SUMMARY REPORT

OF

GEOLOGICAL, GEOPHYSICAL AND OTHER STUDIES

ON THE

TEL DEPOSIT

YELLOW GIANT PROJECT

BANKS ISLAND

NTS 103G/8, 53°22'00", 130°09'45"

SKEENA MINING DIVISION

FROM
JUNE 1986 TO FEBRUARY 1987

FOR

TRADER MINES LTD.

BY

J.T. SHEARER, M.Sc., FGAC.
G.A. SHORE, Ph.D.
S.L. GARDINER, B.Sc., FGAC.

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SUMMARY

(1) The Tel Deposit is located on central Banks Island, 118 km south of Prince Rupert. Access is by boat or float plane.

(2) The original Tel 23-32 claims were staked by J.W. MacLeod on July 1, 1963 for McIntyre Porcupine Mines Limited to cover a portion of the metasedimentary belt indicated by aerial photographs to parallel the Discovery Zone belt.

(3) The surface showing was discovered by A.E. Angus in late September 1963. Trenching and additional prospecting was completed by November 1963.

(4) Geological mapping, diamond drilling and geophysical surveys were conducted by McIntyre from February to October 1964 indicating a small, high-grade gold deposit to the -50 foot level.

(5) Deeper diamond drilling, also under the supervision of J.W. MacLeod, was done in 1975 by Sproatt Silver Mines Ltd. McIntyre sold the Tel claims to Sproatt for $10,000. An IP survey was also conducted.

(6) The results of the 1975 drilling included hole 75B-6 in which 47 feet averaged 1.48 oz/ton gold. This mineralized zone could not be confidently correlated to other zones of similar thickness.

(7) Trader Resource Corp. optioned the entire property in 1983.

(8) After geological mapping and revaluation of the Tel Area by Trader, a major extension of the previously known zone was discovered on October 10, 1985.

(9) Subsequently, a large drill program was completed by Trader between November 1985 and March 1986 to bring the total drilling on the Tel Deposit to 33,679.5 feet (10,265.51 m) in 91 holes.

(10) The Tel Deposit is composed mainly of a deformed, massive sulfide assemblage of pyrite-arsenopyrite-sphalerite. Of lesser importance is late-stage, drusy quartz-pyrite mineralization.

(11) The main rock types are banded grey marble and silty thin-bedded marble. Common host rock strike and dip orientation is 324°/55° E.

(12) Narrow dioritic dykes and sills of variable composition occur throughout the Tel Area. Zircon U/Pb dating gives an age for these dykes of 123 Ma.

(13) The minor fold style is tight isoclinal plunging 45° north and south. Regional tectonic effects suggest that large scale plastic flowage and drag could result in steep plunges of the major folds.

(14) A large scale fold which can be traced from Hepler Creek north to Sproatt Lake is named the Tel Antiform. Its axial plane trends 310°/55° E with an overall width of at least 180 m.

(15) A major fault-shear structure, the McIntyre Fault, now defines the east contact between banded grey marble and silty thin-bedded marble. It is sometimes marked by the "East Limb" of the Tel Deposit and is oriented 320°/60° E. The McIntyre Fault is sub-parallel to the Bank-Barge Lineament and may be a subsidiary splay.

(16) The Tel Fault cross-cuts the regional grain and trends 277°/75° E. The Tel Fault is filled with low-grade, late-stage quartz and appears to offset the massive sulfide zones.

(17) All geological, assay and survey information has been computerized on both the Simons and Wright systems. Mineral inventory and ore reserve calculations for gold were made in May 1986.

(18) In July 1986 results from analyses for silver, arsenic, copper, lead, zinc, iron and sulphur for all mineralized drill intersections were added to the Simons data bank. Grade composites were calculated and contoured plans for six elements and iron sulphide were generated for elevations at 50m intervals within the deposit.

(19) Broad zones of higher grade values for all elements and iron sulphide are outlined on plans for 0m to -50m and -50 to -100m elevations.

(20) Elevated values of iron sulphide and/or zinc are most commonly associated with higher gold grade.

(21) Premier Geophysics Inc. conducted a series of E-SCAN induced polarization and resistivity surveys over the known Tel ore zones in June 1986. Coverage was extended to the north and southeast during the October to December 1986 survey.

(22) The Tel sulphide/gold ore mineralization has a distinct E-SCAN IP signature within a marble rock unit environment.

(23) The lateral boundary of the E-SCAN IP anomaly correlates very closely with most of the drill-indicated ore boundary. Where the E-SCAN boundary extends beyond the limit of drill-indicated ore, it is found that the ore limits are also open in that direction - that is, the area in question is not yet drill-tested.

(24) The marble units (silty thin bedded, and grey banded) have a distinct background IP and resistivity signature which distinguishes them from the adjacent graphitic argillites.

(25) Mise a la masse resistivity can be useful in projecting ore zone orientation from deep ore intersection in drill holes.

(26) E-SCAN surveys on and near the Tel zone have accurately outlined the known Tel ore zone, and mapped six new anomalous areas within 250 meters of the Tel ore zone. Drilling of three of these anomalies and their common, connecting fault zone has been recommended. The other three anomalies lie in different geologic conditions and warrant further mapping and investigation prior to drilling.

INTRODUCTION

This report is a summary of three programs that were carried out during the period of June, 1986 to February, 1987 under the Financial Assistance for Mineral Exploration program. Prior to this time diamond drilling and geological information obtained from previous programs was entered into the H.A. Simons Ltd, and Wright Engineers Computor Systems. Ore reserve calculation, based on gold only were performed by Simons, Wright and Montgomery Consultants Ltd, using three different methods.

In June 1986 detailed geological mapping was done in the area of the Tel Deposit. The information derived from this study was combined with the data from diamond drilling and used to develope a model for the Tel.

A powerful, innovative geophysical system, named E-SCAN, was used to conduct an orientation survey over the Tel area in June 1986. Follow-up surveys were carried out during the months from October to December, 1986.

Analyses for seven other elements from mineralized intersections from diamond drilling were added to the Simons data file for the Tel Deposit. Contoured plots showing grade composites for gold, silver, arsenic, copper, lead, zinc and iron sulphide were generated.

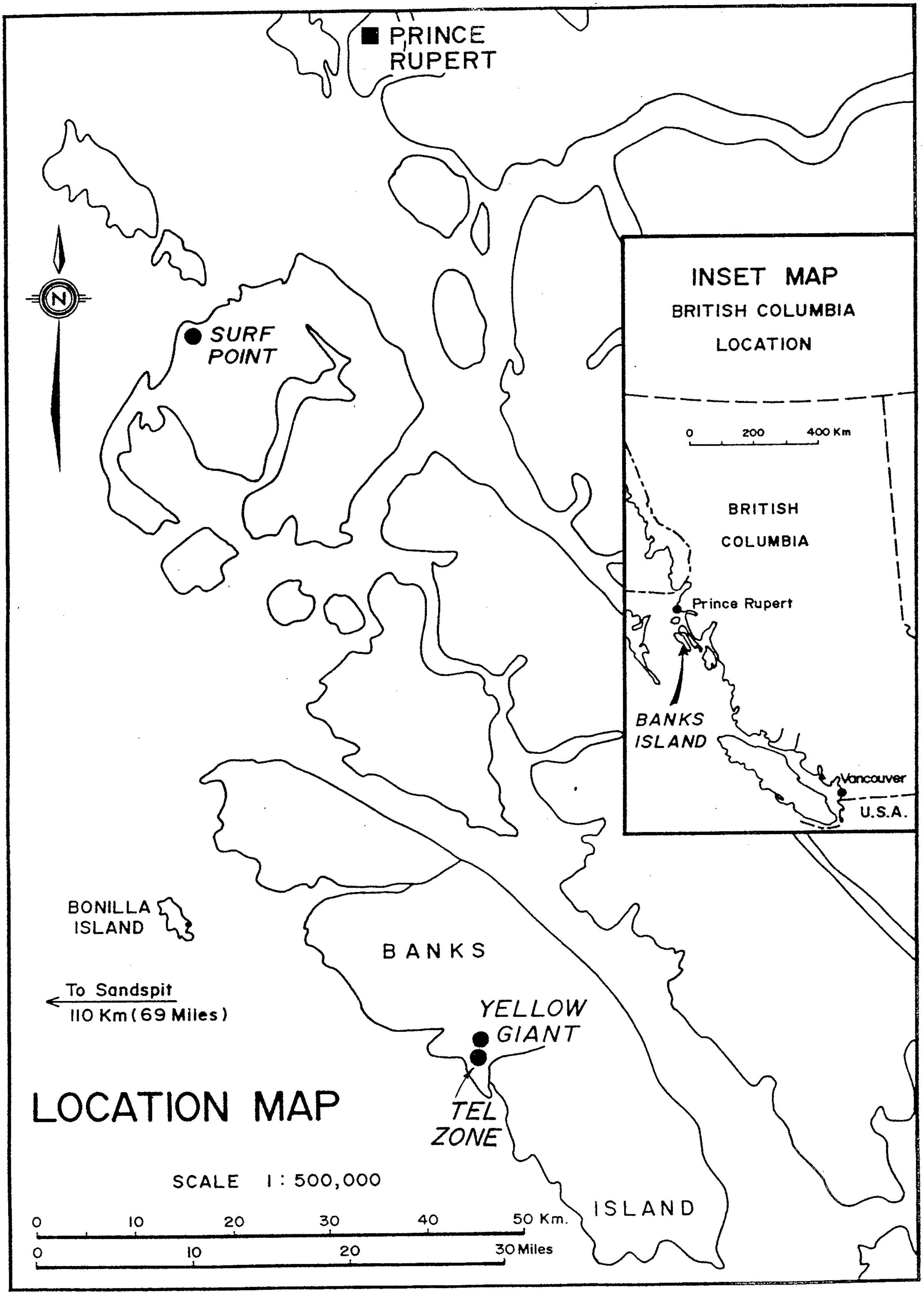

PRINCE RUPERT
SURF POINT
BONILLA ISLAND
To Sandspit
110 Km (69 Miles)
BANKS
YELLOW GIANT
TEL ZONE
ISLAND
LOCATION MAP
SCALE 1 : 500,000
0 10 20 30 40 50 Km.
0 10 20 30 Miles
INSET MAP
BRITISH COLUMBIA
LOCATION
0 200 400 Km
BRITISH COLUMBIA
Prince Rupert
BANKS ISLAND
Vancouver
U.S.A.

Fig. 1

PROPERTY (CLAIM STATUS)

The Tel Deposit is covered by one 20 unit Modified Grid System (MGS) mineral claim, Figure 3, as tabulated below:

TABLE I

List of Claims

Claim Name	Units	Size	Record Number	Record Date	Expiry Date
Yellow Giant 3	20	5W x 4S	3889	June 15/83	1995

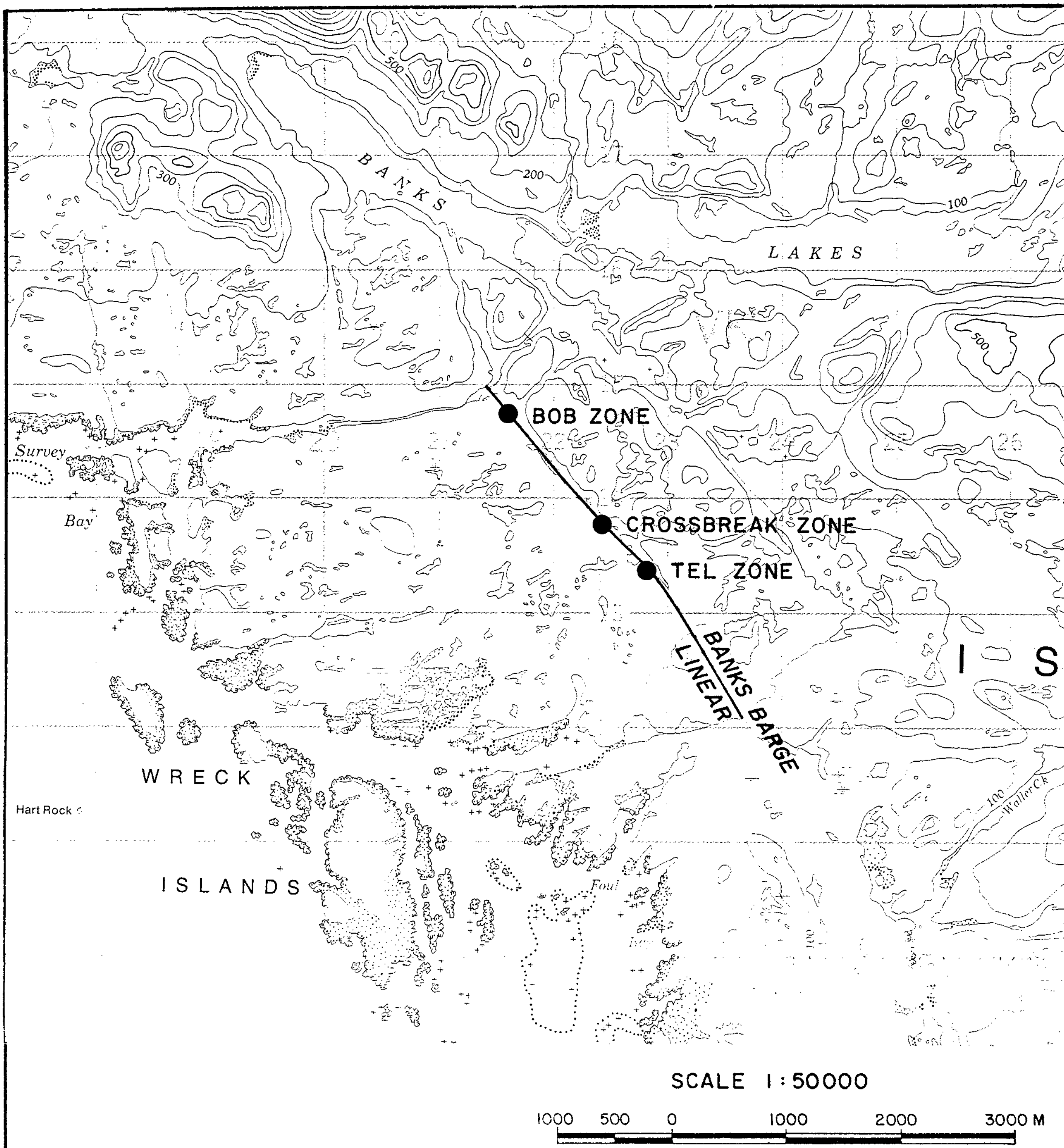
The entire area covering favourable geology and including the proposed mill site is listed in Table II.

TABLE II

List of Claims
Covering Favourable Geology, Tel Area

Claim Name	Individual Units	Record Number	Record Date	Expiry Date
Yellow Giant 3	3, 4, 13 and south half of 14	3889	June 15/83	June 15/95
Yellow Giant 4	4, 13	3890	June 15/83	June 15/95
Yellow Giant 6	27, 28, 29, 30, 32, 33, and 34	3892	June 15/83	June 15/95
Yellow Giant 9 Fr	south half	4443	May 8/84	May 8/95

The original Tel 23, 24, 37 and 38 two-post claims of McIntyre Porcupine Mines Ltd. were abandoned under the provision of the Mineral Act, Section 28(1), and relocated under the Modified Grid System (Mineral Act, Section 28(3)). This property consolidation eliminates the many problems associated with the old two-post system regarding filing assessment, grouping, anniversary dates and multiple fractions.



TRADER RESOURCE CORP.

GOLD ZONES
ALONG
BANKS – BARGE LINEAR

PROJECT : YELLOW GIANT PROJECT

ENG: TRM ENGINEERING LTD.

DWG. NUMBER: FIGURE 2

All new claims were recorded in the names of Host Ventures and Falconbridge Nickel Mines. Host Ventures (which became Hot Resources Ltd. and is now, as of February 11, 1985, Inter-Globe Resources Ltd.) optioned the property to United Mineral Services Ltd. by an agreement dated May 16, 1983. This agreement was assigned to Trader Resource Corp., who further assigned its rights to a wholly owned subsidiary, Trader Mines Ltd. Through continued exploration expenditures, Trader Mines Ltd. now owns an 80% interest in the Yellow Giant Property and can eventually become the 100% owner pursuant to the option agreement.

The legal corner posts (LCP) of each claim were surveyed by McElhanney Group Ltd. with the grid location as follows:

(a) Yellow Giant 1, 2 and 3: 32,297.89 N + 28,441.98 E
(b) Yellow Giant 4, 5, 6, 7: 30,326.07 N + 30,460.51 E

LOCATION AND ACCESS

The Claim Group is situated on south central Banks Island, 112 km south of Prince Rupert, Figure 1. Banks Island is about 70 km long by 20 km wide. The nearest communities are Hartley Bay 60 km east on the mainland, Kitkatla, 52 km to the north and Trutch, 45 km southeast. Kitimat is 120 km northeast of the property. Directly west is Sandspit on the Queen Charlotte Islands, a distance of 110 km.

Bonilla Island weather station is located off the northwest side of Banks Island. B.C. Telephone maintains a close network of repeater stations to service the commercial fishing fleet and local villages. The best communication on Banks Island is via the Noble Mountain FM channel, although satellite receivers will be phased in over the next few years.

Access is mainly by float-equipped, fixed-wing aircraft to the main camp on Hepler Lake, Figure 2. Heavy equipment is barged to Survey Bay. The barge site is 2.1 km by rough tote road west of the Bob Zone where a 15% decline ramp was driven in 1977. A 2.2 km proposed road right-of-way has been slashed out from Indian Bay to the Tel Zone.

Helicopter transportation has been important in the past and there are many natural open spots suitable for landing.

The area is characterized by coastal muskeg over the granitic rocks and by lush cedar-hemlock forests over the narrow metasedimentary belts. The main claims cover mostly undulating lowlands (Hecate lowland) with relief generally less than 50 m. To the east and north the terrain becomes progressively more rugged towards the Carlo Range, whose high point, on Mount Grannell, is 676 m.

HISTORY

The Tel 23 to 32 two-post claims were located by J.W. MacLeod on July 1, 1963 (recorded July 12, 1963) for McIntyre Porcupine Mines Ltd. Mr. MacLeod had been attracted to Banks Island as a result of high grade gold values intersected by Falconbridge Nickel Mines Ltd. in the April 1963 diamond drilling on the Discovery Deposit. Hole LY-2 on Discovery Zone averaged 0.719 oz/ton gold, 1.86 oz/ton silver and 0.25% copper over 50.0 feet (15.24 m). McIntyre had recently purchased a controlling interest in Falconbridge and was thus privy to such confidential information.

Falconbridge (formerly Ventures Ltd.) prospectors M. Hepler and S. Bridcut, under the direction of J.J. McDougall, located the Banker 1-4 claims to cover the Discovery Zone in 1960. Initial exploration focussed along the metasedimentary belts in the vicinity of intersecting airphoto lineaments. Little work was done on Banks Island in 1961 or 1962 due to commitments at the Catface porphyry copper deposit. Several important discoveries were made in 1963 by Falconbridge including the Kim, Bob, Englishman, Keech and Crossbreak Zones.

Prior to locating the Main Tel Zone, J.W. MacLeod staked two other groups as tie-on to the Falconbridge ground. These were Tel 1-10 (North Group) to cover ground along the expected strike of the central metasedimentary belt north of Gladys Lake and along the east shore of West Banks Lake. Tel 11-22 (East Group) were located between Crazy Lake and Kim Zone. As a humourous wordplay on the Bank-Banker claims, MacLeod chose Teller (as in cashier) shortened to "Tel" as the name for his new claims. The Main Tel Zone (claims Tel 23 to 32 called the West Group) were staked to cover a portion of the metasedimentary belt indicated by aerial photographs to parallel the Discovery Zone belt. Subsequently, Falconbridge staked around the Tel 23-32 claims on three sides.

Detail prospecting by A.E. Angus and M. McQuire started on the Tel claims in August 1963 and continued in two phases into the month of November. Mr. Angus was later assisted by prospector Alfie Teed. During late September the main Tel showing was found shortly before the program ended. A gossanous zone assaying 1 to 3 oz/ton gold was found by A.E. Angus within a lightly overburdened area near the shoreline of what is now called Sproatt Lake. By November, stripping and rock trenching indicated that the massive sulfide zone (Main Zone) to be 30 feet long by 7 feet wide and to "finger out" quite abruptly at both ends and "down dip" (Hubacheck, 1963). The West Tel Zone was the second showing to be found (No. 2 showing). It occurs in a creek bed about 500' northwest of the No. 1 showing (Main Tel Zone). Hubacheck (1963) describes the West Tel Zone as follows:

> "Considerable stripping and rock trenching has been done in this area, exposing two intersecting bands of mineralization. The main band consists of a mineralized fault breccia about two feet wide in an east-west trending fault zone, which has now been opened up for a length of 50'. The other consists of a band of sulphides in limestone one foot wide striking northwest and dipping steeply to the northeast. The sulphide mineralization is similar to that of the No. 1 showing but not nearly as heavily concentrated.
>
> Sampling results from the east-west fault breccia zone were as follows: 0.76 oz gold over 2.0' at the west end of the showing (heavy sulphides), 0.08 oz gold over 1.2' near the centre, and 0.04 oz gold over 1.5' near the east end. The mineralized limestone assayed 0.12 oz gold over 1.0'.
>
> Both zones are open on strike."

After the Tel Main Zone discovery, two additional claims, Tel 37 and 38, were staked on October 7, 1963 (recorded

October 17, 1963) to fill the gap between Tel 23 and 24 north to Banker 146 and 147. The Banker 146 and 147 were located on July 9, 1963.

Geophysical orientation surveys were carried out over the Main Tel area. These consisted of self-potential (SP), Magniphase horizontal-loop electromagnetic and Rhonka E.M. 15 units. Reconnaissance self-potential results indicated the presence of the No. 4 zone which is now referred to as Central Tel Zone. SP values also show anomalous trends over what was discovered in 1985 to be the northwest continuation of the Tel Main Zone.

In 1964 a program of geological mapping was conducted by J.W. McLeod and J.H. Evans. This resulted in two 1" = 40' (1:480) sketch maps around the showings and a generalized 1" = 200' (1:2400) property geology map between Sproatt and Witness Lake. A 26 hole packsack diamond drill program was completed in 1964. All the drill holes were near the showings except for holes 13, 15 and 16. Total footage of holes P1 to 12, 14 and 17 to 26 is 1465 feet (446.53 m). The SP anomalies obtained over the graphitic Banks-Barge lineament were investigated by holes P-13, P-15 and P-16 (totalling 259 feet (78.94 m)), and by trenches 1 to 12, excluding 7.

Work by McIntyre Porcupine Mines Ltd. up to 1964 resulted in following conclusions (McLeod, 1964, page 9).

> "The West Zone (Map No. 6) is believed to be primarily due to a quartz vein or a series of quartz veins carrying sulfides and appreciable gold values. Where the opening occupied by the quartz crosses a favourable situation a replacement zone is found. That is, the east end of the zone consists of massive sulfides replacing limestone. This portion of the zone is 50 feet long and averages 1.18 ounces gold over a width of 8.5 feet in five holes drilled under the zone. To the west for 150 feet the zone is indicated by quartz vein intersections in 4 out of 5 holes where the widths vary from 1.5 to 4.5 feet. The gold values range from 0.20 to 1.56 for these intersections but are not considered true values becuase of the poor core recovery. For 200 feet to the west no zone has been indicated by drilling 4 holes at 50 foot intervals. The zone is again picked up by holes 10, 11, 12 and 19 for a length of 120 feet, but again core

> recovery was very poor. In one of these the wide intersection of 6.8 feet is due to the inclusion in the zone of 3.5 feet of replacement type mineral. A granite dike is found in hole 20 at the anticipated vein intersection. Mineralization of both the vein and replacement types is poorly exposed 300 feet west of hole 20 at 10 300 N. There is a possibility that this is the faulted extension of the West Zone. Two attempts to drill this area were frustrated by caving ground."

The Tel claims were dormant between 1964 and 1975. A change in senior management at McIntyre Porcupine Mines Ltd. in 1974 resulted in the new president, R.B. Fulton, arranging the sale of the original McIntyre Gold Mine (a continuous producer since 1912) and the cancellation of the Warman option (to become shortly thereafter the Northair Gold Mine). These changes consequently allowed D.A. MacLeod to arrange the option of the Tel Claims from McIntyre. In a letter dated May 27, 1975, R.B. Fulton confirms the outright sale of Tel 23, 24, 37 and 38 to Sproatt Silver Mines Ltd. for $10,000 payable on or before June 15, 1975.

Technical data were summarized by R.H. Seraphim in his six page report (June 6, 1975) which proposed a 1,000 foot diamond drill program. Diamond drilling by Sproatt Silver Mines Ltd. began on September 30, 1975 and finished on November 22, 1975. The drill program was planned by J.W. MacLeod, who closely supervised site-geologist D. Peel. Holes 75B-1 and 75B-2 investigated the West Tel Zone by drilling along the strike of the enclosing silty thin bedded marble. Holes 75B-3, 75B-4 and 75B-17 were collared around the Central Tel Zone and also were directed subparallel to the general strike of the banded grey marble. One of them, 75B-4, provided twenty feet of sludge which assayed 0.95 ounces gold.

The first 1975 hole through the Main Tel Zone was 75B-5 which intersected directly under the surface exposure 5.04 ounces gold across one foot of core length.

Seraphim (1975b) reports that:

> "The best new intercept, in hole B-6, assayed 1.47 ounces gold, 1 ounce silver, and 2.73 percent zinc. True width is approximately 20 feet and depth below surface approximately 100 feet."

However, in another report dated one week later, Seraphim (1975c) reports about hole 75B-6 that:

> "True width is not known, but holes 7, 8 and 9, drilled into the same area but in opposite direction, each intersected only one to two feet of sulphides."

The apparent general concensus in 1975 concerning hole 75B-6 was that, in the absence of a straightforward, simple explanation to correlate the 47 foot zone of mineralization penetrated by B-6, the information provided by holes 75B-7, 8 and 9 indicated that the zone was less than 2 feet thick. Essentially the results of hole 75B-6 were ignored. Drillholes 75B-10 to 75B-16 were collared mainly to the southeast of 75B-6 with confusing results. In 1976 Sproatt Silver Mines Ltd. (later Hecate Gold Corp.) was able to option the Falconbridge ground. Exploration emphasis was changed toward the Bob Zone, where a major underground exploration program was conducted in 1977-1978.

The complexities of the Tel Zone environment were not recognized by Sproatt Silver Mines Ltd. This is graphically illustrated by examining the large mineralized intersections in drillhole YGTL-85-012. This hole was collared from the same set-up as holes 75B-7, 8 and 9 trending in the same general direction as 75B-8. The narrow intersection found in hole 75B-8 was the East Limb and the larger Central and West limbs would have been found in 1975 if hole 75B-8 was allowed to extend into the second banded grey marble unit.

In June 1975, limited orientation soil sampling was undertaken by B. Manchuk for Falconbridge. The samples were analyzed for zinc, silver and arsenic. Results show strongly anomalous values in all three elements in an east-west direction between the Main Tel Zone and West Tel Zone.

In October 1975, Induced Polarization (IP) and VLF EM surveys were completed by G.E. White Geophysical Inc. The IP chargeability map for N=3 shows a moderate northwest trending anomaly. VLF results did not locate any anomalous conductive responses.

Between November 1975 and June 1984 no further work was done on the Tel Zone. A report written by J.B. Magee and R.H. Seraphim (1977) stated that:

> "However, accurate evaluation is precluded by inadequate core recovery in crumbly sulphides, acute angles of drill intercepts to lode dip, and an insufficient 'population' of drill intercepts. A decline tunnel is recommended initially on either the Bob or the Tel Zone to determine the average grade -- width, length and, if possible, the plunge of the best mineralization. The choice of which shoot to test first is dependent in part upon access from harbour sites. The determination of the best harbour and thence the easiest road route across the mile or two of flat terraine is currently in progress."

Hecate Gold Corp. experienced financial difficulties at the time the Bob Zone program was only partially completed, and the planned underground work on Tel Zone was never started (Shearer, 1985a).

From the end of the Bob Zone underground drilling in June 1978, the entire property lay idle until 1983. In 1983, Trader Resource Corp., through United Mineral Services Ltd., concluded an option agreement with Host Ventures Ltd. (successor company to Hecate Gold Corp.). After a claim relocation in June 1983 a comprehensive "Prefeasibility Study" was compiled from all available data including: geology, mineralogy, photo-structural analysis, geochemistry, geophysics, ore reserves, metallurgy, mine and mill waste disposal, hydro potential, identification of environmental and legislative considerations, capital and operating cost analysis and predevelopment program cost estimate.

International Geosystems Corporation (IGC) calculated, in the "Prefeasibility Study", ore reserves for the Main Tel Area by the inverse distance method as 24,000 short tons averaging 0.914 oz/ton gold equivalent, based on 1964 and 1975 drill results. Errors in hole potting in the Tel computer calculations appear to have increased the zone length by about 30% (Shearer, 1985b).

Field work on the Banks Island claims by Trader Resource Corp. started on February 18, 1984. Later in June and July 1984, R. Kidlark was assigned to conduct geological mapping and generally evaluate the Western Metasedimentary Belt, which included the Bob, Tel, Crossbreak and Foul Bay Zones. An overall geological map at 1:2500 was produced, in conjunction with 1:500 mapping around the main showings. The majority of 1975 drill core was relogged by J. Shearer and R. Kidlark. This core was subsequently moved to the main core storage facilities at Beaver Lakes. Much of the Kidlark work focussed on locating and defining the source of airborne (Dighem) geophysical anomalies, the results of a survey flown in March 1984. To complement the geological mapping, soil samples were collected over the entire area and analyzed for gold.

Diamond drilling by Trader Resource Corp. in October 1985 led to the discovery of a major extension of the Tel Zone, at depth, northwest of the surface showing. A large drilling program between November 1985 and March 1986 delineated several related mineralized zones. Total diamond drilling on the main Tel area is 33,679.5 feet (10,265.5 meters) in 91 holes. Metallurgical testing, conceptual mine planning, mineralography, rock geochemistry, modular mill design, rock stress analysis, access road design, marine infrastructure investigations and environmental baseline sampling were initiated as the success of the drilling program became apparent.

Mineral inventory and ore reserve calculations by different methods were undertaken by several independent groups (Wright Engineers Ltd., H.A. Simons Consulting Engineers and Montgomery Consultants Ltd.). Mineral inventory calculations by Simons Ltd. based only on the vertical cross-sectional model are:

Drill Proven + Probable Reserves 238,140 short tons
averaging 0.78 oz/ton gold

This report summarizes geological mapping, geophysical surveys and additional computer data manipulations carried out on the Tel Deposit since the mineral inventory in June 1986. The geological information is also included in the report "Geological Summary Report on the Tel Deposit, Banks Island" by J.T. Shearer, July 1986. For a detailed description of the reserve calculations and discussion of engineering studies the reader is referred to that report.

FIELD PROCEDURES

The legal corner posts (LCP) were surveyed by McElhanney Group Ltd. who also accurately established a number of designated points throughout the claims. A metric coordinate system was calculated based on station "Camp" (H-44), which was designated 30,480.00 N and 30,480.00 E (elevation 36.30 m) to facilitate correlation with work done since 1960. These points provided the data base on which all 1984 to 1986 transit, steel chain and EDM work is related.

Initially, for the Tel Area, a transit and EDM traverse was accurately closed which tied in old diamond drill holes, trenches and some surface contours. Close-spaced transit and EDM measurements were used as a base for 1:250 geological mapping. All diamond drill hole collars were picked-up by chain and transit. Hole deviation during drilling, both dip and azimuth, was recorded with a Sperry-Sun single shot, type B instrument.

In preparation for the E-SCAN geophysical survey, a grid was flagged and blazed along lines as shown in Appendix I, Figure 2. The lines were tied in to the main Tel baseline by an EDM survey.

GEOLOGY

I. REGIONAL GEOLOGY

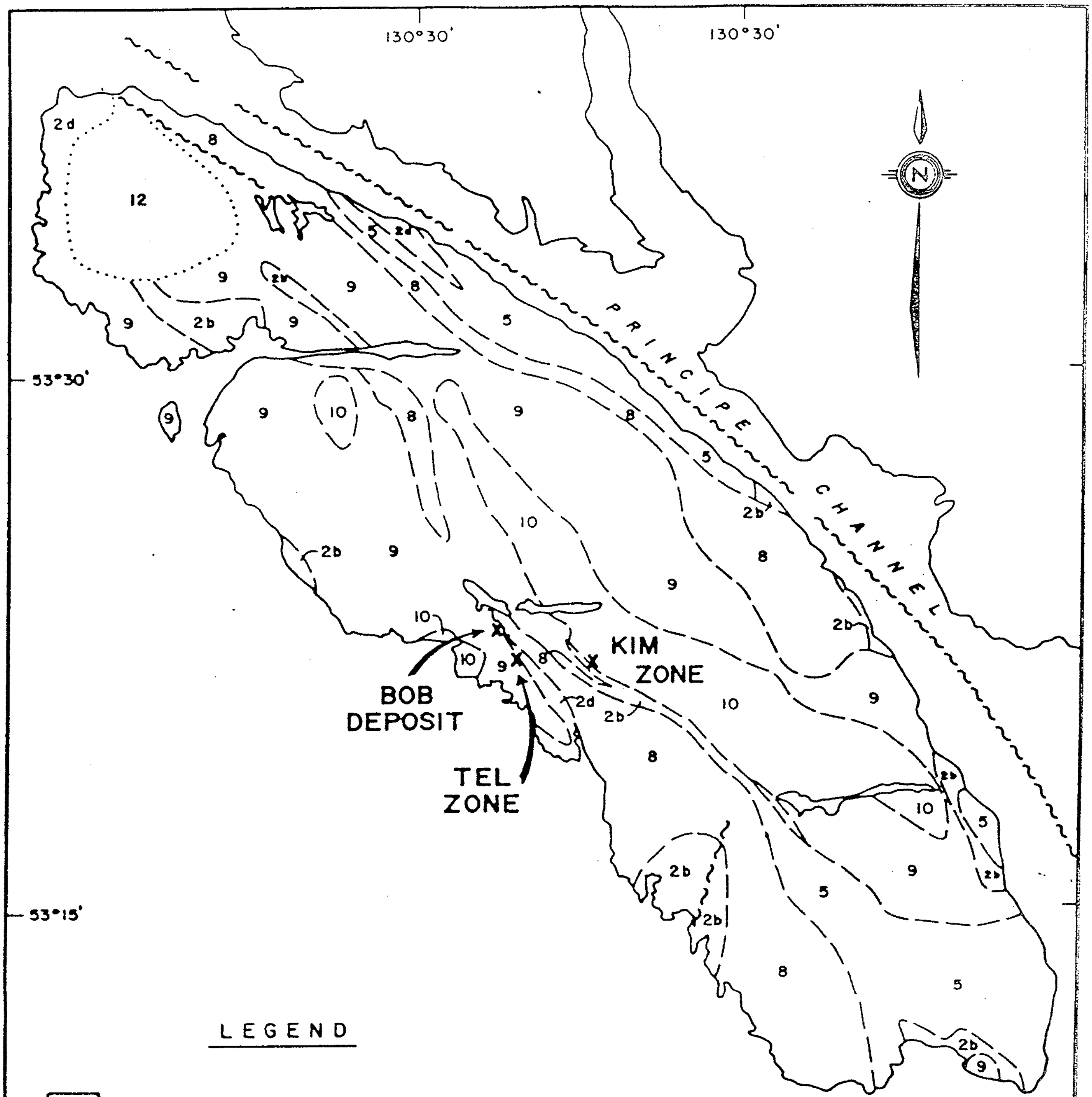
Regional geological features have been compiled by Roddick (1970) as Map 23-1970, Figure 4, mainly from field work conducted by the Geological Survey of Canada in 1963 along coastal exposures and in 1964 by very wide spaced landings with a helicopter on interior sites.

Banks Island lies along the western edge of a long, relatively narrow belt of plutonic and metamorphic rocks called the Coast Plutonic Complex. This forms one of the major geological components of British Columbia, extending from northern Washington through the Coast Mountains into southeast Alaska and Yukon Territory. General descriptions of the Complex have been given by Roddick and Hutchinson (1974) and Woodsworth and Roddick (1977). The following overview is taken mainly from these sources.

Recent interpretations of the western Cordillera (Monger and Irving, 1980) have identified several major terranes which have been accreted to the North American craton by transcurrent faulting and subduction. Banks Island metasedimentary rocks belong to the Alexander terrane.

The Alexander terrane in adjacent less deformed southeast Alaska is composed of Carboniferous carbonate and clastic sediments unconformably overlain by Upper Triassic limestone and Lower and Middle Jurassic felsic to intermediate volcanic rocks.

The Coast Plutonic Complex consists largely of intermediate and basic discrete and coalescing granitoid plutons, bodies of gneiss - migmatite and pendants (septa) of metasediments and volcanics. It is an asymmetric array, with a central gneiss core flanked by diorite and dioritic migmatites, most plentiful in the west, and granodiorite and quartz monzonite, most common in the east. Metamorphic intensity increases from greenschist facies in the eastern part of the belt to amphibolite (locally granulite) facies in the central and east-central parts. Woodsworth and Roddick (1977) suggest that most of the plutons in the Coast Mountains have been emplaced as diapiric solids, analgous to glacier flow and salt domes. Many contacts between plutons and pendants are faults or drag folds formed during formation of the igneous bodies. Some faults have been healed by re-crystallization. The clearest examples of "solid" movement of plutons are the several "tadpole"-shaped intrusions that have gradational to intricate contacts along their "tails". When the rock was more solid, movement could only take place by re-crystallization flowage, and this gave rise to internal foliation within the pluton. Commonly the quartz diorite and granodiorite are rarely uniform over broad areas. Zones of migmatite and small, lensoid amphibolitic inclusions are ubiquitous but variable in abundance.



LEGEND

12	ALLUVIUM
10	QUARTZ MONZONITE, GRANITE
9	GRANODIORITE
8	QUARTZ DIORITE
5	GNEISSIC DIORITE - MIGMATITE COMPLEX
2d	CRYSTALLINE LIMESTONE
2b	MICACEOUS QUARTZITE, SKARN, SCHIST

SCALE 1: 300,000

0 5 10 15 Km.

TRADER RESOURCE CORP.

GENERAL GEOLOGICAL MAP OF BANKS ISLAND

PROJECT: YELLOW GIANT PROJECT

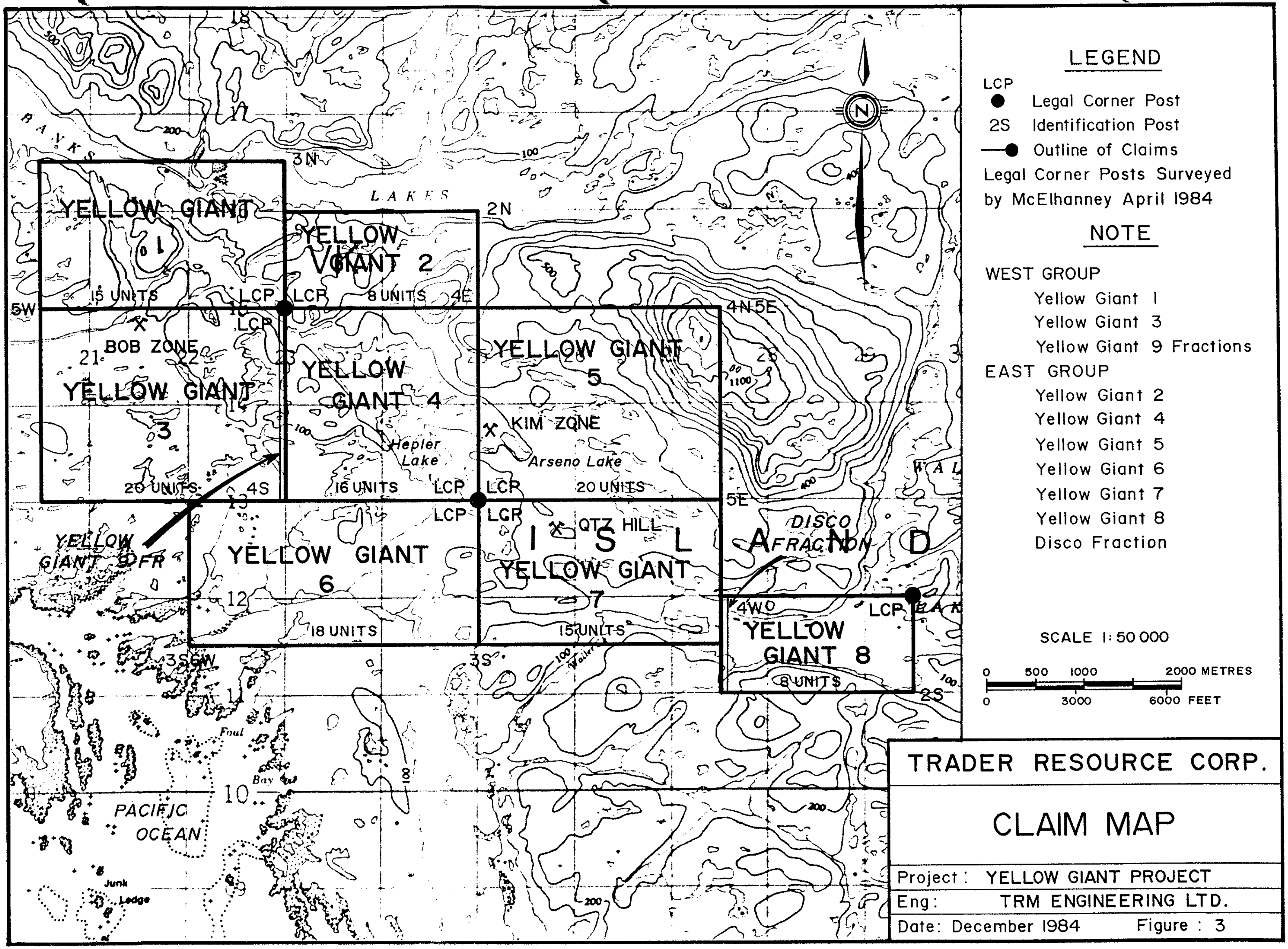
ENG.:

DWG NUMBER: FIG. 4

The main intrusive period lasted through most of the Cretaceous from about 120 Ma (million years ago) to 85 Ma, but was followed by two discrete later pulses at 70 ± 10 Ma, and 50 ± 5 Ma. The plutonism is widely regarded as evidence of heat generation on collision and suturing of the outboard terranes (Wrangellia and Alexander) on the inboard (Stikinia). Study of the metamorphic hosts, now evident as pendants and inliers, and which may be both intruded and protolith, enables tentative identification from the ghost stratigraphy of the terrane of origin. In the study area most inliers south of Burke Channel can be assigned a Wrangellian origin. North of Burke Channel and west of Work Channel lineament, inliers and pendants are fairly certaintly part of Alexander terrane whereas east of the lineament they appear to be part of Stikinia. The prominent Central Gneiss Complex (Tracy Arm) may be a highly deformed and metamorphosed amalgam of Stikinia and Alexander terranes unconformably overlain by an overlap assemblage equivalent to the Gravina-Nutzotin rocks of southeast Alaska.

