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McDAME DEPOSIT

REPORT ON THE 1986 EXPLORATION PROGRAM

by

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SUMMARY

From June 1, 1986 to February 2, 1987 an underground exploration program, consisting of drifting, raising, drilling, and bulk sampling, was conducted on the McDame Asbestos Deposit near Cassiar Mine. The purpose of the program was to delineate reserves and obtain technical data that would allow a comprehensive pre-feasibility study of the deposit. In total, 329.4 m of drifting advance as an extension to the existing 1415 m level adit, 4960.6 m of diamond drilling, and 241 m of raising was completed. Total expenditures for the project are $4,735,400.

Considerable difficulty in ground support escalated costs of underground drifting and reduced productivity. Changes to the program were required to remain within budget. Receipt of a Financial Assistance for Mineral Exploration (FAME) grant provided funds to complete the diamond drilling portion of the program. The Ministry of Energy, Mines and Petroleum Resources of British Columbia is gratefully acknowledged for their incentive program which has directly aided and extended exploration on the McDame project.

Of 27 holes drilled, 2 were in argillite to locate a fault. Of the remaining 25 holes, only 2 did not penetrate significant fibre. Results from all holes will be considered with previous drilling and information from drifting to conduct a pre-feasibility study to determine economic feasibility.

PHOTOGRAPH 1

McDame Hill

Shop and waste dump at portal of 1415 m elevation adit.

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MCDAME EXPLORATION PROJECT - 1986

1. INTRODUCTION

1.1 Location

Cassiar, a town of 1200 people, is located in the Cassiar Mountains of northern British Columbia approximately 160 kilometres southwest of Watson Lake, Yukon. Access is by good all weather road from the Cassiar-Stewart highway (Number 37). The closest airport is Watson Lake, which is serviced by Canadian Pacific Airlines' Boeing 737 jets three times a week (Figure 1).

Cassiar has been the site of open pit asbestos mining since 1953 and a well developed infrastructure for mining and milling of asbestos is established. The McDame deposit is located south of Cassiar pit at a lower elevation in the same mountain (Photo 1).

Access to the 1415 m level portal (lower) is by good dirt road from the mine haul road.

1.2 History

An upper adit at 1563 m elevation driven in 1978-1979 to allow diamond drilling under Cassiar Pit intersected an unsuspected ultramafic body containing abundant asbestos fibre of long length. A 290 m drift was extended southerly to better access the new deposit and a total of 12,092 m in 37 holes was drilled in 1980 and 1981 to outline a new, buried deposit now called McDame (Figure 2).

Airborne magnetic surveys in 1983, followed by a deep drill hole from surface in 1984 indicated the ultramafic body was large and that fibre content extended southerly. Estimated reserves were 62 million tonnes of a grade and fibre value similar to Cassiar Mine.

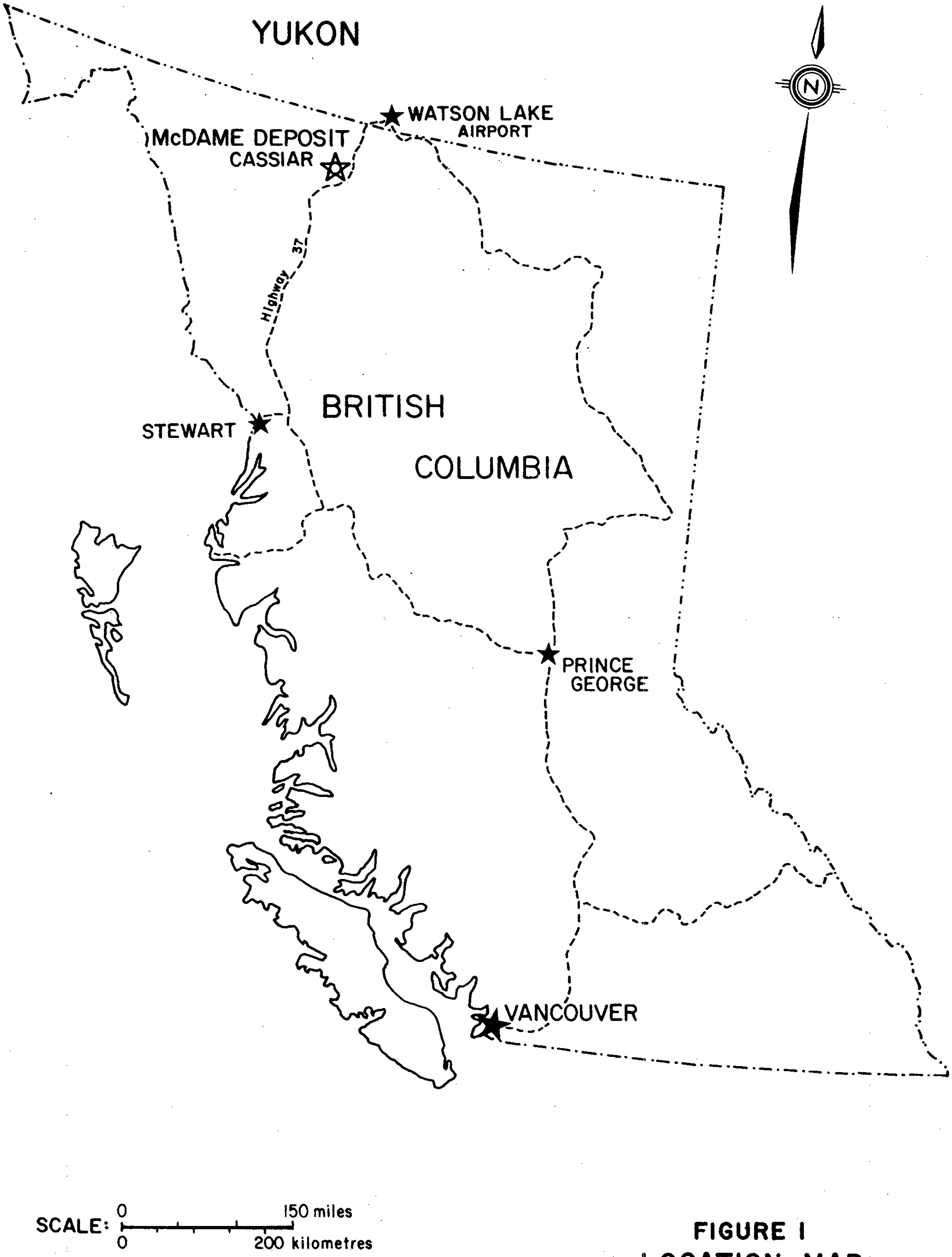
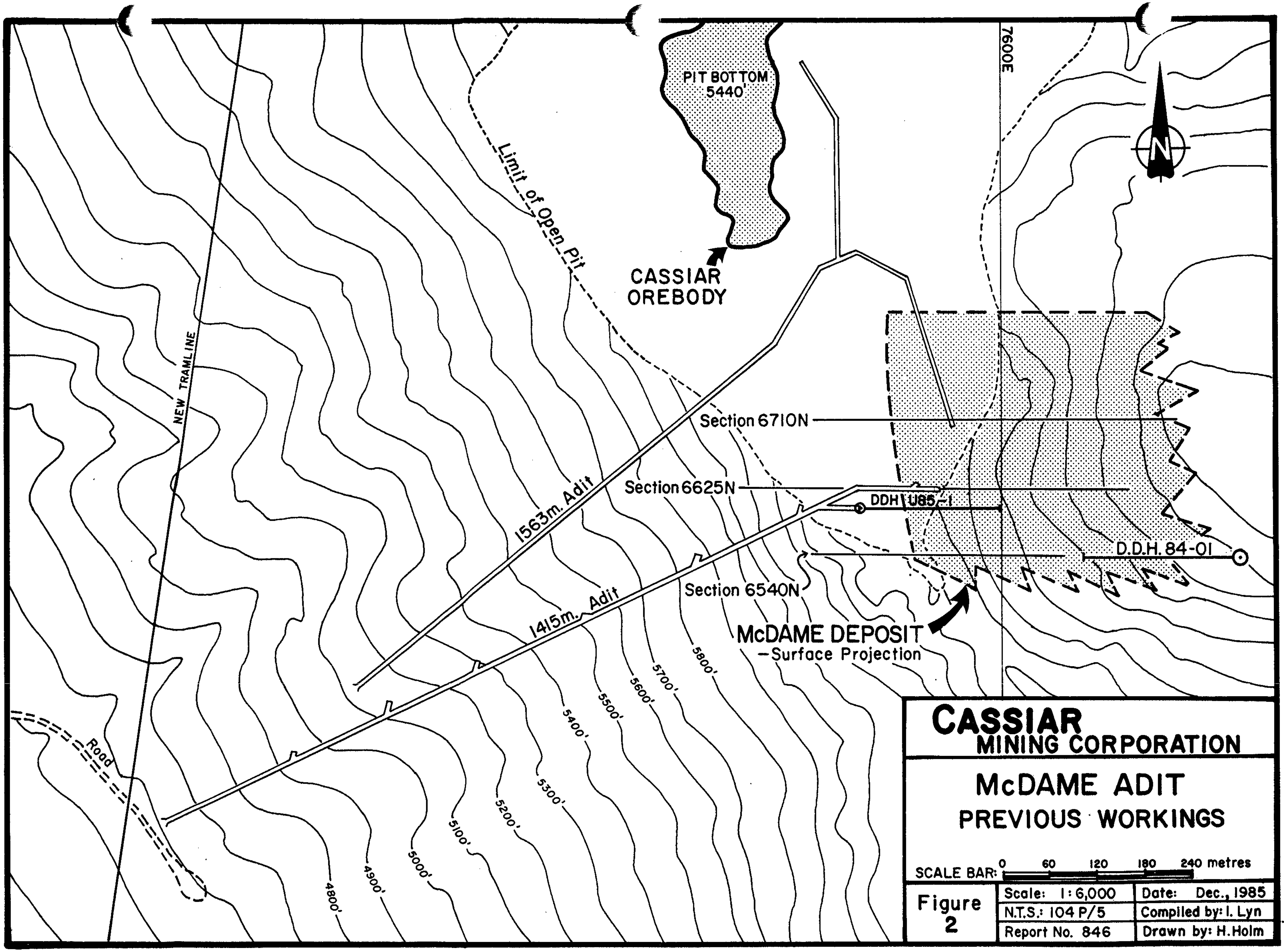


FIGURE I
LOCATION MAP
McDAME DEPOSIT



PIT BOTTOM 5440'
CASSIAR OREBODY
Limit of Open Pit
NEW TRAMLINE
7600E
Section 6710N
Section 6625N
Section 6540N
DDH U85-1
D.D.H. 84-01
1563m. Adit
1415m. Adit
McDAME DEPOSIT
-Surface Projection
Road
4800'
4900'
5000'
5100'
5200'
5300'
5400'
5500'
5600'
5700'
5800'
N
CASSIAR MINING CORPORATION
McDAME ADIT
PREVIOUS WORKINGS
SCALE BAR: 0 60 120 180 240 metres
Figure 2
Scale: 1:6,000
N.T.S.: 104 P/5
Report No. 846
Date: Dec., 1985
Compiled by: I. Lyn
Drawn by: H. Holm

In 1985, the (lower) 1415 m elevation drift was driven 1081 m to intersect the deposit 150 m below the previous workings to confirm the nature of the mineralization, and to obtain a bulk sample for mill test purposes. A total of 875 tonnes was milled averaging 9.65% fibre with a high percentage of long fibre.

1.3 Objectives

In April 1986 an exploration programme was designed to access the footwall of the McDame deposit and to define reserves between the 1350 and 1415 m elevations. A decline to 1350 m was planned with 7000 m of diamond drilling to be done from a footwall drift 275 m in length. A raise was planned to join 1350 m elevation with 1563 m for ventilation and safety purposes. Collection of a bulk sample by means of a test block cave were also planned.

After consultation in June 1986 with Dr. Dennis Laubscher, Consulting Mining Engineer for Steffen, Robertson and Kirsten, the scope of the exploration programme changed. The principal objectives of the programme were defined as:

a) to define 10 million tonnes of ore, or more, recoverable by block cave techniques from a single level, 1350 m,

b) to obtain an adequate bulk sample to determine milling characteristics and fibre quality data, and

c) to determine the most suitable mining and ground support techniques to cope with underground conditions.

Secondary objectives included:

a) to ensure exploration did not prejudice future production,

b) to determine the eastern margin and hanging wall contact of the McDame Deposit,

c) to locate exploration to aid future development, and

d) to obtain rock mechanics data for mine planning.

With these objectives in mind the exploration programme was modified to include extending the 1415 m drift easterly to 7700E and northerly to 6767N, a distance of 300 m. Diamond drilling was to be on east-west sections. The raise shortened to join 1415 m and 1563 m levels and plans for the decline to the 1350 m level, footwall drift and test cave were abandoned.

As the exploration programme progressed it became apparent that:

a) the likelihood of defining the required reserves above 1350 m elevation diminished,

b) the cost of drift advance was much higher than anticipated due to the high cost of ground support, and

c) the rate of drift advance was slow.

A second conference was held in late October 1986 with Dr. Laubscher and a revised exploration emphasis was agreed upon. Drilling was modified, where possible, to give more information on the location and nature of the footwall of the deposit and on the tenor of the fibre adjacent to the footwall. This information is necessary if a footwall draw point plan for mining is contemplated.

1.4 Drifting/Raising

1.4.1 Drifting

Initially, drifting was for three purposes, to extend the 1415 m drift, to ramp down to 1350 m elevation, and to establish a footwall drift. When the program was changed in June, emphasis was placed in establishing drill stations in the northeast corner of the deposit and to obtain a bulk sample from the deposit from a different location than the bulk sample collected in 1985.

As mining techniques were to be experimented with, the mining cycle was changed to determine effect on rate of production, cost per metre and ground stability. Use of a continuous miner (Roadheader) was planned on the assumption that cutting with bits would cause less disturbance than blasting.

Tender documents for the proposed drifting and raising were prepared and sent to 6 mining contractors in April, 1986 and a site visit was provided.

Canadian Mine Development Limited was selected for their low bid and experience in exploration and development drifting in previous years at Cassiar.

CMD personnel arrived on site May 31, 1986, and commenced rehabilitation of the 1415 m adit and portal surface area. Exploration work began on June 6, 1986, utilizing conventional methods (drill and blast) with an electric hydraulic single boom jumbo until July 24, 1986. Drift development after July 25 was performed by a continuous miner (Roadheader).

A Voest-Alpine AM 75 Roadheader arrived on site June 23rd and by July 24 was assembled, modified to meet B.C. Mines Regulations standards, and began its move to the face. It reached the face July 28 and was in use until October 1.

Drift development after October 2, 1986 was performed with jacklegs until completion of the drifting on November 8, 1986.

Over the 154 day drifting period, 329.4 m of underground advance was completed as summarized below:

METHOD	DAYS	ADVANCE (m)	AVERAGE (m/day)
JUMBO	50	104.5	2.09
ROADHEADER	66	129.7	1.97
JACKLEG	38	95.2	2.50
PROJECT	154	329.4	2.14

The days shown represent the time period between when advance began and was completed including all down time.

Ground support requirements were not noticeably different among the three mining methods.

1.4.2 Raising

Initially a ventilation raise was to be constructed between the 1350 m and 1563 m levels. When the decline and footwall drift portions of the program were abandoned, the raise was modified to connect the adits at the 1415 m and 1563 m levels.

Raising commenced from the 1415 m level on June 10, by conventional drill and blast methods and was completed to the 1563 m level on October 16. Over the 129 day period 241 m was completed for an average advance rate of 1.87 m/day. Raise development was considerably slower than anticipated due to shortages of raise miners.

1.5 Diamond Drilling/Geology

The initial programme of 7000 m of diamond drilling from a footwall drift at 1350 m elevation required numerous inclined holes to reach the hanging wall contact. Specialized underground diamond drills with the capability of drilling HQ diameter core (6.35 cm) to depths in excess of 400 m, including inclined holes, were required. Letters requesting tenders for drilling with such equipment were sent to 10 diamond drill companies on April 21, 1986, six of which declined to bid for various reasons.

A comparison of the four bids received was made using metres planned and fixed estimates for such items as standby, moves, consumables, etc. Advanced Diamond Drilling had the lowest bid and was awarded the contract.

On June 16, 1986 a Super Drill (Photo 2) arrived on the property. Holes 86-01 and 86-02 were drilled to provide information on the footwall fault in preparation for the decline, and holes 86-03 and 86-04 were drilled in advance of drifting to gather information on anticipated ground conditions.

In late June the exploration emphasis was changed and a revised programme was initiated. Drilling was suspended July 4 until the next drill station could be prepared. On August 4 drilling resumed, with the Super Drill, from the newly prepared Diamond Drill Station on Section 6650N. Drifting continued towards the drill stations to be located on Sections 6706N and 6767N.

On September 21 a second drill, a converted Boyles Brother 37, arrived on site and was moved underground in the 1563 m elevation drift to commence drilling of the hanging wall of the deposit.

A total of 4960.6 m in 27 holes was completed (Table 1).

PHOTOGRAPH 2

Diamond Drill

Super Drill belonging to Advanced Diamond Drilling. Machine was capable of drilling HQ holes to considerable depth within a 360° radius.

TABLE 1

McDame 1986 Exploration - Drilling Statistics

Hole #	Station	Easting	Northing	Started	Finished	AZ	Decl.	Elevation	Depth M	TOTAL M
U8601		7368.22	6608.03	JUNE 20	JUNE 27	41.0	-21.0	1409.09	113.39	113.39
U8602		7368.22	6608.03	JUNE 27	JULY 2	125.0	-25.0	1409.09	114.30	227.69
U8603	6649	7605.80	6649.90	AUG 4	AUG 5	90.0	-2.5	1414.90	30.17	257.86
U8604	6649	7605.90	6651.00	AUG 6	AUG 13	65.7	-1.8	1415.07	160.93	418.79
U8605	6649	7603.80	6649.90	AUG 14	AUG 20	0.0	-90.0	1413.80	92.35	511.14
U8606	6649	7604.90	6649.75	AUG 21	AUG 22	88.8	48.1	1416.00	16.46	527.60
U8607	6649	7605.00	6649.90	AUG 22	AUG 30	90.0	-44.0	1413.80	141.43	669.03
U8608	6649	7604.40	6649.89	AUG 30	SEPT 7	89.0	-27.0	1414.15	210.01	879.04
U8609	6649	7605.00	6649.90	SEPT 8	SEPT 9	90.0	-4.0	1414.75	72.85	951.88
U8610	6649	7605.60	6649.90	SEPT 10	SEPT 22	90.0	-10.0	1414.60	350.22	1302.10
U8611	6649	7605.85	6649.90	SEPT 22	OCT 4	90.0	-18.0	1414.30	299.31	1601.42
U8612	6649	7601.20	6647.80	OCT 6	OCT 11	270.0	-38.0	1414.00	165.20	1766.62
U8613	6828	7526.25	6827.62	OCT 11	OCT 23	86.0	-40.2	1568.59	238.05	2004.67
U8614	6649	7601.40	6647.80	OCT 12	OCT 18	270.0	-3.0	1414.80	168.86	2173.53
U8615	6649	7601.86	6649.79	OCT 19	OCT 25	277.3	-68.4	1414.27	184.71	2358.24
U8616	6828	7627.80	6827.50	OCT 26	NOV 10	91.45	-25.25	1568.20	297.18	2655.42
U8617	6706	7713.50	6710.19	OCT 27	NOV 3	88.13	-14.27	1416.10	228.30	2883.71
U8618	6706	7710.30	6698.50	NOV 4	NOV 12	181.76	-54.00	1415.20	264.57	3148.28
U8619	6767	7702.90	6765.86	NOV 15	NOV 19	89.50	30.00	1420.10	77.42	3225.70
U8620	6707	7711.09	6714.68	NOV 18	NOV 26	0.62	0.13	1416.52	158.80	3384.50
U8621	6767	7703.20	6765.80	NOV 19	NOV 25	89.08	-14.22	1418.40	194.77	3579.27
U8622	6767	7702.10	6765.80	NOV 26	DEC 3	89.55	-68.47	1417.90	273.71	3852.98
U8623	6706	7713.40	6711.75	NOV 28	DEC 1	89.55	-60.00	1415.40	103.63	3956.61
U8624	6706	7713.50	6711.75	DEC 1	DEC 11	86.67	-52.82	1415.40	286.21	4242.82
U8625	7600	7599.40	6630.00	DEC 5	DEC 10	180.00	-44.00	1413.43	270.66	4513.48
U8626	7600	7600.90	6630.90	JAN 9/87	JAN 19/87	139.90	-46.00	1431.10	228.60	4742.08
U8627	7681	7681.60	6676.20	JAN 20/87	FEB 2/87	157.30	-35.00	1415.20	218.54	4960.62

2. ELECTRICAL POWER

In 1985, electrical power for all underground operations at McDame was supplied by a 750 kW mobile diesel generator located at the portal. Due to high operation and maintenance costs associated with diesel generators, a powerline to the 1415 m portal was proposed as a long-term low cost method of providing electrical power to the project.

Tenders were requested for relocation of a surplus substation from Cassiar Mine to the 1415 m level portal and construction of a power line from the open pit main electrical feeder powerline to the substation. Three companies visited the site, two submited tenders. McGregor Construction of Edmonton, Alberta, was awarded the contract.

A local contractor cleared a right of way for the powerline and prepared a level pad for the substation. McGregor Construction personnel arrived on site June 26 and the substation was relocated and the powerline was completed by July 14, 1986 (Photo 3).

Four months after completion of the powerline, high winds caused the electrical conducters to come in contact with each other resulting in a major power failure. In December, the electrical conducters were tightened and resagged under warranty by McGregor personnel and the problem has abated.

PHOTOGRAPH 3

Powerline and Substation

A Powerline was constructed from the main mine supply line to a substation erected behind the portal of 1415 m elevation adit.

3. DRIFTING/RAISING

3.1 Logistics/Methods

Crews from Canadian Mine Development arrived on site June 1 and began to rehabilitate their maintenance shop facilities and organize their crews. Underground equipment from the 1985 exploration program remained on site during the winter and as a result, minimal maintenance was required to make the equipment fully operational.

All of the underground services were reconnected and the 1415 m level was made safe by scaling down loose material from the back and side walls.

Work on a Diamond Drill Station and the 1563 m level ventilation raise cut-out were performed before drift development commenced. Drifting on the 1415 m level extension by jumbo drill commenced June 11, 1986.

On July 25, 1986, a Voest-Alpine AM75 continuous miner replaced the jumbo drill in the 1415 m level extension. Advance was very slow for the first two weeks because of numerous reasons including: mechanical problems, lack of operator/equipment familiarity, delays, and interruptions to services.

A revised payment plan which included a revised bonus schedule was agreed to with CMD on August 12 and as a result, the daily advance improved dramatically (Table 2). This revised schedule was employed for the remainder of the project and mutually modified when required.

After two months of development with the continuous miner, it was withdrawn from service and replaced by jacklegs. All remaining development was performed by jacklegs which had the greatest overall average advance (Table 2).

TABLE 2

COMPARISON OF RATES OF ADVANCE

METHOD	TIME PERIOD	DAYS	ADVANCE (m)	AVERAGE (m/day)	AREA
Jumbo	June 11 to July 9	29	83.1	2.87	Adit
Jumbo	July 10 to July 24	15	21.4	1.43	DDS 6650
Roadheader	July 28 to Aug. 11	15	20.8	1.39	Adit (Force Acct.)
Roadheader	Aug. 12 to Sept. 21	41	106.9	2.61	Adit/DDS 6706
Jackleg	Oct. 6 to Nov. 8	34	92.2	2.71	N. Drift (7700E)

AVERAGE (EXCLUDING DDS 6650 AND DELAYS IN STARTING N. DRIFT) 2.55 m/day over 119 days

3.2 Roadheader

3.2.1 General

The exploration program permitted the testing of different mining techniques for evaluation for future development. A continuous miner was tested as an alternative to conventional drilling and blasting. It was felt the continuous miner would offer advantages such as:

a) the ability to shape the drift back in the shape of an arch giving improved ground stability, thereby requiring less ground support to maintain the opening,

b) the elimination of the drilling and blasting cycle resulting in greater advance per day and less impact stress to the ground resulting in further reduction in ground support, and

c) the ability to load directly to trucks via a conveyor chain, eliminating the need for LHD mobile equipment.

Two continuous miners were considered, a Dosco LH 1300 and a Voest-Alpine Am 75 (Photo 4). Both are 75 tonne class continuous miners and operate on similar principles with the main differences being the double cutting heads (Photo 5) of the Voest-Alpine over the single head of the Dosco and the articulated discharge conveyor (Photo 6) of the Voest-Alpine versus fixed of the Dosco. Rates for the continuous miners from both Dosco and Voest-Alpine were similar. The AM 75 was selected for the program because of availability.

3.2.2 Description of Voest-Alpine AM 75 Roadheader

The AM 75 measures 11.8 m long by 6.8 m wide by 2.8 m high and weighs 74.8 tonnes (Photo 4). Two cutting drums containing tungsten carbide bits (Photo 5) are located at the end of a boom capable of vertical and horizontal movement. Water sprayed from nozzles located on the boom behind each rotating drum suppresses dust. Gathering arms located on an apron under the boom collect and direct material up a conveyor funnel and onto a chain conveyor (Photo 6). The material is conveyed through the machine and discharges directly into trucks behind the machine.

Electric water-cooled motors operating at 1100v/60/3ø are attached to the continuous miner. A stepdown transformer is required to reduce the primary mine voltage of 4160v/60/3ø for the continuous miner. Water coolant is circulated through the continuous miner at the rate of 10 to 15 gal/minute at 50 p.s.i. during operation.

PHOTOGRAPH 4

Continuous Miner (Roadheader)

Shown here the Roadheader is ready for operation and is being towed to the adit. Note cutting head to right behind bulldozer and conveyor to left.

PHOTOGRAPH 5

Roadheader Head

Cutting teeth on rotating head are well displayed. Gathering arms (right one is being inspected by operator) push muck up apron through hole in centre onto conveyor belt.

Deficiencies were noted when the AM 75 arrived on site as the continuous miner did not meet British Columbia mine regulation standards, the most notable being the need for:

a) a fire suppression system,

b) a current limiting device on the AM 75 transformer for grounding protection,

c) fire resistant water-based hydraulic oil, and

d) a diode on the instrument panel to monitor for an open circuit.

These problems were rectified before the machine was walked underground.

3.2.3 Roadheader Advance

The AM 75 arrived June 23 and required 5 days for assembly. A three week delay occurred before the roadheader could be employed due to the following:

a) upgrading of the roadheader to meet British Columbia Mines Regulation Act Standards,

b) preparation for roadheader development not complete, and

c) change over from diesel generated power to power supplied from the powerline.

On July 24 the roadheader commenced walking to the face with the aid of L.H.D. to transport the transformer and electrical cable.

PHOTOGRAPH 6

Roadheader Conveyor

Articulate conveyor belt allows discharge of muck directly into trucks.

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On July 24 the roadheader commenced walking to the face with the aid of L.H.D. to transport the transformer and electrical cable.

Cutting of the adit sidewalls in areas was required to permit passage of the machine. On July 28 the Voest-Alpine AM 75 reached the development face.

Since this was the first time that a Roadheader had been employed for drift development in serpentenite, and the resultant affect on ground support was unknown, Canadian Mine Development and Cassiar agreed to place development with the Roadheader on a two week trial on Force Account from July 28 to August 11. A time study of the operations was performed. Drift development was 20.8 m for a two week period for an average development rate of 1.39 m/day (Table 2).

Drift development was not satisfactory and discussions were held with CMD officials to determine methods of increasing the daily advance. A bonus, payable to the miners based on productivity, was agreed to and added to the Force Account and between August 12 and September 21 a total of 106.9 m was cut for an average advance of 2.61 m/day.

Water spray from the dust suppression nozzles were generally effective in suppressing dust, although occasionally additional water spray was necessary. Gravimetric sampling performed several times at the face determined that the asbestos fibre count was below the Threshold Limit Value (T.L.V.) of 2 fibres/cc (Appendix I). If dust conditions at the face had become unacceptable, a contingency plan to handle excessive dust had been devised. It involved the hanging of a ventilation curtain behind and alongside the Roadheader. A ventilation duct connected to an electrical ventilation fan would transport air from the face into a dust settling chamber. This system works satisfactorily in potash operations where water cannot be employed for dust suppression.

Numerous development cycles were tried to determine the maximum rate of advance with the Roadheader. The optimum development cycle is as follows:

a) cut 1 m advance with Roadheader,

b) shotcrete back and sides,

c) install rockbolts and straps laterally on back,

d) install welded mesh screen, and

e) apply additional layer of shotcrete, if required.

Advancing more than 1 m in most ground encountered was unfeasible as the ground was incompetent and the size of the Roadheader prevented easy ground support techniques.

3.2.4 Discussion

On this project the model of continuous miner used did not satisfy the original objectives. Problems associated with the operation of the continuous miner are as follows:

a) the Roadheader was so large that men and equipment could not walk past easily. All movement of personnel and materials was over the top,

b) despite no blasting, ground conditions were not noticeably improved and generally the same amount of ground support was required as with conventional mining,

c) cutting the drift opening in a shape of an arch did not assist in ground support. Serpentinite cohesion forces are very low for an arch to be self-supporting. Additional ground support such as shotcrete and spiles are required to maintain the opening,

d) due to the poor ground conditions, the drift width was just large enough for the Roadheader to pass with less than 30 cm of clearance on either side. Access to lower sections of the side walls for ground support was difficult which resulted in several areas not being adequately supported,

e) even experienced operator had difficulty maintaining line and grade. In some instances where the operators did not cut to full width, squeezing of the ground caused the Roadheader to become trapped and recutting of these areas was required,

f) the chain conveyor on the Roadheader is poorly designed and was easily jammed by muck resulting in delays and sometimes breakage of the flights and/or chains,

g) operating the Roadheader with the articulated conveyor in the maximum swing position caused chain conveyor down time preventing the Roadheader from developing curves with radii of less than 15 m, and

h) due to chain conveyor problems, the mechanical availability of the Roadheader was 72% during the test program.

Some of the above problems may be rectified by a smaller machine (i.e. 25 tonne) or cutting a larger drift (not practical with ground support costs). Serious reconsideration should be undertaken before committing to development with continuous miners.

Despite the above reservations, intuitively, the Roadheader should allow faster advance than conventional mining as the number of cycles are reduced. Properly set up to allow rapid ground support from the machine and with adequate muck haulage, the development cost per metre of advance should be lowered.

3.3 Drill and Blast

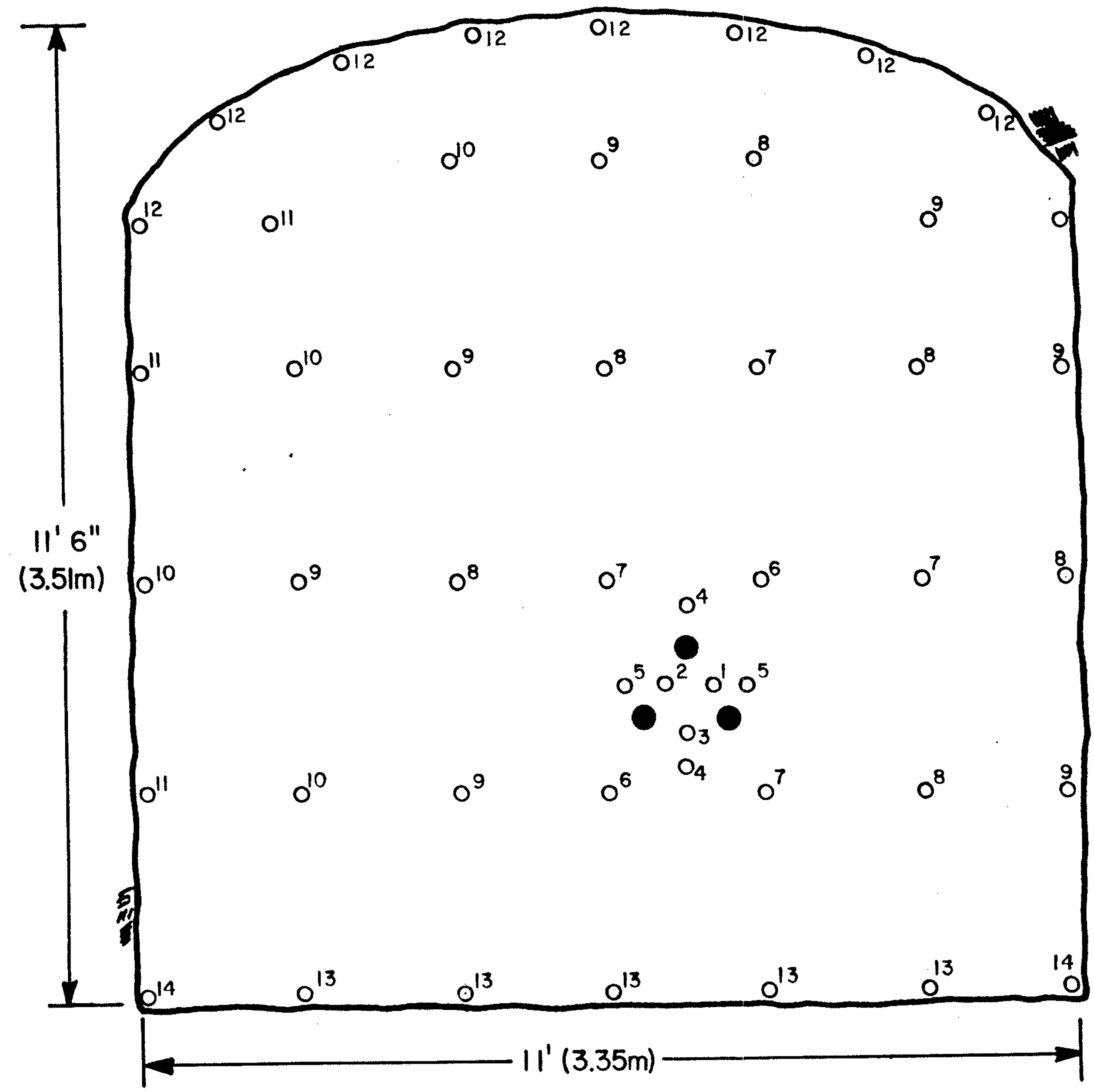
3.3.1 General

At different times during the program a jumbo and jacklegs were used for drilling rounds. The procedure, with both, followed conventional patterns (Figure 3) and standards although ground support techniques, and therefore cycles, were different for each. This was largely due to timing and crew experience gained with ground support as the jumbo was used at the beginning of the program, before support techniques had been tested and the jacklegs were used at the end of the program when a more systematic approach to ground support was taken.

In comparing production rates of the two (Table 2), jacklegs are seen to be more productive. This was due to improved ground support techniques and blasting procedures.

3.3.2 Comparison of Jumbo and Jackleg

The quickest way to compare the two is in tabular form. Table 3 gives statistical information on the two and Table 4 gives cycles.



STANDARD DRILL PATTERN

NOTES:
1) Adjust pattern to suit field conditions.
2) Alternate cut from side to side.
3) Arch holes to be blasted with Xactex.
   a) Blast baby arch first, muck out and then blast the final arch.

CASSIAR MINING CORPORATION
McDAME PROJECT
1415m. ADIT

RIZ MISLANG, Dec'86

SCALE: 1::240

FIGURE 3

TABLE 3
STATISTICS

	Jumbo	Jackleg
Boom	6.1 m (20 ft.)	-
Brand	Tamrock	Sican
Drill	Electric/hydraulic	Pneumatic
Power	Diesel	-
Bit	6.99 cm (2 3/4")	3.49 cm (1 3/8")
Drift	4.0 m x 3.0 m	3.5 m x 3.5 m
Drift Round	2.43 m	1.83 m

TABLE 4
CYCLES

Jumbo	Jackleg
Drill (35 holes)	Drill (35 holes)
- 2.44 m round	- 1.8 m round
Install spiles (non grouted)	Install resin spiles
Pin spiles to back	
Load all holes	Load baby arch
- Forcite (70%) (primer) Amex	- Forcite (70%) and Xactex (shearholes)
Ventilate	Ventilate
Shotcrete	Load full arch - Xactex
Muck out	Ventilate
Bolt, screen, strap	Muck out (Max. 2 buckets)
Shotcrete	Shotcrete
	Bolt, screen, strap
Elapsed time 24-36 hr.	Elapsed time 12 hours

Although the cycle for development with the jackleg has a few more steps, the time was less as the shotcrete machine was moved only once per cycle. The proper thickness of shotcrete was applied by redoing the previous round when shotcrete was applied.

3.4 Ventilation

3.4.1 Air Flow

Ventilation of the 1415 m level adit (Photo 7) was performed by a 75 h.p. Woods Axial vane fan located at the portal in conjunction with two booster Axial vane fans located along the adit. A total of 40,000 c.f.m. was directed to the development face via 42 inch diameter ventilation ducting. An air operated ventilation fan connected to 18 inch vent tubing supplied fresh air to the face of the raise.

When the 1563 m level ventilation raise broke through to the 1563 m level, the ventilation was naturally upcasting. The ventilation system was changed so that the main intake fan was located just on the west side of the raise on 1415 m level. Fresh air was incast on the 1415 m level and then forced to the face. Exhaust air from the face was upcasted up the raise and out the 1563 m level adit. To assist the ventilation, a 40 h.p Woods fan was installed at the ventilation/bulkhead door on 1563 m level to exhaust air to surface (Figure 4).

During winter the natural ventilation caused freezing of services and workings a considerable distance in from the 1415 m level portal. To counteract the problem, the ventilation system was reversed so that intake was in from the 1563 m level portal, down the raise, forced to the face by the 75 h.p. fan (half throttle) and by 40 h.p. booster fan. The outflow of air warmed by the machinery kept the 1415 m level portal from freezing.

PHOTOGRAPH 7

Portal Ventilation

Ventilation fan and flexible ducting leading into 1415 m level portal. Buildings with tarps are lunch/safety room and warehouse, plywood building is shop.

3.4.2 Environmental Control

Testing of airborne asbestos dust and dust from shotcreting were performed on regular intervals. Ventilation surveys were performed on a regular basis.

Gas tests at various locations were within threshold limits set by the Department of Mines.

Dust monitoring by the Department of Mines reported Silca dust levels of 0.010 mg/m^3 and 0.020 mg/m^3 in the area of an operating shotcrete machine, well within the Threshold Limit Value (T.L.V.).

3.5 **Ground Support**

3.5.1 General

All drifting during the 1986 program was within incompetent serpentinite criss-crossed with faults, fault zones, fractures and joints. After cutting with the Roadheader or blasting, in most areas, rock began spalling from the back, face and side walls except in those areas which were spiled with resin bolts. If ground support was not immediately applied after blasting or cutting, the ground could deteriorate by spalling such that several tonnes of muck would have accumulated on the floor within several hours. Even areas of seemingly competent ground gave problems in that if ground support was postponed or delayed, spalling and caving would commence.

The only successful system of mining required initializing ground support as soon as possible after the drift was opened, regardless of the apparent competency of the rock, and maintaining a rigorous and complete ground support program.

Numerous cycles of mining were attempted to reduce this problem, as discussed in other sections. The most effective cycles are those that allow ground support in the shortest period of time.

Rather than discuss various patterns of support attempted, the most effective system developed is described below in sections for each type of support.

3.5.2 Shotcreting

There are two methods of shotcreting, dry and wet. The dry method was used because equipment was already on site. Dry shotcrete, however, has the drawback of a high percentage of rebound, ranging from 20% to 50%, depending largely on the mixture and the application. Wet shotcrete has low rebound.

Properly applied shotcrete is a structurally adequate and durable material capable of excellent bond with rock, steel, wood and other materials. On quality tests, conducted by D.P. Morgan of Hardy Associates (1978) Limited on shotcrete products, the average compressive strength ranges from 27.7 PMa to 60.2 PMa after 28 days, comparable to poured concrete.

The two shotcrete products used during the program were Genstar's Microsil and Target's Superstick, both supplied with 4% Scamper 16 (accelerator). Additional accelerator was added by hand by the miners during application to bring the accelerator to approximately 8%, when faster setting time was required.

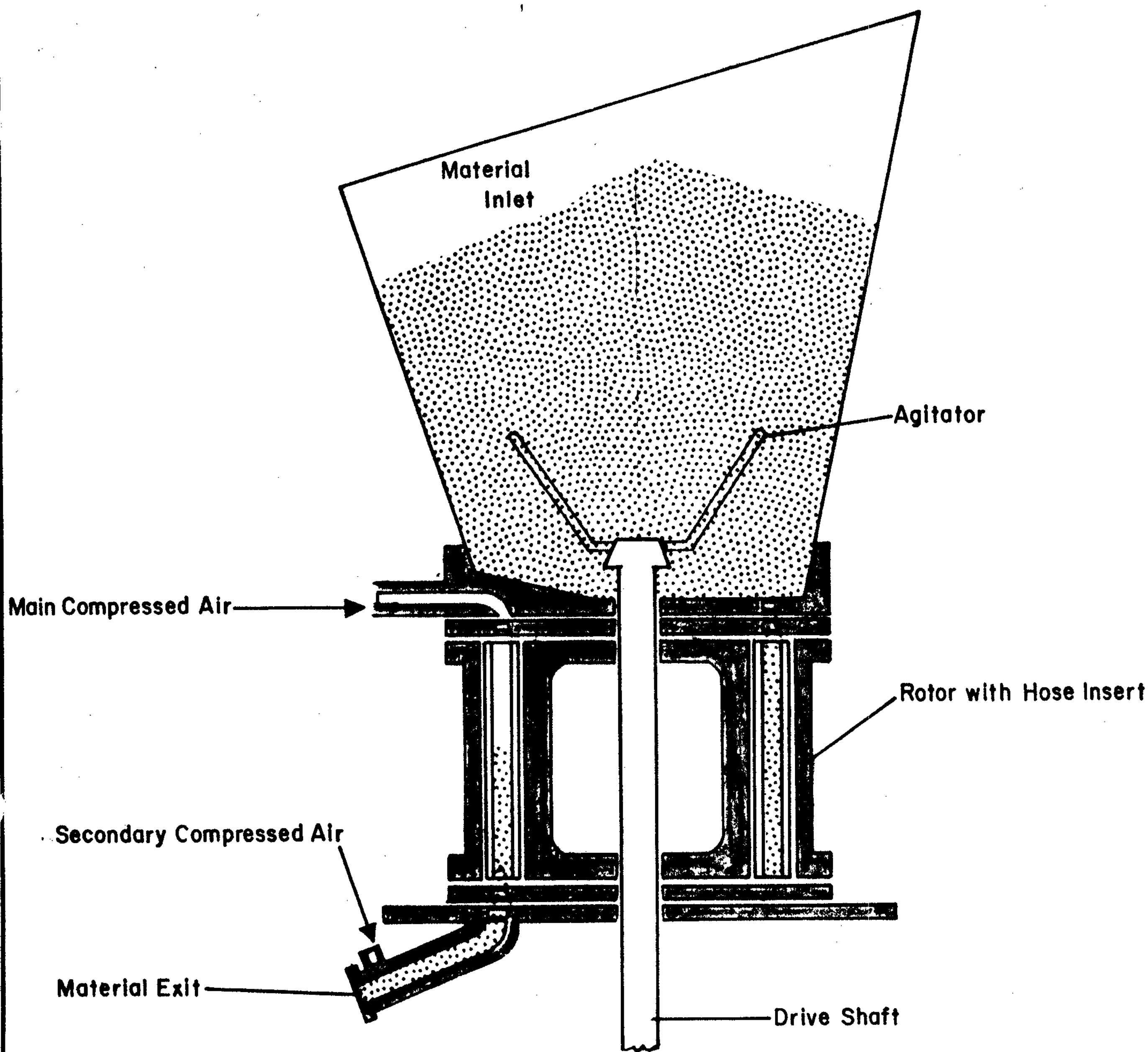
Shotcrete and accelerator were added to the hopper of the shotcrete machine (Figure 5), mixed by a spiral feed and forced by compressed air to the nozzle, where it was mixed with water and discharged at the rate of 5 cubic metres per hour (Photo 8). Special care was taken to maintain constant air pressure to prevent blockage and to regulate water flow for proper consistency and minimum rebound.

Steel fibre when added to shotcrete gives considerable extra strength and from a technical point is the preferred support system; however, steel fibre contaminates asbestos fibre and the two cannot be separated in the mill.

According to Dr. Laubscher, shotcrete should be applied to a thickness of 16 cm at the high points on the rock surface. Shotcrete application during the McDame project determined that if more than approximately 4 cm of shotcrete was applied to a rock surface, the shotcrete would peel from the back or sidewalls. If silica fume was added to the shotcrete, as much as 10 cm could be applied.

Shotcrete was found to be the most effective ground support technique as sealing of the rock from air controlled initial spalling and allowed application of additional ground support.

Optimum support could be obtained by applying a layer of welded wire mesh or heavy gauge screen between two applications of shotcrete. Other asbestos mines employ thick gauge diamond mesh



SHOTCRETE MACHINE X-SECTION

CASSIAR MINING CORPORATION
McDAME PROJECT

FIGURE 5

Riz Mislang, Dec.'86

PHOTOGRAPH 8

Shotcrete Machine

Ground support technique including spiling, straps and shotcreted surfaces may be distinguished in photograph.

instead of welded mesh as diamond mesh is more suitable for application purposes. Unfortunately, no diamond mesh of the required specifications was available on site, so a thick gauge welded mesh was used. Welded mesh is too inflexible for contouring along side walls after an application of shotcrete compared to a thick gauge diamond mesh.

3.5.3 Bolting/Screening

In addition to the application of shotcrete, rockbolts, straps and screens were also applied as part of the ground support system (Figure 6).

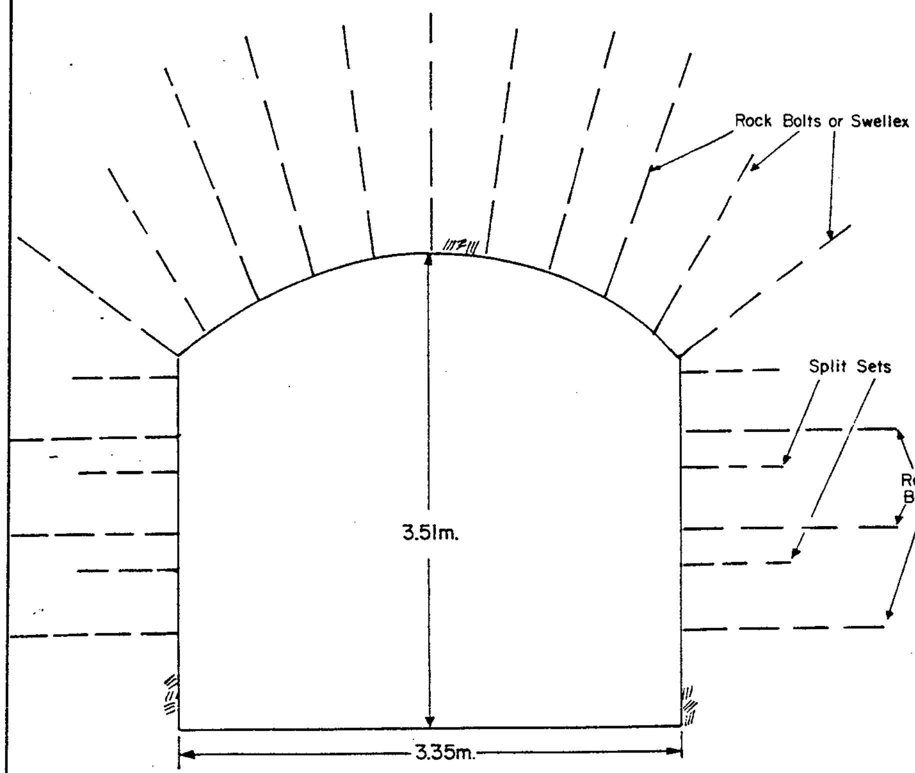
Rockbolt technical data is included in Appendix II.

During the program different types of rockbolts were tested. Ingersol-Rand splitsets are a frictional rockbolt capable of adjusting to changing rock stress, and are compatible with shotcrete as a resistive ground support system. Splitsets permitted supported ground to realign stress around the drift opening, thereby causing the sidewalls to converge.

Other rockbolt systems, such as Atlas Copco Swellex and Dywidag resin bolts, are resistive rockbolts that performed satisfactorily with shotcrete.

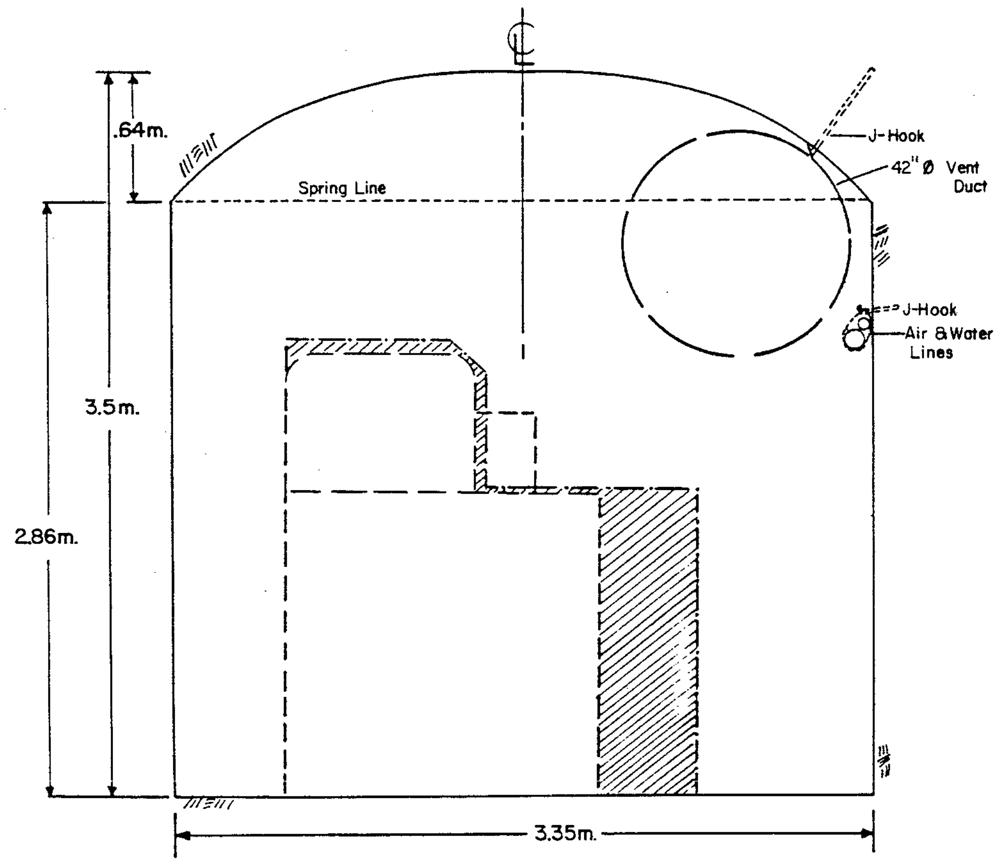
Pull tests were performed on the three different types of rockbolts and the results are:

Rockbolt	Failure Force (tonnes)
Splitset	2.72
Swellex	17.86
Dywidag	41.67



TYPICAL DRIFT GROUND SUPPORT

NOTES:- 1) Walls and backs screened with 4" squares by 8 gauge welded wire mesh.
2) Walls and backs shotcreted to a thickness of 2" to 4" depending on ground contions.
3) Install spillings of resin grouted 8' rebars on each round.



- - - - ST-2B Scoop Outline
-·-·-·- JS-220 Scoop Outline

FIGURE 6

Cassiar Mining Corporation McDAME Exploration Project	
TITLE TYPICAL DRIFT GROUND SUPPORT and X-SECTION	
DRAWN BY Riz Mislang	DATE: NOV. 21 1986
CHECKED BY	DATE:
SCALE NTS	DWG. No. 1500-001-6

Straps measuring 15 cm x 122 cm were used consistently to support the back at the face while miners were working underneath. Straps were applied at right angles to the direction of the drift. Dr. Laubscher reviewed the ground support techniques late in the program and stated that the straps were not performing a ground support function other than increasing the morale of the miners and, in fact, when covered with shotcrete, the straps became zones of weakness as the shotcrete was not in direct contact with the rock. This was verified later by spalling of the shotcrete covering the straps. Further, the straps should be applied parallel to the length of the drift when cracks form in the shotcrete.

Welded steel mesh screen with 10.2 x 10.2 cm openings was supplied in sheets covering an area of 13.01 m^2. It was applied over the first layer of shotcrete to give additional tensile strength to the shotcrete. Flexible diamond mesh screen would have allowed better contouring to surfaces allowing more complete coverage with the second layer of shotcrete thereby becoming an integral part of the ground support system. The welded mesh was difficult to form and in many instances, pockets were formed between the welded mesh and the first layer of shotcrete. These pockets prevent proper adhesion of the second layer of shotcrete to the first.

3.5.4 Discussion

The optimum ground support system is to quickly shotcrete fresh surfaces to a minimum thickness of 10 cm on the high points, install resistive-type rock bolts and diamond link mesh conforming to the surface, and covering with a second layer of shotcrete approximately 6 cm thick.

Rockbolts should be installed at 1 m centres. Rockbolts 2.44 m in length provided superior ground support compared to 1.83 m rockbolts. Dywidag resin rockbolts performed the best, rockbolting costs could be reduced by using fast setting cement rather than resin. Spiling was required for all advance and resin grouted spiles outperformed pinned spiles. All spiles should be installed ahead of the face round by approximately 1 1/2 rounds in length at an angle of 30°.

Ground support should be regimented and the full sequence completed regardless of visual assessment of the serpentinite at the time of advance. Support costs will be high but project costs will be lower as lost time due to caves, spalling, ratholing, etc. will be reduced. Safety will also be improved.

3.6 Raising

To provide adequate ventilation on the 1415 m level and an emergency escape route, a ventilation raise (Figure 4) measuring 2.44 m x 2.74 m was collared on 1415 m level and driven at an average angle of +42° to the 1563 m level adit.

Development of the raise was performed by driving a pilot raise and then slashing the raise to full size at approximately 5 metres from the advancing pilot raise face. Drill staging was not required except for the slashing process due to the raise angle. Even at 42° overall, blasted muck flowed in the raise, and slushing to clean the raise was not required. All ground support was performed as the slashed face advanced. Since the raise was driven in argillite, splitsets of 1.22 m in length and welded mesh screens were satisfactory for ground support. Mucking out of the raise was performed on a regular basis.

Raise ventilation was provided by a small booster fan located on the 1415 m level forcing air to the face through 18" ventilation ducting. Approximately 1 to 1.5 hours was required to clear fumes from the face after blasting.

All equipment and materials such as stoper, jacklegs, powder, bits and steels were brought up the raise in a steel raise box by a 50 h.p. slusher located at the bottom of the raise.

When 157 m had been completed it was necessary to expedite advance to improve ventilation on the 1415 m level. A 1.52 by 1.52 m pilot raise was driven the last 87 m to break through to the 1563 m level. An air slusher and equipment were taken and installed on the 1563 m level at the raise breakthrough. All equipment was then lowered down to the working face by the slusher and the remaining pilot raise was slashed out to the required dimensions.

TABLE 5

RAISE DEVELOPMENT

Purpose:	Ventilation, Emergency escape route
Size:	2.44 m x 2.74 m
Length:	241 m
Inclination:	+ 42°
Equipment:	Secan Jackleg Secan Stoper Joy 50 h.p. slusher (1.59 cm wire rope)
Blasting:	3.49 cm drill holes 70% Cigel Powder 0-13 Nonel delay caps

3.7 1563 m Level Rehabilitation

The Upper 1563 m level adit was rehabilitated as a contingency in order to facilitate diamond drilling on sections 6828N and 6767N and in the event of problems with advance on 1415 m elevation.

Work done by C.M.D. consisted of the following:

1. Clean up of drainage ditches from the portal to the drill stations.
2. Installation of a Trimetal 5 hp elecric fan at the portal.
3. Raise and regrade rails and repair or replace ties.
4. Repair collapsed timber sets to allow 1.8 m width in drift.
5. Replace bent steel arches.
6. Screen and install bolts in bad ground.
7. Slash 40 cubic metres of rock from walls and back of 6767N D.D.S. to accommodate the 5.2 m clearance required by the drill for angle holes.

The work took approximately 2 weeks and was completed within budget.

3.8 6706N D.D.S. Rehabilitation

On the morning of September 23 a rock failure occurred on the northwest wall of the 6706N Drill Station on the 1415 m level. Rock had appeared to be competent but failure may have occurred as a result of three or more intersecting joint planes allowing movement of a very large block of rock. Rehabilitation to safe standards was required as the drill station was important for exploration drilling.

The caved area measured 3.5 m high by 8.0 m long by 3 m breadth and was bounded by joints. Back and side walls of the caved area were reshotcreted and rebolted for ground support. To stabilize the drill station, steel sets located approximately 1.75 m apart through the caved area were installed on site from 8" x 40 lb/ft steel wide flange I-beams. Several timber sets (20 cm x 20 cm timbers) were constructed behind the steel sets to fill the cavity.

The resulting drill station is very secure and no further movement has been noted. Timber sets do not appear to be receiving any load as yet.

3.9 Diamond Drill Stations

Because of the size of the drill required to obtain the necessary depths of HQ core, drill stations had to be relatively large. One drill required 4.6 m and the second 5 m back from the collar of the drill hole in a straight line in the direction of the drill hole. As many holes were planned and it was unknown which drill would be on any setup, each drill station required a ring 5 m in diameter and approximately 2 m wide in the plane of the drilling. In addition, one drill could only drill within an arc of about 20° from the long axis of the machine which meant the station had to be at least 10 m long.

The resultant drill stations were therefore large, particularly since two of the three had to be turned off the drift to allow access for the miners. It was also known that the drillers would be located in each station for a length of time and therefore extra ground support was required. Due to all these factors construction was time consuming and costly.

The drill stations completed were:

6650N at coordinates 6650N, 7600E
6706N at coordinates 6706N, 7712E
6767N at coordinates 6767N, 7700E

3.10 Surveying

At the onset of the program a professional independent surveyor was brought in to tie in the portals of both 1415 m and 1563 m elevations with bench marks in or near the pit and to resurvey 1415 m adit. Survey control was then maintained by a surveyor and later a mine engineer hired for the project.

In the 1563 m level, survey stations were resurveyed and level plans were replotted at a scale of 1:250 (from the old 1" = 20'). Drift offsets were taken to locally correct the outline of the drift and survey control points were established.

As standard practice for surveying during advance on the 1415 m level, front and back lines for a first slash were marked at the start of a new heading and, if necessary, remarked for the second slash. If the drift was to curve, reference line plugs were set and when the straightaway was reached a pair of line plugs and spads were set on line. When the face was approximately 30-35 m beyond the first set of plugs, or when a change in bearing was necessary, a new set of line plugs was set approximately 5 m from the face. Off sets were taken after advance to determine the shape of the drift.

The 1563 ventilation raise was difficult to survey with a transit on a tripod. A special three-pronged metal pipe was attached to an adjustable bar fitted with a coarsely threaded adjusting screw to hold the transit. The bar could be fitted in a 1.5 m x 1.5 m to 2.4 m x 2.7 m raise (Figure 7).

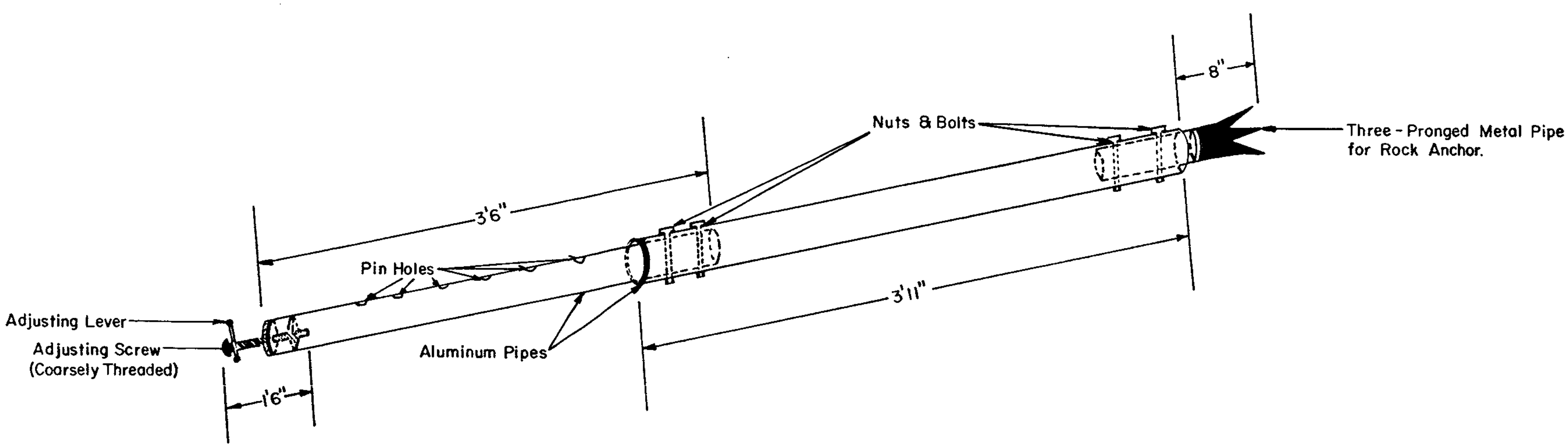
Line was again kept using line plugs and the raise successfully broke through into 1563 m level at the anticipated location.

3.11 Bulk Sample

During advance along 7700N, approximately 846 tonnes of muck was stockpiled near the portal to be used as a bulk sample for test mill purposes. Loaders transferred the material to mine haul trucks which transported it to a concentrator near the mill. Eighty tonnes of material was rejected as oversize at the grizzly, the remaining 766 tonnes were reduced to 588 tonnes by the removal of 149 tonnes of 1.1% fibre by the concentrator.

The 588 tonnes were processed producing 24.5 tonnes of fibre for a grade of 4.2% asbestos fibre.

A complete description of the procedure used for the bulk sample is given in Appendix III.



SURVEY RAISE BAR

FIGURE 7

Cassiar Mining Corporation
McDAME Exploration Project

TITLE: Survey Raise Bar	
DRAWN BY RIZ MISLANG	DATE: NOV 15 1986
CHECKED BY:	DATE:
SCALE: 1:1' 1:12	DWG. No. 1500-001-4

4. DRILLING

4.1 Logistics/Methods

Drill crews from Advanced Diamond Drilling arrived June 16 and began to set up for the first drill hole. Drilling began with a Super Drill (Photo 2) on June 20 and 2 holes, 86-01 and 86-02, were completed by July 2. As no drill station was available, the crews were demobilized between July 5 and 30 to allow drifting to advance.

Drilling with the Super Drill recommenced July 30 and was augmented with a Boyles Brother 37 converted for underground drilling on October 4. By February 2, 1987, a total of 4960.6 m in 27 holes had been completed. Table 6 shows daily production and Table 1 shows drill hole statistics.

Production was slower than anticipated for a number of reasons including:

a) slowness of drifting and availability of drill stations,

b) discontinuous services or interruptions due to the mining sequence, particularly blasting, and

c) extremely incompetent ground conditions causing caving and pinching of the drill holes.

Of the two drills the smaller, tractor-mounted Super Drill outperformed the larger Boyles 37. It was more cost effective for drilling and for moving. For a 61 day period between October 11 and December 10, both drills were operating and obtained the following results:

TABLE 6

DRILL	TOTAL METERAGE	AVERAGE M/DAY	TWO HIGH SHIFTS
SUPER DRILL	1628.5	26.7	64.0 m, 54.9 m
BOYLES 37	1056.0	17.3	48.8 m, 45.7 m

Although the Boyles 37 drill was involved in a move from the upper portal to the lower which caused an abnormal delay during the period, general production with the larger drill was not as good, further substantiated by the smaller production on high shifts.

Each drill was operated with three two-man crews drilling 8 hour shifts each. A foreman acted as shifter to supplement shifter coverage by mine contract personnel but when drifting was completed November 20, a shifter was hired for night coverage.

Services were supplied by normal drifting operations to November 20 when mine crews left. A scoop, jackleg, compressor, ventilation equipment, shop and mechanic were made available by the mine contractor at contract rates until the drilling finished.

4.2 Survey Control

Standard transit surveying procedures were used to establish location, elevation, azimuth and dip of the drill hole collars. In areas of multiple drill holes some holes were located with reference to existing survey plugs or previous drill holes.

Downhole deviations were measured by using a "Gyrolog" manufactured by Techdel International Inc. of Toronto. A pendulum rotor-type dipmeter and deflection indicator are housed in aluminum pipes with adapters on each end to provide a proper fit in HQ rods. The instrument was lowered down the hole in 10 foot increments using the wireline cable of the drill. An internal battery-operated timer activated the equipment recording dip and deflection on microfilm.

After the hole was surveyed the film was removed from the Gyrolog and developed. Dip readings were read directly using a microfilm reader, vertical and horizontal deflection values were obtained and the azimuth was calculated.

To save time a computer programme was devised using Lotus to calculate the easting, northing and elevation for each 5 foot (1.52 m) interval for which a fibre count was obtained. This information was used in accurate plotting of drill holes in section and plan.

A Gyrolog was selected for surveying holes because of the very magnetic nature of the country rock and the fact that survey equipment had to be pumped up steeply inclined holes, two problems the Gyrolog seemed most suitable to overcome. There were problem areas, however, that caused concern. The dipmeter, for example, is sensitive to vibration and is unable to record readings if the water pressure pump is operating (as it is for up holes). Three problems were encountered in the hole logging procedure, which sometimes led to considerable difficulty in reading and interpreting the data on microfilm. Firstly, the internal timer frequently became unreliable causing the camera to record data while the instrument was moving, instead of stationary in the hole. Secondly, malfunctioning in the film advance mechanism caused multiple exposures, making it difficult to discern particular exposures. Lastly, the method of development of the film often led to overexposure or loss of development of sections of the film.

Acid tests were done as a check in many holes and measurements agreed well with Gyrolog readings.

4.3 **Results**

Of 27 holes drilled, only 4 did not intersect significant fibre. Information on fibre content may be found in Appendix IV. Holes 86-01 and 02 were drilled to locate the footwall fault and did not penetrate the deposit and 86-13 and 16 from the upper level (1563 m) intersected a major fault prior to the deposit which has probably displaced the deposit. All other holes intersected fibre and the CCRG (Corrected Core Reading Grade) for specific intersections are shown in Appendix V.

5. GEOLOGY

5.1 Stratigraphy

The McDame Asbestos Deposit occupies the central part of a serpentinite body lying within rocks of the Sylvester Group (Figure 8) of Northern British Columbia. The Serpentinite has not been dated but the hanging-wall sediments have been dated as Lower Mississippian to Permian age (345-250 my) by fossil conodonts.

The Sylvester Group is an allochthonous stratigraphic sequence as it has been thrust from its place of origin to its present location by plate tectonic processes. In general, the sequence consists of numerous fault slices of ocean floor sediments, basalts and ultramafic intrusions that were imbricated amongst themselves by thrust faulting, then thrust and uplifted as a mass onto the continental platform in the Mezozoic Era. The units now dip easterly at around 40 degrees because of regional warping.

The McDame serpentinite is from 20 to 100 m above the basal thrust surface within a predominantly argillite sequence. In the hanging wall above the serpentinite are some basaltic layers that gradually increase to about 50% of the rock at more than 30 m above the contact. The serpentinite itself consists of an outer mantle of older darker green serpentinite with an overprinting green serpentinization of the core that contains most of the ore grade asbestos.

Between the serpentinite and hanging wall argillite is an alteration zone up to 5 m thick, through which serpentinite grades into argillite. The alteration is mainly tremolite-amphibolite. It is overprinted by talcose alteration, which also occurs in the serpentinite.

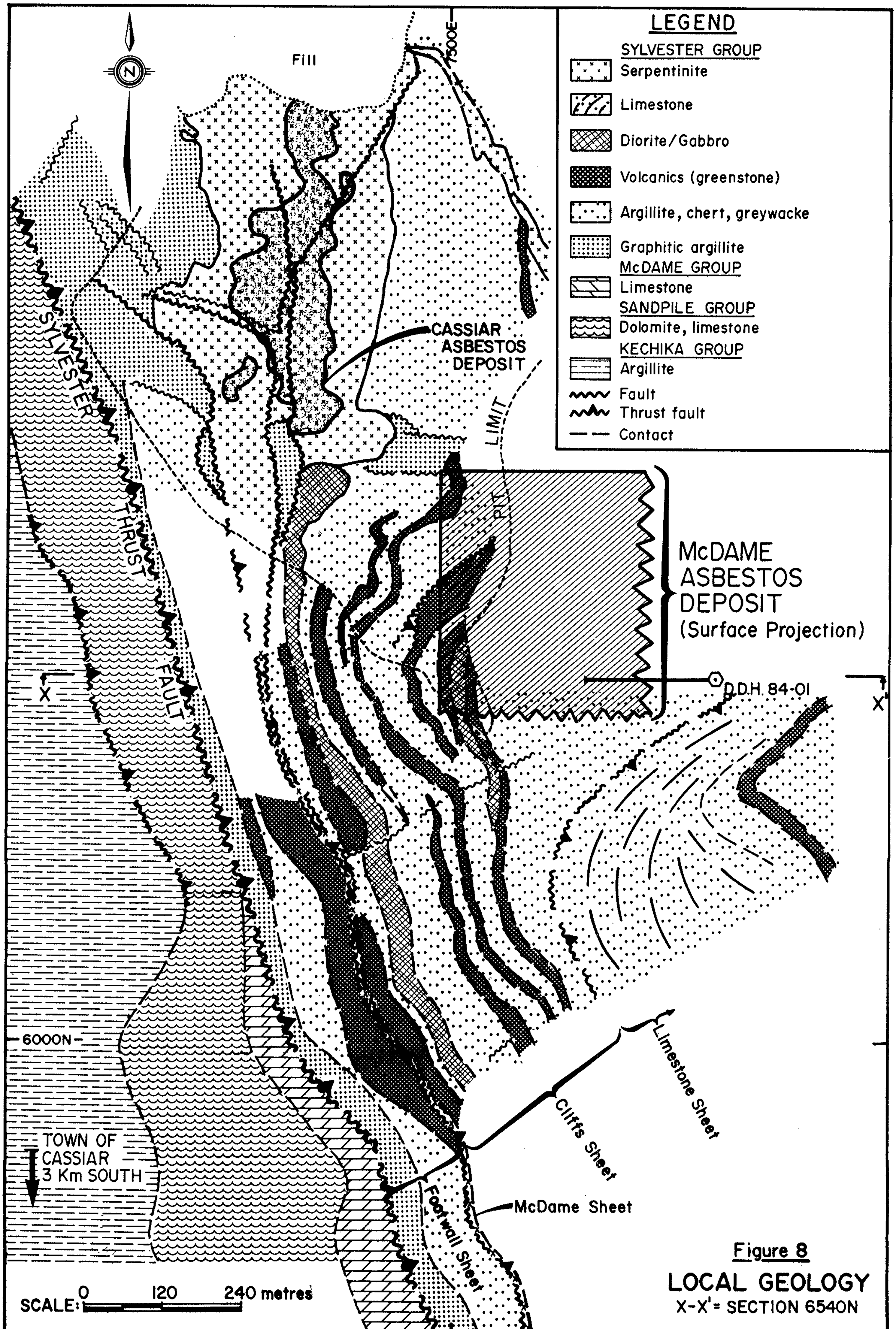


Figure 8

LOCAL GEOLOGY

X-X'= SECTION 6540N

The footwall serpentinite contact is predominantly fault bounded with local remnants of alteration.

Below the Sylvester Group are Paleozoic rocks of the North American platform. They are a sequence of formations of generally alternating argillite and carbonate, the oldest being Late Precambrian. The McDame workings intersect the three upper Groups which go from Middle Cambrian to Upper Devonian (550-350 my). The oldest, the Kechica Group, is a black argillite that is overlain by the Sandpile Group of dolostone and quartzite and the McDame Group of dolostone and limestone capped by black argillite. All three Groups have been strongly deformed by thrust faulting. Close to the McDame Deposit the McDame carbonate rocks have been faulted out completely and the Sandpile thinned severely. The black argillite capping the McDame Group formed a relatively soft lubricating layer over which the Sylvester Group was thrust.

A granitic batholith that intruded the Paleozoic rocks in the Cretaceous Period (100 - 70 my) lies about 1 km west of the McDame deposit. The heat of the intrusion caused contact metamorphism of the Kechica argillite to hornfels at the 1415 m Portal.

5.2 **Structure**

5.2.1 General

The geological history and development of the McDame deposit is dependent upon and related to three important structural events. The first of these occurred during Devonian and Mississippian times when the Sylvester Group basic volcanic and sedimentary rocks were being assembled on the ocean floor. This was followed by movement eastwards and then northwards of a segment of these rocks, now known as the Sylvester Allochthon, to its present site on the continent. The third and final event was the emplacement of the granitic Cassiar Batholith to the immediate west of the allochthon in Cretaceous times (Harms, 1984, 1985).

Regional and detailed structural studies in the Cassiar area and its surroundings have shown that intense tectonic and structural deformation accompanied these three events, and that from an economic standpoint it is the two later episodes that are important, for they are the events that are associated with the development of the asbestos fibre. This occurred in two distinct phases. The first phase is related to motion on faults similar to motion in the allochthon as a whole, the second phase is related to a local motion that was probably induced by the emplacement of the batholith. In addition, it has been found that lineations in the allochthon are northwest trending, indicating a northeasterly direction of motion.

On a local scale, underground mapping in the adits and logging of diamond drill core has disclosed the presence of numerous minor and several major faults and fault systems (Figure 9). These have occurred over an extensive period of time, concomitant with the main tectonic events, and display varying age relationships, both with respect to other faults and with respect to the fibre. Four main sets of faults have been recognized, a set that strikes north-south and dips to the east, a set that strikes northwesterly

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Harms, T. 1985. Pre-emplacement thrust faulting in the Sylvester Allochthon, northeast Cry Lake map area, British Columbia. Current Research, Part A, Geological Survey of Canada Paper 85-1A, p.301-304.

Harms, T. 1984. Structural style of the Sylvester Allochthon, northeastern Cry Lake map area, British Columbia. Current Research, Part A, Geological Survey of Canada Paper 84-1A, p. 109-112.

and strikes steeply to the northeast, a set that strikes east-west and dips to the south, and a set that strikes northeasterly and dips very steeply to the northwest.

Several of these faults are post-fibre in age and are of decided economic importance, for they either dislocate and form boundaries to the orebody, or else, on a small scale, dislocate and form the boundaries between the individual blocks of ore and waste within the orebody itself. The most important of these faults are a northwesterly striking fault that forms a hanging-wall contact, a north-south striking fault that forms a footwall contact and a northeasterly striking fault that is thought to throw the orebody downwards in the southeast area of the deposit.

These features are illustrated on structure-grade maps that have been compiled. An example is Figure 20, the objectives of the structure grade maps is to identify:

1. the role of structure in controlling the broad limits of the deposit, as well as particular internal features within it, and

2. those structures that might affect a block caving operation, both in regard to its operation as well as its initial design.

5.2.2 Sections

Plans of the 1563, 1500, 1450, 1415, 1350 and 1300 m elevations were drawn to 1:1,000 scale. East-west sections at a scale of

1:1,000 and 1:2,000 were drawn for 6650, 6706, 6767, 6828 and 6858 N and north-south sections to the same scales for 7500, 7550, 7600, 7650, 7700 and 7750 E. Plan 1415 (Figure 10) and Sections 6650N through 6828N, 7600E and 7700E (Figures 11-16) at a scale of 1:1000; and sections 6650N, 6767N, 7600E, and 7700E (Figures 17-20) at a scale of 1:2000 are in back pockets.

Structural interpretation was based on geological mapping of the 1415 m and 1563 m level adits and the logs of diamond drill holes 79-83 through 81-171, 84-01, 85-01 and 86-01 through 86-27 (Figure 9, Appendix IV).

Fault intersections recorded in the logs were plotted on the east-west sections and, where appropriate, joined from hole to hole. The mapping in the adits gave basic information on several major structures. The data from these sections was transferred directly to the plans and the north-south sections.

Using cut-offs of 5% and 3%, average grades over significant lengths of CCRG (Corrected Core Reading Grade) percentages were calculated and plotted on plans and sections (Appendix V).

The study has shown the following salient features:

1. The orebody contains grades in excess of 5% over approximate dimensions in the order of 150 m vertically, 300 m east-west and 300 m north-south. Because of its plunge to the south-east, the orebody is, in fact, much larger than these dimensions suggest.

2. Some of the faults are post-mineral and form important contacts that delimit the ore zone. These are described below.

3. The southeast striking South Fault is an important dislocator that separates the Cassiar and McDame deposits. It forms a partial contact in the northeast wall of the deposit.

4. Within the deposit, three major sets of faults are present, a north-south striking, easterly dipping set (Faults A, D, E) and an east-west striking, southerly dipping Fault B. A southwesterly striking feature, F, displays weak structural expression but causes marked dislocation of the ore in the southeast of the deposit.

5. Fault A is post-mineral and in the upper part of the deposit separates the upper western tongue of mineralization from the main body. In some sections it forms a recognizable contact.

6. Below the 1,400 m level, Fault E splits to form two separate faults, E1 (upper) and E2 (lower). E1 acts as an important footwall contact.

7. Fault B forms a hanging wall contact in the northern part of the deposit. It is cut by Fault A, and in turn cuts fault D.

8. Fault D occurs south (hanging wall) of Fault B and flattens with depth.

9. The feature F exhibits weak structural expression, but dislocates ore in the southeast of the deposit. It strikes southwest, dips northwest and widens to the northeast. It appears to cut Fault B.

5.2.3. Rock Mass Rating

Rock Mass Rating (RMR) is a procedure for measuring physical characteristics of rock that allows comparison of any area measured with any other. Zones of weakness, or of competency can be recognized and correlated. Information so collected was used for generation of structural plans and sections. The system used was developed by Dr. Laubscher specifically for McDame to cater to rock properties and time available for measurements.

Three observations were recorded for the same 1.52 m (5 foot) intervals used to calculate fibre grade: the number of natural fractures or joints within the interval; an assessment of joint conditions encompassing parameters such as shape, planar expression, roughness and composition of filling; and intact rock strength.

Joints and fractures are counted for the interval and are corrected by dividing by the percentage recovery within the interval. Using a graph prepared by Dr. Laubscher, a value was obtained and forty percent of it was then recorded.

Using Table 7 prepared by Dr. D. Laubscher, the conditions of the joints were assessed. A value was selected, usually under dry conditions, and reduced by a percentage for roughness, alteration and filling and forty percent of the final value was then recorded.

A number of samples of serpentinite were sent to Hardy and Associates for intact rock strength tests. The results are in Appendix IV. Duplicate samples were maintained at the property for comparison with core. Millipascal values were obtained and using Table 7 values between 0 and 20 were obtained.

A. MEANING OF THE RATINGS

Class	1 A	1 B	2 A	2 B	3 A	3 B	4 A	4 B	5 A	5 B
Rating *	100 - 81		80 - 61		60 - 41		40 - 21		20 - 0	
Description	Very good		Good		Fair		Poor		Very poor	

Notes : * Sum of 1, 2, 3 of B.
** Measured fracture frequency divided by core recovery x 100

B. BASIS OF THE CLASSIFICATION

1	IRS (MPa)	>185	184-165	164-145	144-125	124-105	104- 85	84 - 65	64 - 45	44 - 25	24 - 5
	Rating (= 0,1 x MPa)	20	18	16	14	12	10	8	6	4	2

2	FF/m **	0,2	0,3	0,4	0,5	0,7	1	1,5	2	3	5	7	10	15	20	30	40	80
	Rating	40	40	38	36	33	31	28	26	23	20	17	15	12	10	7	5	2

3	Joint Condition including Ground Water	Refer C. below
	Rating ($40 x A x B x C x D / 10^8$)	40

C. ASSESSMENT OF JOINT CONDITIONS

ACCUMULATIVE % ADJUSTMENT OF POSSIBLE RATING OF 40

Parameter	Description		Dry Cond	Wet Conditions: Moist	Mod Pressure 25 - 125 l/m	Sev Pressure >125 l/m
A Joint Expression (large scale irregularities)	Wavy	Multi-directional	100	100	95	90
		Uni-directional	90	90	90 85	80 75
	Curved		89 80	85 75	80 70	70 60
	Straight		79 70	74 65	60	55
B Joint Expression (small scale irregularities or roughness)	Very rough		100	100	95	90
	Striated or rough		99 85	99 85	80	70
	Smooth		84 60	80 55	60	50
	Polished		59 40	50 35	30	20
C Joint Wall Alteration Zone	Stronger than wall rock		100	100	100	100
	No alteration		100	100	100	100
	Weaker than wall rock		75	70	65	60

C. ASSESSMENT OF JOINT CONDITIONS (Cont'd)

ACCUMULATIVE % ADJUSTMENT OF POSSIBLE RATING OF 40

Parameter	Description		Dry Cond	Wet Conditions: Moist	Mod Pressure 25 - 125 l/m	Sev Pressure >125 l/m
D Joint Filling	No fill - Surface Staining only		100	100	100	100
	Non Softening & sheared material (clay or talc free	Coarse Sheared	95	90	70	50
		Medium sheared	90	85	65	45
		Fine sheared	85	80	60	40
	Soft Sheared Material (eg Talc)	Coarse Sheared	60	55	40	20
		Medium Sheared	55	50	35	15
		Fine Sheared	50	45	30	10
	Gouge thickness <amplitude of irreg		40	30	10	
	Gouge thickness >amplitude of irreg		20	10	Flowing material 5	

MODIFIED GEOMECHANICS ROCK MASS CLASSIFICATION

D.H. LAUBSCHER
1986

Table 7

The three values recorded, one for frequency of joints, one for assessment of joints and one for intact rock strength, were added together to generate a single value for each interval measured. This value was recorded and plotted as Rock Mass Rating, or RMR. Histograms for each hole have been generated (Appendix IV) to give an immediate comparison of zones of weakness.

5.3 Fibre Grade and Distribution

5.3.1 Procedure

Drill holes were marked into 1.52 m (5 foot) intervals and core recovery was measured. Two chalk lines, one along each side of the core, were marked down the length of the core. Each line was followed and the number of fibre veins 1/16 inch or longer were recorded under the actual length. Care was taken to ensure that multiple veins were divided into component lengths and that the true length of the fibre was measured. The latter was a particular problem when long fibre veins had been cut by the drill bit. In more than one case the fibre length was longer than the diameter of an NQ bit (4.76 cm or 1.875 inches).

Only fibre veins intersecting the line were counted and the length at or near the line was used. On completion of the measurements the total sixteenths of all fibre was added and recorded.

When work was finished on the core it was photographed, labelled and moved to core storage racks.

Results from the fibre readings were entered on a spreadsheet utilizing the Lotus program on an IDM computer (IBM compatible).

Footage, recovery, and number of each length of fibre vein were entered by each person measuring. The computer program was designed to convert the footage to metres and calculate the average grade for each interval. This information was printed for each hole and is part of Appendix IV.

The grade is reported as CCRG (Corrected Core Reading Grade) which was calculated by taking the percentage of the interval that is fibre, dividing by recovery to correct for 100% core and multiplying by the cosecant of 45° to allow for the random orientation of the veins as has been done historically at Cassiar. More simply put:

$$\% \text{ CCRG} = \frac{(\text{16ths of fibre})(\text{cosec } 45°)}{(\text{length in 16ths})(\text{recovery})} \times 100$$

The CCRG values were also plotted as a histogram for each hole as shown in Appendix IV.

Utilizing the same computer program, total 16ths for each fibre length were calculated as a percentage of total fibre for each hole. A bar chart showing percentage of each length and a pie diagram showing percentage of 1, 2, 3, 4, 5, and 6, 16ths and plus one half inch were also prepared for each hole and are included in Appendix IV.

5.3.2 Test Mill

Samples from holes U8605, 21, and 25 were sent to the test mill for fibre recovery. Samples were bagged in 15 m intervals for hole 5 and 5 m intervals for holes 21 and 25. At the test mill samples are crushed and processed to recover fibre.

For hole U8605 test mill results compared favourably with core counts (Figure 21). For holes U8621 and 25, test mill results are considerably higher (Figures 22, 23). Possible explanations for the higher readings are:

a) test mill results include dust not included in core counts,

b) fibre veins may not be randomly oriented affecting the constant used in calculating CCRG; i.e., the cosecant of 45° is currently used assuming random distribution, but the value will increase if fibre angle is more shallow with respect to core, and

c) downgrading of fibre length by core measurers.

Regardless of reason, recovered fibre content is higher than estimated.

5.3.3 Results

Appendix IV contains CCRG values, CCRG histogram, RMR histogram, Fibre Length distribution by sixteenth, and fibre length showing plus half sixteenth for each hole. Fibre counts are also shown on sections 6650N, 6700N, 6767N, 6828N, 7700E, 7600E.

Drilling has resulted in positive results in that:

a) the South Fault which occurs in the Cassiar Mine open pit is the northern limit of economic fibre,

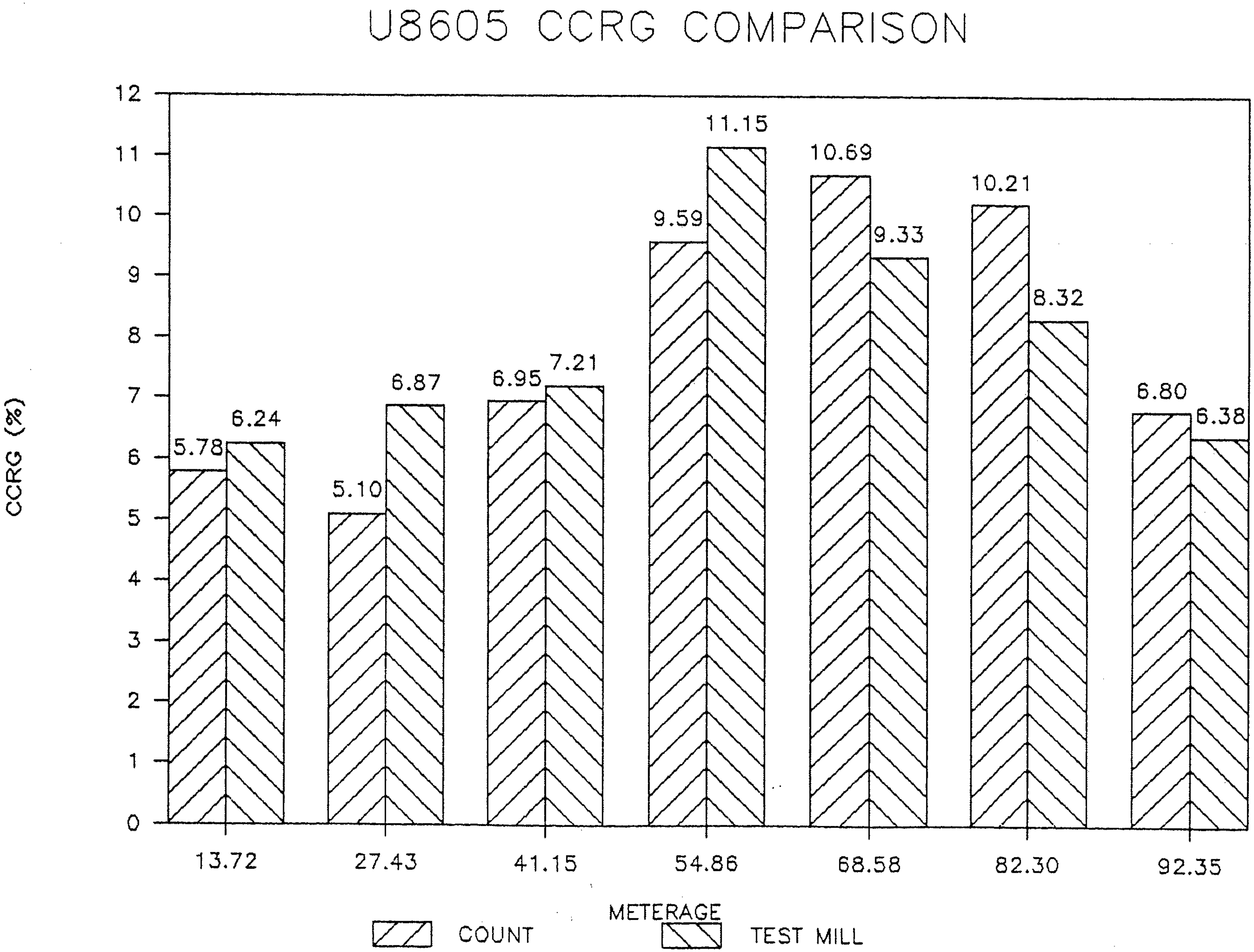
U8605 CCRG COMPARISON
CCRG (%)
0
1
2
3
4
5
6
7
8
9
10
11
12
5.78
6.24
5.10
6.87
6.95
7.21
9.59
11.15
10.69
9.33
10.21
8.32
6.80
6.38
13.72
27.43
41.15
54.86
68.58
82.30
92.35
METERAGE
COUNT
TEST MILL

FIGURE 21

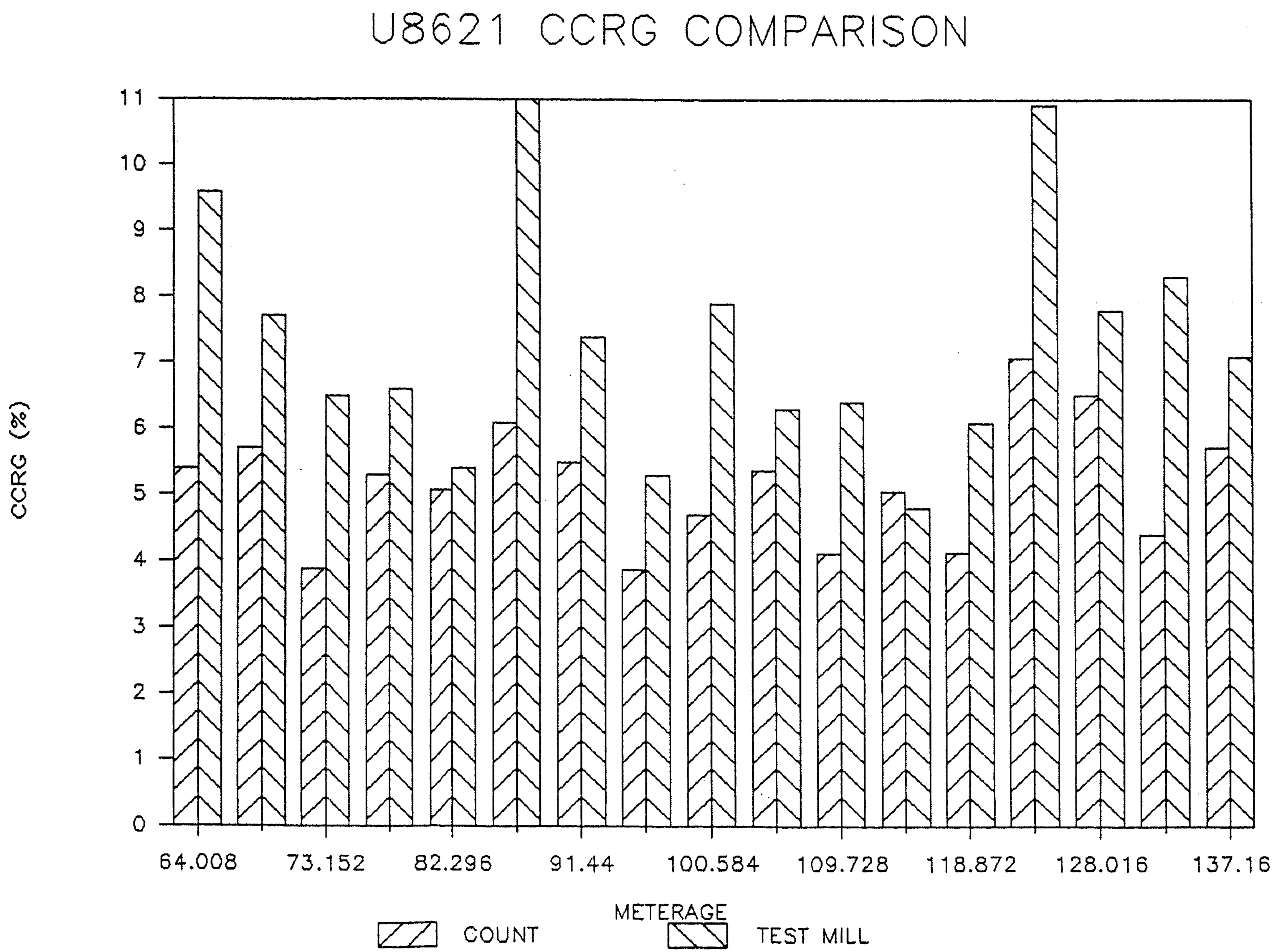
U8621 CCRG COMPARISON
CCRG (%)
0
1
2
3
4
5
6
7
8
9
10
11
64.008
73.152
82.296
91.44
100.584
109.728
118.872
128.016
137.16
METERAGE
COUNT
TEST MILL

FIGURE 22

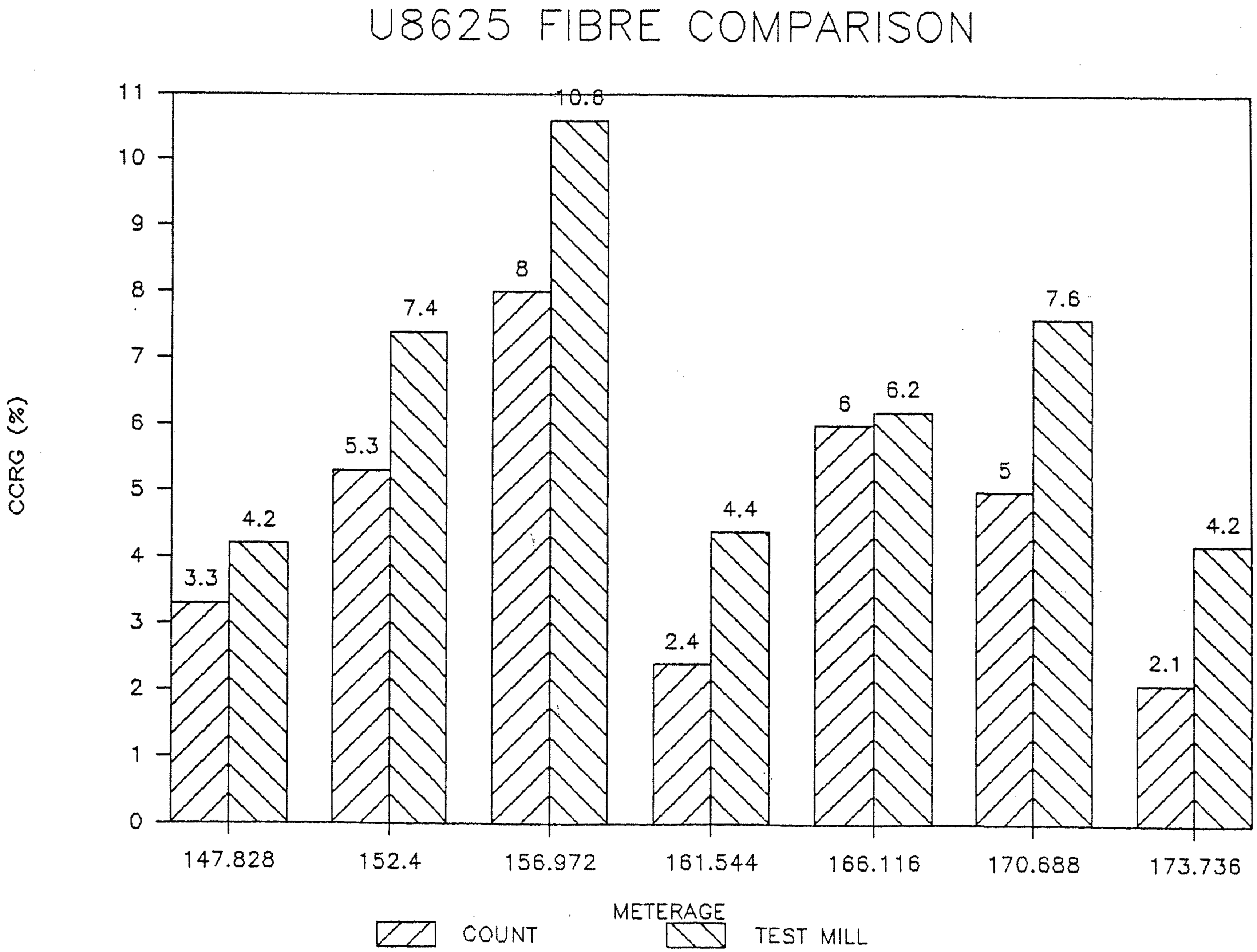
U8625 FIBRE COMPARISON
CCRG (%)
11
10
9
8
7
6
5
4
3
2
1
0
3.3
4.2
5.3
7.4
8
10.6
2.4
4.4
6
6.2
5
7.6
2.1
4.2
147.828
152.4
156.972
161.544
166.116
170.688
173.736
METERAGE
COUNT
TEST MILL

FIGURE 23

b) fibre grades greater than 4% CCRG continue to 7850E before dropping in value, thus defining the eastern limit of the deposit,

c) fibre is long throughout the bulk of the deposit,

d) the western boundary to the deposit trends north-south along 7500E from 6828N to just south of 6650N before swinging to the east,

e) the footwall of the deposit (Figure 24) dips to the east (approximately 47°) from 7500E to 7625E (from 1450m to 1300 m elevation) and then flattens to a 32° dip to 7700E at 1250 m elevation,

f) fibre values within the deposit are more variable than indicated by previous drilling and show more fluctuation from low to high grade in adjacent 1.5 m sections, and

g) the attitude and extent of the deposit to the south is still unconfirmed.

6. PERSONNEL

On a project of this magnitude, many people are involved. Those people directly involved with onsite work or in report preparation are listed below. All contributed to the completion of the project. Many other individuals offered advice and assistance and their help is appreciated though for brevity, their names are not listed.

PERSON	RESPONSIBILITY
Mr. A.A. Burgoyne, P.Eng.	Project Supervisor
Mr. R.S. Hewton, P.Eng.	Field Supervisor, Assistant to Mr. Burgoyne
Mr. K. Minty, P.Eng.	Drifting, Raising
Dr. D. Laubscher	Consultant
Mr. D. Petersen, P.Eng.	Diamond Drilling
Mr. R. Meyers, P.Eng.	Diamond Drilling
Mr. W. Epp	Diamond Drilling
Mr. I. Lyn	Geology, structure
Dr. D. O'Hanley	Geology, structure
Mr. P. McRae	1563 m Rehabilitation
Mr. W. Carter	1563 m Rehabilitation
Mr. H. Holm	CCRG, RMR, Drafting
Mr. S. Avaiki	CCRG, RMR, Labour
Mr. S. Casselman	CCRG, RMR, Labour, Accounting
Mr. C. Turek	Surveying
Mr. R. Mislang	Surveying, Drafting
Mr. G. Valgardson	Site Accounting
Mrs. I. Zubec	Site Accounting
Mr. I. McLean	Ombudsman, Site Accounting
Mrs. B. Sidgwick	Typing
Mrs. S. Martin	Word Processing
Mrs. B. Minnaar	Word Processing

and the personnel of:

Cassiar Mine
Canadian Mine Development
Advanced Drilling
Matthews and Associates
Steffen, Robertson and Kirsten

7. CONCLUSIONS

Conclusions for specific aspects of the exploration program are given within the various subsections throughout the report. Signigicant conclusions on the overall project are:

a) the northern, western and eastern limit of the McDame deposit have been defined by diamond drilling,

b) the hanging wall has been located for the northern half of the deposit but has not been adequately located to the south,

c) the hanging wall contact is generally 10-30 m higher in elevation than previously plotted,

d) McDame fibre is of good length averaging 19.6% plus one half inch within the limits of the deposit,

e) further study is required to determine the efficacy of using a continuous miner,

f) ground support is of prime concern and must be implemented immediately after blasting or cutting,

g) a pattern of ground support cycles has been developed, and

h) preliminary results from the test mill are, on the average, 12% higher than calculated grades implying that grades of fibre listed in the appendices may be low.

8. COST STATEMENT

During the course of the program, an accounting system was set up on site to monitor costs and changes on an ongoing basis. After implementation of the accounting system, all purchases were made by purchase order. Invoices were sent to the project sit for authorization by project supervisors and records were maintained on site. Authorized invoices were then sent to Vancouver by Transmittal for payment.

Costs of services were accrued on a continual basis to allow estimation of total expenditures incurred at anytime.

Invoices paid were tracked by computer in Vancouver. A generalized list of costs for the project are:

COST STATEMENT

VENTILATION		
labour	$ 10,238.43	
supplies	25,291.95	$ 35,530.38
EXPLOSIVES		93,010.84
PIPE		22,983.59
GROUND SUPPORT		
labour	285,436.52	
supplies	445,271.74	730,708.26
ELECTRICAL		
labour	11,096.12	
supplies	39,968.57	51,064.69
CONTINUOUS MINER		
engineer	28,295.75	
machine	221,821.90	250,117.65
LEVEL MAINTENANCE		
labour	24,870.00	
supplies	32,762.50	57,632.50
REHABILITATION		
labour	2,245.84	
supplies	2,038.06	4,283.90
DELAYS		30,048.64
DIAMOND DRILL STATIONS		
labour	59,191.35	
supplies	18,397.26	77,588.61
DIAMOND DRILL		
labour	272,149.08	
supplies	102,525.27	
coring	248,624.05	623,298.40
STAFF SALARIES		241,848.81
SURVEY		51,384.41
VEHICLE		48,143.99
EQUIPMENT AND SUPPLIES		273,393.01
ROOM AND BOARD		74,929.12
TRAVEL		23,047.97
FREIGHT		191,515.05
TELEPHONE		8,155.17
OFFICE SUPPLIES		1,948.69
DRAFTING		6,274.35
TEST MILL		4,192.10
ONTARIO RESEARCH		1,713.98
CONSULTING		51,550.30
FUEL		36,111.86
POWER		205,099.12
LOCAL SUPPORT		
labour	4,552.40	
supplies	28,218.78	32,771.18
SECURITY		1,149.50
6706 REHABILITATION		102,968.12
LATERAL DEVELOPMENT		
labour	782,855.13	
supplies	310,517.95	1,093,373.08
RAISING		
labour	122,408.66	
supplies	37,155.72	159,564.38
MANAGEMENT AND OFFICE COSTS		150,000.00
		$ 4,735,401.65

9. ACKNOWLEDGEMENTS

On a project of this size many people are responsible for a successful completion and compilation of the results. All those people listed in Section 6. Personnel are acknowledged for their contributions. In addition, the authors would like to specifically thank I lyn, H. Holm, D. Petersen, R. Mislang, and D. O'Hanley for their contributions in the completion of this report.

APPENDIX I

GRAVIMETRIC AIRBORNE FIBRE ANALYSIS RESULTS

AIRBORNE ASBESTOS FIBRES

Slide	Location	Date	Time	Volume	Fibres / Field	f/cc	Ctr.	Comments
1	Face	17-07-86	PM	124200	7/100	0.06		
2	Raise	"	PM	124200	9/100	0.08		
3	Portal	"	PM	124200	3/100	0.03		
4	Substation	"	PM	124200	46/100	0.38		
5	Portal	"	AM	124200	23/100	0.20		
6	Face	21-07-86	PM	82800	21/100	0.27		
7	PORTAL	"	PM	"	4/100	0.05		
8	Raise	"	PM	"	44/100	0.55		
9	Substation	"	PM	"	17/100	0.22		
10	Face	22-07-86	AM	82800	11/100	0.15		
11	Raise	"	AM	"	34/100	0.44		
12	Portal 2	"	AM	"	6/100	0.08		
13	Substation	"	AM	"	17/100	0.16		

NOTE: MAXIMUM ALLOWABLE CONCENTRATION = 2 FIBRES / CC.

APPENDIX II

ROCKBOLT TECHNICAL DATA

3.4 Friction Anchored Rockbolts

Friction anchored rockbolts represent the most recent development in rock reinforcement techniques. Two friction anchored rockbolt types are available, the Split Set and the Swellex. For both types of rockbolt system, the frictional resistance to sliding of the rock on the steel (for the Swellex combined with mechanical interlock) is generated by a radial force against the borehole wall over the length of the bolt. Friction anchored rockbolts resemble mechanically anchored bolts in the sense that their installation and operation is unimpaired by wet rock conditions. For use in permanent installations, corrosion may, however, create a problem.

Although the two systems are described under a common heading, they display some major differences. These are related to the anchoring mechanism and their support action, as well as their installation procedure. Strictly speaking, only the Split Set is a true friction anchored rockbolt and as such it is sometimes called the "Split Set Friction Rock Stabilizer".

The anchoring mechanism of the Split Set rockbolt arises from frictional forces to a load which approaches the ultimate load bearing capacity of the bolt, when the bolt will slide. The bolt can then accommodate large displacements without failing.

The anchoring mechanism of the Swellex rockbolt depends on frictional forces combined with mechanical interlocking. The anchoring of the Swellex is provided by frictional forces to a load which approaches the ultimate load bearing capacity of the bolt. Mechanical interlock between the bolt and the rock then prevents the bolt from sliding. This property of the Swellex rockbolt implies that the full strength of the bolt is utilized. A higher pull-out resistance is then obtained.

The action of the Split Set rockbolt, to accommodate gross displacements by sliding is sometimes preferred, however. When required, this action can be obtained by a reduction in the inflation pressure of a standard Swellex. It has been shown that the Swellex can be adapted to a variety of ground conditions by changing the inflation pressure.

Both friction anchored bolt types are commonly used in the mining industry. However, their use in civil engineering applications is limited, but Swellex is increasingly used in tunnelling work.

me[illegible] rock reinforce-
available, the Split Set
nal resistance to sliding
ıechanical interlock) is
ength of the bolt. Fric-
s in the sense that their
ɔns. For use in perma-
n.

ling, they display some
ıism and their support
ıg, only the Split Set is
s called the "Split Set

om frictional forces to
of the bolt, when the
ments without failing.

ı frictional forces com-
llex is provided by fric-
earing capacity of the
prevents the bolt from
full strength of the bolt

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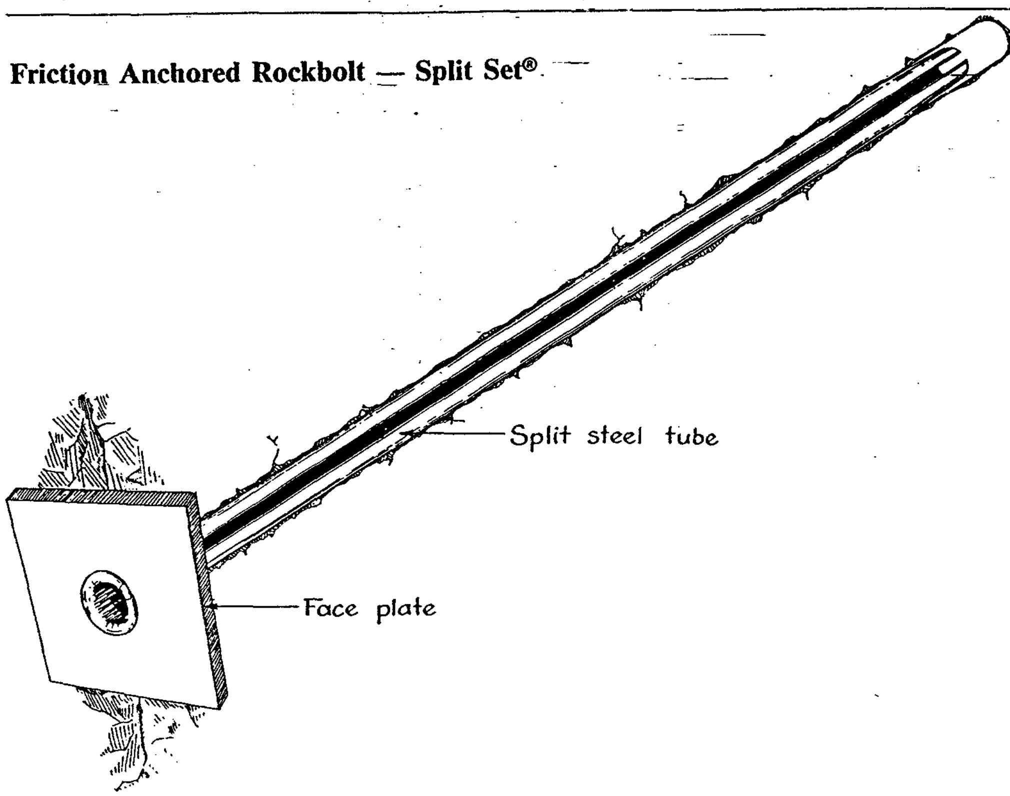
ı can be obtained by a
as been shown that the
changing the inflation

the mining industry.
but Swellex is increas-

Friction Anchored Rockbolt — Split Set®



Typical technical data

Tube diameter:	39 mm	39 mm	11/2 in
Yield load, steel tube:	90 kN	9 tons	10 tons(US)
Ultimate load, steel tube:	110 kN	11 tons	12 tons(US)
Ultimate axial strain, steel tube:	16 %	16 %	16 %
Weight of bolt without face plate:	1.8 kg/m	1.8 kg/m	1.2 lb/ft
Bolt lengths:	0.9—3 m	0.9—3 m	3—10 ft
Recommended borehole diam.:	35—38 mm	35—38 mm (critical)	1 3/8 in

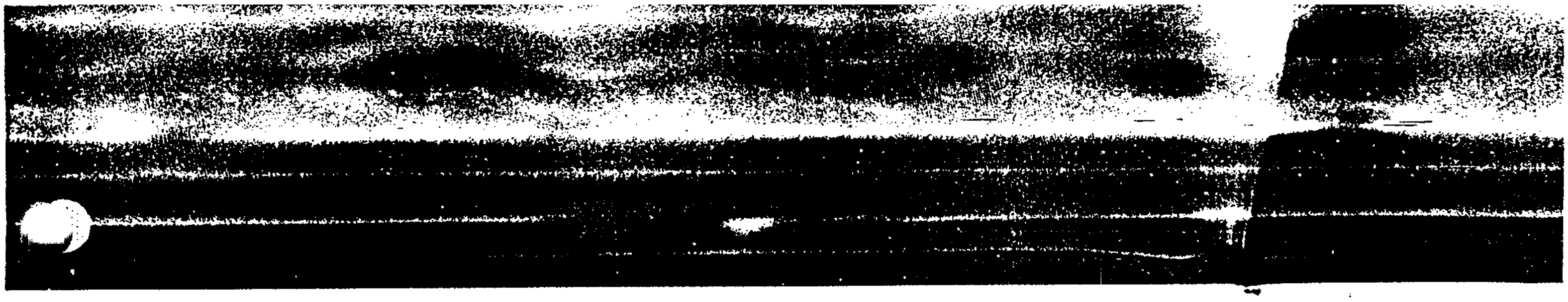
Split Set® is a registered trademark of Ingersoll-Rand Company, USA.

Advantages

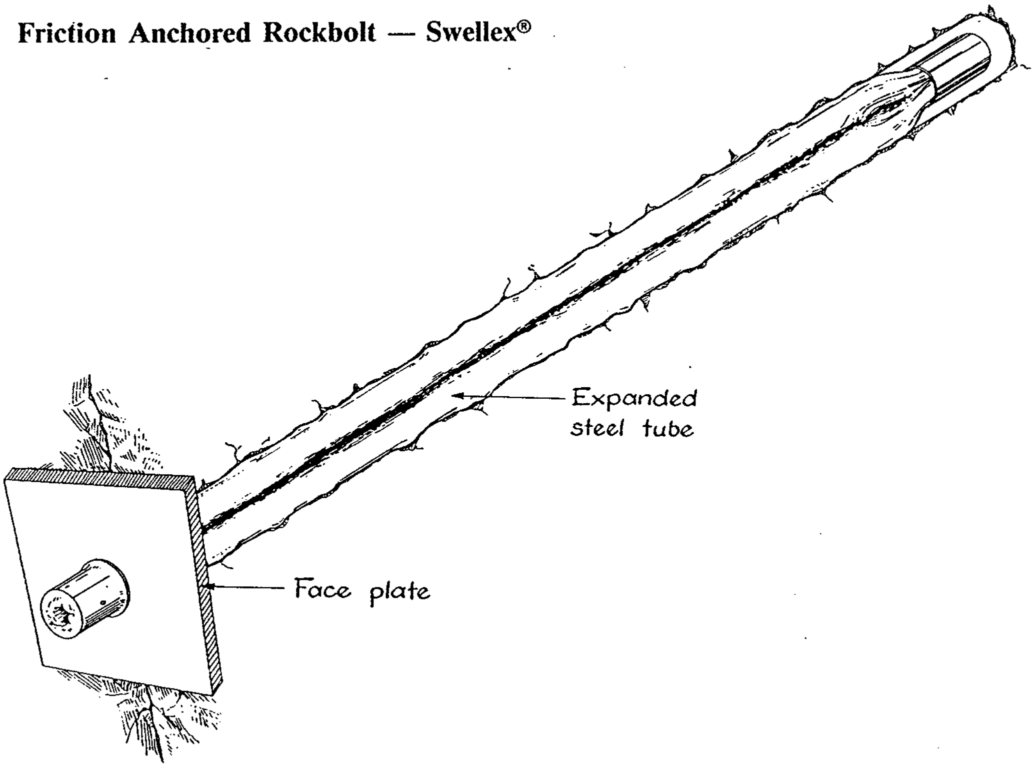
Simple installation. Gives immediate support action after installation. No hardware other than a jackleg or jumbo boom for installation. Easy application of wire mesh.

Disadvantages

Relatively expensive. Borehole diameter is crucial in the prevention of failure during installation and in the provision of the intended holding force. Successful installation of longer bolts can be difficult. Cannot be used in long term installations unless protected against corrosion.



Friction Anchored Rockbolt — Swellex®



Typical technical data

Tube diameter:	26 mm	26 mm	1 in
Yield load, steel tube:	130 kN	13 tons	14 tons(US)
Ultimate load, steel tube:	130 kN	13 tons	14 tons(US)
Ultimate axial strain, steel tube:	10 %	10 %	10 %
Weight of bolt without face plate:	2 kg/m	2 kg/m	1.34 lb/ft
Bolt lengths:	any length required		
Recommended borehole diam.:	35±3 mm	35±3 mm	1 3/8 in

Swellex® is a registered trademark of Atlas Copco AB, Sweden.

Advantages

Rapid and simple installation. Gives immediate support action after installation. Can be used in a variety of ground conditions. The installation causes contraction in the bolt length. This effectively tensions the face plate against the rock surface.

Disadvantages

Relatively expensive. Corrosion protection required if used in long term installations. Requires a pump for installation.

3.5 Support

A number of supp
face plate. Rockbo
rock straps to the

Face plates

A face plate is de
surrounding rock.
face plate is cruci

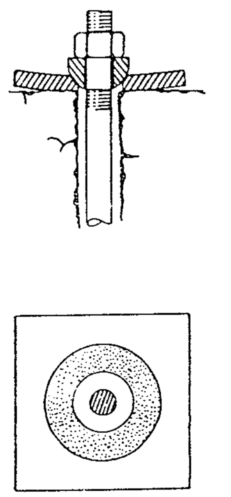


Fig. 2 Some comm
SCHACH (19

The flat plate can
perpendicular to th
nut as in Fig. 2, t
introducing unfav
hemispherical seati
favourable tension
at a few highly st

Advantages

Relatively inexpensive. The bolt gives immediate support action after installation. By rotating the bolt, a torque is applied to the bolt head and tension accumulates in the bolt. By post-grouting, the bolt can serve as permanent reinforcement. In hard rock, high bolt loads can be achieved. It is a versatile system for rock reinforcement, assuming hard rock conditions.

Disadvantages

Limited to use in moderately hard to hard rock. Difficult to install reliably, (see also section 4.1). Must be monitored and checked for proper tensioning. Loses bearing capacity as result of blast vibrations or when rock spalls off around borehole collar due to high rock stresses.

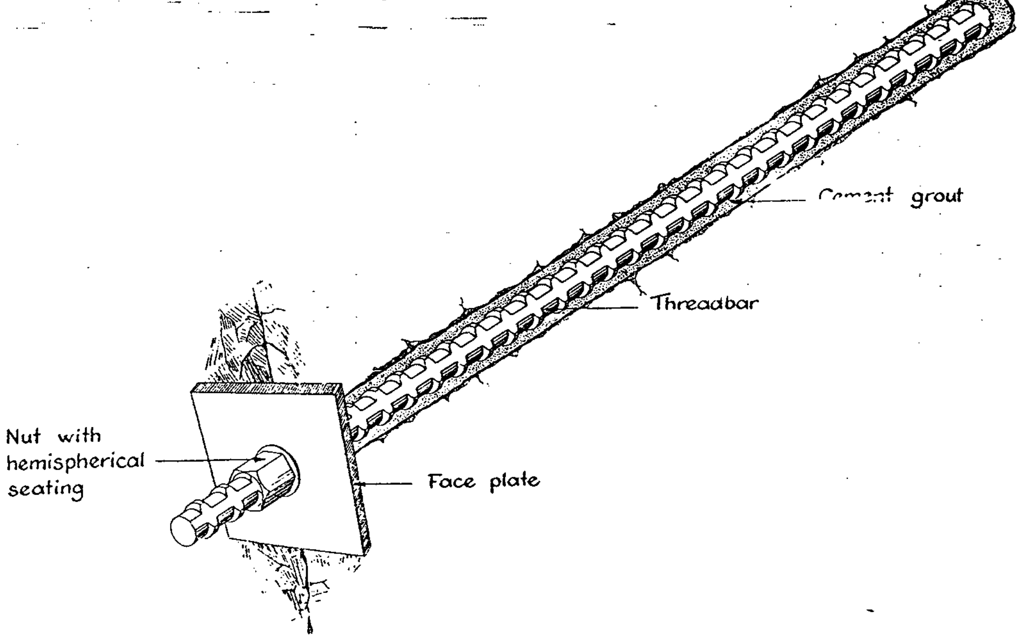
3.2 Grouted Rockbolts

Grouted rockbolts have been commonly used worldwide for the past forty years both in mining and civil engineering applications.

The most commonly used grouted rockbolt is the fully grouted rebar or threaded bar made of steel. Cement or resin are used as grouting agents. The rebar used with resin creates a system commonly used for tensioned rockbolts but the rebar or the threaded bar with cement grout can also be used for untensioned bolts. Both systems are used for temporary as well as permanent support under various rock conditions. The threadbar rockbolt is mainly used in civil engineering applications for permanent installation.

A few years ago it was predicted that the resin would, in general, replace the use of cement as grouting agent for fully grouted rockbolts. However, for a number of reasons, (mainly cost) this did not occur.

Grouted Rockbolt — Dywidag® steel



Typical technical data

Steel quality designation:	1080 N/mm²	110 kp/mm²	157 kpsi
Steel diameter:	20 mm	20 mm	7/9 in
Yield load, steel:	283 kN	28 tons	31 tons(US)
Ultimate load, steel:	339 kN	34 tons	37.5 tons(US)
Ultimate axial strain, steel:	9.5 %	9.5 %	9.5 %
Weight of bolt without face plate and nut:	2.6 kg/m	2.6 kg/m	1.75 lb/ft
Bolt lengths:		any length required	
Recommended borehole diam.:	35±3 mm	35±3 mm	1 3/8 in

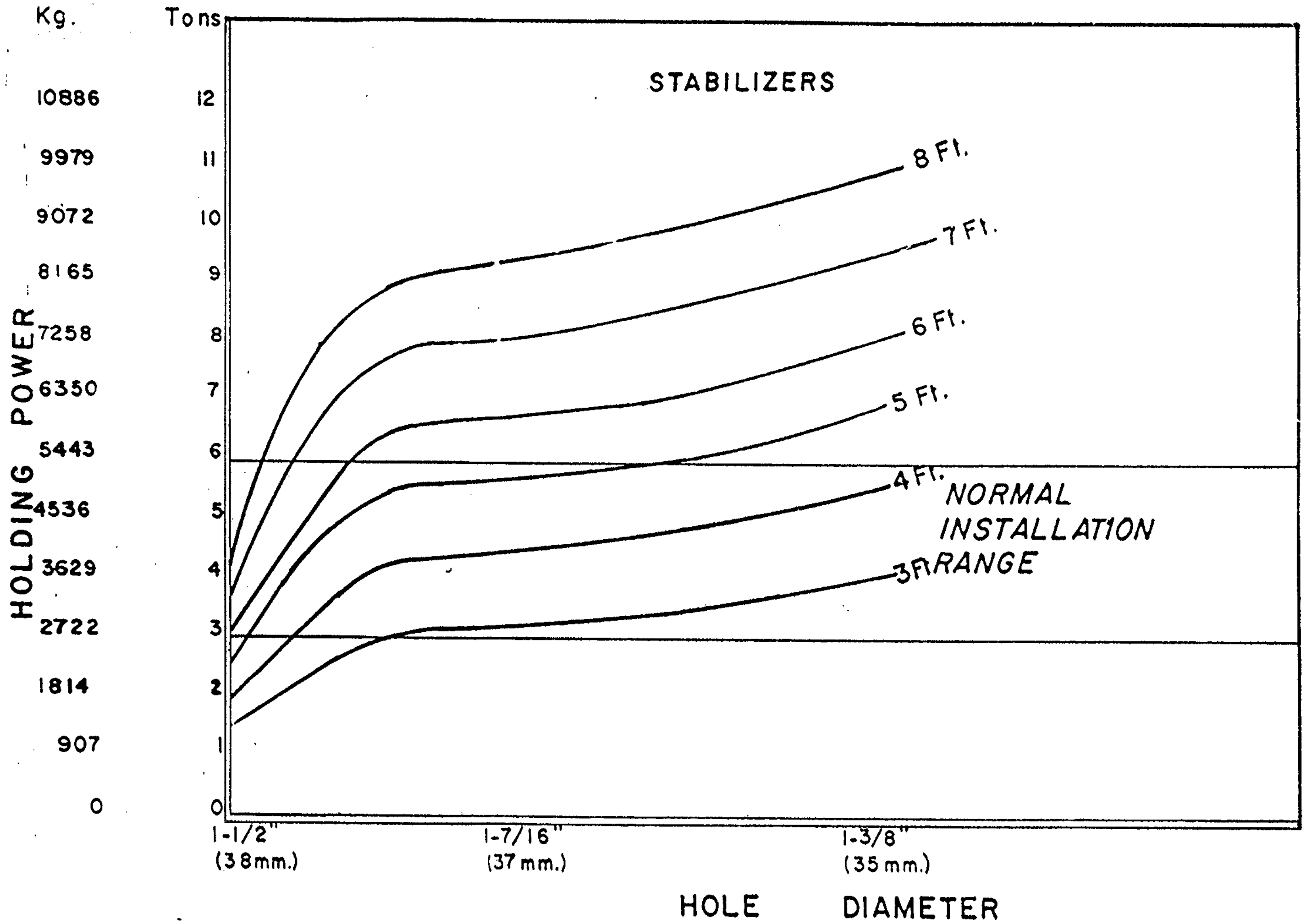
Dywidag® is a registered trademark of Dyckerhoff & Widmann AG, F.R. Germany.

Advantages

Properly installed, it is a competent and durable reinforcement system. Affect of corrosive environments is minimal. The system gives high bolt loads in various rock conditions.

Disadvantages

Expensive. Tensioning of the rockbolt is possible only if special installation procedures are followed. Use of standard cement in the grout requires several days curing before the bolt can take load. Quality of grout is difficult to check and maintain constant.



