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Owners): Regional Resources (td.
Western Canadian Mining (WCM) $1+d$.
Operator: Regional Resources $L+d$.

GEOLOGICAL BRANCH ASSESSMENTPTPODT
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GEOCHEMICAL, GEOPHYSICAL
A N D

DIAMOND DRILLING REPORT
on the
BULL 1,5,7, CLIMAX 1,3,8,11,12,13,15Fr, 16Fr, POST 15, WAY 13 CLAIMS

Liard Mining Division, British Columbia N.T.S. 104-0-16

Latitude $59^{\circ} 56^{\prime} \mathrm{N}$; Longitude $130^{\circ} 15^{\prime} \mathrm{W}$

OWNER/OPERATOR: REGIONAL RESOURCES LTD.

## By

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## INTRODUCTION

### 1.3 HISTORY

The history and geology of the Midway property were reviewed by Cordilleran Engineering in 1981, 1982, 1983 and 1984. During this period Cordilleran Engineering actively explored the property on behalf of Regional Resources Ltd. One hundred and three surface holes totalling 28,767 metres were diamond drilled, 153 kilometres of baseline was cut, 61 kilomtres of Pulse EM surveys and 38 kilometres of gravity surveys were performed, and 9850 soil samples were collected and analyzed. Anomalous areas were prospected, and the property was geologically mapped. Twenty-six kilometres of main access road was reconstructed, and two steel beam bridges erected over major rivers.


Table 1 MIDWAY PROPERTY - BRITISH COLUMBIA CLAIMS (e JAN 31/86) 93 Claims ( 967 Units), Liard Mining Division; NTS 104/0-16; Reg. Owner:Reg. Res.


A: Claims in Area A; B: Claims in Area B.
BETH, STAR, RENEE \& TOOTS Registered Owner: Brinco Mining Limited.
NOTE: All '86 Certificates of Work received (accepted as applied).

Near the end of the 1984 surface drilling program in the Silver Creek area, after a mineralized zone approximately 250 metres by 250 metres had been defined, it was decided to start an underground exploraiton program. Underground access was required to determine mining methods and potential problems, to allow close-spaced diamond drilling of the mineral zone, and to permit in-situ examination of mineralization and alteration.

During September and early October, 1984, the infra-structure required trailer complex, dry, shop, power house, settling pond, storage and waste areas, sewer, water and communication systems - was installed. The first round was taken on October 11, 1984; by October 20, 1984, the portal was faced, air, water and ventilation systems in place, and the decline begun. Excavation continued until May 12, 1985, with a month's break for the Christmas holiday. A total of 1440 metres of ramps and drifts were driven during this period.

From these openings 170 core holes were drilled, predominantly on north-south sections 20 metres apart, to determine the shape, grade and continuity of the mineralization. A geological mineral inventory of 968,400 tonnes grading $532.7 \mathrm{gm} / \mathrm{t} \mathrm{Ag}, 10.1 \% \mathrm{~Pb}, 12.0 \% \mathrm{zn}$ and $0.89 \mathrm{gm} / \mathrm{t}$ Au was inferred from the results.

1986 PROGRAM
Between June 1 and October 19, 1986 a number of areas on the Midway property which were geologically similar to the Silver Creek area (shale overlying carbonate) were explored by prospecting, soil sampling, geophysical surveying and diamond and reverse circulation drilling. 72.7 kilometres of line were cut, 2368 soil samples collected, 153.1 line kilometres of magnetometer and 50.7 line kilometres of surface Pulse EM surveys conducted, and 971 metres of reverse circulation drilling and 1762 metres of diamond core drilling completed.

CHAPTER 2

## GEOLOGY

## REGIONAL GEOLOGY

The Midway property area is located within the Cassiar Platform terrain of the Northern Cordillera. Location and relationships with the major geological units of the region are shown in Figure 2.

The Cassiar Platform is an autochthonous miogeosynclinal wedge of relatively shallow-marine carbonate and clastic sediments, ?Proterozoic to Early Mississippian in age. The sedimentary wedge probably plunged to the southwest towards deeper-water depositional environments. During Mid Jurassic to Early Cretaceous times, a complex of oceanic sediments, volcanics and igneous ultramafics (the "Upper Sylvester Allochton", Gordey et al., 1982a) was thrust, probably from the southwest, and emplaced over the platform, which was later intruded by Mid- to Late-Cretaceous quartz monzonite ("Cassiar Batholith").

The Cassiar Platform is bounded to the east by the Rockie Mountain Trench, filled with basinal clastic facies. The trench is marked by a major dextral strike-slip fault along which the Cassiar Platform may have moved over a distance of at least 450 km during Mesozoic and Cenozoic times (Templeman-Kluit and Blusson, 1977). The Midway property area is underlain by Lower and Middle Paleozoic sediments intruded on the west by the Cassiar Batholith. The sedimentary succession has been assigned to the Kechika, Sandpile, McDame and Sylvester Groups (Gabrielse, 1969).

The Cambrian to Lower Silurian Kechika Group consists of siltstone, phyllite and limestone, altered to hornfels and skarns hear the Batholith contact. The Silurian to Middle Devonian Sandpile and McDame Groups consist of quartzite, dolostone and limestone. These Lower Paleozoic sediments were deposited in shallow water and on tidal flats of the Cassiar Platform. The Upper Devonian to Mississippian Lower Sylvester Group consists of a thick section of argillite, sandstone, and
local conglomerate beds. These clastic rocks were deposited by turbidity currents in an offshore basin or trough, which probably developed by subsidence of fault-bounded blocks, possibly associated with a rifting center. The Mississippian to ?Permain Upper Sylvester Group consists of phyllite, chert, local calcarenite beds, volcanic flows and tuffs and ultramafics. This unit is part of the allochthon which was thrust over the Cassiar Platform (Gordey et al., 1982a).


Figure 3 Regional geological setting of the Midway property (Modified after MacIntyre, 1983).

## 2.2 <br> PROPERTY AND DEPOSIT GEOLOGY

The geology of the Midway property in general and of the deposits area in particular was presented in Cordilleran Engineering, 1984. The stratigraphy as it is presently known, through mapping and diamond drilling, is shown on Figure 3.

Massive sulphide deposits have been found in two stratigraphic locations: "exhalative", shale-hosted, stratabound deposits near the base of Unit 2A of the Lower Sylvester Group, and replacement and open space filling, carbonate-hosted deposits at and below the unconformity between the Lower Sylvester and McDame Groups. The former have not proven to be of economic interest; exploration activity since 1982 has focussed on the latter.

The carbonate-hosted sulphide deposits (Lower Zone or LZ) have been found over a vertical interval of lo0m in McDame carbonate, throughout the upper limestone into the top of the underlying dolostone. The most extensively explored deposits are those immediately below the unconformity in the Silver Creek North zone, where sulphides have been found 20 m to 120 m below the surface. Massive sulphides have been intersected at depths between 175 m and 480 m northeast, east and south of the Silver Creek deposits.

The sulphides are spatially associated with, but not restriced to, altered and brecciated carbonate. In the Silver Creek zone there is a preferred azimuth of veins and tabular shaped bodies of 130 degrees to 150 degrees. The deposits vary in width and thickness from centimetres to tens of metres. The minerals of interest are argentiferous galena, sphalerite, and various silver-bearing sulphosalts, almost invariably accompanied by massive pyrite with lesser pyrrhotite and minor marcasite.

Both pre- and post-Sylvester faults have been found. Pre-Sylvester, post-McDame faults do not appear to have acted as barriers to mineralization. Major post-Sylvester faults are oriented northwest-southeast to north-south, dip to the west and have measured displacements of up to 200 m , east side down.

The source of the mineralizing fluids in the Midway area is unknown. Alteration in the Lower Sylvester clastics, apparent mineral zoning and interpretation of aeromagnetic data indicate a center could lie 1.5 km to 2.0 km southeast of the known deposits.


## CHAPTER 3

## GEOCHEMISTRY

Soil samples were collected during 1986 from grids established over various areas of the Midway property. Two of these were the Keystone Mountain and Donegal Mountain grids (Figures 4 and 7).

### 3.1 SAMPLING

Baselines were cut in both areas to establish control for sampling on chain and compass flagged lines. In the Keystone Mountain area flagged lines were run east-west 200 m or 400 m apart, and samples collected at 50m intervals (Plates 2 to 4). A l00m by l00m sampling grid was used in the Donegal Mountain area (Plates 5 to 7). In each area samples were obtained from the "B" soil horizon using a mattock and placed in kraft paper bags. Grid coordinates were used to identify samples; these were written on the bags, and on flagging left at each sample site. All samples were dried in the bags in a propane-fired drying oven at the base camp, and then sieved to produce a - 80 degree mesh fraction analysis.

### 3.2 ANALYSES

All analyses were performed by Bondar-Clegg and Company Ltd., 130 Pemberton Avenue, North Vancouver, B.C. The samples were digested using hot $\mathrm{HNO}: \mathrm{HCl}$ and $\mathrm{Ag}, \mathrm{Pb}$ and Zn determined by atomic absorption spectroscopy (AAS). The lower detection limits were $0.2 \mathrm{ppm} \mathrm{Ag}, 2 \mathrm{ppm}$ Pb and 1 ppm Zn . Copies of the analytical results are appended.

## 3.3

## 3.4

DEFINITION OF ANOMALIES

Between 1981 and 1984, in excess of 10,000 soil samples were collected from various parts of the Midway property and analyzed for Ag, Pb and 2n. From these results the following categories were defined (Cordilleran Engineering, 1981, 1982).

Table 2. ANOMALOUS CATEGORIES FOR Ag, Pb and Zn

## Category

| Background | $<0.9$ | $<59$ | $<245$ |
| :--- | :---: | :---: | :---: |
| Weakly Anomalous | $0.9-1.9$ | $59-142$ | $245-485$ |
| Moderately Anomalous | $2.0-4.2$ | $143-344$ | $486-964$ |
| Anomalous | $>4.2$ | $>344$ | $>964$ |

## KEYSTONE MOUNTAIN

Soil samples were collected on the northeast slope of Keystone Mountain (Figure 4) because surface mapping and interpretation of the airborne resistivity survey flown in 1981 indicated that the area was underlain by Lower Sylvester clastic rocks on the southwest over McDame carbonates on the northeast. 263 samples were collected at 50m intervals on flagged lines 200 m or 400 m apart. Cut base lines in this area totalled 3.2 km.

Histograms for $\mathrm{Ag}, \mathrm{Pb}$ and Zn are presented on Figure 5. The distributions of Pb and Zn are close to $\log$ normal while that for Ag is strongly skewed due to the high detection limit. Cumulative percent frequency plots (Figure 6) indicate that the samples are from a single population. Comparison of the analytical results (Appendix "A") with the categories in Table 2 shows that there is only one sample with weakly to moderately anomalous results in $\mathrm{Ag}, \mathrm{Pb}$ and $\mathrm{Zn}(2.8 \mathrm{ppm}, 74 \mathrm{ppm}$ and 620 ppm , respectively).


REGIONAL RESOURCES LTD.
KEYSTONE MTN. GRID
LOCATION MAP
SCALE $\quad 1: 50,000$


KEYSTONE MTN.
Histograms of $\mathrm{Ag}, \mathrm{Pb}$ and Zn

Figure 5


### 3.5 DONEGAL MOUNTAIN

Exposed on Hamlet, Table, and Donegal Mountains are slices of Sandpile and Kechika Group rocks thrust over younger Lower Sylvester clastics and McDame carbonate. On the northeast slope of Donegal Mountain McDame dolostone was under thrust by Lower Sylvester sandstone and siltstone. Oxidized breccia from the thrust plane was sampled during mapping in 1984, and returned values of 370 to $514 \mathrm{~g} / \mathrm{t} \mathrm{Ag}, 12 \%$ to $26 \% \mathrm{~Pb}$ and $1.7 \%$ to $3.8 \% \mathrm{Zn}$. oxidized material from a kill-zone in the valley between Table and Hamlet Mountains was anomalous in silver. Iron-oxide stained carbonate from the southeast tip of Smoke Mountain carried 1430 ppm zinc, and similar material was found in carbonate below the Lower Sylvester siltstone on Tiger Terrace.

These sampled points are peripheral to the broad, till covered western end of Moose Valley. Outcrops are sparse to non-existant except on Donegal and Table Mountains. The till is composed predominantly of rounded cobbles to boulders of granitic rock (Cassiar intrusive?) in a sandy clay matrix. There are local patches, up to several hundred square metres in area, of dark grey to black shale/siltstone. The mainly till covered area that was sampled was believed to be underlain by McDame carbonate with local patches of overlying Lower Sylvester siltstone/sandstone.

A total of 727 soil samples were collected from the 6.6 square km of the Donegal Mountain grid (Figure 7). Cut lines for control totalled 7.1 km ; 67.4 km of flagged line were sampled. Histograms for $\mathrm{Ag}, \mathrm{Pb}$ and 2 n from these samples are plotted on Figure 8. The distribution of each element is similar to those for the Keystone Mountain samples. Comparing the analytical results to the categories in Table 2 and the results plotted on Plates 5 to 7 it was noted that there were a few areas weakly to moderately anomalous in $\mathrm{Ag}, \mathrm{Pb}$ and Zn . These have been compiled on Figure 10. The cumulative percent frequency plots in Figure 9 indicate the samples are from a single population.

There are a number of weak zinc anomalies (C, E, G, H and I), and five with moderatey anomalous to anomalous results (A, B, D, F and J). Prospecting in these areas revealed that the majority were underlain by soil derived from carbonaceous clastic sediments. Coincident Ag, Pb and Zn anomalies were found only in areas D1, D2 and D3. These are aligned along the thrust fault, between McDame carbonate and Lower Sylvester sandstone, on which the oxidized breccia showing was found in 1984. Additional prospecting along this fault failed to find any sulphides.


REGIONAL RESOURCES LTD.
DONEGAL MTN. GRID

Pb ppm
DONEGAL MTN.
Histograms of $\mathrm{Ag}, \mathrm{Pb}$ and Zn


Figure 8



## CHAPTER 4

## GEOPHYSICS

Magnetometer surveys were conducted in six areas of the Midway property during 1986. A total of 153 line km was surveyed at 12.5 m intervals, using EDA Instrument of Toronto OMNI 4 field and base station magnetometers. The base station magnetometer sampled the earths total magnetic field every ten seconds, and stored the readings. The field unit recorded the total field at each station. The data from each unit was merged daily using computer software supplied by EDA which made the diurnal corrections and subtracted 58,000 nano teslas from each corrected station reading. The data for each line was then fed to an in-house program which used a five point smoothing formula to provide "smoothed" data. The output for each line gives the station coordinates, the "raw" and the "smoothed" data for each reading. Actual readings are obtained by adding 58,000 nt to each value.

It was anticipated that the magnetic results, combined with other knowledge, would help in defining drill targets. After orientation surveys it was concluded that this technique would be most useful as a mapping tool in areas of extensive overburden cover, such as the Donegal Mountain grid.

### 4.1 DONEGAL MOUNTAIN

A total of 77.4 km of magnetometer survey was conducted in the Donegal Mountain area, on flagged lines 100 m apart. Readings were taken at 12.5 m intervals. The area covered is shown on Figure 7. The raw data, minus 58,000 nt, is plotted and contoured on Plate 8 and listed in Appendix " B ". The contours were computer-generated by Data Plotting Services of Toronto.

The majority of the magnetic features on this plate have a north northwest trend, paralleling the regional trend. The most prominent features, the two linear magnetic "highs" between $2600 \mathrm{~N}-4100 \mathrm{~N}$ and 2800E-3600E, correlate with known and inferred basic dykes in McDame carbonate. The offsets in both anomalies at their southeast ends were caused by a known fault.

The linear anomaly between $3900 \mathrm{~N}-4200 \mathrm{~N}$ and $2300 \mathrm{E}-2500 \mathrm{E}$ also overlies an explosed basic dyke. The remainder of the north northwest trending linear anomalies are concluded to indicate similar dykes.

The contour pattern located between $3200 \mathrm{~N}-3300 \mathrm{~N}$ and $3500 \mathrm{E}-4400 \mathrm{E}$ is believed to indicate an east-west structural break. A fault at the location was not previously suspected. A second east-west fault may be located betwen $3500 \mathrm{~N}-3800 \mathrm{~N}$ and 2700E-4200E. The inferred movement would be north side east.

In general, areas underlain by carbonate or quartzite have minor magnetic relief ( $20 \mathrm{nt} / 100 \mathrm{~m}$ ) while areas underlain by Sylvester clastics have somewhat more ( $40 \mathrm{nt} / 100 \mathrm{~m}$ ).

The coincident second-order soil geochemical anomlies described in the previous chapter are located immediately west of and parallel to the strongest magnetic linear. A possible geochemical-magnetic target is at 3050 N on line 2900E. This is the approximate location of the gossan sampled in 1984.

## CHAPTER 5

## DIAMOND DRILLING

All diamond drilling during the 1986 exploration program was done by E . Caron Diamond Drilling Ltd. of Whitehorse, Y. T. One unitized Longyear 38 was used from July 27 to October 27, and a second from September 12 to October 8. Ten holes, totalling 1762 metres, are listed in Table 3.

Table 3. DIAMOND DRILL HOLES, MIDWAY PROPERTY, 1986

| DDH \# | AREA | CLAIM | AZIMUTH | DIP | DEPTH | DAT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MW-86- |  |  |  |  |  |  |  |
| 274 | Tricorn | Climax 11 | 0 | -90 | 157.60 | 6 | Aug-10 Aug |
| 275 | NW Disco | Bull 5 | 0 | -90 | 102.11 | 14 | Aug-17 Aug |
| 276 | Tour Creek | Climax 1 | 0 | -90 | 111.86 | 11 | Aug-13 Aug |
| 280 | NW Disco | Bull 1 | 270 | -70 | 268.83 | 12 | Sep-21 Sep |
| 281 | NW Disco | Bull 1 | 270 | -70 | 228.60 | 19 | Sep-30 Sep |
| 282 | NW Disco | Bull 5 | 170 | -45 | 152.40 | 21 | Sep-25 Sep |
| 283 | NW Disco | Bull 5 | 0 | -90 | 177.39 | 26 | Sep- 2 Oct |
| 284 | NW Disco | Bull 1 | 270 | -70 | 254.20 | 30 | Sep-11 Oct |
| 293 | Tricorn | Climax 12 | 0 | -90 | 137.77 | 3 | Oct-7 Oct |
| 294 | NW Disco | Bull 1 | 50 | -85 | 171.30 | 12 | Oct-19 Oc |

A copy of the Diamond Drill Core Logging Format, and summary copies of each drill hole log giving the pertinent data, are appended, as are copies of the Assay and Analysis Records.

Diamond drilling in 1986 was concentrated in three areas where shales were known or suspected to overlie carbonates. Three holes (274, 276,293) were drilled on the Tr icorn Mountain grid approximatley 3 km south southeast of the Silver Creek deposits. The remainder were on the NW Disco grid; four (280, 281, 2281, 284, 294) in the vicinity of holes 81 and 88 in the southeast corner of the grid (NW Disco South) and three (275, 282, 283) north of Tricorn Mountain near the center of the grid, 1.5 to 2 km north northwest of the deposits. The results by area are discussed below.

### 5.1 TRICORN MOUNTAIN

A relatively complete stratigraphic section, from Lower Sylvester clastic rocks on the south to Upper Kechika carbonaceous siltstones on the north, is exposed on Tricorn Mountain. Geological, geochemical and geophysical surveys previously conducted on the Tour Creek grid (Cordilleran Engineering 1981, 1982) east of Silvertip Creek were extended west on to Tricorn Mountain. Two target areas were chosen to be tested by diamond drilling, one low on the east flank of Tricorn Mountain and the second at the mouth of Tour Creek (Plate 8). Surface mapping indicated that the desired Sylvester/McDame contact was located just below the valley bottom; the drill targets were chosen after interpretation of the surface Pulse EM data.

A total of 3.0 km of access road was constructed using Caron's D-6C bulldozer. DDH MW-86-274 was collared on the lower slope of Tricorn Mountain; the core confirmed that the Sylvester/McDame contact was about 50 m below the valley. No sulphides or breccias were intersected; the YBR intervals probably represent altered dykes, with the upper one occupying a fault between McDame limestone units ML2 and ML5. A large number of partially to strongly altered, steeply dipping basic dykes are exposed in the limestone on Tricorn Mountain.

DDH MW-86-293 was drilled 60m north of MW-86-274. The McDame/Sylvester contact in DDH 293 was 23 m higher than in DDH 274. This gives an apparent dip of 20 degrees to the south, similar to the dips exposed in the strata on Tricorn Mountain. Sixty metres of variably brecciated and recrystallized Upper McDame limestone was intersected. Four intervals totalling 3.22 m of red to orange iron oxide and oxide-stained limestone were found between 103 m and 118.2 m depth. These returned geochemically anomalous values in Zn , but low values in Ag and Pb .

The combination of recrystallization, brecciation and possibly oxidized sulphides is encouraging.

The third hole, 276, was drilled near the mouth of Tour Creek, east of the inferred Silvertip Creek fault. The unconformity was intersected approximatey 35 m below the valley, at the same elevation as in DDH 274. The upper 32 m of limestone was moderately brecciated Unit ML5. Textures in the limestone below this were obliterated by recrystallization and minor dolomitization. No sulphides were seen.

Displacement on the Silvertip Creek Fault in this area appears to be very minor, as compared to the apparent displacement 3 km to 4 km to the north.

### 5.2 NORTHHEST DISCO

The NW Disco area is covered with glacial till and glacio-fluvial sand and gravel; there are practically no bed rock exposures. Soil sampling, till mapping and magnetometer and EM surveys were combined to produce an approximate subsurface geology map. Three holes were drilled, one for stratigraphic and structural information and two in potentially mineralized zones.

The location of the first hole, MW-86-275, was based on an initial interpretation, and was expected to intersect Lower Sylvester clastics overlying McDame limestone east of the projected northward extension of the Silvertip Creek fault. The interpretation was essentially correct; 56 m of clastics were intersected, but the contact with the limestone was a major fault with up to 270 m of offset, eastside down. A 3 m silicified interval in Unit la contained up to $5 \%$ pyrite, but negligible values in $\mathrm{Ag}, \mathrm{Pb}$, and Zn .

Diamond drilling on the Reg Resources property west of NW Disco during 1985 and 1986 resulted in the definition of a variably mineralized east-west striking, steeply north dipping structure cutting shale (G. Medford, pers. comm., 1986). Drill hole MW-86-282 was drilled east of this area to intercept the mineralized structure and marble, calcareous siltstone and siltstone. It failed to find the structure, or any sulphides of economic interest. The strata have been interpreted as Middle Kechika limy silstones by correlation with similar rocks exposed off the property (J. Nelson, pers.comm., 1986).

The third hole, MW-86-203, was drilled in a fault-bounded block expected to have relatively thin Sylvester siltstone overlying limestone. Two fault zones were defined in core above the siltstone/limestone contact found at a depth of 131 m . The McDame stratigraphy could not be defined because of brecciation, recrystallization and dolomitization. Minor disseminated pyrite was found in brecciated siltstone immediately above the contact; this zone contained negligible $\mathrm{Ag}, \mathrm{Pb}$ and Zn .

### 5.3 NW DISCO SOUTH

The southeast corner of the NW Disco grid has a common border with the Discovery grid. Two holes, MW-84-81 and 84-88, were previously drilled in this area; hole 81 intersected three carbonate-hosted sulphide horizons (LZ's) of which the deepest returned 0.9 m grading $2116 \mathrm{~g} / \mathrm{t} \mathrm{Ag}$, $33.8 \% \mathrm{~Pb}$ and 10.48 Zn . Hole $\mathrm{MW} 84-88,145 \mathrm{~m}$ to the northwest, was blank.

Four holes were drilled during 1986 to determine the extent of the mineralization. Diamond drill hole MW-86-280 was sited 110 m north of MW-84-81; it intersected four Lower Zones, total thickness 12.1 m , between depths of 202 m and 222 m . These were hosted by brecciated MLl limestone. The best intersection graded $176.9 \mathrm{~g} / \mathrm{t} \mathrm{Ag}, 2.6 \% \mathrm{~Pb}$ and $11.7 \%$ Zn across 2.45 m .

Hole MW-86-281 was collared 95 m west of MW-84-81 to determine if the sulphides occurred updip at a shallower depth. Unfortunately, a fault was intersected at 101 m which juxtaposed Lower Sylvester Unit 1B sandstone against 40 m of brecciated upper McDame limestone; the offset on this fault could not be determined, and the stratigraphic trap at the unconformity was not found. A second fault at a depth of 152 m was occupied by a dyke followed by a normal sequence of ML7/ML8; this package was encountered much higher than expected. A similar fault was found by hole MW-84-88 140 m to the north.

The third hole in this area, MW-86-284, was collared 70 m east of MW-84-88 to test for mineralization paralleling the unconformity north of MW-84-81 and MW-86-280. A normal Lower Sylvester clastic sequence was found between the collar and the unconformity at a depth of 211 m , although the Unit $2 B$ sandstone package appeared to have been tectonically thinned by the numerous faults intersected. Once again, brecciation and recrystallization of the limestone precluded indentification of the McDame stratigraphy. An altered dyke between 224 m and 234 m probably occupies a fault; the underlying carbonate is most probably Lower McDame dolsotone (ML8). No Lower Zones were found.

The last hole, MW-86-294, was oriented to intersect the unconformity 75 m east of 86-284. Four faults cut the Unit 2B sandstone; the shale/limestone contact was 80 m lower than in 284 . Two thin Lower Zones were found, 0.5 m at a depth of 16 m below the contact and 0.3 m at 25 m . The limestone was variably brecciated but nor recrystallized.

The results of all the drilling in the southeast corner of the MW Disco grid indicate that the Sylvester strata have been much more structurally disturbed than farther south. These gouged and broken sections make successful drill hole completion difficult. All four 1986 holes were reduced once, and two of them twice. It is possible that these fault zones represent lateral accommodation of the stresses generated during emplacement of the allochthon by bedding plane movement. Alternatively, they could be relatively high angle normal faults generated by release of compression after emplacement of the Cassiar Batholith.

## REVERSE CIRCULATION DRILLING

## 6.1 <br> BULL 7 CLAIM

A large gossan, highly anomalous in $\mathrm{Ag}, \mathrm{Pb}$ and Zn is exposed on the Bull 7 claims. The iron-manganese oxide mineralization is predominantly in a Sylvester siltstone remnant surrounded and underlain by McDame limestone. Trenching of the gossan in the past a) did not uncover any sulphides, and b) indicated that the siltstone cap was relatively thin.

To test this area at depth 4 km of access road was rebuilt (Figure ll), 8 drill sites were constructed, and nine reverse circulation holes, 12 cm in diameter, were drilled on two sections 225 m apart (Plate 9). All holes were vertical, and were spaced approximately 100 m part. It was necessary to drill two holes from one site after the first hole was lost.

The drilling equipment (Nodwell mounted Schramm air rotary drill and down hole hammer, Nodwell TF60 support vehicle) and two man crew were supplied by Midnight Sun Drilling Co. Ltd. of Whitehorse. The holes were completed between September 30 and October 15, 1986.

The down hole hammer produced minus $1 \backslash 4$ inch rock chips which were passed through a cyclone before splitting three times with a Jones riffle to give a final $12.5 \%$ sample. The sampling interval was 1.5 m . The chips were logged, and most samples sent for analysis. The holes are summarized in Table 4, and the logs and analysis sheets are appended.

Table 4 REVERSE CIRCULATION DRILL HOLES, MIDWAY PROPERTY, 1986

| DRILL HOLE | AZIMUTH | DIP | DEPTH | DATES |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MW-86- |  |  |  |  |  |
| 285 | 0 | -90 | 96.62 | 30 Se | - 1 Oct |
| 286 | 0 | -90 | 105.76 | 20 C | - 3 Oct |
| 287 | 0 | -90 | 89.00 | 30 C | - 40 Oct |
| 288 | 0 | -90 | 169.77 | 7 Oc | 8 Oct |
| 289 | 0 | -90 | 127.10 | 90 c | - 10 Oct |
| 290 | 0 | -90 | 93.57 | 110 | - 12 Oct |
| 291 | 0 | -90 | 108.20 | 1200 | - 13 Oct |
| 292 | 0 | -90 | 102.72 | 1300 | - 14 Oct |
| 295 | 0 | -90 | 78.64 | 1400 |  |



## Results:

1. No sulphides of economic interest were found.
2. The shale caprock was much thicker than anticipated. Where 10 m to 20 m was expected, up to 89 m was found.
3. Iron oxides were intersected from surface to depths of 20 m to 70 m , and intermittently at greater depths.
4. In general, the base of continuous oxidation was related to the Sylvester/McDame contact.
5. High Zn results, and to a lesser extent Ba , were predominantly in carbonate-hosted oxides close to the shale/limestone contact.

## CHAPTER 7

## SUMMARY AND CONCLUSIONS

A variety of techniques (geochemical, geophysical, geological mapping, diamond and reverse circulation drilling) were used in different areas of the Midway property during 1986 in an attempt to find more mineralization. Positive indications were found in the Tricorn Mountain area, and the known deep mineralization was extended to the north in the Discovery area. Although strong surface indications are present on the Bull 7 claim, drilling failed to find any sulphides. Limited drilling north of Tricorn Mountain, after extensive surface exploration, did not find either McDame of Atan-hosted mineralizaiton.

It can be concluded that the potential of finding carbonate hosted massive sulphide mineralization within 100 m of the surface in the areas tested is very low, with the possible exception of beneath the east slope of Tricorn Mountain.

## COST STATEMENT

## SALARIES;

Project Manager

- H.Thalenhorst Jun 1 - Oct 19, 79 days (salary included in Project Management)

Project Geologists
-J.J. Hylands, P.Eng.
-W. J. Jakubowski, B. Sc.
-P. Donkersloot, B.Sc.
Assistants

| -G. Lafortune, | Geophysical |
| :--- | :---: |
| -L. Kostyshin, | $n$ |
| -I. Hylands, | $"$ |
| -J.Arnold, | nn |
| -C.Mimnaugh, | " |
| -J. Riddell, | Geochemical |
| -B.Fletcher, | $n$ |


| Jun 18 - Sep 30, 85 days e | $88 / \mathrm{d}$ | $7,480.00$ |  |
| :--- | :--- | ---: | :--- | :--- | :--- |
| Jun 15 - Oct 19, 110 days e | $79 / \mathrm{d}$ | $8,690.00$ |  |
| Sep 21 - Oct 27, 26 days e | $66 / \mathrm{d}$ | $1,716.00$ |  |
| Sep 26 - Oct 19, 24 days e | $79 / \mathrm{d}$ | $1,896.00$ |  |
| Jul 7 - Sep 17, | 31 days e | $84 / \mathrm{d}$ | $2,449.00$ |
| Jun 8 - Sep 14, | 73 days e | $84 / \mathrm{d}$ | $6,132.00$ |
| Jun 8-Sep 17, | 79 days e | $84 / \mathrm{d}$ | $\frac{6,636.00}{44,999.00}$ |

Camp Maintenance
-L. MacDonald
-J. Young

Jun 4 - Sep 12, 75 days @ $\$ 84 / \mathrm{d}$
Oct 10 - Oct 19, 10 days e $78 / \mathrm{d}$ 85 days


TOTAL B.C. SALARIES, 1986
\$39,000.00
27,060.00
8,800.00

7,480.00
8,690.00
, 716.00
2,449.00
6,132.00
$6,636.00$
$34,999.00$

6,300.00
780.00
$7,080.00$

6,014.00
2,756.00
1,881.00
525.00

5,976.00
17,152.00
$\$ 134,691.00$

```
FOOD AND ACCOMMODATION:
Midway Personnel
-Project Manager
-Project Geologists
-Assistants
-Camp Maintenance
-Catering Staff
Midway Personnel
-Project Manager
-Project Geologists
-Assistants
-Camp Maintenance
-Catering Staff
```

B.C. \& Y.T.

100 days
252 days
525 days
95 days
264 days
1236 days
B.C.

79 days
202 days
428 days
85 days
197 days
991 days

```
Contractors Personnel
-Frontier Helicopters, Watson Lake
Various pilots Jun 12 - Sep 6, 78 days total, 26 days in B.C.
-Crone Geophysics Ltd, Toronto
Richard Kurtz, operator Jun 18 - Jul 25, 38 days total, 26 days in B.C.
-G.Clark Contracting, Whitehorse
Various linecutters Jun 10 - Aug 31, 143 days total, 105 days in B.C.
-Caron Diamond Drilling, Whitehorse
Various drillers \& helpers Jul 27 - Oct 19, 494 days total, 360 days in B.C. Catskinners Jun 10 - Oct 3, 89 days total, 56 days in B.C.
-Midnight Sun Drilling, Whitehorse
Driller,helper, supervisor \(\operatorname{Sep} 30\) - Oct 25, 35 days total, 36 days in B.C.
-Canamax Resources Inc., Toronto
A. Watts, geophysicist Jun 22 - Sep 14, 43 days total, 30 days in B.C.
-Strathcona Mineral Services, Toronto
E. Roy, electrician Oct 3 - Oct 7, 5 days total, 5 days in B.C.
FOOD AND ACCOMMODATION
-Visitors, various 70 days total, 13 in B.C.
Total camp mandays, B.C. Y.T. \(=2231\)
Total camp mandays, B.C. only \(=1648\) Period: June 8 - October 19, 1986.
Cost of food and accommodation, B.C. 1648 mandays \(\mathrm{x} \$ 43.99 /\) manday \(=\$ 72,495.52\)
```

```
TRANSPORTATION
    -Return air transportation, Vancouver or Toronto
    to Watson Lake, including meals and lodging ..... = $20,999.00
    B.C. cost prorated on basis of ratio of employee
    mandays in B.C. to total employee mandays on Midway
                                    = \frac{991 }{1236}\times$20,999.00
    -Truck Rentals
    Hertz 4-wheel drive crewcab and pickup .......... = $18,586.00
    B.C. cost prorated on basis of ratio of mandays in
    B.C. to total mandays on Midway
                                    = =1648 < < $18,586.00
                                    = $13,729.15
    -Helicopter Lease
    B.C.Hours: 36.3 hrs x $443.00/hr = $16,080.90
    B.C.Fuel: 36.3 hrs x $7,680.00 = 2,598.17 $18,679.07
    107.3 hrs total
-Freight, express, delivery $15,696.00
RENTALS
-Spacetel installation
    rental Jun l - Oct 19, $ll,320 x 1640
        2231 = $ 8,361.88
    -966 Loader (all B.C.) Jun l - Aug 31 8,520.00
-Fuel tanks (all B.C.)
Jun 1 - Sep 30
                                    900.00
-Magnetometres
Jun 15 - Sep 30 $9,792 x \frac{153.1 km BC}{182.7 km tt }
$8,205.56
SURVEYS
-Crone Geophysics Limited Jun 18 - Jul 25, 38 days; Ground PEM 50.7 line km @ \(\$ 455.25 / \mathrm{km}\), B.C. ( \(\$ 34,053\) for 74.8 line km , total) Total Surveys B.C. \(\overline{\$ 23,081.18}\)
```

ANALYSES
-2325 soil samples analyzed for Ag , Pb , and Zn e $\$ 4.00 /$ sample $\$ 9,300.00$
-20 core samples assayed as follows:Sample preparation $20 \times \$ 3.75=\$ 75.00$
Silver $20 \times 5.50=110.00$
Lead $20 \times 6.25=125.00$
Zinc $20 \times 6.25=125.00$
Gold $20 \times 6.00=120.00$
Specific Gravity $\quad 19 \times 7.75=147.25 \quad 702.25$
-209 core and percussion samples analyzed as follows:
Sample preparation $209 \times \$ 3.25=\$ 679.25$
Silver $\quad 209 \mathrm{x} 2.00=418.00$
Lead $209 \times 1.00=209.00$
Zinc $\quad 209 \mathrm{x} 1.00=209.00$
Barium $\quad 196 \times 4.50=882.00$
Gold $\quad 89 \times 6.75=600.75$
Copper $5 \times 1.00=5.00$
Arsenic $\quad 5 \times 3.75=18.75$
Iron $\quad 12 \times 1.00=12.00$
Total Analyses B.C.
$\frac{3,033.75}{\$ 13,036.00}$

## PROJECT MANAGEMENT

Strathcona Mineral Services, Toronto May 1 - Oct $19=\$ 90,221.00$
Prorated on basis of mandays in B.C. to total mandays in Midway
1648 x \$90,221.00 2231
$=\$ 66,644.65$
To October $30=\$ 96,766 ;$ Oct $19=\$ 90,221$

## LINECUTTING

95 km of cut line, B.C. \& Y.T. $x \$ 315.00 / \mathrm{km}=29.925 .00$
Mobilization and demobilization $\quad \frac{1,300.00}{31,225.00}$
Cost $/ \mathrm{km}=\$ 31,225.00=\$ 328.68 / \mathrm{km}$
95 km
B. C. cost $=72.7 \mathrm{~km} \times \$ 328.68=$
$\$ 23,895.04$
ROAD AND DRILL SITE PREPARATION
E. Caron Diamond Drilling Ltd., Caterpillar D-6C tractor rental Jun 10 - Oct 19, 434.5 hrs x $\$ 75 / \mathrm{hr}$

## DIAMOND DRILLING



REVERSE CIRCULATION DRILLING
Midnight Sun Drilling Co. Ltd., Whitehorse

| $90.53 \mathrm{~m} \mathrm{e} 13.26 / \mathrm{m}$ | \$ 1,200.00 |
| :---: | :---: |
| 837.90 m e $26.40 / \mathrm{m}$ | 22,120.56 |
| 44.77 m a $30.35 / \mathrm{m}$ | 1,358.77 |
| 973.20 m | 24,679.33 |

$\$ 24,679.33$


Mobilization and demobilization

6,435.00
$\$ 32,639.83$

ROAD MAINTENANCE
Thawing of culverts with steam truck 2,146.00

## CAMP OPERATING COSTS

Camp supplies and equipment
Food
Fuel oil
Gasoline
Propane
Oil and lube
Vehicle repairs
Equipment repairs
Field supplies
Telephone
Maps
Draughting

Total to Oct. 31
\$ 5,858.00
36,836.00
27,544.00
7,669.00
4,245.00
1,892.00
1,023.00
342.00

5,786.00
8,255.00
31.00

Draughting
2,439.00
$\$ 101,920.00$

## CAMP MANDAYS

Project Manager Total to Oct. 31Project Geologist109
261Assistants
543
Maintenance ..... 104
Catering ..... 271
Frontier Helicopters ..... 78
Crone Geophysics ..... 381
Linecutters ..... 143
Caron Diamond Drilling ..... 616
Midnight Sun Drilling ..... 36
Canamax Resources ..... 43
Strathcona Mineral Services ..... 5
Visitors ..... 70

## COST SUMMARY

| Salaries | $\$ 175,615.00$ |
| :--- | ---: |
| Food and Accommodation | $72,795.52$ |
| Transportation | $64,940.80$ |
| Rentals | $27,119.10$ |
| Surveys | $23,081.18$ |
| Analyses | $12,268.50$ |
| Management | $66,644.65$ |
| Linecutting | $22,900.50$ |
| Road and Drill Site Preparation | $32,587.50$ |
| Diamond Drilling | $201,011.81$ |
| Reverse Circulation Drilling | $32,639.83$ |
| Road Maintenance | $2,146.00$ |

# CIRCULATION OF COSTS FOR ASSESSMENT WORK <br> Costs incurred between May 1 and October 19, 1986 

A. MANAGEMENT FEES, B.C.
Strathcona Mineral Services ..... \$ $66,644.65$J. J. Hylands, Cordilleran Engineering39,600.00Applicable mandays, B.C.:Midway employees 991 days
Contractors 614 days
Consultants 30 days
Visitors
13 days
1648 days
Management fee/manday $=\frac{\$ 106,244.65}{1648 \text { mandays }}=\$ 64.47 /$ manday
B. CAMP SUPPORT AND MAINTENANCE COST
To October 31, 1986, B.C. and Y.T.
Camp operating costs $\$ 101,920.00$
Plus: Freight and express $\quad 15,696.00$
$\frac{15,696.00}{\$ 117,616.00}$
Cost/manday $=\frac{\$ 117,616.00}{2317 \text { mandays }} \quad=\quad \$ 50.76 /$ manday
To October 19, 1986, B.C. only:
Catering salaries
$\$ 17,152.00$
Maintenance salaries 7,080.00
Transportation of personel
Rentals: telephone, vehicles, loader, fuel tanks
16,836. 58
31,511.08
$\$ 72,579.61$
Cost/manday $=\frac{\$ 72,579.61}{1648 \text { mandays }} \quad=\$ 44.04 /$ manday
Total Camp Support and Maintenance Cost =
$\$ 50.76 /$ manday $+\$ 44.04 /$ manday $\quad=\$ 94.80 /$ manday
C. HELICOPTER COST, B.C.
36.3 hrs $\mathrm{x} \$ 443.00 /$ hour\$16,080. 90
Fuel ..... 2,598.17Camp support 26 days $x$ 94.80/manday
Management 26 days $x$ 64.47/manday2,464.801,676.22$\$ 22,820.09$
Cost/hour $=\$ 22,820.09$
36.3 hours ..... $=\$ 628.65 /$ hour
D. LINECUTTING COST, B.C. \& Y.T.
Line cut $95 \mathrm{~km} \quad \mathrm{x} \$ 315 / \mathrm{km} \quad \$ 29,925.00$
Camp support $\quad 143$ mandays $x$ 94.80/mandayManagement $\quad 143$ mandays $x$ 64.47/manday13,556.40
Mobilization and demobilization9,219.21

$$
\text { Cost/km }=\frac{\$ 54,000.61}{95 \mathrm{~km}}
$$

$$
=\quad \$ 568.43 / \mathrm{km}
$$

E. MAGNETOMETER SURVEY COSTS, B.C.Rental of field and base station magnetometer\$8,205.56
Km surveyed, B.C. $=153.1 \mathrm{~km}$
Cost/km $=\$ 8,05.56$
153.1 km$=\$ 53.60 / \mathrm{km}$
Operator cost/manday - G. LafortuneSalary $\$ 88.00$ /manday
Camp support ..... 94.80/mandayManagement64.47/manday\$247.27/manday
F. SOIL SAMPLING COST Analyses \$4.00/sample
Sample collection and preparationSampler salary \$84.00/mandayCamp support94.80/mandayManagement64.47/manday
\$243.27/manday
G. ACCESS ROAD AND DRILL SITE CONSTRUCTION COSTS

D-6 Caterpillar tractor
Rental
Fuel Cost $\quad 4.5$ gals $/ \mathrm{hr} \times \$ 1.932 / \mathrm{gal}$
$75.00 / \mathrm{hr}$
$\$ 8.69 / \mathrm{hr}$
$\$ 83.69 / \mathrm{hr}$
Operator mandays to October 19, 1986: 89 mandays
Camp support 89 mandays $\mathrm{x} \$ 94.80 /$ manday
\$ 8,437. 20
Management 89 mandays $x$ 64.47/manday
5,737.83
$\$ 14,175.03$
Total Cat hours with operator to October 19,1986 $=762.5 \mathrm{hrs}$.

$$
\text { Operator cost/hour }=\frac{\$ 14,175.03}{762.5 \mathrm{hrs}}=\$ 18.59 / \mathrm{hr}
$$

Hourly cost to project of $\mathrm{D}-6 \mathrm{C}=\$ 83.69+\$ 18.59=\$ 102.28 /$ hour
H. DIAMOND DRILLING COSTS, B.C.
Contractors invoices \$201,011.81

Camp support 360 mandays $x$. $\$ 94.80 /$ day $34,128.00$
Management 360 mandays $x$ 64.47/day 23,209.20
Assays and analyses
20 core samples assayed $\quad 702.25$
18 core samples analyzed $\quad 310.25$
Geologists
W. Jakubowski Aug.ll-Oct. $19 \quad 38$ days $\mathrm{x} \$ 330.00 /$ day $\quad 12,540.00$
P. Donerksloot Sep.12-Sep. 2110 days $x$ 275.00/day 2,750.00

Core helper
L. Kostyshin

Camp support $\quad 108$ mandays $x \$ 94.80 /$ day $\quad 10,238.40$
Management 108 mandays $x \quad 64.47 /$ day $\quad \underset{\$ 295,592.67}{6,962.76}$
Diamond Drilling cost/metre, B.C. $=\frac{\$ 295,592.67}{1762.06 \mathrm{~m}}=\$ 167.75 / \mathrm{m}$
I. REVERSE CIRCULATION DRILLING COSTS, B.C.
Contractos invoices $\$ 32,639.83$

Contractors personnel
Camp support 36 mandays $x$ \$94.80/day 3,412.80
Management 36 mandays $x$ 64.47/day 2,320.92
Analyses
191 chip samples analyzed $2,723.50$
Geologis
P. Donkersloot Sep.30-0ct.16: 17 days $\mathbf{x}$ \$275.00/day $4,675.00$

Helper
I. Hylands Sep. 30-0ct.30: $\frac{17 \text { days }}{34} \mathrm{x}$ 66.00/day $\quad 1,122.00$

Camp support 34 mandays x \$94.80/day 3,223.20
Management 34 mandays $x \quad$ 2,191.98
\$52,309.23

Reverse Circulation drilling cost/metre $=\$ 52,309.23$

## SUMMARY OF ASSESSMENT COSTS

| A. | Management fees |  | \$ 64.47/manday |
| :---: | :---: | :---: | :---: |
| B. | Camp Support and Maintenance |  | 94.80/manday |
| c. | Helicopter |  | 628.65/hour |
| D. | Linecutting |  | $568.43 / \mathrm{km}$ |
| E. | Mangetometer Survey | Instrument | $53.60 / \mathrm{km}$ |
|  |  | Operator | 247.27/manday |
| F. | Soil Sampling | Analyses | 4.00/sample |
|  |  | Samplers | 243.27/manday |
| G. | Access Road, Drill Si | uction, D-6C | 102.28/hour |
| H. | Diamond Drilling |  | 167.75/metre |
| I | Reverse Circulation D |  | 94.86/metre |

## ALLOCATION OF ASSESSMENT COSTS

## BULL 7 GROUP

Work performed:
Reconstruction of existing access road to Bull 7 claim;
4 km road, 4 mm wide, D-6C, 39 hours $\mathrm{x} \$ 102.28 / \mathrm{hr}$
Construction of 0.6 m new road, 9 drill sites,
D-6C, 84 hours $\mathrm{x} \$ 102.28 /$ hour $=8,591.52$
Drilling of nine reverse circulation drill holes,
$973.20 \mathrm{~m} \times \$ 47.86 / \mathrm{m}$
TOTAL PHYSICAL.......... . $\$ 12,580.44$
TOTAL DRILLING
52,309.23
\$64,889.67
$=\$ 3,988.92$
$=\frac{52,309.23}{\$ 64,889.67}$

## WAY GROUP

## Work performed:

Cutting of 3.2 km of baseline $3.2 \mathrm{~km} \quad \mathrm{x} \$ 568.43 / \mathrm{km}=\$ 1,818.98$
Helicopter support $\quad 1.2 \mathrm{hrs} \mathrm{x} 628.65 / \mathrm{hr}=\quad 754.38$
Collection of 263 soil samples $\quad 9$ mandays $\times 243.27 /$ day $=2,189.43$
Analyses of 263 soil samples
Helicopter support
$263 \mathrm{x} 4.00 \mathrm{ea}=1,052.00$
$1.8 \mathrm{hrs} \mathrm{x} 628.65 / \mathrm{hr}=1,131.57$
6,946.36

TOTAL GEOCHEMICAL .............. \$ 6,946.36
PAC WITHDRAWAL $\quad . . . . . . . .$. . $1,053.64$
\$8,000.00

## DONEGAL GROUP

## Work performed:

Cutting of 7.1 km of baseline $7.1 \mathrm{~km} \quad \mathrm{x} \$ 568.43 / \mathrm{km}=\$ 4,035.85$
Helicopter support $\quad 2.0 \mathrm{hrs} \quad \mathrm{x} 628.65 / \mathrm{hr}=1,257.30$
Collection of 727 soil samples 33.0 mandays $x \quad 243.47 /$ day $=8,027.91$
Analyses of 727 soil samples 727 x 4.00 ea $=2,908.00$
Helicopter support $\quad 5.6 \mathrm{hrs} \quad \mathrm{x} 628.65 / \mathrm{hr}=\frac{3,520.44}{10.740 .50}$
$\begin{array}{lclllll}77.4 \mathrm{~km} \text { of magnetometer survey } & 77.4 \mathrm{~km} & \mathrm{x} & 53.60 / \mathrm{km} & = & 4,148.64 \\ \text { Operator } & 10 \text { mandays } & \mathrm{x} & 247.27 / \mathrm{day} & = & 2,472.70 \\ \text { Helicopter support } & 4.2 \mathrm{hrs} & \mathrm{x} & 628.65 / \mathrm{hr} & = & \underline{2,640.33}\end{array}$
TOTAL GEOCHEMICAL
\$19,749.50
TOTAL GEOPHYSICAL
$\begin{array}{r}9,261.67 \\ \hline 292011.17\end{array}$

## BULL 25 GROUP

Work performed:
Diamond drilling of seven holes on Bull 1 and
Bull 5 claims, totalling $1,354.47 \mathrm{~m} \times \$ 167.75 /$ metre $=\$ 227,212.34$

| DDH \# | CLAIM | DATES DRILLED | DEPTH | $\operatorname{COST}$ |
| :---: | :---: | :---: | :---: | :---: |
| 275 | Bull 5 | Aug $14-$ Aug 17 | 102.11 | \$ 17,128.95 |
| 280 | Bull 1 | Sep 12 - Sep 21 | 268.83 | 45,096.23 |
| 281 | Bull 1 | Sep 19 - Sep 30 | 228.60 | 38,347.65 |
| 282 | Bull 5 | Sep $21-$ Sep 25 | 152.04 | 25,504.71 |
| 283 | Bull 5 | Sep 26 - Oct 2 | 177.39 | 29,757.17 |
| 284 | Bull 1 | Sep 30 - Oct 11 | 254.20 | 42,642.05 |
| 284 | Bull 1 | Oct 12 - Oct 19 | 171.30 | 28,735.58 |
|  |  |  | 1354.47 | \$227,212.34 |

Construction of access road and drill sites, D-6C, $140 \mathrm{hrs} \times \$ 102.28 / \mathrm{hr}=\frac{14,319.20}{\$ 241,531.54}$

TOTAL DIAMOND DRILLING ........... = \$241,531.54

## CLIMAX GROUP

Work performed
Diamond drilling of three holes on Climax 1, 11 and 12 claims, totalling $407.23 \mathrm{~m} \times \$ 167.75 / \mathrm{m}=\$ 68,312.83$


TOTAL DIAMOND DRILLING ........... $=\$ 81,200.11$

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## CORDILLERAN ENGINEERING

1980 GUINNESS TOWER. 1055 WEST HASTINGS STREET. VANCOUVER,B.C. V6E $2 E 9$ TEL: (604)681-8381

## CHAPTER 11

## STATEMENT OF QUALIFICATIONS

I, J. J. Hylands, hereby certify that:

1. I am a geologist employed by Cordilleran Engineering of 1980-1055 West Hastings Street, Vancouver, B.C., V6E 2E9.
2. I am a graduate of the University of British Columbia (B.A .Sc., Geological Engienering, 1966).
3. I have engaged in the study and practice of mineral exploration since 1956, in Canada, the United States and the Phillippines.
4. I am the author of this report and a supervisor of the field work conducted on the Midway property during the period June 1 to October 19, 1986.
5. I am a Professional Engineer registered in the Province of British Columbia.
6. I have no beneficial interest in the claims covered by this report or in Regional Resources Ltd.


## APPENDIX "A"

ANALYSIS RECORD SHEETS

SOIL GEOCHEMISTRY

BDNDAR-CLEGG
Geochemical Lab Report REFORT: 126-2805

PROJECT: MIDWAY
PAGE 1

| SAMPLE NUMBER | $\begin{aligned} & \text { ELEKENI } \\ & \text { UNITS } \end{aligned}$ | $\begin{gathered} \mathrm{Pb} \\ \mathrm{PPM} \end{gathered}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{PPH} \end{array}$ | $\begin{gathered} \mathrm{Ag}_{3} \\ \mathrm{PPM} \end{gathered}$ | SAMPLE NUMBER | ELEMENT UNITS | $\begin{gathered} \mathrm{Pb} \\ \mathrm{PPH} \end{gathered}$ | $\begin{array}{r} \text { Zn } \\ \text { PPH } \end{array}$ | $\begin{gathered} A ? \\ P R M \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 513000 E 2800 N |  | 240 | 510 | $<0.2$ | Sl 3400 E 2500 N |  | 27 | 378 | 0.2 |
| Sl 3000 E 2900 N |  | 105 | 289 | <0.2 | Sl 3400E 2600N |  | 15 | 79 | 0.4 |
| Sl 3000 E 3000 N |  | 46 | 202 | 0.2 | Sl 3400E 2700N |  | 16 | 228 | 0.5 |
| Sl 3000E 3100N |  | 67 | 227 | 0.7 | S1 3400E 2800N |  | 18 | 184 | 0.5 |
| S1 3000E 3200N |  | 44 | 221 | $<0.2$ | Sl 3400E 2900N |  | 33 | 94 | 0.3 |
| \$1 3000E 3300n |  | 45 | 364 | 0.2 | Sl 3400E 3000N |  | 20 | 225 | 0.6 |
| Sl 3000E 3400N |  | 40 | 219 | 0.2 | Sl 3400E 3100N |  | 21 | 170 | 0.5 |
| S13100E 2400 N |  | 25 | 237 | 0.3 | S1 3400E 3300N |  | 17 | 62 | $<0.2$ |
| S1 3100E 2500N |  | 27 | 355 | 0.4 | Sl 3400 E 3400 N |  | 22 | 64 | $\bigcirc 0.2$ |
| S1 3100E 2600N |  | 24 | 287 | 0.6 | ST 3500 E 2500N |  | 25 | 343 | 0.5 |
| 513100 E 2700 N |  | 26 | 153 | <0.2 | S1 3500E 2600 N |  | 25 | 348 | $<0.2$ |
| S1 3100E 2800N |  | 24 | 158 | <0.2 | Sl 3500E 2700N |  | 30 | 108 | <0.2 |
| S1 3100E 2900\% |  | 40 | 223 | 0.6 | S1 3500E 2800N |  | 12 | 120 | <0.2 |
| Sl 3100 E 3000 N |  | 10 | 52 | 0.9 | Sl 3500E 2900N |  | 22 | 221 | $<0.2$ |
| S1 3100E 3100N |  | 30 | 111 | $<0.2$ | Sl 3500E 3000N |  | 24 | 163 | $<0.2$ |
| 513100 E 3200 N |  | 31 | 92 | $<0.2$ | 513500 E 3100 N |  | 10 | 58 | 0.8 |
| 513100 E 3300 N |  | 31 | 127 | 0.4 | S1 3500E 3200N |  | 18 | 58 | 0.5 |
| Sl 3100E 3400N |  | 54 | 105 | 0.4 | Sl 3500E 3300N |  | 16 | 71 | 0.4 |
|  |  | 24 | 378 | 6.2 | S1 3500E 3400N |  | 18 | 50 | $\bigcirc 0.2$ |
| S1 3200E 2500N |  | 19 | 381 | 0.7 | S1 3600E 2600 M |  | 24 | 385 | $<0.2$ |
| S1 3200E 2600N |  | 25 | 241 | $<0.2$ | 513600 E 2700 N |  | 41 | 249 | $<0.2$ |
| Sl 3200E 2700N |  | 22 | 150 | <0.2 | Sl 3600E 2800N |  | 26 | 223 | $\bigcirc 0.2$ |
| Sl 3200E 2800H |  | 28 | 179 | 0.8 | Sl 3600E 2900N |  | 21 | 189 | <0.2 |
| 513200 E 2900 N |  | 14 | 43 | 0.5 | S1 3600E 3000N |  | 4 | 44 | <0.2 |
| 513200 E 3000 N |  | 57 | 110 | 0.7 | S1 3600e 3100N |  | 25 | 179 | 10.2 |


| S1 3200E 3100N | 10 | 20 | 0.6 | S13600E 3200N | 8 | 20 | 6.2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S1 3200E 3200N | 11 | 28 | 0.2 | Sl 3600E 3300N | 12 | 40 | 1.2 |  |
| 513200 E 3300 N | 10 | 20 | 0.3 | S1 3600E 3400N | 17 | 48 | 0.4 |  |
| S1 3200E 3400N | 18 | 30 | <0.2 | S1 3700E 2800N | 25 | 150 | 0.1 |  |
| 51 3300E 2480 N | 24 | 295 | <0.2 | S1 3700E 2900N | 14 | 122 | <0.2 |  |
| S1 3300E 2500N | 19 | 197 | 0.4 | S1 3700E 3000N | 20 | 101 | 0.6 |  |
| Sl 3300E 2600H | 28 | 267 | 1.2 | S1 3700E 3100N | 23 | 104 | 0.4 |  |
| 513300 E 2700 H | 22 | 160 | <0.2 | S1 3700E 3200N | 16 | 157 | 0.2 |  |
| 51 3300E 2800\% | 24 | 232 | 0.2 | S1 3700E 3300N | 12 | 42 | <0.2 |  |
| Sl 3300E 2900N | 27 | 271 | 0.4 | Sl 3700E 3400N | 14 | 46 | 0.2 |  |
| S1 3300E 3000N | 20 | 182 |  |  |  |  |  |  |
| Sl 3300E 3100N | 23 | 137 |  |  |  |  |  |  |
| S1 3300E 3200N | 23 | 109 |  |  |  |  |  |  |
| Sl 3300E 3300N | 21 | 148 |  |  |  |  |  |  |
| S1 3300E 3400N | 24 | 129 |  |  |  |  |  |  |

BONDAR-CLEGG
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REPORT: 126-2805
SAMPLE ELEHENI Pb In
NUMBER

Sl 3800E 3300N UNITS PPM PPN PPM

| 17 | 72 | $<0.2$ |
| :--- | :--- | :--- |
| 12 | 52 |  |
| 30 | 190 | 0.9 |
| 22 | 134 | 0.8 |
| 23 | 138 | 0.4 |


| 22 | 106 | 0.4 |
| ---: | ---: | ---: |
| 77 | 288 | 0.6 |
| 17 | 84 | 60.2 |
| 16 | 102 | 00.2 |
| 20 | 147 | 0.2 |

0.4
0.6
0.2
0.2
0.2

| S1 4000E 2900N | 26 | 209 | 0.6 |
| :--- | ---: | ---: | ---: |
| Sl 4000E 3000N | 29 | 163 | 0.8 |
| Sl 4000E 3100N | 25 | 72 | 0.2 |
| Sl 4000E 3200N | 42 | 229 | 1.1 |
| Sl 4000E 3300N | 20 | 33 | 0.2 |

PROJECT: MIIDAY
PAGE 2

| ELEMENT | Pt, | 2 n | 9 |
| :---: | :---: | :---: | :---: |
| UNITS | PPH | PPM | PPN |


| S1 4400E 3400N | 22 | 125 | 0.2 |
| :---: | :---: | :---: | :---: |
| ST 4500 E 3100 N | 13 | 37 | <0.2 |
| S1 4500E 3200N | 12 | 35 | <0.2 |
| S1 4500E 3300N | 10 | 47 | $\bigcirc 0.2$ |
| S1 4500E 3400N | 14 | 47 | 0.2 |
| S] 4600 E 3100 N | 15 | 99 | 0.2 |
| S1 4600E 3200N | 16 | 40 | 0.9 |
| Sl 4600E 3300N | 12 | 44 | $<0.2$ |
| S1 4600E 3400N | 13 | 49 | <0.2 |
| S1 4700E 3100N | 10 | 16 | 0.2 |


| S1 4700E 3200N | 11 | 29 | $<0.2$ |
| ---: | ---: | ---: | ---: |
| S1 4700E 3300N | 14 | 62 | $<0.2$ |
| S1 4700E 3400N | 4 | 7 | $<0.2$ |


| S1 4000 E 3400 N | 10 | 62 | $<0.2$ |
| :--- | :--- | :--- | :--- |
| S1 4100E 2700N | 24 | 286 | 1.2 |
| S1 4100E 2800N | 27 | 227 | 0.7 |
| S1 4100E 2900N | 28 | 148 | 1.2 |
| Sl 4100E 3000N | 23 | 101 | 0.4 |


| S1 4100E 3100N | 29 | 155 | 0.5 |
| :--- | ---: | ---: | ---: | ---: |
| SI 4100E 3200N | 30 | 30 | $<0.2$ |
| S1 4100E 3300N | 21 | 89 | 0.2 |
| S1 4100E 3400N | 11 | 34 | $<0.2$ |
| S1 4200E 2600 N | 13 | 100 | 0.2 |



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REPORT: 126-3013

| SAMPLE | ELEMENT | Pb | 2 ft | Ag | SAMPLE | ELEMENT | 9 | $2 \pi$ | A9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NUMEER | UNIIS | PPFi | PFit | PPM | NUMEER | UNITS | PPli | FPM | PFH |
| 543500443005 |  | 14 | 84 | 0.3 | 543900 N 4100 E |  | 18 | 68 | 0.2 |
| 543500 N 4400 E |  | 8 | 36 | 0.2 | 54390004200 E |  | 18 | 68 | 0.2 |
| 54350014500 E |  | 12 | 42 | 0.2 | $543900 \pm 4300 \mathrm{E}$ |  | 37 | 90 | $<0.2$ |
| 343500146005 |  | 8 | 52 | 0.2 | 543900 L 400 E |  | 25 | 140 | 0.2 |
| 543500 N 4700 E |  | 23 | 105 | ¢0.2 | 543000 d 400 E |  | 13 | 66 | 0.2 |
| 543500 N 4800 E |  | 3 | 33 | 0.4 | 34500 H 400 E |  | 18 | 64 | 0.2 |
| 543700 N 3500 E |  | 16 | 86 | 0.4 | 543900 N 4700 E |  | 23 | 116 | 0.2 |
| 54370053600 E |  | 20 | 20 | $\bigcirc 0.2$ | 543900 N 4800 E |  | 20 | 440 | 0.2 |
| 54 3700E 3700E |  | 16 | 64 | $<0.2$ | 543950 N 4400 E |  | 24 | 56 | 0.2 |
| 54 3700E 3800E |  | 18 | 70 | $<0.2$ | 543950 N 4500 E |  | 15 | 96 | $\bigcirc 0.2$ |
| 543700 E 3900 E |  | 14 | 122 | $<0.2$ | 543950 N 4600 E |  | 20 | 84 | <0.2 |
| 543700 E 4000 E |  | 16 | 116 | $\bigcirc 0.2$ | 543950 N 4700 E |  | 23 | 49 | 0.2 |
| 54 3700E 4100E |  | 41 | 320 | 0.2 | S4 3950N 4800E |  | 20 | 64 | (0.2 |
| S4 3700E 4200E | - | 28 | 620 | $<0.2$ | 544000 N 3500 E |  | 17 | 128 | 0.2 |
| 54 3700E 4300E |  | 20 | 86 | $<0.2$ | 54 4000N 3600E |  | 26 | 135 | $<0.2$ |
| 54 3700E 4400E |  | 16 | 68 | $<0.2$ | 54 4000N 3700E |  | 40 | 370 | 0.4 |
| 54 3700E 4500E |  | 47 | 470 | 0.4 | 544000 N 3800 E |  | 17 | 176 | <0.2 |
| 54 3700E 4600E |  | 42 | 660 | 0.4 | 544000 N 3900 E |  | 21 | 94 | $<0.2$ |
| 54 3700E 4700E |  | 31 | 112 | $<0.2$ | 544000 N 4000 E |  | 18 | 50 | 0.2 |
| 54 3700E 4800E |  | 14 | 60 | <0.2 | S4 4000N 4100E |  | 30 | 296 | $<0.2$ |
| 543800 N 3500 E |  | 84 | 120 | 0.4 | 544000 N 4200 E |  | 17 | 54 | 0.2 |
| $543800 \mathrm{~N} \mathrm{3600E}$ |  | 27 | 120 | 0.2 | S4 4000N 4300E |  | 27 | 152 | 0.4 |
| 543800 N 3700 E |  | 36 | 124 | $<0.2$ | $5441000 \times 5500{ }^{-1}$ |  | 32 | 112 | 0.4 |
| S4 3800N 3800E |  | 28 | 130 | 0.2 | S4 4100N 3600E |  | 44 | 68 | 0.2 |
| 54 3800N 3900E |  | 50 | 420 | 0.4 | 54 4100N 3700E |  | 43 | 124 | 60.2 |
| 543800 N 4000 E |  | 21 | 37 | <0.2 | 544100 N 3800 E |  | 24 | 128 | $<0.2$ |
| 543800 N 4100 E |  | 22 | 53 | $<0.2$ | 54 4100N 3900E |  | 22 | 84 | $<0.2$ |
| S4 3800N 4200 E |  | 21 | 75 | <0.2 | S4 4100N 4000E |  | 38 | 113 | <0.2 |
| 543800 N 4300 E |  | 55 | 180 | 0.2 | 54 4100N 4100E |  | 29 | 284 | 0.6 |
| S4 3800N 4400E |  | 31 | 150 | <0.2 | 54 4100N 4200E |  | 34 | 100 | 0.4 |
| 543800 N 4500 E |  | 23 | 168 | 0.8 | S4 4100N 4300E |  | 22 | 98 | 0.2 |
| S4 3800N 4600E |  | 26 | 266 | 0.2 | 544150 N 4400 E |  | 29 | 136 | 0.4 |
| 54 3800N 4700E |  | 28 | 200 | 0.2 | 54 4150N 4500E |  | 24 | 50 | 0.2 |
| S4 3800N 4800E |  | 19 | 74 | $<0.2$ | 54 4150N 4600E |  | 29 | 110 | 0.2 |
| 543900 N 3500 E |  | 19 | 72 | <0.2 | S4 4150N 4700E |  | 22 | 2100 | 0.5 |
| 543900 N 3600 E |  | 19 | 88 | 1.6 | 54.4150N 4800E |  | 28 | 144 | 0.8 |
| 54 3900N 3700E |  | 24 | 84 | <0.2 | 54 TH8-86 |  | 25 | 170 | 0.4 |
| S4 3900N 3800E |  | 44 | 348 | 0.3 |  |  |  |  |  |
| 54 3900N 3900E |  | 19 | 80 | <0.2 |  |  |  |  |  |
| 543900 N 4000 E |  | 25 | 140 | $<0.2$ |  | . |  |  | . |

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| P4 4900N 2000E | 26 | 56 | 0.2 | P4 5400N 2000E | 25 | 110 | <0.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P4 4900 N 2100 E | 18 | 36 | 0.3 | P4 5400N 2100E | 12 | 40 | $<0.2$ |
| P4 4900N 2200E | 9 | 88 | $\bigcirc 0.2$ | P4 5400N 2200E | 13 | 46 | <0.2 |
| P4 5000N 1600E | 43 | 210 | 0.5 | P4 5400N 2300E | 13 | 110 | <0.2 |
| P4 5000N 1700E | 59 | 320 | $<0.2$ | P4 5400N 2400E | 20 | 108 | <0.2 |
| P4 5000 N 1800 E | 35 | 230 | 0.5 | P4 5500N 1600E | 19 | 60 | 0.8 |
| P4 5000N 1900E | 36 | 194 | 0.2 | P4 5500N 1700E | 12 | 48 | $<0.2$ |
| P4 5000N 2000E | 37 | 180 | 0.2 | P4 5500N 1800E | 41 | 106 | <0.2 |
| P4 5000N 2100 E | 46 | 230 | 0.4 | P4 5500N 1900E | 13 | 72 | $<0.2$ |
| P4 5000N 2200E | 28 | 168 | 0.3 | P4 5500N 2000E | 13 | 58 | <0.2 |


| P4 5000N 2400E | 31 | 150 | 0.3 | 945500 N 2100 E | 10 | 35 | 8.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P4 5100N 1600E | 23 | 136 | 0.2 | P4 5500N 2200E | 20 | 110 | $<0.2$ |
| P4 5100N 1700E | 29 | 178 | 0.4 | P4 5500N 2300E | 11 | 60 | $<0.2$ |
| P4 5100N 1900E | 29 | 160 | 0.2 | P4 5500N 2400E | 13 | 79 | 60.2 |
| P4 5100N 1900E | 21 | 112 | 60.2 | F4 5600N 1600E | 18 | 170 | $<0.2$ |


| P4 5100N 2000E | 26 | 100 | 10.2 | P4 5600N 1700E | 18 | 92 | $<0.2$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P4 5100N 2100E | 29 | 108 | 0.2 | P4 5600N 1800E | 16 | 120 | 0.2 |
| P4 5100N 2200E | 38 | 100 | 0.2 | P4 5600N 1900E | 15 | 100 | 10.2 |
| P45100\% 2300E | 27 | 144 | 0.2 | P4 5600N 2000E | 15 | 129 | <0.2 |
| P4 5200N 1600E | 39 | 152 | 0.6 | P4 5600N 2100E | 13 | 220 | <0.2 |


| P4 5200N 1700E | 40 | 200 | 0.2 | P4 5600N 22000 | 22 | 180 | 0.2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P4 5200 N 1800 E | 41 | 272 | 0.4 | P4 5600N 2300E | 19 | 260 | $<0.2$ |  |
| P4 5200N 1900E | 26 | 152 | $\bigcirc 0.2$ | P4 5600N 2400E | 23 | 182 | $<0.2$ | W ${ }^{\text {cha }}$ |
| P4 5200N 2000E | 53 | 340 | 0.2 | PT 5700 K 1600 E |  |  |  |  |
| P1 5200N 2100E | 37 | 216 | 0.3 | P4 5700N 1700E |  |  |  |  |




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REPORI: 126-2127

| SAMPLE | ELEHENI | Pb | Zn | Ag |
| :---: | :---: | :---: | :---: | :---: |
| NUMBER | UNITS | PPH | PPK | PPH |

PROJECT: MIDMAY


| P4 16800N 16300E | 23 | 90 | 0.2 |
| :---: | :---: | :---: | :---: |
| P4 16800N 16350E | 27 | 108 | $<0.2$ |
| P4 16800N 16400E | 18 | 112 | $<0.2$ |
| P4 16800N 16450E | 21 | 112 | 0.5 |
| P4 16800N 16500E | 13 | 72 | $<0.2$ |
| P4 16800N 16550E | 12 | 58 | 0.2 |

P4 16800N 15200E
P4 16800N 15250E
P4 16800N 15300E
$\begin{array}{rrr}16 & 126 & 0.2 \\ 17 & 113 & 0.3 \\ 22 & 99 & 0.2\end{array}$
22
-

| P4 16800 N 15350 E | 18 | 87 | 0.3 |
| :--- | :--- | ---: | ---: |
| P4 16800N 15400 E | 16 | 114 | 0.4 |
| P4 16800N 15450E | 12 | 70 | 0.2 |
| P4 16800N 15500 E | 15 | 34 | $<0.2$ |
| P4 16800N 15550 E | 21 | 105 | 0.8 |


| P4 16800N 15600E | 23 | 105 | 0.2 |
| :--- | :--- | :--- | :--- |
| P4 16800N 15650E | 27 | 138 | 0.6 |
| P4 16800N 15700E | 15 | 124 | 0.5 |
| P4 16800N 15750E | 16 | 117 | 0.4 |
| P4 16800N 15800E | a | 15 | 150 |