Roddick (1970) reports that contact relationships everywhere indicate the more acid plutonic rock to be younger than any more basic plutonic rock in contact with it, but isotopic ages are related to the position of the plutons across the belt. Isotopic ages range from Early Cretaceous in the west to Late Cretaceous near the axis of the crystalline belt to Tertiary on the east side. The following Time Chart has been compiled to assist in correlation of the mineralizing events.

The central part of Banks Island is underlain by Unit 10b, Figure 4, a biotite-hornblende quartz monzonite. Surrounding rocks are hornblende-biotite granodiorite (unit 9c). To the east and west are large bodies of hornblende-biotite quartz diorite (unit 8b). Basic, gneiss-diorite-migmatite complexes (unit 5b) flank the quartz diorite. This outward zoning from a felsic core to progressively more basic rocks supports a conclusion from the detail petrographic work that intrusive rocks on Banks Island are inter-related and are part of the same zoned pluton. The field observations, discussed under Local Geology, reflect the complexities along the contacts between major phases.



TRADER RESOURCE CORP.

CLAIM MAP

Project: YELLOW GIANT PROJECT
Eng: TRM ENGINEERING LTD.
Date: December 1984 Figure: 3

Metasedimentary rocks are exposed over about 7% of Banks Island. They probably correlate with either the Dunira Formation of Early to Middle Pennsylvanian age (Woodsworth and Orchard, 1985) or Upper (Norian) Triassic Randall Formation exposed on the less metamorphosed islands north-west of Prince Rupert. On Banks Island the metasedimentary rocks are contained mainly in long, narrow northwesterly trending belts. The longest metasedimentary belt, from Banks Lake to Keecha Lake is 18 km in length. North of Waller Lake this Banks-Keecha belt splits into two arms which is the probable result of large scale folding.

It is this area of the Island, together with the parallel sedimentary belt from Foul Bay (Waller Bay) to Bob Zone, that the attention has focussed in the Yellow Giant Project.

TIME CHART

Tel Deposit
Western Coast Plutonic Complex

TIME	NAME or EVENT	REMARKS
Upper tertiary to recent glaciation	Isostatic rebound	Oxidation of sulfides
50 Ma	Intrusive event	
Eocene	Uplift of Coast Mountain core oblique subduction	Northeast dipping thrust faults
70 Ma	Intrusive event	
Tertiary		
85 Ma (80 Ma:k/Ar date on Sericite from Surf Inlet associated with mineralized shear zone)		
Upper Cretaceous	Major transcurrent fault movement of up to 300 km, right lateral	Major faulting/ drag folding
Cretaceous	Formation of Coast Plutonic Complex. Major intrusive event.	Intrusion of diorite/ monzonite
120 Ma (123 Ma:- Zircon date of Tel Zone diorite sill and k/Ar date of Kim Zone sericite - associated with late-stage quartz-pyrite veining)		
Jurassic	Randall Formation limestone-dolostone	
	Upper Triassic intrusions (Windy-Craggy)	Possible first phase pyrite mineralization at Tel Zone
Triassic-Jurassic	Suture of Alexander and Wrangellia terranes into one superterrane	
Early Triassic	Erosional unconformity	(possible karst/solution collapse at Tel Zone)
Early to Middle Pennslyvanian	Dunira Formation equivalent. Marble and shale.	Deposition of Tel Zone host rocks.

In the Coast Plutonic Belt the early structures of the terranes are largely obliterated. However, the Work Channel Lineament and/or the western edge of the Central Gneiss Complex probably originated as the suture of Alexander terrane against Stikinia. The discovery of mineralization resulted from an aircraft assisted prospecting program designed to investigate north coast lineaments (McDougall, 1972). Banks Island has an unusual density of faults, fractures and lineaments. The Island is bounded by deep seated, major faults that are assumed to have right-lateral displacement.

Blanchet (1983) has carried out a preliminary analysis of airphoto linears. Two major, right lateral faults with an average trend of 310° are recognized: (1) Arseno Fault which passes through Arseno Lake; and (2) Hepler Fault which passes through Hepler Lake. A very common direction for linears is 045° which Blanchet attributes to the movement along the 310° trending faults. Left lateral faults trend 090° with important examples being the Survey Bay linear and Crossbreak. At the Kim Zone Area the 045° linears are seen to offset the older 090° faults.

II. LOCAL GEOLOGY

The general geological setting of the Tel area is composed of a northwest trending metasedimentary assemblage dipping moderately to steeply (55°-75°) northeasterly. This assemblage is part of a series of septa which are bordered on the northeast by hornblende quartz diorite and on the southwest by diorite and quartz monzonite. These major intrusive contacts take the form of Lit-par Lit injection and magmatic stoping. Elsewhere, at the Discovery Zone, deep diamond drilling has indicated that the edges of these metasedimentary septa are defined by near vertical major faults. The septa are not shallow "roof pendants" but rather are associated with deep reaching structures.

(a) Lithology

The internal stratigraphy is remarkably consistent throughout all the metasedimentary belts although major large scale folding and faulting has caused complex repetition of some rock units. The stratigraphic sequence at the Tel Zone, as derived from extensive diamond drilling and surface mapping, is from east to west as follows:

TABLE III

Tel Zone Stratigraphy

UNIT		APPROXIMATE THICKNESS
(i)	Hornblende diorite, coarse crystalline	intrusive
(ii)	Altered Marble, skarnified	2-5 m
(iii)	Argillite-siltstone hornfels	5 m
(iv)	Altered Marble, skarnified	4-6 m
(v)	Siltstone-argillite hornfels (Magmatic stoping/Lit par Lit)	approx 30 m
(8)	Hornblende diorite, coarse crystalline	intrusive
(6)	laminated black argillite	27 m
(5)	argillaceous marble and calareous argillite	5.6 m
(iv)	BANK-BARGE Fault Zone	4.4 m
(4)	banded grey marble	30 m
		usually fault contact
(2)	silty thin bedded marble	29 m
(4)	banded grey marble	39 m
(3+4)	folded section with intrusive dykes, silty and banded grey marble	5-10 m
(3)	siltstone (part of folded section)	2 m
(2)	silty thin bedded marble, also hornfels fragments	30 m
(8)	diorite, coarse crystalline	intrusive
(vi)	argillite-siltstone hornfels (Magmatic stoping/Lit par Lit)	> 50 m
(9)	Quartz monzonite, coarse crystalline	intrusive

This sequence now represents approximately 270 m of section but allowing for fold repetitions the original thickness was probably in the order of 150 meters.

A very accurate surface detail geology map (Figure 6A) was prepared in June 1986 at a scale of 1:250 based on numerous transit and EDM reference points. (Figure 7 is a 1:500 which is at the same scale as all other figures included in this report). The most abundant rock type in the Tel area is unit 4, banded grey marble. This unit as a whole weathers light grey and is usually well exposed within a small scale, moss covered karst topography. On fresh surfaces the main component is white calcite of variable grain size. Bedding (banding) is prominent in most exposures although where coarse recrystallization has occurred the thicker, dark grey bands tend to be obscured. Thin delicate layering was consistently noted in the banded grey marble on the northeast margin of the deposit. This sub unit can be mapped at 1:250 scale and was named "unaltered banded grey marble". The contact between "unaltered" banded grey marble and the more typical slightly altered, banded grey marble appears to be an alteration feature related to faulting and dyke intrusion.

The second most abundant rock type in the Tel area is unit 2, silty thin-bedded marble. Unit 2 is generally recessive weathering and forms small scattered exposures. Many of the natural outcrops are under roots or around windfalls. The unit is commonly rusty weathering. Near the McIntyre Fault, unit 2 is commonly very altered and brecciated. Silty thin bedded marble is composed of alternating recrystallized pure carbonate layers and laminated silty sequences usually between 0.5 to 3 cm thick. Hornfelsed unit 2 is common on the east and west margins of the metasedimentary belt.

A thick section of very pyritic, thinly laminated argillite, unit 6, occurs east of the Bank-Barge Lineament. It is a rock composed of alternating black and dark grey laminations 1 to 4 mm thick. There are minor silty lenses. Abundant pyrite up to 20% is distributed in micro-lenses and disseminations parallel to bedding laminations. Some sections are very graphitic.

Unit 5, calcareous argillite and argillaceous marble, has not been seen in outcrop since it occurs under Sproatt Lake in close proximity to the Bank-Barge fault. It appears to be a conformable transition facies between the open marine deposition of the banded grey marble and the largely terrigeneous provenance of the thinly laminated argillite. Fault attenuation has resulted in variable thicknesses for each element of unit 5 as shown below:

Unit 5a	argillaceous marble	
	hole 85-004	1.2 m true thickness
	hole 85-005	4.2 m true thickness
Unit 5b	calcareous argillite	
	hole 85-004	4.4 m true thickness
	hole 85-005	1.6 m true thickness

A narrow, distinctive siltstone bed, unit 3, dark grey siltstone, may be useful in the future as a marker horizon. It has been noted in the following diamond drillholes:

TABLE IV

Dark Grey Siltstone Marker Unit 3

Approximate Thicknesses

Drillhole	Intersection Length	Drillhole Angle	Bedding	True Thickness
85-017	2.82	-59	60°	2.44
86-002	2.95	-51	74°	2.84
86-005	5.23	-59.5	79°	5.13
86-007	3.86	-67	68°	3.58
86-025	1.22	-49.5	74°	1.17
86-029	5.68	-56	66°	5.19
86-031	3.10	-46	76°	3.01
86-036	7.87	-54	72°	7.48
86-037	1.60	-63	59°	1.37
		Average of True Thickness		3.58 m

Although relatively little is known about unit 3 at the present time and it has not been seen in outcrop, a careful note should be made in future drilling or underground work of its orientation since it appears continuous throughout the property.

Map unit 1 is a general group for altered siltstone, argillite and hornfels found on the margins of the metasedimentary belts. These areas generally have very sparse outcrop and are covered by thin muskeg-swamp. Much of this area is probably underlain by recessive intrusive rocks which are present as Lit par Lit injection and zones of magmatic stoping. Rock exposed in these margin areas are the more resistant altered siltstone and biotite hornfels which form narrow linear mini-ridges with an elevation contrast of 1-2 m.

Unit 7 is composed of altered diorite sills and dykes. They are usually white-weathering with buff to rusty iron oxide staining. Most surface orientations of the intrusives are close to parallel with the enclosing marble but some cross-cut bedding at high angles. These sills have been folded along with the enclosing metasediments. Rocks mapped as pyritic quartz felsite sills in the "Crack Area" have assayed up to 0.46 oz/ton gold. Petrographic examination of six typical specimens show that the "sills" are a mixture of several plutonic types although in core specimens these intrusives are uniform when unaltered. Granodiorite is the most common rock type (Shearer, 1984b) with representatives of quartz monzonite, quartz diorite and hornblende-tremolite hornfels. Two specimens exhibited strongly developed cataclastic textures. Quartz granulation is common. A very distinctive characteristic of the intrusive sills are that many are boudins or even isolated fragments.

As indicated on the Time Chart, Page 15, Trader Resource Corp. commissioned a U/Pb date using Zircons obtained from a unit 7 skarnified dyke. A preliminary age from P. van der Henden for this dyke is 123 $\pm$ 4 Ma.

A large pluton to the east of Tel Zone is composed of magnetic, coarse crystalline, hornblende diorite to quartz diorite (unit 8). Several specimens of this rock have been examined in thin section (Shearer, 1985b). Over 70 hand specimens from outcrops around the Bob Zone were stained for potassium feldspar. Results show no mappable distribution of K-spar alteration with the possible exception of increasing potassium feldspars near the Bank-Barge lineament. An inspection of the lithotheque boards shows that there is considerable visual variation between the Bob Zone specimens, yet they are all within the quartz diorite field.

Three lithotheque boards have been constructed (Laznicka, 1974, 1975) in duplicate. One set will be stored in the Vancouver office and the other is stored at the Banks Island Camp. There is also a third set composed of the section off-cut blocks (the mirror image of each thin section) which have been stained for potassium feldspars, presently stored in Vancouver. The lithotheque library is designed to be clean and portable and can be used in conjunction with maps and other office materials. This system is ideally suited for the Yellow Giant Project which has a number of geologists working on mapping and also has subtle differences between the major granitoid suites. A total of 36 rocks were cut for thin section and summary descriptions are contained in Shearer (1984a). Additional lithotheque boards are planned for the Tel Deposit.

Kim-type intrusive rocks (unit 9) are mainly biotite quartz monzonite but vary from leucocratic granite through to hornblende diorite. The felsic end members are mainly quartz monzonite (lithotheque No. B23-555, BL 140E, QH-1, C-1, QH 180E & 120S, E-1, LY5-53) but also vary between granite and granodiorite. The mafic-rich end members vary between quartz diorite and diorite. However, this wide range of rock types is genetically related as indicated by the mafic constituents. Augite is present in the most mafic-rich in minor amounts but is mainly replaced by hornblende. Minor biotite has developed at the expense of hornblende. On the felsic side, biotite is the dominate mafic mineral and clearly replaces hornblende. Only a few relict grains of augite were noted in the quartz monzonite. Small rounded inclusions of the mafic-rich end members are commonly seen on the outcrop scale within the quartz monzonite. It is clear that the "Kim Zone Granite" is not the homogenous unit defined by Manchuk (1976).

(b) Alteration

Alteration of the host rocks in the vicinity of the sulfide/oxide mineralization is an important feature at the Tel Deposit. The main alteration types are:

(1) In banded grey marble:

(a) recrystallization in varying degree resulting in partial to complete destruction of dark grey bands;
(b) vuggy, white dolomitization which is commonly fracture controlled but occasionally results in massive, pervasive dolomitization;
(c) sparry, white calcite recrystallization apparently in part due to pressure shadows during intense folding (also probable solution feature);
(d) silicification near ore zones;
(e) development of disseminated "graphite" near major faults;
(f) brown iron oxide matrix filling in coarse breccia intervals;
(g) carbonate mylonites at locus of major faults;
(h) minor calc-silicates (skarn) near intrusions.

(2) In silty thin bedded marble:

(a) ankerite (siderite) replacement of breccia fragments;
(b) brecciation-boudinage (disassociation of silty layers);
(c) sparry calcite;
(d) limonite staining; superficial to intense;
(e) hornfels, calc-silicate development and minor skarnification.

(3) In diorite sills and dykes:

(a) chloritization; intense sericite development;
(b) skarnification, for example coarse actinolite stars;
(c) bleaching;
(d) pervasive silification and discrete quartz veining;
(e) grain size variation;
(f) hornfels and digestion of sedimentary fragments.

The most common alteration directly attributable to mineralization is limonite staining but in some cases the sulfide zones have not produced iron oxides. Silicification, as quartz veinlets, is present around some of the ore zones.

The ankerite (siderite) breccia noted in several drill holes may be related to an early karst solution collapse episode. Primary sulfide/oxide mineralization could have filled karstic voids. Intense, vuggy dolomitization also occurs around some of the sulfide zones.

Potassium/Argon age dating done by the B.C. Department of Mines on Kim Zone intense sericite alteration associated with mineralization gave a preliminary age of 123 Ma, which is identical to the U/Pb age of unit 7 dykes.

(c) <u>Structure</u>

Detail surface geological mapping and close-spaced diamond drilling suggest that the structure of the Tel Area is highly complex. A combination of tight, plunging isoclinal folding and a variety of major fault orientations contribute to the relatively large amount of data required to differentiate between the several plausible but differing geological interpretations. Until underground development is initiated, the actual importance and relative age of many major faults will be limited to correlation based largely on surface diamond drilling.

The general distribution of the main map units is controlled by the Tel Antiform which has a core of silty thin bedded marble, flanked by banded grey marble on either side. Apparently, the antiform is somewhat asymmetric since laminated black argillite (unit 6) is not represented on the west unless unit 6 is contained in the hornfelsic zone mapped as unit 1. The Tel Antiform is a large regional feature and can be traced from Hepler Creek in the south to the north end of Sproatt Lake, a distance of 1.8 km. This antiform does not extend into the Crossbreak showing area.

Numerous, relatively small scale folds occur on the west limb of the Tel Antiform which juxtapose short repetitions of banded grey marble, silty thin bedded marble, diorite and unit 3. The sulfide interval found in drillhole YGTL-85-007 could possibly be incorporated in this series of subsidiary folds.

The east limb of the Tel Antiform is now marked by a wide zone of shearing and brecciation called the McIntyre fault which trends 315° and dips 50-55° to the east. Shearing and graphitic slickensides mark the Tel fault immediately north of the Main Tel surface showing. The Tel fault is oriented 284°/74° E and apparently displaces the ore zone to the northwest with left-lateral separation.

Average bedding trends in various rock types are as follows:

TABLE V

Bedding Trends, Tel Area

Rock Type	Range of Strike	Average Strike	Range of Dips	Average Dip
Banded grey marble	306-332°	331°	50-82°E	66°
Silty thin bedded marble	320-332°	329°	58-90°	70°
Quartz veins-breccia	235°	-	-	-
Shearing	269-284°	277°	74-90°	82°
Intrusive sills & dykes	270-358°	323°	63-90°	75°
Hornfels	318-325°	322°	52-66°	59°

Bedding east of the McIntyre fault in banded grey marble is about 324°/70°E whereas to the west around the Central Tel showing bedding is closer to 342°/68°E. Intrusive sills and dykes were usually seen to cross-cut bedding at a small angle although occasionally they cut across at high angles. Overall, the dykes dip steeper than the enclosing metasediments.

Isoclinal minor fold structures are well exposed at 30,797 N + 28,100 E and measured with the following results:

	Minor Fold Plunge
Intrusive dykes	41° toward 349°
	44° toward 149°
	46° toward 149°
Banded grey marble	45-50° toward 350° and 150°

These minor folds are better exposed in the more resistant dykes than the marble. However, the intensity of regional shearing and drag along the northwest trending lineaments suggests that many of the major folds are probably rotated into steeply plunging structures.

MINERALIZATION

(a) Mineralization and Drill Results

Since 1964, the Tel Zone has been tested by 91 diamond drillholes and numerous surface trenches. Total amount of drilling is 33,679.5 feet (10,265.64 m).

All important drill intersections are listed in Table VI. The simple average grades weighted by intersection core length are:

Gold - 0.784 oz/short ton
Silver - 1.40 oz/short ton
Zinc - 1.86%
Lead - 0.57%
Copper - 0.13%

These averages do not consider weighting of drillhole azimuth or strike/dip of the mineralized zone.

By far the most dominant type of mineralization is a massive sulfides aggregate composed of pyrite, arsenopyrite, sphalerite and quartz, listed in decreasing in order of abundance. Occasionally, the massive sulfides are composed almost entirely of coarse crystalline arsenopyrite. Generally arsenopyrite appears to be a late-stage component associated with open-space filling, coarse grained, sparry calcite and monomineralllic chlorite masses. Much of the arsenopyrite-rich ore exhibits breccia textures and varying degrees of gangue replacement by arsenopyrite. Ore types can be summarized as follows:

Most common: (1) massive sulfides:
52% of all Zones pyrite-arsenopyrite-sphalerite-quartz
(1a) massive sulfides:
arsenopyrite dominant
Less common: (2) Breccia ore: arsenopyrite, pyrite,
33% of all Zones sericitic angular fragments

Less common: (3) primary jasperiod
Minor: (4) quartz breccia, pyrite-arsenopyrite,
(drusy quartz) Late stage
(6) graphitic quartz-pyrite
(7) undeformed disseminated arsenopyrite

Some of the massive sulfide mineralization has undergone intense deformation as illustrated by well-developed granulation textures of early phase coarse crystalline pyrite. Later stage arsenopyrite is undeformed. Banding in the massive sulfide intervals are summarized in Table VII.

TABLE VI

Important Drill Intersections, Tel Zone
February 1964 to March 1986

I. Main Tel Zone

Drill Number	Dip	Length (in m)	Gold oz/ton	Silver oz/ton	Copper %	Zinc %	Mineralization Type
P1	-38	1.22	1.52	1.2		13.3	Mass. sulfides
P2	-37	4.72	1.40	1.1		6.6	Mass. sulfides (diss.)
P3	-45	4.51	0.88	0.7		8.6	Mass. sulfides
P4	-48	2.29	1.16	1.2		14.5	Mass. sulfides
P5	-49	0.30	1.24	1.6		20.8	Mass. sulfides

Average 1.2 oz/ton gold over 2.59 m

Note: true widths are about 75% of intercept length (Seraphim, 1975).

P6	-49	1.37	0.66	1.5		4.1	bx qtz sulf
P26	-45	0.61	0.20	1.1			Mass. sulfides
P25	-40	0.46	0.36	0.8			Mass. sulfides
P14	-60	0.58	1.56	3.0	3.5		Mass. sulfides
Trench			1.16				Mass. sulfides

1975 Drilling:

Drill Number	Dip	Length	Gold oz/ton	Silver oz/ton	Copper %	Zinc %	
B-5	-45	33.07 - 33.38 = 0.30	5.04	2.80			Mass. sulfides
		30.48 - 33.53 = 3.05	1.45 sludge				
		35.05 - 35.81 = 0.76	0.25				qtz bx

TABLE VI

I. Main Tel Zone (cont'd)

1975 Drilling:

Drill Number	Dip	Length	Gold oz/ton	Silver oz/ton	Copper %	Zinc %	Type of Mineralization
B-6	-58	5.79 - 7.01 = 1.22	Tr	Tr	0.01	10.05	
		31.55 - 33.07 = 0.61	Tr	0.04	-	-	
		33.07 - 33.83 = 0.76	0.005	0.06	-	-	
		33.83 - 35.36 = 1.52	0.36	0.51	0.10	3.50	
		35.36 - 36.88 = 1.52	1.72	1.40	0.15	2.85	
		36.88 - 38.41 = 1.53	2.30	2.00	0.52	3.25	
		38.41 - 39.93 = 1.52	0.44	0.61	0.19	6.15	
		39.93 - 41.45 = 1.52	4.94	2.40	0.23	3.50	
		41.45 - 42.42 = 1.04	3.78	1.70	0.17	0.55	
		42.42 - 43.28 = 0.79	0.50	0.51	0.17	2.50	
		43.28 - 45.11 = 1.83	0.04	0.02	0.01	0.30	
		45.11 - 46.63 = 1.52	0.16	0.14	0.01	1.05	
		46.63 - 48.16 = 1.53	1.01	0.76	0.07	3.35	
Total B-6		33.83 - 48.16 = 14.33	1.47	1.00	0.15	2.73	mass. & diss.
		33.53 - 48.46 = 14.94	2.10 sludge				sulfides
B-7	-61.5	44.78 - 45.11 = 0.64	0.39	0.43	0.14	5.65	mass. sulfides
B-8	-57	51.97 - 52.58 = 0.61	0.55	0.83	0.14	3.74	mass. sulfides
B-9	-47	37.03 - 38.10 = 1.07	0.48	0.40	0.17	3.19	diss. sulfides
B-11	-70	25.39 - 31.24 = 5.85	1.01	1.23	0.18	4.59	mass. sulfides
B-12	-85	No significant intersections					
B-13	-85	26.06 - 33.53 = 7.47	1.15	2.07			mass. sulfides
		5-10% recovery - 30.48 - 32.92 - 1.15 oz/ton Au in sludge					
B-15	-45	61.42 - 61.54 = 0.12	0.28	0.14		0.25	
B-16		72.85 - 73.91 = 1.06	0.02				diss. sulfides

II. Central Tel Zone

Drill Number	Dip	Length	Gold oz/ton	Silver oz/ton	Copper %	Zinc %	Type of Mineralization
P-11	-43	12.90 - 14.94 = 2.06	0.27	0.8	2.65		mass. sulfides
P-10	-45	16.61 - 16.76 = 0.15	1.16	1.8	50% recovery		mass. sulfides
Trench			2.16	(poor recovery in P-19)			
B-3	-45	73.15 - 76.20 = 3.05	0.06 sludge				diss. sulfides
B-4	-57	27.43 - 30.48 = 3.05	1.54 sludge				diss. sulfides
		30.48 - 35.05 = 4.57	0.36 sludge				

III. West Tel

Drill Number	Dip	Length	Gold oz/ton	Silver oz/ton	Copper %	Zinc %	Type of Mineralization
B-1	-45	19.96 - 21.79 = 1.83	0.018				
B-2	-45	28.96 - 30.18 = 1.22	Tr				diss. sulfides

TABLE VI

DDH	DIP	AZIMUTH	FROM	TO	LENGTH	Au OZ/T	TYPE OF MINERALIZATION
85-004	-42	230	48.00	49.00	1.00	0.100	Mass. sulfides
85-005	-61	227					
85-006	-46	268	85.72	86.54	0.82	0.396	Mass. sulfides
85-007	-60	268	204.01	204.47	0.46	1.140	Mass. sulfides
			206.73	211.50	4.77	0.946	Mass. sulfides
85-010	-66	267	130.81	132.59	1.78	0.372	Mass. sulfides
			223.72	224.35	0.63	0.416	Jasperoid
85-011	-63	249	84.02	84.49	0.47	0.208	Quartz limonite
85-012	-43	266	46.33	47.12	0.79	0.320	Quartz limonite
			59.03	82.34	23.31	0.548	Mass. sulfides
			99.67	101.19	1.52	0.408	Quartz limonite
			107.98	109.57	1.59	0.126	Mass. sulfides
			113.67	115.67	2.00	0.670	Mass. sulfides
85-013	-53	265	50.23	52.40	2.17	4.352	Mass. sulfides
			73.15	74.00	0.85	0.166	Mbl-qtz breccia
			81.70	90.53	8.83	0.268	Mbl-qtz breccia
			107.80	109.70	1.90	0.139	Mass. sulfides
			114.44	117.96	3.52	0.107	Mass. sulfides
85-014	-43.5	268					
85-015	-54	269					
85-016	-50	263	46.28	47.68	1.40	0.415	Mass. sulfides
85-017	-59	265	53.10	53.64	0.54	0.312	Diss. in qtz
			132.59	139.65	7.06	1.422	Mass. sulfides
85-018	-41.5	277	75.00	76.00	1.00	0.080	Fault breccia
			148.60	156.36	7.76	0.274	Oxid. qtz & pyr
			165.00	166.00	1.00	0.120	Graphitic shear
			175.42	178.00	2.58	0.301	Mass. sulfides
			183.00	186.00	3.00	1.362	Graphitic shear
			201.24	206.50	5.26	0.230	Quartz breccia
			209.00	211.84	2.84	0.165	Quartz breccia
85-019	-43	264	61.57	62.40	0.83	0.162	Mass. sulfides
			104.90	105.77	0.87	0.108	Mass. sulfides
			143.60	143.99	0.39	0.120	Diss. sulfides
85-020 TO 85-025	No Significant Intercepts						

TABLE VI

DDH	DIP	AZIMUTH	FROM	TO	LENGTH	Au OZ/T	TYPE OF MINERALIZATION
86-002	-51	277	238.93	239.50	0.57	0.292	Mass. sulfides
			242.93	249.00	6.07	2.981	Mass. sulfides
86-005	-59.5	271	149.79	152.00	2.21	1.043	Mass. sulfides
			206.00	208.70	2.70	0.701	Mass. sulfides
86-007	-67	261	56.57	57.91	1.34	0.342	Mass. sulfides
			111.86	120.00	8.14	0.495	Qtz flt breccia
			131.96	132.48	0.52	0.607	Jasperoid
			135.94	141.00	5.06	0.976	Mass. sulfides
86-009	-75	266	69.09	71.26	2.17	0.228	Qtz limonite
			174.50	176.00	1.50	1.260	Mass. sulfides
86-011	-43.5	249	38.27	39.22	0.96	0.260	Diss. in qtz
86-013	-51	248	39.93	42.35	2.42	0.290	Qtz flt breccia
86-015	-62	245	48.82	50.29	1.47	0.624	Jasp/qtz brccia
86-017	-43	233	35.49	39.93	4.44	0.282	Mass. sulfides
86-019	-52	233	40.20	41.60	1.40	0.244	Lim qtz/diss.
86-020	-56	265.5	26.93	28.08	1.15	1.290	Mass. sulfides
			34.02	48.25	14.23	0.980	Jasp/massive
			59.13	66.46	7.33	0.045	Diss/Jasperoid
86-021	-68	232	50.90	52.42	1.52	0.204	Qtz breccia
86-022	-44	268.5	36.27	38.51	2.24	2.139	Qtz breccia
			43.00	58.22	15.22	0.707	Qtz ank/mass.
86-023	-41	232	54.30	62.25	7.95	0.080	Jasp/qtz brec.
86-024	-46	228					
86-025	-49.5	233					
86-026	-60	228	34.44	40.54	6.10	0.081	Qtz breccia
86-027	-61	237	121.52	126.00	4.48	0.455	Qtz breccia
86-028	-42	223	63.12	68.86	5.74	0.365	Qtz breccia
86-029	-56	223.5	95.56	106.37	10.81	0.462	Qtz limonite

TABLE VI

DDH	DIP	AZIMUTH	FROM	TO	LENGTH	Au OZ/T	TYPE OF MINERALIZATION
86-030	-67	219	139.50	144.98	5.48	1.081	Mass. sulfides
86-031	-46	228.5	89.73	91.50	1.77	0.170	Mass. sulfides
			105.71	106.16	0.45	0.144	Qtz breccia
86-032	-57	229.5					
86-033	-67.5	231.5					
86-034	-46	230	53.04	57.60	4.56	1.650	Jasp/massive
86-035	-42	230	94.84	96.00	1.16	0.085	Diss. in qtz
86-036	-54	230	125.35	127.31	1.96	0.148	Qtz breccia
86-037	-63	230					
86-038A	-60	228	79.74	82.38	2.64	2.239	Mass. sulfides
86-039	-43.5	230.5	61.48	62.91	1.43	0.086	Qtz breccia
			69.35	70.31	0.96	0.815	Mass. sulfides
86-040	-60	230.5					

TABLE VII

List of Banding/Layering
in Massive Sulfide Drill Intersections

Hole No.	Area	Dip of Hole	Azimuth of Hole	Sulfide Layering	Sulfide Contact with Faults or Host Rock
85-007	Central	-60°	268°	55°	55°
85-012	Central	-43°	266°	85°	21°
	W. Limb			42°	
85-013	Central	-53°	265°		55°
85-016	E. Limb	-50°	263°		62°
85-017	E. Limb			40°	
85-018		-41.5°	277°	60°	
				26°	10°
86-002		-51°	277°		13°
86-007	E. Limb	-67°	261°		42°
86-021	E. Limb	-68°	232°		52°
86-031	W. Limb	-46°	228.5°		73°
86-034	W. Limb	-46°	230°		28°
86-038A	W. Limb	-60°	228°		15°
86-039		-43.5°	230.5°		15-25°

The jasperiod ore is a hard, crustified and colloform limonitic iron oxide, finely laminated with very fine grained silica that carries high gold values. It has been encountered in several widely spaced holes. Jasperoid usually forms the entire mineralized section but in hole YGTL-85-012 it is in fault contact with fresh massive sulfides. Fragments of jasperoid have been noted in the quartz-arsenopyrite breccia. Samples of jasperoid examined by Harris (1986) contained traces of sericite, amphiboles, graphite and native copper.

Relatively abundant gold up to 100 microns in size was noted by Harris (1986) in specimens of pyrite-arsenopyrite-sphalerite massive sulfides, mainly within or on the contacts of various sulfide and gangue minerals. He states that (Harris, 1986):

> "The two samples from the Central Tel Zone (069X and 070X) are mineralogically similar to those from the A Zone. They consists dominantly of well segregated clumps of pyrite and sphalerite, with accessory

arsenopyrite, in a texturally heterogenous siliceous gangue. Carbonate is essentially absent, and no graphite was seen. Gold occurs in both samples, as grains up to 100 microns in 069X but finer-grained in 070X. It shows no consistent textural relationships, occurring totally enclosed in sulfides and quartz as well as on sulfide/sulfide and sulfide/silicate contacts.

The A Zone and B Zone samples both show more or less banded, crustified textures suggestive of vein origin.

The two samples from the West Tel Zone (071X and 072X) are only weekly mineralized, arsenopyrite being essentially the only sulfide. It occurs as disseminated clumps and strings of euhedral grains, apparently following grain boundaries and micro-structures in the hosting gangue. In 071X the gangue is largely quartz with minor carbonate, whilst in 072X these proportions are reversed. No gold was observed."

Possibly, the massive pyrite mineralization formed as a result of early filling of karst/solution collapse cavities. Decisive information may be found by carefully examining all mineralized intersections for overlooked cross-cutting diorite dykes. Coarse arsenopyrite phase mineralization may be related to a thermal event at 123 Ma. More work is required to resolve the history of mineralization and subsequent deformation.

(b) Computerization of Assay Results

In July 1986 analytical data for silver, arsenic, copper, lead, zinc, iron and sulphur and calculated values for iron sulphide from mineralized intersections from all Tel drilling, was submitted to Simons and entered into the data bank for the deposit.

Grade composites were calculated (see Appendix II) and contoured plans, Figures 8 to 42, were generated. The values plotted are average grades weighted by sample length in 10 m segments over vertical intervals of 50m. The intervals are:

above 0m elevation
0m to -50m elevation
- 50m to -100m elevation
-100m to -150m elevation, and
< -150m elevation.

Zero elevation is sea level as in other Simons sections and plans for the Tel Deposit.

Figure 7 shows the drill indicated ore zones, as developed by the mineral inventory, and two anomalies outlined by the June 1986 E-SCAN survey. Two northwesterly trending ore zones, one between surface and -30m and the second at depth greater than 50m and two E-SCAN anomalies of similar trend and elevation are outlined. When compared with the contoured plans, the following information is displayed:

(1) The range of average grade values in the ore zones are 0.001 to 0.500 oz gold /ton, 0.001 to 1.000 oz silver /ton, 0.001 to 1.000 % arsenic, 0.001 to 0.100 % copper, 0.001 to 0.500 % lead, 0.001 to 2.500 % zinc and 0.001 to 5.000 % iron sulphide.

(2) Broader zones of contoured values for all elements are outlined from 0m to -50m and -50m to -100m elevations. These are at similar elevations to the drill indicated ore zones, and have similar elevation and outline to the E-SCAN anomalies.

(3) Several anomalies, or areas of higher grade mineralization occur within each ore zone.

(4) Elevated values of iron sulphide and/or zinc are most commonly associated with gold anomalies. Higher grade contours for all elements are present in the central part of the ore zones (near 30700N, 28250E) from 0m to -100m elevation. Below -100m, fewer sections with higher grade values of silver, arsenic, copper and lead occur.

(5) In the southeastern part of the ore zone, there appears to be a correlation between gold and iron sulphide. E-SCAN anomalies indicate that there may be a southern extension to the main ore zone in this area.

GEOPHYSICS

In 1986, Premier Geophysics Inc. of Vancouver conducted two phases of E-SCAN geophysical surveys in the area of the Tel Deposit.

The following describes the E-SCAN system and its application at the Tel property. Reference to figures in the appended report is suggested.

Initial E-SCAN Testing of the Tel Ore Zone

In June 1986, induced polarization (IP) and resistivity surveys over a 150 by 225 meter grid centered on the known Tel ore zones (Report, Figure 2) was carried out. The survey was conducted on a 15 meter grid spacing, and was intended to determine whether the technique could:

1. detect the known ore zones of the Tel Deposit, from near-surface to >150 meters depth; and

2. discriminate between sulphide ore signatures and those of other non-ore rock units, for example the graphitic, pyritic argillite metasediments of the Banks-Barge lineament.

E-SCAN utilizes a new data acquisition technology which provides for saturation coverage of a property with the equivalent of thirty to forty spearate conventional electrical surveys, all conducted simultaneously, and covering every orientation of measurement. One benefit cited is that the explorationist does not need to commit to just one orientation of sampling, as is the conventional case, but can rely on saturation coverage for an objective assessment of all possible ore zone and structural configurations, combinations and orientations. Where overburden covers most of the area, and where structural conditions and ore shapes and orientations can be highly variable (the Tel area), E-SCAN saturation coverage can be expected to identify geologic zones and structures regardless of size or orientation.

Summary Report on
E-SCAN
Induced Polarization
and Resistivity
Surveys

Tel Property,
Banks Island,
British Columbia

June, October, November, 1986

for

TRADER RESOURCE CORP.

Report by Greg A. Shore
Premier Geophysics Inc.
Vancouver, British Columbia.

Report submitted February 18, 1986

Contents

FIGURES:

Tel ore zone area data plots:

North Grid Extension area data plots:

1.0 SUMMARY Refer to Figures 3 and 5.

E-SCAN induced polarization (IP) and resistivity surveys over the Tel ore zone and adjacent land have detected anomalous responses in six areas, in addition to mapping the signature of the known ore zone itself. Four of these anomalies are connected to the main ore zone by fault zones which are themselves anomalous in signature.

The six anomalous zones that have been identified and warrant follow-up work are:

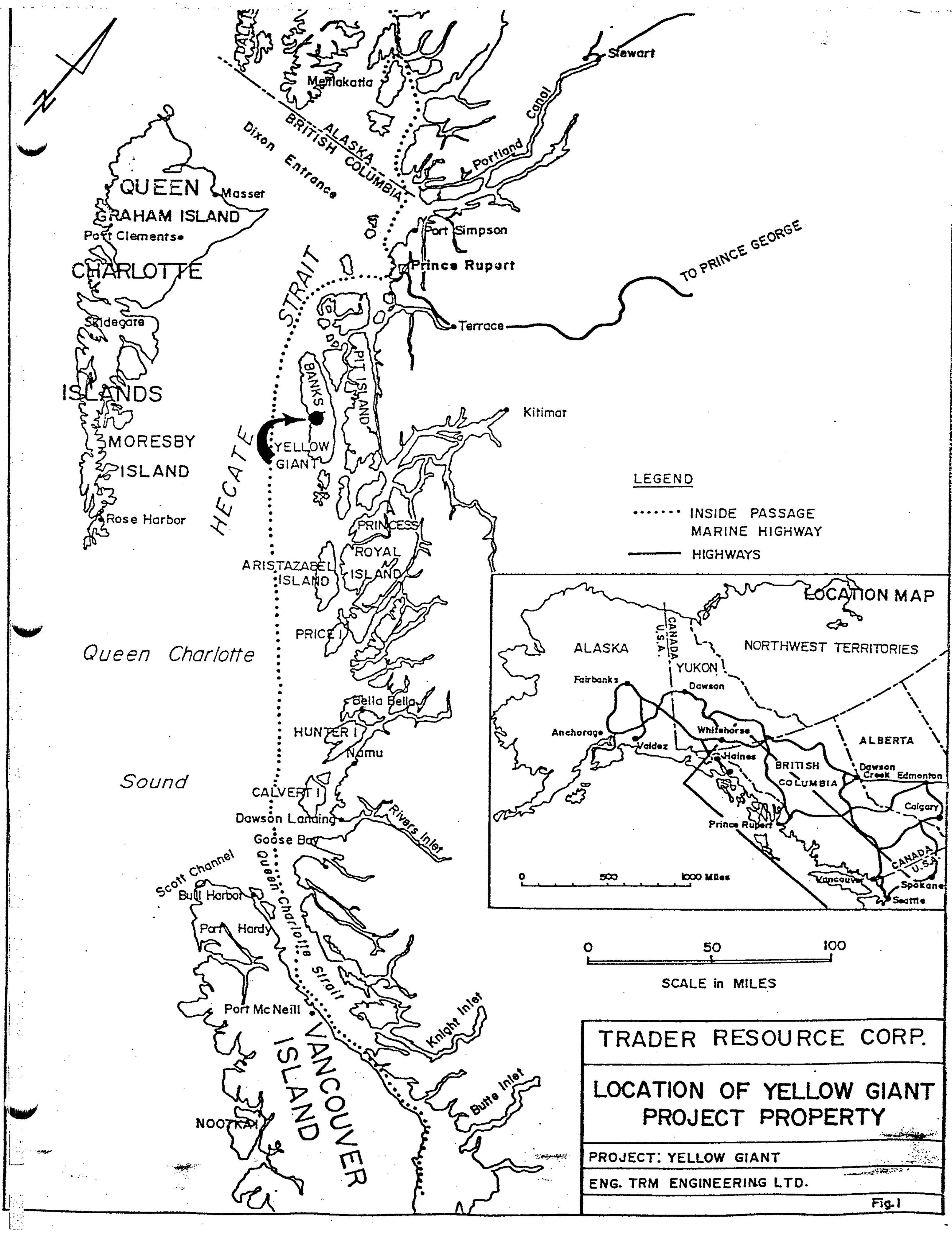
1: The IP anomaly defining the known Tel ore zone extends southeast into undrilled ground and represents a possible extension of the known ore structures in this direction. This is a first-priority drill-test area.

