

VOLUME 2 OF 4
FAME GRANT REPORT

FOR

EQUITY SILVER MINES LIMITED

1986 MINESITE EXPLORATION PROGRAMME

ID No. 10963 M-19

OMINECA MINING DIVISION

NTS 93 L/1

LATITUDE 54 10' N

LONGITUDE 126 15' W

WORK BY: EQUITY SILVER MINES LIMITED

REPORT BY: R. B. PEASE

FILMED

FEBRUARY 1987

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

15,710

PART 2 OF 4

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APPENDIX II

Coded Geologic Logs

and

Assay Data

Drillholes: X86CH231 to X86CH245

X86CH253 to X86CH268

IDEN6B0201 X86CH231 NQ 14FEB86RBP G&D FEB86S38 0.0
 IPRJ EQUITY SILVER MINES LTD BUCK CREEK ZONE - ST GEOCODE
 S000 00 1134 MT 113.4 090.0 -45.0 4077.12 6907.08 990.47
 /SCL MT.2MT.1
 LSCL MT.2
 /NAM
 LNAM

MSCLQZPYCPTTASPR
 CB MGHESLGLMO

R THIS IS THE FIRST HOLE OF THE 1986 DRILL PROGRAMME
 / 00 933 OVBN P
 L
 R CASED TO 60.7 M. CORED CLAY RICH TILL AND BOULDERS TO 93.3.
 / 933 993 51 3D22QZCL <<BR P +1+1J+D.
 L 05 5A)1+2
 R CORE IS VERY BROKEN, CRUMBLY, SOFT. NO OXIDE ZONE.
 R MINOR PATCHES OF ARGILLACEOUS RX. MAIN CLASTS ARE QTZ AND
 R ARGILLITE.
 / 993 1017 22 3E12QZCL <<MX P +1<* D-
 L 02 7ACY +++1
 R CORE VERY BROKEN. POSSIBLE SS ON SOME <<.
 / 1017 1065 43 3D12CYCL <<BR P D.
 L 08 7A)1+2 C/ 60
 R CORE STILL VERY BROKEN, CRUMBLY IN PATCHES. CLASTS AS ABOVE.
 / 1065 1084 15 3E11CY <<MX P
 L 00 8A +++1
 R OCCASIONAL CLASTS, MAINLY SST. MINOR CLAY ZONE 0.5 M WIDE.
 / 1084 1115 28 3D21CBCL <<BR P
 L 03 3ACY)1+2 <=
 R CORE STILL BROKEN. CB IN FRACTURES AND MATRIX.
 / 1115 1134 16 3K11CBCL <<MX P
 L 02 1A +1)2
 R CORE STILL BROKEN. GRAPHITIC IN SPOTS. COARSER GRAINED IN
 R SPOTS. HOLE ABANDONED AT 113.4 M DUE TO SQUEEZING OF THE
 R RODS. DRILLERS ONLY HAD ENOUGH CASING TO 60.7 M., AND
 R THEREFORE CORED OVBN TO REACH BEDROCK. THE OVBN DID NOT HOLD
 R AND STARTED TO SQUEEZE.
 R END OF HOLE.

A001
 ALAB
 ATYP
 AMTH
 AUMM

EQUITY MINESITE LABORATORY

ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

AUMM	RCDVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001 9330 9700	5001	.005	10.0	.040	.005	.005	2.500	.030	
A001 9700 10000	5002	.005	.5	.050	.030	.010	2.090	.005	
A001 10000 10300	5003	.005	.5	.440	.005	.010	2.400	.005	
A001 10300 10600	5004	.005	.5	.020	.010	.005	3.240	.005	
A001 10600 10900	5005	.005	.5	.005	.005	.005	1.920	.005	
A001 10900 11200	5006	.005	.5	.070	.005	.005	1.810	.005	
A001 11200 11340	5007	.005	.5	.120	.005	.005	1.930	.005	

R SUSPECT PRIMARY CRUSHER CONTAMINATION OF SAMPLE 5001
 R END OF ASSAYS

L			38	4A		3115	BD	027<+
R			MINOR INTERLEVED 3D AND 3I					
/	1169	1254	83	3D10	<<		P BD	030*1
L			56	4A		1315		<+
R			10% INTERLEVED 3E					
/	1182	1182		X			D2V/	036V1
L								V9
/	1246	1246		X			D F/	039
R			0.2 M BXIA : MINOR GRAPHITE ON FAULT SURFACE					
/	1254	1274	20	3E10	<<		P	
L			06	4A		+112		<+
R			MINOR GYPS ON <<					
/	1274	1304	30	3D10	<<		P	*1
L			21	5A		+112		<+
R			15% INTERLEVED 3E					
/	1280	1280		X			D F/	034
R			MINOR GRAPHITE ON FAULT SURFACE					
/	1304	1330	26	3E10	<<		P	<.<.
L			11	5A		+112		<+
R			15% INTERLEVED 3D : MINOR GYPS ON <<					
/	1323	1323		X			D F/	
R			CLAY GOUGE					
/	1330	1361	31	3D10	<<		P	*1
L			21	5A		+112		<+
R			1-2% CB IN MATRIX : MINOR GYPS ON <<					
/	1361	1382	21	3E10	<<		P	
L			18	5A)1)1		<+
R			5% INTERLEVED 3D : 10% PEBBLES IN 3E : 1-2% GYPS IN <<					
/	1382	1393	11	3D10	<<		P	*1 <+
L			06	5A		==)1		
R			NOTE QUARTZ IN <<					
/	1393	1420	27	3E10	<<		P	
L			16	5A)2)2		<+
R			10% PEBBLE CLASTS					
/	1415	1415		X			D3F/	034
R			GYPS AND BXIA IN FAULT ZONE					
/	1420	1451	31	3D10	<<		P	*1
L			27	5A)2)2		<+
/	1425	1425		X			D F/	018
R			SLICKENSIDES ON FAULT SURFACE					
/	1451	1470	19	3E10	<<		P BD	040
L			11	5A)2)2		<+
R			10% INTERLEVED 3D					
/	1470	1483	13	3D10	<<		P	*1
L			09	4A)1)1		<+
/	1483	1504	21	3E24MS	<<		P	+4<=V+
L			01	7A		172X		<=
R			NOTE MORE INTENSE FRACTURING AND ALT'N					
/	1504	1525	21	3E10	<<		P	
L			06	5A)3)4		<+
R			GRADES LOCALLY TO 3I					
/	1525	1540	15	3E10	<<		P	
L			11	5A)'=1		<+
R			3-5% CB IN MATRIX : 20% INTERLEVED 3D					
/	1540	1553	13	3D10	<<		P	*1

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L           08           5A           )==1           <+
/ 1553 1618 65 3E10 << P <+
L           61           4A           )224           <+
R           30% INTERLEVED 3D : GRADES TO 3E20 LOCALLY
/ 1561 1561 X D F/ 045
/ 1572 1572 X D F/ 030
/ 1618 1640 22 3D10 << P *1
L           17           5A           )11           <+
/ 1640 1676 36 3D10 << P *1 <+
L           18           5A           )3)3           <+
R           20% INTERLEVED 3E : .5-1% CB IN MATRIX OF 3D
/ 1645 1645 X D F/
R CLAY GOUGE ZONE : NO ANGLE OBTAINABLE
/ 1676 1716 40 3E10 << P
L           26           4A           )224           <+
R           15% INTERLEVED 3D
/ 1716 1780 64 3D10 << P *1
L           48           4A           )325           <+
R           10% INTERLEVED 3E
/ 1780 1848 68 3D10 << P *1
L           51           5A           )213           <+
R SOME CLASTS WITH CHL+MS ALT'N RIMS
/ 1848 1866 17 3E10 << P
L           07           4A           1==2           <+
/ 1859 1859 X D F/
R BXIA AND GOUGE ZONE : STEEPLY DIPPING
/ 1866 1911 45 3D10 << P *1 <+
L           29           4A           )213           <+
/ 1882 1882 X D F/ 025
/ 1911 1930 18 3E10 << P
L           16           5A           )1)1           <+
R           5% INTERLEVED 3D
/ 1930 1930 X D F/ 053
/ 1930 1993 63 3D10 << P *1
L           29           4A           1517           <+
/ 1966 1966 X D F/ 020
R END OF HOLE.

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A001

ALAB

ATYP

AMTH

AUMM

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EQUITY MINESITE LABORATORY
ASSAY
WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
RCOVSAMPLE   RGD % CU   G/TAG G/TAU % SB % AS % FE % ZN
A001 6550 6780 5008 .005 .5 .050 .005 .005 2.530 .005
A001 6780 7080 5009 .005 .5 .050 .005 .005 2.850 .005
A001 7080 7320 5010 .005 .5 .005 .020 .005 2.990 .005
A001 7320 7600 5011 .005 .5 .070 .005 .005 2.860 .005
A001 7600 7900 5012 .005 .5 .140 .005 .005 2.570 .005
A001 7900 8200 5013 .005 .5 .100 .005 .005 2.190 .005
A001 8200 8500 5014 .005 .5 .180 .005 .005 2.470 .005
A001 8500 8800 5015 .005 .5 .040 .005 .005 2.320 .005
A001 8800 9100 5016 .005 .5 .040 .005 .005 2.440 .005
A001 9100 9400 5017 .005 .5 .050 .005 .005 2.710 .005
A001 9400 9700 5018 .005 .5 .180 .010 .005 2.740 .005
A001 9700 10000 5019 .005 .5 .050 .020 .005 2.760 .005
A001 10000 10300 5020 .005 .5 .030 .040 .020 3.130 .005

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A001	10300	10600	5021	.005	.5	.080	.050	.005	2.160	.005
A001	10600	10900	5022	.005	.5	.080	.005	.005	1.700	.005
A001	10900	11200	5023	.005	.5	.060	.005	.005	2.580	.005
A001	11200	11500	5024	.005	.5	.090	.005	.005	3.250	.005
A001	11500	11800	5025	.005	.5	.040	.005	.005	1.900	.005
A001	11800	12100	5026	.005	.5	.020	.005	.005	1.870	.005
A001	12100	12400	5027	.005	.5	.010	.005	.005	2.900	.005
A001	12400	12700	5028	.005	.5	.020	.005	.005	2.930	.005
A001	12700	13000	5029	.005	.5	.010	.005	.005	2.860	.005
A001	13000	13300	5030	.005	.5	.060	.005	.005	2.610	.005
A001	13300	13600	5031	.005	1.0	.020	.005	.005	2.460	.005
A001	13600	13900	5032	.005	.5	.060	.005	.005	2.670	.005
A001	13900	14200	5033	.005	1.0	.040	.005	.005	2.820	.005
A001	14200	14500	5034	.005	.5	.060	.005	.005	2.720	.005
A001	14500	14830	5035	.005	.5	.100	.005	.005	2.650	.005
A001	14830	15040	5036	.005	.5	.020	.005	.005	1.850	.005
A001	15040	15300	5037	.005	1.0	.020	.005	.005	2.940	.005
A001	15300	15600	5038	.005	2.0	.080	.005	.005	2.440	.005
A001	15600	15900	5039	.005	1.0	.010	.005	.005	2.940	.005
A001	15900	16200	5040	.005	2.0	.090	.005	.005	2.660	.005
A001	16200	16500	5041	.005	1.0	.090	.005	.005	2.500	.005
A001	16500	16800	5042	.005	1.0	.430	.005	.005	2.720	.005
A001	16800	17100	5043	.005	1.0	.370	.005	.005	3.540	.005
A001	17100	17400	5044	.010	1.0	.010	.005	.005	3.130	.005
A001	17400	17700	5045	.005	.5	.040	.005	.005	2.470	.005
A001	17700	18000	5046	.005	2.0	.170	.005	.005	2.690	.005
A001	18000	18300	5047	.005	1.0	.150	.005	.005	2.900	.005
A001	18300	18600	5048	.005	1.0	.010	.005	.005	2.940	.005
A001	18600	18900	5049	.005	1.0	.010	.005	.005	2.910	.005
A001	18900	19200	5050	.005	.5	.640	.005	.005	3.100	.005
A001	19200	19500	5051	.005	.5	.060	.005	.005	3.010	.005
A001	19500	19700	5052	.005	.5	.010	.005	.005	2.590	.005
A001	19700	19930	5053	.005	1.0	.010	.005	.010	2.690	.005

R

END OF ASSAYS

IDEN6B0201 XB6CH233 NQ 27FEB86RBP G&D FEB86S38 0.0
 IPRJ EQUITY SILVER MINES LTD BUCK CREEK ZONE - ST GEOCODE
 S000 00 1330 MT 133.0 090.0 -60.0 4063.39 7090.31 994.44
 /SCL MT.2MT.1
 LSCL MT.2
 /NAM
 LNAM MSCLQZPYCPTTASPR
 CB MGHESLGLMO
 / 00 750 QVBN P
 L
 R CASED TO 70.1 M. CORED TILL TO 75.0 M.
 / 750 803 42 3D10CL << P BD 55 <(D
 L 06 5G +1)2 <)
 R VERY LITTLE OXIDE. CORE NOT BADLY BROKEN. CLASTS DOMINANTLY
 R BLACK SILTY ARGILLITE AND ACIDIC VOLCANICS, WELL ROUNDED.
 / 803 971 158 3H11CL << P BN 25 <(D.
 L 52 5A 12+4 <)
 / 803 803 X D F/ 50
 / 895 895 X D F/ 55
 R SMALL ZONE OF VOLC. SANDSTONE FROM 89.0 TO 89.3 M. SOME
 R LAPILLI ARE ELONGATED, ABUNDANT BLACK SHARDS.
 / 971 1004 30 3H21CL <<BR P BN 30 <(D.
 L 09 3A +214 <+
 R ROCK CHANGED VERY LITTLE, HIGHER DEGREE OF FRACTURING.
 / 1004 1020 14 3H11CL << P BN 25 <(D.
 L 06 5A)+(1 <)
 / 1020 1050 29 3H21CL <<BR P <(D.
 L 09 3A +113 <)
 R MOTTLED PURPLE COLOUR IN ROCK.
 / 1050 1061 11 3H11CL << P BN 25 <(D.
 L 09 3A)+1 <)
 R SOME FRAGMENTS HAVE SERICITE ALTERATION.
 / 1061 1093 31 3F11CL <<BR P <(D.
 L 20 5P +113 <)
 R MAYBE COARSER THAN DUST TUFF, BUT VERY FEW FRAGMENTS.
 / 1093 1152 57 3H11CL <<BR P BN 20 <)D.
 L 42 4A +214 BD 35<)
 R SANDSTONE FROM 111.1 TO 111.5 AND AGAIN FROM 112.2 TO 112.4 M.
 / 1152 1204 49 3H21CL <<BR P BN 25*) <)D.
 L 13 5A)112 <)
 R ABUNDANT SHARDS. SOME SERICITE ALTERED LAPILLI, SOME ALTERED
 R RIMS ON LAPILLI.
 / 1204 1261 54 3E11CL <<BR P <+D.
 L 11 7A +113 <)
 R UPPER CONTACT GRADATIONAL OVER 0.3 M. MAINLY TUFFACEOUS DEBRIS.
 / 1261 1285 22 3H11CL <<BR P BN 30*) <)D.
 L 03 3A)+12 C/ 65<)
 R LOWER CONTACT VERY SHARP.
 / 1285 1316 27 3F11CY << P <)
 L 03 6M)+12 <)
 R CORE VERY SOFT. "RED TUFF".
 / 1316 1330 11 3H11CL << P BN 40 <)
 L 00 4A <)
 R CORE VERY BROKEN.
 R END OF HOLE.
 A001

ALAB	EQUITY MINESITE LABORATORY									
ATYP	ASSAY									
AMTH	WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST									
AUMM	RCDV	SAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001	7500	7800	5054	.005	2.0	.050	.005	.001	2.530	.005
A001	7800	8100	5055	.005	3.0	.020	.005	.001	2.560	.005
A001	8100	8400	5056	.005	2.0	.060	.005	.001	3.210	.010
A001	8400	8700	5057	.005	2.0	.060	.005	.001	3.910	.010
A001	8700	9000	5058	.005	3.0	.100	.005	.001	3.460	.010
A001	9000	9300	5059	.005	2.0	.090	.005	.001	3.510	.010
A001	9300	9600	5060	.005	4.0	.060	.005	.001	3.370	.010
A001	9600	9900	5061	.005	4.0	.080	.005	.001	3.490	.010
A001	9900	10200	5062	.005	4.0	.040	.005	.001	3.630	.010
A001	10200	10500	5063	.005	3.0	.090	.005	.001	3.560	.010
A001	10500	10800	5064	.005	2.0	.020	.005	.001	3.590	.010
A001	10800	11100	5065	.005	3.0	.070	.005	.001	3.680	.010
A001	11100	11400	5066	.005	2.0	.030	.005	.001	3.350	.005
A001	11400	11700	5067	.005	3.0	.080	.005	.001	3.340	.005
A001	11700	12000	5068	.005	2.0	.040	.005	.001	3.640	.005
A001	12000	12300	5069	.005	2.0	.060	.005	.001	2.340	.005
A001	12300	12600	5070	.005	3.0	.050	.005	.001	2.140	.005
A001	12600	12850	5071	.005	2.0	.080	.005	.001	3.170	.010
A001	12850	13160	5072	.005	2.0	.060	.005	.001	2.050	.005
A001	13160	13300	5073	.005	2.0	.040	.005	.001	3.240	.010
R	END OF ASSAYS									

IDEN6B0201		X86CH234 NQ 28FEB86RBP	G&D FEB86S38	0.0		
IPRJ		EQUITY SILVER MINES LTD	BUCK CREEK ZONE - ST	GEOCODE		
S000	00	884 MT 88.4 090.0 -45.0		4066.27	7200.40	1012.52
/SCL		MT.2MT.1				
LSCL		MT.2				
/NAM				MSCLQZPYCPTTASPR		
LNAM				CB	MGHESLGLMO	
/	00	884	OVBN	P		
L						
R		CASED TO 88.4 M AND DID NOT REACH BEDROCK. HOLE ABANDONED.				
R		END OF HOLE.				
A001						
ALAB		EQUITY MINESITE LABORATORY				
ATYP		ASSAY				
AMTH		WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST				
AUMM		RCOVSAMPLE RQD % CU G/TAG G/TAU % SB % AS % FE % ZN				
R		NO CORE - NO ASSAYS				
R		END OF ASSAYS - END OF LOG				

L			16	AW				
/	440	470	27	3A10	<<	P		#)D.D.
L			09	AW				#.
R			: 0.3 M 3A50 W/ QZ + CB INFILLING (45.2 - 45.5 M)					
/	470	500	29	3A10	<<	P		<)
L			24	AW				
R			: 1-2% DISS. PY IN MATRIX :TR. PY IN CHERT CLASTS					
/	500	530	30	3A10	<<	P		<.D.
L			19	AW				<.
/	512	512		X		D F/	012	
R			: MINOR BXIA. ASSOCIATED W/ FAULT					
/	530	560	28	3A10	<<	P		<*)D*
L			24	AW				<*
/	560	590	30	3A10	<<	P		<)
L			25	AW				
R			IRREG. PATCHES PY					
/	590	620	29	3A10	<<	P		<.)D.
L			23	AW				<.
R			: TO 3A50 LOC.					
/	620	650	29	3A10	<<	P		#)<.
L			26	AW				
R			: TO 3A50 LOC. W/ QZ INFILLING					
/	650	680	27	3A10	<<	P		<.<*
L			16	AW				<.
R			: TR. PY PATCHES					
/	680	710	29	3A10	<<	P		<.<)
L			23	AW				<.
/	710	727	17	3A10	<<	P		<***
L			11	AW				<*
/	727	735	08	3B10	<<	P		<)<*
L			05	GA				<)
R			CNTS. GRAD. OVER 5 CMS - NO ATTITUDES OBTAINABLE					
/	735	770	34	3A10	<<	P		<*<.
L			27	AW				
/	770	800	27	3A10	<<	P		<.
L			12	AW				
R			: VERY WEAK FRACTURING AND MINERALIZATION					
/	800	830	30	3A10	<<	P		<.
L			21	AW				
/	830	860	29	3A10	<<	P		<*)
L			25	AW				
/	860	874	13	3A10	<<	P		<.<.
L			11	AW				<.
R			: 3B10 86.9 - 87.4 M - NO BEDDING ATT. OBTAINABLE					
/	869	869		X		D C/	060	
/	874	890	13	3C11CL	<<	P BD	050	<*) <)<.
L			05	TG				
R			CNT. NOT VISIBLE DUE TO LOST CORE					
/	890	933	30	3C11CL	<<	P BD	055	<*) <)
L			13	TG				
R			AS ABOVE 87.4-89.0 M : LOWER CNT. OBSCURED IN BROKEN CORE					
/	933	964	31	3A10	<<	P		<*)
L			24	AW				<*
R			TO 3B LOC.					
/	938	938		X		D V/	050	V1V9

/	964	972	08	BA02CL	A*	P C/	025	
L			08	AG		C/	038	
R				GOOD INTRUSIVE CONTACTS W/ CHILLED MARGINS AND FLOW BANDING				
/	972	980	07	3B10		P		<><
L			05	AW				
R				: 0.25 M 2C AT 97.5 M ,CNTS. OBSCURRED IN BROKEN AND LOST CORE				
/	980	1000	17	2C23CLMS	<<	P		<> <><
L			08	TG				
R				: CL ALSO AS << ENVELOPES : NOTE CHANGE FROM UNIT 3 TO UNIT 2				
/	1000	1030	26	2C33CLMS	<<	P		<*><
L			07	TG				
R				: TO 2C23 LOC. : PATCHY MS ALT'N : TO 2D LOC.				
/	1030	1060	27	2C23CLMS	<<	P		<><><*
L			21	TG				
/	1060	1090	25	2C23CLMS	<<	P		E.<<*<
L			09	TG				
R				: TO 2D LOC. : PATCHY MS ALT'N (APPEARS MORE INTENSE IN 2D)				
/	1069	1069		X		D V/	028	V5V5
R				: HEAVILY BROKEN CORE 106.9 107.3 M (FEW PIECES MASS. PY W/				
R				0-20% QZ				
/	1090	1120	29	2C13CLMS	<<	P		<*><
L			23	TG				
R				: TO FINE GRAINED 2D LOC. : PY VEINS GENERALLY LESS THAN 10 MM				
/	1120	1150	29	2C13CLMS	<<	P		<*>
L			21	TG				
R				: TO 2D LOC. : TO 2C23 LOC.				
/	1150	1180	27	2C24CLMS	<<	P		<.<+<
L			15	TG				
R				: TO 2D LOC. : TO 2C34 LOC.				
/	1180	1210	29	2C24CLMS	<<	P		<*<+<+<
L			17	TG				
/	1210	1240	27	2C24MSCL	<<	P		<.<><><*<
L			22	GT				
/	1240	1270	29	2C23CLMS	<<	P		<*<*><
L			26	TG				
/	1270	1300	27	2C23CLMS	<<	P		<*<*><
L			15	TG				
R				: NO 2D SINCE 115.0 - 118.0 M				
/	1300	1330	26	2C23CLMS	<<	P		<*<*><
L			07	TG				
/	1330	1360	28	2C24MSCL	<<	P		<.<+<=<
L			14	GT				
R				: STRONG PY + QZ 133.8-134.4 (COALESCING VEINS ?)				
/	1360	1390	22	2C24MSCL	<<	P		<.<V.<>
L			09	GT				
/	1390	1420	25	2C24MSCL	<<	P		<*<.<>
L			14	GT				
/	1373	1373		X		D2V/	027	V7V3
/	1420	1450	26	2C25MS	<<	P		<*<*>
L			04	ST				
/	1450	1470	20	2C25MS	<<	P		<*<*<+<
L			01	ST				
/	1467	1467		X		D3V/	020	V1V9
/	1470	1486	16	2C25MS	<<	P		<*<*<+<
L			03	ST				

R : TO 2C23 TOWARDS END OF INT. : 3 * PY + QZ VV
/ 1473 1473 X D3V/ 012 V2V8
/ 1486 1494 08 BA01CL A* P C/ 069
L 08 AG C/ 030
R : GOOD INTRUSIVE CNTS. W/ CHILLED MARGINS : CB FILLED A*
/ 1494 1520 25 2C23CLMS << P <><<<<<
L 04 TG
R : TO 2C24 LOC.
/ 1520 1550 26 2C23CLMS << P <><<<<<
L 07 TG
R : TO 2C25 LOC.
/ 1550 1580 26 2C34CLMS << P <<<<<<<
L 03 TG
R : 3*(PY+QZ) VV 2-10 MM
/ 1580 1610 26 2C35MS << P <*>V)=
L 00 5T
/ 1610 1640 27 2C35MS << P V)=
L 01 5T
/ 1610 1610 X D F/ 045
R : 10 CM CLAY GOUGE IN FAULT
/ 1640 1670 28 2C35MS << P V)V)
L 03 5T
R : NOTE - PY+QZ VEINS DECREASING IN FREQUENCY
/ 1670 1700 30 2C35MS << P V)V)
L 06 5T
R : TO 2C55 LOC.
/ 1700 1730 24 2C35MS << P V+V+
L 00 5T
/ 1730 1760 27 2C35MS << P <*>V)V)
L 11 5T
R : ONLY 1 QZ+PY VV
/ 1760 1790 30 2C25MS << P <*>V)V)
L 16 5T
R : TO 2C23 LOC. W/ TG COLOR
/ 1790 1820 28 2C23CLMS << P V)V)
L 19 TG
/ 1820 1850 28 2C25MS << P V)V+
L 05 5T
/ 1850 1880 29 2C25MS << P <*>
L 18 5T
/ 1880 1880 X D F/ 052
R : 2 CM CLAY GOUGE ON FAULT
/ 1880 1910 26 2C25MS <<BR P <.<.)
L 02 5T
R : TO 2C85 LOC.
/ 1910 1940 29 2C35MS << P <.<.)
L 04 5T
R : OCC. QZ+PY VV 2-4 MM
/ 1940 1970 27 2C35MS << P <.<.)
L 00 5T
R : HEAVILY BROKEN CORE
/ 1970 2000 28 2C45MS <<BR P <*>=
L 09 5T
R : TO 2C55 LOC.
/ 1913 1913 X D4V/ 040 V7V3

R : TO 2C14 LOC.
/ 2940 2970 28 2C25MS <<BR P <*>#.
L 07 5T #.
R : TO 2C55 LOC W/ MINOR QZ+PY+--HE(SPEC) IONFILLING : TR CP W/ HE
/ 2970 3000 28 2C45MS << P <*>=<.
L 20 5T #.
R : TO 2C55 LOC. W/ MINOR QZ+PY+--HE(SPEC) INFILLING
/ 2983 2983 X D F/ 045
R : 1.5 CM BR & CY GOUGE
/ 3000 3030 29 2C25MS << P <*>
L 04 5T
/ 3030 3060 29 2C25MS << P <*>
L 04 5T
R : OCC. PY+QZ VEIN
/ 3060 3090 29 2C25MS << P <*>
L 04 5T
/ 3090 3120 29 2C35MS <<BR P <*>+
L 19 5T
R : TO 2C55 LOC. : FEW PY+QZ VEINS
/ 3120 3135 15 2C35MS <<BR P <*>+
L 10 5T
R : TO 2C55 LOC.
/ 3135 3168 32 2C85MS BR<< P #2#2
L 24 5T <*>
R : 40% MATRIX
/ 3168 3179 10 8C13MS << P CU 060 <*>*>
L 10 7A CL 057
R : MOD. PHYLLIC ALT. : PRE-MIN DYKE ? : 2C85 317.6-317.9 M
/ 3179 3194 15 BA01CLCB A* P CU 058
L 13 3G CL 065 D*
R : 5% A* W/ CB INFILLING : LOWER CNT. IRREG.
/ 3194 3217 22 8C10MS <<A* P FB 075 <.<.<.
L 18 7A C/ 060
R : PRE-MIN DYKE AS ABOVE 316.8-317.9 M : 2C85 W/ 30% PY 319.8-
R 319.95 AND 320.05-320.3 AND 321.5-321.7 : WEAK A* TEXT.
R WITH CL+CB INFILLING AMYGDS. FLATTENED @ 075
/ 3217 3234 15 BA01CLCB P*A* P CU 050
L 13 3G D*
R : AS ABOVE 317.9-319.4 M : 20 % PHENOS. TO 3 MM
/ 3234 3278 44 8C01MS P* P CU 060 D.
L 22 TW CL 055
R : WEAK FLAG ALT'N (SAUSS.) : TYP. POST MIN. 8C
/ 3278 3292 14 BA01CLCB A* P
L 12 3G D*
R : 2% A* W/ CB INFILLING
R : END OF HOLE AT 329.2 M

A001

ALAB

ATYP

AMTH

AUMM

EQUITY MINESITE LABORATORY

ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

AUMM	RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN	
A001	92	122	5074	0.020	0.5	0.030	0.005	0.005	1.330	0.005
A001	122	160	5075	0.100	25.0	0.050	0.040	0.005	3.450	0.020
A001	160	171	5076	0.080	0.5	0.040	0.010	0.005	1.840	0.010
A001	171	200	5077	0.050	0.5	0.070	0.005	0.005	2.510	0.005

A001	200	230	5078	0.080	0.5	0.060	0.005	0.005	1.950	0.005
A001	230	260	5079	0.080	0.5	0.140	0.005	0.005	1.550	0.005
A001	260	290	5080	0.030	0.5	0.030	0.005	0.005	1.280	0.005
A001	290	320	5081	0.040	0.5	0.030	0.005	0.005	1.190	0.005
A001	320	350	5082	0.040	0.5	0.070	0.005	0.005	1.340	0.005
A001	350	380	5083	0.210	0.5	0.160	0.005	0.005	2.530	0.005
A001	380	410	5084	0.270	0.5	0.210	0.005	0.005	2.110	0.005
A001	410	440	5085	0.160	0.5	0.110	0.005	0.005	2.870	0.005
A001	440	470	5086	0.050	0.5	0.340	0.005	0.005	1.850	0.005
A001	470	500	5087	0.020	0.5	0.080	0.005	0.005	1.430	0.005
A001	500	530	5088	0.020	0.5	0.070	0.005	0.005	1.270	0.005
A001	530	560	5089	0.150	0.5	0.050	0.005	0.005	2.390	0.005
A001	560	590	5090	0.100	0.5	0.060	0.005	0.005	1.710	0.005
A001	590	620	5091	0.040	0.5	0.060	0.005	0.005	1.860	0.005
A001	620	650	5092	0.010	0.5	0.070	0.005	0.005	1.110	0.005
A001	650	680	5093	0.020	0.5	0.030	0.005	0.005	1.880	0.005
A001	680	710	5094	0.030	0.5	0.050	0.005	0.005	1.900	0.005
A001	710	740	5095	0.030	0.5	0.040	0.005	0.005	2.180	0.005
A001	740	770	5096	0.010	0.5	0.050	0.005	0.005	1.610	0.005
A001	770	800	5097	0.020	0.5	0.050	0.005	0.005	1.690	0.005
A001	800	830	5098	0.030	0.5	0.040	0.005	0.005	1.200	0.005
A001	830	860	5099	0.050	0.5	0.070	0.005	0.005	1.800	0.005
A001	860	890	5100	0.050	0.5	0.290	0.005	0.005	4.880	0.010
A001	890	921	5101	0.005	0.5	0.180	0.005	0.005	5.470	0.030
A001	921	950	5102	0.040	0.5	0.070	0.005	0.005	3.250	0.001
A001	950	964	5103	0.020	0.5	0.220	0.005	0.005	2.230	0.005
A001	972	1000	5104	0.100	0.5	0.120	0.060	0.005	3.140	0.005
A001	1000	1030	5105	0.190	0.5	0.140	0.040	0.005	3.690	0.010
A001	1030	1060	5106	0.050	0.5	0.090	0.010	0.005	4.280	0.005
A001	1060	1090	5107	0.050	0.5	0.100	0.010	0.005	8.320	0.005
A001	1090	1120	5108	0.100	0.5	0.110	0.010	0.005	4.600	0.005
A001	1120	1150	5109	0.030	0.5	0.100	0.010	0.005	3.620	0.005
A001	1150	1180	5110	0.140	0.5	0.090	0.090	0.005	4.760	0.040
A001	1180	1210	5111	0.060	0.5	0.130	0.040	0.005	4.300	0.005
A001	1210	1240	5112	0.020	0.5	0.230	0.005	0.005	4.260	0.005
A001	1240	1270	5113	0.050	0.5	0.080	0.005	0.005	4.100	0.005
A001	1270	1300	5114	0.020	0.5	0.020	0.005	0.005	3.880	0.005
A001	1300	1330	5115	0.040	0.5	0.060	0.005	0.005	4.190	0.005
A001	1330	1360	5116	0.005	0.5	0.090	0.005	0.005	8.780	0.005
A001	1360	1390	5117	0.050	0.5	0.090	0.005	0.005	4.390	0.005
A001	1390	1420	5118	0.040	0.5	0.050	0.005	0.005	3.910	0.005
A001	1420	1450	5119	0.020	0.5	0.005	0.005	0.005	4.820	0.005
A001	1450	1470	5120	0.005	0.5	0.005	0.005	0.005	6.410	0.005
A001	1470	1486	5121	0.005	0.5	0.040	0.005	0.005	4.380	0.005
A001	1494	1520	5122	0.005	0.5	0.030	0.005	0.005	4.020	0.005
A001	1520	1550	5123	0.010	0.5	0.080	0.005	0.005	4.270	0.005
A001	1550	1580	5124	0.060	3.0	0.070	0.005	0.005	3.970	0.005
A001	1580	1610	5125	0.010	2.0	0.060	0.010	0.005	9.190	0.005
A001	1610	1640	5126	0.005	2.0	0.040	0.010	0.005	2.800	0.005
A001	1640	1670	5127	0.005	2.0	0.090	0.005	0.005	6.290	0.005
A001	1670	1700	5128	0.060	3.0	0.130	0.020	0.010	4.150	0.005
A001	1700	1730	5129	0.020	2.0	0.030	0.005	0.005	5.630	0.005
A001	1730	1760	5130	0.030	2.0	0.060	0.005	0.005	3.250	0.005
A001	1760	1790	5131	0.040	3.0	0.070	0.005	0.005	6.470	0.005
A001	1790	1820	5132	0.020	3.0	0.060	0.010	0.005	5.190	0.005

A001	1820	1850	5133	0.010	3.0	0.100	0.010	0.010	7.030	0.005
A001	1850	1880	5134	0.030	5.0	0.080	0.010	0.005	4.410	0.010
A001	1880	1910	5135	0.020	2.0	0.090	0.005	0.005	3.050	0.005
A001	1910	1940	5136	0.010	3.0	0.080	0.005	0.005	4.470	0.005
A001	1940	1970	5137	0.010	2.0	0.060	0.005	0.005	3.030	0.005
A001	1970	2000	5138	0.005	1.0	0.100	0.005	0.005	5.180	0.005
A001	2000	2030	5139	0.005	1.0	0.010	0.005	0.020	4.330	0.005
A001	2030	2060	5140	0.005	1.0	0.070	0.005	0.005	4.130	0.005
A001	2060	2093	5141	0.005	2.0	0.100	0.010	0.010	8.770	0.005
A001	2577	2610	5142	0.005	4.0	0.070	0.005	0.005	4.940	0.020
A001	2610	2640	5143	0.090	5.0	0.180	0.010	0.005	4.380	0.005
A001	2640	2670	5144	0.030	7.0	0.040	0.010	0.010	8.070	0.040
A001	2670	2700	5145	0.005	4.0	0.040	0.005	0.005	9.050	0.005
A001	2700	2730	5146	0.005	12.0	0.280	0.020	0.020	38.000	0.010
A001	2730	2760	5147	0.005	6.0	0.110	0.005	0.005	6.540	0.050
A001	2760	2790	5148	0.005	5.0	0.080	0.005	0.005	5.730	0.005
A001	2790	2820	5149	0.005	2.0	0.050	0.005	0.005	4.620	0.005
A001	2820	2850	5150	0.005	3.0	0.270	0.005	0.005	2.950	0.005
A001	2850	2880	5151	0.005	3.0	0.080	0.005	0.005	3.420	0.005
A001	2880	2910	5152	0.005	3.0	0.080	0.005	0.005	4.970	0.005
A001	2910	2940	5153	0.005	2.0	0.040	0.005	0.005	1.570	0.005
A001	2940	2970	5154	0.050	25.0	0.200	0.030	0.010	11.000	0.270
A001	2970	3000	5155	0.040	32.0	0.160	0.030	0.010	10.100	0.680
A001	3000	3030	5156	0.005	5.0	0.070	0.010	0.005	4.660	0.040
A001	3030	3060	5157	0.005	5.0	0.080	0.010	0.005	7.120	0.020
A001	3060	3090	5158	0.005	2.0	0.050	0.005	0.005	6.250	0.005
A001	3090	3120	5159	0.005	3.0	0.110	0.010	0.010	8.450	0.010
A001	3120	3135	5160	0.050	31.0	0.740	0.060	0.010	14.000	0.520
A001	3135	3168	5161	0.030	12.0	0.300	0.040	0.030	14.100	0.430
A001	3168	3179	5162	0.030	2.0	0.140	0.005	0.020	6.140	0.030
A001	3194	3217	5163	0.030	3.0	0.090	0.010	0.010	9.360	0.005

R

END OF ASSAYS - END OF LOG

/	1021	1051	28	2C23CL	<<	P		<*(
L			05	4T		=1=2			
/	1051	1095	42	2C44CL	<<BR	P F/		<*(
L			16	5T		=1+2		<.	
R				FAULT GOUGE ON LOWER CONTACT.					
/	1095	1119	22	2C13CL	<<	P		<((
L			06	6T		+1+2			
/	1119	1187	66	2C23CL	<<	P		<((+	
L			27	5T		1326			
/	1187	1201	15	2C34CL	<<BR	P		<)<=	
L			13	5T)++1			
/	1201	1216	15	8A00	MX	P BN	40	D.	
L			15	7G					
R				FAULT GOUGE ON UPPER DYKE CONTACT.					
/	1216	1244	27	2C23CL	<<	P		<((
L			11	5T		==+1			
/	1244	1284	38	2C33CL	<<BR	P		<)<+	
L			21	5A		+1=3			
R				SOME PY OCCURS IN TENSION GASHES. MINOR BRECCIATION.					
/	1284	1299	14	8A10	MX	P		D.	
L			09	5G)+=			
/	1299	1339	39	2C43CL	<<BR	P		<)<+	
L			23	6T		=1=2			
R				LAST 0.6 M IS BRECCIATED.					
/	1339	1368	28	8A10	MX	P		D(
L			24	2G					
R				DYKE CONTAINS XENOLITHS OF 2C.					
/	1368	1410	41	8C10	VU	P		D(
L			12	8U					
R				VUGS ARE WEATHERED FELDSPAR.					
/	1410	1422	11	2C59QZ	<<BR	P		#3#1 D.	
L			09	8A		+++1			
R				CONTACT WITH DYKE BELOW NOT PRESERVED.					
/	1422	1445	21	8C10	<<	P		<(
L			09	8U		+1+2			
/	1437	1437				D F/	55		
/	1445	1465	20	2C89QZ	<<BR	P		#3#2 D?	
L			17	8A)+=			
/	1465	1471	06	8B00	TC	P			
L			03	5G					
/	1471	1476	05	2C89QZ	<<BR	P		#3#2 D?	
L			00	8A					
/	1476	1483	07	8A00	MX	P C/	60		
L			07	3B					
/	1483	1492	08	2C23	<<	P		<((
L			03	8A					
/	1492	1502	10	8A00	MX	P C/	28		
L			09	4G					
R				DYKE HAS GOOD 0.1 M CHILLED MARGINS.					
/	1502	1539	36	2C33	<<BR	P		<)<)<+*	
L			27	8T		=1=2			
R				TENSION GASHES FILLED WITH CL, PY, CP.					
/	1539	1577	36	2C22CL	<<WP	P		<+<)<)<*	
L			27	8G		=2=3			
R				WISPY COLOURATION.					

/	1577	1629	50	2C12CL	<<WP	.P		<)<*<).	
L			31	BA		=1=2			
/	1629	1668	38	2C11CL	<<WP	P BN	37	<)<*<).	
L			29	BG		++=1			
/	1668	1681	12	2C53	<<BR	P		#)#+	
L			09	7T)+=			
/	1681	1751	67	2C21CL	<<WP	P BN	42	<+<(<*	
L			42	7G		+=12		<*	
R				MINOR BRECCIA IN SPOTS.					
/	1751	1805	51	2C11CL	<<WP	P BN	53	<)<-<(<).	
L			33	BG		++=1		<(<	
/	1805	1824	18	2C21CL	<<WP	P BN	60	<+<*<)<-<?	
L			15	6T		+=12		<(<	
R				CL RICH SPOTS TO 2.0 CM DIAMETER.					
/	1824	1871	45	2C11CL	<<	P		<+<)<*<(<	
L			35	6P		+=12			
/	1871	1897	25	2C32CL	<<WP	P		<=<)<)<-	
L			12	AT		+213			
R				PATCH OF 2D FROM 188.8 TO 189.0 M.					
/	1897	1936	38	2C21CL	<<	P C/	58	<+<*<)<(<?)	
L			14	7A		+123 BD	58		
R				UPPER CONTACT VERY SHARP.					
/	1936	1963	26	2C22CL	<<BR	P BD	73	<+<*<+<*<V.	
L			14	6A		+=12			
R				CL RICH SPOTS.					
/	1963	1969	05	2H21	<<	P		<)	
L			00	5A		+++1			
/	1969	1991	22	2G11CL	<<	P BD	68	<)<)<)<*<	
L			19	BA		+)=1			
R				TUFFACEOUS MATRIX.					
/	1991	2010	19	2C11CL	<<	P		<*<(<-<).	
L			16	PA		++)1			
/	2010	2026	16	2C22CL	<<WP	P BN	58	B+<-<(<-<	
L			11	6T				<(<	
/	2026	2053	29	2C21	<<BR	P		<)<)<).	
L			10	5A		+++1			
/	2053	2076	22	1A11	<<	P BD	47	<)<)<D)<*<	
L			09	6A)+=1			
R				MORE OPEN FRAMEWORK TOWARDS BOTTOM OF INTERVAL.					
/	2076	2162	83	2C22CL	<<BR	P		<+<)<)<*<?<?	
L			58	BA		1213			
R				MINOR BRECCIATION.					
/	2162	2173	11	8A10	MX	P CU	43		
L			11	4G		CL	40		
R				GOOD CHILLED MARGINS, TOP AND BOTTOM.					
/	2173	2233	67	2C21	<<	P BD	62	<)<)<*<).	
L			46	BA					
/	2233	2259	26	1A10	<<	P BD	43	<)<*<)<?	
L			21	5A		++=1			
R				DOMINANT CLASTS ARE CHERT (QTZ), SOME ARGILLITE, TUFF. SOME CLASTS ALTERED, <<'D.					
/	2259	2279	19	2C11	<<WP	P BD	65	<*<)	
L			11	GA		++=1			
R				CONTAINS MINOR CLASTS AS ABOVE.					
/	2279	2303	23	1A10	<<	P C/	56	<*<)<*<	

L 12 5A +=+1
 R SAME AS 1A ABOVE (223.3 TO 225.9 M.).
 / 2303 2335 30 2C21CL << P <><><*<.
 L 11 BA =1=2 BN 48
 / 2335 2389 54 1A11CL << P <*<+<<
 L 47 5A ++++1
 R SAME AS 1A ABOVE, BUT MORE CL IN FRACTURES. MINOR 1D AT TOP
 R AND BOTTOM OF INTERVAL.
 / 2389 2411 21 2C22CL << P BD 25 <><+<*<.
 L 17 BA =+++1
 R THIN BAND OF 1A AT 239.4 M.
 R END OF HOLE.
 R SHUT HOLE DOWN BEFORE DESIRED END DUE TO BAD GROUND CONDITIONS
 R AT DRILLSITE, IE. DRILL WAS SINKING.

