	6	.61	176	.01	8	1.23	.02	.21	1	195
K86R 1629	15	111	25	103	.8	4	3	636	5.04	106	5	ND	1	20	1	2	2	49	.17	.143	5	11	.42	185	.02	7	1.04	.02	.20	2	395
K86R 1630	35	1296	277	222	2.7	4	5	601	9.58	151	5	ND	1	19	1	9	4	52	.09	.172	2	3	.17	59	.01	2	.83	.02	.19	1	435
STD C/AU-0.5	22	60	40	138	7.1	75	30	1153	3.95	42	15	7	35	51	19	16	22	72	.48	.109	40	64	.89	189	.09	37	1.73	.09	.14	15	515

R

SAMPLE# Rock.	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R 002	1	20	12	31	.4	3	2	3953	.41	13	8	ND	1	342	1	2	2	2	6.35	.011	2	1	.06	104	.01	2	.06	.05	.02	1	12
K86R 003	1	114	90	73	8.5	5	3	235	4.52	165	5	ND	1	10	1	9	3	12	.04	.095	2	2	.10	105	.01	9	.32	.01	.17	1	700
K86R 004	2	78	89	55	3.9	4	7	403	5.71	274	5	2	1	17	1	14	2	15	.07	.115	3	1	.06	327	.01	11	.43	.01	.22	1	1290
K86R 005	2	115	48	298	.4	24	18	2037	5.76	30	5	ND	1	8	1	2	7	88	.25	.133	5	30	2.40	155	.01	9	2.73	.04	.20	1	60
K86R 006	2	235	906	208	55.4	4	2	914	3.17	292	5	7	1	10	1	108	2	12	.08	.059	2	2	.10	135	.01	8	.26	.01	.15	1	11300
K86R 007	4	137	91	120	4.8	2	2	669	8.76	269	5	ND	1	6	1	4	4	25	.01	.135	2	15	.27	210	.02	5	.55	.01	.20	1	500
K86R 008	40	515	81	98	3.4	4	2	557	3.50	18	5	ND	1	8	1	5	4	36	.14	.120	2	1	.55	430	.11	6	.89	.02	.26	2	275
K86R 009	30	268	659	219	442.3	2	1	40	9.91	316	5	28	1	17	1	524	13	28	.01	.271	2	1	.02	80	.01	2	.13	.02	.13	1	33200
K86R 1300	4	169	59	198	7.8	19	17	3605	7.48	101	5	ND	1	75	1	5	4	50	2.84	.133	6	40	1.52	131	.01	7	1.60	.05	.18	2	1610
K86R 1301	3	56	54	153	2.5	16	8	2023	4.70	24	5	ND	1	9	1	2	6	42	.21	.141	2	18	1.61	144	.01	10	1.69	.02	.23	1	500
K86R 1302	2	32	40	73	1.4	6	3	896	5.32	19	5	ND	1	5	1	2	8	35	.10	.166	2	14	1.07	156	.01	8	1.14	.02	.18	1	255
K86R 1303	3	36	20	16	1.1	2	1	167	4.75	69	5	ND	1	2	1	5	2	17	.01	.121	2	5	.15	93	.01	8	.37	.01	.18	1	175
K86R 1304	3	45	156	83	1.3	3	1	945	5.46	28	5	ND	1	3	1	5	8	43	.01	.086	2	25	.73	103	.01	9	.88	.02	.17	1	65
K86R 1305	2	70	1254	107	2.7	5	2	900	6.67	66	5	ND	1	5	1	3	3	47	.01	.124	2	33	.66	105	.01	8	.96	.02	.16	1	110
K86R 1306	2	82	133	186	1.2	9	2	1906	7.03	109	5	ND	1	5	1	2	6	66	.04	.170	2	37	1.43	116	.01	7	1.74	.02	.15	1	175
K86R 1307	3	86	197	193	2.6	15	3	1898	8.75	132	5	ND	1	6	1	2	3	67	.03	.134	2	38	1.14	139	.01	5	1.63	.02	.14	2	595
K86R 1308	2	72	39	598	.9	13	11	2175	4.37	39	5	ND	1	40	3	2	6	69	1.46	.144	7	18	1.40	138	.08	11	2.02	.04	.23	3	70
K86R 1309	3	206	32	139	2.8	6	8	1510	6.96	34	5	ND	1	5	1	2	5	56	.11	.173	3	10	1.15	132	.01	7	1.66	.02	.17	1	190
K86R 1310	9	97	34	41	1.1	2	2	411	4.14	41	5	ND	1	3	1	5	2	26	.03	.097	2	6	.30	144	.01	9	.65	.01	.19	2	340
K86R 1311	15	52	22	8	1.4	2	2	31	2.19	46	5	ND	1	2	1	10	2	12	.01	.059	2	3	.02	89	.01	5	.22	.01	.15	1	520
K86R 1312	22	37	21	113	2.5	2	2	870	3.87	23	5	ND	1	6	1	7	2	14	.12	.116	7	2	.82	111	.01	9	1.45	.02	.18	1	230
K86R 1313	37	159	82	129	9.2	2	2	583	3.81	23	5	4	5	4	1	8	4	8	.08	.057	13	1	.72	82	.01	8	1.41	.02	.13	1	3280
K86R 1314	24	76	21	34	1.1	2	1	157	3.22	34	5	ND	3	3	1	5	2	10	.02	.044	4	4	.10	107	.01	8	.44	.01	.19	2	180
K86R 1315	8	70	67	4	2.6	2	1	31	3.82	59	5	ND	1	5	1	12	2	20	.01	.098	2	6	.03	107	.01	12	.25	.01	.18	1	385
K86R 1316	11	85	71	8	2.7	1	1	63	4.81	83	5	ND	1	3	1	78	2	20	.01	.082	2	5	.05	99	.01	10	.31	.01	.19	1	725
K86R 1317	12	80	26	74	.9	3	2	741	4.55	33	5	ND	2	4	1	6	2	23	.04	.094	7	5	.39	104	.01	12	.83	.02	.18	1	140
K86R 1318	18	52	152	32	1.8	1	1	341	3.71	50	5	ND	1	4	1	9	2	22	.03	.126	2	4	.21	114	.01	10	.56	.01	.23	1	320
K86R 1319	6	51	33	91	1.4	2	2	1036	4.27	46	5	ND	1	5	1	3	3	22	.08	.125	2	2	.52	108	.01	9	1.09	.02	.21	2	320
K86R 1320	9	54	59	15	5.5	1	1	116	2.97	48	5	ND	1	5	1	7	2	20	.01	.087	2	1	.07	101	.01	7	.34	.01	.21	1	585
K86R 1321	15	231	85	135	6.4	2	2	600	8.02	91	5	2	2	5	1	2	2	30	.07	.211	2	3	.33	98	.01	8	.71	.02	.20	3	1410
K86R 1322	6	153	28	95	1.3	3	3	1046	6.78	54	5	ND	2	8	1	3	4	48	.09	.180	2	6	.74	106	.01	11	1.20	.02	.21	1	160
K86R 1323	27	148	30	72	2.1	2	2	605	5.38	67	5	ND	1	5	1	10	3	31	.05	.145	2	6	.39	102	.01	10	.79	.01	.20	1	230
K86R 1324	20	180	44	47	1.9	2	1	151	7.48	71	5	ND	1	7	1	4	2	24	.02	.141	2	4	.06	115	.02	9	.37	.02	.22	1	160
K86R 1325	11	189	45	41	2.1	2	2	218	5.34	41	5	ND	1	7	1	6	4	24	.02	.127	2	3	.13	119	.02	9	.49	.01	.21	1	560
K86R 1326	16	177	61	76	2.5	2	2	570	6.45	37	5	ND	2	5	1	2	2	41	.03	.135	2	4	.37	118	.02	10	.75	.02	.20	1	330
K86R 1327	14	98	33	38	1.1	2	2	282	4.07	20	5	ND	1	6	1	2	2	28	.02	.116	5	2	.26	152	.01	8	.61	.01	.24	1	70
STD C/AU-0.5	21	61	41	141	7.0	74	29	1141	3.98	38	17	7	35	49	19	17	20	70	.48	.108	37	61	.88	186	.08	39	1.73	.09	.12	15	495

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File Kerr Geochem

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-8 ROCKS P9-TALUS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 27 1986 DATE REPORT MAILED: Sept 3/86 ASSAYER. D. Toye ..DEAN TOYE. CERTIFIED B.C. ASSAYER.

CASSIAR MINING PROJECT - 7506 FILE # 86-2303 PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-010	92	493	128	125	77.6	3	2	376	6.55	234	8	3	1	5	1	29	4	82	.05	.089	3	4	.10	126	.03	4	.34	.02	.20	1	3010
K86R-011	42	213	106	40	11.0	9	4	758	5.11	250	5	9	2	5	1	2	2	74	.10	.128	4	12	.27	118	.06	7	.57	.02	.23	2	7220
K86R-012	36	351	83	95	22.6	7	3	1172	5.45	162	5	2	2	8	1	7	2	78	.12	.115	5	11	.42	198	.08	6	.82	.02	.22	1	1620
K86R-013	15	131	316	186	6.3	15	4	1558	4.09	77	5	ND	2	10	1	5	2	98	.30	.121	6	18	.82	163	.09	7	1.25	.03	.23	1	125
K86R-014	3	267	1299	866	14.5	8	11	1868	4.29	236	5	6	1	43	5	7	2	42	1.05	.096	6	8	1.17	151	.06	6	1.44	.05	.22	1	3760
K86R-015	24	740	269	173	308.7	4	5	794	7.21	462	5	10	1	11	3	3592	119	25	.14	.117	6	3	.23	113	.04	2	.63	.02	.27	1	8920
K86R-016	63	430	86	103	22.4	6	7	1175	3.86	164	5	ND	1	13	1	12	2	29	.27	.116	6	6	.35	212	.01	6	.77	.02	.26	1	1780
K86R-017	82	4398	84	159	332.2	5	8	1806	6.67	290	5	6	1	4	2	594	7	50	.10	.051	3	4	.24	16	.04	4	.57	.02	.21	10	5240
K86R-018	2	355	16	51	5.4	1	2	3187	1.13	8	5	ND	3	402	1	8	2	2	11.25	.005	5	2	.14	159	.01	2	.30	.07	.03	1	55
K86R-019	3	480	22	108	2.0	1	1	523	2.74	15	5	ND	5	48	1	6	2	3	.92	.031	22	1	.28	120	.01	4	.80	.04	.11	1	12
K86R-020	7	1451	33	203	3.1	3	4	186	5.47	415	5	ND	1	17	1	7	2	24	.16	.085	2	2	.23	19	.01	5	.69	.03	.12	1	65
K86R-021	7	2107	14	576	1.4	3	1	282	3.66	69	5	ND	1	9	2	3	2	19	.08	.084	2	4	.37	62	.01	5	.80	.02	.05	1	30
K86R-022	3	1096	4	57	.7	2	1	989	1.65	11	5	ND	1	22	1	4	2	5	.64	.028	2	4	.38	39	.01	6	.50	.03	.03	1	11
K86R-023	2	3313	23	120	2.6	4	17	320	17.05	282	9	ND	1	10	1	2	2	7	.11	.036	2	1	.28	3	.01	2	.54	.04	.03	1	75
K86R-024	2	235	25	125	1.1	33	23	435	8.91	93	5	ND	1	13	1	2	2	21	.56	.041	3	18	.45	7	.01	2	.61	.04	.12	1	41
K86R-025	132	249	168	1	.6	35	73	30	15.21	23	9	ND	1	21	1	2	2	3	.01	.007	2	1	.03	3	.01	2	.08	.03	.04	1	250
K86R-026	5	877	55	110	2.7	18	7	3175	16.51	197	6	ND	2	36	1	54	4	6	2.16	.015	8	1	1.18	6	.01	2	.03	.06	.03	1	845
K86R-027	7	2122	19	29	10.1	4	3	211	2.38	160	7	ND	1	88	1	5	2	24	.22	.112	3	3	.06	62	.01	4	.25	.02	.18	1	760
* K86R-028	33	19406	208	553	318.6	1	2	331	33.44	545	7	6	3	7	3	10	2	48	.02	.016	2	1	.04	10	.01	2	.24	.05	.05	1	11000
K86R-619	10	210	23	32	.2	7	9	476	4.05	902	5	ND	1	10	1	14	2	39	.35	.165	4	8	.66	38	.05	8	1.07	.03	.28	1	155
K86R-620	3	146	20	41	.2	5	7	566	3.54	393	5	ND	2	11	1	10	2	53	.37	.167	6	8	.75	113	.08	8	1.13	.03	.28	2	95
K86R-621	2	199	24	167	1.4	3	8	1016	4.58	104	5	ND	1	14	1	40	2	65	.51	.149	6	3	1.11	67	.07	5	1.39	.04	.25	1	315
K86R-622	3	210	10	59	.4	5	11	866	4.05	62	5	ND	2	10	1	2	2	64	.52	.169	6	4	1.02	41	.05	6	1.36	.04	.26	1	65
K86R-623	3	153	13	78	.4	20	10	769	3.72	61	5	ND	2	8	1	3	2	66	.42	.168	7	2	.88	51	.06	7	1.26	.04	.23	1	85
K86R-624	3	188	12	28	.4	6	12	595	4.61	197	5	ND	1	14	1	6	2	72	.65	.168	6	5	.50	23	.06	6	.98	.05	.27	1	195
K86R-625	4	117	10	19	.5	4	8	405	3.23	54	5	ND	1	16	1	2	2	46	.81	.152	6	2	.32	49	.05	5	.73	.05	.26	1	70
K86R-626	9	171	33	26	.7	5	7	387	4.73	179	5	ND	2	6	1	5	2	41	.30	.162	6	5	.48	70	.11	7	.97	.03	.30	6	145
K86R-627	2	130	12	69	.6	6	9	950	4.12	26	5	ND	2	26	1	2	2	89	.52	.115	4	14	1.33	114	.09	6	1.66	.06	.14	1	29
K86R-628	2	195	6	54	.6	6	10	773	4.16	13	5	ND	2	42	1	10	2	92	.49	.115	5	16	1.34	93	.10	5	1.52	.06	.10	1	36
K86R-629	7	329	62	88	2.7	5	11	491	4.29	28	5	2	2	13	1	2	2	73	.55	.170	8	5	.60	33	.08	7	1.08	.05	.27	1	815
K86R-630	13	512	22	46	.8	21	21	564	7.60	318	5	ND	1	5	1	5	2	52	.35	.165	5	20	.68	19	.04	2	1.63	.03	.30	5	165
K86R-631	13	422	41	77	1.2	13	12	703	6.46	87	5	ND	1	6	1	12	2	72	.27	.149	5	23	1.00	87	.05	2	1.86	.03	.22	1	75
K86R-632	16	490	85	51	1.0	7	12	325	4.03	394	5	ND	1	8	1	17	2	32	.34	.179	4	8	.45	49	.01	6	1.02	.03	.27	1	165
K86R-633	7	144	34	10	.8	3	6	132	4.01	232	5	ND	1	8	1	6	2	21	.22	.179	3	4	.21	83	.01	6	.73	.02	.31	1	155
K86R-634	30	405	67	28	1.0	8	11	337	5.21	319	5	ND	2	5	1	5	2	34	.26	.166	2	8	.52	48	.01	3	1.10	.03	.28	1	145
K86R-636	1	115	75	181	1.7	17	10	2345	3.99	22	5	ND	2	109	1	7	2	53	2.59	.132	9	16	1.07	77	.01	8	1.70	.06	.22	1	13
STD C/AU-0.5	20	60	39	137	7.3	71	29	1120	3.96	41	16	7	36	50	18	18	21	69	.47	.105	38	60	.88	188	.09	40	1.72	.09	.14	14	575

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK CHIPS P9&10 SOILS/TALUS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 18 1986 DATE REPORT MAILED: Aug 23/86 ASSAYER. D.Toye ..DEAN TOYE. CERTIFIED B.C. ASSAYER.

CASSIAR MINING PROJECT - 7506 FILE # 86-2114

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-553	3	138	50	230	1.1	17	15	3636	4.98	37	5	ND	1	123	1	7	2	28	3.92	.159	2	9	1.13	33	.01	5	1.04	.06	.20	1	22
K86R-554	4	161	376	299	9.2	6	4	1081	7.84	169	5	ND	1	17	1	61	2	41	.08	.153	2	18	1.09	257	.01	2	1.04	.03	.21	1	310
K86R-555	3	105	327	469	4.8	17	10	2501	7.49	115	5	ND	1	27	1	6	2	57	.50	.156	2	25	1.89	32	.02	2	1.68	.04	.19	1	210
K86R-556	4	128	159	870	1.8	32	22	5696	6.49	53	5	ND	1	32	3	2	2	57	1.23	.172	2	35	2.36	18	.05	2	2.12	.05	.22	1	37
K86R-557	3	73	96	694	.8	29	17	4486	5.60	27	5	ND	1	32	2	2	2	65	1.36	.179	4	38	2.25	33	.17	6	2.03	.06	.21	1	14
K86R-558	4	120	96	510	1.8	23	12	3174	6.88	53	5	ND	1	18	1	2	2	91	.48	.192	2	43	2.81	39	.24	2	2.24	.05	.18	1	20
K86R-559	3	56	73	201	1.3	12	7	1266	4.83	13	5	ND	2	17	1	2	2	48	.25	.164	2	21	1.92	42	.15	7	1.54	.04	.21	1	30
K86R-560	2	68	59	119	.8	7	7	885	4.67	20	5	ND	1	34	1	2	2	40	.26	.183	2	8	.94	19	.01	9	.97	.03	.24	1	15
K86R-561	3	90	51	464	.6	27	13	2485	5.41	18	5	ND	1	19	1	2	2	69	.60	.156	2	45	3.26	34	.04	7	2.59	.05	.17	1	11
K86R-562	3	97	33	418	.4	34	17	2935	6.12	23	5	ND	1	22	1	2	2	78	.69	.177	3	50	3.40	50	.02	5	2.81	.05	.19	1	16
K86R-563	4	75	53	208	1.4	10	3	1040	5.04	56	5	ND	1	7	1	5	2	42	.09	.147	2	22	1.31	148	.01	9	1.25	.02	.21	1	70
K86R-564	4	88	46	374	1.0	23	9	2846	5.68	26	5	ND	1	24	1	2	2	55	.68	.182	2	32	2.24	209	.01	7	1.99	.04	.18	1	65
K86R-565	2	86	33	288	.4	32	25	2335	6.87	10	5	ND	1	25	1	2	2	122	.77	.171	2	65	3.71	19	.16	2	3.01	.06	.12	1	8
K86R-566	4	31	26	107	1.4	6	2	608	3.29	17	5	ND	1	5	1	2	2	28	.03	.087	2	20	.71	125	.01	9	.93	.02	.22	1	210
K86R-567	5	101	32	319	.5	13	4	1486	7.09	32	5	ND	1	11	1	2	2	67	.05	.201	3	58	2.26	170	.01	2	2.19	.03	.17	1	125
K86R-568	11	157	49	58	1.0	4	2	251	6.12	34	5	ND	1	10	1	6	2	27	.01	.173	3	15	.29	307	.01	8	.59	.02	.24	1	250
K86R-569	9	185	24	212	.5	15	3	1191	7.26	10	5	ND	1	29	1	2	2	85	.07	.149	3	61	2.38	362	.01	2	2.28	.03	.17	1	95
K86R-570	3	175	26	356	.3	12	3	1496	8.71	24	5	ND	1	11	1	5	2	97	.05	.171	2	73	2.52	156	.01	2	2.44	.04	.16	1	85
K86R-571	5	128	30	33	.8	2	1	154	7.48	31	5	ND	2	8	1	7	2	39	.01	.160	2	20	.22	155	.01	2	.50	.02	.21	1	350
K86R-572	4	103	25	52	.5	4	1	343	6.02	27	5	ND	1	8	1	6	2	34	.02	.126	2	22	.47	164	.01	7	.70	.02	.20	1	210
K86R-573	3	137	19	191	.2	15	4	1526	7.71	19	5	ND	1	17	1	2	2	105	.11	.169	3	87	2.73	333	.05	2	2.47	.04	.14	1	30
K86R-574	7	192	40	134	.6	10	3	1073	7.76	17	5	ND	1	20	1	2	2	70	.04	.145	4	55	1.80	333	.01	2	1.76	.04	.19	1	60
K86R-575	8	111	20	159	.7	12	3	1296	6.62	14	5	ND	1	6	1	7	2	63	.05	.146	3	45	1.93	136	.01	7	1.85	.03	.17	1	125
K86R-576	11	134	50	15	.7	1	1	51	5.91	38	5	ND	3	10	1	29	2	14	.01	.062	13	3	.05	133	.01	11	.33	.02	.20	1	125
K86R-577	12	136	26	22	1.4	1	1	107	6.97	124	5	3	1	16	1	67	4	21	.01	.067	2	8	.08	522	.01	6	.40	.02	.20	1	2290
K86R-578	9	124	31	22	1.6	1	1	174	5.51	63	5	ND	2	11	1	13	2	16	.01	.060	8	6	.15	507	.01	9	.44	.02	.19	1	610
K86R-579	9	81	22	133	.4	3	1	1225	5.17	15	5	ND	3	13	1	5	2	28	.08	.145	11	10	.84	449	.01	11	1.36	.03	.20	1	160
K86R-580	6	58	11	91	.1	1	1	465	2.72	10	5	ND	7	3	1	3	2	2	.01	.049	41	1	.27	114	.01	10	.99	.03	.19	1	42
K86R-581	9	117	40	76	.9	2	2	714	5.99	43	5	ND	2	9	1	5	2	13	.04	.066	8	3	.34	197	.01	9	.82	.02	.20	1	870
K86R-582	9	155	25	66	.8	4	3	614	8.80	30	5	ND	1	14	1	2	2	44	.06	.157	2	13	.88	182	.01	2	1.19	.03	.19	1	350
K86R-583	9	239	19	97	.5	8	5	791	7.70	11	5	ND	1	21	1	2	2	69	.11	.236	2	22	1.38	145	.01	2	1.68	.04	.24	1	36
K86R-584	6	214	14	139	.3	7	4	1182	7.95	15	5	ND	1	23	1	2	2	74	.07	.218	2	27	1.67	298	.01	2	1.87	.03	.22	1	29
K86R-585	4	139	32	126	1.3	5	3	848	7.84	35	5	ND	1	13	1	2	2	56	.05	.198	4	21	1.01	186	.01	2	1.19	.03	.25	1	665
K86R-586	5	194	30	155	.6	6	3	1216	8.56	22	7	ND	2	13	1	2	2	85	.09	.184	3	30	1.91	157	.07	2	1.80	.04	.20	1	65
K86R-587	2	72	14	189	.1	2	21	2912	9.31	14	5	ND	1	17	1	2	2	271	.20	.117	9	1	3.94	998	.03	2	4.09	.05	.07	1	16
K86R-588	18	210	14	72	.6	5	2	573	4.84	17	5	ND	2	96	1	5	2	50	.13	.187	4	10	1.15	151	.18	11	1.43	.04	.26	2	75
STD C/AU 0.5	23	62	42	144	7.4	72	30	1163	3.97	39	18	8	37	51	18	16	19	72	.48	.111	39	62	.89	192	.09	41	1.72	.09	.13	13	510

CASSIAR MINING PROJECT - 7506 FILE # 86-2114

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
KB6R-589	5	109	10	73	.4	3	2	534	3.82	9	5	ND	2	62	1	2	2	43	.20	.177	2	7	1.02	279	.16	6	1.19	.03	.22	2	25
KB6R-590	11	211	19	56	.6	4	4	494	4.77	20	5	ND	2	48	1	2	2	46	.15	.159	2	16	.93	441	.20	7	1.13	.03	.22	1	55
KB6R-591	19	151	19	36	.5	4	3	302	4.47	19	5	ND	2	28	1	4	2	30	.07	.149	2	13	.62	283	.19	6	.83	.03	.25	3	50
KB6R-592	2	106	6	54	.3	4	4	819	3.87	5	5	ND	1	38	1	4	2	68	.15	.128	2	10	1.39	877	.17	3	1.58	.04	.20	1	40
KB6R-606	5	142	62	136	.5	10	4	797	8.16	19	5	ND	1	49	1	2	2	128	.07	.157	2	65	2.18	181	.35	2	1.87	.04	.17	1	32
KB6R-607	6	139	16	127	.3	13	5	810	6.92	13	5	ND	1	26	1	2	2	115	.21	.151	2	63	2.29	114	.33	3	2.11	.05	.17	1	57
KB6R-608	5	130	12	118	.2	12	6	595	6.61	9	5	ND	2	13	1	2	2	113	.23	.155	2	49	2.30	68	.32	3	1.95	.05	.17	1	35
KB6R-609	5	54	18	77	.1	10	2	464	5.20	10	5	ND	2	15	1	2	2	100	.15	.148	2	42	1.88	339	.32	7	1.55	.04	.21	1	15
KB6R-610	6	138	38	75	.4	4	2	467	6.88	19	5	ND	2	25	1	2	2	51	.01	.150	2	28	.82	326	.10	5	.88	.03	.20	1	54
KB6R-611	8	99	9	75	.2	12	5	555	5.84	13	5	ND	2	11	1	4	2	104	.14	.141	2	45	2.02	61	.29	6	1.73	.04	.17	1	22
KB6R-612	3	90	9	49	.1	8	2	379	6.27	8	5	ND	2	11	1	2	2	98	.05	.107	2	43	1.88	137	.27	5	1.56	.04	.16	1	18
KB6R-613	2	135	15	45	.3	4	2	463	6.81	20	5	ND	2	18	1	2	2	60	.01	.147	2	29	.88	259	.01	5	.91	.03	.20	2	125
KB6R-614	3	116	19	116	.1	6	2	620	7.57	54	5	ND	2	18	1	4	2	98	.05	.169	2	43	1.74	362	.12	2	1.63	.04	.19	1	27
KB6R-615	3	82	12	24	.3	3	1	189	7.50	15	5	ND	1	21	1	4	2	56	.01	.101	2	29	.92	418	.02	2	.98	.04	.15	1	29
KB6R-616	5	96	15	62	1.1	5	1	370	5.31	13	5	ND	1	13	1	2	2	52	.01	.069	2	28	1.29	414	.01	8	1.25	.03	.20	1	125
KB6R-617	1	61	19	42	.1	5	1	349	6.18	7	5	ND	1	19	1	2	2	69	.02	.088	2	33	1.46	235	.01	6	1.28	.05	.18	1	20
KB6R-618	4	110	43	94	.2	5	1	328	6.73	9	5	ND	2	43	1	2	2	63	.01	.099	2	29	1.28	352	.01	4	1.23	.04	.19	1	23
KB6R-1341	3	94	618	442	2.9	11	6	1512	7.22	308	5	ND	2	12	1	11	2	29	.14	.195	2	16	.73	176	.01	4	1.15	.03	.25	1	125
KB6R-1342	1	32	1165	237	8.9	3	2	969	2.34	198	5	ND	1	17	2	13	2	9	.40	.111	3	2	.09	167	.01	2	.26	.02	.21	1	425
KB6R-1355	2	111	7101	315	51.0	2	1	5129	3.38	254	5	3	1	39	1	42	2	10	.78	.075	2	2	.19	66	.01	5	.17	.03	.15	1	2630
KB6R-1356	1	69	390	239	3.7	4	2	858	4.86	576	5	ND	1	13	1	13	3	11	.02	.147	2	3	.04	130	.01	9	.26	.01	.24	1	750
KB6R-1378	2	81	374	232	4.4	6	4	1326	6.36	57	5	ND	1	12	1	8	2	48	.15	.133	2	21	1.33	204	.28	6	1.20	.03	.20	1	150
KB6R-1379	1	75	56	312	1.8	8	4	2244	5.77	45	5	ND	1	15	1	2	2	62	.17	.138	4	30	2.58	272	.28	6	1.98	.04	.17	1	85
KB6R-1380	1	82	47	279	1.8	11	5	2422	5.79	63	5	ND	1	21	1	2	2	60	.33	.166	5	29	2.44	135	.29	7	1.95	.04	.18	1	60
KB6R-1381	1	52	34	181	.8	3	3	1297	3.60	23	5	ND	1	24	1	2	2	33	.27	.174	5	4	1.11	377	.14	6	1.23	.03	.21	1	23
KB6R-1382	1	100	101	524	3.4	9	6	2828	6.96	93	5	ND	1	14	1	2	2	71	.23	.163	2	23	2.05	164	.30	2	1.90	.04	.18	1	85
KB6R-1383	3	104	129	454	2.6	13	11	4186	6.86	104	5	ND	1	24	1	3	2	80	.66	.146	5	31	2.99	52	.23	3	2.37	.05	.15	1	50
KB6R-1384	1	109	61	283	1.2	9	5	1482	5.65	65	5	ND	1	9	1	2	2	42	.18	.160	2	18	1.16	183	.23	6	1.21	.03	.21	1	95
KB6R-1385	23	157	122	51	3.5	3	5	409	4.53	59	5	ND	2	7	1	3	3	25	.06	.133	2	3	.19	170	.02	9	.55	.02	.27	1	370
KB6R-1386	2	178	18	121	2.1	6	8	1257	5.81	43	5	ND	1	17	1	2	2	79	.16	.178	2	8	1.04	251	.26	7	1.69	.03	.19	5	335
KB6R-1387	5	211	30	107	3.2	5	10	1295	6.55	66	5	ND	2	28	1	2	2	58	.26	.151	2	7	.75	362	.17	6	1.25	.03	.23	1	605
KB6R-1388	62	158	11	14	2.4	2	3	117	3.85	48	5	ND	2	11	1	3	3	22	.07	.131	2	1	.10	107	.13	6	.48	.02	.35	11	625
KB6R-1391	1	174	5	74	.5	7	13	1429	5.24	16	5	ND	1	127	1	2	2	119	.55	.142	5	14	2.54	1256	.21	6	2.52	.06	.13	1	215
KB6R-1392	3	248	30	62	3.5	4	7	1113	4.81	108	5	2	2	22	1	2	2	48	.26	.144	3	9	1.02	118	.13	9	1.41	.04	.26	1	1290
KB6R-1393	9	153	16	18	.7	2	5	114	3.80	31	5	ND	2	6	1	3	3	18	.07	.132	3	1	.08	98	.01	7	.49	.02	.35	1	90
KB6R-1394	13	109	21	30	.5	2	6	292	2.96	29	5	ND	2	6	1	3	2	19	.16	.142	3	1	.15	92	.01	4	.62	.02	.36	1	75
STD C/AU-0.5	20	62	41	142	7.1	73	31	1199	4.02	40	18	8	38	53	20	15	22	75	.48	.112	41	65	.89	187	.09	41	1.73	.10	.14	12	510

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ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK CHIPS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: SEPT 27 1986 DATE REPORT MAILED: Oct 4/86 ASSAYER. [signature]....DEAN TOYE. CERTIFIED B.C. ASSAYER.

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
KB6R-594	10	112	17	43	.3	6	7	535	3.60	5	5	ND	1	28	1	2	3	37	.21	.149	3	13	1.29	442	.15	2	1.28	.02	.23	5	63
KB6R-595	2	150	5	95	.2	6	15	1070	3.42	8	5	ND	1	38	1	2	2	43	.24	.125	5	9	1.04	1415	.09	2	1.07	.02	.18	2	111
KB6R-596	1	100	19	130	.2	3	10	1395	1.56	9	5	ND	1	34	1	2	3	18	.85	.088	5	2	.59	1184	.05	5	.91	.01	.26	1	69
KB6R-597	3	126	6	58	.3	5	11	809	3.01	19	5	ND	1	63	1	2	6	38	.15	.107	5	9	1.55	1047	.10	2	1.60	.01	.19	1	310
KB6R-600	8	114	20	31	1.0	4	8	140	4.14	34	5	ND	1	32	1	15	2	21	.05	.114	6	7	.29	325	.01	2	.49	.01	.15	1	515
KB6R-601	6	158	8	46	1.1	5	15	2076	4.61	19	5	ND	1	32	1	2	3	11	.29	.139	5	5	.49	96	.01	6	.71	.01	.17	1	310
KB6R-602	3	190	11	48	.4	1	10	223	5.49	19	5	ND	1	61	1	2	2	42	.02	.263	10	5	.58	589	.01	4	.85	.01	.16	1	33
KB6R-603	3	210	22	100	.7	14	14	762	7.30	21	5	ND	1	49	1	2	4	100	.07	.154	3	60	1.97	421	.29	5	1.99	.01	.14	1	77
KB6R-604	7	242	34	112	.6	14	15	790	6.05	9	5	ND	1	41	1	2	2	97	.10	.144	5	57	2.13	267	.27	4	2.06	.01	.12	1	44
KB6R-605	3	262	19	78	.6	14	16	918	7.43	18	5	ND	1	30	1	2	2	82	.06	.155	4	56	2.26	191	.29	2	2.05	.01	.12	1	46
STD C/AU-R	21	59	43	134	7.1	71	30	1017	3.96	41	20	8	33	48	17	15	21	63	.48	.109	36	59	.88	179	.08	39	1.73	.06	.14	13	485