REVISIONS			Cassiar Mining Corporation McDAME Exploration Project		
NO.	DATE	BY	CHART OF SPLIT STABILIZERS		
1			DRAWN BY R. M.	SCALE NTS	MATERIAL
2			CHK'D	DATE 86 - 12 - 16	DRAWING NO.
3			TRACED	APP'D	
4					
5					

APPENDIX III

BULK SAMPLE PROCEDURE

P Jones 04/12/86

MCDAME DEVELOPMENT ORE BULK SAMPLE #2

Preamble:

Data collected from the test milling of the McDame development ore sample #2 has been compiled using two separate yardsticks - the Bauer McNett classifier and the Turner and Newall classifier.

During the milling of the bulk sample, mill tails were collected for processing through the wet mill circuit as back-up data to test milled tails.

McDame Development Ore (November 1986)
Statistical Summary

Concentration and Drying:

Delivered	=	766 tonnes
Dried	=	617 tonnes
Rejected	=	149 tonnes
Running Time	=	7.5 hours + 8.5 delays
Feed Rate	=	102 t.p.h.
Average moisture (-0.25") feed	=	5.2 %
Average moisture (-0.25") dried	=	2.0 %
Fuel Consumed	=	380 litres (0.62 l/tonne)

*More ore was delivered, however, this was not milled due to the low grade of the oversized (+6") rock. Approximately 80 tonnes of oversized rocks were dumped.

Milling:

Tonnes Milled	=	588 tonnes
Operating Time	=	5 hours, 30 minutes
Feedrate	=	175 tonnes/hr
Yield	=	4.16 %
Fibre Produced	=	24.55 tonnes

Grade Distribution:	'A'	=	0 tonnes	0%
	'AK'	=	1.8 tonnes	7.4%
	'AX'	=	7.2 tonnes	29.5%
	'AY'	=	9.6 tonnes	39.9%
	'AZ'	=	5.9 tonnes	24.1%
	Total	=	24.5 tonnes	100%

McDame Ore Composite Results:

Bauer McNett:

Mesh Size	MA	MK	MX	MY	MZ
+4	81	44	6	2	2
+14	4	25	38	6	4
+35	2	7	30	27	19
+200	1	5	8	22	30
-200	12	19	18	43	45

Test Mill and Laboratory Results:

Due to the tendency of the Bauer McNett Classifier to over-value the total +35 mesh fraction, duplicate samples were taken for evaluation on the T&N Classifier for comparative reasons.

Both Bauer McNett and T&N Classifier results were mathematically adjusted to a common -200 mesh dust content to allow accurate comparison. This was set at 22% which closely represents the average -200 mesh dust content in the total fibre production.

Adjustment for Dust Calculation:

1. The average dust of fibre produced on the McDame fibre is greater than 22% (-200M) based on Bauer McNett results. However, all the test results from the concentrating and drying of the fibre was adjusted to 22% dust (-200M).

2. The standard formula used to adjust percent recovery results to 22% dust (or whatever -200 mesh required) is as follows:

   Adjusted Percent Recovery =

   $$\text{Actual \% Recovery} \times \frac{100 - (\text{actual \% -200M dust in fibre})}{100 - (\text{required \% -200M dust in fibre}}$$

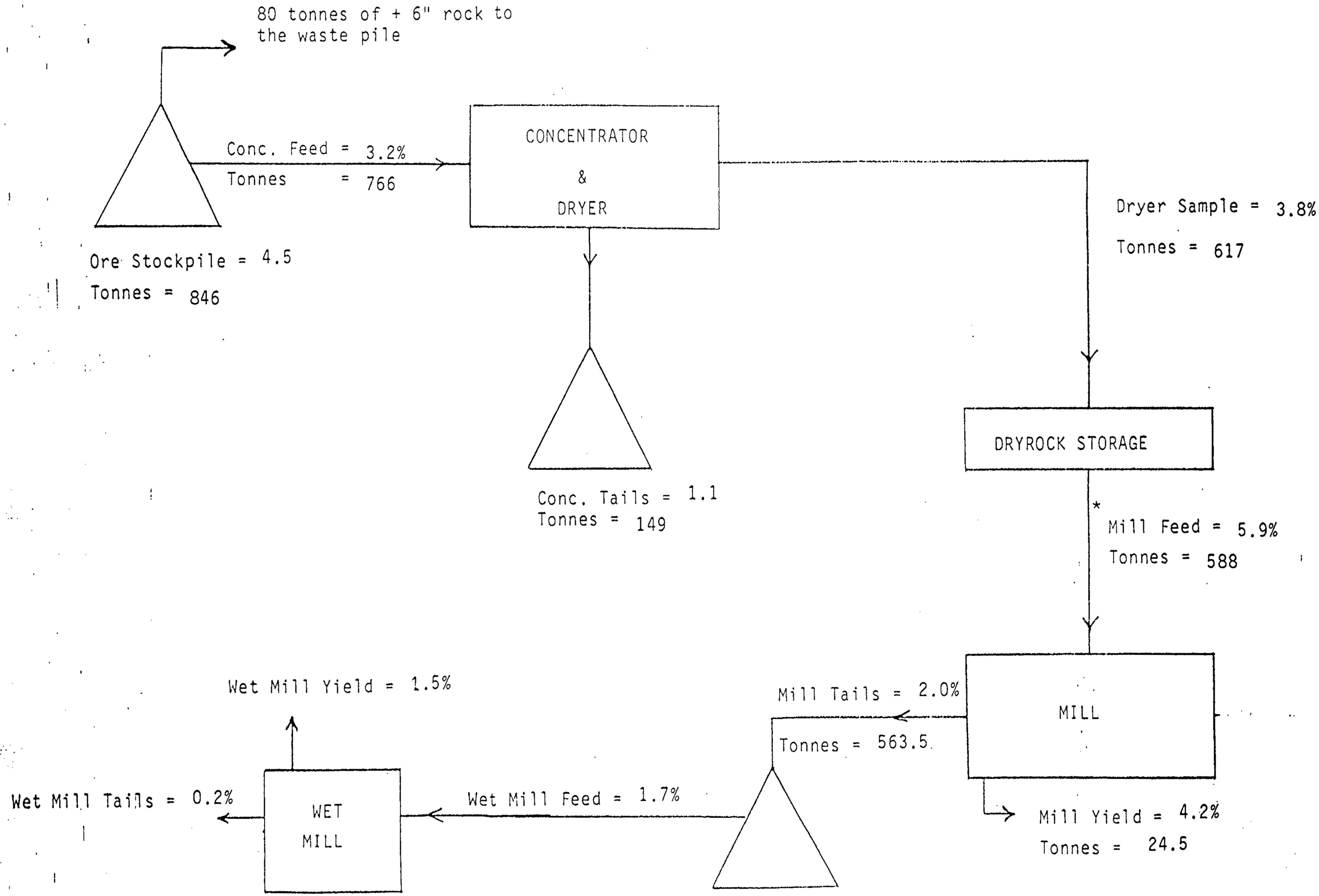
3. The standard formula used to adjust each Bauer McNett or T&N Classifier fraction to the required -200 mesh dust result is as follows:

   Adjusted fraction =

   $$\text{Actual fraction result} \times \frac{(100 - (\text{actual \% -200M dust in fibre}))}{(100 - (\text{required \% -200M dust in fibre}))}$$

TABLE III

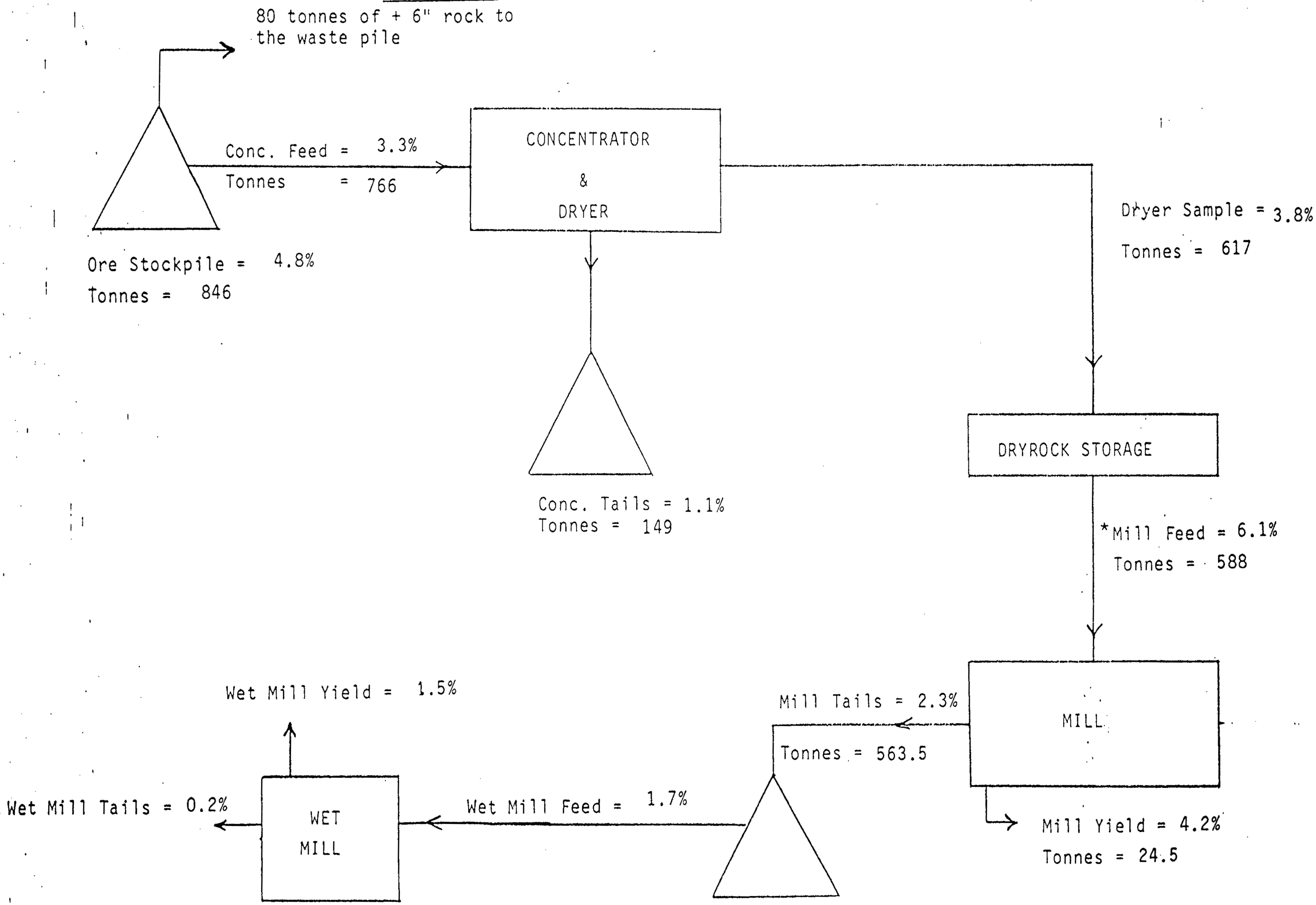
Flowsheet for Adjusted Bauer-McNett Results



*Hand Sampled

TABLE I.

Flowsheet for Adjusted T & N Classifier Results



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List of Tables:

Table:

McDame Ore Concentrator and Mill Tests.

INTRODUCTION:

During November, 1986, test milling was performed on McDame development ore. On November 17, the concentrator received 766 tonnes of McDame ore. From this amount, 149 tonnes grading 1.1% fibre, were removed as concentrator tails. The upgraded concentrator ore was dried to an average moisture of 2%, then stockpiled separately in the dry rock storage.

On November 21, 588 tonnes of the ore were processed through the Cassiar mill. The mill produced 24.5 tonnes of relatively short fibre. This yield of 4.16% compared favorably with test mill results.

A bulk sample, taken from the mill tails, was tested on the new wet mill research circuit. The wet mill recovered 1.5% fibre, which theoretically brings the total milling yield to 5.7%.

In summary, the McDame ore was run through three processing stages. The first was a concentrating and drying process, followed by a dry milling phase then, thirdly, a wet milling procedure. The following is a detailed description of each of the three processes or phases used.

Concentrator Test:

Approximately 1 000 tonnes of McDame contact ore was delivered to the Cassiar Mill via 40 ton haul trucks in November, 1986. Grab samples taken from the stockpile of this ore, then treated in the test mill, indicated the recoverable fibre content to be about 4.5%.

The concentrator test run was scheduled to include initial crushing with a portable gravel pit crusher but, because the crusher proved to be undersized for the job (the main fuse blew upon loading, and the hopper was too small), the McDame ore was fed directly to the grizzly. As expected, direct feeding resulted in a considerable amount of down time due to plugged chutes.

On November 17, 1986, at 10:35 a.m. the first bucket of ore was dumped, and the concentrator test officially ended 14.1/2 hours later, at 1:00 a.m. November 18. Including the 1.1/2 hours of pre-test waiting, the total test wait and down time was 8.5 hours. Table 3 outlines these delays:

Table 3

	Delay Description	Total Delay Time
1.	Plugged feed chutes to CIA and CIB tyrock secreens	4 hours
2.	Problems with gravel crusher	2 hours
3.	Waiting for loader	1.1/2 hours
4.	Broken diesel line	1.1/2 hours
5.	Plugged pan feeder	1.1/2 hours

McDame Ore Concentrator and Mill Tests:

During the 7.1/2 hours of operation, an average of 102 tonnes of ore per hour were fed through the concentrator. The concentrator rejected 19.45% of the feed at 1.1% fibre. The remaining 617 tonnes was dried from 5.2% to 2.0% moisture content levels. This ore was isolated in the dry rock storage area, in preparation for the mill test. The results of the Bauer-McNett, T&N classifier runs, and screen analysis for the concentrator are shown in Tables 4,5, and 6, respectively.

Three laborers were responsible for removing contaminants and oversized rock from the CO1 and CO3 betls. Table 7 is a list of contaminants removed from the McDame ore. Though the contamination level was found to be high in this case, actual production from underground ore should be almost contamination free for the proposed block caving method.

[illegible] will be [illegible]

Table 4

McDame Ore Concentrator Test Results with Bauer-McNetts

Sample Type	Adjusted for Dust					Adj-Ave Bauer-McNett					Ave.Act.Bauer-McNett				
	%F.F.	%C.F.	%FF/CF	ADD PASS	TOTAL FIBRE	+4	+14	+35	+200	-200	+4	+14	+35	+200	-200
McDame Ore (Stock pile)	1.32	2.49	3.81	0.64	4.45	10	23	25	20	22	9	21	26	17	27
C01 (Conc. Feed)	0.81	1.72	2.53	0.65	3.18	7	19	23	29	22	6	16	26	18	34
C09 (Dryer Feed)	0.77	2.27	3.04	0.75	3.79	6	24	26	22	22	6	21	27	15	31
T1A (Conc. Tails)	0.18	0.56	0.74	0.4	1.14	7	15	20	38	20	5	12	23	21	39
C1A&C1B 'Thrus'	2.03	1.96	3.99	0.98	4.97	6	19	24	29	22	5	16	27	18	34
C03 (C02 'Overs')	0.12	0.65	0.77	0.49	1.26	10	19	15	35	21	6	13	15	18	48
C03 'Thrus'	0.39	1.31	1.7	0.88	2.58	4	17	34	23	22	3	16	35	17	29

Notes: 1. The T1A (tailings sample was removed from this year's sample points)

TABLE 5

McDAME ORE CONCENTRATOR TEST RESULTS WITH T&N CLASSIFIER

Sample Type	ADJUSTED FOR DUST %F.F.	%C.F.	%FF/CF	ADD PASS	TOTAL FIBRE	ADJ-AVE T&N CLASSIFIER +7	+14	+25	+50	+200	-200	AVE. ACT. T&N CLASSIFIER +7	+14	+25	+50	+200	-200
McDame Ore (Stockpile)	1.38	2.65	4.03	0.75	4.78	3	8	22	27	18	22	3	8	20	24	16	29
C01 (conc.feed)	0.88	1.79	2.67	0.67	3.34	3	4	20	31	20	22	3	4	18	28	16	31
C09 (dryer feed)	0.73	2.35	3.08	0.71	3.79	3	5	22	25	23	22	3	5	20	22	20	30
T1A (conc.tails)	0.16	0.55	0.71	0.38	1.09	3	8	21	28	18	22	2	6	15	20	15	42
C1A &C1B 'thrus'	2.04	2.14	4.18	1.07	5.25	1	3	25	28	21	22	1	3	22	25	18	31
C03 (C01'overs')	0.11	1.05	1.16	0.51	1.67	3	4	22	31	18	22	3	3	19	27	16	32
C03 'thrus'	0.14	1.4	1.8	0.91	2.71	1	3	24	34	16	22	1	3	23	33	15	25

TABLE 6
McDAME ORE CONCENTRATOR SAMPLES BOX ANALYSIS
NOVEMBER, 1986

Sample Type	Sample Wt.Kg.	% Fibre	Particle Size Distribution							
			+3"	+1.1/2"	+1"	+3/4"	+1/2"	+1/4"	Pan	
McDame Ore (S.P.)*	49.5		12.3	21.2	9.1				57.4	Not screened on +3/4" -1/4" screens
C01 belt (conc.feed)	41.5		11.3	20.0	14.4				54.3	" "
C09 dryer	23.0				1.7				98.3	" "
C03 ('overs'C02 screen	34.5		2.3	31.9	30.7				35.1	" "
C01A&B screen 'thrus'	46.0					8.3	14.1	17.8	59.8	Not screened on +3"---1" screens
C03 screen -thrus'	35.0						0.1	2.0	97.9	" "
T1A conc. tails	19.5			8.7	10.3	13.8	23.6	29.7	13.9	Not screened on +3" screen

Note: *Sample collected from outside stockpile before concentrating.

TABLE 7

McDAME ORE CONTAMINATION (NOVEMBER, 1986)

Location Collected	Type	Description of Contamination	Weight (Kg)
1. C01-C09	Wood		1.7
2. C01-C09	Metals	Roof plates, chains, wire, strapping, wire mesh, cable armour	6.0
3. C01-C09	Paper Rubber	Fruit juice containers, cigarette packs Gloves, dust masks, survey tape, sand paper, ear plug bags, rope, electric cable covers, explosive covers	6.0
4. C01-C09	Shotcrete		18.0
5. 22-HS-A4A 22-HS-A4B		Rubber tire bits, Nonel tubes, survey tape, wood, handi-wipes, cigarette butts explosive paper.	1.0

Mill Test:

At 8:30 a.m. on November 21st, McDame ore was processed by the Cassiar mill at a rate of 175 tonnes per hour. As closely as possible, the mill was configured to the November, 1985 set-up. There was no blending between circuits, and all floats were sent to tails. As opposed to last year, there were few milling or bagging problems. For bag swelling results, see Table 8. The last of the McDame ore was fed into the plant at 12:45 p.m. and fibre bagging was completed by 2:15 p.m. A layer of frozen muck formed a crust on the McDame dry rock stockpile. This layer produced frozen lumps in the feed and caused a plugging of the mill feeder chute DR-BF-R02. During the 35 minute delay, while clearing of the chute took place, the remaining frozen lumps were broken up by the loader.

Four fibre grades were produced during this run. Tables 9 and 10 summarize the fibre quantities and qualities yielded. The 'AK' circuit produced a long and clean 'AK' fibre. The 'AX' fibre was shorter than normal Cassiar fibre, but contained less dust. Both the 'AY' and 'AZ' fibres were short and dusty and basically of 'AZ' quality. Only 25 Kg of 'A' grade fibre was bagged during the McDame ore test run. Another 13 Kg of 'A' fibre, and 1 Kg of contaminants, (see Table 7), were collected from the table after HS-A4A & B. The high level of contaminants in the 'A' circuit is a concern needing attention and addressing.

The sample points for this years test were identical to the 1985 McDame ore run. Inadequate sample sizes were obtained from some sample points, however, due to the lower ore grade and shorter test period.

Consequently, a full range of laboratory tests could not be performed on all sample points. Where this was the case, a notation of 'inadequate sample' was inserted in place of data values. The T&N classifier and Bauer-McNett results for mill sample points are shown in Tables 11 and 12. The actual mill yield was 4.2%, as 24.5 tonnes of fibre wasproduced from 588 tonnes of mill feed.

TABLE 8

The following results are the unit dimensions of the McDame 2 fibre measured on November 24, 1986.

MK	MX	MY
(1) 48.1/2 x 41"	(1) 48.1/4" x 41"	(1) 48.1/4" x 41"
	(2) 48.1/4" x 41"	(2) 48" x 41.1/4"

MZ

(1) 47.3/4" x 40.1/2"
(2) 47.3/4" x 40.1/2"

The following results are the unit dimensions of the McDame 2 fibre measured on December 8, 1986.

MK	MX	MY
(1) 48.1/2" x 41"	(1) 48.1/2" x 41"	(1) 48.1/2" x 41"
	(2) 48.1/2" x 41"	(2) 48" x 41.1/4"

MZ

(1) 47.3/4 x 40.1/2"
(2) 47.3/4 x 40.1/2"

Note: Very little change occurred on the McDame fibre probably due to shorter fibre. (M.S. Taylor).

TABLE 9

McDame Fibre - Composite Sample Test Results - Cassiar

Grade	Mach #	Bauer McNett 4	14	35	200	-200	Combing Av.L.	%+1/2	1/16"	Quebec Standard Box 1	Box 2	Box 3	Pan	Rock Cont	Surf Area	Mag. Rating
MA65	4	81	4	2	1	12	.346	24.9	13	14.4	1.2	0.3	0.1	-	6300	0.15
MK	3	39	31	8	5	17	.244	5.1	23	13	2.2	0.7	0.1	-	6700	0.6
MX	2	7	37	30	8	19	-	-	-	-	9.2	5.2	1.6	0.1	5100	.95
MY	1	2	6	26	21	45	-	-	-	-	-	10.8	5.2	0.1	8200	2.67
MZ	4	2	5	18	31	44	-	-	-	-	-	6.0	10.0	0.5	5000	3.05

TABLE 10

McDAME FIBRE - COMPOSITE SAMPLE TEST RESULTS - CASSIAR

		T&N Classifier									T&N Elutriator			
Grade	Mach #	.25	7	14	25	50	200	-200	G.F.	Freeness	Crude	Partly Open	Open	-200
MA	-	48	15	20	8	-	3	6	207	10.4				
MK	-	-	41	25	16	6	6	10	144	10.7	20	10	60	10
MX	-	-	1	15	43	17	8	16	91	22.7	27	10	48	15
MY	-	-	-	1	10	29	24	36	51	206.0	9	14	42	35
MZ	-	-	-	-	3	24	35	38	44	203.0	15	14	38	33

TABLE II

McDame Ore - Mill Circuit Tests - Bauer McNetts

Sample Type	Adjusted for Dust														
	%F.F.	%C.F.	%FF/CF	Pass	Fibre	4	14	35	200	-200	4	14	35	200	-200
Mill Feed	1.58	3.04	4.62	1.24	5.86	8	19	23	28	22	7	16	27	16	34
Mill Tails	.78	.69	1.48	.50	1.98	4	10	14	50	22	2	6	19	24	49
Mill Tails [Tailings Pile]															
Conc.Tails [Tailings Pile]															
FC-X3A&B;X4A&B 'overs']															
HS-R7C&D 'overs']		"Inadequate Sample"													
HS-R8A&B, O.M.T.]															
FC-R8C&D 'overs']															
Ay,AZ,Tails & 1954 w/b]															
AZ tails]															
T4C]															

TABLE 12

McDame Ore Mill Circuit Test Results with T&N Classifier

Sample Type	Adjusted for Dust					Adj-Ave T&N Clasifier						Ave.Act.T&N Classifier					
	%F.F.	% C.F.	%FF/CF	Add Pass	Total Fibre	+7	+14	+25	+50	+200	-200	+7	+14	+25	+50	+200	-200
Mill Feed	1.73	3.08	4.81	1.27	6.08	4	5	22	29	18	22	3	4	19	26	16	32
Mill Tails	0.94	0.08	1.74	0.58	2.32	1	1	9	30	38	21	1	1	7	23	28	40
FC-X3A&B;X4A&B 'overs'	0.12	0.13	0.25	-	0.25	1	2	12	37	31	17	1	2	13	40	28	16
HS-R7C&D 'overs'	0.02	0.18	0.2	-	0.2	4	3	17	37	19	20	4	3	16	34	16	27
HS-R8A&B	0.18	0.81	0.99	-	0.99	-	-	17	51	10	22	-	-	17	50	10	23
FC-R8C&D 'overs'(T4A)	0.02	0.21	0.23	-	0.23	1	1	16	39	23	20	1	1	16	37	20	25
AY,AZ Tails&1954 W/B	1.63	0.25	1.88	-	1.88	-	-	5	37	36	22	-	-	3	21	21	55
AZ Tails	1.0	0.26	1.26	-	1.26	-	1	6	36	35	22	-	-	5	28	26	41
T4C	0.13	0.72	0.85	-	0.85	1	1	11	39	30	18	1	1	11	38	24	25

Wet Milling of McDame Tailings:

A feed sample of approximately 1.5 tonnes was obtained from the sample point at the third floor pugmill. This represents total mill tailings (less concentrator tails.) This was fed at a rate of approximately 7 Kg/min. to the standard wet mill rock/fibre circuit. Samples were taken over a 30 minute period after the circuit was allowed to reach an operating balance.

Fibre yield was calculated to be 1.5%. Insufficient fibre was generated to allow processing in the grading circuit Test milling of the feed and coarse tailings gave results of 1.7 and 0.2% total (free and contained) fibre respectively. These results are normalized at 8% dust to match the fibre produced.

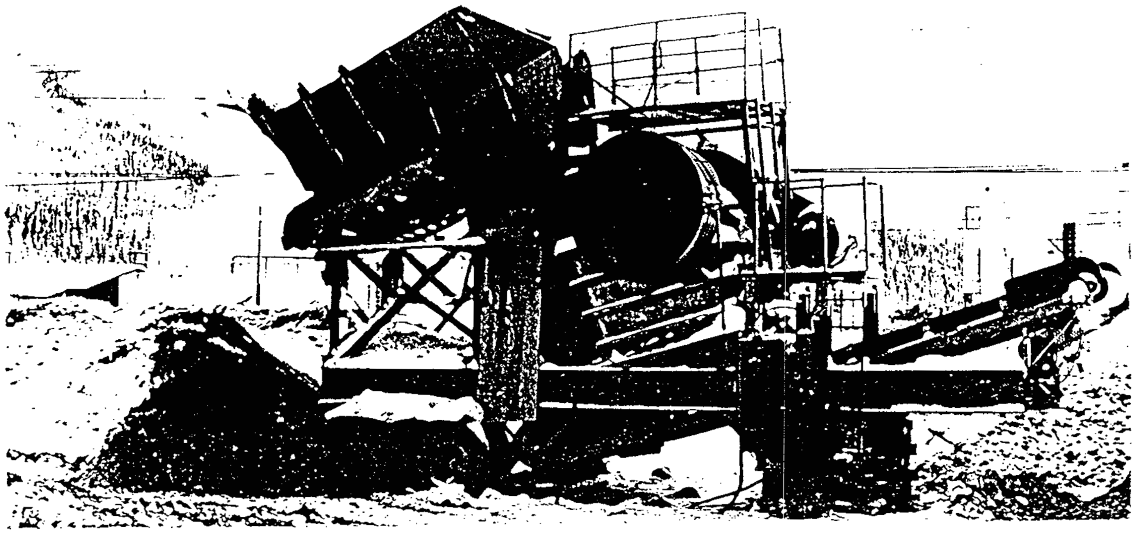
There were no major deviations from wet milling either present tails or material from the tails pile. The fibre production rate was low, consistent with the low feed grade. Most noticeable was the finer size of the feed material.

Recommendations:

1. To minimize down time during the concentrator test, the McDame ore should be crushed to produce a feed distribution similar to normal production. The best way to accomplish this would be to run the ore through the tramline crusher and then feed the concentrator site via the tramline. If the portable crusher is to be used, a suitable feed hopper must be fabricated to prevent bridging of material over the apron feeder.

2. An effort should be made to ensure adequate sample sizes at all tailings sample points. (This mill run of McDame was too short for obtaining larger samples.

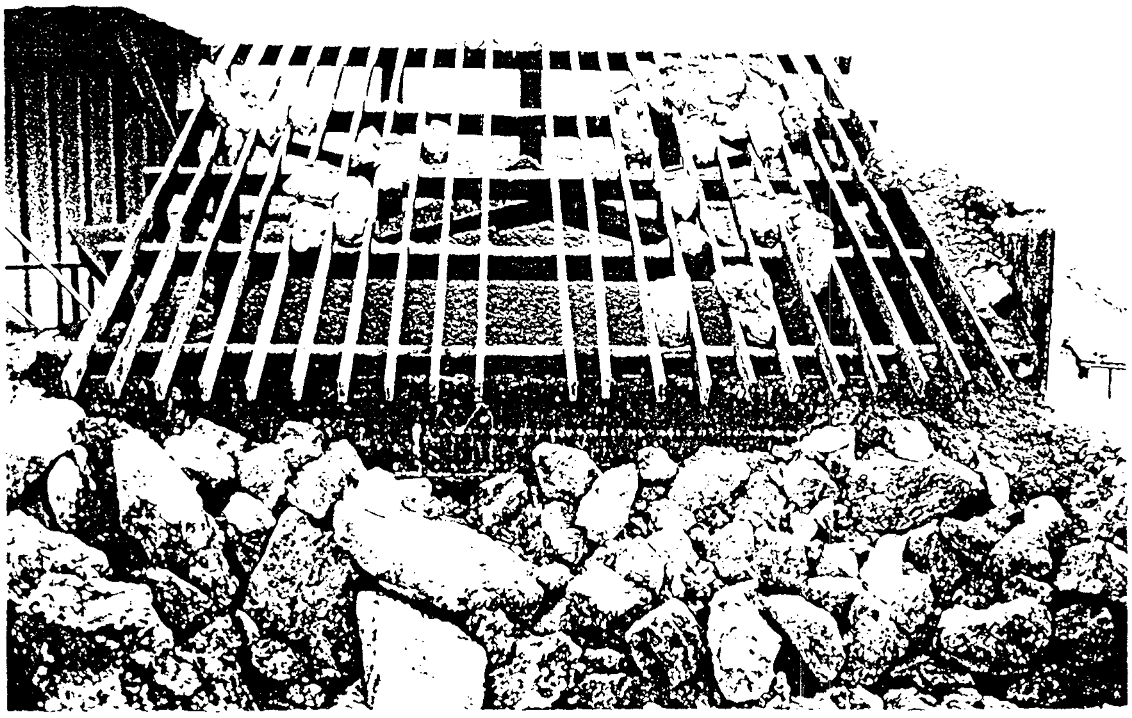
3. Samples collected should be sent to a consulting laboratory for verification as soon as a suitable testing laboratory is determined.



1. Gravel Pit Crusher

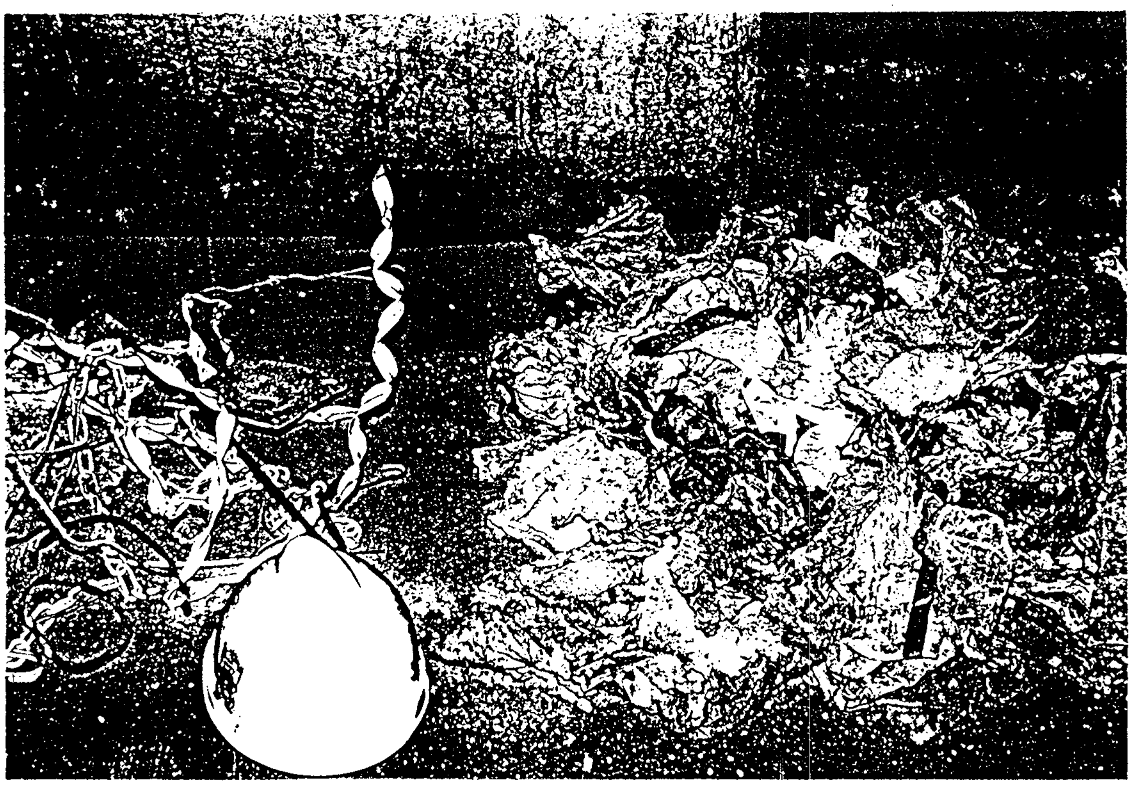
2. McDame Ore Before Concentrator

3. Feeding McDame Ore into Grizzly Outside Concentrator.

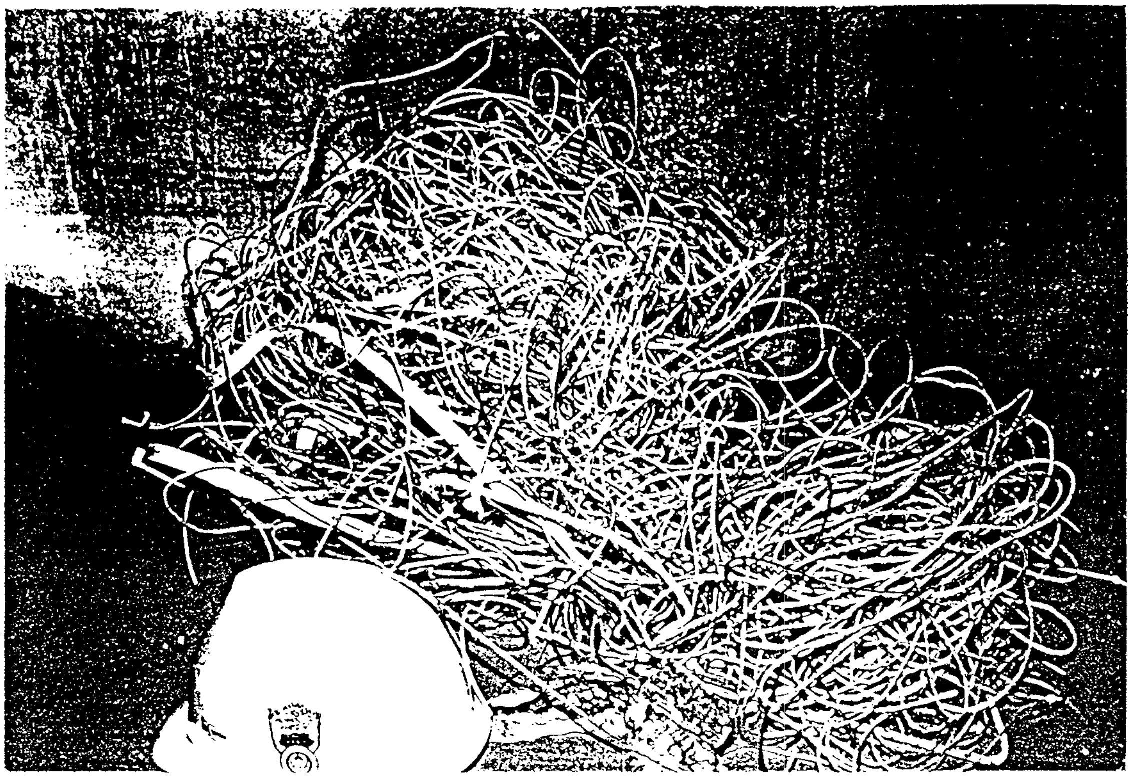


4. Grizzly with Oversized McDame Ore.

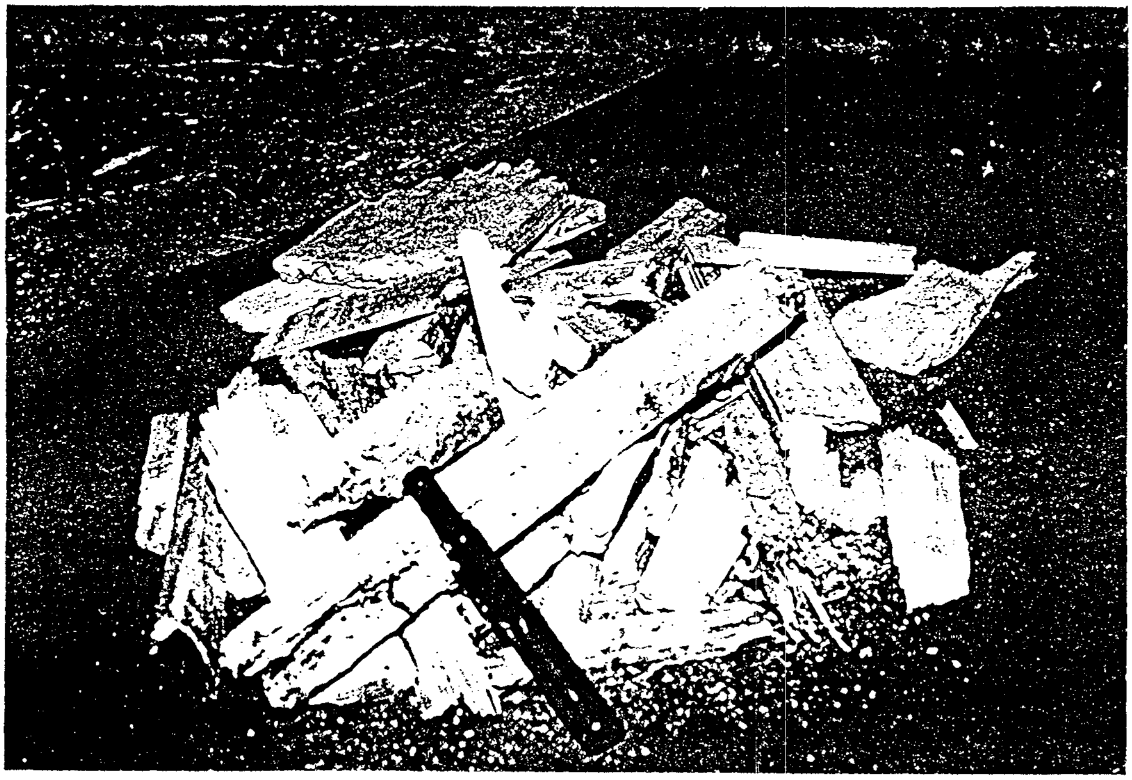
5. Oversized McDame Ore Rejected as waste.



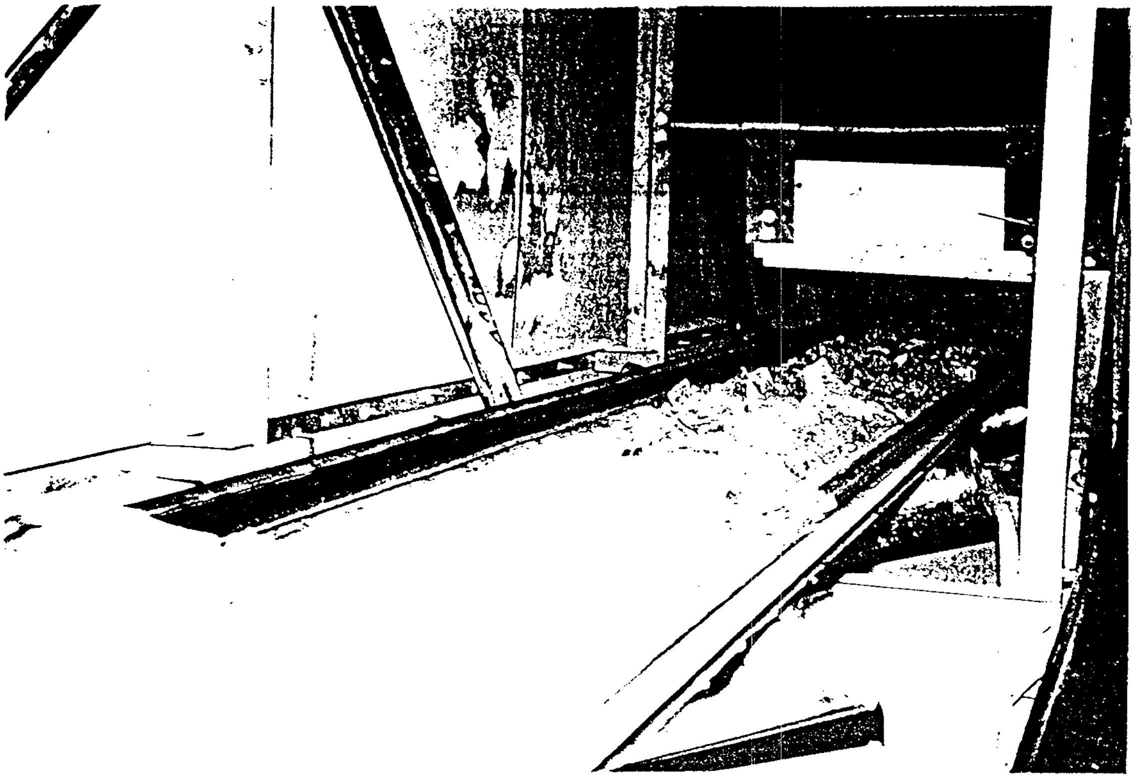
6. Metal and Paper Contaminants Removed from CO_1 & CO_2.



7. Plastic Contaminants removed from CO_1 & CO_3 Conveyors.

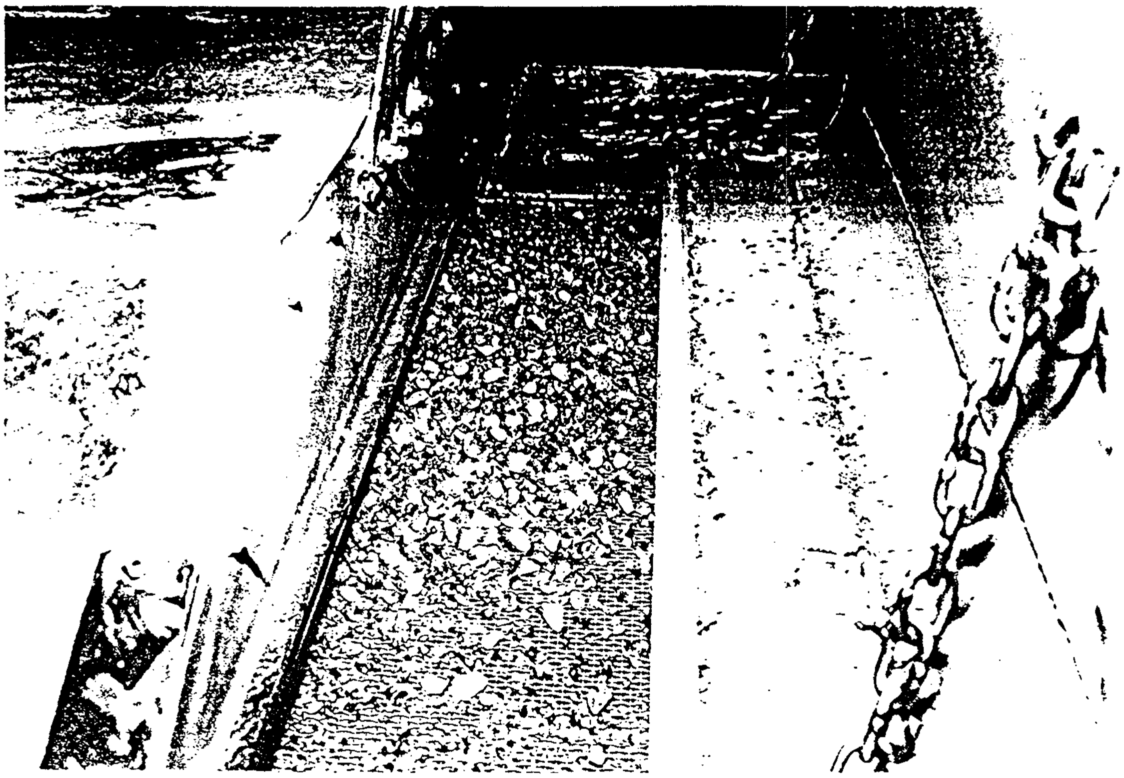


8. Wood Contaminats Removed from CO_1 & CO_3 Conveyors.

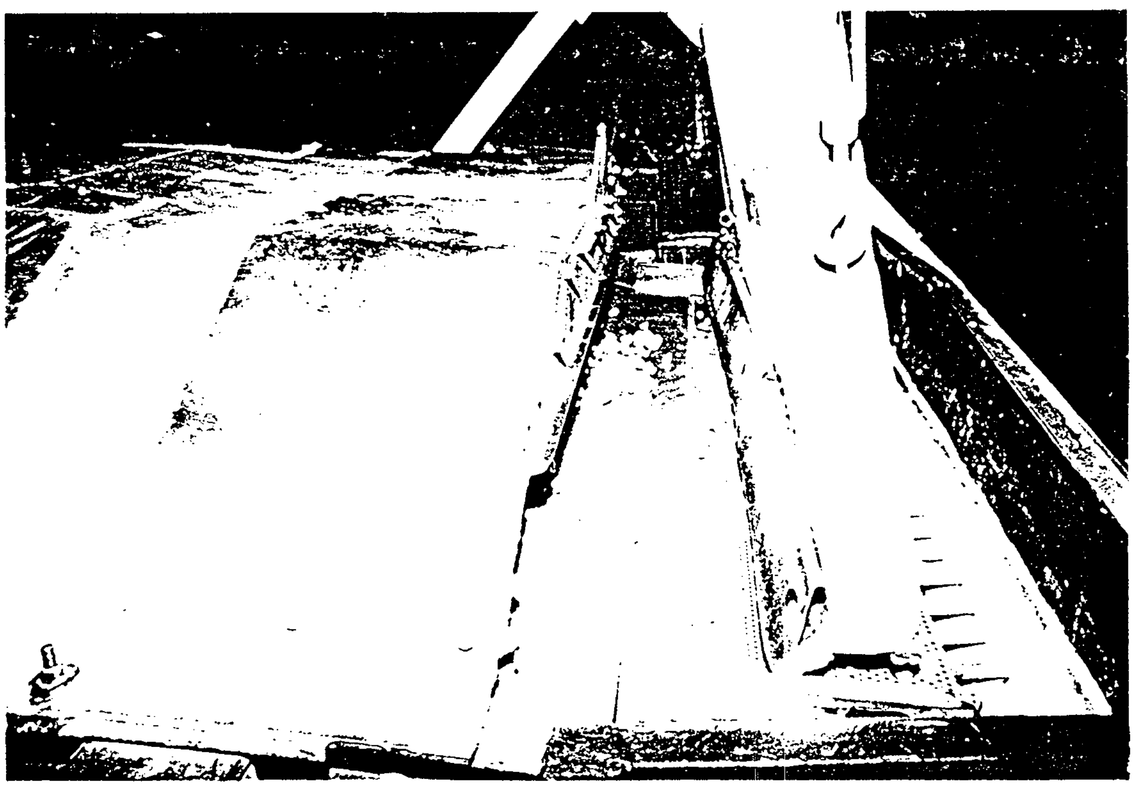


9. Mill Feed #14 Conveyor

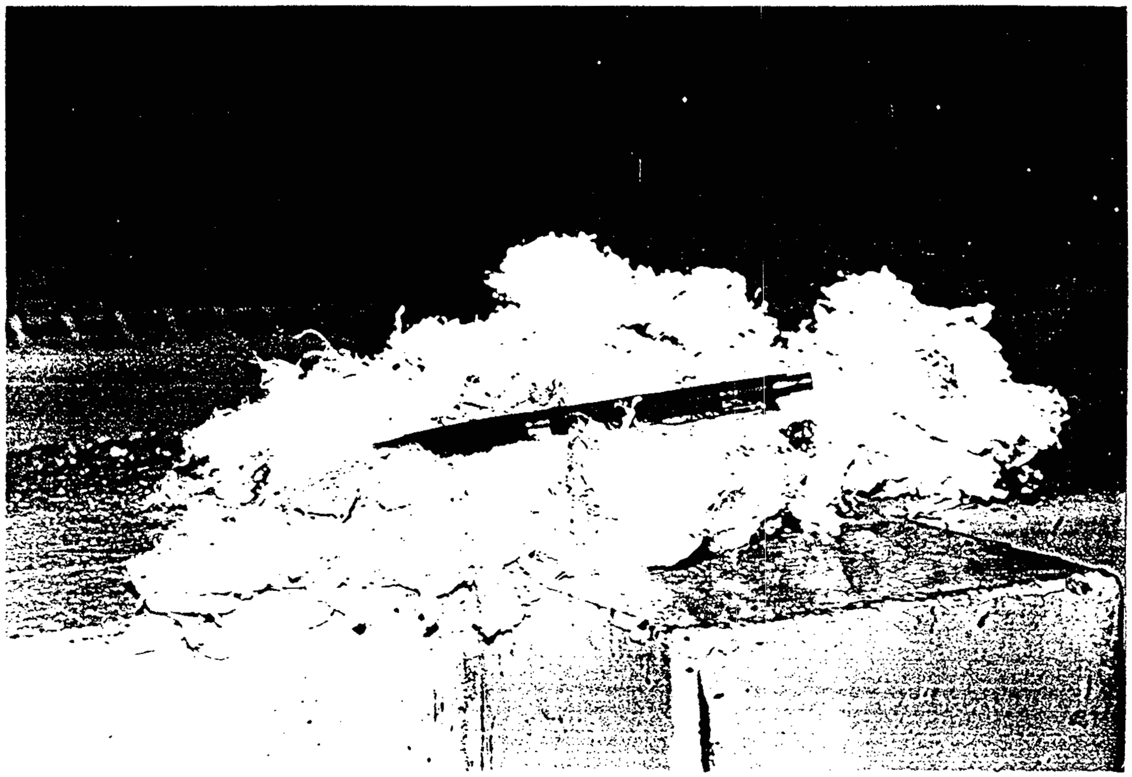
10. Normal Cassiar Feed 9% VS McDame Feed 4%.



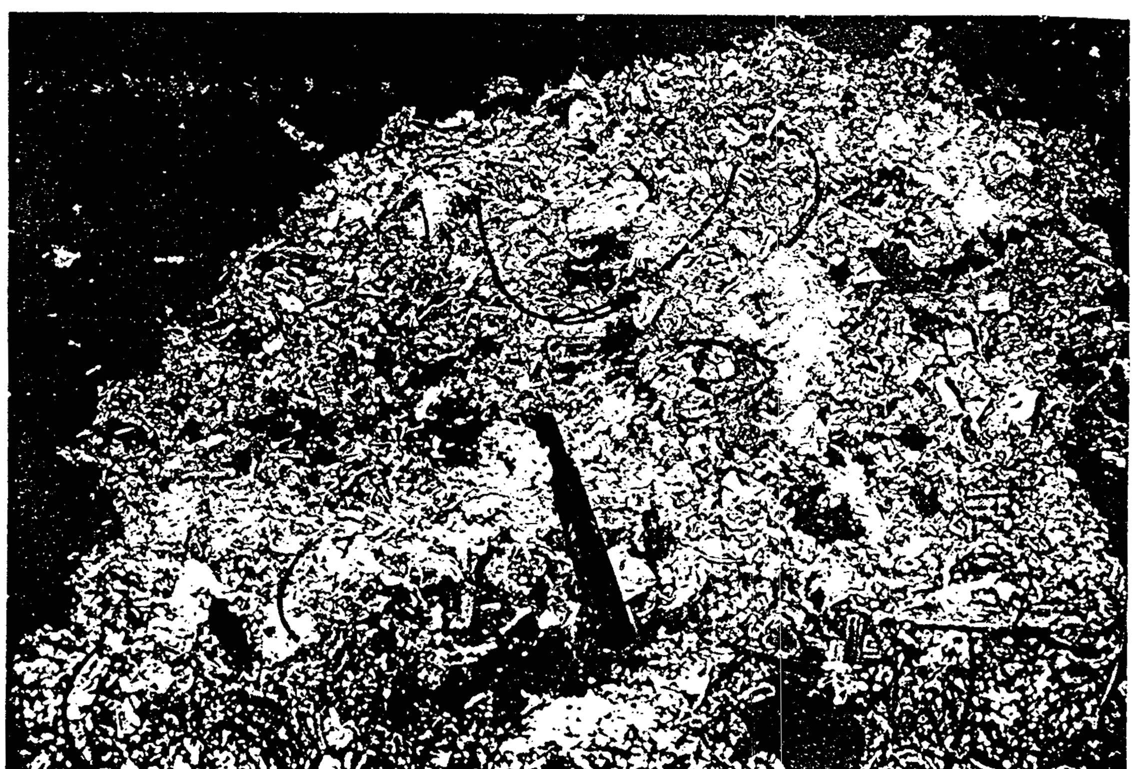
11. Rockline HS-R2 Hall Screen.



12. Rockline HS-R1 Hall Screen



13. Reject Material Off of HS-A4 Hall Screens



14. Garbage from HS-A4 Hall Screens.

APPENDIX IV

DIAMOND DRILL HOLE DATA

FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDame	HOLE	U86-1	DEPTH	113.39 m
AZIMUTH	041°	INCLINATION	-21°	SECTION	
LATITUDE	6608.03 N	DEPARTURE	7368.22	ELEVATION	1409.09 m
STARTED	June 20	FINISHED	June 27	LOGGED	by I.L. date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH m	DESCRIPTION	VISUAL LOG
1.5	45.7		Siliceous Argillite, very poor elongate nodular bedding,	
			moderately broken.	
			22.4 m Reduced HQ to NQ	
47.5	50		Black Graphitic Deformed Argillite. Blebs of pyrite common.	
50	57.5		Ribbon Chert/Argillite. 2-4 cm chert beds with ½-1 cm	
			interbeds of Argillite at 30° c/a.	
			Abundant fine disseminated and occasional blebs of pyrite	
			in argillite. Total pyrite ~ 1%.	
57.5	65.5		Laminated Argillite, parts pyritic.	
65.5	113.39		Ribbon chert/Argillite. Varying pyrite content.	
			Core mostly broken.	
			Fault zones 74 - 81.7, 85.3 - 93.3, 96.6 - 113.39	
			Slight colour alteration past 106 m (Near Serpentinite).	
113.39			E.O.H. Due to difficulty of penetration.	

FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDame | HOLE U86-2 | DEPTH 114.30 m

AZIMUTH 125^{o} | INCLINATION -25^{o} | SECTION

LATITUDE 6608.03N | DEPARTURE 7368.22E | ELEVATION 1409.09 m

STARTED June 27 | FINISHED July 2 | LOGGED by I. Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH m	DESCRIPTION	VISUAL LOG
1.5	5.03		Siliceous Argillite, Massive.	
5.03	7.13		Calcareous Argillite	
7.13	39.6		Siliceous Argillite, poor wispy pinch & swell bedding	
39.6	50.6		Fault Zone, Argillite mylonite and crush breccias	
50.6	52.7		Fault Zone, Chert/Argillite crush breccia	
52.7	77.7		Ribbon chert/Argillite. Very fine disseminated pyrite and	
			occasional lamellae	
			66.1-70 crush breccias	
			74.7 - 77.7 Fault and crush breccias	
77.7	84.4		Argillite Fault gouge	
84.4	89.0		Chert/Argillite crush breccia. Slightly bleached	
89.0	99.4		Argillite Fault gouge	
99.4	114.3		Ribbon Chert/Argillite, deformed, broken, much core lost	
			108.4 reduce NQ to BQ	
114.3			E.O.H. due to very slow penetration	

FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDame	HOLE	U86-3	DEPTH	30.18 m
ZIMUTH	90°	INCLINATION	-2.5°	SECTION	6649
LATITUDE	6649.9N	DEPARTURE	7605.8E	ELEVATION	1414.9 m
STARTED	Aug. 4	FINISHED	Aug. 5	LOGGED	by I. Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH m	DESCRIPTION	VISUAL LOG
0.1	13.4		Serpentinite, Dark green, with fibre veins, fairly competent.	
13.4	30.2		Fault zone, crushed and fractured serpentinite, parts gouge,	
			light to medium green	
30.2			E.O.H.	

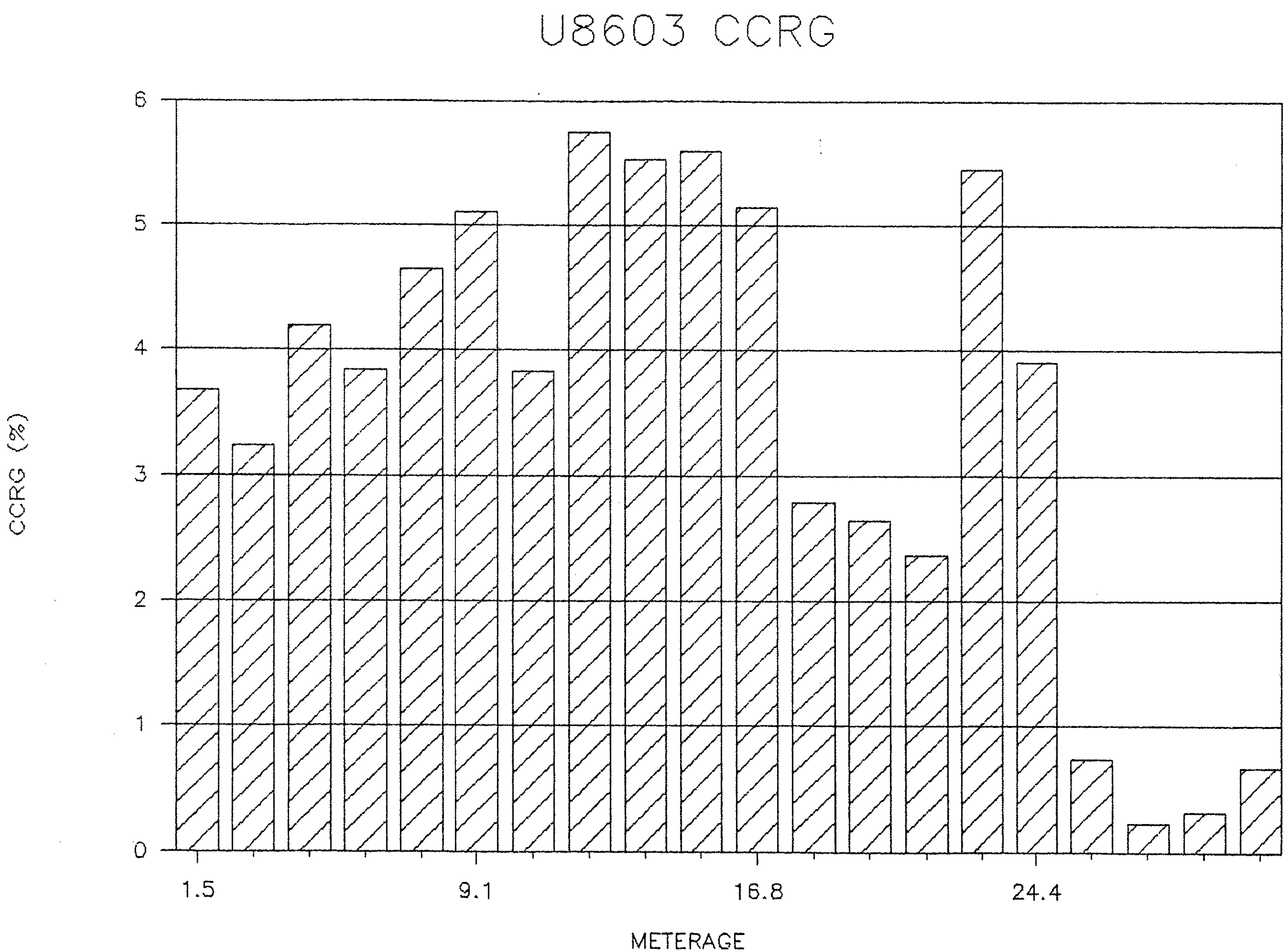
8603

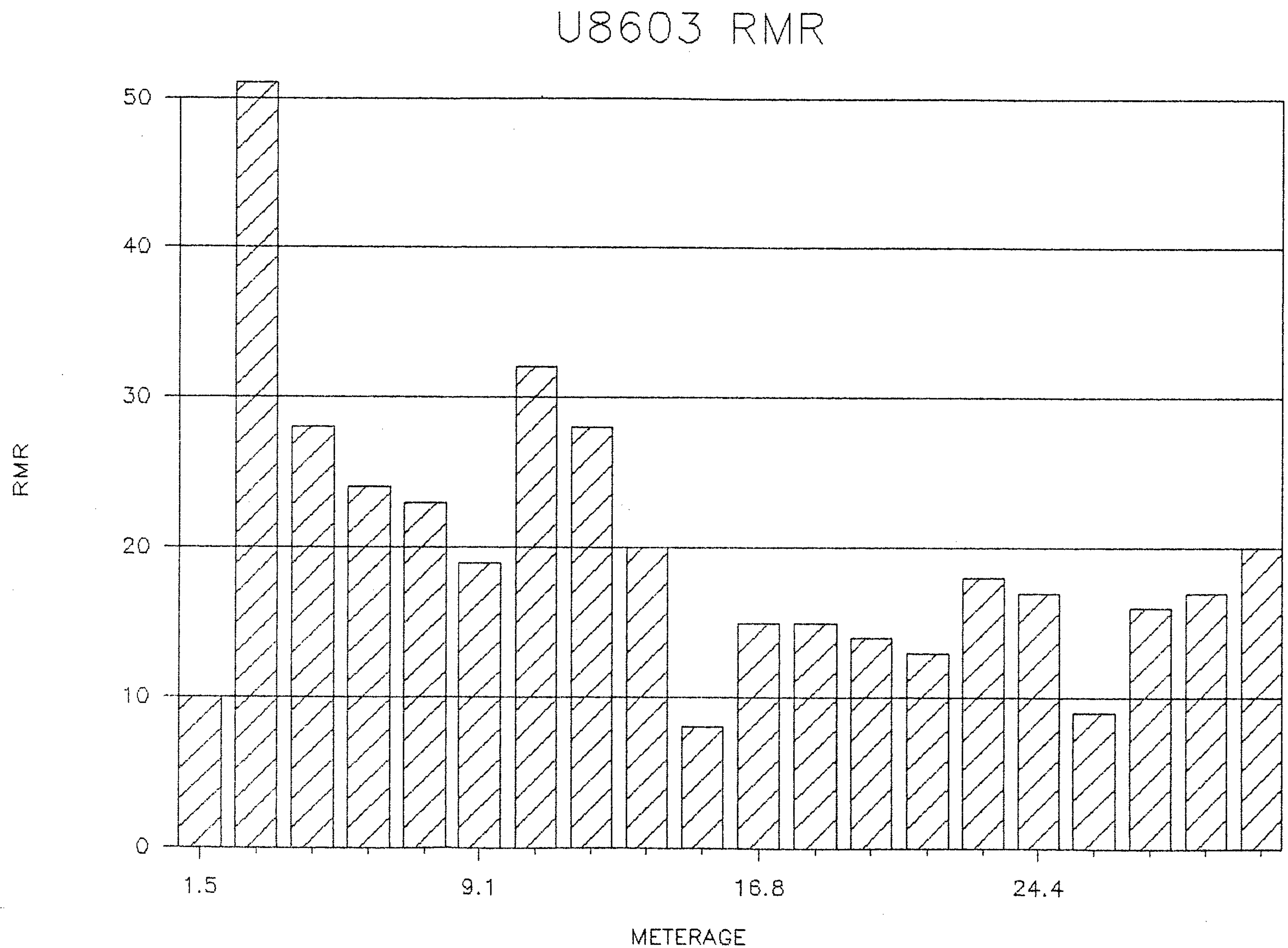
AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

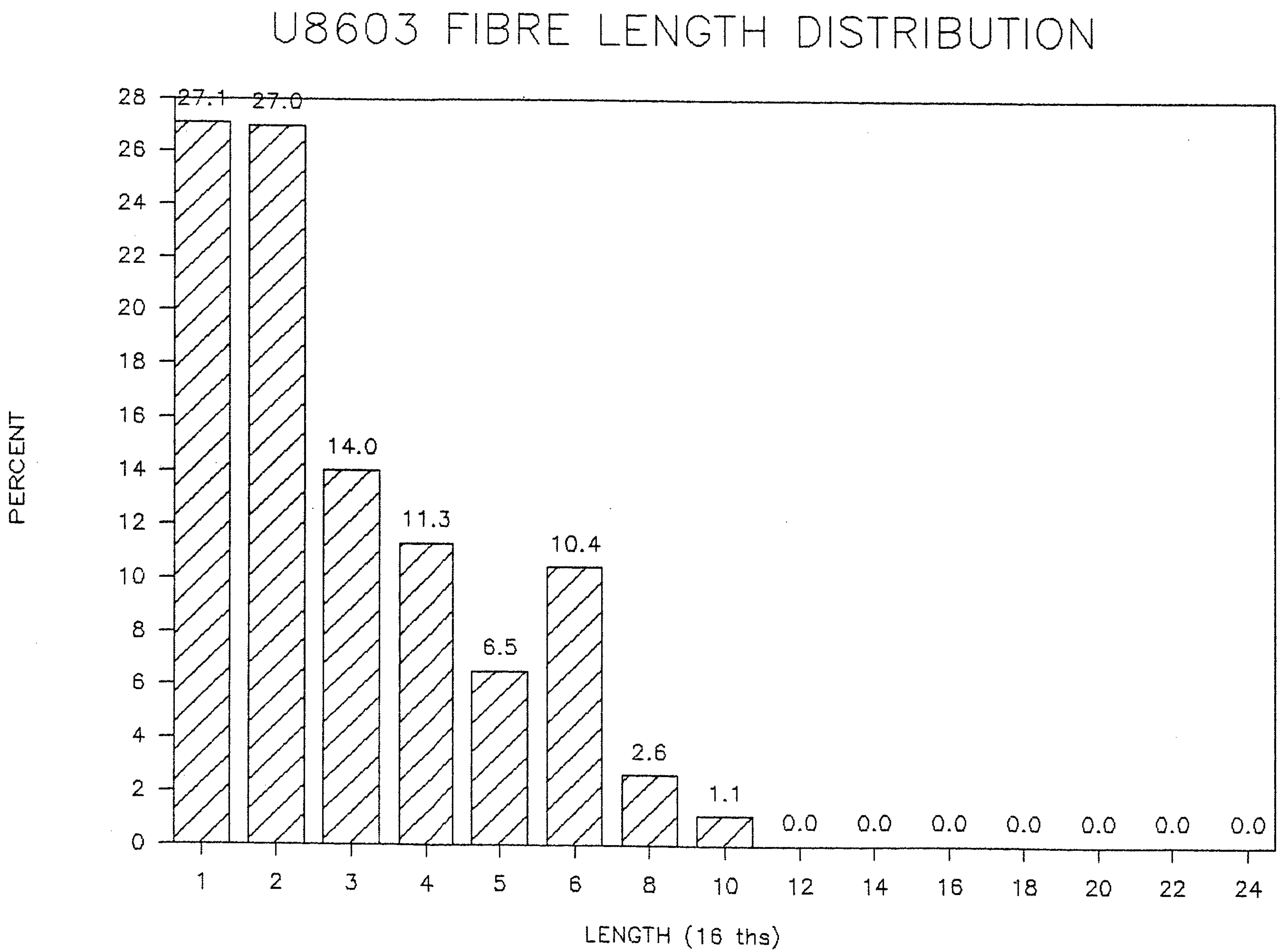
TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
1.5	1.5	10	5	3.5	1	2.5	0	0	0	0	0	0	0	0	0	0	0	25	3.68
3.0	1.5	53	6	3.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	22	3.24
4.6	1.5	28	4	2.5	0.5	0	1	1.5	0.5	0	0	0	0	0	0	0	0	28.5	4.19
6.1	1.4	24	8.5	0.5	0.5	2.5	0	0.5	0	0	0	0	0	0	0	0	0	24	3.84
7.6	1.5	23	7.5	2	3	0	1	1	0	0	0	0	0	0	0	0	0	31.5	4.63
9.1	1.5	19	7	5	0.5	1	0.5	1.5	0	0	0	0	0	0	0	0	0	34	5.11
10.7	1.5	32	4.5	1	2.5	1.5	0	1	0	0	0	0	0	0	0	0	0	26	3.82
12.2	1.5	28	7	3.5	1.5	0.5	0.5	0.5	1	0.5	0	0	0	0	0	0	0	39	5.74
13.7	1.5	20	9.5	8	1.5	0	0	1	0	0	0	0	0	0	0	0	0	36	5.52
15.2	1.5	8	12.5	3	1	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	38	5.59
16.8	1.5	15	12.5	7.5	1	0	0	0.5	0	0	0	0	0	0	0	0	0	33.5	5.14
18.3	1.5	15	5.5	4	1	0.5	0	0	0	0	0	0	0	0	0	0	0	18.5	2.78
19.8	1.2	14	6.5	1	0.5	1	0	0	0	0	0	0	0	0	0	0	0	14	2.64
21.3	1.3	13	2.5	2.5	2	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.36
22.9	1.5	18	8.5	8	2	1	0.5	0	0	0	0	0	0	0	0	0	0	37	5.45
24.4	1.5	17	8	5.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	26.5	3.90
25.9	1.5	9	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.73
27.4	1.5	16	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.22
29.0	1.4	17	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.31
30.2	1.5	20	2	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.66

EOH

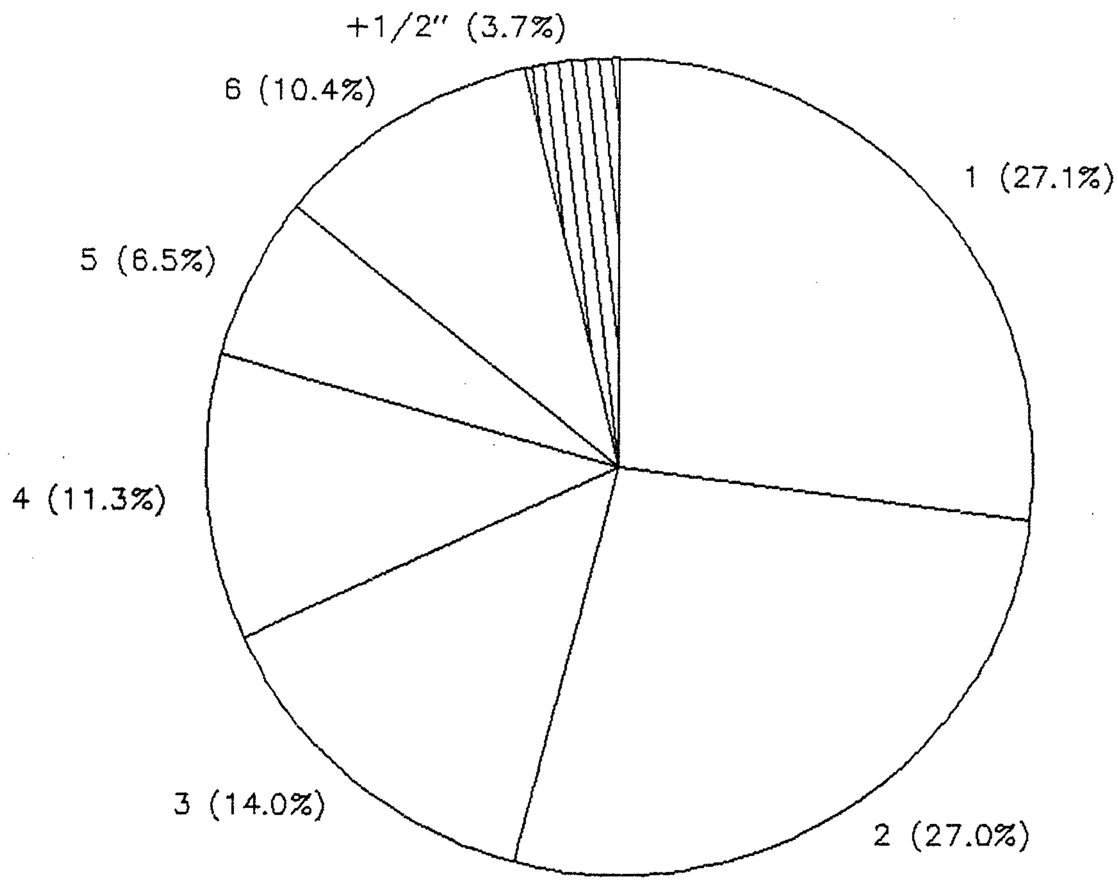

U8603 CCRG
CCRG (%)
6
5
4
3
2
1
0
1.5
9.1
16.8
24.4
METERAGE



U8603 RMR
RMR
50
40
30
20
10
0
1.5
9.1
16.8
24.4
METERAGE


U8603 FIBRE LENGTH DISTRIBUTION
PERCENT
LENGTH (16 ths)
27.1
27.0
14.0
11.3
6.5
10.4
2.6
1.1
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0
2
4
6
8
10
12
14
16
18
20
22
24
26
28
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24

U8603 FIBRE DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDame | HOLE U86-4 | DEPTH 160.93

AZIMUTH 65.7° | INCLINATION -1.8° | SECTION 6649

LATITUDE 6651.0N | DEPARTURE 7605.9E | ELEVATION 1415.07

STARTED Aug. 6 | FINISHED Aug. 13 | LOGGED by I. Lyn date

LEGEND	
W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH m	DESCRIPTION	VISUAL LOG
0.3	21.34		Serpentinite, medium dark green, with fibre veins, occasional	
			minor broken and gouge zones.	
21.34	27.4		Fault zone, cleaved and broken Serpentinite.	
27.4	42.7		Serpentinite, sparse fibre.	
			30.5 - 35 Broken, Fault zone	
42.7	54.8		Fault zone, Broken with occasional gouges	
			Minor fibre	
54.8	67		Fibre bearing, occasional minor faults	
67	81		Fault Zone, Broken and Gouge	
			74 m reduced HQ to NQ	
81	121		Dark green, Talcy, minor fibre, scattered minor shears	
121	124.4		Fault Zone, cleaved and gouge	
124.4	160.9		Dark green, becomes medium green, fibre bearing beyond	
			129 m, competent, few joints.	
160.9			E.O.H.	

DDH U 8604

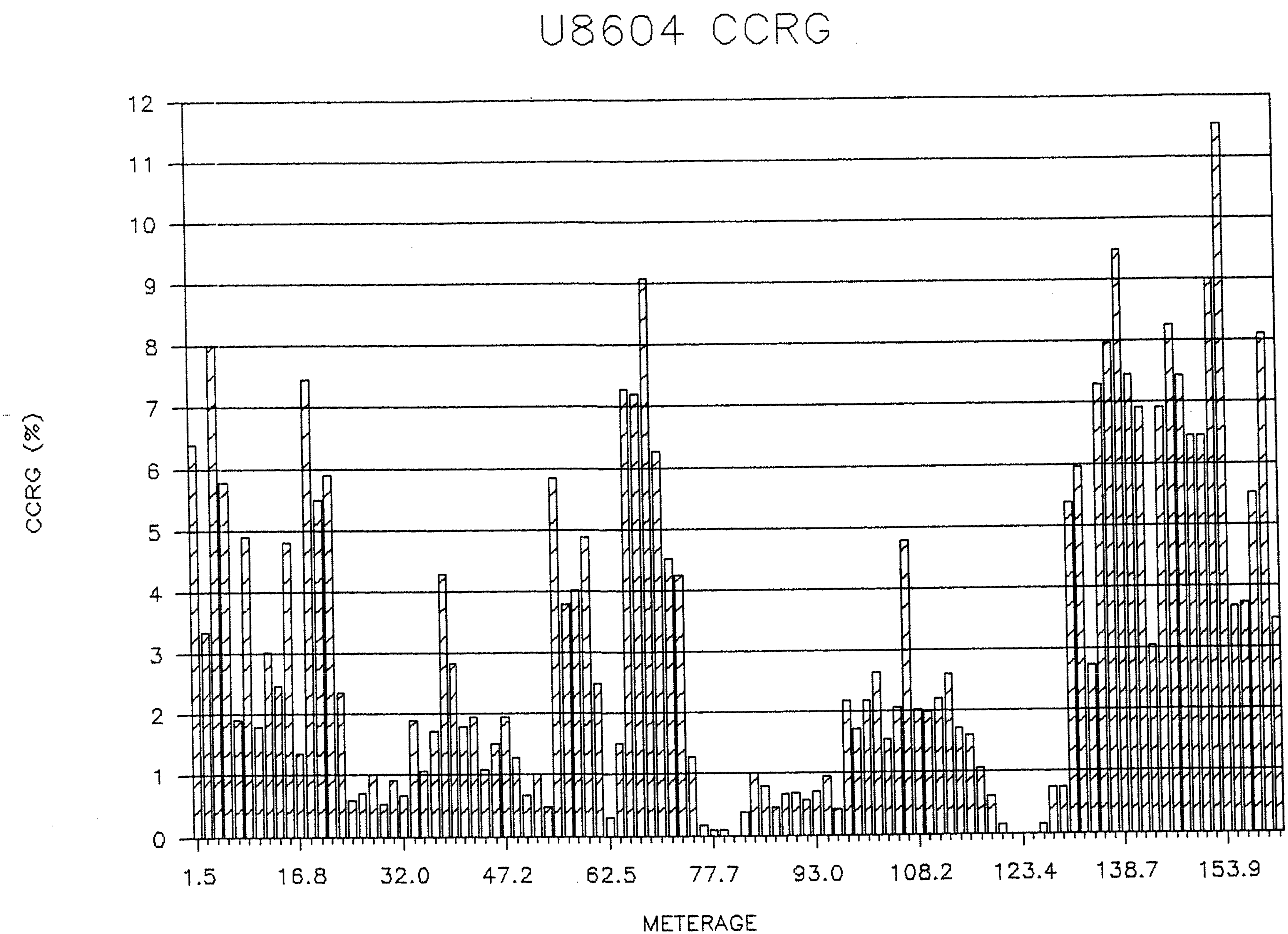
AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

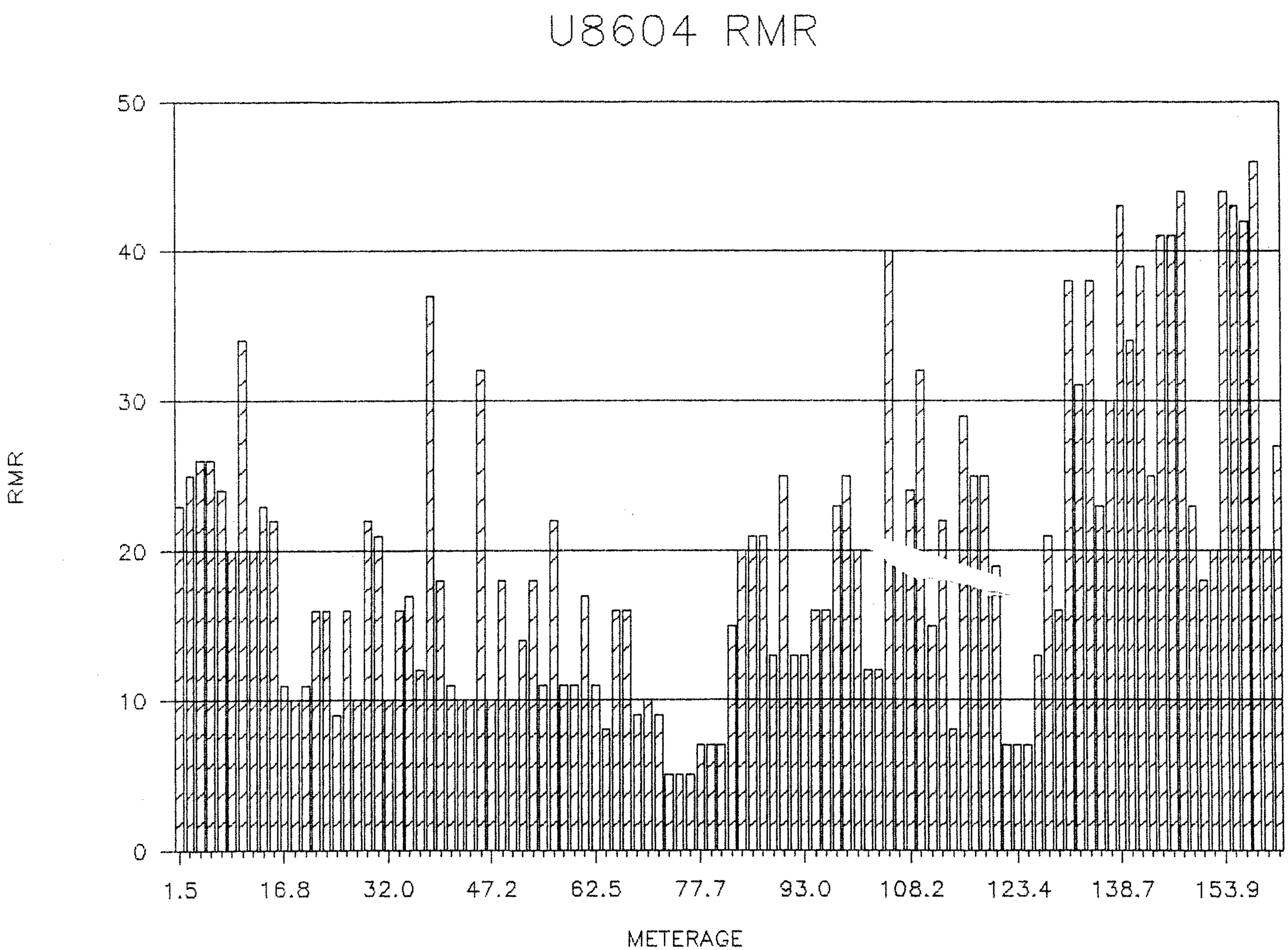
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.0	1.5	1.2	23	4.5	2.5	1	0.5	0.5	0	0.5	0	1	0	0	0	0	0	0	33	6.39
1.5	3.0	1.5	25	6.5	0	1	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	22	3.34
3.0	4.6	1.5	26	8	6.5	1	0.5	1	1	2	0	0	0	0	0	0	0	0	53	8.00
4.6	6.1	1.3	26	9	3	0	0	0.5	0	0.5	0	0.5	0.5	0	0	0	0	0	34.5	5.77
6.1	7.6	1.5	24	5.5	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	13	1.91
7.6	9.1	1.3	20	7	4	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	28.5	4.91
9.1	10.7	1.5	34	6	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	12	1.79
10.7	12.2	1.5	20	6	5.5	1	0	0	0	0	0	0	0	0	0	0	0	0	20	3.02
12.2	13.7	1.5	23	7	1	0.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	16.5	2.46
13.7	15.2	1.4	22	5	1.5	1.5	1.5	0	0.5	0.5	0.5	0	0	0	0	0	0	0	30.5	4.80
15.2	16.8	1.4	11	2	1	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	8.5	1.36
16.8	18.3	1.3	10	6.5	4.5	4	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	43	7.45
18.3	19.8	1.4	11	8.5	3.5	2.5	0	0.5	1.5	0	0	0	0	0	0	0	0	0	34.5	5.49
19.8	21.3	1.5	16	8.5	3.5	2.5	1.5	1	1	0	0	0	0	0	0	0	0	0	40	5.89
21.3	22.9	1.2	16	6.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	2.34
22.9	24.4	1.4	9	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.57
24.4	25.9	1.3	16	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.69
25.9	27.4	1.5	10	4	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.00
27.4	29.0	1.5	22	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.53
29.0	30.5	1.5	21	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.90
30.5	32.0	1.4	10	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.65
32.0	33.5	1.5	16	5.5	0.5	1	0	0	0.5	0	0	0	0	0	0	0	0	0	12.5	1.87
33.5	35.1	1.5	17	4	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.05
35.1	36.6	1.5	12	9	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11.5	1.71
36.6	38.1	1.5	37	4	2.5	0.5	2.5	1	0.5	0	0	0	0	0	0	0	0	0	28.5	4.28
38.1	39.6	1.4	18	5	2	1	0	0.5	0.5	0	0	0	0	0	0	0	0	0	17.5	2.83
39.6	41.1	1.4	11	6	0.5	0	1	0	0	0	0	0	0	0	0	0	0	0	11	1.79
41.1	42.7	1.4	10	6	3	0	0	0	0	0	0	0	0	0	0	0	0	0	12	1.94
42.7	44.2	1.4	10	4	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.09
44.2	45.7	1.5	32	5	1	1	0	0	0	0	0	0	0	0	0	0	0	0	10	1.50
45.7	47.2	1.2	10	6	0	1.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.94
47.2	48.8	1.3	18	3	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.26
48.8	50.3	1.4	10	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.65
50.3	51.8	1.4	14	2.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.00
51.8	53.3	1.4	18	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	3	0.48
53.3	54.9	1.5	11	8.5	2.5	4	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	38.5	5.84
54.9	56.4	1.5	22	8	2	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	25	3.79
56.4	57.9	1.5	11	10.5	3	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	26.5	4.02
57.9	59.4	1.5	11	8	3	1.5	1	0	0	0.5	0	0.5	0	0	0	0	0	0	32.5	4.88
59.4	61.0	1.4	17	6.5	0.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	16	2.48
61.0	62.5	1.5	11	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.29
62.5	64.0	1.5	8	4	0	2	0	0	0	0	0	0	0	0	0	0	0	0	10	1.50
64.0	65.5	1.4	16	6	2.5	2.5	0	0.5	2.5	0.5	0.5	0	0	0	0	0	0	0	45	7.28
65.5	67.1	1.4	16	11.5	2.5	2	1	0.5	1	0	1	0	0	0	0	0	0	0	45	7.20
67.1	68.6	1.4	9	12	6	6	1.5	0	0	0.5	0.5	0	0	0	0	0	0	0	57	9.07
68.6	70.1	1.4	10	13	5.5	4	1	0	0	0	0	0	0	0	0	0	0	0	40	6.26
70.1	71.6	1.5	9	7	4	1.5	1	0	1	0	0	0	0	0	0	0	0	0	29.5	4.52
71.6	73.2	1.3	5	5.5	3.5	3	1	0	0	0	0	0	0	0	0	0	0	0	25.5	4.24
73.2	74.7	1.5	5	1.5	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	8.5	1.27
74.7	76.2	1.4	5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
76.2	77.7	1.4	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.07
77.7	79.2	1.2	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09

79.2	80.8	1.4	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
80.8	82.3	1.5	15	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.37
82.3	83.8	1.5	20	3.5	0	1	0	0	0	0	0	0	0	0	0	0	0	0	6.5	0.99
83.8	85.3	1.4	21	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.79
85.3	86.9	1.5	21	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.45
86.9	88.4	1.5	13	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.66
88.4	89.9	1.5	25	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.67
89.9	91.4	1.4	13	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.56
91.4	93.0	1.4	13	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.69
93.0	94.5	1.4	16	4	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	6	0.96
94.5	96.0	1.4	16	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
96.0	97.5	1.5	23	8.5	1	0	1	0	0	0	0	0	0	0	0	0	0	0	14.5	2.17
97.5	99.1	1.4	25	6.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11	1.71
99.1	100.6	1.5	20	9.5	1	1	0	0	0	0	0	0	0	0	0	0	0	0	14.5	2.17
100.6	102.1	1.4	12	12.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	16.5	2.64
102.1	103.6	1.4	12	6	2	0	0	0	0	0	0	0	0	0	0	0	0	0	10	1.55
103.6	105.2	1.5	40	7	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	13.5	2.07
105.2	106.7	1.4	20	5.5	3	3.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	30.5	4.77
106.7	108.2	1.4	24	6.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	13	2.01
108.2	109.7	1.4	32	6	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	12	1.98
109.7	111.3	1.4	15	3	2	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	14	2.19
111.3	112.8	1.5	22	2.5	4.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	17	2.59
112.8	114.3	1.5	8	4.5	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	11.5	1.72
114.3	115.8	1.5	29	7.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.59
115.8	117.3	1.5	25	3	2	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.07
117.3	118.9	1.5	25	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.60
118.9	120.4	1.5	19	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
120.4	121.9	1.4	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
121.9	123.4	1.3	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
123.4	125.0	1.4	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
125.0	126.5	1.5	13	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.14
126.5	128.0	1.5	21	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.74
128.0	129.5	1.5	16	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.73
129.5	131.1	1.5	38	15.5	4.5	1	1	1	0	0	0	0	0	0	0	0	0	0	36.5	5.37
131.1	132.6	1.5	31	11.5	4.5	2	0.5	0.5	1.5	0	0	0	0	0	0	0	0	0	40	5.95
132.6	134.1	1.5	38	6.5	2.5	1	1	0	0	0	0	0	0	0	0	0	0	0	18.5	2.72
134.1	135.6	1.5	23	9.5	7.5	5	2	0	0	0	0	0	0	0	0	0	0	0	47.5	7.28
135.6	137.2	1.5	30	15	6.5	3	1	0.5	1.5	0	0	0	0	0	0	0	0	0	52.5	7.97
137.2	138.7	1.5	43	11	5.5	3.5	1.5	0	1.5	0	1.5	0	0	0	0	0	0	0	62.5	9.49
138.7	140.2	1.4	34	7.5	2	4.5	5	0.5	0	0	0	0	0	0	0	0	0	0	47.5	7.44
140.2	141.7	1.5	39	11	6.5	2	1.5	0	1	0.5	0	0	0	0	0	0	0	0	46	6.91
141.7	143.3	1.5	25	11.5	3	1	0	0	0	0	0	0	0	0	0	0	0	0	20.5	3.05
143.3	144.8	1.5	41	16.5	5.5	3	2.5	0	0	0	0	0	0	0	0	0	0	0	46.5	6.91
144.8	146.3	1.5	41	5.5	3	1.5	3.5	1.5	0.5	0.5	0.5	0.5	0	0	0	0	0	0	55.5	8.25
146.3	147.8	1.5	44	17	7	3.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	50.5	7.43
147.8	149.4	1.5	23	8.5	6	3	2	1	0	0	0	0	0	0	0	0	0	0	42.5	6.45
149.4	150.9	1.5	18	9.5	3.5	1	1	0.5	2	0.5	0	0	0	0	0	0	0	0	42	6.44
150.9	152.4	1.5	20	10.5	7	2	2	1	1.5	1	0	0	0	0	0	0	0	0	60.5	9.00
152.4	153.9	1.5	44	10.5	7.5	7	2	2	1.5	0.5	0	0	0	0	0	0	0	0	77.5	11.5
153.9	155.4	1.5	43	11.5	3	2.5	0	0	0	0	0	0	0	0	0	0	0	0	25	3.68
155.4	157.0	1.5	42	10	4	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	25	3.71
157.0	158.5	1.5	46	10	1.5	1	0	0.5	0.5	0	1	0.5	0	0	0	0	0	0	37.5	5.52
158.5	160.0	1.5	20	10	4.5	3.5	2	0.5	2.5	0	0	0	0	0	0	0	0	0	55	8.10
160.0	160.9	1.5	27	5.5	4	2	1	0	0	0	0	0	0	0	0	0	0	0	23.5	3.46

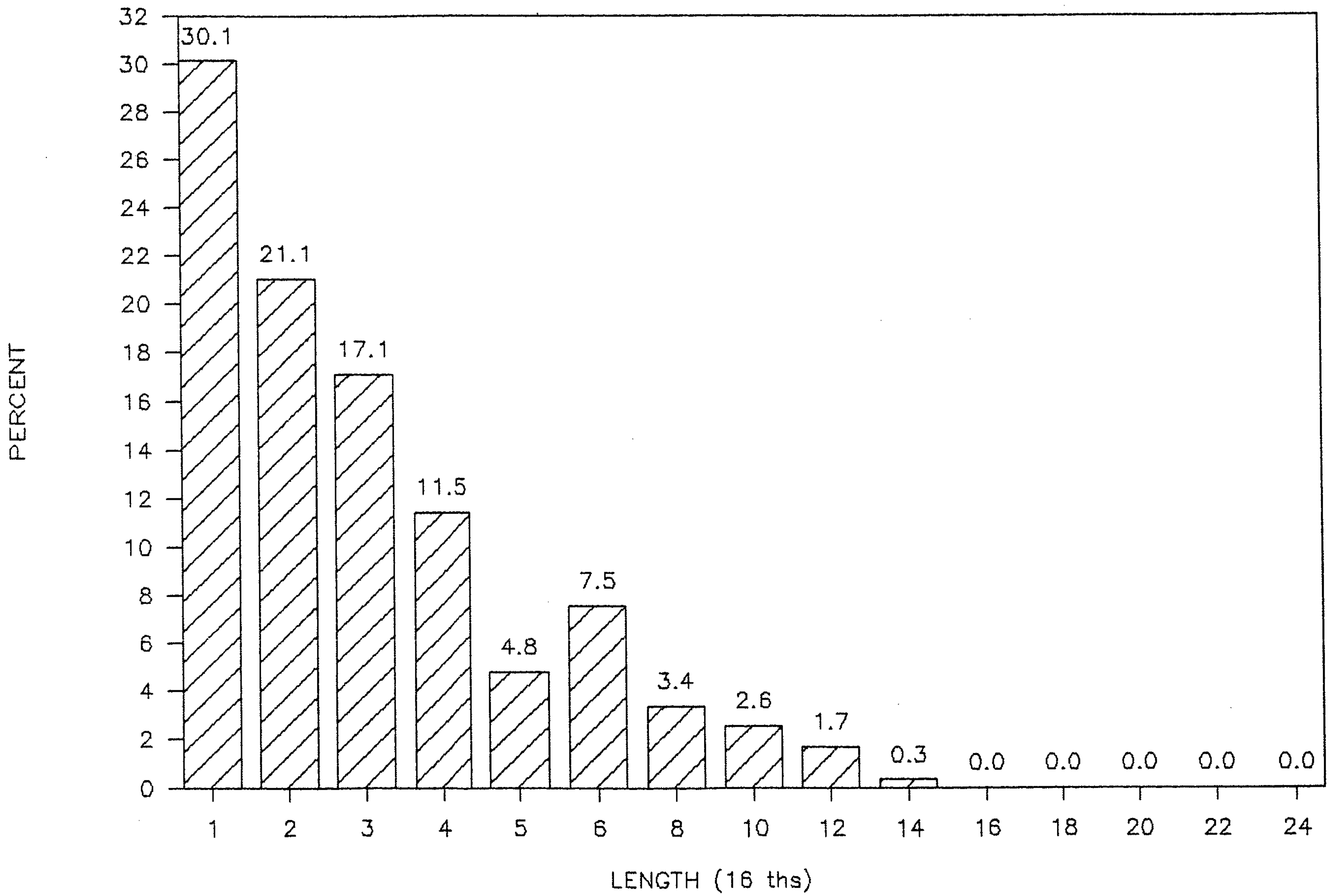
EOH



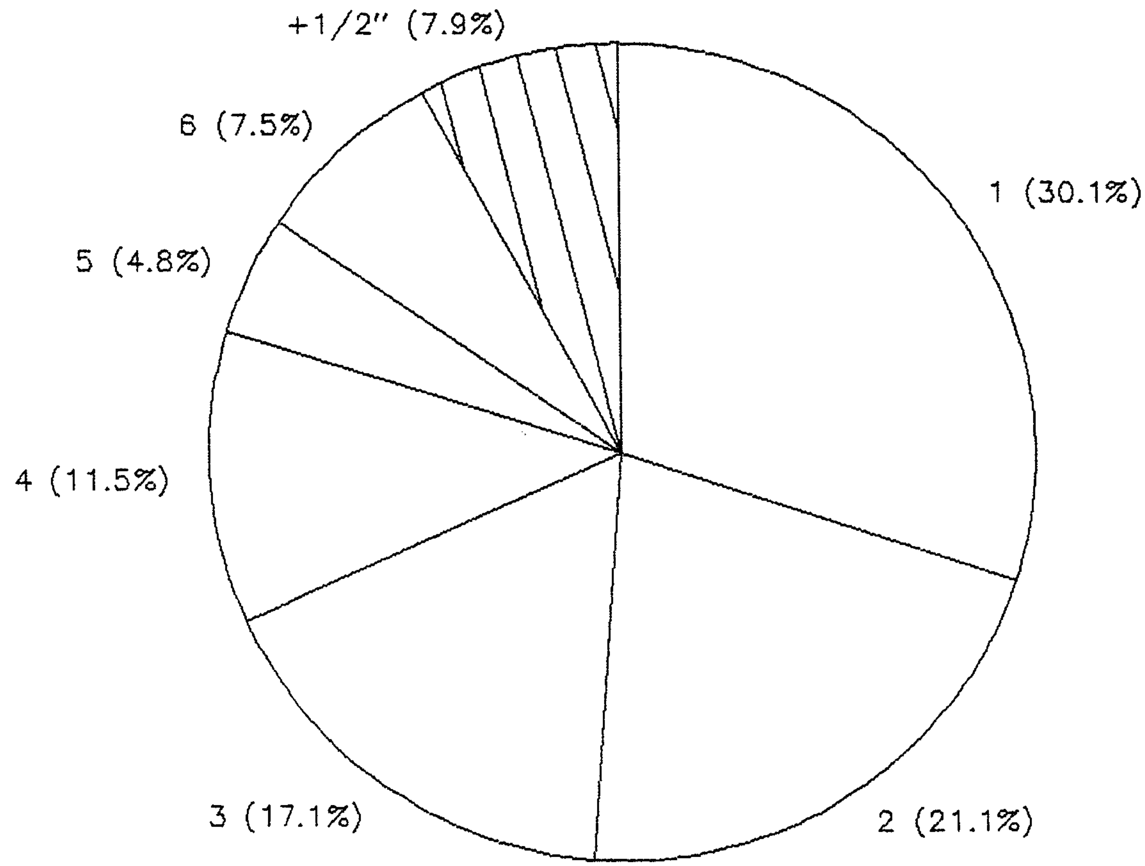
U8604 CCRG
CCRG (%)
0
1
2
3
4
5
6
7
8
9
10
11
12
1.5
16.8
32.0
47.2
62.5
77.7
93.0
108.2
123.4
138.7
153.9
METERAGE


U8604 RMR
RMR
50
40
30
20
10
0
1.5
16.8
32.0
47.2
62.5
77.7
93.0
108.2
123.4
138.7
153.9
METERAGE

U8604 FIBRE DISTRIBUTION



U8604 FIBRE DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDame HOLE U86-5 DEPTH 92.35

AZIMUTH 0 INCLINATION -90 SECTION 6649N

LATITUDE 6649.9N DEPARTURE 7603.8E ELEVATION 1413.8

STARTED Aug.14 FINISHED Aug. 20 LOGGED by I. Lyn date

LEGEND	
W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH m	DESCRIPTION	VISUAL LOG
.6	23.2		Serpentinite, Medium green, low grade fibre bearing.	
			Minor shears 6.2-10, 17 -23	
23.2	30.5		Fault zone, 23.9 - 25.9 gouge, otherwise broken with minor gouge	
30.5	55.8		Light green, good fibre, mottled appearance	
55.8	64		Fault zone, broken with gouges	
64	83.2		Light green, good fibre, gradually become more broken and	
			faulted to bottom of section.	
83.2	84.7		Fault zone, gouge	
84.7	92.35		Medium green, broken, minor shears	
			85.4 - 86.3, 89.3 - 91.4	
92.35			E.O.H.	

DDH U 8605

AVERAGE OF TWO COUNTS

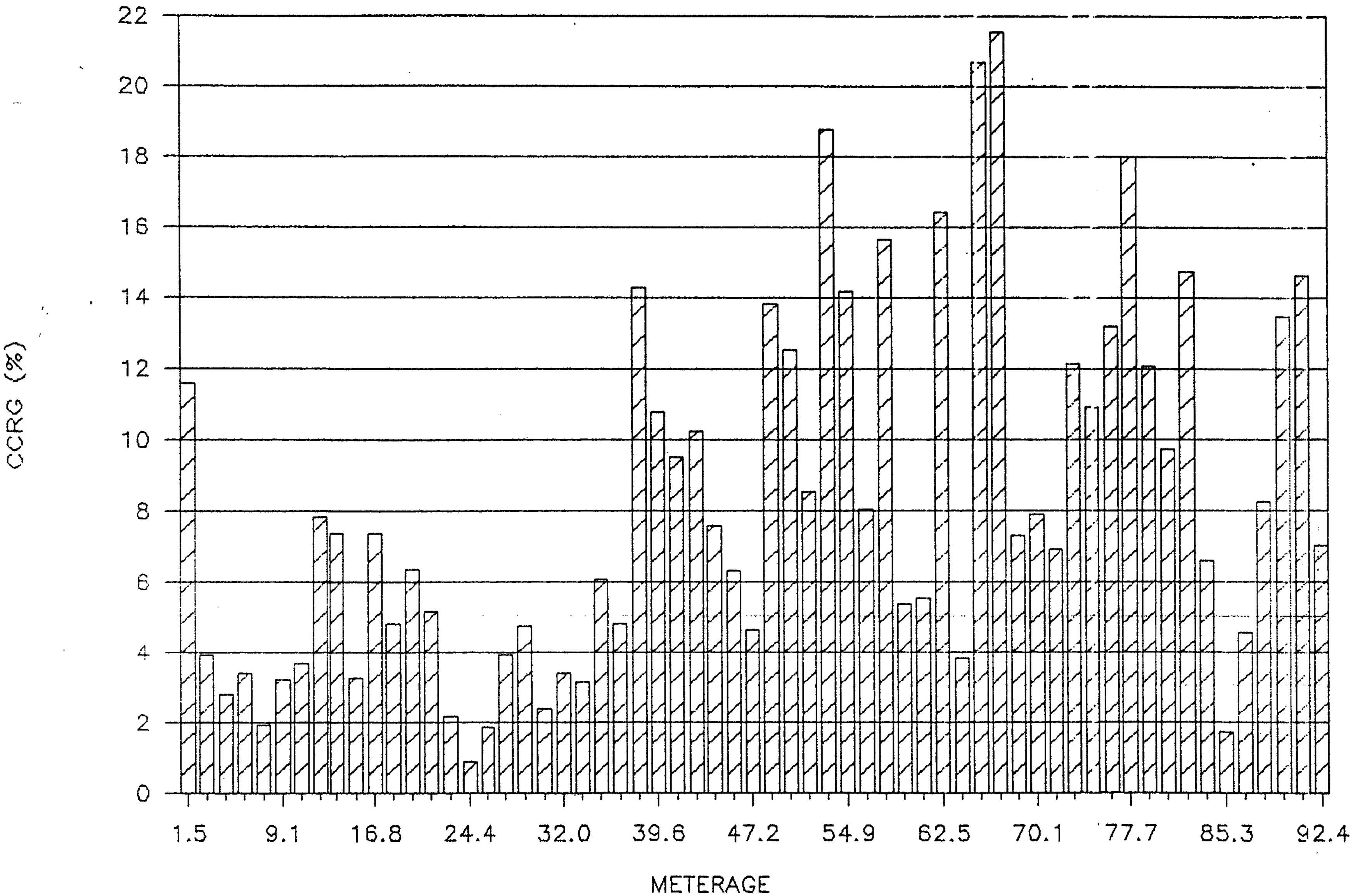
Number of fibre veins counted per 16th category

FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.0	1.5	1.3	19	4.5	3.5	1	1	1	1	0.5	1	1	1	0	0	0	0	0	69.5	12.0
1.5	3.0	1.5	17	4.5	3.5	0.5	0.5	1.5	2	0	0	0	0	0	0	0	0	0	34.5	5.18
3.0	4.6	1.5	12	14	3.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	25.5	3.75
4.6	6.1	1.5	16	8	2.5	1	2	0	0	0	0	0	0	0	0	0	0	0	24	3.53
6.1	7.6	1.5	10	7	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	16.5	2.48
7.6	9.1	1.4	19	6.5	2.5	1.5	0.5	0.5	0	1	0.5	0	0	0	0	0	0	0	33.5	5.30
9.1	10.7	1.5	10	9	5.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	27.5	4.13
10.7	12.2	1.5	25	12.5	8	3.5	2	0.5	1	0	0	0	0	0	0	0	0	0	55.5	8.34
12.2	13.7	1.4	21	6.5	3.5	2.5	0.5	0	0.5	0.5	0	0	0	1	0	0	0	0	46	7.20
13.7	15.2	1.5	26	6.5	2.5	1	1.5	1	0	0	0	0	0	0	0	0	0	0	25.5	3.83
15.2	16.8	1.5	27	5.5	2.5	2.5	0	0.5	1.5	0	1	0	0	1	0	0	0	0	55.5	8.17
16.8	18.3	1.4	10	5.5	4	1.5	0.5	0.5	0.5	0	0	0.5	0.5	0	0	0	0	0	38.5	6.23
18.3	19.8	1.4	10	10	4	2.5	1	1.5	0.5	0.5	0	0	0	0	0	0	0	0	44	6.96
19.8	21.3	1.6	9	5.5	3.5	3.5	1.5	0	1.5	1	0	0.5	0	0	0	0	0	0	52	7.50
21.3	22.9	1.2	16	1	0.5	0	1.5	0	0	0.5	0	0	0	0	0	0	0	0	12	2.18
22.9	24.4	1.3	12	3.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.60
24.4	25.9	1.5	21	7	1.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	22	3.37
25.9	27.4	1.3	20	10.5	4	2	2	0.5	0	0	0	0	0	0	0	0	0	0	35	5.99
27.4	29.0	1.4	11	10.5	5	2.5	2	0.5	0.5	0	0	0	0	0	0	0	0	0	41.5	6.64
29.0	30.5	1.5	17	6.5	1.5	0.5	0.5	0	0.5	1	0	0	0	0	0	0	0	0	24	3.57
30.5	32.0	1.5	25	5.5	4	0.5	1	0	1	0	0	0	0	0	0	0	0	0	25	3.71
32.0	33.5	1.5	27	2.5	2.5	2	1	0	0	0	0	0	0	0	0	0	0	0	17.5	2.65
33.5	35.1	1.4	19	12.5	5.5	1.5	0.5	0	0	0.5	1	0	0	0	0	0	0	0	44	6.82
35.1	36.6	1.5	18	11	3.5	0.5	1	0.5	1.5	1	0	0	0	0	0	0	0	0	43	6.39
36.6	38.1	1.5	22	7	5.5	6	1.5	1	1.5	0.5	1.5	0	0.5	0	0	0	0	0	82	11.9
38.1	39.6	1.3	23	10	1.5	1	0.5	1.5	0.5	0.5	1	0	0	0	0	1	0	0	62.5	10.8
39.6	41.1	1.5	26	7	3.5	1.5	2.5	1.5	0.5	0.5	0	2	0	0	0	0	0	0	67	9.96
41.1	42.7	1.5	12	15	2.5	3.5	2	0.5	2	1.5	0.5	0	0	0	0	0	0	0	70	10.2
42.7	44.2	1.5	20	5.5	5	4	0.5	1	1	0	0	0	1	0	0	0	0	0	54.5	8.36
44.2	45.7	1.5	27	5	1.5	0.5	0	0.5	1	0.5	1.5	0.5	0	0	0	0	0	0	43	6.46
45.7	47.2	1.5	23	7.5	3	3.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	38	5.77
47.2	48.8	1.5	24	7	2	3	2	2	2	0.5	0	0.5	0.5	0	0	0.5	0.5	0	88	12.8
48.8	50.3	1.5	18	8.5	5	2	2	1	2.5	4	0	0	0	0	0	0	0	0	84.5	12.7
50.3	51.8	1.3	24	2	2.5	1	0.5	0.5	0	0.5	0.5	0.5	0	0	0.5	0.5	0	0	48.5	8.11
51.8	53.3	1.5	27	5	1.5	1.5	1.5	1.5	2	1	0	0.5	0	0	0	0	0.5	0.5	75	11.2
53.3	54.9	1.4	21	9	1.5	3	1.5	1	3	2	0	0	0	0	0	0	0	0	66	10.5
54.9	56.4	0.8	25	3	1.5	1	1.5	0	0.5	0.5	0.5	0.5	0	0	0	0	0	0	33	8.83
56.4	57.9	0.8	13	4	2	2.5	2.5	0	0.5	0	0	0	0	0	0	0	0	0	28.5	8.23
57.9	59.4	1.4	9	4.5	3	0	1	1	0.5	0	0	0	0	0	0	0	0	0	22.5	3.64
59.4	61.0	1.4	10	3	23.5	0	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	57.5	9.41
61.0	62.5	1.5	8	6	6.5	3.5	2	2.5	2	0.5	1	1.5	0	1	0	0	0	0	110	16.2
62.5	64.0	1.5	9	2	1	0	0.5	0	0	0	0	0	0.5	0.5	0	0	0	0	21	3.09
64.0	65.5	1.5	21	8	3.5	3.5	4	1	0.5	2.5	1	0.5	0.5	0.5	1	0	0	0	118.5	17.4
65.5	67.1	1.4	19	11	4.5	4	3.5	3	2.5	2.5	1.5	0.5	0.5	0.5	0	0	0	0	132	21.6
67.1	68.6	1.4	22	6	3.5	1	0.5	1.5	4	0	0	0	0	0	0	0	0	0	49.5	7.75
68.6	70.1	1.5	24	2.5	3	1.5	0.5	0.5	0.5	0.5	0.5	0	1	0	0	0	0	0	43.5	6.53
70.1	71.6	1.5	12	8	3.5	1.5	1	0.5	0	0	0	1	0	0	0	0	0	0	38	5.77
71.6	73.2	1.4	10	5	1.5	2	4	1	0	1	1.5	0	0.5	0	0	0	0	0	65	10.0
73.2	74.7	1.5	15	8	3.5	3	1	1	0.5	1.5	0.5	0.5	0.5	0	0	0	0	0	66	9.92
74.7	76.2	1.5	15	9	4	2	1.5	1	1	2	0.5	0	0	0	0	0.5	0.5	0	82	12.3
76.2	77.7	1.3	5	5.5	5	1.5	3	1	2	2.5	1	0	0	1	0	0	0	0	95	16.0
77.7	79.2	1.5	11	12.5	3.5	1	1.5	2	1	2.5	0	0	0	0	0	0	0	0	64.5	9.79

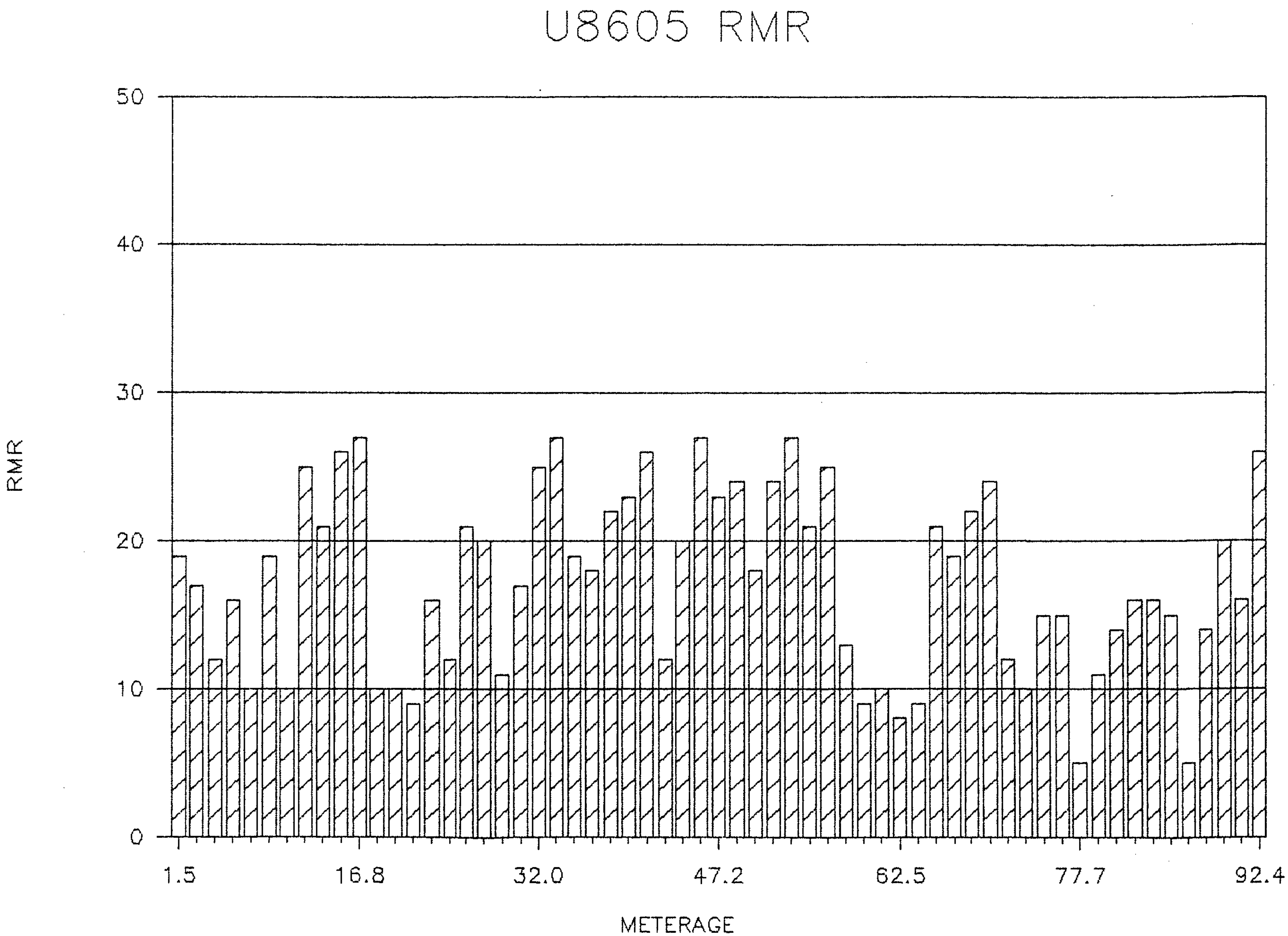
79.2	80.8	1.5	14	5	4	3	1.5	0	1.5	1.5	0.5	0.5	0.5	0	0	0	0	0	67	10.0
80.8	82.3	1.5	16	12	8.5	2.5	1.5	4	1	1	0	0	0	0	0	0	0	0	76.5	11.2
82.3	83.8	1.4	16	8	2.5	2.5	0	0	0	0.5	0	0	0	0	0	0	0	0	24.5	3.83
83.8	85.3	1.5	15	6.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	12	1.76
85.3	86.9	1.4	5	15	3.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	27.5	4.40
86.9	88.4	1.5	14	16	7	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	43	6.46
88.4	89.9	1.4	20	9.5	5	2.5	3	0	1.5	1	0.5	0	0	0	1	0	0	0	79	12.5
89.9	91.4	1.4	16	15	4	2	2.5	1	2.5	0.5	0	0.5	0	0	0	0	0.5	0	80	13.2
91.4	92.4	1.2	26	6.5	1.5	1	0	1	0	0	0.5	0	0.5	0	0	0	0	0	29.5	5.36

EOH

U8605 CCRG

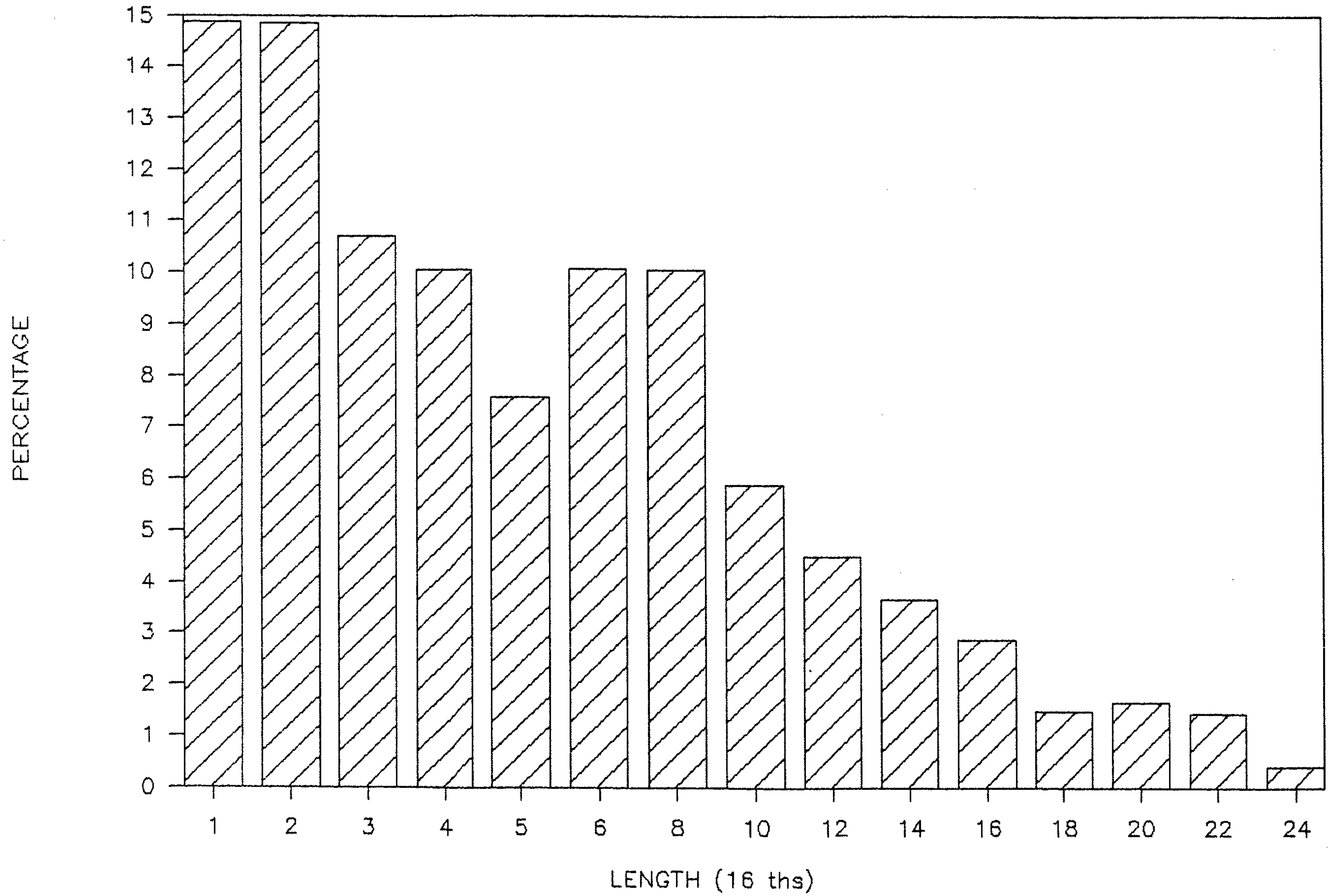


22
20
18
16
14
12
10
8
6
4
2
0
CCRG (%)
1.5
9.1
16.8
24.4
32.0
39.6
47.2
54.9
62.5
70.1
77.7
85.3
92.4
METERAGE

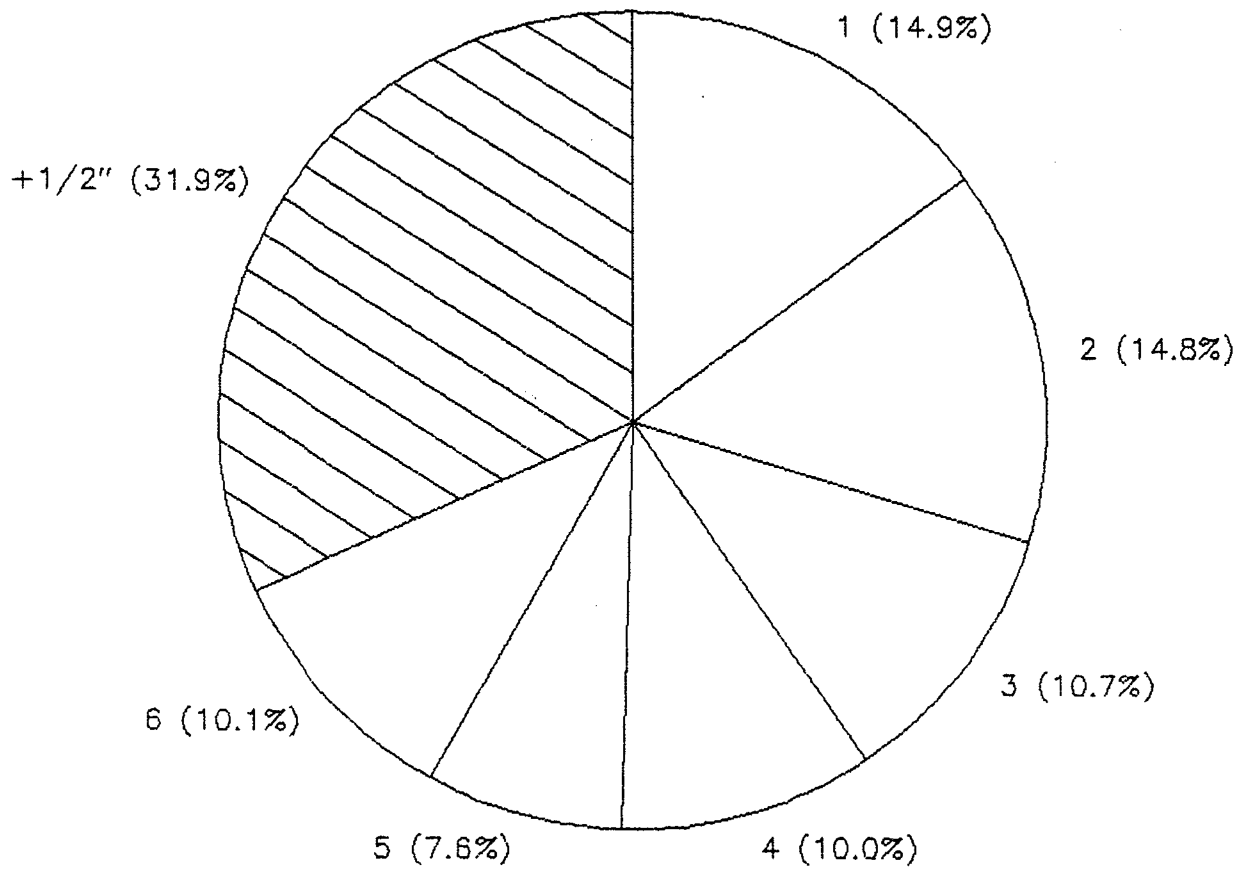


U8605 RMR
RMR
METERAGE
0
10
20
30
40
50
1.5
16.8
32.0
47.2
62.5
77.7
92.4

U8605 FIBRE LENGTH DISTRIBUTION



U8605 FIBRE DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

PROPERTY McDame HOLE - U86-6 DEPTH 16.46 m

AZIMUTH 88.75° INCLINATION +48.1° SECTION 6649N

LATITUDE 6649.75N DEPARTURE 7604.9E ELEVATION 1416.0

STARTED Aug. 21 FINISHED Aug. 22 LOGGED by W.R.E date

FROM Metres	TO	LENGTH m	DESCRIPTION	VISUAL LOG
0	16.5		Serpentinite, medium-dark green, low grade fibre	
			11.8 - 16.5 fault zone, gouge and broken	
16.5			E.O.H.	