2,3: Two broad and distinct IP anomaly zones lying in the marbles southeast of the main ore zone warrant priority drill investigation due to the similarity in size, setting, and electrical signature as compared to the known ore zone anomaly. An anomalously responding fault system connects these anomalies with the main ore zone, all within the known marble environment.

4: An anomalous zone lies along the strike of the cross faults passing through the Tel ore zone. Limited drilling in this area has provided gold values; additional investigation is warranted.

5,6: Two other possibly anomalous zones in unknown or poorly defined rock units require various types of follow-up investigation including drilling to determine geologic/economic interest.

The tight correlation between the known (drill-indicated) gold/sulphide ore zones of the Tel deposit and the E-SCAN anomaly outline establishes the E-SCAN method as a viable mapping tool for the marble environment of the Yellow Giant Property.



TRADER RESOURCE CORP.

LOCATION OF YELLOW GIANT PROJECT PROPERTY

PROJECT: YELLOW GIANT

ENG. TRM ENGINEERING LTD.

Fig.1

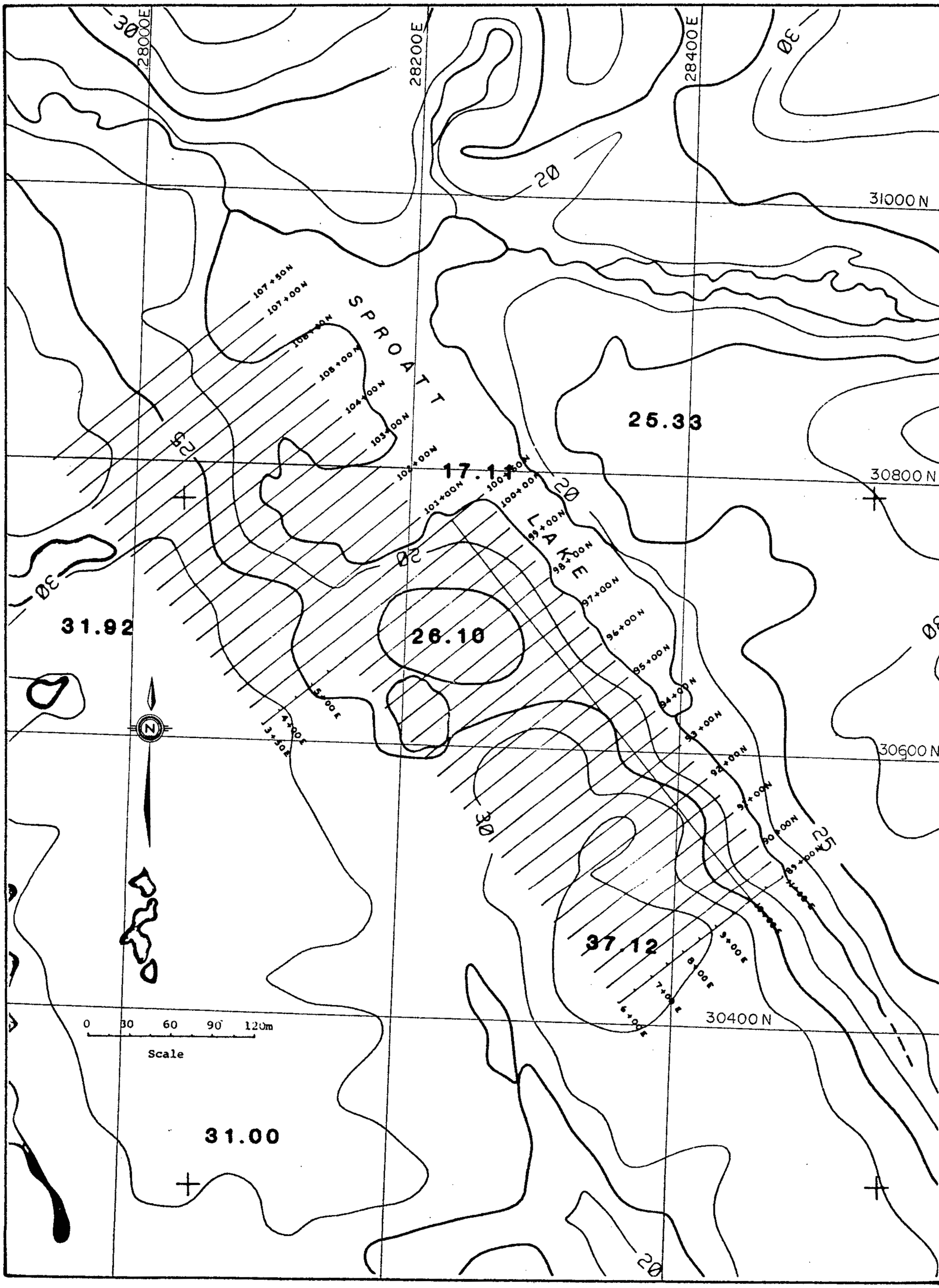


Figure 2

Location of E-SCAN survey grids, Tel Zone and adjacent north grid and southeast extensions.

2.0 INTRODUCTION

In June 1986 Premier Geophysics Inc. operated a series of E-SCAN induced polarization and resistivity surveys over the Trader Resource Tel gold-silver deposit on Banks Island, B.C. The purpose was to evaluate the usefulness of the E-SCAN method in mapping Tel type deposits in the complex area geology.

The marble zone which contains the Tel deposit extends for considerable distances both northwest and southeast of the proven ore zone, in a generally similar geologic setting. Since this area has not been successfully mapped with geophysical methods heretofore, the demonstration of any geophysical (or other) tool which could definitively detect the Tel deposit would be of interest for application elsewhere in the marble zones of the Yellow Giant property.

The E-SCAN surveys operated in June 1986 at Tel were successful in precisely outlining the drill-indicated ore zones (see Figure 6, and section 4.1.1 of this report). Additional E-SCAN coverage was obtained in October and November 1986 to resolve the extent and character of two new anomalous zones which extended beyond the June test grid.

The results of the June test surveys and of the subsequent extension surveys are reported herein, commencing in section 3.0.

2.1 Description of the E-SCAN system

E-SCAN is an automated data acquisition system employing up to 254 individually addressable electrodes installed in the ground at any one time. While the data acquisition is computer controlled and occurs at a very high rate of speed, each measurement is a conventional time domain IP and resistivity measurement, noise-averaged and logged on disc. The principal time savings lies in the elimination of the usual wire dragging and setup for each measurement, allowing actual direct measurement time to occupy 90% of each 8 hour day.

The E-SCAN system uses a conventional reversing DC square wave with an on/off pulse ratio of 1:1 and a total cycle time of 2 seconds. IP measurements for this survey were measured over an integration period of 167 milliseconds following a delay of 167 milliseconds, expressed as a percentage of the measured primary voltage.

The data presented in the plan plots are pole-pole array data, measured using one current electrode and one potential electrode on the property and corresponding current and potential "infinite" reference electrodes located distant from the survey area. The pole-pole array has the advantage of requiring less array space per unit penetration, and provides for the least complicated and least ambiguous interpretation of all survey arrays. This is particularly important in areas of complex geology such as is found in the Yellow Giant project area. The density of measurement and the multi-directional character of the E-SCAN data set allow averaging of noisy data to provide for logical and unambiguous resolution of anomaly and structural details at scales much finer than is possible with conventional surveys.

2.2 Previous IP/resistivity experience, Tel area.

The Yellow Giant property on southwestern Banks Island has a long history of exploration effort. The present program of exploration carried out by Trader Resource Corp. is the first to identify economically significant ore volumes and grades.

The Tel deposit is a series of gold-bearing sulphide zones extending over an area at least 35 metres wide and over 150 metres in length, extending from outcrop to depths over 150 metres. At the time of this report, the Tel deposit remains open at depth and on three sides.

A conventional (pole-dipole) induced polarization and resistivity survey (White, 1975) has been conducted previously over the Tel deposit, with mixed results. While anomalous responses were noted in the vicinity of the known sulphide ore outcrop, the spatial correlation between data and known sulphides was poor. The 1975 IP results indicated a northwesterly trend from the outcropping sulphide area, while the recent drilling (and the E-SCAN results) prove a westerly trend for the main ore zones tested to date.

The interpretation of the 1975 data was further confused by strongly anomalous responses originating from non-ore rock units (the closely adjacent graphitic argillites of the Banks-Barge lineament, and other unidentified rock units lying west of the known ore zone) which were indistinguishable from the responses originating from the sulphide ores.

By providing a hundredfold greater density of measurements, with measurements made in all directions instead of one, and with each of these measurements providing greater resolution at less susceptibility to distortion from nearby rock units, the E-SCAN survey method has been able to precisely outline the Tel ore zone, and to identify geophysically similar drill targets representing possible new ore.

2.3 The Tel deposit as an induced polarization and resistivity target.

Hosted in marbles, the Tel sulphide-gold-silver ore should represent an induced polarization target. However, as with any geophysical target, the anomalous quantity must be distinguishable against the surrounding non-anomalous rock, the background. In the Tel area, there are strong sources of electrical distortion in the Banks-Barge lineament (graphitic pyritic argillites) and in the very conductive layers of recent sediments found in lake-bottoms and depressions.

Initial tests of the E-SCAN system directly over the ore outcrop area confirmed a recognizable IP anomaly (2.5% to 4%) in an otherwise low chargeability (1.8% to 2.5%) marble environment, and indicated a low resistivity anomaly for the outcropping ore zone (600 ohm-metres) in a 1000 to 4000 ohm-metre marble background. By comparison, the responses obtained from the closely adjacent graphitic argillites were extreme, with IP in the 7% to 10% range and with resistivities of less than 50 ohm-metres.

The discrimination of economically significant responses in this complex and largely overburden-covered geology is therefore less straightforward that in the textbook IP case where a uniform low-background rock unit is searched for any higher (anomalous) values. What is anomalous in marble may be normal for the Kim granitic unit and lower than background for the argillite unit. The definition of any value as "background" or "anomalous" first requires identification of the rock type involved, and establishment of its "background" unmineralized signature.

Data interpretation for the area thus has two steps:

1. Identify the marble environment as distinct from the argillite unit by means of its more moderate levels of IP response and higher resistivities, making use of any mapped outcrops and drill information as corroboration.

2. Within the marble unit, look for anomalous IP response (2.5-6%) against a background of 2.5% or less, together with a lower resistivity.

To date, only the marble rock suite (which hosts the known Tel orebody) has been sufficiently tested and drill-correlated to allow confident definition of "anomaly" versus "background".

2.4 Correlation of E-SCAN results with the known Tel ore zones.

See Figure 6.

The lateral boundaries of the Tel deposit are clearly mapped by the induced polarization (IP) results, using standard E-SCAN grid methods with local current injection.

While the conductive nature of the ore environment is indicated in shallow resistivity measurements over the outcrop, the wide and irregular distribution of near surface, strong conductors (Sproatt Lake fault, graphitic argilliite unit, shallow surficial deposits) renders most of the moderate depth resistivity data close to the Tel deposit uninterpretable. However, a conductive axis for the deposit is clearly shown in the mise a la masse survey, its clarity due to the introduction of current directly into the deep target area, away from surface distortions.

The resistivity signature remains a minor part of the Tel orebody electrical signature. The primary telling characteristic is the IP signature, which correlates with the drill-indicated ore zones precisely. Sulphide mineralization, massive or disseminated, will provide IP responses. Coincident resistivity anomalies (conductors) may or may not be present. If the sulphide mineralization is discontinuous or disseminated, there may be no low resistivity signature, and even a high resistivity response if sulphide fracture-filling is complete and/or carbonate or silica precipitation is pervasive. The indicated conductor at Tel suggests a strongly faulted structure at least, and implies substantial lengths of connected conductors (mineralization) in order to provide the strong mise a la masse signature.

3.0 SUMMARY RESULTS AND RECOMMENDATIONS

The data and interpretations are presented on two map bases, one covering the known Tel ore zone and the area adjacent to the southeast, and the other covering the area north and west of the known Tel ore zone, referred to as the North Grid Extension.

The summarized structural features and anomalous IP zones are presented in Figures 3 and 5. Note that only those structures which are identifiable in the E-SCAN data (principally the resistivity data) are presented...it is likely that other faults and contacts occur, but are not detected by E-SCAN due to a lack of measurable electrical response or characteristics. These results can be used to more accurately plot geologically mapped or inferred structures and/or boundaries, and to identify unsuspected features beneath overburden. As is always the case, the intention of the geophysical surveys is to enhance and supplement the geological understanding of the area under study.

ANOMALY 1: Main Tel ore zone anomaly, southeast extension.

Map: Main Tel ore zone and adjacent southeast area (Fig. 3)
Also refer to Figures 6, A.1, A.2

The correlation between IP anomaly and drill-indicated ore is very close on all sides of the ore zone except the southeast. This is the only area where the drilling pattern has not yet cut off the ore zones; it is largely untested to date, having been penetrated partially by only one hole.

The IP anomaly bulges out to the southeast, then thins and extends further along a fault-contact lying between the silty thin-bedded marble and the grey banded marble.

The mise a la masse contours also bulge and thereby indirectly identify anomalous conductivity oriented southeast across the IP anomaly zone, further supporting the probability of ore extension.

The extended zone should be thoroughly drilled from near-surface to depths in excess of 150 metres.

ANOMALY 2: Adjacent to Tel zone, southeast in marbles.

Map: Main Tel ore zone and adjacent southeast area (Fig. 3)

Anomaly 2 lies completely enclosed by marble units, its center 135 metres southeast of the main Tel ore zone. The anomalous IP values are entirely consistent with those mapped over the known Tel zone, and the background IP levels are also comparable.

The data suggest that the mineralized zone may not extensively subcrop (the area is mostly covered by overburden), but detailed prospecting should be undertaken nonetheless in advance of drilling and/or trenching.

There is a narrow but clear IP anomaly extending between Anomaly 2 and Anomaly 1 (Main Tel ore zone) along the fault-contact between the silty thin-bedded and grey banded marbles. A narrow anomalous zone also extends southeast to Anomaly 3, again along an indicated fault. In anticipation of a possible continuous zone of mineralization extending from the Main Tel ore zone through to Anomaly 3, a drill pattern should be established along a new skid trail located parallel to, and 50 to 80 metres northeast of, the average strike of Anomalies 1, 2, and 3. Initial holes would test for economic mineralization at six to eight points along strike, with infill drilling depending on initial positive results. The zone's indicated lateral boundaries should be drilled from near-surface to at least 150 metres vertical depth.

ANOMALY 3: Adjacent to Anomaly 2, southeast in marbles.

Map: Main Tel ore zone and adjacent southeast area (Fig. 3)
Also, read ANOMALY 2 details above.

Anomaly 3 is identical in IP and resistivity characteristics to Anomaly 2, and lies a further distance along the marble units southeast of Anomaly 2. It is well defined within the present coverage, but is open to the southeast on a 50 metre wide front.

Anomaly 3 should be drilled from the same baseline of holes proposed under Anomaly 2 above, and to similar depths. If economic mineralization is detected, the E-SCAN coverage should be extended further southeast to outline and define the rest of the anomaly prior to extending drilling southeast.

ANOMALY 4: On westerly strike of Tel ore zone main fault(s).

Map: Main Tel ore zone and adjacent southeast area (Fig. 3)
Also, North Grid Extension (Fig. 5)

Anomaly 4 lies west of the Main Tel ore zone, on or near the westward extension of the main Tel cross-fault(s) and on strike with the deepening trend of mineralization. The area has only a few drill holes and is poorly understood geologically at present. Some gold-bearing intersections (associated with graphite) are noted deep in this area, and some surface showings occur.

While the area is nominally mapped as marble, the deeper geology is little understood. Adjacent to Anomaly 4 to the west and northwest is a broad lithological unit whose apparent "background" IP signature is the same as the values recorded in the Anomaly 4 area. This area may be anomalously chargeable marbles (and therefore a priority drilling target) or perhaps a fault-shifted pocket of the broad unit mapped to the west and northwest (non-anomalous).

INTERPRETED GEOLOGY

Figure # 3

program: /tel/plotsumm.8
DT: 87/02/17 16:03:35
Premier Geophysics Inc.
Vancouver, B.C.

INTERPRETED ANOMALOUS IP ZONE, NEAR-SURFACE TO -30 METRES (AMSL).

INTERPRETED ANOMALOUS IP ZONE, DEEPER THAN -30 METRES (AMSL).

DEEPER LYING INTERPRETED ANOMALOUS IP ZONE, DEEPER THAN -50 METRES (AMSL).

TRADER RESOURCE CORP.
Tel Zone and adjacent area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

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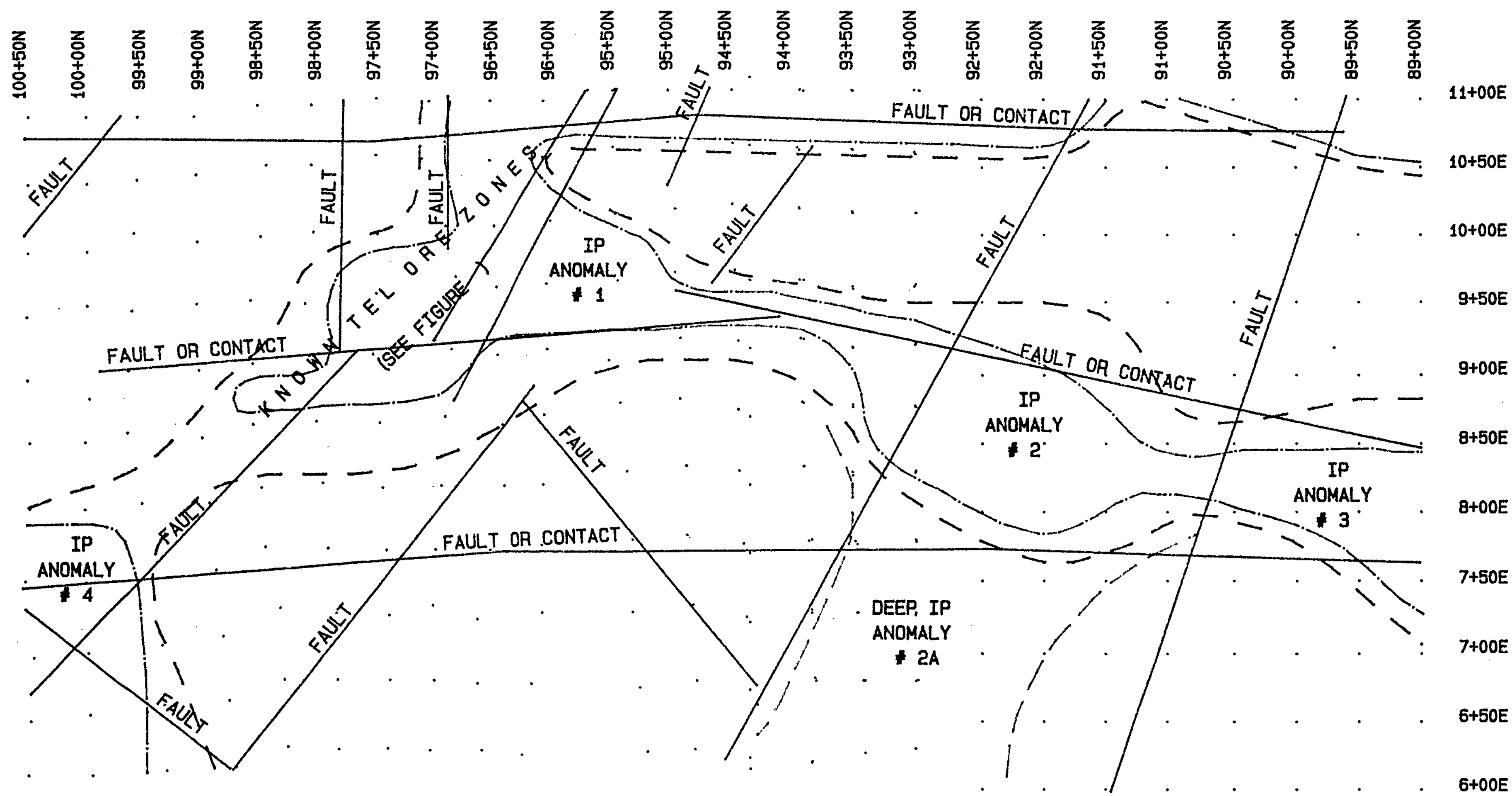
METRES



RECOMMENDED DRILL TESTING
OF ANOMALIES 1, 2, 2A, 3.
Figure # 4

program: /tel/plotsumm.8
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Premier Geophysics Inc.
Vancouver, B.C.

INTERPRETED ANOMALOUS IP ZONE, NEAR-SURFACE TO -30 METRES (AMSL).

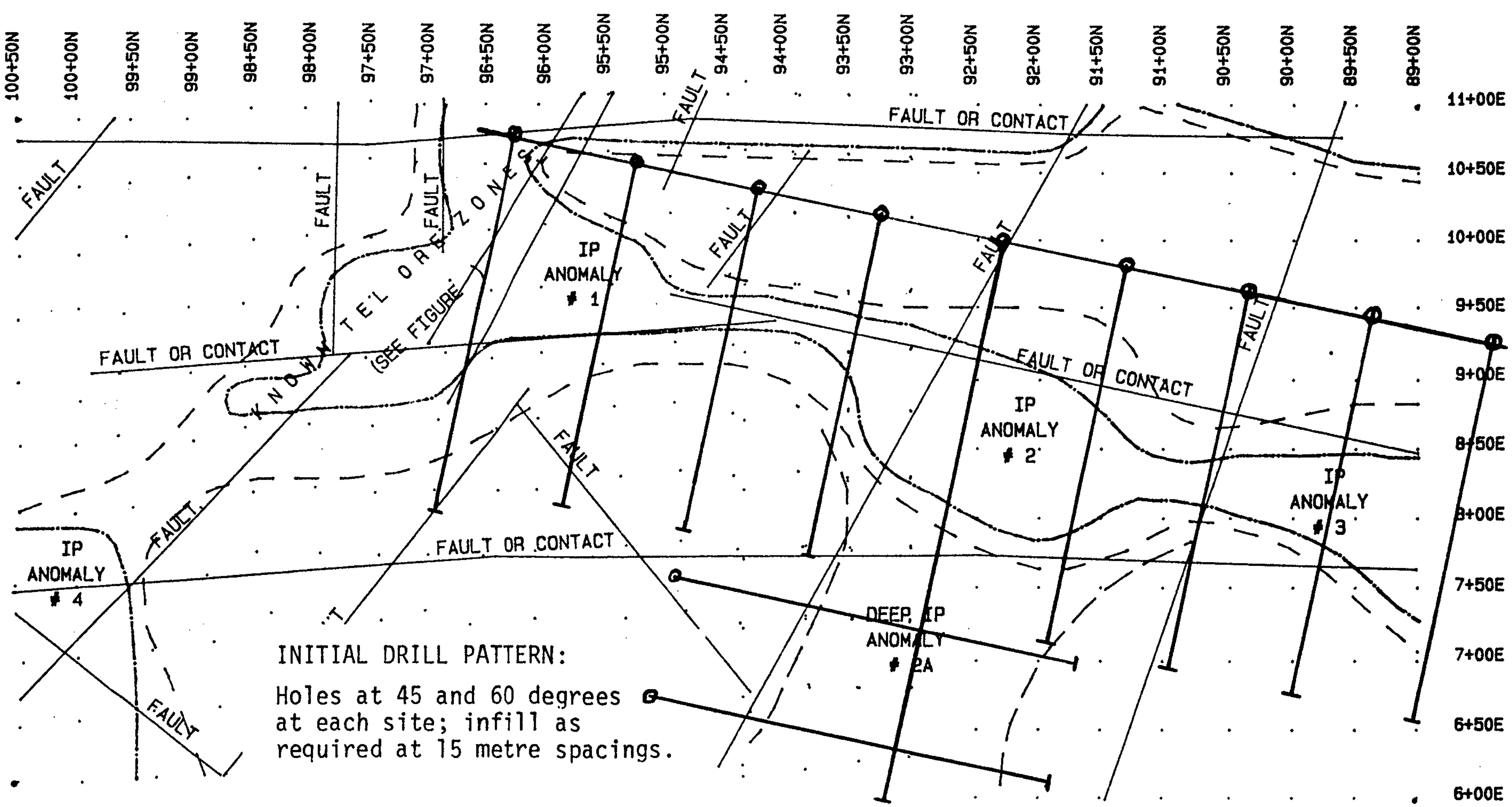
INTERPRETED ANOMALOUS IP ZONE, DEEPER THAN -30 METRES (AMSL).

DEEPER LYING INTERPRETED ANOMALOUS IP ZONE, DEEPER THAN -50 METRES (AMSL).

TRADER RESOURCE CORP.
Tel Zone and adjacent area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES



Initial drilling of this area should establish rock type first. If it is marble, watch for other (non-ore related) sources of IP response such as graphitic zones. If the typical Tel zone sulphide and gold association is not present, then care should be taken to test for other gold associations which may define a second economic E-SCAN signature to be watched for (Tel sulphides in marble being the first to be established).

ANOMALY 5: On strike west from Anomaly 4; uncertain geology.

Map: North Grid Extension (Fig. 5)

Anomaly 5 has the distinction of lying further west, on strike with the Main Tel ore zone and Anomaly 4. Little is known of the geology here, and the principal interest lies in the combination of location on strike with the Tel zone cross structure(s) and the occurrence of locally anomalous IP levels with anisotropic characteristics in both IP and resistivity.

Resistivity anisotropy is widely measured in and around Anomaly 5, and is in itself not an unexpected signature across the edge of steeply plunging metasediments. Anisotropic IP values may also occur readily in these circumstances, but in fact do not, except in this one area on strike with the Main Tel fault(s).

If the anisotropy is due to a zone of strong shearing or other directionally preferential structure rather than original bedding now tilted, then the possibility of mineralization occurs and should be evaluated.

This area should be drilled (again shallow and deep) from north to south from at least two sites. More intensive mapping of this area should identify general rock types, at which time the E-SCAN results should be re-assessed and a drill site decision made.

ANOMALY 6: Northwest of the Tel ore zone, in uncertain geology.

Map: North Grid Extension (Fig. 5)

Anomaly 6 lies in unknown geology. It is of interest if it lies in marble, or if it is in the same rock unit as the surrounding lower chargeability rocks (thereby an "anomalous" zone). This is the lowest priority anomaly of the six reported here, but only because of the many unknowns at present.

The area should be mapped to determine rock types, and the possibility of anomaly status reviewed with that information in hand. A single drill hole through the area would establish geology and therefore mineralization potential. Such a hole should be long enough, however, to establish rock types within and outside the potential anomaly area.

4.0 REVIEW OF SELECTED DATA RESULTS

Figures A.1 and B.1 show IP responses at the shallowest sampling levels. The grids of dots represent the location of the 452 electrodes making up the total E-SCAN network. Over 19,000 individual IP readings were logged, along with over 19,000 apparent resistivity measurements. These data form the master data set from which all plots of specific depths or other characteristics are identified and used.

The data used in the following plots are pole-pole array IP responses, calculated from the master E-SCAN data set, with the value plotted at the mid-point between the two electrodes responsible. The orientation of the data tic indicates the orientation of the current flow for the measurement (as well as pointing to the electrodes). The colour and length of the tic encode the IP value according to the key at right. IP and resistivity pole-pole data are plotted using similar conventions for this particular pseudo-depth plan viewing of the E-SCAN data.

4.1 DATA SET A: Tel Zone and adjacent area to southeast.

4.1.1 Correlation of E-SCAN with Tel ore zones.

See Figure 6.

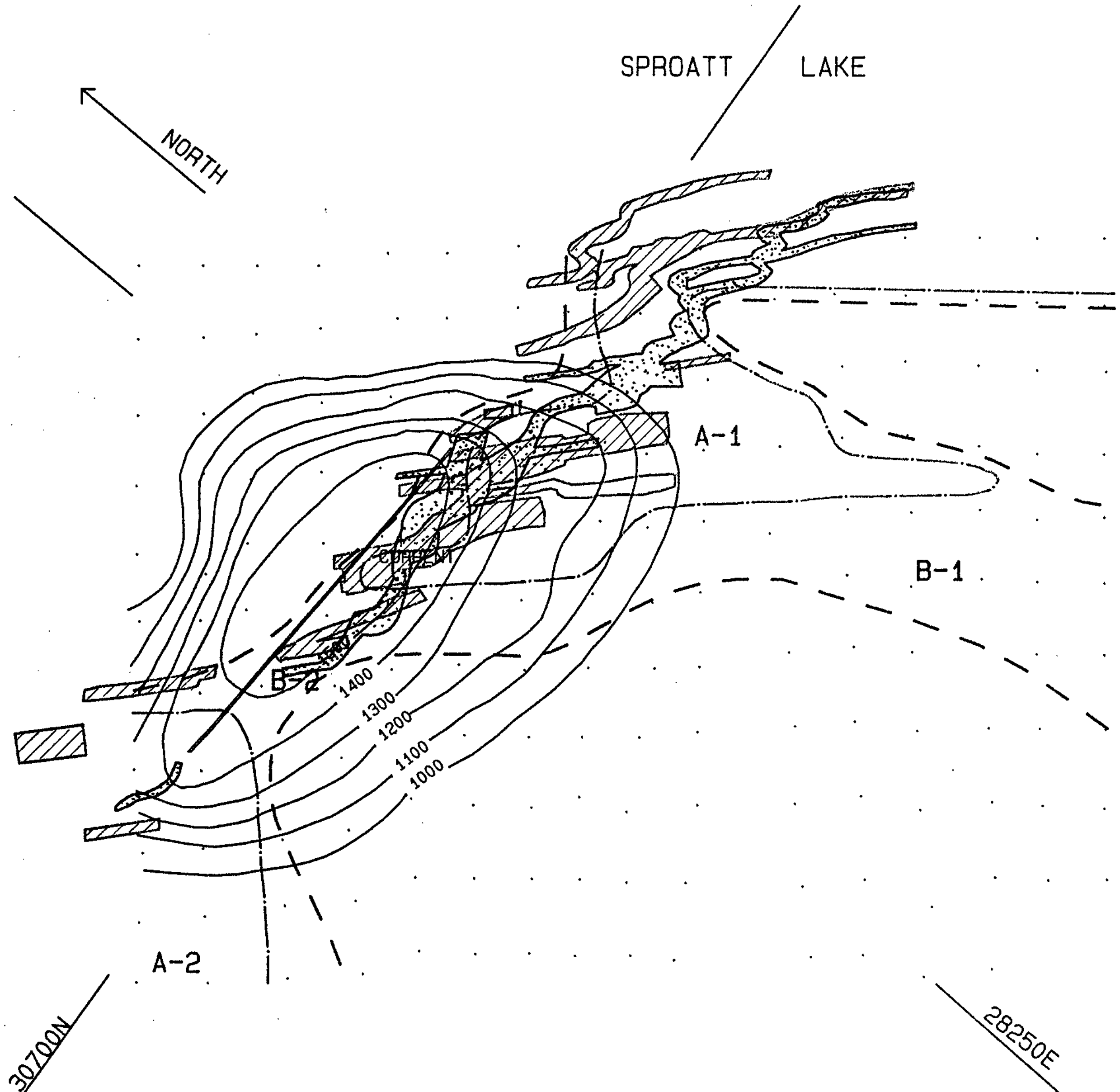
Features:

- virtually all known ore zones are contained within the IP anomaly outline.
- mise a la masse conductive axis correlates with deep ore zone position and orientation.

The lateral boundaries of the Tel deposit are clearly mapped by the induced polarization (IP) results, using standard E-SCAN grid methods with local current injection.

While the conductive nature of the ore environment is indicated in shallow resistivity measurements over the outcrop, the wide and irregular distribution of near surface, strong conductors (Sproatt Lake fault, graphitic argilliite unit, shallow surficial deposits) renders most of the moderate depth resistivity data close to the Tel deposit uninterpretable. However, a conductive axis for the deposit is clearly shown in the mise a la masse survey, its clarity due to the introduction of current directly into the deep target area, away from surface distortions.

The resistivity signature remains a minor part of the Tel orebody electrical signature. The primary telling characteristic is the IP signature, which correlates with the drill-indicated ore zones precisely. Sulphide mineralization, massive or disseminated, will provide IP responses. Coincident resistivity anomalies (conductors) may or may not be present. If the sulphide



TRADER RESOURCE CORP.
Tel Zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June 1986

0 10 20 30
METRES

SUMMARY E-SCAN RESULTS
shown over drilling
results as at June 1986

MISE A LA MASSE SURVEY

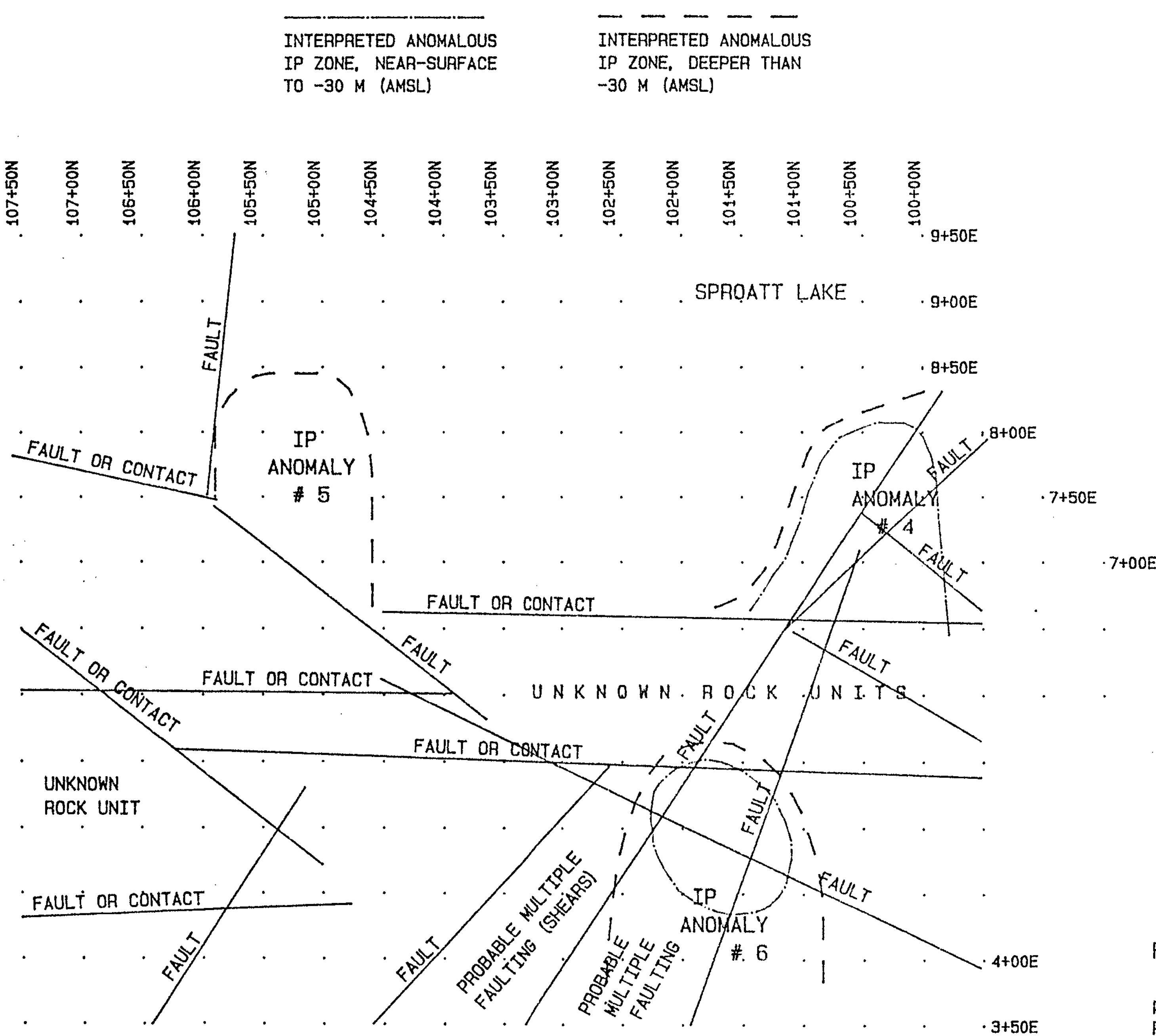
Axis of deep conductor
Contours in millivolts.

INDUCED POLARIZATION
ANOMALY OUTLINES:
A: surface to elev. -30 m.
B: deeper than elev. -30 m.

DRILL-INDICATED ORE ZONES
PROJECTED TO SURFACE:
surface to elev. -30 m.
elev. -50 to -170 metres

Figure # 6

prog: /mise/EPR.2.9.2
data file: /mise/deepLINE
data file: /mise/shalLINE
Premier Geophysics Inc.
Vancouver, B.C.



TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES

INTERPRETED
GEOLOGY

Figure # 5

program: /tln/plot.summ.7
Premier Geophysics Inc.
Vancouver, B.C.

11

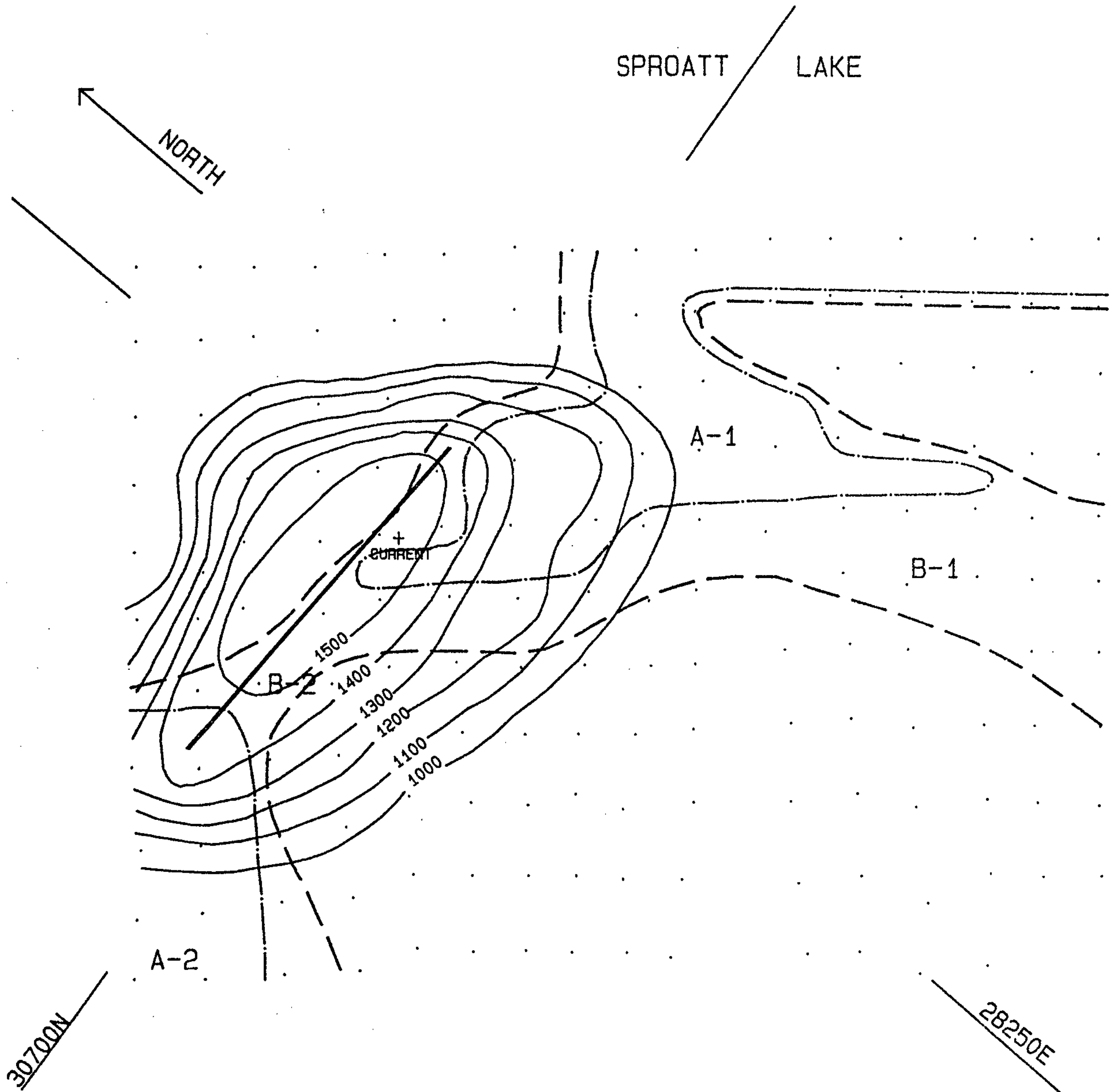
mineralization is discontinuous or disseminated, there may be no low resistivity signature, and even a high resistivity response if sulphide fracture-filling is complete and/or carbonate or silica precipitation is pervasive. The conductor mapped with a mise a la masse technique at Tel suggests a strongly faulted structure at least, and implies substantial lengths of connected conductors (mineralization).

4.1.2 Mise a la masse survey results

See Figures 6 and 7.