REPORT: 126-2127

| SAMPLE NUMEER | ELENENI <br> UNITS | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{PPH} \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{PPM} \end{array}$ | ${ }_{\text {PPM }}$ |
| :---: | :---: | :---: | :---: | :---: |
| P4 17000N 15900E |  | 17 | 84 | 60.2 |
| P4 17000N 15950E |  | 17 | 120 | 0.2 |
| P4 17000N 16000E |  | 14 | 80 | 0.4 |
| P4 17000N 16050E |  | 23 | 168 | 0.2 |
| P4 17000N 16100E |  | 16 | 90 | 0.2 |
| P4 17000N 16150E |  | 27 | 116 | 0.2 |
| P4 17000N 16200E |  | 25 | 120 | $<0.2$ |
| P4 17000N 16250E |  | 14 | 97 | $<0.2$ |
| P4 17000N 16300E |  | 15 | 112 | $<0.2$ |
| P4 17000N 16350E |  | 18 | 116 | 0.2 |
| P4 17000N 16400 E |  | 25 | 120 | <0.2 |
| P4 17000N 16450E |  | 20 | 124 | 0.2 |
| P4 17000 N 16500 E |  | 15 | 104 | $<0.2$ |
| P4 17000N 16550E |  | 14 | 64 | 0.2 |
| P4 17000N 16600E |  | 13 | 50 | $<0.2$ |
| P4 17000N 16650E |  | 15 | 90 | 0.2 |
| P4 17000N 16700E |  | 17 | 85 | 0.4 |
| P4 17000N 16750E |  | 18 | 140 | 0.2 |
| P4 17000N 16800E |  | 13 | 116 | <0.2 |
| P4 17000N 16850E |  | 18 | 116 | 0.4 |

PROJECT: MIDMAY
$\begin{array}{lrrrr}\text { SAMPLE } & \text { ELEMENT } & \mathrm{Fb} & \mathrm{Zn} & \text { A3 } \\ \text { NURBER } & \text { UNITS } & \text { PPH } & \mathrm{PPM} & \text { PFM }\end{array}$

| P4 17200 N 15650 E | 10 | 40 | 60.2 |
| :--- | ---: | ---: | ---: |
| P4 17200N 15700E | 16 | 76 | 60.2 |
| P4 17200 N 15750 E | 17 | 102 | 60.2 |
| P4 17200 N 15800 E | 17 | 34 | 6.2 |
| PA 17200 N 15850 E | 17 | 72 | 0.2 |

$\begin{array}{lllll}P 4 & 17200 N & 15900 E & 74 & 0.2\end{array}$
P4 17200N 15950E
P4 17200N 16000E
P4 17200N 16050E
P4 17200N 16100E

| P4 17200 N 16150 E | 20 | 139 | $<0.2$ |
| :--- | ---: | ---: | ---: |
| P4 17200 N 16200 E | 11 | 60 | $<0.2$ |
| P4 17200 N 16250 E | 21 | 106 | $<0.2$ |
| P4 17200 N 16300 E | 5 | 44 | $<0.2$ |
| P4 17200 N 16350 E | 8 | 58 | 0.2 |


| P4 17200E 16400E | 14 | 76 | $<0.2$ |
| :--- | ---: | ---: | ---: |
| P4 17200E 16450E | 18 | 59 | $<0.2$ |
| P4 17200E 16500E | 8 | 30 | 0.2 |
| P4 17200E 16550E | 21 | 96 | $<0.2$ |
| P4 17200E 16600E | 6 | 27 | $<0.2$ |

P4 17000N 16900E
P4 17000N 16950E
P4 17000N 17000E
P4 17000N 17050E
P4 17000N 17100E
15. $84<0.2$

12
$13 \quad 78 \quad 0$.
$13 \quad 80 \quad 0.2$
$8 \quad 92 \quad 0.2$

## 16

## 11

9
14
13
$\cdots \cdots$
$75<0.2$
$\begin{array}{rr}52 & 0.2 \\ 114 & 0.2\end{array}$
$\begin{array}{rr}52 & 0.2 \\ 114 & 0.2\end{array}$
0.2

P4 17000N 17200E
P4 17200E 16650E 20

| 20 | 98 | 60.2 |
| ---: | ---: | ---: |
| 13 | 192 | 0.4 |
| 15 | 120 | 0.2 |
| 16 | 142 | 0.2 |
| 27 | 390 | 0.2 |

P4 17000N 17250E

| 13 | 70 | 0.2 |
| ---: | ---: | ---: |
| 10 | 40 | 0.4 |
| 12 | 58 | 0.2 |
| 16 | 52 | 60.2 |
| 7 | 30 | 0.2 |

<0.2
$<0.2$
<0.2
0.2
0.6

| 7 | 36 | $<0.2$ |
| ---: | ---: | ---: |
| 12 | 50 | $<0.2$ |
| 17 | 63 | $<0.2$ |
| 16 | 64 | 0.2 |
| 18 | 90 | 0.6 |


| P4 17200N 17400E | -42 | 170 | 0.4 |
| :--- | ---: | ---: | ---: |
| P4 17400N 15500E | 7 | 34 | 0.4 |
| P4 17400N 15550E | 16 | 80 | 0.6 |
| P4 17400N 15600E | 9 | 60 | 0.2 |
| P4 17400N 15650E | 9 | 58 | $<0.2$ |

BONDAR-CLEGG
*e: . A

REPORT: 126-2127

| SAMPLE | ELEMENT | Pb | 7n | A |
| :---: | :---: | :---: | :---: | :---: |
| NUMEER | UNIIS | PPM | PPM | PPH |
| P4 17400N 15700E |  | 23 | 222 | <0.2 |
| P4 17400N 15750E |  | 17 | 170 | <0.2 |
| P4 17400N 15800E |  | 18 | 96 | <0.2 |
| P4 17400N 15850E |  | 17 | 110 | <0.2 |
| P4 17400N 15900E |  | 14 | 56 | 0.3 |
| P4 17400N 15950E |  | 17 | 68 | $\bigcirc 0.2$ |
| P4 17400N 16000E |  | 13 | 52 | 0.2 |
| P4 17400N 16050E |  | 18 | 100 | 0.2 |
| P4 17400N 16100E |  | 20 | 108 | <0.2 |
| P4 17400N 16150E |  | 12 | 68 | <0.2 |
| P4 17400N 16200E |  | 7 | 48 | <0.2 |
| P4 17400N 16250E |  | 4 | 32 | <0.2 |
| P4 17400N 16300E |  | 18 | 76 | <0.2 |
| P4 17400N 16350E |  | 18 | 112 | <0.2 |
| P4 17400N 16400E |  | 23 | 80 | 0.2 |
| P4 17400N 16450E |  | 14 | 56 | $<0.2$ |
| P4 17400N 16500E |  | 23 | 75 | <0.2 |
| P4 17400N 16550E |  | 23 | 103 | 0.3 |
| P4 17400N 16600E |  | 19 | 71 | 0.2 |
| P4 17400N 16650E |  | 24 | 134 | 0.2 |


| SAMPLE | ELEMENT | $P t$ | $2 n$ | $A A$ |
| :--- | ---: | ---: | ---: | ---: |
| NUMBER | UNITS | $P Y H$ | $P P N$ | $P H_{H}$ |

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RED日RT: 126-2899

| $\begin{aligned} & \text { SAMPLE } \\ & \text { HLMPES } \end{aligned}$ |  |
| :---: | :---: |
| $24.15200 \%$ | 16500E |
| 74 152004 | 165505 |
| 74 15900 | 166008 |
| P4 15300 | 166509 |
| 3 15200 | 15700E |

DROJECT: MTNHAV

| $A Q$ | SCKPLE | ETSMEN: | $P b$ | $2 n$ | $A 9$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $2 P M$ |  |  |  |  |  |

PACE 1

P4 152004167505
P4 15200k 26800 E
P4 15200K 16850E
P4 15200स 16900 E
P4 15200N 16950 E
gen
18
19
:.
$: 9$
19
20
19 .
$17 \quad 70$
$20 \quad 125$
18
22
22
$40 \quad 122$

51
0.4

95
92
101
161

112
$125 \quad 0.5$
1710.5
$114 \quad 0.2$
1220.2
0.2
0.6 P4 25000世 162008

24 :60ccy $162=0 \mathrm{E}$
P4 :5000 16300 E
94: 2908: : 6350E
P4 15000 16500E
15
$\because 24$
0.7
1.2

128
0.4
0.3

| 24 152003 164505 | 18 | 114 | 0.3 |
| :---: | :---: | :---: | :---: |
| P4 16000N 16500E | 20 | 101 | 0.2 |
| P4 150004 16550E | 22 | 134 | 0.2 |
| P4 16000k 16600 E | 20 | 127 | 0.3 |
| P4 16000N 16650E | 20 | 122 | 0.3 |


| P4 16000 N 16700 E | 22 | 103 | 0.4 |
| :--- | ---: | ---: | ---: |
| P4 16000 N 16750 E | 20 | 98 | 0.2 |
| P4 16000 N 16300 E | 24 | 125 | 0.4 |
| P4 16000 N 16850 E | 22 | 116 | 0.3 |
| P4 16000 N 16900 E | 25 | 160 | 0.7 |


| P4 16000 H 16950 E | 25 | 153 | 0.9 |
| :--- | :--- | :--- | :--- |
| P4 16000 N 17000 E | 24 | 130 | 0.4 |
| P4 16000 H 17050 E | 14 | 104 | 0.4 |
| P4 16000 H 17100 E | 18 | 100 | 0.6 |
| P4 16000 N 17150 E | 21 | 157 | 0.8 |


| P4 15600N 16550E | 25 | 150 | 0.8 | P4 16000N 17200E | 22 | 116 | 0.3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P4 15600N 16600E | 24 | 121 | 0.3 | P4 16000N 17300E | 25 | 106 | 0.2 |
| P4 15600N 16650E | 24 | 141 | 0.4 | P4 16000N 17350E | 26 | 138 | 0.4 |
| 9415600 N 16700 E | 20 | 121 | 0.4 | P4 16000N 17400E | 18 | 99 | 0.3 |
| P4 15600N 16750E | 23 | 155 | 0.4 | P4 16400N 16500E | 22 | 124 | 0.4 |
| P4 15600N 16800E | 23 | 141 | 0.2 | P4 16400N 16550E | 29 | 151 | 0.4 |
| P4 15600N 16350E | 22 | 151 | 0.4 | P4 16400 N 16500 E | 24 | 174 | 1.0 |
| P4 15600N 16900E | 13 | 51 | $<0.2$ | P4 16400N 167502 | 20 | 103 | 0.4 |
| P4 15600N 16950E | 13 | 40 | 0.4 | P4 15400N 16800E | 22 | 146 | 0.5 |
| P4 15600N 17000E | 17 | 31 | 0.2 | P4 16400N 16900E | 18 | 136 | 0.4 |
| P4 15600N 17050E | 16 | 126 | 0.3 | P4 16400N 16950E | 20 | 152 | 0.4 |
| P4 15600N 17100E | 15 | 69 | 0.2 | P4 16400N 17000E | 21 | 169 | 0.6 |
| P4 15600N 171502 | 22 | 127 | 0.5 | P4 16400N 17050E | 17 | 114 | 0.4 |
| P4 15600N 17200E | 11 | 59 | 0.2 | P4 164004 17100E | 16 | 125 | 0.4 |
| P4 15600N 17250E | 16 | 109 | 0.4 | P4 16400N 17150E | 14 | 110 | 0.4 |


| P4 15600 N | 17300 E | 16 | 58 | 0.5 | P4 16400 N 17200 E | 9 | 86 | 0.2 |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| P4 15600 N | 17350 E | 13 | 44 | 0.3 | P4 16400 N 17250 E | 14 | 114 | 0.2 |
| P4 15600 N | 17400 E | 16 | 137 | $<0.2$ | P4 16400 N 17300 E | 12 | 88 | 0.3 |
| P4 16000 N | 16100 E | 13 | 101 | 0.2 | P4 16400 N 17350 E | 17 | 116 | 0.5 |
| P4 16000 N | 16150 E | 12 | 69 | 0.2 | P4 16400 N 17400 E | 17 | 133 | 0.4 |

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Geochemica Lab Repori


## APPENDIX "B"

MAGNETOMETER READINGS

DONEGAL MOUNTAIN GRID

## MIDWAY PROJECT

DONEGAL MOUNTAIN GRID

## 1986 MAGNETOMETER READINGS

In the following listing, some lines have a denotation slightly different from their actual line number, e.g. 3401 and 3402 instead of 3400 ; this is necessitated by the structure of the computer files from which these data were copied.

## 1. EAST - WEST LINES

1.1 Line 3400 N

| Station <br> E | Line <br> N | Original <br> Readings |  |
| :---: | :---: | :---: | :---: |
| 2400.0 | 3401.0 | 7.3 | 7.1 |
| 2412.5 | 3401.0 | 6.8 | 7.4 |
| 2425.0 | 3401.0 | 7.1 | 7.3 |
| 2437.5 | 3401.0 | 8.3 | 7.6 |
| 2450.0 | 3401.0 | 7.2 | 8.0 |
| 2462.5 | 3401.0 | 8.5 | 8.4 |
| 2475.0 | 3401.0 | 8.7 | 9.0 |
| 2487.5 | 3401.0 | 9.5 | .9 .8 |
| 2500.0 | 3401.0 | 11.2 | 10.7 |
| 2512.5 | 3401.0 | 11.1 | 11.7 |
| 2525.0 | 3401.0 | 13.2 | 12.6 |
| 2537.5 | 3401.0 | 13.5 | 13.7 |
| 2550.0 | 3401.0 | 13.9 | 15.1 |
| 2562.5 | 3401.0 | 16.8 | 16.4 |
| 2575.0 | 3401.0 | 18.0 | 18.3 |
| 2587.5 | 3401.0 | 19.9 | 20.4 |
| 2600.0 | 3401.0 | 23.1 | 22.3 |
| 2612.5 | 3401.0 | 24.2 | 24.5 |
| 2625.0 | 3401.0 | 26.2 | 26.6 |
| 2637.5 | 3401.0 | 29.0 | 27.8 |
| 2650.0 | 3401.0 | 30.7 | 28.7 |
| 2662.5 | 3401.0 | 29.1 | 29.1 |
| 2675.0 | 3401.0 | 28.7 | 29.1 |
| 2687.5 | 3401.0 | 28.1 | 29.6 |
| 2700.0 | 3401.0 | 28.7 | 33.5 |
| 2712.5 | 3401.0 | 33.2 | 44.1 |
| 2725.0 | 3401.0 | 48.6 | 58.0 |
| 2737.5 | 3401.0 | 82.1 | 60.3 |
| 2750.0 | 3401.0 | 97.2 | 50.5 |
| 2762.5 | 3401.0 | 40.4 | 35.8 |
| 2775.0 | 3401.0 | -15.8 | 14.5 |
| 2787.5 | 3401.0 | -24.7 | -8.6 |


| 2800.0 | 3401.0 | -24.8 | -19.5 |
| ---: | ---: | ---: | ---: |
| 2812.5 | 3401.0 | -18.1 | -17.9 |
| 2825.0 | 3401.0 | -14.2 | -14.0 |
| 2837.5 | 3401.0 | -7.8 | -8.7 |
| 2850.0 | 3401.0 | -5.2 | -3.9 |
| 2862.5 | 3401.0 | 1.8 | 1.7 |
| 2875.0 | 3401.0 | 6.0 | 7.5 |
| 2887.5 | 3401.0 | 13.8 | 14.5 |
| 2900.0 | 3401.0 | 21.2 | 23.1 |
| 2912.5 | 3401.0 | 29.8 | 34.7 |
| 2925.0 | 3401.0 | 44.7 | 49.9 |
| 2937.5 | 3401.0 | 64.1 | 69.5 |
| 2950.0 | 3401.0 | 89.7 | 95.6 |
| 2962.5 | 3401.0 | 119.3 | 126.5 |
| 2975.0 | 3401.0 | 160.1 | 149.0 |
| 2987.5 | 3401.0 | 199.1 | 154.5 |
| 3000.0 | 3401.0 | 176.6 | 143.0 |
| 3012.5 | 3401.0 | 117.5 | 113.8 |
| 3025.0 | 3401.0 | 61.5 | 69.0 |
| 3037.5 | 3401.0 | 14.2 | 29.0 |
| 3050.0 | 3401.0 | -24.9 | .6 |
| 3062.5 | 3401.0 | -23.5 | -9.7 |
| 3075.0 | 3401.0 | -24.2 | -8.4 |
| 3087.5 | 3401.0 | 10.0 | -4.7 |
| 3100.0 | 3401.0 | 20.4 | -3.1 |
| 3112.5 | 3401.0 | -6.4 | -1.1 |
| 3125.0 | 3401.0 | -15.4 | .4 .2 |
| 3137.5 | 3401.0 | -14.0 | 21.9 |
| 3150.0 | 3401.0 | 16.2 | 63.6 |
| 3162.5 | 3401.0 | 129.3 | 77.9 |
| 3175.0 | 3401.0 | 202.1 | 90.3 |
| 3187.5 | 3401.0 | 55.9 | 108.5 |
| 3200.0 | 3401.0 | 47.8 | 118.4 |
| 3212.5 | 3401.0 | 107.6 | 99.9 |
| 3225.0 | 3401.0 | 178.4 | 86.3 |
| 3237.5 | 3401.0 | 109.6 | 71.5 |
| 3250.0 | 3401.0 | -11.7 | 46.5 |
| 3262.5 | 3401.0 | -26.4 | 5.7 |
| 3275.0 | 3401.0 | -17.4 | -23.8 |
| 3287.5 | 3401.0 | -25.8 | -32.3 |
| 3300.0 | 3401.0 | -37.6 | -35.1 |
| 3312.5 | 3401.0 | -54.1 | -39.1 |
| 3325.0 | 3401.0 | -40.7 | -42.6 |
| 3337.5 | 3401.0 | -37.3 | -44.9 |
| 3350.0 | 3401.0 | -43.4 | -41.2 |
| 3362.5 | 3401.0 | -49.1 | -40.6 |
| 3375.0 | 3401.0 | -35.4 | -42.1 |
| 3387.5 | 3401.0 | -37.8 | -40.3 |
| 3400.0 | 3401.0 | -44.9 | -38.3 |
| 3412.5 | 3401.0 | -34.3 | -37.3 |
| 3425.0 | 3401.0 | -39.2 | -34.0 |
| 3437.5 | 3401.0 | -30.5 | -31.5 |
| 3450.0 | 3401.0 | -21.2 | -30.5 |
|  |  |  |  |


| 3462.5 | 3401.0 | -32.5 | -26.5 |
| ---: | ---: | ---: | ---: |
| 3475.0 | 3401.0 | -29.2 | -9.7 |
| 3487.5 | 3401.0 | -18.9 | -6.8 |
| 3500.0 | 3401.0 | 53.5 | 1.8 |
| 3512.5 | 3402.0 | 250.1 | 97.2 |
| 3525.0 | 3402.0 | 71.4 | 73.8 |
| 3537.5 | 3402.0 | 18.8 | 58.3 |
| 3550.0 | 3402.0 | -19.8 | 3.8 |
| 3562.5 | 3402.0 | -29.0 | -14.2 |
| 3575.0 | 3402.0 | -22.5 | -19.9 |
| 3587.5 | 3402.0 | -18.5 | -21.8 |
| 3600.0 | 3402.0 | -9.9 | -19.7 |
| 3612.5 | 3402.0 | -29.2 | -19.7 |
| 3625.0 | 3402.0 | -18.6 | -22.0 |
| 3637.5 | 3402.0 | -22.5 | -24.4 |
| 3650.0 | 3402.0 | -30.0 | -22.0 |
| 3662.5 | 3402.0 | -21.6 | -18.2 |
| 3675.0 | 3402.0 | -17.5 | -15.2 |
| 3687.5 | 3402.0 | -1.6 | -11.6 |
| 3700.0 | 3402.0 | -7.4 | -17.8 |
| 3712.5 | 3402.0 | -12.1 | -19.7 |
| 3725.0 | 3402.0 | -52.5 | -23.7 |
| 3737.5 | 3402.0 | -26.9 | -26.7 |
| 3750.0 | 3402.0 | -19.8 | -23.5 |
| 3762.5 | 3402.0 | -22.4 | -4.8 |
| 3775.0 | 3402.0 | 4.1 | 1.8 |
| 3787.5 | 3402.0 | 40.9 | 23.8 |
| 3800.0 | 3402.0 | 6.3 | 101.1 |
| 3812.5 | 3402.0 | 90.1 | 119.9 |
| 3825.0 | 3402.0 | 364.1 | 134.9 |
| 3837.5 | 3402.0 | 98.1 | 175.5 |
| 3850.0 | 3402.0 | 115.8 | 170.3 |
| 3862.5 | 3402.0 | 209.4 | 110.0 |
| 3875.0 | 3402.0 | 64.1 | 103.8 |
| 3887.5 | 3402.0 | 62.6 | 102.6 |
| 3900.0 | 3402.0 | 67.2 | 125.5 |
| 3912.5 | 3402.0 | 109.8 | 319.5 |
| 3925.0 | 3402.0 | 323.7 | 340.0 |
| 3937.5 | 3402.0 | 1034.3 | 333.9 |
| 3950.0 | 3402.0 | 165.1 | 322.1 |
| 3962.5 | 3402.0 | 36.7 | 260.9 |
| 3975.0 | 3402.0 | 50.7 | 50.3 |
| 3987.5 | 3402.0 | 17.9 | 16.2 |
| 4000.0 | 3402.0 | -18.7 | 11.3 |
| 4012.5 | 3402.0 | -5.7 | 2.4 |
| 4025.0 | 3402.0 | 12.4 | 6.9 |
| 4037.5 | 3402.0 | 6.0 | 18.1 |
| 4050.0 | 3402.0 | 40.6 | 16.2 |
| 4062.5 | 3402.0 | 37.4 | 14.9 |
| 4075.0 | 3402.0 | -15.6 | 12.3 |
| 4087.5 | 3402.0 | 6.3 | -1.5 |
| 4100.0 | 3402.0 | -7.2 | -8.5 |
| 4112.5 | 3402.0 | -28.4 | -7.0 |


|  |  |  |  |
| ---: | ---: | ---: | ---: |
| 4125.0 | 3402.0 | 2.2 | -12.0 |
| 4137.5 | 3402.0 | -7.9 | -14.5 |
| 4150.0 | 3402.0 | -18.8 | -12.1 |
| 4162.5 | 3402.0 | -19.6 | -11.7 |
| 4175.0 | 3402.0 | -16.5 | -8.4 |
| 4187.5 | 3402.0 | 4.3 | -9.6 |
| 4200.0 | 3402.0 | 8.5 | -12.6 |
| 4212.5 | 3402.0 | -24.6 | -6.4 |
| 4225.0 | 3402.0 | -34.7 | -4.4 |
| 4237.5 | 3402.0 | 14.6 | -4.8 |
| 4250.0 | 3402.0 | 14.4 | 2.0 |
| 4262.5 | 3402.0 | 6.1 | 6.5 |
| 4275.0 | 3402.0 | 9.7 | 4.6 |
| 4287.5 | 3402.0 | -12.1 | 1.7 |
| 4300.0 | 3402.0 | 4.7 | -4.3 |
| 4312.5 | 3402.0 | .1 | -8.1 |
| 4325.0 | 3402.0 | -23.7 | -4.1 |
| 4337.5 | 3402.0 | -9.6 | .6 |
| 4350.0 | 3402.0 | 8.0 | 19.2 |
| 4362.5 | 3402.0 | 26.4 | 46.7 |
| 4375.0 | 3402.0 | 94.7 | 56.7 |
| 4387.5 | 3402.0 | 114.2 | 59.9 |
| 4400.0 | 3402.0 | 40.2 | 59.3 |
| 4412.5 | 3402.0 | 23.8 | 45.1 |
| 4425.0 | 3402.0 | 23.6 | 27.7 |
| 4437.5 | 3402.0 | 23.6 | 27.8 |
| 4450.0 | 3402.0 | 27.5 | 36.7 |
| 4462.5 | 3402.0 | 40.6 | 42.3 |
| 4475.0 | 3402.0 | 68.4 | 47.3 |
| 4487.5 | 3402.0 | 51.4 | 46.8 |
| 4500.0 | 3402.0 | 48.7 | 44.2 |
| 4512.5 | 3402.0 | 24.8 | 31.1 |
| 4525.0 | 3402.0 | 27.6 | 20.9 |
| 4537.5 | 3402.0 | 2.9 | 13.0 |
| 4550.0 | 3402.0 | .5 | 10.9 |
| 4562.5 | 3402.0 | 9.1 | 4.2 |
| 4575.0 | 3402.0 | 14.4 | 3.1 |
| 4587.5 | 3402.0 | -5.7 | 11.5 |
| 4600.0 | 3402.0 | -3.0 | 9.7 |
| 4612.5 | 3402.0 | 42.7 | 8.1 |
| 4625.0 | 3402.0 | -.1 | 13.7 |
| 4637.5 | 3402.0 | 6.7 | 15.1 |
| 4650.0 | 3402.0 | 22.2 | 7.0 |
| 4662.5 | 3402.0 | 4.0 | 7.6 |
| 4675.0 | 3402.0 | 4.5 | 8.6 |
| 4687.5 | 3402.0 | .5 | 7.0 |
| 4700.0 | 3402.0 | 9.2 | 13.0 |
| 4712.5 | 3402.0 | 17.7 | 19.1 |
| 4725.0 | 3402.0 | 33.1 | 20.9 |
| 4737.5 | 3402.0 | 35.2 | 21.7 |
| 4750.0 | 3402.0 | 9.4 | 20.6 |
| 4762.5 | 3402.0 | 13.0 | 18.0 |
| 4775.0 | 3402.0 | 12.2 | 14.8 |
| 4800.0 | 3402.0 | 19.3 | 17.2 |
|  |  |  |  |

### 1.2 Line 3500 N

| 4800.0 | 3502.0 | 3.1 | -1.2 |
| ---: | ---: | ---: | ---: |
| 4787.5 | 3502.0 | -7.6 | 16.5 |
| 4775.0 | 3502.0 | .8 | 19.0 |
| 4762.5 | 3502.0 | 69.5 | 24.3 |
| 4750.0 | 3502.0 | 29.0 | 33.2 |
| 4737.5 | 3502.0 | 29.7 | 33.6 |
| 4725.0 | 3502.0 | 36.8 | 21.0 |
| 4712.5 | 3502.0 | 3.2 | 16.3 |
| 4700.0 | 3502.0 | 6.4 | 11.1 |
| 4687.5 | 3502.0 | 5.3 | 4.8 |
| 4675.0 | 3502.0 | 3.8 | 5.7 |
| 4662.5 | 3502.0 | 5.3 | 35.8 |
| 4650.0 | 3502.0 | 7.5 | 76.2 |
| 4637.5 | 3502.0 | 157.3 | 74.7 |
| 4625.0 | 3502.0 | 207.0 | 69.1 |
| 4612.5 | 3502.0 | -3.7 | 69.9 |
| 4600.0 | 3502.0 | -22.7 | 42.9 |
| 4587.5 | 3502.0 | 11.6 | 10.0 |
| 4575.0 | 3502.0 | 22.3 | 16.4 |
| 4562.5 | 3502.0 | 42.4 | 26.2 |
| 4550.0 | 3502.0 | 28.3 | 31.3 |
| 4537.5 | 3502.0 | 26.2 | 34.8 |
| 4525.0 | 3502.0 | 37.2 | 31.4 |
| 4512.5 | 3502.0 | 39.7 | 31.6 |
| 4500.0 | 3502.0 | 25.7 | 31.2 |
| 4487.5 | 3502.0 | 29.1 | 28.4 |
| 4475.0 | 3502.0 | 24.1 | 24.5 |
| 4462.5 | 3502.0 | 23.3 | 23.5 |
| 4450.0 | 3502.0 | 20.5 | 20.9 |
| 4437.5 | 3502.0 | 20.3 | 18.5 |
| 4425.0 | 3502.0 | 16.1 | 15.5 |
| 4412.5 | 3502.0 | 12.4 | 12.5 |
| 4400.0 | 3502.0 | 8.0 | 12.7 |
| 4387.5 | 3502.0 | 5.8 | 5.7 |
| 4375.0 | 3502.0 | 21.0 | 1.6 |
| 4362.5 | 3502.0 | -18.6 | -.9 |
| 4350.0 | 3502.0 | -8.0 | -4.4 |
| 4337.5 | 3502.0 | -4.7 | -12.1 |
| 4325.0 | 3502.0 | -11.5 | -10.1 |
| 4312.5 | 3502.0 | -17.8 | -9.8 |
| 4300.0 | 3502.0 | -8.7 | -10.2 |
| 4287.5 | 3502.0 | -6.3 | -11.3 |
| 4275.0 | 3502.0 | -6.8 | -10.4 |
| 4262.5 | 3502.0 | -16.7 | -6.8 |
| 4250.0 | 3502.0 | -13.7 | -1.9 |
| 4237.5 | 3502.0 | 9.4 | -2.5 |
| 4225.0 | 3502.0 | 18.2 | -.2 |
| 4212.5 | 3502.0 | -9.9 | 3.0 |
| 4200.0 | 3502.0 | -5.1 | 3.1 |
| 4187.5 | 3502.0 | 2.5 | 3.3 |
|  |  |  |  |


| 4175.0 | 3502.0 | 9.9 | 7.7 |
| ---: | ---: | ---: | ---: |
| 4162.5 | 3502.0 | 19.2 | 2.7 |
| 4150.0 | 3502.0 | 12.2 | -1.3 |
| 4137.5 | 3502.0 | -30.1 | -7.7 |
| 4125.0 | 3502.0 | -17.7 | -15.6 |
| 4112.5 | 3502.0 | -22.0 | -22.2 |
| 4100.0 | 3502.0 | -20.3 | -21.2 |
| 4087.5 | 3502.0 | -21.1 | -23.2 |
| 4075.0 | 3502.0 | -24.7 | -25.2 |
| 4062.5 | 3502.0 | -27.7 | -26.6 |
| 4050.0 | 3502.0 | -32.2 | -25.2 |
| 4037.5 | 3502.0 | -27.2 | -22.5 |
| 4025.0 | 3502.0 | -14.3 | -20.3 |
| 4012.5 | 3502.0 | -11.1 | 118.5 |
| 4000.0 | 3502.0 | -16.9 | 227.2 |
| 3987.5 | 3502.0 | 661.9 | 253.3 |
| 3975.0 | 3502.0 | 516.4 | 246.8 |
| 3962.5 | 3502.0 | 116.3 | 226.7 |
| 3950.0 | 3502.0 | -43.8 | 101.3 |
| 3937.5 | 3502.0 | -117.1 | 239.0 |
| 3925.0 | 3502.0 | 34.8 | 240.9 |
| 3912.5 | 3502.0 | 1204.6 | 258.5 |
| 3900.0 | 3502.0 | 125.8 | 288.2 |
| 3887.5 | 3502.0 | 44.4 | 285.3 |
| 3875.0 | 3502.0 | 31.3 | 46.5 |
| 3862.5 | 3502.0 | 20.5 | 20.8 |
| 3850.0 | 3502.0 | 10.4 | 13.8 |
| 3837.5 | 3502.0 | -2.7 | 14.7 |
| 3825.0 | 3502.0 | 9.7 | 19.5 |
| 3812.5 | 3502.0 | 35.8 | 37.4 |
| 3800.0 | 3502.0 | 44.2 | 74.3 |
| 3787.5 | 3502.0 | 99.9 | 83.7 |
| 3775.0 | 3502.0 | 181.9 | 81.8 |
| 3762.5 | 3502.0 | 56.6 | 77.3 |
| 3750.0 | 3502.0 | 26.2 | 57.9 |
| 3737.5 | 3502.0 | 21.7 | 18.5 |
| 3725.0 | 3502.0 | 3.3 | 5.8 |
| 3712.5 | 3502.0 | -15.1 | -6.1 |
| 3700.0 | 3502.0 | -7.3 | -6.4 |
| 3687.5 | 3502.0 | -2.1 | -10.1 |
| 3675.0 | 3502.0 | -10.8 | -10.6 |
| 3662.5 | 3502.0 | -15.3 | -6.4 |
| 3650.0 | 3502.0 | -17.7 | -9.4 |
| 3637.5 | 3502.0 | 13.9 | -11.9 |
| 3625.0 | 3502.0 | -17.3 | -13.5 |
| 3612.5 | 3502.0 | -23.0 | -14.4 |
| 3600.0 | 3502.0 | -23.3 | -21.2 |
| 3587.5 | 3502.0 | -22.1 | -21.9 |
| 3575.0 | 3502.0 | -20.4 | -22.2 |
| 3562.5 | 3502.0 | -20.6 | -22.4 |
| 3550.0 | 3502.0 | -24.4 | -24.7 |
| 3537.5 | 3502.0 | -24.7 | -27.8 |
| 3525.0 | 3502.0 | -33.6 | -26.3 |
|  |  |  |  |


| 3512.5 | 3502.0 | -35.7 | -26.8 |
| ---: | ---: | ---: | ---: |
| 3500.0 | 3502.0 | -13.0 | -27.4 |
| 3487.5 | 3501.0 | -32.1 | -39.4 |
| 3475.0 | 3501.0 | -43.3 | -37.1 |
| 3462.5 | 3501.0 | -45.1 | -27.0 |
| 3450.0 | 3501.0 | -27.7 | -13.1 |
| 3437.5 | 3501.0 | 13.4 | 1.4 |
| 3425.0 | 3501.0 | 37.3 | 13.2 |
| 3412.5 | 3501.0 | 28.9 | 20.5 |
| 3400.0 | 3501.0 | 13.9 | 18.1 |
| 3387.5 | 3501.0 | 9.0 | 4.2 |
| 3375.0 | 3501.0 | 1.5 | -7.8 |
| 3362.5 | 3501.0 | -32.3 | -16.7 |
| 3350.0 | 3501.0 | -31.0 | -26.2 |
| 3337.5 | 3501.0 | -30.9 | -33.4 |
| 3325.0 | 3501.0 | -38.3 | -31.7 |
| 3312.5 | 3501.0 | -34.6 | -33.4 |
| 3300.0 | 3501.0 | -23.8 | -33.5 |
| 3287.5 | 3501.0 | -39.2 | -32.1 |
| 3275.0 | 3501.0 | -31.5 | -33.8 |
| 3262.5 | 3501.0 | -31.3 | -36.4 |
| 3250.0 | 3501.0 | -43.2 | -36.7 |
| 3237.5 | 3501.0 | -36.8 | -37.8 |
| 3225.0 | 3501.0 | -40.5 | -39.3 |
| 3212.5 | 3501.0 | -37.2 | -38.2 |
| 3200.0 | 3501.0 | -39.0 | -38.3 |
| 3187.5 | 3501.0 | -37.5 | -33.9 |
| 3175.0 | 3501.0 | -37.5 | -15.8 |
| 3162.5 | 3501.0 | -18.1 | 40.9 |
| 3150.0 | 3501.0 | 53.1 | 61.3 |
| 3137.5 | 3501.0 | 244.4 | 71.6 |
| 3125.0 | 3501.0 | 64.4 | 76.3 |
| 3112.5 | 3501.0 | 14.0 | 73.3 |
| 3100.0 | 3501.0 | 5.8 | 25.9 |
| 3087.5 | 3501.0 | 38.1 | 13.0 |
| 3075.0 | 3501.0 | 7.1 | 9.0 |
| 3062.5 | 3501.0 | -6 | 4.9 |
| 3050.0 | 3501.0 | -6.3 | -3.9 |
| 3037.5 | 3501.0 | -14.4 | -6.9 |
| 3025.0 | 3501.0 | -6.3 | -12.0 |
| 3012.5 | 3501.0 | -7.7 | -16.5 |
| 3000.0 | 3501.0 | -25.5 | -16.4 |
| 2987.5 | 3501.0 | -28.8 | -17.1 |
| 2975.0 | 3501.0 | -13.7 | -16.1 |
| 2962.5 | 3501.0 | -9.6 | -9.5 |
| 2950.0 | 3501.0 | -3.0 | 2.0 |
| 2937.5 | 3501.0 | 7.5 | 18.5 |
| 2925.0 | 3501.0 | 28.8 | 46.7 |
| 2912.5 | 3501.0 | 68.8 | 79.2 |
| 2900.0 | 3501.0 | 131.4 | 107.2 |
| 2887.5 | 3501.0 | 159.4 | 124.6 |
| 2875.0 | 3501.0 | 147.8 | 126.3 |
| 2862.5 | 3501.0 | 115.7 | 109.3 |
|  |  |  |  |


| 2850.0 | 3501.0 | 77.0 | 84.0 |
| ---: | ---: | ---: | ---: |
| 2837.5 | 3501.0 | 46.7 | 58.6 |
| 2825.0 | 3501.0 | 32.8 | 39.0 |
| 2812.5 | 3501.0 | 20.8 | 24.9 |
| 2800.0 | 3501.0 | 17.8 | 14.4 |
| 2787.5 | 3501.0 | 6.3 | 9.0 |
| 2775.0 | 3501.0 | -5.9 | 4.5 |
| 2762.5 | 3501.0 | 6.0 | -1.6 |
| 2750.0 | 3501.0 | -1.7 | -7.2 |
| 2737.5 | 3501.0 | -12.5 | -6.7 |
| 2725.0 | 3501.0 | -21.8 | -8.6 |
| 2712.5 | 3501.0 | -3.6 | -12.7 |
| 2700.0 | 3501.0 | -3.3 | -15.4 |
| 2687.5 | 3501.0 | -22.5 | -15.4 |
| 2675.0 | 3501.0 | -26.0 | -20.4 |
| 2662.5 | 3501.0 | -21.7 | -25.6 |
| 2650.0 | 3501.0 | -28.4 | -16.4 |
| 2637.5 | 3501.0 | -29.5 | -4.3 |
| 2625.0 | 3501.0 | 23.4 | 6.5 |
| 2612.5 | 3501.0 | 34.8 | 15.9 |
| 2600.0 | 3501.0 | 32.1 | 24.3 |
| 2587.5 | 3501.0 | 18.5 | 21.6 |
| 2575.0 | 3501.0 | 12.5 | 17.1 |
| 2562.5 | 3501.0 | 9.9 | 12.8 |
| 2550.0 | 3501.0 | 12.6 | 10.8 |
| 2537.5 | 3501.0 | 10.7 | 9.2 |
| 2525.0 | 3501.0 | 8.4 | 7.6 |
| 2512.5 | 3501.0 | 4.3 | 5.3 |
| 2500.0 | 3501.0 | 2.0 | 3.8 |
| 2487.5 | 3501.0 | .9 | 3.6 |
| 2475.0 | 3501.0 | 3.2 | 4.6 |
| 2462.5 | 3501.0 | 7.7 | 6.2 |
| 2450.0 | 3501.0 | 9.1 | 8.3 |
| 2437.5 | 3501.0 | 10.1 | 10.9 |
| 2425.0 | 3501.0 | 11.5 | 12.4 |
| 2412.5 | 3501.0 | 16.0 | 13.2 |
| 2400.0 | 3501.0 | 15.3 | 14.3 |

### 1.3 Line 3600 N

| 2400.0 | 3601.0 | 22.2 | 21.2 |
| :--- | :--- | :--- | :--- |
| 2412.5 | 3601.0 | 20.6 | 20.7 |
| 2425.0 | 3601.0 | 20.8 | 20.0 |
| 2437.5 | 3601.0 | 19.3 | 18.3 |
| 2450.0 | 3601.0 | 17.1 | 16.8 |
| 2462.5 | 3601.0 | 13.5 | 15.2 |
| 2475.0 | 3601.0 | 13.4 | 14.2 |
| 2487.5 | 3601.0 | 12.8 | 14.2 |
| 2500.0 | 3601.0 | 14.4 | 16.8 |
| 2512.5 | 3601.0 | 17.1 | 25.9 |
| 2525.0 | 3601.0 | 26.4 | 28.6 |


| 2537.5 | 3601.0 | 58.7 | 31.8 |
| ---: | ---: | ---: | ---: |
| 2550.0 | 3601.0 | 26.3 | 45.6 |
| 2562.5 | 3601.0 | 30.7 | 50.6 |
| 2575.0 | 3601.0 | 85.8 | 45.5 |
| 2587.5 | 3601.0 | 51.6 | 39.9 |
| 2600.0 | 3601.0 | 33.0 | 29.4 |
| 2612.5 | 3601.0 | -1.7 | 8.4 |
| 2625.0 | 3601.0 | -21.6 | -6.6 |
| 2637.5 | 3601.0 | -19.1 | -16.6 |
| 2650.0 | 3601.0 | -23.4 | -18.4 |
| 2662.5 | 3601.0 | -17.0 | -18.6 |
| 2675.0 | 3601.0 | -11.1 | -20.1 |
| 2687.5 | 3601.0 | -22.3 | -19.8 |
| 2700.0 | 3601.0 | -26.8 | -20.4 |
| 2712.5 | 3601.0 | -22.0 | -20.9 |
| 2725.0 | 3601.0 | -20.0 | -18.7 |
| 2737.5 | 3601.0 | -13.3 | -14.8 |
| 2750.0 | 3601.0 | -11.6 | -10.2 |
| 2762.5 | 3601.0 | -6.9 | -3.0 |
| 2775.0 | 3601.0 | .9 | 4.6 |
| 2787.5 | 3601.0 | 15.8 | 16.5 |
| 2800.0 | 3601.0 | 24.7 | 32.1 |
| 2812.5 | 3601.0 | 48.1 | 58.1 |
| 2825.0 | 3601.0 | 71.2 | 59.7 |
| 2837.5 | 3601.0 | 130.8 | 61.9 |
| 2850.0 | 3601.0 | 23.8 | 60.1 |
| 2862.5 | 3601.0 | 35.6 | 43.5 |
| 2875.0 | 3601.0 | 39.0 | 9.1 |
| 2887.5 | 3601.0 | -11.7 | -5.1 |
| 2900.0 | 3601.0 | -41.3 | -19.6 |
| 2912.5 | 3601.0 | -47.3 | -35.1 |
| 2925.0 | 3601.0 | -36.5 | -38.7 |
| 2937.5 | 3601.0 | -38.8 | -34.8 |
| 2950.0 | 3601.0 | -29.7 | -30.3 |
| 2962.5 | 3601.0 | -21.9 | -25.5 |
| 2975.0 | 3601.0 | -24.8 | -20.0 |
| 2987.5 | 3601.0 | -12.1 | -16.6 |
| 3000.0 | 3601.0 | -11.7 | -12.0 |
| 3012.5 | 3601.0 | -12.7 | -2.5 |
| 3025.0 | 3601.0 | 1.3 | 7.7 |
| 3037.5 | 3601.0 | 22.8 | 22.3 |
| 3050.0 | 3601.0 | 38.8 | 23.6 |
| 3062.5 | 3601.0 | 61.1 | 20.3 |
| 3075.0 | 3601.0 | -6.0 | 16.0 |
| 3087.5 | 3601.0 | -15.1 | 13.6 |
| 3100.0 | 3601.0 | 1.3 | -6.7 |
| 3112.5 | 3601.0 | 26.5 | -8.9 |
| 3125.0 | 3601.0 | -40.3 | -10.4 |
| 3137.5 | 3601.0 | -16.7 | -17.1 |
| 3150.0 | 3601.0 | -23.0 | -29.0 |
| 3162.5 | 3601.0 | -31.8 | -24.2 |
| 3175.0 | 3601.0 | -33.4 | -20.6 |
| 3187.5 | 3601.0 | -16.3 | -14.2 |
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| ---: | ---: | ---: | ---: |
| 3200.0 | 3601.0 | 1.7 | -8.7 |
| 3212.5 | 3601.0 | 8.7 | -7.2 |
| 3225.0 | 3601.0 | -4.3 | -10.2 |
| 3237.5 | 3601.0 | -25.7 | -19.4 |
| 3250.0 | 3601.0 | -31.5 | -30.6 |
| 3262.5 | 3601.0 | -44.0 | -37.1 |
| 3275.0 | 3601.0 | -47.4 | -38.4 |
| 3287.5 | 3601.0 | -36.8 | -31.3 |
| 3300.0 | 3601.0 | -32.5 | -26.5 |
| 3312.5 | 3601.0 | 4.2 | -22.5 |
| 3325.0 | 3601.0 | -19.8 | -19.2 |
| 3337.5 | 3601.0 | -27.6 | -14.3 |
| 3350.0 | 3601.0 | -20.5 | -14.4 |
| 3362.5 | 3601.0 | -8.0 | -10.2 |
| 3375.0 | 3601.0 | 3.9 | -7.5 |
| 3387.5 | 3601.0 | 1.3 | -4.6 |
| 3400.0 | 3601.0 | -14.2 | -4.4 |
| 3412.5 | 3601.0 | -5.9 | -5.5 |
| 3425.0 | 3601.0 | -6.9 | -6.3 |
| 3437.5 | 3601.0 | -1.8 | -5.5 |
| 3450.0 | 3601.0 | -2.5 | -1.3 |
| 3462.5 | 3601.0 | -10.3 | 1.5 |
| 3475.0 | 3601.0 | 15.1 | -3.4 |
| 3487.5 | 3601.0 | 6.9 | -3.6 |
| 3500.0 | 3601.0 | -26.3 | -1.4 |
| 3512.5 | 3602.0 | -28.5 | -23.0 |
| 3525.0 | 3602.0 | -12.8 | -23.1 |
| 3537.5 | 3602.0 | -25.8 | -22.2 |
| 3550.0 | 3602.0 | -23.5 | -19.9 |
| 3562.5 | 3602.0 | -20.3 | -20.3 |
| 3575.0 | 3602.0 | -17.0 | -17.5 |
| 3587.5 | 3602.0 | -14.9 | -14.9 |
| 3600.0 | 3602.0 | -11.6 | -11.8 |
| 3612.5 | 3602.0 | -10.7 | -10.4 |
| 3625.0 | 3602.0 | -4.9 | -9.2 |
| 3637.5 | 3602.0 | -10.1 | -9.2 |
| 3650.0 | 3602.0 | -8.6 | -7.1 |
| 3662.5 | 3602.0 | -11.9 | -5.3 |
| 3675.0 | 3602.0 | .2 | -.1 |
| 3687.5 | 3602.0 | 3.7 | 5.1 |
| 3700.0 | 3602.0 | 16.2 | 12.7 |
| 3712.5 | 3602.0 | 17.3 | 22.0 |
| 3725.0 | 3602.0 | 26.2 | 35.0 |
| 3737.5 | 3602.0 | 46.5 | 44.9 |
| 3750.0 | 3602.0 | 69.0 | 47.7 |
| 3762.5 | 3602.0 | 65.6 | 49.0 |
| 3775.0 | 3602.0 | 31.4 | 45.0 |
| 3787.5 | 3602.0 | 32.7 | 43.1 |
| 3800.0 | 3602.0 | 27.5 | 44.6 |
| 3812.5 | 3602.0 | 58.3 | 43.9 |
| 3825.0 | 3602.0 | 72.9 | 46.3 |
| 3837.5 | 3602.0 | 28.0 | 46.1 |
| 3850.0 | 3602.0 | 44.8 | 42.5 |
|  |  |  |  |


| 3862.5 | 3602.0 | 26.3 | 40.2 |
| ---: | ---: | ---: | ---: |
| 3875.0 | 3602.0 | 40.7 | 44.4 |
| 3887.5 | 3602.0 | 61.3 | 43.1 |
| 3900.0 | 3602.0 | 48.8 | 48.3 |
| 3912.5 | 3602.0 | 38.2 | 59.6 |
| 3925.0 | 3602.0 | 52.5 | 126.7 |
| 3937.5 | 3602.0 | 97.2 | 137.9 |
| 3950.0 | 3602.0 | 396.8 | 153.2 |
| 3962.5 | 3602.0 | 104.9 | 208.9 |
| 3975.0 | 3602.0 | 114.7 | 178.5 |
| 3987.5 | 3602.0 | 331.1 | 94.9 |
| 4000.0 | 3602.0 | -55.2 | 77.5 |
| 4012.5 | 3602.0 | -20.8 | 57.8 |
| 4025.0 | 3602.0 | 17.7 | -3.7 |
| 4037.5 | 3602.0 | 16.0 | 12.0 |
| 4050.0 | 3602.0 | 23.7 | 17.0 |
| 4062.5 | 3602.0 | 23.4 | 20.7 |
| 4075.0 | 3602.0 | 4.1 | 23.3 |
| 4087.5 | 3602.0 | 36.3 | 19.7 |
| 4100.0 | 3602.0 | 29.0 | 14.2 |
| 4112.5 | 3602.0 | 5.5 | 11.7 |
| 4125.0 | 3602.0 | -4.1 | 1.4 |
| 4137.5 | 3602.0 | -8.0 | -5.6 |
| 4150.0 | 3602.0 | -15.3 | -13.4 |
| 4162.5 | 3602.0 | -6.2 | -15.9 |
| 4175.0 | 3602.0 | -33.5 | -19.2 |
| 4187.5 | 3602.0 | -16.3 | -12.2 |
| 4200.0 | 3602.0 | -24.8 | -9.4 |
| 4212.5 | 3602.0 | 19.8 | -8.2 |
| 4225.0 | 3602.0 | 7.9 | -5.5 |
| 4237.5 | 3602.0 | -27.6 | -.5 |
| 4250.0 | 3602.0 | -2.6 | -4.1 |
| 4262.5 | 3602.0 | -.1 | -4.9 |
| 4275.0 | 3602.0 | 1.9 | -1.3 |
| 4287.5 | 3602.0 | 3.9 | -1.3 |
| 4300.0 | 3602.0 | -9.7 | -.2 |
| 4312.5 | 3602.0 | -2.4 | -.7 |
| 4325.0 | 3602.0 | 5.5 | -.2 |
| 4337.5 | 3602.0 | -1.0 | 3.2 |
| 4350.0 | 3602.0 | 6.7 | 9.2 |
| 4362.5 | 3602.0 | 7.1 | 10.3 |
| 4375.0 | 3602.0 | 27.5 | 16.5 |
| 4387.5 | 3602.0 | 11.3 | 21.5 |
| 4400.0 | 3602.0 | 29.7 | 26.8 |
| 4412.5 | 3602.0 | 32.1 | 30.5 |
| 4425.0 | 3602.0 | 33.4 | 32.9 |
| 4437.5 | 3602.0 | 46.0 | 31.3 |
| 4450.0 | 3602.0 | 23.2 | 30.4 |
| 4462.5 | 3602.0 | 21.7 | 30.9 |
| 4475.0 | 3602.0 | 27.5 | 28.0 |
| 4487.5 | 3602.0 | 35.9 | 26.0 |
| 4500.0 | 3602.0 | 31.6 | 23.5 |
| 4512.5 | 3602.0 | 13.3 | 23.6 |


| 4525.0 | 3602.0 | 9.3 | 19.6 |
| ---: | ---: | ---: | ---: |
| 4537.5 | 3602.0 | 27.9 | 20.2 |
| 4550.0 | 3602.0 | 15.9 | 28.3 |
| 4562.5 | 3602.0 | 34.7 | 37.2 |
| 4575.0 | 3602.0 | 53.7 | 42.2 |
| 4587.5 | 3602.0 | 53.7 | 41.2 |
| 4600.0 | 3602.0 | 52.9 | 31.1 |
| 4612.5 | 3602.0 | 11.0 | 24.5 |
| 4625.0 | 3602.0 | -15.8 | 57.1 |
| 4637.5 | 3602.0 | 20.8 | 88.3 |
| 4650.0 | 3602.0 | 216.5 | 94.7 |
| 4662.5 | 3602.0 | 209.1 | 95.1 |
| 4675.0 | 3602.0 | 43.1 | 92.6 |
| 4687.5 | 3602.0 | -14.0 | 49.5 |
| 4700.0 | 3602.0 | 8.1 | 6.3 |
| 4712.5 | 3602.0 | 1.2 | -.1 |
| 4725.0 | 3602.0 | -7.0 | 7.1 |
| 4737.5 | 3602.0 | 11.4 | 8.3 |
| 4750.0 | 3602.0 | 21.9 | 13.6 |
| 4762.5 | 3602.0 | 13.8 | 21.7 |
| 4775.0 | 3602.0 | 27.7 | 26.0 |
| 4787.5 | 3602.0 | 33.5 | 27.0 |
| 4800.0 | 3602.0 | 33.1 | 31.4 |

1.4 Line 3700 N , West of Baseline 2400 E

| 1600.0 | 3700.0 | 53.6 | 31.0 |
| ---: | ---: | ---: | ---: |
| 1612.5 | 3700.0 | 33.2 | 20.6 |
| 1625.0 | 3700.0 | 6.1 | 16.1 |
| 1637.5 | 3700.0 | -10.6 | 6.4 |
| 1650.0 | 3700.0 | -1.8 | 1.7 |
| 1662.5 | 3700.0 | 5.2 | 1.8 |
| 1675.0 | 3700.0 | 9.7 | 4.0 |
| 1687.5 | 3700.0 | 6.6 | 3.7 |
| 1700.0 | 3700.0 | .5 | 1.6 |
| 1712.5 | 3700.0 | -3.5 | -2.2 |
| 1725.0 | 3700.0 | -5.4 | -5.2 |
| 1737.5 | 3700.0 | -9.2 | -5.4 |
| 1750.0 | 3700.0 | -8.6 | -4.5 |
| 1762.5 | 3700.0 | -.3 | -3.1 |
| 1775.0 | 3700.0 | 1.0 | -2.1 |
| 1787.5 | 3700.0 | 1.8 | -3.5 |
| 1800.0 | 3700.0 | -4.3 | -7.9 |
| 1812.5 | 3700.0 | -15.7 | -10.4 |
| 1825.0 | 3700.0 | -22.3 | -13.4 |
| 1837.5 | 3700.0 | -11.6 | -15.2 |
| 1850.0 | 3700.0 | -13.2 | -17.2 |
| 1862.5 | 3700.0 | -13.4 | -18.8 |
| 1875.0 | 3700.0 | -25.4 | -22.4 |
| 1887.5 | 3700.0 | -30.6 | -25.4 |
| 1900.0 | 3700.0 | -29.3 | -28.2 |
| 1912.5 | 3700.0 | -28.5 | -28.2 |


| 1925.0 | 3700.0 | -27.1 | -26.7 |
| :--- | :--- | :--- | ---: |
| 1937.5 | 3700.0 | -25.5 | -25.6 |
| 1950.0 | 3700.0 | -23.3 | -25.2 |
| 1962.5 | 3700.0 | -23.7 | -24.9 |
| 1975.0 | 3700.0 | -26.4 | -24.1 |
| 1987.5 | 3700.0 | -25.7 | -22.6 |
| 2000.0 | 3700.0 | -21.2 | -19.6 |
| 2012.5 | 3700.0 | -16.1 | -14.9 |
| 2025.0 | 3700.0 | -8.5 | -9.2 |
| 2037.5 | 3700.0 | -3.1 | -2.4 |
| 2050.0 | 3700.0 | 2.9 | 4.5 |
| 2062.5 | 3700.0 | 13.0 | 9.3 |
| 2075.0 | 3700.0 | 18.4 | 13.8 |
| 2087.5 | 3700.0 | 15.1 | 15.9 |
| 2100.0 | 3700.0 | 19.6 | 15.9 |
| 2112.5 | 3700.0 | 13.2 | 15.2 |
| 2125.0 | 3700.0 | 13.0 | 14.9 |
| 2137.5 | 3700.0 | 15.0 | 14.0 |
| 2150.0 | 3700.0 | 13.8 | 14.7 |
| 2162.5 | 3700.0 | 15.0 | 16.1 |
| 2175.0 | 3700.0 | 16.6 | 17.6 |
| 2187.5 | 3700.0 | 19.9 | 19.6 |
| 2200.0 | 3700.0 | 22.6 | 22.2 |
| 2212.5 | 3700.0 | 24.1 | 25.0 |
| 2225.0 | 3700.0 | 27.6 | 28.0 |
| 2237.5 | 3700.0 | 30.6 | 31.4 |
| 2250.0 | 3700.0 | 35.2 | 35.4 |
| 2262.5 | 3700.0 | 39.5 | 39.8 |
| 2275.0 | 3700.0 | 44.3 | 44.9 |
| 2287.5 | 3700.0 | 49.5 | 49.7 |
| 2300.0 | 3700.0 | 56.0 | 53.3 |
| 2312.5 | 3700.0 | 59.0 | 54.6 |
| 2325.0 | 3700.0 | 57.8 | 52.9 |
| 2337.5 | 3700.0 | 50.8 | 49.1 |
| 2350.0 | 3700.0 | 40.7 | 43.9 |
| 2362.5 | 3700.0 | 37.1 | 38.0 |
| 2375.0 | 3700.0 | 33.0 | 32.7 |
| 2387.5 | 3700.0 | 28.5 | 30.7 |
| 2400.0 | 3700.0 | 24.1 | 28.5 |
|  |  |  |  |

1.5 Line 3700 N , East of Baseline 2400 E

| 4800.0 | 3702.0 | 42.4 | 52.0 |
| :--- | :--- | :--- | :--- |
| 4787.5 | 3702.0 | 58.1 | 63.6 |
| 4775.0 | 3702.0 | 55.5 | 69.3 |
| 4762.5 | 3702.0 | 98.5 | 76.6 |
| 4750.0 | 3702.0 | 92.0 | 76.6 |
| 4737.5 | 3702.0 | 79.1 | 73.0 |
| 4725.0 | 3702.0 | 57.7 | 56.7 |
| 4712.5 | 3702.0 | 37.6 | 40.3 |
| 4700.0 | 3702.0 | 17.3 | 26.2 |
| 4687.5 | 3702.0 | 10.0 | 15.6 |


| 4675.0 | 3702.0 | 8.4 | 10.3 |
| ---: | ---: | ---: | ---: |
| 4662.5 | 3702.0 | 4.5 | 9.8 |
| 4650.0 | 3702.0 | 11.5 | 11.1 |
| 4637.5 | 3702.0 | 14.5 | 13.1 |
| 4625.0 | 3702.0 | 16.7 | 17.1 |
| 4612.5 | 3702.0 | 18.1 | 22.6 |
| 4600.0 | 3702.0 | 24.5 | 28.1 |
| 4587.5 | 3702.0 | 39.2 | 33.1 |
| 4575.0 | 3702.0 | 41.8 | 37.6 |
| 4562.5 | 3702.0 | 41.7 | 39.3 |
| 4550.0 | 3702.0 | 40.7 | 37.9 |
| 4537.5 | 3702.0 | 33.0 | 35.8 |
| 4525.0 | 3702.0 | 32.1 | 36.5 |
| 4512.5 | 3702.0 | 31.5 | 34.5 |
| 4500.0 | 3702.0 | 45.0 | 25.6 |
| 4487.5 | 3702.0 | 31.1 | 12.7 |
| 4475.0 | 3702.0 | -11.8 | 3.8 |
| 4462.5 | 3702.0 | -32.1 | -3.9 |
| 4450.0 | 3702.0 | -13.1 | -13.4 |
| 4437.5 | 3702.0 | 6.2 | -8.0 |
| 4425.0 | 3702.0 | -16.1 | .2 |
| 4412.5 | 3702.0 | 15.3 | 1.0 |
| 4400.0 | 3702.0 | 8.6 | -1.2 |
| 4387.5 | 3702.0 | -9.2 | 10.9 |
| 4375.0 | 3702.0 | -4.7 | 22.9 |
| 4362.5 | 3702.0 | 44.3 | 29.8 |
| 4350.0 | 3702.0 | 75.3 | 37.2 |
| 4337.5 | 3702.0 | 43.3 | 43.8 |
| 4325.0 | 3702.0 | 28.0 | 44.8 |
| 4312.5 | 3702.0 | 28.2 | 37.1 |
| 4300.0 | 3702.0 | 49.3 | 32.9 |
| 4287.5 | 3702.0 | 36.6 | 30.7 |
| 4275.0 | 3702.0 | 22.4 | 28.6 |
| 4262.5 | 3702.0 | 16.8 | 18.9 |
| 4250.0 | 3702.0 | 17.7 | 9.8 |
| 4237.5 | 3702.0 | 1.2 | 4.6 |
| 4225.0 | 3702.0 | -9.0 | -1.0 |
| 4212.5 | 3702.0 | -3.9 | -7.5 |
| 4200.0 | 3702.0 | -11.1 | -10.3 |
| 4187.5 | 3702.0 | -14.7 | -10.5 |
| 4175.0 | 3702.0 | -12.9 | -12.1 |
| 4162.5 | 3702.0 | -9.9 | -12.3 |
| 4150.0 | 3702.0 | -11.8 | -12.1 |
| 4137.5 | 3702.0 | -12.1 | -12.2 |
| 4125.0 | 3702.0 | -13.8 | -13.4 |
| 4112.5 | 3702.0 | -13.2 | -15.0 |
| 4100.0 | 3702.0 | -15.9 | -17.3 |
| 4087.5 | 3702.0 | -20.0 | -20.8 |
| 4075.0 | 3702.0 | -23.8 | -25.1 |
| 4062.5 | 3702.0 | -31.1 | -32.0 |
| 4050.0 | 3702.0 | -34.6 | -36.1 |
| 4037.5 | 3702.0 | -50.6 | -38.9 |
| 4025.0 | 3702.0 | -40.4 | -41.9 |
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| 4012.5 | 3702.0 | -37.7 | -41.9 |
| ---: | ---: | ---: | ---: |
| 4000.0 | 3702.0 | -46.4 | -39.1 |
| 3987.5 | 3702.0 | -34.3 | -32.6 |
| 3975.0 | 3702.0 | -36.8 | -25.2 |
| 3962.5 | 3702.0 | -8.0 | -17.8 |
| 3950.0 | 3702.0 | -.5 | -13.9 |
| 3937.5 | 3702.0 | -9.3 | 7.6 |
| 3925.0 | 3702.0 | -14.8 | 38.0 |
| 3912.5 | 3702.0 | 70.8 | 60.5 |
| 3900.0 | 3702.0 | 143.9 | 91.0 |
| 3887.5 | 3702.0 | 111.8 | 124.7 |
| 3875.0 | 3702.0 | 143.2 | 131.5 |
| 3862.5 | 3702.0 | 153.9 | 114.4 |
| 3850.0 | 3702.0 | 104.9 | 99.2 |
| 3837.5 | 3702.0 | 58.0 | 75.6 |
| 3825.0 | 3702.0 | 35.8 | 46.3 |
| 3812.5 | 3702.0 | 25.4 | 26.2 |
| 3800.0 | 3702.0 | 7.3 | 14.5 |
| 3787.5 | 3702.0 | 4.5 | 9.4 |
| 3775.0 | 3702.0 | -.3 | 9.8 |
| 3762.5 | 3702.0 | 10.3 | 15.4 |
| 3750.0 | 3702.0 | 27.1 | 28.0 |
| 3737.5 | 3702.0 | 35.6 | 39.2 |
| 3725.0 | 3702.0 | 67.5 | 45.3 |
| 3712.5 | 3702.0 | 55.5 | 46.1 |
| 3700.0 | 3702.0 | 40.7 | 42.0 |
| 3687.5 | 3702.0 | 31.0 | 30.4 |
| 3675.0 | 3702.0 | 15.5 | 19.7 |
| 3662.5 | 3702.0 | 9.1 | 10.9 |
| 3650.0 | 3702.0 | 2.2 | 3.5 |
| 3637.5 | 3702.0 | -3.1 | -1.8 |
| 3625.0 | 3702.0 | -6.1 | -4.4 |
| 3612.5 | 3702.0 | -11.0 | -7.6 |
| 3600.0 | 3702.0 | -4.1 | -10.4 |
| 3587.5 | 3702.0 | -13.8 | -13.0 |
| 3575.0 | 3702.0 | -17.2 | -12.5 |
| 3562.5 | 3702.0 | -19.0 | -11.5 |
| 3550.0 | 3702.0 | -8.2 | -11.7 |
| 3537.5 | 3702.0 | .5 | -11.6 |
| 3525.0 | 3702.0 | -14.5 | -8.0 |
| 3512.5 | 3702.0 | -16.9 | -7.9 |
| 3500.0 | 3702.0 | -.8 | -10.7 |
| 3487.5 | 3701.0 | -25.8 | -24.6 |
| 3475.0 | 3701.0 | -18.3 | -32.3 |
| 3462.5 | 3701.0 | -50.3 | 8.3 |
| 3450.0 | 3701.0 | -62.9 | 33.0 |
| 3437.5 | 3701.0 | 198.7 | 42.2 |
| 3425.0 | 3701.0 | 97.7 | 50.1 |
| 3412.5 | 3701.0 | 28.0 | 65.3 |
| 3400.0 | 3701.0 | -11.2 | 26.8 |
| 3387.5 | 3701.0 | 13.5 | 5.8 |
| 3375.0 | 3701.0 | 5.8 | -5.1 |
| 3362.5 | 3701.0 | -7.1 | -4.6 |
|  |  |  |  |


| 3350.0 | 3701.0 | -26.5 | -7.9 |
| ---: | ---: | ---: | ---: |
| 3337.5 | 3701.0 | -8.8 | -15.5 |
| 3325.0 | 3701.0 | -2.9 | -19.7 |
| 3312.5 | 3701.0 | -32.0 | -19.7 |
| 3300.0 | 3701.0 | -28.5 | -22.8 |
| 3287.5 | 3701.0 | -26.4 | -26.8 |
| 3275.0 | 3701.0 | -24.0 | -25.8 |
| 3262.5 | 3701.0 | -23.3 | -26.5 |
| 3250.0 | 3701.0 | -26.6 | -28.2 |
| 3237.5 | 3701.0 | -32.4 | -31.8 |
| 3225.0 | 3701.0 | -34.8 | -34.7 |
| 3212.5 | 3701.0 | -42.0 | -38.2 |
| 3200.0 | 3701.0 | -37.5 | -40.7 |
| 3187.5 | 3701.0 | -44.1 | -40.8 |
| 3175.0 | 3701.0 | -44.9 | -32.3 |
| 3162.5 | 3701.0 | -35.7 | 32.1 |
| 3150.0 | 3701.0 | .5 | 55.8 |
| 3137.5 | 3701.0 | 284.6 | 63.3 |
| 3125.0 | 3701.0 | 74.3 | 67.4 |
| 3112.5 | 3701.0 | -7.4 | 62.4 |
| 3100.0 | 3701.0 | -14.8 | 1.8 |
| 3087.5 | 3701.0 | -24.8 | -9.8 |
| 3075.0 | 3701.0 | -18.2 | -9.4 |
| 3062.5 | 3701.0 | 16.0 | -10.3 |
| 3050.0 | 3701.0 | -5.1 | -7.9 |
| 3037.5 | 3701.0 | -19.6 | -9.9 |
| 3025.0 | 3701.0 | -12.8 | -18.0 |
| 3012.5 | 3701.0 | -27.9 | -21.9 |
| 3000.0 | 3701.0 | -24.7 | -24.5 |
| 2987.5 | 3701.0 | -24.7 | -28.4 |
| 2975.0 | 3701.0 | -32.3 | -24.0 |
| 2962.5 | 3701.0 | -32.5 | -25.6 |
| 2950.0 | 3701.0 | -6.0 | -27.3 |
| 2937.5 | 3701.0 | -32.3 | -27.4 |
| 2925.0 | 3701.0 | -33.3 | -27.5 |
| 2912.5 | 3701.0 | -33.0 | -32.7 |
| 2900.0 | 3701.0 | -32.8 | -33.4 |
| 2887.5 | 3701.0 | -31.9 | -35.3 |
| 2875.0 | 3701.0 | -36.0 | 23.4 |
| 2862.5 | 3701.0 | -42.7 | 43.6 |
| 2850.0 | 3701.0 | 260.6 | 54.3 |
| 2837.5 | 3701.0 | 68.2 | 63.1 |
| 2825.0 | 3701.0 | 21.3 | 71.5 |
| 2812.5 | 3701.0 | 8.0 | 18.0 |
| 2800.0 | 3701.0 | -.7 | 1.0 |
| 2787.5 | 3701.0 | -6.8 | -8.5 |
| 2775.0 | 3701.0 | -16.9 | -15.7 |
| 2762.5 | 3701.0 | -26.3 | -21.9 |
| 2750.0 | 3701.0 | -27.6 | -26.3 |
| 2737.5 | 3701.0 | -32.0 | -29.4 |
| 2725.0 | 3701.0 | -28.6 | -30.9 |
| 2712.5 | 3701.0 | -32.4 | -34.4 |
| 2700.0 | 3701.0 | -33.7 | -37.6 |
|  |  |  |  |


| 2687.5 | 3701.0 | -45.2 | -41.7 |
| ---: | ---: | ---: | ---: |
| 2675.0 | 3701.0 | -48.2 | -44.4 |
| 2662.5 | 3701.0 | -49.1 | -45.3 |
| 2650.0 | 3701.0 | -45.9 | -35.5 |
| 2637.5 | 3701.0 | -38.1 | -16.6 |
| 2625.0 | 3701.0 | 3.6 | .2 |
| 2612.5 | 3701.0 | 46.6 | 12.1 |
| 2600.0 | 3701.0 | 34.7 | 18.0 |
| 2587.5 | 3701.0 | 13.6 | 15.7 |
| 2575.0 | 3701.0 | -8.3 | 21.4 |
| 2562.5 | 3701.0 | -7.9 | 23.1 |
| 2550.0 | 3701.0 | 74.7 | 25.6 |
| 2537.5 | 3701.0 | 43.4 | 30.6 |
| 2525.0 | 3701.0 | 25.9 | 35.1 |
| 2512.5 | 3701.0 | 16.7 | 22.6 |
| 2500.0 | 3701.0 | 14.8 | 15.8 |
| 2487.5 | 3701.0 | 12.0 | 12.9 |
| 2475.0 | 3701.0 | 9.7 | 11.9 |
| 2462.5 | 3701.0 | 11.5 | 11.7 |
| 2450.0 | 3701.0 | 11.5 | 12.4 |
| 2437.5 | 3701.0 | 13.6 | 14.1 |
| 2425.0 | 3701.0 | 15.9 | 16.2 |
| 2412.5 | 3701.0 | 18.0 | 17.4 |
| 2400.0 | 3701.0 | 22.0 | 18.6 |

1.6 Line 3800 N , West of Baseline 2400 E

| 2387.5 | 3800.0 | 4.6 | 6.1 |
| ---: | ---: | ---: | ---: |
| 2375.0 | 3800.0 | 5.9 | 7.4 |
| 2362.5 | 3800.0 | 8.7 | 9.5 |
| 2350.0 | 3800.0 | 12.5 | 12.8 |
| 2337.5 | 3800.0 | 16.0 | 17.7 |
| 2325.0 | 3800.0 | 20.9 | 27.0 |
| 2312.5 | 3800.0 | 30.3 | 46.1 |
| 2300.0 | 3800.0 | 55.2 | 90.6 |
| 2287.5 | 3800.0 | 107.9 | 123.1 |
| 2275.0 | 3800.0 | 238.8 | 144.8 |
| 2262.5 | 3800.0 | 183.1 | 151.6 |
| 2250.0 | 3800.0 | 138.9 | 142.0 |
| 2237.5 | 3800.0 | 89.4 | 103.0 |
| 2225.0 | 3800.0 | 59.8 | 73.6 |
| 2212.5 | 3800.0 | 43.8 | 52.3 |
| 2200.0 | 3800.0 | 36.2 | 38.8 |
| 2187.5 | 3800.0 | 32.5 | 30.8 |
| 2175.0 | 3800.0 | 21.9 | 25.7 |
| 2162.5 | 3800.0 | 19.5 | 22.4 |
| 2150.0 | 3800.0 | 18.2 | 19.3 |
| 2137.5 | 3800.0 | 19.7 | 17.6 |
| 2125.0 | 3800.0 | 17.0 | 15.5 |
| 2112.5 | 3800.0 | 13.7 | 13.0 |
| 2100.0 | 3800.0 | 8.9 | 8.7 |


| 2087.5 | 3800.0 | 5.8 | 4.8 |
| ---: | ---: | ---: | ---: |
| 2075.0 | 3800.0 | -1.8 | 2.7 |
| 2062.5 | 3800.0 | -2.4 | .9 |
| 2050.0 | 3800.0 | 2.8 | -1.5 |
| 2037.5 | 3800.0 | -2.7 | -2.0 |
| 2025.0 | 3800.0 | -3.5 | -3.4 |
| 2012.5 | 3800.0 | -4.3 | -6.3 |
| 2000.0 | 3800.0 | -9.4 | -7.7 |
| 1987.5 | 3800.0 | -11.4 | -8.5 |
| 1975.0 | 3800.0 | -10.0 | -9.1 |
| 1962.5 | 3800.0 | -7.6 | -10.0 |
| 1950.0 | 3800.0 | -7.2 | -12.0 |
| 1937.5 | 3800.0 | -13.9 | -14.7 |
| 1925.0 | 3800.0 | -21.4 | -18.6 |
| 1912.5 | 3800.0 | -23.3 | -22.8 |
| 1900.0 | 3800.0 | -27.4 | -23.3 |
| 1887.5 | 3800.0 | -27.8 | -21.5 |
| 1875.0 | 3800.0 | -16.4 | -19.1 |
| 1862.5 | 3800.0 | -12.5 | -15.9 |
| 1850.0 | 3800.0 | -11.5 | -12.1 |
| 1837.5 | 3800.0 | -11.1 | -8.4 |
| 1825.0 | 3800.0 | -9.1 | -8.9 |
| 1812.5 | 3800.0 | 2.3 | -12.1 |
| 1800.0 | 3800.0 | -15.2 | -15.0 |
| 1787.5 | 3800.0 | -27.6 | -17.6 |
| 1775.0 | 3800.0 | -25.2 | -22.5 |
| 1762.5 | 3800.0 | -22.4 | -24.3 |
| 1750.0 | 3800.0 | -22.1 | -21.8 |
| 1737.5 | 3800.0 | -24.4 | -20.3 |
| 1725.0 | 3800.0 | -15.1 | -20.5 |
| 1712.5 | 3800.0 | -17.4 | -20.1 |
| 1700.0 | 3800.0 | -23.4 | -18.6 |

