47-54-15555
2/88

GEOCHEMICAL, GEOPHYSICAL, AND PHYSICAL WORK

REPORT

ON THE BRENDA GROUP OF MINERAL

CLAIMS CONSISTING OF:

THE

BRENDA 1,4,5,6,7,8 2 POST CLAIMS 6 UNITS TOTAL
RECORD No.s 2822,2825,2826,2827,2828,2829,

JAN 1 MINERAL CLAIM 6 UNITS TOTAL RECORD NO. 6098

JAN 2 MINERAL CLAIM 16 UNITS TOTAL RECORD NO. 6099

JAN 3 MINERAL CLAIM 9 UNITS TOTAL RECORD NO. 6125

JAN 4 MINERAL CLAIM 6 UNITS TOTAL RECORD NO. 6126

JAN 5 MINERAL CLAIM 20 UNITS TOTAL RECORD NO. 6127

JAN 6 MINERAL CLAIM 4 UNITS TOTAL RECORD NO. 7499

JAN 7 MINERAL CLAIM 20 UNITS TOTAL RECORD NO. 7500

JAN 8 MINERAL CLAIM 10 UNITS TOTAL RECORD NO. 7501

MAX 2 POST CLAIMS 3 UNITS TOTAL
RECORD NO.s 6623,6624,6625

LOCATED IN THE OMINECA MINING DIVISION
OF BRITISH COLUMBIA

N.T.S. : 94E/7W, 94E/2W

LATITUDE : 57 DEGREES ~~16~~ 15.3 MINUTES NORTH

LONGITUTE: 126 DEGREES ~~54~~ 53.6 MINUTES WEST

WORK APPLIED TO: ALL OF THE ABOVE CLAIMS

OWNER AND OPERATOR

CANASIL RESOURCES INCORPORATED
1695 MARINE DRIVE
NORTH VANCOUVER, B.C.

PREPARED BY: Paul Weishaupt *P.J. Weishaupt*

Richard Weishaupt *R. Weishaupt*

DATE SUBMITTED: FEB. 12. 1987

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INTRODUCTION AND SUMMARY

The purpose of the surveys was to test the effectiveness of the EMR-16 in tracing out silicified zones of quartz-chalcedony breccias located by prospecting. The geochemical soil sampling survey was conducted over the zones which in some cases host gold-silver mineralization. These surveys, along with the physical work performed, proved the presents of gold and silver mineralization throughout the property. For the purpose of this report the property has been divided up into three map areas, (see 86-8) these map areas are refered to as area 1, area 2, and area 3 throughout the report.

LOCATION AND ACCESS

The Brenda Group of claims lie along and south of Jock Creek which flows easterly and northerly into the Toodoggone River in the Omineca Mining Division. The center of the claim group is at latitude 57 degrees 15 minutes North, longitude 126 degrees 53 minutes West and on N.T.S. sheets 94E/7W and 94E/2W. Elevations range from 1200 meters in the Jock Creek valley to 1800 meters on the peaks to the South.The lower parts of the valleys are lightly timbered with spruce and pine, and uplands are bare rock or talus.

Current work is supported by helicopter flight to landing sites on the claim group from the newly constructed air strip on the Sturdee River. This airstrip is suitable for landing by Hercules aircraft. This airstrip lies about 15 km Southwest of the property and forms the base for helicopters working in the Toodoggone area during the summer season.

INTRODUCTION CONT.

CLIMATE

The climate of the Brenda Claim Group is severe. Winter temperatures fall to about -40 degrees Celsius for short periods between November and March, while summer temperatures can rise to +30 degrees Celsius. The typical northern interior British Columbia climate limits the field season to about five months from mid May to mid October due to frost and snow. The area is generally snow-free from June to September. Total precipitation in the area is about 1.0 meter.

CLAIMS AND HOW HELD

The property is held under a property option agreement with Canmine Development Company Inc. dated the 7th day of February, 1986. Canmine has agreed to grant to Canasil Resources Inc. an option to purchase an undivided 100% interest in the property, in consideration of $150,000 over a period of five years. The property consists of 19 claims. Details as on record at Vancouver Mine Records Office are listed on the following page:

INTRODUCTION CONT

CLAIMS AND HOW HELD CONT.

Claim Name	No. of Units	Record No.	Owner/Operator
BRENDA 1	2PC	2822 (6)	CANASIL RESOURCES INC.
BRENDA 2	2PC	2823 (6)	" " "
BRENDA 3	2PC	2824 (6)	" " "
BRENDA 4	2PC	2825 (6)	" " "
BRENDA 5	2PC	2826 (6)	" " "
BRENDA 6	2PC	2827 (6)	CANASIL RESOURCES INC.
BRENDA 7	2PC	2828 (6)	" " "
BRENDA 8	2PC	2829 (6)	" " "
JAN 1	6	6098 (3)	CANASIL RESOURCES INC.
JAN 2	16	6099 (3)	" " "
JAN 3	9	6125 (4)	" " "
JAN 4	6	6126 (4)	" " "
JAN 5	20	6127 (4)	" " "
JAN 6	4	7499 (2)	" " "
JAN 7	20	7500 (2)	" " "
JAN 8	10	7501 (2)	" " "
MAX 1	2PC	6623 (8)	CANASIL RESOURCES INC.
MAX 2	2PC	6624 (8)	" " "
MAX 3	2PC	6625 (8)	" " "

2PC Indicates a 2 post claim.

The claims were transferred to Canasil Resources Inc. by Bill of Sale 233816 on April 11, 1986.

HISTORY

In 1950 and 1951, Bralorne Mines Ltd. engaged Mr. E. Bronlund to prospect the Toodoggone Area for possible gold-silver mineralization. Quartz floats of gold-silver mineralization were located on the present claim group. In 1969 Kennco Exploration conducted an exploration program on the Pillar Claims, which now form parts of the Brenda Group of claims. In 1980, P.J. Weishaupt caused the first eight claims to be staked (Brenda 1-8).

INTRODUCTION CONT.

REGIONAL GEOLOGY

The regional geology of the area covered by the Brenda group is provided by open File Map 483 and Preliminary Map G1 of the Geological Survey of Canada. These maps indicate that rock outcroppings are part of the sequence of mesozoic rocks which extend through the Toodoggone area with a Northwest direction. A regional fault with the same trend has been traced for over 50 km from Spruce Hill to a point at the headwaters of Jock Creek about 8 km above the claim group. Its continuation through the Brenda Group along this part of Jock Creek can be inferred. Other valley structures follow to cross the Finlay River and in 25 km to converge into the Finlay fault. Rock exposures Northeast of the fault are determined as Hazelton Group rocks of lower jurassic age and of mainly sedimentary origin. Those to the Southwest are volcanic formations.The Toodoggone formation are of middle jurassic age and the Takla group of late triassic age. The Toodoggone volcanic rocks rest structurally on the Takla formation. On the Brenda group and near by two granodiorite intrusive masses one kilometer or more in diameter have been mapped. The Toodoggone formation along with Takla group volcanics, host most of the known precious metal prospects to date in the district.

INTRODUTION CONT.

REGIONAL GEOLOGY

The gold-silver occurences are localized by fault and cross fracture structures with hot springs type of alteration and related bleaching. Alteration suites are typical of epithermal deposits with internal silicification, clay minerals and locally alunite, grading outward to sericite and clay minerals, chloride epidote and pyrite. These deposits comprise fissure veins, quartz chalcedony stock works, breccia zones and areas of silicification in which principle ore minerals are fine grained argentite, electrum, native gold and silver with lesser chalcopyrite, galena and sphalerite.

PROPERTY GEOLOGY

The areas in which the surveys were conducted are underlain by Toodoggone and Takla volcanic rocks and intrusive dikes related to the Toodoggone volcanism. The upper Triassic Takla volcanic rocks are characterized by dark green augite and white lath shaped plagioclase phenocrysts in a dark green ground mass. Mafic minerals are pervasively altered to chlorite, probably as a result of lower green schist facies metamorphism. The phenocrysts range in size from very coarse to fine grained.

PROPERTY GEOLOGY CONT.

The lower jurasic Toodoggone volcanic rocks appear to fall into two groups in this area:

Group 1: having feldspar and hornblende phenocrysts
Group 2: having feldspar, quartz, hornblende and biotite phenocrysts.

Feldspar-hornblende porphyries include dikes which intrude Takla and possibly the quartz-bearing Toodoggone volcanics.

The feldspar is orange-coloured and may be either plagioclase with hematite dust or sanidine. These volcanics are similar to trachy andesite-trachyte sequences mapped elsewhere in the Toodoggone District, for example the hanging wall sequence, Amethyst Breccia Zone, and the Lawyers property.

A moderately welded crystal lapilli tuff outcrops on the cliffs at the head of the valley. This unit contains approximately 30% flattened lapilli-sized fragments in feldspar and hornblende phenocrysts similar in appearance to those in the dikes. Lapilli ground mass is preferentially altered to chlorite, and epidote fracture fillings are common.

PROPERTY GEOLOGY CONT.

The quartz-bearing Toodoggone volcanics and volcanic clastics in this area include crystal tuffs, crystal lapilli tuffs, tuff breccia, greywacke and siltstone. The volcanics are similar in appearance to quartz-feldspar crystal tuffs on the Newmont Shasta and Serem Jock claims. Overall composition is andesitic to dacitic, with feldspar being mainly plagioclase. The sediments appear to be restricted to a small area, they exhibit graded bedding and poor to moderate sorting.

The exact nature of the Toodoggone/Takla contact has not yet been determined. Elsewhere in the region, both unconformities, where the Toodoggone volcanics have been extruded onto an eroded Takla surface, and fault contacts have been observed, the observed shearing in the Takla suggests a fault contact. A traverse was made across the intrusive located on the JAN 1 Claim. A suite of rocks were collected. The bulk of the intrusion appears to be a quartz monozonite intruded by fine grained monzonite to syenite dikes. These rocks are probably the intrusive equivalents of the Toodoggone volcanics.

INTRODUTION CONT.

ALTERATION AND MINERALIZATION

Two showings on the claim group were examined. A large area of quartz-chalcedony breccia in outcrop and float called the Tarn showing was discovered by prospecting up the right split of the left fork of Red Creek. Float Sample No. 746: Au 1.87 oz/ton, Ag 102.0 oz/ton was located in this area in 1951. Quartz-chalcedony breccia float is particularly abundant approximately 60 meters Northeast of the Tarn Lake. This area is snow-covered most of the year, one snow patch 50 by 20 meters in the middle of the float area still remained in late August. Examination of the outcrop above the quartz float indicates that the float is probably in place and the breccia narrows into veinlets in outcrops. Resistivity readings also support this. Quartz-chalcedony breccia and veins are quite extensive. Initial prospecting of outcrop and frostheave indicated silicification over an exposed area at least 200 meters long and 40 to 60 meters wide.

The veins consist of colourless to white or light grey quartz and chalcedony. Banding indicates multiple-stage silicification and cockscomb quartz indicates open space fracture filling. Late-stage calcite occurs in the centers of some veins. Rebrecciation and silicification is indicated by cross-cutting textures.

INTRODUTION CONT.

ALTERATION AND MINERALIZATION CONT.

Several pulses of mineralizing fluids are required for the concentration of gold and silver, these multiple-stage silicification features are therefore favourable for the formation of ore grade mineralization. These textures are also observed in Serem's AGB and Cliff Creek zones, the Baker Mine veins and the Shasta showings.

The veins contain euhedral pyrite or limonite boxworks forming less than 1% to 10%. Minor amounts of base metal sulphides (chalcopyrite, galene, sphalerite) occur in some veins. The wall rocks have been pyritized in places, iron rich minerals are replaced by pyrite. Argillic alteration occurs as a result of pyrite breakdown and sulphuric acid leaching. It is difficult to distinguish between hypogene and supergene argillic alteration. Generally the supergene alteration has the effect of widening the argillic alteration envelopes.

Epidote fracture filling are extensive and form a wide envelope around the quartz-chalcedony breccia zones. Calcic plagioclase and lapilli are commonly altered to epidote. Epidote alteration and pyritization are common throughout the basin and are probably related to an underlying or adjacent intrusion. However, there is a distinct concentration of epidote and pyrite in the quartz-chalcedony breccia zones.

INTRODUTION CONT.

ALTERATION AND MINERALIZATION CONT.

Intense hematization occurs in several places. Detailed mapping is required to trace this alteration and determine where it is related to a syngenetic event, or the epithermal system which produced the quartz breccia and epidote/pyrite alteration.

Chalcopyrite mineralization occurs in narrow quartz-epidote fractures filling in the intrusion. Potassic feldspar alteration is common, it is pervasive adjacent to and within the fine grained dikes. The border of the intrusion is pyritized.

Skarn and limestone floats, derived from the cliffs above occur at the head of the valley. The skarn contains chalcopyrite, galena and sphalerite. One sheared sample contains abundant molybdenite and graphite.

WORK DONE

The following described work is to be applied to the BRENDA GROUP of Claims consisting of:

CLAIM NAME		No. OF UNITS	RECORD No.		OWNER/OPERATOR
BRENDA	1	1	2822	(6)	CANASIL RESOURCES
BRENDA	4	1	2825	(6)	CANASIL RESOURCES
BRENDA	5	1	2826	(6)	CANASIL RESOURCES
BRENDA	6	1	2827	(6)	CANASIL RESOURCES
BRENDA	7	1	2828	(6)	CANASIL RESOURCES
BRENDA	8	1	2829	(6)	CANASIL RESOURCES
JAN	1	6	6098	(3)	CANASIL RESOURCES
JAN	2	16	6099	(3)	CANASIL RESOURCES
JAN	3	9	6125	(4)	CANASIL RESOURCES
JAN	4	6	6126	(4)	CANASIL RESOURCES
JAN	5	20	6127	(4)	CANASIL RESOURCES
JAN	6	4	7499	(2)	CANASIL RESOURCES
JAN	7	20	7500	(2)	CANASIL RESOURCES
JAN	8	10	7501	(2)	CANASIL RESOURCES
MAX	1	1	6623	(8)	CANASIL RESOURCES
MAX	2	1	6624	(8)	CANASIL RESOURCES
MAX	3	1	6625	(8)	CANASIL RESOURCES

GEOPHYSICAL SURVEY

A geophysical survey was conducted in areas 1 and 2 using a Geonics EMR-16. A total of 1776 readings were obtained, utilizing 888 stations.

TEST SURVEY

A test survey was carried out in area 1 at grid location 1+25SE 1+00SW. This was the initial EMR-16 survey and was performed to determine which transmitting stations were appropriate, and the workability of this particular geophysical instrument in this particular area.

The base line ran due east and west with perpendicular cross lines running due north and south. 10 meter lines were used with stations every 10 meters. Lines were surveyed with brunton and chain and stations were flagged with the appropriate station number mark on each flag with a black marker. This survey determined that this particular instrument (EMR-16) is usefull in this area when using Hawaii and Seattle as transmitting stations. A total of 45 stations were used resulting in 90 readings. These results are included on map 86-1 and 86-2.

GEOPHYSICAL SURVEY CONT.

GRID SYSTEM

Control for the grid system was by Brunton and chain. All lines were picketed every 20 meters, writing the station number on the picket. The survey lines were set perpendicular to the baseline, using a Brunton and backsight for control, and likewise picketed every 20 meters. A square grid pattern was used to avoid introducing a bias in the data.

In map area 1 all cross lines, North 30 degrees East - South 30 degrees West were clear cut with axe and power saw. 5.34 km of baseline and cross lines were surveyed resulting in 482 stations.

In map area 2 the baseline was set at an azimuth of 060 degrees and picketed every 20 meters with cross lines perpendicular to the baseline. A total of 6.07 km of baseline and cross lines were surveyed with 406 stations.

The grid system was used for a soils sampling survey in area 1 and a geological survey in areas 1 and 2.

GEOPHYSICAL SURVEY CONT.

INSTRUMENT AND PROCEDURE

The instrument used is a Geonics EMR-16. It consist of a VLF (very low frequency) EM receiver with a resistivity unit attached. Two probes connected to the instrument by a cable are inserted in the ground ten meters apart. These measure the electric field between the probes and a coil in the instrument measures the magnetic field perpendicular to the electric field. The apparent resistivity is a ratio of the magnitude of the two fields. This can be mathematically expressed as follows:

$$pa = \frac{1}{uw} - \left(\frac{Ex}{Hy}\right) 2$$

where pa = apparent resistivity in ohm-meters
Ex = horizontal components of the radial electric field (the field between the probes)
Hy = vertical component of the tangential magnetic field (perpendicular to the electrical field)
u = the magnetic permeablilty of the medium
w = the angular frequency of the signal 2-f where f is the frequency in hertz (Scott, 1974)

The phase difference between Ex and Hy is also measured in degrees. A phase angle of 45 degrees indicates homogeneous conditions down to the depth of penetration (skin depth). When two layers are present, the phase angle will generally decrease if the lower layer is more resistive, and increase if it is more conductive.

GEOPHYSICAL SURVEY CONT.

INSTRUMENT AND PROCEDURE

The effective depth of penetration depends on the electrical resistivity and very slightly on the transmitter frequency. Surveys conducted on the Shasta claims which have very similar geology to the Jan claims indicate skin depth variation from 35 to 350 meters, with a general estimated skin depth of 40 to 60 meters in unaltered rock. (Limion and Downing, 1984)

When variations in geology are horizontal (e.g. conductive overburden over resistive bedrock) it is possible to use the phase angle reading to calculate the respective resistivities of two layers. However, the quartz and breccias on these claims are vertical to subvertical and the effect of the phase angle is difficult to quantify. Therefore the pa measurements have been plotted without phase angle corrections. The measurements are taken by the following method: A transmitting station is selected and the selection switches on the EM-16 and attached resistivity unit are tuned to that station. The instrument is set in the "16" mode and the coil is oriented towards the station. Station direction is determined by tuning the instrument back and forth until the audio signal is nulled.

INSTRUMENT AND PROCEDURE

The probes,which are attached to the resistivity unit by a cable, are inserted in the ground 10 meters apart in line with the signal direction. It is important to have good contacts, preferably in moist soil. The mode switch is then flipped to "16R" with the instrument coil still oriented towards the station. The signal is then further nulled by tuning the EM quadrature dial and the EMR phase angle dial back and forth. There are three scales 10X, 100X, and 1000X. The apparent resistivity is read from the quadrature dial (the number across from the red "0" is multiplied by the scale factor). The phase angle is read directly from the phase angle dial.

In choosing a transmitting station, one has to consider orientation with respect to geology, audio signal strength and hours of transmitter operation. The preferred direction is across the strike of the resistive zone (in contrast to an EM survey, where the preferred direction is along the strike).

Where the strike is unknown or uncertain, it is preferable to take readings on more than one station. The instrument is designed to use two stations conveniently.

GEOPHYSICAL SURVEY CONT.

INSRUMENT AND PROCEDURE

In this survey NLK Seattle, Washington (18.6 KHz) and NPM Lualvalei, Hawaii (23.4 KHz) were used. The azimuth of the Seattle signal is approximately 155 degrees and that of Hawaii aproximately 235 degrees. No major variations in signal orientation were detected. Seattle signal strength is strong and it is relatively easy to pinpoint the null positions, whereas Hawaii signal strength is weak and the null positions sometimes have to be estimated. The Seattle transmitter is shut down for maintenance on Thursday (1600 to 2400 UT, 1500 to 2300 UT daylight savings time) and the Hawaii transmitter on Wednesday and Thursday (1800 to 0200 UT)

INTERPRETATION

Results are plotted on maps 86-1 and 86-2 for area 1, and on 86-3 and 86-4 for area 2.

Values are contoured at 500 ohm-meter intervals to 2000 ohm-meters. Values above 2000 ohm-meters are contoured at 1000 ohm meter intervals.

GEOPHYSICAL SURVEY CONT.

INTERPRETATION

High resistivity values correspond in general to silicified zones. Values greater than 2000 ohm-meters are arbitrarily designated as high.

Further geological work is required to determine a more accurate correspondence between rock and alteratin types and resistivity values, however the 2000 ohm contour is considered realistic.

Comparison of the Seattle and Hawaii maps shows a bias introduced by the station direction. In some areas, one station will read low while the other reads high. This suggests that readings should be taken on both stations whenever possible. Apparently the readings are strongly affected by the relative orientations of the siliceous zones and the station directions.

In many areas, high resistivity zones are only one or two stations wide. This indicates the necessity of closely-spaced readings (e.g. no more than twenty meters apart). For detailed targetting, ten meter intervals are recommended.

GEOPHYSICAL SURVEY CONT.

INTERPRETATION

The survey conducted near the Takla vein in area 2 produced a strong multi-station anomaly with resistivity values ranging from 2000ohm-m to 3500ohm-m down strike of the outcropping vein This anomaly is only evident while using the Seattle orientation. Further to the north west approximatly 80 m there is a persistent anomaly approximatly 140 by 20 meters in dimention with values ranging from 2000-4500 ohm-m. This anomaly is evident using both the Hawaii and Seattle orientations.

The effect of silicification on resistivity is probably offset by the high pyrite (greater than 25%) content of the wall rock. The presence of ferricrete does not appear to affect resistivity readings.