Features:

- the deep conductive axis corresponds with IP trend.
- the strength of the conductor implies very conductive fault materials, alteration products, graphite and/or massive metallic sulphides.
- bulges in the contours on the southeast side mark secondary (to this survey) zones of conductivity lying between the plotted bulge and the deep conductor. No depth information is available, except for a lower limitation of about half the depth to the current source, or .5 x 60 = 30 metres (or less).



—·—·—·— INTERPRETED ANOMALOUS IP ZONE, SURFACE TO ELEVATION -30 METRES

— — — — INTERPRETED ANOMALOUS IP ZONE, ELEVATION -30 METRES AND DEEPER

TRADER RESOURCE CORP.
Tel zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June 1986

0 10 20 30
METRES

MISE A LA MASSE SURVEY
potential field contours
(millivolts Vp)

Current injection is at 95.3 metres in DDH 85-012, elevation -47.5 metres, location marked as +.

——— AXIS OF DEEP CONDUCTOR

Plotted over IP anomaly zones.

Figure # 7

prog: /TEL/mise/EPR.2.27
data file: /mise/deepLINE
data file: /mise/shalLINE
Premier Geophysics Inc.
Vancouver, B.C.

4.1.3 General E-SCAN results

Figure A.1 Shallow pole-pole array IP 5-20 metres

Features:

- the Tel ore zone area is outlined (yellow) at 2.6% to 4% IP. An extension of the ore zone anomaly extends southeast for over 30 metres in undrilled ground.
- the lobe of anomalous ground extending southeast thins along the fault-contact between silty thin-bedded marble and grey banded marble before widening in a broader anomalous zone centered about 120 metres SE of the main ore zone.
- the edge of another anomaly (yellow) is evident at the southeast margin of the grid.
- the edge of the chargeable argillite unit is seen along the northeast (top) edge of the grid. It moves in and out showing fault displacement. (This unit has not been evaluated for gold content or for useful E-SCAN signatures relevant to any such gold occurrences.)
- at lower left, another anomalous zone (assuming we are still in marbles here) extends off the grid, positioned accurately on strike with the main Tel ore zone faults. (The few drill penetrations in this area have encountered gold values, some with graphite.)
- a background IP signature for the marbles (both types) appears to be 1.5% to 2.5%.

Figure A.2 Shallow pole-pole array IP 20-40 metres

Features:

- looking deeper, the anomalous zones lying southeast of the Tel zone are filled out, and now display significant volumetric status.
- the connecting, chargeable, probable fault zones between the three anomalies are confirmed, though the evidence is not straightforward to the untrained eye.
- no additions, changes or surprises.

Overlay of Figure 3 on Figure A.2

- cross-faults and the marble fault-contacts combine to permit substantial fracturing (shearing) in and around principal anomalies. If the mineralizing fluids arrived post-faulting, then these permeable zones may have served as conduits and precipitation surfaces.
- the near edge of the argillites should be investigated to determine whether that fault (shown at top of plot) was also mineralized. There is insufficient

E-SCAN coverage at present to resolve the significance of the elevated argillite IP levels opposite the marble IP anomalies.

Figure A.3 Moderate pole-pole array IP 40-60 metres

Features:

- scatter of data as a result of the plotting convention makes this and the next deeper plot dangerously ambiguous to the casual observer. While these depths of data require secondary processing (not shown here) to develop interpretation, three conclusions you might attempt as an observer deserve comment:

1. The southeast (untested) lobe of the main Tel anomaly # 1 **is more responsive** than the known (drilled) area; possibly indicating more intense mineralization.

2. Most of the scattered (yellow) anomalous values west and southwest of Anomaly # 2 (use the overlay to locate) **represent a deep IP anomaly lying to the west**, along the strike of the west cross-fault.

3. Most of the scattered (yellow) anomalous values east and west of Anomaly # 3 (use the overlay to locate) **do not represent a broader anomaly at depth** but are effects of the plotting convention placing responses due to a single electrode at the center of electrode pair. The lack of confirming (yellow) anomalous reponses in the north-west/south-east oriented data (all green) confirm that the yellow values result from arrays oriented with one electrode within the anomaly area, and one outside. (The data at this depth are becoming incomplete this close to the edge of the grid. Expanded coverage may indicate true deeper offset anomalies.)

Figure A.4 Deep pole-pole array IP 60-80 metres

Features:

- the deep IP anomalous zone west of Anomaly 2 continues to be independently defined.
- no equivalent deep definition near Anomalies 1, 3, and 4 is available from visual inspection of this plot. All other apparent deep "anomalous" values are plot-convention scatter.

Figure A.5 Shallow pole-pole array resistivity 5-20 metres

Features:

- outcropping Tel ore area is moderately conductive.
- area over deeper Main Tel ore is resistive.
- Sproatt Lake fault and graphitic argillite area are very conductive.
- pond and lake edge areas are very conductive.
- most of the marbles resistive (2500 - 5000 ohm-metres).
- the area including Anomalies 2 and 3 is uniformly resistive above 2500 ohm-metres,

Figure A.6 Shallow pole-pole array resistivity 20-40 m.

Features:

- pond area conductivities are shown to be very thin, surficial. (More resistive rocks underneath are showing.)
- the distorted (low) values due to the pond area at lower left now form a "halo" around the pond, a result of plot-convention displacement of true effects from the in-pond electrode site to the arbitrary mid-point between electrodes.

Figure A.7 Moderate pole-pole array resistivity 40-60 m.

Features:

- no significant developments.
- the broad area of yellow at left is largely due to plot-convention displacement as in A.7. If there is information about the Tel ore zone as well, it cannot be separated from the known, overwhelming effects of the lake and pond sediments.

Figure A.8 Deep pole-pole array resistivity 60-80 metres

Features:

- as per A.7

GEOPHYSICS

In 1986, Premier Geophysics Inc. of Vancouver conducted two phases of E-SCAN geophysical surveys in the area of the Tel Deposit.

The following describes the E-SCAN system and its application at the Tel property. Reference to figures in the appended report is suggested.

(a) Initial E-SCAN Testing of the Tel Ore Zone

In June 1986, induced polarization (IP) and resistivity surveys over a 150 by 225 meter grid centered on the known Tel ore zones (Report, Figure 2) was carried out. The survey was conducted on a 15 meter grid spacing, and was intended to determine whether the technique could:

1. detect the known ore zones of the Tel Deposit, from near-surface to >150 meters depth; and

2. discriminate between sulphide ore signatures and those of other non-ore rock units, for example the graphitic, pyritic argillite metasediments of the Banks-Barge lineament.

E-SCAN utilizes a new data acquisition technology which provides for saturation coverage of a property with the equivalent of thirty to forty spearate conventional electrical surveys, all conducted simultaneously, and covering every orientation of measurement. One benefit cited is that the explorationist does not need to commit to just one orientation of sampling, as is the conventional case, but can rely on saturation coverage for an objective assessment of all possible ore zone and structural configurations, combinations and orientations. Where overburden covers most of the area, and where structural conditions and ore shapes and orientations can be highly variable (the Tel area), E-SCAN saturation coverage can be expected to identify geologic zones and structures regardless of size or orientation.

It is reported that over 19,000 individual induced polarization measurements and an equal number of resistivity measurements were obtained over the Tel and adjacent areas during the two field programs.

Field data acquisition of the test phase was completed in June 1986 and the data were evaluated and compared to the ore distribution model which H.A. Simons Ltd. engineering consultants had developed from the Tel area drill records (Report, Figure 6. -A 1:500 scale version of this map is Figure 7, located in the map pocket).

The conclusions reached at that time were:

1. The Tel sulphide/gold ore mineralization has a distinct E-SCAN IP signature within a marble rock unit environment.

2. The lateral boundary of the E-SCAN IP anomaly correlates very closely with about most of the drill-indicated ore boundary. Where the E-SCAN boundary extends beyond the limit of drill-indicated ore, it is found that the ore limits are also open in that direction - that is, the area in question is not yet drill-tested.

3. The marble units (silty thin-bedded, and grey banded) have a distinct background IP and resistivity signature which distinguish them from the adjacent graphitic argillites.

4. Mise a la masse resistivity can be useful in projecting ore zone orientation from deep ore intersection in drillholes (Report, Figure 7).

The close correlation of E-SCAN results with the drilled ore zone confirmed the utility of using E-SCAN first to detect the areas of favourable geology (marble), and subsequently to discriminate within the marble those anomalous conditions which may indicate ore of the type occurring in the Tel zone.

The anomalous zone detected over the main Tel zone showed a conspicuous bulge to the southeast (anomaly #1), extending into an area not yet drill tested. In addition, the anomalous zone extended off the grid to the east and to the west, along the strike of the main ore zone cross-faults. Finally, a subtle but unambiguous indication of anomalous conditions existed in the marble southeast of the main ore zone, at the edge of the June grid coverage.

(b) <u>Subsequent E-SCAN Surveys - October, November 1986</u>

Additional E-SCAN services were contracted in September 1986 to extend coverage into the area north and northwest of the initial grid, and to extend coverage in the area of the subtle indication to the southeast.

<u>Adjacent Area Southeast of the Tel Zone</u>

The extension to the southeast revealed two substantial IP anomalies (#2 and #3), with anomaly #3 remaining open to the southeast at the edge of the survey grid. These anomalies are connected to the main Tel ore zone anomaly (#1) by a fault zone which is itself anomalous. Shore suggests that the broad anomaly areas and the connecting fault zone should be systematically drill tested along the full 225m strike, since the entire system actually forms one long, continuous anomaly.

Cross-faults cut the marble near the anomalies, at approximately the orientation of the faults passing through the Tel ore zone. West of the central anomaly, a zone of deep (-50 meters AMSL and deeper) anomalous IP of considerable spatial extent (#2A) lies within the marble regime. This is cited as a drill target as well (Report, Figures 3, 4, A-1, A-2, A-3, A-4).

The anomalies (#1, #2, #2A and #3) provide, at rough estimate, approximately four to six times the surface area (lateral extent) of the presently proven Tel ore zone. Shore reports that the IP signatures over these anomalies are similar to that over the main Tel zone, while the differences in resistivity are nominal and do not diminish the interest in the anomalies.

North Grid Extension

The north grid extension encounters different rock types (as yet unidentified) in bands west of the marble zone. The coverage overlaps the E-SCAN IP anomaly #4 lying west of the main Tel ore zone, and identifies two other anomalies (Report, Figures 5, B-1, B-2).

Anomaly #6 is possibly in marble northwest of the main ore zone, and, while a subtle feature, it is nonetheless of significant areal extent, at 30 by 40 meters. Mapping and exploratory drilling are suggested by Shore, but recommended as last priority of the six anomalous zones.

Anomaly #5 lies in non-marble rock, down-strike from the main ore zone and anomaly #4, in distinctly anisotropic resistivity and IP conditions. Anisotropy is characteristic of certain rock fabrics and bedding orientations, but may also be diagnostic of the type of intense shearing or multiple faulting that would be conducive to circulation of mineralizing fluids. Partly because of the density of faulting identified through the anomaly area, the latter possibility is favoured by Shore, although he observes that a different mineralogy than that of the Tel zone is likely here, probably involving graphite but not excluding gold. Further mapping prior to drilling is recommended by Shore.

CONCLUSIONS AND RECOMMENDATIONS

The Tel ore zone is contained in a complex structural environment. The effects of plunging isoclinal folding and several generations of faulting have required close-spaced diamond drilling to define the mineralized zone. Generally, stratigraphy is consistent throughout the deposit area. The most common host rocks are banded grey marble and silty thin bedded marble. The main structural elements include the regional Tel Antiform, McIntyre Fault and locally the Tel Fault.

The Tel Deposit is mainly composed of massive pyrite-arsenopyrite and sphalerite. Less common ore types are compact jasperoid, sericite-arsenopyrite breccia and late stage, drusy quartz-pyrite assemblages.

The Tel Deposit is open at depth and along strike to the northwest. The possibility of additional ore lenses to the southeast has not been investigated in enough detail.

Contoured plans for gold, silver, arsenic, copper, lead, zinc and iron sulphide show zones of anomalous values for all elements are present between Øm and -1ØØm elevations. Elevated values of iron sulphide and/or zinc are most commonly associated with higher gold grades.

E-SCAN induced polarization and resistivity surveys on and near the Tel Zone have accurately outlined the known Tel ore zone, and mapped six new anomalous areas within 250 meters of the Tel ore zone.

Of these six, one is a direct extension of the main ore zone anomaly, and two others are similar in appearance to the main ore zone anomaly, and occur in similar geologic conditions (marble, near cross-faulting). Drilling of these three anomalies and their common, connecting fault zone has been recommended by Premier geophysicist Greg Shore.

The other three anomalies lie in different geologic conditions, and warrant further mapping and investigation prior to drilling.

The E-SCAN method appears to have provided clearly defined anomalies despite the presence of significant potential sources of survey distortion. It also appears to have provided detailed information on the structural features of the Tel ore zone and adjacent areas. The value of these findings must now be tested by further mapping and drill testing of the anomalies.

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APPENDIX I

E-SCAN REPORT

February 1987

Depth of penetration (Ze):
5-20 metres

Figure # A . 1

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data file: /TLS/TLSD2 f: 1
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Premier Geophysics Inc.
Vancouver, B.C.

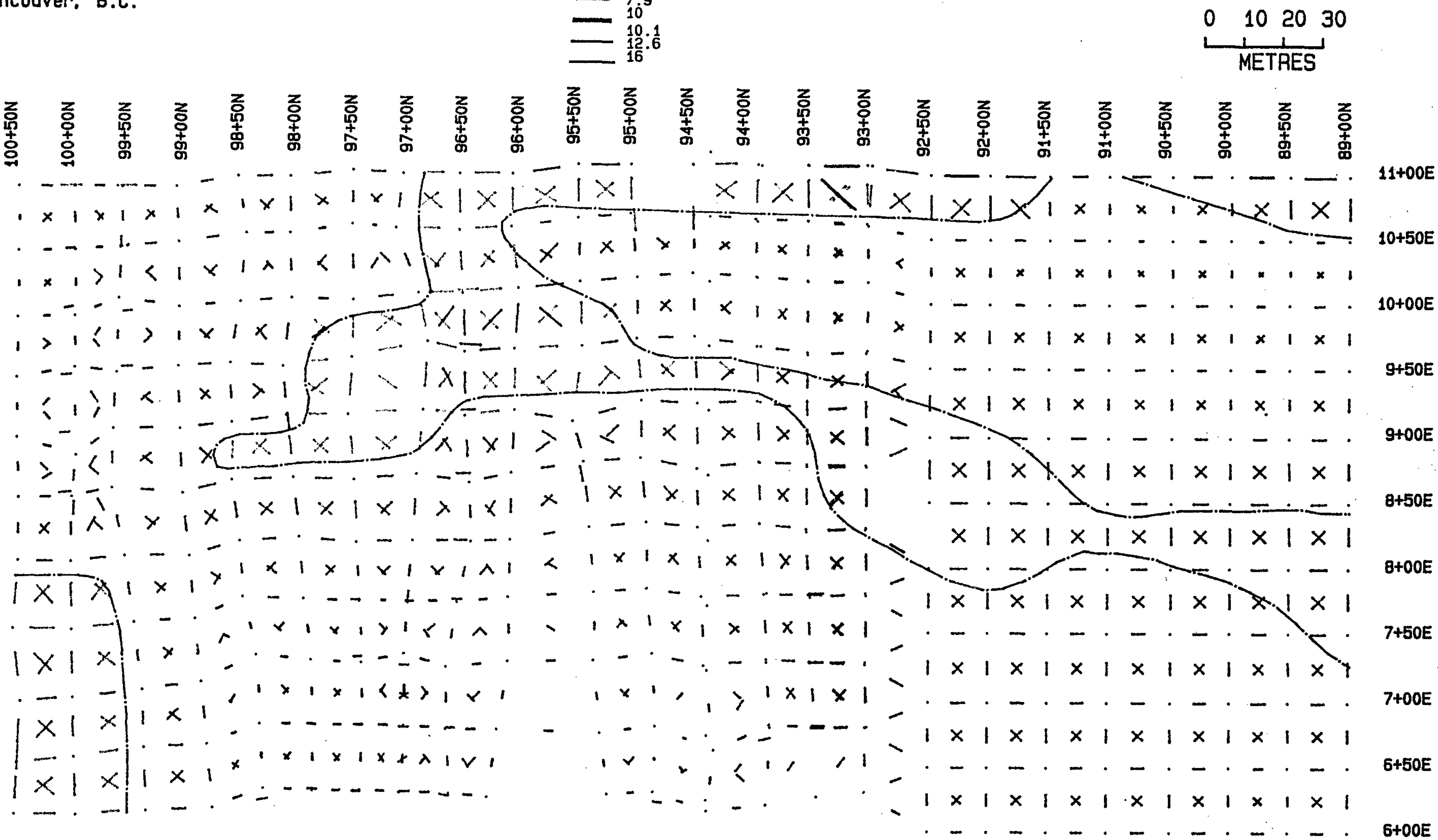
INTERPRETED ANOMALOUS IP ZONE, NEAR-SURFACE TO -30 METRES (AMSL)

0.73
0.8
1
1.1
1.3
1.6
1.7
2
2.5
2.6
3.2
4
4.1
5
6.3
6.4
7.9
10
10.1
12.6
16

INDUCED POLARIZATION
% of Vp

TRADER RESOURCE CORP.
Tel Zone and adjacent area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986



INTERPRETED GEOLOGY

Figure # 3

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Premier Geophysics Inc.
Vancouver, B.C.

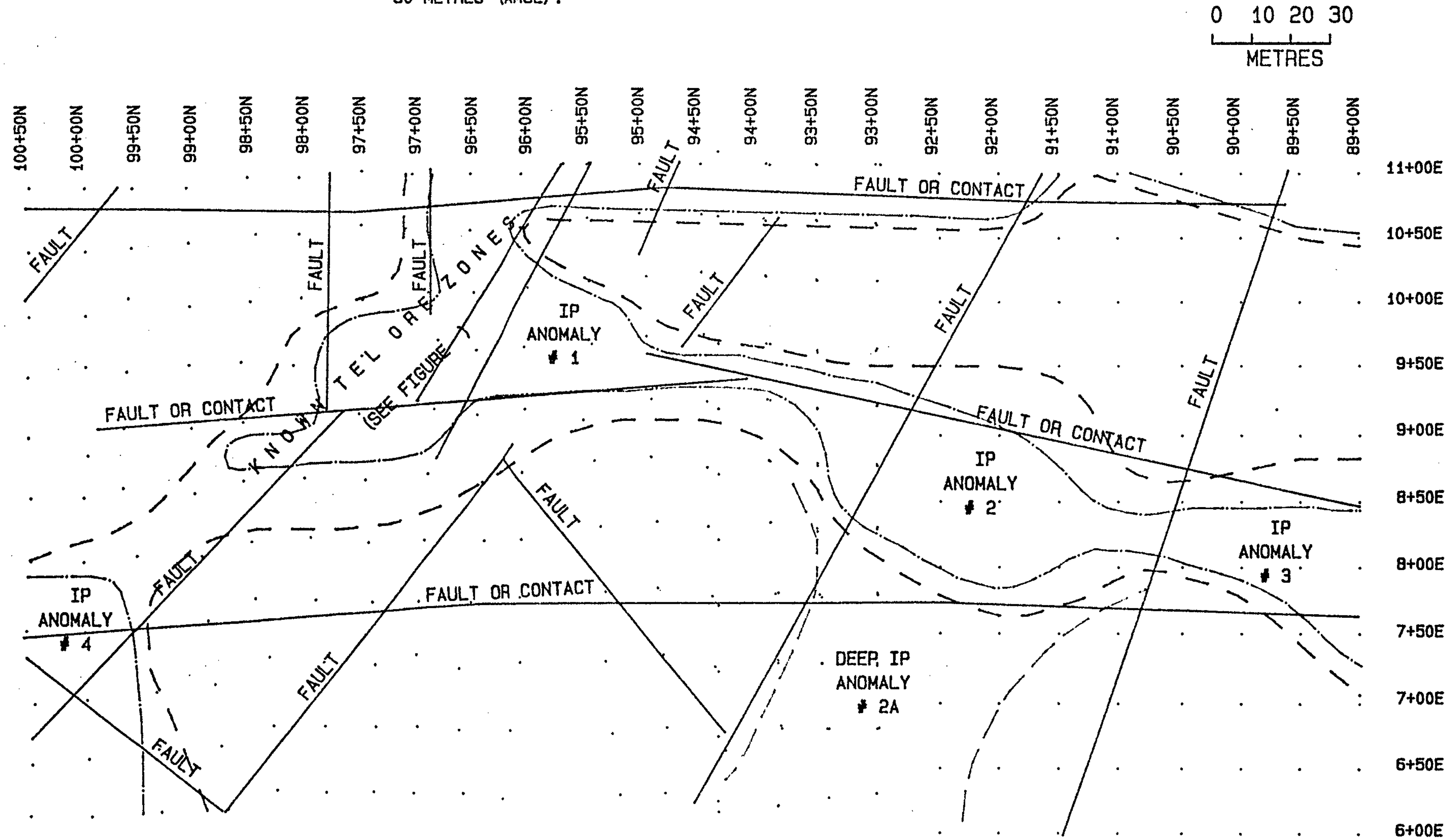
TRADER RESOURCE CORP.
Tel Zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

INTERPRETED ANOMALOUS IP ZONE, NEAR-SURFACE TO -30 METRES (AMSL).

INTERPRETED ANOMALOUS IP ZONE, DEEPER THAN -30 METRES (AMSL).

DEEPER LYING INTERPRETED ANOMALOUS IP ZONE, DEEPER THAN -50 METRES (AMSL).



4.2 DATA SET B: North Grid Extension area.

4.2.1 General E-SCAN results

Figure B.1 Shallow pole-pole array IP 5-20 metres

Features:

- a band of <2.6% IP covers the upper part of the plot. These vales are typical of the marble signatures further southeast.
- IP Anomaly # 4 sits as a distinct higher IP zone within the lower IP probable marble, at the edge of an unknown rock type with higher IP levels as "normal" background.
- IP Anomaly # 5 is a subtly higher IP zone within probable marble.
- a band of (yellow) 2.5% to 4% IP rock separates the probable marble (green, blue) from another more chargeable rock type (orange) extending along the bottom of the plot.

Figure B.2 Shallow pole-pole array IP 20-40 metres

Features:

- this is essentially a deeper view of the same features described in B.1 above.
- Anomaly # 6 emerges more visually as an area of anisotropic, elevated IP within the orange unit. IP values in a westerly orientation are higher than those observed in a northerly orientation, suggesting that the chargeable mineral(s) occurs in a directionally preferential mode, along faults or fractures or within a rock fabric of distinct orientation. The magnitude of the IP response (>6.3%) suggests graphite (with or without sulphides).

Overlay of Figure 5 on Figure B.2

- Anomalies 4 and 6 lie on strike along the Main Tel area cross fault zone.
- Intense faulting or shearing indicated by anisotropic resistivity measurements characterize the area to the left (northwest) of Anomaly # 6.
- Anomaly # 6 is also intersected by a north-trending fault.

Figure B.3 Moderate pole-pole array IP 40-60 metres

Features:

- scatter of data as a result of the plotting convention provide a blurred picture, but principal features can still be seen.

Depth of penetration (Ze):
20-40 metres

Figure # A . 2

program: /disc/EPR.2.22
data file: /TLS/TLSD3 f: 1
DT: 87/02/17 16:48:03
Premier Geophysics Inc.
Vancouver, B.C.

INTERPRETED ANOMALOUS IP ZONE, NEAR-SURFACE TO -30 METRES (AMSL)

INTERPRETED ANOMALOUS IP ZONE, DEEPER THAN -30 METRES (AMSL).

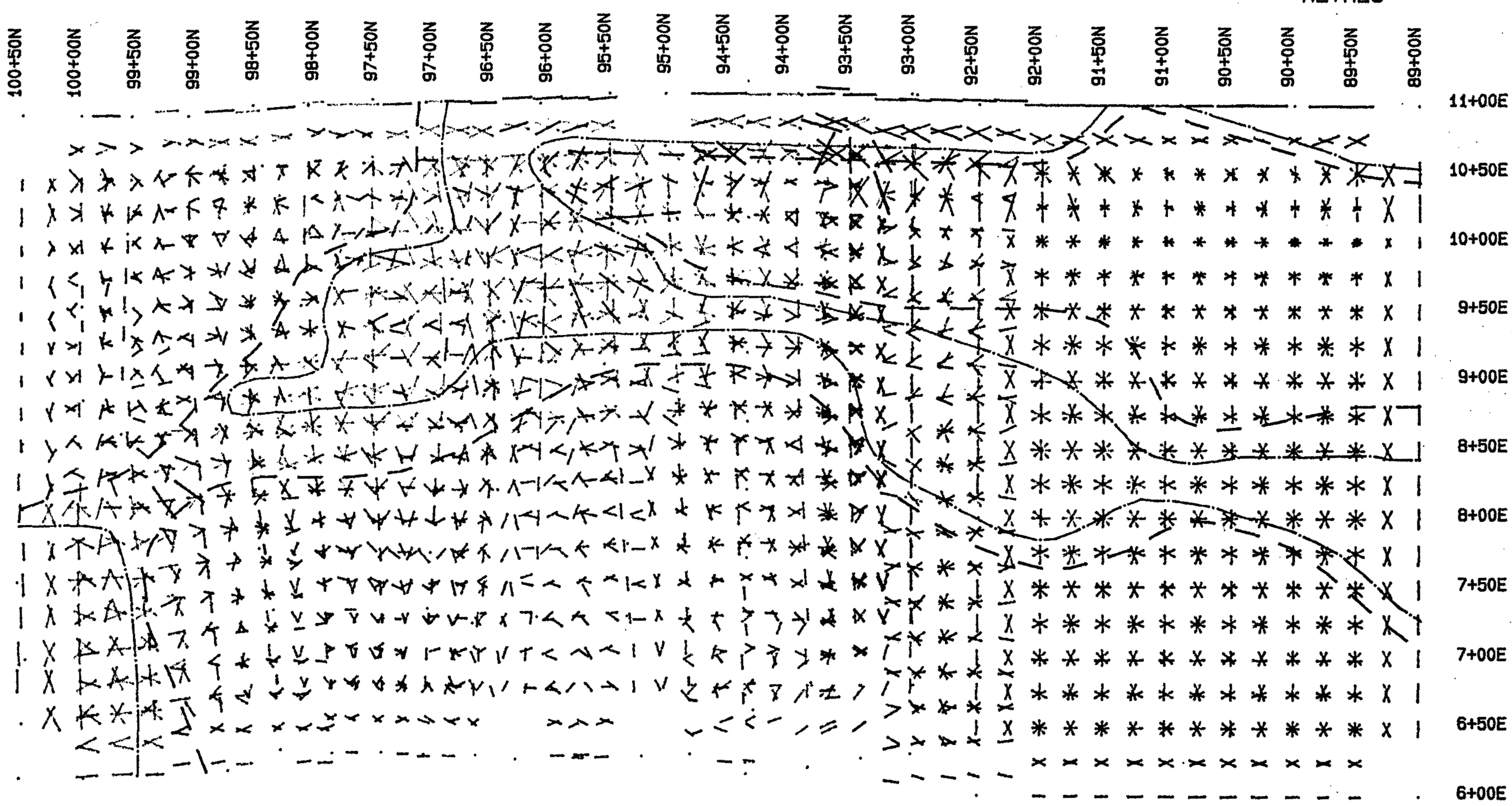
0.73
0.8
1
1.1
1.3
1.6
1.7
2
2.5
2.6
3.2
4
4.1
5
6.3
6.4
7.9
10
10.1
12.6
16

INDUCED POLARIZATION
% of Vp

TRADER RESOURCE CORP.
Tel Zone and adjacent area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

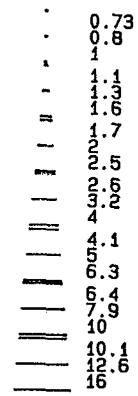
0 10 20 30
METRES



Depth of penetration (Ze):
40-60 metres

Figure # A . 3

program: /disc/EPA.2.20
data file: /TLS/TLSD4 f: 1
DT: 87/02/05 19:35:09
Premier Geophysics Inc.
Vancouver, B.C.

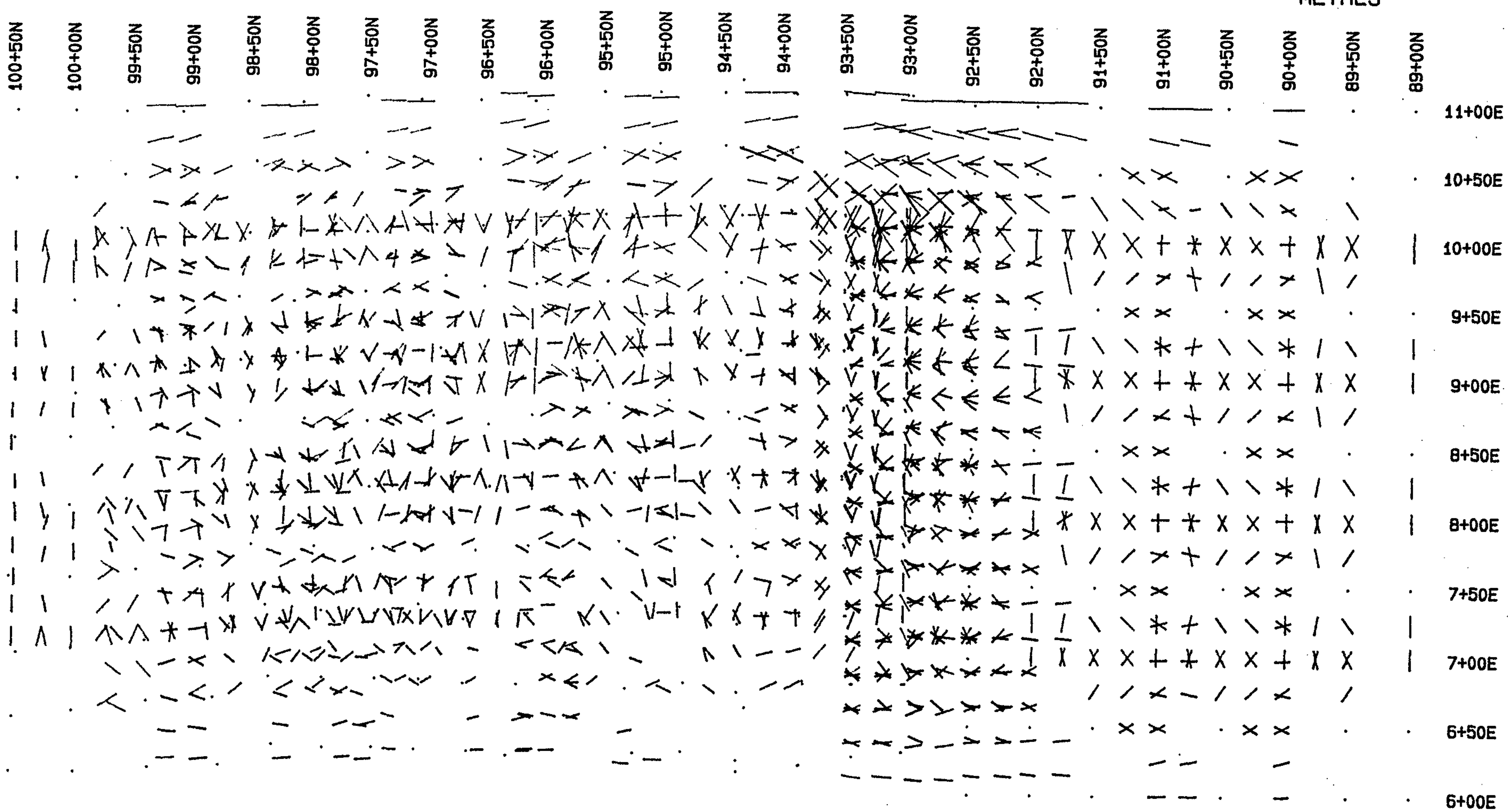


INDUCED POLARIZATION
% of Vp

TRADER RESOURCE CORP.
Tel Zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES



Depth of penetration (Ze):
60-80 metres

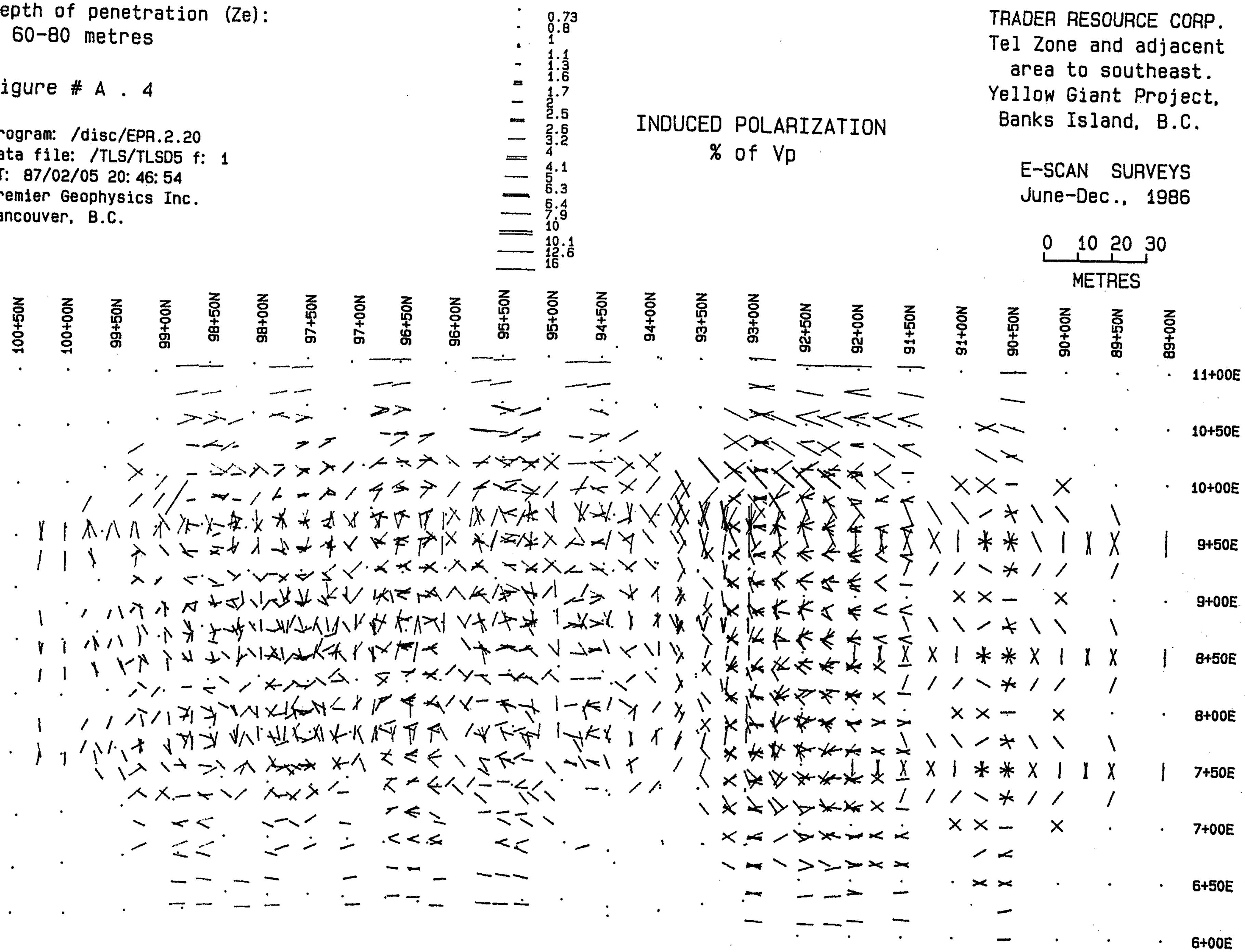
Figure # A . 4

program: /disc/EPR.2.20
data file: /TLS/TLSD5 f: 1
DT: 87/02/05 20: 46: 54
Premier Geophysics Inc.
Vancouver, B.C.

INDUCED POLARIZATION
% of Vp

TRADER RESOURCE CORP.
Tel Zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

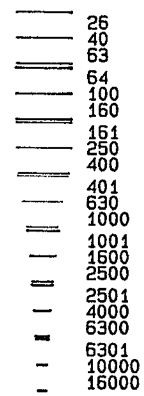
E-SCAN SURVEYS
June-Dec., 1986



Depth of penetration (Ze):
5-20 metres

Figure # A . 5

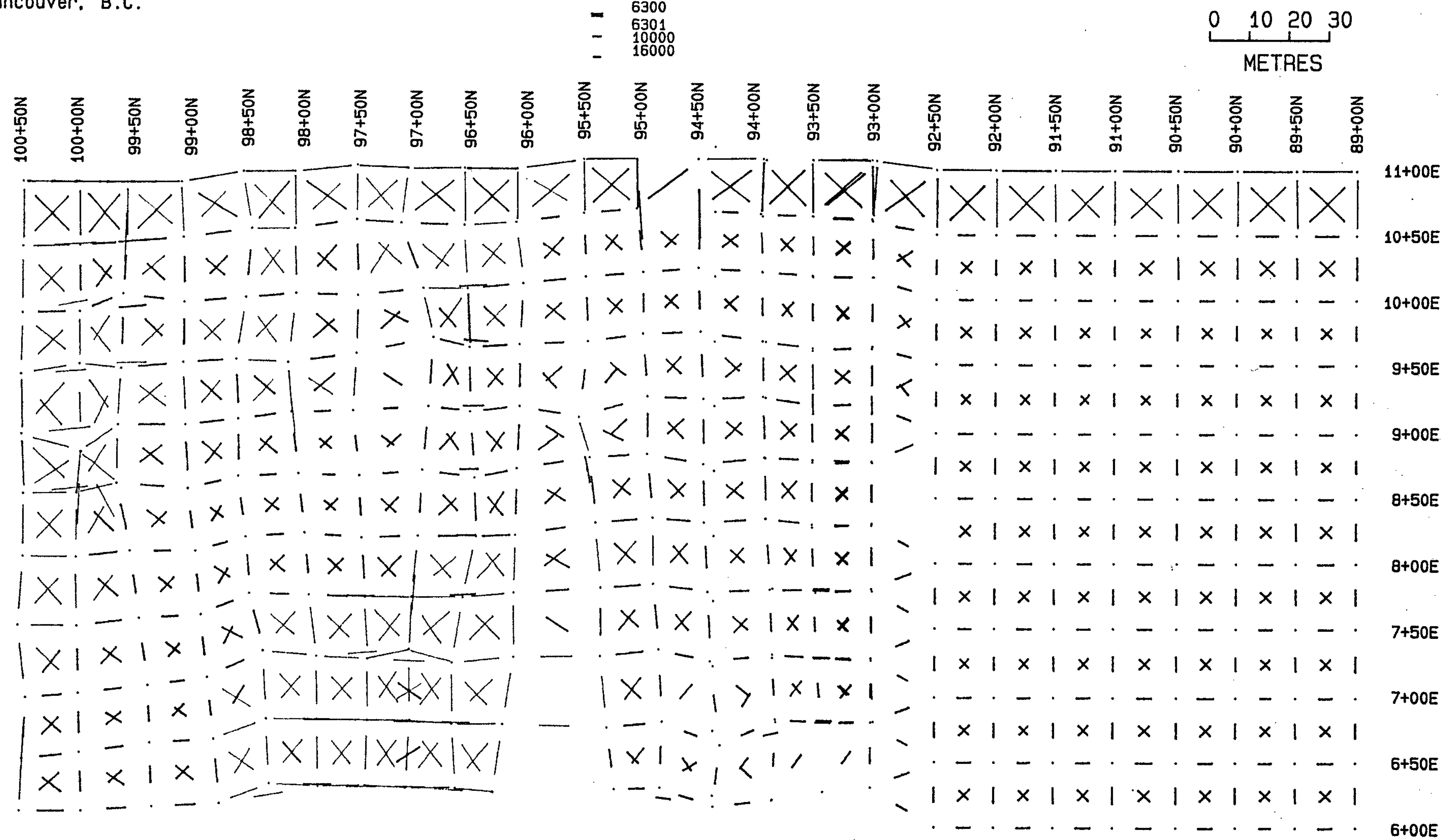
program: /disc/EPR.2.20
data file: /TLS/TLSD2 f: 10
DT: 87/02/05 16: 41: 29
Premier Geophysics Inc.
Vancouver, B.C.



APPARENT RESISTIVITY
ohm-metres

TRADER RESOURCE CORP.
Tel Zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986



Depth of penetration (Ze):
20-40 metres

Figure # A . 6

program: /disc/EPR.2.20
data file: /TLS/TLSD3 f: 10
DT: 87/02/05 18:16:25
Premier Geophysics Inc.
Vancouver, B.C.