A001

ALAB

ATYP

AMTH

AUMM

EQUITY MINESITE LABORATORY

ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCOV	SAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001	195	254	5164	0.010	0.5	0.090	0.005	0.005	2.750	0.040
A001	254	297	5165	0.005	0.5	0.100	0.005	0.005	2.680	0.070
A001	417	440	5166	0.005	0.5	0.080	0.005	0.005	7.340	0.380
A001	440	470	5167	0.005	0.5	0.080	0.005	0.005	4.070	0.270
A001	470	500	5168	0.005	0.5	0.080	0.005	0.005	4.010	0.050
A001	500	540	5169	0.005	0.5	0.060	0.005	0.005	3.260	0.010
A001	540	570	5170	0.005	0.5	0.040	0.005	0.005	3.800	0.005
A001	570	600	5171	0.005	0.5	0.050	0.005	0.005	5.390	0.005
A001	600	630	5172	0.005	0.5	0.005	0.005	0.005	7.480	0.010
A001	630	660	5173	0.005	0.5	0.180	0.005	0.005	7.010	0.005
A001	660	690	5174	0.010	9.0	0.180	0.005	0.005	7.720	0.040
A001	690	720	5175	0.005	0.5	0.040	0.005	0.005	4.220	0.090
A001	720	750	5176	0.005	0.5	0.030	0.005	0.005	4.270	0.030
A001	750	780	5177	0.005	0.5	0.100	0.005	0.005	6.880	0.005
A001	780	810	5178	0.005	0.5	0.110	0.005	0.005	5.410	0.005
A001	810	840	5179	0.005	0.5	0.160	0.005	0.005	7.530	0.005
A001	840	870	5180	0.005	0.5	0.100	0.005	0.005	5.600	0.005
A001	870	900	5181	0.005	0.5	0.080	0.005	0.005	7.760	0.005
A001	900	930	5182	0.005	0.5	0.060	0.005	0.005	3.870	0.005
A001	930	960	5183	0.005	0.5	0.090	0.005	0.005	5.040	0.005
A001	960	980	5184	0.005	0.5	0.100	0.005	0.005	4.890	0.030
A001	980	1002	5185	0.005	0.5	0.110	0.005	0.005	4.310	0.005
A001	1020	1050	5186	0.005	0.5	0.110	0.005	0.005	4.270	0.010
A001	1050	1080	5187	0.005	0.5	0.100	0.005	0.005	7.110	0.005
A001	1080	1110	5188	0.020	0.5	0.070	0.010	0.005	3.930	0.040
A001	1110	1140	5189	0.090	0.5	0.060	0.020	0.010	3.450	0.005
A001	1140	1170	5190	0.005	0.5	0.070	0.005	0.010	5.300	0.005
A001	1170	1202	5191	0.005	0.5	0.100	0.005	0.010	7.640	0.020
A001	1215	1250	5192	0.005	0.5	0.110	0.005	0.010	4.340	0.005
A001	1250	1284	5193	0.005	0.5	0.110	0.005	0.010	12.970	0.010
A001	1294	1320	5194	0.020	0.5	0.110	0.005	0.010	4.680	0.010
A001	1320	1340	5195	0.005	0.5	0.100	0.005	0.010	5.010	0.005
A001	1410	1422	5196	0.005	0.5	0.160	0.005	0.010	7.280	0.005
A001	1445	1470	5197	0.020	12.0	0.180	0.020	0.010	15.890	0.040
A001	1470	1500	5198	0.005	0.5	0.430	0.005	0.010	4.270	0.020
A001	1500	1530	5199	0.340	0.5	0.110	0.005	0.090	9.400	0.005

A001	1530	1560	5200	0.260	0.5	0.080	0.005	0.010	4.890	0.005
A001	1560	1590	5201	0.140	0.5	0.070	0.005	0.005	2.370	0.005
A001	1590	1620	5202	0.040	0.5	0.050	0.005	0.005	2.500	0.005
A001	1620	1650	5203	0.030	0.5	0.090	0.005	0.005	3.320	0.005
A001	1650	1680	5204	0.005	0.5	0.040	0.005	0.005	4.780	0.005
A001	1680	1710	5205	0.005	0.5	0.100	0.005	0.005	4.320	0.005
A001	1710	1740	5206	0.005	0.5	0.050	0.005	0.005	3.890	0.005
A001	1740	1770	5207	0.005	0.5	0.140	0.005	0.005	3.060	0.005
A001	1770	1800	5208	0.030	0.5	0.120	0.005	0.005	3.240	0.005
A001	1800	1830	5209	0.020	0.5	0.060	0.005	0.005	3.870	0.005
A001	1830	1860	5210	0.070	0.5	0.060	0.005	0.005	2.770	0.005
A001	1860	1890	5211	0.040	0.5	0.120	0.005	0.005	3.540	0.005
A001	1890	1920	5212	0.140	3.0	0.020	0.005	0.005	3.720	0.005
A001	1920	1950	5213	0.180	4.0	0.030	0.005	0.005	3.400	0.005
A001	1950	1980	5214	0.110	4.0	0.030	0.005	0.005	3.440	0.005
A001	1980	2010	5215	0.120	7.0	0.020	0.005	0.005	3.690	0.010
A001	2010	2040	5216	0.040	2.0	0.050	0.005	0.005	4.310	0.005
A001	2040	2070	5217	0.050	4.0	0.050	0.005	0.005	4.260	0.010
A001	2070	2100	5218	0.090	4.0	0.030	0.005	0.005	3.110	0.010
A001	2100	2130	5219	0.230	8.0	0.050	0.005	0.005	4.450	0.010
A001	2130	2162	5220	0.040	3.0	0.020	0.005	0.005	4.560	0.005
A001	2173	2200	5221	0.005	2.0	0.020	0.005	0.005	3.840	0.010
A001	2200	2230	5222	0.005	1.0	0.040	0.005	0.005	3.960	0.005
A001	2230	2260	5223	0.010	1.0	0.030	0.005	0.005	4.310	0.010
A001	2260	2290	5224	0.005	1.0	0.060	0.005	0.005	3.730	0.005
A001	2290	2320	5225	0.010	2.0	0.060	0.005	0.005	4.210	0.010
A001	2320	2350	5226	0.005	1.0	0.080	0.005	0.005	3.020	0.005
A001	2350	2380	5227	0.010	2.0	0.080	0.005	0.005	3.180	0.010
A001	2380	2411	5228	0.005	2.0	0.090	0.005	0.005	4.010	0.005

R

END OF ASSAYS - END OF LOG

IDEN6B0201			XB6CH237 NQ 17MAR86DJH	G&D MARB6S38	0.0
IPRJ			EQUITY SILVER MINES LTD	SOUTH OF S.T. - ST GEOCODE	
S000	00	466	MT 190.8 090.0 -45.0		6403.12 7940.80 1318.41
S001	466	1420	190.8 090.0 -44.0		
S002	1429	1908	190.8 090.0 -42.0		
/SCL			MT.2MT.1		
LSCL			MT.2		
/NAM					MSCLQZPYCPTTASPR
LNAM					CB MGHESLGLMO
/	00	101	OVEN	P	
L					
R			:TRICONED AND CASED - NO CORE		
/	101	130	26 2C14MSCL <<	P	<.<.<*<.
L			00 GT		
R			:HEAVILY BROKEN CORE W/ LI ON FRACTURE SURFACES		
/	130	169	38 2C13CL <<	P	<.<.<*
L			12 7G		<.
R			:HEAVILY BROKEN CORE OVER FIRST HALF OF INT. :NO OXIDES		
R			:PATCHY MAROON COLOR		
/	169	190	21 2D12CL <<	P	<.<.
L			02 5G		
R			:MINOR 1A INTERLEVED WITH TUFFACEOUS MATRIX		
/	190	220	30 2D22CLMS <<	P	E.<.<.
L			02 5G		
R			:MINOR 1A INTERLEVED AS ABOVE W/CL RICH MATRIX :NO CNT. ATT.		
/	220	250	30 2D22CLMS <<	P	<*<.<.
L			05 6G		
R			:MINOR 1A INTERLEVED AS ABOVE INT. :2% LAPILLI FRAGS		
/	250	280	24 2D13CLMS <<	P	<*<*<.
L			02 6G		
R			:5% LAPILLI FRAGS. :TO 2E LOC. :NO 1A		
/	280	310	29 2D12CL <<	P	<*<*<.
L			04 5G		
R			:30% INTERLEVED 1A AND 2G (FINE EQUIV. OF 1A) :5% LAPILLI FRAGS.		
/	310	340	28 2D12CL <<	P	<*<*<.
L			02 6G		
R			:10% INTERLEVED 1A :2% LAPILLI FRAGS.		
/	340	362	21 2D12CL <<	P	<*<*
L			02 6G		
R			:TO 2C AND 2E LOC. :MINOR 1A? INTERLEVED		
/	362	392	29 2C13CLMS <<	P	<*<.
L			02 TG		
/	368	368	X	D	
R			:CLAY GOUGE (FAULT?) - NO ATTITUDE		
/	392	414	20 8A02CL P*	P CU 080	
L			18 4G	CL 075	
R			:20% FLAG PHENDS TO 10*2 MM :WEAK TRACHYTIC TEXT. :		
/	414	442	20 2C23CLMS <<	P	<*<.
L			03 7G		
R			:TO 2C25 LOC.		
/	442	457	14 1C20 <<	P	<*
L			00 AW		
/	457	489	28 1D20 <<	P	<.<.)
L			11 AW		
R			:TO 1C LOC. :10% INTERLEVED 2C		

/	489	530	40	2C12	<<	P	E.	<*<
L			03	6G				
R			:HEAVILY BROKEN UP INT.					
/	530	560	26	2C13CLMS	<<	P	E.	<><>
L			00	7G				
/	560	587	26	2C32CLMS	<<BR	P	<>	<><>
L			06	7G				
R			:TO 2C35 LOC. :TR MT?(MARCASITE)					
/	587	595	08	8A12CL	<<	P	CU 068	<.<.
L			06	6G			CL 040	
R			:PRE-MIN. DYKE :UPPER CNT. IRREG. :LOWER CNT. V. SHARP					
/	595	629	33	8A02CL	A*	P	A.	
L			30	5G			CL 045A.	
R			:2% QZ+CB A*					
/	629	660	30	2C23CLMS	<<	P	<*&*<*	
L			05	7G				
R			:8A W/ PHENOS 63.1-63.4 M					
/	660	690	29	2C34CLMS	<<	P	<>	<><>
L			05	TG				
R			:TO 2C44 LOC.					
/	690	720	29	2C44CLMS	<<	P	<>	<><>
L			15	TG				
R			:TO 2C11 @ EOI					
/	720	750	29	2C13CLMS	<<	P	<*	<.<.
L			03	TG				
R			:TO 2C14 LOC. AND 2C12 LOC.					
/	750	780	29	2C12CL	<<	P	S.<*	<.
L			04	6G				
R			: TO 2C13 LOC. W/ MS AS ENVELOPES : 8A 75.1-75.4 M (POST MIN.)					
/	780	810	30	2C12CL	<<	P	<*	<.
L			02	5G				
/	810	841	29	2C12CL	<<	P	<*	<.<.
L			04	5G				
R			:TO 2C23 LOC.					
/	841	859	16	1D10	<<	P	<*<><*	
L			03	5A				
R			:10% INTERLEVED 2C : NO BEDDING VISIBLE					
/	859	900	41	2C12CL	<<	P	<*	<.
L			05	5G				
R			: TO 2E NEAR EOI					
/	900	930	29	2C12CL	MS <<	P	<*	
L			03	5G				
R			: TO 2C24 LOC. : MINOR 2E @ 90.0 M.					
/	930	960	30	2C12CL	<<	P	<*	<.
L			02	5G				
R			: TO 2C24 LOC. AS ABOVE					
/	960	978	17	2C12CL	<<	P	<*	<.
L			01	5G				
R			: TO 2C23 LOC.					
/	978	994	15	1D12CL	<<	P	<.<.	<.
L			05	GA				
R			: NO CNTS. OBSERVED (SUSPECT GRADATIONAL) : MINOR 2C INTERLEVED					
/	994	1020	29	2C23CLMS	<<	P	<.<*	<.
L			03	TG				
/	1020	1050	29	2C12CL	MS <<	P	E*<*	

L 03 5G
 / 1050 1080 29 2C13CLMS << P <.* <.*
 L 19 7G
 / 1080 1110 27 2C13CLMS << P <.* <.*
 L 03 TG <.*
 / 1110 1140 29 2C12CL << P <.* <.*
 L 03 5G
 R : TO 2C13 LOC. : TR. TA ON << : TO 2C23 LOC.
 / 1140 1170 29 2C13CLMS << P <.* <.*
 L 03 TG
 R : TR. TA ON << : 0.2 M 1D INTERLEVED (NO ATTITUDES)
 / 1170 1200 29 2C12CL << P <.* <.*
 L 00 5G
 R : TO 2C13 LOC. : MINOR 1D INTERLEVED (NO ATTITUDES)
 / 1200 1230 29 2C12CL << P BN 051 <.* <.*
 L 03 5G <.*
 R : TO 2C13 LOC. : V. MINOR 1D INTERLEVED (NO ATTITUDES)
 / 1230 1260 29 2C12CL << P <.* <.*
 L 10 5G
 / 1260 1280 20 1D12CL << P <.* <.*
 L 03 5G
 R : W/ 10% INTERLEVED 2C : 15% CL RICH (TUFFACEOUS) MATRIX
 R : MINOR 1C AT SOI
 / 1280 1320 40 2C12CL << P <.* <.*
 L 30 5G
 / 1320 1350 29 2C12CL << P <.* <.*
 L 15 5G <.*
 R : TO 7G COLOR LOC. : MINOR 1D AS ABOVE 126.0-128.0 M : MINOR
 R 2C24 (GT COLOR)
 / 1350 1380 30 2C12CLMS << P <.* <.*
 L 25 5G
 R : TO 2C24 LOC. W/ST COLOR : 1D TO 1C LOC. 137.8-138.0 M
 / 1380 1410 29 2C25MSCL << P BD 040<.* <.*
 L 17 5T
 R : 30% INTERLEVED 1D
 / 1400 1400 X D F/ 013
 / 1410 1440 29 2C22CL MS << P E.* <.*
 L 03 5G
 R : 0.3 M 2C14 @ SOI (7G COLOR)
 / 1440 1470 30 2C22CL MS << P <.* <.* <.*
 L 09 5G <.*
 R : TO 7G COLOR LOC. : MOST OF CP IN ONE 2 CM THICK VEIN
 / 1470 1500 29 2C12CL << P E.* <.* <.*
 L 18 4G
 R : TO 2C24 LOC.
 / 1500 1528 28 2C12CL << P <.* <.* <.*
 L 17 4G
 R : 20% INTERLEVED 1D
 / 1528 1547 19 8A02CL P* P CU 04B
 L 16 4G CL 050 D.
 R : 3% ALTERED PYROX. PHENOS : GOOD INT. CNTS. X-CUTTING <<
 / 1547 1580 32 2C12CL << P BD 070E.* <.* <.*
 L 20 4G
 R : 10% INTERLEVED 1D
 / 1580 1610 30 2C23CLMS << P <.* <.* <.*

L 11 6G
 R : 20% INTERLEVED 1D AND 1C : TO 2C24 LOC.
 / 1610 1640 29 2C12CL << P <* <<.
 L 06 6G
 R : 10% INTERLEVED 1D AND 1C
 / 1640 1670 29 2J23CLMS << P BD 050 <* <*

 L 21 MG
 R : V. DISTINCT RX. TYPE W/ MAROON, GREEN & BUFF COLORAT'N
 R : OCC. LAPILLI FRAGS.
 / 1670 1700 29 2J12CL << P < <.
 L 23 MG
 R : TR. EP ON << : SAME DISTINCTIVE COLOR AS ABOVE INT.
 / 1700 1730 29 2J12CL << P <* <*

 L 17 MG <.
 R : TR. EP ON << : NO REGULAR BD ATTITUDE
 / 1730 1760 30 2J12CL << P BD 055<.* <*

 L 26 MG
 R : MINOR INTERLEVED 1D
 / 1760 1790 29 2J12CL << P <.<.<.

 L 21 MG <.
 R : AS ABOVE
 / 1790 1820 28 2J12CL MS << P BD 055 <*.<.<.

 L 19 MG
 R : TR. EP ON VV (QZ+PY+EP) : AS ABOVE INT. W/ LESS ASH : MINOR
 R 2D15
 / 1820 1850 29 2J12CL MS << P <*.<.<.

 L 24 MG
 R : MINOR 2D15
 / 1850 1880 30 2J12CL EP << P <*.<.<.

 L 23 MG
 R : EP ON SOME << : MINOR 2D15 : MINOR INTERLEVED 1D
 / 1880 1908 27 2J12CL EP << P BD 060 <.<.<*

 L 22 MG <.
 R : EP ON SOME << : 13% INTERLEVED 1A
 R END OF HOLE.

A001

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EQUITY MINESITE LABORATORY

ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCDV	SAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001	101	130	5229	0.020	0.5	0.090	.005	.005	3.300	0.005
A001	130	160	5230	0.005	1.0	0.090	.005	.005	3.930	0.005
A001	160	190	5231	0.01	2.0	0.110	.005	.005	6.260	0.010
A001	190	220	5232	0.01	1.0	0.040	.005	.005	5.270	0.005
A001	220	250	5233	0.03	3.0	0.030	.005	.005	5.300	0.005
A001	250	280	5234	0.020	3.0	0.070	0.001	0.001	5.120	0.001
A001	280	310	5235	0.030	3.0	0.150	0.001	0.001	5.290	0.001
A001	310	340	5236	0.040	3.0	0.090	0.001	0.005	5.480	0.001
A001	340	366	5237	0.005	0.5	0.050	0.001	0.020	3.850	0.001
A001	366	392	5238	0.020	0.5	0.070	0.001	0.001	3.770	0.001
A001	414	440	5239	0.001	0.5	0.060	0.001	0.020	3.060	0.001
A001	440	470	5240	0.005	0.5	0.040	0.001	0.001	2.720	0.001
A001	470	500	5241	0.020	0.5	0.040	0.001	0.001	3.010	0.001
A001	500	530	5242	0.130	5.0	0.040	0.001	0.001	3.220	0.001
A001	530	560	5243	0.250	8.0	0.050	0.001	0.001	3.490	0.001

A001	560	587	5244	0.150	5.0	0.050	0.001	0.001	3.190	0.001
A001	587	595	5245	0.005	2.0	0.120	0.001	0.005	3.750	0.005
A001	629	660	5246	0.060	3.0	0.250	0.001	0.001	2.750	0.001
A001	660	690	5247	0.170	5.0	0.040	0.001	0.001	3.430	0.001
A001	690	720	5248	0.920	16.0	0.060	0.001	0.001	4.230	0.001
A001	720	750	5249	0.140	5.0	0.050	0.001	0.001	3.440	0.001
A001	750	780	5250	0.005	0.5	0.060	0.001	0.001	3.520	0.001
A001	780	810	5251	0.001	0.5	0.010	0.001	0.001	3.490	0.001
A001	810	840	5252	0.005	0.5	0.020	0.001	0.001	3.460	0.001
A001	840	870	5253	0.200	5.0	0.090	0.001	0.001	3.000	0.001
A001	870	900	5254	0.005	0.5	0.040	0.005	0.030	3.340	0.005
A001	900	930	5255	0.005	0.5	0.050	0.005	0.010	3.740	0.005
A001	930	960	5256	0.005	0.5	0.050	0.005	0.005	3.760	0.005
A001	960	990	5257	0.005	0.5	0.070	0.005	0.010	4.000	0.005
A001	990	1020	5258	0.010	0.5	0.050	0.005	0.005	3.110	0.005
A001	1020	1050	5259	0.005	0.5	0.050	0.005	0.020	4.270	0.005
A001	1050	1080	5260	0.005	0.5	0.060	0.005	0.030	3.980	0.005
A001	1080	1110	5261	0.005	0.5	0.090	0.005	0.010	3.970	0.005
A001	1110	1140	5262	0.005	0.5	0.080	0.005	0.005	3.680	0.005
A001	1140	1170	5263	0.005	0.5	0.070	0.005	0.020	3.750	0.005
A001	1170	1200	5264	0.010	0.5	0.050	0.005	0.020	3.500	0.005
A001	1200	1230	5265	0.005	0.5	0.040	0.005	0.005	3.590	0.005
A001	1230	1260	5266	0.020	0.5	0.020	0.005	0.030	2.980	0.005
A001	1260	1290	5267	0.005	0.5	0.050	0.005	0.010	3.280	0.005
A001	1290	1320	5268	0.010	0.5	0.040	0.005	0.020	3.190	0.005
A001	1320	1350	5269	0.005	0.5	0.030	0.005	0.010	3.640	0.005
A001	1350	1380	5270	0.005	0.5	0.110	0.005	0.040	3.470	0.005
A001	1380	1410	5271	0.005	0.5	0.050	0.005	0.020	3.440	0.005
A001	1410	1440	5272	0.010	0.5	0.050	0.005	0.030	3.400	0.005
A001	1440	1470	5273	0.070	0.5	0.110	0.005	0.020	4.640	0.005
A001	1470	1500	5274	0.005	0.5	0.050	0.005	0.030	3.660	0.005
A001	1500	1528	5275	0.010	0.5	0.050	0.005	0.010	3.260	0.005
A001	1547	1580	5276	0.005	0.5	0.040	0.005	0.020	3.460	0.005
A001	1580	1610	5277	0.005	0.5	0.040	0.005	0.010	3.250	0.005
A001	1610	1640	5278	0.010	0.5	0.080	0.005	0.005	2.810	0.005
A001	1640	1670	5279	0.005	0.5	0.050	0.005	0.010	5.900	0.005
A001	1670	1700	5280	0.005	0.5	0.070	0.005	0.005	3.140	0.005
A001	1700	1730	5281	0.005	0.5	0.070	0.005	0.005	2.010	0.005
A001	1730	1760	5282	0.005	0.5	0.040	0.005	0.005	1.920	0.005
A001	1760	1790	5283	0.005	0.5	0.050	0.005	0.005	2.310	0.005
A001	1790	1820	5284	0.005	0.5	0.060	0.005	0.005	2.290	0.005
A001	1820	1850	5285	0.005	0.5	0.030	0.005	0.005	2.480	0.005
A001	1850	1880	5286	0.005	0.5	0.010	0.005	0.005	2.390	0.005
A001	1880	1908	5287	0.005	0.5	0.010	0.005	0.005	1.740	0.005

R

END OF ASSAYS - END OF LOG

IDEN6B0201										
IPRJ										
S000	00	419 MT	157.3	090.0	-45.0					
S001	419	1206	157.3	090.0	-42.0					
S002	1206	1573	157.3	090.0	-44.0					
/SCL		MT.2MT.1								
L SCL		MT.2								
/NAM										
LNAM										
/	00	152								
L										
R										
R										
/	152	184	20	2C13MS	<<	P			<><<<*	
L			00	5T						
R										
R										
/	184	244	54	2C12CL	<<	P			<+ <<	
L			06	TG						
R										
R										
/	244	293	35	2C13MS	<<	P			E)<<<*	
L			05	5T						
R										
R										
/	293	315	21	2C34MS	<<	P			E(<<)<+<<	
L			13	6T			++=1		<-	
R										
R										
/	315	332	16	2C45MS	<<	P			<<<*	
L			09	7T			+1=2		<<	
R										
R										
/	331	332							D F/	
L										
R										
R										
/	332	389	54	2C34MS	<<BR	P			E(<<)<	
L			15	6T			12=4		<<	
R										
R										
/	389	408	09	2C45MS	<<	P			D) D)	
L			00	7T						
R										
R										
/	398	408							D F/	
L										
R										
R										
/	408	439	11	2C34MS	<<BR	P			E(++D)<.	
L			00	6T						
R										
R										
/	420	439							D F/	
L										
R										
R										
/	439	497	55	2C23MS	<<	P			E*(<)<+	
L			13	5T			++23			
R										
R										
/	497	503	16	2C75MSQZ	BR<<	P			#1#+	
L			13	6T) +=			
R										
R										
/	503	532	27	2C13MS	<<	P			<*<	
L			19	TA			=1+2			
R										
R										
/	532	566	32	2C14MS	<<	P			<*<	
L			11	5T			=2=3			
R										
R										
/	566	590	22	2C55MSQZ	BR<<	P			<(#=#+	
L			09	5T			+=1			
R										
R										
/	590	674	77	2C24MS	<<	P			E)<*<	
L			19	6T			1214			

R CHLORITE GIVES BLUE COLOUR TO <<'S. CORE QUITE BROKEN, BUT
 R UNIFORM.
 / 674 689 15 2C13 << P <)<<<*<
 L 13 TG)1+2
 / 689 725 26 2C24MS <<BR P <*)V)+<
 L 00 6T
 R MINOR BRECCIATION. CORE QUITE BROKEN, POOR RECOVERY.
 / 725 813 80 2C14MS << P <)<V)*<)<
 L 21 6T 11+3
 / 813 820 07 2C55MS BR<< P <)<#)+#=<
 L 03 TA
 R BLUE TARNISH ON SOME PYRITE GRAINS.
 / 820 831 10 2C23 << P <)<)<)<
 L 00 5T 1102
 / 831 856 23 2C13 <<BR P <)<V)*V)+<
 L 06 AT 11=3
 R MINOR BRECCIATION.
 / 856 912 51 2C24MS << P E)Q)Q)+<
 L 03 AT 12=4
 R CORE QUITE BROKEN, DISRUPTED. IE. MINOR DISPLACEMENT ON <<'S.
 / 912 942 29 2C14MS << P E)(<)<)<
 L 03 5T 11+3
 / 942 1001 56 2C24MS <<BR P E)V)+Q)=<
 L 11 AT VU 12=4
 R CORE VERY BROKEN. VERY SIMILIAR TO 85.6 TO 91.2 M.
 / 1001 1073 55 2C14MS << P E)(<)<)+<?<
 L 03 5T <.<
 R CORE VERY BROKEN, POOR RECOVERY.
 / 1073 1099 25 2C13 <<WP P <*)V)*<)<
 L 11 5T +1+2
 / 1099 1137 37 2C12CL << P V/ 68 <)<V)(<<(D.D)?<
 L 31 4A ==+2 V.<
 R SPOT OF ASH TUFF AT 112.0 M.
 / 1137 1146 09 2C29QZ <<BR P <)<)+1Q)+ D)?<
 L 06 AW +=)1
 R MINOR BRECCIATION - DISRUPTION.
 / 1146 1161 15 8B10 TC P CU 75 <*<
 L 13 3G +=)1 CL 73
 / 1161 1198 37 8A10 MX P CU 73 <*)D.<
 L 29 BG +=)1 F/ 73
 R CONTACT BETWEEN DYKES IS FAULTED.
 / 1198 1226 27 2C33 <<BR P <)<)+=Q)+<
 L 23 BT 11=3
 R SLIGHTLY BRECCIATED NEAR LOWER CONTACT. UNIT MAYBE XENLITH.
 / 1226 1252 24 8C11 VJMX P CU 70 D-<
 L 16 YW
 R SMALL XENLITH OF DUST TUFF AT 125.0 M.
 / 1252 1287 34 8A00 MX P F/ 68 <(D.<
 L 27 GB
 / 1287 1293 06 8C10 MX P D-<
 L 06 AW
 R CONTACT BETWEEN TWO ABOVE DYKES GRADATIONAL.
 / 1293 1304 11 2C55MS BR P #=#)+<
 L 06 5T)))<)+<
 / 1304 1332 26 2C24MS <<BR P E)*<)<)+<

L 09 5T =1+2
 R MINOR BRECCIATION.
 / 1332 1344 11 2C13 <<VU P E*(<+<+
 L 03 5T +=+1
 R VUGS HAVE COARSE GRAINED PYRITE CRYSTALS (EUHEDRAL).
 / 1344 1354 10 2D13 << P (<)<
 L 03 7A)))<+
 / 1354 1389 33 2C14 << P E*(<)<
 L 09 5T =1+2
 / 1389 1409 19 2C23 <<BR P (<)<+<
 L 03 AT =1+2 <-
 R MINOR BRECCIATION.
 / 1409 1438 27 2C13 << P E*(<*<*)
 L 03 5T =1=2
 / 1438 1450 11 2D13 << P E(<)<+<
 L 03 AT)++1
 / 1450 1488 34 2C23 << P E(<*<*)
 L 03 5T 5
 R CORE VERY BROKEN. HARD TO ESTIMATE FRACTURES.
 / 1488 1515 25 2C34MS <<BR P V/ 10 (<0)<+<
 L 06 5T 1214
 R MINOR BRECCIATION.
 / 1515 1540 23 2C24MS << P E*(<*<*)
 L 05 4T 1124
 R MINOR EUHEDRAL PYRITE IN <<'S.
 / 1540 1573 32 2C13 << P V/ 48 E*(<*<*)<
 L 11 AT 11+2 <.
 R PATCH OF ASH TUFF AT 156.3 M., AND AT VERY END OF HOLE,
 R 157.3 M.
 R END OF HOLE.

A001
 ALAB
 ATYP
 AMTH
 AUMM

EQUITY MINESITE LABORATORY
 ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCDVSAMPLE	RDD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN	
A001	152	180	5288	0.005	0.5	0.020	0.005	0.005	2.010	0.005
A001	180	210	5289	0.005	0.5	0.020	0.005	0.005	3.240	0.005
A001	210	240	5290	0.010	0.5	0.080	0.005	0.005	4.300	0.005
A001	240	270	5291	0.020	0.5	0.050	0.005	0.005	3.360	0.005
A001	270	300	5292	0.040	0.5	0.240	0.005	0.005	4.120	0.005
A001	300	330	5293	0.210	0.5	0.070	0.005	0.005	3.950	0.005
A001	330	360	5294	0.020	0.5	0.080	0.005	0.005	2.940	0.005
A001	360	390	5295	0.040	0.5	0.120	0.005	0.005	2.980	0.005
A001	390	440	5296	0.020	0.5	0.050	0.005	0.005	5.010	0.005
A001	440	470	5297	0.010	0.5	0.030	0.005	0.005	2.870	0.005
A001	470	500	5298	0.005	0.5	0.030	0.005	0.005	6.500	0.005
A001	500	530	5299	0.005	0.5	0.030	0.005	0.005	6.540	0.005
A001	530	560	5300	0.005	0.5	0.050	0.005	0.005	4.330	0.005
A001	560	590	5301	0.005	0.5	0.040	0.005	0.005	7.760	0.005
A001	590	620	5302	0.005	0.5	0.040	0.005	0.005	3.660	0.005
A001	620	650	5303	0.005	0.5	0.040	0.005	0.005	4.310	0.005
A001	650	680	5304	0.020	0.5	0.070	0.005	0.005	4.140	0.005
A001	680	720	5305	0.010	0.5	0.050	0.005	0.005	7.050	0.005
A001	720	750	5306	0.005	0.5	0.040	0.005	0.005	4.130	0.005
A001	750	780	5307	0.005	0.5	0.070	0.005	0.005	3.800	0.005

A001	780	810	5308	0.020	0.5	0.040	0.005	0.005	3.490	0.005
A001	810	840	5309	0.005	0.5	0.050	0.005	0.005	7.160	0.005
A001	840	870	5310	0.010	0.5	0.040	0.005	0.005	3.470	0.005
A001	870	900	5311	0.005	0.5	0.080	0.005	0.005	3.150	0.005
A001	900	930	5312	0.005	0.5	0.050	0.005	0.005	4.580	0.005
A001	930	950	5313	0.020	0.5	0.060	0.005	0.005	9.150	0.010
A001	950	980	5314	0.005	5.0	0.080	0.005	0.005	6.000	0.005
A001	980	1010	5315	0.005	3.0	0.060	0.005	0.005	7.360	0.005
A001	1010	1040	5316	0.005	2.0	0.060	0.005	0.005	4.120	0.005
A001	1040	1070	5317	0.005	2.0	0.020	0.005	0.005	4.570	0.020
A001	1070	1100	5318	0.005	3.0	0.040	0.005	0.005	4.940	0.005
A001	1100	1125	5319	0.015	11.0	0.050	0.010	0.060	5.670	0.150
A001	1125	1146	5320	0.022	11.0	0.070	0.010	0.005	4.220	0.090
A001	1198	1226	5321	0.005	4.0	0.080	0.005	0.020	5.210	0.005
A001	1293	1320	5322	0.005	3.0	0.080	0.005	0.005	5.360	0.005
A001	1320	1350	5323	0.005	5.0	0.230	0.005	0.005	8.130	0.010
A001	1350	1380	5324	0.005	3.0	0.070	0.005	0.005	6.910	0.005
A001	1380	1410	5325	0.005	9.0	0.060	0.010	0.005	7.030	0.005
A001	1410	1440	5326	0.005	4.0	0.050	0.005	0.005	6.200	0.005
A001	1440	1470	5327	0.005	4.0	0.040	0.005	0.005	6.610	0.010
A001	1470	1500	5328	0.005	2.0	0.040	0.005	0.005	3.200	0.010
A001	1500	1530	5329	0.005	4.0	0.030	0.010	0.010	4.680	0.010
A001	1530	1573	5330	0.005	3.0	0.020	0.005	0.005	4.530	0.010

R

END OF ASSAYS - END OF LOG

L 19 TG
 R : LOCAL CL SPOTS (2D?)
 / 470 500 30 2C24CLMS << P <<<<<<
 L 23 TG
 R : TO 2C13 LOC. : TO 2C25 TOWARDS EDI
 / 500 530 29 2C13CLMS << P <<<<<<
 L 16 6G
 R : LOCAL CL SPOTTING
 / 502 502 X VU D4V/ 030 V4V6
 / 530 560 27 2C25MS << P <.V*V+
 L 03 5T
 R : TO 2C13 TOWARDS EDI : NUMEROUS THIN QZ+PY VEINS
 / 560 590 29 2C14CLMS << P <.<.<*<
 L 13 6T
 R : 20% 2C25
 / 590 620 27 2C25MS << P <.<(<<+
 L 03 6T
 R : TO 2C13 LOC. : NUMEROUS QZ+PY VEINS :CL IN 2C13 MICRO VEINS
 / 620 650 29 2C25MS << P <(<<+<.
 L 07 6T
 R : TO 2C33 TOWARDS EDI W/ CL IN << + TR. CP
 / 634 634 X D3V/ 035 V2V8
 / 650 680 30 2C33CLMS << P <*<.<.
 L 24 5G
 / 676 676 X D3V/ 040 V7V3
 / 680 710 29 2C33CLMS << P <*<.<*<
 L 21 TG
 R : TO 2C35 LOC. W/ 5T COLOR
 / 710 740 28 2C23CLMS << P <*<.<(<)
 L 19 TG
 R : TO 2C35 LOC. W/ 5T COLOR
 / 740 770 29 2C24MSCL << P <*<.<(<(<)
 L 24 6T
 / 770 800 29 2C24MSCL << P <*<.<(<(<)
 L 23 6T
 R : TO 2C12 TOWARDS EDI
 / 800 830 27 2C25MS << P <(<(<)
 L 18 6T
 R : TO 2C12 AT SOI
 / 830 860 29 2C25MS << P <.<(<(<)
 L 07 6T
 R : TO 2C24 LOC.
 / 857 857 X D2V/ 030 V2V8
 / 860 890 28 2C24MSCL << P <(<(<(<)
 L 19 6T
 / 890 920 28 2C34MSCL << P <(<(<(<)
 L 21 6T
 / 920 950 26 2C24MSCL << P <(<(<(<)
 L 05 6T
 R : HEAVILY BROKEN CORE W/ CLAY (GOUGE?) AND LOST CORE 94.0-94.9
 R : TO 2C15 LOC. W/D CL ON <<
 / 923 923 X D2V/ 035 V6V4
 / 950 980 27 2C35MS << P <.<(<(<)
 L 05 6T
 R : TO 2C55 97.0-98.0 M W/ MINOR CY

/ 980 1010 29 2C25MS << P <<<<
 L 05 6T
 R : TO 2C35 LOC.
 / 1010 1040 29 2C24MSCL << P <<<.<*<
 L 11 6T
 / 1040 1070 29 2C24MSCL << P <<<.<*<
 L 09 6T
 R : TO 2C25 AND 2C12 LOC.
 / 1070 1100 29 2C13CLMS << P <<<.<*<
 L 03 6T
 / 1100 1130 28 2C13CLMS << P <<<*<*<
 L 10 6T
 R : TO 2C25 TOWARDS EOI
 / 1130 1160 29 2C25MS << P <*<+
 L 04 5T
 R : NOTE ABSENCE OF CL.
 / 1160 1190 25 2C25MS << P <<<+
 L 02 5T
 R : HEAVILY BROKEN AND LOST CORE 117.0-117.7 M : QZ+PY ENVELOPES
 / 1190 1220 28 2C25MS << P <<<*<
 L 00 5T
 R : FAULT ZONE 121-122 M (NO ATTITUDE) CLAY GOUGE
 / 1220 1250 15 2C25MS << P <<<*<
 L 00 5T
 R : HEAVILY BROKEN CORE W/ NUMEROUS ZONES CLAY GOUGE
 / 1250 1280 25 2C25MS << P <<<*<
 L 00 5T
 R : HEAVILY BROKEN CORE W/ NUMEROUS ZONES OF CLAY GOUGE
 / 1280 1310 28 2C25MS << P <<<*<
 L 05 5T
 R : HEAVILY BROKEN CORE W/ LOCAL CLAY GOUGE
 / 1310 1340 29 2C25MS CL << P +<<<<*<
 L 04 5T
 R : V. MINOR CL AS FLOODING : NO CL IN MICROVEINS
 / 1340 1370 29 2C25MS << P <<<*<
 L 00 5T
 R : MOD. BROKEN CORE W/O GOUGE
 / 1370 1400 28 2C25MS CL << P +<<<<*<
 L 03 5T
 R : PY ALSO AS SPOTS TO 0.5 MM : LOOKS LIKE 2D LOC. : TR CL LOC.
 / 1400 1430 29 2C25MS << P <<<*< <.
 L 04 5T
 R : TR. SHINEY GREY SDE. MINERAL W/ QZ (TT?)
 / 1430 1460 19 2C25MS << P <<<<
 L 00 5T
 R : HEAVILY BROKEN CORE
 / 1460 1490 13 2C25MS CL << P +.<<<<
 L 00 5T
 R : LOST AND BROKEN CORE W/ CLAY GOUGE 146.0-147.8 M (0.2 M CORE)
 R : MINOR LOCAL CL ALT'N
 / 1490 1520 20 2C25MS << P <<<<
 L 00 5T
 R : LOC'LLY PY SPOTTED : HEAVILY BROKEN CORE W/O GOUGE
 / 1520 1550 28 2C25MS << P <<<<
 L 04 5T

R : HEAVILY BROKEN CORE : LOC. PY SPOTTING
 / 1550 1580 29 2C25MS << P <<+>
 L 00 5T
 R : TO 2C35 LOC. : HEAVILY BROKEN CORE : MINOR TECTONIC BXIA W/
 R CLAY GOUGE
 / 1580 1610 27 2C25MS << P <<<<
 L 00 5T
 R : LIGHT GREY QZ. RICH ENVELOPES
 / 1585 1585 X D3V/ 062 V7V3
 / 1610 1640 29 2C25MS << P <<<<
 L 04 5T
 R : STILL NO CL ON MICROVEINS
 / 1640 1670 25 2C25MS << P <<<<
 L 02 5T
 R : TO 2D TOWARDS EOI
 / 1670 1700 25 2C25MS << P <<<<
 L 00 5T
 R : HEAVILY BROKEN CORE W/O GOUGE
 / 1700 1728 26 2C25MS << P <<<<
 L 00 5T
 R : HEAVILY BROKEN CORE W/ PATCHES GOUGE
 / 1728 1767 34 2C45MS QZ << P <<<+>
 L 25 4T
 R : NOTE STRANGE COLOR- UNLIKE TYPICAL 2C : TO 2D45 LOC. : TR.
 R TO? W/ SDES. :LIGHT GREY QZ RICH ENVELOPES
 / 1750 1750 X D F/ 050
 / 1767 1786 16 8A02CL P* P CU 045
 L 08 5G
 R : 20% PLAG PHENOS TO 10 MM : LOWER CNT. NOT OBSERVED
 / 1786 1798 11 8A06CY P
 L 00 7T
 R : TOTALLY ALTERED TO CLAY : 8A? : CNTS NOT OBSERVED
 / 1798 1820 21 2C45MS QZ <<BR P <*<.<>
 L 16 4T
 R : TO 2C55 AT SOI : UT COLOR LOCALLY : TR TO? IN SDE PATCHES
 R :LIGHT GREY QZ RICH ENVELOPES
 / 1820 1844 24 2C45MS QZ << P <.<.<>
 L 20 4T
 R : TO 2C35 LOC. : UT COLOR LOC. : TO 2D LOC. : NOTE SAME
 R STRANGE COLOR AS ABOVE : LIGHT GREY QZ RICH ENVELOPES
 / 1844 1919 73 8C03MS P* P CU 060
 L 51 7C
 R : 10% PLAG PHENOS TO 3 MM : 7G COLOR LOC. : LOWER CNT. NOT
 R OBSERVED DUE TO BROKEN CORE
 / 1919 1950 29 2C25MS QZ << P <.<+<+>
 L 06 4T
 R : TO 5T COLOR TOWARDS EOI : NOTE TR CL
 / 1950 1980 29 2C25MS << P << 045 <*<+>
 L 02 5T
 / 1980 2010 28 2C25MS << P << 060 <*<+>
 L 03 5T
 / 2010 2040 29 2C15MS << P BD 060 <<<<
 L 02 5T
 R : 10% INTERLEVED 1D : LIGHT GREY QZ RICH ENVELOPES
 / 2040 2064 23 2C25MS << P <*<+>

L 00 5T
 R : MINOR 1D INTERLEVED
 / 2064 2079 14 BA02CL A* P CU 070 A(
 L 14 4G A(
 R : LOWER CNT. NDT EXPOSED
 / 2079 2110 30 2C25MS << P <*<+
 L 03 5T
 R : LIGHT GREY QZ RICH ENVELOPES
 / 2110 2140 30 2C35MS << P <*<=
 L 05 5T
 R : TO 2C25 LOC. : LIGHT GREY QZ RICH ENVELOPES
 / 2140 2170 28 2C35MS <<BR P <*<=
 L 07 5T
 R : 2C85 LAST 0.2 M OF INT.
 / 2166 2166 X D F/
 R : CLAY GOUGE - NO ATTITUDE
 / 2170 2179 09 BA02CL A* P CU 065
 L 07 4G CL 055A=
 R : GOOD CHILLED INTRUSIVE CNTS.
 / 2179 2184 04 2C85MS BR P ==#=
 L 02 5T
 / 2184 2246 61 BA02CL A*P* P CU 039
 L 57 4G CL 051 D.
 R : TO 8A06 W/ 8G COLOR AT SOI AND EOI
 / 2246 2270 22 2C35MS <<BR P <)<=
 L 05 5T
 R : 2C85 (TECTONIC BXIA) AT SOI
 / 2270 2300 28 2C25MS << P << 061 <(<(<
 L 04 5T
 R : TR DARK GREY SDE? MINERAL (TT?)
 / 2300 2330 28 2C25MS << P << 048 <(<(<
 L 02 5T
 R : 2D? (PHYLIC ALT'N MAY MAKE IT DIFFICULT TO DETERMINE
 ORIGINAL TEXTURE!!)
 / 2330 2360 29 2C15MS << P <(<(<
 L 00 5T
 R : TR DARK GREY SDE? AS ABOVE 227-230 M : TO 2D LOC.
 / 2360 2390 28 2C15MS << P <(<(<
 L 00 5T <.
 R : TR DARK GREY SDE? AS ABOVE : 2D?
 / 2390 2420 28 2D25MS << P << 060 <)<+
 L 05 5T
 R : TO 2C LOC. : TO 2D15 LOC.
 / 2420 2457 32 2D15MS << P << 047 <(<(<
 L 00 5T
 R : TO 2C LOC.
 R END OF HOLE.

A001
 ALAB
 ATYP
 AMTH
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EQUITY MINESITE LABORATORY
 ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCOV	SAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001	46	79	5331	0.036	1.0	0.010	0.005	0.005	4.370	0.005
A001	79	110	5332	0.022	1.0	0.060	0.005	0.005	3.430	0.005
A001	110	140	5333	0.023	2.0	0.070	0.005	0.005	3.910	0.005

A001	140	170	5334	0.010	0.5	0.080	0.005	0.005	4.170	0.005
A001	170	200	5335	0.010	0.5	0.120	0.005	0.005	4.330	0.005
A001	200	230	5336	0.020	0.5	0.060	0.005	0.005	4.440	0.005
A001	230	260	5337	0.020	0.5	0.060	0.005	0.005	7.630	0.005
A001	260	290	5338	0.030	0.5	0.100	0.005	0.005	4.260	0.005
A001	290	320	5339	0.020	0.5	0.090	0.005	0.005	2.850	0.005
A001	320	350	5340	0.020	0.5	0.050	0.005	0.005	4.250	0.005
A001	350	380	5341	0.010	0.5	0.060	0.005	0.005	3.830	0.005
A001	380	410	5342	0.020	0.5	0.050	0.005	0.005	3.960	0.005
A001	410	440	5343	0.010	0.5	0.080	0.005	0.005	3.950	0.005
A001	440	470	5344	0.020	0.5	0.080	0.005	0.005	4.160	0.005
A001	470	500	5345	0.020	0.5	0.070	0.005	0.005	4.290	0.005
A001	500	530	5346	0.040	2.0	0.040	0.010	0.005	5.500	0.005
A001	530	560	5347	0.020	1.0	0.070	0.005	0.005	4.640	0.005
A001	560	590	5348	0.010	0.5	0.020	0.005	0.005	3.930	0.005
A001	590	620	5349	0.020	2.0	0.040	0.005	0.005	4.430	0.005
A001	620	650	5350	0.020	1.0	0.060	0.005	0.005	4.200	0.005
A001	650	680	5351	0.030	0.5	0.060	0.005	0.005	4.970	0.005
A001	680	710	5352	0.020	1.0	0.060	0.005	0.005	4.880	0.100
A001	710	740	5353	0.060	3.0	0.050	0.005	0.005	5.600	0.020
A001	740	770	5354	0.050	0.5	0.040	0.005	0.005	4.150	0.005
A001	770	800	5355	0.030	0.5	0.060	0.005	0.005	4.000	0.005
A001	800	830	5356	0.010	0.5	0.050	0.005	0.005	3.620	0.005
A001	830	860	5357	0.040	0.5	0.040	0.005	0.005	4.070	0.005
A001	860	890	5358	0.030	7.0	0.210	0.010	0.005	3.980	0.005
A001	890	920	5359	0.020	5.0	0.060	0.010	0.005	4.640	0.005
A001	920	950	5360	0.020	4.0	0.050	0.005	0.005	3.770	0.005
A001	950	980	5361	0.005	0.5	0.040	0.005	0.005	4.780	0.005
A001	980	1010	5362	0.010	1.0	0.080	0.005	0.005	3.340	0.005
A001	1010	1040	5363	0.040	12.0	0.050	0.020	0.005	4.600	0.005
A001	1040	1070	5364	0.020	1.0	0.070	0.005	0.005	3.790	0.005
A001	1070	1100	5365	0.005	1.0	0.070	0.005	0.005	4.880	0.005
A001	1100	1130	5366	0.010	3.0	0.040	0.005	0.005	4.380	0.005
A001	1130	1160	5367	0.005	1.0	0.050	0.005	0.005	5.110	0.005
A001	1160	1190	5368	0.005	1.0	0.040	0.005	0.005	4.080	0.030
A001	1190	1220	5369	0.010	2.0	0.040	0.005	0.005	4.290	0.005
A001	1220	1250	5370	0.020	3.0	0.030	0.010	0.005	5.240	0.005
A001	1250	1280	5371	0.020	2.0	0.060	0.010	0.005	5.550	0.005
A001	1280	1310	5372	0.005	3.0	0.040	0.005	0.005	4.710	0.005
A001	1310	1340	5373	0.020	3.0	0.050	0.010	0.010	4.730	0.005
A001	1340	1370	5374	0.030	1.0	0.050	0.005	0.005	4.640	0.005
A001	1370	1400	5375	0.010	2.0	0.060	0.005	0.020	3.440	0.005
A001	1400	1430	5376	0.010	3.0	0.050	0.010	0.010	5.570	0.005
A001	1430	1460	5377	0.005	2.0	0.040	0.010	0.005	5.600	0.005
A001	1460	1490	5378	0.010	2.0	0.040	0.005	0.005	2.720	0.005
A001	1490	1520	5379	0.020	3.0	0.050	0.005	0.005	3.560	0.005
A001	1520	1550	5380	0.005	4.0	0.070	0.005	0.030	3.720	0.005
A001	1550	1580	5381	0.005	1.0	0.050	0.005	0.005	4.240	0.005
A001	1580	1610	5382	0.005	3.0	0.050	0.005	0.005	3.290	0.005
A001	1610	1640	5383	0.005	2.0	0.050	0.005	0.005	3.590	0.005
A001	1640	1670	5384	0.020	7.0	0.040	0.010	0.005	4.770	0.005
A001	1670	1700	5385	0.005	2.0	0.060	0.005	0.005	3.860	0.005
A001	1700	1730	5386	0.005	0.5	0.040	0.005	0.005	3.250	0.010
A001	1730	1767	5387	0.005	0.5	0.040	0.005	0.005	5.760	0.060
A001	1798	1820	5388	0.005	0.5	0.040	0.005	0.005	7.320	0.005

A001	1820	1844	5389								
A001	1919	1950	5390	0.005	0.5	0.040	0.005	0.005	3.200	0.005	
A001	1950	1980	5391	0.005	0.5	0.010	0.005	0.005	2.730	0.005	
A001	1980	2010	5392	0.005	0.5	0.020	0.005	0.005	4.390	0.005	
A001	2010	2040	5393	0.005	0.5	0.070	0.005	0.005	3.700	0.005	
A001	2040	2064	5394	0.005	0.5	0.030	0.005	0.005	2.540	0.005	
A001	2079	2110	5395	0.005	0.5	0.020	0.005	0.005	4.890	0.005	
A001	2110	2140	5396	0.005	0.5	0.010	0.005	0.005	4.810	0.005	
A001	2140	2170	5397	0.030	16.0	0.030	0.005	0.005	8.050	0.120	
A001	2170	2184	5398	0.030	11.0	0.040	0.005	0.005	5.170	0.050	
A001	2246	2270	5399	0.005	0.5	0.020	0.005	0.005	8.670	0.050	
A001	2270	2300	5400	0.005	0.5	0.010	0.005	0.005	5.520	0.060	
A001	2300	2330	5401	0.005	0.5	0.040	0.005	0.005	5.370	0.005	
A001	2330	2360	5402	0.005	0.5	0.070	0.005	0.005	3.580	0.005	
A001	2360	2390	5403	0.005	0.5	0.010	0.005	0.005	3.900	0.030	
A001	2390	2420	5404	0.005	0.5	0.020	0.005	0.005	5.300	0.005	
A001	2420	2457	5405	0.005	0.5	0.010	0.005	0.005	2.510	0.005	

R

END OF ASSAYS - END OF LOG

IDEN6B0201			X86CH240	NO	27MAR86	DJH	G&D	MAR86	S38	0.0
IPRJ			EQUITY	SILVER	MINES	LTD				SOUTH OF S.T. - ST GEOCODE
S000	00	457	MT	148.1	090.0	-45.0				6029.20 7648.38 1258.98
S001	457	1198		148.1	090.0	-44.0				
S002	1198	1481		148.1	090.0	-46.0				
/SCL			MT.2	MT.1						
LSCL			MT.2							
/NAM										MSCLQZPYCPTTASPR
LNAM										CBGY MGHESLGLMO
/	00	280		OVBN						P
R				: TRICONED AND CASED - NO CORE						
/	280	302	11	2C25MS	<<					P <*>
L			00	5T						
R				: HEAVILY BROKEN CORE : NO FE OXIDES : CLAY GOUGE? ZONES						
R				: NO CL ON MICROVEINS						
/	302	332	21	2C35MS	<<					P <*>
L			00	5T						
R				: HEAVILY BROKEN UP CORE W/O CLAY ZONES : TO 2C55 LOC.						
/	332	360	20	2C55MS	<<BR					P <*> <.
L			02	5T						
R				: MOD.-STRONGLY BROKEN UP CORE W/O GOUGE : TO 2C45 LOC.						
R				: NOTE TR. GREY SDE. (TT?)						
/	360	390	22	2C45MS	<<					P <*> <.
L			00	5T						
R				: MOD. BROKEN UP CORE W/O GOUGE : TR GREY SDE (TT?)						
/	390	418	21	2C45MS	<<					P <*>
L			00	5T						
R				: MOD. BROKEN UP CORE W/O GOUGE						
/	418	445	06	2C25MS	<<					P <*>
L			00	5T						
R				: HEAVILY BROKEN AND LOST CORE W/O GOUGE : 1 QZ+PY VEIN > 50 MM						
R				- NO ATTITUDE POSSIBLE						
/	445	466	10	2C45MS	<<					P <*> <.
L			00	5T						
R				: MOD. BROKEN UP CORE W/O GOUGE : LOST CORE						
/	466	485	11	2C45MS	<<BR					P <*> <.
L			00	5T						
R				: MOD. BROKEN CORE W/O GOUGE : LOST CORE : TO 2C55 LOC. : TR						
R				GREY SDE? (TT?)						
/	485	506	05	2C45MS	<<BR					P <*> <.
L			00	5T						
R				: MOD. BROKEN UP CORE W/O GOUGE : LOST CORE : TO 2C55 LOC. : TR						
R				GREY SDE? AS ABOVE						
/	506	530	17	2C45MS	<<BR					P <*> <.
L			02	5T						
R				: MOD. BROKEN UP CORE W/O CLAY GOUGE : LOST CORE : TO 2C55 LOC.						
R				: TR GREY SDE? (TT?)						
/	530	560	25	2C45MS	<<					P <*> <.
L			04	5T						
R				: MOD. BROKEN UP CORE - W/O GOUGE : TO 2C55 LOC. : TR TT?						
/	560	590	29	2C45MS	<<					P <*> <.
L			04	5T						
R				: LESS BROKEN UP THAN ABOVE INTS. : TO 2C85 LOC. : TR TT?						
/	590	620	29	2C35MS	<<					P <*> <.
L			02	5T						

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R      : TR TT?
/      620 650 24 2C35MS << P <*> <.
L      04 5T
R      : TR TT?
/      642 642 X D F/
R      : CLAY GOUGE (FAULT?) - NO ATTITUDE POSSIBLE
/      650 680 18 2C35MS << P <*> <.
L      02 5T
R      : HEAVILY BROKEN UP CORE : LOST CORE 66.2-68.0 M : TR TT?
/      680 701 17 2C45MS << P <*> <.
L      00 5T
R      : HEAVILY BROKEN CORE W/O GOUGE : LOST CORE : TR. TT?
/      701 735 17 2C45MS << P <*>
L      02 5T
R      : HEAVILY BROKEN UP CORE W/ MINOR CLAY GOUGE : LOST CORE : TO
R      2C55 LOC.
/      735 760 24 2C45MS << P >>=< <.
L      14 5T
R      : TR TT?
/      760 790 28 2C35MS << P <>=< <.
L      09 5T
R      : HEAVILY BROKEN UP LOCALLY : TR TT?
/      790 823 24 2C45MS <<BR P <>=< <.
L      02 5T
R      : HEAVILY BROKEN UP LOCALLY W/ SOME GOUGE : TO 2C55 LOC.: TR
R      TT?
/      823 892 61 8A01CL P* P
L      45 4G D.
R      : CNTS OBSCURRED IN BROKEN CORE : 5% ALTERED, UNALIGNED FLAG
R      PHENOS TO 10*2 MM : POST-MIN DYKE
/      892 917 20 2C45MS <<BR P <*> <.
L      00 5T
R      : TR TT? : 8A 91.1-91.4 M W/ MG
/      917 950 32 8A02CL A* P CU 052 A)
L      28 4G CL 085A)
R      : 5% AMYGDS. W/ CB+QZ INFILLING
/      950 972 16 2C45MS << P <*> <.
L      05 5T
R      : TR TT? : HEAVILY BROKEN UP CORE EXCEPT FOR DYKE 95.4-95.9 M
/      972 997 12 2C25MS << P <*> <.
L      00 5T
R      : V. MINOR 2D INTERLEVED : TR. TT? : HEAVILY BROKEN UP CORE
/      997 1027 25 2C25MS << P <<<*> <.
L      00 5T
R      : MOD.-STRONGLY BROKEN UP CORE : TR TT?
/      1027 1061 26 2C15MS << P <<<*> <.
L      00 5T
R      : TR TT?
/      1061 1090 27 2C25MS << P <*> <.
L      02 5T
R      : HEAVILY BROKEN UP CORE : TR. TT?
/      1090 1120 27 2C25MS << P <*> <.
L      00 5T
R      : HEAVILY BROKEN UP CORE LOCALLY : TR. TT?
/      1120 1150 27 2C25MS << P <*> <.