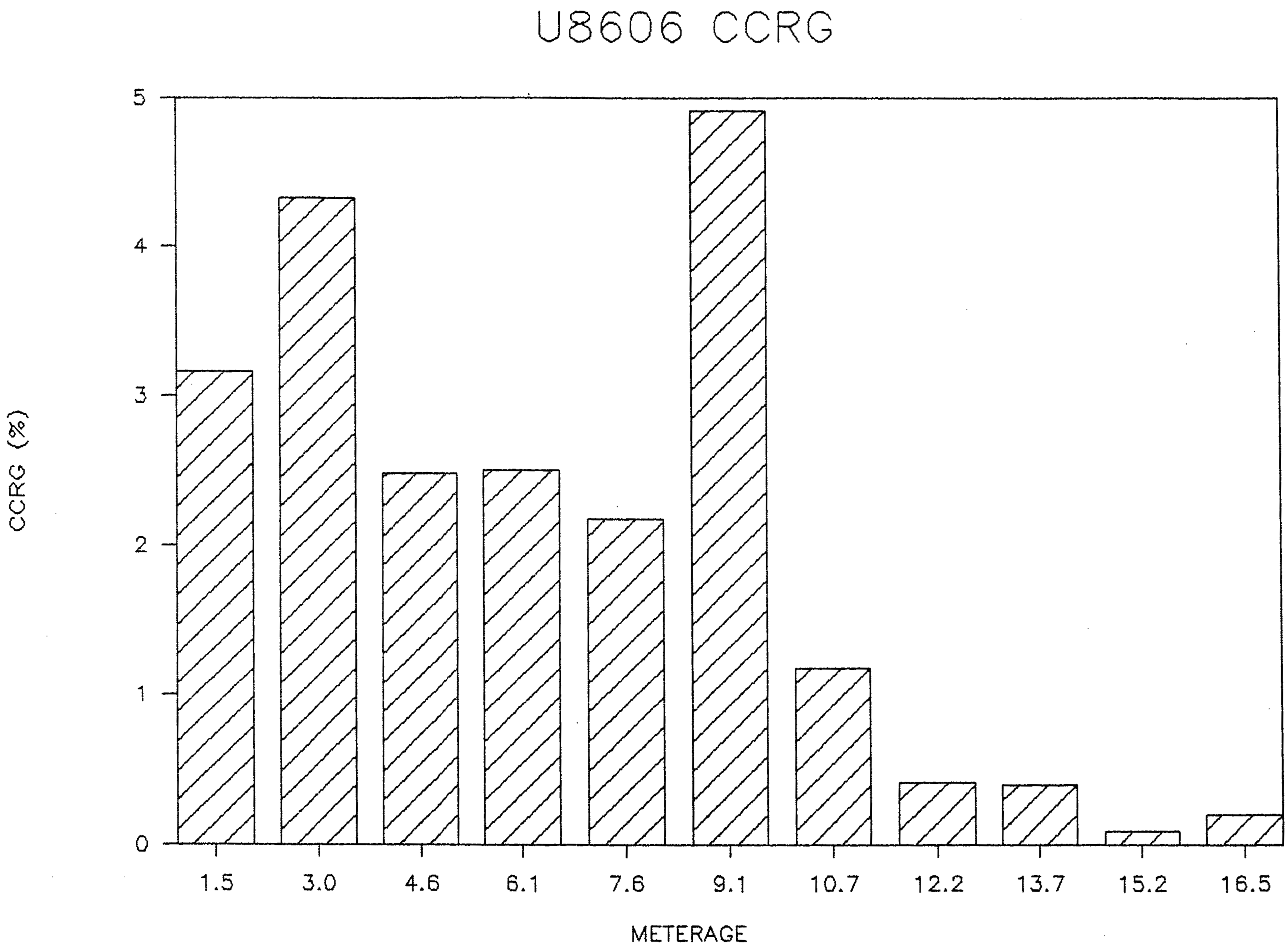
DDH U 8606

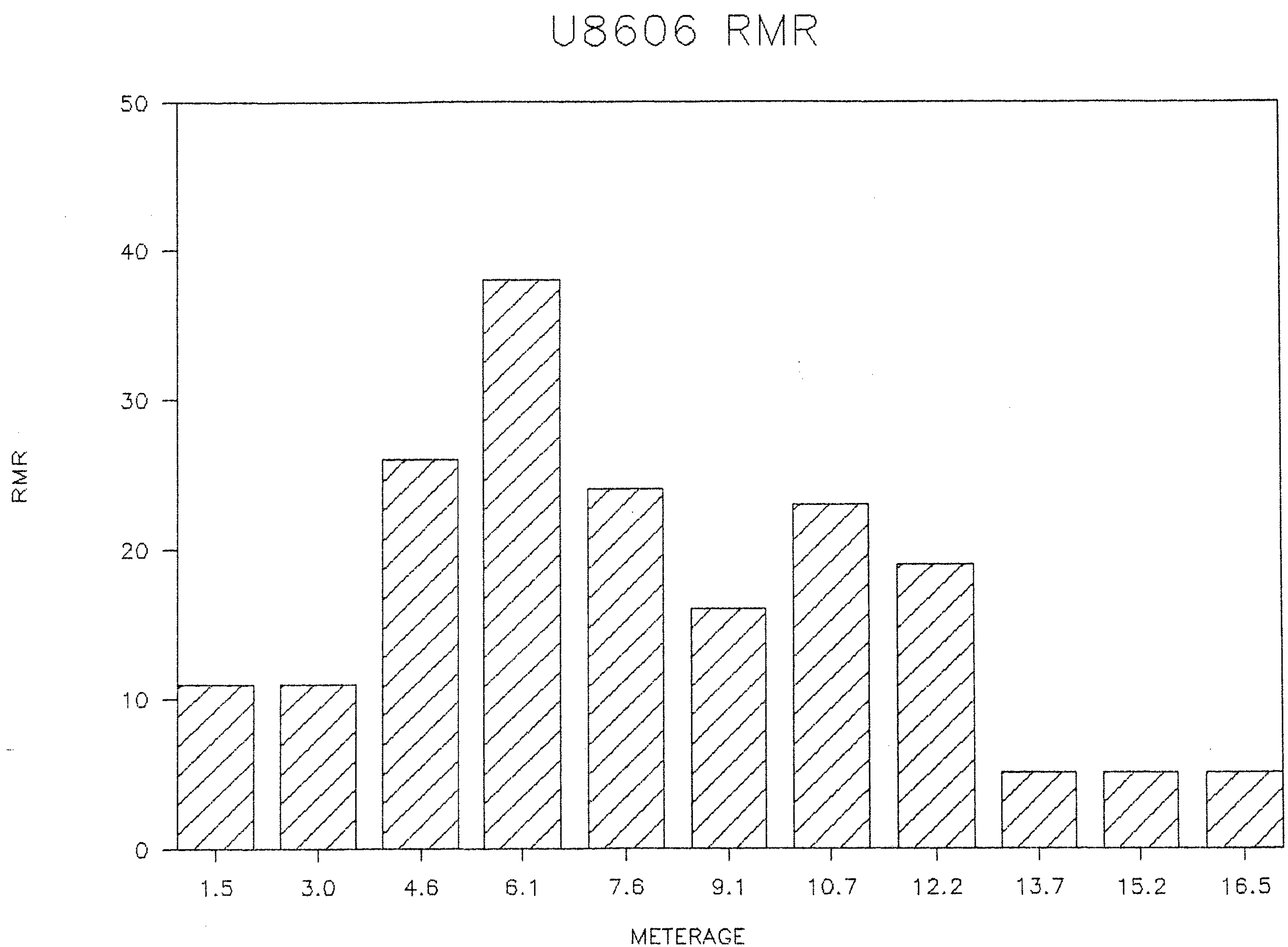
AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

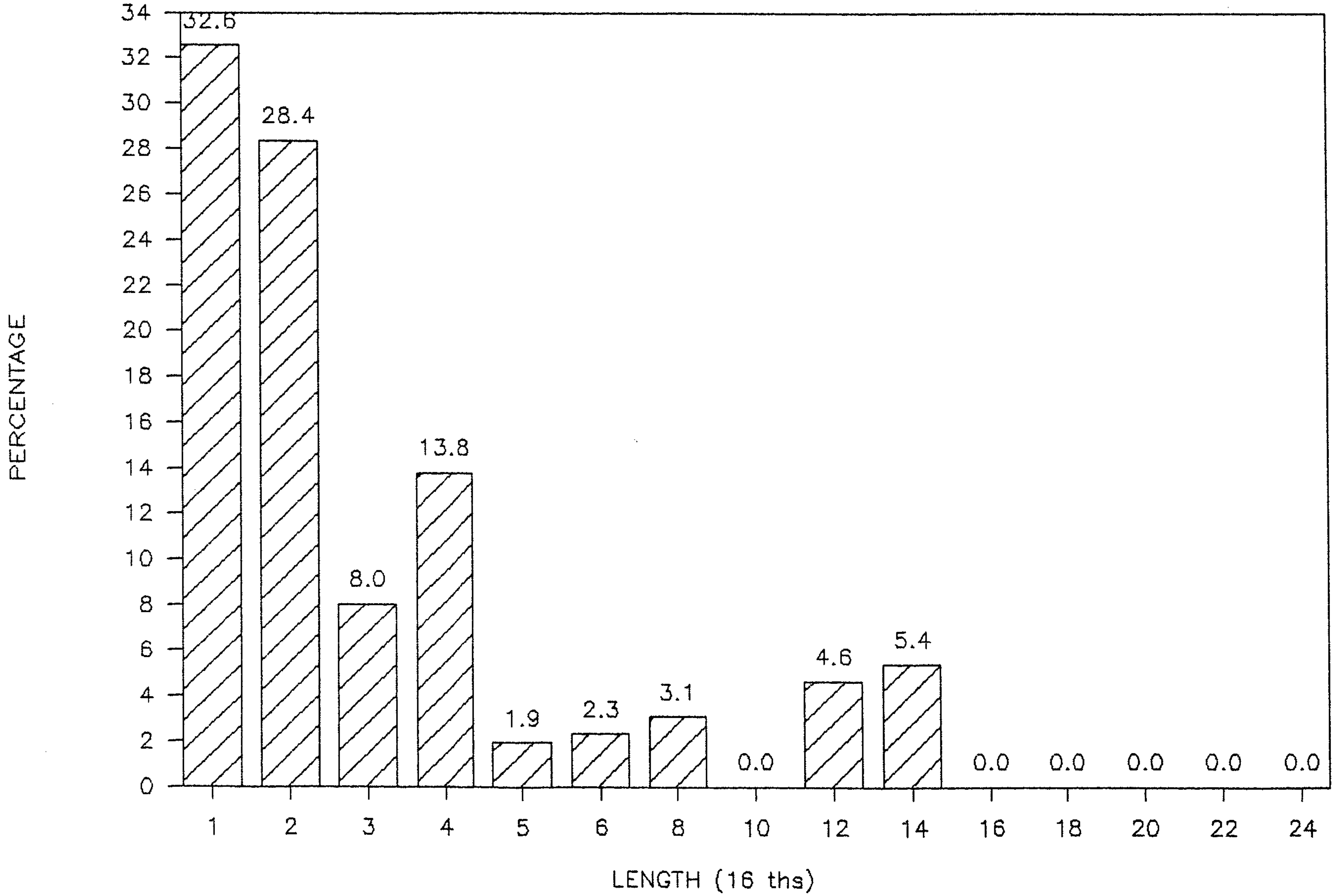
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.0	1.5	1.1	11	3	1.5	1	0.5	0	0	0.5	0	0	0	0	0	0	0	0	15	3.15
1.5	3.0	1.2	11	5.5	3.5	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	23.5	4.32
3.0	4.6	1.4	26	6	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.48
4.6	6.1	1.4	38	6.5	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	16	2.50
6.1	7.6	1.5	24	6.5	3	0	0.5	0	0	0	0	0	0	0	0	0	0	0	14.5	2.17
7.6	9.1	1.5	16	8	3	1	0.5	0	0	0	0	0.5	0.5	0	0	0	0	0	32	4.91
9.1	10.7	1.5	23	3	0.5	0	1	0	0	0	0	0	0	0	0	0	0	0	8	1.17
10.7	12.2	1.4	19	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
12.2	13.7	1.4	5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
13.7	15.2	1.3	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
15.2	16.5	0.6	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.19

EOH

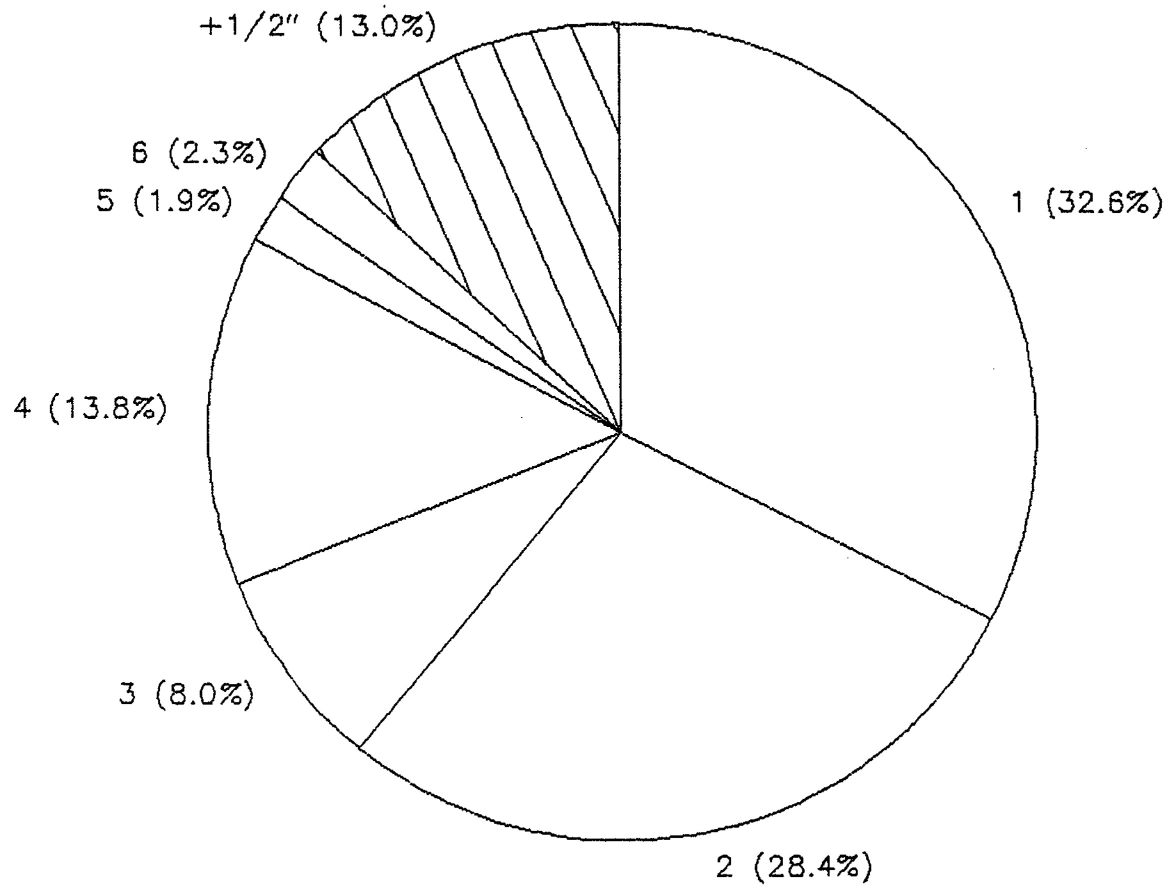

U8606 CCRG
CCRG (%)
METERAGE
0
1
2
3
4
5
1.5
3.0
4.6
6.1
7.6
9.1
10.7
12.2
13.7
15.2
16.5


U8606 RMR
RMR
50
40
30
20
10
0
1.5
3.0
4.6
6.1
7.6
9.1
10.7
12.2
13.7
15.2
16.5
METERAGE

U8606 FIBRE DISTRIBUTION



U8606 FIBRE DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME	HOLE	U86-7	DEPTH	141.43
AZIMUTH	90°	INCLINATION	-44	SECTION	6649
LATITUDE	6649.9N	DEPARTURE	7605.0E	ELEVATION	1413.8 m
STARTED	Aug. 22	FINISHED	Aug. 30	LOGGED	by I. Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH m	DESCRIPTION	VISUAL LOG
1.15	141.4		Serpentinite, dark green to medium dark green, good fibre,	
			occasional minor shears	
			Broken & fractured 16.8 - 25.6, 49.1 - 51.8; 57.9 - 76.5	
			fault zone, cleaved and gouge; 67.8 - 76.5 fault zone, broken	
			cleaved and gouge	
			Minor shears 92 - 98	
			Broken 94.5 - 103.6	
			Minor shear 110 - 112	
			114 - 118.1 fault zone, mostly gouge, picrolite and lizardite	
			veining at base	
			121.6 Reduced HQ to NQ	
			123-1 - 126.2 Minor fault, fractured and broken with short	
			sections of gouge	
			Serp with occasional gouges to E.O.H.	
141.4			E.O.H.	

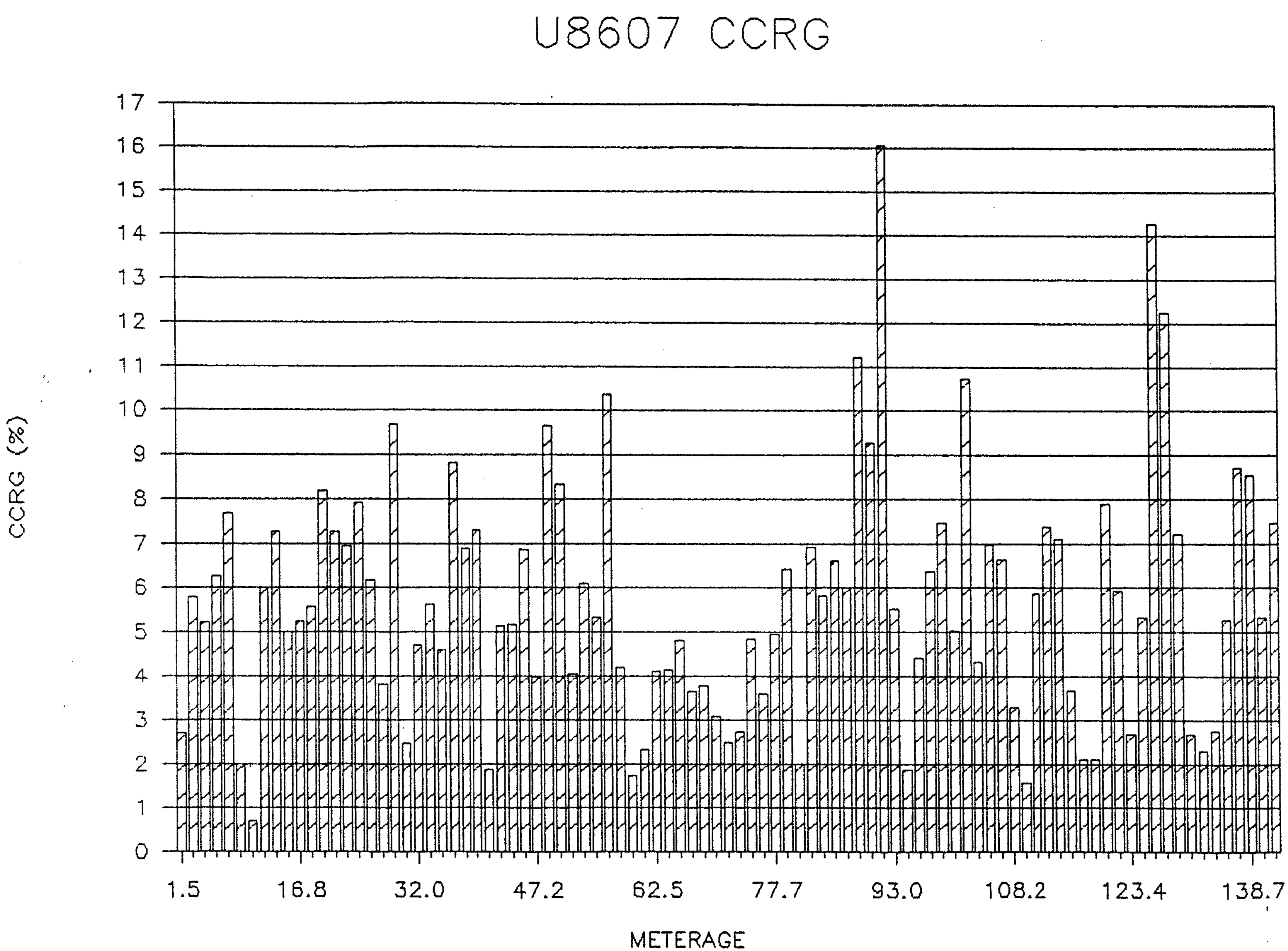
DDH U 8607

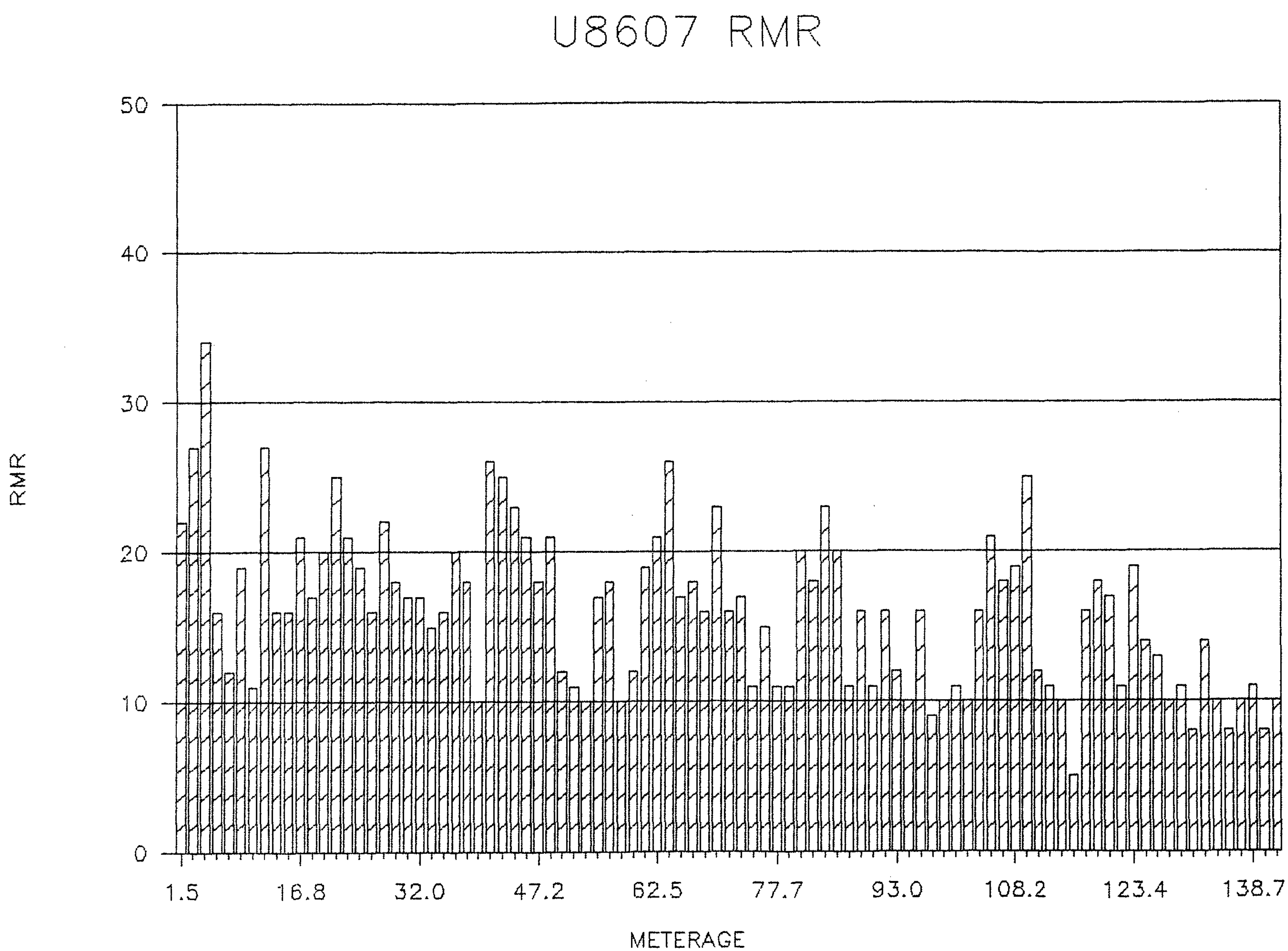
AVERAGE OF TWO COUNTS

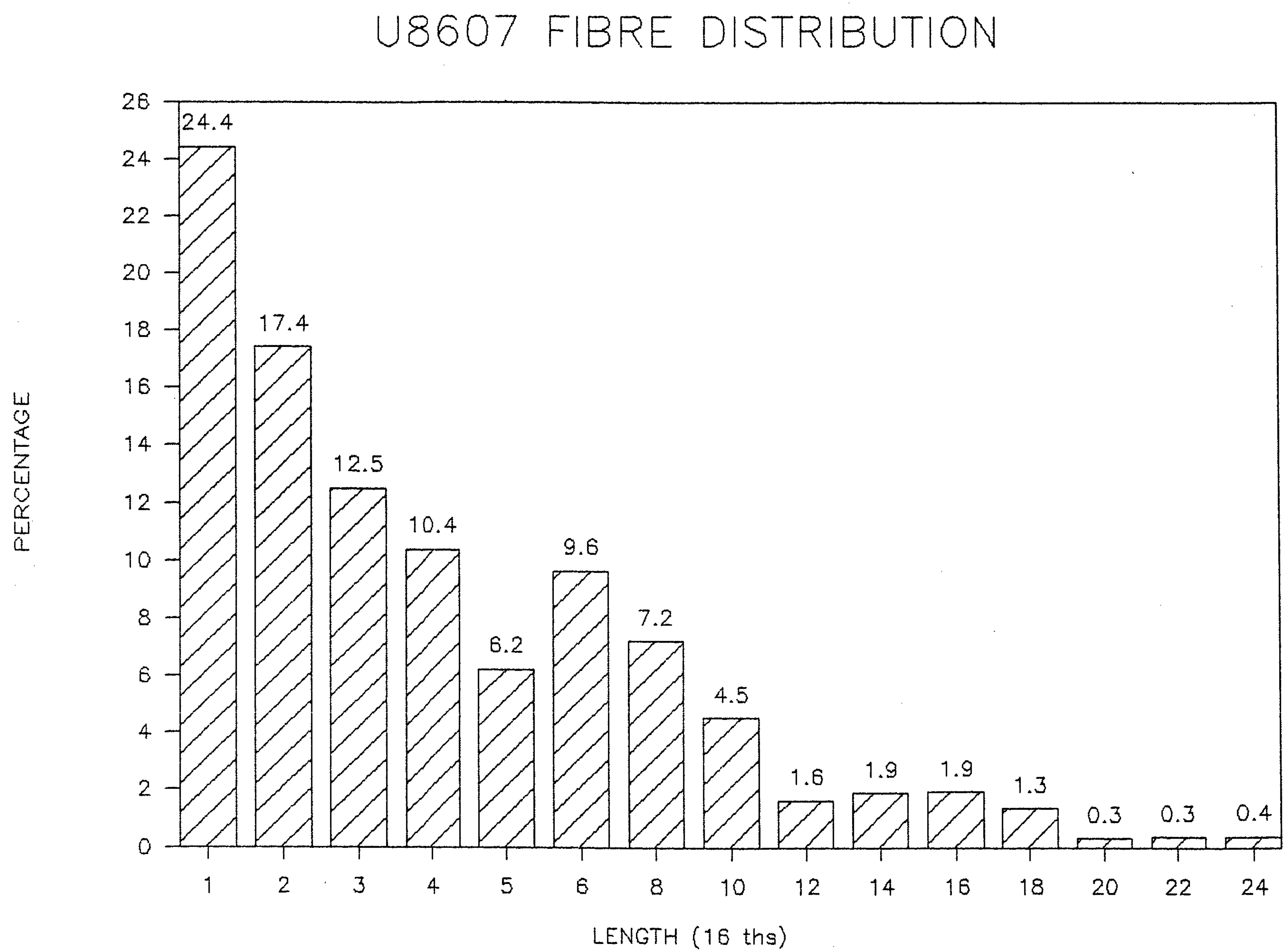
Number of fibre veins counted per 16th category

FROM	TO	REC	RQD	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG
M	M	M																		%
0.0	1.5	1.0	22	5	0.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	11.5	2.68
1.5	3.0	1.3	27	6.5	4	3.5	0	1	0.5	0	0	0	0	0	0	0	0	0	33	5.78
3.0	4.6	1.5	34	7.5	2.5	2	2	0	1.5	0	0	0	0	0	0	0	0	0	35.5	5.22
4.6	6.1	1.3	16	7.5	3.5	2	2	0.5	1	0	0	0	0	0	0	0	0	0	37	6.26
6.1	7.6	1.4	12	5.5	3	11	1	0	0	0	0	0	0	0	0	0	0	0	48.5	7.68
7.6	9.1	1.5	19	8	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	13.5	1.98
9.1	10.7	1.5	11	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.69
10.7	12.2	1.4	27	6	4	1.5	1	1.5	0	1	0	0	0	0	0	0	0	0	38	6.01
12.2	13.7	1.4	16	5.5	4	1.5	2.5	0	0.5	1	0.5	0	0	0	0	0	0	0	44	7.28
13.7	15.2	1.5	16	6.5	4	2.5	2	0	0.5	0	0	0	0	0	0	0	0	0	33	5.01
15.2	16.8	1.5	21	10	5	1	1	0	1.5	0	0	0	0	0	0	0	0	0	36	5.25
16.8	18.3	1.4	17	5.5	1.5	0.5	1.5	0.5	0.5	1	0.5	0	0	0	0	0	0	0	34.5	5.58
18.3	19.8	1.4	20	8	2.5	1	0	1.5	0.5	0	1	0.5	0.5	0	0	0	0	0	49.5	8.19
19.8	21.3	1.4	25	11	4	2	1.5	0	1.5	0.5	0	0	0	0	0	0	0	0	44	7.28
21.3	22.9	1.4	21	11.5	3	1.5	2	1	0.5	0.5	0	0	0	0	0	0	0	0	42	6.95
22.9	24.4	1.4	19	9	4	2.5	0	1.5	0.5	1	0	0	0	0.5	0	0	0	0	51	7.90
24.4	25.9	1.4	16	8	2.5	2.5	1.5	0	1.5	0.5	0	0	0	0	0	0	0	0	39.5	6.18
25.9	27.4	1.3	22	6.5	2	0.5	0	0	0	0	1	0	0	0	0	0	0	0	22	3.81
27.4	29.0	1.5	18	14	5.5	3.5	0.5	0.5	1.5	0	1	0.5	0	0	0	0	0	0	65	9.67
29.0	30.5	1.5	17	8	2	1.5	0	0	0	0	0	0	0	0	0	0	0	0	16.5	2.45
30.5	32.0	1.4	17	8	5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	30.5	4.72
32.0	33.5	1.4	15	10	3.5	1	1	0.5	1.5	0	0	0	0	0	0	0	0	0	35.5	5.62
33.5	35.1	1.3	16	6.5	2.5	1	1	0	1.5	0	0	0	0	0	0	0	0	0	27.5	4.60
35.1	36.6	1.5	20	10	3.5	3	1.5	0.5	0.5	0.5	0	0	0	1	0	0	0	0	57.5	8.82
36.6	38.1	1.4	18	12.5	0.5	1	1	0.5	1	0	0	0	0.5	0.5	0	0	0	0	44	6.89
38.1	39.6	1.5	10	11.5	5	2.5	1.5	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	49.5	7.29
39.6	41.1	1.4	26	6	3	0	0	0	0	0	0	0	0	0	0	0	0	0	12	1.86
41.1	42.7	1.5	25	8.5	3	2	0.5	0.5	1	0.5	0	0	0	0	0	0	0	0	35	5.15
42.7	44.2	1.5	23	12.5	4	1	0.5	0	0	0.5	0.5	0	0	0	0	0	0	0	34.5	5.18
44.2	45.7	1.5	21	5.5	2.5	1.5	1	0.5	0.5	0.5	0	0	0	0	1	0	0	0	46.5	6.84
45.7	47.2	1.3	18	5	2.5	0.5	0.5	0	0	0.5	0	0.5	0	0	0	0	0	0	23.5	3.97
47.2	48.8	1.5	21	6	5	3	3	0.5	2	0.5	1	0	0	0	0	0	0	0	65.5	9.64
48.8	50.3	1.5	12	9.5	4.5	2	0	1	0	0	0	0.5	0	0	0	0.5	0.5	0	56.5	8.32
50.3	51.8	1.5	11	7	2	0.5	1	0	1	0.5	0	0	0	0	0	0	0	0	26.5	4.06
51.8	53.3	1.5	10	11	4.5	1	0.5	0.5	1	1	0	0	0	0	0	0	0	0	41.5	6.11
53.3	54.9	1.5	17	12	4.5	1.5	1.5	0	0	0.5	0	0	0	0	0	0	0	0	35.5	5.33
54.9	56.4	1.5	18	15	2	1.5	0	1.5	0.5	2	0.5	0.5	0	0.5	0	0	0	0	69	10.3
56.4	57.9	1.4	10	7.5	2	1.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	26.5	4.19
57.9	59.4	1.4	12	3	0	0	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	10.5	1.71
59.4	61.0	1.5	19	2.5	0.5	0	0.5	0	1	0.5	0	0	0	0	0	0	0	0	15.5	2.32
61.0	62.5	1.4	21	12	3	2	0.5	0	0	0	0	0	0	0	0	0	0	0	26	4.11
62.5	64.0	1.5	26	15.5	3	1	0	0.5	0	0	0	0	0	0	0	0	0	0	27	4.14
64.0	65.5	1.4	17	9	5.5	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	30.5	4.83
65.5	67.1	1.5	18	10.5	3.5	1	1	0	0	0	0	0	0	0	0	0	0	0	24.5	3.64
67.1	68.6	1.4	16	11	3	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	24	3.80
68.6	70.1	1.5	23	6.5	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	21	3.09
70.1	71.6	1.2	16	9.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.48
71.6	73.2	1.5	17	12	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	18.5	2.72
73.2	74.7	1.4	11	7.5	4	1.5	0.5	1	0	0.5	0	0	0	0	0	0	0	0	31	4.85
74.7	76.2	1.5	15	8	2.5	0	1	0.5	0	0	0.5	0	0	0	0	0	0	0	24.5	3.60
76.2	77.7	1.5	11	6	2.5	0.5	0.5	0.5	1	0	1	0	0	0	0	0	0	0	33	4.96
77.7	79.2	1.4	11	4.5	2.5	1.5	1	1.5	2	0.5	0	0	0	0	0	0	0	0	41.5	6.43

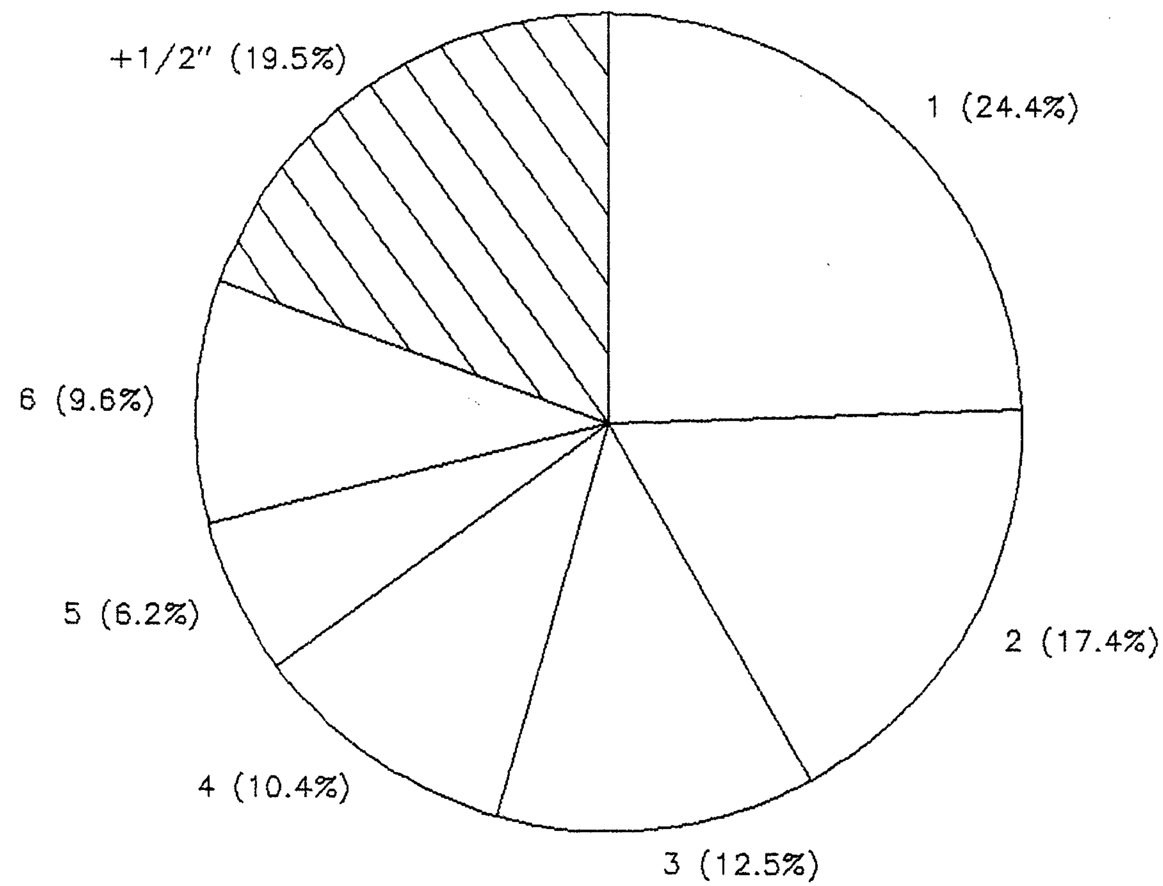
79.2	80.8	1.5	20	4	2.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	13.5	1.98
80.8	82.3	1.5	18	8	3.5	0.5	2	0.5	0	0.5	0	0	1	0	0	0	0	0	45	6.90
82.3	83.8	1.5	23	11.5	5	0.5	2	0.5	1	0	0	0	0	0	0	0	0	0	39.5	5.81
83.8	85.3	1.5	20	8.5	1.5	1.5	0.5	1	0	0	0.5	0	0.5	0	0.5	0	0	0	44	6.61
85.3	86.9	1.4	11	6.5	1.5	1.5	2.5	0.5	1	0	0.5	0	0	0	0	0	0	0	37.5	6.00
86.9	88.4	1.3	16	7.5	1	1.5	2	1	2.5	0.5	1.5	0.5	0	0	0	0	0	0	67	11.2
88.4	89.9	1.5	11	4	3.5	1.5	0.5	0.5	1	1.5	2.5	0	0	0	0	0	0	0	63	9.27
89.9	91.4	1.4	16	8.5	3	2.5	2.5	1.5	1.5	1.5	0.5	0.5	0.5	1.5	0	0	0	0	102.5	16.0
91.4	93.0	1.5	12	8	5.5	1.5	0.5	0	0.5	1	0	0	0	0	0	0	0	0	36.5	5.54
93.0	94.5	1.3	10	4	2	0	0	0.5	0	0	0	0	0	0	0	0	0	0	10.5	1.86
94.5	96.0	1.5	16	8	2	1	1	0	0	0.5	0	0.5	0	0	0	0	0	0	29	4.40
96.0	97.5	1.3	9	13	4	2.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	38	6.36
97.5	99.1	1.4	10	4	3	1	1	0.5	0	1.5	0.5	0	0	0	0.5	0	0	0	45.5	7.44
99.1	100.6	1.4	11	7	1.5	1	1.5	1.5	1	0	0	0	0	0	0	0	0	0	32.5	5.03
100.6	102.1	1.3	10	11	4.5	1	1.5	0	1	0.5	0	0.5	0.5	0	0	0	0	0.5	64	10.7
102.1	103.6	1.4	16	6.5	2.5	1.5	3	0	0	0	0	0	0	0	0	0	0	0	28	4.34
103.6	105.2	1.5	21	9	3	2	1	0	0	1.5	0	0	0	0	0.5	0	0	0	46	6.98
105.2	106.7	1.4	18	15	4.5	2.5	0	0	1	0.5	0	0	0	0	0	0	0	0	41.5	6.64
106.7	108.2	1.4	19	15.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	21	3.29
108.2	109.7	1.4	25	9.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.55
109.7	111.3	1.4	12	18.5	2.5	0.5	0.5	1	0	0.5	0	0	0	0	0	0	0	0	36	5.89
111.3	112.8	1.3	11	11	4.5	2	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	41.5	7.36
112.8	114.3	1.3	10	8.5	4.5	2	2.5	0	0.5	0.5	0	0	0	0	0	0	0	0	40.5	7.10
114.3	115.8	1.3	5	10.5	2.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	22	3.68
115.8	117.3	1.5	16	6.5	2	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	14	2.10
117.3	118.9	1.4	18	3.5	2	0.5	1	0	0	0	0	0	0	0	0	0	0	0	13	2.10
118.9	120.4	1.5	17	7	5.5	1.5	1.5	0.5	1.5	1.5	0	0	0	0	0	0	0	0	52	7.89
120.4	121.9	1.4	11	7.5	2.5	2.5	2.5	1.5	0	0	0	0	0	0	0	0	0	0	37.5	5.93
121.9	123.4	1.3	19	6.5	2	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	15	2.66
123.4	125.0	1.4	14	6	2	2	0	2	0.5	0.5	0	0	0	0	0	0	0	0	33	5.34
125.0	126.5	1.3	13	8.5	5	3	0	2	3.5	1	0	0	1	0	0	0	0	0	80.5	14.2
126.5	128.0	1.4	10	12.5	4.5	2.5	1.5	2	4	0	0.5	0	0	0	0	0	0	0	74	12.2
128.0	129.5	1.4	11	15	5.5	3	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	46.5	7.20
129.5	131.1	1.4	8	8	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	17	2.66
131.1	132.6	1.4	14	7.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	14	2.29
132.6	134.1	1.3	10	8	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	16	2.77
134.1	135.6	1.5	8	13.5	3	2	1	0	1	0	0	0	0	0	0	0	0	0	35.5	5.28
135.6	137.2	1.3	10	13	5.5	2	3	0.5	0.5	0.5	0	0	0	0	0	0	0	0	51.5	8.71
137.2	138.7	1.4	11	14.5	4	2.5	0.5	0	1.5	1	0.5	0	0	0	0	0	0	0	54	8.55
138.7	140.2	1.4	8	15	3.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	33	5.34
140.2	141.4	1.2	10	10	6	1.5	1	0.5	1	0	0	0	0	0	0	0	0	0	39	7.46


U8607 CCRG
CCRG (%)
17
16
15
14
13
12
11
10
9
8
7
6
5
4
3
2
1
0
1.5
16.8
32.0
47.2
62.5
77.7
93.0
108.2
123.4
138.7
METERAGE


U8607 RMR
RMR
50
40
30
20
10
0
1.5
16.8
32.0
47.2
62.5
77.7
93.0
108.2
123.4
138.7
METERAGE


U8607 FIBRE DISTRIBUTION
PERCENTAGE
LENGTH (16 ths)
0
2
4
6
8
10
12
14
16
18
20
22
24
26
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
24.4
17.4
12.5
10.4
6.2
9.6
7.2
4.5
1.6
1.9
1.9
1.3
0.3
0.3
0.4

U8607 FIBRE DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME | HOLE U86-8 | DEPTH 210-0 m

AZIMUTH 89° | INCLINATION -27° | SECTION 6649N

LATITUDE 6649.89 | DEPARTURE 7604.4 | ELEVATION 1414.15

STARTED Aug. 30 | FINISHED Sept. 7 | LOGGED by I. Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
//////	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1.2	159.4		Serpentinite, dark green to medium green, mottled, fibre	
			bearing, fractured, occasional shears with thin gouges.	
			5.5 - 7.3 shear zone	
			9.5 - 16.2 Fractured, thin gouges spaced ½ to 1 m	
			42 - 54.6 Fault zone with gouge	
			54.6 - 155.4 Occasional broken sections, minor shears at	
			117.8 - 122.2	
			150.6 Reduce HQ to NQ	
			155.4 - 159.4 Shear zone, numerous curving slips	
159.4	203.9		Light green serpentinite, fibre bearing, curving joints,	
			talcy, occasional lizardite veins, broken, minor sheared sections	
203.9	210		Medium green serpentinite, fibre bearing, minor sheared sections.	
210			E.O.H.	

DDH U 8608

AVERAGE OF TWO COUNTS

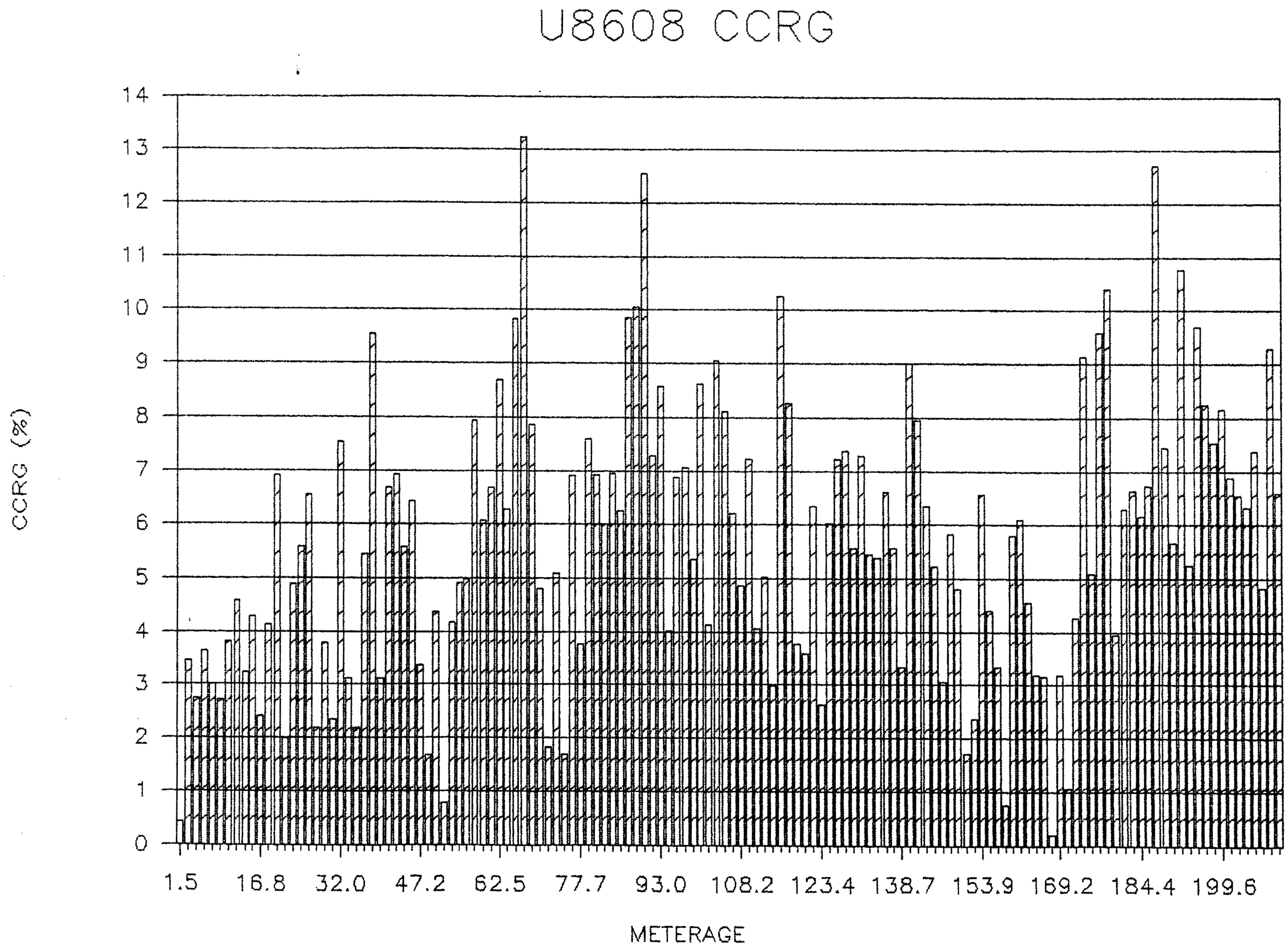
Number of fibre veins counted per 16th category

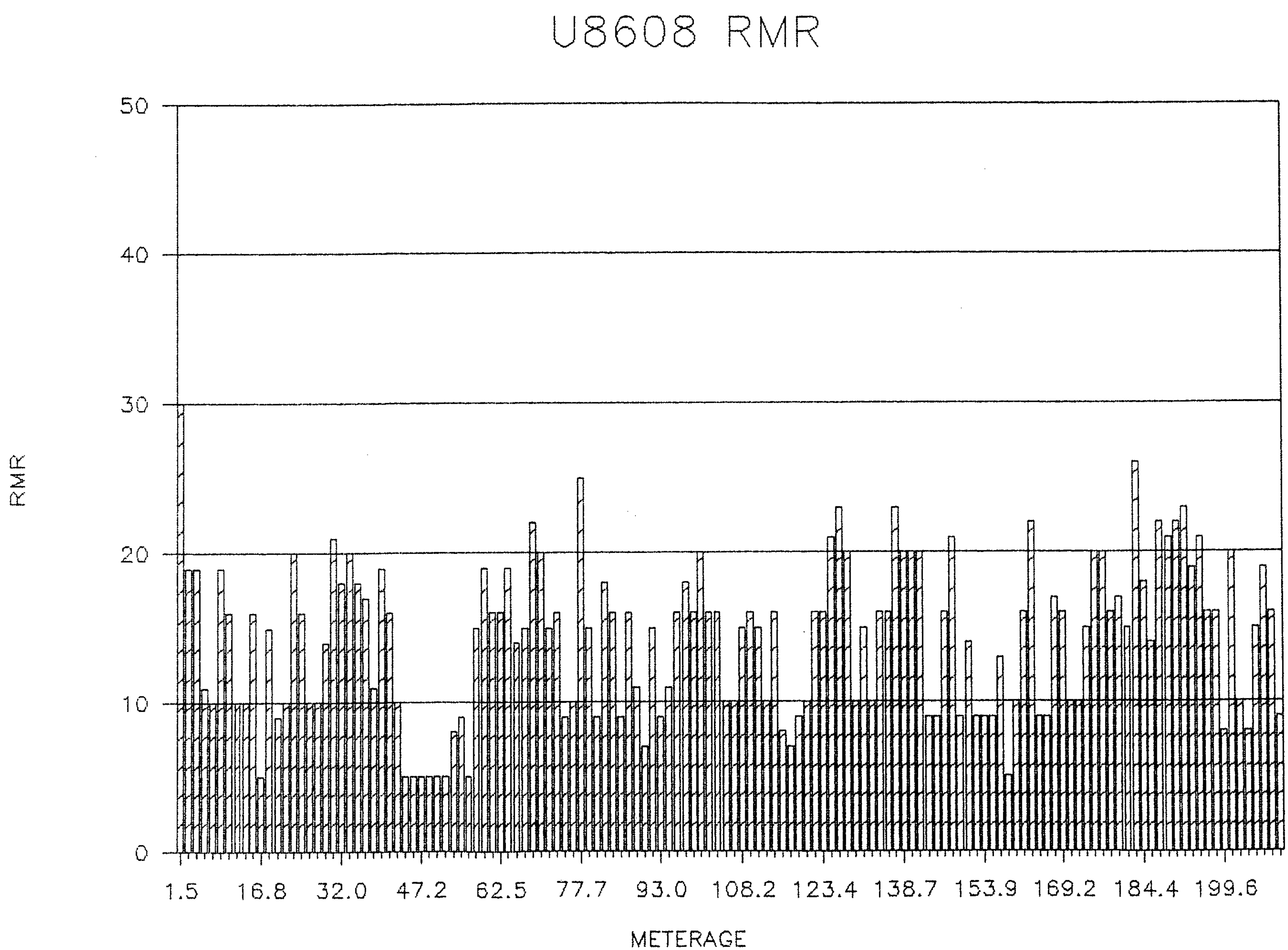
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.0	1.5	0.3	30	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.40
1.5	3.0	1.5	19	8	1.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	23	3.45
3.0	4.6	1.5	19	7.5	2	0.5	0	1	0	0	0	0	0	0	0	0	0	0	18	2.73
4.6	6.1	1.5	11	9	1.5	1	1	1	0	0	0	0	0	0	0	0	0	0	24	3.64
6.1	7.6	1.4	10	7	4	1.5	0	0	0	0	0	0	0	0	0	0	0	0	19.5	3.02
7.6	9.1	1.5	19	6.5	1	1	1	0	0.5	0	0	0	0	0	0	0	0	0	18.5	2.72
9.1	10.7	1.4	16	4.5	2	0	1	1	1	0	0	0	0	0	0	0	0	0	23.5	3.80
10.7	12.2	1.3	10	6.5	2	1	0.5	0.5	1.5	0	0	0	0	0	0	0	0	0	27	4.57
12.2	13.7	1.4	10	7	1	1	0	1.5	0	0	0	0	0	0	0	0	0	0	19.5	3.22
13.7	15.2	1.3	16	3.5	1	1.5	0.5	0.5	1	0.5	0	0	0	0	0	0	0	0	24.5	4.29
15.2	16.8	1.5	5	8	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	16	2.40
16.8	18.3	1.5	15	10	3	1	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	28	4.12
18.3	19.8	1.5	9	7	2	0.5	1.5	1	2	0.5	0	0.5	0	0	0	0	0	0	45.5	6.90
19.8	21.3	1.5	10	5.5	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13.5	1.98
21.3	22.9	1.5	20	6	1.5	1	0	0.5	0.5	0.5	0.5	0.5	0	0	0	0	0	0	32.5	4.88
22.9	24.4	1.4	16	6	0.5	1.5	2	0.5	1.5	0	0.5	0	0	0	0	0	0	0	36	5.58
24.4	25.9	1.5	10	4.5	3	0.5	1	0.5	1.5	1.5	0.5	0	0	0	0	0	0	0	44.5	6.55
25.9	27.4	1.4	10	5.5	0.5	1	1	0	0	0	0	0	0	0	0	0	0	0	13.5	2.18
27.4	29.0	1.4	14	6	2	0.5	1	0.5	1	0	0	0	0	0	0	0	0	0	24	3.80
29.0	30.5	1.3	21	9	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	14	2.34
30.5	32.0	1.4	18	6.5	2.5	1.5	0.5	0.5	0.5	0.5	1	0	0	0	0	0	0.5	0	48.5	7.52
32.0	33.5	1.5	20	6.5	4	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	21	3.12
33.5	35.1	1.3	18	3.5	2.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	13	2.17
35.1	36.6	1.5	17	10.5	4.5	2.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	37	5.45
36.6	38.1	1.4	11	8	2.5	0.5	1	2	2	0.5	1	0	0.5	0	0	0	0	0	61.5	9.53
38.1	39.6	1.4	19	6	1.5	1	0	0	0	1	0	0	0	0	0	0	0	0	20	3.13
39.6	41.1	1.5	16	9.5	2	1.5	1	1	1	0.5	0	0	0.5	0	0	0	0	0	44	6.68
41.1	42.7	1.3	10	9	2.5	3	2	0	0	0.5	0.5	0	0	0	0	0	0	0	40	6.93
42.7	44.2	1.3	5	8.5	6	2	1	0.5	0	0	0	0	0	0	0	0	0	0	33	5.58
44.2	45.7	1.3	5	8	4.5	2	1.5	1	0	0.5	0	0	0	0	0	0	0	0	38	6.43
45.7	47.2	1.1	5	6.5	3	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	16.5	3.37
47.2	48.8	1.4	5	8.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.66
48.8	50.3	1.4	5	7	5	2	1	0	0	0	0	0	0	0	0	0	0	0	27	4.37
50.3	51.8	1.4	5	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.77
51.8	53.3	1.4	8	8	4.5	2	0	0.5	0	0	0	0	0	0	0	0	0	0	25.5	4.17
53.3	54.9	1.4	9	13	3.5	2	1	0	0	0	0	0	0	0	0	0	0	0	30	4.91
54.9	56.4	1.2	5	3.5	1	1	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	26	4.97
56.4	57.9	1.4	15	6.5	6.5	0.5	2	0.5	1	1.5	0	0	0	0	0	0	0	0	49.5	7.92
57.9	59.4	1.5	19	8	3.5	2.5	1.5	1	1	0	0	0	0	0	0	0	0	0	39.5	6.06
59.4	61.0	1.5	16	2.5	2.5	1.5	0.5	0.5	1.5	1	0.5	0.5	0	0	0	0	0	0	44.5	6.68
61.0	62.5	1.4	16	8	3	1	2	0.5	1	1	0.5	0.5	0	0	0	0	0	0	52.5	8.68
62.5	64.0	1.4	19	5	3	2.5	1	1	0.5	0	1	0	0	0	0	0	0	0	40.5	6.27
64.0	65.5	1.3	14	5.5	3.5	2.5	2.5	0	0.5	2	0	0	0.5	0	0	0	0	0	56	9.82
65.5	67.1	1.4	15	2	4.5	1	2	3	2.5	3.5	0	0	0	0	0	0	0	0	80	13.2
67.1	68.6	1.4	22	2.5	3.5	2.5	2	0.5	0.5	0.5	0	0.5	0.5	0	0	0	0	0	47.5	7.86
68.6	70.1	1.5	20	10.5	3.5	2	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	32.5	4.78
70.1	71.6	1.4	15	8	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11.5	1.82
71.6	73.2	1.4	16	7.5	1.5	0.5	1.5	0.5	1	0	0.5	0	0	0	0	0	0	0	31.5	5.09
73.2	74.7	1.3	9	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10	1.69
74.7	76.2	1.5	10	9	2.5	1	0.5	0.5	0.5	0	0.5	0	0	1	0	0	0	0	45.5	6.90
76.2	77.7	1.4	25	7.5	5	2	0	0	0	0	0	0	0	0	0	0	0	0	23.5	3.76
77.7	79.2	1.5	15	5.5	2.5	1	0.5	0	2	0	0.5	0.5	0	0	0	0	0	0.5	50.5	7.59

79.2	80.8	1.5	9	10.5	2	2	1.5	1	1	0.5	0.5	0	0	0	0	0	0	0	46.5	6.91
80.8	82.3	1.4	18	8	5	1	1	0	1.5	0.5	0	0	0	0	0	0	0	0	38	6.01
82.3	83.8	1.4	16	4	0	0.5	0.5	0	0	1	1.5	1	0	0	0	0	0	0	42.5	6.95
83.8	85.3	1.3	9	6.5	2	1.5	1	0	1	1.5	0	0	0	0	0	0	0	0	37	6.26
85.3	86.9	1.5	16	8.5	0.5	1.5	0.5	0.5	1	0.5	0.5	0	1	0	0.5	0	0.5	0	67.5	9.84
86.9	88.4	1.2	11	5.5	2	3	2	0.5	0	0	1	0	0.5	0.5	0	0	0	0	54	10.0
88.4	89.9	1.1	7	8	4	0.5	0	0.5	2	0	0.5	0.5	0	0	0.5	0	0	0.5	64	12.5
89.9	91.4	1.3	15	5.5	1	0	1.5	0.5	0	0.5	0	0	0	0	0	0	0.5	0.5	43	7.28
91.4	93.0	1.4	9	6	3.5	2	2	1	1	0	1.5	0	0	0	0	0	0	0	53	8.57
93.0	94.5	1.5	11	11	3	0	1.5	0	0	0.5	0	0	0	0	0	0	0	0	27	4.01
94.5	96.0	1.4	16	6.5	2.5	0.5	2.5	0.5	1.5	1	0	0	0	0	0	0	0	0	42.5	6.87
96.0	97.5	1.5	18	6	2	2.5	0	2	0.5	2	0	0	0	0	0	0	0	0	46.5	7.06
97.5	99.1	1.4	16	6.5	3.5	0.5	0.5	0.5	1.5	0	0	0.5	0	0	0	0	0	0	34.5	5.34
99.1	100.6	1.3	20	6	1.5	1	0.5	0.5	0	0	1.5	1	0	0.5	0	0	0	0	51.5	8.62
100.6	102.1	1.4	16	4.5	2.5	0.5	0.5	0	0	0	0.5	0	0	0.5	0	0	0	0	26	4.11
102.1	103.6	1.5	16	6	4	1	0.5	1	0.5	2	1	0.5	0	0	0	0	0	0	59	9.05
103.6	105.2	1.5	10	7.5	4.5	1	0.5	0.5	1	1	1	0.5	0	0	0	0	0	0	54	8.11
105.2	106.7	1.4	10	4	2	2.5	1.5	0.5	2	0.5	0	0	0	0	0	0	0	0	40	6.20
106.7	108.2	1.4	15	9.5	2.5	1.5	0	0	0.5	0.5	0.5	0	0	0	0	0	0	0	31	4.85
108.2	109.7	1.5	16	6	3	1	1	1.5	0.5	0.5	0.5	0	0	0	0.5	0	0	0	47.5	7.21
109.7	111.3	1.3	15	10	5.5	0	0	0	0.5	0	0	0	0	0	0	0	0	0	24	4.06
111.3	112.8	1.3	10	9.5	1	0.5	0.5	1	1.5	0	0	0	0	0	0	0	0	0	29	5.02
112.8	114.3	1.4	16	8.5	1	0	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	18	2.97
114.3	115.8	0.7	8	1.5	1.5	1	1.5	0.5	0.5	1	0.5	0	0	0	0	0	0	0	32	10.2
115.8	117.3	1.4	7	5	3	3	0.5	1	0.5	1	0	1	0	0	0	0	0	0	50	8.27
117.3	118.9	1.4	9	5	6.5	2	0	0	0	0	0	0	0	0	0	0	0	0	24	3.76
118.9	120.4	1.3	10	9.5	2.5	1	1	0	0	0	0	0	0	0	0	0	0	0	21.5	3.59
120.4	121.9	1.3	16	7	2.5	2	2	0.5	1.5	0	0	0	0	0	0	0	0	0	37.5	6.34
121.9	123.4	1.4	16	10.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	17	2.63
123.4	125.0	1.5	21	15	4	1.5	0	0	0.5	0	1	0	0	0	0	0	0	0	40.5	6.02
125.0	126.5	1.5	23	12	3.5	1	1	1	0.5	0	0.5	0	0	0	0	0.5	0	0	49	7.21
126.5	128.0	1.4	20	12.5	6	2.5	0.5	1.5	1	0	0	0	0	0	0	0	0	0	47.5	7.36
128.0	129.5	1.4	10	5.5	3.5	2.5	1	1.5	0	0.5	0	0	0	0	0	0	0	0	35.5	5.56
129.5	131.1	1.4	15	15	5.5	1.5	0.5	1.5	1	0	0	0	0	0	0	0	0	0	46	7.28
131.1	132.6	1.4	10	9.5	2	0.5	1	0	0.5	1.5	0	0	0	0	0	0	0	0	34	5.44
132.6	134.1	1.5	16	14.5	2.5	1	1	0.5	1	0	0	0	0	0	0	0	0	0	35	5.37
134.1	135.6	1.3	16	7.5	4.5	2	0.5	1	0.5	0	0	0	0.5	0	0	0	0	0	39.5	6.61
135.6	137.2	1.4	23	10	2.5	1.5	1	1	0.5	0.5	0	0	0	0	0	0	0	0	35.5	5.56
137.2	138.7	1.4	20	10.5	0.5	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	21.5	3.33
138.7	140.2	1.4	20	9.5	8	4	2	0	0	1.5	0	0	0	0	0	0	0	0	57.5	9.01
140.2	141.4	1.5	20	12	4.5	2	1	1	1.5	0.5	0.5	0	0	0	0	0	0	0	54	7.95
141.7	143.3	1.4	9	11	2.5	1	0.5	0	1.5	0.5	0	0.5	0	0	0	0	0	0	40	6.33
143.3	144.8	1.4	9	8.5	4.5	0.5	0	0	1	1	0	0	0	0	0	0	0	0	33	5.22
144.8	146.3	1.4	16	6.5	3	0.5	0	0	0	0	0.5	0	0	0	0	0	0	0	19	3.04
146.3	147.8	1.5	21	16.5	3	1	2.5	0.5	0	0	0	0	0	0	0	0	0	0	38	5.83
147.8	149.4	1.4	9	8.5	3	1.5	0	1	0.5	0.5	0	0	0	0	0	0	0	0	31	4.80
149.4	150.9	1.4	14	9	1	0	0	0	0	0	0	0	0	0	0	0	0	0	11	1.72
150.9	152.4	1.3	9	3	1.5	0.5	0	0	1	0	0	0	0	0	0	0	0	0	13.5	2.36
152.4	153.9	1.3	9	8.5	4	3	1	1	0.5	0	0	0	0	0	0	0	0	0	37.5	6.57
153.9	155.4	1.4	9	7.5	6	2	0.5	0	0	0	0	0	0	0	0	0	0	0	27.5	4.40
155.4	157.0	1.3	13	11.5	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	19.5	3.33
157.0	158.5	1.3	5	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.75
158.5	160.0	1.4	10	10.5	4	1	0.5	1	0	0.5	0.5	0	0	0	0	0	0	0	37.5	5.81
160.0	161.5	1.4	16	7.5	5	1	1	1	0.5	0	0	0.5	0	0	0	0	0	0	38.5	6.09
161.5	163.1	1.4	22	10	4.5	2	0	0.5	0	0	0	0	0	0	0	0	0	0	27.5	4.55
163.1	164.6	1.4	9	7	4	1.5	0	0	0	0	0	0	0	0	0	0	0	0	19.5	3.19

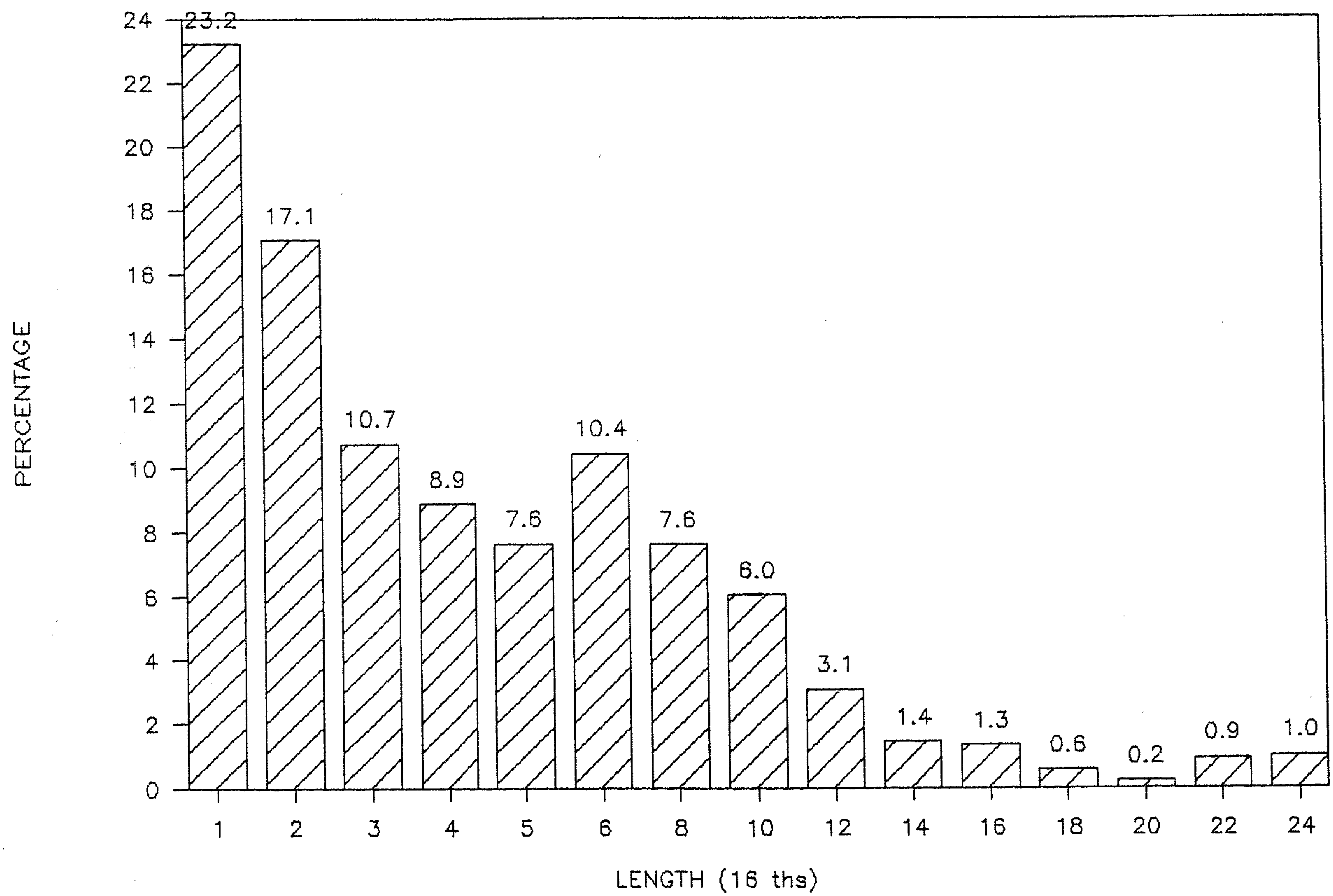
164.6	166.1	1.2	9	8.5	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	17	3.16
166.1	167.6	1.2	17	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
167.6	169.2	1.5	16	10	3	1	0.5	0	0	0	0	0	0	0	0	0	0	0	21	3.18
169.2	170.7	1.4	10	4.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.05
170.7	172.2	1.4	10	14	2	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	26	4.25
172.2	173.7	1.4	15	8.5	5.5	3.5	1	0	0.5	0	1.5	0	0.5	0	0	0	0	0	59	9.14
173.7	175.3	1.5	20	11.5	4	0.5	1	0.5	1	0	0	0	0	0	0	0	0	0	33.5	5.08
175.3	176.8	1.3	20	10.5	2	1.5	0.5	0	0	0.5	0	0.5	0	0	0	0	0.5	0.5	54	9.58
176.8	178.3	1.5	16	8	4.5	1.5	2.5	0.5	2	0.5	2	0	0	0	0	0	0	0	70	10.4
178.3	179.8	1.4	17	9	2.5	0	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	25.5	3.95
179.8	181.4	1.5	15	10.5	2	1.5	1	0.5	2	0.5	0	0	0	0	0	0	0	0	41.5	6.30
181.4	182.9	1.5	26	8	5	1.5	0	0.5	2.5	0	0.5	0	0	0	0	0	0	0	45	6.62
182.9	184.4	1.5	18	10.5	4	0.5	0.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	41.5	6.17
184.4	185.9	1.4	14	7	3	1.5	0.5	0	1	0	0.5	1	0	0	0	0	0	0	42.5	6.73
185.9	187.5	1.4	22	16.5	5	1	1.5	3	1.5	1	0.5	0.5	0	0	0	0	0	0	78.5	12.7
187.5	189.0	1.4	21	15	4	1.5	0.5	0.5	1.5	0	0	0	0.5	0	0	0	0	0	48	7.44
189.0	190.5	1.5	22	12.5	3	2.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	38.5	5.67
190.5	192.0	1.4	23	5	5.5	1.5	1.5	0	0.5	0	1	0.5	0	1.5	0	0	0	0	69.5	10.7
192.0	193.5	1.4	19	7.5	4	0.5	0.5	0.5	0	0	0	1	0	0	0	0	0	0	33.5	5.24
193.5	195.1	1.5	21	7.5	1.5	2.5	1	0.5	3	1.5	1	0	0	0	0	0	0	0	64.5	9.69
195.1	196.6	1.5	16	23.5	6.5	0.5	0.5	2	1	0	0	0	0	0	0	0	0	0	56	8.24
196.6	198.1	1.5	16	12.5	7	2.5	0	2	1	0	0	0	0	0	0	0	0	0	50	7.51
198.1	199.6	1.3	8	10	5.5	2.5	1.5	0.5	1	0.5	0	0	0	0	0	0	0	0	47	8.14
199.6	201.2	1.4	20	12.5	6	1.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	43	6.88
201.2	202.7	1.5	10	10.5	3	2.5	0.5	1.5	0.5	1	0	0	0	0	0	0	0	0	44.5	6.55
202.7	204.2	1.4	8	7	4.5	1.5	0.5	1	2	0	0	0	0	0	0	0	0	0	39.5	6.32
204.2	205.7	1.4	15	14	5	2.5	2.5	1	0	0	0	0	0	0	0	0	0	0	46.5	7.36
205.7	207.3	1.4	19	14.5	4.5	2	0	0	0	0	0	0	0	0	0	0	0	0	29.5	4.82
207.3	208.8	1.4	16	17	3.5	2	0.5	2	0.5	1	0.5	0	0	0	0	0	0	0	58	9.28
208.8	210.0	1.2	9	10	4	1	2	1	0	0	0	0	0	0	0	0	0	0	34	6.58

EOH


U8608 CCRG
CCRG (%)
METERAGE
0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
1.5
16.8
32.0
47.2
62.5
77.7
93.0
108.2
123.4
138.7
153.9
169.2
184.4
199.6


U8608 RMR
RMR
50
40
30
20
10
0
1.5
16.8
32.0
47.2
62.5
77.7
93.0
108.2
123.4
138.7
153.9
169.2
184.4
199.6
METERAGE

U8608 FIBRE DISTRIBUTION



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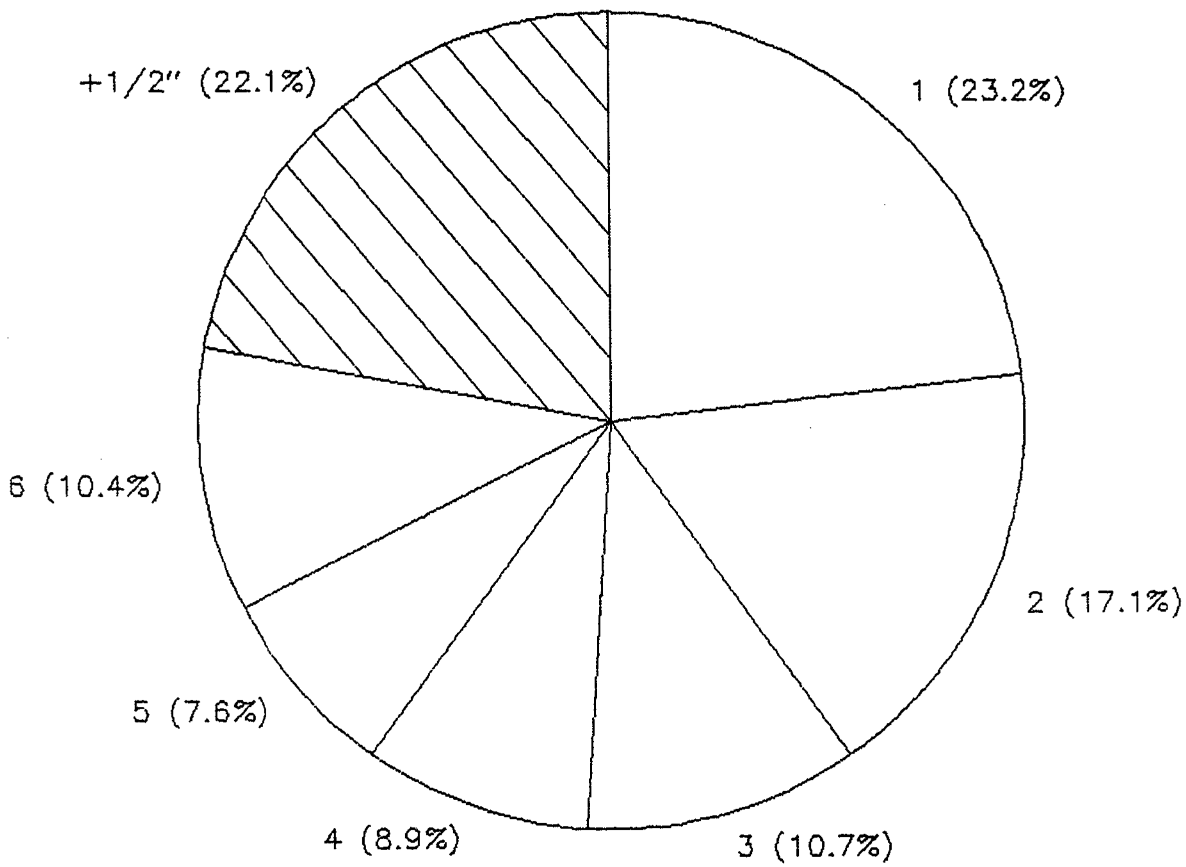


DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME | HOLE U86-9 | DEPTH 72.8

AZIMUTH 90 | INCLINATION -4° | SECTION 6649

LATITUDE 6649.9N | DEPARTURE 7605.0E | ELEVATION 1414.75

STARTED Sept. 8 | FINISHED Sept. 9 | LOGGED by I. Lyn date

LEGEND	
W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1	14.4		Serpentinite, medium green, mottled, low grade fibre	
			8 - 9.1 minor fault, broken and gouge	
14.4	32.4		Fault zone, broken and fractured with sections at gouge, talcy,	
			medium green to dark green. Gouges at 16.8 - 18.2, 19.6 - 21.9,	
			22.6 - 23.8	
32.4	69.4		Medium green, broken, curving joints, talcy, often minor gouges,	
			low grade fibre, broken 36.2 - 38.1, 39.6 - 41.8.	
			50.9 - 57.9 Fault zone, broken & gouges	
69.4	72.8		Fault zone with gouge	
72.8			E.O.H. Rods stuck	

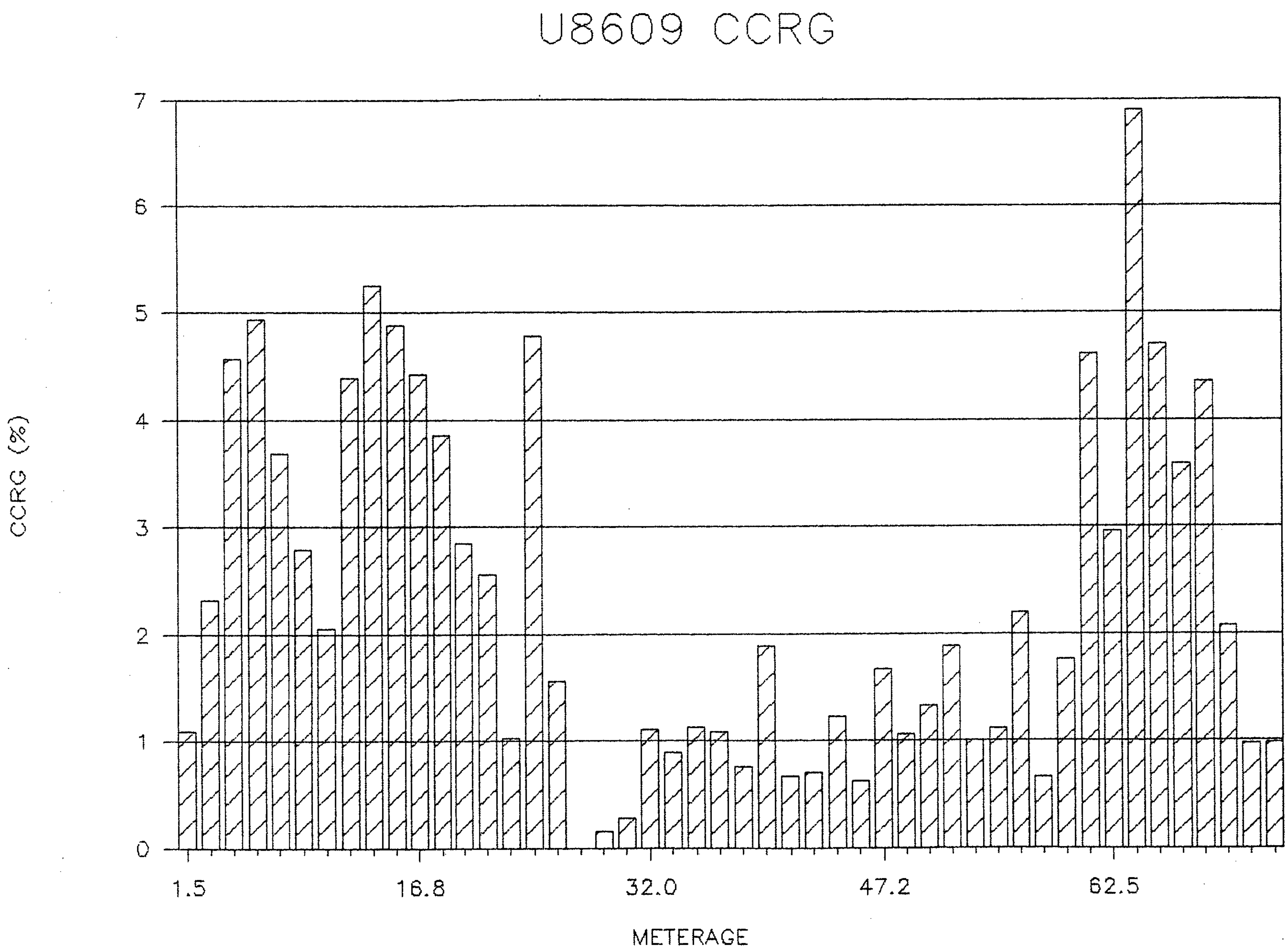
DDH U 8609

AVERAGE OF TWO COUNTS

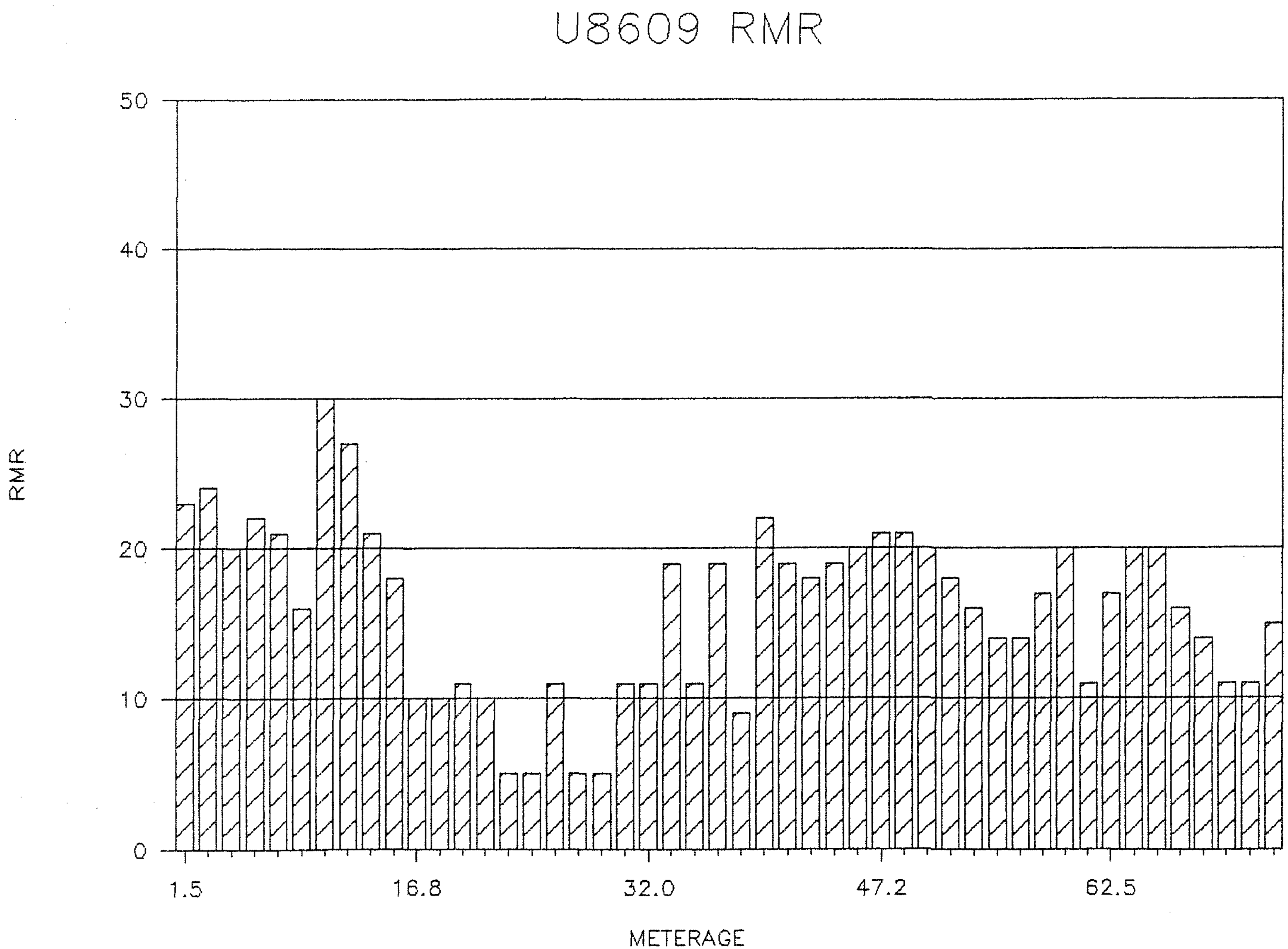
Number of fibre veins counted per 16th category

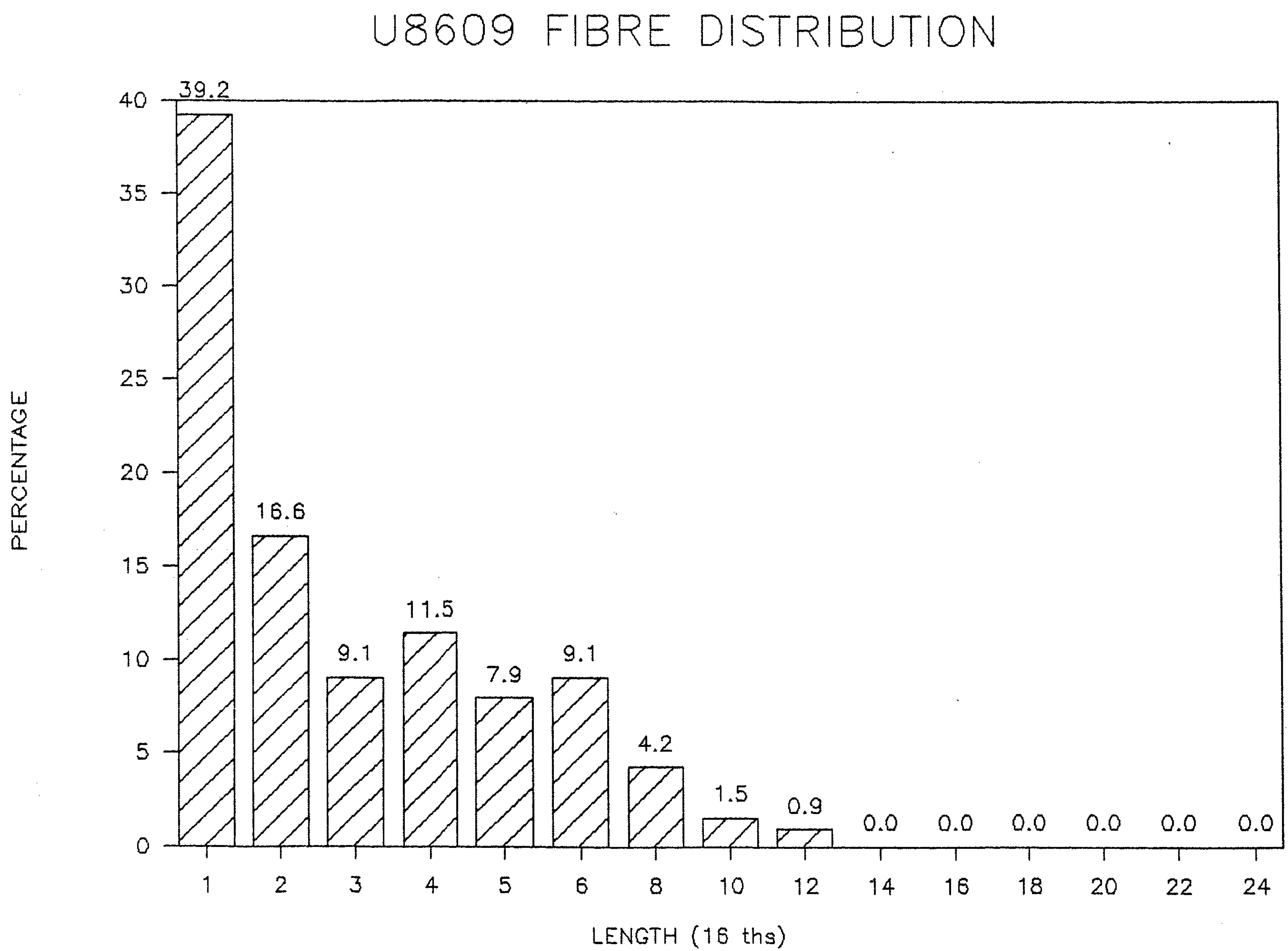
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.0	1.5	0.4	23	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	1.09
1.5	3.0	1.4	24	7.5	2	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	15	2.32
3.0	4.6	1.5	20	7	1	1.5	0	1.5	0	0	1	0	0	0	0	0	0	0	31	4.56
4.6	6.1	1.5	22	4	3	1	1	0.5	1	1	0	0	0	0	0	0	0	0	33.5	4.93
6.1	7.6	1.5	21	9.5	1	2	0.5	1	0	0	0	0	0	0	0	0	0	0	24.5	3.68
7.6	9.1	1.4	16	7	3	0	0	1	0	0	0	0	0	0	0	0	0	0	18	2.79
9.1	10.7	1.5	30	6.5	0.5	0	1.5	0	0	0	0	0	0	0	0	0	0	0	13.5	2.05
10.7	12.2	1.4	27	8.5	3.5	1.5	0.5	0	1	0	0	0	0	0	0	0	0	0	28	4.38
12.2	13.7	1.4	21	3.5	0.5	0.5	1	0.5	1.5	1.5	0	0	0	0	0	0	0	0	33.5	5.24
13.7	15.2	1.4	18	11.5	4	1	1	0	0.5	0	0	0	0	0	0	0	0	0	29.5	4.88
15.2	16.8	1.4	10	6	3.5	0	1	0	1	0.5	0	0	0	0	0	0	0	0	27	4.41
16.8	18.3	1.3	10	8	1	1	1	0.5	0.5	0	0	0	0	0	0	0	0	0	22.5	3.85
18.3	19.8	1.3	11	7.5	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	17	2.84
19.8	21.3	1.1	10	8.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	2.55
21.3	22.9	1.2	5	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.02
22.9	24.4	1.1	5	8	2	0.5	2	0.5	0	0	0	0	0	0	0	0	0	0	24	4.77
24.4	25.9	1.2	11	4.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.56
25.9	27.4	1.0	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27.4	29.0	0.7	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.15
29.0	30.5	0.8	11	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.27
30.5	32.0	0.9	11	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	1.10
32.0	33.5	1.3	19	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.88
33.5	35.1	1.4	11	3.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7	1.12
35.1	36.6	1.4	19	5.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.07
36.6	38.1	1.3	9	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.75
38.1	39.6	1.4	22	10	1	0	0	0	0	0	0	0	0	0	0	0	0	0	12	1.88
39.6	41.1	1.3	19	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.66
41.1	42.7	1.4	18	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.70
42.7	44.2	1.5	19	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.22
44.2	45.7	1.4	20	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.62
45.7	47.2	1.3	21	7	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	10	1.67
47.2	48.8	1.4	21	5.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.05
48.8	50.3	1.4	20	3	0	1	0.5	0	0	0	0	0	0	0	0	0	0	0	8	1.32
50.3	51.8	1.4	18	6.5	1	1	0	0	0	0	0	0	0	0	0	0	0	0	11.5	1.88
51.8	53.3	1.2	16	3.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.00
53.3	54.9	1.0	14	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	1.11
54.9	56.4	1.0	14	1.5	0.5	0.5	0	0	1	0	0	0	0	0	0	0	0	0	10	2.19
56.4	57.9	1.4	17	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.65
57.9	59.4	1.4	20	4	1	0	0	1	0	0	0	0	0	0	0	0	0	0	11	1.76
59.4	61.0	1.1	11	7.5	2	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	23.5	4.61
61.0	62.5	1.4	17	6	3.5	0	0	0.5	0.5	0	0	0	0	0	0	0	0	0	18.5	2.96
62.5	64.0	1.4	20	7.5	1.5	1	2.5	1.5	1.5	0.5	0	0	0	0	0	0	0	0	44	6.89
64.0	65.5	1.4	20	7	1.5	0.5	1	0.5	1	0	0	0.5	0	0	0	0	0	0	30	4.70
65.5	67.1	1.2	16	8.5	2.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	19	3.58
67.1	68.6	1.4	14	5.5	1.5	2	2	1	0	0	0	0	0	0	0	0	0	0	27.5	4.35
68.6	70.1	1.5	11	9	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.07
70.1	71.6	1.4	11	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.97
71.6	72.8	0.5	15	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.98

EOH



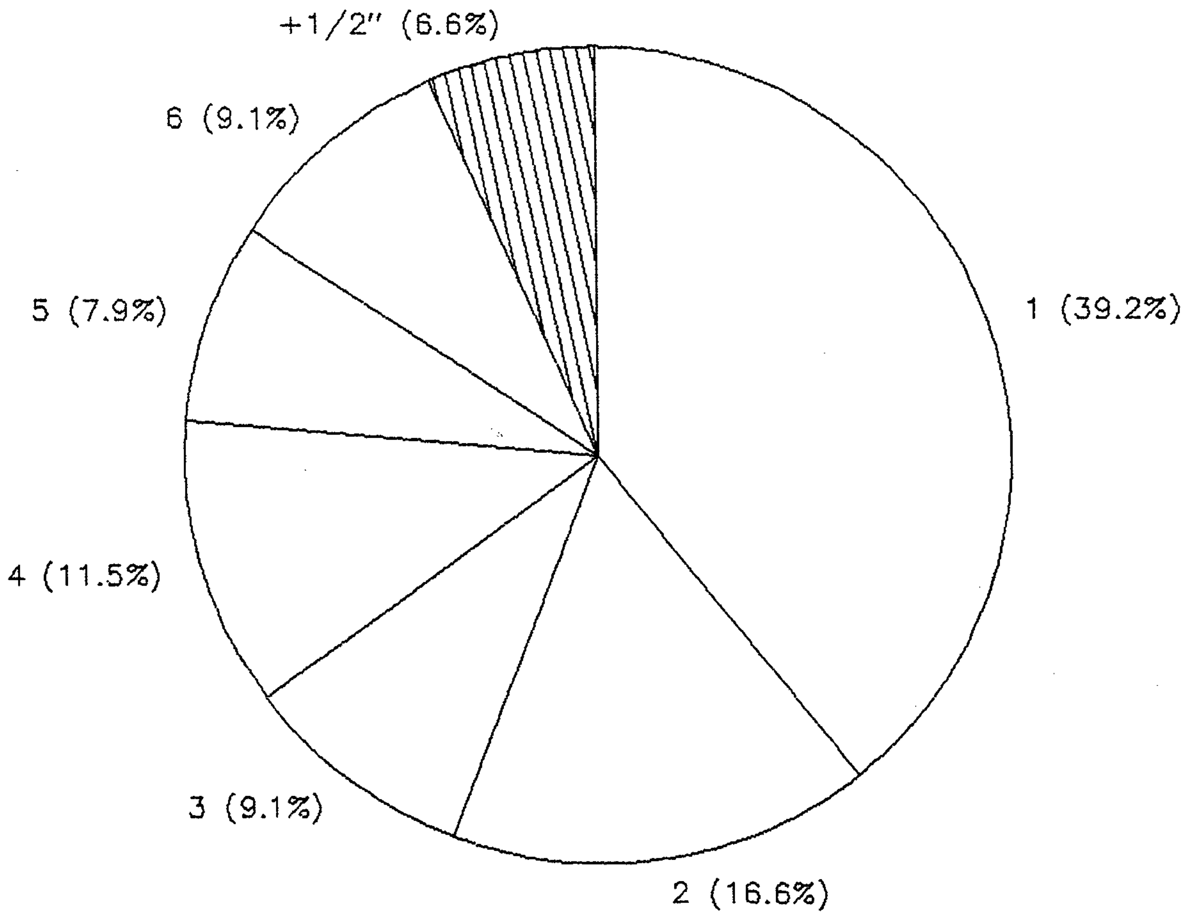
U8609 CCRG
CCRG (%)
0
1
2
3
4
5
6
7
1.5
16.8
32.0
47.2
62.5
METERAGE


U8609 RMR
RMR
0
10
20
30
40
50
1.5
16.8
32.0
47.2
62.5
METERAGE



U8609 FIBRE DISTRIBUTION
PERCENTAGE
40
35
30
25
20
15
10
5
0
39.2
16.6
9.1
11.5
7.9
9.1
4.2
1.5
0.9
0.0
0.0
0.0
0.0
0.0
0.0
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16 ths)

U8609 FIBRE DISTRIBUTION



DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME	HOLE	U86-10	DEPTH	350.22 m
AZIMUTH	90°	INCLINATION	-10.3°	SECTION	6649
LATITUDE	6649.9N	DEPARTURE	7605.6E	ELEVATION	1414.6
STARTED	Sept. 10	FINISHED	Sept. 22	LOGGED	by I. Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
0.5	15.2		Serpentinite, dark green, mottled, low grade fibre	
			12.2 - 14.3 Minor fault with gouge	
15.2	35.4		Fault zone, broken with gouges, main gouges	
			23.4 - 24.7, 27.4 - 30.2	
35.4	51.8		Dark green serpentinite, with poorly developed network of	
			diffuse magnetite veins, minor fibre	
			40.8 - 43.6 Fault zone, broken and cleaved	
			Minor faults 46.9 - 47.8, 55.2 - 55.5	
51.8	92.7		Medium green, parts light green, mottled, fibre bearing, talcy	
			74.6 - 79.7 Minor fault, broken	
92.7	100		Fault zone, dark, cleaved broken and gouge	
100	137.2		Dark green, very broken, many joints with lizardite and talc,	
			sparse - no fibre	
			Fault zones 113 - 114.9, 124.9 - 129.7	
			130.15 reduced HQ to NQ	
137.2	249.9		Gradual change to dark-medium green, mottled, fibre bearing	
			Very little breakage or faults - joints	
249.9	284.8		Gradual change to dark, slightly greyish green, diffuse	
			magnetite veins, talcy, sparse fibre, little breakage	
284.8	288		Rodingite Dyke with reaction rims of ~ 0.45 m. Non-magnetic	
			serpentinite each side	
288	291.6		Very dark green serpentinite	
291.6	293		Rodingite Dyke with ~ .2 m rims of non-magnetic serpentine	
293	349.6		Very dark greyish green serp. 303.3 - 306.3 Fault zone, broken	
			320.2 - 322.2 Fault, core lost, broken to 326.7, minor broken	

.../2

FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME | HOLE U86-10 | DEPTH 350.22 m

AZIMUTH 90° | INCLINATION -10.3° | SECTION 6649

LATITUDE 6649.9N | DEPARTURE 7605.6E | ELEVATION 1414.6

STARTED Sept.10 | FINISHED Sept. 22 | LOGGED by I. Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
			sections to 342. Picrolite and brucite on joints	
			344.7 - 345.3 Altered serp.	
349.6			E.O.H.	

DDH U 8610

AVERAGE OF TWO COUNTS

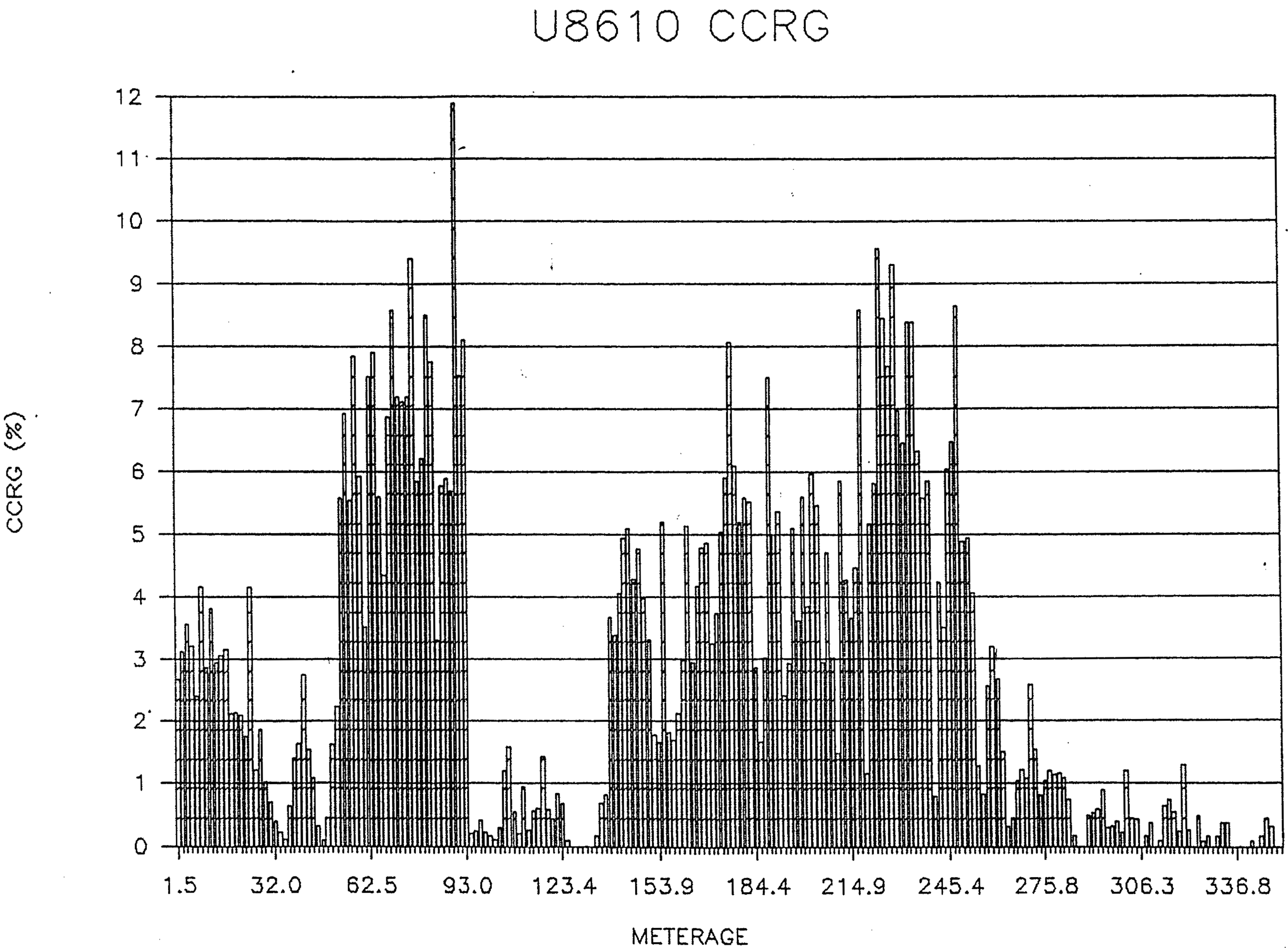
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
				Number of fibre veins counted per 16th category																
0.0	1.5	1.1	26	4.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	2.66
1.5	3.0	1.4	26	7	1	1	0	0.5	0	0	0.5	0	0	0	0	0	0	0	19.5	3.12
3.0	4.6	1.4	17	8	2	2	0	0	0	0	0.5	0	0	0	0	0	0	0	23	3.56
4.6	6.1	1.4	21	5.5	4	1	1	0	0	0	0	0	0	0	0	0	0	0	20.5	3.21
6.1	7.6	1.4	11	5	1.5	0.5	0	0	1	0	0	0	0	0	0	0	0	0	15.5	2.40
7.6	9.1	1.4	21	8.5	2	1	1	0.5	0	0.5	0	0	0	0	0	0	0	0	26	4.16
9.1	10.7	1.4	29	4	3	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	17.5	2.86
10.7	12.2	1.3	24	7.5	2	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	22.5	3.80
12.2	13.7	1.4	10	12	0	0	0.5	0	0	0.5	0	0	0	0	0	0	0	0	18	2.94
13.7	15.2	1.4	10	10	1.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	18.5	3.06
15.2	16.8	1.3	10	13	1	1	0	0	0	0	0	0	0	0	0	0	0	0	18	3.15
16.8	18.3	1.1	19	7.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	10.5	2.11
18.3	19.8	1.4	16	4.5	2	0	0	1	0	0	0	0	0	0	0	0	0	0	13.5	2.13
19.8	21.3	1.0	11	8	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	2.10
21.3	22.9	1.2	5	6	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.74
22.9	24.4	1.2	5	7.5	3	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	22.5	4.14
24.4	25.9	1.4	16	6.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.21
25.9	27.4	1.1	5	6	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.86
27.4	29.0	1.5	5	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.03
29.0	30.5	1.3	11	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.69
30.5	32.0	1.2	16	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.38
32.0	33.5	1.0	11	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.22
33.5	35.1	1.0	11	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.11
35.1	36.6	1.4	21	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4	0.63
36.6	38.1	1.4	16	4.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9	1.41
38.1	39.6	1.4	21	5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	1.64
39.6	41.1	1.1	11	8	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	14	2.74
41.1	42.7	1.2.	11	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.55
42.7	44.2	1.2	11	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.07
44.2	45.7	1.4	20	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.31
45.7	47.2	1.3	18	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
47.2	48.8	1.2	5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.45
48.8	50.3	1.2	16	5.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	9	1.61
50.3	51.8	1.4	17	8	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	14	2.24
51.8	53.3	1.1	19	6	1	2	1	0	1	0.5	0	0	0	0	0	0	0	0	28	5.57
53.3	54.9	1.3	19	7	4	1.5	3	0.5	1	0	0	0	0	0	0	0	0	0	40	6.93
54.9	56.4	1.5	9	3	2.5	1	1	1.5	0.5	0	0.5	0.5	0	0	0	0	0	0	36.5	5.54
56.4	57.9	1.4	16	6.5	3	1	1	0.5	2.5	1.5	0	0	0	0	0	0	0	0	49	7.84
57.9	59.4	1.4	9	6.5	1	0	1	0.5	1	1	0	0	0	0.5	0	0	0	0	37	5.92
59.4	61.0	1.5	9	9	2	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	23	3.52
61.0	62.5	1.4	19	10	4.5	1	1	1	2	0	0.5	0	0	0	0	0	0	0	48	7.52
62.5	64.0	1.5	12	6	2.5	1	2.5	2.5	1	0.5	0.5	0	0	0	0	0	0	0	51.5	7.90
64.0	65.5	1.4	19	6.5	2	1.5	1	0.5	1.5	0.5	0	0	0	0	0	0	0	0	34.5	5.58
65.5	67.1	1.4	9	7	2	1	1.5	1	0.5	0	0	0	0	0	0	0	0	0	28	4.34
67.1	68.6	1.4	14	6.5	1	1.5	1	1.5	2	0	0.5	0	0	0	0	0	0	0	41.5	6.86
68.6	70.1	1.4	23	5	1.5	0.5	1.5	0.5	1	1.5	0.5	1	0	0	0	0	0	0	53	8.57
70.1	71.6	1.3	13	6.5	2.5	2	1.5	1	0.5	0	0.5	0.5	0	0	0	0	0	0	42.5	7.19
1.6	73.2	1.4	21	7	3	4	2	0.5	1.5	0	0	0	0	0	0	0	0	0	44.5	7.12
3.2	74.7	1.3	17	5	1	1	1	0	4	0.5	0	0	0	0	0	0	0	0	42	7.19
74.7	76.2	1.2	12	8.5	4	2.5	1	0.5	0.5	1	0	0	0.5	0	0	0	0	0	48.5	9.40
76.2	77.7	1.3	16	7	3.5	1	2.5	1.5	0	0	0	0	0	0	0	0	0	0	34.5	5.84
77.7	79.2	1.2	10	4.5	5	2.5	1	0	1	0	0	0	0	0	0	0	0	0	32	6.20

79.2	80.8	1.3	10	6.5	3	1.5	1	0.5	0.5	1.5	1	0	0	0	0	0	0	0	48.5	8.50
80.8	82.3	1.4	17	6.5	3.5	3	0.5	0.5	0.5	1	0.5	0	0.5	0	0	0	0	0	50	7.75
82.3	83.8	1.4	10	5.5	3	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	20.5	3.31
83.8	85.3	1.4	10	9	1.5	2.5	0.5	0.5	2	0	0	0	0	0	0	0	0	0	36	5.76
85.3	86.9	1.3	15	9.5	4.5	1.5	0.5	0.5	0	0	0	0.5	0	0	0	0	0	0	33.5	5.87
86.9	88.4	1.2	7	7	4	1.5	0.5	0	0	0.5	0.5	0	0	0	0	0	0	0	30.5	5.68
88.4	89.9	1.2	8	6.5	6	2	2.5	1	0.5	1.5	1	0	0	0	0	0	0	0	64.5	11.8
89.9	91.4	1.2	11	8	4	1.5	1.5	0.5	0.5	1	0	0	0	0	0	0	0	0	40	7.55
91.4	93.0	1.2	8	7	3	2	1.5	1	1	1	0	0	0	0	0	0	0	0	44	8.10
93.0	94.5	1.1	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
94.5	96.0	0.9	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.24
96.0	97.5	0.8	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.40
97.5	99.1	1.1	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.21
99.1	100.6	1.5	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
100.6	102.1	1.1	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
102.1	103.6	1.2	14	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.28
103.6	105.2	1.4	16	4	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.20
105.2	106.7	1.2	9	3.5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.58
106.7	108.2	1.4	8	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	3.5	0.54
108.2	109.7	1.2	20	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
109.7	111.3	1.4	18	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.96
111.3	112.8	0.9	19	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.26
112.8	114.3	1.0	9	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.57
114.3	115.8	1.1	18	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.60
115.8	117.3	0.9	15	3.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6	1.42
117.3	118.9	1.0	14	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.58
118.9	120.4	1.1	16	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.42
120.4	121.9	1.4	14	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.82
121.9	123.4	1.5	20	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.69
123.4	125.0	1.3	19	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
125.0	126.5	1.0	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
126.5	128.0	1.2	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
128.0	129.5	1.1	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
129.5	131.1	1.3	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
131.1	132.6	1.2	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
132.6	134.1	1.4	19	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
134.1	135.6	1.5	20	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.69
135.6	137.2	1.4	19	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.80
137.2	138.7	1.4	21	12	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	22.5	3.68
138.7	140.2	1.5	31	9.5	2.5	2	0	0.5	0	0	0	0	0	0	0	0	0	0	23	3.38
140.2	141.4	1.5	32	7.5	2.5	1	0	0	2	0	0	0	0	0	0	0	0	0	27.5	4.05
141.7	143.3	1.5	27	9	2	1	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	33.5	4.93
143.3	144.8	1.5	28	12.5	3.5	3	1.5	0	0	0	0	0	0	0	0	0	0	0	34.5	5.08
144.8	146.3	1.5	30	8.5	3.5	1	0.5	1	0.5	0	0	0	0	0	0	0	0	0	28.5	4.28
146.3	147.8	1.5	21	12	4	1	1.5	0	0.5	0	0	0	0	0	0	0	0	0	32	4.76
147.8	149.4	1.5	24	7.5	2	0.5	1.5	0	0	1	0	0	0	0	0	0	0	0	27	3.97
149.4	150.9	1.3	23	9.5	2.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	19.5	3.30
150.9	152.4	1.5	25	3.5	0	0	0	0.5	1	0	0	0	0	0	0	0	0	0	12	1.76
152.4	153.9	1.5	21	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	11	1.65
153.9	155.4	1.5	21	4.5	1.5	1	1	1	0	1	0	0	0.5	0	0	0	0	0	34.5	5.18
155.4	157.0	1.5	25	7.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	12	1.80
157.0	158.5	1.5	32	5	0.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	11.5	1.69
158.5	160.0	1.5	30	2	1	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	14	2.12
160.0	161.5	1.4	23	8	1.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	19	2.97
161.5	163.1	1.5	25	11.5	1.5	0.5	2.5	0.5	0	0	0.5	0	0	0	0	0	0	0	33.5	5.14
163.1	164.6	1.5	21	10.5	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	20	2.94

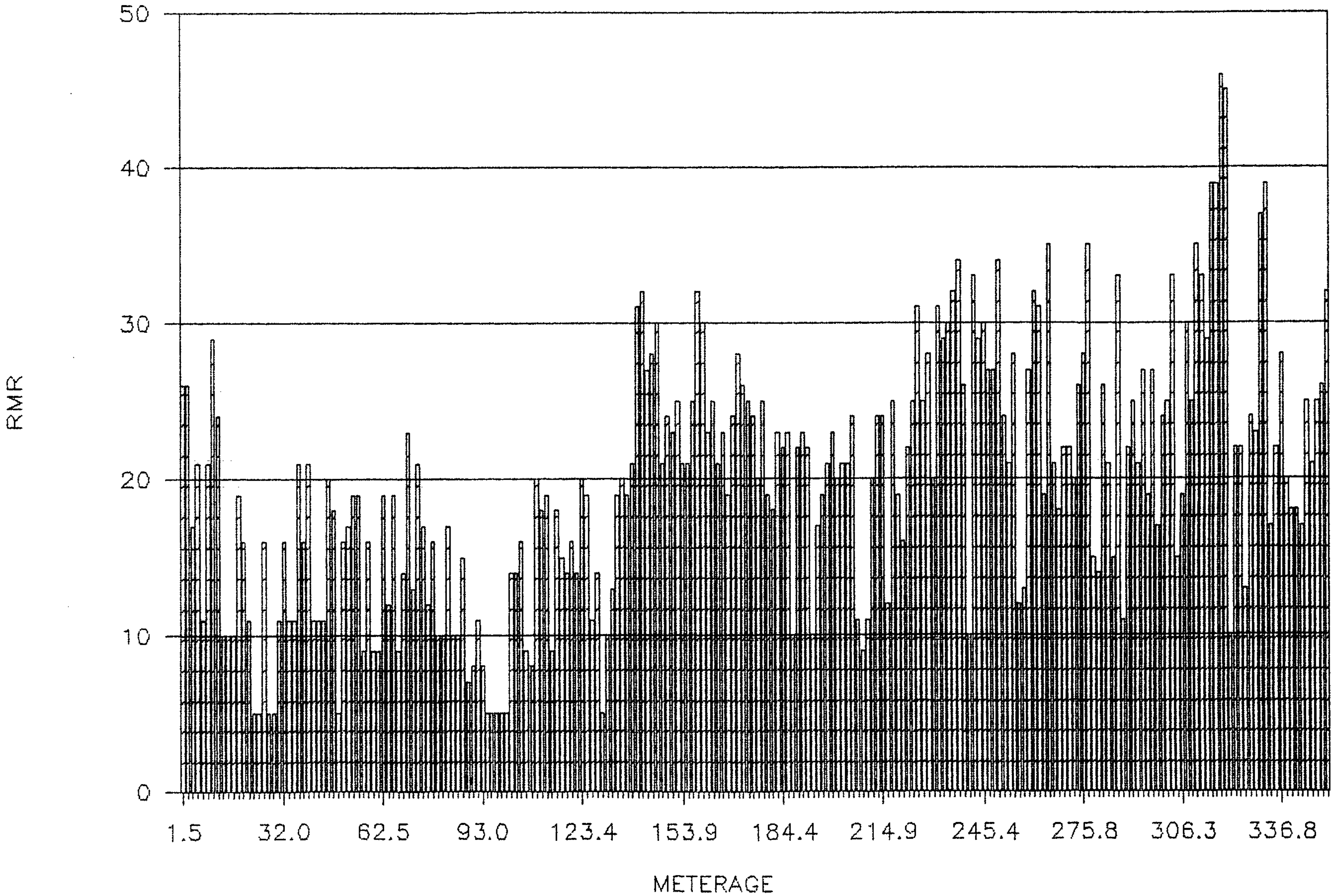
164.6	166.1	1.5	23	3.5	1.5	1.5	1	1	0.5	0	0.5	0	0	0	0	0	0	0	28	4.16
166.1	167.6	1.5	19	7	2.5	1.5	1	0	0.5	0.5	0.5	0	0	0	0	0	0	0	32.5	4.78
167.6	169.2	1.5	24	11	2.5	1	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	33	4.86
169.2	170.7	1.5	28	2.5	1.5	2.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	22	3.24
170.7	172.2	1.4	26	3.5	1	0.5	1.5	1	0	0	0.5	0	0	0	0	0	0	0	23	3.72
172.2	173.7	1.4	25	6	2	0.5	0.5	1	1	0	0	0	0.5	0	0	0	0	0	31.5	5.04
173.7	175.3	1.5	24	7	3.5	2	0	0.5	1	0.5	0	0.5	0	0	0	0	0	0	38.5	5.90
175.3	176.8	1.4	20	8	3	1.5	3.5	1	0.5	0	0.5	0.5	0	0	0	0	0	0	51.5	8.07
176.8	178.3	1.5	25	10.5	5.5	0.5	0	0.5	0.5	1.5	0	0	0	0	0	0	0	0	40.5	6.08
178.3	179.8	1.4	19	7.5	5	0.5	2	0.5	0	0.5	0	0	0	0	0	0	0	0	33.5	5.19
179.8	181.4	1.5	18	10	4.5	1.5	0.5	1.5	0	0.5	0	0	0	0	0	0	0	0	37	5.56
181.4	182.9	1.5	23	5.5	3.5	1.5	0.5	0.5	0.5	1	0.5	0	0	0	0	0	0	0	37.5	5.52
182.9	184.4	1.5	22	6.5	2.5	0.5	0	0.5	0	0.5	0	0	0	0	0	0	0	0	19.5	2.87
184.4	185.9	1.5	23	6	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	11	1.65
185.9	187.5	1.4	10	12.5	1	0	0	1	0	0	0	0	0	0	0	0	0	0	19.5	3.02
187.5	189.0	1.5	22	19.5	4	2.5	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	50.5	7.51
189.0	190.5	1.5	23	10	6.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	32.5	4.98
190.5	192.0	1.3	22	9	2.5	1	1.5	1	0	0.5	0	0	0	0	0	0	0	0	32	5.35
192.0	193.5	1.3	10	9	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	14	2.39
193.5	195.1	1.5	17	7	1	1	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	19.5	2.93
195.1	196.6	1.5	19	14	2	1.5	0	1	0.5	0.5	0	0	0	0	0	0	0	0	34.5	5.08
196.6	198.1	1.5	21	5	2	0	1	1	1	0	0	0	0	0	0	0	0	0	24	3.60
198.1	199.6	1.5	23	9.5	1.5	2.5	2	2	0	0	0	0	0	0	0	0	0	0	38	5.59
199.6	201.2	1.5	20	7.5	0.5	0.5	0.5	0.5	0	0.5	0	0	0.5	0	0	0	0	0	25.5	3.83
201.2	202.7	1.5	21	6	1.5	0.5	3	0.5	0	0	0	0	0.5	0.5	0	0	0	0	40	5.95
202.7	204.2	1.5	21	9.5	2.5	0.5	1	0	0.5	0	0	0.5	0	0.5	0	0	0	0	37	5.45
204.2	205.7	1.4	24	9	1.5	1	1	0	0	0	0	0	0	0	0	0	0	0	19	2.94
205.7	207.3	1.4	11	8.5	1	1.5	0.5	0	1.5	0.5	0	0	0	0	0	0	0	0	30	4.70
207.3	208.8	1.4	9	5	0.5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	18.5	3.02
208.8	210.3	1.4	11	6	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	9.5	1.48
210.3	211.8	1.5	20	11.5	2.5	2.5	1.5	0	0	1	0	0	0	0	0	0	0	0	38	5.83
211.8	213.4	1.5	24	13	3	1	0	0	0.5	0.5	0	0	0	0	0	0	0	0	29	4.27
213.4	214.9	1.5	24	10	2.5	1.5	0	1	0	0	0	0	0	0	0	0	0	0	24.5	3.64
214.9	216.4	1.5	12	16	3	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	29	4.44
216.4	217.9	1.5	25	14.5	2.5	3	0.5	2	2	0.5	0	0	0	0	0	0	0	0	56.5	8.57
217.9	219.5	1.4	19	6.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.16
219.5	221.0	1.3	16	6	3	0.5	1	0	0	1.5	0	0	0	0	0	0	0	0	29.5	5.17
221.0	222.5	1.4	22	8.5	1	1.5	0.5	1	0	1	0	0	0.5	0	0	0	0	0	37	5.79
222.5	224.0	1.5	25	6.5	3	3	1	1.5	1.5	1	0.5	0	0	0.5	0	0	0	0	63	9.56
224.0	225.6	1.5	31	6.5	2.5	2.5	1	2	2	0.5	0	0.5	0	0	0	0	0	0	55	8.43
225.6	227.1	1.4	25	7	2.5	3	2.5	1.5	0	0	0.5	0.5	0	0	0	0	0	0	49.5	7.67
227.1	228.6	1.4	28	9	2	3.5	1.5	0	0	0.5	0	0.5	0	0	1	0	0	0	57.5	9.30
228.6	230.1	1.4	20	6.5	2	1	0.5	1.5	1.5	1.5	0	0	0	0	0	0	0	0	44	6.96
230.1	231.6	1.5	31	8	2.5	1	1	0.5	0.5	0.5	0.5	0	0	0.5	0	0	0	0	42.5	6.45
231.6	233.2	1.5	29	10.5	4	2.5	1.5	3	1	0.5	0	0	0	0	0	0	0	0	57	8.39
233.2	234.7	1.5	30	5.5	3.5	3	0.5	0.5	1	1	0.5	1	0	0	0	0	0	0	57	8.39
234.7	236.2	1.5	32	14	8	2	1	0.5	0	0	0	0	0	0	0	0	0	0	42.5	6.32
236.2	237.7	1.5	34	9.5	3.5	2	1.5	0.5	1	0	0	0	0	0	0	0	0	0	37	5.56
237.7	239.3	1.5	26	8	1	2	1.5	1	0.5	1	0	0	0	0	0	0	0	0	38	5.83
239.3	240.8	1.4	10	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.79
240.8	242.3	1.4	33	9	3	2	1.5	0	0	0	0	0	0	0	0	0	0	0	27	4.23
242.3	243.8	1.5	29	6.5	2.5	2.5	1	0	0	0	0	0	0	0	0	0	0	0	23	3.49
243.8	245.4	1.5	30	4.5	5	2	1.5	0.5	2	0	0	0	0	0	0	0	0	0	41	6.03
245.4	246.9	1.5	27	3.5	2	2	0.5	1.5	2	0.5	0.5	0	0	0	0	0	0	0	44	6.48
246.9	248.4	1.5	27	17	7	5.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	57.5	8.64
248.4	249.9	1.4	34	5.5	2	1.5	1.5	1.5	0	0.5	0	0	0	0	0	0	0	0	31.5	4.88

249.9	251.5	1.4	24	9	1	1	1.5	0.5	1.5	0	0	0	0	0	0	0	0	0	31.5	4.93
251.5	253.0	1.5	21	7.5	2	0.5	1.5	1.5	0	0	0	0	0	0	0	0	0	0	26.5	4.06
253.0	254.5	1.5	28	7.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.26
254.5	256.0	1.5	12	4	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.84
256.0	257.6	1.4	13	12.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	16	2.56
257.6	259.1	1.4	27	7	1.5	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	19.5	3.19
259.1	260.6	1.5	32	7	0	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	17.5	2.68
260.6	262.1	1.4	31	5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.50
262.1	263.7	1.4	19	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.31
263.7	265.2	1.5	35	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.44
265.2	266.7	1.3	21	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.03
266.7	268.2	1.3	18	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.22
268.2	269.7	1.4	22	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.08
269.7	271.3	1.5	22	11	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	17.5	2.57
271.3	272.8	1.5	20	6	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.54
272.8	274.3	1.5	26	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.81
274.3	275.8	1.5	28	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.04
275.8	277.4	1.5	35	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.19
277.4	278.9	1.4	15	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.14
278.9	280.4	1.5	14	4	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	7.5	1.15
280.4	281.9	1.4	26	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.08
281.9	283.5	1.4	21	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.74
283.5	285.0	1.4	15	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
285.0	286.5	1.4	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
286.5	288.0	1.3	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
288.0	289.6	1.4	22	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.48
289.6	291.1	1.5	25	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.52
291.1	292.6	1.5	21	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.59
292.6	294.1	1.5	27	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.88
294.1	295.7	1.5	19	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.29
295.7	297.2	1.4	27	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.31
297.2	298.7	1.4	17	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.38
298.7	300.2	1.5	24	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.22
300.2	301.8	1.5	25	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.19
301.8	303.3	1.5	33	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.46
303.3	304.8	1.3	15	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.42
304.8	306.3	1.5	19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
306.3	307.8	1.4	30	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
307.8	309.4	1.5	25	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.37
309.4	310.9	1.5	35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
310.9	312.4	1.4	33	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.07
312.4	313.9	1.4	29	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.63
313.9	315.5	1.5	39	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.73
315.5	317.0	1.5	39	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.53
317.0	318.5	1.4	46	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.24
318.5	320.0	1.3	45	5.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.29
320.0	321.6	0.4	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.26
321.6	323.1	0.9	22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
323.1	324.6	1.4	22	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.48
324.6	326.1	1.2	13	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
326.1	327.7	1.4	24	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
327.7	329.2	1.4	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
329.2	330.7	1.4	37	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
330.7	332.2	1.5	39	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.36
332.2	333.8	1.5	17	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.37
333.8	335.3	1.5	22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

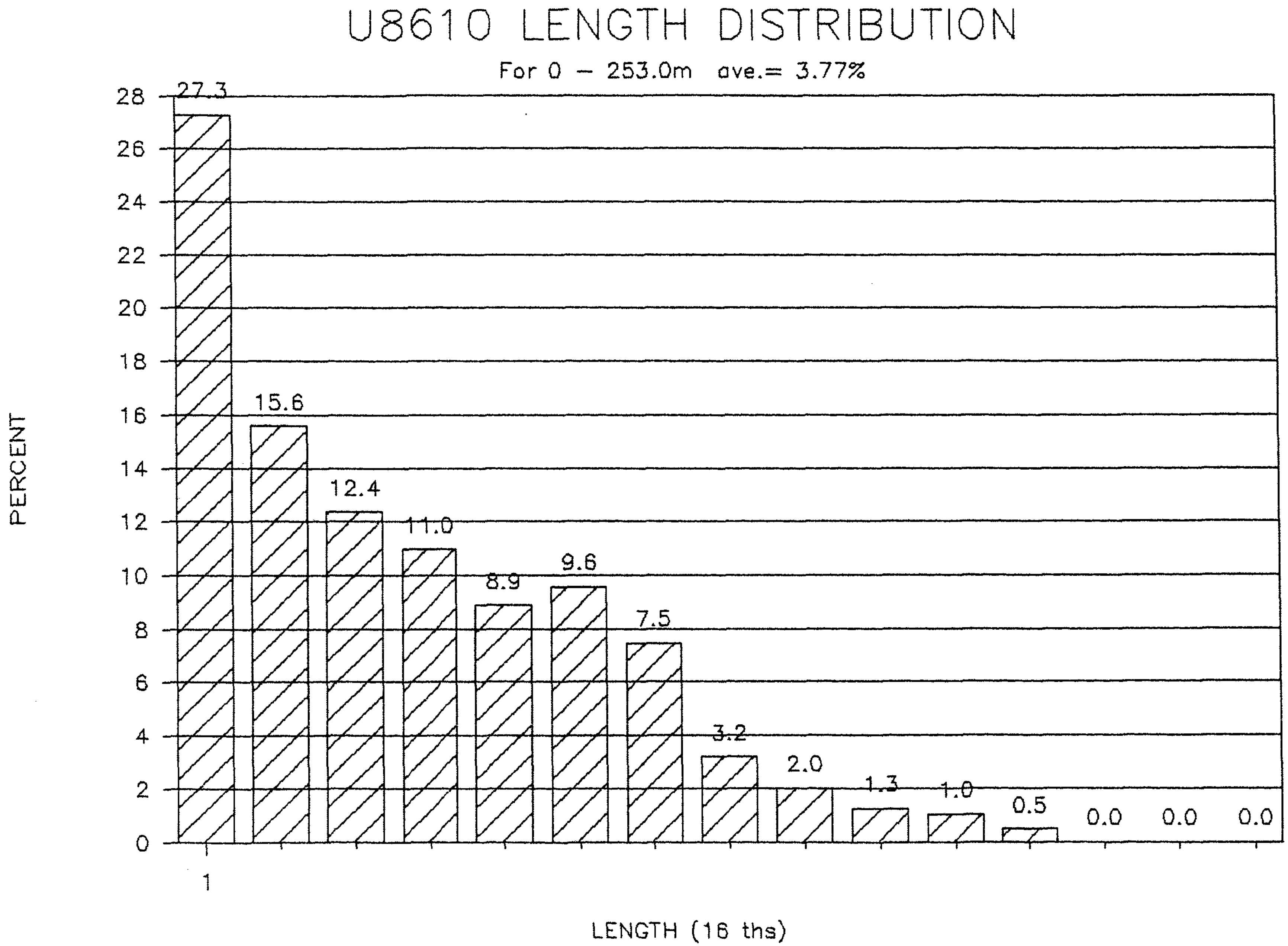
335.3	336.8	1.4	28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
336.8	338.3	1.5	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
338.3	339.9	1.2	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
339.9	341.4	1.3	18	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
341.4	342.9	1.3	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
342.9	344.4	1.4	25	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
344.4	345.9	1.5	21	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.45
345.9	347.5	1.5	25	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.30
347.5	349.0	1.4	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
349.0	350.2	1.3	32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0


U8610 CCRG
12
11
10
9
8
7
6
5
4
3
2
1
0
CCRG (%)
1.5
32.0
62.5
93.0
123.4
153.9
184.4
214.9
245.4
275.8
306.3
336.8
METERAGE

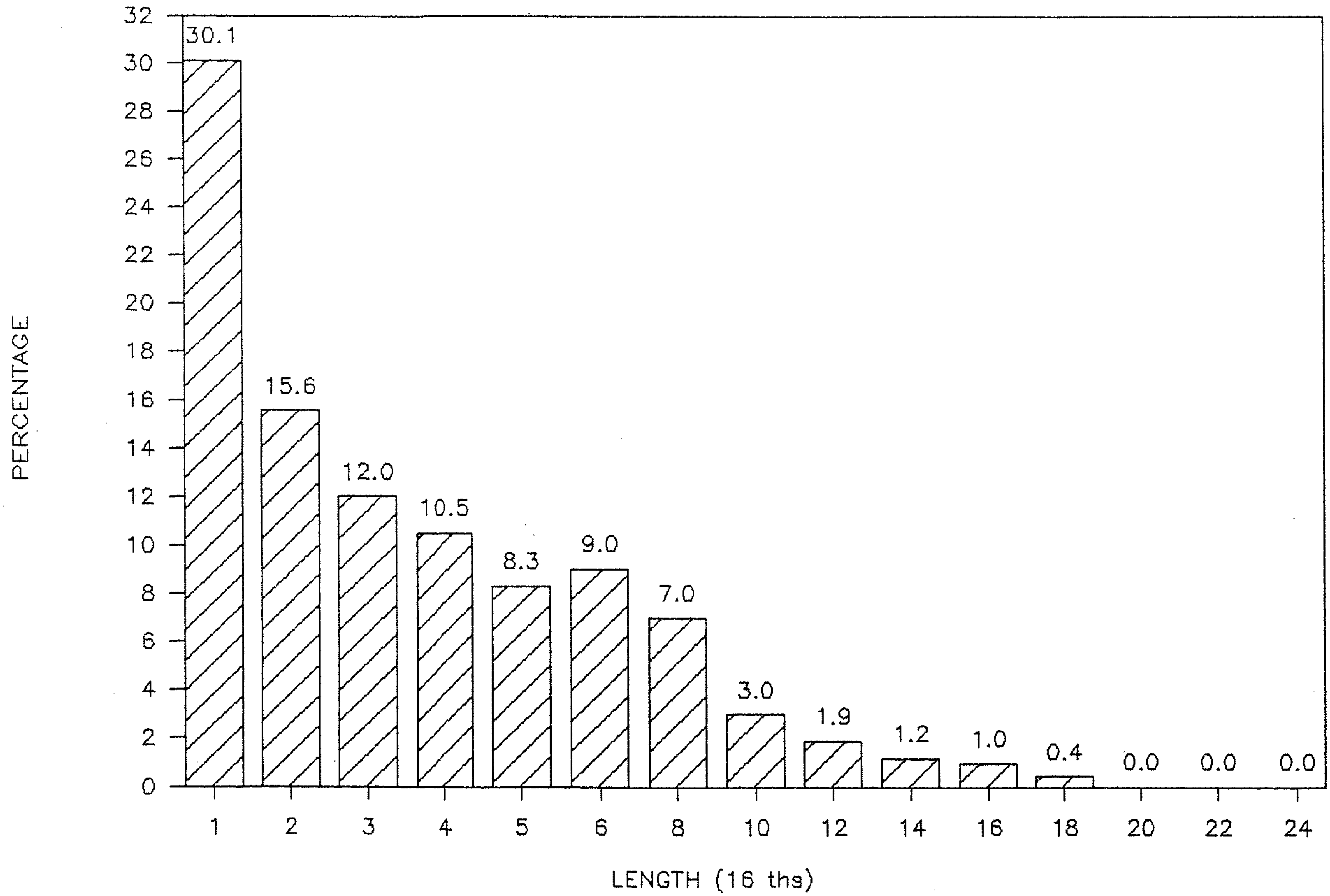
U8610 RMR



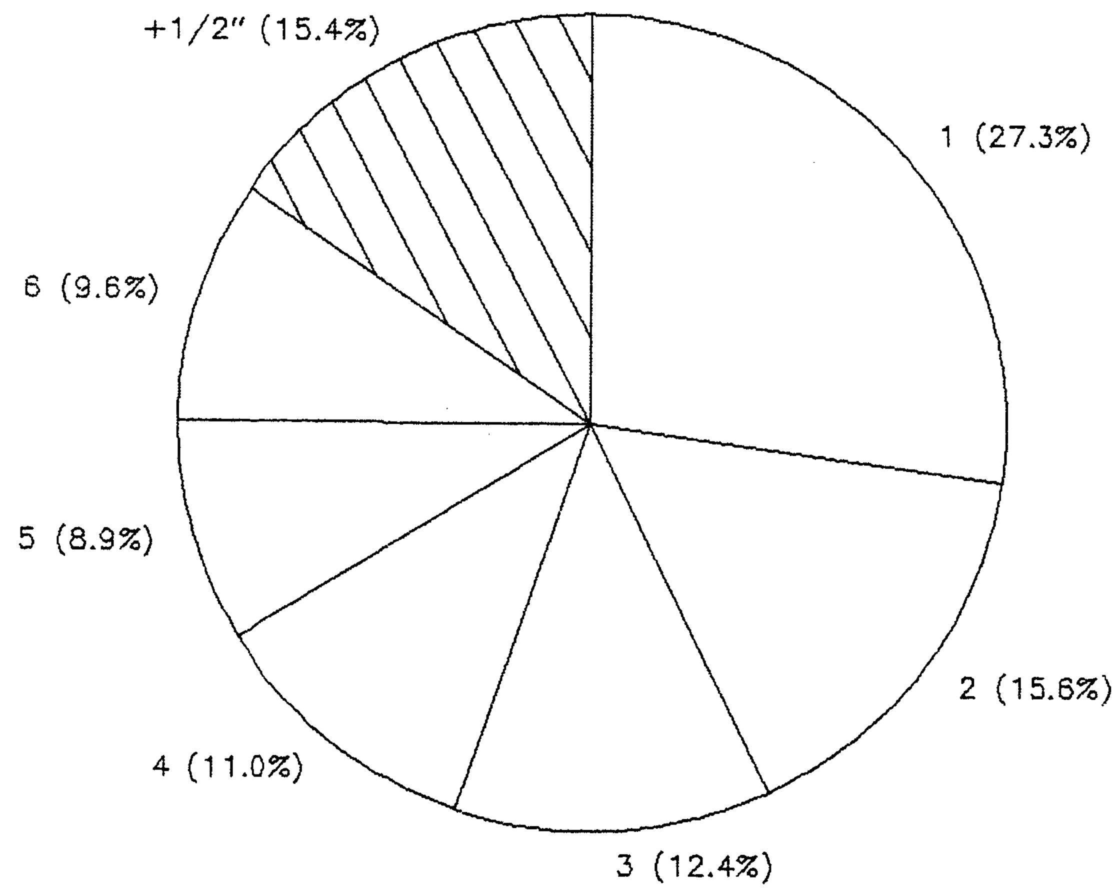
RMR
50
40
30
20
10
0
1.5
32.0
62.5
93.0
123.4
153.9
184.4
214.9
245.4
275.8
306.3
336.8
METERAGE


U8610 LENGTH DISTRIBUTION
For 0 – 253.0m ave.= 3.77%
PERCENT
LENGTH (16 ths)
28
26
24
22
20
18
16
14
12
10
8
6
4
2
0
1
27.3
15.6
12.4
11.0
8.9
9.6
7.5
3.2
2.0
1.3
1.0
0.5
0.0
0.0
0.0

U8610 FIBRE DISTRIBUTION



U8610 LENGTH DISTRIBUTION



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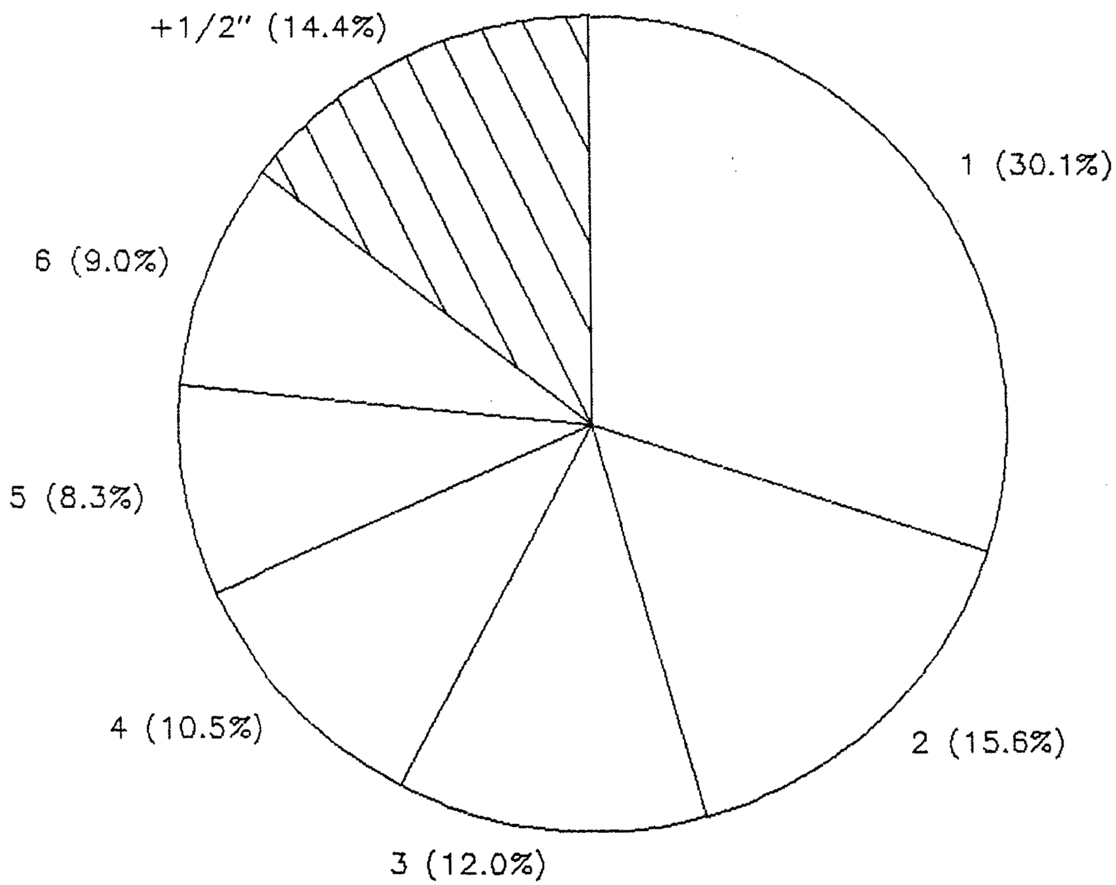


FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME | HOLE - U86-11 | DEPTH 299.3

AZIMUTH 90 | INCLINATION -18.4 | SECTION 6649

LATITUDE 6649.9N | DEPARTURE 7605.85E | ELEVATION 1414.3

STARTED Sept. 22 | FINISHED Oct. 4 | LOGGED by I. Lyn date

LEGEND	
W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
0.37	58.5		Serpentinite, dark-medium green, low grade fibre bearing,	
			fractured, broken sections and scattered thin gouges	
			Fault zones @ 6.3 - 9.4, 11.8 - 12.8, 14.3 - 17.4, 26.4 - 36.6,	
			40.4 - 42.5, 44.8 - 45.8	
			53.3 - 58.5 Fault zone, cleaved and broken, talcy	
58.5	112.9		Medium green, mottled, good fibre, broken	
			Fault zones @ 61 - 62.33	
			92 - 99.8 Shear zone, rock generally hard and compact	
112.9	130.2		Fault zone, broken & fractured, main gouge at 123.4 - 127.	
			Talcy, lizardite veins, changes colour to dark green	
130.2	173.2		Dark green, minor fibre, broken, and occasional minor fault	
			zones.	
			165.9 - 173.2 Fault zone, fractured and gouge	
173.2	299.3		Medium green, fibre bearing, little fractured, occasional	
			lizardite veins, talcy.	
			178.9 Reduce HQ to NQ	
			Minor fibre below 282 m, sparse below 291 m	
299.3			E.O.H.	