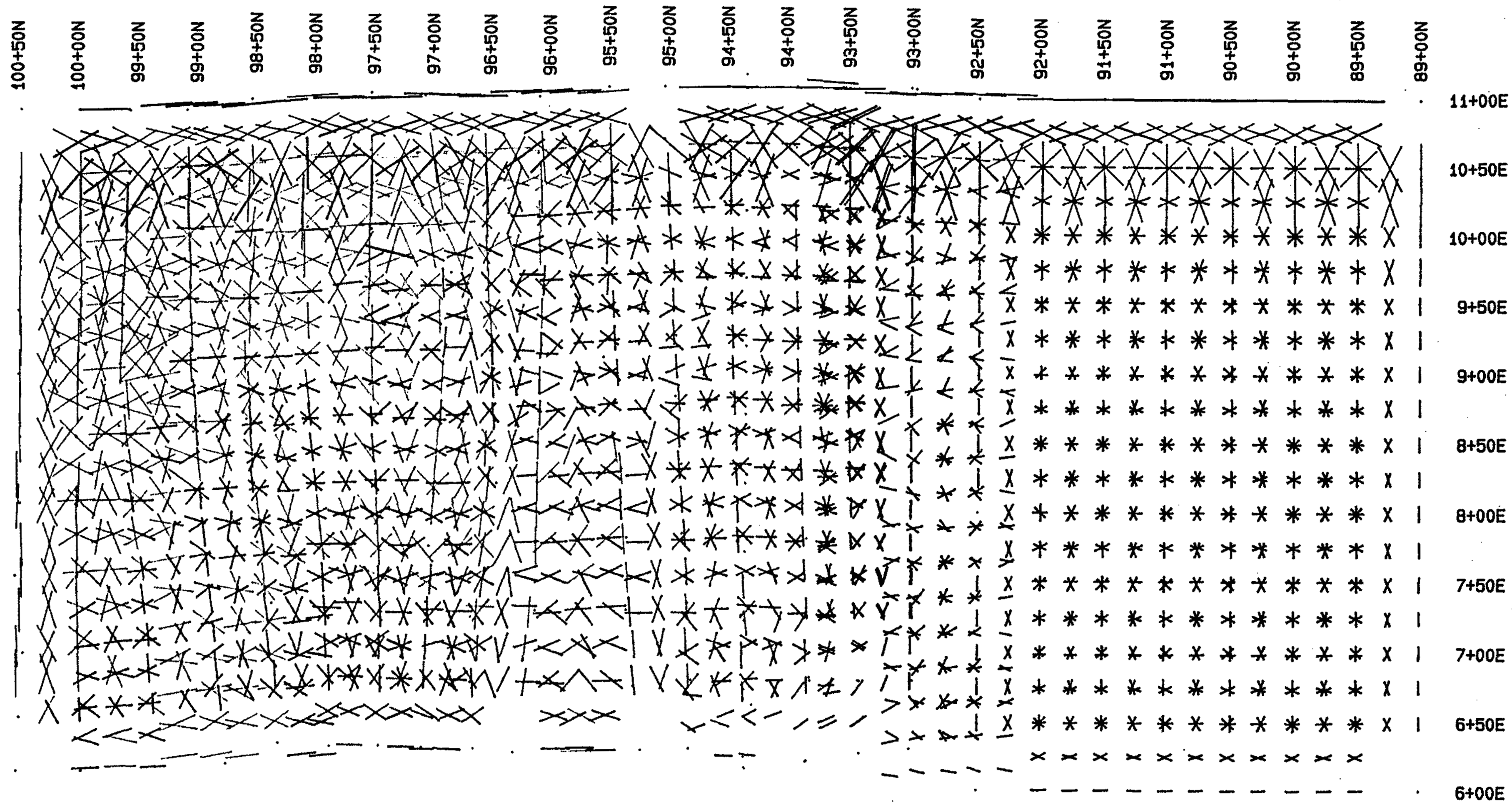
APPARENT RESISTIVITY
ohm-metres

26 40 63 64 100 160 161 250 400 401 630 1000 1001 1600 2500 2501 4000 6300 6301 10000 16000

TRADER RESOURCE CORP.
Tel Zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

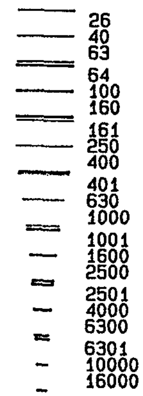
0 10 20 30
METRES



Depth of penetration (Ze):
40-60 metres

Figure # A . 7

program: /disc/EPR.2.20
data file: /TLS/TLSD4 f: 10
DT: 87/02/05 19:52:50
Premier Geophysics Inc.
Vancouver, B.C.

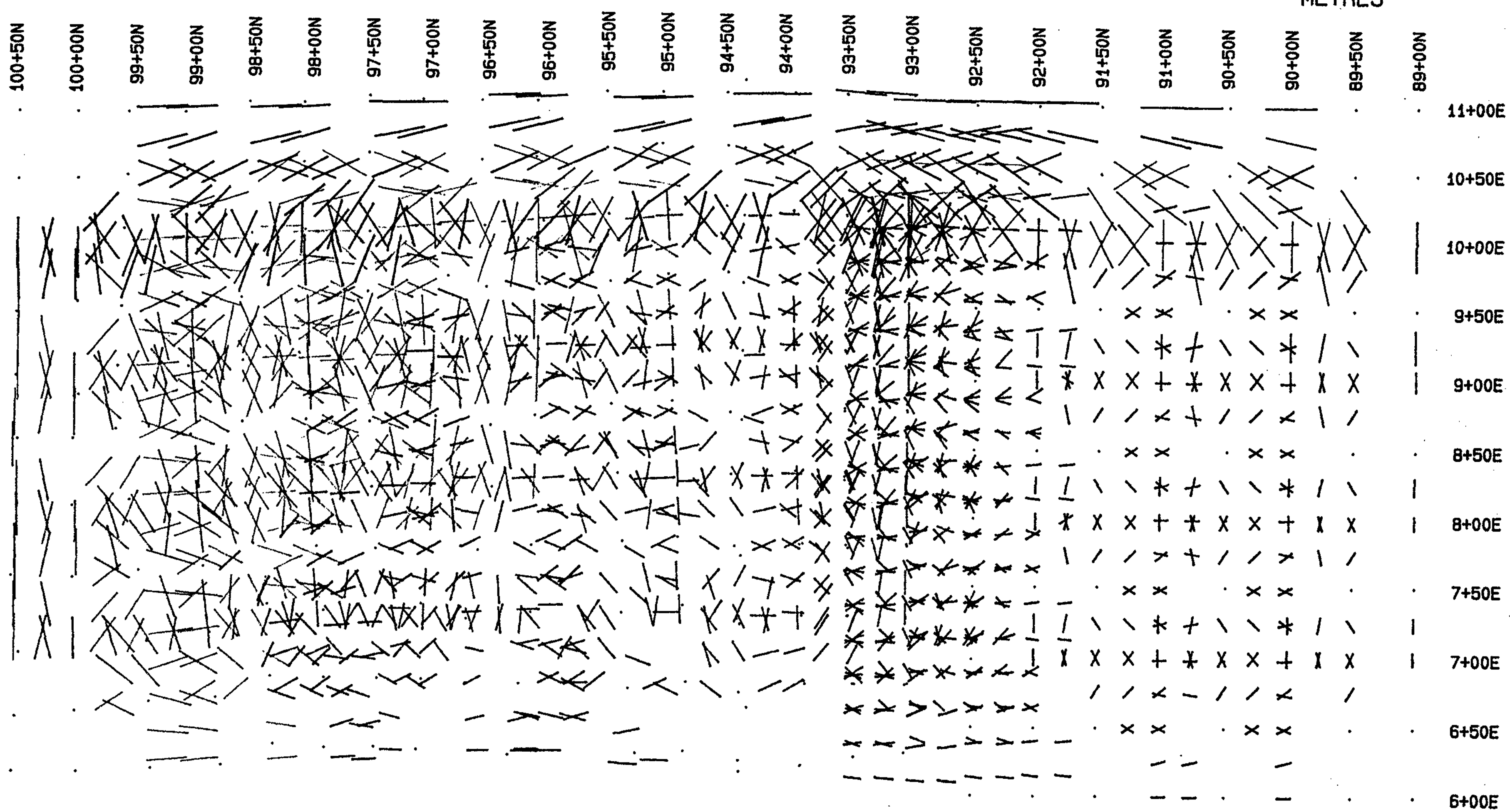


APPARENT RESISTIVITY
ohm-metres

TRADER RESOURCE CORP.
Tel Zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

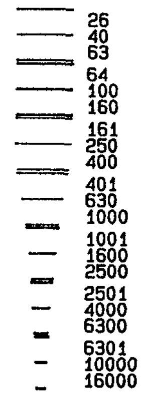
0 10 20 30
METRES



Depth of penetration (Ze):
60-80 metres

Figure # A . 8

program: /disc/EPR.2.20
data file: /TLS/TLSD5 f: 10
DT: 87/02/05 21:39:45
Premier Geophysics Inc.
Vancouver, B.C.

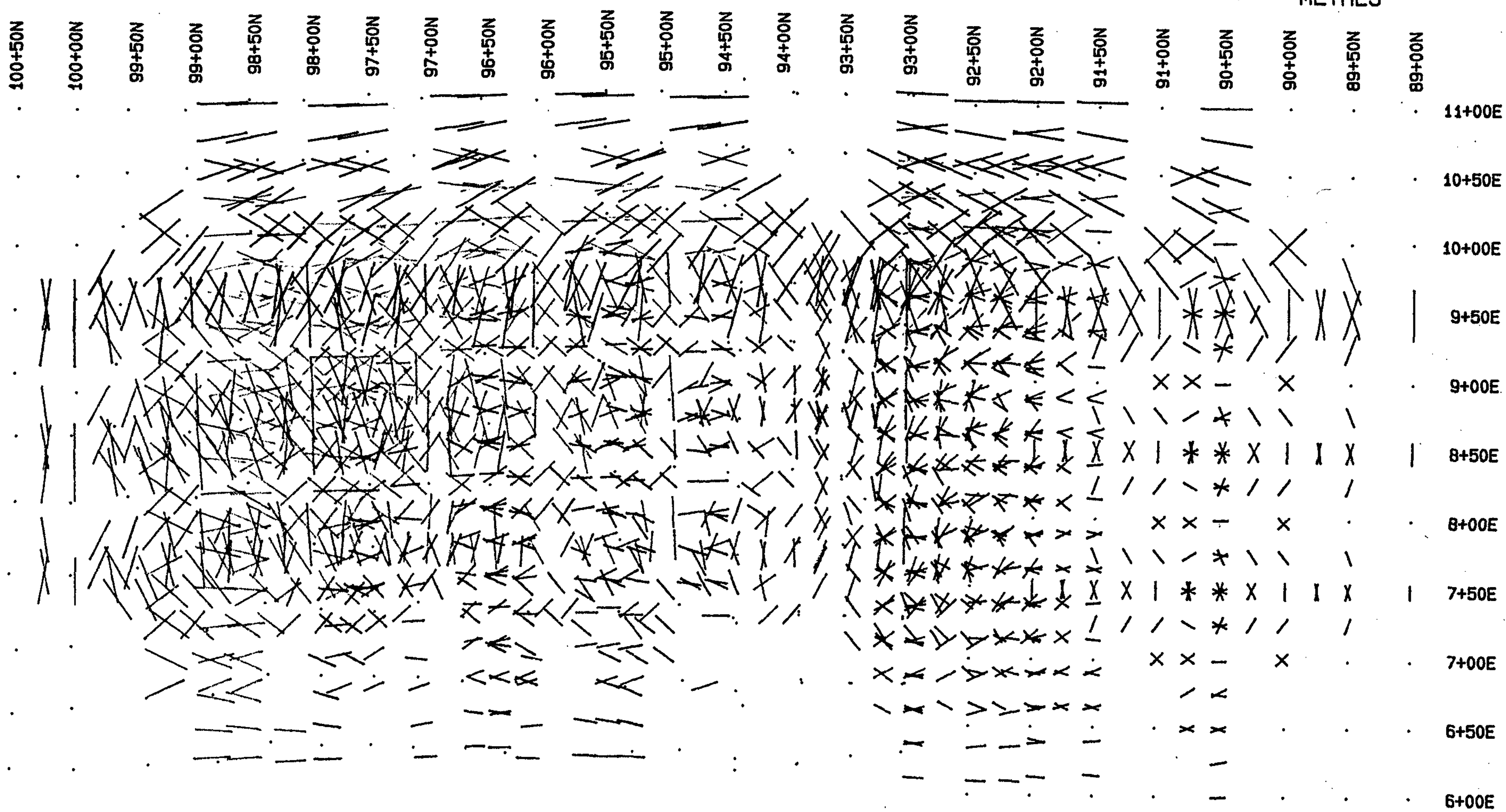


APPARENT RESISTIVITY
ohm-metres

TRADER RESOURCE CORP.
Tel Zone and adjacent
area to southeast.
Yellow Giant Project,
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES

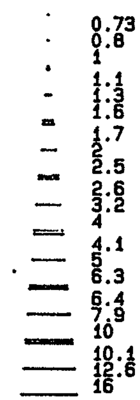


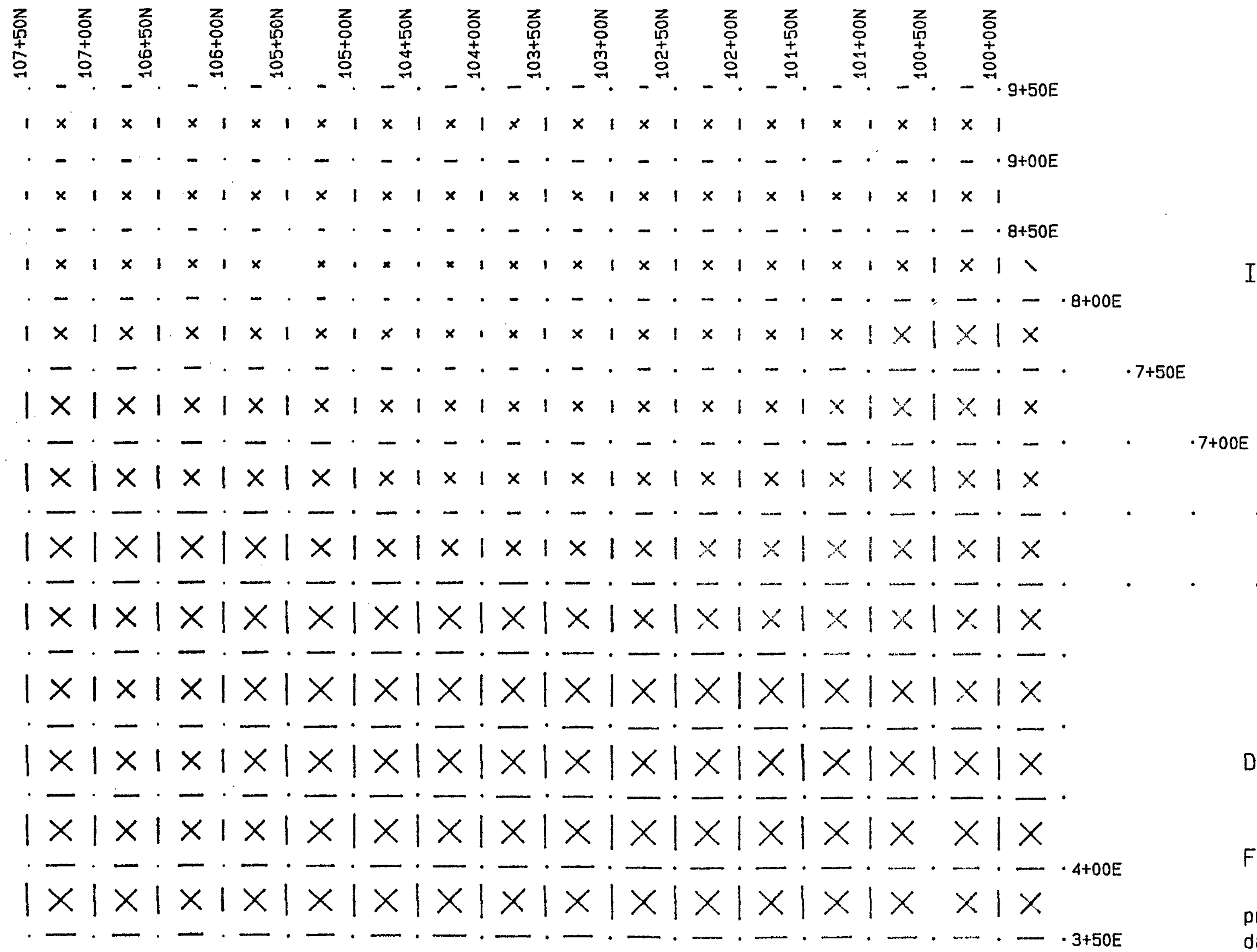
TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES

INDUCED POLARIZATION
% of Vp





Depth of penetration (Ze):
5-20 metres

Figure # B . 1

program: /disc/EPR.2.14
data file: /TLN/TLND2 f: 1
Premier Geophysics Inc.
Vancouver, B.C.

INTERPRETED ANOMALOUS IP ZONE, NEAR-SURFACE TO -30 M (AMSL)

INTERPRETED ANOMALOUS IP ZONE, DEEPER THAN -30 M (AMSL)

TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES

INTERPRETED
GEOLOGY

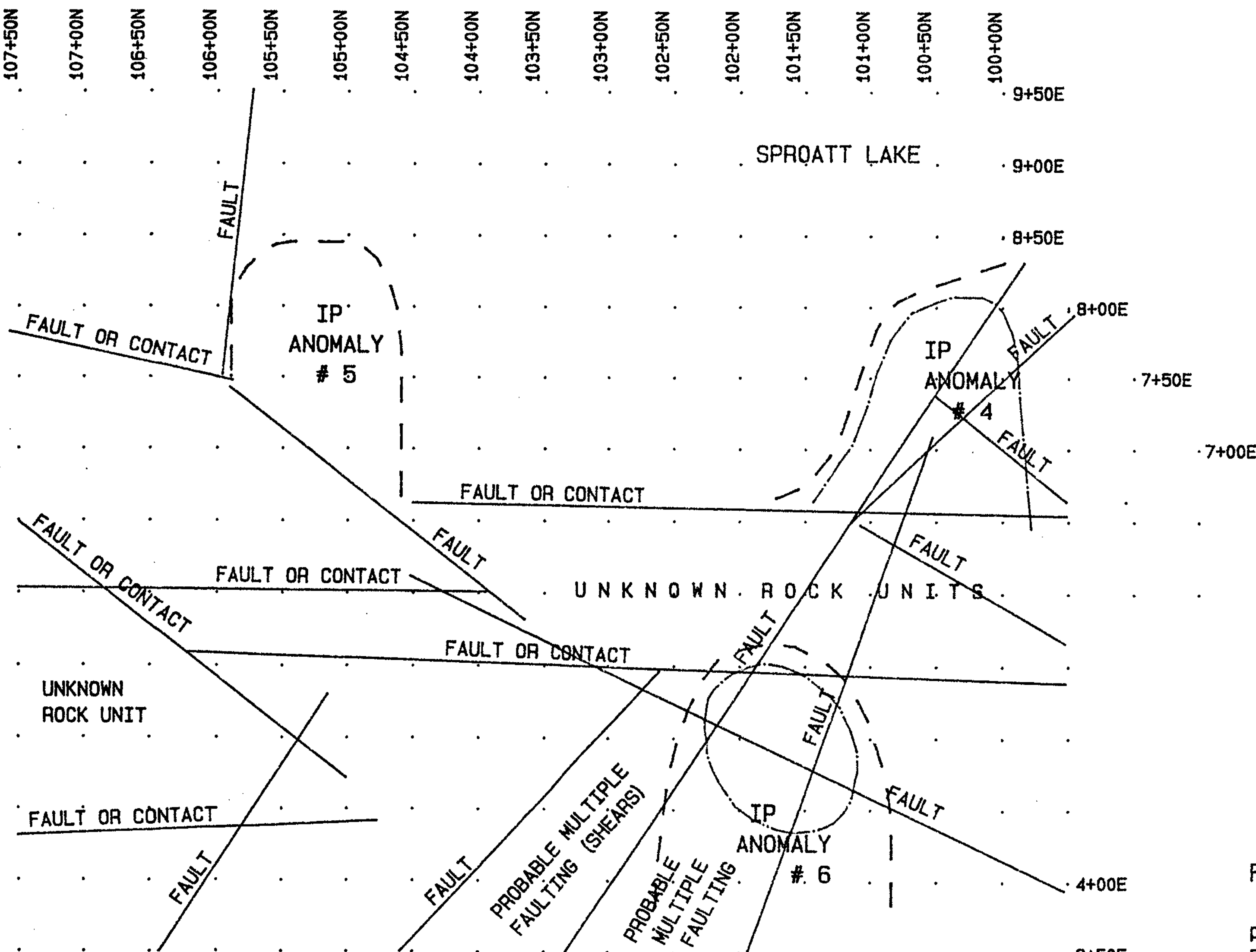
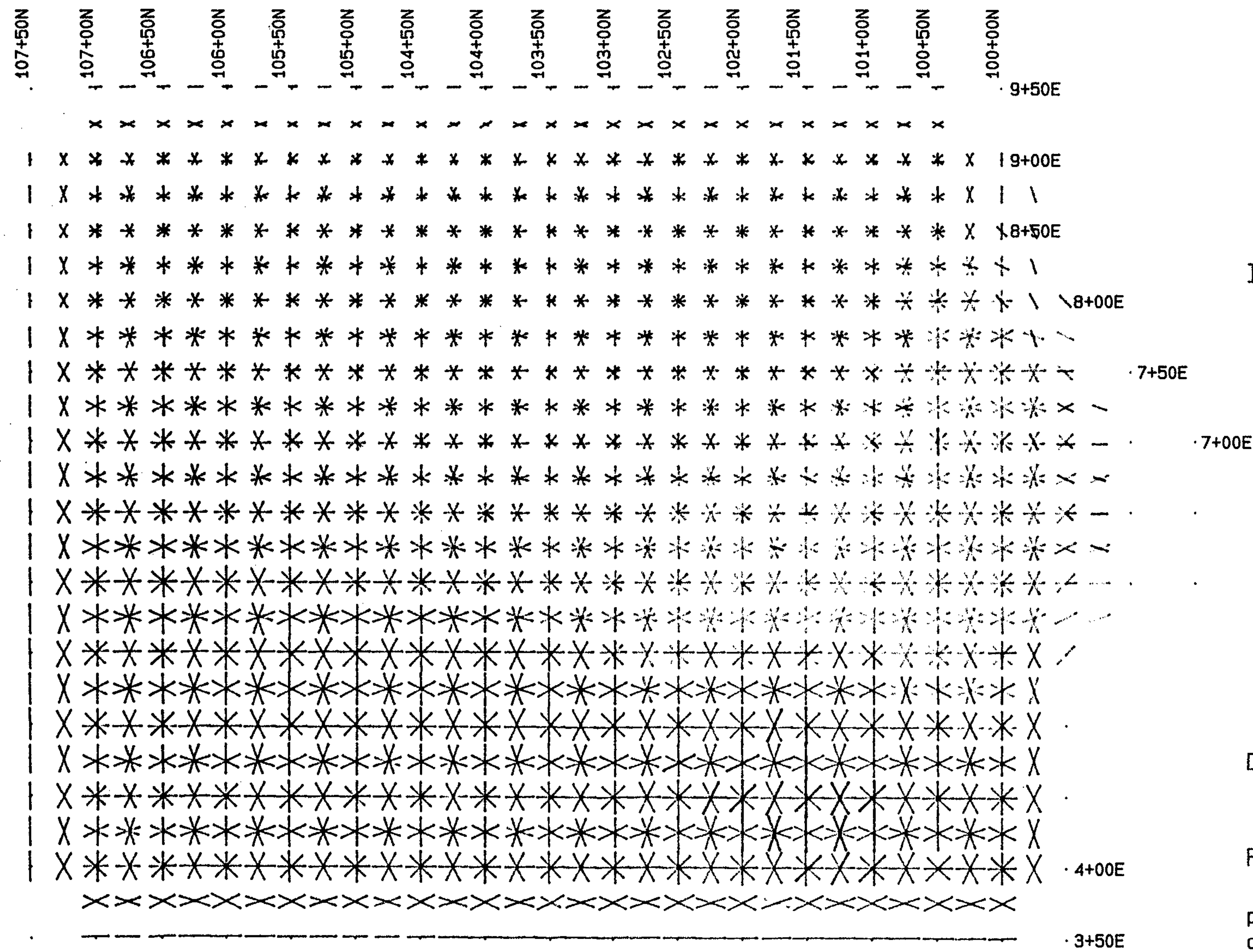


Figure # 5

program: /tln/plot.summ.7
Premier Geophysics Inc.
Vancouver, B.C.



TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES

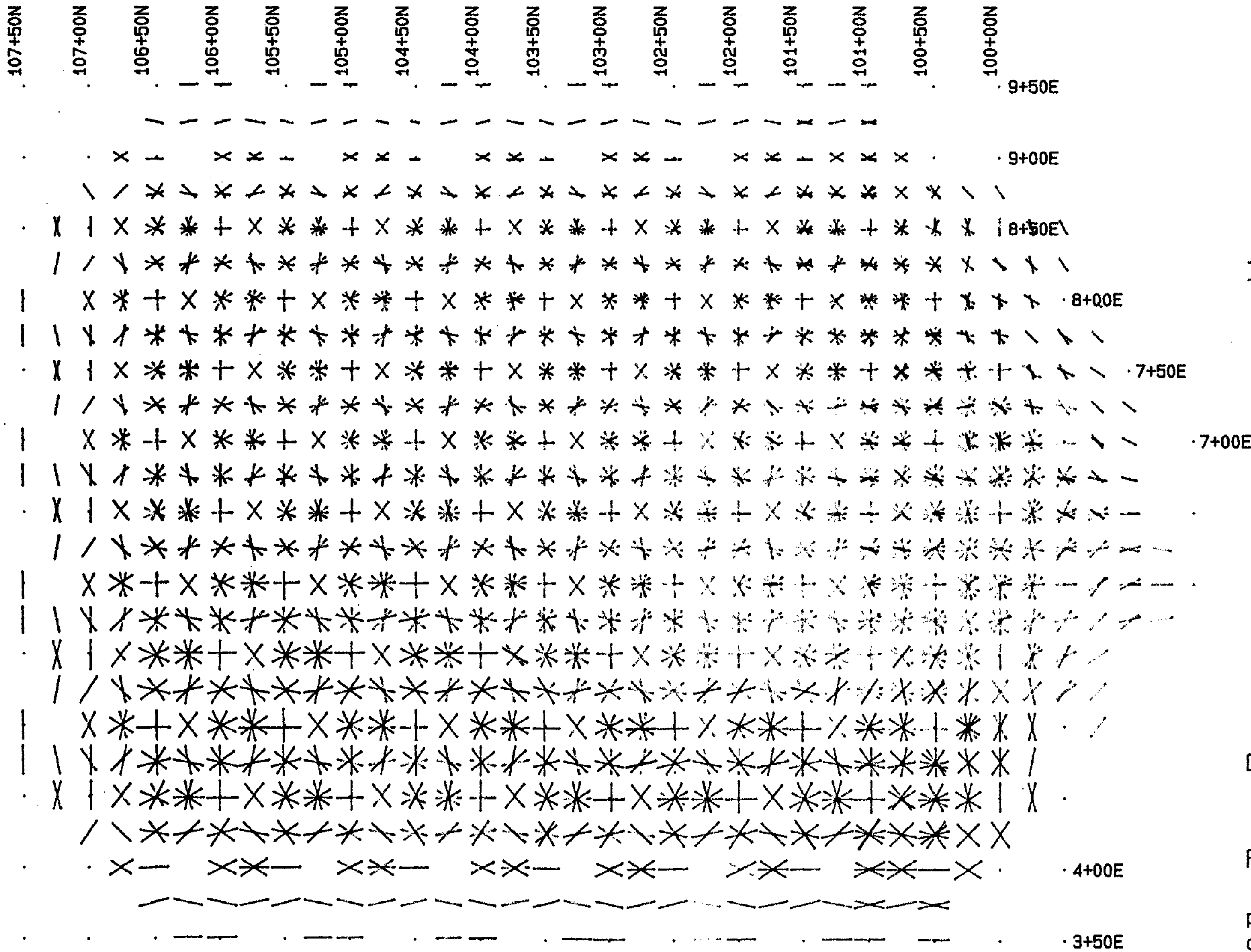
INDUCED POLARIZATION
% of Vp

0.73
0.8
1
1.1
1.3
1.6
1.7
2
2.5
2.6
3.2
4
4.1
5
6.3
6.4
7.9
10
10.1
12.6
16

Depth of penetration (Ze):
20-40 metres

Figure # B . 2

program: /disc/EPR.2.14
data file: /TLN/TLND3 f: 1
Premier Geophysics Inc.
Vancouver, B.C.



TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES

INDUCED POLARIZATION
% of Vp

0.73
0.8
1
1.1
1.3
1.6
1.7
2
2.5
2.6
3.2
4
4.1
5
6.3
6.4
7.9
10
10.1
12.6
16

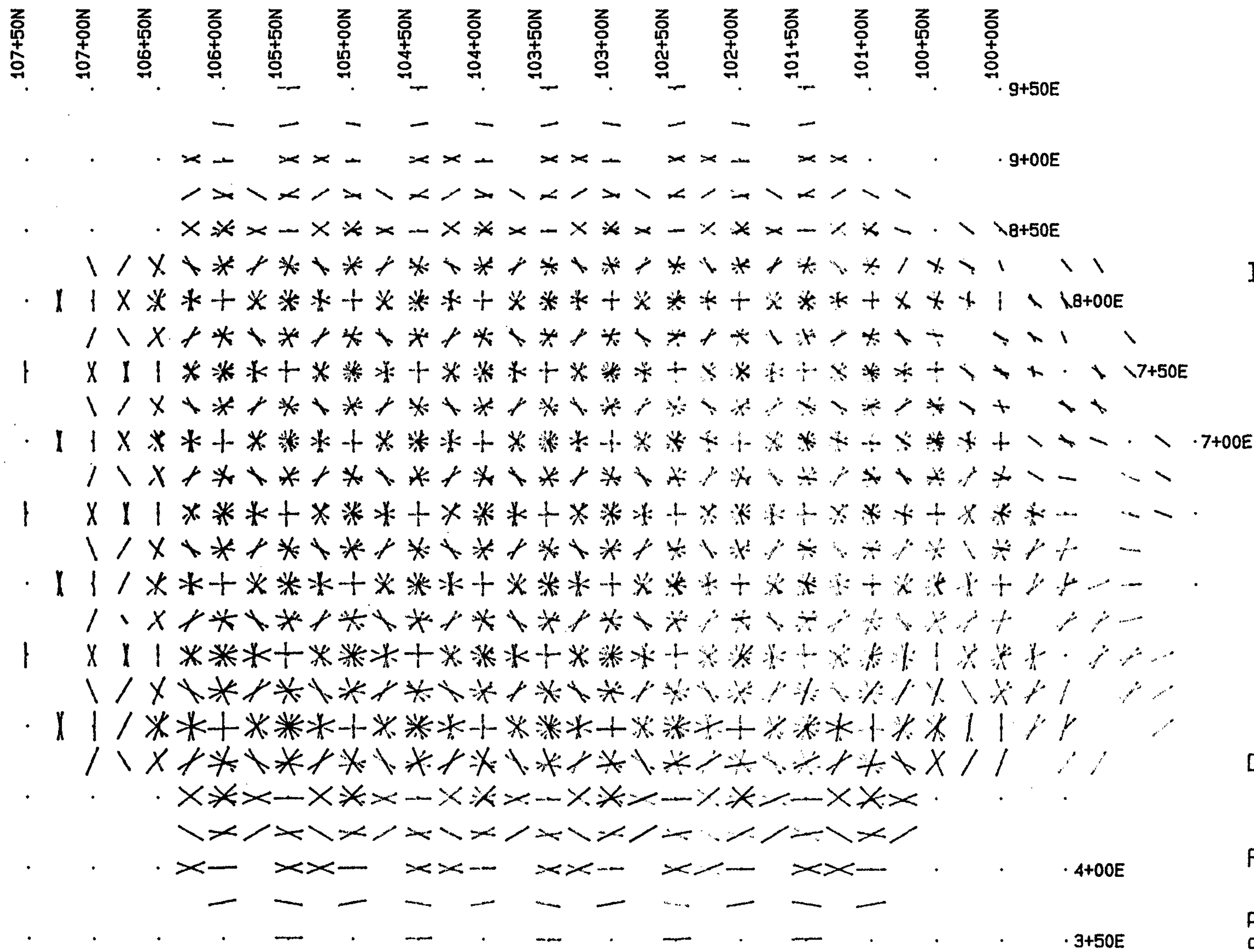
Depth of penetration (Ze):
40-60 metres

Figure # B . 3

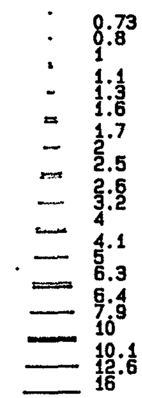
program: /disc/EPR.2.14
data file: /TLN/TLND4 f: 1
Premier Geophysics Inc.
Vancouver, B.C.

TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986



INDUCED POLARIZATION
% of Vp



Depth of penetration (Ze):
60-80 metres

Figure # B . 4

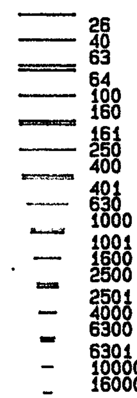
program: /disc/EPR.2.14
data file: /TLN/TLND5 f: 1
Premier Geophysics Inc.
Vancouver, B.C.

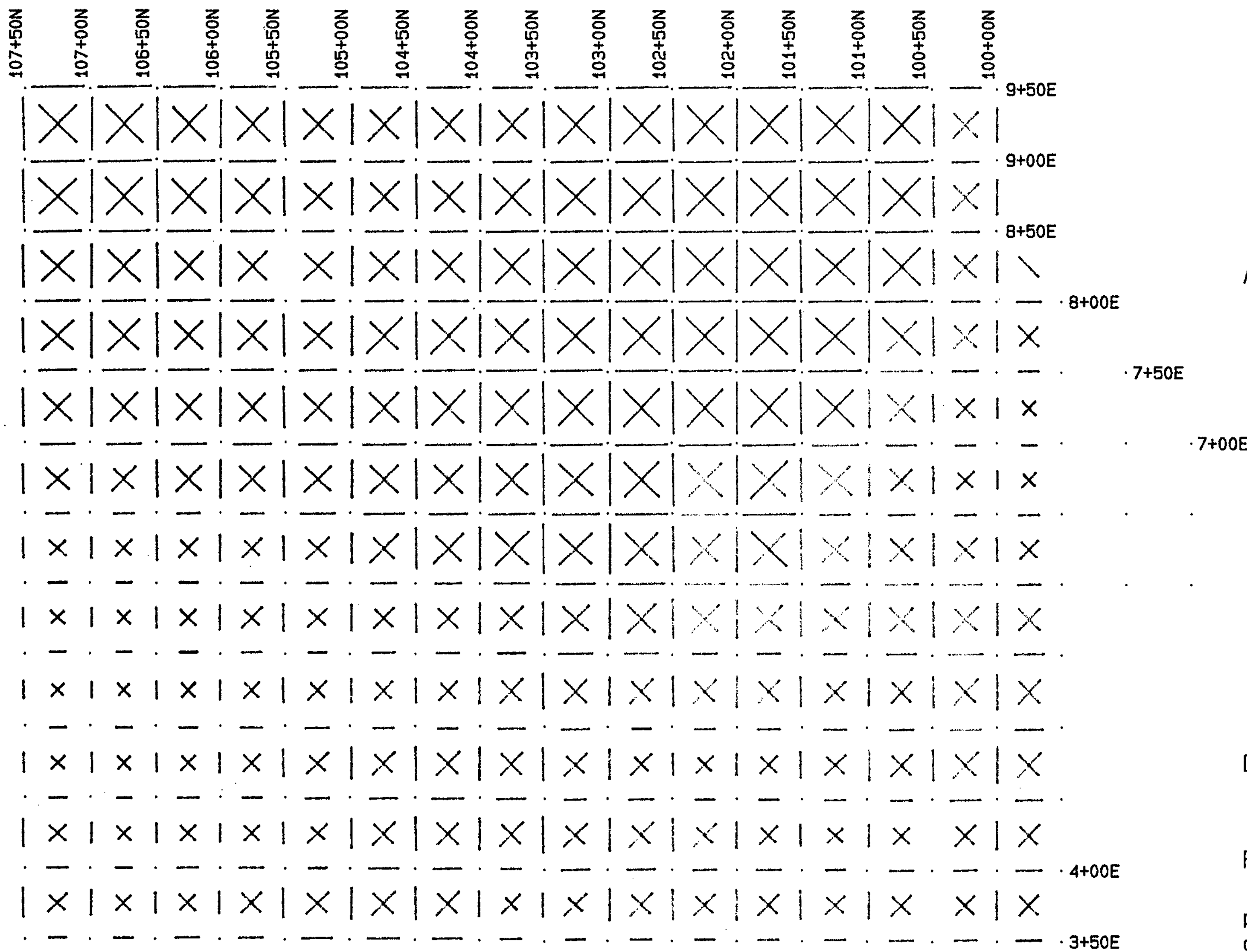
TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES

APPARENT RESISTIVITY
ohm-metres





Depth of penetration (Ze):
5-20 metres

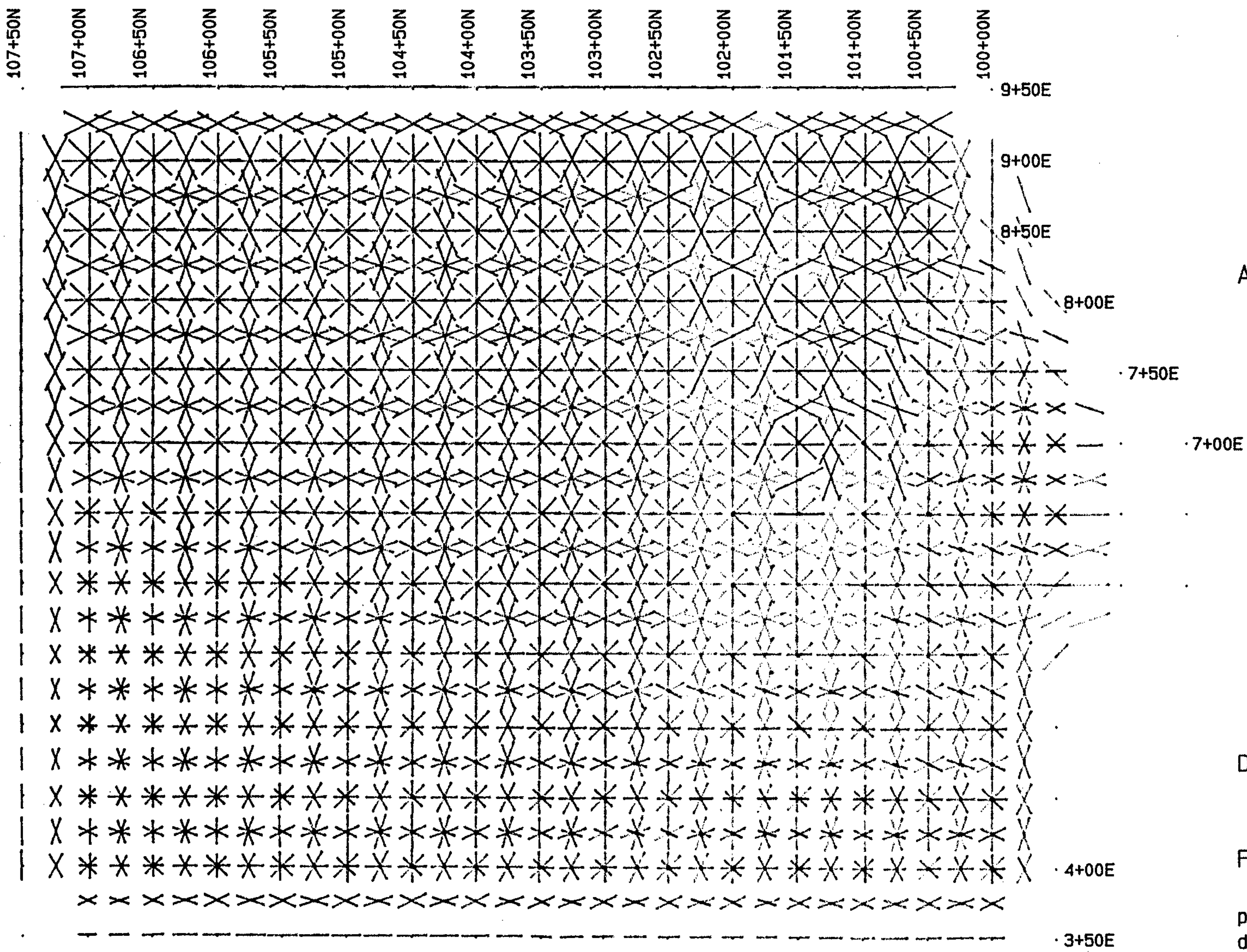
Figure # B . 5

program: /disc/EPR.2.14
data file: /TLN/TLND2 f: 10
Premier Geophysics Inc.
Vancouver, B.C.

TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES



APPARENT RESISTIVITY
ohm-metres

26
40
63
64
100
160
161
250
400
401
630
1000
1001
1600
2500
2501
4000
6300
6301
10000
16000

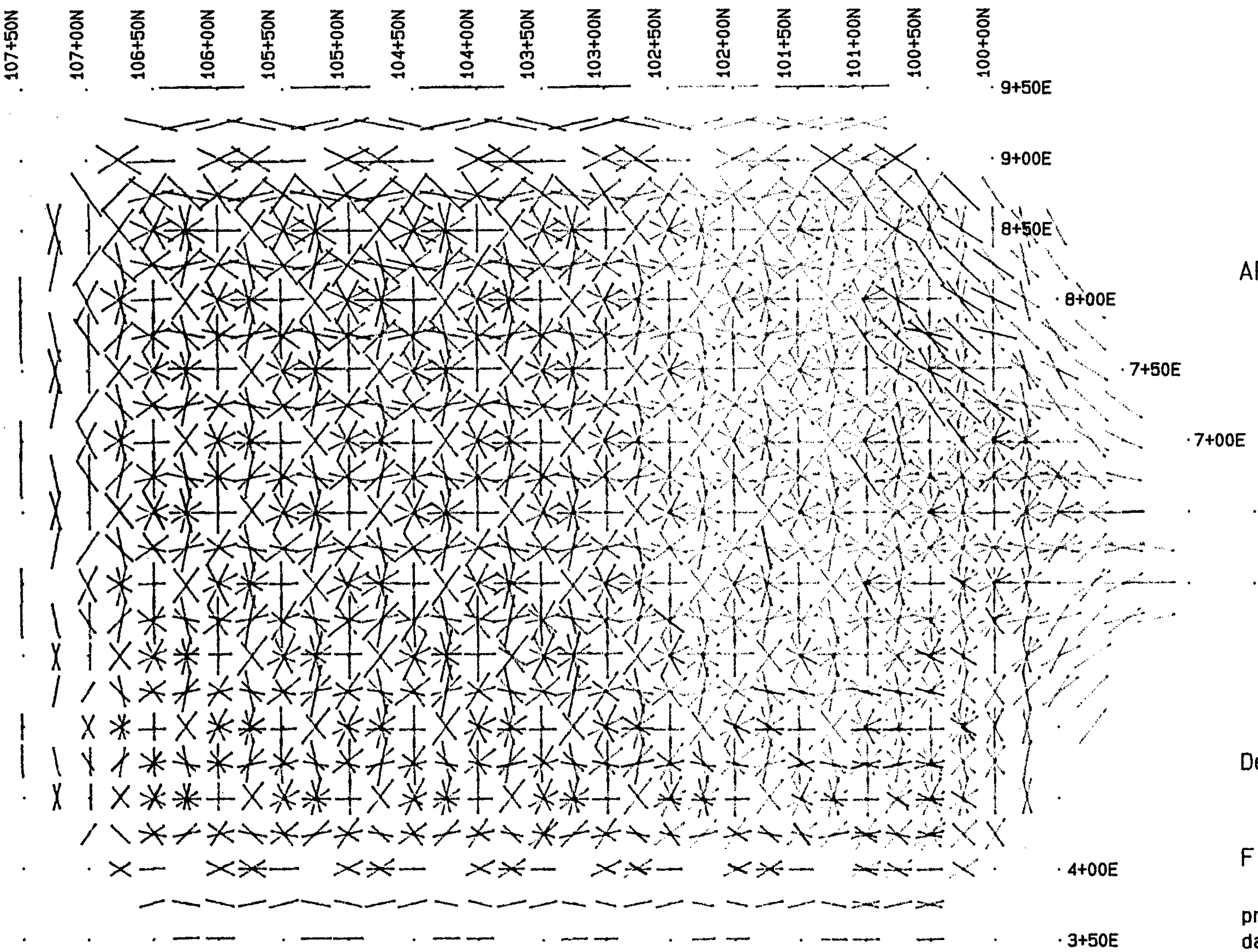
Depth of penetration (Ze):
20-40 metres

Figure # B . 6

program: /disc/EPR.2.14
data file: /TLN/TLND3 f: 10
Premier Geophysics Inc.
Vancouver, B.C.

TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986



0 10 20 30
METRES

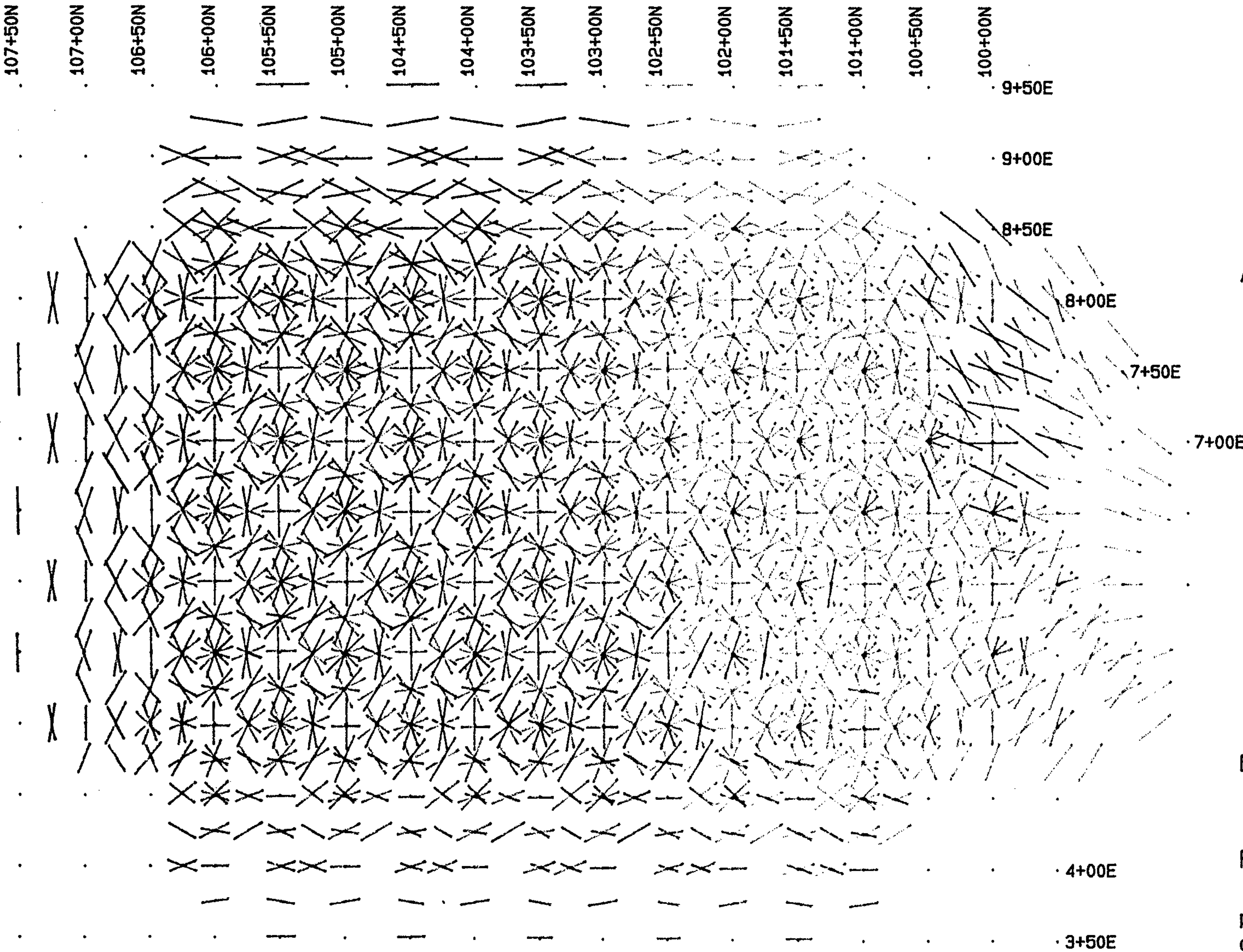
APPARENT RESISTIVITY
ohm-metres

26
40
63
64
100
160
161
250
400
401
630
1000
1001
1600
2500
2501
4000
6300
6301
10000
16000

Depth of penetration (Ze):
40-60 metres

Figure # B . 7

program: /disc/EPR.2.14
data file: /TLN/TLND4 f: 10
Premier Geophysics Inc.
Vancouver, B.C.



TRADER RESOURCE CORP.
North Grid Extension,
Tel Property,
Yellow Giant Project
Banks Island, B.C.

E-SCAN SURVEYS
June-Dec., 1986

0 10 20 30
METRES

APPARENT RESISTIVITY
ohm-metres

26
40
63
64
100
160
161
250
400
401
630
1000
1001
1600
2500
2501
4000
6300
6301
10000
16000

Depth of penetration (Ze):
60-80 metres

Figure # B . 8

program: /disc/EPR.2.14
data file: /TLN/TLND5 f: 10
Premier Geophysics Inc.
Vancouver, B.C.

- no new occurrences or changes of mode at this depth are evident.

Figure B.4 Deep pole-pole array IP 60-80 metres

Features:

- as B.3 above.

Figure B.5 Shallow pole-pole array resistivity 5-20 metres

Features:

- the orange values closely define the parts of the grid that lie in Sproatt Lake. The conductivity (<400 ohm-metres) is due to shallow sediments in the lake. This conductivity will affect (lower) the measured values of all rocks beneath.
- the very chargeable rock unit lying along the lower part of the plot shows moderate resistivity here (green, 1000-2500 ohm-metres), with anisotropic signatures to the left (northwest) of IP anomaly # 6.
- the wedge of unknown rock at left (blue, >2500 ohm-metres) is distinct from all of the other rock units.
- the band of rocks between the probable marbles and the lower unit report a (yellow) signature of 400 to 1000 ohm-metres.

Figure B.6 Shallow pole-pole array resistivity 20-40 m.

Features:

- this plot confirms the characteristics of B.1 at greater depth.
- the shallower parts of the lake sediment area are yielding to higher resistivity values as the underlying rocks are sampled (orange in B.1 become yellow; higher resistivity).

Figure B.7 Moderate pole-pole array resistivity 40-60 m.

Features:

- no significant developments.
- the resolution of boundaries is becoming obscure due to the plotting convention.

Figure B.8 Deep pole-pole array resistivity 60-80 metres

Features:

- as per B.7

5.0 PERSPECTIVE ON FURTHER USE OF E-SCAN IN VARIOUS YELLOW GIANT GEOLOGIC UNITS

The present survey interpretation is effective because there is previous drill-confirmed experience in the marble ore setting to refer to. The range of additional non-marble settings for gold mineralization across the Yellow Giant property is broad, and includes metasedimentary and granitic hosts, and mineralization assemblages featuring significant amounts of graphite. While effective exploration can continue within the marble environment, the extension of effective survey coverage to other rock types depends upon the detection and recognition of a distinct electrical signature for gold mineralization within these rock units. This is a process which can be developed gradually as drill coverage, geologic understanding, and high-density E-SCAN coverage of the subject geologies becomes available for correlation, as was the case in establishing the E-SCAN parameters for the marble environment using Tel drill results.

February 18, 1987

Greg A. Shore
Premier Geophysics Inc.

CERTIFICATE

I, Gregory A. Shore, do hereby certify that:

1. I am a geophysicist with business office at Suite 307, 100 West Pender Street, Vancouver, B.C. V6B 1R8, and President of Premier Geophysics Inc. and of E-SCAN Service Company Inc.

2. I have practiced my profession continuously for the past 15 years, and have been continuously active in geophysical survey planning, execution and interpretation for the past 21 years.

3. I am a member in good standing of the Society of Exploration Geophysicists (SEG), European Association of Exploration Geophysicists (EAEG), and the Society of Mining Engineers (SME of AIME).

4. The information, opinions and recommendations in this report are based on my personal knowledge of the survey work done, and on on-site observations made by me in the course of work on the project.

5. I have no direct or indirect interest in the the Yellow Giant property, in Trader Resource Corp. Ltd., nor do I expect to receive same.

6. This report may be used intact or excerpted for any purpose provided that the sense and meaning of the excerpted material remains unaltered.

Dated at Vancouver, British Columbia, this 18th day of February, 1987.

Gregory A. Shore

Statement of Costs.

E-SCAN Surveys
Tel Property Area
Yellow Giant Project
Banks Island, B.C.

Premier Geophysics' invoiced charges for the work reported herein are as follows:

Phase 1: June 1986:

E-SCAN contract survey services, including all survey supplies, equipment and survey personnel; mobilization and demobilization:	$ 30,000.00

Phase 2: October-November 1986:

E-SCAN contract survey services, including all survey supplies, equipment and survey personnel; mobilization and demobilization:	$ 81,224.63
Data processing and report preparation:	$ 7,234.00
TOTAL CHARGES:	$118,458.63

Greg A. Shore
Premier Geophysics Inc.

APPENDIX II

GRADE COMPOSITE DATA

SIMONS

H.A. Simons Ltd.
Consulting Engineers

425 Carrall Street
Vancouver, B.C. Canada V6B 2J6
604-664-4315
Telex 04-51150

August 20, 1986

Trader Resource Corporation
701 - 744 West Hastings Street
Vancouver, B.C. V6C 1A5

Attention: Mr. J. Shearer
Chief Geologist

Dear Joe:

Subject: Grade Contours - Tel Deposit

This letter is to cover delivery of 35 drawings showing the grade contours of 7 elements in 5 horizontal benches. The data used for the contours is in the accompanying data files.

The contours are plotted for gold, copper, lead, zinc, arsenic, silver and iron sulphide. The values plotted are 10 m composites along the drillhole over the distance noted. For example, in the interval of -50 m<EL<0 m there would be 5 values for each drill-hole which extends through the 50 m section.

The data files have been sorted by drillhole and by easting and northing. The file names containing "04" is for the elements gold, copper, lead and zinc. The file names containing "58" is for the elements arsenic, sulphur (not contoured), silver and iron sulphide.

This completes the work described by Proposed Scope Change No. 2 for P. 3013C dated July 29, 1986. If you have any questions, please do not hesitate to call.

Yours truly,

O. Syberg
Mining & Mineral Processing Division

OS:sb
Encl.

```
***************
*  I N P U T  *
***************

CAL-XYZ data file                             : TNABENA04T.ASY
Number of elements for Bench composites       : 4
Elements ident. Nos.                          : 1 , 2 , 3 , 4 ,
Height of bench                               :   10.00
Elevation of top of uppermost bench           :   50.00
Proportion of bench height                    :    0.50
```

```
*****************
*  O U T P U T  *
*****************
```

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD001	28304.16	30678.08	25.00	0.25364	0.00000	0.00000	0.00000	20.00	7.32

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD002	28302.82	30678.12	25.00	0.75626	0.00000	0.00000	0.00000	20.00	7.62

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD003	28313.00	30684.85	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.04
P64DD003	28305.36	30678.43	15.00	0.35004	0.00000	0.00000	0.00000	10.00	11.42

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD004	28309.82	30682.40	15.00	0.20069	0.00000	0.00000	0.00000	10.00	13.46

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD006	28304.27	30691.06	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.30
P64DD006	28297.61	30685.47	15.00	0.07088	0.00000	0.00000	0.00000	10.00	12.99

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE

P64DD010	28164.86	30709.73	25.00	0.00000	0.00000	0.00000	0.00000	20.00	11.04
P64DD010	28168.28	30719.14	15.00	0.02422	0.00000	0.00000	0.00000	10.00	6.95

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD011	28169.23	30708.72	25.00	0.00000	0.00000	0.00000	0.00000	20.00	11.44
P64DD011	28172.90	30718.80	15.00	0.10346	0.00000	0.00000	0.00000	10.00	5.32

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD014	28261.07	30702.79	25.00	0.00036	0.00000	0.00000	0.00000	20.00	10.20
P64DD014	28261.68	30708.53	15.00	0.17395	0.00000	0.00000	0.00000	10.00	5.19

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD025	28278.62	30714.20	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.98
P64DD025	28277.58	30702.32	15.00	0.01055	0.00000	0.00000	0.00000	10.00	15.56

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD026	28299.74	30697.22	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.21
P64DD026	28293.31	30689.56	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
P64DD026	28286.88	30681.90	5.00	0.01895	0.00000	0.00000	0.00000	0.00	6.39

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD001	28063.57	30730.10	25.00	0.00000	0.00000	0.00000	0.00000	20.00	14.14
B75DD001	28068.57	30738.76	15.00	0.00387	0.00000	0.00000	0.00000	10.00	14.14

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD002	28064.95	30728.90	25.00	0.00000	0.00000	0.00000	0.00000	20.00	14.14
B75DD002	28072.61	30735.33	15.00	0.00001	0.00000	0.00000	0.00000	10.00	14.14

B75DD002	28080.27	30741.76	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD003	28169.38	30704.72	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.92
B75DD003	28167.64	30714.57	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
B75DD003	28165.90	30724.42	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14
B75DD003	28164.16	30734.27	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14
B75DD003	28162.43	30744.12	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.14
B75DD003	28160.69	30753.96	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.14
B75DD003	28158.96	30763.81	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.14

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD004	28170.88	30703.17	25.00	0.00000	0.00000	0.00000	0.00000	20.00	9.22
B75DD004	28173.32	30709.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.92
B75DD004	28175.75	30715.22	5.00	0.00179	0.00000	0.00000	0.00000	0.00	11.92
B75DD004	28178.18	30721.24	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	6.26

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD005	28291.31	30669.04	25.00	0.00000	0.00000	0.00000	0.00000	20.00	8.88
B75DD005	28298.38	30676.11	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
B75DD005	28305.45	30683.18	5.00	0.12252	0.00000	0.00000	0.00000	0.00	14.14
B75DD005	28312.52	30690.25	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14
B75DD005	28319.59	30697.32	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.14
B75DD005	28326.66	30704.39	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.75

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD006	28289.75	30669.05	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.56
B75DD006	28292.20	30674.80	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.79
B75DD006	28294.63	30680.55	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.79
B75DD006	28297.08	30686.31	-5.00	1.61223	0.00000	0.00000	0.00000	-10.00	11.80
B75DD006	28299.53	30692.06	-15.00	0.36734	0.00000	0.00000	0.00000	-20.00	5.53

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE

B75DD007	28311.14	30702.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.38
B75DD007	28306.92	30698.78	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.38
B75DD007	28302.70	30695.37	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.38
B75DD007	28298.48	30691.95	-15.00	0.01307	0.00000	0.00000	0.00000	-20.00	11.38
B75DD007	28294.26	30688.53	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.38

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD008	28309.79	30703.85	15.00	0.00008	0.00000	0.00000	0.00000	10.00	11.92
B75DD008	28303.33	30703.18	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.93
B75DD008	28296.87	30702.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.93
B75DD008	28290.41	30701.81	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.93
B75DD008	28283.95	30701.13	-25.00	0.02886	0.00000	0.00000	0.00000	-30.00	11.92

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD009	28308.73	30700.22	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.90
B75DD009	28300.92	30694.54	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.90
B75DD009	28293.11	30688.87	-5.00	0.03776	0.00000	0.00000	0.00000	-10.00	13.90
B75DD009	28285.29	30683.19	-15.00	0.00015	0.00000	0.00000	0.00000	-20.00	13.90
B75DD009	28277.48	30677.51	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.90
B75DD009	28269.67	30671.84	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	5.00

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD011	28319.20	30687.63	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.64
B75DD011	28316.67	30685.02	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.64
B75DD011	28314.14	30682.40	-5.00	0.56915	0.00000	0.00000	0.00000	-10.00	10.64
B75DD011	28311.62	30679.78	-15.00	0.00291	0.00000	0.00000	0.00000	-20.00	10.64
B75DD011	28309.09	30677.16	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.64

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD013	28332.89	30680.57	15.00	0.00630	0.00000	0.00000	0.00000	10.00	10.04
B75DD013	28332.22	30680.01	5.00	0.00152	0.00000	0.00000	0.00000	0.00	10.04
B75DD013	28331.54	30679.44	-5.00	0.57803	0.00000	0.00000	0.00000	-10.00	10.04
B75DD013	28330.88	30678.88	-15.00	0.37833	0.00000	0.00000	0.00000	-20.00	10.04
B75DD013	28330.21	30678.32	-25.00	0.00273	0.00000	0.00000	0.00000	-30.00	10.04
B75DD013	28329.53	30677.76	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.04
B75DD013	28328.86	30677.19	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.04
B75DD013	28328.19	30676.63	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	5.52

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD014	28331.35	30679.21	15.00	0.00057	0.00000	0.00000	0.00000	10.00	10.64
B75DD014	28328.56	30676.87	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.64
B75DD014	28325.77	30674.53	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.64
B75DD014	28322.99	30672.19	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.64

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD015	28316.52	30645.35	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.39
B75DD015	28323.83	30652.17	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
B75DD015	28331.15	30658.99	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14
B75DD015	28338.46	30665.81	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14
B75DD015	28345.77	30672.63	-15.00	0.00391	0.00000	0.00000	0.00000	-20.00	14.14
B75DD015	28353.09	30679.45	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.15
B75DD015	28360.40	30686.28	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.34

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD016	28316.93	30644.90	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.49
B75DD016	28325.59	30649.90	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
B75DD016	28334.24	30654.90	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14
B75DD016	28342.90	30659.90	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14
B75DD016	28351.56	30664.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.14
B75DD016	28360.23	30669.90	-25.00	0.00357	0.00000	0.00000	0.00000	-30.00	12.19

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD017	28183.75	30742.87	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.55
B75DD017	28182.75	30737.19	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55
B75DD017	28181.74	30731.50	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.55
B75DD017	28180.74	30725.82	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.55
B75DD017	28179.74	30720.13	-25.00	0.00018	0.00000	0.00000	0.00000	-30.00	11.55

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-004	28396.39	30677.87	15.00	0.00027	0.00000	0.00000	0.00000	10.00	15.11
YG85-004	28387.38	30670.76	5.00	0.00013	0.00000	0.00000	0.00000	0.00	15.34

YG85-004	28378.10	30663.63	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	15.46
YG85-004	28368.65	30656.47	-15.00	0.00750	0.00000	0.00000	0.00513	-20.00	15.55
YG85-004	28359.14	30649.30	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	15.56
YG85-004	28349.63	30642.13	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.56

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-005	28399.63	30680.28	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.41
YG85-005	28395.56	30676.60	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.41
YG85-005	28391.46	30672.92	-5.00	0.00017	0.00000	0.00000	0.00000	-10.00	11.44
YG85-005	28387.28	30669.21	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.48
YG85-005	28383.02	30665.47	-25.00	0.00087	0.00000	0.00000	0.00000	-30.00	11.51
YG85-005	28378.69	30661.69	-35.00	0.00017	0.00000	0.00000	0.00000	-40.00	11.56
YG85-005	28374.09	30657.78	-45.00	0.00003	0.00000	0.00000	0.00000	-50.00	11.81
YG85-005	28369.27	30653.74	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.81
YG85-005	28364.45	30649.71	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.81
YG85-005	28359.63	30645.68	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.81
YG85-005	28354.80	30641.64	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.81
YG85-005	28349.83	30637.53	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.99
YG85-005	28344.64	30633.32	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.06
YG85-005	28339.40	30629.07	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.06
YG85-005	28334.16	30624.83	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	12.06
YG85-005	28328.92	30620.58	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	8.96

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-006	28395.98	30681.75	15.00	0.00054	0.00000	0.00000	0.00000	10.00	13.77
YG85-006	28386.63	30681.59	5.00	0.00001	0.00000	0.00000	0.00000	0.00	13.62
YG85-006	28377.38	30681.51	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.62
YG85-006	28368.13	30681.43	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.62
YG85-006	28358.91	30681.37	-25.00	0.00044	0.00000	0.00000	0.00000	-30.00	13.59
YG85-006	28349.69	30681.36	-35.00	0.00022	0.00000	0.00000	0.00000	-40.00	13.61
YG85-006	28340.41	30681.36	-45.00	0.02588	0.00120	0.00000	0.08793	-50.00	13.67
YG85-006	28331.06	30681.36	-55.00	0.00012	0.00000	0.00000	0.00000	-60.00	13.71
YG85-006	28321.62	30681.35	-65.00	0.00015	0.00000	0.00000	0.00000	-70.00	13.79
YG85-006	28312.13	30681.32	-75.00	0.00087	0.00000	0.00000	0.00000	-80.00	13.80
YG85-006	28302.56	30681.23	-85.00	0.00022	0.00000	0.00000	0.00000	-90.00	13.88
YG85-006	28292.89	30681.05	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.94
YG85-006	28283.15	30680.77	-105.00	0.00014	0.00000	0.00000	0.00000	-110.00	13.98
YG85-006	28273.40	30680.45	-115.00	0.00021	0.00000	0.00000	0.00000	-120.00	13.96
YG85-006	28263.66	30680.11	-125.00	0.00043	0.00000	0.00000	0.00000	-130.00	13.96
YG85-006	28253.97	30679.77	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	13.90
YG85-006	28244.32	30679.43	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	13.90
YG85-006	28234.67	30679.09	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	13.90
YG85-006	28225.02	30678.75	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	13.90
YG85-006	28215.37	30678.41	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	10.49

ELEVATION
OF MID

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-007	28398.45	30681.80	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.56
YG85-007	28392.64	30681.71	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.56
YG85-007	28386.83	30681.61	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.56
YG85-007	28381.02	30681.52	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.56
YG85-007	28375.11	30681.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.67
YG85-007	28369.05	30681.52	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.72
YG85-007	28362.94	30681.59	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.72
YG85-007	28356.84	30681.65	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.72
YG85-007	28350.69	30681.73	-65.00	0.00155	0.00000	0.00000	0.00000	-70.00	11.77
YG85-007	28344.46	30681.83	-75.00	0.00074	0.00000	0.00000	0.00000	-80.00	11.79
YG85-007	28338.21	30681.93	-85.00	0.00169	0.00000	0.00000	0.00000	-90.00	11.79
YG85-007	28331.95	30682.04	-95.00	0.00025	0.00000	0.00000	0.00000	-100.00	11.80
YG85-007	28325.67	30682.16	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.82
YG85-007	28319.31	30682.27	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.89
YG85-007	28312.84	30682.38	-125.00	0.00184	0.00000	0.00000	0.00000	-130.00	11.94
YG85-007	28306.28	30682.49	-135.00	0.00050	0.00000	0.00000	0.00000	-140.00	11.98
YG85-007	28299.67	30682.61	-145.00	0.00017	0.00000	0.00000	0.00000	-150.00	11.99
YG85-007	28293.05	30682.72	-155.00	0.42161	0.02458	0.00146	1.24529	-160.00	12.00

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-010	28399.83	30681.81	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.87
YG85-010	28395.58	30681.64	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.87
YG85-010	28391.33	30681.47	-5.00	0.00055	0.00000	0.00000	0.00000	-10.00	10.87
YG85-010	28386.97	30681.32	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.96
YG85-010	28382.49	30681.16	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.96
YG85-010	28378.01	30681.01	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.96
YG85-010	28373.53	30680.85	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.96
YG85-010	28369.05	30680.69	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.96
YG85-010	28364.57	30680.54	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.96
YG85-010	28360.09	30680.38	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.96
YG85-010	28355.52	30680.22	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.04
YG85-010	28350.79	30680.05	-95.00	0.02260	0.00146	0.00135	0.03826	-100.00	11.09
YG85-010	28345.93	30679.88	-105.00	0.03836	0.00413	0.00344	0.06832	-110.00	11.15
YG85-010	28340.94	30679.71	-115.00	0.00036	0.00000	0.00000	0.00000	-120.00	11.20
YG85-010	28335.87	30679.54	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.22
YG85-010	28330.78	30679.36	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.22
YG85-010	28325.69	30679.18	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.22
YG85-010	28320.60	30679.00	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.22
YG85-010	28315.50	30678.82	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.22
YG85-010	28310.41	30678.65	-175.00	0.00232	0.00000	0.00000	0.00000	-180.00	11.22
YG85-010	28305.32	30678.47	-185.00	0.02590	0.00730	0.00000	0.06626	-190.00	11.23
YG85-010	28300.22	30678.29	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.22
YG85-010	28295.13	30678.11	-205.00	0.00000	0.00000	0.00000	0.00000	-210.00	11.22
YG85-010	28290.04	30677.93	-215.00	0.00000	0.00000	0.00000	0.00000	-220.00	11.22
YG85-010	28284.95	30677.76	-225.00	0.00000	0.00000	0.00000	0.00000	-230.00	11.22
YG85-010	28279.86	30677.58	-235.00	0.00000	0.00000	0.00000	0.00000	-240.00	11.22
YG85-010	28274.77	30677.40	-245.00	0.00000	0.00000	0.00000	0.00000	-250.00	11.22

ELEVATION

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-011	28399.31	30680.97	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.41
YG85-011	28394.11	30679.23	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.41
YG85-011	28388.90	30677.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.41
YG85-011	28383.69	30675.75	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.41
YG85-011	28378.48	30674.01	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.41
YG85-011	28373.27	30672.27	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.41
YG85-011	28368.06	30670.54	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.41
YG85-011	28362.77	30668.87	-55.00	0.00897	0.00082	0.00041	0.03036	-60.00	11.46
YG85-011	28357.42	30667.31	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.44
YG85-011	28352.09	30665.79	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.44
YG85-011	28346.73	30664.30	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.44
YG85-011	28341.35	30662.90	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.45
YG85-011	28335.94	30661.54	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.45
YG85-011	28330.54	30660.18	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.45
YG85-011	28325.13	30658.82	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.45
YG85-011	28319.70	30657.49	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.48
YG85-011	28314.16	30656.22	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.53
YG85-011	28308.55	30655.01	-155.00	0.00035	0.00000	0.00000	0.00000	-160.00	11.54
YG85-011	28302.91	30653.83	-165.00	0.00062	0.00000	0.00000	0.00000	-170.00	11.55
YG85-011	28297.24	30652.73	-175.00	0.00035	0.00000	0.00000	0.00000	-180.00	11.55
YG85-011	28291.56	30651.69	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	11.55
YG85-011	28285.88	30650.67	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.55
YG85-011	28280.20	30649.65	-205.00	0.00000	0.00000	0.00000	0.00000	-210.00	11.55
YG85-011	28274.51	30648.64	-215.00	0.00000	0.00000	0.00000	0.00000	-220.00	11.55
YG85-011	28268.83	30647.63	-225.00	0.00000	0.00000	0.00000	0.00000	-230.00	11.55

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-012	28306.60	30703.73	15.00	0.00083	0.00000	0.00000	0.00000	10.00	14.45
YG85-012	28296.22	30703.30	5.00	0.00015	0.00000	0.00000	0.00000	0.00	14.39
YG85-012	28285.91	30702.93	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.36
YG85-012	28275.60	30702.57	-15.00	0.02794	0.00000	0.00000	0.00000	-20.00	14.37
YG85-012	28265.37	30702.22	-25.00	0.34624	0.00000	0.00000	0.00000	-30.00	14.27
YG85-012	28255.32	30701.92	-35.00	0.57821	0.00000	0.00000	0.00000	-40.00	14.08
YG85-012	28245.52	30701.68	-45.00	0.05592	0.00000	0.00000	0.00000	-50.00	13.93
YG85-012	28235.91	30701.48	-55.00	0.11184	0.00000	0.00000	0.00000	-60.00	13.80
YG85-012	28226.41	30701.32	-65.00	0.00291	0.00000	0.00000	0.00000	-70.00	13.78
YG85-012	28216.93	30701.15	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	13.79

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-013	28308.64	30703.65	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.52
YG85-013	28301.13	30702.99	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.52
YG85-013	28293.63	30702.34	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.52
YG85-013	28286.12	30701.68	-15.00	0.74449	0.01361	0.00821	0.07369	-20.00	12.52
YG85-013	28278.61	30701.02	-25.00	0.01069	0.00030	0.00363	0.03317	-30.00	12.52

YG85-013	28271.11	30700.37	-35.00	0.01477	0.00000	0.01155	0.00883	-40.00	12.52
YG85-013	28263.60	30699.71	-45.00	0.18755	0.01567	0.15936	0.06531	-50.00	12.52
YG85-013	28256.09	30699.05	-55.00	0.03645	0.00359	0.01395	0.01113	-60.00	12.52
YG85-013	28248.59	30698.40	-65.00	0.02242	0.09022	0.11492	0.24272	-70.00	12.52
YG85-013	28241.08	30697.74	-75.00	0.04144	0.00000	0.00000	0.00169	-80.00	9.07

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-014	28287.96	30728.18	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.33
YG85-014	28277.70	30728.15	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.33
YG85-014	28267.44	30728.13	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.33
YG85-014	28257.18	30728.11	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.33
YG85-014	28246.91	30728.08	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.33
YG85-014	28236.65	30728.06	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.33
YG85-014	28226.43	30728.04	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.28
YG85-014	28216.27	30728.04	-55.00	0.00007	0.00000	0.00000	0.00000	-60.00	14.24
YG85-014	28206.16	30728.04	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.20
YG85-014	28196.07	30728.04	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.21
YG85-014	28186.00	30728.04	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.18
YG85-014	28175.97	30728.04	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.15
YG85-014	28165.96	30728.04	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.72

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-015	28289.75	30728.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.02
YG85-015	28282.82	30728.37	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.17
YG85-015	28275.89	30728.55	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.17
YG85-015	28268.96	30728.72	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.17
YG85-015	28262.04	30728.90	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.17
YG85-015	28255.11	30729.08	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.17
YG85-015	28248.18	30729.26	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.17
YG85-015	28241.27	30729.44	-55.00	0.00049	0.00000	0.00000	0.00000	-60.00	12.14
YG85-015	28234.42	30729.66	-65.00	0.00015	0.00000	0.00000	0.00000	-70.00	12.11
YG85-015	28227.60	30729.91	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.10
YG85-015	28220.80	30730.14	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.10
YG85-015	28213.99	30730.38	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.10
YG85-015	28207.18	30730.62	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.10

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-016	28308.87	30702.93	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.90
YG85-016	28300.76	30702.16	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.90
YG85-016	28292.67	30701.40	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.87
YG85-016	28284.63	30700.68	-15.00	0.04587	0.01929	0.05755	0.14516	-20.00	12.84
YG85-016	28276.61	30699.96	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.84
YG85-016	28268.59	30699.23	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.84

YG85-016	28260.57	30698.51	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.84
YG85-016	28252.57	30697.75	-55.00	0.00647	0.00000	0.00000	0.00000	-60.00	12.83
YG85-016	28244.72	30696.94	-65.00	0.01181	0.00072	0.00144	0.00576	-70.00	12.66
YG85-016	28237.11	30696.07	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.54
YG85-016	28229.60	30695.18	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.53
YG85-016	28222.10	30694.28	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.54
YG85-016	28214.59	30693.38	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.53

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-017	28310.54	30703.30	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.62
YG85-017	28304.63	30703.06	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.62
YG85-017	28298.73	30702.82	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.62
YG85-017	28292.82	30702.59	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.61
YG85-017	28286.95	30702.49	-25.00	0.01448	0.00138	0.00092	0.01886	-30.00	11.59
YG85-017	28281.09	30702.49	-35.00	0.00026	0.00000	0.00000	0.00000	-40.00	11.59
YG85-017	28275.23	30702.49	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.59
YG85-017	28269.37	30702.49	-55.00	0.00181	0.00000	0.00000	0.00000	-60.00	11.59
YG85-017	28263.50	30702.49	-65.00	0.03383	0.00000	0.00090	0.00224	-70.00	11.60
YG85-017	28257.62	30702.49	-75.00	0.00078	0.00000	0.00000	0.00000	-80.00	11.61
YG85-017	28251.69	30702.49	-85.00	0.00100	0.00000	0.00000	0.00000	-90.00	11.64
YG85-017	28245.72	30702.49	-95.00	0.86861	0.11858	0.02608	1.01765	-100.00	11.66
YG85-017	28239.71	30702.49	-105.00	0.00064	0.00000	0.00000	0.00218	-110.00	11.67
YG85-017	28233.70	30702.49	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.66
YG85-017	28227.70	30702.49	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.67
YG85-017	28221.69	30702.49	-135.00	0.00086	0.00000	0.00000	0.00000	-140.00	11.66
YG85-017	28215.68	30702.49	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.67
YG85-017	28209.67	30702.49	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.67
YG85-017	28203.66	30702.49	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	5.03

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-018	28306.23	30705.18	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.86
YG85-018	28295.47	30707.00	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.75
YG85-018	28284.79	30708.88	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.75
YG85-018	28274.11	30710.77	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.75
YG85-018	28263.46	30712.68	-25.00	0.00725	0.00000	0.00000	0.00000	-30.00	14.71
YG85-018	28253.09	30714.74	-35.00	0.00288	0.00000	0.00000	0.00000	-40.00	14.40
YG85-018	28242.99	30716.93	-45.00	0.00021	0.00000	0.00000	0.00000	-50.00	14.37
YG85-018	28232.98	30719.18	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.27
YG85-018	28223.07	30721.47	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.27
YG85-018	28213.15	30723.76	-75.00	0.00004	0.00000	0.00000	0.00000	-80.00	14.27
YG85-018	28203.23	30726.04	-85.00	0.15244	0.00840	0.01291	0.08607	-90.00	14.28
YG85-018	28193.28	30728.34	-95.00	0.01991	0.01026	0.00171	0.09459	-100.00	14.30
YG85-018	28183.29	30730.65	-105.00	0.33048	0.00981	0.12484	0.22961	-110.00	14.34
YG85-018	28173.25	30732.97	-115.00	0.03590	0.00682	0.00107	0.00760	-120.00	14.37
YG85-018	28163.20	30735.29	-125.00	0.15579	0.00507	0.00169	0.03077	-130.00	8.08

ELEVATION

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-019	28234.36	30741.64	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.97
YG85-019	28223.75	30740.75	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.61
YG85-019	28213.14	30739.86	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.61
YG85-019	28202.53	30738.98	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.60
YG85-019	28191.96	30738.26	-15.00	0.00930	0.00967	0.39093	0.05064	-20.00	14.55
YG85-019	28181.42	30737.78	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.53
YG85-019	28170.88	30737.41	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.53
YG85-019	28160.37	30737.06	-45.00	0.00683	0.00120	0.00000	0.02637	-50.00	14.51
YG85-019	28149.94	30736.81	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.40
YG85-019	28139.58	30736.63	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.40
YG85-019	28129.24	30736.45	-75.00	0.00393	0.00000	0.00000	0.00000	-80.00	14.37
YG85-019	28118.97	30736.27	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.30
YG85-019	28108.77	30736.09	-95.00	0.00042	0.00000	0.00000	0.00000	-100.00	14.27

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-020	28227.60	30740.86	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.19
YG85-020	28220.66	30740.21	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.19
YG85-020	28213.72	30739.55	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.19
YG85-020	28206.79	30738.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.19
YG85-020	28199.85	30738.25	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.19
YG85-020	28192.91	30737.60	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.19
YG85-020	28185.98	30736.95	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.19
YG85-020	28179.04	30736.29	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.19
YG85-020	28172.10	30735.64	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.19
YG85-020	28165.15	30735.01	-75.00	0.00052	0.00000	0.00000	0.00000	-80.00	12.20
YG85-020	28158.18	30734.40	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.21
YG85-020	28151.21	30733.79	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.21

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-022	28225.28	30778.96	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.91
YG85-022	28218.25	30778.81	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.22
YG85-022	28211.22	30778.66	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.22
YG85-022	28204.20	30778.51	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.22
YG85-022	28197.17	30778.36	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.22
YG85-022	28190.20	30778.31	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.16
YG85-022	28183.31	30778.39	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.13
YG85-022	28176.44	30778.50	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.13
YG85-022	28169.56	30778.61	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.13
YG85-022	28162.62	30778.76	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.22
YG85-022	28155.60	30778.95	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.22
YG85-022	28148.56	30779.13	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.23
YG85-022	28141.54	30779.32	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.22
YG85-022	28134.51	30779.51	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.22
YG85-022	28127.48	30779.70	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	12.22

YG85-022	28120.45	30779.89	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	12.22
YG85-022	28113.42	30780.08	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	12.22

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-023	28227.12	30759.93	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.51
YG85-023	28215.87	30759.51	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.05
YG85-023	28204.62	30759.09	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.06
YG85-023	28193.38	30758.68	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	15.05
YG85-023	28182.12	30758.26	-15.00	0.00096	0.00000	0.00000	0.00000	-20.00	15.06
YG85-023	28170.84	30757.85	-25.00	0.00017	0.00000	0.00000	0.00000	-30.00	15.10
YG85-023	28159.55	30757.46	-35.00	0.00013	0.00000	0.00000	0.00000	-40.00	15.09
YG85-023	28148.26	30757.07	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	15.09
YG85-023	28136.96	30756.67	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	15.10

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-024	28219.99	30759.84	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.09
YG85-024	28213.20	30759.79	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.09
YG85-024	28206.40	30759.75	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.09
YG85-024	28199.61	30759.70	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.09
YG85-024	28192.80	30759.70	-25.00	0.00016	0.00000	0.00000	0.00000	-30.00	12.11
YG85-024	28185.92	30759.80	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.16
YG85-024	28178.92	30760.05	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.26
YG85-024	28171.84	30760.38	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.26
YG85-024	28164.75	30760.72	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.26
YG85-024	28157.66	30761.05	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.26
YG85-024	28150.58	30761.39	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.26

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-025	28163.80	30843.53	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.27
YG85-025	28152.77	30844.79	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.95
YG85-025	28141.73	30846.10	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.95
YG85-025	28130.70	30847.46	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.95
YG85-025	28119.67	30848.81	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.87

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-002	28308.65	30704.72	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.71
YG86-002	28300.86	30705.62	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.71
YG86-002	28293.06	30706.52	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.71

YG86-002	28285.26	30707.41	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.72
YG86-002	28277.43	30708.26	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.73
YG86-002	28269.51	30709.09	-35.00	0.00016	0.00000	0.00000	0.00000	-40.00	12.83
YG86-002	28261.51	30709.93	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.85
YG86-002	28253.48	30710.78	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.85
YG86-002	28245.46	30711.62	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.85
YG86-002	28237.43	30712.46	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.86
YG86-002	28229.35	30713.28	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.91
YG86-002	28221.23	30714.07	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.91
YG86-002	28213.08	30714.84	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.94
YG86-002	28204.84	30715.53	-115.00	0.00086	0.00000	0.00000	0.00000	-120.00	13.02
YG86-002	28196.48	30716.13	-125.00	0.00046	0.00000	0.00000	0.00000	-130.00	13.08
YG86-002	28188.03	30716.69	-135.00	0.00015	0.00000	0.00000	0.00000	-140.00	13.14
YG86-002	28179.49	30717.21	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	13.18
YG86-002	28170.88	30717.69	-155.00	0.00165	0.00000	0.00000	0.00000	-160.00	13.23
YG86-002	28162.15	30718.09	-165.00	1.58898	0.00128	0.00344	0.05991	-170.00	13.33
YG86-002	28153.26	30718.35	-175.00	0.00349	0.00000	0.00000	0.00370	-180.00	13.44
YG86-002	28144.34	30718.49	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	13.49