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L           03      5T      <.
R           : HEAVILY BROKEN UP CORE TO 114.0 M : TR. TT?
/    1123  1123      X      D4V/  025  V5V5
/    1150  1180  28  2C13CLMS  <<      P      <.<<<
L           07      TG      <<      <.
R           : TO 2C15 LOC.
/    1180  1210  25  2C15MS  <<      P      <.<<<
L           02      5T      <.
R           : TO 2C13 TOWARDS EOI
/    1210  1231  20  2C13CLMS  <<      P      <.<<<
L           00      TG
R           : MOD. BROKEN UP CORE : TO 2C15 LOC.
/    1231  1243  11  8A02CL  A*      P FB  050  A(
L           10      6G      CL  080A(
R           : POST-MIN DYKE : UPPER CNT. IRREG.-NO ATTITUDE
/    1243  1254  11  2C23CL  <<      P      <<<<<
L           10      5G      <.
R           : TO 2C25 @ EOI
/    1254  1274  12  2C25MS  <<      P      <.<<<
L           00      5T
/    1274  1302  25  2C25MS  <<      P      <<< <.
L           02      5T      <<
R           : TR. TT?
/    1302  1332  29  1D200Z  <<      P      <<< <.
L           13      AW      <<
R           : TR. TT? : MINOR 2C INTERLEVED AT SOI & EOI
/    1332  1360  27  2D25MSCL  <<      P <<  045  <<<<<+
L           22      5T
R           : TO 2D23 & 2C LOC.
/    1360  1390  29  2C23CLMS  <<      P      <<<<<+
L           14      TG
R           : TO 2C25 & 2D LOC.
/    1390  1420  30  2C24CLMS  <<      P      <<<<<
L           12      TG      <.
/    1420  1450  29  2C13CLMS  <<      P      <<<<<
L           00      TG
R           : TO 2C12 & 2C15 LOC.
/    1450  1481  28  2C24CLMS  <<      P      <)<<<
L           05      TG
R           : MINOR 2D INTERLEVED
R           :END OF HOLE @ 148.1 M

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A001
ALAB      EQUITY MINESITE LABORATORY
ATYP      ASSAY
AMTH      WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM      RCOVSAMPLE  RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
A001  280  302      5406      0.005  0.5 0.200 0.005 0.005 2.660 0.005
A001  302  332      5407      0.005  0.5 0.010 0.010 0.005 2.590 0.005
A001  332  360      5408      0.010  0.5 0.100 0.010 0.005 3.990 0.005
A001  360  390      5409      0.005  2.0 0.030 0.010 0.005 6.140 0.010
A001  390  418      5410      0.005  0.1 0.005 0.005 0.005 5.500 0.010
A001  418  445      5411      0.005  0.1 0.010 0.005 0.005 4.600 0.010
A001  445  466      5412      0.005  0.1 0.010 0.005 0.005 4.420 0.010
A001  466  506      5413      0.001  0.1 0.020 0.005 0.005 5.640 0.010
A001  506  530      5415      0.001  0.1 0.020 0.005 0.005 3.330 0.005

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A001	530	560	5416	0.005	0.1	0.020	0.005	0.005	3.830	0.060
A001	560	590	5417	0.005	0.1	0.010	0.005	0.005	10.040	0.005
A001	590	620	5418	0.005	0.1	0.020	0.005	0.005	5.580	0.005
A001	620	650	5419	0.001	0.1	0.030	0.005	0.005	2.840	0.005
A001	650	680	5420	0.001	0.1	0.090	0.005	0.005	3.690	0.005
A001	680	701	5421	0.001	0.1	0.040	0.005	0.005	1.770	0.005
A001	701	735	5422	0.005	2.0	0.030	0.010	0.005	5.140	0.005
A001	735	760	5423	0.005	1.0	0.040	0.010	0.005	8.560	0.005
A001	760	790	5424	0.005	0.1	0.030	0.005	0.005	7.980	0.005
A001	790	823	5425	0.005	0.1	0.050	0.005	0.005	2.930	0.005
A001	892	917	5426	0.005	1.0	0.040	0.010	0.005	5.070	0.005
A001	950	972	5427	0.005	0.1	0.020	0.010	0.005	2.280	0.005
A001	972	997	5428	0.005	0.1	0.020	0.010	0.005	4.100	0.005
A001	997	1027	5429	0.005	1.0	0.020	0.005	0.005	4.240	0.005
A001	1027	1061	5430	0.005	1.0	0.010	0.005	0.005	5.420	0.005
A001	1061	1090	5431	0.005	0.1	0.030	0.005	0.005	5.420	0.005
A001	1090	1120	5432	0.005	1.0	0.050	0.010	0.001	5.080	0.005
A001	1120	1150	5433	0.010	0.5	0.060	0.010	0.001	6.430	0.005
A001	1150	1180	5434	0.030	0.5	0.060	0.005	0.005	4.170	0.005
A001	1180	1210	5435	0.005	3.0	0.080	0.005	0.005	4.240	0.005
A001	1210	1231	5436	0.005	1.0	0.060	0.010	0.010	4.090	0.005
A001	1243	1274	5437	0.040	4.0	0.090	0.010	0.005	5.680	0.020
A001	1274	1302	5438	0.005	18.0	0.120	0.005	0.001	3.280	0.010
A001	1302	1332	5439	0.005	3.0	0.100	0.010	0.005	5.890	0.005
A001	1332	1360	5440	0.005	2.0	0.050	0.005	0.005	4.100	0.005
A001	1360	1390	5441	0.005	1.0	0.050	0.005	0.005	4.060	0.005
A001	1390	1420	5442	0.005	2.0	0.070	0.005	0.005	3.540	0.005
A001	1420	1450	5443	0.005	5.0	0.050	0.010	0.005	5.320	0.005
A001	1450	1481	5444	0.010	1.0	0.060	0.005	0.005	5.220	0.005

R

END OF ASSAYS - END OF LOG

IDEN6B0201		X86CH241	NO	02APR86DJH	G&D	MAR86S38	0.0	
IPRJ		EQUITY	SILVER	MINES LTD		NORTH ZONE - MZ	GEOCODE	
S000	00	457	MT.	274.8	090.0	-45.0	8918.30	8818.97 1301.84
S001	457	1396		274.8	090.0	-43.0		
S002	1396	2313		274.8	090.0	-44.0		
S003	2313	2748		274.8	090.0	-43.0		
/SCL		MT.2	MT.1					
LSCL			MT.2					
/NAM								
LNAM								QZSZTOPYCPTTASPR
								DMCBCLMGHESLGLMO
/	00	189		OVBN				P
R			:	TRICONED AND CASED - NO CORE				
/	189	195	05	2C03	<<			P <*
L			00	3A				
R			:	20% LIGHT GREY ASH FRAGS. IN A DARK GREY APH. (DUST/GLASS?)				
R			:	MATRIX				
/	195	219	23	8A10CLCB	P*<<		P CU 055	<.
L			06	7A				
R			:	15% UNALIGNED PLAG PHENOS TO 3*3 MM IN A V.F.G. TO APH				
R			:	MATRIX : RARE MICROVEINS : WEAK PROPYLITIC ALT'N				
R			:	LOWER CNT. OBSCURED IN BROKEN CORE				
/	219	262	25	2C03	<<			P <*
L			02	3A				
R			:	AS ABOVE 18.9-19.5 M : TO 2D LOC. : HEAVILY BROKEN UP CORE				
R			:	W/ NUMEROUS ZONES OF CLAY GOUGE?				
/	262	277	04	8A10CL				P
L			00	8G				
R			:	TOTALLY ALTERED - NO RELICT TEXT. : 8A? : NO CNTS OBSERVED				
R			:	DUE TO BROKEN CORE : CY @ LOWER CNT.				
/	277	371	80	2C03	<<			P <*
L			00	3A				
R			:	NUMEROUS ZONES HEAVILY BROKEN CORE AND CLAY GOUGE? : AS ABOVE				
R			:	21.9-26.2 M : OCC. COARSER, MED. GREY ASH TUFF INTERLEVED				
/	371	382	11	2D13CLMS	<<			P <<
L			03	7G				
R			:	50% ACID TO INTER. ASH FRAGS (3-4 MM AV.) IN A FINER ASH				
R			:	MATRIX				
/	382	411	26	2C00				P
L			00	3A				
R			:	10% INTERLEVED 2D : NO SDES.				
/	411	420	08	2D13CL	<<			P <<
L			04	AG				
R			:	OCC. LAPILLI : RARE PATCHES PY : AS ABOVE 37.1-38.2				
/	420	456	23	2C03	<<			P < <<
L			00	3A				
R			:	TO 2D LOC. W/ OCC. LAPILLI FRAGS.				
/	456	479	19	2D03	<<			P < <
L			00	5A				
R			:	NO CL UNLIKE ABOVE 2D INTS.				
/	479	494	14	2E03MS	<<			P < <
L			00	TA				
R			:	30% TAN COLORED LAPILLI FRAGS IN A DUST/ASH MATRIX : PY IN				
R			:	OCC. FRAGS				
/	494	510	14	2D03	<<			P <.
L			02	4A				

L 23 4G <<
 R : 30% INTERLEVED LIGHT GREY 2D : OCC. MASSIVE SDE CLAST
 / 1100 1130 27 2H11CL P D(
 L 24 4G
 R : NO MICROVEIN TEXT.
 / 1130 1160 29 2H13CL << P <<
 L 15 AG <)
 R : TO 2C & 2D LOC. : TYPICAL LIGHT GRAY SANDY MATRIX
 / 1160 1190 29 2H13CL << P J) <<
 L 18 4G <.<)
 R : TO 2C & 2D LOC.
 / 1190 1220 29 2H13CL << P <.< <<
 L 14 4G <.<)
 R : TO 2C AND 2D AT EDI
 / 1220 1250 29 2D13CL << P <.< <*<
 L 25 GA <.<+
 R : MINOR 2E INTERLEVED : MOD. RETICULATED FRACTURING W/ CL +- PY
 / 1250 1280 29 2D13CL << P <.< <*<
 L 23 GA <.<+
 R : MINOR 2E
 / 1280 1310 29 2D13CL << P <.< <+
 L 07 GA <.<+ <.<
 / 1310 1340 29 2D13CL << P <.< <+
 L 16 GA <+
 R : TO 2E LOC.
 / 1340 1370 27 2J11CL << P <.< <+
 L 12 GA <+
 R : BD IRREGULAR (NO ATTITUDES)
 / 1370 1400 28 2J11CL << P <.< <+
 L 13 GA <+
 R : AS ABOVE W/ ZONES OF CLAY GOUGE?
 / 1400 1430 29 2J13CL << P <.< <+
 L 21 GA <+
 R : AS ABOVE INT. W/ MORE PY : MINOR 2E INTERLEVED : CLAY ZONES
 / 1430 1460 29 2D14CL << P <.< <+
 L 27 GA <.< <.<+
 R : TO 2C & 2E LOC. : NOTE PRESENCE OF SL & GL
 / 1460 1490 30 2E11CL P D(
 L 29 TG
 R : 75% LAPILLI W/ ASH MATRIX
 / 1490 1520 28 2D13CLMS << P <.< <.<+
 L 21 GT <+
 R : TO 2C LOC. : 2E @ SOI
 / 1520 1550 29 2D13CL << P <.< <.<+
 L 05 6G <.<+
 R : FINE GRAINED (DUST?)
 / 1550 1574 24 2D13CL << P <.< <+
 L 18 6G <+
 R : AS ABOVE W/ INCREASING PY
 / 1574 1651 75 8C10MSCL P* P CU 052
 L 66 9G CL 055
 R : POST-MIN DYKE : 5% FLAG PHENOS TO 2*1 MM : FB @ CNTS
 / 1651 1680 28 2D13CL << P <+ <+
 L 26 6G <+V.<+
 R : 2C ? : LIGHTER GREEN NEAR DYKE CNT.

/	1680	1710	28	2D13CL	<<	P	<<	<<
L			24	6G			<.<<	
R			: 8A 170.4-170.7 M.					
/	1710	1740	29	2D13CLMS	<<	P		<<
L			25	6T				<+
R			: 8A 171.1-171.7 : TO 2C LOC.					
/	1740	1770	28	2D13CL	<<	P		<<
L			23	5G				<+
R			: TO 2C LOC.					
/	1770	1852	81	8A10CL	A*	P CU	053A(
L			73	AG				A(A.
R			: 5% QZ+CB FILLED AMYGDS.					
/	1852	1862	10	8A10CL	<<	P CL	067<=	
L			06	AG			<=	
R			: AS ABOVE W/ MOD. RETIC. MICROVEINING W/ QZ+CB INFILLING					
/	1862	1880	17	2C13CLMS	<<	P	<<	<<
L			14	6T			<<<+	
/	1880	1890	10	8B10CL	P*	P CU	075	
L			10	4G		CL	080	D.
R			: 10% SUBALIGNED FLAG PHENOS TO 10*5 MM					
/	1890	1920	28	2C13CLMS	<<	P	<<	<<
L			23	6T				<+
R			: TO 2C83 LOC.					
/	1920	1950	28	2C13CL	<<	P	<<	<<
L			24	6G				<+
/	1950	1980	29	2C13CL	<<	P	<<	<<
L			27	6G				<+
R			: MAROON COLOR NEAR EOI : TO 2D LOC. : TR. GY ON << : STRONG					
R			RETIC. MICROVEINING - ABOVE TWO INTS ALSO					
/	1980	2010	29	2C13CL	<<	P		<<
L			22	6G				<+
R			: MOD.-STRONG RETIC. MICROVEINS : TR GY ON <<					
/	2010	2021	10	2C13CL	<<	P		<<
L			07	6G				<+
/	2021	2044	23	8A10CL	P*A*	P CU	080	D(
L			12	4G		CL	075	
R			: TR. EP					
/	2044	2070	25	2E13CLMS	<<	P	<<	<)
L			04	6T				<+ <.
R			: TO 2D LOC. : REACTION RIMS ON LAPILL : 0.3 M 8A					
/	2070	2100	29	2C13CL	<<	P		<+
L			07	6G				<+ <.
R			: STRONG RETIC. MICROVEINING W/CL +-PY +-HE					
/	2100	2130	30	2D13CL	<<	P		<)
L			07	AG				<)<<
R			: DARK GREY GREEN COLOR : 0.4M 8A					
/	2130	2160	29	2C13CLMS	<<	P		<)
L			21	6G				<)<<
R			: TO TAN/GREEN COLOR LOC. : TO DARK GREY/GREEN COLOR LOC.					
/	2160	2195	34	2C13CL	<<	P		<)
L			16	6G				<)<<
R			: STRONGER MS ALT'N AND MORE PY 0.3 M NEXT TO DYKE					
/	2195	2220	23	8A10CL	A*<<	P CU	045	
L			19	5G		CL	060 <<	
/	2220	2231	10	8A11MSCL	<<	P		D(

L 04 5A
 R : TR GY ON MICROVEINS : CNTS OBSCURED IN BROKEN CORE
 R : PRE-MIN DYKE
 / 2231 2250 17 2C13CL << P <<
 L 06 6G <<
 R : TR GY ON MICROVEINS : TO 2D LOC.
 / 2250 2280 29 2C13CL << P <<
 L 17 6G <+
 R : LOCALLY DARK GREY (UNALTERED?)
 / 2280 2310 30 2C13CLMS << P <<
 L 26 TG <+
 R : TO 2C83 LOC.
 / 2310 2340 29 2D12CLMS << P Q+
 L 25 TG <+Q.
 R : TO 2C83 LOC. : MG DISS. IN PY PATCHES
 / 2340 2370 29 2D12CLMS << P Q+
 L 25 TG <+Q.
 R : AS ABOVE W/ MINOR 2E LOC. : STRONG RETIC. MICROVEINING
 / 2370 2400 29 2D12CLMS << P Q+
 L 22 TG <+Q.Q(
 R : AS ABOVE W/ RED HE ASS. W/ PY+CL+MG : TO 2C83 & 2E LOC.
 / 2400 2430 29 2D13CLMS << P Q+
 L 24 TG <+Q.<<
 R : AS ABOVE W/ 2C8 & 2E LOC.
 / 2430 2443 13 2E04MS << P << J+
 L 08 5T <<
 R : MS ATL'N OF FRAGS - NO CL
 / 2443 2459 14 8A10CLMS <<P* P CL 070<<
 L 12 AG <<
 R : PRE - MIN. DYKE? : QZ+CB MICROVEINS X-CUT DYKE CNT. : UPPER
 R CNT. V. IRREGULAR - NO ATTITUDE
 / 2459 2490 30 2E03MS << P << <<
 L 16 MT << D(
 R : FRAGS. ARE GENERALLY TAN DUST TUFF W/ OCC. COOLING RIMS :
 R : NOTE MINOR CL ON MICROVEINS : NO POST - LITH ALT'N
 / 2490 2507 17 2E03MS << P <<
 L 03 MT << D(
 R : AS ABOVE
 / 2507 2520 12 2D13CL << P <)
 L 00 MG <+ D.
 / 2520 2550 29 2D13CL << P <)
 L 06 MG <+ D.
 R : TO 2C LOC. : MAROON COLORED PATCHES (HE?) : 8A 245.3-254.7 M
 R (PRE-MIN.?)
 / 2550 2580 27 2D13CL << P <)
 L 04 MG <+ D.
 / 2580 2610 27 2D13CL << P <)
 L 05 MG <+ D.
 R : DISTINCTIVE MAROON (HE?) GREEN COLOR: MAROON ZONES MAY BE
 R UNALTERED
 / 2610 2640 29 2D13CLMS << P <=
 L 05 TG <+ <<
 R : TO 2C83 LOC.
 / 2640 2661 18 2C83MSCL << P <=
 L 02 GT <. <<

R : TO 2D LOC. : TR CL ON MICROVEINS
 / 2661 2675 14 2C13CLMS << P <=
 L 07 TG <<
 R : 20% ASH FRAGS IN A DUST MATRIX : BA 266.1-266.4 & 267.1-267.5
 R M W/ CNTS @ 055 TO C.A. (PRE-MIN DYKE)
 / 2675 2700 24 2C13CLMS << P <)
 L 19 MG << <.
 R : TO 2C83 LOC. : MAROON GREEN COLOR : MS ALT'N ENVS. ON MICRO-
 R VEINS : 20% ASH FRAGS
 / 2700 2730 28 2C13CL << P <<
 L 10 MG << D.
 R : AS ABOVE W/ MORE MAROON COLORAT'N : TO 2D & 2C8 LOC.
 / 2730 2738 07 2C13CLMS << P <)
 L 00 MG << <.
 R : POST-MIN BA DYKE 273.8-274.8 M W/ UPPER CNT. @ 043 TO C.A.
 / 2738 2748 10 BA10CL P* P
 L 08 4G
 R : POST-MIN. DYKE
 R : EDH AT 274.8 M

A001
 ALAB
 ATYP
 AMTH
 AUMM

EQUITY MINESITE LABORATORY

ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

A001	RCQVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN	
A001	189	195	5445	0.005	1.0	0.120	0.010	0.060	4.380	0.005
A001	219	256	5446	0.005	0.5	0.130	0.010	0.020	8.060	0.005
A001	256	293	5447	0.020	3.0	0.040	0.010	0.130	6.180	0.230
A001	293	323	5448	0.050	9.0	0.320	0.020	0.430	5.040	0.010
A001	323	354	5449	0.005	1.0	0.100	0.010	0.080	5.690	0.005
A001	354	384	5450	0.005	1.0	0.080	0.010	0.005	9.260	0.005
A001	384	412	5451	0.005	1.0	0.090	0.005	0.005	4.910	0.005
A001	412	445	5452	0.005	2.0	0.060	0.010	0.060	6.820	0.005
A001	445	476	5453	0.030	5.0	0.190	0.010	0.780	7.370	0.005
A001	476	506	5454	0.010	2.0	0.090	0.010	0.050	6.110	0.070
A001	506	530	5455	0.005	1.0	0.005	0.010	0.240	5.350	0.030
A001	530	560	5456	0.005	1.0	0.030	0.010	0.030	5.180	0.030
A001	560	585	5457	0.005	2.0	0.050	0.010	0.005	7.280	0.030
A001	585	610	5458	0.005	2.0	0.040	0.010	0.005	8.110	0.010
A001	610	640	5459	0.010	3.0	0.030	0.010	0.005	7.050	0.320
A001	640	670	5460	0.005	2.0	0.040	0.010	0.010	8.560	0.020
A001	670	700	5461	0.005	2.0	0.020	0.010	0.005	6.960	0.040
A001	700	730	5462	0.001	0.5	0.010	0.005	0.030	9.100	0.020
A001	730	762	5463	0.001	6.0	0.010	0.005	0.070	9.590	0.510
A001	810	834	5464	0.001	3.0	0.070	0.001	0.030	5.550	0.700
A001	834	860	5465	0.001	3.0	0.040	0.001	0.001	7.680	0.080
A001	860	890	5466	0.001	3.0	0.005	0.001	0.001	7.880	0.100
A001	890	920	5467	0.001	3.0	0.005	0.001	0.001	7.690	0.005
A001	920	950	5468	0.001	3.0	0.030	0.001	0.001	8.470	0.120
A001	950	980	5469	0.001	3.0	0.020	0.001	0.001	6.920	0.080
A001	980	1010	5470	0.001	3.0	0.005	0.001	0.001	6.200	0.050
A001	1010	1040	5471	0.001	3.0	0.040	0.001	0.001	5.480	0.080
A001	1040	1070	5472	0.001	3.0	0.030	0.001	0.001	5.330	0.030
A001	1070	1100	5473	0.001	0.5	0.060	0.001	0.001	6.690	0.030
A001	1100	1130	5474	0.001	0.5	0.005	0.001	0.001	7.490	0.020
A001	1130	1160	5475	0.001	0.5	0.005	0.001	0.001	6.560	0.005

A001	1160	1190	5476	0.001	0.5	0.050	0.001	0.001	7.380	0.020
A001	1190	1220	5477	0.001	0.5	0.040	0.001	0.020	7.810	0.005
A001	1220	1250	5478	0.001	0.5	0.040	0.001	0.030	6.130	0.005
A001	1250	1280	5479	0.001	0.5	0.100	0.001	0.005	5.610	0.005
A001	1280	1310	5480	0.001	0.5	0.130	0.001	0.005	5.410	0.005
A001	1310	1340	5481	0.001	0.5	0.240	0.001	0.001	6.170	0.005
A001	1340	1370	5482	0.001	0.5	0.090	0.001	0.001	4.360	0.005
A001	1370	1400	5483	0.001	0.5	0.110	0.001	0.001	5.130	0.005
A001	1400	1430	5484	0.001	2.0	0.100	0.001	0.030	7.900	0.090
A001	1430	1460	5485	0.005	2.0	0.190	0.001	0.030	8.150	0.260
A001	1460	1490	5486	0.001	0.1	0.030	0.001	0.005	6.190	0.040
A001	1490	1520	5487	0.001	0.1	0.050	0.001	0.020	6.840	0.005
A001	1520	1550	5488	0.001	0.1	0.040	0.001	0.001	6.780	0.001
A001	1550	1574	5489	0.001	0.1	0.020	0.001	0.001	5.790	0.005
A001	1651	1680	5490	0.010	0.5	0.100	0.020	0.005	6.610	0.030
A001	1680	1710	5491	0.005	0.1	0.100	0.010	0.005	5.630	0.020
A001	1710	1740	5492	0.005	0.1	0.070	0.020	0.005	6.500	0.020
A001	1740	1770	5493	0.005	0.1	0.070	0.020	0.005	5.040	0.020
A001	1852	1880	5494	0.005	0.1	0.130	0.020	0.005	3.380	0.010
A001	1890	1920	5495	0.005	0.1	0.030	0.020	0.005	4.230	0.005
A001	1920	1950	5496	0.005	0.1	0.070	0.020	0.005	4.000	0.005
A001	1950	1980	5497	0.005	0.1	0.120	0.010	0.005	4.210	0.010
A001	1980	2010	5498	0.005	0.1	0.060	0.010	0.005	4.800	0.005
A001	2010	2021	5499	0.005	0.1	0.050	0.010	0.005	3.600	0.005
A001	2044	2070	5500	0.005	0.1	0.070	0.010	0.005	4.220	0.010
A001	2070	2100	5501	0.005	0.1	0.100	0.010	0.005	4.890	0.005
A001	2100	2130	5502	0.005	0.1	0.120	0.010	0.005	3.570	0.005
A001	2130	2160	5503	0.005	0.5	0.060	0.010	0.005	3.460	0.005
A001	2160	2195	5504	0.005	0.5	0.080	0.010	0.005	3.090	0.005
A001	2220	2250	5505	0.005	0.5	0.200	0.010	0.005	4.010	0.020
A001	2250	2280	5506	0.005	0.5	0.080	0.010	0.005	3.800	0.005
A001	2280	2310	5507	0.005	0.5	0.040	0.010	0.005	3.150	0.005
A001	2310	2340	5508	0.005	0.5	0.040	0.010	0.005	6.490	0.005
A001	2340	2370	5509	0.005	0.5	0.050	0.010	0.005	5.260	0.005
A001	2370	2400	5510	0.005	0.5	0.030	0.010	0.005	4.590	0.005
A001	2400	2430	5511	0.005	0.5	0.060	0.005	0.005	3.630	0.010
A001	2430	2459	5512	0.005	0.5	0.050	0.020	0.005	3.430	0.010
A001	2459	2490	5513	0.005	0.5	0.040	0.010	0.005	3.910	0.010
A001	2490	2520	5514	0.005	0.5	0.110	0.010	0.005	3.900	0.010
A001	2520	2550	5515	0.005	0.5	0.050	0.005	0.005	3.400	0.010
A001	2550	2580	5516	0.005	0.5	0.060	0.005	0.005	3.100	0.005
A001	2580	2610	5517	0.005	0.5	0.070	0.005	0.005	3.420	0.005
A001	2610	2640	5518	0.005	0.5	0.060	0.005	0.005	4.190	0.005
A001	2640	2670	5519	0.005	0.5	0.040	0.005	0.005	3.540	0.005
A001	2670	2700	5520	0.005	0.5	0.070	0.005	0.005	3.970	0.005
A001	2700	2730	5521	0.005	0.5	0.120	0.010	0.005	3.710	0.005
A001	2730	2749	5522	0.005	0.5	0.080	0.005	0.005	4.640	0.010

R

END OF ASSAYS - END OF LOG


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/ 539 554 14 2C83MS << P <<
L 00 5T <. <.<<
R : 10% ASH FRAGS. IN DUST MATRIX
/ 554 580 26 2G13CL << P <<
L 21 4G <<
R : AS ABOVE 49.0-52.0 M : TO 2C LOC.
/ 580 616 34 2D13CLMS << P <
L 21 TG <+ <.
R : LOCAL SERICITE ALT'N : MAROON COLOR LAST .5 M OF INT.
/ 616 633 16 2G10CL BD P BD 062 <.
L 14 4G <.
R : INDISTINCT BEDDING
/ 633 669 34 2D13CL << P <
L 29 5G <.<+
R : 10% INTERLEVED 2G W/ GRAD. CNTS. : V. MINOR MAROON COLORAT'N
/ 669 685 14 2G13CL << P < <+
L 13 5G <)<
R : MINOR 2D INTERLEVED
/ 685 730 43 2D13CLMS << P < <+
L 40 6G <)<+
R : MINOR MAROON COLORAT'N : MS ON <<
/ 730 760 29 2D13CL << P <(< <
L 26 4G <(<<+
R : 10% INTERLEVED 2G -NO BEDDING : 2C?
/ 760 774 14 2D13CL << P <(< <
L 07 5G <(<<+ <.
R : AS ABOVE W/ 2G
/ 774 793 19 1D03QZ <<BD P BD 063<(< <(<
L 08 5A <(<<
R : MINOR 2D INTERLEVED
/ 793 871 75 8C80MS P* P CU 033
L 47 W CL 065
/ 871 900 28 2D13CLMS <<BD P BD 070<* <
L 20 TG <(<<*
R : TO 2D83 @ SOI : 30% INTERBEDDED 1D : LOCAL MAROON COLORAT'N
R : TO 2C LOC.
/ 900 930 30 2D13CL << P <. <
L 23 MG <.<*
/ 930 960 30 2D10CL << P <.
L 25 MG <.<*
R : NO PY : 10% INTERLEVED 1D : PATCHY MAROON GREEN COLORAT'N
/ 960 990 29 2D13CL << P <. <(<
L 17 MG <.<*
R : 5% INTERLEVED 1D
/ 990 1020 29 2D13CL << P <
L 22 MG <*
R : 5% INTERLEVED 1D
/ 1020 1050 29 1C00QZ P *(<
L 25 5A *(<
R : 10% INTERLEVED 1D : 10% GREY SANDY MATRIX : NOTE OCC. CLASTS
R W/ PY ( I.E. - SOME SOURCE RXS. WERE MINERALIZED W/ PY)
R : 90% WHITE TO LIGHT GREY CHERTY CLASTS AND 10% LIGHT GREEN
R VOLC. CLASTS : NO << TEXT.
/ 1050 1083 32 1C00QZ << P <.
L 27 5A *

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R : 10% SANDY MATRIX : V. WEAK << TEXT.
/ 1083 1094 10 8A11CL P* << P <.
L 07 AG CL 080
R : UPPER CNT. OBSCURED IN GOUGE : PRE-MIN. DYKE?
/ 1094 1120 25 1C00QZ P *(<
L 19 SA
R : 10-15% SANDY MATRIX : 15% INTERLEVED 1D W/ 10% WHITE PEBBLES
/ 1120 1141 19 1C03QZ << P < <<
L 06 SA <.
R : V. WEAK << TEXT.
/ 1141 1180 37 2D13CL <<BD P BD 075 <<
L 31 MG <*<
R : 20% INTERBEDDED 1D (MAINLY IN TOP 1.5 M OF INT)
/ 1180 1210 30 2D13CL << P <(<
L 26 MG << <<(<
R : 5% INTERLEVED 1D
/ 1210 1240 30 2D13CL << P <(<
L 21 MG <*< <.
R : NO 1D : NOTE - FOR << READ MICROVEINED OR CRACKLED
/ 1240 1250 09 2D13CL << P <+
L 06 GM <*< <.
R : MINOR 1D INTERLEVED
/ 1250 1268 17 8A10CL P*A* P CU 080 A.
L 12 5G CL 064 A(A(
R : POST-MIN. DYKE
/ 1268 1300 32 2D13CL << P << <*<
L 31 6G <+ <<(<
R : LOCAL DARK GREY COLORAT'N
/ 1300 1329 29 2D13CLMS << P << <*<
L 25 TG <+
R : TO 2C83 LOC. W/ TAN COLOR : TO 1D TOWARDS EQI
/ 1329 1338 07 8A10CL A* << P
L 00 5G <<(<
R : CNTS. OBSCURED IN BROKEN CORE AND GOUGE : POST-MIN. DYKE
/ 1338 1360 22 2D13CL << P <*<
L 17 5G <<<+
R : 30% ASH FRAGS IN DUST MATRIX
/ 1360 1390 29 2D13CLMS << P <*<
L 24 TG <<(<(<
R : 10% INTERLEVED 2E : TO 2C LOC. W/ MS ALT'N AND OCC. LAPILLI
OF MASS. PY
/ 1390 1411 20 8A11CL P* << P D)
L 16 6G
R : PRE-MIN. DYKE : NO CNT. ATTITUDES POSSIBLE DUE TO BROKEN UP
CORE : V. WEAK P* TEXT. : DYKE OR POSSIBLE TUFF?
/ 1411 1424 13 8B11CL P* << P FB 062<) D)
L 09 AG <(<
R : NOTE FB IS TRACHYTIC ALIGNMENT : POST-MIN. DYKE
/ 1424 1480 53 8A14CL A* << P Q+
L 27 5G CL 052 <(<*<
R : PY+CL PATCHES : PRE-MIN. DYKE : 5% FLATTENED A* W/ CB+CL+-PY
/ 1480 1510 29 2C13CL << P <<(<
L 15 6G <(<
R : TO 2D LOC. : MINOR 1D INTERLEVED : WEAK ZONES OF MS ALT'N
/ 1510 1542 31 2D13CL << P <<(<

L 04 56 <<<
 R : TO 2C LOC. : TO MAROON COLOR AT EDI : 30% ASH FRAGS IN DUST
 R END OF HOLE.

			EQUITY MINESITE LABORATORY								
			ASSAY								
			WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST								
AUMM			RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001	183	210	5523		0.005	1.0	0.080	0.010	0.001	3.620	0.020
A001	210	238	5524		0.010	1.0	0.050	0.010	0.005	4.690	0.020
A001	238	268	5525		0.010	1.0	0.070	0.010	0.005	4.700	0.010
A001	268	293	5526		0.005	1.0	0.050	0.010	0.010	5.330	0.010
A001	293	323	5527		0.005	3.0	0.030	0.005	0.010	4.590	0.010
A001	323	354	5528		0.005	1.0	0.020	0.005	0.020	4.620	0.020
A001	354	380	5529		0.005	1.0	0.040	0.010	0.005	5.330	0.010
A001	380	410	5530		0.005	4.0	0.150	0.010	0.030	5.540	0.350
A001	410	425	5531		0.005	2.0	0.040	0.010	0.040	4.950	0.150
A001	437	460	5532		0.005	4.0	0.090	0.010	0.010	30680	0.050
A001	460	490	5533		0.005	1.0	0.060	0.005	0.005	3.210	0.005
A001	490	520	5534		0.005	1.0	0.050	0.010	0.005	3.420	0.005
A001	520	550	5535		0.005	5.0	0.060	0.020	0.010	4.380	0.230
A001	550	580	5536		0.005	2.0	0.070	0.005	0.005	4.520	0.040
A001	580	610	5537		0.005	1.0	0.040	0.010	0.005	3.850	0.030
A001	610	640	5538		0.005	1.0	0.030	0.010	0.005	4.620	0.010
A001	640	670	5539		0.005	2.0	0.030	0.005	0.010	5.080	0.020
A001	670	700	5540		0.005	1.0	0.030	0.010	0.020	6.100	0.040
A001	700	730	5541		0.005	2.0	0.070	0.010	0.005	4.940	0.010
A001	730	760	5542		0.005	1.0	0.070	0.010	0.010	4.700	0.010
A001	760	793	5543		0.005	1.0	0.060	0.005	0.010	5.080	0.020
A001	871	900	5544		0.005	1.0	0.030	0.010	0.005	4.290	0.020
A001	900	930	5545		0.005	2.0	0.060	0.005	0.005	4.780	0.020
A001	930	960	5546		0.005	1.0	0.070	0.010	0.005	5.520	0.010
A001	960	990	5547		0.005	1.0	0.060	0.010	0.005	5.490	0.005
A001	990	1020	5548		0.005	1.0	0.070	0.010	0.005	4.700	0.005
A001	1020	1050	5549		0.005	0.5	0.100	0.005	0.005	2.370	0.005
A001	1050	1083	5550		0.005	0.5	0.050	0.005	0.005	1.770	0.005
A001	1094	1120	5551		0.005	1.0	0.060	0.005	0.005	2.220	0.005
A001	1120	1150	5552		0.005	1.0	0.060	0.005	0.005	3.050	0.030
A001	1150	1180	5553		0.005	1.0	0.060	0.005	0.005	4.930	0.005
A001	1180	1210	5554		0.005	1.0	0.050	0.005	0.005	4.420	0.005
A001	1210	1240	5555		0.005	1.0	0.040	0.005	0.005	4.080	0.005
A001	1240	1250	5556		0.005	1.0	0.040	0.010	0.005	5.090	0.005
A001	1268	1300	5557		0.005	1.0	0.060	0.005	0.005	5.670	0.005
A001	1300	1329	5558		0.005	1.0	0.060	0.005	0.005	4.090	0.005
A001	1329	1360	5559		0.005	1.0	0.060	0.005	0.030	4.240	0.005
A001	1360	1390	5560		0.005	1.0	0.080	0.005	0.030	4.660	0.005
A001	1390	1411	5561		0.005	1.0	0.100	0.005	0.010	3.490	0.010
A001	1424	1450	5562		0.005	1.0	0.120	0.005	0.005	2.630	0.020
A001	1450	1480	5563		0.005	1.0	0.070	0.005	0.005	2.460	0.010
A001	1480	1510	5564		0.005	0.5	0.030	0.005	0.005	3.940	0.010
A001	1510	1542	5565		0.005	1.0	0.020	0.005	0.010	5.230	0.010

R END OF ASSAYS - END OF LOG


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R      : WEAK MICROVEIN TEXT : TO 2C LOC.
/      770  800  29  2D13CL  <<                               <)
L      25      GM                               <)
R      : WEAK TO MOD. MICROVEIN TEXT : OCC. PATCHES PY
/      800  824  19  2D13CL  <<           P           <<
L      15      GM                               <<
R      : WEAK MICROVEIN TEXT. : TO 2C LOC. : WEAK CL+-MS ENVS. ON <<
/      824  835  07  8A10CL  A*P*           P           <<
L      02      4G
R      : POST-MIN. DYKE : NO CNTS OBSERVED DUE TO BROKEN CORE
/      835  870  33  2D13CL  <<           P           <)
L      12      MG                               <) <<
R      : WEAK TO STRONG MICROVEIN TEXT.
/      870  894  23  2D13CL  <<           P BN   042   <)
L      09      GM                               <) <<
R      : WEAK TO STRONG MICROVEIN TEXT. W/ WEAK ALT'N ENVS. ON <<
R      : TO 2C LOCALLY : COLOR BN COULD BE BEDDING
/      894  921  25  8A10CL  A*P*           P CU   040A(
L      12      4G                               A(
R      : BECOMING LESS ALTERED FROM 90.0 M : TR. QZ+CB MICROVEINS
R      : POST-MIN. DYKE
R      : END OF HOLE AT 92.1 M

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A001

ALAB

ATYP

AMTH

AUMM

EQUITY MINESITE LABORATORY

ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCQVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN	
A001	232	260	5566	0.030	6.0	0.030	0.005	0.005	2.250	0.005
A001	260	290	5567	0.010	2.0	0.050	0.005	0.005	2.160	0.005
A001	290	320	5568	0.005	1.0	0.030	0.005	0.005	1.250	0.005
A001	320	345	5569	0.005	0.5	0.020	0.005	0.005	1.390	0.005
A001	371	400	5570	0.005	1.0	0.020	0.005	0.005	1.260	0.005
A001	400	430	5571	0.005	0.5	0.030	0.005	0.005	1.320	0.005
A001	430	460	5572	0.005	2.0	0.020	0.005	0.005	1.500	0.005
A001	460	480	5573	0.005	1.0	0.030	0.005	0.005	1.260	0.005
A001	480	497	5574	0.005	1.0	0.020	0.005	0.005	1.830	0.005
A001	582	610	5575	0.005	2.0	0.010	0.005	0.005	5.740	0.005
A001	610	640	5576	0.005	1.0	0.010	0.005	0.005	5.020	0.005
A001	640	670	5577	0.005	1.0	0.020	0.005	0.005	3.610	0.005
A001	670	705	5578	0.005	1.0	0.100	0.005	0.005	3.630	0.005
A001	739	770	5579	0.005	2.0	0.020	0.005	0.005	3.570	0.005
A001	770	800	5580	0.005	1.0	0.010	0.005	0.005	3.530	0.005
A001	800	824	5581	0.005	2.0	0.010	0.005	0.005	4.770	0.005
A001	824	850	5582	0.005	2.0	0.010	0.010	0.005	4.980	0.005
A001	850	870	5583	0.005	2.0	0.010	0.005	0.005	3.980	0.005
A001	870	894	5584	0.005	2.0	0.010	0.005	0.005	4.050	0.005

R

END OF ASSAYS - END OF LOG

IDEN6B0201 XB6CH244 NO 09APR86DJH G&D APR86S38 0.0
 IPRJ EQUITY SILVER MINES LTD NORTH ZONE - MZ GEOCODE
 S000 00 532 MT 106.4 090.0 -45.0 9115.31 9106.44 1337.33
 S001 532 1064 106.4 090.0 -44.0
 /SCL MT.2MT.1
 LSCL MT.2
 /NAM QZSZTOPYCPTTASPR
 LNAM DMCBCLMGHESLGLMO
 / 00 152 OVEN P
 L
 R : TRICONED AND CASED - NO CORE
 / 152 234 62 BA1OCL P* P
 L 00 6G
 R : POST-MIN. DYKE : LOWER CNT. NOT EXPOSED DUE TO BROKEN CORE
 R : 5% UNALIGNED EUHEDRAL FLAG PHENOS TO 5*1 MM
 / 234 248 12 2E00 P *(
 L 00 TG
 R : 90% ACID TO INTER. VOLC. FRAGS (PYROCLASTICS) W/ OCC.
 R REACTION RIMS AND 10% SUBROUNDED CHERTY FRAGS : 30% 2D
 / 248 265 15 BA1OCL P* P D.
 L 00 GA
 R : NO CNTS DUE TO LOST AND BROKEN CORE : DARK GREEN GREY COLOR
 R : FAIRLY WEAK ALT'N : POST-MIN DYKE
 / 265 274 09 2E00 P *(
 L 00 TG
 R : AS ABOVE 23.4-24.8 M
 / 274 299 24 BA1OCL A*P* P A(A)
 L 00 6G A(
 R : PRE-MIN. DYKE : NO CNT. ATTITUDES DUE TO BROKEN CORE
 R : 0.2 M 2E 28.2-28.4 M
 / 299 333 31 2E00 P *(
 L 09 TG
 R : TO 2D LOC. 31.6-32.5 M
 / 333 365 28 2CB3MSCL << P (<
 L 02 GW <*)
 R : HEAVILY BROKEN CORE W/CLAY AT 35.6 M : WEAK MICROVEIN TEXT.
 R : TO 2D LOCALLY
 / 365 410 45 2E00 P *)
 L 21 GU <.
 R : ACID AND INTER. TUFF FRAGS IN AN APHANITIC BROWN MATRIX
 R : NO POST-LITH'N ALT'N
 / 410 440 30 2E00 P *)
 L 08 GU <.
 R : AS ABOVE W/ LOCAL REACTION RIMS
 / 440 470 28 2E00 P *(
 L 17 GU <.
 R : AS ABOVE : TO 2D LOC. W/ 5% LAPILLI
 / 470 500 28 2E00 P *(
 L 05 GU
 R : AS ABOVE W/ TR. PY IN MICROVEINS
 / 500 530 22 2E00 P *.
 L 00 GU
 R : HEAVILY BROKEN UP CORE W/ ZONES OF CLAY AND LOST CORE
 / 530 560 28 2E00 P *.
 L 04 GU <.

R : AS ABOVE W/ OCC. BXIA BLOCKS : NO CLAY ZONES
/ 560 588 20 2E00 << P <.
L 00 GU <.<.
R : HEAVILY BROKEN UP CORE W/NUMEROUS CLAY ZONES : V. WEAK
R MICROVEIN TEXT.
/ 588 619 17 2E00 P *.
L 00 GU
R : HEAVILY BROKEN UP AND GROUND CORE W/ NUMEROUS CLAY ZONES
/ 619 637 18 2D00 P *.
L 03 GU
R : AS ABOVE INT. BUT W/D LAPILLI
/ 637 650 13 2E00 << P *.
L 02 GU
R : AS ABOVE 58.8-61.9 M W/V.WEAK MICROVEIN TEXT. W/ TR. PY
/ 650 683 28 2D03 << P <<
L 02 GM <.
R : HEAVILY BROKEN UP CORE : V. WEAK MICROVEIN TEXT. : V. WEAK
R ALT'N ENVS. ON << : TO 2E LOC
/ 683 698 15 2D03 << P <<
L 03 GM <<
R : HEAVILY BROKEN UP CORE : V. WEAK MICROVEIN TEXT. : AS ABOVE
/ 698 740 41 2E03 << P <<
L 03 GM <.
R : LOCAL TAN COLOR : V. WEAK MICROVEIN TEXT.
/ 740 780 22 2E03 << P <<
L 00 GM <.
R : HEAVILY BROKEN UP CORE W/ OCC. ZONES OF CLAY : V. WEAK MICRO-
R VEIN TEXT.
/ 780 817 28 8B10CLCY P*A* P
L 00 TG
R : NO CNT ATTITUDES DUE TO HEAVILY BROKEN AND LOST CORE : WEAK
R TRACHYTIC ALIGNMENT W/ PHENOS TO 12*2 MM : POST-MIN DYKE
/ 817 830 13 2D03CL << P V. <<
L 00 GU V.<<
R : V. WEAK MICROVEIN TEXT. : TO 2E LOC. : MINOR VEINLETS QZ+CB
R : OCC. CLAY ZONES
/ 830 860 26 2E03 << P V. <<
L 04 GU V.<<
R : AS ABOVE 74.0-78.0 M : HEAVILY BROKEN UP CORE W/ MINOR CLAY
R ZONES : V. WEAK MICROVEIN TEXT
/ 860 890 28 2E03 << P <)
L 05 GU <.
R : AS ABOVE W/ WEAK MICROVEIN TEXT : LOCAL DISTINCT FRAGS OF
R XTL TUFF W/ 40% FLAG? SHARDS
/ 890 936 25 2E03 << P <)
L 00 GU
R : HEAVILY BROKEN UP CORE W/ MINOR ZONES OF CLAY : V. WEAK
R MICROVEIN TEXT. : MINOR PY IN FRAGS : TO 2D LOCALLY
/ 936 972 18 2E03 << P <)
L 00 GU
R : HEAVILY BROKEN UP CORE W/ MINOR CLAY ZONES : WEAK MICROVEIN
R TEXT. : 2% PY IN FRAGS.
/ 972 1003 24 2E03 << P <)
L 00 GU
R : HEAVILY BROKEN UP CORE W/ MINOR CLAY ZONES : WEAK MICROVEIN

R TEXT. : OCC. REACTION RIMS ON LAPILLI
 / 1003 1039 26 2E03 << P <)
 L 00 GU
 R : HEAVILY BROKEN UP CORE W/ MINOR CLAY ZONES : WEAK MICROVEIN
 R TEXT. : TO 2D LOC. : 2% PY IN FRAGS
 / 1039 1064 24 2E03 << P <)
 L 00 GU
 R : HEAVILY BROKEN UP CORE W/ MINOR CLAY ZONES : 2% PY IN FRAGS
 R : TO 2D LOC.
 R END OF HOLE.