R

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-637	2	98	80	345	.7	25	12	1697	4.60	31	9	ND	2	84	1	24	2	69	1.42	.125	7	22	1.50	149	.01	6	2.09	.06	.22	1	11
K86R-638	2	83	24	179	.7	20	15	1426	5.54	31	5	ND	2	27	1	5	2	96	.68	.152	4	19	1.54	102	.01	4	2.16	.07	.18	1	4
K86R-639	2	155	23	115	.7	23	11	1484	4.15	163	9	ND	1	82	1	17	2	56	1.71	.123	7	14	.69	112	.01	8	1.14	.07	.16	1	8
K86R-640	3	198	25	154	.6	14	12	1418	5.25	524	5	ND	2	22	1	14	3	99	.41	.156	7	9	1.18	113	.01	7	1.78	.05	.15	1	55
K86R-641	49	186	6	33	.5	6	6	372	3.27	104	5	ND	2	13	1	9	2	33	.25	.135	2	8	.35	205	.01	8	1.05	.03	.30	1	85
K86R-643	10	176	36	85	1.7	6	5	844	4.72	78	5	ND	1	37	1	34	3	53	.21	.151	2	10	.80	151	.01	7	1.39	.03	.26	1	49
K86R-644	2	163	378	516	4.3	22	11	1275	4.46	95	5	ND	2	14	1	16	7	31	.32	.132	7	11	.76	96	.01	12	1.59	.03	.28	1	16
K86R-645	2	132	14	126	.4	14	10	1760	4.30	43	5	ND	1	44	1	2	2	70	1.00	.138	4	12	1.27	172	.06	7	1.79	.05	.25	1	58
K86R-646	1	54	7	80	.1	8	11	1098	4.61	17	9	ND	2	52	1	5	2	101	1.04	.159	5	6	1.64	72	.01	6	2.02	.07	.13	1	2
K86R-647	1	64	5	96	.5	9	13	1300	4.65	20	6	ND	2	64	1	6	2	84	1.21	.175	7	7	1.87	139	.01	6	2.28	.07	.24	1	2
K86R-648	1	126	7	122	.1	8	12	1143	4.90	22	5	ND	2	41	1	6	2	92	.84	.181	7	6	1.57	115	.01	5	2.02	.06	.20	1	3
K86R-649	4	162	19	55	1.0	7	7	502	3.28	95	5	ND	2	26	1	11	2	41	.46	.146	4	11	.54	206	.01	7	1.06	.03	.31	1	55
K86R-650	4	112	15	68	.7	19	7	1069	2.78	54	6	ND	3	30	1	6	2	96	.79	.138	6	24	1.07	169	.02	9	1.39	.04	.29	1	60
K86R-651	2	66	93	69	.5	12	8	863	2.14	38	5	ND	1	33	1	2	2	35	.72	.136	4	9	.58	180	.02	8	1.01	.04	.30	1	36
K86R-652	2	77	10	106	.6	11	9	926	2.37	35	5	ND	1	22	1	3	2	47	.61	.145	4	13	.70	232	.03	6	1.16	.04	.30	1	55
K86R-653	5	171	30	120	.8	16	10	1113	4.10	112	5	ND	2	12	1	2	2	83	.35	.143	7	16	1.30	240	.03	7	1.79	.04	.27	1	95
K86R-655	13	456	12	54	.5	4	13	49	5.82	182	5	ND	1	15	1	17	2	13	.15	.093	4	1	.15	8	.01	5	.45	.03	.22	1	75
K86R-656	4	346	51	75	1.0	3	8	25	4.27	163	5	ND	1	10	1	14	2	10	.07	.069	4	1	.03	10	.01	6	.34	.02	.21	1	95
K86R-657	6	130	8	2	.1	5	9	13	4.77	26	5	ND	1	9	1	4	2	9	.03	.038	3	1	.04	9	.01	5	.34	.03	.18	1	80
K86R-658	5	210	25	20	.3	6	10	184	6.14	40	5	ND	1	36	1	3	2	10	.23	.046	3	1	.12	5	.01	5	.36	.03	.17	1	65
K86R-659	2	358	32	11	.4	5	10	19	8.46	37	5	ND	1	14	1	2	2	10	.14	.072	2	1	.07	5	.01	2	.38	.03	.19	1	95
K86R-660	22	2782	31	114	1.5	13	19	41	7.68	266	6	ND	1	41	1	44	2	15	.18	.106	2	1	.14	5	.01	2	.40	.03	.21	1	155
K86R-661	57	1625	15	118	2.9	9	13	17	5.00	157	5	ND	1	64	1	101	2	9	.03	.062	4	2	.04	6	.01	5	.28	.02	.18	1	195
K86R-662	35	576	78	31	.8	46	23	21	9.15	114	5	ND	1	33	1	25	2	9	.04	.062	2	4	.06	5	.01	2	.28	.03	.17	1	85
K86R-663	24	647	37	29	.7	23	32	25	13.31	123	5	ND	1	14	1	10	2	11	.02	.010	2	3	.10	3	.01	2	.28	.03	.15	1	135
K86R-664	93	1175	49	87	2.3	21	21	22	11.32	161	5	ND	2	20	1	25	2	12	.04	.019	2	2	.07	3	.01	2	.30	.03	.17	1	175
K86R-665	5	450	21	41	.5	55	18	24	7.48	100	5	ND	1	24	1	16	2	9	.07	.045	5	7	.12	6	.01	2	.35	.03	.17	1	95
K86R-666	452	325	90	110	.4	23	42	22	15.96	96	5	ND	2	555	1	2	2	4	.05	.005	2	1	.02	2	.01	2	.08	.03	.06	1	335
K86R-667	17	513	23	11	.2	13	15	26	7.44	55	5	ND	1	22	1	2	2	12	.19	.118	2	1	.06	6	.01	2	.36	.04	.18	1	48
K86R-668	10	341	16	22	.4	6	9	43	4.63	17	5	ND	1	10	1	2	2	9	.06	.015	4	2	.11	9	.01	5	.35	.02	.17	1	65
K86R-669	2	289	13	73	.9	3	10	911	4.64	62	5	ND	1	25	1	13	2	10	.56	.125	4	1	.25	8	.01	5	.42	.04	.17	1	55
K86R-670	4	388	6	17	.5	3	11	30	5.62	28	5	ND	1	17	1	4	2	10	.19	.124	2	2	.08	7	.01	6	.39	.03	.19	1	75
K86R-671	7	602	9	20	.4	5	12	44	6.89	25	5	ND	1	11	1	2	2	10	.16	.085	6	2	.10	6	.01	3	.37	.03	.17	1	95
K86R-672	9	899	10	201	.3	23	13	913	4.81	18	7	ND	1	51	1	2	2	33	1.38	.146	5	18	1.00	14	.01	5	1.24	.05	.17	1	120
K86R-673	16	874	19	20	.5	2	10	57	5.57	52	5	ND	1	13	1	4	2	8	.24	.118	2	2	.05	10	.01	4	.36	.03	.18	1	135
K86R-674	9	1066	14	19	.5	2	10	111	4.74	30	5	ND	1	12	1	4	2	9	.26	.100	3	1	.06	12	.01	6	.37	.03	.19	1	295
STD C/AU 0.5	22	60	38	138	7.3	71	29	1126	3.95	35	19	7	36	50	18	15	20	69	.48	.105	36	59	.88	187	.09	36	1.73	.09	.15	13	515

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
KB6R-675	13	212	16	67	.8	2	6	308	5.05	44	5	ND	2	46	1	5	2	9	.18	.146	3	1	.30	25	.01	5	.83	.03	.16	1	20
KB6R-676	34	178	15	1	.4	4	14	16	3.94	7	5	ND	1	7	1	2	2	7	.04	.038	2	1	.02	21	.01	5	.26	.02	.17	1	65
KB6R-677	19	415	22	20	1.0	3	10	92	7.26	37	5	ND	1	30	1	3	2	11	.11	.239	2	1	.12	10	.01	7	.52	.03	.19	1	100
KB6R-678	5	274	13	273	.1	1	7	1470	7.20	12	5	ND	2	73	1	2	2	7	.57	.211	13	1	1.40	136	.01	6	2.85	.04	.11	2	6
KB6R-679	5	201	10	230	.1	1	6	1116	6.73	8	5	ND	3	28	1	2	2	7	.49	.215	10	1	1.27	299	.01	5	2.74	.04	.12	1	9
KB6R-680	7	150	12	173	.2	1	5	721	5.85	21	5	ND	2	42	1	2	2	8	.47	.232	7	1	.85	431	.01	7	1.98	.04	.11	1	48
KB6R-681	4	162	10	162	.1	2	4	497	5.08	18	5	ND	2	35	1	2	2	7	.29	.147	8	1	.66	256	.01	5	1.57	.03	.10	1	16
KB6R-682	55	823	8	14	.6	4	10	39	3.84	8	5	ND	1	45	1	2	2	10	.04	.034	2	1	.11	8	.01	4	.42	.02	.18	1	290
KB6R-683	73	895	13	18	.8	4	15	65	5.88	10	5	ND	1	87	1	5	2	11	.08	.057	2	1	.14	7	.01	4	.41	.02	.15	1	325
KB6R-684	49	932	8	6	.5	5	15	32	4.31	3	5	ND	1	100	1	5	2	12	.09	.071	2	1	.08	8	.01	6	.46	.03	.23	1	185
KB6R-685	41	723	9	4	.5	2	11	12	3.22	5	5	ND	1	37	1	2	2	6	.03	.035	2	1	.04	10	.01	3	.23	.02	.14	1	200
KB6R-686	6	370	12	9	.2	3	14	28	5.18	16	5	ND	1	20	1	2	2	8	.13	.067	2	1	.07	8	.01	5	.29	.02	.15	1	100
KB6R-687	33	963	9	6	.2	2	10	17	4.14	3	5	ND	1	10	1	2	2	8	.06	.040	2	1	.05	10	.01	3	.28	.02	.15	1	170
KB6R-688	75	1548	11	16	.3	3	14	27	4.51	2	5	ND	1	20	1	4	2	10	.14	.083	2	2	.11	12	.01	6	.39	.02	.19	1	175
KB6R-689	50	1179	8	8	.2	4	14	22	4.81	15	5	ND	1	38	1	2	2	10	.15	.102	2	2	.05	8	.01	5	.34	.03	.19	1	215
KB6R-690	37	1175	9	4	.3	5	13	18	3.49	9	5	ND	1	80	1	2	2	8	.05	.053	2	1	.02	10	.01	3	.27	.02	.17	1	275
KB6R-691	120	900	29	2	.5	3	6	13	4.29	16	5	ND	1	70	1	9	2	11	.01	.093	2	1	.01	15	.01	4	.21	.02	.16	1	320
KB6R-692	54	381	9	11	.4	3	4	40	3.08	5	5	ND	1	111	1	2	2	10	.02	.038	2	2	.08	15	.01	2	.41	.02	.18	1	250
KB6R-693	84	788	13	31	.5	3	7	12	2.93	86	5	ND	1	59	1	25	2	9	.01	.035	2	1	.02	13	.01	2	.25	.02	.16	1	180
KB6R-694	150	1425	10	152	1.1	2	9	11	3.18	380	5	ND	1	66	1	88	2	11	.01	.052	2	1	.01	13	.01	2	.26	.02	.17	1	170
KB6R-695	47	1099	15	197	1.9	3	9	13	5.82	253	6	ND	1	80	1	137	2	8	.04	.054	2	1	.02	8	.01	6	.24	.02	.14	1	255
KB6R-696	105	628	11	23	.8	3	6	47	3.05	24	5	ND	1	75	1	12	2	13	.07	.109	2	1	.10	13	.01	2	.37	.02	.17	1	250
KB6R-697	71	358	17	9	.5	2	7	24	6.39	19	9	ND	1	144	1	2	3	17	.06	.149	2	1	.10	17	.01	7	.37	.03	.20	1	150
KB6R-698	47	432	19	18	.8	2	4	12	3.49	45	5	ND	1	64	1	28	2	9	.01	.089	2	1	.03	22	.01	4	.22	.02	.14	1	145
KB6R-703	9	219	33	100	.5	1	4	352	5.70	20	5	ND	1	12	1	2	2	47	.12	.174	2	3	1.07	38	.01	6	1.15	.03	.13	1	65
KB6R-704	8	205	22	191	.2	1	3	515	5.39	8	5	ND	1	16	1	2	2	57	.14	.191	5	1	1.42	164	.01	5	1.50	.03	.13	1	70
KB6R-705	6	873	31	232	1.3	1	7	436	6.28	16	5	ND	2	39	1	2	2	22	.20	.174	7	1	.83	88	.01	4	1.63	.03	.13	1	180
KB6R-706	4	653	27	346	.3	1	13	947	7.51	18	5	ND	3	97	1	2	2	22	.38	.237	20	1	1.41	831	.01	4	2.90	.04	.12	1	41
KB6R-707	2	188	5	171	.1	1	3	391	2.59	2	5	ND	7	10	1	2	2	2	.04	.020	46	1	.26	299	.01	2	.88	.02	.12	1	4
KB6R-710	5	344	32	28	.7	2	1	131	4.42	137	5	ND	1	12	1	34	2	12	.01	.047	2	4	.08	557	.01	3	.25	.02	.10	1	125
KB6R-711	3	596	48	28	1.9	2	1	26	3.73	546	5	ND	1	10	1	133	2	12	.01	.030	2	1	.01	108	.01	4	.17	.02	.09	1	330
KB6R-712	2	243	59	2	1.0	2	1	20	3.84	81	5	ND	1	14	1	22	2	13	.01	.069	2	1	.02	256	.01	2	.24	.02	.15	1	260
KB6R-713	6	233	45	5	1.0	2	1	38	4.35	50	5	ND	1	18	1	7	2	13	.01	.078	2	1	.01	491	.01	4	.19	.02	.12	1	850
KB6R-714	7	644	33	10	1.8	1	1	20	4.05	69	5	ND	1	13	1	33	2	12	.01	.058	2	1	.02	98	.01	2	.18	.02	.11	1	385
KB6R-715	9	485	124	4	1.6	2	2	18	4.45	54	5	ND	1	18	1	17	2	12	.02	.131	2	1	.02	44	.01	2	.27	.02	.17	1	340
KB6R-716	5	104	58	106	.4	41	3	214	4.96	26	5	ND	2	85	1	2	2	71	.29	.299	11	58	1.08	302	.01	4	1.43	.04	.18	1	100
STD C/AU-0.5	21	62	43	141	7.3	73	30	1151	3.97	36	16	8	36	51	19	16	21	71	.48	.112	36	62	.89	189	.09	34	1.73	.09	.15	12	500

R

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
K86R-717	18	100	53	2	.3	1	2	12	3.75	24	5	ND	1	25	1	3	2	11	.17	.227	10	1	.03	93	.01	4	.35	.02	.19	1	95
K86R-718	17	164	19	7	.2	1	2	53	4.37	14	5	ND	1	11	1	2	3	11	.09	.158	3	1	.04	122	.01	8	.36	.02	.18	1	80
K86R-719	11	126	20	141	.3	38	5	757	4.39	22	5	ND	1	61	1	4	2	62	.61	.204	12	49	1.22	671	.01	5	1.47	.04	.15	1	105
K86R-720	2	704	18	132	.1	2	9	1062	3.46	10	5	ND	3	33	1	2	2	24	.32	.099	16	2	.80	227	.01	3	1.35	.05	.14	1	6
K86R-721	2	357	11	110	.2	1	7	1453	3.16	8	5	ND	3	67	1	2	2	27	1.41	.090	13	2	.87	1179	.01	2	1.42	.07	.11	1	5
K86R-722	2	336	13	117	.1	1	7	1031	3.20	28	5	ND	3	77	1	2	2	22	.33	.112	13	1	.87	1229	.01	3	1.45	.05	.17	1	6
K86R-723	1	190	18	135	.1	1	5	803	3.62	94	5	ND	3	40	1	2	2	21	.24	.096	16	2	.82	223	.01	4	1.22	.05	.13	1	12
K86R-724	2	278	11	127	.1	1	7	1080	3.27	53	5	ND	3	29	1	2	2	24	.23	.100	15	1	.99	267	.01	3	1.43	.05	.15	2	23
K86R-725	5	233	12	133	.1	1	6	601	5.99	13	5	ND	2	32	1	5	2	25	.16	.169	14	1	.90	733	.01	4	1.62	.04	.15	1	29
K86R-729	3	131	23	27	.6	6	3	80	5.57	89	5	ND	2	8	1	8	3	18	.04	.165	13	8	.11	146	.01	6	.36	.02	.18	1	145
K86R-730	2	141	15	30	.5	9	2	80	5.60	138	5	ND	2	4	1	15	3	14	.04	.182	15	9	.09	85	.01	5	.33	.02	.16	1	135
K86R-731	3	113	22	81	.5	11	2	77	5.52	38	5	ND	2	5	1	11	2	14	.03	.153	14	9	.08	108	.01	4	.33	.02	.16	1	130
K86R-732	3	96	16	33	.4	5	2	117	3.81	40	5	ND	1	4	1	3	3	12	.05	.121	7	7	.08	67	.01	4	.30	.02	.14	1	210
K86R-733	4	69	15	16	.3	3	1	39	2.92	34	5	ND	1	5	1	5	4	10	.03	.110	10	7	.07	71	.01	3	.32	.01	.17	1	140
K86R-734	4	140	48	52	.7	31	5	84	5.85	59	5	ND	1	10	1	7	3	14	.08	.186	5	28	.04	105	.01	8	.30	.02	.16	1	130
K86R-735	5	131	28	135	3.0	25	3	218	5.82	38	5	ND	1	5	1	5	4	20	.10	.193	11	34	.14	105	.01	9	.45	.02	.19	1	335
K86R-736	4	195	40	93	1.8	20	3	427	8.09	153	5	ND	1	6	1	3	5	17	.03	.148	11	48	.10	82	.01	3	.32	.02	.13	1	365
K86R-737	3	165	46	130	2.3	8	2	198	5.78	88	5	ND	2	9	1	7	3	16	.12	.250	10	10	.14	133	.01	6	.48	.02	.20	1	350
K86R-744	2	74	67	48	.8	9	5	58	2.73	38	5	ND	1	5	1	9	2	10	.03	.012	7	1	.20	22	.01	3	.41	.02	.16	2	90
K86R-745	3	164	40	151	.5	11	6	234	3.39	59	5	ND	1	7	1	5	2	11	.14	.062	7	2	.27	21	.01	3	.50	.02	.16	1	60
K86R-746	4	626	40	162	5.1	11	7	460	5.33	253	5	ND	1	6	1	56	2	14	.16	.096	9	1	.41	16	.01	4	.62	.03	.14	1	135
K86R-747	4	115	7	141	1.4	1	5	841	5.00	92	5	ND	1	24	1	4	2	40	.63	.163	6	1	1.26	61	.01	4	1.39	.04	.14	1	30
K86R-748	6	179	17	246	.2	7	7	703	5.92	115	5	ND	1	23	1	9	2	49	.31	.164	7	19	2.19	66	.01	5	2.18	.04	.08	1	36
K86R-749	2	162	9	145	.2	2	8	1458	4.14	27	5	ND	1	43	1	2	2	45	1.99	.163	6	2	1.60	83	.01	2	1.91	.05	.13	1	34
K86R-750	3	241	17	223	.1	1	7	1909	5.15	68	5	ND	1	81	1	5	2	35	1.12	.229	9	2	1.27	43	.01	4	1.47	.05	.13	2	38
K86R-751	6	185	60	88	.9	8	8	733	6.09	83	5	ND	1	17	1	6	2	14	.39	.071	4	2	.22	6	.01	5	.43	.03	.16	1	90
K86R-752	8	546	42	137	.6	18	8	207	5.38	62	5	ND	1	8	1	14	2	13	.13	.031	6	2	.18	9	.01	3	.47	.02	.18	1	65
K86R-753	3	299	36	330	.2	5	11	3608	4.51	71	5	ND	1	37	1	3	2	15	2.15	.184	7	2	.86	16	.01	3	.47	.05	.17	2	31
K86R-754	2	167	30	235	.2	4	9	2319	4.31	77	5	ND	1	32	1	3	2	15	1.58	.190	7	1	.69	15	.01	5	.48	.05	.15	1	39
K86R-756	4	262	19	41	.4	23	19	41	7.76	140	5	ND	1	9	1	12	2	14	.13	.081	2	1	.10	5	.01	3	.42	.03	.14	1	50
K86R-757	3	190	26	22	.4	30	20	59	8.69	122	5	ND	1	10	1	6	2	19	.23	.120	4	5	.18	4	.01	2	.52	.03	.12	1	53
K86R-758	4	182	15	22	.4	23	15	21	6.90	90	5	ND	1	9	1	17	4	11	.07	.058	2	3	.08	6	.01	4	.33	.02	.10	1	65
K86R-759	3	280	23	49	1.0	25	20	17	9.43	203	5	ND	1	4	1	25	2	10	.01	.090	2	1	.03	5	.01	3	.21	.03	.11	1	90
K86R-761	5	3112	39	78	.5	5	8	254	3.76	68	5	ND	1	19	1	3	2	26	.08	.080	3	1	.47	27	.01	4	.82	.02	.09	1	85
K86R-762	5	4392	31	116	1.2	9	4	152	2.67	54	5	ND	1	13	4	4	2	22	.04	.057	2	8	.24	39	.01	2	.56	.02	.13	1	65
K86R-763	3	1009	104	423	.5	35	5	3568	3.44	59	5	ND	1	41	5	2	2	60	.65	.112	2	47	1.14	78	.01	2	1.41	.04	.10	1	49
STD C/AU-0.5	20	60	42	139	7.2	73	30	1133	3.97	41	17	8	35	49	19	16	21	69	.48	.108	38	63	.88	182	.09	33	1.73	.09	.14	15	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
KB6R-765	5	207	143	1658	.9	3	5	3754	5.74	144	5	ND	1	28	8	8	2	53	1.17	.149	7	1	1.62	36	.01	2	1.61	.05	.12	1	115
KB6R-766	2	659	33	252	.2	5	14	3166	5.45	66	5	ND	1	22	1	2	2	41	.56	.203	8	5	1.16	155	.01	4	1.62	.04	.14	1	75
KB6R-767	3	343	18	189	.4	4	13	6267	4.50	21	5	ND	1	69	1	2	2	27	4.11	.161	4	1	1.77	25	.01	3	.85	.06	.13	1	47
KB6R-768	2	381	13	181	.3	3	14	4988	4.21	19	5	ND	1	75	1	3	2	31	3.86	.189	4	1	1.75	64	.01	3	1.47	.06	.14	1	34
KB6R-769	3	437	16	147	.5	5	27	3971	5.65	26	5	ND	1	50	1	2	2	36	2.84	.177	4	1	1.79	29	.01	2	1.62	.06	.13	1	50
KB6R-770	3	433	12	117	.2	3	12	1717	4.55	15	7	ND	2	134	1	2	3	41	2.79	.193	5	1	1.35	56	.01	2	1.82	.06	.14	1	70
KB6R-771	2	1006	15	238	.2	4	17	3205	6.48	5	6	ND	2	81	1	6	2	43	1.86	.180	4	1	1.29	51	.01	2	1.76	.05	.13	1	31
KB6R-772	2	225	12	211	.3	3	12	7337	3.93	57	5	ND	1	156	1	2	4	31	6.43	.154	7	1	1.85	39	.01	2	.89	.07	.14	1	42
KB6R-773	2	284	13	157	.4	2	7	9602	4.16	23	5	ND	1	73	1	2	2	30	4.27	.160	3	2	1.47	72	.01	2	.66	.07	.14	1	60
KB6R-774	1	327	26	156	1.6	2	9	2060	5.63	19	5	ND	1	35	1	2	5	35	.62	.107	5	1	.63	389	.01	3	1.09	.04	.16	1	195
KB6R-775	1	895	12	197	.6	5	14	4929	6.13	19	5	ND	1	70	1	2	3	40	3.42	.177	5	1	1.38	49	.01	2	1.42	.06	.14	1	90
KB6R-776	1	241	10	119	.3	3	12	4036	4.79	3	5	ND	2	235	1	2	2	35	7.13	.151	10	1	1.22	214	.01	3	1.42	.07	.13	1	13
KB6R-777	1	222	4	102	.4	3	12	3480	4.71	13	5	ND	1	57	1	2	2	33	2.06	.198	6	2	.83	364	.01	4	1.40	.05	.15	1	19
KB6R-778	2	1325	11	85	.7	3	12	6982	3.93	12	5	ND	1	76	1	2	3	26	.84	.206	6	1	.44	71	.01	6	1.02	.04	.18	1	17
KB6R-779	8	79	12	91	.2	1	1	323	5.47	13	5	ND	1	14	1	5	3	34	.10	.135	2	1	.65	165	.01	2	1.28	.03	.15	1	46
KB6R-1886	7	192	24	14	1.1	9	8	151	5.35	2748	5	ND	2	13	1	68	3	22	.23	.161	8	4	.13	50	.01	7	.71	.02	.27	1	270
KB6R-1887	11	172	728	36	13.4	6	4	217	3.66	404	5	ND	2	11	1	28	3	29	.27	.172	9	6	.30	166	.01	6	.95	.02	.28	1	860
KB6R-1888	15	633	27	54	.6	6	8	581	6.65	280	5	ND	2	13	1	24	2	65	.23	.171	7	11	.93	154	.01	2	1.79	.03	.27	1	240
KB6R-1889	24	808	46	55	1.1	2	5	371	4.71	280	5	ND	2	9	1	68	2	43	.27	.181	9	1	.70	153	.01	6	1.31	.03	.32	15	90
KB6R-1890	22	477	34	58	1.4	4	9	877	4.29	160	5	ND	2	22	1	115	2	62	.64	.194	8	4	1.19	129	.04	5	1.59	.04	.30	1	70
KB6R-1891	30	1174	37	58	2.1	9	14	843	5.70	103	5	ND	2	10	1	58	2	59	.32	.177	8	7	.84	26	.05	4	1.50	.03	.32	1	125
KB6R-1892	32	1058	84	76	3.9	5	9	870	4.80	201	5	3	2	17	1	84	3	42	.26	.180	7	2	.46	89	.02	5	1.10	.03	.34	1	3720
KB6R-1893	20	1039	59	74	171.6	4	6	1374	5.41	1202	5	ND	2	16	1	654	4	58	.42	.181	6	4	.51	92	.03	3	1.21	.03	.32	1	915
KB6R-1894	1	231	14	166	.5	6	20	1897	6.29	17	5	ND	2	22	1	2	2	133	.78	.186	11	7	2.63	221	.13	4	2.78	.07	.17	1	29
KB6R-1895	3	176	14	104	1.4	5	14	1512	5.57	40	5	ND	2	29	1	8	2	109	.88	.177	11	8	2.03	226	.10	4	2.28	.06	.21	2	47
KB6R-1896	6	372	40	69	3.2	8	8	790	6.97	138	5	ND	2	10	1	21	4	73	.22	.183	5	22	.69	132	.11	2	1.36	.03	.34	1	265
KB6R-1898	2	252	11	63	.5	3	16	1726	5.18	14	6	ND	2	138	1	9	2	91	1.35	.186	8	2	1.66	305	.17	3	2.00	.07	.22	1	48
KB6R-1899	6	78	16	175	.1	3	8	1475	7.14	456	5	ND	3	26	1	2	2	19	.40	.204	19	1	.92	242	.01	2	2.42	.05	.20	1	30
KB6R-1900	4	94	23	60	.7	3	7	350	4.70	460	5	ND	2	79	1	8	2	19	.26	.211	9	1	.21	44	.01	5	.87	.03	.34	1	135
KB6R-1901	4	93	22	179	.1	2	7	1224	6.70	86	5	ND	4	13	1	5	2	11	.30	.140	22	1	.72	228	.03	2	2.31	.05	.18	1	10
KB6R-1902	5	49	23	91	.1	2	2	582	3.04	40	5	ND	3	8	1	3	2	2	.13	.066	20	1	.29	196	.01	6	1.19	.03	.23	1	16
KB6R-1903	5	85	17	101	.2	1	3	1000	5.39	58	5	ND	2	8	1	6	2	17	.21	.154	11	1	.55	211	.01	4	1.68	.03	.26	1	33
KB6R-1905	4	171	13	180	.1	3	7	1003	5.18	27	5	ND	2	14	1	3	2	6	.27	.130	19	1	.62	324	.04	2	1.79	.05	.20	1	16
KB6R-1906	1	102	26	139	.7	30	13	1275	5.06	59	5	ND	2	26	1	6	2	57	.57	.154	21	24	1.30	194	.01	5	2.23	.05	.33	1	12
KB6R-1908	2	470	1660	1544	13.6	13	13	1380	5.17	407	5	ND	1	52	7	11	8	54	1.24	.165	9	9	.91	150	.01	6	1.84	.05	.33	1	495
KB6R-1910	4	92	23	64	.5	32	10	854	3.72	58	5	ND	2	11	1	7	3	82	.27	.143	9	30	.81	253	.02	6	1.60	.04	.35	1	60
STD C/AU 0.5	20	62	42	141	7.3	73	30	1155	3.97	44	16	8	37	51	19	15	22	71	.48	.109	39	61	.89	190	.09	36	1.73	.10	.13	13	505

CASSIAR MINING PROJECT - 7506 FILE # 86-2303

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
KB6R-1911	8	89	26	97	.9	19	9	1346	5.26	39	5	ND	2	19	1	4	2	110	.50	.144	4	15	1.50	153	.06	3	1.96	.05	.21	1	200
KB6R-1913	2	36	23	64	.2	8	3	430	2.43	164	5	ND	1	13	1	10	2	22	.41	.128	3	8	.38	152	.13	6	.85	.02	.26	1	39
KB6R-1915	3	230	119	30	.8	3	4	50	2.63	44	5	ND	1	7	1	4	2	9	.19	.015	2	2	.09	24	.01	4	.25	.01	.13	2	100
KB6R-1917A	2	191	64	498	.4	3	8	881	4.02	65	5	ND	1	28	2	5	2	8	.83	.142	2	1	.21	9	.01	5	.25	.03	.11	1	90
KB6R-1918	3	82	95	48	.5	1	3	117	1.97	44	5	ND	1	8	1	4	2	10	.31	.023	4	1	.28	50	.01	5	.40	.01	.12	1	70
KB6R-1919	3	172	87	379	.8	4	8	86	3.91	117	11	ND	1	111	2	8	2	8	.45	.039	2	1	.11	7	.01	6	.31	.02	.15	1	110
KB6R-1920	3	151	27	171	.4	3	11	3221	4.54	44	7	ND	1	76	1	3	2	26	3.76	.151	2	1	1.07	14	.01	4	1.03	.06	.10	1	30
KB6R-1921	2	150	32	162	.5	3	10	1516	4.73	35	5	ND	1	35	1	2	2	24	2.00	.147	2	1	.76	15	.01	4	1.03	.05	.13	1	41
KB6R-1922	2	169	47	242	.4	2	7	818	4.57	46	5	ND	1	17	1	2	2	20	1.15	.182	2	1	.49	17	.01	5	.73	.03	.10	1	30
KB6R-1923	3	115	53	444	.3	2	9	3728	4.26	31	6	ND	1	58	2	2	2	18	3.83	.154	2	1	1.13	9	.01	4	.66	.06	.12	1	19
KB6R-1924	2	124	11	172	.3	2	9	3596	4.00	24	9	ND	2	90	1	2	2	22	5.73	.151	2	2	1.13	28	.01	4	.80	.07	.09	1	15
KB6R-1925	2	127	34	276	.4	2	12	4482	4.85	47	5	ND	1	34	1	3	2	20	2.84	.166	2	1	.99	12	.01	4	.65	.05	.09	1	18
KB6R-1926	1	156	49	103	.5	1	3	11	1.50	69	5	ND	1	7	1	10	2	8	.95	.004	2	1	.07	36	.01	3	.32	.02	.11	1	42
KB6R-1927	3	493	16	163	.4	4	7	3269	4.37	60	5	ND	1	42	1	6	2	16	2.57	.140	2	2	.85	12	.01	4	.63	.05	.11	1	70
KB6R-1928	4	215	13	19	.6	5	10	23	6.65	72	16	ND	1	214	1	11	3	5	1.11	.020	2	1	.02	5	.01	3	.17	.02	.10	1	80
KB6R-1929	3	421	15	13	.6	8	9	53	5.50	43	5	ND	1	78	1	10	6	7	1.28	.063	2	1	.04	5	.01	4	.24	.02	.11	1	80
KB6R-1930	3	386	19	19	.5	7	9	75	5.75	59	11	ND	1	171	1	14	3	9	1.49	.112	2	1	.06	5	.01	7	.30	.03	.12	1	46
KB6R-1931	4	316	29	37	.8	6	11	15	6.83	129	5	ND	1	15	1	30	4	7	1.47	.097	2	1	.02	5	.01	2	.24	.03	.14	1	100
KB6R-1932	18	528	54	76	1.1	5	9	93	5.50	107	5	ND	1	18	1	29	3	14	1.46	.095	2	4	.24	5	.01	3	.36	.02	.11	1	90
KB6R-1933	6	115	30	177	.2	3	6	1185	3.16	29	5	ND	3	23	1	3	2	38	1.90	.065	11	6	1.27	130	.01	5	1.65	.04	.13	1	17
KB6R-1934	4	408	16	569	.5	4	2	461	3.93	28	5	ND	1	36	1	4	2	41	1.62	.073	2	2	.89	104	.01	4	1.52	.03	.07	1	26
KB6R-1935	57	2437	78	340	1.7	6	18	517	6.56	77	5	ND	1	12	1	5	2	29	1.68	.052	2	1	.78	12	.01	3	1.26	.03	.09	1	35
KB6R-1936	7	468	23	93	1.5	2	3	150	6.10	159	5	ND	1	22	1	3	2	29	1.75	.102	2	1	.25	56	.01	2	.64	.02	.13	1	38
KB6R-1937	20	1248	5	12	.4	4	10	11	4.05	23	5	ND	1	13	1	26	2	4	1.88	.086	2	1	.01	11	.01	4	.19	.02	.13	1	90
KB6R-1938	11	279	8	2	.4	5	10	7	4.06	10	5	ND	1	12	1	14	2	5	1.93	.049	3	1	.02	9	.01	6	.21	.02	.15	1	60
KB6R-1939	6	220	7	1	.3	2	8	8	3.18	6	5	ND	1	5	1	7	2	4	1.92	.025	2	2	.02	16	.01	4	.18	.01	.13	1	80
KB6R-1940	10	75	6	1	.4	3	8	5	3.51	5	5	ND	1	12	1	4	2	4	1.98	.050	2	2	.01	12	.01	4	.16	.01	.12	1	60
KB6R-1941	31	180	12	6	.3	7	9	26	4.85	2	5	ND	1	72	1	3	2	7	2.21	.035	2	5	.11	7	.01	4	.26	.02	.12	1	100
KB6R-1942	15	248	12	68	.3	51	11	368	4.90	11	5	ND	1	677	1	3	2	50	2.69	.182	3	52	1.11	13	.01	5	1.23	.04	.13	1	95
KB6R-1943	78	662	10	1	.7	4	13	11	4.72	12	5	ND	1	62	1	3	2	8	2.35	.092	2	1	.02	9	.01	4	.16	.02	.13	1	240
KB6R-1944	80	1343	12	1	1.1	3	9	11	4.04	6	20	ND	1	316	1	3	2	5	2.42	.073	2	1	.01	8	.01	5	.16	.01	.12	1	360
KB6R-1945	36	518	14	1	1.2	3	10	11	5.25	4	9	ND	1	182	1	4	2	6	2.51	.023	2	1	.02	7	.01	4	.18	.02	.14	1	330
KB6R-1946	55	538	12	1	.6	3	10	7	3.72	5	5	ND	1	74	1	4	2	7	2.58	.058	2	1	.01	10	.01	4	.18	.01	.15	1	230
KB6R-1947	64	866	10	1	.5	2	13	9	4.01	3	5	ND	1	63	1	2	2	6	2.66	.034	2	1	.01	8	.01	4	.17	.01	.12	1	175
KB6R-1948	53	430	10	4	.6	3	8	9	4.76	3	5	ND	1	57	1	5	2	5	2.72	.032	2	1	.01	7	.01	4	.16	.01	.13	1	230
KB6R-1949	52	510	20	8	.9	2	9	6	3.22	27	5	ND	1	15	1	47	2	6	2.80	.049	2	1	.01	14	.01	4	.17	.01	.13	1	270
KB6R-1950	77	326	16	34	1.2	2	6	10	2.56	57	5	ND	1	28	1	30	2	4	2.86	.035	2	2	.01	12	.01	4	.14	.01	.11	2	400
STD C/AU 0.5	22	59	38	137	7.0	71	29	1119	3.94	39	17	8	36	49	18	16	18	69	3.41	.106	38	59	.88	186	.09	36	1.73	.09	.14	12	500