### 1.7 Line 3800 N , East of Baseline 2400 E

| 2400.0 | 3801.0 | 4.4 | 6.6 |
| ---: | ---: | ---: | ---: |
| 2412.5 | 3801.0 | 5.8 | 10.1 |
| 2425.0 | 3801.0 | 9.5 | 15.7 |
| 2437.5 | 3801.0 | 20.6 | 29.0 |
| 2450.0 | 3801.0 | 38.1 | 64.1 |
| 2462.5 | 3801.0 | 70.9 | 192.9 |
| 2475.0 | 3801.0 | 181.5 | 165.3 |
| 2487.5 | 3801.0 | 653.2 | 134.1 |
| 2500.0 | 3801.0 | -117.2 | 119.9 |
| 2512.5 | 3801.0 | -118.0 | 99.4 |
| 2525.0 | 3801.0 | -.1 | -24.1 |
| 2537.5 | 3801.0 | 79.3 | -4.6 |
| 2550.0 | 3801.0 | 35.5 | 5.1 |
| 2562.5 | 3801.0 | -19.5 | -6.7 |
| 2575.0 | 3801.0 | -69.7 | -34.6 |
| 2587.5 | 3801.0 | -59.3 | -54.0 |
| 2600.0 | 3801.0 | -60.2 | -58.8 |


| 2612.5 | 3801.0 | -61.5 | -65.4 |
| ---: | ---: | ---: | ---: |
| 2625.0 | 3801.0 | -43.4 | -71.2 |
| 2637.5 | 3801.0 | -102.7 | -70.1 |
| 2650.0 | 3801.0 | -88.4 | -66.7 |
| 2662.5 | 3801.0 | -54.3 | -64.6 |
| 2675.0 | 3801.0 | -44.6 | -48.9 |
| 2687.5 | 3801.0 | -32.9 | -31.3 |
| 2700.0 | 3801.0 | -24.4 | -23.8 |
| 2712.5 | 3801.0 | -.3 | -20.5 |
| 2725.0 | 3801.0 | -17.0 | -18.5 |
| 2737.5 | 3801.0 | -27.7 | -12.6 |
| 2750.0 | 3801.0 | -23.2 | 3.4 |
| 2762.5 | 3801.0 | 5.1 | 1.0 |
| 2775.0 | 3801.0 | 79.8 | 1.1 |
| 2787.5 | 3801.0 | -28.9 | 1.0 |
| 2800.0 | 3801.0 | -27.2 | -3.4 |
| 2812.5 | 3801.0 | -24.0 | -20.1 |
| 2825.0 | 3801.0 | -16.7 | -14.6 |
| 2837.5 | 3801.0 | -3.8 | -13.8 |
| 2850.0 | 3801.0 | -1.2 | -14.6 |
| 2862.5 | 3801.0 | -23.1 | -13.7 |
| 2875.0 | 3801.0 | -28.1 | -15.4 |
| 2887.5 | 3801.0 | -12.4 | -15.5 |
| 2900.0 | 3801.0 | -12.3 | -10.5 |
| 2912.5 | 3801.0 | -1.8 | -3.9 |
| 2925.0 | 3801.0 | 2.0 | -.2 |
| 2937.5 | 3801.0 | 4.8 | 5.0 |
| 2950.0 | 3801.0 | 6.4 | 20.8 |
| 2962.5 | 3801.0 | 13.6 | 38.1 |
| 2975.0 | 3801.0 | 77.3 | 43.6 |
| 2987.5 | 3801.0 | 88.5 | 44.2 |
| 3000.0 | 3801.0 | 32.2 | 43.1 |
| 3012.5 | 3801.0 | 9.5 | 30.4 |
| 3025.0 | 3801.0 | 8.1 | 16.4 |
| 3037.5 | 3801.0 | 13.5 | 13.8 |
| 3050.0 | 3801.0 | 18.5 | 13.4 |
| 3062.5 | 3801.0 | 19.4 | 12.6 |
| 3075.0 | 3801.0 | 7.7 | 10.6 |
| 3087.5 | 3801.0 | 4.1 | 8.0 |
| 3100.0 | 3801.0 | 3.4 | 4.1 |
| 3112.5 | 3801.0 | 5.2 | 1.6 |
| 3125.0 | 3801.0 | -1.0 | -1.3 |
| 3137.5 | 3801.0 | -4.8 | -4.0 |
| 3150.0 | 3801.0 | -10.5 | -13.8 |
| 3162.5 | 3801.0 | -10.2 | -22.5 |
| 3175.0 | 3801.0 | -43.4 | -20.3 |
| 3187.5 | 3801.0 | -43.6 | -15.4 |
| 3200.0 | 3801.0 | 6.4 | -14.1 |
| 3212.5 | 3801.0 | 13.9 | -7.8 |
| 3225.0 | 3801.0 | -3.9 | -5.3 |
| 3237.5 | 3801.0 | -11.8 | -16.6 |
| 3250.0 | 3801.0 | -31.2 | -24.7 |
| 3262.5 | 3801.0 | -50.0 | -24.9 |
|  |  |  |  |


| 3275.0 | 3801.0 | -26.8 | -23.2 |
| ---: | ---: | ---: | ---: |
| 3287.5 | 3801.0 | -4.8 | -16.7 |
| 3300.0 | 3801.0 | -3.4 | -3.1 |
| 3312.5 | 3801.0 | 1.6 | 8.5 |
| 3325.0 | 3801.0 | 18.0 | 18.0 |
| 3337.5 | 3801.0 | 30.9 | 28.8 |
| 3350.0 | 3801.0 | 42.8 | 40.7 |
| 3362.5 | 3801.0 | 50.9 | 50.7 |
| 3375.0 | 3801.0 | 60.7 | 57.8 |
| 3387.5 | 3801.0 | 68.1 | 62.8 |
| 3400.0 | 3801.0 | 66.6 | 59.6 |
| 3412.5 | 3801.0 | 67.8 | 50.0 |
| 3425.0 | 3801.0 | 34.8 | 35.3 |
| 3437.5 | 3801.0 | 12.6 | 18.7 |
| 3450.0 | 3801.0 | -5.1 | 2.3 |
| 3462.5 | 3801.0 | -16.4 | -10.3 |
| 3475.0 | 3801.0 | -14.5 | -18.7 |
| 3487.5 | 3801.0 | -28.3 | -22.1 |
| 3500.0 | 3801.0 | -29.3 | -24.0 |
| 3512.5 | 3802.0 | -37.4 | -35.6 |
| 3525.0 | 3802.0 | -34.9 | -35.8 |
| 3537.5 | 3802.0 | -39.2 | -37.3 |
| 3550.0 | 3802.0 | -36.7 | -34.4 |
| 3562.5 | 3802.0 | -38.1 | -30.1 |
| 3575.0 | 3802.0 | -23.0 | -25.4 |
| 3587.5 | 3802.0 | -13.7 | -19.8 |
| 3600.0 | 3802.0 | -15.4 | -16.0 |
| 3612.5 | 3802.0 | -8.8 | -17.0 |
| 3625.0 | 3802.0 | -19.1 | -19.6 |
| 3637.5 | 3802.0 | -28.0 | -19.5 |
| 3650.0 | 3802.0 | -26.5 | -20.6 |
| 3662.5 | 3802.0 | -14.9 | -19.1 |
| 3675.0 | 3802.0 | -14.5 | -14.5 |
| 3687.5 | 3802.0 | -11.7 | -9.7 |
| 3700.0 | 3802.0 | -4.9 | 45.2 |
| 3712.5 | 3802.0 | -2.7 | 41.2 |
| 3725.0 | 3802.0 | 259.7 | 38.0 |
| 3737.5 | 3802.0 | -34.6 | 37.3 |
| 3750.0 | 3802.0 | -27.6 | 37.5 |
| 3762.5 | 3802.0 | -8.3 | -14.7 |
| 3775.0 | 3802.0 | -1.8 | -8.3 |
| 3787.5 | 3802.0 | -1.2 | -1.5 |
| 3800.0 | 3802.0 | -2.5 | -1.1 |
| 3812.5 | 3802.0 | 6.3 | -1.4 |
| 3825.0 | 3802.0 | -6.4 | -.1 |
| 3837.5 | 3802.0 | -3.0 | 2.9 |
| 3850.0 | 3802.0 | 4.9 | 58.2 |
| 3862.5 | 3802.0 | 12.9 | 83.1 |
| 3875.0 | 3802.0 | 282.5 | 88.3 |
| 3887.5 | 3802.0 | 118.0 | 86.0 |
| 3900.0 | 3802.0 | 23.3 | 83.3 |
| 3912.5 | 3802.0 | -6.7 | 26.4 |
| 3925.0 | 3802.0 | -.4 | 2.2 |
|  |  |  |  |


| 3937.5 | 3802.0 | -2.0 | -3.3 |
| :---: | :---: | :---: | :---: |
| 3950.0 | 3802.0 | -3.1 | -3.1 |
| 3962.5 | 3802.0 | -4.2 | -3.4 |
| 3975.0 | 3802.0 | -5.6 | -3.9 |
| 3987.5 | 3802.0 | -2.2 | -7.4 |
| 4000.0 | 3802.0 | -4.3 | -11.8 |
| 4012.5 | 3802.0 | -20.5 | -18.7 |
| 4025.0 | 3802.0 | -26.5 | -24.8 |
| 4037.5 | 3802.0 | -40.0 | -31.2 |
| 4050.0 | 3802.0 | -32.7 | -37.0 |
| 4062.5 | 3802.0 | -36.4 | -36.9 |
| 4075.0 | 3802.0 | -49.6 | -34.7 |
| 4087.5 | 3802.0 | -25.7 | -31.9 |
| 4100.0 | 3802.0 | -29.1 | -27.1 |
| 4112.5 | 3802.0 | -18.9 | -13.5 |
| 4125.0 | 3802.0 | -12.0 | -3.3 |
| 4137.5 | 3802.0 | 18.0 | 7.5 |
| 4150.0 | 3802.0 | 25.5 | 17.1 |
| 4162.5 | 3802.0 | 24.7 | 24.9 |
| 4175.0 | 3802.0 | 29.2 | 29.1 |
| 4187.5 | 3802.0 | 27.1 | 29.0 |
| 4200.0 | 3802.0 | 38.9 | 27.0 |
| 4212.5 | 3802.0 | 25.3 | 23.5 |
| 4225.0 | 3802.0 | 14.4 | 18.8 |
| 4237.5 | 3802.0 | 12.0 | 15.6 |
| 4250.0 | 3802.0 | 3.6 | 12.1 |
| 4262.5 | 3802.0 | 22.5 | 12.5 |
| 4275.0 | 3802.0 | 8.1 | 14.1 |
| 4287.5 | 3802.0 | 16.1 | 22.9 |
| 4300.0 | 3802.0 | 20.1 | 28.8 |
| 4312.5 | 3802.0 | 47.7 | 35.2 |
| 4325.0 | 3802.0 | 51.8 | 41.8 |
| 4337.5 | 3802.0 | 40.2 | 46.5 |
| 4350.0 | 3802.0 | 49.2 | 43.0 |
| 4362.5 | 3802.0 | 43.6 | 38.4 |
| 4375.0 | 3802.0 | 30.4 | 32.4 |
| 4387.5 | 3802.0 | 28.8 | 26.3 |
| 4400.0 | 3802.0 | 10.0 | 35.6 |
| 4412.5 | 3802.0 | 18.6 | 49.9 |
| 4425.0 | 3802.0 | 90.2 | 56.1 |
| 4437.5 | 3802.0 | 101.9 | 72.7 |
| 4450.0 | 3802.0 | 59.9 | 83.3 |
| 4462.5 | 3802.0 | 93.0 | 81.0 |
| 4475.0 | 3802.0 | 71.3 | 80.6 |
| 4487.5 | 3802.0 | 79.0 | 90.3 |
| 4500.0 | 3802.0 | 99.6 | 85.7 |
| 4512.5 | 3802.0 | 108.8 | 88.7 |
| 4525.0 | 3802.0 | 69.6 | 85.5 |
| 4537.5 | 3802.0 | 86.6 | 73.9 |
| 4550.0 | 3802.0 | 63.1 | 56.3 |
| 4562.5 | 3802.0 | 41.2 | 40.9 |
| 4575.0 | 3802.0 | 21.1 | 23.5 |
| 4587.5 | 3802.0 | -7.7 | 10.1 |


| 4600.0 | 3802.0 | .0 | .4 |
| ---: | ---: | ---: | ---: |
| 4612.5 | 3802.0 | -4.0 | -5.7 |
| 4625.0 | 3802.0 | -7.2 | -5.2 |
| 4637.5 | 3802.0 | -9.8 | -7.7 |
| 4650.0 | 3802.0 | -5.1 | -8.8 |
| 4662.5 | 3802.0 | -12.4 | -2.6 |
| 4675.0 | 3802.0 | -9.7 | .5 |
| 4687.5 | 3802.0 | 24.1 | 4.6 |
| 4700.0 | 3802.0 | 5.7 | 20.6 |
| 4712.5 | 3802.0 | 15.5 | 37.5 |
| 4725.0 | 3802.0 | 67.2 | 42.7 |
| 4737.5 | 3802.0 | 75.1 | 49.6 |
| 4750.0 | 3802.0 | 50.0 | 52.8 |
| 4762.5 | 3802.0 | 40.2 | 52.6 |
| 4775.0 | 3802.0 | 31.4 | 50.4 |
| 4787.5 | 3802.0 | 66.1 | 50.5 |
| 4800.0 | 3802.0 | 64.3 | 53.9 |

### 1.8 Line 3900 N , West of Baseline 2400 E

| 1700.0 | 3900.0 | -37.7 | -37.2 |
| ---: | ---: | ---: | ---: |
| 1712.5 | 3900.0 | -35.9 | -38.7 |
| 1725.0 | 3900.0 | -38.0 | -40.1 |
| 1737.5 | 3900.0 | -43.2 | -42.2 |
| 1750.0 | 3900.0 | -45.9 | -44.5 |
| 1762.5 | 3900.0 | -47.9 | -47.0 |
| 1775.0 | 3900.0 | -47.5 | -47.3 |
| 1787.5 | 3900.0 | -50.7 | -47.7 |
| 1800.0 | 3900.0 | -44.7 | -47.3 |
| 1812.5 | 3900.0 | -47.8 | -45.6 |
| 1825.0 | 3900.0 | -45.7 | -43.4 |
| 1837.5 | 3900.0 | -39.3 | -41.9 |
| 1850.0 | 3900.0 | -39.4 | -37.5 |
| 1862.5 | 3900.0 | -37.3 | -32.9 |
| 1875.0 | 3900.0 | -25.7 | -28.5 |
| 1887.5 | 3900.0 | -22.6 | -22.2 |
| 1900.0 | 3900.0 | -17.6 | -15.2 |
| 1912.5 | 3900.0 | -7.8 | -9.0 |
| 1925.0 | 3900.0 | -2.4 | -1.4 |
| 1937.5 | 3900.0 | 5.4 | 8.3 |
| 1950.0 | 3900.0 | 15.5 | 17.6 |
| 1962.5 | 3900.0 | 31.0 | 28.1 |
| 1975.0 | 3900.0 | 38.5 | 37.8 |
| 1987.5 | 3900.0 | 50.0 | 46.5 |
| 2000.0 | 3900.0 | 54.2 | 53.1 |
| 2012.5 | 3900.0 | 58.6 | 57.5 |
| 2025.0 | 3900.0 | 64.4 | 57.3 |
| 2037.5 | 3900.0 | 60.2 | 54.8 |
| 2050.0 | 3900.0 | 49.2 | 50.7 |
| 2062.5 | 3900.0 | 41.6 | 45.7 |
| 2075.0 | 3900.0 | 37.9 | 41.3 |


| 2087.5 | 3900.0 | 39.7 | 37.8 |
| ---: | ---: | ---: | ---: |
| 2100.0 | 3900.0 | 38.3 | 35.4 |
| 2112.5 | 3900.0 | 31.7 | 33.1 |
| 2125.0 | 3900.0 | 29.3 | 30.0 |
| 2137.5 | 3900.0 | 26.7 | 27.2 |
| 2150.0 | 3900.0 | 23.9 | 25.7 |
| 2162.5 | 3900.0 | 24.6 | 25.5 |
| 2175.0 | 3900.0 | 24.2 | 27.6 |
| 2187.5 | 3900.0 | 28.2 | 32.5 |
| 2200.0 | 3900.0 | 37.3 | 41.8 |
| 2212.5 | 3900.0 | 48.3 | 58.6 |
| 2225.0 | 3900.0 | 70.9 | 105.6 |
| 2237.5 | 3900.0 | 108.4 | 221.5 |
| 2250.0 | 3900.0 | 263.0 | 227.4 |
| 2262.5 | 3900.0 | 617.0 | 222.2 |
| 2275.0 | 3900.0 | 77.5 | 207.0 |
| 2287.5 | 3900.0 | 44.9 | 159.1 |
| 2300.0 | 3900.0 | 32.5 | 38.5 |
| 2312.5 | 3900.0 | 23.8 | 24.6 |
| 2325.0 | 3900.0 | 13.9 | 16.3 |
| 2337.5 | 3900.0 | 7.8 | 10.2 |
| 2350.0 | 3900.0 | 3.7 | 5.5 |
| 2362.5 | 3900.0 | 1.7 | 1.8 |
| 2375.0 | 3900.0 | .3 | -2.3 |
| 2387.5 | 3900.0 | -4.7 | -3.8 |
| 2400.0 | 3900.0 | -12.3 | -5.6 |

### 1.9 Line 3900 N , East of Baseline 2400 E

| 4800.0 | 3902.0 | 49.9 | 56.3 |
| :--- | :--- | :--- | :--- |
| 4787.5 | 3902.0 | 55.4 | 61.3 |
| 4775.0 | 3902.0 | 63.7 | 63.5 |
| 4762.5 | 3902.0 | 76.4 | 68.4 |
| 4750.0 | 3902.0 | 72.1 | 68.7 |
| 4737.5 | 3902.0 | 74.5 | 65.0 |
| 4725.0 | 3902.0 | 56.7 | 62.9 |
| 4712.5 | 3902.0 | 45.3 | 64.5 |
| 4700.0 | 3902.0 | 65.8 | 66.8 |
| 4687.5 | 3902.0 | 80.3 | 72.4 |
| 4675.0 | 3902.0 | 86.1 | 79.4 |
| 4662.5 | 3902.0 | 84.6 | 80.8 |
| 4650.0 | 3902.0 | 80.1 | 79.4 |
| 4637.5 | 3902.0 | 73.1 | 80.4 |
| 4625.0 | 3902.0 | 73.1 | 81.1 |
| 4612.5 | 3902.0 | 91.3 | 81.0 |
| 4600.0 | 3902.0 | 87.8 | 82.1 |
| 4587.5 | 3902.0 | 79.7 | 83.4 |
| 4575.0 | 3902.0 | 78.5 | 81.2 |
| 4562.5 | 3902.0 | 79.7 | 80.7 |
| 4550.0 | 3902.0 | 80.4 | 79.1 |
| 4537.5 | 3902.0 | 85.0 | 78.4 |
| 4525.0 | 3902.0 | 71.9 | 77.2 |


| 4512.5 | 3902.0 | 75.2 | 75.0 |
| ---: | ---: | ---: | ---: |
| 4500.0 | 3902.0 | 73.6 | 71.9 |
| 4487.5 | 3902.0 | 69.2 | 72.1 |
| 4475.0 | 3902.0 | 69.5 | 68.0 |
| 4462.5 | 3902.0 | 73.0 | 62.9 |
| 4450.0 | 3902.0 | 54.5 | 60.7 |
| 4437.5 | 3902.0 | 48.3 | 56.6 |
| 4425.0 | 3902.0 | 58.3 | 50.8 |
| 4412.5 | 3902.0 | 48.8 | 44.2 |
| 4400.0 | 3902.0 | 44.1 | 38.0 |
| 4387.5 | 3902.0 | 21.4 | 33.2 |
| 4375.0 | 3902.0 | 17.4 | 34.1 |
| 4362.5 | 3902.0 | 34.4 | 34.6 |
| 4350.0 | 3902.0 | 53.2 | 40.8 |
| 4337.5 | 3902.0 | 46.8 | 48.3 |
| 4325.0 | 3902.0 | 52.3 | 54.1 |
| 4312.5 | 3902.0 | 54.9 | 54.8 |
| 4300.0 | 3902.0 | 63.1 | 55.6 |
| 4287.5 | 3902.0 | 56.7 | 49.3 |
| 4275.0 | 3902.0 | 50.9 | 44.4 |
| 4262.5 | 3902.0 | 20.8 | 37.9 |
| 4250.0 | 3902.0 | 30.7 | 36.2 |
| 4237.5 | 3902.0 | 30.6 | 35.5 |
| 4225.0 | 3902.0 | 48.2 | 34.2 |
| 4212.5 | 3902.0 | 47.2 | 30.2 |
| 4200.0 | 3902.0 | 14.5 | 22.8 |
| 4187.5 | 3902.0 | 10.3 | 17.2 |
| 4175.0 | 3902.0 | -6.1 | 12.7 |
| 4162.5 | 3902.0 | 20.3 | 9.0 |
| 4150.0 | 3902.0 | 24.7 | 2.6 |
| 4137.5 | 3902.0 | -4.1 | 2.1 |
| 4125.0 | 3902.0 | -21.6 | -2.6 |
| 4112.5 | 3902.0 | -8.9 | -7.1 |
| 4100.0 | 3902.0 | -3.2 | -6.5 |
| 4087.5 | 3902.0 | 2.1 | -3.0 |
| 4075.0 | 3902.0 | -.8 | 3.0 |
| 4062.5 | 3902.0 | -4.1 | 7.7 |
| 4050.0 | 3902.0 | 21.2 | 13.5 |
| 4037.5 | 3902.0 | 20.2 | 13.7 |
| 4025.0 | 3902.0 | 30.9 | 12.0 |
| 4012.5 | 3902.0 | -12.4 | 8.8 |
| 4000.0 | 3902.0 | -1 | 8.8 |
| 3987.5 | 3902.0 | 5.5 | 7.4 |
| 3975.0 | 3902.0 | 16.7 | 12.2 |
| 3962.5 | 3902.0 | 27.4 | 18.8 |
| 3950.0 | 3902.0 | 24.0 | 17.2 |
| 3937.5 | 3902.0 | 20.6 | 18.2 |
| 3925.0 | 3902.0 | -2.7 | 20.4 |
| 3912.5 | 3902.0 | 21.8 | 23.6 |
| 3900.0 | 3902.0 | 38.4 | 26.4 |
| 3887.5 | 3902.0 | 40.0 | 35.8 |
| 3875.0 | 3902.0 | 34.3 | 45.5 |
| 3862.5 | 3902.0 | 44.6 | 59.7 |
|  |  |  |  |


| 3850.0 | 3902.0 | 70.4 | 55.0 |
| ---: | ---: | ---: | ---: |
| 3837.5 | 3902.0 | 109.2 | 49.6 |
| 3825.0 | 3902.0 | 16.7 | 40.3 |
| 3812.5 | 3902.0 | 7.1 | 27.4 |
| 3800.0 | 3902.0 | -2.0 | 6.4 |
| 3787.5 | 3902.0 | 6.0 | 2.2 |
| 3775.0 | 3902.0 | 4.3 | -1.4 |
| 3762.5 | 3902.0 | -4.5 | -4.0 |
| 3750.0 | 3902.0 | -10.8 | -9.1 |
| 3737.5 | 3902.0 | -15.2 | -13.5 |
| 3725.0 | 3902.0 | -19.2 | -9.1 |
| 3712.5 | 3902.0 | -17.6 | 3.6 |
| 3700.0 | 3902.0 | 17.5 | 12.5 |
| 3687.5 | 3902.0 | 52.4 | 22.4 |
| 3675.0 | 3902.0 | 29.2 | 28.1 |
| 3662.5 | 3902.0 | 30.3 | 33.7 |
| 3650.0 | 3902.0 | 11.1 | 27.0 |
| 3637.5 | 3902.0 | 45.4 | 24.0 |
| 3625.0 | 3902.0 | 19.0 | 21.8 |
| 3612.5 | 3902.0 | 14.3 | 24.7 |
| 3600.0 | 3902.0 | 19.3 | 18.8 |
| 3587.5 | 3902.0 | 25.6 | 17.0 |
| 3575.0 | 3902.0 | 15.8 | 17.2 |
| 3562.5 | 3902.0 | 10.1 | 15.9 |
| 3550.0 | 3902.0 | 15.1 | 10.6 |
| 3537.5 | 3902.0 | 12.7 | 8.7 |
| 3525.0 | 3902.0 | -.6 | 8.5 |
| 3512.5 | 3902.0 | 6.0 | 6.8 |
| 3500.0 | 3902.0 | 9.2 | 4.9 |
| 3487.5 | 3901.0 | 8.3 | 4.5 |
| 3475.0 | 3901.0 | 5.4 | 4.7 |
| 3462.5 | 3901.0 | -.6 | 7.5 |
| 3450.0 | 3901.0 | 5.4 | 8.5 |
| 3437.5 | 3901.0 | 18.9 | 10.1 |
| 3425.0 | 3901.0 | 13.6 | 16.0 |
| 3412.5 | 3901.0 | 13.2 | 18.5 |
| 3400.0 | 3901.0 | 28.8 | 12.6 |
| 3387.5 | 3901.0 | 17.8 | 7.9 |
| 3375.0 | 3901.0 | -10.3 | 8.1 |
| 3362.5 | 3901.0 | -10.1 | 4.6 |
| 3350.0 | 3901.0 | 14.2 | 5.6 |
| 3337.5 | 3901.0 | 11.6 | 5.1 |
| 3325.0 | 3901.0 | 22.5 | 2.0 |
| 3312.5 | 3901.0 | -12.9 | -8.4 |
| 3300.0 | 3901.0 | -25.4 | -16.5 |
| 3287.5 | 3901.0 | -37.8 | -25.2 |
| 3275.0 | 3901.0 | -28.7 | -25.1 |
| 3262.5 | 3901.0 | -21.2 | -19.8 |
| 3250.0 | 3901.0 | -12.4 | -6.3 |
| 3237.5 | 3901.0 | 1.1 | 2.6 |
| 3225.0 | 3901.0 | 29.8 | 4.6 |
| 3212.5 | 3901.0 | 15.7 | .3 |
| 3200.0 | 3901.0 | -11.4 | -4.5 |
|  |  |  |  |


| 3187.5 | 3901.0 | -33.6 | -12.6 |
| ---: | ---: | ---: | ---: |
| 3175.0 | 3901.0 | -23.2 | -14.2 |
| 3162.5 | 3901.0 | -10.4 | -13.1 |
| 3150.0 | 3901.0 | 7.6 | -4.6 |
| 3137.5 | 3901.0 | -6.1 | .4 |
| 3125.0 | 3901.0 | 9.0 | 2.8 |
| 3112.5 | 3901.0 | 1.7 | 2.1 |
| 3100.0 | 3901.0 | 2.0 | 1.0 |
| 3087.5 | 3901.0 | 3.8 | -4.4 |
| 3075.0 | 3901.0 | -11.5 | -7.8 |
| 3062.5 | 3901.0 | -17.8 | -9.4 |
| 3050.0 | 3901.0 | -15.4 | -9.6 |
| 3037.5 | 3901.0 | -6.3 | -8.6 |
| 3025.0 | 3901.0 | 2.9 | -5.6 |
| 3012.5 | 3901.0 | -6.4 | -1.0 |
| 3000.0 | 3901.0 | -3.0 | 1.3 |
| 2987.5 | 3901.0 | 7.9 | 4.0 |
| 2975.0 | 3901.0 | 5.1 | 4.5 |
| 2962.5 | 3901.0 | 16.4 | 6.5 |
| 2950.0 | 3901.0 | -4.0 | 6.6 |
| 2937.5 | 3901.0 | 7.1 | 9.2 |
| 2925.0 | 3901.0 | 8.3 | 7.7 |
| 2912.5 | 3901.0 | 18.2 | 8.5 |
| 2900.0 | 3901.0 | 8.8 | 9.2 |
| 2887.5 | 3901.0 | .0 | 9.5 |
| 2875.0 | 3901.0 | 10.5 | 6.2 |
| 2862.5 | 3901.0 | 10.0 | 4.5 |
| 2850.0 | 3901.0 | 1.8 | 4.0 |
| 2837.5 | 3901.0 | .0 | -.5 |
| 2825.0 | 3901.0 | -2.5 | -4.6 |
| 2812.5 | 3901.0 | -12.0 | -5.1 |
| 2800.0 | 3901.0 | -10.5 | -9.1 |
| 2787.5 | 3901.0 | -.6 | -12.3 |
| 2775.0 | 3901.0 | -19.8 | -14.7 |
| 2762.5 | 3901.0 | -18.8 | -17.4 |
| 2750.0 | 3901.0 | -23.7 | -19.0 |
| 2737.5 | 3901.0 | -24.1 | -16.9 |
| 2725.0 | 3901.0 | -8.5 | -12.4 |
| 2712.5 | 3901.0 | -9.3 | -7.3 |
| 2700.0 | 3901.0 | 3.6 | -1.7 |
| 2687.5 | 3901.0 | 1.9 | -1.1 |
| 2675.0 | 3901.0 | 4.0 | -2.1 |
| 2662.5 | 3901.0 | -5.9 | -7.3 |
| 2650.0 | 3901.0 | -14.1 | -13.3 |
| 2637.5 | 3901.0 | -22.6 | -21.0 |
| 2625.0 | 3901.0 | -27.7 | -27.3 |
| 2612.5 | 3901.0 | -34.6 | -32.9 |
| 2600.0 | 3901.0 | -37.5 | -37.1 |
| 2587.5 | 3901.0 | -42.2 | -40.0 |
| 2575.0 | 3901.0 | -43.6 | -42.8 |
| 2562.5 | 3901.0 | -42.3 | -46.1 |
| 2550.0 | 3901.0 | -48.3 | -49.3 |
| 2537.5 | 3901.0 | -53.9 | -53.3 |
|  |  |  |  |


| 2525.0 | 3901.0 | -58.4 | -57.5 |
| :--- | :--- | :--- | :--- |
| 2512.5 | 3901.0 | -63.6 | -59.1 |
| 2500.0 | 3901.0 | -63.1 | -57.5 |
| 2487.5 | 3901.0 | -56.7 | -54.9 |
| 2475.0 | 3901.0 | -45.9 | -49.7 |
| 2462.5 | 3901.0 | -45.4 | -46.8 |
| 2450.0 | 3901.0 | -37.6 | -45.7 |
| 2437.5 | 3901.0 | -48.4 | -44.2 |
| 2425.0 | 3901.0 | -51.3 | -38.0 |
| 2412.5 | 3901.0 | -38.3 | -38.1 |
| 2400.0 | 3901.0 | -14.4 | -34.7 |

1.10

Line

## 4000 N

4000.0 West of Baseline 2400E

| 2387.5 | 4000.0 | -53.4 | -73.8 |
| ---: | ---: | ---: | ---: |
| 2375.0 | 4000.0 | -76.5 | -38.7 |
| 2362.5 | 4000.0 | -126.7 | -39.6 |
| 2350.0 | 4000.0 | 102.1 | -35.1 |
| 2337.5 | 4000.0 | -43.5 | -19.6 |
| 2325.0 | 4000.0 | -30.7 | 17.7 |
| 2312.5 | 4000.0 | 1.0 | 31.8 |
| 2300.0 | 4000.0 | 59.4 | 141.2 |
| 2287.5 | 4000.0 | 172.9 | 203.9 |
| 2275.0 | 4000.0 | 503.4 | 226.0 |
| 2262.5 | 4000.0 | 282.6 | 229.7 |
| 2250.0 | 4000.0 | 111.6 | 266.1 |
| 2237.5 | 4000.0 | 77.8 | 192.8 |
| 2225.0 | 4000.0 | 355.3 | 158.5 |
| 2212.5 | 4000.0 | 136.8 | 151.7 |
| 2200.0 | 4000.0 | 111.1 | 147.0 |
| 2187.5 | 4000.0 | 77.3 | 83.4 |
| 2175.0 | 4000.0 | 54.6 | 62.3 |
| 2162.5 | 4000.0 | 37.2 | 45.9 |
| 2150.0 | 4000.0 | 31.4 | 35.8 |
| 2137.5 | 4000.0 | 28.9 | 30.4 |
| 2125.0 | 4000.0 | 27.0 | 28.6 |
| 2112.5 | 4000.0 | 27.7 | 29.2 |
| 2100.0 | 4000.0 | 28.2 | 30.9 |
| 2087.5 | 4000.0 | 34.4 | 35.2 |
| 2075.0 | 4000.0 | 37.0 | 43.1 |
| 2062.5 | 4000.0 | 48.5 | 52.6 |
| 2050.0 | 4000.0 | 67.4 | 60.6 |
| 2037.5 | 4000.0 | 75.6 | 67.0 |
| 2025.0 | 4000.0 | 74.4 | 69.2 |
| 2012.5 | 4000.0 | 69.0 | 64.2 |
| 2000.0 | 4000.0 | 59.7 | 54.2 |
| 1987.5 | 4000.0 | 42.3 | 41.9 |
| 1975.0 | 4000.0 | 25.5 | 29.0 |
| 1962.5 | 4000.0 | 12.8 | 14.8 |
| 1950.0 | 4000.0 | 4.5 | 3.2 |
| 1937.5 | 4000.0 | -11.0 | -7.3 |
| 1925.0 | 4000.0 | -15.9 | -15.7 |
|  |  |  |  |


| 1912.5 | 4000.0 | -26.7 | -22.1 |
| ---: | ---: | ---: | ---: |
| 1900.0 | 4000.0 | -29.6 | -25.9 |
| 1887.5 | 4000.0 | -27.5 | -29.3 |
| 1875.0 | 4000.0 | -30.0 | -30.4 |
| 1862.5 | 4000.0 | -32.7 | -32.0 |
| 1850.0 | 4000.0 | -32.0 | -34.8 |
| 1837.5 | 4000.0 | -38.0 | -35.9 |
| 1825.0 | 4000.0 | -41.4 | -36.4 |
| 1812.5 | 4000.0 | -35.4 | -35.8 |
| 1800.0 | 4000.0 | -35.1 | -32.0 |
| 1787.5 | 4000.0 | -29.1 | -27.0 |
| 1775.0 | 4000.0 | -19.2 | -21.7 |
| 1762.5 | 4000.0 | -16.1 | -15.1 |
| 1750.0 | 4000.0 | -9.2 | -9.5 |
| 1737.5 | 4000.0 | -2.1 | -6.0 |
| 1725.0 | 4000.0 | -.8 | -3.1 |
| 1712.5 | 4000.0 | -1.6 | -1.5 |
| 1700.0 | 4000.0 | -1.6 | -1.3 |

1.11 Line 4000 N , East of Baseline 2400 E

| 2400.0 | 4001.0 | -51.1 | -30.7 |
| ---: | ---: | ---: | ---: |
| 2412.5 | 4001.0 | -30.4 | -16.9 |
| 2425.0 | 4001.0 | -10.6 | 9.6 |
| 2437.5 | 4001.0 | 24.4 | 46.3 |
| 2450.0 | 4001.0 | 115.5 | 80.6 |
| 2462.5 | 4001.0 | 132.6 | 82.0 |
| 2475.0 | 4001.0 | 141.3 | 89.7 |
| 2487.5 | 4001.0 | -3.7 | 63.6 |
| 2500.0 | 4001.0 | 63.0 | 25.9 |
| 2512.5 | 4001.0 | -15.0 | -12.3 |
| 2525.0 | 4001.0 | -55.9 | -21.0 |
| 2537.5 | 4001.0 | -50.1 | -41.6 |
| 2550.0 | 4001.0 | -46.9 | -45.3 |
| 2562.5 | 4001.0 | -40.3 | -40.0 |
| 2575.0 | 4001.0 | -33.5 | -33.4 |
| 2587.5 | 4001.0 | -29.1 | -26.4 |
| 2600.0 | 4001.0 | -17.2 | -17.5 |
| 2612.5 | 4001.0 | -12.0 | -8.7 |
| 2625.0 | 4001.0 | 4.2 | -2.8 |
| 2637.5 | 4001.0 | 10.8 | -2.8 |
| 2650.0 | 4001.0 | -1.4 | -4.3 |
| 2662.5 | 4001.0 | -17.3 | -11.1 |
| 2675.0 | 4001.0 | -19.7 | -17.4 |
| 2687.5 | 4001.0 | -29.9 | -18.4 |
| 2700.0 | 4001.0 | -20.4 | -17.5 |
| 2712.5 | 4001.0 | -4.8 | -14.5 |
| 2725.0 | 4001.0 | -12.6 | -7.7 |
| 2737.5 | 4001.0 | -4.8 | -2.9 |
| 2750.0 | 4001.0 | 4.3 | -.6 |
| 2762.5 | 4001.0 | 3.5 | 4.1 |
| 2775.0 | 4001.0 | 6.8 | 4.7 |


| 2787.5 | 4001.0 | 10.5 | 1.1 |
| ---: | ---: | ---: | ---: |
| 2800.0 | 4001.0 | -1.5 | -.9 |
| 2812.5 | 4001.0 | -14.0 | -2.7 |
| 2825.0 | 4001.0 | -6.5 | -6.4 |
| 2837.5 | 4001.0 | -1.9 | -6.2 |
| 2850.0 | 4001.0 | -8.1 | -1.7 |
| 2862.5 | 4001.0 | -.5 | 1.3 |
| 2875.0 | 4001.0 | 8.3 | 4.3 |
| 2887.5 | 4001.0 | 8.7 | 8.9 |
| 2900.0 | 4001.0 | 13.3 | 14.4 |
| 2912.5 | 4001.0 | 14.9 | 21.1 |
| 2925.0 | 4001.0 | 26.9 | 30.1 |
| 2937.5 | 4001.0 | 41.8 | 38.9 |
| 2950.0 | 4001.0 | 53.6 | 43.0 |
| 2962.5 | 4001.0 | 57.4 | 37.5 |
| 2975.0 | 4001.0 | 35.4 | 28.4 |
| 2987.5 | 4001.0 | -.9 | 18.1 |
| 3000.0 | 4001.0 | -3.5 | 5.3 |
| 3012.5 | 4001.0 | 2.2 | -4.4 |
| 3025.0 | 4001.0 | -6.8 | -6.3 |
| 3037.5 | 4001.0 | -13.2 | -6.2 |
| 3050.0 | 4001.0 | -10.0 | -6.2 |
| 3062.5 | 4001.0 | -3.1 | -5.4 |
| 3075.0 | 4001.0 | 2.1 | -3.6 |
| 3087.5 | 4001.0 | -2.9 | -4.8 |
| 3100.0 | 4001.0 | -4.2 | -3.4 |
| 3112.5 | 4001.0 | -15.9 | -2.5 |
| 3125.0 | 4001.0 | 3.8 | .7 |
| 3137.5 | 4001.0 | 6.7 | 6.4 |
| 3150.0 | 4001.0 | 13.0 | 10.8 |
| 3162.5 | 4001.0 | 24.5 | 9.0 |
| 3175.0 | 4001.0 | 5.9 | 8.6 |
| 3187.5 | 4001.0 | -5.1 | 9.0 |
| 3200.0 | 4001.0 | 4.8 | 8.8 |
| 3212.5 | 4001.0 | 15.0 | 10.1 |
| 3225.0 | 4001.0 | 23.6 | 10.4 |
| 3237.5 | 4001.0 | 12.2 | 9.8 |
| 3250.0 | 4001.0 | -3.4 | 8.7 |
| 3262.5 | 4001.0 | 1.6 | 7.3 |
| 3275.0 | 4001.0 | 9.6 | 9.0 |
| 3287.5 | 4001.0 | 16.4 | 15.0 |
| 3300.0 | 4001.0 | 20.7 | 21.5 |
| 3312.5 | 4001.0 | 26.6 | 22.9 |
| 3325.0 | 4001.0 | 34.1 | 23.3 |
| 3337.5 | 4001.0 | 16.8 | 21.8 |
| 3350.0 | 4001.0 | 18.3 | 19.5 |
| 3362.5 | 4001.0 | 13.2 | 12.1 |
| 3375.0 | 4001.0 | 15.2 | 5.8 |
| 3387.5 | 4001.0 | -2.8 | -1.9 |
| 3400.0 | 4001.0 | -15.0 | -11.5 |
| 3412.5 | 4001.0 | -20.1 | -23.4 |
| 3425.0 | 4001.0 | -34.7 | -31.2 |
| 3437.5 | 4001.0 | -44.4 | -37.8 |
|  |  |  |  |


| 3450.0 | 4001.0 | -41.7 | -43.7 |
| ---: | ---: | ---: | ---: |
| 3462.5 | 4001.0 | -48.2 | -46.7 |
| 3475.0 | 4001.0 | -49.3 | -42.7 |
| 3487.5 | 4001.0 | -50.1 | -42.9 |
| 3500.0 | 4001.0 | -24.1 | -41.2 |
| 3512.5 | 4002.0 | -2.2 | -5.3 |
| 3525.0 | 4002.0 | -9.6 | -2.0 |
| 3537.5 | 4002.0 | 6.3 | 3.7 |
| 3550.0 | 4002.0 | 10.9 | 8.7 |
| 3562.5 | 4002.0 | 13.3 | 16.8 |
| 3575.0 | 4002.0 | 22.4 | 24.3 |
| 3587.5 | 4002.0 | 31.2 | 30.5 |
| 3600.0 | 4002.0 | 43.6 | 38.6 |
| 3612.5 | 4002.0 | 42.2 | 39.2 |
| 3625.0 | 4002.0 | 53.8 | 35.5 |
| 3637.5 | 4002.0 | 25.2 | 28.1 |
| 3650.0 | 4002.0 | 12.9 | 17.7 |
| 3662.5 | 4002.0 | 6.5 | -1.6 |
| 3675.0 | 4002.0 | -9.9 | -11.0 |
| 3687.5 | 4002.0 | -42.8 | -17.6 |
| 3700.0 | 4002.0 | -21.5 | -18.9 |
| 3712.5 | 4002.0 | -20.3 | -9.2 |
| 3725.0 | 4002.0 | .2 | 15.9 |
| 3737.5 | 4002.0 | 38.2 | 37.4 |
| 3750.0 | 4002.0 | 82.7 | 66.8 |
| 3762.5 | 4002.0 | 86.2 | 96.9 |
| 3775.0 | 4002.0 | 126.9 | 105.6 |
| 3787.5 | 4002.0 | 150.5 | 99.0 |
| 3800.0 | 4002.0 | 81.9 | 80.0 |
| 3812.5 | 4002.0 | 49.7 | 60.1 |
| 3825.0 | 4002.0 | -9.0 | 37.1 |
| 3837.5 | 4002.0 | 27.4 | 28.2 |
| 3850.0 | 4002.0 | 35.6 | 20.0 |
| 3862.5 | 4002.0 | 37.4 | 24.1 |
| 3875.0 | 4002.0 | 8.6 | 22.4 |
| 3887.5 | 4002.0 | 11.3 | 15.5 |
| 3900.0 | 4002.0 | 19.3 | 9.5 |
| 3912.5 | 4002.0 | .7 | 8.5 |
| 3925.0 | 4002.0 | 7.4 | 3.2 |
| 3937.5 | 4002.0 | 4.0 | -1.3 |
| 3950.0 | 4002.0 | -15.3 | -1.5 |
| 3962.5 | 4002.0 | -3.5 | -4.2 |
| 3975.0 | 4002.0 | -.2 | -4.0 |
| 3987.5 | 4002.0 | -6.0 | 1.6 |
| 4000.0 | 4002.0 | 4.8 | 4.4 |
| 4012.5 | 4002.0 | 13.1 | 1.7 |
| 4025.0 | 4002.0 | 10.2 | .9 |
| 4037.5 | 4002.0 | -13.7 | -4.5 |
| 4050.0 | 4002.0 | -11.0 | -13.0 |
| 4062.5 | 4002.0 | -21.1 | -12.1 |
| 4075.0 | 4002.0 | -29.4 | -2.8 |
| 4087.5 | 4002.0 | 14.9 | 4.9 |
| 4100.0 | 4002.0 | 32.6 | 11.6 |


| 4112.5 | 4002.0 | 27.6 | 20.0 |
| :--- | :--- | :--- | :--- |
| 4125.0 | 4002.0 | 12.4 | 21.5 |
| 4137.5 | 4002.0 | 12.5 | 19.1 |
| 4150.0 | 4002.0 | 22.2 | 17.0 |
| 4162.5 | 4002.0 | 21.0 | 22.5 |
| 4175.0 | 4002.0 | 16.8 | 31.8 |
| 4187.5 | 4002.0 | 40.0 | 36.2 |
| 4200.0 | 4002.0 | 59.2 | 38.5 |
| 4212.5 | 4002.0 | 44.1 | 41.1 |
| 4225.0 | 4002.0 | 32.4 | 39.1 |
| 4237.5 | 4002.0 | 29.6 | 35.7 |
| 4250.0 | 4002.0 | 30.2 | 34.9 |
| 4262.5 | 4002.0 | 42.1 | 29.7 |
| 4275.0 | 4002.0 | 40.4 | 37.3 |
| 4287.5 | 4002.0 | 6.1 | 40.4 |
| 4300.0 | 4002.0 | 67.7 | 33.3 |
| 4312.5 | 4002.0 | 45.7 | 30.2 |
| 4325.0 | 4002.0 | 6.6 | 33.3 |
| 4337.5 | 4002.0 | 24.9 | 25.0 |
| 4350.0 | 4002.0 | 21.8 | 19.6 |
| 4362.5 | 4002.0 | 26.0 | 21.4 |
| 4375.0 | 4002.0 | 18.8 | 22.6 |
| 4387.5 | 4002.0 | 15.5 | 27.8 |
| 4400.0 | 4002.0 | 31.0 | 34.4 |
| 4412.5 | 4002.0 | 47.5 | 35.4 |
| 4425.0 | 4002.0 | 59.1 | 39.2 |
| 4437.5 | 4002.0 | 23.8 | 41.7 |
| 4450.0 | 4002.0 | 34.7 | 40.8 |
| 4462.5 | 4002.0 | 43.2 | 40.2 |
| 4475.0 | 4002.0 | 43.0 | 47.4 |
| 4487.5 | 4002.0 | 56.2 | 52.0 |
| 4500.0 | 4002.0 | 60.1 | 54.3 |
| 4512.5 | 4002.0 | 57.4 | 55.1 |
| 4525.0 | 4002.0 | 54.8 | 53.9 |
| 4537.5 | 4002.0 | 47.1 | 51.9 |
| 4550.0 | 4002.0 | 50.1 | 52.3 |
| 4562.5 | 4002.0 | 50.0 | 53.3 |
| 4575.0 | 4002.0 | 59.4 | 51.9 |
| 4587.5 | 4002.0 | 59.8 | 48.2 |
| 4600.0 | 4002.0 | 40.4 | 48.5 |
| 4612.5 | 4002.0 | 31.2 | 49.3 |
| 4625.0 | 4002.0 | 51.6 | 49.8 |
| 4637.5 | 4002.0 | 63.4 | 52.3 |
| 4650.0 | 4002.0 | 62.5 | 57.7 |
| 4662.5 | 4002.0 | 53.0 | 59.2 |
| 4675.0 | 4002.0 | 58.2 .0 | 58.6 |
| 4687.5 | 4002.0 | 59.0 | 56.1 |
| 4700.0 | 4002.0 | 60.3 | 56.0 |
| 4712.5 | 4002.0 | 49.8 | 53.0 |
| 4725.0 | 4002.0 | 52.6 | 49.2 |
| 4737.5 | 4002.0 | 43.3 | 48.7 |
| 4750.0 | 4002.0 | 40.0 | 52.6 |
| 4762.5 | 4002.0 | 57.8 | 56.5 |
| 4 |  |  |  |


| 4775.0 | 4002.0 | 69.4 | 61.0 |
| :--- | :--- | :--- | :--- |
| 4787.5 | 4002.0 | 72.0 | 66.3 |
| 4800.0 | 4002.0 | 66.0 | 69.1 |

### 1.12 Line 4025 N

$4800.0 \quad 4012.0$
4787.5
4775.0
4012.0
4762.5
4750.0
4737.5
4725.0
4712.5
4700.0
4687.5
4012.0
. 8
71.1
68.1
68.7
68.3
66.4
61.6
61.2
57.3
57.6
$50.8 \quad 56.6$
$50.1 \quad 55.1$
$63.2 \quad 53.7$
$53.9 \quad 48.9$
$50.7 \quad 50.4$
$26.8 \quad 50.4$
57.249 .9
4662.54012 .0
$4650.0 \quad 4012.0$
4637.54012 .0
$4625.0 \quad 4012.0$
4612.54012 .0
$4600.0 \quad 4012.0$
4587.5
4012.0
4575.0
4562.5
4550.0
4537.5
4525.0
4512.5
4500.0
4487.5
4012.0
4012.0
4012.0
4012.0
4012.0
4012.0
4012.0
4012.0
$4475.0 \quad 4012.0$
4462.54012 .0
$4450.0 \quad 4012.0$
4437.54012 .0
$4425.0 \quad 4012.0$
4412.54012 .0
4400.04012 .0
$63.3 \quad 50.5$
$51.7 \quad 57.4$
$53.5 \quad 56.4$
$61.3 \quad 57.5$
$52.2 \quad 56.3$
$68.6 \quad 53.3$
$45.9 \quad 53.8$
$38.4 \quad 57.4$
$64.0 \quad 58.3$
$69.9 \quad 61.7$
$73.1 \quad 63.2$
$63.3 \quad 56.1$
$45.9 \quad 47.6$
$28.2 \quad 38.2$
$27.4 \quad 35.2$
$26.0 \quad 36.7$
$48.7 \quad 38.5$
$53.0 \quad 37.9$
$37.3 \quad 36.1$
$24.7 \quad 33.0$
$17.0 \quad 26.3$
1.13 Line 4075 N

| 4400.0 | 4112.0 | 28.8 | 37.8 |
| :--- | :--- | :--- | :--- |
| 4412.5 | 4112.0 | 39.8 | 40.4 |
| 4425.0 | 4112.0 | 44.7 | 41.7 |
| 4437.5 | 4112.0 | 48.4 | 45.4 |
| 4450.0 | 4112.0 | 46.8 | 48.7 |
| 4462.5 | 4112.0 | 47.3 | 50.5 |
| 4475.0 | 4112.0 | 56.4 | 53.4 |
| 4487.5 | 4112.0 | 53.4 | 54.1 |


| 4500.0 | 4112.0 | 63.3 | 54.5 |
| :--- | :--- | :--- | :--- |
| 4512.5 | 4112.0 | 50.3 | 52.0 |
| 4525.0 | 4112.0 | 48.9 | 50.9 |
| 4537.5 | 4112.0 | 43.9 | 48.2 |
| 4550.0 | 4112.0 | 48.3 | 49.2 |
| 4562.5 | 4112.0 | 49.8 | 50.4 |
| 4575.0 | 4112.0 | 55.3 | 51.4 |
| 4587.5 | 4112.0 | 54.5 | 49.3 |
| 4600.0 | 4112.0 | 48.9 | 47.3 |
| 4612.5 | 4112.0 | 38.2 | 43.8 |
| 4625.0 | 4112.0 | 39.8 | 43.7 |
| 4637.5 | 4112.0 | 37.5 | 44.2 |
| 4650.0 | 4112.0 | 54.3 | 45.2 |
| 4662.5 | 4112.0 | 51.2 | 46.9 |
| 4675.0 | 4112.0 | 43.2 | 50.3 |
| 4687.5 | 4112.0 | 48.5 | 48.7 |
| 4700.0 | 4112.0 | 54.4 | 47.0 |
| 4712.5 | 4112.0 | 46.2 | 47.0 |
| 4725.0 | 4112.0 | 42.8 | 48.8 |
| 4737.5 | 4112.0 | 43.0 | 52.3 |
| 4750.0 | 4112.0 | 57.6 | 56.2 |
| 4762.5 | 4112.0 | 72.1 | 60.3 |
| 4775.0 | 4112.0 | 65.7 | 61.6 |
| 4787.5 | 4112.0 | 63.1 | 62.5 |
| 4800.0 | 4112.0 | 49.3 | 59.4 |

1.14 Line 4100 N , West of Baseline 2400 E

| 1700.0 | 4100.0 | -8.2 | -10.6 |
| ---: | ---: | ---: | ---: |
| 1712.5 | 4100.0 | -11.1 | -11.7 |
| 1725.0 | 4100.0 | -12.5 | -12.9 |
| 1737.5 | 4100.0 | -15.0 | -14.9 |
| 1750.0 | 4100.0 | -17.8 | -16.4 |
| 1762.5 | 4100.0 | -18.1 | -18.0 |
| 1775.0 | 4100.0 | -18.4 | -19.4 |
| 1787.5 | 4100.0 | -20.7 | -20.9 |
| 1800.0 | 4100.0 | -21.8 | -20.9 |
| 1812.5 | 4100.0 | -25.6 | -20.9 |
| 1825.0 | 4100.0 | -18.2 | -19.5 |
| 1837.5 | 4100.0 | -18.3 | -16.5 |
| 1850.0 | 4100.0 | -13.4 | -12.0 |
| 1862.5 | 4100.0 | -7.0 | -6.5 |
| 1875.0 | 4100.0 | -3.0 | 3.7 |
| 1887.5 | 4100.0 | 9.1 | 13.8 |
| 1900.0 | 4100.0 | 32.7 | 23.2 |
| 1912.5 | 4100.0 | 37.3 | 33.0 |
| 1925.0 | 4100.0 | 39.9 | 38.7 |
| 1937.5 | 4100.0 | 45.8 | 37.4 |
| 1950.0 | 4100.0 | 37.7 | 33.4 |
| 1962.5 | 4100.0 | 26.2 | 31.9 |
| 1975.0 | 4100.0 | 17.6 | 29.8 |
| 1987.5 | 4100.0 | 32.0 | 26.5 |


| 2000.0 | 4100.0 | 35.5 | 22.2 |
| ---: | ---: | ---: | ---: |
| 2012.5 | 4100.0 | 21.4 | 19.4 |
| 2025.0 | 4100.0 | 4.5 | 14.3 |
| 2037.5 | 4100.0 | 3.5 | 10.0 |
| 2050.0 | 4100.0 | 6.8 | 10.6 |
| 2062.5 | 4100.0 | 13.6 | 15.2 |
| 2075.0 | 4100.0 | 24.4 | 22.7 |
| 2087.5 | 4100.0 | 27.9 | 31.3 |
| 2100.0 | 4100.0 | 40.8 | 39.2 |
| 2112.5 | 4100.0 | 49.6 | 50.1 |
| 2125.0 | 4100.0 | 53.3 | 67.6 |
| 2137.5 | 4100.0 | 79.1 | 88.1 |
| 2150.0 | 4100.0 | 115.0 | 94.8 |
| 2162.5 | 4100.0 | 143.3 | 87.8 |
| 2175.0 | 4100.0 | 83.4 | 75.3 |
| 2187.5 | 4100.0 | 18.2 | 74.7 |
| 2200.0 | 4100.0 | 16.4 | 93.8 |
| 2212.5 | 4100.0 | 112.2 | 89.9 |
| 2225.0 | 4100.0 | 238.9 | 78.0 |
| 2237.5 | 4100.0 | 63.7 | 61.0 |
| 2250.0 | 4100.0 | -41.1 | 23.6 |
| 2262.5 | 4100.0 | -68.8 | -38.2 |
| 2275.0 | 4100.0 | -74.6 | -64.2 |
| 2287.5 | 4100.0 | -70.0 | -51.1 |
| 2300.0 | 4100.0 | -66.6 | -50.9 |
| 2312.5 | 4100.0 | 24.7 | -49.8 |
| 2325.0 | 4100.0 | -68.1 | -47.6 |
| 2337.5 | 4100.0 | -69.2 | -43.0 |
| 2350.0 | 4100.0 | -58.7 | -53.7 |
| 2362.5 | 4100.0 | -43.7 | -40.3 |
| 2375.0 | 4100.0 | -29.0 | -17.8 |
| 2387.5 | 4100.0 | -.9 | -7.5 |

1.15 Line 4100 N , East of Baseline 2400 E

| 4800.0 | 4102.0 | 59.9 | 63.4 |
| :--- | :--- | ---: | ---: |
| 4787.5 | 4102.0 | 72.3 | 61.1 |
| 4775.0 | 4102.0 | 58.0 | 58.4 |
| 4762.5 | 4102.0 | 54.2 | 52.3 |
| 4750.0 | 4102.0 | 47.8 | 43.3 |
| 4737.5 | 4102.0 | 29.1 | 33.1 |
| 4725.0 | 4102.0 | 27.3 | 21.7 |
| 4712.5 | 4102.0 | 7.0 | 19.6 |
| 4700.0 | 4102.0 | -2.5 | 22.0 |
| 4687.5 | 4102.0 | 37.1 | 22.8 |
| 4675.0 | 4102.0 | 41.1 | 23.9 |
| 4662.5 | 4102.0 | 31.2 | 26.5 |
| 4650.0 | 4102.0 | 12.4 | 23.7 |
| 4637.5 | 4102.0 | 10.9 | 23.8 |
| 4625.0 | 4102.0 | 22.9 | 23.8 |
| 4612.5 | 4102.0 | 41.6 | 29.5 |
| 4600.0 | 4102.0 | 31.1 | 34.7 |


| 4587.5 | 4102.0 | 40.9 | 38.4 |
| ---: | ---: | ---: | ---: |
| 4575.0 | 4102.0 | 37.1 | 38.3 |
| 4562.5 | 4102.0 | 41.1 | 43.0 |
| 4550.0 | 4102.0 | 41.4 | 44.1 |
| 4537.5 | 4102.0 | 54.6 | 47.8 |
| 4525.0 | 4102.0 | 46.3 | 49.2 |
| 4512.5 | 4102.0 | 55.5 | 52.2 |
| 4500.0 | 4102.0 | 48.4 | 51.1 |
| 4487.5 | 4102.0 | 56.3 | 53.0 |
| 4475.0 | 4102.0 | 49.1 | 54.9 |
| 4462.5 | 4102.0 | 55.5 | 55.2 |
| 4450.0 | 4102.0 | 65.4 | 55.2 |
| 4437.5 | 4102.0 | 49.9 | 58.1 |
| 4425.0 | 4102.0 | 56.0 | 56.3 |
| 4412.5 | 4102.0 | 63.8 | 51.4 |
| 4400.0 | 4102.0 | 46.6 | 48.5 |
| 4387.5 | 4102.0 | 40.9 | 47.8 |
| 4375.0 | 4102.0 | 35.2 | 43.2 |
| 4362.5 | 4102.0 | 52.4 | 41.3 |
| 4350.0 | 4102.0 | 40.9 | 39.1 |
| 4337.5 | 4102.0 | 37.2 | 37.7 |
| 4325.0 | 4102.0 | 30.0 | 31.7 |
| 4312.5 | 4102.0 | 27.9 | 29.6 |
| 4300.0 | 4102.0 | 22.4 | 25.9 |
| 4287.5 | 4102.0 | 30.3 | 24.6 |
| 4275.0 | 4102.0 | 18.8 | 23.6 |
| 4262.5 | 4102.0 | 23.8 | 21.5 |
| 4250.0 | 4102.0 | 22.8 | 17.5 |
| 4237.5 | 4102.0 | 11.8 | 18.1 |
| 4225.0 | 4102.0 | 10.2 | 18.7 |
| 4212.5 | 4102.0 | 21.8 | 18.5 |
| 4200.0 | 4102.0 | 27.0 | 20.6 |
| 4187.5 | 4102.0 | 21.9 | 25.6 |
| 4175.0 | 4102.0 | 22.1 | 28.1 |
| 4162.5 | 4102.0 | 35.1 | 29.2 |
| 4150.0 | 4102.0 | 34.2 | 30.6 |
| 4137.5 | 4102.0 | 32.5 | 32.1 |
| 4125.0 | 4102.0 | 29.1 | 27.7 |
| 4112.5 | 4102.0 | 29.8 | 25.8 |
| 4100.0 | 4102.0 | 12.8 | 24.9 |
| 4087.5 | 4102.0 | 24.8 | 21.1 |
| 4075.0 | 4102.0 | 28.2 | 16.1 |
| 4062.5 | 4102.0 | 10.0 | 13.5 |
| 4050.0 | 4102.0 | 4.8 | 8.0 |
| 4037.5 | 4102.0 | -.4 | 2.0 |
| 4025.0 | 4102.0 | -.1 | 3.0 |
| 4012.5 | 4102.0 | -4.1 | 8.0 |
| 4000.0 | 4102.0 | 14.9 | 15.9 |
| 3987.5 | 4102.0 | 33.3 | 17.6 |
| 3975.0 | 4102.0 | 31.6 | 15.6 |
| 3962.5 | 4102.0 | 12.5 | 13.4 |
| 3950.0 | 4102.0 | -14.2 | 9.3 |
| 3937.5 | 4102.0 | 3.6 | 7.4 |
|  |  |  |  |


| 3925.0 | 4102.0 | 12.9 | 11.2 |
| :---: | :---: | :---: | :---: |
| 3912.5 | 4102.0 | 22.4 | 18.2 |
| 3900.0 | 4102.0 | 31.2 | 23.2 |
| 3887.5 | 4102.0 | 20.7 | 27.5 |
| 3875.0 | 4102.0 | 28.9 | 28.9 |
| 3862.5 | 4102.0 | 34.5 | 25.0 |
| 3850.0 | 4102.0 | 29.0 | 22.5 |
| 3837.5 | 4102.0 | 12.0 | 15.8 |
| 3825.0 | 4102.0 | 8.0 | 8.9 |
| 3812.5 | 4102.0 | -4.6 | -2.0 |
| 3800.0 | 4102.0 | . 2 | -10.8 |
| 3787.5 | 4102.0 | -25.8 | -17.2 |
| 3775.0 | 4102.0 | -31.6 | -20.5 |
| 3762.5 | 4102.0 | -24.2 | -22.6 |
| 3750.0 | 4102.0 | -20.9 | -16.0 |
| 3737.5 | 4102.0 | -10.3 | -6.3 |
| 3725.0 | 4102.0 | 7.2 | -. 5 |
| 3712.5 | 4102.0 | 16.6 | 2.6 |
| 3700.0 | 4102.0 | 4.8 | 1.4 |
| 3687.5 | 4102.0 | -5.1 | -4.8 |
| 3675.0 | 4102.0 | -16.6 | -12.5 |
| 3662.5 | 4102.0 | -23.8 | -17.2 |
| 3650.0 | 4102.0 | -21.8 | -20.9 |
| 3637.5 | 4102.0 | -18.5 | -23.6 |
| 3625.0 | 4102.0 | -23.6 | 1.0 |
| 3612.5 | 4102.0 | -30.1 | 22.7 |
| 3600.0 | 4102.0 | 99.0 | 22.5 |
| 3587.5 | 4102.0 | 86.6 | 23.2 |
| 3575.0 | 4102.0 | -19.6 | 26.7 |
| 3562.5 | 4102.0 | -19.9 | 2.2 |
| 3550.0 | 4102.0 | -12.7 | -20.6 |
| 3537.5 | 4102.0 | -23.4 | -21.9 |
| 3525.0 | 4102.0 | -27.2 | -25.8 |
| 3512.5 | 4102.0 | -26.1 | -29.0 |
| 3500.0 | 4102.0 | -39.4 | -30.9 |
| 3487.5 | 4101.0 | -35.6 | -34.7 |
| 3475.0 | 4101.0 | -35.4 | -30.3 |
| 3462.5 | 4101.0 | -27.2 | -19.9 |
| 3450.0 | 4101.0 | -12.5 | -12.7 |
| 3437.5 | 4101.0 | 11.3 | -3.4 |
| 3425.0 | 4101.0 | . 4 | 3.4 |
| 3412.5 | 4101.0 | 11.2 | 7.9 |
| 3400.0 | 4101.0 | 6.8 | 8.6 |
| 3387.5 | 4101.0 | 9.9 | 12.6 |
| 3375.0 | 4101.0 | 14.8 | 16.0 |
| 3362.5 | 4101.0 | 20.1 | 19.5 |
| 3350.0 | 4101.0 | 28.5 | 22.4 |
| 3337.5 | 4101.0 | 24.3 | 27.0 |
| 3325.0 | 4101.0 | 24.4 | 22.3 |
| 3312.5 | 4101.0 | 37.6 | 14.7 |
| 3300.0 | 4101.0 | -3.1 | 6.0 |
| 3287.5 | 4101.0 | -9.9 | . 6 |
| 3275.0 | 4101.0 | -19.2 | -7.9 |


| 3262.5 | 4101.0 | -2.6 | -11.9 |
| ---: | ---: | ---: | ---: |
| 3250.0 | 4101.0 | -4.7 | -14.3 |
| 3237.5 | 4101.0 | -23.3 | -15.7 |
| 3225.0 | 4101.0 | -21.7 | -23.0 |
| 3212.5 | 4101.0 | -26.2 | -30.7 |
| 3200.0 | 4101.0 | -39.2 | -35.3 |
| 3187.5 | 4101.0 | -43.1 | -43.1 |
| 3175.0 | 4101.0 | -46.4 | -43.5 |
| 3162.5 | 4101.0 | -60.8 | -42.1 |
| 3150.0 | 4101.0 | -28.1 | -38.7 |
| 3137.5 | 4101.0 | -32.1 | -34.0 |
| 3125.0 | 4101.0 | -26.3 | -30.2 |
| 3112.5 | 4101.0 | -22.5 | -31.8 |
| 3100.0 | 4101.0 | -41.8 | -30.5 |
| 3087.5 | 4101.0 | -36.2 | -31.2 |
| 3075.0 | 4101.0 | -25.6 | -35.5 |
| 3062.5 | 4101.0 | -30.0 | -40.1 |
| 3050.0 | 4101.0 | -43.8 | -37.4 |
| 3037.5 | 4101.0 | -64.7 | -34.3 |
| 3025.0 | 4101.0 | -22.9 | -37.9 |
| 3012.5 | 4101.0 | -10.3 | -37.6 |
| 3000.0 | 4101.0 | -48.0 | -31.0 |
| 2987.5 | 4101.0 | -42.0 | -25.8 |
| 2975.0 | 4101.0 | -31.6 | -20.0 |
| 2962.5 | 4101.0 | 2.9 | -4.9 |
| 2950.0 | 4101.0 | 18.8 | 6.0 |
| 2937.5 | 4101.0 | 27.2 | 13.8 |
| 2925.0 | 4101.0 | 12.7 | 16.0 |
| 2912.5 | 4101.0 | 7.5 | 13.4 |
| 2900.0 | 4101.0 | 13.6 | 7.9 |
| 2887.5 | 4101.0 | 6.1 | 7.5 |
| 2875.0 | 4101.0 | -.5 | 8.1 |
| 2862.5 | 4101.0 | 10.7 | 3.5 |
| 2850.0 | 4101.0 | 10.5 | 1.6 |
| 2837.5 | 4101.0 | -9.4 | 3.1 |
| 2825.0 | 4101.0 | -3.5 | .0 |
| 2812.5 | 4101.0 | 7.1 | -4.2 |
| 2800.0 | 4101.0 | -3.8 | -5.5 |
| 2787.5 | 4101.0 | -11.5 | -7.8 |
| 2775.0 | 4101.0 | -15.7 | -12.6 |
| 2762.5 | 4101.0 | -15.1 | -12.7 |
| 2750.0 | 4101.0 | -17.0 | -6.0 |
| 2737.5 | 4101.0 | -4.1 | 3.8 |
| 2725.0 | 4101.0 | 21.8 | 12.1 |
| 2712.5 | 4101.0 | 33.3 | 19.3 |
| 2700.0 | 4101.0 | 26.5 | 21.2 |
| 2687.5 | 4101.0 | 19.0 | 15.9 |
| 2675.0 | 4101.0 | 5.4 | 7.3 |
| 2662.5 | 4101.0 | -4.8 | -2.9 |
| 2650.0 | 4101.0 | -9.7 | -13.5 |
| 2637.5 | 4101.0 | -24.3 | -22.7 |
| 2625.0 | 4101.0 | -34.3 | -31.7 |
| 2612.5 | 4101.0 | -40.4 | -40.4 |
|  |  |  |  |


| 2600.0 | 4101.0 | -49.9 | -46.9 |
| ---: | ---: | ---: | ---: |
| 2587.5 | 4101.0 | -53.1 | -51.8 |
| 2575.0 | 4101.0 | -56.6 | -56.2 |
| 2562.5 | 4101.0 | -59.1 | -59.2 |
| 2550.0 | 4101.0 | -62.3 | -63.2 |
| 2537.5 | 4101.0 | -65.0 | -67.3 |
| 2525.0 | 4101.0 | -72.9 | -73.1 |
| 2512.5 | 4101.0 | -77.1 | -77.5 |
| 2500.0 | 4101.0 | -88.3 | -82.6 |
| 2487.5 | 4101.0 | -84.4 | -86.8 |
| 2475.0 | 4101.0 | -90.5 | -87.3 |
| 2462.5 | 4101.0 | -93.7 | -65.7 |
| 2450.0 | 4101.0 | -79.8 | 5.5 |
| 2437.5 | 4101.0 | 19.8 | 38.7 |
| 2425.0 | 4101.0 | 271.9 | 66.1 |
| 2412.5 | 4101.0 | 75.5 | 102.6 |
| 2400.0 | 4101.0 | 43.1 | 130.2 |