A001
 ALAB
 ATYP
 AMTH
 AUMM

EQUITY MINESITE LABORATORY
 ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

			RQD	% CU	G/TAG	G/TAU	% SE	% AS	% FE	% ZN
A001	234	262	5585	0.005	2.0	0.010	0.005	0.020	4.340	0.010
A001	262	293	5586	0.010	3.0	0.020	0.005	0.010	4.740	0.030
A001	293	323	5587	0.005	2.0	0.02	0.005	0.02	5.88	0.020
A001	323	354	5588	0.020	2.0	0.030	0.005	0.005	4.360	0.020
A001	354	380	5589	0.005	0.5	0.010	0.005	0.005	7.590	0.020
A001	380	410	5590	0.001	0.5	0.020	0.005	0.005	5.760	0.020
A001	410	440	5591	0.001	0.5	0.380	0.005	0.040	5.840	0.005
A001	440	470	5592	0.001	0.5	0.020	0.005	0.005	4.550	0.005
A001	470	500	5593	0.001	0.5	0.020	0.005	0.005	4.290	0.005
A001	500	530	5594	0.001	0.5	0.020	0.005	0.005	3.060	0.020
A001	530	560	5595	0.001	0.5	0.030	0.005	0.030	5.540	0.020
A001	560	588	5596	0.001	0.5	0.040	0.005	0.005	4.580	0.020
A001	588	619	5597	0.001	0.5	0.080	0.005	0.005	6.240	0.030
A001	619	650	5598	0.001	0.5	0.310	0.005	0.001	7.820	0.020
A001	650	683	5599	0.001	0.5	0.320	0.005	0.005	8.240	0.020
A001	683	710	5600	0.001	0.5	0.090	0.005	0.001	6.520	0.005
A001	710	740	5601	0.001	0.5	0.030	0.005	0.005	4.700	0.005
A001	740	760	5602	0.001	0.5	0.030	0.005	0.001	9.440	0.005
A001	760	780	5603	0.001	0.5	0.100	0.005	0.001	3.280	0.005
A001	817	830	5604	0.001	0.1	0.140	0.005	0.001	4.980	0.005
A001	830	860	5605	0.001	0.1	0.040	0.005	0.001	5.090	0.005
A001	860	890	5606	0.001	0.1	0.070	0.005	0.001	4.460	0.005
A001	890	911	5607	0.001	0.1	0.090	0.005	0.001	4.070	0.005
A001	911	936	5608	0.001	0.1	0.060	0.005	0.001	4.930	0.005
A001	936	957	5609	0.001	0.5	0.060	0.005	0.001	8.820	0.005
A001	957	988	5610	0.001	0.5	0.130	0.005	0.001	5.280	0.005
A001	988	1024	5611	0.005	0.5	0.060	0.005	0.001	4.980	0.001
A001	1024	1055	5612	0.001	0.1	0.070	0.005	0.001	5.550	0.001
A001	1055	1064	5613	0.005	0.5	0.030	0.005	0.001	5.200	0.005

R END OF ASSAYS - END OF LOG

IDEN6B0201			X86CH245 NQ 11APR86DJH	G&D APR86S38	0.0
IFRJ			EQUITY SILVER MINES LTD	NORTH ZONE - MZ	GEOCODE
S000	00	457	MT 172.5 090.0 -45.0	9118.23	9007.43 1322.01
S001	457	1320	172.5 090.0 -47.0		
S002	1320	1725	172.5 090.0 -45.0		
/SCL			MT.2MT.1		
LSCL			MT.2		
/NAM					QZSZTOPYCPPTTASFR
LNAM					DMCBCLMGHESLGLMO
/	00	192	OVBN	P	
L					
R			: TRICONED AND CASSED - NO CORE		
/	192	210	12 1C03QZ <<	P	<=
L			00 AW		
/	210	249	14 1C03QZ <<	P	<=
L			00 AW		
R			: 60% WHITE CHERT CLASTS : 40% DARK GREY CHERT CLASTS		
/	249	263	10 2D83MS <<	P	<<
L			00 6T		
R			: 5% INTERLEVED 1D : V. WEAK MICROVEIN TEXT.		
/	263	307	31 2C03 <<	P	<<
L			00 4A		
R			: LOC. HEAVILY BROKEN UP CORE W/SOME CLAY : POSSIBLE SILTSTONE		
R			W/O BEDDING : NO ALT'N ENVS. DN << : V. WEAK MICROVEIN TEXT.		
/	307	319	06 2C83MS <<	P	<<
L			00 5T		
R			: HEAVILY BROKEN CORE & CLAY 31.9-32.3 M : V. WEAK MICROVEIN		
R			TEXT. : CNTS. GRAD. OVER 0.1 M		
/	319	339	13 2D03 <<	P	<<
L			00 4A		<.
R			: V. WEAK MICROVEIN TEXT. : WEAK MS ENVS. LOCALLY		
/	339	346	07 1D01QZ	P	*(
L			00 4A		
/	346	380	32 1C04QZ	P	Q)Q)
L			21 AW		Q(
R			: AS ABOVE 19.2-24.9 M		
/	380	410	28 1C04QZ <<	P	<. Q)
L			23 AW		
R			: AS ABOVE W/O CP : V. WEAK MICROVEIN TEXT : 5% DISSEM. PY		
/	410	440	29 1C03QZ <<	P	<<
L			26 AW		
R			: V. WEAK MICROVEIN TEXT : BA 43.8-44.0 M		
/	440	468	23 1C01QZ <<	P	<. *(
L			13 AW		
R			: V. WEAK MICROVEIN TEXT.		
/	468	518	45 2D00 <<	P	
L			21 6A		
R			: POSSIBLY A TUFFACEOUS SILTSTONE (NO TEXT) : V. FINE RETIC.		
R			MICROVEINS W/MS : NO SDES		
/	518	544	26 1F00CY	P	
L			06 4A		
R			: DARK GREY TO BLACK SILTSTONE / MUDSTONE W/O BEDDING : NO PY		
R			: HEAVILY BROKEN UP CORE AND CLAY 54.4-56.4 M : BASIC (LAMP?)		
R			DYKE 54.0 TO 54.4 M. W/ 20% CL PHENOS (V. DARK GREEN COLOR)		
/	544	579	16 2D03 <<	P	<<

L 02 5A <.

R : WEAK MICROVEIN TEXT. : 8A 56.4- 56.7 M

/ 579 608 22 BA11CL A*P* P <(<(

L 08 6G CL 085 <.

R : UPPER CNT. OBSCURRED IN BROKEN CORE : POST-MIN. DYKE : V.

R WEAK MICROVEIN TEXT W/QZ+CB

/ 608 636 27 2D03 << P <(<(

L 17 5A <.

R : 10% INTERLEVED 2E

/ 636 654 17 BA11MS A* P CU 080A(A(

L 09 5T CL 060 A.

R : AMYGDS. FLATTENED & ALIGNED @ 070 : PRE-MIN. DYKE

/ 654 680 25 2C00 << P <.

L 08 5A <.

R : 8A AS ABOVE 65.8-66.1 & 66.7-67.0 M : 10% INTERLEVED 1F

/ 680 698 14 2C00 << P <.

L 07 5A <.

R : AS ABOVE 65.4-68.0 M : 5% INTERLEVED 2E : NO PY

/ 698 715 17 BA10CL A* P CU 075A(

L 10 5G

R : TAN COLOR @ CNT.

/ 715 807 92 BA10 P

L 58 4A

R : V. FINE GRAINED AND.? W/ OCC. PLAG PHENOS AND/OR AMYGDS.

R : WEAKLY ALTERED EXCEPT LAST METER OF INT. : NO SDES - POST

R MIN. DYKE : OCC. QZ+CB MICROVEINS

/ 807 1022 214 BCB0MS P* P CU 050

L 142 7T

R : 5% PLAG PHENOS TO 3*3 MM : LOWER CNT. OBSCURRED IN LOST CORE

R : POST-MIN DYKE

/ 1022 1030 08 2C00 << P BD 048

L 06 5A

R : MINOR INTERBEDDED 2E :WEAK MICROVEIN TEXT. W/MS :NO SDES

/ 1030 1095 65 BA10 A*<< P CU 042A(

L 31 4A CL 080

R : AS ABOVE 71.5-80.7 : WEAK AMYGD. TEXT. LOCALLY : WEAKLY

R ALTERED EXCEPT NEAR CNTS. : V. WEAK MICROVEIN TEXT. W/CB+QZ

/ 1095 1133 35 2D00 << P

L 30 5A

R : MASSIVE SILTSTONE? : V. WEAK MICROVEIN TEXT.

/ 1133 1154 19 2E01 P <(

L 10 6A

R : OCC. BXIA BLOCKS

/ 1154 1176 20 BA10CL A* P CU 085 <.

L 18 6G CL 085

/ 1176 1202 24 2D00 << P

L 19 5A

R : AS ABOVE 109.5-113.3 M : MINOR 2E LOC. INTERBEDDED? (V. STEEP

R ANGLE TO C.A.

/ 1202 1241 37 BA10CL A* P CU 085A(

L 18 4G CL 040

/ 1241 1270 28 2D00 << P <(

L 23 6A <(

R : V.WEAK MICROVEIN TEXT : TO 2E LOC.

/ 1270 1290 18 2D13CL << P <(

L 11 AG
 R : W/ 50% BA 128.0-129.0 M (STEEP CNT.) : TO 2D8 LOC W/ST COLOR
 / 1290 1367 74 BA10CL A* << P CU 075A(
 L 52 4G CL 051 A(
 R : FINE GRAINED TO APHANITIC MATRIX : 3% AMYGDS. : OCC. MICRO-
 R VEINS W/ QZ+CB
 / 1367 1400 33 2D13CL << P <<
 L 27 5G <<
 R : POSSIBLE MASSIVE SILTSTONE : WEAK MICROVEINED TEXT.
 / 1400 1430 30 2D13CLMS << P BD 015 Q(
 L 24 TG Q(
 R : MINOR 2D & 1D INTERLEVED : 2D83 LOC. W/6A COLOR
 / 1430 1448 13 2D11OCL P BD 058
 L 04 6G
 R : NO PY : MINOR 2E INTERBEDDED @ EOI
 / 1448 1457 09 1D14CL P CL 050 Q(
 L 08 4G
 R : TUFFACEOUS?
 / 1457 1486 29 2D13CL << P <.
 L 21 5G <.
 R : WEAK MICROVEIN TEXT. W/ MS+-CL+-PY
 / 1486 1500 14 2CB3MS << P <+
 L 10 6T <<
 / 1500 1535 34 2D10CLMS << P BD 053
 L 21 GA
 R : WEAK MICROVEIN TEXT. W/ MS : MINOR 2D8 INTERLEVED : LOCAL
 R WELDED? TEXT.
 / 1535 1560 26 BA10CL A*P* P CU 063
 L 19 4G CL 075
 R : WEAK PORPHYRITIC TEXT. : POST-MIN.DYKE
 / 1560 1592 32 2I10CLMS << P BD 042
 L 26 GA <<<.
 R : LOCAL MAROON COLOR : 2D & 2C LOCALLY INTERBEDDED : WEAK MICRO
 R -VEINED TEXT W/ CB OR CL
 / 1592 1618 28 BA10CL P* P CU 049
 L 20 4G CL 039
 R : 15% UNALIGNED PLAG. PHENOS TO 10*2 MM
 / 1618 1650 30 2D13CLMS << P <<
 L 19 TG <<
 R : WEAK MICROVEIN TEXT. W/ MS +-CL+-PY : TO 2C LOC. : 8A 163.4-
 R 163.8 M
 / 1650 1669 19 2D13CLMS << P <<
 L 17 TG <)
 R : AS ABOVE 161.8-165.0 M
 / 1669 1725 52 2E00 << P
 L 42 GU <.
 R : V. WEAK MICROVEIN TEXT. W/ MS +-CL : 20-80% BROWN ASH/DUST
 R MATRIX : LAPILLI FRAGS OF ACID TO INTER. PYROCLASTIC VOLC.
 / 1708 1708 X VU D V/ 025VB
 L V2
 R END OF HOLE AT 172.5 M

A001
 ALAB
 ATYP
 AMTH

EQUITY MINESITE LABORATORY
 ASSAY
 WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

AUMM		RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001	192	210	5614	0.005	3.0	0.080	0.005	0.090	7.570	0.040
A001	210	241	5615	0.005	2.0	0.060	0.005	0.070	6.150	0.020
A001	241	265	5616	0.005	2.0	0.070	0.020	0.100	10.200	0.005
A001	265	293	5617	0.005	0.1	0.050	0.005	0.020	6.410	0.001
A001	293	323	5618	0.005	0.1	0.030	0.005	0.005	3.660	0.001
A001	323	350	5619	0.005	0.1	0.050	0.005	0.020	3.520	0.001
A001	350	380	5620	0.330	14.0	0.150	0.020	0.100	9.890	0.060
A001	380	410	5621	0.090	10.0	0.150	0.040	0.005	6.520	0.005
A001	410	440	5622	0.010	0.5	0.080	0.010	0.005	3.490	0.005
A001	440	470	5623	0.010	0.5	0.090	0.010	0.005	2.670	0.005
A001	470	500	5624	0.005	0.5	0.070	0.010	0.005	5.140	0.005
A001	500	530	5625	0.005	0.5	0.009	0.010	0.005	6.500	0.005
A001	530	564	5626	0.010	0.5	0.110	0.010	0.005	5.000	0.005
A001	564	579	5627	0.005	0.5	0.070	0.010	0.005	4.710	0.005
A001	608	636	5628	0.005	0.5	0.090	0.005	0.005	4.900	0.005
A001	654	680	5629	0.005	0.5	0.120	0.005	0.005	4.660	0.005
A001	680	698	5630	0.005	0.5	0.130	0.005	0.005	4.360	0.005
A001	1022	1030	5631	0.005	0.5	0.060	0.005	0.005	4.040	0.005
A001	1095	1133	5632	0.005	0.5	0.100	0.005	0.005	4.480	0.005
A001	1133	1154	5633	0.005	0.5	0.040	0.010	0.005	4.690	0.005
A001	1176	1202	5634	0.005	0.5	0.120	0.005	0.005	4.390	0.005
A001	1241	1270	5635	0.005	0.5	0.090	0.005	0.005	6.140	0.005
A001	1270	1290	5636	0.005	0.5	0.040	0.005	0.005	10.920	0.005
A001	1367	1400	5637	0.005	0.5	0.130	0.005	0.005	4.410	0.005
A001	1400	1430	5638	0.005	0.5	0.130	0.005	0.005	4.090	0.005
A001	1430	1460	5639	0.005	0.5	0.130	0.005	0.005	6.890	0.005
A001	1460	1490	5640	0.005	0.5	0.060	0.005	0.005	6.200	0.005
A001	1490	1520	5641	0.005	0.5	0.190	0.005	0.005	4.990	0.005
A001	1520	1535	5642	0.005	0.5	0.030	0.005	0.005	3.770	0.005
A001	1561	1592	5643	0.005	0.5	0.040	0.005	0.005	2.680	0.005
A001	1618	1650	5644	0.005	0.5	0.040	0.005	0.005	5.250	0.005
A001	1650	1680	5645	0.005	0.5	0.030	0.005	0.005	4.740	0.005
A001	1680	1710	5646	0.005	0.5	0.030	0.005	0.005	4.870	0.005
A001	1710	1725	5647	0.005	0.5	0.060	0.005	0.005	4.480	0.005

R

END OF ASSAYS - END OF LOG


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IDEN6B0201      XB6CH253 NQ   JUN DJH   G&D JUN86S38      0.0
IPRJ            EQUITY SILVER MINES LTD   TAILINGS POND ZONE - MZ GEOCODE
S000 00 457 MT 291.4 090.0 -45.0      8942.20 8404.65 1276.52
S001 457 1513      291.4 090.0 -46.0
S002 1513 2513      291.4 090.0 -46.0
S003 2513 2914      291.4 090.0 -44.0
/SCL           MT.2MT.1
LSCL          MT.2
/NAM
LNAM
/ 00 104      QVBN      P
R :TRICONED -NO CORE
/ 104 171 67 2D83MSCL <<      P      <><.
L 15 6A      <>
R :A FEW STRINGERS OF PY +- CL +- TR CP :SPOTTED TEXT V
R :DISTINCTIVE (20-50% GREEN "SPOTS" TO 2 MM -(POSSIBLY
R :ANDALUSITE - A FEW W/ CUBIC X-SECTIONS - BUT MOST ARE
R :ANHEDRAL)
/ 171 204 33 2E13CY <<      P      <+ <>
L 18 6A
R :A FEW STRINGERS & << W/ PY + DARK GREY QZ +? :VARICOLORED
R : (GREEN, GREY, REDDISH FRAGS)
R :A FEW SUB-ROUNDED BUT MOST ARE ANGULAR :ANDESITE/ DACITE
R :LAPILLI TUFF :FRAGS ARE V CLOSELY PACKED (~75%) W/25%
R :ASH MATRIX :A FEW GOUGE ZONES
/ 204 224 18 2D83MSCL <<      P      <*<.
L 06 6A      <*<
R :V FEW STRINGERS & << W/ PY +- CL +- CP :SPOTTED TEXT AS
R :ABOVE 10.4 - 17.1 M :5% LAPILLI FRAGS (GREY)
/ 224 332 108 2C10CLCY <<      P
L 21 6A      <>
R :PALE GREENISH GREY COLOR :V WEAK << TEXT W/ CL ONLY :2D LOCALLY
/ 332 393 61 2C83MS <<      P      <*<
L 03 6A      <>
R :W/30% 2D INTERLEVED (IE. -GRADATIONAL BETWEEN 2C &2D) :AS
R :ABOVE INT. W/PY ::V WEAK TO MOD RETICULATE << W/ CL +- PY
/ 340 340      X      D4V/      V=      V9
L      V.
R :V/? OR THIN LENS (NO ANGLE DUE TO BROKEN UP CORE)
/ 393 407 14 2D10CL <<      P
L 00 5G      <>
R :V WEAK << TEXT W/ CL ONLY :30% TAN COLORED AND 70% PALE
R :GREEN COLORED FRAGS
/ 407 436 29 2C10CLCY <<      P
L 03 TG      <*<>
R :V PALE TG COLOR :NO GOUGE :V WEAK << TEXT W/ CL +- CB
R :(ANKERITE?)
/ 436 456 20 2C83MS <<      P      <>
L 00 6A      <*<
R :V WEAK << TEXT :ZONES OF CLAY GOUGE & BROKENUP CORE
/ 453 453      X      D4V/      030V=      V9
R :MINOR GOUGE @ UC
/ 456 474 18 2C10CL <<      P
L 03 GT      <=
R :MOD << TEXT W/CL ONLY :V PALE GREENISH TAN COLOR

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/ 474 486 12 8A10CL A* P CU 037
L 09 5G CL 082 A=
R :5% WHITE CALC A*
/ 486 520 34 2C10CL << P
L 10 7G <+
R :ONE << W/ PY AND MS ALT'N SELVAGE
/ 520 530 10 2D44CLQZ << P Q10.
L 00 5G
R :MINOR CY GOUGE @ 52.8 M :WEAK << TEXT W/ CL +- PY
/ 530 550 19 2C10CL << P
L 05 7G <+
R :AS ABOVE 48.6-52.0 :MOD << (RETICULATE) TEXT W/CL ONLY
/ 550 585 35 2E10CL << P BD 046
L 17 7G <)
R :20% LAPILLI FRAGS (15% ANDESITIC / 5% DACITIC) :V WEAK
R :<< TEXT W/ CL ONLY
/ 584 584 X D F/ 045
/ 585 604 19 2H10CL CT P CU 060
L 16 5G
R :2% GREY QZ CLASTS :NO << TEXT :NO CL NO PY :SHARP UPPER CNT
R : (UNDULATING) -MEASUREMENT IS AN AVERAGE
/ 604 660 55 2C13CLCY << P <<
L 21 7G < *
R :TO 2D LOCALLY :V WEAK << TEXT
/ 660 736 76 8A00CY P*A* P CU 053
L 51 4A A= D.
R :20% SUBALIGNED PLAG PHENOS (ALTERED TO CY) 2 X 10 MM IN A
R :DARK GREY/BROWN APHANITIC UNALTERED MATRIX
R :5% A* :SHARP, BLEACHED UPPER CNT AND LOWER CNT :NO < @
R :LOWER CNT DUE TO BROKEN CORE :2 INCLUSION OF TUFF @ 66.9-67.1
R :AND 68.5-68.7 M
/ 736 789 53 8A10CYCY A* P
L 40 AG CL 037 A+ D.
R :~3% A* :VARIABLY ALT'D (GENERALLY WEAK TO MOD)
/ 789 827 38 2C10CLCY << P
L 23 7G <)
R :V WEAK << TEXT W/CL ONLY :8A 79.8-80.1 M :PALE GREY AND
R :GREEN COLOR
/ 827 841 14 8A10CYCL P* P
L 08 UA
R :25% PLAG PHENOS (ALT'D TO CY) AS ABOVE 66.0-73.6 M - W/O
R :AMYGDS :BLEACHED UPPER CNT
R :CNT ANGLES NOT OBSERVED DUE TO BROKEN CORE
/ 841 848 07 2H10CL CT<< P <)
L 02 5G
R :ROUNDED TO SUB ROUNDED TO SUB ANG CLASTS AS ABOVE 58.5-60.4 M
R :V WEAK << TEXT
/ 848 896 48 2C10CLCY << P
L 21 7G <)
R :V WEAK << TEXT W/CL ONLY :TO 2E LOC :MINOR BXIA & GOUGE
/ 896 908 12 8A10CLCY P* P
L 09 AG LC 030 D.
R :5% ALT'D (CLAY) PLAG PHENOS IN MED GR MATRIX :UPPER CNT
R :IRREGULAR -NO ANGLE POSSIBLE
R :GOOD SHARP, CHILLED CNTS

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/ 908 972 64 2C10CLCY << P
L 47 7G <>
R :AS ABOVE 84.8-89.6 M :0.1 M BXIA ZONE @ 89.0 M W/15% PY
R :IN MATRIX
/ 972 985 13 2D10CL << P
L 06 5G <>
R :10% 2C INTERLEVED :V WEAK << TEXT W/ CL ONLY :V IRREG SHARP
R :UPPER CNT
/ 985 991 06 BA110CL P* P CU 057
L 04 5G
R :SHARP, CHILLED CNTS :20% UNALIGNED ALT'D FLAG PHENOS
R :LOWER CNT IRREGULAR (NO<)
/ 991 1000 09 2C10CL << P
L 05 MG <>
R :MOD << TEXT W/ CL
/ 1000 1006 06 2H10CL P CU 045
L 02 5G CL 053
R :NO SDES -NO << TEXT
/ 1006 1014 08 2D10CL << P
L 05 MG <>
R :MOD << TEXT W/ CL ONLY :AS ABOVE 99.1-100.0 ONLY COARSER
/ 1014 1053 39 BA10CLCY P* P CU 055
L 28 AG D.
R :LOWER CNT OBSCURRED IN BROKEN CORE :15% ALT'D (SAUSS)
R :FLAG PHENOS
/ 1053 1075 22 2E10CL << P
L 00 5G <>
R :MINOR CY GOUGE @ 107.0 M :TO 2C & 2D LOC :WEAK TO MOD << TEXT
R :W/CL ONLY
/ 1075 1085 10 BA10CL P*A* P
L 08 5G A+
R :20% ALT'D (SAUSS) FLAG PHENOS :2% CA AMGGDS :CNTS OBSCURRED
R :IN LAST CORE
/ 1085 1094 09 2E10CL << P
L 00 GA <<<<
R :FAULT GOUGE @ LOWER CNT :V WEAK << TEXT W/CB
/ 1094 1146 52 2C10CY << P
L 27 4A <>
R :~10% 2D INTERLEVED :V WEAK << TEXT W/ MS +- CL
/ 1146 1167 19 2D10CL << P BD 052<< <<<.
L 16 5G <<
R :TO 2C LOC :WEAK << TEXT
/ 1167 1187 20 2C13CY << P << <><.
L 08 4A <<<<
R :V WEAK << TEXT W/ QZ + CL + CB + PY +- CP
R :NOTE DARK GREY COLOR :TO 2D LOCALLY
/ 1187 1250 63 2C10CY << P <<
L 40 4A <<<+
R :AS ABOVE 116.7-118.7 ONLY W/O SDES :V WEAK << TEXT
R :W/ QZ + CB + CL :TO 2D LOC
/ 1250 1285 35 2DB3MS <<BR P <1<.
L 03 5T
R :HEAVILY BROKEN CORE W/ GOUGE AND FAULT BXIA :STRONG << TEXT
R :TO WEAK BXIA*N
/ 1285 1380 95 2CB3MS <<BR P <1<.

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L 43 5T <.
 R :STRONG << TEXT TO WEAK BXIA'N :10% INTERLEVED 2D
 R :NO GOUGE ZONES
 / 1380 1389 09 8A10CL P* << P CU 051(<)
 L 07 AG CL 047 (<)
 R :15% RANDOM PLAG PHENOS (ALT'D TO SAUSS)
 / 1389 1419 28 2D87MS BR P #1 #1
 L 16 7T
 R :GREY SDE? + QZ + PY AS BXIA MATRIX
 / 1390 1390 X D3V1 048V1 V9
 / 1419 1429 10 2D47CYQZ BR << P #) #=
 L 08 4A
 R :GREY SDE + QZ + PY AS BXIA MATRIX :AS ABOVE ONLY GREY COLOR
 R :AND MORE CY :IRREG PY STRINGER @ 142.8 M
 / 1429 1441 12 4B11CL P* << P D.
 L 07 7G
 R :LOOKS LIKE 4B BUT CONTAINS INCLUSIONS OF MINERALIZED UNIT 2
 R :5% ANHEDRAL PLAG PHENOS (WHITE) IN A F.G. PALE GREEN MATRIX
 R :W/ WEAK << TEXT
 / 1441 1463 22 8A10CL P* << P (<)
 L 19 5G (<)
 R :10% ALTERED PLAG PHENOS :5% AMYGDS (QZ + CB)
 / 1463 1552 89 4B13CL <<P* P <. (< (<
 L 65 6G <.
 R :AS ABOVE 142.9-144.1 M :10-20% ANHEDRAL TO EUHEDRAL PLAG
 R :PHENOS (WHITE) IN A MED TO PALE GREEN MATRIX :BA 149.0-149.4;
 R :151.6-151.8; 152.0-152.2
 R :NO QZ PHENOS BUT MATRIX IS GENERALLY WEAKLY ALTERED
 R :(IE. -SILICEOUS?)
 / 1552 1597 45 2D13CL <<BR P <+
 L 21 7G (<)
 R :LOCAL BR TEXT :BA 157.8-158.1
 / 1597 1613 16 2H13CL CT << P (<)
 L 14 5G D.
 R :V WEAK << TEXT :PY ALSO IN PATCHES :CLASTS ARE ROUNDED TO
 R :SUBROUNDED, TO 30 MM DIA
 / 1613 1743 120 2D83MS <<BR P <=
 L 53 7T << (< (<
 R :LOCAL BXIA TEXT W/ PY + QZ + GREY SDE? MATRIX
 R :TO 2E & 2C LOCALLY
 / 1743 1768 25 2D11CL <<BR P (< (< (< (<
 L 21 7G (<)
 R :V WEAK << TEXT W/ PY + CL +- TO ? :V MINOR BXIA
 / 1768 1782 14 2D83MS <<BR P (< <=
 L 10 7T
 R :AS ABOVE 161.3-174.3 M
 / 1782 1794 12 2D13CL <<BR P (< <+
 L 06 6G
 R :LOCAL BXIA W/ QZ + PY + GREY SDE? INFILLING
 / 1794 1811 15 2D10CLCY << P CU 075
 L 00 AG
 R :WEAK << TEXT W/ MS +- QZ? :V SHARP UPPER CNT :DARK GREY/GREEN
 R :COLOR :NO SDES
 / 1811 1827 16 2D00 LM P BD 045
 L 00 4A

R :GOOD LAMINATED BEDDING
/ 1827 1871 44 2D03CY << P <<
L 00 4A
R :V WEAK << TEXT W/ PY :LOTS OF CY GOUGE (FAULT ZONE?)
R :WEAK ALT'N & MIN
/ 1871 1878 07 8A10CL P*A* P CU 045<)
L 00 5G CL 055 <)
R :BLEACHED & CHILLED CNTS :PHENOS TO 2 MM X .5 MM (25%)
/ 1878 1899 21 2I00 << P BD 041
L 03 4A <+
R :MOD << TEXT W/+- CL + MS :LIGHT GREY FRAGS (OCC LAPILLI)
R :BD WELDED :LOWER CNT GRAD OVER 1 M
/ 1899 1950 51 2D93QZMS <<BR P #) <)<+
L 39 7T <)
R :LOCAL BXIA TEXT W/ QZ + PY +- TO INFILLING :ALSO XTL
R :CLUSTERS OF TO
/ 1950 1978 28 8A10CL A* P CU 072A)
L 24 5G CL 073 A)
R :3-5% AMYGDS :NO PHENOS
/ 1978 2000 21 2E13CL << P <+
L 10 6G <.
R :20% LAPILLI (PALE GREY AND GREEN COLORED)
R :WEAK TO MOD << TEXT :ASH + DUST MATRIX
/ 2000 2007 07 8A10CY A* P CU 075
L 05 5T CL 052
R :BLEACHED? ANDESITE? :CHILLED & FLOW BANDED CNTS :5% AMYGDS
/ 2007 2016 09 2E13CL << P <)
L 00 6G
R :AS ABOVE 197.8-200.0 :MOD << TEXT :ASH + DUST MATRIX
R :20% LAPILLI FRAGS
/ 2016 2043 27 4B13QZCL <<P* P <+
L 21 6G
R :PY ALSO OCCURS IN PATCHES
/ 2043 2116 73 8C10CY P* P CU 040
L 68 7G FB 058 <.
R :TYPICAL LATITE DYKE :LOWER CNT IRREG (TOOK FB INSTEAD)
/ 2116 2210 94 2E93QZCL <<BR P <)<R)<+
L 79 7G <)
R :LOCAL BXIA W/ QZ + PY + TO INFILLING :LOWER CNT GRAD OVER 1 M
R :TO 2F LOC
/ 2210 2298 105 2E93QZCL << P <*<R)<<
L 73 7G <<
R :AS ABOVE W/O LESS TO AND PY :SILICIFICATION MAINLY IN MATRIX
R :NOT FRAGS :NOTE -IN THESE TWO INTERVALS SOME FRAGS LOOK LIKE
R :4A/B!! -IS THIS POSSIBLE? :QZ + PY + TO INCREASING TOWARDS EOI
/ 2298 2315 17 2E93QZCL << P <=<R)<=
L 15 7G <<
/ 2315 2322 07 8A10CLCY A* P CU 046
L 07 UG CL 042
R :SHARP, INTRUSIVE CNTS W/ FLOW BANDING
/ 2322 2356 34 2D13CL WD<< P BN 038 <<<<
L 30 AG <<
R :2E @ START OF INT :TO 2C LOCALLY :TO 2D13 LOC W/ PY + QZ
R :WD = WELDED TEXT
R :V WEAK << TEXT W/ +- PY +- HE +- TO

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/ 2356 2396 40 8A10CY A* P CU 060A)
L 34 7G CL 065
R :BLEACHED & CHILLED THROUGHOUT :TUFF INCLUSION? 237.9-238.5 M
R :MINOR GOUGE @ LOWER CNT
/ 2396 2437 41 2D93MSCL << P BD 025<( <)<<
L 37 GT
R :TO 2E LOC. :V WEAK << TEXT :TO ALSO IN PATCHES (R)
R :INTERBEDDED DUST TUFF (THIN)
/ 2437 2454 17 2D10CL WD P BN 030
L 06 7G
R :PART WELDED (NOT ENOUGH TO BE 2I :NO SDES
/ 2454 2501 47 2D93MSCL << P BD 030<( <)<<
L 17 GT WD 030
R :AS ABOVE 239.6-243.7 :TO 2E LOC
/ 2501 2536 35 8A10CL P* P CU 070
L 32 AG
R :20% ALT'D (SAUSS) PLAG PHENOS TO 3 X 10 MM
/ 2536 2584 48 2D93QZMS << P <*< <)<
L 22 GT
R :WEAK TO MOD << TEXT :TO 2E LOC.
/ 2584 2598 14 8A10CY A* P CU 020A+
L 14 7A CL 010 A+
R :BLEACHED 8A? :LOWER CNT IRREG
/ 2598 2770 172 2D43QZMS << P BD 025<( <)<<
L 124 GT << #.
R :WEAK TO MOD << TEXT :TO 2E LOC. :MINOR INTERBEDDED DUST TUFF
R :V LOCAL BXIA W/PY INFILLING +TR SL
R :NOT ENOUGH TO FOR 2D93 :8A 273.9-274.6
/ 2770 2784 14 4B91MS << P <)< D+
L 11 5A <)<
R :MOD << TEXT W/ QZ + CB
/ 2784 2792 07 8A13HECY <<A* P CU 045A= <*<
L 04 MU A=
R :FAULTED CNTS :BLEACHED ENVELOPES ON << :PRE-MINERAL DYKE?
R :5% AMYGDS TO 2 MM DIA
/ 2792 2829 37 2E43QZCL << P <=< <=<
L 18 GA <)<
R :TR GREY SDE? :MOD TO STRONG << TEXT
/ 2829 2837 08 8A10CY A* P CU 045A*
L 07 7A CL 015 A+
R :BLEACHED 8A? OR 8C? :5% AMYGDS TO 2 MM
/ 2837 2914 77 2E43QZCL << P <+ <)<
L 68 GT <<
R :TO 2D LOC :OCC SPEC TO? :WEAK << TEXT
R :EOH @ 291.4 M

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A001
ALAB EQUITY MINESITE LABORATORY
ATYP ASSAY
AMTH WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM RCOVSAMPLE RQD % CU G/TAG G/TAU % SB % AS % FE % ZN
A001 104 130 6370 0.001 0.5 0.040 0.005 0.010 2.790 0.040
A001 130 160 6371 0.005 0.5 0.020 0.005 0.005 3.560 0.020
A001 160 190 6372 0.005 0.5 0.050 0.005 0.001 3.910 0.030
A001 190 220 6373 0.005 0.5 0.020 0.005 0.001 5.060 0.020
A001 220 250 6374 0.005 0.5 0.040 0.005 0.020 3.960 0.020

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A001	250	280	6375	0.005	0.5	0.070	0.005	0.001	4.980	0.020
A001	280	310	6376	0.005	0.5	0.010	0.001	0.020	4.010	0.020
A001	310	340	6377	0.005	0.5	0.020	0.001	0.001	6.050	0.020
A001	340	370	6378	0.005	0.5	0.040	0.005	0.010	3.310	0.020
A001	370	400	6379	0.005	0.5	0.060	0.005	0.001	4.970	0.020
A001	400	430	6380	0.005	0.5	0.010	0.001	0.040	5.280	0.020
A001	430	456	6381	0.005	0.5	0.010	0.001	0.001	7.230	0.020
A001	456	474	6382	0.005	0.5	0.020	0.005	0.005	4.450	0.030
R	474	486	:DYKE -NO SAMPLES							
A001	486	510	6383	0.005	0.5	0.010	0.005	0.001	4.390	0.030
C001	510	540	6384	0.005	0.5	0.020	0.005	0.010	6.620	0.030
A001	540	570	6385	0.005	0.5	0.010	0.005	0.001	5.560	0.030
A001	570	600	6386	0.005	0.5	0.030	0.005	0.001	5.410	0.030
A001	600	630	6387	0.005	0.5	0.020	0.001	0.001	2.840	0.030
A001	630	660	6388	0.005	0.5	0.010	0.005	0.010	1.810	0.020
R	660	789	:DYKE -NO SAMPLES							
A001	789	827	6389	0.005	0.5	0.030	0.005	0.001	3.200	0.030
R	827	841	:DYKE -NO SAMPLES							
A001	841	870	6390	0.005	0.5	0.010	0.005	0.001	4.870	0.030
A001	870	896	6391	0.005	0.5	0.010	0.005	0.001	3.590	0.030
R	896	908	:DYKE -NO SAMPLES							
A001	908	930	6392	0.005	0.5	0.010	0.005	0.001	5.070	0.030
A001	930	960	6393	0.005	0.5	0.010	0.005	0.001	5.180	0.030
A001	960	990	6394	0.005	0.5	0.020	0.005	0.001	4.450	0.030
A001	990	1014	6395	0.005	0.5	0.010	0.005	0.010	4.960	0.030
R	1014	1053	:DYKE -NO SAMPLES							
A001	1053	1075	6396	0.005	0.5	0.010	0.005	0.030	3.570	0.030
R	1075	1085	:DYKE -NO SAMPLE							
A001	1085	1110	6397	0.005	0.5	0.010	0.005	0.010	3.460	0.030
A001	1110	1140	6398	0.005	0.5	0.020	0.001	0.001	3.350	0.030
A001	1140	1170	6399	0.005	0.5	0.010	0.001	0.030	4.600	0.030
A001	1170	1200	6400	0.005	0.5	0.010	0.001	0.010	4.950	0.030
A001	1200	1230	6401	0.005	0.5	0.010	0.001	0.001	5.590	0.030
A001	1230	1260	6402	0.070	0.5	0.100	0.010	0.001	5.720	0.040
A001	1260	1290	6403	0.080	7.0	0.160	0.005	0.040	5.890	0.040
A001	1290	1320	6404	0.030	19.0	0.280	0.005	0.010	9.840	0.080
A001	1320	1350	6405	0.005	0.5	0.150	0.001	0.090	5.040	0.040
A001	1350	1380	6406	0.040	0.5	0.230	0.010	0.001	6.310	0.040
R	1380	1389	:DYKE -NO SAMPLES							
A001	1389	1420	6407	0.005	0.5	0.190	0.001	0.030	9.870	0.040
A001	1420	1441	6408	0.005	0.1	0.040	0.005	0.070	3.380	0.040
R	1441	1463	:DYKE -NO SAMPLES							
A001	1463	1490	6409	0.005	0.1	0.050	0.005	0.010	1.720	0.030
A001	1490	1520	6410	0.005	0.1	0.020	0.005	0.001	2.100	0.040
A001	1520	1550	6411	0.005	0.1	0.030	0.005	0.001	1.790	0.050
A001	1550	1580	6412	0.005	0.1	0.010	0.005	0.001	3.660	0.210
A001	1580	1610	6413	0.005	0.1	0.020	0.005	0.010	5.360	0.070
A001	1610	1640	6414	0.001	0.1	0.005	0.001	0.001	3.710	0.050
A001	1640	1670	6415	0.005	2.0	0.005	0.005	0.005	4.510	0.080
A001	1670	1700	6416	0.005	3.0	0.020	0.005	0.005	4.560	0.190
A001	1700	1730	6417	0.005	0.5	0.005	0.005	0.005	3.510	0.040
A001	1730	1760	6418	0.005	0.5	0.005	0.005	0.005	3.680	0.005
A001	1760	1790	6419	0.005	0.5	0.005	0.005	0.005	4.680	0.010
A001	1790	1820	6420	0.005	1.0	0.030	0.005	0.005	3.710	0.030
A001	1820	1850	6421	0.005	5.0	0.070	0.005	0.010	0.330	0.005

A001	1850	1871	6422	0.005	1.0	0.010	0.005	0.010	3.100	0.005
R	1871	1878	:DYKE	-NO SAMPLE						
A001	1878	1900	6423	0.005	0.5	0.010	0.005	0.010	4.290	0.005
A001	1900	1930	6424	0.005	0.5	0.030	0.005	0.005	4.030	0.010
A001	1930	1950	6425	0.005	0.5	0.020	0.005	0.005	3.840	0.040
R	1950	1978	:DYKE	-NO SAMPLE						
A001	1978	2000	6426	0.005	1.0	0.020	0.005	0.005	2.300	0.080
R	2000	2007	:DYKE	-NO SAMPLE						
A001	2007	2021	6427	0.005	1.0	0.030	0.005	0.005	5.080	0.010
A001	2021	2043	6428	0.050	3.0	0.005	0.020	0.005	5.180	0.020
R	2043	2116	:DYKE	-NO SAMPLES						
A001	2116	2140	6429	0.005	2.0	0.005	0.005	0.005	3.020	0.070
A001	2140	2170	6430	0.005	0.5	0.005	0.005	0.005	2.960	0.040
A001	2170	2200	6431	0.005	0.5	0.005	0.005	0.005	3.260	0.030
A001	2200	2230	6432	0.005	0.5	0.020	0.005	0.005	3.300	0.160
A001	2230	2260	6433	0.005	2.0	0.030	0.005	0.005	5.740	0.090
A001	2260	2290	6434	0.005	1.0	0.030	0.005	0.005	4.380	0.060
A001	2290	2315	6435	0.005	2.0	0.040	0.005	0.005	5.540	0.030
R	2315	2322	:DYKE	-NO SAMPLE						
A001	2322	2356	6436	0.005	0.5	0.020	0.005	0.005	3.520	0.020
R	2356	2396	:DYKE	-NO SAMPLES						
A001	2396	2420	6437	0.005	0.5	0.020	0.005	0.005	2.790	0.010
A001	2420	2450	6438	0.005	0.5	0.005	0.005	0.005	2.450	0.005
A001	2450	2480	6439	0.005	1.0	0.030	0.005	0.005	3.190	0.040
A001	2480	2501	6440	0.005	0.5	0.020	0.005	0.005	2.920	0.005
R	2501	2536	:DYKE	-NO SAMPLES						
A001	2536	2560	6441	0.005	0.5	0.020	0.005	0.005	2.830	0.005
A001	2560	2584	6442	0.005	0.5	0.010	0.005	0.005	3.080	0.005
R	2584	2598	:DYKE	-NO SAMPLE						
A001	2598	2620	6443	0.005	0.5	0.010	0.005	0.005	4.450	0.050
A001	2620	2650	6444	0.005	1.0	0.030	0.005	0.005	3.530	0.090
A001	2650	2680	6445	0.005	0.5	0.020	0.005	0.005	3.220	0.010
A001	2680	2710	6446	0.005	1.0	0.020	0.005	0.005	4.640	0.090
A001	2710	2740	6447	0.005	0.5	0.050	0.005	0.005	4.460	0.050
A001	2740	2770	6448	0.005	0.5	0.020	0.005	0.005	4.120	0.100
A001	2770	2784	6449	0.005	3.0	0.050	0.005	0.005	3.980	0.350
R	2784	2792	:DYKE	-NO ASSAY						
A001	2792	2811	6450	0.005	2.0	0.010	0.005	0.005	4.320	0.250
A001	2811	2829	6451	0.005	2.0	0.020	0.005	0.005	3.430	0.130
R	2829	2837	:DYKE	-NO ASSAY						
A001	2837	2860	6452	0.010	1.0	0.030	0.005	0.005	5.390	0.040
A001	2860	2890	6453	0.005	1.0	0.010	0.005	0.005	5.140	0.250
A001	2890	2914	6454	0.005	1.0	0.010	0.005	0.005	4.620	0.200
R			:END OF HOLE							
R			END OF ASSAYS - END OF LOG							

IDEN6B0201		X86CH254 NO 23JUN86RBP	G&D JUN86S38	0.0
IPRJ		EQUITY SILVER MINES LTD	TAILINGS POND ZONE - MZ CODE	
S000	00	457 MT 260.9 070.0 -45.0		8899.71 8205.52 1281.34
S001	457	1753 260.9 070.0 -43.0		
S002	1753	2609 260.9 070.0 -44.5		
/SCL		MT.2MT.1		
LSCL		MT.2		
/NAM				QZSZTOPYCFPTTASPR
LNAM				DMCBCLMGHESLGLMO
/	00	229	OVBN	P
R			CASING TO 22.9 M	CASED THRU FILL ROCK OF NO.2 TAILINGS DAM.
/	229	235	05 2E43QZ	<< P <*<+
L			00 7T	
R			ROCK VERY BROKEN	
/	235	247	09 8B00FL	TC P <)
L			00 6G	S)
R			CHLORITE REPLACES FELDSPAR PHENOS.	
/	247	264	13 2E93QZ	<< P <)<+<.
L			00 BR	<.
/	264	314	39 2E93QZ	<< P <)<+<.
L			06 9R	
R			LAPILLI FRAG. ALTERED TO SERICITE. MATRIX SILICOUS.	
/	314	320	06 2E91	<< P F/ <*(
L			03 8R	
/	320	350	29 2F91	<<BR P FU 50 <*(
L			05 8W	
R			UPPER CONTACT HAS FAULT GOUGE. ROCK TYPE POSSIBLY WELDED.	
/	350	380	29 2F91QZ	<<BR P Q)Q+Q.
L			05 8W WL	
R			CLASTS UP TO 5.0 CM DIA. MIN. OCCUR IN BOTH << + Q'S.	
/	380	410	27 2F91QZ	<<BR P Q)Q+Q.
L			03 8W WL	
R			COMMENT ON RX TYPE: LOOKS LIKE WELDED TUFF THAT HAS BEEN BX'D.	
/	410	440	29 2F91QZ	<<BR P Q*Q)
L			11 8W	
R			AS ABOVE.	
/	440	470	28 2F91QZ	<< P Q(Q*Q.
L			06 8W	
R			BX FRAGMENTS NOT AS LARGE, IAS ABOVE. FRAG. ALTERED TO SERICITE.	
/	470	500	29 2E91	<< P <) Q-Q)
L			05 8A	
R			MATRIX SILICA FLOODED, LAPILLI TO SER.	
/	500	550	47 2E91	<<WL P <) Q-Q)
L			09 8A	
R			AS ABOVE.	
/	550	600	46 2F91QZ	<<BR P <) Q(Q+
L			07 8A	
R			BX CLASTS UNIFORM 1.0 CM TUFFACEOUS.	
/	600	650	42 2E91QZ	<<WL P <) Q(Q)
L			10 8A	
R			PATCH AT 63.8 WITH ABUNDANT TO. FRAG. TO SERICITE.	
/	650	689	2E91QZ	<< P <) Q-Q)
L			8A	
R			AS ABOVE.	
/	689	734	39 2I41	<<WL P F/ D*

L			00	8G	WP			
R			FAULT ZONE (WHOLE INTERVAL).					
/	734	805	65	2F91QZ	<<BR	P	<)	Q+Q+
L			21	8R				
R			LOTS OF TO. SERICITE ALT'N OF FRAG.					
/	805	820	14	2E91QZ	<<	P		Q-Q)
L			00	8A				
/	820	835	14	2F91QZ	<<	P		Q+Q+
L			05	8R				
R			SAME AS 80.5 TO 82.0 ABOVE.					
/	835	868	30	8A00		P	<)	
L			16	3G				
R			DYKE HAS CHILLED UPPER AND LOWER CONTACTS.					
/	868	977	101	2E91QZ	<<	P	<)	Q+Q+D.
L			50	8W				
R			SOME FRAG. ALTERED TO SERICITE., QTZ FLOODED. SOME FRAG. ELONGATED.					
R			RARE PINK STAINING TO K-FELDSPAR FLOODING ?					
/	977	989	11	8B10	TC	P	<-	
L			06	49				E1
/	989	1079	84	2E91		P		Q)Q)
L			21	8R				
R			SIMILAR TO 86.8 TO 97.7 ABOVE. MORE PINKISH. FRAG. < 1.0 CM.					
/	1079	1091	11	8B10	TC	P		
L			00	3G				S+
/	1091	1110	17	2E91CY	BR	P F/		Q)D-
L			00	9T				
R			ZONE IS LIKELY MYLONITE IE FAULT BX. LITTLE TO, RARE SULPHIDE.					
/	1110	1141	30	2H11		P BD	25	Q-D)D.
L			11	5R				
R			MULTI COLORED. SOME ROOUNDED, SOME ANGULAR FRAG.					
/	1141	1180	38	2C51QZ	MX	P		Q+
L			21	4A				
R			MASSIVE UNIT. MINOR FRAG. UP TO 1.0 CM.					
/	1180	1210	29	2D51QZ	MX<<	P		Q+
L			12	4A				
R			SIMILAR TO ABOVE UNIT.					
/	1210	1250	36	2D51QZ	<<	P		Q+
L			12	4A				
R			AS ABOVE. SMALL DYKE 123.6 TO 123.8.					
/	1250	1288	31	8A10	BR<<	P		
L			05	5G				
/	1288	1334	41	2H91		P	<*	D)D(
L			08	8R				
R			SOME OF MATRIX ALTERED TO CLAY. VERY SIMILAR TO 111.0 TO 114.1					
R			ABOVE. COLOR VARIES.					
/	1334	1346	11	2C11CY	BR<<	P F/		D(
L			00	5G				Q+
R			LIKELY FAULT BX. CORE VERY BROKEN.					
/	1346	1388	40	8B10	TC	P BN	35<<	
L			09	5G				S+
R			XENOLITH OF 2C AT 135.4					
/	1388	1410	20	2C91	<<	P	<+	Q(Q(
L			03	6G			<=	
/	1410	1419	07	2E41	BR	P	<1	Q-D.
L			00	8G				

R MYLONITE SIMILAR TO 109.1 TO 111.0.
 / 1419 1464 44 8A10 << P <=
 L 12 6G <1 D)
 / 1464 1490 25 2E91 << P Q(Q+
 L 16 8R
 R SIMILAR TO LAPILLI AND BX AS BEFORE. CLAY IN SMALL SHEARS.
 / 1490 1547 54 2E91 <<BX P BN 30< Q+Q+D.
 L 29 8R WF
 R UPPER CONTACT-FAULT BX. SEVERAL CY RICH SHEARS. OCCASIONAL ANGULAR FRAG
 / 1547 1570 21 2F91 <<BX P F/ Q(D(
 L 03 8R WF BN 40
 R SUSPECT LOST CORE BETWEEN THIS INTERVAL AND LAST ONE.
 R DOG'S BREAKFAST BOTTOM OF INTERVAL TO FAULT GOUGE.
 / 1570 1610 37 8A10 <<VU P CL 20B+
 L 06 6G <=
 R MINOR SERICITE ALTERATION.
 / 1610 1630 19 2F91 BR<< P Q(D+
 L 05 4A
 R BX'D 2C. GRADES INTO 2E. BX MOST INTENSE AT TOP OF INTERVAL.
 / 1630 1664 32 2E91 << P Q*B+D.
 L 15 5A
 R MATRIX SILICIFIED.
 / 1664 1671 07 8B10 TC P BN 50<)
 L 4A S2
 R CHILLED MARGINS.
 / 1671 1706 33 2E91 << P Q(B+D.
 L 20 5G
 R MATRIX SILICIFIED. VERY SIMILAR TO 163.0 TO 166.4 ABOVE.
 / 1706 1713 06 2F91 BR P << Q)D)
 L 02
 R LIKELY LAHAR. SAME ALT'N AND MIN OVERPRINTED AS ABOVE. DOG'S BREK.
 / 1713 1760 44 2E91 << P <) Q(B+
 L 32 5G
 R AS 167.1 TO 170.6 ABOVE. LAPILLI INDISTINCT GENERALLY.
 R PATCH OF INTENSE TO AT 174.3
 / 1760 1790 29 2E91 << P <) Q)B(
 L 11 5G
 / 1790 1850 57 2C41 << P <+ Q.<+
 L 15 5G <<
 R RANDOM LAPILLI, VERY LITTLE TO. PYRITE ALSO DISSEM. & PATCHY.
 / 1850 1897 45 2E41 << P <+ Q-<)
 L 17 6G
 R SIMILAR TO ABOVE.
 / 1897 1916 15 8B10 <<TC P BN 75<)
 L 3A CM S2
 / 1916 1973 2D41 <<WP P <+ Q(D=
 L 5G
 R CONTAINS MINOR LAPILLI.
 / 1973 1983 10 8A00 <<CM P CU 35<=
 L 07 5A CL 35 S2
 R MARGINS ALTERED TO SERICITE.
 / 1983 2010 26 2D41 <<WP P <) Q-D=
 L 09 5G
 R SIMILAR TO 2D ABOVE. PY IN << AND PATCHES AS WELL.
 / 2010 2017 07 8B10 TCCM P CU 20

L			02	3A		CL	35	S1
R			SOME SERICITE ALT'N OF FELDSPAR.					
/	2017	2040	22	2D41	<<WP	P	<)	Q)D=
L			19	5G				
/	2040	2085	42	2D41	<<WP	P		Q-D=
L			31	5G				
R			PYRITE ALSO IN <<. VERY LITTLE TO.					
/	2085	2104	18	2C41	<<	P	<+	B+
L			11	5G				
/	2104	2140	34	2D41	<<	P	<)	Q-B+
L			11	5G				
/	2140	2170	29	2C41	<<	P	<)	D.B+
L			06	5G				
R			SOME CL ON SHEAR AT 215.9					
/	2170	2195	24	2D51	<<	P	<+	Q(B=
L			09	5G				
/	2195	2214	18	8A10	CM	P CU	35<<	
L			11	7G				
/	2214	2226	11	2D51	<<	P	<<	QCB=
L			06	5G				
/	2226	2260	32	2E91	<<BR	P	<-	Q+B+D.
L			18	8G				<=
R			UPPER CONTACT GRADATIONAL. PY IN << AS WELL.					
/	2260	2304	42	2E91	<<BR	P	<+	<)<+<+
L			19	5G				
R			CORE BX'D IE DISRUPTED.					
/	2304	2321	15	2F91	BR<<	P	++	Q)B+
L			00	9T				
R			VERTICAL BX'D COARSE, UP TO 4.0 CM. LIKELY CONTACT ZONE BETWEEN					
R			TUFFS AND BRECCIA. SERICITE ALT'N OF SOME FRAG.					
/	2321	2360	37	2F91	<<BR	P		Q-D)D.
L			21	8T				
R			COARSE BX, FRAG UP TO 4.0 CM. VERY SILICIOUS, SOME CLAY * SHEARS					
R			FRAG. ARE TUFFACEOUS, VARY WIDELY IN COLOR AND SIZE.					
/	2360	2390	29	2F91	<<BR	P	<)	Q+B=
L			17	8T				
R			AS ABOVE, MORE TO.					
/	2390	2408	18	8B00	T<<M	P CU	55<*	
L			13	5G	VU			
/	2408	2436	26	2F91	<<BR	P	<)	Q+B=
L			19	8T				
R			SAME BX AS ABOVE					
/	2436	2487	49	2F91	<<BR	P		<(D*
L			21	7M				
R			SIMILAR TO ABOVE, EXCEPT SMALLER BX FRAG. IE 1.0CM. VERY SILICIOUS,					
R			OCCASIONAL SERICITE ALT'N FRAG.					
/	2487	2510	23	2F41	BR	P		D*
L			04	9M				
R			NO TO. FRAG. UP TO 2.0 CM. FRAG. STILL TUFFACEOUS, SOME FRAG.					
R			HAVE SERICITE ALT'N.					
/	2510	2524	14	2F41	BR	P		D)
L			07	7M				
/	2524	2579	53	2F91	BR<<	P	<)	<)*D+
L			28	9M				
R			VERY SILICIOUS. SOME CLAY ON A FEW SMALL SHEARS. OCCASIONAL SERICITE					

CM.