The survey conducted in area one produced a very consistent anomaly with a length of 380 meters and width of 25 meters, utilizing approximately 28 stations with resistivity values ranging from 1500 to 6000 ohm-meters. This particular anomaly is evident on both the Seattle and Hawaii orientation maps, possibly indicating a narrow silicified zone at depth.

GEOCHEMICAL SURVEY

A geochemical survey was carried out in area one, obtaining 189 soil samples from 189 picket stations.

FIELD PROCEDURE

One hundred and eighty nine soil samples were collected at 20 meter intervals along the control grid of area one. Holes were dug with a shovel and the B horizon sampled. The samples were collected in 10 cm by 25 cm kraft paper sample envelopes, which were filled to capacity by the sample.

All samples were sent to Acme Analytical Laboratories Ltd. of Vancouver, B.C. for analysis: The soil samples were analysed by ICP with the exception of gold (Au) where the AA method was used. (See Appendix E)

SAMPLE ANALYSIS

Assay sheets are located in appendix A. The arithmetic mean was calculated for both gold (Au) and silver (Ag) on all soil samples in area one.

ELEMENT	ARITHMETIC MEAN
Au	24 ppb
Ag	1.4 ppm

GEOCHEMICAL SURVEY CONT.

SAMPLE ANALYSIS

The enclosed maps (86-6, 86-7) show the geochemical assay values at each station. Contours were drawn at 25, 50, +100 ppb for gold and 2,3, +4 ppm for silver.

INTERPRETATION

All gold values greater than 50 ppb are concidered anomalous and are detailed on drawing 86-7. All anomalous silver values, greater than 4 ppm, are detailed on drawing 86-6. The anomalies occur at random over the grid area with no or poor correlation between gold and silver values. However taking into consideration resistivity values, topograpgy, geology, and geochem values, certain gold-silver bearing structures can be inferred. Using this method various structures have been interpreted so far, but further ground work is required to justify these interpretations.

PHYSICAL WORK

A detailed prospecting, trenching, sampling, and test hole diamond drilling program was also carried out in conjuntion with the geophysical and geochemical surveys previously mentioned in this report.

PHYSICAL WORK CONT.

AREA 1

Prospecting was systematicly carried out along the pre-cut grid lines and particularly in areas of high geophysical and geochemical values. Once these targets areas were defined further follow-up work, such as trenching,test hole drilling and sampling was carried out.

In area 1 there were three main areas investigated thoroughly these areas lie at grid locations :

0+64 SE 0+27 NE
1+50 SE 0+10 SW
2+50 SE 0+60 SW

A total of eighty square meters was hand trenched along with over sixty meters of test hole drilling, using the J.K.Smit Winkie Diamond Drill. 35 rock samples were collected from this area with values ranging from 0.4-135.5 ppm for silver and 1-640 ppb for gold. See figure 1,2 and drawing 86-5.

AREA 2

Two main area were investigated in area 2,(see figure 3, 86-8) located at grid locations:

0+30S 0+00W
1+10W 4+00S

A total of seventy square meters of hand trenching including fifty meters of test hole drilling was completed. 18 rock samples were collected insitue from area 2 with values ranging from 5-51000 ppb for gold and 0.1-314 ppm for silver.

PHYSICAL WORK CONT.

GENERAL

Prospecting and sampling was done over geologically interesting areas in the remainder of the claim group. A total of 12 float samples were assayed as well as 48 silt and soil samples obtained from various areas in the claim group.(see 86-8)

INTERPRETATION

From the general and detailed exploration work carried out on the claim group it is evident that there area a variety of gold and silver bearing structures on the property.

CONCLUSION

In our surveys and geological investigation of areas one and two, we discovered similarities to the settings of the Lawyers deposits, the Baker Mine and the Shasta showings. Banded chalcedony quartz breccia occurs in both Toodoggone and Takla volcanic rocks. Further investigation should include both units. The Baker deposit is proof that mineralization can occur in Takla volcanics, in spite of the current general attitude of exploring only Toodoggone rocks. Previous sampling in areas one and two, have also indicated gold-silver mineralization in both units. The potential of locating several zones of mineralization in the claim area is excellent. Past experience on other claims in the Toodoggone District indicates that where there is one zone, there are more. Geochemical sampling to date on the claims support this possibility. Numerous geochemical gold and silver anomalies have been located to date on the Brenda Group of claims.

APPENDIX A

ASSAYS

AC[illegible] ANALYTICAL LABORATORIES LTD.
8[illegible]E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: JULY 8 1986

DATE REPORT MAILED: July 12/86..

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL -80 MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: D Toye .DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-1356

SAMPLE#	Ag PPM	Au* PPB
G1-1	.1	9
G1-2	.1	4
G1-3	.1	16
G1-4	.2	5
G1-5	.5	27
G1-6	.1	7
G1-7	.1	2
G1-8	1.2	6
G1-9	.3	8
G1-10	.3	7
G1-11	.3	32
G1-12	.2	5
G1-13	.6	13
G1-14	.4	20
G1-15	.6	20
G1-16	.5	5
G1-17	.5	9
G1-18	.5	90
G1-19	.4	6
G1-20	.2	2
G1-21	.5	25
G1-22	.3	10
G1-23	.1	6
G1-24	.6	4
G1-25	.6	3
G1-26	.6	15
86R-1	.1	4
86R-2	1.0	26
86R-3	.7	10
86R-4	.7	5
86R-5	.3	4
86R-6	.8	7
86R-7	.5	8
86R-8	.4	80
86R-9	.5	6
86R-10	.3	6
STD C/AU 0.5	7.0	500

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
86R-11	-	-	-	1.0	-	19
86R-12	-	-	-	1.1	-	21
86R-13	-	-	-	.3	-	4
86R-14	-	-	-	.2	-	4
86R-15	-	-	-	.4	-	4
86R-16	-	-	-	.3	-	3
86R-17	-	-	-	.6	-	1
86R-18	-	-	-	.3	-	7
1SE 0+20SW	35	56	206	1.7	6	13
1SE 0+40SW	29	40	207	1.8	2	7
1SE 0+60SW	106	738	166	7.3	18	8
1SE 0+80SW	82	431	289	7.9	3	7
1SE 1+00SW	55	277	184	1.7	11	7
1SE 1+20SW	232	942	146	2.6	6	4
1SE 1+40SW	30	145	106	.8	6	16
1SE 1+60SW	34	85	94	1.6	5	16
1SE 1+80SW	51	126	141	1.3	12	5
1SE 2+00SW	38	87	118	.5	12	1
1SE 2+20SW	56	93	143	1.3	2	7
1SE 2+40SW	41	84	111	.4	11	6
1SE 2+60SW	52	77	158	1.2	8	5
1SE 2+80SW	48	66	145	2.4	8	5
1SE 3+00SW	31	68	83	1.3	15	6
1SE 3+20SW	35	86	87	.9	2	7
1SE 3+40SW	44	57	118	.6	4	11
1SE 3+60SW	53	74	282	1.8	13	9
STD C/AU-0.5	60	39	138	7.1	42	485

AC'¯ ANALYTICAL LABORATORIES LTD.
85▬E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: JULY 15 1986

DATE REPORT MAILED: July 18/86

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS & SILTS -80 MESH & ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: D. Toye. DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-1488

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
0+00SE 1+20SW	59	64	177	.3	5	110
0+00SE 1+40SW	46	47	132	1.1	3	6
0+00SE 1+60SW	48	55	131	.1	2	29
0+00SE 1+80SW	41	53	136	.9	7	12
0+00SE 2+00SW	60	62	130	2.7	9	17
0+50SE 1+20SW	42	38	124	.7	7	3
0+50SE 1+40SW	46	65	127	1.3	2	4
0+50SE 1+60SW	28	38	83	.4	3	3
0+50SE 1+80SW	39	47	120	.7	9	70
0+50SE 2+00SW	43	49	157	.7	4	9
1+50SE 1+20SW	97	964	172	4.6	5	9
1+50SE 1+40SW	43	491	99	10.2	5	20
1+50SE 1+60SW	53	59	166	.6	5	10
1+50SE 1+80SW	48	64	137	.9	7	12
2+00SE 0+80NE	77	45	348	1.0	9	3
2+00SE 0+60NE	172	89	376	.3	2	5
2+00SE 0+40NE	26	53	90	.6	4	5
2+00SE 1+20SW	113	208	84	1.3	5	12
2+00SE 1+40SW	73	229	94	1.7	7	18
2+00SE 1+60SW	61	185	86	2.2	16	26
2+00SE 1+80SW	42	72	100	1.4	3	8
2+00SE 2+00SW	67	59	131	.8	7	10
SR-1	114	39	445	8.0	8	3
SR-2	79	19	161	3.0	16	9
SR-3	19	12	89	.4	11	1
SR-4	9	14	102	.2	15	1
SSR-1	35	17	173	.2	9	6
SSR-2	32	15	177	.1	9	4
SSR-3	27	14	156	.1	3	1
SSR-4	27	11	169	.1	3	1
SSR-5	33	19	181	.2	5	5
SSR-6	34	17	166	.2	10	2
SSR-7	37	22	168	.2	8	1
SSR-8	28	12	150	.4	5	3
1304	13	7	43	.4	8	5
STD C/AU-0.5	61	42	142	7.1	40	490

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-ROCKS P2-3 SOILS -80MESH AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JUL 28 1986 DATE REPORT MAILED: Aug 1/86 ASSAYER.. D.Toye. DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-1692 PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
X 1305	1	23	12	107	86.5 ✓	1	7	2128	.83	19	5	ND	3	53	1	2	2	35	11.41	.009	4	2	.40	11	.02	2	.34	.01	.01	1	160
X 1306	1	19	7	77	4.9	1	4	1600	1.76	12	5	ND	2	35	1	2	2	67	7.75	.035	8	3	.36	19	.06	2	.32	.01	.05	1	3
X 1307	1	21	3	59	2.7	1	4	814	1.42	7	5	ND	1	9	1	2	2	53	2.27	.023	4	3	.42	16	.04	2	.36	.01	.04	1	10
X 1308	1	16	3	57	1.8	1	3	596	1.52	6	5	ND	1	6	1	2	3	59	.62	.025	5	4	.39	16	.06	2	.41	.01	.05	1	6
X 1309	1	12	5	53	.6	2	6	658	2.62	9	5	ND	1	10	1	2	2	117	.73	.054	11	5	.36	36	.13	3	.47	.01	.10	1	1
X 1342	1	9	12	64	.1	1	4	1418	3.23	18	5	ND	1	29	1	2	3	50	.43	.088	5	3	1.73	32	.14	3	1.55	.13	.07	1	2
X 1343	2	19	6	279	.1	1	4	1674	.88	4	5	ND	3	93	3	2	2	4	.72	.011	15	1	.17	1311	.01	2	.35	.03	.09	1	1
X 1344	69	210	584	420	28.0	1	9	56	1.73	14	5	ND	1	7	3	5	6	1	.01	.006	7	2	.01	158	.01	2	.06	.01	.04	1	255
55830	68	197	130	4521	298.1 ✓	1	9	43	2.02	187	5	15	1	3	49	2	2	7	.02	.002	3	3	.01	37	.03	2	.14	.01	.09	1	17000 ✓
55831	5	11	5	24	.7	6	3	300	.96	2	5	ND	2	53	1	2	2	33	1.28	.063	6	43	.58	126	.07	2	1.63	.10	.05	2	27
55832	50	7	7	16	8.6	2	2	55	1.76	6	5	ND	1	3	1	2	2	3	.03	.013	2	3	.02	36	.03	2	.15	.01	.10	1	85
STD C/AU 0.5	21	57	42	134	6.9	68	30	1082	3.94	39	18	8	33	47	17	15	19	63	.48	.104	40	59	.88	176	.08	37	1.72	.06	.13	13	500

✓ Assay required for correct result

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
0+50SE 0+20NE	4	70	107	224	2.2	15	8	592	5.74	12	5	ND	4	35	1	2	2	75	.13	.081	10	29	.56	149	.07	2	2.56	.01	.06	1
1+50SE 0+40NE	6	198	353	233	1.4	5	12	595	5.69	11	5	ND	2	60	1	2	2	66	.10	.115	19	16	.49	183	.04	2	2.20	.01	.06	1
2+50SE 0+60NE	7	149	339	151	3.2	2	8	685	4.95	11	6	ND	2	73	1	2	3	49	.07	.116	13	7	.49	273	.04	2	2.07	.02	.12	1
2+50SE 0+40NE	20	117	64	181	.6	16	19	929	6.21	10	6	ND	2	84	1	2	2	100	.71	.115	9	43	.88	125	.14	2	2.53	.01	.06	1
2+50SE 0+20NE	4	37	61	265	1.3	14	11	626	5.23	12	5	ND	3	38	1	2	2	68	.19	.115	12	24	.59	177	.06	2	3.02	.01	.05	1
2+50SE 0+20SW	8	160	359	158	3.4	2	9	715	5.32	12	5	ND	2	79	1	2	2	51	.07	.127	13	10	.51	303	.05	2	2.24	.02	.14	1
2+50SE 0+40SW	46	152	463	121	10.6	7	9	342	6.21	24	5	ND	3	39	1	2	7	47	.07	.142	15	19	.32	162	.02	2	2.03	.02	.19	1
2+50SE 0+60SW	44	164	480	127	10.4	6	10	338	6.68	21	5	ND	4	37	1	2	4	51	.07	.147	14	17	.34	162	.02	3	2.13	.02	.19	1
2+50SE 0+80SW	9	152	306	128	6.2	7	10	420	5.59	12	5	ND	1	36	1	2	2	64	.13	.109	13	23	.46	100	.07	2	2.19	.01	.06	1
2+50SE 1+00SW	5	87	341	85	5.3	4	8	328	10.31	13	5	ND	3	32	1	2	2	57	.05	.357	8	20	.27	204	.05	2	1.96	.02	.08	1
2+50SE 1+20SW	4	53	179	79	1.5	3	5	460	5.87	15	5	ND	2	45	1	2	2	51	.07	.090	9	15	.40	321	.03	3	1.57	.04	.12	1
2+50SE 1+40SW	3	43	159	89	1.4	6	6	476	4.99	13	5	ND	2	56	1	2	2	50	.09	.103	11	22	.42	343	.06	3	1.59	.04	.12	1
2+50SE 1+60SW	3	40	135	94	1.1	7	6	488	4.81	9	5	ND	3	47	1	2	2	52	.10	.093	9	20	.43	251	.07	4	1.88	.03	.09	1
2+50SE 1+80SW	3	35	87	81	.7	6	5	362	4.44	7	5	ND	2	41	1	2	2	68	.10	.060	7	20	.33	162	.06	2	1.80	.01	.06	1
2+50SE 2+00SW	5	19	141	52	1.2	1	4	509	4.34	10	5	ND	2	31	1	2	2	82	.11	.081	7	15	.14	201	.06	3	1.89	.01	.06	1
3+00SE 0+60NE	30	181	86	232	.8	14	25	1059	6.56	18	5	ND	2	95	1	2	2	86	.91	.122	8	34	.92	119	.14	2	3.14	.01	.08	1
3+00SE 0+40NE	24	138	75	211	.4	14	22	939	5.38	10	5	ND	1	100	1	2	2	74	1.06	.121	8	30	.89	107	.12	3	3.01	.02	.08	1
3+00SE 0+20NE	19	106	62	159	.6	13	20	1001	5.77	12	5	ND	1	75	1	2	2	93	.70	.154	6	45	.81	113	.11	3	2.55	.01	.06	1
3+00SE 1+20SW	3	28	93	72	1.6	4	5	303	4.81	6	5	ND	3	35	1	2	2	83	.10	.091	8	19	.22	116	.05	2	1.82	.01	.04	1
3+00SE 1+40SW	6	64	186	101	4.0	2	7	614	7.01	13	5	ND	3	51	1	2	3	47	.07	.185	13	12	.47	392	.02	4	1.93	.03	.22	1
3+00SE 1+60SW	7	60	394	83	2.8	1	6	475	5.46	17	5	ND	2	38	1	2	2	60	.07	.112	10	12	.36	344	.02	2	1.90	.02	.09	1
3+00SE 1+80SW	5	38	319	109	1.8	4	7	843	6.22	14	5	ND	2	39	1	2	2	57	.09	.147	9	16	.42	294	.06	2	2.88	.02	.09	1
3+00SE 2+00SW	4	29	99	86	1.9	3	5	418	6.01	11	5	ND	2	33	1	2	2	77	.09	.095	10	19	.31	170	.09	5	2.79	.02	.06	1
3+00SE 2+20SW	4	33	120	93	1.1	7	5	451	5.93	8	5	ND	3	37	1	2	2	67	.10	.102	10	23	.38	197	.07	3	2.37	.02	.06	1
3+00SE 2+40SW	3	31	80	86	.9	3	5	388	5.00	4	5	ND	2	41	1	2	2	69	.11	.066	9	18	.34	147	.06	2	2.17	.01	.05	1
3+50SE 0+60NE	27	171	89	231	.6	16	23	1040	5.88	10	5	ND	1	108	1	2	2	80	.97	.108	12	31	.97	160	.13	5	3.42	.02	.07	1
3+50SE 0+40NE	24	148	88	221	.7	12	26	1140	5.92	12	5	ND	1	100	2	2	2	82	.98	.149	11	34	.90	133	.12	5	3.10	.02	.08	1
3+50SE 0+20NE	35	187	82	224	.7	12	28	1260	7.71	12	5	ND	1	87	3	2	2	84	.82	.146	12	34	.81	119	.12	4	3.15	.01	.08	1
3+50SE 0+20SW	3	37	42	125	2.8	10	8	483	4.59	7	5	ND	3	31	1	2	2	71	.24	.161	9	23	.40	82	.07	4	3.50	.01	.04	1
3+50SE 0+40SW	6	40	241	82	4.7	1	5	566	4.57	9	5	ND	2	58	1	2	2	45	.05	.107	10	8	.44	187	.04	2	2.57	.02	.07	1
3+50SE 0+60SW	7	66	424	99	4.4	1	5	522	5.72	14	5	ND	3	77	1	2	2	59	.05	.191	16	8	.37	322	.03	2	2.91	.02	.11	1
3+50SE 0+80SW	9	108	700	79	2.0	1	8	741	7.03	10	5	ND	2	80	1	2	2	58	.06	.235	18	7	.49	288	.05	4	2.15	.02	.12	1
3+50SE 1+00SW	4	139	227	68	8.0	3	8	412	6.55	10	5	ND	1	42	1	2	2	49	.10	.147	16	15	.42	100	.03	2	2.19	.01	.04	1
3+50SE 1+20SW	4	69	199	66	3.4	4	6	434	4.82	10	5	ND	1	43	1	2	3	49	.08	.092	13	14	.41	114	.05	2	1.53	.01	.05	1
3+50SE 1+40SW	4	71	169	76	6.3	5	6	504	4.55	6	5	ND	1	52	1	2	2	52	.11	.101	11	16	.50	143	.07	2	1.58	.01	.05	1
3+50SE 1+60SW	4	94	200	80	2.1	2	8	565	5.70	8	5	ND	1	55	1	2	2	60	.11	.111	14	17	.53	179	.06	2	1.77	.01	.06	1
STD C	20	58	38	131	6.9	67	29	1074	3.94	38	18	7	33	47	17	15	19	61	.48	.102	36	59	.88	174	.08	38	1.73	.06	.12	14

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
3+50SE 1+80SW	3	42	142	78	1.6	5	5	460	4.29	5	5	ND	1	40	1	2	2	51	.08	.087	9	16	.43	176	.08	2	1.05	.01	.06	1
3+50SE 2+00SW	3	41	94	81	2.0	5	6	416	4.81	5	5	ND	1	40	1	2	2	50	.08	.076	7	17	.41	166	.07	2	1.14	.01	.05	1
4+00SE 0+60NE	19	144	76	210	.6	13	25	960	4.66	5	7	ND	1	81	1	2	2	64	.74	.090	8	27	.79	118	.09	2	2.59	.02	.06	1
4+00SE 0+40NE	27	157	71	192	.9	9	23	881	6.25	9	8	ND	2	73	2	2	4	78	.62	.109	7	34	.79	105	.10	2	2.55	.01	.06	1
4+00SE 0+20NE	28	157	66	166	.7	12	22	875	6.27	6	7	ND	2	74	1	2	2	77	.64	.113	6	36	.79	107	.10	3	2.57	.01	.06	1
4+00SE 1+20SW	6	56	352	121	2.5	3	8	733	8.28	18	5	ND	2	53	1	2	8	49	.09	.256	11	12	.44	355	.01	3	2.43	.02	.14	1
4+00SE 1+40SW	3	55	120	82	.8	4	6	421	4.40	7	5	ND	2	37	1	4	3	53	.09	.089	7	15	.42	190	.05	2	1.48	.01	.06	1
4+00SE 1+60SW	2	64	92	90	1.4	6	8	400	9.72	6	5	ND	2	29	1	3	8	59	.07	.087	5	19	.40	160	.06	2	1.24	.01	.05	1
4+00SE 1+80SW	3	49	306	132	1.0	8	7	615	4.70	8	5	ND	2	45	1	2	2	58	.09	.138	8	17	.52	245	.03	2	1.56	.01	.07	1
4+00SE 2+00SW	3	40	97	101	.8	9	7	578	5.15	5	5	ND	2	39	1	3	2	56	.09	.117	8	25	.47	215	.05	3	2.34	.01	.06	1
STD C	20	57	38	130	6.8	67	29	1057	3.91	39	19	7	32	46	16	15	18	61	.48	.100	35	58	.88	171	.08	38	1.72	.06	.13	13

ACME ANALYTICAL LABORATORIES LTD.
852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 TELEX 04-53124

DATE RECEIVED: JULY 28 1986

DATE REPORT MAILED: Aug 1/86....