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-005	28310.61	30704.12	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.33
YG86-005	28305.27	30704.21	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.33
YG86-005	28299.94	30704.30	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.33
YG86-005	28294.60	30704.40	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.33
YG86-005	28289.34	30704.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.27
YG86-005	28284.17	30704.56	-35.00	0.01232	0.00000	0.00000	0.00000	-40.00	11.24
YG86-005	28279.06	30704.61	-45.00	0.00080	0.00000	0.00000	0.00000	-50.00	11.22
YG86-005	28273.97	30704.65	-55.00	0.00394	0.00000	0.00000	0.00000	-60.00	11.22
YG86-005	28268.87	30704.70	-65.00	0.00071	0.00000	0.00000	0.00000	-70.00	11.22
YG86-005	28263.76	30704.73	-75.00	0.00030	0.00000	0.00000	0.00000	-80.00	11.24
YG86-005	28258.59	30704.74	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.28
YG86-005	28253.38	30704.74	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.27
YG86-005	28248.18	30704.74	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.28
YG86-005	28242.94	30704.74	-115.00	0.20344	0.03970	0.00000	0.01453	-120.00	11.30
YG86-005	28237.67	30704.74	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.30
YG86-005	28232.41	30704.74	-135.00	0.00142	0.00000	0.00000	0.00000	-140.00	11.30
YG86-005	28227.16	30704.74	-145.00	0.00008	0.00000	0.00000	0.00000	-150.00	11.30
YG86-005	28221.90	30704.74	-155.00	0.00036	0.00000	0.00000	0.00000	-160.00	11.29
YG86-005	28216.60	30704.78	-165.00	0.16835	0.00753	0.00000	0.06616	-170.00	11.34
YG86-005	28211.21	30704.85	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	11.37
YG86-005	28205.72	30704.97	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	11.45
YG86-005	28200.13	30705.15	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.47
YG86-005	28194.51	30705.34	-205.00	0.00056	0.00000	0.00000	0.00000	-210.00	11.48
YG86-005	28188.87	30705.57	-215.00	0.00839	0.00000	0.01310	0.05909	-220.00	11.49
YG86-005	28183.22	30705.84	-225.00	0.00000	0.00000	0.00000	0.00000	-230.00	11.49
YG86-005	28177.57	30706.11	-235.00	0.00000	0.00000	0.00000	0.00000	-240.00	10.53

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE

YG86-007	28311.89	30703.01	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.84
YG86-007	28307.77	30702.33	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.84
YG86-007	28303.65	30701.66	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.84
YG86-007	28299.54	30700.99	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.84
YG86-007	28295.35	30700.29	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.89
YG86-007	28291.01	30699.55	-35.00	0.04483	0.01814	0.00000	0.05536	-40.00	10.97
YG86-007	28286.48	30698.78	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.04
YG86-007	28281.88	30698.01	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.04
YG86-007	28277.28	30697.24	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.04
YG86-007	28272.63	30696.48	-75.00	0.00082	0.00000	0.00000	0.00000	-80.00	11.07
YG86-007	28267.86	30695.72	-85.00	0.36641	0.01651	0.03911	0.14810	-90.00	11.14
YG86-007	28263.00	30694.98	-95.00	0.02990	0.01175	0.09718	0.13490	-100.00	11.15
YG86-007	28258.12	30694.25	-105.00	0.44496	0.05331	0.05128	0.99438	-110.00	11.16
YG86-007	28253.20	30693.55	-115.00	0.00143	0.00000	0.00000	0.00000	-120.00	11.17
YG86-007	28248.27	30692.85	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.18
YG86-007	28243.33	30692.16	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.17
YG86-007	28238.39	30691.46	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.17
YG86-007	28233.46	30690.77	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.17
YG86-007	28228.52	30690.07	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	6.51

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-009	28313.09	30703.39	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.34
YG86-009	28310.46	30703.27	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.34
YG86-009	28307.82	30703.14	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.34
YG86-009	28305.18	30703.02	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.34
YG86-009	28302.54	30702.90	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.34
YG86-009	28299.90	30702.78	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.34
YG86-009	28297.27	30702.65	-45.00	0.04796	0.02551	0.18826	0.14780	-50.00	10.34
YG86-009	28294.60	30702.51	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.36
YG86-009	28291.90	30702.37	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.36
YG86-009	28289.21	30702.23	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.36
YG86-009	28286.48	30702.09	-85.00	0.00404	0.00000	0.00000	0.00000	-90.00	10.37
YG86-009	28283.72	30701.94	-95.00	0.00029	0.00000	0.00000	0.00000	-100.00	10.38
YG86-009	28280.95	30701.79	-105.00	0.00011	0.00000	0.00000	0.00000	-110.00	10.38
YG86-009	28278.18	30701.65	-115.00	0.00846	0.00000	0.00000	0.00000	-120.00	10.38
YG86-009	28275.41	30701.51	-125.00	0.00663	0.00000	0.00000	0.00000	-130.00	10.38
YG86-009	28272.64	30701.38	-135.00	0.00039	0.00000	0.00000	0.00000	-140.00	10.38
YG86-009	28269.87	30701.29	-145.00	0.18525	0.02304	0.00000	0.01205	-150.00	10.38
YG86-009	28267.10	30701.23	-155.00	0.00266	0.00000	0.00000	0.00000	-160.00	10.38
YG86-009	28264.32	30701.19	-165.00	0.00027	0.00000	0.00000	0.00000	-170.00	5.86

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-011	28307.70	30700.70	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.33
YG86-011	28298.01	30697.33	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.33
YG86-011	28288.31	30694.11	-5.00	0.01755	0.00268	0.00067	0.07177	-10.00	14.27
YG86-011	28278.58	30691.11	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.26
YG86-011	28268.85	30688.29	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.21
YG86-011	28259.13	30685.57	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.20

YG86-011	28249.41	30682.88	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.20
YG86-011	28239.69	30680.28	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.17
YG86-011	28229.98	30677.85	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.14
YG86-011	28220.24	30675.56	-75.00	0.00042	0.00000	0.00000	0.00000	-80.00	14.14
YG86-011	28210.46	30673.49	-85.00	0.00088	0.00000	0.00000	0.00000	-90.00	14.14
YG86-011	28200.65	30671.56	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.14
YG86-011	28190.83	30669.65	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	14.14
YG86-011	28181.02	30667.74	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	14.14
YG86-011	28171.21	30665.83	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	6.67

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-013	28309.60	30701.34	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.77
YG86-013	28302.11	30698.71	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.77
YG86-013	28294.61	30696.14	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.76
YG86-013	28286.98	30693.77	-15.00	0.05430	0.00894	0.04434	0.28419	-20.00	12.85
YG86-013	28279.13	30691.55	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.96
YG86-013	28271.19	30689.36	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.96
YG86-013	28263.17	30687.22	-45.00	0.00046	0.00000	0.00000	0.00000	-50.00	13.03
YG86-013	28255.04	30685.23	-55.00	0.00020	0.00000	0.00000	0.00000	-60.00	13.06
YG86-013	28246.84	30683.42	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	13.06
YG86-013	28238.61	30681.77	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	13.06
YG86-013	28230.31	30680.27	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	13.10
YG86-013	28221.94	30678.90	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.12
YG86-013	28213.55	30677.60	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	13.12
YG86-013	28205.13	30676.33	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	13.15
YG86-013	28196.68	30675.12	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	13.15
YG86-013	28188.23	30673.93	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	13.15
YG86-013	28179.78	30672.74	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	6.94

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-015	28311.64	30701.88	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.28
YG86-015	28306.82	30699.86	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.28
YG86-015	28302.00	30697.84	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.28
YG86-015	28297.15	30695.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.28
YG86-015	28292.26	30694.09	-25.00	0.08261	0.02797	0.00410	0.27871	-30.00	11.28
YG86-015	28287.32	30692.35	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.29
YG86-015	28282.32	30690.65	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.32
YG86-015	28277.30	30688.98	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.32
YG86-015	28272.25	30687.32	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.33
YG86-015	28267.15	30685.69	-75.00	0.00018	0.00000	0.00000	0.00000	-80.00	11.36
YG86-015	28261.95	30684.10	-85.00	0.00017	0.00000	0.00000	0.00000	-90.00	11.40
YG86-015	28256.71	30682.55	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.39
YG86-015	28251.47	30681.04	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.39
YG86-015	28246.24	30679.53	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.39
YG86-015	28241.01	30678.03	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.38
YG86-015	28235.79	30676.54	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.37
YG86-015	28230.63	30675.05	-145.00	0.00054	0.00000	0.00000	0.00000	-150.00	11.34
YG86-015	28225.50	30673.58	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.33

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-021	28313.26	30701.52	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.76
YG86-021	28310.08	30699.13	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.76
YG86-021	28306.90	30696.75	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.76
YG86-021	28303.70	30694.38	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.77
YG86-021	28300.46	30692.03	-25.00	0.02905	0.00704	0.00422	0.10841	-30.00	10.78
YG86-021	28297.17	30689.69	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.79
YG86-021	28293.83	30687.35	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.80
YG86-021	28290.49	30685.01	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.80
YG86-021	28287.14	30682.66	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.80
YG86-021	28283.77	30680.30	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.82
YG86-021	28280.36	30677.91	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.84
YG86-021	28276.92	30675.51	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.84
YG86-021	28273.48	30673.11	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.84
YG86-021	28270.05	30670.70	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	10.84
YG86-021	28266.60	30668.29	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.86
YG86-021	28263.13	30665.86	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.86
YG86-021	28259.65	30663.42	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	10.86
YG86-021	28256.18	30660.99	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	9.86

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-022	28284.63	30702.86	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.94
YG86-022	28274.28	30702.59	15.00	0.00014	0.00000	0.00000	0.00000	10.00	14.40
YG86-022	28263.93	30702.32	5.00	0.04875	0.00838	0.00484	0.07029	0.00	14.39
YG86-022	28253.58	30702.04	-5.00	1.00107	0.05478	0.33837	1.36270	-10.00	14.40
YG86-022	28243.23	30701.77	-15.00	0.04175	0.05618	0.59942	1.25751	-20.00	14.10

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-023	28288.66	30724.25	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.24
YG86-023	28279.48	30717.32	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.24
YG86-023	28270.24	30710.47	-5.00	0.00088	0.00000	0.00000	0.00000	-10.00	15.25
YG86-023	28260.90	30703.75	-15.00	0.04439	0.04748	0.35873	0.53969	-20.00	15.24
YG86-023	28251.54	30697.16	-25.00	0.01553	0.00500	0.03160	0.10143	-30.00	15.16
YG86-023	28242.21	30690.62	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.15
YG86-023	28232.90	30684.10	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	15.12
YG86-023	28223.60	30677.60	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	15.12
YG86-023	28214.31	30671.09	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	15.12
YG86-023	28205.04	30664.60	-75.00	0.00238	0.00000	0.00000	0.00000	-80.00	15.09

	COMPOSITE	COMPOSITE	ELEVATION OF MID POINT OF					BASE OF	WIDTH OF

HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE
YG86-024	28273.13	30714.01	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.87
YG86-024	28266.14	30707.72	15.00	0.00385	0.00092	0.00092	0.02248	10.00	13.73
YG86-024	28259.15	30701.42	5.00	0.00030	0.00000	0.00000	0.00000	0.00	13.73
YG86-024	28252.16	30695.13	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.73
YG86-024	28245.18	30688.85	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.69

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-025	28290.29	30725.62	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.08
YG86-025	28283.43	30720.73	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.08
YG86-025	28276.53	30715.91	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.05
YG86-025	28269.60	30711.18	-15.00	0.00225	0.00000	0.00000	0.00000	-20.00	13.06
YG86-025	28262.65	30706.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.05
YG86-025	28255.69	30701.79	-35.00	0.10859	0.04589	0.58169	0.46592	-40.00	13.06
YG86-025	28248.73	30697.10	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	13.05
YG86-025	28241.80	30692.46	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	13.00
YG86-025	28234.92	30687.90	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.94
YG86-025	28228.07	30683.38	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.94
YG86-025	28221.22	30678.88	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.93
YG86-025	28214.40	30674.42	-95.00	0.00013	0.00000	0.00000	0.00000	-100.00	12.87
YG86-025	28207.61	30670.01	-105.00	0.00065	0.00000	0.00000	0.00000	-110.00	12.87
YG86-025	28200.82	30665.59	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.86

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-026	28273.36	30714.18	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.46
YG86-026	28269.07	30710.31	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.55
YG86-026	28264.78	30706.45	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55
YG86-026	28260.49	30702.59	-5.00	0.04297	0.04552	1.14118	1.80152	-10.00	11.55

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-027	28291.73	30727.02	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.39
YG86-027	28287.04	30724.26	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.39
YG86-027	28282.35	30721.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.39
YG86-027	28277.66	30718.72	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.39
YG86-027	28272.96	30715.96	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.39
YG86-027	28268.27	30713.19	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.39
YG86-027	28263.59	30710.49	-45.00	0.00022	0.00000	0.00000	0.00000	-50.00	11.35
YG86-027	28258.91	30707.84	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.35
YG86-027	28254.25	30705.18	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.34
YG86-027	28249.58	30702.52	-75.00	0.00175	0.00000	0.00000	0.00000	-80.00	11.36
YG86-027	28244.87	30699.85	-85.00	0.18104	0.06848	0.00626	0.25510	-90.00	11.39
YG86-027	28240.07	30697.17	-95.00	0.00045	0.00000	0.00000	0.00000	-100.00	11.43

YG86-027	28235.24	30694.48	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.43
YG86-027	28230.39	30691.80	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.43
YG86-027	28225.55	30689.11	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.43
YG86-027	28220.71	30686.42	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	7.13

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-028	28284.95	30731.77	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.50
YG86-028	28276.65	30723.32	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.50
YG86-028	28267.96	30714.88	-5.00	0.00025	0.00000	0.00000	0.00000	-10.00	15.92
YG86-028	28258.75	30706.50	-15.00	0.00249	0.00000	0.00000	0.00000	-20.00	16.02
YG86-028	28249.42	30698.21	-25.00	0.13049	0.00000	0.00000	0.00000	-30.00	15.96
YG86-028	28240.01	30690.14	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.90
YG86-028	28230.49	30682.26	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	15.89
YG86-028	28220.94	30674.44	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	15.89
YG86-028	28211.39	30666.61	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	15.89
YG86-028	28201.79	30658.85	-75.00	0.00013	0.00000	0.00000	0.00000	-80.00	15.89
YG86-028	28192.09	30651.20	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	15.89
YG86-028	28182.36	30643.59	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	9.85

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-029	28287.62	30734.41	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.06
YG86-029	28282.98	30729.52	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.06
YG86-029	28278.34	30724.63	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.06
YG86-029	28273.69	30719.73	-15.00	0.00021	0.00000	0.00000	0.00000	-20.00	12.06
YG86-029	28269.04	30714.84	-25.00	0.00068	0.00000	0.00000	0.00000	-30.00	12.06
YG86-029	28264.40	30709.95	-35.00	0.00015	0.00000	0.00000	0.00000	-40.00	12.06
YG86-029	28259.76	30705.06	-45.00	0.00238	0.00000	0.00000	0.00000	-50.00	12.06
YG86-029	28255.12	30700.16	-55.00	0.02503	0.00082	0.00082	0.05864	-60.00	12.06
YG86-029	28250.48	30695.27	-65.00	0.39434	0.07419	0.19247	0.35375	-70.00	12.07
YG86-029	28245.83	30690.38	-75.00	0.00004	0.00000	0.00000	0.00000	-80.00	12.06
YG86-029	28241.19	30685.48	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.06
YG86-029	28236.54	30680.59	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.06
YG86-029	28231.90	30675.69	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.06
YG86-029	28227.26	30670.80	-115.00	0.00001	0.00000	0.00000	0.00000	-120.00	12.06
YG86-029	28222.62	30665.91	-125.00	0.00033	0.00000	0.00000	0.00000	-130.00	12.07
YG86-029	28217.98	30661.02	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	12.06

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-030	28289.16	30735.73	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.86
YG86-030	28286.49	30732.43	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.86
YG86-030	28283.82	30729.13	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.86
YG86-030	28281.15	30725.83	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.86
YG86-030	28278.47	30722.54	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.86

YG86-030	28275.80	30719.24	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.86
YG86-030	28273.13	30715.94	-45.00	0.00037	0.00000	0.00000	0.00000	-50.00	10.86
YG86-030	28270.46	30712.64	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.86
YG86-030	28267.79	30709.34	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.86
YG86-030	28265.12	30706.04	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.86
YG86-030	28262.45	30702.74	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.86
YG86-030	28259.77	30699.44	-95.00	0.00386	0.00000	0.00000	0.00000	-100.00	10.86
YG86-030	28257.10	30696.14	-105.00	0.48468	0.05417	0.04040	0.32672	-110.00	10.86
YG86-030	28254.43	30692.85	-115.00	0.02478	0.00728	0.00000	0.84707	-120.00	10.86
YG86-030	28251.76	30689.55	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.50

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-031	28277.72	30745.70	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.80
YG86-031	28270.34	30739.70	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.80
YG86-031	28262.96	30733.71	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.80
YG86-031	28255.58	30727.71	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.80
YG86-031	28248.20	30721.71	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.80
YG86-031	28240.75	30715.78	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	13.82
YG86-031	28233.16	30709.96	-45.00	0.02237	0.00893	0.02667	0.05304	-50.00	13.86
YG86-031	28225.43	30704.24	-55.00	0.00883	0.00147	0.00294	0.03638	-60.00	13.88
YG86-031	28217.65	30698.66	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	13.81
YG86-031	28209.86	30693.17	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	13.81
YG86-031	28202.08	30687.68	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	13.81
YG86-031	28194.29	30682.19	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.81

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-032	28279.17	30747.09	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.88
YG86-032	28274.04	30743.24	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.88
YG86-032	28268.90	30739.39	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.88
YG86-032	28263.77	30735.55	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.88
YG86-032	28258.64	30731.71	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.88
YG86-032	28253.51	30727.86	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.88
YG86-032	28248.37	30724.02	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.88
YG86-032	28243.24	30720.17	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.88
YG86-032	28237.98	30716.45	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.92
YG86-032	28232.54	30712.89	-75.00	0.00142	0.00000	0.00000	0.00000	-80.00	11.94
YG86-032	28226.98	30709.44	-85.00	0.00194	0.00000	0.00000	0.00000	-90.00	11.96
YG86-032	28221.35	30706.05	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.97
YG86-032	28215.69	30702.68	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	6.27

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-033	28280.42	30748.03	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.79
YG86-033	28277.21	30745.56	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.79

YG86-033	28274.00	30743.08	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.79
YG86-033	28270.79	30740.61	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.79
YG86-033	28267.58	30738.14	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.79
YG86-033	28264.37	30735.67	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.79
YG86-033	28261.15	30733.21	-45.00	0.00140	0.00000	0.00000	0.00000	-50.00	10.79
YG86-033	28257.93	30730.77	-55.00	0.00330	0.00000	0.00000	0.00000	-60.00	10.79
YG86-033	28254.71	30728.33	-65.00	0.00253	0.00000	0.00000	0.00000	-70.00	10.79
YG86-033	28251.48	30725.90	-75.00	0.00056	0.00000	0.00000	0.00000	-80.00	10.79
YG86-033	28248.22	30723.52	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.79
YG86-033	28244.92	30721.18	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.78
YG86-033	28241.62	30718.85	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.79
YG86-033	28238.32	30716.52	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	10.79
YG86-033	28235.01	30714.20	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.79
YG86-033	28231.68	30711.91	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.79
YG86-033	28228.34	30709.65	-145.00	0.00216	0.00000	0.00000	0.00000	-150.00	10.79
YG86-033	28224.99	30707.39	-155.00	0.00023	0.00000	0.00000	0.00000	-160.00	10.78

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-034	28261.03	30723.11	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.72
YG86-034	28253.63	30716.90	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.90
YG86-034	28246.24	30710.69	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.90
YG86-034	28238.84	30704.49	-5.00	0.00145	0.00000	0.00000	0.00000	-10.00	13.90
YG86-034	28231.44	30698.28	-15.00	0.54584	0.08076	0.29481	0.44803	-20.00	13.90
YG86-034	28224.05	30692.07	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.58

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-035	28266.73	30756.79	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.63
YG86-035	28258.36	30750.16	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.63
YG86-035	28249.99	30743.53	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.63
YG86-035	28241.62	30736.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.63
YG86-035	28233.24	30730.28	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.63
YG86-035	28224.76	30723.84	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.60
YG86-035	28216.11	30717.70	-45.00	0.01010	0.00352	0.03379	0.08724	-50.00	14.56
YG86-035	28207.40	30711.72	-55.00	0.00131	0.00000	0.00000	0.00000	-60.00	14.54
YG86-035	28198.66	30705.82	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.53
YG86-035	28189.92	30699.93	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.53
YG86-035	28181.18	30694.03	-85.00	0.00080	0.00000	0.00000	0.00000	-90.00	14.53
YG86-035	28172.45	30688.14	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.53
YG86-035	28163.71	30682.24	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	14.53

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-036	28268.54	30758.47	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.36
YG86-036	28262.67	30754.20	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.36

YG86-036	28256.80	30749.93	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.36
YG86-036	28250.93	30745.66	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.36
YG86-036	28245.05	30741.39	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.36
YG86-036	28239.18	30737.12	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.36
YG86-036	28233.31	30732.84	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.36
YG86-036	28227.44	30728.57	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.36
YG86-036	28221.56	30724.30	-65.00	0.00002	0.00000	0.00000	0.00000	-70.00	12.36
YG86-036	28215.60	30720.15	-75.00	0.00014	0.00000	0.00000	0.00000	-80.00	12.36
YG86-036	28209.53	30716.14	-85.00	0.02457	0.00130	0.00065	0.01730	-90.00	12.36
YG86-036	28203.24	30712.22	-95.00	0.00018	0.00000	0.00000	0.00000	-100.00	12.54
YG86-036	28196.73	30708.35	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.54
YG86-036	28190.22	30704.48	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.54
YG86-036	28183.72	30700.62	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	12.54
YG86-036	28177.21	30696.75	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	12.54
YG86-036	28170.70	30692.88	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	12.54
YG86-036	28164.19	30689.02	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	12.54
YG86-036	28157.69	30685.15	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	7.01

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-037	28269.90	30759.49	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.25
YG86-037	28265.78	30756.40	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.25
YG86-037	28261.66	30753.31	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.25
YG86-037	28257.54	30750.22	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.25
YG86-037	28253.43	30747.13	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.25
YG86-037	28249.31	30744.04	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.25
YG86-037	28245.19	30740.95	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.25
YG86-037	28241.07	30737.85	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.25
YG86-037	28236.95	30734.76	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.25
YG86-037	28232.83	30731.67	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.25
YG86-037	28228.71	30728.58	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.25
YG86-037	28224.59	30725.49	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.25
YG86-037	28220.47	30722.40	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.25
YG86-037	28216.31	30719.34	-115.00	0.00018	0.00000	0.00000	0.00000	-120.00	11.27
YG86-037	28211.99	30716.35	-125.00	0.00317	0.00000	0.00000	0.00000	-130.00	11.33
YG86-037	28207.54	30713.43	-135.00	0.00096	0.00000	0.00000	0.00000	-140.00	11.33
YG86-037	28203.09	30710.52	-145.00	0.00062	0.00000	0.00000	0.00000	-150.00	11.33
YG86-037	28198.63	30707.63	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.33
YG86-037	28194.17	30704.73	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.33
YG86-037	28189.71	30701.83	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	11.33

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-038	28261.36	30723.38	25.00	0.00000	0.00000	0.00000	0.00000	20.00	6.59
YG86-038	28257.07	30719.51	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.55
YG86-038	28252.78	30715.65	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55
YG86-038	28248.48	30711.79	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.55
YG86-038	28244.19	30707.93	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.55
YG86-038	28239.90	30704.06	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.55
YG86-038	28235.61	30700.20	-35.00	0.02012	0.03422	0.37878	0.69343	-40.00	11.54

YG86-038	28231.32	30696.34	-45.00	0.51725	0.05970	0.11637	0.12556	-50.00	11.55

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-039	28248.94	30731.65	25.00	0.00000	0.00000	0.00000	0.00000	20.00	9.88
YG86-039	28240.81	30724.95	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.53
YG86-039	28232.68	30718.25	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.53
YG86-039	28224.55	30711.55	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.53
YG86-039	28216.41	30704.84	-15.00	0.00957	0.00144	0.05286	0.12895	-20.00	14.53
YG86-039	28208.28	30698.14	-25.00	0.09643	0.01034	0.00154	0.08527	-30.00	8.21

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CAL-XYZ data file                             : TNABENA58T.ASY
Number of elements for Bench composites       : 4
Elements ident. Nos.                          : 1 , 2 , 3 , 4 ,
Height of bench                               :   10.00
Elevation of top of uppermost bench           :   50.00
Proportion of bench height                    :    0.50
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HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD001	28304.16	30678.08	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.32

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD002	28302.82	30678.12	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.62

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD003	28313.00	30684.85	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.04
P64DD003	28305.36	30678.43	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.42

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD004	28309.82	30682.40	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.46

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD006	28304.27	30691.06	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.30
P64DD006	28297.61	30685.47	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.99

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE

P64DD010	28164.86	30709.73	25.00	0.00000	0.00000	0.00000	0.00000	20.00	11.04
P64DD010	28168.28	30719.14	15.00	0.00000	0.00000	0.00000	0.00000	10.00	6.95

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD011	28169.23	30708.72	25.00	0.00000	0.00000	0.00000	0.00000	20.00	11.44
P64DD011	28172.90	30718.80	15.00	0.00000	0.00000	0.00000	0.00000	10.00	5.32

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD014	28261.07	30702.79	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.20
P64DD014	28261.68	30708.53	15.00	0.00000	0.00000	0.00000	0.00000	10.00	5.19

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD025	28278.62	30714.20	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.98
P64DD025	28277.58	30702.32	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.56

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
P64DD026	28299.74	30697.22	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.21
P64DD026	28293.31	30689.56	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
P64DD026	28286.88	30681.90	5.00	0.00000	0.00000	0.00000	0.00000	0.00	6.39

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD001	28063.57	30730.10	25.00	0.00000	0.00000	0.00000	0.00000	20.00	14.14
B75DD001	28068.57	30738.76	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD002	28064.95	30728.90	25.00	0.00000	0.00000	0.00000	0.00000	20.00	14.14
B75DD002	28072.61	30735.33	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14

B75DD002	28080.27	30741.76	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14	

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD003	28169.38	30704.72	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.92
B75DD003	28167.64	30714.57	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
B75DD003	28165.90	30724.42	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14
B75DD003	28164.16	30734.27	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14
B75DD003	28162.43	30744.12	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.14
B75DD003	28160.69	30753.96	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.14
B75DD003	28158.96	30763.81	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.14

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD004	28170.88	30703.17	25.00	0.00000	0.00000	0.00000	0.00000	20.00	9.22
B75DD004	28173.32	30709.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.92
B75DD004	28175.75	30715.22	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.92
B75DD004	28178.18	30721.24	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	6.26

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD005	28291.31	30669.04	25.00	0.00000	0.00000	0.00000	0.00000	20.00	8.88
B75DD005	28298.38	30676.11	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
B75DD005	28305.45	30683.18	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14
B75DD005	28312.52	30690.25	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14
B75DD005	28319.59	30697.32	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.14
B75DD005	28326.66	30704.39	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.75

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD006	28289.75	30669.05	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.56
B75DD006	28292.20	30674.80	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.79
B75DD006	28294.63	30680.55	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.79
B75DD006	28297.08	30686.31	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.80
B75DD006	28299.53	30692.06	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	5.53

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE

B75DD007	28311.14	30702.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.38
B75DD007	28306.92	30698.78	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.38
B75DD007	28302.70	30695.37	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.38
B75DD007	28298.48	30691.95	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.38
B75DD007	28294.26	30688.53	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.38

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD008	28309.79	30703.85	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.92
B75DD008	28303.33	30703.18	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.93
B75DD008	28296.87	30702.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.93
B75DD008	28290.41	30701.81	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.93
B75DD008	28283.95	30701.13	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.92

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD009	28308.73	30700.22	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.90
B75DD009	28300.92	30694.54	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.90
B75DD009	28293.11	30688.87	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.90
B75DD009	28285.29	30683.19	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.90
B75DD009	28277.48	30677.51	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.90
B75DD009	28269.67	30671.84	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	5.00

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD011	28319.20	30687.63	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.64
B75DD011	28316.67	30685.02	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.64
B75DD011	28314.14	30682.40	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.64
B75DD011	28311.62	30679.78	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.64
B75DD011	28309.09	30677.16	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.64

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD013	28332.89	30680.57	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.04
B75DD013	28332.22	30680.01	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.04
B75DD013	28331.54	30679.44	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.04
B75DD013	28330.88	30678.88	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.04
B75DD013	28330.21	30678.32	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.04
B75DD013	28329.53	30677.76	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.04
B75DD013	28328.86	30677.19	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.04
B75DD013	28328.19	30676.63	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	5.52

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD014	28331.35	30679.21	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.64
B75DD014	28328.56	30676.87	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.64
B75DD014	28325.77	30674.53	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.64
B75DD014	28322.99	30672.19	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.64

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD015	28316.52	30645.35	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.39
B75DD015	28323.83	30652.17	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
B75DD015	28331.15	30658.99	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14
B75DD015	28338.46	30665.81	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14
B75DD015	28345.77	30672.63	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.14
B75DD015	28353.09	30679.45	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.15
B75DD015	28360.40	30686.28	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.34

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD016	28316.93	30644.90	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.49
B75DD016	28325.59	30649.90	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14
B75DD016	28334.24	30654.90	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14
B75DD016	28342.90	30659.90	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14
B75DD016	28351.56	30664.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.14
B75DD016	28360.23	30669.90	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.19

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
B75DD017	28183.75	30742.87	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.55
B75DD017	28182.75	30737.19	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55
B75DD017	28181.74	30731.50	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.55
B75DD017	28180.74	30725.82	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.55
B75DD017	28179.74	30720.13	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.55

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-004	28396.39	30677.87	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.11
YG85-004	28387.38	30670.76	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.34

YG85-004	28378.10	30663.63	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	15.46
YG85-004	28368.65	30656.47	-15.00	0.00006	0.00577	0.00513	0.00577	-20.00	15.55
YG85-004	28359.14	30649.30	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	15.56
YG85-004	28349.63	30642.13	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.56

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-005	28399.63	30680.28	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.41
YG85-005	28395.56	30676.60	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.41
YG85-005	28391.46	30672.92	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.44
YG85-005	28387.28	30669.21	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.48
YG85-005	28383.02	30665.47	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.51
YG85-005	28378.69	30661.69	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.56
YG85-005	28374.09	30657.78	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.81
YG85-005	28369.27	30653.74	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.81
YG85-005	28364.45	30649.71	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.81
YG85-005	28359.63	30645.68	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.81
YG85-005	28354.80	30641.64	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.81
YG85-005	28349.83	30637.53	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.99
YG85-005	28344.64	30633.32	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.06
YG85-005	28339.40	30629.07	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.06
YG85-005	28334.16	30624.83	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	12.06
YG85-005	28328.92	30620.58	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	8.96

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-006	28395.98	30681.75	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.77
YG85-006	28386.63	30681.59	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.62
YG85-006	28377.38	30681.51	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.62
YG85-006	28368.13	30681.43	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.62
YG85-006	28358.91	30681.37	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.59
YG85-006	28349.69	30681.36	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	13.61
YG85-006	28340.41	30681.36	-45.00	0.00884	0.31543	0.02754	0.50831	-50.00	13.67
YG85-006	28331.06	30681.36	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	13.71
YG85-006	28321.62	30681.35	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	13.79
YG85-006	28312.13	30681.32	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	13.80
YG85-006	28302.56	30681.23	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	13.88
YG85-006	28292.89	30681.05	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.94
YG85-006	28283.15	30680.77	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	13.98
YG85-006	28273.40	30680.45	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	13.96
YG85-006	28263.66	30680.11	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	13.96
YG85-006	28253.97	30679.77	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	13.90
YG85-006	28244.32	30679.43	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	13.90
YG85-006	28234.67	30679.09	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	13.90
YG85-006	28225.02	30678.75	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	13.90
YG85-006	28215.37	30678.41	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	10.49

ELEVATION
OF MID

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-007	28398.45	30681.80	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.56
YG85-007	28392.64	30681.71	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.56
YG85-007	28386.83	30681.61	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.56
YG85-007	28381.02	30681.52	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.56
YG85-007	28375.11	30681.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.67
YG85-007	28369.05	30681.52	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.72
YG85-007	28362.94	30681.59	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.72
YG85-007	28356.84	30681.65	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.72
YG85-007	28350.69	30681.73	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.77
YG85-007	28344.46	30681.83	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.79
YG85-007	28338.21	30681.93	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.79
YG85-007	28331.95	30682.04	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.80
YG85-007	28325.67	30682.16	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.82
YG85-007	28319.31	30682.27	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.89
YG85-007	28312.84	30682.38	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.94
YG85-007	28306.28	30682.49	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.98
YG85-007	28299.67	30682.61	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.99
YG85-007	28293.05	30682.72	-155.00	0.06450	2.78004	0.29552	4.12506	-160.00	12.00

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-010	28399.83	30681.81	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.87
YG85-010	28395.58	30681.64	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.87
YG85-010	28391.33	30681.47	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.87
YG85-010	28386.97	30681.32	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.96
YG85-010	28382.49	30681.16	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.96
YG85-010	28378.01	30681.01	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.96
YG85-010	28373.53	30680.85	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.96
YG85-010	28369.05	30680.69	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.96
YG85-010	28364.57	30680.54	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.96
YG85-010	28360.09	30680.38	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.96
YG85-010	28355.52	30680.22	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.04
YG85-010	28350.79	30680.05	-95.00	0.01213	0.25475	0.03625	0.43101	-100.00	11.09
YG85-010	28345.93	30679.88	-105.00	0.01716	0.47842	0.05338	0.81763	-110.00	11.15
YG85-010	28340.94	30679.71	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.20
YG85-010	28335.87	30679.54	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.22
YG85-010	28330.78	30679.36	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.22
YG85-010	28325.69	30679.18	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.22
YG85-010	28320.60	30679.00	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.22
YG85-010	28315.50	30678.82	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.22
YG85-010	28310.41	30678.65	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	11.22
YG85-010	28305.32	30678.47	-185.00	0.01319	0.00000	0.01684	0.00000	-190.00	11.23
YG85-010	28300.22	30678.29	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.22
YG85-010	28295.13	30678.11	-205.00	0.00000	0.00000	0.00000	0.00000	-210.00	11.22
YG85-010	28290.04	30677.93	-215.00	0.00000	0.00000	0.00000	0.00000	-220.00	11.22
YG85-010	28284.95	30677.76	-225.00	0.00000	0.00000	0.00000	0.00000	-230.00	11.22
YG85-010	28279.86	30677.58	-235.00	0.00000	0.00000	0.00000	0.00000	-240.00	11.22
YG85-010	28274.77	30677.40	-245.00	0.00000	0.00000	0.00000	0.00000	-250.00	11.22

ELEVATION

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-011	28399.31	30680.97	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.41
YG85-011	28394.11	30679.23	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.41
YG85-011	28388.90	30677.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.41
YG85-011	28383.69	30675.75	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.41
YG85-011	28378.48	30674.01	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.41
YG85-011	28373.27	30672.27	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.41
YG85-011	28368.06	30670.54	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.41
YG85-011	28362.77	30668.87	-55.00	0.01522	0.00082	0.00697	0.00000	-60.00	11.46
YG85-011	28357.42	30667.31	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.44
YG85-011	28352.09	30665.79	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.44
YG85-011	28346.73	30664.30	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.44
YG85-011	28341.35	30662.90	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.45
YG85-011	28335.94	30661.54	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.45
YG85-011	28330.54	30660.18	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.45
YG85-011	28325.13	30658.82	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.45
YG85-011	28319.70	30657.49	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.48
YG85-011	28314.16	30656.22	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.53
YG85-011	28308.55	30655.01	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.54
YG85-011	28302.91	30653.83	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.55
YG85-011	28297.24	30652.73	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	11.55
YG85-011	28291.56	30651.69	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	11.55
YG85-011	28285.88	30650.67	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.55
YG85-011	28280.20	30649.65	-205.00	0.00000	0.00000	0.00000	0.00000	-210.00	11.55
YG85-011	28274.51	30648.64	-215.00	0.00000	0.00000	0.00000	0.00000	-220.00	11.55
YG85-011	28268.83	30647.63	-225.00	0.00000	0.00000	0.00000	0.00000	-230.00	11.55

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-012	28306.60	30703.73	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.45
YG85-012	28296.22	30703.30	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.39
YG85-012	28285.91	30702.93	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.36
YG85-012	28275.60	30702.57	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.37
YG85-012	28265.37	30702.22	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.27
YG85-012	28255.32	30701.92	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.08
YG85-012	28245.52	30701.68	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	13.93
YG85-012	28235.91	30701.48	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	13.80
YG85-012	28226.41	30701.32	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	13.78
YG85-012	28216.93	30701.15	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	13.79

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-013	28308.64	30703.65	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.52
YG85-013	28301.13	30702.99	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.52
YG85-013	28293.63	30702.34	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.52
YG85-013	28286.12	30701.68	-15.00	0.01170	1.09155	0.35762	1.98320	-20.00	12.52
YG85-013	28278.61	30701.02	-25.00	0.00161	0.00593	0.06161	0.00000	-30.00	12.52

YG85-013	28271.11	30700.37	-35.00	0.00116	0.00000	0.01019	0.00000	-40.00	12.52
YG85-013	28263.60	30699.71	-45.00	0.10246	0.02139	0.11513	0.00268	-50.00	12.52
YG85-013	28256.09	30699.05	-55.00	0.01407	0.01508	0.01430	0.00987	-60.00	12.52
YG85-013	28248.59	30698.40	-65.00	0.37558	0.52089	0.24272	0.41778	-70.00	12.52
YG85-013	28241.08	30697.74	-75.00	1.68420	0.94431	0.01010	0.41400	-80.00	9.07

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-014	28287.96	30728.18	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.33
YG85-014	28277.70	30728.15	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.33
YG85-014	28267.44	30728.13	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.33
YG85-014	28257.18	30728.11	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.33
YG85-014	28246.91	30728.08	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.33
YG85-014	28236.65	30728.06	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.33
YG85-014	28226.43	30728.04	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.28
YG85-014	28216.27	30728.04	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.24
YG85-014	28206.16	30728.04	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.20
YG85-014	28196.07	30728.04	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.21
YG85-014	28186.00	30728.04	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.18
YG85-014	28175.97	30728.04	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.15
YG85-014	28165.96	30728.04	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.72

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-015	28289.75	30728.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.02
YG85-015	28282.82	30728.37	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.17
YG85-015	28275.89	30728.55	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.17
YG85-015	28268.96	30728.72	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.17
YG85-015	28262.04	30728.90	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.17
YG85-015	28255.11	30729.08	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.17
YG85-015	28248.18	30729.26	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.17
YG85-015	28241.27	30729.44	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.14
YG85-015	28234.42	30729.66	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.11
YG85-015	28227.60	30729.91	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.10
YG85-015	28220.80	30730.14	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.10
YG85-015	28213.99	30730.38	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.10
YG85-015	28207.18	30730.62	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.10

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-016	28308.87	30702.93	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.90
YG85-016	28300.76	30702.16	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.90
YG85-016	28292.67	30701.40	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.87
YG85-016	28284.63	30700.68	-15.00	0.08884	0.51046	0.12585	0.73373	-20.00	12.84
YG85-016	28276.61	30699.96	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.84
YG85-016	28268.59	30699.23	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.84

YG85-016	28260.57	30698.51	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.84
YG85-016	28252.57	30697.75	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.83
YG85-016	28244.72	30696.94	-65.00	0.00101	0.00144	0.01657	0.00000	-70.00	12.66
YG85-016	28237.11	30696.07	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.54
YG85-016	28229.60	30695.18	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.53
YG85-016	28222.10	30694.28	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.54
YG85-016	28214.59	30693.38	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.53

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-017	28310.54	30703.30	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.62
YG85-017	28304.63	30703.06	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.62
YG85-017	28298.73	30702.82	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.62
YG85-017	28292.82	30702.59	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.61
YG85-017	28286.95	30702.49	-25.00	0.00718	0.13386	0.01334	0.22724	-30.00	11.59
YG85-017	28281.09	30702.49	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.59
YG85-017	28275.23	30702.49	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.59
YG85-017	28269.37	30702.49	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.59
YG85-017	28263.50	30702.49	-65.00	0.00049	0.01167	0.02155	0.01931	-70.00	11.60
YG85-017	28257.62	30702.49	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.61
YG85-017	28251.69	30702.49	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.64
YG85-017	28245.72	30702.49	-95.00	0.33296	6.59896	0.75672	11.32777	-100.00	11.66
YG85-017	28239.71	30702.49	-105.00	0.00084	0.00552	0.00275	0.00746	-110.00	11.67
YG85-017	28233.70	30702.49	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.66
YG85-017	28227.70	30702.49	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.67
YG85-017	28221.69	30702.49	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.66
YG85-017	28215.68	30702.49	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.67
YG85-017	28209.67	30702.49	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.67
YG85-017	28203.66	30702.49	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	5.03