CASSIAR MINING PROJECT - 7506 FILE # 86-2303

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-1951	65	808	24	39	1.5	3	10	43	5.59	41	5	ND	1	60	1	20	2	11	.04	.135	2	1	.20	7	.01	5	.40	.02	.15	2	425
K86R-1952	34	5123	46	121	2.9	3	11	13	15.47	211	5	ND	1	15	1	166	2	5	.01	.038	4	1	.02	2	.01	2	.16	.03	.11	1	435
K86R-1953	95	173	19	2	.7	1	3	9	2.82	14	5	ND	1	92	1	6	2	8	.01	.051	2	2	.01	24	.01	2	.19	.01	.15	1	350
K86R-1954	59	362	12	3	.4	2	5	13	1.67	2	6	ND	1	65	1	2	2	6	.01	.044	2	1	.01	20	.01	2	.18	.01	.13	1	185
K86R-1955	47	225	13	4	.6	2	3	10	2.83	5	5	ND	1	18	1	3	2	7	.01	.077	2	4	.01	49	.01	2	.19	.01	.13	1	425
K86R-1956	49	109	12	15	.3	1	1	19	3.00	8	5	ND	1	29	1	5	2	7	.01	.059	2	2	.06	562	.01	3	.23	.01	.11	1	160
K86R-1957	26	261	16	9	.7	1	2	19	3.08	14	5	ND	1	23	1	5	2	9	.03	.127	2	1	.02	106	.01	3	.22	.02	.13	1	385
K86R-1958	21	221	10	12	.8	2	1	47	3.65	10	5	ND	1	20	1	10	2	8	.02	.094	2	1	.07	255	.01	3	.29	.02	.11	1	315
K86R-1959	19	295	13	107	.6	1	2	108	3.92	15	5	ND	1	7	1	2	2	17	.13	.186	2	1	.44	59	.01	4	.70	.03	.10	1	150
K86R-1960	16	323	25	141	.5	1	1	114	4.52	31	5	ND	1	13	1	6	2	17	.03	.134	2	1	.46	251	.01	5	.68	.02	.10	1	190
K86R-1961	13	211	19	6	.6	1	1	22	4.68	22	5	ND	1	8	1	7	2	8	.03	.157	2	1	.03	240	.01	4	.24	.02	.12	1	190
K86R-1962	22	182	40	14	1.4	1	1	23	4.71	81	5	ND	1	23	1	38	2	8	.01	.166	2	1	.02	430	.01	4	.20	.02	.13	1	190
K86R-1963	14	153	6	35	.5	1	1	36	3.22	4	5	ND	1	10	1	2	2	13	.07	.146	2	1	.16	252	.01	2	.38	.02	.11	1	110
K86R-1964	20	300	17	12	1.1	1	1	29	3.06	10	5	ND	1	27	1	5	2	10	.03	.127	3	1	.04	529	.01	3	.23	.02	.12	1	195
K86R-1965	8	277	10	200	.2	1	2	257	4.54	10	5	ND	1	35	1	2	2	36	.19	.197	3	1	1.00	686	.01	4	1.28	.03	.12	1	55
K86R-1966	4	389	15	26	.5	1	7	1069	6.69	8	5	ND	2	13	1	2	2	15	.08	.242	8	1	.17	317	.01	5	.41	.02	.12	1	85
K86R-1967	6	395	16	53	.4	1	1	93	4.82	9	5	ND	1	21	1	5	2	15	.07	.179	4	1	.22	209	.01	6	.46	.02	.13	1	125
K86R-1968	3	356	7	70	.5	1	3	228	4.91	8	5	ND	1	14	1	2	2	21	.13	.146	3	1	.46	53	.01	5	.74	.02	.12	1	125
K86R-1969	7	210	59	141	1.0	1	2	252	6.04	322	18	ND	1	236	1	2	2	69	.10	.385	5	1	1.00	67	.01	5	1.29	.03	.12	1	210
K86R-1970	4	149	44	20	2.3	2	1	74	2.01	35	5	ND	1	51	1	11	2	19	.02	.055	2	3	.19	132	.01	2	.35	.01	.12	1	220
K86R-1971	3	150	20	24	.9	2	1	90	2.82	24	6	ND	1	50	1	3	2	27	.01	.064	2	2	.35	276	.01	3	.53	.02	.14	1	350
K86R-1972	6	40	5	100	.1	2	2	322	3.27	9	5	ND	5	10	1	4	2	8	.19	.054	33	1	.44	90	.01	3	1.05	.03	.12	1	38
K86R-1973	9	63	15	109	.1	2	2	235	7.67	55	5	ND	2	26	1	6	2	35	.06	.121	12	1	.47	101	.01	3	.96	.06	.04	1	49
K86R-1974	4	39	11	57	.1	5	4	126	3.66	22	5	ND	1	16	1	2	2	16	.02	.034	6	1	.28	28	.01	2	.60	.03	.09	1	65
K86R-1975	6.	68	21	81	.4	11	4	298	5.49	28	5	ND	1	23	1	3	2	27	.21	.064	7	16	.35	86	.01	5	.79	.03	.10	1	110
K86R-1976	3	85	13	89	.4	14	6	279	7.94	49	5	ND	1	19	1	4	2	27	.21	.088	10	9	.43	28	.01	3	.95	.03	.10	1	85
K86R-1978	1	257	26	294	.2	2	10	4091	4.45	67	5	ND	1	28	1	2	2	15	1.81	.174	5	1	.66	11	.01	5	.50	.05	.12	1	27
K86R-1980	2	955	77	263	.3	2	9	2111	4.38	61	5	ND	1	27	2	2	2	15	1.21	.123	4	1	.49	12	.01	4	.48	.05	.11	1	39
K86R-1981	2	364	90	440	.2	2	8	1858	4.35	66	5	ND	1	24	2	2	2	18	1.16	.180	4	1	.43	12	.01	4	.63	.05	.11	1	33
K86R-1982	2	419	27	574	.2	3	17	4828	6.01	68	5	ND	1	26	2	2	2	19	1.24	.184	8	1	.59	9	.01	5	.63	.05	.11	1	50
K86R-1983	2	141	10	216	.1	2	10	2597	4.26	51	5	ND	1	39	1	3	2	20	1.41	.127	5	2	.78	9	.01	4	.69	.05	.09	1	47
K86R-1984	1	205	20	276	.4	3	10	73	4.54	104	5	ND	1	23	1	9	2	12	.15	.124	4	1	.08	7	.01	5	.37	.03	.10	1	85
K86R-1985	3	31924	17	117	.1	4	4	52	4.28	131	5	ND	1	30	4	19	6	13	.12	.087	3	2	.19	17	.01	4	.50	.02	.10	1	55
K86R-1986	4	19435	8	59	.1	1	2	29	2.53	96	5	ND	1	34	2	13	4	7	.10	.072	2	1	.04	28	.01	2	.27	.02	.10	1	24
K86R-1987	2	16051	9	60	.1	10	3	42	3.24	6891	5	ND	1	12	2	8	2	8	.04	.053	2	1	.12	19	.01	2	.34	.02	.09	1	55
K86R-1988	4	8110	16	21	.6	1	1	13	3.69	118	5	ND	1	27	1	7	2	11	.01	.087	3	1	.03	22	.01	5	.23	.02	.12	1	31
STD C/AU 0.5	20	60	41	141	7.2	71	30	1134	3.97	39	16	7	35	50	19	17	18	70	.48	.108	42	59	.89	185	.09	35	1.73	.09	.14	12	510

R

CASSIAR MINING PROJECT - 7506 FILE # 86-2303

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM
K86R-1989	2	2593	15	11	.6	2	3	24	2.65	102	5	ND	1	14	1
K86R-1990	3	564	11	8	.4	2	4	36	2.44	43	5	ND	1	15	1
K86R-1991	54	889	20	3	2.1	1	4	11	5.67	13	5	ND	1	33	1
K86R-1992	133	1910	22	33	1.1	2	12	12	9.05	4	5	ND	1	31	1
K86R-1993	48	789	8	1	1.2	3	10	17	3.88	5	5	ND	1	92	1
K86R-1994	118	1292	13	13	1.9	2	9	19	4.18	2	5	ND	1	114	1
K86R-1995	50	727	10	1	1.9	3	8	19	6.22	2	5	ND	1	57	1
STD C/AU-0.5	21	61	39	134	7.3	70	29	1105	3.97	41	19	8	35	49	18

SAMPLE#	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-1989	4	2	8	.03	.036	2	1	.02	14	.01	4	.27	.01	.09	1	60
K86R-1990	4	2	10	.02	.025	2	2	.06	21	.01	10	.29	.01	.06	1	22
K86R-1991	2	2	4	.01	.110	2	1	.01	5	.01	7	.17	.02	.13	1	240
K86R-1992	2	2	6	.01	.049	2	1	.01	3	.01	2	.16	.02	.11	1	185
K86R-1993	4	2	7	.01	.081	2	1	.01	7	.01	6	.19	.01	.11	1	230
K86R-1994	2	2	8	.05	.033	2	2	.05	6	.01	7	.26	.02	.13	1	360
K86R-1995	3	2	9	.01	.010	2	1	.01	4	.01	6	.19	.02	.12	1	480
STD C/AU-0.5	15	20	68	.48	.104	38	60	.88	184	.08	37	1.73	.09	.13	12	505

— Assay required for correct result for Ag > 34 PPM
Cu > 10,000 PPM
Sb > 1000 PPM

CASSIAR MINING PROJECT - 7506 FILE # 86-2114

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-1395	20	101	42	43	.6	1	2	326	3.19	25	5	ND	1	6	1	3	4	19	.10	.138	9	2	.20	105	.01	5	.65	.02	.33	1	55
K86R-1396	16	607	18	74	1.7	25	9	432	5.42	48	6	ND	4	61	1	2	2	53	.69	.200	21	21	.83	232	.11	6	.91	.08	.29	1	125
K86R-1397	20	158	21	19	1.5	3	2	68	3.02	25	5	ND	2	7	1	3	3	15	.04	.130	7	3	.07	283	.02	5	.42	.01	.31	1	95
K86R-1398	29	161	24	17	1.7	2	2	57	3.49	43	5	ND	2	8	1	6	3	14	.02	.118	6	3	.08	418	.05	4	.37	.01	.26	2	255
K86R-1399	41	318	16	80	.9	4	5	661	4.27	9	5	ND	2	17	1	2	2	51	.22	.166	9	7	1.21	323	.07	6	1.57	.03	.30	4	125
K86R-1400	33	270	14	60	1.3	3	3	466	4.44	6	5	ND	3	14	1	2	2	40	.12	.157	5	6	.80	370	.10	9	1.07	.03	.29	3	250
K86R-1401	30	127	17	15	1.7	1	1	91	3.62	19	5	ND	2	12	1	2	3	19	.03	.142	8	2	.13	395	.09	7	.47	.02	.30	4	290
K86R-1402	15	216	21	32	1.7	2	2	228	3.93	18	7	ND	2	18	1	2	3	31	.05	.147	9	3	.31	479	.03	5	.68	.02	.31	2	975
K86R-1403	1	220	2	70	.1	2	8	769	2.09	2	5	ND	1	10	1	2	2	30	.22	.088	5	6	.66	432	.09	3	1.13	.03	.18	1	135
K86R-1404	12	246	14	28	2.3	2	5	333	2.09	32	5	2	1	12	1	3	3	19	.08	.100	5	1	.14	411	.02	4	.56	.01	.28	2	1570
K86R-1405	28	290	31	10	1.3	1	3	134	4.08	34	5	ND	2	8	1	2	3	14	.11	.186	8	3	.03	249	.02	5	.37	.02	.25	1	275
K86R-1406	18	222	28	16	1.1	2	2	179	3.17	17	5	ND	2	8	1	2	3	19	.14	.180	6	4	.09	213	.02	4	.42	.02	.27	1	185
K86R-1407	27	225	18	58	1.6	3	3	406	4.06	6	5	ND	2	21	1	2	2	33	.10	.170	6	4	.53	161	.05	4	.90	.03	.30	1	235
K86R-1408	12	204	20	20	1.9	2	2	151	3.51	15	5	ND	2	16	1	3	2	18	.06	.159	5	5	.10	426	.01	4	.43	.02	.30	1	225
K86R-1409	33	303	39	25	2.2	5	3	135	5.48	30	5	ND	2	29	1	2	2	17	.03	.204	4	9	.10	168	.01	3	.39	.02	.26	1	435
K86R-1410	20	222	24	34	1.7	2	3	281	3.35	8	5	ND	2	23	1	6	2	21	.07	.168	6	2	.20	421	.01	2	.50	.02	.30	1	195
K86R-1411	53	214	31	16	3.4	1	2	98	3.84	23	7	ND	2	33	1	2	3	16	.03	.141	6	3	.10	314	.01	5	.40	.02	.27	1	360
K86R-1412	23	162	35	10	2.4	3	1	60	3.33	16	5	ND	2	26	1	7	2	12	.04	.118	7	6	.04	287	.01	4	.31	.03	.24	1	230
K86R-1413	22	122	24	14	1.9	2	1	43	3.64	22	5	ND	2	23	1	2	4	12	.02	.166	5	3	.05	344	.01	4	.31	.03	.24	1	135
K86R-1414	25	128	39	7	2.3	3	1	39	4.47	86	5	ND	2	17	1	47	3	11	.01	.192	5	7	.03	308	.01	3	.25	.02	.23	1	155
K86R-1415	14	135	23	11	1.1	1	1	104	3.86	22	5	ND	2	10	1	16	3	14	.02	.181	3	1	.07	354	.01	2	.37	.02	.25	1	95
K86R-1416	8	84	17	12	.4	1	1	58	3.17	10	5	ND	2	9	1	4	4	13	.02	.185	8	1	.06	363	.01	5	.36	.01	.26	1	30
K86R-1417	13	85	13	9	.7	1	2	119	2.83	23	5	ND	2	8	1	6	2	12	.05	.228	8	2	.07	342	.01	3	.40	.01	.25	1	55
K86R-1418	25	72	16	11	.5	1	1	82	2.53	10	5	ND	1	9	1	7	2	16	.03	.138	6	3	.11	328	.01	4	.42	.01	.27	1	50
K86R-1419	6	133	28	33	1.1	2	2	204	4.18	41	5	ND	2	22	1	37	2	24	.02	.200	11	5	.20	595	.01	6	.50	.02	.23	1	220
K86R-1420	5	117	30	89	1.5	2	2	868	5.44	20	5	ND	2	14	1	2	2	48	.02	.212	11	3	.54	346	.01	8	.92	.02	.26	1	250
K86R-1421	4	185	30	46	4.0	2	1	625	4.81	22	5	2	1	10	1	5	3	27	.02	.180	6	3	.22	355	.01	10	.62	.02	.28	1	990
K86R-1422	16	271	66	36	9.7	3	2	180	6.43	59	6	3	1	14	1	22	3	23	.01	.114	5	4	.04	402	.01	2	.30	.02	.20	2	1630
K86R-1423	5	269	18	53	1.8	3	3	508	4.07	22	5	ND	2	27	1	2	4	33	.13	.177	9	4	.48	598	.01	4	.94	.02	.29	1	330
K86R-1424	1	129	29	20	1.3	2	2	213	3.52	49	5	ND	1	18	1	4	3	20	.05	.199	5	4	.12	505	.01	3	.40	.01	.24	1	350
K86R-1430	1	117	17	110	1.0	13	19	2535	5.53	41	5	ND	1	51	1	2	2	45	1.64	.176	2	13	1.56	72	.01	2	2.05	.05	.20	1	22
K86R-1431	2	79	13	143	1.4	10	13	2704	4.75	15	5	ND	1	31	1	2	2	43	.98	.157	6	14	1.68	182	.01	4	1.95	.05	.19	1	18
K86R-1432	1	119	71	211	1.6	29	26	2466	7.68	38	5	ND	1	27	1	2	2	111	.80	.164	2	73	3.21	23	.13	4	2.91	.05	.13	1	17
K86R-1433	1	141	123	368	1.9	17	11	1944	6.06	32	5	ND	1	18	1	2	3	48	.09	.114	4	29	1.98	30	.01	2	1.70	.03	.18	1	50
K86R-1434	1	78	86	151	.6	8	8	1332	6.10	27	5	ND	1	19	1	2	2	32	.06	.153	2	10	1.01	33	.01	4	1.03	.02	.19	1	95
K86R-1435	2	54	19	334	.4	16	4	2156	6.06	16	5	ND	1	20	1	2	2	66	.06	.112	5	33	2.43	152	.01	5	2.24	.03	.19	1	290
STD C/AU 0.5	20	63	41	144	7.2	76	30	1167	3.98	38	17	7	37	51	19	16	20	72	.48	.108	39	62	.88	191	.09	37	1.73	.10	.13	13	510

R

CASSIAR MINING PROJECT 7504 FILE # 86-2114

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-1436	2	80	22	110	1.1	9	3	1238	5.48	20	7	ND	1	6	1	2	2	49	.04	.172	9	23	1.18	177	.01	6	1.29	.02	.19	1	295
K86R-1437	14	68	12	105	1.4	7	3	1093	4.94	54	5	ND	1	7	1	2	2	39	.06	.095	8	10	.84	288	.01	4	1.25	.02	.20	1	485
K86R-1438	5	122	25	54	.5	5	2	558	7.60	50	6	ND	1	14	1	4	2	40	.04	.177	8	16	.47	460	.01	5	.87	.02	.21	1	175
K86R-1439	2	130	27	130	.7	10	5	1299	7.33	22	6	ND	1	12	1	2	2	60	.05	.147	10	27	1.72	435	.01	8	1.82	.03	.20	1	165
K86R-1440	1	153	23	120	1.5	10	4	1030	7.92	48	11	ND	1	8	1	2	2	55	.04	.154	6	25	.96	250	.01	6	1.39	.02	.19	1	290
K86R-1441	1	207	34	174	1.2	8	6	1221	9.09	56	13	ND	1	5	1	2	2	53	.02	.170	14	27	.91	130	.01	11	1.47	.02	.16	1	215
K86R-1442	21	295	31	73	.9	5	5	634	7.09	29	5	ND	1	3	1	2	2	37	.02	.149	7	13	.53	131	.01	7	.83	.02	.14	1	130
K86R-1443	15	78	20	4	.9	2	2	32	2.97	37	5	ND	1	4	1	7	2	12	.03	.127	4	5	.02	121	.01	3	.26	.01	.18	1	210
K86R-1444	24	122	30	5	2.7	1	1	38	6.01	59	8	ND	1	4	1	8	2	19	.01	.151	8	3	.03	144	.01	5	.26	.01	.23	1	610
K86R-1445	11	201	29	104	.9	3	3	791	6.19	27	7	ND	1	5	1	4	2	30	.01	.131	9	15	.78	92	.01	8	1.14	.02	.14	1	110
K86R-1446	10	56	40	6	2.7	1	1	42	4.69	63	5	ND	1	4	1	9	3	21	.01	.176	5	1	.04	169	.01	6	.36	.02	.27	1	345
K86R-1447	16	160	51	138	1.5	2	3	1397	6.67	40	7	ND	1	6	1	5	2	24	.11	.161	9	3	.75	89	.02	5	1.33	.03	.15	1	315
K86R-1448	9	137	40	32	2.4	2	1	279	6.94	48	6	ND	1	6	1	13	2	37	.02	.151	4	8	.25	127	.02	5	.51	.02	.19	1	315
K86R-1449	12	82	43	34	2.2	2	1	285	4.94	41	6	ND	1	4	1	11	2	30	.01	.132	6	10	.27	99	.01	6	.48	.02	.17	1	265
K86R-1450	4	133	18	288	.9	3	6	2051	3.50	20	5	ND	1	30	2	2	2	25	1.23	.107	5	4	.70	168	.01	5	.99	.04	.19	1	485
K86R-1451	2	272	33	215	1.0	2	4	1271	7.54	39	8	ND	1	26	1	2	2	27	.69	.167	6	9	.48	150	.04	12	.75	.03	.19	1	275
K86R-1452	13	77	27	67	1.4	3	2	408	3.85	37	6	ND	1	6	1	2	2	25	.11	.127	5	5	.50	164	.03	7	.69	.02	.22	1	210
K86R-1453	2	128	19	126	.9	2	4	923	4.17	23	5	ND	1	12	1	6	2	33	.21	.151	8	5	.94	134	.08	5	1.05	.03	.19	1	105
K86R-1454	14	144	31	141	1.7	6	2	994	5.23	26	6	ND	1	10	1	2	2	51	.13	.150	4	24	1.25	186	.13	5	1.26	.03	.18	1	165
K86R-1455	6	167	20	207	1.4	2	2	758	5.47	20	5	ND	1	12	1	2	2	43	.12	.170	7	4	.80	184	.08	6	.91	.03	.18	1	175
K86R-1456	11	56	39	31	1.2	1	1	130	3.57	25	5	ND	1	8	1	6	2	17	.02	.114	5	2	.15	195	.06	7	.36	.01	.20	1	125
K86R-1457	10	86	40	50	1.7	1	1	402	4.66	33	5	ND	1	18	1	2	2	21	.25	.134	4	2	.15	221	.07	5	.39	.02	.21	1	210
K86R-1458	14	55	63	28	1.6	1	2	58	3.94	33	5	ND	1	12	1	6	2	15	.02	.175	5	2	.04	146	.09	6	.27	.02	.20	1	145
K86R-1459	9	41	90	31	1.3	3	1	71	3.31	24	5	ND	1	9	1	3	2	15	.02	.149	6	7	.07	139	.07	6	.29	.01	.21	1	75
K86R-1460	6	49	35	61	.6	1	2	251	3.10	49	5	ND	1	7	1	4	2	20	.04	.093	5	2	.28	157	.03	4	.58	.02	.20	1	215
K86R-1461	1	214	66	142	.2	4	10	1086	3.27	2	5	ND	1	43	1	4	2	19	.16	.130	4	3	.78	1364	.02	3	1.50	.03	.18	1	90
K86R-1462	1	148	13	119	.2	3	8	1457	2.31	10	5	ND	1	34	1	2	2	16	.60	.082	5	2	.52	1109	.01	5	.99	.03	.22	1	85
K86R-1463	1	108	15	33	7.6	1	3	480	2.76	47	5	49	1	15	1	4	2	10	.06	.076	3	2	.18	738	.01	4	.61	.02	.24	1	43000*
K86R-1464	14	131	25	38	.3	3	3	276	4.03	31	5	ND	1	11	1	6	2	20	.07	.146	5	2	.29	122	.02	5	.76	.02	.26	1	120
K86R-1465	16	102	37	23	1.1	2	2	230	3.91	68	5	ND	2	17	1	8	2	28	.06	.116	3	1	.36	334	.04	4	.70	.02	.28	1	610
K86R-1466	24	196	18	87	.7	5	8	981	7.64	30	7	ND	2	26	1	2	2	78	.11	.211	8	9	1.58	746	.11	4	2.01	.04	.17	1	130
K86R-1467	48	240	34	40	1.6	1	3	271	4.28	38	6	ND	1	10	1	56	2	23	.18	.172	4	1	.41	97	.08	5	.60	.02	.25	2	160
K86R-1468	5	83	23	47	.6	2	3	472	4.76	9	5	ND	1	17	1	8	2	31	.21	.169	6	4	.74	131	.11	6	.78	.03	.21	3	110
K86R-1469	18	207	15	25	1.2	6	4	367	4.77	30	6	ND	1	10	1	2	2	28	.15	.150	4	10	.44	129	.08	8	.66	.03	.24	2	245
K86R-1470	2	50	12	147	.4	1	11	1782	7.57	12	9	ND	1	19	1	2	2	129	.40	.136	7	3	2.61	283	.21	3	3.00	.05	.14	2	70
K86R-1471	33	109	12	65	.8	1	4	764	4.73	13	5	ND	2	12	1	5	2	72	.20	.156	2	1	1.52	389	.11	4	1.66	.03	.24	2	140
STD C/AU-0.5	21	61	39	142	7.0	73	29	1140	3.97	43	17	8	36	50	18	16	20	71	.48	.108	38	60	.89	187	.09	37	1.73	.09	.13	14	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-1472	10	82	24	9	.8	2	2	108	3.09	14	5	ND	1	10	1	4	3	16	.08	.130	7	4	.08	270	.07	6	.37	.02	.27	2	95
K86R-1473	16	142	14	9	1.1	1	2	45	3.49	13	5	ND	1	7	1	2	2	13	.02	.137	5	3	.05	367	.05	6	.32	.01	.24	2	135
K86R-1474	26	888	16	41	1.4	3	6	236	18.04	57	5	ND	2	9	1	2	2	66	.01	.191	9	3	.15	317	.10	2	.51	.03	.16	4	440
K86R-1475	36	469	14	46	1.3	3	7	335	6.48	45	5	ND	2	15	1	5	2	37	.06	.162	8	6	.32	451	.15	4	.66	.03	.23	4	270
K86R-1476	43	337	33	48	1.3	3	5	504	5.74	22	5	ND	2	9	1	2	2	37	.15	.190	5	5	.74	372	.12	6	.92	.03	.25	2	175
K86R-1477	14	164	13	55	1.0	2	3	493	4.21	23	5	ND	2	10	1	2	2	35	.11	.133	4	5	.64	347	.10	8	.88	.03	.26	1	210
K86R-1478	1	105	13	51	.5	2	4	797	3.98	13	5	ND	1	17	1	2	2	46	.20	.136	5	9	.91	283	.14	5	1.05	.04	.25	1	105
K86R-1479	13	185	15	48	.9	2	3	345	3.68	4	5	ND	1	10	1	3	2	29	.18	.177	6	3	.56	254	.11	6	.83	.03	.32	1	75
K86R-1480	37	225	35	23	1.8	1	4	197	3.42	10	5	ND	2	14	1	2	2	18	.13	.173	7	3	.11	206	.04	6	.52	.02	.32	2	595
K86R-1481	48	337	12	60	1.7	2	2	507	4.57	10	5	ND	2	13	1	2	2	44	.07	.167	7	3	.77	716	.12	5	.96	.03	.23	1	350
K86R-1482	19	359	17	16	2.0	7	2	103	5.19	16	5	ND	2	12	1	2	2	27	.02	.172	11	12	.13	428	.06	5	.42	.02	.26	5	370
K86R-1483	20	490	21	71	1.5	14	8	672	5.69	14	5	ND	3	48	1	2	2	73	.27	.196	17	16	1.20	546	.12	4	1.28	.06	.27	1	260
K86R-1484	9	177	19	53	1.8	1	4	481	5.00	13	5	ND	2	15	1	2	2	68	.06	.097	9	2	1.06	366	.02	5	1.25	.03	.24	1	670
K86R-1485	2	422	6	117	.1	12	6	791	3.93	5	5	ND	3	35	1	2	2	24	.30	.105	23	13	1.25	376	.10	5	1.71	.07	.19	1	36
K86R-1486	3	305	11	129	.2	2	3	718	4.05	8	5	ND	2	9	1	2	2	7	.08	.061	15	1	.80	375	.02	4	1.63	.03	.21	1	27
K86R-1487	15	428	19	83	.9	4	5	511	5.42	14	5	ND	2	48	1	2	2	29	.07	.115	12	4	.63	774	.03	5	1.24	.03	.21	1	135
K86R-1488	25	240	18	34	2.8	2	2	223	3.93	8	5	2	2	45	1	2	2	26	.06	.159	5	1	.30	632	.08	3	.62	.03	.24	1	2420
K86R-1489	13	201	12	26	.9	1	2	157	4.08	15	5	ND	1	26	1	2	2	24	.04	.131	3	4	.23	599	.08	3	.49	.02	.23	3	215
K86R-1490	11	358	7	60	1.0	2	3	469	4.83	8	5	ND	2	18	1	2	2	37	.09	.187	5	1	.70	411	.10	5	.98	.03	.22	1	195
K86R-1491	17	322	14	49	1.3	3	2	412	4.96	11	5	ND	2	21	1	2	2	31	.07	.190	4	4	.56	445	.10	6	.84	.03	.22	1	270
K86R-1492	13	266	22	50	.8	4	4	391	3.13	6	5	ND	1	21	1	2	2	23	.06	.090	4	5	.38	1201	.05	5	.89	.02	.23	1	695
K86R-1493	23	402	12	82	1.0	6	4	891	5.27	9	5	ND	1	20	1	2	2	43	.12	.170	5	12	1.07	465	.13	3	1.23	.03	.23	1	1270
K86R-1494	19	213	11	29	.9	3	2	224	4.11	10	5	ND	2	24	1	2	2	25	.07	.175	5	6	.29	534	.18	4	.54	.02	.23	2	170
K86R-1495	17	219	19	48	.6	6	3	522	5.67	12	5	ND	1	27	1	2	3	37	.06	.171	8	10	.82	408	.07	4	1.01	.03	.24	1	75
K86R-1496	27	258	32	21	1.0	2	2	153	5.35	13	5	ND	1	27	1	2	2	23	.01	.110	4	5	.26	550	.02	3	.58	.02	.25	1	180
K86R-1744	16	281	8	31	.8	11	10	242	6.68	10	5	ND	1	13	1	4	2	96	.43	.259	4	21	1.06	35	.25	2	1.14	.05	.33	4	110
K86R-1745	49	193	10	23	.8	8	4	220	6.09	9	5	ND	2	29	1	4	2	145	.35	.230	5	28	1.28	75	.29	2	1.24	.05	.24	4	95
K86R-1746	36	154	10	41	.7	7	3	342	6.76	11	5	ND	2	31	1	2	2	171	.44	.304	9	24	1.84	84	.32	2	1.55	.06	.20	4	55
K86R-1747	54	251	8	30	.8	8	11	278	7.40	6	5	ND	1	15	1	2	2	97	.36	.222	7	20	1.15	23	.25	2	1.13	.05	.27	2	95
K86R-1748	38	123	12	40	1.0	4	4	340	7.56	11	5	ND	2	12	1	2	2	111	.22	.251	5	19	1.50	44	.31	2	1.27	.05	.29	3	105
K86R-1749	22	305	8	24	.9	6	10	213	6.30	8	5	ND	1	10	1	2	2	56	.31	.192	7	7	.77	21	.20	3	.84	.04	.30	4	110
K86R-1750	24	111	8	23	.8	7	9	256	5.58	8	5	ND	1	11	1	2	2	71	.30	.187	3	12	.95	24	.24	5	.96	.05	.32	8	85
K86R-1751	25	278	7	9	.6	6	11	91	4.63	5	5	ND	2	8	1	2	2	35	.35	.211	4	2	.34	26	.21	5	.67	.04	.40	11	90
K86R-1752	6	414	2	110	.2	13	12	794	2.54	4	5	ND	1	46	1	2	2	89	1.78	.157	6	11	.88	47	.14	4	1.04	.06	.17	1	8
K86R-1753	8	71	2	20	.2	4	3	223	1.31	4	5	ND	1	29	1	2	2	64	.72	.150	6	8	.33	36	.13	3	.59	.05	.13	2	4
K86R-1754	21	190	7	66	.3	10	5	737	3.70	7	5	ND	2	62	1	2	2	117	1.24	.145	9	51	.83	31	.23	3	.93	.06	.08	10	7
STD C/AU-0.5	20	60	43	140	7.1	73	31	1193	3.99	43	17	8	37	52	20	15	20	73	.48	.111	38	61	.89	183	.09	38	1.73	.10	.14	14	505

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R 1723	1	155	445	893	4.0	15	6	1300	7.07	166	5	ND	1	19	4	5	12	52	.30	.126	9	12	1.16	133	.09	10	2.50	.02	.27	7	16
K86R 1724	1	53	207	603	2.9	15	7	1291	5.97	151	5	ND	1	14	2	4	8	76	.44	.155	10	12	1.31	123	.05	8	2.38	.03	.23	4	6
K86R 1728	5	117	24	76	1.9	5	4	296	6.13	161	5	ND	2	20	1	11	5	38	.05	.150	6	9	.27	378	.01	7	.64	.01	.22	1	225
K86R 1729	8	159	18	68	.8	2	3	758	4.23	34	5	ND	1	39	1	4	2	30	.10	.138	6	4	.49	358	.01	8	.91	.02	.24	1	260
K86R 1730	18	144	25	85	7.7	3	3	479	4.55	69	5	3	2	9	1	8	2	25	.09	.135	6	3	.35	118	.01	10	.69	.02	.23	600	1850
K86R 1731	13	250	25	35	5.7	3	4	469	5.10	95	5	3	1	16	1	7	5	21	.07	.125	5	1	.15	201	.07	6	.50	.01	.22	16	3100
K86R 1732	11	432	21	44	2.2	3	4	486	4.80	64	7	ND	2	10	1	5	3	26	.10	.143	2	3	.25	128	.09	7	.69	.01	.23	3	370
K86R 1734	5	82	22	47	1.0	3	3	687	4.68	75	5	ND	1	13	1	6	2	36	.09	.126	5	10	.47	141	.03	7	.83	.02	.20	2	75
K86R 1735	11	224	12	3	1.0	1	1	18	4.92	65	5	ND	2	48	1	15	2	13	.02	.221	7	1	.02	193	.02	7	.30	.01	.23	3	65
K86R 1736	64	87	62	3	2.3	1	1	15	4.11	54	5	ND	1	24	1	68	3	13	.01	.129	4	2	.02	205	.01	6	.29	.01	.26	5	70
K86R 1737	26	133	53	7	1.7	1	2	20	4.92	60	6	ND	2	37	1	68	3	13	.01	.169	7	3	.02	165	.01	7	.29	.01	.24	1	75
K86R 1738	15	268	27	43	1.3	5	4	319	6.83	100	5	ND	2	13	1	21	2	41	.05	.165	6	5	.34	178	.02	7	.71	.02	.26	2	150
K86R 1739	24	155	19	12	.9	1	2	56	4.74	83	5	ND	2	17	1	62	3	14	.02	.123	9	1	.06	178	.01	7	.34	.01	.20	1	120
K86R 1740	17	132	23	29	.8	2	2	261	4.27	77	5	ND	2	78	1	9	2	28	.13	.192	6	3	.26	243	.01	7	.70	.02	.25	1	90
K86R 1741	7	94	21	48	.5	1	2	425	4.43	57	5	ND	1	33	1	5	3	17	.10	.113	7	1	.40	192	.01	7	.97	.01	.20	1	85
STD C/AU-0.5	21	61	41	140	7.3	73	29	1143	4.00	39	17	8	35	50	19	16	19	71	.48	.108	40	60	.88	187	.08	37	1.73	.08	.13	15	505