ASSAY CERTIFICATE

SAMPLE TYPE: ROCK CHIPS AU* 10 GRAM REGULAR ASSAY

ASSAYER: ..D. Toye.. DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-1692A

SAMPLE#	Cu %	Pb %	Zn %	Ag OZ/T	Au OZ/T
X 1311	.01	.03	.01	.04	.001
X 1312	.01	.03	.02	.03	.001
X 1313	.01	.02	.06	.02	.001
X 1314	.01	.03	.03	.05	.001
X 1315	.01	.02	.01	.06	.001
X 1316	.01	.04	.03	.09	.001
X 1317	.01	.02	.05	.02	.001
X 1318	.02	.26	.30	1.02	.001
X 1319	.04	.73	.75	1.89	.004
X 1320	.01	.47	.07	.51	.004
X 1321	.02	.02	.29	.15	.001
X 1322	.01	.03	.13	.21	.001
X 1323	.05	.03	.96	.30	.002
X 1324	.04	.01	.21	.18	.001
X 1325	.01	.03	.03	.19	.001
X 1326	.01	.03	.04	.41	.001
X 1327	.01	.01	.01	.05	.001
X 1328	.02	.06	.12	.21	.001
X 1329	.02	.04	.05	.17	.001
X 1330	.04	.02	.05	.24	.001
X 1331	.01	.02	.02	.16	.002
X 1332	.01	.02	.02	.12	.001
X 1333	.03	.08	.48	.32	.001
X 1334	.01	.11	.03	.21	.001
X 1335	.01	.13	.02	.21	.001
X 1336	.01	.06	.02	.19	.001
X 1337	.02	.01	.12	.19	.001
X 1338	.02	.02	.05	.40	.001
X 1339	.03	.01	.04	.15	.001
X 1340	.01	.01	.02	.07	.001
X 1341	.01	.01	.02	.10	.001
55827	-	-	-	.04	.011
55828	-	-	-	.18	.061
55829	-	-	-	.51	.088

ME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS, VANCOUVER B.C.
PH: (604)253-3158 COMPUTER LINE:251-1011

DATE RECEIVED AUG 4 1986
DATE REPORTS MAILED Aug 8/86

ASSAY CERTIFICATE

SAMPLE TYPE : PULP
AG** AND AU** BY FIRE ASSAY

ASSAYER D Toye DEAN TOYE . CERTIFIED B.C. ASSAYER

CANASIL RESOURCES FILE# 86-1692 R PAGE# 1

SAMPLE	Ag** oz/t	Au** oz/t
55830	63.77	.530

ACME ANALYTICAL LABORATORIES LTD.
852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: AUG 4 1986

DATE REPORT MAILED: Aug. 13/86..

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS -80 MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

P3-Rocks

ASSAYER: D. Toye. DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-1819 PAGE 1

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
0+50NW 0+80NE	82	48	354	.5	7	4
0+50NW 0+60NE	87	57	337	.6	8	12
0+50NW 0+40NE	160	205	492	2.9	6	42
0+50NW 0+20NE	140	187	507	2.3	6	31
0+50NW 0+20SW	110	178	351	2.9	11	6
0+50NW 0+40SW	44	132	101	.8	8	9
0+50NW 0+60SW	49	98	160	1.1	7	4
0+50NW 0+80SW	49	70	120	2.4	5	6
0+50NW 1+00SW	56	64	130	3.3	3	4
0+50NW 1+20SW	60	50	140	1.1	2	32
0+50NW 1+40SW	44	109	99	2.6	15	5
0+50NW 1+60SW	40	42	103	1.0	7	3
0+50NW 1+80SW	38	56	107	.6	4	9
0+50NW 2+00SW	44	53	123	.6	7	7
0+50NW 2+20SW	38	49	110	.5	5	3
0+50NW 2+40SW	162	197	457	3.4	8	30
4+50SE 0+60NE	159	96	227	1.5	3	21
4+50SE 0+40NE	141	86	197	.8	6	15
4+50SE 0+20NE	28	29	144	.5	5	7
4+50SE 0+20SW	44	91	69	.4	9	5
4+50SE 0+40SW	81	110	43	1.3	38	12
4+50SE 0+60SW	38	53	123	.7	8	6
4+50SE 0+80SW	42	233	96	1.2	10	75
4+50SE 1+00SW	31	110	113	2.5	8	22
4+50SE 1+20SW	40	182	121	2.0	9	10
4+50SE 1+40SW	42	91	121	.9	8	13
4+50SE 1+60SW	38	85	108	.7	7	12
4+50SE 1+80SW	50	115	128	1.4	10	19
4+50SE 2+00SW	52	80	130	.2	2	12
5+00SE 0+60NE	164	86	233	.5	5	17
5+00SE 0+40NE	123	63	224	.5	7	19
5+00SE 0+20NE	28	42	141	.2	12	9
5+00SE 1+20SW	36	139	78	1.4	6	11
5+00SE 1+40SW	38	83	100	1.7	11	21
5+00SE 1+60SW	39	79	99	.8	10	5
5+00SE 1+80SW	44	99	133	1.0	9	6
STD C/AU-0.5	59	37	138	7.3	40	490

CANASIL RESOURCES FILE # 86-1819

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
5+00SE 2+00SW	23	90	138	.5	9	70
5+00SE 2+20SW	43	96	98	1.3	7	5
5+50SE 0+20NE	143	88	252	.6	10	15
5+50SE 0+20SW	27	117	109	.9	49	10
5+50SE 0+40SW	44	144	123	.9	6	7
5+50SE 0+60SW	64	123	143	.3	7	9
5+50SE 0+80SW	68	207	113	1.5	8	13
5+50SE 1+00SW	56	127	116	.8	6	10
5+50SE 1+20SW	54	68	133	.7	8	9
5+50SE 1+40SW	34	198	86	1.2	4	10
5+50SE 1+60SW	45	82	115	.7	7	6
5+50SE 1+80SW	36	92	100	.8	7	49
5+50SE 2+00SW	18	79	51	.5	7	2
5+50SE 2+20SW	31	129	100	.7	8	8
6+00SE 1+20SW	48	93	126	1.5	10	22
6+00SE 1+40SW	47	78	131	1.6	11	9
6+00SE 1+60SW	20	81	67	1.1	3	4
6+00SE 1+80SW	46	92	159	1.3	5	6
6+00SE 2+00SW	62	84	139	1.5	7	12
STD C/AU 0.5	60	41	139	7.3	41	500

CANASIL RESOURCES FILE # 86-1819

✓

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB	Au** OZ/T
55833	1126	16123✓	12143	563.6✓	15	28000	.836
55834	28	109	61	3.2	2	3650	.106
55835	17	23	91	.4	4	65	-
55836	703	1486	10670	6.1	4	20	-

✓ Assay required for correct result ___

ACME ANALYTICAL LABORATORIES LTD.
852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: AUG 15 1986

DATE REPORT MAILED: Aug 20/86....

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK CHIPS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: D.Toye. DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-2071 PAGE 1

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
1345	6	3	2	.2	2	3
1346	8	19	22	3.2	273	195
1347	4	4	1	.1	4	5
1348	8	22	9	2.5	4	100
1349	84	15	5	2.3	12	105
1350	40	8	207	.2	2	5

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB	Ba* PPM
1360	57	295	552	.7	11	4	-
1361	92	1870	151	3.2	17	9	-
1362	1583	56	91	6.2	10	210	-
1363	459	80	206	5.9	4	63	-
1364	358	290	1794	27.2	4	42	-
1365	331	561	1751	20.1	2	68	-
1366	8	8	11	.2	2	5	1182
1367	146	564	755	5.6	10	28	-
1368	7	3	3	.1	4	6	839
1369	12	37	86	.5	8	4	-
1370	1288	22330 ✓	43313 ✓	332.0 ✓	3	84	-
1371	759	4768	1581	7.1	2	12	-
STD C/AU-R	59	40	140	7.2	37	510	-

✓ Assay required for correct result

Ba is total

ˉCME ANALYTICAL LABORATORIES LTD.
52 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: AUG 29 1986

DATE REPORT MAILED: Sept.4/86...

GEOCHEMICAL/ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCKS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE. AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: .D.Toye.DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-2359

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB	Au OZ/T
1351	2139	18573✓	30122✓	135.5✓	25	220	-
1352	288	4808	4457	122.5✓	29	640	-
1353	885	12048✓	14201	77.2✓	8	190	-
1354	45	2067	634	9.5	22	620	-
1355	943	336	4323	10.9	6	33	-
1356	86	231	2854	7.0	14	39	-
1357	17545✓	414	4621	66.6✓	5	69	-
1358	57	308	582	16.8	5	23	-
1359	120	91	1000	5.9	4	35	-
55837	854	15851✓	2081	22.4	5	9	-
55838	1400	3938	8822	17.1	3	10	-
55839	896	5858	12411	12.7	2	31	-
55840	112	313	1759	113.7✓	247	20000	.598
55841	8588	205	727	10.6	6	380	-
55842	20	25	34	.4	25	19	-
55843	162	1448	11388	211.6✓	178	5560	.165
55844	305	782	2936	314.0✓	128	51000	1.440
55845	31	104	127	5.1	4	200	-
55846	103	1259	468	7.5	4	152	-
55847	63	101	397	3.5	2	210	-
55848	11	47	103	5.6	301	157	-
55849	25	50	379	6.9	178	180	-
55850	10	11	4	1.4	37	300	-
STD C/AU-0.5	55	39	128	6.8	37	520	-

——— Assay required for correct result ———

ACME ANALYTICAL LABORATORIES LTD.
852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: SEPT 15 1986

DATE REPORT MAILED: Sept 20/86...

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-SOILS P2-ROCKS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: ..D. Toye..DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-2660

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
7+50SE 2+40NE	75	43	306	.7	2	31
7+50SE 2+20NE	207	36	111	.9	2	1
7+50SE 1+95NE	37	47	115	7.6	2	6
7+50SE 1+80NE	40	67	158	.4	5	10
7+50SE 1+60NE	30	80	121	.3	2	7
7+50SE 1+40NE	29	78	171	1.4	5	11
7+50SE 1+20NE	36	141	115	2.6	5	22
7+50SE 1+00NE	33	127	103	1.1	4	37
7+50SE 0+80NE	31	133	108	1.6	9	26
7+50SE 0+60NE	74	107	143	2.3	3	17
7+50SE 0+40NE	28	73	72	.5	6	4
7+50SE 0+20NE	48	86	138	.4	5	35
8+00SE 2+18NE	76	61	212	.9	2	13
8+00SE 2+00NE	41	54	137	.4	2	34
8+00SE 1+80NE	48	71	209	1.0	5	12
8+00SE 1+60NE	30	53	140	.6	2	490
8+00SE 1+40NE	21	62	327	2.4	2	3
8+00SE 1+20NE	41	129	109	1.2	8	29
8+00SE 1+00NE	50	138	138	.9	5	24
8+00SE 0+80NE	35	81	144	.9	2	8
8+00SE 0+60NE	35	97	112	.4	5	7
8+00SE 0+40NE	47	52	130	.2	2	9
8+00SE 0+20NE	46	66	111	.3	3	12
STD C/AU-S	60	42	141	7.3	40	49

ACME ANALYTICAL LABORATORIES LTD.
852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: SEPT 22 1986

DATE REPORT MAILED: Sept 30/86...

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: CORES//ROCKS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: D. Toye ...DEAN TOYE. CERTIFIED B.C. ASSAYER.

CANASIL RESOURCES FILE # 86-2801

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
51628	3344	148	5251	15.3	5	15
51629	478	405	3886	5.5	9	9
51630	2101	165	12719	9.7	6	10
51631	274	112	4504	4.4	5	1
51632	621	153	5731	13.9	3	14
51633	379	71	4674	3.7	2	3
51634	199	120	1015	3.1	2	2
51635	765	709	5088	6.1	2	11
51636	468	436	4220	5.0	4	7
51637	1904	268	12479	13.4	6	18
51638	1779	172	6686	12.8	4	9
STD C/AU-R	58	38	132	6.9	40	515

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
1+00SE 2+00SW	79	441	90	9.6	10	22
6+00SE 1+00NE	43	48	97	.5	4	9
6+00SE 1+20NE	106	61	130	.9	5	7
6+00SE 1+40NE	174	74	211	.5	9	17
6+00SE 1+60NE	188	80	204	1.1	11	11
6+00SE 1+80NE	167	87	207	.4	10	6
6+50SE 0+20NE	52	62	93	.2	5	4
6+50SE 0+40NE	42	104	107	1.1	4	31
6+50SE 0+60NE	37	161	103	1.1	13	11
6+50SE 0+80NE	32	47	226	1.5	7	4
6+50SE 1+00NE	20	33	183	1.4	9	2
6+50SE 1+20NE	24	40	95	.9	7	1
6+50SE 1+40NE	56	62	165	.3	4	4
6+50SE 1+60NE	101	71	153	1.1	2	87
6+50SE 1+80NE	108	71	180	1.5	6	12
7+00SE 0+20NE	34	153	73	.9	13	3
7+00SE 0+40NE	26	163	72	1.6	13	3
7+00SE 0+60NE	32	142	81	1.1	13	6
7+00SE 0+80NE	40	136	96	2.1	9	13
7+00SE 1+00NE	19	41	126	.5	10	1
7+00SE 1+20NE	23	56	124	1.4	5	42
7+00SE 1+40NE	24	41	87	.6	6	1
7+00SE 1+60NE	18	28	48	.2	2	1
7+00SE 1+80NE	76	49	134	.6	4	10
7+00SE 2+00NE	99	53	161	.4	4	7
TO+00E 0+80N	30	94	118	1.7	6	2
TO+00E 1+00N	26	219	97	.7	11	3
TO+00E 1+20N	21	83	115	.6	5	1
TO+00E 1+40N	34	111	100	2.2	11	6
TO+00E 1+60N	31	162	91	.9	11	4
TO+20E 0+80N	37	143	129	1.2	9	6
TO+20E 1+00N	30	131	123	.6	8	10
TO+20E 1+20N	27	104	120	1.1	10	3
TO+20E 1+40N	28	124	109	.6	11	7
TO+20E 1+60N	29	98	92	.7	6	3
TO+40E 0+80N	32	145	105	.6	11	17
STD C/AU-0.5	59	40	136	7.1	38	510

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	As PPM	Au* PPB
TO+40E 1+00N	32	267	177	.4	5	20
TO+40E 1+20N	33	122	113	.7	10	9
TO+40E 1+40N	22	127	75	.9	6	1
TO+40E 1+60N	30	134	101	1.0	15	11
TO+20W 0+20S	108	103	490	.7	6	20
TO+20W 0+40S	29	41	131	.3	7	142
TO+20W 0+60S	19	59	105	.8	6	11
TO+40W 0+20S	39	87	145	.3	5	2
TO+40W 0+40S	109	100	499	.7	11	3
TO+40W 0+60S	22	42	123	.2	6	2
TO+40W 0+80S	25	93	113	.6	11	1
TBL 0+20E	52	91	138	.4	16	21
TBL 0+40E	36	108	116	.6	10	18
TBL 0+60E	40	139	142	.6	11	38
TBL 0+80E	44	276	93	1.3	19	19
TBL 1+00E	21	135	73	.6	6	3
TBL 1+20E	29	111	113	.5	12	1
TBL 1+40E	40	159	123	1.2	11	2
TBL 1+60E	30	101	77	.7	8	104
TBL 0+20W	55	94	133	.6	6	26
TBL 0+40W	41	145	129	1.1	16	22
TBL 0+60W	34	152	103	1.4	9	16
TBL 0+80W	27	149	92	.8	8	8
TBL 1+00W	43	137	151	.8	14	3
STD C/AU 0.5	60	40	139	7.2	42	500

APPENDIX B

AREA 1 EMR-16 DATA

CANASIL EMR-16 SURVEY
1986

AREA 1

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
0+00SE	0+00	120	35	170	35
0+00SE	0+10NE	115	42	150	34
0+00SE	0+10SW	120	25	300	35
0+00SE	0+15NE	150	40	210	42
0+00SE	0+20SW	550	24	500	32
0+00SE	0+30SW	950	27	400	31
0+00SE	0+40SW	1500	27	600	32
0+00SE	0+50SW	750	30	300	31
0+00SE	0+60SW	350	32	350	32
0+00SE	0+80SW	300	42	800	36
0+00SE	1+00SW	450	42	800	37
0+00SE	1+20SW	600	36	750	36
0+00SE	1+40SW	800	37	800	38
0+00SE	1+60SW	1700	36	1300	39
0+00SE	1+80SW	750	42	900	46
0+00SE	2+00SW	650	48	650	42
0+25SE	0+00	1400	28	1300	33
0+25SE	0+10SW	350	42	300	37
0+25SE	0+10SW	2300	32	1300	30
0+25SE	0+20SW	1600	32	1300	30
0+25SE	0+30SW	500	37	200	40
0+25SE	0+40SW	200	39	180	39
0+25SE	0+50SW	45	75	170	44
0+50NW	0+00	350	42	350	42
0+50NW	0+20NE	250	44	300	42
0+50NW	0+20SW	350	34	400	31
0+50NW	0+40NE	350	42	350	43
0+50NW	0+40SW	140	43	80	43
0+50NW	0+60NE	250	39	240	38
0+50NW	0+60SW	600	30	600	33
0+50NW	0+75NE	210	37	200	37
0+50NW	0+80SW	1400	28	1500	26
0+50NW	1+00SW	500	42	950	34
0+50NW	1+20SW	450	43	400	42
0+50NW	1+40SW	500	42	400	40
0+50NW	1+60SW	900	42	1100	40
0+50NW	1+80SW	1300	38	1100	42
0+50NW	2+00SW	850	42	800	42
0+50NW	2+20SW	450	43	400	45
0+50NW	2+40SW	1000	40	1700	43
0+50SE	0+00	4500	28	3000	34
0+50SE	0+10SW	450	35	500	36
0+50SE	0+10SW	850	30	950	31
0+50SE	0+20NE	350	37	350	42
0+50SE	0+20SW	500	38	350	42
0+50SE	0+30SW	170	43	190	42
0+50SE	0+40SW	160	44	160	42

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
0+50SE	0+60SW	400	38	500	36
0+50SE	0+80SW	400	43	270	45
0+50SE	1+00SW	1200	39	1100	44
0+50SE	1+20SW	500	42	1100	40
0+50SE	1+40SW	2000	38	1300	37
0+50SE	1+60SW	1050	37	1300	37
0+50SE	1+80SW	350	44	300	43
0+50SE	2+00SW	130	48	200	53
0+75SE	0+00	1300	33	1200	25
0+75SE	0+10NE	2000	34	1200	25
0+75SE	0+10SW	650	39	750	41
0+75SE	0+20NE	750	34	1100	35
0+75SE	0+20SW	150	51	170	46
0+75SE	0+30NE	650	38	1100	37
0+75SE	0+30SW	170	47	260	44
0+75SE	0+40SW	300	47	250	47
0+75SE	0+50SW	900	36	800	35
0+75SE	0+60SW	550	35	1100	38
0+75SE	0+70SW	220	47	300	47
0+75SE	0+80SW	300	47	210	47
0+75SE	0+90SW	1100	37	800	39
0+75SE	1+00SW	1100	34	850	36
0+75SE	1+10SW	700	41	750	37
0+75SE	1+20SW	500	45	450	50
1+00SE	0+00	2400	34	4500	32
1+00SE	0+10NE	3000	35	6000	34
1+00SE	0+10SW	170	42	280	39
1+00SE	0+20NE	160	37	220	38
1+00SE	0+20SW	240	50	230	43
1+00SE	0+30NE	160	42	110	44
1+00SE	0+30SW	280	49	250	40
1+00SE	0+40SW	850	36	750	39
1+00SE	0+50SW	450	39	750	42
1+00SE	0+60SW	450	32	700	41
1+00SE	0+80SW	1100	38	1000	40
1+00SE	1+00SW	650	42	450	46
1+00SE	1+20SW	450	43	650	47
1+00SE	1+40SW	2400	32	5000	36
1+00SE	1+60SW	700	45	1500	47
1+00SE	1+80SW	240	44	45	54
1+00SE	2+00SW	240	39	100	51
1+25SE	0+00	850	35	3000	31
1+25SE	0+10NE	550	36	950	34
1+25SE	0+10SW	1000	34	3000	31
1+25SE	0+20NE	300	38	270	37
1+25SE	0+20SW	300	47	400	39
1+25SE	0+30NE	200	40	140	45
1+25SE	0+30SW	450	44	700	42
1+25SE	0+40NE	850	39	1100	39
1+25SE	0+40SW	550	42	450	42
1+50SE	0+00	750	34	1200	30