DDH U 8611

AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

FROM M	TO M	REC M	RQD	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.0	1.5	1.3	22	9	3.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	24	4.06
1.5	3.0	1.3	22	6.5	1	3	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	29	4.91
3.0	4.6	1.4	28	7	1.5	0.5	0	0	0.5	0	0	0.5	0	0	0	0	0	0	20.5	3.31
4.6	6.1	1.5	18	5	2	2	0	0.5	0	0	0	0	0	0	0	0	0	0	17.5	2.60
6.1	7.6	1.2	9	5.5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.88
7.6	9.1	1.3	9	6	2.5	0.5	1.5	0.5	0	1.5	0	0	0	0	0	0	0	0	33	5.85
9.1	10.7	1.4	19	5.5	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.23
10.7	12.2	1.4	5	7.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	11.5	1.84
12.2	13.7	1.3	5	9.5	3	0	0	0	0	0	0	0	0	0	0	0	0	0	15.5	2.62
13.7	15.2	1.1	5	6.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.34
15.2	16.8	1.1	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
16.8	18.3	1.2	9	5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.34
18.3	19.8	1.0	10	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.35
19.8	21.3	1.0	9	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.75
21.3	22.9	1.2	10	5	4	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	20.5	3.92
22.9	24.4	1.1	16	7.5	3.5	1.5	0	0	0	1	0	0	0.5	0	0	0	0	0	34	6.76
24.4	25.9	1.2	10	7	4	0	1	0.5	1.5	1	0	0.5	0	0.5	0	0	0	0	52.5	9.78
25.9	27.4	1.0	8	6	1.5	0	0.5	2	0.5	0	0	0.5	0	0.5	0	0	0	0	38	8.88
27.4	29.0	1.1	11	5	1	0	1.5	0.5	0	0	0	0	0	0	0	0	0	0	15.5	3.21
29.0	30.5	1.2	10	5	2	1	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	19.5	3.54
30.5	32.0	1.4	11	7.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	1.71
32.0	33.5	1.4	12	7	1	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.44
33.5	35.1	1.2	12	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.13
35.1	36.6	1.4	17	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.73
36.6	38.1	1.4	16	6	0.5	0	0	0.5	0.5	0	0	0	0	0	0	0	0	0	12.5	2.04
38.1	39.6	1.4	17	5	3.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	18	2.79
39.6	41.1	1.1	16	4.5	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	16	3.27
41.1	42.7	1.5	15	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.61
42.7	44.2	1.5	16	5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.45
44.2	45.7	1.4	16	3.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.88
45.7	47.2	1.4	19	7.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.68
47.2	48.8	1.3	19	7	3	1	0	0	0	0	0	0	0	0	0	0	0	0	16	2.77
48.8	50.3	1.3	18	5.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.68
50.3	51.8	1.4	16	7.5	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	15	2.45
51.8	53.3	1.1	14	8	2	0	0	0	0.5	0	0	0	0	0	0	0	0	0	15	3.02
53.3	54.9	1.1	5	7	3.5	1.5	0.5	0	0.5	1.5	0	0	0	0	0	0	0	0	35.5	6.97
54.9	56.4	1.1	9	7	3.5	0.5	0	0.5	1.5	0	0	0	0	0	0	0	0	0	27	5.37
56.4	57.9	1.1	5	2.5	2.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	14	2.86
57.9	59.4	1.2	5	4	5	1	1	1.5	1	0.5	0	0	0	0	0	0	0	0	38.5	7.00
59.4	61.0	1.4	15	7	4	1	1	0.5	0	0	0	0	0	0	0	0	0	0	24.5	3.92
61.0	62.5	1.2	5	6	3.5	1.5	0	0.5	1.5	0.5	0	0	0	0	0	0	0	0	33	6.23
62.5	64.0	1.1	8	8	4	1.5	3	0.5	1	0	0	0	0	0	0	0	0	0	41	8.38
64.0	65.5	1.4	8	5	5.5	3	1.5	1	2	0	0	0	0	0.5	0	0	0	0	56	9.26
65.5	67.1	1.5	16	4	2	1	0.5	1	0.5	0.5	0.5	0	0	0	0	0	0	0	30	4.55
67.1	68.6	1.4	16	11.5	4.5	2	1.5	1	1	0	0.5	0	0	0	0	0	0	0	48.5	7.60
68.6	70.1	1.3	17	4	1.5	0.5	0.5	0.5	0.5	1	0	0.5	0	0.5	0	0	0	0	38	6.66
70.1	71.6	1.4	16	4.5	3	1	0	1	1	0	0	0	0	0	0	0	0	0	24.5	3.96
71.6	73.2	1.5	9	9	4.5	2	1.5	2	2	0	0.5	0	0	0	0	0	0	0	57	8.74
73.2	74.7	1.3	16	5	3.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	18	3.04
74.7	76.2	1.4	10	6.5	1	2	0.5	0	0.5	0	1	1.5	0	0	0	0	0	0	47.5	7.44
76.2	77.7	1.3	10	4.5	2.5	2.5	0.5	0.5	1	1	1.5	0.5	0.5	0	0.5	0	0	0	72.5	12.2
77.7	79.2	1.4	8	9	4	0	1	0.5	1	0	0	0	0	0	0	0	0	0	29.5	4.72

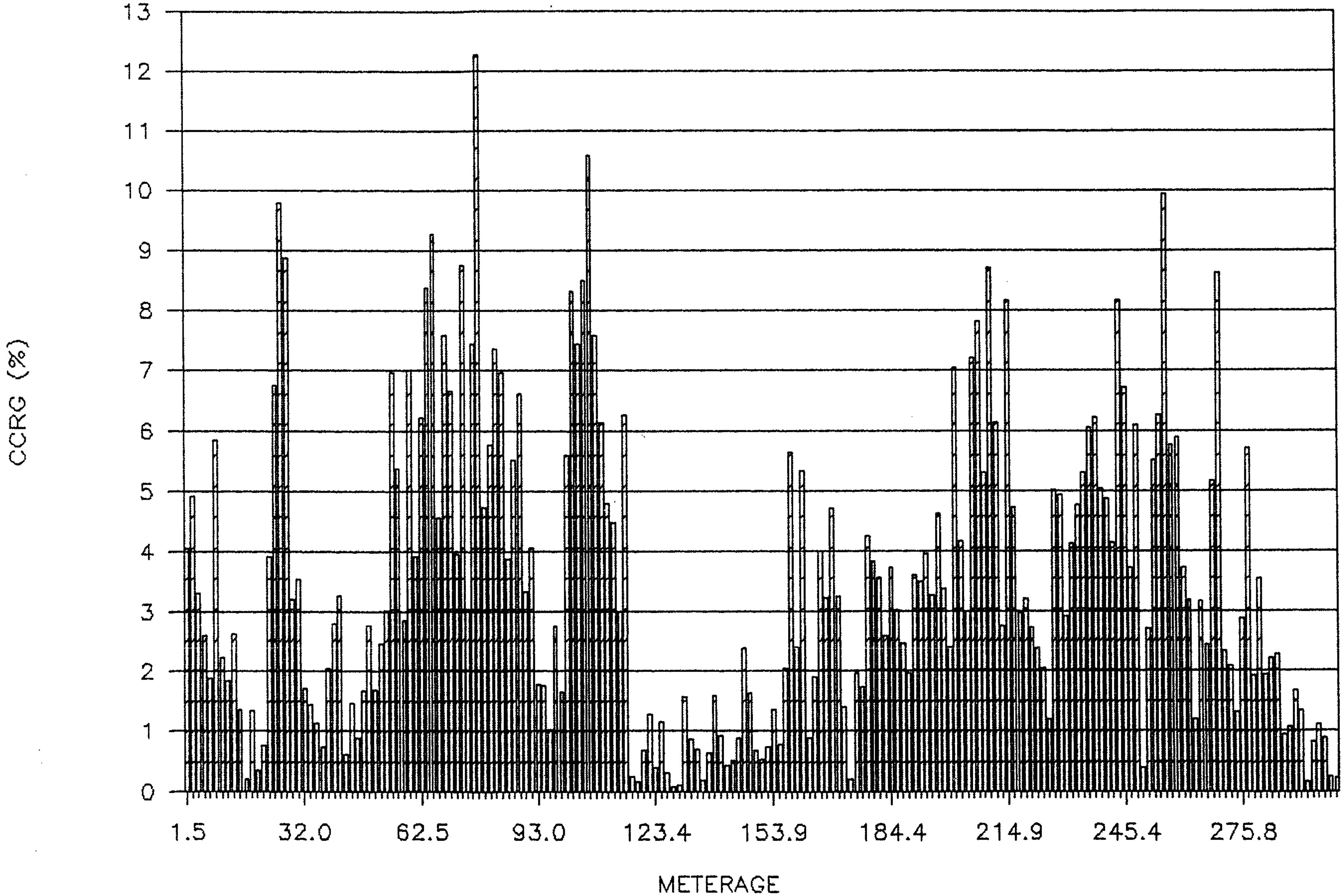
79.2	80.8	1.2	8	9	4	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	30.5	5.75
80.8	82.3	1.2	10	7.5	5	1.5	0	0	2.5	0.5	0	0	0	0	0	0	0	0	41	7.36
82.3	83.8	1.4	18	9.5	4	1	1.5	1.5	0	0.5	0	0.5	0	0	0	0	0	0	44	6.96
83.8	85.3	1.4	9	9	3.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	25	3.87
85.3	86.9	1.4	15	13.5	3	2.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	34.5	5.52
86.9	88.4	1.3	16	13.5	3.5	1.5	1	1.5	0.5	0	0	0	0	0	0	0	0	0	39.5	6.61
88.4	89.9	1.5	9	11.5	3	1.5	0	0	0	0	0	0	0	0	0	0	0	0	22	3.34
89.9	91.4	1.5	10	8	4	0.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	26.5	4.06
91.4	93.0	1.4	17	8.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	11.5	1.78
93.0	94.5	1.4	20	4.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	11	1.76
94.5	96.0	1.4	11	5.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.04
96.0	97.5	1.3	9	6	0.5	1	1	0.5	0	0	0	0	0	0	0	0	0	0	16.5	2.76
97.5	99.1	1.2	10	5.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.64
99.1	100.6	1.4	10	16	2	3.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	35	5.60
100.6	102.1	1.3	10	9.5	4.5	0	2	1.5	1	1	0	0	0	0	0	0	0	0	48	8.31
102.1	103.6	1.3	10	11.5	7	2	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	43	7.45
103.6	105.2	1.4	8	7.5	4.5	3	1.5	1	0	0	1	0.5	0	0	0	0	0	0	52.5	8.49
105.2	106.7	1.5	17	20	7.5	3.5	3.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	69	10.5
106.7	108.2	1.4	19	12.5	3	3	0.5	0.5	0	2	0	0	0	0	0	0	0	0	48	7.60
108.2	109.7	1.5	18	5.5	4	3	1	0.5	1	0	0.5	0	0	0	0	0	0	0	40	6.13
109.7	111.3	1.4	19	9	2	2	0.5	1	0.5	0	0	0	0	0	0	0	0	0	29	4.79
111.3	112.8	1.3	15	8.5	4.5	0	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	26.5	4.48
112.8	114.3	1.5	16	3.5	4	2	0.5	0	0	0	0	0	0	0	0	0	0	0	19.5	2.99
114.3	115.8	1.2	7	4	4.5	2	1	0.5	1.5	0	0	0	0	0	0	0	0	0	34.5	6.27
115.8	117.3	1.4	7	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.24
117.3	118.9	1.4	20	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
118.9	120.4	1.3	19	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.66
120.4	121.9	1.3	11	5.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.28
121.9	123.4	1.2	9	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.38
123.4	125.0	1.4	11	2.5	1	0	0	0.5	0	0	0	0	0	0	0	0	0	0	7	1.14
125.0	126.5	1.5	7	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.30
126.5	128.0	1.4	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.07
128.0	129.5	1.2	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
129.5	131.1	1.4	7	5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.57
131.1	132.6	1.3	7	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.86
132.6	134.1	1.3	10	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4	0.68
134.1	135.6	1.3	13	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
135.6	137.2	1.2	16	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.64
137.2	138.7	1.1	17	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.59
138.7	140.2	1.2	26	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.92
140.2	141.4	1.3	23	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.42
141.7	143.3	1.1	22	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.51
143.3	144.8	1.0	23	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4	0.89
144.8	146.3	1.0	21	6.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	11	2.38
146.3	147.8	1.4	20	4.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10	1.63
147.8	149.4	1.3	13	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.66
149.4	150.9	1.5	16	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.52
150.9	152.4	1.4	24	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.72
152.4	153.9	1.3	10	6	1	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.35
153.9	155.4	1.3	14	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.78
155.4	157.0	1.4	25	8.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	12.5	2.04
157.0	158.5	1.4	18	9.5	4.5	0.5	1.5	0	1	0.5	0	0	0	0	0	0	0	0	36	5.64
158.5	160.0	1.4	16	5	2	1	0	0.5	0	0	0	0	0	0	0	0	0	0	14.5	2.39
160.0	161.5	1.3	21	5.5	6.5	3	1	0	0	0	0	0	0	0	0	0	0	0	31.5	5.33
161.5	163.1	1.3	10	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.88
163.1	164.6	1.1	10	6	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.89

164.6	166.1	1.2	18	8.5	6.5	0	0	0	0	0	0	0	0	0	0	0	0	0	21.5	4.00
166.1	167.6	1.4	17	10	1.5	1	1	0	0	0	0	0	0	0	0	0	0	0	20	3.23
167.6	169.2	1.2	15	9	4	1.5	1	0	0	0	0	0	0	0	0	0	0	0	25.5	4.69
169.2	170.7	1.3	9	9.5	3	1	0	0	0	0	0	0	0	0	0	0	0	0	18.5	3.24
170.7	172.2	1.4	10	8.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.40
172.2	173.7	1.2	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
173.7	175.3	1.5	27	7	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	13	1.97
175.3	176.8	1.4	16	6.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11	1.74
176.8	178.3	1.4	28	8	2.5	2	0	1.5	0	0	0	0	0	0	0	0	0	0	26.5	4.24
178.3	179.8	1.5	14	11.5	1	2.5	1	0	0	0	0	0	0	0	0	0	0	0	25	3.83
179.8	181.4	1.5	24	4	2	1	0	0	1.5	0.5	0	0	0	0	0	0	0	0	24	3.57
181.4	182.9	1.5	24	6.5	2.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	17	2.58
182.9	184.4	1.4	21	7.5	3	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	23.5	3.72
184.4	185.9	1.4	28	7	1.5	1	0	0.5	0	0.5	0	0	0	0	0	0	0	0	19.5	3.02
185.9	187.5	1.4	11	6	2	0	0	0.5	0.5	0	0	0	0	0	0	0	0	0	15.5	2.45
187.5	189.0	1.4	23	8.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	12.5	1.95
189.0	190.5	1.4	17	8	3.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	22.5	3.60
190.5	192.0	1.4	11	14.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	22.5	3.48
192.0	193.5	1.4	28	6.5	4	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	25	3.95
193.5	195.1	1.5	27	6	2	4	0	0	0	0	0	0	0	0	0	0	0	0	22	3.27
195.1	196.6	1.5	27	8.5	2.5	2	1	0	0.5	0.5	0	0	0	0	0	0	0	0	30.5	4.63
196.6	198.1	1.5	19	11	4	1	0	0	0	0	0	0	0	0	0	0	0	0	22	3.37
198.1	199.6	1.4	21	4.5	2.5	0	1.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.40
199.6	201.2	1.5	23	14.5	4	2	0	1	0.5	0	1	0	0	0	0	0	0	0	46.5	7.06
201.2	202.7	1.5	21	7.5	5.5	0.5	2	0	0	0	0	0	0	0	0	0	0	0	28	4.16
202.7	204.2	1.5	26	8	3.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	19.5	2.99
204.2	205.7	1.5	28	15.5	4.5	2	1.5	0	0.5	1	0	0	0	0	0	0	0	0	47.5	7.21
205.7	207.3	1.4	20	16.5	7	2	1.5	1	0.5	0	0	0	0	0	0	0	0	0	50.5	7.83
207.3	208.8	1.4	25	8.5	4	0.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	33.5	5.30
208.8	210.3	1.5	23	9.5	3.5	3	3.5	0.5	2	0.5	0	0	0	0	0	0	0	0	58	8.71
210.3	211.8	1.5	13	6.5	1.5	2.5	0.5	0.5	1.5	0	1	0	0	0	0	0	0	0	40.5	6.15
211.8	213.4	1.5	13	4.5	1.5	1	0	1.5	0	0	0	0	0	0	0	0	0	0	18	2.76
213.4	214.9	1.3	18	8	5.5	3.5	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	46	8.16
214.9	216.4	1.4	10	4.5	3.5	2.5	1	1.5	0	0	0	0	0	0	0	0	0	0	30.5	4.72
216.4	217.9	1.4	12	8.5	0.5	1	0	0.5	0	0.5	0	0	0	0	0	0	0	0	19	2.97
217.9	219.5	1.4	12	6.5	2	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	20.5	3.21
219.5	221.0	1.4	27	6.5	1.5	0.5	0	0	1	0	0	0	0	0	0	0	0	0	17	2.72
221.0	222.5	1.5	18	6.5	1.5	2	0	0	0	0	0	0	0	0	0	0	0	0	15.5	2.37
222.5	224.0	1.5	20	3	1.5	0.5	1.5	0	0	0	0	0	0	0	0	0	0	0	13.5	2.05
224.0	225.6	1.4	14	5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.20
225.6	227.1	1.4	17	10.5	6	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	32	5.01
227.1	228.6	1.4	21	10	4	2.5	0	0	1	0	0	0	0	0	0	0	0	0	31.5	4.93
228.6	230.1	1.5	22	6.5	5	1	0	0	0	0	0	0	0	0	0	0	0	0	19.5	2.93
230.1	231.6	1.5	31	11.5	3	0	0.5	0.5	1	0	0	0	0	0	0	0	0	0	28	4.12
231.6	233.2	1.5	16	12	4	0	1	1	0.5	0	0	0	0	0	0	0	0	0	32	4.76
233.2	234.7	1.5	28	9	3.5	1.5	1	0.5	1.5	0	0	0	0	0	0	0	0	0	36	5.30
234.7	236.2	1.5	24	12	3.5	1	1.5	0.5	1.5	0	0	0	0	0	0	0	0	0	39.5	6.06
236.2	237.7	1.5	30	12.5	5.5	1	0.5	0.5	1	0.5	0	0	0	0	0	0	0	0	41	6.22
237.7	239.3	1.4	32	8	5	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	31.5	5.04
239.3	240.8	1.5	19	14	5.5	0	2	0	0	0	0	0	0	0	0	0	0	0	33	4.86
240.8	242.3	1.5	18	11	3.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	27	4.14
242.3	243.8	1.4	25	13	3	3	2.5	0.5	1	0.5	0	0	0	0	0	0	0	0	50.5	8.17
243.8	245.4	1.4	22	10.5	4	1	2	0.5	0.5	0	0	0.5	0	0	0	0	0	0	41	6.71
245.4	246.9	1.4	16	16	1	1	0.5	0	0	0	0	0	0	0	0	0	0	0	23	3.72
246.9	248.4	1.4	12	12	5	1	0.5	0.5	1.5	0	0	0	0	0	0	0	0	0	38.5	6.09
248.4	249.9	1.5	20	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.37

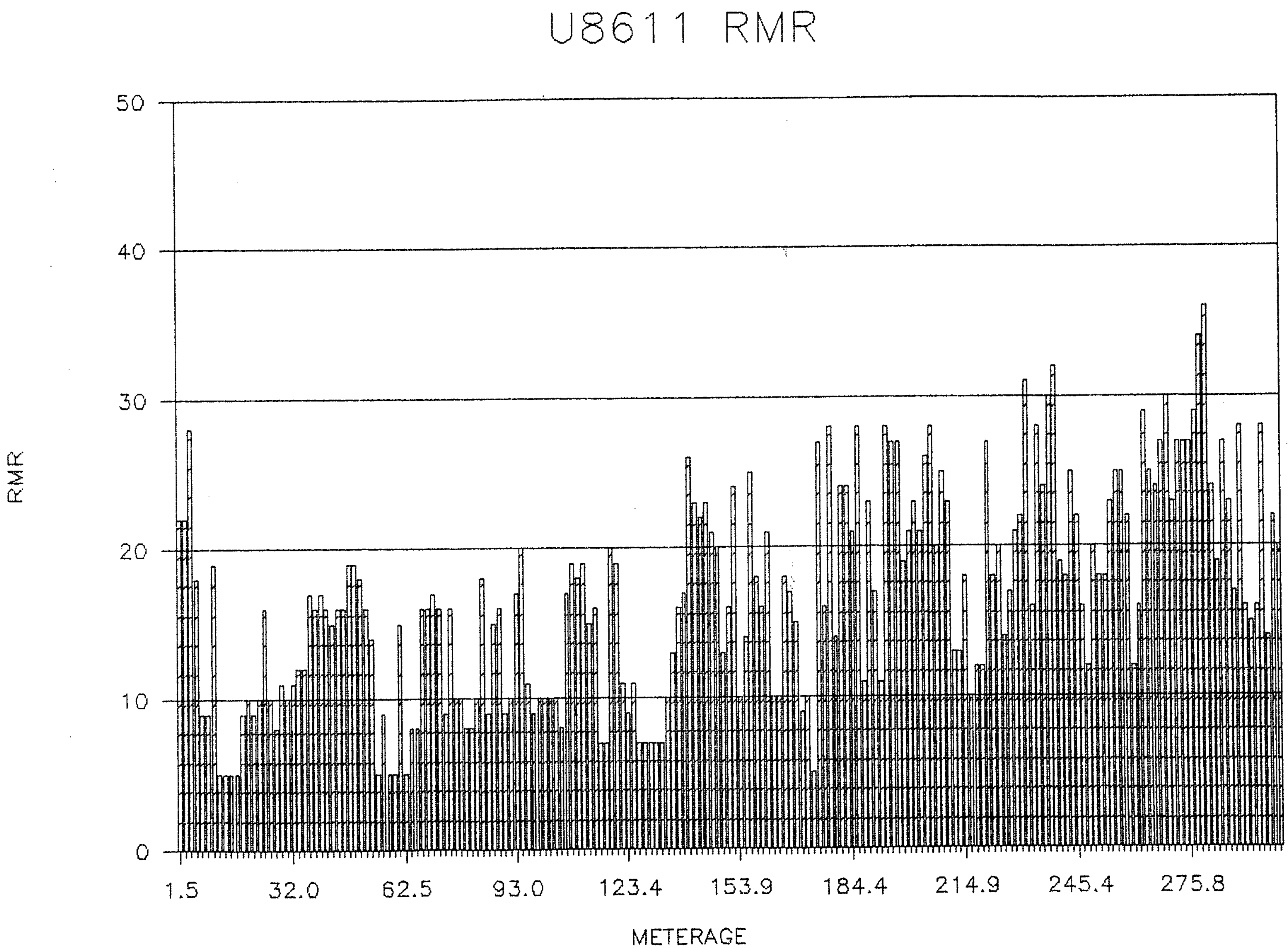
249.9	251.5	1.4	18	5.5	2.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	17.5	2.71
251.5	253.0	1.4	18	7	2	0	0	0.5	0.5	1	1	0	0	0	0	0	0	0	34.5	5.52
253.0	254.5	1.5	23	10.5	4.5	3.5	0.5	0.5	0	1	0	0	0	0	0	0	0	0	42.5	6.26
254.5	256.0	1.5	25	11	5.5	1	1	1.5	2	1.5	0.5	0	0	0	0	0	0	0	65.5	9.94
256.0	257.6	1.5	25	14.5	3.5	1.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	37.5	5.75
257.6	259.1	1.4	22	5.5	5	2	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	38	5.89
259.1	260.6	1.4	12	12	1.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	23.5	3.72
260.6	262.1	1.5	16	6.5	1.5	0	0	0.5	1.5	0	0	0	0	0	0	0	0	0	21	3.18
262.1	263.7	1.5	29	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.20
263.7	265.2	1.5	25	11	3	1.5	0	0	0	0	0	0	0	0	0	0	0	0	21.5	3.16
265.2	266.7	1.5	24	11.5	1	1	0	0	0	0	0	0	0	0	0	0	0	0	16.5	2.43
266.7	268.2	1.5	27	11.5	3	1.5	2	1	0	0	0	0	0	0	0	0	0	0	35	5.15
268.2	269.7	1.4	30	11.5	2	1.5	1.5	0.5	3	1	0	0	0	0	0	0	0	0	54.5	8.63
269.7	271.3	1.5	23	10.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.32
271.3	272.8	1.5	27	9.5	0	1.5	0	0	0	0	0	0	0	0	0	0	0	0	14	2.08
272.8	274.3	1.5	27	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.32
274.3	275.8	1.5	27	7.5	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	19	2.88
275.8	277.4	1.5	29	9.5	4	2.5	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	38	5.71
277.4	278.9	1.5	34	5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	13	1.91
278.9	280.4	1.5	36	9.5	1.5	3	0	0.5	0	0	0	0	0	0	0	0	0	0	24	3.53
280.4	281.9	1.5	24	5.5	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	13	1.93
281.9	283.5	1.5	19	9.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	15	2.20
283.5	285.0	1.4	27	9	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	14.5	2.27
285.0	286.5	1.4	23	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.94
286.5	288.0	1.5	17	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.06
288.0	289.6	1.4	28	5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.66
289.6	291.1	1.4	16	4.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.34
291.1	292.6	1.4	15	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
292.6	294.1	1.4	16	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.81
294.1	295.7	1.5	28	5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.11
295.7	297.2	1.5	14	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.89
297.2	298.7	1.4	22	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.23
298.7	299.3	1.5	20	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.22

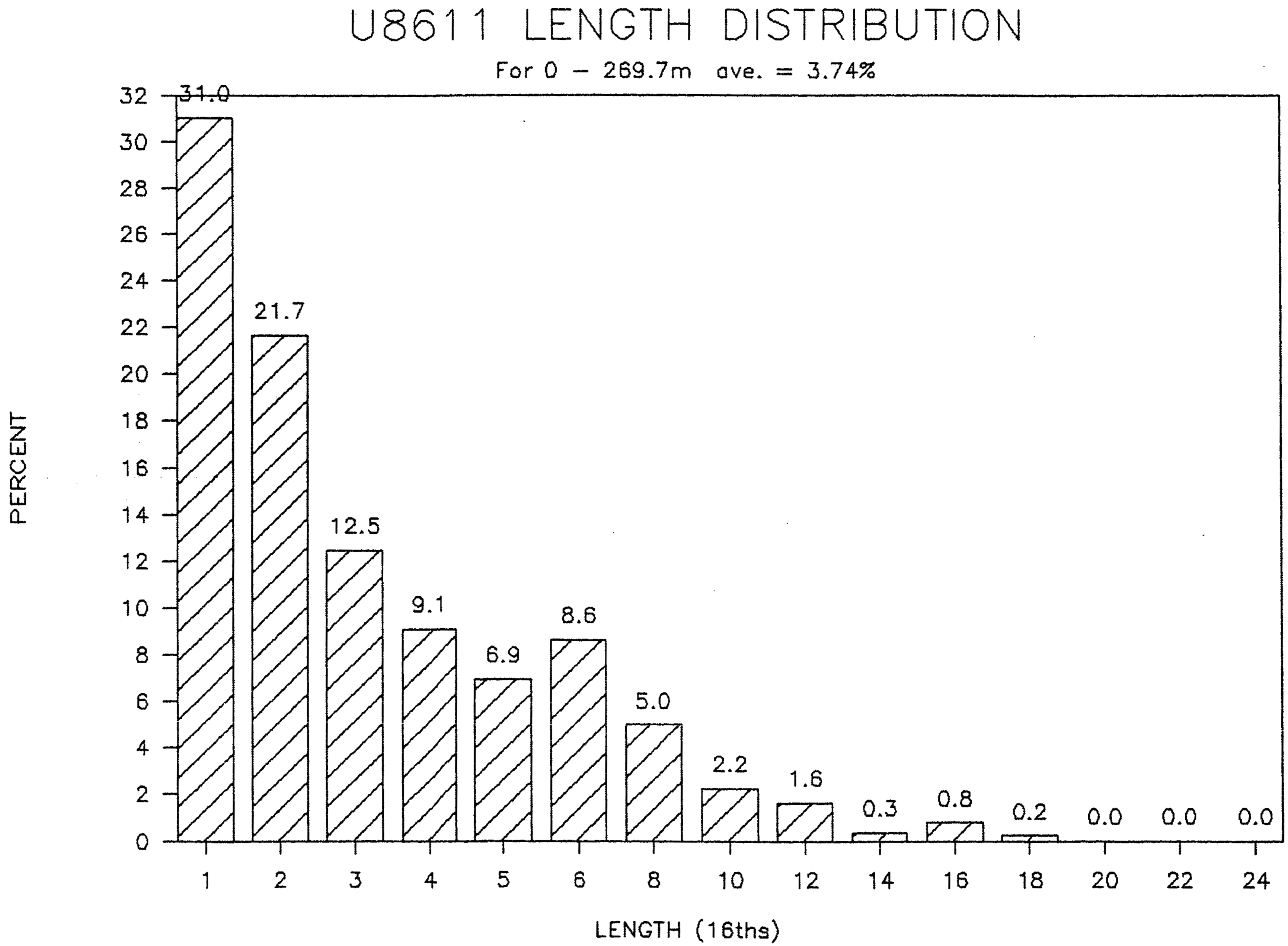
EOH

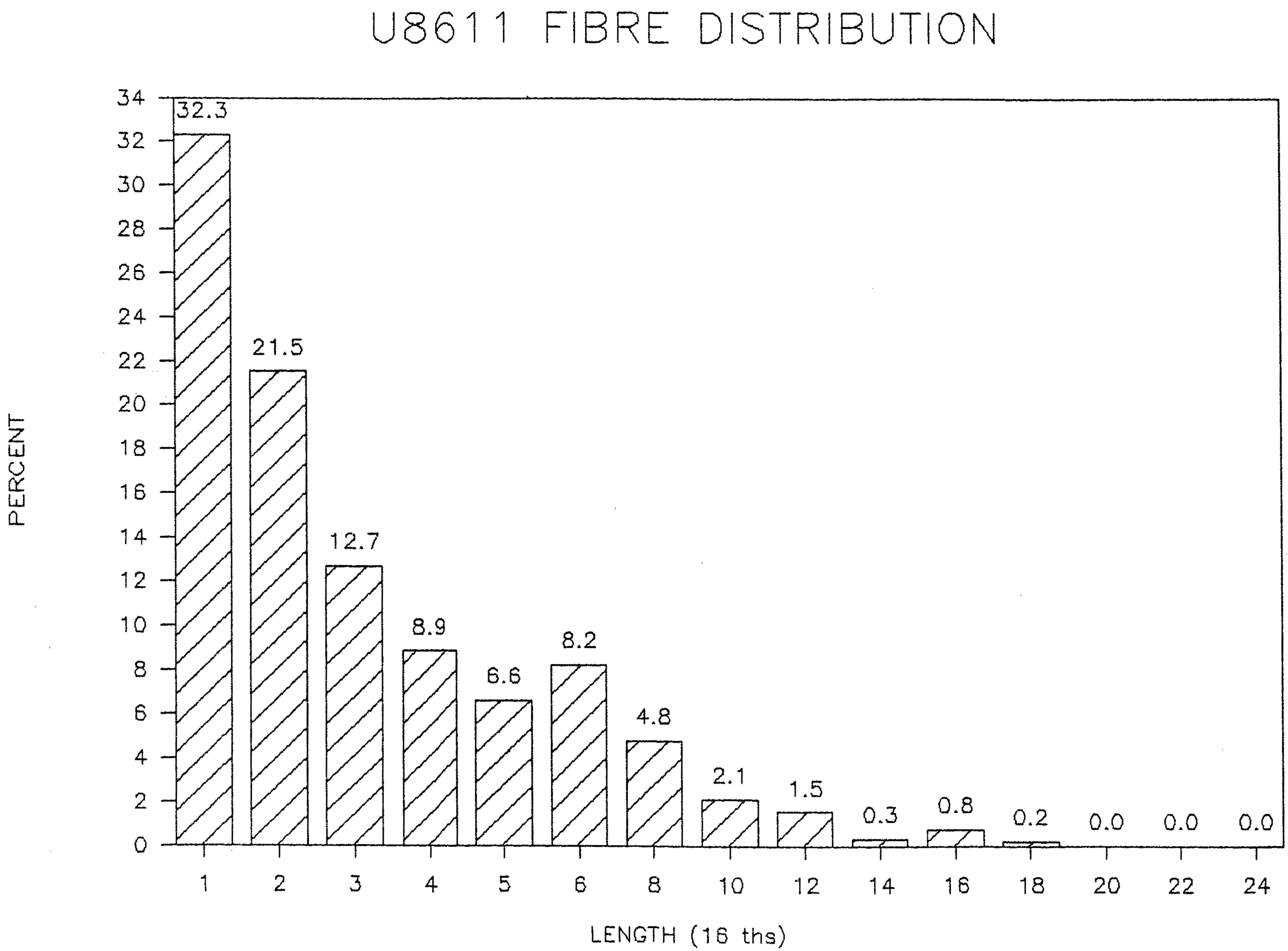
U8611 CCRG



CCRG (%)
0
1
2
3
4
5
6
7
8
9
10
11
12
13
1.5
32.0
62.5
93.0
123.4
153.9
184.4
214.9
245.4
275.8
METERAGE

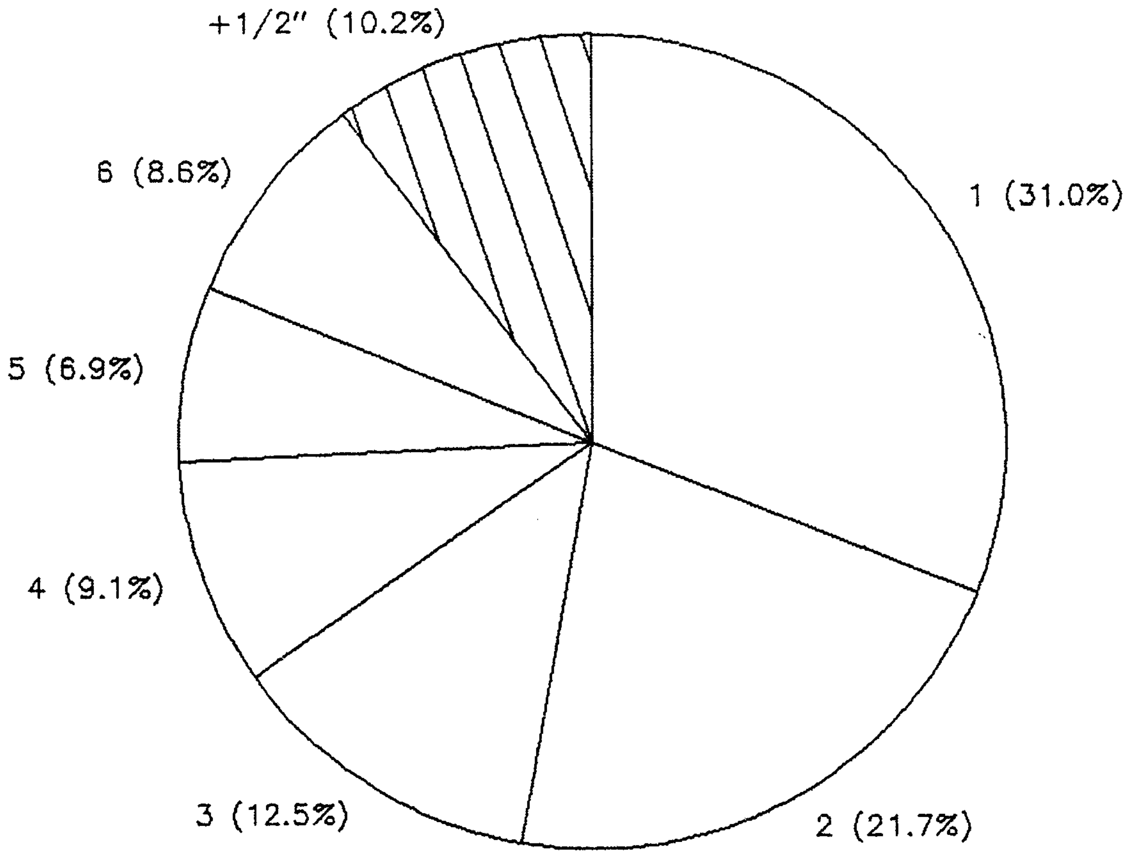

U8611 RMR
50
40
30
20
10
0
RMR
1.5
32.0
62.5
93.0
123.4
153.9
184.4
214.9
245.4
275.8
METERAGE


U8611 LENGTH DISTRIBUTION
For 0 – 269.7m ave. = 3.74%
PERCENT
LENGTH (16ths)
32
30
28
26
24
22
20
18
16
14
12
10
8
6
4
2
0
31.0
21.7
12.5
9.1
6.9
8.6
5.0
2.2
1.6
0.3
0.8
0.2
0.0
0.0
0.0
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24

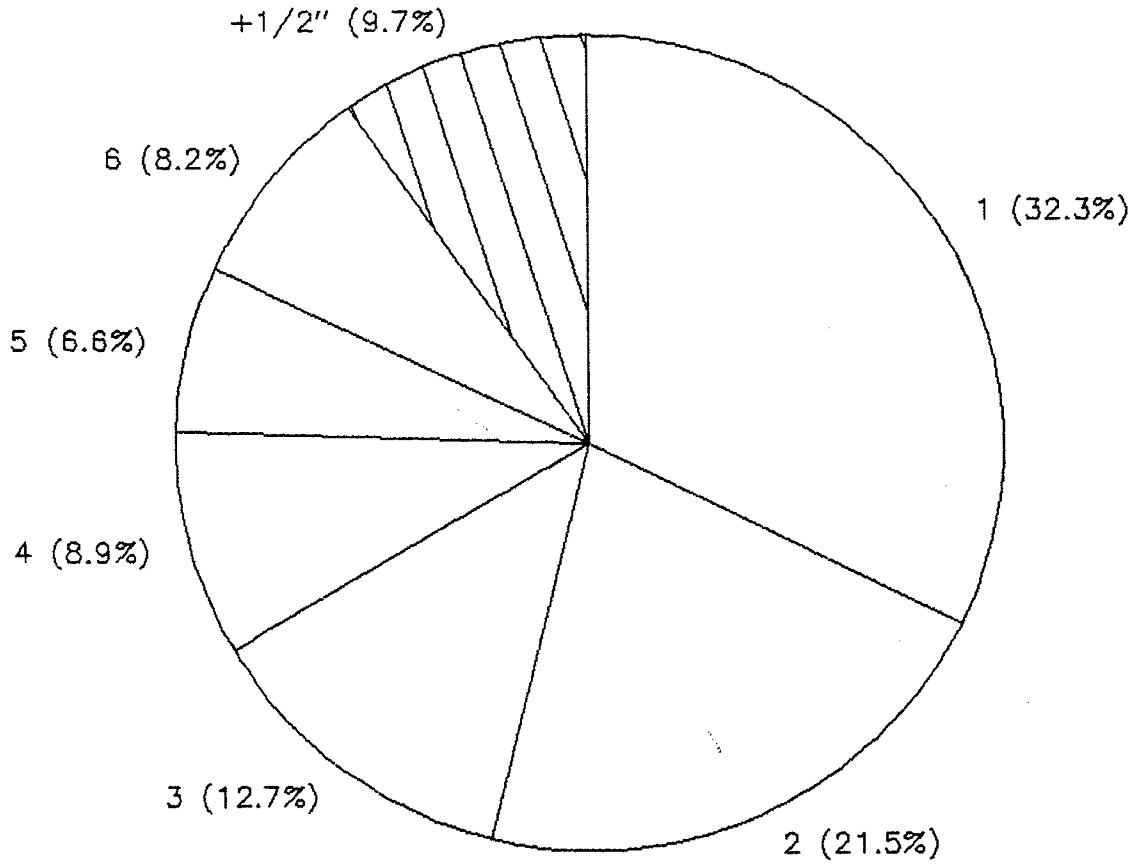


U8611 FIBRE DISTRIBUTION
PERCENT
34
32
30
28
26
24
22
20
18
16
14
12
10
8
6
4
2
0
32.3
21.5
12.7
8.9
6.6
8.2
4.8
2.1
1.5
0.3
0.8
0.2
0.0
0.0
0.0
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16 ths)

U8611 LENGTH DISTRIBUTION



U8611 FIBRE DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME | HOLE U 86-12 | DEPTH 165.2 m

AZIMUTH 270° | INCLINATION -38° | SECTION 6649

LATITUDE 6647.8N | DEPARTURE 7601.2E | ELEVATION 1414.0 m

STARTED Oct. 6 | FINISHED Oct. 11 | LOGGED by I. Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1	12.6		Serpentinite, medium green, mottled, low grade fibre	
			3.7 - 7.5 Fault, fractured and gouge	
12.6	46.6		Dark green to medium green, good fibre to 32.3	
			Fault zones 35.5 - 36.5, 40.2 - 43.9	
46.6	86.9		Medium - dark green, good fibre, very broken	
			Fault zones 54.6 - 56.5	
86.9	100.3		Faulted and broken, low grade fibre, main fault 92.7 - 95.1	
100.3	130.2		Dark green, fibre bearing	
			103.9 - 121.9 Fault and fractured zone, broken and fractured	
			Springy fibre to end of section	
130.2	138.4		Very dark green, below 136.6 is slightly altered to lighter	
			greyish colour. Occasional picrolite veins	
138.4	139.9		Altered serpentine - light greenish grey	
139.9	142.7		Dark greenish grey less altered serpentine	
142.7	144.3		Medium grey talcy alteration	
144.3	148.4		Fault zone - slightly altered very dark green serp.	
148.4	149		Rodingite	
149	156.7		Altered serp. Very dark grey going to light grey	
156.7	158.5		Contact fault zone. White powdery gouge.	
158.5	165.2		Argillite, very broken and faulted.	
165.2			E.O.H.	

DDH U86-12

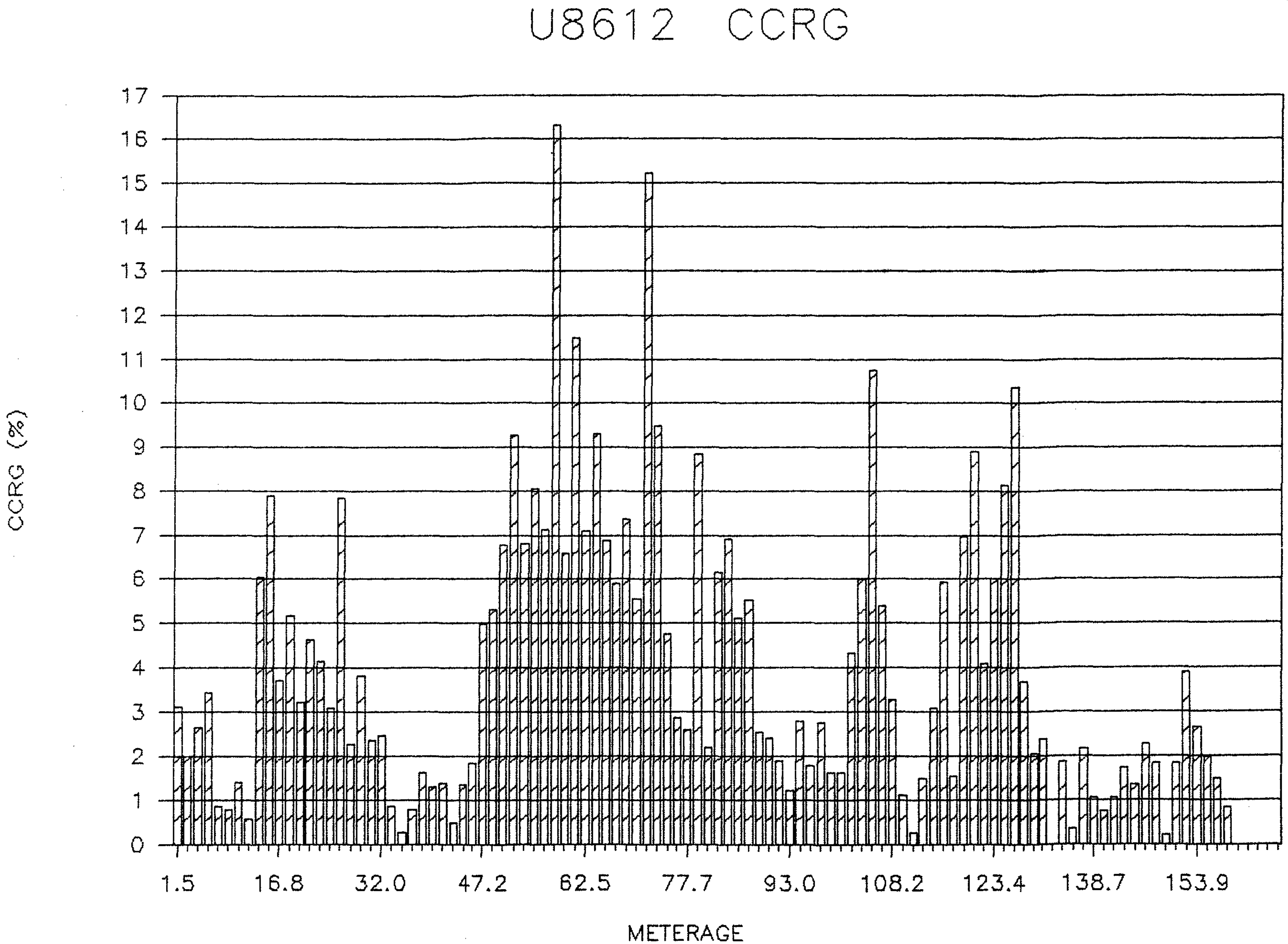
AVERAGE OF TWO COUNTS
Number of fibre veins counted per 16th category

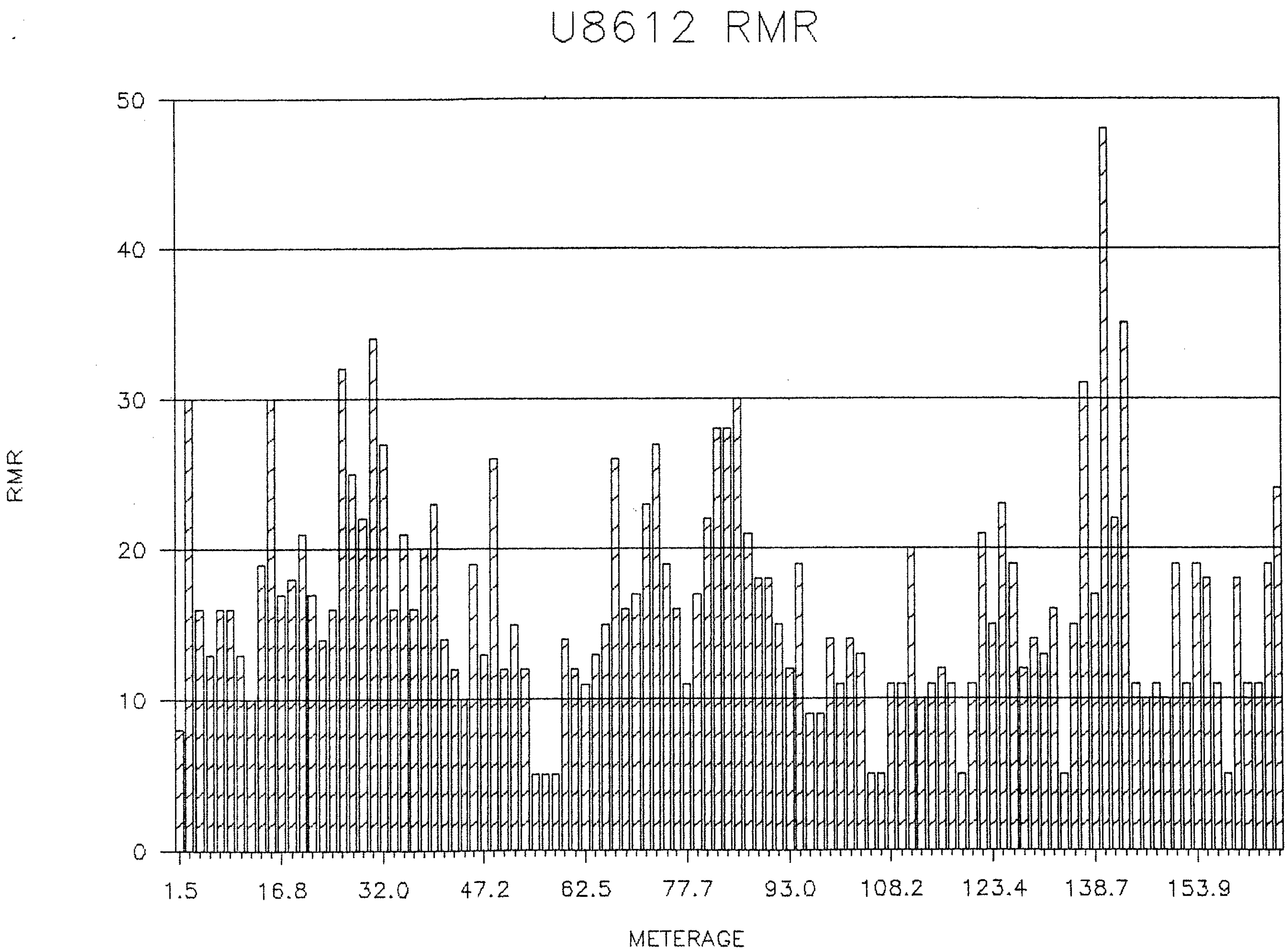
FROM	TO	REC	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL	CCRG
M	M	M																	16'S	%
0.0	1.5	0.3	8	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	3.10
1.5	3.0	1.2	30	6	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	2.01
3.0	4.6	1.5	16	7.5	2	2	0	0	0	0	0	0	0	0	0	0	0	0	17.5	2.66
4.6	6.1	1.3	13	4.5	3.5	1	1.5	0	0	0	0	0	0	0	0	0	0	0	20.5	3.43
6.1	7.6	1.4	16	2	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.87
7.6	9.1	1.4	16	2	0	0	0	0	0.5	0	0	0	0	0	0	0	0	0	5	0.78
9.1	10.7	1.4	13	5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.40
10.7	12.2	1.4	10	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.55
12.2	13.7	1.4	19	14	5.5	0.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	39	6.05
13.7	15.2	1.5	30	4.5	2.5	1.5	1.5	0.5	3	0	0.5	0.5	0	0	0	0	0	0	51.5	7.90
15.2	16.8	1.5	17	11	4	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	25	3.72
16.8	18.3	1.4	18	10.5	1	0.5	1	0	0	0	0	0	0.5	0.5	0	0	0	0	33	5.17
18.3	19.8	1.5	21	7.5	3.5	1	1	0	0	0	0	0	0	0	0	0	0	0	21.5	3.23
19.8	21.3	1.5	17	9	3	1	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	30.5	4.63
21.3	22.9	1.5	14	14	2.5	0	2	0	0	0	0	0	0	0	0	0	0	0	27	4.14
22.9	24.4	1.5	16	12	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	20.5	3.08
24.4	25.9	1.4	32	5.5	1.5	2.5	2.5	1	0	0	0	0	0	0	0.5	0.5	0	0	50	7.84
25.9	27.4	1.4	25	8	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	14.5	2.27
27.4	29.0	1.5	22	8	5	0.5	1.5	0	0	0	0	0	0	0	0	0	0	0	25.5	3.83
29.0	30.5	1.3	34	9	1	1	0	0	0	0	0	0	0	0	0	0	0	0	14	2.34
30.5	32.0	1.3	27	8.5	3	0	0	0	0	0	0	0	0	0	0	0	0	0	14.5	2.46
32.0	33.5	1.4	16	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.87
33.5	35.1	1.3	21	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
35.1	36.6	1.4	16	2	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	5	0.78
36.6	38.1	1.5	20	6	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.61
38.1	39.6	1.4	23	5.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8	1.29
39.6	41.1	1.3	14	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.39
41.1	42.7	1.2	12	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.47
42.7	44.2	1.3	10	3	0.5	0	0	0	0	0.5	0	0	0	0	0	0	0	0	8	1.34
44.2	45.7	1.3	19	4.5	1.5	0	0	0	0.5	0	0	0	0	0	0	0	0	0	10.5	1.82
45.7	47.2	1.3	13	10	2	0.5	1	0	1	0.5	0	0	0	0	0	0	0	0	29.5	4.99
47.2	48.8	1.5	26	13	2.5	2	0	0	0.5	1	0	0	0	0	0	0	0	0	35	5.31
48.8	50.3	1.1	12	6.5	2.5	3.5	0.5	0	1	0.5	0	0	0	0	0	0	0	0	34	6.77
50.3	51.8	1.1	15	6.5	3.5	2.5	0	0.5	2.5	0	0.5	0	0	0	0	0	0	0	43.5	9.29
51.8	53.3	1.0	12	6.5	5.5	1	1	0.5	0.5	0	0	0	0	0	0	0	0	0	30	6.80
53.3	54.9	1.1	5	4	4.5	0.5	1	0.5	2	1	0	0	0	0	0	0	0	0	41	8.05
54.9	56.4	0.9	5	7.5	1	0	1	0.5	1.5	0	0.5	0	0	0	0	0	0	0	30	7.13
56.4	57.9	0.9	5	3.5	3.5	0.5	1.5	0.5	3	2	0.5	0	0.5	0	0	0	0	0	66.5	16.33
57.9	59.4	1.3	14	6.5	4.5	3	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	38.5	6.59
59.4	61.0	1.1	12	8	5.5	3.5	2	1	2	0	0	0	0	0	0	0	0	0	54.5	11.47
61.0	62.5	1.4	11	2	0.5	2	1	1	1.5	2	0	0	0	0	0	0	0	0	43	7.12
62.5	64.0	1.3	13	3.5	2	1.5	2	1	1.5	0	0	0	0	0	0.5	0	0	0.5	55	9.31
64.0	65.5	1.4	15	6.5	5	1.5	2.5	0	0.5	1	0	0	0	0	0	0	0	0	42	6.87
65.5	67.1	1.4	26	6	2	0.5	0	0	1	0.5	0	0	0.5	0.5	0	0	0	0	36.5	5.91
67.1	68.6	1.3	16	3.5	3	3	0.5	1.5	1	1	0	0	0	0	0	0	0	0	42	7.37
68.6	70.1	1.4	17	5.5	2.5	1	0.5	2	0.5	0	0.5	0	0	0	0	0	0	0	33.5	5.54
70.1	71.6	1.4	23	6	3	2.5	0.5	2.5	2.5	3.5	0.5	1	0	0	0	0	0	0	94	15.22
71.6	73.2	1.5	27	6.5	3	1.5	0.5	0.5	1	0.5	0	0	0.5	1.5	0	0	0	0	62.5	9.49
73.2	74.7	1.4	19	2.5	0.5	2.5	0.5	0	0	1.5	0.5	0	0	0	0	0	0	0	30	4.75
74.7	76.2	1.4	16	5	3	0	0.5	1	0	0	0	0	0	0	0	0	0	0	18	2.85
76.2	77.7	1.3	11	9.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	15.5	2.59
77.7	79.2	1.4	17	5	3.5	2.5	0.5	0.5	0.5	1	0.5	0.5	0	0.5	0	0	0	0	54	8.84

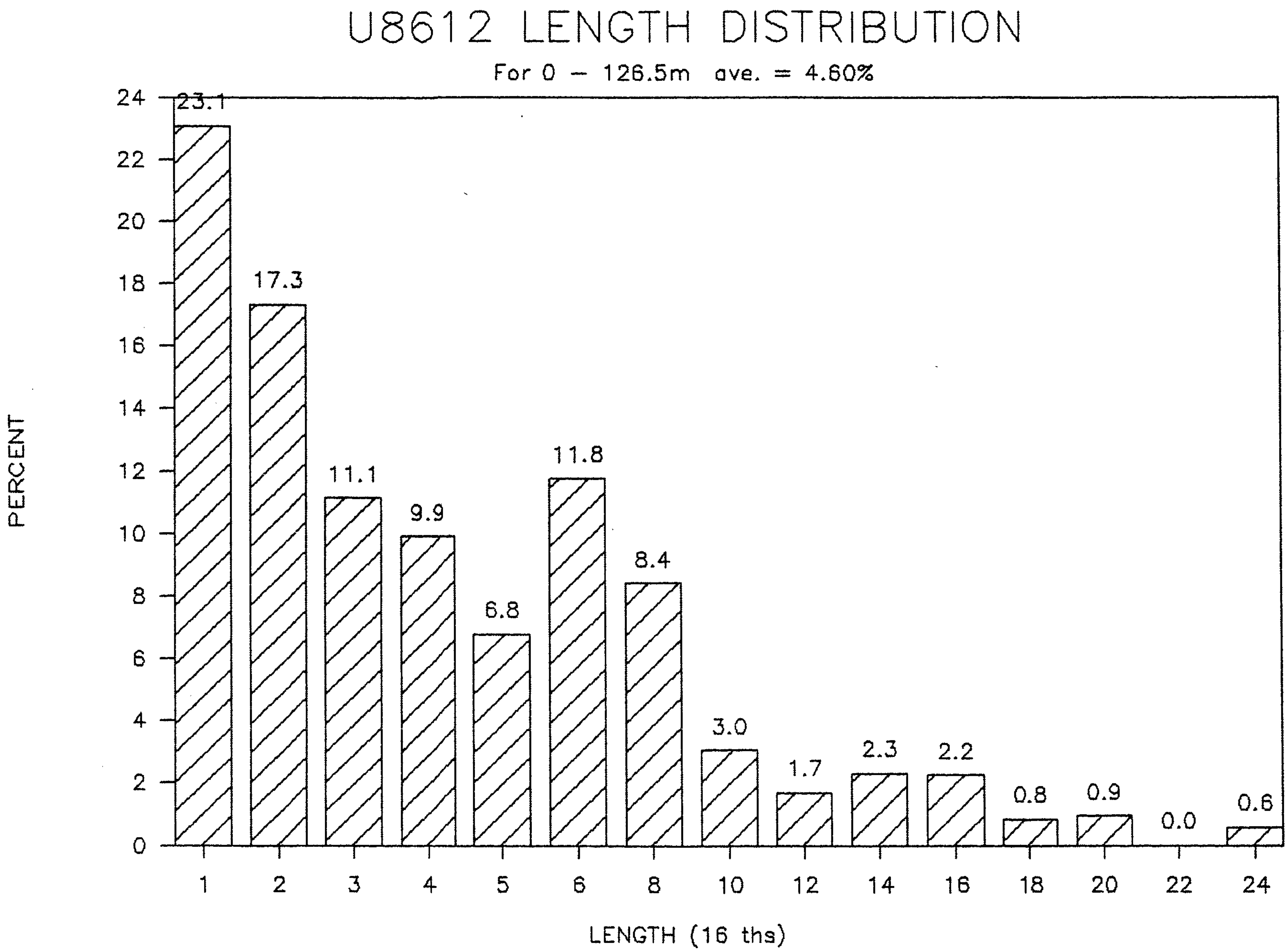
79.2	80.8	1.4	22	8.5	1	1	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.19
80.8	82.3	1.4	28	9.5	2	1.5	1.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	38.5	6.16
82.3	83.8	1.5	28	7.5	3.5	1.5	1.5	0.5	1	1	0.5	0	0	0	0	0	0	0	46.5	6.92
83.8	85.3	1.3	30	2.5	1.5	3	0.5	1	1.5	0	0	0	0	0	0	0	0	0	30.5	5.11
85.3	86.9	1.4	21	7.5	4	1.5	0.5	0	0	0	0	0.5	0.5	0	0	0	0	0	35	5.54
86.9	88.4	1.4	18	5.5	0.5	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	16	2.53
88.4	89.9	1.4	18	6.5	3.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.40
89.9	91.4	1.2	15	6	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.89
91.4	93.0	1.4	12	6.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.21
93.0	94.5	1.4	19	7	2	0.5	0	1	0	0	0	0	0	0	0	0	0	0	17.5	2.80
94.5	96.0	1.4	9	5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	11	1.78
96.0	97.5	1.4	9	5	2	0.5	1	0	0.5	0	0	0	0	0	0	0	0	0	17.5	2.77
97.5	99.1	1.4	14	7	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	10	1.62
99.1	100.6	1.4	11	6.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.63
100.6	102.1	1.4	14	9	3	1.5	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	28	4.34
102.1	103.6	1.4	13	9	4	2	1.5	1	0.5	0	0	0	0	0	0	0	0	0	37	5.99
103.6	105.2	0.9	5	6	5	1	0.5	0.5	1	0.5	0.5	0.5	0	0	0	0	0	0	44.5	10.75
105.2	106.7	0.8	5	7.5	2.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	19	5.38
106.7	108.2	1.2	11	6.5	2	0.5	1.5	0	0	0	0	0	0	0	0	0	0	0	18	3.27
108.2	109.7	1.2	11	3	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.09
109.7	111.3	0.9	20	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.25
111.3	112.8	1.1	10	5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.47
112.8	114.3	1.2	11	3.5	2.5	0	0.5	0	1	0	0	0	0	0	0	0	0	0	16.5	3.08
114.3	115.8	1.2	12	1.5	1.5	1	2	1	0.5	1	0	0	0	0	0	0	0	0	31.5	5.95
115.8	117.3	0.7	11	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	5	1.53
117.3	118.9	0.9	5	4	1	0.5	1.5	0	1	1	0	0	0	0	0	0	0	0	27.5	6.98
118.9	120.4	1.0	11	6.5	5	0.5	1.5	0.5	1.5	0	0.5	0	0	0	0	0	0	0	40.5	8.90
120.4	121.9	1.1	21	5.5	5.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	20	4.09
121.9	123.4	1.2	15	3	1.5	1.5	0.5	1.5	1	0	0.5	0	0	0	0	0.5	0	0	31	6.01
123.4	125.0	1.2	23	4.5	1	0.5	0.5	1	1	0.5	0	0	0.5	0	0	0	0	0	42	8.14
125.0	126.5	1.2	19	4.5	3	2.5	2.5	0.5	1.5	0.5	0.5	0	0.5	0	0	0	0	0	55.5	10.35
126.5	128.0	1:4	12	5.5	2.5	1	1.5	0	0.5	0	0	0	0	0	0	0	0	0	22.5	3.68
128.0	129.5	1.4	14	3	1.5	0	1	0.5	0	0	0	0	0	0	0	0	0	0	12.5	2.05
129.5	131.1	1.3	13	3.5	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	13.5	2.37
131.1	132.6	1.1	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
132.6	134.1	1.2	5	2	1	2	0	0	0	0	0	0	0	0	0	0	0	0	10	1.86
134.1	135.6	1.3	15	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.35
135.6	137.2	1.4	31	2.5	2.5	1	0	0	0.5	0	0	0	0	0	0	0	0	0	13.5	2.16
137.2	138.7	1.5	17	4	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	7	1.05
138.7	140.2	1.5	48	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	5	0.74
140.2	141.7	1.5	22	2	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.05
141.7	143.3	1.5	35	4.5	2	1	0	0	0	0	0	0	0	0	0	0	0	0	11.5	1.73
143.3	144.8	1.5	11	1.5	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9	1.34
144.8	146.3	1.3	10	0.5	1.5	1	0.5	1	0	0	0	0	0	0	0	0	0	0	13.5	2.26
146.3	147.8	1.1	11	3.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9	1.84
147.8	149.4	1.2	10	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
149.4	150.9	1.4	19	2.5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	0	11.5	1.84
150.9	152.4	1.2	11	4.5	3	3	0.5	0	0	0	0	0	0	0	0	0	0	0	21.5	3.91
152.4	153.9	1.2	19	5	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	14.5	2.64
153.9	155.4	1.3	18	3	1	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	11.5	1.97
155.4	157.0	1.3	11	2	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	8.5	1.49
157.0	158.5	1.1	5	0	0	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	4	0.82
158.5	160.0	1.4	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
160.0	161.5	1.1	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
161.5	163.1	0.9	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
163.1	164.6	1.2	19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

164.6	165.2	0.4	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

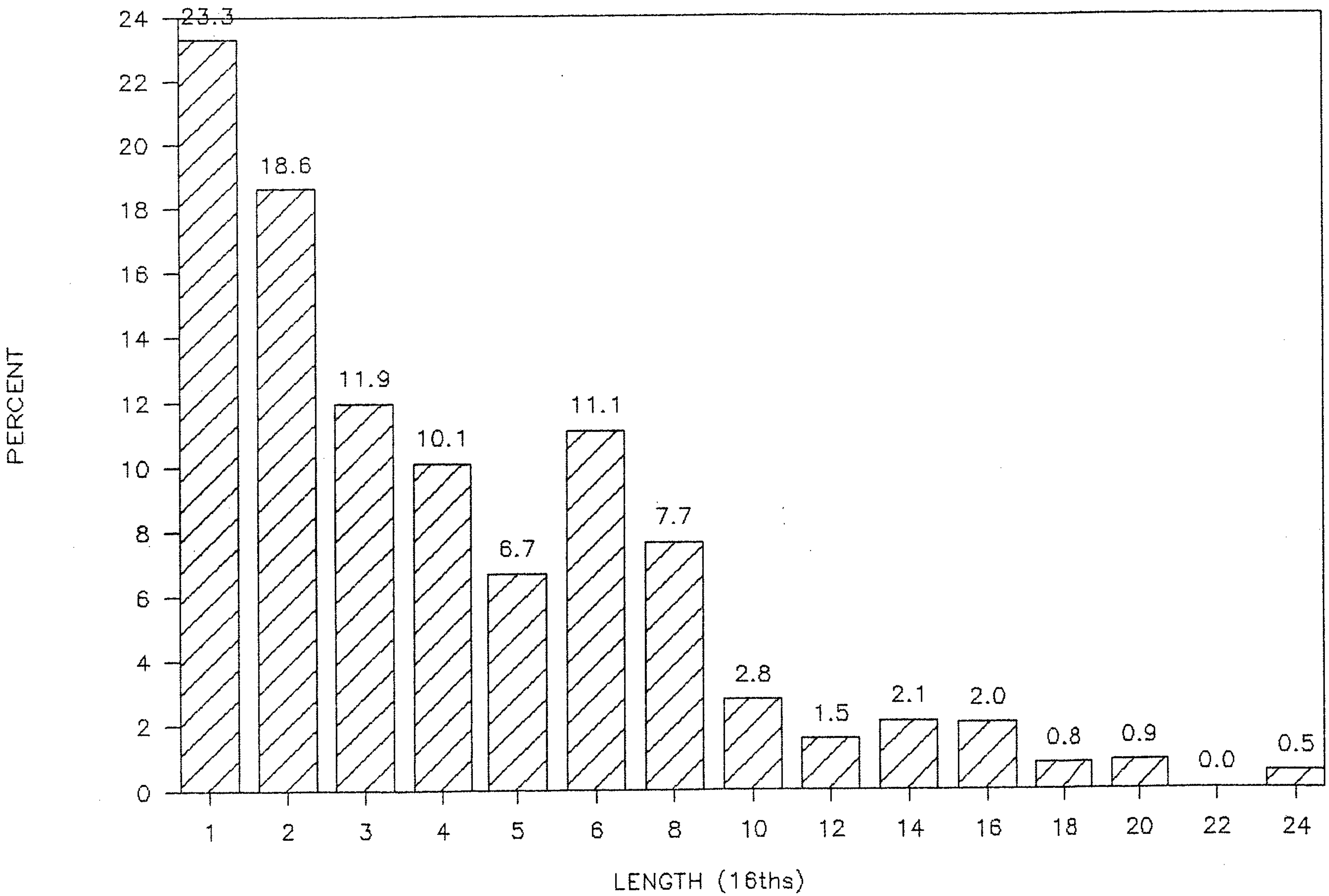
EOH


U8612 CCRG
CCRG (%)
17
16
15
14
13
12
11
10
9
8
7
6
5
4
3
2
1
0
1.5
16.8
32.0
47.2
62.5
77.7
93.0
108.2
123.4
138.7
153.9
METERAGE

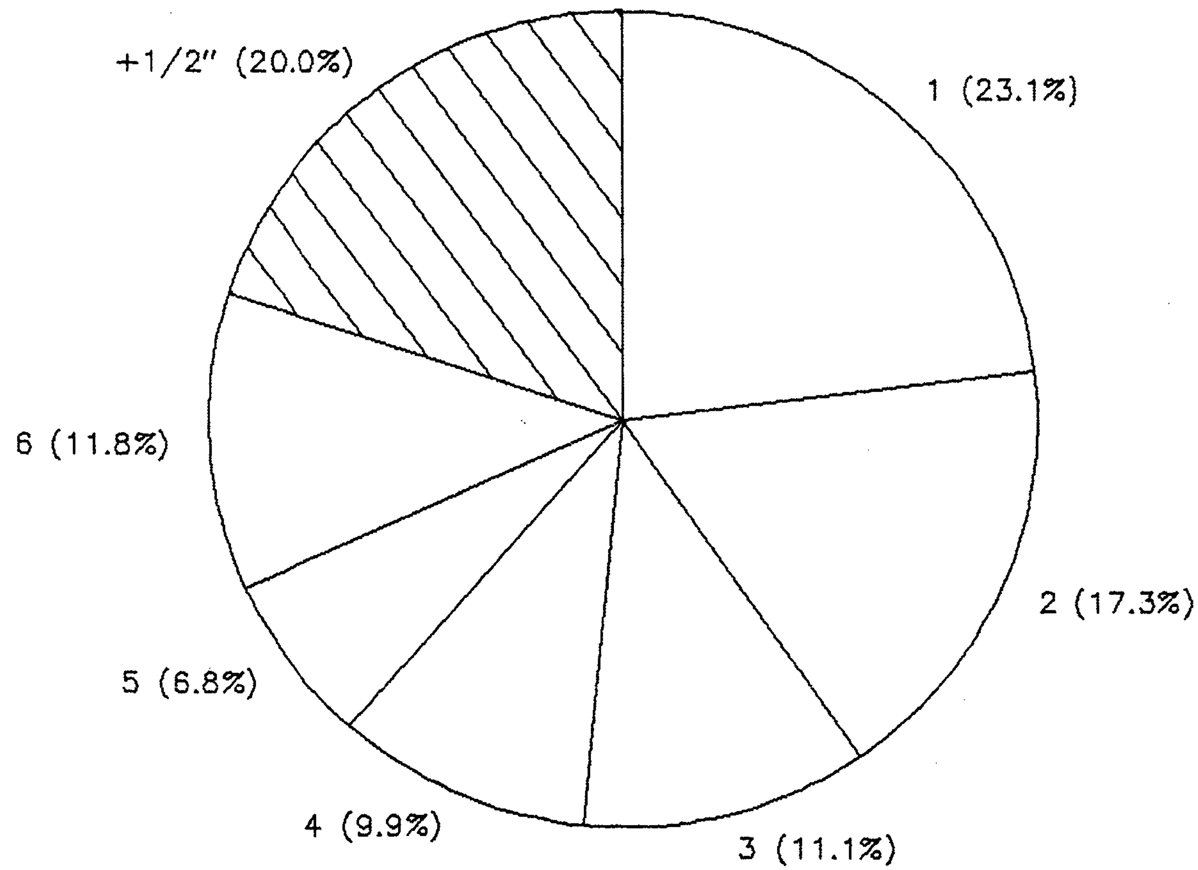

U8612 RMR
RMR
0
10
20
30
40
50
1.5
16.8
32.0
47.2
62.5
77.7
93.0
108.2
123.4
138.7
153.9
METERAGE


U8612 LENGTH DISTRIBUTION
For 0 – 126.5m ave. = 4.60%
PERCENT
0
2
4
6
8
10
12
14
16
18
20
22
24
23.1
17.3
11.1
9.9
6.8
11.8
8.4
3.0
1.7
2.3
2.2
0.8
0.9
0.0
0.6
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16 ths)

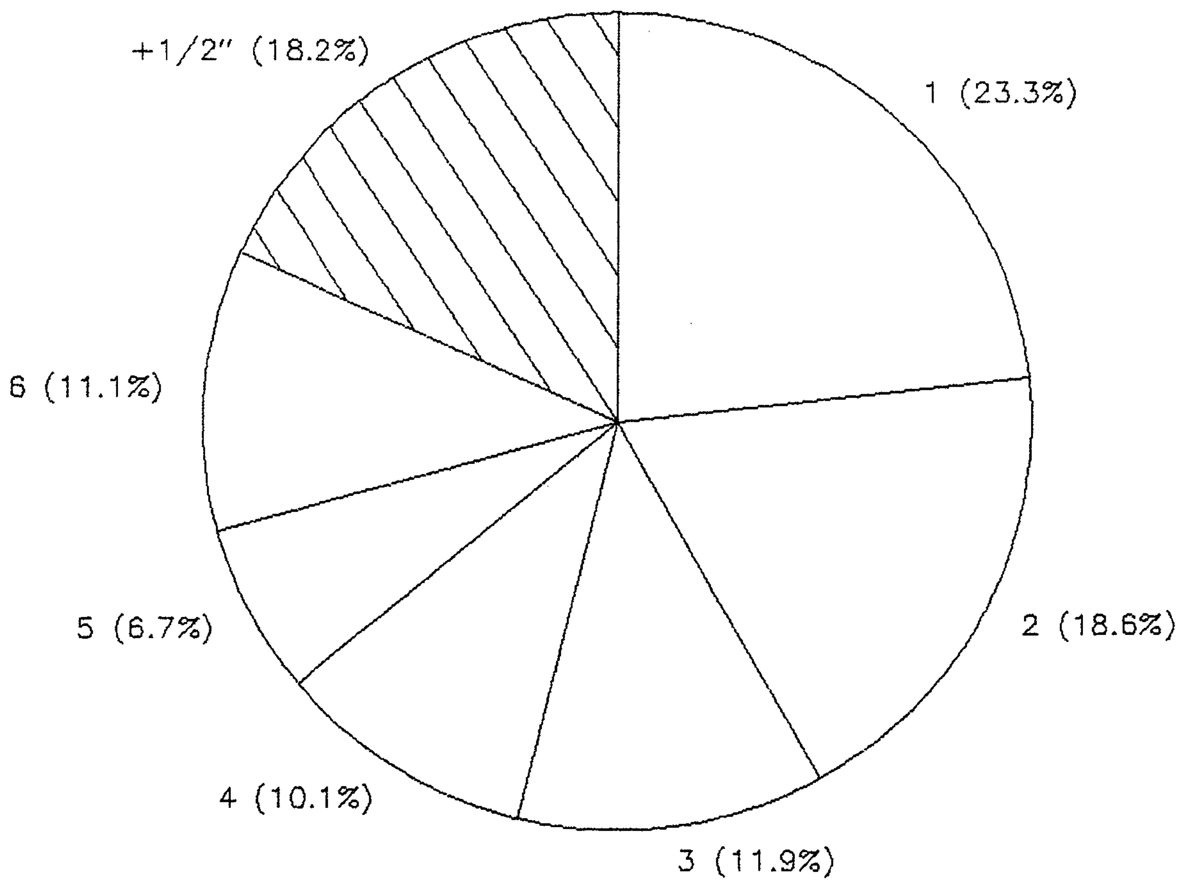
U8612 FIBRE DISTRIBUTION



U8612 LENGTH DISTRIBUTION



U8612 FIBRE DISTRIBUTION



DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME | HOLE U86-13 | DEPTH 238.05 m

AZIMUTH 86.00° | INCLINATION -40.15° | SECTION 6828 m

LATITUDE 6728.618N | DEPARTURE 7625.253E | ELEVATION 1568.589

STARTED Oct. 11 | FINISHED Oct. 23 | LOGGED by I. Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1.13	18.3		Very dark grey slightly greenish serpentinite with dark green	
			lizardite veins.	
18.3	20.9		Rodingite, light greenish grey	
20.9	142.2		Very dark greyish green serp, sparse fibre, talcy	
			Fault zones: 27.4 - 42.2 Broken, sections of gouge	
			48.1 - 49.4, 60.6 - 62.5 Extremely cleaved and gouge	
			81.2 - 84.7	
			89.3 - 102.6 Fault zone, broken with cleaved zones, brucite	
			and picrolite veins	
			Fault zones: 109.1 - 110, 119.2 - 125, 127.6 - 130, 139.9 -	
			142.2	
142.2	156.7		Gradual change to dark green serpentinite, sparse to minor	
			fibre. Fault zone 151.4 - 154.1. No fibre	
156.7	238.1		Fault zone Dark green to very dark green. Very broken and	
			cleaved with sections of gouge	
238.05			E.O.H. Rods broke	

DDH U 8613

EAST: 7525 AZ: 90
NORTH: 6828 INCL: -40
ELEV: 1563 DEPTH:238.1

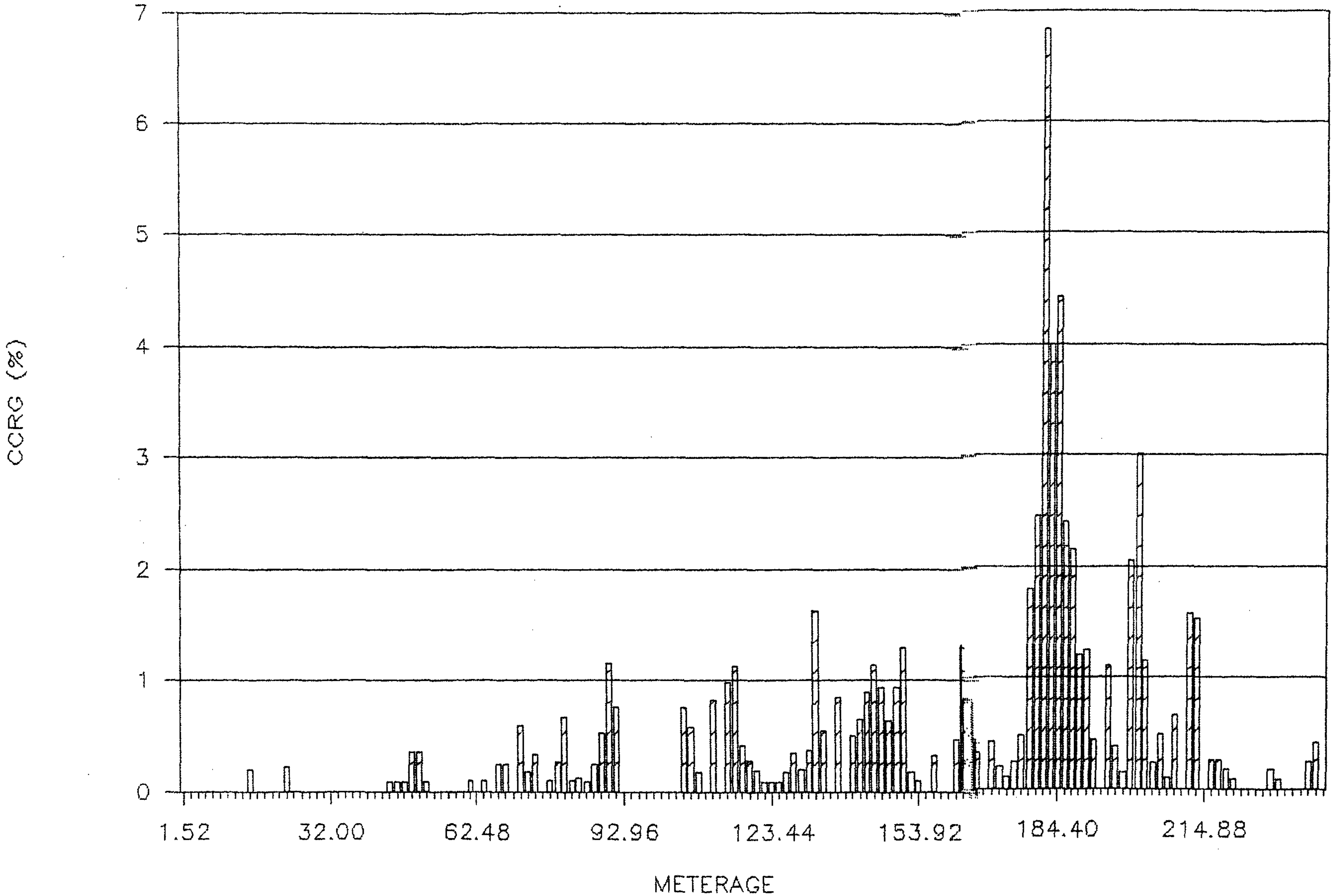
AVERAGE OF TWO COUNTS
Number of fibre veins counted per 16th category

FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRB %
0.00	1.52	0.30	27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
1.52	3.05	1.30	30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
3.05	4.57	1.42	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
4.57	6.10	1.46	35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
6.10	7.62	1.49	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
7.62	9.14	1.25	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
9.14	10.67	1.11	19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
10.67	12.19	0.87	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
12.19	13.72	1.40	29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
13.72	15.24	1.17	25	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
15.24	16.76	1.28	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
16.76	18.29	1.28	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
18.29	19.81	1.52	36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
19.81	21.34	1.52	30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
21.34	22.86	1.52	29	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.22
22.86	24.38	1.52	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
24.38	25.91	1.20	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
25.91	27.43	1.05	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
27.43	28.96	0.64	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
28.96	30.48	0.40	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
30.48	32.00	0.58	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
32.00	33.53	0.79	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
33.53	35.05	0.43	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
35.05	36.58	0.29	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
36.58	38.10	0.43	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
38.10	39.62	0.72	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
39.62	41.15	0.99	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
41.15	42.67	1.39	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
42.67	44.20	1.46	15	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
44.20	45.72	1.46	21	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
45.72	47.24	1.34	23	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
47.24	48.77	1.25	22	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.36
48.77	50.29	1.28	19	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.35
50.29	51.82	1.46	17	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
51.82	53.34	1.30	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
53.34	54.86	1.37	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
54.86	56.39	1.43	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
56.39	57.91	1.34	30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
57.91	59.44	1.28	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
59.44	60.96	1.17	21	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
60.96	62.48	1.16	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
62.48	64.01	1.26	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
64.01	65.53	1.28	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
65.53	67.06	1.39	15	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.24
67.06	68.58	1.40	29	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.24
68.58	70.10	1.40	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
70.10	71.63	1.34	27	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.59
71.63	73.15	1.30	26	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17

73.15	74.68	1.34	21	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.33
74.68	76.20	1.25	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
76.20	77.72	1.26	12	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
77.72	79.25	1.30	11	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
79.25	80.77	1.34	18	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.67
80.77	82.30	1.14	15	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
82.30	83.82	0.99	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.11
83.82	85.34	1.33	17	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
85.34	86.87	1.37	17	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
86.87	88.39	1.31	18	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.51
88.39	89.92	1.26	11	1.5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.15
89.92	91.44	1.19	10	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.76
91.44	92.96	1.14	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
92.96	94.49	1.20	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
94.49	96.01	1.17	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
96.01	97.54	1.04	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
97.54	99.06	1.04	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
99.06	100.58	1.31	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
100.58	102.11	1.30	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
102.11	103.63	1.30	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
103.63	105.16	1.19	15	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.76
105.16	106.68	1.36	20	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.58
106.68	108.20	1.34	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
108.20	109.73	1.19	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
109.73	111.25	1.10	13	1	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.82
111.25	112.78	0.94	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
112.78	114.30	1.37	13	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.98
114.30	115.82	1.40	17	3	2	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.12
115.82	117.35	1.36	26	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
117.35	118.87	1.23	20	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.27
118.87	120.40	1.25	21	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
120.40	121.92	1.43	12	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
121.92	123.44	1.36	13	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
123.44	124.97	1.36	12	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
124.97	126.49	1.28	20	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
126.49	128.02	1.33	18	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.34
128.02	129.54	1.16	11	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
129.54	131.06	1.23	13	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.36
131.06	132.59	1.45	32	4.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.63
132.59	134.11	1.46	20	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.54
134.11	135.64	1.42	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
135.64	137.16	1.33	20	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.85
137.16	138.68	1.26	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
138.68	140.21	1.11	12	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.50
140.21	141.73	0.87	5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.65
141.73	143.26	1.39	11	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.89
143.26	144.78	1.08	10	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.14
144.78	146.30	1.45	10	3	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.93
146.30	147.83	1.42	21	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.63
147.83	149.35	1.33	14	4	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.93
149.35	150.88	1.39	20	6	1	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.29
150.88	152.40	1.34	12	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
152.40	153.92	1.26	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
153.92	155.45	1.31	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
155.45	156.97	1.39	11	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.32
156.97	158.50	1.23	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

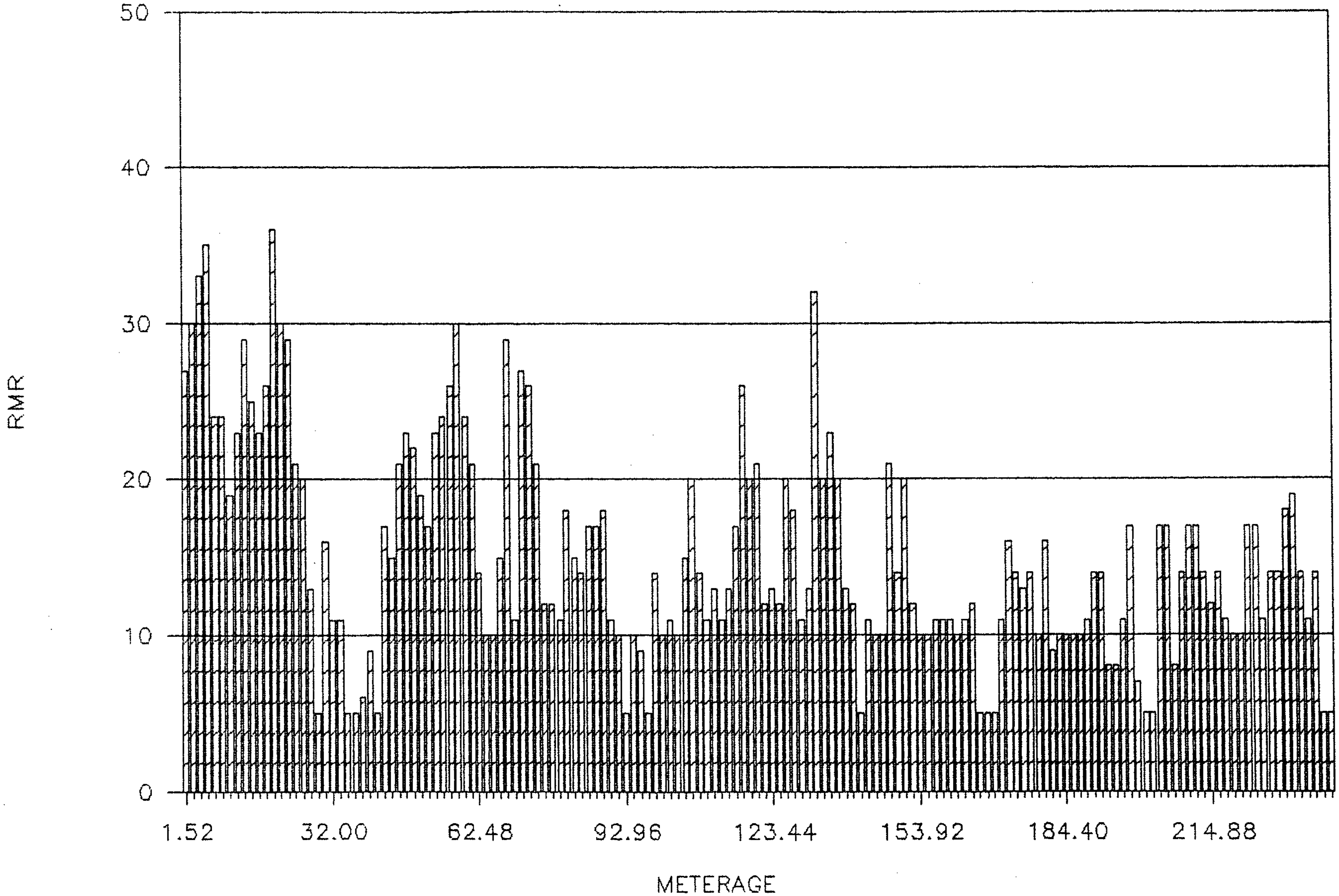
158.50	160.02	1.31	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
160.02	161.54	0.96	10	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.47
161.54	163.07	1.22	11	4.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7	1.29
163.07	164.59	0.98	12	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.81
164.59	166.12	1.02	5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.44
166.12	167.64	1.05	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.32
167.64	169.16	1.07	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
169.16	170.69	1.07	11	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.42
170.69	172.21	1.14	16	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
172.21	173.74	1.02	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.11
173.74	175.26	0.91	13	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.25
175.26	176.78	1.17	14	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.48
176.78	178.31	1.25	10	2	2	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	10	1.80
178.31	179.83	1.05	16	6	0.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	11.5	2.46
179.83	181.36	1.25	9	4	2	1.5	1.5	0.5	0.5	1	0	0.5	0	0	0	0	0	0	38	6.83
181.36	182.88	0.90	10	5	0.5	0	0.5	0	0	1	0	0	0	0	0	0	0	0	16	3.99
182.88	184.40	0.99	10	7.5	2.5	1	1	0	0	0	0	0	0	0	0	0	0	0	19.5	4.42
184.40	185.93	1.22	10	6.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	13	2.39
185.93	187.45	1.25	10	5.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	12	2.16
187.45	188.98	0.84	11	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	4.5	1.21
188.98	190.50	0.81	14	1.5	0	1	0	0	0	0	0	0	0	0	0	0	0	0	4.5	1.25
190.50	192.02	0.78	14	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.43
192.02	193.55	0.88	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
193.55	195.07	0.91	8	2	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4.5	1.10
195.07	196.60	0.90	11	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.37
196.60	198.12	0.76	17	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.15
198.12	199.64	0.66	7	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	6	2.06
199.64	201.17	0.67	5	3	1	0	1	0	0	0	0	0	0	0	0	0	0	0	9	3.01
201.17	202.69	0.69	5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	1.15
202.69	204.22	0.98	17	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.23
204.22	205.74	1.14	17	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.49
205.74	207.26	1.19	8	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
207.26	208.79	1.20	14	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.65
208.79	210.31	1.16	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
210.31	211.84	0.93	17	2	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.57
211.84	213.36	1.17	14	2	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	8	1.53
213.36	214.88	1.05	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
214.88	216.41	1.33	14	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
216.41	217.93	1.31	11	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
217.93	219.46	1.34	10	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
219.46	220.98	1.34	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
220.98	222.50	1.02	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
222.50	224.03	1.05	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
224.03	225.55	1.14	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
225.55	227.08	1.26	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
227.08	228.60	1.26	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
228.60	230.12	1.34	18	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
230.12	231.65	1.34	19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
231.65	233.17	1.13	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
233.17	234.70	0.81	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
234.70	236.22	0.93	14	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.24
236.22	237.74	0.82	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.41
237.74	238.05	0.12	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

U8613 CCRG

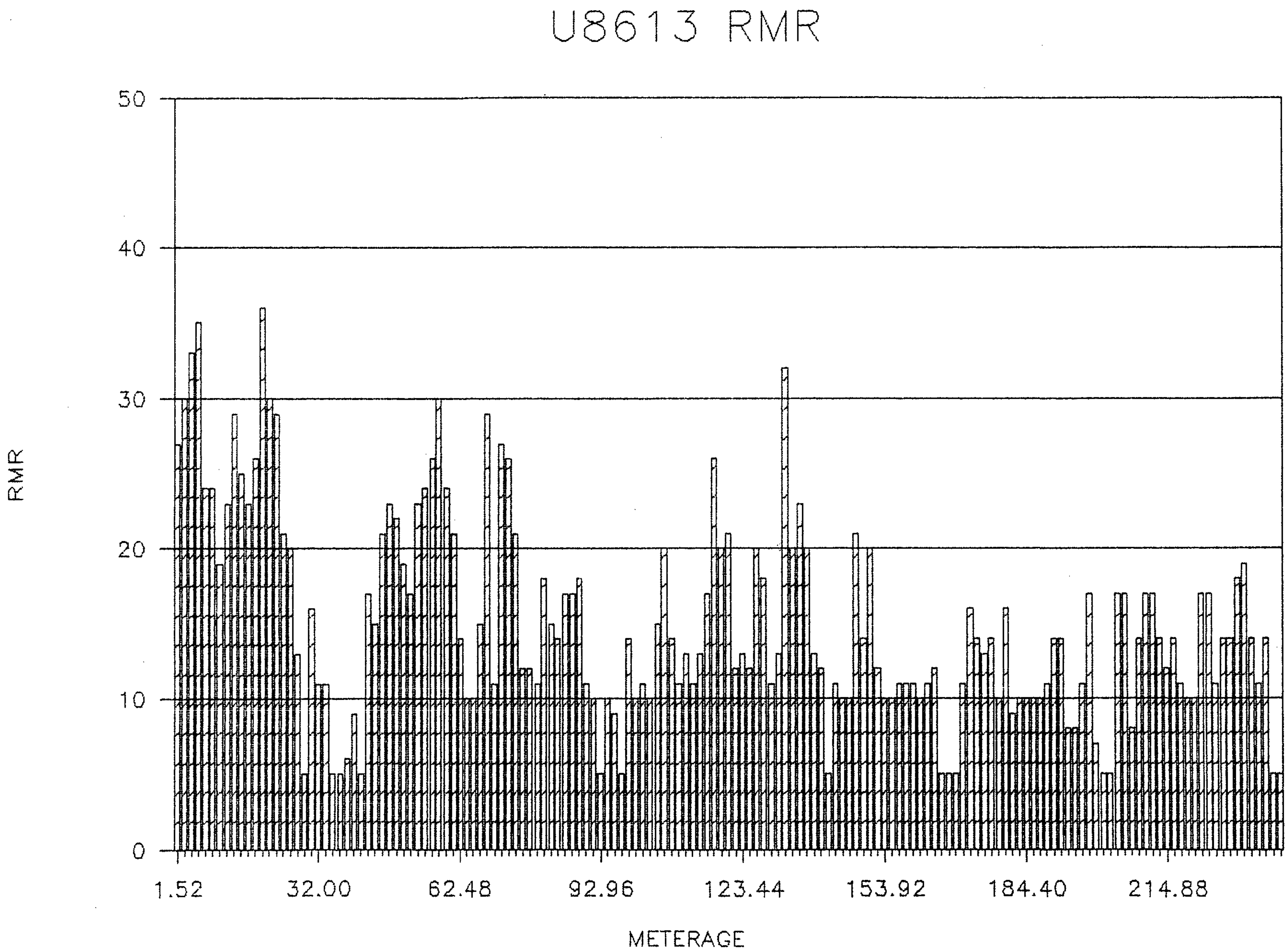


CCRG (%)
7
6
5
4
3
2
1
0
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
METERAGE

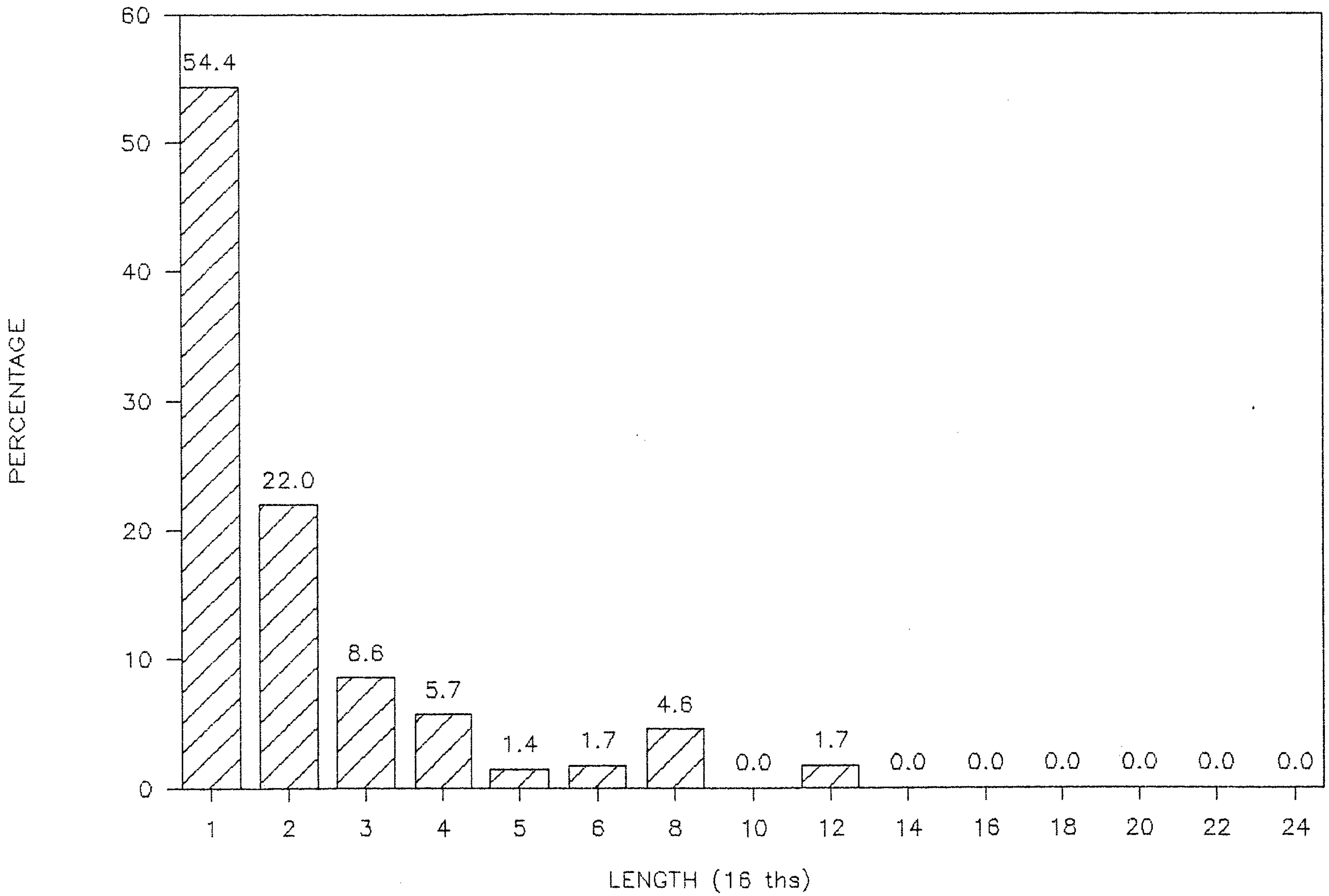
U8613 RMR



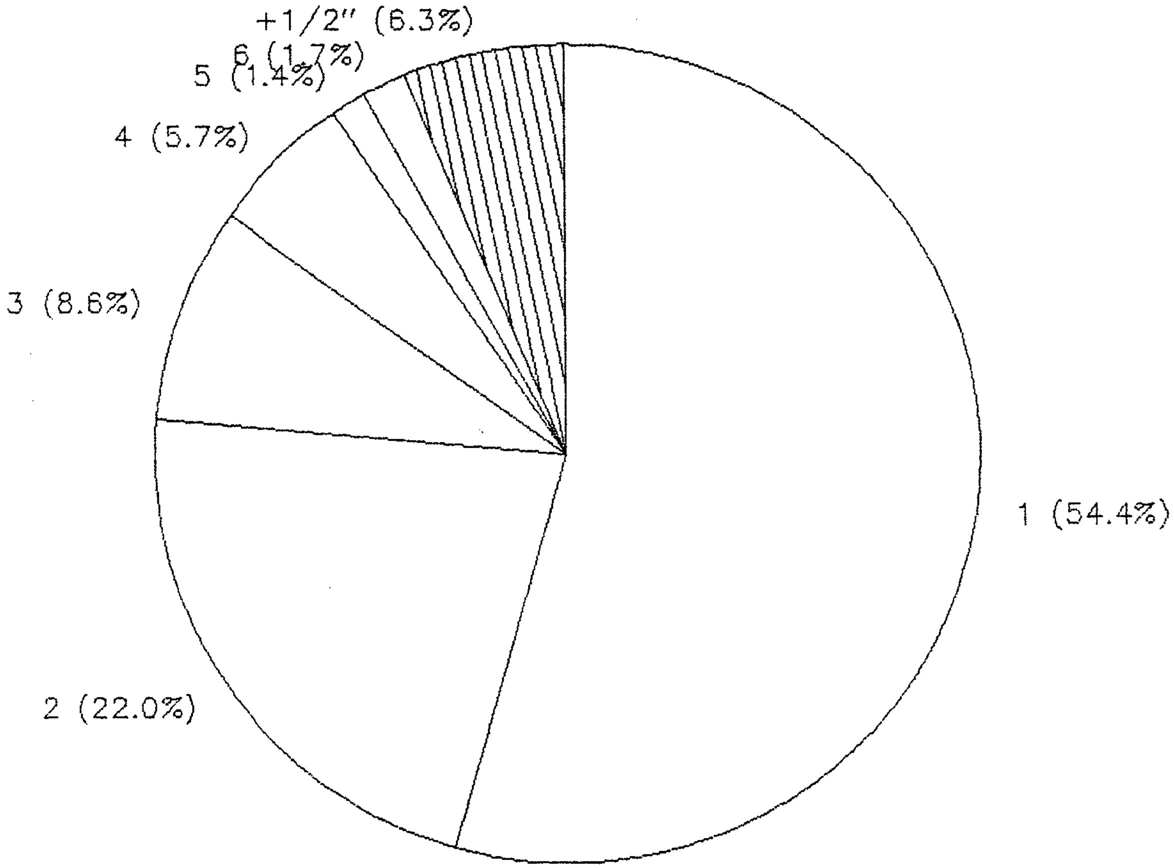
50
40
30
20
10
0
RMR
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
METERAGE


U8613 RMR
RMR
50
40
30
20
10
0
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
METERAGE

U8613 LENGTH DISTRIBUTION



U8613 LENGTH DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME | HOLE U86-14 | DEPTH 168.86 m

AZIMUTH 270° | INCLINATION -3° | SECTION 6649

LATITUDE 6647.8N | DEPARTURE 7601.4E | ELEVATION 1414.8

STARTED Oct. 12 | FINISHED Oct. 18 | LOGGED by R.E.M. date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1.5	18.9		Serpentinite. Medium dark green, fractured, low grade fibre	
			Fault zone 5.2 - 6.3	
18.9	37.5		Good fibre, blocky, medium green, mottled	
37.5	62.5		Medium dark green, minor fibre, broken	
			Fault zones 37.5 - 39.3, gouge and lizardite veins; 49.4 - 50,	
			51 - 55.2, 57.2 - 62.5	
62.5	90.5		Medium dark grey green, good fibre, lizardite veins 77.4 - 83.5	
			Fault zone 82 - 83.5 Fibre decreasing, broken	
			Fault zone 88.4 - 89.8	
90.5	91.9		Rodingite, sheared	
91.9	142.8		Medium dark grey green to dark green serp. Scattered fibre	
			veins, lizardite veining, occasional minor shears	
			Fault zones 114.6 - 115.7, 136.9 - 142.8	
142.8	148.1		Dark grey to greenish black serp, minor fibre, lizardite and	
			white mineral on joints and slips	
148.1	159.1		Fault zone, gouge and breccia, altered, some fibre, gets	
			springier with alteration	
159.1	168.9		Argillite, broken and sheared, graphitic some chert	
168.9			E.O.H.	