1.16 Line $4200 N_{\text {, }}$ West of Baseline 2400 E

| 2387.5 | 4200.0 | -29.1 | 36.6 |
| ---: | ---: | ---: | ---: |
| 2375.0 | 4200.0 | 82.2 | 35.0 |
| 2362.5 | 4200.0 | 138.0 | 36.5 |
| 2350.0 | 4200.0 | 28.9 | 36.1 |
| 2337.5 | 4200.0 | -37.5 | 10.6 |
| 2325.0 | 4200.0 | -31.2 | -23.6 |
| 2312.5 | 4200.0 | -45.1 | -17.8 |
| 2300.0 | 4200.0 | -33.1 | 7.1 |
| 2287.5 | 4200.0 | 57.8 | 18.0 |
| 2275.0 | 4200.0 | 87.1 | 33.1 |
| 2262.5 | 4200.0 | 23.2 | 40.3 |
| 2250.0 | 4200.0 | 30.7 | 25.1 |
| 2237.5 | 4200.0 | 2.6 | .1 |
| 2225.0 | 4200.0 | -18.0 | -12.8 |
| 2212.5 | 4200.0 | -37.9 | -22.7 |
| 2200.0 | 4200.0 | -41.5 | -15.5 |
| 2187.5 | 4200.0 | -18.9 | 5.9 |
| 2175.0 | 4200.0 | 39.0 | 25.2 |
| 2162.5 | 4200.0 | 88.8 | 53.7 |
| 2150.0 | 4200.0 | 58.4 | 133.7 |
| 2137.5 | 4200.0 | 101.3 | 302.6 |
| 2125.0 | 4200.0 | 381.2 | 397.7 |
| 2112.5 | 4200.0 | 883.5 | 437.5 |
| 2100.0 | 4200.0 | 564.2 | 442.9 |
| 2087.5 | 4200.0 | 257.3 | 414.6 |
| 2075.0 | 4200.0 | 128.4 | 280.3 |
| 2062.5 | 4200.0 | 239.7 | 182.6 |
| 2050.0 | 4200.0 | 212.0 | 138.4 |
| 2037.5 | 4200.0 | 75.8 | 112.7 |
| 2025.0 | 4200.0 | 36.0 | 62.5 |
| 2012.5 | 4200.0 | .0 | 16.7 |
| 2000.0 | 4200.0 | -11.5 | 1.9 |


| 1987.5 | 4200.0 | -17.0 | .7 |
| ---: | ---: | ---: | ---: |
| 1975.0 | 4200.0 | 2.0 | 10.5 |
| 1962.5 | 4200.0 | 30.0 | 28.7 |
| 1950.0 | 4200.0 | 49.2 | 43.6 |
| 1937.5 | 4200.0 | 79.3 | 50.1 |
| 1925.0 | 4200.0 | 57.7 | 46.8 |
| 1912.5 | 4200.0 | 34.1 | 39.0 |
| 1900.0 | 4200.0 | 13.7 | 24.9 |
| 1887.5 | 4200.0 | 10.3 | 15.2 |
| 1875.0 | 4200.0 | 8.9 | 9.6 |
| 1862.5 | 4200.0 | 8.9 | 8.3 |
| 1850.0 | 4200.0 | 6.3 | 7.1 |
| 1837.5 | 4200.0 | 7.3 | 5.2 |
| 1825.0 | 4200.0 | 4.3 | 2.7 |
| 1812.5 | 4200.0 | -1.0 | .1 |
| 1800.0 | 4200.0 | -3.5 | -3.0 |
| 1787.5 | 4200.0 | -6.8 | -6.0 |
| 1775.0 | 4200.0 | -8.2 | -7.7 |
| 1762.5 | 4200.0 | -10.3 | -9.3 |
| 1750.0 | 4200.0 | -9.7 | -10.1 |
| 1737.5 | 4200.0 | -11.5 | -10.6 |
| 1725.0 | 4200.0 | -11.0 | -10.5 |
| 1712.5 | 4200.0 | -10.5 | -10.8 |
| 1700.0 | 4200.0 | -10.0 | -10.5 |

1.17 Line 4200 N , East of Baseline 2400 E

| 2400.0 | 4201.0 | -47.7 | -49.6 |
| ---: | ---: | ---: | ---: |
| 2412.5 | 4201.0 | -52.1 | -42.8 |
| 2425.0 | 4201.0 | -49.1 | -38.0 |
| 2437.5 | 4201.0 | -22.2 | -33.0 |
| 2450.0 | 4201.0 | -18.8 | -26.4 |
| 2462.5 | 4201.0 | -22.6 | -20.5 |
| 2475.0 | 4201.0 | -19.5 | -18.9 |
| 2487.5 | 4201.0 | -19.6 | -15.5 |
| 2500.0 | 4201.0 | -14.1 | -9.4 |
| 2512.5 | 4201.0 | -1.5 | 4.7 |
| 2525.0 | 4201.0 | 7.5 | 27.4 |
| 2537.5 | 4201.0 | 51.2 | 47.7 |
| 2550.0 | 4201.0 | 93.8 | 52.8 |
| 2562.5 | 4201.0 | 87.6 | 47.1 |
| 2575.0 | 4201.0 | 23.7 | 28.4 |
| 2587.5 | 4201.0 | -20.9 | 3.5 |
| 2600.0 | 4201.0 | -42.4 | -19.8 |
| 2612.5 | 4201.0 | -30.4 | -27.5 |
| 2625.0 | 4201.0 | -29.1 | -25.6 |
| 2637.5 | 4201.0 | -14.8 | -18.6 |
| 2650.0 | 4201.0 | -11.5 | -16.2 |
| 2662.5 | 4201.0 | -7.4 | -17.8 |
| 2675.0 | 4201.0 | -18.4 | -24.5 |
| 2687.5 | 4201.0 | -37.0 | -30.9 |
| 2700.0 | 4201.0 | -48.2 | -38.6 |


| 2712.5 | 4201.0 | -43.6 | -43.1 |
| ---: | ---: | ---: | ---: |
| 2725.0 | 4201.0 | -46.0 | -43.4 |
| 2737.5 | 4201.0 | -40.6 | -39.8 |
| 2750.0 | 4201.0 | -38.7 | -34.2 |
| 2762.5 | 4201.0 | -30.0 | -29.0 |
| 2775.0 | 4201.0 | -15.6 | -27.0 |
| 2787.5 | 4201.0 | -20.1 | -25.7 |
| 2800.0 | 4201.0 | -30.5 | -26.0 |
| 2812.5 | 4201.0 | -32.1 | -24.2 |
| 2825.0 | 4201.0 | -31.9 | -23.1 |
| 2837.5 | 4201.0 | -6.6 | -21.8 |
| 2850.0 | 4201.0 | -14.6 | -14.9 |
| 2862.5 | 4201.0 | -23.9 | -12.0 |
| 2875.0 | 4201.0 | 2.3 | -14.1 |
| 2887.5 | 4201.0 | -17.0 | -23.4 |
| 2900.0 | 4201.0 | -17.4 | -30.4 |
| 2912.5 | 4201.0 | -61.1 | -41.5 |
| 2925.0 | 4201.0 | -58.7 | -44.3 |
| 2937.5 | 4201.0 | -53.3 | -47.1 |
| 2950.0 | 4201.0 | -30.8 | -38.8 |
| 2962.5 | 4201.0 | -31.8 | -26.6 |
| 2975.0 | 4201.0 | -19.4 | -14.8 |
| 2987.5 | 4201.0 | 2.3 | -11.7 |
| 3000.0 | 4201.0 | 5.9 | -8.5 |
| 3012.5 | 4201.0 | -15.7 | -6.8 |
| 3025.0 | 4201.0 | -15.7 | -11.5 |
| 3037.5 | 4201.0 | -10.7 | -13.3 |
| 3050.0 | 4201.0 | -21.4 | -10.8 |
| 3062.5 | 4201.0 | -2.8 | -12.4 |
| 3075.0 | 4201.0 | -3.3 | -9.7 |
| 3087.5 | 4201.0 | -23.6 | -5.6 |
| 3100.0 | 4201.0 | 2.6 | -8.0 |
| 3112.5 | 4201.0 | -.9 | -11.4 |
| 3125.0 | 4201.0 | -14.9 | -10.6 |
| 3137.5 | 4201.0 | -20.0 | -14.6 |
| 3150.0 | 4201.0 | -19.6 | -17.7 |
| 3162.5 | 4201.0 | -17.8 | -14.5 |
| 3175.0 | 4201.0 | -16.0 | -11.1 |
| 3187.5 | 4201.0 | -7 | -5.6 |
| 3200.0 | 4201.0 | -3.0 | -.9 |
| 3212.5 | 4201.0 | 8.2 | 3.7 |
| 3225.0 | 4201.0 | 5.5 | 6.2 |
| 3237.5 | 4201.0 | 7.1 | 9.7 |
| 3250.0 | 4201.0 | 13.4 | 11.8 |
| 3262.5 | 4201.0 | 14.3 | 15.0 |
| 3275.0 | 4201.0 | 18.5 | 18.3 |
| 3287.5 | 4201.0 | 21.7 | 19.3 |
| 3300.0 | 4201.0 | 23.5 | 18.5 |
| 3312.5 | 4201.0 | 18.4 | 16.9 |
| 3325.0 | 4201.0 | 10.5 | 17.0 |
| 3337.5 | 4201.0 | 10.2 | 17.4 |
| 3350.0 | 4201.0 | 22.4 | 15.3 |
| 3362.5 | 4201.0 | 25.6 | 11.5 |
|  |  |  |  |


| 3375.0 | 4201.0 | 7.6 | 5.0 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 4201.0 | -8.1 | -7.4 |
| 3400.0 | 4201.0 | -22.5 | -15.3 |
| 3412.5 | 4201.0 | -39.6 | -22.4 |
| 3425.0 | 4201.0 | -13.7 | -24.0 |
| 3437.5 | 4201.0 | -28.2 | -28.1 |
| 3450.0 | 4201.0 | -15.8 | -26.0 |
| 3462.5 | 4201.0 | -43.0 | -26.7 |
| 3475.0 | 4201.0 | -29.5 | -19.4 |
| 3487.5 | 4201.0 | -17.1 | -20.3 |
| 3500.0 | 4201.0 | 8.4 | -12.7 |

1.18 Line 4300 N , West of Baseline 2400 E

| 1700.0 | 4300.0 | -9.2 | -6.5 |
| ---: | ---: | ---: | ---: |
| 1712.5 | 4300.0 | -6.9 | -4.9 |
| 1725.0 | 4300.0 | -3.5 | -2.5 |
| 1737.5 | 4300.0 | . .1 | 2.0 |
| 1750.0 | 4300.0 | 7.0 | 7.4 |
| 1762.5 | 4300.0 | 13.1 | 13.8 |
| 1775.0 | 4300.0 | 20.4 | 21.9 |
| 1787.5 | 4300.0 | 28.6 | 29.2 |
| 1800.0 | 4300.0 | 40.2 | 36.2 |
| 1812.5 | 4300.0 | 43.9 | 41.6 |
| 1825.0 | 4300.0 | 47.7 | 44.8 |
| 1837.5 | 4300.0 | 47.7 | 44.8 |
| 1850.0 | 4300.0 | 44.4 | 42.9 |
| 1862.5 | 4300.0 | 40.1 | 40.8 |
| 1875.0 | 4300.0 | 34.6 | 40.1 |
| 1887.5 | 4300.0 | 37.0 | 52.5 |
| 1900.0 | 4300.0 | 44.3 | 73.3 |
| 1912.5 | 4300.0 | 106.4 | 82.4 |
| 1925.0 | 4300.0 | 144.0 | 71.6 |
| 1937.5 | 4300.0 | 80.3 | 63.2 |
| 1950.0 | 4300.0 | -17.2 | 45.5 |
| 1962.5 | 4300.0 | 2.5 | 23.5 |
| 1975.0 | 4300.0 | 18.1 | 19.6 |
| 1987.5 | 4300.0 | 33.7 | 35.7 |
| 2000.0 | 4300.0 | 60.9 | 52.3 |
| 2012.5 | 4300.0 | 63.3 | 91.4 |
| 2025.0 | 4300.0 | 85.7 | 204.6 |
| 2037.5 | 4300.0 | 213.6 | 437.4 |
| 2050.0 | 4300.0 | 599.7 | 451.6 |
| 2062.5 | 4300.0 | 1224.6 | 405.7 |
| 2075.0 | 4300.0 | 134.6 | 354.0 |
| 2087.5 | 4300.0 | -143.8 | 256.7 |
| 2100.0 | 4300.0 | -45.0 | 8.3 |
| 2112.5 | 4300.0 | 113.3 | -30.0 |
| 2125.0 | 4300.0 | -17.6 | -17.0 |
| 2137.5 | 4300.0 | -56.7 | -22.6 |
| 2150.0 | 4300.0 | -79.1 | -58.5 |


| 2162.5 | 4300.0 | -72.7 | -67.2 |
| ---: | ---: | ---: | ---: |
| 2175.0 | 4300.0 | -66.6 | -65.9 |
| 2187.5 | 4300.0 | -60.7 | -56.3 |
| 2200.0 | 4300.0 | -50.5 | -36.3 |
| 2212.5 | 4300.0 | -31.2 | -4.1 |
| 2225.0 | 4300.0 | 27.6 | 23.3 |
| 2237.5 | 4300.0 | 94.1 | 25.0 |
| 2250.0 | 4300.0 | 76.5 | 24.4 |
| 2262.5 | 4300.0 | -42.2 | 3.8 |
| 2275.0 | 4300.0 | -34.1 | -23.9 |
| 2287.5 | 4300.0 | -75.5 | -42.0 |
| 2300.0 | 4300.0 | -44.2 | -31.8 |
| 2312.5 | 4300.0 | -13.9 | -25.8 |
| 2325.0 | 4300.0 | 8.9 | -18.2 |
| 2337.5 | 4300.0 | -4.5 | -19.0 |
| 2350.0 | 4300.0 | -37.5 | -25.8 |
| 2362.5 | 4300.0 | -48.2 | -38.1 |
| 2375.0 | 4300.0 | -47.6 | -46.9 |
| 2387.5 | 4300.0 | -52.6 | -49.3 |

1.19 Line 4300N, East of Baseline 2400 E

| 1700.0 | 4300.0 | -9.2 | -6.5 |
| ---: | ---: | ---: | ---: |
| 1712.5 | 4300.0 | -6.9 | -4.9 |
| 1725.0 | 4300.0 | -3.5 | -2.5 |
| 1737.5 | 4300.0 | .1 | 2.0 |
| 1750.0 | 4300.0 | 7.0 | 7.4 |
| 1762.5 | 4300.0 | 13.1 | 13.8 |
| 1775.0 | 4300.0 | 20.4 | 21.9 |
| 1787.5 | 4300.0 | 28.6 | 29.2 |
| 1800.0 | 4300.0 | 40.2 | 36.2 |
| 1812.5 | 4300.0 | 43.9 | 41.6 |
| 1825.0 | 4300.0 | 47.7 | 44.8 |
| 1837.5 | 4300.0 | 47.7 | 44.8 |
| 1850.0 | 4300.0 | 44.4 | 42.9 |
| 1862.5 | 4300.0 | 40.1 | 40.8 |
| 1875.0 | 4300.0 | 34.6 | 40.1 |
| 1887.5 | 4300.0 | 37.0 | 52.5 |
| 1900.0 | 4300.0 | 44.3 | 73.3 |
| 1912.5 | 4300.0 | 106.4 | 82.4 |
| 1925.0 | 4300.0 | 144.0 | 71.6 |
| 1937.5 | 4300.0 | 80.3 | 63.2 |
| 1950.0 | 4300.0 | -17.2 | 45.5 |
| 1962.5 | 4300.0 | 2.5 | 23.5 |
| 1975.0 | 4300.0 | 18.1 | 19.6 |
| 1987.5 | 4300.0 | 33.7 | 35.7 |
| 2000.0 | 4300.0 | 60.9 | 52.3 |
| 2012.5 | 4300.0 | 63.3 | 91.4 |
| 2025.0 | 4300.0 | 85.7 | 204.6 |
| 2037.5 | 4300.0 | 213.6 | 437.4 |
| 2050.0 | 4300.0 | 599.7 | 451.6 |
| 2062.5 | 4300.0 | 1224.6 | 405.7 |


| 2075.0 | 4300.0 | 134.6 | 354.0 |
| ---: | ---: | ---: | ---: |
| 2087.5 | 4300.0 | -143.8 | 256.7 |
| 2100.0 | 4300.0 | -45.0 | 8.3 |
| 2112.5 | 4300.0 | 113.3 | -30.0 |
| 2125.0 | 4300.0 | -17.6 | -17.0 |
| 2137.5 | 4300.0 | -56.7 | -22.6 |
| 2150.0 | 4300.0 | -79.1 | -58.5 |
| 2162.5 | 4300.0 | -72.7 | -67.2 |
| 2175.0 | 4300.0 | -66.6 | -65.9 |
| 2187.5 | 4300.0 | -60.7 | -56.3 |
| 2200.0 | 4300.0 | -50.5 | -36.3 |
| 2212.5 | 4300.0 | -31.2 | -4.1 |
| 2225.0 | 4300.0 | 27.6 | 23.3 |
| 2237.5 | 4300.0 | 94.1 | 25.0 |
| 2250.0 | 4300.0 | 76.5 | 24.4 |
| 2262.5 | 4300.0 | -42.2 | 3.8 |
| 2275.0 | 4300.0 | -34.1 | -23.9 |
| 2287.5 | 4300.0 | -75.5 | -42.0 |
| 2300.0 | 4300.0 | -44.2 | -31.8 |
| 2312.5 | 4300.0 | -13.9 | -25.8 |
| 2325.0 | 4300.0 | 8.9 | -18.2 |
| 2337.5 | 4300.0 | -4.5 | -19.0 |
| 2350.0 | 4300.0 | -37.5 | -25.8 |
| 2362.5 | 4300.0 | -48.2 | -38.1 |
| 2375.0 | 4300.0 | -47.6 | -46.9 |
| 2387.5 | 4300.0 | -52.6 | -49.3 |

1.19 Line 4300 N , East of Baseline 2400 E

| 3500.0 | 4301.0 | -10.9 | -12.5 |
| ---: | ---: | ---: | ---: |
| 3487.5 | 4301.0 | -10.8 | -12.7 |
| 3475.0 | 4301.0 | -15.8 | -11.7 |
| 3462.5 | 4301.0 | -13.4 | -11.4 |
| 3450.0 | 4301.0 | -7.5 | -13.6 |
| 3437.5 | 4301.0 | -9.4 | -14.4 |
| 3425.0 | 4301.0 | -21.8 | -15.8 |
| 3412.5 | 4301.0 | -19.8 | -20.0 |
| 3400.0 | 4301.0 | -20.5 | -27.4 |
| 3387.5 | 4301.0 | -28.5 | -25.0 |
| 3375.0 | 4301.0 | -46.3 | -29.8 |
| 3362.5 | 4301.0 | -10.1 | -24.6 |
| 3350.0 | 4301.0 | -43.7 | -17.6 |
| 3337.5 | 4301.0 | 5.7 | -6.3 |
| 3325.0 | 4301.0 | 6.5 | -1.4 |
| 3312.5 | 4301.0 | 10.0 | 7.4 |
| 3300.0 | 4301.0 | 14.3 | 7.2 |
| 3287.5 | 4301.0 | .4 | 5.7 |
| 3275.0 | 4301.0 | 4.7 | 3.0 |
| 3262.5 | 4301.0 | -1.1 | .4 |
| 3250.0 | 4301.0 | -3.3 | 1.5 |
| 3237.5 | 4301.0 | 1.2 | -1.1 |
| 3225.0 | 4301.0 | 6.1 | 2.9 |


| 3212.5 | 4301.0 | -8.2 | 2.9 |
| ---: | ---: | ---: | ---: |
| 3200.0 | 4301.0 | 18.6 | 1.7 |
| 3187.5 | 4301.0 | -3.4 | -.9 |
| 3175.0 | 4301.0 | -4.5 | 4.0 |
| 3162.5 | 4301.0 | -6.9 | 2.3 |
| 3150.0 | 4301.0 | 16.0 | 2.1 |
| 3137.5 | 4301.0 | 10.1 | 2.0 |
| 3125.0 | 4301.0 | -4.0 | -1.1 |
| 3112.5 | 4301.0 | -5.2 | -14.1 |
| 3100.0 | 4301.0 | -22.3 | -29.6 |
| 3087.5 | 4301.0 | -49.2 | -43.7 |
| 3075.0 | 4301.0 | -67.2 | -55.6 |
| 3062.5 | 4301.0 | -74.8 | -63.2 |
| 3050.0 | 4301.0 | -64.3 | -59.2 |
| 3037.5 | 4301.0 | -60.5 | -52.8 |
| 3025.0 | 4301.0 | -29.4 | -49.0 |
| 3012.5 | 4301.0 | -35.0 | -36.4 |
| 3000.0 | 4301.0 | -55.9 | -22.5 |
| 2987.5 | 4301.0 | -1.3 | -14.6 |
| 2975.0 | 4301.0 | 9.2 | -5.1 |
| 2962.5 | 4301.0 | 9.9 | 8.3 |
| 2950.0 | 4301.0 | 12.6 | 6.5 |
| 2937.5 | 4301.0 | 11.3 | 2.3 |
| 2925.0 | 4301.0 | -10.3 | -4.5 |
| 2912.5 | 4301.0 | -12.2 | -12.7 |
| 2900.0 | 4301.0 | -24.0 | -17.3 |
| 2887.5 | 4301.0 | -28.4 | -16.7 |
| 2875.0 | 4301.0 | -11.5 | -14.7 |
| 2862.5 | 4301.0 | -7.3 | -11.9 |
| 2850.0 | 4301.0 | -2.4 | -9.7 |
| 2837.5 | 4301.0 | -10.1 | -14.3 |
| 2825.0 | 4301.0 | -17.4 | -13.4 |
| 2812.5 | 4301.0 | -34.3 | -11.5 |
| 2800.0 | 4301.0 | -3.0 | -10.3 |
| 2787.5 | 4301.0 | 7.3 | -10.2 |
| 2775.0 | 4301.0 | -4.1 | -7.3 |
| 2762.5 | 4301.0 | -17.0 | -7.0 |
| 2750.0 | 4301.0 | -19.5 | -9.0 |
| 2737.5 | 4301.0 | -1.6 | -11.3 |
| 2725.0 | 4301.0 | -2.7 | -12.7 |
| 2712.5 | 4301.0 | -15.6 | -14.0 |
| 2700.0 | 4301.0 | -24.0 | -20.5 |
| 2687.5 | 4301.0 | -26.3 | -27.5 |
| 2675.0 | 4301.0 | -34.0 | -31.9 |
| 2662.5 | 4301.0 | -37.5 | -33.8 |
| 2650.0 | 4301.0 | -37.6 | -34.0 |
| 2637.5 | 4301.0 | -33.7 | -31.6 |
| 2625.0 | 4301.0 | -27.4 | -28.5 |
| 2612.5 | 4301.0 | -21.6 | -26.1 |
| 2600.0 | 4301.0 | -22.2 | -23.9 |
| 2587.5 | 4301.0 | -25.6 | -25.5 |
| 2575.0 | 4301.0 | -22.6 | -29.7 |
| 2562.5 | 4301.0 | -35.6 | -31.0 |
|  |  |  |  |


| 2550.0 | 4301.0 | -42.6 | -23.1 |
| ---: | ---: | ---: | ---: |
| 2537.5 | 4301.0 | -28.5 | -10.8 |
| 2525.0 | 4301.0 | 14.0 | -.9 |
| 2512.5 | 4301.0 | 38.5 | 8.4 |
| 2500.0 | 4301.0 | 13.9 | 11.3 |
| 2487.5 | 4301.0 | 4.2 | 3.0 |
| 2475.0 | 4301.0 | -13.9 | -10.1 |
| 2462.5 | 4301.0 | -27.7 | -18.3 |
| 2450.0 | 4301.0 | -27.0 | -27.9 |
| 2437.5 | 4301.0 | -27.2 | -34.4 |
| 2425.0 | 4301.0 | -43.7 | -38.7 |
| 2412.5 | 4301.0 | -46.3 | -41.7 |
| 2400.0 | 4301.0 | -49.4 | -46.5 |

1.20 Line 4400 N , West of Baseline 2400 E

| 2387.5 | 4400.0 | -31.3 | -35.5 |
| ---: | ---: | ---: | ---: |
| 2375.0 | 4400.0 | -34.0 | -37.8 |
| 2362.5 | 4400.0 | -43.5 | -42.1 |
| 2350.0 | 4400.0 | -47.2 | -46.7 |
| 2337.5 | 4400.0 | -54.3 | -50.1 |
| 2325.0 | 4400.0 | -54.4 | -51.2 |
| 2312.5 | 4400.0 | -51.2 | -50.6 |
| 2300.0 | 4400.0 | -48.8 | -47.3 |
| 2287.5 | 4400.0 | -44.1 | -44.3 |
| 2275.0 | 4400.0 | -38.0 | -46.7 |
| 2262.5 | 4400.0 | -39.2 | -52.4 |
| 2250.0 | 4400.0 | -63.6 | -59.2 |
| 2237.5 | 4400.0 | -76.9 | -53.4 |
| 2225.0 | 4400.0 | -78.2 | -25.1 |
| 2212.5 | 4400.0 | -9.0 | -6.4 |
| 2200.0 | 4400.0 | 102.4 | .5 |
| 2187.5 | 4400.0 | 29.8 | 8.0 |
| 2175.0 | 4400.0 | -42.4 | -.2 |
| 2162.5 | 4400.0 | -40.7 | -32.7 |
| 2150.0 | 4400.0 | -49.9 | -53.3 |
| 2137.5 | 4400.0 | -60.4 | -62.3 |
| 2125.0 | 4400.0 | -73.0 | -73.0 |
| 2112.5 | 4400.0 | -87.5 | -85.6 |
| 2100.0 | 4400.0 | -94.0 | -101.7 |
| 2087.5 | 4400.0 | -113.0 | -59.7 |
| 2075.0 | 4400.0 | -140.9 | -15.7 |
| 2062.5 | 4400.0 | 137.0 | 58.3 |
| 2050.0 | 4400.0 | 132.3 | 186.7 |
| 2037.5 | 4400.0 | 276.2 | 274.1 |
| 2025.0 | 4400.0 | 528.7 | 273.4 |
| 2012.5 | 4400.0 | 296.1 | 260.0 |
| 2000.0 | 4400.0 | 133.5 | 213.8 |
| 1987.5 | 4400.0 | 65.5 | 114.7 |
| 1975.0 | 4400.0 | 45.1 | 60.0 |
| 1962.5 | 4400.0 | 33.3 | 36.5 |
| 1950.0 | 4400.0 | 22.8 | 22.8 |


| 1937.5 | 4400.0 | 15.7 | 10.9 |
| ---: | ---: | ---: | ---: |
| 1925.0 | 4400.0 | -3.0 | 11.2 |
| 1912.5 | 4400.0 | -14.5 | 21.7 |
| 1900.0 | 4400.0 | 35.1 | 25.0 |
| 1887.5 | 4400.0 | 75.1 | 31.3 |
| 1875.0 | 4400.0 | 32.2 | 41.5 |
| 1862.5 | 4400.0 | 28.8 | 40.8 |
| 1850.0 | 4400.0 | 36.2 | 33.0 |
| 1837.5 | 4400.0 | 31.9 | 33.0 |
| 1825.0 | 4400.0 | 36.0 | 30.9 |
| 1812.5 | 4400.0 | 31.9 | 26.4 |
| 1800.0 | 4400.0 | 18.4 | 23.4 |
| 1787.5 | 4400.0 | 13.8 | 18.9 |
| 1775.0 | 4400.0 | 16.7 | 14.1 |
| 1762.5 | 4400.0 | 13.7 | 11.3 |
| 1750.0 | 4400.0 | 7.8 | 8.9 |
| 1737.5 | 4400.0 | 4.3 | 5.1 |
| 1725.0 | 4400.0 | 1.9 | 1.1 |
| 1712.5 | 4400.0 | -2.4 | -2.5 |
| 1700.0 | 4400.0 | -6.3 | -6.0 |
| 1687.5 | 4400.0 | -10.1 | -9.3 |
| 1675.0 | 4400.0 | -13.0 | -12.3 |
| 1662.5 | 4400.0 | -14.8 | -14.3 |
| 1650.0 | 4400.0 | -17.1 | -16.4 |
| 1637.5 | 4400.0 | -16.6 | -18.3 |
| 1625.0 | 4400.0 | -20.4 | -19.9 |
| 1612.5 | 4400.0 | -22.4 | -20.6 |
| 1600.0 | 4400.0 | -23.0 | -21.9 |


| 1.21 | Line | 4400 N, | East of Baseline |
| :---: | ---: | ---: | ---: | ---: |
|  | 2400 |  |  |
| 2400.0 | 4401.0 | -43.3 | -30.8 |
| 2412.5 | 4401.0 | -24.0 | -30.2 |
| 2425.0 | 4401.0 | -25.1 | -27.3 |
| 2437.5 | 4401.0 | -28.4 | -17.4 |
| 2450.0 | 4401.0 | -15.6 | -12.6 |
| 2462.5 | 4401.0 | 6.2 | -10.7 |
| 2475.0 | 4401.0 | -.1 | -13.3 |
| 2487.5 | 4401.0 | -15.7 | -16.7 |
| 2500.0 | 4401.0 | -41.4 | -23.7 |
| 2512.5 | 4401.0 | -32.4 | -31.9 |
| 2525.0 | 4401.0 | -29.1 | -34.9 |
| 2537.5 | 4401.0 | -40.7 | -33.2 |
| 2550.0 | 4401.0 | -30.8 | -32.2 |
| 2562.5 | 4401.0 | -33.0 | -33.7 |
| 2575.0 | 4401.0 | -27.6 | -32.2 |
| 2587.5 | 4401.0 | -36.5 | -31.7 |
| 2600.0 | 4401.0 | -32.9 | -31.0 |
| 2612.5 | 4401.0 | -28.6 | -31.3 |
| 2625.0 | 4401.0 | -29.5 | -28.7 |
| 2637.5 | 4401.0 | -29.0 | -25.5 |
| 2650.0 | 4401.0 | -23.3 | -20.4 |


| 2662.5 | 4401.0 | -17.1 | -14.0 |
| ---: | ---: | ---: | ---: |
| 2675.0 | 4401.0 | -2.9 | -6.1 |
| 2687.5 | 4401.0 | 2.5 | 1.8 |
| 2700.0 | 4401.0 | 10.3 | 6.3 |
| 2712.5 | 4401.0 | 16.2 | 11.3 |
| 2725.0 | 4401.0 | 5.3 | 9.2 |
| 2737.5 | 4401.0 | 22.4 | 6.1 |
| 2750.0 | 4401.0 | -8.3 | 1.0 |
| 2762.5 | 4401.0 | -4.9 | -3.4 |
| 2775.0 | 4401.0 | -9.5 | -8.5 |
| 2787.5 | 4401.0 | -16.8 | -11.1 |
| 2800.0 | 4401.0 | -3.1 | -13.0 |
| 2812.5 | 4401.0 | -21.3 | -10.8 |
| 2825.0 | 4401.0 | -14.1 | -8.2 |
| 2837.5 | 4401.0 | 1.3 | -12.8 |
| 2850.0 | 4401.0 | -3.8 | -17.6 |
| 2862.5 | 4401.0 | -26.3 | -20.8 |
| 2875.0 | 4401.0 | -45.3 | -25.2 |
| 2887.5 | 4401.0 | -30.0 | -24.6 |
| 2900.0 | 4401.0 | -20.6 | -18.9 |
| 2912.5 | 4401.0 | -.7 | -10.0 |
| 2925.0 | 4401.0 | 2.3 | -5.5 |
| 2937.5 | 4401.0 | -.9 | -.3 |
| 2950.0 | 4401.0 | -7.6 | 1.0 |
| 2962.5 | 4401.0 | 5.2 | -1.0 |
| 2975.0 | 4401.0 | 6.2 | -1.9 |
| 2987.5 | 4401.0 | -8.1 | 1.2 |
| 3000.0 | 4401.0 | -5.4 | -2.1 |
| 3012.5 | 4401.0 | 8.2 | -8.6 |
| 3025.0 | 4401.0 | -11.2 | -12.5 |
| 3037.5 | 4401.0 | -26.3 | -12.8 |
| 3050.0 | 4401.0 | -27.6 | -14.4 |
| 3062.5 | 4401.0 | -7.2 | -15.6 |
| 3075.0 | 4401.0 | .3 | -12.1 |
| 3087.5 | 4401.0 | -17.3 | -10.4 |
| 3100.0 | 4401.0 | -8.5 | -10.4 |
| 3112.5 | 4401.0 | -19.3 | -11.8 |
| 3125.0 | 4401.0 | -7.0 | -8.0 |
| 3137.5 | 4401.0 | -7.1 | -5.1 |
| 3150.0 | 4401.0 | 2.0 | -.3 |
| 3162.5 | 4401.0 | 6.0 | 2.0 |
| 3175.0 | 4401.0 | 4.6 | 4.6 |
| 3187.5 | 4401.0 | 4.5 | 3.7 |
| 3200.0 | 4401.0 | 6.0 | -1.3 |
| 3212.5 | 4401.0 | -2.6 | -3.5 |
| 3225.0 | 4401.0 | -18.9 | -6.5 |
| 3237.5 | 4401.0 | -6.7 | -9.3 |
| 3250.0 | 4401.0 | -10.5 | -11.4 |
| 3262.5 | 4401.0 | -7.7 | -11.7 |
| 3275.0 | 4401.0 | -13.3 | -13.5 |
| 3287.5 | 4401.0 | -20.1 | -9.5 |
| 3300.0 | 4401.0 | -15.8 | -8.9 |
| 3312.5 | 4401.0 | 9.4 | -8.8 |
|  |  |  |  |


| 3325.0 | 4401.0 | -4.5 | -7.9 |
| ---: | ---: | ---: | ---: |
| 3337.5 | 4401.0 | -13.1 | -3.6 |
| 3350.0 | 4401.0 | -15.4 | -4.2 |
| 3362.5 | 4401.0 | 5.5 | -2.9 |
| 3375.0 | 4401.0 | 6.5 | 1.0 |
| 3387.5 | 4401.0 | 2.2 | 4.9 |
| 3400.0 | 4401.0 | 6.3 | 2.9 |
| 3412.5 | 4401.0 | 4.1 | 2.6 |
| 3425.0 | 4401.0 | -4.6 | 4.1 |
| 3437.5 | 4401.0 | 4.8 | 4.0 |
| 3450.0 | 4401.0 | 10.0 | 1.7 |
| 3462.5 | 4401.0 | 5.6 | 3.1 |
| 3475.0 | 4401.0 | -7.5 | 4.5 |
| 3487.5 | 4401.0 | 2.4 | 3.1 |
| 3500.0 | 4401.0 | 11.9 | 2.3 |

1.22 Line 4450 N

| 2900.0 | 4451.0 | -25.8 | -26.0 |
| ---: | ---: | ---: | ---: |
| 2887.5 | 4451.0 | -28.5 | -17.3 |
| 2875.0 | 4451.0 | -23.7 | -13.1 |
| 2862.5 | 4451.0 | 8.9 | -8.0 |
| 2850.0 | 4451.0 | 3.7 | -2.5 |
| 2837.5 | 4451.0 | -.3 | 3.0 |
| 2825.0 | 4451.0 | -1.3 | -2.7 |
| 2812.5 | 4451.0 | 4.1 | -6.2 |
| 2800.0 | 4451.0 | -19.6 | -9.9 |
| 2787.5 | 4451.0 | -13.9 | -14.0 |
| 2775.0 | 4451.0 | -18.7 | -15.6 |
| 2762.5 | 4451.0 | -22.0 | -11.4 |
| 2750.0 | 4451.0 | -3.8 | -6.2 |
| 2737.5 | 4451.0 | 1.5 | 4.0 |
| 2725.0 | 4451.0 | 12.0 | 11.4 |
| 2712.5 | 4451.0 | 32.4 | 15.2 |
| 2700.0 | 4451.0 | 14.7 | 16.9 |
| 2687.5 | 4451.0 | 15.4 | 16.8 |
| 2675.0 | 4451.0 | 9.9 | 10.2 |
| 2662.5 | 4451.0 | 11.8 | 2.1 |
| 2650.0 | 4451.0 | -.6 | -6.6 |
| 2637.5 | 4451.0 | -26.0 | -13.9 |
| 2625.0 | 4451.0 | -28.2 | -22.5 |
| 2612.5 | 4451.0 | -26.7 | -29.9 |
| 2600.0 | 4451.0 | -31.0 | -31.9 |
| 2587.5 | 4451.0 | -37.8 | -35.3 |
| 2575.0 | 4451.0 | -35.6 | -36.3 |
| 2562.5 | 4451.0 | -45.4 | -36.3 |
| 2550.0 | 4451.0 | -31.6 | -33.3 |
| 2537.5 | 4451.0 | -31.2 | -30.9 |
| 2525.0 | 4451.0 | -22.7 | -27.1 |
| 2512.5 | 4451.0 | -23.8 | -26.9 |
| 2500.0 | 4451.0 | -26.0 | -28.4 |


| 2487.5 | 4451.0 | -31.0 | -31.9 |
| :--- | :--- | :--- | :--- |
| 2475.0 | 4451.0 | -38.7 | -34.4 |
| 2462.5 | 4451.0 | -40.0 | -36.5 |
| 2450.0 | 4451.0 | -36.4 | -36.6 |
| 2437.5 | 4451.0 | -36.6 | -34.2 |
| 2425.0 | 4451.0 | -31.1 | -31.8 |
| 2412.5 | 4451.0 | -27.0 | -30.7 |
| 2400.0 | 4451.0 | -28.1 | -28.7 |

1.23 Line

## 4500N

| 3500.0 | 4501.0 | 10.7 | 12.7 |
| ---: | ---: | ---: | ---: |
| 3487.5 | 4501.0 | 13.5 | 13.1 |
| 3475.0 | 4501.0 | 13.8 | 14.0 |
| 3462.5 | 4501.0 | 14.3 | 14.4 |
| 3450.0 | 4501.0 | 17.7 | 13.5 |
| 3437.5 | 4501.0 | 12.8 | 11.6 |
| 3425.0 | 4501.0 | 8.8 | 9.7 |
| 3412.5 | 4501.0 | 4.2 | 6.7 |
| 3400.0 | 4501.0 | 4.9 | 4.2 |
| 3387.5 | 4501.0 | 2.6 | .9 |
| 3375.0 | 4501.0 | -6 | -2.3 |
| 3362.5 | 4501.0 | -7.6 | -3.6 |
| 3350.0 | 4501.0 | -11.8 | -4.3 |
| 3337.5 | 4501.0 | -1.6 | -4.0 |
| 3325.0 | 4501.0 | -1.3 | -3.4 |
| 3312.5 | 4501.0 | 2.2 | -2.1 |
| 3300.0 | 4501.0 | -4.5 | -2.8 |
| 3287.5 | 4501.0 | -5.1 | -4.8 |
| 3275.0 | 4501.0 | -5.5 | -4.7 |
| 3262.5 | 4501.0 | -10.9 | -4.5 |
| 3250.0 | 4501.0 | 2.3 | -6.3 |
| 3237.5 | 4501.0 | -3.2 | -6.4 |
| 3225.0 | 4501.0 | -14.4 | -6.4 |
| 3212.5 | 4501.0 | -5.9 | -10.3 |
| 3200.0 | 4501.0 | -10.6 | -12.4 |
| 3187.5 | 4501.0 | -17.5 | -9.9 |
| 3175.0 | 4501.0 | -13.7 | -11.2 |
| 3162.5 | 4501.0 | -1.9 | -13.5 |
| 3150.0 | 4501.0 | -12.5 | -12.7 |
| 3137.5 | 4501.0 | -21.7 | -12.8 |
| 3125.0 | 4501.0 | -13.7 | -15.6 |
| 3112.5 | 4501.0 | -14.2 | -15.2 |
| 3100.0 | 4501.0 | -15.8 | -12.4 |
| 3087.5 | 4501.0 | -10.5 | -10.2 |
| 3075.0 | 4501.0 | -7.9 | -9.9 |
| 3062.5 | 4501.0 | -2.5 | -10.0 |
| 3050.0 | 4501.0 | -12.6 | -14.3 |
| 3037.5 | 4501.0 | -16.6 | -15.5 |
| 3025.0 | 4501.0 | -31.7 | -16.9 |
| 3012.5 | 4501.0 | -14.3 | -12.9 |


| 3000.0 | 4501.0 | -9.4 | -10.9 |
| ---: | ---: | ---: | ---: |
| 2987.5 | 4501.0 | -6.7 | -12.2 |
| 2975.0 | 4501.0 | -6.6 | -13.4 |
| 2962.5 | 4501.0 | -38.3 | -13.5 |
| 2950.0 | 4501.0 | -20.3 | -14.5 |
| 2937.5 | 4501.0 | -10.0 | -12.1 |
| 2925.0 | 4501.0 | 2.8 | -7.2 |
| 2912.5 | 4501.0 | 5.2 | -2.2 |
| 2900.0 | 4501.0 | -13.9 | -2.2 |
| 2887.5 | 4501.0 | 4.9 | -2.9 |
| 2875.0 | 4501.0 | -10.1 | -4.9 |
| 2862.5 | 4501.0 | -.5 | -4.8 |
| 2850.0 | 4501.0 | -4.9 | -11.1 |
| 2837.5 | 4501.0 | -13.5 | -10.5 |
| 2825.0 | 4501.0 | -26.5 | -10.5 |
| 2812.5 | 4501.0 | -7.0 | -13.9 |
| 2800.0 | 4501.0 | -.4 | -16.2 |
| 2787.5 | 4501.0 | -22.1 | -11.1 |
| 2775.0 | 4501.0 | -25.2 | -9.4 |
| 2762.5 | 4501.0 | -.7 | -10.8 |
| 2750.0 | 4501.0 | 1.3 | -9.5 |
| 2737.5 | 4501.0 | -7.5 | -8.1 |
| 2725.0 | 4501.0 | -15.3 | -9.2 |
| 2712.5 | 4501.0 | -18.3 | -9.8 |
| 2700.0 | 4501.0 | -6.3 | -9.0 |
| 2687.5 | 4501.0 | -1.8 | -5.6 |
| 2675.0 | 4501.0 | -3.3 | -3.9 |
| 2662.5 | 4501.0 | 1.6 | -1.8 |
| 2650.0 | 4501.0 | -9.6 | -4.6 |
| 2637.5 | 4501.0 | 4.3 | -9.1 |
| 2625.0 | 4501.0 | -15.9 | -11.9 |
| 2612.5 | 4501.0 | -25.9 | -12.0 |
| 2600.0 | 4501.0 | -12.2 | -14.7 |
| 2587.5 | 4501.0 | -10.5 | -14.9 |
| 2575.0 | 4501.0 | -9.1 | -14.1 |
| 2562.5 | 4501.0 | -16.9 | -17.2 |
| 2550.0 | 4501.0 | -21.9 | -20.0 |
| 2537.5 | 4501.0 | -27.5 | -24.9 |
| 2525.0 | 4501.0 | -24.7 | -27.2 |
| 2512.5 | 4501.0 | -33.7 | -29.5 |
| 2500.0 | 4501.0 | -28.4 | -30.6 |
| 2487.5 | 4501.0 | -33.0 | -31.3 |
| 2475.0 | 4501.0 | -33.1 | -29.6 |
| 2462.5 | 4501.0 | -28.1 | -32.0 |
| 2450.0 | 4501.0 | -25.6 | -33.1 |
| 2437.5 | 4501.0 | -40.0 | -35.1 |
| 2425.0 | 4501.0 | -38.5 | -32.1 |
| 2412.5 | 4501.0 | -43.5 | -33.8 |
| 2400.0 | 4501.0 | -13.0 | -31.7 |
| 2387.5 | 4500.0 | -37.0 | -41.0 |
| 2375.0 | 4500.0 | -52.2 | -41.0 |
| 2362.5 | 4500.0 | -43.8 | -43.6 |
| 2350.0 | 4500.0 | -40.8 | -42.9 |
|  |  |  |  |


| 2337.5 | 4500.0 | -44.1 | -40.7 |
| ---: | ---: | ---: | ---: |
| 2325.0 | 4500.0 | -33.4 | -43.4 |
| 2312.5 | 4500.0 | -41.2 | -44.3 |
| 2300.0 | 4500.0 | -57.5 | -43.3 |
| 2287.5 | 4500.0 | -45.4 | -43.9 |
| 2275.0 | 4500.0 | -38.9 | -42.9 |
| 2262.5 | 4500.0 | -36.5 | -37.5 |
| 2250.0 | 4500.0 | -36.2 | -35.9 |
| 2237.5 | 4500.0 | -30.6 | -36.1 |
| 2225.0 | 4500.0 | -37.4 | -36.7 |
| 2212.5 | 4500.0 | -39.7 | -37.0 |
| 2200.0 | 4500.0 | -39.5 | -36.8 |
| 2187.5 | 4500.0 | -37.8 | -37.8 |
| 2175.0 | 4500.0 | -29.8 | -37.0 |
| 2162.5 | 4500.0 | -42.3 | -37.0 |
| 2150.0 | 4500.0 | -35.5 | -37.8 |
| 2137.5 | 4500.0 | -39.8 | -40.0 |
| 2125.0 | 4500.0 | -41.4 | -38.0 |
| 2112.5 | 4500.0 | -40.8 | -34.9 |
| 2100.0 | 4500.0 | -32.6 | -28.7 |
| 2087.5 | 4500.0 | -19.8 | -20.3 |
| 2075.0 | 4500.0 | -8.8 | -11.8 |
| 2062.5 | 4500.0 | .5 | -4.6 |
| 2050.0 | 4500.0 | 1.5 | .6 |
| 2037.5 | 4500.0 | 3.6 | 4.3 |
| 2025.0 | 4500.0 | 6.4 | 7.0 |
| 2012.5 | 4500.0 | 9.6 | 9.8 |
| 2000.0 | 4500.0 | 14.0 | 13.2 |
| 1987.5 | 4500.0 | 15.3 | 15.3 |
| 1975.0 | 4500.0 | 20.7 | 16.8 |
| 1962.5 | 4500.0 | 16.7 | 17.4 |
| 1950.0 | 4500.0 | 17.1 | 17.2 |
| 1937.5 | 4500.0 | 17.2 | 15.0 |
| 1925.0 | 4500.0 | 14.3 | 13.2 |
| 1912.5 | 4500.0 | 9.8 | 11.2 |
| 1900.0 | 4500.0 | 7.7 | 8.4 |
| 1887.5 | 4500.0 | 7.2 | 6.7 |
| 1875.0 | 4500.0 | 3.1 | 5.4 |
| 1862.5 | 4500.0 | 5.5 | 5.6 |
| 1850.0 | 4500.0 | 3.7 | 7.2 |
| 1837.5 | 4500.0 | 8.5 | 11.0 |
| 1825.0 | 4500.0 | 15.2 | 15.2 |
| 1812.5 | 4500.0 | 21.9 | 19.7 |
| 1800.0 | 4500.0 | 26.7 | 23.7 |
| 1787.5 | 4500.0 | 26.2 | 28.1 |
| 1775.0 | 4500.0 | 28.5 | 30.2 |
| 1762.5 | 4500.0 | 37.0 | 30.7 |
| 1750.0 | 4500.0 | 32.8 | 29.5 |
| 1737.5 | 4500.0 | 29.2 | 26.6 |
| 1725.0 | 4500.0 | 19.9 | 20.8 |
| 1712.5 | 4500.0 | 14.2 | 15.0 |
| 1700.0 | 4500.0 | 7.9 | 8.9 |
| 1687.5 | 4500.0 | 3.9 | 3.6 |
|  |  |  |  |


| 1675.0 | 4500.0 | -1.2 | -2.1 |
| ---: | ---: | ---: | ---: |
| 1662.5 | 4500.0 | -6.6 | -6.6 |
| 1650.0 | 4500.0 | -14.6 | -11.3 |
| 1637.5 | 4500.0 | -14.5 | -15.6 |
| 1625.0 | 4500.0 | -19.5 | -18.2 |
| 1612.5 | 4500.0 | -22.8 | -19.1 |
| 1600.0 | 4500.0 | -19.6 | -20.6 |

### 1.24 Line 4600 N

| 1600.0 | 4600.0 | -4.3 | -2.6 |
| ---: | ---: | ---: | ---: |
| 1612.5 | 4600.0 | -2.4 | -.7 |
| 1625.0 | 4600.0 | -1.1 | 1.8 |
| 1637.5 | 4600.0 | 4.9 | 5.1 |
| 1650.0 | 4600.0 | 11.7 | 9.0 |
| 1662.5 | 4600.0 | 12.5 | 12.5 |
| 1675.0 | 4600.0 | 17.0 | 14.2 |
| 1687.5 | 4600.0 | 16.2 | 15.0 |
| 1700.0 | 4600.0 | 13.4 | 15.8 |
| 1712.5 | 4600.0 | 15.8 | 15.9 |
| 1725.0 | 4600.0 | 16.7 | 15.2 |
| 1737.5 | 4600.0 | 17.6 | 12.7 |
| 1750.0 | 4600.0 | 12.6 | 8.6 |
| 1762.5 | 4600.0 | -4.8 | 3.4 |
| 1775.0 | 4600.0 | -4.9 | -3.4 |
| 1787.5 | 4600.0 | -9.0 | -11.6 |
| 1800.0 | 4600.0 | -16.4 | -16.3 |
| 1812.5 | 4600.0 | -28.3 | -16.5 |
| 1825.0 | 4600.0 | -22.9 | -13.6 |
| 1837.5 | 4600.0 | -5.7 | -9.1 |
| 1850.0 | 4600.0 | 5.5 | 1.0 |
| 1862.5 | 4600.0 | 6.1 | 9.7 |
| 1875.0 | 4600.0 | 22.1 | 14.3 |
| 1887.5 | 4600.0 | 20.6 | 17.0 |
| 1900.0 | 4600.0 | 17.2 | 19.3 |
| 1912.5 | 4600.0 | 18.8 | 21.0 |
| 1925.0 | 4600.0 | 17.9 | 23.5 |
| 1937.5 | 4600.0 | 30.4 | 26.5 |
| 1950.0 | 4600.0 | 33.3 | 28.7 |
| 1962.5 | 4600.0 | 31.9 | 31.8 |
| 1975.0 | 4600.0 | 29.8 | 30.0 |
| 1987.5 | 4600.0 | 33.4 | 27.7 |
| 2000.0 | 4600.0 | 21.8 | 24.4 |
| 2012.5 | 4600.0 | 21.5 | 19.2 |
| 2025.0 | 4600.0 | 15.6 | 10.3 |
| 2037.5 | 4600.0 | 3.5 | 2.2 |
| 2050.0 | 4600.0 | -11.0 | -6.9 |
| 2062.5 | 4600.0 | -18.7 | -14.8 |
| 2075.0 | 4600.0 | -23.7 | -22.5 |
| 2087.5 | 4600.0 | -24.3 | -29.3 |
| 2100.0 | 4600.0 | -34.8 | -34.4 |
| 2112.5 | 4600.0 | -44.9 | -35.7 |


| 2125.0 | 4600.0 | -44.3 | -35.5 |
| :---: | :---: | :---: | :---: |
| 2137.5 | 4600.0 | -30.2 | -31.7 |
| 2150.0 | 4600.0 | -23.1 | -24.2 |
| 2162.5 | 4600.0 | -16.1 | -17.0 |
| 2175.0 | 4600.0 | -7.3 | -12.9 |
| 2187.5 | 4600.0 | -8.2 | -9.1 |
| 2200.0 | 4600.0 | -9.7 | -7.1 |
| 2212.5 | 4600.0 | -4.2 | -6.5 |
| 2225.0 | 4600.0 | -6.2 | -8.1 |
| 2237.5 | 4600.0 | -4.2 | -12.6 |
| 2250.0 | 4600.0 | -16.3 | -20.1 |
| 2262.5 | 4600.0 | -32.1 | -24.5 |
| 2275.0 | 4600.0 | -41.9 | -29.3 |
| 2287.5 | 4600.0 | -27.9 | -32.9 |
| 2300.0 | 4600.0 | -28.2 | -32.8 |
| 2312.5 | 4600.0 | -34.5 | -30.2 |
| 2325.0 | 4600.0 | -31.3 | -29.3 |
| 2337.5 | 4600.0 | -29.0 | -25.7 |
| 2350.0 | 4600.0 | -23.6 | -17.2 |
| 2362.5 | 4600.0 | -10.0 | -7.2 |
| 2375.0 | 4600.0 | 8.1 | 1.8 |
| 2387.5 | 4600.0 | 18.7 | 8.1 |
| 2400.0 | 4600.0 | 15.6 | 14.1 |
| 2412.5 | 4601.0 | -8.2 | -15.0 |
| 2425.0 | 4601.0 | -28.5 | -17.7 |
| 2437.5 | 4601.0 | -38.9 | -30.5 |
| 2450.0 | 4601.0 | -28.6 | -34.7 |
| 2462.5 | 4601.0 | -48.2 | -35.8 |
| 2475.0 | 4601.0 | -29.2 | -35.4 |
| 2487.5 | 4601.0 | -34.0 | -36.7 |
| 2500.0 | 4601.0 | -37.2 | -32.5 |
| 2512.5 | 4601.0 | -34.8 | -31.2 |
| 2525.0 | 4601.0 | -27.4 | -29.1 |
| 2537.5 | 4601.0 | -22.5 | -25.8 |
| 2550.0 | 4601.0 | -23.7 | -22.8 |
| 2562.5 | 4601.0 | -20.7 | -22.1 |
| 2575.0 | 4601.0 | -19.7 | -24.1 |
| 2587.5 | 4601.0 | -23.7 | -23.3 |
| 2600.0 | 4601.0 | -32.5 | -22.2 |
| 2612.5 | 4601.0 | -20.0 | -21.2 |
| 2625.0 | 4601.0 | -15.2 | -20.0 |
| 2637.5 | 4601.0 | -14.8 | -16.9 |
| 2650.0 | 4601.0 | -17.4 | -17.0 |
| 2662.5 | 4601.0 | -17.1 | -16.9 |
| 2675.0 | 4601.0 | -20.3 | -19.3 |
| 2687.5 | 4601.0 | -15.0 | -18.0 |
| 2700.0 | 4601.0 | -26.7 | -17.2 |
| 2712.5 | 4601.0 | -10.8 | -14.9 |
| 2725.0 | 4601.0 | -13.0 | -11.0 |
| 2737.5 | 4601.0 | -8.9 | -8.9 |
| 2750.0 | 4601.0 | 4.6 | -10.4 |
| 2762.5 | 4601.0 | -16.3 | -8.9 |
| 2775.0 | 4601.0 | -18.4 | -7.6 |


| 2787.5 | 4601.0 | -5.7 | -6.1 |
| ---: | ---: | ---: | ---: |
| 2800.0 | 4601.0 | -2.3 | -1.5 |
| 2812.5 | 4601.0 | 12.0 | 1.5 |
| 2825.0 | 4601.0 | 6.7 | 1.3 |
| 2837.5 | 4601.0 | -3.4 | .7 |
| 2850.0 | 4601.0 | -6.5 | .0 |
| 2862.5 | 4601.0 | -5.4 | -4.8 |
| 2875.0 | 4601.0 | 8.8 | -3.1 |
| 2887.5 | 4601.0 | -17.7 | -2.5 |
| 2900.0 | 4601.0 | 5.4 | -.4 |
| 2912.5 | 4601.0 | -3.8 | -1.6 |
| 2925.0 | 4601.0 | 5.2 | 1.8 |
| 2937.5 | 4601.0 | 2.9 | .3 |
| 2950.0 | 4601.0 | -.5 | -.3 |
| 2962.5 | 4601.0 | -2.4 | -3.0 |
| 2975.0 | 4601.0 | -6.8 | -6.3 |
| 2987.5 | 4601.0 | -8.2 | -6.4 |
| 3000.0 | 4601.0 | -13.8 | -4.8 |
| 3012.5 | 4601.0 | -.9 | -4.5 |
| 3025.0 | 4601.0 | 5.7 | -6.3 |
| 3037.5 | 4601.0 | -5.5 | -6.2 |
| 3050.0 | 4601.0 | -17.2 | -7.2 |
| 3062.5 | 4601.0 | -12.9 | -10.2 |
| 3075.0 | 4601.0 | -6.3 | -9.4 |
| 3087.5 | 4601.0 | -9.0 | -6.7 |
| 3100.0 | 4601.0 | -1.4 | -6.1 |
| 3112.5 | 4601.0 | -3.9 | -7.2 |
| 3125.0 | 4601.0 | -9.8 | -8.3 |
| 3137.5 | 4601.0 | -12.0 | -10.4 |
| 3150.0 | 4601.0 | -14.4 | -10.9 |
| 3162.5 | 4601.0 | -11.9 | -10.7 |
| 3175.0 | 4601.0 | -6.3 | -9.0 |
| 3187.5 | 4601.0 | -9.0 | -8.0 |
| 3200.0 | 4601.0 | -3.2 | -7.6 |
| 3212.5 | 4601.0 | -9.7 | -7.4 |
| 3225.0 | 4601.0 | -9.6 | -6.8 |
| 3237.5 | 4601.0 | -5.6 | -5.8 |
| 3250.0 | 4601.0 | -6.1 | -3.0 |
| 3262.5 | 4601.0 | 2.2 | -.9 |
| 3275.0 | 4601.0 | 4.1 | 2.1 |
| 3287.5 | 4601.0 | 1.0 | 4.5 |
| 3300.0 | 4601.0 | 9.2 | 4.3 |
| 3312.5 | 4601.0 | 6.2 | 4.5 |
| 3325.0 | 4601.0 | 1.1 | 5.2 |
| 3337.5 | 4601.0 | 4.9 | 5.6 |
| 3350.0 | 4601.0 | 4.6 | 6.2 |
| 3362.5 | 4601.0 | 11.3 | 7.7 |
| 3375.0 | 4601.0 | 9.0 | 9.7 |
| 3387.5 | 4601.0 | 8.8 | 15.3 |
| 3400.0 | 4601.0 | 14.7 | 24.4 |
| 3412.5 | 4601.0 | 32.6 | 27.9 |
| 3425.0 | 4601.0 | 57.0 | 29.2 |
| 3437.5 | 4601.0 | 26.4 | 28.3 |


| 3450.0 | 4601.0 | 15.5 | 23.9 |
| ---: | ---: | ---: | ---: |
| 3462.5 | 4601.0 | 9.9 | 14.8 |
| 3475.0 | 4601.0 | 10.7 | 12.9 |
| 3487.5 | 4601.0 | 11.3 | 12.2 |
| 3500.0 | 4601.0 | 17.0 | 13.0 |

### 1.25 Line 4700 N

| 2400.0 | 4700.0 | -41.3 | -37.4 |
| ---: | ---: | ---: | ---: |
| 2387.5 | 4700.0 | -38.0 | -35.3 |
| 2375.0 | 4700.0 | -33.0 | -33.4 |
| 2362.5 | 4700.0 | -28.9 | -30.1 |
| 2350.0 | 4700.0 | -26.0 | -28.9 |
| 2337.5 | 4700.0 | -24.5 | -30.0 |
| 2325.0 | 4700.0 | -31.9 | -31.2 |
| 2312.5 | 4700.0 | -38.7 | -33.9 |
| 2300.0 | 4700.0 | -34.7 | -37.1 |
| 2287.5 | 4700.0 | -39.8 | -37.9 |
| 2275.0 | 4700.0 | -40.5 | -35.1 |
| 2262.5 | 4700.0 | -35.6 | -34.8 |
| 2250.0 | 4700.0 | -24.9 | -33.6 |
| 2237.5 | 4700.0 | -33.4 | -33.6 |
| 2225.0 | 4700.0 | -33.4 | -31.7 |
| 2212.5 | 4700.0 | -40.7 | -26.8 |
| 2200.0 | 4700.0 | -26.0 | -18.1 |
| 2187.5 | 4700.0 | -.4 | -10.4 |
| 2175.0 | 4700.0 | 10.1 | -.1 |
| 2162.5 | 4700.0 | 4.9 | 4.7 |
| 2150.0 | 4700.0 | 10.9 | 2.3 |
| 2137.5 | 4700.0 | -1.9 | -1.9 |
| 2125.0 | 4700.0 | -12.6 | -4.4 |
| 2112.5 | 4700.0 | -10.6 | -9.7 |
| 2100.0 | 4700.0 | -7.7 | -9.9 |
| 2087.5 | 4700.0 | -15.5 | -9.4 |
| 2075.0 | 4700.0 | -3.0 | -8.4 |
| 2062.5 | 4700.0 | -10.0 | -5.5 |
| 2050.0 | 4700.0 | -5.9 | -.8 |
| 2037.5 | 4700.0 | 6.8 | 5.0 |
| 2025.0 | 4700.0 | 8.2 | 12.7 |
| 2012.5 | 4700.0 | 25.9 | 20.2 |
| 2000.0 | 4700.0 | 28.7 | 24.7 |
| 1987.5 | 4700.0 | 31.4 | 30.8 |
| 1975.0 | 4700.0 | 29.2 | 33.2 |
| 1962.5 | 4700.0 | 38.8 | 35.6 |
| 1950.0 | 4700.0 | 37.9 | 38.1 |
| 1937.5 | 4700.0 | 40.5 | 40.6 |
| 1925.0 | 4700.0 | 44.0 | 40.7 |
| 1912.5 | 4700.0 | 41.6 | 39.0 |
| 1900.0 | 4700.0 | 39.3 | 36.3 |
| 1887.5 | 4700.0 | 29.4 | 33.4 |
| 1875.0 | 4700.0 | 27.0 | 28.7 |
| 1862.5 | 4700.0 | 29.7 | 22.0 |
|  |  |  |  |


| 1850.0 | 4700.0 | 18.3 | 16.2 |
| ---: | ---: | ---: | ---: |
| 1837.5 | 4700.0 | 5.7 | 9.3 |
| 1825.0 | 4700.0 | . .1 | .9 |
| 1812.5 | 4700.0 | -7.2 | -7.2 |
| 1800.0 | 4700.0 | -12.3 | -12.4 |
| 1787.5 | 4700.0 | -22.3 | -16.1 |
| 1775.0 | 4700.0 | -20.1 | -15.8 |
| 1762.5 | 4700.0 | -18.4 | -12.0 |
| 1750.0 | 4700.0 | -6.0 | -.5 |
| 1737.5 | 4700.0 | 7.0 | 13.8 |
| 1725.0 | 4700.0 | 34.8 | 25.0 |
| 1712.5 | 4700.0 | 51.8 | 34.0 |
| 1700.0 | 4700.0 | 37.6 | 38.2 |
| 1687.5 | 4700.0 | 38.6 | 37.0 |
| 1675.0 | 4700.0 | 28.2 | 32.3 |
| 1662.5 | 4700.0 | 28.9 | 29.4 |
| 1650.0 | 4700.0 | 28.3 | 22.9 |
| 1637.5 | 4700.0 | 22.9 | 16.0 |
| 1625.0 | 4700.0 | 6.4 | 8.2 |
| 1612.5 | 4700.0 | -6.7 | 3.2 |
| 1600.0 | 4700.0 | -9.7 | -3.3 |

### 1.26 Line 4800 N

| 1600.0 | 4800.0 | 16.9 | 13.0 |
| ---: | ---: | ---: | ---: |
| 1612.5 | 4800.0 | 10.0 | 15.1 |
| 1625.0 | 4800.0 | 12.1 | 16.7 |
| 1637.5 | 4800.0 | 21.6 | 15.8 |
| 1650.0 | 4800.0 | 22.8 | 17.8 |
| 1662.5 | 4800.0 | 12.6 | 18.2 |
| 1675.0 | 4800.0 | 20.0 | 15.5 |
| 1687.5 | 4800.0 | 13.8 | 16.3 |
| 1700.0 | 4800.0 | 8.3 | 17.4 |
| 1712.5 | 4800.0 | 27.0 | 14.6 |
| 1725.0 | 4800.0 | 17.7 | 10.8 |
| 1737.5 | 4800.0 | 6.2 | 8.4 |
| 1750.0 | 4800.0 | -5.3 | 4.7 |
| 1762.5 | 4800.0 | -3.7 | 1.5 |
| 1775.0 | 4800.0 | 8.6 | 2.3 |
| 1787.5 | 4800.0 | 1.5 | 8.3 |
| 1800.0 | 4800.0 | 10.2 | 14.0 |
| 1812.5 | 4800.0 | 25.1 | 18.1 |
| 1825.0 | 4800.0 | 24.5 | 23.7 |
| 1837.5 | 4800.0 | 29.2 | 28.4 |
| 1850.0 | 4800.0 | 29.7 | 26.5 |
| 1862.5 | 4800.0 | 33.5 | 26.9 |
| 1875.0 | 4800.0 | 15.4 | 28.3 |
| 1887.5 | 4800.0 | 26.8 | 29.5 |
| 1900.0 | 4800.0 | 36.1 | 30.1 |
| 1912.5 | 4800.0 | 35.6 | 31.0 |
| 1925.0 | 4800.0 | 36.8 | 26.9 |
| 1937.5 | 4800.0 | 19.6 | 20.4 |


| 1950.0 | 4800.0 | 6.6 | 13.9 |
| ---: | ---: | ---: | ---: |
| 1962.5 | 4800.0 | 3.4 | 6.0 |
| 1975.0 | 4800.0 | 3.0 | 1.6 |
| 1987.5 | 4800.0 | -2.8 | -3.3 |
| 2000.0 | 4800.0 | -2.1 | -8.5 |
| 2012.5 | 4800.0 | -18.0 | -12.2 |
| 2025.0 | 4800.0 | -22.5 | -12.7 |
| 2037.5 | 4800.0 | -15.4 | -10.7 |
| 2050.0 | 4800.0 | -5.7 | -4.1 |
| 2062.5 | 4800.0 | 8.3 | 7.5 |
| 2075.0 | 4800.0 | 15.0 | 23.5 |
| 2087.5 | 4800.0 | 35.1 | 43.3 |
| 2100.0 | 4800.0 | 65.0 | 55.1 |
| 2112.5 | 4800.0 | 93.0 | 57.4 |
| 2125.0 | 4800.0 | 67.2 | 47.1 |
| 2137.5 | 4800.0 | 26.9 | 29.3 |
| 2150.0 | 4800.0 | -16.5 | 3.3 |
| 2162.5 | 4800.0 | -24.1 | -15.9 |
| 2175.0 | 4800.0 | -36.9 | -26.4 |
| 2187.5 | 4800.0 | -28.9 | -28.9 |
| 2200.0 | 4800.0 | -25.7 | -27.8 |
| 2212.5 | 4800.0 | -29.1 | -22.6 |
| 2225.0 | 4800.0 | -18.4 | -16.6 |
| 2237.5 | 4800.0 | -10.8 | -11.9 |
| 2250.0 | 4800.0 | .9 | -1.8 |
| 2262.5 | 4800.0 | -2.0 | 7.5 |
| 2275.0 | 4800.0 | 21.1 | 13.0 |
| 2287.5 | 4800.0 | 28.3 | 13.9 |
| 2300.0 | 4800.0 | 16.5 | 13.1 |
| 2312.5 | 4800.0 | 5.6 | -.4 |
| 2325.0 | 4800.0 | -5.8 | -11.7 |
| 2337.5 | 4800.0 | -46.5 | -21.5 |
| 2350.0 | 4800.0 | -28.3 | -31.1 |
| 2362.5 | 4800.0 | -32.3 | -37.4 |
| 2375.0 | 4800.0 | -42.4 | -32.5 |
| 2387.5 | 4800.0 | -37.4 | -33.6 |
| 2400.0 | 4800.0 | -22.2 | -34.0 |

1.27 Line 4900 N

| 2400.0 | 4900.0 | -12.3 | -21.0 |
| :--- | :--- | :--- | :--- |
| 2387.5 | 4900.0 | -17.4 | -22.8 |
| 2375.0 | 4900.0 | -33.3 | -24.1 |
| 2362.5 | 4900.0 | -28.1 | -25.3 |
| 2350.0 | 4900.0 | -29.5 | -25.1 |
| 2337.5 | 4900.0 | -18.3 | -20.7 |
| 2325.0 | 4900.0 | -16.2 | -17.8 |
| 2312.5 | 4900.0 | -11.3 | -15.2 |
| 2300.0 | 4900.0 | -13.5 | -14.4 |
| 2287.5 | 4900.0 | -16.7 | -14.2 |
| 2275.0 | 4900.0 | -14.4 | -15.2 |
| 2262.5 | 4900.0 | -14.9 | -14.3 |


| 2250.0 | 4900.0 | -16.4 | -12.3 |
| ---: | ---: | ---: | ---: |
| 2237.5 | 4900.0 | -9.1 | -11.4 |
| 2225.0 | 4900.0 | -6.6 | -11.0 |
| 2212.5 | 4900.0 | -9.8 | -10.9 |
| 2200.0 | 4900.0 | -13.2 | -12.1 |
| 2187.5 | 4900.0 | -16.0 | -16.2 |
| 2175.0 | 4900.0 | -14.7 | -17.3 |
| 2162.5 | 4900.0 | -27.1 | -16.4 |
| 2150.0 | 4900.0 | -15.7 | -15.0 |
| 2137.5 | 4900.0 | -8.4 | -13.3 |
| 2125.0 | 4900.0 | -9.2 | -7.9 |
| 2112.5 | 4900.0 | -6.1 | -3.2 |
| 2100.0 | 4900.0 | -.3 | -1.5 |
| 2087.5 | 4900.0 | 8.1 | .6 |
| 2075.0 | 4900.0 | .0 | 2.1 |
| 2062.5 | 4900.0 | 1.1 | 2.3 |
| 2050.0 | 4900.0 | 1.8 | 1.7 |
| 2037.5 | 4900.0 | .6 | -1.1 |
| 2025.0 | 4900.0 | 5.0 | -3.8 |
| 2012.5 | 4900.0 | -13.8 | -6.1 |
| 2000.0 | 4900.0 | -12.4 | -5.9 |
| 1987.5 | 4900.0 | -9.9 | -4.6 |
| 1975.0 | 4900.0 | 1.7 | .1 |
| 1962.5 | 4900.0 | 11.3 | 5.3 |
| 1950.0 | 4900.0 | 9.8 | 11.5 |
| 1937.5 | 4900.0 | 13.5 | 17.6 |
| 1925.0 | 4900.0 | 21.0 | 21.9 |
| 1912.5 | 4900.0 | 32.5 | 25.8 |
| 1900.0 | 4900.0 | 32.5 | 28.2 |
| 1887.5 | 4900.0 | 29.3 | 28.8 |
| 1875.0 | 4900.0 | 25.7 | 28.6 |
| 1862.5 | 4900.0 | 24.0 | 25.7 |
| 1850.0 | 4900.0 | 31.6 | 25.3 |
| 1837.5 | 4900.0 | 17.7 | 25.8 |
| 1825.0 | 4900.0 | 27.4 | 25.8 |
| 1812.5 | 4900.0 | 28.4 | 23.9 |
| 1800.0 | 4900.0 | 23.9 | 26.0 |
| 1787.5 | 4900.0 | 22.3 | 21.5 |
| 1775.0 | 4900.0 | 28.1 | 15.9 |
| 1762.5 | 4900.0 | 5.0 | 12.2 |
| 1750.0 | 4900.0 | .0 | 8.0 |
| 1737.5 | 4900.0 | 5.5 | .9 |
| 1725.0 | 4900.0 | 1.2 | -2.4 |
| 1712.5 | 4900.0 | -7.6 | -1.4 |
| 1700.0 | 4900.0 | -11.3 | -.5 |
| 1687.5 | 4900.0 | 5.2 | 2.8 |
| 1675.0 | 4900.0 | 10.2 | 7.4 |
| 1662.5 | 4900.0 | 17.7 | 9.0 |
| 1650.0 | 4900.0 | 15.3 | 10.2 |
| 1637.5 | 4900.0 | -3.4 | 12.3 |
| 1625.0 | 4900.0 | 11.0 | 12.5 |
| 1612.5 | 4900.0 | 20.9 | 11.9 |
| 1600.0 | 4900.0 | 18.9 | 16.9 |


| 1600.0 | 5000.0 | 7.8 | 9.9 |
| ---: | ---: | ---: | ---: |
| 1612.5 | 5000.0 | 7.8 | 9.5 |
| 1625.0 | 5000.0 | 14.1 | 10.0 |
| 1637.5 | 5000.0 | 8.4 | 11.3 |
| 1650.0 | 5000.0 | 11.7 | 13.5 |
| 1662.5 | 5000.0 | 14.6 | 15.1 |
| 1675.0 | 5000.0 | 18.9 | 16.8 |
| 1687.5 | 5000.0 | 21.8 | 16.6 |
| 1700.0 | 5000.0 | 17.1 | 18.1 |
| 1712.5 | 5000.0 | 10.5 | 18.4 |
| 1725.0 | 5000.0 | 22.3 | 22.1 |
| 1737.5 | 5000.0 | 20.1 | 26.2 |
| 1750.0 | 5000.0 | 40.5 | 31.0 |
| 1762.5 | 5000.0 | 37.4 | 34.6 |
| 1775.0 | 5000.0 | 34.8 | 37.6 |
| 1787.5 | 5000.0 | 40.3 | 31.6 |
| 1800.0 | 5000.0 | 34.8 | 24.7 |
| 1812.5 | 5000.0 | 10.9 | 18.6 |
| 1825.0 | 5000.0 | 2.7 | 14.2 |
| 1837.5 | 5000.0 | 4.3 | 9.0 |
| 1850.0 | 5000.0 | 18.1 | 5.3 |
| 1862.5 | 5000.0 | 8.8 | 2.4 |
| 1875.0 | 5000.0 | -7.3 | .3 |
| 1887.5 | 5000.0 | -12.1 | -6.1 |
| 1900.0 | 5000.0 | -6.0 | -9.4 |
| 1912.5 | 5000.0 | -13.7 | -5.4 |
| 1925.0 | 5000.0 | -8.1 | -.2 |
| 1937.5 | 5000.0 | 12.9 | 2.4 |
| 1950.0 | 5000.0 | 13.7 | 13.9 |
| 1962.5 | 5000.0 | 7.2 | 30.9 |
| 1975.0 | 5000.0 | 43.9 | 44.7 |
| 1987.5 | 5000.0 | 77.0 | 58.5 |
| 2000.0 | 5000.0 | 81.9 | 71.5 |
| 2012.5 | 5000.0 | 82.4 | 70.6 |
| 2025.0 | 5000.0 | 72.4 | 60.6 |
| 2037.5 | 5000.0 | 39.5 | 46.8 |
| 2050.0 | 5000.0 | 26.6 | 32.2 |
| 2062.5 | 5000.0 | 13.1 | 16.9 |
| 2075.0 | 5000.0 | 9.3 | 5.5 |
| 2087.5 | 5000.0 | -4.0 | -3.4 |
| 2100.0 | 5000.0 | -17.3 | -7.1 |
| 2112.5 | 5000.0 | -18.0 | -8.4 |
| 2125.0 | 5000.0 | -5.7 | -5.7 |
| 2137.5 | 5000.0 | 3.0 | 1.0 |
| 2150.0 | 5000.0 | 9.7 | 9.8 |
| 2162.5 | 5000.0 | 16.2 | 14.7 |
| 2175.0 | 5000.0 | 25.8 | 18.6 |
| 2187.5 | 5000.0 | 18.7 | 22.6 |
| 2200.0 | 5000.0 | 22.8 | 25.2 |
| 2212.5 | 5000.0 | 29.3 | 24.8 |
| 2225.0 | 5000.0 | 29.3 | 23.7 |
|  | 50 |  |  |


| 2237.5 | 5000.0 | 23.8 | 18.7 |
| ---: | ---: | ---: | ---: |
| 2250.0 | 5000.0 | 13.2 | 10.6 |
| 2262.5 | 5000.0 | -2.0 | 2.8 |
| 2275.0 | 5000.0 | -11.3 | -3.6 |
| 2287.5 | 5000.0 | -9.5 | -9.7 |
| 2300.0 | 5000.0 | -8.2 | -12.1 |
| 2312.5 | 5000.0 | -17.7 | -12.6 |
| 2325.0 | 5000.0 | -13.9 | -14.3 |
| 2337.5 | 5000.0 | -13.9 | -16.9 |
| 2350.0 | 5000.0 | -17.7 | -17.8 |
| 2362.5 | 5000.0 | -21.4 | -19.5 |
| 2375.0 | 5000.0 | -22.0 | -23.7 |
| 2387.5 | 5000.0 | -22.4 | -25.2 |
| 2400.0 | 5000.0 | -35.0 | -26.5 |