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
1+50SE	0+10NE	1150	33	700	36
1+50SE	0+10SW	1200	35	3000	33
1+50SE	0+20NE	600	35	350	37
1+50SE	0+20SW	900	38	1000	36
1+50SE	0+30NE	200	40	350	43
1+50SE	0+30SW	450	37	650	39
1+50SE	0+40NE	550	38	1000	38
1+50SE	0+40SW	450	33	450	42
1+50SE	0+50NE	250	40	280	41
1+50SE	0+50SW	1100	37	900	40
1+50SE	0+60SW	950	38	800	44
1+50SE	0+70SW	1300	37	1300	39
1+50SE	0+80SW	2200	38	2300	43
1+50SE	1+00SW	300	51	550	48
1+50SE	1+20SW	1800	38	1100	39
1+50SE	1+40SW	2100	32	2000	33
1+50SE	1+60SW	1100	33	1500	47
1+50SE	1+80SW	900	47	1000	47
1+75SE	0+00	600	34	650	41
1+75SE	0+10NE	550	38	260	43
1+75SE	0+10SW	750	35	850	35
1+75SE	0+20NE	800	36	400	41
1+75SE	0+20SW	450	35	1300	35
1+75SE	0+30NE	1100	35	700	36
1+75SE	0+39SW	850	33	850	35
1+75SE	0+40NE	900	36	500	39
1+75SE	0+40SW	1900	33	1400	36
1+75SE	0+50SW	1200	36	800	39
1+75SE	0+60SW	1800	36	1200	38
1+75SE	0+70SW	1300	36	800	41
1+75SE	0+80SW	350	42	600	42
1+75SE	0+90SW	500	43	550	45
1+75SE	1+00SW	450	41	550	46
1+75SE	1+10SW	1500	31	1100	37
1+75SE	1+20SW	3500	30	1900	36
2+00SE	0+00	1000	37	700	35
2+00SE	0+10NE	170	42	300	54
2+00SE	0+10SW	600	37	800	43
2+00SE	0+20NE	350	40	150	53
2+00SE	0+20SW	1300	32	1050	36
2+00SE	0+30SW	550	37	550	43
2+00SE	0+30SW	450	37	900	34
2+00SE	0+40NE	1300	35	1700	38
2+00SE	0+40SW	1100	32	1500	36
2+00SE	0+50SW	1100	38	1400	38
2+00SE	0+50SW	850	34	1200	35
2+00SE	0+60NE	500	30	550	42
2+00SE	0+60SW	700	37	750	37
2+00SE	0+70SW	450	42	450	42
2+00SE	0+70SW	550	39	500	39
2+00SE	0+80NE	300	42	300	44

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
2+00SE	0+80SW	750	38	750	42
2+00SE	0+90SW	1300	33	950	34
2+00SE	1+00SW	3500	29	2300	34
2+00SE	1+10SW	3500	30	1900	36
2+00SE	1+20SW	1000	36	900	32
2+00SE	1+30SW	950	39	550	43
2+00SE	1+40SW	1000	39	600	46
2+00SE	1+60SW	750	45	850	44
2+00SE	1+80SW	150	43	210	45
2+00SE	2+00SW	300	45	300	42
2+25SE	0+00	750	34	1000	43
2+25SE	0+10SW	1500	28	850	30
2+25SE	0+20SW	300	36	260	39
2+25SE	0+30SW	700	29	1000	32
2+25SE	0+40SW	200	34	1100	31
2+25SE	0+50SW	300	34	100	43
2+25SE	0+60SW	75	37	100	39
2+25SE	0+70SW	95	45	110	42
2+25SE	0+80SW	350	37	300	40
2+25SE	0+90SW	130	35	90	32
2+25SE	1+00SW	350	37	450	42
2+25SE	1+10SW	110	40	550	37
2+25SE	1+20SW	110	47	700	41
2+50SE	0+00	2100	37	2300	39
2+50SE	0+10SW	550	36	450	42
2+50SE	0+20NE	500	42	350	42
2+50SE	0+20NE	500	42	350	42
2+50SE	0+20SW	500	38	210	35
2+50SE	0+20SW	500	38	210	35
2+50SE	0+30SW	1900	32	1300	32
2+50SE	0+40NE	800	37	1400	42
2+50SE	0+40NE	800	37	1400	42
2+50SE	0+40SW	950	33	550	37
2+50SE	0+40SW	950	33	550	37
2+50SE	0+50SW	400	33	230	27
2+50SE	0+60NE	750	37	550	41
2+50SE	0+60NE	750	37	550	41
2+50SE	0+60SW	900	32	600	30
2+50SE	0+60SW	900	32	600	30
2+50SE	0+70SW	1100	34	950	25
2+50SE	0+80NE	450	40	350	40
2+50SE	0+80NE	450	40	350	40
2+50SE	0+80SW	1200	28	1300	26
2+50SE	0+80SW	1200	28	1300	26
2+50SE	0+90SW			1100	25
2+50SE	1+00SW	550	30	700	28
2+50SE	1+00SW	550	30	700	28
2+50SE	1+20SW	300	40	400	30
2+50SE	1+20SW	300	40	400	30
2+50SE	1+40SW	200	40	140	41
2+50SE	1+40SW	200	40	140	41

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
2+50SE	1+60SW	80	52	110	47
2+50SE	1+60SW	80	52	110	47
2+50SE	1+80SW	130	52	210	45
2+50SE	1+80SW	130	52	210	45
2+50SE	2+00SW	1100	51	1000	42
2+50SE	2+00SW	1100	51	1000	42
2+50SE	2+15SW	400	47	350	42
2+50SE	2+15SW	400	47	350	42
2+50SE	0+00	2100	37	2300	39
2+75SE	0+10NE	300	38	240	43
2+75SE	0+10SW	1100	34	2000	32
3+00SE	0+00	180	45	90	38
3+00SE	0+10NE	650	35	700	36
3+00SE	0+10SW	650	37	1300	34
3+00SE	0+20NE	550	34	800	32
3+00SE	0+20NE	550	34	800	32
3+00SE	0+20SW	1000	35	1400	32
3+00SE	0+40NE	350	37	400	37
3+00SE	0+40NE	350	37	400	37
3+00SE	0+40SW	450	37	350	36
3+00SE	0+60NE	210	37	220	36
3+00SE	0+60NE	210	37	220	36
3+00SE	0+60SW	500	30	600	30
3+00SE	0+80NE	450	33	400	37
3+00SE	0+80NE	450	33	400	37
3+00SE	0+80SW	1100	28	1000	25
3+00SE	1+00NE	350	37	350	37
3+00SE	1+00NE	350	37	350	37
3+00SE	1+00SW	750	32	850	28
3+00SE	1+20SW	1500	35	1000	36
3+00SE	1+40SW	210	36	280	35
3+00SE	1+60SW	300	40	160	38
3+00SE	1+80SW	250	43	240	43
3+00SE	1+90SW	300	45	350	40
3+00SE	2+00SW	900	43	1400	40
3+00SE	2+20SW	800	42	800	40
3+00SE	2+40SW	600	44	450	43
3+50SE	0+00	150	45	80	45
3+50SE	0+20NE	1200	38	1300	41
3+50SE	0+20SW	950	37	1100	38
3+50SE	0+30SW	500	39	550	38
3+50SE	0+40NE	450	34	450	39
3+50SE	0+40SW	600	41	750	41
3+50SE	0+60NE	350	36	350	37
3+50SE	0+60SW	800	30	750	31
3+50SE	0+80NE	180	41	250	35
3+50SE	0+80SW	450	23	600	18
3+50SE	1+00NE	350	35	450	31
3+50SE	1+00SW	180	32	190	38
3+50SE	1+20SW	110	38	110	36
3+50SE	1+40SW	130	39	95	42

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
3+50SE	1+60SW	220	35	90	43
3+50SE	1+80SW	350	36	350	38
3+50SE	2+00SW	260	32	450	35
4+00SE	0+00	140	43	100	47
4+00SE	0+00SW	550	35	550	36
4+00SE	0+20NE	900	39	700	43
4+00SE	0+40NE	950	35	750	37
4+00SE	0+40SW	220	39	180	38
4+00SE	0+60NE	800	33	750	31
4+00SE	0+60SW	850	29	1100	26
4+00SE	0+80NE	400	35	550	35
4+00SE	0+80SW	650	29	700	26
4+00SE	1+00NE	280	38	300	36
4+00SE	1+00SW	260	38	270	35
4+00SE	1+20NE	210	40	230	40
4+00SE	1+20SW	230	37	450	35
4+00SE	1+40NE	350	39	260	39
4+00SE	1+40SW	190	43	300	43
4+00SE	1+60NE	350	38	450	36
4+00SE	1+60SW	130	42	140	39
4+00SE	1+80NE	350	37	350	35
4+00SE	1+80SW	140	41	200	39
4+00SE	2+00NE	350	33	450	35
4+00SE	2+00SW	500	37	400	36
4+00SE	2+20NE	450	38	350	39
4+50SE	0+00	160	44	260	43
4+50SE	0+20NE	200	43	160	43
4+50SE	0+20SW	300	40	300	42
4+50SE	0+40NE	1500	36	1100	40
4+50SE	0+40SW	300	35	110	38
4+50SE	0+60NE	1400	34	1300	35
4+50SE	0+60SW	1500	28	1500	28
4+50SE	0+80NE	950	34	1100	33
4+50SE	0+80SW	350	43	500	34
4+50SE	1+00NE	450	39	500	37
4+50SE	1+00SW	140	62	300	48
4+50SE	1+20NE	450	42	300	42
4+50SE	1+20SW	750	45	400	45
4+50SE	1+40NE	160	48	190	43
4+50SE	1+40SW	350	48	190	47
4+50SE	1+60SW	280	48	350	47
4+50SE	1+80SW	500	48	450	50
4+50SE	2+00SW	850	41	850	42
4+50SE	2+17SW	850	41	1100	40
5+00SE	0+00	400	45	600	45
5+00SE	0+20NE	300	43	300	41
5+00SE	0+20SW	550	41	300	43
5+00SE	0+40NE	900	41	750	39
5+00SE	0+40SW	200	37	500	33
5+00SE	0+60NE	1000	36	1500	34
5+00SE	0+60SW	300	30	300	30

		SEATTLE		HAWAII	
LINE	STATION	RES OHM-M	PHASE ANGLE	RES OHM-M	PHASE ANGLE
5+00SE	0+80NE	1700	35	1500	36
5+00SE	0+80SW	500	32	450	32
5+00SE	1+00NE	1000	35	1100	34
5+00SE	1+00SW	110	24	400	30
5+00SE	1+20NE	350	39	350	37
5+00SE	1+20SW	140	50	130	51
5+00SE	1+40SW	350	41	600	43
5+00SE	1+60SW	550	42	650	43
5+00SE	1+80SW	900	42	700	37
5+00SE	2+00SW	500	49	400	49
5+00SE	2+20SW	550	45	650	41
5+50SE	0+00	600	40	600	41
5+50SE	0+20NE	450	45	750	42
5+50SE	0+20SW	170	42	220	43
5+50SE	0+30SW	650	26	800	28
5+50SE	0+40NE	200	43	300	47
5+50SE	0+40SW	1100	25	1400	25
5+50SE	0+50SW	650	31	550	29
5+50SE	0+60NE	500	43	500	45
5+50SE	0+60SW	350	28	200	24
5+50SE	0+80NE	1200	35	950	40
5+50SE	0+80SW	130	35	85	32
5+50SE	0+90NE	2300	33	1800	35
5+50SE	1+00NE	3000	35	2400	37
5+50SE	1+00SW	95	30	70	42
5+50SE	1+10NE	1500	32	1500	35
5+50SE	1+20NE	1300	35	1300	37
5+50SE	1+20SW	280	30	220	35
5+50SE	1+40NE	850	38	500	39
5+50SE	1+40SW	300	35	400	42
5+50SE	1+60SW	400	43	450	42
5+50SE	1+70SW	500	40	1100	39
5+50SE	1+80SW	1200	42	800	40
5+50SE	1+90SW	1800	40	750	40
5+50SE	2+00SW	1300	41	350	40
5+50SE	2+10SW	550	39	350	39
5+50SE	2+20SW	450	42	850	42
6+00SE	0+00	250	42	850	42
6+00SE	0+20NE	500	42	800	42
6+00SE	0+20SW	750	37	650	35
6+00SE	0+40NE	230	42	230	48
6+00SE	0+40SW	140	40	280	37
6+00SE	0+60NE	650	42	650	42
6+00SE	0+60SW	220	32	2200	28
6+00SE	0+70NE	450	42	1000	42
6+00SE	0+80NE	350	47	350	47
6+00SE	0+80SW	90	32	55	20
6+00SE	1+00NE	700	37	900	37
6+00SE	1+00SW	210	40	180	35
6+00SE	1+10NE	1900	34	2000	34
6+00SE	1+20NE	5000	30	5000	32

		SEATTLE		HAWAII	
LINE	STATION	RES OHM-M	PHASE ANGLE	RES OHM-M	PHASE ANGLE
6+00SE	1+20SW	110	39	80	43
6+00SE	1+30NE	2200	34	2100	33
6+00SE	1+40NE	2000	30	1400	30
6+00SE	1+40SW	180	42	170	46
6+00SE	1+50NE	1000	36	900	36
6+00SE	1+60NE	950	38	600	36
6+00SE	1+60SW	550	39	400	35
6+00SE	1+70NE	700	35	700	37
6+00SE	1+80NE	650	36	550	33
6+00SE	1+80SW	190	51	190	40
6+00SE	2+00SW	110	45	550	39
6+50SE	0+00	450	39	650	43
6+50SE	0+20NE	400	40	300	47
6+50SE	0+20SW	650	42	600	39
6+50SE	0+40NE	750	47	950	42
6+50SE	0+40SW	550	39	450	40
6+50SE	0+60NE	400	51	700	42
6+50SE	0+60SW	200	45	260	45
6+50SE	0+70SW	180	40	600	45
6+50SE	0+80NE	450	48	450	47
6+50SE	0+80SW	140	40	700	46
6+50SE	0+90SW	550	39	950	39
6+50SE	1+00NE	500	47	600	47
6+50SE	1+00SW	300	41	850	38
6+50SE	1+10NE	300	44	300	41
6+50SE	1+10SW	350	38	600	35
6+50SE	1+20NE	400	45	800	42
6+50SE	1+20SW	300	36	550	28
6+50SE	1+30NE	1500	34	1400	34
6+50SE	1+40NE	2800	30	3000	32
6+50SE	1+40SW	90	44	80	42
6+50SE	1+50NE	4500	30	4000	30
6+50SE	1+60NE	1000	31	1100	32
6+50SE	1+60SW	110	39	90	36
6+50SE	1+70NE	650	37	650	32
6+50SE	1+80SW	100	41	70	37
6+50SE	2+00SW	700	28	240	32
7+00SE	0+00	1900	40	1000	42
7+00SE	0+10NE	2400	41	1000	43
7+00SE	0+20NE	1800	43	1300	42
7+00SE	0+40NE	1400	44	1500	43
7+00SE	0+60NE	850	45	900	39
7+00SE	0+80NE	600	48	750	43
7+00SE	1+00NE	500	46	550	48
7+00SE	1+20NE	700	43	600	45
7+00SE	1+30NE	300	43	350	39
7+00SE	1+40NE	850	35	850	37
7+00SE	1+50NE	1200	32	1200	32
7+00SE	1+60NE	4500	39	6000	27
7+00SE	1+70NE	3000	25	3500	27
7+00SE	1+80NE	650	30	750	29

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
7+00SE	1+90NE	650	33	750	31
7+50SE	0+00	75	55	40	60
7+50SE	0+20NE	550	50	450	51
7+50SE	0+40NE	1700	45	1400	45
7+50SE	0+50NE	5000	41	4500	41
7+50SE	0+60NE	3500	45	3000	45
7+50SE	0+70NE	2200	36	3000	37
7+50SE	0+80NE	400	60	450	57
7+50SE	1+00NE	600	45	600	48
7+50SE	1+20NE	800	45	900	45
7+50SE	1+40NE	300	47	250	47
7+50SE	1+60NE	650	39	700	39
7+50SE	1+70NE	1600	31	1800	33
7+50SE	1+80NE	3500	27	5000	26
7+50SE	1+90NE	4000	27	4000	27
7+50SE	2+00NE	1100	27	1200	28
7+50SE	2+20NE	1200	27	1300	38
7+50SE	2+40NE	300	33	350	33
8+00SE	0+00	450	47	500	47
8+00SE	0+20NE	400	56	190	51
8+00SE	0+40NE	1700	47	1100	50
8+00SE	0+50NE	2300	43	3000	43
8+00SE	0+60NE	2100	43	4000	43
8+00SE	0+70NE	2800	42	3000	42
8+00SE	0+80NE	1200	43	1400	44
8+00SE	1+00NE	350	41	350	47
8+00SE	1+20NE	450	41	350	47
8+00SE	1+40NE	1000	41	850	42
8+00SE	1+60NE	180	43	190	38
8+00SE	1+80NE	850	32	1300	32
8+00SE	1+90NE	2000	28	2000	30
8+00SE	2+00NE	2800	26	3000	24
8+00SE	2+10NE	3500	25	5000	23

END OF EMR-16 SURVEY AREA 1

APPENDIX C

AREA 2 EMR-16 DATA

CANASIL EMR-16 SURVEY
AREA 2
1986

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
0+00E	0+00S	650	37	1100	37
0+00E	0+10S	850	36	1400	40
0+00E	0+20S	400	40	1100	40
0+00E	0+30S	650	42	900	43
0+00E	0+40S	650	45	600	47
0+00W	0+00S	800	43	1000	35
0+00W	0+20N	1100	38	1100	41
0+00W	0+30N	2000	38	2200	37
0+00W	0+40N	1200	40	2400	37
0+00W	0+50N	700	43	1100	42
0+00W	0+60N	1400	40	1400	40
0+00W	0+60S	800	38	1200	39
0+00W	0+70N	2000	44	1900	45
0+00W	0+80N	1900	41	1400	48
0+00W	0+80S	900	39	2000	39
0+00W	0+90N	2400	42	1800	44
0+00W	1+00N	2100	39	1600	45
0+00W	1+00S	1100	39	1400	42
0+00W	1+10N	2000	43	1100	43
0+00W	1+20N	550	47	120	63
0+00W	1+20S	1500	40	1200	43
0+00W	1+40N	1200	36	1200	35
0+00W	1+60N	900	50	1900	47
0+00W	1+80N	2500	44	2000	41
0+00W	2+00N	700	60	1900	44
0+00W	2+20N	1900	55	4500	25
0+10E	0+00S	800	37	1000	43
0+10E	0+10N	2600	35	1100	39
0+10E	0+10S	750	35	1100	40
0+10E	0+20N	1300	34	1300	35
0+10E	0+20S	800	40	550	47
0+10E	0+30N	1900	36	2000	37
0+10E	0+30S	850	42	450	47
0+10E	0+40N	850	41	1200	41
0+10E	0+40S	240	47	950	42
0+10E	0+50N	950	40	1100	41
0+10W	0+00S	1500	39	1400	38
0+10W	0+10S	750	39	650	35
0+10W	0+20S	1200	33	200	37
0+10W	0+30S	650	36	1900	39
0+10W	0+40S	750	35	2100	36

		SEATTLE		HAWAII	
LINE	STATION	RES OHM-M	PHASE ANGLE	RES OHM-M	PHASE ANGLE
0+10W	0+50S	1200	37	1300	37
0+10W	2+60S	850	42	1400	36
0+10W	2+80S	1500	37	1700	37
0+10W	3+00S	1050	41	1400	40
0+10W	3+20S	1300	39	1600	38
0+10W	3+40S	700	36	1500	37
0+20E	0+00S	600	41	750	42
0+20E	0+10N	2200	32	950	41
0+20E	0+10S	750	35	1100	40
0+20E	0+20N	3500	36	1400	39
0+20E	0+20S	1100	40	650	47
0+20E	0+30N	1000	40	800	40
0+20E	0+30S	500	45	750	44
0+20E	0+40N	600	45	950	43
0+20E	0+40S	350	47	650	52
0+20E	0+60N	1500	44	1700	43
0+20E	0+60S	1000	36	1200	41
0+20E	0+80N	1200	46	1700	45
0+20E	0+80S	1500	37	1100	37
0+20E	1+00N	3000	36	400	34
0+20E	1+00S	950	40	1700	42
0+20E	1+20N	3500	36	4500	36
0+20E	1+20S	800	42	1300	39
0+20E	1+40N	1700	35	4000	35
0+20E	1+60N	2600	43	3500	42
0+20E	1+80N	2700	46	2300	42
0+20E	2+00N	1200	43	2800	46
0+20E	2+20N	400	55	1000	42
0+20W	0+00S	950	40	350	41
0+20W	0+10S	1200	42	1400	34
0+20W	0+14N	105	45	400	40
0+20W	0+20S	800	35	700	38
0+20W	0+30S	1400	34	1800	35
0+20W	0+40N	1500	39	1900	37
0+20W	0+40S	800	36	1500	35
0+20W	0+50S	950	40	1500	36
0+20W	0+60N	800	43	1100	42
0+20W	0+60S	1300	39	900	35
0+20W	0+80N	1900	37	2800	38
0+20W	0+80S	1000	38	1300	36
0+20W	1+00N	2000	38	1100	43
0+20W	1+00S	1300	42	1600	40
0+20W	1+20N	2100	42	950	43
0+20W	1+40N	3000	45	1100	44
0+20W	1+60N	1800	48	1050	43
0+20W	1+80N	2000	42	1300	34
0+20W	2+00N	900	47	1100	43
0+20W	2+20N	140	40	1600	41
0+30E	0+00S	350	39	900	44
0+30E	0+10N	2000	30	800	33
0+30E	0+10S	850	40	800	44