R

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-1755	11	367	17	175	1.2	38	13	977	4.31	23	5	ND	2	43	1	2	2	129	1.03	.176	6	83	1.31	79	.22	3	1.36	.09	.25	1	70
K86R-1756	2	88	18	168	1.0	23	6	697	5.53	19	5	ND	1	29	1	2	2	146	.40	.162	7	132	1.37	86	.27	3	1.09	.07	.17	4	70
K86R-1757	1	127	13	248	1.8	5	4	875	5.48	10	5	ND	1	17	1	4	2	82	.15	.127	2	34	1.16	136	.14	2	1.17	.05	.33	2	225
K86R-1758	6	335	13	111	1.8	6	7	438	6.13	15	5	ND	1	24	1	2	2	94	.28	.160	2	23	.84	61	.16	2	.89	.06	.26	3	155
K86R-1759	4	143	7	54	1.3	6	7	469	5.37	12	5	ND	1	33	1	2	2	140	.50	.196	2	19	1.03	83	.20	2	1.14	.06	.29	2	130
K86R-1760	10	144	55	37	2.0	5	5	205	4.60	29	5	ND	2	35	1	2	2	109	.33	.198	2	25	.39	92	.18	3	.61	.05	.30	12	330
K86R-1761	4	123	7	32	.5	8	6	223	4.08	2	5	ND	1	34	1	2	2	91	.41	.145	2	27	.71	74	.16	4	.80	.05	.26	2	80
K86R-1783	23	228	18	114	1.6	4	9	1369	6.57	44	5	ND	2	9	1	2	2	38	.17	.194	4	2	.51	142	.01	3	1.25	.03	.30	1	315
K86R-1784	16	298	54	90	2.4	3	4	832	7.00	59	5	ND	2	14	1	2	2	36	.08	.251	5	2	.32	234	.01	2	.94	.02	.32	2	800
K86R-1785	18	208	70	43	12.8	2	2	224	4.65	62	5	19	3	17	1	2	3	17	.04	.196	3	1	.07	271	.02	3	.40	.02	.27	7	15500
K86R-1786	1	188	22	32	2.0	2	4	287	3.05	43	5	ND	1	31	1	2	2	10	.03	.151	2	2	.10	1705	.01	6	.46	.02	.27	1	350
K86R-1787	1	221	19	62	3.8	3	8	1013	2.82	8	5	ND	1	46	1	5	2	20	.10	.097	4	8	.41	1560	.07	6	.90	.03	.27	5	70
K86R-1788	21	270	16	91	2.9	4	11	2341	8.97	46	5	ND	1	7	1	2	2	53	.24	.188	3	4	.52	61	.02	2	1.67	.04	.32	4	80
K86R-1789	40	293	18	57	16.0	2	6	1036	6.25	30	5	ND	2	9	1	2	2	29	.12	.140	2	6	.25	235	.03	2	.90	.02	.30	2	1910
K86R-1790	1	34	15	8	.7	2	1	72	3.06	24	5	ND	1	6	1	2	3	11	.02	.116	2	2	.06	136	.01	5	.34	.01	.25	1	60
K86R-1791	2	152	32	85	1.4	3	7	581	4.05	41	5	ND	2	8	1	2	3	17	.08	.134	2	1	.15	132	.03	4	.54	.02	.26	6	65
K86R-1792	2	129	30	61	2.1	14	7	318	3.32	27	5	ND	1	24	1	4	2	35	.36	.143	12	16	.52	143	.20	5	.70	.04	.23	1	35
K86R-1793	6	44	39	22	2.4	1	1	32	2.45	26	5	ND	1	12	1	7	2	10	.01	.099	2	2	.03	128	.01	4	.25	.01	.23	1	125
K86R-1794	5	61	29	11	1.8	1	1	77	3.98	75	5	ND	1	8	1	2	2	15	.02	.136	2	1	.06	119	.01	3	.33	.02	.24	7	75
K86R-1795	5	180	27	29	2.7	1	1	239	5.82	36	5	ND	1	23	1	2	2	30	.04	.249	2	2	.16	161	.02	2	.54	.02	.22	1	120
K86R-1796	6	144	10	25	1.0	1	2	162	4.77	55	5	ND	1	16	1	7	2	20	.04	.154	4	4	.08	135	.01	4	.43	.02	.24	1	110
K86R-1797	10	903	158	111	2.1	1	5	689	6.89	70	5	ND	2	14	1	2	2	36	.09	.234	8	1	.31	132	.01	2	.84	.02	.23	1	590
K86R-1798	7	380	154	75	2.5	2	3	283	6.43	64	5	ND	3	12	1	2	2	28	.04	.184	3	4	.16	157	.01	2	.52	.02	.23	1	210
K86R-1799	6	132	48	21	2.4	1	1	133	4.06	47	5	ND	1	14	1	2	2	18	.03	.137	4	1	.12	118	.01	4	.38	.02	.21	1	115
K86R-1800	6	86	21	28	1.0	3	1	247	3.60	67	5	ND	1	16	1	2	2	26	.09	.182	4	4	.25	144	.01	4	.59	.02	.26	1	100
K86R-1801	3	53	15	14	.4	1	1	137	3.02	60	5	ND	1	13	1	2	2	20	.04	.179	4	1	.17	140	.01	5	.48	.01	.25	1	52
K86R-1802	2	298	13	65	.4	4	6	611	6.68	63	5	ND	2	21	1	2	2	51	.09	.352	4	10	.61	207	.07	2	1.03	.03	.26	4	70
K86R-1803	43	425	6	33	.8	1	3	221	5.75	13	5	ND	2	14	1	2	2	33	.04	.258	4	4	.30	256	.01	2	.78	.03	.29	1	120
K86R-1804	22	166	14	81	.7	5	4	991	5.25	14	5	ND	2	8	1	2	2	110	.10	.110	4	4	1.62	323	.04	2	2.06	.04	.28	1	120
K86R-1805	39	82	10	6	2.1	1	1	40	2.64	23	5	ND	1	12	1	2	2	13	.02	.105	3	1	.05	291	.01	4	.37	.02	.35	1	290
K86R-1806	23	219	15	16	.6	1	2	91	4.77	20	5	ND	2	19	1	2	2	21	.02	.174	6	1	.11	400	.01	5	.46	.02	.33	1	130
K86R-1807	164	195	37	6	3.3	5	2	30	2.72	9	5	ND	1	12	1	2	2	9	.03	.106	6	2	.04	300	.01	5	.33	.02	.32	1	400
K86R-1808	92	133	20	7	1.8	2	1	51	3.14	32	5	ND	1	12	1	5	4	9	.01	.061	5	1	.04	441	.01	8	.29	.02	.29	1	450
K86R-1809	36	107	24	11	2.6	2	1	43	3.27	17	5	ND	1	6	1	2	2	10	.01	.082	5	1	.03	284	.01	5	.31	.01	.26	1	125
K86R-1810	75	300	19	12	3.4	2	2	64	5.23	35	5	ND	1	40	1	2	2	11	.01	.147	5	1	.03	390	.01	4	.31	.02	.36	3	315
K86R-1811	36	231	16	10	2.3	2	2	92	3.70	62	5	ND	1	21	1	3	2	13	.06	.174	4	4	.06	436	.01	6	.40	.02	.35	1	280
STD C/AU 0.5	20	63	39	140	7.0	71	31	1195	3.97	36	16	8	38	52	20	16	17	74	.48	.111	39	67	.89	185	.09	38	1.73	.10	.14	13	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-1812	36	160	20	10	7.3	3	2	61	2.69	70	5	ND	2	11	1	4	2	20	.10	.170	6	5	.07	295	.01	3	.60	.02	.51	1	115
K86R-1813	54	183	36	27	1.5	1	2	178	3.09	73	5	ND	3	13	1	4	2	26	.13	.159	8	2	.10	395	.01	4	.70	.03	.56	1	100
K86R-1814	47	213	142	26	1.2	2	2	122	2.77	55	5	ND	2	12	1	2	2	25	.15	.158	6	2	.12	328	.01	4	.76	.02	.54	1	75
K86R-1815	61	201	13	129	1.4	4	4	550	3.89	50	5	ND	2	7	1	7	2	43	.05	.115	8	2	.75	306	.01	6	1.28	.02	.38	1	70
K86R-1816	46	59	21	8	1.2	1	1	41	1.91	43	5	ND	2	6	1	5	2	12	.03	.127	6	1	.05	152	.01	2	.44	.01	.37	1	125
K86R-1817	7	91	14	25	.4	1	1	109	2.27	41	5	ND	2	18	1	5	2	19	.12	.165	5	2	.12	440	.01	3	.62	.02	.43	1	120
K86R-1818	12	163	30	14	1.2	4	4	169	3.76	48	5	ND	3	24	1	3	2	19	.03	.163	7	6	.07	406	.01	3	.53	.03	.43	1	150
K86R-1819	8	209	20	54	.8	2	4	469	4.73	56	5	ND	2	16	1	5	2	21	.11	.164	11	1	.54	390	.01	6	1.23	.02	.37	1	95
K86R-1820	22	189	8	100	.9	4	5	994	5.52	42	5	ND	3	12	1	4	2	35	.12	.146	11	3	1.25	330	.01	6	1.95	.03	.31	1	610
K86R-1821	41	262	5	61	.9	4	6	1231	4.53	18	5	ND	3	10	1	2	2	28	.13	.162	11	4	.83	363	.01	5	1.51	.03	.41	1	39
K86R-1822	16	275	17	97	4.0	2	3	1370	6.59	80	5	ND	3	8	1	76	2	30	.07	.156	8	1	.87	257	.01	6	1.51	.03	.33	1	435
K86R-1823	12	158	85	31	5.0	1	1	2220	2.72	174	5	2	1	15	1	208	3	15	.01	.099	6	4	.05	222	.01	4	.38	.01	.29	1	705
K86R-1824	8	155	200	54	6.5	3	1	49	2.96	304	5	ND	2	5	1	325	2	16	.02	.153	9	6	.03	284	.01	5	.41	.01	.31	1	560
K86R-1825	3	81	83	333	.6	15	9	2285	4.94	12	5	ND	1	13	1	2	2	49	.21	.170	5	18	1.79	156	.01	5	1.79	.03	.29	1	19
K86R-1826	3	92	31	285	.5	25	12	2918	6.44	24	5	ND	1	23	1	2	2	75	.21	.191	5	33	2.87	492	.01	4	2.65	.04	.28	1	15
K86R-1827	3	72	88	269	.5	16	12	2957	4.90	9	5	ND	1	16	1	2	2	59	.19	.130	2	21	2.17	358	.01	4	2.04	.03	.31	1	18
K86R-1829	3	64	66	181	1.0	7	2	1231	6.55	73	5	ND	1	10	1	9	2	59	.02	.121	3	29	.79	141	.01	5	1.22	.03	.23	1	290
K86R-1830	8	83	62	48	.6	2	1	237	7.72	73	5	ND	1	6	1	2	4	44	.01	.167	2	20	.22	127	.01	4	.53	.02	.24	1	180
K86R-1831	6	74	29	35	1.2	5	4	154	5.35	62	5	ND	1	10	1	10	3	28	.02	.148	5	10	.22	111	.01	5	.52	.02	.28	1	250
K86R-1832	5	268	39	132	.6	10	5	768	10.84	74	5	ND	2	14	1	2	2	79	.04	.265	8	42	1.23	485	.01	2	1.56	.03	.27	1	45
K86R-1833	4	210	29	105	.4	11	3	735	8.89	45	5	ND	1	28	1	2	2	74	.03	.178	8	36	1.39	625	.01	4	1.70	.03	.25	1	65
K86R-1834	11	193	28	75	.9	5	3	702	7.85	30	5	ND	2	20	1	2	2	52	.02	.178	5	17	1.00	363	.01	6	1.22	.03	.27	1	235
K86R-1835	3	164	23	127	.8	9	4	1289	8.30	11	5	ND	1	8	1	2	2	80	.04	.170	2	48	1.85	208	.01	2	1.92	.03	.24	1	75
K86R-1836	16	206	30	150	.4	7	3	959	6.21	35	5	ND	3	23	1	5	2	57	.02	.122	12	33	1.53	761	.03	6	1.57	.03	.26	1	80
K86R-1837	27	152	17	81	.4	5	3	733	5.55	16	5	ND	2	19	1	2	2	50	.09	.155	3	17	.99	372	.10	5	1.24	.03	.32	1	48
K86R-1838	30	71	13	17	1.0	2	2	114	2.89	20	5	ND	2	12	1	4	3	20	.05	.140	2	5	.13	372	.05	2	.51	.01	.35	2	110
K86R-1839	28	150	21	36	.8	4	2	211	4.85	10	5	ND	2	39	1	2	2	28	.08	.176	2	10	.27	154	.09	6	.61	.02	.33	3	70
K86R-1840	26	150	65	18	12.4	2	2	133	5.16	24	5	2	2	17	1	29	3	19	.03	.164	2	2	.10	469	.05	5	.40	.02	.30	1	1600
K86R-1841	29	99	16	18	1.1	2	1	139	3.98	15	5	ND	2	12	1	2	2	19	.02	.155	2	3	.13	354	.06	2	.45	.02	.32	1	155
K86R-1842	53	108	20	7	1.7	3	1	91	3.26	5	5	ND	2	31	1	4	2	20	.05	.142	2	5	.07	262	.10	2	.43	.02	.34	3	185
K86R-1843	34	220	45	17	2.4	2	3	116	5.24	26	5	ND	3	24	1	2	3	26	.09	.176	2	4	.14	188	.05	4	.51	.02	.35	2	225
K86R-1844	21	157	20	15	1.7	2	3	289	5.95	20	5	ND	3	22	1	5	2	22	.11	.182	4	2	.19	192	.06	5	.54	.02	.35	2	160
K86R-1845	2	106	10	55	.5	3	3	710	4.24	10	5	ND	1	42	1	2	2	54	.07	.142	5	9	.93	745	.06	3	1.27	.03	.28	2	185
K86R-1846	17	140	23	58	2.5	1	2	362	4.50	16	5	ND	2	18	1	3	3	25	.11	.143	4	4	.23	389	.03	2	.58	.02	.32	5	735
K86R-1847	24	177	32	70	2.1	3	4	317	4.51	21	5	ND	1	7	1	2	2	29	.07	.157	2	6	.31	206	.15	3	.67	.02	.34	2	600
K86R-1848	12	143	9	80	1.0	2	4	1093	5.22	18	5	ND	2	14	1	2	2	52	.16	.163	2	5	.93	409	.17	3	1.27	.03	.29	3	205
STD C/AU 0.5	21	63	44	140	7.2	76	31	1192	3.97	42	18	8	38	52	19	15	21	74	.48	.112	39	65	.89	184	.09	36	1.73	.10	.15	13	510

CASSIAR MINING PROJECT - 7506 FILE # 86-2114

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86R-1849	22	169	19	20	.6	5	2	223	3.76	15	5	ND	2	28	1	2	2	30	.15	.164	2	9	.33	330	.17	3	.55	.03	.23	2	55
K86R-1850	15	149	20	56	.8	7	4	771	5.38	18	5	ND	2	23	1	2	2	61	.20	.183	2	18	1.44	94	.19	2	1.45	.04	.21	1	75
K86R-1851	33	187	16	39	.8	4	2	445	4.22	26	5	ND	2	33	1	2	2	47	.17	.159	3	5	.80	342	.18	3	.91	.03	.21	1	65
K86R-1852	34	278	20	65	1.1	9	5	782	4.18	12	5	ND	2	36	1	2	2	63	.30	.184	7	16	1.54	231	.16	2	1.54	.04	.23	1	110
K86R-1853	19	206	8	35	1.0	6	4	555	3.33	13	6	ND	2	31	1	2	2	38	.29	.181	2	10	.69	282	.15	4	.90	.03	.27	5	100
K86R-1854	11	172	25	40	1.1	3	5	564	5.17	17	5	ND	2	14	1	6	2	35	.14	.180	4	10	.51	114	.12	2	.75	.03	.26	3	115
K86R-1855	16	220	20	36	.6	4	3	367	6.60	27	5	ND	2	21	1	6	2	45	.09	.205	2	8	.56	196	.15	2	.87	.03	.26	4	90
K86R-1856	24	378	15	51	.9	8	6	539	4.83	27	5	ND	2	21	1	2	2	46	.12	.162	2	10	.94	564	.10	2	1.40	.03	.26	1	85
K86R-1857	27	348	24	52	1.0	7	6	608	5.03	17	5	ND	2	37	1	8	2	54	.16	.169	3	10	1.12	248	.09	2	1.55	.03	.25	1	60
K86R-1858	83	318	21	67	1.4	9	5	707	4.57	16	5	ND	2	16	1	4	2	52	.28	.169	5	14	1.33	154	.12	4	1.51	.04	.27	1	110
K86R-1859	13	279	13	75	.8	5	5	859	4.23	15	5	ND	2	12	1	9	2	46	.23	.157	6	10	.91	243	.16	3	1.22	.03	.31	1	75
K86R-1860	23	205	13	52	1.4	8	3	670	3.80	10	5	ND	1	7	1	3	2	44	.20	.121	3	10	1.18	217	.14	3	1.28	.03	.29	1	110
K86R-1861	18	138	14	9	.8	2	1	91	4.21	18	5	ND	2	11	1	2	3	18	.05	.131	2	3	.09	203	.08	4	.35	.03	.27	1	135
K86R-1862	33	203	20	67	1.4	5	2	329	5.90	20	5	ND	1	22	1	8	2	29	.09	.180	3	6	.47	135	.14	2	.68	.03	.34	1	295
K86R-1863	25	345	20	45	1.3	4	3	269	7.66	13	5	ND	2	10	1	2	2	40	.05	.164	3	10	.45	167	.17	2	.71	.03	.28	3	210
K86R-1864	4	161	18	34	.3	4	3	382	4.51	16	5	ND	2	15	1	2	3	27	.09	.144	3	12	.59	372	.11	2	.76	.02	.25	2	115
K86R-1865	14	137	13	12	.7	5	2	101	3.94	22	5	ND	2	21	1	2	2	14	.03	.123	2	10	.12	658	.10	3	.36	.02	.22	1	140
K86R-1866	23	147	18	8	.5	6	2	43	4.35	17	6	ND	2	23	1	2	3	12	.02	.158	2	8	.07	248	.12	3	.31	.02	.23	2	75
K86R-1867	3	97	11	20	.3	7	3	232	3.46	12	5	ND	3	32	1	2	2	20	.11	.136	2	8	.31	117	.14	2	.53	.02	.20	3	37
K86R-1868	4	218	15	18	.3	5	3	181	5.58	26	5	ND	2	24	1	2	2	36	.05	.170	3	4	.29	231	.20	3	.69	.02	.27	2	60
K86R-1869	12	136	23	9	.7	3	3	46	5.28	43	5	ND	3	20	1	5	2	16	.02	.135	5	4	.05	304	.18	3	.34	.02	.20	1	270
K86R-1871	9	180	19	58	.4	6	3	734	5.80	9	5	ND	1	11	1	4	2	52	.07	.144	4	13	1.24	362	.10	2	1.45	.02	.24	1	65
K86R-1872	15	179	7	60	.2	10	3	886	5.75	18	5	ND	1	22	1	2	2	60	.09	.174	5	27	1.52	462	.16	2	1.65	.03	.21	1	55
K86R-1880	10	134	32	87	.3	9	2	502	6.72	28	5	ND	1	29	1	3	2	72	.01	.240	7	58	1.74	543	.01	2	1.62	.03	.15	1	35
K86R-1883	15	379	28	89	.9	6	3	585	2.54	16	5	ND	2	42	1	2	2	61	.32	.153	4	4	.90	416	.22	4	1.39	.04	.24	1	41
K86R-1884	37	530	49	105	1.1	6	3	755	3.83	7	5	ND	2	33	1	8	2	60	.26	.170	3	1	.74	827	.20	2	1.32	.03	.29	1	75
K86R-1885	20	505	31	90	1.0	11	3	643	2.59	6	5	ND	2	29	1	4	2	60	.33	.173	4	11	.89	863	.21	2	1.31	.04	.23	1	65
STD C/AU-0.5	19	62	42	137	7.2	74	31	1172	3.99	43	15	8	38	52	19	16	21	73	.48	.109	38	61	.89	187	.09	37	1.72	.10	.14	12	510

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL & STREAM SED & TALUS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.
-80 mesh

DATE RECEIVED: JULY 28 1986 DATE REPORT MAILED: Aug 1/86 ASSAYER. D. Toye ..DEAN TOYE. CERTIFIED B.C. ASSAYER.

CASSIAR MINING PROJECT - 7506 FILE # 86-1702

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 501	46	1059	59	86	.5	8	11	542	12.04	201	5	ND	1	161	1	11	2	159	.34	.488	15	29	.73	60	.09	3	3.64	.10	.07	1	210
K86S 502	17	709	60	210	1.4	5	20	1921	10.14	149	5	ND	1	45	2	8	2	140	.41	.278	11	13	.52	132	.05	2	2.05	.01	.06	3	140
K86L 503	19	1453	132	274	2.3	3	26	2168	18.22	510	5	ND	2	29	1	9	2	192	.15	.437	18	17	.95	58	.16	4	2.69	.01	.05	1	395
K86L 504	24	1407	185	278	2.2	4	39	2470	17.35	271	5	ND	2	25	1	10	2	142	.18	.393	10	14	.80	78	.17	2	2.40	.02	.06	1	415
K86L 505	23	1263	118	218	3.9	6	28	1779	18.14	272	5	ND	1	36	1	11	2	165	.35	.389	19	13	.96	52	.24	5	2.56	.11	.07	1	420
K86L 506	24	1233	58	167	3.2	1	12	849	27.23	152	5	ND	2	17	1	14	2	154	.17	.592	20	18	.60	51	.10	2	.80	.01	.08	1	175
K86S 507	17	373	52	114	1.5	7	28	1616	6.79	132	5	ND	1	80	1	6	2	102	.38	.215	10	12	.60	108	.11	2	1.60	.11	.10	1	105
K86T 508	29	374	98	78	2.3	1	20	552	11.06	73	5	ND	1	23	1	24	3	56	.03	.392	8	12	.42	333	.04	2	.94	.01	.10	2	190
K86S 509	16	446	39	46	4.2	1	20	378	11.86	50	5	ND	1	14	1	11	3	61	.05	.158	9	10	.13	148	.02	6	.89	.01	.07	1	85
K86S 510	10	364	61	84	1.1	1	19	361	7.13	42	5	ND	1	45	1	14	2	38	.04	.215	18	6	.32	401	.02	5	1.22	.01	.10	1	135
K86S 511	12	117	57	33	2.6	2	7	165	4.88	35	5	ND	1	16	1	5	2	38	.05	.226	13	16	.10	130	.03	5	1.12	.01	.07	3	145
K86S 512	22	165	36	56	1.2	1	9	236	4.49	39	5	ND	1	15	1	9	2	33	.05	.169	11	8	.14	114	.01	5	.73	.01	.09	1	90
K86S 513	7	150	45	77	1.0	6	16	700	4.66	29	5	ND	1	49	1	5	2	62	.43	.120	14	19	.89	126	.15	4	1.77	.20	.12	1	115
K86T 514	11	260	52	74	3.4	5	21	1214	6.77	45	5	ND	1	22	1	6	2	41	.06	.279	10	12	.41	280	.03	3	.89	.01	.09	1	435
K86T 515	8	150	60	79	1.9	8	17	1507	6.32	43	5	ND	1	30	1	5	2	62	.23	.262	9	10	.55	331	.09	2	.96	.07	.12	1	135
K86S 516	4	85	67	121	1.1	5	15	2349	5.24	57	5	ND	1	14	1	6	2	74	.12	.223	7	13	.32	139	.01	2	1.05	.01	.09	1	70
K86S 517	2	127	72	216	.7	11	30	3544	5.61	49	5	ND	1	15	1	4	2	93	.10	.188	8	19	1.19	244	.01	8	2.05	.01	.09	1	210
K86S 518	6	222	193	247	2.3	13	44	6407	8.68	118	5	ND	1	16	1	7	2	47	.14	.268	9	20	1.02	545	.01	3	1.55	.01	.09	1	195
K86S 519	2	188	146	277	2.1	18	37	3885	7.43	98	5	ND	1	40	1	4	2	63	.56	.179	8	23	1.56	402	.14	3	1.86	.13	.10	1	95
K86S 520	4	349	297	479	3.2	26	61	5286	8.69	133	5	ND	1	26	2	5	2	121	.16	.209	6	73	2.53	1012	.09	2	2.56	.01	.06	1	105
K86S 521	5	320	284	304	7.1	21	54	5101	11.94	293	5	2	1	13	2	12	5	32	.27	.139	7	12	1.00	276	.01	2	1.04	.01	.10	1	550
K86S 522	2	80	47	72	.3	4	28	3708	3.82	19	5	ND	1	58	1	5	2	50	1.14	.333	6	13	.52	387	.01	3	1.33	.01	.10	1	21
K86S 523	1	61	49	139	.2	6	23	2474	4.30	25	5	ND	1	38	1	6	2	65	.62	.115	5	12	1.03	440	.03	3	1.69	.02	.12	1	7
K86S 524	1	87	45	171	2.6	10	20	1672	4.72	39	5	ND	1	16	1	4	2	68	.12	.134	4	15	1.19	117	.03	6	2.23	.01	.11	1	31
K86S 525	1	62	22	104	.6	8	19	1919	4.78	17	5	ND	1	17	1	3	2	63	.16	.179	4	14	1.15	191	.01	2	1.99	.01	.11	1	27
K86T 526	60	1160	37	106	2.0	10	27	1603	12.95	342	5	ND	1	44	1	13	2	166	.69	.300	10	19	.87	34	.15	4	2.94	.16	.08	5	425
K86S 527	27	2198	29	81	3.7	3	10	467	12.26	143	5	ND	1	15	1	11	2	143	.24	.220	7	15	.33	14	.03	9	2.73	.01	.03	1	350
K86S 528	45	873	33	108	1.5	1	12	915	11.76	332	5	ND	1	25	1	12	4	139	.17	.212	9	13	.38	57	.04	6	2.36	.01	.04	2	225
K86T 529	55	2016	68	146	1.8	11	38	2070	21.80	582	5	ND	2	25	1	19	2	165	.22	.342	7	25	.64	41	.13	5	2.78	.05	.06	1	615
K86T 530	20	1993	76	314	2.2	11	40	2527	23.15	134	5	ND	2	31	1	10	2	194	.23	.455	9	20	.78	40	.17	3	2.38	.01	.04	1	360
K86T 531	10	1699	47	263	.9	5	45	2735	19.51	54	5	ND	2	33	1	8	2	125	.18	.448	5	15	.82	94	.18	2	1.99	.01	.04	1	440
K86T 532	17	1164	24	135	1.7	1	11	713	23.49	84	5	ND	2	20	1	6	2	143	.13	.458	8	9	.61	49	.15	2	.89	.01	.04	1	75
K86T 533	15	363	76	79	3.6	1	18	400	8.62	57	5	ND	1	78	1	9	3	56	.04	.263	9	16	.87	239	.06	2	.89	.01	.07	1	260
K86T 534	22	293	76	73	2.9	2	15	352	9.42	61	5	ND	3	322	1	11	3	63	.04	.480	32	26	.61	429	.17	3	.79	.01	.13	1	150
K86S 535	32	174	118	50	3.2	1	9	239	6.39	64	5	ND	1	22	1	24	2	24	.03	.287	9	6	.27	284	.01	2	.63	.01	.10	1	265
K86S 536	18	241	83	63	2.7	3	16	429	11.61	60	5	ND	1	32	1	13	5	53	.06	.460	8	16	.53	348	.06	2	.71	.02	.11	1	295
STD C/AU 0.5	21	60	43	135	6.9	68	30	1092	3.94	39	19	7	33	49	18	17	18	63	.48	.109	36	60	.88	179	.08	38	1.72	.06	.14	14	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 537	13	410	82	84	2.1	1	21	820	6.84	46	5	ND	1	12	1	10	5	28	.03	.244	15	13	.39	264	.01	2	2.35	.01	.09	3	350
K86S 538	15	198	63	48	1.3	3	14	518	5.99	38	5	ND	1	12	1	9	3	45	.02	.164	12	17	.30	148	.01	6	1.51	.01	.10	4	225
K86S 539	31	331	108	53	3.9	3	18	1687	7.91	67	5	ND	1	20	1	9	2	35	.04	.259	8	10	.18	362	.01	3	1.30	.01	.13	2	560
K86S 540	27	123	63	36	1.1	1	8	314	4.23	26	5	ND	1	19	1	6	2	32	.04	.168	11	11	.38	153	.01	6	1.15	.02	.09	1	315
K86S 541	8	89	62	55	3.7	5	7	304	4.05	30	5	ND	1	16	1	5	2	42	.06	.128	11	16	.41	156	.02	3	1.51	.01	.10	2	270
K86S 542	8	201	77	100	2.1	4	15	921	4.97	52	5	ND	1	25	1	9	2	49	.08	.221	8	12	.23	229	.01	5	.95	.01	.11	2	190
K86S 543	8	162	97	59	4.0	5	13	518	13.16	96	5	ND	2	20	1	15	2	34	.07	.347	10	11	.34	187	.08	2	.48	.03	.08	1	360
K86S 544	12	256	89	98	3.2	7	26	2242	8.10	69	5	ND	1	15	1	8	2	62	.05	.251	10	10	.47	308	.04	2	1.32	.01	.11	3	305
K86S 545	9	229	61	136	1.4	11	30	3668	6.06	52	5	ND	1	23	1	7	4	61	.11	.224	9	21	.47	300	.01	4	1.54	.01	.09	1	255
K86S 546	18	554	52	116	1.3	12	37	2376	9.02	49	5	ND	1	26	1	6	3	49	.10	.314	14	18	.83	492	.03	3	1.83	.02	.08	2	365
K86L 547	5	308	192	357	2.8	22	49	4686	9.52	91	5	ND	1	12	1	3	2	44	.14	.217	7	25	1.45	119	.04	2	1.63	.01	.09	1	190
K86S 548	3	234	262	467	2.0	24	46	5185	8.74	78	5	ND	1	11	1	4	2	81	.05	.181	10	41	1.96	482	.06	4	2.44	.01	.11	2	145
K86S 1001	28	7895	94	1158	11.1	156	43	60857	12.76	51	7	ND	4	46	7	6	45	10	.63	.098	300	5	.47	1565	.01	2	2.90	.01	.02	1	390
K86S 1002	12	252	242	246	2.5	17	29	3268	8.67	234	5	ND	1	40	1	10	4	75	.22	.201	16	23	.73	147	.12	2	1.71	.11	.11	1	815
K86S 1003	18	502	215	266	4.0	17	41	2724	11.94	229	5	ND	2	51	1	7	4	91	.16	.282	14	29	.84	116	.13	2	1.80	.07	.10	1	625
K86S 1004	15	261	171	45	1.0	3	16	381	21.33	186	5	ND	3	10	1	19	5	65	.01	.473	8	11	.05	273	.06	2	.10	.01	.09	1	245
K86S 1005	31	168	90	24	1.1	3	12	512	15.26	403	5	ND	2	58	1	55	5	16	.01	.431	6	3	.03	111	.01	2	.07	.01	.23	1	215
K86S 1006	14	108	94	23	.6	3	8	118	7.57	188	5	ND	2	23	1	41	2	10	.01	.304	11	6	.03	358	.01	3	.22	.01	.13	1	160
K86T 1007	40	84	39	32	.7	4	7	171	6.82	65	5	ND	1	18	1	7	2	14	.01	.245	5	4	.09	302	.01	2	.30	.01	.13	1	275
K86T 1008	27	119	37	34	.5	4	7	189	3.98	63	5	ND	1	15	1	16	2	18	.02	.098	7	5	.16	163	.01	4	.40	.01	.12	1	85
K86T 1009	38	298	71	111	1.2	8	23	1343	6.27	82	5	ND	1	35	1	14	2	38	.12	.172	14	12	.49	463	.07	2	1.27	.05	.10	2	350
K86S 1010	5	382	378	947	6.7	19	40	5053	22.18	339	5	2	2	5	3	2	13	26	.03	.560	18	6	.07	104	.01	2	.76	.01	.06	1	2960
K86S 1011	7	140	88	189	1.2	12	15	1634	6.72	272	5	ND	1	8	1	9	4	114	.04	.119	9	30	.32	94	.02	2	2.40	.01	.08	1	265
K86T 1012	12	531	95	202	2.5	21	43	2676	17.15	340	5	ND	2	10	2	25	3	135	.34	.292	7	46	.77	49	.08	2	2.39	.01	.07	1	325
K86T 1013	21	741	141	315	3.7	69	89	7728	23.13	390	5	ND	3	8	2	66	2	138	.08	.468	14	67	1.13	73	.20	2	1.85	.01	.07	1	925
K86T 1014	19	777	1540	1115	25.3	70	81	9847	18.09	13269	5	5	1	6	9	84	9	64	.10	.247	14	27	.60	82	.03	2	1.54	.01	.08	1	7130
K86T 1015	7	236	141	420	2.6	36	26	3697	6.03	263	5	ND	1	21	2	8	2	82	.52	.164	7	49	1.03	104	.08	8	1.48	.01	.16	2	865
K86T 1016	7	338	201	542	4.2	42	36	5019	7.51	551	5	ND	1	11	3	16	3	82	.26	.192	11	40	.96	164	.05	2	1.49	.01	.15	1	270
K86T 1017	1	75	59	258	.8	14	12	3222	4.81	290	5	ND	1	15	1	7	2	80	.50	.201	6	23	1.07	206	.02	7	1.59	.01	.20	2	55
K86T 1018	24	161	136	97	1.9	6	13	712	8.22	139	5	ND	1	11	1	31	3	45	.02	.199	4	17	.26	190	.04	5	.58	.01	.10	1	980
K86T 1019	11	60	73	46	.9	2	5	188	3.24	101	5	ND	1	18	1	57	2	13	.01	.086	13	6	.08	456	.01	5	.32	.01	.08	1	210
K86T 1020	9	37	109	40	1.1	4	4	83	2.35	76	5	ND	1	8	1	29	2	6	.01	.058	11	5	.02	571	.01	2	.16	.01	.08	1	140
K86T 1021	73	160	58	53	.9	4	10	293	4.47	63	5	ND	1	21	1	15	2	23	.04	.104	11	11	.17	485	.01	5	.53	.02	.18	2	220
K86T 1022	62	75	62	26	1.3	3	4	47	2.24	61	5	ND	1	48	1	15	2	11	.01	.069	22	6	.03	479	.01	5	.21	.01	.07	3	390
K86T 1023	95	250	99	14	3.1	1	14	63	12.35	163	5	ND	2	22	1	56	2	19	.01	.320	7	2	.03	368	.01	3	.15	.01	.17	1	610
K86S 1024	51	165	114	123	2.0	5	8	195	4.92	76	5	ND	1	40	1	12	2	35	.01	.155	8	8	.35	415	.01	6	.99	.01	.11	1	535
STD C/AU 0.5	20	58	40	133	7.0	66	29	1071	3.93	39	21	7	33	48	17	16	19	62	.48	.104	39	59	.88	177	.08	38	1.72	.07	.13	15	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86T-549	22	252	82	81	3.1	7	11	809	7.84	52	5	ND	2	35	1	16	2	46	.23	.264	4	6	.54	283	.12	3	.95	.14	.13	1	685
K86T-550	21	245	60	76	4.1	11	14	926	6.73	46	5	ND	2	61	1	8	2	63	.58	.183	6	9	1.04	228	.27	7	1.21	.32	.16	1	775
K86T-551	17	292	66	45	1.7	3	5	567	5.87	45	5	ND	2	11	1	12	2	24	.04	.222	2	1	.24	191	.02	13	.53	.03	.13	1	630
K86T-552	14	139	47	12	11.1	1	1	50	4.65	87	5	5	2	13	1	2	3	12	.02	.121	11	1	.06	118	.02	11	.15	.02	.27	1	4250
K86T-593	43	676	50	81	2.3	5	13	1347	11.65	40	5	ND	3	21	1	7	2	59	.03	.329	5	9	.65	488	.12	2	1.56	.04	.12	4	725
K86T-598	27	437	49	73	1.6	6	9	1163	9.18	35	5	ND	1	22	1	6	2	61	.03	.294	2	11	.60	381	.08	2	1.67	.04	.11	1	520
K86T-599	29	921	60	98	1.8	8	12	1241	12.10	38	5	ND	3	46	1	7	2	52	.01	.324	13	16	1.09	304	.08	2	2.24	.04	.10	2	405
K86T-1330	2	176	151	363	2.3	12	25	2280	4.85	54	5	ND	1	21	2	5	2	85	.31	.135	4	11	1.29	412	.04	10	2.56	.03	.13	1	335
K86T-1331	3	147	139	379	1.8	14	32	2918	5.54	69	5	ND	1	25	2	2	2	92	.31	.120	5	13	1.46	269	.11	11	2.62	.09	.14	1	120
K86T-1332	4	194	167	391	2.4	12	29	2604	5.52	72	5	ND	1	19	1	8	2	84	.12	.177	4	14	1.28	247	.07	11	2.46	.03	.13	1	230
K86S-1333	4	144	226	313	2.8	11	33	4782	6.20	91	5	ND	1	14	1	7	2	110	.07	.187	4	14	1.03	152	.05	11	2.58	.03	.17	1	170
K86S-1334	4	158	564	563	3.8	13	29	5843	6.97	149	5	ND	1	16	1	7	2	75	.06	.137	4	16	1.06	203	.04	9	2.51	.03	.12	1	315
K86S-1335	6	189	282	551	1.1	15	27	5408	6.60	113	5	ND	1	15	1	7	2	105	.08	.144	6	21	1.30	255	.03	10	2.79	.03	.14	1	105
K86S-1336	5	103	111	317	.9	11	15	2169	5.93	92	5	ND	1	13	1	8	2	100	.12	.108	4	14	.94	244	.03	12	2.06	.03	.16	1	70
K86S-1337	10	116	222	331	1.5	11	20	3139	7.55	120	5	ND	1	7	1	10	2	124	.05	.125	2	17	1.14	207	.03	7	2.57	.03	.12	1	90
K86S-1338	3	77	80	170	.5	11	16	2326	4.62	66	5	ND	1	8	1	8	2	89	.20	.175	2	15	1.07	211	.01	10	1.89	.03	.13	1	145
K86S-1339	5	93	156	213	3.4	9	26	8009	6.55	117	5	ND	1	10	1	4	2	125	.08	.125	4	13	.68	433	.03	11	2.06	.03	.17	1	100
K86T-1340	6	340	255	364	3.0	24	59	14646	7.34	190	5	ND	1	21	7	7	2	98	.24	.127	15	17	1.33	550	.05	6	2.80	.09	.13	1	410
K86S-1344	8	233	125	1092	3.7	29	49	9438	8.25	270	5	ND	1	41	6	19	2	15	.24	.113	9	1	.09	843	.01	2	.54	.03	.11	1	225
K86S-1345	3	170	228	464	1.3	26	27	4109	6.23	157	5	ND	1	10	1	9	2	113	.16	.093	5	25	1.64	260	.01	13	2.75	.03	.16	1	130
K86S-1346	4	121	62	164	.5	10	38	8170	6.80	86	5	ND	1	26	1	2	2	93	.41	.188	5	11	.87	254	.01	10	2.26	.04	.16	1	70
K86S-1347	3	69	163	287	1.0	12	37	8442	5.69	54	5	ND	1	22	3	3	2	82	.33	.257	4	13	.63	325	.01	13	1.72	.03	.14	1	23
K86S-1348	2	97	34	138	.6	8	26	4659	5.49	68	5	ND	1	12	1	6	2	77	.23	.260	2	7	.65	237	.01	12	1.94	.03	.11	1	7
K86S-1349	1	74	30	117	1.2	9	23	3363	6.02	33	5	ND	1	5	1	3	2	94	.06	.156	2	12	.78	215	.01	11	2.34	.02	.10	1	5
K86S-1350	3	69	65	267	1.6	8	28	5258	5.82	64	5	ND	1	30	2	7	2	98	.47	.189	9	8	.61	370	.01	14	1.67	.03	.19	1	8
K86S-1351	1	51	34	123	.3	9	25	4174	4.79	21	5	ND	1	16	1	2	2	116	.46	.115	5	6	1.21	239	.03	13	1.88	.04	.11	1	9
K86S-1352	3	68	54	144	1.1	8	16	2506	6.53	65	5	ND	1	5	1	4	2	137	.04	.086	5	9	.75	172	.02	10	2.15	.02	.12	1	10
K86T-1353	10	269	1947	906	4.5	16	49	11126	7.17	311	5	ND	2	22	3	11	2	27	.07	.142	7	3	.23	272	.01	9	.77	.02	.11	1	355
K86T-1354	7	153	158	785	6.5	23	81	15973	13.59	206	5	ND	2	196	4	7	2	58	.29	.354	17	16	.44	30	.01	2	1.19	.05	.92	1	265
K86T-1357	7	261	641	1763	8.5	39	42	23307	10.07	818	5	ND	2	35	8	17	2	28	.27	.184	13	6	.53	393	.01	2	.90	.04	.13	1	2350
K86T-1358	3	158	176	371	1.7	19	27	7743	5.65	83	5	ND	1	43	2	2	2	70	.57	.131	15	13	1.68	756	.13	11	2.38	.17	.14	1	240
K86S-1359	8	109	382	409	1.4	12	40	12462	6.41	192	5	ND	1	21	3	3	2	58	.25	.186	4	9	.69	689	.01	11	1.82	.04	.10	1	270
K86S-1360	7	101	240	515	1.3	16	37	13137	6.76	108	5	ND	1	27	4	4	2	77	.34	.222	8	11	1.08	482	.04	10	2.28	.10	.15	1	185
K86T-1361	5	185	717	326	18.5	4	22	5744	6.94	184	5	7	1	24	1	8	9	41	.06	.247	5	6	.34	244	.01	11	1.14	.02	.16	1	4350
K86T-1362	5	177	492	456	2.5	12	43	5973	6.66	121	5	ND	1	13	1	8	2	78	.10	.153	9	14	1.04	310	.03	11	2.58	.04	.14	1	380
K86T-1363	5	138	209	330	1.7	15	29	4232	6.09	79	5	ND	1	49	1	6	2	85	.51	.157	10	14	1.31	187	.20	11	2.25	.26	.15	1	480
STD C/AU-0.5	18	60	38	138	7.3	70	29	1112	3.96	38	15	7	35	49	18	15	17	69	.48	.102	36	57	.88	183	.08	42	1.72	.09	.13	12	495