### 1.29 Line 5100 N

| 2400.0 | 5100.0 | -30.5 | -33.5 |
| ---: | ---: | ---: | ---: |
| 2387.5 | 5100.0 | -33.8 | -33.6 |
| 2375.0 | 5100.0 | -36.3 | -31.8 |
| 2362.5 | 5100.0 | -33.9 | -2.3 |
| 2350.0 | 5100.0 | -24.3 | 60.0 |
| 2337.5 | 5100.0 | 117.0 | 82.6 |
| 2325.0 | 5100.0 | 277.5 | 96.0 |
| 2312.5 | 5100.0 | 76.9 | 101.2 |
| 2300.0 | 5100.0 | 33.1 | 79.7 |
| 2287.5 | 5100.0 | 1.3 | 25.8 |
| 2275.0 | 5100.0 | 9.9 | 9.6 |
| 2262.5 | 5100.0 | 7.9 | -.6 |
| 2250.0 | 5100.0 | -4.0 | -5.3 |
| 2237.5 | 5100.0 | -18.0 | -10.9 |
| 2225.0 | 5100.0 | -22.3 | -13.6 |
| 2212.5 | 5100.0 | -17.9 | -4.2 |
| 2200.0 | 5100.0 | -5.7 | 15.8 |
| 2187.5 | 5100.0 | 43.0 | 29.1 |
| 2175.0 | 5100.0 | 82.0 | 37.0 |
| 2162.5 | 5100.0 | 44.3 | 41.2 |
| 2150.0 | 5100.0 | 21.2 | 34.9 |
| 2137.5 | 5100.0 | 15.3 | 27.6 |
| 2125.0 | 5100.0 | 11.7 | 28.9 |
| 2112.5 | 5100.0 | 45.3 | 29.3 |
| 2100.0 | 5100.0 | 50.9 | 28.7 |
| 2087.5 | 5100.0 | 23.1 | 26.5 |
| 2075.0 | 5100.0 | 12.5 | 17.4 |
| 2062.5 | 5100.0 | .5 | 10.0 |
| 2050.0 | 5100.0 | .0 | 4.3 |
| 2037.5 | 5100.0 | 14.0 | -.2 |
| 2025.0 | 5100.0 | -5.6 | -1.5 |
| 2012.5 | 5100.0 | -9.8 | -.6 |
| 2000.0 | 5100.0 | -6.3 | -3.2 |
| 1987.5 | 5100.0 | 4.9 | -2.7 |


| 1975.0 | 5100.0 | .9 | -2.2 |
| ---: | ---: | ---: | ---: |
| 1962.5 | 5100.0 | -3.4 | -1.7 |
| 1950.0 | 5100.0 | -6.9 | -2.4 |
| 1937.5 | 5100.0 | -4.0 | -1.5 |
| 1925.0 | 5100.0 | 1.2 | 1.9 |
| 1912.5 | 5100.0 | 5.7 | 6.6 |
| 1900.0 | 5100.0 | 13.3 | 10.8 |
| 1887.5 | 5100.0 | 16.8 | 13.2 |
| 1875.0 | 5100.0 | 16.8 | 14.8 |
| 1862.5 | 5100.0 | 13.5 | 14.6 |
| 1850.0 | 5100.0 | 13.4 | 13.0 |
| 1837.5 | 5100.0 | 12.5 | 11.7 |
| 1825.0 | 5100.0 | 8.6 | 13.9 |
| 1812.5 | 5100.0 | 10.5 | 18.9 |
| 1800.0 | 5100.0 | 24.5 | 25.0 |
| 1787.5 | 5100.0 | 38.2 | 28.7 |
| 1775.0 | 5100.0 | 43.2 | 30.0 |
| 1762.5 | 5100.0 | 26.9 | 28.5 |
| 1750.0 | 5100.0 | 17.3 | 22.1 |
| 1737.5 | 5100.0 | 17.0 | 15.5 |
| 1725.0 | 5100.0 | 6.0 | 13.6 |
| 1712.5 | 5100.0 | 10.3 | 13.4 |
| 1700.0 | 5100.0 | 17.5 | 11.6 |
| 1687.5 | 5100.0 | 16.1 | 12.2 |
| 1675.0 | 5100.0 | 8.0 | 10.1 |
| 1662.5 | 5100.0 | 8.9 | 6.4 |
| 1650.0 | 5100.0 | .0 | 2.9 |
| 1637.5 | 5100.0 | -1.0 | -.4 |
| 1625.0 | 5100.0 | -1.2 | -4.0 |
| 1612.5 | 5100.0 | -8.8 | -5.1 |
| 1600.0 | 5100.0 | -9.2 | -6.4 |

1.30 Line 5200 N

| 1600.0 | 5200.0 | -11.0 | -22.0 |
| ---: | ---: | ---: | ---: |
| 1612.5 | 5200.0 | -25.5 | -22.6 |
| 1625.0 | 5200.0 | -29.5 | -20.6 |
| 1637.5 | 5200.0 | -24.6 | -19.9 |
| 1650.0 | 5200.0 | -12.3 | -14.7 |
| 1662.5 | 5200.0 | -7.4 | -7.3 |
| 1675.0 | 5200.0 | .4 | 1.3 |
| 1687.5 | 5200.0 | 7.3 | 5.5 |
| 1700.0 | 5200.0 | 18.4 | 10.1 |
| 1712.5 | 5200.0 | 8.6 | 13.2 |
| 1725.0 | 5200.0 | 16.0 | 13.1 |
| 1737.5 | 5200.0 | 15.5 | 12.7 |
| 1750.0 | 5200.0 | 7.2 | 12.3 |
| 1762.5 | 5200.0 | 16.2 | 8.2 |
| 1775.0 | 5200.0 | 6.8 | 3.0 |
| 1787.5 | 5200.0 | -4.7 | -1.6 |
| 1800.0 | 5200.0 | -10.7 | -10.8 |


| 1812.5 | 5200.0 | -15.4 | -18.7 |
| :--- | :--- | :--- | ---: |
| 1825.0 | 5200.0 | -30.0 | -23.5 |
| 1837.5 | 5200.0 | -32.5 | -26.6 |
| 1850.0 | 5200.0 | -28.9 | -26.9 |
| 1862.5 | 5200.0 | -26.1 | -24.4 |
| 1875.0 | 5200.0 | -16.9 | -22.2 |
| 1887.5 | 5200.0 | -17.7 | -20.2 |
| 1900.0 | 5200.0 | -21.2 | -18.7 |
| 1912.5 | 5200.0 | -19.3 | -22.4 |
| 1925.0 | 5200.0 | -18.5 | -24.7 |
| 1937.5 | 5200.0 | -35.5 | -25.6 |
| 1950.0 | 5200.0 | -28.9 | -26.4 |
| 1962.5 | 5200.0 | -26.0 | -28.0 |
| 1975.0 | 5200.0 | -23.1 | -26.6 |
| 1987.5 | 5200.0 | -26.7 | -25.7 |
| 2000.0 | 5200.0 | -28.2 | -26.6 |
| 2012.5 | 5200.0 | -24.7 | -28.6 |
| 2025.0 | 5200.0 | -30.2 | -30.2 |
| 2037.5 | 5200.0 | -33.2 | -33.4 |
| 2050.0 | 5200.0 | -34.6 | -33.7 |
| 2062.5 | 5200.0 | -44.1 | -32.0 |
| 2075.0 | 5200.0 | -26.4 | -32.2 |
| 2087.5 | 5200.0 | -21.9 | -30.6 |
| 2100.0 | 5200.0 | -34.2 | -28.2 |
| 2112.5 | 5200.0 | -26.2 | -33.5 |
| 2125.0 | 5200.0 | -32.4 | -37.3 |
| 2137.5 | 5200.0 | -52.6 | -37.2 |
| 2150.0 | 5200.0 | -41.3 | -39.0 |
| 2162.5 | 5200.0 | -33.5 | -38.8 |
| 2175.0 | 5200.0 | -35.0 | -33.7 |
| 2187.5 | 5200.0 | -31.6 | -30.7 |
| 2200.0 | 5200.0 | -26.9 | -27.3 |
| 2212.5 | 5200.0 | -26.4 | -22.8 |
| 2225.0 | 5200.0 | -16.8 | -19.7 |
| 2237.5 | 5200.0 | -12.2 | 31.6 |
| 2250.0 | 5200.0 | -16.4 | 39.9 |
| 2262.5 | 5200.0 | 229.9 | 48.2 |
| 2275.0 | 5200.0 | 14.8 | 56.9 |
| 2287.5 | 5200.0 | 24.7 | 67.2 |
| 2300.0 | 5200.0 | 31.5 | 22.3 |
| 2312.5 | 5200.0 | 35.1 | 19.3 |
| 2325.0 | 5200.0 | 5.5 | 13.3 |
| 2337.5 | 5200.0 | -.5 | 3.7 |
| 2350.0 | 5200.0 | -5.3 | -6.8 |
| 2362.5 | 5200.0 | -16.5 | -11.3 |
| 2375.0 | 5200.0 | -17.4 | -16.5 |
| 2387.5 | 5200.0 | -17.0 | -19.3 |
| 2400.0 | 5200.0 | -26.4 | -20.3 |
|  |  |  |  |

1.31 Line 5300 N

| 2400.0 | 5300.0 | -50.9 | -36.4 |
| ---: | ---: | ---: | ---: |
| 2387.5 | 5300.0 | -35.6 | -31.7 |
| 2375.0 | 5300.0 | -22.7 | -28.5 |
| 2362.5 | 5300.0 | -17.7 | -20.5 |
| 2350.0 | 5300.0 | -15.4 | -14.6 |
| 2337.5 | 5300.0 | -11.1 | -10.8 |
| 2325.0 | 5300.0 | -6.3 | -7.8 |
| 2312.5 | 5300.0 | -3.5 | -3.9 |
| 2300.0 | 5300.0 | -2.8 | -.5 |
| 2287.5 | 5300.0 | 4.3 | 1.4 |
| 2275.0 | 5300.0 | 5.8 | 1.1 |
| 2262.5 | 5300.0 | 3.0 | -2.4 |
| 2250.0 | 5300.0 | -4.6 | -3.4 |
| 2237.5 | 5300.0 | -20.4 | 18.9 |
| 2225.0 | 5300.0 | -.6 | 32.4 |
| 2212.5 | 5300.0 | 117.3 | 64.7 |
| 2200.0 | 5300.0 | 70.4 | 96.2 |
| 2187.5 | 5300.0 | 156.6 | 86.8 |
| 2175.0 | 5300.0 | 137.1 | 54.2 |
| 2162.5 | 5300.0 | -47.6 | 31.3 |
| 2150.0 | 5300.0 | -45.7 | -8.3 |
| 2137.5 | 5300.0 | -44.0 | -44.0 |
| 2125.0 | 5300.0 | -41.5 | -42.7 |
| 2112.5 | 5300.0 | -41.1 | -43.1 |
| 2100.0 | 5300.0 | -41.4 | -39.7 |
| 2087.5 | 5300.0 | -47.3 | -37.0 |
| 2075.0 | 5300.0 | -27.0 | -32.8 |
| 2062.5 | 5300.0 | -28.4 | -26.4 |
| 2050.0 | 5300.0 | -20.1 | -26.3 |
| 2037.5 | 5300.0 | -9.1 | -25.9 |
| 2025.0 | 5300.0 | -47.0 | -26.5 |
| 2012.5 | 5300.0 | -25.0 | -28.2 |
| 2000.0 | 5300.0 | -31.5 | -32.2 |
| 1987.5 | 5300.0 | -28.6 | -28.7 |
| 1975.0 | 5300.0 | -28.8 | -28.2 |
| 1962.5 | 5300.0 | -29.4 | -26.5 |
| 1950.0 | 5300.0 | -22.9 | -24.7 |
| 1937.5 | 5300.0 | -22.6 | -22.9 |
| 1925.0 | 5300.0 | -19.8 | -20.1 |
| 1912.5 | 5300.0 | -19.9 | -19.3 |
| 1900.0 | 5300.0 | -15.4 | -16.0 |
| 1887.5 | 5300.0 | -18.6 | -11.7 |
| 1875.0 | 5300.0 | -6.2 | -7.6 |
| 1862.5 | 5300.0 | 1.4 | -7.3 |
| 1850.0 | 5300.0 | 1.0 | -5.8 |
| 1837.5 | 5300.0 | -13.9 | -7.0 |
| 1825.0 | 5300.0 | -11.3 | -11.1 |
| 1812.5 | 5300.0 | -12.4 | -14.1 |
| 1800.0 | 5300.0 | -18.8 | -14.6 |
| 1787.5 | 5300.0 | -14.0 | -16.7 |
|  |  |  |  |


| 1775.0 | 5300.0 | -16.4 | -18.2 |
| ---: | ---: | ---: | ---: |
| 1762.5 | 5300.0 | -21.7 | -16.1 |
| 1750.0 | 5300.0 | -20.1 | -17.1 |
| 1737.5 | 5300.0 | -8.5 | -17.1 |
| 1725.0 | 5300.0 | -19.0 | -17.1 |
| 1712.5 | 5300.0 | -16.4 | -16.0 |
| 1700.0 | 5300.0 | -21.4 | -16.5 |
| 1687.5 | 5300.0 | -14.7 | -15.4 |
| 1675.0 | 5300.0 | -11.2 | -13.6 |
| 1662.5 | 5300.0 | -13.1 | -15.5 |
| 1650.0 | 5300.0 | -7.8 | -19.1 |
| 1637.5 | 5300.0 | -30.5 | -20.3 |
| 1625.0 | 5300.0 | -32.7 | -21.0 |
| 1612.5 | 5300.0 | -17.3 | -24.3 |
| 1600.0 | 5300.0 | -16.8 | -22.3 |

1.32 Line 5400 N

| 1600.0 | 5400.0 | 6.3 | -6.6 |
| ---: | ---: | ---: | ---: |
| 1612.5 | 5400.0 | -13.6 | -6.8 |
| 1625.0 | 5400.0 | -12.4 | -8.1 |
| 1637.5 | 5400.0 | -7.6 | -11.5 |
| 1650.0 | 5400.0 | -13.4 | -11.2 |
| 1662.5 | 5400.0 | -10.3 | -11.2 |
| 1675.0 | 5400.0 | -12.1 | -11.7 |
| 1687.5 | 5400.0 | -12.4 | -10.7 |
| 1700.0 | 5400.0 | -10.4 | -10.4 |
| 1712.5 | 5400.0 | -8.4 | -8.7 |
| 1725.0 | 5400.0 | -8.9 | -7.4 |
| 1737.5 | 5400.0 | -3.6 | -6.2 |
| 1750.0 | 5400.0 | -5.7 | -5.5 |
| 1762.5 | 5400.0 | -4.3 | -5.0 |
| 1775.0 | 5400.0 | -5.1 | -5.1 |
| 1787.5 | 5400.0 | -6.1 | -5.9 |
| 1800.0 | 5400.0 | -4.3 | -9.0 |
| 1812.5 | 5400.0 | -9.9 | -14.8 |
| 1825.0 | 5400.0 | -19.8 | -25.5 |
| 1837.5 | 5400.0 | -34.0 | -42.3 |
| 1850.0 | 5400.0 | -59.7 | -65.5 |
| 1862.5 | 5400.0 | -88.1 | -89.2 |
| 1875.0 | 5400.0 | -126.1 | -93.6 |
| 1887.5 | 5400.0 | -138.1 | 8.2 |
| 1900.0 | 5400.0 | -55.9 | 8.8 |
| 1912.5 | 5400.0 | 449.2 | 23.0 |
| 1925.0 | 5400.0 | -85.1 | 47.8 |
| 1937.5 | 5400.0 | -55.3 | 55.9 |
| 1950.0 | 5400.0 | -13.8 | -33.4 |
| 1962.5 | 5400.0 | -15.6 | -10.4 |
| 1975.0 | 5400.0 | 2.8 | 15.2 |
| 1987.5 | 5400.0 | 30.1 | 24.8 |
| 2000.0 | 5400.0 | 72.5 | 25.3 |


| 2012.5 | 5400.0 | 34.4 | 18.0 |
| ---: | ---: | ---: | ---: |
| 2025.0 | 5400.0 | -13.1 | -1.3 |
| 2037.5 | 5400.0 | -33.8 | 15.0 |
| 2050.0 | 5400.0 | -66.7 | 20.5 |
| 2062.5 | 5400.0 | 154.0 | 32.5 |
| 2075.0 | 5400.0 | 62.2 | 52.0 |
| 2087.5 | 5400.0 | 46.8 | 79.1 |
| 2100.0 | 5400.0 | 63.8 | 64.2 |
| 2112.5 | 5400.0 | 68.9 | 68.1 |
| 2125.0 | 5400.0 | 79.2 | 74.3 |
| 2137.5 | 5400.0 | 81.8 | 75.2 |
| 2150.0 | 5400.0 | 77.6 | 72.7 |
| 2162.5 | 5400.0 | 68.4 | 65.2 |
| 2175.0 | 5400.0 | 56.6 | 53.7 |
| 2187.5 | 5400.0 | 41.4 | 42.1 |
| 2200.0 | 5400.0 | 24.7 | 31.1 |
| 2212.5 | 5400.0 | 19.5 | 22.2 |
| 2225.0 | 5400.0 | 13.4 | 15.5 |
| 2237.5 | 5400.0 | 12.0 | 11.6 |
| 2250.0 | 5400.0 | 7.7 | 8.3 |
| 2262.5 | 5400.0 | 5.5 | 10.9 |
| 2275.0 | 5400.0 | 3.1 | 12.8 |
| 2287.5 | 5400.0 | 26.2 | 16.0 |
| 2300.0 | 5400.0 | 21.5 | 17.9 |
| 2312.5 | 5400.0 | 23.7 | 19.5 |
| 2325.0 | 5400.0 | 15.0 | 16.1 |
| 2337.5 | 5400.0 | 11.2 | 12.9 |
| 2350.0 | 5400.0 | 8.9 | 10.2 |
| 2362.5 | 5400.0 | 5.8 | 9.0 |
| 2375.0 | 5400.0 | 10.0 | 9.2 |
| 2387.5 | 5400.0 | 9.1 | 9.3 |
| 2400.0 | 5400.0 | 12.4 | 10.5 |

### 1.33 Line 5500 N

| 2400.0 | 5500.0 | 16.1 | 16.0 |
| ---: | ---: | ---: | ---: |
| 2387.5 | 5500.0 | 16.2 | 14.1 |
| 2375.0 | 5500.0 | 15.8 | 12.7 |
| 2362.5 | 5500.0 | 8.2 | 10.5 |
| 2350.0 | 5500.0 | 7.1 | 8.1 |
| 2337.5 | 5500.0 | 5.3 | 6.8 |
| 2325.0 | 5500.0 | 3.9 | 6.3 |
| 2312.5 | 5500.0 | 9.4 | 6.2 |
| 2300.0 | 5500.0 | 5.6 | 8.4 |
| 2287.5 | 5500.0 | 7.0 | 15.5 |
| 2275.0 | 5500.0 | 16.1 | 25.6 |
| 2262.5 | 5500.0 | 39.3 | 28.4 |
| 2250.0 | 5500.0 | 60.2 | 31.6 |
| 2237.5 | 5500.0 | 19.5 | 32.7 |
| 2225.0 | 5500.0 | 23.0 | 29.7 |
| 2212.5 | 5500.0 | 21.5 | 23.9 |


| 2200.0 | 5500.0 | 24.4 | 27.6 |
| ---: | ---: | ---: | ---: |
| 2187.5 | 5500.0 | 31.3 | 30.9 |
| 2175.0 | 5500.0 | 37.6 | 35.4 |
| 2162.5 | 5500.0 | 39.8 | 39.6 |
| 2150.0 | 5500.0 | 43.7 | 42.1 |
| 2137.5 | 5500.0 | 45.6 | 42.7 |
| 2125.0 | 5500.0 | 43.9 | 41.4 |
| 2112.5 | 5500.0 | 40.6 | 37.8 |
| 2100.0 | 5500.0 | 33.2 | 32.8 |
| 2087.5 | 5500.0 | 25.9 | 27.1 |
| 2075.0 | 5500.0 | 20.5 | 22.1 |
| 2062.5 | 5500.0 | 15.5 | 18.6 |
| 2050.0 | 5500.0 | 15.2 | 17.7 |
| 2037.5 | 5500.0 | 16.1 | 18.4 |
| 2025.0 | 5500.0 | 21.2 | 20.3 |
| 2012.5 | 5500.0 | 24.0 | 23.8 |
| 2000.0 | 5500.0 | 25.1 | 26.9 |
| 1987.5 | 5500.0 | 32.5 | 29.8 |
| 1975.0 | 5500.0 | 31.5 | 33.4 |
| 1962.5 | 5500.0 | 35.7 | 39.5 |
| 1950.0 | 5500.0 | 42.1 | 45.2 |
| 1937.5 | 5500.0 | 55.7 | 50.7 |
| 1925.0 | 5500.0 | 60.9 | 56.5 |
| 1912.5 | 5500.0 | 59.2 | 67.8 |
| 1900.0 | 5500.0 | 64.6 | 86.0 |
| 1887.5 | 5500.0 | 98.5 | 114.3 |
| 1875.0 | 5500.0 | 147.0 | 158.1 |
| 1862.5 | 5500.0 | 202.4 | 210.6 |
| 1850.0 | 5500.0 | 278.1 | 245.7 |
| 1837.5 | 5500.0 | 327.1 | 249.1 |
| 1825.0 | 5500.0 | 273.9 | 229.3 |
| 1812.5 | 5500.0 | 164.1 | 187.0 |
| 1800.0 | 5500.0 | 103.2 | 131.4 |
| 1787.5 | 5500.0 | 66.8 | 84.6 |
| 1775.0 | 5500.0 | 49.2 | 57.4 |
| 1762.5 | 5500.0 | 39.7 | 40.4 |
| 1750.0 | 5500.0 | 28.1 | 30.0 |
| 1737.5 | 5500.0 | 18.1 | 22.1 |
| 1725.0 | 5500.0 | 15.1 | 17.2 |
| 1712.5 | 5500.0 | 9.3 | 12.3 |
| 1700.0 | 5500.0 | 15.4 | 9.8 |
| 1687.5 | 5500.0 | 3.8 | 7.2 |
| 1675.0 | 5500.0 | 5.6 | 5.5 |
| 1662.5 | 5500.0 | 1.9 | 2.9 |
| 1650.0 | 5500.0 | 2.9 | 1.6 |
| 1637.5 | 5500.0 | 2.1 | .9 |
| 1625.0 | 5500.0 | -2.3 | .0 |
| 1612.5 | 5500.0 | 1.8 | -.2 |
| 1600.0 | 5500.0 | -2.3 | -.9 |
|  |  |  |  |

### 1.34 Line 5600 N

| 1600.0 | 5600.0 | 11.6 | 16.4 |
| ---: | ---: | ---: | ---: |
| 1612.5 | 5600.0 | 13.5 | 20.2 |
| 1625.0 | 5600.0 | 24.2 | 23.0 |
| 1637.5 | 5600.0 | 31.4 | 30.0 |
| 1650.0 | 5600.0 | 34.3 | 38.1 |
| 1662.5 | 5600.0 | 46.7 | 45.2 |
| 1675.0 | 5600.0 | 53.7 | 53.4 |
| 1687.5 | 5600.0 | 59.7 | 64.6 |
| 1700.0 | 5600.0 | 72.7 | 76.0 |
| 1712.5 | 5600.0 | 90.0 | 88.1 |
| 1725.0 | 5600.0 | 103.7 | 98.8 |
| 1737.5 | 5600.0 | 114.5 | 106.5 |
| 1750.0 | 5600.0 | 113.1 | 107.7 |
| 1762.5 | 5600.0 | 111.0 | 103.3 |
| 1775.0 | 5600.0 | 96.0 | 93.9 |
| 1787.5 | 5600.0 | 82.1 | 85.5 |
| 1800.0 | 5600.0 | 67.4 | 75.3 |
| 1812.5 | 5600.0 | 71.0 | 65.5 |
| 1825.0 | 5600.0 | 59.8 | 56.2 |
| 1837.5 | 5600.0 | 47.0 | 49.0 |
| 1850.0 | 5600.0 | 35.9 | 39.7 |
| 1862.5 | 5600.0 | 31.2 | 31.9 |
| 1875.0 | 5600.0 | 24.7 | 26.6 |
| 1887.5 | 5600.0 | 20.8 | 23.7 |
| 1900.0 | 5600.0 | 20.6 | 21.9 |
| 1912.5 | 5600.0 | 21.0 | 22.1 |
| 1925.0 | 5600.0 | 22.5 | 22.2 |
| 1937.5 | 5600.0 | 25.7 | 20.4 |
| 1950.0 | 5600.0 | 21.2 | 17.6 |
| 1962.5 | 5600.0 | 11.5 | 14.7 |
| 1975.0 | 5600.0 | 7.0 | 11.5 |
| 1987.5 | 5600.0 | 8.0 | 9.2 |
| 2000.0 | 5600.0 | 9.7 | 8.3 |
| 2012.5 | 5600.0 | 9.8 | 8.8 |
| 2025.0 | 5600.0 | 7.0 | 9.0 |
| 2037.5 | 5600.0 | 9.5 | 9.5 |
| 2050.0 | 5600.0 | 9.2 | 10.5 |
| 2062.5 | 5600.0 | 11.9 | 12.2 |
| 2075.0 | 5600.0 | 14.9 | 13.7 |
| 2087.5 | 5600.0 | 15.4 | 15.9 |
| 2100.0 | 5600.0 | 17.3 | 17.7 |
| 2112.5 | 5600.0 | 19.8 | 19.3 |
| 2125.0 | 5600.0 | 21.1 | 20.9 |
| 2137.5 | 5600.0 | 22.8 | 23.9 |
| 2150.0 | 5600.0 | 23.7 | 26.2 |
| 2162.5 | 5600.0 | 32.2 | 29.2 |
| 2175.0 | 5600.0 | 31.2 | 32.0 |
| 2187.5 | 5600.0 | 35.9 | 30.1 |
| 2200.0 | 5600.0 | 37.2 | 27.3 |
| 2212.5 | 5600.0 | 14.2 | 31.4 |
| 2225.0 | 5600.0 | 17.8 | 41.4 |
|  |  |  |  |


| 2237.5 | 5600.0 | 52.1 | 46.3 |
| ---: | ---: | ---: | ---: |
| 2250.0 | 5600.0 | 85.6 | 49.9 |
| 2262.5 | 5600.0 | 61.6 | 50.1 |
| 2275.0 | 5600.0 | 32.5 | 42.4 |
| 2287.5 | 5600.0 | 18.8 | 27.4 |
| 2300.0 | 5600.0 | 13.3 | 18.3 |
| 2312.5 | 5600.0 | 10.7 | 14.4 |
| 2325.0 | 5600.0 | 16.1 | 13.3 |
| 2337.5 | 5600.0 | 13.2 | 12.8 |
| 2350.0 | 5600.0 | 13.1 | 11.8 |
| 2362.5 | 5600.0 | 11.0 | 9.5 |
| 2375.0 | 5600.0 | 5.8 | 9.6 |
| 2387.5 | 5600.0 | 4.6 | 8.8 |
| 2400.0 | 5600.0 | 13.6 | 8.0 |


| 1.35 Lin | 5700N |  |  |
| :---: | :---: | :---: | :---: |
| 2400.0 | 5700.0 | 38.2 | 35.1 |
| 2387.5 | 5700.0 | 32.5 | 32.9 |
| 2375.0 | 5700.0 | 34.6 | 33.1 |
| 2362.5 | 5700.0 | 26.4 | 33.5 |
| 2350.0 | 5700.0 | 33.7 | 34.1 |
| 2337.5 | 5700.0 | 40.4 | 31.6 |
| 2325.0 | 5700.0 | 35.5 | 29.0 |
| 2312.5 | 5700.0 | 22.2 | 24.6 |
| 2300.0 | 5700.0 | 13.3 | 19.2 |
| 2287.5 | 5700.0 | 11.8 | 13.3 |
| 2275.0 | 5700.0 | 13.4 | 9.9 |
| 2262.5 | 5700.0 | 5.7 | 8.4 |
| 2250.0 | 5700.0 | 5.2 | 10.4 |
| 2237.5 | 5700.0 | 5.9 | 10.4 |
| 2225.0 | 5700.0 | 21.7 | 9.7 |
| 2212.5 | 5700.0 | 13.4 | 7.7 |
| 2200.0 | 5700.0 | 2.4 | 11.5 |
| 2187.5 | 5700.0 | -4.8 | 11.8 |
| 2175.0 | 5700.0 | 24.7 | 11.9 |
| 2162.5 | 5700.0 | 23.5 | 14.7 |
| 2150.0 | 5700.0 | 13.5 | 18.3 |
| 2137.5 | 5700.0 | 16.8 | 16.0 |
| 2125.0 | 5700.0 | 13.0 | 14.3 |
| 2112.5 | 5700.0 | 13.2 | 13.7 |
| 2100.0 | 5700.0 | 15.2 | 12.7 |
| 2087.5 | 5700.0 | 10.4 | 12.4 |
| 2075.0 | 5700.0 | 11.8 | 11.2 |
| 2062.5 | 5700.0 | 11.3 | 9.4 |
| 2050.0 | 5700.0 | 7.1 | 8.5 |
| 2037.5 | 5700.0 | 6.2 | 7.3 |
| 2025.0 | 5700.0 | 6.3 | 7.0 |
| 2012.5 | 5700.0 | 5.7 | 6.8 |
| 2000.0 | 5700.0 | 9.8 | 6.9 |
| 1987.5 | 5700.0 | 5.9 | 7.4 |


| 1975.0 | 5700.0 | 6.9 | 7.5 |
| ---: | ---: | ---: | ---: |
| 1962.5 | 5700.0 | 8.5 | 7.8 |
| 1950.0 | 5700.0 | 6.6 | 9.4 |
| 1937.5 | 5700.0 | 11.3 | 10.4 |
| 1925.0 | 5700.0 | 13.7 | 12.0 |
| 1912.5 | 5700.0 | 11.8 | 14.1 |
| 1900.0 | 5700.0 | 16.8 | 15.0 |
| 1887.5 | 5700.0 | 16.9 | 16.7 |
| 1875.0 | 5700.0 | 15.9 | 18.4 |
| 1862.5 | 5700.0 | 21.9 | 20.6 |
| 1850.0 | 5700.0 | 20.4 | 24.5 |
| 1837.5 | 5700.0 | 27.7 | 29.6 |
| 1825.0 | 5700.0 | 36.7 | 34.3 |
| 1812.5 | 5700.0 | 41.5 | 41.4 |
| 1800.0 | 5700.0 | 45.0 | 48.3 |
| 1787.5 | 5700.0 | 56.3 | 55.6 |
| 1775.0 | 5700.0 | 61.8 | 66.4 |
| 1762.5 | 5700.0 | 73.4 | 78.9 |
| 1750.0 | 5700.0 | 95.3 | 92.3 |
| 1737.5 | 5700.0 | 107.5 | 110.7 |
| 1725.0 | 5700.0 | 123.6 | 127.5 |
| 1712.5 | 5700.0 | 153.9 | 141.5 |
| 1700.0 | 5700.0 | 157.2 | 154.5 |
| 1687.5 | 5700.0 | 165.1 | 162.6 |
| 1675.0 | 5700.0 | 172.8 | 162.2 |
| 1662.5 | 5700.0 | 164.1 | 157.0 |
| 1650.0 | 5700.0 | 151.8 | 147.4 |
| 1637.5 | 5700.0 | 131.4 | 131.2 |
| 1625.0 | 5700.0 | 117.0 | 113.4 |
| 1612.5 | 5700.0 | 91.7 | 103.8 |
| 1600.0 | 5700.0 | 75.1 | 94.6 |

1.36 Line 5800 N

| 1600.0 | 5800.0 | 122.2 | 120.2 |
| ---: | ---: | ---: | ---: |
| 1612.5 | 5800.0 | 115.9 | 123.6 |
| 1625.0 | 5800.0 | 122.5 | 125.4 |
| 1637.5 | 5800.0 | 133.8 | 125.7 |
| 1650.0 | 5800.0 | 132.8 | 126.9 |
| 1662.5 | 5800.0 | 123.6 | 124.9 |
| 1675.0 | 5800.0 | 121.8 | 119.4 |
| 1687.5 | 5800.0 | 112.3 | 111.4 |
| 1700.0 | 5800.0 | 106.5 | 102.7 |
| 1712.5 | 5800.0 | 92.7 | 92.4 |
| 1725.0 | 5800.0 | 80.2 | 82.4 |
| 1737.5 | 5800.0 | 70.3 | 72.2 |
| 1750.0 | 5800.0 | 62.3 | 63.3 |
| 1762.5 | 5800.0 | 55.7 | 55.3 |
| 1775.0 | 5800.0 | 47.8 | 47.4 |
| 1787.5 | 5800.0 | 40.4 | 40.4 |
| 1800.0 | 5800.0 | 30.7 | 33.7 |


| 1812.5 | 5800.0 | 27.6 | 27.6 |
| :---: | :---: | :---: | :---: |
| 1825.0 | 5800.0 | 22.1 | 23.0 |
| 1837.5 | 5800.0 | 17.4 | 19.9 |
| 1850.0 | 5800.0 | 17.1 | 17.6 |
| 1862.5 | 5800.0 | 15.2 | 16.1 |
| 1875.0 | 5800.0 | 16.3 | 14.8 |
| 1887.5 | 5800.0 | 14.5 | 13.0 |
| 1900.0 | 5800.0 | 11.0 | 11.8 |
| 1912.5 | 5800.0 | 8.2 | 9.7 |
| 1925.0 | 5800.0 | 9.1 | 8.3 |
| 1937.5 | 5800.0 | 5.8 | 7.8 |
| 1950.0 | 5800.0 | 7.6 | 7.3 |
| 1962.5 | 5800.0 | 8.5 | 5.5 |
| 1975.0 | 5800.0 | 5.4 | 4.6 |
| 1987.5 | 5800.0 | . 3 | 5.2 |
| 2000.0 | 5800.0 | 1.3 | 7.0 |
| 2012.5 | 5800.0 | 10.6 | 7.0 |
| 2025.0 | 5800.0 | 17.4 | 7.4 |
| 2037.5 | 5800.0 | 5.4 | 6.9 |
| 2050.0 | 5800.0 | 2.5 | 4.4 |
| 2062.5 | 5800.0 | -1.3 | 1.9 |
| 2075.0 | 5800.0 | -2.0 | 4.4 |
| 2087.5 | 5800.0 | 5.0 | 4.8 |
| 2100.0 | 5800.0 | 17.6 | 6.5 |
| 2112.5 | 5800.0 | 4.8 | 8.1 |
| 2125.0 | 5800.0 | 7.0 | 8.6 |
| 2137.5 | 5800.0 | 6.2 | 7.6 |
| 2150.0 | 5800.0 | 7.3 | 12.2 |
| 2162.5 | 5800.0 | 12.8 | 19.3 |
| 2175.0 | 5800.0 | 27.9 | 26.3 |
| 2187.5 | 5800.0 | 42.3 | 28.3 |
| 2200.0 | 5800.0 | 41.0 | 30.7 |
| 2212.5 | 5800.0 | 17.4 | 28.8 |
| 2225.0 | 5800.0 | 25.1 | 24.4 |
| 2237.5 | 5800.0 | 18.3 | 18.2 |
| 2250.0 | 5800.0 | 20.0 | 15.8 |
| 2262.5 | 5800.0 | 10.2 | 12.5 |
| 2275.0 | 5800.0 | 5.5 | 10.8 |
| 2287.5 | 5800.0 | 8.5 | 8.8 |
| 2300.0 | 5800.0 | 9.9 | 9.9 |
| 2312.5 | 5800.0 | 10.0 | 16.5 |
| 2325.0 | 5800.0 | 15.6 | 23.6 |
| 2337.5 | 5800.0 | 38.7 | 31.6 |
| 2350.0 | 5800.0 | 43.8 | 42.3 |
| 2362.5 | 5800.0 | 50.0 | 52.7 |
| 2375.0 | 5800.0 | 63.3 | 58.8 |
| 2387.5 | 5800.0 | 67.8 | 62.6 |
| 2400.0 | 5800.0 | 69.1 | 66.7 |

### 1.37 Line <br> 5900N

| 2400.0 | 5900.0 | .5 | 1.5 |
| ---: | ---: | ---: | ---: |
| 2387.5 | 5900.0 | 1.4 | 2.9 |
| 2375.0 | 5900.0 | 2.7 | 3.6 |
| 2362.5 | 5900.0 | 7.0 | 7.0 |
| 2350.0 | 5900.0 | 6.4 | 9.3 |
| 2337.5 | 5900.0 | 17.7 | 11.2 |
| 2325.0 | 5900.0 | 12.9 | 12.4 |
| 2312.5 | 5900.0 | 11.9 | 13.3 |
| 2300.0 | 5900.0 | 13.2 | 11.8 |
| 2287.5 | 5900.0 | 11.0 | 10.9 |
| 2275.0 | 5900.0 | 10.1 | 9.3 |
| 2262.5 | 5900.0 | 8.5 | 7.2 |
| 2250.0 | 5900.0 | 3.9 | 7.3 |
| 2237.5 | 5900.0 | 2.3 | 5.8 |
| 2225.0 | 5900.0 | 11.6 | 5.0 |
| 2212.5 | 5900.0 | 2.9 | 3.0 |
| 2200.0 | 5900.0 | 4.2 | 1.6 |
| 2187.5 | 5900.0 | -5.9 | .2 |
| 2175.0 | 5900.0 | -4.6 | -.1 |
| 2162.5 | 5900.0 | 4.4 | -.2 |
| 2150.0 | 5900.0 | 1.6 | 1.8 |
| 2137.5 | 5900.0 | 3.4 | 2.3 |
| 2125.0 | 5900.0 | 4.0 | .2 |
| 2112.5 | 5900.0 | -1.9 | -.1 |
| 2100.0 | 5900.0 | -6.3 | 1.0 |
| 2087.5 | 5900.0 | .3 | 1.9 |
| 2075.0 | 5900.0 | 9.1 | 2.4 |
| 2062.5 | 5900.0 | 8.5 | 5.1 |
| 2050.0 | 5900.0 | .4 | 7.1 |
| 2037.5 | 5900.0 | 7.2 | 6.2 |
| 2025.0 | 5900.0 | 10.4 | 5.9 |
| 2012.5 | 5900.0 | 4.7 | 6.5 |
| 2000.0 | 5900.0 | 6.7 | 6.1 |
| 1987.5 | 5900.0 | 3.5 | 5.1 |
| 1975.0 | 5900.0 | 5.3 | 5.4 |
| 1962.5 | 5900.0 | 5.1 | 5.8 |
| 1950.0 | 5900.0 | 6.5 | 6.9 |
| 1937.5 | 5900.0 | 8.7 | 8.3 |
| 1925.0 | 5900.0 | 8.9 | 9.5 |
| 1912.5 | 5900.0 | 12.2 | 10.9 |
| 1900.0 | 5900.0 | 11.4 | 12.3 |
| 1887.5 | 5900.0 | 13.4 | 15.0 |
| 1875.0 | 5900.0 | 15.7 | 17.0 |
| 1862.5 | 5900.0 | 22.1 | 18.5 |
| 1850.0 | 5900.0 | 22.4 | 22.1 |
| 1837.5 | 5900.0 | 18.7 | 25.0 |
| 1825.0 | 5900.0 | 31.8 | 26.7 |
| 1812.5 | 5900.0 | 30.0 | 28.8 |
| 1800.0 | 5900.0 | 30.4 | 32.1 |
| 1787.5 | 5900.0 | 33.2 | 33.5 |
|  |  |  |  |


| 1775.0 | 5900.0 | 35.1 | 35.8 |
| :--- | :--- | :--- | :--- |
| 1762.5 | 5900.0 | 38.8 | 38.6 |
| 1750.0 | 5900.0 | 41.5 | 41.5 |
| 1737.5 | 5900.0 | 44.3 | 45.6 |
| 1725.0 | 5900.0 | 48.0 | 50.6 |
| 1712.5 | 5900.0 | 55.2 | 55.8 |
| 1700.0 | 5900.0 | 64.1 | 61.2 |
| 1687.5 | 5900.0 | 67.2 | 67.0 |
| 1675.0 | 5900.0 | 71.7 | 72.1 |
| 1662.5 | 5900.0 | 76.7 | 76.9 |
| 1650.0 | 5900.0 | 80.8 | 81.5 |
| 1637.5 | 5900.0 | 87.9 | 86.0 |
| 1625.0 | 5900.0 | 90.3 | 90.5 |
| 1612.5 | 5900.0 | 94.1 | 93.0 |
| 1600.0 | 5900.0 | 99.5 | 94.6 |

## 2. NORTH - SOUTH LINES

2.1 Line 1700 E

| Station <br> N | Line <br> $E$ | Original <br> Readings |  |
| :---: | :---: | :---: | :---: |
| - |  |  |  |
| 2200.0 | 1700.0 | -7.6 | -8.4 |
| 2212.5 | 1700.0 | -20.5 | -3.0 |
| 2225.0 | 1700.0 | 3.0 | 2.5 |
| 2237.5 | 1700.0 | 13.2 | 1.5 |
| 2250.0 | 1700.0 | 24.5 | -11.2 |
| 2262.5 | 1700.0 | -12.5 | -32.5 |
| 2275.0 | 1700.0 | -84.3 | -55.6 |
| 2287.5 | 1700.0 | -103.6 | -79.2 |
| 2300.0 | 1700.0 | -102.3 | -94.5 |
| 2312.5 | 1700.0 | -93.5 | -94.7 |
| 2325.0 | 1700.0 | -88.8 | -90.0 |
| 2337.5 | 1700.0 | -85.3 | -85.2 |
| 2350.0 | 1700.0 | -80.3 | -81.4 |
| 2362.5 | 1700.0 | -78.3 | -78.5 |
| 2375.0 | 1700.0 | -74.5 | -76.1 |
| 2387.5 | 1700.0 | -74.3 | -72.9 |
| 2400.0 | 1700.0 | -73.2 | -70.4 |
| 2412.5 | 1700.0 | -64.0 | -68.8 |
| 2425.0 | 1700.0 | -65.8 | -66.9 |
| 2437.5 | 1700.0 | -66.7 | -65.0 |
| 2450.0 | 1700.0 | -64.6 | -64.0 |
| 2462.5 | 1700.0 | -64.1 | -62.4 |
| 2475.0 | 1700.0 | -58.6 | -61.3 |
| 2487.5 | 1700.0 | -57.8 | -59.1 |
| 2500.0 | 1700.0 | -61.2 | -57.1 |
| 2512.5 | 1700.0 | -54.0 | -54.7 |


| 2525.0 | 1700.0 | -53.9 | -52.2 |
| ---: | ---: | ---: | ---: |
| 2537.5 | 1700.0 | -46.6 | -49.3 |
| 2550.0 | 1700.0 | -45.5 | -47.7 |
| 2562.5 | 1700.0 | -46.6 | -45.4 |
| 2575.0 | 1700.0 | -45.9 | -44.6 |
| 2587.5 | 1700.0 | -42.6 | -43.8 |
| 2600.0 | 1700.0 | -42.3 | -42.7 |
| 2612.5 | 1700.0 | -41.4 | -40.9 |
| 2625.0 | 1700.0 | -41.2 | -39.8 |
| 2637.5 | 1700.0 | -36.9 | -38.8 |
| 2650.0 | 1700.0 | -37.2 | -37.2 |
| 2662.5 | 1700.0 | -37.1 | -34.7 |
| 2675.0 | 1700.0 | -33.8 | -32.8 |
| 2687.5 | 1700.0 | -28.7 | -31.0 |
| 2700.0 | 1700.0 | -27.2 | -28.2 |
| 2712.5 | 1700.0 | -28.3 | -25.4 |
| 2725.0 | 1700.0 | -23.0 | -22.7 |
| 2737.5 | 1700.0 | -19.7 | -20.0 |
| 2750.0 | 1700.0 | -15.5 | -18.0 |
| 2762.5 | 1700.0 | -13.3 | -16.3 |
| 2775.0 | 1700.0 | -18.3 | -15.2 |
| 2787.5 | 1700.0 | -14.6 | -11.4 |
| 2800.0 | 1700.0 | -14.5 | -8.2 |
| 2812.5 | 1700.0 | 3.6 | -6.3 |
| 2825.0 | 1700.0 | 2.6 | -3.8 |
| 2837.5 | 1700.0 | -8.6 | .7 |
| 2850.0 | 1700.0 | -2.0 | .0 |
| 2862.5 | 1700.0 | 7.8 | -.1 |
| 2875.0 | 1700.0 | .6 | 1.7 |
| 2887.5 | 1700.0 | 1.9 | 2.6 |
| 2900.0 | 1700.0 | .3 | 2.8 |
| 2912.5 | 1700.0 | 2.6 | 3.5 |
| 2925.0 | 1700.0 | 8.4 | 4.1 |
| 2937.5 | 1700.0 | 4.4 | 7.7 |
| 2950.0 | 1700.0 | 4.9 | 11.5 |
| 2962.5 | 1700.0 | 18.3 | 13.0 |
| 2975.0 | 1700.0 | 21.4 | 16.0 |
| 2987.5 | 1700.0 | 16.1 | 18.7 |
| 3000.0 | 1700.0 | 19.2 | 19.2 |
| 3012.5 | 1700.0 | 18.4 | 19.4 |
| 3025.0 | 1700.0 | 21.1 | 20.8 |
| 3037.5 | 1700.0 | 22.3 | 22.6 |
| 3050.0 | 1700.0 | 23.1 | 21.8 |
| 3062.5 | 1700.0 | 28.3 | 19.5 |
| 3075.0 | 1700.0 | 14.2 | 15.6 |
| 3087.5 | 1700.0 | 9.8 | 11.2 |
| 3100.0 | 1700.0 | 2.7 | 7.0 |
| 3112.5 | 1700.0 | 1.1 | 11.1 |
| 3125.0 | 1700.0 | 7.2 | 19.6 |
| 3137.5 | 1700.0 | 34.9 | 51.1 |
| 3150.0 | 1700.0 | 52.1 | 72.7 |
| 3162.5 | 1700.0 | 160.2 | 148.7 |
| 3175.0 | 1700.0 | 109.3 | 185.3 |
| 3187.5 | 1700.0 | 387.0 | 224.7 |
|  |  |  |  |


| 3200.0 | 1700.0 | 218.0 | 211.5 |
| ---: | ---: | ---: | ---: |
| 3212.5 | 1700.0 | 249.1 | 196.2 |
| 3225.0 | 1700.0 | 94.2 | 123.0 |
| 3237.5 | 1700.0 | 32.9 | 83.4 |
| 3250.0 | 1700.0 | 20.9 | 36.6 |
| 3262.5 | 1700.0 | 19.8 | 19.6 |
| 3275.0 | 1700.0 | 15.3 | 15.1 |
| 3287.5 | 1700.0 | 9.0 | 13.7 |
| 3300.0 | 1700.0 | 10.6 | 12.9 |
| 3312.5 | 1700.0 | 13.9 | 14.2 |
| 3325.0 | 1700.0 | 15.7 | 16.7 |
| 3337.5 | 1700.0 | 21.9 | 20.1 |
| 3350.0 | 1700.0 | 21.6 | 25.0 |
| 3362.5 | 1700.0 | 27.4 | 30.4 |
| 3375.0 | 1700.0 | 38.6 | 35.5 |
| 3387.5 | 1700.0 | 42.4 | 40.7 |
| 3400.0 | 1700.0 | 47.5 | 44.8 |
| 3412.5 | 1700.0 | 47.5 | 47.5 |
| 3425.0 | 1700.0 | 47.9 | 49.3 |
| 3437.5 | 1700.0 | 52.0 | 50.9 |
| 3450.0 | 1700.0 | 51.5 | 54.3 |
| 3462.5 | 1700.0 | 55.4 | 59.0 |
| 3475.0 | 1700.0 | 64.9 | 64.5 |
| 3487.5 | 1700.0 | 71.4 | 71.3 |
| 3500.0 | 1700.0 | 79.1 | 78.6 |
| 3512.5 | 1700.0 | 85.7 | 83.6 |
| 3525.0 | 1700.0 | 91.8 | 85.6 |
| 3537.5 | 1700.0 | 89.8 | 84.2 |
| 3550.0 | 1700.0 | 81.6 | 81.5 |
| 3562.5 | 1700.0 | 72.1 | 76.3 |
| 3575.0 | 1700.0 | 72.2 | 68.0 |
| 3587.5 | 1700.0 | 65.7 | 58.6 |
| 3600.0 | 1700.0 | 48.4 | 49.6 |
| 3612.5 | 1700.0 | 34.4 | 39.0 |
| 3625.0 | 1700.0 | 27.1 | 30.0 |
| 3637.5 | 1700.0 | 19.5 | 25.2 |
| 3650.0 | 1700.0 | 20.8 | 24.7 |
| 3662.5 | 1700.0 | 24.0 | 27.4 |
| 3675.0 | 1700.0 | 32.3 | 34.1 |
| 3687.5 | 1700.0 | 40.4 | 37.5 |
| 3700.0 | 1700.0 | 53.2 | 42.0 |

### 2.2 Line 1800 E

| 3700.0 | 1800.0 | 1.9 | 2.2 |
| :--- | :--- | :--- | :--- |
| 3687.5 | 1800.0 | .4 | 3.1 |
| 3675.0 | 1800.0 | 4.2 | 3.8 |
| 3662.5 | 1800.0 | 6.0 | 4.6 |
| 3650.0 | 1800.0 | 6.5 | 5.7 |
| 3637.5 | 1800.0 | 6.0 | 6.7 |
| 3625.0 | 1800.0 | 5.6 | 7.7 |
| 3612.5 | 1800.0 | 9.2 | 9.5 |


| 3600.0 | 1800.0 | 11.2 | 12.4 |
| ---: | ---: | ---: | ---: |
| 3587.5 | 1800.0 | 15.7 | 16.1 |
| 3575.0 | 1800.0 | 20.5 | 19.3 |
| 3562.5 | 1800.0 | 24.0 | 22.8 |
| 3550.0 | 1800.0 | 25.3 | 25.6 |
| 3537.5 | 1800.0 | 28.7 | 27.5 |
| 3525.0 | 1800.0 | 29.7 | 29.0 |
| 3512.5 | 1800.0 | 29.8 | 31.1 |
| 3500.0 | 1800.0 | 31.4 | 33.2 |
| 3487.5 | 1800.0 | 35.7 | 36.1 |
| 3475.0 | 1800.0 | 39.3 | 39.2 |
| 3462.5 | 1800.0 | 44.2 | 41.8 |
| 3450.0 | 1800.0 | 45.2 | 43.1 |
| 3437.5 | 1800.0 | 44.5 | 42.9 |
| 3425.0 | 1800.0 | 42.2 | 40.2 |
| 3412.5 | 1800.0 | 38.6 | 35.8 |
| 3400.0 | 1800.0 | 30.5 | 29.7 |
| 3387.5 | 1800.0 | 23.1 | 22.2 |
| 3375.0 | 1800.0 | 14.0 | 14.0 |
| 3362.5 | 1800.0 | 4.9 | 6.4 |
| 3350.0 | 1800.0 | -2.3 | -.5 |
| 3337.5 | 1800.0 | -7.9 | -6.3 |
| 3325.0 | 1800.0 | -11.0 | -9.8 |
| 3312.5 | 1800.0 | -15.4 | -12.2 |
| 3300.0 | 1800.0 | -12.2 | -12.0 |
| 3287.5 | 1800.0 | -14.7 | -8.2 |
| 3275.0 | 1800.0 | -6.6 | -1.7 |
| 3262.5 | 1800.0 | 7.8 | 6.3 |
| 3250.0 | 1800.0 | 17.4 | 19.3 |
| 3237.5 | 1800.0 | 27.7 | 37.3 |
| 3225.0 | 1800.0 | 50.1 | 51.3 |
| 3212.5 | 1800.0 | 83.4 | 52.9 |
| 3200.0 | 1800.0 | 78.0 | 52.2 |
| 3187.5 | 1800.0 | 25.3 | 49.7 |
| 3175.0 | 1800.0 | 24.1 | 44.1 |
| 3162.5 | 1800.0 | 37.8 | 47.9 |
| 3150.0 | 1800.0 | 55.4 | 72.0 |
| 3137.5 | 1800.0 | 97.1 | 87.8 |
| 3125.0 | 1800.0 | 145.6 | 100.5 |
| 3112.5 | 1800.0 | 103.1 | 108.2 |
| 3100.0 | 1800.0 | 101.3 | 107.7 |
| 3087.5 | 1800.0 | 93.9 | 101.4 |
| 3075.0 | 1800.0 | 94.6 | 107.2 |
| 3062.5 | 1800.0 | 114.2 | 107.3 |
| 3050.0 | 1800.0 | 131.8 | 104.3 |
| 3037.5 | 1800.0 | 102.2 | 100.3 |
| 3025.0 | 1800.0 | 78.7 | 91.9 |
| 3012.5 | 1800.0 | 74.4 | 79.2 |
| 3000.0 | 1800.0 | 72.5 | 70.5 |
| 2987.5 | 1800.0 | 68.3 | 64.5 |
| 2975.0 | 1800.0 | 58.4 | 57.6 |
| 2962.5 | 1800.0 | 48.8 | 49.6 |
| 2950.0 | 1800.0 | 40.0 | 40.7 |
|  |  |  |  |


| 2937.5 | 1800.0 | 32.4 | 32.8 |
| ---: | ---: | ---: | ---: |
| 2925.0 | 1800.0 | 24.0 | 25.6 |
| 2912.5 | 1800.0 | 18.6 | 19.2 |
| 2900.0 | 1800.0 | 13.1 | 13.4 |
| 2887.5 | 1800.0 | 8.1 | 8.0 |
| 2875.0 | 1800.0 | 3.3 | 3.0 |
| 2862.5 | 1800.0 | -3.1 | -.7 |
| 2850.0 | 1800.0 | -6.5 | -3.6 |
| 2837.5 | 1800.0 | -5.1 | -3.7 |
| 2825.0 | 1800.0 | -6.6 | -3.4 |
| 2812.5 | 1800.0 | 2.8 | -4.1 |
| 2800.0 | 1800.0 | -1.8 | -5.6 |
| 2787.5 | 1800.0 | -9.9 | -6.9 |
| 2775.0 | 1800.0 | -12.7 | -9.8 |
| 2762.5 | 1800.0 | -12.8 | -12.3 |
| 2750.0 | 1800.0 | -12.0 | -14.2 |
| 2737.5 | 1800.0 | -14.1 | -16.3 |
| 2725.0 | 1800.0 | -19.3 | -18.7 |
| 2712.5 | 1800.0 | -23.3 | -20.9 |
| 2700.0 | 1800.0 | -24.7 | -23.5 |
| 2687.5 | 1800.0 | -23.3 | -25.8 |
| 2675.0 | 1800.0 | -26.9 | -27.8 |
| 2662.5 | 1800.0 | -30.6 | -28.8 |
| 2650.0 | 1800.0 | -33.3 | -30.5 |
| 2637.5 | 1800.0 | -29.8 | -33.4 |
| 2625.0 | 1800.0 | -32.0 | -35.7 |
| 2612.5 | 1800.0 | -41.1 | -37.5 |
| 2600.0 | 1800.0 | -42.5 | -40.4 |
| 2587.5 | 1800.0 | -42.1 | -43.1 |
| 2575.0 | 1800.0 | -44.5 | -44.2 |
| 2562.5 | 1800.0 | -45.3 | -45.4 |
| 2550.0 | 1800.0 | -46.8 | -47.2 |
| 2537.5 | 1800.0 | -48.5 | -48.4 |
| 2525.0 | 1800.0 | -51.0 | -50.5 |
| 2512.5 | 1800.0 | -50.2 | -51.8 |
| 2500.0 | 1800.0 | -55.8 | -53.6 |
| 2487.5 | 1800.0 | -53.4 | -55.1 |
| 2475.0 | 1800.0 | -57.7 | -56.1 |
| 2462.5 | 1800.0 | -58.4 | -57.7 |
| 2450.0 | 1800.0 | -55.3 | -59.7 |
| 2437.5 | 1800.0 | -63.7 | -61.5 |
| 2425.0 | 1800.0 | -63.5 | -63.1 |
| 2412.5 | 1800.0 | -66.7 | -65.6 |
| 2400.0 | 1800.0 | -66.5 | -66.8 |
| 2387.5 | 1800.0 | -67.7 | -68.5 |
| 2375.0 | 1800.0 | -69.4 | -69.5 |
| 2362.5 | 1800.0 | -72.2 | -71.6 |
| 2350.0 | 1800.0 | -71.9 | -74.1 |
| 2337.5 | 1800.0 | -76.7 | -75.2 |
| 2325.0 | 1800.0 | -80.2 | -79.2 |
| 2312.5 | 1800.0 | -75.1 | -81.8 |
| 2300.0 | 1800.0 | -91.9 | -84.3 |
| 2287.5 | 1800.0 | -85.0 | -88.1 |
| 2 |  |  |  |


| 2275.0 | 1800.0 | -89.2 | -98.0 |
| ---: | ---: | ---: | ---: |
| 2262.5 | 1800.0 | -99.5 | -86.6 |
| 2250.0 | 1800.0 | -124.6 | -62.0 |
| 2237.5 | 1800.0 | -34.6 | -41.6 |
| 2225.0 | 1800.0 | 37.7 | -28.7 |
| 2212.5 | 1800.0 | 13.0 | -4.8 |
| 2200.0 | 1800.0 | -35.2 | 5.2 |

2.3 Line 1900 E

| 3000.0 | 1900.0 | -5.8 | -4.8 |
| ---: | ---: | ---: | ---: |
| 2987.5 | 1900.0 | -4.4 | -4.6 |
| 2975.0 | 1900.0 | -4.3 | -4.5 |
| 2962.5 | 1900.0 | -3.9 | -4.0 |
| 2950.0 | 1900.0 | -3.9 | -3.8 |
| 2937.5 | 1900.0 | -3.6 | -3.5 |
| 2925.0 | 1900.0 | -3.2 | -3.3 |
| 2912.5 | 1900.0 | -2.9 | -3.0 |
| 2900.0 | 1900.0 | -2.7 | -2.2 |
| 2887.5 | 1900.0 | -2.4 | -1.6 |
| 2875.0 | 1900.0 | .0 | -1.0 |
| 2862.5 | 1900.0 | -.1 | -.6 |
| 2850.0 | 1900.0 | -.0 | -.4 |
| 2837.5 | 1900.0 | -.4 | -.2 |
| 2825.0 | 1900.0 | -1.6 | -.2 |
| 2812.5 | 1900.0 | 1.0 | .0 |
| 2800.0 | 1900.0 | .0 | .0 |
| 2787.5 | 1900.0 | -.8 | .8 |
| 2775.0 | 1900.0 | -.2 | .7 |
| 2762.5 | 1900.0 | 2.2 | .4 |
| 2750.0 | 1900.0 | .6 | -.4 |
| 2737.5 | 1900.0 | -1.3 | -1.1 |
| 2725.0 | 1900.0 | -3.2 | -1.3 |
| 2712.5 | 1900.0 | -3.7 | -2.0 |
| 2700.0 | 1900.0 | 1.3 | -3.0 |
| 2687.5 | 1900.0 | -3.1 | -4.8 |
| 2675.0 | 1900.0 | -6.1 | -7.0 |
| 2662.5 | 1900.0 | -12.6 | -10.2 |
| 2650.0 | 1900.0 | -14.3 | -13.2 |
| 2637.5 | 1900.0 | -15.0 | -16.3 |
| 2625.0 | 1900.0 | -17.9 | -17.9 |
| 2612.5 | 1900.0 | -21.5 | -19.5 |
| 2600.0 | 1900.0 | -20.6 | -22.7 |
| 2587.5 | 1900.0 | -22.7 | -25.8 |
| 2575.0 | 1900.0 | -30.7 | -28.5 |
| 2562.5 | 1900.0 | -33.5 | -32.3 |
| 2550.0 | 1900.0 | -35.1 | -36.1 |
| 2537.5 | 1900.0 | -39.3 | -38.0 |
| 2525.0 | 1900.0 | -42.1 | -39.5 |
| 2512.5 | 1900.0 | -39.9 | -41.6 |
| 2500.0 | 1900.0 | -41.2 | -43.0 |
| 2487.5 | 1900.0 | -45.3 | -44.5 |


| 2475.0 | 1900.0 | -46.6 | -46.5 |
| :--- | :--- | :--- | :--- |
| 2462.5 | 1900.0 | -49.6 | -48.7 |
| 2450.0 | 1900.0 | -49.9 | -50.1 |
| 2437.5 | 1900.0 | -52.0 | -50.8 |
| 2425.0 | 1900.0 | -52.3 | -52.3 |
| 2412.5 | 1900.0 | -50.4 | -54.8 |
| 2400.0 | 1900.0 | -56.7 | -57.3 |
| 2387.5 | 1900.0 | -62.8 | -59.8 |
| 2375.0 | 1900.0 | -64.5 | -61.5 |
| 2362.5 | 1900.0 | -64.5 | -62.7 |
| 2350.0 | 1900.0 | -59.0 | -64.2 |
| 2337.5 | 1900.0 | -62.9 | -64.1 |
| 2325.0 | 1900.0 | -70.2 | -64.2 |
| 2312.5 | 1900.0 | -64.0 | -66.3 |
| 2300.0 | 1900.0 | -64.7 | -69.4 |
| 2287.5 | 1900.0 | -69.6 | -70.4 |
| 2275.0 | 1900.0 | -78.4 | -73.7 |
| 2262.5 | 1900.0 | -75.5 | -76.7 |
| 2250.0 | 1900.0 | -80.3 | -81.3 |
| 2237.5 | 1900.0 | -79.7 | -84.0 |
| 2225.0 | 1900.0 | -92.8 | -84.8 |
| 2212.5 | 1900.0 | -91.6 | -85.9 |
| 2200.0 | 1900.0 | -79.4 | -87.9 |

### 2.4 Line 2000 E

| 2200.0 | 2000.0 | -71.1 | -71.2 |
| :--- | :--- | :--- | :--- |
| 2212.5 | 2000.0 | -70.1 | -73.3 |
| 2225.0 | 2000.0 | -72.5 | -73.0 |
| 2237.5 | 2000.0 | -79.4 | -72.8 |
| 2250.0 | 2000.0 | -71.7 | -72.2 |
| 2262.5 | 2000.0 | -70.2 | -70.8 |
| 2275.0 | 2000.0 | -67.2 | -68.4 |
| 2287.5 | 2000.0 | -65.3 | -66.2 |
| 2300.0 | 2000.0 | -67.4 | -64.4 |
| 2312.5 | 2000.0 | -60.7 | -62.1 |
| 2325.0 | 2000.0 | -61.6 | -60.3 |
| 2337.5 | 2000.0 | -55.5 | -57.2 |
| 2350.0 | 2000.0 | -56.4 | -55.5 |
| 2362.5 | 2000.0 | -51.8 | -53.4 |
| 2375.0 | 2000.0 | -52.0 | -52.1 |
| 2387.5 | 2000.0 | -51.4 | -50.6 |
| 2400.0 | 2000.0 | -49.0 | -50.5 |
| 2412.5 | 2000.0 | -48.7 | -49.1 |
| 2425.0 | 2000.0 | -51.6 | -46.7 |
| 2437.5 | 2000.0 | -44.8 | -45.3 |
| 2450.0 | 2000.0 | -39.5 | -42.8 |
| 2462.5 | 2000.0 | -41.9 | -39.3 |
| 2475.0 | 2000.0 | -36.1 | -37.2 |
| 2487.5 | 2000.0 | -34.1 | -36.7 |
| 2500.0 | 2000.0 | -34.3 | -35.4 |


| 2512.5 | 2000.0 | -37.3 | -34.9 |
| :--- | :--- | :--- | :--- |
| 2525.0 | 2000.0 | -35.0 | -34.9 |
| 2537.5 | 2000.0 | -33.7 | -33.4 |
| 2550.0 | 2000.0 | -34.1 | -30.4 |
| 2562.5 | 2000.0 | -26.9 | -26.9 |
| 2575.0 | 2000.0 | -22.3 | -25.2 |
| 2587.5 | 2000.0 | -17.7 | -22.1 |
| 2600.0 | 2000.0 | -25.1 | -20.1 |
| 2612.5 | 2000.0 | -18.3 | -18.5 |
| 2625.0 | 2000.0 | -17.1 | -17.2 |
| 2637.5 | 2000.0 | -14.3 | -13.8 |
| 2650.0 | 2000.0 | -11.2 | -11.7 |
| 2662.5 | 2000.0 | -7.9 | -9.8 |
| 2675.0 | 2000.0 | -8.1 | -8.3 |
| 2687.5 | 2000.0 | -7.4 | -6.6 |
| 2700.0 | 2000.0 | -6.9 | -6.0 |
| 2712.5 | 2000.0 | -2.7 | -5.0 |
| 2725.0 | 2000.0 | -4.8 | -3.9 |
| 2737.5 | 2000.0 | -3.0 | -3.3 |
| 2750.0 | 2000.0 | -2.3 | -4.6 |
| 2762.5 | 2000.0 | -3.9 | -5.4 |
| 2775.0 | 2000.0 | -8.8 | -6.5 |
| 2787.5 | 2000.0 | -8.8 | -7.9 |
| 2800.0 | 2000.0 | -8.9 | -9.1 |
| 2812.5 | 2000.0 | -8.9 | -9.6 |
| 2825.0 | 2000.0 | -9.9 | -10.7 |
| 2837.5 | 2000.0 | -11.4 | -12.0 |
| 2850.0 | 2000.0 | -14.6 | -13.5 |
| 2862.5 | 2000.0 | -15.4 | -14.7 |
| 2875.0 | 2000.0 | -16.1 | -15.8 |
| 2887.5 | 2000.0 | -16.2 | -16.1 |
| 2900.0 | 2000.0 | -16.5 | -16.4 |
| 2912.5 | 2000.0 | -16.2 | -16.6 |
| 2925.0 | 2000.0 | -17.1 | -16.8 |
| 2937.5 | 2000.0 | -17.0 | -17.0 |
| 2950.0 | 2000.0 | -17.4 | -17.1 |
| 2962.5 | 2000.0 | -17.2 | -17.0 |
| 2975.0 | 2000.0 | -17.0 | -16.8 |
| 2987.5 | 2000.0 | -16.3 | -16.6 |
| 3000.0 | 2000.0 | -15.9 | -16.4 |

### 2.5 Line 2100 E

| 3000.0 | 2100.0 | 3.0 | 3.6 |
| ---: | ---: | ---: | ---: |
| 2987.5 | 2100.0 | 3.9 | 3.3 |
| 2975.0 | 2100.0 | 4.0 | 2.9 |
| 2962.5 | 2100.0 | 2.1 | 2.3 |
| 2950.0 | 2100.0 | 1.5 | 1.3 |
| 2937.5 | 2100.0 | .1 | -1.3 |
| 2925.0 | 2100.0 | -1.2 | -4.0 |
| 2912.5 | 2100.0 | -8.8 | -7.2 |
| 2900.0 | 2100.0 | -11.5 | -11.6 |


| 2887.5 | 2100.0 | -14.4 | -16.3 |
| :--- | :--- | :--- | :--- |
| 2875.0 | 2100.0 | -22.1 | -19.2 |
| 2862.5 | 2100.0 | -24.7 | -21.7 |
| 2850.0 | 2100.0 | -23.5 | -23.4 |
| 2837.5 | 2100.0 | -23.6 | -23.4 |
| 2825.0 | 2100.0 | -22.9 | -22.7 |
| 2812.5 | 2100.0 | -22.4 | -22.1 |
| 2800.0 | 2100.0 | -21.2 | -21.5 |
| 2787.5 | 2100.0 | -20.2 | -20.8 |
| 2775.0 | 2100.0 | -20.6 | -20.5 |
| 2762.5 | 2100.0 | -19.6 | -20.3 |
| 2750.0 | 2100.0 | -21.0 | -20.2 |
| 2737.5 | 2100.0 | -20.0 | -19.0 |
| 2725.0 | 2100.0 | -19.8 | -17.8 |
| 2712.5 | 2100.0 | -14.4 | -16.9 |
| 2700.0 | 2100.0 | -14.0 | -16.6 |
| 2687.5 | 2100.0 | -16.4 | -16.3 |
| 2675.0 | 2100.0 | -18.7 | -16.6 |
| 2650.0 | 2100.0 | -18.1 | -17.6 |
| 2625.0 | 2100.0 | -15.7 | -18.2 |
| 2600.0 | 2100.0 | -19.0 | -18.6 |
| 2575.0 | 2100.0 | -19.6 | -20.0 |
| 2550.0 | 2100.0 | -20.6 | -22.8 |
| 2525.0 | 2100.0 | -25.0 | -25.3 |
| 2500.0 | 2100.0 | -29.9 | -27.7 |
| 2487.5 | 2100.0 | -31.6 | -30.7 |
| 2475.0 | 2100.0 | -31.5 | -33.0 |
| 2462.5 | 2100.0 | -35.4 | -35.5 |
| 2450.0 | 2100.0 | -36.8 | -38.2 |
| 2437.5 | 2100.0 | -42.2 | -40.7 |
| 2425.0 | 2100.0 | -45.0 | -42.4 |
| 2412.5 | 2100.0 | -43.9 | -44.3 |
| 2400.0 | 2100.0 | -44.0 | -45.7 |
| 2387.5 | 2100.0 | -46.3 | -46.5 |
| 2375.0 | 2100.0 | -49.2 | -47.9 |
| 2362.5 | 2100.0 | -49.1 | -49.6 |
| 2350.0 | 2100.0 | -50.7 | -50.4 |
| 2337.5 | 2100.0 | -52.5 | -50.7 |
| 2325.0 | 2100.0 | -50.7 | -50.9 |
| 2312.5 | 2100.0 | -50.6 | -50.7 |
| 2300.0 | 2100.0 | -49.8 | -50.5 |
| 2287.5 | 2100.0 | -49.7 | -51.2 |
| 2275.0 | 2100.0 | -51.9 | -52.6 |
| 2262.5 | 2100.0 | -53.8 | -54.9 |
| 2250.0 | 2100.0 | -57.9 | -56.9 |
| 2237.5 | 2100.0 | -61.2 | -57.8 |
| 2225.0 | 2100.0 | -59.6 | -58.1 |
| 2212.5 | 2100.0 | -56.7 | -58.2 |
| 2220.0 | 2100.0 | -55.2 | -57.2 |
|  |  |  |  |