		SEATTLE		HAWAII	
LINE	STATION	RES OHM-M	PHASE ANGLE	RES OHM-M	PHASE ANGLE
0+30E	0+20N	3000	27	500	42
0+30E	0+20S	750	42	1200	42
0+30E	0+30N	400	42	900	42
0+30E	0+30S	700	42	1300	43
0+30E	0+40N	800	39	1300	43
0+30E	0+40S	500	45	1600	43
0+30E	0+50N	1000	43	1000	45
0+30W	0+00S	500	48	1400	35
0+30W	0+10S	950	37	550	35
0+30W	0+20S	1100	40	1950	32
0+30W	0+30S	950	36	750	33
0+30W	0+40S	1000	33	900	36
0+30W	0+50S	1000	35	1400	35
0+30W	0+60S	1300	35	2200	35
0+30W	0+70S	1600	35	900	36
0+30W	2+60S	1100	40	1900	35
0+30W	2+80S	1300	41	1500	36
0+30W	3+00S	2200	39	1400	37
0+30W	3+20S	1800	36	2000	35
0+30W	3+40S	900	36	1700	35
0+40E	0+10N	1500	31	1400	42
0+40E	0+20N	3000	35	1900	39
0+40E	0+30N	1100	37	1500	41
0+40E	0+40N	1200	34	1800	35
0+40E	0+60N	750	45	1100	42
0+40E	0+60S	900	37	1300	45
0+40E	0+80N	2200	34	1500	40
0+40E	0+80S	900	40	1700	42
0+40E	1+00N	3500	32	3000	35
0+40E	1+00S	600	45	1100	45
0+40E	1+20N	2100	34	2600	38
0+40E	1+20S	1700	35	800	39
0+40E	1+40N	2300	38	3000	40
0+40E	1+60N	900	45	1100	45
0+40E	1+80N	2500	43	1500	47
0+40E	2+00N	1000	53	1300	46
0+40E	2+20N	1200	40	500	48
0+40E	2+40N	500	56	1200	47
0+40W	0+00S	700	42	800	40
0+40W	0+00S	750	37	1200	42
0+40W	0+10S	300	42	650	47
0+40W	0+10S	950	39	750	34
0+40W	0+20S	800	34	700	38
0+40W	0+20S	700	40	1300	42
0+40W	0+30S	1100	40	1400	43
0+40W	0+30S	1600	42	2200	35
0+40W	0+40S	850	40	1300	43
0+40W	0+40S	1200	36	1800	35
0+40W	0+50S	1600	36	2000	40
0+40W	0+60S	1800	35	1100	36
0+40W	0+80S	700	42	550	40

		SEATTLE		HAWAII	
LINE	STATION	RES OHM-M	PHASE ANGLE	RES OHM-M	PHASE ANGLE
0+40W	1+00S	1100	38	850	42
0+40W	1+20S	1950	42	1800	40
0+40W	1+20S	1200	39	1700	42
0+40W	1+40S	1100	38	1400	36
0+40W	1+40S	950	43	900	43
0+40W	1+60S	750	46	1100	42
0+50E	0+00S	1500	32	1100	41
0+50E	0+10N	2600	29	900	39
0+50E	0+20N	2400	32	750	38
0+50E	0+30N	600	41	1000	41
0+50E	0+40N	700	40	1200	45
0+50E	0+50N	1000	40	1400	40
0+50E	0+60N	1000	41	750	45
0+50W	0+00S	950	40	1100	39
0+50W	2+60S	1000	40	1400	35
0+50W	2+80S	1600	39	2100	31
0+50W	3+00S	3500	37	3500	33
0+50W	3+20S	1700	37	2400	33
0+50W	3+40S	800	38	1700	33
0+50W	3+60S	750	44	1300	35
0+50W	3+80S	1100	40	3000	33
0+50W	4+00S	1600	39	2500	33
0+50W	4+20S	1100	37	2100	34
0+50W	4+40S	2000	38	3000	32
0+60E	0+00S	1400	33	850	40
0+60E	0+20N	1400	30	750	39
0+60E	0+20S	1100	39	750	51
0+60E	0+30N	1600	30	600	39
0+60E	0+40N	1200	37	1050	31
0+60E	0+40S	700	40	400	55
0+60E	0+60N	750	35	1100	41
0+60E	0+60S	750	39	500	48
0+60E	0+80N	1700	34	1200	38
0+60E	0+80S	1200	37	1050	44
0+60E	1+00N	2400	30	2000	43
0+60E	1+00S	1600	36	700	45
0+60E	1+20N	1000	39	1300	50
0+60E	1+20S	1100	35	850	43
0+60E	1+40N	2200	37	1700	45
0+60E	1+60N	1800	42	1400	47
0+60E	1+80N	2300	40	750	55
0+60E	2+00N	1400	40	1500	43
0+60E	2+20N	2600	39	3500	37
0+60E	2+40N	450	39	1500	56
0+60E	2+60N	250	65	1200	35
0+60W	0+00S	750	38	1700	34
0+60W	0+10S	1000	40	1600	39
0+60W	0+20S	950	39	1100	40
0+60W	0+30S	350	41	900	37
0+60W	0+40S	1200	39	550	34
0+60W	0+50S	2100	37	1300	37

		SEATTLE		HAWAII	
LINE	STATION	RES OHM-M	PHASE ANGLE	RES OHM-M	PHASE ANGLE
0+60W	0+60S	1600	37	1100	38
0+60W	0+70S	700	39	950	42
0+60W	0+80S	850	36	600	41
0+60W	1+00S	900	41	1000	45
0+60W	1+20S	1100	37	750	39
0+60W	1+40S	1100	37	1300	41
0+60W	1+60S	1800	42	1800	40
0+70E	0+00S	2000	32	1400	42
0+70W	0+00S	900	41	1300	41
0+70W	2+60S	550	42	1900	39
0+70W	2+80S	750	43	2300	36
0+70W	3+00S	2300	37	1900	35
0+70W	3+20S	900	40	1300	34
0+70W	3+40S	1000	36	1400	34
0+70W	3+60S	850	39	1300	40
0+70W	3+80S	1200	40	2200	34
0+70W	4+00S	1000	42	3000	35
0+70W	4+20S	1300	40	3500	34
0+70W	4+40S	850	42	2000	37
0+70W	4+52S	2300	36	1800	36
0+80E	0+00S	1500	36	900	42
0+80W	0+00S	650	40	1500	35
0+80W	0+20S	1200	39	900	37
0+80W	0+40S	650	37	1100	39
0+80W	0+50S	950	39	700	39
0+80W	0+60S	800	38	450	34
0+80W	0+70S	1400	41	1300	41
0+80W	0+80S	1300	36	1100	37
0+80W	0+90S	1000	37	1500	39
0+80W	1+00S	550	37	2300	35
0+80W	1+20S	800	39	1300	39
0+80W	1+40S	850	41	900	43
0+80W	1+60S	1700	38	1500	42
0+90E	0+00S	1600	34	2300	36
0+90W	0+00S	350	45	210	53
0+90W	2+60S	500	41	900	43
0+90W	2+80S	1300	34	1000	37
0+90W	3+00S	800	37	950	36
0+90W	3+14S	550	42	950	43
0+90W	3+60S	1800	36	4500	34
0+90W	3+80S	1000	41	3000	37
0+90W	4+00S	650	43	1600	44
0+90W	4+20S	700	35	1300	37
0+90W	4+40S	2400	34	2200	34
0+90W	4+60S	1500	36	450	42
0+90W	4+80S	3000	32	1400	39
1+00E	0+00S	1400	34	3000	35
1+00W	0+00S	1300	41	2000	36
1+00W	0+20S	850	38	900	39
1+00W	0+40S	650	40	600	43
1+00W	0+60S	450	47	1000	40

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
1+00W	0+80S	600	39	550	40
1+00W	0+90S	1600	37	950	39
1+00W	1+00S	1800	34	1100	41
1+00W	1+10S	800	36	1500	38
1+00W	1+20S	700	40	1100	40
1+00W	1+40S	550	41	1000	40
1+00W	1+60S	2200	36	2100	37
1+00W	1+80S	1200	39	1800	38
1+10E	0+00S	1000	40	3000	34
1+10W	0+00S	900	40	850	47
1+10W	2+60S	850	39	300	38
1+10W	2+80S	500	37	200	43
1+10W	3+00S	1000	36	2000	38
1+10W	3+20S	1750	35	2300	35
1+10W	3+35S	1300	35	1700	40
1+10W	3+80S	950	40	450	49
1+10W	4+00S	400	43	280	53
1+10W	4+20S	300	39	400	38
1+10W	4+40S	2200	32	1500	32
1+10W	4+60S	1200	38	500	43
1+10W	4+80S	2800	34	750	37
1+10W	5+00S	700	42	350	50
1+20E	0+00S	850	43	2000	37
1+20W	0+00S	950	39	650	42
1+20W	0+20S	550	42	450	47
1+20W	0+40S	800	39	450	41
1+20W	0+60S	600	38	400	41
1+20W	0+80S	300	47	750	41
1+20W	0+90S	600	30	550	39
1+20W	1+00S	1600	33	550	42
1+20W	1+10S	1000	33	350	40
1+20W	1+20S	450	35	300	45
1+20W	1+30S	120	38	350	45
1+20W	1+40S	1300	37	700	42
1+20W	1+60S	1500	39	500	40
1+20W	1+80S	550	39	350	51
1+30E	0+00S	950	38	27800	35
1+30W	2+60S	450	42	950	37
1+30W	2+80S	350	43	1100	37
1+30W	3+00S	1000	38	1050	41
1+30W	3+20S	1300	34	170	53
1+30W	3+40S	1300	37	150	49
1+30W	3+60S	1800	35	550	47
1+30W	3+80S	700	42	1100	38
1+30W	4+00S	550	42	1000	34
1+30W	4+10S	150	54	350	51
1+30W	4+20S	450	45	100	61
1+30W	4+30S	450	47	150	47
1+30W	4+40S	3500	34	300	35
1+30W	4+50S	3500	39	400	44
1+30W	4+60S	2600	39	450	51

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
1+30W	4+80S	450	52	750	47
1+30W	5+00S	1450	40	500	52
1+40E	0+00S	950	41	1600	37
1+40W	0+00S	750	39	700	42
1+40W	0+20S	600	39	800	41
1+40W	0+40S	650	39	950	45
1+40W	0+60S	850	38	1200	39
1+40W	0+80S	700	40	950	39
1+40W	1+00S	700	40	1300	39
1+40W	1+10S	800	34	1300	39
1+40W	1+20S	1900	37	1400	39
1+40W	1+30S	800	36	1500	39
1+40W	1+40S	500	36	1700	36
1+40W	1+50S	950	35	2400	37
1+40W	1+60S	1000	38	1400	42
1+40W	1+80S	1050	41	1400	45
1+40W	2+00S	1200	39	950	39
1+50E	0+00S	650	42	900	41
1+50W	2+60S	650	42	1000	41
1+50W	2+80S	450	44	850	43
1+50W	3+00S	1200	35	900	43
1+50W	3+20S	1300	36	1300	35
1+50W	3+40S	1900	37	1100	39
1+50W	3+60S	2400	37	12000	37
1+50W	3+80S	400	45	800	43
1+50W	4+00S	1500	42	850	40
1+50W	4+20S	110	58	1700	42
1+50W	4+40S	2400	35	2000	39
1+50W	4+60W	3500	34	3000	36
1+50W	4+80W	1000	40	2400	39
1+50W	4+90W	1300	34	2000	40
1+60E	0+00S	500	43	1500	35
1+60W	0+00S	700	40	900	42
1+70W	1+00S	550	43	1300	35
1+70W	1+20S	800	37	500	44
1+70W	1+40S	850	43	1000	41
1+70W	1+60S	700	42	2300	36
1+70W	1+80S	850	45	850	45
1+70W	2+00S	550	46	1100	42
1+70W	2+20S	750	43	950	42
1+70W	2+40S	700	45	750	42
1+70W	2+60S	450	44	700	42
1+70W	2+80S	900	39	1400	37
1+70W	3+00S	1100	39	1400	40
1+70W	3+20S	1000	40	1000	40
1+70W	3+40S	2400	34	1300	40
1+70W	3+60S	1700	37	900	43
1+70W	3+80S	350	47	500	54
1+70W	4+00S	650	47	500	46
1+70W	4+20S	230	50	700	44
1+70W	4+40S	3000	37	3000	40

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
1+70W	4+55S	6500	32	5000	35
1+80W	0+00S	600	47	1000	40
1+90W	1+80S	400	43	1400	36
1+90W	2+00S	700	45	900	42
1+90W	2+20S	650	45	1000	40
1+90W	2+40S	550	43	230	58
1+90W	2+60S	700	42	400	47
1+90W	2+80S	750	41	900	40
1+90W	3+00S	750	40	1000	40
1+90W	3+20S	800	41	1100	40
1+90W	3+40S	3000	33	1300	38
1+90W	3+60S	2000	34	900	39
1+90W	3+80S	1100	41	500	48
1+90W	4+00S	1100	39	1300	42
1+90W	4+20S	2000	34	3000	38
1+90W	4+40S	2000	38	1700	39
2+10W	2+00S	800	45	1300	43
2+10W	2+23S	500	49	750	45
2+10W	2+40S	600	43	1100	38
2+10W	2+60S	1200	41	1700	38
2+10W	2+80S	700	42	1000	40
2+10W	3+00S	1000	39	1000	39
2+10W	3+20S	750	38	1000	38
2+10W	3+40S	1950	35	1600	38
2+10W	3+60S	1700	35	1100	40
2+10W	3+80S	1200	39	750	41
2+10W	4+00S	1800	36	1300	40
2+10W	4+20S	1300	36	1900	38
2+10W	4+40S	2400	32	2100	35
2+30W	2+00S	300	46	750	39
2+30W	2+20S	950	42	650	43
2+30W	2+40S	1100	41	700	46
2+30W	2+60S	950	40	1300	39
2+30W	2+80S	850	41	750	42
2+30W	3+00S	1400	36	1300	35
2+30W	3+20S	850	38	1500	35
2+30W	3+40S	900	39	1100	36
2+30W	3+60S	1500	35	1200	38
2+30W	3+80S	1000	34	1400	40
2+30W	4+00S	1400	37	1000	42
2+30W	4+20S	1100	36	1200	40
2+30W	4+36S	1200	36	750	41
2+50W	3+00S	1600	36	1050	38
2+50W	3+20S	650	40	800	40
2+50W	3+40S	650	37	1100	36
2+50W	3+60S	1000	36	1400	36
2+50W	3+80S	1400	36	1650	37
2+50W	4+00S	1300	34	1300	36
2+50W	4+10S	3500	34	1100	38
2+50W	4+20S	550	39	700	35
2+50W	4+39S	2800	33	1300	34

		SEATTLE		HAWAII	
LINE	STATION	RES OHM-M	PHASE ANGLE	RES OHM-M	PHASE ANGLE
2+70W	3+00S	900	37	600	38
2+70W	3+20S	500	36	850	36
2+70W	3+40S	650	38	850	35
2+70W	3+60S	1400	34	1800	34
2+70W	3+80S	1600	32	3000	33
2+70W	4+00S	1900	34	4000	36
2+70W	4+20S	550	38	2300	39
2+70W	4+38S	1800	34	800	37

END OF EMR SURVEY
AREA 2

APPENDIX D

EMR-16 TEST SURVEY DATA

CANASIL RESOURCES
TEST
SURVEY
AREA 1
1986

LINE	STATION	SEATTLE RES OHM-M	SEATTLE PHASE ANGLE	HAWAII RES OHM-M	HAWAII PHASE ANGLE
0+00	0+00	350	47	300	50
0+00	0+10S	110	54	65	57
0+00	0+20S	750	43	600	47
0+00	0+30S	1600	33	900	43
0+00	0+40S	2500	30	2200	35
0+00	0+10N	450	38	300	43
0+00	0+20N	1100	41	550	46
0+00	0+30N	1900	35	2200	38
0+00	0+40N	400	44	400	44
0+10E	0+00	500	45	750	47
0+10E	0+10N	350	43	650	43
0+10E	0+20N	2000	38	2000	39
0+10E	0+30N	1100	42	1400	43
0+10E	0+40N	750	39	900	41
0+10E	0+10S	220	47	790	51
0+10E	0+20S	450	42	240	43
0+10E	0+30S	2200	34	1000	45
0+10E	0+40S	2100	34	650	47
0+10W	0+00	240	47	290	51
0+10W	0+10N	500	40	500	40
0+10W	0+20N	1100	34	900	34
0+10W	0+30N	1000	38	850	41
0+10W	0+40N	500	42	450	45
0+10W	0+10S	280	49	350	54
0+10W	1+20S	1100	38	1100	41
0+10W	0+30S	1500	34	1500	39
0+10W	0+40S	2800	34	2700	39
0+20W	0+00	130	52	210	54
0+20W	0+10N	350	52	450	60
0+20W	0+20N	700	40	600	42
0+20W	0+30N	1900	31	1700	34
0+20W	0+40N	1100	38	850	40
0+20W	0+10S	600	43	650	49
0+20W	0+20S	1100	35	1300	43
0+20E	0+00	400	43	650	47
0+20E	0+10N	900	38	1500	39
0+20E	0+20N	1100	39	2100	42
0+20E	0+30N	900	38	850	42
0+20E	0+40N	850	39	950	39
0+20E	0+10S	300	46	600	47
0+20E	0+20S	400	43	300	51
0+20E	0+30S	2600	33	1500	38
0+20E	0+40S	2900	31	1000	41
0+20E	0+50S	1100	34	400	47
0+20E	0+60S	1600	35	1100	41

END OF EMR-16 SURVEY MAX TRENCH
JULY 4th 1986

APPENDIX E

ANALYTICAL PROCEDURES

APPENDIX E

GEOCHEMICAL LABORATORY METHODOLOGY - 1986

Sample Preparation

1. Soil samples are dried at 60 degrees Celsius an sieved to -80 mesh.

2. Rock samples are pulverized to -100 mesh.

Geochemical Analysis (AA and ICP)

0.5 gram samples are digested in hot dilute aqua regia in a boiling water bath and diluted to 10 ml with demineralized water. Extracted metals are determined by:

1. ICP Geochemical Analysis - A .500 gram of sample is digested with 3 ml of 3:1:3 nitric acid to hydrochloric acid to water at 90 degrees Celsius for one hour.

   The results are reported in ppm except for : Fe, Ca, P, Mg, Ba, Ti, Al, Na, and K which are in percent.

Geochemical Analysis for Au

10.0 gram samples that have been ignited overnite at 600 degrees Celsius are digested with hot dilute aqua regia, and the clear solution obtained is extracted with Methyl Isobutyl Ketone.

Au is determined in the MIBK extract by Atomic Absorption using background correaction (detection limit = 5 ppb direct AA and 1 ppb grahite AA.)

APPENDIX F

STATEMENT OF EXPENDITURES

APPENDIX F

CANASIL RESOURCES INC.