R FRAG. FRAG. MAINLY TUFFACEOUS IE 2C TYPE. LIGHT COLORED FRAG. UP TO 3.0
 / 2579 2609 29 2F91 BR P SH 40V+ Q)B+
 L 19 7M
 R QTZ-FY-TO VIEN AT 159.4. STILL VERY SILICIOUS. QTZ-PY-CY SHEAR
 R AT 159.8.
 R ALL THE BX SINCE 232.1 TO THE END OF HOLE ARE VERY SIMILAR,
 R WITH SLIGHT VARIATIONS IN FRAG. SIZE AND MATRIX COLOR, HOWEVER
 R CONSIDERABLE VARIATION IN TO. AND PY. CONTENT. ALL BX VERY
 R SILICIOUS WITH A FEW SERICITE ALT'N FRAG.
 R END OF HOLE.

A001 EQUITY MINESITE LABORATORY
 ALAB ASSAY
 ATYP WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
 AMTH
 ALUMM

RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001 229 260 6481	0.005	2.0	0.010	0.005	0.005	4.580	0.010	
A001 260 290 6482	0.005	1.0	0.005	0.005	0.005	4.140	0.005	
A001 290 320 6483	0.005	0.5	0.005	0.005	0.005	4.070	0.005	
A001 320 350 6484	0.005	0.5	0.010	0.005	0.005	1.980	0.005	
A001 350 380 6485	0.005	0.5	0.005	0.005	0.005	2.560	0.005	
A001 380 410 6486	0.005	0.5	0.005	0.005	0.005	2.650	0.005	
A001 410 440 6487	0.005	0.5	0.010	0.005	0.005	3.180	0.005	
A001 440 470 6488	0.005	0.5	0.020	0.005	0.005	4.010	0.005	
A001 470 500 6489	0.005	2.0	0.030	0.010	0.005	3.810	0.030	
A001 500 530 6490	0.005	1.0	0.040	0.005	0.005	3.830	0.030	
A001 530 560 6491	0.005	1.0	0.050	0.005	0.005	2.650	0.020	
A001 560 590 6492	0.005	0.5	0.030	0.005	0.005	2.700	0.030	
A001 590 620 6493	0.005	0.5	0.040	0.005	0.005	4.200	0.030	
A001 620 650 6494	0.005	0.5	0.040	0.005	0.005	4.870	0.090	
A001 650 680 6495	0.005	0.5	0.040	0.005	0.020	3.160	0.010	
A001 680 710 6496	0.005	3.0	0.050	0.010	0.020	4.450	0.060	
A001 710 740 6497	0.005	4.0	0.040	0.010	0.005	4.460	0.080	
A001 740 770 6498	0.005	2.0	0.100	0.010	0.005	5.180	0.010	
A001 770 800 6499	0.005	1.0	0.040	0.005	0.005	3.920	0.010	
A001 800 853 6500	0.005	0.5	0.030	0.005	0.005	2.640	0.005	
A001 868 900 6501	0.005	1.0	0.040	0.005	0.005	2.400	0.005	
A001 900 930 6502	0.005	2.0	0.020	0.010	0.005	4.260	0.020	
A001 930 960 6503	0.005	0.5	0.020	0.005	0.005	3.400	0.030	
A001 960 977 6504	0.005	1.0	0.020	0.005	0.005	2.470	0.010	
A001 989 1020 6505	0.005	0.5	0.020	0.005	0.005	3.030	0.010	
A001 1020 1050 6506	0.005	0.5	0.020	0.005	0.010	3.130	0.005	
A001 1050 1079 6507	0.005	1.0	0.030	0.005	0.005	1.200	0.005	
A001 1091 1120 6508	0.020	1.0	0.020	0.005	0.005	1.380	0.005	
A001 1120 1150 6509	0.020	1.0	0.040	0.005	0.005	3.660	0.005	
A001 1150 1180 6510	0.005	0.5	0.030	0.005	0.005	4.140	0.005	
A001 1180 1210 6511	0.010	1.0	0.040	0.010	0.005	4.410	0.005	
A001 1210 1230 6512	0.020	1.0	0.010	0.005	0.005	6.490	0.005	
A001 1230 1250 6513	0.020	0.5	0.030	0.010	0.005	5.920	0.005	
A001 1288 1316 6514	0.005	0.5	0.020	0.005	0.005	4.510	0.005	
A001 1316 1346 6515	0.005	0.5	0.030	0.005	0.005	3.470	0.005	
A001 1388 1419 6516	0.005	0.5	0.020	0.005	0.005	1.980	0.005	
A001 1464 1490 6517	0.005	0.5	0.010	0.005	0.005	3.140	0.005	
A001 1490 1520 6518	0.005	0.5	0.020	0.010	0.005	2.850	0.005	
A001 1520 1547 6519	0.005	0.5	0.110	0.010	0.005	4.790	0.005	
A001 1547 1570 6520	0.005	0.5	0.140	0.010	0.005	4.040	0.030	

A001	1610	1640	6521	0.030	0.5	0.010	0.010	0.010	6.310	0.005
A001	1640	1664	6522	0.040	0.5	0.010	0.010	0.010	5.230	0.005
A001	1671	1700	6523	0.030	0.5	0.010	0.020	0.020	6.910	0.010
A001	1700	1730	6524	0.005	0.5	0.020	0.010	0.005	6.940	0.010
A001	1730	1760	6525	0.005	0.5	0.010	0.005	0.005	7.940	0.005
A001	1760	1790	6526	0.005	0.5	0.040	0.005	0.005	7.320	0.005
A001	1790	1820	6527	0.005	0.5	0.020	0.005	0.005	6.030	0.005
A001	1820	1850	6528	0.005	0.5	0.010	0.005	0.005	6.660	0.010
A001	1850	1875	6529	0.020	0.5	0.010	0.005	0.005	5.270	0.010
A001	1875	1897	6530	0.040	0.5	0.010	0.005	0.010	5.390	0.005
A001	1916	1945	6531	0.005	0.5	0.010	0.010	0.005	6.800	0.010
A001	1945	1973	6532	0.005	0.5	0.010	0.005	0.005	8.080	0.005
A001	1983	2010	6533	0.010	0.5	0.030	0.005	0.005	6.710	0.010
A001	2017	2050	6534	0.005	0.5	0.050	0.005	0.005	6.730	0.010
A001	2050	2080	6535	0.005	0.5	0.040	0.005	0.005	7.030	0.005
A001	2080	2110	6536	0.005	0.5	0.040	0.005	0.005	7.190	0.005
A001	2110	2140	6537	0.020	0.5	0.040	0.005	0.005	7.110	0.040
A001	2140	2170	6538	0.005	0.5	0.030	0.010	0.005	5.930	0.010
A001	2170	2195	6539	0.005	0.5	0.030	0.005	0.005	7.080	0.010
A001	2214	2240	6540	0.005	0.5	0.050	0.005	0.005	5.900	0.060
A001	2240	2270	6541	0.005	0.5	0.030	0.005	0.005	6.880	0.005
A001	2270	2300	6542	0.005	0.5	0.030	0.005	0.005	6.400	0.005
A001	2300	2330	6543	0.005	0.5	0.020	0.005	0.005	1.960	0.005
A001	2330	2360	6544	0.005	0.5	0.020	0.005	0.005	2.640	0.005
A001	2360	2390	6545	0.005	0.5	0.020	0.005	0.005	2.580	0.005
A001	2408	2440	6546	0.005	0.5	0.010	0.005	0.005	2.690	0.005
A001	2440	2470	6547	0.005	0.5	0.030	0.005	0.005	2.800	0.005
A001	2470	2500	6548	0.005	0.5	0.020	0.005	0.005	2.260	0.005
A001	2500	2530	6549	0.005	0.5	0.020	0.005	0.005	2.850	0.005
A001	2530	2560	6550	0.005	0.5	0.020	0.005	0.005	2.150	0.005
A001	2560	2580	6551	0.005	0.5	0.010	0.005	0.005	1.780	0.005
A001	2580	2609	6552	0.005	0.5	0.020	0.005	0.005	2.420	0.005

R

:END OF HOLE

R

END OF ASSAYS - END OF LOG

IDEN6B0201		X86CH255 NO	JUN DJH	G&D JUN8&S38	0.0		
IPRJ		EQUITY SILVER MINES LTD		TAILINGS POND ZONE - MZ	GEocode		
S000	00	628 MT	125.6 090.0 -45.0		9207.62	7891.48	1277.71
S001	628	1256	125.6 090.0 -45.0				
/SCL		MT.2MT.1					
LSCL		MT.2					
/NAM							
LNAM							QZSZTOPYCPTTASPR
/	00	223	OVBN	P			DMCBCLMGHESLGLMO
R			:TRICONED AND CASED (NO CORE). COLLARED ON DIVERSION DAM.				
/	223	282	59 4A13CL P* <<	P	<+	<+	
L			24 5G				
R			:WEAK << TEXTURE.				
/	282	292	08 2D55QZPY <<VU	P	+7	M2	
L			02 4A				
R			:2D ? - TOTALLY SILICIFIED				
/	292	383	91 4A13CL P* <<	P	<)	<+	
L			40 AG				
R			:TYPICAL 4A W/10-15% EUHEDRAL PLAG PHENOS :GOUGE & BROKEN				
R			& LOST CORE 29.2-31.6.				
/	383	419	36 8A10CL P*A*	P CU	080A+		
L			31 5G		CL 050 A+		
R			:2% AMYGDS :10% ALT'D (SAUSS) PLAG. PHENOS. TO 3 BY .5 MM.				
/	419	425	05 4A13CL <<P*	P	<)	<)	
L			AG				
R			:BXIA @ END OF INT. :AS ABOVE 29.2-38.3				
/	425	439	14 8CB0MS <<P*	P FB	074		
L			02 5T				
R			:GOUGE @ UPPER CNT. :DARK GREY ENVELOPES ON << :1% PHENOS TO				
R			.5 BY 1MM IN APHANITIC MATRIX.				
R			:NO SDES :LOWER CNT. NOT OBSERVED DUE TO LOST CORE :NOT TYPICAL				
R			BC (DARK GREY ENVS. ARE NOT TYPICAL IN THIS UNIT) :POSSIBLY 4B?				
/	439	483	44 4A13CL <<P*	P	<)	<+	
L			AG			<)<.	
R			:AS ABOVE 29.2-38.3				
/	483	506	15 8A10CLCY P*	P			
L			00 GB		CL 020		
R			:BLEACHED @ LOWER CNT. (0.3M) :15% EUHEDRAL, ALT'D(SAUSS + CY)				
R			PLAG. PHENOS. TO 5 BY 2 MM.				
R			:UPPER CNT. NOT OBSERVED DUE TO BROKEN CORE :CY GOUGE @ 50.3M				
/	506	678	172 4A13CL P* <<	P <<	025<)	<+	
L			128 AG			<)	
R			:WEAK PROPYLITIC ALT'N :AS ABOVE 29.2-38.3 :FAULT GOUGE & BXIA				
R			66.1-67.8				
R			:<<-PARALLEL TO FAULT @ 63.2M. :QZ+CB << X-CUT PY <<.				
/	678	690	12 8A10CL A*	P CU	020A=		
L			09 5G		CL 05/ A=		
R			:10% AMYGDS TO 4MM DIAMETER.				
/	690	747	57 4A13CL P* <<	P		<)	
L			29 AG BR				
R			:BXIA ZONE W/15% PY + 15% QZ + 5% GY + 15% CY (70.4-71.3)				
R			:GOUGE AT LOWER CNT.				
/	747	762	03 2D55QZPY <<	P	+7	M2	
L			00 4A				Q=
R			:AS ABOVE 28.2-29.2M :FG GREY SDE MINERAL(5%) :LOW RECOVERY				

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R           :COULD THIS BE A SULPHIDE RICH CHERTY UNIT OR IS IT REALLY A
R           SILICIFIED 2D :NO CNT'S OBSERVED DUE TO GOUGE & BROKEN CORE
R           (POSSIBLE BXIA ZONE).
/ 762 779 17 4A13CL <<P* P <+
L           04 AG
R           :10C. GOUGE ZONES (FAULT) :WEAK << TEXT.
/ 779 796 17 4B83MS <<P* P <+
L           02 BR
R           :PINKISH COLOR :LOCAL GOUGE ZONES :GRADATIONAL CONTACTS.
/ 796 836 37 4A13CL <<P* P <) <+
L           04 AG
R           :10C GOUGE ZONES : WEAK << TEXT
/ 825 825 X D2V1 035 V2
L           V7
/ 836 870 34 4B83MS <<P* P <) <+
L           17 BR
R           :GRADATIONAL CONTACTS :AS ABOVE 77.9-79.6M :WEAK << TEXT.
/ 870 914 44 4A13CL <<P* P <) <+
L           24 AG
R           :WEAK TO MODERATE << TEXT.
/ 914 954 40 4B83MS <<P* P <) <+
L           31 BR
R           :GRADATIONAL CNTS. :WEAK TO MOD. << TEXT
/ 954 970 16 4A13CL <<P* P <+
L           06 AG <<
R           :WEAK << TEXT
/ 970 983 13 4B83MS <<P* P <) <+
L           04 BR <<
R           :GRADATIONAL CNTS. :WEAK << TEXT.
/ 983 1025 42 4A13CL <<P* P <) <+
L           32 AG <)
R           :WEAK << TEXT
/ 1025 1039 14 4B83MS <<P* P << 048<+ <=
L           02 7T <<
R           :10C PINK COLOR :LOCAL GOUGE ZONES :GRADATIONAL CNTS.
/ 1039 1065 26 4A13CL <<P* P << <+
L           19 5G <<<
R           :WEAK << TEXT
/ 1065 1072 07 8A10CL P*<< P CU 080
L           05 AG CL 040 <.
R           :V. WEAK << TEXT
/ 1072 1086 14 4A13CL <<P* P <) <+
L           11 5G <<<
/ 1086 1100 14 4B83MS <<P* P <) <+
L           11 BR <<<
R           :GRAD. CNTS. :WEAK TO MOD. << TEXT
/ 1100 1161 61 4A13CL <<P* P << <)
L           56 5G <)
R           :WEAK << TEXT :V. LOCAL STRONG << TEXT
/ 1161 1190 29 4B83MS <<P* P <+ <+
L           07 BR <<
R           :TO 4A 10C :GRADATIONAL CNTS. :LOCAL GOUGE ZONES :WEAK << TEXT
/ 1190 1256 66 4A13CL <<P* P <+ <+
L           42 AG <<<
R           :TO 4B 10C :WEAK << TEXT

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R          :END OF HOLE @ 125.6 M.
A001      EQUITY MINESITE LABORATORY
ALAB      ASSAY
ATYP      WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AMTH      RCOVSAMPLE  RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
AUMM
R          0  223  TRI-CONE NO CORE
A001  223  250      6455      0.005  0.1 0.050  .005  .005  4.530  0.010
A001  250  282      6456      0.005  0.1 0.030  .010  .005  5.770  0.010
A001  282  292      6457      0.005  0.5 0.050  .020  .005  8.39  0.03
A001  292  320      6458      0.005  0.5 0.140  .010  .005 18.39  0.02
A001  320  350      6459      0.005  0.5 0.030  .010  .005  5.89  0.02
A001  350  383      6460      0.005  0.5 0.040  0.005  0.005  5.31  0.02
R          383  419  DYKE NO SAMPLE
A001  419  439      6461      0.005  0.5 0.040  0.005  0.005  2.58  0.01
A001  439  460      6462      0.005  0.5 0.040  0.005  0.005  5.28  0.01
A001  460  483      6463      0.005  0.5 0.200  0.005  0.005  4.57  0.01
R          483  506  DYKE NO SAMPLE
A001  506  530      6464      0.005  0.5 0.030  0.01  0.005  5.81  0.01
A001  530  560      6465      0.005  0.5 0.040  0.005  0.005  5.13  0.01
A001  560  590      6466      0.005  0.5 0.040  0.005  0.010  4.94  0.01
A001  590  620      6467      0.005  0.5 0.050  0.005  0.010  4.63  0.005
A001  620  650      6468      0.005  0.5 0.150  0.005  0.010  5.43  0.005
A001  650  678      6469      0.005  0.5 0.040  0.005  0.010  5.59  0.005
R          678  690  DYKE NO SAMPLE
A001  690  720      6470      0.005  0.5 0.030  0.005  0.005  7.44  0.020
A001  720  747      6471      0.005  0.5 0.040  0.005  0.005  6.57  0.010
A001  747  762      6472      0.070  28.0 0.100  0.02  0.010 13.91  1.490
A001  762  790      6473      0.005  0.5 0.040  0.005  0.01  5.23  0.020
A001  790  820      6474      0.020  25.0 0.060  0.01  0.02  6.57  0.020
A001  820  850      6475      0.090 109.0 0.070  0.040  0.040  6.72  0.280
A001  850  880      6476      0.005  0.5 0.050  0.005  0.005  5.35  0.020
A001  880  910      6477      0.005  0.5 0.040  0.01  0.01  5.05  0.005
A001  910  940      6478      0.005  0.5 0.030  0.005  0.005  5.64  0.005
A001  940  970      6479      0.005  0.5 0.030  0.005  0.005  4.82  0.005
A001  970 1000      6480      0.005  0.5 0.010  0.005  0.005  4.43  0.005
A001 1000 1030      6561      0.005  0.5 0.050  0.005  0.005  4.35  0.005
A001 1030 1065      6562      0.005  0.5 0.050  0.005  0.005  5.96  0.005
R          1065 1072  DYKE NO SAMPLE
A001 1072 1100      6563      0.005  0.5 0.050  0.005  0.005  4.45  0.005
A001 1100 1130      6564      0.005  0.5 0.010  0.005  0.005  4.26  0.005
A001 1130 1160      6565      0.005  0.5 0.020  0.005  0.005  4.85  0.005
A001 1160 1190      6566      0.005  0.5 0.050  0.005  0.005  4.49  0.005
A001 1190 1220      6567      0.005  0.1 0.040  0.005  0.005  5.01  0.005
A001 1220 1256      6568      0.005  0.1 0.05  0.005  0.005  4.87  0.005
R          END OF ASSAYS - END OF LOG

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IDEN6B0201		X86CH256 NO	JUN86DJH	G&D JUN86S38	0.0	
IPRJ		EQUITY SILVER MINES LTD		NORTH ZONE - MZ	GEocode	
S000	00	935 MT	124.1 082.0 -45.0		8926.94	8618.79 1276.97
S001	935	1241	124.1 082.0 -45.0			
/SCL		MT.2MT.1				
LSCL		MT.2				
/NAM						
LNAM						QZSZTOPYCPTTASPR
/	00	159	OVBN			DMCBCLMGHESLGLMO
R			:TRICONED - NO CORE			
/	159	172	13 2G10CL CT			
L			23 5G			
R			:ACTUALLY CLASTS ARE GRANULE SIZE W/OCC. PEBBLES.			
/	172	201	29 8A10CL A*		P CU	015A)
L			23 5G		CL	080 A)
R			:CLAY SEAM @ 18.3M (FAULT?).			
/	201	221	20 2D10CL			
L			04 5A			
R			:2G @ 20.9M (UPPER CNT. 45degs - LOWER 70degs) :NO SDES.			
/	221	233	12 2E10CL			
L			00 AG			
R			:DARK GREY GREEN COLOR :LOCAL GOUGE & BXIA ZONES :NO SDES.			
/	233	286	53 8C80MS FB		P CU	040
L			49 9G			
R			:GOUGE @ UPPER & LOWER CNTS.			
/	286	337	51 2C10CL		P BD	050
L			23 4A			
R			:20% INTERBEDDED 2G :LOCAL GOUGE ZONES :DARK GREY GREEN COLOR			
/	337	363	26 2H14CL			Q*
L			03 5G			
R			:SANDY MATRIX			
/	363	449	86 8A10CL P*			
L			4G		CL	030 D.
R			:BROKEN UP CORE @ UPPER CNT :20% FLAG PHENOS (LATHS 10 X 2 MM)			
R			:MINOR GOUGE @ LOWER CNT			
/	449	461	12 2D10CL <<			
L			00 AG			<>
/	461	480	19 2H10CL <<		P BD	035<. <.
L			04 5G			<.
R			:V WEAK << TEXT :40% 2G INTERLEVED (GRAD CNTS)			
R			:CLASTS ARE 2 - 20 MM			
/	480	493	11 2C13CL <<			<+
L			03 AG			<+
R			:MOD << TEXT			
/	493	524	31 2H10CL			
L			05 5G			
R			:GRAD UPPER CNT :MINOR 2CD INTERLEVED :NO SDES			
R			:MINOR 2E INTERLEVED ALSO			
/	524	550	26 8A10CL P*			
L			02 6G			
R			:10% FLAG PHENOS TO 10 X 2 MM :CNTS NOT OBSERVED DUE TO BROKEN			
R			:CORE AND GOUGE			
/	550	594	42 2G13CL <<BD		P BD	045<(<)
L			12 4G			<<
R			:WEAK << TEXT :15% INTERLEVED 2H AND 10% INTERLEVED 2D			

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/ 594 641 47 2G13CL <<BD P BD 050 <
L 28 4A <.
R :V WEAK << TEXT :TD 2C LOCALLY (10%)
/ 641 649 08 2H10CL P
L 06 5G
R :PALE GREEN & GREY VOLC CLASTS
/ 649 659 10 2G10CL P
L 02 AG
R :W/10% INTERLEVED 2C
/ 659 669 10 8A10CL P* P
L 06 AG
R :LIGHT GREY/GREEN COLOR :NO CNT ATTITUDE OBSERVED
R :NOT LIKE TYPICAL 8A (PYROX PHENOS)
/ 669 678 09 2D10CL << P <<
L 07 AG <<
R :TD 2E LOC :V WEAK << TEXT
/ 678 704 26 8A10CL P* P
L 22 GA CL 045
R :AS ABOVE 65.9 - 66.9 :UPPER CNT IRREGULAR
R :25% PLAG PHENOS TO 10 X 3 MM :5% PYROX PHENOS
/ 704 788 84 2G10CL <<BD P BD 045 <<
L 07 GA <<
R :V WEAK << TEXT :2% INTERLEVED 2H
/ 788 807 19 8A10CL P* P
L 14 6G
R :15% PLAG PHENOS TO 10 X 2 MM :TYPICAL 8A :UPPER CNT NOT
R :OBSERVED DUE TO MISSING CORE
R :LOWER CNT NOT OBSERVED
/ 807 850 32 2G10CL BD<< P BD 050<<
L 04 GA <<
R :LOST CORE 81.1 - 84.1 = 1.4 M CORE :15% INTERLEVED 2H
R :V WEAK << W/QZ + CB
/ 850 863 13 2H110CL P
L 08 AG
R :ROUNDED VOLC CLASTS TO 30 MM (SOME PORPHYRITIC) :NO SDES
/ 863 875 12 2G13CL << P <
L 00 GA <
R :NO BEDDING :V WEAK << TEXT
/ 875 916 41 2H13CL << P << <.
L 22 AG <.
R :V WEAK << TEXT PY ALSO AS PATCHES (1%) IN MATRIX
/ 916 954 38 2G10CL BD P BD 032
L 18 GA
R :MINOR 2H INTERLEVED :NO SDES
/ 954 1007 53 2H10CL << P <.
L 28 AG <
R :V WEAK << TEXT MAINLY CB
/ 1007 1019 12 2G10CL BD P BD 030 <.
L 04 GA
/ 1019 1035 16 2H10CL << P
L 11 AG <
R :V WEAK << TEXT
/ 1035 1043 08 2G10CL BD P BD 035
L 00 GA
R :AS ABOVE 100.7 - 101.9 ; 91.6 - 95.4

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/ 1043 1108 64 2H13CL << P <
L 46 AG < <
R :ONE << W/ PY + SL? (REST ARE CB) :GRANULES TO PEBBLES
/ 1108 1139 31 2E10CL << P *
L 17 GA <
R :V DISTINCTIVE UNIT W/ LIGHT GREEN LAPILLI FRAGS IN A GREY
R :ASH MATRIX :SOME FRAGS ARE WELL ROUNDED
R :MARKER UNIT?? :V WEAK << TEXT
/ 1139 1160 20 2H10CL << P
L 15 AG <
R :V WEAK << TEXT W/CB ONLY
/ 1160 1168 08 2G10CL BD P BD 031
L 05 GA
R :AS ABOVE 103.5 - 104.3 M
/ 1168 1200 32 2H10CL << P
L 11 AG <*
R :UPPER CNT GRADATIONAL :LOWER CNT WEAKLY GRADATIONAL
/ 1200 1219 19 2E10CL << P
L 09 GA <*
R :AS ABOVE 110.8 - 113.9 M
/ 1219 1241 22 2H13CL << P <*
L 11 AG <
R :WEAK TO MOD << TEXT
R :EOH @ 124.1 M
R :HOLE ABANDONED DUUE TO CAVING

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A001
ALAB
ATYP
AMTH
AUMM

EQUITY MINESITE LABORATORY
ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCDVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN	
R	00	159	:TRICONED - NO CORE							
A001	159	172	6569	0.005	0.1	0.030	0.005	0.005	5.180	0.005
R	172	201	DYKE NO SAMPLE							
A001	201	233	6570	0.005	0.5	0.030	0.005	0.005	4.45	0.005
R	233	286	DYKE NO SAMPLE							
A001	286	310	6571	0.010	0.5	0.050	0.005	0.005	5.19	0.010
A001	310	340	6572	0.005	0.5	0.030	0.005	0.005	5.000	0.005
A001	340	363	6573	0.005	0.5	0.030	0.005	0.005	5.440	0.005
R	363	449	DYKE NO SAMPLE							
A001	449	480	6574	0.005	0.1	0.050	0.005	0.005	4.360	0.005
A001	480	510	6575	0.005	0.1	0.020	0.005	0.005	4.840	0.005
A001	510	524	6576	0.005	0.1	0.030	0.005	0.005	6.330	0.005
R	524	550	DYKE NO SAMPLE							
A001	550	580	6577	0.005	0.5	0.060	0.005	0.005	4.860	0.005
A001	580	610	6578	0.005	0.5	0.030	0.005	0.005	5.240	0.005
A001	610	640	6579	0.005	0.5	0.020	0.005	0.005	4.470	0.005
A001	640	678	6580	0.005	0.5	0.020	0.005	0.005	3.640	0.005
R	678	704	DYKE NO SAMPLE							
A001	704	730	6581	0.005	0.5	0.030	0.005	0.005	4.310	0.005
A001	730	760	6582	0.005	0.5	0.030	0.005	0.005	3.820	0.005
A001	760	788	6583	0.005	0.5	0.030	0.005	0.005	3.710	0.010
R	788	807	DYKE NO SAMPLE							
A001	807	840	6584	0.005	0.5	0.040	0.005	0.005	3.640	0.005
A001	840	870	6585	0.005	0.5	0.040	0.005	0.005	4.650	0.010
A001	870	900	6586	0.005	0.5	0.030	0.005	0.005	4.510	0.010

A001	900	930	6587	0.005	0.5	0.020	0.005	0.005	4.030	0.020
A001	930	960	6588	0.005	0.5	0.005	0.005	0.005	3.300	0.010
A001	960	990	6589	0.005	0.5	0.020	0.005	0.005	4.450	0.010
A001	990	1020	6590	0.005	0.5	0.030	0.005	0.005	4.070	0.040
A001	1020	1050	6591	0.005	0.5	0.020	0.005	0.005	3.220	0.020
A001	1050	1080	6592	0.005	0.5	0.020	0.005	0.005	5.370	0.050
A001	1080	1110	6593	0.005	0.5	0.030	0.005	0.005	4.590	0.020
A001	1110	1140	6594	0.005	0.5	0.020	0.005	0.005	2.800	0.010
A001	1140	1170	6595	0.005	0.5	0.040	0.005	0.005	3.730	0.010
A001	1170	1200	6596	0.005	0.5	0.030	0.005	0.005	4.750	0.010
A001	1200	1241	6597	0.005	0.5	0.020	0.005	0.005	3.650	0.010

R

:EDH @ 124.1 M

R

END OF ASSAYS - END OF LOG

IDEN6B0201			X86CH257 NQ 30JUN86RBP	G&D JUN86S38		0.0		
IPRJ			EQUITY SILVER MINES LTD			NORTH ZONE - MZ	GEocode	
S000	00	467	MT 291.4	090.0	-45.0		9122.23	8655.75 1275.95
S001	467	1381		291.4	090.0 -43.0			
S002	1381	2286		291.4	090.0 -46.0			
S003	2286	2914		291.4	090.0 -41.0			
/SCL			MT.2	MT.1				
LSCL			MT.2					
/NAM								
LNAM								
/	00	137		OVBN				
R				CASED TO 13.7 M.				
/	137	168	25	2CB1	<<			
L			00	8A				<)
R				CORE IS VERY BROKEN.				
/	168	225	50	2CB1	<<		<)	<+D.
L			03	2A				
R				:CORE STILL VERY BROKEN				
/	225	244	18	2GB0	<<G;	P BD	60<*	
L			05	6A				
R				:ABUNDENT GLASS SHARDS				
/	244	264	19	8B00FL	TCCM	P CL	40<*	
L			05	7A				
R				:UPPER CONTACT MAYBE FAULTED				
/	264	301	35	2H81	<<	P		<)
L			11	6A				
R				:WELL-ROUNDED CLASTS UP TO 2.0 CM. SOME SHARDS				
R				:MAINLY TUFF FRAG				
/	301	328	26	2GB1	<<G;	P BD	55<)	<)
L			08	2A				
R				:BEDS DISRUPTURED				
/	328	393	60	2H81	<<G;	P BD	55<)	<(*-
L			39	6A				
R				:VERY SIMILAR TO 2H FROM 26.4 TO 30.1 ONE CLAST OF CP AT 37.0				
/	393	506	102	2GB0	<<G;	P BD	40<*	<-
L			00	1A				
R				:SOFT, CORE VERY BROKEN, MINOR THIN < 0.2 M BEDS OF 2C + 2H				
R				:SOME OF UNIT VERY FINE GRAINED TO SILTSTONE				
/	506	566	58	2H80	<<G;	P BD	60<-	B.
L			17	8G				B-
R				:GRAIN SIZE INCREASES TOWARDS BOTTOM OF INTERVAL CLASTS ARE				
R				:MAINLY 2C. CLASTS UP TO 4.0 CM				
/	566	597	28	2E80	<<	P		<)
L			03	2A				
R				:ABUNDENT GLASS SHARDS. CORE VERY BROKEN				
/	597	622	24	2A80	<<	P BN	40<*	
L			03	2A		FL		
R				:INTERVAL ENDS IN FAULT GOUGE				
/	622	670	45	2CB1	<<	P	<)	<<<.
L			03	1A				<<
R				:MINOR LAPILLI, GLASS SHARDS. CORE VERY BROKEN.				
R				:MINOR CP AT 63.2 M				
/	670	683	13	2H80	<<	P CU	50<)	
L			06	3G		CL	60	
/	683	711	27	2GB0	<<	P BD	65<+	

L 05 2A
 R :SOME THIN INTERBEDS OF 2H
 / 711 718 07 2H80 << P BD 60<*<
 L 05 3G
 / 718 780 69 2680 <<<< P < <.
 L 21 1A <.
 / 780 799 18 2681 << P <*< <)
 L 00 1A <.
 R :SAME ROCK AS INTERVAL ABOVE, BUT PY
 / 799 841 40 2H81 << P BD 55<*< <)
 L 03 8A
 R :MINOR 2G INTERBEDDED. FRAG OF 2C + VOLC SHARDS.
 R :FRAG UP TO 4.0 CM
 R :FAULT GOUGE AT 83.5
 / 841 890 47 8C00 FB P BN 50
 L 09 7Y
 R :CONTACT ZONE OF DYKE, SLIGHTLY BX'D AND FLOW BANDED.
 R :TYPICAL 8C
 / 890 1038 145 8C00FL P
 L 85 9A P* D+
 R :TYPICAL 8C
 / 1038 1095 55 8C00FL P* P
 L 29 8Y D+
 / 1095 1195 97 8C00 FBP* P
 L 59 8Y D*
 / 1195 1310 112 8C00 P* P
 L 68 8Y D(
 / 1310 1350 39 8C00 FBP* P
 L 21 8Y D*
 / 1350 1453 100 8C00 P* P
 L 60 8Y D(
 / 1453 1477 23 8C00 P*FB P BN 55
 L 09 7T BR<< D*
 R :LOWER CONTACT ZONE
 / 1477 1517 38 2F81 <<BR P < <+
 L 09 6A
 R :SOME FRAG ALT'N TO SERICITE. FRAG UP TO 5.0 CM
 / 1517 1560 42 2F81 <<BR P BN 40 <+
 L 16 8G <)
 R :FRAG UP TO 6.0 CM. MANY FRAG WELL ROUNDED
 / 1560 1586 25 2H81 << P B+
 L 09 7A <-
 R :CONGLOMERATE DISRUPTED TO PY, FRACTURING
 / 1586 1600 14 2F81 P B)
 L 09 9G <*<
 R :VERY STRANGE ROCK! MASSIVE, DYKE-LIKE
 / 1600 1621 21 2K51 FBER P <(< B*
 L 13 2A
 R :MUD FLOW.
 / 1621 1655 33 2H51 << P BD 30 <)
 L 24 4A <*<
 R :ABUNDENT SHARDS. TUFF FRAGMENTS, SERICITE ALT'N (FRAG)
 / 1655 1687 31 2H81 << P <*< <)
 L 6G <*<
 R :VERY COURSE, CLASTS UP TO 10.0 CM

/ 1687 1698 11 2G01 << P BD 40< <*
L 09 3G
/ 1698 1734 35 2H81 << P < <+
L 21 6G <-
R :SAME AS 165.5 TO 168.7 ABOVE
/ 1734 1756 22 2H81 << P <* B=
L 06 9A
R :PYRITE RIMS FRAG
/ 1756 1783 26 2H81 <<BR P < <+
L 09 6G <<
R :CLASTS DISRUPTED, BR'D. PY-HE VEIN AT 177.2
/ 1783 1827 53 2C81 << P <* <
L 21 5A <
R :CONTAINS SOME LAPILLI, SHARDS.
/ 1827 1846 17 2D81 P F/ < <+
L 00
R :SERICITE-CLAY-PYRITE GOUGE COMMON, VERY BROKEN CORE.
/ 1846 1868 21 2H81 << P < <+ <<
L 11 4A <-<>
R :SOME SHARDS, MORE AND COARSER CLASTS AT BOTTOM OF INTERVAL.
R :SOME MINERAL
/ 1868 1902 33 2G81 << P BD 35< <+<.*
L 15 4A <
R :FEW CONGLOMERATE SIZE CLASTS, SHARDS, MORE MINERAL
/ 1902 1955 51 2H81 << P < <+
L 21 6G <<<.
R :TYPICAL LARGE CLAST CONGLOMERATE
/ 1955 1970 15 8B00FL TC P CU 20
L 05 8G CL 35
/ 1970 2050 75 2H81 << P < <<<.
L 30 4G <*
R :POOR RECOVERY FROM 203.5 TO 205.0
/ 2050 2080 30 2EB3MS <<WD P BN 055 <<
L 19 6T <
R :MOD << TEXT (RETIC) :~10% LAPILLI :LOWER CNT GRADATIONAL
R :UPPER CNT SHARP BUT NO ANGLE DUE TO MISSING CORE
/ 2080 2093 13 2H11CL << P << D<
L 08 6A <<
R :50% MATRIX SUPPORTED GREEN ANDESITE CLASTS IN A MED GREY
R :SANDY MATRIX :V WEAK << TEXT
/ 2093 2144 51 3K03CY BD<< P BD 055<< <<
L 19 4A << <<
R :UNITS ABOVE MAYBE BELONG TO UNIT 3 ALSO (LOTS OF CONGLOM &
R :SANDSTONE W/ MINOR PYROCLASTICS)
R :HETEROLITHIC INT W/20% INTERLEVED 2H, & 30% 2G (IE- TRANSITION
R :FROM COARSE TO FINE CLASTICS)
R :GENERALLY WEAK << TEXT :GRAD LOWER CNT
/ 2144 2282 126 3K03CY << P < <.
L 52 4A <
R :W/5% INTERLEVED 2G & 2H COMBINED :MOD << TEXT
R :LOCAL ZONES OF GOUGE & HEAVILY BROKEN CORE
/ 2282 2334 50 8A13CL <<P* P CU 070< <*
L 48 5G CL 065 <<
R :PRE-MINERAL DYKE :10% PLAG PHENOS (4 X 2 MM) :CNTS SHARP AND
R :CHILLED


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/ 2334 2350 15 3K03CY << P << <<
L 4A <<
R :WEAK TO MOD << TEXT
/ 2350 2363 13 BA10CL <<A* P CU 042<)
L 11 6G P* CL 033 <)
R :WEAK << TEXT :10% AMYGDS :NO SDES BUT DOESN'T LOOK LIKE
R :POST-MIN DYKE
/ 2363 2375 12 3K03CY << P << <=
L 08 4A <<
R :MOD TO INTENSE << TEXT
/ 2375 2418 41 BA10CL P* << P FB 061<<
L 36 AG FB CL 074 <<
R :UPPER CNT NOT OBSERVED DUE TO MISSING CORE :V WEAK << TEXT
R :POST-MIN DYKE
/ 2418 2425 07 3K03CY << P << <=
L 00 4A <<
R :TD 3E LOC :CLAY GOUGE @ 242.3 M
/ 2425 2460 23 BC80MS P* << P CU 080<<
L 19 6T <<
R :V WEAK << TEXT :TYPICAL LATITE DYKE :LOWER CNT V IRREGULAR
R :(POSSIBLE XENOLITHS)
/ 2460 2480 19 BC80MS P* << P <<
L 12 6T CL 035 <<
R :AS ABOVE W/20% 3K XENOLITHS
/ 2480 2510 30 3K03CY << P << <)
L 17 4A <<
R :HETEROLITHIC INT W/ 3D & 3E INTERLEVED :LATITE DYKE
R :250.6 - 251.0 (STEEP CONTACTS) :WEAK << TEXT
/ 2510 2563 52 3K43QZ << P << <1<) <)
L 4A
R :MOD << TEXT :HETEROLITHIC INT AS ABOVE W/ 3D & 3E
/ 2563 2572 09 BA13CL <<P* P <+ <)
L 07 6G
R :WEAK << TEXT :PRE-MIN DYKE :CNTS IRREG -NO ATTITUDES
R :MEASURABLE
/ 2572 2589 17 3K43QZ << P <=
L 12 4A
R :MOD TO WEAK << TEXT (DECREASING TOWARD EOI :PY ALSO
R :DECREASING TOWARDS EOI
R :HETEROLITHIC INT AS ABOVE 251.0 - 256.3 M W/ 3D & 3E
/ 2589 2602 13 BA10CL A*P* P CU 045<) <<
L 11 6G << CL 050
/ 2602 2612 10 3K03CY << P <) <)
L 04 4A
R :WEAK << TEXT :MOD << TOWARDS EOI
/ 2612 2622 10 3K43QZ << P <+ <2<= <=
L 08 4A <+
R :MOD TO STRONG << TEXT
/ 2622 2652 30 3E03CY BD<< P BD 055<< <)
L 06 4A
R :WEAK << TEXT :HETEROLITHIC INT W/ INTERBEDDED 3D & 3K
/ 2652 2670 18 3K03CY << P << <1
L 03 4A CL 048
R :GRAD UPPER CNT -FAULTED LOWER CNT :MOD TO STRONG << TEXT
R :MINOR BXIA

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/ 2670 2703 33 3E00CY <<BD P BD 065<<
L 24 4A <<
R :V WEAK << TEXT :HETEROLITHIC INT W/ 3K & 3D INTERLEVED
/ 2703 2753 49 3D10CL << P << (*)
L 38 4G <<
R :GRADES LOC TO 3E :NO EPIGENETIC PY :V WEAK << TEXT
/ 2753 2764 11 3E00CY << P << <.
L 04 4A <<
R :TO 3K LOC :V WEAK << TEXT :UPPER CNT GRADATIONAL (WEAKLY)
/ 2764 2778 13 8A10CL A*<< P <<
L 08 5G CL 075 <<
R :V WEAK << TEXT :UPPER CNT IRREGULAR
/ 2778 2863 75 3E00CYGR <<BD P <.
L 37 4A << <>
R :3D 277.9 - 278.7 :V WEAK << TEXT :TO 3K LOC
R :IRREG BEDDING -NO ATTITUDE :LOCALLY GRAPHITIC
/ 2863 2880 17 3E80MS <<BD P BD 025
L 08 7G <+
R :MOD << TEXT :MINOR PY IN PEBBLE DYKES
/ 2880 2901 19 8A10CLCB <<P* P CU 055<<
L 16 5G CL 070 <>
/ 2901 2914 13 3E03CY << P << <<
L 00 4A <<
R :WEAK << TEXT :OCC PEBBLE SIZED CLASTS (SOME W/ PY)
R :3E80 290.1 - 290.4
R :EDH @ 291.4 M

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A001
ALAB
ATYP
AMTH
AUMM

EQUITY MINESITE LABORATORY
ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCOV	SAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001	137	170	6553	0.005	0.5	0.030	0.005	0.005	10.220	0.005
A001	170	200	6554	0.005	0.5	0.04	0.005	0.005	8.98	0.005
A001	200	220	6555	0.005	0.1	0.04	0.005	0.005	4.430	0.005
A001	220	244	6556	0.01	0.1	0.05	0.005	0.005	6.340	0.01
A001	264	290	6557	0.01	0.1	0.04	0.005	0.005	8.99	0.01
A001	290	320	6558	0.005	0.5	0.02	0.005	0.005	5.67	0.005
A001	320	350	6559	0.005	0.1	0.04	0.005	0.005	6.83	0.005
A001	350	380	6560	0.005	0.1	0.04	0.005	0.005	5.49	0.005
A001	380	420	6601	0.005	0.5	0.02	0.005	0.005	5.79	0.03
A001	420	450	6602	0.005	0.5	0.04	0.005	0.005	5.63	0.01
A001	450	480	6603	0.005	0.5	0.06	0.005	0.005	4.59	0.01
A001	480	510	6604	0.005	0.5	0.04	0.005	0.005	4.56	0.01
A001	510	540	6605	0.005	2.0	0.03	0.005	0.001	6.26	0.04
A001	540	570	6606	0.005	1.0	0.02	0.005	0.001	6.55	0.03
A001	570	600	6607	0.005	0.5	0.02	0.005	0.001	5.03	0.005
A001	600	630	6608	0.005	1.0	0.04	0.005	0.001	4.52	0.005
A001	630	660	6609	0.02	1.0	0.03	0.005	0.001	4.45	0.005
A001	660	690	6610	0.005	2.0	0.03	0.005	0.001	5.89	0.04
A001	690	720	6611	0.005	1.0	0.03	0.005	0.001	5.78	0.005
A001	720	750	6612	0.005	1.0	0.05	0.005	0.001	4.28	0.005
A001	750	780	6613	0.005	0.5	0.03	0.005	0.001	5.44	0.005
A001	780	810	6614	0.005	2.0	0.03	0.005	0.001	3.19	0.005
A001	810	841	6615	0.005	4.0	0.02	0.005	0.001	2.14	0.005
A001	1477	1510	6616	0.005	2.0	0.02	0.005	0.001	5.55	0.02