### 2.6 Line 2200E

| 3300.0 | 2200.0 | .3 | .6 |
| ---: | ---: | ---: | ---: |
| 3287.5 | 2200.0 | .8 | 1.0 |
| 3275.0 | 2200.0 | .7 | 1.5 |
| 3262.5 | 2200.0 | 2.1 | 1.5 |
| 3250.0 | 2200.0 | 3.7 | 2.5 |
| 3237.5 | 2200.0 | .1 | 2.7 |
| 3225.0 | 2200.0 | 5.7 | 2.5 |
| 3212.5 | 2200.0 | 1.8 | 2.2 |
| 3200.0 | 2200.0 | 1.4 | 2.8 |
| 3187.5 | 2200.0 | 1.9 | 2.3 |
| 3175.0 | 2200.0 | 3.1 | 2.3 |
| 3162.5 | 2200.0 | 3.3 | 2.5 |
| 3150.0 | 2200.0 | 2.0 | 2.8 |
| 3137.5 | 2200.0 | 2.1 | 3.1 |
| 3125.0 | 2200.0 | 3.5 | 2.9 |
| 3112.5 | 2200.0 | 4.7 | 3.3 |
| 3100.0 | 2200.0 | 2.4 | 3.4 |
| 3087.5 | 2200.0 | 3.6 | 2.8 |
| 3075.0 | 2200.0 | 2.7. | 2.1 |
| 3062.5 | 2200.0 | .6 | 2.1 |
| 3050.0 | 2200.0 | 1.1 | 2.0 |
| 3037.5 | 2200.0 | 2.4 | 2.2 |
| 3025.0 | 2200.0 | 3.4 | 3.5 |
| 3012.5 | 2200.0 | 3.6 | 5.4 |
| 3000.0 | 2200.0 | 6.9 | 7.5 |
| 2987.5 | 2200.0 | 10.6 | 8.8 |
| 2975.0 | 2200.0 | 13.0 | 9.8 |
| 2962.5 | 2200.0 | 9.7 | 10.1 |
| 2950.0 | 2200.0 | 8.9 | 9.2 |
| 2937.5 | 2200.0 | 8.2 | 7.4 |
| 2925.0 | 2200.0 | 6.4 | 5.6 |
| 2912.5 | 2200.0 | 3.6 | 2.7 |
| 2900.0 | 2200.0 | .8 | -1.1 |
| 2887.5 | 2200.0 | -5.6 | -3.6 |
| 2875.0 | 2200.0 | -10.6 | -7.3 |
| 2862.5 | 2200.0 | -6.2 | -10.7 |
| 2850.0 | 2200.0 | -15.0 | -13.8 |
| 2837.5 | 2200.0 | -16.1 | -16.4 |
| 2825.0 | 2200.0 | -21.2 | -20.5 |
| 2812.5 | 2200.0 | -23.6 | -22.7 |
| 2800.0 | 2200.0 | -26.7 | -25.5 |
| 2787.5 | 2200.0 | -25.9 | -27.6 |
| 2775.0 | 2200.0 | -30.0 | -29.5 |
| 2762.5 | 2200.0 | -32.0 | -30.4 |
| 2750.0 | 2200.0 | -32.7 | -31.6 |
| 2737.5 | 2200.0 | -31.3 | -32.3 |
| 2725.0 | 2200.0 | -31.8 | -32.3 |
| 2712.5 | 2200.0 | -33.5 | -31.9 |
| 2700.0 | 2200.0 | -32.0 | -31.6 |
| 2687.5 | 2200.0 | -31.1 | -31.4 |
| 2675.0 | 2200.0 | -29.4 | -30.7 |
|  |  |  |  |


| 2662.5 | 2200.0 | -30.9 | -30.6 |
| :--- | :--- | :--- | :--- |
| 2650.0 | 2200.0 | -30.3 | -30.1 |
| 2637.5 | 2200.0 | -31.4 | -30.3 |
| 2625.0 | 2200.0 | -28.4 | -30.0 |
| 2612.5 | 2200.0 | -30.5 | -30.1 |
| 2600.0 | 2200.0 | -29.6 | -30.5 |
| 2587.5 | 2200.0 | -30.6 | -31.4 |
| 2575.0 | 2200.0 | -33.6 | -32.4 |
| 2562.5 | 2200.0 | -32.6 | -33.5 |
| 2550.0 | 2200.0 | -35.6 | -34.0 |
| 2537.5 | 2200.0 | -35.2 | -34.5 |
| 2525.0 | 2200.0 | -32.9 | -35.3 |
| 2512.5 | 2200.0 | -36.0 | -36.3 |
| 2500.0 | 2200.0 | -37.0 | -37.4 |
| 2487.5 | 2200.0 | -40.2 | -38.8 |
| 2475.0 | 2200.0 | -40.9 | -40.3 |
| 2462.5 | 2200.0 | -39.8 | -41.8 |
| 2450.0 | 2200.0 | -43.4 | -43.3 |
| 2437.5 | 2200.0 | -44.8 | -45.2 |
| 2425.0 | 2200.0 | -47.8 | -47.1 |
| 2412.5 | 2200.0 | -50.1 | -48.9 |
| 2400.0 | 2200.0 | -49.4 | -50.6 |
| 2387.5 | 2200.0 | -52.6 | -51.6 |
| 2375.0 | 2200.0 | -53.3 | -52.4 |
| 2362.5 | 2200.0 | -52.4 | -53.4 |
| 2350.0 | 2200.0 | -54.3 | -53.4 |
| 2337.5 | 2200.0 | -54.2 | -52.0 |
| 2325.0 | 2200.0 | -52.7 | -52.1 |
| 2312.5 | 2200.0 | -46.4 | -53.0 |
| 2300.0 | 2200.0 | -52.8 | -53.7 |
| 2287.5 | 2200.0 | -58.9 | -55.2 |
| 2275.0 | 2200.0 | -57.6 | -56.9 |
| 2262.5 | 2200.0 | -60.4 | -57.8 |
| 2250.0 | 2200.0 | -54.9 | -58.7 |
| 2237.5 | 2200.0 | -57.3 | -61.1 |
| 2225.0 | 2200.0 | -63.4 | -63.7 |
| 2212.5 | 2200.0 | -69.3 | -65.9 |
| 2200.0 | 2200.0 | -73.6 | -68.8 |

### 2.7 Line 2300 E

| 2200.0 | 2300.0 | -54.8 | -52.0 |
| :--- | :--- | :--- | :--- |
| 2212.5 | 2300.0 | -54.2 | -50.7 |
| 2225.0 | 2300.0 | -46.9 | -51.6 |
| 2237.5 | 2300.0 | -46.8 | -50.7 |
| 2250.0 | 2300.0 | -55.1 | -50.1 |
| 2262.5 | 2300.0 | -50.5 | -51.3 |
| 2275.0 | 2300.0 | -51.1 | -51.4 |
| 2287.5 | 2300.0 | -52.9 | -49.9 |
| 2300.0 | 2300.0 | -47.3 | -49.6 |
| 2312.5 | 2300.0 | -47.6 | -48.2 |


| 2325.0 | 2300.0 | -49.1 | -47.1 |
| :--- | :--- | :--- | :--- |
| 2337.5 | 2300.0 | -43.9 | -47.8 |
| 2350.0 | 2300.0 | -47.5 | -47.7 |
| 2362.5 | 2300.0 | -50.9 | -47.3 |
| 2375.0 | 2300.0 | -47.0 | -47.1 |
| 2387.5 | 2300.0 | -47.2 | -46.7 |
| 2400.0 | 2300.0 | -42.8 | -45.7 |
| 2412.5 | 2300.0 | -45.6 | -44.1 |
| 2425.0 | 2300.0 | -46.0 | -42.6 |
| 2437.5 | 2300.0 | -39.1 | -42.2 |
| 2450.0 | 2300.0 | -39.4 | -41.1 |
| 2462.5 | 2300.0 | -40.7 | -40.3 |
| 2475.0 | 2300.0 | -40.4 | -41.2 |
| 2487.5 | 2300.0 | -42.0 | -41.6 |
| 2500.0 | 2300.0 | -43.6 | -41.1 |
| 2512.5 | 2300.0 | -41.4 | -41.6 |
| 2525.0 | 2300.0 | -38.3 | -40.9 |
| 2537.5 | 2300.0 | -42.7 | -39.9 |
| 2550.0 | 2300.0 | -38.7 | -39.4 |
| 2562.5 | 2300.0 | -38.5 | -39.9 |
| 2575.0 | 2300.0 | -38.8 | -39.4 |
| 2587.5 | 2300.0 | -40.9 | -40.2 |
| 2600.0 | 2300.0 | -40.2 | -41.0 |
| 2612.5 | 2300.0 | -42.5 | -42.6 |
| 2625.0 | 2300.0 | -42.5 | -44.6 |
| 2637.5 | 2300.0 | -47.0 | -48.0 |
| 2650.0 | 2300.0 | -50.6 | -51.0 |
| 2662.5 | 2300.0 | -57.3 | -53.0 |
| 2675.0 | 2300.0 | -57.4 | -53.6 |
| 2687.5 | 2300.0 | -52.8 | -51.1 |
| 2700.0 | 2300.0 | -50.1 | -45.7 |
| 2712.5 | 2300.0 | -37.9 | -40.1 |
| 2725.0 | 2300.0 | -30.2 | -34.8 |
| 2737.5 | 2300.0 | -29.4 | -29.8 |
| 2750.0 | 2300.0 | -26.3 | -26.7 |
| 2762.5 | 2300.0 | -25.2 | -24.6 |
| 2775.0 | 2300.0 | -22.6 | -22.6 |
| 2787.5 | 2300.0 | -19.5 | -21.1 |
| 2800.0 | 2300.0 | -19.6 | -19.2 |
| 2812.5 | 2300.0 | -18.6 | -17.5 |
| 2825.0 | 2300.0 | -15.7 | -16.2 |
| 2837.5 | 2300.0 | -14.2 | -14.7 |
| 2850.0 | 2300.0 | -12.7 | -13.1 |
| 2862.5 | 2300.0 | -12.1 | -12.0 |
| 2875.0 | 2300.0 | -10.9 | -10.9 |
| 2887.5 | 2300.0 | -10.2 | -10.1 |
| 2900.0 | 2300.0 | -8.8 | -9.2 |
| 2912.5 | 2300.0 | -8.3 | -8.5 |
| 2925.0 | 2300.0 | -7.7 | -8.0 |
| 2937.5 | 2300.0 | -7.7 | -7.8 |
| 2950.0 | 2300.0 | -7.7 | -7.6 |
| 2962.5 | 2300.0 | -7.5 | -7.4 |
| 2975.0 | 2300.0 | -7.3 | -7.1 |
|  |  |  |  |


| 2987.5 | 2300.0 | -6.9 | -6.8 |
| ---: | ---: | ---: | ---: |
| 3000.0 | 2300.0 | -6.0 | -6.5 |
| 3012.5 | 2300.0 | -6.3 | -6.2 |
| 3025.0 | 2300.0 | -6.0 | -5.8 |
| 3037.5 | 2300.0 | -5.6 | -5.2 |
| 3050.0 | 2300.0 | -4.9 | -4.7 |
| 3062.5 | 2300.0 | -3.2 | -4.4 |
| 3075.0 | 2300.0 | -3.9 | -4.0 |
| 3087.5 | 2300.0 | -4.4 | -3.7 |
| 3100.0 | 2300.0 | -3.6 | -3.8 |
| 3112.5 | 2300.0 | -3.5 | -2.9 |
| 3125.0 | 2300.0 | -3.7 | -2.4 |
| 3137.5 | 2300.0 | .6 | -2.5 |
| 3150.0 | 2300.0 | -2.0 | -2.1 |
| 3162.5 | 2300.0 | -4.0 | -2.0 |
| 3175.0 | 2300.0 | -1.3 | -2.5 |
| 3187.5 | 2300.0 | -3.5 | -2.5 |
| 3200.0 | 2300.0 | -1.7 | -2.4 |
| 3212.5 | 2300.0 | -2.1 | -2.5 |
| 3225.0 | 2300.0 | -3.4 | -2.4 |
| 3237.5 | 2300.0 | -2.0 | -2.3 |
| 3250.0 | 2300.0 | -2.9 | -2.1 |
| 3262.5 | 2300.0 | -1.0 | -1.3 |
| 3275.0 | 2300.0 | -1.1 | -.6 |
| 3287.5 | 2300.0 | .7 | .8 |
| 3300.0 | 2300.0 | 1.3 | 2.0 |
| 3312.5 | 2300.0 | 3.9 | 2.0 |
| 3325.0 | 2300.0 | 5.2 | 1.9 |
| 3337.5 | 2300.0 | -1.1 | 1.6 |
| 3350.0 | 2300.0 | .2 | 1.1 |
| 3362.5 | 2300.0 | -.2 | .5 |
| 3375.0 | 2300.0 | 1.5 | 1.8 |
| 3387.5 | 2300.0 | 2.0 | 2.2 |
| 3400.0 | 2300.0 | 5.4 | 3.0 |

### 2.8 Line 2400 E

| 2200.0 | 2400.0 | -51.6 | -42.8 |
| :--- | :--- | :--- | :--- |
| 2212.5 | 2400.0 | -43.5 | -42.8 |
| 2225.0 | 2400.0 | -33.2 | -43.2 |
| 2237.5 | 2400.0 | -42.8 | -45.2 |
| 2250.0 | 2400.0 | -45.1 | -48.4 |
| 2262.5 | 2400.0 | -61.5 | -53.3 |
| 2275.0 | 2400.0 | -59.5 | -55.6 |
| 2287.5 | 2400.0 | -57.4 | -58.2 |
| 2300.0 | 2400.0 | -54.4 | -57.7 |
| 2312.5 | 2400.0 | -58.1 | -55.6 |
| 2325.0 | 2400.0 | -59.0 | -55.3 |
| 2337.5 | 2400.0 | -49.2 | -55.2 |
| 2350.0 | 2400.0 | -55.7 | -53.2 |
| 2362.5 | 2400.0 | -53.9 | -52.1 |


| 2375.0 | 2400.0 | -48.2 | -51.6 |
| :--- | :--- | :--- | :--- |
| 2387.5 | 2400.0 | -53.7 | -50.0 |
| 2400.0 | 2400.0 | -46.3 | -49.1 |
| 2412.5 | 2400.0 | -47.7 | -48.3 |
| 2425.0 | 2400.0 | -49.7 | -46.4 |
| 2437.5 | 2400.0 | -44.1 | -46.0 |
| 2450.0 | 2400.0 | -44.2 | -46.3 |
| 2462.5 | 2400.0 | -44.3 | -45.0 |
| 2475.0 | 2400.0 | -49.1 | -44.6 |
| 2487.5 | 2400.0 | -43.4 | -43.4 |
| 2500.0 | 2400.0 | -42.1 | -42.3 |
| 2512.5 | 2400.0 | -37.9 | -40.2 |
| 2525.0 | 2400.0 | -39.2 | -39.7 |
| 2537.5 | 2400.0 | -38.2 | -39.7 |
| 2550.0 | 2400.0 | -40.9 | -39.8 |
| 2562.5 | 2400.0 | -42.1 | -39.9 |
| 2575.0 | 2400.0 | -38.5 | -40.4 |
| 2587.5 | 2400.0 | -40.0 | -40.3 |
| 2600.0 | 2400.0 | -40.3 | -40.5 |
| 2612.5 | 2400.0 | -40.5 | -41.8 |
| 2625.0 | 2400.0 | -43.1 | -42.2 |
| 2637.5 | 2400.0 | -45.3 | -43.2 |
| 2650.0 | 2400.0 | -41.9 | -45.2 |
| 2662.5 | 2400.0 | -45.1 | -46.3 |
| 2675.0 | 2400.0 | -50.7 | -47.0 |
| 2687.5 | 2400.0 | -48.7 | -48.9 |
| 2700.0 | 2400.0 | -48.6 | -51.4 |
| 2712.5 | 2400.0 | -51.3 | -53.1 |
| 2725.0 | 2400.0 | -57.5 | -55.6 |
| 2737.5 | 2400.0 | -59.5 | -56.0 |
| 2750.0 | 2400.0 | -61.1 | -54.4 |
| 2762.5 | 2400.0 | -50.7 | -50.7 |
| 2775.0 | 2400.0 | -43.1 | -45.5 |
| 2787.5 | 2400.0 | -39.3 | -39.7 |
| 2800.0 | 2400.0 | -33.1 | -35.1 |
| 2812.5 | 2400.0 | -32.1 | -30.9 |
| 2825.0 | 2400.0 | -27.8 | -27.6 |
| 2837.5 | 2400.0 | -22.4 | -25.3 |
| 2850.0 | 2400.0 | -22.5 | -23.0 |
| 2862.5 | 2400.0 | -21.6 | -21.4 |
| 2875.0 | 2400.0 | -20.6 | -20.6 |
| 2887.5 | 2400.0 | -20.0 | -18.9 |
| 2900.0 | 2400.0 | -18.1 | -17.7 |
| 2912.5 | 2400.0 | -14.0 | -16.6 |
| 2925.0 | 2400.0 | -15.7 | -15.4 |
| 2937.5 | 2400.0 | -15.0 | -14.4 |
| 2950.0 | 2400.0 | -14.0 | -14.3 |
| 2962.5 | 2400.0 | -13.4 | -13.9 |
| 2975.0 | 2400.0 | -13.4 | -13.5 |
| 2987.5 | 2400.0 | -13.5 | -13.3 |
| 3000.0 | 2400.0 | -13.4 | -12.9 |
| 3012.5 | 2400.0 | -12.6 | -12.3 |
| 3025.0 | 2400.0 | -11.5 | -11.7 |
|  |  |  |  |


| 3037.5 | 2400.0 | -10.6 | -11.0 |
| ---: | ---: | ---: | ---: |
| 3050.0 | 2400.0 | -10.4 | -10.4 |
| 3062.5 | 2400.0 | -10.1 | -9.4 |
| 3075.0 | 2400.0 | -9.3 | -9.0 |
| 3087.5 | 2400.0 | -6.6 | -8.3 |
| 3100.0 | 2400.0 | -8.6 | -7.7 |
| 3112.5 | 2400.0 | -6.8 | -7.5 |
| 3125.0 | 2400.0 | -7.1 | -7.1 |
| 3137.5 | 2400.0 | -8.3 | -5.7 |
| 3150.0 | 2400.0 | -4.6 | -4.9 |
| 3162.5 | 2400.0 | -1.9 | -4.2 |
| 3175.0 | 2400.0 | -2.8 | -3.6 |
| 3187.5 | 2400.0 | -3.6 | -3.3 |
| 3200.0 | 2400.0 | -5.3 | -3.9 |
| 3212.5 | 2400.0 | -2.7 | -3.5 |
| 3225.0 | 2400.0 | -5.0 | -3.2 |
| 3237.5 | 2400.0 | -1.1 | -2.3 |
| 3250.0 | 2400.0 | -2.1 | -2.6 |
| 3262.5 | 2400.0 | -.4 | -2.3 |
| 3275.0 | 2400.0 | -4.3 | -2.3 |
| 3287.5 | 2400.0 | -3.5 | -2.0 |
| 3300.0 | 2400.0 | -1.4 | -1.8 |
| 3312.5 | 2400.0 | -.4 | -.7 |
| 3325.0 | 2400.0 | .6 | .4 |
| 3337.5 | 2400.0 | 1.4 | 1.3 |
| 3350.0 | 2400.0 | 1.7 | 2.2 |
| 3362.5 | 2400.0 | 3.1 | 3.0 |
| 3375.0 | 2400.0 | 4.1 | 4.0 |
| 3387.5 | 2400.0 | 4.8 | 4.6 |
| 3400.0 | 2400.0 | 6.3 | 5.1 |

### 2.9 Line 2500E

| 3400.0 | 2500.0 | 10.8 | 9.8 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 2500.0 | 10.0 | 9.4 |
| 3375.0 | 2500.0 | 8.6 | 8.7 |
| 3362.5 | 2500.0 | 8.0 | 7.4 |
| 3350.0 | 2500.0 | 6.0 | 6.1 |
| 3337.5 | 2500.0 | 4.5 | 5.1 |
| 3325.0 | 2500.0 | 3.5 | 3.8 |
| 3312.5 | 2500.0 | 3.4 | 2.7 |
| 3300.0 | 2500.0 | 1.7 | 1.6 |
| 3287.5 | 2500.0 | .3 | .7 |
| 3275.0 | 2500.0 | -.8 | -.4 |
| 3262.5 | 2500.0 | -1.3 | -1.3 |
| 3250.0 | 2500.0 | -1.9 | -2.2 |
| 3237.5 | 2500.0 | -2.9 | -2.8 |
| 3225.0 | 2500.0 | -3.9 | -3.5 |
| 3212.5 | 2500.0 | -4.2 | -4.3 |
| 3200.0 | 2500.0 | -4.8 | -5.1 |
| 3187.5 | 2500.0 | -5.5 | -6.0 |


| 3175.0 | 2500.0 | -7.3 | -6.8 |
| :--- | :--- | ---: | ---: |
| 3162.5 | 2500.0 | -8.3 | -7.8 |
| 3150.0 | 2500.0 | -8.2 | -8.6 |
| 3137.5 | 2500.0 | -9.5 | -9.3 |
| 3125.0 | 2500.0 | -9.9 | -9.7 |
| 3112.5 | 2500.0 | -10.4 | -10.6 |
| 3100.0 | 2500.0 | -10.7 | -11.2 |
| 3087.5 | 2500.0 | -12.3 | -12.0 |
| 3075.0 | 2500.0 | -12.9 | -12.9 |
| 3062.5 | 2500.0 | -13.9 | -13.7 |
| 3050.0 | 2500.0 | -14.5 | -14.2 |
| 3037.5 | 2500.0 | -14.7 | -14.3 |
| 3025.0 | 2500.0 | -15.2 | -14.5 |
| 3012.5 | 2500.0 | -13.0 | -14.6 |
| 3000.0 | 2500.0 | -14.9 | -14.8 |
| 2987.5 | 2500.0 | -15.2 | -14.8 |
| 2975.0 | 2500.0 | -15.9 | -15.5 |
| 2962.5 | 2500.0 | -15.0 | -15.8 |
| 2950.0 | 2500.0 | -16.4 | -15.8 |
| 2937.5 | 2500.0 | -16.3 | -15.3 |
| 2925.0 | 2500.0 | -15.3 | -14.3 |
| 2912.5 | 2500.0 | -13.4 | -12.6 |
| 2900.0 | 2500.0 | -9.9 | -10.9 |
| 2887.5 | 2500.0 | -8.2 | -8.2 |
| 2875.0 | 2500.0 | -7.7 | -5.9 |
| 2862.5 | 2500.0 | -1.9 | -4.3 |
| 2850.0 | 2500.0 | -1.9 | -2.8 |
| 2837.5 | 2500.0 | -1.6 | -1.5 |
| 2825.0 | 2500.0 | -1.1 | -1.8 |
| 2812.5 | 2500.0 | -1.0 | -1.1 |
| 2800.0 | 2500.0 | -3.5 | -1.8 |
| 2787.5 | 2500.0 | 1.8 | -2.7 |
| 2775.0 | 2500.0 | -5.2 | -3.2 |
| 2762.5 | 2500.0 | -5.7 | -4.8 |
| 2750.0 | 2500.0 | -3.4 | -9.9 |
| 2737.5 | 2500.0 | -11.3 | -17.0 |
| 2725.0 | 2500.0 | -24.0 | -24.9 |
| 2712.5 | 2500.0 | -40.7 | -32.4 |
| 2700.0 | 2500.0 | -45.0 | -39.7 |
| 2687.5 | 2500.0 | -40.8 | -44.8 |
| 2675.0 | 2500.0 | -47.9 | -48.5 |
| 2662.5 | 2500.0 | -49.5 | -50.1 |
| 2650.0 | 2500.0 | -59.4 | -52.2 |
| 2637.5 | 2500.0 | -52.8 | -52.0 |
| 2625.0 | 2500.0 | -51.2 | -51.2 |
| 2612.5 | 2500.0 | -47.3 | -48.4 |
| 2600.0 | 2500.0 | -45.4 | -47.4 |
| 2587.5 | 2500.0 | -45.5 | -48.2 |
| 2575.0 | 2500.0 | -47.4 | -48.8 |
| 2562.5 | 2500.0 | -55.3 | -46.8 |
| 2550.0 | 2500.0 | -50.2 | -46.3 |
| 2537.5 | 2500.0 | -35.5 | -44.9 |
| 2525.0 | 2500.0 | -43.0 | -42.6 |
|  |  |  |  |


| 2512.5 | 2500.0 | -40.5 | -40.6 |
| :--- | :--- | :--- | :--- |
| 2500.0 | 2500.0 | -43.9 | -42.4 |
| 2487.5 | 2500.0 | -40.0 | -42.9 |
| 2475.0 | 2500.0 | -44.7 | -45.1 |
| 2462.5 | 2500.0 | -45.5 | -45.2 |
| 2450.0 | 2500.0 | -51.2 | -46.0 |
| 2437.5 | 2500.0 | -44.8 | -49.3 |
| 2425.0 | 2500.0 | -43.9 | -49.4 |
| 2412.5 | 2500.0 | -61.1 | -47.1 |
| 2400.0 | 2500.0 | -46.1 | -46.9 |
| 2387.5 | 2500.0 | -39.4 | -47.6 |
| 2375.0 | 2500.0 | -43.9 | -44.5 |
| 2362.5 | 2500.0 | -47.4 | -43.7 |
| 2350.0 | 2500.0 | -45.6 | -47.4 |
| 2337.5 | 2500.0 | -42.1 | -51.3 |
| 2325.0 | 2500.0 | -58.1 | -52.7 |
| 2312.5 | 2500.0 | -63.4 | -55.4 |
| 2300.0 | 2500.0 | -54.2 | -58.8 |
| 2287.5 | 2500.0 | -59.2 | -63.1 |
| 2275.0 | 2500.0 | -59.1 | -61.3 |
| 2262.5 | 2500.0 | -79.4 | -59.1 |
| 2250.0 | 2500.0 | -54.8 | -56.0 |
| 2237.5 | 2500.0 | -43.0 | -54.5 |
| 2225.0 | 2500.0 | -43.8 | -52.0 |
| 2212.5 | 2500.0 | -51.7 | -51.3 |
| 2200.0 | 2500.0 | -66.7 | -54.1 |

2.10 Line 2600 E

| 2200.0 | 2600.0 | -81.4 | -47.9 |
| ---: | ---: | ---: | ---: |
| 2212.5 | 2600.0 | -43.2 | -40.0 |
| 2225.0 | 2600.0 | -19.2 | -35.0 |
| 2237.5 | 2600.0 | -16.2 | -24.6 |
| 2250.0 | 2600.0 | -15.0 | -24.5 |
| 2262.5 | 2600.0 | -29.5 | -28.3 |
| 2275.0 | 2600.0 | -42.8 | -28.3 |
| 2287.5 | 2600.0 | -38.1 | -24.7 |
| 2300.0 | 2600.0 | -15.9 | -20.3 |
| 2312.5 | 2600.0 | 2.7 | -11.6 |
| 2325.0 | 2600.0 | -7.5 | -16.1 |
| 2337.5 | 2600.0 | .8 | -23.6 |
| 2350.0 | 2600.0 | -60.6 | -36.4 |
| 2362.5 | 2600.0 | -53.6 | -46.5 |
| 2375.0 | 2600.0 | -61.0 | -57.8 |
| 2387.5 | 2600.0 | -58.1 | -57.5 |
| 2400.0 | 2600.0 | -55.8 | -59.1 |
| 2412.5 | 2600.0 | -58.9 | -51.6 |
| 2425.0 | 2600.0 | -61.5 | -46.0 |
| 2437.5 | 2600.0 | -23.5 | -43.2 |
| 2450.0 | 2600.0 | -30.1 | -42.3 |
| 2462.5 | 2600.0 | -42.0 | -42.1 |


| 2475.0 | 2600.0 | -54.4 | -48.0 |
| ---: | ---: | ---: | ---: |
| 2487.5 | 2600.0 | -60.3 | -51.7 |
| 2500.0 | 2600.0 | -53.1 | -51.9 |
| 2512.5 | 2600.0 | -48.8 | -49.0 |
| 2525.0 | 2600.0 | -42.8 | -44.1 |
| 2537.5 | 2600.0 | -39.8 | -40.3 |
| 2550.0 | 2600.0 | -36.0 | -37.0 |
| 2562.5 | 2600.0 | -34.1 | -34.5 |
| 2575.0 | 2600.0 | -32.1 | -33.2 |
| 2587.5 | 2600.0 | -30.3 | -33.7 |
| 2600.0 | 2600.0 | -33.4 | -35.9 |
| 2612.5 | 2600.0 | -38.8 | -37.7 |
| 2625.0 | 2600.0 | -44.8 | -39.7 |
| 2637.5 | 2600.0 | -41.3 | -41.5 |
| 2650.0 | 2600.0 | -40.4 | -42.3 |
| 2662.5 | 2600.0 | -42.0 | -42.6 |
| 2675.0 | 2600.0 | -42.8 | -43.9 |
| 2687.5 | 2600.0 | -46.6 | -46.0 |
| 2700.0 | 2600.0 | -47.7 | -48.8 |
| 2712.5 | 2600.0 | -50.8 | -51.7 |
| 2725.0 | 2600.0 | -56.3 | -52.6 |
| 2737.5 | 2600.0 | -57.1 | -53.4 |
| 2750.0 | 2600.0 | -51.0 | -53.2 |
| 2762.5 | 2600.0 | -51.9 | -51.7 |
| 2775.0 | 2600.0 | -49.6 | -45.3 |
| 2787.5 | 2600.0 | -49.0 | -37.4 |
| 2800.0 | 2600.0 | -24.9 | -27.1 |
| 2812.5 | 2600.0 | -11.8 | -17.4 |
| 2825.0 | 2600.0 | -.3 | -8.8 |
| 2837.5 | 2600.0 | -1.2 | -5.7 |
| 2850.0 | 2600.0 | -5.8 | -5.5 |
| 2862.5 | 2600.0 | -9.5 | -8.2 |
| 2875.0 | 2600.0 | -10.5 | -10.7 |
| 2887.5 | 2600.0 | -13.9 | -12.3 |
| 2900.0 | 2600.0 | -13.9 | -13.4 |
| 2912.5 | 2600.0 | -13.9 | -14.3 |
| 2925.0 | 2600.0 | -14.7 | -14.5 |
| 2937.5 | 2600.0 | -15.2 | -15.0 |
| 2950.0 | 2600.0 | -15.0 | -15.4 |
| 2962.5 | 2600.0 | -16.1 | -15.8 |
| 2975.0 | 2600.0 | -16.0 | -16.1 |
| 2987.5 | 2600.0 | -16.6 | -16.5 |
| 3000.0 | 2600.0 | -17.0 | -16.5 |
| 3012.5 | 2600.0 | -16.6 | -16.5 |
| 3025.0 | 2600.0 | -16.5 | -16.4 |
| 3037.5 | 2600.0 | -16.0 | -16.2 |
| 3050.0 | 2600.0 | -15.8 | -16.0 |
| 3062.5 | 2600.0 | -16.3 | -15.5 |
| 3075.0 | 2600.0 | -15.5 | -14.6 |
| 3087.5 | 2600.0 | -13.8 | -14.1 |
| 3100.0 | 2600.0 | -11.7 | -13.4 |
| 3112.5 | 2600.0 | -13.3 | -12.7 |
| 3125.0 | 2600.0 | -12.9 | -12.0 |


| 3137.5 | 2600.0 | -11.8 | -11.7 |
| ---: | ---: | ---: | ---: |
| 3150.0 | 2600.0 | -10.5 | -10.9 |
| 3162.5 | 2600.0 | -9.8 | -10.0 |
| 3175.0 | 2600.0 | -9.6 | -7.8 |
| 3187.5 | 2600.0 | -8.1 | -5.5 |
| 3200.0 | 2600.0 | -1.1 | -3.2 |
| 3212.5 | 2600.0 | 1.3 | -.7 |
| 3225.0 | 2600.0 | 1.7 | 1.4 |
| 3237.5 | 2600.0 | 2.8 | 2.3 |
| 3250.0 | 2600.0 | 2.4 | 2.8 |
| 3262.5 | 2600.0 | 3.3 | 3.8 |
| 3275.0 | 2600.0 | 3.6 | 5.0 |
| 3287.5 | 2600.0 | 7.0 | 6.4 |
| 3300.0 | 2600.0 | 8.5 | 8.0 |
| 3312.5 | 2600.0 | 9.7 | 9.9 |
| 3325.0 | 2600.0 | 11.4 | 11.2 |
| 3337.5 | 2600.0 | 13.0 | 12.9 |
| 3350.0 | 2600.0 | 13.3 | 14.0 |
| 3362.5 | 2600.0 | 17.2 | 15.6 |
| 3375.0 | 2600.0 | 15.3 | 17.6 |
| 3387.5 | 2600.0 | 19.4 | 18.7 |
| 3400.0 | 2600.0 | 22.8 | 19.2 |

### 2.11 Line

2700E

| 3400.0 | 2700.0 | 27.8 | 28.9 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 2700.0 | 28.4 | 29.0 |
| 3375.0 | 2700.0 | 30.5 | 29.0 |
| 3362.5 | 2700.0 | 29.5 | 29.1 |
| 3350.0 | 2700.0 | 28.8 | 28.3 |
| 3337.5 | 2700.0 | 28.5 | 27.1 |
| 3325.0 | 2700.0 | 24.4 | 27.4 |
| 3312.5 | 2700.0 | 24.2 | 29.2 |
| 3300.0 | 2700.0 | 31.0 | 31.3 |
| 3287.5 | 2700.0 | 37.8 | 33.3 |
| 3275.0 | 2700.0 | 39.0 | 34.1 |
| 3262.5 | 2700.0 | 34.5 | 32.4 |
| 3250.0 | 2700.0 | 28.1 | 28.5 |
| 3237.5 | 2700.0 | 22.8 | 23.5 |
| 3225.0 | 2700.0 | 18.0 | 19.4 |
| 3212.5 | 2700.0 | 14.2 | 16.0 |
| 3200.0 | 2700.0 | 13.8 | 13.4 |
| 3187.5 | 2700.0 | 11.3 | 11.6 |
| 3175.0 | 2700.0 | 9.8 | 10.5 |
| 3162.5 | 2700.0 | 8.9 | 8.8 |
| 3150.0 | 2700.0 | 8.5 | 6.8 |
| 3137.5 | 2700.0 | 5.4 | 5.1 |
| 3125.0 | 2700.0 | 1.6 | 2.9 |
| 3112.5 | 2700.0 | .9 | .6 |
| 3100.0 | 2700.0 | -2.1 | -1.9 |
| 3087.5 | 2700.0 | -2.6 | -3.9 |
| 3075.0 | 2700.0 | -7.2 | -6.1 |


| 3062.5 | 2700.0 | -8.3 | -8.3 |
| :--- | :--- | ---: | ---: |
| 3050.0 | 2700.0 | -10.5 | -11.0 |
| 3037.5 | 2700.0 | -12.7 | -13.1 |
| 3025.0 | 2700.0 | -16.4 | -15.0 |
| 3012.5 | 2700.0 | -17.4 | -16.6 |
| 3000.0 | 2700.0 | -18.0 | -17.7 |
| 2987.5 | 2700.0 | -18.3 | -18.5 |
| 2975.0 | 2700.0 | -18.6 | -19.1 |
| 2962.5 | 2700.0 | -20.1 | -19.5 |
| 2950.0 | 2700.0 | -20.4 | -19.6 |
| 2937.5 | 2700.0 | -19.9 | -19.5 |
| 2925.0 | 2700.0 | -18.9 | -19.4 |
| 2912.5 | 2700.0 | -18.1 | -19.8 |
| 2900.0 | 2700.0 | -19.8 | -20.5 |
| 2887.5 | 2700.0 | -22.1 | -21.2 |
| 2875.0 | 2700.0 | -23.4 | -22.2 |
| 2862.5 | 2700.0 | -22.6 | -23.6 |
| 2850.0 | 2700.0 | -23.3 | -24.7 |
| 2837.5 | 2700.0 | -26.7 | -26.0 |
| 2825.0 | 2700.0 | -27.5 | -27.5 |
| 2812.5 | 2700.0 | -30.1 | -28.2 |
| 2800.0 | 2700.0 | -29.7 | -28.0 |
| 2787.5 | 2700.0 | -26.8 | -28.1 |
| 2775.0 | 2700.0 | -25.9 | -29.5 |
| 2762.5 | 2700.0 | -28.1 | -32.1 |
| 2750.0 | 2700.0 | -37.0 | -35.7 |
| 2737.5 | 2700.0 | -42.8 | -39.4 |
| 2725.0 | 2700.0 | -44.9 | -43.4 |
| 2712.5 | 2700.0 | -44.3 | -45.7 |
| 2700.0 | 2700.0 | -48.1 | -46.6 |
| 2687.5 | 2700.0 | -48.6 | -46.0 |
| 2675.0 | 2700.0 | -47.0 | -45.4 |
| 2662.5 | 2700.0 | -42.1 | -42.9 |
| 2650.0 | 2700.0 | -41.2 | -40.6 |
| 2637.5 | 2700.0 | -35.8 | -38.8 |
| 2625.0 | 2700.0 | -36.7 | -37.9 |
| 2612.5 | 2700.0 | -38.3 | -36.4 |
| 2600.0 | 2700.0 | -37.7 | -36.3 |
| 2587.5 | 2700.0 | -33.4 | -36.6 |
| 2575.0 | 2700.0 | -35.2 | -38.0 |
| 2562.5 | 2700.0 | -38.2 | -39.4 |
| 2550.0 | 2700.0 | -45.4 | -40.6 |
| 2537.5 | 2700.0 | -44.9 | -41.1 |
| 2525.0 | 2700.0 | -39.5 | -40.8 |
| 2512.5 | 2700.0 | -37.4 | -38.7 |
| 2500.0 | 2700.0 | -36.7 | -33.7 |
| 2487.5 | 2700.0 | -35.1 | -24.2 |
| 2475.0 | 2700.0 | -20.0 | -19.7 |
| 2462.5 | 2700.0 | 8.4 | -17.5 |
| 2450.0 | 2700.0 | -14.9 | -4.7 |
| 2437.5 | 2700.0 | -25.8 | -.1 |
| 2425.0 | 2700.0 | 28.9 | -12.8 |
| 2412.5 | 2700.0 | 3.0 | -20.4 |
|  |  |  |  |


| 2400.0 | 2700.0 | -55.3 | -19.7 |
| ---: | ---: | ---: | ---: |
| 2387.5 | 2700.0 | -53.0 | -27.2 |
| 2375.0 | 2700.0 | -22.0 | -33.8 |
| 2362.5 | 2700.0 | -8.5 | -38.4 |
| 2350.0 | 2700.0 | -30.2 | -47.9 |
| 2337.5 | 2700.0 | -78.5 | -56.5 |
| 2325.0 | 2700.0 | -100.4 | -62.6 |
| 2312.5 | 2700.0 | -64.7 | -48.3 |
| 2300.0 | 2700.0 | -39.0 | -27.5 |
| 2287.5 | 2700.0 | 41.3 | -3.9 |
| 2275.0 | 2700.0 | 25.4 | 13.8 |
| 2262.5 | 2700.0 | 17.5 | 29.0 |
| 2250.0 | 2700.0 | 23.6 | 26.6 |
| 2237.5 | 2700.0 | 37.2 | 25.7 |
| 2225.0 | 2700.0 | 29.3 | 25.4 |
| 2212.5 | 2700.0 | 20.7 | 25.8 |
| 2200.0 | 2700.0 | 16.1 | 22.0 |

### 2.12 Line 2800 E

| 3400.0 | 2800.0 | -24.6 | -20.7 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 2800.0 | -21.6 | -19.4 |
| 3375.0 | 2800.0 | -15.9 | -18.6 |
| 3362.5 | 2800.0 | -15.4 | -17.8 |
| 3350.0 | 2800.0 | -15.5 | -17.6 |
| 3337.5 | 2800.0 | -20.6 | -15.8 |
| 3325.0 | 2800.0 | -20.4 | -6.3 |
| 3312.5 | 2800.0 | -7.2 | 8.8 |
| 3300.0 | 2800.0 | 32.2 | 24.5 |
| 3287.5 | 2800.0 | 60.1 | 39.3 |
| 3275.0 | 2800.0 | 57.6 | 51.0 |
| 3262.5 | 2800.0 | 54.0 | 52.7 |
| 3250.0 | 2800.0 | 51.0 | 47.9 |
| 3237.5 | 2800.0 | 41.0 | 42.5 |
| 3225.0 | 2800.0 | 35.7 | 38.0 |
| 3212.5 | 2800.0 | 30.6 | 34.3 |
| 3200.0 | 2800.0 | 31.9 | 32.2 |
| 3187.5 | 2800.0 | 32.2 | 31.6 |
| 3175.0 | 2800.0 | 30.6 | 30.3 |
| 3162.5 | 2800.0 | 32.6 | 27.6 |
| 3150.0 | 2800.0 | 24.0 | 24.3 |
| 3137.5 | 2800.0 | 18.8 | 20.6 |
| 3125.0 | 2800.0 | 15.7 | 16.0 |
| 3112.5 | 2800.0 | 12.1 | 12.3 |
| 3100.0 | 2800.0 | 9.5 | 8.9 |
| 3087.5 | 2800.0 | 5.5 | 5.6 |
| 3075.0 | 2800.0 | 1.6 | 2.7 |
| 3062.5 | 2800.0 | -.5 | -.2 |
| 3050.0 | 2800.0 | -2.4 | -3.1 |
| 3037.5 | 2800.0 | -5.2 | -5.3 |
| 3025.0 | 2800.0 | -9.2 | -7.0 |


| 3012.5 | 2800.0 | -9.1 | -9.6 |
| ---: | ---: | ---: | ---: |
| 3000.0 | 2800.0 | -9.2 | -12.0 |
| 2987.5 | 2800.0 | -15.1 | -14.9 |
| 2975.0 | 2800.0 | -17.5 | -18.4 |
| 2962.5 | 2800.0 | -23.6 | -22.3 |
| 2950.0 | 2800.0 | -26.8 | -25.5 |
| 2937.5 | 2800.0 | -28.5 | -27.4 |
| 2925.0 | 2800.0 | -30.9 | -27.6 |
| 2912.5 | 2800.0 | -27.2 | -28.5 |
| 2900.0 | 2800.0 | -24.8 | -29.3 |
| 2887.5 | 2800.0 | -31.3 | -29.9 |
| 2875.0 | 2800.0 | -32.3 | -30.8 |
| 2862.5 | 2800.0 | -34.0 | -31.0 |
| 2850.0 | 2800.0 | -31.7 | -28.3 |
| 2837.5 | 2800.0 | -25.8 | -26.2 |
| 2825.0 | 2800.0 | -17.8 | -23.6 |
| 2812.5 | 2800.0 | -21.8 | -22.0 |
| 2800.0 | 2800.0 | -20.7 | -22.6 |
| 2787.5 | 2800.0 | -24.1 | -23.3 |
| 2775.0 | 2800.0 | -28.8 | -22.6 |
| 2762.5 | 2800.0 | -21.1 | -23.1 |
| 2750.0 | 2800.0 | -18.2 | -23.5 |
| 2737.5 | 2800.0 | -23.2 | -23.4 |
| 2725.0 | 2800.0 | -26.3 | -26.2 |
| 2712.5 | 2800.0 | -28.1 | -30.7 |
| 2700.0 | 2800.0 | -35.2 | -35.1 |
| 2687.5 | 2800.0 | -40.5 | -39.8 |
| 2675.0 | 2800.0 | -45.4 | -43.8 |
| 2662.5 | 2800.0 | -49.8 | -46.9 |
| 2650.0 | 2800.0 | -48.0 | -49.4 |
| 2637.5 | 2800.0 | -50.7 | -50.1 |
| 2625.0 | 2800.0 | -53.0 | -52.3 |
| 2612.5 | 2800.0 | -49.2 | -51.6 |
| 2600.0 | 2800.0 | -60.5 | -38.3 |
| 2587.5 | 2800.0 | -44.6 | -21.2 |
| 2575.0 | 2800.0 | 15.6 | -14.8 |
| 2562.5 | 2800.0 | 32.6 | .3 |
| 2550.0 | 2800.0 | -17.1 | 10.5 |
| 2537.5 | 2800.0 | 15.2 | 13.3 |
| 2525.0 | 2800.0 | 6.3 | 17.1 |
| 2512.5 | 2800.0 | 29.3 | 24.9 |
| 2500.0 | 2800.0 | 51.9 | 27.8 |
| 2487.5 | 2800.0 | 21.8 | 35.8 |
| 2475.0 | 2800.0 | 29.9 | 31.8 |
| 2462.5 | 2800.0 | 46.0 | 20.1 |
| 2450.0 | 2800.0 | 9.3 | 12.0 |
| 2437.5 | 2800.0 | -6.4 | 15.8 |
| 2425.0 | 2800.0 | -18.7 | 14.5 |
| 2412.5 | 2800.0 | 49.0 | 18.5 |
| 2400.0 | 2800.0 | 39.2 | 25.3 |
| 2387.5 | 2800.0 | 29.5 | 34.9 |
| 2375.0 | 2800.0 | 27.5 | 32.2 |
| 2362.5 | 2800.0 | 29.5 | 23.7 |
|  |  |  |  |


| 2350.0 | 2800.0 | 35.2 | 12.3 |
| ---: | ---: | ---: | ---: |
| 2337.5 | 2800.0 | -3.3 | -2.4 |
| 2325.0 | 2800.0 | -27.6 | -17.7 |
| 2312.5 | 2800.0 | -45.7 | -30.8 |
| 2300.0 | 2800.0 | -47.2 | -43.7 |
| 2287.5 | 2800.0 | -30.1 | -49.8 |
| 2275.0 | 2800.0 | -68.0 | -51.1 |
| 2262.5 | 2800.0 | -58.0 | -53.6 |
| 2250.0 | 2800.0 | -52.1 | -59.2 |
| 2237.5 | 2800.0 | -59.6 | -60.0 |
| 2225.0 | 2800.0 | -58.4 | -64.0 |
| 2212.5 | 2800.0 | -71.7 | -67.0 |
| 2200.0 | 2800.0 | -78.4 | -69.5 |

### 2.13 Line 2900 E

| 2300.0 | 2900.0 | 30.9 | 11.8 |
| ---: | ---: | ---: | ---: |
| 2312.5 | 2900.0 | 32.4 | -2.8 |
| 2325.0 | 2900.0 | -27.9 | -7.9 |
| 2337.5 | 2900.0 | -46.5 | -18.3 |
| 2350.0 | 2900.0 | -28.2 | -39.3 |
| 2362.5 | 2900.0 | -21.2 | -47.7 |
| 2375.0 | 2900.0 | -72.7 | -47.4 |
| 2387.5 | 2900.0 | -69.9 | -42.4 |
| 2400.0 | 2900.0 | -45.1 | -37.8 |
| 2412.5 | 2900.0 | -3.2 | -27.8 |
| 2425.0 | 2900.0 | 1.9 | -14.5 |
| 2437.5 | 2900.0 | -22.9 | -5.9 |
| 2450.0 | 2900.0 | -3.1 | -3.1 |
| 2462.5 | 2900.0 | -2.0 | -5.4 |
| 2475.0 | 2900.0 | 10.6 | -5.4 |
| 2487.5 | 2900.0 | -9.6 | -9.1 |
| 2500.0 | 2900.0 | -22.9 | -11.9 |
| 2512.5 | 2900.0 | -21.7 | -15.8 |
| 2525.0 | 2900.0 | -15.7 | -5.9 |
| 2537.5 | 2900.0 | -9.2 | -3.4 |
| 2550.0 | 2900.0 | 39.9 | -6.9 |
| 2562.5 | 2900.0 | -10.4 | -14.5 |
| 2575.0 | 2900.0 | -39.2 | -18.0 |
| 2587.5 | 2900.0 | -53.6 | -38.5 |
| 2600.0 | 2900.0 | -26.6 | -46.3 |
| 2612.5 | 2900.0 | -62.5 | -44.7 |
| 2625.0 | 2900.0 | -49.4 | -44.9 |
| 2637.5 | 2900.0 | -31.3 | -50.7 |
| 2650.0 | 2900.0 | -54.7 | -49.4 |
| 2662.5 | 2900.0 | -55.6 | -50.8 |
| 2675.0 | 2900.0 | -55.8 | -54.7 |
| 2687.5 | 2900.0 | -56.7 | -52.9 |
| 2700.0 | 2900.0 | -50.9 | -50.3 |
| 2712.5 | 2900.0 | -45.5 | -43.1 |
| 2725.0 | 2900.0 | -42.6 | -37.8 |


| 2737.5 | 2900.0 | -19.6 | -34.7 |
| ---: | ---: | ---: | ---: |
| 2750.0 | 2900.0 | -30.4 | -32.7 |
| 2762.5 | 2900.0 | -35.6 | -31.5 |
| 2775.0 | 2900.0 | -35.2 | -34.2 |
| 2787.5 | 2900.0 | -36.9 | -30.9 |
| 2800.0 | 2900.0 | -32.7 | -29.6 |
| 2812.5 | 2900.0 | -14.2 | -28.5 |
| 2825.0 | 2900.0 | -29.2 | -27.1 |
| 2837.5 | 2900.0 | -29.4 | -27.6 |
| 2850.0 | 2900.0 | -29.8 | -31.3 |
| 2862.5 | 2900.0 | -35.2 | -30.5 |
| 2875.0 | 2900.0 | -32.7 | -29.4 |
| 2887.5 | 2900.0 | -25.3 | -27.1 |
| 2900.0 | 2900.0 | -23.8 | -22.8 |
| 2912.5 | 2900.0 | -18.5 | -18.7 |
| 2925.0 | 2900.0 | -13.8 | -16.0 |
| 2937.5 | 2900.0 | -11.9 | -13.5 |
| 2950.0 | 2900.0 | -11.8 | -11.9 |
| 2962.5 | 2900.0 | -11.5 | -9.8 |
| 2975.0 | 2900.0 | -10.3 | -9.3 |
| 2987.5 | 2900.0 | -3.7 | -10.2 |
| 3000.0 | 2900.0 | -9.4 | -5.8 |
| 3012.5 | 2900.0 | -16.1 | 30.5 |
| 3025.0 | 2900.0 | 10.4 | 133.3 |
| 3037.5 | 2900.0 | 171.3 | 95.7 |
| 3050.0 | 2900.0 | 510.3 | 75.5 |
| 3062.5 | 2900.0 | -197.5 | 65.6 |
| 3075.0 | 2900.0 | -117.1 | 27.7 |
| 3087.5 | 2900.0 | -38.9 | -73.2 |
| 3100.0 | 2900.0 | -18.4 | -1.9 |
| 3112.5 | 2900.0 | 5.7 | 17.9 |
| 3125.0 | 2900.0 | 159.1 | 21.4 |
| 3137.5 | 2900.0 | -18.1 | 21.5 |
| 3150.0 | 2900.0 | -21.1 | 16.3 |
| 3162.5 | 2900.0 | -18.3 | -19.8 |
| 3175.0 | 2900.0 | -19.9 | -20.4 |
| 3187.5 | 2900.0 | -21.7 | -19.3 |
| 3200.0 | 2900.0 | -21.1 | -18.8 |
| 3212.5 | 2900.0 | -15.7 | -16.9 |
| 3225.0 | 2900.0 | -15.6 | -14.3 |
| 3237.5 | 2900.0 | -10.3 | -11.5 |
| 3250.0 | 2900.0 | -8.7 | -8.4 |
| 3262.5 | 2900.0 | -7.3 | -4.6 |
| 3275.0 | 2900.0 | .0 | -1.3 |
| 3287.5 | 2900.0 | 3.5 | 1.8 |
| 3300.0 | 2900.0 | 6.2 | 4.8 |
| 3312.5 | 2900.0 | 6.7 | 6.7 |
| 3325.0 | 2900.0 | 7.8 | 9.4 |
| 3337.5 | 2900.0 | 9.5 | 11.6 |
| 3350.0 | 2900.0 | 16.6 | 14.3 |
| 3362.5 | 2900.0 | 17.4 | 16.9 |
| 3375.0 | 2900.0 | 20.0 | 19.5 |
| 3387.5 | 2900.0 | 21.2 | 20.3 |
| 3400.0 | 2900.0 | 22.4 | 21.2 |
|  |  |  |  |

### 2.14 Line 3000 E

| 3400.0 | 3000.0 | 176.9 | 198.1 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 3000.0 | 188.2 | 206.9 |
| 3375.0 | 3000.0 | 229.1 | 210.8 |
| 3362.5 | 3000.0 | 233.4 | 221.4 |
| 3350.0 | 3000.0 | 226.2 | 217.6 |
| 3337.5 | 3000.0 | 230.0 | 199.4 |
| 3325.0 | 3000.0 | 169.2 | 178.6 |
| 3312.5 | 3000.0 | 138.0 | 160.8 |
| 3300.0 | 3000.0 | 129.4 | 135.1 |
| 3287.5 | 3000.0 | 137.6 | 117.3 |
| 3275.0 | 3000.0 | 101.5 | 102.6 |
| 3262.5 | 3000.0 | 80.1 | 88.9 |
| 3250.0 | 3000.0 | 64.6 | 71.3 |
| 3237.5 | 3000.0 | 60.5 | 58.5 |
| 3225.0 | 3000.0 | 50.0 | 48.7 |
| 3212.5 | 3000.0 | 37.1 | 41.6 |
| 3200.0 | 3000.0 | 31.5 | 35.1 |
| 3187.5 | 3000.0 | 28.7 | 28.5 |
| 3175.0 | 3000.0 | 28.1 | 24.8 |
| 3162.5 | 3000.0 | 16.9 | 21.3 |
| 3150.0 | 3000.0 | 19.0 | 15.3 |
| 3137.5 | 3000.0 | 14.0 | 8.9 |
| 3125.0 | 3000.0 | -1.5 | 5.1 |
| 3112.5 | 3000.0 | -3.8 | .9 |
| 3100.0 | 3000.0 | -2.4 | -2.1 |
| 3087.5 | 3000.0 | -2.7 | -3.0 |
| 3075.0 | 3000.0 | -.1 | -4.9 |
| 3062.5 | 3000.0 | -6.4 | -6.6 |
| 3050.0 | 3000.0 | -13.1 | -8.3 |
| 3037.5 | 3000.0 | -11.1 | -10.4 |
| 3025.0 | 3000.0 | -11.0 | -9.7 |
| 3012.5 | 3000.0 | -10.3 | -8.5 |
| 3000.0 | 3000.0 | -3.1 | -9.2 |
| 2987.5 | 3000.0 | -7.2 | -11.3 |
| 2975.0 | 3000.0 | -14.5 | -13.3 |
| 2962.5 | 3000.0 | -21.5 | -16.3 |
| 2950.0 | 3000.0 | -20.1 | -19.0 |
| 2937.5 | 3000.0 | -18.0 | -20.4 |
| 2925.0 | 3000.0 | -21.1 | -20.4 |
| 2912.5 | 3000.0 | -21.1 | -22.2 |
| 2900.0 | 3000.0 | -21.7 | -26.7 |
| 2887.5 | 3000.0 | -29.2 | -29.5 |
| 2875.0 | 3000.0 | -40.3 | -31.9 |
| 2862.5 | 3000.0 | -35.4 | -37.5 |
| 2850.0 | 3000.0 | -33.1 | -40.8 |
| 2837.5 | 3000.0 | -49.7 | -41.8 |
| 2825.0 | 3000.0 | -45.3 | -43.8 |
| 2812.5 | 3000.0 | -45.6 | -45.8 |
| 2800.0 | 3000.0 | -45.1 | -44.2 |
| 2787.5 | 3000.0 | -43.3 | -42.9 |
| 2775.0 | 3000.0 | -41.7 | -41.1 |
|  |  |  |  |


| 2762.5 | 3000.0 | -38.9 | -39.4 |
| ---: | ---: | ---: | ---: |
| 2750.0 | 3000.0 | -36.4 | -37.0 |
| 2737.5 | 3000.0 | -36.9 | -33.8 |
| 2725.0 | 3000.0 | -31.0 | -31.7 |
| 2712.5 | 3000.0 | -25.9 | -30.3 |
| 2700.0 | 3000.0 | -28.3 | -21.0 |
| 2687.5 | 3000.0 | -29.3 | -6.9 |
| 2675.0 | 3000.0 | 9.7 | 7.3 |
| 2662.5 | 3000.0 | 39.3 | 20.8 |
| 2650.0 | 3000.0 | 45.1 | 34.2 |
| 2637.5 | 3000.0 | 39.1 | 43.7 |
| 2625.0 | 3000.0 | 37.6 | 49.8 |
| 2612.5 | 3000.0 | 57.6 | 55.5 |
| 2600.0 | 3000.0 | 69.8 | 59.5 |
| 2587.5 | 3000.0 | 73.5 | 59.4 |
| 2575.0 | 3000.0 | 58.9 | 50.9 |
| 2562.5 | 3000.0 | 37.0 | 40.5 |
| 2550.0 | 3000.0 | 15.5 | 26.2 |
| 2537.5 | 3000.0 | 17.5 | 14.0 |
| 2525.0 | 3000.0 | 2.3 | 4.8 |
| 2512.5 | 3000.0 | -2.3 | -2.6 |
| 2500.0 | 3000.0 | -9.2 | -2.0 |
| 2487.5 | 3000.0 | -21.2 | -8.2 |
| 2475.0 | 3000.0 | 20.3 | -17.6 |
| 2462.5 | 3000.0 | -28.4 | -24.9 |
| 2450.0 | 3000.0 | -49.6 | -24.7 |
| 2437.5 | 3000.0 | -45.6 | -26.6 |
| 2425.0 | 3000.0 | -20.3 | -25.0 |
| 2412.5 | 3000.0 | 10.7 | -20.0 |
| 2400.0 | 3000.0 | -20.3 | -14.5 |
| 2387.5 | 3000.0 | -24.5 | -10.8 |
| 2375.0 | 3000.0 | -18.2 | -10.8 |
| 2362.5 | 3000.0 | -1.7 | -2.7 |
| 2350.0 | 3000.0 | 10.8 | 6.4 |
| 2337.5 | 3000.0 | 19.9 | 7.8 |
| 2325.0 | 3000.0 | 21.0 | 6.2 |
| 2312.5 | 3000.0 | -10.8 | 5.0 |
| 2300.0 | 3000.0 | -10.1 | .0 |
|  |  |  |  |

### 2.15 Line 3100 E

| 2400.0 | 3100.0 | -47.0 | -43.6 |
| ---: | ---: | ---: | ---: |
| 2412.5 | 3100.0 | -44.3 | -41.3 |
| 2425.0 | 3100.0 | -39.4 | -39.4 |
| 2437.5 | 3100.0 | -34.5 | -34.5 |
| 2450.0 | 3100.0 | -31.9 | -28.0 |
| 2462.5 | 3100.0 | -22.4 | -20.4 |
| 2475.0 | 3100.0 | -12.0 | -14.9 |
| 2487.5 | 3100.0 | -1.0 | -11.0 |
| 2500.0 | 3100.0 | -7.1 | -9.4 |
| 2512.5 | 3100.0 | -12.3 | -10.2 |


| 2525.0 | 3100.0 | -14.5 | -13.3 |
| ---: | ---: | ---: | ---: |
| 2537.5 | 3100.0 | -16.0 | -14.2 |
| 2550.0 | 3100.0 | -16.5 | -14.5 |
| 2562.5 | 3100.0 | -11.5 | -14.0 |
| 2575.0 | 3100.0 | -13.8 | -13.1 |
| 2587.5 | 3100.0 | -12.4 | -13.0 |
| 2600.0 | 3100.0 | -11.2 | -15.5 |
| 2612.5 | 3100.0 | -16.0 | -17.8 |
| 2625.0 | 3100.0 | -24.2 | -20.0 |
| 2637.5 | 3100.0 | -25.2 | -21.3 |
| 2650.0 | 3100.0 | -23.6 | -19.8 |
| 2662.5 | 3100.0 | -17.4 | -16.5 |
| 2675.0 | 3100.0 | -8.8 | -14.3 |
| 2687.5 | 3100.0 | -7.3 | -13.1 |
| 2700.0 | 3100.0 | -14.5 | -12.5 |
| 2712.5 | 3100.0 | -17.3 | -11.4 |
| 2725.0 | 3100.0 | -14.4 | -12.4 |
| 2737.5 | 3100.0 | -3.5 | -12.7 |
| 2750.0 | 3100.0 | -12.5 | -11.4 |
| 2762.5 | 3100.0 | -16.0 | -12.6 |
| 2775.0 | 3100.0 | -10.5 | -18.2 |
| 2787.5 | 3100.0 | -20.6 | -17.0 |
| 2800.0 | 3100.0 | -31.2 | -14.6 |
| 2812.5 | 3100.0 | -6.8 | -15.8 |
| 2825.0 | 3100.0 | -4.0 | -13.0 |
| 2837.5 | 3100.0 | -16.3 | -12.2 |
| 2850.0 | 3100.0 | -6.8 | -15.7 |
| 2862.5 | 3100.0 | -27.2 | -24.8 |
| 2875.0 | 3100.0 | -24.0 | -32.0 |
| 2887.5 | 3100.0 | -49.7 | -36.0 |
| 2900.0 | 3100.0 | -52.3 | -32.7 |
| 2912.5 | 3100.0 | -26.9 | -30.6 |
| 2925.0 | 3100.0 | -10.4 | -19.6 |
| 2937.5 | 3100.0 | -13.9 | -7.2 |
| 2950.0 | 3100.0 | 5.7 | 3.4 |
| 2962.5 | 3100.0 | 9.6 | 14.2 |
| 2975.0 | 3100.0 | 26.0 | 26.6 |
| 2987.5 | 3100.0 | 43.5 | 33.4 |
| 3000.0 | 3100.0 | 48.0 | 40.2 |
| 3012.5 | 3100.0 | 39.7 | 45.5 |
| 3025.0 | 3100.0 | 43.8 | 50.1 |
| 3037.5 | 3100.0 | 52.5 | 60.4 |
| 3050.0 | 3100.0 | 66.7 | 78.3 |
| 3062.5 | 3100.0 | 99.4 | 103.5 |
| 3075.0 | 3100.0 | 129.2 | 133.7 |
| 3087.5 | 3100.0 | 169.9 | 178.1 |
| 3100.0 | 3100.0 | 203.3 | 206.0 |
| 3112.5 | 3100.0 | 288.8 | 218.3 |
| 3125.0 | 3100.0 | 238.6 | 226.0 |
| 3137.5 | 3100.0 | 190.7 | 235.2 |
| 3150.0 | 3100.0 | 208.5 | 215.7 |
| 3162.5 | 3100.0 | 249.4 | 175.5 |
| 3175.0 | 3100.0 | 191.4 | 133.2 |
|  |  |  |  |


| 3187.5 | 3100.0 | 37.3 | 84.2 |
| ---: | ---: | ---: | ---: |
| 3200.0 | 3100.0 | -20.4 | 33.2 |
| 3212.5 | 3100.0 | -36.8 | -6.6 |
| 3225.0 | 3100.0 | -5.5 | -19.8 |
| 3237.5 | 3100.0 | -7.7 | -21.3 |
| 3250.0 | 3100.0 | -28.8 | -18.3 |
| 3262.5 | 3100.0 | -27.8 | -21.1 |
| 3275.0 | 3100.0 | -21.5 | -24.3 |
| 3287.5 | 3100.0 | -19.5 | -25.5 |
| 3300.0 | 3100.0 | -23.9 | -29.5 |
| 3312.5 | 3100.0 | -34.8 | -35.2 |
| 3325.0 | 3100.0 | -48.0 | -41.1 |
| 3337.5 | 3100.0 | -49.7 | -45.8 |
| 3350.0 | 3100.0 | -48.9 | -45.0 |
| 3362.5 | 3100.0 | -47.5 | -39.1 |
| 3375.0 | 3100.0 | -31.0 | -25.0 |
| 3387.5 | 3100.0 | -18.4 | -19.0 |
| 3400.0 | 3100.0 | 21.0 | -9.5 |

### 2.16 Line 3200 E

| 3400.0 | 3200.0 | 50.2 | 57.9 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 3200.0 | 75.9 | 60.6 |
| 3375.0 | 3200.0 | 47.6 | 80.9 |
| 3362.5 | 3200.0 | 68.7 | 97.8 |
| 3350.0 | 3200.0 | 161.9 | 90.7 |
| 3337.5 | 3200.0 | 135.1 | 92.3 |
| 3325.0 | 3200.0 | 40.0 | 86.5 |
| 3312.5 | 3200.0 | 55.7 | 54.6 |
| 3300.0 | 3200.0 | 39.6 | 24.2 |
| 3287.5 | 3200.0 | 2.7 | 11.9 |
| 3275.0 | 3200.0 | -16.8 | -3.3 |
| 3262.5 | 3200.0 | -21.7 | -15.5 |
| 3250.0 | 3200.0 | -20.1 | -20.3 |
| 3237.5 | 3200.0 | -21.4 | -23.4 |
| 3225.0 | 3200.0 | -21.3 | -25.4 |
| 3212.5 | 3200.0 | -32.3 | -28.1 |
| 3200.0 | 3200.0 | -32.0 | -28.7 |
| 3187.5 | 3200.0 | -33.4 | -30.6 |
| 3175.0 | 3200.0 | -24.7 | -30.0 |
| 3162.5 | 3200.0 | -30.7 | -29.4 |
| 3150.0 | 3200.0 | -29.2 | -29.1 |
| 3137.5 | 3200.0 | -29.0 | -32.3 |
| 3125.0 | 3200.0 | -31.7 | -33.9 |
| 3112.5 | 3200.0 | -41.1 | -33.8 |
| 3100.0 | 3200.0 | -38.5 | -34.2 |
| 3087.5 | 3200.0 | -28.8 | -33.5 |
| 3075.0 | 3200.0 | -30.9 | -29.7 |
| 3062.5 | 3200.0 | -28.2 | -19.8 |
| 3050.0 | 3200.0 | -22.2 | -7.4 |
| 3037.5 | 3200.0 | 11.2 | 16.1 |


| 3025.0 | 3200.0 | 33.1 | 56.9 |
| ---: | ---: | ---: | ---: |
| 3012.5 | 3200.0 | 86.5 | 126.0 |
| 3000.0 | 3200.0 | 175.7 | 216.2 |
| 2987.5 | 3200.0 | 323.6 | 309.1 |
| 2975.0 | 3200.0 | 462.0 | 376.7 |
| 2962.5 | 3200.0 | 497.8 | 392.9 |
| 2950.0 | 3200.0 | 424.2 | 357.7 |
| 2937.5 | 3200.0 | 256.8 | 291.8 |
| 2925.0 | 3200.0 | 147.6 | 229.9 |
| 2912.5 | 3200.0 | 132.6 | 176.8 |
| 2900.0 | 3200.0 | 188.3 | 155.6 |
| 2887.5 | 3200.0 | 158.6 | 155.2 |
| 2875.0 | 3200.0 | 150.9 | 153.1 |
| 2862.5 | 3200.0 | 145.7 | 134.3 |
| 2850.0 | 3200.0 | 122.1 | 120.0 |
| 2837.5 | 3200.0 | 94.4 | 101.2 |
| 2825.0 | 3200.0 | 87.0 | 81.5 |
| 2812.5 | 3200.0 | 56.7 | 65.2 |
| 2800.0 | 3200.0 | 47.4 | 52.2 |
| 2787.5 | 3200.0 | 40.5 | 38.3 |
| 2775.0 | 3200.0 | 29.6 | 30.0 |
| 2762.5 | 3200.0 | 17.2 | 23.5 |
| 2750.0 | 3200.0 | 15.5 | 17.0 |
| 2737.5 | 3200.0 | 14.8 | 11.6 |
| 2725.0 | 3200.0 | 7.8 | 8.0 |
| 2712.5 | 3200.0 | 2.5 | 3.5 |
| 2700.0 | 3200.0 | -.5 | -2.2 |
| 2687.5 | 3200.0 | -7.0 | -7.5 |
| 2675.0 | 3200.0 | -13.8 | -12.5 |
| 2662.5 | 3200.0 | -18.7 | -17.3 |
| 2650.0 | 3200.0 | -22.5 | -20.8 |
| 2637.5 | 3200.0 | -24.6 | -22.8 |
| 2625.0 | 3200.0 | -24.4 | -23.9 |
| 2612.5 | 3200.0 | -23.7 | -24.9 |
| 2600.0 | 3200.0 | -24.5 | -24.8 |
| 2587.5 | 3200.0 | -27.2 | -24.1 |
| 2575.0 | 3200.0 | -24.3 | -22.1 |
| 2562.5 | 3200.0 | -20.9 | -19.4 |
| 2550.0 | 3200.0 | -13.7 | -17.1 |
| 2537.5 | 3200.0 | -10.7 | -17.4 |
| 2525.0 | 3200.0 | -15.7 | -19.9 |
| 2512.5 | 3200.0 | -26.2 | -24.5 |
| 2500.0 | 3200.0 | -33.0 | -30.6 |
| 2487.5 | 3200.0 | -37.0 | -35.8 |
| 2475.0 | 3200.0 | -41.1 | -38.4 |
| 2462.5 | 3200.0 | -41.5 | -39.7 |
| 2450.0 | 3200.0 | -39.6 | -40.5 |
| 2437.5 | 3200.0 | -39.4 | -40.4 |
| 2425.0 | 3200.0 | -40.7 | -40.8 |
| 2412.5 | 3200.0 | -41.0 | -41.1 |
| 2400.0 | 3200.0 | -43.3 | -41.7 |
|  |  |  |  |