LIST IF EXPENDITURES: BRENDA GROUP, TOODOGGONE AREA 1986

WAGES

NAME AND POSITION		DAILY RATE	TIME	TOTAL
S.Crawford,	Geologist	$195.00	June 25-Sept 10 1986	$15,405
P.J.Weishaupt,	Manager	$155.00	June 25-Sept 20 1986	$13,485
R.Weishaupt,	Technician	$142.00	June 25-Sept 20 1986	$12,354
H.Stirniman,	Prospector	$ 95.00	June 25-Sept 20 1986	$ 8,265
G.McCrady,	Helper	$ 76.00	June 25-Aug 28 1986	$ 4,940
			TOTAL WAGES	$54,449

TRUCK EXPENSES	**$11,735**
SURVEY EQUIPMENT RENTAL	
EMR-16 $225/WEEK AT 13 WEEKS	$ 2,925
SURVEY SUPPLIES	$ 1,066
LAB FEES	$ 4,570
CAMP AND PROVISIONS 405 MAN DAYS AT $35.00 / DAY	$14,175
AIRCRAFT CHARTER SMITHERS-STURDEE AIRSTRIP MOB AND DEMOB BEACH 18 GROCERY AND SUPPLIES CESSNA 185	$ 8,508
HELICOPTER CHARTER FUEL INCLUDED	$16,182
EQUIPMENT RENTAL WINKIE DRILL, PUMPS, RODS, GENERATOR	$ 4,675
TRAVEL AND ACCOMODATIONS	$ 2,073
FREIGHT	$ 1,407
TOTAL EXPLORATION COST ON THE BRENDA GROUP OF CLAIMS DURING THE 1986 FEILD SEASON	**$121,765**

APPENDIX G

STATEMENT OF QUALIFICATIONS

Paul J. Weishaupt

1160 Tall Tree Lane
North Vancouver, British Columbia

EDUCATION:	High School, Graduated in Agriculture Technology Switzerland
AFFILIATIONS:	Canadian Institute of Mining and Metallurgy Geological Association of Canada
1956 - 1967	Bralorne - Pioneer Mines Exploration and Underground, Junior Geologist
1967 - 1970	Can-Fer Mines Ltd. Toronto Western Exploration Representative
1970 - 1973	Bralorne Resources Ltd. Manager of Exploration
1973 - 1975	Westfor Resources Ltd. Open Pit and Underground Manager
1975 - 1977	Dolmage Mason & Stewart Ltd Soil Reinforcements, Tunnel Rehabilitation Design & Supervision. Project Manager
1977 - 1981	Mcintyre Coal Mines Environmental Consultant
1981 - 1984	Canmine Development Company Inc. President
1984 - present	Weishaupt Exploration Services Ltd. President

Paul J. Weishaupt

Paul J. Weishaupt

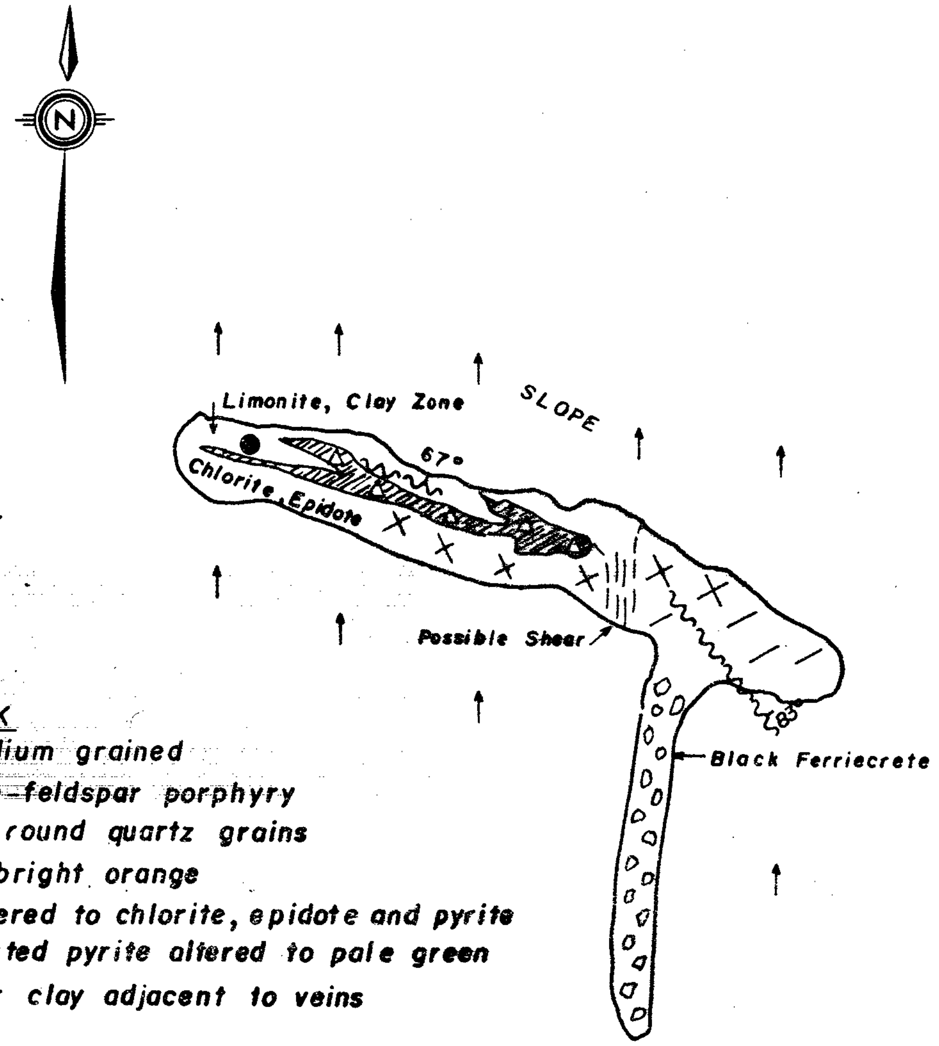
Richard J. Weishaupt

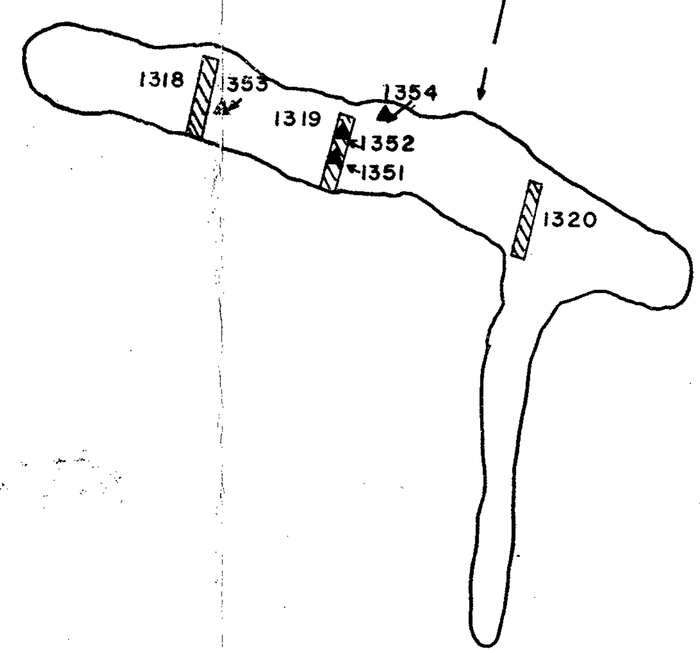
M101-135 west 21st
North Vancouver
British Columbia

EDUCATION :	High School Graduate
	BCIT Graduate Mining Technology 1985
	Surface and Under Ground Mine Rescue 1986
1982 - 1983	June 3rd to August 31st
	Canmine Development Company Inc.
	Geologist Helper
1983 - 1984	June 6th to September 4th
	Canmine Development Company Inc.
	Geologist Helper
1984 - 1985	June 1st to September 30th
	Canmine Development Company
	Mining Technician
1985 - 1986	May 1st to December 31st
	Canasil Resources Inc.
	Project Forman
1986 - 1987	January 1st to Present
	Weishaupt Exploration Services
	Assistant Manager

R J Weishaupt
Richard Weishaupt

Soilsample Ag 0.8ppm Au 10700ppb → Base Line 1+50 SE





ASSAY SAMPLE LOCALITIES

TAG NUMBER	WIDTH	Ag, ppm	Au, ppb
1318	1.1m	35.5	50
1319	1.0m	64.3	125
1320	0.9m	16.7	95
1351	Grab	135.5	220
1352	"	122.5	640
1353	"	77.2	190
1354	Grab	9.5	620

HOSTROCK

fine to medium grained
hornblende-feldspar porphyry
with 1-2% round quartz grains
Feldspar bright orange
mafics altered to chlorite, epidote and pyrite
disseminated pyrite altered to pale green
sericite or clay adjacent to veins

Veins are zoned, sulphides concentraded on footwall
Mineralization Pyrite, Sphalerite, Galena minor Chalcopyrite, Manganese cross-cut by vuggy quartz-calcite veinlets, mineralized as above

LEGEND

- Quartz - Chalcedony Breccia
- Quartz - Chalcedony Veinlets 10%
- Quartz - Chalcedony Veinlets 5%
- Shear
- 1318 Assay tag number Ag/Au (ppm/ppb)
- ● Test Hole

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,555

BRENDA CLAIM TRENCH AT 1+50 SE 0+10 SW

DRAWN BY: P.J.W.	GEOLOGY and ASSAYS	DATE: Dec. 1986
GEOLOGY BY: S.C.	0 1 2 3 4 5 METERS	
SCALE: 1: 100		FIGURE: 1

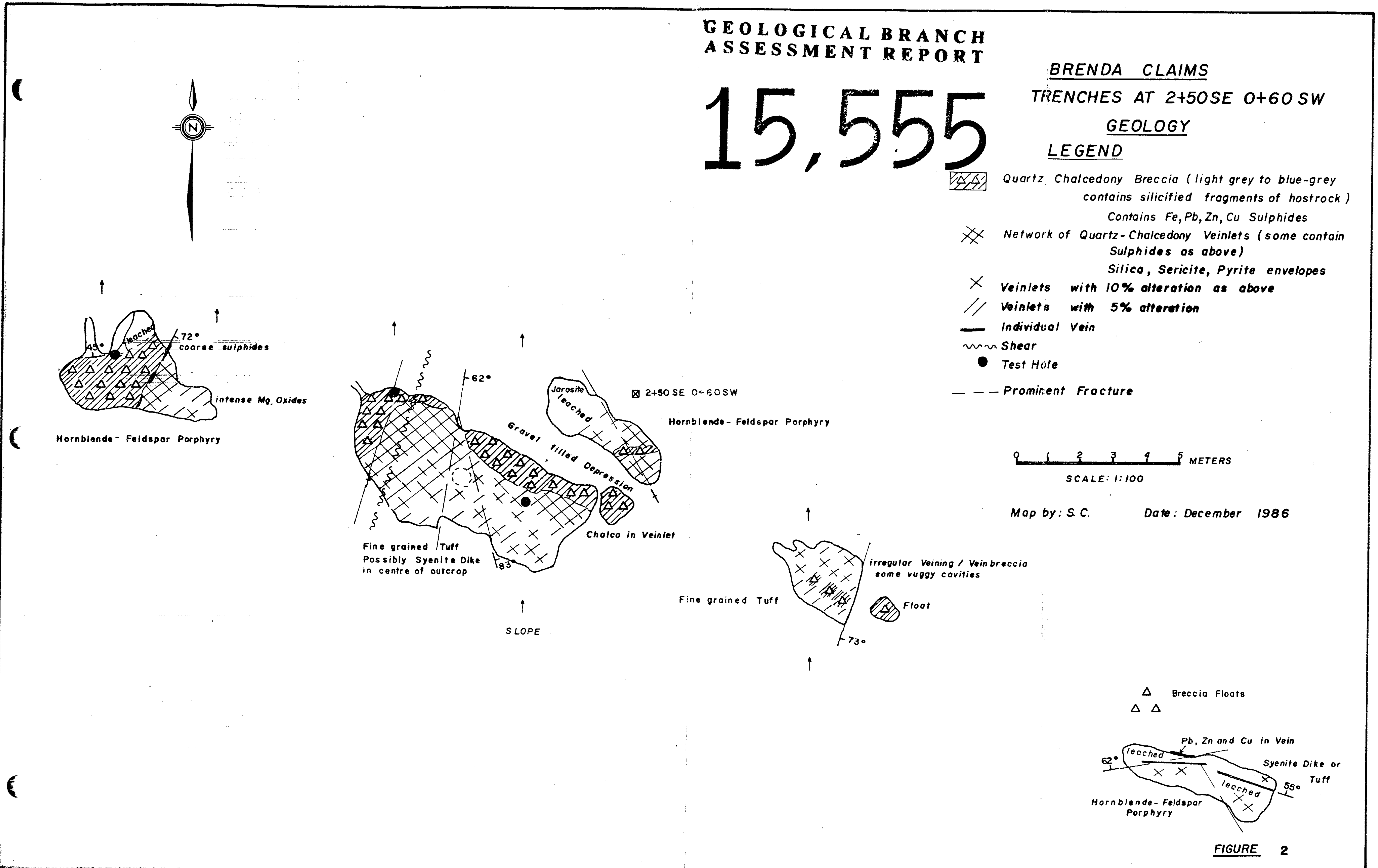
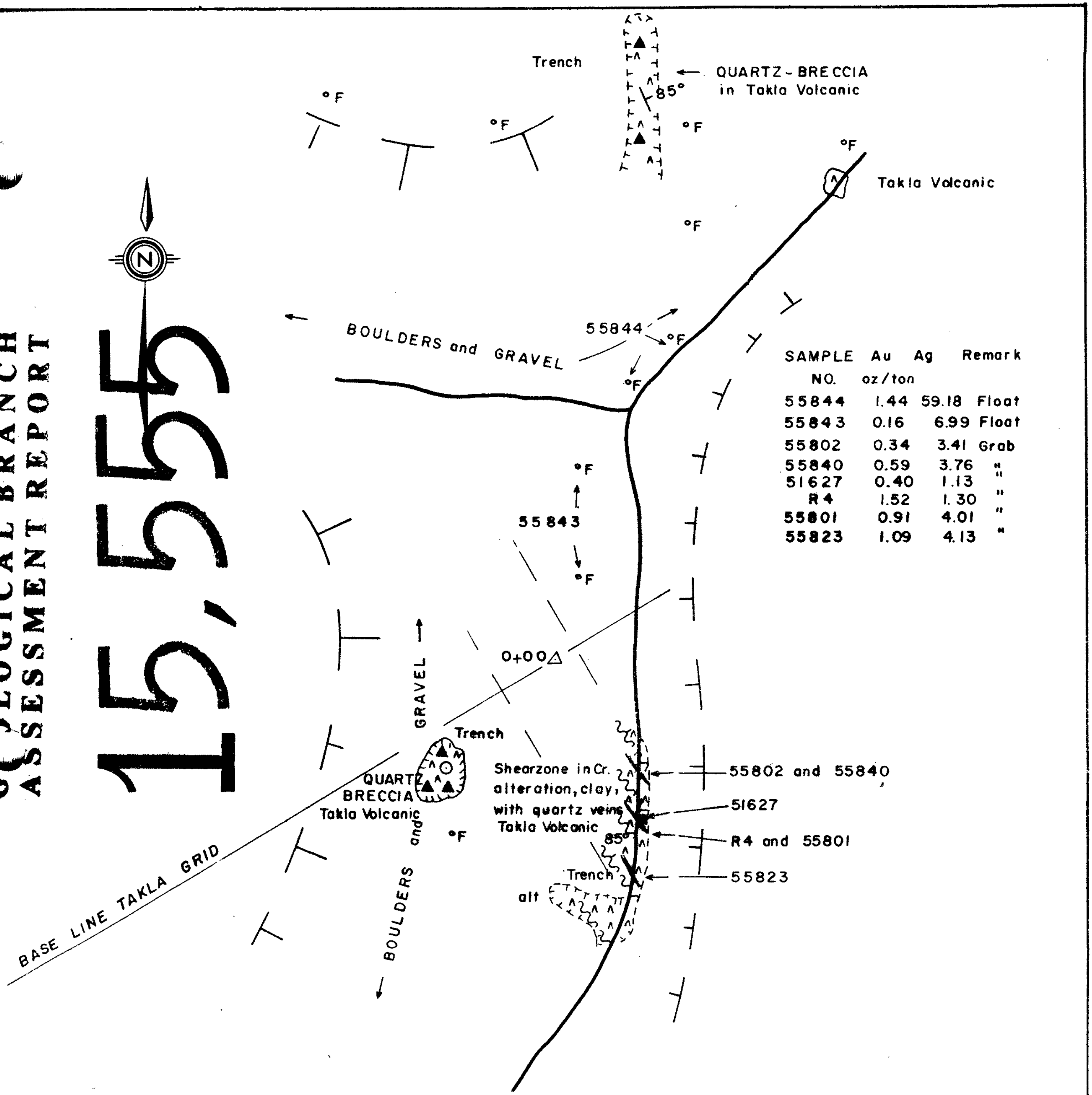

GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
BRENDA CLAIMS
TRENCHES AT 2+50SE 0+60SW
GEOLOGY
LEGEND
Quartz Chalcedony Breccia (light grey to blue-grey contains silicified fragments of hostrock)
Contains Fe, Pb, Zn, Cu Sulphides
Network of Quartz-Chalcedony Veinlets (some contain Sulphides as above)
Silica, Sericite, Pyrite envelopes
Veinlets with 10% alteration as above
Veinlets with 5% alteration
Individual Vein
Shear
Test Hole
Prominent Fracture
0 1 2 3 4 5 METERS
SCALE: 1:100
Map by: S.C.
Date: December 1986
N
leached
72°
45°
coarse sulphides
intense Mg. Oxides
Hornblende- Feldspar Porphyry
62°
Gravel filled Depression
Jarosite
leached
2+50 SE 0+60 SW
Hornblende- Feldspar Porphyry
Chalco in Veinlet
Fine grained Tuff
Possibly Syenite Dike in centre of outcrop
83°
SLOPE
irregular Veining / Vein breccia
some vuggy cavities
Fine grained Tuff
Float
73°
Breccia Floats
Pb, Zn and Cu in Vein
leached
62°
Syenite Dike or Tuff
leached
55°
Hornblende- Feldspar Porphyry

FIGURE 2



SAMPLE NO.	Au oz/ton	Ag	Remark
55844	1.44	59.18	Float
55843	0.16	6.99	Float
55802	0.34	3.41	Grab
55840	0.59	3.76	"
51627	0.40	1.13	"
R4	1.52	1.30	"
55801	0.91	4.01	"
55823	1.09	4.13	"

BRENDA CLAIM GROUP MAP AREA 2 Takla Vein

DRAWN BY: P.J.W.