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-018	28306.23	30705.18	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.86
YG85-018	28295.47	30707.00	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.75
YG85-018	28284.79	30708.88	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.75
YG85-018	28274.11	30710.77	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.75
YG85-018	28263.46	30712.68	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.71
YG85-018	28253.09	30714.74	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.40
YG85-018	28242.99	30716.93	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.37
YG85-018	28232.98	30719.18	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.27
YG85-018	28223.07	30721.47	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.27
YG85-018	28213.15	30723.76	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.27
YG85-018	28203.23	30726.04	-85.00	0.36431	1.46925	0.14625	2.37846	-90.00	14.28
YG85-018	28193.28	30728.34	-95.00	0.01199	0.29112	0.02328	0.44692	-100.00	14.30
YG85-018	28183.29	30730.65	-105.00	0.30823	1.47578	0.28579	2.27212	-110.00	14.34
YG85-018	28173.25	30732.97	-115.00	0.04691	0.64710	0.11573	1.16432	-120.00	14.37
YG85-018	28163.20	30735.29	-125.00	0.57715	2.31786	0.29990	3.84413	-130.00	8.08

ELEVATION

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-019	28234.36	30741.64	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.97
YG85-019	28223.75	30740.75	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.61
YG85-019	28213.14	30739.86	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.61
YG85-019	28202.53	30738.98	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.60
YG85-019	28191.96	30738.26	-15.00	0.30410	0.34939	0.35053	0.25036	-20.00	14.55
YG85-019	28181.42	30737.78	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.53
YG85-019	28170.88	30737.41	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.53
YG85-019	28160.37	30737.06	-45.00	0.03739	0.12764	0.01199	0.18457	-50.00	14.51
YG85-019	28149.94	30736.81	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.40
YG85-019	28139.58	30736.63	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.40
YG85-019	28129.24	30736.45	-75.00	0.30112	0.19161	0.00165	0.11700	-80.00	14.37
YG85-019	28118.97	30736.27	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.30
YG85-019	28108.77	30736.09	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.27

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-020	28227.60	30740.86	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.19
YG85-020	28220.64	30740.21	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.19
YG85-020	28213.72	30739.55	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.19
YG85-020	28206.79	30738.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.19
YG85-020	28199.85	30738.25	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.19
YG85-020	28192.91	30737.60	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.19
YG85-020	28185.98	30736.95	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.19
YG85-020	28179.04	30736.29	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.19
YG85-020	28172.10	30735.64	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.19
YG85-020	28165.15	30735.01	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.20
YG85-020	28158.18	30734.40	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.21
YG85-020	28151.21	30733.79	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.21

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-022	28225.28	30778.96	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.91
YG85-022	28218.25	30778.81	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.22
YG85-022	28211.22	30778.66	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.22
YG85-022	28204.20	30778.51	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.22
YG85-022	28197.17	30778.36	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.22
YG85-022	28190.20	30778.31	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.16
YG85-022	28183.31	30778.39	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.13
YG85-022	28176.44	30778.50	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.13
YG85-022	28169.56	30778.61	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.13
YG85-022	28162.62	30778.76	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.22
YG85-022	28155.60	30778.95	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.22
YG85-022	28148.56	30779.13	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.23
YG85-022	28141.54	30779.32	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.22
YG85-022	28134.51	30779.51	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.22
YG85-022	28127.48	30779.70	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	12.22

YG85-022	28120.45	30779.89	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	12.22
YG85-022	28113.42	30780.08	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	12.22

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-023	28227.12	30759.93	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.51
YG85-023	28215.87	30759.51	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.05
YG85-023	28204.62	30759.09	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.06
YG85-023	28193.38	30758.68	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	15.05
YG85-023	28182.12	30758.26	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	15.06
YG85-023	28170.84	30757.85	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	15.10
YG85-023	28159.55	30757.46	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.09
YG85-023	28148.26	30757.07	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	15.09
YG85-023	28136.96	30756.67	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	15.10

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-024	28219.99	30759.84	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.09
YG85-024	28213.20	30759.79	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.09
YG85-024	28206.40	30759.75	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.09
YG85-024	28199.61	30759.70	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.09
YG85-024	28192.80	30759.70	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.11
YG85-024	28185.92	30759.80	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.16
YG85-024	28178.92	30760.05	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.26
YG85-024	28171.84	30760.38	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.26
YG85-024	28164.75	30760.72	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.26
YG85-024	28157.66	30761.05	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.26
YG85-024	28150.58	30761.39	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.26

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG85-025	28163.80	30843.53	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.27
YG85-025	28152.77	30844.79	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.95
YG85-025	28141.73	30846.10	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.95
YG85-025	28130.70	30847.46	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.95
YG85-025	28119.67	30848.81	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.87

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-002	28308.65	30704.72	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.71
YG86-002	28300.86	30705.62	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.71
YG86-002	28293.06	30706.52	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.71

YG86-002	28285.26	30707.41	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.72
YG86-002	28277.43	30708.26	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.73
YG86-002	28269.51	30709.09	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.83
YG86-002	28261.51	30709.93	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.85
YG86-002	28253.48	30710.78	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.85
YG86-002	28245.46	30711.62	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.85
YG86-002	28237.43	30712.46	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.86
YG86-002	28229.35	30713.28	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.91
YG86-002	28221.23	30714.07	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.91
YG86-002	28213.08	30714.84	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.94
YG86-002	28204.84	30715.53	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	13.02
YG86-002	28196.48	30716.13	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	13.08
YG86-002	28188.03	30716.69	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	13.14
YG86-002	28179.49	30717.21	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	13.18
YG86-002	28170.88	30717.69	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	13.23
YG86-002	28162.15	30718.09	-165.00	0.77897	2.35333	0.95359	3.72078	-170.00	13.33
YG86-002	28153.26	30718.35	-175.00	0.00876	0.17735	0.02044	0.32018	-180.00	13.44
YG86-002	28144.24	30718.49	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	13.49

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-005	28310.61	30704.12	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.33
YG86-005	28305.27	30704.21	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.33
YG86-005	28299.94	30704.30	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.33
YG86-005	28294.60	30704.40	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.33
YG86-005	28289.34	30704.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.27
YG86-005	28284.17	30704.56	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.24
YG86-005	28279.06	30704.61	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.22
YG86-005	28273.97	30704.65	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.22
YG86-005	28268.87	30704.70	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.72
YG86-005	28263.76	30704.73	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.24
YG86-005	28258.59	30704.74	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.28
YG86-005	28253.38	30704.74	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.27
YG86-005	28248.18	30704.74	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.28
YG86-005	28242.94	30704.74	-115.00	0.07653	1.63459	0.12924	3.00605	-120.00	11.30
YG86-005	28237.67	30704.74	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.30
YG86-005	28232.41	30704.74	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.30
YG86-005	28227.16	30704.74	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.30
YG86-005	28221.90	30704.74	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.29
YG86-005	28216.60	30704.78	-165.00	0.03412	1.23601	0.10258	2.22384	-170.00	11.34
YG86-005	28211.21	30704.85	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	11.37
YG86-005	28205.72	30704.97	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	11.45
YG86-005	28200.13	30705.15	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.47
YG86-005	28194.51	30705.34	-205.00	0.00000	0.00000	0.00000	0.00000	-210.00	11.48
YG86-005	28188.87	30705.57	-215.00	0.11252	0.16762	0.02654	0.16889	-220.00	11.49
YG86-005	28183.22	30705.84	-225.00	0.00000	0.00000	0.00000	0.00000	-230.00	11.49
YG86-005	28177.57	30706.11	-235.00	0.00000	0.00000	0.00000	0.00000	-240.00	10.53

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE

YG86-007	28311.89	30703.01	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.84
YG86-007	28307.77	30702.33	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.84
YG86-007	28303.65	30701.66	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.84
YG86-007	28299.54	30700.99	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.84
YG86-007	28295.35	30700.29	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.89
YG86-007	28291.01	30699.55	-35.00	0.19543	0.50810	0.06969	0.74306	-40.00	10.97
YG86-007	28286.48	30698.78	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.04
YG86-007	28281.88	30698.01	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.04
YG86-007	28277.28	30697.24	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.04
YG86-007	28272.63	30696.48	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.07
YG86-007	28267.86	30695.72	-85.00	0.02868	0.04374	0.26327	0.01864	-90.00	11.14
YG86-007	28263.00	30694.98	-95.00	0.00180	0.00152	0.15942	0.00000	-100.00	11.15
YG86-007	28258.12	30694.25	-105.00	0.43907	5.68491	0.31855	9.71325	-110.00	11.16
YG86-007	28253.20	30693.55	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.17
YG86-007	28248.27	30692.85	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.18
YG86-007	28243.33	30692.16	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.17
YG86-007	28238.39	30691.46	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.17
YG86-007	28233.46	30690.77	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.17
YG86-007	28228.52	30690.07	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	6.51

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-009	28313.09	30703.39	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.34
YG86-009	28310.46	30703.27	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.34
YG86-009	28307.82	30703.14	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.34
YG86-009	28305.18	30703.02	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.34
YG86-009	28302.54	30702.90	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.34
YG86-009	28299.90	30702.78	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.34
YG86-009	28297.27	30702.65	-45.00	0.04469	0.00264	0.13988	0.00000	-50.00	10.34
YG86-009	28294.60	30702.51	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.36
YG86-009	28291.90	30702.37	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.36
YG86-009	28289.21	30702.23	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.36
YG86-009	28286.48	30702.09	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.37
YG86-009	28283.72	30701.94	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.38
YG86-009	28280.95	30701.79	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.38
YG86-009	28278.18	30701.65	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	10.38
YG86-009	28275.41	30701.51	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.38
YG86-009	28272.64	30701.38	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.38
YG86-009	28269.87	30701.29	-145.00	0.00718	1.19843	0.12130	2.21700	-150.00	10.38
YG86-009	28267.10	30701.23	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	10.38
YG86-009	28264.32	30701.19	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	5.86

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-011	28307.70	30700.70	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.33
YG86-011	28298.01	30697.33	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.33
YG86-011	28288.31	30694.11	-5.00	0.29733	0.35481	0.02146	0.35950	-10.00	14.27
YG86-011	28278.58	30691.11	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.26
YG86-011	28268.85	30688.29	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.21
YG86-011	28259.13	30685.57	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.20

YG86-011	28249.41	30682.88	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.20
YG86-011	28239.69	30680.28	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.17
YG86-011	28229.98	30677.85	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.14
YG86-011	28220.24	30675.56	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.14
YG86-011	28210.46	30673.49	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.14
YG86-011	28200.65	30671.56	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.14
YG86-011	28190.83	30669.65	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	14.14
YG86-011	28181.02	30667.74	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	14.14
YG86-011	28171.21	30665.83	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	6.67

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-013	28309.60	30701.34	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.77
YG86-013	28302.11	30698.71	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.77
YG86-013	28294.61	30696.14	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.76
YG86-013	28286.98	30693.77	-15.00	0.20873	0.42131	0.10174	0.39013	-20.00	12.85
YG86-013	28279.13	30691.55	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.96
YG86-013	28271.19	30689.36	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.96
YG86-013	28263.17	30687.22	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	13.03
YG86-013	28255.04	30685.23	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	13.06
YG86-013	28246.84	30683.42	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	13.06
YG86-013	28238.61	30681.77	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	13.06
YG86-013	28230.31	30680.27	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	13.10
YG86-013	28221.94	30678.90	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.12
YG86-013	28213.55	30677.60	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	13.12
YG86-013	28205.13	30676.33	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	13.15
YG86-013	28196.68	30675.12	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	13.15
YG86-013	28188.23	30673.93	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	13.15
YG86-013	28179.78	30672.74	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	6.94

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-015	28311.64	30701.88	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.28
YG86-015	28306.82	30699.86	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.28
YG86-015	28302.00	30697.84	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.28
YG86-015	28297.15	30695.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.28
YG86-015	28292.26	30694.09	-25.00	0.08362	0.50063	0.10755	0.77040	-30.00	11.28
YG86-015	28287.32	30692.35	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.29
YG86-015	28282.32	30690.65	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.32
YG86-015	28277.30	30688.98	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.32
YG86-015	28272.25	30687.32	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.33
YG86-015	28267.15	30685.69	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.36
YG86-015	28261.95	30684.10	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.40
YG86-015	28256.71	30682.55	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.39
YG86-015	28251.47	30681.04	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.39
YG86-015	28246.24	30679.53	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.39
YG86-015	28241.01	30678.03	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.38
YG86-015	28235.79	30676.54	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.37
YG86-015	28230.63	30675.05	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.34
YG86-015	28225.50	30673.58	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.33

YG86-015	28220.39	30672.11	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.33
YG86-015	28215.29	30670.64	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	9.11

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-017	28309.27	30698.64	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.40
YG86-017	28300.92	30692.57	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.35
YG86-017	28292.55	30686.61	-5.00	1.01549	3.39980	0.10939	4.82248	-10.00	14.33
YG86-017	28283.99	30680.78	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.48
YG86-017	28275.24	30675.01	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.49
YG86-017	28266.47	30669.25	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.49
YG86-017	28257.71	30663.49	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.49
YG86-017	28248.83	30657.76	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.61
YG86-017	28239.79	30652.06	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.66
YG86-017	28230.70	30646.38	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.66
YG86-017	28221.61	30640.70	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.66

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-019	28311.00	30699.91	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.62
YG86-019	28304.77	30695.38	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.62
YG86-019	28298.52	30690.97	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.55
YG86-019	28292.20	30686.80	-15.00	0.17865	0.32697	4.11407	0.19826	-20.00	12.54
YG86-019	28285.76	30682.80	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.56
YG86-019	28279.25	30678.88	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.56
YG86-019	28272.74	30674.95	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.56
YG86-019	28266.24	30671.02	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.56
YG86-019	28259.73	30667.09	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.56
YG86-019	28253.22	30663.17	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.56
YG86-019	28246.72	30659.24	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.56
YG86-019	28240.20	30655.36	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.54
YG86-019	28233.68	30651.57	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.52
YG86-019	28227.16	30647.80	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.52
YG86-019	28220.63	30644.03	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	8.59

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-020	28285.11	30702.89	25.00	0.00000	0.00000	0.00000	0.00000	20.00	6.22
YG86-020	28278.39	30702.36	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.06
YG86-020	28271.67	30701.83	5.00	0.11460	0.84483	0.16155	1.13026	0.00	12.06
YG86-020	28264.94	30701.30	-5.00	0.47382	4.67757	1.83605	8.14552	-10.00	12.06
YG86-020	28258.22	30700.78	-15.00	0.17617	2.62369	5.62829	3.77765	-20.00	12.06
YG86-020	28251.49	30700.24	-25.00	0.00837	0.00826	0.04479	0.00000	-30.00	12.06
YG86-020	28244.76	30699.72	-35.00	0.00004	0.00078	0.00272	0.00000	-40.00	12.07
YG86-020	28238.04	30699.19	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.06

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-021	28313.26	30701.52	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.76
YG86-021	28310.08	30699.13	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.76
YG86-021	28306.90	30696.75	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.76
YG86-021	28303.70	30694.38	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.77
YG86-021	28300.46	30692.03	-25.00	0.04674	0.22246	0.04083	0.27737	-30.00	10.78
YG86-021	28297.17	30689.69	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.79
YG86-021	28293.83	30687.35	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.80
YG86-021	28290.49	30685.01	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.80
YG86-021	28287.14	30682.66	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.80
YG86-021	28283.77	30680.30	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.82
YG86-021	28280.36	30677.91	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.84
YG86-021	28276.92	30675.51	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.84
YG86-021	28273.48	30673.11	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.84
YG86-021	28270.05	30670.70	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	10.84
YG86-021	28266.60	30668.29	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.86
YG86-021	28263.13	30665.86	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.86
YG86-021	28259.65	30663.42	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	10.86
YG86-021	28256.18	30660.99	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	9.86

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-022	28284.63	30702.86	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.94
YG86-022	28274.28	30702.59	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.40
YG86-022	28263.93	30702.32	5.00	0.01248	0.16411	0.07577	0.23118	0.00	14.39
YG86-022	28253.58	30702.04	-5.00	0.29257	0.74008	1.01892	0.91762	-10.00	14.40
YG86-022	28243.23	30701.77	-15.00	0.62072	0.20478	1.36645	0.00000	-20.00	14.10

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-023	28288.66	30724.25	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.24
YG86-023	28279.48	30717.32	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.24
YG86-023	28270.24	30710.47	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	15.25
YG86-023	28260.90	30703.75	-15.00	0.05974	0.01057	0.50433	0.00000	-20.00	15.24
YG86-023	28251.54	30697.16	-25.00	0.00665	0.00158	0.02613	0.00000	-30.00	15.16
YG86-023	28242.21	30690.62	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.15
YG86-023	28232.90	30684.10	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	15.12
YG86-023	28223.60	30677.60	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	15.12
YG86-023	28214.31	30671.09	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	15.12
YG86-023	28205.04	30664.60	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	15.09

	COMPOSITE	COMPOSITE	ELEVATION OF MID POINT OF					BASE OF	WIDTH OF

HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE
YG86-024	28273.13	30714.01	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.87
YG86-024	28266.14	30707.72	15.00	0.00376	0.02385	0.01009	0.02064	10.00	13.73
YG86-024	28259.15	30701.42	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.73
YG86-024	28252.16	30695.13	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.73
YG86-024	28245.18	30688.85	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.69

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-025	28290.29	30725.62	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.08
YG86-025	28283.43	30720.73	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.08
YG86-025	28276.53	30715.91	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.05
YG86-025	28269.60	30711.18	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.06
YG86-025	28262.65	30706.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.05
YG86-025	28255.69	30701.79	-35.00	0.08924	0.02134	0.61747	0.00000	-40.00	13.06
YG86-025	28248.73	30697.10	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	13.05
YG86-025	28241.80	30692.46	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	13.00
YG86-025	28234.92	30687.90	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.94
YG86-025	28228.07	30683.38	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.94
YG86-025	28221.22	30678.88	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.93
YG86-025	28214.40	30674.42	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.87
YG86-025	28207.61	30670.01	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.87
YG86-025	28200.82	30665.59	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.86

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-026	28273.36	30714.18	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.46
YG86-026	28269.07	30710.31	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.55
YG86-026	28264.78	30706.45	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55
YG86-026	28260.49	30702.59	-5.00	0.53762	0.24569	1.12008	0.01041	-10.00	11.55

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-027	28291.73	30727.02	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.39
YG86-027	28287.04	30724.26	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.39
YG86-027	28282.35	30721.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.39
YG86-027	28277.66	30718.72	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.39
YG86-027	28272.96	30715.96	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.39
YG86-027	28268.27	30713.19	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.39
YG86-027	28263.59	30710.49	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.35
YG86-027	28258.91	30707.84	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.35
YG86-027	28254.25	30705.18	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.34
YG86-027	28249.58	30702.52	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.36
YG86-027	28244.87	30699.85	-85.00	0.05472	1.48112	0.20472	2.58161	-90.00	11.39
YG86-027	28240.07	30697.17	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.43

YG86-027	28235.24	30694.48	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.43
YG86-027	28230.39	30691.80	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.43
YG86-027	28225.55	30689.11	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.43
YG86-027	28220.71	30686.42	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	7.13

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-028	28284.95	30731.77	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.50
YG86-028	28276.65	30723.32	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.50
YG86-028	28267.96	30714.88	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	15.92
YG86-028	28258.75	30706.50	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	16.02
YG86-028	28249.42	30698.21	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	15.96
YG86-028	28240.01	30690.14	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.90
YG86-028	28230.49	30682.26	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	15.89
YG86-028	28220.94	30674.44	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	15.89
YG86-028	28211.39	30666.61	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	15.89
YG86-028	28201.79	30658.85	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	15.89
YG86-028	28192.09	30651.20	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	15.89
YG86-028	28182.36	30643.59	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	9.85

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-029	28287.62	30734.41	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.06
YG86-029	28282.98	30729.52	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.06
YG86-029	28278.34	30724.63	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.06
YG86-029	28273.69	30719.73	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.06
YG86-029	28269.04	30714.84	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.06
YG86-029	28264.40	30709.95	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.06
YG86-029	28259.76	30705.06	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.06
YG86-029	28255.12	30700.16	-55.00	0.32803	0.05180	0.10140	0.00000	-60.00	12.06
YG86-029	28250.48	30695.27	-65.00	0.51516	0.07446	0.47160	0.02578	-70.00	12.07
YG86-029	28245.83	30690.38	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.06
YG86-029	28241.19	30685.48	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.06
YG86-029	28236.54	30680.59	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.06
YG86-029	28231.90	30675.69	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.06
YG86-029	28227.26	30670.80	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.06
YG86-029	28222.62	30665.91	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	12.07
YG86-029	28217.98	30661.02	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	12.06

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-030	28289.16	30735.73	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.86
YG86-030	28286.49	30732.43	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.86
YG86-030	28283.82	30729.13	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.86
YG86-030	28281.15	30725.83	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.86
YG86-030	28278.47	30722.54	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.86

YG86-030	28275.80	30719.24	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.86
YG86-030	28273.13	30715.94	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.86
YG86-030	28270.46	30712.64	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.86
YG86-030	28267.79	30709.34	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.86
YG86-030	28265.12	30706.04	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.86
YG86-030	28262.45	30702.74	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.86
YG86-030	28259.77	30699.44	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.86
YG86-030	28257.10	30696.14	-105.00	0.36847	1.86245	0.64185	2.87831	-110.00	10.86
YG86-030	28254.43	30692.85	-115.00	0.12535	1.27796	0.02978	1.51268	-120.00	10.86
YG86-030	28251.76	30689.55	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.50

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-031	28277.72	30745.70	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.80
YG86-031	28270.34	30739.70	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.80
YG86-031	28262.96	30733.71	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.80
YG86-031	28255.58	30727.71	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.80
YG86-031	28248.20	30721.71	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.80
YG86-031	28240.75	30715.78	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	13.82
YG86-031	28233.16	30709.96	-45.00	1.06910	1.02653	0.15387	1.00734	-50.00	13.86
YG86-031	28225.43	30704.24	-55.00	0.06422	0.09364	0.01422	0.08971	-60.00	13.88
YG86-031	28217.65	30698.66	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	13.81
YG86-031	28209.86	30693.17	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	13.81
YG86-031	28202.08	30687.68	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	13.81
YG86-031	28194.29	30682.19	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.81

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-032	28279.17	30747.09	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.88
YG86-032	28274.04	30743.24	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.88
YG86-032	28268.90	30739.39	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.88
YG86-032	28263.77	30735.55	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.88
YG86-032	28258.64	30731.71	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.88
YG86-032	28253.51	30727.86	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.88
YG86-032	28248.37	30724.02	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.88
YG86-032	28243.24	30720.17	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.88
YG86-032	28237.98	30716.45	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.92
YG86-032	28232.54	30712.89	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.94
YG86-032	28226.98	30709.44	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.96
YG86-032	28221.35	30706.05	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.97
YG86-032	28215.69	30702.68	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	6.27

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-033	28280.42	30748.03	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.79
YG86-033	28277.21	30745.56	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.79

YG86-033	28274.00	30743.08	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.79
YG86-033	28270.79	30740.61	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.79
YG86-033	28267.58	30738.14	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.79
YG86-033	28264.37	30735.67	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.79
YG86-033	28261.15	30733.21	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.79
YG86-033	28257.93	30730.77	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.79
YG86-033	28254.71	30728.33	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.79
YG86-033	28251.48	30725.90	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.79
YG86-033	28248.22	30723.52	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.79
YG86-033	28244.92	30721.18	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.78
YG86-033	28241.62	30718.85	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.79
YG86-033	28238.32	30716.52	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	10.79
YG86-033	28235.01	30714.20	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.79
YG86-033	28231.68	30711.91	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.79
YG86-033	28228.34	30709.65	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	10.79
YG86-033	28224.99	30707.39	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	10.78

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-034	28261.03	30723.11	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.72
YG86-034	28253.63	30716.90	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.90
YG86-034	28246.24	30710.69	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.90
YG86-034	28238.84	30704.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.90
YG86-034	28231.44	30698.28	-15.00	1.10547	3.31534	2.37040	4.88795	-20.00	13.90
YG86-034	28224.05	30692.07	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.58

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-035	28266.73	30756.79	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.63
YG86-035	28258.36	30750.16	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.63
YG86-035	28249.99	30743.53	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.63
YG86-035	28241.62	30736.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.63
YG86-035	28233.24	30730.28	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14.63
YG86-035	28224.76	30723.84	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.60
YG86-035	28216.11	30717.70	-45.00	0.73265	0.78390	0.03899	0.79033	-50.00	14.56
YG86-035	28207.40	30711.72	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.54
YG86-035	28198.66	30705.82	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.53
YG86-035	28189.92	30699.93	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.53
YG86-035	28181.18	30694.03	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.53
YG86-035	28172.45	30688.14	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.53
YG86-035	28163.71	30682.24	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	14.53

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-036	28268.54	30758.47	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.36
YG86-036	28262.67	30754.20	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.36

YG86-036	28256.80	30749.93	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.36
YG86-036	28250.93	30745.66	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.36
YG86-036	28245.05	30741.39	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.36
YG86-036	28239.18	30737.12	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.36
YG86-036	28233.31	30732.84	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.36
YG86-036	28227.44	30728.57	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.36
YG86-036	28221.56	30724.30	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.36
YG86-036	28215.60	30720.15	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.36
YG86-036	28209.53	30716.14	-85.00	0.01603	0.03448	0.01779	0.04493	-90.00	12.36
YG86-036	28203.24	30712.22	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.54
YG86-036	28196.73	30708.35	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.54
YG86-036	28190.22	30704.48	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.54
YG86-036	28183.72	30700.62	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	12.54
YG86-036	28177.21	30696.75	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	12.54
YG86-036	28170.70	30692.88	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	12.54
YG86-036	28164.19	30689.02	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	12.54
YG86-036	28157.69	30685.15	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	7.01

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-037	28269.90	30759.49	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.25
YG86-037	28265.78	30756.40	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.25
YG86-037	28261.66	30753.31	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.25
YG86-037	28257.54	30750.22	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.25
YG86-037	28253.43	30747.13	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.25
YG86-037	28249.31	30744.04	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.25
YG86-037	28245.19	30740.95	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.25
YG86-037	28241.07	30737.85	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.25
YG86-037	28236.95	30734.76	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.25
YG86-037	28232.83	30731.67	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.25
YG86-037	28228.71	30728.58	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.25
YG86-037	28224.59	30725.49	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.25
YG86-037	28220.47	30722.40	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.25
YG86-037	28216.31	30719.34	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.27
YG86-037	28211.99	30716.35	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.33
YG86-037	28207.54	30713.43	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.33
YG86-037	28203.09	30710.52	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.33
YG86-037	28198.63	30707.63	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.33
YG86-037	28194.17	30704.73	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.33
YG86-037	28189.71	30701.83	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	11.33

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-038	28261.36	30723.38	25.00	0.00000	0.00000	0.00000	0.00000	20.00	6.59
YG86-038	28257.07	30719.51	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.55
YG86-038	28252.78	30715.65	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55
YG86-038	28248.48	30711.79	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.55
YG86-038	28244.19	30707.93	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.55
YG86-038	28239.90	30704.06	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.55
YG86-038	28235.61	30700.20	-35.00	0.47714	1.07284	0.58727	0.87867	-40.00	11.54

YG86-038	28231.32	30696.34	-45.00	0.46027	2.05652	0.60952	3.33599	-50.00	11.55

HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE
YG86-039	28248.94	30731.65	25.00	0.00000	0.00000	0.00000	0.00000	20.00	9.88
YG86-039	28240.81	30724.95	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.53
YG86-039	28232.68	30718.25	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.53
YG86-039	28224.55	30711.55	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.53
YG86-039	28216.41	30704.84	-15.00	0.17970	0.10234	0.05371	0.00000	-20.00	14.53
YG86-039	28208.28	30698.14	-25.00	0.22952	0.79462	0.20278	1.22407	-30.00	8.21

APPENDIX III

EXPENDITURES JUNE, 1986 TO FEBRUARY, 1987

NOTES

(1) The June, 1986 E-SCAN Geophysical Program was an experimental program, therefore the rates charged by Premier Geophysics were lower than normal. Regular rates were charged for the October-December, 1986 program.

(2) Since several projects were underway on Banks Island at the time of the projects listed here, transportation costs are apportioned from the total amount incurred during each time period.

(3) Two boats & motors were purchased to transport crews on site during the field projects. The cost has been apportioned as a rate per day used.

APPENDIX III

GEOPHYSICAL SURVEY PERIOD OF FIELD WORK: JUNE 3 - JUNE 22, 1986

(1) Linecutting & grid preparation

Wages K. Burton	June 6	1 day @ 169.71/day		169.71
P. Huxley	June 6	1 days@ 146.57/day		146.57
Equipment Rental	EDM Survey Equip.	1 day @ 15/day		15.00
Field Supplies	Chain Saw, gas & oil			20.00
Camp/Costs	2 man days @ $40/day			80.00
Transportation	Boat & Motor	1 day @ $46.80/day		46.80
			Total	$558.08 X 478.08

(2) PREMIER GEOPHYSICS INC.

Wages	G.Shore	June 3-22	12 days @ $360/day	$4320.00
	A.Ryder	June 3-22	11.4 days @ $285/day	3249.00
	B.Pielak	June 3-9,14,22	9.6 days @ $240/day	2304.00
	M.Marchant	June 11-22	7.2 days @ $285/day	2052.00
				11,925

Total = 12,403.08 -

Equipment Rental	E-SCAN System 11 days @ $1140/day	$12540.00	
Field Supplies		1346.61	
MOB/DEMOB COSTS		2140.11	
		16,026.72	28671.19
CAMP/COSTS	58 Man days @ $40/day	2320.00	
Wages	J. Burton(cook) 15 days @ $108/day	1620.00	
TRANSPORTATION	Airfare J.Burton Vanc-Pr Rupert	286.77	
	Float Plane 1.1 Flights @ 392/flt	435.00	
	Helicopter 3.58 hrs @ $495.00/hr	1774.31	
	Boat & Motor 12 days @ $46.80	561.60	
COMMUNICATIONS		230.00	
			7227.68 ✓
REPORT PREPARATION			
	G.Shore June 30,July 14,31,1986 3 days @ $360/day	1080.00	
	Computer Costs 12.81 hours @ $60/hour	608.81	
			1688.81 ✓
	TOTAL		37587.68

27951.72

= 28,429.80

Total $37,346.29

GEOLOGICAL SURVEY PERIOD OF FIELD WORK: JUNE 10-20, 1986

CONTROL SURVEY			
	K. Burton June 9-17, 8 days @ $169.71/day	1357.68	
	P. Huxley June 9,14,16,17 4 days @ $146.57/day	586.78	
	A. Helfors June 10-13 4 days @ $114.75/day	459.00	
EQUIPMENT RENTAL	EDM EQUIPMENT 8 days @ $15/day	120.00	
GEOLOGICAL SURVEY			
	J. Shearer June 10-20 10 days @ $216.00/day	2160.00	
	A. Freeze June 10-17 8 days @ $216.00/day	1728.00	
			6411.46 ✓
CAMP COSTS	42 Man Days @ $40/day	1760.00	
	Wages J. Burton(cook) 8 days @ $108/day	756.00	
TRANSPORTATION	AIRFARE -J. Shearer	284.90	
	FLOAT PLANE 1.1 Flights @ 392/flt	435.00	
	BOAT & MOTOR 11 days @ $46.80/day	514.80	
COMMUNICATIONS		150.00	
			3900.70 ✓
REPORT PREPARATION			
Wages	J. Shearer July 3-8,1986 5 days @ $216.00	1080.00	
	J. Michell Jan 14,Feb 23, 1987 @ days @ 270.00	540.00	
	S. Gardiner Aug 14,feb 19-20 4 days @ 182.25	729.00	
	I. Korec Sept 24,29,1986 10 hours @ $15/Hour	150.00	
	C. Mantik July 7,8,1986,Feb20,1986 3 days @ $135/day	405.00	
	S. Johnson Feb 24,25 2 days @ 135/day	270.00	
REPRODUCTION		150.00	
			3324.00
	TOTAL		$13636.16 ✓

COMPUTERIZATION OF ASSAY RESULTS PERIOD OF DATA PROCESSING: July 3-Aug21,1986

H.A. SIMONS (INTERNATIONAL) LTD.

Wages				
O. Syberg July 3-23,Aug 8-21	27 days @ $320/day	$8640.00		
Computer Charges	27 days @ $50/day	1350.00		
Plotting	35 plans @25.29/plan	885.00		
			$10,875.00	✓
REPORT PREPARATION				
J. Shearer July 2,24	1 day @ 216/day	216.00		
S. Gardiner Feb 10,19,22,23	4 days @ 182.25/day	$729.00		
S. Skermer Feb 21	6 Hours @ $15/Hour	90.00		
Reproduction		250.00	2185.00 ✗	1285 1285.00
	TOTAL		$12160.00	✓

GEOPHYSICAL SURVEY PERIOD OF FIELD WORK: OCT 20-DEC 10,1986

(1) LINECUTTING & GRID PREPARATION

Wages	K.Burton	Nov8,10,11	3 days @ $169.71/day	$848.55
	A.Helfors	Nov5,8,11	3 days @ 131.14/day	393.42
Equipment Rental		EDM Equipment	1 day @$15/day	15.00
		Walkie Talkie	2 days @$5/day	15.00
Field Supplies		Chainsaw,Gas & Oil		115.00
Camp Accomodation	9 Man days @ $40/day			240.00
Transportation	Boat & Motor 5 days @$46.80/day			~~140.40~~

-1767.37 1427.95 X

(2) PREMIER GEOPHYSICS

Wages

G.Shore	Oct24-28,31,Nov1-16,Dec7	21 days @$486/day	10206.00
M.Marchant	Oct24-31,Nov1,2,4-16	21.66 days @$386/day	8360.00
B.Pielak	Oct24-31,Nov1-5,7-10,13,14,18.32 Dec7,8,	days @$310/day	4129.20
T.Gee	Oct24,31,Nov1-6,8-15,Dec7,8	21.32 days @$310/day	6609.20
B.Smith	Oct24-31,Nov1-4,6-10,Dec7,8	16.32 days @$244/day	3982.08

Equipment Rental 23 1/3 days @ $1776.00/day	41434.08
Field Supplies	726.81
Mob/Demob	2410.46
	77857.63

~~79,674.80~~

79,625.00

CAMP/COSTS	123 1/3 Man day @ $40/day	$4933.~~20~~ 33	
Wages	J.Burton(cook) 26 2/3 days @$123.43	~~3331.80~~ 3291.47	
Transportation	J & K Burton — ? Split Charter	296.00	
Float Plane	4.79 Flights @ $392/flt	1876.71	
Helicopter	3.25 hrs @$495/hr	1609.84	
Boat & Motor	21 days @$46.80/day	982.80	
Communications		482.50	
			13458.65 X = 13472.65
Report Preparation			
G.Shore	Feb 9-18 7.94 days @ $480/day	3810.00	
Computer Costs	68.5 hours @ $50/hour	3424.00	
S.Gardiner	Aug 13,Dec 11,Feb 18,22 4 days @ 182.25	729.00	
			7963.00
	TOTAL		$99279.28

Total ~~24,753.45~~ 21,435.65

166,553
+ 1,766.97
168,319.97

APPENDIX IV

PERSONNEL AND DAYS WORKED

APPENDIX IV

Personnel & Days Worked

Trader Resource Corp

J. Shearer	Geologist/Project Manager	June10-20,July3-8, 1986
A. Freeze	Geologist	June10-17,1986
J.Michell	Mining Engineer/Fame Project Supervisor	Jan14,Feb23,1987
S.Gardiner	Geologist/Fame Project Geologist	Aug 14,Dec,11,1986 February13-21,1987
K.Burton	Surveyor/Field Supervisor	June6,Nov8,10, 11,1986
P.Huxley	Camp Manager/Labourer	June 6,1986
A.Helfors	Labourer	Nov,8,11,1986
J.Burton	Camp Cook	June3-22,Oct23-31, Nov1-16,1986
I.Korec	Draughtsman	
S.Skermer	Draughtsman	February 21,1986
C.Mantik	Secretary	July 7,8,1986, February 20, 1987
S.Johnson	Secretary	Feb. 24,25,1987

Premier Geophysics Inc.

G.Shore	Geophysicist/Crew Chief	June3-22,Oct24-22, Nov1-16,DEc 7,1986
A.Ryder	Geologist/Geophysical Technition IV	June 3-22,1986
M.Marchant	Engineer/Crew Chief/ Geophysical Operator	June11-22,Oct24-31 Nov1,2,4,16,1986
B.Pielak	Crew Chief/Geophysical Operator	June3-9,14-22,Oct 24-31,Nov1-5,1-10, 13,14,Dec7,8
T.Gee	Geophysical Technition IV/ Field Supervisor	Oct24-31,Nov1-6,8, -15,Dec 7,8,1986
B.Smith	Geophysical Technition II	Oct24-31,Nov1-4, 6-10,Dec7,8,1986

H.A. Simon (International) Ltd.

O.Syberg	Engineer	July3-23,Aug8-21, 1986

APPENDIX V

STATEMENTS OF QUALIFICATIONS

STATEMENT OF QUALIFICATIONS

I, Johan T. Shearer of the City of Port Coquitlam, in the Province of British Columbia, do hereby certify:

1. I graduated in Honours Geology (B.Sc. 1973) from the University of British Columbia and the University of London, Imperial College (M.Sc. 1977).

2. I have practiced my profession as an Exploration Geologist continuously since graduation and have been employed by such mining companies as McIntyre Mines Ltd., J.C. Stephen Explorations Ltd. and Carolin Mines Ltd. I am presently employed by TRM Engineering Ltd.

3. I am a fellow of the Geological Association of Canada. I am also a member of the Canadian Institute of Mining and Metallurgy, the Geological Society of London and the Mineralogical Association of Canada.

4. I have personally conducted detail geological mapping, logged all diamond core and supervised general exploration field work on the Tel Deposit, Banks Island. This report is an interpretation of the data obtained.

Vancouver, B.C.
July 8, 1986

STATEMENT OF QUALIFICATIONS

I, Sharon L. Gardiner, of the District of North Vancouver, in thr Province of British Columbia, do hereby certify:

1. I graduated with a Bachelor of Science, Honours Degree in Earth Sciences (cooperative program) from the University of Waterloo in May, 1979.

2. I have practiced my profession continuously since graduation.

3. I am a Fellow of the Geological Association of Canada.

4. I compiled this summary using reports written by J. Shearer, G. Shore, and data from H.A. Simon Ltd.

Dated at Vancouver this 25th day of February, 1986.

S. Gardiner

VICTORIA

FAME REPORT (E161) 15759

Province of British Columbia

Ministry of Energy, Mines and Petroleum Resources

173

TYPE OF REPORT/SURVEY(S): GEOPHYSICAL; GEOLOGICAL 164,649.15

AUTHOR(S): J.T. Shearer, G.A. Shore, S.L. Gardiner

SIGNATURE(S):

DATE STATEMENT OF EXPLORATION AND DEVELOPMENT FILED: Feb. 26 /87

YEAR OF WORK: 1986

PROPERTY NAME(S): YELLOW GIANT

COMMODITIES PRESENT: Au, Ag, Zn, Pb, Cu

B.C. MINERAL INVENTORY NUMBER(S), IF KNOWN: 103G - 26

MINING DIVISION: Skeena

NTS: 103G/8E

LATITUDE: 53°21'57"

LONGITUDE: 130°9'38"

NAMES and NUMBERS of all mineral tenures in good standing (when work was done) that form the property [Examples: ... (12 units); PHOENIX (Lot 1706); Mineral Lease M 123; Mining or Certified Mining Lease ML 12 (claims involved)]:

Yellow Giant 3

OWNER(S):

(1) Trader Resource Corp.

(2)

MAILING ADDRESS:

OPERATOR(S) [that is, Company paying for the work]:

(1) as above

(2)

MAILING ADDRESS:

SUMMARY GEOLOGY (lithology, age, structure, alteration, mineralization, size, and attitude):

On the west flank of the Coast Plutonic Complex, northwest trending granitic bodies are separated by narrow, but persistent belts of sedimentary rocks. The Tel Deposit belongs to a series of high grade veins that are controlled by faults and replacement zones within the metasedimentary rock. The section is cut by many faults and shears. The main host rocks are banded grey marble and silty thin bedded marble in the unaltered and altered slates.

REFERENCES TO PREVIOUS WORK:

A.R. 12719, 14171

TYPE OF WORK IN THIS REPORT	EXTENT OF WORK (IN METRIC UNITS)	ON WHICH CLAIMS	COST APPORTIONED
GEOLOGICAL (scale, area)	1:5000 1000 ha		
Ground GEOL	1:250 37		
Photo			
GEOPHYSICAL (line kilometres)	1:500		
Ground			
Magnetic			
Electromagnetic		Yellow Giant 3	
Induced Polarization IPOL	7.0 km 1:500		
Radiometric			
Seismic			
Other			
Airborne			
GEOCHEMICAL (number of samples analysed for ...)			
Soil			
Silt			
Rock			
Other			
DRILLING (total metres; number of holes, size)			
Core			
Non-core			
RELATED TECHNICAL			
Sampling/assaying			
Petrographic			
Mineralogic			
Metallurgic			
PROSPECTING (scale, area)			
PREPARATORY/PHYSICAL			
Legal surveys (scale, area)			
Topographic (scale, area)			
Photogrammetric (scale, area)		"	
Line/grid (kilometres) LINE	7.9 km		
Road, local access (kilometres)			
Trench (metres)			
Underground (metres)			
		TOTAL COST	164,649.15

FOR MINISTRY USE ONLY	NAME OF PAC ACCOUNT	DEBIT	CREDIT	REMARKS:
Value work done (from report) 164,649.15				
Value of work approved				
Value claimed (from statement)				
Value credited to PAC account				
Value debited to PAC account				
Accepted ... Date Feb.26/88	Rept. No. 15759			Information Class (3)