A001	1510	1540	6617	0.005	1.0	0.01	0.005	0.001	6.43	0.005
A001	1540	1570	6618	0.005	0.5	0.01	0.005	0.001	6.44	0.005
A001	1570	1600	6619	0.005	1.0	0.02	0.005	0.001	6.43	0.02
A001	1600	1630	6620	0.02	1.0	0.01	0.005	0.001	6.42	0.02
A001	1630	1660	6621	0.005	0.5	0.01	0.005	0.001	6.15	0.03
A001	1660	1690	6622	0.005	0.5	0.01	0.005	0.001	6.46	0.02
A001	1690	1720	6623	0.005	0.5	0.04	0.005	0.001	6.56	0.01
A001	1720	1750	6624	0.005	3.0	0.04	0.005	0.001	10.99	0.005
A001	1750	1780	6625	0.005	2.0	0.02	0.005	0.001	9.83	0.01
A001	1780	1810	6626	0.005	1.0	0.02	0.005	0.001	3.77	0.02
A001	1810	1840	6627	0.005	6.0	0.02	0.005	0.001	11.22	0.10
A001	1840	1870	6628	0.005	6.0	0.03	0.005	0.001	9.04	0.06
A001	1870	1900	6629	0.005	4.0	0.01	0.005	0.001	5.37	0.33
A001	1900	1930	6630	0.005	6.0	0.03	0.005	0.001	8.35	0.03
A001	1930	1960	6631	0.005	1.0	0.01	0.005	0.001	6.21	0.02
A001	1960	1990	6632	0.005	0.5	0.02	0.005	0.001	5.91	0.01
A001	1990	2020	6633	0.005	0.5	0.01	0.005	0.001	5.82	0.03
A001	2020	2050	6634	0.005	0.5	0.01	0.005	0.001	4.81	0.03
A001	2050	2080	6635	0.005	0.5	0.01	0.005	0.001	3.40	0.05
A001	2080	2110	6636	0.005	12.0	0.04	0.005	0.001	5.49	0.05
A001	2110	2140	6637	0.005	1.0	0.03	0.005	0.001	6.64	0.02
A001	2140	2170	6638	0.005	0.5	0.02	0.005	0.001	5.27	0.01
A001	2170	2200	6639	0.005	0.5	0.03	0.005	0.001	4.15	0.005
A001	2200	2230	6640	0.01	1.0	0.03	0.005	0.001	5.96	0.005
A001	2230	2260	6641	0.005	0.5	0.02	0.005	0.001	4.20	0.005
A001	2260	2282	6642	0.02	3.0	0.03	0.005	0.04	6.55	0.01
A001	2282	2304	6652	0.005	1.0	0.01	0.005	0.001	7.91	0.09
A001	2304	2334	6653	0.030	2.0	0.01	0.005	0.001	8.29	0.04
A001	2334	2350	6643	0.02	0.5	0.03	0.005	0.001	5.33	0.02
A001	2350	2363	6644	0.005	1.0	0.02	0.005	0.001	3.26	0.02
A001	2363	2375	6645	0.01	1.0	0.01	0.005	0.001	5.20	0.14
R	2375	2418	DYKE NO SAMPLE							
A001	2418	2425	6646	0.050	52.0	0.06	0.020	0.080	5.24	0.06
R	2425	2460	DYKE NO SAMPLE							
A001	2460	2480	6447	0.001	0.5	0.04	0.005	0.001	6.11	0.005
A001	2480	2510	6448	0.030	2.0	0.04	0.005	0.440	7.66	0.005
A001	2510	2540	6449	0.001	0.1	0.02	0.001	0.001	3.88	0.005
A001	2540	2572	6650	0.030	7.0	0.40	0.005	0.730	8.46	0.090
A001	2572	2589	6651	0.005	8.0	0.07	0.005	0.120	6.99	0.050
R	2589	2602	DYKE NO SAMPLE							
A001	2602	2612	6654	0.005	11.0	0.13	0.005	0.050	4.13	0.080
A001	2612	2622	6655	4.200	2410.0	2.50	2.300	7.100	15.80	1.100
A001	2622	2650	6656	0.001	2.0	0.02	0.005	0.030	3.43	0.060
A001	2650	2670	6657	0.001	11.0	0.04	0.005	0.080	8.71	0.040
A001	2670	2700	6658	0.001	0.5	0.01	0.005	0.001	5.32	0.005
A001	2700	2730	6659	0.001	0.5	0.01	0.005	0.001	4.44	0.140
A001	2730	2764	6660	0.001	3.0	0.04	0.005	0.001	4.98	0.040
R	2764	2778	DYKE NO SAMPLE							
A001	2778	2810	6661	0.001	0.5	0.005	0.001	0.001	3.86	0.005
A001	2810	2840	6662	0.001	2.0	0.010	0.001	0.001	4.95	0.005
A001	2840	2863	6663	0.001	0.5	0.060	0.001	0.001	4.94	0.005
A001	2863	2880	6664	0.001	0.5	0.010	0.001	0.001	5.00	0.020
R	2880	2901	DYKE NO SAMPLE							
A001	2901	2914	6665	0.005	2.0	0.030	0.005	0.001	4.82	0.290
R			END OF ASSAYS-END OF HOLE							

IDEN6B0201				XB6CH258 NO	JUL86DJH	G&D JUL86S38	0.0
IPRJ				EQUITY SILVER MINES LTD		NORTH ZONE - MZ	GEOCODE
S000	00	488	MT	190.2	090.0	-45.0	9337.14 8666.04 1275.95
S001	488	1411		190.2	090.0	-43.0	
S002	1411	1902		190.2	090.0	-44.0	
/SCL				MT.2	MT.1		
LSCL				MT.2			
/NAM							QZSZTOPYCPTTASPR
LNAM							DMCBCLMGHESLGLMO
/	00	195			OVBN		P
R					:TRICONED -NO CORE		
/	195	202	07	BA10	CLCY	P*	P
L			00		5G		
R					:V HEAVILY BROKEN UP CORE :NO LOWER CNT OBSERVED DUE TO		
R					:BROKEN CORE		
/	202	251	16	3E13	CYCL	<<	P << <<
L			00		AG		<<
R					:V HEAVILY BROKEN UP CORE W/ CY GOUGE -POSSIBLE FAULT ZONE		
R					:V WEAK << TEXT		
/	251	285	20	BA10	CLCY	P*	P
L			00		5G		
R					:V HEAVILY BROKEN UP CORE W/CY GOUGE :NO CNTS OBSERVED		
/	285	332	31	3K13	CLCY	<<	P <)
L			00		4A		
R					:10% 3E INTERLEVED :V HEAVILY BROKEN UP CORE W/OCC CY GOUGE		
R					:SHARP, IRREGULAR LOWER CNT (NO ATTITUDE MEASURED)		
/	332	347	15	3E14	CL	<<	P Q=
L			00		AG		
R					:50% CY GOUGE (FAULT ZONE?) :V WEAK << TEXT W/ PY ONLY		
R					:DIFFICULT TO LOCATE LOWER CNT DUE TO GOUGE		
/	347	412	55	3K11	CLCY		P D.
L			00		4A		
R					:HEAVILY BROKEN UP CORE W/ CY GOUGE :LOWER CNT NOT OBSERVED		
R					:DUE TO BROKEN UP CORE :NO << TEXT		
/	412	445	33	3D13	CL	<<	P <<
L			27		GA		
R					:PEBBLE CONGLOM W/ 3E LOCALLY INTERLEVED :FAIRLY COMPETENT CORE		
R					:V WEAK << TEXT		
R					:LOWER CNT NOT OBSERVED DUE TO BROKEN & MISSING CORE		
/	445	456	11	3K00	CY	<<	P
L			00		4A		
R					:HEAVILY BROKEN UP CORE W/ MINOR CY GOUGE :V WEAK << TEXT W/GY		
R					:LOWER CNT NOT OBSERVED		
/	456	472	16	3E13	CL	<<ST	P ST 035<< <<
L			12		AG		<<
R					:V WEAK << TEXT :STREAKY TEXT (RELATED TO BEDDING?) -ST		
R					:NO LOWER CNT OBSERVED		
/	472	527	47	3K13	CLCY	<<	P << <<
L			00		GA		<
R					:V WEAK << TEXT :HEAVILY BROKEN UP CORE W/O CY GOUGE		
R					:LOWER CNT NOT OBSERVED		
/	527	532	04	3E10	CL	<<	P <<
L			00		GA		<<
R					:V WEAK << TEXT W/HF ONLY :LOWER CNT NOT OBSERVED		
/	532	591	44	3K13	CLCY	<<	P << <<

L 63 GA CL 052 <<
 R :WEAK << TEXT :TO 3D44 LOC W/15% PY IN PATCHES
 R :NOTE -PROPYLITIC ALT'N IS CONFINED TO CLASTS AND NOT RELATED
 R :TO << (PROBABLY SHOULD CALL THESE ROCKS 3D03 :LOWER CNT IS
 R :VERY SHARP
 / 1147 1160 13 3K03CY << P << <<
 L 08 5A <<
 R :V WEAK << TEXT :LOWER CNT GRADATIONAL
 / 1160 1173 13 3E13CL << P << <<
 L 09 GA <<
 R :V WEAK << TEXT :LOWER CNT IS GRADATIONAL
 / 1173 1258 84 3D13CL << P << <<
 L 65 GA <<
 R :AS ABOVE 107.4 - 114.7 M :V WEAK << TEXT :TO 3D44 LOC W/10-15%
 R :PY IN PATCHES
 R :OCC DARK GREY TO BLACK SILICEOUS MATRIX
 / 1258 1365 107 3E13CL <<BD P BD 035<< <<
 L 65 AG <<
 R :V WEAK << TEXT :MINOR 3K @ START OF INT
 / 1365 1379 13 8A10CL A* P CU 039A)
 L 08 AG A)
 R :LOWER CNT NOT OBSERVED
 / 1379 1398 18 8C80MS P* P
 L 00 6T
 R :QZ PHENOS TO 3 MM :LOWER CNT NOT OBSERVED DUE TO BROKEN CORE
 / 1398 1412 14 8A10CL A*<< P <<
 L 03 AG CL 068
 R :3% AMYGDS W/QZ :LOWER CNT IRREGULAR
 / 1412 1829 417 8C80MS P* P
 L 254 6T
 R :TYPICAL LATITE DYKE :5% SAUSSURITIZED FLAG PHENOS (4 X 1 MM)
 R :LOWER CNT GRADATIONAL
 / 1829 1847 17 8C80MSCL <<F* P
 L 00 6T << <<
 R :WEAK TO MOD << TEXT :LOWER CNT NOT OBSERVED :UNUSUAL BC
 R : (CONTAINS <<)
 / 1847 1856 06 3F80MS << P
 L 00 6T <+
 R :MOD << TEXT :LOWER CNT NOT OBSERVED
 / 1856 1884 28 8A10CLCY << P <<
 L 00 GA <<
 R :V WEAK << TEXT :LOWER CNT NOT OBSERVED
 / 1884 1902 17 7D10 <<P* P <<
 L 04 4A <<
 R :V WEAK << TEXT :V WEAK P* TEXT
 R :EDH @ 190.2 M
 R :END OF HOLE.

A001
 ALAB
 ATYP
 AMTH
 AUMM

EQUITY MINESITE LABORATORY
 ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCOVSAMPLE	RQD %	CU	G/TAG	G/TAU %	SB %	AS %	FE %	ZN %
R	00	195	:TRICONED - NO CORE						
R	195	202	:DYKE - NO SAMPLE						
A001	202	251	6666	0.005	2.0	0.005	0.005	0.001	4.920 0.005

R	251	285	:DYKE - NO SAMPLE								
A001	285	315	6667	0.005	0.5	0.010	0.005	0.001	6.060	0.005	
A001	315	340	6668	0.020	11.0	0.040	0.005	0.001	8.250	0.005	
A001	340	370	6669	0.001	0.5	0.030	0.005	0.001	5.790	0.005	
A001	370	400	6670	0.001	0.5	0.005	0.005	0.001	5.840	0.005	
A001	400	430	6671	0.001	0.5	0.005	0.005	0.001	8.300	0.020	
A001	430	460	6672	0.010	0.1	0.005	0.005	0.010	6.140	0.010	
A001	460	490	6673	0.010	3.0	0.005	0.010	0.010	4.960	0.010	
A001	490	520	6674	0.005	0.5	0.005	0.010	0.005	5.020	0.010	
A001	520	560	6675	0.005	0.1	0.020	0.010	0.001	3.740	0.010	
A001	560	590	6676	0.005	0.5	0.020	0.005	0.005	5.190	0.005	
A001	590	620	6677	0.005	0.5	0.020	0.010	0.001	5.440	0.005	
A001	620	650	6678	0.010	1.0	0.020	0.010	0.030	6.750	0.010	
A001	650	680	6679	0.005	2.0	0.010	0.010	0.005	6.580	0.010	
A001	680	710	6680	0.005	1.0	0.010	0.005	0.010	4.650	0.010	
A001	710	740	6681	0.010	0.5	0.005	0.005	0.005	4.020	0.010	
A001	740	770	6682	0.005	3.0	0.005	0.010	0.005	4.990	0.020	
A001	770	800	6683	0.005	1.0	0.005	0.005	0.001	4.700	0.070	
A001	800	830	6684	0.005	3.0	0.005	0.010	0.005	5.780	0.040	
A001	830	860	6685	0.005	1.0	0.010	0.010	0.005	5.540	0.060	
A001	860	890	6686	0.005	1.0	0.010	0.010	0.010	7.630	0.070	
A001	890	920	6687	0.005	1.0	0.005	0.010	0.005	7.240	0.010	
A001	920	950	6688	0.005	1.0	0.005	0.005	0.010	6.680	0.020	
A001	950	980	6689	0.005	1.0	0.010	0.010	0.005	5.190	0.020	
A001	980	1010	6690	0.005	3.0	0.010	0.010	0.005	6.740	0.080	
A001	1010	1040	6691	0.005	0.5	0.010	0.010	0.005	10.320	0.030	
A001	1040	1070	6692	0.020	2.0	0.010	0.010	0.005	8.790	0.010	
A001	1070	1100	6693	0.010	0.5	0.020	0.010	0.005	6.650	0.050	
A001	1100	1130	6694	0.005	0.5	0.005	0.005	0.005	5.570	0.050	
A001	1130	1160	6695	0.005	0.1	0.010	0.010	0.020	4.210	0.040	
A001	1160	1190	6696	0.005	0.1	0.005	0.010	0.010	4.530	0.070	
A001	1190	1220	6697	0.010	0.1	0.005	0.010	0.005	4.380	0.100	
A001	1220	1250	6698	0.005	0.1	0.005	0.010	0.005	3.720	0.030	
A001	1250	1280	6699	0.005	0.5	0.005	0.010	0.005	3.390	0.010	
A001	1280	1310	6700	0.005	1.0	0.010	0.010	0.010	5.310	0.020	
A001	1310	1340	6701	0.005	1.0	0.030	0.010	0.010	4.310	0.020	
A001	1340	1365	6702	0.005	2.0	0.030	0.010	0.010	3.650	0.010	
R	1365	1829	:DYKE - NO SAMPLE								
A001	1829	1856	6703	0.005	2.0	0.070	0.010	0.005	4.330	0.020	
R	1856	1902	:DYKE - NO SAMPLE								
R			:END OF HOLE @ 190.2 (PREMATURE) - END OF LOG								

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IDEN6B0201      XB6CH259 NO   JUL86DJH   G&D JUL86S38      0.0
IPRJ            EQUITY SILVER MINES LTD      NORTH ZONE - MZ GEOCODE
S000  00  457 MT  257.9 090.0 -45.5          8918.64  8704.02  1288.39
S001  457 1372      257.9 090.0 -43.0
S002  1372 2174      257.9 090.0 -42.0
S003  2174 2579      257.9 090.0 -40.0
/SCL          MT.2MT.1
LSCL          MT.2
/NAM
LNAM
/      00  201      QVBN      P
R      :TRICONED - NO CORE
/      201  223  14  8A10CL  P* <<<      P      <>
L      06      4G      <<<
R      :V. WEAK << TEXT:15 % SAUSSURITIZED PLAG PHENOS (10 X 2 MM)
R      :LOWER CONTACT NOT OBSERVED
/      223  232  07  3E10CL  <<<      P      <>
L      00      AG      <<<<< <<
R      :CLAY GOUGE @ 22.9 M :WEAK TO MOD << TEXT
/      232  287  50  8A10CLCY P* <<<      P      <>
L      07      AG      <<
R      :GENERALLY WEAK << TEXT (TO STRONG LOC) :MINOR CY GOUGE
R      :CNTS NOT OBSERVED
/      287  310  23  3E13CL  <<<      P      << <>
L      12      AG
R      :WEAK << TEXT
/      310  342  32  8A10CLCY P* <<<      P      <<
L      18      AG      <<
R      :V WEAK << TEXT :NO CNTS OBSERVED
/      342  395  53  3E13CL  <<<BD      P BD  048<< <<
L      18      AG      <<
R      :W/10% 3D INTERBEDDED :V WEAK << TEXT
/      395  405  10  8A10CLCY P* <<<      P      <<
L      02      AG      <<
R      :V WEAK << TEXT :20% RANDOM PLAG PHENOS ALTERED TO CY
R      :NO CNTS OBSERVED
/      405  438  33  3E13CL  <<<BD      P BD  038<< <<
L      26      AG      <<
R      :V WEAK << TEXT :AS ABOVE 34.2 - 39.5 M
R      :NOTE -NUMEROUS HAIRLINE FRACTURES W/ OFFSET OF BEDS
R      :LOWER CNT GRADATIONAL
/      438  470  30  3D13CL  <<<      P      << <<
L      24      AG      <<
R      :PEBBLE TO COBBLE CONGLOM :V WEAK << TEXT
R      :LOWER CNT GRADATIONAL
/      470  487  16  3E13CL  <<<BD      P BD  046<< <<
L      02      AG      CL  045 <<
R      :5% INTERBEDDED 3D :LOWER CNT SHARP // BEDDING
/      487  510  23  3D13CL  <<<      P      << <<
L      21      5G      <<
R      :COBBLE CONGLOMERATE :8A 50.3 - 50.5 M :WEAK TO MOD << TEXT
/      510  585  74  8A10CL  P*A*      P      <>
L      55      AG      <<      CL  057 <>
R      :WEAK TO MOD (LOC) << TEXT :UPPER CNT NOT OBSERVED
R      :LOWER CNT SHARP & SLIGHTLY IRREGULAR

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/ 585 593 08 3D13CL << P << <)
 L 06 AG <<
 R :WEAK << TEXT :LOWER CNT NOT OBSERVED
 / 593 597 04 3E13CL << P BD 059<< <<
 L 03 GA <<
 R :WEAK << TEXT :LOWER CNT WEAKLY GRADATIONAL -NO ATTITUDE
 / 597 623 25 3H13CL << P <<
 L 15 GA
 R :PORPHYRITIC ANDESITE LAPILLI TUFF (40% LIGHT GREY GREEN
 R :ANDESITE FRAGS IN A DARK GREY ASH MATRIX)
 R :LOWER CNT IRREG (GRADATIONAL?) :V WEAK << TEXT :OCC BOMBS?
 / 623 674 50 3H113CL << P << <<
 L 46 66
 R :V WEAK << TEXT :ANDESITIC AS ABOVE BUT MATRIX IS LIGHT GREY
 R :GREEN ASH :MINOR 3H AS ABOVE 59.7 - 62.3 M INTERLEVED
 R :MINOR 3E INTERLEVED :THIS COULD BE UNIT 2 (IE 2E)
 R :LOWER CNT GRADATIONAL
 / 674 696 22 3H13CL << P << <)
 L 19 GA <<
 R :LOWER CNT GRADATIONAL :AS ABOVE 59.7 - 62.3 M :WEAK << TEXT
 R :LAPILLI ARE V PALE GREENISH GREY
 / 696 756 57 3D13CL << P << <<
 L 39 AG <<
 R :COBBLE CONGLOM :5% 3E INTERLEVED :LOTS OF PORPHYRITIC VOLC
 R :CLASTS :V WEAK << TEXT
 / 756 788 32 3H13CL <<<< P <+ <<
 L 12 AG <<
 R :SIMILAR TO 3D ABOVE (MORE ANGULAR FRAGS) :STRONG << TEXT
 R :GOUGE @ 75.8 M :3D?
 / 788 817 29 8A10CL P*<< P <*<<
 L 26 AG <*<<
 R :WEAK << TEXT :CNTS ARE IRREG (NO ATTITUDES)
 / 817 843 26 3H13CL << P << <)
 L 20 AG <<
 R :V WEAK << TEXT :LOWER CNT GRADATIONAL :AS ABOVE 75.6 - 78.8
 R :3D?
 / 843 950 100 3G13CL << P BD 032 <<
 L 48 AG << <<
 R :WEAK << TEXT EXCEPT MOD (87.0 - 88.1) :3E? :5% 3H?/3D?
 R :LOC INTERLEVED
 R :3F 87.0 - 88.1 M :LOWER CNT GRADATIONAL
 / 950 969 18 3H13CL << P <<
 L 07 GA
 R :V WEAK << TEXT :80% LAPILLI (SUBANGULAR) :2E?
 / 969 1001 30 3G13CL << P BD 037 <)
 L 06 GA << << (Q.B.
 R :TO 3G43 LOC W/STRONG << TEXT :GENERALLY WEAK << TEXT
 R :GRADATIONAL LOWER CNT
 / 1001 1013 12 3H13CL << P <<
 L 10 GA <<
 R :AS ABOVE 95.0 - 96.9 M :10% DARK GREY, SILICEOUS FRAGS
 R :WEAK << TEXT :MATRIX OCC REDDISH
 R :GRADATIONAL LOWER CNT
 / 1013 1035 20 3G13CL << P << < .
 L 09 GA << < .

R :WEAK << TEXT :OCC LAPILLI
/ 1035 1050 14 8A13CL <<A* P << A+
L 00 GA P* <<
R :CONTACT ZONE (20% DARK GREY/BLACK 3K) - STEEP CNT?
R :GOUGE @ UPPER CNT
R :WEAK << TEXT :10% A* W/ QZ +- PY :PRE-MINERAL DYKE
/ 1050 1122 72 8A13CL P*<< P <) A)
L 29 6G A* <)
R :5% A* W/ QZ + CB +- PY :PRE-MINERAL DYKE :WEAK << TEXT
/ 1122 1163 41 8A13CL << P <+
L 35 5G <<
R :CNTS NOT OBSERVED :NON P* TEXT :LOCALLY DISSEM PY -10% AND
R :SL -2% :WEAK << TEXT :PRE-MIN DYKE
/ 1163 1168 04 3G03 << P <+<.
L 00 4A
R :MINOR 8A AS ABOVE
/ 1168 1175 04 8A113CL <<P* P <)
L 02 5G A*
R :AS ABOVE 105.0 - 112.2 M
/ 1175 1200 25 3K03 << P B* <=
L 06 3A
R :VOLCANIC SILTSTONE? :MOD << TEXT :10% 3E (MAINLY TOWARDS EOI)
R :8A 118.9 - 119.3 M
R :NOTE OCCURANCE OF SZ
/ 1200 1220 20 8A13CL P*<< P CU 035< <<
L 08 6G <.
R :V WEAK << TEXT :LOWER CNT NOT OBSERVED :UPPER CNT IS SHARP
R :AND CHILLED
/ 1220 1243 23 3K03 << P <)
L 00 3A <<
R :WEAK << TEXT :AS ABOVE 117.5 - 120.0 BUT W/O SZ
/ 1243 1251 07 8A13CL <<P* P CU 022 <)
L 00 6G CL 048
R :V WEAK << TEXT :PRE-MIN DYKE
/ 1251 1374 123 2D13CL << P <+
L 45 6A < <<<.
R :TO 2D43 LOC :WEAK TO MOD << TEXT :TO 2E LOC :MINOR GOUGE
R :A CHAOTIC MIX OF ASH W/ LAPILLI & DUST
/ 1374 1420 46 8A13CL P*A* P << <<
L 28 6G << CL 050 <<
R :UPPER CNT NOT OBSERVED :GOUGE @ LOWER CNT :PRE-MIN DYKE
R :WEAK << TEXT :2% A* W/ QZ + CB +- PY
/ 1420 1525 100 2E13CL <<BR P <+#) <)
L 71 6A <)
R :TO 2E45 LOC W/ +- CP +- AS +- PY :TO 2E47 LOC
R :MOD << TEXT TO WEAK LOCALLY
R :GRADATIONAL LOWER CNT :TO 2C LOC
/ 1525 1562 37 2C13CY <<BR P <=#)#<)<
L 23 4A
R :TO 2C67 LOC :MOD << TEXT :MINOR BXIA @ EOI
/ 1562 1585 23 2C83MS << P <= <)
L 03 5T
R :MOD TO STRONG << TEXT :TO 2D LOC
/ 1585 1660 73 2C83MS << P <)
L 36 5T

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R      :TO 2D LOC :WEAK << TEXT
/      1660 1669 09 2C87MSQZ BR P CU 050 B( #2 #+
L      07 5T
R      :STRONG BR TEXT :LOWER CNT NOT OBSERVED
/      1669 1687 16 2D83MS << <= <
L      12 5T
R      :MOD << TEXT :TO 2E LOC
/      1687 1692 04 MSDEPY P MX
L      00 5Y
R      :VEIN? (CNTS NOT OBSERVED)
/      1692 1768 76 2D23SZMS <<BR P B( <+. <
L      46 5T
R      :WEAK TO MOD << TEXT :V MINOR ZONES BR :MINOR CLAY (GOUGE?)
R      :ZONES
/      1768 1784 16 8A11CL <<P* P CU 065<( D+
L      12 AG CL 073 <.
R      :V WEAK << TEXT
/      1784 1855 71 2E23MS << P B( <+
L      37 5T <(< <
R      :20% 2D INTERLEVED :MAJORITY OF LAPILLI ARE PORPHYRITIC VOLC
R      : (DACITE?) :MINOR ZONES CY (GOUGE?)
R      :MOD << TEXT
/      1855 2008 153 2E13CL << P <. <
L      56 <.<
R      :WEAK TO MOD << TEXT :5% 2D INTERLEVED :NOTE -APPEARANCE OF
R      :GREEN ROCK COINCIDES W/ LOSS OF SZ :LOWER CNT GRADATIONAL
R      :OVER 1 M
/      2008 2059 51 2D13CL << P BD 055<( <
L      39 4G <((
R      :IRREGULAR BEDDING (AV = 055) :WEAK << TEXT TO MOD LOCALLY
R      :5% 2E INTERLEVED
R      :LOWER CNT GRADATIONAL OVER 0.5 M :MINOR CY (GOUGE?) ZONES
/      2059 2083 21 2E13CL << P <(< <
L      17 5G <(((
R      :V WEAK << TEXT :LOWER CNT GRADATIONAL OVER 0.3 M
/      2083 2127 44 2D13CL << P <(< <
L      33 AG <((( <.
R      :MOD << TEXT :10% 2E INTERLEVED :MINOR CY (GOUGE?) ZONES
/      2127 2145 18 8A10CL P*A* P CU 058
L      17 AG CL 050
R      :LOWER CNT SLIGHTLY IRREGULAR :GOOD INTRUSIVE (CHILLED, SHARP)
R      :CNTS
/      2145 2191 39 2D83MSCL << P <
L      22 6T CL 050 <(< <
R      :<5% 2E INTERLEVED :MOD << TEXT :LOWER CNT SHARP & IRREGULAR
R      :MINOR CY (GOUGE?) ZONES
/      2191 2501 301 1C03QZ << P BD 074<( <
L      246 AT CL 043 <. <.
R      :V WEAK << TEXT :10% 1D INTERLEVED :TUFFACEOUS MATRIX LOCALLY
R      :LOWER CNT FAIRLY SHARP
/      2501 2534 31 1D03QZ << P <
L      00 AT
R      :V WEAK << TEXT :LOWER CNT NOT OBSERVED
/      2534 2556 22 2D13CL <<BD P BD 063 <
L      19 5G

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R           :W/ 30% 1D (TUFFACEOUS) INTERLEVED :V WEAK << TEXT
R           :GRADATIONAL LOWER CNT
/    2556  2576  16    2C13CL    <<      P      <<
L           10      MG          << <<
R           :WEAK TO MOD << TEXT :LOWER CNT NOT OBSERVED
/    2576  2579  03    1C03QZ    <<      P      <<
L           00      AT
R           :V WEAK << TEXT
R           :EDH @ 257.9 M

A001
ALAB       EQUITY MINESITE LABORATORY
ATYP      ASSAY
AMTH      WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM      RCOVSAMPLE  RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R    00    201  :TRICONED - NO CORE
R    201  223  :DYKE - NO SAMPLE
A001  223  232      6704      0.005  1.0 0.020 0.005 0.001 4.770 0.020
R    232  287  :DYKE - NO SAMPLE
A001  287  310      6705      0.005  1.0 0.01  0.001 0.001 4.71  0.01
R    310  342  :DYKE - NO SAMPLE
A001  342  366      6706      0.005  1.0 0.02  0.005 0.001 3.32  0.005
A001  366  395      6707      0.001  1.0 0.02  0.005 0.01  3.94  0.01
R    395  405  :DYKE - NO SAMPLE
A001  405  436      6708      0.005  1.0 0.02  0.005 0.01  4.83  0.01
A001  436  455      6709      0.005  1.0 0.01  0.001 0.005 5.09  0.02
A001  455  485      6710      0.001  0.5 0.02  0.005 0.02  5.12  0.01
A001  485  510      6711      0.005  0.5 0.02  0.005 0.01  5.83  0.02
R    510  585  :DYKE - NO SAMPLE
A001  585  600      6712      0.001  0.5 0.02  0.001 0.03  3.59  0.01
A001  600  630      6713      0.005  0.5 0.04  0.005 0.005 5.64  0.02
A001  630  660      6714      0.005  0.1 0.02  0.005 0.005 7.16  0.02
A001  660  690      6715      0.001  0.5 0.02  0.005 0.01  3.84  0.02
A001  690  720      6716      0.005  0.1 0.02  0.005 0.001 4.13  0.02
A001  720  750      6717      0.005  0.5 0.03  0.005 0.005 7.08  0.04
A001  750  770      6718      0.01   2.0 0.03  0.005 0.65  6.38  1.96
A001  770  788      6719      0.005  0.5 0.02  0.005 0.21  6.16  0.20
R    788  817  :DYKE NO SAMPLE
A001  817  850      6720      0.01   1.0 0.02  0.005 0.01  6.09  0.02
A001  850  880      6721      0.005  1.0 0.02  0.005 0.05  4.22  0.03
A001  880  910      6722      0.001  1.0 0.02  0.001 0.08  4.02  0.01
A001  910  940      6723      0.005  0.5 0.03  0.001 0.04  4.10  0.03
A001  940  970      6724      0.005  0.5 0.03  0.005 0.08  2.23  0.02
A001  970 1000      6725      0.005  0.5 0.02  0.001 0.08  3.00  0.08
A001 1000 1035      6726      0.005  0.5 0.02  0.001 0.12  1.47  0.01
A001 1035 1060      6727      0.005  0.1 0.02  0.010 0.03  5.06  0.02
A001 1060 1090      6728      0.005  0.1 0.06  0.010 0.03  4.15  0.01
A001 1090 1120      6729      0.005  0.5 0.02  0.005 0.04  5.10  0.04
A001 1120 1150      6730      0.010  1.0 0.02  0.010 0.46  5.49  0.13
A001 1150 1175      6731      0.010  1.0 0.23  0.005 0.37  6.46  0.17
A001 1175 1200      6732      0.020  0.1 0.01  0.010 0.27  6.10  0.05
A001 1200 1220      6733      0.005  0.1 0.03  0.005 0.01  5.75  0.03
A001 1220 1243      6734      0.005  1.0 0.03  0.005 0.54  5.98  0.28
A001 1243 1270      6735      0.005  1.0 0.02  0.010 0.37  7.03  0.18
A001 1270 1300      6736      0.010  1.0 0.01  0.010 0.29  5.19  0.37
A001 1300 1330      6737      0.005  1.0 0.02  0.010 0.79  5.55  0.43

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A001	1330	1350	6738	0.005	0.5	0.06	0.010	0.35	4.69	0.03
A001	1350	1374	6739	0.005	0.5	0.03	0.010	0.18	3.88	0.04
A001	1374	1400	6740	0.005	0.5	0.04	0.010	0.04	4.60	0.01
A001	1400	1420	6741	0.005	1.0	0.25	0.005	0.03	4.81	0.01
A001	1420	1450	6742	0.300	118.0	1.20	0.060	0.98	7.47	0.24
A001	1450	1480	6743	0.020	5.0	0.24	0.005	0.75	5.76	0.71
A001	1480	1510	6744	0.040	16.0	0.87	0.010	0.97	7.42	0.005
A001	1510	1540	6745	0.100	27.0	0.84	0.020	0.89	6.11	0.03
A001	1540	1570	6746	0.290	144.0	3.46	0.090	1.98	6.88	0.08
A001	1570	1600	6747	0.010	35.0	0.06	0.010	0.08	9.30	0.005
A001	1600	1630	6748	0.005	1.0	0.06	0.005	0.27	1.03	0.005
A001	1630	1660	6749	0.005	1.0	0.88	0.001	0.27	3.28	0.001
A001	1660	1687	6750	0.060	5.0	0.38	0.020	2.88	16.10	0.005
A001	1687	1720	6751	0.040	5.0	0.50	0.005	0.51	19.60	0.005
A001	1720	1750	6752	0.005	2.0	0.11	0.005	0.16	7.83	0.001
A001	1750	1768	6753	0.001	0.5	0.05	0.005	0.16	2.76	0.001
A001	1768	1784	6754	0.001	0.5	0.01	0.005	0.04	4.22	0.005
A001	1784	1810	6755	0.001	0.5	0.06	0.005	0.04	4.79	0.020
A001	1810	1840	6756	0.001	0.5	0.05	0.005	0.15	6.24	0.090
A001	1840	1870	6757	0.001	0.5	0.02	0.005	0.06	5.89	0.005
A001	1870	1900	6758	0.005	0.5	0.03	0.005	0.005	5.91	0.030
A001	1900	1930	6759	0.005	0.5	0.05	0.005	0.03	7.15	0.005
A001	1930	1960	6760	0.005	0.5	0.07	0.005	0.001	4.78	0.005
A001	1960	1990	6761	0.005	0.5	0.04	0.001	0.001	4.95	0.005
A001	1990	2020	6762	0.005	0.5	0.06	0.001	0.001	7.92	0.005
A001	2020	2050	6763	0.001	0.5	0.06	0.001	0.001	5.95	0.02
A001	2050	2080	6764	0.005	0.5	0.04	0.001	0.001	6.86	0.03
A001	2080	2110	6765	0.005	0.5	0.10	0.001	0.001	6.41	0.02
A001	2110	2127	6766	0.005	0.5	0.06	0.001	0.03	7.14	0.03
R	2127	2145	:DYKE - NO SAMPLE							
A001	2145	2170	6767	0.005	0.5	0.07	0.001	0.03	7.11	0.03
A001	2170	2200	6768	0.005	0.5	0.04	0.001	0.005	4.71	0.07
A001	2200	2230	6769	0.001	0.5	0.05	0.001	0.03	5.71	0.24
A001	2230	2260	6770	0.001	0.5	0.03	0.001	0.001	2.75	0.005
A001	2260	2290	6771	0.001	0.5	0.03	0.001	0.001	1.60	0.001
A001	2290	2320	6772	0.001	0.1	0.02	0.001	0.001	1.57	0.001
A001	2320	2350	6773	0.001	0.1	0.02	0.001	0.001	2.03	0.001
A001	2350	2380	6774	0.001	0.1	0.02	0.001	0.001	1.61	0.001
A001	2380	2410	6775	0.005	2.0	0.06	0.005	0.001	2.00	0.030
A001	2410	2440	6776	0.020	3.0	0.05	0.001	0.001	2.89	0.005
A001	2440	2470	6777	0.005	2.0	0.02	0.001	0.001	2.49	0.005
A001	2470	2500	6778	0.005	0.5	0.02	0.001	0.001	2.95	0.005
A001	2500	2530	6779	0.005	3.0	0.03	0.001	0.001	2.51	0.005
A001	2530	2554	6780	0.005	0.5	0.09	0.001	0.001	4.98	0.005
A001	2554	2579	6781	0.005	0.5	0.04	0.001	0.001	3.53	0.005

R :EOH @ 257.9 M
R END OF ASSAYS - END OF LOG

IDEN6B0201		X86CH260 NQ	JUL86DJH	G&D JUL86S38	0.0	
IPRJ		EQUITY SILVER MINES LTD		SOUTH OF S. TAIL - ST GEOCODE		
S000	00	555 MT	116.1 090.0 -45.0		6252.31	7919.61 1312.56
S001	555	1161	116.1 090.0 -43.0			
/SCL		MT.2MT.1				
LSCL		MT.2				
/NAM					MSCLOZPYCPTTASPR	
LNAM					CBGY MGHESLGLMO	
/	00	152	OVBN	P		
R			:TRICONED - NO CORE			
/	152	212	34 2C25MSQZ <<	P		<<<+<.
L			00 5T			
R			:LIMONITE ON FRACTURES FROM 20.1 - 21.2			
/	212	225	12 8A02CLCB A*	P		A)
L			06 4G			A(
R			:1-2% AMYGDS :CNTS NOT OBSERVED (GOUGE @ UPPER CNT)			
/	225	250	25 2C24MSCL <<	P		<) <+
L			00 GT			
R			:10% 2D INTERLEVED :LIMONITE ON FRACTS			
/	250	280	28 2D24MSCL <<	P		<.<<<<
L			00 GT			
R			:LIMONITE ON FRACTS			
/	280	310	29 2D23CLMS <<	P		<.<<<<<.
L			00 TG			
/	310	340	26 2D23CLMS <<	P		<<<<<<
L			00 TG			
R			:10% 2C INTERLEVED			
/	340	370	27 2D23CLMS <<	P		<< (<<<<
L			00 TG			
R			:10% 1A INTERLEVED (20% CHERT CLASTS)			
/	370	400	30 2C24MSCL <<	P		<*<<<<<.
L			06 GT			
/	400	430	29 2C23CLMS <<	P	BD 045	<<<.<)
L			18 TG			
R			:~25% 2D INTERLEVED			
/	430	446	15 2C24MSCL <<	P		<<<.<)<.
L			09 GT		CL 047	
R			:LOWER CNT V SHARP			
/	446	462	15 1C10QZ <<	P		<<<<
L			12 5A		CL 049	
R			:LOWER CNT V SHARP			
/	462	490	27 2C24MSCL <<	P		<)<<<+<(<
L			13 GT			
/	490	520	29 2C23CLMS <<	P		<+<<<<<.
L			24 TG			
/	520	550	29 2C23CLMS <<	P		<+<<(<=
L			20 TG			
R			:TO STRONG << TEXT LOC			
/	550	580	27 2C23CLMS <<	P		<*<<<<.< <.
L			20 TG			
R			:TO STRONG << TEXT LOC			
/	580	609	29 2C23CLMS <<	P		<)<<<<<<.
L			11 TG			
R			:TO 2C15 LOC			
/	609	614	05 8A20CLCB A*	P	CU 060	

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L           04          4G          CL 060
R           :LOWER CNT IRREGULAR
/ 614 637 22 2C22CL << P <><<<<
L           10          6G
/ 637 673 36 BA20CLCB P* P
L           311         4G          CL 070 D)
R           :UPPER CNT IRREG W/ MINOR BXIA :LOWER CNT WEAKLY IRREGULAR
/ 673 700 26 2C22CL << P <><<<<
L           18          5G
R           :TO 2C25 LOC :10% 1D INTERLEVED
/ 700 730 30 2C22CL << P <><<<<
L           19          5G
R           :TO 2C25 LOC :10% 1D INTERLEVED :V IRREGULAR GREEN/TAN COLOR
R           :BANDING
/ 730 760 30 2C22CL << P <><<<<
L           16          5G
R           :AS ABOVE W/ 2C25 LOC AND TAN/GREEN COLOR BANDING
/ 760 790 27 2C22CL << P BD 071 <><<<<
L           20          5G <
R           :5% 1D INTERBEDDED
/ 790 820 29 2C22CL << P <><*<<
L           19          5G <
/ 820 846 26 2C22CL << P <><*<*<
L           07          5G <
R           :LOWER CNT FAIRLY SHARP BUT IRREGULAR (NO ATTITUDE
/ 846 857 10 1D12CL << P <<.<
L           03          AG
R           :TUFACEOUS MATRIX? :V WEAK << TEXT :30% 1C (EOI)
/ 857 880 23 2C21CL << P <><<<<
L           18          6A <<
/ 880 910 28 2C23CLMS << P <><<<<
L           19          TG
R           :10% 2D INTERLEVED
/ 910 940 30 2C10 << P <<<<<<
L           21          4M
R           :PROPYLITIC ALT'N CNV ON << :TO 2C22 @ START OF INT
/ 940 970 29 2C10 << P <<<<<<
L           14          4M
R           :TO 2C22 LOC
/ 970 1000 29 2C22CL << P <><<<<*<
L           23          AG
R           :LOCAL IRREGULAR GREEN/BUFF COLOR BANDING
/ 1000 1030 28 2C22CL << P <><<<<*<
L           19          AG
R           :PY ALSO IN PATCHES
/ 1030 1060 30 2C21CL << P <><<<<
L           21          6M
/ 1060 1084 24 2C21CL << P <><<.<
L           07          6M <
/ 1084 1096 12 BA02CLCB A* P
L           08          AG
R           :CNTS NOT OBSERVED
/ 1096 1125 27 2C22CL << P <><<.<
L           14          5G
R           :MINOR BXIA @ 112.5 M

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/ 1125 1132 07 BA12CLCB << P CU 045
L 02 5G CL 053<)
/ 1132 1161 29 2C22CL << P <)<<<<
L 02 5G <
R :MINOR BXIA @ 113.2 M :1D 115.8 - 116.1
R :EOH @ 116.1 M
R END OF HOLE.

A001
ALAB EQUITY MINESITE LABORATORY
ATYP ASSAY
AMTH WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM RCOVSAMPLE RQD % CU G/TAG G/TAU % SB % AS % FE % ZN
R 00 152 :OVBN - NO CORE (TRICONED)
A001 152 186 6782 0.100 3.0 0.20 0.001 0.13 3.10 0.005
A001 186 212 6783 0.11 5.0 0.23 0.001 0.06 4.37 0.005
R :DYKE - NO SAMPLE
A001 225 250 6784 0.19 8.0 0.18 0.001 0.005 4.80 0.05
A001 250 280 6785 0.08 3.0 0.18 0.005 0.05 5.65 0.02
A001 280 310 6786 0.22 7.0 0.18 0.020 0.04 5.42 0.005
A001 310 340 6787 0.07 2.0 0.09 0.005 0.04 4.96 0.005
A001 340 370 6788 0.17 4.0 0.04 0.005 0.001 6.04 0.005
A001 370 400 6789 0.08 4.0 0.14 0.001 0.070 4.58 0.005
A001 400 430 6790 0.03 2.0 0.03 0.005 0.001 4.85 0.005
A001 430 460 6791 0.09 3.0 0.08 0.005 0.030 4.80 0.005
A001 460 490 6792 0.19 3.0 0.08 0.030 0.020 4.73 0.005
A001 490 520 6793 0.05 2.0 0.04 0.005 0.001 5.35 0.005
A001 520 550 6794 0.03 2.0 0.02 0.005 0.001 7.15 0.005
A001 550 580 6795 0.04 4.0 0.10 0.005 0.350 5.30 0.005
A001 580 610 6796 0.02 2.0 0.05 0.005 0.001 3.10 0.005
A001 610 637 6797 0.02 6.0 0.01 0.005 0.001 2.77 0.001
R :DYKE - NO SAMPLE
A001 673 700 6798 0.005 0.5 0.050 0.005 0.001 3.95 0.001
A001 700 730 6799 0.02 0.5 0.04 0.005 0.001 3.94 0.02
A001 730 760 6800 0.02 0.5 0.03 0.005 0.001 4.67 0.001
A001 760 790 6801 0.02 0.5 0.02 0.005 0.001 3.47 0.001
A001 790 820 6802 0.02 0.5 0.02 0.005 0.001 4.10 0.001
A001 820 850 6803 0.005 0.5 0.01 0.005 0.001 3.20 0.001
A001 850 880 6804 0.005 0.5 0.02 0.005 0.001 2.98 0.001
A001 880 910 6805 0.03 0.5 0.01 0.005 0.001 3.19 0.001
A001 910 940 6806 0.005 0.5 0.01 0.005 0.001 4.02 0.001
A001 940 970 6807 0.005 0.5 0.01 0.005 0.001 3.75 0.001
A001 970 1000 6808 0.005 0.5 0.02 0.005 0.03 5.22 0.06
A001 1000 1030 6809 0.005 0.5 0.01 0.005 0.001 4.92 0.001
A001 1030 1060 6810 0.005 0.5 0.01 0.005 0.001 3.76 0.001
A001 1060 1084 6811 0.005 0.5 0.01 0.005 0.001 4.28 0.001
R 1084 1096 :DYKE - NO SAMPLE
A001 1096 1125 6812 0.005 0.5 0.01 0.005 0.001 4.04 0.001
R 1125 1132 :DYKE - NO SAMPLE
A001 1132 1161 6813 0.001 0.5 0.01 0.005 0.001 3.61 0.001
R :EOH @ 116.1 M
R END OF ASSAYS - END OF LOG

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R				TYPICAL 2C13.				
/	690	720	29	2C14	<<	P		<) <*
L			08	AT				
/	720	754	33	2C13	<<WP	P		<) <<
L			09	GT				
/	754	763	09	8C00	P*	P FB	40	D.
L			05	8A				
R				FAULT GOUGE ON UPPER CONTACT, LOWER CONTACT NOT PRESERVED.				
/	763	788	24	2C54MSQZ	BR<<	P		<) <)Q-
L			08	AT				Q.
R				ZONE WEAKLY BX'D.				
/	788	802	13	8A00	MS	P		I=
L			09	2A				
/	802	830	27	2C14	<<	P		<)<+<)<.
L			09	AT				
R				PATCH OF 1C AT 80.4				
/	830	860	29	2C13	<<	P		<)<)<+
L			09	7A				
R				PATCH OF 1C AT 85.2.				
/	860	895	34	2C23	<<BR	P		<)<+<)
L			06	7A				
R				CONTAINS OCCASIONAL CLASTS OF QZ PEBBLES.				
/	895	917	21	1C11	<<	P CU	55	<(< <*
L			07	AW				D.
R				LOWER CONTACT GRADATIONAL INTO 2C.				
/	917	950	32	2C13	<<	P V/	35	<)<+<)
L			11	AT				
R				PATCH OF 1C AT 93.2. OCCASIONAL QZ CLASTS				
/	950	980	29	2C13	<<	P V/	45	<)<V+V+
L			11	5A				
R				PATCH OF 1C AT 95.8 AND 98.0.				
/	980	1010	29	2C23	<<BR	P		<+<)<+
L			09	5A				
R				CLASTS OF QTZ IN 2C. SLIGHTLY BX'D.				
/	1010	1040	28	2C22	<<BR	P		<+ <+B(
L			00	5A				
R				PATCH OF 1C AT 102.7.				
/	1040	1070	28	2C22	<<	P		<= <*B(
L			00	6A				
R				CORE VERY BROKEN. SOME CP IN << AS WELL.				
/	1070	1100	29	2C22CL	<<	P		<1<)<+B.
L			06	GT				
/	1100	1123	22	2C22CL	<<	P		<1<*<+B.
L			03	GT				
/	1123	1140	17	2E12	<<	P CU	85	<* D+
L			07	2A				
/	1140	1160	20	2C29	<<	P		<(<)<+<)<-
L			06	5A				<<
R				CP BLEBS AS WELL, GOOD INTERVAL.				
/	1160	1190	29	2C19	<<	P		<*B*V+B(
L			09	5A				
R				OCCASIONAL LAPILLI.				
/	1190	1209	19	2E12	<<	P		V)V)
L			05	AG				
R				SOME LAPILLI SILICIFIED.				