2.17 Line 3300 E

| 2400.0 | 3300.0 | -1.7 | 6.9 |
| ---: | ---: | ---: | ---: |
| 2412.5 | 3300.0 | 6.8 | 10.8 |
| 2425.0 | 3300.0 | 15.7 | 14.4 |
| 2437.5 | 3300.0 | 22.4 | 13.2 |
| 2450.0 | 3300.0 | 28.7 | 7.1 |
| 2462.5 | 3300.0 | -7.5 | -1.1 |
| 2475.0 | 3300.0 | -23.8 | -11.0 |
| 2487.5 | 3300.0 | -25.5 | -22.5 |
| 2500.0 | 3300.0 | -26.9 | -26.2 |
| 2512.5 | 3300.0 | -29.0 | -25.9 |
| 2525.0 | 3300.0 | -25.6 | -24.9 |
| 2537.5 | 3300.0 | -22.5 | -23.0 |
| 2550.0 | 3300.0 | -20.3 | -21.1 |
| 2562.5 | 3300.0 | -17.7 | -19.5 |
| 2575.0 | 3300.0 | -19.6 | -18.2 |
| 2587.5 | 3300.0 | -17.4 | -16.9 |
| 2600.0 | 3300.0 | -16.1 | -15.7 |
| 2612.5 | 3300.0 | -13.8 | -13.9 |
| 2625.0 | 3300.0 | -11.6 | -11.7 |
| 2637.5 | 3300.0 | -10.5 | -8.2 |
| 2650.0 | 3300.0 | -6.3 | -3.7 |
| 2662.5 | 3300.0 | 1.3 | 2.0 |
| 2675.0 | 3300.0 | 8.5 | 9.6 |
| 2687.5 | 3300.0 | 16.9 | 18.7 |
| 2700.0 | 3300.0 | 27.7 | 29.9 |
| 2712.5 | 3300.0 | 39.2 | 43.8 |
| 2725.0 | 3300.0 | 57.4 | 59.0 |
| 2737.5 | 3300.0 | 77.6 | 73.0 |
| 2750.0 | 3300.0 | 93.2 | 85.5 |
| 2762.5 | 3300.0 | 97.7 | 92.2 |
| 2775.0 | 3300.0 | 101.7 | 90.0 |
| 2787.5 | 3300.0 | 90.8 | 80.9 |
| 2800.0 | 3300.0 | 66.4 | 67.9 |
| 2812.5 | 3300.0 | 47.9 | 54.3 |
| 2825.0 | 3300.0 | 32.5 | 43.4 |
| 2837.5 | 3300.0 | 33.9 | 40.3 |
| 2850.0 | 3300.0 | 36.5 | 40.6 |
| 2862.5 | 3300.0 | 50.6 | 39.4 |
| 2875.0 | 3300.0 | 49.5 | 33.3 |
| 2887.5 | 3300.0 | 26.3 | 23.9 |
| 2900.0 | 3300.0 | 3.4 | 10.6 |
| 2912.5 | 3300.0 | -10.3 | -3.9 |
| 2925.0 | 3300.0 | -16.0 | -15.7 |
| 2937.5 | 3300.0 | -22.8 | -23.9 |
| 2950.0 | 3300.0 | -32.7 | -29.5 |
| 2962.5 | 3300.0 | -37.9 | -34.8 |
| 2975.0 | 3300.0 | -38.0 | -41.0 |
| 2987.5 | 3300.0 | -42.6 | -45.9 |
| 3000.0 | 3300.0 | -53.9 | -51.3 |
| 3012.5 | 3300.0 | -57.2 | -55.8 |
| 3025.0 | 3300.0 | -64.9 | -54.8 |
| 2 |  |  |  |


| 3037.5 | 3300.0 | -60.2 | -49.0 |
| ---: | ---: | ---: | ---: |
| 3050.0 | 3300.0 | -37.7 | -35.6 |
| 3062.5 | 3300.0 | -24.9 | -26.4 |
| 3075.0 | 3300.0 | 9.6 | -10.6 |
| 3087.5 | 3300.0 | -18.9 | 3.6 |
| 3100.0 | 3300.0 | 18.9 | 14.1 |
| 3112.5 | 3300.0 | 33.4 | 7.6 |
| 3125.0 | 3300.0 | 27.7 | 2.5 |
| 3137.5 | 3300.0 | -22.9 | -8.2 |
| 3150.0 | 3300.0 | -44.6 | -19.1 |
| 3162.5 | 3300.0 | -34.7 | -27.5 |
| 3175.0 | 3300.0 | -20.8 | -21.8 |
| 3187.5 | 3300.0 | -14.5 | -8.4 |
| 3200.0 | 3300.0 | 5.5 | 19.6 |
| 3212.5 | 3300.0 | 22.5 | 89.2 |
| 3225.0 | 3300.0 | 105.4 | 186.9 |
| 3237.5 | 3300.0 | 327.3 | 224.8 |
| 3250.0 | 3300.0 | 474.0 | 204.7 |
| 3262.5 | 3300.0 | 194.7 | 163.5 |
| 3275.0 | 3300.0 | -77.9 | 80.6 |
| 3287.5 | 3300.0 | -100.5 | -29.7 |
| 3300.0 | 3300.0 | -87.3 | -80.1 |
| 3312.5 | 3300.0 | -77.7 | -75.7 |
| 3325.0 | 3300.0 | -57.0 | -64.6 |
| 3337.5 | 3300.0 | -56.1 | -55.5 |
| 3350.0 | 3300.0 | -45.0 | -49.4 |
| 3362.5 | 3300.0 | -41.9 | -45.6 |
| 3375.0 | 3300.0 | -46.9 | -41.7 |
| 3387.5 | 3300.0 | -38.1 | -40.8 |
| 3400.0 | 3300.0 | -36.4 | -40.5 |

2.18 Line 3400 E

| 3400.0 | 3400.0 | -44.7 | -44.5 |
| :--- | :--- | :--- | :--- |
| 3387.5 | 3400.0 | -45.9 | -43.6 |
| 3375.0 | 3400.0 | -43.0 | -43.5 |
| 3362.5 | 3400.0 | -40.9 | -43.4 |
| 3350.0 | 3400.0 | -42.9 | -45.5 |
| 3337.5 | 3400.0 | -44.1 | -47.4 |
| 3325.0 | 3400.0 | -56.5 | -51.2 |
| 3312.5 | 3400.0 | -52.7 | -55.6 |
| 3300.0 | 3400.0 | -59.7 | -61.2 |
| 3287.5 | 3400.0 | -64.8 | -59.7 |
| 3275.0 | 3400.0 | -72.3 | -67.8 |
| 3262.5 | 3400.0 | -49.1 | -69.9 |
| 3250.0 | 3400.0 | -93.0 | -71.2 |
| 3237.5 | 3400.0 | -70.2 | -69.6 |
| 3225.0 | 3400.0 | -71.2 | -72.2 |
| 3212.5 | 3400.0 | -64.5 | -66.9 |
| 3200.0 | 3400.0 | -61.9 | -64.8 |
| 3187.5 | 3400.0 | -66.9 | -63.9 |


| 3175.0 | 3400.0 | -59.6 | -64.8 |
| ---: | ---: | ---: | ---: |
| 3162.5 | 3400.0 | -66.8 | -66.3 |
| 3150.0 | 3400.0 | -68.8 | -64.7 |
| 3137.5 | 3400.0 | -69.5 | -57.3 |
| 3125.0 | 3400.0 | -58.9 | -35.6 |
| 3112.5 | 3400.0 | -22.7 | -.2 |
| 3100.0 | 3400.0 | 41.8 | 41.3 |
| 3087.5 | 3400.0 | 108.4 | 76.0 |
| 3075.0 | 3400.0 | 138.1 | 95.4 |
| 3062.5 | 3400.0 | 114.2 | 100.5 |
| 3050.0 | 3400.0 | 74.4 | 88.1 |
| 3037.5 | 3400.0 | 67.2 | 75.9 |
| 3025.0 | 3400.0 | 46.8 | 57.4 |
| 3012.5 | 3400.0 | 76.8 | 41.6 |
| 3000.0 | 3400.0 | 22.0 | 28.8 |
| 2987.5 | 3400.0 | -4.6 | 27.8 |
| 2975.0 | 3400.0 | 3.2 | 16.6 |
| 2962.5 | 3400.0 | 41.6 | 9.4 |
| 2950.0 | 3400.0 | 20.6 | 6.4 |
| 2937.5 | 3400.0 | -14.0 | 2.8 |
| 2925.0 | 3400.0 | -19.3 | -5.7 |
| 2912.5 | 3400.0 | -14.9 | -6.0 |
| 2900.0 | 3400.0 | -.9 | .9 |
| 2887.5 | 3400.0 | 19.0 | 7.7 |
| 2875.0 | 3400.0 | 20.4 | 12.0 |
| 2862.5 | 3400.0 | 14.9 | 12.0 |
| 2850.0 | 3400.0 | 6.6 | 7.0 |
| 2837.5 | 3400.0 | -.8 | 2.5 |
| 2825.0 | 3400.0 | -6.0 | .5 |
| 2812.5 | 3400.0 | -2.0 | 2.7 |
| 2800.0 | 3400.0 | 4.5 | 10.2 |
| 2787.5 | 3400.0 | 17.8 | 20.1 |
| 2775.0 | 3400.0 | 36.8 | 25.0 |
| 2762.5 | 3400.0 | 43.5 | 29.6 |
| 2750.0 | 3400.0 | 22.2 | 31.7 |
| 2737.5 | 3400.0 | 27.6 | 25.3 |
| 2725.0 | 3400.0 | 28.5 | 16.4 |
| 2712.5 | 3400.0 | 4.6 | 10.0 |
| 2700.0 | 3400.0 | -1.0 | 1.7 |
| 2687.5 | 3400.0 | -9.5 | -6.8 |
| 2675.0 | 3400.0 | -14.2 | -10.5 |
| 2662.5 | 3400.0 | -13.9 | -13.2 |
| 2650.0 | 3400.0 | -14.0 | -14.3 |
| 2637.5 | 3400.0 | -14.5 | -14.0 |
| 2625.0 | 3400.0 | -15.1 | -13.0 |
| 2612.5 | 3400.0 | -12.7 | -12.1 |
| 2600.0 | 3400.0 | -8.5 | -11.2 |
| 2587.5 | 3400.0 | -9.8 | -10.6 |
| 2575.0 | 3400.0 | -9.9 | -9.9 |
| 2562.5 | 3400.0 | -12.0 | -10.1 |
| 2550.0 | 3400.0 | -9.1 | -10.3 |
| 2537.5 | 3400.0 | -9.8 | -10.9 |
| 2525.0 | 3400.0 | -10.7 | -11.2 |
|  |  |  |  |


| 2512.5 | 3400.0 | -12.7 | -12.2 |
| :--- | :--- | :--- | :--- |
| 2500.0 | 3400.0 | -13.8 | -13.2 |
| 2487.5 | 3400.0 | -14.2 | -15.0 |
| 2475.0 | 3400.0 | -14.5 | -16.4 |
| 2462.5 | 3400.0 | -19.7 | -17.0 |
| 2450.0 | 3400.0 | -19.9 | -17.6 |
| 2437.5 | 3400.0 | -16.5 | -18.2 |
| 2425.0 | 3400.0 | -17.4 | -17.9 |
| 2412.5 | 3400.0 | -17.4 | -17.4 |
| 2400.0 | 3400.0 | -18.2 | -17.7 |

### 2.19 Line 3500 E

| 2500.0 | 3500.0 | -5.3 | -1.9 |
| ---: | ---: | ---: | ---: |
| 2512.5 | 3500.0 | -2.2 | .1 |
| 2525.0 | 3500.0 | 1.7 | 1.5 |
| 2537.5 | 3500.0 | 6.4 | 3.9 |
| 2550.0 | 3500.0 | 6.9 | 6.1 |
| 2562.5 | 3500.0 | 6.8 | 8.0 |
| 2575.0 | 3500.0 | 8.8 | 8.9 |
| 2587.5 | 3500.0 | 10.9 | 9.4 |
| 2600.0 | 3500.0 | 11.1 | 10.6 |
| 2612.5 | 3500.0 | 9.6 | 11.8 |
| 2625.0 | 3500.0 | 12.4 | 14.7 |
| 2637.5 | 3500.0 | 15.0 | 20.3 |
| 2650.0 | 3500.0 | 25.4 | 27.9 |
| 2662.5 | 3500.0 | 38.9 | 36.2 |
| 2675.0 | 3500.0 | 47.7 | 43.6 |
| 2687.5 | 3500.0 | 54.2 | 49.9 |
| 2700.0 | 3500.0 | 51.7 | 53.9 |
| 2712.5 | 3500.0 | 56.9 | 63.8 |
| 2725.0 | 3500.0 | 58.9 | 89.5 |
| 2737.5 | 3500.0 | 97.2 | 119.4 |
| 2750.0 | 3500.0 | 182.8 | 114.8 |
| 2762.5 | 3500.0 | 201.2 | 102.3 |
| 2775.0 | 3500.0 | 33.7 | 80.1 |
| 2787.5 | 3500.0 | -3.3 | 39.2 |
| 2800.0 | 3500.0 | -13.7 | -6.0 |
| 2812.5 | 3500.0 | -22.0 | -17.8 |
| 2825.0 | 3500.0 | -24.9 | -21.9 |
| 2837.5 | 3500.0 | -24.9 | -23.3 |
| 2850.0 | 3500.0 | -24.0 | -23.1 |
| 2862.5 | 3500.0 | -20.8 | -22.8 |
| 2875.0 | 3500.0 | -20.8 | -19.5 |
| 2887.5 | 3500.0 | -23.6 | -17.3 |
| 2900.0 | 3500.0 | -8.4 | -18.3 |
| 2912.5 | 3500.0 | -12.8 | -17.7 |
| 2925.0 | 3500.0 | -25.7 | -16.2 |
| 2937.5 | 3500.0 | -18.1 | -16.9 |
| 2950.0 | 3500.0 | -16.2 | -15.7 |
| 2962.5 | 3500.0 | -11.8 | -9.1 |


| 2975.0 | 3500.0 | -6.8 | -6.2 |
| ---: | ---: | ---: | ---: |
| 2987.5 | 3500.0 | 7.4 | -3.7 |
| 3000.0 | 3500.0 | -3.7 | -2.7 |
| 3012.5 | 3500.0 | -3.8 | .4 |
| 3025.0 | 3500.0 | -6.5 | 21.8 |
| 3037.5 | 3500.0 | 8.8 | 36.0 |
| 3050.0 | 3500.0 | 114.1 | 29.5 |
| 3062.5 | 3500.0 | 67.5 | 22.2 |
| 3075.0 | 3500.0 | -36.3 | 14.8 |
| 3087.5 | 3500.0 | -43.0 | -12.1 |
| 3100.0 | 3500.0 | -28.3 | -29.5 |
| 3112.5 | 3500.0 | -20.5 | -28.8 |
| 3125.0 | 3500.0 | -19.6 | -29.5 |
| 3137.5 | 3500.0 | -32.6 | -34.2 |
| 3150.0 | 3500.0 | -46.5 | -32.9 |
| 3162.5 | 3500.0 | -51.7 | -42.3 |
| 3175.0 | 3500.0 | -14.2 | -45.8 |
| 3187.5 | 3500.0 | -66.7 | -49.6 |
| 3200.0 | 3500.0 | -50.0 | -53.6 |
| 3212.5 | 3500.0 | -65.6 | -63.6 |
| 3225.0 | 3500.0 | -71.3 | -60.6 |
| 3237.5 | 3500.0 | -64.5 | -61.8 |
| 3250.0 | 3500.0 | -51.8 | -59.5 |
| 3262.5 | 3500.0 | -56.0 | -51.4 |
| 3275.0 | 3500.0 | -53.8 | -45.6 |
| 3287.5 | 3500.0 | -31.1 | -44.7 |
| 3300.0 | 3500.0 | -35.2 | -43.7 |
| 3312.5 | 3500.0 | -47.4 | -49.5 |
| 3325.0 | 3500.0 | -50.8 | -52.4 |
| 3337.5 | 3500.0 | -83.2 | -41.4 |
| 3350.0 | 3500.0 | -45.2 | -37.4 |
| 3362.5 | 3500.0 | 19.4 | -28.3 |
| 3375.0 | 3500.0 | -27.1 | -1.9 |
| 3387.5 | 3500.0 | -5.2 | 9.0 |
| 3400.0 | 3500.0 | 48.8 | 5.5 |

### 2.20 Line 3600 E

| 3400.0 | 3600.0 | -9.5 | -18.6 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 3600.0 | -19.1 | -19.9 |
| 3375.0 | 3600.0 | -27.1 | -13.4 |
| 3362.5 | 3600.0 | -23.9 | -4.6 |
| 3350.0 | 3600.0 | 12.7 | -6.1 |
| 3337.5 | 3600.0 | 34.2 | -2.7 |
| 3325.0 | 3600.0 | -26.3 | -4.2 |
| 3312.5 | 3600.0 | -10.3 | -11.6 |
| 3300.0 | 3600.0 | -31.5 | -25.0 |
| 3287.5 | 3600.0 | -24.3 | -17.5 |
| 3275.0 | 3600.0 | -32.7 | 27.4 |
| 3262.5 | 3600.0 | 11.1 | 46.5 |
| 3250.0 | 3600.0 | 214.5 | 57.2 |


| 3237.5 | 3600.0 | 63.9 | 68.8 |
| ---: | ---: | ---: | ---: |
| 3225.0 | 3600.0 | 29.0 | 90.1 |
| 3212.5 | 3600.0 | 25.3 | 76.6 |
| 3200.0 | 3600.0 | 117.9 | 77.4 |
| 3187.5 | 3600.0 | 146.7 | 74.3 |
| 3175.0 | 3600.0 | 68.3 | 64.5 |
| 3162.5 | 3600.0 | 13.3 | 38.3 |
| 3150.0 | 3600.0 | -23.7 | 6.8 |
| 3137.5 | 3600.0 | -13.2 | -8.7 |
| 3125.0 | 3600.0 | -10.9 | -5.9 |
| 3112.5 | 3600.0 | -8.8 | 19.4 |
| 3100.0 | 3600.0 | 27.2 | 32.7 |
| 3087.5 | 3600.0 | 102.9 | 37.8 |
| 3075.0 | 3600.0 | 53.0 | 41.6 |
| 3062.5 | 3600.0 | 14.6 | 37.0 |
| 3050.0 | 3600.0 | 10.2 | 17.9 |
| 3037.5 | 3600.0 | 4.2 | 8.6 |
| 3025.0 | 3600.0 | 7.6 | 5.7 |
| 3012.5 | 3600.0 | 6.6 | -.8 |
| 3000.0 | 3600.0 | -14.1 | -2.9 |
| 2987.5 | 3600.0 | -14.1 | -5.3 |
| 2975.0 | 3600.0 | -14.4 | -8.6 |
| 2962.5 | 3600.0 | -4.7 | -11.7 |
| 2950.0 | 3600.0 | -9.8 | -10.6 |
| 2937.5 | 3600.0 | -15.5 | -9.0 |
| 2925.0 | 3600.0 | -8.6 | -9.9 |
| 2912.5 | 3600.0 | -6.3 | -10.7 |
| 2900.0 | 3600.0 | -9.4 | -11.0 |
| 2887.5 | 3600.0 | -13.7 | -12.0 |
| 2875.0 | 3600.0 | -17.2 | -14.0 |
| 2862.5 | 3600.0 | -13.4 | -15.5 |
| 2850.0 | 3600.0 | -16.2 | -15.9 |
| 2837.5 | 3600.0 | -17.0 | -15.4 |
| 2825.0 | 3600.0 | -15.9 | -14.9 |
| 2812.5 | 3600.0 | -14.4 | -13.1 |
| 2800.0 | 3600.0 | -11.0 | -9.7 |
| 2787.5 | 3600.0 | -7.2 | -5.0 |
| 2775.0 | 3600.0 | .1 | .0 |
| 2762.5 | 3600.0 | 7.3 | 8.8 |
| 2750.0 | 3600.0 | 14.3 | 18.2 |
| 2737.5 | 3600.0 | 29.3 | 25.1 |
| 2725.0 | 3600.0 | 39.9 | 34.6 |
| 2712.5 | 3600.0 | 34.8 | 43.8 |
| 2700.0 | 3600.0 | 54.9 | 48.8 |
| 2687.5 | 3600.0 | 60.0 | 48.8 |
| 2675.0 | 3600.0 | 54.2 | 48.4 |
| 2662.5 | 3600.0 | 40.1 | 43.4 |
| 2650.0 | 3600.0 | 32.9 | 36.6 |
| 2637.5 | 3600.0 | 29.6 | 29.7 |
| 2625.0 | 3600.0 | 26.0 | 24.5 |
| 2612.5 | 3600.0 | 20.0 | 22.4 |
| 2600.0 | 3600.0 | 14.0 | 20.0 |


| 2800.0 | 3700.0 | -5.4 | -5.2 |
| ---: | ---: | ---: | ---: |
| 2812.5 | 3700.0 | -5.1 | -5.2 |
| 2825.0 | 3700.0 | -5.2 | -4.8 |
| 2837.5 | 3700.0 | -5.2 | -4.2 |
| 2850.0 | 3700.0 | -3.1 | -3.2 |
| 2862.5 | 3700.0 | -2.2 | -1.9 |
| 2875.0 | 3700.0 | -.2 | -.6 |
| 2887.5 | 3700.0 | 1.0 | 1.1 |
| 2900.0 | 3700.0 | 1.6 | 3.3 |
| 2912.5 | 3700.0 | 5.3 | 6.2 |
| 2925.0 | 3700.0 | 9.0 | 9.0 |
| 2937.5 | 3700.0 | 14.1 | 13.4 |
| 2950.0 | 3700.0 | 15.1 | 19.5 |
| 2962.5 | 3700.0 | 23.7 | 26.3 |
| 2975.0 | 3700.0 | 35.5 | 34.9 |
| 2987.5 | 3700.0 | 43.3 | 46.1 |
| 3000.0 | 3700.0 | 57.1 | 59.5 |
| 3012.5 | 3700.0 | 70.8 | 85.5 |
| 3025.0 | 3700.0 | 90.8 | 111.3 |
| 3037.5 | 3700.0 | 165.5 | 98.4 |
| 3050.0 | 3700.0 | 172.4 | 82.8 |
| 3062.5 | 3700.0 | -7.7 | 64.0 |
| 3075.0 | 3700.0 | -7.1 | 31.7 |
| 3087.5 | 3700.0 | -2.9 | -1.6 |
| 3100.0 | 3700.0 | 4.0 | 1.5 |
| 3112.5 | 3700.0 | 5.6 | 3.9 |
| 3125.0 | 3700.0 | 8.1 | 6.0 |
| 3137.5 | 3700.0 | 4.5 | 8.7 |
| 3150.0 | 3700.0 | 8.0 | 10.8 |
| 3162.5 | 3700.0 | 17.3 | 18.5 |
| 3175.0 | 3700.0 | 16.3 | 39.5 |
| 3187.5 | 3700.0 | 46.4 | 41.5 |
| 3200.0 | 3700.0 | 109.7 | 39.1 |
| 3212.5 | 3700.0 | 17.6 | 36.6 |
| 3225.0 | 3700.0 | 5.7 | 31.8 |
| 3237.5 | 3700.0 | 3.7 | 21.4 |
| 3250.0 | 3700.0 | 22.1 | 46.1 |
| 3262.5 | 3700.0 | 57.9 | 83.5 |
| 3275.0 | 3700.0 | 141.1 | 93.5 |
| 3287.5 | 3700.0 | 192.9 | 86.0 |
| 3300.0 | 3700.0 | 53.6 | 67.6 |
| 3312.5 | 3700.0 | -15.6 | 34.5 |
| 3325.0 | 3700.0 | -34.0 | -9.6 |
| 3337.5 | 3700.0 | -24.3 | -23.2 |
| 3350.0 | 3700.0 | -27.6 | -24.5 |
| 3362.5 | 3700.0 | -14.4 | -20.6 |
| 3375.0 | 3700.0 | -22.2 | -16.8 |
| 3387.5 | 3700.0 | -14.3 | -14.1 |
| 3400.0 | 3700.0 | -5.4 | -14.0 |
|  |  |  |  |


| 3400.0 | 3800.0 | 5.1 | 68.9 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 3800.0 | 19.6 | 74.7 |
| 3375.0 | 3800.0 | 181.9 | 71.3 |
| 3362.5 | 3800.0 | 92.3 | 80.8 |
| 3350.0 | 3800.0 | 57.7 | 92.9 |
| 3337.5 | 3800.0 | 52.6 | 69.0 |
| 3325.0 | 3800.0 | 79.9 | 62.3 |
| 3312.5 | 3800.0 | 62.4 | 89.0 |
| 3300.0 | 3800.0 | 59.1 | 101.3 |
| 3287.5 | 3800.0 | 190.9 | 95.7 |
| 3275.0 | 3800.0 | 114.3 | 97.2 |
| 3262.5 | 3800.0 | 51.7 | 92.9 |
| 3250.0 | 3800.0 | 70.2 | 64.3 |
| 3237.5 | 3800.0 | 37.5 | 49.6 |
| 3225.0 | 3800.0 | 48.0 | 45.2 |
| 3212.5 | 3800.0 | 40.4 | 36.5 |
| 3200.0 | 3800.0 | 29.9 | 30.7 |
| 3187.5 | 3800.0 | 26.5 | 23.4 |
| 3175.0 | 3800.0 | 8.9 | 16.0 |
| 3162.5 | 3800.0 | 11.1 | 11.4 |
| 3150.0 | 3800.0 | 3.8 | 7.9 |
| 3137.5 | 3800.0 | 6.9 | 7.4 |
| 3125.0 | 3800.0 | 8.6 | 5.9 |
| 3112.5 | 3800.0 | 6.5 | 5.3 |
| 3100.0 | 3800.0 | 3.6 | 4.2 |
| 3087.5 | 3800.0 | 1.1 | 4.1 |
| 3075.0 | 3800.0 | 1.1 | 4.7 |
| 3062.5 | 3800.0 | 8.0 | 5.3 |
| 3050.0 | 3800.0 | 9.7 | 6.0 |
| 3037.5 | 3800.0 | 6.5 | 6.7 |
| 3025.0 | 3800.0 | 4.8 | 6.4 |
| 3012.5 | 3800.0 | 4.3 | 6.4 |
| 3000.0 | 3800.0 | 6.7 | 7.0 |
| 2987.5 | 3800.0 | 9.7 | 7.4 |
| 2975.0 | 3800.0 | 9.3 | 7.0 |
| 2962.5 | 3800.0 | 7.0 | 5.9 |
| 2950.0 | 3800.0 | 2.2 | 4.3 |
| 2937.5 | 3800.0 | 1.2 | 2.6 |
| 2925.0 | 3800.0 | 1.7 | 1.5 |
| 2912.5 | 3800.0 | .8 | 1.2 |
| 2900.0 | 3800.0 | 1.8 | 1.3 |
| 2887.5 | 3800.0 | .6 | 1.7 |
| 2875.0 | 3800.0 | 1.7 | 2.4 |
| 2862.5 | 3800.0 | 3.4 | 2.6 |
| 2850.0 | 3800.0 | 4.6 | 2.9 |
| 2837.5 | 3800.0 | 2.9 | 3.0 |
| 2825.0 | 3800.0 | 2.0 | 2.6 |
| 2812.5 | 3800.0 | 2.0 | 2.1 |
| 2800.0 | 3800.0 | 1.5 | 1.8 |
|  |  |  |  |

### 2.23 Line 3900 E

| 2800.0 | 3900.0 | 5.8 | 6.2 |
| ---: | ---: | ---: | ---: |
| 2812.5 | 3900.0 | 6.7 | 6.4 |
| 2825.0 | 3900.0 | 6.2 | 6.7 |
| 2837.5 | 3900.0 | 6.9 | 7.0 |
| 2850.0 | 3900.0 | 7.7 | 7.3 |
| 2862.5 | 3900.0 | 7.6 | 7.8 |
| 2875.0 | 3900.0 | 8.3 | 7.9 |
| 2887.5 | 3900.0 | 8.3 | 8.3 |
| 2900.0 | 3900.0 | 7.8 | 8.6 |
| 2912.5 | 3900.0 | 9.3 | 9.2 |
| 2925.0 | 3900.0 | 9.2 | 10.0 |
| 2937.5 | 3900.0 | 11.5 | 10.7 |
| 2950.0 | 3900.0 | 12.3 | 11.4 |
| 2962.5 | 3900.0 | 11.4 | 12.1 |
| 2975.0 | 3900.0 | 12.6 | 12.8 |
| 2987.5 | 3900.0 | 12.7 | 13.1 |
| 3000.0 | 3900.0 | 14.9 | 13.2 |
| 3012.5 | 3900.0 | 14.1 | 13.3 |
| 3025.0 | 3900.0 | 11.9 | 13.4 |
| 3037.5 | 3900.0 | 13.1 | 13.3 |
| 3050.0 | 3900.0 | 13.2 | 13.0 |
| 3062.5 | 3900.0 | 14.0 | 13.4 |
| 3075.0 | 3900.0 | 13.0 | 13.2 |
| 3087.5 | 3900.0 | 13.9 | 13.4 |
| 3100.0 | 3900.0 | 11.7 | 12.4 |
| 3112.5 | 3900.0 | 14.3 | 11.7 |
| 3125.0 | 3900.0 | 9.0 | 12.4 |
| 3137.5 | 3900.0 | 9.5 | 12.7 |
| 3150.0 | 3900.0 | 17.3 | 13.4 |
| 3162.5 | 3900.0 | 13.6 | 14.1 |
| 3175.0 | 3900.0 | 17.7 | 17.8 |
| 3187.5 | 3900.0 | 12.6 | 30.3 |
| 3200.0 | 3900.0 | 27.7 | 35.8 |
| 3212.5 | 3900.0 | 79.7 | 39.3 |
| 3225.0 | 3900.0 | 41.4 | 41.0 |
| 3237.5 | 3900.0 | 34.9 | 43.8 |
| 3250.0 | 3900.0 | 21.3 | 57.3 |
| 3262.5 | 3900.0 | 41.6 | 59.2 |
| 3275.0 | 3900.0 | 147.5 | 69.4 |
| 3287.5 | 3900.0 | 50.6 | 79.5 |
| 3300.0 | 3900.0 | 85.8 | 77.5 |
| 3312.5 | 3900.0 | 71.8 | 58.4 |
| 3325.0 | 3900.0 | 31.7 | 59.8 |
| 3337.5 | 3900.0 | 51.9 | 53.2 |
| 3350.0 | 3900.0 | 58.0 | 52.2 |
| 3362.5 | 3900.0 | 52.8 | 60.8 |
| 3375.0 | 3900.0 | 66.5 | 63.9 |
| 3387.5 | 3900.0 | 75.0 | 65.3 |
| 3400.0 | 3900.0 | 67.0 | 69.5 |
|  |  |  |  |

### 2.24 Line 4000E

| 3400.0 | 4000.0 | -20.1 | 11.9 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 4000.0 | -29.9 | 22.8 |
| 3375.0 | 4000.0 | 85.7 | 24.5 |
| 3362.5 | 4000.0 | 55.6 | 38.3 |
| 3350.0 | 4000.0 | 31.1 | 54.9 |
| 3337.5 | 4000.0 | 49.0 | 49.7 |
| 3325.0 | 4000.0 | 52.9 | 53.3 |
| 3312.5 | 4000.0 | 60.0 | 66.7 |
| 3300.0 | 4000.0 | 73.6 | 70.0 |
| 3287.5 | 4000.0 | 97.9 | 69.5 |
| 3275.0 | 4000.0 | 65.8 | 63.0 |
| 3262.5 | 4000.0 | 50.1 | 55.4 |
| 3250.0 | 4000.0 | 27.4 | 40.0 |
| 3237.5 | 4000.0 | 36.0 | 35.3 |
| 3225.0 | 4000.0 | 20.5 | 30.2 |
| 3212.5 | 4000.0 | 42.6 | 29.3 |
| 3200.0 | 4000.0 | 24.4 | 26.4 |
| 3187.5 | 4000.0 | 23.0 | 26.1 |
| 3175.0 | 4000.0 | 21.7 | 20.4 |
| 3162.5 | 4000.0 | 18.9 | 19.6 |
| 3150.0 | 4000.0 | 14.1 | 18.6 |
| 3137.5 | 4000.0 | 20.4 | 17.1 |
| 3125.0 | 4000.0 | 17.8 | 16.1 |
| 3112.5 | 4000.0 | 14.5 | 16.4 |
| 3100.0 | 4000.0 | 13.9 | 15.6 |
| 3087.5 | 4000.0 | 15.2 | 15.8 |
| 3075.0 | 4000.0 | 16.8 | 16.8 |
| 3062.5 | 4000.0 | 18.4 | 18.0 |
| 3050.0 | 4000.0 | 19.9 | 19.0 |
| 3037.5 | 4000.0 | 19.5 | 19.6 |
| 3025.0 | 4000.0 | 20.3 | 19.9 |
| 3012.5 | 4000.0 | 19.7 | 19.9 |
| 3000.0 | 4000.0 | 20.1 | 19.8 |
| 2987.5 | 4000.0 | 19.8 | 19.3 |
| 2975.0 | 4000.0 | 19.2 | 18.5 |
| 2962.5 | 4000.0 | 17.8 | 17.3 |
| 2950.0 | 4000.0 | 15.7 | 15.8 |
| 2937.5 | 4000.0 | 13.9 | 14.1 |
| 2925.0 | 4000.0 | 12.5 | 12.3 |
| 2912.5 | 4000.0 | 10.5 | 10.7 |
| 2900.0 | 4000.0 | 9.0 | 9.6 |
| 2887.5 | 4000.0 | 7.8 | 8.6 |
| 2875.0 | 4000.0 | 8.3 | 7.7 |
| 2862.5 | 4000.0 | 7.4 | 6.8 |
| 2850.0 | 4000.0 | 5.8 | 6.8 |
| 2837.5 | 4000.0 | 4.5 | 6.3 |
| 2825.0 | 4000.0 | 8.1 | 6.3 |
| 2812.5 | 4000.0 | 5.7 | 6.5 |
| 2800.0 | 4000.0 | 7.6 | 7.1 |
|  |  |  |  |


| 2.25 Line | 4100E |  |  |
| :--- | :--- | ---: | ---: |
| 2700.0 | 4100.0 |  |  |
| 2712.5 | 4100.0 | 11.9 | 10.9 |
| 2725.0 | 4100.0 | 11.7 | 11.3 |
| 2737.5 | 4100.0 | 12.3 | 11.8 |
| 2750.0 | 4100.0 | 12.9 | 12.1 |
| 2762.5 | 4100.0 | 11.1 | 12.4 |
| 2775.0 | 4100.0 | 12.4 | 12.6 |
| 2787.5 | 4100.0 | 13.2 | 12.8 |
| 2800.0 | 4100.0 | 13.4 | 13.7 |
| 2812.5 | 4100.0 | 14.1 | 14.5 |
| 2825.0 | 4100.0 | 15.4 | 15.3 |
| 2837.5 | 4100.0 | 16.4 | 16.5 |
| 2850.0 | 4100.0 | 17.3 | 17.8 |
| 2862.5 | 4100.0 | 19.1 | 19.1 |
| 2875.0 | 4100.0 | 20.9 | 20.5 |
| 2887.5 | 4100.0 | 22.0 | 21.7 |
| 2900.0 | 4100.0 | 23.2 | 22.6 |
| 2912.5 | 4100.0 | 23.1 | 23.0 |
| 2925.0 | 4100.0 | 23.8 | 23.4 |
| 2937.5 | 4100.0 | 23.1 | 23.8 |
| 2950.0 | 4100.0 | 23.8 | 24.4 |
| 2962.5 | 4100.0 | 25.3 | 25.3 |
| 2975.0 | 4100.0 | 26.2 | 26.4 |
| 2987.5 | 4100.0 | 28.0 | 27.7 |
| 3000.0 | 4100.0 | 28.5 | 28.9 |
| 3012.5 | 4100.0 | 30.4 | 29.9 |
| 3025.0 | 4100.0 | 31.6 | 30.8 |
| 3037.5 | 4100.0 | 31.2 | 31.6 |
| 3050.0 | 4100.0 | 32.4 | 31.9 |
| 3062.5 | 4100.0 | 32.5 | 32.1 |
| 3075.0 | 4100.0 | 32.0 | 31.7 |
| 3087.5 | 4100.0 | 32.3 | 31.2 |
| 3100.0 | 4100.0 | 29.4 | 30.7 |
| 3112.5 | 4100.0 | 29.6 | 31.7 |
| 3125.0 | 4100.0 | 30.1 | 33.3 |
| 3137.5 | 4100.0 | 37.1 | 35.7 |
| 3150.0 | 4100.0 | 40.3 | 38.1 |
| 3162.5 | 4100.0 | 41.2 | 40.6 |
| 3175.0 | 4100.0 | 41.8 | 42.9 |
| 3187.5 | 4100.0 | 42.8 | 58.2 |
| 3200.0 | 4100.0 | 48.3 | 100.2 |
| 3212.5 | 4100.0 | 117.1 | 126.0 |
| 3225.0 | 4100.0 | 251.1 | 163.8 |
| 3237.5 | 4100.0 | 170.7 | 163.8 |
| 3250.0 | 4100.0 | 231.7 | 143.8 |
| 3262.5 | 4100.0 | 48.3 | 106.7 |
| 3275.0 | 4100.0 | 17.2 | 86.0 |
| 3287.5 | 4100.0 | 65.6 | 46.5 |
| 3300.0 | 4100.0 | 67.1 | 43.1 |
| 3312.5 | 4100.0 | 34.1 | 42.4 |
| 3325.0 | 4100.0 | 31.6 | 38.4 |


| 3337.5 | 4100.0 | 13.5 | 18.6 |
| ---: | ---: | ---: | ---: |
| 3350.0 | 4100.0 | 45.8 | 14.2 |
| 3362.5 | 4100.0 | -32.1 | 4.0 |
| 3375.0 | 4100.0 | 12.0 | .2 |
| 3387.5 | 4100.0 | -19.0 | -11.3 |
| 3400.0 | 4100.0 | -5.9 | -4.3 |

2.26 Line 4200E

| 3400.0 | 4200.0 | 5.4 | -5.9 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 4200.0 | -16.7 | -1.7 |
| 3375.0 | 4200.0 | -6.5 | 4.0 |
| 3362.5 | 4200.0 | 11.1 | -.8 |
| 3350.0 | 4200.0 | 26.6 | -2.6 |
| 3337.5 | 4200.0 | -18.4 | -4.2 |
| 3325.0 | 4200.0 | -26.0 | -8.9 |
| 3312.5 | 4200.0 | -14.4 | -16.1 |
| 3300.0 | 4200.0 | -12.4 | -13.9 |
| 3287.5 | 4200.0 | -9.2 | -13.9 |
| 3275.0 | 4200.0 | -7.4 | 6.3 |
| 3262.5 | 4200.0 | -26.2 | 9.2 |
| 3250.0 | 4200.0 | 86.6 | 11.6 |
| 3237.5 | 4200.0 | 2.0 | 11.1 |
| 3225.0 | 4200.0 | 3.1 | 16.4 |
| 3212.5 | 4200.0 | -10.0 | 2.2 |
| 3200.0 | 4200.0 | .5 | 1.8 |
| 3187.5 | 4200.0 | 15.2 | 4.2 |
| 3175.0 | 4200.0 | .4 | 16.8 |
| 3162.5 | 4200.0 | 14.9 | 33.5 |
| 3150.0 | 4200.0 | 52.9 | 52.1 |
| 3137.5 | 4200.0 | 84.1 | 68.5 |
| 3125.0 | 4200.0 | 108.4 | 81.0 |
| 3112.5 | 4200.0 | 82.4 | 86.3 |
| 3100.0 | 4200.0 | 77.4 | 83.4 |
| 3087.5 | 4200.0 | 79.4 | 77.8 |
| 3075.0 | 4200.0 | 69.4 | 74.9 |
| 3062.5 | 4200.0 | 80.5 | 75.5 |
| 3050.0 | 4200.0 | 67.9 | 71.6 |
| 3037.5 | 4200.0 | 80.4 | 68.5 |
| 3025.0 | 4200.0 | 59.6 | 63.2 |
| 3012.5 | 4200.0 | 54.3 | 60.8 |
| 3000.0 | 4200.0 | 53.7 | 55.2 |
| 2987.5 | 4200.0 | 56.0 | 52.1 |
| 2975.0 | 4200.0 | 52.6 | 49.6 |
| 2962.5 | 4200.0 | 43.9 | 47.6 |
| 2950.0 | 4200.0 | 42.0 | 43.3 |
| 2937.5 | 4200.0 | 43.5 | 38.3 |
| 2925.0 | 4200.0 | 34.3 | 35.9 |
| 2912.5 | 4200.0 | 27.7 | 33.6 |
| 2900.0 | 4200.0 | 31.9 | 29.9 |
| 2887.5 | 4200.0 | 30.6 | 27.8 |


| 2875.0 | 4200.0 | 24.9 | 26.5 |
| ---: | ---: | ---: | ---: |
| 2862.5 | 4200.0 | 24.0 | 24.8 |
| 2850.0 | 4200.0 | 21.0 | 22.6 |
| 2837.5 | 4200.0 | 23.3 | 21.4 |
| 2825.0 | 4200.0 | 19.7 | 19.4 |
| 2812.5 | 4200.0 | 19.0 | 17.2 |
| 2800.0 | 4200.0 | 14.2 | 13.9 |
| 2787.5 | 4200.0 | 9.8 | 10.4 |
| 2775.0 | 4200.0 | 6.6 | 6.3 |
| 2762.5 | 4200.0 | 2.3 | 3.8 |
| 2750.0 | 4200.0 | -1.3 | 2.3 |
| 2737.5 | 4200.0 | 1.5 | 3.0 |
| 2725.0 | 4200.0 | 2.3 | 4.7 |
| 2712.5 | 4200.0 | 10.1 | 6.5 |
| 2700.0 | 4200.0 | 11.1 | 5.9 |
| 2687.5 | 4200.0 | 7.4 | 4.3 |
| 2675.0 | 4200.0 | -1.2 | 4.2 |
| 2662.5 | 4200.0 | -6.1 | 63.8 |
| 2650.0 | 4200.0 | 10.0 | 97.0 |
| 2637.5 | 4200.0 | 308.8 | 115.3 |
| 2625.0 | 4200.0 | 173.7 | 128.9 |
| 2612.5 | 4200.0 | 90.3 | 158.6 |
| 2600.0 | 4200.0 | 61.5 | 108.5 |

### 2.27 Line 4300E

| 3100.0 | 4300.0 | 1.4 | 1.8 |
| ---: | ---: | ---: | ---: |
| 3112.5 | 4300.0 | 3.3 | -1.2 |
| 3125.0 | 4300.0 | .8 | -4.5 |
| 3137.5 | 4300.0 | -10.4 | -3.6 |
| 3150.0 | 4300.0 | -17.8 | -6.0 |
| 3162.5 | 4300.0 | 6.3 | -7.2 |
| 3175.0 | 4300.0 | -8.9 | -3.3 |
| 3187.5 | 4300.0 | -5.1 | -1.4 |
| 3200.0 | 4300.0 | 9.2 | -5.6 |
| 3212.5 | 4300.0 | -8.5 | 3.7 |
| 3225.0 | 4300.0 | -14.5 | -.4 |
| 3237.5 | 4300.0 | 37.2 | -9.5 |
| 3250.0 | 4300.0 | -25.3 | -13.8 |
| 3262.5 | 4300.0 | -36.5 | -9.4 |
| 3275.0 | 4300.0 | -29.8 | -20.5 |
| 3287.5 | 4300.0 | 7.2 | 2.0 |
| 3300.0 | 4300.0 | -17.9 | 27.4 |
| 3312.5 | 4300.0 | 87.1 | 40.6 |
| 3325.0 | 4300.0 | 90.3 | 38.8 |
| 3337.5 | 4300.0 | 36.4 | 41.3 |
| 3350.0 | 4300.0 | -2.1 | 28.2 |
| 3362.5 | 4300.0 | -5.0 | 13.4 |
| 3375.0 | 4300.0 | 21.3 | 7.7 |
| 3387.5 | 4300.0 | 16.3 | 10.1 |
| 3400.0 | 4300.0 | 8.0 | 15.2 |


| 3400.0 | 4400.0 | 37.9 | 25.6 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 4400.0 | 14.1 | 24.3 |
| 3375.0 | 4400.0 | 24.9 | 18.8 |
| 3362.5 | 4400.0 | 20.3 | 9.5 |
| 3350.0 | 4400.0 | -3.2 | 5.0 |
| 3337.5 | 4400.0 | -8.7 | -3.0 |
| 3325.0 | 4400.0 | -8.1 | -10.3 |
| 3312.5 | 4400.0 | -15.5 | -6.5 |
| 3300.0 | 4400.0 | -16.1 | -1.8 |
| 3287.5 | 4400.0 | 16.0 | -.5 |
| 3275.0 | 4400.0 | 14.9 | 1.8 |
| 3262.5 | 4400.0 | -1.7 | 8.5 |
| 3250.0 | 4400.0 | -4.3 | .5 |
| 3237.5 | 4400.0 | 17.4 | -2.6 |
| 3225.0 | 4400.0 | -23.6 | -6.9 |
| 3212.5 | 4400.0 | -1.0 | -4.8 |
| 3200.0 | 4400.0 | -22.9 | -5.0 |
| 3187.5 | 4400.0 | 6.3 | -.5 |
| 3175.0 | 4400.0 | 16.1 | -5.3 |
| 3162.5 | 4400.0 | -1.0 | 3.1 |
| 3150.0 | 4400.0 | -25.2 | 2.8 |
| 3137.5 | 4400.0 | 19.3 | 7.3 |
| 3125.0 | 4400.0 | 4.9 | 9.1 |
| 3112.5 | 4400.0 | 38.4 | 17.7 |
| 3100.0 | 4400.0 | 8.3 | 17.2 |

### 2.29 Line 4500E

| 3100.0 | 4500.0 | -2.0 | 3.4 |
| ---: | ---: | ---: | ---: |
| 3112.5 | 4500.0 | 5.8 | 6.1 |
| 3125.0 | 4500.0 | 6.4 | 5.1 |
| 3137.5 | 4500.0 | 14.3 | 11.0 |
| 3150.0 | 4500.0 | 1.2 | 13.1 |
| 3162.5 | 4500.0 | 27.4 | 17.2 |
| 3175.0 | 4500.0 | 16.2 | 17.9 |
| 3187.5 | 4500.0 | 26.9 | 19.8 |
| 3200.0 | 4500.0 | 17.9 | 17.6 |
| 3212.5 | 4500.0 | 10.7 | 15.6 |
| 3225.0 | 4500.0 | 16.2 | 15.8 |
| 3237.5 | 4500.0 | 6.2 | 14.3 |
| 3250.0 | 4500.0 | 28.0 | 17.5 |
| 3262.5 | 4500.0 | 10.4 | 21.1 |
| 3275.0 | 4500.0 | 26.6 | 24.9 |
| 3287.5 | 4500.0 | 34.2 | 24.6 |
| 3300.0 | 4500.0 | 25.5 | 24.6 |
| 3312.5 | 4500.0 | 26.3 | 24.6 |
| 3325.0 | 4500.0 | 10.2 | 23.9 |
| 3337.5 | 4500.0 | 26.8 | 19.2 |
| 3350.0 | 4500.0 | 30.6 | 12.7 |


| 3362.5 | 4500.0 | 2.3 | 13.3 |
| ---: | ---: | ---: | ---: |
| 3375.0 | 4500.0 | -6.4 | 18.1 |
| 3387.5 | 4500.0 | 13.2 | 14.9 |
| 3400.0 | 4500.0 | 50.6 | 19.1 |

2.30 Line 4600 E

| 3400.0 | 4600.0 | 45.8 | 24.7 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 4600.0 | 31.6 | 20.5 |
| 3375.0 | 4600.0 | -3.3 | 15.1 |
| 3362.5 | 4600.0 | 8.1 | 4.9 |
| 3350.0 | 4600.0 | -6.5 | -1.7 |
| 3337.5 | 4600.0 | -5.3 | 5.1 |
| 3325.0 | 4600.0 | -1.5 | 16.1 |
| 3312.5 | 4600.0 | 30.9 | 22.3 |
| 3300.0 | 4600.0 | 63.0 | 26.0 |
| 3287.5 | 4600.0 | 24.6 | 30.0 |
| 3275.0 | 4600.0 | 12.8 | 30.1 |
| 3262.5 | 4600.0 | 18.6 | 12.9 |
| 3250.0 | 4600.0 | 31.5 | 9.8 |
| 3237.5 | 4600.0 | -22.8 | 11.2 |
| 3225.0 | 4600.0 | 9.1 | 12.3 |
| 3212.5 | 4600.0 | 19.7 | 10.9 |
| 3200.0 | 4600.0 | 23.8 | 23.3 |
| 3187.5 | 4600.0 | 24.5 | 18.6 |
| 3175.0 | 4600.0 | 39.4 | 15.0 |
| 3162.5 | 4600.0 | -14.2 | 11.5 |
| 3150.0 | 4600.0 | 1.6 | 6.7 |
| 3137.5 | 4600.0 | 6.3 | -.8 |
| 3125.0 | 4600.0 | .6 | 4.0 |
| 3112.5 | 4600.0 | 1.8 | 4.6 |
| 3100.0 | 4600.0 | 9.7 | 4.0 |


| 3100.0 | 4700.0 | 37.6 | 9.2 |
| ---: | ---: | ---: | ---: |
| 3112.5 | 4700.0 | -11.6 | 8.1 |
| 3125.0 | 4700.0 | 1.7 | 7.9 |
| 3137.5 | 4700.0 | 4.6 | 3.8 |
| 3150.0 | 4700.0 | 7.2 | 4.2 |
| 3162.5 | 4700.0 | 17.1 | 14.4 |
| 3175.0 | 4700.0 | -9.8 | 14.1 |
| 3187.5 | 4700.0 | 52.9 | 14.3 |
| 3200.0 | 4700.0 | 3.1 | 13.2 |
| 3212.5 | 4700.0 | 8.0 | 18.4 |
| 3225.0 | 4700.0 | 11.8 | 10.8 |
| 3237.5 | 4700.0 | 16.1 | 21.8 |
| 3250.0 | 4700.0 | 15.0 | 28.2 |
| 3262.5 | 4700.0 | 58.1 | 26.3 |


| 3275.0 | 4700.0 | 40.1 | 24.1 |
| ---: | ---: | ---: | ---: |
| 3287.5 | 4700.0 | 2.4 | 20.7 |
| 3300.0 | 4700.0 | 4.7 | 15.6 |
| 3312.5 | 4700.0 | -1.8 | 7.7 |
| 3325.0 | 4700.0 | 32.4 | 3.3 |
| 3337.5 | 4700.0 | .6 | 8.9 |
| 3350.0 | 4700.0 | -19.4 | 10.1 |
| 3362.5 | 4700.0 | 32.6 | 5.3 |
| 3375.0 | 4700.0 | 4.2 | 7.3 |
| 3387.5 | 4700.0 | 8.6 | 14.0 |
| 3400.0 | 4700.0 | 10.7 | 7.8 |

2.32 Line 4800E

| 3400.0 | 4800.0 | 20.0 | 6.9 |
| ---: | ---: | ---: | ---: |
| 3387.5 | 4800.0 | -1.6 | 2.0 |
| 3375.0 | 4800.0 | 2.2 | 6.0 |
| 3362.5 | 4800.0 | -12.5 | 5.9 |
| 3350.0 | 4800.0 | 21.9 | 8.4 |
| 3337.5 | 4800.0 | 19.6 | 11.0 |
| 3325.0 | 4800.0 | 10.9 | 15.2 |
| 3312.5 | 4800.0 | 15.2 | 15.2 |
| 3300.0 | 4800.0 | 8.2 | 14.1 |
| 3287.5 | 4800.0 | 22.0 | 16.1 |
| 3275.0 | 4800.0 | 14.0 | 19.5 |
| 3262.5 | 4800.0 | 21.2 | 27.6 |
| 3250.0 | 4800.0 | 32.0 | 39.1 |
| 3237.5 | 4800.0 | 49.0 | 51.4 |
| 3225.0 | 4800.0 | 79.3 | 51.5 |
| 3212.5 | 4800.0 | 75.4 | 56.1 |
| 3200.0 | 4800.0 | 22.0 | 53.9 |
| 3187.5 | 4800.0 | 54.6 | 42.4 |
| 3175.0 | 4800.0 | 38.0 | 30.8 |
| 3162.5 | 4800.0 | 22.0 | 28.7 |
| 3150.0 | 4800.0 | 17.2 | 17.7 |
| 3137.5 | 4800.0 | 11.5 | 15.7 |
| 3125.0 | 4800.0 | -.4 | 21.7 |
| 3112.5 | 4800.0 | 28.4 | 22.8 |
| 3100.0 | 4800.0 | 51.6 | 26.5 |

END OF MAGNETOMETER DATA, DONEGAL MOUNTAIN GRID

## APPENDIX "C"

## DIAMOND DRILL CORE

 LOGGING FORMAT
## DIAMOND DRILL CORE LOGGING FORMAT

## INTRODUCTION

All the diamond drill core from the Regional Resources Ltd. - Canamax Resources Inc. Midway Property has been logged using coded logging forms to aid in the rapid recording and retrieval of information. The following is a short guide to the coding format.

## "DIAMOND DRILL RECORD" (Form DDR-82-1)

The first page of each drill hole log is a summary page and is generally selfexplanatory.

| - Survey Co-ordinates: | UTM co-ordinates tied to the Universal Transverse <br> Mercator (UTM) grid. |
| :--- | :--- |
| - Elevation: | In metres above sea level. |
| - Stick Up: | Height of casing above ground. |
| - Scale: | Of Diamond Drill Record graphic logs. |
| - Symmetry statement: | Refers to the recording of structural information. |

GEOLOGY:

Unit As per the mineralization and major rock unit codes explained below.

Int.
Drill core length of intercept.
T.W.

Thickness of unit corrected for plunge of drill hole and dip of regional stratigraphy.

# THE MAJOR STRATIGRAPHIC SUBDIVISIONS 

LOWER SYLVESTER GROUP: Upper Devonian-Mississippian

| 2B | SANDSTONE | - Light grey, medium to coarse grained, massive to bedded. |
| :---: | :---: | :---: |
|  | CONGLOMERATE | - Light grey, fine to medium grained, massive <br> - generally Bouma $A$ and lesser $B$ sequences. |
| 2A | SUBDIVIDED BELOW |  |
| 2AP | SLUMP BRECCIA | - Light grey sandstone clasts in a dark grey siltstone/sandstone matrix. |
| 2AS | SILTSTONE | - Dark to medium grey, variably carbonaceous, variably siliceous, variably pyritic, noncalcareous. |
|  | CALCARENITE | - Light grey, laminated to massive; present toward top of unit. |
| 2AC | SILTSTONE | - Dark to medium grey, slightly to moderately carbonaceous, non-siliceous, slightly to moderately pyritic, generally non-calcareous. |
|  | CALCARENITE | - Light grey, laminated to massive. |
|  | SANDSTONE | - Light grey, laminated to massive; only locally present. |
| 2AA | SILTSTONE | - Dark grey to black, moderately to very carbonaceous non-siliceous, locally pyritic, non-calcareous; may contain abundant chert and/or calcareous nodules. |
| 1B | SA: ${ }^{\text {d }}$ STONE | - Light grey, laminated to massive |
|  | SILTSTONE | - Dark to medium grey, slightly to moderately carbonaceous, non-siliceous, slightly pyritic, non-calcareous. |
|  | CONGLOMERATE | - Light grey, fine to locally medium grained, massive. <br> - Coarser grained Bouma $A$ and $B$ sequences generally occur toward the upper portion of the unit while finer grained Bouma D sequences occur toward the lower portion of the unit. |
| 1 BA |  | - This is the basal transition zone of unit lB dominated by siltstones with $5-25$ sandstone. |

IA This unit is transitional with the lBA unit above and is defined as containing $<5 \%$ sandstone beds.

- Dark grey to black, moderately to very carbonaceous, locally siliceous, locally pyritic, generally non-calcareous.

IAC CALCAREOUS SILTSTONE/CALCARENITE

- Medium to dark grey, usually non-carbonaceous, non-siliceous, non-pyritic, moderately to very calcareous. This is a local calcareous "wash" occasionally immediately overlying the McDame Group carbonates.


## ALTERATION

In the Lower Sylvester Group there are zones of siltstone and/or sandstone and/or calcarenite which have been altered to phyllite ( Ph ) and/or siliceous chert-like rocks with or without pyrrhotite $\pm$ pyrite $\pm$ chalcopyrite. These altered rocks are placed in the Lower Sylvester Group under their respective unit names with a precursor letter "A", (e.g., AlB is altered Unit lB).

MCDAME GROUP: Middle Devonian

## :cDame Lithostratigraphic Units

|  | $\left\|\begin{array}{c} \stackrel{\rightharpoonup}{c} \\ \underline{c} \\ \underline{0} \end{array}\right\|$ | Thickness | Major | Components | Lesser Components | Minor Components |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 SIT | $\cdots$ | $\cdots$ | Facies | Lithologies | Facies | Facies | Notes |
| $x:-1$ | A | $28+$ | Dense <br> Aephipora | Packstone to Mudstone Rudstone to floatstone | - | Massive <br> Stromatoporoid |  |
|  | E | 5.4 | Thamopora | Rudstone E Floatstone | Massive Stronatoporoid | Asphipora |  |
|  | $こ$ | 16.8 | Densc Anphípora Massive. Stromatoporoid | Packstone to Mudstone Rudstone $\bar{c}$ FIoatstone <br>  <br> Floatstone |  | stromatoporoj̄ $\varepsilon$ Dense | Upper <br> Lower |
|  | 0 | 2.5-4.3 | Crinoidal | Packstone C Hackestone |  |  |  |
|  | E | 4-10 | Anphipora Dense | ```Floatstone Bioclastic-peloj\overline{al} Packstone to Mudstone``` |  | Massive Stromatoporoid |  |
| ' ${ }^{\prime}$-2 |  | up to 23 | Massive <br> Stronatoporoid | Rudstone to Floatstone, local chert, Framestone | Hixed Asphipora <br> © Stromatoporoid | Rugosan <br> Euryanphipora <br> Ihannopora |  |

THE MAJOR STRATIGRAPHIC SUBDIVISIONS
McDame Group: Middle Devonian (cont'd)
McDame Lithostratigraphic Units


INTRUSIVE ROCKS

㒸:I工
YBR
DIKES AND ALTERED ROCKS OF UNCERTAIN PARENTAGE

- Greenstone dikes are found mainly in the McDame Group but also occur locally in the Lower Sylvester Group.
- Variably altered rocks are usually associated with the dikes but are much more extensive than the greenstones themselves. The altered rocks probably represent, for the most part; highly altered dikes.


## MINERALIZATION

"EXHALITES" These are light brown to light grey cherty units found in Unit 2 A of the Lower Sylvester Group. They are generally composed of quartz, sericite, and pyrite but locally grade to massive sulphides (pyrite-sphalerite-galena). Different "exhalite" horizons have been given letter designations to distinguish them.
e.g., FZ $=F$-Zone "exhalite"

FZP $=F$-Zone "exhalite" package - usually used when thin
"exhalites" believed to be related are interbedded with other lithologies.

The major rock type designation (e.g., XQ (siliceous exhalite) is used in the unit column when the identification of the "exhalite" horizon is uncertain.

## LOWER ZONE MINERALIZATION

The carbonate-hosted Lower Zones have been designated LZ1, LZ2, LZ 3, etc., as they were encountered down the drillhole.

OTHER SYMBOLS USED

| $O B$ | - | Overburden |
| :--- | :--- | :--- |
| $N R$ | - | No recovery |
| $G M$ | - | Gouge Zone |

## APPENDIX "D"

## DIAMOND DRILL S UMMARY LOGS

MW-86-274
MW-86-275
MW-86-276
MW-86-279
MW-86-280
MW-86-281
MW-86-282
MW-86-283
MW-86-284
MW-86-293
MW-86-294

## inıGluival REsulUnu'Es lTu.



## REGIUNAL RESOURCES LTD.

DIAMOND DRILL RECORD




## ktGIUIval RESOURCES LTU.

DIAMOND DRILL . .ECORD

PROPERTY
MIDWAY
D.D.H.MW $8 G-E 79 \cdots$

PAGE 1
OF 1

| AREA:__NW OISCO | DIP: - 70 A $\quad$ AIMUTH ( t : $\quad 180 \%$ |
| :---: | :---: |
| CLAIM: FULIL 5 | NORTHING:_ EE45619.E7 |
| SECTION:_ 24500 | EASTING: 4 24493. 5 |
| CORE SIZE: ___ HQ | ELEVATION: 1156. 9 m |
| CORE RECOVERY: | AT: RACK 10 EAYS FG |

DEPTH: EG9. 40 m
DATE STARTED
DATE FINISHED:
SEPT. $4 D 1786$
SEPT 18 D 1986
CONTRACTOR: CARIN DIAMOND DRILLING LTU. LOGGED BY: In.J. H. $/ H_{\text {. Th. }}$

COMMENTS: HOLE DRILLED TO TEST PROJECTED EASTWARD EXTENSION OF REG RESOURCES MINERALIZED STRUCTURE
HOLE AEPNDONED WHEN RODS DROPPED WHILE TRYING TO REDUCE TO NO
REG STRICTURE NOT FOND; NO ECONOMIC SURFIDES FOUND

| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | Az (t) | From (a) | To (m) | Int. (m) | T.W. (m) | Geology | Sample No. | Rec. \% | S.G. | Ag oz/h | Pb \% |  | $\mathrm{Zn} \%$ | Au oz/t | Fe \% | Ag $\mathrm{Mm} / \mathrm{MT}$ | Au gm/mT |
| 0.00 | -70.009 | $180.00{ }^{+}$ | 0.00 | 14.20 | 14.20 |  | 08 |  |  |  |  |  |  |  |  |  |  |  |
| 36.73 | -70.000 | $183.00 \%$ | 14.20 | 56.30 | 42.10 |  | STMB |  |  |  |  |  |  |  |  |  |  |  |
| 67.21 | $-73.200$ | 181.004 | 56.30 | 62.70 | 6.60 |  | Q7CA |  |  |  |  |  |  |  |  |  |  |  |
| 97.69 | -76.009 | 188.50\% | 62.90 | 88.20 | 25,30 |  | STME |  |  |  |  |  |  |  |  |  |  |  |
| -128.17 | $-76.300$ | 195.009 | 88.20 | 94.50 | 6.30 |  | ST |  |  |  |  |  |  |  |  |  |  |  |
| 158,65 | $-77.709$ | 200.009 | 94.50 | 128.60 | 34.10 |  | STME |  |  |  |  |  |  |  |  |  |  |  |
| 189.13 | $-76.00^{\circ}$ | $210.00 \%$ | 128.60 | 134.10 | 5.50 |  | ST |  |  |  |  |  |  |  |  |  |  |  |
| 219.61 | $-78.00^{\circ}$ | 220.009 | 134.10 | 163.70 | 29.60 |  | STME |  |  |  |  |  |  |  |  |  |  |  |
| 250.09 | $-78.00^{\circ}$ | $230.00^{\circ}$ | 163.70 | 186.20 | 22.50 |  | ST |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 186.20 | 225.10 | 38.70 |  | STMA |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 225.10 | 225.50 | 0.40 |  | 02 VN |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 225.50 | 227.90 | 2.40 |  | ST |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 227.90 | 236.00 | 8.10 |  | STMB |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 236.00 | 250.60 | 14.60 |  | ST |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 250.60 | 255.60 | 5.00 |  | STME |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 255.60 | 269.40 | 13.80 |  | ST |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | Cu | Pt | Zn | A ${ }^{\text {a }}$ | As | Au | P3 |  |
|  |  |  |  |  |  |  |  | ASSAYS |  |  | PPM | PPM | PPM | PPM | PPM | PPS | PPM |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 43.42 | 44.10 | 0.68 |  | STME | 13728 | 100 |  | 23 | 24 | 107 | 60.2 | 300 | 15 | 830 |  |
|  |  |  | 57.90 | 58.80 | 0.70 |  | Q2-CA | 13729 | 100 |  | 24 | 4 | 33 | 0.2 | 60 | 10 | <20 |  |
|  |  |  | 225.10 | 225.50 | 0.40 |  | QZ VN | 13730 | 100 |  | 44 | 4 | 22 | $<0.2$ | 2 | < | 150 |  |
|  |  |  | 225.10 | 244.80 | 19.70 |  | ST | 13731 | 100 |  | 18 | 5 | 18 | <0.2 | 2 | < | 1200 |  |
|  |  |  | 255.60 | 264.40 | 8.80 |  | ST | 13732 | 100 |  | 26 | 6 | 38 | <0.2 | 2 | < 5 | 1000 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## REGIONAL RESOURCES LTD.

## DIAMOND DRILL RECORD



| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | Az (t) | From (I) | To (1) | Int. ( $\mathbf{l}$ ) | T.W. (E) | Gealogy | Sample No. | Rec. \% | s.G. | Ag oz/t | Pb \% | Zn \% | Au oz/t | Fe \% | Ag ge/MT | Au ga/MT |
| 0.00 | -70.009 | 270.00 | 0.00 | 15.25 | 15.25 |  | NR |  |  |  |  |  |  |  |  |  |  |
| 172.67 | $-72.00^{\circ}$ | 260.50 | 15.25 | 39.30 | 24.05 |  | OB |  |  |  |  |  |  |  |  |  |  |
| 203.15 | $-72.80$ | 256.50 | 39.30 | 69.95 | 30.65 |  | 2 AC |  |  |  |  |  |  |  |  |  |  |
| 233.68 | $-72.50^{\circ}$ | 258.00 | 69.95 | 71.90 | 1.95 |  | $\mathrm{UZ}+\mathrm{CH}$ |  |  |  |  |  |  |  |  |  |  |
| 265.94 | -74.009 | 255.00 | 71.90 | 72.90 | 1.00 |  | 2 AC |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 72.90 | 77.72 | 4.82 |  | GH |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 7.72 | 78.70 | 0.98 |  | XO+GH |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 78.70 | 101.65 | 22.95 |  | 2AC |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 101.65 | 109.15 | 7.50 |  | GH |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 109.15 | 118.00 | 8.85 |  | 1 B |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 118.00 | 121.90 | 3.90 |  | GH |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 121.90 | 125.50 | 3.60 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 125.50 | 128.95 | 3.45 |  | GH |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 128.95 | 151.20 | 22.25 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 151.20 | 154.00 | 2.80 |  | G |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 154.00 | 166.00 | 12.00 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 166.00 | 179.00 | 13.00 |  | 1BA |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 179.00 | 190.00 | 11.00 |  | 1 AA |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 190.00 | 196.90 | 6.90 |  | 1AC |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 196.90 | 202.10 | 5.20 |  | MLICR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 202.10 | 202.65 | 0.55 |  | 12 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 202.65 | 203.88 | 1.23 |  | HLICR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 203.88 | 210.75 | 6.87 |  | 12 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 210.75 | 216.10 | 5.35 |  | MLICR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 216.10 | 218.55 | 2.45 |  | 12 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 218.55 | 220.04 | 1.49 |  | MLICR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 220.04 | 222.30 | 2.26 |  | 12 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 222.30 | 224.55 | 2.25 |  | MLI? |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 224.55 | 225.90 | 1.35 |  | GOUGE |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 225.90 | -226.90 | 1.00 |  | MLIRB |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | CONTINUED |  |  |  |  |  |  |  |  |  |

PROPERTY MIDWAY
MIDWAY D.D.H._MW 86-280-

## AREA:

 CLAIM: SECTION:$\qquad$ :
$\qquad$ COVERY: CORE RECOVERY: COMMENTS: $\qquad$ NORTHING EASTING: ELEVATION: AT:

## DEPTH:

DATE STARTED:
date finished
CONTRACTOR
LOGGED BY:

| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depin | Dip | Az (1) | From (n) | To (n) | Int (n) | T.W. (I) | Geology | Sample No. | Rec. \% | s.g. | Ag oz/t | Pb \% | 2n \% | Au 0z/t | Fe \% | AR gn/ $/ 15$ | AU SIMIT |
|  |  |  | 226.90 | 232.60 | 5.70 |  | MLICR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 232.60 | 233.80 | 1.20 |  | MLIRB |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 233.80 | 236.40 | 2.60 |  | MLICR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 236.40 | 237.25 | 0.85 |  | HL1? |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 237.25 | 255.70 | 18.45 |  | HL2 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 255.70 | 258.25 | 2.55 |  | M12CR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 258.25 | 260.30 | 2.05 |  | HL3 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 260.30 | 268.83 | 8.53 |  | H13CR |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | ASSAYS |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 201.10 | 202.10 | 1.00 |  | ML1? | 13733 | 85 | 2.8 | < 0.02 | 0.08 | 0.10 | 0.002 |  | 1 0.69 | 0.07 |
|  |  |  | 202.10 | 202.65 | 0.55 |  | L2 | 13734 | 100 | 3.9 | 1.15 | 0.05 | 0.82 | co.002 |  | 39.63 | - 0.07 |
|  |  |  | 202.65 | 203.88 | 1.23 |  | MLI? | 13735 | 95 | 2.8 | - 0.02 | 0.03 | 0.06 | 0.004 |  | - 0.69 | 0.14 |
|  |  |  | 203.88 | 204.88 | 1.00 |  | L | 13736 | -80 | 3.9 | 1.88 | 0.16 | 12.00 | c 0.002 |  | 64.46 | 10.07 |
|  |  |  | 204.88 | 205.70 | 0.82 |  | 12 | 13737 | 95 | 4.3 | 4.76 | 0.22 | 0.12 | 0.002 |  | 163.20 | 0.07 |
|  |  |  | 205.70 | 206.90 | 1.20 |  | 12 | 13738 | 95 | 4.1 | 1.35 | 0.10 | 2.80 | - 0.002 |  | 46.29 | 1 0.07 |
|  |  |  | 206.20 | 207.90 | 1.00 |  | 12 | 13739 | 95 | 4.1 | 1.75 | 0.11 | 3.00 | 10.002 |  | 60.00 | 1.0 .07 |
|  |  |  | 207.90 | 208.90 | 1.00 |  | 12 | 13740 | 100 | 3.9 | 0.82 | 0.16 | 5.10 | - 0002 |  | 28.11 | 1 0.07 |
|  |  |  | 208.90 | 209.90 | 1.00 |  | 12 | 13741 | 100 | 3.9 | 1.51 | 0.34 | 8.20 | - 0,002 |  | 51.77 | 10.07 |
|  |  |  | 209.90 | 210.75 | 0.85 |  | L2 | 13742 | 95 | 3.8 | 1.60 | 0.26 | 12.00 | 10.002 |  | 54.86 | 1.07 |
|  |  |  | 210.75 | 211.75 | 1.00 |  | ML1? | 13743 | 100 | 2.8 | - 0.02 | 10.01 | 0.11 | c 0.002 |  | 10.69 | 1 0.07 |
|  |  |  | 215.10 | 216.10 | 1.00 |  | ML1? | 13744 | 100 | 2.8 | 0.03 | 0.01 | 0.12 | -0.002 |  | 1.03 | 1 0.07 |
|  |  |  | 216.10 | 217.10 | 1.00 |  | 12 | 13745 | 100 | 4 | 1.90 | 0.14 | 12.00 | - 0.002 |  | 65.14 | 10.07 |
|  |  |  | 217.10 | 217.80 | 0.70 |  | 12 | 13746 | -95 | 4.1 | 1.77 | 0.40 | 7.55 | - 0.002 |  | 60.69 | 10.07 |
|  |  |  | 217.80 | 218.55 | 0.75 |  | 12 | 13747 | 100 | 3.9 | 12.96 | 8. 20 | -15.40 | c 0.002 |  | 444.34 | , 0.07 |
|  |  |  | 218.55 | 220.04 | 1.49 |  | ML1? | 13748 | 100 | 2.8 | 0.17 | . 0.11 | 0.24 | ¢0.002 |  | 5.83 | -1 0.07 |
|  |  |  | 220.06 | 221.40 | 1.36 |  | 12 | 13749 | 100 | 4.2 | 1.27 | 0.36 | 3.60 | 0.002 |  | 43.54 | 0.07 |
|  |  |  | 221.40 | 222.30 | 0.90 |  | 12 | 13750 | 100 | 4.2 | 4.98 | 1.49 | 7.23 | - 0.002 |  | 170.74 | 1. 0.07 |
|  |  |  | 222.30 | 223.30 | 1.00 |  | ML1? | 13751 | 100 | 2.8 | 0.96 | 0.07 | 0.34 | c 0.002 |  | 32.91 | , 0.07 |
|  |  |  |  |  |  |  |  | NTI |  |  |  |  |  |  |  |  |  |

## REGIUNAL RESOURCES LTU.



## keGIUnil RESOURCES LTU.

DIAMOND DRILL . ECCORD



## REGIOFAL RESOURCES LTD.

## DIAMOND DRILL , iECORD

| PROPERTY | MIDWAY |  | H. MW 9 |  | PAGE | $\pm$ OF | 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AREA: |  | DIP: | AZIMUTH (t): | DEPTH: |  |  |  |
| CLAIM: |  | NOR |  | DATE STARTED: |  |  |  |
| SECTION: |  | EAS |  | DATE FINISHED: |  |  |  |
| CORE SIZE: |  | ELEV |  | CONTRACTOR: |  |  |  |
| CORE RECOVERY: COMMENTS. |  | D AT: |  | LOGGED BY: |  |  |  |


| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | Az (t) | From (in) | To (m) | Int. (m) | T.W. (m) | Geology | Sample No. | Rec. \% | S.G. | Ag oz/t | Pb \% | 2n \% | Au oz/t | $\mathrm{Fe} \%$ | An $\mathrm{Bm} / \mathrm{MT}$ | Ald $\mathrm{nm} / \mathrm{MT}$ |
|  |  |  | 151.50 | 151.80 | 0.30 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 151.80 | 152.00 | 0.20 |  | MLSR8 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 152.00 | 153.20 | 1.20 |  | YRR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 153.20 | 159.85 | 6.65 |  | DYKE |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 153.85 | 169.40 | 9.55 |  | YER |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 169.40 | -169.30 | 0.50 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 169.90 | 170.30 | Q. 40 |  | YR8 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 170.30 | 172.15 | 1.85 |  | MLTRE |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 172.15 | 173.70 | 1.55 |  | ML7 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 173.70 | 174.00 | 0.30 |  | MLIR8 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 174.00 | 174.25 | 0.35 |  | 1 LL 7 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 174.25 | 174.80 | 0.55 |  | ML.7R8 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 174.80 | 175,00 | 0.20 |  | ML7 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 175.00 | 175.40 | 0.40 |  | M 7 IMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 175.40 | 175.60 | 0.20 |  | ML 7 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 175.60 | 181.40 | 5.80 |  | MLTCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 181.40 | 181.60 | 0,20 |  | M27 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 181.60 | 182.10 | 0.50 |  | MLBCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 182.10 | 182.80 | 0.70 |  | M $\mathrm{ML}_{6}$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 182.80 | 183.20 | 0.40 |  | MLPMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 183.20 | 184.30 | 1.10 |  | MLA |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 184.30 | 184.65 | 0.35 | , | MLBMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 184.65 | 191.40 | 6.75 |  | M 4 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 191.40 | 191.80 | 0.40 |  | MLECR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 191.80 | 195.10 | 3.30 |  | M. 8 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 195.10 | 195.40 | 0.30 |  | MLACR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 195.40 | 197.90 | 2.50 |  | M 8 B |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 197.90 | 198.10 | 0.20 |  | MLBMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 198.10 | 200.50 | 2.40 |  | ML8 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 200.50 | 200.80 | 0.30 |  | MLOMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 200.80 | 201.30 | 0.50 |  | MLB | CONTINUED |  |  | ..... |  |  |  |  |  |  |




| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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| Depth | Dip | Az (t) | From (田) | To (m) | Int. (m) | T.W. (m) | Geology | Sample No. | Rec. \% | S.G. | Ag oz/t | Pb \% | 2n \% | Av oz/t | Fe \% | Aq, $\mathrm{gm} / \mathrm{mT}$ | A4 9 m/MT |
| 0.00 | $-45.00^{\circ}$ | 170.00 | 0.00 | 2.30 | 2.30 |  | N. F . |  |  |  |  |  |  |  |  |  |  |
| 48.98 | $-52.50{ }^{\circ}$ | 169.00 | 2.30 | 24.40 | 22.10 |  | STMB |  |  |  |  |  |  |  |  |  |  |
| 97,96 | $-60.00^{\circ}$ | 168.00 | 24.49 | 29.40 | 5.00 |  | CST |  |  |  |  |  |  |  |  |  |  |
| 143.41 | $-64.00^{\circ}$ | 175.50 | 29.40 | 92.40 | 63.00 |  | STME |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 92.40 | 95.30 | 2.90 |  | ST |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 95.30 | 126.00 | 30.70 |  | STME |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 126.00 | 131.00 | 5.610 |  | ST |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 131.00 | 147.20 | 16.20 |  | STME |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 147.20 | 152.04 | 4.84 |  | PBLST |  |  |  |  |  |  |  |  |  |  |
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## ktGIUNAL RESOURCES LTi.