DDH U 8614

EAST: 7604 AZ: 270
NORTH: 6649 INCL: -5
ELEV: 1414 DEPTH: 0

AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

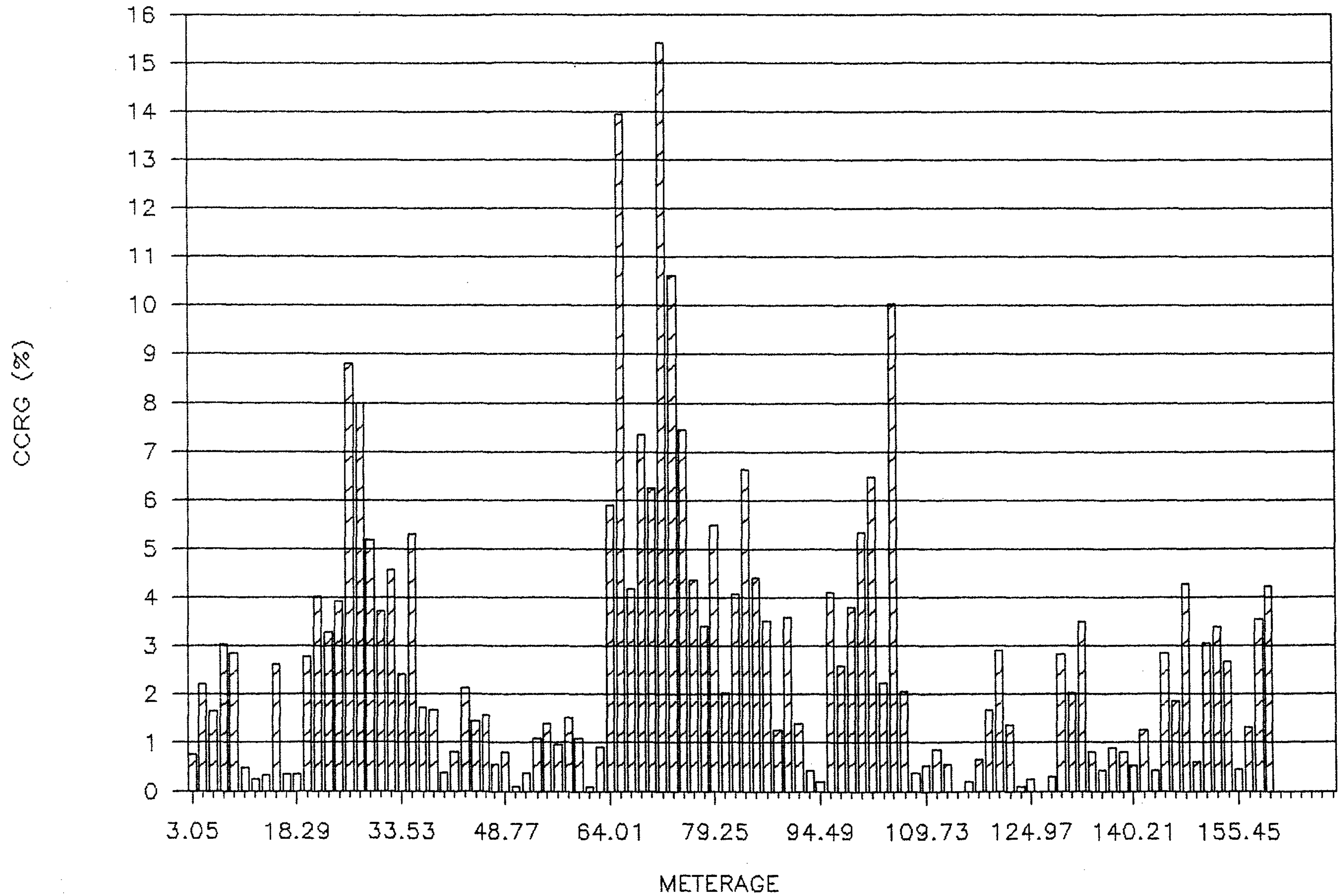
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRS %
1.52	3.05	1.04	11	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.76
3.05	4.57	1.33	12	9	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13	2.20
4.57	6.10	1.49	9	4.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11	1.65
6.10	7.62	1.48	11	13.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	20	3.04
7.62	9.14	1.34	10	13	2	0	0	0	0	0	0	0	0	0	0	0	0	0	17	2.85
9.14	10.67	1.39	24	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.49
10.67	12.19	1.34	22	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
12.19	13.72	1.36	18	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.33
13.72	15.24	1.45	9	4.5	3.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	17	2.64
15.24	16.76	1.26	7	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.35
16.76	18.29	1.31	8	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.34
18.29	19.81	1.45	19	8.5	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	18	2.79
19.81	21.34	1.45	26	8.5	4	1	1	0.5	0	0	0	0	0	0	0	0	0	0	26	4.03
21.34	22.86	1.43	16	6	2	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	21	3.29
22.86	24.38	1.37	17	6	5.5	1	1	0	0	0	0	0	0	0	0	0	0	0	24	3.93
24.38	25.91	1.48	30	9.5	3.5	1.5	3	3	1	0.5	0	0	0	0	0	0	0	0	58	8.81
25.91	27.43	1.46	23	8.5	2.5	2.5	0.5	1	2	1.5	0	0	0	0	0	0	0	0	52	7.98
27.43	28.96	1.43	19	6	2.5	0.5	1.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	33	5.17
28.96	30.48	1.42	21	9.5	1	2	0	0	1	0	0	0	0	0	0	0	0	0	23.5	3.72
30.48	32.00	1.33	17	10	4.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	27	4.57
32.00	33.53	1.39	19	4.5	2	0.5	0	1	0	0	0	0	0	0	0	0	0	0	15	2.43
33.53	35.05	1.31	14	16	2.5	0	2.5	0	0	0	0	0	0	0	0	0	0	0	31	5.31
35.05	36.58	1.37	17	8.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.72
36.58	38.10	1.40	8	4.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.68
38.10	39.62	1.19	11	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.38
39.62	41.15	1.40	15	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.80
41.15	42.67	1.26	15	7.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	12	2.13
42.67	44.20	1.31	24	5.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.45
44.20	45.72	1.42	16	9	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	10	1.58
45.72	47.24	1.25	17	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.54
47.24	48.77	1.26	16	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.80
48.77	50.29	1.26	15	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
50.29	51.82	1.23	15	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.36
51.82	53.34	0.82	6	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4	1.09
53.34	54.86	1.46	6	2	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	9	1.38
54.86	56.39	1.39	9	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.97
56.39	57.91	1.26	8	4.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	8.5	1.51
57.91	59.44	1.25	7	3	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.08
59.44	60.96	1.30	9	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
60.96	62.48	1.34	7	3.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	5.5	0.92
62.48	64.01	1.39	10	7.5	1.5	1	1	1	1	1	0	0	0	0	0	0	0	0	36.5	5.91
64.01	65.53	1.43	13	6.5	3.5	3.5	1	1	1.5	1.5	1.5	0.5	1	0	0	0	0	0	89	13.95
65.53	67.06	1.37	14	4	1.5	2.5	0.5	0	1.5	0	0	0	0	0	0	0	0	0	25.5	4.17
67.06	68.58	1.40	13	3	2	2	1	1	1.5	0.5	0.5	0.5	0	0	0	0	0	0	46	7.37
68.58	70.10	1.22	11	5	2.5	2.5	1	0.5	0	0.5	0	0.5	0	0	0	0	0	0	34	6.26
70.10	71.63	1.33	14	4	1	2	2.5	4	3	1.5	0	1	0.5	0	0	0	0	0	91	15.41
71.63	73.15	1.48	16	1.5	2	0	3	1.5	0.5	0	1.5	1	0.5	0.5	0	0	0	0	70	10.63

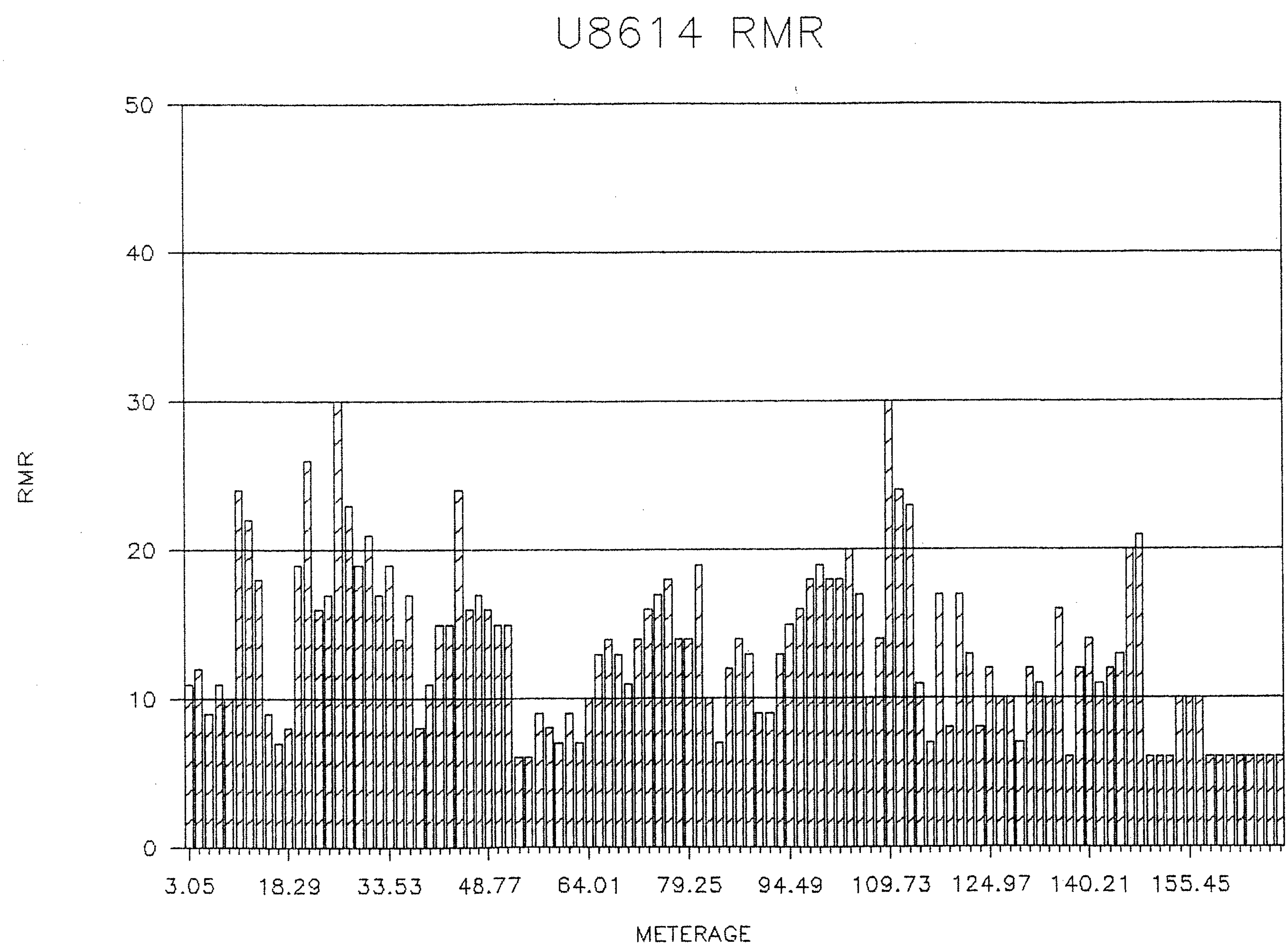
73.15	74.68	1.26	17	2.5	1	0.5	0	0	0	1	0.5	0	0.5	1	0	0	0	0	42	7.45
74.68	76.20	1.46	18	5	3.5	1.5	0.5	0	0	0.5	0	0.5	0	0	0	0	0	0	28.5	4.37
76.20	77.72	1.42	14	5	2.5	0	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	21.5	3.41
77.72	79.25	1.43	14	7	1.5	2	1	0	0.5	0.5	0	0	0	0.5	0	0	0	0	35	5.48
79.25	80.77	1.49	19	3	1.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	13.5	2.03
80.77	82.30	1.16	10	3	2	2.5	1	0.5	0	0	0	0	0	0	0	0	0	0	21	4.07
82.30	83.82	1.25	7	3	2.5	0.5	1	0.5	1.5	1.5	0	0	0	0	0	0	0	0	37	6.65
83.82	85.34	1.48	12	6	1.5	1	0.5	0	0.5	1.5	0	0	0	0	0	0	0	0	29	4.40
85.34	86.87	1.40	14	4.5	2	1	0.5	0.5	1	0	0	0	0	0	0	0	0	0	22	3.52
86.87	88.39	1.42	13	4	2	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.27
88.39	89.92	1.22	9	1.5	1.5	0.5	0.5	0.5	0.5	0	0	0.5	0	0	0	0	0	0	19.5	3.59
89.92	91.44	1.22	9	2.5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.38
91.44	92.96	1.36	13	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
92.96	94.49	1.13	15	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
94.49	96.01	1.34	16	6	0.5	0	0.5	0.5	0.5	0.5	0	0.5	0	0	0	0	0	0	24.5	4.10
96.01	97.54	1.39	18	5	2	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	16	2.59
97.54	99.06	1.36	19	4.5	1	0	0.5	0.5	0.5	0	0	0	0	0	0.5	0	0	0	23	3.81
99.06	100.58	1.39	18	9	3	2	0	0	0.5	0	0	0	0	0	0.5	0	0	0	33	5.34
100.58	102.11	1.42	18	9	1.5	1	0	0	0.5	1	1.5	0	0	0	0	0	0	0	41	6.49
102.11	103.63	1.40	20	6	0.5	1	1	0	0	0	0	0	0	0	0	0	0	0	14	2.24
103.63	105.16	1.43	17	8	5.5	1.5	1	1.5	1.5	0.5	0	0	0.5	0	0.5	0	0	0	64	10.03
105.16	106.68	1.31	10	4.5	0	0	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	12	2.06
106.68	108.20	1.48	14	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.38
108.20	109.73	1.51	30	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.52
109.73	111.25	1.45	24	2.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.85
111.25	112.78	1.45	23	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.54
112.78	114.30	1.28	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
114.30	115.82	1.16	7	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
115.82	117.35	1.37	17	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.65
117.35	118.87	1.20	8	6	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.68
118.87	120.40	1.31	17	7	3.5	1	0	0	0	0	0	0	0	0	0	0	0	0	17	2.91
120.40	121.92	1.33	13	4.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8	1.35
121.92	123.44	1.43	8	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
123.44	124.97	1.33	12	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
124.97	126.49	1.22	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
126.49	128.02	1.14	10	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.29
128.02	129.54	1.23	7	6.5	3	1	0	0	0	0	0	0	0	0	0	0	0	0	15.5	2.82
129.54	131.06	1.33	12	3.5	2	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	12	2.03
131.06	132.59	1.36	11	5.5	3	1	0	0.5	0	0.5	0	0	0	0	0	0	0	0	21	3.48
132.59	134.11	1.26	10	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.80
134.11	135.64	1.36	16	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
135.64	137.16	1.02	6	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.88
137.16	138.68	1.37	12	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5	0.82
138.68	140.21	1.26	14	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.53
140.21	141.73	1.34	11	5	0	0	0	0.5	0	0	0	0	0	0	0	0	0	0	7.5	1.26
141.73	143.26	1.34	12	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.42
143.26	144.78	1.42	13	4.5	2	1	1	0.5	0	0	0	0	0	0	0	0	0	0	18	2.85
144.78	146.30	1.52	20	5.5	2	1	0	0	0	0	0	0	0	0	0	0	0	0	12.5	1.84
146.30	147.83	1.42	21	7	2	2	1	0	1	0	0	0	0	0	0	0	0	0	27	4.28
147.83	149.35	1.30	6	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.61
149.35	150.88	1.25	6	3	0	1	0.5	0	0	0.5	0.5	0	0	0	0	0	0	0	17	3.05
150.88	152.40	0.93	6	10	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	14	3.38
152.40	153.92	1.39	10	10	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	16.5	2.67
153.92	155.45	1.49	10	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.45
155.45	156.97	1.45	10	4.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.32
156.97	158.50	1.23	6	2.5	0.5	0.5	1	0.5	0.5	0	0.5	0	0	0	0	0	0	0	19.5	3.55

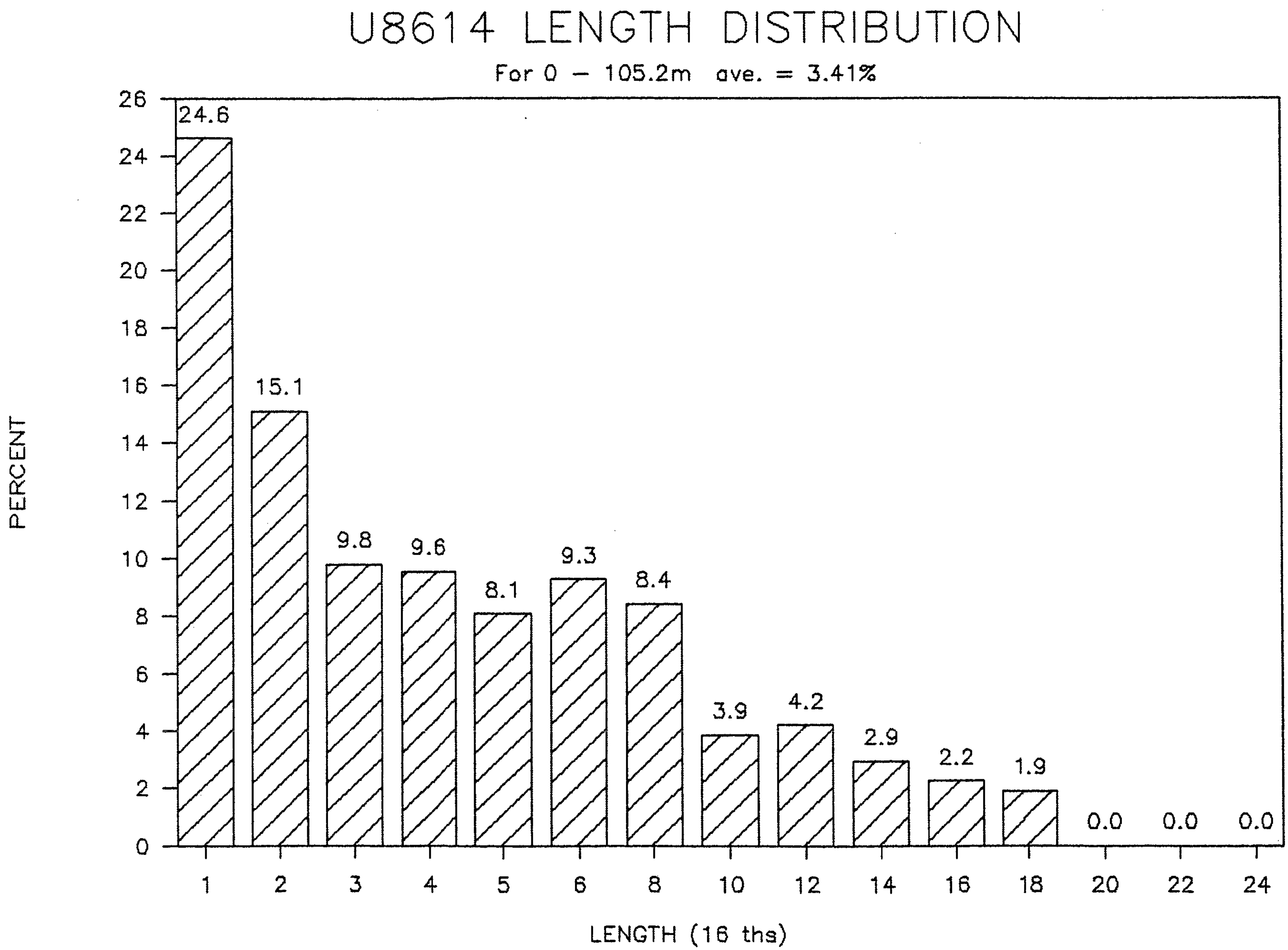
158.50	160.02	0.72	6	0.5	2.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	13.5	4.23
160.02	161.54	0.17	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
161.54	163.07	0.17	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
163.07	164.59	0.23	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
164.59	166.12	0.23	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
166.12	167.64	0.56	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
167.64	168.86	0.27	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

EOH

U8614 CCRG


CCRG (%)
16
15
14
13
12
11
10
9
8
7
6
5
4
3
2
1
0
3.05
18.29
33.53
48.77
64.01
79.25
94.49
109.73
124.97
140.21
155.45
METERAGE


U8614 RMR
50
40
30
20
10
0
RMR
3.05
18.29
33.53
48.77
64.01
79.25
94.49
109.73
124.97
140.21
155.45
METERAGE


U8614 LENGTH DISTRIBUTION
For 0 – 105.2m ave. = 3.41%
PERCENT
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16
18
20
22
24
26
24.6
15.1
9.8
9.6
8.1
9.3
8.4
3.9
4.2
2.9
2.2
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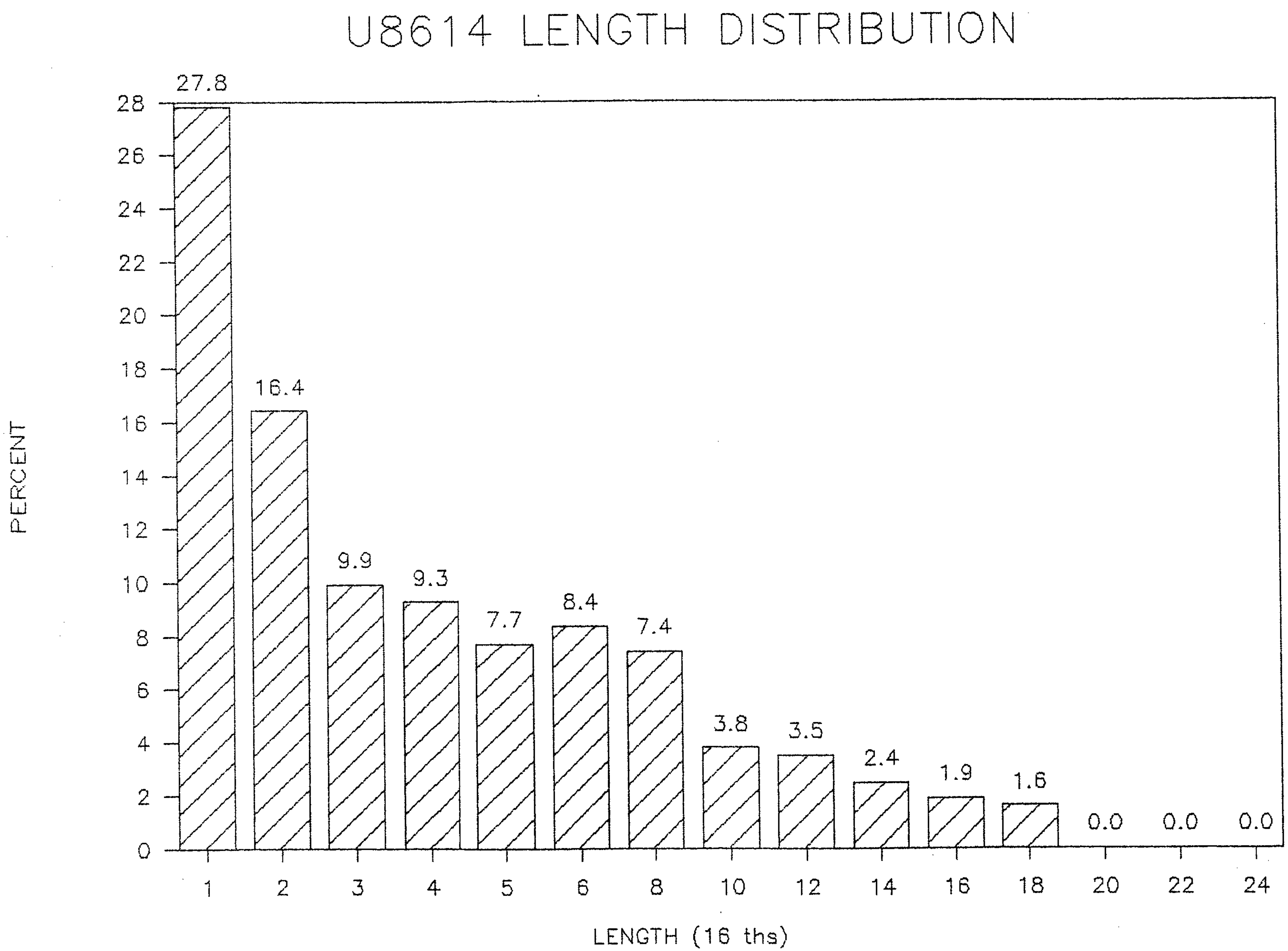
LENGTH (16 ths)



U8614 LENGTH DISTRIBUTION
PERCENT
LENGTH (16 ths)
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27.8
16.4
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7.7
8.4
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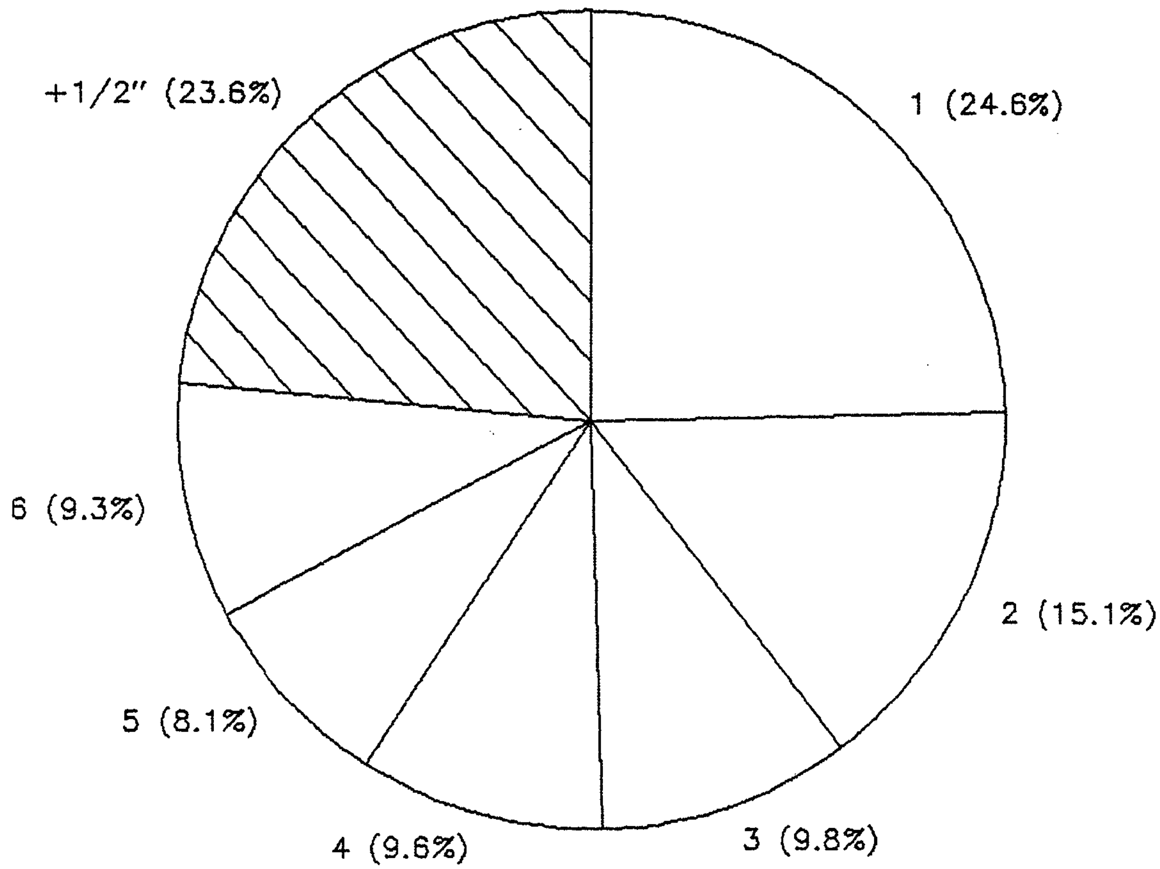
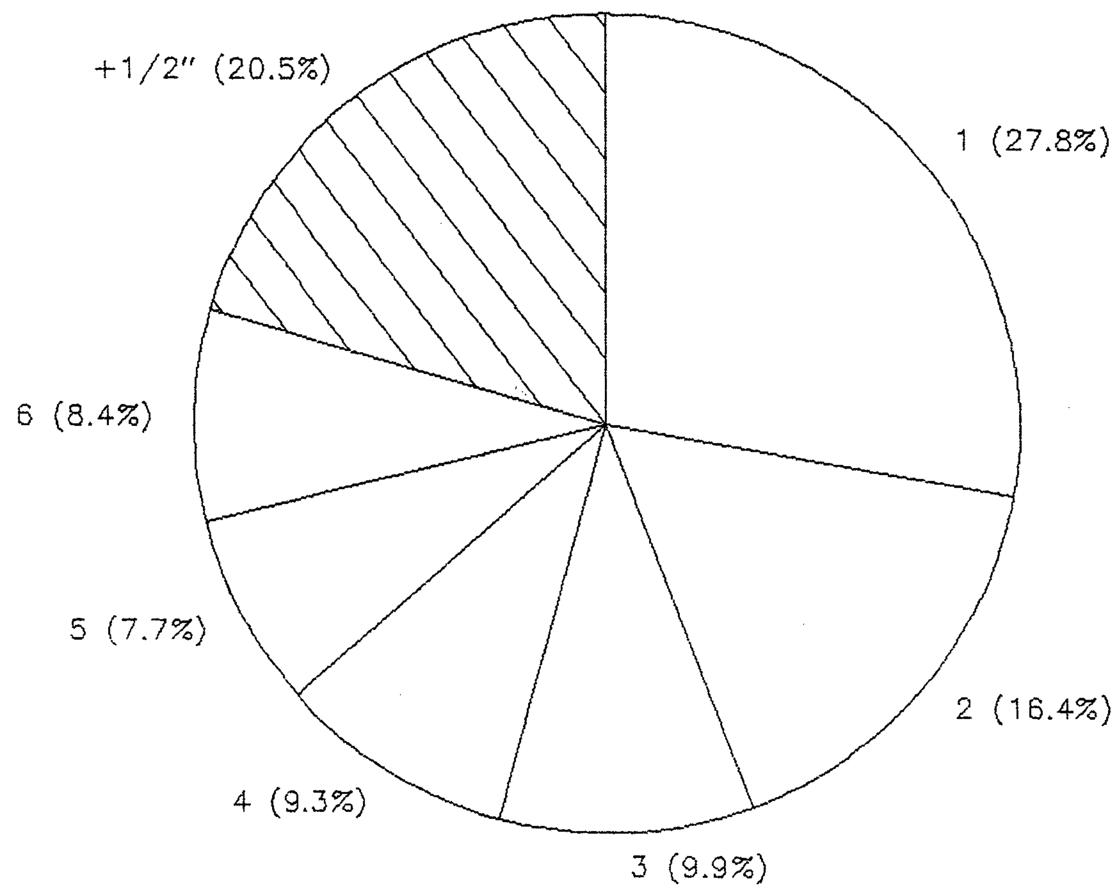
3.8
3.5
2.4
1.9
1.6
0.0
0.0
0.0

U8614 LENGTH DISTRIBUTION



U8614 LENGTH DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME	HOLE	U86-15	DEPTH	184.71 m
AZIMUTH	277.27	INCLINATION	-68.43°	SECTION	6649
LATITUDE	6647.792N	DEPARTURE	7601.862E	ELEVATION	1414.286 m
STARTED	Oct. 19	FINISHED	Oct. 25	LOGGED	by R.E.M. date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1.22	14.6		Serpentinite, medium-dark green, fibre bearing, broken	
14.6	61.3		Lighter grey green, good fibre, often broken	
			Fault zones: 16.3 - 17.1, 24.4 - 25.8, 28.6 - 32.9, 58.2 - 61.3	
61.3	65.8		Very dark grey to black serp, fibre bearing	
65.8	91.9		Dark green to apple green, fractured, fibre bearing	
			Broken 67.4 - 69.2, 70.7 - 71.9, 79.6 - 90.2	
			Fault zone 90.2 - 91.9	
91.9	113.7		Dark grey green, fibre bearing	
			Fault zones 98.2 - 107.6, lizardite co-mon, 112.2 - 113.7	
113.7	149.7		Very dark grey green to blackish green, minor fibre	
			Fault zones 118.6 - 122.8, begin to get greyish	
			alteration past 138.4 m, minor faults scattered.	
149.7	152		Light grey green altered serp., broken and sheared	
152	159.6		Dark grey serp, fault 156.1 - 159.7 gouge and broken	
159.6	160.9		Rodingite, light greyish green	
160.9	178.9		Serp fault zone, mostly altered to mottled med. grey-dark grey,	
			some fibre	
			Strongly altered light grey-greenish grey serp	
178.9	184.7		Argillite, fractured and broken	
184.7			E.O.H.	

DDH U 8615

EAST: 7604 AZ: 270
NORTH: 6649 INCL: -70
ELEV: 1415 DEPTH:184.7

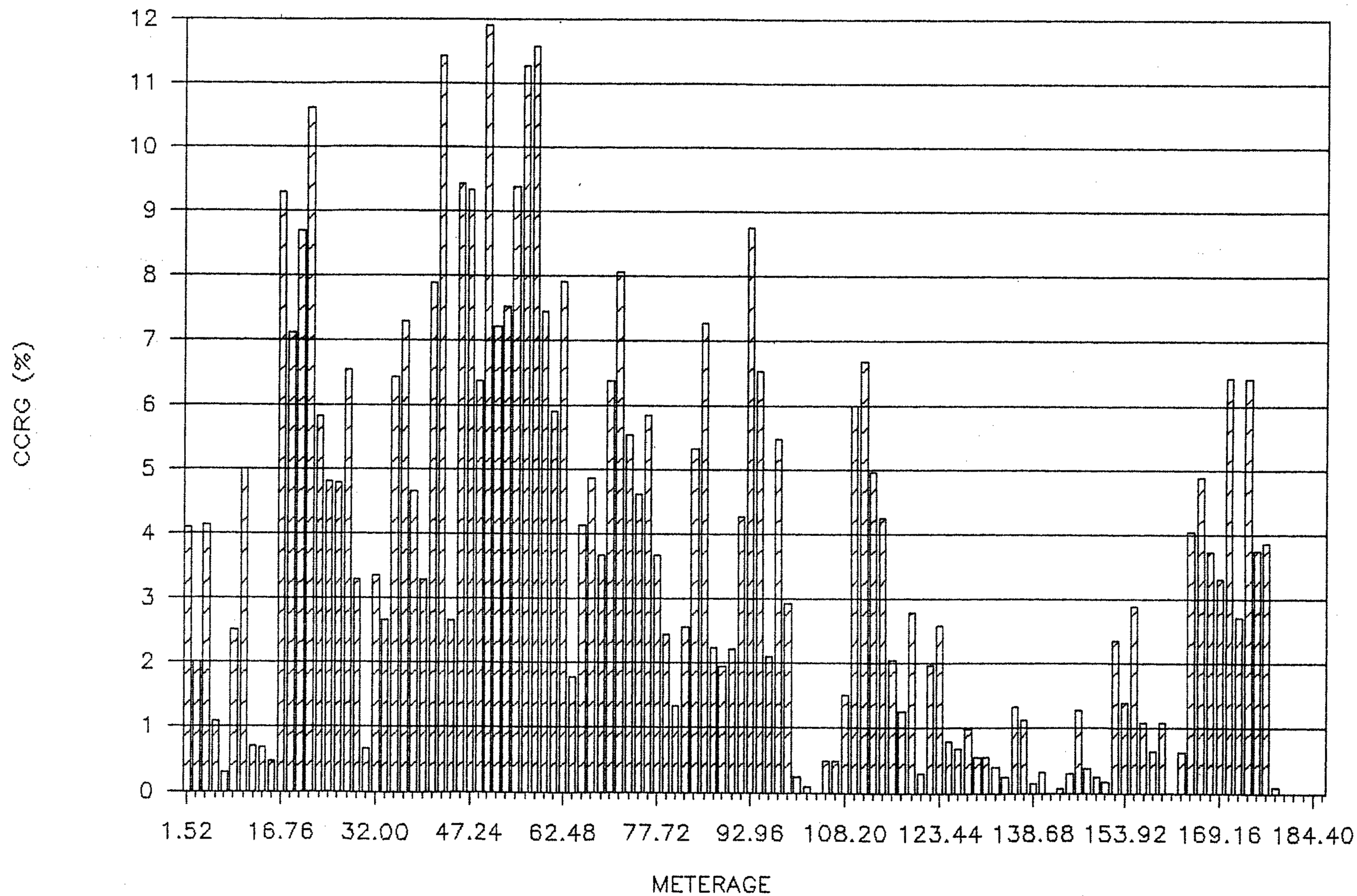
AVERAGE OF TWO COUNTS
Number of fibre veins counted per 16th category

FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCR8 %
0.00	1.52	0.14	14	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	2.5	4.09
1.52	3.05	0.90	17	4.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8	2.00
3.05	4.57	1.36	7	6.5	2	0.5	0.5	1	1	0	0	0	0	0	0	0	0	0	25	4.14
4.57	6.10	1.25	5	4	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	6	1.08
6.10	7.62	1.13	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.30
7.62	9.14	1.39	10	7.5	2.5	0	0	0	0.5	0	0	0	0	0	0	0	0	0	15.5	2.51
9.14	10.67	1.42	19	13.5	3.5	1	1	0	0	0.5	0	0	0	0	0	0	0	0	31.5	4.99
10.67	12.19	1.45	27	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.70
12.19	13.72	1.48	21	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	4.5	0.68
13.72	15.24	1.42	18	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	3	0.48
15.24	16.76	1.46	10	5	3	1.5	1	1	0	1.5	0	0.5	0	0.5	0	0.5	0	0	60.5	9.28
16.76	18.29	1.40	11	8.5	1	1	2.5	1	2	0.5	0	0	0	0	0	0	0	0	44.5	7.12
18.29	19.81	1.43	27	9.5	3.5	1	1.5	0	1.5	2	0.5	0	0	0	0	0	0	0	55.5	8.70
19.81	21.34	1.42	23	7	2	1	1	1	4.5	0.5	0	0.5	0.5	0	0	0	0	0	67	10.61
21.34	22.86	1.39	22	7.5	0.5	0	2.5	0.5	0.5	0	0	1	0	0	0	0	0	0	36	5.83
22.86	24.38	1.40	28	4.5	3.5	2	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	30	4.80
24.38	25.91	1.22	8	10.5	3	1	0	0.5	0	0.5	0	0	0	0	0	0	0	0	26	4.79
25.91	27.43	1.52	19	8.5	1.5	1	1	1	0.5	1.5	0	0.5	0	0	0	0	0	0	44.5	6.55
27.43	28.96	1.46	19	10	3	1	0	0.5	0	0	0	0	0	0	0	0	0	0	21.5	3.30
28.96	30.48	1.37	9	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.65
30.48	32.00	1.34	5	4	2	0	0.5	0	0	0	1	0	0	0	0	0	0	0	20	3.35
32.00	33.53	1.43	8	7.5	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	17	2.66
33.53	35.05	1.33	8	15.5	4	2.5	0.5	1	0	0	0	0	0	0	0	0	0	0	38	6.43
35.05	36.58	1.45	16	13.5	5	2.5	1.5	0	1	0.5	0	0	0	0	0	0	0	0	47	7.29
36.58	38.10	1.45	10	14.5	3	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	30	4.65
38.10	39.62	1.43	8	7	3	0	0	0	0	1	0	0	0	0	0	0	0	0	21	3.29
39.62	41.15	1.49	18	4.5	1.5	1	0.5	0	0.5	0	0	0.5	0.5	0	0	0	0	1	52.5	7.89
41.15	42.67	1.39	10	5	3.5	0.5	2.5	1	0	0	0.5	0	0.5	0.5	0	0.5	0	0.5	70.5	11.41
42.67	44.20	1.43	9	3	1.5	0	0	0	0.5	1	0	0	0	0	0	0	0	0	17	2.66
44.20	45.72	1.31	14	4.5	1	1	1	0.5	1.5	1	0	0.5	0	1	0	0	0	0	55	9.42
45.72	47.24	1.43	18	4.5	2.5	2	0	0	1	0	0	0	1	0	0	0	0	1	59.5	9.32
47.24	48.77	1.46	22	12	5.5	0.5	3	0	0	0	0.5	0	0	0	0	0	0	0	41.5	6.37
48.77	50.29	1.39	17	2	2	1	1.5	1.5	2.5	2.5	1	0.5	0	0	0	0	0	0	73.5	11.90
50.29	51.82	1.51	11	9	2	2.5	0.5	1	0.5	0.5	0.5	0	0	0	0.5	0	0	0	48.5	7.22
51.82	53.34	1.37	17	7	5	1	0.5	1	0.5	2	0	0	0	0	0	0	0	0	46	7.53
53.34	54.86	1.11	16	5	2	1.5	0.5	0	0	0.5	0	1	0.5	0.5	0	0	0	0	46.5	9.38
54.86	56.39	1.33	17	4.5	3.5	2	2	3	1	1.5	0	0	0	0.5	0	0	0	0	66.5	11.26
56.39	57.91	1.39	17	5.5	6	1	1	1	1.5	1.5	0.5	0	0.5	0	0.5	0	0	0	71.5	11.57
57.91	59.44	1.48	8	12	5.5	3.5	2	0.5	0	0	0.5	0	0	0	0	0	0	0	49	7.44
59.44	60.96	1.39	10	5	2	1	0.5	0.5	0	1	0	1	0	0	0	0	0	0	36.5	5.91
60.96	62.48	1.43	10	9.5	3.5	0	1	1	0.5	1	0	0	1	0	0	0	0	0	50.5	7.91
62.48	64.01	1.52	26	2	0	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	12	1.77
64.01	65.53	1.52	24	3	1.5	0.5	1.5	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	28	4.12
65.53	67.06	1.52	9	5.5	5	2	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	33	4.86
67.06	68.58	1.37	12	6	3	2.5	0	0	0.5	0	0	0	0	0	0	0	0	0	22.5	3.68
68.58	70.10	1.48	19	4.5	3	2.5	1	2	1	0.5	0	0	0	0	0	0	0	0	42	6.38
70.10	71.63	1.28	7	7.5	5	1	1	0.5	2	0	0	0	0.5	0	0	0	0	0	46	8.07
71.63	73.15	1.48	11	8	4.5	0	1.5	0.5	0	0.5	0	0	0.5	0	0	0	0	0	36.5	5.54

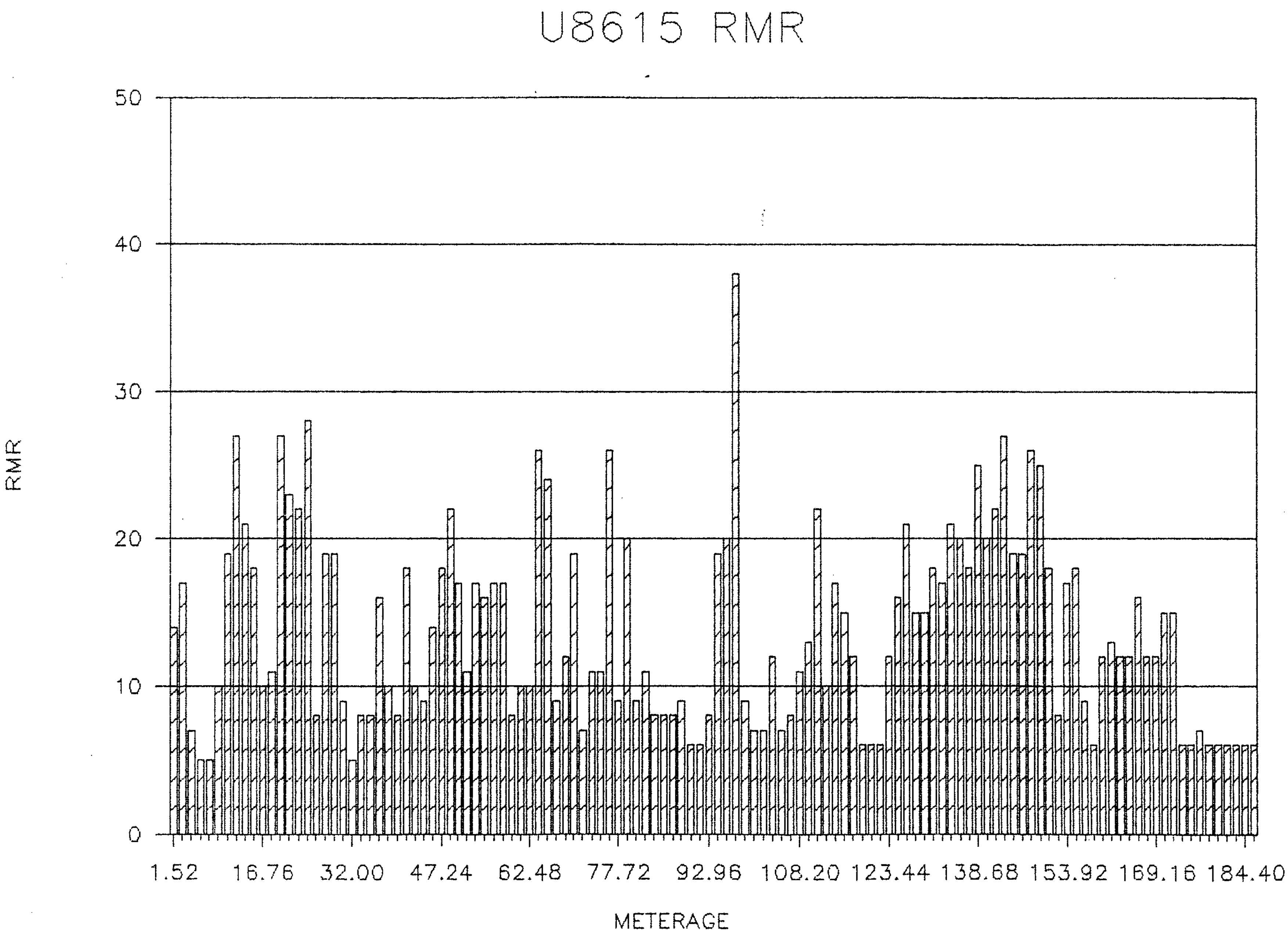
73.15	74.68	1.51	11	5.5	1.5	3	0.5	0.5	1.5	0	0	0	0	0	0	0	0	0	31	4.61
74.68	76.20	1.40	26	10	4	2.5	1.5	1	0	0	0	0	0	0	0	0	0	0	36.5	5.84
76.20	77.72	1.43	9	8.5	3	1	0.5	0	0	0.5	0	0	0	0	0	0	0	0	23.5	3.68
77.72	79.25	1.51	20	10	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	16.5	2.46
79.25	80.77	1.51	9	5.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9	1.34
80.77	82.30	1.49	11	11	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	17	2.56
82.30	83.82	1.43	8	10.5	1.5	1.5	1	1	0.5	0.5	0	0	0	0	0	0	0	0	34	5.33
83.82	85.34	1.39	8	8.5	1	1.5	1	2	2	0.5	0	0	0	0	0	0	0	0	45	7.28
85.34	86.87	1.40	8	5	1	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	14	2.24
86.87	88.39	1.39	9	7	0	1	0.5	0	0	0	0	0	0	0	0	0	0	0	12	1.94
88.39	89.92	1.22	6	1.5	1	1.5	1	0	0	0	0	0	0	0	0	0	0	0	12	2.21
89.92	91.44	1.42	6	8	6	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	27	4.28
91.44	92.96	1.37	8	11.5	1.5	1.5	1.5	0.5	0	0	1	0	0	1	0	0	0	0	53.5	8.76
92.96	94.49	1.48	19	8.5	3.5	1	0.5	0.5	0	1	0	1	0	0	0	0	0	0	43	6.53
94.49	96.01	1.39	20	4.5	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	13	2.10
96.01	97.54	1.42	38	6	3	1.5	2	0	1	0.5	0	0	0	0	0	0	0	0	34.5	5.46
97.54	99.06	1.49	9	6.5	1	0.5	0.5	1.5	0	0	0	0	0	0	0	0	0	0	19.5	2.93
99.06	100.58	1.36	7	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
100.58	102.11	1.34	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
102.11	103.63	1.26	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
103.63	105.16	1.37	7	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.49
105.16	106.68	1.39	8	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.49
106.68	108.20	1.49	11	3.5	1	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	10	1.50
108.20	109.73	1.48	13	11	5	1.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	39.5	6.00
109.73	111.25	1.49	22	8	3.5	3	2	0.5	0	0	1	0	0	0	0	0	0	0	44.5	6.69
111.25	112.78	1.36	10	6.5	2	0.5	0	1	0.5	0	1	0	0	0	0	0	0	0	30	4.97
112.78	114.30	1.48	17	5.5	1	1.5	1	1	0.5	0.5	0	0	0	0	0	0	0	0	28	4.25
114.30	115.82	1.43	15	5	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13	2.04
115.82	117.35	1.25	12	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.26
117.35	118.87	1.20	6	6	2	0	0.5	0	0.5	0	0	0	0	0	0	0	0	0	15	2.80
118.87	120.40	1.17	6	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.29
120.40	121.92	0.91	6	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.96
121.92	123.44	0.91	12	2.5	1.5	0	0.5	0	0.5	0	0	0	0	0	0	0	0	0	10.5	2.58
123.44	124.97	1.40	16	2	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.80
124.97	126.49	1.49	21	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.68
126.49	128.02	1.36	15	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.99
128.02	129.54	1.45	15	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.54
129.54	131.06	1.46	18	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.54
131.06	132.59	1.46	17	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.38
132.59	134.11	1.42	21	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.24
134.11	135.64	1.43	20	4	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.33
135.64	137.16	1.51	18	5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.12
137.16	138.68	1.51	25	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
138.68	140.21	1.39	20	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.32
140.21	141.73	1.49	22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
141.73	143.26	1.52	27	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.07
143.26	144.78	1.48	19	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.30
144.78	146.30	1.42	19	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.27
146.30	147.83	1.48	26	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.38
147.83	149.35	1.42	25	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.24
149.35	150.88	1.43	18	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
150.88	152.40	1.43	8	1.5	3	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	15	2.35
152.40	153.92	1.46	17	4	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.38
153.92	155.45	1.48	18	2	1.5	0	0.5	0	2	0	0	0	0	0	0	0	0	0	19	2.89
155.45	156.97	1.36	9	1.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	6.5	1.08
156.97	158.50	0.70	6	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.64

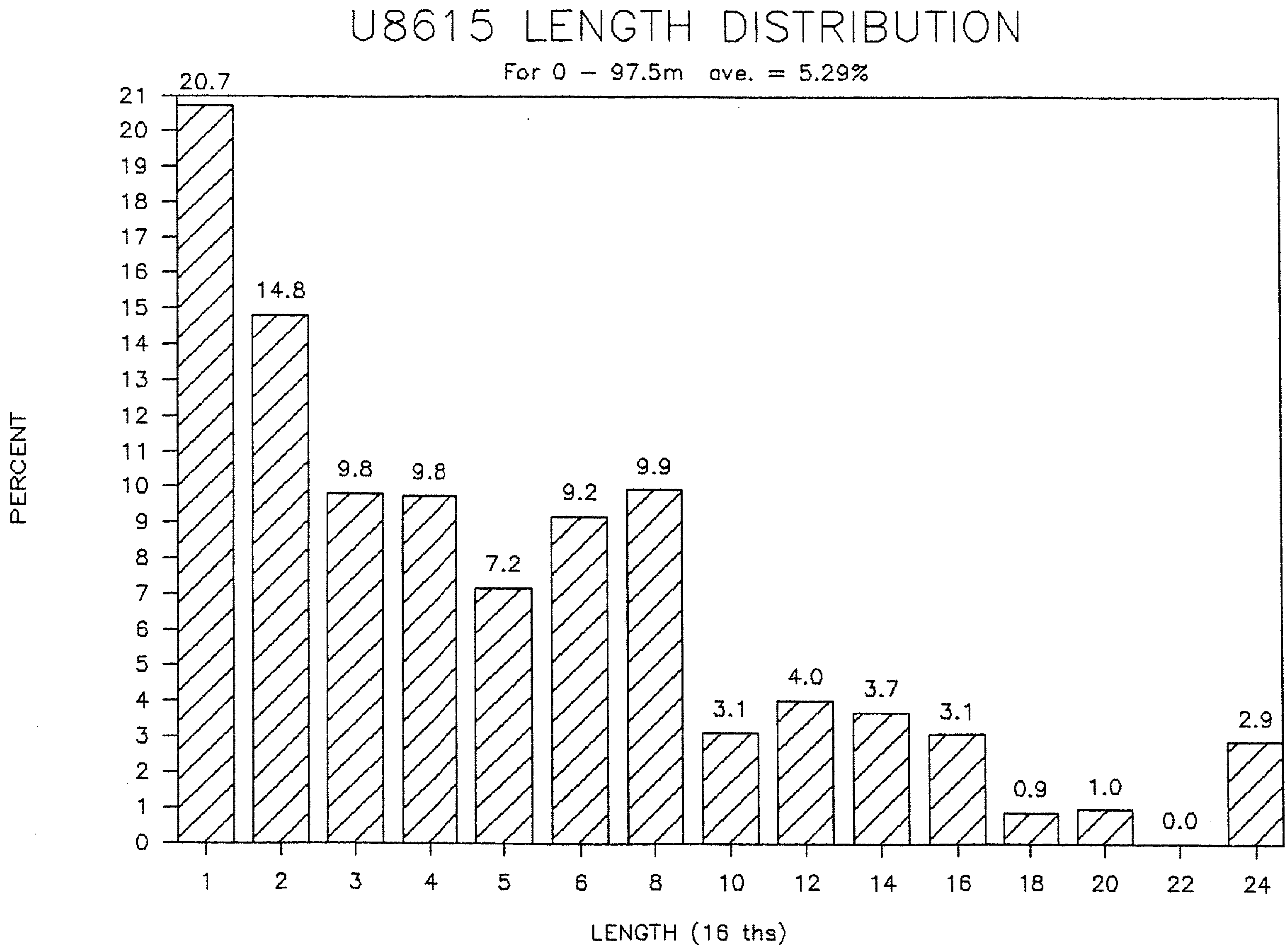
158.50	160.02	1.25	12	2	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	6	1.08
160.02	161.54	1.31	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
161.54	163.07	1.08	12	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.62
163.07	164.59	1.25	12	8.5	4	0	0	0	1	0	0	0	0	0	0	0	0	0	22.5	4.04
164.59	166.12	1.36	16	7	3.5	2	1	0.5	0.5	0	0	0	0	0	0	0	0	0	29.5	4.88
166.12	167.64	1.23	12	7.5	3	1	1	0	0	0	0	0	0	0	0	0	0	0	20.5	3.73
167.64	169.16	1.33	12	7	2.5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	19.5	3.30
169.16	170.69	1.33	15	7	1.5	0.5	1	0.5	0.5	0	1	0	0.5	0	0	0	0	0	38	6.43
170.69	172.21	1.45	15	5	3	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	17.5	2.71
172.21	173.74	1.07	6	11.5	2.5	0.5	1	0.5	1	0	0	0	0	0	0	0	0	0	30.5	6.42
173.74	175.26	0.99	6	5.5	3.5	0	1	0	0	0	0	0	0	0	0	0	0	0	16.5	3.74
175.26	176.78	1.19	7	4	2.5	1	1.5	0.5	0	0	0	0	0	0	0	0	0	0	20.5	3.87
176.78	178.31	1.17	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
178.31	179.83	1.13	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
179.83	181.36	0.79	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
181.36	182.88	0.66	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
182.88	184.40	0.66	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
184.40	184.71	0.21	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
	EOH																			

U8615 CCRG

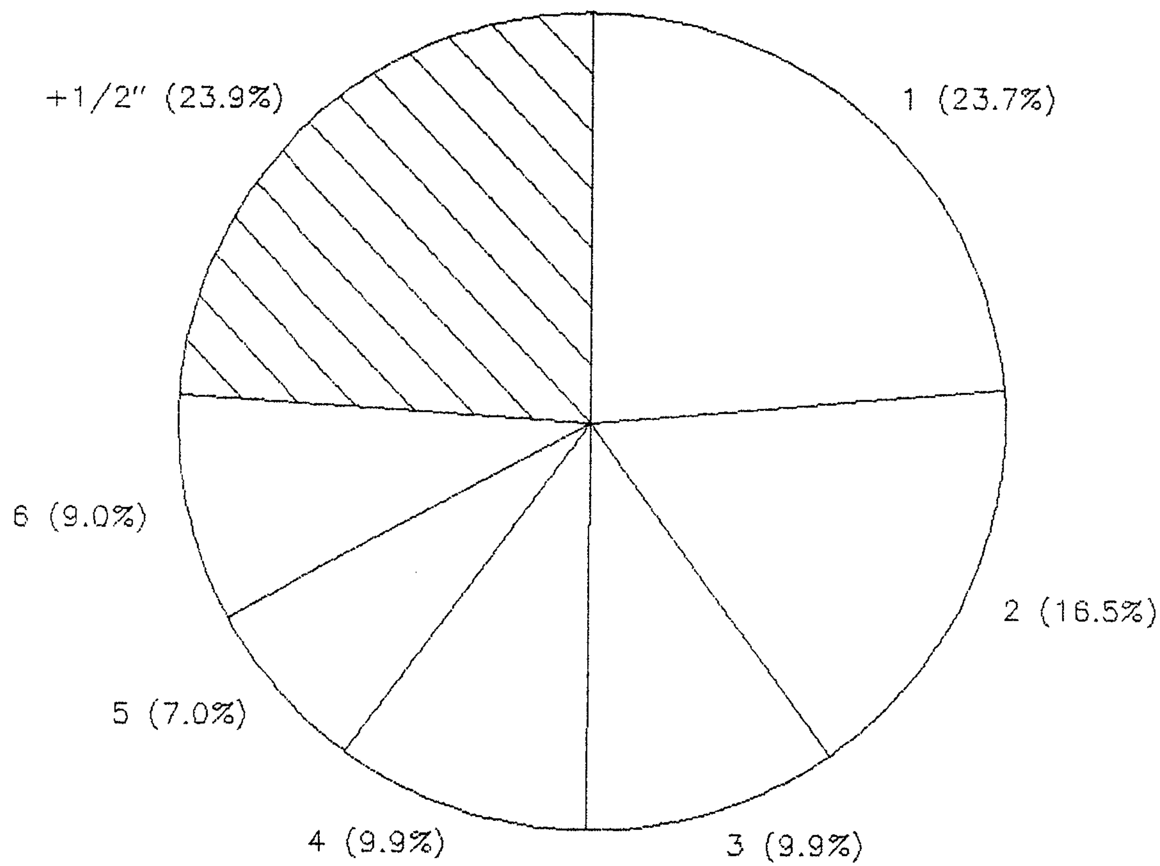


12
11
10
9
8
7
6
5
4
3
2
1
0
CCRG (%)
1.52
16.76
32.00
47.24
62.48
77.72
92.96
108.20
123.44
138.68
153.92
169.16
184.40
METERAGE

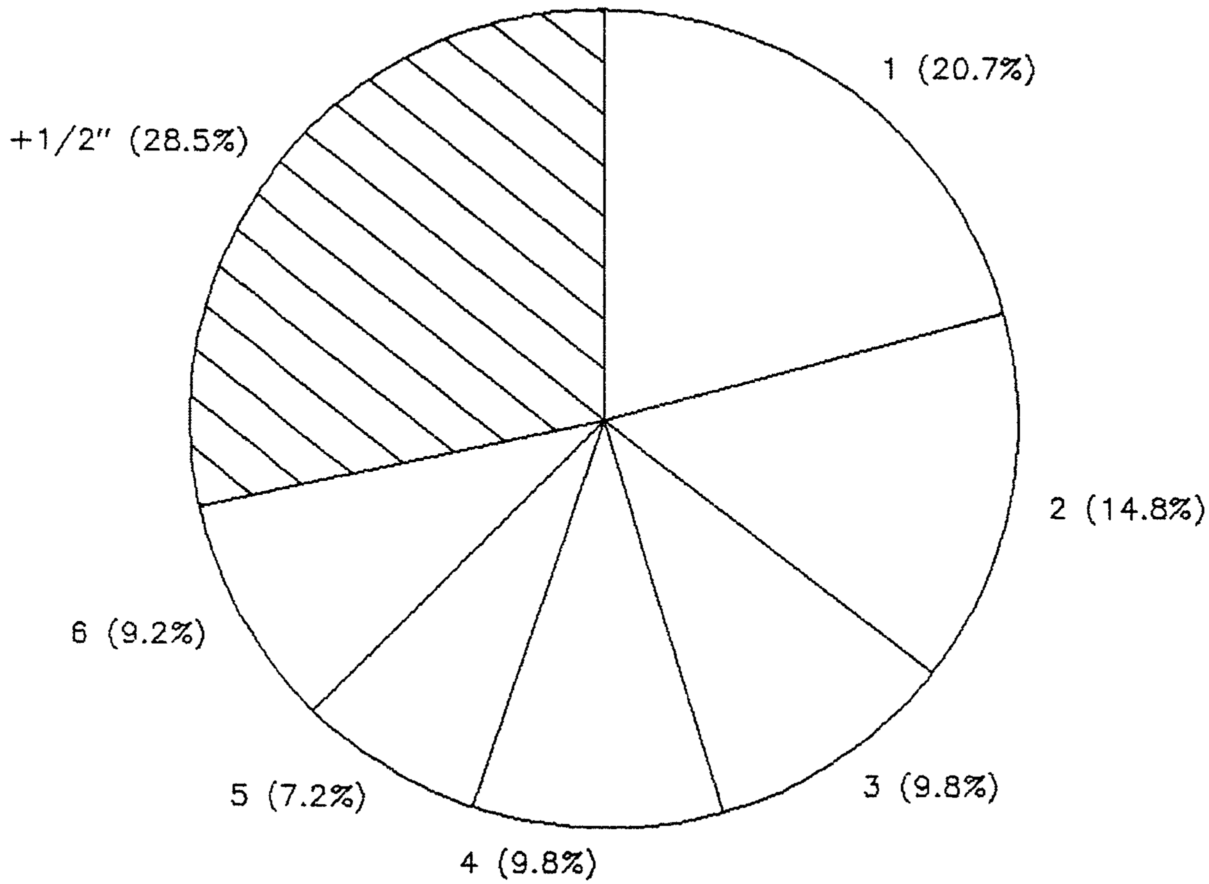

U8615 RMR
RMR
METERAGE
0
10
20
30
40
50
1.52
16.76
32.00
47.24
62.48
77.72
92.96
108.20
123.44
138.68
153.92
169.16
184.40


U8615 LENGTH DISTRIBUTION
For 0 – 97.5m ave. = 5.29%
PERCENT
0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
20.7
14.8
9.8
9.8
7.2
9.2
9.9
3.1
4.0
3.7
3.1
0.9
1.0
0.0
2.9
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16 ths)

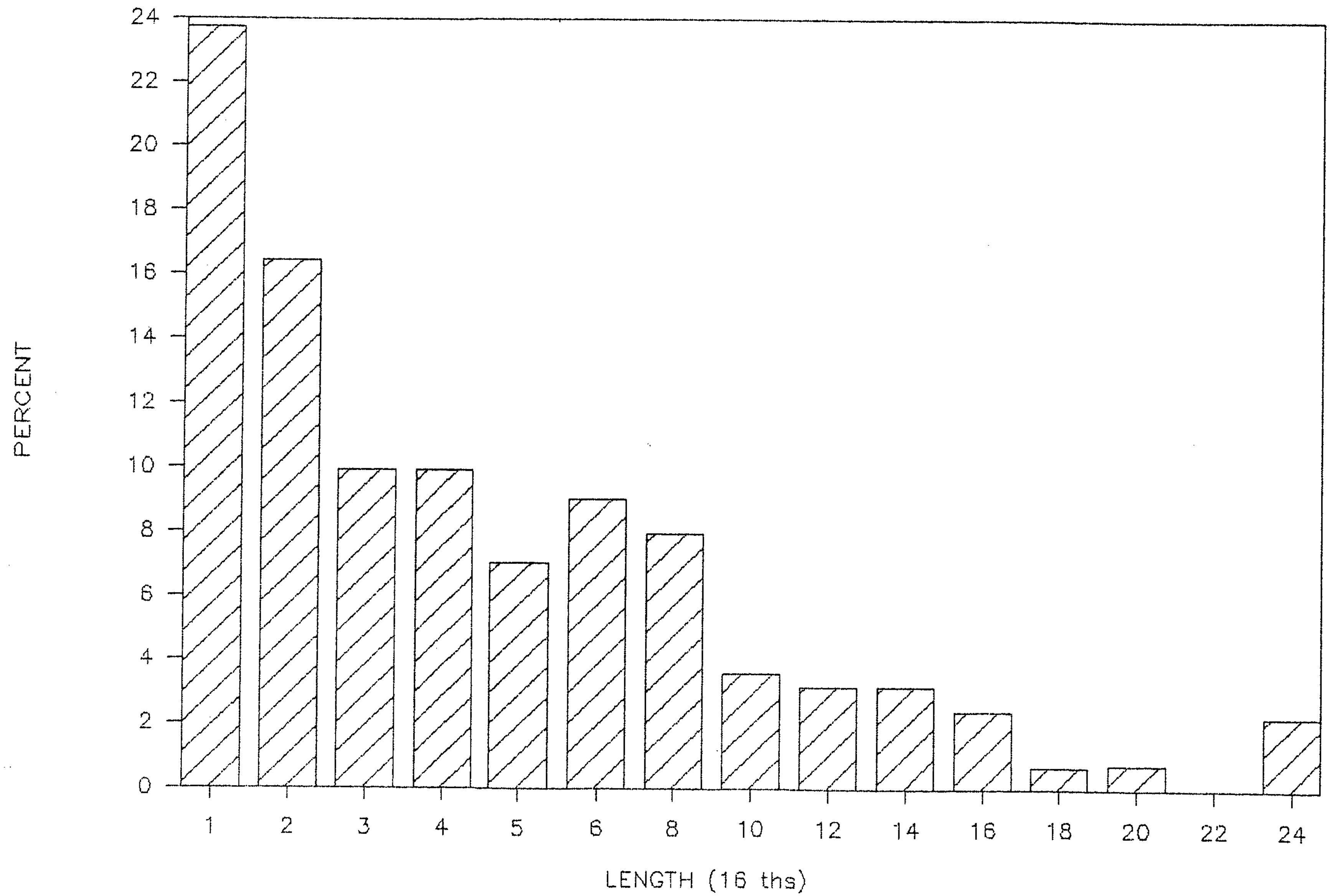
U8615 FIBRE DISTRIBUTION



U8615 LENGTH DISTRIBUTION



U8615 DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME HOLE U86-16 DEPTH 297.18 m

AZIMUTH 91.45° INCLINATION -25.25° SECTION 6828N

LATITUDE 6827.5N DEPARTURE 7627.8E ELEVATION 1568.2 m

STARTED Oct. 26 FINISHED Nov. 10 LOGGED by I.L., D.B.P. date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1.4	15.7		Serpentinite, dark grey, occasional lizardite stringers	
15.7	16.5		Rodingite, whitish green	
16.5	22.8		Serpentinite with innumerable stringers of Rodingite	
22.8	38.6		Rodingite, white	
38.6	57		Dark greenish grey serp., some talcy joints	
57	151.5		Fault zone - fault breccia, gouge, broken	
			Non magnetic serp 61.6 - 67.1	
151.5	197.2		Very dark greyish green, occasional talc stringers and	
			lizardite veinlets, sparse fibre	
			Fault zones 173.4 - 175, 183.8 - 185, 189.6 - 191.7	
197.2	264.6		Very dark grey green to greenish black; talc, lizardite	
			and calcite on joints, sparse fibre, weakly sheared	
			Fault zones 202.7 - 219.5, 263.7 - 264.6 fault breccia	
			211.5 reduced HQ to NQ	
264.6	272.8		Medium dark greyish altered serp.	
			266 - 267 Fault breccia, carbonate cemented	
272.8	274.6		Rodingite, light grey	
274.6	278.3		Argillite, cherty, dark grey	
278.3	278.9		Rodingite	
278.9	279.4		Serpentinite, very dark green	
279.4	280.2		Rodingite	
280.2	297.2		Argillite	
297.2			E.O.H.	

DDH U 8616

EAST: 7525 AZ: 90
NORTH: 6828 INCL: -25
ELEV: 1563 DEPTH: 297

AVERAGE OF TWO COUNTS
Number of fibre veins counted per 16th category

FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.00	1.52	0.34	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
1.52	3.05	1.34	28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
3.05	4.57	1.48	29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
4.57	6.10	1.52	38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
6.10	7.62	1.52	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
7.62	9.14	1.51	30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
9.14	10.67	1.52	32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
10.67	12.19	1.46	29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
12.19	13.72	1.33	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
13.72	15.24	1.43	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
15.24	16.76	1.48	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
16.76	18.29	1.43	25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
18.29	19.81	1.45	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
19.81	21.34	1.49	27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
21.34	22.86	1.37	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
22.86	24.38	1.48	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
24.38	25.91	1.48	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
25.91	27.43	1.51	35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
27.43	28.96	1.52	35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
28.96	30.48	1.45	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
30.48	32.00	1.39	32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
32.00	33.53	1.42	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
33.53	35.05	1.46	35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
35.05	36.58	1.48	28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
36.58	38.10	1.43	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
38.10	39.62	1.37	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
39.62	41.15	1.33	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
41.15	42.67	1.40	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
42.67	44.20	1.36	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
44.20	45.72	1.43	19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
45.72	47.24	1.42	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
47.24	48.77	1.52	29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
48.77	50.29	1.42	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
50.29	51.82	1.39	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
51.82	53.34	1.10	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
53.34	54.86	1.45	22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
54.86	56.39	1.37	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
56.39	57.91	1.23	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
57.91	59.44	1.31	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
59.44	60.96	1.51	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
60.96	62.48	1.39	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
62.48	64.01	1.36	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
64.01	65.53	1.36	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
65.53	67.06	1.45	12	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.39
67.06	68.58	1.49	12	0	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	2	0.30
68.58	70.10	1.30	9	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
70.10	71.63	1.39	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
71.63	73.15	1.31	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

73.15	74.68	1.37	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
74.68	76.20	1.51	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
76.20	77.72	1.19	12	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
77.72	79.25	1.39	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
79.25	80.77	1.40	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
80.77	82.30	1.43	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
82.30	83.82	0.78	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
83.82	85.34	0.67	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.17
85.34	86.87	0.85	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
86.87	88.39	0.84	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
88.39	89.92	1.36	6	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.33
89.92	91.44	0.99	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
91.44	92.96	0.98	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.12
92.96	94.49	1.28	6	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
94.49	96.01	1.30	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
96.01	97.54	1.30	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
97.54	99.06	1.34	8	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.42
99.06	100.58	1.14	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
100.58	102.11	1.25	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
102.11	103.63	1.17	6	3	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.24
103.63	105.16	1.01	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
105.16	106.68	1.13	6	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.60
106.68	108.20	1.01	22	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.33
108.20	109.73	1.20	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
109.73	111.25	1.23	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
111.25	112.78	1.07	6	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.42
112.78	114.30	1.04	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
114.30	115.82	1.01	6	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.45
115.82	117.35	0.93	6	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.85
117.35	118.87	0.52	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
118.87	120.40	0.93	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
120.40	121.92	1.11	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
121.92	123.44	1.26	6	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.44
123.44	124.97	1.14	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
124.97	126.49	1.17	6	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.77
126.49	128.02	0.87	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
128.02	129.54	0.99	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.11
129.54	131.06	1.13	6	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.30
131.06	132.59	0.91	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
132.59	134.11	1.16	6	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.87
134.11	135.64	0.99	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
135.64	137.16	1.04	6	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.65
137.16	138.68	1.25	6	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.27
138.68	140.21	1.08	6	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.83
140.21	141.73	1.19	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
141.73	143.26	1.20	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
143.26	144.78	1.26	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
144.78	146.30	1.22	6	4.5	0	0.5	1	0	0	0	0	0	0	0	0	0	0	0	10	1.84
146.30	147.83	1.28	16	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.44
147.83	149.35	0.98	6	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.58
149.35	150.88	1.16	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
150.88	152.40	1.13	13	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.30
152.40	153.92	1.26	6	4.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.51
153.92	155.45	1.20	18	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.56
155.45	156.97	1.31	19	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	4	0.69
156.97	158.50	1.37	18	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16

158.50	160.02	1.37	17	1.5	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	7.5	1.23
160.02	161.54	1.34	17	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.59
161.54	163.07	1.39	18	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.73
163.07	164.59	1.48	16	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.38
164.59	166.12	1.49	17	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.60
166.12	167.64	1.37	19	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
167.64	169.16	1.23	17	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.45
169.16	170.69	1.30	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
170.69	172.21	1.30	7	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.43
172.21	173.74	1.28	14	2	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.88
173.74	175.26	1.23	5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.45
175.26	176.78	1.31	16	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4	0.69
176.78	178.31	1.16	12	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.48
178.31	179.83	0.91	5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.49
179.83	181.36	1.08	11	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4	0.83
181.36	182.88	1.31	9	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.60
182.88	184.40	1.19	6	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.38
184.40	185.93	1.02	5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.44
185.93	187.45	1.26	14	2	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.89
187.45	188.98	1.36	15	3.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6	0.99
188.98	190.50	1.14	5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.39
190.50	192.02	0.90	5	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.75
192.02	193.55	1.02	13	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.44
193.55	195.07	1.14	11	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.69
195.07	196.60	1.14	11	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.29
196.60	198.12	1.33	17	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
198.12	199.64	1.37	17	4.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.06
199.64	201.17	1.40	11	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
201.17	202.69	1.33	14	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.34
202.69	204.22	0.73	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
204.22	205.74	1.25	5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
205.74	207.26	1.26	5	5.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	11.5	2.04
207.26	208.79	1.02	5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.55
208.79	210.31	0.32	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
210.31	211.84	0.12	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
211.84	213.36	0.09	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
213.36	214.88	0.30	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
214.88	216.41	0.49	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.23
216.41	217.93	0.38	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
217.93	219.46	1.02	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.22
219.46	220.98	1.02	13	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.33
220.98	222.50	0.61	5	1.5	0	0	0	0.5	0	0	0	0	0	0	0	0	0	0	4	1.47
222.50	224.03	0.99	11	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.68
224.03	225.55	1.10	11	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.23
225.55	227.08	1.01	11	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.33
227.08	228.60	0.81	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
228.60	230.12	1.31	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
230.12	231.65	1.34	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
231.65	233.17	1.01	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
233.17	234.70	1.05	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
234.70	236.22	1.33	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
236.22	237.74	1.33	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
237.74	239.27	1.07	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
239.27	240.79	0.96	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
240.79	242.32	1.19	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
242.32	243.84	1.40	24	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.32

243.84	245.36	1.31	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
245.36	246.89	1.34	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
246.89	248.41	1.39	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
248.41	249.94	1.37	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
249.94	251.46	1.01	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
251.46	252.98	1.30	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
252.98	254.51	1.51	19	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.67
254.51	256.03	1.45	18	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.62
256.03	257.56	1.43	16	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
257.56	259.08	1.42	19	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
259.08	260.60	1.46	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
260.60	262.13	1.48	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
262.13	263.65	1.42	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
263.65	265.18	1.36	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
265.18	266.70	1.20	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
266.70	268.22	1.30	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
268.22	269.75	1.40	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
269.75	271.27	1.43	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
271.27	272.80	1.37	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
272.80	274.32	1.43	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
274.32	275.84	1.42	19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
275.84	277.37	1.36	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
277.37	278.89	1.46	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
278.89	280.42	1.48	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
280.42	281.94	1.45	27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
281.94	283.46	1.42	27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
283.46	284.99	1.42	30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
284.99	286.51	1.37	27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
286.51	288.04	0.93	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
288.04	289.56	1.07	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
289.56	291.08	1.10	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
291.08	292.61	1.11	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
292.61	294.13	0.98	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
294.13	295.66	1.25	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
295.66	297.18	1.49	22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

EOH

FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME | HOLE U86-17 | DEPTH 228.3

AZIMUTH 88.13 | INCLINATION -14.27 | SECTION 6706

LATITUDE 6710.191 | DEPARTURE 7713.5 | ELEVATION 1416.1

STARTED Oct. 27 | FINISHED Nov. 3 | LOGGED by REM/DBP date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
2.1	16.8		Serpentinite, very dark grey green, low grade fibre bearing,	
			broken, better fibre below 13 m	
16.8	20.1		Medium green serp.	
20.1	153.9		Medium dark green, fractured, fibre bearing lightens to	
			yellowish green 27 - 56 m and 76 - 96	
153.9	167.6		Dark green, low grade fibre, occasional lizardite	
167.6	228.3		Dark green, gradually becomes darker, occasional lizardite	
			veins and on joints , minor fibre	
			Fault zone 195 - 196.3	
28.3			E.O.H.	

DDH U 8617

EAST: 7714 AZ: 90
NORTH: 6710 INCL: -15
ELEV: 1423 DEPTH: 228

AVERAGE OF TWO COUNTS

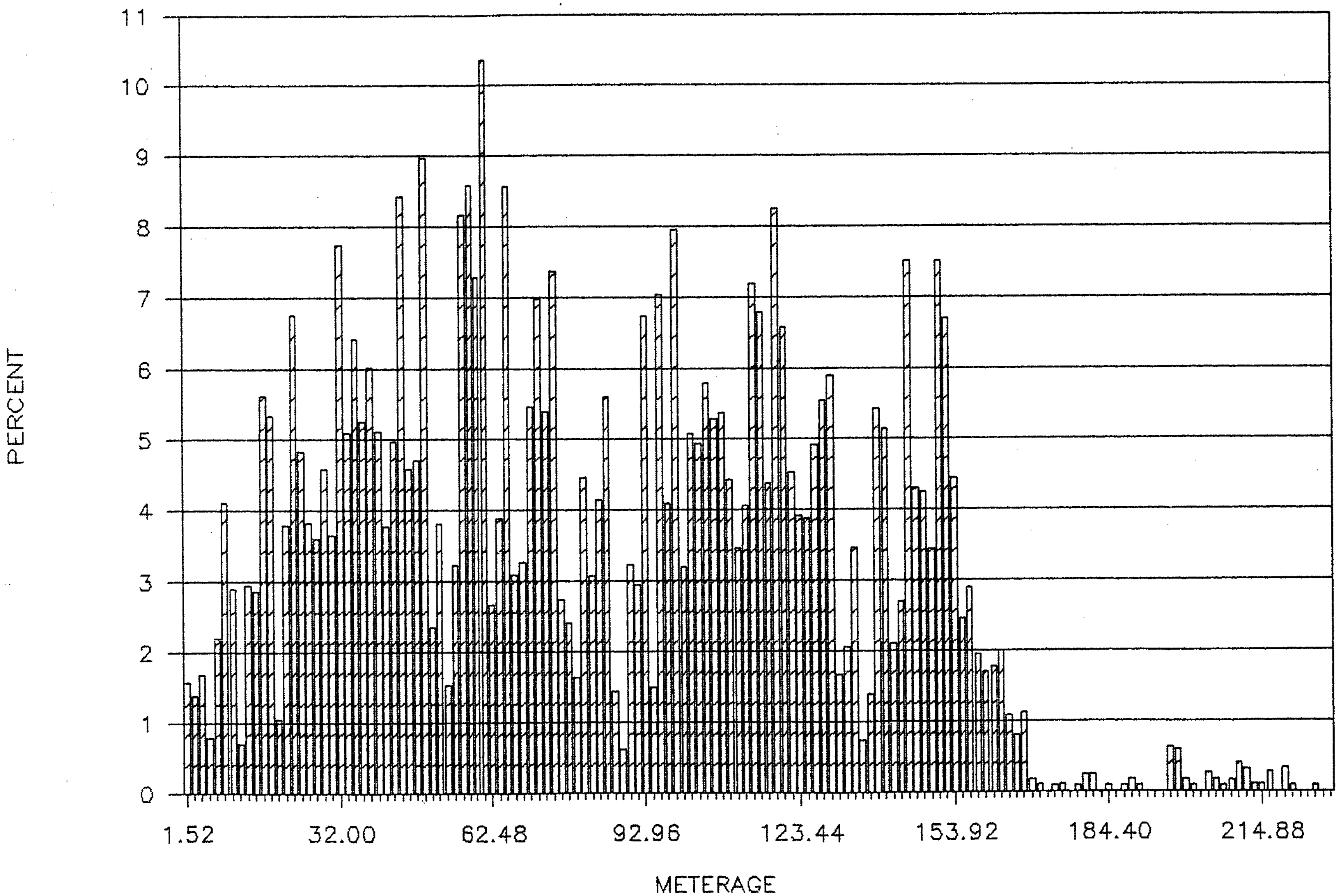
Number of fibre veins counted per 16th category

FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.00	1.52	0.21	25	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	1.58
1.52	3.05	0.98	22	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.38
3.05	4.57	1.34	28	6.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10	1.67
4.57	6.10	1.42	31	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.79
6.10	7.62	1.39	26	7	1	1.5	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.19
7.62	9.14	1.48	26	9	1.5	1.5	0.5	0.5	1	0	0	0	0	0	0	0	0	0	27	4.10
9.14	10.67	1.20	19	7.5	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	15.5	2.89
10.67	12.19	1.13	28	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.70
12.19	13.72	0.99	18	9	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13	2.95
13.72	15.24	1.14	29	7	1	1	0	0.5	0	0	0	0	0	0	0	0	0	0	14.5	2.85
15.24	16.76	1.42	29	14	5	0.5	0	0	1	0.5	0	0	0	0	0	0	0	0	35.5	5.62
16.76	18.29	1.43	23	13	6	2	0	0	0.5	0	0	0	0	0	0	0	0	0	34	5.33
18.29	19.81	1.17	25	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.05
19.81	21.34	1.07	33	2	1.5	1	0.5	0	0.5	0	0.5	0	0	0	0	0	0	0	18	3.79
21.34	22.86	1.31	28	6.5	2	3	0.5	1	0	1	0.5	0	0	0	0	0	0	0	39.5	6.77
22.86	24.38	1.37	20	10	4	2	0	0.5	0.5	0	0	0	0	0	0	0	0	0	29.5	4.83
24.38	25.91	1.49	28	10	3	1	1	0.5	0	0	0	0	0	0	0	0	0	0	25.5	3.83
25.91	27.43	1.37	23	6	2	2	0.5	0	0	0.5	0	0	0	0	0	0	0	0	22	3.60
27.43	28.96	1.33	17	7.5	3.5	0.5	2	0	0.5	0	0	0	0	0	0	0	0	0	27	4.57
28.96	30.48	1.39	22	6.5	5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	22.5	3.64
30.48	32.00	1.48	18	5	4	1	4	2	0.5	0	0	0.5	0	0	0	0	0	0	51	7.74
32.00	33.53	1.43	31	9	4	2.5	2	0	0	0	0	0	0	0	0	0	0	0	32.5	5.09
33.53	35.05	1.43	27	8.5	5	2	0.5	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	41	6.42
35.05	36.58	1.48	30	6.5	3	1.5	0.5	0.5	1.5	0.5	0	0	0	0	0	0	0	0	34.5	5.24
36.58	38.10	1.49	23	6.5	3	4	1	0.5	1.5	0	0	0	0	0	0	0	0	0	40	6.01
38.10	39.62	1.30	26	4.5	3	0	0	0	1	1	0.5	0	0	0	0	0	0	0	29.5	5.11
39.62	41.15	1.31	26	8	1	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	22	3.77
41.15	42.67	1.26	16	8	2	0.5	0	0.5	0	0	0	1	0	0	0	0	0	0	28	4.97
42.67	44.20	1.37	26	6	2	2	2.5	0.5	2.5	1	0	0	0	0	0	0	0	0	51.5	8.43
44.20	45.72	1.49	28	8	1.5	2	0.5	1.5	0	0.5	0	0	0	0	0	0	0	0	30.5	4.58
45.72	47.24	1.43	25	5	1.5	1	0.5	0	1.5	1	0	0	0	0	0	0	0	0	30	4.70
47.24	48.77	1.46	24	5	4	3	1.5	1.5	0.5	2.5	0	0	0	0	0	0	0	0	58.5	8.98
48.77	50.29	1.39	23	6.5	0.5	0	0	0	0.5	0.5	0	0	0	0	0	0	0	0	14.5	2.35
50.29	51.82	1.45	23	6	4	0.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	24.5	3.80
51.82	53.34	1.48	26	5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	10	1.52
53.34	54.86	1.36	14	3.5	1	0	0.5	0	2	0	0	0	0	0	0	0	0	0	19.5	3.23
54.86	56.39	1.40	15	9.5	5.5	3.5	1.5	1	1.5	0	0	0	0	0	0	0	0	0	51	8.17
56.39	57.91	1.46	29	8.5	3.5	2.5	1	3	0.5	0	0.5	0.5	0	0	0	0	0	0	56	8.59
57.91	59.44	1.43	29	1	1.5	0	0.5	1.5	1.5	1	1	0.5	0	0	0	0	0	0	46.5	7.29
59.44	60.96	1.46	32	7.5	4	2	2	1	1.5	0.5	0.5	0	0.5	0.5	0	0	0	0	67.5	10.36
60.96	62.48	1.48	33	4	2	0	1	0.5	0.5	0	0	0	0	0	0	0	0	0	17.5	2.66
62.48	64.01	1.42	32	7.5	3	1	0.5	0	1	0	0	0	0	0	0	0	0	0	24.5	3.88
64.01	65.53	1.48	24	4.5	2.5	0	1	0	1	2	0	0.5	0.5	0.5	0	0	0	0	56.5	8.58
65.53	67.06	1.49	29	2.5	1.5	0.5	1	0.5	0.5	0.5	0	0	0	0	0	0	0	0	20.5	3.08
67.06	68.58	1.48	32	2.5	2	2	1	0	0	0	0.5	0	0	0	0	0	0	0	21.5	3.26
68.58	70.10	1.42	30	0.5	1.5	2	1	0	0.5	1	1	0	0	0	0	0	0	0	34.5	5.46
70.10	71.63	1.52	32	5.5	1	0.5	0.5	0.5	1	0.5	0.5	1	0.5	0	0	0	0	0	47.5	7.00
71.63	73.15	1.48	29	8.5	4	0.5	1	0.5	0.5	1	0	0	0	0	0	0	0	0	35.5	5.39

73.15	74.68	1.40	26	4.5	3.5	1.5	2.5	0	0	2.5	0	0	0	0	0	0	0	0	46	7.37
74.68	76.20	1.31	17	5.5	1	1.5	0	0	0	0.5	0	0	0	0	0	0	0	0	16	2.74
76.20	77.72	1.26	17	7.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.40
77.72	79.25	1.31	17	5.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.63
79.25	80.77	1.51	25	6	2.5	1.5	1.5	0.5	1	0	0	0	0	0	0	0	0	0	30	4.46
80.77	82.30	1.46	25	4.5	3	1	0	0.5	0	0.5	0	0	0	0	0	0	0	0	20	3.07
82.30	83.82	1.33	27	8.5	4.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	24.5	4.15
83.82	85.34	1.40	23	7.5	2	0.5	0	1	0.5	0.5	1	0	0	0	0	0	0	0	35	5.60
85.34	86.87	1.42	17	3.5	0.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	9	1.43
86.87	88.39	1.46	24	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.61
88.39	89.92	1.46	29	6.5	3	0.5	0.5	1	0	0	0	0	0	0	0	0	0	0	21	3.22
89.92	91.44	1.52	36	7.5	2.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	20	2.95
91.44	92.96	1.46	28	6	5	3.5	1	0.5	1	0	0.5	0	0	0	0	0	0	0	44	6.75
92.96	94.49	1.43	22	4	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	9.5	1.49
94.49	96.01	1.37	28	8	4	1.5	2	0.5	2	0	0	0	0	0	0	0	0	0	43	7.04
96.01	97.54	1.40	24	1	2	2	1	0.5	0	1	0	0	0	0	0	0	0	0	25.5	4.08
97.54	99.06	1.33	24	5	1.5	1	2	0	0	3.5	0	0	0	0	0	0	0	0	47	7.96
99.06	100.58	1.37	29	3	2.5	2	0	0.5	0.5	0	0	0	0	0	0	0	0	0	19.5	3.19
100.58	102.11	1.37	22	5	4	1	0.5	0	0	0	0	0.5	0.5	0	0	0	0	0	31	5.07
102.11	103.63	1.34	19	3	3	3	1	0.5	0	0	0.5	0	0	0	0	0	0	0	29.5	4.94
103.63	105.16	1.43	23	7	5	2.5	1	0.5	1	0	0	0	0	0	0	0	0	0	37	5.80
105.16	106.68	1.51	24	4.5	3.5	1	1	1	1	0	0	0.5	0	0	0	0	0	0	35.5	5.28
106.68	108.20	1.52	38	6.5	2	1	1.5	1	1	0	0	0.5	0	0	0	0	0	0	36.5	5.38
108.20	109.73	1.45	27	5.5	2	1	0.5	2	0	0.5	0	0	0	0	0	0	0	0	28.5	4.42
109.73	111.25	1.23	31	5	2.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	19	3.46
111.25	112.78	1.36	24	3.5	3	0.5	2	0.5	0.5	0	0	0	0	0	0	0	0	0	24.5	4.05
112.78	114.30	1.40	22	3	1	2	2	0	0.5	0.5	0.5	0.5	0	0.5	0	0	0	0	45	7.20
114.30	115.82	1.37	23	6	2	0.5	0.5	1	0	1.5	0.5	0.5	0	0	0	0	0	0	41.5	6.79
115.82	117.35	1.39	25	2.5	2.5	0.5	2	0	1	0.5	0	0	0	0	0	0	0	0	27	4.37
117.35	118.87	1.26	25	4	2.5	2	1	0.5	1	1	0.5	0.5	0	0	0	0	0	0	46.5	8.25
118.87	120.40	1.30	22	6	1.5	1	2	1	1.5	0.5	0	0	0	0	0	0	0	0	38	6.59
120.40	121.92	1.39	22	7	3	1	1.5	0	1	0	0	0	0	0	0	0	0	0	28	4.53
121.92	123.44	1.52	22	3.5	3	1	1	1	0	0	0.5	0	0	0	0	0	0	0	26.5	3.90
123.44	124.97	1.22	20	10	2	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	21	3.87
124.97	126.49	1.42	27	7	4	2	2.5	0	0	0	0	0	0	0	0	0	0	0	31	4.91
126.49	128.02	1.42	21	6	6.5	1	0.5	0	0.5	1	0	0	0	0	0	0	0	0	35	5.54
128.02	129.54	1.52	24	5.5	4	2.5	1.5	0	0.5	0	1	0	0	0	0	0	0	0	40	5.89
129.54	131.06	1.49	31	3.5	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	11	1.65
131.06	132.59	1.48	24	6	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.05
132.59	134.11	1.43	32	2.5	2.5	1	1	1.5	0	0	0	0	0	0	0	0	0	0	22	3.45
134.11	135.64	1.52	29	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.74
135.64	137.16	1.46	25	1	1	0	1.5	0	0	0	0	0	0	0	0	0	0	0	9	1.38
137.16	138.68	1.45	20	6	2.5	2	0.5	0	0.5	1	0.5	0	0	0	0	0	0	0	35	5.43
138.68	140.21	1.46	24	7.5	2.5	2	0.5	1	0.5	0	0.5	0	0	0	0	0	0	0	33.5	5.14
140.21	141.73	1.34	21	3	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	2.09
141.73	143.26	1.33	16	7	2	0	0.5	0	0.5	0	0	0	0	0	0	0	0	0	16	2.71
143.26	144.78	1.46	25	6	5	2.5	2	1.5	1	0.5	0	0	0	0	0	0	0	0	49	7.52
144.78	146.30	1.46	27	7	2.5	2.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	28	4.30
146.30	147.83	1.40	28	9	2.5	1	1	0.5	0.5	0	0	0	0	0	0	0	0	0	26.5	4.24
147.83	149.35	1.40	25	7.5	2.5	2	0	0	0.5	0	0	0	0	0	0	0	0	0	21.5	3.44
149.35	150.88	1.46	28	9	3	3	2.5	1	1	0.5	0	0	0	0	0	0	0	0	49	7.52
150.88	152.40	1.52	27	4.5	2	2.5	1	2.5	1.5	0.5	0	0	0	0	0	0	0	0	45.5	6.70
152.40	153.92	1.49	36	11.5	3.5	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	29.5	4.43
153.92	155.45	1.51	32	7	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	16.5	2.46
155.45	156.97	1.51	31	5.5	3	2	0.5	0	0	0	0	0	0	0	0	0	0	0	19.5	2.90
156.97	158.50	1.39	33	7	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	12	1.94

158.50	160.02	1.52	22	5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11.5	1.69
160.02	161.54	1.52	32	7.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	12	1.77
161.54	163.07	1.52	33	7.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13.5	1.99
163.07	164.59	1.46	31	3.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7	1.07
164.59	166.12	1.40	31	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5	0.80
166.12	167.64	1.51	28	4.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.12
167.64	169.16	1.40	13	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
169.16	170.69	1.08	8	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
170.69	172.21	1.30	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
172.21	173.74	1.30	17	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
173.74	175.26	1.22	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
175.26	176.78	1.48	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
176.78	178.31	1.46	32	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
178.31	179.83	1.45	28	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.23
179.83	181.36	1.43	32	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.24
181.36	182.88	1.42	34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
182.88	184.40	1.39	28	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
184.40	185.93	1.26	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
185.93	187.45	1.34	21	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
187.45	188.98	1.28	24	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
188.98	190.50	1.30	20	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
190.50	192.02	1.36	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
192.02	193.55	1.30	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
193.55	195.07	1.10	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
195.07	196.60	1.45	30	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.62
196.60	198.12	1.51	31	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.60
198.12	199.64	1.39	24	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
199.64	201.17	1.48	23	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
201.17	202.69	1.31	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
202.69	204.22	1.37	21	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
204.22	205.74	1.40	18	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
205.74	207.26	1.40	23	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
207.26	208.79	1.45	27	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
208.79	210.31	1.39	28	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
210.31	211.84	1.45	31	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.31
211.84	213.36	1.10	21	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
213.36	214.88	1.17	25	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
214.88	216.41	1.20	29	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.28
216.41	217.93	1.40	25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
217.93	219.46	1.37	27	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.33
219.46	220.98	1.31	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
220.98	222.50	1.30	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
222.50	224.03	1.39	29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
224.03	225.55	1.52	30	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.07
225.55	227.08	1.51	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
227.08	228.30	1.20	28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
	EOH																			

U8617 CCRG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32.00
62.48
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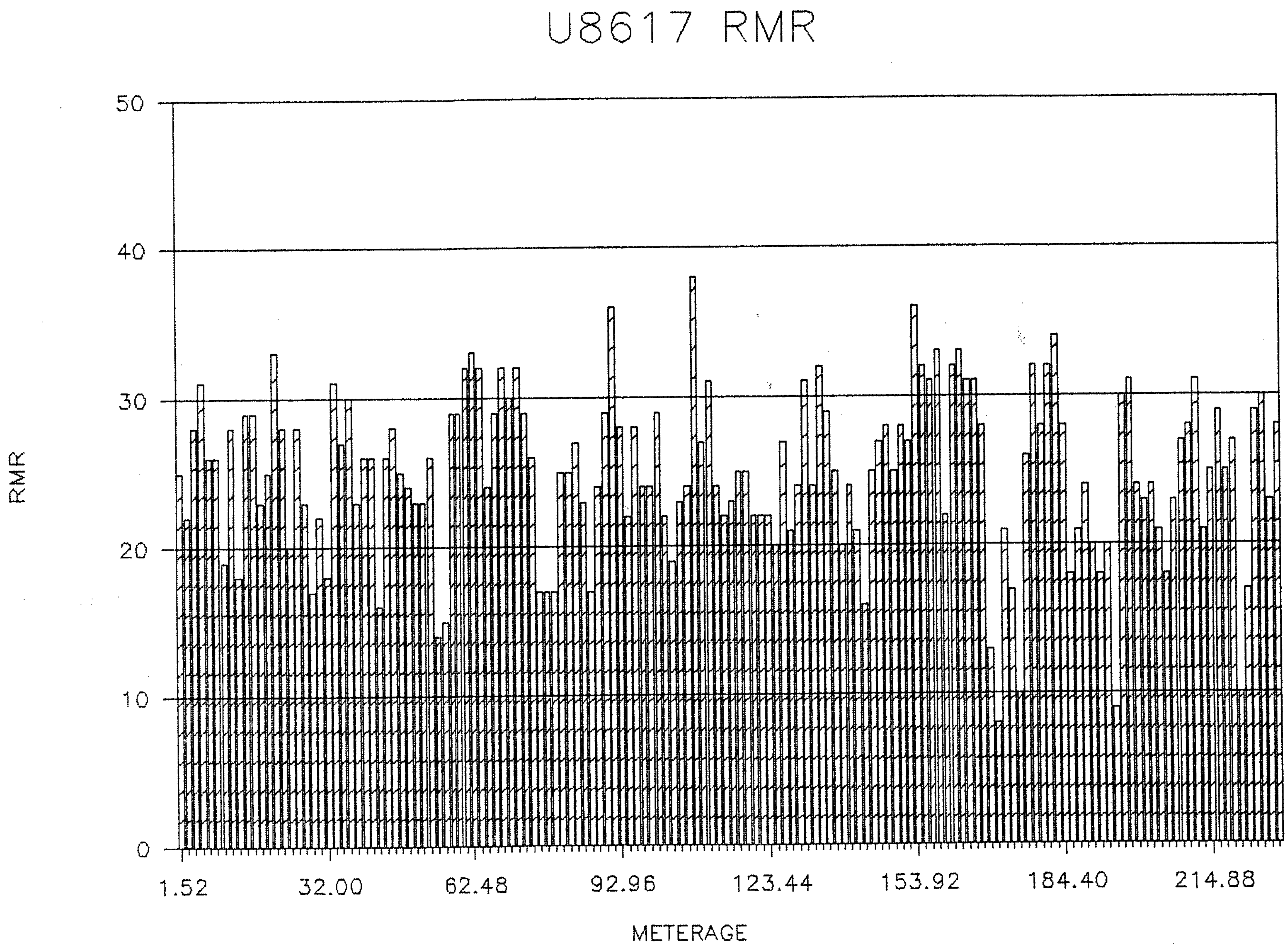
123.44
153.92
184.40
214.88
METERAGE


U8617 RMR
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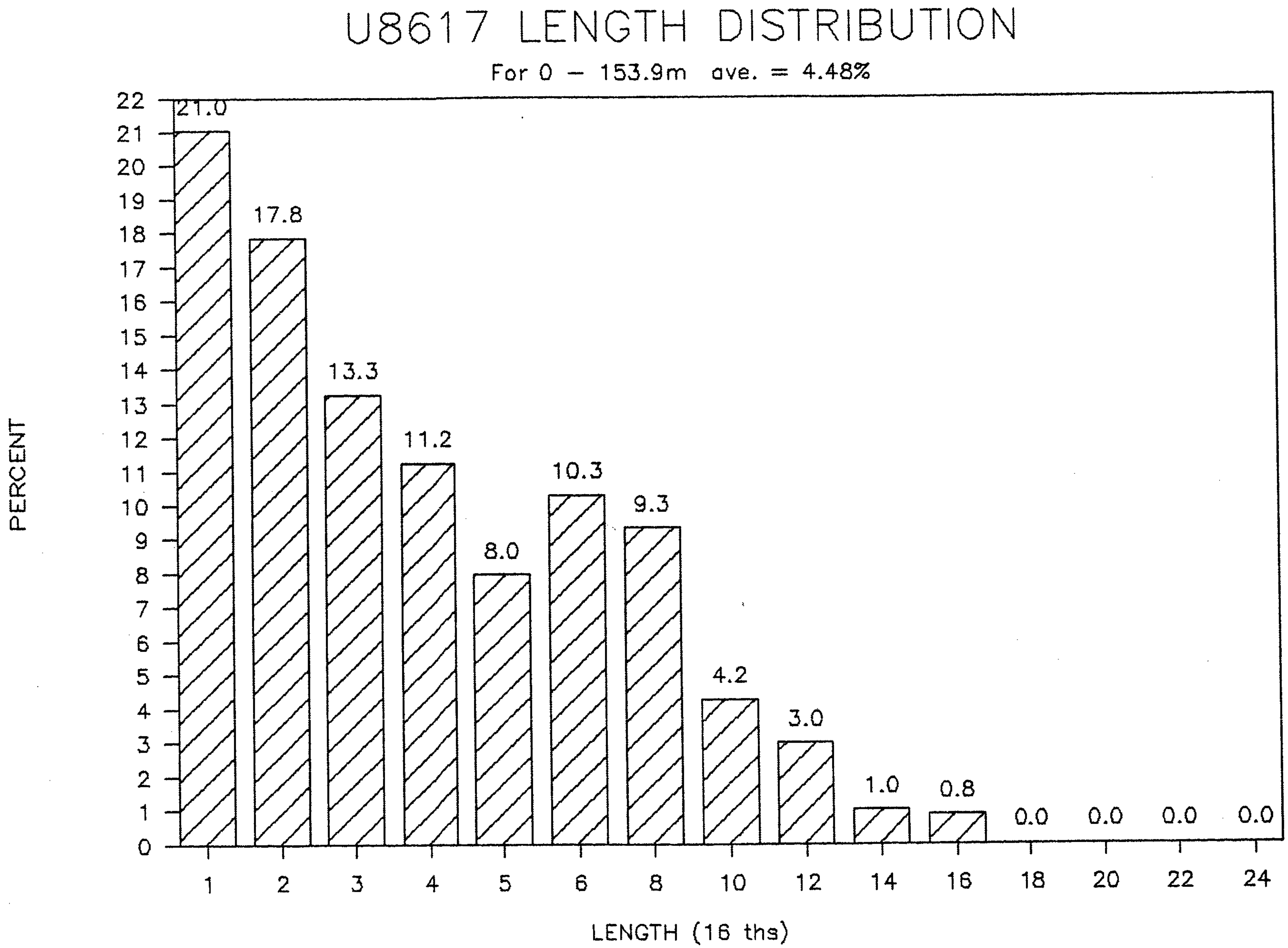
METERAGE


U8617 LENGTH DISTRIBUTION
For 0 - 153.9m ave. = 4.48%
PERCENT
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21
20
19
18
17
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15
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13
12
11
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9
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7
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5
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3
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1
0
21.0
17.8
13.3
11.2
8.0
10.3
9.3
4.2
3.0
1.0
0.8
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0.0
0.0
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1
2
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10
12
14
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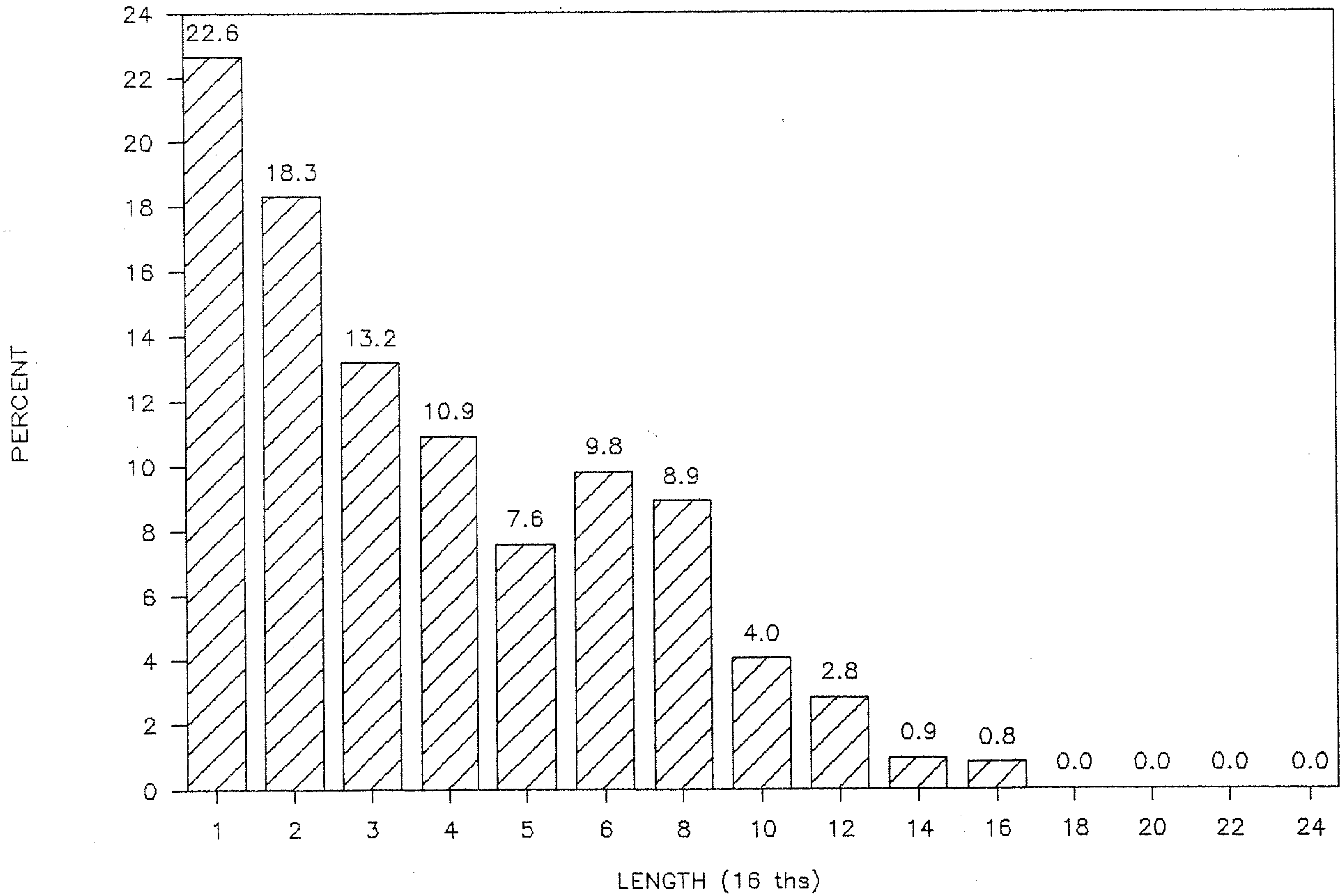
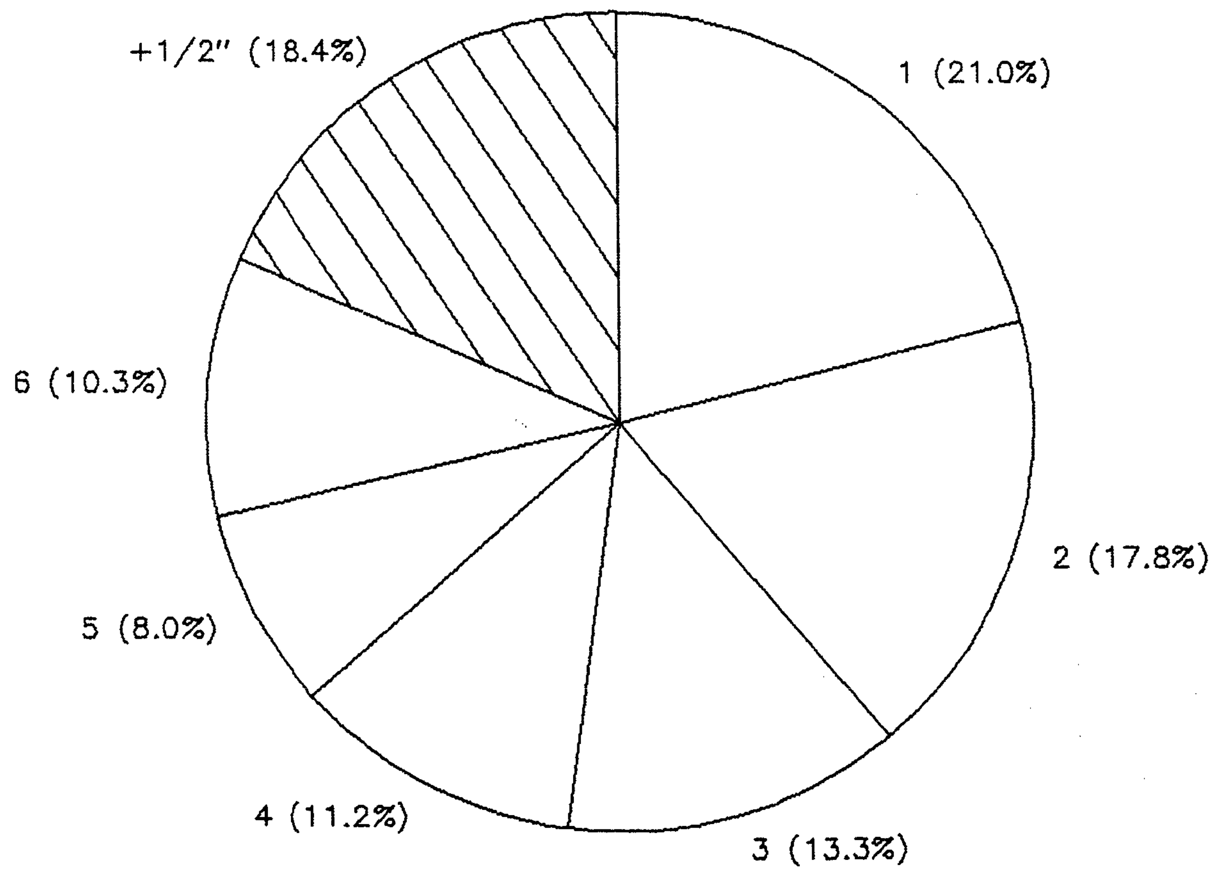
18
20
22
24
LENGTH (16 ths)

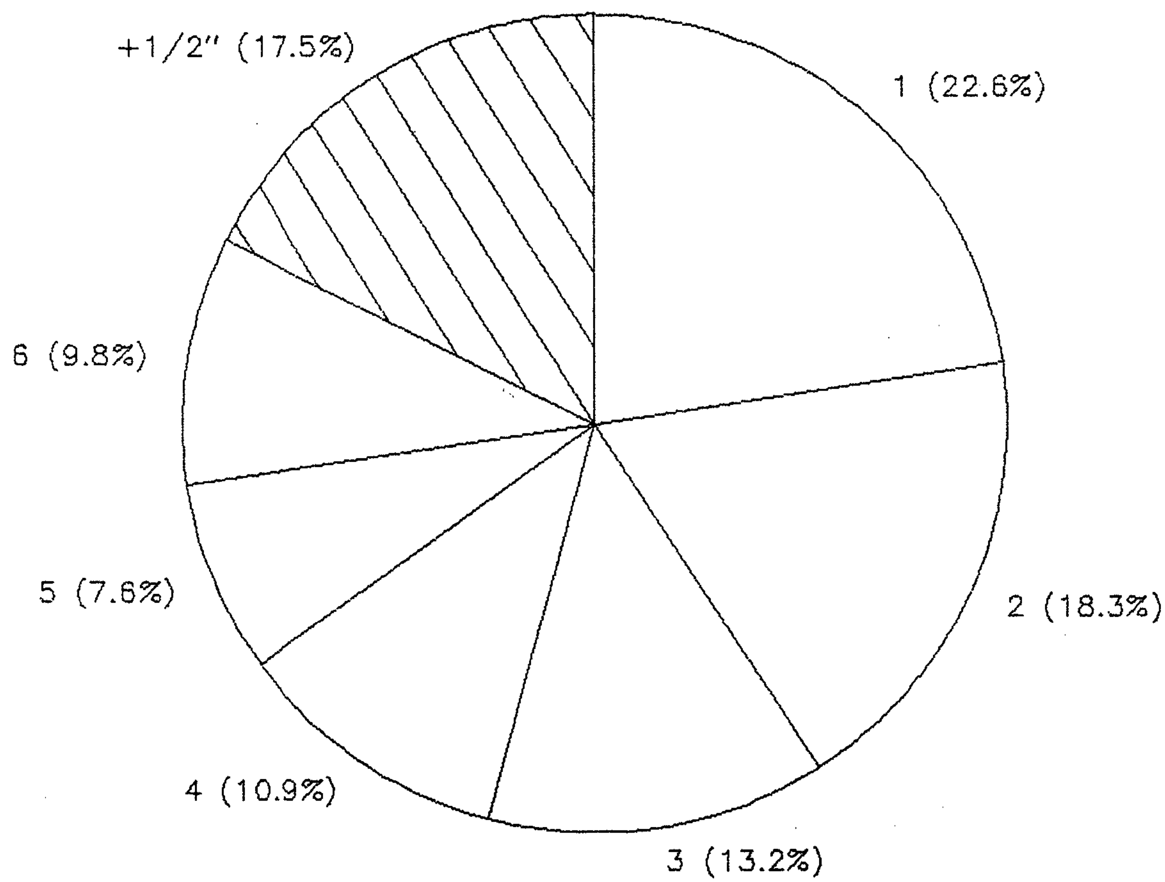
U8617 LENGTH DISTRIBUTION



U8617 LENGTH DISTRIBUTION



U8617 LENGTH DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME	HOLE	U86-18	DEPTH	264.57 m
AZIMUTH	181.76°	INCLINATION	-54°	SECTION	6706N
LATITUDE	6698.50N	DEPARTURE	7710.3E	ELEVATION	1415.2 m
STARTED	Nov. 4	FINISHED	Nov. 12	LOGGED	by DBP, IL date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
(hatched)	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
3	7		Fault zone, gouge and fractured serpentinite	
7	31.3		Medium green serp, fibre bearing, lizardite stringers	
			Fault zone 23.8 - 27, 28.4 - 31.3	
31.3	135		Medium to medium dark green, good fibre	
			Fault zones 37.5 - 59.4, 68.3 - 70.9, 83.5 - 85.5, 129.2 - 130.7	
135	182.3		Becoming greyer green, fibre decreasing,	
			Low below 169, sparse below 177	
182.3	196.3		Fault zone, strongly sheared, compact, no fibre to 194.6,	
			then more broken with fibre	
196.3	212.1		Medium dark green, fibre bearing, broken with minor faults	
			common.	
			Fault zones 200 - 202.4, 204.8 - 205.7	
212.1	237.7		Medium dark green, sparse fibre, joints often coated with	
			magnetite	
			234.7 - 237.7 core getting broken approaching fault zone	
237.7	240.8		Fault zone. Hard compact gouge and fractured, fibre bearing,	
			talcy.	
240.8	264.6		Medium dark green, generally minor fibre	
			Fault zone 260 - 262.6	
264.6			E.O.H.	