/ 1209 1240 30 2C12 << P <+<*+<
 L 17 AG <
 R ROCK CONTAINS OCCASIONAL LAPILLI.
 / 1240 1263 23 2C22 << P BN 55 <+ <)<.
 L 05 AG
 / 1247 1248 X D B2B+D(B1
 L B)
 / 1263 1290 27 8B01FL TC P CU 55 E=<-
 L 21 GA CL 65 D*
 / 1290 1320 30 2C12 <<BR P <+ <+<)
 L 05 AG
 R SOME LAPILLI, DISRUPTION, BX'D. SMALL 8< 131.0 TO 131.1.
 / 1320 1350 29 2C22 << P BN 55 <+B*
 L 06 GA
 R OCCASIONAL LAPILLI.
 / 1350 1381 30 2C29 << P <+B(B)<.
 L 11 GA
 R STILL CONTAINS OCCASIONAL LAPILLI.
 / 1381 1388 07 8A00 MS P CU 75 <-
 L 07 1A CL 40 D)
 / 1388 1393 05 2C22 << P <+ B)
 L 02 GA
 R END OF HOLE.

A001
 ALAB
 ATYP
 AMTH
 AUMM

EQUITY MINESITE LABORATORY
 ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCOV	SAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
A001	183	210	6841	0.001	0.5	0.005	0.005	0.001	2.60	0.001
A001	210	240	6842	0.001	0.5	0.005	0.005	0.001	5.14	0.001
A001	240	270	6843	0.001	0.5	0.07	0.005	0.001	5.09	0.001
A001	270	300	6844	0.001	0.5	0.005	0.005	0.001	4.76	0.001
A001	300	330	6845	0.005	0.5	0.03	0.005	0.001	2.31	0.001
A001	330	360	6846	0.02	0.5	0.31	0.005	0.04	5.13	0.001
A001	360	390	6847	0.001	0.5	0.03	0.005	0.001	1.64	0.001
A001	390	440	6848	0.001	0.1	0.01	0.001	0.001	0.72	0.001
A001	440	480	6849	0.001	0.5	0.03	0.005	0.001	2.21	0.001
A001	480	510	6850	0.001	0.5	0.02	0.005	0.001	5.19	0.001
A001	510	540	6851	0.001	0.5	0.06	0.005	0.03	3.24	0.001
A001	540	570	6852	0.001	0.5	0.08	0.005	0.03	2.31	0.001
A001	570	600	6853	0.001	0.5	0.04	0.005	0.001	3.11	0.001
A001	600	630	6854	0.005	0.5	0.03	0.005	0.001	3.44	0.001
A001	630	660	6855	0.005	0.5	0.03	0.005	0.001	5.27	0.001
A001	660	690	6856	0.02	0.5	0.05	0.005	0.001	5.00	0.001
A001	690	720	6857	0.005	0.5	0.03	0.005	0.001	4.26	0.001
A001	720	750	6858	0.005	0.5	0.03	0.005	0.001	4.60	0.001
A001	750	788	6859	0.040	0.5	0.05	0.005	0.001	2.95	0.001
A001	802	830	6860	0.050	3.0	0.22	0.020	0.050	5.45	0.020
A001	830	860	6861	0.020	0.5	0.13	0.005	0.040	3.73	0.001
A001	860	890	6862	0.020	0.5	0.05	0.020	0.005	3.09	0.001
A001	890	920	6863	0.030	3.0	0.12	0.020	0.050	2.46	0.001
A001	920	950	6864	0.005	0.5	0.12	0.020	0.050	4.55	0.001
A001	950	980	6865	0.001	0.1	0.03	0.005	0.001	3.60	0.001
A001	980	1010	6866	0.020	0.1	0.03	0.005	0.001	3.03	0.001
A001	1010	1040	6867	0.080	0.1	0.03	0.005	0.001	2.55	0.001

A001	1040	1070	6868	0.130	2.0	0.03	0.005	0.001	1.79	0.001
A001	1070	1100	6869	0.070	3.0	0.04	0.005	0.001	3.49	0.001
A001	1100	1130	6870	0.005	3.0	0.06	0.005	0.001	3.70	0.140
A001	1130	1160	6871	0.380	28.0	0.05	0.005	0.001	5.36	0.030
A001	1160	1190	6872	0.080	4.0	0.05	0.005	0.020	5.64	0.030
A001	1190	1220	6873	0.030	4.0	0.05	0.005	0.020	7.41	0.020
A001	1220	1240	6874	0.060	4.0	0.04	0.005	0.010	4.41	0.020
A001	1240	1263	6875	0.240	15.0	0.16	0.005	0.610	6.82	0.170
A001	1290	1320	6876	0.050	3.0	0.03	0.005	0.001	4.36	0.020
A001	1320	1350	6877	0.030	2.0	0.05	0.005	0.030	3.49	0.010
A001	1350	1370	6878	0.080	5.0	0.04	0.005	0.010	4.27	0.020
A001	1370	1393	6879	0.010	1.0	0.03	0.005	0.005	4.17	0.005

R

END OF ASSAYS - END OF LOG

IDEN6B0201			X86CH262 NG	JUL86DJHRBPG&D	JUL86S38		0.0
IPRJ			EQUITY SILVER MINES LTD				SOUTH OF S. TAIL - ST GEOCODE
S000	00	457	MT	312.7	090.0	-45.0	6033.06 7496.15 1213.20
S001	457	1372		312.7	090.0	-44.0	
S002	1372	2478		312.7	090.0	-44.0	
S003	2478	3127		312.7	090.0	-44.0	
/SCL			MT.2	MT.1			
LSCL				MT.2			
/NAM							MSCLQZPYCPTTASPR
LNAM							CBGY MGHESLGLMO
/	00	244		OVBN			P
R				:TRICONED - NO CORE			
/	244	270	20	3A10QZ	<<VU		P <<<<
L			00	AN			
R				:FE OXIDE STAINS ON FRACTS	:VUGS MAY BE CAUSED BY DISSOLUTION		
R				OF PY.			
/	270	300	30	3A20DZ	<<		P <><>
L			06	AN			
R				:FE OXIDE STAINS ON FRACTS.			
/	300	330	18	3A10QZ	<<		P <<<*
L			00	AN			
R				:TO 3A20/OC :FE OXIDE STAIN ON SOME FRACTS	:NOTE -CHERT CLASTS		
R				ARE LOCALLY INDISTINCT (SILICIFICATION?).			
/	330	372	22	3A10QZ	<<		P <<<<
L			10	AN		CL 070	
R				:AS ABOVE 300 TO 330 :MINOR FE OXIDE STAIN ON FRACTS	:CORE		
R				HEAVILY BROKEN TO 34.1 M.			
R				:MOST OF CORE LOSS FROM 33-34.1 M. :LOWER CNT SHARP AND REG.			
R				:TO 3B LOCALLY :AGAIN THERE SEEMS TO BE A SILICA OVERPRINT ON			
R				THE CLASTS.			
/	372	409	24	3G12CL	<<		P <<<+<>
L			07	5G			
R				:TO 3F LOC. :MINOR OXIDE STAINS ON FRACTS. :LOWER CNT NOT			
R				OBSERVED.			
/	409	437	21	3A10QZ	<<		P <<<+
L			09	AN			<<
R				:AS ABOVE 33.0-37.2 M :LOWER CNT GRADATIONAL :TR FE OXIDES ON			
R				FRACTS.			
/	437	450	13	3B10QZ	<<		P <<<<
L			05	AN			<<
R				:W/10% 1C INTERLEVED :LOWER CNT SHARP BUT VERY IRREGULAR.			
/	450	480	29	3G12CL	<<		P <<<<<<<
L			04	5G			
R				:TO AG LOCALLY :TO MOD FRACT LOCALLY.			
/	480	510	29	3G12CL	<<		P <><<<<
L			06	5G			<<
R				:REMARKS AS ABOVE.			
/	510	540	30	3G12CL	<<		P <*<*<*
L			05	5G			
R				:REMARKS AS ABOVE.			
/	540	570	30	3G12CL	<<		P <*<<<<
L			11	5G			<<
R				:REMARKS AS ABOVE :NOTE-FINE ASH			
/	570	600	29	3G12CL	<<		P <><<<<
L				5G			

L			17		GT					
R					:LOC 2D34 INTERBEDDED. SOFT, GREEN, GREASY MINERAL IN <<					
/	1790	1820	29		2C34MSCL <<	P			<-<)<)*<-	
L			21		GT					
R					:MINOR TT OCCURRING WITH CP IN <<					
/	1820	1850	29		2C44MSCL <<BR	P			<-<)<=<*<-	
L			17		GT					<-
R					:MINOR BRECCIA					
/	1850	1880	30		2C34MSCL <<BR	P			<-<)*<=<-	
L			21		GT					
/	1880	1910	29		2C44MSCL <<	P			<-<)<+<(<	
L			11		GT					
/	1910	1940	30		2C34MSCL <<	P			<(<)<+<(<	
L			21		GT					
/	1940	1970	30		2C23MSCL <<	P			<+<*<)<.<.	
L			19		TG					<.
R					:TT AND SL IN << AT 196.6					
/	1970	2000	30		2C34MSCL <<BR	P			<-<(<)<.<(<	
L			20		AT					<-
R					:MINOR BX'D. GOOD TT IN <<					
/	2000	2030	30		2C34MSCL <<	P			<-<)<+<.<-	
L			15		GT					
R					:ROCK BECOMING SILICIOUS TOWARDS BOTTOM OF INTERVAL					
/	2030	2057	26		2C44MSCL <<BR	P			<(<+<+<(<	
L			11		GT					
R					:MINOR BR'X					
/	2057	2062	05		8C00	MXCM	P	CL	40	
L			02		9T					
/	2062	2082	20		8B01	TCCM	P	CL	55	
L			16		AG					D(
/	2082	2110	27		2C43MSCL <<BR	P	F/	35	<(<)<)<B.	
L			06		GT					
R					:CLAY RICH FAULT GOUGE					
/	2110	2140	28		2C53MSCL <<BR	P			<(<)<)<.	
L			09		GTCY					
/	2140	2160	19		2C53MSCL <<BR	P			<(<)*<*<-	
L			03		GTCL					
/	2160	2185	24		2C44MSCL <<BR	P			<(<+<=<-<-	
L			06		GT					
/	2185	2194	09		8C01FL	P*	P	CU	50	
L			06		GY			CL	60	
/	2194	2230	34		2C44MSCL <<BR	P			<(<(<)	
L			03		GTCY					
R					:BR'X ON UPPER CONTACT WITH DYKE					
/	2230	2260	29		2C44MSCL <<	P			<*<(<)	
L			06		GT					<(< <-
/	2260	2290	30		2C24MSCL <<	P			<)<*<+	
L			09		6T					<-
/	2290	2320	29		2C25MSCL <<	P			<(<(<)	
L			08		6T					
R					:BX FILLING PY AT 229.1					
/	2320	2350	29		2C25MSCL <<	P			<(<)<+	
L			06		5T					<-
R					:CLASSIC 2C25 !					
/	2350	2380	29		2C24MSCL <<	P			<(<)<)<.<-	


```

L          05          GT          <-
R          :VERY FINE TT IN WITH HE IN <<'S
/ 2380 2410 29 2C24MSCL << P <<((*)<-<-
L          02          GT
/ 2410 2440 29 2C34MSCL << P <<((*)<+<((
L          11          GT          <<
R          :TT, HE IN <<'S
/ 2440 2470 30 2C55MSCL <<BR P <<((*)<+<-<(*)
L          19          GT          <.
R          :GOOD LOOKING ROCK!!
/ 2470 2500 29 2C34MSCL << P <<((<)<
L          05          GT          <-
/ 2500 2530 30 2C34MSCL << P <<((<)<+<.<.
L          11          GT          <-
/ 2530 2563 33 2C34MSCL <<BR P <<((+<+< <.
L          09          GT          <-
R          :MINOR BR'X AT CONTACT WITH DYKE BELOW
/ 2563 2582 19 8A00 CM P CU 45 <<
L          11          BG CL 60 D(
/ 2582 2600 18 8C00 CMP* P <<
L          06          9T CL 60
/ 2600 2617 17 8A00 CM P <<
L          11          BG D(
R          :LOWER CONTACT IRREGULAR
/ 2617 2636 19 2C55MSCL BR<< P ##=#
L          15          5T <-
R          :COULD BE XENOLITH
/ 2636 2663 26 8A00 MSCM P CU 60 <)<-
L          17          CL 50 D(
/ 2663 2669 06 2C55MSCL BR<< P ##=#
L          03          5T #.
/ 2669 2675 06 8A00 MS P CU 70
L          04          2B CL 50 D(
/ 2675 2700 23 2C35MSCL <<BR P F/ <*<*<+
L          11          5T
R          :MINOR BR'X UNDER DYKE. FAULT GOUGE 268.3 TO 268.5
/ 2700 2723 23 2C24MSCL << P <*<*<
L          06          GT
/ 2723 2760 36 2C12CL << P <)<-<)<
L          06          4G
R          :BANG! GREEN ROCK, FASTEST TRANSITION I'VE SEEN!
/ 2760 2790 28 2C24MSCL << P <*<)<
L          00          GT
R          :CORE VERY BROKEN
/ 2790 2820 28 2C24MSCL << P <<((+<+
L          00          GT
/ 2820 2850 30 2C12CL << P <)<-<-<*<
L          11          TG
/ 2850 2880 30 2C12CL << P <)<+<+<.
L          17          TG
/ 2880 2910 30 2C12CL << P <+<-<)<
L          13          5G
/ 2910 2940 30 2C12CL << P <+<-<-<*<
L          11          5G
/ 2940 2968 27 2C23CLMS << P <*<((+

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```

L          06          GT
/ 2968 2997 29      8B01    <<P*      P CL    25    <-
L          19          BG      CM          D(
/ 2997 3031 33      2C23CLMS <<      P      <+<*<+<.
L          08          GT          <-
/ 3031 3044 13      1C12CL    <<      P      <-<((
L          03          5G
/ 3044 3127 81      2C12CL    <<      P      <+<((*<.
L          36          TG
R          :CONTAINS TO SMALL (0.1 M) INTERVALS OF 1C. TUFF ALSO CONTAINS
R          :OCCASIONAL CHERT PEBBLES.
R          :END OF HOLE AT 312.7 M

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A001
ALAB      EQUITY MINESITE LABORATORY.
ATYP      ASSAY
AMTH      WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM      RCOVSAMPLE  RQD % CU  G/TAG G/TAU % SB % AS % FE % ZN
R          :TRICONED - NO CORE
A001 244 270      6814      0.04      0.5 0.07  0.005 0.005 1.10 0.001
A001 270 300      6815      0.04      0.5 0.05  0.010 0.001 1.88 0.005
A001 300 330      6816      0.09      1.0 0.05  0.020 0.010 1.86 0.010
A001 330 360      6817      0.10      0.5 0.05  0.005 0.010 1.14 0.005
A001 360 390      6818      0.14      0.5 0.09  0.005 0.010 2.30 0.005
A001 390 420      6819      0.09      0.5 0.07  0.005 0.005 2.86 0.005
A001 420 450      6820      0.15      0.5 0.08  0.005 0.001 1.86 0.005
A001 450 480      6821      0.11      0.5 0.08  0.001 0.005 3.46 0.005
A001 480 510      6822      0.13      1.0 0.07  0.001 0.001 4.26 0.005
A001 510 540      6823      0.04      0.5 0.05  0.005 0.001 4.54 0.005
A001 540 570      6824      0.03      0.5 0.03  0.005 0.001 3.87 0.005
A001 570 600      6825      0.03      1.0 0.04  0.005 0.001 4.37 0.005
A001 600 630      6826      0.07      1.0 0.03  0.001 0.010 4.55 0.005
A001 630 660      6827      0.06      1.0 0.05  0.005 0.001 1.46 0.001
A001 660 690      6828      0.06      0.5 0.04  0.010 0.001 1.10 0.005
A001 690 720      6829      0.02      0.5 0.04  0.010 0.010 0.90 0.005
A001 720 750      6830      0.05      0.5 0.05  0.005 0.001 1.14 0.010
A001 750 780      6831      0.08      1.0 0.07  0.010 0.001 2.07 0.010
A001 780 810      6832      0.11      4.0 0.08  0.040 0.005 3.18 0.020
A001 810 830      6833      0.02      0.5 0.04  0.005 0.001 2.69 0.005
A001 830 851      6834      0.06      2.0 0.07  0.010 0.020 3.45 0.005
R 851 860 :DYKE-NO SAMPLE
A001 860 890      6835      0.03      1.0 0.05  0.005 0.001 4.29 0.005
A001 890 920      6836      0.05      1.0 0.09  0.001 0.001 4.08 0.005
A001 920 950      6837      0.10      0.5 0.07  0.005 0.001 3.01 0.005
A001 950 980      6838      0.05      1.0 0.03  0.005 0.001 0.89 0.005
A001 980 1009     6839      0.08      1.0 0.04  0.005 0.001 1.33 0.010
R 1009 1015 :NO CORE-TUBE DIDN'T LOCK
A001 1015 1040     6840      0.05      0.5 0.05  0.005 0.001 2.17 0.005
A001 1040 1070     6880      0.07      1.0 0.06  0.010 0.005 3.82 0.010
A001 1070 1100     6881      0.04      0.5 0.03  0.005 0.005 3.37 0.010
A001 1100 1130     6882      0.19      9.0 0.05  0.050 0.010 4.89 0.020
A001 1130 1160     6883      0.14      3.0 0.05  0.010 0.001 4.54 0.040
A001 1160 1190     6884      0.31      5.0 0.05  0.005 0.010 4.85 0.005
A001 1190 1220     6885      0.15      5.0 0.04  0.010 0.001 4.56 0.050
A001 1220 1250     6886      0.03      2.0 0.05  0.010 0.010 4.73 0.010
A001 1250 1280     6887      0.03      2.0 0.04  0.010 0.020 2.01 0.005

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A001	1280	1310	6888	0.05	2.0	0.03	0.100	0.020	2.66	0.030	
A001	1310	1340	6889	0.04	2.0	0.04	0.010	0.010	2.44	0.020	
A001	1340	1370	6890	0.05	2.0	0.04	0.010	0.005	2.58	0.005	
A001	1370	1400	6891	0.02	2.0	0.03	0.010	0.010	4.22	0.005	
A001	1400	1430	6892	0.02	1.0	0.03	0.010	0.005	2.71	0.005	
A001	1430	1460	6893	0.03	1.0	0.02	0.005	0.005	2.18	0.010	
A001	1460	1490	6894	0.05	3.0	0.04	0.020	0.020	4.71	0.020	
A001	1490	1520	6895	0.01	1.0	0.03	0.005	0.010	4.83	0.005	
A001	1520	1550	6896	0.04	1.0	0.12	0.005	0.010	3.93	0.005	
A001	1550	1580	6897	0.04	2.0	0.09	0.005	0.020	5.33	0.030	
A001	1580	1610	6898	0.03	1.0	0.02	0.005	0.010	5.74	0.005	
A001	1610	1640	6899	0.05	3.0	0.06	0.005	0.010	5.02	0.040	
A001	1640	1670	6900	0.09	2.0	0.04	0.010	0.001	4.54	0.005	
A001	1670	1700	6901	0.30	4.0	0.04	0.010	0.020	4.34	0.005	
A001	1700	1730	6902	1.48	26.0	0.08	0.010	0.010	6.49	0.010	
A001	1730	1760	6903	0.86	11.0	0.04	0.005	0.005	5.04	0.005	
A001	1760	1790	6904	0.32	9.0	0.03	0.005	0.010	4.96	0.001	
A001	1790	1820	6905	0.97	26.0	0.08	0.010	0.020	5.57	0.005	
A001	1820	1850	6906	0.41	22.0	0.13	0.010	0.030	7.76	0.010	
A001	1850	1880	6907	0.16	11.0	0.11	0.010	0.020	10.35	0.020	
A001	1880	1910	6908	0.23	5.0	0.04	0.010	0.005	6.42	0.001	
A001	1910	1940	6909	0.44	8.0	0.04	0.005	0.005	6.85	0.005	
A001	1940	1970	6910	0.11	3.0	0.05	0.005	0.001	4.70	0.140	
A001	1970	2000	6911	0.16	16.0	0.10	0.005	0.020	5.48	0.260	
A001	2000	2030	6912	0.52	25.0	0.06	0.030	0.080	5.17	0.460	
A001	2030	2057	6913	0.18	18.0	0.09	0.001	0.100	5.93	0.020	
R	2057	2082	:DYKE-NO SAMPLE								
A001	2082	2110	6914	0.27	22.0	0.07	0.001	0.001	4.62	0.005	
A001	2110	2140	6915	0.23	9.0	0.04	0.020	0.001	4.11	0.005	
A001	2140	2160	6916	0.14	8.0	0.05	0.020	0.005	3.48	0.005	
A001	2160	2185	6917	0.19	12.0	0.07	0.040	0.020	6.35	0.005	
R	2185	2194	:DYKE-NO SAMPLE								
A001	2194	2230	6918	0.03	3.0	0.04	0.001	0.001	3.95	0.001	
A001	2230	2260	6919	0.03	10.0	0.04	0.005	0.001	4.39	0.001	
A001	2260	2290	6920	0.03	22.0	0.06	0.020	0.001	8.57	0.001	
A001	2290	2320	6921	0.02	2.0	0.05	0.005	0.001	8.50	0.001	
A001	2320	2350	6922	0.07	16.0	0.08	0.020	0.001	4.88	0.005	
A001	2350	2380	6923	0.08	34.0	0.07	0.020	0.001	3.95	0.005	
A001	2380	2410	6924	0.14	83.0	0.08	0.005	0.020	3.85	0.020	
A001	2410	2440	6925	0.83	234.0	0.13	0.130	0.100	4.08	0.070	
A001	2440	2470	6926	0.91	1030.0	0.19	0.480	0.070	5.25	0.170	
A001	2470	2500	6927	0.22	173.0	0.10	0.080	0.020	4.75	0.040	
A001	2500	2530	6928	0.51	511.0	0.14	0.240	0.050	5.79	0.080	
A001	2530	2563	6929	0.03	24.0	0.07	0.005	0.005	4.66	0.001	
R	2563	2617	:DYKE-NO SAMPLE								
A001	2617	2636	6930	0.07	47.0	0.12	0.020	0.001	4.86	0.005	
R	2636	2663	:DYKE-NO SAMPLE								
A001	2663	2669	6931	0.03	23.0	0.12	0.005	0.001	8.50	0.001	
R	2669	2675	:DYKE-NO SAMPLE								
A001	2675	2700	6932	0.03	31.0	0.05	0.005	0.001	9.40	0.005	
A001	2700	2730	6933	0.005	0.1	0.06	0.001	0.001	5.07	0.001	
A001	2730	2760	6934	0.005	0.5	0.05	0.001	0.001	4.39	0.001	
A001	2760	2790	6935	0.005	0.1	0.04	0.001	0.001	3.66	0.001	
A001	2790	2820	6936	0.005	0.1	0.03	0.001	0.001	5.47	0.001	
A001	2820	2850	6937	0.02	0.1	0.07	0.001	0.001	4.67	0.001	

A001	2850	2880	6938	0.07	0.1	0.06	0.001	0.001	5.39	0.001
A001	2880	2910	6939	0.02	0.1	0.08	0.001	0.001	4.03	0.001
A001	2910	2940	6940	0.02	0.1	0.04	0.001	0.001	4.12	0.001
A001	2940	2968	6941	0.03	2.0	0.03	0.001	0.001	3.25	0.001
R	2968	2997	:DYKE-NO SAMPLE							
A001	2997	3030	6942	0.10	0.5	0.04	0.001	0.001	2.65	0.001
A001	3030	3060	6943	0.03	0.5	0.05	0.001	0.001	3.17	0.001
A001	3060	3090	6944	0.02	0.5	0.07	0.001	0.001	3.59	0.001
A001	3090	3127	6945	0.03	0.5	0.03	0.001	0.001	4.22	0.001
R	END OF ASSAYS - END OF LOG									

IDEN6B0201																				
IPRJ																				
S000	00	552	MT	195.7	062.0	-45.0														
S001	552	1515		195.7	062.0	-44.0														
S002	1515	1957		195.7	062.0	-44.5														
/SCL			MT.2	MT.1																
LSCL				MT.2																
/NAM																				
LNAM																				
/	00	37																		
R																				
/	37	61	20	2C12CL	<<															
L			00	6G																
/	61	85	15	2C12CL	<<															
L			00	6G																
R																				
/	85	140	00	NREC																
L			00																	
R																				
/	140	170	22	2C12CL	<<															
L			00	TG																
/	170	198	23	2C22CL	<<															
L			03	5G																
R																				
/	198	238	32	8C00	P*															
L			09	9G																
/	238	270	27	2C12CL	<<															
L			00	6G																
/	270	300	28	2C12CL	<<															
L			05	6G																
/	300	330	28	2C12CL	<<															
L			09	AG																
R																				
/	330	360	29	2C12CL	<<															
L			00	AG																
/	360	390	29	2C12CL	<<															
L			00	AG																
/	390	420	28	2C12CL	<<															
L			00	AG																
R																				
/	420	450	26	2C12CL	<<															
L			00	AG																
R																				
/	450	546	30	2C12CL	<<															
L			00	AG																
R																				
/	546	551	04	8B01FL	P*CM															
L			00	6A	<<VU															
/	551	570	18	2C24MS	<<															
L			00	GT																
R																				
/	570	600	29	2C23MS	<<															
L			05	GT																
/	589	590		X																
L																				

/	600	637	35	2C13MS	<<	P		<*((<)
L			03	AG				
/	637	652	15	8B01	P*TC	P	CU	45 <-
L			09	4A			CL	50 D-
/	652	680	27	2C23MS	<<	P		<)<-(<)
L			00	GT				
R				:CORE VERY BROKEN				
/	680	710	29	2C34MS	<<	P		<)<)<+(<)
L			02	GT				
/	710	740	29	2C34MS	<<BR	P		<)<=<+
L			00	GT				
/	740	770	25	2C23MS	<<	P		<)<)<=<-
L			00	GT				
R				:MASSIVE CG. PYRITE SEAM AT 75.3, BUT POOR RECOVERY				
/	770	800	26	2C23MS	<<	P		<)<)<)
L			00	GT				
/	800	830	29	2C22	<<	P		<)<+<+<.
L			00	GA				
/	830	860	29	2C24MS	<<	P		<*<+<+<-
L			03	AT				<-
/	860	890	28	2C34MS	<<	P		<((+<=<((?<)
L			03	6T				<-<-
/	890	944	43	2C35M6	<<BR	P		<((+<+<-
L			03	6T				
R				:POOR RECOVERY				
/	944	961	17	8B00	TCCM	P	CU	30 <<
L			08	2A			CL	25 D-
/	961	986	24	2C65	<<	P		<-#1#2#(<)
L			09					#-
R				:MINOR 8B AT 96.7				
/	986	1038		8B00	CMTC	P	CU	20 <<
L				3A			CL	35 D-
/	1038	1052	14	2C44MS	<<	P		<*((<)<+(<)
L			00					
/	1052	1100	47	8B01FL	CM	P		<)<D.
L			21	5A				D-
R				:CONTACTS NOT PRESERVED				
/	1100	1130	29	2C44MS	<<	P		<*<+<=<- <-
L			09	GT				<-
R				:LOTS OF DISSEM PY AS WELL				
/	1130	1160	27	2C44MS	<<BR	P		<(((<)<+(<)
L			00	AT				<-
/	1160	1190	29	2C33MS	<<	P		<((+<+<-
L			00	AT				<<
/	1190	1199	09	8A00	MS<<	P	CL	65 <<
L			06	GA	CM			D-
/	1199	1209	09	2C95MSQZ	BR<<	P		#=
L			03	6T				
/	1209	1262	52	8A00	MS	P		<<
L			26	GA				D-Q-
R				:CONTACTS NOT PRESERVED				
/	1262	1304	40	2C34MS	<<BR	P		<-<+<+<.<?
L			08	AT				
/	1304	1316	12	8A00	CM<<	P	CU	65 <-
L			08	GB			CL	35 D-