T

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
-80mesh	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
K86T-635	2	195	99	219	1.3	25	20	1886	4.29	97	5	ND	2	14	1	2	2	44	.26	.141	15	17	1.03	89	.06	9	1.72	.03	.14	1	80
K86T-642	3	200	453	918	4.2	29	32	4929	4.89	262	5	ND	3	15	8	11	3	37	.33	.160	19	12	.73	177	.05	8	1.58	.03	.14	1	49
K86T-654	55	3016	269	243	7.0	10	44	5154	12.49	375	5	4	4	23	2	49	2	37	.05	.301	5	1	.24	176	.01	2	.76	.03	.13	1	4550
K86T-699	29	117	78	22	1.6	1	2	162	4.90	208	5	ND	1	44	1	50	3	15	.01	.171	2	1	.11	284	.01	7	.22	.02	.07	1	510
K86T-700	24	32	55	19	1.3	2	1	88	1.75	285	5	ND	1	37	1	49	2	10	.03	.084	3	3	.13	412	.02	3	.18	.02	.07	1	620
K86T-701	36	99	89	34	1.5	1	1	97	3.33	209	5	ND	1	69	1	35	3	15	.01	.101	2	1	.20	343	.01	5	.31	.02	.05	1	415
K86T-702	27	149	97	53	2.3	2	2	249	5.66	96	15	ND	4	169	1	18	3	27	.03	.135	12	6	.27	282	.06	8	.56	.04	.08	1	345
K86T-708	18	50	176	130	1.4	3	1	323	1.93	35	5	ND	1	1873	1	5	3	39	.08	.292	12	3	.87	940	.01	5	1.27	.02	.09	1	270
K86T-709	9	41	127	36	2.2	2	1	97	1.72	56	5	ND	1	591	1	12	3	18	.03	.154	4	4	.27	599	.01	2	.43	.01	.05	1	345
K86T-726	21	90	145	24	1.1	1	1	28	8.26	46	8	ND	3	47	1	8	3	13	.01	.476	2	1	.02	211	.01	5	.10	.02	.18	1	480
K86T-727	15	74	107	9	.7	3	1	34	13.50	298	11	ND	3	29	1	18	3	24	.01	.389	2	3	.02	270	.01	2	.06	.04	.19	1	370
K86T-728	5	220	209	111	2.9	9	5	543	14.85	362	7	2	3	8	1	16	2	74	.03	.360	2	24	.15	113	.08	2	.32	.04	.08	1	480
K86T-738	6	304	249	412	6.9	38	39	3853	7.02	336	10	ND	2	90	3	35	2	74	.92	.172	12	18	1.31	261	.26	10	1.84	.36	.16	1	215
K86T-739	32	539	242	308	7.4	27	27	3037	7.35	343	8	ND	2	72	2	39	3	43	.37	.213	8	12	.68	373	.06	7	1.05	.10	.16	1	490
K86T-740	116	131	66	23	3.8	2	1	71	3.51	99	6	ND	2	69	1	52	3	12	.02	.131	4	1	.05	234	.01	5	.15	.04	.24	1	485
K86T-741	29	826	102	104	6.7	6	20	1160	18.18	342	28	2	4	273	2	93	2	61	.10	.721	4	5	.40	53	.02	2	.73	.08	.42	1	905
K86T-742	15	1246	201	299	5.4	18	36	2637	8.58	473	8	ND	2	34	2	49	2	55	.26	.214	7	9	.96	192	.03	3	1.36	.06	.12	1	1650
K86T-743	21	166	156	39	3.1	3	3	173	4.99	182	6	ND	2	65	1	41	4	27	.07	.125	2	5	.21	232	.09	7	.31	.06	.17	1	415
K86T-755	35	198	137	60	1.6	1	1	71	2.11	107	5	ND	1	64	1	20	4	14	.05	.096	4	2	.13	220	.01	5	.25	.02	.13	1	254
K86T-760	14	207	59	38	1.9	1	1	40	2.56	502	5	ND	1	40	1	51	3	8	.03	.134	2	1	.09	193	.01	4	.16	.01	.08	1	900
K86T-764	21	133	67	28	2.1	1	1	47	2.37	180	5	ND	1	58	1	41	2	10	.05	.118	2	1	.13	214	.01	4	.23	.02	.11	1	370
K86T-780	70	30	79	9	3.6	1	1	20	2.66	54	5	ND	2	55	1	32	4	9	.01	.295	2	1	.02	187	.02	3	.09	.02	.18	1	415
K86T-781	88	71	108	20	3.4	1	1	14	3.00	38	7	ND	2	66	1	16	3	9	.01	.185	2	1	.03	238	.01	5	.10	.01	.12	1	560
K86T-1897	35	885	215	159	21.9	9	13	1609	10.04	1698	8	2	5	13	1	109	2	56	.03	.234	10	12	.60	133	.07	2	1.46	.04	.08	3	2000
K86T-1904	20	455	74	84	2.2	6	8	1105	7.54	146	5	ND	2	19	1	4	2	43	.02	.245	6	8	.50	401	.03	7	1.33	.04	.14	1	400
K86T-1907	5	208	277	346	3.7	39	38	6363	6.68	217	5	ND	5	16	3	10	4	56	.20	.167	18	19	.82	209	.06	7	2.04	.08	.11	1	120
K86T-1909	4	214	311	427	5.3	34	38	5119	6.34	240	7	ND	4	20	3	11	3	55	.26	.169	20	19	.87	197	.06	6	1.97	.08	.12	1	85
K86T-1912	13	487	146	217	4.2	13	16	2068	8.17	310	6	ND	5	23	1	18	2	44	.08	.194	24	11	.50	257	.08	5	1.69	.07	.12	1	985
K86T-1914	11	560	125	382	6.0	12	22	3376	8.65	323	5	3	5	13	2	66	2	46	.07	.210	22	11	.44	190	.07	2	1.88	.06	.08	1	950
K86T-1916	50	526	145	45	5.5	1	2	147	3.93	206	6	ND	1	68	1	40	5	16	.06	.125	5	1	.10	131	.01	7	.23	.03	.28	1	611
K86T-1917	43	612	182	50	5.0	1	1	134	5.73	258	12	ND	1	84	1	40	3	21	.17	.209	3	2	.16	86	.01	6	.29	.04	.33	1	735
K86T-1977	36	289	209	38	3.0	1	1	67	3.79	219	5	ND	2	55	1	30	2	14	.03	.138	3	1	.07	164	.01	6	.18	.03	.19	1	294
K86T-1979	6	103	129	77	1.3	1	1	131	3.86	142	10	ND	1	71	1	16	2	21	.12	.166	2	1	.29	125	.01	7	.45	.03	.16	1	138
STD C/AU 0.5	20	62	41	142	7.1	74	30	1164	3.95	42	18	7	37	51	19	18	21	72	.48	.108	39	62	.88	191	.09	38	1.73	.09	.15	13	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86T-1364	8	185	265	491	1.5	16	32	6695	6.38	113	5	ND	1	33	1	2	2	77	.34	.145	7	17	1.41	367	.10	6	2.57	.17	.20	1	245
K86T-1365	5	173	101	438	.9	27	35	2284	5.31	84	5	ND	1	23	1	7	2	68	.36	.160	10	27	1.49	568	.02	8	2.82	.05	.24	1	110
K86T-1366	5	129	66	272	1.2	27	19	1520	5.99	71	5	ND	2	28	2	21	2	50	.47	.183	11	18	1.08	167	.03	6	1.45	.05	.06	1	26
K86T-1367	7	113	82	370	1.4	29	18	1560	6.50	98	5	ND	3	26	3	31	2	48	.41	.167	10	14	.87	191	.02	15	1.19	.03	.07	1	80
K86T-1368	6	111	96	326	1.4	28	20	1735	6.45	104	5	ND	2	25	2	22	2	47	.41	.187	12	17	.94	194	.01	14	1.28	.04	.07	1	70
K86T-1369	4	186	175	562	2.8	20	37	6026	6.81	178	5	ND	1	32	4	7	2	56	.54	.156	7	9	1.11	199	.01	6	1.71	.04	.16	1	190
K86T-1370	4	193	132	488	2.6	21	39	6386	7.11	161	5	ND	1	39	3	10	2	64	.64	.162	8	10	1.30	222	.03	4	1.92	.06	.16	1	180
K86T-1371	3	263	130	756	1.7	24	50	5118	6.74	277	5	ND	1	38	6	9	2	72	.93	.167	13	13	1.33	282	.01	5	2.21	.05	.17	1	330
K86T-1372	3	181	69	249	1.1	19	33	4539	6.44	98	5	ND	1	39	1	2	2	105	.66	.160	15	16	1.67	306	.05	16	2.75	.08	.22	1	37
K86T-1373	4	266	63	225	1.1	22	42	4878	6.73	87	5	ND	1	39	2	4	2	106	.65	.166	17	19	1.73	280	.05	12	2.99	.09	.21	1	27
K86T-1374	3	198	74	392	2.8	19	30	3787	6.40	87	5	ND	2	17	2	9	2	116	.28	.162	14	18	1.50	254	.02	6	2.92	.04	.22	1	33
K86T-1375	3	211	101	356	1.5	17	34	4055	6.36	71	5	ND	2	17	2	2	2	116	.30	.130	16	16	1.52	250	.02	5	2.87	.05	.20	1	23
K86T-1376	3	140	69	227	.9	19	32	3674	6.91	60	5	ND	1	37	1	2	2	149	.43	.147	10	34	1.81	142	.13	4	2.92	.16	.18	1	65
K86T-1377	2	194	53	337	1.4	21	30	2296	7.25	54	5	ND	2	40	2	3	2	144	.69	.146	8	20	2.09	130	.23	13	2.78	.08	.15	1	22
K86T-1389	18	639	50	138	2.5	7	20	1482	10.70	109	5	ND	4	29	1	14	2	60	.11	.292	10	9	.77	401	.15	2	1.85	.08	.12	4	450
K86T-1390	33	648	54	87	2.2	6	11	578	15.75	148	5	ND	4	25	1	15	2	63	.08	.466	2	5	.48	238	.18	2	.77	.06	.14	3	360
K86T-1425	38	480	76	52	4.0	4	9	951	10.25	94	5	ND	2	18	1	12	2	37	.03	.392	7	4	.24	496	.03	2	.71	.04	.19	1	675
K86T-1426	32	402	74	50	3.2	5	11	970	9.95	73	5	ND	3	25	1	16	2	43	.13	.366	6	5	.43	384	.08	2	.84	.10	.18	1	490
K86T-1427	29	631	42	62	2.8	6	33	3055	7.59	63	5	ND	2	31	1	7	3	39	.15	.263	6	6	.58	549	.05	3	1.00	.09	.17	1	770
K86T-1428	18	587	42	71	2.4	6	22	2431	6.44	56	5	ND	2	25	1	12	2	41	.20	.220	6	7	.71	312	.06	8	1.13	.09	.16	1	500
K86T-1429	20	348	76	76	2.3	8	14	1214	8.31	87	5	ND	3	61	1	19	2	61	.47	.273	11	8	.82	292	.21	2	1.32	.28	.18	1	500
K86T-1497	47	873	76	62	2.4	3	9	784	11.19	64	5	2	2	27	1	7	2	49	.04	.378	14	4	.37	614	.08	2	1.25	.05	.18	2	815
K86T-1498	49	613	57	65	3.3	3	11	995	10.95	57	5	ND	3	31	1	2	2	39	.07	.413	10	3	.37	481	.09	2	.88	.06	.17	1	720
K86T-1499	38	406	71	62	2.4	3	9	875	8.73	51	5	ND	2	28	1	12	2	33	.06	.339	8	4	.39	424	.05	2	1.00	.06	.19	1	310
K86T-1828	8	918	646	766	1.8	68	112	15707	12.93	89	5	ND	2	11	16	2	2	64	.04	.348	18	28	1.60	245	.04	2	3.57	.05	.06	1	170
K86T-1870	33	811	51	86	2.7	10	11	846	10.62	79	5	ND	2	48	1	14	2	69	.12	.355	21	16	.69	538	.14	2	1.68	.09	.17	1	1350
K86T-1873	28	675	56	94	3.0	9	12	1077	10.00	67	5	ND	3	30	1	7	2	64	.04	.322	18	13	.69	436	.13	2	1.89	.05	.16	2	925
K86T-1874	29	607	56	72	2.8	5	9	808	10.06	59	5	ND	2	29	1	5	2	55	.04	.323	12	7	.53	512	.10	2	1.37	.05	.16	2	1050
K86T-1876	24	441	60	79	2.1	10	11	850	7.48	40	5	ND	3	34	1	11	2	45	.13	.282	11	11	.59	372	.10	3	1.27	.09	.16	1	550
K86T-1877	18	105	39	59	.7	5	5	496	4.56	29	5	ND	1	33	1	5	2	57	.21	.128	11	16	.45	337	.15	8	1.26	.12	.12	1	120
K86T-1878	7	158	28	60	.8	3	8	833	3.98	26	5	ND	1	18	1	5	3	36	.11	.172	4	8	.47	322	.03	8	.94	.03	.13	1	95
K86T-1879	10	121	54	54	1.0	4	3	340	5.18	26	5	ND	1	25	1	7	2	50	.08	.145	15	23	.50	195	.07	9	1.77	.08	.12	1	150
K86T-1881	19	236	57	51	1.5	4	2	283	6.18	41	5	ND	1	32	1	8	2	46	.02	.188	12	24	.50	394	.02	9	1.20	.04	.13	1	305
K86T-1882	17	457	56	55	1.4	6	11	1471	6.43	51	5	ND	2	26	1	7	2	49	.14	.228	12	14	.57	190	.07	8	1.56	.10	.13	1	430
STD C/AU 0.5	20	62	40	140	7.2	72	30	1140	3.96	43	16	7	36	50	18	17	20	70	.48	.105	38	62	.88	187	.09	40	1.72	.09	.14	12	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 1025	27	463	77	103	1.4	2	24	1078	5.19	76	5	ND	1	35	1	8	2	23	.05	.158	13	7	.31	264	.03	2	.99	.01	.07	1	465
K86T 1026	41	385	134	50	2.3	1	18	282	10.98	230	5	ND	2	40	1	26	8	33	.03	.362	5	8	.20	185	.02	2	.44	.01	.22	1	510
K86T 1027	13	484	168	121	1.4	2	31	865	12.53	128	5	ND	2	11	1	4	6	32	.01	.301	2	6	.45	141	.01	2	.86	.01	.05	1	305
K86T 1028	40	148	64	31	1.2	1	11	128	11.27	205	5	ND	1	14	1	32	7	26	.01	.219	2	2	.15	121	.02	2	.20	.01	.09	2	180
K86S 1029	7	488	157	692	1.5	18	46	4742	7.86	249	5	ND	1	20	1	5	2	104	.16	.156	12	27	1.28	98	.04	3	2.83	.02	.07	1	410
K86S 1030	43	815	1324	342	27.0	27	39	4623	12.46	1403	5	13	1	9	1	26	9	113	.10	.188	2	41	.95	59	.06	2	1.68	.01	.06	1	3150
K86T 1031	99	1020	140	249	3.4	20	50	3807	18.15	216	5	ND	2	5	1	13	4	138	.04	.425	2	15	1.19	43	.10	2	1.83	.01	.05	2	360
K86T 1032	58	507	100	208	2.7	24	28	2789	10.40	110	5	ND	1	13	1	7	2	117	.21	.323	2	34	1.33	43	.09	2	1.79	.02	.07	3	225
K86T 1033	23	390	73	224	1.5	15	32	2877	5.94	74	5	ND	1	16	1	2	2	125	.29	.204	3	38	1.68	60	.07	2	1.88	.01	.07	1	105
K86T 1034	13	489	188	416	4.0	39	75	23275	9.98	831	5	ND	1	20	2	16	4	61	.18	.249	15	12	.61	1084	.02	4	2.00	.04	.11	1	590
K86T 1035	6	169	114	216	1.9	13	39	8544	7.33	324	5	ND	1	9	1	6	5	61	.14	.250	19	18	.53	261	.02	2	2.45	.03	.09	2	460
K86S 1036 A	5	86	103	164	.8	6	13	3107	7.96	235	5	ND	1	5	1	3	4	67	.06	.165	6	16	.29	106	.01	2	1.72	.02	.06	1	115
K86S 1036 B	11	474	107	96	6.8	2	26	502	21.67	165	5	ND	2	6	1	10	15	67	.02	.178	2	13	.07	47	.04	2	.49	.01	.04	1	365
K86T 1037	34	120	113	43	2.0	1	7	147	4.56	77	5	ND	1	314	1	27	2	26	.09	.199	5	4	.29	467	.04	2	.55	.04	.10	1	370
K86T 1038	39	130	82	23	2.2	1	7	89	4.28	57	5	ND	1	146	1	22	2	15	.01	.164	7	1	.06	455	.01	2	.31	.01	.10	1	495
K86T 1039	50	153	75	19	1.8	1	6	42	3.23	50	5	ND	1	95	1	5	2	12	.01	.092	8	1	.03	429	.01	4	.26	.01	.09	1	485
K86T 1040	55	157	159	25	4.2	1	7	48	3.03	163	5	ND	1	26	1	43	2	12	.01	.074	7	2	.07	342	.01	2	.37	.01	.10	1	495
K86T 1041	42	145	105	24	.9	1	9	107	7.53	157	5	ND	1	10	1	7	2	25	.01	.202	3	6	.03	156	.01	4	.17	.01	.05	1	615
K86T 1042	37	88	1387	23	7.7	1	6	57	6.01	254	5	ND	1	54	1	10	2	20	.01	.364	2	2	.03	188	.01	3	.14	.01	.23	1	625
K86T 1043	16	3256	436	341	1.0	10	66	6919	14.15	310	5	ND	2	256	2	8	3	59	.08	.590	3	6	.60	414	.01	2	3.22	.01	.07	1	2650
K86T 1044	28	273	104	44	1.6	1	15	270	8.96	86	5	ND	4	26	1	12	3	31	.01	.257	5	6	.12	429	.04	2	.47	.01	.12	2	415
K86T 1045	42	420	134	53	3.0	1	20	301	11.29	199	5	7	5	62	1	6	7	33	.02	.355	8	5	.18	302	.06	2	.52	.01	.11	2	3750
K86T 1046 A	24	485	88	139	1.0	10	32	810	7.63	113	5	ND	2	19	1	2	4	37	.13	.220	8	10	.48	171	.07	5	1.76	.06	.10	1	210
K86T 1046 B	16	267	181	22	6.6	1	12	114	6.82	262	5	ND	2	29	1	112	5	21	.03	.283	3	2	.10	120	.01	2	.29	.01	.11	1	665
K86T 1047	27	354	85	60	1.4	3	18	401	9.86	164	5	ND	1	21	1	9	5	34	.01	.297	2	6	.24	269	.02	3	.63	.01	.10	1	370
K86T 1048	18	476	71	88	1.3	6	25	780	7.56	134	5	ND	1	17	1	7	4	37	.02	.235	6	10	.53	305	.03	4	1.31	.02	.10	1	360
K86T 1049	73	884	136	115	13.1	6	21	1784	8.86	986	5	2	3	20	1	187	4	58	.12	.215	5	10	.84	148	.05	6	1.62	.02	.11	5	1390
K86T 1050	11	443	161	140	6.3	8	32	1650	6.68	211	5	ND	1	8	1	28	2	52	.21	.191	4	10	.83	101	.05	2	1.46	.02	.13	4	590
K86T 1051	11	777	144	190	4.1	12	27	2687	8.07	642	5	ND	3	11	1	41	4	42	.10	.210	14	11	.63	117	.06	2	1.95	.02	.09	2	1890
K86T 1052	26	825	1241	345	77.3	8	37	3899	10.18	768	5	ND	1	135	1	396	5	64	.05	.264	3	20	.53	247	.07	5	1.41	.01	.10	2	1210
K86T 1053	19	197	158	76	2.0	4	10	244	6.23	75	5	ND	1	22	1	11	4	42	.01	.120	7	28	.42	178	.02	4	1.24	.01	.07	3	565
K86T 1054	60	269	197	45	3.0	5	13	466	4.33	117	5	ND	1	55	1	38	2	22	.04	.073	9	8	.17	221	.03	3	.59	.02	.07	4	445
K86T 1055	56	91	131	18	2.7	1	5	49	2.89	46	5	ND	1	49	1	14	2	21	.01	.078	7	9	.11	537	.01	2	.48	.01	.12	1	495
K86T 1056	21	231	95	42	2.2	1	13	147	7.86	166	5	ND	1	18	1	11	4	26	.02	.253	2	4	.18	341	.01	2	.40	.02	.09	2	475
K86T 1057	11	356	69	44	3.0	2	15	312	3.00	121	5	ND	1	67	1	17	2	13	.02	.064	10	3	.11	175	.01	3	.48	.01	.06	1	965
K86T 1058	22	236	64	56	2.4	2	11	133	4.76	71	5	ND	1	19	1	12	2	19	.01	.126	13	6	.21	330	.01	5	.88	.02	.09	1	335
STD C/AU 0.5	20	56	40	131	6.8	65	28	1046	3.92	38	20	7	32	46	16	16	19	61	.48	.103	38	58	.88	171	.08	38	1.72	.06	.13	15	495

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86T 1059	44	247	126	52	1.3	2	14	244	7.82	110	5	ND	2	22	1	11	2	33	.03	.262	8	5	.15	279	.04	4	.47	.01	.09	1	295
K86T 1060	22	230	61	29	.9	1	11	106	7.15	138	5	ND	2	17	1	5	2	17	.02	.245	7	3	.07	153	.01	2	.27	.01	.13	2	375
K86T 1061	36	760	120	82	1.7	1	8	409	14.82	222	5	ND	3	36	1	8	7	41	.03	.431	4	5	.14	246	.02	4	.45	.01	.15	1	505
K86T 1062	51	599	166	60	2.8	2	8	289	16.24	239	5	2	4	44	1	11	6	41	.02	.503	10	3	.09	384	.05	3	.37	.01	.17	1	2130
K86T 1063	38	445	221	65	6.5	3	21	225	17.26	1140	5	ND	2	28	1	8	7	50	.03	.743	4	2	.10	55	.01	3	.29	.01	.63	1	955
K86T 1064	36	1211	183	84	7.6	5	11	281	25.67	521	5	2	4	24	1	12	7	70	.01	.562	2	4	.10	121	.01	4	.52	.01	.34	2	2320
K86T 1065	11	301	22	72	1.2	3	12	272	6.70	37	5	ND	9	3	1	2	2	8	.04	.094	34	5	.06	54	.09	5	3.33	.07	.08	2	480
K86T 1066	34	415	77	73	2.0	5	21	651	9.23	122	5	ND	3	26	1	7	2	36	.01	.324	12	6	.32	581	.02	4	.98	.02	.17	1	380
K86S 1067	38	387	60	64	1.5	4	18	448	8.18	90	5	ND	1	23	1	6	2	39	.02	.259	6	5	.18	444	.01	4	.90	.01	.17	1	240
K86T 1068	27	427	53	91	2.9	2	23	1045	7.77	72	5	ND	6	21	1	8	2	30	.08	.212	19	7	.34	373	.07	2	1.80	.09	.15	1	350
K86T 1069	17	690	52	98	1.9	8	9	870	7.63	66	5	ND	4	14	1	11	2	34	.03	.213	23	14	.45	351	.08	2	1.99	.05	.12	1	450
K86T 1070	19	500	42	104	2.9	5	26	976	7.34	68	7	2	7	13	1	11	4	28	.03	.208	24	10	.40	383	.09	2	2.14	.06	.13	1	350
K86T 1071	18	624	83	94	2.6	6	10	879	8.01	86	5	ND	4	22	1	12	2	40	.02	.255	19	14	.61	373	.07	2	1.65	.03	.13	2	440
K86T 1072	16	494	208	199	4.9	3	38	2014	13.03	981	5	ND	3	14	1	59	4	55	.05	.321	9	5	.55	307	.05	2	1.04	.02	.11	3	530
K86T 1073	25	804	119	181	9.6	30	40	2953	11.63	1720	5	ND	3	13	1	69	7	87	.09	.346	7	22	.73	147	.13	2	1.60	.03	.09	6	1180
K86T 1074	17	1294	455	342	19.4	23	35	4167	9.77	298	5	ND	2	18	2	52	2	55	.13	.230	16	13	.74	211	.06	3	1.91	.01	.08	1	2830
K86T 1075	16	750	402	295	7.4	24	37	3906	9.90	663	5	2	2	12	1	28	4	65	.08	.234	12	16	.86	167	.08	2	2.03	.02	.09	1	3330
K86S 1076	19	226	82	197	2.0	7	22	2369	6.84	132	5	ND	4	7	1	11	2	48	.05	.137	28	10	.26	60	.12	3	3.10	.07	.08	1	325
K86T 1077	409	4776	293	3271	12.1	136	212	26172	13.82	261	5	ND	1	24	21	12	2	87	.43	.182	61	14	1.24	269	.04	2	3.01	.02	.06	1	890
K86T 1078	57	1110	151	755	3.7	33	89	11525	11.91	221	5	ND	1	17	4	14	7	86	.31	.210	14	17	.99	148	.03	9	2.51	.01	.07	1	470
K86T 1079	45	648	129	543	2.0	24	112	12236	13.23	210	5	ND	1	13	2	12	7	109	.17	.328	6	19	1.23	104	.03	2	2.46	.01	.08	1	685
K86T 1080	41	779	160	498	2.7	25	97	10400	13.82	233	5	ND	1	15	1	13	5	111	.12	.358	10	23	1.23	89	.08	3	2.69	.02	.09	1	990
K86T 1081	30	601	129	509	3.0	21	58	8001	11.75	193	5	ND	1	15	2	10	4	105	.16	.237	7	21	.85	108	.03	5	2.37	.01	.07	1	630
K86S 1082	8	311	289	388	3.2	15	47	8911	8.56	387	5	ND	1	34	1	9	3	112	.33	.206	8	19	.97	154	.06	5	2.20	.11	.11	1	265
K86T 1083	8	355	317	406	3.7	19	48	8791	9.22	453	5	ND	1	46	1	11	2	108	.43	.192	10	18	1.17	149	.14	2	2.51	.19	.13	1	475
K86T 1084	26	719	531	341	9.0	15	41	3369	11.58	685	5	ND	2	103	1	29	2	95	.10	.293	9	30	.87	366	.15	2	1.59	.04	.16	1	895
K86T 1085	24	784	759	339	6.5	15	45	4327	12.55	502	5	ND	3	57	1	21	3	120	.04	.304	9	32	1.12	374	.13	7	2.20	.02	.14	1	795
K86T 1086	25	842	669	395	6.0	17	45	4486	11.58	434	5	ND	3	53	1	21	2	110	.08	.266	14	34	1.08	297	.14	2	2.27	.03	.13	1	690
K86T 1087	18	794	480	379	7.8	21	45	4674	11.32	529	5	ND	2	40	1	17	3	120	.16	.294	9	34	1.37	199	.14	2	2.22	.06	.12	1	550
K86T 1088	21	795	491	389	4.2	17	42	4782	12.04	376	5	ND	2	30	1	14	5	118	.05	.316	16	37	1.27	128	.12	9	2.53	.02	.09	2	640
K86T 1089	22	873	515	453	5.3	25	50	4801	12.40	367	5	ND	3	52	1	17	4	120	.17	.322	12	35	1.30	212	.18	2	2.40	.08	.13	2	615
K86T 1090	23	680	231	459	3.9	22	84	9404	12.10	199	5	ND	1	16	1	9	2	146	.13	.338	14	27	1.41	93	.08	2	2.83	.04	.08	1	615
K86T 1091	10	227	154	317	1.6	14	39	6274	7.28	185	5	ND	1	29	1	6	2	128	.27	.265	5	24	.68	142	.05	3	2.04	.05	.09	1	140
K86T 1092	41	168	279	106	2.9	3	15	802	5.09	141	5	ND	2	60	1	25	3	45	.14	.124	10	13	.46	211	.12	5	.86	.06	.09	1	430
K86T 1093	19	983	6353	793	21.0	11	49	8175	13.00	1202	5	5	1	47	3	25	5	100	.03	.321	6	21	.88	200	.08	2	1.72	.01	.13	1	2120
K86T 1094	16	2174	3832	2297	12.6	40	118	21937	18.48	952	5	ND	2	49	20	26	12	106	.03	.336	11	26	1.24	183	.11	2	2.79	.01	.09	1	2320
STD C/AU 0.5	21	60	38	137	7.1	66	31	1184	3.93	38	17	7	33	48	17	16	18	63	.48	.107	38	59	.88	179	.08	37	1.73	.07	.13	15	495

CASSIAR MINING PROJECT - 7506 FILE # 86-1702

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86T 1095	22	943	2366	906	9.9	28	66	8491	13.25	736	5	ND	2	43	5	23	2	115	.07	.304	25	35	1.23	196	.13	2	2.44	.03	.12	1	995
K86T 1096	17	991	1046	721	5.0	35	48	5824	11.76	462	5	ND	1	27	4	14	4	132	.24	.228	16	42	1.69	118	.17	2	2.49	.05	.10	1	645
K86T 1097	12	650	257	281	3.5	17	38	4513	8.51	263	5	ND	1	40	2	10	2	116	.19	.238	17	31	.92	78	.09	2	2.68	.06	.08	1	350
K86T 1098	12	252	133	166	2.1	6	17	1627	6.93	172	5	ND	1	21	1	7	2	67	.06	.215	15	20	.29	72	.03	2	1.93	.02	.07	1	130
K86T 1099	9	205	159	182	1.1	7	27	5385	7.55	253	5	ND	1	17	2	5	2	110	.06	.195	15	16	.41	86	.05	2	2.07	.02	.09	1	150
K86T 1100	9	111	125	274	.9	8	29	8422	5.13	123	5	ND	1	38	2	5	2	104	.51	.218	10	19	.28	343	.02	3	.88	.03	.09	1	55
K86T 1101	57	178	239	61	2.5	6	10	331	4.27	97	5	ND	1	71	1	20	3	32	.11	.119	11	8	.30	239	.07	4	.76	.04	.09	2	415
K86S 1102	29	124	150	31	2.9	1	6	93	1.77	43	5	ND	1	58	1	10	4	17	.02	.069	12	9	.12	124	.01	2	.66	.01	.05	1	490
K86S 1103	32	110	64	31	2.3	1	6	135	4.52	43	5	ND	1	19	1	16	2	15	.02	.067	8	9	.10	200	.01	2	1.33	.01	.06	1	780
K86S 1104	30	83	123	30	1.7	2	6	111	5.30	96	5	ND	1	20	1	13	2	20	.01	.198	12	8	.05	355	.01	4	.28	.01	.12	2	325
K86T 1105	19	99	129	40	1.5	2	8	169	4.89	79	5	ND	1	21	1	7	2	24	.04	.184	10	4	.15	274	.03	2	.36	.02	.10	2	275
K86T 1106	10	144	92	49	1.1	1	9	259	5.40	85	5	ND	1	18	1	8	3	28	.01	.217	10	3	.16	273	.01	2	.45	.01	.09	1	250
K86T 1107	12	94	79	24	1.2	1	6	70	4.87	92	5	ND	1	18	1	7	2	19	.01	.241	6	3	.06	287	.01	2	.27	.01	.11	1	140
K86T 1108	16	75	69	29	1.3	2	7	132	4.95	67	5	ND	2	25	1	9	2	25	.08	.212	7	3	.21	326	.06	4	.35	.04	.13	1	115
K86T 1109	18	253	67	57	1.5	3	14	271	8.86	77	5	ND	2	27	1	7	2	50	.02	.405	9	5	.20	333	.07	2	.81	.01	.13	2	250
K86T 1110	35	322	86	69	1.6	3	18	429	11.99	77	5	ND	4	25	1	9	2	57	.02	.378	10	5	.22	415	.14	5	.66	.01	.14	3	295
K86T 1111	38	494	97	85	1.3	5	27	665	15.25	82	5	ND	3	28	1	6	2	53	.02	.402	9	6	.24	234	.12	2	.57	.01	.13	4	325
K86T 1112	63	318	83	43	1.5	1	17	222	13.24	185	5	ND	3	28	1	6	2	38	.01	.451	7	4	.10	346	.05	7	.40	.01	.15	4	350
K86T 1113	45	479	74	61	1.1	3	22	377	9.07	76	5	ND	1	21	1	4	4	35	.02	.305	12	8	.28	347	.02	5	1.21	.02	.13	1	255
K86T 1114	49	495	88	58	2.5	3	24	638	9.79	81	5	ND	2	47	1	20	4	34	.01	.390	7	6	.21	528	.02	2	.68	.02	.20	1	715
K86T 1115	36	416	73	63	3.0	4	23	1280	9.81	76	5	ND	2	79	1	9	2	30	.03	.412	4	5	.13	443	.02	2	.42	.02	.23	1	610
K86T 1116	26	497	101	49	3.5	1	8	633	9.26	114	5	ND	2	25	1	50	2	35	.01	.295	5	12	.27	500	.02	2	.63	.01	.14	2	595
K86T 1117	40	806	46	38	2.2	4	25	1896	15.09	129	5	ND	3	13	1	9	5	28	.01	.486	2	5	.12	250	.01	2	.41	.01	.12	1	545
K86T 1118	68	646	67	47	7.9	2	32	2175	12.50	94	5	ND	3	25	1	13	3	40	.01	.423	4	7	.26	460	.06	2	.65	.01	.17	2	615
K86T 1119	22	519	63	46	.6	4	6	354	6.54	45	5	ND	1	12	1	6	2	33	.04	.163	12	11	.25	344	.04	3	1.67	.02	.09	2	295
K86T 1120	57	218	149	21	5.0	2	13	200	7.61	76	5	ND	3	29	1	20	2	21	.01	.272	5	3	.05	454	.03	2	.27	.01	.15	2	665
K86T 1121	23	326	52	57	3.0	9	20	379	9.35	75	5	ND	1	38	1	9	2	45	.03	.261	2	13	.33	654	.07	2	1.01	.01	.18	1	295
K86S 1122	17	152	59	34	1.5	6	9	96	7.52	70	5	ND	1	8	1	7	2	41	.02	.118	8	21	.10	105	.02	2	1.48	.02	.06	4	465
K86T 1123	23	387	167	82	3.2	7	19	538	7.62	94	5	2	1	15	1	12	2	48	.10	.151	2	18	.33	152	.03	2	1.21	.01	.09	1	990
K86T 1124	51	348	79	53	4.9	4	20	364	13.24	198	5	ND	1	33	1	59	2	32	.05	.502	2	4	.19	132	.04	2	.40	.01	.10	1	345
K86S 1125	20	86	168	29	2.6	2	4	107	1.48	39	5	ND	1	87	1	8	3	15	.02	.078	12	6	.13	147	.01	2	.51	.01	.06	3	495
K86S 1126	56	64	105	35	1.9	2	5	506	3.17	62	5	ND	1	46	1	16	2	19	.03	.078	6	7	.10	79	.01	2	.62	.01	.05	3	325
K86S 1127	31	72	82	49	2.8	1	5	262	4.20	45	5	2	1	12	1	11	2	12	.03	.055	6	8	.08	110	.03	2	1.12	.02	.06	5	475
K86S 1128	43	70	107	33	3.3	1	5	249	4.40	74	5	ND	1	12	1	8	2	30	.02	.090	6	6	.06	213	.01	2	.67	.01	.07	2	315
K86S 1129	36	151	87	47	2.4	2	9	378	5.34	66	5	ND	1	24	1	11	2	25	.03	.149	6	8	.12	214	.02	3	.78	.01	.08	2	225
K86T 1130	6	143	108	60	1.8	4	12	425	6.58	76	5	ND	1	77	1	9	2	45	.29	.300	6	6	.48	251	.15	3	.76	.14	.13	1	195
STD C/AU 0.5	21	60	39	135	7.0	69	30	1096	3.94	40	20	7	34	48	18	15	18	64	.48	.107	36	60	.88	179	.08	37	1.72	.07	.13	14	505