DDH U 8618

EAST: 7705 AZ: 180
NORTH: 6700 INCL: -53
ELEV: 1415 DEPTH:264.6

AVERAGE OF TWO COUNTS
Number of fibre veins counted per 16th category

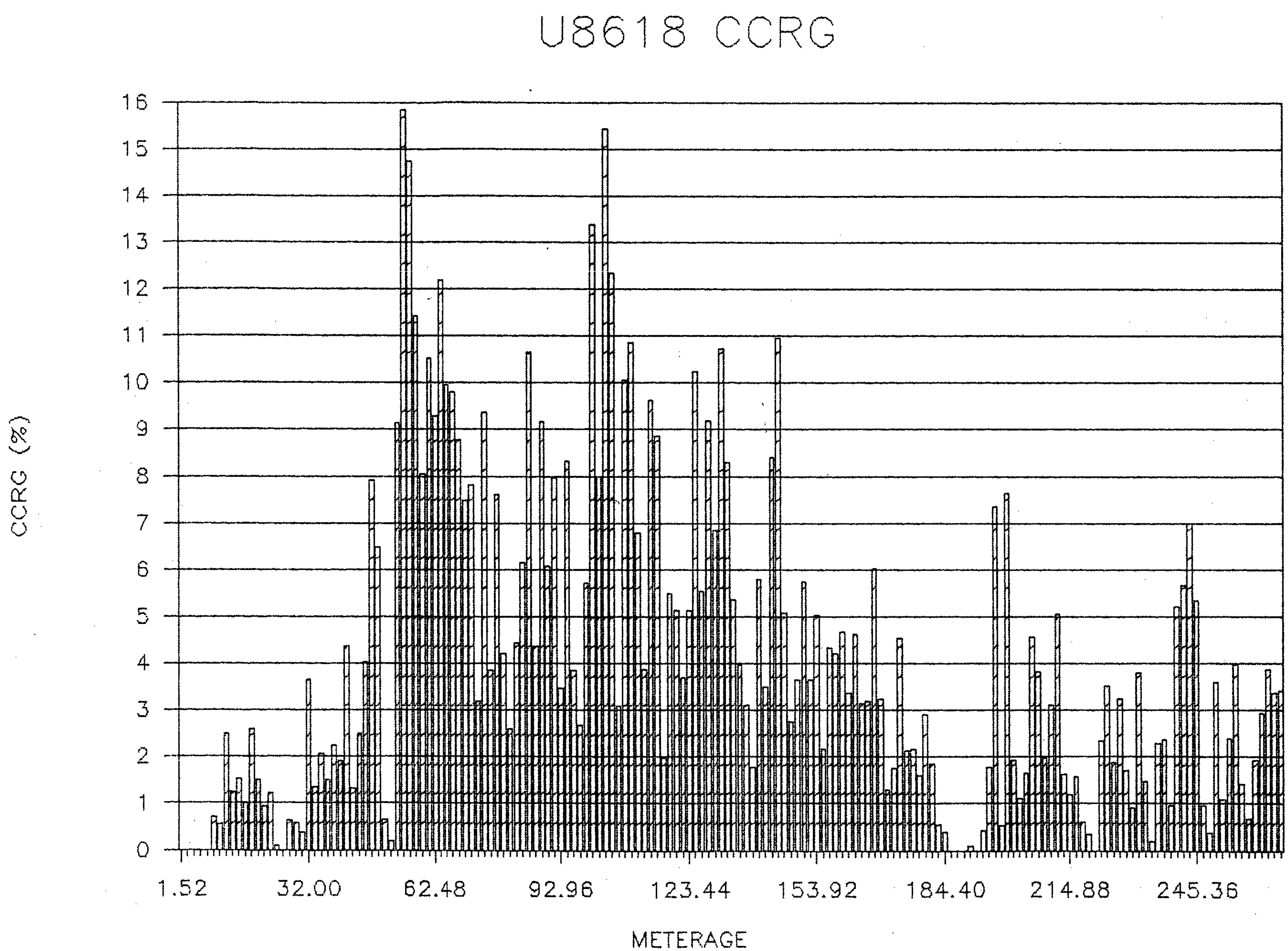
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.00	1.52	0.00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
1.52	3.05	0.00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
3.05	4.57	1.01	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
4.57	6.10	0.78	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
6.10	7.62	1.17	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
7.62	9.14	1.30	16	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.69
9.14	10.67	1.42	16	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.55
10.67	12.19	1.45	18	8.5	1.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	16	2.48
12.19	13.72	1.26	10	2.5	1	0	0	0.5	0	0	0	0	0	0	0	0	0	0	7	1.24
13.72	15.24	1.40	20	7	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.52
15.24	16.76	1.45	22	6.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.01
16.76	18.29	1.39	17	10.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	16	2.59
18.29	19.81	1.20	16	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.49
19.81	21.34	1.33	16	2.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	5.5	0.93
21.34	22.86	1.39	16	2	0.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	7.5	1.21
22.86	24.38	1.19	16	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
24.38	25.91	0.84	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
25.91	27.43	1.07	8	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	3	0.63
27.43	28.96	0.98	8	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.58
28.96	30.48	0.88	6	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.38
30.48	32.00	1.20	10	6.5	2.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	19.5	3.64
32.00	33.53	0.93	14	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.33
33.53	35.05	1.14	8	4	0.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	10.5	2.06
35.05	36.58	1.20	10	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.49
36.58	38.10	1.05	6	6	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	2.24
38.10	39.62	0.82	8	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.91
39.62	41.15	0.90	8	2.5	2	0	0.5	1	0	0.5	0	0	0	0	0	0	0	0	17.5	4.37
41.15	42.67	1.02	6	2.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6	1.32
42.67	44.20	0.90	5	3	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	10	2.50
44.20	45.72	1.14	9	3	1.5	2	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	20.5	4.03
45.72	47.24	1.01	6	2	2.5	1.5	2	1	1	0	0.5	0	0	0	0	0	0	0	35.5	7.92
47.24	48.77	1.01	7	8.5	3	1	0	0.5	1.5	0	0	0	0	0	0	0	0	0	29	6.47
48.77	50.29	1.22	9	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	3.5	0.64
50.29	51.82	1.22	8	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
51.82	53.34	0.94	11	10	2.5	3.5	0	1	0	1	0	0	0	0	0	0	0	0	38.5	9.15
53.34	54.86	1.11	13	9	5.5	2.5	3.5	2	0.5	1.5	0	1	0	0	0	0	0	0	78.5	15.84
54.86	56.39	0.93	14	5	5	3.5	1.5	1.5	1.5	1	0.5	0	0	0	0	0	0	0	61	14.73
56.39	57.91	0.61	3	5	1.5	1	1	1	0.5	1	0	0	0	0	0	0	0	0	31	11.42
57.91	59.44	0.99	8	4.5	0.5	2	0.5	1	1.5	1	0	0	0	0	0	0	0	0	35.5	8.04
59.44	60.96	1.07	8	7	2.5	1	2	1	3	0.5	0	0	0	0	0	0	0	0	50	10.52
60.96	62.48	1.22	14	6.5	5.5	3	1.5	0	0	1	1	0	0	0	0	0	0	0	50.5	9.30
62.48	64.01	1.14	13	6	2	2.5	3	1.5	2.5	0.5	0	0.5	0	0	0	0	0	0	62	12.18
64.01	65.53	1.08	16	9.5	2	2.5	3	1	1	0.5	0	0	0	0	0	0	0	0	48	9.96
65.53	67.06	1.33	16	8	5.5	2	1.5	1	3	0.5	0	0	0	0	0	0	0	0	58	9.82
67.06	68.58	1.26	15	3.5	3	2.5	0	0.5	0	0.5	2	0.5	0	0	0	0	0	0	49.5	8.78
68.58	70.10	1.10	14	10	4.5	2	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	36.5	7.47
70.10	71.63	1.23	14	10	2.5	2.5	1.5	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	43	7.82
71.63	73.15	1.34	21	7.5	1	0.5	1	0	0	0.5	0	0	0	0	0	0	0	0	19	3.18

73.15	74.68	1.34	22	5	1.5	0.5	1	0.5	1	0.5	1	0.5	1	0	0	0	0	0	56	9.37
74.68	76.20	1.28	11	7.5	3	1.5	1	0	0	0	0	0	0	0	0	0	0	0	22	3.86
76.20	77.72	1.36	22	2	1	1	0	0	0	0.5	1	0	0.5	0	1	0	0	0	46	7.61
77.72	79.25	1.31	21	4.5	3	2	0.5	0	1	0	0	0	0	0	0	0	0	0	24.5	4.20
79.25	80.77	1.34	21	4	1	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	15.5	2.59
80.77	82.30	1.19	18	4.5	2.5	2.5	1	0.5	0	0	0	0	0	0	0	0	0	0	23.5	4.44
82.30	83.82	1.01	18	6.5	2.5	1	0.5	0	0.5	1	0	0	0	0	0	0	0	0	27.5	6.14
83.82	85.34	1.16	8	8.5	3	1	1	0.5	1	2	0	0	0	0	0.5	0	0	0	55	10.66
85.34	86.87	1.49	12	10	4	2	0.5	0	0.5	0	0	0	0	0	0	0	0	0	29	4.30
86.87	88.39	1.43	21	5.5	2	2.5	3	0.5	2	0	0	0.5	0	0	0.5	0	0	0	58.5	9.17
88.39	89.92	1.40	28	7.5	4.5	0.5	1.5	1	1.5	0	0	0	0	0	0	0	0	0	38	6.08
89.92	91.44	1.13	18	5	3	2.5	3	0.5	0.5	0.5	0	0	0	0	0	0	0	0	40	7.96
91.44	92.96	1.33	18	8.5	2	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	20.5	3.47
92.96	94.49	1.40	24	11	5	3	1	0	1.5	0.5	0.5	0	0	0	0	0	0	0	52	8.33
94.49	96.01	1.46	11	7.5	1	1.5	0.5	0	0	0.5	0.5	0	0	0	0	0	0	0	25	3.84
96.01	97.54	1.43	13	4	1	0	0.5	0	1.5	0	0	0	0	0	0	0	0	0	17	2.66
97.54	99.06	1.36	11	3.5	0.5	0	0.5	0	0.5	0.5	0.5	0	0	1	0	0	0	0	34.5	5.71
99.06	100.58	1.25	16	10	4	5	0.5	1.5	1.5	1	1.5	0	0	0	0	0	0	0	74.5	13.38
100.58	102.11	1.25	20	2	4	0.5	1.5	0	0.5	0	0	0	0	0	0	0	0	1	44.5	7.99
102.11	103.63	1.10	16	3	3	1	0.5	1.5	1.5	2.5	0	0.5	0.5	0	0	0	0	0.5	75.5	15.45
103.63	105.16	1.17	16	7.5	3.5	2	1	0	1	1	0.5	0	0	0	0	0.5	0.5	0	64.5	12.34
105.16	106.68	1.39	23	4	1.5	1	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	19	3.08
106.68	108.20	1.42	23	7	2	0.5	2.5	1	0	1	1	0	0	0	1	0	0	0	63.5	10.06
108.20	109.73	1.39	22	9	2.5	4	3	0	3	0	0.5	0.5	0	0	0	0	0	0	67	10.85
109.73	111.25	1.36	17	4.5	3	2.5	1	2	1.5	0	0	0	0	0	0	0	0	0	41	6.79
111.25	112.78	1.39	20	4.5	3	1.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	24	3.88
112.78	114.30	1.39	18	8	3	1.5	1	2	1	0.5	0.5	1	0	0	0	0	0	0	59.5	9.63
114.30	115.82	1.36	17	11	4.5	1.5	1.5	0	0.5	0.5	1	0.5	0	0	0	0	0	0	53.5	8.85
115.82	117.35	1.13	16	4	1.5	0	0	0	0.5	0	0	0	0	0	0	0	0	0	10	1.99
117.35	118.87	1.13	20	7	2.5	1	1	0.5	1	0	0	0	0	0	0	0	0	0	27.5	5.47
118.87	120.40	1.40	19	6.5	3	1.5	0	0	0	0	0	0	0.5	0.5	0	0	0	0	32	5.12
120.40	121.92	1.52	18	9	2.5	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	25	3.68
121.92	123.44	1.25	16	6	3	0.5	1	0	0.5	1	0	0	0	0	0	0	0	0	28.5	5.12
123.44	124.97	1.37	20	7	6.5	2.5	0.5	1	1	0.5	1	0	0	0.5	0	0	0	0	62.5	10.23
124.97	126.49	1.52	25	7	2	0.5	2.5	0	0.5	0	0	0	0	0	0	0	0	0.5	37.5	5.52
126.49	128.02	1.36	20	5.5	3.5	1.5	1.5	0.5	1	1	1	0.5	0	0	0	0	0	0	55.5	9.19
128.02	129.54	1.26	9	8.5	2.5	2	1	1	1	0.5	0	0	0	0	0	0	0	0	38.5	6.83
129.54	131.06	1.20	8	7	3.5	2	2	0.5	1.5	1.5	0	0.5	0	0	0	0	0	0	57.5	10.72
131.06	132.59	1.43	19	4	3	2.5	0.5	0.5	0.5	0.5	0.5	1	0.5	0	0	0	0	0	53	8.31
132.59	134.11	1.46	20	2	2	0	0.5	1	1	0	0	0	0	1	0	0	0	0	35	5.37
134.11	135.64	1.39	22	4	1.5	0.5	0	0	2	0.5	0	0	0	0	0	0	0	0	24.5	3.97
135.64	137.16	0.90	20	3.5	1.5	1	0	0	0.5	0	0	0	0	0	0	0	0	0	12.5	3.12
137.16	138.68	1.45	23	2.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	11.5	1.78
138.68	140.21	1.43	22	4.5	0.5	2	0.5	0.5	1	0.5	0.5	0.5	0	0	0	0	0	0	37	5.80
140.21	141.73	1.36	25	8	1.5	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	21	3.48
141.73	143.26	1.42	19	7.5	3	1	1	1.5	1.5	0	0	0	0.5	0	0.5	0	0	0	53	8.39
143.26	144.78	1.22	18	7.5	4.5	1	0.5	1	0.5	1	0	0	0	0	0	0.5	0	0.5	59.5	10.96
144.78	146.30	1.37	19	6.5	4.5	1.5	1.5	1	0	0	0	0	0	0	0	0	0	0	31	5.07
146.30	147.83	1.34	11	4	2	0	1.5	0.5	0	0	0	0	0	0	0	0	0	0	16.5	2.76
147.83	149.35	1.36	18	7	1.5	1.5	0	0.5	0	0	0.5	0	0	0	0	0	0	0	22	3.64
149.35	150.88	1.33	10	5	3.5	1	1	1	1	0.5	0	0	0	0	0	0	0	0	34	5.76
150.88	152.40	1.33	11	4.5	1.5	2.5	1	0.5	0	0	0	0	0	0	0	0	0	0	21.5	3.64
152.40	153.92	1.30	10	6.5	3.5	1.5	2	0	0.5	0	0	0	0	0	0	0	0	0	29	5.03
153.92	155.45	1.40	17	7	1	1.5	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.16
155.45	156.97	1.52	30	6	2.5	1.5	0.5	0	0.5	0.5	0.5	0	0	0	0	0	0	0	29.5	4.35
156.97	158.50	1.46	28	4	1.5	1.5	0.5	1	1.5	0	0	0	0	0	0	0	0	0	27.5	4.22

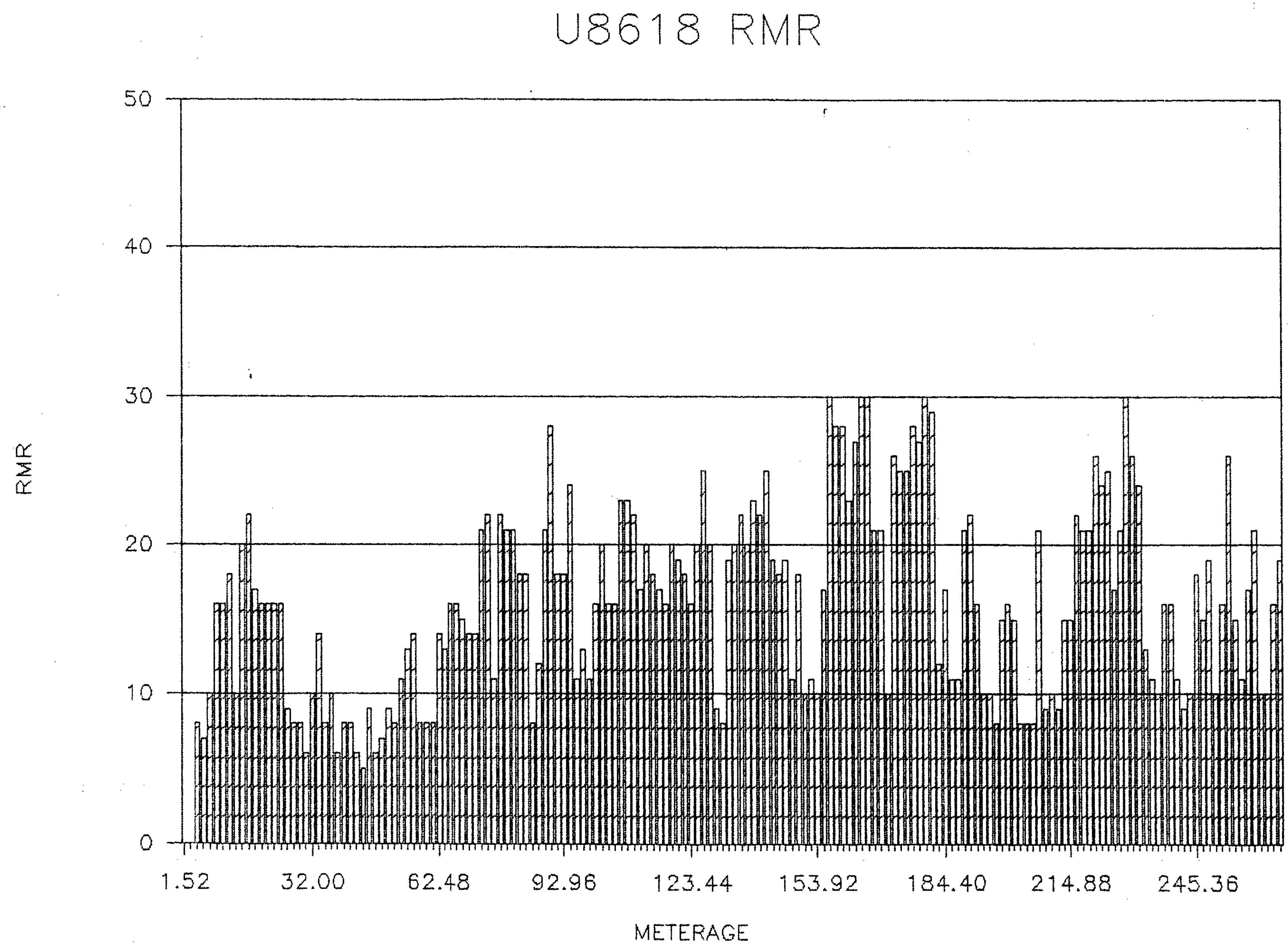
158.50	160.02	1.37	28	9	4	1	1.5	0.5	0	0	0	0	0	0	0	0	0	0	28.5	4.66
160.02	161.54	1.40	23	10	2	0	0.5	1	0	0	0	0	0	0	0	0	0	0	21	3.36
161.54	163.07	1.51	27	2.5	1	0.5	1	0	0.5	0	0	0	0	0.5	0	0.5	0	0	31	4.61
163.07	164.59	1.51	30	5	4	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	21	3.12
164.59	166.12	1.48	30	12	3	1	0	0	0	0	0	0	0	0	0	0	0	0	21	3.19
166.12	167.64	1.34	21	7	2	1.5	1.5	0.5	0	0	0	1	0	0	0	0	0	0	36	6.03
167.64	169.16	1.36	21	7	2.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	19.5	3.23
169.16	170.69	1.31	10	3.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.28
170.69	172.21	1.34	26	5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.76
172.21	173.74	1.39	25	7.5	3	2	1.5	0.5	0	0	0	0	0	0	0	0	0	0	28	4.53
173.74	175.26	1.46	25	8	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	14	2.15
175.26	176.78	1.51	28	8	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	14.5	2.16
176.78	178.31	1.46	27	3.5	1	1	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	1.61
178.31	179.83	1.46	30	9.5	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	19	2.92
179.83	181.36	1.45	29	4.5	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	12	1.86
181.36	182.88	1.42	12	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.55
182.88	184.40	1.39	17	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
184.40	185.93	1.39	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
185.93	187.45	1.42	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
187.45	188.98	1.42	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
188.98	190.50	1.46	22	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
190.50	192.02	1.42	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
192.02	193.55	1.04	10	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.43
193.55	195.07	1.14	10	1	1	2	0	0	0	0	0	0	0	0	0	0	0	0	9	1.77
195.07	196.60	1.02	8	11.5	3.5	1	1	1	0.5	0	0	0	0	0	0	0	0	0	33.5	7.37
196.60	198.12	1.26	15	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.53
198.12	199.64	1.25	16	9	4.5	2	0.5	1.5	1.5	0	0	0	0	0	0	0	0	0	42.5	7.63
199.64	201.17	1.16	15	5.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10	1.94
201.17	202.69	1.20	8	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.12
202.69	204.22	1.30	8	6.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.65
204.22	205.74	1.20	8	6.5	4	1	0.5	1	0	0	0	0	0	0	0	0	0	0	24.5	4.57
205.74	207.26	1.33	21	7	2	1	1.5	0.5	0	0	0	0	0	0	0	0	0	0	22.5	3.81
207.26	208.79	1.25	9	9	1	0	0	0	0	0	0	0	0	0	0	0	0	0	11	1.98
208.79	210.31	1.16	10	6.5	2	0.5	1	0	0	0	0	0	0	0	0	0	0	0	16	3.10
210.31	211.84	1.22	9	7.5	3	0	1	2	0	0	0	0	0	0	0	0	0	0	27.5	5.06
211.84	213.36	1.10	15	5.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8	1.64
213.36	214.88	1.13	15	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.19
214.88	216.41	1.22	22	5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.57
216.41	217.93	1.33	21	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.59
217.93	219.46	1.26	21	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.35
219.46	220.98	1.40	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
220.98	222.50	1.43	24	3.5	0.5	1	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	15	2.35
222.50	224.03	1.31	25	10	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	20.5	3.51
224.03	225.55	1.31	17	5	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	11	1.88
225.55	227.08	1.52	21	7	2.5	0	0.5	0	0	1	0	0	0	0	0	0	0	0	22	3.24
227.08	228.60	1.46	30	3.5	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	11	1.69
228.60	230.12	1.37	26	1.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	5.5	0.90
230.12	231.65	1.42	24	4	1.5	1.5	0	0.5	1	0.5	0	0	0	0	0	0	0	0	24	3.80
231.65	233.17	1.37	13	4	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.47
233.17	234.70	1.26	11	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
234.70	236.22	1.28	10	4	2.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	13	2.28
236.22	237.74	1.37	16	8	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	14.5	2.37
237.74	239.27	1.28	16	5.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.96
239.27	240.79	1.19	11	5.5	3	1	0.5	1	1	0	0	0	0	0	0	0	0	0	27.5	5.19
240.79	242.32	1.33	9	6.5	3.5	0.5	1	0.5	2	0	0	0	0	0	0	0	0	0	33.5	5.67
242.32	243.84	1.20	10	4.5	5	1	0	0	1	0.5	1	0	0	0	0	0	0	0	37.5	6.99

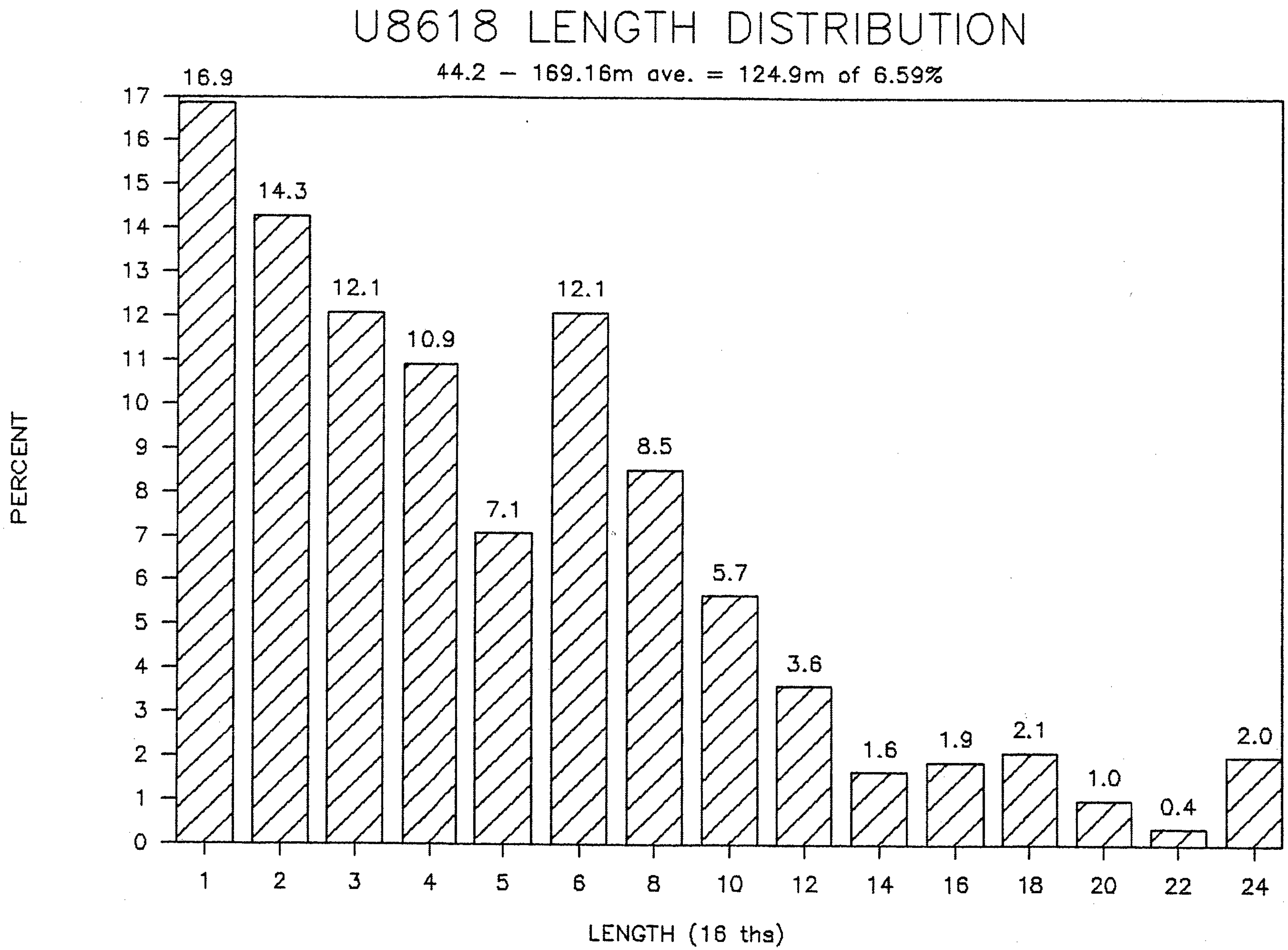
243.84	245.36	1.39	18	5.5	2.5	0.5	1	0	1	0.5	0	0	0.5	0	0	0	0	0	33	5.34
245.36	246.89	1.42	15	3.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6	0.95
246.89	248.41	1.48	19	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.38
248.41	249.94	1.40	10	6	2	0.5	1.5	1	0	0	0	0	0	0	0	0	0	0	22.5	3.60
249.94	251.46	1.25	16	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.08
251.46	252.98	1.46	26	9	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	15.5	2.38
252.98	254.51	1.30	15	6	2.5	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	23	3.99
254.51	256.03	1.34	11	5.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.42
256.03	257.56	1.33	17	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.68
257.56	259.08	1.40	21	3.5	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	12	1.92
259.08	260.60	1.26	10	6.5	3.5	0	0	0	0.5	0	0	0	0	0	0	0	0	0	16.5	2.93
260.60	262.13	1.13	10	5.5	2	1	1	0	0.5	0	0	0	0	0	0	0	0	0	19.5	3.88
262.13	263.65	1.40	16	8	1.5	1	0	0	0.5	0.5	0	0	0	0	0	0	0	0	21	3.36
263.65	264.57	0.82	19	7	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	3.41

E.O.H.

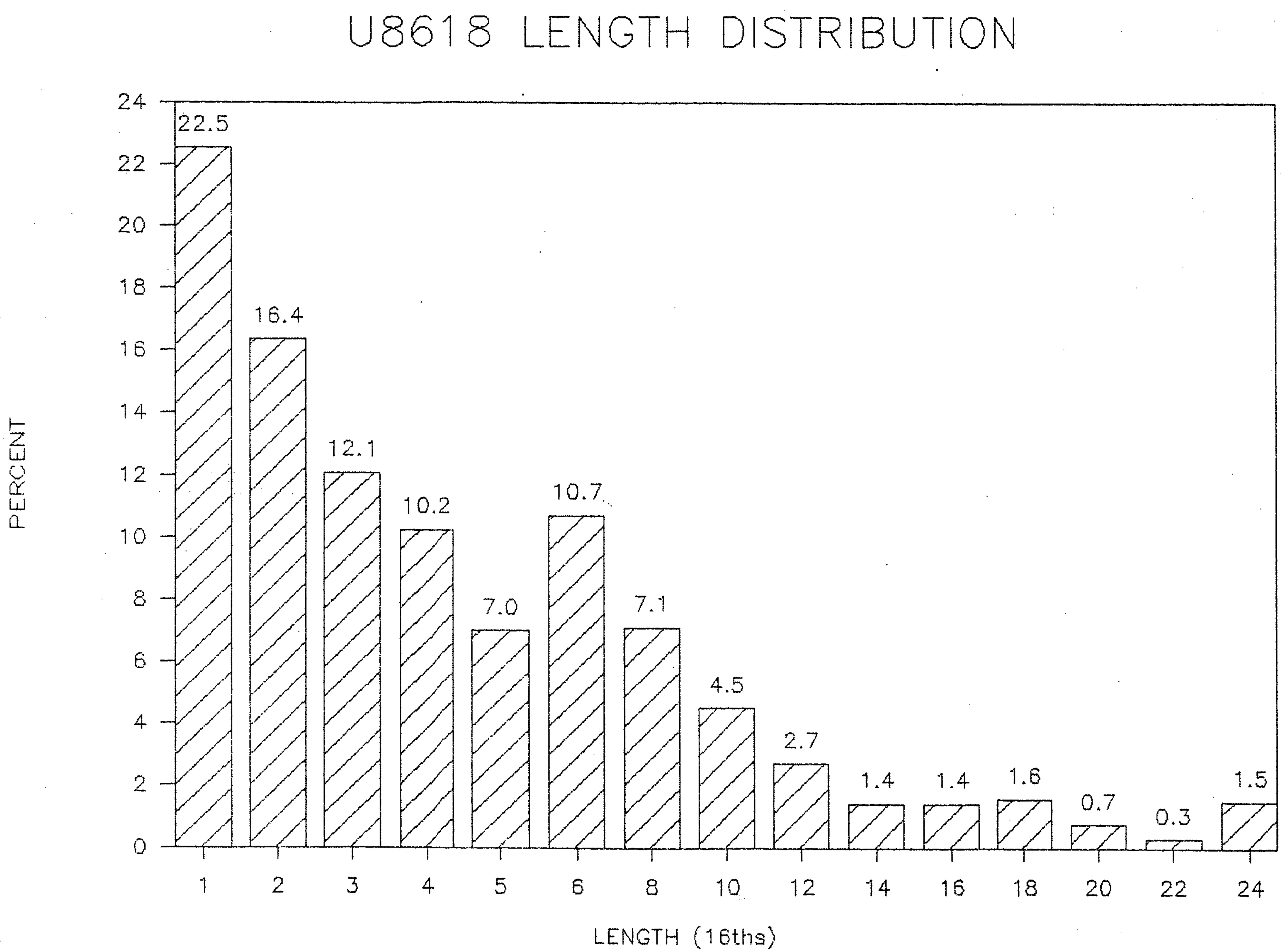


U8618 CCRG
CCRG (%)
16
15
14
13
12
11
10
9
8
7
6
5
4
3
2
1
0
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
245.36
METERAGE

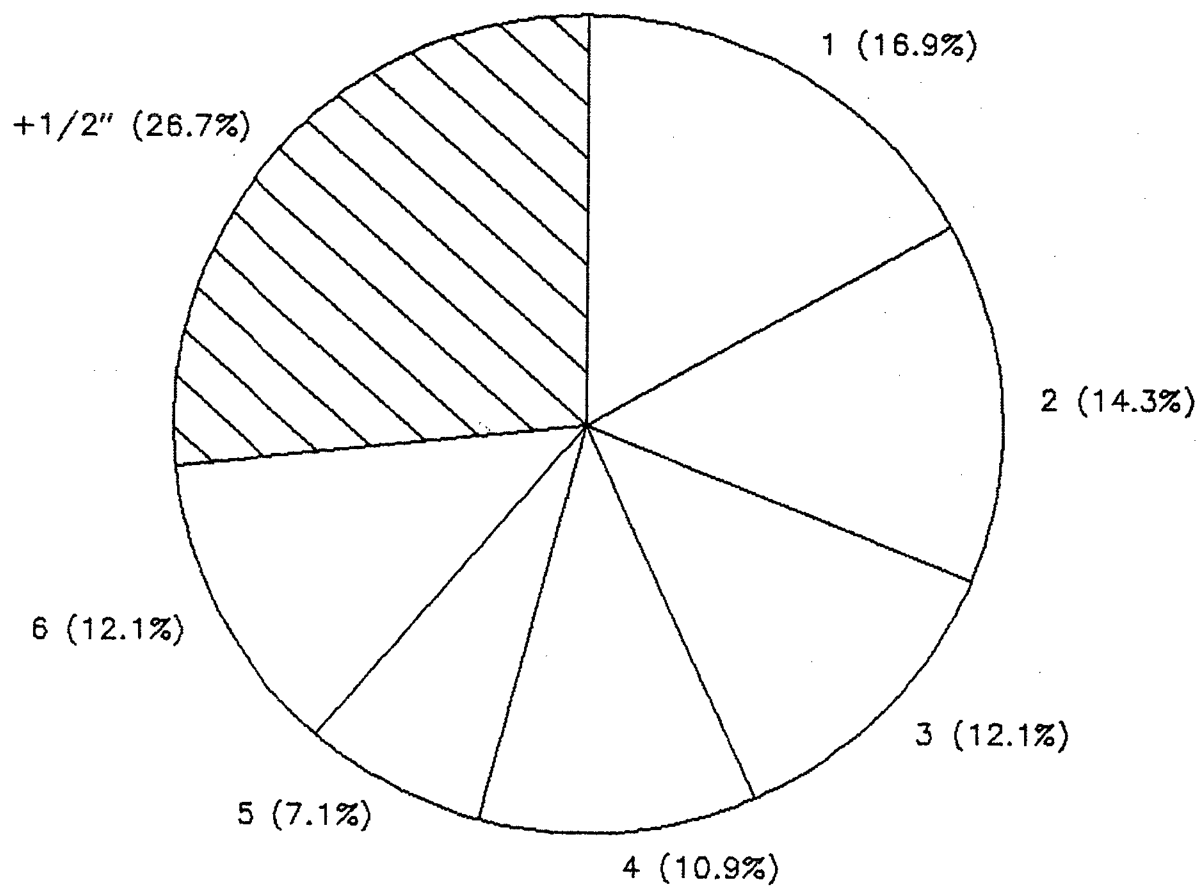

U8618 RMR
50
40
30
20
10
0
RMR
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
245.36
METERAGE



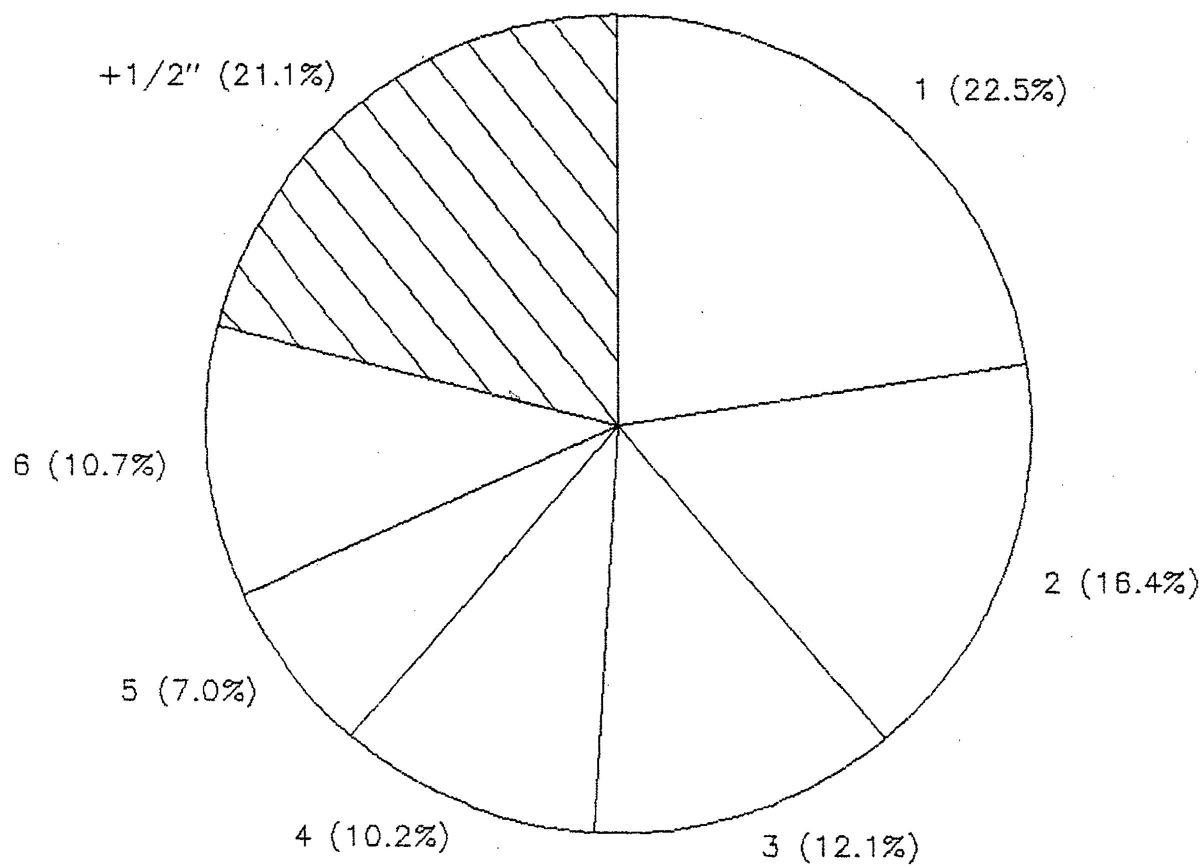
U8618 LENGTH DISTRIBUTION
44.2 – 169.16m ave. = 124.9m of 6.59%
PERCENT
LENGTH (16 ths)
0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
16.9
14.3
12.1
10.9
7.1
12.1
8.5
5.7
3.6
1.6
1.9
2.1
1.0
0.4
2.0


U8618 LENGTH DISTRIBUTION
PERCENT
24
22
20
18
16
14
12
10
8
6
4
2
0
22.5
16.4
12.1
10.2
7.0
10.7
7.1
4.5
2.7
1.4
1.4
1.6
0.7
0.3
1.5
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16ths)

U8618 LENGTH DISTRIBUTION



U8618 LENGTH DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME
HOLE	U86-19
DEPTH	77.42
AZIMUTH	89.5°
INCLINATION	$+ 30^{\circ}$
SECTION	6767
LATITUDE	6765.86N
DEPARTURE	7702.9E
ELEVATION	1420.1 m
STARTED	Nov. 15
FINISHED	Nov. 19
LOGGED by	DBP
date	

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
(hatched)	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
.9	4.5		Serpentinite, greyish green, minor fibre, lizardite stringers	
4.5	10.7		Fault zone, gouge and extremely broken, no fibre	
10.7	25.6		Greyish green, minor fibre, lizardite stringers	
			22.8 - 24.4 fault zone broken and gouge	
25.6	44.8		Medium green, fibre bearing	
44.8	56.1		Medium green, low to minor fibre	
			Fault zone 44.8 - 46.3	
56.1	77.4		Very dark green serpentinite, sparse fibre, lizardite	
			stringers common	
77.4			E.O.H.	

DDH U 8619

EAST:7703.2 AZ:89.05
NORTH:6765.8 INCL:+31,40'
ELEV:1421.3 DEPTH:77.42m

AVERAGE OF TWO COUNTS

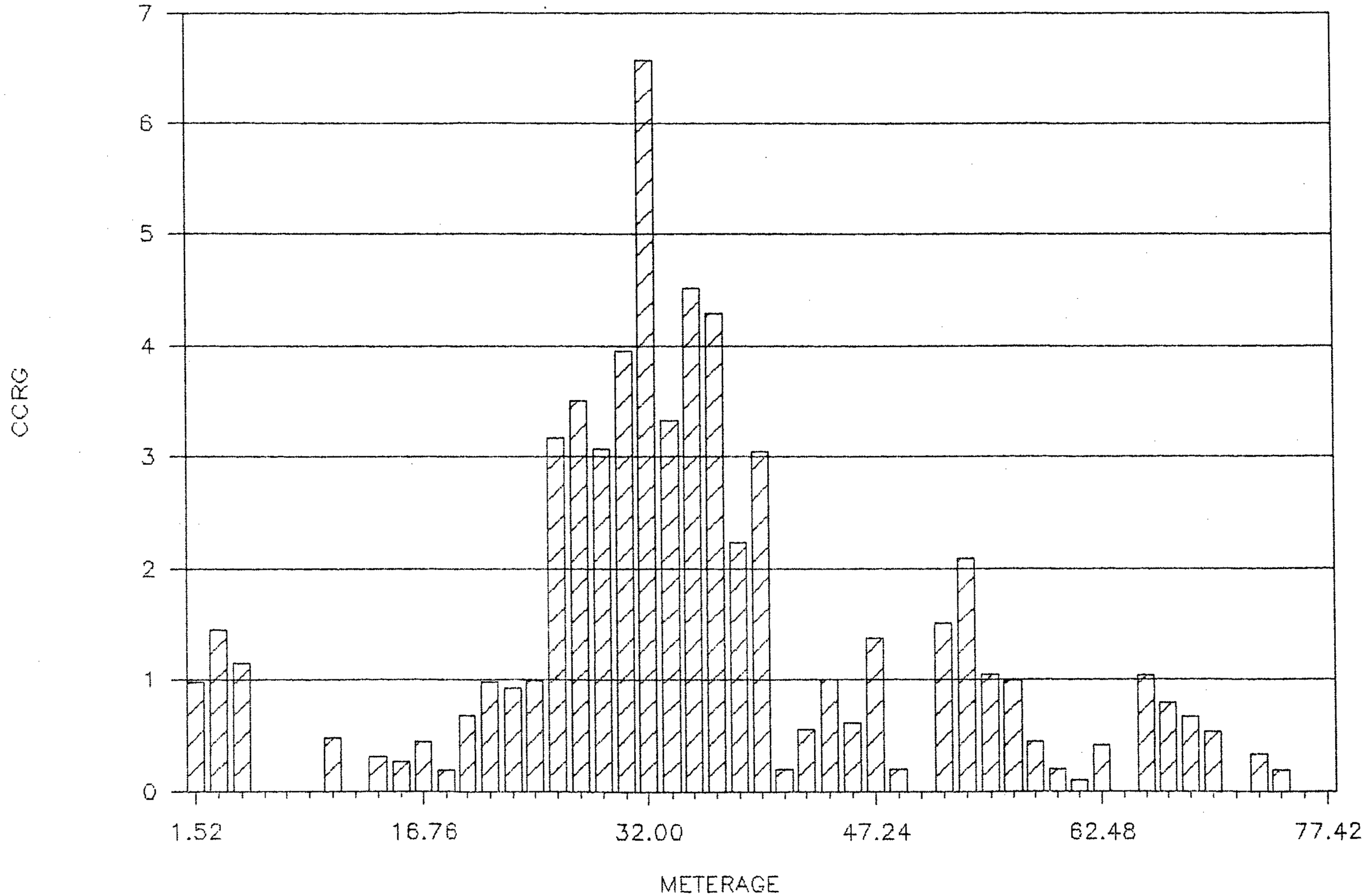
Number of fibre veins counted per 16th category

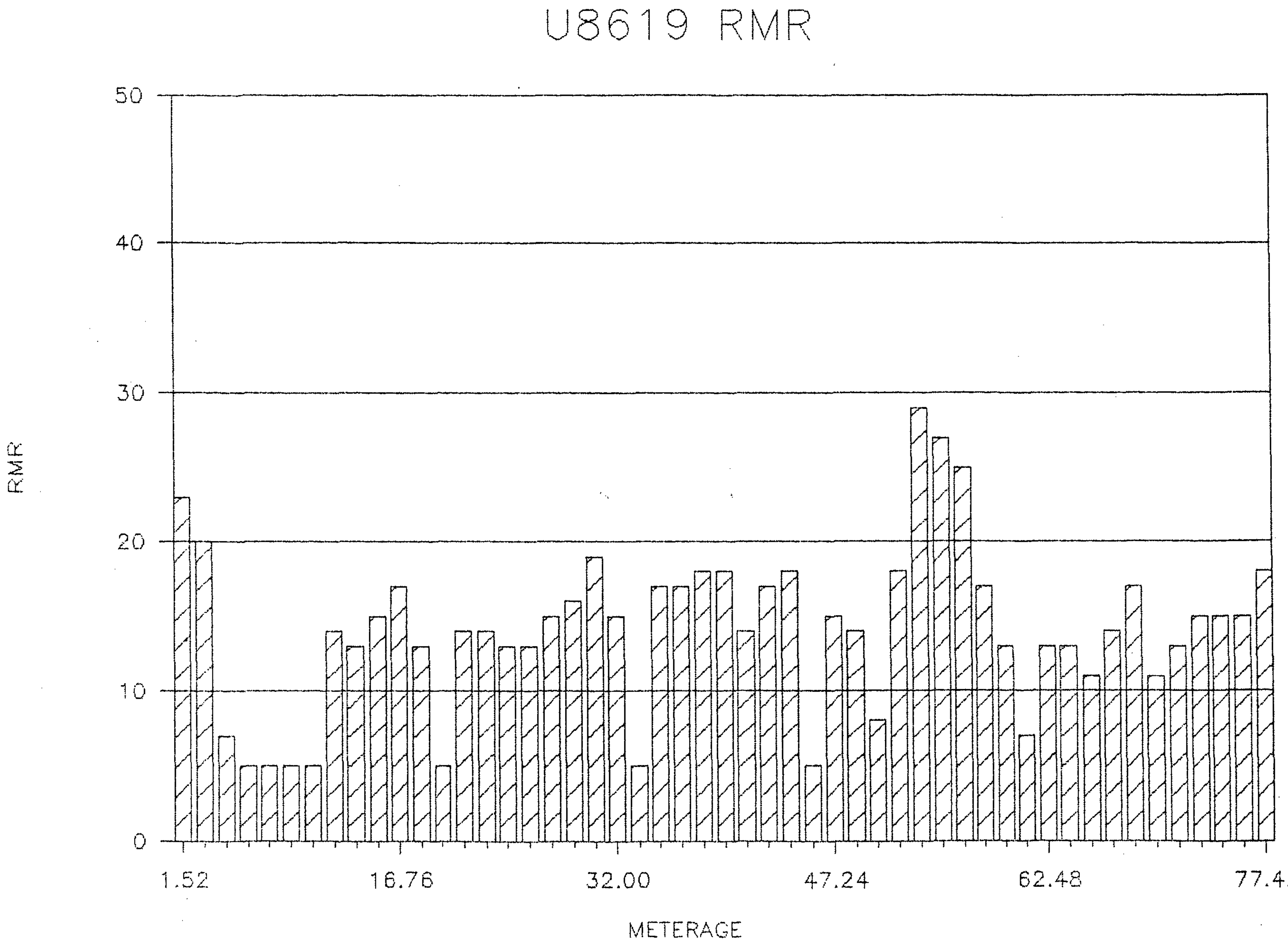
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.00	1.52	0.91	23	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.98
1.52	3.05	1.08	20	4.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7	1.45
3.05	4.57	1.17	7	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.15
4.57	6.10	0.93	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
6.10	7.62	0.81	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
7.62	9.14	0.64	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
9.14	10.67	0.70	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.48
10.67	12.19	0.69	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
12.19	13.72	1.11	13	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.30
13.72	15.24	1.26	15	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.27
15.24	16.76	1.26	17	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.44
16.76	18.29	1.23	13	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
18.29	19.81	1.16	5	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	3.5	0.68
19.81	21.34	1.26	14	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.98
21.34	22.86	1.22	14	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.92
22.86	24.38	1.25	13	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.99
24.38	25.91	1.20	13	6	1	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	17	3.17
25.91	27.43	1.25	15	7	2	2	0	0.5	0	0	0	0	0	0	0	0	0	0	19.5	3.50
27.43	28.96	1.20	16	5	1.5	1	0	0.5	0.5	0	0	0	0	0	0	0	0	0	16.5	3.08
28.96	30.48	1.45	19	10.5	3	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	25.5	3.95
30.48	32.00	1.26	15	6	3.5	1	0	1	0.5	1	0.5	0	0	0	0	0	0	0	37	6.57
32.00	33.53	0.94	5	2.5	2	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	14	3.33
33.53	35.05	1.22	17	6.5	2.5	1	0.5	1	0.5	0	0	0	0	0	0	0	0	0	24.5	4.51
35.05	36.58	1.28	17	2.5	1.5	3	1	0	1	0	0	0	0	0	0	0	0	0	24.5	4.30
36.58	38.10	1.36	18	6	1.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	13.5	2.23
38.10	39.62	1.33	18	13	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	18	3.05
39.62	41.15	1.11	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
41.15	42.67	1.40	17	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.56
42.67	44.20	1.46	18	4.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.00
44.20	45.72	1.11	5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.61
45.72	47.24	1.31	15	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.37
47.24	48.77	1.11	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
48.77	50.29	1.16	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
50.29	51.82	1.42	18	9.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.50
51.82	53.34	1.51	29	4.5	0.5	0.5	1	0	0.5	0	0	0	0	0	0	0	0	0	14	2.08
53.34	54.86	1.51	27	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.04
54.86	56.39	1.36	25	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.99
56.39	57.91	1.26	17	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.44
57.91	59.44	1.14	13	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
59.44	60.96	1.20	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
60.96	62.48	1.11	13	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.40
62.48	64.01	0.93	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
64.01	65.53	0.98	11	1	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4.5	1.04
65.53	67.06	1.14	14	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.79
67.06	68.58	1.36	17	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.66
68.58	70.10	1.07	11	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.53
70.10	71.63	1.28	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
71.63	73.15	1.37	15	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.33

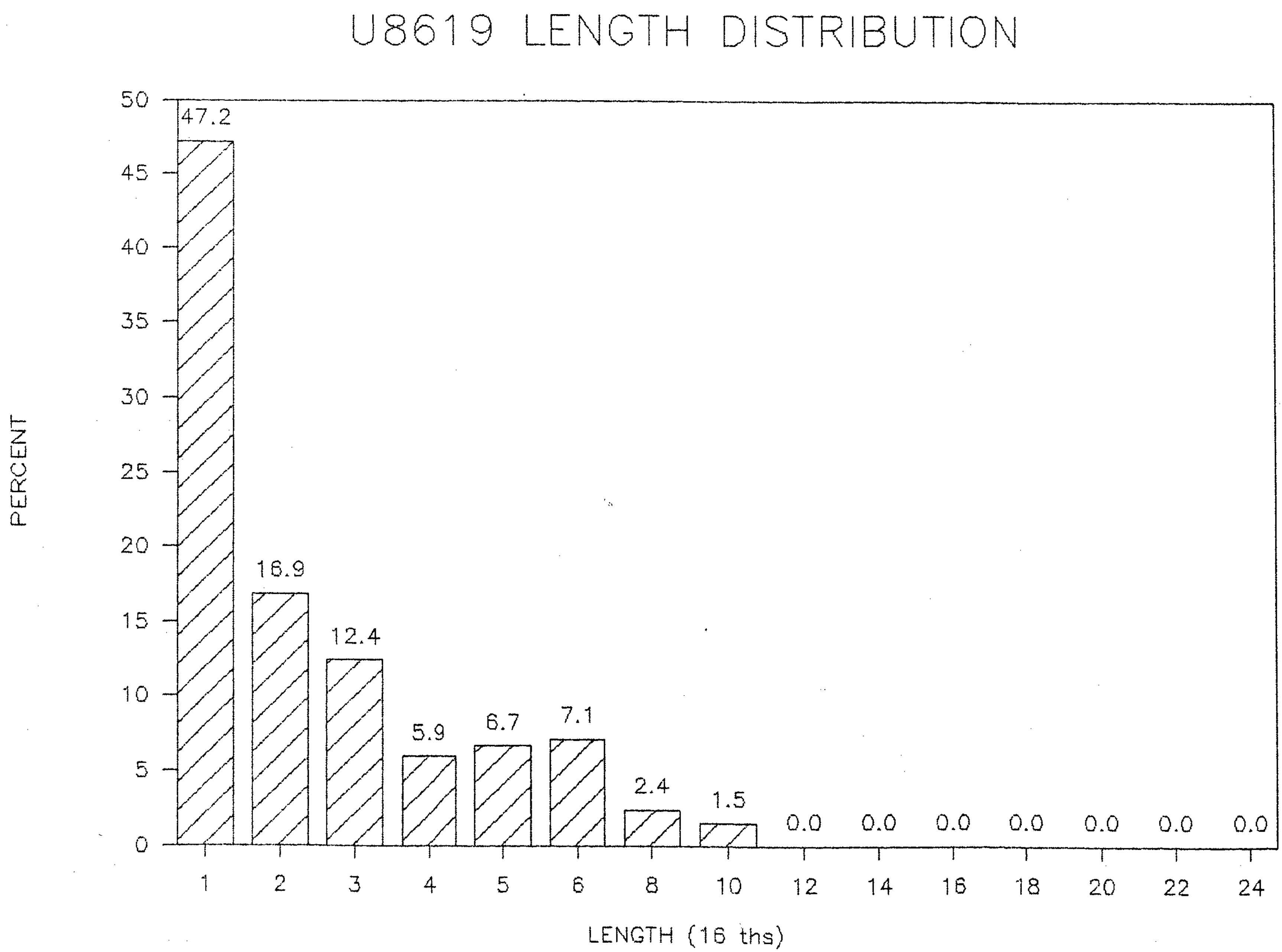
73.15	74.68	1.20	15	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
74.68	76.20	1.25	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
76.20	77.42	1.04	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

E.O.H.

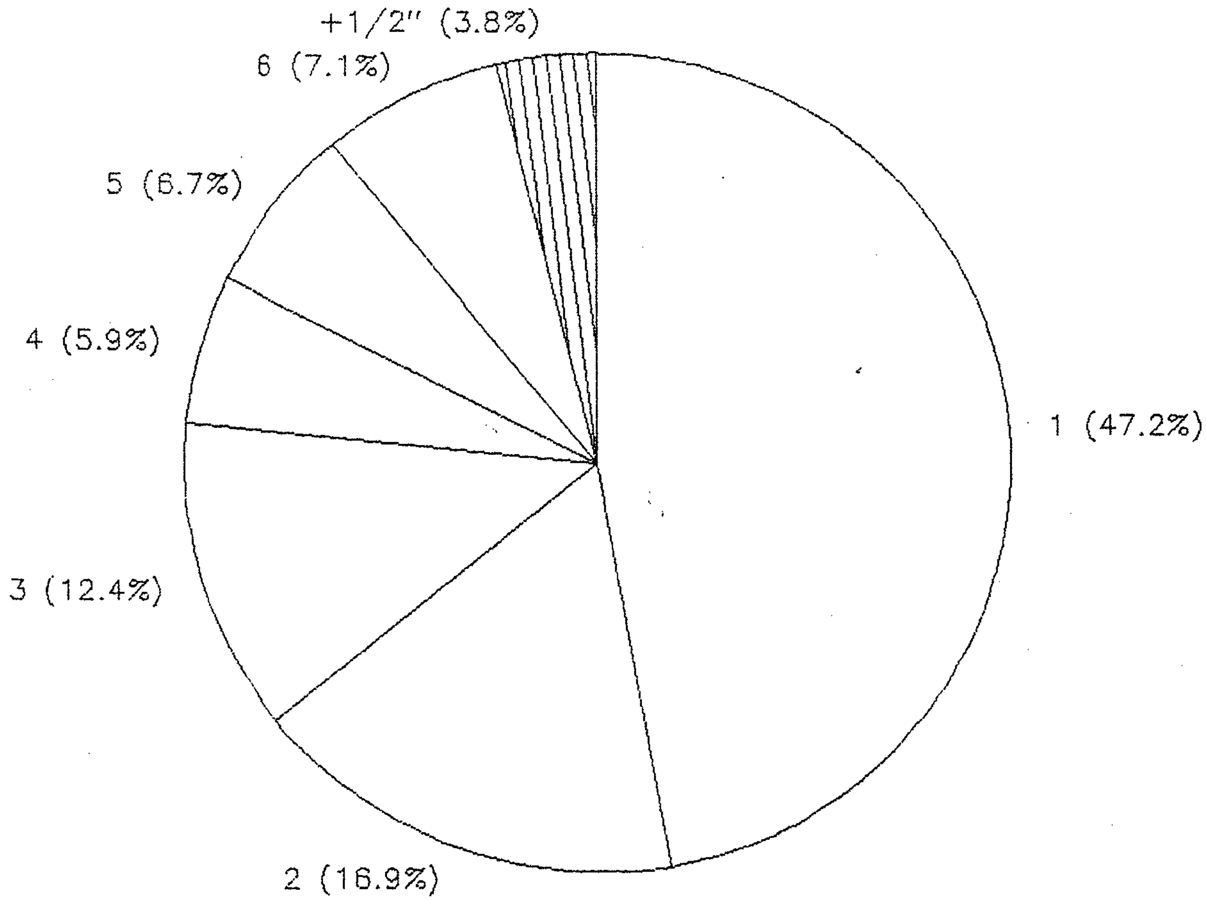
U8619 CCRG




U8619 RMR
RMR
50
40
30
20
10
0
1.52
16.76
32.00
47.24
62.48
77.42
METERAGE


U8619 LENGTH DISTRIBUTION
PERCENT
50
45
40
35
30
25
20
15
10
5
0
47.2
16.9
12.4
5.9
6.7
7.1
2.4
1.5
0.0
0.0
0.0
0.0
0.0
0.0
0.0
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16 ths)

U8619 LENGTH DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDAME HOLE U86-20 DEPTH 158.8

AZIMUTH 0.6164° INCLINATION +0.132° SECTION

LATITUDE 6714.682N DEPARTURE 7711.091E ELEVATION 1416.520

STARTED Nov. 18 FINISHED Nov. 26 LOGGED by DBP date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
0	7		Fault zone. Shattered serpentinite	
7	63.1		Serpentinite, very dark green, gradually going to dark green,	
			minor fibre	
			Fault zone 60.7 - 63.1	
63.1	107.6		Medium dark green, fibre bearing	
			Fault zone 104.2 - 106.1	
107.6	126.5		Fault zone, fractured & broken, some gouge, sparse fibre	
126.5	126.8		Rodingite	
126.8	158.8		Very dark green serp, lizardite stringers, sparse fibre,	
			broken	
			Fault zones 127.1 - 130.8, 132.9 - 136.9, 146.3 - 158.8	
158.8			E.O.H.	

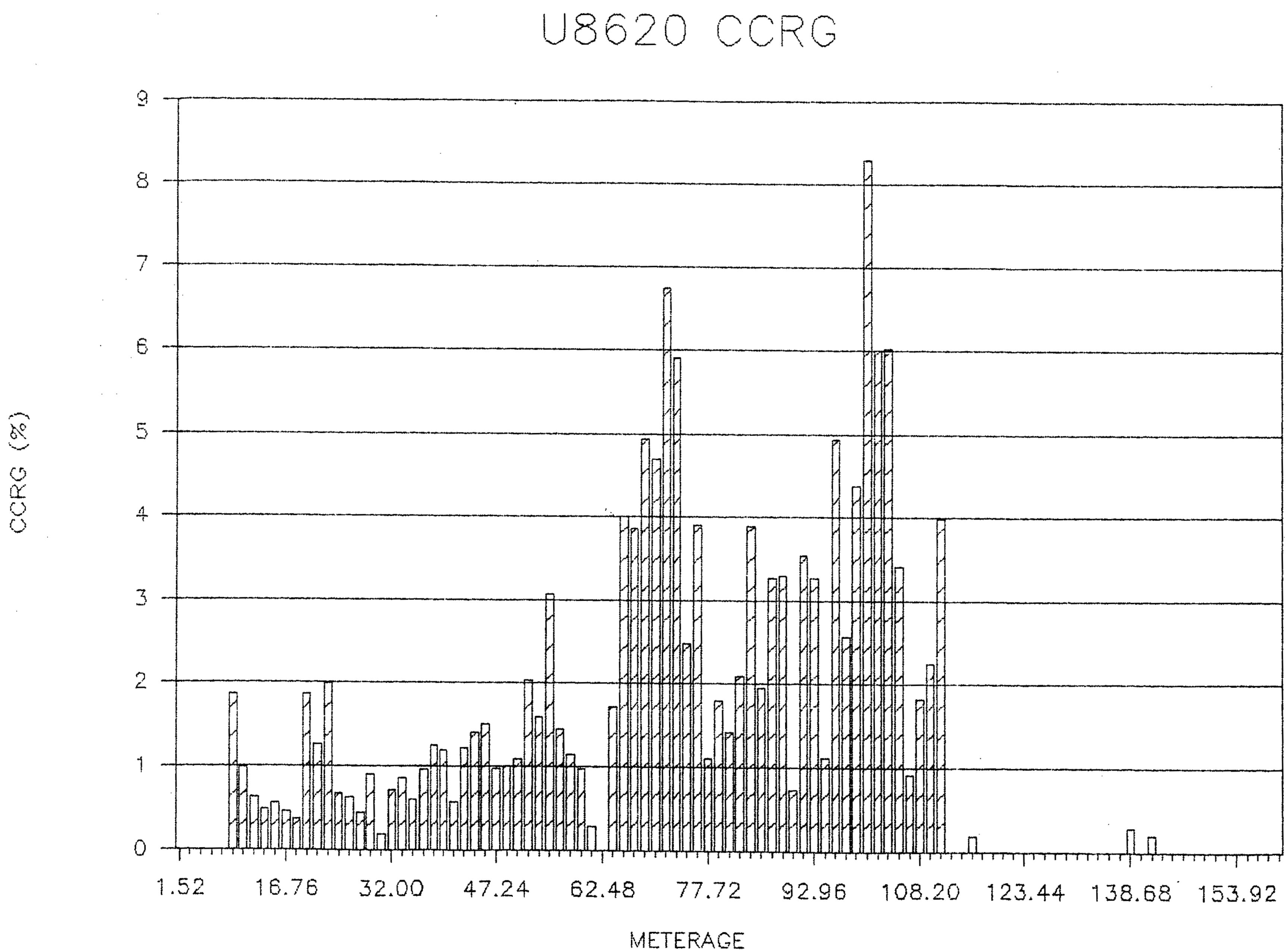
DDH U 8620

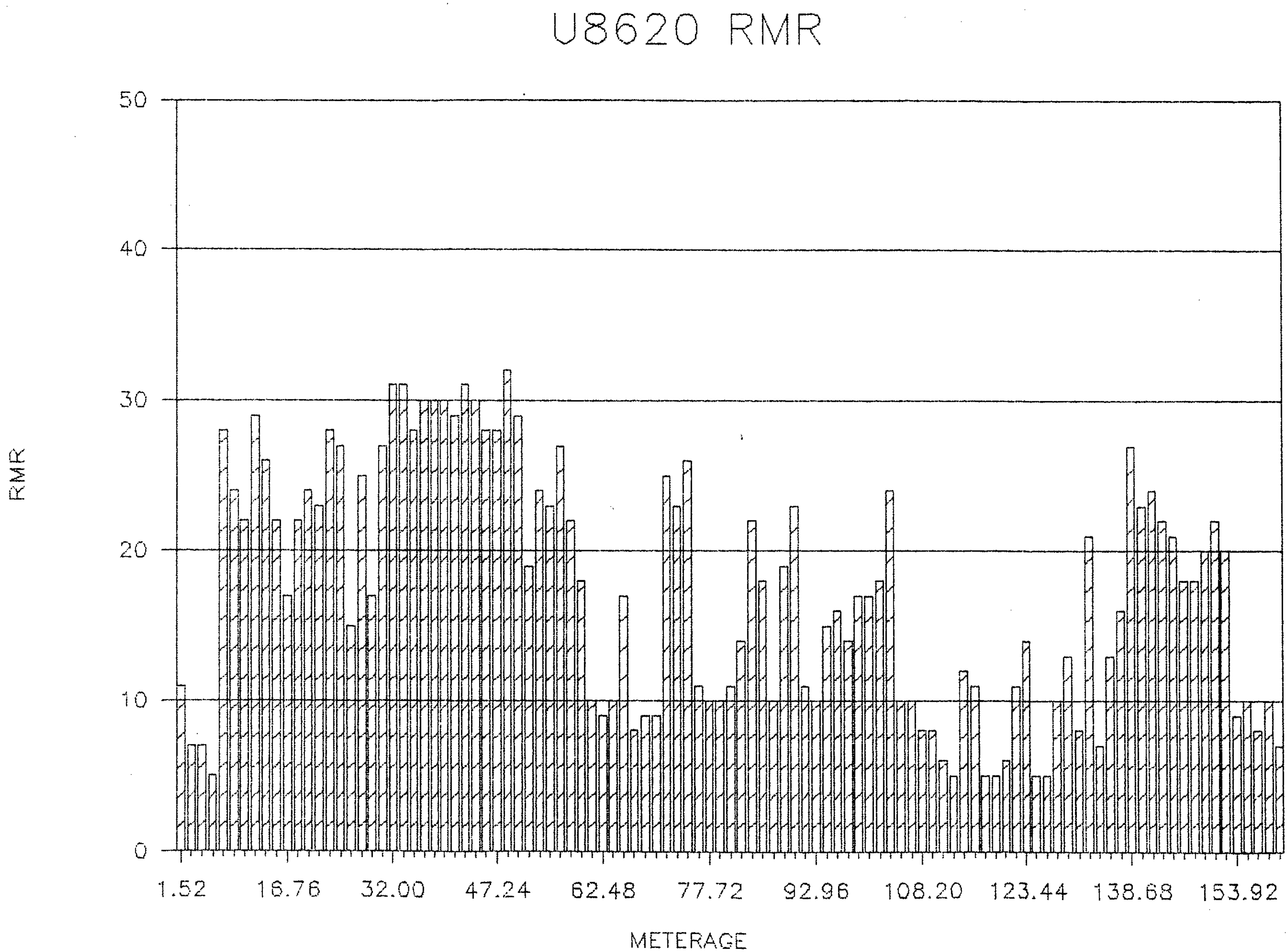
EAST: 6715 AZ: 0.6
NORTH: 7711 INCL: 0.13
ELEV:1416.5 DEPTH:158.8

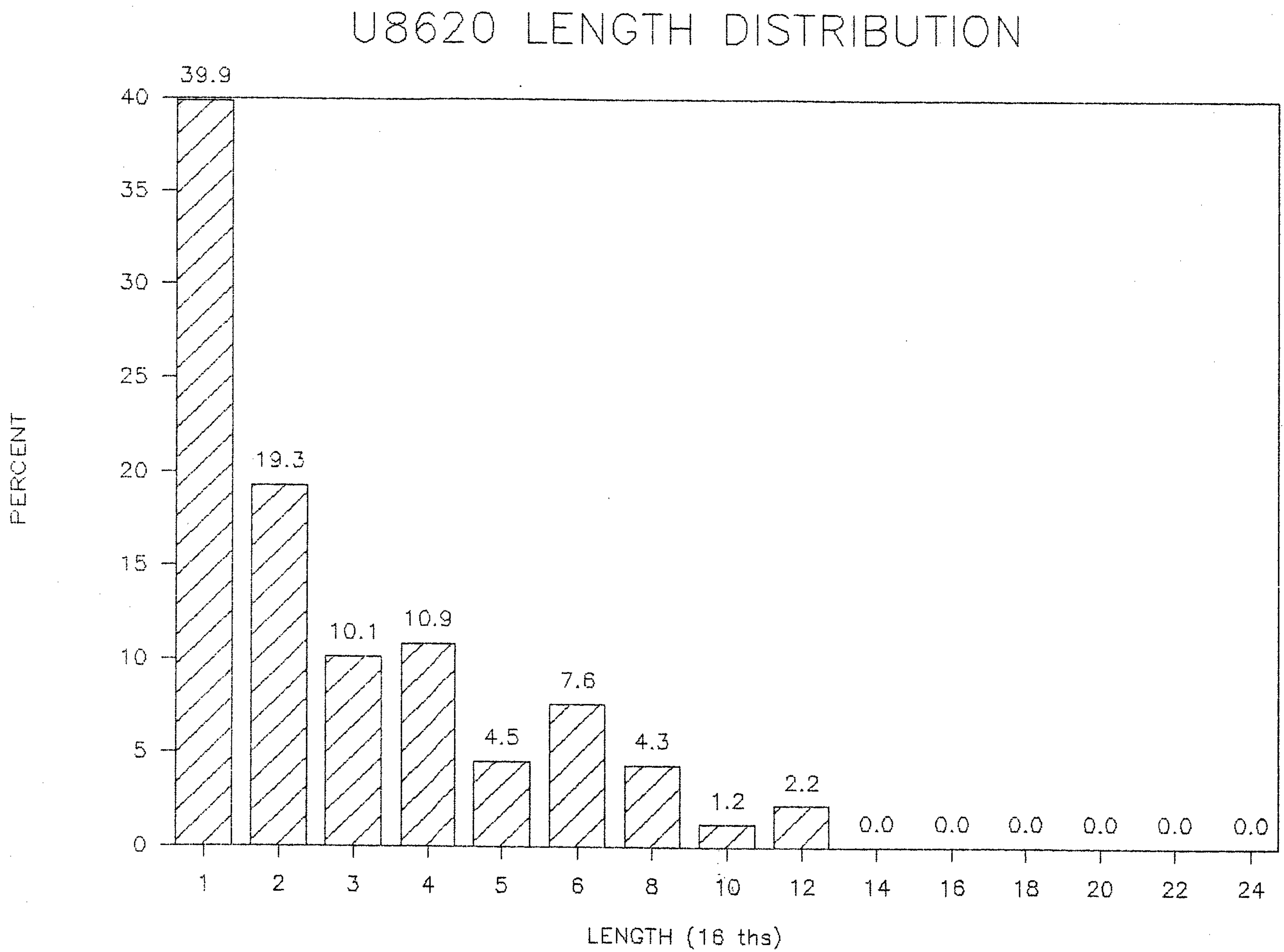
AVERAGE OF TWO COUNTS
Number of fibre veins counted per 16th category

FROM	TO	REC	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL	CCRG
M	M	M																	16's	%
0.00	1.52	0.12	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
1.52	3.05	0.58	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
3.05	4.57	0.79	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
4.57	6.10	0.67	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
6.10	7.62	0.59	28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
7.62	9.14	1.20	24	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10	1.86
9.14	10.67	1.25	22	5.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.99
10.67	12.19	1.42	29	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.63
12.19	13.72	1.17	26	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.48
13.72	15.24	1.02	22	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.55
15.24	16.76	0.99	17	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.45
16.76	18.29	0.91	22	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.37
18.29	19.81	1.26	24	2.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	1.86
19.81	21.34	1.43	23	6	1	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.25
21.34	22.86	1.36	28	7.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	12	1.99
22.86	24.38	1.36	27	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.66
24.38	25.91	1.25	15	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.63
25.91	27.43	1.01	25	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.45
27.43	28.96	0.99	17	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.91
28.96	30.48	1.20	27	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
30.48	32.00	1.42	31	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.71
32.00	33.53	1.43	31	5.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.86
33.53	35.05	1.33	28	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.59
35.05	36.58	1.42	30	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.95
36.58	38.10	1.45	30	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.24
38.10	39.62	1.42	30	4.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.19
39.62	41.15	1.39	29	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.57
41.15	42.67	1.39	31	6.5	0,5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.21
42.67	44.20	1.45	30	4.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9	1.40
44.20	45.72	1.42	28	7	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.50
45.72	47.24	1.39	28	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0.97
47.24	48.77	1.45	32	6.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.01
48.77	50.29	1.45	29	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.09
50.29	51.82	1.33	19	3	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	12	2.03
51.82	53.34	1.42	24	6.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10	1.58
53.34	54.86	1.36	23	4	4	0.5	0	0	0	0	0.5	0	0	0	0	0	0	0	18.5	3.06
54.86	56.39	1.40	27	8	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.44
56.39	57.91	1.37	22	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.15
57.91	59.44	1.26	18	5.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.98
59.44	60.96	1.20	10	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.28
60.96	62.48	0.94	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
62.48	64.01	0.91	10	4.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7	1.72
64.01	65.53	1.07	17	8.5	2	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	19	4.00
65.53	67.06	0.90	8	2.5	2	1	1.5	0	0	0	0	0	0	0	0	0	0	0	15.5	3.87
67.06	68.58	1.16	9	9	3	2.5	0	0	0.5	0	0	0	0	0	0	0	0	0	25.5	4.94
68.58	70.10	1.22	9	6	2.5	0.5	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	25.5	4.70
70.10	71.63	1.26	25	11	3.5	1.5	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	38	6.74
71.63	73.15	1.39	23	12.5	3	1.5	2	0.5	0.5	0	0	0	0	0	0	0	0	0	36.5	5.91

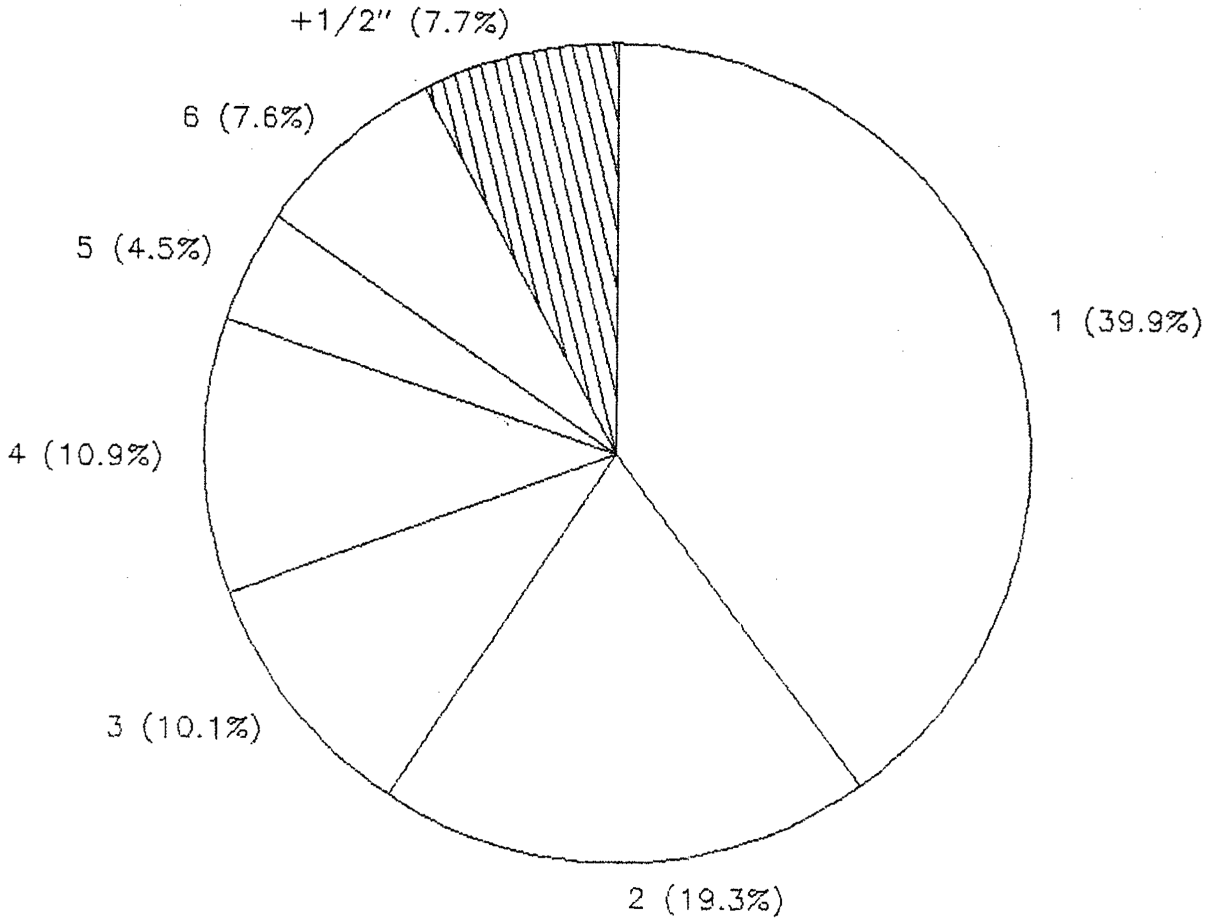
73.15	74.68	1.40	26	2.5	3.5	0	0	0	1	0	0	0	0	0	0	0	0	0	15.5	2.48
74.68	76.20	1.30	11	3	0.5	1	0.5	0.5	0.5	1	0	0	0	0	0	0	0	0	22.5	3.90
76.20	77.72	1.33	10	5.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.10
77.72	79.25	1.25	10	5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	10	1.80
79.25	80.77	1.19	11	4.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.42
80.77	82.30	1.34	14	4.5	1	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	12.5	2.09
82.30	83.82	1.36	22	7.5	4	2	0.5	0	0	0	0	0	0	0	0	0	0	0	23.5	3.89
83.82	85.34	1.33	18	4.5	1	1	0.5	0	0	0	0	0	0	0	0	0	0	0	11.5	1.95
85.34	86.87	1.23	10	3	1	1	0.5	1	0.5	0	0	0	0	0	0	0	0	0	18	3.27
86.87	88.39	1.19	19	4	2	1	1	0.5	0	0	0	0	0	0	0	0	0	0	17.5	3.30
88.39	89.92	1.23	23	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.73
89.92	91.44	1.17	11	7	3	1	0	0.5	0	0	0	0	0	0	0	0	0	0	18.5	3.54
91.44	92.96	1.10	10	2.5	1.5	0.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	0	16	3.27
92.96	94.49	1.20	15	2.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	6	1.12
94.49	96.01	1.30	16	2	1.5	0.5	0.5	0	0.5	0	0.5	1	0	0	0	0	0	0	28.5	4.94
96.01	97.54	1.26	14	6.5	1.5	0	0.5	0	0.5	0	0	0	0	0	0	0	0	0	14.5	2.57
97.54	99.06	1.36	17	7	3	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	26.5	4.39
99.06	100.58	1.34	17	8.5	3.5	1	2	0	1.5	1	0	0.5	0	0	0	0	0	0	49.5	8.29
100.58	102.11	1.40	18	4	3	1	2.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	37.5	6.00
102.11	103.63	1.42	24	9	3.5	1	2.5	0	1.5	0	0	0	0	0	0	0	0	0	38	6.02
103.63	105.16	1.25	10	3.5	2	2.5	0	0	0	0.5	0	0	0	0	0	0	0	0	19	3.41
105.16	106.68	1.22	10	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.92
106.68	108.20	0.99	8	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.81
108.20	109.73	0.94	8	5.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	9.5	2.26
109.73	111.25	0.73	6	2.5	0.5	0	0	0.5	0.5	0.5	0	0	0	0	0	0	0	0	13	3.99
111.25	112.78	0.70	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
112.78	114.30	0.66	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
114.30	115.82	0.59	11	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.19
115.82	117.35	0.32	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
117.35	118.87	0.29	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
118.87	120.40	0.38	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
120.40	121.92	0.23	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
121.92	123.44	0.23	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
123.44	124.97	0.69	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
124.97	126.49	1.05	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
126.49	128.02	0.99	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
128.02	129.54	0.72	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
129.54	131.06	0.94	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
131.06	132.59	1.02	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
132.59	134.11	0.88	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
134.11	135.64	0.78	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
135.64	137.16	0.98	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
137.16	138.68	1.22	27	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.28
138.68	140.21	1.14	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
140.21	141.73	1.14	24	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
141.73	143.26	1.10	22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
143.26	144.78	0.99	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
144.78	146.30	0.96	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
146.30	147.83	0.61	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
147.83	149.35	0.53	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
149.35	150.88	0.66	22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
150.88	152.40	0.81	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
152.40	153.92	0.62	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
153.92	155.45	0.62	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
155.45	156.97	0.62	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
156.97	158.50	0.62	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00


U8620 CCRG
CCRG (%)
METERAGE
0
1
2
3
4
5
6
7
8
9
1.52
16.76
32.00
47.24
62.48
77.72
92.96
108.20
123.44
138.68
153.92


U8620 RMR
50
40
30
20
10
0
RMR
1.52
16.76
32.00
47.24
62.48
77.72
92.96
108.20
123.44
138.68
153.92
METERAGE


U8620 LENGTH DISTRIBUTION
PERCENT
0
5
10
15
20
25
30
35
40
39.9
19.3
10.1
10.9
4.5
7.6
4.3
1.2
2.2
0.0
0.0
0.0
0.0
0.0
0.0
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16 ths)

U8620 LENGTH DISTRIBUTION



DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME	HOLE	U86-21	DEPTH	192.9 m
AZIMUTH	89.08^{O}	INCLINATION	-14.22^{O}	SECTION	6767N
LATITUDE	6765.80N	DEPARTURE	7703.20E	ELEVATION	1418.40 m
STARTED	Nov. 19	FINISHED	Nov. 25	LOGGED	by DBP date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1.2	29.6		Serpentinite, dark green, occasional lizardite stringers,	
			fibre bearing, broken	
			Fault zone 7.32 - 29.6, broken, minor gouge	
29.6	142		Medium dark green to medium green, good fibre, generally broken	
			Fault zone 91.7 - 94.2, 98.8 - 99.7, 112.5 - 113.4	
142	189.6		Dark green, minor to sparse fibre, broken	
			Fault zone 156.4 - 159.1, 181.4 - 188.4	
189.6	192.9		Diorite	
192.9			E.O.H.	

DDH U 8621

EAST:7703.2 AZ:89.05
NORTH:6765.8 INCL:14.13
ELEV: 1418 DEPTH:194.7

AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

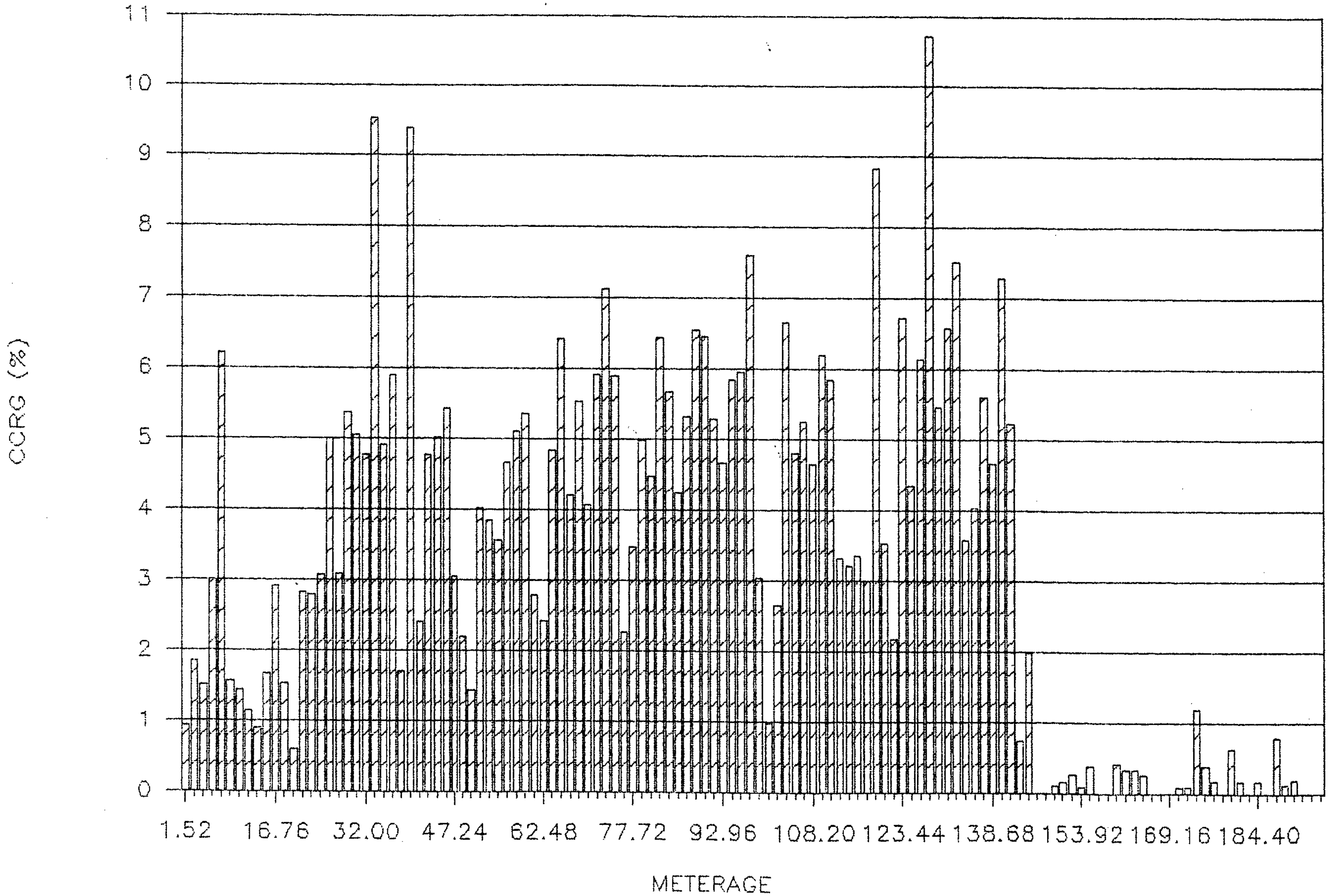
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.00	1.52	0.85	25	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.92
1.52	3.05	0.91	24	3.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.84
3.05	4.57	1.19	14	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.51
4.57	6.10	1.16	15	9.5	3	0	0	0	0	0	0	0	0	0	0	0	0	0	15.5	3.00
6.10	7.62	1.26	15	9	5	2	0.5	0	0	1	0	0	0	0	0	0	0	0	35	6.21
7.62	9.14	0.79	5	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.56
9.14	10.67	1.02	13	5.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.43
10.67	12.19	0.79	13	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	1.13
12.19	13.72	0.88	7	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.89
13.72	15.24	0.81	5	3	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.67
15.24	16.76	0.81	11	3.5	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	2.92
16.76	18.29	0.88	5	3	0	1	0	0	0	0	0	0	0	0	0	0	0	0	6	1.52
18.29	19.81	0.58	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.58
19.81	21.34	1.04	5	1.5	1.5	0.5	1	0	0.5	0	0	0	0	0	0	0	0	0	13	2.82
21.34	22.86	0.81	5	5	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	10	2.78
22.86	24.38	0.91	5	4	1	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	3.07
24.38	25.91	0.76	5	3.5	1	1.5	0.5	1	0	0	0	0	0	0	0	0	0	0	17	5.01
25.91	27.43	0.94	7	6.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	13	3.09
27.43	28.96	1.23	12	10	1.5	0.5	0	0	0.5	0	0.5	0	0.5	0	0	0	0	0	29.5	5.36
28.96	30.48	1.36	13	6.5	1.5	1.5	1	0.5	1	0.5	0	0	0	0	0	0	0	0	30.5	5.05
30.48	32.00	1.34	18	11	2	2.5	1.5	0	0	0	0	0	0	0	0	0	0	0	28.5	4.77
32.00	33.53	1.19	17	5.5	3	0.5	1	1.5	1.5	0.5	0.5	0	0	0.5	0	0	0	0	50.5	9.54
33.53	35.05	0.78	11	7	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	17	4.91
35.05	36.58	1.07	5	3.5	2	0.5	1.5	0	0.5	0	1	0	0	0	0	0	0	0	28	5.89
36.58	38.10	1.19	14	5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	9	1.70
38.10	39.62	1.16	13	8	5	1	1.5	0.5	1.5	0.5	0	0.5	0	0	0	0	0	0	48.5	9.40
39.62	41.15	0.70	5	6.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	2.40
41.15	42.67	1.39	16	13	4.5	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	29.5	4.78
42.67	44.20	1.34	18	7.5	4.5	0	1	0.5	0.5	0.5	0	0	0	0	0	0	0	0	30	5.02
44.20	45.72	1.33	22	4.5	2.5	1	1	0.5	0.5	0.5	0	0.5	0	0	0	0	0	0	32	5.42
45.72	47.24	1.36	17	6	2	0.5	0	0	0.5	0.5	0	0	0	0	0	0	0	0	18.5	3.06
47.24	48.77	1.39	16	7.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.19
48.77	50.29	1.33	17	6.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.44
50.29	51.82	1.34	17	7.5	3.5	1	0	0.5	0	0.5	0	0	0	0	0	0	0	0	24	4.02
51.82	53.34	1.43	19	8	3.5	1	0	0.5	0	0.5	0	0	0	0	0	0	0	0	24.5	3.84
53.34	54.86	1.48	19	5.5	3	0.5	0.5	0.5	1	0	0	0	0	0	0	0	0	0	23.5	3.57
54.86	56.39	1.37	18	9.5	4	0.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	28.5	4.66
56.39	57.91	1.39	17	6.5	3.5	2	1.5	0	1	0	0	0	0	0	0	0	0	0	31.5	5.10
57.91	59.44	1.28	13	2	2	1.5	1	0	0.5	1	0.5	0	0	0	0	0	0	0	30.5	5.35
59.44	60.96	1.37	18	10.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	17	2.78
60.96	62.48	1.25	13	7.5	0.5	0	0.5	0	0.5	0	0	0	0	0	0	0	0	0	13.5	2.43
62.48	64.01	1.34	16	6.5	2.5	1.5	1	1	0	0.5	0	0	0	0	0	0	0	0	29	4.85
64.01	65.53	1.19	7	7	3	1	2	0	1	0.5	0	0	0	0	0	0	0	0	34	6.42
65.53	67.06	1.49	17	10.5	2.5	0.5	0	0	0.5	1	0	0	0	0	0	0	0	0	28	4.21
67.06	68.58	1.40	29	6	2.5	1.5	0.5	1	1	0	0	0.5	0	0	0	0	0	0	34.5	5.52
68.58	70.10	1.33	23	4.5	4	0.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	24	4.06
70.10	71.63	1.48	25	8	2	2	1	0	0.5	1	0	0.5	0	0	0	0	0	0	39	5.92
71.63	73.15	1.42	25	8	2.5	2.5	2.5	0.5	1	0	0	0.5	0	0	0	0	0	0	45	7.13

73.15	74.68	1.45	28	11	2.5	2.5	1	1.5	0.5	0	0	0	0	0	0	0	0	0	38	5.89
74.68	76.20	1.34	18	5.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	13.5	2.26
76.20	77.72	1.36	26	5	1	2	0	1	0.5	0	0	0	0	0	0	0	0	0	21	3.48
77.72	79.25	1.46	11	7.5	4	0.5	0.5	1.5	1	0	0	0	0	0	0	0	0	0	32.5	4.99
79.25	80.77	1.48	20	6	2	1.5	1	0	0.5	1	0	0	0	0	0	0	0	0	29.5	4.48
80.77	82.30	1.46	29	10	3	0.5	1.5	1.5	1	0	0.5	0	0	0	0	0	0	0	42	6.44
82.30	83.82	1.45	17	6	3.5	1.5	1	0	0	0.5	0.5	0.5	0	0	0	0	0	0	36.5	5.66
83.82	85.34	1.48	25	5.5	1	1	1	0.5	0.5	1	0	0	0	0	0	0	0	0	28	4.25
85.34	86.87	1.48	27	8	3	0.5	0.5	0.5	1	0.5	0.5	0	0	0	0	0	0	0	35	5.31
86.87	88.39	1.39	23	6	3	3.5	0.5	0	2	0.5	0	0	0	0	0	0	0	0	40.5	6.56
88.39	89.92	1.36	23	7	5	0	0.5	0	1	1	0	0.5	0	0	0	0	0	0	39	6.45
89.92	91.44	1.30	19	8	1	2	1	0.5	0.5	0	0.5	0	0	0	0	0	0	0	30.5	5.29
91.44	92.96	1.25	13	3.5	1.5	0	1	0.5	1.5	0.5	0	0	0	0	0	0	0	0	26	4.67
92.96	94.49	1.25	13	6.5	4	1	1	0	0.5	1	0	0	0	0	0	0	0	0	32.5	5.84
94.49	96.01	1.36	19	9.5	6.5	0.5	2	0	0	0.5	0	0	0	0	0	0	0	0	36	5.96
96.01	97.54	1.40	23	5	2.5	0.5	3	1	0.5	0	1	0.5	0	0	0	0	0	0	47.5	7.61
97.54	99.06	1.30	14	6.5	3.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	17.5	3.03
99.06	100.58	1.26	14	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.98
100.58	102.11	1.40	21	3	3.5	0	1	0.5	0	0	0	0	0	0	0	0	0	0	16.5	2.64
102.11	103.63	1.26	14	4.5	0.5	0.5	1	1.5	1	1	0.5	0	0	0	0	0	0	0	37.5	6.66
103.63	105.16	1.49	20	5.5	1.5	0.5	1.5	0	0	0	0	0	0.5	0	0.5	0	0	0	32	4.81
105.16	106.68	1.43	21	7	1.5	1.5	0.5	1	0	0	0	1	0	0	0	0	0	0	33.5	5.25
106.68	108.20	1.33	20	7	2.5	0	0	0.5	0	1	0.5	0	0	0	0	0	0	0	27.5	4.66
108.20	109.73	1.45	20	6.5	0.5	2	1	1.5	0	0.5	0.5	0.5	0	0	0	0	0	0	40	6.20
109.73	111.25	1.40	26	6	2	2.5	1	1	1	0.5	0	0	0	0	0	0	0	0	36.5	5.84
111.25	112.78	1.36	16	6.5	3.5	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	20	3.31
112.78	114.30	1.40	20	9	1	3	0	0	0	0	0	0	0	0	0	0	0	0	20	3.20
114.30	115.82	1.48	26	5.5	2	1.5	1	0	0	0.5	0	0	0	0	0	0	0	0	22	3.34
115.82	117.35	1.49	25	5.5	3	1.5	1	0	0	0	0	0	0	0	0	0	0	0	20	3.01
117.35	118.87	1.46	29	11	2.5	2	1	1.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	57.5	8.82
118.87	120.40	1.40	25	4.5	3	2	0	0.5	0.5	0	0	0	0	0	0	0	0	0	22	3.52
120.40	121.92	1.45	26	12	1	0	0	0	0	0	0	0	0	0	0	0	0	0	14	2.17
121.92	123.44	1.39	19	12	3	2.5	2	1	0.5	0	0	0	0	0	0	0	0	0	41.5	6.72
123.44	124.97	1.49	18	12	1.5	1	0	0	0	0	0.5	0.5	0	0	0	0	0	0	29	4.36
124.97	126.49	1.48	22	12.5	4	2	3.5	0	0	0	0	0	0	0	0	0	0	0	40.5	6.15
126.49	128.02	1.37	20	7.5	2.5	4	1.5	1	2	0.5	0	0.5	0	0.5	0	0	0	0	65.5	10.72
128.02	129.54	1.42	23	5.5	3.5	1.5	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	34.5	5.46
129.54	131.06	1.42	29	4.5	2	2	2.5	1	2	0	0	0	0	0	0	0	0	0	41.5	6.57
131.06	132.59	1.52	28	8	4.5	1	5	1	1	0	0	0	0	0	0	0	0	0	51	7.51
132.59	134.11	1.51	31	4.5	1.5	1.5	0	0	0.5	0.5	0.5	0	0	0	0	0	0	0	24	3.57
134.11	135.64	1.42	21	10.5	2.5	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	25.5	4.04
135.64	137.16	1.46	32	2	2	1.5	1	1	1.5	1	0	0	0	0	0	0	0	0	36.5	5.60
137.16	138.68	1.42	18	15.5	4	1	0	0	0.5	0	0	0	0	0	0	0	0	0	29.5	4.67
138.68	140.21	1.28	14	4.5	3.5	0.5	1	0.5	1	2	0	0	0	0	0	0	0	0	41.5	7.28
140.21	141.73	1.31	16	8.5	2	2.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	30.5	5.22
141.73	143.26	1.37	15	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.74
143.26	144.78	1.31	14	6.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	11.5	1.97
144.78	146.30	1.25	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
146.30	147.83	1.25	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
147.83	149.35	1.13	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
149.35	150.88	0.78	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.14
150.88	152.40	1.33	14	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
152.40	153.92	1.26	8	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
153.92	155.45	1.46	16	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.38
155.45	156.97	1.13	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
156.97	158.50	0.88	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

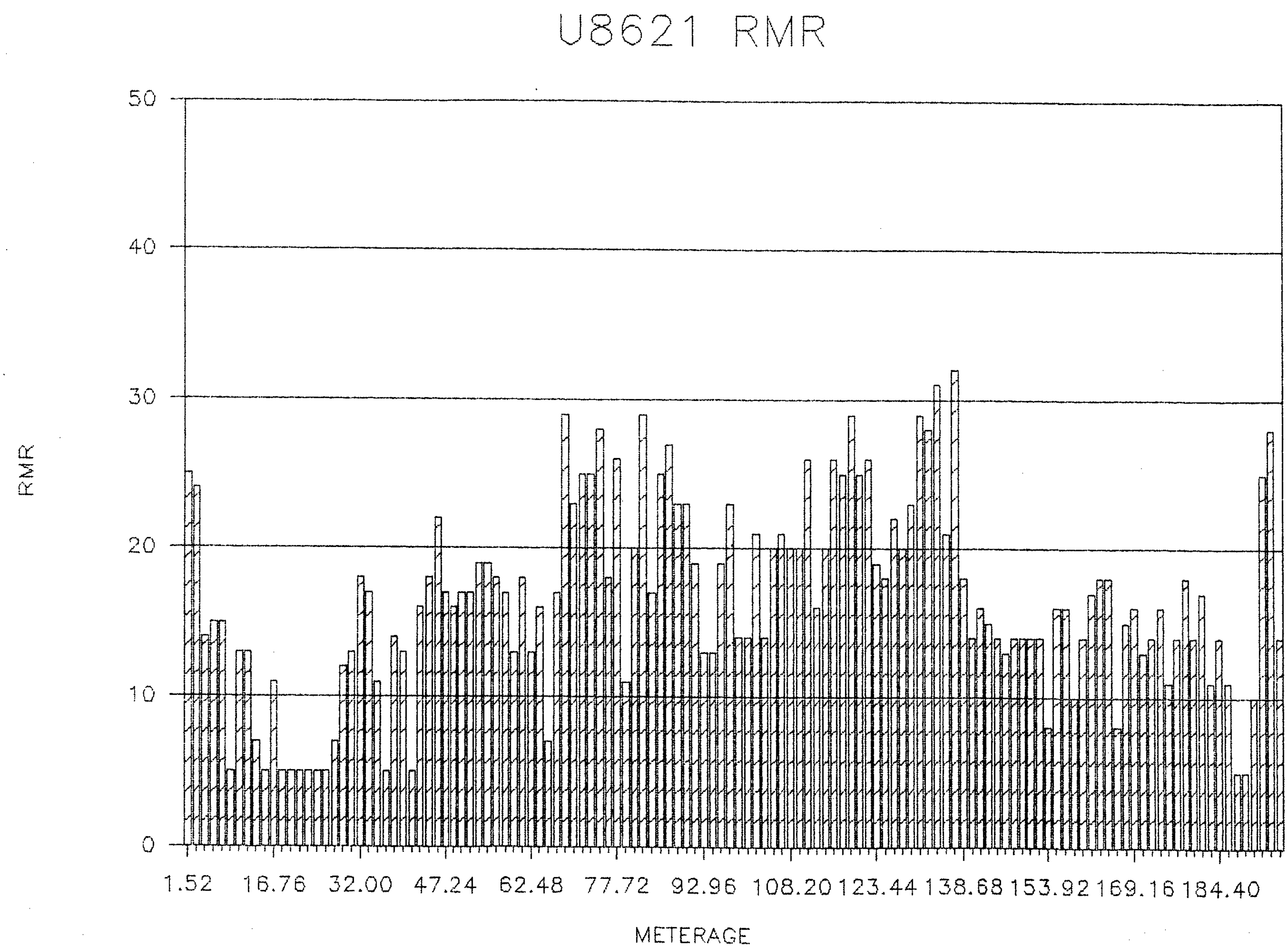
158.50	160.02	1.37	14	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
160.02	161.54	1.39	17	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.32
161.54	163.07	1.37	18	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.33
163.07	164.59	1.37	18	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
164.59	166.12	1.30	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
166.12	167.64	1.22	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
167.64	169.16	1.31	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
169.16	170.69	1.31	13	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
170.69	172.21	1.37	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
172.21	173.74	1.42	16	3	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.19
173.74	175.26	1.19	11	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.38
175.26	176.78	1.28	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
176.78	178.31	1.40	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
178.31	179.83	1.25	14	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.63
179.83	181.36	1.33	17	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
181.36	182.88	1.04	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
182.88	184.40	1.42	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
184.40	185.93	1.33	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
185.93	187.45	1.01	5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.78
187.45	188.98	0.98	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.12
188.98	190.50	1.26	10	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
190.50	192.02	1.28	25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
192.02	193.55	1.51	28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
193.55	194.77	0.98	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

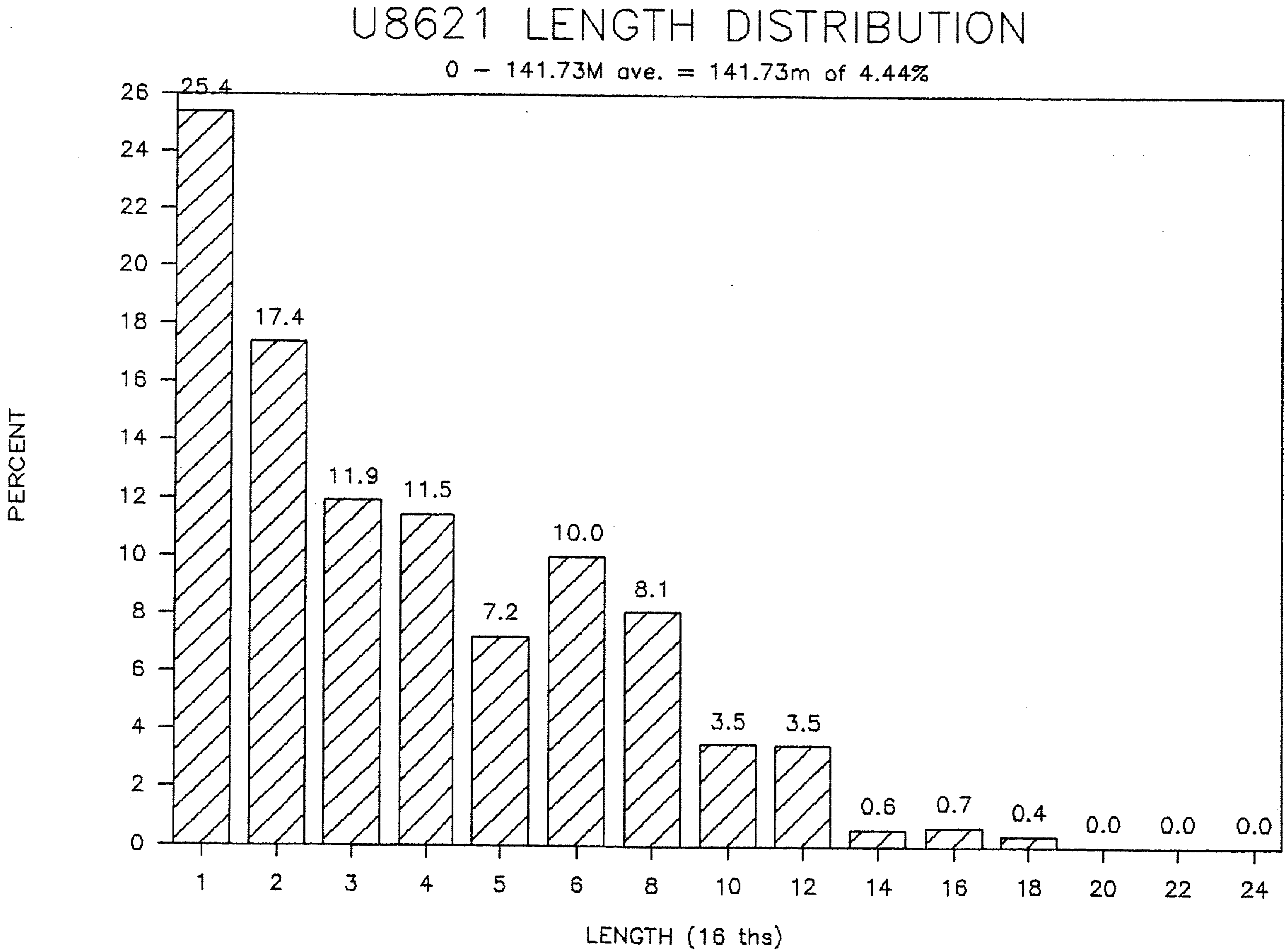
EOH

U8621 CCRG



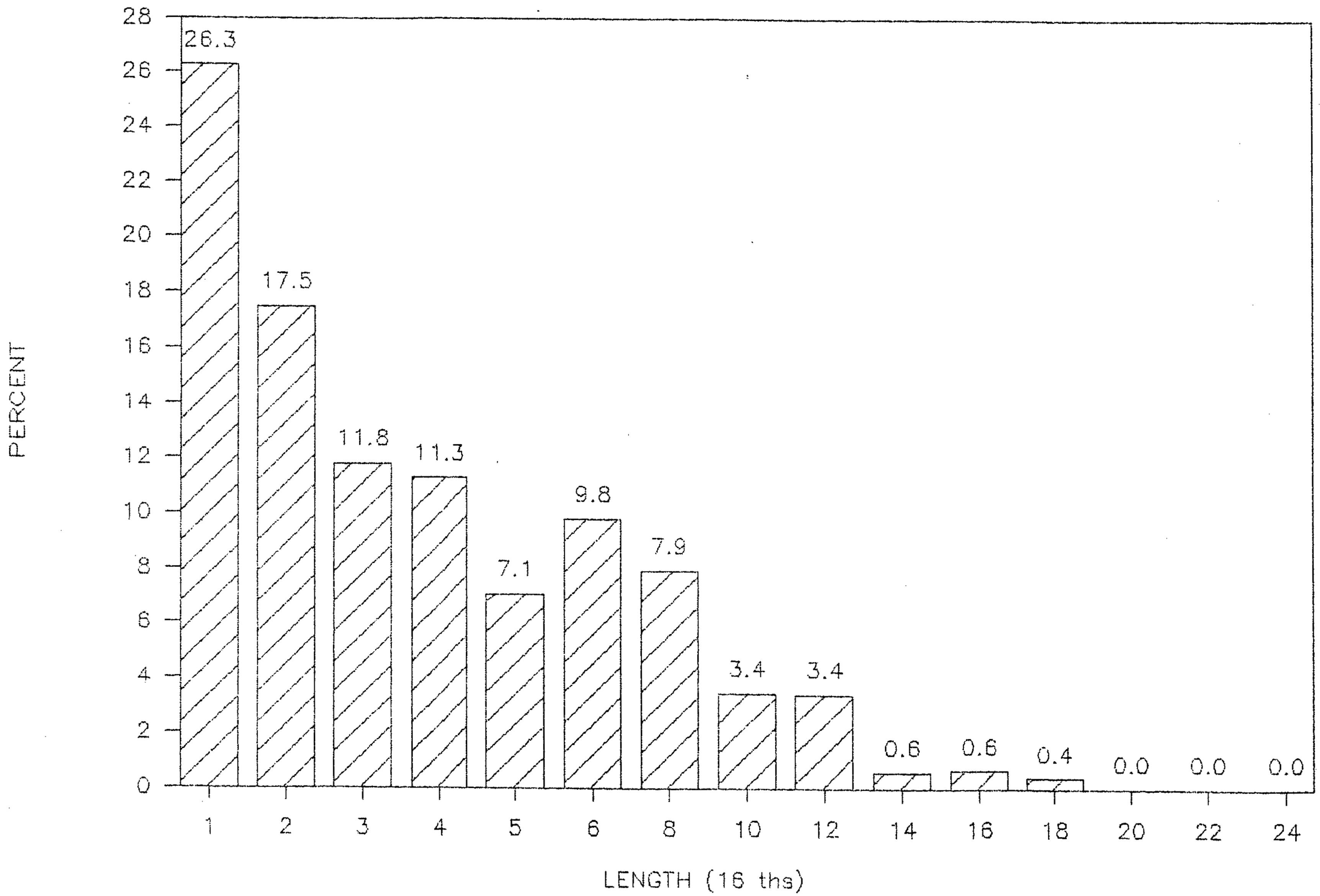
CCRG (%)
0
1
2
3
4
5
6
7
8
9
10
11
1.52
16.76
32.00
47.24
62.48
77.72
92.96
108.20
123.44
138.68
153.92
169.16
184.40
METERAGE


U8621 RMR
50
40
30
20
10
0
RMR
1.52
16.76
32.00
47.24
62.48
77.72
92.96
108.20
123.44
138.68
153.92
169.16
184.40
METERAGE

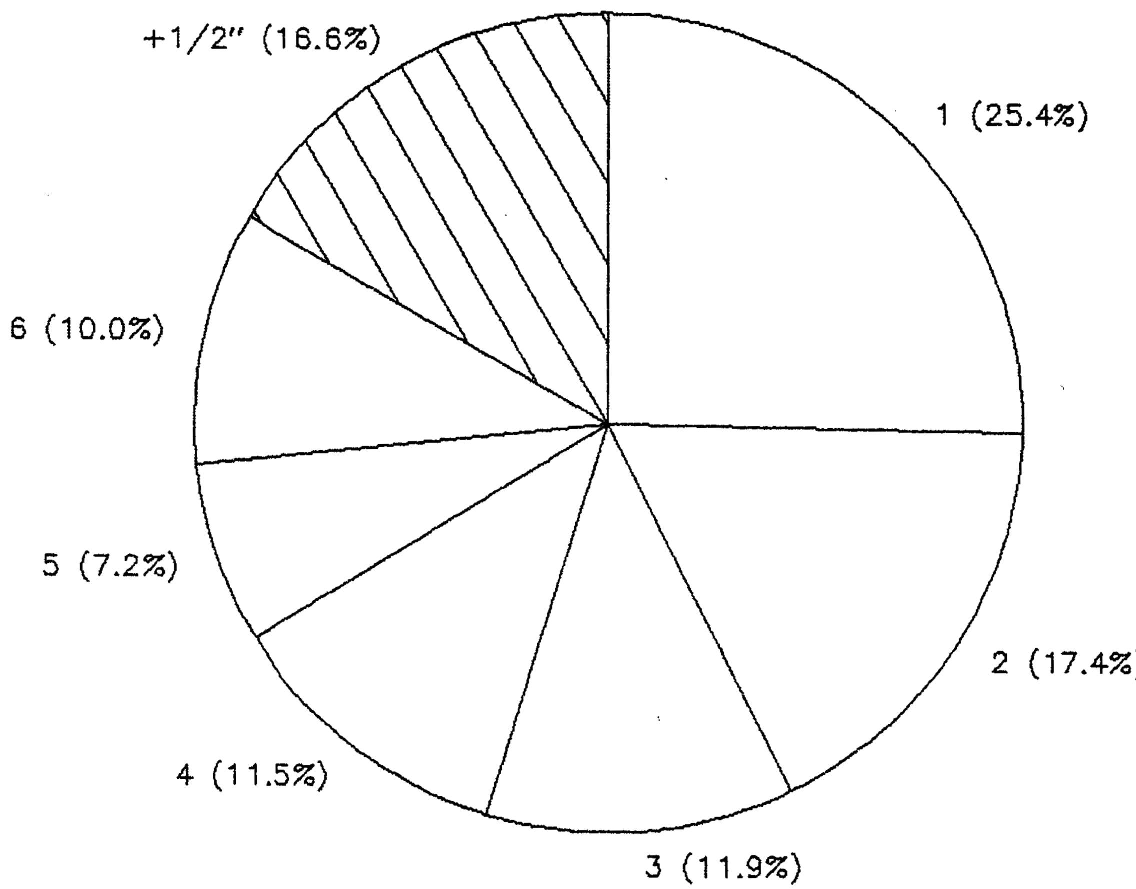


U8621 LENGTH DISTRIBUTION
0 – 141.73M ave. = 141.73m of 4.44%
PERCENT
0
2
4
6
8
10
12
14
16
18
20
22
24
26
25.4
17.4
11.9
11.5
7.2
10.0
8.1
3.5
3.5
0.6
0.7
0.4
0.0
0.0
0.0
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16 ths)

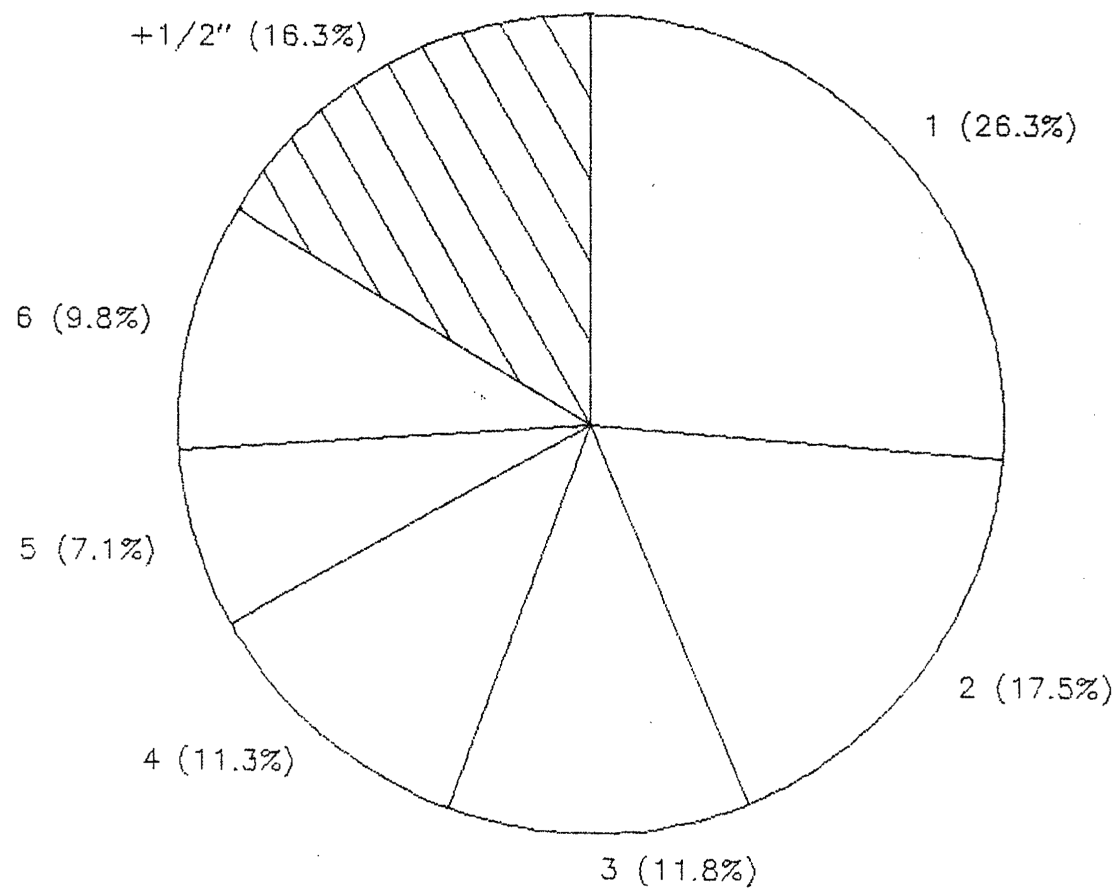
U8621 LENGTH DISTRIBUTION



U8621 LENGTH DISTRIBUTION



U8621 LENGTH DISTRIBUTION



DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME	HOLE	U86-22	DEPTH	273.71
AZIMUTH	89.5489°	INCLINATION	-69°	SECTION	6767N
LATITUDE	6765.8N	DEPARTURE	7702.1	ELEVATION	1417.9
STARTED	Nov. 26	FINISHED	Dec. 3	LOGGED	by DBP date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
1.5	223.7		Serpentinite, medium dark green, fibre bearing	
			Fault zones 1.5 - 5.5, 39 - 42.7, 80.8 - 87.2, 96.3 - 101.5,	
			108.2 - 110.3, 137.2 - 138, 170 - 172.2, 189.9 - 202, 217 - 218.7	
223.7	273.71		Dark green, sparse fibre, lizardite stringers, broken	
			Fault zone 223.7 - 228.6	
273.71			E.O.H.	

DDH U 8622

EAST: 6766 AZ: 89.5
NORTH: 7702 INCL: -69
ELEV: 1418 DEPTH:273.7

AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

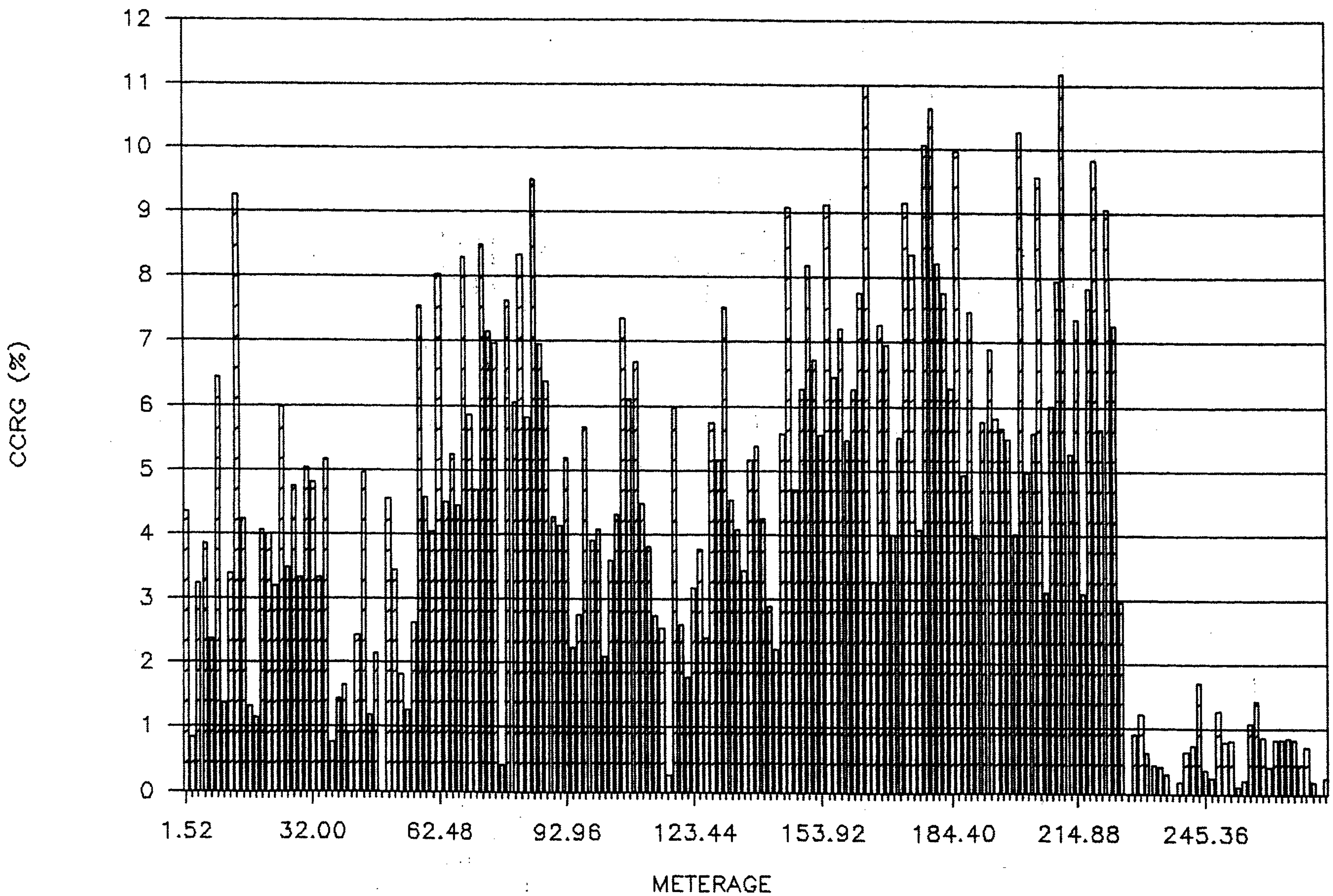
FROM	TO	REC	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL	CCRG
M	M	M																	16's	%
0.00	1.52	0.26	11	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5	4.33
1.52	3.05	0.81	11	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.83
3.05	4.57	1.01	13	6.5	4	0	0	0	0	0	0	0	0	0	0	0	0	0	14.5	3.24
4.57	6.10	1.05	5	4.5	4.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	18	3.84
6.10	7.62	1.19	14	6.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	2.36
7.62	9.14	1.33	18	15	3.5	0.5	1.5	0.5	1	0	0	0	0	0	0	0	0	0	38	6.43
9.14	10.67	1.07	11	5.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.37
10.67	12.19	1.10	13	6	0.5	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	16.5	3.38
12.19	13.72	1.19	17	6	5	1	2	1	1	0	0.5	0.5	0	0	0	0	0	0	49	9.25
13.72	15.24	1.25	13	2.5	2.5	0.5	0.5	0.5	1	0.5	0	0	0	0	0	0	0	0	23.5	4.22
15.24	16.76	1.28	16	4.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	7.5	1.32
16.76	18.29	1.19	15	4.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6	1.13
18.29	19.81	1.49	14	8.5	2	1	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	27	4.06
19.81	21.34	1.46	16	8.5	4	1	1	0.5	0	0	0	0	0	0	0	0	0	0	26	3.99
21.34	22.86	1.40	9	3.5	2	1.5	1	0	0	0.5	0	0	0	0	0	0	0	0	20	3.20
22.86	24.38	1.45	10	6	5	0.5	2	1	0	1	0	0	0	0	0	0	0	0	38.5	5.97
24.38	25.91	1.45	14	5	4	1.5	0	1	0	0	0	0	0	0	0	0	0	0	22.5	3.49
25.91	27.43	1.33	15	1	0.5	1.5	0.5	0.5	0	0.5	0.5	0	0	0.5	0	0	0	0	28	4.74
27.43	28.96	1.42	11	6	0.5	0.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	21	3.33
28.96	30.48	1.49	15	9	4.5	3	1	0.5	0	0	0	0	0	0	0	0	0	0	33.5	5.04
30.48	32.00	1.40	9	13	5	0	1	0	0.5	0	0	0	0	0	0	0	0	0	30	4.80
32.00	33.53	1.42	8	7.5	3	0.5	1.5	0	0	0	0	0	0	0	0	0	0	0	21	3.33
33.53	35.05	1.39	8	10.5	4.5	1	1	0.5	0.5	0	0	0	0	0	0	0	0	0	32	5.18
35.05	36.58	1.34	14	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.75
36.58	38.10	1.26	15	6	1	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.42
38.10	39.62	1.16	15	6	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.65
39.62	41.15	0.99	5	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.91
41.15	42.67	1.07	5	6	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	11.5	2.42
42.67	44.20	1.40	17	10.5	2.5	0.5	2	0	1	0	0	0	0	0	0	0	0	0	31	4.96
44.20	45.72	1.43	16	4	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.18
45.72	47.24	1.37	21	7	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13	2.13
47.24	48.77	1.25	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
48.77	50.29	1.48	17	4.5	2	0	0.5	0.5	1	0	0.5	0.5	0	0	0	0	0	0	30	4.56
50.29	51.82	1.43	19	8.5	2.5	2	0	0.5	0	0	0	0	0	0	0	0	0	0	22	3.45
51.82	53.34	1.42	17	4.5	1	0	0	1	0	0	0	0	0	0	0	0	0	0	11.5	1.82
53.34	54.86	1.43	17	4	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	8	1.25
54.86	56.39	1.33	16	5	0.5	0	1	0.5	0.5	0	0	0	0	0	0	0	0	0	15.5	2.62
56.39	57.91	1.28	13	5	0.5	0.5	2	1.5	0	1.5	0	0	0	0.5	0	0	0	0	43	7.54
57.91	59.44	1.25	15	7	3	1	1	0.5	0.5	0	0	0	0	0	0	0	0	0	25.5	4.58
59.44	60.96	1.42	16	5	2	0.5	0.5	0	0	1	0.5	0	0	0	0	0	0	0	25.5	4.04
60.96	62.48	1.19	14	10.5	2.5	2	2	1	0.5	0	0.5	0	0	0	0	0	0	0	42.5	8.03
62.48	64.01	1.25	5	3.5	0.5	1	0	0.5	0.5	1.5	0	0	0	0	0	0	0	0	25	4.49
64.01	65.53	1.33	17	3.5	3	0.5	1.5	2	0	0.5	0	0	0	0	0	0	0	0	31	5.25
65.53	67.06	1.49	10	6	1.5	2.5	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	29.5	4.43
67.06	68.58	1.46	23	13	7	1	1	0	0	1.5	0	0	0	0.5	0	0	0	0	54	8.29
68.58	70.10	1.42	24	7.5	6	2.5	1	0	1	0	0	0	0	0	0	0	0	0	37	5.86
70.10	71.63	1.39	18	13	5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	29	4.69
71.63	73.15	1.30	20	10	5	3.5	1.5	0.5	1	0.5	0	0	0	0	0	0	0	0	49	8.49

73.15	74.68	1.48	18	9.5	2.5	1	2	0.5	0	1.5	0	0	0.5	0	0	0	0	0	47	7.14
74.68	76.20	1.45	20	6.5	2	1	2	1.5	0.5	1	0.5	0	0	0	0	0	0	0	45	6.98
76.20	77.72	1.34	16	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.42
77.72	79.25	1.33	16	7	5	1	2	1	2	0	0	0	0	0	0	0	0	0	45	7.62
79.25	80.77	1.28	13	12.5	2.5	1.5	1	0.5	1	0	0	0	0	0	0	0	0	0	34.5	6.05
80.77	82.30	1.28	11	5.5	5.5	2	2.5	0	0.5	1.5	0	0	0	0	0	0	0	0	47.5	8.33
82.30	83.82	1.08	11	5	2	2	2.5	0	0.5	0	0	0	0	0	0	0	0	0	28	5.81
83.82	85.34	1.05	5	7.5	2	3	2	1	0.5	1	0	0	0	0	0	0	0	0	44.5	9.50
85.34	86.87	1.36	5	3	1	0.5	2.5	0.5	0.5	0.5	0	0	0.5	0	0.5	0	0	0	42	6.95
86.87	88.39	1.13	13	6	2.5	1	1.5	0	0.5	0.5	0.5	0	0	0	0	0	0	0	32	6.37
88.39	89.92	1.34	16	6.5	0.5	2	1.5	0	1	0	0	0	0	0	0	0	0	0	25.5	4.27
89.92	91.44	1.14	18	10	1.5	0	0.5	0	1	0	0	0	0	0	0	0	0	0	21	4.12
91.44	92.96	1.23	13	10.5	2	0	1	0	0	0	1	0	0	0	0	0	0	0	28.5	5.18
92.96	94.49	1.40	16	6.5	1	0.5	1	0	0	0	0	0	0	0	0	0	0	0	14	2.24
94.49	96.01	1.26	14	9	1	1.5	0	0	0	0	0	0	0	0	0	0	0	0	15.5	2.75
96.01	97.54	1.13	11	9	4	0.5	1	0	1	0	0	0	0	0	0	0	0	0	28.5	5.67
97.54	99.06	1.01	11	3	2	2	0.5	0.5	0	0	0	0	0	0	0	0	0	0	17.5	3.91
99.06	100.58	1.16	11	4	1.5	0.5	1	0.5	1	0	0	0	0	0	0	0	0	0	21	4.07
100.58	102.11	1.28	11	4.5	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	12	2.10
102.11	103.63	1.25	14	2	0.5	1	0	0	0	0.5	1	0	0	0	0	0	0	0	20	3.59
103.63	105.16	1.33	14	7	1.5	0	0.5	0.5	0.5	1	0	0	0	0	0	0	0	0	25.5	4.32
105.16	106.68	1.39	16	5.5	4.5	2	2	0	0.5	1	0	0.5	0	0	0	0	0	0	45.5	7.37
106.68	108.20	1.16	11	6.5	1.5	0	1	0	0.5	0.5	0.5	0.5	0	0	0	0	0	0	31.5	6.11
108.20	109.73	0.98	5	6.5	2.5	3	1.5	0.5	0	0	0	0	0	0	0	0	0	0	29	6.67
109.73	111.25	1.20	5	9	3.5	0.5	0	0.5	0	0.5	0	0	0	0	0	0	0	0	24	4.47
111.25	112.78	1.33	15	7	2.5	0.5	1	1	0	0	0	0	0	0	0	0	0	0	22.5	3.81
112.78	114.30	1.40	14	6.5	2	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	17	2.72
114.30	115.82	1.37	16	9	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.54
115.82	117.35	1.28	14	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
117.35	118.87	1.30	13	5	1.5	0	2	0.5	1	0.5	0	0.5	0	0	0	0	0	0	34.5	5.98
118.87	120.40	1.34	17	4.5	1.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.59
120.40	121.92	1.33	13	6	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.78
121.92	123.44	1.31	17	9.5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	0	18.5	3.17
123.44	124.97	1.31	13	8	6	0	0.5	0	0	0	0	0	0	0	0	0	0	0	22	3.77
124.97	126.49	1.22	16	8	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	13	2.39
126.49	128.02	1.46	16	11.5	5	2	1.5	0	0	0.5	0	0	0	0	0	0	0	0	37.5	5.75
128.02	129.54	1.39	19	14.5	3.5	2	0.5	0.5	0	0	0	0	0	0	0	0	0	0	32	5.18
129.54	131.06	1.36	18	9	2.5	1.5	2.5	1	2	0	0	0	0	0	0	0	0	0	45.5	7.53
131.06	132.59	1.19	14	8.5	1.5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	24	4.53
132.59	134.11	1.30	14	7	2	1.5	0	0	0.5	0	0.5	0	0	0	0	0	0	0	23.5	4.07
134.11	135.64	1.17	15	6.5	2.5	0	1	0.5	0	0	0	0	0	0	0	0	0	0	18	3.44
135.64	137.16	1.28	14	8	3.5	1	0	0.5	0.5	0	0	0.5	0	0	0	0	0	0	29.5	5.17
137.16	138.68	1.30	13	8	1.5	1	1	0	0.5	0	1	0	0	0	0	0	0	0	31	5.37
138.68	140.21	1.37	16	10.5	2.5	0.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	26	4.26
140.21	141.73	1.28	15	5	1	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	16.5	2.89
141.73	143.26	1.31	15	4	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	13	2.23
143.26	144.78	1.37	17	12	3.5	1	1.5	0	1	0	0	0	0	0	0	0	0	0	34	5.56
144.78	146.30	1.37	17	9.5	4	1	1	1	1.5	1.5	0.5	0	0	0	0	0	0	0	55.5	9.08
146.30	147.83	1.31	14	9.5	2	0.5	1	0.5	1	0	0	0	0	0	0	0	0	0	27.5	4.71
147.83	149.35	1.11	13	4.5	3.5	1.5	0.5	2	0.5	0	0	0	0	0	0	0	0	0	31	6.26
149.35	150.88	1.11	13	8	5	2.5	3	0	0.5	0	0	0	0	0	0	0	0	0	40.5	8.17
150.88	152.40	1.40	5	5	5.5	1	1	1	1	1	0	0	0	0	0	0	0	0	42	6.72
152.40	153.92	1.30	16	5.5	1.5	4.5	0.5	0	0	1	0	0	0	0	0	0	0	0	32	5.55
153.92	155.45	1.40	17	7	3.5	2	2	0	0.5	0	0.5	0	1.5	0	0	0	0	0	57	9.13
155.45	156.97	1.36	17	5.5	2	1.5	1.5	2	0	0.5	0.5	0	0	0	0	0	0	0	39	6.45
156.97	158.50	1.36	14	7	2.5	3.5	1	2	0.5	0.5	0	0	0	0	0	0	0	0	43.5	7.20