```

/ 1316 1350 33 2C24MS <<BR P <)<)<+
L 09 AT
/ 1350 1380 29 2C34MS <<BR P <)<+<+
L 06 AT
/ 1380 1410 30 2C34MS <<BR P <((+<+
L 15 AT
/ 1410 1440 30 2C34MS << V/ 65 <*<=<+
L 17 AT
/ 1440 1470 30 2C34MS << P V/ 70 <)<=<+
L 05 AT
R :BIG VEINS IN LAST TWO INTERVALS ARE QZ-PY, 5 CM WIDE
/ 1470 1500 30 2C24MS << P <(()<+
L 07 AT
/ 1500 1530 29 2C24MS << P V/ 65 <-<)<+<.
L 05 AT
R :VEIN IS PY-QZ, 5 CM WIDE
/ 1530 1560 29 2C34MS << P <((+<+
L 05 6T
/ 1560 1590 30 2C34MS << P <-<+<+ <.
L 09 AT
/ 1590 1620 30 2C34MS <<BR P <-<+<+<.<*<
L 11 6T <<
R :GOOD TT, IN << AND ANGULAR BX AT 161.3
/ 1620 1650 30 2C55MSQZ <<BR P <.<=<+ <<
L 16 AT <<
R :BX WEAK., TT IN <<
/ 1650 1680 30 2C34MS <<BR P <((+<+ <<
L 09 AT <-
/ 1680 1710 30 2C33MSCL << P <*<((*<
L 15 6T
/ 1710 1740 28 2C34MS <<BR P <(((<(< <<
L 03 AT
R :MINOR BX'D
/ 1740 1770 28 2C34MS << P <*<+<+ <-
L 00 AT <<
/ 1770 1800 29 2C33MS << P <*<+<+ <.
L 05 AT <.
R :<< WITH TT-SL AT 178.6, ONLY OCCURRANCE
/ 1800 1830 30 2C23MSCL << P <)<)<(<
L 09 6T
R :ROCK TURNING GREEN!
/ 1830 1862 31 2C33MS << P <*<+<+<. <<
L 00 6T <-<-
R :ESSENTIALLY ALL TT, SL, CP OCCUR FROM 185.8 TO 186.1
/ 1862 1890 28 2C34MS << P <((=<+
L 09 AT <-
/ 1890 1923 32 2C33MSCL << P <*<+<+<.
L 09 6T <<
/ 1923 1957 33 2C23MSCL << P <*<)<(<
L 12 AT
R :END OF HOLE

```

A001
ALAB
ATYP
AMTH

EQUITY MINESITE LABORATORY
ASSAY
WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

AUMM		RCOVSAMPLE	RQD % CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN	
R	00	37 :TRICONED -	NO CORE							
A001	37	61	6946	0.03	2.0	0.01	0.005	0.010	4.17	0.010
A001	61	85	6947	0.02	0.5	0.02	0.005	0.001	2.76	0.005
R	85	140 :TRICONED -	NO CORE							
A001	140	170	6948	0.03	1.0	0.02	0.001	0.001	3.75	0.005
A001	170	198	6949	0.02	0.5	0.06	0.001	0.020	3.50	0.005
R	198	238 :DYKE -	NO SAMPLE							
A001	238	270	6950	0.04	1.0	0.02	0.005	0.001	3.22	0.005
A001	270	300	6951	0.05	0.5	0.03	0.005	0.005	3.88	0.005
A001	300	330	6952	0.03	0.5	0.04	0.005	0.010	2.91	0.005
A001	330	360	6953	0.03	0.5	0.01	0.001	0.030	3.14	0.005
A001	360	390	6954	0.04	0.5	0.02	0.001	0.010	2.54	0.005
A001	390	420	6955	0.06	1.0	0.02	0.005	0.005	3.80	0.005
A001	420	450	6956	0.09	2.0	0.01	0.005	0.001	3.38	0.010
A001	450	540	6957	0.06	1.0	0.02	0.005	0.005	3.05	0.030
A001	540	570	6958	0.06	1.0	0.04	0.001	0.010	3.58	0.030
A001	570	600	6959	0.11	2.0	0.11	0.001	0.140	3.85	0.170
A001	600	639	6960	0.03	0.5	0.02	0.010	0.010	3.99	0.010
R	639	652 :DYKE -	NO SAMPLE							
A001	652	680	6961	0.05	3.0	0.03	0.005	0.030	3.08	0.210
A001	680	710	6962	0.39	6.0	0.04	0.005	0.001	3.55	0.005
A001	710	740	6963	0.03	1.0	0.03	0.005	0.020	3.50	0.005
A001	740	770	6964	0.14	2.0	0.02	0.005	0.001	6.20	0.005
A001	770	800	6965	0.11	4.0	0.02	0.005	0.001	3.44	0.005
A001	800	830	6966	0.06	1.0	0.03	0.005	0.005	3.69	0.005
A001	830	860	6967	0.08	2.0	0.03	0.005	0.010	2.47	0.020
A001	860	890	6968	0.29	12.0	0.03	0.010	0.030	3.62	0.300
A001	890	944	6969	0.19	10.0	0.02	0.005	0.005	2.34	0.010
R	944	961 :DYKE -	NO SAMPLE							
A001	961	986	6970	0.16	10.0	0.12	0.005	0.030	7.09	0.010
R	986	1038 :DYKE -	NO SAMPLE							
A001	1038	1052	6971	0.47	14.0	0.03	0.005	0.010	2.84	0.010
R	1052	1100 :DYKE -	NO SAMPLE							
A001	1100	1130	6972	0.38	11.0	0.04	0.001	0.010	5.47	0.005
A001	1130	1160	6973	0.51	20.0	0.04	0.070	0.010	5.24	0.030
A001	1160	1190	6974	0.14	8.0	0.04	0.060	0.001	5.36	0.030
R	1190	1199 :DYKE -	NO SAMPLE							
A001	1199	1209	6975	0.02	1.0	0.03	0.005	0.001	2.46	0.005
R	1209	1262 :DYKE -	NO SAMPLE							
A001	1262	1283	6976	0.03	2.0	0.05	0.005	0.010	3.78	0.005
A001	1283	1304	6977	0.05	4.0	0.07	0.005	0.001	4.18	0.005
R	1304	1316 :DYKE -	NO SAMPLE							
A001	1316	1350	6978	0.07	4.0	0.04	0.005	0.010	3.69	0.005
A001	1350	1380	6979	0.08	3.0	0.07	0.005	0.001	3.96	0.005
A001	1380	1410	6980	0.04	3.0	0.06	0.010	0.010	5.94	0.005
A001	1410	1440	6981	0.02	1.0	0.08	0.010	0.001	6.87	0.005
A001	1440	1470	6982	0.02	1.0	0.03	0.005	0.001	4.85	0.005
A001	1470	1500	6983	0.01	1.0	0.03	0.005	0.001	4.04	0.005
A001	1500	1530	6984	0.01	3.0	0.04	0.005	0.020	4.72	0.005
A001	1530	1560	6985	0.04	2.0	0.04	0.020	0.010	4.32	0.010
A001	1560	1590	6986	0.03	3.0	0.03	0.010	0.001	4.28	0.090
A001	1590	1620	6987	0.19	38.0	0.11	0.080	0.010	3.44	5.140
A001	1620	1650	6988	0.08	10.0	0.07	0.040	0.020	4.41	0.940
A001	1650	1680	6989	0.02	10.0	0.03	0.010	0.030	3.87	0.360

A001	1680	1710	6990	0.04	5.0	0.08	0.010	0.001	3.61	0.380
A001	1710	1740	6991	0.04	13.0	0.04	0.020	0.020	4.00	0.430
A001	1740	1770	6992	0.01	2.0	0.03	0.010	0.010	4.42	0.160
A001	1770	1800	6993	0.005	2.0	0.02	0.010	0.020	4.42	0.010
A001	1800	1830	6994	0.02	3.0	0.04	0.010	0.005	5.13	0.005
A001	1830	1862	6995	0.25	99.0	0.06	0.110	0.005	5.24	0.810
A001	1862	1890	6996	0.02	5.0	0.02	0.020	0.005	6.48	0.010
A001	1890	1923	6997	0.09	0.5	0.06	0.040	0.005	4.99	0.010
A001	1923	1957	6998	0.01	0.5	0.02	0.005	0.005	4.20	0.005

R :END OF ASSAYS - END OF HOLE
R END OF ASSAYS - END OF LOG

IDEN6B0201		X86CH264 NQ	JUL86RBP	G&D JUL86S38	0.0	
IPRJ		EQUITY SILVER MINES LTD		SUPERSTITION ZONE - ST GEOCODE		
S000	00	488 MT	251.5 090.0 -45.0	5611.87	7435.93	1107.05
/SCL		MT.2MT.1				
LSCL		MT.2				
/NAM					MSCLQZPYCPTTASPR	
LNAM					CBGY MGHESLGLMO	
/	00	104		DVBN	P	
R				:TRICONED - NO CORE		
/	104	130	26	3F11CL <<	P	<)<+<*
L			05	GA		
R				:VERY LITTLE RUST ON <<		
/	130	160	30	3F11CL <<	P	<+<)<*
L			19	AG		
/	160	190	30	3F13CLMS <<	P	<)<)<*
L			15	GA		
R				:MINOR MS-QZ ALT'N ENVELOPE ON <<		
/	190	220	30	3F12CL <<	P	<+<((
L			17	GA		
/	220	247	27	3F13CLMS <<	P	<)<+<((
L			09	TG		
/	247	280	33	3A11QZ <<	P	<((+<*
L			12	AW		
R				:TYPICAL, VERY SILICOUS, CHERT PEBBLE CONGLOMERATE		
/	280	310	30	3A21QZ <<	P	<((+<*
L			14	AW		
/	310	340	30	3A21QZ <<	P V/	25 <((=<+ <.
L			10	AW		
R				:NOT SURE ABOUT ARSENO, VERY SMALL OCCURRANCE WITH QZ-PY		
/	340	370	30	3A21QZ <<	P	<((+<)
L			09	AW		
/	370	397	27	8C02CY P*CM	P CU	45 <-
L			09	WT	CL	45
/	397	430	33	3A11QZ <<	P	<(()<*
L			15	AW		
/	430	460	29	3A21QZ <<	P	<((+<)
L			09	AW		
/	460	499	38	3A21QZ <<	P	<((+<)
L			08	AW		
/	499	505	06	3E11 <<	P BD	50 <(((
L			04	TG	CL	50
R				:TOP CONTACT GRADATIONAL, BOTTOM SHARP!		
/	505	569	53	3A11QZ <<	P	<((*)<)<.
L			18	AW		
R				:MINOR CP IN << AT 53.1		
/	569	616	46	3B11QZ <<	P BD	50 <*<)<)<.
L			21	AG	CL	90
R				:TOP CONTACT GRADATIONAL, BOTTOM SHARP. MINOR CP AT 58.5		
R				:BOTTOM CONTACT IRREGULAR		
/	616	670	52	3A11QZ <<	P	<(()<*
L			14	AW		<((
/	670	700	29	3A11QZ <<	P	<.<+<((
L			06	AW		<-
R				:RUST ON FRACTURES (MINOR)		
/	700	729	28	3A21QZ <<	P	<.<+<*

L 11 AW
 R :LOWER CONTACT IS SHARP, BUT IRREGULAR
 / 729 760 31 3F12CL << P <><+<<.
 L 19 AG
 R :SMALL (0.1 M) 3B AT TOP OF INTERVAL. STRAT COULD BE UNIT 2?
 / 760 790 30 3F22CL << P <+<+<<.
 L 17 AG
 / 790 820 30 3F22CL << P V/ 40 <<<+<*.
 L 15 AG
 R :TUFF CONTAINS ABUNDANT BLACK SHARDS. MINOR QZ-SER ALT'N ON
 R :SOME <<
 / 820 846 26 3F23CLMS << P <*><<<.
 L 09 TG
 / 846 858 11 3B12CL << P <<<<<<.
 L 03 AG
 R :UPPER CONTACT IS GRADATIONAL OVER 0.3 M
 / 858 864 05 8A01 << P <*
 L 02 7G CL 70 <*><-
 / 864 873 09 3B12CL << P BD 70
 L 03 AG
 R :LOWER CONTACT GRADATIONAL, CONTAINS 0.2 CM WIDE 2C. TO BEDDING
 / 873 890 17 3J12CL << P BD 70 <<<<<<
 L 09 AG
 R :INTERBEDS ARE JUST OVER 1.0 CM WIDE
 / 890 940 49 2C23CL << P <<<+<*-
 L 20 TG
 R :SLIGHT QZ-SER ALT'N ON <<. THIS IS LIKELY THE ACTUAL
 R :TRANSITION INTO UNIT 2
 / 940 970 30 2C22CL << P <+<><>
 L 11 AG
 / 970 1000 30 2C23CLMS << P <*<+<+<<
 L 19 AT
 R :MINOR 2D INTERBED
 / 1000 1030 30 2C22CL << P <*<<<<-
 L 21 AG
 R :MOST OF CP AT 100.4
 / 1030 1060 30 2C12CL << P <><><*<
 L 11 AG
 R :MINOR 2D
 / 1060 1090 30 2C12CL << P <><><##- #?
 L 09 AG
 R :MOST CP IN SMALL BX AT 107.7 M. MAYBE SOME ARSEND TOO
 / 1090 1120 28 2C13CLMS << P <+<><><-
 L 06 TG
 / 1120 1150 30 2C12CL << P <+<><<<.
 L 14 AG
 / 1150 1180 29 2C22CL << P <+<><><-<-
 L 16 AG <- <<
 R :MINOR QZ-SER ALT'N AT 117.6, WITH TT, SL, CP
 / 1180 1210 30 2C22CL << P <><+<><.
 L 19 AG
 R :AGAIN, MINOR QZ-SER ALT'N
 / 1210 1240 30 2C23CLMS << P <><><*<
 L 19 AG
 / 1240 1270 30 2C23CLMS << P <><+<*-

L			17	TG							
/	1270	1300	30	2C22CL	<<	P		<+<)<*<.			
L			17	AG							
/	1300	1330	29	2C32CL	<<	P		<+<+<*			
L			12	AG							
/	1330	1376	44	2C45MSQZ	<<BR	P		#+<+B(
L			18	6T							
/	1376	1386	08	8B01CY	<<P*	P	CU	40			
L			00	7A			CL	35			
/	1386	1420	31	2C45MSQZ	BR<<	P			#1#+#(
L			17	AT							
R				:NO VISIBLE TT BUT COULD BE LOW GRADE AG							
/	1420	1450	30	2C54MSQZ	<<BR	P	V/	65	<1#+#*		
L			12	AT							
/	1450	1480	29	2C34MSQZ	<<BR	P	V/	60	<=<+<-		
L			05	AT							
/	1480	1500	20	2C44MSQZ	<<BR	P			<+<)<-<?		
L			06	AT							
/	1500	1571	70	8B01CY	<<P*	P	CU	50	D(
L			36	GA	CM		CL	65	D-		
R				:CL-CY REPLACE FL LATHS							
/	1571	1588	17	2C64MSQZ	<<BR	P			#1#+B-		
L			06	AT							
/	1588	1594	06	8A02CL	<<CM	P	CU	55	<=		
L			03	6G			CL	60			
R				:PERSAVSIVE CL ALT'N							
/	1594	1619	23	2C64MSQZ	BR<<	P			+1#+B-B(
L			06	6T							
R				:0.1 M OF 8C AT 160.4. BOTTOM 0.4 M CY RICH BX; LIKELY FAULT							
R				:GDUGE							
/	1619	1623	04	8C12CY	<<	P	CU	50			
L			00				CL	60			
/	1623	1643	20	2C54MSQZ	BR<<	P			<=#)B.		
L			03	AT							
/	1643	1653	10	8A10	<<CM	P	CU	65	A=		
L			10	4G			CL	65A*			
R				:0.1 M 8C MARGINS. SOLID PIECE OF CORE							
/	1653	1680	27	2C43MSQZ	<<BR	P			#=0=B(B(
L			14	AT					B-		
/	1680	1710	29	2C34MSQZ	<<	P			<)<1<=<-<-		
L			13	AT					<-		
/	1710	1740	30	2C34MS	<<	P			<)<+<+<.<-		
L			21	AT					<*		
/	1740	1770	30	2C34MS	<<	P			<)<=<+<-<-B?		
L			17	AT					<*		
/	1770	1800	30	2C34MS	<<	P			<)<+<)<*<-		
L			11	AT					<(
R				:TT OCCURS IN << WITH SL, IDENTIFICATION DIFFICULT							
/	1800	1830	29	2C33MS	<<	P			<*<=<+<(<*		
L			08	AT					<)		
R				:MOST SL, TT, CP OCCURS IN TOP HALF OF INTERVAL							
/	1830	1860	30	2C33MS	<<	P	V/	65	<*<+<-<.		
L			17	AT					<)		
/	1860	1890	30	2C23MS	<<	P			<*<+<-<-		
L			11	AT							

/	1890	1920	30	2C23CLMS	<<	P		<+<><+<.
L			14	GT				
/	1920	1950	29	2C23CLMS	<<	P		<+<><-
L			07	GT				<.
/	1950	1980	30	2C33CLMS	<<	P		<><><+<-<?
L			09	GT				<-
R				:MINOR 2D				
/	1980	2010	30	2C43CLMS	<<	P		<><+<=<(<?
L			09	TG				<<
R				:GENERAL REMARK: MOST OF ABOVE SL, CP, TT OCCURS IN IRREGULAR				
R				:GASHES, ALL THE WAY BACK TO 168.0				
/	2010	2040	30	2C43CLMS	<<	P		<*<=<+<-
L			18	GT				
/	2040	2078	37	2C43CLMS	<<BR	P		<*<+<><-
L			16	TA				<*
R				:MINOR BX, NOT NOT AT DYKE CONTACT				
/	2078	2096	18	8C00FL	P*CM	P		A)
L			16	9G		CL	70	
/	2096	2130	32	2C44MSQZ	<<	P		<+<><(<*<-
L			06	AT				<-
/	2130	2160	30	2C43CLMS	<<	P		<><+<1<><*<-
L			12	TA				<*
R				:MINOR 2D, SPOTTY STRONG DISSEM. FY				
/	2160	2190	30	2C43MS	<<BR	P		<><+<=<(<?
L			13	AT				
R				:VERY FINE GRAINED GRAY-BLUE IN << WITH CP, TT ?				
/	2190	2220	30	2C33CLMS	<<	P		<+<*<+<-<?
L			15	AT				<.
R				:AS ABOVE				
/	2220	2250	30	2C33CLMS	<<	P		<+<><+<(<-
L			21	AT				<-
/	2250	2280	30	2C33CLMS	<<BR	P		<+<*<+<-
L			12	AT				
R				:CP OCCURS ONLY AT 227.0				
/	2280	2310	30	2C33CLMS	<<BR	P		<+<+<=<(<
L			15	AT				
/	2310	2340		2C33CLMS	<<	P		<+<=<=<(<?
L			15	AT				#+
R				:MINOR 2D. LOTS OF SL, NO POSITIVE ID OF TT, BUT SUSPECT SOME				
R				:IN WITH THE SL				
/	2340	2370	30	2D23CLMS	<<	P		<+<=<+<?
L			12	TA				<-
R				:SOME INTERBEDDED 2C. SL OCCURS ONLY IN FIRST 0.2 M OF INTERVAL				
/	2370	2399	28	2C23CLMS	<<	P		<=<+<+
L			05	TA				
/	2399	2408	09	8A11CL	<<P*	P		D+<+D)
L			09	7G				
R				:CONTACTS SHARP, BUT IRREGULAR				
/	2408	2440	31	2D22CL	<<	P	BD	60 <=<*<>
L			09	TA				<.
R				:INTERBEDDED 2C				
/	2440	2462	22	2C44CLMS	<<	P		<=<*<> <?
L			12	AT				<*
R				:NO POSITIVE ID ON TT, BUT SUSPECT IN WITH SL				
/	2462	2484	22	2C44MSCL	<<	P		<=<*<*<?

L 05 GT (<)
R :AS ABOVE, SL OCCURS ONLY IN TWO <<'S
/ 2484 2515 31 BA10 <<A* P CU 40 A=<-
L 28 BA D+
R :QTZ ALSO OCCURS IN <<'S. HOLE ENDS IN DYKE
R :HOLE LIKELY SHOULD HAVE BEEN CONTINUED. I SHUT IT DOWN BECAUSE
R :OF THE INCREASE OF CL IN <<'S
R :END OF HOLE

A001
ALAB
ATYP
AMTH
AUMM

EQUITY MINESITE LABORATORY
ASSAY

WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

	RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN	
R	00	104	:TRICONED - NO CORE							
A001	104	130	6999	0.05	0.5	0.02	0.005	0.005	3.27	0.010
A001	130	160	7000	0.04	0.5	0.02	0.005	0.005	3.64	0.005
A001	160	190	7001	0.04	0.5	0.02	0.005	0.005	4.18	0.005
A001	190	220	7002	0.04	0.5	0.04	0.005	0.005	4.45	0.005
A001	220	250	7003	0.03	0.5	0.01	0.005	0.005	3.35	0.005
A001	250	280	7004	0.04	0.5	0.02	0.005	0.005	0.78	0.005
A001	280	310	7005	0.05	3.0	0.03	0.01	0.005	1.31	0.04
A001	310	340	7006	0.02	2.0	0.02	0.005	0.005	6.01	0.005
A001	340	370	7007	0.06	0.5	0.01	0.005	0.005	1.15	0.005
R	370	397	:DYKE - NO SAMPLE							
A001	397	430	7008	0.06	0.5	0.005	0.005	0.005	0.88	0.005
A001	430	460	7009	0.10	0.5	0.01	0.005	0.005	1.36	0.005
A001	460	490	7010	0.05	0.5	0.005	0.005	0.005	0.58	0.005
A001	490	520	7011	0.05	0.5	0.005	0.005	0.005	2.20	0.005
A001	520	550	7012	0.10	0.5	0.005	0.005	0.005	0.69	0.005
A001	550	580	7013	0.07	0.5	0.07	0.005	0.005	1.06	0.005
A001	580	610	7014	0.14	2.0	0.02	0.005	0.005	1.84	0.005
A001	610	640	7015	0.07	0.5	0.02	0.005	0.005	2.02	0.005
A001	640	670	7016	0.05	0.5	0.03	0.005	0.005	1.48	0.02
A001	670	700	7017	0.06	0.5	0.03	0.005	0.005	0.98	0.005
A001	700	730	7018	0.09	3.0	0.04	0.001	0.001	0.82	0.005
A001	730	760	7019	0.06	2.0	0.04	0.001	0.001	4.04	0.001
A001	760	790	7020	0.09	2.0	0.07	0.001	0.001	2.80	0.001
A001	790	820	7021	0.06	0.5	0.06	0.001	0.001	2.73	0.001
A001	820	850	7022	0.13	2.0	0.06	0.001	0.001	3.10	0.001
A001	850	880	7023	0.10	2.0	0.04	0.001	0.001	2.89	0.001
A001	880	910	7024	0.11	2.0	0.05	0.001	0.001	4.27	0.001
A001	910	940	7025	0.07	0.5	0.04	0.001	0.001	4.01	0.001
A001	940	970	7026	0.09	2.0	0.07	0.001	0.001	3.70	0.001
A001	970	1000	7027	0.26	13.0	0.06	0.001	0.001	3.57	0.001
A001	1000	1030	7028	0.13	4.0	0.03	0.001	0.001	4.07	0.001
A001	1030	1060	7029	0.05	0.1	0.03	0.001	0.001	2.37	0.001
A001	1060	1090	7030	0.13	3.0	0.06	0.001	0.001	3.70	0.001
A001	1090	1120	7031	0.09	3.0	0.02	0.001	0.001	2.52	0.03
A001	1120	1150	7032	0.07	2.0	0.04	0.001	0.001	2.99	0.001
A001	1150	1180	7033	0.11	4.0	0.04	0.001	0.001	2.30	0.12
A001	1180	1210	7034	0.11	3.0	0.03	0.001	0.001	2.42	0.005
A001	1210	1240	7035	0.09	4.0	0.04	0.001	0.001	2.77	0.02
A001	1240	1270	7036	0.08	4.0	0.01	0.001	0.001	3.01	0.005
A001	1270	1300	7037	0.11	6.0	0.05	0.001	0.001	3.64	0.02
A001	1300	1330	7038	0.12	9.0	0.02	0.001	0.001	2.76	0.03

A001	1330	1360	7039	0.28	27.0	0.18	0.005	0.04	2.96	0.05
A001	1360	1390	7040	0.14	28.0	0.18	0.005	0.005	3.84	0.001
A001	1390	1420	7041	0.19	46.0	0.07	0.005	0.001	3.03	0.001
A001	1420	1450	7042	0.22	57.0	0.04	0.005	0.001	4.08	0.001
A001	1450	1480	7043	0.07	8.0	0.04	0.001	0.001	3.56	0.005
A001	1480	1500	7044	0.06	5.0	0.04	0.001	0.001	2.87	0.005
R	1500	1571	:DYKE - NO SAMPLE							
A001	1571	1588	7045	0.33	14.0	0.04	0.02	0.001	3.33	0.21
R	1588	1594	:DYKE - NO SAMPLE							
A001	1594	1619	7046	0.29	7.0	0.04	0.001	0.001	3.01	0.09
R	1619	1623	:DYKE - NO SAMPLE							
A001	1623	1643	7047	0.04	3.0	0.04	0.005	0.001	3.84	0.005
R	1643	1653	:DYKE - NO SAMPLE							
A001	1653	1680	7048	0.33	11.0	0.05	0.005	0.001	4.43	0.09
A001	1680	1710	7049	0.17	6.0	0.03	0.001	0.001	4.34	0.08
A001	1710	1740	7050	0.06	3.0	0.03	0.001	0.001	3.08	0.02
A001	1740	1770	7051	0.05	3.0	0.03	0.001	0.001	2.35	0.02
A001	1770	1800	7052	0.04	3.0	0.03	0.001	0.001	2.48	0.37
A001	1800	1830	7053	0.12	7.0	0.03	0.001	0.001	6.78	0.41
A001	1830	1860	7054	0.13	3.0	0.03	0.001	0.001	5.01	0.005
A001	1860	1890	7055	0.16	0.5	0.03	0.001	0.001	4.54	0.001
A001	1890	1920	7056	0.12	3.0	0.04	0.001	0.001	4.75	0.005
A001	1920	1950	7057	0.10	0.5	0.02	0.04	0.005	3.77	0.03
A001	1950	1980	7058	0.12	0.5	0.02	0.03	0.005	4.11	0.02
A001	1980	2010	7059	0.17	0.5	0.03	0.06	0.005	5.52	0.03
A001	2010	2040	7060	0.08	0.5	0.03	0.01	0.005	4.35	0.02
A001	2040	2078	7061	0.10	0.5	0.03	0.06	0.005	4.15	0.03
R	2078	2096	:DYKE - NO SAMPLE							
A001	2096	2130	7062	0.09	0.5	0.02	0.04	0.005	3.30	0.08
A001	2130	2160	7063	0.26	0.5	0.03	0.09	0.01	5.55	0.06
A001	2160	2190	7064	0.18	0.5	0.03	0.04	0.005	4.46	0.005
A001	2190	2220	7065	0.07	0.5	0.01	0.005	0.005	4.16	0.005
A001	2220	2250	7066	0.08	0.5	0.02	0.005	0.005	3.56	0.11
A001	2250	2280	7067	0.07	0.5	0.02	0.005	0.005	4.95	0.005
A001	2280	2310	7068	0.08	0.5	0.02	0.005	0.005	4.13	0.01
A001	2310	2340	7069	0.10	0.5	0.02	0.01	0.005	5.10	0.54
A001	2340	2370	7070	0.06	0.5	0.02	0.01	0.005	3.07	0.05
A001	2370	2399	7071	0.06	0.5	0.02	0.01	0.005	3.67	0.07
R	2399	2408	:DYKE - NO SAMPLE							
A001	2408	2440	7072	0.04	0.5	0.02	0.01	0.005	3.42	0.02
A001	2440	2462	7073	0.04	0.5	0.04	0.01	0.01	3.45	0.51
A001	2462	2484	7074	0.05	0.5	0.05	0.005	0.01	3.12	0.50
R	2484	2515	:DYKE - NO SAMPLE							
R			:END OF HOLE - END OF LOG							
R			END OF ASSAYS - END OF LOG							

IDEN6B0201										
IPRJ										
S000	00	457	MT	168.9	090.0	-45.0				
S001	457	1302		168.9	090.0	-44.5				
S002	1302	1689		168.9	090.0	-42.5				
/SCL			MT.2	MT.1						
LSCL				MT.2						
/NAM										
LNAM										
/	00	488								
R										
/	488	520	29	2C34MS	<<BR		P <<	60	<<<+<=B.	
L			08	AT						
R										
/	520	549	27	2D44CL	<<BR		P		<<<=<=B.	
L			09	6A						
R										
/	549	552	03	8C11	<<		P CU	65	<.	
L			00	YT	VU					
/	552	579	25	2C44MS	<<BR		P		<<<=<=<-<.	
L			08	AT						
R										
/	579	613	31	2C34MS	<<BR		P		<<<+<=Q*<.	
L			15	AT						
R										
/	613	623	09	8B13MS	<<AA		P		<<	
L			08	5T						
R										
R										
/	623	653	27	2C44MS	<<BR		P		<*<+<=B.	
L			11	AT						
R										
/	653	690	37	2C44MS	<<BR		P		<<<=<=P-	
L			11	AT						
/	690	690		X			D		+4	
R										
/	690	715	25	2C44MS	<<BR		P <<	60	<<<=<=	
L			08	AT						
R										
R										
/	715	745	28	2D44CL	<<BR		P		<+<=	
L			03	TA						
R										
R										
/	745	772	24	2D44CL	<<BR		P		<+<=	
L			06	TA						
R										
/	772	803	28	2D44CL	<<BR		P		<+Q=	
L			08	TA						
R										
/	803	833	26	2C44MS	<<BR		P		<-<+Q=	
L			03	AT						
/	803	805		X			D V1	60		
R										
/	833	863	28	2C34MS	<<BR		P		<<<+<=B.	

L 06 AT
 R :SOME FE STAINING. :AGAIN SOME STRANGE FELDSPARS AS BEFORE
 / 863 893 25 2C34MS << P <<<+<+
 L 00 AT
 / 864 865 X D V1 55
 R :.1 M OF QTZ-PY VEIN FROM 86.4 TO 86.5 M
 / 893 923 26 2C45MS <<BR P <<<+<+.
 L 02 AT
 R :SOME PATCHY PYRITE. :IDENTIFIED BLUE-GRAY MIN. (CHLORITE?)
 R :ROCK CONTAINS FINE GLASS SHARDS. :ALSO SOME FE STAINING.
 R :SOME VEINS OF ALTERED FELDSPAR(?)
 / 923 953 27 2C44MS <<BR P <<<+<=<-
 L 02 AT
 R :SLIGHT FE STAINS. :AGAIN FELDSPAR AS ABOVE. :SOME PY PATCHY
 / 953 983 28 2C44MS << P <*<+<+
 L 02 AT
 R :SOME MASSIVE PY AND SOME MINOR QTZ FLOODING. :SOME FE STAINS
 / 983 1013 29 2C34MS <<BR P WP 35 <<<+<+ <.
 L 06 6T Q-
 R :SOME FE STAINING. :SOME CARONATE AGAIN FELDSPAR TOO
 R :TT ONLY AT 99.2 M
 / 1013 1043 27 2C44MS <<BR P <<<+<+
 L 00 AT
 R :AGAIN ALT. FELDSPAR. :FE STAIN AT BEGINNING OF INT
 / 1043 1073 29 2C44MS <<BR P <<<+<+ B.
 L 00 AT Q.
 R :MINDR FE STAINS :TT ONLY AT 105.9 M :QTZ-PY VEIN FOR 0.1 M
 R :FROM 107.4 - 107.5 M
 / 1073 1103 29 2C44MS <<BR P <<<+<=
 L 05 AT
 R :GOOD BRECCIATION FROM 107.5 - 107.7 M
 / 1103 1133 28 2C43MSCL <<BR P <+<+<.
 L 03 ATAG
 R :0.1 M OF QTZ-PY VEIN FROM 112.9 - 113.0 M :AGAIN FELDS PATCHES
 R :SOME INTERBEDDED 2D :GOOD BR'N AT START OF INT
 / 1133 1163 29 2C44MS <<BR P <<<+<=<-
 L 05 AT <.<.
 R :SOME FE STAINING :SL MAYBE QUESTIONABLE
 / 1163 1193 28 2C44MS <<BR P <*<+<=
 L 03 AT
 R :SOME FE STAINING
 / 1193 1223 29 2C43MS << P <*<+<+
 L 02 AT B.
 R :SOME FELDSPAR BLEBS. FE STAINS
 / 1223 1253 28 2C44MS <<BR P <<<+<+<.
 L 03 AT Q.
 R :CP ONLY FROM 124.0 - 124.1 M :MINOR FE STAINS :LAST METER
 R :MAINLY ASH :QTZ-PY VEIN .1 M - CANNOT DETERMINE C1
 / 1253 1283 27 2C43MS <<BR P <*<+<+<.
 L 00 AT <.B.
 R :SP & GL ONLY AT 127.8 M
 / 1283 1313 28 2C44MS <<BR P <<<+<=
 L 00 AT <*<
 R :GY FROM 129.8 - 130.5 M
 / 1313 1336 26 2C44MS << P <<<+<=Q<<.

L 08 AT ((
 R :GREY-BLUE HIGH LUSTRE MIN - UNIDENTIFIED TT(?)
 / 1336 1360 23 2C44MS <<BR P <<((+<<((.
 L 03 AT <.
 / 1360 1379 19 8A11CL <<FB P <.<.
 L 11 AG A*
 / 1379 1389 09 2C44MS <<BR P CU 50 <+<+<.<)
 L 06 AT <.<*)
 R :STRONGLY BRECCIATED AT BEGINNING OF INT
 / 1389 1415 25 8A11CL << P CL 45 <(
 L 21 AG <.<.
 R :CARBONATE AMYGDS :INTERIOR 8A DYKE WITH SLIGHTLY DIFF. TEXT.
 / 1415 1445 28 2C44MS <<BR P <+<+<=
 L 03 AT <.Q(
 R :HE ONLY AT 144.6 M :PY-QZ VEIN (.2 M) FROM 143.7 - 143.9 M
 / 1445 1475 29 2C44MS << P <)<+<+
 L 08 AT
 R :SOME INTERBEDDED 2D
 / 1475 1505 29 2C44MS <<BR P <<((+<=
 L 05 AT <)
 R :SOME SL IN PATCHES
 / 1505 1535 29 2C44MS <<BR P <<((+<=<.<.
 L 08 AT <(
 R :HE MAY BE MIXED WITH SL :CP ONLY IN 2 PLACES (IN <<)
 / 1535 1550 14 2C44MS <<BR P << 55 <<((+<+<.<.
 L 06 AT <?<(
 R :BLUISH GRAY MIN WITH SL << - MAYBE SPECULARITE - CAN'T TELL!
 / 1550 1558 07 8A11CL << P
 L 06 SG
 R :CARBONATE AMYGDS :CONTACTS NOT MEAS. DUE TO BROKEN CORE
 / 1558 1589 29 2C44MS <<BR P <<((+<=<.<.
 L 08 AT <.
 R :BRITTLE PURPLE-BLUE MIN. AGAIN(?) :3 CM PY-QZ VEIN AT 158.6 M
 / 1589 1621 31 2C44MS <<BR P <<((+<=<*<-
 L 09 AT <?<)
 R :AGAIN BLUE GRAY MIN WITH SL - COULD BE SPECULARITE
 R :0.4 M OF STRONGLY BRECCIATED CORE WITH GOOD TT, CP, SL
 R :FROM 161.6 M
 / 1621 1653 31 2C44MS <<BR P << 50 <<((+<+Q-<-
 L 14 AT Q. <?<(
 R :SOME GOOD FRACTURING :ROCK STARTING TO TURN GREENER AT END
 R :OF INTERVAL
 / 1653 1671 17 2C33MS << P <)<+<)<.<.
 L 06 AT <?<-
 R :TT AT 165.7 M
 / 1671 1689 16 2C43MS <<BR P <)<+<)<.<.
 L 00 GT <.<.
 R :0.1 M QZ-PY VEIN AT 167.5 M :TUFF ASH HAS GREEN COLORATION
 R :END OF LOG

A001
 ALAB EQUITY MINESITE LABORATORY
 ATYP ASSAY
 AMTH WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
 AUMM RCOVSAMPLE RQD % CU G/TAG G/TAU % SB % AS % FE % ZN
 R 00 488 :TRICONED - NO CORE

A001	488	520	7081	0.31	0.5	0.02	0.06	0.03	4.87	0.005
A001	520	550	7082	0.44	11.0	0.04	0.09	0.04	7.50	0.02
A001	550	579	7083	0.35	10.0	0.04	0.10	0.04	6.31	0.005
A001	579	613	7084	0.85	15.0	0.03	0.16	0.06	7.64	0.005
R	613	623	:DYKE - NO SAMPLE							
A001	623	653	7085	0.10	0.5	0.02	0.005	0.005	3.70	0.005
A001	653	683	7086	0.22	0.5	0.07	0.03	0.01	6.01	0.005
A001	683	712	7087	0.02	0.5	0.11	0.005	0.005	7.41	0.005
A001	712	742	7088	0.01	0.5	0.04	0.005	0.005	11.54	0.005
A001	742	772	7089	0.01	0.5	0.04	0.005	0.005	7.49	0.005
A001	772	803	7090	0.02	0.5	0.03	0.005	0.005	8.23	0.005
A001	803	833	7091	0.02	0.5	0.03	0.005	0.005	6.04	0.005
A001	833	863	7092	0.04	0.5	0.03	0.005	0.005	3.82	0.02
A001	863	893	7093	0.03	0.5	0.03	0.005	0.005	5.21	0.005
A001	893	923	7094	0.08	0.5	0.04	0.005	0.005	3.96	0.01
A001	923	953	7095	0.12	0.5	0.03	0.005	0.005	4.37	0.005
A001	953	983	7096	0.06	0.5	0.03	0.02	0.005	4.83	0.005
A001	983	1013	7097	0.03	0.5	0.02	0.01	0.005	2.12	0.005
A001	1013	1043	7098	0.03	0.5	0.02	0.01	0.005	3.41	0.005
A001	1043	1073	7099	0.02	0.5	0.02	0.01	0.005	5.72	0.005
A001	1073	1103	7100	0.03	0.5	0.02	0.01	0.005	5.03	0.005
A001	1103	1133	7101	0.05	0.5	0.03	0.01	0.005	4.32	0.005
A001	1133	1163	7102	0.04	0.5	0.02	0.005	0.005	3.82	0.005
A001	1163	1193	7103	0.04	0.5	0.02	0.005	0.005	3.54	0.005
A001	1193	1223	7104	0.04	0.5	0.02	0.005	0.005	4.71	0.005
A001	1223	1253	7105	0.06	0.5	0.02	0.005	0.005	3.87	0.005
A001	1253	1283	7106	0.11	0.5	0.02	0.04	0.01	3.50	0.02
A001	1283	1313	7107	0.03	0.5	0.03	0.005	0.01	4.72	0.05
A001	1313	1336	7108	0.28	18.0	0.07	0.05	0.01	4.13	0.28
A001	1336	1360	7109	0.06	0.5	0.11	0.01	0.01	4.18	0.25
R	1360	1379	:DYKE - NO SAMPLE							
A001	1379	1389	7110	0.05	0.5	0.03	0.005	0.005	2.73	0.53
R	1389	1415	:DYKE - NO SAMPLE							
A001	1415	1445	7111	0.02	0.5	0.06	0.005	0.005	5.83	0.18
A001	1445	1475	7112	0.05	0.5	0.02	0.005	0.005	4.04	0.05
A001	1475	1505	7113	0.01	0.5	0.04	0.005	0.005	5.80	0.17
A001	1505	1535	7114	0.06	0.5	0.12	0.005	0.005	5.04	0.36
A001	1535	1550	7115	0.09	0.5	0.08	0.005	0.005	2.56	1.00
R	1550	1558	:DYKE - NO SAMPLE							
A001	1558	1589	7116	0.07	0.5	0.12	0.005	0.005	6.00	0.03
A001	1589	1621	7117	0.27	26.0	0.14	0.02	0.04	7.00	1.68
A001	1621	1653	7118	0.10	9.0	0.05	0.005	0.01	5.00	0.74
A001	1653	1671	7119	0.04	1.0	0.01	0.005	0.001	2.31	0.12
A001	1671	1689	7120	0.03	2.0	0.02	0.005	0.005	3.77	0.05
R	:END OF HOLE - END OF LOG AT 168.9 M									
R	END OF ASSAYS - END OF LOG									

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IDEN6B0201      XB6CH266 NO   AUG86DJH   G&D AUG86S38      0.0
IPRJ            EQUITY SILVER MINES LTD   SUPERSTITION ZONE - ST GEOCODE
S000  00      457 MT  230.4 090.0 -45.0      5523.54  7452.69  1128.68
S001  457    1470      230.4 090.0 -43.0
S002  1470   2304      230.4 090.0 -45.0
/SCL          MT.2MT.1
LSCL          MT.2
/NAM
LNAM
/           00      100      OVBN          P
R           :TRICONED 0 - 9.8 M NO CORE :CORED A FEW BOULDERS 9.8 - 10.0 M
/           100    130    25      2C24MSCL  <<          P          <><><.
L           00      GT
R           :LI ON FRACTS :TO 2D LOC
/           130    160    29      2C23CLMS  <<          P <<  028  <><><.
L           00      TG
R           :ONLY MINOR LI PAST 13.7 M :2C24 13.0-13.7 M (GRADATIONAL CNT)
R           :10% MS AS << ENVELOPES
/           160    190    26      2C23CLMS  <<          P <<  .024  <+<><>
L           09      TG          <<
R           :10% MS AS << ENVELOPES :5% CL AS << ENVELOPES
/           190    212    20      2C23CLMS  <<          P <<  036  <+<><+
L           05      TG          <<
R           :5% MS AS << ENVELOPES :10% CL AS << ENVELOPES
/           212    240    22      8C05MSCL  P*          P
L           18      GT
R           :TYPICAL POST-MIN LATITE DYKE :CNTS NOT OBSERVED DUE TO
R           :BROKEN CORE
/           240    270    29      2C23CLMS  <<          P          <<<<<+<<.
L           00      TG
R           :5% MS AS << ENVELOPES :TT?
/           270    300    28      2C23CLMS  <<          P          <<<<<+<.
L           02      TG
R           :TO 2C15 LOC :10% MS AS << ENVELOPES
/           300    330    30      2C23CLMS  <<          P          <><+<<
L           05      TG
R           :10% MS AS << ENVELOPES
/           330    360    20      2C24MSCL  <<          P          <><><.
L           00      GT
R           :HEAVILY BROKEN UP INTERVAL :60% MS
/           360    390    25      2C24CLMS  <<          P          <<<<<<<
L           04      TG
R           :TO 2D LOC :30% MS
/           390    420    30      2C24CLMS  <<          P          <<<<<
L           15      TG
R           :30% MS
/           420    450    28      2C23CLMS  <<          P <<  025  <<<<<
L           12      TG
R           :5% MS AS << ENVELOPES :1% CL AS << ENVELOPES
/           450    480    30      2C23CLMS  <<          P          <<<<<<<.
L           09      TG          <+
R           :5% MS AS << ENVELOPES :2% CL AS << ENVELOPES :TO 2C23 LOC
/           480    510    26      2C23CLMS  <<          P          <<<<<+<.
L           12      TG
R           :TO 2C15 @ END OF INTERVAL :10% MS AS << ENVELOPES

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/ 510 540 29 2C23CLMS << P <<<><+
L 05 TG
R :TO 2C15 @ START OF INTERVAL :10% MS AS << ENVELOPES
/ 540 563 23 2C44MSCL <<BR P <><+<+
L 08 GT <<
R :TO 8A FROM 54.6 - 55.1 M
/ 563 598 35 8A11CLCY <<P* P CU 020 <<
L 30 GA CL 015<<
R :FLAG PHENOS TO 15 X 3 MM (ALTERED TO MONT)
/ 598 611 13 2C34MSCL << P <<<><+
L 05 GT <<
/ 611 624 13 8A11CLCY <<P* P CU 025 <<
L 00 GA <<
R :SIMILAR TO 56.3 - 59.8 EXCEPT LOCALLY BLEACHED WHITE
R :LOWER CNT NOT OBSERVED DUE TO GROUND CORE
/ 624 650 24 2C24CLMS << P <<+><+
L 04 TG <<
R :2% CL AS << ENVELOPES
/ 650 680 28 2C24CLMS << P <<<><+<.
L 02 TG <+
/ 680 710 29 2C34MSCL << P <<<><>
L 13 GT <+
R :TO 2C54 LOC
/ 710 740 28 2C34MSCL << P <<+><.
L 05 GT <<
R :TO 2C12 LOC (EOI)
/ 740 770 29 2C24MSCL << P <><><.
L 06 GT
R :TO 2C12 LOC (SOI)
/ 770 800 28 2C25MS << P <*>
L 00 ST
R :5% QZ AS << ENVELOPES
/ 800 812 11 2C25MS << P <*><.
L 00 ST
R :AS ABOVE 77.0 - 80.0 M
/ 812 822 10 8A01CY P* P CU 070
L 04 5A
R :LOWER CNT NOT OBSERVED DUE TO BROKEN CORE
/ 822 860 36 2C25MS << <*><<.<?
L 02 ST
R :MINOR GOUGE @ 83.5 M :5% QZ AS << ENVELOPES
/ 860 890 28 2C24MSCL << P <*><<<?
L 19 GT
R :BROKEN CORE AND GOUGE 88.8 - 89.0 M :TO 2C34 LOC
/ 890 915 24 2C24MSCL << P <*><<
L 03 GT
R :TO 2C35LOC
/ 915 925 09 8A01CY F*CM P CU 048
L 06 AU CL 045 D(
R :GOOD INTRUSIVE CNTS W/ CHILLED MARGINS :.1 M XENOLITH @
R :UPPER CNT
/ 925 950 23 2C24CLMS << P <*><><.
L 03 TG
R :TO 2C45LOC
/ 950 980 25 2C34CLMS << P <<<><<<

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L           06          TG          <<
/  980  1010  18    2C24MSCL      P          <<<<+<><.
L           00          GT
R           :POOR REC - SMALL CHIPS OF CORE - NO GOUGE
/  1010  1045  40    2C45MS      <<          P          <><>
L           05          AT
R           :GOUGE @ 103.6
/  1024  1024          X          D F/  080
R           :2 CMS GOUGE
/  1045  1101  56    8A11CLCY  P*A*      P CU  070  <*
L           42          AG          <<          <*
R           :GOUGE & BXIA 109.6 - 110.1 M :NOTE 2 TYPES OF ANDESITE DYKE
R           : (AMYGDALOIDAL ONE CUTS PORPHYRITIC ONE)
R           :UNALIGNED PLAG PHENOS (15 X 2 MM) ALTERED TO SAUSS
R           :LOWER CNT OBBSCURED IN GOUGE :.08 M XENOLITH @ 109.6 M
/  1101  1130  27    2C55MS      BR<<          P          #++<+<
L           13          AT
R           :TO 2C35 LOC
/  1130  1160  30    2C55MS      BR<<          P          #++=#)#(
L           09          AT
/  1160  1190  27    2C35MS      <<          P          <+<+<<<<
L           17          5T
/  1190  1220  28    2C35MS      <<          P          <><>
L           02          5T
R           :8A FROM 115.1 - 115.4 (PREVIOUS INTERVAL)
/  1220  1250  25    2C35MS      <<          P <<  068  <+<><<<.
L           08          5T
/  1250  1280  30    2C35MS      <<          P <<  060  <><><<.
L           05          5T
/  1280  1310  30    2C35MS      <<          P <<  060  <><><<<<
L           03          5T
R           :TO 2D LOC :OCC PY + QZ V/
/  1310  1340  29    2C35MS      <<BR          P          <><><<<<.
L           05          5T
/  1331  1331          X          D F/  015
/  1340  1370  27    2C35MS      <<          P          <><><<<<
L           06          5T
R           :8A FROM 134.2 - 134.8 M
/  1370  1400  30    2C35MS      <<          P          <><><*<<
L           10          5T
/  1400  1416  16    2C35MS      <<          P          <><><<<
L           00          5T
R           :TO 2C45 LOC :TO 2D LOC
/  1416  1428  12    8A02CLCB  P*A*      P CU  060
L           10          5G          CL  085
/  1428  1460  32    2C25MS      <<          P <<  060  <><><<<<.
L           03          5T
R           :TO 2D LOC
/  1460  1490  30    2C25MS      <<          P V/  050  <+<+<<<.
L           04          5T
R           :4 - V/ QZ + PY 2 - 4 CMS WIDE
/  1490  1520  30    2C35MS      <<BR          P          <><><*<?
L           13          5T
R           :TO 2C55 LOC
/  1520  1550  29    2C55MS      BR<<          P          #)#+ <?

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L           14           5T                               <?<*
R           :TT POSSIBLY IN W/ SL - DIFFICULT TO IDENTIFY POSITIVELY
R           :TO 2C35 LOC :POSSIBLY HE (HS) IN W/ SL
/ 1550 1580 30 2C65MS BR<< P #####.#?
L           04           5T                               Q( #?
R           :TO 2C35 LOC :APPEARS TO BE TECTONIC BXIA W/ SOME GOUGE
/ 1580 1610 29 2C35MS << P << 040 <)<)<(<
L           07           5T                               <?<(<
/ 1610 1640 29 2C55MS BR<< P #####
L           22           5T
R           :TO 2C35 TOWARDS EOI
/ 1640 1670 29 2C35MS << P << 070 <)<)<(<
L           16           5T
/ 1670 1700 30 2C35MS << P << 050 <)<)<Q(
L           12           5T
/ 1700 1730 30 2C35MS << P << 052 <)<)<(<
L           15           5T
/ 1730 1760 29 2C35MS << P << 060 <)<)<
L           04           5T
/ 1760 1790 26 2C55MS << P #)#+ #?
L           02           5T
R           :GOUGE @ 177.3 M
/ 1790 1820 30 2C35MS << P <)<)<
L           04           5T
/ 1820 1850 28 2C45MS << P <)<)+
L           08           5T
/ 1850 1880 30 2C55MS << P #)#) ##
L           19           5T
/ 1880 1910 27 2C45MS << P <*)<).#(
L           02           5T
R           :TO 2C55 LOC
/ 1910 1940 26 2C45MS << P <)<)<(<)<
L           20           5T
R           :TO 2C55 LOC :TT OBSERVED TO CROSS-CUT PY :LOST CORE @ 191.1 M
/ 1940 1953 13 2C45MS << P <)<)<)*
L           07           5T
/ 1953 1965 12 8A02CL A* P CU 042
L           09           5G CL 045 D(
/ 1965 2000 33 2C45MS <<<< P <)<)+<)*
L           17           5T <<
/ 2000 2030 30 2C45MS << P <)<)+<)*
L           04           5T
/ 2030 2060 30 2C24CLMS << P <*)<*)<)*
L           09           TG
R           :2C25 TO 204.2 :8A 203.7 - 203.9 M :CP ONLY TO 204.2
/ 2060 2090 30 2C24CLMS << P <*)<*)<).<?
L           22           TG
R           :GREY UNIDENTIFIED MINERAL W/ SL :NOTE COLOR CHANGE @ 204.2 M
/ 2090 2120 29 2C24CLMS << P <*)<*)<).
L           04           TG
/ 2120 2150 29 2C24CLMS << P <((*)<)*
L           05           TG
R           :TO 2C25 LOC
/ 2150 2170 20 2C24CLMS << P <((*)<)*
L           08           TG

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R      :TO 2C25 LOC
/      2170 2195 20 2C24MSCL << P <.<*<*<
L      12 GT <*<
/      2195 2225 30 BA02CLCB A*<< P
L      29 4G CL 050<.
R      :V WEAK << TEXT W/ CR :UPPER CNT NOT OBSERVED
/      2225 2255 30 2C24CLMS << P <(<*<*<.
L      03 TG
R      :TO 2C25 @ END OF INTERVAL
/      2255 2285 30 2C24MSCL << P <(<*<)
L      02 GT
R      :TO 2C25 LOC :TO 2D LOC
/      2285 2304 19 2C24CLMS << P <(<*<)
L      03 TG
R      :EDH @ 230.4
A001
ALAB EQUITY MINESITE LABORATORY
ATYP ASSAY
AMTH WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM RCOVSAMPLE RQD % CU G/TAG G/TAU % SB % AS % FE % ZN
R      00 100 :OVBN - NO CORE
A001 100 130 7161 0.13 0.5 0.03 0.02 0.005 2.13 0.001
A001 130 160 7162 0.09 0.5 0.02 0.01 0.005 2.46 0.001
A001 160 190 7163 0.05 0.5 0.03 0.005 0.005 2.61 0.001
A001 190 212 7164 0.06 0.5 0.04 0.005 0.005 2.88 0.001
R      212 240 :DYKE - NO SAMPLE
A001 240 270 7165 0.05 0.5 0.02 0.005 0.005 3.17 0.001
A001 270 300 7166 0.08 0.5 0.02 0.005 0.005 2.44 0.001
A001 300 330 7167 0.07 0.5 0.02 0.005 0.005 2.01 0.001
A001 330 360 7168 0.09 0.5 0.02 0.005 0.005 1.75 0.001
A001 360 390 7169 0.06 0.5 0.02 0.005 0.005 2.980 0.001
A001 390 420 7170 0.12 0.5 0.02 0.02 0.005 2.41 0.001
A001 420 450 7171 0.11 0.5 0.03 0.02 0.005 3.52 0.001
A001 450 480 7172 0.04 0.5 0.03 0.005 0.005 5.31 0.001
A001 480 510 7173 0.07 0.5 0.01 0.01 0.005 2.35 0.001
A001 510 540 7174 0.09 0.5 0.02 0.01 0.005 2.01 0.001
A001 540 563 7175 0.05 0.5 0.02 0.01 0.005 2.74 0.001
R      563 598 :DYKE - NO SAMPLES
A001 598 622 7176 0.06 0.5 0.02 0.01 0.005 3.12 0.001
A001 622 650 7177 0.10 0.5 0.02 0.03 0.005 2.64 0.001
A001 650 680 7178 0.07 0.5 0.02 0.005 0.005 2.99 0.001
A001 680 710 7179 0.18 1.0 0.04 0.005 0.001 4.02 0.005
A001 710 740 7180 0.09 1.0 0.01 0.005 0.001 2.51 0.005
A001 740 770 7181 0.07 0.5 0.01 0.001 0.01 2.55 0.005
A001 770 800 7182 0.14 1.0 0.01 0.005 0.005 2.58 0.005
A001 800 812 7183 0.12 1.0 0.01 0.005 0.005 2.80 0.005
A001 812 860 7184 0.07 0.5 0.01 0.005 0.005 2.84 0.005
A001 860 890 7185 0.07 0.5 0.05 0.005 0.001 3.29 0.005
A001 890 915 7186 0.14 0.5 0.02 0.005 0.001 3.23 0.005
R      915 925 :DYKE - NO SAMPLE
A001 925 950 7187 0.12 2.0 0.01 0.005 0.01 2.48 0.005
A001 950 980 7188 0.17 2.0 0.01 0.005 0.001 2.87 0.005
A001 980 1010 7189 0.07 1.0 0.01 0.005 0.005 1.65 0.005
A001 1010 1045 7190 0.03 1.0 0.02 0.005 0.02 3.39 0.005
R      1045 1101 :DYKE - NO SAMPLES

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A001	1101	1130	7191	0.19	7.0	0.05	0.01	0.03	6.22	0.02
A001	1130	1160	7192	0.78	20.0	0.03	0.005	0.01	5.58	0.01
A001	1160	1190	7193	0.13	6.0	0.01	0.02	0.005	3.64	0.09
A001	1190	1220	7194	0.08	3.0	0.01	0.01	0.001	1.65	0.02
A001	1220	1250	7195	0.04	8.0	0.02	0.01	0.005	2.44	0.06
A001	1250	1280	7196	0.13	4.0	0.01	0.01	0.001	4.48	0.01
A001	1280	1310	7197	0.19	8.0	0.07	0.02	0.02	5.58	0.01
A001	1310	1340	7198	0.18	6.0	0.04	0.005	0.01	2.85	0.06
A001	1340	1370	7199	0.06	3.0	0.04	0.001	0.001	3.22	0.06
A001	1370	1400	7200	0.14	4.0	0.01	0.005	0.005	4.41	0.01
A001	1400	1416	7201	0.10	3.0	0.03	0.005	0.001	2.16	0.01
R	1416	1428	:DYKE - NO SAMPLE							
A001	1428	1460	7202	0.37	15.0	0.03	0.005	0.005	3.37	0.03
A001	1460	1490	7203	0.06	12.0	0.03	0.01	0.005	4.95	0.03
A001	1490	1520	7204	0.16	16.0	0.14	0.01	0.01	4.23	0.01
A001	1520	1550	7205	0.05	8.0	0.24	0.005	0.01	6.68	0.44
A001	1550	1580	7206	0.14	33.0	0.79	0.01	0.10	9.46	0.10
A001	1580	1610	7207	0.12	6.0	0.04	0.005	0.01	3.73	0.10
A001	1610	1640	7208	0.02	3.0	0.22	0.005	0.01	5.98	0.005
A001	1640	1670	7209	0.12	14.0	0.03	0.01	0.01	5.12	0.005
A001	1670	1700	7210	0.05	14.0	0.38	0.005	0.02	6.16	0.005
A001	1700	1730	7211	0.20	33.0	0.29	0.01	0.005	5.34	0.01
A001	1730	1760	7212	0.02	5.0	0.11	0.005	0.005	5.25	0.03
A001	1760	1790	7213	0.02	7.0	0.11	0.005	0.001	7.24	0.02
A001	1790	1820	7214	0.02	6.0	0.04	0.005	0.01	6.00	0.005
A001	1820	1850	7215	0.04	4.0	0.52	0.005	0.01	3.15	0.005
A001	1850	1880	7216	0.02	7.0	0.13	0.005	0.17	6.15	0.005
A001	1880	1910	7217	0.12	52.0	0.31	0.03	0.26	4.94	0.02
A001	1910	1940	7218	0.27	42.0	0.33	0.05	0.63	8.53	0.01
A001	1940	1953	7219	0.43	28.0	0.07	0.01	0.03	4.21	0.005
R	1953	1965	:DYKE - NO SAMPLE							
A001	1965	2000	7220	0.32	22.0	0.06	0.01	0.001	4.78	0.30
A001	2000	2030	7221	0.37	20.0	0.09	0.005	0.005	5.00	0.06
A001	2030	2060	7222	0.04	3.0	0.01	0.001	0.005	3.97	0.02
A001	2060	2090	7223	0.15	10.0	0.04	0.01	0.005	3.65	0.07
A001	2090	2120	7224	0.04	4.0	0.04	0.001	0.005	2.74	0.07
A001	2120	2150	7225	0.03	5.0	0.03	0.005	0.01	3.16	0.09
A001	2150	2170	7226	0.03	2.0	0.01	0.001	0.01	4.51	0.02
A001	2170	2195	7227	0.01	2.0	0.02	0.001	0.005	4.99	0.98
R	2195	2225	:DYKE - NO SAMPLE							
A001	2225	2255	7228	0.03	2.0	0.02	0.005	0.01	5.81	0.005
A001	2255	2285	7229	0.02	1.0	0.01	0.001	0.001	5.00	0.005
A001	2285	2304	7230	0.02	1.0	0.02	0.005	0.001	7.11	0.005
R			:EOH @ 230.4 M							
R			END OF ASSAYS - END OF LOG							

IDEN6B0201									
IPRJ									
S000	00	434	MT	108.2	090.0	-45.0			
S001	434	1082		108.2	090.0	-44.0			
/SCL				MT.2	MT.1				
L SCL					MT.2				
/NAM									
LNAM									
/	00	52							
R									
/	52	80	26	2C13CLMS	<<				
L			00	TG					
R									
/	80	110	29	2C13CLMS	<<				
L			00	TG					
R									
/	110	140	29	2C13CLMS	<<				
L			12	TG					
R									
/	140	170	27	2C13CLMS	<<				
L			11	TG					
R									
/	170	200	29	2C13CLMS	<<				
L			07	TG					
R									
/	200	230	28	2C13CLMS	<<				
L			02	TG					
R									
/	230	260	28	2C13CLMS	<<				
L			09	TG					
R									
/	260	290	29	2C13CLMS	<<				
L			04	TG					
R									
/	290	320	28	2C13CLMS	<<				
L			04	TG					
R									
/	320	350	28	2C13CLMS	<<				
L			18	TG					
R									
/	350	380	28	2C13CLMS	<<				
L			05	TG					
R									
/	380	402	12	2C13CLMS	<<				
L			00	TG					
R									
/	402	428	19	2C65MSQZ	BR				
L			00	5A					
R									
/	428	474	42	BA02CLCB	P*				
L			18	5G					
R									
/	474	500	25	2C35MSQZ	<<				
L			03	5T					
R									

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/ 500 530 29 2C25MSQZ << P Q+Q+
L 09 5T
R :PY + QZ ALSO IN << - STRANGE RX TYPE - POSSIBLE 2C55?
R :MINOR GOUGE ZONES
/ 530 560 30 2C35MSQZ << P (<)<
L 22 5A
R :TO 2D LOC
/ 560 593 31 2C35MSQZ << P (<)<.<
L 19 5T
R :TO 2D LOC
/ 593 626 32 VEINQZPY P VBV2
L 24 AW
R :A FEW SHORT SECTIONS OF 2C35 :NO CNT ATTITUDES POSSIBLE
/ 626 650 23 2C35MSQZ <<BR P <=<=
L 12 5A
R :TO 2C75 LOC
/ 650 680 29 2C25MSQZ << P (<.<)<
L 14 5A
R :TO 2D LOC
/ 680 710 29 2D25MSQZ << P (<)<+
L 21 5A
R :TO 2C LOC
/ 710 740 29 2D25MSQZ << P (<)<
L 13 5A
R :TO 2C65
/ 740 770 27 2D25MSQZ << P (<)<
L 15 5A
/ 770 800 29 2D25MSQZ << P (<)<
L 07 5A
/ 800 820 18 2D25MSQZ << P (<+<+
L 10 5A
R :TO 2D55 LOC
/ 820 840 17 2C25MSQZ << P (<)<
L 03 5T
/ 840 858 15 8A02CL A* P CU 064 A(
L 12 6G CL 075 A.
R :CL AS A* ENVELOPES
/ 858 889 31 2C25MSQZ << P (<<<)<
L 04 5T
R :TO 2C22 @ END OF INTERVAL W/ CL ON <<
/ 889 937 45 8B02CLCB P*A* P TC 044
L 38 4G A. A.
R :NO CNTS OBSERVED BUT PROBABLY // TO TC
/ 937 970 31 2C25MSQZ << P (<<<)<.<
L 14 5T
R :TO 2C22 @ START OF INT :TO 2D LOC
/ 970 1000 25 2C25MSQZ << P (<)<
L 00 5T
R :CORE HEAVILY BROKEN UP
/ 1000 1033 31 2C25MSQZ << P (<)<
L 04 5T
R :V BROKEN UP CORE :TO 2C23 LOC
/ 1033 1060 27 1D10QZ << P (<*<*<.<
L 19 5A
/ 1060 1082 20 2D25QZMS << P (<)<.<

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L          08          5A
R          :UPPER CNT GRADATIONAL OVER 0.2 M - ENTIRE INT MAY HAVE
R          :QZ GRAINS (IE - COMFORMABLE TRANSITION ZONE)
R          :EDH @ 108.2 :RODS STRUCK WHILE TRIPPING OUT OF HOLE -
R          :BLASTED OFF
R          :COLLAR LOCATION LOST WHILE MOVING DRILL (RE-POSITIONED
R          :WITHIN 0.5 M RADIUS)
A001
ALAB      EQUITY MINESITE LABORATORY
ATYP      ASSAY
AMTH      WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM      RCOVSAMPLE  RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R         00      52 :TRICONED - NO CORE
A001 52      80      7231      0.11      0.5 0.03  0.005 0.001 2.56 0.005
A001 80     110      7232      0.10      1.0 0.02  0.005 0.001 3.40 0.005
A001 110    140      7233      0.06      1.0 0.04  0.005 0.001 3.47 0.005
A001 140    170      7234      0.07      1.0 0.04  0.005 0.001 3.04 0.005
A001 170    200      7235      0.13      1.0 0.03  0.005 0.001 3.71 0.005
A001 200    230      7236      0.13      1.0 0.03  0.005 0.001 3.28 0.005
A001 230    260      7237      0.15      1.0 0.03  0.001 0.005 3.93 0.005
A001 260    290      7238      0.05      0.5 0.01  0.005 0.005 4.10 0.005
A001 290    320      7239      0.09      1.0 0.02  0.005 0.005 3.79 0.005
A001 320    350      7240      0.07      1.0 0.01  0.005 0.005 3.43 0.005
A001 350    380      7241      0.16      1.0 0.01  0.005 0.005 2.89 0.005
A001 380    402      7242      0.11      4.0 0.06  0.01  0.001 3.82 0.04
A001 402    428      7243      0.16      5.0 0.05  0.005 0.001 3.05 0.005
R         428    474 :DYKE - NO ASSAYS
A001 474    500      7244      0.05      1.0 0.14  0.005 0.001 2.21 0.005
A001 500    530      7245      0.01      1.0 0.05  0.01  0.001 3.70 0.005
A001 530    560      7246      0.005     1.0 0.04  0.01  0.001 4.69 0.005
A001 560    590      7247      0.02      1.0 0.05  0.01  0.001 5.71 0.005
A001 590    620      7248      0.01      3.0 0.33  0.02  0.02 12.40 0.005
A001 620    650      7249      0.02      8.0 0.26  0.03  0.01 18.50 0.005
A001 650    680      7250      0.04      2.0 0.16  0.01  0.001 4.43 0.005
A001 680    710      7251      0.01      2.0 0.04  0.02  0.01  7.14 0.005
A001 710    740      7252      0.02      2.0 0.25  0.02  0.02  7.59 0.005
A001 740    770      7253      0.01      2.0 0.05  0.01  0.01  6.11 0.005
A001 770    800      7254      0.005     2.0 0.02  0.02  0.01  8.13 0.005
A001 800    820      7255      0.005     2.0 0.09  0.01  0.01  8.08 0.005
A001 820    840      7256      0.005     2.0 0.02  0.01  0.001 7.16 0.005
R         840    858 :DYKE - NO SAMPLE
A001 858    889      7257      0.06     16.0 0.02  0.01  0.04  6.21 0.005
R         889    937 :DYKE - NO SAMPLE
A001 937    970      7258      0.11      8.0 0.04  0.01  0.01  4.71 0.01
A001 970   1000      7259      0.05      2.0 0.04  0.01  0.001 5.25 0.005
A001 1000   1030      7260      0.07      2.0 0.06  0.005 0.01  2.89 0.02
A001 1030   1060      7261      0.19      1.0 0.01  0.005 0.001 1.73 0.005
A001 1060   1082      7262      0.08      3.0 0.03  0.005 0.001 2.67 0.005
R          :END OF ASSAYS - END OF HOLE
R          :HOLE TERMINATED DUE TO STUCK RODS - BLASTED OFF @ 200 FT
R          END OF ASSAYS - END OF LOG

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/ 600 632 29 2C23CLMS << P <<<<<<.
L 13 TG
R :TO 2C34 LOC
/ 632 669 36 8A01CL P* P CU 060
L 32 6G CL 075
R :POSSIBLY LATITE
/ 669 700 31 2C13CLMS << P <<<<<<.
L 17 TG
R :TO 2C55 @ DYKE CNT
/ 700 729 25 2C13CLMS << P <<<<<<
L 02 TG
R :CLAY GOUGE & HEAVILY BROKEN CORE 72.4 - 72.9
R :EOH @ 72.9 M - COULDN'T GET THROUGH FAULT ZONE
A001
ALAB EQUITY MINESITE LABORATORY
ATYP ASSAY
AMTH WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM RCDVSAMPLE RQD % CU G/TAG G/TAU % SB % AS % FE % ZN
R 00 183 :TRICONED - NO CORE
A001 183 210 7075 0.05 1.0 0.03 0.01 0.001 2.83 0.005
A001 210 240 7076 0.06 1.0 0.02 0.01 0.001 3.04 0.005
A001 240 270 7077 0.07 1.0 0.02 0.01 0.001 3.34 0.005
A001 270 300 7078 0.07 1.0 0.04 0.01 0.001 3.90 0.005
A001 300 323 7079 0.14 6.0 0.06 0.02 0.01 6.65 0.01
A001 323 351 7080 0.04 0.5 0.06 0.005 0.001 2.12 0.005
A001 351 374 7121 0.13 1.0 0.01 0.005 0.001 2.85 0.005
R 374 393 :DYKE - NO SAMPLE
A001 393 420 7122 0.12 1.0 0.04 0.01 0.001 4.67 0.02
A001 420 450 7123 0.13 2.0 0.03 0.01 0.001 4.06 0.005
A001 450 480 7124 0.13 1.0 0.03 0.01 0.001 3.28 0.005
A001 480 510 7125 0.08 1.0 0.03 0.005 0.001 2.80 0.005
A001 510 540 7126 0.09 1.0 0.04 0.01 0.001 2.87 0.005
A001 540 570 7127 0.04 1.0 0.02 0.01 0.001 2.50 0.01
A001 570 600 7128 0.10 1.0 0.04 0.01 0.001 3.31 0.005
A001 600 632 7129 0.03 0.5 0.01 0.01 0.001 2.30 0.005
R 632 669 :DYKE - NO SAMPLE
A001 669 700 7130 0.03 1.0 0.01 0.01 0.001 3.31 0.005
A001 700 729 7131 0.03 1.0 0.05 0.01 0.001 2.80 0.005
R :END OF HOLE - COULDN'T GET THROUGH SAND SEAM
R END OF ASSAYS - END OF LOG

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