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86T 1131	6	88	146	33	2.4	1	6	139	4.31	59	5	ND	1	29	1	8	2	27	.09	.227	10	5	.22	388	.06	2	.47	.03	.09	1	185
K86T 1132	10	107	135	42	3.0	1	8	164	7.26	90	5	ND	2	351	1	12	2	28	.07	.381	14	4	.25	631	.05	2	.44	.02	.13	1	465
K86T 1133	10	164	205	52	2.5	1	11	179	9.38	72	5	ND	2	28	1	13	2	30	.03	.388	10	3	.23	281	.05	2	.30	.01	.12	1	890
K86T 1134	19	342	62	57	1.0	1	18	346	11.64	58	5	ND	2	23	1	8	2	45	.04	.325	15	5	.29	261	.09	5	.71	.02	.10	1	240
K86T 1135	20	226	95	48	1.2	1	13	324	8.24	53	5	ND	3	20	1	12	2	28	.02	.269	15	3	.21	278	.05	4	.65	.02	.10	1	330
K86T 1136	20	342	113	44	2.0	1	17	236	13.94	61	5	ND	3	25	1	12	5	42	.02	.481	14	6	.19	307	.07	2	.45	.01	.10	1	275
K86T 1137	30	179	87	35	1.4	2	11	161	8.37	43	5	ND	2	27	1	9	2	32	.03	.296	12	5	.22	373	.07	2	.40	.02	.13	2	255
K86T 1138	37	272	65	43	1.1	2	13	222	7.90	48	5	ND	1	34	1	5	2	35	.02	.277	17	8	.25	590	.02	2	1.08	.03	.14	1	235
K86T 1139	19	423	86	69	.8	2	22	624	9.45	61	5	ND	2	41	1	8	3	40	.07	.283	18	11	.58	418	.04	2	1.40	.05	.12	1	280
K86T 1140	15	384	72	54	2.5	4	18	395	5.98	44	5	ND	1	23	1	5	2	43	.14	.194	17	13	.50	225	.08	4	1.65	.07	.10	1	325
K86T 1141	28	362	178	69	5.6	4	21	918	8.06	61	5	2	2	36	1	14	3	40	.15	.284	13	8	.43	526	.09	2	.86	.08	.18	1	1060
K86T 1142	23	361	102	68	3.6	8	24	936	8.47	52	5	ND	2	37	1	12	2	45	.23	.299	12	11	.62	377	.16	5	.88	.11	.15	1	580
K86T 1143	43	597	99	52	3.9	4	8	577	10.81	52	5	ND	1	26	1	6	3	33	.05	.457	13	4	.32	598	.03	3	.95	.02	.14	1	670
K86T 1144	41	694	97	59	2.2	2	17	1152	13.41	79	5	ND	3	17	1	8	6	44	.02	.411	11	5	.31	354	.11	2	.68	.01	.12	2	765
K86T 1145	30	812	59	106	2.7	7	16	951	13.51	102	5	ND	3	35	1	15	2	62	.05	.440	17	14	.76	332	.18	2	1.14	.02	.14	1	590
K86T 1146	26	592	70	87	2.3	5	19	1485	11.05	84	5	ND	3	22	1	12	4	59	.04	.363	12	9	.74	472	.13	3	1.34	.01	.13	4	705
K86T 1147	22	600	90	95	5.0	4	15	903	13.63	103	5	ND	2	18	1	11	3	58	.04	.374	13	7	.49	593	.07	2	1.26	.01	.10	3	1950
K86T 1148	31	241	102	62	5.1	5	17	484	12.43	104	5	ND	1	23	1	8	5	57	.16	.353	8	11	.46	174	.10	2	.74	.07	.12	1	1700
K86T 1149	27	304	230	52	16.0	1	20	351	21.62	177	5	6	2	19	1	11	5	62	.10	.489	7	7	.28	137	.14	3	.27	.04	.14	2	2700
K86T 1150	26	159	215	43	10.5	1	12	212	16.10	215	5	2	2	17	1	22	3	44	.04	.494	11	11	.20	142	.05	2	.19	.01	.22	1	2100
K86S 1501	19	1228	30	28	.4	3	7	219	20.57	124	5	ND	1	9	1	4	2	81	.07	.104	7	17	.12	12	.04	2	.65	.01	.04	1	47
K86S 1502	21	1208	43	116	2.0	2	11	1053	10.25	270	5	ND	1	27	1	8	4	122	.21	.246	10	13	.53	73	.08	2	1.92	.05	.07	1	53
K86T 1503	5	340	92	142	4.1	3	21	2079	7.92	188	5	ND	1	27	1	2	2	111	.57	.293	5	24	1.06	89	.10	2	1.60	.01	.09	1	290
K86S 1504	9	341	80	95	2.4	5	17	518	8.28	103	5	ND	1	17	1	5	2	108	.15	.186	5	13	.32	69	.04	2	1.13	.01	.06	1	150
K86S 1505	5	345	53	182	1.0	13	30	1647	6.05	44	5	ND	1	13	1	9	2	70	.10	.122	10	13	1.12	151	.03	2	1.96	.01	.11	1	95
K86T 1506	34	1268	92	125	2.0	1	10	759	31.84	258	5	ND	3	18	1	2	4	163	.12	.923	10	14	.52	83	.10	5	.76	.01	.07	1	225
K86T 1507	20	766	187	133	2.9	7	16	1130	17.55	109	5	ND	2	33	1	36	10	101	.20	.465	2	14	.92	168	.18	2	1.09	.05	.09	1	365
K86S 1508	8	957	213	173	8.4	4	13	930	26.40	258	5	ND	2	20	1	9	9	226	.16	.320	7	24	.64	36	.17	3	1.41	.01	.05	1	780
K86S 1509	21	1089	81	97	4.0	2	10	514	23.37	99	5	ND	3	17	1	9	10	181	.09	.321	2	7	.30	83	.19	4	.93	.01	.07	1	640
K86S 1510	16	667	98	61	2.1	7	6	411	10.85	48	5	ND	1	26	1	8	2	61	.13	.489	7	10	.19	169	.01	2	1.04	.01	.09	1	22
K86S 1511	5	1780	38	18	2.6	1	7	155	37.27	49	5	ND	2	7	1	2	2	35	.02	.390	11	12	.11	60	.01	7	.77	.01	.05	1	80
K86S 1512	20	429	58	78	1.3	4	20	711	6.83	42	5	ND	1	32	1	4	5	54	.02	.148	10	12	.72	385	.02	2	1.52	.01	.12	1	215
K86S 1513	13	325	66	91	2.7	3	23	1200	7.81	48	5	ND	1	22	1	6	2	49	.04	.251	11	13	.51	177	.02	2	1.44	.01	.11	1	265
K86S 1514	8	354	65	152	1.3	7	34	2571	6.01	47	5	ND	1	20	1	9	2	52	.05	.162	16	15	.86	223	.02	2	2.13	.01	.10	1	200
K86S 1515	8	702	96	157	3.8	13	31	3742	7.52	57	5	ND	1	16	1	4	2	49	.03	.240	10	20	.85	172	.02	2	3.44	.01	.08	1	280
K86S 1516	10	120	71	67	2.5	3	9	490	4.91	41	5	ND	1	21	1	2	2	45	.09	.243	10	11	.38	253	.01	2	1.19	.02	.09	1	220
STD C/AU 0.5	20	59	38	132	6.8	64	29	1075	3.93	40	20	7	33	48	17	16	21	62	.48	.103	39	59	.88	178	.08	38	1.72	.06	.13	15	490

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ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-TALUS P2-3 ROCKS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JULY 31 1986 DATE REPORT MAILED: Aug 4/86 ASSAYER. D. Toye ...DEAN TOYE. CERTIFIED B.C. ASSAYER.

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86T 1151	12	516	126	209	5.5	11	15	2030	8.13	232	5	ND	6	12	1	18	5	46	.08	.187	24	12	.46	117	.10	5	2.21	.09	.09	3	695
K86T 1152	9	292	79	154	3.0	7	15	2361	7.31	89	5	ND	3	9	1	8	2	60	.13	.194	8	8	1.00	193	.05	5	1.59	.03	.13	1	215
K86T 1173	18	962	201	123	1.5	5	15	1115	14.44	146	5	ND	5	18	1	3	2	63	.01	.386	13	7	.32	516	.07	2	1.04	.03	.13	1	1800
K86T 1613	23	3111	907	281	122.3 ✓	19	34	11927	11.17	599	5	5	6	14	2	319	16	73	.03	.273	16	12	.73	240	.10	2	1.91	.04	.08	13	5100 ✓
K86T 1615	13	557	79	223	12.0	17	25	2441	7.34	1194	5	ND	2	19	1	70	2	69	.25	.173	10	13	1.03	131	.11	4	1.59	.10	.12	3	605
K86T 1622	14	1369	73	118	2.0	13	49	4123	7.72	137	5	ND	3	20	1	12	3	68	.08	.264	11	29	1.06	753	.07	8	1.78	.03	.12	4	785
K86T 1623	38	463	73	82	3.3	9	33	4063	7.81	102	5	ND	2	23	1	7	2	46	.01	.247	13	7	.24	467	.02	5	1.28	.02	.13	2	410
STD C/AU-0.5	22	60	40	138	7.1	75	30	1153	3.95	42	15	7	35	51	19	16	22	72	.48	.109	40	64	.89	189	.09	37	1.73	.09	.14	15	515

✓ Assay required for correct result

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS/TALUS -80MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

P8-9 Rocks

DATE RECEIVED: AUG 5 1986 DATE REPORT MAILED: Aug 9/86 ASSAYER. D. Toye...DEAN TOYE. CERTIFIED B.C. ASSAYER.

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86T 1176	1	211	16	101	.2	18	27	1780	6.24	7	5	ND	3	9	1	5	2	68	.07	.060	3	13	2.42	423	.01	3	3.65	.03	.09	1	10
K86S 1177	1	81	81	221	4.3	11	20	2561	5.74	41	5	ND	1	14	1	3	2	86	.14	.146	2	11	1.05	225	.02	6	2.53	.03	.13	1	60
K86S 1178	2	155	54	186	1.3	11	24	2484	5.13	52	5	ND	1	12	1	2	2	87	.07	.059	2	12	1.15	118	.06	5	2.94	.02	.12	1	60
K86S 1179	1	134	79	272	1.2	10	26	3897	5.85	67	5	ND	1	13	1	4	2	74	.11	.106	5	9	1.23	222	.03	4	2.77	.03	.14	1	75
K86S 1180	1	137	21	139	.4	12	15	1591	5.91	28	5	ND	1	13	1	5	2	90	.11	.099	4	17	1.45	173	.03	4	3.28	.02	.14	1	10
K86S 1181	2	115	30	148	.3	13	31	5578	6.74	36	5	ND	1	15	1	2	2	83	.31	.208	2	11	1.67	217	.02	4	3.08	.03	.13	1	4
K86T 1182	2	204	16	128	.3	16	25	2636	6.37	14	5	ND	1	111	1	2	2	151	.57	.139	3	20	2.53	165	.21	3	3.30	.06	.08	1	4
K86T 1183	1	276	30	158	.4	17	27	2758	6.47	24	5	ND	2	56	1	2	2	140	.36	.109	5	18	2.41	218	.18	4	3.37	.04	.12	1	26
K86S 1184	2	129	50	138	1.3	12	25	2562	5.66	31	5	ND	1	19	1	5	2	103	.11	.071	3	14	1.42	140	.10	4	3.10	.04	.11	1	27
K86S 1185	1	72	26	140	.8	6	7	729	2.42	18	5	ND	3	7	1	7	2	30	.07	.085	22	6	.52	187	.01	6	1.68	.02	.19	1	32
K86S 1186	2	124	80	382	1.5	13	33	3545	5.63	40	5	ND	1	14	1	7	2	54	.17	.138	2	8	1.23	508	.02	8	2.28	.03	.16	1	23
K86S 1187	5	202	105	255	3.6	21	42	5171	9.65	174	5	ND	1	38	1	11	2	25	.09	.207	2	8	.33	530	.01	2	1.07	.02	.24	2	245
K86S 1188	4	174	97	267	1.2	19	26	3045	6.37	187	5	ND	1	18	1	6	2	88	.15	.133	2	15	1.02	284	.02	4	2.19	.02	.12	1	100
K86S 1189	3	119	91	223	.9	12	25	3360	5.80	85	5	ND	1	48	1	5	2	102	.48	.176	3	10	1.07	418	.02	4	2.34	.03	.16	1	48
K86S 1190	3	189	67	239	4.4	15	18	2521	5.57	122	5	ND	1	10	1	9	2	69	.08	.171	6	15	.88	206	.01	4	2.67	.02	.15	1	240
K86T 1191	3	163	111	292	1.1	20	31	4215	5.44	96	5	ND	1	26	1	6	2	72	.30	.131	6	16	1.13	264	.04	4	2.52	.10	.16	1	110
K86T 1192	3	225	143	295	3.4	19	27	3142	6.10	126	5	ND	2	21	1	6	2	51	.26	.163	7	11	1.10	221	.03	4	1.98	.04	.13	1	280
K86S 1193	2	121	56	184	2.1	13	23	3328	5.84	40	5	ND	1	20	1	4	2	83	.18	.157	5	21	1.57	222	.04	5	2.63	.04	.13	2	130
K86S 1194	2	97	42	142	.6	17	26	3663	5.50	26	5	ND	1	24	1	3	2	73	.33	.157	4	21	1.52	295	.03	4	2.28	.04	.12	1	10
K86S 1195	2	108	53	129	1.0	13	23	2920	5.84	41	5	ND	1	18	1	8	3	69	.22	.252	2	16	1.16	182	.02	5	2.03	.02	.09	1	34
K86S 1196	3	85	39	133	1.0	9	20	3225	5.39	32	5	ND	1	32	1	2	2	90	.48	.240	2	15	.73	309	.01	9	1.45	.03	.13	1	40
K86S 1197	2	225	57	238	2.0	18	23	3144	6.88	73	5	ND	1	18	1	5	2	72	.22	.161	4	17	1.56	225	.03	4	2.36	.04	.14	1	620
K86T 1198	5	301	135	426	2.4	28	36	4763	8.81	90	5	ND	2	24	2	3	2	63	.32	.211	4	27	1.75	470	.08	4	2.02	.06	.09	1	205
K86T 1199	5	341	150	392	2.3	26	37	4873	9.14	88	5	ND	2	20	2	2	2	60	.26	.218	4	26	1.71	374	.07	2	1.96	.05	.10	2	220
K86T 1200	5	271	114	304	1.9	22	32	4005	8.30	81	5	ND	1	20	1	5	2	60	.22	.197	3	21	1.63	413	.08	3	1.88	.07	.09	1	160
K86S 1201	4	286	108	294	1.6	19	29	3277	7.64	61	5	ND	1	20	1	2	2	76	.17	.161	5	24	1.50	334	.04	5	2.32	.04	.09	1	100
K86S 1202	5	424	118	295	1.3	21	40	3316	7.78	100	5	ND	1	18	1	12	2	86	.08	.163	9	22	1.42	266	.04	3	2.47	.02	.09	1	150
K86S 1203	5	377	99	247	1.4	15	27	3583	7.00	77	5	ND	1	19	1	7	2	80	.05	.155	8	18	1.40	177	.04	5	2.67	.02	.10	2	110
K86S 1204	6	365	105	281	1.8	17	31	4117	7.46	92	5	ND	2	25	1	7	2	82	.14	.141	5	19	1.43	326	.04	3	2.50	.04	.12	1	125
K86S 1205	4	220	128	346	.7	18	25	3271	6.55	82	5	ND	1	29	1	2	2	84	.32	.185	4	17	1.54	428	.03	5	2.27	.03	.12	1	95
K86S 1206	4	264	127	320	1.1	17	26	3178	6.54	69	5	ND	1	24	1	2	2	88	.18	.205	3	15	1.29	276	.02	5	2.32	.03	.11	1	95
K86S 1207	6	531	123	506	2.8	29	35	4506	7.42	120	5	ND	1	32	3	2	2	81	.26	.127	12	20	1.56	936	.04	4	2.61	.03	.14	2	100
K86S 1208	5	788	73	266	1.5	21	41	4010	6.76	75	5	ND	1	42	1	9	2	82	.08	.139	12	19	1.29	283	.04	10	3.20	.03	.12	1	200
K86S 1209	17	278	60	124	2.8	8	15	1970	6.35	49	5	ND	1	36	1	9	3	89	.06	.223	5	11	.33	416	.01	4	1.32	.02	.12	1	120
K86S 1210	10	256	47	153	1.5	10	15	1707	5.61	58	5	ND	1	33	1	8	2	77	.07	.165	4	13	.59	233	.02	5	1.91	.02	.09	1	85
K86S 1211	152	287	47	48	5.4	2	4	256	4.75	19	5	ND	1	164	1	9	5	36	.06	.256	8	3	.18	730	.07	5	.74	.03	.18	2	640
STD C/AU-0.5	22	62	42	134	7.1	70	30	1148	3.99	39	17	7	35	50	18	15	20	64	.48	.108	39	61	.88	189	.09	37	1.73	.09	.13	15	515

CASSIAR MINING PROJECT - 7506 FILE # 86-1868

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86T 1212	9	87	56	355	.9	29	15	972	5.85	96	5	ND	2	24	3	34	3	48	.37	.165	4	8	.79	146	.02	3	1.02	.03	.05	1	48
K86T 1213	62	551	61	110	2.8	9	10	1105	8.12	62	5	ND	1	53	1	13	2	80	.06	.247	2	13	.64	360	.06	2	1.51	.03	.12	1	420
K86S 1214	27	710	54	153	1.3	13	20	2013	8.25	56	5	ND	1	47	1	11	2	87	.06	.192	2	14	.93	313	.07	2	2.12	.03	.11	1	780
K86S 1215	33	626	68	126	1.1	10	17	1876	7.14	64	5	ND	1	32	1	14	2	80	.03	.182	2	15	.70	240	.04	2	1.78	.02	.08	1	320
K86T 1216	71	1034	153	125	2.7	13	15	1178	8.54	50	5	ND	3	67	1	11	4	66	.20	.362	2	11	.92	352	.18	2	1.53	.10	.13	1	440
K86T 1217	60	1482	126	144	5.1	9	21	2295	6.74	58	5	ND	1	102	1	32	2	60	.11	.213	3	9	.76	286	.10	3	1.56	.05	.24	1	470
K86S 1218	5	261	84	282	2.8	18	24	3049	7.83	86	5	ND	1	13	1	9	2	77	.06	.176	2	22	1.45	187	.03	4	2.17	.03	.10	1	120
K86S 1219	13	370	133	192	3.1	12	22	2619	6.72	77	5	ND	1	61	1	33	2	68	.10	.241	3	17	1.07	443	.06	4	1.71	.03	.12	2	370
K86T 1220	9	314	106	316	1.8	21	29	3590	7.34	81	6	ND	1	16	1	13	4	66	.15	.214	2	19	1.53	577	.04	6	1.92	.03	.07	1	160
K86T 1221	7	247	92	244	2.2	21	29	3001	8.00	68	5	ND	1	44	1	8	2	69	.42	.173	2	18	1.54	328	.19	3	1.80	.22	.10	1	330
K86T 1222	7	301	110	261	2.2	18	33	3829	8.15	78	5	ND	2	24	1	9	2	61	.23	.224	2	20	1.40	365	.09	3	1.73	.07	.08	1	240
K86T 1223	5	269	121	336	2.0	26	32	3955	7.94	92	5	ND	2	17	2	5	2	63	.21	.195	2	21	1.59	481	.06	2	1.84	.04	.07	1	170
K86T 1224	6	346	132	376	2.4	26	37	4739	9.16	102	5	ND	1	17	2	5	2	65	.21	.210	2	25	1.65	392	.07	2	1.87	.05	.08	1	170
K86T 1225	6	341	128	346	2.6	24	35	4260	8.99	94	5	ND	2	18	2	4	2	63	.22	.215	2	24	1.55	408	.06	2	1.84	.05	.07	1	190
K86T 1226	2	279	76	231	1.6	14	27	3033	5.88	55	5	ND	1	22	1	7	4	68	.28	.166	5	12	1.38	375	.07	5	2.14	.03	.10	1	325
K86T 1227	1	154	47	186	1.1	16	21	1899	5.17	42	5	ND	2	28	1	2	2	70	.43	.144	7	13	1.47	292	.07	5	2.15	.05	.11	1	100
K86S 1228	2	146	159	330	2.4	17	28	4314	6.09	78	6	ND	1	42	2	6	2	82	.43	.130	4	13	1.50	251	.16	6	2.34	.17	.14	1	270
K86S 1229	5	375	604	818	6.3	21	29	9308	10.33	185	5	ND	1	16	8	8	2	39	.17	.214	2	17	.95	233	.14	2	1.44	.03	.08	2	750
K86S 1230	12	1073	1409	1833	7.2	29	88	22234	8.65	328	8	ND	1	36	12	19	2	64	.16	.178	10	15	1.22	1251	.02	2	2.38	.03	.10	5	2070
K86S 1231	8	281	645	1627	4.7	16	20	10339	6.26	253	5	ND	1	29	9	14	2	62	.30	.174	10	11	.86	386	.02	5	1.83	.03	.12	1	835
K86S 1232	2	190	73	251	1.9	17	23	3086	4.75	89	5	ND	1	13	1	8	2	105	.08	.092	3	15	1.37	183	.05	5	2.92	.02	.11	1	200
K86S 1233	5	212	92	205	6.9	15	19	3153	7.57	212	5	13	1	13	1	13	2	56	.12	.163	4	11	.73	199	.02	6	1.95	.02	.12	1	13400
K86S 1234	2	105	51	196	.8	11	15	1904	5.52	88	5	ND	1	22	1	4	3	77	.17	.141	2	11	.81	219	.02	11	1.70	.02	.15	1	55
K86S 1235	1	84	86	253	1.1	11	26	4045	5.24	69	5	ND	1	20	2	4	3	86	.26	.195	2	9	.82	380	.02	6	1.89	.02	.12	1	185
K86S 1236	1	113	63	246	1.4	12	17	1902	5.86	71	5	ND	1	12	1	8	2	99	.05	.066	2	13	1.16	119	.07	6	2.67	.02	.12	2	75
K86S 1237	3	121	108	442	3.6	12	27	4319	6.02	99	7	ND	2	26	1	7	2	78	.06	.133	2	13	.84	279	.02	7	2.26	.02	.15	1	125
K86S 1238	4	119	167	813	2.3	20	37	5667	6.63	272	5	ND	1	28	4	7	2	91	.39	.173	3	19	1.07	414	.02	8	2.51	.04	.14	1	48
K86S 1239	3	214	53	201	5.0	27	28	2777	6.68	125	5	ND	2	7	1	10	3	87	.04	.088	3	36	1.82	136	.02	8	3.06	.02	.13	1	90
K86S 1240	12	224	537	435	4.0	13	56	17034	7.31	139	5	ND	2	10	1	9	2	89	.08	.195	8	10	.89	605	.01	6	2.88	.02	.11	1	295
K86S 1241	1	122	33	151	.9	14	20	1511	5.99	38	5	ND	1	9	1	8	2	134	.04	.096	2	18	1.52	158	.03	7	3.09	.02	.11	1	15
K86S 1242	2	84	79	197	4.2	12	24	3352	6.98	50	5	ND	1	22	1	8	2	158	.20	.116	2	14	.95	381	.04	9	2.55	.03	.13	1	12
K86S 1243	2	98	83	220	1.5	11	21	3001	7.02	72	5	ND	1	17	1	5	2	151	.12	.103	4	14	1.07	169	.06	7	2.73	.02	.12	2	23
K86S 1244	2	98	45	228	3.1	10	15	2259	5.63	62	5	ND	1	14	1	8	2	111	.14	.103	5	13	.84	165	.04	9	2.42	.03	.12	1	18
K86S 1245	1	131	20	117	1.3	12	18	1774	6.30	23	5	ND	1	9	1	6	3	98	.09	.144	4	16	1.41	146	.01	9	3.33	.03	.12	1	11
K86S 1246	1	61	30	110	1.4	8	11	1173	4.55	33	5	ND	1	13	1	11	3	138	.06	.071	4	15	.81	116	.08	9	2.38	.02	.10	1	10
K86T 1247	1	207	38	166	.6	22	27	2341	6.51	39	5	ND	3	17	1	11	4	145	.22	.115	7	28	1.72	195	.06	7	3.41	.03	.15	1	7
STD C/AU-0.5	22	63	39	137	7.1	74	30	1176	4.01	40	19	8	37	51	19	17	22	73	.48	.112	40	60	.89	184	.09	40	1.73	.09	.13	15	485

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 1248	2	191	47	201	.5	19	26	3143	6.82	28	5	ND	2	26	1	9	4	152	.34	.114	8	26	1.85	237	.08	3	3.32	.03	.17	2	9
K86S 1249	6	121	89	166	7.6	9	25	4540	8.31	100	5	ND	1	13	1	9	2	111	.14	.192	2	15	.41	178	.01	2	2.17	.02	.13	1	170
K86S 1250	5	172	57	223	9.2	11	29	6210	7.76	146	5	ND	1	13	1	13	3	88	.15	.245	2	13	.70	245	.01	2	2.37	.02	.16	1	12
K86S 1251	3	72	42	143	5.7	9	22	3917	7.88	53	5	ND	1	11	1	8	3	95	.12	.201	2	23	.49	183	.01	2	2.03	.02	.15	1	8
K86S 1252	2	118	16	131	3.4	12	14	1253	6.34	36	5	ND	1	8	1	6	3	95	.07	.198	2	16	1.21	189	.02	4	3.21	.02	.15	1	11
K86S 1253	2	115	22	172	.7	11	15	1701	6.09	42	5	ND	1	10	1	9	2	124	.08	.229	5	13	1.15	200	.01	4	2.91	.02	.19	1	9
K86S 1254	2	84	28	129	1.3	8	13	1728	6.01	40	5	ND	1	12	1	9	3	115	.07	.117	3	11	.75	240	.02	3	2.43	.02	.15	1	12
K86S 1255	3	82	61	128	1.3	7	20	3907	5.49	61	5	ND	1	14	1	4	2	105	.17	.162	2	11	.50	253	.02	4	1.78	.02	.15	1	20
K86S 1256	3	122	39	203	1.4	14	25	3069	6.22	50	5	ND	2	18	1	4	2	108	.15	.099	5	16	1.38	198	.05	6	2.98	.04	.16	2	40
K86S 1257	2	116	31	196	1.5	12	18	2090	5.80	48	5	ND	2	18	1	4	2	106	.12	.094	4	18	1.21	169	.04	4	3.04	.03	.15	1	29
K86S 1258	2	97	46	251	2.1	10	19	2465	5.50	65	5	ND	1	12	1	4	2	91	.06	.100	4	14	1.03	166	.03	2	2.72	.02	.15	1	52
K86S 1259	3	70	72	198	1.3	8	27	4085	6.04	70	5	ND	1	13	1	3	2	94	.07	.088	2	14	.73	178	.05	2	2.22	.02	.15	1	60
K86S 1260	2	104	50	249	1.0	9	12	1745	4.06	62	5	ND	2	9	1	4	2	62	.05	.089	13	13	.66	144	.02	4	2.39	.02	.15	1	55
K86S 1261	3	194	109	432	2.4	20	22	4514	6.35	170	5	ND	1	18	1	11	2	59	.08	.137	8	11	.86	270	.02	6	2.05	.02	.16	2	650
K86S 1262	11	288	449	517	4.9	21	38	9241	6.97	153	5	ND	1	17	3	7	2	86	.18	.145	4	21	1.28	435	.03	4	2.81	.03	.19	1	240
K86S 1263	7	282	208	290	17.0	16	62	8493	10.66	314	5	ND	2	8	1	2	2	53	.09	.178	6	16	1.13	222	.04	2	3.35	.03	.14	1	610
K86S 1264	9	296	170	471	10.1	27	43	15307	6.81	234	5	ND	2	52	3	8	2	62	.51	.236	6	30	1.29	1293	.04	4	2.13	.04	.18	2	570
K86T 1265	5	182	164	355	1.7	23	45	10204	6.39	132	5	ND	1	28	2	2	2	75	.36	.206	5	27	1.24	600	.03	4	2.63	.03	.15	2	230
K86T 1266	5	136	247	344	4.6	15	28	6891	6.54	124	5	ND	1	31	2	24	4	71	.27	.163	5	18	.98	460	.07	8	1.97	.06	.16	1	480
K86T 1267	2	143	116	283	2.4	14	22	2970	5.76	71	5	ND	1	21	1	3	4	83	.19	.145	6	16	1.35	218	.06	5	2.51	.04	.15	1	130
K86T 1268	99	373	101	90	5.2	6	7	698	12.69	68	5	ND	2	79	1	20	2	62	.07	.411	2	8	.49	122	.06	2	.96	.05	.25	1	640
K86T 1269	33	756	68	134	2.3	12	126	7062	8.79	69	5	ND	2	45	1	7	2	59	.06	.254	6	16	.95	463	.07	2	1.83	.03	.15	1	310
K86T 1270	33	1119	64	170	2.4	20	147	11468	9.59	82	5	ND	3	52	1	16	2	56	.03	.270	10	12	.86	389	.06	2	2.01	.03	.15	1	240
K86T 1271	50	518	70	126	1.9	10	23	1726	12.78	55	5	ND	3	33	1	17	2	68	.12	.311	6	14	1.02	278	.10	2	1.32	.05	.14	1	280
K86T 1272	8	256	32	180	1.3	21	20	1278	8.96	43	5	ND	2	48	1	8	2	122	.59	.245	12	14	1.67	208	.07	2	1.85	.04	.08	1	43
K86T 1273	7	206	42	243	.9	24	21	1391	6.84	105	5	ND	3	34	2	19	2	96	.52	.215	13	18	1.52	174	.07	3	1.70	.05	.08	3	40
K86T 1274	5	148	39	270	.8	28	20	1166	6.81	48	5	ND	2	41	2	19	2	128	.56	.199	12	32	1.95	153	.07	3	2.00	.05	.10	1	27
K86T 1275	7	153	44	271	1.1	26	19	1326	6.67	68	5	ND	2	37	2	16	2	103	.51	.201	13	18	1.53	145	.05	5	1.61	.04	.09	2	21
K86T 1276	11	614	37	266	1.3	23	27	1668	10.14	58	5	ND	2	44	2	8	2	152	.52	.212	12	17	2.04	132	.08	2	1.97	.05	.10	2	42
K86T 1277	12	1546	56	206	.8	26	33	2087	5.97	77	5	ND	3	24	1	19	2	79	.31	.143	11	15	1.21	155	.04	3	2.44	.03	.11	1	11
K86T 1278	11	698	77	174	.6	14	9	528	12.58	87	5	ND	3	9	1	59	2	79	.06	.180	8	25	1.01	146	.07	2	1.38	.03	.09	1	20
K86S 1279	1	140	80	247	1.8	13	37	4511	6.84	71	5	ND	1	11	2	4	2	89	.18	.222	8	13	1.22	221	.01	3	2.94	.04	.14	1	15
K86S 1280	2	83	44	167	2.2	8	27	4563	5.60	56	5	ND	1	8	1	6	2	76	.07	.192	8	11	.54	180	.01	3	1.97	.02	.16	1	24
K86S 1281	6	143	105	173	7.9	7	39	7603	7.55	80	5	ND	1	10	1	7	2	93	.11	.251	11	8	.68	251	.01	4	2.62	.02	.17	1	240
K86S 1282	2	112	88	242	2.3	9	33	5985	6.50	57	5	ND	2	9	1	5	3	94	.05	.213	7	10	.82	404	.02	6	2.78	.03	.16	1	26
K86S 1283	4	62	73	128	1.2	6	36	9468	5.99	54	5	ND	1	16	1	7	2	116	.11	.264	6	9	.45	260	.03	5	1.48	.02	.16	1	70
STD C/AU-0.5	22	61	37	135	7.2	70	30	1154	3.99	41	19	8	36	50	18	15	18	64	.48	.109	38	59	.88	190	.09	35	1.73	.09	.13	15	480

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 1284	5	96	160	270	3.4	11	49	10675	6.02	107	5	ND	1	19	2	11	3	75	.31	.301	2	7	.65	514	.01	6	1.80	.02	.20	1	65
K86S 1285	5	327	210	494	1.8	26	48	4698	7.12	98	5	ND	2	8	1	10	2	92	.15	.137	6	30	2.14	180	.01	5	3.45	.03	.14	1	145
K86S 1286	5	186	45	562	.8	24	28	4823	5.39	36	5	ND	1	11	1	14	2	76	.22	.113	3	24	2.09	217	.07	7	3.45	.03	.17	1	95
K86T 1287	22	214	1233	1260	3.1	20	56	15108	6.87	205	5	ND	1	18	6	14	2	68	.15	.161	5	13	1.18	453	.03	5	2.62	.03	.17	5	325
K86S 1288	5	104	294	426	1.4	8	15	2343	5.93	232	5	ND	1	10	1	15	2	89	.09	.105	2	9	.45	278	.02	5	1.73	.02	.16	1	435
K86S 1289	9	185	243	509	4.8	12	28	5212	6.56	117	5	ND	1	12	2	13	2	100	.17	.139	2	15	1.03	288	.03	6	2.45	.02	.16	2	110
K86S 1290	7	233	122	279	4.9	11	15	3239	5.08	85	5	ND	1	8	1	13	2	80	.06	.146	2	16	.84	271	.04	7	2.53	.02	.13	7	175
K86S 1291	9	278	103	775	6.2	20	16	3723	5.09	91	5	ND	1	12	2	10	2	80	.10	.157	2	22	1.20	374	.02	7	3.12	.02	.16	1	250
K86S 1292	6	146	898	983	3.0	19	36	11246	7.40	164	5	ND	1	14	4	10	2	84	.13	.166	2	30	1.33	341	.05	4	2.95	.03	.15	3	210
K86S 1293	4	134	120	315	2.1	13	24	3755	6.04	86	5	ND	1	16	1	12	2	91	.12	.154	3	14	1.19	218	.04	6	2.80	.03	.15	1	115
K86S 1294	4	131	108	279	1.2	11	28	4373	6.50	92	5	ND	1	15	1	9	2	92	.11	.173	3	11	1.16	205	.04	6	2.75	.03	.15	1	95
K86S 1295	4	149	159	351	2.0	15	30	4011	6.05	84	5	ND	1	28	2	5	2	83	.34	.149	5	15	1.41	336	.09	5	2.61	.06	.14	2	135
K86S 1296	3	169	145	366	2.1	17	29	3569	5.97	72	5	ND	2	27	2	9	2	77	.32	.136	6	15	1.51	279	.11	7	2.64	.08	.14	1	215
K86S 1297	3	163	118	327	1.6	15	27	3068	5.50	66	5	ND	1	21	2	10	2	70	.26	.149	6	13	1.40	295	.06	9	2.44	.04	.14	1	150
K86S 1298	2	160	98	283	1.8	18	28	3177	5.70	72	5	ND	1	31	1	12	3	63	.49	.181	7	13	1.55	505	.05	7	2.26	.04	.12	1	110
K86S 1299	2	147	89	267	1.4	18	26	2675	5.49	62	5	ND	1	23	1	9	2	64	.43	.166	7	11	1.50	287	.05	7	2.17	.03	.11	1	195
K86T 1328	31	360	76	85	3.1	4	8	909	14.20	93	5	ND	5	11	1	7	2	46	.04	.284	2	5	.31	145	.08	2	1.20	.05	.10	1	650
K86T 1329	28	486	106	133	3.8	5	14	1157	14.50	101	5	ND	4	17	1	18	2	54	.05	.385	5	5	.48	411	.09	2	1.17	.06	.16	5	990
K86S 1631	2	203	47	209	.4	14	22	4295	6.11	28	5	ND	3	20	1	10	2	80	.22	.149	15	12	1.51	350	.02	9	3.38	.03	.17	1	40
K86S 1632	1	108	69	162	.7	9	23	3065	4.85	50	5	ND	1	17	1	2	4	68	.17	.112	5	10	1.05	172	.04	7	2.49	.04	.11	1	135
K86S 1633	1	113	171	281	2.5	10	18	2148	5.39	33	5	ND	1	14	1	6	5	79	.14	.091	5	12	1.30	328	.06	8	2.66	.04	.15	1	55
K86S 1634	1	199	46	186	1.4	14	24	1807	6.14	31	5	ND	1	30	1	2	2	130	.27	.089	7	14	2.07	214	.13	8	3.27	.04	.11	1	26
K86S 1635	1	113	25	128	.7	11	16	1455	4.25	10	5	ND	1	21	1	5	3	90	.14	.082	5	13	1.50	177	.08	7	2.67	.03	.10	1	28
K86S 1636	1	156	35	142	.9	13	21	2066	5.88	20	5	ND	1	23	1	6	2	108	.15	.086	7	17	1.72	217	.06	8	3.14	.03	.11	1	28
K86S 1637	1	76	64	168	1.7	9	14	1613	4.31	70	5	ND	1	13	1	6	2	68	.04	.099	5	10	.77	201	.02	9	1.95	.02	.15	1	75
K86S 1638	2	64	59	120	1.0	6	13	1645	4.58	70	5	ND	1	14	1	8	2	63	.06	.089	5	10	.55	168	.02	8	1.67	.02	.12	1	80
K86S 1639	2	150	54	190	1.4	13	18	1841	5.98	66	5	ND	1	13	1	9	2	90	.11	.107	8	17	1.39	232	.03	10	3.05	.03	.15	1	115
K86S 1640	4	177	76	206	1.9	21	50	5876	5.98	103	5	ND	1	26	1	7	2	99	.26	.169	10	21	1.29	424	.02	9	2.92	.03	.15	1	75
K86S 1641	16	361	64	509	3.0	70	77	27832	6.05	234	8	ND	2	146	3	20	2	60	.49	.174	18	16	1.07	1497	.02	8	2.05	.04	.21	2	71
K86T 1642	6	273	1583	1227	3.6	24	29	5414	7.68	689	5	ND	2	12	6	14	2	24	.16	.204	11	3	.47	299	.01	10	.89	.02	.13	6	915
K86T 1643	4	180	137	392	2.3	34	39	5463	5.92	166	5	ND	1	22	2	8	2	39	.28	.171	14	13	.93	424	.01	8	1.52	.03	.12	1	195
K86S 1644	2	86	45	150	.5	10	22	3014	4.71	28	5	ND	1	27	1	3	2	70	.39	.187	8	11	1.02	379	.01	10	2.10	.03	.13	1	34
K86S 1645	3	67	53	146	.4	9	21	3014	4.63	38	5	ND	1	23	1	2	2	75	.32	.245	7	13	.78	322	.01	8	1.62	.02	.12	1	54
K86S 1646	3	86	38	110	1.0	9	19	3522	4.56	25	5	ND	1	36	1	2	2	59	.65	.224	6	13	.70	539	.01	8	1.61	.03	.12	2	41
K86S 1647	2	61	57	177	1.2	12	18	2489	5.85	45	5	ND	1	22	1	4	2	83	.28	.165	5	26	1.23	257	.02	8	2.01	.02	.11	1	55
K86S 1648	2	115	62	207	.3	16	22	2385	6.13	51	5	ND	1	20	1	5	3	87	.20	.133	9	25	1.64	163	.03	8	2.44	.02	.10	2	41
STD C/AU-0.5	22	60	41	138	7.3	71	29	1122	3.80	41	19	8	35	49	18	16	23	62	.46	.106	39	57	.84	184	.08	40	1.72	.08	.13	15	505