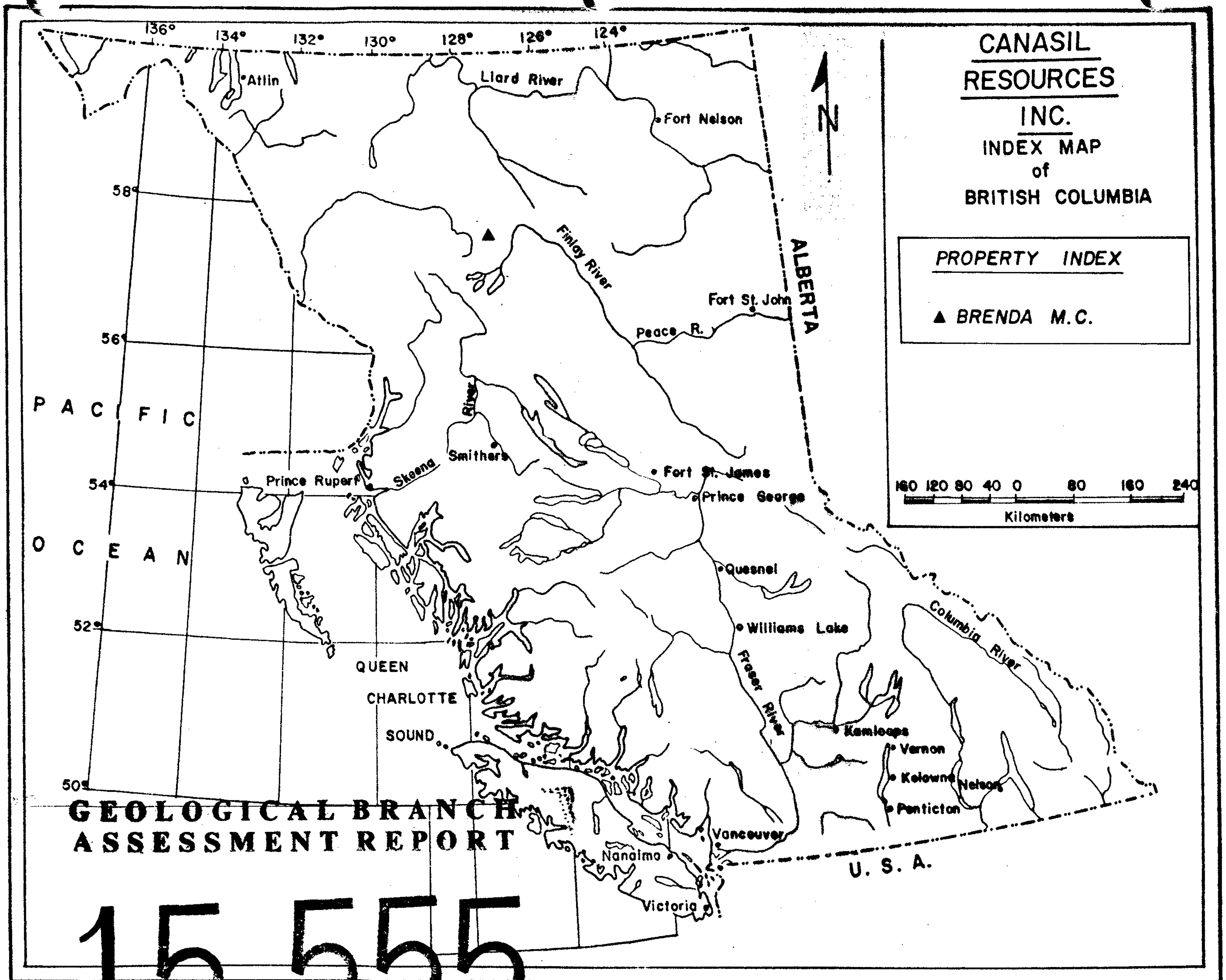
TAKLA VEIN TRENCHING, ASSAYS

DATE: Dec. 1986

0 2 4 6 8 10
METER

SCALE: 1:200

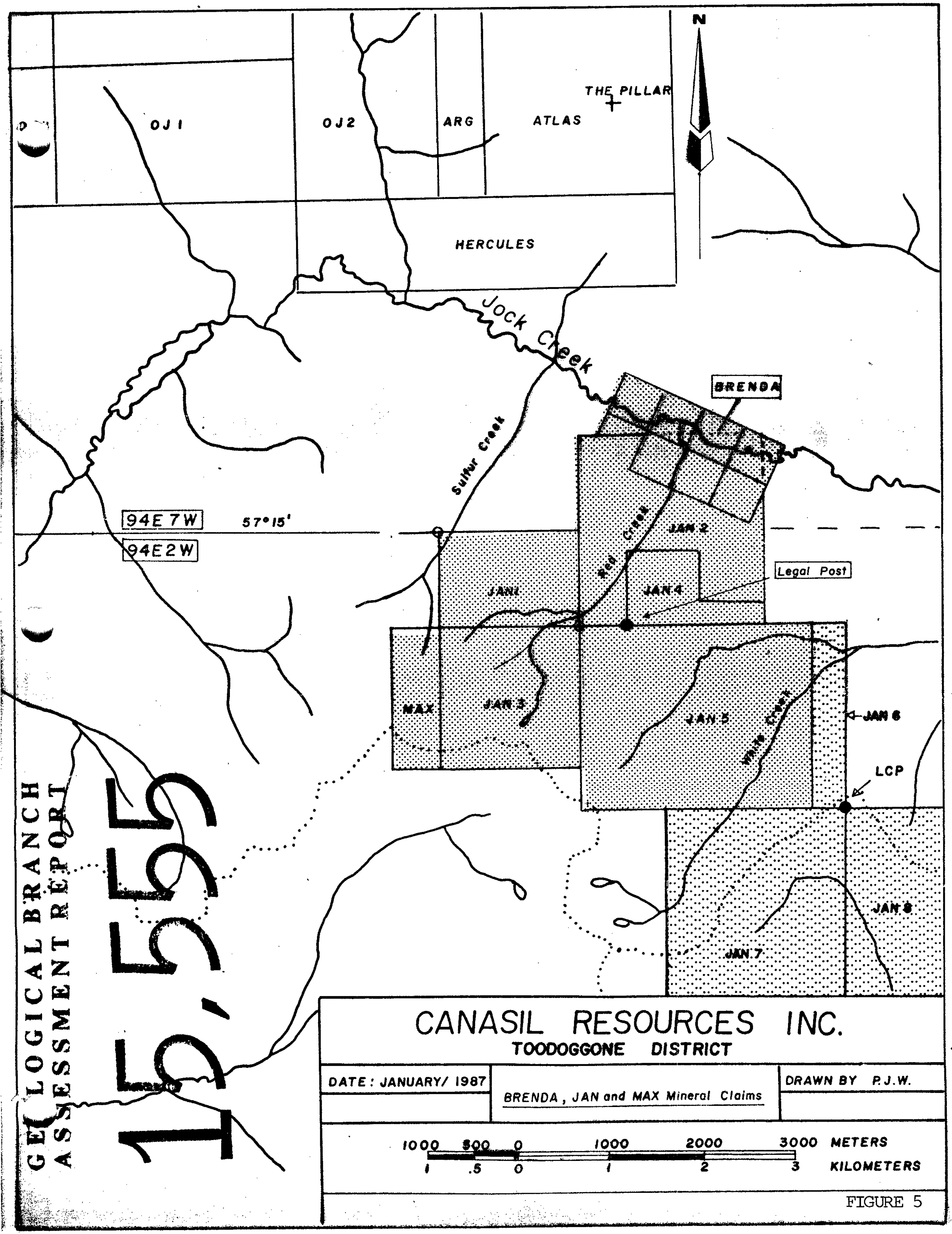
FIGURE: 3



GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,555

FIGURE 4



CANASIL RESOURCES INC.

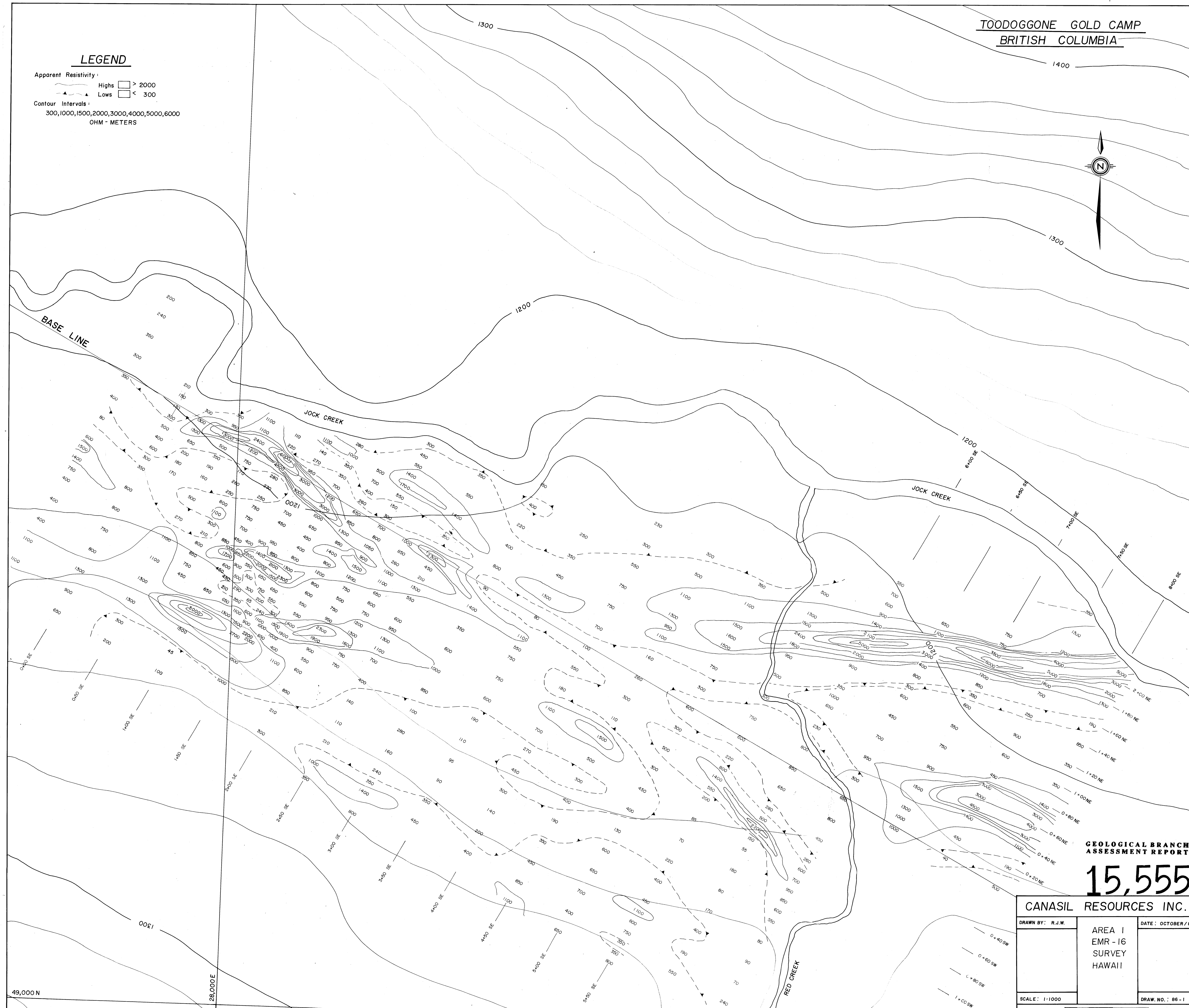
TOODOGGONE DISTRICT

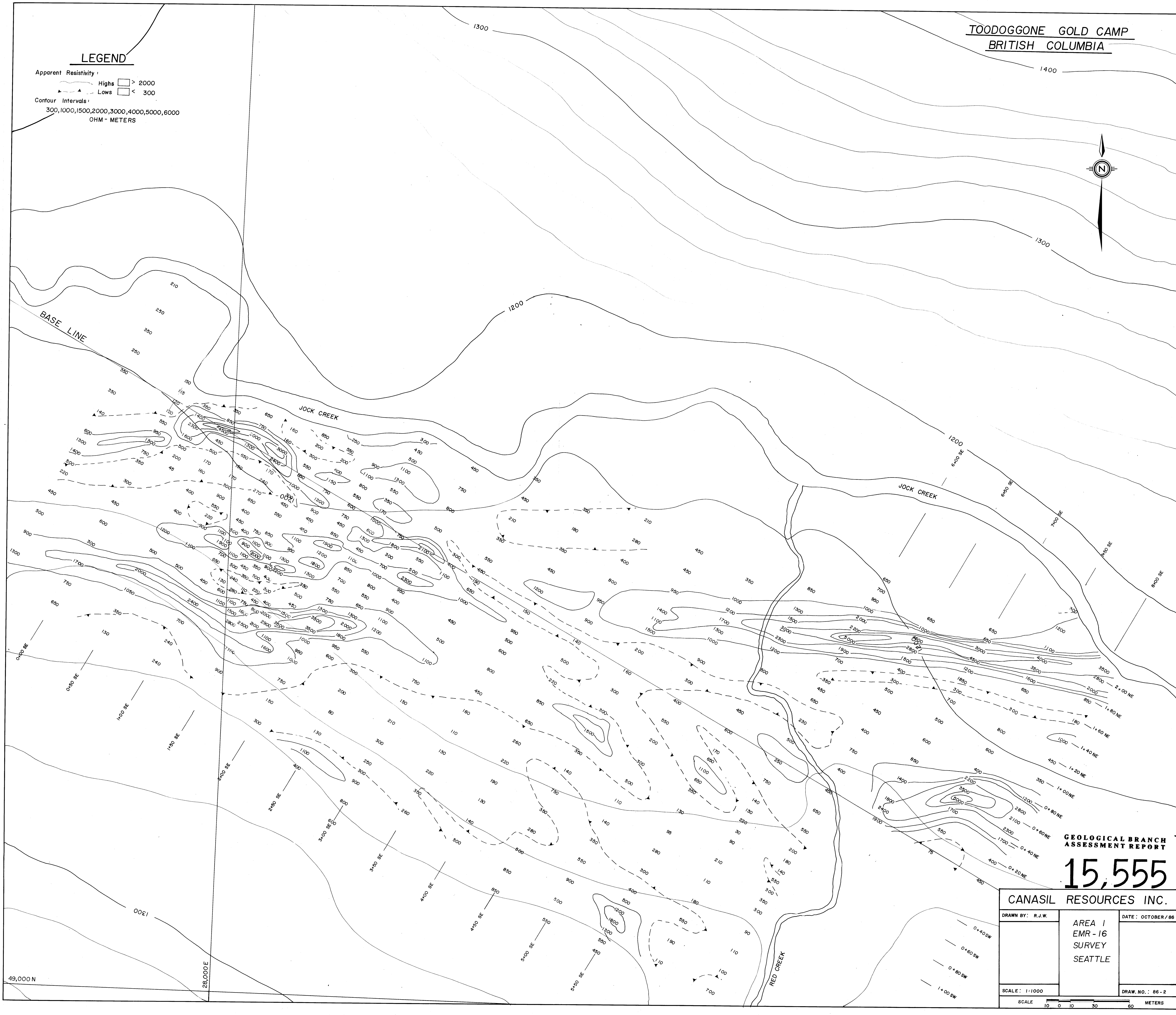
DATE: JANUARY/ 1987

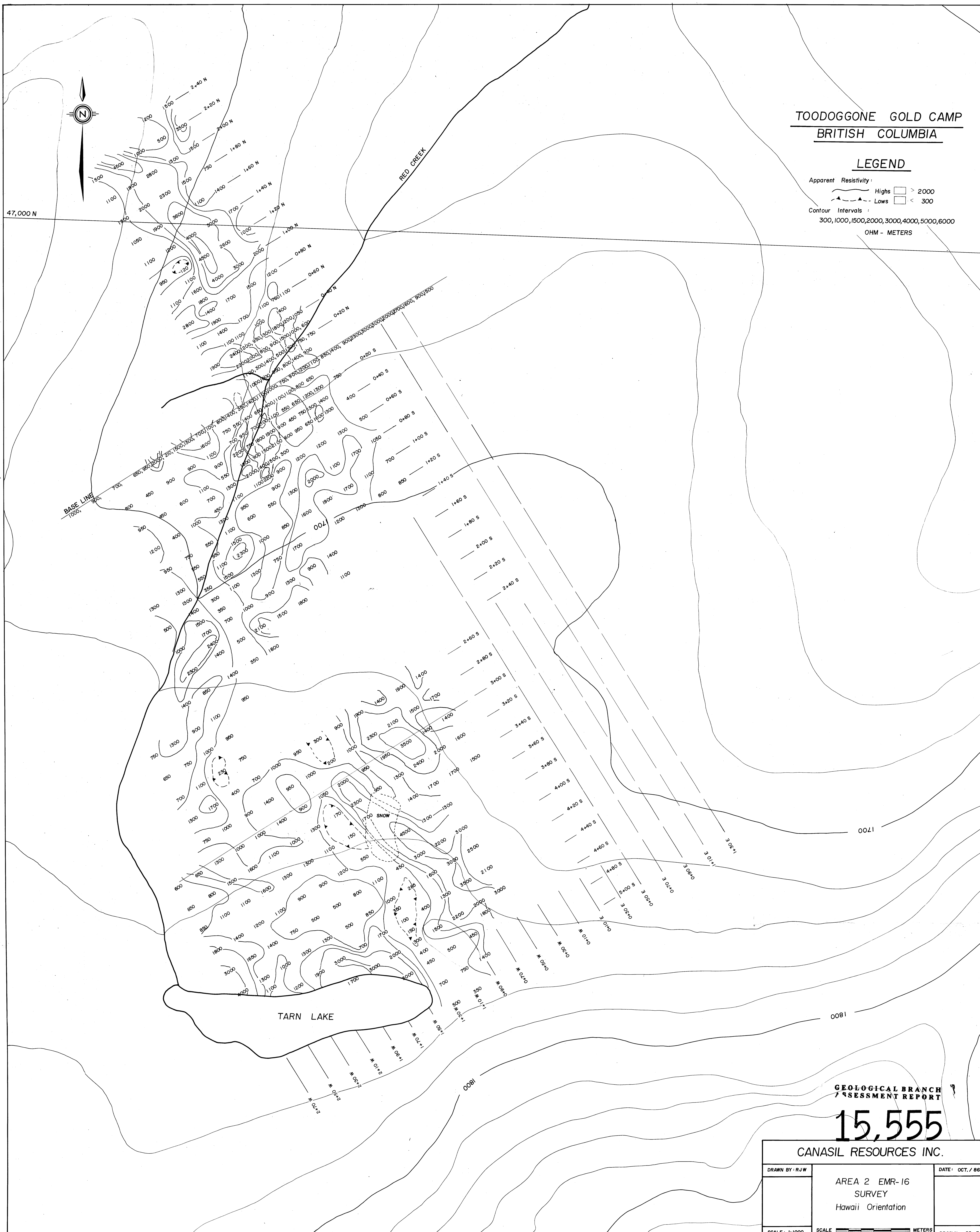
BRENDA, JAN and MAX Mineral Claims

DRAWN BY P.J.W.

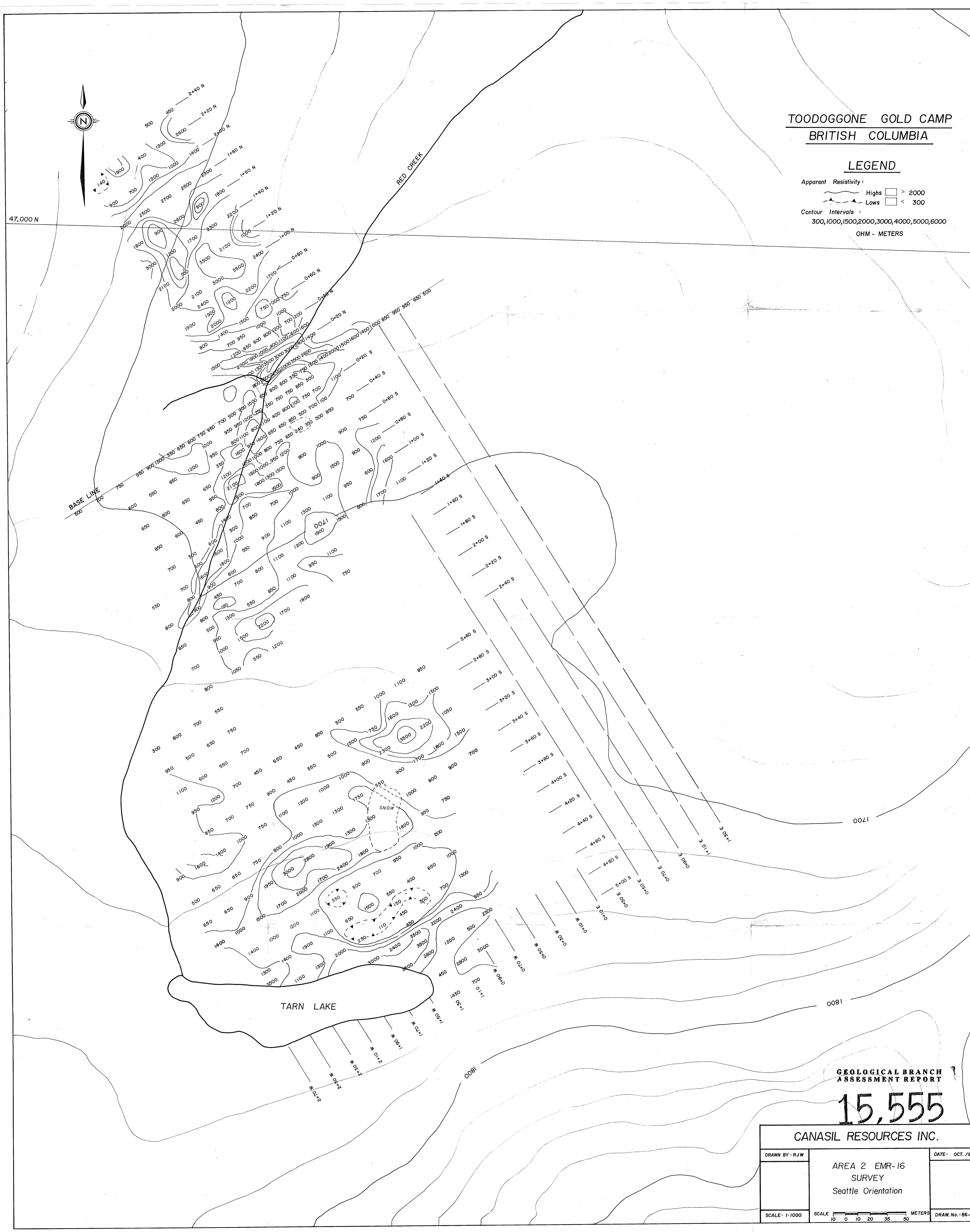
FIGURE 5

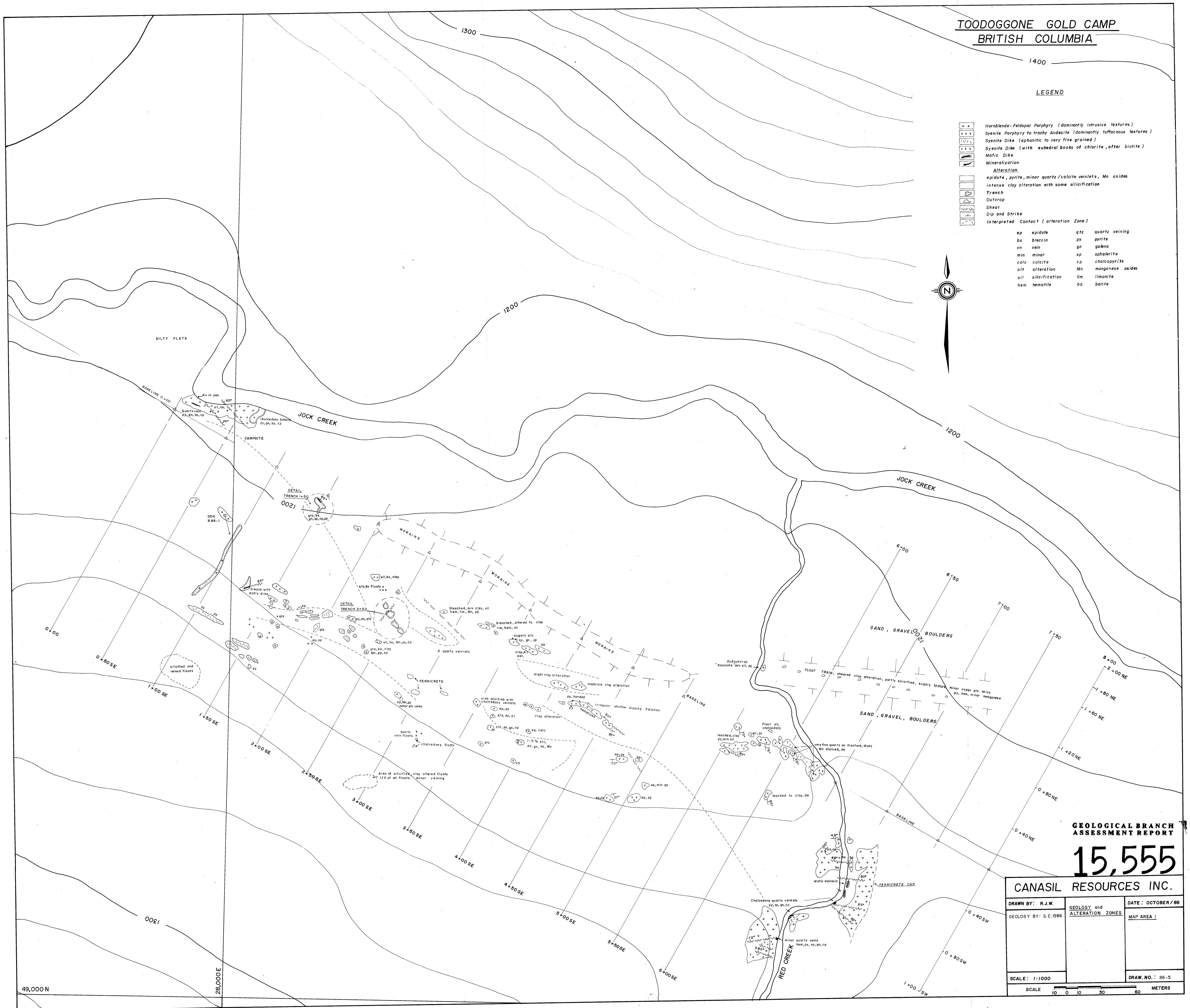

TOODOGGONE GOLD CAMP
BRITISH COLUMBIA
LEGEND
Apparent Resistivity :
Highs > 2000
Lows < 300
Contour Intervals :
300,1000,1500,2000,3000,4000,5000,6000
OHM - METERS
BASE LINE
JOCK CREEK
RED CREEK
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
CANASIL RESOURCES INC.
DRAWN BY: R.J.W.
AREA I
EMR - 16
SURVEY
HAWAII
DATE: OCTOBER/86
SCALE: 1:1000
DRAW. NO.: 86-1
SCALE
METERS
49,000 N
28,000 E