DIAMOND DRILL RECORD

PROPERTY
MIDWAY
AREA:_NW DISCOVERY
CLAIM: BULL 5
SECTION: $\quad 45300 \mathrm{~N}$
CORE SIZE: HQ:62.48:NQ:140.51:B
CORE RECOVERY: $\quad \mathrm{S}-59 \mathrm{KM}$ - $94 \%$ CORE STORED
RACK 10 BAY K
$\ldots$ PAGE 1 OF 2 DEPTH: $\quad 177.39 \mathrm{~m}$
DATE STARTED: SEPT. 26D 1986
DATE FINISHED:-OCT. 3 N 1986
CONTRACTOR:- CARON DIAMOND DRILLING LTD.

Hinor pyrite occurs disseninated in unit 1AMT. No significant mineralization intersected.
Plastic pipe installed and renoved

| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | $\mathrm{Az}^{\text {( }}$ ) | From ( m ) | To ( $\mathbf{I}$ ) | Int. ( $\mathbf{I}^{\text {a }}$ | T.W.(1) | Geology | Sample No. | Rec. \% | S.a | Ag oz/t | Pb \% | 2n \% | Au ozt | Fe \% | Ag gil/M | Au ga/MT |
| 0.00 | -90.00 ${ }^{\circ}$ | $0.00^{\circ}$ | 0.00 | 36.00 | 36.00 |  | 0 B |  |  |  |  |  |  |  |  |  |  |
| 174.50 | $-88.00^{\circ}$ | $335.00^{\circ}$ | 36.00 | 45.50 | 9.50 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 45.50 | 53.20 | 7.70 |  | GM |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 53.20 | 117.00 | 63.80 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 117.00 | 123.50 | 6.50 |  | 1BA |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 123.50 | 128.50 | 5.00 |  | GM |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 128.50 | 131.35 | 2.85 |  | 1AMT |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 131.35 | 133.35 | 2.00 |  | MLSRB |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 133.35 | 134.00 | 0.65 |  | ML.SMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 134.00 | 135.90 | 1.90 |  | MLSST |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 135.90 | 136.80 | 0.90 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 136.80 | 137.90 | 1.10 |  | MLSMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 137.90 | 138.65 | 0.75 |  | MLSST |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 138.65 | 142.40 | 3.75 |  | MLSMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 142.40 | 142.60 | 0.20 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 142.60 | 143.00 | 0.40 |  | MLSST |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 143.00 | 144.70 | 1.70 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 144.70 | 145.05 | 0.35 |  | MLSMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 145.05 | 146.35 | 1.30 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 146.35 | 146.80 | 0.45 |  | MLSMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 146.80 | 147.50 | 0.70 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 147.50 | 148.00 | 0.50 |  | MLSMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 148.00 | 154.90 | 6.90 |  | HLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 154.90 | 160.15 | 5.25 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 160.15 | 163.00 | 2.85 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 163.00 | 163.70 | 0.70 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 163.70 | 164.40 | 0.70 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 164.40 | 165.90 | 1.50 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 165.90 | 167.15 | 1.25 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 167.15 | 167.80 | 0.65 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | CONTINUED |  |  |  | -- - |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## keGIUNiAl RESUURCES lTu.

UIAMUND URILL , iELORD



| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | Az (t) | From (m) | To (m) | Int. (m) | T.W. (m) | Geology | Sample No. | Rec. \% | s.g. | Ag oz/f | Pb \% | 2n\% | Au oz/t | Fe\% | A3 5 aim | As $\mathrm{cm} / \mathrm{mT}$ |
| 0.00 | -70.000 | $270.00^{\circ}$ | 0.00 | 12.80 | 12.80 |  | Of |  |  |  |  |  |  |  |  |  |  |
| 30.48 | $-71.50^{\circ}$ | 270.009 | 12.80 | 18.90 | 5.10 |  | 2 AC |  |  |  |  |  |  |  |  |  |  |
| 60.96 | $-71.500^{6}$ | $270.00^{\circ}$ | 18.50 | 31.10 | 12.20 |  | U3P |  |  |  |  |  |  |  |  |  |  |
| 91.44 | $-72.00^{\circ}$ | 287.009 | 31.10 | 43,60 | 12.50 |  | anc |  |  |  |  |  |  |  |  |  |  |
| 121.92 | $-71.70^{\circ}$ | 262.001 | 43.60 | 44.30 | 0.70 |  | $\times 0$ |  |  |  |  |  |  |  |  |  |  |
| 243,84 | $-72.00^{\circ}$ | 248.00 | 44.30 | 130.00 | 55.70 |  | EAC |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 130.00 | 134.00 | 4.00 |  | GM |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 134.00 | 135.40 | 1.40 |  | 18? |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 135.40 | 141.50 | E. 10 |  | 5 M |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 141.50 | 144.50 | 3.00 |  | 15 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 144.50 | 147, ${ }^{20}$ | 2,70 |  | 5 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 147.20 | 183.48 | 36. 38 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 183.48 | 195.00 | 11.52 |  | 6 m |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 195.00 | 210.00 | 15.00 |  | 1ARGM |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 210.00 | 211.25 | 1.25 |  | 1RC |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 21.25 | 215.50 | 4.25 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 215,50 | 216, 晈 | 1.35 |  | ML5MS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 216.85 | 217.00 | 2.15 |  | ML5RE |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 219.00 | 221.28 | 2.28 |  | MLSMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 22128 | 22.55 | 0.57 |  | YER |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 221.85 | 223.77 | 1.92 |  | ML5\% |  |  |  |  |  |  |  |  |  |  |
|  |  |  | E23.77 | 234.30 | 10.53 |  | YER |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 234,30 | 234.80 | 0.50 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 234.80 | 235.40 | 0.60 |  | YER |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 235.40 | 239.45 | 4.06 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 239.46 | 239.75 | 0.29 |  | MLSMS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 239.75 | 243.84 | 4.09 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 243.84 | 244.75 | 0.91 |  | M. 5 M 5 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 244.75 | 245.10 | 0.35 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 245.10 | 245.40 | 0.30 |  | MLSCR |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | COMTEMED |  |  |  |  |  |  |  |  |  |

keGlunil resuurces lTu.

## DIÄMOND DRILL , ,ECORD



## ktGIUNAL RESUURCES LTU.

DIAMOND DRILL RECORD


kEGIUIN.AL RESOURCES LTU.

## DIAMUND DRILL . $E$ ECORD



## ktGlunAl RESUUUrces lTu.

## DIAMOND DRILL RECORD



| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | Az (1) | From ( ${ }^{\text {a }}$ | To (n) | Int. (1) | T.W. ( $\mathbf{I}^{\text {a }}$ | Geology | Sampie No. | Rec. \% | s.G. | Ag oz/t | Pb \% | 2 m | Au oz/t | $\mathrm{Fe} \%$ | Ag gimm | Au gm/MT |
| 0.00 | $-85.00^{\circ}$ | 50.00 | 0.00 | 12.30 | 12.30 |  | NR |  |  |  |  |  |  |  |  |  |  |
| 36.70 | $-84.00^{\circ}$ | $50.00^{\circ}$ | 12.30 | 12.50 | 0.20 |  | OB |  |  |  |  |  |  |  |  |  |  |
| 67.20 | $-84.00^{\circ}$ | 60.00 | 12.50 | 21.95 | 9.45 |  | 2AC |  |  |  |  |  |  |  |  |  |  |
| 97.70 | $-86.00^{\circ}$ | $42.00^{\circ}$ | 21.95 | 22.70 | 0.75 |  | XQ |  |  |  |  |  |  |  |  |  |  |
| 122.70 | $-88.00^{\circ}$ | $70.00{ }^{\circ}$ | 22.70 | 24.80 | 2.10 |  | 2 AC |  |  |  |  |  |  |  |  |  |  |
| 153.20 | $-89.00^{\circ}$ | 80.000 | 24.80 | 27.43 | 2.63 |  | CAVE |  |  |  |  |  |  |  |  |  |  |
| 275.10 | $-88.00^{\circ}$ | $220.00^{\circ}$ | 27.43 | 31.80 | 4.37 |  | SAND |  |  |  |  |  |  |  |  |  |  |
| 317.80 | $-87.50^{\circ}$ | $250.00^{\circ}$ | 31.80 | 157.60 | 125.80 |  | 2AC |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 157.60 | 170.70 | 13.10 |  | GH |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 170.70 | 171.30 | 0.60 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 171.30 | 173.60 | 2.30 |  | GM |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 173.60 | 205.44 | 31.84 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 205.44 | 208.80 | 3.36 |  | NR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 208.80 | 214.00 | 5.20 |  | 1B |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 214.00 | 214.90 | 0.90 |  | NR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 214.90 | 257.00 | 42.10 |  | 18 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 257.00 | 271.90 | 14.90 |  | 1BA |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 271.90 | 278.30 | 6.40 |  | 1 AA |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 278.30 | 280.10 | 1.80 |  | IAC |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 280.10 | 288.20 | 8.10 |  | MLI |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 288.20 | 289.70 | 1.50 |  | ML2 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 289.70 | 290.20 | 0.50 |  | ML2MS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 290.20 | 291.10 | 0.90 |  | ML2CR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 291.10 | 291.80 | 0.70 |  | ML2MS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 291.80 | 293.60 | 1.80 |  | ML2 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 293.60 | 294.20 | 0.60 |  | M L 2 CR |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 294.20 | 295.90 | 1.70 |  | ML2 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 295.90 | 296.40 | 0.50 |  | 12 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 296.40 | 298.80 | 2.40 |  | ML2 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 298.80 | 299.00 | 0.20 |  | ML2CR |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | --.. |  |  |  | Continued |  |  | --- |  |  |  |  |  |  |

## keGIunAl RESUURCES LTu.

DIAMOND DRILL RECORD


## APPENDIX "E"

## ASSAY \& ANALSIS RECORDS CORE

NOTE: The first three digits of the sample number are the drill hole number i.e., 275-13701 denotes DDH MW-86-275.

| AMPLE | ELENENT | Aq | AU | Pb | Zn |
| :--- | ---: | ---: | ---: | ---: | ---: |
| IMBEER | UNITS | OPI | OPI | PCI | PCI |
| $2275-13701$ |  | 0.02 | $<0.002$ | 0.01 | 0.01 |

$\qquad$

PROJECT: MIDUAY
PAGE 1

| SAMPLE NUMPEER | ELEMENT | Cu PPM | P4, PPM | Zn PPM | AP9 | As PPM | Au PFS | Ph Pra |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NLMEER | UNITS | PPM | PPM | PPM | PPP |  | PFS | PPM |
| $102279-13728$ |  | 23 | 24 | 107 | 0.2 | 300 | 15 | 830 |
| 12 279-13729 |  | 24 | 4 | 33 | 0.2 | 60 | 10 | <20 |

Geochemical Lab Report

REPORT: 126-5531

| SAMPLE | ELEMENI | Cu | Pb | Zn | Ag | Fe | A5 | Au | Ba |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NUMRER | UNITS | PPM | PPM | PPM | PPH | PCI | PPM | PPB | PPM |  |
| $\because$ |  |  |  |  |  |  |  |  |  |  |
| 12 279-13730 |  | 44 | 4 | 22 | <0.2 |  | 2 | < | 150 |  |
| D2 279-13731 |  | 18 | 5 | 18 | <0.2 |  | 2 | < | 1200 |  |
| D2 279-13732 |  | 26 | 8 | 38 | <0.2 |  | 2 | < | 1000 |  |
| [12 283-13752 |  |  | 10 | 52 | 0.4 |  |  | 10 |  |  |
| D2 293-13753 |  |  | <2 | 12 | $<0.2$ | 0.30 |  | < |  |  |
| D2 293-13754 |  |  | <2 | 145 | $<0.2$ | 0.80 |  | < 5 |  |  |
| D2 293-13755 |  |  | 260 | 3000 | 1.4 | 7.00 |  | < |  |  |
| D2 293-13756 |  |  | 50 | 1000 | 0.2 | 3.45 |  | < |  |  |
| D2 293-13757 |  |  | 9 | 264 | <0.2 | 1.35 |  | < |  |  |
| D2 293-13758 |  |  | <2 | 81 | $<0.2$ | 0.45 |  | < |  |  |
| D2 293-13759 |  |  | 77 | 2200 | 0.6 | 8.00 |  | 5 |  |  |
| D2 293-13760 |  |  | <2 | 60 | $<0.2$ | 0.80 |  | (5) |  |  |
| 02 293-13761 |  |  | <2 | 140 | $<0.2$ | 0.75 |  | < 5 |  |  |
| 12 293-13762 |  |  | 11 | 700 | <0.2 | 5.00 |  | < |  |  |
| D2 293-13763 |  |  | 42 | 950 | <0.2 | >10.00 |  | < |  |  |
| D2 293-13764 |  |  | <2 | 530 | $<0.2$ | 0.75 |  | <5 |  |  |


| REPORT: 426-4947 |  |  |  |  |  | PROJECT: MIDUAY | PAGE 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SAMPLE NUMBER | $\begin{array}{cc} \text { ELEMENI } & \text { Au } \\ \text { UNITS } & \text { OPI } \\ \hline \end{array}$ | $\begin{gathered} \text { Ag } \\ \text { OPI } \end{gathered}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{PCD} \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{PCI} \end{array}$ | SG |  |  |
| 12 280-13733 | 0.002 | <0.02 | 0.08 | 0.10 | 2.8 |  |  |
| D2 280-13734 | $<0.002$ | 1.15 | 0.05 | 0.82 | 3.9 |  |  |
| D2 280-13735 | 0.004 | <0.02 | 0.03 | 0.06 | 2.8 |  |  |
| 12280-13736 | $<0.002$ | 1.88 | 0.16 | 12.00 | 3.9 |  |  |
| D2 280-13737 | 0.002 | 4.76 | 0.22 | 0.12 | 4.3 |  |  |
| D2 280-13738 | $<0.002$ | 1.35 | 0.10 | 2.80 | 4.1 |  |  |
| D2 280-13739 | <0.002 | 1.75 | 0.11 | 3.00 | 4.1 |  |  |
| D2 280-13740 | $<0.002$ | 0.82 | 0.16 | 5.10 | 3.9 |  |  |
| 12 280-13741 | $<0.002$ | 1.51 | 0.34 | 8.20 | 3.9 |  |  |
| D2 280-13742 | <0.002 | 1.60 | 0.26 | 12.00 | 3.8 |  |  |
| 12 280-13743 | <0.002 | <0.02 | <0.01 | 0.11 | 2.8 |  |  |
| D2 280-13744 | $<0.002$ | 0.03 | 0.01 | 0.12 | 2.8 |  |  |
| D2 280-13745 | <0.002 | 1.90 | 0.14 | 12.00 | 4.0 |  |  |
| D2 280-13746 | <0.002 | 1.77 | 0.40 | 7.55 | 4.1 |  |  |
| D2 280-13747 | <0.002 | 12.96 | 8.20 | 15.40 | 3.9 |  |  |
| D2 280-13748 | $<0.002$ | 0.17 | 0.11 | 0.24 | 2.8 |  |  |
| D2 280-13749 | 0.002 | 1.27 | 0.36 | 3.60 | 4.2 |  |  |
| B2 280-13750 | $<0.002$ | 4.98 | 1.49 | 7.23 | 4.2 |  |  |
| D2 280-13751 | <0.002 | 0.96 | 0.07 | 0.34 | 2.8 |  |  |



## Certificate of Analysis

 Tex: 04-352667
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Registered Assayer, Province of British Columbia

## APPENDIX F

## REVERSECIRCULATION DRILL S UMMARY LOGS

MW-86-285
MW-86-286
MW-86-287
MW-86-288
MW-86-289
MW-86-290
MW-86-291
MW-86-292
MW-86-295

#  



| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | Az (1) | From (m) | To (th) | Int. (m) | T.W. (m) | Geology | Sample No. | Rec. \% | s.G. | Ag ozf | Pb \% | 2n \% | Au ozn | Fe\% | Ag ¢1M/AT | Au gu/RT |
| 0.80 | $-32.00^{\circ}$ | 0.00 | 0.00 | 禹玨 | 3.23 |  | NS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 8.83 | 18.30 | -0.07 |  | 08? |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 20.30 | 13.81 | 1.51 |  | $0 \times+6$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 17.81 | 79.85 | 60.05 |  | MLS |  |  |  |  | , |  |  |  |  |  |
|  |  |  | 73.86 | 82.30 | 2.44 |  | CA UN |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 82, 30 | 35.63 | 14.3 3 |  | MLS |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | Pb | Zn | A9 | Av | Ba |  |  |
|  |  |  |  |  |  |  |  | ASSAYS |  |  | PPM | PPK | PPM | PPB | PPH |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 8.23 | 3.75 | 1.52 |  | 08? | 13851 | 0 |  | 280 | 2500 | 0.4 | 5 | 1700= |  |  |
|  |  |  | 9.75 | 11.28 | 1.53 |  | 08? | 13852 | 0 |  | 330 | 4600 | 0.4 | 10 | 2200 |  |  |
|  |  |  | 11.28 | 13.80 | 2. 52 |  | CE? | 13653 | 0 |  | 1280 | 9200 | 1.1 | 15 | 2700 |  |  |
|  |  |  | 12.80 | 14.33 | 1.53 |  | 09 ? | 13854 | 0 |  | 760 | 6900 | 1.0 | <5 | 1500 |  |  |
|  |  |  | 14.33 | 15.65 | :. 52 |  | 08? | 13855 | 0 |  | 560 | 5000 | 0.9 | 5 | 2300 |  |  |
|  |  |  | 15.85 | 17.37 | 1. 52 |  | 08? | 13856 | 0 |  | 440 | 6400 | 0.8 | 10 | 3300 |  |  |
|  |  |  | 17.37 | 16.90 | :. 53 |  | $08+\mathrm{M}$ | 13857 | 0 |  | 270 | 4800 | 0.4 | 5 | 1800 |  |  |
|  |  |  | 18.90 | 19.81 | 0.91 |  |  | 13856 | 0 |  | 149 | 4000 | 0.2 | <5 | 4200 |  |  |
|  |  |  | 19.81 | 21.95 | 2.14 |  | MLS | 13859 | 0 |  | 28 | 830 | <0.2 | 5 | 820 |  |  |
|  |  |  | 21.35 | 23.50 | 1.55 |  | M | 13860 | 0 |  | 16 | 440 | <0.2 | $\stackrel{5}{5}$ | 330 |  |  |
|  |  |  | 23.50 | 25.00 | 1.50 |  | M | 13861 | 0 |  | 6 | 224 | <0.2 | < 5 | 640 |  |  |
|  |  |  | 25.00 | 25.59 | 1.52 |  | MLS | 13862 | 0 |  | 60 | 1200 | $<0.2$ | <5 | 1900 |  |  |
|  |  |  | 35.66 | 37.13 | 1.53 |  | MLS | 13863 | 0 |  | 32 | 540 | $<0.2$ | < | 490 |  |  |
|  |  |  | 43.28 | 44,81 | 1.53 |  | MLS | 13864 | 0 |  | 74 | 860 | <0.2 | <5 | 840 |  |  |
|  |  |  | 46.33 | 47, 85 | 1.58 |  | MLS | 13865 | 0 |  | 24 | 320 | <0.2 | < | 260 |  |  |
|  |  |  | 73.76 | 75.23 | 1.53 |  | M | 13865 | 0 |  | 4 | 200 | $<0.2$ | 5 | 980 |  |  |
|  |  |  | 75.29 | 76.8: | 1.52 |  | MLS | 13867 | 0 |  | 3 | 140 | $<0.2$ | < 5 | 790 |  |  |
|  |  |  | 76.81 | 78.33 | 1.5 |  | MLS | 13868 | 0 |  | $<2$ | 95 | <0.2 | < | 800 |  |  |
|  |  |  | 26.58 | 3E.6E | 3.14 |  | CO:MPO | 13897 | 0 |  | 23 | 520 | <0.2 | < | 630 |  |  |
|  |  |  | 37.19 | 43.29 | 6.09 |  | CCMPO | 13898 | 0 |  | 15 | 352 | <0.2 | < 5 | 160 |  |  |
|  |  |  |  |  |  |  |  | CONTINUED |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## hcàlGryL REsullkleS LTL.



## Finalcial ineülhues lTL.

## La



| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | $A_{2}$ (i) | From (m) | To ini | [mt (m) | T.W. (m) | Geology | Sample No. | Rec. \% | s.G. | Ag oz/ | Pb |  | 2n \% | Au ozt | Fe \% | Ag. $\mathrm{cm} / \mathrm{ht}$ | Au gn/Mt |
| 0.00 | -90.090 | 0.00 | 0.00 | 5 | 5.15 |  | NS |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 5.18 | E0.00 | i5.8t |  | LSY |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 25.00 | 37.30 | 2. 30 |  | LStox |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 67,30 | 26.09 | 0.73 |  | M + ax |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 28.19 | $3: 09$ | 3.4 |  | MLS |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 31.09 | 41.75 | -10.67 |  | M $2+0 \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 4.76 | 55.47 | 13.71 |  | MLS |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 55.47 | 57.00 | 1.53 |  | ML+0x |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 57.061 | 58.52 | 1.5 |  | M. 5 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 56.59 | 65.09 | 4.57 |  | M $2+0 \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 63.09 | 36.30 | 23.21 |  | MLS |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 85.30 | 37.00 | 10.70 |  | CA VN: |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 97.00 | 105.75 | 8.75 |  | M, 5 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 2n | Ag | A | B2 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | PPM | PPr | PPB | PPM |  |  |
|  |  |  |  |  |  |  |  | ASSAYS |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 18.50 | 20.48 | 2.5E |  | LSY | 13869 | 0 |  |  |  | 500 | $<0.2$ | 5 | 4300 |  |  |
|  |  |  | 20.42 | 21.35 | 1.53 |  | LSY | 13870 | 0 |  |  |  | 188 | $<0.2$ | <5 | 3900 |  |  |
|  |  |  | 21.55 | 23.47 | :. 5 E |  | LSY | 13871 | 0 |  |  |  | 220 | $<0.2$ | <5 | 3400 |  |  |
|  |  |  | 23.47 | 23. 00 | 1. 53 |  | LSY | 13872 | 0 |  |  |  | 160 | $<0.2$ | 10 | 4200 |  |  |
|  |  |  | 25.00 | 25.5E | 1.52 |  | LS+ $\mathrm{D}^{\text {X }}$ | 13873 | O |  |  |  | 350 | <0.2 | 5 | 5400 |  |  |
|  |  |  | 66.52 | 38.63 | 2.57 |  | LStox | 13874 | 0 |  |  |  | 860 | 0.2 | 10 | 4100 |  |  |
|  |  |  | 28.15 | 23.57 | 2.40 |  | MLS | 13875 | 0 |  |  |  | 145 | <0.2 | 10 | 960 |  |  |
|  |  |  | 29.57 | $3: 109$ | 1.53 |  | MLS | 13876 | 0 |  |  |  | 324 | $<0.2$ | 10 | 2400 |  |  |
|  |  |  | 3i.09 | 32.61 | 1.5E |  | M2+5X | 13877 | 0 |  |  |  | 820 | $<0.2$ | < 5 | 2900 |  |  |
|  |  |  | $3 \mathrm{E} .6!$ | 34.14 | 1.53 |  | 0x+mic | 13878 | - |  |  |  | 1080 | <0.2 | 5 | 2000 |  |  |
|  |  |  | 34.14 | $35.6 E$ | i. 3.5 |  | mictox | 13879 | 0 |  |  |  | 770 | <0.2 | <5 | 1200 |  |  |
|  |  |  | 35.65 | 37.13 | 1.53 |  | mitox | 13880 | 0 |  |  |  | 880 | <0.2 | 5 | 1400 |  |  |
|  |  |  | 37.19 | 36.71 | . $5 \times$ |  | $0 \times+x_{2}$ | 13881 | 0 |  |  |  | 1360 | $<0.2$ | < | 1400 |  |  |
|  |  |  |  |  |  |  |  | CONTINED |  |  |  |  |  |  |  |  |  |  |
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## ReùlGril reSullkuēS lTL.

## [ıaMuND uRILL : itcoku

| PROPE | TY |  | MIDWA |  |  |  |  | D.H. ${ }^{\text {IVWh }}$ | 96 | Eg | - |  |  | - PA | E E | - ${ }^{\text {a }}$ | E |
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| AREA: |  |  |  |  |  | DIP: |  | Azimut | (t): |  |  | DEPT |  |  |  |  |  |
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| SECTIO |  |  |  |  |  | EAS | ING: |  |  |  |  | DATE | NISHED: |  |  |  |  |
| CORE |  |  |  |  |  | ELE | Vation: |  |  |  |  | CO | ACTOR: |  |  |  |  |
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| COM | S |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  | VEY |  |  |  |  |  |  | GEO | LOGY A | ND A | Say re po | Zn | Ag | Au | Ba |  |  |
| Depth | Dip | $A_{2}$ (1) | From (n) | To in | mitim | TW. (m) | Geology | Sample No. | Rec. \% | s.G. | $\mathrm{Ag} \mathrm{oz}^{\text {O2 }}$ PPM | PPM | PPK | PPB | PPK | qum/MT | Au gu/MT |
|  |  |  | 38.71 | 40.35 |  |  | M $+0 \times$ | 13988 | 0 |  | 95 | 1260 | <0.2 | < | 1600 |  |  |
|  |  |  | 40.23 | 4.76 | -1.65 |  | Mi, CO | 13863 | 0 |  | 92 | 1900 | <0.2 |  | 1200 |  |  |
|  |  |  | 4 4 .76 | 43.25 | :. 5 ? |  | M ${ }^{\text {S }}$ | 13894 | 0 |  | 34 | 880 | <0.2 | 5 | 640 |  |  |
|  |  |  | 43, 20. | 44.8. | :. 53 |  | MS | 13885 | 0 |  | 8 | 280 | <0.2 | < | 150 |  |  |
|  |  |  | 53.93 | 55.47 | 1.52 |  | MLS | 13885 | 0 |  | 14 | 232 | <0.2 | <5 | 370 |  |  |
|  |  |  | 55.47 | 57.00 | 1.5 |  | M $\mathrm{m}_{2}+\mathrm{CX}$ | 13887 | 0 |  | 27 | 640 | <0.2 | < | 400 |  |  |
|  |  |  | 57.00 | 53.5 | : \% \% |  | M. 5 | 13888 | 0 |  | 7 | 279 | <0.2 | < | 290 |  |  |
|  |  |  | 58.53 | 60. 6.4 | 1.5 |  | Mitox | 13889 | 0 |  | 42 | 920 | <0.2 | < | 520 |  |  |
|  |  |  | 60.04 | 61.60 | - 1.55 |  | mi $+0 x$ | 13890 | 0 |  | 22 | 490 | <0.2 | 10 | 210 |  |  |
|  |  |  | 6. 612 | 6 C .95 | 1.49 |  | M 4 +0x | 13891 | 0 |  | 19 | 470 | <0.2 | <5 | 160 |  |  |
|  |  |  | 63.92 | 64.62 | L. 5 |  | M $\mathrm{LS}_{5}$ | 13992 | 0 |  | 23 | 480 | $<0.2$ | < | 220 |  |  |
|  |  |  | 54.62 | -6E. 14 | L.5e |  | MLS | 13893 | 0 |  | 9 | 96 | <0.2 | < | 110 |  |  |
|  |  |  | 78.33 | 73.36 | - |  | 4.5 | 13894 | 0 |  | 4 | 168 | <0.2 | < | 40 |  |  |
|  |  |  | 79,66 | -8.30 | 1.52 |  | W2. | :3995 | 0 |  | 4 | 200 | <0.2 | 5 | 90 |  |  |
|  |  |  | 101.19 | 10.72 | 1.53 |  | MLS | 13836 | 0 |  | 12 | 200 | <0.2 | <5 | 410 |  |  |
|  |  |  | 5.18 | 18. 50 | 13.72 |  | COMPJ | 13501 | 0 |  | 46 | 82 | <0.2 | < | 2800 |  |  |
|  |  |  | 44.8: | 53.5 | 3.14 |  | COMPC | 13902 | 0 |  | 3 | -136 | $<0.2$ | < | 150 |  |  |
|  |  |  | E5. 14 | 78.35 | 12.6 |  | caipo | 13903 | 0 |  | 5 | 152 | <0.2 | < | 380 |  |  |
|  |  |  | 31. 39 | 101. 19 | 19.81 |  | COMPC | 133014 | 0 |  | <2 | 50 | <0.2 | < 5 | 370 |  |  |
|  |  |  | :00. 72 | 105.75 | -3.04 |  | compl | 13905 | 0 |  | 6 | 45 | <0.2 | < | 830 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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## Feùlural resullkles lTU．

## ［IAMUND URILL $A E C O R D$



| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | $A z$（1） | From（ia） | To（in） | Int（ n ） | T．W．（m） | Geology | Sample No． | Rec．\％ | S．G． | Ag 02f |  | Pb \％ |  | Zn \％ | Au ozth | Fe\％ | Ag $\mathrm{gm} / \mathrm{MT}$ | Au gm／Mt |
| 0.00 | $-50,000$ | 0.009 | 0.00 | 36 | 3.65 |  | NS |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 3.65 | 58.59 | 54.85 |  | His |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 58.52 | 63.03 | 4． 57 |  | OX＋${ }^{\text {and }}$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 63.19 | 67．E？ | 4.58 |  | NS |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 67.67 | 69.13 | $\therefore 52$ |  | Mis |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 69.19 | 37.48 | 18.23 |  | NS |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 87.48 | 89.00 | 1．5 |  | $0 \times+$ W |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  | AS5AYS |  |  |  | Pb |  | Zn | Ag | Au | Ba |  |  |
|  | ． |  |  |  | ， |  |  |  |  |  |  | PPM |  | PPK | PPM | PP8 | PPY |  |  |
|  |  |  | 3.65 | Fin | 1．5E |  | 禹S | ：3905 | 0 |  |  | 290 |  | 6600 | $<0.2$ | 5 | 740 |  |  |
|  | ． |  | 5.18 | 6.71 | 1.33 |  | N： 5 | 13907 | 0 |  |  | 67 |  | 2500 | $<0.2$ | ＜ | 720 |  |  |
|  |  |  | 11.28 | 12.86 | － 1.5 FE |  | HLS | 13908 | 0 |  |  | 86 |  | 1210 | ＜0．2 | 5 | 530 |  |  |
|  | ： |  | 17.37 | 18．70 | 11.33 |  | MiS | 13909 | 0 |  |  | 75 |  | 560 | $<0.2$ | ＜5 | 280 |  |  |
|  |  |  | 18.50 | 20.4 | ！ 1.5 |  | \％LS | 13910 | 0 |  |  | 40 |  | 570 | ＜0．2 | ＜ 5 | 320 |  |  |
| r |  |  | 20， 42 | 21.95 | ：，5j |  | M ${ }_{\text {L }}$ | 13911 | 0 | ． |  | 134 |  | 520 | ＜0．2 | く5 | 530 |  |  |
|  |  |  | 55.47 | 57.00 | $1 . \mathrm{E}$ |  | MLS | 13912 | 0 |  |  | ＜2 |  | 144 | ＜0．2 | く | 350 |  |  |
|  |  |  | 57.00 | 55.5 | 1.58 |  | MLS | 13913 | 0 |  |  | 18 |  | 156 | ＜0．2 | ＜5 | 370 |  |  |
|  |  |  | 58.32 | 60.65 | －1．53 |  | M $x^{2}+0 \times$ | 13914 | 0 |  |  | 26 |  | 780 | ＜0．2 | ＜ | 470 |  |  |
|  |  |  | 60.05 | 61.57 | 1.59 |  | $0 \times+8$ | 13915 | 0 |  |  | 40 |  | 1100 | $<0.2$ | 5 | 560 |  |  |
|  |  |  | 6：． 57 | 63.05 | 1 ¢．5E |  | OX＋M | 13916 | 0 |  |  | 57 |  | 1520 | く0．2 | 5 | 500 |  |  |
|  |  |  | 67.67 | 59.15 | 1． E $_{\text {E }}$ |  | MLS | 13917 | 0 |  |  | 56 |  | 720 | $<0.2$ | 5 | 350 |  |  |
|  | ， |  | 87.48 | 53.6 | － 1.5 |  | $\mathrm{CX}_{2} \mathrm{M}_{-}$ | 13919 | 0 |  |  | 71 |  | 900 | ＜0．2 | ＜ 5 | 1000 |  |  |
|  |  |  | 6.71 | 1.29 | 4.57 |  | Carpo | 13919 | 0 |  |  | 47 |  | 540 | ＜0．2 | ＜ | 760 |  |  |
|  |  |  | 12.80 | ［17．37 | 1－4．57 |  | Cowip | 13920 | 0 |  |  | 25 |  | 400 | ＜0．2 | ＜ 5 | 300 |  |  |
|  |  |  | 21． 35 | 5.47 | 35．5 |  | ［ampo | 13921 | 0 |  |  | 31 |  | 250 | $<0.2$ | ＜ | 790 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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## heùluril resuulkuES lTL.





| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | $\mathrm{A}_{2}(1)$ | From ! \% ) | 10 in) | Int ( m ) | T.W. (x) | Geology | Sample No. | Rec. \% | S.G. | Ag oz/t | Pb \% | Zn \% | Au ozll | $\mathrm{Fe} \%$ | Ag $\mathrm{gm} / \mathrm{MT}$ | Au gm/xT |
| 0.00 | $-70.80$ | 0.009 | 0,00 | E, 5 | E. 28 |  | 15 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 5.10 | 2.5 | ;6.7? |  | ML3 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 2: 95 | 24.93 | 3.64 |  | M y + + X |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 24. 39 | 65.14 | 40.35 |  | MS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 55.34 | E6. 75 | 0.91 |  | CRVE |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 66.73. | 77.73 | 0.37 |  | YiS |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 77.72 | 76.15 | 2, 45 |  | CRVE |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 70.:8 | 59.5 | :9. 97 |  | Mis |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 58.15 | 95. 67 |  |  | Hitix |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 33.57 | :10,36 | 0.57 |  | M C S |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 110.35 | 2insis | 0.57 |  | Fincx |  |  |  |  |  |  |  |  |  |  |
|  |  |  | $121.0 \pm$ | 159.77 | 43.76 |  | \% ${ }_{2}$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  | Pb | \% | Ag | Ba |  |  |
|  |  |  |  |  |  |  |  | ASSAYS |  |  |  | PPM | PPK | PPM | PPK |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 9.75 | :1, 20 | 2. 53 |  | MS | 13929 | 0 |  |  | 13 | \% | <0.2 | 280 |  |  |
|  |  |  | 11.28 | S2.80 | i. $\mathrm{E}^{\text {2 }}$ |  | \% | 13323 | 0 |  |  | 61 | 176 | <0.2 | 200 |  |  |
|  |  |  | 57.37 |  | $\therefore .55$ |  | MLS | 13924 | 0 |  |  | 44 | 322 | <0.2 | 450 |  |  |
|  |  |  | 15.90 | 60.43 | 1.32 |  | MLS | 13935 | 0 |  |  | 31 | 285 | <0.2 | 300 |  |  |
|  |  |  | 20.42 | 2., 35 | 2.55 |  | Pitax | 13926 | 0 |  |  | 83 | 1410 | <0.2 | 520 |  |  |
|  |  |  | 83.95 | 83.47 | 1.28 |  | \% $2+0 x$ | 13987 | 0 |  |  | 94 | 1300 | <0.2 | 350 |  |  |
|  |  |  | E3. 47 | 24.95 | - 5.5 |  | PiL $+0 \times$ | 13928 | 0 |  |  | 75 | 930 | <0.2 | 270 |  |  |
|  |  |  | 24.39 | E.EE | 1.5 |  | MLS | 13923 | 0 |  |  | 24 | 368 | $<0.2$ | 180 |  |  |
|  |  |  | 6530 | \% 28 | 1.5 |  | MS | 13730 | 0 |  |  | 24 | 260 | <0.2 | 220 |  |  |
|  |  |  | 41.75 | $4{ }_{4} 5$ | 湤 |  | MS | 13331 | 0 |  |  | 30 | 460 | <0.2 | 150 |  |  |
|  |  |  | 6.. 57 | 63. 0 | $\therefore 2$ |  | YLS | 13922 | 0 |  |  | 18 | 206 | <0.2 | 310 |  |  |
|  |  | . | 63.03 | 64.63 | $\underline{1.53}$ |  | MLS | 13933 | 0 |  |  | 21 | 170 | <0.2 | 270 |  |  |
|  |  |  | 64.5 | E6. 14 | 1.5 |  | MLS | 13934 | 0 |  |  | 16 | 224 | <0.2 | 120 |  |  |
|  |  |  | 65.14 | 67.67 | . 5.5 |  | MLS | 13935 | 0 |  |  | 34 | 273 | $<0.2$ | 260 |  |  |
|  |  |  |  |  |  |  |  | CONTINUSD |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORI |  |  |  |  |  |  |  |  | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{PPH} \\ 15 \end{array}$ | $\begin{aligned} & \mathrm{Zn} \\ & \mathrm{PPH} \\ & 150 \end{aligned}$ | $\begin{array}{r} \text { Ag } \\ \text { PPH } \\ <0.2 \end{array}$ |  | a |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | $A z(1)$ | From $(m)$ | To imi | Int（io） | T．W．（n） | Geology | Sample No． | Rec．\％ | S．G． | Ag oz／t |  |  |  |  | An Em／MT | Au gn／mT |
|  |  |  | 67.67 | 53.3 | 1，3 |  | 7tis | 13936 | 0 |  |  |  |  |  |  |  |  |
|  |  |  | 63.2 | 72.75 | $\therefore 52$ |  | Mis | 13937 | 0 |  |  | 545 | 480 | 0.2 | 710 |  |  |
|  |  |  | 70．71 | 75.24 | 1.53 |  | 颜 | 13938 | 0 |  |  | 29 | 158 | $<0.2$ | 430 |  |  |
|  |  |  | 72． 24 | 72．75 | －河 |  | \＃5 | 13929 | 0 |  |  | 31 | 112 | $<0.2$ | 220 |  |  |
|  |  |  | 73.75 | 7 7 | 1.53 |  | $0 \times 5$ | 13940 | 0 |  |  | 13 | 100 | ＜0．2 | 280 |  |  |
|  |  |  | 75． 27 | － 75.8 | $\therefore \mathrm{E}$ |  | 4.5 | 13941 | 0 |  |  | 12 | 72 | $<0.2$ | 200 |  |  |
|  |  |  | 76.61 | 75.33 | 1.5 |  | $\underline{4}$ | 13942 | 0 |  |  | 10 | 77 | $<0.2$ | 280 |  |  |
|  |  |  | $7 \mathrm{C}, ~ 3{ }^{3}$ | 79.8 | －i．55 |  | KLS | 13943 | 0 |  |  | 27 | 104 | $<0.2$ | 580 |  |  |
|  |  |  | 73.85 | 51．35 | 1．5： |  | 75 | 13344 | 0 |  |  | 66 | 160 | $<0.2$ | 270 |  |  |
|  |  |  | 81.35 | 953： | $\therefore 53$ |  | ， | 13545 | 0 |  |  | 34 | 92 | $<0.2$ | 240 |  |  |
|  |  |  | 93， 10 | 95 5 | 1． 5 |  | H5 | 13346 | 0 |  |  | 37 | 450 | ＜0．2 | 730 |  |  |
|  |  |  | 56，65 |  | － 5 |  | Y， | 13347 | 0 |  |  | 29 | 350 | ＜0．2 | 770 |  |  |
|  |  |  | 98． 15 | 95．${ }^{1}$ | $\therefore$ ¢ |  | M $+2 X$ | 13948 | 0 |  |  | 52 | 260 | ＜0．2 | 1000 |  |  |
|  |  |  | 93.67 | 101． 3 | $\therefore$－ 5 |  | Mis | 13943 | 0 |  |  | 18 | 210 | ＜0．2 | 720 |  |  |
|  |  |  | 101.13 | ： 03.75 | － 1.5 |  | Y－S | 13350 | 0 |  |  | 31 | 390 | ＜0．2 | 950 |  |  |
|  |  |  | 10， 72 | 104.54 | ：E\％ |  | 4， 5 | 1395］ | 0 |  |  | 42 | 520 | ＜0．2 | 3000 |  |  |
|  |  |  | 104．24 | 105.77 | $\therefore 53$ |  | MS | 1395 | 0 |  |  | 28 | 260 | $<0.2$ | 720 |  |  |
|  |  |  | $10 \mathrm{E}, 77$ | ：07，$=5$ | ¢ E |  | MES | 13953 | 0 |  |  | 23 | 324 | $<0.2$ | 890 |  |  |
|  |  |  | 107.29 | 16E．E | 1．55 |  | M，S | 13954 | 0 |  |  | 15 | 170 | ＜0．2 | 860 |  |  |
|  |  |  | ：09， 8 ¢ | 101035 | $\therefore$ |  | MES | 13955 | 0 |  |  | 29 | 248 | ＜0．2 | 1500 |  |  |
|  |  |  | $: 10.34$ | 211.85 | $\therefore \mathrm{Cz}$ |  |  | 13956 | 0 |  |  | 21 | 296. | ＜0．2 | 800 |  |  |
|  |  |  | 112．Ė | ＂运 | 湤它 |  | $0 \times$ | 13957 | 0 |  |  | 32 | 300 | 0.3 | 7100 |  |  |
|  |  |  | 113.35 | ：14．5． | $\bigcirc 5$ |  | Ex＋$x_{2}$ | 13358 | 0 |  |  | 49 | 520 | 0.2 | 4000 |  |  |
|  |  |  | 1：4．9： | $\therefore$ ¢ 48 | $\therefore 5$ |  | $\cdots \mathrm{M}+0 \mathrm{X}$ | 13957 | 0 |  |  | 33 | 420 | 0.2 | 1600 |  |  |
|  |  |  | 116.43 | $\because 17.95$ | 2.5 |  | $\cdots$ | 13350 | 0 |  |  | 58 | 700 | 0.2 | 2600 |  |  |
|  |  |  | 1：7，9\％ | ¢ ${ }^{2}$ | ：58 |  | $\cdots$ | 13361 | 0 |  |  | 51 | 720 | 0.2 | 720 |  |  |
|  |  |  | $\pm: 7.48$ | 1500 | $\therefore 53$ |  | M $2+ \pm X$ | 13582 | 0 |  |  | 27 | 392 | ＜0．2 | 360 |  |  |
|  |  | ． | －E\％． 01 | \％ | － 5.5 |  | MS | 13363 | 0 |  |  | 24 | 336 | ＜0．2 | 730 |  |  |
|  |  |  | ：E2， 5 |  | ，号 |  | MS | 13364 | 0 |  |  | 13 | 110 | $<0.2$ | 760 |  |  |
|  |  |  | 5.18 | 3，${ }^{\text {I }}$ | 4.57 |  | CCOFO | 13365 | 0 |  |  | 30 | 304 | $<0.2$ | 230 |  |  |
|  |  |  | 12.36 | 17．3\％ | 4．：37 |  | COYPD | 13956 | 0 |  |  | 11 | 360 | $<0.2$ | 90 |  |  |
|  |  |  |  |  |  |  |  | CONTINUED |  |  |  |  |  |  |  |  |  |



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| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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| Depth | Dip | $A_{2}(1)$ | From (m) | To (ix) | 1 nm [ ;in) | T.W. (m) | Geology | Sample No. | Hec. \% | S.G. | Ag ozil | Pb \% |  | 2n \% | Au ozh | Fe \% | Ag gm/MT | Au gu/h |
| 0.00 | $-20.00{ }^{\circ}$ | 0.00 | 0.00 | $3.6 \div$ | . 3.56 |  | N |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 3.65 | 28.04 | -34,38. |  | LSY |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 28.04 | 44.812 | . 8.77 |  | 15+0x |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 44.8: | 53.80 | 13.79 |  | LSY |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 54.80 | 59.50 | 0.70 |  | GU16E |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 59.50 | 53.05 | 3.53 |  | LSY |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 63,03 | 54.62 | : 53. |  | LStox |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 64.62 | 67.67. | 3.25 |  | M CO |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 67.67 | 305 | 1_30.86 |  | WH. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 22.53 | 3545 | $3{ }^{3}$ |  | NS |  |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |  |  |  | MIIS | PPM | PPM |  |  | PPM |  |  |
|  |  |  | 28.04 | 34.14 | 6.10 |  | LStix | 14201 | 0 |  |  | ${ }^{1} 43$ | 272 |  |  | 2900 |  |  |
|  |  |  | 34. 14 | 40.23 | 5.69 |  | LStox | 18202 | 0 |  |  | 57 | 100 |  |  | 1900 |  |  |
|  |  |  | 40.23 | 4.5 | 5.:0 |  | LStiox | 18203 | 0 |  |  | 36 | 94 |  |  | 2000 |  |  |
|  |  |  | $4{ }^{4} .33$ | 52.45 | 5.10 |  | LSY | 18204 | 0 |  |  | 25 | 98 |  |  | 2100 |  |  |
|  |  |  | 52.43 | 5.5 | 1 E.03 |  | LSY | 18205 | 0 |  |  | 19 | 174 |  |  | 3500 |  |  |
|  |  |  | 50.53 | 63.05 | 4, 57 |  | LSY | 18205 | 0 |  |  | 24 | 180 |  |  | 3700 |  |  |
|  |  |  | 63.05 | 64.60 | 1.55 |  | LS+DX | 18207 | 0 |  |  | 43 | 460 |  |  | 5000 |  |  |
|  |  |  | 64.52 | 66.94 | 1.92 |  | mi +0 x | 18208 | 0 |  |  | . 164 | 480 |  |  | 1900 |  |  |
|  |  |  | 66.14 | 67.67 | : 5.5 |  | PL $2+0 \mathrm{~L}$ | 18209 | 0 |  |  | 34 | -335 |  |  | 860 |  |  |
|  |  |  | 57.67 | 69.3 |  |  | kLS | 18210 | 0 |  |  | 12 | 114 |  |  | 330 |  |  |
|  |  |  | 82.00 | 90. 5 | , 55 |  | \% 15 | 18211 | 0 |  |  | 53 | 290 |  |  | 80 |  |  |
|  |  |  | 26 | 25, 㐱 | 34.38 |  | compo | 18212 | 0 |  |  | 18 | 170 |  |  | 2200 |  |  |
|  |  |  | 69.9. | 72.84 | 3.6 |  | C0, 9 | 16213 | 0 |  |  | 22. | 182 |  |  | 110 |  |  |
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| SURVEY DATA |  |  | GEOLOGY AND AS |  |  |  |  |  |  |  | $\begin{aligned} & \text { EMEXIEI } \\ & \text { UNITS } \end{aligned}$ | Pb <br> PPY | $\begin{array}{r} \mathbf{Z n} \\ \text { PPM } \end{array}$ |  | $\begin{gathered} \text { Ba } \\ \text { PPM } \end{gathered}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | Dip | A2 (1) | From 18i | 10 | Int. O | T.W. $\{n\}$ | Geology | Sample No. | Rec. \% | S.G. |  |  |  |  |  | AO Qm/MT | Au 03/MT |
|  |  |  | 73.75 | 3, 5 | 3-5 |  | EExpo | 18331 | 0 |  |  | 18 | 153 | $<0.2$ | 210 |  |  |
|  |  |  | E0\% |  | -7.57 |  | corod | 18.35 | 0 |  |  | 10 | 115 | $<0.2$ | 590 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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SURVEY DATA

| Depth | Dip | $\wedge_{2}$ (1) | Fromi (0) | in | Int in | T.W. (m) | Geology | Sample No. | Rec. \% | s.G. | Ag oz/h | Pb \% | Zn \% | Au ozf | Fe\% | Ag_gu/mT | Au gm/RT |
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| 0.00 | -30,00\% | 0.00 | 0.00 | E.15. | 5.15 |  | 13 |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 5 |  | 20, 43 |  | LSY |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 55.55 | 47.85 | ¢ 3.9 |  | LStox |  |  |  |  |  |  |  |  |  |  |
|  |  |  | -- 47.EE | 43.30 | ... |  | 1.5Y |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 49.38 | 8.3) | 1.E |  | -Stcx |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 50.90 | $5 \mathrm{E}, 5$ | - Fi |  | cx |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 53.42 | E5. ${ }^{\text {E }}$ | 1_ |  | $\mathrm{rax}_{\sim}+3 \mathrm{x}$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 58.56 | 16.iE | 1-4.20 |  | $\mathrm{H}_{3}$ |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  | ASSAYS |  |  | HLEXENI | Pb | 7n | Ag | B3 |  |  |
|  |  |  |  |  |  |  |  |  |  |  | WNITS | PPK | PPM | PPM | PPY |  |  |
|  |  |  | E5.56 | 4.0 | E. 10 |  | :S+DX | 18933 | 0 |  |  | 23 | 105. | <0.2 | 1200 |  |  |
|  |  |  | 4.75 | 47.35 | 8. 03 |  | LStDX | 18234 | 0 |  |  | 67 | 220 | $<0.2$ | 3200 |  |  |
|  |  |  | 47.85 | 43.10 | $\underline{15}$ |  | LSY | 18235 | 0 |  |  | 26 | 398 | $<0.2$ | 4800 |  |  |
|  |  |  | 49.35 | E, 2 | 1. 3 |  | $0 \times+25$ | 18236 | 0 |  |  | 50 | 395 | $<0.2$ | 4900 |  |  |
|  |  |  | E0, 00 | 1-EE.43 | $\therefore .5$ |  | DX | 18237 | 0 |  |  | 152 | 780 | 0.3 | 3900 |  |  |
|  |  |  | 52.43 | E, 5 | $\therefore .53$ |  | M2 + UX | 18238 | 0 |  |  | 66 | 1400 | 0.5 | 1600 |  |  |
|  |  |  | 53. E® $^{4}$ | ! E2, 47 | : 2. |  | $x+0 x$ | 10399 | 0 |  |  | 62 | 1000 | 0.2 | 1500 |  |  |
|  |  |  | E3.67 | 57.90 | 1 $\therefore 35$ |  | $0 x+$ Y | 18340 | 0 |  |  | 75 | 1560 | 0.4 | 2000 |  |  |
|  |  |  | 67.00 | 55.5 | 1.5 |  | OXPM M | 18241 | 0 |  |  | 50 | 640 | <0.2 | 1900 |  |  |
|  |  |  | 58.5 | O, 2 | $\therefore 2$ |  | M, 5 | 18:42 | 0 |  |  | 15 | 245 | <0.2 | 740 |  |  |
|  |  |  | 5.15 | TE, 6 |  |  | CGYEO | 18543 | 0 |  |  | 45 | 145 | $<0.2$ | 1600 |  |  |
|  |  |  | 60,04 | E1. 3 | 2i.5i |  | cexpe | $18: 44$ | 0 |  |  | 15 | 80 | <0.2 | 710 |  |  |
|  |  |  | 5:23 | Cintis | $\because 5$ |  | CMPT | 18e. ${ }^{5}$ | 0 |  |  | 13 | 65 | 0.2 | 910 |  |  |
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GEOLOGY AND ASSAY RECORD


| SURVEY DATA |  |  | GEOLOGY AND ASSAY RECORD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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| Depth | Dip | $A_{2}$ (i) | Fromi ${ }^{\text {jol }}$ | 70 \% | Wer | T.W. (f) | Geology | Sample No. | Rec. \% | s.g. | Ag ozh | Pb \% | 2n \% | Av 02/ | Fe\% | Ag om/MT | Au gm/MT |
| 0.00 | $-72,609$ | 0.008 | 0.00 | 4.51 | 4.75 |  | Ns |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 5.57. | 2.20 | -7a3 |  | L.5Y |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 21.23 | 24.6) | 二景 |  | $15+5 \times$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 24.00 | $\therefore 00$ | $\therefore 0$ |  | $x+0 x$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 25010 | 53.4 | - -34.44 |  | Mis |  |  |  |  |  |  |  |  |  |  |
|  |  |  | -53.44 | -. 78.64 | -520 |  | NS |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  | ASSAYS |  |  | EIEMENI | Pb | Zn | Ag | Ba |  |  |
|  |  |  |  |  |  |  |  |  |  |  | LNITS | PPM | PPM | PPM | PPM |  |  |
|  |  |  | 14.5 | 2.42 | 6.02 |  | L. 59 | 18246 | 0 |  |  | 34 | 110 | $<0.2$ | 4500 |  |  |
|  |  |  | 2.42 | 2 Ca | ..53 |  | LSY | 18247 | 0 |  |  | 38 | 140 | $<0.2$ | 4700 |  |  |
|  |  |  | 3.55 | 20.47 | :. 5 2 |  | OX+LS | 18248 | 0 |  |  | 195 | 1300 | 0.2 | 9700 |  |  |
|  |  |  | 23.47 | 24.93 | 1 1.E2 |  | M 2 +0x | 18249 | 0 |  |  | 570 | 17000 | 1.9 | 4200= |  |  |
|  |  |  | 24.95 | EE | $\underline{.65}$ |  | YLS | 18250 | 0 |  |  | 172 | 8800 | 0.5 | 1400 |  |  |
|  |  |  | 8 | 36.4 | ¢ ${ }^{5}$ |  | YLS | 1825: | 0 |  |  | 62 | 3100 | 0.5 | 550 |  |  |
|  |  |  | 4.57 | 443 | 2.5 |  | camio | 18252 | 0 |  |  | 36 | 108 | 0.2 | 2500 |  |  |
|  |  |  | 23.04 | 76.56 |  |  | caryen | 19253 | 0 |  |  | 65 | 1100 | 0.3 | 670 |  |  |
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## APPENDIX "G"

ASSAY AND ANALYSIS RECORDS SHEETS- CHIPS
CERTIEICATES Of ANALYSIS - CHIPS
NOTE: The first three digits of the samplenumber are the drill hole numberi.e., 285-13851 denotes RCD MW-86-285.

|  | SAMPLE NUMBER | $\begin{gathered} \text { ELEMENT } \\ \text { UNITS } \end{gathered}$ | Pb PPM | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{PPK} \end{array}$ | $\begin{aligned} & \text { Ag } \\ & \text { PPM } \end{aligned}$ | $\begin{aligned} & \text { AU } \\ & \text { PPB } \end{aligned}$ | $\begin{gathered} \mathrm{Ba} \\ \mathrm{PPM} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | R2 285-13851 |  | 280 | 2500 | 0.4 | 5 | $1700=$ |
|  | R2 285-13852 |  | 330 | 4600 | 0.4 | 10 | 2200 |
|  | R2 285-13853 |  | 1280 | 9200 | 1.1 | 15 | 2700 |
|  | R2 285-13854 |  | 760 | 6900 | 1.0 | <5 | 1500 |
|  | R2 285-13855 |  | 560 | 5000 | 0.9 | 5 | 2300 |
|  | R2 285-13856 |  | 440 | 6400 | 0.8 | 10 | 3300 |
|  | R2 285-13857 |  | 270 | 4800 | 0.4 | 5 | 1800 |
|  | R2 285-13858 |  | 149 | 4000 | 0.2 | <5 | 4200 |
|  | R2 285-13859 |  | 28 | 830 | <0.2 | 5 | 820 |
|  | R2 285-13860 |  | 16 | 440 | <0.2 | < | 330 |
|  | R2 285-13861 |  | 6 | 224 | <0.2 | < | 640 |
|  | R2 285-13862 |  | 60 | 1200 | $\langle 0.2$ | < | 1900 |
|  | R2 285-13863 |  | 32 | 540 | <0.2 | < | 490 |
|  | R2 285-13864 |  | 74 | 860 | <0.2 | <5 | 840 |
|  | R2 285-13865 |  | 24 | 320 | <0.2 | く5 | 260 |
|  | R2 285-13866 |  | 4 | 200 | <0.2 | 5 | 980 |
|  | R2 285-13867 |  | 3 | 140 | <0.2 | < 5 | 790 |
|  | R2 285-13868 |  | <2 | 95 | <0.2 | < | 800 |
|  | R2 286-13869. |  | 34 | 500 | <0.2 | 5 | 4300 |
|  | R2 286-13870 |  | 21 | 188 | <0.2 | < | 3900 |
|  | R2 286-13871 |  | 18 | 220 | <0.2 | <5 | 3400 |
|  | R2 286-13872 |  | 32 | 160 | $<0.2$ | 10 | 4200 |
|  | R2 286-13873 |  | 57 | 350 | <0.2 | 5 | 5400 |
|  | R2 286-13874 |  | 78 | 860 | 0.2 | 10 | 4100 |
|  | R2 286-13875 |  | 10 | 145 | $<0.2$ | 10 | 960 |
|  | R2 286-13876 |  | 29 | 324 | <0.2 | 10 | 2400 |
|  | R2 286-13877 |  | 85 | 820 | <0.2 | < | 2900 |
|  | R2 286-13878 |  | 75 | 1080 | <0.2 | 5 | 2000 |
|  | R2 286-13879 |  | 34 | 770 | <0.2 | <5 | 1200 |
|  | R2 286-13880 |  | 35 | 880 | $<0.2$ | 5 | 1400 |
|  | R2 286-13881 |  | 112 | 1360 | <0.2 | < | 1400 |
|  | 82 286-13882 |  | 95 | 1260 | <0.2 | < | 1600 |
|  | R2 286-13883 |  | 92 | 1900 | $<0.2$ | 5 | 1200 |
|  | R2 286-13884 |  | 34 | 880 | <0.2 | 5 | 640 |
|  | R2 286-13885 |  | , | 280 | <0.2 | < | 150 |
|  | R2 286-13886 |  | 14 | 232 | <0.2 | <5 | 370 |
|  | R2 286-13887 |  | 27 | 640 | <0.2 | < 5 | 400 |
|  | R2 286-13888 |  | 7 | 279 | $<0.2$ | < | 290 |
|  | R2 286-13889 |  | 42 | 920 | <0.2 | < | 520 |
|  | R2 286-13890 |  | 22 | 490 | $<0.2$ | 10 | 210 |


| SAMPLE NUKBER | ELETENT UNITS | $\begin{gathered} \text { Pb } \\ \text { PPK } \end{gathered}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{PPK} \end{array}$ | $\begin{array}{r} \text { Ag } \\ \text { PPK } \end{array}$ | $\begin{array}{r} \text { AU } \\ \text { PPB } \end{array}$ | $\begin{gathered} \text { Ba } \\ \text { PPY } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R2 286-13891 |  | 19 | 470 | <0.2 | < | 160 |
| R2 286-13892 |  | 23 | 480 | <0.2 | <5 | 220 |
| R2 286-13893 |  | 9 | 96 | <0.2 | <5 | 110 |
| R2 286-13894 |  | 4 | 168 | <0.2 | <5 | 40 |
| 22 286-13895 |  | 4 | 200 | $<0.2$ | 5 | 90 |
| R2 286-13896 |  | 12 | 200 | $<0.2$ | <5 | 410 |
| R2 285-13897 |  | 23 | 520 | $<0.2$ | く5 | 630 |
| R2 285-13898 |  | 15 | 352 | <0.2 | <5 | 160 |
| R2 285-13899 |  | 82 | 124 | <0.2 | く5 | 290 |
| 12 285-13900 |  | 32 | 36 | <0.2 | < | 1200 |
| R2 286-13901 |  | 46 | 82 | <0.2 | < | 2800 |
| R2 286-13902 |  | 3 | 136 | 6.2 | < 5 | 150 |
|  |  | 5 | 152 | <0.2 | < | 380 |
| L2 286-13904 |  | <2 | 50 | $<0.2$ | <5 | 370 |
| R2 286-13905 |  | 6 | 45 | $<0.2$ | < | 830 |
| 22 287-13906 |  | 290 | 16600 | $<0.2$ | 5 | 740 |
| R2 287-13907 |  | 67 | 2500 | $<0.2$ | <5 | 720 |
| R2 287-13908 |  | 86 | 1210 | <0.2 | 5 | 530 |
| R2 287-13909 |  | 75 | 560 | $<0.2$ | < | 280 |
| R2 287-13910 |  | 40 | 570 | $<0.2$ | < | 320 |
| R2 287-13911 |  | 134 | 520 | <0.2 | < 5 | 530 |
| R2 287-13912 |  | <2 | 144 | <0.2 | < | 350 |
| R2 287-13913 |  | 18 | 156 | $<0.2$ | <5 | 370 |
| R2 287-13914 |  | 26 | 780 | <0.2 | < | 470 |
| R2 287-13915 |  | 40 | 1100 | $<0.2$ | 5 | 560 |
| R2 287-13916 |  | 57 | 1520 | $<0.2$ | 5 | 500 |
| R2 287-13917 |  | 56 | 720 | $<0.2$ | 5 | 350 |
| R2 287-13918 |  | 71 | 900 | <0.2 | < 5 | 1000 |
| R2 287-13919 |  | 47 | 540 | $<0.2$ | < | 760 |
| R2 287-13920 |  | 25 | 400 | <0.2 | < | 300 |
| R2 287-13921 | , | 31 | 250 | $<0.2$ | < 5 | 790 |

## Geochemical

Lab Report
Tclex: 04-352667


## Geochemical <br> Lab Report

## REPORT: 126-5677

PROJECI: HIDUAY
PAGE 1

| SAKPLE | ELEYENI | Pb | $Z_{n}$ | Ag | AU | Ba | Ba |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| NUKBER | UNITS | PPH | PPH | PPM | PPB | PPH | PCI |


| R2 289-13976 | 43 | 1930 | 0.2 | 960 |
| :--- | :--- | ---: | ---: | ---: |
| R2 289-13977 | 50 | 7000 | 0.4 | 1400 |
| R2 289-13978 | 43 | 3400 | 0.4 | 910 |
| R2 289-13979 | 29 | 1260 | $<0.2$ | 1200 |
| R2 289-13980 | 22 | 640 | $<0.2$ | 1100 |


| R2 289-13981 | 19 | 230 |
| :--- | :--- | :--- |
| R2 289-13982 | 14 | 152 |
| R2 289-13983 | 17 | 194 |
| R2 289-13984 | 19 | 296 |
| R2 289-13985 | 11 | 203 |


| R2 289-13986 | 24 | 460 |
| :--- | ---: | ---: |
| R2 298-13987 | 5 | 150 |
| R2 299-13988 | 15 | 90 |
| R2 289-15331 | 5840 | 410 |
| R2 289-15332 | 5910 | 6800 |


| R2 289-15333 | $>10000$ | 15800 | 14.0 | 240 | $>20000$ |
| :--- | ---: | ---: | ---: | ---: | ---: |
| R2 289-15334 | $>10000$ | 11600 | 15.0 | 260 | $>20000$ |
| R2 290-18201 | 430 | 272 | 0.3 |  | 2900 |
| R2 290-18202 | 57 | 100 | $<0.2$ |  | 1900 |
| R2 290-18203 | 36 | 94 | $<0.2$ |  | 2000 |
| R2 290-18204 |  |  |  |  |  |
| R2 290-12805 | 25 | 98 | $<0.2$ |  | 2100 |
| R2 290-18206 | 19 | 174 | $<0.2$ | 3500 |  |
| R2 290-18207 | 24 | 180 | $<0.2$ | 3700 |  |
| R2 290-18208 | 43 | 460 | $<0.2$ | 5000 |  |
| R2 290-18209 | 164 | 480 | $<0.2$ | 1900 |  |
| R2 290-18210 |  |  |  |  |  |
| R2 290-18211 | 34 | 335 | $<0.2$ | 860 |  |
| R2 290-18212 | 12 | 114 | $<0.2$ | 330 |  |
| R2 290-18213 | 53 | 290 | $<0.2$ | 80 |  |
|  | 18 | 170 | $<0.2$ |  | 2200 |
|  | 22 | 182 | $<0.2$ | 110 |  |

59
109
21
24
$14 \quad 1780$
780

| 550 | 2.4 | 6000 |
| :--- | :--- | :--- |510

$2.8 \quad 680$
$0.9 \quad 1900$
0.91900
0.21000
-

| 0.2 | 110 |
| ---: | ---: |
| $<0.2$ | 60 |
| $<0.2$ | 90 |
| $<0.2$ | 130 |
| 0.2 | 70 |

## 530

| 0.2 | 530 |
| ---: | ---: |
| $<0.2$ | 210 |
| $<0.2$ | 270 |


| 5.6 | 780 | $>20000$ | 5.3 |
| :--- | :--- | :--- | :--- |

14.0
$760>20000$17.0
10.0
12.0
PROJECT: MIDWAY

| גEPORT: 126-5858 |  |  |  |  |  | PROJECT: MIDUAY | PAGE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2AMPLE <br> HAMBER | ELEXENI WIIS | $\begin{gathered} \mathrm{Pb} \\ \mathrm{PPM} \end{gathered}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{PPH} \end{array}$ | Ag PPM | $\begin{array}{r} \text { Ba } \\ \text { PPM } \end{array}$ |  |  |
| R2 291-18214 |  | 16 | 75 | 0.2 | 2200 |  |  |
| 22 291-18215 |  | 20 | 60 | $<0.2$ | 1900 |  |  |
| R2 291-18216 |  | 19 | 180 | $<0.2$ | 2600 |  |  |
| R2 291-18217 |  | 22 | 440 | $<0.2$ | 4200 |  |  |
| 22 291-18218 |  | 24 | 490 | $<0.2$ | 3900 |  |  |
| 22 291-18219 |  | 23 | 420 | <0.2 | 3900 |  |  |
| 12 291-18220 |  | 66 | 520 | 0.2 | 4300 |  |  |
| 22 291-18221 |  | 85 | 840 | 0.4 | 1500 |  |  |
| R2 291-18222 |  | 42 | 640 | 0.2 | 800 |  |  |
| 2291-18223 |  | 21 | 180 | $<0.2$ | 320 |  |  |
| R2 291-18224 |  | 37 | 530 | 0.5 | 350 |  |  |
| R2 291-18225 |  | 19 | 240 | 0.2 | 170 |  |  |
| R2 291-18226 |  | 64 | 980 | 0.5 | 720 |  |  |
| $2291-18227$ |  | 47 | 670 | 0.3 | 490 |  |  |
| R2 291-18228 |  | 27 | 315 | 0.2 | 220 |  |  |
| 12 291-18229 |  | 29 | 170 | 0.3 | 1900 |  |  |
| R2 291-18230 |  | 31 | 85 | $<0.2$ | 2000 |  |  |
| 22 291-18231 |  | 18 | 153 | $<0.2$ | 210 |  |  |
| 32 291-18232 |  | 10 | 115 | $<0.2$ | 590 |  |  |
| K2 292-18233 |  | 23 | 105 | <0.2 | 1200 | . |  |
| 12 292-18234 |  | 67 | 220 | $<0.2$ | 3200 |  |  |
| .12 292-18235 |  | 26 | 398 | <0.2 | 4800 |  |  |
| R2 292-18236 |  | 50 | 395 | <0.2 | 4900 |  |  |
| 12 292-18237 |  | 152 | 780 | 0.3 | 3900 |  |  |
| 12 292-18238 |  | 66 | 1400 | 0.5 | 1600 |  |  |
| 22 292-18239 |  | 62 | 1000 | 0.2 | 1500 |  |  |
| R2 292-18240 |  | 75 | 1560 | 0.4 | 2000 |  |  |
| R2 292-18241 |  | 50 | 640 | $<0.2$ | 1900 |  |  |
| R2 292-18242 |  | 15 | 245 | <0.2 | 740 |  |  |
| $\times 2$ 292-18243 |  | 45 | 145 | $<0.2$ | 1600 |  |  |
| R2 292-18244 |  | 15 | 80 | <0.2 | 710 |  |  |
| 2 292-18245 |  | 13 | 65 | 0.2 | 910 |  |  |
| 12 295-18246 |  | 34 | 110 | <0.2 | 4500 |  |  |
| R2 295-18247 |  | 38 | 140 | <0.2 | 4700 |  |  |
| 92 295-18248 |  | 195 | 1300 | 0.2 | 9700 |  |  |
| $\times 2$ 295-18249 |  | 570 | 17000 | 1.9 | $4200=$ |  |  |
| R2 295-18250 |  | 172 | 8800 | 0.5 | 1400 |  |  |
| 12 295-18251 |  | 62 | 3100 | 0.5 | 550 |  |  |
| .2 295-18252 |  | 36 | 108 | 0.2 | 2500 |  |  |
| R2 295-18253 |  | 65 | 1100 | 0.3 | 670 |  |  |


| SAAPLE <br> MMFBER | ELEMENI <br> UNITS | Pb <br> PCI |
| :--- | ---: | ---: |
| R2 289-15333 |  | 4.12 |
| R2 289-15334 |  | 2.50 |

$\qquad$