CASSIAR MINING PROJECT - 7506 FILE # 86-1868

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 1649	3	133	61	187	1.4	14	19	2702	5.75	48	5	ND	1	21	1	9	4	75	.23	.184	11	21	1.51	318	.02	9	2.62	.03	.20	1	65
K86T 1650	7	321	137	320	2.5	23	35	4267	9.54	89	5	ND	2	19	1	11	3	60	.19	.218	8	27	1.70	282	.08	2	2.04	.05	.16	2	290
K86T 1651	7	290	121	293	2.0	22	32	3905	8.71	74	5	ND	2	24	1	13	4	64	.22	.199	11	25	1.67	360	.09	2	2.08	.06	.15	1	140
K86T 1652	7	227	90	224	1.3	19	28	3264	7.32	58	5	ND	2	62	1	11	4	81	.54	.165	11	19	1.63	204	.21	5	2.54	.27	.17	1	100
K86S 1653	6	280	126	301	1.6	16	24	4052	7.12	82	5	ND	1	17	1	11	2	74	.09	.198	10	21	1.47	182	.03	7	2.66	.03	.16	1	105
K86S 1654	5	373	98	244	1.8	18	28	3281	6.80	71	5	ND	2	18	1	13	4	83	.06	.104	10	20	1.46	181	.06	10	3.01	.03	.17	1	90
K86T 1655	3	409	50	175	2.2	17	24	2137	6.05	36	5	ND	1	22	1	10	2	92	.12	.076	6	18	1.60	261	.11	7	3.15	.03	.21	1	70
K86S 1656	9	129	57	126	.6	7	17	2726	5.76	54	5	ND	1	28	1	10	2	91	.20	.162	6	11	.51	286	.02	6	1.41	.02	.17	1	27
K86S 1657	8	120	54	192	2.4	9	16	2059	5.72	52	5	ND	1	27	1	12	4	67	.21	.204	10	12	.71	343	.02	5	1.89	.03	.19	1	60
K86S 1658	8	193	60	183	2.3	8	21	3370	7.69	39	5	ND	1	29	1	14	2	65	.33	.176	9	13	.71	502	.04	6	1.51	.03	.16	2	150
K86T 1659	8	372	99	265	1.8	18	24	2364	7.34	71	5	ND	2	35	1	13	2	62	.16	.135	13	18	1.16	500	.08	6	2.02	.03	.16	1	400
K86S 1660	12	219	78	84	1.3	5	5	702	7.09	59	5	ND	2	38	1	26	2	36	.07	.140	11	14	.34	623	.02	8	.83	.02	.14	1	610
K86T 1661	10	184	65	142	1.3	8	9	1074	6.11	41	5	ND	2	61	1	11	3	49	.04	.172	7	17	.92	458	.04	8	1.64	.03	.31	1	290
K86S 1662	5	413	25	77	.2	4	64	4526	5.58	10	5	ND	1	69	1	10	2	98	.61	.044	5	2	.43	95	.07	6	2.63	.02	.30	1	9
K86S 1663	37	718	51	137	3.6	11	10	993	5.95	48	5	ND	1	59	1	14	2	67	.07	.190	7	16	.84	350	.02	7	2.47	.02	.16	1	400
K86S 1664	13	374	65	142	1.5	11	16	1805	7.37	60	5	ND	1	32	1	13	2	92	.05	.230	8	19	.73	262	.02	6	2.31	.02	.15	1	130
K86S 1665	16	508	71	164	1.5	13	16	1456	7.40	63	5	ND	1	32	1	11	2	79	.04	.179	10	16	.86	279	.03	4	2.46	.02	.16	1	220
K86S 1666	11	248	82	243	1.9	12	25	3195	5.45	59	5	ND	1	35	1	9	2	90	.21	.137	9	15	1.04	375	.05	8	2.36	.05	.20	1	80
K86S 1667	10	417	97	263	3.1	13	25	3299	8.11	80	5	ND	1	30	2	9	2	83	.13	.224	7	18	.85	440	.02	5	2.25	.03	.20	1	170
K86S 1668	12	359	61	194	1.2	10	17	2016	6.47	48	5	ND	1	26	1	6	2	69	.21	.190	7	14	.89	554	.02	6	1.87	.02	.22	1	140
K86S 1669	5	234	74	276	1.6	18	19	2492	6.38	68	5	ND	1	28	1	7	2	87	.19	.161	7	22	1.41	337	.02	6	2.75	.03	.21	2	125
K86S 1670	2	128	31	93	2.9	11	8	521	3.37	28	5	ND	1	36	2	4	2	52	.50	.124	4	11	.82	545	.03	5	1.58	.04	.14	1	37
K86S 1671	8	195	73	193	1.2	12	16	2126	6.12	54	5	ND	1	31	1	8	2	84	.14	.263	9	19	1.21	186	.05	6	2.52	.06	.19	1	95
K86S 1672	7	311	125	271	1.7	17	30	3045	7.71	64	5	ND	2	13	1	14	2	69	.08	.240	8	25	1.43	211	.04	2	2.40	.03	.14	1	370
K86S 1673	7	336	129	301	2.1	20	27	3835	8.86	75	5	ND	1	20	1	9	2	72	.14	.203	13	26	1.62	489	.05	2	2.50	.04	.15	2	170
K86T 1674	6	298	133	370	2.3	26	34	4518	9.06	85	5	ND	1	20	2	12	2	61	.25	.207	11	26	1.78	371	.08	2	2.10	.04	.13	1	180
K86T 1675	6	330	140	397	2.7	26	35	4442	9.50	87	5	ND	1	20	2	7	3	59	.24	.211	8	25	1.72	278	.08	2	2.02	.05	.13	1	200
K86L 1676	6	460	96	388	2.0	28	35	3979	9.24	64	5	ND	2	25	2	11	2	63	.33	.165	9	22	1.66	28	.08	2	1.99	.03	.16	3	150
K86T 1677	4	233	95	274	2.3	19	27	3524	8.18	116	5	ND	1	17	1	8	2	72	.18	.179	9	21	1.59	317	.05	9	2.48	.03	.18	1	155
K86S 1678	3	177	52	188	2.1	16	20	2237	6.84	82	5	ND	1	21	1	5	2	86	.16	.133	10	18	1.53	188	.04	6	2.67	.03	.18	1	80
K86S 1679	2	104	31	129	.8	12	15	1764	5.59	26	5	ND	1	29	1	6	2	90	.22	.159	9	16	1.26	238	.03	6	2.54	.02	.17	1	18
K86S 1680	2	217	46	187	.9	17	24	2407	6.53	57	5	ND	1	28	1	8	2	88	.28	.113	16	19	1.66	276	.06	6	2.69	.03	.16	1	38
K86T 1681	2	144	48	159	.8	15	23	3200	5.75	40	5	ND	1	31	1	8	2	74	.32	.122	14	16	1.59	311	.10	6	2.52	.05	.17	1	30
K86T 1682	5	214	734	1048	3.1	19	31	10206	8.47	307	5	ND	1	16	5	22	2	35	.07	.195	12	10	.75	380	.01	2	1.47	.02	.17	4	660
K86S 1683	5	268	236	753	2.7	28	42	14479	8.75	535	6	ND	1	36	3	14	2	40	.11	.225	13	10	.96	329	.01	2	1.70	.02	.18	3	380
K86S 1684	2	126	124	164	3.8	10	17	5133	5.64	221	5	ND	1	9	1	15	2	59	.05	.163	9	14	.62	193	.01	10	1.85	.02	.22	1	440
STD C/AU-0.5	21	59	37	135	7.0	70	28	1089	3.90	38	19	7	34	48	18	16	21	60	.46	.103	38	58	.88	179	.08	36	1.72	.08	.13	15	520

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 1685	1	145	68	202	3.0	16	17	1793	5.85	58	5	ND	2	16	1	3	2	115	.09	.093	7	23	1.24	121	.05	5	2.71	.02	.12	1	225
K86S 1686	1	202	68	249	3.8	22	27	3395	6.77	82	5	ND	1	27	1	2	2	216	.23	.183	7	31	1.23	236	.02	3	2.81	.03	.12	1	65
K86S 1687	1	320	52	221	1.6	14	22	2063	6.13	56	5	ND	2	22	1	7	2	177	.12	.131	12	16	1.35	316	.02	4	3.44	.03	.14	1	70
K86S 1688	1	291	98	269	1.6	15	27	3748	6.08	63	5	ND	1	19	1	2	2	91	.19	.094	8	12	1.53	403	.04	4	2.90	.03	.14	1	55
K86S 1689	1	145	117	237	2.0	12	27	3918	6.14	78	5	ND	1	15	1	2	2	89	.15	.127	6	13	1.28	422	.03	4	2.68	.03	.13	1	41
K86S 1690	3	288	248	593	4.7	24	52	7408	7.26	123	5	ND	2	13	4	2	2	80	.09	.136	8	19	1.64	784	.01	3	3.48	.03	.17	2	75
K86S 1691	1	123	51	138	3.1	13	23	2873	6.19	50	5	ND	1	12	1	3	2	108	.09	.136	6	19	1.04	197	.03	4	2.59	.02	.15	1	31
K86S 1692	1	110	66	182	2.4	10	15	1694	5.83	60	5	ND	1	16	1	2	2	101	.13	.105	6	11	1.00	210	.06	3	2.35	.02	.15	1	44
K86S 1693	1	122	70	231	1.8	11	19	1888	5.73	54	5	ND	1	16	1	2	2	97	.16	.081	5	13	1.27	171	.07	5	2.72	.02	.14	2	39
K86S 1694	1	176	146	447	2.9	13	26	3022	6.21	113	5	ND	1	18	1	2	2	91	.22	.097	8	14	1.54	247	.06	4	2.80	.03	.13	1	120
K86S 1695	1	64	88	145	2.1	9	21	2707	5.56	54	5	ND	1	14	1	2	2	106	.11	.116	5	14	.74	226	.03	9	2.34	.02	.11	1	34
K86S 1696	1	78	42	140	1.8	9	12	1384	5.40	41	5	ND	1	10	1	2	3	96	.06	.116	6	13	.84	134	.02	5	2.66	.02	.11	1	46
K86S 1697	1	102	52	180	1.6	12	27	2857	5.94	55	5	ND	1	17	1	2	2	113	.16	.125	8	14	1.46	211	.03	4	3.14	.07	.13	1	26
K86S 1698	5	142	32	110	.8	14	31	2545	5.79	51	5	ND	1	23	1	2	2	104	.25	.094	6	13	1.03	157	.07	5	2.57	.09	.14	1	20
K86S 1699	1	220	45	167	.4	15	26	3051	6.74	32	5	ND	1	21	1	2	2	199	.25	.109	9	24	1.49	264	.08	5	3.40	.04	.15	2	26
K86T 1700	5	600	236	1207	8.7	26	58	14610	9.43	282	5	ND	1	37	4	6	2	67	.08	.160	8	20	1.27	590	.08	4	2.65	.04	.12	10	615
K86S 1701	2	176	121	340	3.1	14	19	3260	6.31	96	5	ND	1	14	1	10	2	96	.06	.133	10	23	1.28	173	.04	4	2.80	.02	.15	1	270
K86S 1702	1	128	83	230	2.7	12	18	2534	5.19	62	5	ND	1	17	1	4	2	88	.11	.140	8	19	1.03	241	.03	5	2.29	.02	.14	1	160
K86S 1703	1	157	109	284	2.1	15	28	3497	5.87	68	5	ND	1	27	2	2	2	88	.30	.150	10	17	1.43	250	.07	6	2.48	.07	.14	2	180
K86S 1704	1	163	78	231	1.5	20	27	3163	6.06	65	5	ND	2	28	2	2	2	72	.50	.188	10	17	1.67	324	.05	5	2.25	.03	.12	1	60
K86S 1705	1	138	79	233	1.2	18	27	3050	6.03	77	5	ND	2	26	2	2	2	65	.47	.182	9	15	1.61	247	.07	4	2.06	.05	.10	1	110
K86S 1706	4	252	579	864	5.4	25	38	14526	6.51	167	5	ND	1	28	4	2	2	83	.24	.187	11	35	1.28	754	.04	4	2.94	.03	.15	4	455
K86S 1707	6	386	3201	720	3.3	19	39	10317	7.03	144	5	ND	1	10	7	2	2	66	.15	.153	5	31	1.43	166	.06	4	2.61	.03	.12	1	590
K86S 1708	1	148	93	190	2.1	10	18	1869	5.67	57	5	ND	2	11	1	2	2	112	.05	.068	9	17	1.08	127	.06	4	3.19	.02	.11	1	60
K86T 1709	18	1879	253	951	8.4	19	55	13983	5.62	183	5	ND	1	16	8	7	2	76	.08	.150	9	19	1.16	337	.06	5	3.21	.02	.12	7	260
K86S 1710	2	221	105	520	2.8	15	23	3194	6.05	76	7	ND	2	14	2	2	2	113	.12	.117	6	23	1.33	209	.04	5	3.03	.02	.15	4	175
K86T 1711	9	231	224	790	4.3	16	35	5067	6.30	107	5	ND	1	16	4	2	2	104	.18	.154	8	20	1.24	244	.03	6	2.73	.03	.16	3	65
K86S 1712	3	90	90	223	2.4	7	19	3742	5.78	76	5	ND	1	17	2	3	2	97	.19	.122	5	10	.34	203	.03	4	1.37	.02	.15	1	140
K86S 1713	2	87	61	187	1.7	7	15	2973	6.48	66	7	ND	1	10	1	3	2	119	.06	.147	7	16	.64	200	.02	5	2.23	.02	.14	1	32
K86S 1714	2	65	47	157	1.0	6	16	3474	5.30	59	5	ND	1	13	1	2	4	109	.12	.152	5	12	.43	264	.02	5	1.54	.02	.14	1	41
K86S 1715	3	91	70	262	1.7	10	30	5590	5.51	85	5	ND	1	11	1	2	2	84	.09	.156	8	12	.70	305	.02	5	2.10	.03	.13	1	50
K86S 1716	1	92	65	138	3.5	8	35	5739	5.65	74	5	ND	2	12	1	2	2	89	.08	.182	6	11	.54	148	.02	5	1.96	.02	.12	1	165
K86S 1717	1	49	38	86	.6	5	13	2426	4.45	44	5	ND	1	13	1	2	2	142	.10	.150	6	12	.41	142	.04	5	1.49	.02	.15	1	310
K86S 1718	1	102	30	106	1.1	8	24	2222	4.26	30	5	ND	1	12	1	2	2	105	.13	.186	9	13	.73	179	.01	5	2.14	.02	.13	1	19
K86S 1719	1	134	41	200	.9	11	23	3395	5.25	35	5	ND	1	50	4	2	2	110	.75	.248	10	11	1.04	361	.01	6	2.44	.05	.15	1	22
K86S 1720	2	116	61	196	1.8	12	38	5617	6.51	72	6	ND	1	30	1	2	2	93	.39	.171	10	10	.81	299	.04	5	2.25	.10	.15	1	17
STD C/AU-0.5	19	61	40	134	7.0	71	30	1186	4.00	41	17	8	36	52	19	16	20	73	.48	.112	41	63	.88	176	.09	38	1.73	.09	.14	15	515

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 1721	1	87	61	184	3.0	10	25	4590	7.63	61	5	ND	1	6	1	2	2	70	.07	.230	4	10	.83	192	.01	3	2.59	.02	.13	1	6
K86S 1722	2	89	31	124	.4	11	26	3561	6.78	48	5	ND	2	21	1	2	2	74	.46	.267	5	11	.93	312	.01	4	2.40	.03	.13	1	8
K86T 1725	6	334	805	1476	9.2	45	59	9382	7.70	768	5	ND	3	34	13	15	3	63	.52	.181	18	19	1.01	563	.05	3	2.05	.03	.16	6	175
K86T 1726	2	256	535	1732	4.7	28	29	4123	5.50	471	5	ND	1	30	13	11	3	45	.60	.177	12	13	.97	253	.05	4	1.71	.03	.15	9	260
K86T 1727	1	183	269	702	2.8	27	21	3377	5.46	281	5	ND	1	30	5	9	2	47	.53	.175	11	15	1.02	219	.06	4	1.73	.03	.17	1	55
K86T 1733	9	276	127	245	2.6	7	16	2287	7.83	250	5	ND	2	18	1	16	2	49	.17	.191	10	9	.89	201	.03	4	1.75	.03	.12	1	335
K86T 1742	19	572	234	140	6.4	7	24	2436	10.80	255	5	ND	2	17	1	46	2	44	.09	.252	3	10	.41	140	.06	2	1.26	.06	.08	2	3980
K86S 1743	10	200	87	217	2.0	4	15	3129	7.55	163	5	ND	1	19	2	4	2	60	.29	.170	7	9	.63	348	.04	2	1.59	.05	.11	3	570
K86T 1770	8	89	64	346	.9	30	15	954	5.89	78	5	ND	2	25	3	30	2	48	.39	.160	9	10	.82	126	.02	5	1.10	.03	.05	1	18
K86T 1771	8	146	98	432	1.3	30	21	2066	6.93	122	5	ND	2	28	3	18	2	50	.41	.158	7	11	1.02	246	.03	3	1.28	.04	.05	1	145
K86T 1772	7	95	62	332	1.1	28	16	1097	6.05	84	5	ND	2	30	3	24	2	48	.47	.171	9	11	.91	161	.02	4	1.18	.03	.06	1	20
K86T 1773	7	234	116	369	2.1	25	28	3182	7.82	88	5	ND	2	23	3	12	2	58	.31	.191	8	18	1.30	437	.05	2	1.59	.04	.06	1	145
K86T 1774	7	322	118	363	2.8	20	26	3920	7.11	85	5	ND	1	24	2	2	2	81	.17	.189	7	20	1.40	531	.04	3	2.17	.03	.09	2	115
K86T 1775	9	346	109	262	2.1	17	27	3279	7.15	63	5	ND	1	31	1	2	2	67	.24	.215	4	20	1.33	393	.07	3	1.77	.05	.09	1	145
K86T 1776	5	321	144	315	2.2	20	32	4263	8.39	79	5	ND	2	15	2	2	2	65	.12	.218	5	22	1.59	371	.06	2	1.93	.04	.08	1	195
K86T 1777	3	289	130	329	1.8	22	29	3653	7.62	72	5	ND	2	17	1	2	2	63	.20	.176	5	23	1.59	373	.06	8	1.90	.04	.08	1	150
K86T 1778	3	240	135	370	1.7	24	32	4041	8.12	84	5	ND	2	21	2	2	2	65	.27	.192	6	26	1.69	488	.08	2	1.89	.06	.07	1	145
K86T 1779	5	306	149	393	2.7	27	34	4375	9.00	101	5	ND	2	22	2	3	2	68	.26	.215	5	23	1.62	505	.08	3	1.96	.05	.08	2	190
K86T 1780	4	298	161	389	2.1	26	35	5072	8.67	84	5	ND	1	14	2	4	2	63	.16	.217	6	25	1.59	499	.05	3	1.89	.03	.07	2	290
K86T 1781	3	359	160	461	3.1	32	40	5316	10.04	103	5	ND	2	19	3	2	2	67	.25	.229	6	26	1.71	452	.07	2	1.99	.04	.08	2	590
K86T 1782	9	345	183	487	3.0	32	41	5295	10.37	113	5	ND	2	20	3	3	2	68	.24	.246	5	26	1.73	539	.07	2	2.02	.04	.08	1	165
STD C/AU-0.5	20	61	43	140	7.2	73	29	1146	3.99	39	16	7	35	50	19	15	21	70	.48	.108	37	61	.88	187	.08	37	1.73	.09	.13	15	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 1517	2	116	63	185	.6	14	16	1559	6.76	43	5	ND	1	11	1	3	3	59	.06	.155	3	24	1.26	119	.02	2	2.28	.01	.06	1	65
K86S 1518	4	306	128	278	2.3	17	37	3460	7.84	72	5	ND	1	9	1	3	2	68	.04	.167	7	26	1.31	173	.03	5	2.50	.01	.08	1	340
K86S 1519	5	302	122	246	1.8	18	43	3373	9.01	74	5	ND	1	19	1	4	2	56	.17	.222	8	25	1.51	495	.07	4	1.80	.03	.08	1	330
K86S 1520	1	140	68	195	.7	18	31	3172	6.02	45	5	ND	1	38	1	2	2	74	.56	.145	8	25	1.64	359	.09	6	2.27	.09	.10	1	56
K86S 1521	2	70	106	152	.5	8	32	4791	4.88	49	5	ND	1	20	1	3	2	68	.33	.295	5	14	.68	287	.01	5	1.37	.01	.10	1	100
K86S 1522	1	126	94	355	1.1	12	30	4176	4.71	47	5	ND	1	40	2	2	2	50	.75	.205	7	17	1.17	353	.01	6	1.87	.01	.10	1	80
K86S 1523	1	83	43	148	.9	11	23	2327	5.68	37	5	ND	1	15	1	3	2	80	.15	.143	4	17	1.25	226	.02	3	2.12	.01	.11	1	34
K86S 1524	1	152	38	145	.4	15	27	2605	5.50	24	5	ND	1	24	1	2	2	59	.41	.169	9	15	1.77	423	.09	3	2.47	.02	.10	1	37
K86S 1525	1	145	33	141	.3	14	26	2547	5.41	21	5	ND	1	26	1	2	2	57	.45	.178	8	16	1.77	392	.09	4	2.38	.03	.09	1	16
K86S 1526	5	148	37	73	1.8	17	40	3107	8.28	366	5	ND	1	17	1	19	3	30	.27	.152	8	6	.58	344	.01	6	1.04	.01	.10	1	950
K86S 1527	62	1698	49	42	2.2	2	13	601	25.76	132	5	ND	2	22	1	8	6	165	.17	.412	10	15	.46	114	.14	2	1.01	.03	.06	1	230
K86S 1528	11	2118	49	31	.7	1	9	449	26.84	58	5	ND	3	23	1	7	2	145	.16	.261	5	9	.39	100	.19	7	.87	.02	.06	1	270
K86S 1529	23	1210	58	130	.9	18	27	1887	12.37	219	5	ND	1	17	1	14	2	209	.35	.221	9	20	.96	44	.10	3	3.79	.01	.04	1	280
K86S 1530	13	146	100	50	2.1	1	10	216	5.54	46	5	ND	1	22	1	17	2	28	.04	.216	11	7	.26	352	.03	2	.59	.02	.09	2	255
K86S 1531	13	131	104	41	2.3	1	8	145	5.01	42	5	ND	1	26	1	15	2	22	.02	.209	10	5	.20	355	.01	3	.43	.01	.09	2	295
K86S 1532	15	173	49	33	1.1	1	11	163	6.07	42	5	ND	1	28	1	12	2	25	.05	.255	9	4	.22	261	.03	2	.42	.03	.09	1	225
K86S 1533	17	759	44	42	1.9	1	9	225	17.78	179	5	ND	1	17	1	11	5	63	.10	.505	6	8	.32	152	.05	2	.53	.04	.06	2	145
K86S 1534	11	919	32	42	.8	1	7	359	20.60	63	5	ND	2	7	1	3	8	47	.02	.336	3	4	.26	141	.01	2	.49	.01	.05	1	465
K86T 1535	16	165	65	54	2.4	1	10	179	5.35	36	5	ND	1	11	1	11	3	22	.02	.206	10	11	.31	179	.01	2	.55	.01	.08	1	350
K86T 1536	16	182	96	63	2.6	2	11	249	7.39	46	5	ND	1	17	1	18	2	27	.03	.278	9	7	.33	273	.03	5	.50	.02	.09	1	320
K86T 1537	78	201	76	54	2.3	1	12	515	6.71	53	5	ND	2	25	1	21	3	21	.01	.306	7	5	.21	315	.01	3	.45	.01	.09	1	430
K86T 1538	40	229	241	53	3.1	1	12	317	6.04	52	5	ND	2	40	1	13	4	21	.02	.334	14	4	.19	586	.01	4	.51	.01	.11	1	1280
K86S 1539	31	189	67	53	1.9	4	15	371	6.49	33	5	ND	2	46	1	12	2	37	.35	.291	7	6	.58	218	.17	2	.82	.17	.12	1	430
K86S 1540	49	439	59	47	2.4	4	23	294	8.04	32	5	ND	1	67	1	7	2	52	.28	.295	7	14	.67	530	.10	2	1.13	.13	.13	1	620
K86S 1541	51	565	62	38	2.1	3	4	175	7.93	33	5	ND	1	53	1	7	2	39	.02	.308	8	17	.35	341	.01	3	.97	.01	.08	2	340
K86S 1542	17	136	61	31	1.3	1	7	185	5.15	22	5	ND	1	21	1	5	2	33	.02	.144	12	18	.27	180	.02	4	1.19	.01	.07	1	230
K86S 1543	13	271	53	48	3.2	1	14	581	5.41	29	6	ND	1	12	1	7	2	37	.02	.123	9	22	.50	139	.02	2	1.30	.01	.06	2	390
K86S 1544	12	89	51	48	7.2	1	8	997	5.90	24	5	ND	1	18	1	3	2	49	.05	.262	8	20	.27	186	.04	4	1.05	.01	.06	1	90
K86S 1545	4	61	59	45	2.9	3	7	466	3.92	29	5	ND	1	21	1	15	4	36	.12	.114	9	10	.39	436	.04	4	.95	.05	.07	2	190
K86S 1546	5	133	44	49	2.2	5	10	243	6.52	45	5	ND	1	21	1	8	2	37	.11	.216	8	8	.37	184	.09	2	.92	.04	.07	1	190
K86S 1547	20	213	79	65	3.3	1	17	801	9.52	57	5	ND	1	21	1	9	4	48	.08	.303	7	11	.37	464	.09	2	.85	.02	.10	3	1350
K86S 1548	12	112	47	56	1.9	5	11	1152	5.47	30	5	ND	1	20	1	5	4	44	.11	.207	5	17	.26	276	.04	3	.78	.02	.08	1	380
K86S 1549	11	513	53	140	1.2	10	46	2074	6.79	33	5	ND	2	37	1	7	4	67	.11	.203	19	18	1.04	495	.13	2	2.98	.03	.11	1	250
K86S 1550	11	222	117	93	4.0	4	18	1440	7.71	45	5	ND	1	52	1	10	5	41	.01	.183	12	24	.52	441	.01	2	1.26	.01	.14	1	880
K86S 1551	17	453	183	191	2.1	20	53	4029	10.84	65	5	ND	2	49	1	4	6	40	.02	.295	6	30	.61	418	.01	2	1.11	.01	.13	1	430
K86S 1552	18	414	231	305	2.3	25	57	13380	11.61	93	5	ND	1	44	1	2	3	53	.07	.274	6	28	1.15	1024	.04	4	1.39	.03	.10	1	430
STD C/AU 0.5	21	59	43	131	6.7	70	29	1095	3.93	36	19	7	33	47	16	17	20	62	.48	.103	35	60	.88	177	.08	36	1.72	.06	.13	12	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
K86S 1553	19	118	61	64	.8	3	10	878	9.78	35	7	ND	3	18	1	4	2	28	.04	.088	3	19	.16	71	.08	2	2.40	.03	.06	2	110
K86S 1554	10	188	112	44	1.4	3	11	223	7.76	67	5	ND	2	54	1	14	2	27	.02	.287	2	2	.19	278	.03	2	.45	.01	.08	1	210
K86S 1555	10	142	124	44	2.3	2	9	161	6.15	56	5	ND	1	50	1	9	2	27	.02	.261	2	4	.18	266	.01	5	.59	.01	.08	3	225
K86T 1556	8	156	103	43	1.3	1	9	163	6.20	46	5	ND	1	32	1	12	2	22	.01	.235	3	2	.18	267	.01	2	.40	.01	.08	1	175
K86T 1557	18	915	65	33	1.3	1	10	170	19.15	96	5	ND	3	13	1	11	2	60	.04	.306	2	2	.17	154	.06	2	.32	.01	.08	1	165
K86T 1558	11	101	98	35	2.4	2	6	126	4.45	33	5	ND	1	16	1	13	2	21	.02	.194	4	1	.16	274	.01	4	.41	.01	.08	3	210
K86S 1559	14	107	151	41	2.4	1	8	138	4.88	39	5	ND	1	31	1	16	2	22	.02	.208	4	1	.18	422	.02	4	.41	.02	.10	3	165
K86T 1560	12	132	87	40	1.7	1	7	108	4.86	37	5	ND	1	19	1	12	2	21	.02	.197	5	3	.15	452	.01	2	.45	.01	.09	1	265
K86T 1561	13	97	60	32	1.6	2	6	142	4.39	30	5	ND	1	31	1	10	2	20	.05	.174	6	3	.19	431	.02	5	.53	.03	.10	2	205
K86T 1562	19	151	72	33	1.9	1	8	181	5.69	50	5	ND	2	22	1	16	2	19	.01	.243	4	2	.12	381	.01	3	.35	.01	.09	1	245
K86T 1563	32	156	85	36	2.7	1	9	263	4.64	53	5	ND	2	21	1	22	2	14	.01	.190	7	2	.10	361	.01	4	.43	.01	.10	3	425
K86T 1564	25	116	102	27	2.8	1	7	142	4.49	39	5	ND	2	15	1	10	2	13	.01	.196	6	2	.09	235	.01	4	.28	.01	.09	1	365
K86T 1565	50	208	59	28	.9	4	11	156	5.54	36	5	ND	2	20	1	7	2	18	.02	.183	6	4	.14	214	.01	2	.50	.01	.10	1	275
K86S 1566	36	135	75	27	.6	1	8	227	5.43	32	5	ND	1	16	1	5	2	29	.02	.192	8	13	.18	228	.03	2	.79	.01	.07	1	345
K86S 1567	19	140	76	41	1.2	2	10	337	4.95	38	5	ND	1	27	1	10	2	34	.09	.149	6	15	.38	240	.05	3	.94	.04	.09	1	295
K86S 1568	12	98	76	65	2.5	1	7	420	6.38	43	5	ND	1	22	1	18	2	34	.02	.168	11	17	.44	266	.03	3	2.16	.02	.08	2	195
K86S 1569	6	127	73	61	1.0	4	10	308	7.77	26	5	ND	1	40	1	5	2	58	.04	.241	2	29	.32	463	.01	2	1.29	.01	.09	1	85
K86S 1570	12	182	56	60	1.1	6	12	304	8.80	35	5	ND	1	27	1	5	2	74	.02	.199	2	27	.48	245	.06	2	1.45	.01	.07	1	150
K86T 1571	20	413	64	59	1.9	5	22	682	7.81	40	5	ND	1	22	1	2	3	49	.05	.208	6	14	.48	301	.07	2	1.59	.02	.10	1	595
K86T 1572	16	238	56	44	1.4	3	12	449	5.01	21	5	ND	1	17	1	4	2	45	.03	.154	8	17	.50	183	.04	2	1.68	.01	.08	1	375
K86S 1573	20	586	44	71	1.1	8	9	619	7.43	28	5	ND	1	22	1	4	2	48	.04	.282	9	19	.60	382	.04	2	2.90	.01	.09	2	395
K86S 1574	18	233	82	58	3.4	2	15	838	8.83	54	5	ND	1	18	1	8	2	41	.04	.275	3	9	.27	518	.03	2	.84	.01	.10	1	555
K86S 1575	22	384	73	74	4.2	3	20	656	11.39	60	5	ND	2	20	1	10	2	53	.03	.309	6	16	.46	284	.08	2	1.15	.02	.10	1	815
K86T 1576	22	241	86	57	2.7	1	16	648	10.45	64	5	ND	2	16	1	12	2	49	.02	.272	4	15	.37	306	.04	2	.94	.01	.10	1	650
K86T 1577	12	162	111	45	3.1	3	11	345	11.89	81	5	ND	2	19	1	26	3	36	.02	.245	4	15	.23	293	.03	2	.42	.01	.11	1	990
K86S 1578	6	201	97	91	1.8	7	20	1230	9.58	60	5	ND	1	12	1	6	2	50	.07	.254	2	28	.51	159	.01	2	1.12	.01	.12	1	595
K86T 1579	4	268	217	421	2.5	38	46	5080	10.51	148	5	ND	2	29	1	4	4	48	.30	.331	5	22	.69	75	.12	2	1.01	.15	.09	1	515
K86S 1580	2	263	714	298	20.8	10	28	3116	8.44	308	5	3	1	26	1	8	2	45	.13	.260	3	20	.37	130	.05	2	.63	.06	.11	1	3160
K86S 1581	8	176	522	460	4.9	30	32	5819	10.37	433	5	2	2	5	1	10	8	14	.13	.207	17	12	.13	51	.03	2	2.04	.02	.05	1	2090
K86S 1582	4	234	371	341	5.8	23	46	8163	8.90	430	5	ND	1	7	1	14	8	75	.04	.227	7	33	.92	113	.01	4	2.04	.01	.08	1	195
K86S 1583	4	341	210	522	1.7	40	44	5964	8.34	672	5	ND	1	19	1	22	2	76	.06	.160	8	29	.74	169	.01	2	2.31	.01	.09	1	465
K86S 1584	16	560	182	290	2.8	21	46	6690	10.87	242	5	ND	1	42	1	15	2	78	.23	.209	10	13	.98	129	.06	2	2.10	.01	.08	1	195
K86T 1585	4	431	210	840	4.5	64	49	6445	7.68	548	5	ND	1	14	2	14	2	56	.14	.220	17	30	.66	449	.01	2	1.52	.01	.12	1	385
K86T 1586	6	300	365	1113	3.7	40	52	9787	9.51	621	5	ND	1	10	4	12	2	31	.09	.275	11	7	.37	271	.01	2	.82	.01	.10	1	215
K86T 1587	4	260	200	358	4.9	35	41	7261	8.43	376	5	ND	1	8	1	14	2	28	.11	.215	11	12	.25	231	.01	2	.75	.01	.10	1	275
K86T 1588	6	204	579	754	3.3	52	62	18522	12.31	152	5	ND	1	18	2	2	5	29	.06	.388	3	22	.20	137	.02	2	.50	.02	.07	1	470
STD C/AU 0.5	21	60	40	137	6.9	69	30	1100	3.94	41	20	7	34	49	18	15	21	64	.48	.103	37	61	.89	182	.08	37	1.73	.07	.14	17	485

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au† PPB
K86T 1589	3	245	160	412	2.0	14	50	13101	12.94	108	5	ND	1	10	4	2	3	44	.07	.535	19	4	.24	507	.03	2	.77	.03	.06	1	185
K86T 1590	3	76	2596	228	12.0	4	11	1500	7.97	307	5	ND	2	19	1	12	2	32	.01	.333	17	8	.04	299	.01	2	.21	.01	.14	1	215
K86S 1591	3	220	391	481	2.0	36	34	7395	8.42	375	5	ND	1	6	1	8	2	41	.02	.208	21	20	.36	178	.01	2	1.14	.01	.08	1	210
K86S 1592	2	114	107	196	.6	30	20	3502	6.38	328	5	ND	1	3	1	8	2	42	.02	.192	12	30	.14	159	.01	7	.93	.01	.06	1	90
K86S 1593	6	45	24	104	.9	3	7	931	5.07	48	5	ND	2	3	1	3	2	10	.05	.080	40	8	.10	67	.07	6	3.54	.07	.07	1	95
K86S 1594	2	62	35	143	.5	16	9	1264	4.74	167	5	ND	1	4	1	6	2	56	.04	.150	11	28	.16	143	.01	3	1.82	.01	.05	1	55
K86S 1595	1	155	102	264	1.2	25	27	2912	6.28	216	5	ND	1	28	1	6	2	42	.52	.209	14	13	.83	166	.01	3	1.41	.01	.07	1	70
K86S 1596	2	87	41	143	.1	22	21	4472	6.16	145	5	ND	1	3	1	6	2	21	.02	.250	9	11	.07	80	.01	4	.43	.01	.07	1	65
K86S 1597	5	261	340	404	2.8	41	41	6813	15.03	1595	5	ND	1	8	3	7	3	53	.04	.463	15	48	.41	44	.01	2	.62	.01	.03	1	135
K86S 1598	5	173	233	558	1.7	40	35	5191	9.56	361	5	ND	1	13	2	9	2	46	.15	.223	14	31	.48	213	.01	2	1.53	.01	.06	1	490
K86S 1599	11	384	669	995	4.2	104	46	16363	11.20	223	5	ND	2	11	7	12	3	26	.08	.320	20	16	.25	240	.01	2	.74	.01	.05	1	315
K86S 1600	2	129	120	283	1.2	34	23	3663	6.79	341	5	ND	1	7	1	9	2	45	.08	.189	14	34	.45	116	.01	4	1.19	.01	.07	1	165
K86S 1601	1	157	124	301	4.6	46	34	4694	7.84	446	5	ND	1	8	1	11	2	39	.10	.178	15	22	.30	234	.01	4	.84	.01	.07	1	395
K86S 1602	1	150	173	334	2.1	27	30	6481	7.56	426	5	ND	1	6	1	10	2	34	.05	.187	10	16	.14	206	.01	2	.73	.01	.08	1	175
K86T 1603	2	258	72	147	1.7	36	40	5323	6.56	295	5	ND	1	15	1	6	2	31	.23	.184	10	18	.34	232	.01	2	.80	.01	.09	1	160
K86S 1604	4	38	21	63	.6	5	5	403	4.36	38	7	ND	1	2	1	2	2	8	.03	.103	43	7	.05	40	.06	6	3.23	.05	.06	1	75
K86S 1605	2	963	215	560	1.5	23	28	9865	7.35	171	5	ND	1	9	3	4	2	30	.08	.157	15	8	.11	347	.01	2	.57	.01	.07	1	135
STD C/AU 0.5	20	59	43	135	6.9	72	30	1107	3.92	40	18	8	34	49	18	17	18	63	.48	.105	37	61	.88	182	.08	36	1.72	.07	.14	15	490

APPENDIX III

STATEMENT OF QUALIFICATIONS

STATEMENT OF QUALIFICATIONS

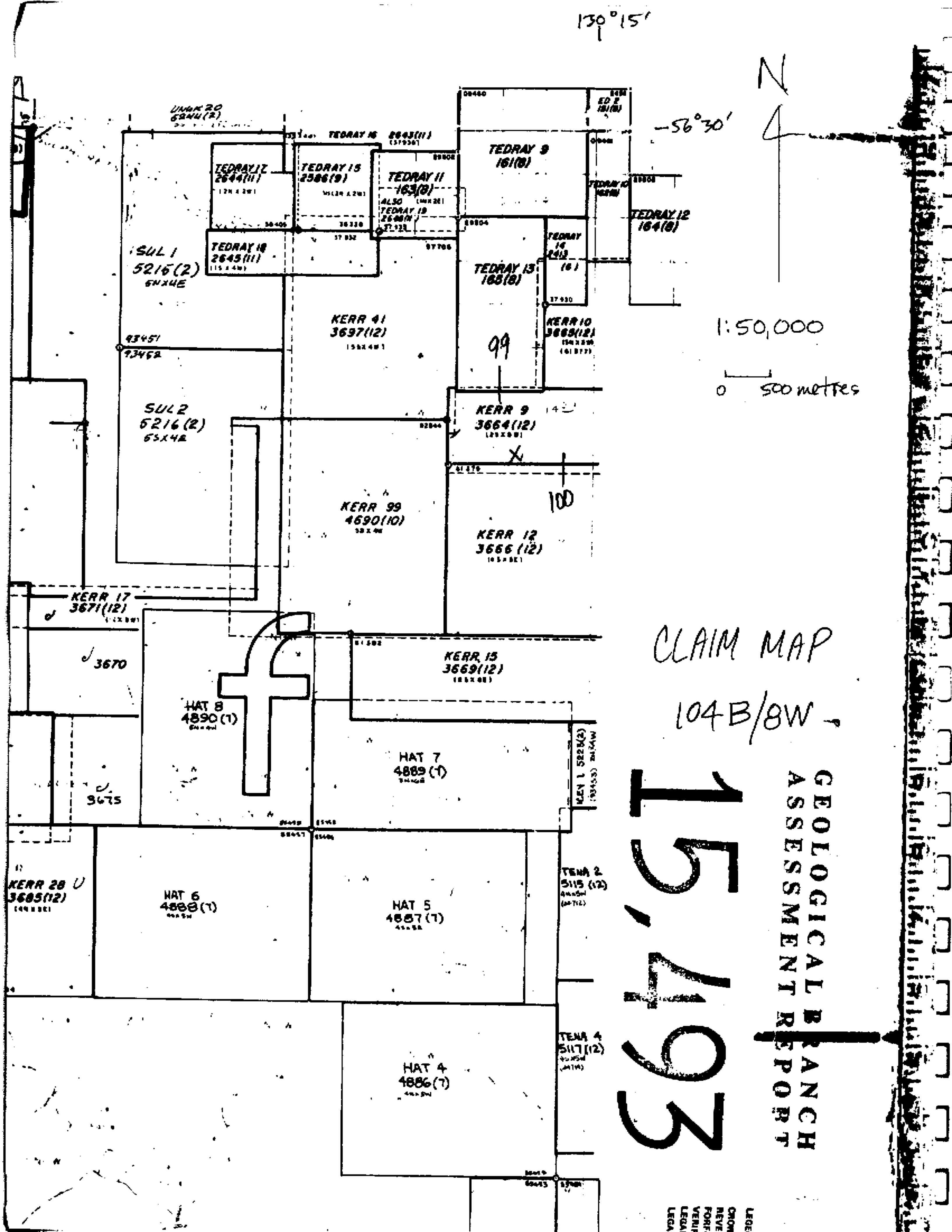
RICHARD E. MEYERS

B.Sc. Geology - Carleton University, Ottawa, 1974

M.Sc. Economic Geology - McGill University, Montreal, 1980

I have practised my profession continuously since graduation in 1974, including three years as a mining and evaluation geologist (1974-77), two years in economic geology research (1977-79) and seven years as an exploration geologist.

R E Meyers



130°15'
-56°30'
N
1:50,000
0 500 metres
CLAIM MAP
104B/8W
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,493
TEDRAY 9 161(8)
TEDRAY 11 163(8)
TEDRAY 12 164(8)
TEDRAY 13 168(8)
TEDRAY 15 2586(9)
TEDRAY 16 2643(11)
TEDRAY 17 2644(11)
TEDRAY 18 2645(11)
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SUL 2 5216(2)
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KERR 28 3685(12)
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3675
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HAT 7 4889(7)
HAT 6 4888(7)
HAT 5 4887(7)
HAT 4 4886(7)
TENA 2 5115(12)
TENA 4 5117(12)
99
100

LEGEND

UPPER SEQUENCE

- 14 Andesite Flows
- 13 Siltstone
- 12 Upper Conglomerate
- 11 Siltstone
- 10 Andesite Flows (Epidote)
- 9 Pyroclastic Breccia

MAJOR TECTONIC SHEAR ZONE

- 8 Andesite Dykes
- 7 Andesite Tuffs, and schistose equivalents (highly altered)

LOWER SEQUENCE

- 6 Greywacke and Siltstone
- 5 Andesitic Feldspar Porphyries
- 4 Silicified Andesite Flows
- 3 Laminated Siltstone
- 2 Lower Conglomerates

Symbols

- Claim Boundaries
- Geological Contacts
- Boundaries of Major Tectonic Shear Zones
- 70 Bedding Attitude
- 30 Fracture Attitude
- 70 Foliation Attitude
- Outcrop
- Δ 2002 Thin Section Sample Locations
- M0179 Mineralogical XRD Scan

NORTH SHEET

MAP BY: EAGLE MAPPING SERVICES LTD. (85-42) JULY 1985
COMPILED FROM AIR PHOTOS TAKEN IN 1982

WESTERN CANADIAN MINING LTD.

KERR PROJECT - 1985 (1986)
GEOLOGY
1986 GRID AREA

SCALE : 1 5000	CONTOUR INTERVAL : 10 METRES
DRAWN BY: K. Akhurst, H.H.	DATE : Dec., 1985
DRAFTING BY: W. Epp, H.H.	N.T.S. : 104 B/8
REPORT 847 & 962 (1986)	FIGURE No. 4

15,493

GEOLOGICAL BRANCH
ASSESSMENT REPORT

WESTERN CANADIAN MINING LTD.

KERR PROJECT
1986
DETAILED PROPERTY GEOLOGY

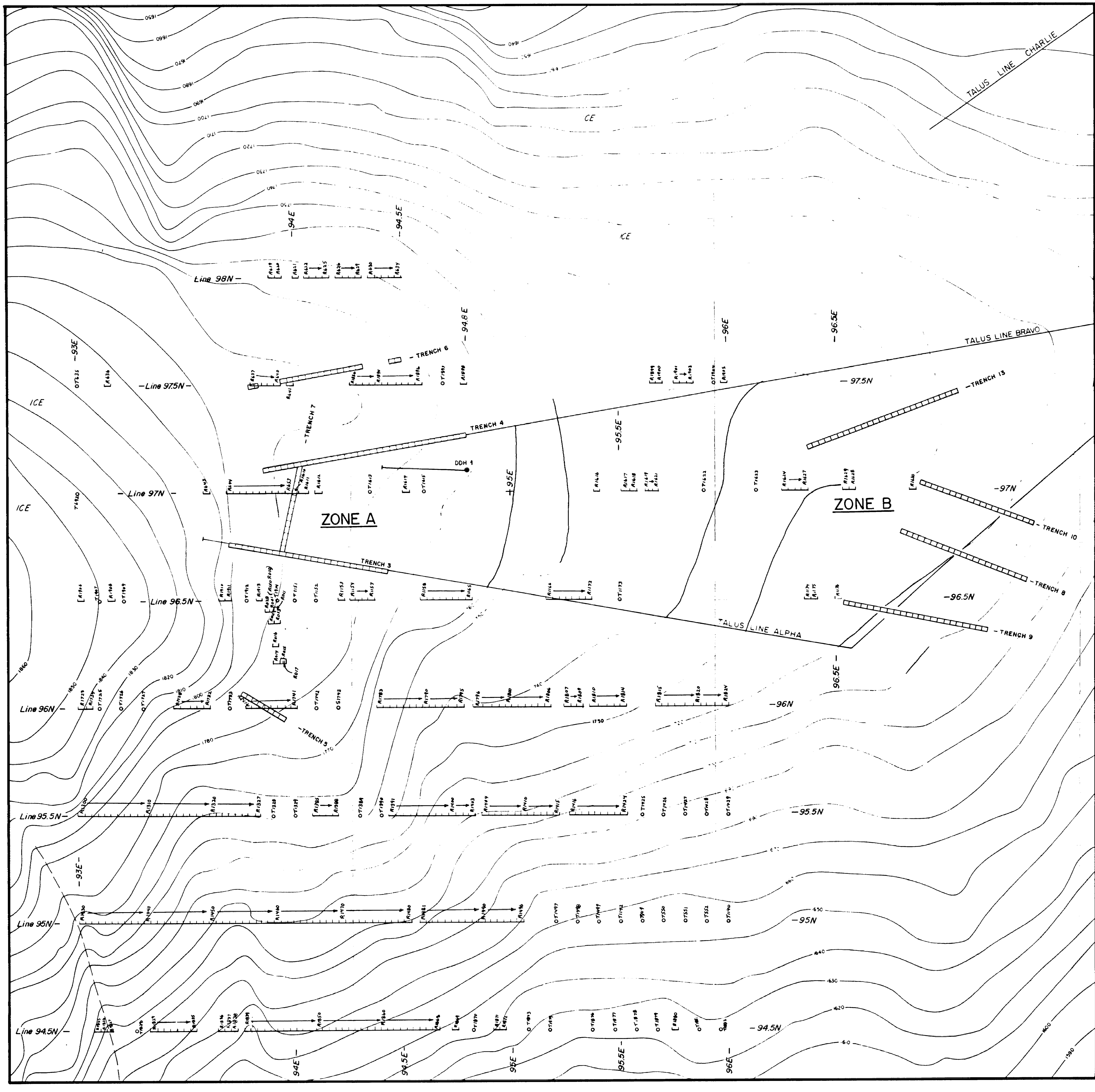
(2)

DRAWN BY: R. MEYERS	DATE: OCTOBER, 1986
DRAFTED BY: H. HOLM	N.T.S. 104B/8
REPORT No. 962	FIGURE NO. 5

N
ZONE A
ZONE B
ZONE C
ZONE D
ZONE F
ZONE L
Line 103N
Line 102.5N
Line 102N
Line 101.5N
Line 101N
Line 100N
L100N
Line 99N
Line 98N
Line 97N
Line 96N
Line 95N
Line 94N
Line 93N
Line 92N
Line 91N
Line 90N
Line 89.5N
Line 89.25N
Line 89N
Line 88.75N
Line 88.5N
Line 88.25N
Line 88N
Line 87.75N
Line 87.5N
92.5E
93E
94E
95E
96E
97E
98E
99E
100E
101E
102E
Baseline
Legal Corner Post
Lake
+1916
+1922
+1619
1634
1400
1450
1500
1550
1600
1650
1700
1750
1800
1850
1900
LEGEND
Soil sample
Talus sample
Rock sample
Silt sample
NOTE - Contours in metres.
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,493
SCALE 0 25 50 75 100 125 metres
1:2,500
WESTERN CANADIAN MINING LTD.
1986
KERR PROJECT
Zones A,B,C,D,F&L
SAMPLE LOCATIONS
(3)
DRAWN BY: R. MEYERS
DATE: OCTOBER, 1986
DRAFTED BY: H. HOLM
N.T.S. 104B/8
REPORT No. 962
FIGURE NO. 6a

N
ZONE A
ZONE B
ZONE C
ZONE D
ZONE F
ZONE L
Line 103N
Line 102.5N
Line 102N
Line 101.5N
Line 101N
Line 100N
Line 99N
Line 98N
Line 97N
Line 96N
Line 95N
Line 94N
Line 93N
Line 92N
Line 91N
Line 90N
Line 89.5N
Line 89.25N
Line 89N
Line 88.75N
Line 88.5N
Line 88.25N
Line 88N
Line 87.75N
Line 87.5N
92.5E
93E
94E
95E
96E
97E
98E
99E
100E
101E
102E
Baseline
LCP KERR 99
+1916
+1922
+1619
1634
LEGEND
Soil sample
Talus sample
Rock sample
Silt sample
≥1000 ppb
500 – 999 ppb
Note - Topographic contours in metres.
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,493
SCALE: 0 25 50 75 metres
1:2,500
WESTERN CANADIAN MINING LTD.
-1986-
KERR PROJECT
GOLD (in PPB)
GEOCHEMISTRY
Zones A,B,C,D,F,&L
(4)
DRAWN BY: R. MEYERS
DATE: OCTOBER, 1986
DRAFTED BY: H. HOLM
N.T.S. 104B/8
REPORT No. 962
FIGURE NO. 6b


N
ZONE A
ZONE B
ZONE C
ZONE D
ZONE F
ZONE L
Line 103N
Line 102.5N
Line 102N
Line 101.5N
Line 101N
Line 100N
L100N
Line 99N
Line 98N
Line 97N
Line 96N
Line 95N
Line 94N
Line 93N
Line 92N
Line 91N
Line 90N
Line 89.5N
Line 89.25N
Line 89N
Line 88.75N
Line 88.5N
Line 88.25N
Line 88N
Line 87.75N
Line 87.5N
92.5E
93E
94E
95E
96E
97E
98E
99E
100E
101E
102E
Baseline
Lake
+1619
1634
+1916
+1922
LEGEND
Soil sample
Talus sample
Rock sample
Silt sample
Note – Topographic contours in metres.
GEOLOGICAL BRANCH ASSESSMENT REPORT
15,493
WESTERN CANADIAN MINING LTD.
1986
KERR PROJECT
Zones A,B,C,D,F,&L
SILVER (in ppm)
GEOCHEMISTRY
DRAWN BY: R. MEYERS
DATE: OCTOBER, 1986
DRAFTED BY: H. HOLM
N.T.S. 104B/8
REPORT No. 962
FIGURE NO. 6c
SCALE
0 25 50 75 100 125 metres.
1:2,500



N

LEGEND

o Talus sample

⊔ Rock sample interval

Contours in metres.

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,493

SCALE 1:1000

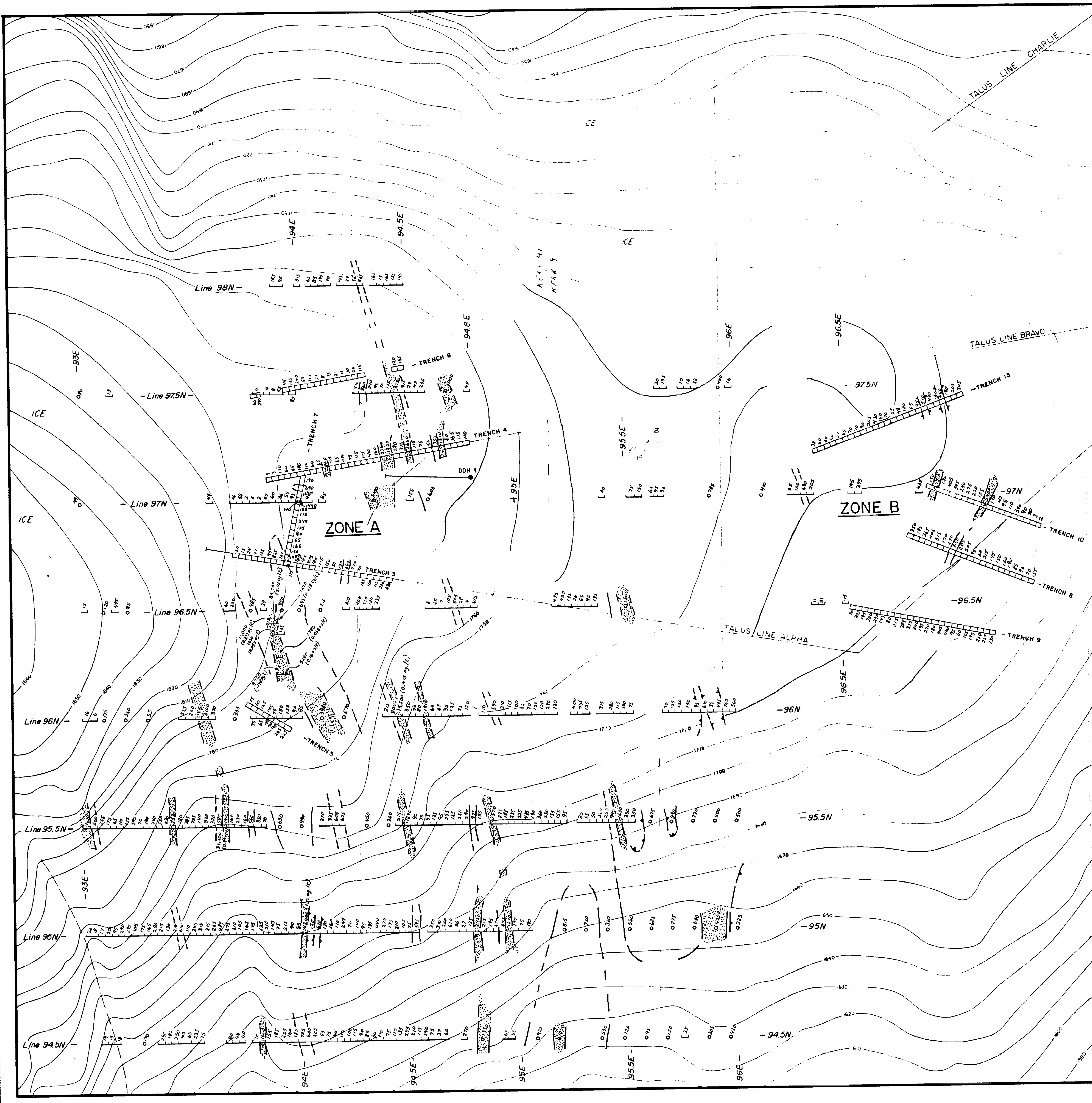
m 0 10 20 40 60 80 100 m

WESTERN CANADIAN MINING LTD.

KERR PROJECT (1986)
ZONES A&B
SAMPLE LOCATIONS
(TALUS & ROCK CHIP)

(6)

DRAWN BY B.H.W., S.C.	DATE Oct., 1986
DRAFTED BY H.H.	N.T.S. 104 B/8
REPORT No 962	FIGURE No 7a



LEGEND

- o Talus sample
- ⌊ Rock sample interval
- ▩ ≥1000 ppb
- □ 500 – 999 ppb

NOTE – Bracketed values are gold in ounces/ton by a...

– Topographic contours in metres.

SCALE 1:1000

m 0 10 20 40 60 80 100 m

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,493

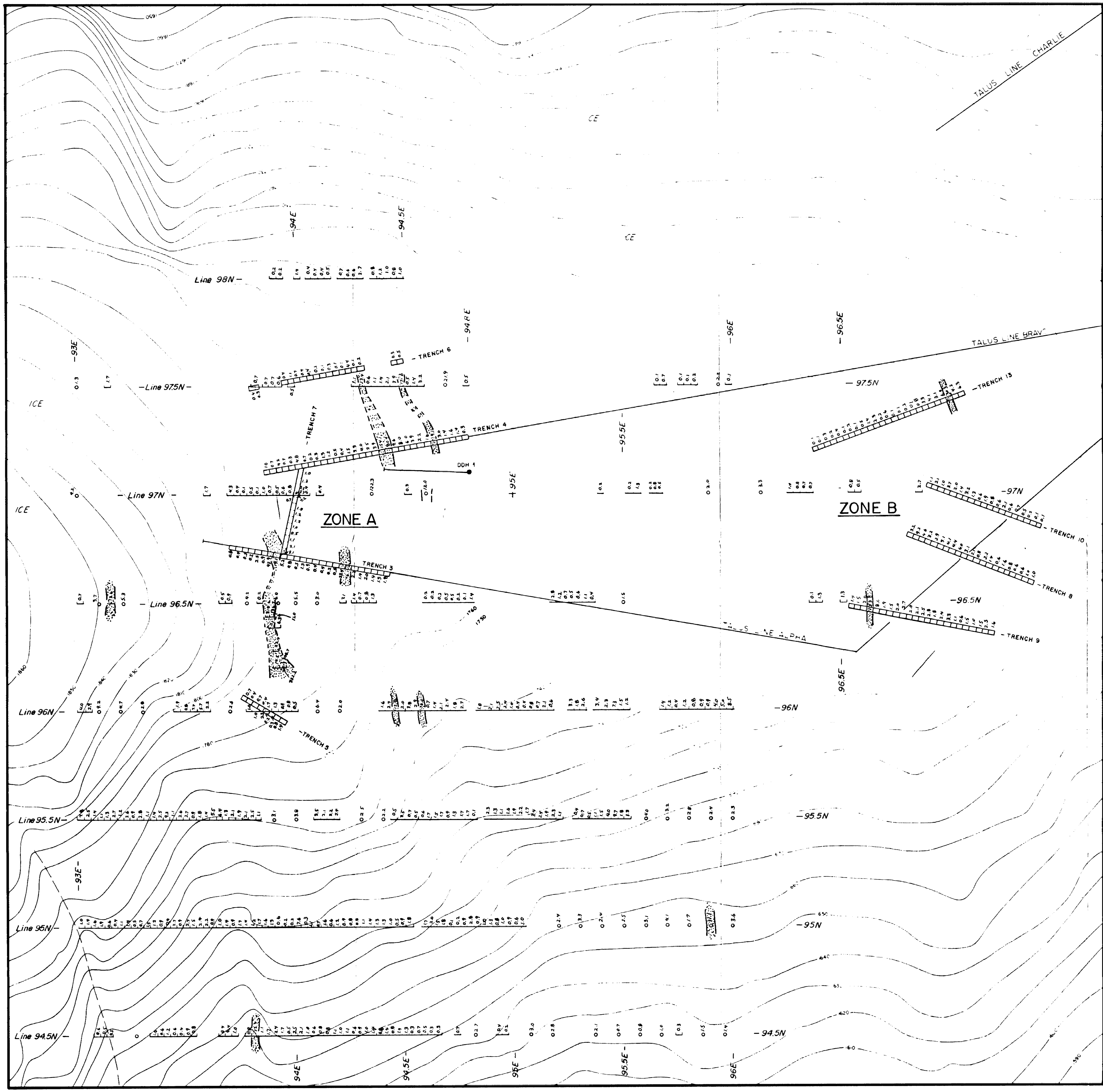
WESTERN CANADIAN MINING LTD.

KERR PROJECT (1986)

GOLD
GEOCHEMISTRY
in ppb.
ZONE A & B

(7)

DRAWN BY B.H.W., S.C.	DATE Oct., 1986
DRAFTED BY H.H.	N.T.S. 104 B/8
REPORT No. 962	FIGURE No. 7b



N

LEGEND

○ Talus sample

⊔ Rock sample interval

▨ ≥10 ppm

NOTE – Topographic contours in metres

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,493

SCALE 1:1000

m 0 10 20 40 60 80 100 m

WESTERN CANADIAN MINING LTD.

KERR PROJECT (1986)

SILVER
GEOCHEMISTRY
in ppm.

ZONES A&B

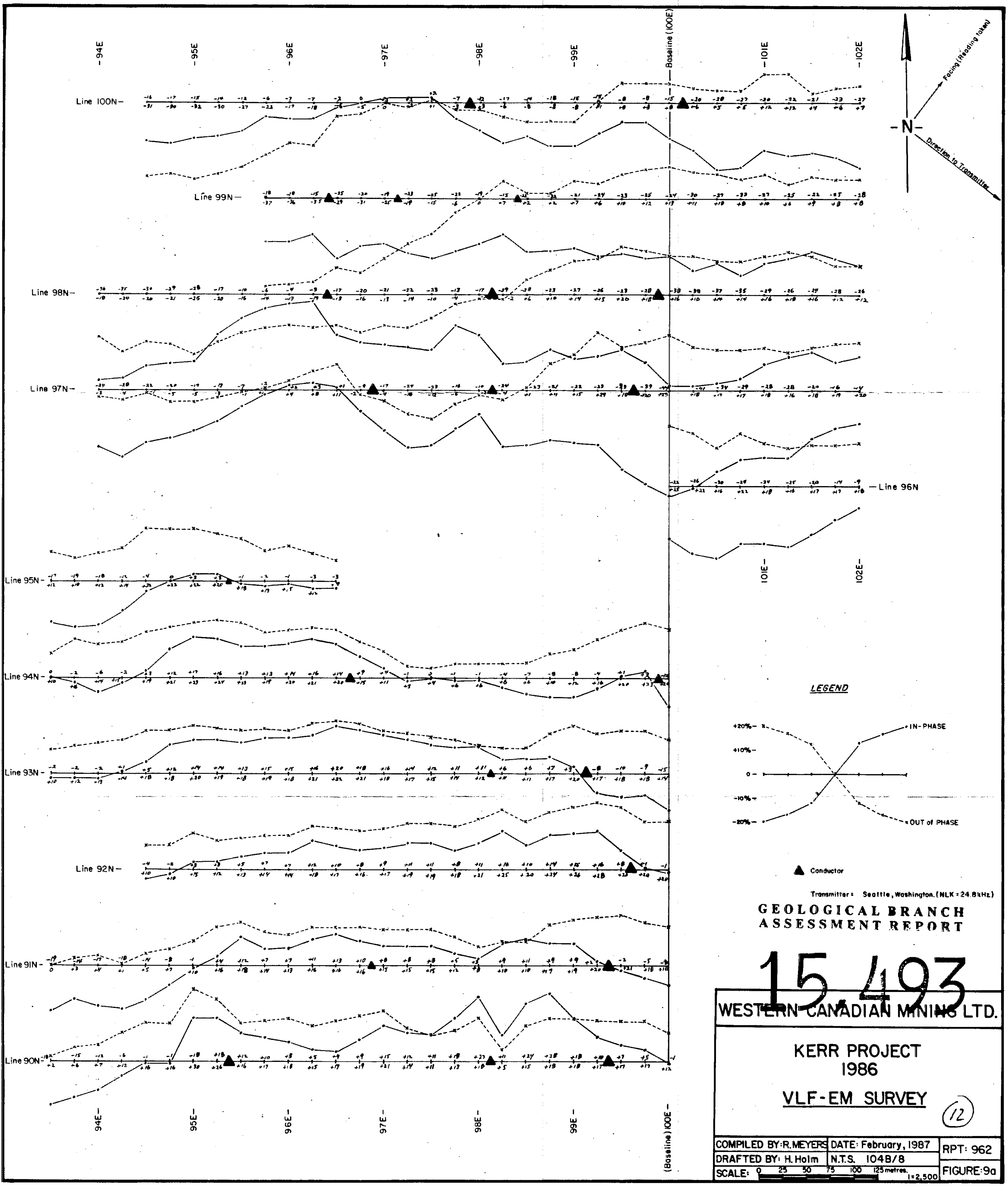
(8)

DRAWN BY B.H.W., S.C.	DATE Oct., 1986
DRAFTED BY H.H.	N.T.S. 104 B/8
REPORT No. 962	FIGURE No. 7c

ZONE D
ZONE C
TRENCH 11
TRENCH 12
TRENCH 14
TRENCH 1
BASELINE (100E)
DDH 3
DDH2
SNOW
Line 103N
Line 102.5N
Line 102N
Line 101.5N
Line 101N
92.5E
93E
94E
95E
96E
97E
98E
99E
103N
102.5N
102N
101.5N
101N
421,500E
420,000E
6,259,000N
1350m
1400m
1450m
1500m
1550m
1600m
1650m
+1619m.
1634m.+
Upper Lake
N
LEGEND
Soil Sample
Talus Sample
Rock Chip Sample Interval
NOTE - Zone C trenching in 1985.
- Zone D rock chip lines - 1986.
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,493
WESTERN CANADIAN MINING LTD.
1986
- KERR PROJECT -
ZONES C&D
SAMPLE LOCATIONS
9
COMPILED BY: R.M., S.C.
DATE: December, 1986
DRAFTED BY: H.H.
N.T.S.: 104B/8
RPT. No. 962
SCALE: 0 10 20 30 40 50 metres 1:1,000
FIGURE: 8a


N
421,500E
420,000E
6,259,000N
ZONE C
ZONE D
TRENCH 1
TRENCH 11
TRENCH 12
TRENCH 14
DDH 2
DDH 3
BASELINE (100E)
Line 103N
Line 102.5N
Line 102N
Line 101.5N
Line 101N
SNOW
1350m
1400m
1450m
1500m
1550m
1600m
1650m
+1619m.
1634m.+
Upper Lake
AVERAGE OF THREE ASSAY VALUES = 5.75OZ./ton.
LEGEND
Soil Sample
Talus Sample
Rock Chip Sample Interval
NOTE - Zone C trenching in 1985.
- Zone D rock chip lines - 1986.
GEOLOGICAL BRANCH ASSESSMENT REPORT
15,493
WESTERN CANADIAN MINING LTD.
1986
- KERR PROJECT -
ZONES C&D
GOLD GEOCHEMISTRY in PPB.
10
COMPILED BY: R.M., S.C.
DATE: December, 1986
DRAFTED BY: H.H.
N.T.S.: 104B/8
SCALE: 0 10 20 30 40 50 metres 1:1,000
RPT. No. 962
FIGURE: 8b

421,500E
420,000E
6,259,000N
6,259,000N
ZONE D
ZONE C
SNOW
TRENCH 1
TRENCH 11
TRENCH 12
TRENCH 14
DDH 2
DDH 3
BASE LINE (100E)
Line 103N
Line 102.5N
Line 102N
Line 101.5N
Line 101N
1350m
1400m
1450m
1500m
1550m
1600m
1650m
+1619m
1634m+
Upper Lake
LEGEND
Soil Sample
Talus Sample
Rock Chip Sample Interval
NOTE - Zone C trenching in 1985.
- Zone D rock chip lines - 1986.
N
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,493
WESTERN CANADIAN MINING LTD.
1986
- KERR PROJECT -
ZONES C&D
SILVER GEOCHEMISTRY
in PPM.
COMPILED BY R.M., S.C.
DRAFTED BY: H.H.
DATE: December, 1986
N.T.S.: 104B/8
SCALE 0 10 20 30 40 50 metres 1:1,000
RPT. No. 962
FIGURE: 8c



GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,493

WESTERN CANADIAN MINING LTD.

KERR PROJECT
1986

VLF-EM SURVEY

(12)

COMPILED BY: R. MEYERS	DATE: February, 1987	RPT: 962
DRAFTED BY: H. Holm	N.T.S. 104B/8	
SCALE: 0 25 50 75 100 125 metres 1:2,500		FIGURE: 9a


N
ZONE D
ZONE C
ZONE L
ZONE B
ZONE A
ZONE F
Lake
+ 1619
1634
+1916
+1922
Line 103N
Line 102.5N
Line 102N
Line 101.5N
Line 101N
Line 100N
-L100N
Line 99N
Line 98N
Line 97N
Line 96N
Line 94N
Line 93N
Line 92N
Line 91N
Line 90N
Line 89N
Line 88N
Baseline
1250
1300
1350
1400
1450
1500
1550
1600
1650
1700
1750
1800
1850
1900
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,493
Note:- Topographic contours in metres.
NOTES
Station with magnetic field value in nanoteslas.
Contours at 50 nanotesla intervals. (from -50 to 350)
Instrument = McPhar M-700 Fluxgate Magnetometer.
SCALE 0 25 50 75 100 125 metres
1:2,500
WESTERN CANADIAN MINING LTD.
1986
KERR PROJECT
GROUND MAGNETICS
Zones A,B,C,D,E,F,L
(13)
DRAWN BY: R.M., S.C., H.H.
DATE: OCTOBER, 1986
DRAFTED BY: H. HOLM
N.T.S. 104B/8
REPORT No. 962
FIGURE NO. 9b