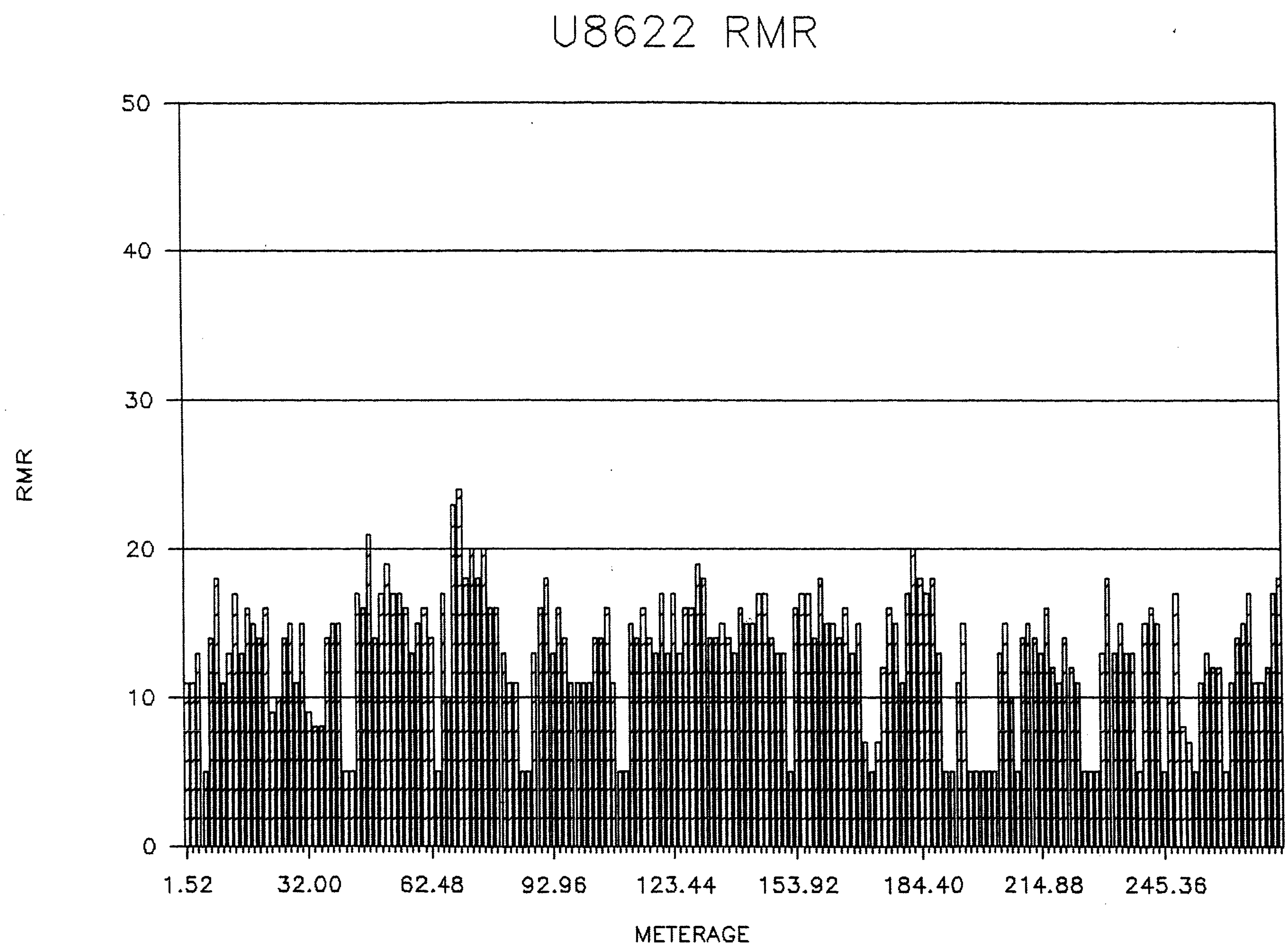
158.50	160.02	1.42	18	7.5	2.5	0	2	1	0	0.5	0.5	0	0	0	0	0	0	0	34.5	5.46
160.02	161.54	1.52	15	5.5	3.5	0.5	0.5	0.5	2	1.5	0	0	0	0	0	0	0	0	42.5	6.26
161.54	163.07	1.11	15	4	2	0	0.5	0.5	0	1	1	0	0	0.5	0	0	0	0	38.5	7.77
163.07	164.59	1.26	14	9	3.5	3.5	2.5	1.5	0	1	1	0	0	0	0	0	0	0	62	11.00
164.59	166.12	1.23	16	7.5	2	0.5	0	0	0	0	0.5	0	0	0	0	0	0	0	18	3.27
166.12	167.64	1.19	13	6.5	2	0	0.5	0	0.5	1.5	0.5	0.5	0	0	0	0	0	0	38.5	7.27
167.64	169.16	1.36	15	15	5	2	1.5	1	0	0	0	0	0	0	0	0	0	0	42	6.95
169.16	170.69	1.23	7	6	1.5	2.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	22	4.00
170.69	172.21	1.04	5	9	4.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	25.5	5.52
172.21	173.74	1.01	7	2.5	3.5	2.5	1	0	0.5	1.5	0.5	0	0	0	0	0	0	0	41	9.15
173.74	175.26	1.13	12	4	2	1	1	1	1	0.5	0	1	0	0	0	0	0	0	42	8.36
175.26	176.78	1.26	16	7.5	3	1	1	0.5	0	0	0	0	0	0	0	0	0	0	23	4.08
176.78	178.31	1.25	15	8	5	2	2	1	0	1	0.5	0.5	0	0	0	0	0	0	56	10.06
178.31	179.83	1.20	11	6	6	2	1.5	0	1	2	0.5	0	0	0	0	0	0	0	57	10.63
179.83	181.36	1.43	17	10	4	2	1.5	0.5	2	1	0	0	0	0	0	0	0	0	52.5	8.23
181.36	182.88	1.43	20	10	5	2.5	1.5	1	1	0	0.5	0	0	0	0	0	0	0	49.5	7.76
182.88	184.40	1.45	18	6	3.5	1.5	1.5	1	2	0	0	0	0	0	0	0	0	0	40.5	6.28
184.40	185.93	1.39	17	6	4.5	2.5	2	1	1	2.5	0	0	0	0	0	0	0	0	61.5	9.95
185.93	187.45	1.34	18	4	0.5	1	0.5	1.5	2	0	0	0	0	0	0	0	0	0	29.5	4.94
187.45	188.98	1.16	13	8.5	2.5	1.5	1	0.5	1	1	0	0	0	0	0	0	0	0	38.5	7.46
188.98	190.50	1.19	5	7	0.5	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	21	3.97
190.50	192.02	1.19	5	8	1	3	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	30.5	5.76
192.02	193.55	1.17	11	6.5	1.5	3.5	0.5	0	0	0	0.5	0	0	0	0.5	0	0	0	36	6.89
193.55	195.07	1.23	15	5	3.5	1	3	1	0	0	0	0	0	0	0	0	0	0	32	5.82
195.07	196.60	1.26	5	6.5	2.5	2.5	1	1	0	0.5	0	0	0	0	0	0	0	0	32	5.68
196.60	198.12	1.08	5	6.5	2.5	0	1	1	1	0	0	0	0	0	0	0	0	0	26.5	5.50
198.12	199.64	0.98	5	4	1	2.5	1	0	0	0	0	0	0	0	0	0	0	0	17.5	4.03
199.64	201.17	1.08	5	8	5	2.5	1.5	2	0	1	0	0	0	0	0	0	0	0	49.5	10.27
201.17	202.69	1.22	5	7	4	2	1.5	0	0	0	0	0	0	0	0	0	0	0	27	4.97
202.69	204.22	1.20	13	6.5	2.5	2	1	0.5	1	0	0	0	0	0	0	0	0	0	30	5.59
204.22	205.74	1.33	15	7.5	4.5	0	3.5	1	1.5	1.5	0	0	0	0	0	0	0	0	56.5	9.57
205.74	207.26	1.26	10	9.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	17.5	3.11
207.26	208.79	1.16	5	5.5	3	0.5	2.5	1	0.5	0	0	0	0	0	0	0	0	0	31	6.01
208.79	210.31	1.34	14	7.5	3.5	2	1.5	2	0.5	1	0	0	0	0	0	0	0	0	47.5	7.95
210.31	211.84	1.33	15	8.5	3.5	1	0.5	1.5	1.5	1.5	0	0	0	0.5	0.5	0	0	0	66	11.17
211.84	213.36	1.13	14	4.5	2	0.5	0.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	26.5	5.27
213.36	214.88	1.05	13	2	1	1.5	0.5	1	1.5	0.5	0	0.5	0	0	0	0	0	0	34.5	7.37
214.88	216.41	1.34	16	10	2	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	18.5	3.10
216.41	217.93	1.20	12	9	3.5	2.5	1.5	2.5	0	0	0	0	0	0	0	0	0	0	42	7.83
217.93	219.46	1.05	11	6	4	1	1.5	0	1	1.5	0.5	0	0	0	0	0	0	0	46	9.82
219.46	220.98	1.17	14	9.5	4	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	29.5	5.64
220.98	222.50	1.33	12	13.5	6	3	2	1	1	0	0	0	0	0	0	0	0	0	53.5	9.06
222.50	224.03	1.05	11	9.5	2.5	1	2	0.5	1	0	0	0	0	0	0	0	0	0	34	7.26
224.03	225.55	1.17	5	7	1	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.97
225.55	227.08	1.07	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
227.08	228.60	1.36	5	2.5	0	0	0	0	0.5	0	0	0	0	0	0	0	0	0	5.5	0.91
228.60	230.12	1.19	13	5.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.23
230.12	231.65	1.26	18	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.62
231.65	233.17	1.30	13	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.43
233.17	234.70	1.37	15	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
234.70	236.22	1.14	13	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.29
236.22	237.74	1.31	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
237.74	239.27	1.23	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
239.27	240.79	1.23	15	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.64
240.79	242.32	1.37	16	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.74
242.32	243.84	1.37	15	6.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.72

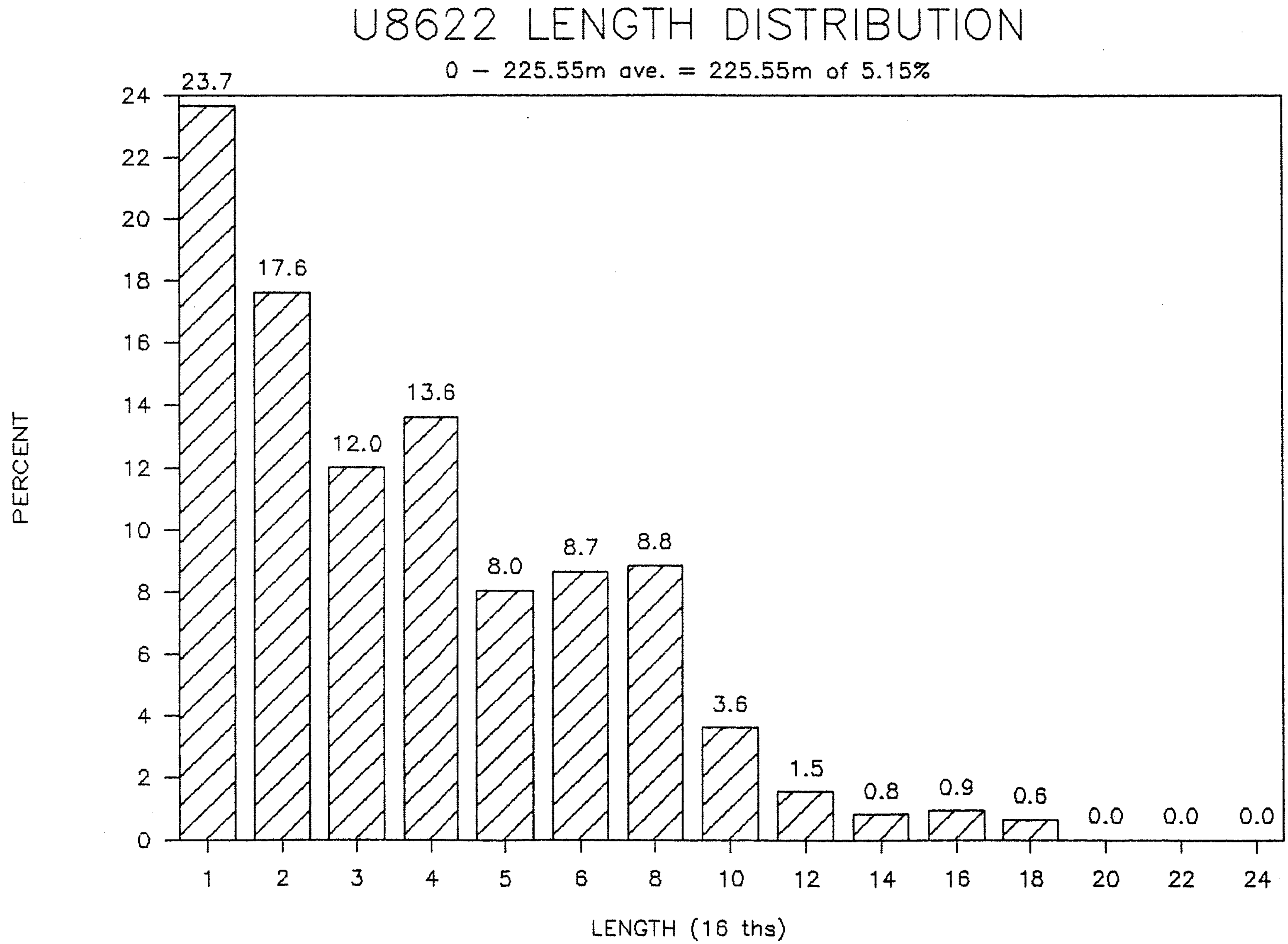
243.84	245.36	1.28	5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.35
245.36	246.89	1.36	10	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
246.89	248.41	1.40	17	6	1	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.28
248.41	249.94	1.40	8	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.80
249.94	251.46	1.23	7	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.82
251.46	252.98	1.10	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
252.98	254.51	1.10	11	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
254.51	256.03	1.36	13	5.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.08
256.03	257.56	1.17	12	7.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.43
257.56	259.08	1.02	12	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.88
259.08	260.60	1.07	5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.42
260.60	262.13	1.20	11	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.84
262.13	263.65	1.34	14	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.84
263.65	265.18	1.43	15	5.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.86
265.18	266.70	1.36	17	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.83
266.70	268.22	1.26	11	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.44
268.22	269.75	1.08	11	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.73
269.75	271.27	1.20	12	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.19
271.27	272.80	1.48	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
272.80	273.71	0.90	18	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.25
	EOH																			

U8622 CCRG

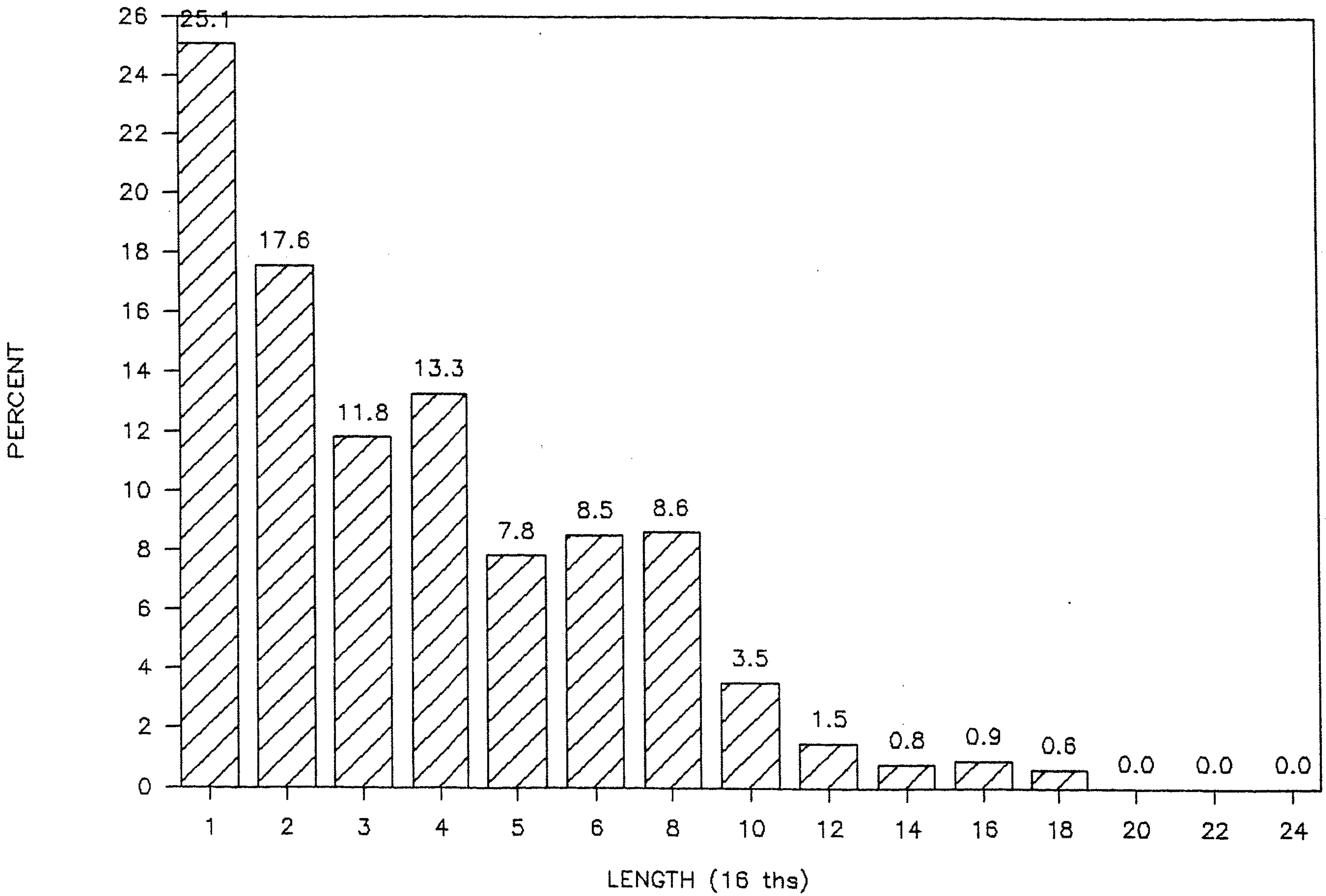


12
11
10
9
8
7
6
5
4
3
2
1
0
CCRG (%)
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
245.36
METERAGE


U8622 RMR
RMR
METERAGE
50
40
30
20
10
0
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
245.36


U8622 LENGTH DISTRIBUTION
0 – 225.55m ave. = 225.55m of 5.15%
PERCENT
LENGTH (16 ths)
24
22
20
18
16
14
12
10
8
6
4
2
0
23.7
17.6
12.0
13.6
8.0
8.7
8.8
3.6
1.5
0.8
0.9
0.6
0.0
0.0
0.0
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24

U8622 LENGTH DISTRIBUTION



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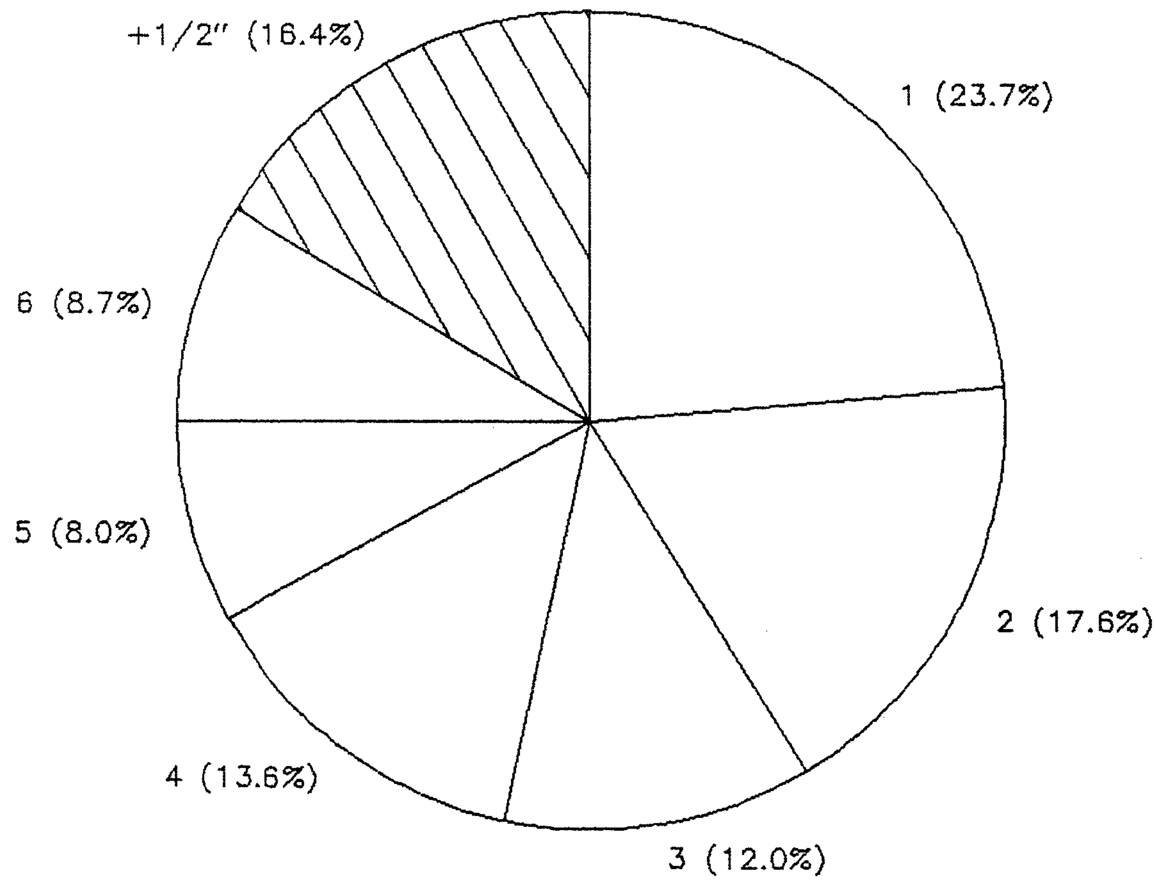

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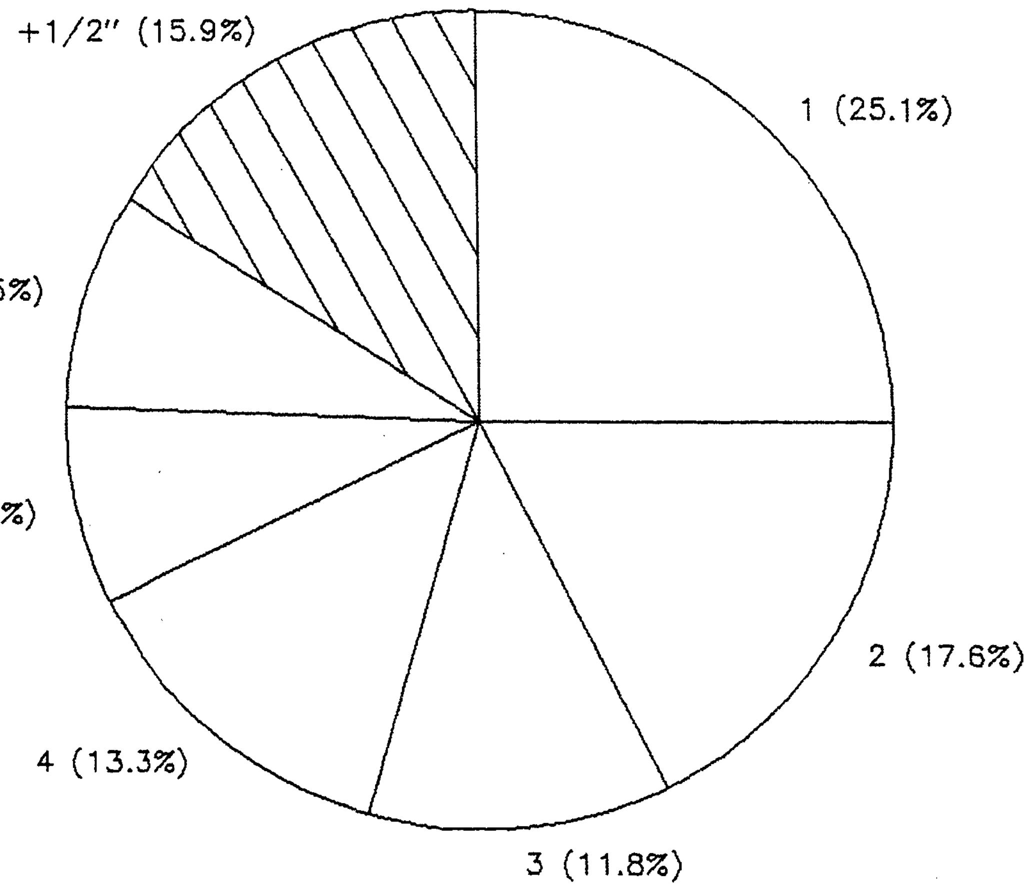


FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME	HOLE	U86-23	DEPTH	103.63 m
AZIMUTH	$89^{\circ}55^{\circ}$	INCLINATION	-60°	SECTION	6706N
LATITUDE	6711.75N	DEPARTURE	7713.4E	ELEVATION	1415.4 m
STARTED	Nov. 28	FINISHED	Dec. 1	LOGGED	by I.Lyn date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
3.7	19.8		Serpentinite, dark green, talcy, sparse fibre, lizardite stringers	
19.8	29.5		Gradual change to medium dark green, mottled, fibre bearing	
29.5	47.7		Dark green, minor to sparse fibre	
47.7	50.6		Fault zone, intensly sheared and gouge	
50.6	82.3		Medium dark green, fibre bearing	
			74.5 - 75.3 minor fault	
82.3	103.6		Gradual change to minor fibre, dark green, sheared texture, lizardite on joints, talcy	
			Fault zone 88.4 - 91.4 gouge with talcy lizardite	
103.6			E.O.H. Rods broke, hole caved	

DDH U 8623

EAST: AZ: 90
NORTH: INCL: -60
ELEV: DEPTH:103.6

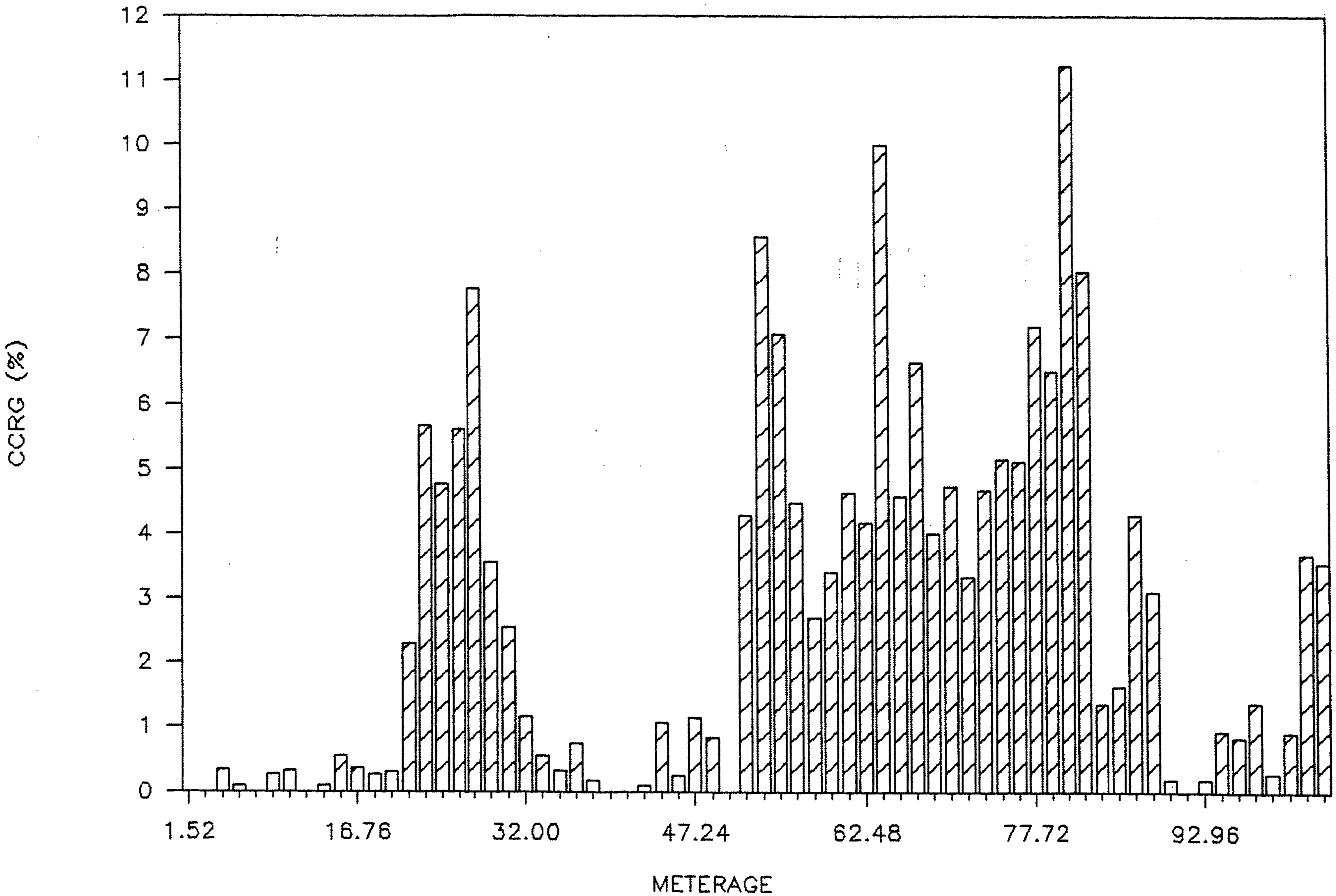
AVERAGE OF TWO COUNTS
Number of fibre veins counted per 16th category

FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CORG %
0.00	1.52	0.00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
1.52	3.05	0.00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
3.05	4.57	0.67	10	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.33
4.57	6.10	1.31	16	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
6.10	7.62	1.16	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
7.62	9.14	1.28	16	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
9.14	10.67	1.45	23	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.31
10.67	12.19	1.26	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
12.19	13.72	1.17	16	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
13.72	15.24	1.43	24	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.55
15.24	16.76	1.28	15	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.35
16.76	18.29	1.30	24	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
18.29	19.81	1.49	31	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.30
19.81	21.34	1.33	29	8	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	13.5	2.29
21.34	22.86	1.46	23	10	4.5	0	0.5	2	1	0	0	0	0	0	0	0	0	0	37	5.68
22.86	24.38	1.51	29	11.5	3.5	1.5	0	1	0	0.5	0	0	0	0	0	0	0	0	32	4.76
24.38	25.91	1.48	29	12.5	6.5	0.5	1	0	1	0	0	0	0	0	0	0	0	0	37	5.62
25.91	27.43	1.39	26	10	2.5	0.5	1.5	1.5	1	0	0	1	0	0	0	0	0	0	48	7.77
27.43	28.96	1.45	19	6	1	0	0.5	1	0.5	0	0.5	0	0	0	0	0	0	0	23	3.57
28.96	30.48	1.42	21	7.5	1.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	16	2.53
30.48	32.00	1.26	20	4.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.15
32.00	33.53	1.23	9	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.55
33.53	35.05	1.45	17	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.31
35.05	36.58	1.52	32	3	1	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.74
36.58	38.10	1.43	16	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
38.10	39.62	1.34	21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
39.62	41.15	1.37	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
41.15	42.67	1.40	18	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
42.67	44.20	1.37	26	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	6.5	1.06
44.20	45.72	1.40	22	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.24
45.72	47.24	1.39	16	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.13
47.24	48.77	1.34	10	2	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	5	0.84
48.77	50.29	1.16	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
50.29	51.82	1.28	10	5	3.5	1.5	0	1	0.5	0	0	0	0	0	0	0	0	0	24.5	4.30
51.82	53.34	1.30	15	4	4	0.5	2	1	1	1.5	0.5	0	0	0	0	0	0	0	49.5	8.58
53.34	54.86	1.22	17	8.5	3.5	1.5	1	0.5	2	0	0	0	0	0	0	0	0	0	38.5	7.09
54.86	56.39	1.48	21	4.5	0.5	2.5	2	0.5	1	0	0	0	0	0	0	0	0	0	29.5	4.48
56.39	57.91	1.42	21	9	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	17	2.69
57.91	59.44	1.42	20	8	3.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	21.5	3.41
59.44	60.96	1.36	20	12	3	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	25	4.60
60.96	62.48	1.48	21	5.5	1	1	1.5	1	1	0	0	0	0	0	0	0	0	0	27.5	4.18
62.48	64.01	1.45	31	6.5	3.5	1.5	2.5	0.5	1	1	0	1	0	0.5	0	0	0	0	64.5	10.00
64.01	65.53	1.33	26	10	1.5	0.5	1	0.5	1	0	0	0	0	0	0	0	0	0	27	4.57
65.53	67.06	1.42	17	6	3	1	1.5	2	0.5	1	0	0	0	0	0	0	0	0	42	6.65
67.06	68.58	1.43	19	3	1.5	0	1	1.5	0.5	0	0	0	0	0	0	0	0	0	25.5	4.00
68.58	70.10	1.40	19	8	3.5	0.5	2.5	0	0.5	0	0	0	0	0	0	0	0	0	29.5	4.72
70.10	71.63	1.28	16	6	1.5	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	19	3.32
71.63	73.15	1.42	17	10.5	4.5	0.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	29.5	4.67

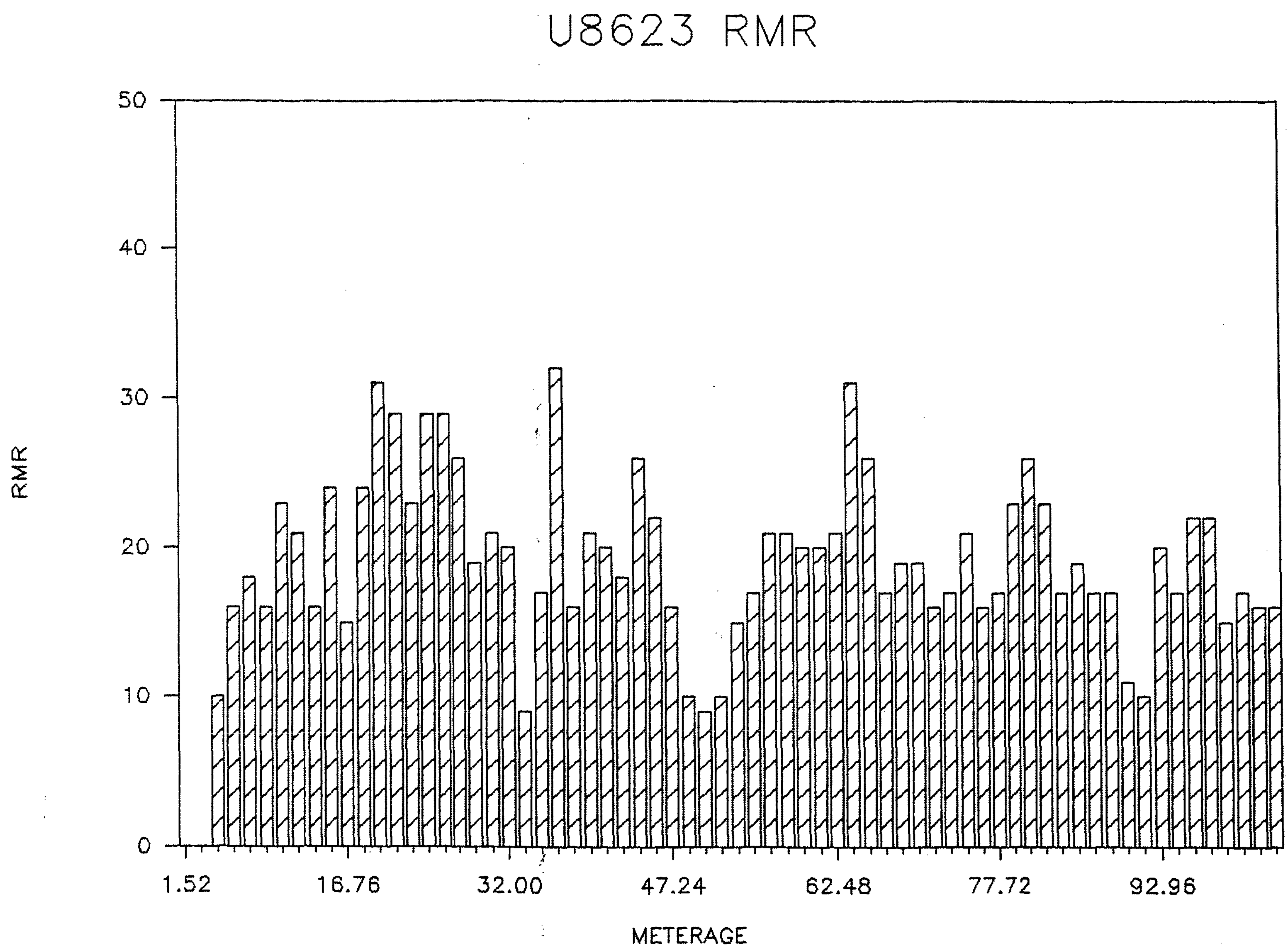
73.15	74.68	1.37	21	12.5	5	2	0	0	0.5	0	0	0	0	0	0	0	0	0	31.5	5.16
74.68	76.20	1.30	16	7.5	3	1	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	29.5	5.11
76.20	77.72	1.37	17	16	3	0	0	1	0.5	0.5	1	0	0	0	0	0	0	0	44	7.20
77.72	79.25	1.43	23	15	5	2.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	41.5	6.50
79.25	80.77	1.51	26	15	6	4.5	5.5	0	1.5	0.5	0	0	0	0	0	0	0	0	75.5	11.23
80.77	82.30	1.48	23	14.5	6	3	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	53	8.05
82.30	83.82	1.33	17	6	1	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.35
83.82	85.34	1.31	19	4.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	9.5	1.63
85.34	86.87	1.46	17	13	5	1	0.3	0	0	0	0	0	0	0	0	0	0	0	28	4.30
86.87	88.39	1.34	17	8	3	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	18.5	3.10
88.39	89.92	1.30	11	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
89.92	91.44	1.16	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
91.44	92.96	1.26	20	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
92.96	94.49	1.33	17	4	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.93
94.49	96.01	1.36	22	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.83
96.01	97.54	1.31	22	5.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8	1.37
97.54	99.06	1.22	13	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.28
99.06	100.58	1.36	17	3.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	5.5	0.91
100.58	102.11	1.43	16	10.5	4.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	23.5	3.68
102.11	103.63	1.26	16	8	2	2	0.5	0	0	0	0	0	0	0	0	0	0	0	20	3.55

EOH

U8623 CCRG



CCRG (%)
0
1
2
3
4
5
6
7
8
9
10
11
12
1.52
16.76
32.00
47.24
62.48
77.72
92.96
METERAGE


U8623 RMR
RMR
METERAGE
50
40
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20
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16.76
32.00
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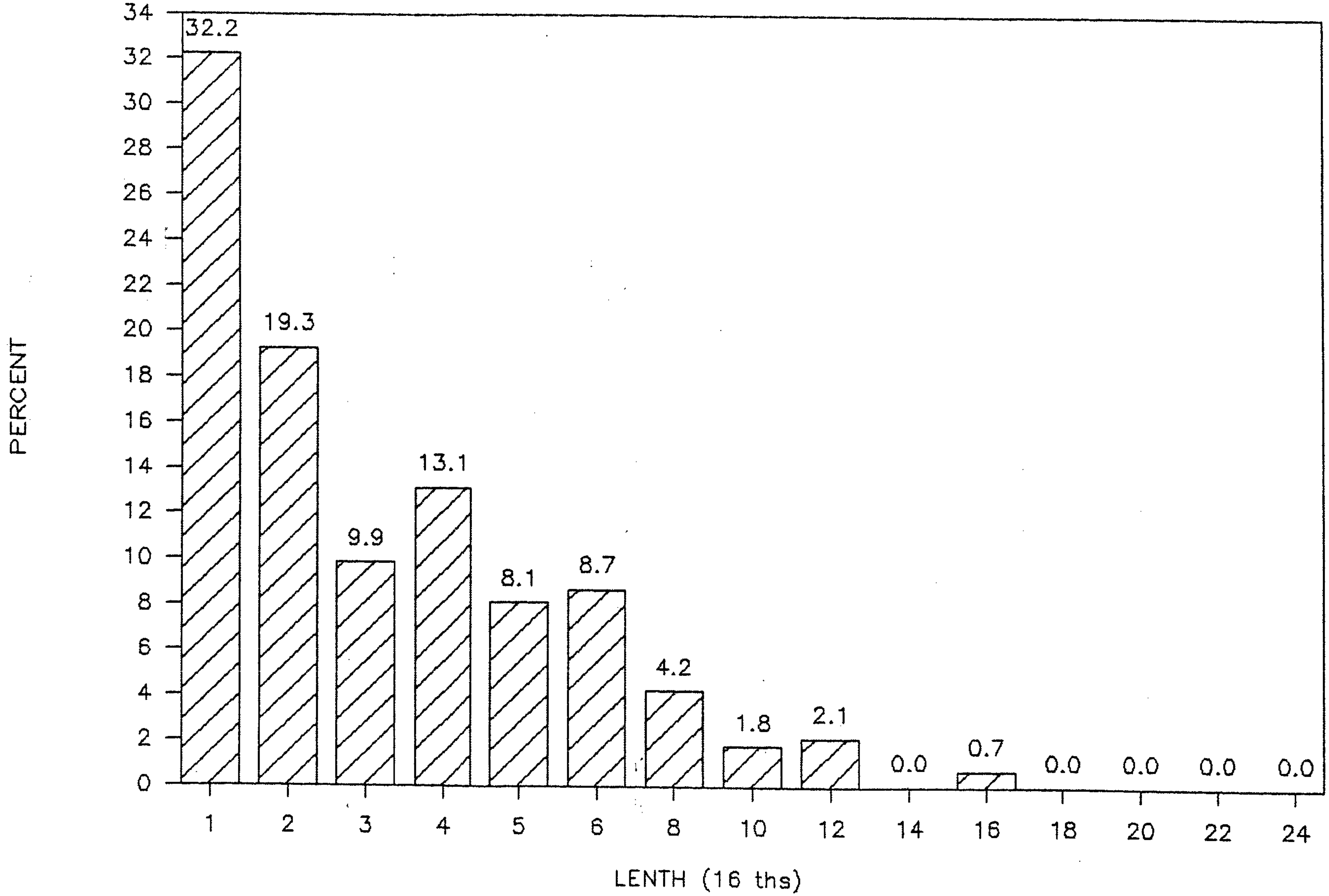
77.72
92.96

U8623 LENGTH DISTRIBUTION



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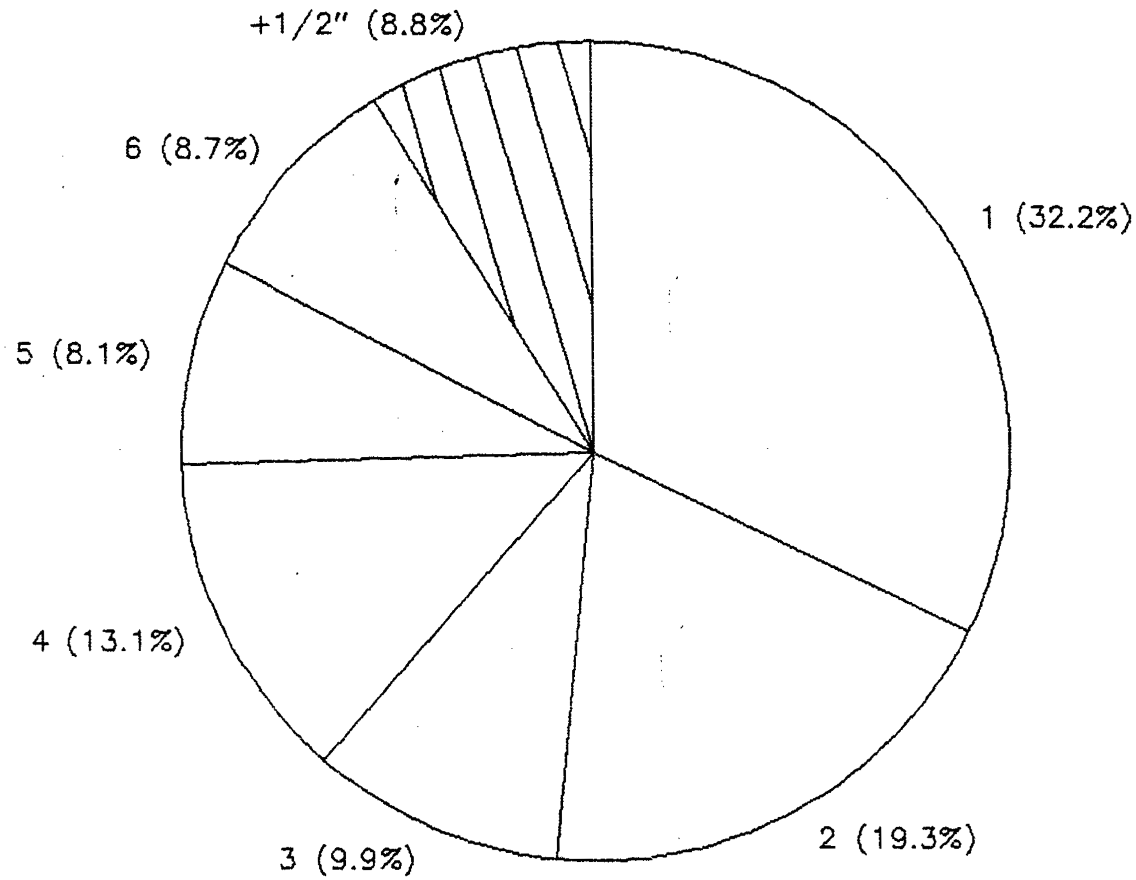


FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME
HOLE	U86-24
DEPTH	286.21
AZIMUTH	86.67°
INCLINATION	-55°
SECTION	6707N
LATITUDE	6711.750N
DEPARTURE	7713.50E
ELEVATION	1415.40 m
STARTED	Dec. 1
FINISHED	Dec. 11
LOGGED by	I. Lyn
date	

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
2.1	16.8		Serpentinite, dark green, sparse fibre, lizardite stringers	
			Fault zone 2.1 - 6.4, minor fault 12.8 - 16.5	
16.8	125.9		Medium dark green, mottled, minor fibre	
			Fault zones 55.17 - 59.3, less faulted 59.3 - 64, talcy	
			Faults 96.6 - 97.5	
125.9	137.2		Dark green, deformed, fault 125.9 - 133.8, minor fibre	
137.2	286.2		Medium green, mottled, minor fibre to 143 then better, minor	
			fibre below 174, sparse below 182	
			Fault zone 181.4 - 182.3, 192 - 195	
			Fibre bearing again below 197, occasional lizardite - magnetite	
			veins.	
			Fault zone 234 - 238	
			259.4 Reduce HQ to NQ. Fibre becoming sparse.	
			Fault zones 265.8 - 268.2 gouge and cleaved, talc + lizardite	
			274.6 - 275.8, 278.3 - 280.4	
286.2			E.O.H.	

DDH U 8624

EAST: AZ:
NORTH: INCL:
ELEV: DEPTH:286.2

AVERAGE OF TWO COUNTS
Number of fibre veins counted per 16th category

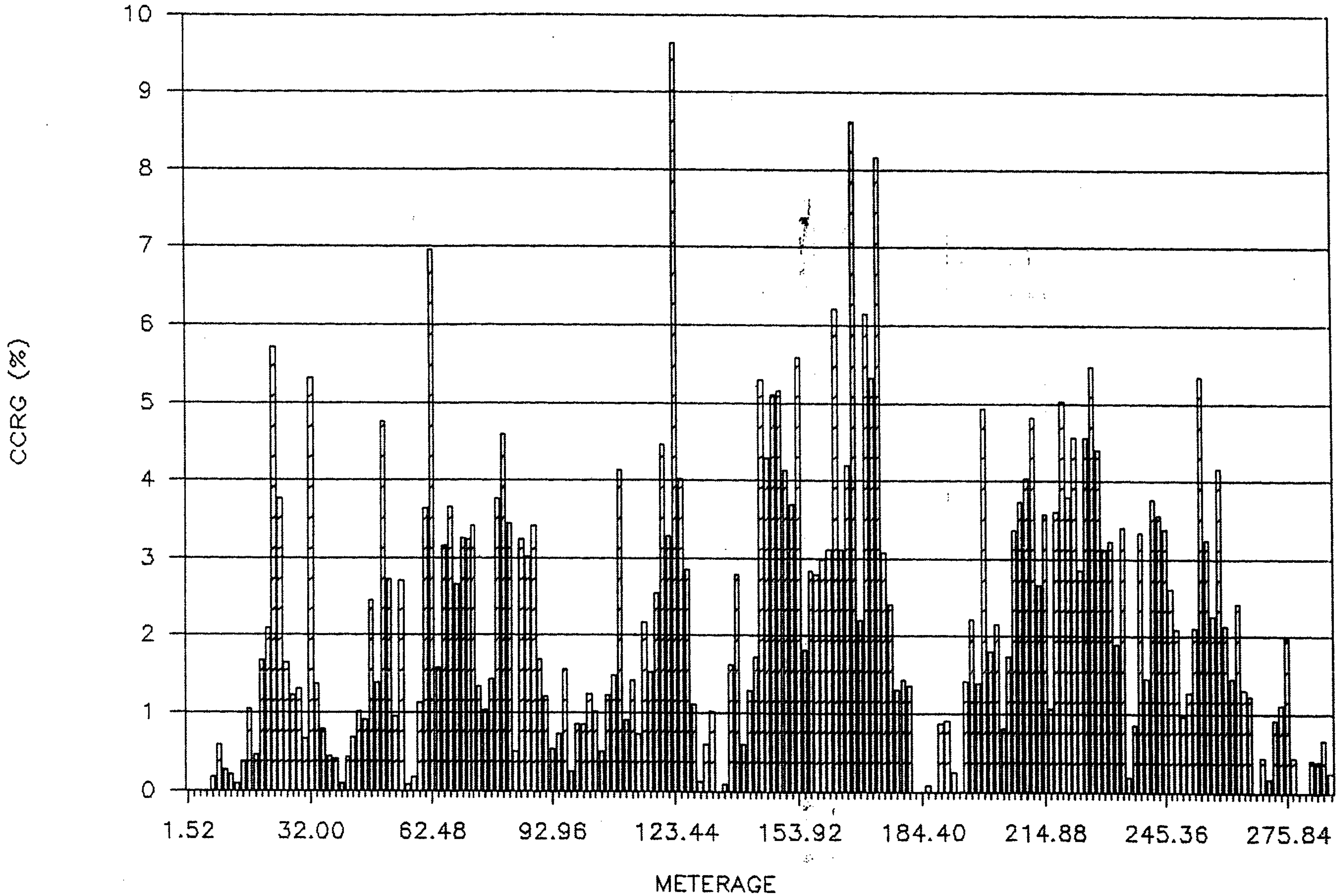
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	TOTAL 16's	CORG %
0.00	1.52	0.00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	ERR
1.52	3.05	0.26	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
3.05	4.57	0.38	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
4.57	6.10	0.87	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
6.10	7.62	1.34	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
7.62	9.14	0.96	16	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.58
9.14	10.67	1.26	30	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.27
10.67	12.19	1.13	22	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.20
12.19	13.72	1.36	18	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
13.72	15.24	0.91	9	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.37
15.24	16.76	1.08	10	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5	1.04
16.76	18.29	1.49	23	3	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.45
18.29	19.81	1.42	28	5	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	10.5	1.66
19.81	21.34	1.40	30	8	1	0	0	0	0.5	0	0	0	0	0	0	0	0	13	2.08
21.34	22.86	1.22	23	8	3	2	0.5	0	1.5	0	0	0	0	0	0	0	0	31	5.71
22.86	24.38	1.31	26	11	2	1	1	0	0	0	0	0	0	0	0	0	0	22	3.77
24.38	25.91	1.23	21	4	0	1	0.5	0	0	0	0	0	0	0	0	0	0	9	1.64
25.91	27.43	1.28	19	5	1	0	0	0	0	0	0	0	0	0	0	0	0	7	1.23
27.43	28.96	1.37	22	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8	1.31
28.96	30.48	1.34	22	1	1.5	0	0	0	0	0	0	0	0	0	0	0	0	4	0.67
30.48	32.00	1.48	28	8	3	2.5	2	0.5	0.5	0	0	0	0	0	0	0	0	35	5.31
32.00	33.53	1.40	24	6.5	1	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.36
33.53	35.05	1.42	26	5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.79
35.05	36.58	1.51	28	3	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.45
36.58	38.10	1.36	26	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
38.10	39.62	1.33	15	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
39.62	41.15	1.33	17	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.42
41.15	42.67	1.33	16	4	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.68
42.67	44.20	1.33	18	3	1.5	0	0	0	0	0	0	0	0	0	0	0	0	6	1.02
44.20	45.72	1.36	18	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.91
45.72	47.24	1.37	19	7	1	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	15	2.46
47.24	48.77	1.39	19	6.5	1	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.38
48.77	50.29	1.37	27	13.5	3.5	1	0	0.5	0.5	0	0	0	0	0	0	0	0	29	4.75
50.29	51.82	1.36	24	7	2.5	1.5	0	0	0	0	0	0	0	0	0	0	0	16.5	2.73
51.82	53.34	1.30	17	3	0	0	0	0.5	0	0	0	0	0	0	0	0	0	5.5	0.95
53.34	54.86	1.37	18	5.5	1.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	16.5	2.70
54.86	56.39	1.40	13	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
56.39	57.91	1.34	12	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
57.91	59.44	1.39	13	3.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	7	1.13
59.44	60.96	1.23	11	8	2.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	20	3.64
60.96	62.48	1.10	15	10	2	0.5	2.5	0.5	1	0	0	0	0	0	0	0	0	34	6.96
62.48	64.01	1.49	10	5	1.5	0	0	0.5	0	0	0	0	0	0	0	0	0	10.5	1.58
64.01	65.53	1.39	17	3	1.5	1.5	1	0	0.5	0	0	0	0	0	0	0	0	19.5	3.16
65.53	67.06	1.48	24	6	3	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	24	3.64
67.06	68.58	1.22	22	5	2.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	14.5	2.67
68.58	70.10	1.45	20	11	3	0	0	0	0	0.5	0	0	0	0	0	0	0	21	3.26
70.10	71.63	1.39	23	10.5	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	20	3.24
71.63	73.15	1.05	12	4	1.5	0	0	0	1.5	0	0	0	0	0	0	0	0	16	3.42

73.15	74.68	1.43	16	6.5	1	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.33
74.68	76.20	1.31	16	4.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	6	1.03
76.20	77.72	1.49	30	6	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	9.5	1.43
77.72	79.25	1.40	35	11.5	1.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	23.5	3.76
79.25	80.77	1.46	29	8.5	3	1.5	1	0	0.5	0.5	0	0	0	0	0	0	0	30	4.60
80.77	82.30	1.40	35	10.5	1.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	21.5	3.44
82.30	83.82	1.34	25	3	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.50
83.82	85.34	1.52	26	9	2.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	22	3.24
85.34	86.87	1.49	31	8.5	1.5	0.5	1	0	0.5	0	0	0	0	0	0	0	0	20	3.01
86.87	88.39	1.48	32	12.5	1	0	0.5	0	1	0	0	0	0	0	0	0	0	22.5	3.42
88.39	89.92	1.46	28	7	0.5	1	0	0	0	0	0	0	0	0	0	0	0	11	1.69
89.92	91.44	1.39	28	3.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	7.5	1.21
91.44	92.96	1.46	31	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.54
92.96	94.49	1.39	26	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.73
94.49	96.01	1.30	22	4	2.5	0	0	0	0	0	0	0	0	0	0	0	0	9	1.56
96.01	97.54	1.36	17	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
97.54	99.06	1.45	22	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.85
99.06	100.58	1.45	23	4	0	0.5	0	0	0	0	0	0	0	0	0	0	0	5.5	0.85
100.58	102.11	1.45	28	7	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8	1.24
102.11	103.63	1.22	21	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.01
103.63	105.16	1.31	21	3	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.51
105.16	106.68	1.46	21	5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	6	1.23
106.68	108.20	1.30	11	7.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.47
108.20	109.73	1.52	31	6.5	3.5	1.5	0.5	1	0.5	0	0	0	0	0	0	0	0	28	4.12
109.73	111.25	1.36	19	2.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	5.5	0.91
111.25	112.78	1.26	22	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	8	1.42
112.78	114.30	1.23	21	2	1	0	0	0	0	0	0	0	0	0	0	0	0	4	0.73
114.30	115.82	1.45	26	8	2	0	0.5	0	0	0	0	0	0	0	0	0	0	14	2.17
115.82	117.35	1.40	20	6	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	9.5	1.52
117.35	118.87	1.28	16	9.5	1	0	0	0	0.5	0	0	0	0	0	0	0	0	14.5	2.54
118.87	120.40	1.36	21	9	2.5	0	1.5	0	0.5	0.5	0	0	0	0	0	0	0	27	4.47
120.40	121.92	1.30	14	9.5	1.5	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	19	3.29
121.92	123.44	1.34	22	10.5	5	3	1	1	1.5	0	1	0	0	0	0	0	0	57.5	9.62
123.44	124.97	1.17	16	10	2.5	1	0	0	0.5	0	0	0	0	0	0	0	0	21	4.02
124.97	126.49	1.34	17	5.5	1.5	1.5	1	0	0	0	0	0	0	0	0	0	0	17	2.85
126.49	128.02	1.20	14	3	0	0	0	0	0.5	0	0	0	0	0	0	0	0	6	1.12
128.02	129.54	0.98	16	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.12
129.54	131.06	0.93	9	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.60
131.06	132.59	0.99	8	2.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	4.5	1.02
132.59	134.11	1.13	15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
134.11	135.64	1.25	18	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
135.64	137.16	1.31	20	8	0	0.5	0	0	0	0	0	0	0	0	0	0	0	9.5	1.63
137.16	138.68	1.33	22	6	1.5	0	0.5	0.5	0.5	0	0	0	0	0	0	0	0	16.5	2.79
138.68	140.21	1.31	20	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.60
140.21	141.73	1.40	24	4	0.5	1	0	0	0	0	0	0	0	0	0	0	0	8	1.28
141.73	143.26	1.37	20	6	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	1.72
143.26	144.78	1.42	24	10.5	4	0	0.5	1	0	1	0	0	0	0	0	0	0	33.5	5.31
144.78	146.30	1.46	17	9.5	2.5	1.5	1	1	0	0	0	0	0	0	0	0	0	28	4.30
146.30	147.83	1.49	23	6	2	0	2.5	0	0	0.5	1	0	0	0	0	0	0	34	5.11
147.83	149.35	1.42	26	11.5	4	1.5	1.5	0.5	0	0	0	0	0	0	0	0	0	32.5	5.15
149.35	150.88	1.39	16	4	1.5	1.5	1	0	0	0	1	0	0	0	0	0	0	25.5	4.13
150.88	152.40	1.37	22	7	2	0.5	0.5	1	0.5	0	0	0	0	0	0	0	0	22.5	3.68
152.40	153.92	1.45	19	4	3.5	2	2	0	0.5	1	0	0	0	0	0	0	0	36	5.58
153.92	155.45	1.45	21	8	0.5	1	0	0	0	0	0	0	0	0	0	0	0	12	1.82
155.45	156.97	1.39	20	7.5	2.5	0	0	1	0	0	0	0	0	0	0	0	0	17.5	2.83
156.97	158.50	1.45	23	5.5	4	1.5	0	0	0	0	0	0	0	0	0	0	0	18	2.79

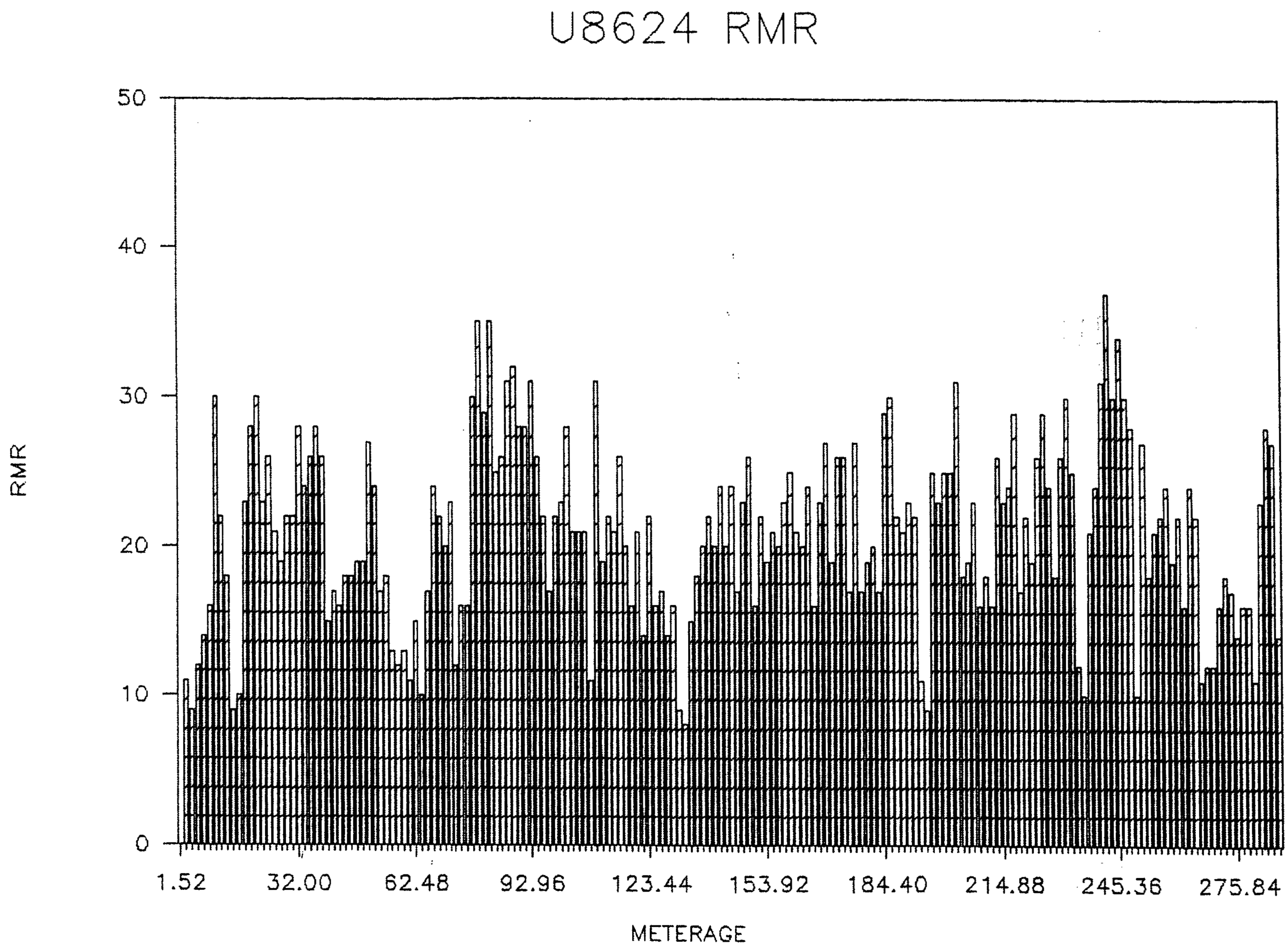
158.50	160.02	1.43	25	9	1.5	0	0	0	0.5	0.5	0	0	0	0	0	0	0	19	2.98
160.02	161.54	1.37	21	5	2	0	0.5	1	0.5	0	0	0	0	0	0	0	0	19	3.11
161.54	163.07	1.46	20	10	5.5	1.5	1	0	0	0	0.5	0.5	0	0	0	0	0	40.5	6.21
163.07	164.59	1.48	24	4	1	0.5	0.5	1	1	0	0	0	0	0	0	0	0	20.5	3.11
164.59	166.12	1.42	16	7	1	1	1	0.5	0	1	0	0	0	0	0	0	0	26.5	4.20
166.12	167.64	1.43	23	5.5	4	1	1	0.5	1.5	0	0.5	0	0	0	1	0	0	55	8.62
167.64	169.16	1.49	27	5.5	0.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	14.5	2.20
169.16	170.69	1.30	19	7	1.5	0	0	0.5	1	0.5	0.5	0	0	0.5	0	0	0	35.5	6.15
170.69	172.21	1.43	26	10	4	0.5	1	0.5	0	1	0	0	0	0	0	0	0	34	5.33
172.21	173.74	1.40	26	6.5	1.5	1	1	0.5	2	1	0.5	0	0.5	0	0	0	0	51	8.17
173.74	175.26	1.39	17	9.5	1.5	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	19	3.08
175.26	176.78	1.49	27	5	1	0	0.5	0	0.5	0.5	0	0	0	0	0	0	0	16	2.40
176.78	178.31	1.37	17	4	2	0	0	0	0	0	0	0	0	0	0	0	0	8	1.31
178.31	179.83	1.40	19	5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	9	1.44
179.83	181.36	1.42	20	6.5	1	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.35
181.36	182.88	1.37	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
182.88	184.40	1.34	29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
184.40	185.93	1.51	30	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.07
185.93	187.45	1.37	22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
187.45	188.98	1.28	21	3	1	0	0	0	0	0	0	0	0	0	0	0	0	5	0.88
188.98	190.50	1.36	23	5.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.91
190.50	192.02	1.37	22	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
192.02	193.55	1.14	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
193.55	195.07	1.04	9	3.5	0	1	0	0	0	0	0	0	0	0	0	0	0	6.5	1.41
195.07	196.60	1.37	25	4.5	0.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	13.5	2.21
196.60	198.12	1.22	23	3	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	7.5	1.38
198.12	199.64	1.48	25	7	3	3	2	0.5	0	0	0	0	0	0	0	0	0	32.5	4.94
199.64	201.17	1.37	25	8	1.5	0	0	0	0	0	0	0	0	0	0	0	0	11	1.80
201.17	202.69	1.51	31	6.5	2.5	1	0	0	0	0	0	0	0	0	0	0	0	14.5	2.16
202.69	204.22	1.25	18	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.81
204.22	205.74	1.30	19	6.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	10	1.73
205.74	207.26	1.40	23	8.5	3	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	21	3.36
207.26	208.79	1.36	16	9	2.5	0.5	0.5	1	0	0	0	0	0	0	0	0	0	22.5	3.72
208.79	210.31	1.14	18	3	2	1.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	20.5	4.03
210.31	211.84	1.28	16	6	3	0.5	0.5	1	0.5	0.5	0	0	0	0	0	0	0	27.5	4.82
211.84	213.36	1.43	26	6	3	1	0.5	0	0	0	0	0	0	0	0	0	0	17	2.66
213.36	214.88	1.51	23	12	0.5	2	0.5	0	0.5	0	0	0	0	0	0	0	0	24	3.57
214.88	216.41	1.48	24	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7	1.06
216.41	217.93	1.52	29	8	1.5	0.5	1	1	0.5	0	0	0	0	0	0	0	0	24.5	3.61
217.93	219.46	1.30	17	13	2	2	1.5	0	0	0	0	0	0	0	0	0	0	29	5.03
219.46	220.98	1.45	22	11.5	2	0	1	0	0	0	0.5	0	0	0	0	0	0	24.5	3.80
220.98	222.50	1.28	19	6	3	0.5	1	0.5	1	0	0	0	0	0	0	0	0	26	4.56
222.50	224.03	1.49	26	8	3.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	19	2.86
224.03	225.55	1.48	29	12	3	1	0	1	0	0.5	0	0	0	0	0	0	0	30	4.56
225.55	227.08	1.42	24	8.5	3	1.5	1	0.5	1.5	0	0	0	0	0	0	0	0	34.5	5.46
227.08	228.60	1.33	18	6.5	4.5	0.5	0	1	0	0.5	0	0	0	0	0	0	0	26	4.40
228.60	230.12	1.22	26	6.5	1	0	1.5	0.5	0	0	0	0	0	0	0	0	0	17	3.13
230.12	231.65	1.43	30	7	4	0.5	1	0	0	0	0	0	0	0	0	0	0	20.5	3.21
231.65	233.17	1.42	25	10	1	0	0	0	0	0	0	0	0	0	0	0	0	12	1.90
233.17	234.70	1.36	12	8	3	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	20.5	3.39
234.70	236.22	1.22	10	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
236.22	237.74	1.17	21	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.86
237.74	239.27	1.42	24	8	0.5	1.5	0	1.5	0	0	0	0	0	0	0	0	0	21	3.33
239.27	240.79	1.48	31	7.5	1	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.44
240.79	242.32	1.52	37	8	4	1	0	0.5	0	0.5	0	0	0	0	0	0	0	25.5	3.76
242.32	243.84	1.42	30	7	2	1.5	1	0	0.5	0	0	0	0	0	0	0	0	22.5	3.56

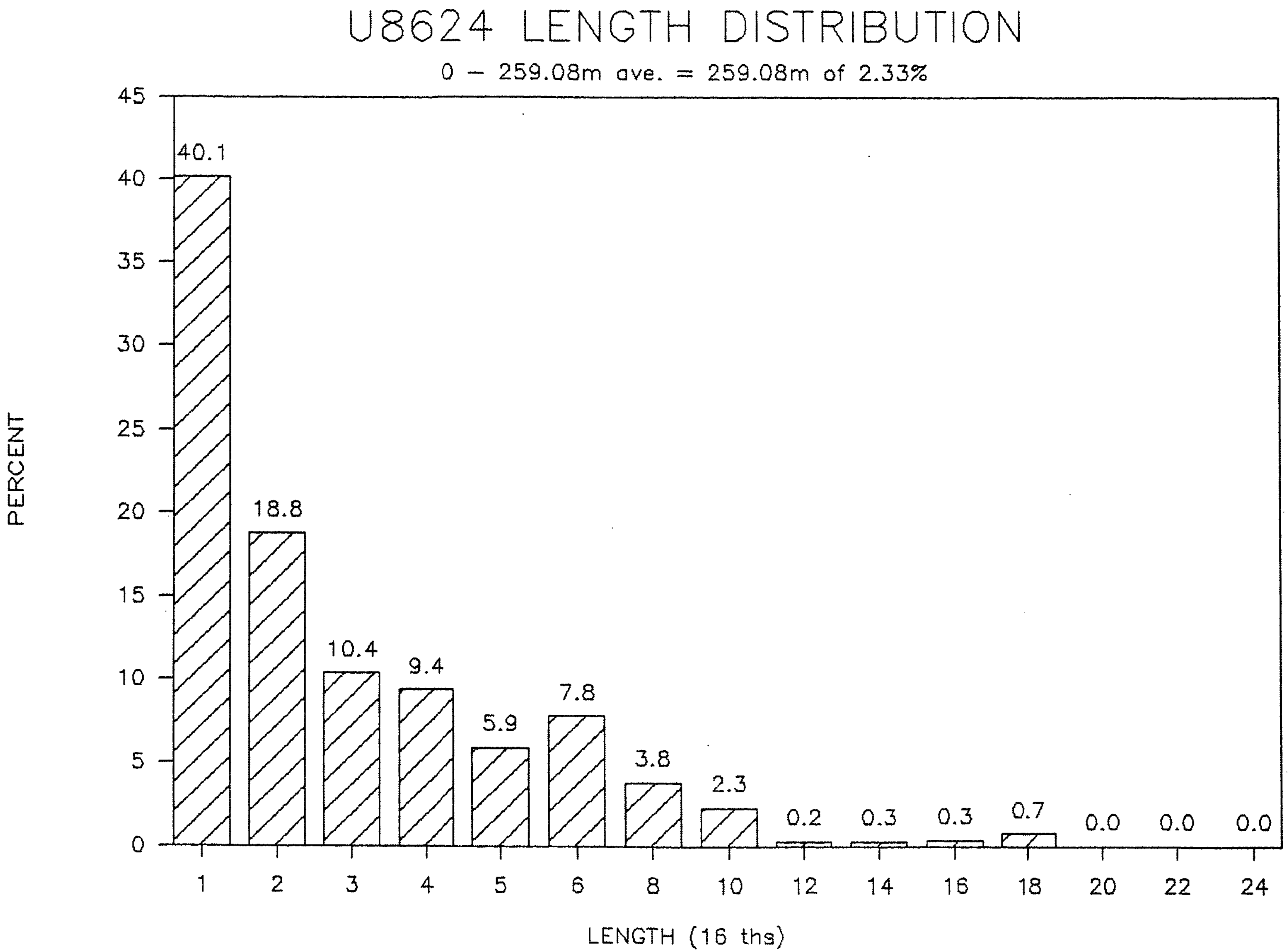
243.84	245.36	1.30	34	11	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	19.5	3.38
245.36	246.89	1.37	30	12	1	0	0.5	0	0	0	0	0	0	0	0	0	0	16	2.62
246.89	248.41	1.40	28	10	1.5	0	0	0	0	0	0	0	0	0	0	0	0	13	2.08
248.41	249.94	1.16	10	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5	0.97
249.94	251.46	1.42	27	3.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	8	1.27
251.46	252.98	1.39	18	8	1	1	0	0	0	0	0	0	0	0	0	0	0	13	2.10
252.98	254.51	1.39	21	11.5	2.5	2.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	33	5.34
254.51	256.03	1.49	22	9	2.5	0.5	1.5	0	0	0	0	0	0	0	0	0	0	21.5	3.23
256.03	257.56	1.39	24	5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	14	2.27
257.56	259.08	1.30	19	10.5	0.5	0.5	0	1	1	0	0	0	0	0	0	0	0	24	4.16
259.08	260.60	1.16	22	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11	2.13
260.60	262.13	0.78	16	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5	1.44
262.13	263.65	1.39	24	5	3.5	1	0	0	0	0	0	0	0	0	0	0	0	15	2.43
263.65	265.18	1.30	22	6.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.30
265.18	266.70	0.64	11	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	3.5	1.23
266.70	268.22	0.52	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
268.22	269.75	1.28	12	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.44
269.75	271.27	1.30	16	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
271.27	272.80	1.22	18	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5	0.92
272.80	274.32	1.31	17	4.5	1	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.11
274.32	275.84	0.91	14	4	0.5	1	0	0	0	0	0	0	0	0	0	0	0	8	1.96
275.84	277.37	1.01	16	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	2	0.45
277.37	278.89	0.82	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
278.89	280.42	0.61	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
280.42	281.94	1.10	23	2	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.41
281.94	283.46	1.43	25	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.39
283.46	284.99	1.37	27	4	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.65
284.99	286.21	0.91	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.2[illegible]
	EOH																		

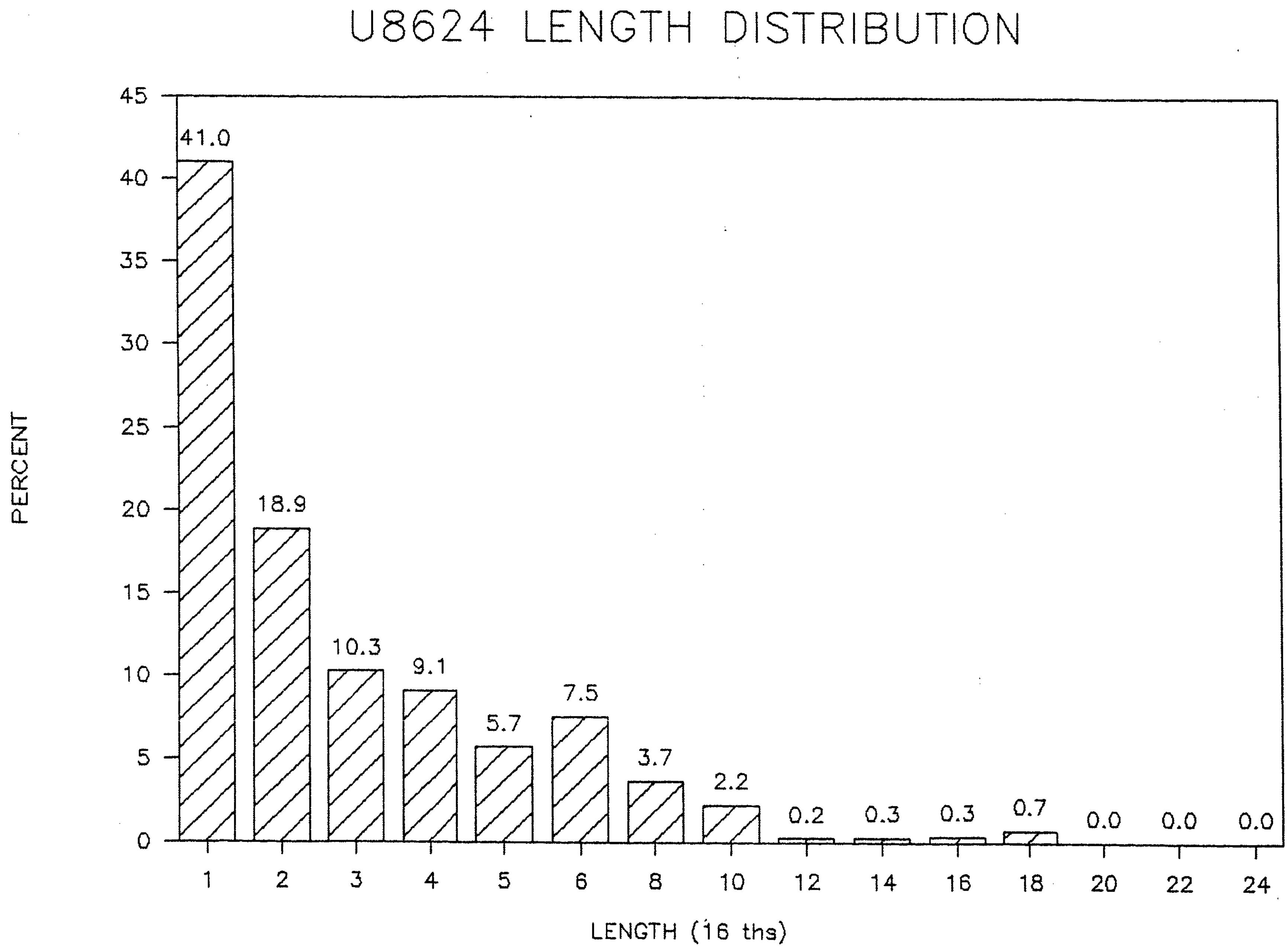
U8624 CCRG



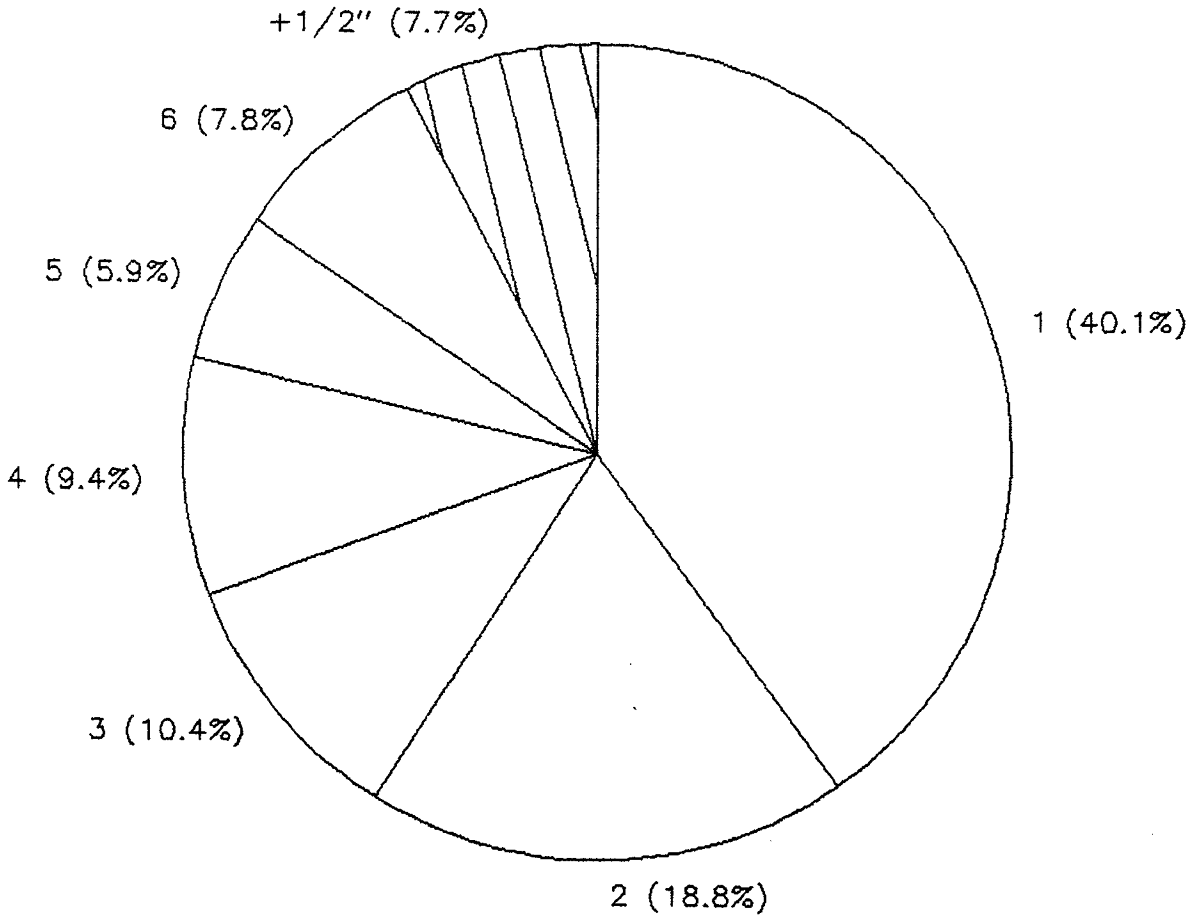
CCRG (%)
10
9
8
7
6
5
4
3
2
1
0
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
245.36
275.84
METERAGE


U8624 RMR
RMR
50
40
30
20
10
0
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
245.36
275.84
METERAGE

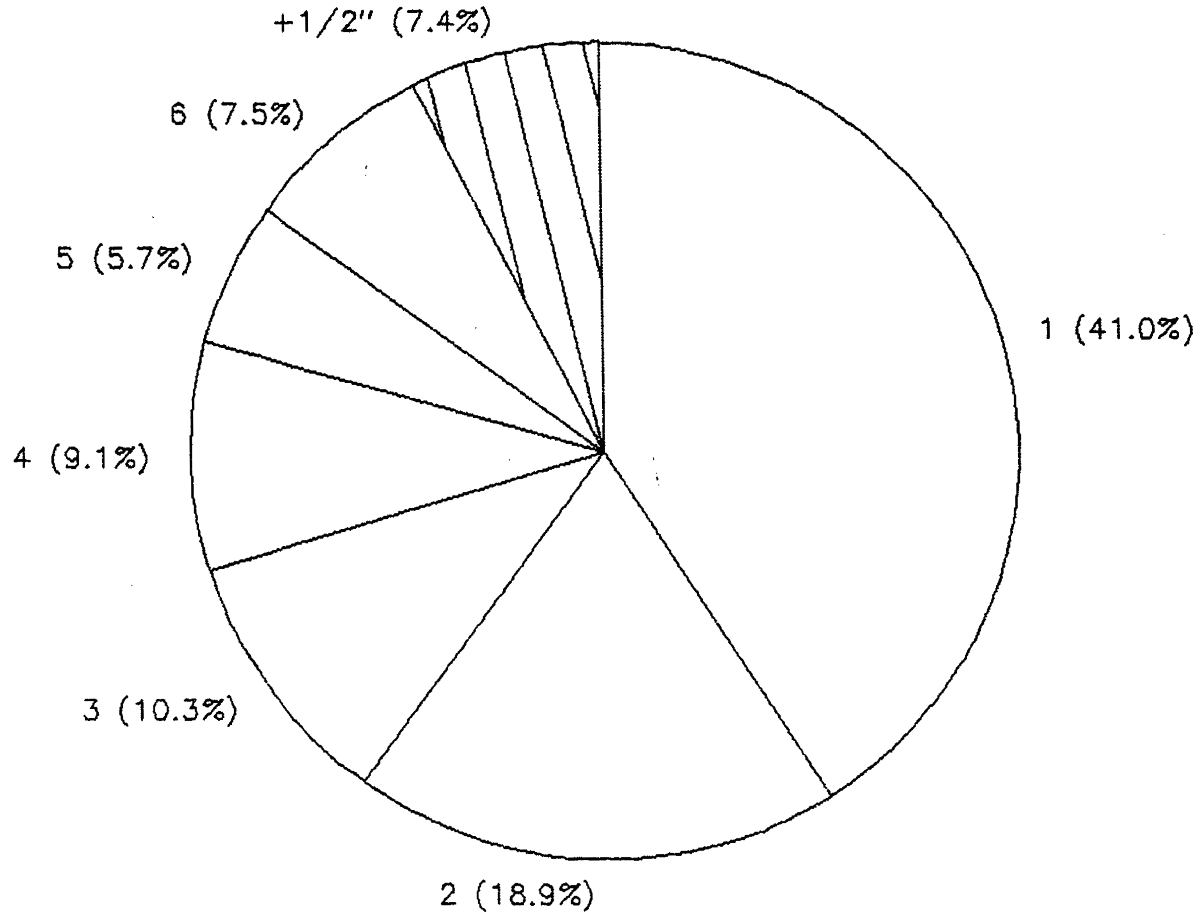

U8624 LENGTH DISTRIBUTION
0 – 259.08m ave. = 259.08m of 2.33%
PERCENT
45
40
35
30
25
20
15
10
5
0
40.1
18.8
10.4
9.4
5.9
7.8
3.8
2.3
0.2
0.3
0.3
0.7
0.0
0.0
0.0
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16 ths)


U8624 LENGTH DISTRIBUTION
PERCENT
LENGTH (16 ths)
41.0
18.9
10.3
9.1
5.7
7.5
3.7
2.2
0.2
0.3
0.3
0.7
0.0
0.0
0.0
0
5
10
15
20
25
30
35
40
45
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24

U8624 LENGTH DISTRIBUTION



U8624 LENGTH DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDAME	HOLE	U86-25	DEPTH	270.66 m
AZIMUTH	180°	INCLINATION	-44°	SECTION	
LATITUDE	6630N	DEPARTURE	7599E	ELEVATION	1413.43
STARTED	Dec. 5	FINISHED	Dec. 10	LOGGED	by DBP date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
0	68.4		Serpentinite, dark green, minor to low grade fibre, sparse	
			fibre below 49 m	
			Fault zones 0 - 2.7, 27.7 - 33.2, 52.4 - 53.6, 57.9 - 68.4	
68.4	141.9		Medium dark green, lizardite and magnetite stringers	
			Minor to sparse fibre	
			Fault zones 94.8 - 98.2, 106.1 - 113.5, 122.5 - 125.6,	
			132.6 - 138.1, 141.1 - 141.9	
141.9	196.6		Medium green, good fibre, harsh	
			Fault zones 145.8 - 146.3, 152.4 - 153.9, 158.5 - 160.3	
196.6	208.7		Medium green, minor fibre	
208.7	258.8		Dark green, minor fibre, lizardite stringers	
			Fault zone 245.7 - 246.6	
			249.9 - 256 increase in fibre	
258.8	262.4		Alteration zone. Serp. increasingly altered downwards	
			261.8 - 262.4 rodingite	
262.4	270.7		Argillite	
270.7			E.O.H.	

DDH U 8625

EAST: 7599 AZ: 180
NORTH: 6630 INCL: -44
ELEV: 1413 DEPTH:270.6

AVERAGE OF TWO COUNTS

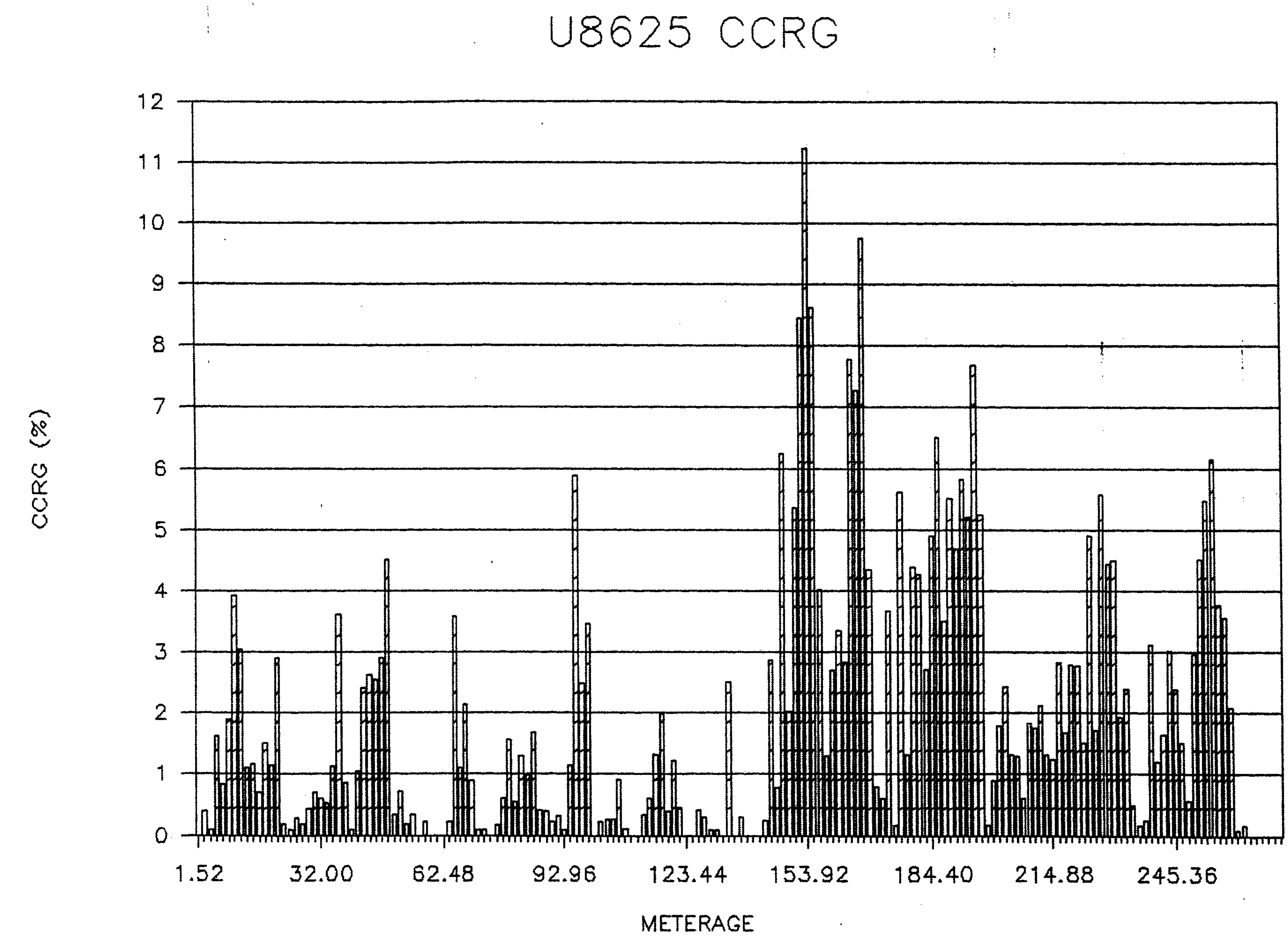
Number of fibre veins counted per 16th category

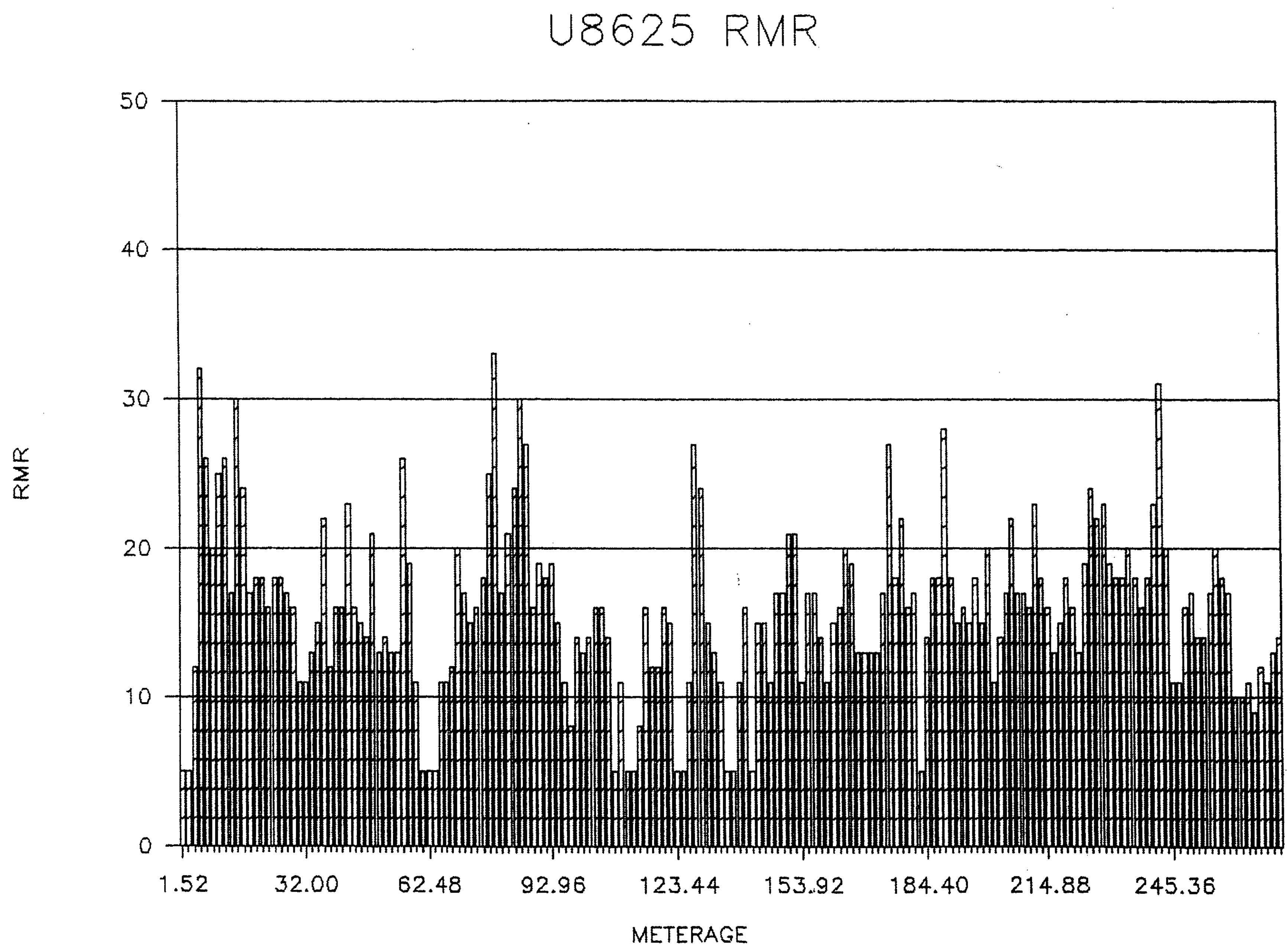
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.00	1.52	0.40	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
1.52	3.05	0.85	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.39
3.05	4.57	1.30	12	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
4.57	6.10	1.45	32	6.5	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	1.63
6.10	7.62	1.34	26	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.84
7.62	9.14	1.37	20	6.5	0.5	0	1	0	0	0	0	0	0	0	0	0	0	0	11.5	1.88
9.14	10.67	1.43	25	6.5	1	0.5	1.5	0	0.5	0	0	0.5	0	0	0	0	0	0	25	3.92
10.67	12.19	1.40	26	7	2	1	0	1	0	0	0	0	0	0	0	0	0	0	19	3.04
12.19	13.72	1.42	17	3.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	7	1.11
13.72	15.24	1.46	30	5.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.15
15.24	16.76	1.30	24	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.69
16.76	18.29	1.42	17	4	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9.5	1.50
18.29	19.81	1.37	18	4	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.15
19.81	21.34	1.31	18	6.5	1.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	17	2.91
21.34	22.86	1.30	16	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.17
22.86	24.38	1.37	18	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
24.38	25.91	1.25	18	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.27
25.91	27.43	1.25	17	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
27.43	28.96	1.33	16	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.42
28.96	30.48	1.28	11	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.70
30.48	32.00	1.11	11	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.61
32.00	33.53	1.08	13	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.52
33.53	35.05	1.20	15	3.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6	1.12
35.05	36.58	1.43	22	7.5	1	1	0.5	0.5	1	0	0	0	0	0	0	0	0	0	23	3.60
36.58	38.10	1.19	12	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.85
38.10	39.62	1.26	16	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
39.62	41.15	1.19	16	4	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.04
41.15	42.67	1.36	23	6	1.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	14.5	2.40
42.67	44.20	1.33	16	7	2	1.5	0	0	0	0	0	0	0	0	0	0	0	0	15.5	2.62
44.20	45.72	1.19	15	6.5	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	13.5	2.55
45.72	47.24	1.23	14	7.5	2	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	16	2.91
47.24	48.77	1.49	21	8.5	4.5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	30	4.51
48.77	50.29	1.34	13	0	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	2	0.33
50.29	51.82	1.25	14	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.72
51.82	53.34	1.22	13	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.18
53.34	54.86	1.33	13	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.34
54.86	56.39	1.46	26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
56.39	57.91	1.02	19	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.22
57.91	59.44	0.93	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
59.44	60.96	1.07	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
60.96	62.48	1.10	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
62.48	64.01	1.05	5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.21
64.01	65.53	1.13	11	2.5	1	0.5	1	1	0.5	0	0	0	0	0	0	0	0	0	18	3.58
5.53	67.06	1.11	11	2.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.11
67.06	68.58	1.16	12	4.5	1	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	11	2.13
68.58	70.10	1.40	20	4.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.88
70.10	71.63	1.36	17	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
71.63	73.15	1.34	15	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08

73.15	74.68	1.36	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
74.68	76.20	1.48	18	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.15
76.20	77.72	1.49	25	1	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.60
77.72	79.25	1.51	33	5	0.5	0.5	0	0	0.5	0	0	0	0	0	0	0	0	0	10.5	1.56
79.25	80.77	1.43	17	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.55
80.77	82.30	1.48	21	2	1	1.5	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.29
82.30	83.82	1.48	24	3	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	0.99
83.82	85.34	1.48	30	3	1	2	0	0	0	0	0	0	0	0	0	0	0	0	11	1.67
85.34	86.87	1.36	27	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
86.87	88.39	1.40	16	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
88.39	89.92	1.48	19	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.23
89.92	91.44	1.43	18	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.31
91.44	92.96	1.43	19	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
92.96	94.49	1.37	15	3	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	7	1.15
94.49	96.01	1.20	11	3.5	3	1	0	0	2.5	0.5	0	0	0	0	0	0	0	0	31.5	5.87
96.01	97.54	1.26	8	6	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	14	2.48
97.54	99.06	1.23	14	4.5	2	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	19	3.46
99.06	100.58	1.13	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
100.58	102.11	1.04	14	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.22
102.11	103.63	1.28	16	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
103.63	105.16	1.28	16	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
105.16	106.68	1.37	14	3.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	5.5	0.90
106.68	108.20	1.08	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.10
108.20	109.73	1.04	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
109.73	111.25	1.16	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
11.25	112.78	1.01	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.33
2.78	114.30	1.11	8	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.61
114.30	115.82	1.37	16	2.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	8	1.31
115.82	117.35	1.13	12	3	1	1	0.5	0	0	0	0	0	0	0	0	0	0	0	10	1.99
117.35	118.87	1.17	12	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.38
118.87	120.40	1.30	16	3.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7	1.21
120.40	121.92	1.26	15	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.44
121.92	123.44	1.28	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
123.44	124.97	0.70	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
124.97	126.49	1.39	11	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
126.49	128.02	1.48	27	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.30
128.02	129.54	1.40	24	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.08
129.54	131.06	1.28	15	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
131.06	132.59	1.20	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
132.59	134.11	0.85	11	2	1	0.5	1	0	0	0	0	0	0	0	0	0	0	0	9.5	2.50
134.11	135.64	1.01	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
135.64	137.16	1.16	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.29
137.16	138.68	1.17	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
138.68	140.21	1.25	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
140.21	141.73	1.07	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
141.73	143.26	1.37	15	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
143.26	144.78	1.17	15	2	0.5	0	0	0	0	0	0	1	0	0	0	0	0	0	15	2.87
144.78	146.30	1.31	11	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.77
146.30	147.83	1.30	17	6.5	2	1.5	2	0	0	0	0	0.5	0.5	0	0	0	0	0	36	6.24
147.83	149.35	1.33	17	1	1	0	1.5	0	0.5	0	0	0	0	0	0	0	0	0	12	2.03
149.35	150.88	1.34	21	5.5	2.5	1.5	0.5	1	1	0.5	0	0	0	0	0	0	0	0	32	5.36
0.88	152.40	1.25	21	4.5	2.5	1	0.5	0.5	1.5	2	0.5	0	0	0	0	0	0	0	47	8.44
52.40	153.92	1.22	11	8.5	3.5	0.5	0.5	1	1	1.5	0	1	0.5	0	0	0	0	0	61	11.23
153.92	155.45	1.34	17	8.5	2	2	1.5	1	1.5	0	0.5	0	0	0.5	0	0	0	0	51.5	8.62
155.45	156.97	1.34	17	6	1.5	0	1	1	1	0	0	0	0	0	0	0	0	0	24	4.02
156.97	158.50	1.13	14	2	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.29

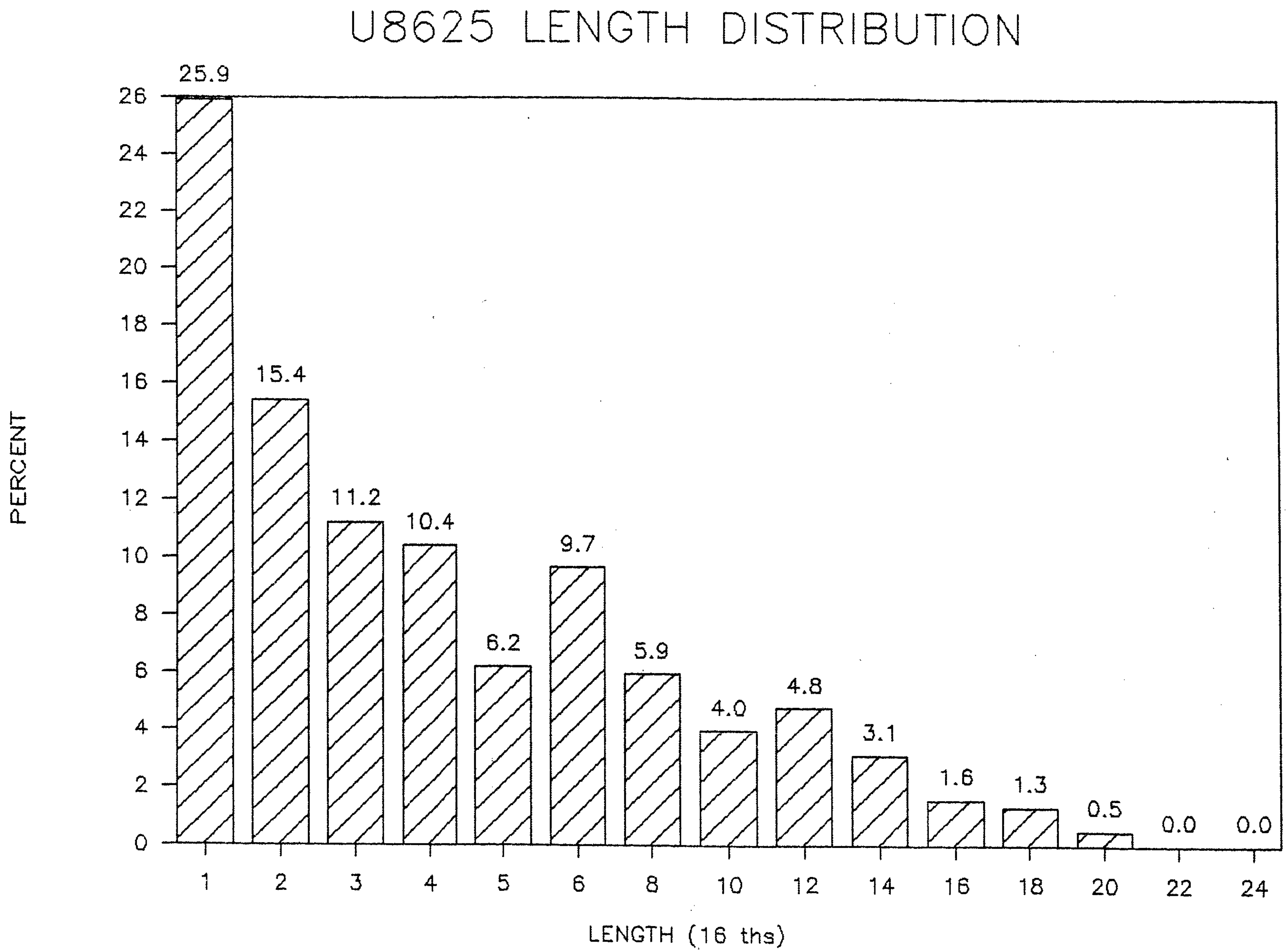
158.50	160.02	1.08	11	3	2.5	0	0.5	0	0.5	0	0	0	0	0	0	0	0	0	13	2.70
160.02	161.54	1.17	15	3.5	0.5	0	0	0	0	1	0.5	0	0	0	0	0	0	0	17.5	3.35
161.54	163.07	1.39	16	8.5	3	1	0	0	0	0	0	0	0	0	0	0	0	0	17.5	2.83
163.07	164.59	1.37	20	5.5	2	1	0	0	2	0	0.5	1.5	0	0	0	0	0	0	47.5	7.77
164.59	166.12	1.28	19	1.5	0	1.5	0.5	0.5	0	1.5	0.5	0	1	0	0	0	0	0	41.5	7.28
166.12	167.64	1.17	13	7.5	3	2	1.5	0.5	1.5	1	0	0.5	0	0	0	0	0	0	51	9.76
167.64	169.16	1.26	13	5	1	0.5	1	0	1	0	0	0.5	0	0	0	0	0	0	24.5	4.35
169.16	170.69	1.26	13	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.80
170.69	172.21	1.31	13	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	3.5	0.60
172.21	173.74	1.40	17	6	1.5	2	2	0	0	0	0	0	0	0	0	0	0	0	23	3.68
173.74	175.26	1.45	27	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
175.26	176.78	1.34	18	3	1	1.5	0	0	1	1	1	0	0	0	0	0	0	0	33.5	5.61
176.78	178.31	1.37	22	5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8	1.31
178.31	179.83	1.36	16	2.5	0	0	0	0	0	0	0.5	0	0	0	0.5	0.5	0	0	26.5	4.39
179.83	181.36	1.23	17	3	1.5	0.5	0	1	0.5	0	0	0	0	0.5	0	0	0	0	23.5	4.27
181.36	182.88	1.16	5	2	0.5	0.5	0.5	0.5	0	0	0.5	0	0	0	0	0	0	0	14	2.71
182.88	184.40	1.19	14	5	1.5	0.5	0.5	0.5	0	1.5	0	0	0	0	0	0	0	0	26	4.91
184.40	185.93	1.31	18	3.5	2.5	1	0	0.5	1	1	1	0	0	0	0	0	0	0	38	6.51
185.93	187.45	1.19	18	5.5	3.5	1	0	0	0.5	0	0	0	0	0	0	0	0	0	18.5	3.49
187.45	188.98	1.46	28	5	1	1	1	1	1	0.5	0	0	0.5	0	0	0	0	0	36	5.52
188.98	190.50	1.39	18	6	3.5	0	1.5	0	1	0.5	0	0	0	0	0	0	0	0	29	4.69
190.50	192.02	1.31	15	2.5	2.5	1	1.5	0.5	0	0	0	0	0.5	0.5	0	0	0	0	34	5.82
192.02	193.55	1.36	16	5	2.5	1	2.5	0.5	1	0	0	0	0	0	0	0	0	0	31.5	5.21
193.55	195.07	1.39	15	4	1.5	2	0.5	0.5	0.5	0.5	0.5	0	0	0	1	0	0	0	47.5	7.69
195.07	196.60	1.33	18	2.5	0.5	0	0	0.5	2	0	0.5	0	0	0.5	0	0	0	0	31	5.25
196.60	198.12	1.39	15	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
198.12	199.64	1.39	20	1.5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	0.89
199.64	201.17	1.19	11	4	0	0.5	1	0	0	0	0	0	0	0	0	0	0	0	9.5	1.79
201.17	202.69	1.30	14	3.5	2	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	14	2.43
202.69	204.22	1.37	17	5.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8	1.31
204.22	205.74	1.31	22	4	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.28
205.74	207.26	1.31	17	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.60
207.26	208.79	1.34	17	6	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	11	1.84
208.79	210.31	1.40	16	8	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	11	1.76
210.31	211.84	1.43	23	3.5	0.5	0.5	0	1.5	0	0	0	0	0	0	0	0	0	0	13.5	2.12
211.84	213.36	1.37	18	4	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	8	1.31
213.36	214.88	1.36	16	2	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.24
214.88	216.41	1.51	13	8	1.5	0	2	0	0	0	0	0	0	0	0	0	0	0	19	2.83
216.41	217.93	1.40	15	5.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	1.68
217.93	219.46	1.33	18	2	1	0.5	0	0	0	0	0.5	0.5	0	0	0	0	0	0	16.5	2.79
219.46	220.98	1.34	16	4	2	0.5	1	0	0.5	0	0	0	0	0	0	0	0	0	16.5	2.76
220.98	222.50	1.19	13	3	1	0	0	0	0.5	0	0	0	0	0	0	0	0	0	8	1.51
222.50	224.03	1.42	19	2.5	0.5	2	1.5	0.5	0	0	0	0.5	0.5	0	0	0	0	0	31	4.91
224.03	225.55	1.51	24	2.5	1.5	0	0	0	0	0	0	0.5	0	0	0	0	0	0	11.5	1.71
225.55	227.08	1.43	22	4	1.5	2.5	1	2	0	0	0	0	0.5	0	0	0	0	0	35.5	5.56
227.08	228.60	1.49	23	3.5	1.5	1.5	1	0.5	0.5	0.5	0.5	0	0	0	0	0	0	0	29.5	4.43
228.60	230.12	1.37	19	4	1.5	0.5	0.5	0	1	0.5	0	0	0.5	0	0	0	0	0	27.5	4.50
230.12	231.65	1.34	18	2.5	0.5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	11.5	1.92
231.65	233.17	1.46	18	5	3.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.38
233.17	234.70	1.34	20	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.50
234.70	236.22	1.40	18	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
236.22	237.74	1.36	16	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.25
237.74	239.27	1.40	18	7	2	1.5	1	0	0	0	0	0	0	0	0	0	0	0	19.5	3.12
239.27	240.79	1.49	23	2	1.5	1	0	0	0	0	0	0	0	0	0	0	0	0	8	1.20
240.79	242.32	1.51	31	2	0.5	1	0	1	0	0	0	0	0	0	0	0	0	0	11	1.64
242.32	243.84	1.26	20	2	1.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	17	3.02

[illegible]3.84	245.36	1.17	11	6	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	2.39
[illegible]5.36	246.89	0.98	11	3.5	0	1	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.50
246.89	248.41	1.40	16	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.56
248.41	249.94	1.33	17	6.5	1.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	17.5	2.96
249.94	251.46	1.14	14	2.5	3	0.5	0.5	1	1	0	0	0	0	0	0	0	0	0	23	4.52
251.46	252.98	1.13	14	3.5	2	1	1	1	0	1	0	0	0	0	0	0	0	0	27.5	5.47
252.98	254.51	1.30	17	3	3	2.5	0.5	0	2	0	0.5	0	0	0	0	0	0	0	35.5	6.15
254.51	256.03	1.46	20	5.5	1	1	0.5	0	0	0	0	1	0	0	0	0	0	0	24.5	3.76
256.03	257.56	1.42	18	4	0.5	0.5	2	1	0.5	0	0	0	0	0	0	0	0	0	22.5	3.56
257.56	259.08	1.30	17	4	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	12	2.08
259.08	260.60	1.22	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.09
260.60	262.13	1.40	10	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.16
262.13	263.65	1.46	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
263.65	265.18	1.17	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
265.18	266.70	0.79	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
266.70	268.22	0.81	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
268.22	269.75	1.42	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
269.75	270.66	0.85	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
	EOH																			


U8625 CCRG
CCRG (%)
0
1
2
3
4
5
6
7
8
9
10
11
12
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
245.36
METERAGE



U8625 RMR
RMR
50
40
30
20
10
0
1.52
32.00
62.48
92.96
123.44
153.92
184.40
214.88
245.36
METERAGE


U8625 LENGTH DISTRIBUTION
PERCENT
LENGTH (16 ths)
25.9
15.4
11.2
10.4
6.2
9.7
5.9
4.0
4.8
3.1
1.6
1.3
0.5
0.0
0.0
0
2
4
6
8
10
12
14
16
18
20
22
24
26
1
2
3
4
5
6
8
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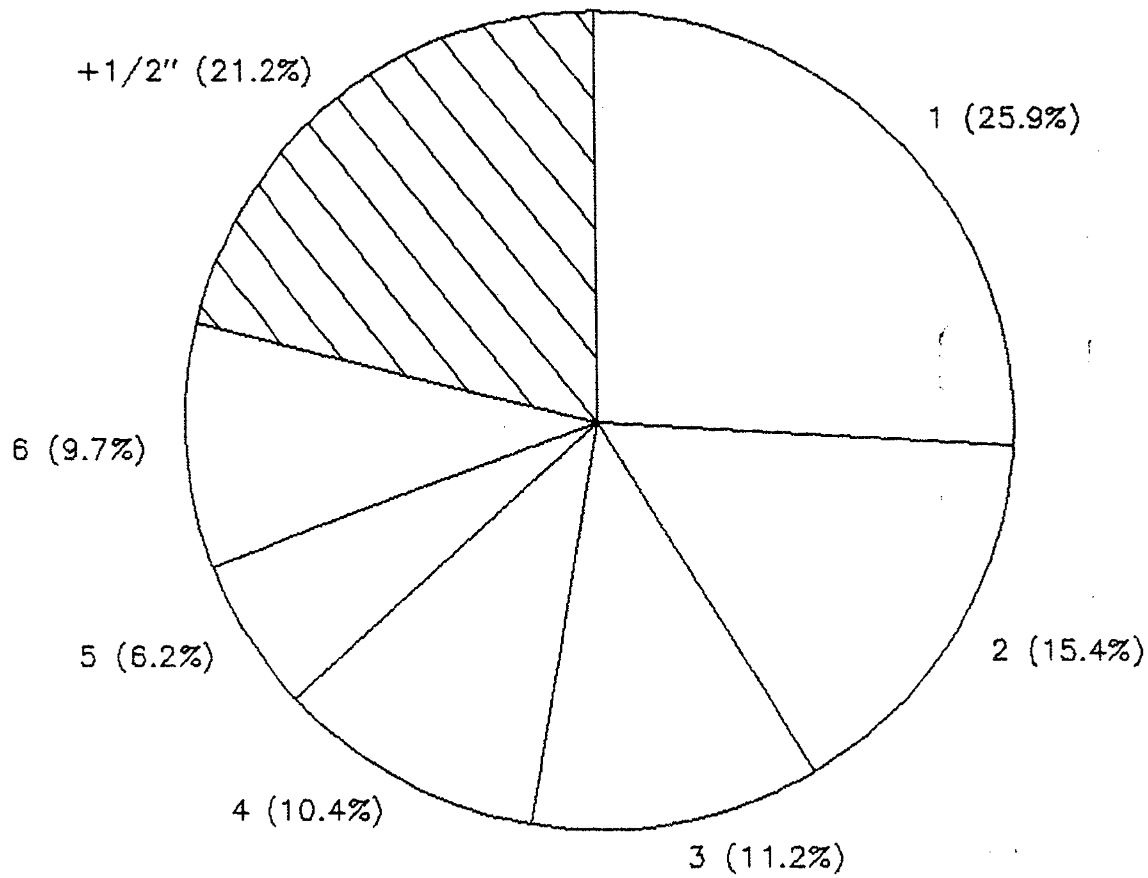
12
14
16
18
20
22
24

U8625 LENGTH DISTRIBUTION



FORM DD-3

DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY McDame — HOLE U87-26 — DEPTH 228.6 m

AZIMUTH 139.9° — INCLINATION -46° — SECTION

LATITUDE 6630.94 N — DEPARTURE 7600.88E — ELEVATION 1413.10 m

STARTED 9 Jan, 87 — FINISHED 19 Jan, 87 — LOGGED by DBP date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
2.1	56.0		Medium dark green serpentinite, minor fibre some lizardite	
			and magnetitite stringers	
			Faults 32-33, 38.1 - 39.9, 51.8 - 56	
56.0	91.7		Medium dark green, fibre bearing	
			Fault 87.2 - 88.1	
91.7	104.2		Fault zone. Broken and shattered with lizardite	
104.2	135.3		Medium green to medium dark green with good fibre.	
			Fault @ 122.5 - 123.4	
			Hole stopped @ 135.3, caved and redrilled NQ from 103.6 m	
103.6	170.1		As above, fibre decreasing below 137 m	
170.1	197.5		Medium dark green, minor fibre	
197.5	202.1		Fault, broken and shattered, dark	
202.1	228.6		Medium dark green, good fibre	
			217.3 reduced to BQ	
	228.6		E.O.H. Core tube stuck and lost	

[illegible]H U86-26 COMPLETE HOLE COMBINES HQ and NQ CORE - NQ STARTS WHERE HQ LEAVES OFF.