TOODOGGONE GOLD CAMP
BRITISH COLUMBIA
LEGEND
Apparent Resistivity:
Highs > 2000
Lows < 300
Contour Intervals:
300,1000,1500,2000,3000,4000,5000,6000
OHM - METERS
BASE LINE
JOCK CREEK
RED CREEK
49,000 N
28,000 E
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
CANASIL RESOURCES INC.
DRAWN BY: R.J.W.
AREA I
EMR - 16
SURVEY
SEATTLE
DATE: OCTOBER/86
SCALE: 1:1000
DRAW. NO.: 86-2
SCALE
METERS

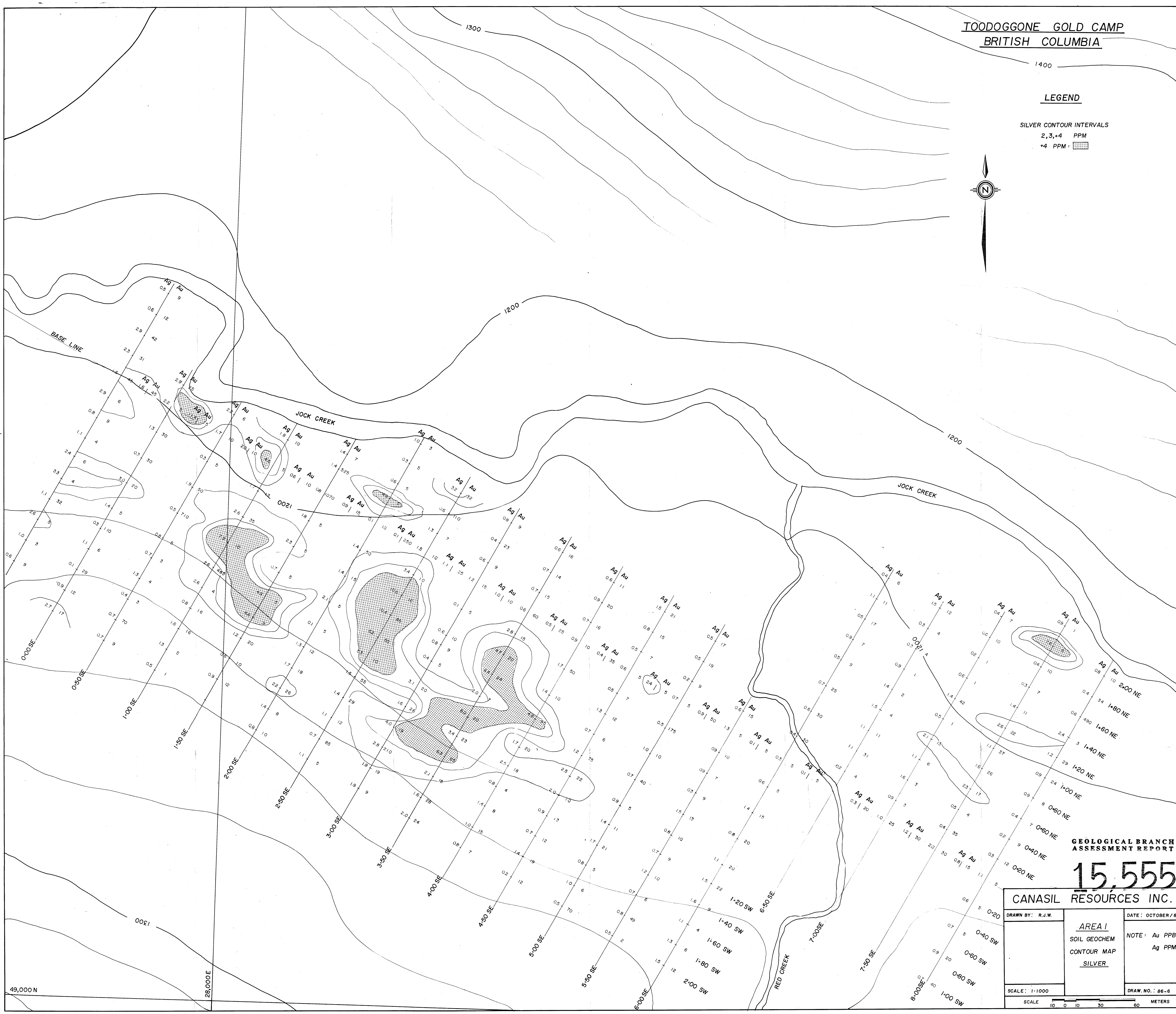


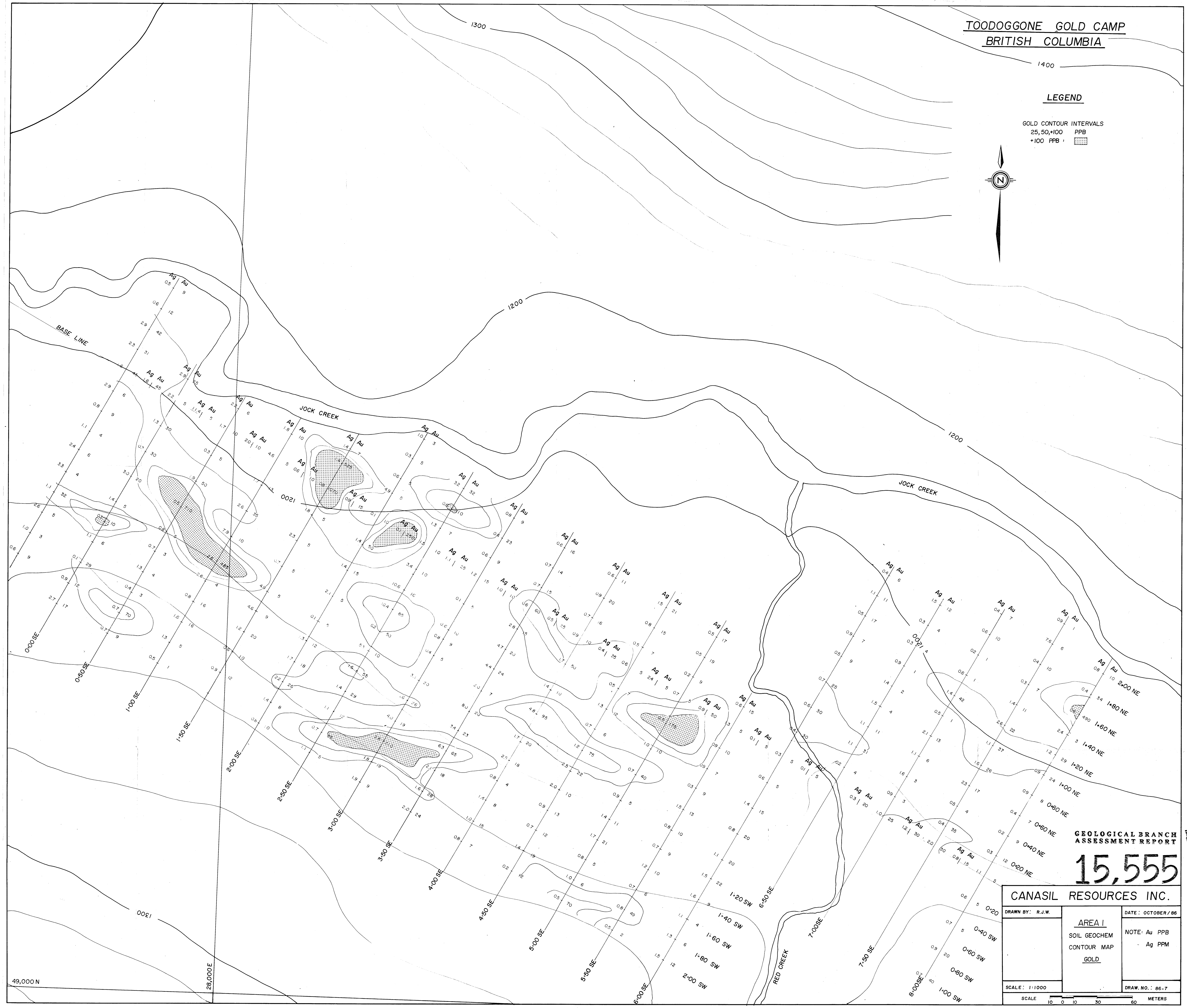
TOODOGGONE GOLD CAMP
BRITISH COLUMBIA
LEGEND
Apparent Resistivity :
Highs > 2000
Lows < 300
Contour Intervals :
300, 1000, 1500, 2000, 3000, 4000, 5000, 6000
OHM - METERS
47,000 N
RED CREEK
BASE LINE
SNOW
TARN LAKE
1700
1800
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
CANASIL RESOURCES INC.
DRAWN BY : RJW
DATE : OCT. / 86
AREA 2 EMR-16
SURVEY
Hawaii Orientation
SCALE : 1:1000
SCALE
10 0 10 20 35 50
METERS
DRAW. No. 86-3

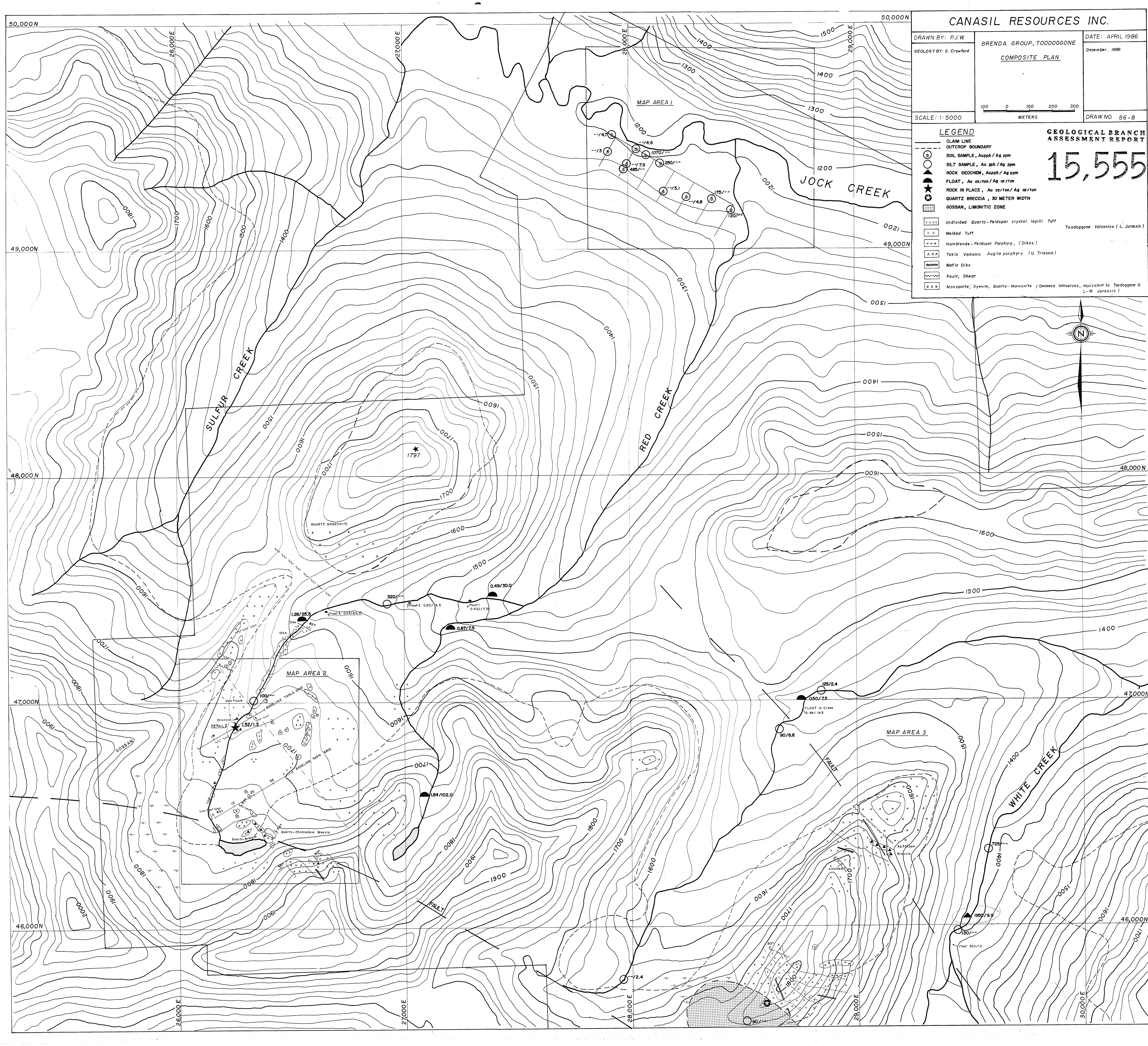

TOODOGGONE GOLD CAMP
BRITISH COLUMBIA
LEGEND
Apparent Resistivity :
Highs > 2000
Lows < 300
Contour Intervals :
300,1000,1500,2000,3000,4000,5000,6000
OHM - METERS
47,000 N
RED CREEK
BASE LINE
TARN LAKE
SNOW
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
CANASIL RESOURCES INC.
DRAWN BY : RJW
DATE : OCT. /86
AREA 2 EMR-16
SURVEY
Seattle Orientation
SCALE : 1:1000
SCALE
METERS
DRAW. No. : 86-4



TOODOGGONE GOLD CAMP
BRITISH COLUMBIA
LEGEND
Hornblende-Feldspar Porphyry (dominantly intrusive textures)
Syenite Porphyry to trachy Andesite (dominantly tuffaceous textures)
Syenite Dike (aphanitic to very fine grained)
Syenite Dike (with euhedral books of chlorite, after biotite)
Mafic Dike
Mineralization
Alteration
epidote, pyrite, minor quartz/calcite veinlets, Mn oxides
intense clay alteration with some silicification
Trench
Outcrop
Shear
Dip and Strike
Interpreted Contact (alteration Zone)
ep epidote
bx breccia
vn vein
min minor
calc calcite
alt alteration
sil silicification
hem hematite
qtz quartz veining
py pyrite
gn galena
sp sphalerite
cp chalcopyrite
Mn manganese oxides
lim limonite
ba barite
N
1300
1400
1200
1200
1300
SILTY FLATS
JOCK CREEK
JOCK CREEK
RED CREEK
BASELINE 0+00
CAMPSITE
DETAIL TRENCH 1+50
DETAIL TRENCH 2+50
DDH 886-1
MORAINE
MORAINE
MORAINE
FERRICRETE
FERRICRETE CAP
SAND, GRAVEL, BOULDERS
SAND, GRAVEL, BOULDERS
BASELINE
BASELINE
Mafic Volcanic
0+00
0+50 SE
1+00 SE
1+50 SE
2+00 SE
2+50 SE
3+00 SE
3+50 SE
4+00 SE
4+50 SE
5+00 SE
5+50 SE
6+00 SE
6+00
6+50
7+00
7+50
8+00
2+00 NE
1+80 NE
1+60 NE
1+20 NE
0+80 NE
0+40 NE
0+40 SW
0+80 SW
1+00 SW
49,000 N
28,000 E
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
CANASIL RESOURCES INC.
DRAWN BY: R.J.W.
GEOLOGY BY: S.C.1986
GEOLOGY and ALTERATION ZONES
DATE: OCTOBER/86
MAP AREA I
SCALE: 1:1000
DRAW. NO.: 86-5
SCALE 10 0 10 30 60 METERS


TOODOGGONE GOLD CAMP
BRITISH COLUMBIA
LEGEND
SILVER CONTOUR INTERVALS
2,3,+4 PPM
+4 PPM
N
JOCK CREEK
RED CREEK
BASE LINE
1200
1300
1400
49,000 N
28,000 E
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
CANASIL RESOURCES INC.
DRAWN BY: R.J.W.
DATE: OCTOBER/86
AREA I
SOIL GEOCHEM
CONTOUR MAP
SILVER
NOTE: Au PPB
Ag PPM
SCALE: 1:1000
DRAW. NO.: 86-6
SCALE
METERS


TOODOGGONE GOLD CAMP
BRITISH COLUMBIA
LEGEND
GOLD CONTOUR INTERVALS
25, 50, +100 PPB
+100 PPB
N
1300
1400
1200
BASE LINE
JOCK CREEK
RED CREEK
Ag Au
0+00 SE
0+50 SE
1+00 SE
1+50 SE
2+00 SE
2+50 SE
3+00 SE
3+50 SE
4+00 SE
4+50 SE
5+00 SE
5+50 SE
6+00 SE
6+50 SE
7+00SE
7+50 SE
8+00SE
2+00 NE
1+80 NE
1+60 NE
1+40 NE
1+20 NE
1+00 NE
0+80 NE
0+60 NE
0+40 NE
0+20 NE
0+20
0+40 SW
0+60 SW
0+80 SW
1+00 SW
1+20 SW
1+40 SW
1+60 SW
1+80 SW
2+00 SW
49,000 N
28,000 E
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
CANASIL RESOURCES INC.
DRAWN BY: R.J.W.
AREA I
SOIL GEOCHEM
CONTOUR MAP
GOLD
DATE: OCTOBER/86
NOTE: Au PPB
- Ag PPM
SCALE: 1:1000
DRAW. NO.: 86-7
SCALE
10 0 10 30 60
METERS


CANASIL RESOURCES INC.
DRAWN BY: P.J.W.
GEOLOGY BY: S. Crawford
BRENDA GROUP, TOODOGGONE
COMPOSITE PLAN
DATE: APRIL 1986
December. 1986
SCALE: 1:5000
100 0 100 200 300
METERS
DRAW.NO. 86-8
LEGEND
CLAIM LINE
OUTCROP BOUNDARY
SOIL SAMPLE, Auppb / Ag ppm
SILT SAMPLE, Au ppb / Ag ppm
ROCK GEOCHEM, Auppb / Ag ppm
FLOAT, Au oz/ton / Ag oz/ton
ROCK IN PLACE, Au oz/ton / Ag oz/ton
QUARTZ BRECCIA, 30 METER WIDTH
GOSSAN, LIMONITIC ZONE
Undivided Quartz-Feldspar crystal lapilli Tuff
Welded Tuff
Toodoggone Volcanics (L. Jurassic)
Hornblende-Feldspar Porphyry, (Dikes)
Takla Volcanic Augite porphyry (U. Triassic)
Mafic Dike
Fault, Shear
Monzonite, Syenite, Quartz-Monzonite (Omineca Intrusives, equivalent to Toodoggone V. L-M Jurassic)
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,555
JOCK CREEK
SULFUR CREEK
RED CREEK
WHITE CREEK
MAP AREA 1
MAP AREA 2
MAP AREA 3
QUARTZ MONZONITE
FAULT
GOSSAN
Quartz-Chalcedony Breccia
1797
50,000N
49,000N
48,000N
47,000N
46,000N
26,000E
27,000E
28,000E
29,000E
30,000E