EAST:7600.9 AZ:139.9
NORTH:6630.9 INCL:-46
ELEV:1431.1 DEPTH:135.3m. AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

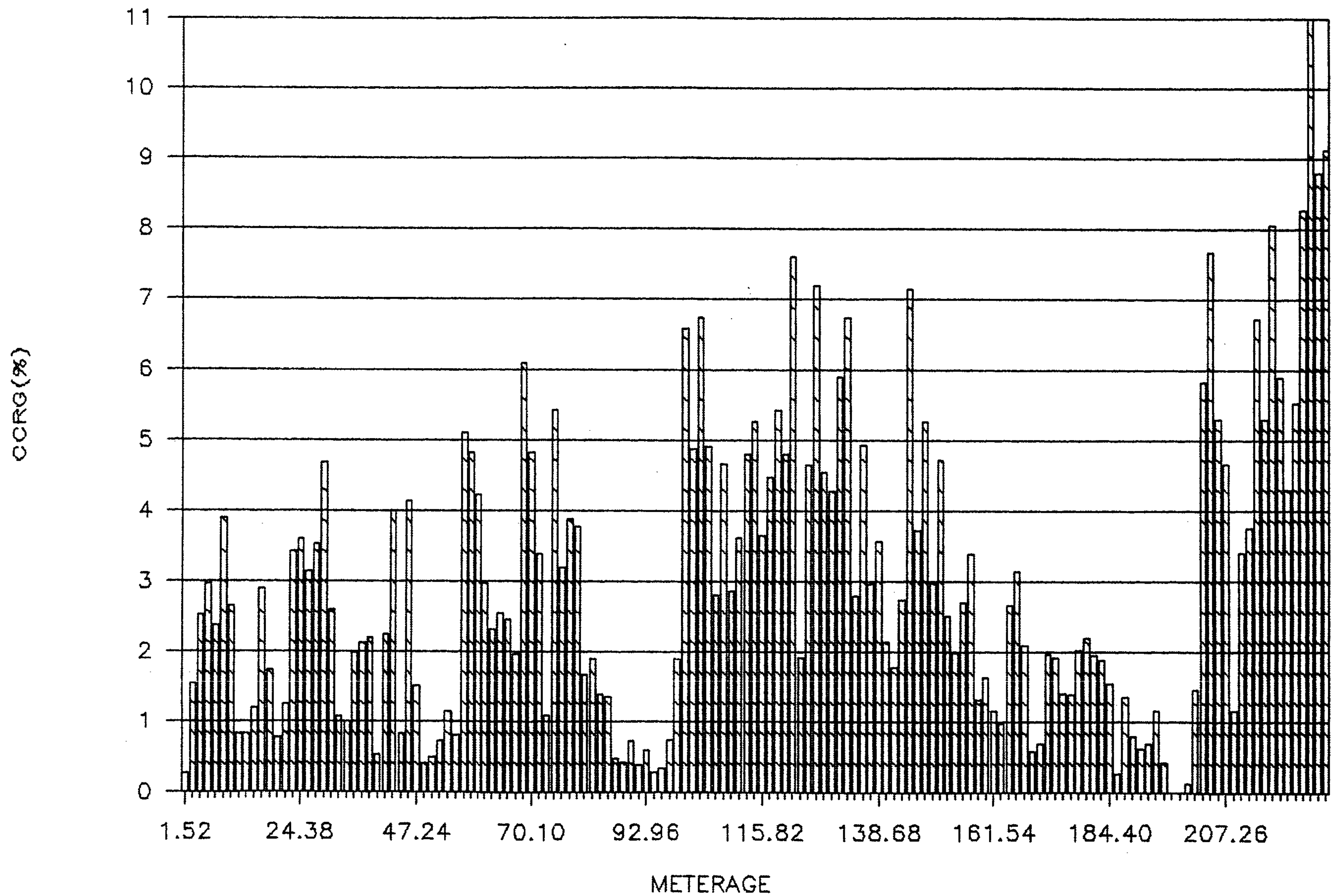
FROM	TO	REC	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL	CCRG
M	M	M																	16's	%
0.00	1.52	0.00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	ERR
1.52	3.05	0.46	14	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.25
3.05	4.57	0.66	15	4.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	1.54
4.57	6.10	1.02	13	6.5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	11.5	2.53
6.10	7.62	1.33	18	9	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	17.5	2.96
7.62	9.14	1.37	22	9	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	14.5	2.37
9.14	10.67	1.39	23	5	2.5	0.5	0	0.5	0	0	1	0	0	0	0	0	0	0	24	3.88
10.67	12.19	1.23	22	6	1	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	14.5	2.64
12.19	13.72	0.82	15	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.82
13.72	15.24	0.69	13	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.82
15.24	16.76	0.76	11	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	1.18
16.76	18.29	1.13	8	6.5	0	0	0	0	0	1	0	0	0	0	0	0	0	0	14.5	2.89
18.29	19.81	1.36	21	5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	10.5	1.74
19.81	21.34	1.33	16	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.76
21.34	22.86	1.26	8	6	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.24
22.86	24.38	1.45	21	7.5	2	1	0	0.5	0	0	0.5	0	0	0	0	0	0	0	22	3.41
24.38	25.91	1.43	21	5	0.5	0.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	23	3.60
[illegible].91	27.43	1.43	24	7	2	1	0.5	0	0	0.5	0	0	0	0	0	0	0	0	20	3.13
27.43	28.96	1.40	26	10.5	3	0.5	0	0	0	0.5	0	0	0	0	0	0	0	0	22	3.52
28.96	30.48	1.46	20	13	1.5	1.5	0.5	0	0.5	0	0.5	0	0	0	0	0	0	0	30.5	4.68
30.48	32.00	1.34	16	4.5	1	0	0	0	0	0.5	0.5	0	0	0	0	0	0	0	15.5	2.59
32.00	33.53	1.37	14	5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.06
33.53	35.05	1.46	17	4.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.00
35.05	36.58	1.42	19	6.5	2	0	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	1.98
36.58	38.10	1.43	20	9.5	0.5	1	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.12
38.10	39.62	1.39	9	7.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	13.5	2.19
39.62	41.15	1.28	8	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.53
41.15	42.67	1.40	18	8.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	14	2.24
42.67	44.20	1.40	20	9	2.5	1	2	0	0	0	0	0	0	0	0	0	0	0	25	4.00
44.20	45.72	1.39	17	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.81
45.72	47.24	1.36	20	10.5	3.5	0.5	1.5	0	0	0	0	0	0	0	0	0	0	0	25	4.14
47.24	48.77	1.34	18	6.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	9	1.51
48.77	50.29	1.40	19	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
50.29	51.82	1.37	18	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.49
51.82	53.34	1.25	14	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.72
53.34	54.86	1.19	17	3	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.13
54.86	56.39	1.26	12	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.80
56.39	57.91	1.39	18	8.5	3	1.5	0.5	0.5	0.5	0	0.5	0	0	0	0	0	0	0	31.5	5.10
57.91	59.44	1.37	24	6	2	2.5	1	0	0.5	0	0.5	0	0	0	0	0	0	0	29.5	4.83
59.44	60.96	1.25	18	8	2.5	0	0.5	0.5	1	0	0	0	0	0	0	0	0	0	23.5	4.22
60.96	62.48	1.36	19	10	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	18	2.98
62.48	64.01	1.36	20	3.5	0.5	1	0	0.5	0	0.5	0	0	0	0	0	0	0	0	14	2.32
[illegible].01	65.53	1.28	22	9.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	14.5	2.54
65.53	67.06	1.14	17	7.5	0.5	0	1	0	0	0	0	0	0	0	0	0	0	0	12.5	2.46
67.06	68.58	1.49	17	6.5	0	0.5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	13	1.95
68.58	70.10	1.49	19	8.5	4	1	0	0	0.5	1	1	0	0	0	0	0	0	0	40.5	6.09
70.10	71.63	1.51	17	10	2	0.5	0	0	0	1.5	0.5	0	0	0	0	0	0	0	32.5	4.84
71.63	73.15	1.49	20	9.5	1.5	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	22.5	3.38

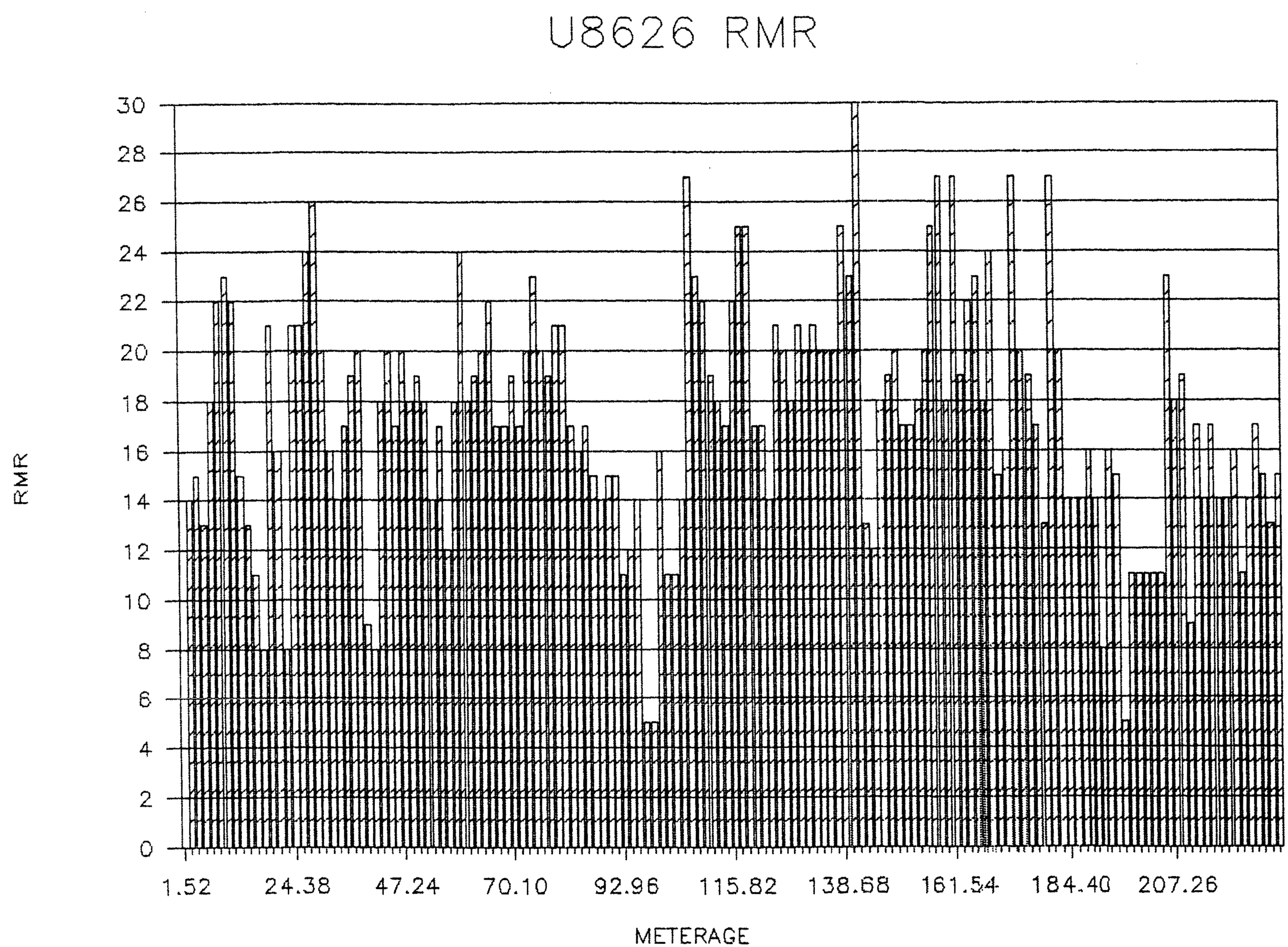
73.15	74.68	1.34	23	4	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.09
74.68	76.20	1.33	20	5	5	1	1.5	0	0	1	0	0	0	0	0	0	0	0	32	5.42
76.20	77.72	1.37	19	12.5	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	19.5	3.19
77.72	79.25	1.48	21	6	0.5	1.5	0	0	1	1	0	0	0	0	0	0	0	0	25.5	3.87
79.25	80.77	1.37	21	4	2	1	0	1	0.5	0.5	0	0	0	0	0	0	0	0	23	3.76
80.77	82.30	1.22	17	4	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.66
82.30	83.82	1.25	16	5	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	10.5	1.89
83.82	85.34	1.39	17	6.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.38
85.34	86.87	1.25	15	2.5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.35
86.87	88.39	1.19	14	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.47
88.39	89.92	1.33	15	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.42
89.92	91.44	1.26	15	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.71
91.44	92.96	1.17	11	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.38
92.96	94.49	1.36	12	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.58
94.49	96.01	1.26	14	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.27
96.01	97.54	1.34	5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.33
97.54	99.06	1.39	5	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.73
99.06	100.58	1.31	16	6.5	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11	1.88
100.58	102.11	1.16	11	5	3.5	0	0.5	1	0.5	1.5	0	0	0	0	0	0	0	0	34	6.59
102.11	103.63	0.99	11	4	2.5	0.5	0	0	1	0	0.5	0	0	0	0	0	0	0	21.5	4.87
103.63	105.16	1.45	14	11	2	1.5	1.5	0	3	0	0	0	0	0	0	0	0	0	43.5	6.74
105.16	106.68	1.46	27	8	0.5	2	1	0	1.5	0.5	0	0	0	0	0	0	0	0	32	4.91
106.68	108.20	1.36	23	3.5	1.5	1	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	17	2.81
108.20	109.73	1.42	22	7	0.5	1	1.5	0.5	1	0.5	0	0	0	0	0	0	0	0	29.5	4.67
109.73	111.25	1.42	19	6	2	2	0.5	0	0	0	0	0	0	0	0	0	0	0	18	2.85
111.25	112.78	1.49	18	4	1.5	1	0	0	1	1	0	0	0	0	0	0	0	0	24	3.61
112.78	114.30	1.45	17	2	1.5	0	0	0	0.5	1.5	0.5	0.5	0	0	0	0	0	0	31	4.81
114.30	115.82	1.39	22	2	2	2	0.5	0.5	2	0.5	0	0	0	0	0	0	0	0	32.5	5.26
115.82	117.35	1.48	25	9.5	2	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	24	3.64
117.35	118.87	1.43	25	11	2	1	0.5	0.5	1	0	0	0	0	0	0	0	0	0	28.5	4.47
118.87	120.40	1.39	17	8	3.5	1	0.5	1.5	1	0	0	0	0	0	0	0	0	0	33.5	5.42
120.40	121.92	1.40	17	7.5	0.5	1.5	0.5	0	0.5	0	0	1	0	0	0	0	0	0	30	4.80
121.92	123.44	1.46	14	7	4	2	1	1.5	0.5	0.5	1	0	0	0	0	0	0	0	49.5	7.60
123.44	124.97	1.36	21	2.5	1.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	11.5	1.90
124.97	126.49	1.45	20	1.5	1	1.5	1	0	1	1.5	0	0	0	0	0	0	0	0	30	4.65
126.49	128.02	1.31	18	4.5	1.5	0	1	0.5	1	0.5	1	0	0	0.5	0	0	0	0	42	7.19
128.02	129.54	1.36	21	7	2	1	1.5	0.5	0	0	0.5	0	0	0	0	0	0	0	27.5	4.55
129.54	131.06	1.49	20	8	2.5	1	1.5	0.5	0	0.5	0	0	0	0	0	0	0	0	28.5	4.28
131.06	132.59	1.45	21	3.5	1	0.5	0	2	1.5	1.5	0	0	0	0	0	0	0	0	38	5.89
132.59	134.11	1.46	20	4	2	0.5	1	0.5	0.5	1	0	0	0	0.5	0.5	0	0	0	44	6.75
134.11	135.33	1.45	20	7	1.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	18	2.79
135.64	137.16	1.48	20	7.5	1.5	2	0.5	0	0	1	0	0.5	0	0	0	0	0	0	32.5	4.94
137.16	138.68	1.48	25	8.5	0.5	0.5	0	0.5	0	0	0	0.5	0	0	0	0	0	0	19.5	2.96
138.68	140.21	1.48	23	4	2	1	0	0.5	1	0.5	0	0	0	0	0	0	0	0	23.5	3.57
140.21	141.73	1.31	30	3.5	0.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	12.5	2.14
141.73	143.26	1.26	13	4.5	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	10	1.77
143.26	144.78	1.36	12	6	1	1.5	1	0	0	0	0	0	0	0	0	0	0	0	16.5	2.73
144.78	146.30	1.46	18	9.5	5	2	2.5	1	1	0	0	0	0	0	0	0	0	0	46.5	7.13
146.30	147.83	1.51	19	5	2	1	0	0	0	0	0	0.5	0.5	0	0	0	0	0	25	3.72
147.83	149.35	1.49	20	11.5	5	1	0.5	0.5	0	0	0	0.5	0	0	0	0	0	0	35	5.26
149.35	150.88	1.51	17	10.5	2	1	0	0.5	0	0	0	0	0	0	0	0	0	0	20	2.98
150.88	152.40	1.45	17	7.5	3.5	0.5	1.5	0.5	1	0	0	0	0	0	0	0	0	0	30.5	4.73
152.40	153.92	1.39	18	7.5	2	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	15.5	2.51
153.92	155.45	1.42	20	3	2.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	12.5	1.98
155.45	156.97	1.42	25	5.5	1	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	17	2.69
156.97	158.50	1.49	27	9	1	1	1.5	0.5	0	0	0	0	0	0	0	0	0	0	22.5	3.38

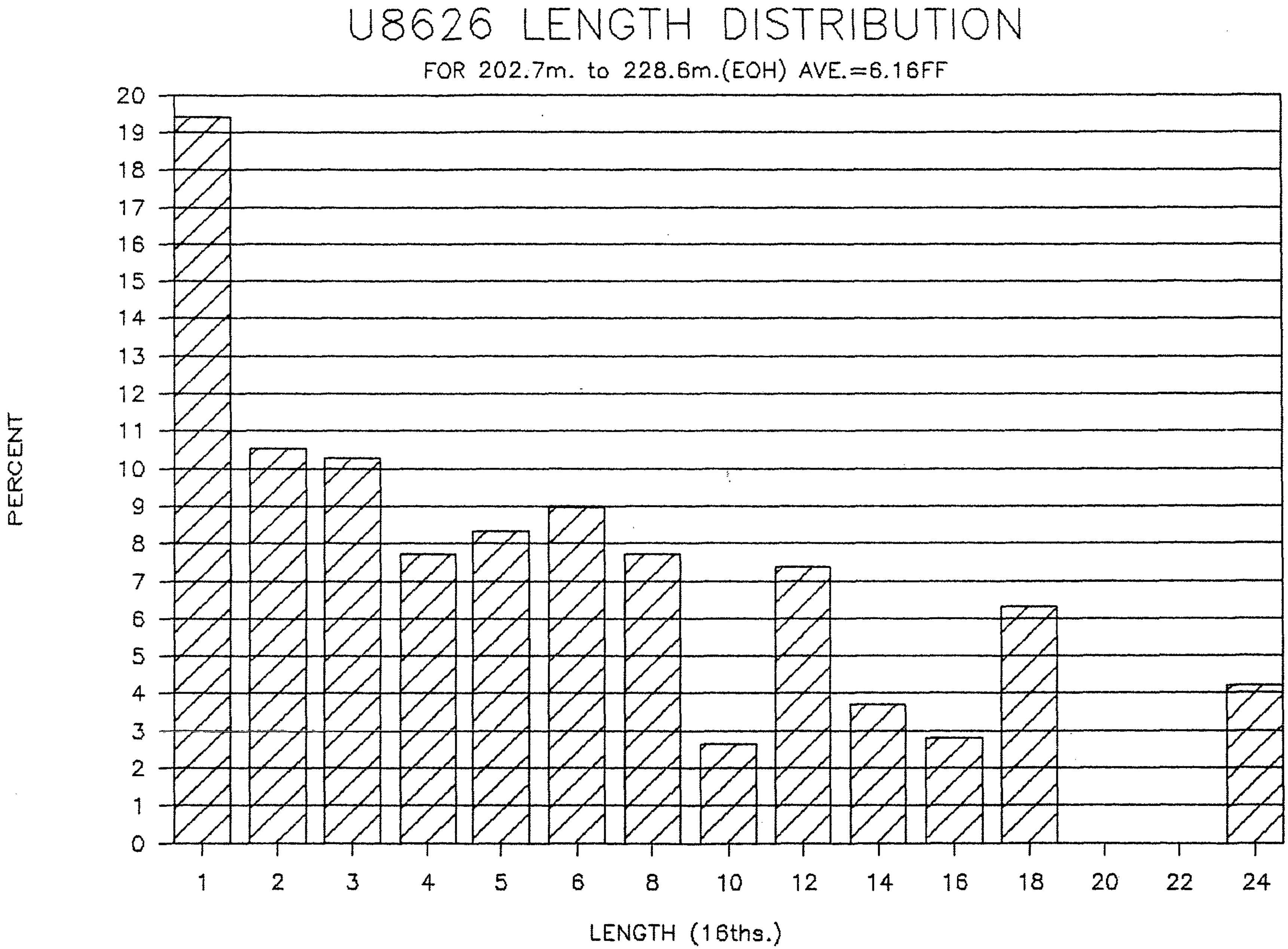
[illegible].50	160.02	1.45	18	5.5	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.32
160.02	161.54	1.52	27	2.5	0.5	0.5	0	0	1	0	0	0	0	0	0	0	0	0	11	1.62
161.54	163.07	1.46	19	5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7.5	1.15
163.07	164.59	1.49	22	5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	0.98
164.59	166.12	1.48	23	8.5	1	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	17.5	2.66
166.12	167.64	1.36	18	9.5	1	0.5	1.5	0	0	0	0	0	0	0	0	0	0	0	19	3.14
167.64	169.16	1.40	24	8.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	13	2.08
169.16	170.69	1.37	15	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.57
170.69	172.21	1.31	16	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.69
172.21	173.74	1.37	27	7	1	1	0	0	0	0	0	0	0	0	0	0	0	0	12	1.96
173.74	175.26	1.46	20	7.5	0	0	0	1	0	0	0	0	0	0	0	0	0	0	12.5	1.92
175.26	176.78	1.45	19	6	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	9	1.40
176.78	178.31	1.39	17	7	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.38
178.31	179.83	1.39	13	5.5	1.5	0	1	0	0	0	0	0	0	0	0	0	0	0	12.5	2.02
179.83	181.36	1.43	27	6	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	14	2.19
181.36	182.88	1.39	20	7	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	12	1.94
182.88	184.40	1.43	14	4.5	1	0.5	1	0	0	0	0	0	0	0	0	0	0	0	12	1.88
184.40	185.93	1.39	14	4	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	9.5	1.54
185.93	187.45	1.31	14	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
187.45	188.98	1.34	16	5	0.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	8	1.34
188.98	190.50	1.30	14	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.78
190.50	192.02	1.28	8	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.61
192.02	193.55	1.31	16	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.69
193.55	195.07	1.37	15	3	1	0	0.5	0	0	0	0	0	0	0	0	0	0	0	7	1.15
195.07	196.60	1.36	5	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.41
[illegible].60	198.12	1.17	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
198.12	199.64	1.08	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
199.64	201.17	1.01	11	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.11
201.17	202.69	1.23	11	3.5	0	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	8	1.45
202.69	204.22	1.39	11	11	3.5	2.5	2	0.5	0	0	0	0	0	0	0	0	0	0	36	5.83
204.22	205.74	1.43	23	8.5	3.5	3	1	1.5	1.5	0.5	0	0	0	0	0	0	0	0	49	7.68
205.74	207.26	1.46	18	8	3	2	1	1.5	0.5	0	0	0	0	0	0	0	0	0	34.5	5.29
207.26	208.79	1.37	19	10.5	4	1	0.5	1	0	0	0	0	0	0	0	0	0	0	28.5	4.66
208.79	210.31	1.37	9	4.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	7	1.15
210.31	211.84	1.39	17	8	2	0	1.5	0	0.5	0	0	0	0	0	0	0	0	0	21	3.40
211.84	213.36	1.46	14	11	2.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	24.5	3.76
213.36	214.88	1.39	17	6	3	0.5	1	0	0.5	1	0	0.5	0.5	0	0	0	0	0	41.5	6.72
214.88	216.41	1.36	14	10	2.5	2	0.5	1	0	0.5	0	0	0	0	0	0	0	0	32	5.30
216.41	217.93	1.28	14	10.5	1.5	2.5	1	1	2	0.5	0	0	0	0	0	0	0	0	46	8.07
217.93	219.46	0.99	16	8	1.5	1	0.5	0	0	0.5	0	0.5	0	0	0	0	0	0	26	5.89
219.46	220.98	0.73	11	1.5	0	1	1	0.5	0.5	0	0	0	0	0	0	0	0	0	14	4.30
220.98	222.50	0.98	14	4.5	0.5	1	0	0.5	0.5	0.5	0	0.5	0	0	0	0	0	0	24	5.52
222.50	224.03	1.25	17	1.5	0	0	0	0.5	0	0	0.5	1	0.5	0	1	0	0	0	46	8.26
224.03	225.55	1.11	15	1	0	0	0	1.5	1.5	0.5	0.5	1	0	1	0	0	0	0	54.5	11.00
225.55	227.08	1.25	13	2	0.5	0	0	0	1	0.5	0.5	0	0.5	0	0	0	0	1	49	8.80
227.08	228.60	0.88	15	4	1.5	1	0	0	0	1	0	0	0	0	1	0	0	0	36	9.14

EOH=228.6m.

U8626 CCRG

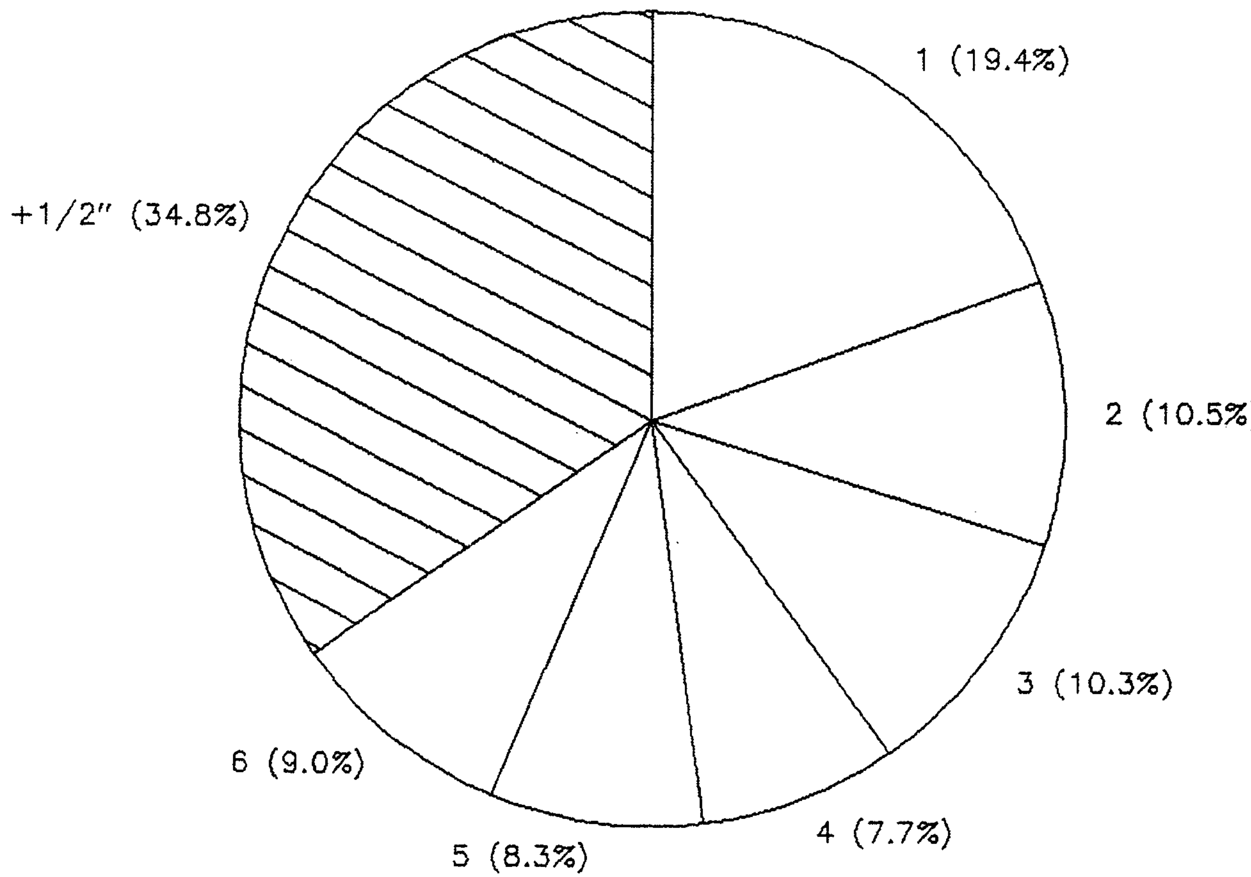

CCRG(%)
11
10
9
8
7
6
5
4
3
2
1
0
1.52
24.38
47.24
70.10
92.96
115.82
138.68
161.54
184.40
207.26
METERAGE


U8626 RMR
30
28
26
24
22
20
18
16
14
12
10
8
6
4
2
0
RMR
1.52
24.38
47.24
70.10
92.96
115.82
138.68
161.54
184.40
207.26
METERAGE


U8626 LENGTH DISTRIBUTION
FOR 202.7m. to 228.6m.(EOH) AVE.=6.16FF
PERCENT
0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16ths.)

U8626 LENGTH DISTRIBUTION

FOR 202.7m. to 228.6m.(EOH) AVE.=6.16FF



DIAMOND DRILL CORE GEOLOGY LOG

PROPERTY	McDame	HOLE	86-27	DEPTH	218.54 m
AZIMUTH	157.3°	INCLINATION	-35°	SECTION	
LATITUDE	6676.2N	DEPARTURE	7681.6E	ELEVATION	1415.2 m
STARTED	Jan. 20/87	FINISHED	Feb. 2/87	LOGGED	by DBP date

LEGEND

W	OVERBURDEN
B	SLATE
C	CARBONATE
Q	QUARTZITE
D	DIORITE
V	VOLCANIC
S	SERPENTINE
	SHEARING

SCALE:

FROM Metres	TO	LENGTH	DESCRIPTION	VISUAL LOG
0.9	9.5		Serpentinite, medium dark green, broken and blocky, minor fibre,	
			lizardite and Magnetite stringers.	
9.5	22.3		Fault zone, broken and shattered.	
22.3	128.0		Medium green to light green with good fibre	
			Fault 45.1 - 50.6, minor fibre	
			68.27 Reduce HQ to NQ	
			Fault 108.2 - 112.2	
			Serpentine medium dark green below 80 m, fibre gradually	
			decreases.	
128.0	218.5		Medium dark green, minor fibre	
			Fault 141.1 - 159.4, shattered, some gouge	
			156.4 Reduce NQ to BQ	
			Fault 217 - 218.5	
218.5			E.O.H. Lost in fault	

H U86-27

EAST:7681.6m. AZ:+157.3
NORTH:6676.2m. INCL:-35.00
ELEV:1415.2m. DEPTH:218.54m.

AVERAGE OF TWO COUNTS

Number of fibre veins counted per 16th category

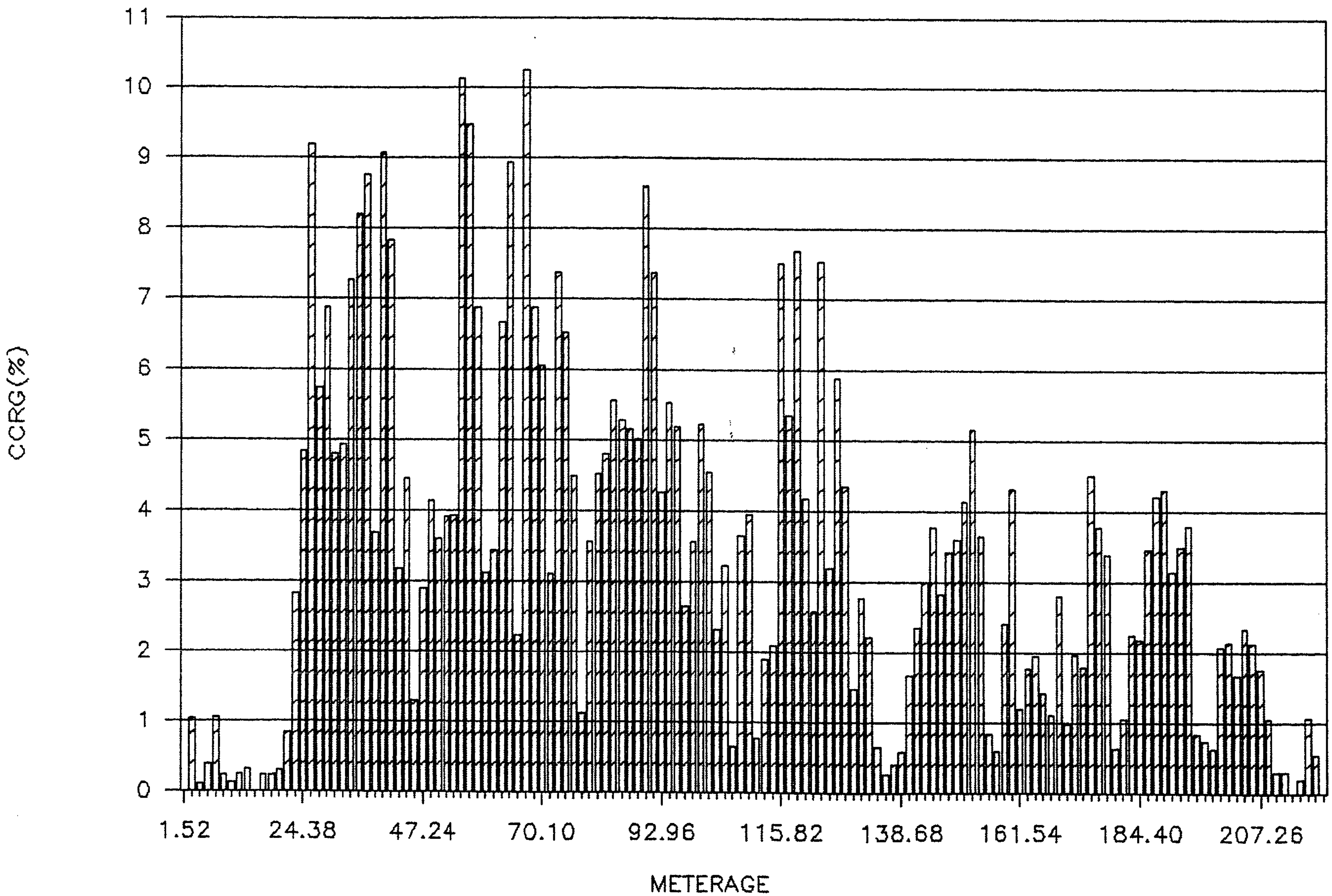
FROM M	TO M	REC M	RMR	1	2	3	4	5	6	8	10	12	14	16	18	20	22	24	TOTAL 16's	CCRG %
0.00	1.52	0.61	23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
1.52	3.05	0.87	22	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	1.03
3.05	4.57	1.07	22	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.11
4.57	6.10	1.19	22	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0.38
6.10	7.62	1.17	22	5.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.05
7.62	9.14	0.99	16	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.23
9.14	10.67	0.94	15	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.12
10.67	12.19	0.93	17	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.24
12.19	13.72	1.10	21	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.31
13.72	15.24	0.88	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
15.24	16.76	0.99	10	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.23
16.76	18.29	1.01	10	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0.22
18.29	19.81	1.19	11	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.28
19.81	21.34	1.20	11	2.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	4.5	0.84
21.34	22.86	1.19	18	7	2.5	1	0	0	0	0	0	0	0	0	0	0	0	0	15	2.83
22.86	24.38	1.25	17	6	4.5	0	1	1	0.5	0	0	0	0	0	0	0	0	0	27	4.85
24.38	25.91	1.22	17	7.5	3.5	2.5	1	1	2.5	0.5	0	0	0	0	0	0	0	0	50	9.21
25.91	27.43	1.17	21	9.5	3.5	1.5	0	0	1.5	0	0	0	0	0	0	0	0	0	30	5.74
27.43	28.96	1.17	17	3.5	3.5	1	1	0.5	1	0.5	0	0.5	0	0	0	0	0	0	36	6.89
28.96	30.48	1.36	17	9.5	3	1.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	29	4.80
30.48	32.00	1.30	25	4.5	1.5	1	1.5	0	2	0	0	0	0	0	0	0	0	0	28.5	4.94
32.00	33.53	1.25	17	9	2	2	1.5	1.5	0.5	0	0.5	0	0	0	0	0	0	0	40.5	7.28
33.53	35.05	1.20	27	8	2.5	0.5	3	0.5	0	0	0	0	0.5	0.5	0	0	0	0	44	8.20
35.05	36.58	1.20	18	5.5	1.5	3	1.5	1.5	0.5	1	0.5	0	0	0	0	0	0	0	47	8.76
36.58	38.10	1.28	19	7.5	1	1	1.5	0.5	0	0	0	0	0	0	0	0	0	0	21	3.68
38.10	39.62	1.25	17	5	3	2.5	3	0	0	1	0	1	0	0	0	0	0	0	50.5	9.07
39.62	41.15	1.19	17	4.5	3	0.5	2	0.5	1	1	0.5	0	0	0	0	0	0	0	41.5	7.84
41.15	42.67	1.20	17	4.5	1.5	1	1	0.5	0	0	0	0	0	0	0	0	0	0	17	3.17
42.67	44.20	1.23	19	9	3	1	1	0.5	0	0	0	0	0	0	0	0	0	0	24.5	4.46
44.20	45.72	1.13	16	4	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.29
45.72	47.24	1.28	12	1.5	1.5	0.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	16.5	2.89
47.24	48.77	1.25	11	1.5	1.5	1.5	2	0	1	0	0	0	0	0	0	0	0	0	23	4.13
48.77	50.29	1.37	10	6	2	0	1.5	0	1	0	0	0	0	0	0	0	0	0	22	3.60
50.29	51.82	1.43	12	9	0	1.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	25	3.92
51.82	53.34	1.37	24	7	3.5	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	0	24	3.93
53.34	54.86	1.34	18	7.5	4	0.5	1.5	1.5	1	3	0	0	0	0	0	0	0	0	60.5	10.13
54.86	56.39	1.22	23	5	0.5	2	1	0.5	0.5	0.5	1	0	0.5	0	0.5	0	0	0	51.5	9.48
56.39	57.91	1.39	19	4.5	2	0.5	1.5	1.5	0	1.5	0	0	0.5	0	0	0	0	0	42.5	6.88
57.91	59.44	1.40	11	9.5	1.5	0	0	0	0.5	0.5	0	0	0	0	0	0	0	0	19.5	3.12
59.44	60.96	1.40	24	6	1	0	0.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	21.5	3.44
60.96	62.48	1.45	16	4.5	3.5	2	2.5	0.5	0	1	0.5	0	0	0	0	0	0	0	43	6.67
62.48	64.01	1.36	23	6	2	0.5	2	2.5	1	1	0	0	0	0.5	0	0	0	0	54	8.94
64.01	65.53	1.31	28	6.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	13	2.23
65.53	67.06	1.36	16	3	1	2.5	0.5	0.5	0.5	3	0.5	0.5	0.5	0	0	0	0	0	62	10.26
67.06	68.58	1.16	19	2	0.5	1	0.5	0.5	1	0.5	1.5	0	0	0	0	0	0	0	35.5	6.88
68.58	70.10	1.04	19	8	0.5	1	0.5	1	0	0.5	0.5	0	0	0	0	0	0	0	28	6.07
70.10	71.63	1.05	15	4.5	2.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	14.5	3.10
71.63	73.15	1.07	9	5.5	0.5	1.5	0	0	1.5	0	0	0	0.5	0.5	0	0	0	0	35	7.37

3.15	74.68	1.22	17	4	1	0.5	1	0	1	0	0	0	0	0.5	0	0.5	0	0	35.5	6.54
74.68	76.20	1.37	25	5	1.5	0	2	0.5	0	0.5	0.5	0	0	0	0	0	0	0	27.5	4.50
76.20	77.72	1.40	17	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7	1.12
77.72	79.25	1.36	25	4.5	1	0.5	0.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	21.5	3.56
79.25	80.77	1.26	27	6	1.5	1.5	3	0	0	0	0	0	0	0	0	0	0	0	25.5	4.53
80.77	82.30	1.49	24	6	3	1.5	1	0.5	0	0.5	0.5	0	0	0	0	0	0	0	32	4.81
82.30	83.82	1.43	14	7.5	2.5	2	0	2	0.5	0.5	0	0	0	0	0	0	0	0	35.5	5.56
83.82	85.34	1.51	21	12.5	4	1.5	2	0.5	0	0	0	0	0	0	0	0	0	0	35.5	5.28
85.34	86.87	1.48	12	4.5	1.5	1	1.5	0.5	1	0.5	0.5	0	0	0	0	0	0	0	34	5.16
86.87	88.39	1.39	21	9.5	2.5	0.5	2	0	0.5	0.5	0	0	0	0	0	0	0	0	31	5.02
88.39	89.92	1.45	30	6	2	2	0.5	0.5	0	1	0.5	0.5	0.5	0	0.5	0	0	0	55.5	8.61
89.92	91.44	1.46	28	6.5	2.5	1	1.5	1.5	0.5	0	0.5	1	0	0	0	0	0	0	48	7.37
91.44	92.96	1.45	17	7	4	1	1	0.5	0.5	0	0	0	0	0	0	0	0	0	27.5	4.26
92.96	94.49	1.40	30	4	1	1	3.5	0.5	0	0.5	0.5	0	0	0	0	0	0	0	34.5	5.52
94.49	96.01	1.30	11	9	1.5	2	0	0	0.5	0.5	0.5	0	0	0	0	0	0	0	30	5.20
96.01	97.54	1.40	19	5.5	1.5	1	0.5	0	0.5	0	0	0	0	0	0	0	0	0	16.5	2.64
97.54	99.06	1.30	18	9	1.5	0.5	1	0	0.5	0	0	0	0	0	0	0	0	0	20.5	3.55
99.06	100.58	1.42	20	7	7	0.5	0	1.5	0.5	0	0	0	0	0	0	0	0	0	33	5.23
100.58	102.11	1.31	20	7.5	4	1	2	0	0	0	0	0	0	0	0	0	0	0	26.5	4.54
102.11	103.63	1.26	17	6.5	0.5	0.5	0	0	0	0.5	0	0	0	0	0	0	0	0	13	2.31
103.63	105.16	1.36	28	4.5	3.5	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	19.5	3.23
105.16	106.68	1.39	31	2.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	4	0.65
106.68	108.20	1.39	26	8.5	1.5	1	0	1	0.5	0	0	0	0	0	0	0	0	0	22.5	3.64
108.20	109.73	1.28	8	6	3	1.5	1.5	0	0	0	0	0	0	0	0	0	0	0	22.5	3.95
109.73	111.25	1.17	16	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.77
1.25	112.78	1.31	11	10	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	11	1.88
2.78	114.30	1.51	13	7	1.5	0	0	0	0	0.5	0	0	0	0	0	0	0	0	14	2.08
114.30	115.82	1.51	25	6	1.5	2.5	2.5	0	1	0	0.5	0.5	0.5	0	0	0	0	0	50.5	7.51
115.82	117.35	1.51	28	12	3.5	1.5	0.5	0.5	0	1	0	0	0	0	0	0	0	0	36	5.36
117.35	118.87	1.40	23	15	3.5	2.5	2	0.5	0.5	0	0.5	0	0	0	0	0	0	0	48	7.69
118.87	120.40	1.34	18	9	1.5	1	0.5	1	0.5	0	0	0	0	0	0	0	0	0	25	4.18
120.40	121.92	1.31	19	7	1	0	0.5	0	0	0.5	0	0	0	0	0	0	0	0	15	2.57
121.92	123.44	0.66	22	2.5	1	0	0.5	0.5	0	0	0	0.5	0.5	0	0	0	0	0	22	7.54
123.44	124.97	1.37	17	5.5	3	0	0.5	0	1	0	0	0	0	0	0	0	0	0	19.5	3.19
124.97	126.49	1.43	24	9.5	1	1	1	0	1	0	0	0.5	0.5	0	0	0	0	0	37.5	5.88
126.49	128.02	1.34	21	7	1.5	1	1	0	0.5	0	0	0.5	0	0	0	0	0	0	26	4.35
128.02	129.54	1.37	17	2.5	1.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	9	1.47
129.54	131.06	1.30	27	8	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	16	2.77
131.06	132.59	1.37	21	5.5	1.5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	13.5	2.21
132.59	134.11	1.40	19	3	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.64
134.11	135.64	1.31	15	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.26
135.64	137.16	1.40	17	2.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.40
137.16	138.68	1.39	27	3.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.57
138.68	140.21	1.36	10	3.5	1	1.5	0	0	0	0	0	0	0	0	0	0	0	0	10	1.66
140.21	141.73	1.30	10	7	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	13.5	2.34
141.73	143.26	1.31	9	8.5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	0	17.5	3.00
143.26	144.78	1.34	16	7	1.5	2	1	0.5	0	0	0	0	0	0	0	0	0	0	22.5	3.77
144.78	146.30	1.23	16	7.5	0	2	0.5	0	0	0	0	0	0	0	0	0	0	0	15.5	2.82
146.30	147.83	1.31	16	4	2	2.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	20	3.43
147.83	149.35	1.22	18	5.5	3	0.5	1	0.5	0	0	0	0	0	0	0	0	0	0	19.5	3.59
149.35	150.88	1.25	16	7.5	3.5	1	0	0.5	0.5	0	0	0	0	0	0	0	0	0	23	4.13
.88	152.40	1.48	10	5.5	4	2.5	1.5	0	0.5	0.5	0	0	0	0	0	0	0	0	34	5.16
152.40	153.92	1.30	11	8	3	1	1	0	0	0	0	0	0	0	0	0	0	0	21	3.64
153.92	155.45	1.07	9	2	1	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0.84
155.45	156.97	0.58	9	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.58
156.97	158.50	0.56	8	2	0	0	1	0	0	0	0	0	0	0	0	0	0	0	6	2.39

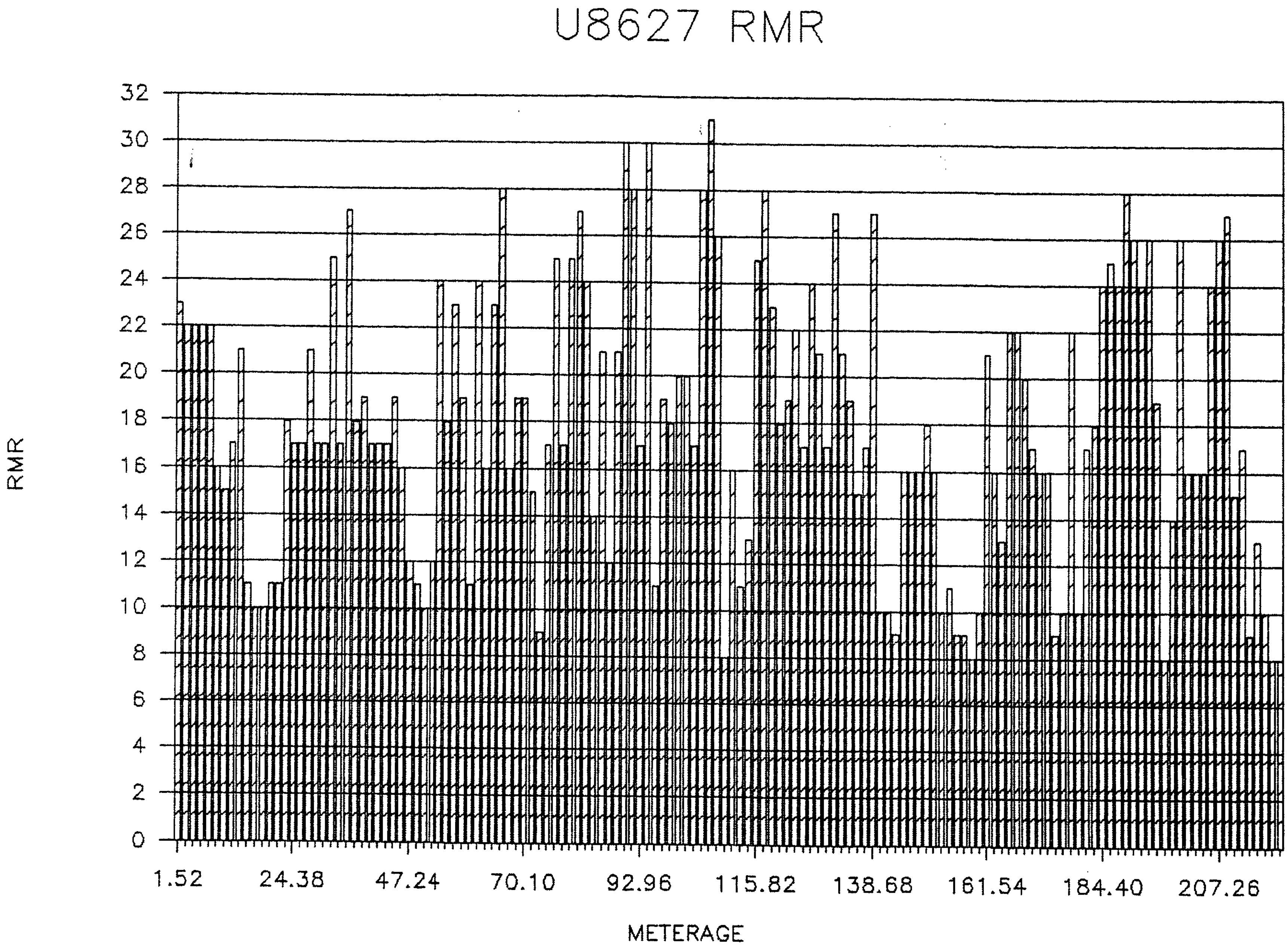
8.50	160.02	0.81	10	6.5	1	1	1	0	0	0	0	0	0	0	0	0	0	0	15.5	4.31
160.02	161.54	1.14	21	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.18
161.54	163.07	0.82	16	2	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	6.5	1.77
163.07	164.59	0.81	13	2	0	0	0.5	0	0.5	0	0	0	0	0	0	0	0	0	7	1.95
164.59	166.12	1.34	22	5	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.42
166.12	167.64	1.33	22	6.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.5	1.10
167.64	169.16	1.28	20	6.5	3	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	16	2.81
169.16	170.69	1.14	17	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	0.98
170.69	172.21	0.98	16	5.5	0	1	0	0	0	0	0	0	0	0	0	0	0	0	8.5	1.96
172.21	173.74	1.01	16	3.5	0.5	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	8	1.79
173.74	175.26	0.94	9	3	1	0	1	0	0	0	1	0	0	0	0	0	0	0	19	4.51
175.26	176.78	1.28	10	5.5	2.5	1	0	1	0.5	0	0	0	0	0	0	0	0	0	21.5	3.77
176.78	178.31	1.33	22	12	1	2	0	0	0	0	0	0	0	0	0	0	0	0	20	3.39
178.31	179.83	1.25	10	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.63
179.83	181.36	1.19	17	5.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.5	1.04
181.36	182.88	1.20	18	4	3	0	0.5	0	0	0	0	0	0	0	0	0	0	0	12	2.24
182.88	184.40	1.30	24	7	1	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	2.17
184.40	185.93	1.26	25	5.5	0	1	1.5	1	0	0	0	0	0	0	0	0	0	0	19.5	3.46
185.93	187.45	1.49	24	12.5	1.5	1	1	0.5	0.5	0	0	0	0	0	0	0	0	0	28	4.21
187.45	188.98	1.46	28	5.5	3	0.5	0	0	0.5	0	0	1	0	0	0	0	0	0	28	4.30
188.98	190.50	1.43	26	4.5	1	1.5	1	0	0	0	0.5	0	0	0	0	0	0	0	20	3.13
190.50	192.02	1.45	24	7	3.5	1.5	1	0	0	0	0	0	0	0	0	0	0	0	22.5	3.49
192.02	193.55	1.48	26	8.5	3.5	0.5	2	0	0	0	0	0	0	0	0	0	0	0	25	3.80
193.55	195.07	1.20	19	3.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	4.5	0.84
195.07	196.60	0.93	8	2	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0.72
6.60	198.12	1.25	14	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	3.5	0.63
8.12	199.64	1.31	26	7.5	0	0	0.5	0.5	0	0	0	0	0	0	0	0	0	0	12	2.06
199.64	201.17	1.20	16	6.5	1.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	11.5	2.14
201.17	202.69	1.28	16	7.5	0	0	0.5	0	0	0	0	0	0	0	0	0	0	0	9.5	1.67
202.69	204.22	1.25	16	6.5	2.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	13	2.34
204.22	205.74	1.33	24	5	2	0.5	0.5	0	0	0	0	0	0	0	0	0	0	0	12.5	2.12
205.74	207.26	1.42	26	9.5	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	11	1.74
207.26	208.79	1.28	27	5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	6	1.05
208.79	210.31	1.13	15	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.30
210.31	211.84	1.16	17	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.5	0.29
211.84	213.36	1.11	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00
213.36	214.88	0.62	13	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.18
214.88	216.41	1.05	10	4	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	5	1.07
216.41	217.93	1.05	8	1.5	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5	0.53
217.93	218.54	0.91	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.00

EOH=218.54m.(717')

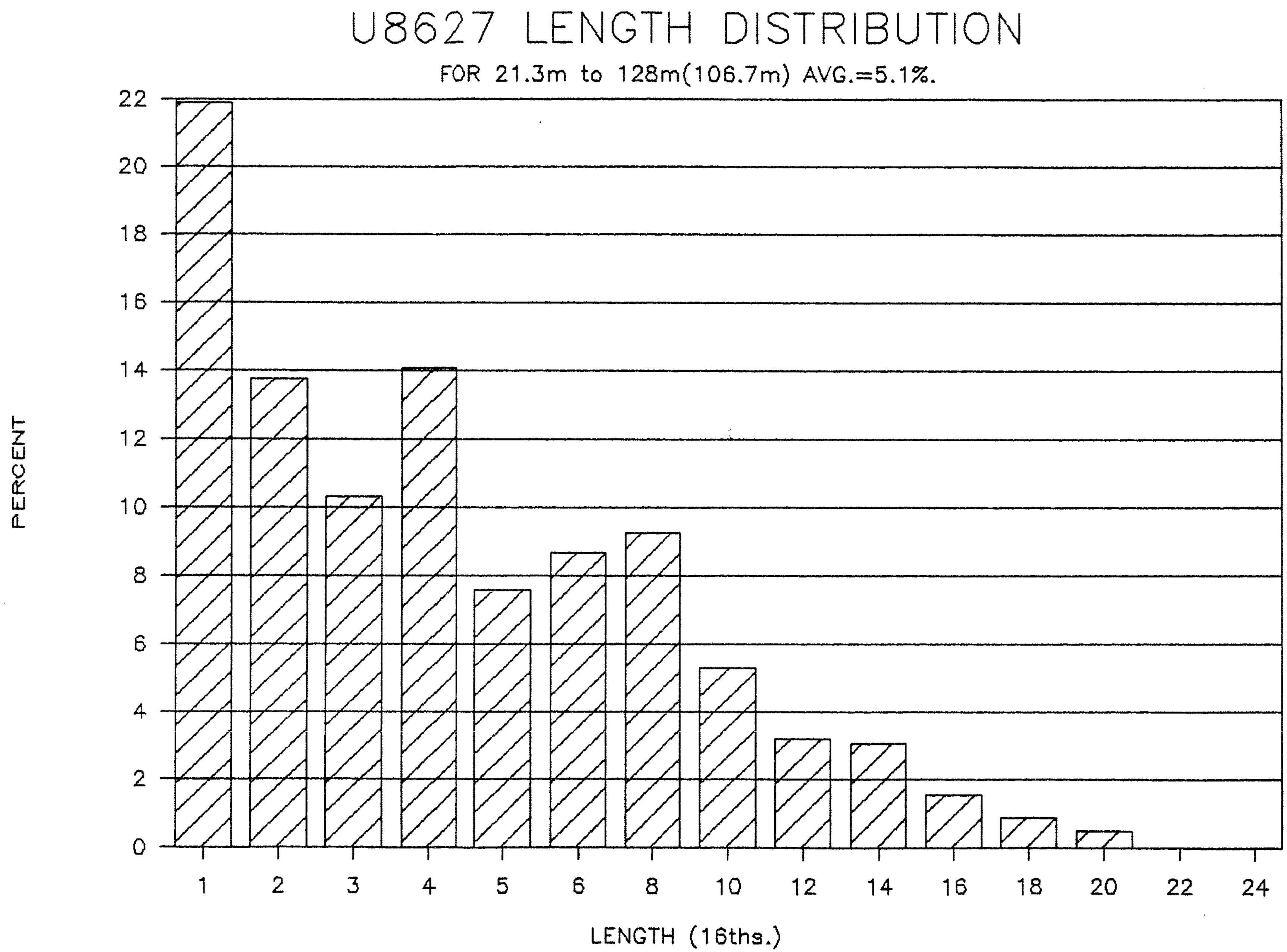
U8627 CCRG



CCRG(%)
0
1
2
3
4
5
6
7
8
9
10
11
1.52
24.38
47.24
70.10
92.96
115.82
138.68
161.54
184.40
207.26
METERAGE

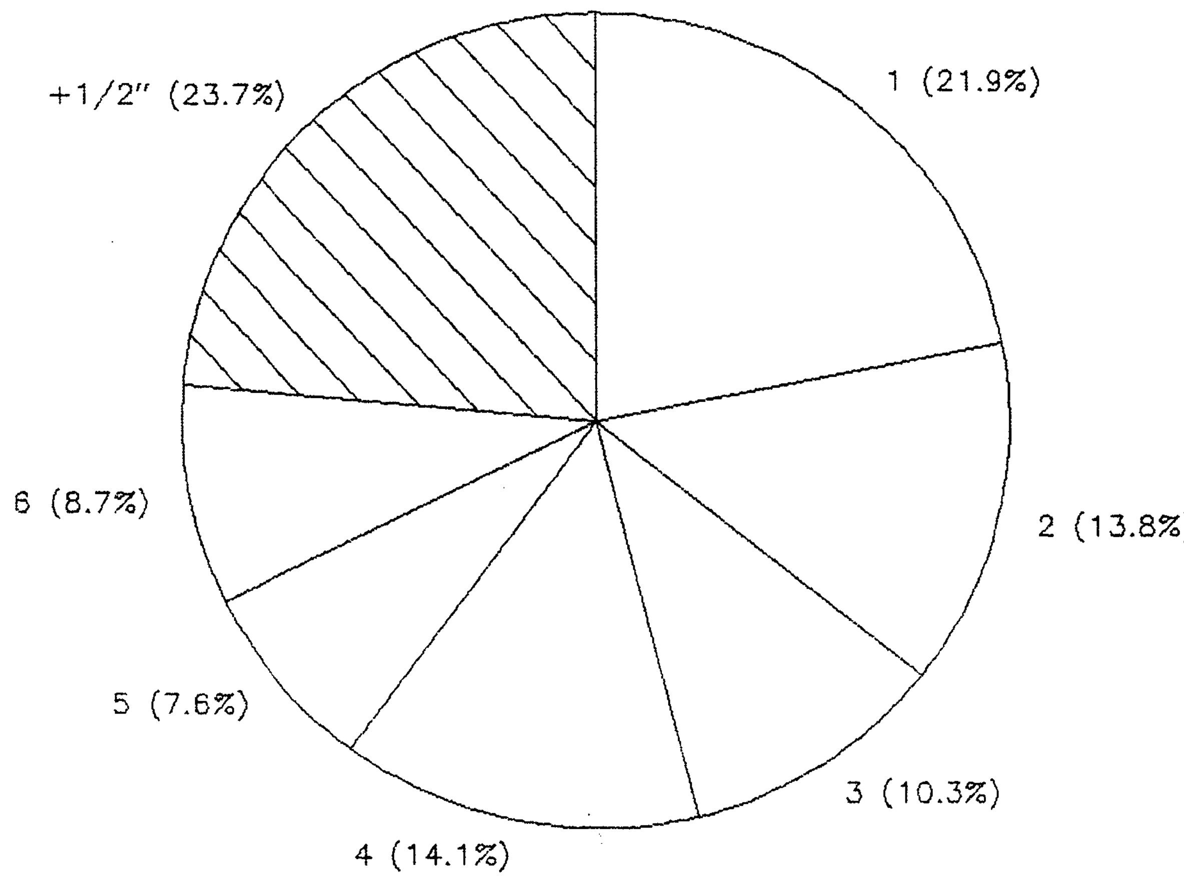


U8627 RMR
RMR
METERAGE
32
30
28
26
24
22
20
18
16
14
12
10
8
6
4
2
0
1.52
24.38
47.24
70.10
92.96
115.82
138.68
161.54
184.40
207.26


U8627 LENGTH DISTRIBUTION
FOR 21.3m to 128m(106.7m) AVG.=5.1%.
PERCENT
0
2
4
6
8
10
12
14
16
18
20
22
1
2
3
4
5
6
8
10
12
14
16
18
20
22
24
LENGTH (16ths.)

U8627 LENGTH DISTRIBUTION

FOR 21.3m to 128m(106.7m) AVG.=5.1%.



APPENDIX V

DRILL HOLE INTERSECTIONS

DRILL HOLE INTERSECTIONS

HOLE NO.	FM (M)	TO (M)	LENGTH (M)	CCRG (%)
U8601	Drilled for geology outside ore zone			
U8602	Drilled for geology outside ore zone			
U8603	0	24.4	24.4	4.23
	24.4	30.2	5.8	0.48
	Hole was abandoned			
U8604	0	129.4	129.4	2.29
	129.4	160.9	31.5	6.51
U8605	0	33.5	33.5	4.31
	33.5	92.4	58.9	10.44
U8606	0	9.1	9.1	3.26
	9.1	16.4	7.3	0.27
U8607	0	56.4	56.4	5.85
	56.4	80.8	24.4	3.68
	80.8	141.4	60.6	6.32
	OR			
	0	141.4	141.4	5.68
U8608	0	35.1	35.1	3.71
	35.1	56.4	21.3	4.85
	56.4	210	153.6	6.24
U8609	0	72.8	72.8	2.31
U8610	0	51.8	51.8	1.95
	51.8	93	41.2	6.79
	93	137.2	44.2	0.45
	137.2	172.2	35	3.63
	172.2	253	80.8	5.26
	253	350.2	97.2	0.63
	OR			
	51.8	248.4	196.6	4.33
U8611	0	53.3	53.3	2.77
	53.5	109.7	56.2	5.83
	109.7	155.4	45.7	1.3
	155.4	199.6	44.2	3.06
	199.6	214.9	15.3	6.03
	214.9	233.2	18.3	3.41
	233.2	269.7	36.5	5.01
	269.7	299.3	29.6	1.73
	OR			
	53.3	269.7	216.4	3.98

U8612	0	12.2	12.2	1.85
	12.2	25.9	13.7	5.08
	25.9	45.7	19.8	1.59
	45.7	86.9	41.2	7.2
	86.9	126.5	39.6	4.09
	126.5	158.5	32	1.68
	158.5	165.2	6.7	0
	OR			
	12.2	126.5	114.3	4.9
U8613	Hole lost in fault zone before fibre			
U8614	0	19.8	19.8	1.47
	19.8	35.1	15.3	4.92
	35.1	62.5	27.4	1.03
	62.5	105.2	42.7	5.23
	105.2	160.02	54.82	1.48
	160.02	168.9	8.88	0
U8615	0	15.2	15.2	2.1
	15.2	62.5	47.3	6.98
	62.5	97.5	35	4.39
	97.5	163.1	65.6	1.35
	163.1	176.8	13.7	4.35
	176.8	184.7	7.9	0
	OR			
	15.24	117.4	102.16	5.16
U8616	0	65.53	65.53	0
	65.53	227.03	161.5	0.39
	227.03	297.18	70.15	0
U8617	0	15.24	15.24	2.11
	15.24	30.48	15.24	4.3
	30.48	74.68	44.2	5.62
	74.68	91.44	16.76	2.93
	91.44	153.92	62.48	4.72
	153.92	167.64	13.72	1.75
	167.64	228.3	60.66	0.13
	OR			
	15.24	153.92	138.68	4.75
U8618	0	7.62	7.62	0
	7.62	45.72	38.1	1.59
	45.72	146.3	100.58	7.22
	146.3	173.74	27.44	3.74
	173.74	264.57	90.83	2.26
	OR			
	44.2	173.74	129.54	6.44
U8619	0	24.38	24.38	0.55
	24.38	39.62	15.24	3.77
	39.62	77.42	37.8	0.57

U8620	0	7.62	7.62	0
	7.62	64.01	56.39	1.05
	64.01	103.63	39.62	3.7
	103.63	111.25	7.62	2.48
	111.25	158.8	47.55	0.02
U8621	0	24.38	24.38	2.12
	24.38	141.73	117.35	4.93
	141.73	190.5	48.77	0.28
	190.5	194.77	4.27	0
U8622	0	225.55	225.55	5.15
	225.55	273.71	48.16	0.62
U8623	0	19.81	19.81	0.2
	19.81	30.48	10.67	4.17
	30.48	50.29	19.81	0.48
	50.29	82.3	32.01	5.74
	82.3	103.63	21.33	1.59
U8624	0	59.4	59.4	1.29
	59.4	143.3	83.9	2.16
	143.3	173.7	30.4	4.53
	173.7	205.7	32	1.34
	205.7	259.08	53.38	3.13
	259.08	260.06	0.98	0.85
U8625	0	146.3	146.3	0.94
	146.3	196.6	50.3	4.79
	196.6	222.5	25.9	1.66
	222.5	259.08	36.58	2.84
	259.08	270.66	11.58	0.03
U8626	0	22.9	22.9	1.87
	22.9	30.5	7.6	3.67
	30.5	56.4	25.9	1.63
	56.4	80.8	24.4	3.63
	80.8	100.6	19.8	0.93
	100.6	152.4	51.8	4.5
	152.4	202.7	50.3	1.45
	202.7	228.6	25.9	6.16

NOTE: HOLE LOST IN HIGH GRADE(LAST SECTION = 9.14%).

U8627	0	21.34	21.34	0.36
	21.34	128.02	106.68	5.08
	128.02	141.73	13.71	1.37
	141.73	193.55	51.82	2.73
	193.55	216.54	22.99	1.04

APPENDIX VI

UNCONFINED STRENGTH TESTING ON CORE SAMPLES

HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

Our Project No. VG-04108
Your Reference No.

August 28, 1986

Cassiar Asbestos Corp.,
#2000 - 1055 W. Hastings St.,
VANCOUVER, B.C.
V6E 3V3

ATTENTION: Mr. R.S. Hewton, P. Eng.

Dear Sirs:

Re: Unconfined Strength Testing
On Cores Supplied.

At your request, we have conducted unconfined strength tests on a total of 7 cores supplied by you. The results are summarized below. In some cases, in spite of special precautions, it was not possible to prepare samples suitable for unconfined compressive strength testing due to the occurrence of frequent microfractures, weak layers or weak asbestos layers. In these cases, we have conducted point load tests which involves loading the sample between two conical plattens. These results may be very approximately correlated to unconfined compressive strength using established correlations.

Results are summarized in Table 1 and other details including sample unit weight are available from the attached laboratory data sheets.

If we can provide any further information or assistance, please do not hesitate to contact us at your convenience.

Yours truly,

HARDY ASSOCIATES (1978) LTD.

Per: DCavers

D.S. Cavers, M.Eng., P. Eng.,
Associate, Geological Engineer.

DSC:wc

Enclosures

4052 GRAVELEY STREET, BURNABY, BRITISH COLUMBIA V5C 3T6 — TELEPHONE (604) 294-3811 — TELEX 04-354841
GEOTECHNICAL AND MATERIALS ENGINEERING — ENVIRONMENTAL, MATERIALS AND CHEMICAL SCIENCES
CALGARY EDMONTON FORT McMURRAY LETHBRIDGE LLOYDMINSTER MEDICINE HAT PEACE RIVER RED DEER
SASKATOON VANCOUVER

TABLE 1

VG-04108

SUMMARY OF RESULTS

SAMPLE	UNCONFINED COMPRESSIVE STRENGTH		POINT LOAD CORRELATED STRENGTH		REMARKS
	MPa	Psi	MPa	Psi	
I-01			19.1 55.1 30.4 112.5 139.5	2770 7890 4408 16312 20227	
I-02	11.4	1653	29.9 73.6	4330 10670	Ribbon Chert. -Premature failure. -Point load results are parallel and perpendicular to banding, respectfully.
I-03	47.4	6873			H/W argillite.
I-04	92.2	13370	28.0	4060	Serpentinite.
I-05	21.7	3150			Serpentinite with asbestos.
I-06	93.7	13590			Serpentinite.
I-07	193.9	28110			
I-08	173.2	25110			Metasiltstone, (argillite), metaquartzite.

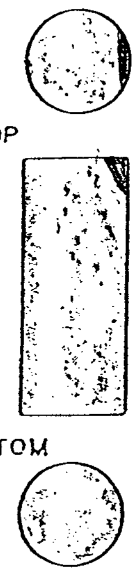
HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING AND PROFESSIONAL SERVICES

UNCONFINED COMPRESSION TEST (ASTM D2938)

JOB Nº. VGO 4108
PROJECT Rock Mechanics
LOCATION
HOLE ______ DEPTH ______ m SAMPLE I-02
TEST DATE 86-08-12 SAMPLE DATE
TECHNICIAN L.P.

ROCK TYPE DESCRIPTION: RIBBON CHERT

SKETCH OF PREPARED SAMPLE



- chipped!

DIAMETER D = 47.3 mm
LENGTH L = 133.4 mm
RATIO L/D = 2.82

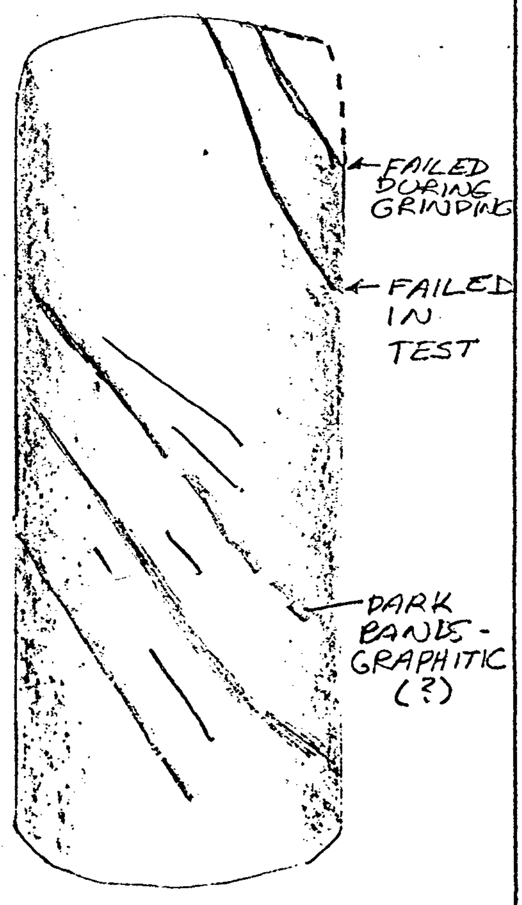
AREA A = $\pi D^2/4 \times 10^{-6}$ = 1.757×10^{-3} m^2
VOLUME V = $A \times L/10^3$ = 2.343×10^{-4} m^3
WEIGHT W = .6681 kg
UNIT WEIGHT W/V = 2851.5 kg/m^3

LOAD DEFORMATION RATE ~~mm/sec~~
= 1.8 kN/sec
MAXIMUM LOAD P = 20 KN
COMPRESSIVE STRENGTH Co = P/A
= 11.4 MPa
UNCONFINED COMPRESSIVE STRENGTH C = K* Co = 11.4 MPa

MOISTURE CONTENT / DEGREE OF SATURATION AT TEST N/A %

SAMPLE STORAGE CONDITIONS:
N/A

FAILURE PHOTOGRAPH/SKETCH



FAILURE CONDITION (TYPE, RAPIDITY, ANGLE OF FAILURE OR CONE, ETC.):
- broke along chipped end of sample ∴ reading is not representative of sample strength.

STRESS/STRAIN CURVE MADE YES ☐ NO ☑
MODULUS TESTING AVAILABLE YES ☐ NO ☑

* IF L/D > 2.0, K = 1.0; IF L/D < 2.0, K = 1/[0.88 + (0.24 D/L)]

PLATE

HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING AND PROFESSIONAL SERVICES

UNCONFINED COMPRESSION TEST (ASTM D2938)

JOB No.: VGO-4108
PROJECT: Rock Mechanics
LOCATION:
HOLE: ______ DEPTH: ______ m SAMPLE: I-03
TEST DATE: 86-08-12 SAMPLE DATE: ______
TECHNICIAN: L.P.

ROCK TYPE DESCRIPTION:
H/W ARGILLITE

DIAMETER D = 63.9 mm
LENGTH L = 120.9 mm
RATIO L/D = 1.89

AREA A = $\pi D^2/4 \times 10^{-6}$ = 3.205×10^{-3} m^2
VOLUME V = $A \times L/10^3$ = 3.875×10^{-4} m^3
WEIGHT W = 1.0775 kg
UNIT WEIGHT W/V = 2780.7 kg/m^3

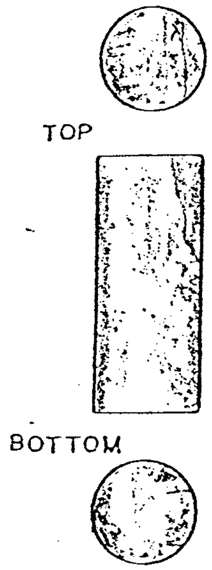
LOAD DEFORMATION RATE ~~mm/sec~~
= 1.8 kN/sec
MAXIMUM LOAD P = 152 kN
COMPRESSIVE STRENGTH Co = P/A
= 47.4 MPa
UNCONFINED COMPRESSIVE STRENGTH C = K* Co = N/A MPa
MOISTURE CONTENT / DEGREE OF SATURATION AT TEST N/A %
SAMPLE STORAGE CONDITIONS:
N/A

FAILURE CONDITION (TYPE, RAPIDITY, ANGLE OF FAILURE OR CONE, ETC.):
FAILURE INITIATED ON QUARTZ VEIN.

STRESS/STRAIN CURVE MADE YES ☐ NO ☑
MODULUS TESTING AVAILABLE YES ☐ NO ☑

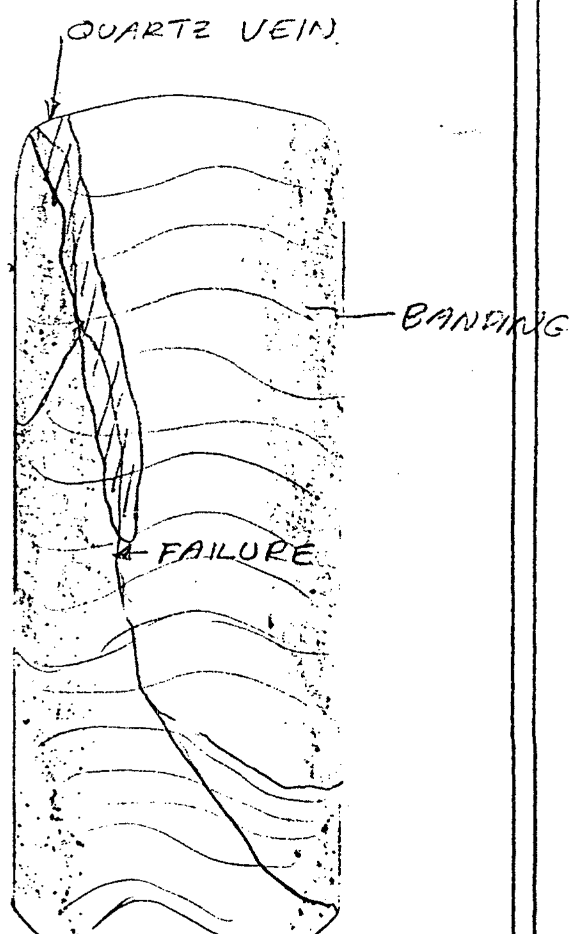
* IF $L/D \geq 2.0$, K = 1.0; IF $L/D < 2.0$, K = $1/[0.88 + (0.24\ D/L)]$

SKETCH OF PREPARED SAMPLE



- few hair line cracks present

FAILURE PHOTOGRAPH/SKETCH



PLATE

HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING AND PROFESSIONAL SERVICES

UNCONFINED COMPRESSION TEST (ASTM D2938)

JOB No. VCO 4108
PROJECT Rock Mechanics
LOCATION
HOLE ______ DEPTH ______ m SAMPLE I-04
TEST DATE 86-08-13 SAMPLE DATE ______
TECHNICIAN L.P.

ROCK TYPE DESCRIPTION:

Serpentinite - dark green
massive

DIAMETER D = 47.3 mm
LENGTH L = 111.1 mm
RATIO L/D = 2.35

AREA A $= \pi D^2/4 \times 10^{-6} =$ 1.757×10^{-3} m^2
VOLUME V $= A \times L/10^3 =$ 1.951×10^{-4} m^3
WEIGHT W = .5185 kg
UNIT WEIGHT W/V = 2657.6 kg/m^3

LOAD DEFORMATION RATE ~~mm/sec~~
= 1.8 kN/sec
MAXIMUM LOAD P = 162 kN
COMPRESSIVE STRENGTH Ca $= P/A$
= 92.2 MPa

UNCONFINED COMPRESSIVE STRENGTH C $= K^* Ca$ = 92.2 MPa

MOISTURE CONTENT / DEGREE OF SATURATION AT TEST N/A / %

SAMPLE STORAGE CONDITIONS:
N/A

FAILURE CONDITION (TYPE, RAPIDITY, ANGLE OF FAILURE OR CONE, ETC.):

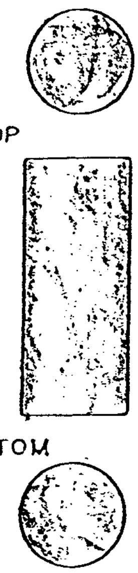
violent
NO OBVIOUS DISCONTINUITIES

STRESS/STRAIN CURVE MADE YES ☐ NO ☑
MODULUS TESTING AVAILABLE YES ☐ NO ☑

* IF $L/D > 2.0$, $K = 1.0$; IF $L/D < 2.0$, $K = 1/[0.88 + (0.24\ D/L)]$

SKETCH OF PREPARED SAMPLE

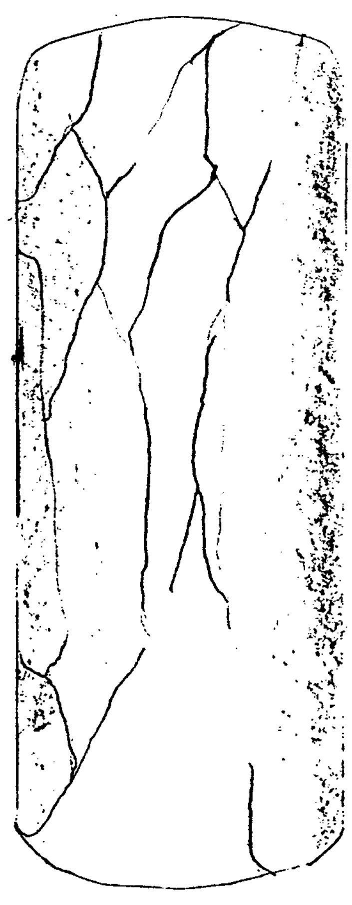
TOP



BOTTOM

NO apparent cracks

FAILURE PHOTOGRAPH/SKETCH



PLATE

HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING AND PROFESSIONAL SERVICES

UNCONFINED COMPRESSION TEST (ASTM D2938)

JOB No. VG04108
PROJECT Rock Mechanics
LOCATION
HOLE ______ DEPTH ______ m SAMPLE I-05
TEST DATE 86-08-13 SAMPLE DATE
TECHNICIAN L.P.

ROCK TYPE DESCRIPTION:

- Serpentinite - massive

DIAMETER D = 47.3 mm
LENGTH L = 87.0 mm
RATIO L/D = 1.84

AREA A = $\pi D^2/4 \times 10^{-6}$ = 1.757×10^{-3} m²
VOLUME V = $A \times L/10^3$ = 1.528×10^{-4} m³
WEIGHT W = .4090 kg
UNIT WEIGHT W/V = 2676.7 kg/m³

LOAD DEFORMATION RATE ~~mm/sec~~
= 1.8 kN/sec

MAXIMUM LOAD P = 38.2 kN

COMPRESSIVE STRENGTH Co = P/A
= 21.7 MPa

UNCONFINED COMPRESSIVE STRENGTH C = K* Co = ______ MPa

MOISTURE CONTENT / DEGREE OF SATURATION AT TEST N/A %

SAMPLE STORAGE CONDITIONS:
N/A

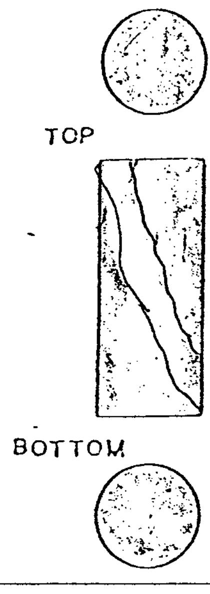
FAILURE CONDITION (TYPE, RAPIDITY, ANGLE OF FAILURE OR CONE, ETC.):

- Failure on asbestos vein
@ 40° to core axis.

STRESS/STRAIN CURVE MADE YES ☐ NO ☑
MODULUS TESTING AVAILABLE YES ☐ NO ☑

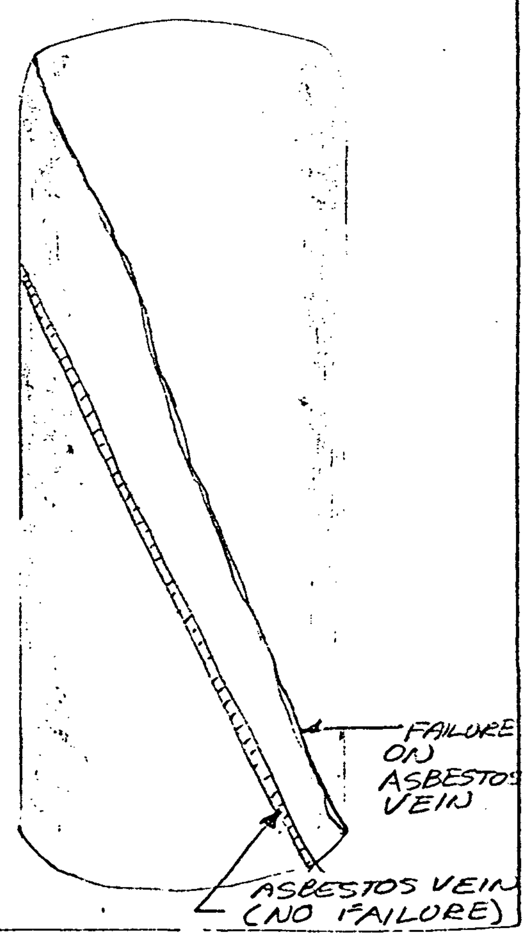
* IF L/D > 2.0, K = 1.0; IF L/D < 2.0, K = 1/(0.88 + (0.24 D/L))

SKETCH OF PREPARED SAMPLE



- NO apparent cracks
- 2 ASBESTOS VEINS AS BELOW.

FAILURE PHOTOGRAPH/SKETCH



PLATE

HARDY ASSOCIATES ( )B) LTD.
CONSULTING ENGINEERING AND PROFESSIONAL SERVICES

UNCONFINED COMPRESSION TEST (ASTM D2938)

JOB Nº VGO 4108
PROJECT Rock Mechanics
LOCATION
HOLE ______ DEPTH ______ m SAMPLE I-06
TEST DATE 86-08-12 SAMPLE DATE ______
TECHNICIAN L.P.

ROCK TYPE DESCRIPTION:

Serpentinite - massive

DIAMETER D = 47.2 mm
LENGTH L = 106.0 mm
RATIO L/D = 2.25

AREA A = $\pi D^2/4 \times 10^{-6}$ = 1.7497×10^{-3} m²
VOLUME V = $A \times L/10^3$ = 1.854×10^{-4} m³
WEIGHT W = .4872 kg
UNIT WEIGHT W/V = 2627.8 kg/m³

LOAD DEFORMATION RATE ~~mm/sec~~
= 1.8 kN/sec
MAXIMUM LOAD P = 164 kN
COMPRESSIVE STRENGTH Co = P/A
= 93.7 MPa
UNCONFINED COMPRESSIVE
STRENGTH C = K* Co = 93.7 MPa
MOISTURE CONTENT / DEGREE OF
SATURATION AT TEST N/A %
SAMPLE STORAGE CONDITIONS:
N/A

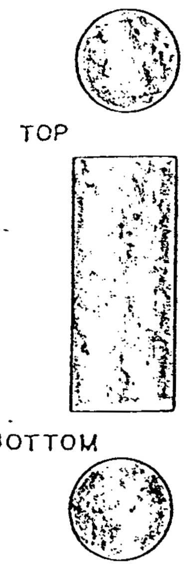
FAILURE CONDITION (TYPE, RAPIDITY, ANGLE OF FAILURE OR CONE, ETC.):

violent
NO OBVIOUS DISCONTINUITIES

STRESS/STRAIN CURVE MADE YES ☐ NO ☑
MODULUS TESTING AVAILABLE YES ☐ NO ☑

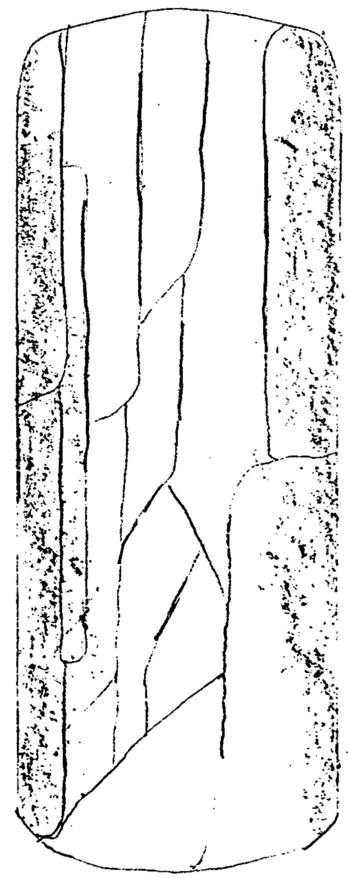
* IF L/D > 2.0, K = 1.0; IF L/D < 2.0,
K = 1/[0.88 + (0.24 D/L)]

SKETCH OF PREPARED SAMPLE



- no apparent cracks

FAILURE PHOTOGRAPH/SKETCH



PLATE

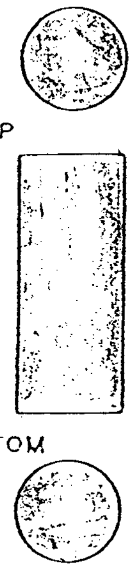
HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING AND PROFESSIONAL SERVICES

UNCONFINED COMPRESSION TEST (ASTM D2938)

JOB Nº. VG04108
PROJECT Rock Mechanics
LOCATION
HOLE ______ DEPTH ______ m SAMPLE 1-07
TEST DATE 86-08-13 SAMPLE DATE ______
TECHNICIAN L.P.

ROCK TYPE DESCRIPTION:

SKETCH OF PREPARED SAMPLE



TOP

BOTTOM

- NO apparent cracks.

DIAMETER D = 63.4 mm
LENGTH L = 95.0 mm
RATIO L/D = 1.50

AREA A = $\pi D^2/4 \times 10^{-6}$ = 3.157×10^{-3} m²
VOLUME V = $A \times L/10^3$ = 2.998×10^{-4} m³
WEIGHT W = .8402 kg
UNIT WEIGHT W/V = 2802.5 kg/m³

LOAD DEFORMATION RATE ~~mm/sec~~
= 1.8 kN/sec

MAXIMUM LOAD P = 612 kN

COMPRESSIVE STRENGTH Co = P/A
= 193.9 MPa

UNCONFINED COMPRESSIVE STRENGTH C = K* Co = ______ MPa

MOISTURE CONTENT / DEGREE OF SATURATION AT TEST N/A %

SAMPLE STORAGE CONDITIONS:
N/A

FAILURE PHOTOGRAPH/SKETCH

FAILURE CONDITION (TYPE, RAPIDITY, ANGLE OF FAILURE OR CONE, ETC.):
violent
NO OBVIOUS DISCONTINUITIES

STRESS/STRAIN CURVE MADE YES ☐ NO ☑
MODULUS TESTING AVAILABLE YES ☐ NO ☑

* IF $L/D \geq 2.0$, K = 1.0; IF $L/D < 2.0$,
$K = 1/[0.88 + (0.24\ D/L)]$

PLATE

HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING AND PROFESSIONAL SERVICES

UNCONFINED COMPRESSION TEST (ASTM D2938)

JOB No. VGO 4108
PROJECT Rock Mechanics
LOCATION
HOLE ____ DEPTH ____ m SAMPLE I-08
TEST DATE 86-08-12 SAMPLE DATE
TECHNICIAN L.P.

ROCK TYPE DESCRIPTION:

Metasiltstone (Argillite)
MetaQuartzite

DIAMETER D = 63.0 mm
LENGTH L = 134.7 mm
RATIO L/D = 2.14

AREA A = $\pi D^2/4 \times 10^{-6}$ = .003117 m^2
VOLUME V = $A \times L/10^3$ = 4.197×10^{-4} m^3
WEIGHT W = 1.1357 kg
UNIT WEIGHT W/V = 2706.0 kg/m^3

LOAD DEFORMATION RATE ~~mm/sec~~
= 1.8 kN/sec

MAXIMUM LOAD P = 540 kN
COMPRESSIVE STRENGTH Co = P/A
= 173.2 MPa
UNCONFINED COMPRESSIVE STRENGTH C = K* Co = 173.2 MPa

MOISTURE CONTENT / DEGREE OF SATURATION AT TEST N/A %

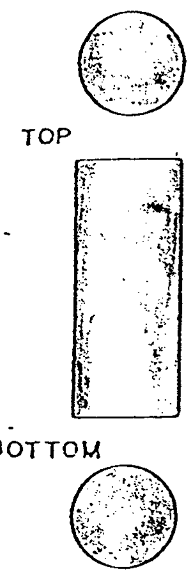
SAMPLE STORAGE CONDITIONS:
N/A

FAILURE CONDITION (TYPE, RAPIDITY, ANGLE OF FAILURE OR CONE, ETC.):
- violent
NO OBVIOUS DISCONTINUITIES

STRESS/STRAIN CURVE MADE YES ☐ NO ☑
MODULUS TESTING AVAILABLE YES ☐ NO ☑

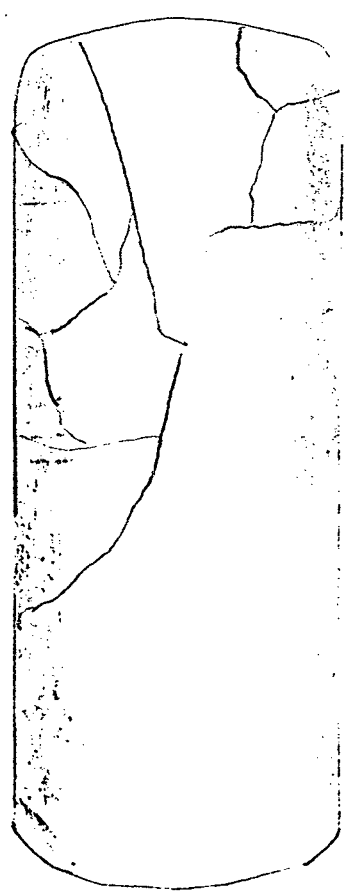
* IF L/D > 2.0, K = 1.0; IF L/D < 2.0,
K = 1/[0.88 + (0.24 D/L)]

SKETCH OF PREPARED SAMPLE



- no apparent cracks.

FAILURE PHOTOGRAPH/SKETCH



PLATE

APPENDIX VII

STATEMENT OF QUALIFICATIONS

STATEMENT OF QUALIFICATIONS

I, Robert S. Hewton of West Vancouver, British Columbia, hereby certify that:

1) I am a geologist residing at 2709 Marine Drive, West Vancouver, B.C., and am currently employed by Cassiar Mining Corporation of #2000 - 1055 West Hastings Street, Vancouver, B.C. V6E 3V3.

2) I graduated from McMaster University, Hamilton, Ontario with a B.Sc. in Geology in 1969 and have practised by profession since.

3) I am currently registered with the Association of Professional Engineers for the Province of British Columbia and with the Association of Professional Engineers of Yukon Territory.

4) I am a Fellow of the Geological Association of Canada, a Member of the Canadian Institute of Mining and Metallurgy and a Member of the Society of Economic Geologists.

5) Work on the property was done under my direct supervision.

Respectfully,

CASSIAR MINING CORPORATION

Robert S Hewton

R.S. Hewton, P.Eng.

Dated at Vancouver, British Columbia
this 20th day of February, 1987

CASSIAR MINING CORPORATION
(Cassiar Mine)
Bag 1000, Cassiar, B.C. V0C 1E0
Telephone: (604) 778-7435
Telex: 036-88533

Statement of Qualifications:

I, Keith C. Minty graduated from Queen's University at Kingston, Ontario with a B.Sc. in Mining Engineering in 1978. Upon graduation I obtained employment with Bamangwato Concessions Limited at Selebi-Pikwe, Botswana as an Underground Production Shift Boss. In 1979, I joined Fording Coal Limited at Elkford, British Columbia as a Mine Planning Engineer in which I was involved in all aspects of open pit coal mine engineering planning and production. In 1983, I joined Giant Yellowknife Gold Mines at Yellowknife, NorthWest Territories as the Ventilation Engineer. At Giant Yellowknife Mines Limited, I also held the positions of Project Engineer and Acting Chief Engineer. In May 1987, I joined Cassiar Mining Corporation at Cassiar, British Columbia as the Chief Engineer.

I am registered as a Professional Engineer and in good standing in the Province of British Columbia (Reg. No.13796) and in the NorthWest Territories (Reg. No. 1089).

Keith C. Minty, P. Eng.

STATEMENT OF QUALIFICATIONS

I, Alfred A. Burgoyne, do hereby certify:

1. I am a Geologist residing at 912 York Street, New Westminster, B.C. V3L 4S4.

2. I am currently employed by Cassiar Mining Corporation, Suite 2000 - 1055 West Hastings Street, Vancouver, B.C. V6E 3V3 as Vice President, Exploration.

3. I graduated from the University of British Columbia in 1962 with a Bachelor of Science Degree in Geology and from the University of New Mexico in 1967 with a Master of Science Degree in Geology.

4. I am a registered Professional Engineer in the Association of Professional Engineers for the Province of British Columbia and Yukon Territory.

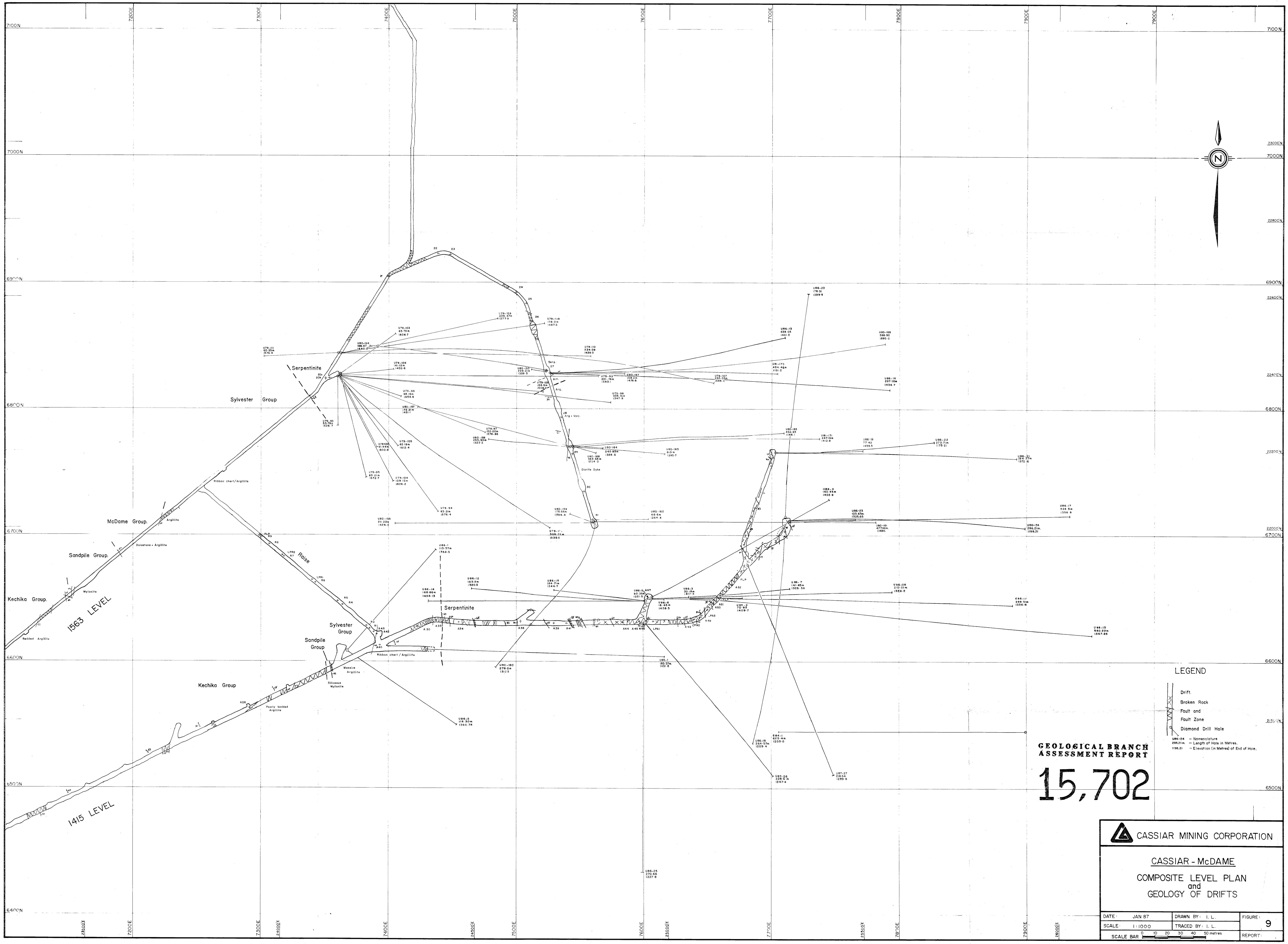
5. I am registered as a Fellow of the Geological Association of Canada, and as a member of the Canadian Institute of Mining and Metallurgy and the Association of Exploration Geochemists.

6. I have practised my profession for over 24 years.

Dated at Vancouver, British Columbia,
this 20th day of February, 1987

AA Burgoyne

A.A. Burgoyne, P. Eng.

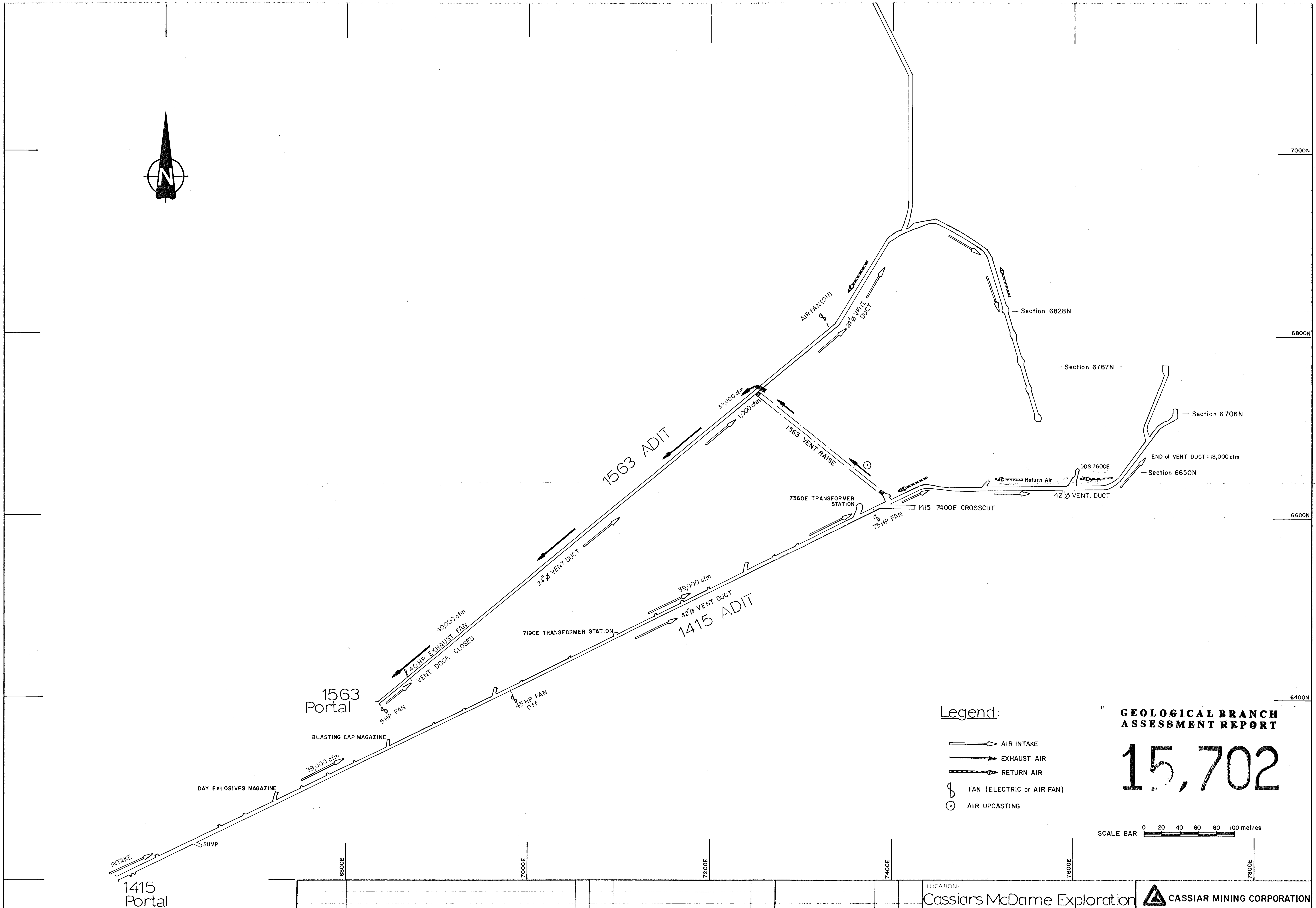


CASSIAR MINING CORPORATION

CASSIAR - McDAME

COMPOSITE LEVEL PLAN
and
GEOLOGY OF DRIFTS

DATE: JAN 87	DRAWN BY: I. L.	FIGURE:	9
SCALE: 1:1000	TRACED BY: I. L.		
SCALE BAR 0 10 20 30 40 50 metres		REPORT:	



DRWG. No.	REFERENCE	No.	DATE	REVISIONS	BY	ISSUED FOR ABOVE PURPOSE	DATE	APP'D

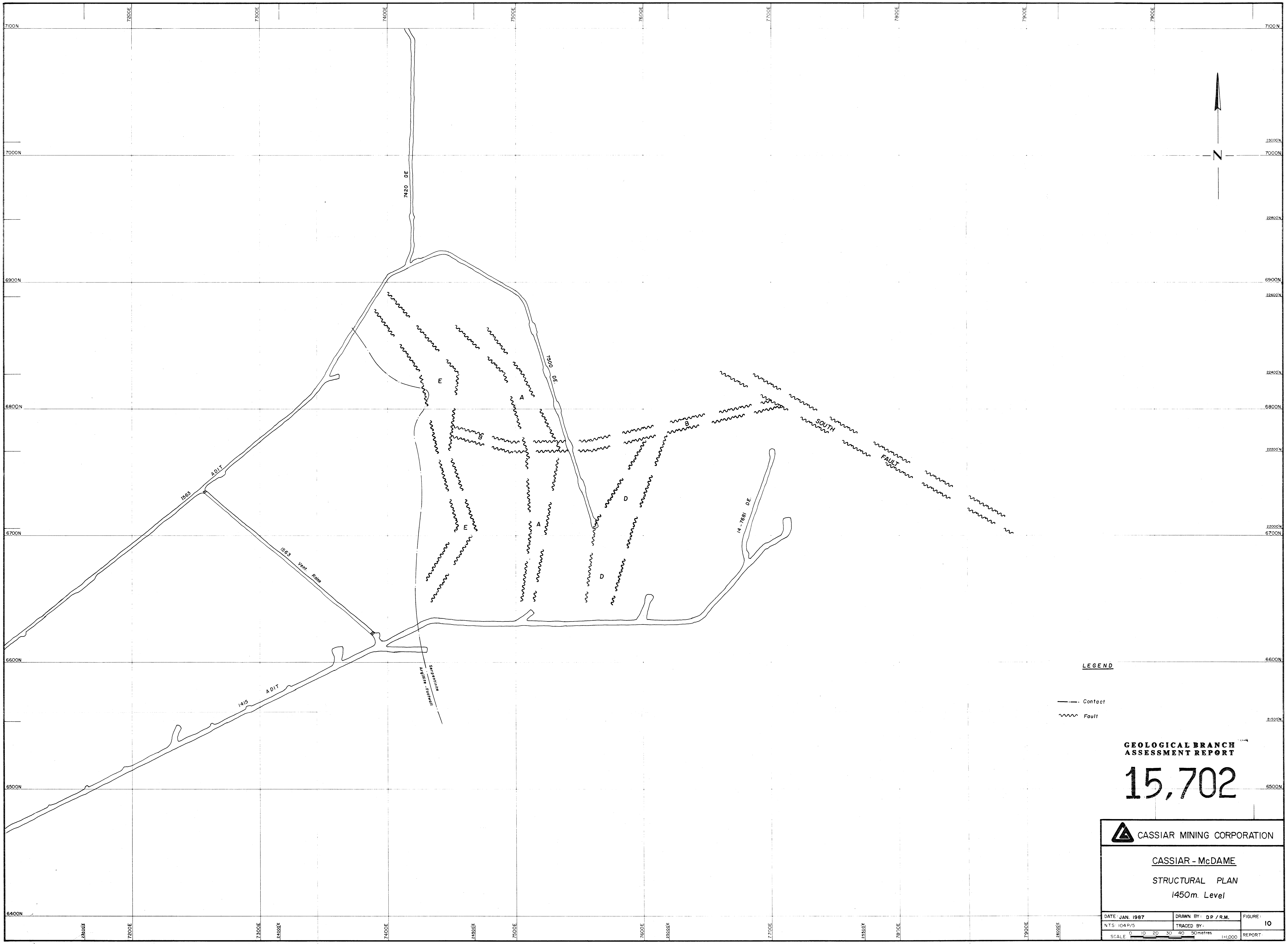
LOCATION: Cassiars McDame Exploration

TITLE: **VENTILATION SYSTEM**

CASSIAR MINING CORPORATION

DRAWN BY RIZ MISLANG	DATE OCT 10, 86
CHECKED BY	DATE:
APPROVED BY	DATE:
SECTION	PROJ. No.
SCALE 1:2000	FIGURE 4 — REV

WEST
EAST
1600m
1500m
1400m
1300m
1200m
1100m
1000m
7200E
7300E
7400E
7500E
7600E
7700E
7800E
7900E
8000E
8100E
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,702
CASSIAR MINING CORPORATION
CASSIAR - McDAME
SECTION 6650m.N (21,818')
AVERAGE GRADE
SCALE: 0 10 20 30 40 50 metres
DATE: NOVEMBER, 1986
DRAWN BY: H. Holm
FIGURE: 11
SCALE: 1:1000
TRACED BY:
REPORT:



GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,702

CASSIAR MINING CORPORATION

CASSIAR - McDAME

STRUCTURAL PLAN
1450m. Level

DATE: JAN. 1987	DRAWN BY: DP / R.M.	FIGURE: 10
N.T.S. 104P/5	TRACED BY:	
SCALE 0 10 20 30 40 50 metres 1:1,000		REPORT

WEST
EAST
7200E
7300E
7400E
7500E
7600E
7700E
7800E
7900E
8000E
8100E
1600
1500
1400
1300
1200
1100
1000
1563 ADIT
U79-94
E.O.H. 132m.
X-CUT
U80-160
21m.
U80-158
211.2m
U80-159
175.6m
U79-101
308.8m.
263m.
U81-162
415.8m.
U81-161
477.6m
U86-20
U86-6
83.63m.
145.76m.
U86-23
103.63m.
U86-17
228.3m.
U86-24
286.21m.
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,702
CASSIAR MINING CORPORATION
CASSIAR - McDAME
SECTION 6706 m.N (22,000')
AVERAGE GRADE
SCALE 0 10 20 30 40 50 metres
DATE:
SCALE: 1:1000
DRAWN BY:
TRACED BY:
FIGURE: 12
REPORT

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,702

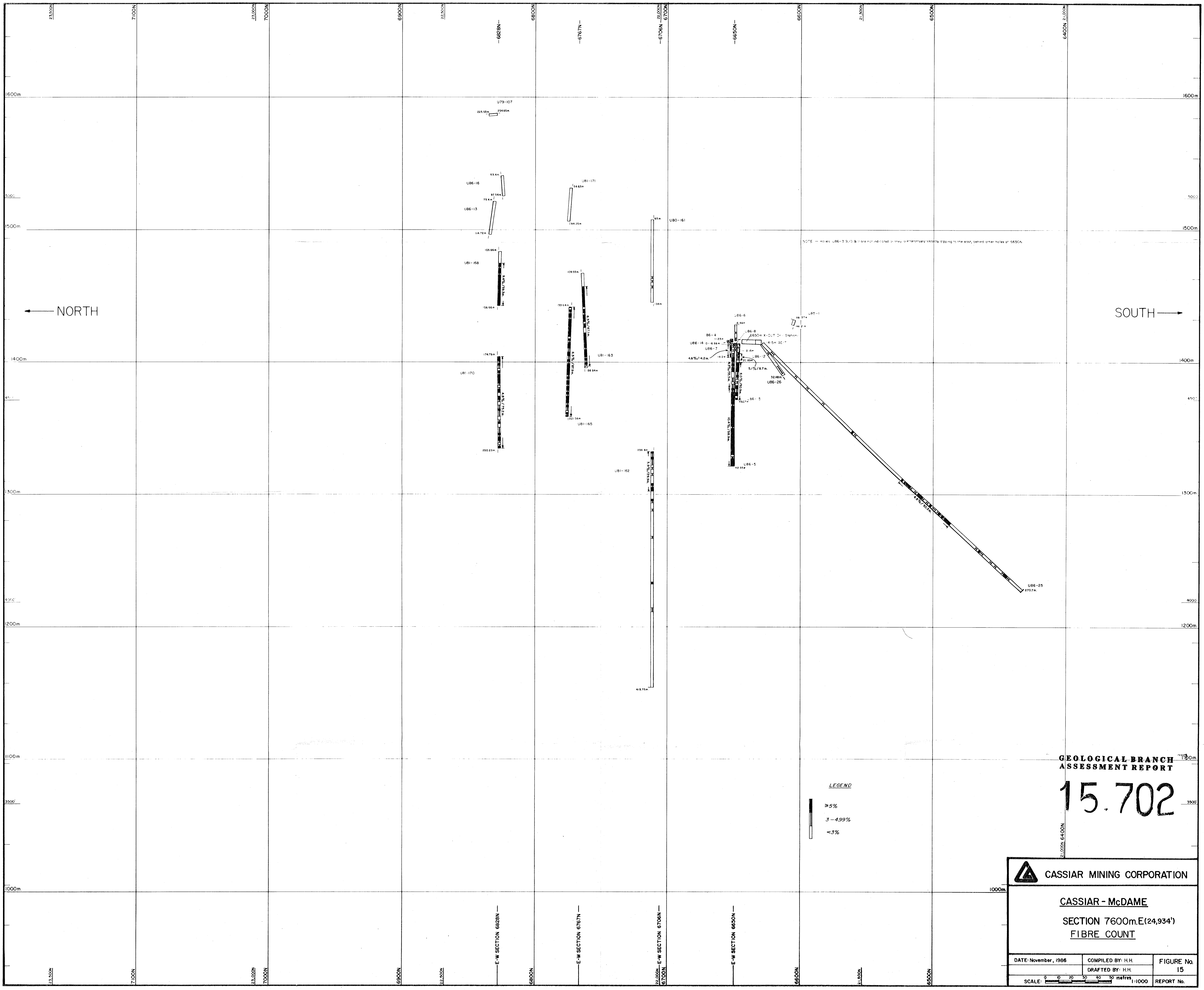
CASSIAR MINING CORPORATION

CASSIAR - McDAME

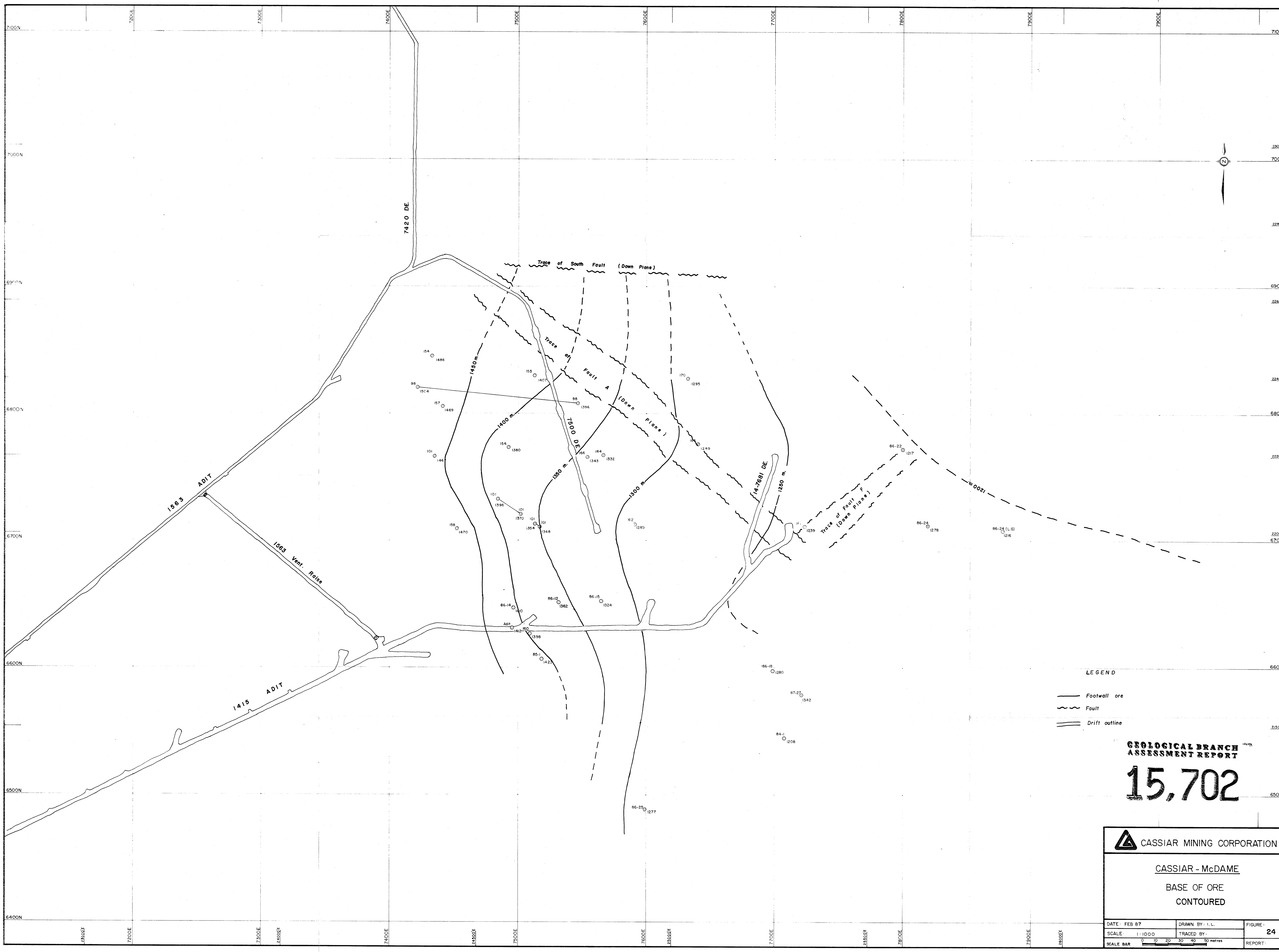
SECTION 6767m.N (22,200')

AVERAGE GRADE

DATE:	DRAWN BY:	FIGURE: 13
SCALE: 1:1000	TRACED BY:	REPORT:



NORTH
SOUTH
1600m
1500m
1400m
1300m
1200m
1100m
1000m
7100N
7000N
6900N
6800N
6700N
6600N
6500N
6400N
E-W SECTION 6828N
E-W SECTION 6767N
E-W SECTION 6706N
E-W SECTION 6650N
U79-107
U86-16
U86-13
U81-168
U81-170
U81-171
U81-163
U81-165
U80-161
U81-162
U86-6
U86-8
U86-4
U86-14
U86-7
U86-2
U86-26
U86-5
U85-1
U86-25
6650N X-CUT
4-5# ADIT
LEGEND
≥5%
3-4.99%
<3%
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15.702
CASSIAR MINING CORPORATION
CASSIAR - McDAME
SECTION 7600m.E(24,934')
FIBRE COUNT
DATE: November, 1986
COMPILED BY: H.H.
DRAFTED BY: H.H.
FIGURE No. 15
SCALE: 1:1000
REPORT No.



Trace of South Fault (Down Plane)
Trace of Fault A (Down Plane)
Trace of Fault F (Down Plane)
7420 DE.
7500 DE.
14-7681 DE.
1563 ADIT
1563 Vent. Raise
1415 ADIT
1450 m.
1400 m.
1350 m.
1300 m.
1250 m.
1200 m.
LEGEND
Footwall ore
Fault
Drift outline
GEOLOGICAL BRANCH ASSESSMENT REPORT
15,702
CASSIAR MINING CORPORATION
CASSIAR - McDAME
BASE OF ORE
CONTOURED
DATE: FEB 87
DRAWN BY: I.L.
FIGURE: 24
SCALE 1:1000
TRACED BY:
SCALE BAR 0 10 20 30 40 50 metres
REPORT:

CASSIAR MINING CORPORATION

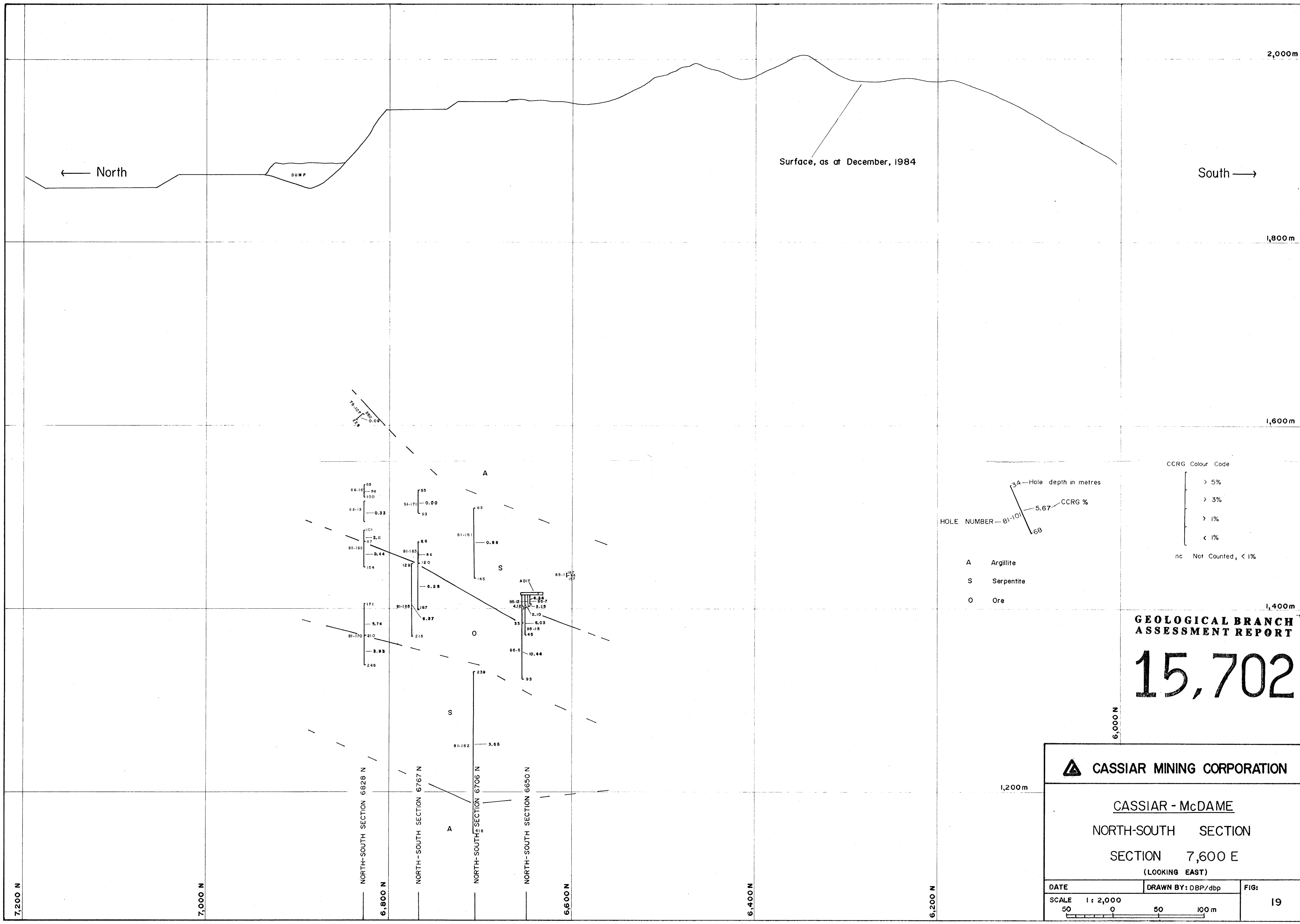
CASSIAR - McDAME

NORTH-SOUTH SECTION

SECTION 7,700 E

(LOOKING EAST)

DATE	DRAWN BY: DBP/dbp	FIG:
SCALE 1: 2,000		20



North
South
DUMP
Surface, as at December, 1984
2,000m
1,800m
1,600m
1,400m
1,200m
7,200 N
7,000 N
6,800 N
6,600 N
6,400 N
6,200 N
6,000 N
NORTH-SOUTH SECTION 6828 N
NORTH-SOUTH SECTION 6767 N
NORTH-SOUTH SECTION 6706 N
NORTH-SOUTH SECTION 6650 N
ADIT
A
S
O
HOLE NUMBER
Hole depth in metres
CCRG %
A Argillite
S Serpentite
O Ore
CCRG Colour Code
> 5%
> 3%
> 1%
< 1%
nc Not Counted, < 1%
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,702
CASSIAR MINING CORPORATION
CASSIAR - McDAME
NORTH-SOUTH SECTION
SECTION 7,600 E
(LOOKING EAST)
DATE
DRAWN BY: DBP/dbp
FIG: 19
SCALE 1 : 2,000
50 0 50 100 m

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,702

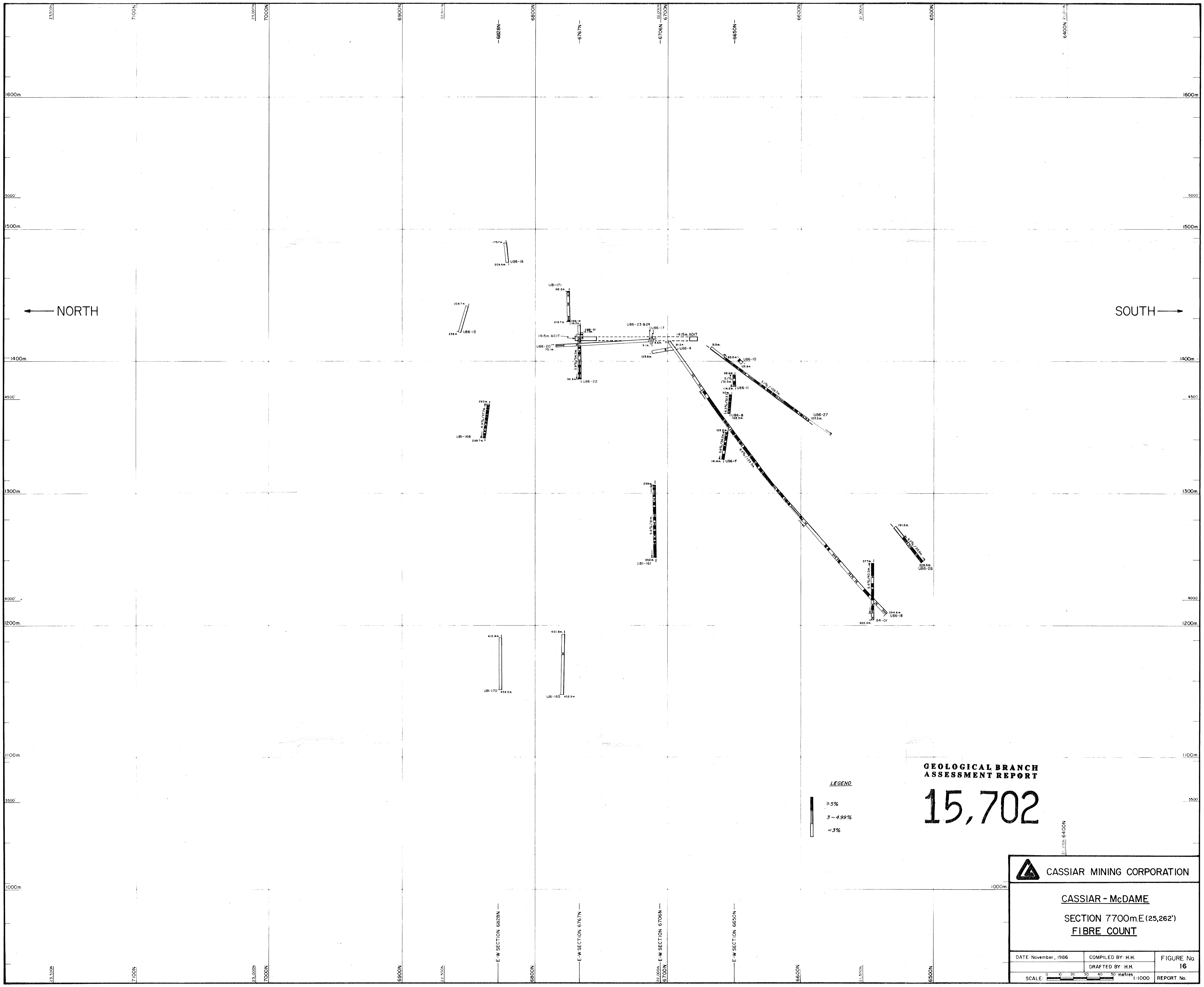
CASSIAR MINING CORPORATION

CASSIAR - McDAME

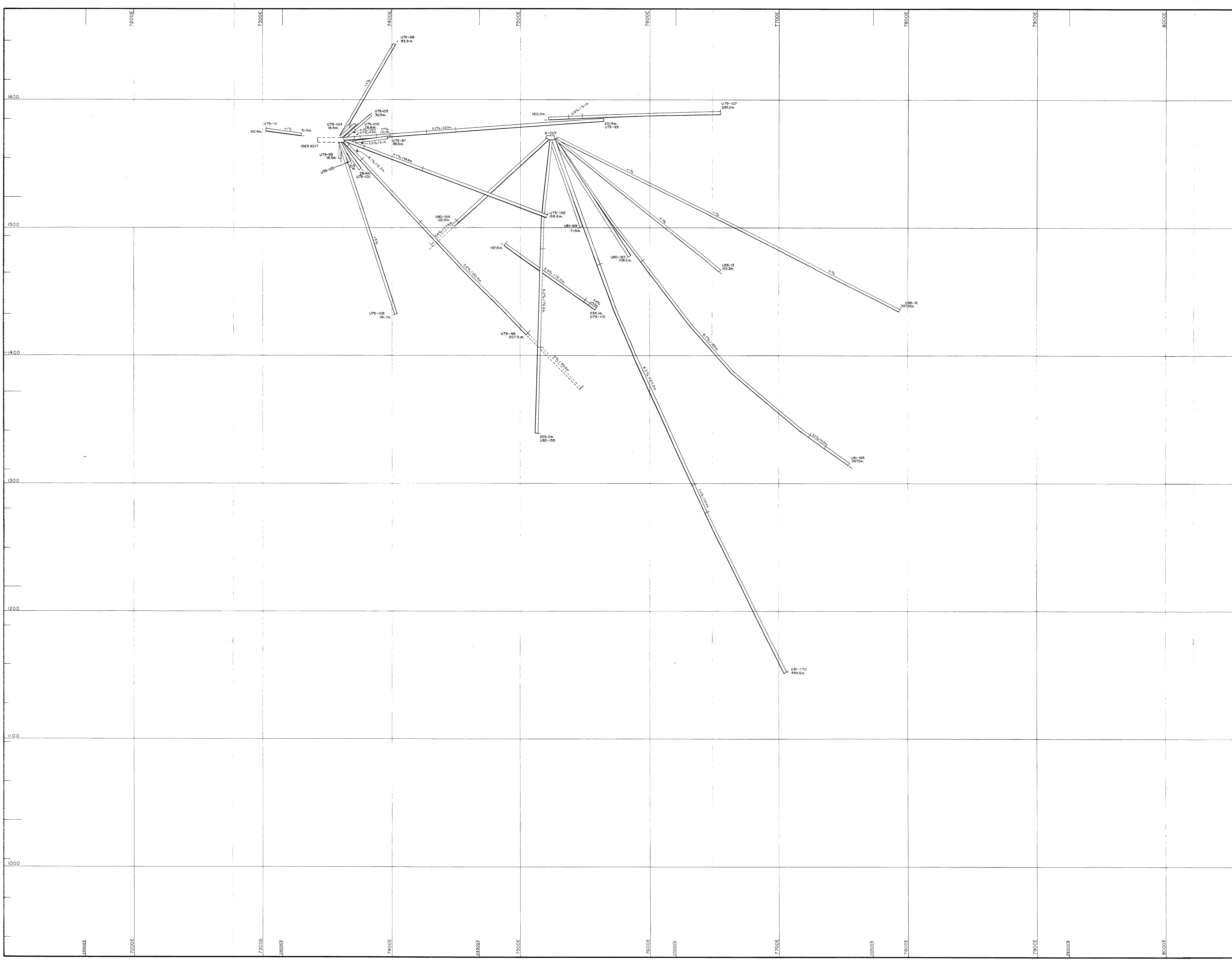
SECTION 6,650 N

DATE Jan. 1987	COMPILED BY DBP	FIGURE No 17
	DRAFTED BY HH, DBP	
SCALE 0 20 40 60 80 100 metres 1:2000		RPT No

WEST
EAST
2000m
1800m
1600m
1400m
1200m
Dump
Surface, as at December, 1984
Diamond Drill Holes
E Faults
A Argillite
S Serpentinite
O Ore, > 3% CCRG
X-Cut
Adit
South
Fault
7000E
7200E
7400E
7600E
7800E
8000E
8200E
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,702
CASSIAR MINING CORPORATION
CASSIAR - McDAME
SECTION 6,767 N
DATE: Jan. 1987
COMPILED BY: DBP
DRAFTED BY: HH, DBP
FIGURE No 18
SCALE 1:2000
RPT No



NORTH
SOUTH
1600m
1500m
1400m
1300m
1200m
1100m
1000m
5000'
4500'
4000'
3500'
7100N
7000N
6900N
6800N
6700N
6600N
6500N
6400N
6828N
6767N
6706N
6650N
E-W SECTION 6828N
E-W SECTION 6767N
E-W SECTION 6706N
E-W SECTION 6650N
1415m. ADIT
U86-16
U86-13
U81-171
U86-20
U86-22
U86-23 & 24
U86-17
U86-4
U86-10
U86-11
U86-8
U86-7
U86-27
U81-168
U81-161
U86-26
U86-18
84-01
U81-170
U81-165
LEGEND
≥5%
3 – 4.99%
<3%
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,702
CASSIAR MINING CORPORATION
CASSIAR - McDAME
SECTION 7700m.E (25,262')
FIBRE COUNT
DATE: November, 1986
COMPILED BY: H.H.
DRAFTED BY: H.H.
FIGURE No. 16
SCALE 1:1000
metres
REPORT No.



GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,702

CASSIAR MINING CORPORATION

CASSIAR - McDAME

SECTION 6828m.N (22,400')

AVERAGE GRADE

DATE:	DRAWN BY:	FIGURE: 14
SCALE: 1:1000	TRACED BY:	
		REPORT: