#### SUMMARY REPORT

OF

GEOLOGICAL, GEOPHYSICAL AND OTHER STUDIES

ON THE

TEL DEPOSIT

YELLOW GIANT PROJECT

BANKS ISLAND

NTS 103G/8, 53°22'00", 130°09'45"

SKEENA MINING DIVISION

FROM JUNE 1986 TO FEBRUARY 1987

FOR

.

TRADER MINES LTD.

ВΥ

J.T. SHEARER, M.Sc., FGAC.

FILMED

G.A. SHORE, Ph.D. S.L. GARDINER, B.Sc., FGAC. GEOLOGICAL BRANCH ASSESSMENT REPORT

FAME Project No 10962E-161 10

February 26, 1987 Vancouver, B.C.

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#### SUMMARY

- (1) The Tel Deposit is located on central Banks Island, 118 km south of Prince Rupert. Access is by boat or float plane.
- (2) The original Tel 23-32 claims were staked by J.W. MacLeod on July 1, 1963 for McIntyre Porcupine Mines Limited to cover a portion of the metasedimentary belt indicated by aerial photographs to parallel the Discovery Zone belt.
- (3) The surface showing was discovered by A.E. Angus in late September 1963. Trenching and additional prospecting was completed by November 1963.
- (4) Geological mapping, diamond drilling and geophysical surveys were conducted by McIntyre from February to October 1964 indicating a small, high-grade gold deposit to the -50 foot level.
- (5) Deeper diamond drilling, also under the supervision of J.W. MacLeod, was done in 1975 by Sproatt Silver Mines Ltd. McIntyre sold the Tel claims to Sproatt for \$10,000. An IP survey was also conducted.
- (6) The results of the 1975 drilling included hole 75B-6 in which 47 feet averaged 1.48 oz/ton gold. This mineralized zone could not be confidently correlated to other zones of similar thickness.
- (7) Trader Resource Corp. optioned the entire property in 1983.
- (8) After geological mapping and revaluation of the Tel Area by Trader, a major extension of the previously known zone was discovered on October 10, 1985.
- (9) Subsequently, a large drill program was completed by Trader between November 1985 and March 1986 to bring the total drilling on the Tel Deposit to 33,679.5 feet (10,265.51 m) in 91 holes.

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- (10) The Tel Deposit is composed mainly of a deformed, massive sulfide assemblage of pyrite-arsenopyritesphalerite. Of lesser importance is late-stage, drusy quartz-pyrite mineralization.
- (11) The main rock types are banded grey marble and silty thin-bedded marble. Common host rock strike and dip orientation is 324°/55° E.
- (12) Narrow dioritic dykes and sills of variable composition occur throughout the Tel Area. Zircon U/Pb dating gives an age for these dykes of 123 Ma.
- (13) The minor fold style is tight isoclinal plunging 45° north and south. Regional tectonic effects suggest that large scale plastic flowage and drag could result in steep plunges of the major folds.
- (14) A large scale fold which can be traced from Hepler Creek north to Sproatt Lake is named the Tel Antiform. Its axial plane trends 310°/55° E with an overall width of at least 180 m.
- (15) A major fault-shear structure, the McIntyre Fault, now defines the east contact between banded grey marble and silty thin-bedded marble. It is sometimes marked by the "East Limb" of the Tel Deposit and is oriented 320°/60° E. The McIntyre Fault is sub-parallel to the Bank-Barge Lineament and may be a subsidiary splay.
- (16) The Tel Fault cross-cuts the regional grain and trends 277°/75° E. The Tel Fault is filled with lowgrade, late-stage quartz and appears to offset the massive sulfide zones.
- (17) All geological, assay and survey information has been computerized on both the Simons and Wright systems. Mineral inventory and ore reserve calculations for gold were made in May 1986.

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- (18) In July 1986 results from analyses for silver, arsenic, copper, lead, zinc, iron and sulphur for all mineralized drill intersections were added to the Simons data bank. Grade composites were calculated and contoured plans for six elements and iron sulphide were generated for elevations at 50m intervals within the deposit.
- (19) Broad zones of higher grade values for all elements and iron sulphide are outlined on plans for Om to -50m and -50 to -100m elevations.
- (20) Elevated values of iron sulphide and/or zinc are most commonly associated with higher gold grade.
- (21) Premier Geophysics Inc. conducted a series of E-SCAN induced polarization and resistivity surveys over the known Tel ore zones in June 1986. Coverage was extended to the north and southeast during the October to December 1986 survey.
- (22) The Tel sulphide/gold ore mineralization has a distinct E-SCAN IP signature within a marble rock unit environment.
- (23) The lateral boundary of the E-SCAN IP anomaly correlates very closely with most of the drillindicated ore boundary. Where the E-SCAN boundary extends beyond the limit of drill-indicated ore, it is found that the ore limits are also open in that direction - that is, the area in question is not yet drill-tested.
- (24) The marble units (silty thin bedded, and grey banded) have a distinct background IP and resistivity signature which distinguishes them from the adjacent graphitic argillites.
- (25) Mise a la masse resistivity can be useful in projecting ore zone orientation from deep ore intersection in drill holes.
- Tel and near thezone have (26) E-SCAN surveys on accurately outlined the known Tel ore zone, and mapped six new anomalous areas within 250 meters of the Tel Drilling of three of these anomalies and ore zone. faulthas been common, connecting zone their anomalies lie in The other three recommended. different geologic conditions and warrant further mapping and investigation prior to drilling.

#### INTRODUCTION

This report is a summary of three programs that were carried out during the period of June, 1986 to February, 1987 under the Financial Assistance for Mineral Exploration program. Prior to this time diamond drilling and geological information obtained from previous programs was entered into the H.A. Simons Ltd, and Wright Engineers Computor Systems. Ore reserve calculation, based on gold only were performed by Simons, Wright and Montgomery Consultants Ltd, using three different methods.

In June 1986 detailed geological mapping was done in the area of the Tel Deposit. The information derived from this study was combined with the data from diamond drilling and used to develope a model for the Tel.

A powerful, innovative geophysical system, named E-SCAN, was used to conduct an orientation survey over the Tel area in June 1986. Follow-up surveys were carried out during the months from October to December, 1986.

Analyses for seven other elements from mineralized intersections from diamond drilling were added to the Simons data file for the Tel Deposit. Contoured plots showing grade composites for gold, silver, arsenic, copper, lead, zinc and iron sulphide were generated.



Fig.1 Tag

## PROPERTY (CLAIM STATUS)

The Tel Deposit is covered by one 20 unit Modified Grid System (MGS) mineral claim, Figure 3, as tabulated below:

## TABLE I

## List of Claims

<u>Claim Name</u>	<u>Units</u>	Size	Record <u>Number</u>	Record Date	Expiry Date
Yellow Giant 3	20	5W x 4S	3889	June 15/83	1995

The entire area covering favourable geology and including the proposed mill site is listed in Table II.

#### TABLE II

List of Claims Covering Favourable Geology, Tel Area

<u>Claim Name</u>	Individual Units	Record <u>Number</u>	Record Date	Expiry Date
Yellow Giant 3	3, 4, 13 and south half of 14	3889	June 15/83	June 15/95
Yellow Giant 4	4,13	3890	June 15/83	<b>June 15/</b> 95
Yellow Giant 6	27, 28, 29, 30, 32, 33, and 34	3892	June 15/83	<b>June 15/</b> 95
Yellow Giant 9	Fr south half	4443	Mav 8/84	Mav 8/95

The original Tel 23, 24, 37 and 38 two-post claims of McIntyre Porcupine Mines Ltd. were abandoned under the provision of the Mineral Act, Section 28(1), and relocated under the Modified Grid System (Mineral Act, Section 28(3)). This property consolidation eliminates the many problems associated with the old two-post system regarding filing assessment, grouping, anniversary dates and multiple fractions.



A11 new claims were recorded in the names of Host Ventures Falconbridge Nickel Mines. Host Ventures (which became and Hot Resources Ltd. and is now, as of February 11, 1985, Inter-Globe Resources Ltd.) optioned the property to United Mineral Services Ltd. by an agreement dated May 16, 1983. Mineral This agreement was assigned to Trader Resource Corp., who further assigned its rights to a wholly owned subsidiary, Trader Mines Ltd. Through continued exploration Trader Mines Ltd. now owns an 80% interest in Ltd. expenditures, the Yellow Giant Property and can eventually become the 100% owner pursuant to the option agreement.

The legal corner posts (LCP) of each claim were surveyed by McElhanney Group Ltd. with the grid location as follows:

(a) Yellow Giant 1, 2 and 3: 32,297.89 N + 28,441.98 E
(b) Yellow Giant 4, 5, 6, 7: 30,326.07 N + 30,460.51 E

#### LOCATION AND ACCESS

The Claim Group is situated on south central Banks Island, 112 km south of Prince Rupert, Figure 1. Banks Island is about 70 km long by 20 km wide. The nearest communities are Hartley Bay 60 km east on the mainland, Kitkatla, 52 km to the north and Trutch, 45 km southeast. Kitimat is 120 km northeast of the property. Directly west is Sandspit on the Queen Charlotte Islands, a distance of 110 km.

Bonilla Island weather station is located off the northwest side of Banks Island. B.C. Telephone maintains a close network of repeater stations to service the commercial fishing fleet and local villages. The best communication on Banks Island is via the Noble Mountain FM channel, although satellite receivers will be phased in over the next few years.

Access is mainly by float-equipped, fixed-wing aircraft to the main camp on Hepler Lake, Figure 2. Heavy equipment is barged to Survey Bay. The barge site is 2.1 km by rough tote road west of the Bob Zone where a 15% decline ramp was driven in 1977. A 2.2 km proposed road right-of-way has been slashed out from Indian Bay to the Tel Zone. Helicopter transportation has been important in the past and there are many natural open spots suitable for landing.

The area is characterized by coastal muskeg over the granitic rocks and by lush cedar-hemlock forests over the narrow metasedimentary belts. The main claims cover mostly undulating lowlands (Hecate lowland) with relief generally less than 50 m. To the east and north the terrain becomes progressively more rugged towards the Carlo Range, whose high point, on Mount Grannell, is 676 m.

## HISTORY

The Tel 23 to 32 two-post claims were located by J.W. MacLeod on July 1, 1963 (recorded July 12, 1963) for McIntyre Porcupine Mines Ltd. Mr. MacLeod had been attracted to Banks Island as a result of high grade gold values intersected by Falconbridge Nickel Mines Ltd. in the April 1963 diamond drilling on the Discovery Deposit. Hole LY-2 on Discovery Zone averaged 0.719 oz/ton gold, 1.86 oz/ton silver and 0.25% copper over 50.0 feet (15.24 m). McIntyre had recently purchased a controlling interest in Falconbridge and was thus privy to such confidential information.

Falconbridge (formerly Ventures Ltd.) prospectors M. Hepler and S. Bridcut, under the direction of J.J. McDougall, the Banker 1-4 claims to cover the Discovery Zone located in 1960. Initial exploration focussed along themetasedimentary belts in the vicinity of intersecting lineaments. Little work was done on Banks Island airphoto or 1962 due to commitments at the Catface porphyry in 1961 copper deposit. Several important discoveries were made in 1963 by Falconbridge including the Kim, Bob, Englishman, Keech and Crossbreak Zones.

Prior to locating the Main Tel Zone, J.W. MacLeod staked two other groups as tie-on to the Falconbridge ground. These were Tel 1-10 (North Group) to cover ground along the expected strike of the central metasedimentary belt north of Gladys Lake and along the east shore of West Banks Lake. Tel 11-22 (East Group) were located between Crazy Lake and Kim Zone. As a humourous wordplay on the Bank-Banker claims, MacLeod chose Teller (as in cashier) shortened to "Tel" as the name for his new claims. The Main Tel Zone (claims Tel 23 to 32 called the West Group) were staked to cover a portion of the metasedimentary belt indicated by aerial photographs to parallel the Discovery Zone belt. Subsequently, Falconbridge staked around the Tel 23-32 claims on three sides.

Detail prospecting by A.E. Angus and M. McQuire started on Tel in August 1963 and continued in two phases the claims the of November. Mr. Angus was later assisted into month by prospector Alfie Teed. During late September the main showing was found shortly before the program ended. Tel A gossanous assaying 1 to 3 oz/ton gold was found by zone within a lightly overburdened area near the A.E. Angus of what is now called Sproatt Lake. By November, shoreline stripping and rock trenching indicated that the massive sulfide zone (Main Zone) to be 30 feet long by 7 feet wide "finger out" quite abruptly at both ends and "down and to dip" (Hubacheck, 1963). The West Tel Zone was the second showing to be found (No. 2 showing). It occurs in a creek bed about 500' northwest of the No. 1 showing (Main Tel Zone). Hubacheck (1963) describes the West Tel Zone as follows:

"Considerable stripping and rock trenching has been in this area, exposing two intersecting bands of done mineralization. The main band consists of a mineralfault breccia about two feet wide in an east-west ized trending fault zone, which has now been opened up for 50'. The other consists of a band of а length of sulphides limestone in one foot wide striking and northwest dipping steeply to the northeast. The sulphide mineralization is similar to that of the No. 1 showing but not nearly as heavily concentrated.

Sampling results from the east-west fault breccia zone were as follows: 0.76 oz gold over 2.0' at the west end of the showing (heavy sulphides), 0.08 oz gold over 1.2' near the centre, and 0.04 oz gold over 1.5' near the east end. The mineralized limestone assayed 0.12 oz gold over 1.0'.

Both zones are open on strike."

After the Tel Main Zone discovery, two additional claims, Tel 37 and 38, were staked on October 7, 1963 (recorded October 17, 1963) to fill the gap between Tel 23 and 24 north to Banker 146 and 147. The Banker 146 and 147 were located on July 9, 1963.

Geophysical orientation surveys were carried out over the These consisted of self-potential (SP), Tel Main area. Magniphase horizontal-loop electromagnetic and Rhonka E.M. 15 Reconnaissance self-potential results indicated units. the presence of the No. 4 zone which is now referred to as Central Tel Zone. SP values also show anomalous trends in 1985 to be the northwest over what was discovered continuation of the Tel Main Zone.

1964 a program of geological mapping was conducted by In McLeod and J.H. Evans. This resulted in two 1" = 40' J.W. sketch maps around the showings and a generalized (1:480)= 200' (1:2400) property geology map between Sproatt and 1" Witness Lake. A 26 hole packsack diamond drill program was completed in 1964. All the drill holes were near the for holes 13, 15 and 16. showings except Total footage of 12, 14 and 17 to 26 is 1465 feet (446.53 m). P1 holes to The SP anomalies obtained over the graphitic Banks-Barge lineament were investigated by holes P-13, P-15 and P-16 m)), and by trenches 1 to 12, (totalling 259 feet (78.94 excluding 7.

Work by McIntyre Porcupine Mines Ltd. up to 1964 resulted in following conclusions (McLeod, 1964, page 9).

"The West Zone (Map No. 6) is believed to be primarily due to a quartz vein or a series of quartz veins carrying sulfides and appreciable gold values. Where opening occupied by the quartz crosses a favourthe That is, able situation a replacement zone is found. end of the zone consists of massive sulfides the east replacing limestone. This portion of the zone is 50 long and averages 1.18 ounces gold over a width feet of 8.5 feet in five holes drilled under the zone. TO west for 150 feet the zone is indicated by quartz the out of 5 holes where the 4.5 feet. The gold values vein intersections in 4 widths vary from 1.5 to to 1.56 for these intersections but from 0.20 range considered true values becuase of the poor are notFor 200 feet to the west no zone has core recovery. been indicated by drilling 4 holes at 50 foot zone is again picked up by holes 10, intervals. The 11, 12 and 19 for a length of 120 feet, but again core recovery was very poor. In one of these the wide intersection of 6.8 feet is due to the inclusion in zone of 3.5 feet of replacement type mineral. the A granite dike is found in hole 20 at the anticipated Mineralization of both the vein vein intersection. and replacement types is poorly exposed 300 feet west of hole 20 at 10 300 N. There is a possibility that the faulted extension of the West Zone. this is Two to drill this area were frustrated by caving attempts ground."

The claims were dormant between 1964 and 1975. Tel Α change McIntyre Porcupine Mines in senior management at Ltd. 1974 resulted in the new president, R.B. Fulton, in arranging the sale of the original McIntyre Gold Mine (a continuous producer since 1912) and the cancellation of the Warman option (to become shortly thereafter the Northair Mine). Gold These changes consequently allowed D.A. MacLeod to arrange the option of the Tel Claims from McIntyre. In a letter dated May 27, 1975, R.B. Fulton confirms the outright sale of Tel 23, 24, 37 and 38 to Sproatt Silver Mines Ltd. for \$10,000 payable on or before June 15, 1975.

Technical data were summarized by R.H. Seraphim in his six page report (June 6, 1975) which proposed a 1,000 foot diamond drill program. Diamond drilling by Sproatt Silver Mines Ltd. began on September 30, 1975 and finished on November 22, 1975. The drill program was planned by J.W. who closely supervised site-geologist D. Peel. MacLeod. 75B-1 and 75B-2 investigated the West Tel Zone by Holes along the strike of the enclosing silty thin arble. Holes 75B-3, 75B-4 and 75B-17 were collared drilling bedded marble. Central Tel Zone and also were directed around thesubparallel to the general strike of the banded grey One of them, 75B-4, provided twenty feet of sludge marble. which assayed 0.95 ounces gold.

The first 1975 hole through the Main Tel Zone was 75B-5 which intersected directly under the surface exposure 5.04 ounces gold across one foot of core length.

Seraphim (1975b) reports that:

"The best new intercept, in hole B-6, assayed 1.47 ounces gold, 1 ounce silver, and 2.73 percent zinc. True width is approximately 20 feet and depth below surface approximately 100 feet." However, in another report dated one week later, Seraphim (1975c) reports about hole 75B-6 that:

"True width is not known, but holes 7, 8 and 9, drilled into the same area but in opposite direction, each intersected only one to two feet of sulphides."

apparent general concensus in 1975 concerning hole The 75B-6 was that, in the absence of a straightforward, simple explanation to correlate the 47 foot zone of mineralization penetrated by B-6, the information provided by holes 75B-7, indicated that the less than 2 feet 8 and 9 zone was Essentially the results of hole 75B-6 were thick. Drillholes 75B-10 to 75B-16 were collared mainly ignored. the southeast of 75B-6 with confusing results. In 1976 to Sproatt Silver Mines Ltd. (later Hecate Gold Corp.) was to option the Falconbridge ground. able Exploration emphasis was changed toward the Bob Zone, where a major underground exploration program was conducted in 1977-1978.

The complexities of the Tel Zone environment were not recognized by Sproatt Silver Mines Ltd. This is graphically illustrated by examining the large mineralized intersections in drillhole YGTL-85-012. This hole was collared from the same set-up as holes 75B-7, 8 and 9 trending in the same general direction as 75B-8. The narrow intersection found in hole 75B-8 was the East Limb and the larger Central and West limbs would have been found in 1975 if hole 75B-8 was allowed to extend into the second banded grey marble unit.

In June 1975, limited orientation soil sampling was undertaken by B. Manchuk for Falconbridge. The samples were analyzed for zinc, silver and arsenic. Results show strongly anomalous values in all three elements in an east-west direction between the Main Tel Zone and West Tel Zone.

In October 1975, Induced Polarization (IP) and VLF EM surveys were completed by G.E. White Geophysical Inc. The IP chargeability map for N=3 shows a moderate northwest trending anomaly. VLF results did not locate any anomalous conductive responses.

Between November 1975 and June 1984 no further work was done on the Tel Zone. A report written by J.B. Magee and R.H. Seraphim (1977) stated that:

"However, accurate evaluation is precluded Ъv inadequate core recovery in crumbly sulphides, acute of drill intercepts to lode dip, and angles an 'population' drill insufficient of intercepts. Α decline tunnel is recommended initially on either the the Tel Zone to determine the average grade --Bob or length and, if possible, the plunge of the best width. mineralization. The choice of which shoot to test first is in part upon access from harbour dependent sites. The determination of the best harbour and the easiest road route across the mile or two thence of flat terraine is currently in progress."

Hecate Gold Corp. experienced financial difficulties at the time the Bob Zone program was only partially completed, and the planned underground work on Tel Zone was never started (Shearer, 1985a).

From the end of the Bob Zone underground drilling in June 1978. the entire property lay idle until 1983. In 1983, Trader Resource Corp., through United Mineral Services Ltd., concluded an option agreement with Host Ventures Ltd. (successor company to Hecate Gold Corp.). After a claim 1983 a comprehensive "Prefeasibility relocation in June Study" was compiled from all available data including: mineralogy, photo-structural geology, analysis, geochemistry, geophysics, ore reserves, metallurgy, mine mill waste disposal, hydro potential, identification of and environmental and legislative considerations, capital and operating cost analysis and predevelopment program cost estimate.

International Geosystems Corporation (IGC) calculated, in the "Prefeasibility Study", ore reserves for the Main Tel Area by the inverse distance method as 24,000 short tons averaging 0.914 oz/ton gold equivalent, based on 1964 and 1975 drill results. Errors in hole potting in the Tel computer calculations appear to have increased the zone length by about 30% (Shearer, 1985b).

the Banks Island claims by Trader Resource Field work on started on February 18, 1984. Later in June and July Corp. R. Kidlark was assigned to conduct geological mapping 1984. and generally evaluate the Western Metasedimentary Belt, which included the Bob, Tel, Crossbreak and Foul Bay Bay Zones. overall geological map at 1:2500 was produced, An conjunction in with 1:500 mapping around the main The majority of 1975 drill core was relogged by showings. J. Shearer and R. Kidlark. This core was subsequently moved to the main core storage facilities at Beaver Lakes. the Kidlark work focussed on locating and defining Much of source of airborne (Dighem) geophysical anomalies, the theresults of a survey flown in March 1984. To complement the soil samples were collected over the geological mapping, entire area and analyzed for gold.

drilling by Trader Resource Corp. in October 1985 Diamond led tothe discovery of a major extension of the Tel Zone, the surface showing.  $\mathbf{at}$ depth, northwest of A large drilling program between November 1985 and March 1986 related mineralized zones. delineated several Total diamond drilling on the main Tel area is 33,679.5 feet (10,265.5 meters) in 91 holes. Metallurgical testing, conceptual mine planning, mineralography, rock geochemistry, milldesign, rock stress analysis, modular access road design, marine infrastructure investigations environmental baseline sampling were initiated as the and success of the drilling program became apparent.

Mineral inventory and ore reserve calculations by different methods were undertaken by several independent groups Simons Consulting Engineers (Wright Engineers Ltd., H.A. Ltd.). Montgomery Consultants Mineral and inventory calculations by Simons Ltd. based only on the vertical cross-sectional model are:

Drill Proven + Probable Reserves 238,140 short tons averaging 0.78 oz/ton gold

mapping, geophysical This report summarizes geological and additional computer data manipulations carried surveys the Tel Deposit since the mineral inventory in June out on The geological information is also included in the 1986. "Geological Summary Report on the Tel Deposit, Banks report Island" by J.T. Shearer, July 1986. For а detailed description of the reserve calculations and discussion of engineering studies the reader is referred to that report.

#### FIELD PROCEDURES

legal corner posts (LCP) were surveyed by McElhanney The Group Ltd. who also accurately established a number of the claims. designated throughout points A metric coordinate system was calculated based on station "Camp" which was designated 30,480.00 N and 30,480.00 E (H-44), (elevation 36.30 m) to facilitate correlation with work done since 1960. These points provided the data base on which all 1984 to 1986 transit, steel chain and EDM work is related.

for the Tel Area, a transit and EDM traverse was Initially, accurately closed which tied in old diamond drill holes, trenches and some surface contours. Close-spaced transit EDM measurements were used as a base for 1:250 and All diamond drill hole collars were geological mapping. picked-up by chain and transit. Hole deviation during drilling, both dip and azimuth, was recorded with a Sperry-Sun single shot, type B instrument.

In preparation for the E-SCAN geophysical survey, a grid was flagged and blazed along lines as shown in Appendix I, Figure 2. The lines were tied in to the main Tel baseline by an EDM survey.

#### GEOLOGY

## I. REGIONAL GEOLOGY

Regional geological features have been compiled by Roddick (1970) as Map 23-1970, Figure 4, mainly from field work conducted by the Geological Survey of Canada in 1963 along coastal exposures and in 1964 by very wide spaced landings with a helicopter on interior sites.

Banks Island lies along the western edge of a long, relatively narrow belt of plutonic and metamorphic rocks called the Coast Plutonic Complex. This forms one of the major geological components of British Columbia, extending from northern Washington through the Coast Mountains into southeast Alaska and Yukon Territory. General descriptions of the Complex have been given by Roddick and Hutchinson (1974) and Woodsworth and Roddick (1977). The following overview is taken mainly from these sources.

Recent interpretations of the western Cordillera (Monger and Irving, 1980) have identified several major terranes which have been accreted to the North American craton by transcurrent faulting and subduction. Banks Island metasedimentary rocks belong to the Alexander terrane.

The Alexander terrane in adjacent less deformed southeast composed of Carboniferous carbonate and clastic Alaska is sediments unconformably overlain by Upper Triassic limestone and Lower Middle and Jurassic felsic tointermediate volcanic rocks.

Coast Plutonic Complex consists largely of intermediate The and basic discrete and coalescing granitoid plutons, bodies of gneiss - migmatite and pendants (septa) of metasediments and volcanics. It is an asymmetric array, with a central s core flanked by diorite and dioritic migmatites, plentiful in the west, and granodiorite and quartz gneiss most monzonite, most common in the east. Metamorphic intensity increases from greenschist facies in the eastern part of belt to amphibolite (locally granulite) facies in the the and east-central parts. central Woodsworth and Roddick (1977) suggest that most of the plutons in the Coast Mountains have been emplaced as diapiric solids, analgous to glacier flow and salt domes. Many contacts between plutons and pendants are faults or drag folds formed during formation of the igneous bodies. Some faults have been healed by re-crystallization. The clearest examples of "solid" movement of plutons are the several "tadpole"shaped that intrusions have gradational to intricate their "tails". contacts along When the rock was more solid. movement could only take place by re-crystallization flowage, and this gave rise to internal foliation within the pluton. Commonly the quartz diorite and granodiorite are rarely uniform over broad areas. Zones of migmatite small, lensoid amphibolitic inclusions are ubiquitous and but variable in abundance.



main intrusive period lasted through most The of the Cretaceous from about 120 Ma (million years ago) to 85 Ma, but was followed by two discrete later pulses at 70  $\pm$  10 Ma, and 50 + 5 Ma. The plutonism is widely regarded as evidence of heat generation on collision and suturing of outboard terranes (Wrangellia and Alexander) on the the inboard (Stikinia). Study of the metamorphic hosts, now evident as pendants and inliers, and which may be both intruded and protolith, enables tentative identification from the ghost stratigraphy of the terrane of origin. In the study area most inliers south of Burke Channel can be assigned a Wrangellian origin. North of Burke Channel and west of Work Channel lineament, inliers and pendants are fairly certaintly part of Alexander terrane whereas east of lineament they appear to be part of Stikinia. The nent Central Gneiss Complex (Tracy Arm) may be a the prominent Central highly deformed and metamorphosed amalgam of Stikinia and Alexander terranes unconformably overlain by an overlap assemblage equivalent to the Gravina-Nutzotin rocks of southeast Alaska.

Roddick (1970)reports that contact relationships everywhere indicate the more acid plutonic rock to be younger than any more basic plutonic rock in contact with but isotopic ages are related to the position of the it, plutons across the belt. Isotopic ages range from Early in the west to Late Cretaceous near the axis of Cretaceous the crystalline belt to Tertiary on the east side. The Time following Chart has been compiled to assist in correlation of the mineralizing events.

The central part of Banks Island is underlain by Unit 10b, Figure 4, a biotite-hornblende quartz monzonite. Surrounding rocks are hornblende-biotite granodiorite To the east and west are large bodies of (unit 9c). hornblende-biotite quartz diorite (unit 8b). Basic. complexes (unit 5b) flank gneiss-diorite-migmatite thequartz diorite. This outward zoning from a felsic core to progressively more basic rocks supports a conclusion from the detail petrographic work that intrusive rocks on Banks Island are inter-related and are part of the same zoned The field observations, discussed under Local pluton. Geology, reflect the complexities along the contacts between major phases.



Metasedimentary rocks are exposed over about 7% of Banks Island. They probably correlate with either the Dunira Formation of Early to Middle Pennsylvanian age (Woodsworth and Orchard, 1985) or Upper (Norian) Triassic Randall Formation exposed on the less metamorphosed islands northwest of Prince Rupert. On Banks Island the metasedimentary rocks are contained mainly in long, narrow northwesterly trending belts. The longest metasedimentary belt, from Banks Lake to Keecha Lake is 18 km in length. North of Waller Lake this Banks-Keecha belt splits into two arms which is the probable result of large scale folding.

It is this area of the Island, together with the parallel sedimentary belt from Foul Bay (Waller Bay) to Bob Zone, that the attention has focussed in the Yellow Giant Project.

# TIME CHART

## Tel Deposit Western Coast Plutonic Complex

TIME	NAME or EVENT	REMARKS
Upp <b>er tertiary</b> to <b>recent</b> glaciation	Isostatic rebound	Oxidation of sulfides
50 <b>Ma</b>	Intrusive event	
Eo <b>cene</b>	Uplift of Coast Mountain core oblique subduction	Northeast dipping thrust faults
70 <b>Ma</b>	Intrusive event	
Tertiary		
85 Ma (80 Ma:k/Ar mineralized	date on Sericite from Surf Inlet as shear zone)	sociated with
Upp <b>er</b> Cret <b>aceous</b>	Major transcurrent fault movement of up to 300 km, right lateral	Major faulting/ drag folding
Cre <b>taceous</b>	Formation of Coast Plutonic Complex. Major intrusive event.	Intrusion of diorite/ monzonite
120 Ma <b>(123 Ma:- Z</b> sericite -	ircon date of Tel Zone diorite sill associated with late-stage quartz-p	and k/Ar date of Kim Zone yrite veining)
Jur <b>assic</b>	Randall Formation limestone-dolostone	
	Upper Triassic intrusions (Windy-Craggy)	Possible first phase pyrite mineralization at Tel Zone
Triassic- Jurassic	Suture of Alexander and Wrangellia terranes into one superterrane	
Early Triassic	Erosional unconformity	(possible karst/solution collapse at Tel Zone)
Early to Middle Pennslvvanian	Dunira Formation equivalent. Marble and shale.	Deposition of Tel Zone host rocks.

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Plutonic Belt the early structures of the Τn the Coast largely obliterated. However, the Work terranes are Lineament and/or the western edge of the Central Channel originated as the suture of Gneiss Complex probably against Stikinia. The discovery of Alexander terrane aircraft assisted mineralization resulted from aninvestigate north coast prospecting program designed to(McDougall, 1972). Banks Island has an unusual lineaments of faults, fractures and lineaments. The Island is density bounded by deep seated, major faults that are assumed to have right-lateral displacement.

(1983) has carried out a preliminary analysis of Blanchet Two major, right lateral faults with an airphoto linears. 310° are recognized: (1) Arseno Fault average trend of through Arseno Lake; and (2) Hepler Fault which passes through Hepler Lake. A very common direction which passes 045° which Blanchet attributes to for linears is thethe 310° 090° with 310° trending faults. Left lateral movement along trend important examples being the faults Bay linear and Crossbreak. At the Kim Zone Area the Survey 045° linears are seen to offset the older 090° faults.

#### **II. LOCAL GEOLOGY**

general geological setting of the Tel area is composed The a northwest trending metasedimentary assemblage dipping of (55°-75°) northeasterly. moderately steeply This tois part of a series of septa which are bordered assemblage the northeast by hornblende quartz diorite and on the on by diorite and quartz monzonite. These major southwest contacts take the form of Lit-par Lit injection intrusive Elsewhere, at the Discovery Zone, and magmatic stoping. diamond drilling has indicated that the edges of these deep septa are defined by near vertical major metasedimentary shallow "roof pendants" but The septa are not faults. rather are associated with deep reaching structures.

#### (a) <u>Lithology</u>

The internal stratigraphy is remarkably consistent throughout all the metasedimentary belts although major

large scale folding and faulting has caused complex repetition of some rock units. The stratigraphic sequence at the Tel Zone, as derived from extensive diamond drilling and surface mapping, is from east to west as follows:

#### TABLE III

#### Tel Zone Stratigraphy

UNIT		APPROXIMATE THICKNESS
(i) (ii)	Hornblende diorite, coarse crystalline Altered Marble, skarnified	intrusive 2-5 m
(iii)	Argillite-siltstone hornfels	5 m
(iv)	Altered Marble, skarnified	4-6 m
(v)	Siltstone-argillite hornfels	approx 30 m
$\langle \alpha \rangle$	(Magmatic stoping/Lit par Lit)	
(8)	Hornblende diorite, coarse crystalline	intrusive
	laminated black argillite	27 m
(2)	argillaceous marble and	5 6 m
(iv)	BANK-BADGE Foult Zone	5.0 m
$(1 \vee)$	banded grew marble	30 m
(+)	usually f	ault contact
(2)	silty thin bedded marble	29 m
$(\dot{4})$	banded grev marble	39 m
(3+4)	folded section with intrusive	
	dykes, silty and banded grey marble	5-10 m
(3)	siltstone (part of folded section)	2 m
(2)	silty thin bedded marble,	
	also hornfels fragments	30 m
(8)	diorite, coarse crystalline	intrusive
(vi)	argillite-siltstone hornfels (Magmatic stoping/Lit par Lit)	> 50 m
(9)	Quartz monzonite, coarse crystalline	intrusive

This sequence now represents approximately 270 m of section but allowing for fold repetitions the original thickness was probably in the order of 150 meters.

A very accurate surface detail geology map (Figure 6A) was prepared in June 1986 at a scale of 1:250 based on numerous transit and EDM reference points. (Figure 7 is a 1:500 which is at the same scale as all other figures included in this report). The most abundant rock type in the Tel area is unit 4, banded grey marble. This unit as a whole weathers light grey and is usually well exposed within a small scale, moss covered karst topography. On fresh surfaces the main component is white calcite of Bedding (banding) is prominent in variable grain size. most exposures although where coarse recrystallization has occurred the thicker, dark grey bands tend to be obscured. Thin delicate layering was consistently noted in the banded marble on the northeast margin of the deposit. grey This sub unit can be mapped at 1:250 scale and was named "unaltered banded grey marble". The contact between "unaltered" banded grey marble and the more typical slightly altered, banded grey marble appears to be an alteration feature related to faulting and dyke intrusion.

The second most abundant rock type in the Tel area is unit 2, silty thin-bedded marble. Unit 2 is generally recessive weathering and forms small scattered exposures. Many of the natural outcrops are under roots or around windfalls. The unit is commonly rusty weathering. Near the McIntyre Fault, unit 2 is commonly very altered and brecciated. Silty thin bedded marble is composed of alternating recrystallized pure carbonate layers and laminated silty sequences usually between 0.5 to 3 cm thick. Hornfelsed unit 2 is common on the east and west margins of the metasedimentary belt.

section of very pyritic, thinly laminated thick A unit 6, occurs east of the Bank-Barge argillite, It is a rock composed of alternating black and Lineament. dark grey laminations 1 to 4 mm thick. There are minor silty lenses. Abundant pyrite up to 20% is distributed in micro-lenses disseminations parallel and to bedding laminations. Some sections are very graphitic.

Unit 5, calcareous argillite and argillaceous marble, has not been seen in outcrop since it occurs under Sproatt Lake in close proximity to the Bank-Barge fault. It appears to be a conformable transition facies between the open marine deposition of the banded grey marble and the largely terrigeneous provenance of the thinly laminated argillite. Fault attenuation has resulted in variable thicknesses for each element of unit 5 as shown below:

Unit 5a argillaceous marble hole 85-004 1.2 m true thickness hole 85-005 4.2 m true thickness calcareous argillite hole 85-004 4.4 m true thickness hole 85-005 1.6 m true thickness A narrow, distinctive siltstone bed, unit 3, dark grey siltstone, may be useful in the future as a marker horizon. It has been noted in the following diamond drillholes:

#### TABLE IV

#### Dark Grey Siltstone Marker Unit 3

	Intersection	Drillhole		True
Drillhole	<u>Length</u>	Angle	Bedding	Thickness
85-017	2.82	-59	60°	2.44
86-002	2.95	-51	74°	2.84
86-005	5.23	-59.5	79°	5.13
86-007	3.86	-67	68º	3.58
86-025	1.22	-49.5	74°	1.17
86-029	5.68	-56	66°	5.19
86-031	3.10	-46	76°	3.01
86-036	7.87	-54	72°	7.48
86-037	1.60	-63	59°	1.37

#### Approximate Thicknesses

Average of True Thickness 3.58 m

Although relatively little is known about unit 3 at the present time and it has not been seen in outcrop, a careful note should be made in future drilling or underground work of its orientation since it appears continuous throughout the property.

Map unit 1 is a general group for altered siltstone, hornfels found on the margins of argillite and themetasedimentary belts. These areas generally have very sparse outcrop and are covered by thin muskeg-swamp. Much of this area is probably underlain by recessive intrusive which are present as Lit par Lit injection and zones rocks of magmatic stoping. Rock exposed in these margin areas the more resistant altered siltstone are and biotite hornfels which form narrow linear mini-ridges with an elevation contrast of 1-2 m.

Unit 7 is composed of altered diorite sills and dykes. They usually white-weathering with buff to rusty iron oxide are Most surface orientations of the intrusives are staining. close to parallel with the enclosing marble but some crosscut bedding at high angles. These sills have been folded with theenclosing metasediments. Rocks mapped as along quartz "Crack felsite sills in the Area" have pyritic to 0.46 oz/ton gold. assayed Petrographic examination up typical specimens show that the "sills" are a mixof six ture of several plutonic types although in core specimens these intrusives are uniform when unaltered. Granodiorite is the most common rock type (Shearer, 1984b) with representatives of quartz monzonite, quartz diorite and hornblende-tremolite hornfels. Two specimens exhibited strongly developed cataclastic textures. Quartz granulation is common. A very distinctive characteristic of the intrusive sills are that many are boudins or even isolated fragments.

As indicated on the Time Chart, Page 15, Trader Resource Corp. commissioned a U/Pb date using Zircons obtained from a unit 7 skarnified dyke. A preliminary age from P. van der Henden for this dyke is 123 + 4 Ma.

Α large pluton to the east of Tel Zone is composed of magnetic, coarse crystalline, hornblende diorite to quartz diorite (unit 8). Several specimens of this rock have been examined in thin section (Shearer, 1985b). Over 70 hand specimens from outcrops around the Bob Zone were stained for potassium feldspar. Results show no mappable distribution of K-spar alteration with the possible exception of increasing potassium feldspars near the Bank-Barge An inspection of the lithotheque boards shows lineament. that there is considerable visual variation between the Bob Zone specimens, yet they are all within the quartz diorite field.

Three lithotheque boards have been constructed (Laznicka, 1974, 1975) in duplicate. One set will be stored in the Vancouver office and the other is stored at the Banks is also a third set composed of the Island Camp. There section off-cut blocks (the mirror image of each thin section) which have been stained for potassium feldspars, presently stored in Vancouver. The lithotheque library is designed to be clean and portable and can be used in conjunction with maps and other office materials. This system is ideally suited for the Yellow Giant Project which a number of geologists working on mapping and also has has

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subtle differences between the major granitoid suites. A total of 36 rocks were cut for thin section and summary descriptions are contained in Shearer (1984a). Additional lithotheque boards are planned for the Tel Deposit.

intrusive rocks (unit 9) are mainly biotite quartz Kim-type monzonite but vary from leucocratic granite through to end members are mainly diorite. The felsic hornblende monzonite (lithotheque No. B23-555, BL 140E, QH-1, guartz 180E & 120S, E-1, LY5-53) but also vary between C-1, QH granite and granodiorite. The mafic-rich end members vary quartz diorite and diorite. However, this wide between rock types is genetically related as indicated by ofrange Augite is present in the most the mafic constituents. mafic-rich in minor amounts but is mainly replaced by Minor biotite has developed at the expense of hornblende. the felsic side, biotite is the dominate hornblende. On and clearly replaces hornblende. Only a few mafic mineral relict grains of augite were noted in the quartz Small rounded inclusions of the mafic-rich end monzonite. commonly seen on the outcrop scale within the members are It is clear that the "Kim Zone Granite" quartz monzonite. is not the homogenous unit defined by Manchuk (1976).

## (b) <u>Alteration</u>

Alteration of the host rocks in the vicinity of the sulfide/oxide mineralization is an important feature at the Tel Deposit. The main alteration types are:

- (1) In banded grey marble:
  - (a) recrystallization in varying degree resulting in partial to complete destruction of dark grey bands:
  - (b) vuggy, white dolomitization which is commonly fracture controlled but occasionally results in massive, pervasive dolomitization;
  - (c) sparry, white calcite recrystallization apparently in part due to pressure shadows during intense folding (also probable solution feature);
  - (d) silicification near ore zones;
  - (e) development of disseminated "graphite" near major faults;
  - (f) brown iron oxide matrix filling in coarse breccia intervals;
  - (g) carbonate mylonites at locus of major faults;
  - (h) minor calc-silicates (skarn) near intrusions.
- (2) In silty thin bedded marble:
  - (a) ankerite (siderite) replacement of breccia fragments;
  - (b) brecciation-boudinage (disassociation of silty layers);
  - (c) sparry calcite;
  - (d) limonite staining; superficial to intense;
  - (e) hornfels, calc-silicate development and minor skarnification.
- (3) In diorite sills and dykes:
  - (a) chloritization; intense sericite development;
  - (b) skarnification, for example coarse actinolite stars;
  - (c) bleaching;
  - (d) pervasive silification and discrete quartz veining;
  - (e) grain size variation;
  - (f) hornfels and digestion of sedimentary fragments.

The most common alteration directly attributable to mineralization is limonite staining but in some cases the sulfide zones have not produced iron oxides. Silicification, as quartz veinlets, is present around some of the ore zones.

The ankerite (siderite) breccia noted in several drill holes may be related to an early karst solution collapse episode. Primary sulfide/oxide mineralization could have filled karstic voids. Intense, vuggy dolomitization also occurs around some of the sulfide zones.

Potassium/Argon age dating done by the B.C. Department of Mines on Kim Zone intense sericite alteration associated with mineralization gave a preliminary age of 123 Ma, which is identical to the U/Pb age of unit 7 dykes.

(c) Structure

Detail surface geological mapping and close-spaced diamond drilling suggest that the structure of the Tel Area is highly complex. A combination of tight, plunging isoclinal folding and a variety of major fault orientations contribute to the relatively large amount of data required to differentiate between the several plausible but differing geological interpretations. Until underground development is initiated, the actual importance and relative age of many major faults will be limited to correlation based largely on surface diamond drilling.

general distribution of the main map units is con-The trolled by the Tel Antiform which has a core of silty thin bedded marble, flanked by banded grey marble on either Apparently, the antiform is somewhat asymmetric since side. laminated black argillite (unit 6) is not represented on unless unit 6 is contained in the hornfelsic zone the west The Tel Antiform is a large regional mapped as unit 1. feature and can be traced from Hepler Creek in the south to north end of Sproatt Lake, a distance of 1.8 km. This theantiform does not extend into the Crossbreak showing area.

Numerous, relatively small scale folds occur on the west limb of the Tel Antiform which juxtapose short repetitions of banded grey marble, silty thin bedded marble, diorite and unit 3. The sulfide interval found in drillhole YGTL-85-007 could possibly be incorporated in this series of subsidiary folds.

limb of the Tel Antiform is now marked by a wide The east zone of shearing and brecciation called the McIntyre fault 315° and dips 50-55° to the east. which trends and graphitic slickensides mark the Tel fault Shearing immediately north of the Main Tel surface showing. The Tel is oriented 284°/74° E and apparently displaces fault the ore zone to the northwest with left-lateral separation.

Average bedding trends in various rock types are as follows:

#### TABLE V

# Bedding Trends, Tel Area

Rock Type	Range of Strike	Average Strike	Range of Dips	Average 
Pondod gnog monblo	306-3320	3310	50-82°F	660
Silty thin bedded marble	320-332°	329°	58-90°	70°
Quartz veins-breccia	235°	-	-	-
Shearing	269-284°	277°	74-90°	82°
Intrusive sills & dykes	270-358°	323º	63-90°	75°
Hornfels	318-325°	322°	52-66°	59°

Bedding east of the McIntyre fault in banded grey marble is about 324°/70°E whereas to the west around the Central Tel showing bedding is closer to 342°/68°E. Intrusive sills and dykes were usually seen to cross-cut bedding at a small angle although occasionally they cut across at high angles. Overall, the dykes dip steeper than the enclosing metasediments.

Isoclinal minor fold structures are well exposed at 30,797 N + 28,100 E and measured with the following results:

# Minor Fold Plunge

Intrusive dykes	41° toward 349°
-	44° toward 149°
	46° toward 149°
Banded grey marble	45-50° toward 350° and 150°

These minor folds are better exposed in the more resistant dykes than the marble. However, the intensity of regional shearing and drag along the northwest trending lineaments suggests that many of the major folds are probably rotated into steeply plunging structures.

### MINERALIZATION

(a) Mineralization and Drill Results

Since 1964, the Tel Zone has been tested by 91 diamond drillholes and numerous surface trenches. Total amount of drilling is 33,679.5 feet (10,265.64 m).

All important drill intersections are listed in Table VI. The simple average grades weighted by intersection core length are: Gold - 0.784 oz/short ton Silver - 1.40 oz/short ton Zinc - 1.86% Lead - 0.57% Copper - 0.13%

These averages do not consider weighting of drillhole azimuth or strike/dip of the mineralized zone.

By far the most dominant type of mineralization is a massive sulfides composed aggregate of pyrite, arsenopyrite, sphalerite and quartz, listed in decreasing abundance. Occasionally, the massive sulfides almost entirely of coarse crystalline in order of are composed Generally arsenopyrite appears to be arsenopyrite. а late-stage component associated with open-space filling, coarse grained, sparry calcite and monominerallic chlorite Much of the arsenopyrite-rich ore exhibits breccia masses. and varying degrees of gangue replacement by textures arsenopyrite. Ore types can be summarized as follows:

Most common: (1) massive sulfides: 52% of all Zones pyrite-arsenopyrite-sphalerite-quartz (1a) massive sulfides: arsenopyrite dominant (2) Breccia ore: arsenopyrite, pyrite, Less common: 33% of all Zones sericitic angular fragments Less common: (3) primary jasperiod (4) quartz breccia, pyrite-arsenopyrite, Minor: (drusy quartz) Late stage (6) graphitic quartz-pyrite (7) undeformed disseminated arsenopyrite

Some of the massive sulfide mineralization has undergone deformation intense as illustrated by well-developed textures of early phase coarse granulation crystalline Later stage arsenopyrite is undeformed. pyrite. Banding massive sulfide intervals in the are summarized in Table VII.

# TABLE VI

# Important Drill Intersections, Tel Zone February 1964 to March 1986

I. Main Tel Zone

Drill		Length	Gold	Silver	Copper	Zinc	Mineralization
Number	<u>Dip</u>	<u>(in m)</u>	<u>oz/ton</u>	<u>oz/ton</u>	95	<u>%</u>	Туре
P1	-38	1.22	1.52	1.2		13.3	Mass. sulfides
P2	-37	4.72	1.40	1.1		6.6	Mass. sulfides
							(diss.)
P3	-45	4.51	0.88	0.7		8.6	Mass. sulfides
P4	-48	2.29	1.16	1.2		14.5	Mass. sulfides
P5	-49	0.30	1.24	1.6		20.8	Mass. sulfides

# Average 1.2 oz/ton gold over 2.59 m

Note: true widths are about 75% of intercept length (Seraphim, 1975).

P6	49	1.37	0.66	1.5		4.1	bx qtz sulf
P26	-45	0.61	0.20	1.1			Mass. sulfides
P25	-40	0.46	0.36	0.8			Mass. sulfides
P14	-60	0.58	1.56	3.0	3.5		Mass. sulfides
Trench			1.16				Mass. sulfides

1975 Drilling:

Drill <u>Number</u>	Dip	Length	Gold <u>oz/ton</u>	Silver <u>oz/ton</u>	Copper <u>%</u>	Zinc %	
B-5	-45	33.07 - 33.38 = 0.30	5.04	2.80		Mass	. <b>sulfide</b> s
		35.05 - 35.81 = 0.76	0.25	ruuge		qtz I	x

# I. Main Tel Zone (cont'd)

1975 Drilling:

Drill			Gold	Silver	Copper	Zinc	Type of
Number	Dip	Length	<u>oz/ton</u>	oz/ton	%	%	<u>Mineralization</u>
B-6	-58	5.79 - 7.01 = 1.22	Tr	Tr	0.01	10.05	
		31.55 - 33.07 = 0.61	Tr	0.04	-		
		33.07 - 33.83 = 0.76	0.005	0.06	-	-	
		33.83 - 35.36 = 1.52	0.36	0.51	0.10	3.50	
		35.36 - 36.88 = 1.52	1.72	1.40	0.15	2.85	
		36 88 - 38 41 = 153	2 30	2 00	0 52	3 25	
		$38 \ h1 = 30 \ 03 = 152$	0.66	0.61	0.02	6 15	
		30.03 - 41.45 - 1.52	4 94	2 40	0.13	3 50	
		59.95 = 41.45 = 1.52	4.34	2.40	0.23	J.JU 0 EE	
		41.45 - 42.42 = 1.04	5.76	1.70	0.17	0.55	
		42.42 - 45.28 = 0.79	0.50	0.51	0.17	2.50	
		45.28 - 45.11 = 1.85	0.04	0.02	0.01	0.30	
		45.11 - 46.63 = 1.52	0.16	0.14	0.01	1.05	
		46.63 - 48.16 = 1.53	1.01	0.76	0.07	3.35	
Total B	8-6	33.83 - 48.16 = 14.33	5 1.47	1.00	0.15	2.73	mass. & diss.
		33.53 - 48.46 = 14.94	4 2.10 s	ludge			sulfides
B-7	-61.5	44.78 - 45.11 = 0.64	0.39	0.43	0.14	5.65	<b>mass. s</b> ulfides
B-8	-57	51.97 - 52.58 = 0.61	0.55	0.83	0.14	3.74	<b>mass. s</b> ulfides
B9	-47	37.03 - 38.10 = 1.07	0.48	0.40	0.17	3.19	<b>diss. sulf</b> ides
B-11	-70	25.39 - 31.24 = 5.85	1.01	1.23	0.18	4.59	<b>mass. sulf</b> ides
B-12	-85	No significant inter	enctione				
	00	No significant inter	500 010113				
B-13	-85	26 06 - 33 53 = 7 47	1 15	2 07			mass sulfides
510	00	5-104 recovery $-30$	1.10 hg - 32 0	2.07	az/ton	Au in e	
		5-10% recovery - 50.	+0 - JZ.3	<b>z</b> - 1.15	02/001	AU IN S	studge
D 15	45	61 42 61 F4 - 0 12	0.20	0 14		0.25	
D-10 D 10	-40	01.42 - 01.54 = 0.12	0.20	0.14		0.25	dian nulfidoo
8-10		72.85 - 75.91 = 1.06	0.02				diss. Suitides
<b>TT</b> 0		<b>T</b> - <b>1</b> - <b>1</b>					
<u>11. Cer</u>	itral	Tel Zone					
	. –						
P-11	-43	12.90 - 14.94 = 2.06	0.27	0.8	2.65		<b>mass. s</b> ulfides
P-10	-45	16.61 - 16.76 = 0.15	1.16	1.8	50%	recover	<b>y mass. sul</b> fides
Trench			2.16	(poor	recovery	in P-1	9)
B-3	-45	73.15 - 76.20 = 3.05	0.06 s	ludge			<b>diss. sulfid</b> es
B-4	-57	27.43 - 30.48 = 3.05	1.54 s	ludge			diss. sulfides
		30.48 - 35.05 = 4.57	0.36 s	ludge			
				-			
III. We	est Te	1					
		_					
B-1	-45	19.96 - 21.79 = 1.83	0,018				
B_2	-45	$28 \ 96 \ - \ 30 \ 18 \ = \ 1 \ 22$	Tr				diss, sulfides
							Saco, Sustando

TABLE VI

							TYPE OF
DDH	DIP	AZIMUTH	FROM	<u>то</u>	LENGTH	<u>Au OZ/T</u>	MINERALIZATION
85-004	-42	230	48.00	49.00	1.00	0.100	Mass. sulfides
85-005	-61	227					
85-006	-46	268	85.72	86.54	0.82	0.396	Mass. sulfides
85-007	-60	268	204.01	204.47	0.46	1.140	Mass. sulfides
			206.73	211.50	4.77	0.946	Mass. sulfides
85-010	-66	267	130.81	132.59	1.78	0.372	Mass. sulfides
			223.72	224.35	0.63	0.416	Jasperoid
85-011	-63	249	84.02	84.49	0.47	0.208	Quartz limonite
85-012	-43	266	46.33	47.12	0.79	0.320	Quartz limonite
			59.03	82.34	23.31	0.548	Mass. sulfides
			99.67	101.19	1.52	0.408	Quartz limonite
			107.98	109.57	1.59	0.126	Mass. sulfides
			113.67	115.67	2.00	0.670	Mass. sulfides
85-013	-53	265	50.23	52.40	2.17	4.352	Mass. sulfides
			73.15	74.00	0.85	0.166	Mbl-qtz breccia
			81.70	90.53	8.83	0.268	Mbl-qtz breccia
			107.80	109.70	1.90	0.139	Mass. sulfides
			114.44	117.96	3.52	0.107	Mass. sulfides
85-014	-43.5	268					
85-015	-54	269					
85-016	-50	263	46.28	47.68	1.40	0.415	Mass. sulfides
85-017	-59	265	53.10	53.64	0.54	0.312	Diss. in qtz
			132.59	139.65	7.06	1.422	Mass. sulfides
85-018	-41.5	277	75.00	76.00	1.00	0.080	Fault breccia
			148.60	156.36	7.76	0.274	Oxid. qtz & pyr
			165.00	166.00	1.00	0.120	Graphitic shear
			175.42	178.00	2.58	0.301	Mass. sulfides
			183.00	186.00	3.00	1.362	Graphitic shear
			201. <b>2</b> 4	206.50	5.26	0.230	Quartz breccia
			209.00	211.84	2.84	0.165	Quartz breccia
85-019	-43	264	61.57	62.40	0.83	0.162	Mass. sulfides
			104.90	105.77	0.87	0.108	Mass. sulfides
			143.60	143.99	0.39	0.120	Diss. sulfides
85-020	No						

85-020 No TO Significant

85-025 Intercepts

TABLE VI

							TYPE OF
DDH	DIP	AZIMUTH	FROM	<u>T0</u>	LENGTH	<u>Au OZ/T</u>	MINERALIZATION
86-002	-51	277	238.93	239.50	0.57	0.292	Mass. sulfides
			242.93	249.00	6.07	2.981	Mass. sulfides
86-005	-59.5	271	149.79	152.00	2.21	1.043	Mass. sulfides
			206.00	208.70	2.70	0.701	Mass. sulfides
86-007	-67	261	56.57	57.91	1.34	0.342	Mass. sulfides
			111.86	120.00	8.14	0.495	<b>Qtz flt brecci</b> a
			131.96	132.48	0.52	0.607	Jasperoid
			135.94	141.00	5.06	0.976	Mass. sulfides
86-009	-75	266	69.09	71.26	2.17	0.228	Qtz limonite
			174.50	176.00	1.50	1.260	Mass. sulfides
86-011	-43.5	249	38.27	39.22	0.96	0.260	Diss. in qtz
86-013	-51	248	39.93	42.35	2.42	0.290	<b>Qtz flt brecc</b> ia
86-015	-62	245	48.82	50.29	1.47	0.624	<b>Jasp/qtz brcci</b> a
86-017	-43	233	35.49	39.93	4.44	0.282	Mass. sulfides
86-019	-52	233	40.20	41.60	1.40	0.244	Lim qtz/diss.
86-020	-56	265.5	26.93	28,08	1.15	1.290	Mass. sulfides
			34.02	48.25	14.23	0.980	Jasp/massive
			59.13	66.46	7.33	0.045	Diss/Jasperoid
86-021	-68	232	50.90	52.42	1.52	0.204	Qtz breccia
86-022	-44	268.5	36.27	38.51	2.24	2.139	Qtz breccia
			43.00	58.22	15.22	0.707	Qtz ank/mass.
86-023	-41	232	54.30	62.25	7.95	0.080	Jasp/qtz brec.
86-024	-46	228					
86-025	-49.5	233					
86-026	-60	228	34.44	40.54	6.10	0.081	Qtz breccia
86-027	-61	237	121.52	126.00	4.48	0.455	Qtz breccia
86-028	-42	223	63.12	68.86	5.74	0.365	Qtz breccia
86-029	-56	223.5	95.56	106.37	10.81	0.462	Qtz limonite

Т	A	в	L	Ε	V	I
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							TYPE OF
DDH	DIP	AZIMUTH	FROM	<u>T0</u>	LENGTH	<u>Au OZ/T</u>	MINERALIZATION
86-030	-67	219	139.50	144.98	5.48	1.081	Mass. sulfides
86-031	-46	228.5	89.73 105.71	91.50 106.16	1.77 0.45	0.170 0.144	Mass. sulfides Qtz breccia
86-032	-57	229.5					
86-033	-67.5	231.5					
86-034	-46	230	53.04	57.60	4.56	1.650	Jasp/massive
86-035	-42	230	94.84	96.00	1.16	0.085	Diss. in qtz
86-036	-54	230	125.35	127.31	1.96	0.148	Qtz breccia
86-037	-63	230					
86-038A	-60	228	79.74	82 <i>.</i> 38	2.64	2.239	Mass. sulfides
86-039	-43.5	230.5	61.48 69.35	62.91 70.31	1.43 0.96	0.086 0.815	Qtz breccia Mass. sulfides
86-040	-60	230.5					

30.

# TABLE VII

# List of Banding/Layering in Massive Sulfide Drill Intersections

<u>Hole No.</u>	<u>Area</u>	Dip of Hole	Azimuth of Hole	Sulfide Layering	Sulfide Contact with Faults <u>or Host Rock</u>
85-007	Central	-60°	268°	55°	55°
85-012	Central W. Limb	-43°	266°	85° 42°	21º
85-013	Central	-53º	265°		55°
85-016	E. Limb	-50°	263°		62°
85-017	E. Limb			40°	
85-018		-41.5°	277°	60°	
				26°	1 O°
86-002		-51°	277°		13°
86-007	E. Limb	-67°	261°		42°
86-021	E. Limb	-68°	232°		52°
86-031	W. Limb	-46°	228.5°		73°
86-034	W. Limb	-46°	230°		28°
86-038A	W. Limb	-60°	228°		15°
86-039		-43.5°	230 <b>.</b> 5°		15-25°

The jasperiod ore is a hard, crustified and colloform limonitic iron oxide, finely laminated with very fine grained silica that carries high gold values. It has been encountered in several widely spaced holes. Jasperoid usually forms the entire mineralized section but in hole YGTL-85-012 it is in fault contact with fresh massive sulfides. Fragments of jasperoid have been noted in the quartz-arsenopyrite breccia. Samples of jasperoid examined by Harris (1986) contained traces of sericite, amphiboles, graphite and native copper.

Relatively abundant gold up to 100 microns in size was noted by Harris (1986) in specimens of pyrite-arsenopyritesphalerite massive sulfides, mainly within or on the contacts of various sulfide and gangue minerals. He states that (Harris, 1986):

"The two samples from the Central Tel Zone (069X and 070X) are mineralogically similar to those from the A Zone. They consists dominantly of well segregated clumps of pyrite and sphalerite, with accessory

arsenopyrite, in a texturally heterogenous siliceous gangue. Carbonate is essentially absent, and no graphite was seen. Gold occurs in both samples, as grains up to 100 microns in 069X but finer-grained in 070X. It shows no consistent textural relationships, occurring totally enclosed in sulfides and quartz as well as on sulfide/sulfide and sulfide/silicate contacts.

The A Zone and B Zone samples both show more or less banded, crustified textures suggestive of vein origin.

The two samples from the West Tel Zone (071X and 072X) are only weekly mineralized, arsenopyrite being essentially the only sulfide. It occurs as disseminated clumps and strings of euhedral grains, apparently following grain boundaries and micro-structures in the hosting gangue. In 071X the gangue is largely quartz with minor carbonate, whilst in 072X these proportions are reversed. No gold was observed."

Possibly, the massive pyrite mineralization formed as a ofresult early filling of karst/solution collapse cavities. Decisive information may be found by carefully all mineralized intersections examining for overlooked cross-cutting diorite dykes. Coarse arsenopyrite phase mineralization may be related to a thermal event at 123 Ma. More work is required to resolve the history of mineralization and subsequent deformation.

(b) Computerization of Assay Results

In July 1986 analytical data for silver, arsenic, copper, lead, zinc, iron and sulphur and calculated values for iron sulphide from mineralized intersections from all Tel drilling, was submitted to Simons and entered into the data bank for the deposit.

Grade composites were calculated (see Appendix II) and contoured plans, Figures 8 to 42, were generated. The values plotted are average grades weighted by sample length in 10 m segments over vertical intervals of 50m. The intervals are:

> above Om elevation Øm to -50m elevation - 50m to -100m elevation -100m to -150m elevation, and < -150m elevation.

Zero elevation is sea level as in other Simons sections and plans for the Tel Deposit.

Figure 7 shows the drill indicated ore zones, as developed by the mineral inventory, and two anomalies outlined by the June 1986 E-SCAN survey. Two northwesterly trending ore zones, one between surface and -30m and the second at depth greater than 50m and two E-SCAN anomalies of similar trend and elevation are outlined. When compared with the contoured plans, the following information is displayed:

- (1) The range of average grade values in the ore zones are 0.001 to 0.500 oz gold /ton, 0.001 to 1.000 oz silver /ton, 0.001 to 1.000 % arsenic, 0.001 to 0.100 % copper, 0.001 to 0.500 % lead, 0.001 to 2.500 % zinc and 0.001 to 5.000 % iron sulphide.
- (2)Broader zones of contoured values for all elements are outlined from Øm to-50m and -50m to -100m elevations. These at similar elevations to the are drill indicated ore zones, and have similar elevation and outline to the E-SCAN anomalies.
- (3) Several anomalies, or areas of higher grade mineralization occur within each ore zone.

- (4) Elevated values of iron sulphide and/or zinc are most commonly associated with gold anomalies. Higher grade contours for all elements are present in the central part of the ore zones (near 30700N, 28250E) from 0m to -100m elevation. Below -100m, fewer sections with higher grade values of silver, arsenic, copper and lead occur.
- (5) In the southeastern part of the ore zone, there appears to be a correlation between gold and iron sulphide. E-SCAN anomalies indicate that there may be a southern extension to the main ore zone in this area.

### GEOPHYSICS

In 1986, Premier Geophysics Inc. of Vancouver conducted two phases of E-SCAN geophysical surveys in the area of the Tel Deposit.

The following describes the E-SCAN system and its application at the Tel property. Reference to figures in the appended report is suggested.

# Initial E-SCAN Testing of the Tel Ore Zone

In June 1986, induced polarization (IP) and resistivity surveys over a 150 by 225 meter grid centered on the known Tel ore zones (Report, Figure 2) was carried out. The survey was conducted on a 15 meter grid spacing, and was intended to determine whether the technique could:

- 1. detect the known ore zones of the Tel Deposit, from near-surface to >150 meters depth; and
- 2. discriminate between sulphide ore signatures and those of other non-ore rock units, for example the graphitic, pyritic argillite metasediments of the Banks-Barge lineament.

E-SCAN utilizes a new data acquisition technology which provides for saturation coverage of a property with the ofto forty spearate conventional equivalent thirty electrical surveys, all conducted simultaneously, and covering every orientation of measurement. One benefit cited is that the explorationist does not need to commit to one just orientation of sampling, as is the conventional case, can rely on saturation coverage for an objective but assessment of all possible ore zone and structural combinations configurations. and orientations. Where overburden covers most of the area, and where structural and ore shapes and orientations can be highly conditions variable (the Tel area), E-SCAN saturation coverage can be identify geologic expected tozones and structures regardless of size or orientation.

Summary Report on E-SCAN Induced Polarization and Resistivity Surveys

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Tel Property, Banks Island, British Columbia

June, October, November, 1986

for

TRADER RESOURCE CORP.

Report by Greg A. Shore Premier Geophysics Inc. Vancouver, British Columbia.

Report submitted February 18, 1986

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YELLOW GIANT GEOLOGIC UNITS

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B.7 E-SCAN Apparent Resistivity data, 40-60 metres
B.8 E-SCAN Apparent Resistivity data, 60-80 metres

#### **1.0 SUMMARY** Refer to Figures 3 and 5.

E-SCAN induced polarization (IP) and resistivity surveys over the Tel ore zone and adjacent land have detected anomalous responses in six areas, in addition to mapping the signature of the known ore zone itself. Four of these anomalies are connected to the main ore zone by fault zones which are themselves anomalous in signature.

The six anomalous zones that have been identified and warrant follow-up work are:

1: The IP anomaly defining the known Tel ore zone extends southeast into undrilled ground and represents a possible extension of the known ore structures in this direction. This is a first-priority drill-test area.

2,3: Two broad and distinct IP anomaly zones lying in the marbles southeast of the main one zone warrant priority drill investigation due to the similarity in size, setting, and electrical signature as compared to the known one zone anomaly. An anomalously responding fault system connects these anomalies with the main one zone, all within the known marble environment.

4: An anomalous zone lies along the strike of the cross faults passing through the Tel ore zone. Limited drilling in this area has provided gold values; additional investigation is warranted.

5,6: Two other possibly anomalous zones in unknown or poorly defined rock units require various types of follow-up investigation including drilling to determine geologic/economic interest.

The tight correlation between the known (drill-indicated) gold/sulphide ore zones of the Tel deposit and the E-SCAN anomaly outline establishes the E-SCAN method as a viable mapping tool for the marble environment of the Yellow Giant Property.





Figure 2

Location of E-SCAN survey grids, Tel Zone and adjacent north grid and southeast extensions.

#### 2.0 INTRODUCTION

In June 1986 Premier Geophysics Inc. operated a series of E-SCAN induced polarization and resistivity surveys over the Trader Resource Tel gold-silver deposit on Banks Island, B.C. The purpose was to evaluate the usefulness of the E-SCAN method in mapping Tel type deposits in the complex area geology.

The marble zone which contains the Tel deposit extends for considerable distances both northwest and southeast of the proven ore zone, in a generally similar geologic setting. Since this area has not been successfully mapped with geophysical methods heretofore, the demonstration of any geophysical (or other) tool which could definitively detect the Tel deposit would be of interest for application elsewhere in the marble zones of the Yellow Giant property.

The E-SCAN surveys operated in June 1986 at Tel were successful in precisely outlining the drill-indicated ore zones (see Figure 6, and section 4.1.1 of this report). Additional E-SCAN coverage was obtained in October and November 1986 to resolve the extent and character of two new anomalous zones which extended beyond the June test grid.

The results of the June test surveys and of the subsequent extension surveys are reported herein, commencing in section 3.0.

2.1 Description of the E-SCAN system

E-SCAN is an automated data acquisition system employing up to 254 individually addressable electrodes installed in the ground at any one time. While the data acquisition is computer controlled and occurs at a very high rate of speed, each measurement is a conventional time domain IP and resistivity measurement, noise-averaged and logged on disc. The principal time savings lies in the elimination of the usual wire dragging and setup for each measurement, allowing actual direct measurement time to occupy 90% of each 8 hour day.

The E-SCAN system uses a conventional reversing DC square wave with an on/off pulse ratio of 1:1 and a total cycle time of 2 seconds. IP measurements for this survey were measured over an integration period of 167 milliseconds following a delay of 167 milliseconds, expressed as a percentage of the measured primary voltage.

The data presented in the plan plots are pole-pole array data, measured using one current electrode and one potential electrode on the property and corresponding current and potential "infinite" reference electrodes located distant from the survey area. The pole-pole array has the advantage of requiring less array space per unit penetration, and provides for the least complicated and least ambiguous interpretation of all survey arrays. This is particularly important in areas of complex geology such as is found in the Yellow Giant project area. The density of measurement and the multi-directional character of the E-SCAN data set allow averaging of noisy data to provide for logical and unambiguous resolution of anomaly and structural details at scales much finer than is possible with conventional surveys.

### 2.2 Previous IP/resistivity experience, Tel area.

The Yellow Giant property on southwestern Banks Island has a long history of exploration effort. The present program of exploration carried out by Trader Resource Corp. is the first to identify economically significant ore volumes and grades.

The Tel deposit is a series of gold-bearing sulphide zones extending over an area at least 35 metres wide and over 150 metres in length, extending from outcrop to depths over 150 metres. At the time of this report, the Tel deposit remains open at depth and on three sides.

A conventional (pole-dipole) induced polarization and resistivity survey (White, 1975) has been conducted previously over the Tel deposit, with mixed results. While anomalous responses were noted in the vicinity of the known sulphide ore outcrop, the spatial correlation between data and known sulphides was poor. The 1975 IP results indicated a northwesterly trend from the outcropping sulphide area, while the recent drilling (and the E-SCAN results) prove a westerly trend for the main ore zones tested to date.

The interpretation of the 1975 data was further confused by strongly anomalous responses originating from non-ore rock units (the closely adjacent graphitic argillites of the Banks-Barge lineament, and other unidentified rock units lying west of the known ore zone) which were indistinguishable from the responses originating from the sulphide ores.

By providing a hundredfold greater density of measurements, with measurements made in all directions instead of one, and with each of these measurements providing greater resolution at less susceptibility to distortion from nearby rock units, the E-SCAN survey method has been able to precisely outline the Tel ore zone, and to identify geophysically similar drill targets representing possible new ore.

# 2.3 The Tel deposit as an induced polarization and resistivity target.

Hosted in marbles, the Tel sulphide-gold-silver ore should represent an induced polarization target. However, as with any geophysical target, the anomalous quantity must be distinguishable against the surrounding non-anomalous rock, the background. In the Tel area, there are strong sources of electrical distortion in the Banks-Barge lineament (graphitic pyritic argillites) and in the very conductive layers of recent sediments found in lake-bottoms and depressions.

Initial tests of the E-SCAN system directly over the ore outcrop area confirmed a recognizable IP anomaly (2.5% to 4%) in an otherwise low chargeability (1.8% to 2.5%) marble environment, and indicated a low resistivity anomaly for the outcropping ore zone (600 ohm-metres) in a 1000 to 4000 ohm-metre marble background. By comparison, the responses obtained from the closely adjacent graphitic argillites were extreme, with IP in the 7% to 10% range and with resistivities of less than 50 ohm-metres.

The discrimination of economically significant responses in this complex and largely overburden-covered geology is therefore less straightforward that in the textbook IP case where a uniform low-background rock unit is searched for any higher (anomalous) values. What is anomalous in marble may be normal for the Kim granitic unit and lower than background for the argillite unit. The definition of any value as "background" or "anomalous" first requires identification of the rock type involved, and establishment of its "background" unmineralized signature.

Data interpretation for the area thus has two steps:

1. Identify the marble environment as distinct from the argillite unit by means of its more moderate levels of IP response and higher resistivities, making use of any mapped outcrops and drill information as corroboration.

2. Within the marble unit, look for anomalous IP response (2.5-6%) against a background of 2.5% or less, together with a lower resistivity.

To date, only the marble rock suite (which hosts the known Tel orebody) has been sufficiently tested and drill-correlated to allow confident definition of "anomaly" versus "background". See Figure 6.

The lateral boundaries of the Tel deposit are clearly mapped by the induced polarization (IP) results, using standard E-SCAN grid methods with local current injection.

While the conductive nature of the ore environment is indicated in shallow resistivity measurements over the outcrop, the wide and irregular distribution of near surface, strong conductors (Sproatt Lake fault, graphitic argilliite unit, shallow surficial deposits) renders most of the moderate depth resistivity data close to the Tel deposit uninterpretable. However, a conductive axis for the deposit is clearly shown in the mise a la masse survey, its clarity due to the introduction of current directly into the deep target area, away from surface distortions.

The resistivity signature remains a minor part of the Tel orebody electrical signature. The primary telling characteristic is the IP signature, which correlates with the drill-indicated ore zones precisely. Sulphide mineralization, massive or disseminated, will provide IP responses. Coincident resistivity anomalies (conductors) may or may not be present. If the sulphide mineralization is discontinuous or disseminated, there may be no low resistivity signature, and even a high resistivity response if sulphide fracture-filling is complete and/or carbonate or silica precipitation is pervasive. The indicated conductor at Tel suggests a strongly faulted structure at least, and implies substantial lengths of connected conductors (mineralization) in order to provide the strong mise a la masse signature.

#### 3.0 SUMMARY RESULTS AND RECOMMENDATIONS

The data and interpretations are presented on two map bases, one covering the known Tel ore zone and the area adjacent to the southeast, and the other covering the area north and west of the known Tel ore zone, referred to as the North Grid Extension.

The summarized structural features and anomalous IP zones are presented in Figures 3 and 5. Note that only those structures which are identifiable in the E-SCAN data (principally the resistivity data) are presented...it is likely that other faults and contacts occur, but are not detected by E-SCAN due to a lack of measurable electrical response or characteristics. These results can be used to more accurately plot geologically mapped or inferred structures and/or boundaries, and to identify unsuspected features beneath overburden. As is always the case, the intention of the geophysical surveys is to enhance and supplement the geological understanding of the area under study.

ANOMALY 1: Main Tel ore zone anomaly, southeast extension.

Map: Main Tel ore zone and adjacent southeast area (Fig. 3) Also refer to Figures 6, A.1, A.2

The correlation between IP anomaly and drill-indicated ore is very close on all sides of the ore zone except the southeast. This is the only area where the drilling pattern has not yet cut off the ore zones; it is largely untested to date, having been penetrated partially by only one hole.

The IP anomaly bulges out to the southeast, then thins and extends further along a fault-contact lying between the silty thin-bedded marble and the grey banded marble.

The mise a la masse contours also bulge and thereby indirectly identify anomalous conductivity oriented southeast across the IP anomaly zone, further supporting the probability of ore extension.

The extended zone should be thoroughly drilled from near-surface to depths in excess of 150 metres.

ANOMALY 2: Adjacent to Tel zone, southeast in marbles.

Map: Main Tel ore zone and adjacent southeast area (Fig. 3)

Anomaly 2 lies completely enclosed by marble units, its center 135 metres southeast of the main Tel ore zone. The anomalous IP values are entirely consistent with those mapped over the known Tel zone, and the background IP levels are also comparable.

The data suggest that the mineralized zone may not extensively subcrop (the area is mostly covered by overburden), but detailed

prospecting should be undertaken nonetheless in advance of drilling and/or trenching.

There is a narrow but clear IP anomaly extending between Anomaly 2 and Anomaly 1 (Main Tel ore zone) along the fault-contact between the silty thin-bedded and grey banded marbles. A narrow anomalous zone also extends southeast to Anomaly 3, again along an indicated fault. In anticipation of a possible continuous zone of mineralization extending from the Main Tel ore zone through to Anomaly 3, a drill pattern should be established along a new skid trail located parallel to, and 50 to 80 metres northeast of, the average strike of Anomalies 1, 2, and 3. Initial holes would test for economic mineralization at six to eight points along strike, with infill drilling depending on initial positive results. The zone's indicated lateral boundaries should be drilled from near-surface to at least 150 metres vertical depth.

ANOMALY 3: Adjacent to Anomaly 2, southeast in marbles.

Map: Main Tel ore zone and adjacent southeast area (Fig. 3) Also, read ANOMALY 2 details above.

Anomaly 3 is identical in IP and resistivity characteristics to Anomaly 2, and lies a further distance along the marble units southeast of Anomaly 2. It is well defined within the present coverage, but is open to the southeast on a 50 metre wide front.

Anomaly 3 should be drilled from the same baseline of holes proposed under Anomaly 2 above, and to similar depths. If economic mineralization is detected, the E-SCAN coverage should be extended further southeast to outline and define the rest of the anomaly prior to extending drilling southeast.

ANOMALY 4: On westerly strike of Tel ore zone main fault(s).

Map: Main Tel ore zone and adjacent southeast area (Fig. 3) Also, North Grid Extension (Fig. 5)

Anomaly 4 lies west of the Main Tel ore zone, on or near the westward extension of the main Tel cross-fault(s) and on strike with the deepening trend of mineralization. The area has only a few drill holes and is poorly understood geologically at present. Some gold-bearing intersections (associated with graphite) are noted deep in this area, and some surface showings occur.

While the area is nominally mapped as marble, the deeper geology is little understood. Adjacent to Anomaly 4 to the west and northwest is a broad lithological unit whose apparent "background" IP signature is the same as the values recorded in the Anomaly 4 area. This area may be anomalously chargeable marbles (and therefore a priority drilling target) or perhaps a fault-shifted pocket of the broad unit mapped to the west and northwest (non-anomalous).





Initial drilling of this area should establish rock type first. If it is marble, watch for other (non-ore related) sources of IP response such as graphitic zones. If the typical Tel zone sulphide and gold association is not present, then care should be taken to test for other gold associations which may define a second economic E-SCAN signature to be watched for (Tel sulphides in marble being the first to be established).

ANOMALY 5: On strike west from Anomaly 4; uncertain geology.

Map: North Grid Extension (Fig. 5)

Anomaly 5 has the distinction of lying further west, on strike with the Main Tel ore zone and Anomaly 4. Little is known of the geology here, and the principal interest lies in the combination of location on strike with the Tel zone cross structure(s) and the occurrence of locally anomalous IP levels with anisotropic characteristics in both IP and resistivity.

Resistivity anisotropy is widely measured in and around Anomaly 5, and is in itself not an unexpected signature across the edge of steeply plunging metasediments. Anisotropic IP values may also occur readily in these circumstances, but in fact do not, except in this one area on strike with the Main Tel fault(s).

If the anisotropy is due to a zone of strong shearing or other directionally preferential structure rather than original bedding now tilted, then the possibility of mineralization occurs and should be evaluated.

This area should be drilled (again shallow and deep) from north to south from at least two sites. More intensive mapping of this area should identify general rock types, at which time the E-SCAN results should be re-assessed and a drill site decision made.

ANOMALY 5: Northwest of the Tel ore zone, in uncertain geology.

Map: North Grid Extension (Fig. 5)

Anomaly 6 lies in unknown geology. It is of interest if it lies in marble, or if it is in the same rock unit as the surrounding lower chargeability rocks (thereby an "anomalous" zone). This is the lowest priority anomaly of the six reported here, but only because of the many unknowns at present.

The area should be mapped to determine rock types, and the possibility of anomaly status reviewed with that information in hand. A single drill hole through the area would establish geology and therefore mineralization potential. Such a hole should be long enough, however, to establish rock types within and outside the potential anomaly area.

#### 4.0 REVIEW OF SELECTED DATA RESULTS

Figures A.1 and B.1 show IP responses at the shallowest sampling levels. The grids of dots represent the location of the 452 electrodes making up the total E-SCAN network. Over 19,000 individual IP readings were logged, along with over 19,000 apparent resistivity measurements. These data form the master data set from which all plots of specific depths or other characteristics are identified and used.

The data used in the following plots are pole-pole array IP responses, calculated from the master E-SCAN data set, with the value plotted at the mid-point between the two electrodes responsible. The orientation of the data tic indicates the orientation of the current flow for the measurement (as well as pointing to the electrodes). The colour and length of the tic encode the IP value according to the key at right. IP and resistivity pole-pole data are plotted using similar conventions for this particular pseudo-depth plan viewing of the E-SCAN data.

4.1 DATA SET A: Tel Zone and adjacent area to southeast.

4.1.1 Correlation of E-SCAN with Tel ore zones.

See Figure 6.

Features:

- virtually all known ore zones are contained within the IP anomaly outline.
- mise a la masse conductive axis correlates with deep ore zone position and orientation.

The lateral boundaries of the Tel deposit are clearly mapped by the induced polarization (IP) results, using standard E-SCAN grid methods with local current injection.

While the conductive nature of the ore environment is indicated in shallow resistivity measurements over the outcrop, the wide and irregular distribution of near surface, strong conductors (Sproatt Lake fault, graphitic argilliite unit, shallow surficial deposits) renders most of the moderate depth resistivity data close to the Tel deposit uninterpretable. However, a conductive axis for the deposit is clearly shown in the mise a la masse survey, its clarity due to the introduction of current directly into the deep target area, away from surface distortions.

The resistivity signature remains a minor part of the Tel orebody electrical signature. The primary telling characteristic is the IP signature, which correlates with the drill-indicated ore zones precisely. Sulphide mineralization, massive or disseminated, will provide IP responses. Coincident resistivity anomalies (conductors) may or may not be present. If the sulphide



TRADER RESOURCE CORP. Tel Zone and adjacent area to southeast. Yellow Giant Project, Banks Island, B.C.

> E-SCAN SURVEYS June 1986

> > 0 10 20 30 METRES

SUMMARY E-SCAN RESULTS shown over drilling results as at June 1986

MISE A LA MASSE SURVEY

Axis of deep conductor Contours in millivolts.

INDUCED POLARIZATION ANOMALY OUTLINES: A: surface to elev. -30 m. B: deeper than elev. -30 m.

DRILL-INDICATED ORE ZONES **PROJECTED TO SURFACE:** surface to elev. -30 m. elev. -50 to -170 metres 177

1

Figure #6

prog: /mise/EPR.2.9.2 data file: /mise/deepLINE data file: /mise/shalLINE Premier Geophysics Inc. Vancouver, B.C.

TRADER RESOURCE CORP. INTERPRETED ANOMALOUS INTERPRETED ANOMALOUS North Grid Extension. IP ZONE, NEAR-SURFACE IP ZONE, DEEPER THAN Tel Property, TO -30 M (AMSL) -30 M (AMSL) Yellow Giant Project Banks Island, B.C. 107+00N 106+50N 106+00N 104+50N 104+00N 103+50N 103+00N 102+00N 101+50N 101+00N 100+50N 100+001 105+00N 105+50N 107+50N 102+50N E-SCAN SURVEYS June-Dec., 1986 · 9+50E 10 20 30 SPROATT LAKE · 9+00E METRES FAULT · 8+50E INTERPRETED ID. 18+00E GEOLOGY FAULT OR CONTACT ANOMALY IP # 5 ANOMAL ·7+50E ·7+00E FAULT OR CONTACT FAULT OR CONTACT FAULT OR CONTACT UNKNOWN. B 0 К N I. FAULT OR CONTACT UNKNOWN FAUL ROCK UNIT FAULT FAULT OR CONTACT JP PAGEAD E MULTINE FAULTINE ANOMALY Figure # 5 **#**. 6 4+00E program: /tln/plot.summ.7 · 3+50E

1.5

Premier Geophysics Inc. Vancouver, B.C.

11

mineralization is discontinuous or disseminated, there may be no low resistivity signature, and even a high resistivity response if sulphide fracture-filling is complete and/or carbonate or silica precipitation is pervasive. The conductor mapped with a mise a la masse technique at Tel suggests a strongly faulted structure at least, and implies substantial lengths of connected conductors (mineralization).

#### 4.1.2 Mise a la masse survey results

See Figures 6 and 7.

Features:

- the deep conductive axis corresponds with IP trend.
- the strength of the conductor implies very conductive fault materials, alteration products, graphite and/or massive metallic sulphides.
- bulges in the contours on the southeast side mark secondary (to this survey) zones of conductivity lying between the plotted bulge and the deep conductor. No depth information is available, except for a lower limitation of about half the depth to the current source, or .5 x 60 = 30 metres (or less).



TRADER RESOURCE CORP. Tel zone and adjacent area to southeast. Yellow Giant Project, Banks Island, B.C.

> E-SCAN SURVEYS June 1986

> > 0 10 20 30 METRES

MISE A LA MASSE SURVEY potential field contours (millivolts Vp)

Current injection is at 95.3 metres in DDH 85-012, elevation -47.5 metres, location marked as +.

AXIS OF DEEP CONDUCTOR

Plotted over IP anomaly zones.

Figure #7

prog: /TEL/mise/EPR.2.27 data file: /mise/deepLINE data file: /mise/shalLINE Premier Geophysics Inc. Vancouver, B.C.

#### 4.1.3 General E-SCAN results

Figure A.1 Shallow pole-pole array IP 5-20 metres

Features:

- the Tel ore zone area is outlined (yellow) at 2.6% to
   4% IP. An extension of the ore zone anomaly extends
   southeast for over 30 metres in undrilled ground.
- the lobe of anomalous ground extending southeast thins along the fault-contact between silty thin-bedded marble and grey banded marble before widening in a broader anomalous zone centered about 120 metres SE of the main ore zone.
- the edge of another anomaly (yellow) is evident at the southeast margin of the grid.
- the edge of the chargeable argillite unit is seen along the northeast (top) edge of the grid. It moves in and out showing fault displacement. (This unit has not been evaluated for gold content or for useful E-SCAN signatures relevant to any such gold occurrences.)
- at lower left, another anomalous zone (assuming we are still in marbles here) extends off the grid, positioned accurately on strike with the main Tel ore zone faults. (The few drill penetrations in this area have encountered gold values, some with graphite.)
- a background IP signature for the marbles (both types) appears to be 1.5% to 2.5%.

Figure A.2 Shallow pole-pole array IP 20-40 metres

Features:

- looking deeper, the anomalous zones lying southeast of the Tel zone are filled out, and now display significant volumetric status.
- the connecting, chargeable, probable fault zones between the three anomalies are confirmed, though the evidence is not straightforward to the untrained eye.
   no additions, changes or surprises.

## Overlay of Figure 3 on Figure A.2

- cross-faults and the marble fault-contacts combine to permit substantial fracturing (shearing) in and around principal anomalies. If the mineralizing fluids arrived post-faulting, then these permeable zones may have served as conduits and precipitation surfaces.
- the near edge of the argillites should be investigated to determine whether that fault (shown at top of plot) was also mineralized. There is insufficient

of the elevated argillite IP levels opposite the marble IP anomalies.

Figure A.3 Moderate pole-pole array IP 40-60 metres

Features:

- scatter of data as a result of the plotting convention makes this and the next deeper plot dangerously ambiguous to the casual observer. While these depths of data require secondary processing (not shown here) to develop interpretation, three conclusions you might attempt as an observer deserve comment:
  - 1. The southeast (untested) lobe of the main Tel anomaly # 1 is more responsive than the known (drilled) area; possibly indicating more intense mineralization.
  - 2. Most of the scattered (yellow) anomalous values west and southwest of Anomaly # 2 (use the overlay to locate) represent a deep IP anomaly lying to the west, along the strike of the west cross-fault.
  - 3. Most of the scattered (yellow) anomalous values east and west of Anomaly # 3 (use the overlay to locate) do not represent a broader anomaly at depth but are effects of the plotting convention placing responses due to a single electrode at the center of electrode pair. The lack of confirming (yellow) anomalous reponses in the north-west/south-east oriented data (all green) confirm that the yellow values result from arrays oriented with one electrode within the anomaly area, and one outside. (The data at this depth are becoming incomplete this close to the edge of the grid. Expanded coverage may indicate true deeper offset anomalies.)

Figure A.4 Deep pole-pole array IP 60-80 metres

Features:

- the deep IP anomalous zone west of Anomaly 2 continues to be independently defined.
- no equivalent deep definition near Anomalies 1, 3, and 4 is available from visual inspection of this plot. All other apparent deep "anomalous" values are plotconvention scatter.

(12)
## Figure A.5 Shallow pole-pole array resistivity 5-20 metres

#### Features:

- outcropping Tel ore area is moderately conductive.
- area over deeper Main Tel ore is resistive.
- Sproatt Lake fault and graphitic argillite area are very conductive.
- pond and lake edge areas are very conductive.
- most of the marbles resistive (2500 5000 ohm-metres).
- the area including Anomalies 2 and 3 is uniformly resistive above 2500 ohm-metres.

#### Figure A.6 Shallow pole-pole array resistivity 20-40 m.

#### Features:

- pond area conductivities are shown to be very thin, surficial. (More resistive rocks underneath are showing.)
- the distorted (low) values due to the pond area at lower left now form a "halo" around the pond, a result of plot-convention displacement of true effects from the in-pond electrode site to the arbitrary mid-point between electrodes.

## Figure A.7 Moderate pole-pole array resistivity 40-60 m.

#### Features:

- no significant developments.
- the broad area of yellow at left is largely due to plot-convention displacement as in A.7. If there is information about the Tel ore zone as well, it cannot be separated from the known, overwhelming effects of the lake and pond sediments.

Figure A.8 Deep pole-pole array resistivity 60-80 metres

Features: -

- as per A.7

## (13)

## GEOPHYSICS

In 1986, Premier Geophysics Inc. of Vancouver conducted two phases of E-SCAN geophysical surveys in the area of the Tel Deposit.

The following describes the E-SCAN system and its application at the Tel property. Reference to figures in the appended report is suggested.

## (a) Initial E-SCAN Testing of the Tel Ore Zone

In June 1986, induced polarization (IP) and resistivity surveys over a 150 by 225 meter grid centered on the known Tel ore zones (Report, Figure 2) was carried out. The survey was conducted on a 15 meter grid spacing, and was intended to determine whether the technique could:

- 1. detect the known ore zones of the Tel Deposit, from near-surface to >150 meters depth; and
- 2. discriminate between sulphide ore signatures and those other of non-ore rock units, for example the graphitic. pyritic argillite metasediments of the Banks-Barge lineament.

E-SCAN utilizes data acquisition technology which а new provides for saturation coverage of a property with the equivalent of thirty to forty spearate conventional surveys, electrical all conducted simultaneously, and covering every orientation of One benefit measurement. cited is that the explorationist does not need to commit to orientation of just one sampling, as is the conventional case. but can rely on saturation coverage for an objective assessment of all possible ore zone and structural configurations. combinations and Where orientations. overburden covers most of the area, and where structural conditions and ore shapes and orientations can be highly (the variable Tel area), E-SCAN saturation coverage can be expected to identify geologic zones and structures regardless of size or orientation.

Ιt is reported that over 19,000 individual induced polarization measurements and an equal number of resistivity measurements were obtained over the Tel and adjacent areas during the two field programs.

Field data acquisition of the test phase was completed in June 1986 and the data were evaluated and compared to the ore distribution model which H.A. Simons Ltd. engineering consultants had developed from the Tel area drill records (Report, Figure 6. -A 1:500 scale version of this map is Figure 7, located in the map pocket).

The conclusions reached at that time were:

- 1. The Tel sulphide/gold ore mineralization has a distinct E-SCAN IP signature within a marble rock unit environment.
- 2. The lateral boundary of the E-SCAN ΙP anomaly correlates very closely with about most of thedrill-indicated boundary. Where E-SCAN ore the boundary extends beyond the limit of drill-indicated it is found that the ore limits are also open in ore. direction - that is, the area in question is not that yet drill-tested.
- 3. The marble units (silty thin-bedded, and grey banded) have a distinct background IP and resistivity signature which distinguish them from the adjacent graphitic argillites.

4. Mise a la masse resistivity can be useful in projecting ore zone orientation from deep ore intersection in drillholes (Report, Figure 7).

The close correlation of E-SCAN results with the drilled ore zone confirmed the utility of using E-SCAN first to detect the areas of favourable geology (marble), and subsequently to discriminate within the marble those anomalous conditions which may indicate ore of the type occurring in the Tel zone.

The anomalous zone detected over the main Tel zone showed a conspicuous bulge to the southeast (anomaly #1), extending into an area not yet drill tested. In addition, the anomalous zone extended off the grid to the east and to the west, along the strike of the main ore zone cross-faults. Finally, a subtle but unambiguous indication of anomalous conditions existed in the marble southeast of the main ore zone, at the edge of the June grid coverage.

## (b) Subsequent E-SCAN Surveys - October, November 1986

Additional E-SCAN services were contracted in September 1986 to extend coverage into the area north and northwest of the initial grid, and to extend coverage in the area of the subtle indication to the southeast.

#### Adjacent Area Southeast of the Tel Zone

The extension to the southeast revealed two substantial IP anomalies (#2 and #3), with anomaly #3 remaining open to the southeast at the edge of the survey grid. These

anomalies are connected to the main Tel ore zone anomaly (#1) by a fault zone which is itself anomalous. Shore suggests that the broad anomaly areas and the connecting fault zone should be systematically drill tested along the full 225m strike, since the entire system actually forms one long, continuous anomaly.

Cross-faults cut the marble near the anomalies, at approximately the orientation of the faults passing through the Tel ore zone. West of the central anomaly, a zone of deep (-50 meters AMSL and deeper) anomalous IP of considerable spatial extent (#2A) lies within the marble regime. This is cited as a drill target as well (Report, Figures 3, 4, A-1, A-2, A-3, A-4).

The anomalies (#1, #2, #2A and #3) provide, at rough estimate, approximately four to six times the surface area (lateral extent) of the presently proven Tel ore zone. Shore reports that the IP signatures over these anomalies are similar to that over the main Tel zone, while the differences in resistivity are nominal and do not diminish the interest in the anomalies.

## North Grid Extension

The north grid extension encounters different rock types (as yet unidentified) in bands west of the marble zone. The coverage overlaps the E-SCAN IP anomaly #4 lying west of the main Tel ore zone, and identifies two other anomalies (Report, Figures 5, B-1, B-2).

Anomaly #6 is possibly in marble northwest of the main ore zone, and, while a subtle feature, it is nonetheless of significant areal extent, at 30 by 40 meters. Mapping and exploratory drilling are suggested by Shore, but recommended as last priority of the six anomalous zones.

Anomaly #5 lies in non-marble rock, down-strike from the main ore zone and anomaly #4, in distinctly anisotropic resistivity and IP conditions. Anisotropy is characteristic of certain rock fabrics and bedding orientations, but may also be diagnostic of the type of intense shearing or multiple faulting that would be conducive to circulation of mineralizing fluids. Partly because of the density of faulting identified through the anomaly area, the latter possibility is favoured by Shore, although he observes that a different mineralogy than that of the Tel zone is likely here, probably involving graphite but not excluding gold. Further mapping prior to drilling is recommended by Shore.

## CONCLUSIONS AND RECOMMENDATIONS

The Tel ore zone is contained in a complex structural environment. The effects of plunging isoclinal folding and several generations of faulting have required close-spaced diamond drilling todefine themineralized zone. Generally, stratigraphy is consistent throughout the deposit area. The most common host rocks are banded grey marble and silty thin bedded marble. The main structural elements include the regional Tel Antiform, McIntyre Fault and locally the Tel Fault.

The Tel Deposit is mainly composed of massive pyritearsenopyrite and sphalerite. Less common ore types are compact jasperoid, sericite-arsenopyrite breccia and late stage, drusy quartz-pyrite assemblages.

The Tel Deposit is open at depth and along strike to the northwest. The possibility of additional ore lenses to the southeast has not been investigated in enough detail.

Contoured plans for gold, silver, arsenic, copper, lead, zinc and iron sulphide show zones of anomalous values for all elements are present between 0m and -100m elevations. Elevated values of iron sulphide and/or zinc are most commonly associated with higher gold grades. E-SCAN induced polarization and resistivity surveys on and near the Tel Zone have accurately outlined the known Tel ore zone, and mapped six new anomalous areas within 250 meters of the Tel ore zone.

Of these six, one is a direct extension of the main ore zone anomaly, and two others are similar in appearance to the main ore zone anomaly, and occur in similar geologic conditions (marble, near cross-faulting). Drilling of these three anomalies and their common, connecting fault zone has been recommended by Premier geophysicist Greg Shore.

The other three anomalies lie in different geologic conditions, and warrant further mapping and investigation prior to drilling.

The E-SCAN method appears to have provided clearly defined anomalies despite the presence of significant potential sources of survey distortion. It also appears to have provided detailed information on the structural features of the Tel ore zone and adjacent areas. The value of these findings must now be tested by further mapping and drill testing of the anomalies.

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# APPENDIX I

# E-SCAN REPORT

# February 1987

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#### 4.2 DATA SET B: North Grid Extension area.

#### 4.2.1 General E-SCAN results

Figure B.1 Shallow pole-pole array IP 5-20 metres

Features:

- a band of <2.6% IP covers the upper part of the plot.</li>
   These vales are typical of the marble signatures further southeast.
- IP Anomaly # 4 sits as a distinct higher IP zone within the lower IP probable marble, at the edge of an unknown rock type with higher IP levels as "normal" background.
- IP Anomaly # 5 is a subtly higher IP zone within probable marble.
- a band of (yellow) 2.5% to 4% IP rock separates the probable marble (green, blue) from another more chargeable rock type (orange) extending along the bottom of the plot.

Figure B.Z Shallow pole-pole array IP 20-40 metres

#### Features:

- this is essentially a deeper view of the same features described in B.1 above.
- Anomaly # 6 emerges more visually as an area of anisotropic, elevated IP within the orange unit. IP values in a westerly orientation are higher than those observed in a northerly orientation, suggesting that the chargeable mineral(s) occurs in a directionally preferential mode, along faults or fractures or within a rock fabric of distinct orientation. The magnitude of the IP response (>6.3%) suggests graphite (with or without sulphides).

#### Overlay of Figure 5 on Figure B.2

- Anomalies 4 and 6 lie on strike along the Main Tel area cross fault zone.
- Intense faulting or shearing indicated by anisotropic resistivity measurements characterize the area to the left (northwest) of Anomaly # 6.
- Anomaly # 6 is also intersected by a north-trending fault.

#### Figure B.3 Moderate pole-pole array IP 40-60 metres

#### Features:

 scatter of data as a result of the plotting convention provide a blurred picture, but principal features can still be seen.



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Premier Geophysics Inc. Vancouver, B.C.

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Vancouver, B.C.

TRADER RESOURCE CORP. North Grid Extension, Tel Property, Yellow Giant Project Banks Island, B.C.

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## APPARENT RESISTIVITY ohm-metres



Depth of penetration (Ze): 20-40 metres

Figure # 🕑 . 6

program: /disc/EPR.2.14 data file: /TLN/TLND3 f: 10 Premier Geophysics Inc. Vancouver, B.C.



TRADER RESOURCE CORP. North Grid Extension, Tel Property, Yellow Giant Project Banks Island, B.C. E-SCAN SURVEYS June-Dec., 1986

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Depth of penetration (Ze): 40-60 metres

Figure # B . 7

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Tel Property, Yellow Giant Project Banks Island, B.C. 107+00N 106+50N 106+00N 105+50N 101+00N 100+50N 100+001 107+50N 104+00N 103+50N 105+00N 102+50N 101+50N 104+50N 103+00N 102+00N E-SCAN SURVEYS June-Dec., 1986 · 9+50E 10 20 30 · 9+00E METRES 8+50E APPARENT RESISTIVITY 8+00E ohm-metres 7+50E 100 160 ·7+00E 161 250 400 401 630 1000 1001 1600 2500 2501 4000 6300 6301 10000 16000 . Depth of penetration (Ze): 60-80 metres Figure # B. 8 · 4+00E program: /disc/EPR.2.14 · 3+50E data file: /TLN/TLND5 f: 10 Premier Geophysics Inc. Vancouver, B.C.

TRADER RESOURCE CORP. North Grid Extension. - no new occurrences or changes of mode at this depth are evident.

Figure B.4 Deep pole-pole array IP 60-80 metres

Features:

- as B.3 above.

Figure B.5 Shallow pole-pole array resistivity 5-20 metres

Features:

- the orange values closely define the parts of the grid that lie in Sproatt Lake. The conductivity (<400 ohm-metres) is due to shallow sediments in the lake. This conductivity will affect (lower) the measured values of all rocks beneath.
- the very chargeable rock unit lying along the lower part of the plot shows moderate resistivity here (green, 1000-2500 ohm-metres), with anisotropic signatures to the left (northwest) of IP anomaly # 6.
- the wedge of unknown rock at left (blue, >2500 ohm-metres) is distinct from all of the other rock units.
- the band of rocks between the probable marbles and the lower unit report a (yellow) signature of 400 to 1000 ohm-metres.

Figure B.6 Shallow pole-pole array resistivity 20-40 m.

Features:

- this plot confirms the characteristics of B.1 at greater depth.
- the shallower parts of the lake sediment area are yielding to higher resistivity values as the underlying rocks are sampled (orange in 8.1 become yellow; higher resistivity).

Figure B.7 Moderate pole-pole array resistivity 40-60 m.

Features:

- no significant developments.
- the resolution of boundaries is becoming obscure due to the plotting convention.

Figure B.8 Deep pole-pole array resistivity 60-80 metres

Features:

- as per B.7
## 5.0 PERSPECTIVE ON FURTHER USE OF E-SCAN IN VARIOUS YELLOW GIANT GEOLOGIC UNITS

The present survey interpretation is effective because there is previous drill-confirmed experience in the marble ore setting to refer to. The range of additional non-marble settings for gold mineralization across the Yellow Giant property is broad, and includes metasedimentary and granitic hosts, and mineralization assemblages featuring significant amounts of graphite. While effective exploration can continue within the marble environment, the extension of effective survey coverage to other rock types depends upon the detection and recognition of a distinct electrical signature for gold mineralization within these rock units. This is a process which can be developed gradually as drill coverage, geologic understanding, and high-density E-SCAN coverage of the subject geologies becomes available for correlation, as was the case in establishing the E-SCAN parameters for the marble environment using Tel drill results.

February 18, 1987

Coreg A. Shore Premier Geophysics Inc.

## CERTIFICATE

I, Gregory A. Shore, do hereby certify that:

- I am a geophysicist with business office at Suite 307, 100 West Pender Street, Vancouver, B.C. V6B 1R8, and President of Premier Geophysics Inc. and of E-SCAN Service Company Inc.
- 2. I have practiced my profession continuously for the past 15 years, and have been continuously active in geophysical survey planning, execution and interpretation for the past 21 years.
- 3. I am a member in good standing of the Society of Exploration Geophysicists (SEG), European Association of Exploration Geophysicists (EAEG), and the Society of Mining Engineers (SME of AIME).
- 4. The information, opinions and recommendations in this report are based on my personal knowledge of the survey work done, and on on-site observations made by me in the course of work on the project.
- 5. I have no direct or indirect interest in the the Yellow Giant property, in Trader Resource Corp. Ltd., nor do I expect to receive same.
- 6. This report may be used intact or excerpted for any purpose provided that the sense and meaning of the excerpted material remains unaltered.

Dated at Vancouver, British Columbia, this 18th day of February, 1987.

Gregory A. Shore

Statement of Costs.

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E-SCAN Surveys Tel Property Area Yellów Giant Project Banks Island, B.C.

Premier Geophysics' invoiced charges for the work reported herein are as follows:

Phase 1: June 1986:

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E-SCAN contract survey services, including all survey supplies, equipment and survey personnel; mobilization and demobilization: \$ 30,000.00

Phase 2: October-November 1986:

E-SCAN contract survey services, including all survey supplies, equipment and survey personnel; mobilization and demobilization:	\$ 81,224.63
Data processing and report preparation:	\$ 7,234.00

TOTAL CHARGES:

\$118,458.63

Greg A. Shore Premier Geophysics Inc.

## APPENDIX II

GRADE COMPOSITE DATA

.



**H.A. Simons Ltd.** Consulting Engineers

425 Carrall Street Vancouver, B.C. Canada V6B 2J6 604-664-4315 Telex 04-51150

August 20, 1986

Trader Resource Corporation 701 - 744 West Hastings Street Vancouver, B.C. V6C 1A5

Attention: Mr. J. Shearer Chief Geologist

Dear Joe:

Subject: Grade Contours - Tel Deposit

This letter is to cover delivery of 35 drawings showing the grade contours of 7 elements in 5 horizontal benches. The data used for the contours is in the accompanying data files.

The contours are plotted for gold, copper, lead, zinc, arsenic, silver and iron sulphide. The values plotted are 10 m composites along the drillhole over the distance noted. For example, in the interval of  $-50 \text{ m} \leq \text{EL} < 0 \text{ m}$  there would be 5 values for each drillhole which extends through the 50 m section.

The data files have been sorted by drillhole and by easting and northing. The file names containing "04" is for the elements gold, copper, lead and zinc. The file names containing "58" is for the elements arsenic, sulphur (not contoured), silver and iron sulphide.

This completes the work described by Proposed Scope Change No. 2 for P. 3013C dated July 29, 1986. If you have any questions, please do not hesitate to call.



OS:sb Encl.

Mining & Mineral Processing Division

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		COMPOSITE	COMPOSITE	POINT OF	COL 5				BASE OF	WIDTH OF			
	NULE NU+	X-COOKU	T-COOKD	CUMPUSITE	6000	COPPER	LEAU	ZINC	LEVEL	COMPOSITE			
<u></u>	F6400011	28169.23	30708.72	25.00	0.00000	0.00000	0.00000	0.00000	20.00	11.44			
	P6400011	28172.90	30718.80	15.00	0.10346	0.00000	0+00000	0.00000	10.00	5.32			
01												·	
1				ELEVATION									
			COMPOSITE	OF MID									
- '  -	HOLE NO.	X-CORD	Y-COORD	COMPOSITE	6010	COPPER	LEAD	7100	I FUFI				
	nonne nove	X 93000	1 00000	0011 0.01 11.	() () <u>.</u>	0.01 T E.IX		2110	0.0	CONFOULTE	. ·		
1	P64DD014	28261.07	30702.79	25.00	0.00036	0.00000	0.00000	0+00000	20.00	10.20			
	P64UU014	58591*98	30708+53	15.00	0.17395	0.00000	0.00000	0.00000	10.00	5.19			
) )													
				ELEVATION									
OL		COMPOSITE	COMPOSITE	OF MID POINT OF					RASE OF	NITTH OF			
1	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
$\neg$													
	P6400025	282/8+62	30714.20	25,00	0.01055	0.00000	0.00000	0.00000	20.00	7.98			
$\sim$	1				0102000	0100000	0.00000	0.00000	10+00				
				OF MID									
) [_		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
0	P64DD026	28299.74	30697.22	25.00	0.00000	0,00000	0.00000	0.00000	20.00	7.21			
	P64DD026	28293.31	30689.56	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14			
	P64DD026	28286.88	30681.90	5.00	0.01895	0.00000	0,00000	0.00000	0.00	6.39			
_													
]				ELEVATION									
		COMPOSITE	COMPOSITE	OF MID		· · · ·							
	HOLE NO.	X-COURD	Y-COURD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	IFVFI	COMPOSITE			
) [_													
	B75DD001 B75DD001	28063.57	30730,10	25.00	0.00000	0.00000	0.00000	0,00000	20.00	14.14			
- 2	27.500000		00700170	1.0+1/1/	0+00007	0.00000	0.00000	0.00000	10+00	14+14			
$\cdot$				ELEVATION OF MID									
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF			
. )	HOLE NO.	X-0080	Y-C0080	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
	B7500002	28064.95	30728.90	25.00	0.0000	0.00000	0.00000	0 00000	20 00				
	B75DD002	28072.61	30735.33	15.00	0.00001	0.00000	0.00000	0.00000	10.00	14+14			

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B75DD002	28080+27	30741.76	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14			
		an ann a' anna a raige ag			· · · · · · · · · · · · · · · · · · ·				, ,			
			ELEVATION	1. A. A. A.					· .			
	COMEOSITE	COMPOSITE	OF MID									
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
B75DD003	28169.38	30704.72	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.92	·· · · · ·		
B75DD003	28167.64	30714.57	15.00	0.00000	0.00000	0+00000	0.00000	10.00	14.14			
B7500003	28165.90	30724.42	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14			
87500003	28164+16	30/34+2/	-5.00	0.00000	0.00000	0.00000	0+00000	-10.00	14.14			
B7500003	28160.69	30753.94	-25,00	0.00000	0.00000	0.00000	0.00000	-20.00	14+14			
B75DD003	28158.96	30763.81	-35,00	0.00000	0.00000	0.00000	0.00000	-40.00	14.14			•
									1,00,01			
			ELEVATION							,,,,,,, _		
	COMBOGITE	COMPOSITE	OF MID									
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
87500004	28170.90	20702.17	25 00	0.00000	0.00000	0 00000	0 00000	20 00	0 00			
B75DD004	28173.32	30709.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	7+22			
B75DD004	28175.75	30715.22	5.00	0.00179	0.00000	0.00000	0.00000	0.00	11.92			
B7500004	28178.18	30721.24	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	6.26			
			ELEVATION									
			OF MID									
	COMPOSITE	COMPOSITE	POINT OF	0010	0000000			BASE OF	WIDTH OF			
HULL NU+	X-COORD	THOUGKD	COMPOSITE.	6960	LUPPER	LEAU	ZINC	LEVEL .	COMPUSITE			
B75DD005	28291.31	30669.04	25.00	0.00000	0.00000	0.00000	0.00000	20.00	8.88			
B7500005	28298,38	30676.11	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14			
8/5/1005 07500005	28305+45	30683+18	5.00	0+12252	0.00000	0.00000	0.00000	0.00	14.14			
87500005 87500005	20012+02 28310.50	30670+20	-5.00	0.00000	0.00000	0.00000	0.00000	-10+00	14+14			
B7500005	28326.66	30704.39	-25,00	0.00000	0.00000	0.00000	0.00000	-30,00	10.75			
			,, <b>,</b> ,, ,,		0100000	0100000	010000		10+70			
			ELEVATION	<u></u>						9799 1887 8887 987 <sup>9</sup> 1974		
	COMPOSITE	COMPOSITE	UF MID POINT OF					BASE OF	цтрти ос			
HOLE NO.	X-CONED	Y-COORD	COMPOSITE	GOLD	COPPER	IFAD	7110	IFUEL	COMPOSITE			
	2 C C C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C	1 000000	-2007 (1) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2	للدخوان. و .	5591 T 14A	1	<del>ب</del> ۲۱۴ ته ب	tota Viala	CON COTTE			
B75DD006	28289.75	30669.05	25.00	0.00000	0.00000	0.00000	0,00000	20,00	7,56			
B75DU006	28292.20	30674.80	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.79			
87500006	28294.63	30680.55	5,00	0.00000	0.00000	0.00000	0.00000	0.00	11.79			
875000008 87500004	28200 E7	30000.31	-15 00	L+61223 0.74774	0.00000		0.0000		11+80			
97.9949AAB	న-నుగు ∕7 శందభి	01072+100		V 4 0 0 / 0 M	V • V V V V V	*******	v • 00000	- × 0 + 0 0	J+33			
······································			ELEVATION									
	00×000175	004000175	OF MID						112 5 5 1 1 5 5 5			
	Y-COOPT	V-CORRE	COMPOSITIC	001.0	CODDCD	I E A D	7710	BASE UF	WINTH UF		· .	• •
noite NO+	X~000K0	1-00080	CONFUSILE	ບບພະ	CUFFER	LEAD	ZINU	LEVEL	CUMPUSITE			

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	ſ													
$\sim$	B7500007	28311.14	30702+20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.38		,		
52	B75DD007	28306+92	30698.78	5.00	0.00000		0+00000			11.38				
	B750D007	28302+70	30695.37	-5+00	0+00000	0.00000	0.00000	0.00000	-10,00	11.38				
	E75DR007	28298.48	30691.95	-15.00	0.01307	0.00000	0.00000	0.00000	-20,00	11.38				
)	<u>B7500007</u>	28294.26		-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.38		· · · · ·		
	ſ													
-														
- 31				ELEVATION										
				OF MID										
		COMPOSITE	COMPOSITE	POINT OF					RASE OF					
<b>)</b>	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	I FUFI	COMPOSITE				
	87500008	28309.79	30703.85	15.00	0.00008	0.00000	0 00000	0 00000	10 00	11 00				
$\supset$	87500008	28303.33	30703.19	5.00	0.00000	0.00000	0.00000	0.00000	10.00	11 07				
	07500000		70703 40			0 00000			V.+ V	11+75	· ·			
	57300000	20200	30702+47	-3+00	0+00000	0.00000	0.00000	0.00000	-10.00	11+73			•	
$\neg$	573000003	2027V+41 20207 05	30/01+81	-10.00	0.00000	0+00000	0.00000	0.00000	~20.00	11.73				
	8/0111008	20203.70	30/01+13	-23.00	0.02888	0.00000	0+00000	0,00000	-30.00	11.92			······	
1														
				ELEVALUN										
				OF MID										
5		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
O	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	I.EAD	ZINC	LEVEL	COMPOSITE				
~	B75DD009	28308.73	30700.22	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.90				
	B7500009	28300.92	30694.54	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13,90				
	B75DD009	28293.11	30688.87	-5.00	0+03776	0.00000	0.00000	0.00000	-10.00	13,90				
	87500009	28285.29	30683.19	-15,00	0.00015	0.00000	0.00000	0.00000	-20.00	13.90				
$\odot$	8750000	28277.48	30677.51	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	17.00				
Ì	87500009	28249.47	30471.84	-35.00	0.00000	0.00000	0.00000	0 00000	-40.00	= <u>= 5 00</u>				
ł				00100	0000000	0100000	V + V V V V V	******	40400	0+00				
- Ô -														
				FIFUATION										
				DE MIN										
		COMPOSITE	COMPAGITE	00 NID 20181 05					DACE OF					
	UNE NO	V_00000	V. COODO	COMPOSITION	001.0		1	7710	BHSE UF					
	MOC.5 1810 +	X-000R0	1-COOVD	COMPUSITE	60LD	UUPPER	LEAD	ZINC	LEVEL	COMPOSITE				
- 5	0750DA4	00740 04	70/07 /7	1										
	0/000011	20317+20	30687+63	10,00	0.00000	0+00000	0+00000	0,,00000	10.00	10.64				
	B7500011	28316+67	30685.02	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.64				
25	B75DD011	28314.14	30682.40	-5+00	0.56915	0.00000	0.00000	0.00000	-10+00	10.64				
. / ]	B7500011	28311.62	30679.78	-15.00	0.00291	0.00000	0.00000	0.00000	-20.00	10,64				
1	87500011	28309.09	30677.16	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.64				
-,														
				ELEVATION										
				OF MID										
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
	HOLE NO.	X-COORD	Y-CUORD	COMPOSITE	GOLD	COPPER	LEAD	7 TNC	I FUEL	COMPOSITE				
							···· · · · · · · · · · · · · · · · · ·		1, 1, <b>1</b> , <b>1</b> , 1, 1,	oom oorre				
	B75DD013	28332.89	30680.57	15.00	0.00430	0.00000	0.00000	0.00000	10.00	10.04				
	87550013	28332.00	30480.01	5.00	0.00157	. <u>«</u>	<u></u>						· · ·	
	37500013	28331 54	30470 44	-5 00	0.57007	0 00000	0.00000		0+00	10+04				
- )	87500017	28220.80	300//+44 30470 00		V+0/0V3 A 77077	0.00000		0.00000	-10+00	10.04				
-	57-30074-3 57-50074-3		70/07/04/00		<u>0,00000</u>	0.00000	0.00000	0.00000		10+04				
1	573901013	2033V•21 20720 ET	300/8+32	-23.00	0+00273	0.00000	0.00000	0.00000	-30,00	10.04				
- 1 I	8/500013	28327+D3 00700-07	39877+76	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.04				
- 1	\$\5\1\1\1\1\2	20320+00	306//+19	-43.00	0+00000	0.00000	0.00000	0.00000	-50.00	10.04				
	8/500013	28328+19	306/6+83	-55.00	0.00000	0.00000	0+00000	0.00000	-60.00	5.52				
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				FIFUATION									
	a			DE MID		·		· · · · · · · · · · · · · · · · · · ·					
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	ี่พำกาห กร			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE		 •	
	B750D014	28331.35	30679.21	15.00	0.00057	0.00000	0.00000	0.00000	10.00	10.64			
	B/500014	28328+56	30676+87	5.00	0.00000	0.00000	0.00000	0.00000		10.64	• • •		
	87500014 87500014	20323+77	308/4+33	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10+64			
	57505714	600 40 / C + 7 /	00072417	10+00	V+VV0VV	0100000	0.00000	0100000	-20+00	10+04		 	
				ELEVATION OF MID									
		COMPOSITE	COMPOSITE	POINT OF					BASE OF				
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
	B75DD015	28316.52	30645.35	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.39			
	B750D015	28323.83	30652.17	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14			
	B7500015	28331.15	30658.99	5,00	0.00000	0,00000	0.00000	0.00000	0.00	14.14			
	B7500015	28338+46	30465+81	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14			
	B7500015	28345.77	30672.63	-15.00	0.00391	0.00000	0.00000	0.00000	-20.00	14.14			
	B/500015	28353+09	30679.45	-25+00	0.00000	0.00000	0.00000	0+00000	-30,00	14+15		 · · · · · · · · · · · · · · · · · · ·	
	B/500015	28360+40	30886+58	-35,00	0.00000	0.00000	0.00000	0.00000	-40.00	10.34			
				ELEVATION									
				OF MID									
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WINTH OF		 	
	HOLE NO.	X-COORD	Y-CO0R0	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
	v.,												
	57500016	28310,73		25,00	0.00000	0.+00000	0.+00000.	0.00000	20.00	10+49			
	8/300016	28320+07	30647+90	15+00	0.00000	0.00000	0.00000	0.00000	10.00	14.14			
	87300016	200304+24 20722 00	30334+90	5,00	0.00000	0.00000	0.00000	0.00000	0.00	14.14			
-	87550016 87500016	00751.54	70444 90	-15.00	0.00000	0+00000	0.00000	0.00000	-20.00	<u>+4+14</u>		 	
	D7500010	20001100	20004.70	-25.00	0.00000	0.000000	0.00000	0.00000	-20+00	14+14			
	17.000010	20000420	59067+79	-20+00	V+VV-3-37	0.00000	0+00000	0.00000	-30+00	12+17			
				ELEVATION									
		COMERCETTE	COMPOSITE	DOINT OF						UTOTU OF		 	
	HOLE NO.	V-COORD	V_COOPD	COINT OF	COLD	CODDED	LEAD	7740	DHOR UP	WINIH OF			
	1101.0 1014	X GOODD	1 0000000	GUNE UDITE	(31361)	GUFFER	1.EHD	ZINC.	LEVEL	CONFUSITE			
	B75DD017	28183.75	30742.87	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11,55			
	87500017	28182.75	30737.19	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55			
	B75DD017	28181.74	30731,50	-5.00	0.00000	0.00000	0.00000	0,00000	-10.00	11.55			
	B750D017	28180.74	30725.82	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.55		 · · <u> </u>	
	87500017	28179.74	30720.13	-25+00	0.00018	0.00000	0.00000	0.00000	-30.00	11.55			
				FLEUATION									
				OF MID									
		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF		 	
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
									· · · · · · · · · · · · · · ·			 	
	VOOE OOA	28396.39	30677.87	15.00	0.00027	0.00000	0.00000	0.00000	10.00	15.11			
	1000-004				••••••				30700				

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YG85-004	28378.10	30663+63	-5+00	0.00000	0.00000	0.00000	0.00000	-10.00	15.46			
Y685-004	28359.14	30649.30	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	-15,54			
YG85-004	28349.63	30642.13	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.56			
	<del></del>	· · · · · · · · · · · · · · · · · · ·			······		<del>_</del> <del>_</del>			······································	·	
			ELEVATION OF M1D									
	COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF			
HOLE NO+	X-COORD	Y-COORD	COMPOSTIE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
YG85-005	28399.63	30680.28	15.00	0.00000	0.0000	0.00000	0.00000	10.00	11.41			
YG85-005	28395.56	30676+60	5+00	0.00000	0.00000	0+00000	0,00000	0.00	11.41			
1683-000	20202 20	300/2+72		0+00017		0.00000	0.00000	-10.00	11 444			
1000-000	- 20307+20 - 20707 A3	30007421		0.00000	0.00000	0+00000	0.00000	-20+00	11 - 40			·
Y685-005	28378.49	30663.47	-35.00	0.00017	0.00000	0.00000	0.00000	-40.00	11.54			
Y685-005	28374.09	30457.78	-45.00	0.00003	0.00000	0.00000	0.00000	-50.00	11.81			
YG85-005	28369.27	30653.74	-35.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.81			
Y685-005	28364.45	30649.71	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11,81			
YG85-005	28359.63	30645.68	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.81			
YG85-005	28354.80	30641.64	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.81	•		
YG85-005	28349.83	30637.53	-95,00	0.00000	0.00000	0.00000	0.00000	-100.00	11.99			
YG85-005	28344.64	30633+32	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.06			
YG85-005	28339.40	30629.07	-115.00	0.00000	0.00000	0+00000	0.00000	-120.00	12.06			
YG85-005	28334+16	30624.83	-125.00	0.00000	0.00000	0+00000	0.00000	-130.00	12.06			
YG85-005	28328.92	30620.58	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	8.96			
		·····	CI CHATTON									
			DE MID									
	COMPOSITE	COMPOSITE	POINT OF					BASE OF	WINTH OF			
HOLE NO.	X-COORD	Y-COOR))	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
Voor AA/	00705 00	70/04 75		0.000	0.00000	0.00000		10.00				
1683-006	28373.78	30081+/3	12.00	0.00054	0.00000	0.00000	0.00000	10.00	13.//			
1080-00a		30881+37	5+00	0.00001	0.00000	0.00000	0.00000	10.00	13+62			
1060-008 Y685-004	28748.13	30661+31	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.42			
Y885-006	28358.91	30481.37	-25.00	0.00044	0.00000	0.00000	0.00000	-30.00	13.59			
Y685-006	28349.69	30481.34	-35,00	0,00022	0.00000	0.00000	0.00000	-40.00	13.61			
YG85-006	28340.41	30681.36	-45.00	0.02588	0.00120	0.00000	0.08793	-50.00	13,67			
YG85-006	28331.06	30681.36	-55.00	0.00012	0.00000	0.00000	0.00000	-60.00	13.71			
YG85-006	28321.62	30681.35	-65.00	0.00015	0.00000	0.00000	0.00000	-70.00	13.79			
YG85-006	28312.13	30681.32	-75.00	0.00087	0.00000	0+00000	0.00000	-80,.00	13.80			
YG85-006	28302.56	30681.23	-85.00	0.00022	0.00000	0.00000	0.00000	-90.00	13.88			
YG85-006	28292.89	30681.05	-95.00	0.00000	0.00000	0.00000	0.00000	-100+00	13.94			
YG85-006	28283.15	30680.77	-105.00	0.00014	0,00000	0.00000	0.00000	-110.00	13.98			
Y685-006	28273.40	30680.45	-115.00	0.00021	0.0000	0+00000	0.00000	-120.00	13.96			
YG85-006	28263.66	30680.11	-125.00	0+00043	0.00000	0.00000	0.00000	-130.00	13.96			
1085-006	28233+97	306/9.77	-135.00	0.00000	0,000000	0,00000	0+00000	-140+00				
1989-006	20294+32	306/9+43	-140,00	0.00000	0.0000	0.0000	0.00000	-150+00	13.90			
1080-000 Y885-00A	28225.02	303/7,07	-165.00	0+00000	0.00000	0.00000	0.00000	-120.00	13.90			
Y685-006	28215.37	30678.41	-175.00	0.00000	0.00000	0.00000	0.00000	-180,00	10.49			

2 Vežna provenska vezera provenska provinska provinska provinska provinska provinska provinska provinska provinska

્ર	_MOZART\$D	UAO: ERESP:	NOZA . TELL 3	ITNABENA04T.	BEN:2	11-AUG-1986	5 14:11	Pase 8				 	
		COMPOSITE	COMPOSITE	POINT OF	001 5	000000	1 5 4 5	7110	BASE OF	WIDTH OF			
2	HULE NU.	X-CUURII	T-COURD	CUMPUSITE		<u>uurrek</u>	L.F.AU	Z.1 NG		COMPOSITE		 	
$\mathbf{a}$	YG85-007	28398.45	30681.80	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.56			
	Y095-007	20272+04	30481.41	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.54	 	 	
	Y685-007	28381.02	30481.52	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.56			
O	YG85-007	28375.11	30681.48	-25,00	0.00000	0.00000	0.00000	0.00000	-30.00	11.67			
	Y685-007	28369.05	30681.52	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.72		- 	
$\sim$	YG85-007	28362+94	30681.59	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.72			
)	Y685-007	28356.84	30681.65	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.72	 	 	
	YG85-007	28350.69	30681.73	-65.00	0.00155	0.00000	0.00000	0.00000	-70.00	11.77			
$\gamma$	YG85-007	28344.46	30681.83	-75.00	0.00074	0.00000	0.00000	0.00000	-80,00	11+79			
</th <th>Y685-007</th> <th>28338.21</th> <th>30681.93</th> <th>~85+00</th> <th>0.00169</th> <th>0.00000</th> <th>0.00000</th> <th>0,00000</th> <th>-90.00</th> <th>11+/7</th> <th>·</th> <th></th> <th></th>	Y685-007	28338.21	30681.93	~85+00	0.00169	0.00000	0.00000	0,00000	-90.00	11+/7	·		
	Y685-007	28331.95	30682+04	-95.00	0.00025	0.00000	0.00000	0.00000	-110.00	11.80			•
3	1080-007 VC05-007	28320+67	30002+10	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.89			
	Y085-007	20017+01	30492.38	-125,00	0.00184	0.00000	0.00000	0.00000	-130.00	11,94	 	 ·····	
	Y685-007	28304.28	30482.49	-135.00	0.00050	0.00000	0.00000	0.00000	-140.00	11.98			
0	Y685-007	28299.67	30682.61	-145.00	0.00017	0.00000	0.00000	0.00000	-150.00	11,99			
İ	Y685-007	28293.05	30482.72	-155.00	0,42161	0.02458	0.00146	1.24529	-160.00	12.00			
)								·			 	 	
				ELEVATION									
2				OF MID									
1		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WINTH OF			
	HOLE NO.	х-совкр	Y-COURD	COMPUSIE	HULD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
Э	YG85-010	28399.83	30681.81	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.87			
Ì	Y685-010	28395.58	30681.64	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.87			
-	YG85-010	28391.33	30681,47	~5.00	0.00055	0.00000	0.00000	0.00000	-10.00	10.87			
2	Y685-010	28386+97	30681.32	-15.00	0+00000	0+00000	0,00000	0.00000	-50,00	10.96			
	YG85-010	28382.49	30681.16	-25.00	0.00000	0.00000	0.00000	0.00000	-30+00	10.96			
~	YG85-010	28378.01	30681.01	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10,96			
<u>_</u>	YG85-010	28373.53	30680.85	-45.00	0.00000	0.400000	0.00000	0.00000	-50,00	10.96	 	 	
1	Y685-010	28369+05	30680.69	-55+00	0.00000	0.00000	0.00000	0,00000	-60.00	10.96			
- ) Í	Y585-010	28364.57	30680.54	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10+96			
1	1080-010 V005-010		30000+30	-05 00	0.00000	0.00000	0.00000	0.00000	-80.00	11 04			
	70005-010 V005-010	- 20000+02 - 20750 70	20200V+22 20200 05	-85 00	0.02260	0 00124	0.00175	0.03924	-100 00	11.09			
$\rightarrow$	Y685-010	28345.93	30679.88	-105.00	0.03836	0,00413	0.00344	0.06832	-110.00	11.15			
-	YG85-010	28340.94	30679,71	-115.00	0.00036	0.00000	0.00000	0.00000	-120.00	11.20	 		
	Y685-010	28335.87	30679,54	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.22			
)	YG85-010	28330.78	30679.36	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.22			
	YG85-010	28325+69	30679.18	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.22			
	YG85-010	28320.60	30679.00	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.22			
	YG85-010	28315.50	30678.82	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.22	 	 	
	Y685-010	28310.41	30678.65	-175.00	0,00232	0.00000	0+00000	0.00000	-180.00	11.22			
- 1	YG85-010	28305.32	30678.47	-185.00	0.02590	0.00730	0.00000	0.08626	-190.00	11.23			
2	Y685-010	28300+55	30678.29	-195.00	0.00000	0.00000	0.00000	0+00000	=200+00 .	11.22			
	YG85-010	28295.13	30678+11	-205.00	0+00000	0.00000	0.00000	0,00000	-210.00	11.22			
.,.	Y685-010	28290.04	30677,93	-215,00	0+00000	0+00000	0.00000	0.00000	-220+00	11+22			
	<u>1085-010</u>	20220 01	306//+/6	-220+00 -075 00	0.00000	0.0000	0.00000	0.00000	-240.00	11 00	 	 	
ł	1080-010 Veor A1A	- べおく/ブ・おん - つつつづく ママ	303//+38		0.00000	0.00000	0.00000	0.00000	-250 00	11 22			
0	1003-010	202/4+//	00077+40		0100000	V • VUVUV	V * V U U U U	V + V V V V V	-200.00	11+22			
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$\gamma$		COMPOSITE	COMPOSITE	OF HID					DACE OF				
		CONCOLLE.	V OCOD	COMPORT OF	001 b	000000	1 FT A TO			CONCOLUTE UP.		· · · · · · · · · · · · · · · · · · ·	 
	HULE NU+	X-COCKD	1-00000	COMPOSITE	0000	COFFER	1.680	Z INC	LEVEL	COMPOSITE			
51	VOOF ATT	20700 74	70/00 07	15 00	0 00000	0 00000	0 00000	0 00000	10.00				
Ý	Y005 011	20377+31	30680.77	10,00	0.00000	0,00000	0.00000	0.00000	10.00				 
	1685-011	20374+11	308/7+23	5.00	0.00000	0.00000	0+00000	0.00000	40.00	11+41			
$\mathbf{a} \mid$	Y685-011	28388.90	308/7.49	~5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.41			
· · ].	Y685-011	28383+67	396/5+/3	-15+99	0+00000	0.00000	0.+00000		-20.+00	. 11+41.		n	
	YG85-011	28378.48	30674.01	-25.00	0.00000	0,00000	0.00000	0,00000	-30,00	11.41			•
$\sim$	YG85-011	28373.27	30672+27	-35.00	0.00000	0.00000	0.00000	0.00000	-40+00	11.41			
· [	Y685-011	28368+06	30670+54	-45+00	0.00000	0,00000	0.00000	0.00000	-50.00	11.41			 
	YG85-011	28362.77	30668.87	-55.00	0.00897	0.00082	0.00041	0.03036	-30.00	11.46			
-	YG85-011	28357.42	30667.31	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.44			
.)	Y685-011	28352.09	30665.79	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11+44	1		
	YG85-011	28346.73	30664.30	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.44			
	YG85-011	28341.35	30662.90	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.45			
2	YG8 <u>5-011</u>	28335.94	30661.54	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.45			 
ſ	YG85-011	28330.54	30660.18	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.45			
	YG85-011	28325,13	30658.82	-125,00	0.00000	0.00000	0.00000	0.00000	-130.00	11.45			
0	Y685-011	28319.70	30657.49	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.48			
1.	Y685-011	28314.16	30656.22	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.53			
	YG85-011	28308.55	30455.01	-155.00	0.00035	0.00000	0.00000	0.00000	-140.00	11.54			
$\mathbf{C}$	Y685-011	28302.91	30453.83	-165.00	0.00062	0.00000	0.00000	0.00000	-170.00	11.55			
T	Y685-011	28297.24	30452.73	-175.00	0.00055	0.00000	0.00000	0.00000	-180.00	11.55			 
1	VG05-011	202771.57	70451.49	-185.00	0 00000	0.00000	0.00000	0.00000	-190.00	11.55			
)	Y005-011	20271,00	30450.47	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.55			
	YOOR ALL	20200100	70/10 (5	005 00	<u>0 00000</u>		<u></u>		- 210 00	14 22			
	1000-011	20200+20	30047400	-200+00	0.00000	0+00000	0.00000	0.00000	~210+00	11+04			
3	Y685-011	28274+51	39648+54	-210+00	0.00000	0.00000	0.00000	0.00000	-220.00	11.30			
· -	1685-011	28268.83	30647+83		0.00000	0.00000	0.00000	0.00000	-230+00	11+33			 
-													
2				ELEVATION		1 - 1							
				OF MID									
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF			
1	HOLE NO+	<u>X-COORD</u>	<u>Y-COCRD</u>	<u>COMPOSITE</u>	<u> </u>	<u>COPPER</u>	I EAD	ZINC	LEVEL	COMPOSIIE			 · · · · · · · · · · · · · · · · · · ·
	Y685-012	28306+60	30703.73	15.00	0.00083	0.00000	0.00000	0.00000	10.00	14.45			
$\mathcal{D}$	Y685-012	28296+22	30703.30	5.00	0.00015	0.00000	0.00000	0.00000	0.00	14.39			
	Y685-012	28285.91	30702.93	-5.00	0.00000	0.00000	0,00000	0.00000	-10,00	14,36			
1	Y685-012	28275.60	30702.57	-15.00	0.02794	0.00000	0.00000	0.00000	-20.00	14.37			
)	Y685-012	28265.37	30702.22	-25.00	0.34624	0.00000	0.00000	0.00000	-30,00	14.27		_	 
ī	Y685-012	28255.32	30701.92	-35.00	0,57821	0,00000	0.00000	0.00000	-40.00	14.08			 
ļ	Y685-012	28245.52	30701.68	-45.00	0.05592	0.00000	0.00000	0.00000	-50.00	13.93			
	Y685-012	28235.91	30701.48	-55.00	0.11184	0.00000	0.00000	0.00000	-60.00	13.80			
	V005-012	29224.41	30701.32	-45.00	0.00291	0.00000	0.00000	0.00000	-20.00	17.79			
1	1000 VI2	10014 07	70701 15	- 75 00	A AAAAA	0 00000	0.00000	0 00000	-90.00	17 70			
5	1000-016	20210+70	30701+10	- 7 \ 7 + \ 7 \	····	0.00000	V + V V V V V	V + V V V V V	00+00	63 + 7 7			
-													 
				FLEHATION									
				CLEVHIJUR OF MID									
										UINTH OF	e e e e		
		CUMPUSIIE -	CUMPUSIIE	FUINI OF		0000000		7710	DHOE UP	Willin Ur Govenette			
	HULE NU.	X-000K0	1-00000	COMPUSITE	6060	UUPPER	LEAD	ZINC	LEVEL	COMPOSITE	•		
Ý L													 
	Y685-013	28308.64	30703.65	15.00	0.00000	0.00000	0.00000	0.00000	10,00	12+52			
,	Y685-013	28301.13	30702.99	5.00	0.00000	0.00000	0.00000	0.0000	0.00	12.52			
- í	7685-013	28273+63	30/02+34	-5,00	0.00000	0.00000	0+00000	0+00000	-10.00	12.52	1		
	YG85-013	28286.12	30701.68	-15.00	0.74449	0.01361	0.00821	0.07369	~20,00	12.52			
	YG35-013	28278.61	30701.02	-25.00	0.01069	0.00030	0.00363	0.03317	-30.00	12.52			

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(		20221 11	70700 77		0 01477	0 00000		0 00007	- 40 00	10 50			
51	1083-V13 VCOE-017	20271+11	30/00+3/	45 00	0 10755	0.00000	A 15974	0.04571	-40+00	12+02			
	1000-013	20203+00	70/00 05		0.07/05		A A1705			12+02			• • • •
	1680-013	20230+07	30677+03	-45 00	0.00040	0.000007 0.00007	0+01373 A 11400		-70.00	12+84			
$\gamma$	1000-010 V005-017	20240+07	30676+40	-75 00	0.04144	0.00000	0.00000	0 00149	-90.00	12+34			
Ż	1000 010	2.02.41400		/	VIV-1	( • ( / / / / / / / / / / / / / / / / /	0+00000	<u></u>	00+00	7 + V7			· · · · · · · · · · · · · · · · · · ·
$\supset$				ELEVATION						м.	• * *		
				OF MID									
		COMPOSITE	COMPOSITE	FOINT OF	,				BASE OF	WIDTH OF			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
$\sim$	YG85-014	28287.96	30728+18	15.00	0.00000	0.00000	0.00000	0.00000	10,00	14.33			
·	YG85-014	28277•70	30728+15	3+00	0+00000	0.00000	0+00000	0,00000	0,00	14:33			
1	Y685-014	28267+44	30728+13	-5.00	0.00000	0.00000	0.00000	0.00000	-10,00	14.33			
51	Y685-014 Yeef 014	2823/+18	30/28+11	-15.00	0.00000	0+00000	0.00000	0.00000	~<0,00	14.33			
1	1080-V14	2027/ /F	30/28.08	75.00	0,0000	0.00000	0.00000	0.00000	-30.00	14+00	· · · · · · · · · · · · · · · · · · ·		
	1085-014	20200+00	30728+08	-33+00	0.00000	0.00000	0.00000	0.00000	-40.00	14+33			
	1680-014	- XOXXO+40 - DOD1X D7	30720+04	-40,00	0.00000	0.00000	0.00000	0.00000	-40.00	14+20			
í	1000-014 V005-014	20210+27	30720 04	-45 00	0.00000	0.00000	0.00000	0.00000	-70.00	1 4 5 5	÷		
	100J-014 V005-014	20200+10	30720.04	-75 00	0.00000	0.00000	0.00000	0.00000	-20.00	14+20			
$\gamma$	Y685-014	28186.00	30728+04	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.18			
Ì	Y095-014	28175.97	30728.04	-95.00	0.00000	0.00000	0,00000	0.00000	-100.00	14.15			
	Y685-014	28145.94	30728.04	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.72			
)	roec, er i	7.072.000 47.0	00720101						1 2 0 4 0 0	1 1 1 7 2.			
. 1				ELEVATION									
)				OF MID									
		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF			
<b>,</b> 1	HOLE NO.	X-COORD	Y-CGORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
2													
1	Y685-015	28289.75	30728+20	15,00	0.00000	0.00000	0.00000	0.00000	10.00	12.02			
$\gamma$	YG85-015	28282+82	30728+37	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.17			
- 1   F	<u> </u>	282/3+89	30728+35	-5,00	0+00000	0.00000	0,0000	0.00000	-10,00	12.17			
i	1985-015 Vee5 015	28268+96	30/28+/2	-15,00	0.00000	0.00000	0.00000	0.00000	-20.00	12.17			
11	1683-013 V095-015	20202+04	30728+70	-25,00	0.00000	0.00000	0.00000	0.00000	-30,00	12+17			
	Y005-015	2020010	30727+95	-45.00	0.00000	0.00000	0.00000	0.00000	-======================================	·		÷.	
	1000-010	20240+10	30727+20 70700 AA	-55 00	0.000000	0.00000	0.00000	0.00000	-40.00	10 10			
)	Y685-015	28234.42	30729.66	-65.00	0.00015	0.00000	0.00000	0.00000	-70.00	10.11			
ł	Y685-015	28227.60	30729,91	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12,10			
i	Y685-015	28220.80	30730.14	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.10			
)	Y685-015	28213.99	30730.38	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.10			
	Y685-015	28207.18	30730.62	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.10			
					·····								
				ELEVATION									
.				OF MID									
		COMPOSITE	CUMPUSITE	PUINT OF					BASE OF	WINTH OF			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
A I	VOOR ALZ	00700 07	70700 07	18 00	* *****		0 00000	n ne		10			
· .	1003-V16	28308+87	30702.73	13.00	0.00000	0+00000	0.00000	0.00000	10,00	12.90			
Ì	1085-016	28300+76	30702+16	3.00	0.00000	0.00000	0.00000	0.00000	0.00	12,90			
	1000-016	- /8////+8/ 	30701+40	-3.00	0.00000	0.00000	0.00000	0.00000	-10.00	12+87			
.	4000-010 1000-010	00074 44	20100 01	-25 00	0 00000	0.00000	<u>. 0:00700</u> .	<u>. V+14010</u>	0U+00	10 04	· · · · ·		e e e e e
	Y325-010	202/0+01	30077+70	-23+00	0.00000	0.00000	0.00000	0.00000	-30,00	10 CA			
$\mathcal{D}$	10000-000	20200+07	07077+X3	<3+3 <b>↓</b> <7 <7	V + V V V V V	V + V V V V V	0+00000	0+00000	-40+00	12+04			
``	<b>Name</b>												

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_)	MOZART\$1	DUAD: FRESP	INDZA.TELLI	TNARENA04T.	BENJ2	11-AUG-198	6 14:11	Page 11		· · · · · · · · · · · · · · · · · · ·			
	$\left( \right)$							•					J
$\sim$	Y685-016	28260.57	30698.51	-45+00	0.00000	0.00000	0.00000	0.00000	-50.00	12.84			. 1
2	Y685-016	28252+57	30697.75	-35,00	0,00647	0,00000	0.00000	0+00000			 		1
	Y685-016	28244+72	30696+94	-65+00	0.01181	0.00072	0.00144	0+00576	-70.00	12.66			
	1080-016 Y095-014	28237+11	30676+07	-/3.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.54			;
	Y685-016	28222.10	30694.28	-95.00	0.00000	0.00000	0.00000	0.00000	-100 00	12 54	 		$\rightarrow$
	Y985-016	28214.59	30693.38	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.57			1
<b>)</b>									~~~~~~		· · ·		1
								Carlo on a contrat of the			 	· · ·	
<b>n</b>				ELEVATION									
2				OF MID							 		
		COMPOSITE	COMPOSITE	POINT OF	001 5	000000	1		BASE OF	WIDTH OF			
$\mathbf{a}$	HULE NU+	X-000KD	1-0.000400	CUMPUSITE	DULU	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
	Y095_017	20210 54	30707.70	15.00	0 00000	0 00000	<u> </u>	0 00000	10.00	4.4 7.5	· · · · ·		
	Y685-017	28304.63	30703.06	5.00	0.00000	0.00000	0.00000	0.00000	10+00	11+62			
)	YG85-017	28298.73	30702+82	-5,00	0.00000	0.00000	0.00000	0.00000	-10.00	11.62			
	Y685-017	28292.82	30702.59	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.61	 		
_	YG85-017	28286.95	30702.49	-25.00	0.01448	0.00138	0.00092	0.01886	-30.00	11.59			
2	YG85-017	28281.09	30702.49	-35.00	0+00026	0.00000	0+00000	0+00000	-40.+00	11.59			
	Y685-017	28275.23	30702.49	-45.00	0.00000	0.00000	0.00000	0+00000	-50.00	11.59			
5	Y685-017	28269.37	30702+49	-55.00	0.00181	0.00000	0.00000	0.00000	-60.00	11.59			
	<u>Y685-017</u>	28263.50	30702.49	-65,00	0.03383	0,00000	0.00090	0.00224	-70.00	11.60	 		
	1000-917 V005-017	- 2020/+02 - 2025/ 20	30702+97	-70+00	0.00078	0.00000	0.00000	0.00000	-80+00	11.61			4
$\mathbf{D}$	Y085-017	28245.72	30702.49	-95,00	0.84841	0.11858	0.02408	1 01745		11+04			
	Y685-017	28239.71	30702.49	-105.00	0.00064	0.00000	0.00000	0.00218	-110.00	11.67			
	YG85-017	28233.20	30702+49	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.66			
<u>)</u>	YG85-017	28227,70	30702.49	-125.00	0,00000	0.00000	0.00000	0.00000	-130.00	11.67	 		
	Y685-017	28221.69	30702,49	-135.00	0.00086	0.00000	0.00000	0.00000	-140.00	11.66			
	YG95-017	28215.68	30702.49	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.67			
.'	YG85-017	28209.67	30702.49	-155.00	0.00000	0.00000	0+00000	0+00000	-160.00	11.67			
	YG85-017	28203.66	30702.49	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	5.03			
)													
	·····			FLEUATION					· · · ·		 		
ĺ				OF MID									
)		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF			
1	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
,													
1	1685-018	28306+23	30705,18	15+00	0,00000	0,00000	0.00000	0.00000	10.00	14.86	 		
ĺ	1080-018 VCOE010	28270+47 Dobox 70	30707.00	5.00	0.00000	0.00000	0.00000	0.00000	0+00	14.75			
1	Y685-018	28274.11	30710.77	-15.00	0.00000	0.00000	0.00000	0.00000	-10.00	14+70			
1	YG85-018	28263.46	30712.68	-25.00	0.00725	0.00000	0.00000	0.00000	-30.00	14.71			
	Y685-018	28253.09	30714.74	-35.00	0.00288	0,00000	0.00000	0.00000	-40.00	14.40			
	YG85-018	28242.99	30716.93	-45.00	0.00021	0.00000	0.00000	0.00000	-50.00	14.37			
ļ	YG85-018	28232.98	30719.18	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.27	 		
.,	YG85-018	28223.07	30721.47	-65+00	0.00000	0,00000	0.0000	0.00000	-70.00	14.27			
	YG85-018	28213.15	30723.76	-75.00	0.00004	0.00000	0.00000	0.00000	-80.00	. 14+27			
	1685-018	28203+23	30/28.04	-85.00	0.15244	0.00840	0.01291	0.08607	-90.00	14.28			
	1000-010 VC25-010	- 20170+20 	30738+34	-105 00	0.77040	0+01026	0+001/1	0.09459	-100.00	14.30			
	YC85-018	28173.25	30732.97	-115.00	0.03590	0.00482	0.00107	0,00740	-120.00	14+04			
	YG85-018	28163.20	30735.29	-125.00	0,15579	0.00507	0.00169	0.03077	-130.00	8.08			
)									2004 00	0 + V 0			
				ELEVATION									
23	<u> </u>												,

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- NOVEVIANDA A CVCSLTBOVE	• I E E E E I REPERNENEV + I • DE N • Z	11-100-1700 14:11	F888 12

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$\sim$		COMPOSITE	COMPOSITE	OF MID	••				DARE OF	υγάτυ ος				
	HOLE NO.	X-COORD	Y-COURD	COMPOSITE	GOLD	COPPER	I.EAD	ZINC	LEVEL	COMPOSITE	 			
					•									
2 L	YG85-019	28234.36	30741.64	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.97	 •			
(	YG85-019	28223,75	30740.75	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.61				
	YG85-019	28213.14	30739.86	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.61				
2	YG85-019	28202.53	30738.98	-5,00	0,00000	0.00000	0.00000	0.00000	-10.00	14.60			· .	
	YG85-019	28191.96	30738.26	-15,00	0.00930	0.00967	0.39093	0.05064	-20.00	14+55				
	YG85-019	28181.42	30737+78	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14+53				
	YG85-019	28170.88	30737.41	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.53	 			
ſ	YG85-019	28140.37	30737+06	-45+00	0.00483	0.00120	0.00000	0.02637	-50.00	14.51				
	YG85-019	28149.94	30736.81	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.40				
0	Y685-019	28139.58	30736.63	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.40				
	YG85-019	28129.24	30736.45	-75.00	0.00393	0.00000	0.00000	0.00000	-80.00	14.37		-		
.	YG85-019	28118.97	30736.27	-85.00	0.00000	0+00000	0.00000	0.00000	-90.00	14.30				
	YG85-019	28108.77	30736.09	-95.00	0.00042	0.00000	0.00000	0.00000	-100.00	14.27	 			
ſ														
~ 1														
1				ELEVATION										
				OF MID										
~		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF				
1	HOLE NO.	X-COORD	Y-COURD	<u>COMPOSITE</u>	GOLD	<u>COPPER</u>	<u>I.EAD</u>	ZINC	LEVEL	COMPOSITE	 			
	YG85-020	28227.60	30740.86	15.00	0.00000	0.00000	0.00000	0+00000	10.00	12.19				
	Y085-020	28220.66	30740.21	5.00	0.00000	0.0000	0.0000	0.00000	000	12.19				
	YG85-020	28213.72	30739,55	-5.00	0.00000	0+00000	0.00000	0.00000	-10.00	12.19				
	YG85-020	28206.79	30738.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.19				
1	Y685-020	28199.85	30738,25	-25.00	0,00000	0,00000	0.00000	_0,00000	-30.00	12.19	 			
	YG85-020	28192.91	30737.60	-35.00	0.00000	0.00000	0,00000	0.00000	-40.00	12.19				
	YG85-020	28185.98	30736.95	-45.00	0.0000	0.00000	0.00000	0,00000	-50.00	12.19				
1	Y685-020	28179.04	30736.29	-55:00	0.00000	0.00000	0.00000	0.00000	-60.00	12.19				

YG85-020	28185.98	30736.95	-45.00	0.0000	0.00000	0.00000	0,0000	-50.00	12.19		
Y685-020	28179.04	30736.29	-55+00	0,00000	0+00000	0.00000	0.00000	-60.00	12.19		
YG85-020	28172.10	30735.64	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.19		
YG85-020	28145.15	30735.01	-75.00	0+00025	0,00000	0.00000	0.00000	-80.00	12.20		
YG85-020	28158.18	30734.40	-85.00	0,00000	0.0000	0.00000	0,00000	70.00	12.21		
 Y685-020	28151.21	30733.79	-95.00	0.0000	0.00000	0.00000	0.00000	-100.00	12.21		
		•									

				ELEVATION								
}		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF	 	
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE		
)	Y685-022	28225.28	30778.96	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.91		
	Y685-022	28218.25	30778.81	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.22		
	YG85-022	28211.22	30778.66	-5,00	0.00000	0.00000	0.00000	0.00000	-10.00	12.22		
1	Y685-022	28204.20	30778.51	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.22	 	
	YG85-022	28197.17	30778.36	-25,00	0,00000	0.00000	0.00000	0.00000	-30,00	12+22		
	YG85-022	28190.20	30778.31	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.16		
	YG85-022	28183.31	30778.39	-45.00	0.00000	0.00000	0+00000	0.00000	-50.00	12.13		
	YG85-022	28176.44	30778.50	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	12.13		
. 1	Y685-022	28169.56	30778.61	-65.00	0.00000	0.00000	0,0000	0.00000	-70.00	12.13		
1	<u>Y685-022</u>	28162.62	30778.76	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.22	 	
1	YG85-022	28155.60	30778.95	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.22		
	YG85-022	28148.56	30779.13	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.23		
)	Y685-022	28141.54	30779.32	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.22		
	Y685-022	28134.51	30779.51	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.22		
	YG85-022	28127.48	30779.70	-125.00	0.00000	0.00000	0,00000	0.00000	-130,00	12.22		
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0	Y685-022 Y685-022	28120.45 28113.42	30779.89 30780.08	-135.00 -145.00	0.00000	0.00000	0.00000	0.00000	-140.00 -150.00	12.22	· ····			•
)				ELEVATION						· .				
Э	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF COMPOSITE	GOLD	COPPER	I.EAD	ZINC	BASE OF	WIDTH OF COMPOSITE			· · ·	
Э	YG85-023 YG85-023	28227.12	30759.93 30759.51	25.00 15.00	0.00000	0.00000	0.00000	0.00000	20.00	5.51 15.05				· .
	YG85-023	28204+62	30759.09	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.06				
$\mathbf{O}$	1085-023 Y695-023	28182.12	30/08+68	-5+00	0.00000	0.00000	0.00000	0.00000	-10.00	15.03		,		
	Y685-023	28170.84	30757,85	-25.00	0.00017	0.00000	0,00000	0,00000	-30,00	15.10	. î.			•
	YG85-023	28159.55	30757.46	-35.00	0.00013	0.00000	0.00000	0.00000	-40.00	15,09				
)	Y685-023	28148.26	30757.07	-45,00	0.00000	0.00000	0.00000	0.00000	-50,00	15.09				
	YG85-023	28136.96	30756.67	-55.00	0.00000	0.00000	0.00000	0.00000	-60,00	15.10				
- )														
	··· · ··· · · · · · · · · · · · · · ·			ELEVATION OF MID								·		
)	T 14 19 10 10 10 10 10 10 10 10 10 10 10 10 10	COMPOSITE	COMPOSITE	POINT OF					BASE OF	WINTH OF				
-	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE				
	Y685-024	28219.99	30759.84	15.00	0,00000	0.00000	0.00000	0+00000	10.00	12.09				
	Y685-024	28213+20	30/59+/9	5+00	0.00000	0.00000	0.00000	0.00000	0.00	12.09				
)	Y685-024	28199.41	30759.70	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.09				
	Y685-024	28192.80	30759,70	-25,00	0.00016	0.00000	0.00000	0.00000	-30.00	12.11				
	YG85-024	28185.92	30759.80	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12,16				
)	Y685-024	28178.92	30760.05	-45.00	0,0000	0.00000	0.00000	0,00000	-50+00	12.26				
Í	YG85-024	28171.84	30760+38	-55.00	0+00000	0+00000	0+00000	0.00000	-60+00	12.26				
	Y685-024	28164.75	30760.72	-65.00	0.00000	0,00000	0.00000	0.00000	-70+00	12.26				
	1080-V24 V095-004	20150 50	30761+00	-95 00	0.00000	0.00000	0.00000	0.00000	-80.00	12.26				
Í	1000 024	20100100	00701407	~ 00+00	V+VVVVV	V • V V V V V	V+0000V	0.00000	-70+00	75420				
)				ELEVATION OF MID				/						
)		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF				
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE				
)	Y685-025	28163.80	30843.53	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.97				
	Y685-025	28152.77	30844.79	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14,95				
	YG85-025	28141.73	30846.10	~5.00	0.00000	0.00000	0.00000	0,00000	-10.00	14.95				
	Y685-025	28130.70	30847.46	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.95				
	YG85-025	28119.67	30848.81	-25.00	0.00000	0+00000	0,00000	0.00000	-30+00	11.87				
)														
	· · · ·		t t t tank i se te te - e - e energi et t talen be	ELEVATION OF MID	a e e									
1		<u>COMPOSITE</u>	COMPOSITE	FOINT OF					BASE_OF	WINTH OF				
, I	HOLE NO.	X-COORD	Ү-СООКЪ	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE				
	Y686-002	28308+65	30704.72	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.71				
	1684-002 Y684-002	28300.86	30705+62	5.00	0.00000	0,00000	0+00000	0.00000	0.00	12.71				
) [	1000-002	20273+90	av/ vo+ a/		0+00000	0.00000	0+00000	0.00000	-10+00	1.2.474				

)	MOZART\$	JUAO: ERESPI	INOZA.TELLI	TNABENA04T.	BEN#2	11-AUG-198	5 14:11	Pase 14					 
(													,
2	YG86-002	28285.26	30707.41	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.72			
'	Y <u>686-002</u>	28277.43	30708.26	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00				
1	YG86-002	28269.51	30709.09	~35.00	0.00016	0.00000	0.00000	0+00000	-40.00	12.83			-
-	YG86-002	28261.51	30709.93	-45.00	0.00000.	0.00000	0.00000	0.00000	-50.00	12.85			
) (	Y686-002	28253,48	30710.78	-55,00	0.00000	0.00000	0.00000	0.00000	-60.00	12,85			 
(	YG86-002	28245.46	30711.62	-65.00	0.00000	0.00000	0.00000	0.00000	-70,00	12.85			
$\sim$	YG86-002	28237.43	30712.46	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.86			
- 2	Y686-002	28229+35	30713+28	-85.00	_0.00000	0.00000	0.00000	0,00000	-90+00		·		
1	YG86-002	28221,23	30714.07	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.91			* .
~	YG86-002	28213.08	30714.84	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.94			
1	YG86-002	28204.84	30/15.53	-115+00	0.00086	0.00000	0.00000	0+00000	-120.00	13.02			 
	Y686-002	28196.48	30716+13	-125.00	0.00046	0.00000	0.00000	0.00000	-130.00	13.08			
$\neg$	YG86-002	28188.03	30716+69	-135.00	0.00015	0.00000	0.00000.	0.00000	-140+00	13.14		•	
,	Y686-002	281/9.49	30/1/+21	-145.00	0.00000	0+00000	0.00000	0+00000	-150+00	13+18			
	YG86-002	28170.88	30717+69	-155.00	0.00165	0.00000	0.00000	0.00000	-160.00	13.23			
- A 1	Y684-002	28162.15	30718.09	-165.00	1.58898	0.00128	0.00344	0.05991	-170+00	13.33			
1	Y686-002	28153.26	30718+35	-175.00	0.00349	0,00000	0.00000	0.00370	-180.00	13.44			 
	Y086-002	28144.24	30718.49	-185.00	0.00000	0.00000	0.00000	0+00000	-190.00	13.49			
I	and a second second	•		ET ETTATES									
				ELEVALION									
		COMPOSITE	COMPOSITE	POINT OF					DACE OF	UTDTU OF			
.	UNIS NO.	V-COORD	V-COORD	COMPOSITE	601.0	000050	1 5 40	7780	LCHCI				 
	HOCK NO+	X-COURD	1-000000	com obtre	0.000	GOFFER	L. E. 15 L4	7. I NO	LEVEL.	CONFUSITE			
$\mathbf{D}$	Y68A~005	28310.61	30704.12	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.33			
Į	Y686-065	28305.27	30704.21	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11,33			
	Y684-005	28299.94	30704.30	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.77			
)	Y686-005	28294.40	30704.40	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.33			
	Y684-005	28289.74	30704.48	-25.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.07			 
1	V884-005	28282.07.03	30704.54	-75.00	0.01272	0.00000	0.00000	0.00000	-40 00	11 77 /			
)	Y684-005	28279.04	30704.61	-45.00	0.00080	0.00000	0.00000	0.00000	-50.00	11.00			
	Y686-005	28273.97	30704.65	~55.00	0.00394	0.00000	0.00000	0.00000	-60.00	11.22			
[	Y686-005	28248.87	30704.70	-45.00	0.00071	0.00000	0.00000	0.00000	-70.00	11.22			
	Y686-005	28263.76	30704.73	/5,00	0.00030	0.00000	0.00000	0.00000	-80.00	11.24			
í	Y686-005	28258.59	30704.74	-85.00	0.00000	0.00000	0.00000	0.00000	-90,00	11,28			 
	Y086-005	28253.38	30704.74	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.27			
)	Y686-005	28248,18	30704.74	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.28			
	Y086-005	28242,94	30704.74	-115.00	0.20344	0.03970	0.00000	0+01453	-120.00	11.30			
	YG86-005	28237.67	30704.74	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.30			
	Y686-005	28232.41	30704.74	-135.00	0.00142	0.00000	0.00000	0.00000	-140.00	11.30			
I.	YG86-005	28227.16	30704+74	-145.00	0.00008	0.00000	0.00000	0.00000	-150.00	11.30			
	Y084-005	28221.90	30704.74	-155.00	0.00036	0.00000	0.00000	0.00000	-160.00	11.29			
)	YG86-005	28216.60	30704.78	-165.00	0.16835	0.00753	0.00000	0+06616	-170.00	11.34			
Í	Y686-005	28211.21	30704.85	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	11,37			
	Y686-005	28205.72	30704.97	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	11.45			
)	<u>YG86-005</u>	28200.13	30705.15	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.47			 
1	YG86-005	28194.51	30705.34	-205.00	0.00056	0.00000	0,00000	0.00000	-210.00	11,48			
.	Y686-005	28188.87	30705+57	-215.00	0.00839	0.00000	0.01310	0.05909	-220.00	11.49			
	Y686-005	28183.22	30705.84	-225+00	0,00000	0.00000	0,0000	0,00000	-230+00	. 11+49			
	YG86-005	28177.57	30706.11	-235.00	0+00000	0.00000	0.00000	0.00000	-240.00	10.53			
. 1													
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				ELEVATION									
· ·				OF MID									
/		CUMPUSITE	CUMPOSITE	PUINT OF					BASE OF	WINTH OF			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEI.	COMPOSITE			
· ·													
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	MUZARI¥J	<u>uuao;lresp</u> .	INUZA, TELL.	LINARE NACAL	BEN 2	<u>11-AUG-198</u>	6 14:11	Fage 15			· · · · · · · · · · · · · · · · · · ·
1	(										
	YG86-007	28311.89	30703.01	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.84	
	YG86-007	28307,77	30702.33	5.00	0.00000	0,00000	0.00000	0.00000			and the second second second second second second second second second second second second second second second
	YG86-007	28303.65	30701.66	-5.00	0.00000	0.00000	0.00000	0.00000	-10,00	10.84	•
	Y686-007	28299.54	30700.99	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.84	
1 A .	Y684-007	28295.35	30700.29	-25.00	0.00000	0.00000	0,00000	0.00000	-30.00	10,89	
	Y684-007	20201 01	30400.55	-75.00	0.04487	0.01914	0.00000	0.05536	-40.00	10.97	· · · · · · · · · · · · · · · · · · ·
	1000 007 VC04-007	20271401	20409 70	- 45 00	0 00000	0 00000	0 00000	0 00000	-50 00	11 04	
	1000-007	- 2020G+40 - 20201 00	70400 01	-55 00	0.00000	0.00000	0.00000	0.00000	-40.00	11 04	
	1000-007	20201100	30070+01		0.00000	<u></u>	0.00000				· · · · · · · · · · · · · · · · · · ·
	Y686-007	28277+28	30697+24	-83.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.04	
	Y686-007	28272+63	30696+48	-/5.00	0.00082	0.00000	0.00000	0.00000	-80.00	11.07	
	Y686-007	28267.86	30695.72	-85.00	0.36641	0.01651	0.03711	0.14810	-70.00	11+14	
i	YG86-007	28263.00	30694.98	-95.00	0+02990	0.01175	0.09718	0.13490	-100.00	11.15	
-	YG86-007	28258.12	30694.25	-105.00	0.44496	0.05331	0.05128	0.99438	-110.00	11.16	
	YG86-007	28253.20	30693.55	-115.00	0.00143	0.00000	0.00000	0.00000	-120,00	11.17	
	YG86-007	28248.27	30692.85	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.18	· · · · ·
	Y686-007	28243.33	30692.16	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11,17	
	YG86-007	28238.39	30691.46	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.17	
	Y684-007	28233.46	30690.77	~155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.17	
	Y686-007	28228.52	30490.07	-145.00	0.00000	0.00000	0.00000	0.00000	-170.00	4.51	
)	1000 447	10 10 10 10 10 + C1 K.	· · · · · · · · · · · · · · · · · · ·	200100	0	0.00000	0.00000		., .,	0401	
1											
				ELEVALIUN							
				<u>OF MID</u>							
		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF	
· ^	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE	
1										·	
	YG86-009	28313.09	30703.39	15.00	0,00000	0,00000	0.00000	0.00000	10,00	10.34	
	Y886-009	28310.46	30703.27	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.34	
. 3	YG86-009	28307.82	30703.14	-5.00	0,00000	0.00000	0,00000	0,00000	-10,00	10,34	
1	Y686-009	28305.18	30703.02	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.34	
	Y686-009	28302.54	30702.90	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.34	
$(\gamma)$	Y384-009	28299.90	30702.78	-35.00	0.00000	0.00000	0.00000	0.00000	-40,00	10.34	
	Y684-009	28297.27	30702.45	- 45.00	0.04794	0.02551	0.18824	0.14780	-50.00	10.34	
	Y000 007	28284.40	30702.50	-55 00	0.00000	0 00000	0.00000	0 00000	-40.00	10 74	
	1000-007 VG94-000	- 2027+0V - 20201 0A	30702431	-45 00	0.00000	0.00000	0.00000	0.00000	-70.00	10+30	
1	1000 007 VCO/ 000	20271170	70700 07	75 00		0 00000	<u>0+00000</u>			10 7/	
	1000-007	20207+21 00001 +0	39792+23	-/0.00	0.00000	0.00000	0.00000	0.00000	-80+00	10+38	
1	1386-009	20200+40	30702+07	~83.00	0.00404	0.00000	0.00000	0.00000		10.3/	
	1000-007	20200+73	30701+74	-73.00	0+000×2	0+00000	0.00000	0.00000	-100+00	10+38	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1	1989-008	28580*82	30/01.79	-105.00	0.00011	0.00000	0.00000	0.00000	-110.00	10,38	
. /	Y684-009	28278,18	30701+65	-115.00	0+00846	0.00000	0.00000	0.00000	-120.00	10.38	
	YG86-009	28275+41	30701.51	-125.00	0.00663	0,00000	0,00000	0,00000	-130.00	10.38	
	YG86-009	28272.64	30701.38	-135.00	0.00039	0.00000	0,00000	0.00000	-140.00	t0.38	
	YG86-009	28269.87	30701.29	-145.00	0.18525	0.02304	0.00000	0,01205	-150.00	10.38	
1	YG86-009	28267.10	30701.23	-155.00	0+00266	0.00000	0.00000	0+00000	-160.00	10.38	
1	YG86-009	28264.32	30701.19	-165.00	0.00027	0.00000	0.00000	0.0000	-170.00	5.86	
(				ELEVATION							
				OF MID							
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF	
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ចក) ក	COPPER	IFAD	7100	LEUEL	COMPOSITE	
1	11945-14 1337 B	N 99991313	1 10 10 10 10 10	CONTROLET	0.000	50 (0) 3 LUN	L. L. L. L.	ميا 31 سر بيا.	ta ba ¥in ta		
	Y684-011	28307.70	30700.70	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.77	
l	1000 VII	20007+70	70407 77		<u>0 00000</u>	<u> </u>	<u> </u>	A AAAAA	10+00	<u></u>	
	1000-011	20270+91	30077+33	0+00 E AA		0+00000	0.00000	0.00000	0.00	14+33	
		28288.3] 28278.5]	30374+11		0.01/33	0.00268	0.00067	0.0/1//	-10,00	14+27	
	1000-011	202/0+08	39671+11	<u> </u>	<u></u>	0.00000	_0.000000	0.00000	-20+00		and the second second second second second second second second second second second second second second second
l	1686-011	28268.85	30888+29	-25+00	0.00000	0.00000	0.00000	0.00000	-30.00	14.21	
	YG86-011	28259+13	30685+57	-35+00	0+00000	0,00000	0.00000	0.00000	-40.00	14.20	

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	MOZART\$	DUAO: ERESP:	TNOZA.TELLI	TNABENA04T.	BEN\$2	11-AUG-1986	14:11	Page 16						
(	Y694-011	28249.41	30492.88	-45.00	0.0000	0.0000	0.00000	0.0000	-50.00	14.20				
$\gamma$	Y686-011	28239.69	30680.28	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.17				
	YGS4-011	28229.98	30677.85	-65,00	0.00000	0.00000	0.00000	0.00000	-70.00	14.14	····			-
	Y686-011	28220.24	30675.56	-75.00	0.00042	0.00000	0.00000	0.00000	-80,00	14.14				
) (	Y684-011	28210.46	30673.49	-85.00	0.00088	0.00000	0.00000	0.00000	-90.00	14,14		 ·		
(	Y686-011	28200.65	30671.56	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.14				
0	YG86-011	28190.83	30669.65	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	14.14			· · · · ·	
5.7	Y686-011	28181.02	3066/+/4	-115.00	0.00000	0,00000	0.00000		-170.00				a a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a ser a	
	1000-011	XQ1/14X1	349991499	-120+00	0100000	0+00000	V•VVVVV	0+00000	-130+00	0+07				
0														
ſ				ELEVATION										
0			00V000775	OF MID					-					
9		CONFUSILE.	CUMPUSITE.	POINT OF	COLD	200000	1 5 4 5	7710	BASE UF					
	HULE NU+	X-COOKD	T-CODKD	CONFOSTER	(7)3 L D	COFFER	1.EAU	X I NL	LEVEL	CUMPUSLIE				
0	YG86-013	28309.60	30701.34	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.77				
Ī	YG84-013	28302.11	30698.71	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.77				
	YG86-013	28294.61	30696.14	-5.00	0.00000	0,00000	0,00000	0.00000	-10.00	12.76				
2	Y686-013	28286.98	30693.77	-15.00	0.05430	0.00894	0.04434	0.28419	-20,00	12.85				
	Y686-013	28279+13	30691.55	-25.00	0,00000	0.00000	0.00000	0.00000	-30,00	12.96				
5	Y686-013	28271+19	30687+36	~30+00	0.00000	0.00000	0.00000	0.00000	-40.00	12+96				
- 1	Y686-013	28255.04	30685.23	-55.00	0.00020	0.00000	0.00000	0.00000	-60.00	13.06		 		
	YG86-013	28246.84	30683.42	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	13.06				
0	Y086-013	28238+61	30681.77	-75.00	0.00000	0,00000	0.00000	0.00000	-80.00	13.06				
	Y686-013	28230.31	30680.27	-85.00	0.00000	0.00000	0.00000	0.00000	-90,00	13.10				
	Y684-013	28221.94	30678.90	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.12				
	Y686-013	28213.55	30677.60	-105.00	0.00000	0.00000	0.00000	0,00000	-110.00	13.12		 		
	YG84-013	28205.13	30676+33	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	13.15				
$\supset$	Y685-013 Y684-017	28196+68	306/5+12	-125.00	0.00000	0.00000	0.00000	0.00000	-130+00	13+15				
	Y684-013	28179,78	30672.74	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	6.94				
	1000 010									0				
$\rightarrow$		····		,								 		
				ELEVATION										
· >		COMPOSITE	COMEDETTE	UF MJD POINT OF					DAGE OF	UTDTU OC				
	HOLE NO.	X-COORD	Y-COORT	COMPOSITE	GOLD	COPPER	LEAD	7 TNC	IFVEL	COMPOSITE				
3	Y686-015	28311.64	30701.88	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11,28		 		····
ļ	Y686-015	28304.82	30699.86	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.28				
,	Y686-015	28302.00	30697.84	-5,00	0,00000	0,00000	0.00000	0.00000	-10.00	11.28				
	1000-01J	20277+10	30073+70	-25 00	0.00000	0.00000	0.00410	0.07071	-70.00	11.70				
	YG84-015	28287.32	30492.35	-35.00	0,00000	0.00000	0.00000	0.00000	-40.00	11.29				
	Y686-015	28282.32	30690.65	-45.00	0.00000	0.00000	0.00000	0.00000	50.00	11.32		 		
	Y084-015	28277.30	30688.98	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.32				
	YG86-015	28272.25	30687.32	-65,00	0.00000	0.00000	0.00000	0.00000	-70.00	11.33				
	YG86-015	28267+15	30685.69	-75.00	0.00018	0.00000	0.00000	0.00000	-80.00	. 11.36				
	Y686-015	28261,95	30684.10	-85.00	0.00017	0.00000	0.00000	0,0000	-90.00	11.40				
)	1686-015	28206+/1 282551.47	30682.00		0.00000	0.00000	0.00000	0.00000	~110.00	11 70				
··· [	Y884-015	28244.24	30679.53	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.39		 		-
	YG86-015	28241.01	30678.03	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.38				
	Y684-015	28235.79	30676.54	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.37				
	YG86-015	28230.63	30675.05	-145.00	0.00054	0,00000	0.00000	0.00000	-150.00	11.34				
1	YG86-015	28225.50	30673.58	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.33				

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3				ELEVATION						· - · · ·			
				OF MID						HYDTH OF			
21	UOL 5 NO	COMPOSITE	CUMPOSITE	PUINI UF	601.0	COPPER	1 FAD	ZINC	LEVEL	COMPOSITE			
$\rightarrow$	HULE NU.	X-COOKD	1-00080	CONTROLIC.	0.000	0.0111.018			for here V for the		 and the second sec		
	Y684-021	28313.26	30701.52	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.76			
3	Y686-021	28310.08	30699.13	5.00	0.00000	0.00000	0.00000	0.00000	000	10.76			
	Y686-021	28306.90	30696.75	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.76			
	Y686-021	28303.70	30694.38	-15.00	0.00000	0.0000	0.00000	0.00000	-20.00	10.77			
->	Y686-021	28300.46	30692.03	-25.00	0.02905	0.00704	0.00422	0.10841	-30.00	10.78	 		 
Г	Y686-021	28297.17	30689+69	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.79			
$\sim$	YG86-021	28293.83	30687.35	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.80			
	YG86-021	28290.49	30685.01	-55.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.00		1 .	
	Y686-021	28287.14	30682+66	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.80			
5	YG86-021	28283+77	30680.30	-75+00	0+00000	0.00000	0+00000	0.00000	-30.00	10.84			
	Y686-021	28280.36	306//+91	-85.00	0.00000	0.00000	0.00000	0,00000	-100.00	10.84	 		 
	Y686-021	28276.92	306/5+51	-93.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.84			
-,	YG86-021	28273+48	306/3+11	-105.00	0.00000	0.00000	0.00000	0.00000	-120.00	10.84	· · · ·		
	1686-021	28270.00	30070+79	105 00	0.00000	0 00000	0 00000	0 00000	-130.00	10.86			
	Y686-021	28266+60	30888+27	-1/3+00	0.00000	0.00000	0.00000	0.00000	-140.00	10.84			
>	Y686-021	28263.13	30355+86	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	10,86			
-	1086-021	28237.03	70440 00	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	9.86	 		
	1086-031	20200+10	39000+77	100+00	V + V V V V V			0100078					
> ↓													
i i				ELEVATION									
1				OF MID									
<u></u>		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WINTH OF	 		 
Ļ	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
	1101111 1001												
3	YG86-022	28284,63	30702.86	25.00	0.00000	0+00000	0.00000	0,00000	20.00	7.94			
i	Y686-022	28274+28	30702.59	15.00	0.00014	0.00000	0.00000	0.00000	10.00	14.40			
	YG86-022	28263.93	30702.32	5.00	0.04875	0.00838	0.00484	0.07029	0.00	14.39			
· · · [	YG84-022	28253.58	30702.04	-5,00	1,00107	0.05478	0.33837	1.36270	-10.00	14.40	 		 
	Y686-022	28243.23	30701.77	-15.00	0.04175	0.05618	0.59942	1.25751	-20.00	14.10			
									a sub-market and a				
				ELEVATION									
			CONDOCTO	OF MID					BARE OF	NUDTH OF			
-	101 5 10	CUMPUSIT	<u>CUNFUSIIE</u>	COMPOSITE	601.0	COPPER	ΙΕΔΠ	7100	I FUFI	COMPOSITE	 		 
1	HULL NO.	χ-υουκυ	1-00080	COMPUSITE.	0020	GOLL CN	1.671	7 ± 14 U	To have \$\$ 1 to 5.00	00111 00110			
	V694-007	26288.44	30724.25	15,00	0.00000	0.00000	0.00000	0.00000	10.00	15.24			
	Y604-007	20200.00	30717.32	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.24			
The second second second second second second second second second second second second second second second s	1000-020	202771.24	30710.47	-5.00	0.00088	0.00000	0.00000	0.00000	-10.00	15.25			
,	Y686-023	28260.90	30703+75	-15.00	0.04439	0.04748	0.35873	0.53969	-20.00	15,24	 		 
-	Y686-023	28251.54	30697.16	-25.00	0.01553	0.00500	0.03160	0.10143	-30.00	15.16			
1	Y686-023	28242.21	30690+62	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15.15			
	YG86-023	28232,90	30684,10	-45.00	0.00000	0,00000	0.00000	0.00000	-50.00	15.12			
1	Y686-023	28223.60	30677.60	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	15.12			
1	Y686-023	28214,31	30671.09	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	15.12			
,	YG86-023	28205.04	30664.60	-75.00	0.00238	0.00000	0.00000	0.00000	-80,00	15.09	 		 
Ī													
				ELEVATION									
1				OF MID					DACE OF	MITTH OF			
. ;		COMPOSITE	CUMPOSITE	FUINT OF					DHOC UP	within of			
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)	HOZART\$1	UAO: ERESP1	NOZA . TELLI	ITNABENA04T.	BEN12	11-AUG-198	6 14:11	Pase 19			· · · · · · · · · · · · · · · · · · ·		
с) (	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE			
$\gamma$	Y686-024 Y686-024 Y686-024	28273.13 28266.14 28259.15	30714.01 30707.72 30701.42	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.87			
~ >	V094-024	28252.14	30/01-12	~5.00	0.00000	0.00000	0.00000	0.00000	-10.00	17.77			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
0	YG86-024	28245.18	30688.85	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.69			
5				ELEVATION OF MID								· ·	
0	HOLE NO.	COMPOSITF X-COORD	COMPOSITE Y-COORD	POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WIDTH OF COMPOSITE			
	Y686-025	28290,29	30725.62	15.00	0.00000	0.00000	0.00000	0,00000	10.00	13.08			
i	Y686-025	28283.43	30720.73	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.08			
- D	Y686-025	28276.53	30715.91	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.05			
Ī	Y686-025	28269.60	30711.18	-15.00	0.00225	0.00000	0.00000	0.00000	-20.00	13.06			
1	Y686-025	28262.65	30706.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.05			
0	Y686-025	28255.69	30701.79	-35.00	0.10859	0.04589	0.58169	0.46592	-40.00	13.06			
	Y686-025	28248.73	30697.10	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	13.05			
	Y686-025	28241.80	30692.46	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	13.00			
01	Y686-025	28234.92	30687.90	-65,00	0.00000	0.00000	0.00000	0.00000	-70.00	12,94			
i	Y684-025	28228+07	30483.38	-75,00	0.00000	0.00000	0.00000	0,00000	-80.00	12.94			
1	Y686-025	28221.22	30678.88	-85,00	0.00000	0.00000	0.00000	0.00000	-90.00	12.93			
)	Y686-025	28214.40	30474.42	-95.00	0.00013	0.00000	0.00000	0.00000	-100.00	12.87			
	Y002_075	28207.41	70470.01	-105.00	0.00045	0.00000	0.00000	0 00000	-110.00	17 07			
1	1000-020 V004-025	20207401	20445 50	-115 00	0.00000	0.00000	0.00000	0 00000	-120.00	10 07			
-)	1000-020	2.02.97 + 03.	30000+37	- CX -3 + V/V	V + V V V V V	0.00000	V+VVVVV	0100000	-140.00	14+00			
5		20Magette	COMPOSIT	ELEVATION OF MID					THOP OF	1177.711			
		CONFUSIIE	CUNFUSIIE	PUINI UP	001.0		1 <b>277</b> 4 <b>3</b> 74	T T 115	DASE UF	WINTH UP			
· ,	HULE NU.	х-сооки	1-00080	COMPUSIE	0010	UDFFER	1.1.4.0	ZINC	LEVEL	CUMPUSITE			
	V604-004	20227 74	70710 10	05 AA	0.00000	0 00000	<u> </u>	<u> </u>	20 20	·····			
	1000-V20 V004-004	- 20270+00 	30714+10	15 00	0.00000	0.00000	0.00000	0.00000	10.00	1.440			
	1000-020	- 20207+VZ - 2022A - 20	30710+31	10400	0.00000	0+00000	0+00000	0.00000	10+00	11400			
		20204+70	70700 50		0.00000	0.00000		1 00150	10.00	ុងដេខ្លាស ខ្លាស	100 C		
1	Tupphilo	26200+47	30702+37	-0+00	0+04<77	0+0400<	1.414110	1*00105	-10+00	11:00			
Ē		· · · ·		FLEUATTON									
		4		DE MID									
$\rightarrow$		COMPOSITE	COMPOSITE	POINT OF					BAGE OF	ытаты ог			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	I.EAD	ZINC	LEVEL	COMPOSITE			
; ]	Y694-007	28281 27	20707 00	15 00	0.00000	0.00000	0.00000	0 00000	10.00	11 70			
ſ	Y000 V27	202007 04	70727 24	<u> </u>	0.00000	0.00000	0.00000		10:00	<u> </u>			
ĺ	1000 V27 VC04-007	20207407	7072.7420	- 5 00	0 00000	0.00000	0.00000	0+VVVVV		11 70			
	1000-027	20202+33	30723+47	-15 00	0.00000	0.00000	0.00000	0.00000	~10.00	11+37			
	1000502/	204//+00	<u></u>		0.00000	0.00000	0.00000	0+00000		. 11+37 . ++ ⇒c			
	1000-027	20272+70 	30713470	-23+00 -25 AA	0.00000	0.00000		0.00000	~30.00	11+37			
· · ]	1000772/	<pre></pre>	30713417			0.000000	0+00000	0+00000 2 2222	-40+00 E0 00	44 7E			
	1000-02/	20203+37	30710+47	<u></u>	<u></u>	0.00000	0.00000	0.00000		<u> </u>			
1	Y686-027	28258.91	30/07.84	-55,00	0.00000	0.00000	0.00000	0.00000	-30.00	11.35			
, 1	1686-027	28254.25	30/05+18	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.34			
· '	1686-027	28249+58	30/02+52	-/5+00	0+001/5	0.00000	0.00000	0,00000	-80+00	11.36		·	
	Y686-027	28244.87	30679.85	-85,00	0.18104	0.06848	0+00858	0.25510	-90.00	11.39			
	YG86-027	28240.07	30697.17	-95.00	0.00045	0.00000	0.00000	0.00000	-100.00	11.43			
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ୀ	Y684-027 Y686-027	28235.24 28230.39	30694.48	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.43				
0	YG86-027 YG86-027	28225+55 28220+71	30689+11 30686+42	-125.00 -135.00	0.00000	0.00000	0.00000	0.00000	-140.00	7.13				
a				ELEVATION										
21		and the second s		UF MID										
		COMPOSITE	COMPOSITE	PULNI UF	aci n	005555			BASE OF	WIDTH OF		•		
O	HULE NU.	X-COORD	Y-COURD	COMPUSITE	GOLD	CUPPER	LEAD	ZINC	LEVEL	COMPOSITE				
Ī	Y686-028	28284.95	30731.77	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.50				
01	YG84-028	28276+65	30723+32	5.00	0.00000	0+00000	0+00000	0.00000	0.00	15.50				
2	Y686-028	28267+96	30/14+88	-5.00	0.00025	0.00000	0.00000	0+00000	-10.00	15,92				
	Y686-028	28258,75	30706+50	-15.00	0.00249	0.00000	0.00000	0+00000	-20.00	16.02				
3	Y686-028	28249+42	30698+21	-25.00	0.13049	0.00000	0.00000	0,0000	-30.00	15.96				
1	<u>1686-028</u>	28240.01	30690+14		0.00000	0.00000	0.00000	0.00000	-40.00	15+90			 	
	Y686-028	28230+49	30682+26	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	15,89				
2	YU86-028	28220.74	306/4+44	-00.00	0.00000	0.00000	0.00000	0.00000		13,89				
1	1686-028	28211+37	30000+01		0+00000	0.00000	0.00000	0+00000	=/0+00	10.67				
	Y686-028	28201+79	30658+80	-/5+00	0.00013	0.00000	0.00000	0.00000	-80.00	10,89				
-	Y686-028	28192+09	30301+20	-83.00	0.00000	0,00000	0.00000	0,00000	-90.00	13+89				
1	1000-020	20102400	_30043.07		0.00000	0400000	0+00000	0.00000	-100+00	7+00			 	
31				CLERATION										
				CELEVALION							· · ·			
1				UF DID						سويمر ودميس سورور				
		COMPOSITE	COMPOSITE	PUINI OF		005555	1		BASE OF	WINTH OF				
	HULE NU.	X-COURD	<u>Y-COURD</u>	CUMPUSITE	13UL II	LUFFER_	LEAU	<u>21NU</u>	LEVEL	CUMPUSITE			 	
ļ		00007 /0	70774 41	15 00	A AAAAA	~ ~~~~	A AAAAA	~ ~ ~ ~ ~ ~ ~	+ 0 00	10 0/				
$\mathbb{D}^{+}$	Y886-029	28287+62	30734+41	10.00	0.00000	0.00000	0.00000	0.00000	10.00	12+06				
	Y086-029	28282+78	39727+32		0.00000	0.1000000	0.00000	_0+00000		12+06				•
1	Y686-029	28278+34	30724+63	-5+00	0.00000	0.00000	0.00000	0,00000	-10+00	12.06				
	Y686-029	28273+69	30719+/3	-15.00	0+00021	0+00000	0.00000	0.00000	-20.00	12.06				
	1686-029	28269.04	30/14+84	-23.00	0.0008	0.0000	0.00000	0,00000	~30.00	12.06			 	
-	Y686-029	28264+40	30709.95	-35+00	0.00015	0.00000	0+00000	0+00000	-40+00	12.06				
1	Y686-029	28259.76	30705.06	-45.00	0.00238	0.00000	0.00000	0.00000	-50.00	12.06				
	Y086-029	28255+12	30/00+16		0+02503	0+00082	0+00082	0+05854	-60+00	12+06	· · · ·			
1	YG86-029	28250,48	30695+27	-65.00	0,39434	0.07419	0.19247	0.35375	-70.00	12.07				
. 1	Y386-029	28245.83	30690.38	-75.00	0.00004	0.00000	0.00000	0.00000	-80.00	12.06				
1	<u>YG86-029</u>	28241.19	30685.48	-85+00	0.00000	0.00000	0.00000	0.00000	-90,00	12.06			 	
	YG86-029	28236+54	30680+59	-95+00	0.00000	0,00000	0.00000	0+00000	-100.00	12.06				
	Y686-029	28231.90	30675.69	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12,06				
1	Y684-029	28227+26	30670.80	-115.00	0.00001	0,,00000	0+000000	0+00000	-120.00	12.04				
1	Y086-029	28222.62	30665.91	-125.00	0.00033	0,00000	0.00000	0.00000	-130.00	12,07				
	Y886-029	28217.98	30661.02	-135.00	0.00000	0.00000	0.00000	0+00000	-140.00	15.09				
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				ELEVATION										
1				OF MID										
1		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
~	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	GOLD	COPPER	I.EAD	ZINC	LEVEL	COMPOSITE				
21													 	
	YG86-030	28289.16	30735+73	15.00	0.00000	0.00000	0+00000	0.00000	10.00	10.85				
	YG86-030	28286.49	30732+43	5,00	0.00000	0.00000	0.00000	0.00000	0.00	10.86				
2	YG86-030	28283.82	30729.13	~5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.86				
	YG86-030	28281.15	30725+83	-15.00	0.00000	0.00000	0.00000	000000	-20+00	10.86				
	YG86-030	28278.47	30722.54	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.86				
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$\sim$	YG86-030	28275.80	30719.24	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.86		
- 1	Y686-030	28273.13	30715.94	-45.00	0.00037	0,00000	0+00000	0.+00.000	5000			in a second contraction of the
	YG86-030	28270,46	30712.64	-55.00	0.00000	0.00000	0,00000	0.00000	-60,00	10.86		
21	YG86-030	28267.79	30709.34	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.86		
23	Y686-030	28265.12	30706.04	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.86		
(	YG86-030	28262+45	30702.74	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.86		
$\sim$	YG86-030	28259.77	30699.44	-95,00	0.00386	0.00000	0.00000	0.00000	-100.00	10.86		
2	YG86-030	28257.10	30696.14	-105.00	0.48468	0.05417	0.+04040	.0.+32672		10.86		
1	YG86-030	28254.43	30692.85	-115.00	0+02478	0.00728	0.00000	0.84707	-120.00	10.86		
2	YG84-030	28251.76	30689.55	-125.00	0+00000	0.00000	0.00000	0.00000	-130.00	10.50		
- ' L												
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$\gamma$				ELEVALIUN								
$\sim$	and the second second	noveoster								e de la companya de l		
	1101 7 110	CUMPUSITE	CUMPUSITE	FUINE OF	201 5	0000000		7710	BASE OF	WIDTH OF		·
$\mathbf{O}$	HULE NU.	X-CUURD	Y-своко	CUMPUSLIE	GOLD	COPPER	LEAN	ZINC	LEVEL	COMPOSITE		
	Y084-071	28277.72	30745.70	15.00	0.00000	0.00000	0.00000	0.00000	10.00	17 00		
l	Y694-071	28270.74	30730.70	5.00	0.00000	0.00000	0.00000	0.00000	1 V V V V	13,00		
5	Y684-071	28262.96	30733.71	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	17 00		
	1000 001	- <u>100000, 70</u>	30727.71	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.00		
	Y006-031	20200400	70721 71	-25.00	0.00000	0.00000	0.00000	0.00000	-70.00	13,00		
3	1000-001	20240+20	30715.70	-75.00	0.00000	0.00000	0.00000	0.00000	-40.00	10+00		
·	V004-071	2023017	30709.94	- 45,00	0.02277	0.00007	0.02447	0.05704	-50 00	17 04		
	1000-001	20200+10	30707+70	-90.00	0.002207	0.00147	0.00204	0+03304	-40.00	13+00		
1	1000-001	- AGAKU(10 	70100 11	-45 00	0 00000		0 00000		-70 00	13+00		
	1006-031	- 40417404 - 40417404					$\sim 0.000000$	0.00000	70+00.	. 10+01. 17 01		
	1000-031	20207+00		-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13+81		
31	1000-VSI Y694-071	20202+00	30007+00	-95 00	0.00000	0.00000	0.00000	0.00000	-100.00	13+01		
1 - F	1000-001		0.0000043.7	7.5+9.9	V+VVVVV	V+VVVVV	VIVVVV	V+VVVVV		10+01		
зГ				FIFUATION								
э			· · · · · · · · · · · · · · · · · · ·	ELEVATION								
э		COMPOSITE	COMPOSITE	ELEVATION OF MID POINT OF	. No				BASE OF	ыртн оғ		
э 	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	I.EAD	ZINC	BASE OF LEVEL	WIDTH OF Composite		
	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF LEVEL	WINTH OF COMPOSITE		
э ->	HOLE NO. Y686-032	COMPOSITE X-DOORD 28279.17	COMPOSITE Y-COORD 30747.09	ELEVATION OF MID POINT OF COMPOSITE 15.00	GOLD 0.00000	<u>COPPER</u> 0.00000	LEAD 0.00000	ZINC 0.00000	BASE OF LEVEL 10.00	WIDTH OF COMPOSITE 11.88		
	HOLE ND. Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04	COMPOSITE Y-COORD 30747.09 30743.24	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00	GCLD 0.00000 0.00000	COPPER 0.00000 0.00000	LEAD 0.00000 0.00000	ZINC 0.00000 0.00000	BASE OF LEVEL 10.00 0.00	W1DTH OF COMPOSITE 11.88 11.88		
	HOLE NO. Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90	COMPOSITE Y-COORD 30747.09 30743.24 30739.39	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00	GCLD 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.00 -10.00	W1.5TH OF COMPOSITE 11.88 11.88 11.88		
	HOLE NO. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00	GOLD 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.00 -10.00 -20.00	W10TH OF COMPOSITE 11.88 11.88 11.88 11.88		
	HOLE NO. YG86-032 YG86-032 YG86-032 YG86-032 YG86-032 YG86-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28258.64	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00	GOLD 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000	BASE DF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00	W1.0TH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88		
	HOLE NO. YG86-032 YG86-032 YG86-032 YG86-032 YG86-032 YG86-032 YG86-032	COMPOSITE X-COORD 28279.17 28224.04 28268.90 28263.77 28258.64 28253.51	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00	GOLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE DF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00	W1.5TH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88		
	HOLE NO. YG86-032 YG86-032 YG86-032 YG86-032 YG86-032 YG86-032 YG86-032 YG86-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28258.64 28253.51 28248.37	COMPOSITE Y-COORD 30747.09 30743.24 30735.55 30735.55 30731.71 30727.86 30724.02	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00	W107H OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88		
	HOLE NO. YG84-032 YG84-032 YG84-032 YG84-032 YG84-032 YG84-032 YG84-032 YG84-032 YG84-032 YG84-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28258.64 28253.51 28248.37 28243.24	COMPOSITE Y-COORD 30747.09 30743.24 30735.55 30731.71 30727.86 30724.02 30720.17	ELEVATION OF MID POINT CF COMPOSITE 15.00 -5.00 -15.00 -25.00 -45.00 -55.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00	W107H OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88		
	HOLE NO. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28258.64 28253.64 28248.37 28248.37 28243.24 28237.98	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -5.00 -15.00 -25.00 -45.00 -65.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00	WIDTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92		
	HOLE NO. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28258.64 28253.51 28248.37 28243.24 28237.98 28232.54	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.87	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -65.00 -75.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00	WIDTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92		
	HOLE ND. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28224.04 28268.90 28263.77 28253.51 28248.37 28243.24 28243.24 28243.24 28243.24 28243.24 28243.24 28243.24	COMPOSITE Y-COURD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.87 30709.44	ELEVATION DF MID POINT CF COMPOSITE 15.00 -5.00 -5.00 -35.00 -45.00 -45.00 -45.00 -55.00 -65.00 -75.00 -85.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -70.00	WINTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.94 11.96		
	HOLE ND. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28253.51 28248.37 28237.54 28237.54 28237.54 28232.54 28226.98 28221.35	COMPOSITE Y-COURD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.87 30709.44 30706.05	ELEVATION DF MID POINT CF COMPOSITE 15.00 -5.00 -5.00 -35.00 -45.00 -55.00 -45.00 -55.00 -55.00 -75.00 -75.00 -75.00 -75.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00194 0.00194 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -90.00 -100.00	WINTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.94 11.97		
	HOLE ND. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28253.51 28248.37 28243.24 28237.98 28232.54 28222.58 28222.54 28222.54 28221.35 28221.35	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.89 30709.44 30706.05 30702.68	ELEVATION BF MID POINT CF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -45.00 -55.00 -75.00 -75.00 -75.00 -0 -75.00 -105.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.00194	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -90.00 -100.00 -110.00	WINTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.92 11.94 11.97 6.27		
	HOLE ND. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28253.51 28248.37 28243.24 28237.98 28232.54 28222.54 28222.54 28221.35 28215.69	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30714.45 30712.87 30709.44 30709.44	ELEVATION BF MID POINT CF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -45.00 -55.00 -75.00 -75.00 -0 -75.00 -105.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00194 0.00194 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -90.00 -100.00 -110.00	WINTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.92 11.94 11.97 6.27		
	HOLE ND. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28253.51 28248.37 28243.24 28237.98 28232.54 28226.98 28226.98 28221.35 28215.69	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.89 30709.44 30706.05 30702.68	ELEVATION BF MID POINT CF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -45.00 -55.00 -75.00 -75.00 -105.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.00194	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -90.00 -100.00 -110.00	W1DTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.92 11.94 11.97 6.27		
	HOLE ND. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28253.51 28248.37 28243.24 28237.98 28232.54 28226.98 28226.98 28221.35 28215.69	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.89 30709.44 30706.05 30702.68	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -45.00 -55.00 -75.00 -75.00 -0 -105.00 ELEVATION	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.00194	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -90.00 -100.00 -110.00	WINTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.92 11.94 11.97 6.27	· · · · · · · · · · · · · · · · · · ·	
	HOLE ND. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28253.51 28248.37 28243.24 28237.98 28237.98 28232.54 28226.98 28221.35 28215.69	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30714.45 30712.87 30712.87 30709.44 30706.05 30702.68	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -65.00 -75.00 -75.00 -105.00 ELEVATION OF MID	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.00194	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -70.00 -90.00 -110.00	W) DTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.94 11.97 6.27	· · · · · · · · · · · · · · · · · · ·	
	HOLE ND. Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28253.51 28248.37 28243.24 28237.98 28237.98 28232.54 28226.98 28221.35 28215.69 COMPOSITE	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.87 30709.44 30709.44 30706.05 30702.68	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.09 -65.00 -75.00 -75.00 -25.00 -25.00 ELEVATION OF MID FUINT OF	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -70.00 -100.00 -110.00 BASE OF	WINTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.94 11.97 6.27 WINTH OF	· · · · · · · · · · · · · · · · · · ·	
	HOLE NO. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28253.51 28248.37 28243.24 28237.98 28237.98 28232.54 28226.98 28221.35 28215.69 COMPOSITE X-COORD	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.87 30709.44 30709.44 30709.44 30709.48 COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -5.00 -25.00 -35.00 -45.00 -55.00 -65.00 -75.00 -65.00 -75.00 -25.00 ELEVATION OF MID POINT OF COMPOSITE	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.0000000 0.000000 0.000000 0.00000000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -70.00 -70.00 -70.00 -100.00 -110.00 BASE OF LEVEL	W1DTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.94 11.94 11.97 6.27 WIDTH OF COMFOSITE	· · · · · · · · · · · · · · · · · · ·	
	HOLE NO. Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032 Y684-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28258.64 28253.54 28248.37 28248.37 28248.37 28243.24 28237.98 28232.54 28226.98 28221.35 28215.69 COMPOSITE X-COORD	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.87 30709.44 30705.44 30705.46 30702.68 COMPOSITE Y-COORD	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -5.00 -25.00 -45.00 -45.00 -55.00 -65.00 -75.00 -65.00 -75.00 -25.00 ELEVATION OF MID POINT OF COMPOSITE	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.00194 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.000000 0.0000000 0.0000000 0.00000000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -70.00 -100.00 -100.00 -110.00 BASE OF LEVEL	WIDTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.94 11.94 11.97 6.27 WIDTH OF COMPOSITE	· · · · · · · · · · · · · · · · · · ·	
	HOLE NO. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28258.64 28253.53 28243.24 28237.98 28243.24 28237.98 282232.54 28226.98 28221.35 28215.69 COMPOSITE X-COORD 28280.42	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30720.17 30716.45 30712.87 30709.44 30709.44 30702.68 COMPOSITE Y-COORD 30748.03	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -45.00 -45.00 -55.00 -65.00 -75.00 -75.00 -75.00 -75.00 -105.00 ELEVATION OF MID POINT OF COMPOSITE 15.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -70.00 -70.00 -70.00 -100.00 -110.00 BASE OF LEVEL 10.00	WIDTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.94 11.94 11.94 11.97 6.27 WIDTH OF COMPOSITE 10.79	· · · · · · · · · · · · · · · · · · ·	
	HOLE NO. Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-032 Y686-033 Y686-033 Y686-033	COMPOSITE X-COORD 28279.17 28274.04 28268.90 28263.77 28258.64 28253.51 28248.37 28243.24 28237.98 282232.54 28226.98 28221.35 28215.69 COMPOSITE X-COORD 28280.42 28277.21	COMPOSITE Y-COORD 30747.09 30743.24 30739.39 30735.55 30731.71 30727.86 30724.02 30720.17 30716.45 30712.87 30709.44 30705.05 30702.68 COMPOSITE Y-COORD 30748.03 30745.56	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -45.00 -45.00 -65.00 -75.00 -65.00 -75.00 -75.00 -05.00 ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00	GCLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00142 0.00194 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 -70.00 -100.00 -100.00 -110.00 BASE OF LEVEL 10.00 0.00	WIDTH OF COMPOSITE 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.88 11.92 11.92 11.94 11.94 11.94 11.97 6.27 WIDTH OF COMPOSITE 10.79 10.79	· · · · · · · · · · · · · · · · · · ·	

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1000-	/33 <02/·	+00	70743+00	-0+00	0.00000	0.00000	0+00000	0.00000	-10.00	10+79				
	33 2827	+ / 7	30740.61		0.00000	0.00000			-20,00	10.79				
Y684-4	33 2826	+58	30738+14	-25,00	0+00000	0.00000	0+00000	0+00000	-30,00	10.79				
YG86-0	33 2826-	•37	30735.67	-35.00	0+00000	0.00000	0.00000	0.00000	-40,00	10.79				
Y686-0	33 2826	.15	30733.21	-45.00	0.00140	0.00000	0.00000	0.00000	-50.00	10.79				
Y686-0	33 2825	.93	30730.77	-55,00	0.00330	0.00000	0.00000	0.00000	-60,00	10.79				
Y686-4	33 2825	.71	30728.33	-65.00	0.00253	0.00000	0.00000	0.00000	-70.00	10.79				· .
YG8A-0	33 2825	. 48	30725.90	-75.00	0.00056	0.00000	0.00000	0.00000	-80.00	10.79				
	00 2020. 77 000A	00			A	0.00000	0.00000	0.00000	-00.00	1 V + 7.7				
1000-1	/33 2024/ 	+ 2 4	30743+34	-03.00	0+00000	0+00000	0.00000	0.00000	-70+00	10+79				
1086-9	133 28244 TT 0004	+ 7 2	30721+18	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.78				
1086-0	33 2824	+ 6 2	30718+83	-105.00	0+00000	0.00000	0.0000	0+00000	-110.00	10,79				
Y686-0	33 28238	•32	30716.52	-115.00	0.00000	0.00000	0,00000	0.00000	-120.00	10.79				
YG86-1	33 2823	+01	30714.20	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.79				
Y686-0	33 2823:	+68	30711.91	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.79		•		
Y684-	33 2822	. 34	30709.45	-145.00	0.00216	0.00000	0.00000	0.00000	-150.00	10.79				
VCOL	77 2000	60	70707 70	_155 AA	0 00027	0 00000	0 00000	0.00000	-140.00	10 70				
1000-1		+ 7 7	30707+39	-170+00	0.00028	0.00000	0.00000	0.00000	-100.00	10.78				
				FIGUATION										
			·	OF MID										
	COMPOS	ITE	COMPOSITE	POINT OF					BASE OF	WINTH OF				
HOLE	0, Y-CO	R D	Y-00080	COMPOSITE	GOUN	COPPER	FAD	7 T N C	IFUEL	COMPOSITE				
11 <b>0</b> 1.12		17.13	1 0000000	0000 000416	1999 A. S. L.	sologija (CAV	1 <b>1.1 J.1</b>		1a tan ¥ila tan	COULDOTIE				
	74 0001	~ ~	70707 / .			<u> </u>	0 00000							
Y 686-0	34 2826:	+03	30723+11	25.00	0+00000	0.00000	0.00000	0.00000	50+00	7+72				
Y684-0	34 2825:	+63	30716.90	15.00	0.00000	0.00000	0+00000	0,00000	10.00	13.90				
Y683-(	34 28240	+ 24	30710.69	5.00	0.00000	0,00000	0.00000	0.00000	0.00	13.90				
Y686-(	34 28238	+84	30704.49	-5.00	0.00145	0.00000	0.00000	0.00000	-10.00	13.90				
YGRA-	34 2823	. 44	30698.28	-15.00	0.54584	0.08074	0.29481	0,44803	-20.00	13.90				
Y684-4	34 2822	.05	30692107	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.58				
	and the second s				4.00000						· · · · ······························			
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	COMPOS	ITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
HOLE	COMPOS 0, X-CO	ITE RD	COMPOSITE Y-COORD	POINT OF COMPOSITE	GOLD	COPPER	LEAD	ZINC	BASE OF	WIDTH OF COMPOSITE		and a support of the statement of the support of th		
HOLE ) YG86-(	COMPOS 10+ X-CO 35 28266	ITE <u>RD</u> .73	COMPOSITE Y-COORD 30756.79	POINT OF COMPOSITE 15.00	60LD 0.00000	COFPER 0.00000	1.EAD 0.00000	ZINC	BASE OF <u>LEVEL</u> 10.00	WIDTH OF COMPOSITE 14.63			para apparan a sub P M M Assa	
HOLE ) YG84-0 YG84-0	COMPOS 10+ X-CO 135 28266 135 28259	ITE <u>RD</u> .73	COMPOSITE Y-COORD 30756.79 30750.14	POINT OF COMPOSITE 15.00 5.00	60LD 0.00000	COFPER 0.00000	1.EAD 0.00000 0.00000	ZINC 0.00000 0.00000	BASE OF LEVEL 10.00	WIDTH OF COMPOSITE 14.63 14.63			ani. ang an an an an an an an an an an an an an	
HOLE YG86-( YG86-(	COMPOS 10. X-CO 135 28266 135 28256 135 28256 135 28256 135 28256	ITE RD .73 .36	COMPOSITE Y-COORD 30756+79 30750+14 70747 57	POINT OF COMPOSITE 15.00 5.00	GOLD 0.00000 0.00000	COFFER 0.00000 0.00000	LEAD 0.00000 0.00000	ZINC 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 0.00	WIDTH OF <u>COMPOSITE</u> 14.63 14.63			ani, agarra a can a m a cara	
HOLE ) YG86-( YG86-( YG86-(	COMPOS 10. X-CO 35 2826 35 2825 35 2824	1TE RD .73 .36 .99	COMPOSITE Y-COORD 30756.79 30750.16 30743.53	PDINT OF <u>COMPOSITE</u> 15.00 <u>5.00</u> -5.00	60LD 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 0.00 -10.00	WIDTH OF COMPOSITE 14.63 14.63 14.63			an. aga a a a a a a a a a	
HOLE ) YG86-( YG86-( YG86-( YG86-(	COMPOS 10. X-CO 35 2826 35 2825 35 2824 35 2824 35 2824	ITE RD .73 .36 .99 .62	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90	FOINT OF COMPOSITE 15.00 5.00 -5.00 -15.00	60LD 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 0.00 -10.00 -20.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63			рат. 1990-т. сон т. <del>т.</del> т. на т.	
HOLE ) YG86-( YG86-( YG86-( YG86-( YG86-(	COMPOS 25 2826 35 2825 35 2825 35 2824 35 2824 35 2824 35 2823	ITE RD .73 .36 .99 .62 .24	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30730.28	POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00	GGLB 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 0.00 -10.00 -20.00 -30.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63				
HOLE   Y686-( Y686-( Y686-( Y686-( Y686-( Y686-(	COMPOS 10. X-CO 135 28264 135 2824 135 2825 135 2825 135 2825 135 2825 135 2825 135 2825 135 285	ITE RD .73 .36 .99 .62 .24 .76	COMPOSITE Y-COORD 30756.79 30750.14 30743.53 30736.90 30736.28 30723.84	POINT OF <u>COMPOSITE</u> 15.00 5.00 -5.00 -15.00 -25.00 -35.00	60LD 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.00 -10.00 -20.00 -30.00 -40.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.63				
HOLE   YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-(	COMPOS 20. X-CO 25. 2826 25. 2824 25. 2824 25. 2824 25. 2823 25. 2821 25. 2821	ITE RD .73 .36 .99 .62 .24 .76 .11	COMPOSITE Y-COORD 30756.79 30750.14 30743.53 30736.90 30736.28 30723.84 30717.70	FOINT OF COMPOSITE 15.00 -5.00 -5.00 -25.00 -35.00 -45.00	60LD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.60 14.54				
HOLE 1 Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-(	COMPOS 25 2824 35 2824 35 2824 35 2824 35 2824 35 2823 35 2823 35 2823 35 2823 35 2823 35 2821 35 2821	ITE <u>RD</u> .73 .36 .99 .62 .24 .76 .11 .40	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30717.70 30711.72	FOINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00	GOLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00131	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000	BASE OF <u>LEVEL</u> 10.00 -10.00 -20.00 -30.00 -40.00 -50.00	WIDTH OF <u>COMPOSITE</u> 14.63 14.63 14.63 14.63 <u>14.63</u> 14.63 14.54				
HOLE ) Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-(	COMPOS 25 2826 35 2825 35 2824 35 2	ITE <u>RD</u> •73 •36 •99 •62 •24 •76 •11 •40 <u>-</u> 24	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30717.70 30711.72	POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00	GGLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00131	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379 0.00000 0.03379	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000	BASE OF <u>LEVEL</u> 10.00 0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -40.00 -20.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.63 14.60 14.56 14.56 14.54				
HOLE YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-(	COMPOS 35 2826 35 2825 35 2825 35 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2821 35 2821 35 2821 35 2821	ITE RD •73 •36 •99 •62 •24 •76 •11 •40 •66	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30717.70 30711.72 30705.82	POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -65.00	GGLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00131 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379 0.00000 0.03379	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.60 14.56 14.54 14.54 14.53			,	
HOLE 1 YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-(	COMPOS 20. X-CO 25. 2824 25. 285 25. 285	ITE RD .73 .36 .99 .62 .24 .76 .11 .40 .66 .92	COMPOSITE Y-COORD 30756.79 30750.14 30743.53 30736.90 30736.90 30730.28 30723.84 30717.70 30711.72 30705.82 30699.93	POINT OF <u>COMPOSITE</u> 15.00 <u>-5.00</u> -5.00 <u>-15.00</u> <u>-25.00</u> <u>-35.00</u> <u>-45.00</u> <u>-65.00</u> <u>-75.00</u>	GOLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00131 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379 0.00000 0.03379 0.00000 0.03300	ZINC 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -40.00 -70.00 -80.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.63 14.60 14.55 14.55 14.53 14.53				
HOLE / YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-(	COMPOS 25 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2828 35 2828 35 2816 35 2818 35 2818 35 2818	ITE RD •73 •36 •99 •62 •24 •76 •11 •40 •66 •92 •18	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30730.28 30723.84 30717.70 30711.72 30705.82 30499.93 30694.03	FOINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -45.00 -65.00 -75.00 -85.00	GOLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00131 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379 0.00000 0.00000 0.00000 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -40.00 -70.00 -80.00 -90.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.63 14.63 14.54 14.54 14.53 14.53 14.53				
HOLE 1 Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-(	COMPOS 25 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2821 35 2821 35 2818 35 2818 35 2818 35 2818 35 2818	ITE RD •73 •36 •99 •62 •24 •76 •11 •40 •66 •92 •18 •45	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30717.70 30711.72 30705.82 30699.93 30694.03 30688.14	FOINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -65.00 -75.00 -75.00 -75.00 -95.00	GGLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00131 0.00000 0.00000 0.00000 0.00080 0.00080	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379 0.00000 0.00000 0.00000 0.00000 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -40.00 -70.00 -80.00 -90.00 -100.00	WIDTH OF <u>COMPOSITE</u> 14.63 14.63 14.63 14.63 14.63 14.63 14.53 14.55 14.53 14.53 14.53 14.53 14.53				
HOLE Y086( Y086( Y086( Y086( Y086( Y086( Y086( Y086( Y086( Y086( Y086( Y086(	COMPOS 25 2826 35 2825 35 2824 35 284 35 2	ITE RD .73 .36 .99 .62 .24 .76 .11 .40 .666 .92 .18 .45 .71	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30717.70 30711.72 30705.82 30699.93 30694.03 30688.14 30688.14	POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -65.00 -75.00 -85.00 -95.00 -195.00	GOLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00131 0.00000 0.00080 0.00080 0.00080	COFPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -40.00 -70.00 -30.00 -70.00 -100.00 -110.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.63 14.60 14.56 14.54 14.53 14.53 14.53 14.53 14.53				
HOLE YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-(	COMPOS 35 2824 35 2825 35 2824 35 2824 35 2824 35 2824 35 2824 35 2821 35 2821 35 2819 35 2819 35 2818 35 2818 35 2818 35 2818	ITE RD .73 .36 .99 .62 .24 .76 .11 .40 .66 .92 .18 .45 .71	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30717.70 30711.72 30705.82 30699.93 30694.03 30688.14 30682.24	POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -65.00 -75.00 -75.00 -105.00	GGLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00000 0.00000 0.00080 0.00080 0.00080 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -40.00 -70.00 -30.00 -100.00 -110.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.63 14.53 14.53 14.53 14.53 14.53 14.53 14.53 14.53			· · · · · · · · · · · · · · · · · · ·	
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HOLE Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-( Y684-(	COMPOS 35 2826 35 2825 35 2824 35 2823 35 2823 35 2822 35 2822 35 2822 35 2828 35 2816 35 2818 35 2818 35 2818 35 2818	ITE RD .73 .36 .99 .62 .24 .76 .11 .40 .66 .92 .18 .45 .71	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30717.70 30711.72 30705.82 30694.03 30688.14 30682.24	FOINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -65.00 -75.00 -75.00 -75.00 -75.00 -105.00 ELEVATION OF MID	GOLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.01010 0.00131 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.03379 0.00000 0.03379 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.08724 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -70.00 -90.00 -100.00 -110.00	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.60 14.56 14.54 14.53 14.53 14.53 14.53 14.53 14.53			· · · · · · · · · · · · · · · · · · ·	
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HOLE   YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-( YG84-(	COMPOS 20. X-COU 235 2824 235 2824 235 2824 235 2824 235 2824 235 2824 235 2824 235 2828 235 2818 235 2818 285 285 285 285 2	ITE RD .73 .36 .99 .62 .24 .76 .11 .40 .40 .52 .18 .45 .71 ITE RD	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30711.72 30705.82 30699.93 30694.03 30688.14 30682.24	POINT OF <u>COMPOSITE</u> 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -45.00 -75.00 -75.00 -75.00 -75.00 -95.00 -105.00 ELEVATION OF MID POINT OF COMPOSITE	GOLD 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.0000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.0000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.0000000 0.0000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.0000000 0.0000000 0.0000000 0.00000000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.0000000 0.000000 0.00000 0.000000 0.000000 0.00000000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -20.00 -40.00 -50.00 -70.00 -70.00 -70.00 -100.00 -100.00 -110.00 BASE OF LEVEL	WIDTH OF COMPOSITE 14.63 14.63 14.63 14.63 14.63 14.63 14.63 14.54 14.55 14.53 14.53 14.53 14.53 14.53 14.53 14.53 14.53 14.53				· · · · · · · · · · · · · · · · · · ·
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HOLE YG84-())))))))))))))))))))))))))))))))))))	COMPOS 235 28264 35 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2824 35 2818 35 28268 36 28268 36 28268 36 28268 36 28268	ITE RD .73 .36 .99 .62 .24 .60 .64 .75 .71 ITE RD .54 .67	COMPOSITE Y-COORD 30756.79 30750.16 30743.53 30736.90 30736.28 30723.84 30717.70 30711.72 30705.82 30694.03 30694.03 30688.14 30682.24	POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -65.00 -65.00 -75.00 -75.00 -75.00 -105.00 ELEVATION OF MID FOINT OF COMPOSITE 15.00 5.00	GOLD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	COPPER 0.00000 0.00000 0.00000 0.00000 0.00352 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	LEAD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ZINE 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF <u>LEVEL</u> 10.00 0.00 -10.00 -20.00 -20.00 -40.00 -40.00 -40.00 -70.00 -60.00 -100.00 -110.00 BASE OF LEVEL 10.00 0.00	WIDTH OF <u>COMPOSITE</u> 14.63 14.63 14.63 14.63 14.63 14.63 14.63 14.54 14.53				· · · · · · · · · · · · · · · · · · ·

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~	Y686-036	28256.80	30749.93	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.36				
0	YG86-036	28250.93	30745.66	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.36				
	Y686-036	28245.05	30741.39	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.36				•
	Y686-036	28239.18	30737.12	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.36				
ി	YG86-036	28233.31	30732.84	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.36				
	Y686-036	28227.44	30728.57	-55.00	0.00000	0.00000	0.00000	0.00000	- 40,00	17.34				
	Y694-034	28221.54	30724.30	-45 00	0 00000	0 00000	0 00000	0 00000	-70.00	10 74				
$^{\circ}$	Y686-036	28215.60	30720.15	-75.00	0.00014	0.00000	0.00000	0.00000		12.34		•		
	Y684-0.34	28209.53	30716.14	-85.00	0.02457	0.00130	0.00045	0.01770		10 74				• <u>•</u>
	YG94-074	28207.24	30712.22	-95 00	0 00019	0 00000	0 00000	0 00000		12.400				
$\gamma$	Y684-034	28194.73	30708.35	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12+04				
	AZ0-489V	28190.22	30704.48	-115 00	0.00000	0.00000	0 00000	0.00000	-120.00	10 54				
	Y684-034	28183.72	30700.42	-125.00	0.00000	0.00000	0.00000	0 00000	-170.00	10 54				
$\mathbf{O}$	470-4887 V684-034	28177.21	30494.75	-135.00	0.00000	0.00000	0 00000	0.00000	-140.00	10.54				
• •	Ven/ A7/	00170 70	70/00 00	1 45 77	<u> </u>	<u>Y_YYYYY_</u> _	<u> </u>		150.00				*	
	1000-000	20179479	3007<+00 70100 00	-195+00	0.00000	0.00000	0+00000	0+00000	-100+00	12+34				
)	Y004-030	20157 40	202007402	-145 00	0.00000	0.00000	0.00000	0.00000	170 00	327+04				
	1000-000	<01.07 +07		-100+00	0+00000	0+00000	0.00000	0+00000	-170.00	7+01				
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				UF MID										
3		CUMPUSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
1	HOLE NO.	X-000K0	Y-COORD	COMPOSITE	GOLD	COPPER	LEAD	ZINC	LEVEL	COMPOSITE				
5	YG86-037	28269+90	30759.49	15.00	0.00000	0.0000	0.00000	0.00000	10.00	11.25				
: 4	YG8 <u>6-037</u>	28265.28	30754.40	5,00	0.0000	0.00000	0,00000	0.00000	0 . 0 0 .	11,25				
	Y686-037	28261+66	30753.31	-5+00	0.00000	0.00000	0+00000	0.00000	-10.00	11.25				
. 、	YG86-037	28257.54	30750.22	-15.00	0+00000	0.00000	0.00000	0.00000	-20.00	11.25				
21	<u>Y686-037</u>	28253.43	30747.13	-25.00	0.00000	0.00000	0.00000	0,00000	-30,00	11.25				
	YG86-037	28249.31	30744.04	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.25				
	Y686-037	28245.19	30740.95	-45,00	0.00000	0.00000	0.00000	0.00000	-50.00	11.25				
. 3	YG86-037	28241.07	30737.85	-55,00	0+00000	0,00000	0.00000	0.00000	-60.00					
	YG86-037	28236.95	30734.76	-65,00	0.00000	0,00000	0.00000	0,00000	-70.00	11.25				
	YG86-037	28232+83	30731.47	-75.00	0.00000	0.00000	0.00000	0.00000	-30,00	11.25				
)	YG86-037	28228.71	30728.58	-85,00	0.00000	0.0000	0.00000	0,00000	-90,00	11.25				
ĺ	Y686-037	28224.57	30725.49	-95,00	0.00000	0.00000	0.00000	0.00000	-100.00	11.25				
	YG86-037	28220.47	30722.40	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.25				
)	YG86-037	28216.31	30719.34	-115,00	0.00018	0.00000	0.00000	0.00000	-120.00	11.27				
	Y686-037	28211.99	30716.35	-125.00	0.00317	0.00000	0.00000	0.00000	-130.00	11.33				
1	Y686-037	28207.54	30713.43	-135.00	0.00096	0.00000	0.00000	0.00000	-140.00	11.37				
$\rightarrow$	Y686-037	28203.09	30710.52	-145.00	0.00062	0.00000	0.00000	0.00000	-150.00	11.77				
	Y684-037	28198.43	30707.43	-155,00	0.00000	0.00000	0.00000	0.00000	-140.00	1 1 72 72		• • • • • • • • • • • • • • • • • • • •		
	Y686-037	28194.17	30704.73	-165.00	0.00000	0.00000	0.00000	0.00000	-170 00	11 77				
	Y984-037	28189.71	30701.83	-175.00	0.00000	0.00000	0.00000	0.00000	-190.00	44 77 X				
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ĺ		POMBOSTE	COMPOSITE						5.0F 0F	مسورستي وروسيت والالتراز				
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~	nuce NO+	<u>X-POORN</u>	1-00080	TOULOPTIE	0.050	LUFFER	1.560	ZINC	LEVEL .	CUMPOSITE				
	V00/ 070	000/1 7/		or										
1	1686-038	28201.36	30/23.38	25+00	0.00000	0.00000	0.00000	0,0000	20.00	6.59				
~	1086-038	<u></u>	30/19.51	15.00	0+00000	0.00000	0.00000	0.00000	10.00	11.55				
	Y686-038	28252,78	30715.65	5.00	0.00000	0.00000	0.00000	0.00000	0,00	11.55				
. I	YG86-038	28248.48	30711.79	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11,55				
-'	Y686-038	28244.19	30707.93	-15,00	0+00000	0.00000	0+00000	0.00000	20.00		•			
	Y886-038	28239,90	30704+06	-25.00	0.00000	0.00000	0.00000	0.00000	-30,00	11.55				
	Y686-038	28235.61	30700.20	-35.00	0.02012	0.03422	0.37878	0.69343	-40.00	11.54				
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(686-038	28231.32	30696.34	-45.00	0.51725	0.05970	0.11637	0.12556	-50.00	11,55			
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IOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COURD	OF MID POINT OF COMPOSITE	60LD	COPPER	LEAD	ZINC	BASE OF LEVEL	WINTH OF COMPOSITE	 		
686-039 686-039 686-039	28248.94 28240.81 28232.68	30731.65 30724.95 30718.25	25.00 15.00 5.00	0.00000	0.00000	0.00000	0.00000	20.00	9,88 14,53 14,53	·		
(684-039 (684-039 (684-039	28224.55 28216.41 28208.28	30711.55 30704.84 30698.14	-5.00 -15.00 -25.00	0.00000 0.00957 0.09643	0.00000 0.00144 0.01034	0.00000 0.05286 0.00154	0.00000 0.12895 0.08527	-10.00 -20.00 -30.00	14.53 14.53 8.21			
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· `)	Heisht of bench Elevation of tup of uppermost bench Proportion of bench heisht	: 10.00 : 50.00 : 0.50	· · ·	· · · · · · · ·		
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				ELEVATION								
	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	FOINT OF COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	BASE OF LEVEL	WIDTH OF Composite	•	
<b>`</b>	P6400001	28304.16	30478.08	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.70	 	 
-	1010001	20004410	07070+90	24 CF + 57 SF	A) ♦ Ar Xr Xr Xr Xr Xr	V • V V V V V V	******	~ • ~ ~ ~ ~ ~ ~ ~ ~ ~		7 ♦ x+2±		1
				ELEVATION								4. Brity, 1 and 1
5		COMPOSITE	COMPOSITE	OF MID POINT OF					BASE OF	WINTH OF		
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE	 	 
)	P64DD002	28302+82	30678+12	25+00	0+00000	0.00000	0.00000	0.00000		7.62		;
5				ELEVATION							 	 
	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-CONRD	OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRONS	BASE OF LEVEL	WINTH OF Composite		•
· · ·	P64DD003 P64DD003	28313.00	30684.85 30678.43	25.00 15.00	0.00000	0.00000	0.00000	0.00000	20.00	5.04 11.42	 	 
				FLEVATION								
				OF MID					••••••••••••••••••••••••••••••••••••••			
:	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE	 	 
- Andrewsky a state	P64DD004	28309.82	30682.40	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.46		
-				FLEVATION						· · · ·		
				OF MID							 	 
	HOLE NG.	COMPUSITE X-COORD	Y-COORD	PUINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WINTH OF COMPOSITE		1
	P64DD006 P64DD006	28304.27 28297.61	30691.06 30685.47	25.00 15.00	0.00000	0.00000	0.00000	0.00000	20.00	5.30 12.99		
				ELEVATION OF MID								
	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE	 	,

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$\bigcirc$	_MOZART\$	BUAO: CRESP	INOZA.TELLJ	TNABENA58T.	BEN#1	12-AUG-198	6 16:03	Pase 3		**************************************			
0	P64D0010 P64D0010	281 <u>64+86</u> 28168+28	30709,73 30719,14	25.00	0.00000	0.00000	0.00000	0.00000	20,00	. 11.04	 <b>.</b>		
$\odot$	l												
Э		COMPOSITE	COMPOSITE	ELEVATION OF MID POINT OF					BASE OF	WINTH OF			-
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE			
Э	F64DD011	28169.23	30708.72	25.00	0.00000	0.00000	0.00000	0.00000	20.00	11.44			
	P64D0011	28172.90	30718.80	15.00	0.00000	0.00000	0.00000	0.00000	10,00	5.32			
$\odot$												,	
				ELEVATION								•	
Э		COMPOSITE	COMPOSITE	OF MID POINT OF					BASE OF	WINTH OF			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE	 		
Э	P64DD014 P64DD014	28261.07 28261.68	30702,79 30708,53	25.00 15.00	0.00000	0.00000	0.00000	0.00000	20.00	10.20 5.19	 ·	-	
٦)													
. )		COMPOSITE	COMPOSITE	ELEVATION OF MID FOINT OF					BASE OF	WIDTH OF			т - толон летен ат - ал - шасла шаг
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE			
- D	P64D025	28278.62	30714.20	25.00	0.00000	0.00000	0.00000	0.00000	20.00	7.98			
	P6400025	28277.58	30702+32	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15.56			
.)													

				OF MID							
7.)		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF	
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	tron s	LEVEL	COMPOSITE	
1)	P64DD026	28299.74	30697.22	25.00	0.00000	0.00000	0.00000	0.00000	20,00	7.21	
	P64D0026	28293.31	30689.56	15+00	0.00000	0.00000	0.00000	0.00000	10,00	14.14	
,	P64DD026	28284.88	30681.90	5.00	0.00000	0.00000	0.00000	0.00000	0.00	6.39	

)

				ELEVATION OF MID							
HOLE	NO.	COMFOSITE X-COORD	COMPOSITE Y-COORD	FOINT OF COMPOSITE	ARSENI	SULFHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF Composite	
875DD 875DD	1001 1001	28063.57 28068.57	30730.10 30738.76	25.00 15.00	0.00000	0.00000	0.00000	0.00000	20.00	14.14 14.14	
				F) FUATTON							

			OF MID							
HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE	
 B75DD002 B75DD002	28064.95 28072.61	30728.90 30735.33	25.00 15.00	0.00000	0.00000	0.00000 0.00000	0.00000	20.00 10.00	14.14	

	UADILRESPI	INDZA.TELLJ	TNARENA58T.	REN;1	12-AUG-198	6 16:03	Pase 4			
B75BD002	28080+27	30741.76	5.00	0+00000	0.00000	0.00000	0.00000	0.00	14.14	
			EL ELLATION			INI MAN KINANI			•	
			OF MID							
	COMPOSITE	COMPOSITE	POINT OF		<b>.</b>			BASE OF	WITH OF	
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE	
B75DD003	28169.38	30704.72	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.92	· · · · · ·
B75DD003	28167+64	30714.57	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14	
B7500003	28164.16	30734.42	-5.00	0.00000	0.00000	0.00000	0+00000	-10.00	<u> </u>	
B75DD003	28162.43	30744.12	-15.00	0.00000	0+00000	0.00000	0.00000	-20.00	14.14	
B75D0003	28160.69	30753+96	-25+00	0.00000	0.00000	0,00000	0.00000	-30.00	1.4 - 1.4	
EV300003	20138.70	90109+01	-30+00	0.00000	0.00000	0+00000	0.00000	-40.00	14.14	
							······	····		
			ELEVATION							
i	COMPOSITE	COMPOSITE	POINT OF					BASE OF	WINTH OF	
HOLE ND.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE	
B7500004	28170.88	30703.17	25,00	0.00000	0.00000	0.00000	0.00000	20.00	0.00	
B75DD004	28173.32	30709.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.92	
B75ND004	28175.75	30715.22	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.92	
_B75BD004	28178.18	30721+24	-5+00	0,00000	0.00000	0+00000	0,00000	-10.00	6+26	
· · · · · · · · · · · · · · · · · · ·			OF MID							
ł	COMPOSITE	COMPOSITE	POINT OF					BASE OF	<b>WIDTH OF</b>	
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULFHU	STLVER	IRON S	LEVEL	COMPOSITE	
B75ND005	28291.31	30869.04	25.00	0.00000	0.00000	0.00000	0.00000	20.00	8,88	
<u>B7500005</u>	28298.38	30676.11	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14	
8/500005 87500005	28305+45	30583+18	5+00 ~5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14	
B7550005	28319.59	30697.32	-15.00	0.00000	0.00000	0.00000	0.00000	-20,00	14.14	
B75D0005	28326+66	30704.39	-25.00	0.00000	0.00000	0.00000	0+00000	-30.00	10.75	
			ELEVATION							
	COMPOSITE	сомерстте	OF MID POINT OF					DASE OF	UTDTU OF	
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE	
5.5555.5.0.4		74//8 45	05 00	A AAAAA	A AAAAA	r				
<u>B7500006</u> B7500004	28289+75	30657+05	20+00	0.00000	0.00000	0.00000	0,00000	20.00	11.70	
B75DD006	28294.63	30480.55	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.79	
B7500006	28297.08	30686+31	-5.00	0.00000	0.00000	0+00000	0.00000	-10.00	11.80	
В75ЛЛ006	28299.53	30692.06	-15.00	0,00000	0.00000	010000	0.00000	-20+00	5.53	
			FLENATION							
			OF MID							
	COMPOSITE	COMPOSITE_	FOINT OF					BASE OF	WIDTH OF	
LIGI E SIG	V AAAAA							) mm , t		

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j.	MOZART\$J	UAO: CRESP:	INOZA.TELL	IINABENA58I.	BEN:1	12-AUG-1986	16:03	Pade 5						
(	*****	00711 14	70700 00	61° 0.0	0 00000	0.0000			4.0.00	1 - march				
`	B7500007 B7500007	28306.92	30202+20	15.00	0+000000	0.00000	0.00000	0,00000	0.00	11+38	· ·			
	B7500007	28302.70	30695.37	-5+00	0+00000	0.00000	0.00000	0.00000	-10.00	11.38				
	875DB007	28298.48	30691.95	-15.00	0.00000	0,00000	0.00000	0.00000	-20.00	11.38		•		
7	>B7.000007	<u></u>	<u></u>		0,00000	0.00000	0.00000	0.00000		11.38				
													· .	
				ELEVATION		1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.								•
	•	COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	I.EVEL	COMPOSITE				
	07500AAO	00700 70	70707 05	15 00	0 00000	0 00000	0.00000	0 0000	10.00	11 00				
	B7500008	28303.33	30703+83	5+00	0.00000	0.00000	0.00000	0.00000	0.00	11,93				
	B7511008	28296.87	30702.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.93				
	B75DD008	28290.41	30701+81	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.93				
	6/011008	20203+70	30701.13	-23.00	0.00000	0.00000	0.00000	0.00000	-30.00	11+74				
	,			ELEVATION										
		COMPOSITE	COMPOSITE	UF MID POINT OF					BASE OF	<b>WIDTH OF</b>				
) [	HOLE NO.	X-COORD	Y-COURD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEI.	COMPOSITE				
										( <b></b>				
)	B/500009 B7509009	28308+73	30700+22	15+00	0.00000	0.00000	0,00000	0.00000	10.00	13,90				
	B75DD009	28293.11	30688+87	-5,00	0.00000	0.00000	0.00000	0.00000	-10.00	13.90				
	B7500009	28285.29	30683.19	-15.00	0.00000	0.00000	0.00000	0.00000	-20,00	13.90				
4	<u>B7555009</u>	28277.48	30677.51	-25,00	0.00000	0.00000	0.00000	0.00000	-30.00	13,90				
	BYOURODA	<5×57+57	30871+84	-30:00	0.00000	0+00000	0.00000	0100000	-40.00	2+00				
1														
				ELEVATION										
5		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
ſ	HOLE NO.	X-COORD	Y-COORD	CUMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE				
:	07505611	20210 20	70407 47	15 00	0 00000	0 00000	0 00000	0 00000	10.00	10 / 4				
	B7500011	28316+67	30685.02	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.64	· · - ·			
	B75DD011	28314.14	30682.40	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.64				
ſ	<u>B750D011</u>	28311.62	30679.78	-15.00	0.00000	0.00000	0+00000	0.00000	-20.00	10.64				
	8/500011	×8304±08	39877+18	-22:00	0+00000	0.00000	0+00000	0.00000	-30.00	10.64				
1							No. 16 1 11 11 11 11 11							
				ELEVATION										
)		COMPOSITE	COMPOSITE	0F MIU POINT OF					RASE OF	ытртн ог				
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE				
,							<i>.</i>					•		
	87500013 87500013	28332+87 28332-22	30680.01	<u>15+00</u> 5.00	0.00000	0.00000	0.00000	0.00000	10.00	10.04				
	B75ND013	28331.54	30679.44	-5,00	0.00000	0.00000	0.00000	0.00000	-10.00	10.04				
)	B7500013	28330.88	30678.88	-15+00	0.00000	0.00000	0.00000	0.00000	-20.00	10.04				
	B75DD013 B75DD017	28330.21	30678.32	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	10.04				
	B75DD013	28328.86	30677.19	-45.00	0.00000	0.00000	0.00000	0.00000	-40.00	10+04				
	B750D013	28328.19	30676.63	-55.00	0.00000	0.00000	0+00000	0.00000	-60.00	5.52		• • • •		

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		•	ELEVATION									
			OF MID						· · · · · · · · · · · · · · · · · · ·		· · ·	
	COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF			
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE		· ·	
37500014	28331.35	30679,21	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.64		•	
87500014	28328.56	30676.87	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.64			
37500014	28325.77	30674.53	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.64	· .		
37500014	28322+99	30672+19	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.64			
			ELEVATION				•					
			OF MID									
	COMPOSITE	COMPOSITE	POINT OF		010 0101	074 UEE	7501 0	BASE OF	WIDTH OF			
HOLE NO.	X-COORD	Y-COURD	CUMPUSITE	ARSENI	SULFHU	STLVER	IRUN S	LEVEL	CUMPUSITE			
375DD015	28316.52	30645.35	25.00	0.00000	0.00000	0.00000	0.00000	20.00	10.39			
37500015	28323.83	30652.17	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.14	•		
37500015	28331.15	30658.99	5.00	0.00000	0.00000	0.00000	0.00000		14.14	· .		
8750D015	28338.46	30665.81	-3.00	0.00000	0.00000	0.00000	0+00000	-10.00	14.14			
3/500015 97500015	28343+77	30072+03 30479,45	-10+00	0.00000	0.00000	0.00000	0.00000	-20,00	14.14			
375DD015	28360.40	30686.28	-35.00	0.00000	0.00000	0.00000	0.00000	-40+00	10.34			
		·	ELEVATION									
			OF MID									
	COMPOSITE	COMPOSITE	FOINT OF				·····	BASE OF	WIDTH OF			
HOLE NO.	X-COORD	Y-COORA	COMPOSITE	ARSENI	SULPHU	SILVER	IRUN S	LEVEL	COMPOSITE			
875DDA14	28714.93	30444.90	25.00	0.00000	0,00000	0.00000	0.00000	20.00	10.49			
87556016	28325159	30649.90	15.00	0.00000	0.00000	0.00000	0,00000	10.00	14.14			
875DD016	28334.24	30654.90	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.14			
87590016	28342.90	30659.90	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.14			
B75DD016	28351.56	30664.90	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	14.14			
87500016	28360+23	30669.90	-25,00	0.00000	0.00000	0.00000	0.00000	-30.00	12.19			
			ELEVATION									
			OF MID		· · · <u>-</u> · · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·					
	COMPOSITE	COMPOSITE	POINT OF	4 D. C. M. L. P.	010 olu		T	BASE OF	WIDTH OF			
-101.E NU+	X-COURD	T-CODED	COMPUSITE	ANDERI	SULFHU	SLLVER	INUN 5	LEVEL	CUMPUSITE			
875nn017	28183.75	30742.87	15.00	0,00000	0,00000	0.00000	0.00000	10.00	11.55			
87500017	28182.75	30737.19	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55			
375nn017	28181.74	30731.50	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.55			
87500017	28180.74	30725+82	-15+00	0.00000	0.00000	0.00000	0+00000	-20.00	11.55			
375nn017	28179.74	30720.13	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.55			
	·· · ·											
			ELEVATION								:	
	COMPOSITE	COMPOSITE	POINT OF					BASE OF				
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE			
Y685-004	28394.39	30677.87	15.00	0.00000	0.00000	0.00000	0.00000	10.00	15,11			

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_MOZART\$	DUAO:ERESPI	INDZA.TELLJ	TNABENA58T.	REN;1	<u>12-AUG-198</u>	6 16:03	Fase 7			·	
YG85-004 YG85-004	28378.10 28368.65	30663.63 30656.47	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	15.46		
YG85-004	28359.14	30649.30	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	15.56		
1685-004	28349+63	30842+13	-35.00	0.00000	0,00000	0.00000	0.00000	-40,00	15.56		
			ELEVATION							. · ·	
HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	BASE OF LEVEL	WIDTH OF COMPOSITE		_ · · `
YG85-005	28399.63	30680.28	15.00	0.00000	0.00000	0.00000	0,00000	10.00	11.41		
YG85-005	28395.56	30676+60	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.41		
YG05-005	20371+40	70440 01	-15 00	0.00000	0.00000	0.00000	0.00000	-10+00	11.44	•	
Y685-005	28383.02	30665.47	-25.00	0.00000	0.00000	0.00000	0.00000	-30,00	11,48		
YG85-005	28378.69	30661.69	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.56		
YG85-005	28374.09	30657.78	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.81		
Y685-005	28369.27	30653.24	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.81		
Y685-005	28364.45	30649.71	-65:00	0.00000	0,00000	0.00000	0.00000	-70.00	11.81		
1085-005	28357+63 20754 0A	30640+68	-/5.00	0.00000	0.00000	0.00000	0.00000	-80,00	11.81		
Y685-005	28349.83	30637.53	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.81		
YG85-005	28344.64	30633.32	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.06		
Y685-005	28339.40	30629+07	-115.00	0.00000	0.00000	0.00000	0+00000	-120.00	12.06		
Y685-005	28334.16	30624+83	-125,00	_0+00000	0,00000	0.00000	0.00000	130.00	12+06		
YG85-005	28328+92	30620.38	-135.00	0+00000	0.00000	0+00000	0.0000	-140,00	8.96		
			ELEVATION						201		
			OF MID								
HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF	ARSENI	SULPHU	STLVER	IRON S	BASE OF	. WINTH OF. COMPOSITE		
Y685-004	28395.98	30681.75	15.00	0.00000	0.00000	0.00000	0.00000	10.00	4 T 7 7		
Y085-004	28384+63	30681.59	5.00	0.00000	0.00000	0,00000	0,00000	0.00	13.62		
YG85-006	28377.38	30681.51	-5,00	0.00000	0.00000	0.00000	0,00000	-10,00	13.62		
YG35-006	28368.13	30681+43	-15.00	0.00000	0.00000	0,00000	0+00000	-20.00	13.62		
YG85-006	28358.91	30681.37	-25.00	0.00000	0.00000	0.00000	0.00000	-30,00	13.59		
YC25-004	28349+69	30681+36	-35+00	0.00000	0.00000	0+00000	0.00000	-40.00	13.61		
Y685-004	28331.04	30481.34	-55.00	0.00000	0.00000	0.00000	0.00000	-60,00	13.67		
Y685-006	28321.62	30681.35	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	13.79		
Y685-006	28312.13	30681.32	-75.00	0.00000	0.00000	0.00000	0.00000	-80,00	13.80		
YG85-006	28302.56	30681.23	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	13.88		
Y685-006	28292.89	30481.05	-95.00	0.00000	0.00000	0.00000	0+00000	-100.00	13.94		
1685-006 VCOF 004	28283+15	30680.77	-105.00	0.00000	0.00000	0,00000	0,00000		13.98		
1000-000 V695-004	- 20273+49	30360+43	-125 00	0.00000	0.00000	0+00000	0.00000	-120.00	13+96		
YG85-006	28253.97	30679.77	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	13.70		
YG85-006	28244.32	30679.43	-145.00	0.00000	0.00000	0.00000	0,00000	-150.00	13,90		
YG85-006	28234+62	30679.09	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	13.90		
YG85-006	28225.02	30678.75	-165.00	0.00000	0.00000	0.00000	0.00000	-170,00	13,90		
1685-006	28215+37	306/8+41	-175.00	0.00000	0.00000	0+00000	0.00000	-180.00	10,49		
			ELEVATION						• • • •		
			OF MID								
	}	<u> </u>				<b>`</b>					<u> </u>

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<u>]</u>		COMPOSITE	COMPOSITE	POINT OF	ALCENT	CH1 (111)	0714000		BASE OF	WIDIH UF					
	HULE NU.	X-CUURD	т-сооки	CUMPUSTIE	HNDENI	SULPHU	511.Vr.K	TRUN 2	L L L V fal.	CONFUSILIE .	· · · ·				
	Y685-007	28398.45	30481.80	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.54					
$\supset [$	Y685-007	28392.64	30681.71	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.56					,
5	YG85-007	28386.83	30681.61	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11,56					
	YG85-007	28381.02	30681.52	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.56				•	
.)	Y685-007	28375.11	30681.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.67					
	YG85-007	28369.05	30681+52	-35.00	0.00000	0.00000	0+00000	0.00000	-40.00	11.72					
$\gamma$	YG85-007	28362.94	30681.59	-45+00	0.00000	0.00000	0.00000	0.00000	-50.00	11.72					
	Y685-007	28356+84	30681.65	-55.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.7%					·
	Y685-007	28350+69	39681+/3	-65.00	0.00000	0.00000	0.00000	0.00000	-70+00	11+//					
$\mathbf{D}$	Y685-007	20344+40	30681.93	-85,00	0.00000	0.00000	0.00000	0.00000	-90.00	11.79					
	Y685-007	28331.95	30682.04	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.80			1 .		
i	Y685-007	28325.67	30682.16	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.82					
)	YG85-007	28319.31	30682.27	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.89					
	YG85-007	28312.84	30682.38	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.94					
_	YG85-007	28306.28	30682.49	-135.00	0.00000	0,00000	0.00000	0,00000	-140.00	11.98					
	Y685-007	28299+67	30682.61	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11, 99					
	YG85-007	28293.05	30682.72	-155,00	0.06450	2.78004	0.29552	4.12506	-160.00	12.00					
$\gamma$															
- +				FLENATION											
				CECATION											
$\mathbf{O}$		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	ытатн аг					
	HOLE NO.	X-COORD	Y-C008b	COMPOSITE	ARSENT	SULPHU	STLVER	IRON S	LEVEL	COMPOSITE					
	YG85-010	28399.83	30681.81	15,00	0.00000	0.00000	0.00000	0.00000	10.00	10.87					
	YG85-010	28395.58	30681.64	5.00	0.00000	0.0000	0.00000	0.00000	0.00	10.87					
$\mathbf{x}$	YG85-010	28391.33	30681.47	-5.00	0.00000	0.00000	0+00000	0.00000	-10.00	10.87					
	Y685-010	28386+97	30681.32	-15+00	0,00000	0+00000	0,00000	.0.00000.	-20+00	10.96					
5	Y685-010	28382+49	30881+16	-20,00	0.00000	0.00000	0.00000	0.00000	-30.00	10+96					
$\mathbf{C}$	Y685-010	28373.53	30631+01	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.94					
	Y685-010	28369.05	30680+69	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10.96					
	YG85-010	28364.57	30680.54	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.96					
$) \mid$	Y685-010	28340.09	30680.38	-75+00	0.00000	0.00000	0.00000	0.00000	-80.00	10.96					
Ì	Y685-010	28355.52	30680.22	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.04					
	YG85-010	28350.79	30680.05	-95.00	0.01213	0.25475	0.03625	0.43101	-100.00	11.09					
· 1	YG85-010	28345.93	30679+88	-105,00	0.01716	0+47842	0.05338	0.81763	-110.00	11.15					
	Y885-010	28340.94	30679.71	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.20					
)	Y685-010 V095-010	28335.87	306/9.54	-125.00	0.00000	0,00000	0.00000	0,00000	-130.00	11+22					
	Y685-010	28339470	30479.18	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.00					
1	Y685-010	28320.40	30479.00	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.22					
)	Y685-010	28315.50	30678.82	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.22					
1	Y685-010	28310.41	30678.65	-175.00	0.00000	0.00000	0.00000	0.00000	-180.00	11.22					
	YG85-010	28305.32	30678.47	-185.00	0.01319	0.00000	0.01684	0.00000	-190.00	11.23					
	Y685-010	28300+25	30678.29	-195,00	0.00000	0.00000	. 0.00000	.0.0000.00	-200+00	. 11.22					
Ì	YG85-010	28295.13	30678.11	-205.00	0100000	0.00000	0.00000	0.00000	-210.00	11.22					
	YG85-010	28290+04	30677.93	-215.00	0.00000	0.00000	0.00000	0.00000	-220.00	11.22					
2 F	Y685-010	28284.95	306//./6	-225.00	0.00000	0,00000	0.00000	0.00000	-230.00	11.22					
	1085-V10 VC05-010	- 282/7+86 	306//+58	-245 00	0.00000	0.00000	0.00000	0.00000	-240.00	11+22					
$\mathbf{y}$	1000-010	2.02/4+//	000//+40	"≤ <b>~</b> U+00	V • V V V V V	······································	V + 00000	V + V V V V V	200+00	4. <b>1.</b> 4. 27. 27.					
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				OF MID								
$\bigcirc$		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF		
1	HALE NO.	X-C00RD	Y-0080	COMPOSITE	ARSENI	SHI PHU	STIVER	TRON S	IFUE	COMPOSITE		 •
			1 1917 91112					20000		DOULDOTIC		
$\mathbf{D}$	Y685-011	28399.31	30480.97	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11 01		
2	Y005-011	20794 11	70479.27	5.00	0 00000	0.00000	0 00000	0.00000		<u>_</u>		 · · · · · · · · · · · · · · · · · · ·
	1000 011	203794121	70/77 40	5.00	0.00000	0.00000	0.00000	0.00000	10.00	1 + 4 I		
3	1685-011	28388.70	308//+47	-3+00	0.00000	0.00000	0.00000	0.00000	-10.00	11.41		
	1000-011		300/3+/3	-1+99	0,00000	0+00000	0.00000			11+41		•
- 1	1685-011	28378.48	30874.01	-23.00	0.00000	0.0000	0.00000	0.00000	-30.00	11.41	· · · · · · · · · · · · · · · · · · ·	
$\gamma$	Y685-011	283/3+2/	30672+27	-35+00	0.00000	0.00000	0.00000	0.00000	-40.00	11.41		
' [	YG85-011	28368+06	30670+54	-45+00	0,00000	0.00000	0,00000	0.00000	-50.00			 
	Y685-011	28362+77	30668+87	-55.00	0.01522	0.00082	0.00697	0.00000	-60.00	11.46		
51	YG85-011	28357+42	30667+31	-65,00	0.00000	0.00000	0.00000	0,0000	-70.00	11.44		
21	Y685-011	28352.09	30665.79	-75.00	0.00000	0.00000	0.00000	0.00000	-80+00	11.44	· · · · · · · · · · · · · · · · · · ·	
Í	YG85-011	28346,73	30664.30	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.44		
.	YG85-011	28341.35	30662.90	-95+00	0.00000	0.00000	0.00000	0.00000	-100.00	11.45		
$\rightarrow$	YG85-011	28335,94	30661.54	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.45		
ĥ	YG85-011	28330.54	30660.18	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.45		
	Y685-011	28325.13	30658.82	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.45		
$\rightarrow$	Y685-011	28319.70	30457,49	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.48		
	V005-011	20714 14	70454 00	-145 00	0 00000	0 00000	0 00000	0 00000	-150 00	44 57		
	1000-011	20317410	30000+XX 70/53 04	-140+00 	0+00000	0.000000	0.00000	0 + 0 0 0 0 0 0	- 100+00	11+400		
	1080-011	20000+00	3003J+91 70/57 07	-100+00	0.00000	0.00000	0.00000	0.00000	-130+00	11.04		
· · · [	1080-011	26302+71	<u></u>	<u> </u>	0.00000	0.00000	0.00000	0,0000		11.00		 
	1685-011	28277+24	39802+73	-170+00	0.00000	0.00000	0.00000	0.00000	-180+00	11.55		
	YG85-011	28291.56	30651.69	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	11.55		
7	Y085-011	28285+88	30650+67	-195.00	0+00000	0.00000	0+00000	0,00000	-200+00	11.55		
	YG85-011	28280,20	30649.65	-205.00	0.00000	0.00000	0,00000	0.0000	-210.00	11.55		
	YG85-011	28274.51	30648+64	-215.00	0.00000	0.00000	0.00000	0.00000	-220.00	11,55		
2	V005-011	28248.83	70687 67	- 225 00	0 00000	0.00000	0.00000	A AAAAA	- 270 00	11 EE		
	1000 011	1.0200+00	00047+00	<u> </u>	0+00000	<u> </u>		<u>, , , , , , , , , , , , , , , , , </u>	- 200 + 200	<u> </u>		 
)			00047+03	ELEVATION OF MID								 
5	HOLE NO.	COMPOSITF	COMPOSITE	ELEVATION OF MID POINT OF COMPOSITE	ARSENI		STLUER	IRCN S	BASE OF	WINTH OF		 
	HOLE NO.	COMPOSITF X-COORD	COMPOSITE Y-COURD	ELEVATION OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF	WINTH OF COMPOSITE		 
	HOLE NO.	COMPOSITF X-COORD	COMPOSITE Y-COURD	ELEVATION OF MID FOINT OF COMPOSITE	ARSENI	<u>SULPHU</u>	SILVER	IRON S	BASE OF	WINTH OF COMPOSITE		
	HOLE NO. YG85-012	COMPOSITF X-COORD 28306.60	COMPOSITE Y-COURD 30703.73	ELEVATION OF MID POINT OF COMPOSITE 15.00	ARSEN1 0.00000	<u>SULPHU</u> 0.00000	SILVER 0.00000	IRON 5	BASE OF LEVEL 10.00	WINTH OF COMPOSITE		 
	HOLE NO. Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28276.22	COMPOSITE Y-COURD 30703.73 30703.30	ELEVATION OF MID FOINT OF COMPOSITE 15.00 5.00	ARSENI 0.00000 0.00000	SULPHU 0.00000 0.00000	SILVER 0.00000 0.00000	IRON S 0.00000 0.00000	BASE OF LEVEL 10.00 0.00	WINTH OF COMPOSITE 14.45 14.37		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91	30847.03 COMPOSITE Y-COURD 30703.73 30703.30 30702.93	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00	ARSEN1 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.90 -10.00	WINTH OF COMPOSITE 14.45 14.39 14.36		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60	30347.03 COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.57	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00	ARSEN1 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000	IRGN S 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.90 -10.00 -20.00	WIDTH OF COMPOSITE 14.45 14.39 14.36 14.37		 
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37	30703.73 30703.73 30703.30 30702.93 30702.57 30702.22	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.00 -10.00 -20.00 -30.00	WIDTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.22		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32	30703.73 30703.73 30703.30 30702.93 30702.57 30702.57 30702.22 30701.92	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00 -35.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.90 -10.00 -20.00 -30.00 -40.00	W1DTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28225.60 28265.37 28255.32 28255.32 28245.52	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.57 30702.57 30702.22 30701.92 30701.68	ELEVATION OF MID FOINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93		
	HOLE NO. YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28265.37 28255.32 28245.52 28235.91	COMPOSITE Y-COURD 30703.73 30703.33 30702.93 30702.57 30702.22 30701.92 30701.68 30701.48	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -45.00 -55.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.22 14.08 13.93 13.80		 
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28265.32 28255.32 28245.52 28235.91 28226.41	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.93 30702.27 30702.22 30701.92 30701.48 30701.48 30701.32	ELEVATION OF MID FOINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -65.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.27 14.08 13.93 13.80 13.78		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-CDORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28245.52 28245.52 28235.91 28226.41 28226.41	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.57 30702.22 30701.92 30701.68 30701.48 30701.32 30701.32	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -5.00 -15.00 -25.00 -45.00 -65.00 -75.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRGN S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00 -80.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.79		 
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28225.37 28255.32 28245.52 28235.91 28226.41 28226.41 28216.93	30703.73 30703.73 30703.30 30702.93 30702.93 30702.57 30702.22 30701.92 30701.68 30701.32 30701.15	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -15.00 -25.00 -35.00 -45.00 -65.00 -75.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRGN S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.79		 
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28255.32 28245.52 28235.91 28226.41 28226.41 28216.93	30703.73 30703.73 30703.30 30702.93 30702.93 30702.57 30702.22 30701.92 30701.48 30701.48 30701.32 30701.15	ELEVATION OF MID FOINT OF COMPOSITE 15.00 -5.00 -5.00 -35.00 -45.00 -65.00 -75.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00 -80.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.79		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28245.52 28235.91 28235.91 28225.40 28245.52 28235.91 28226.41 28216.93	30703.73 30703.73 30703.30 30702.93 30702.93 30702.57 30702.22 30701.92 30701.48 30701.48 30701.32 30701.15	ELEVATION OF MID FOINT OF COMPOSITE 15.00 -5.00 -5.00 -35.00 -45.00 -65.00 -75.00 ELEVATION	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00 -80.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.79		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28245.52 28235.91 28226.41 28226.41 28216.93	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.57 30702.57 30702.57 30701.92 30701.66 30701.48 30701.32 30701.15	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00 -45.00 -55.00 -45.00 -75.00 ELEVATION DF MID	ARSEN1 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00 -80.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.79		· · · · · · · · · · · · · · · · · · ·
	HOLE ND. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28225.60 28265.37 28255.32 28245.52 28235.91 28226.41 28226.41 28216.93	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.57 30702.57 30702.57 30701.92 30701.48 30701.48 30701.48 30701.32 30701.15	ELEVATION OF MID FOINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00 -45.00 -55.00 -65.00 -75.00 ELEVATION OF MID FOINT OF	ARSEN1 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON 5 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 BASE OF	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.22 14.08 13.93 13.80 13.78 13.78 13.79 WIDTH OF		
	HOLE NO. YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28245.52 28235.91 28226.41 28216.93 COMPOSITE X-COORD	COMPOSITE Y-COURD 30703.73 30703.33 30702.93 30702.57 30702.22 30701.92 30701.92 30701.48 30701.48 30701.48 30701.15	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00 -5.00 -35.00 -45.00 -55.00 -45.00 -75.00 ELEVATION OF MID POINT OF COMPOSITE	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -50.00 -70.00 -80.00 BASE OF LEVEL	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.22 14.08 13.93 13.80 13.78 13.78 13.79 WINTH OF COMPOSITE		
	HOLE ND. YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28265.37 28255.32 28245.52 28235.91 28226.41 28216.93 COMPOSITE X-COORD	COMPOSITE Y-COURD 30703.30 30703.30 30702.93 30702.93 30702.92 30701.92 30701.92 30701.92 30701.48 30701.48 30701.32 30701.15	ELEVATION OF MID FOINT OF COMPOSITE 15.00 -5.00 -5.00 -15.00 -25.00 -45.00 -55.00 -65.00 -75.00 ELEVATION DF MID POINT OF COMPOSITE	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -70.00 -80.00 BASE OF LEVEL	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.22 14.08 13.93 13.80 13.78 13.79 WINTH OF COMPOSITE		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-013	COMPOSITF X-CDORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28245.52 28245.52 28235.71 28226.41 28216.93 COMPOSITE X-COORD 28308.64	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.93 30702.22 30701.92 30701.92 30701.48 30701.48 30701.48 30701.48 30701.48 30701.15	ELEVATION OF MID FOINT OF COMPOSITE 15.00 -5.00 -5.00 -15.00 -25.00 -35.00 -45.00 -75.00 ELEVATION OF MID POINT OF COMPOSITE 15.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -50.00 -70.00 -80.00 BASE OF LEVEL 10.00	WIDTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.79 WIDTH OF COMPOSITE 12.52		· · · · · · · · · · · · · · · · · · ·
	HOLE NO. YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-013 YG85-013 YG85-013	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28245.52 28235.91 28226.41 28216.93 COMPOSITE X-COORD 28308.64 28308.64	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.93 30702.22 30701.92 30701.48 30701.48 30701.48 30701.48 30701.15 COMPOSITE Y-COURD 30703.65 30702.99	ELEVATION OF MID POINT OF COMPOSITE 15.00 -5.00 -5.00 -5.00 -35.00 -45.00 -55.00 -65.00 -75.00 ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00 -80.00 BASE OF LEVEL 10.00 0.00	WIDTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.79 WIDTH OF COMPOSITE 12.52 12.52		
	HOLE NO. Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-012 Y685-013 Y685-013 Y685-013 Y685-013	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28245.52 28235.91 28226.41 28216.93 COMPOSITE X-COORD 28308.64 28301.13 28293.43	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.57 30702.57 30702.57 30701.92 30701.48 30701.48 30701.48 30701.48 30701.15 COMPOSITE Y-COURD 30703.65 30702.99 30702.34	ELEVATION OF MID POINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00 -35.00 -45.00 -55.00 -45.00 -75.00 ELEVATION DF MID POINT OF COMPOSITE 15.00 -5.00 -5.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00 -80.00 BASE OF LEVEL 10.00 0.00 -10.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.78 13.79 WINTH OF COMPOSITE 12.52 12.52 12.52		
	HOLE NO. YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-013 YG85-013 YG85-013 YG85-013	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28275.60 28265.37 28255.32 28245.52 28235.91 28226.41 28226.41 28216.93 COMPOSITE X-COORD 28308.64 28301.13 28293.63 28284.12	COMPOSITE Y-COURD 30703.73 30703.30 30702.93 30702.57 30702.57 30702.57 30701.48 30701.48 30701.48 30701.48 30701.48 30701.48 30701.48 30703.65 30702.99 30702.34	ELEVATION OF MID FOINT OF COMPOSITE 15.00 5.00 -5.00 -15.00 -25.00 -45.00 -55.00 -65.00 -75.00 ELEVATION OF MID FOINT OF COMPOSITE 15.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -75.00 -5.00 -75.00	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 -0.00 -10.00 -20.00 -30.00 -40.00 -50.00 -60.00 -70.00 -80.00 BASE OF LEVEL 10.00 -0.00 -10.00 -20.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.27 14.08 13.93 13.80 13.78 13.78 13.79 WINTH OF COMPOSITE 12.52 12.52 12.52	· · · · · · ·	· · · · · · · · · · · · · · · · · · ·
	HOLE NO. YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-012 YG85-013 YG85-013 YG85-013 YG85-013 YG85-013 YG85-013	COMPOSITF X-COORD 28306.60 28296.22 28285.91 28225.60 28265.37 28255.32 28245.52 28235.91 28226.41 28226.41 28216.93 COMPOSITE X-COORD 28308.64 28301.13 28293.63 28286.12 2827.61	COMPOSITE Y-COURD 30703.73 30703.30 30702.57 30702.57 30702.57 30702.57 30701.92 30701.48 30701.48 30701.48 30701.48 30701.48 30701.48 30701.48 30701.48 30701.68 30702.99 30702.34 30701.02	ELEVATION OF MID FOINT OF COMPOSITE 15.00 5.00 -5.00 -5.00 -35.00 -45.00 -55.00 -65.00 -65.00 -75.00 ELEVATION DF MID FOINT OF COMPOSITE 15.00 5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -5.00 -6.00 -7.00 -7.00 -6.00 -7	ARSENI 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SULPHU 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	SILVER 0.00000	IRON S 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	BASE OF LEVEL 10.00 0.00 -10.00 -20.00 -40.00 -50.00 -50.00 -70.00 -80.00 BASE OF LEVEL 10.00 0.00 -10.00 -20.00 -70.00	WINTH OF COMPOSITE 14.45 14.39 14.36 14.37 14.22 14.08 13.93 13.80 13.78 13.78 13.78 13.79 WIDTH OF COMPOSITE 12.52 12.52 12.52 12.52	· · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·

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1											
$\sim$	YG85-013	28271.11	30700.37	-35.00	0.00116	0.00000	0.01019	0.00000	-40+00	12.52	
121	1685-013 VC05-017	28263+69	30677+/1	-43.00	0.01407	0.01500		0.00288	-40.00	12+02	· · · · · · · · · ·
	Y685-013	28248.59	30498.40	-65.00	0.37558	0.52089	0.24272	0.41778	-70.00	12.52	
<u>.</u>	Y685-013	28241.08	30697.74	-75.00	1.68420	0.94431	0.01010	0.41400	-80.00	9.07	
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		COMPOSITE	COMPOSITE	ידאד מד דאד מד					BASE OF	<b>ΜΙΝΤΗ ΟΕ</b>	
$\rightarrow$	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE	
1											
- 21	YG85-014	28287.96	30728.18	15.00	0,00000	0.00000	0.00000	0.00000	10.00	14.33	
	1080-014	28277.70	30/28+13	J.VV	0.00000	0.00000	0.00000	0+00000	-10.00	1 14430	
	Y695-014	28257.18	30728+13	-15,00	0.00000	0.00000	0.00000	0.00000	-20.00	14+33	
2	YG85-014	28246.91	30728.08	-25,00	0.00000	0.00000	0.00000	0.00000	-30.00	14.33	
	Y685-014	28236.65	30728.06	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.33	,
	YG85-014	28226+43	30728.04	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.28	
	Y685-014	28216+27	30728.04	-55:00	0.00000	0.00000	0+00000	0+00000.	-60.00	14.24	
	YG85-014	28206.16	30728.04	-65.00	0.00000	0.00000	0.00000	0.00000	-70,00	14.20	
$\odot$	1065-V14 Y685-014	28186.00	30728.04	-85.00	0.000000	0.00000	0.00000	0.00000	-90.00	14.18	
	YG85-014	28175.97	30728.04	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.15	
	Y685-014	28165.96	30728.04	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.72	
$\supset$				OF WID							
		COMPOSITE	COMPOSITE	POINT OF					BASE DE	WIDTH OF	
	HOLE NO.	X-COORD	Y-000RD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE	
)											
	YG85-015	28289.75	30728.20	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.02	
)	YG85-015 YC05-015	28282.82	30728+37	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12+17	
	Y035-015	282/3407	30728.33	-15,00	0.00000	0.00000	0.00000	0,00000	-20.00	12.17	
	YG85-015	28262.04	30728,90	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12,17	
	YG85-015	28255.11	30729.08	-35.00	0.00000	0.00000	0+00000	0.00000	-40,00	12.12	· · · ·
	YG85-015	28248.18	30729.26	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.17	
	YG85-015	28241.27	30729.44	-55.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.14	
	Y825-015	28227.40	30729.91	-75.00	0,00000	0,00000	0.00000	0.00000	-20.00	12.10	
1	YG85-015	28220.80	30730.14	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	12.10	
2	Y685-015	28213.99	30730.38	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.10	
	YG85-015	28207+18	30730.62	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.10	
				FLEVATION							
				OF MID							
		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF	
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE	
<u>.</u>	VODE AF7	00740 07	74749 07	15 ~~	0 00000	~ ~~~~	0 00000	r. 84444	4 4 4 4 4	10 00	
	<u> </u>	<u></u>	30702,73 30703 14	30+00	0.00000	0.00000	0.0000	0.00000	10+00	12.70	
	Y685-01A	28292.67	30701.40	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.87	
	YG85-016	28284+63	30700.68	-15.00	0.09884	0.51046	0.12585	0.73373	-20.00	12.84	
	YG85-016	28276.61	30699.96	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.84	
	YG85-016	28268.59	30699.23	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.84	
	<u> </u>										

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			1 <b>-</b> 0 <b>0</b>										
Y685-017	28260.57	30698.51	-45+00	0.00000	-0.00000	0.00000	0+00000	-50+00	12.84				
Y685-014	28244.72	30696.94	-65,00	0.00101	0.00144	0.01657	0.00000	-70.00	12.400				te de la companya de la companya de la companya de la companya de la companya de la companya de la companya de
Y685-014	28237.11	30696.07	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.54				
YG85-016	28229.60	30495.18	-85.00	0.00000	0.00000	0.00000	0.00000	70,00	12,53				
YG85-016	28222.10	30694.28	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12,54				
YG85-018	28214+59	30693+38	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12,53				4
	· · · · · · · · · · · · · · · · · · ·												. · · .
			FLEVATION								1. A.		•
			OF MID										•
·	COMPOSITE	COMPOSITE	POINT OF		<u></u>			BASE OF	WIDTH OF				
HOLE NO	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER'	IRON S	LEVEL	COMPOSITE				,
													. 1
YG85-017	28310.54	30703.30	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.62				
1085-017 XC85-017	28304+63	30703+08	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.62				
Y695-017	<u>20270+70</u>	<u>30702+02</u> 70702 59	-15 00	0.00000	0.00000	0.00000	0,00000	-20.00	11 (1				
Y685-017	28286.95	30702.49	-25,00	0.00718	0.13386	0.01334	0.22724	-30.00	11 401				
YG85-017	28281.09	30702.49	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.59				
YG85-017	28275.23	30702.49	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	11.59				1
Y685-017	28269.37	30702.49	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.59				
YG85-017	28263.50	30702.49	-65.00	0.00049	0.01167	0.02155	0.01931	-70.00	11.60				
YG85-017	28257+62	30702.49	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.61	•			
YG85-017	28251.69	30702.49	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.64				
YC05 017	28245.72	30/02+49	105 00	0:33276	6.57876	0./56/2	11+32777	-100.00	11.66				1
1000-017	20207+71	30702+47	-115 00	0.00084	0.00002	0.00275	0.00748	-110.00	11+6/				
Y685-017	28227.70	30702.49	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.47				
Y685-017	28221.69	30702.49	-135+00	0.00000	0.00000	0.00000	0.00000	-140.00	11.66				
YG85-017	28215.68	30702.49	-145.00	0.00000	0.00000	0,00000	0.00000	-150,00	11.67				
YG85-017	28209.67	30702+49	-155+00	000000	0+00000	0.00000	0,00000.	-160.00	11.67				
YG85-017	28203.66	30702.49	-165.00	0.00000	0.00000	0.00000	0.00000	-175.00	5+03				
			•										
	· · · · · · · · · · · · · · · · · · ·		FLEUATION									······	
	COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE				•
<u>Y685-018</u>	28306.23	30705.18	15.00	0.00000	0.00000	0.00000	0,00000	10.00	14.86				ten de-aptendan dat av 'n 1 militain oppen alle Albeite
YG85-018	3 28295.47	30707.00	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.75				
Y685-018	28284+79	30/08.88	-5.00	0.00000	0.00000	0.00000	0.00000	~10.00	14.75				
Y685-018	29243.ΔA	30710+77	-25.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.75				
YG85-018	28253.09	30714.74	-35.00	0.00000	0.00000	0.00000	0.00000	-30,00	14.471				
Y685-018	28242.99	30716.93	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.37				
Y085-018	28232.98	30719.18	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14,27				
Y685-018	28223.07	30721.47	-65.00	0.00000	0.00000	0,00000	0.00000	-70.00	14.27				
YG85-018	28213,15	30723.76	-73,00	0.00000	0.00000	0+00000		-80.00	14.27				
Y685-018	28203.23	30726.04	-85.00	0.36431	1.46925	0.14625	2+37846	-90,00	14.28				
1080-018 Y685-019	) X0173+28 28187.20	30728+34	-95,00 -105 00	0.01179	0.29112	0+02328	0.44692	-100.00	14.30				
Y685-018	28177.25	30732.97	-115.00	0.04491	0.64710	0.11577	1 11470	-120.00	14+34				
YG85-01E	28163.20	30735.29	-125.00	0.57715	2.31784	0.29990	1+10402 3.92417	-130.00	8,08 14+37				
							0.001720	A GOVEN Y	0+20				

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7	MN7AFT&T	HIAA TERESP	NOZA.TELL	TNARENASST.	BEN:1	12-416-198/	5 16:03	Page 12				•
		onvicted.			<u></u>	<u>x., 11000 x.700</u>	<u> </u>				 	
				OF MID								
7		COMPOSITE	COMPOSITE	POINT OF					BASE OF	ΜΊΠΤΗ ΟΕ		
		Y-00080	Y-008B	CUMPUSITE	ARSENT	SHI PHU	STLUER	TRON S	IFUEL	COMEDSITE		
	HOLL RO+	V-000KD	1 GUUKD		1112031-1212	10101011110			1-1- + 1-1-	CONTOSTIC		•
5	V685-019	28274.74	30741.44	25.00	0.00000	0.00000	0.00000	0.00000	20.00	5.07		
	Y685-019	28223.75	30740.75	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.61	 	
	VC05_010	20217 14	70770 94	5.00	0.00000	0.00000	0.00000	0.00000	0 00	1 1 2 1		
3	Y005-019	28213+14	30732+00	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14+01		
	V005-019	20101 04	30738.24	-15.00	0.30410	0.34939	0.35053	0.25078	-20.00	14.55		
	YG95-019	20121.42	30730.78	-25.00	0.00000	0.00000	0.00000	0.00000	30 00	14.57		
)	Y685-019	28170.88	30737.41	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.5%		
	Y685-019	28160.37	30737.04	-45.00	0.03739	0.12764	0.01199	0.18457	-50.00	14.51	 	
	Y685-019	28149.94	30734.81	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	14.40		
)	Y685-019	28139.58	30736.63	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14:40		
.	V005_010	70170 74	70774 45	-75.00	0 30113	0.10141	0.00145	0.11700	-80.00	1 4 777		
	V005-019	20127427	20736.27	-85.00	0.00000	0.00000	0.00000	0.00000		14.30		
3	YG85-019	28108.77	30736.09	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.27		
	1000 017	2.0.1.0.0.777	00/00/07	7.774.4					<u></u>		 	
)				FLEUATTON								
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1		COMPOSITE	COMPOSITE						DACE OF	UTITU OF		
5	HOLE HO	V_CODER	V-CONBR V-CONBR	COMPOSITE	ADDENT	011.500	CTI UED	тром е	LENET	POMPORTE		
		X-COUKD	1-GOURD	GOMEUGLIE			0.1.V.N		<u>la C. V C. (.</u>	<u>conrustic</u>		
	V005000	00007 40	70740 04	15 00	A AAAAA	0 00000	0 00000	0 00000	10 00	10 10		
$\rightarrow$	1080-020	20227+00	30740+00	10.00	0.00000	0.00000	0.00000	0.00000	0.00	12+17		
	10605020			-5.00	0.00000	0.00000	0+00000	0.00000		12+17		
	1080-020	20213477	20737+33	-0400	0.00000	0.00000	0.00000	0.00000	-10+00	. 12.17		
>	1680-020 VCDE-000	28290+77	30/38+70		0.00000	0.00000	0.00000	0+00000	-20.00	12+17		
	<u>1000-020</u>	20177.03	30/30+23	75 00	0.00000	0.00000	0.00000	0.00000		12 10	 	
	1685-020 V005-020	20172+71	30737480	-33100	0.00000	0.00000	0+00000	0100000		12+17		
)	YG85-020	28183.78	30738+70		0.00000	0.00000	0.00000	0+00000		12417		
	10007020	20177494	30733467					0,00000		14117		
	1685-020	28172+10	30733+64		0.00000	0.00000	0.00000	0.00000	-70.00	12.17		
	Y085-020	28160+10	30730+01	-/0.00	0.00000	0.00000	0.00000	0.00000	-80.00	12+20		
· ' ;	<u>1660-020</u>	<u>20100+10</u>	<u>- 30/34+40</u> 7077770	-05 00	0.00000	0.00000	0.00000	0.00000	-100.00		 	
	1060-020	<0101+21	30/334/7	-70+90	0.00000	0+00000	0.00000	0100000	-100+00	1.4.4.4		
· )												
				FLEHATTON	e de la construcción de la construcción de la construcción de la construcción de la construcción de la constru							
				OF KID								
)		COMPOSITE	COMPOSITE	501NT OF					DACE OF	111010 OF		
	UNLE HO	V-CODED	<u>V_COOST</u>	COMPACT OF	ADOCHT		CTINCO	TOON C	E 51151	<u>WAND1_0</u>	 	
	FROME ROUTE	Y. COOUN	1 0.001010	çom oarre	m17397487	(2)(2)(2) (1)(U)	ማ መደረ ዎ የነበላ	C+ 2147741	ta ta Vita ta	0000 0011E		
	Y685-022	28225.28	30778.94	15.00	0.00000	0.0000	0.00000	0.00000	10.00	11,01		
	Y005-022	20220120	70779 01	E 00	0.00000	0.00000	0.00000	O	··· ·····	10 00		
	1000-022	20210+20	30770+01		0.00000	0.00000	0+00000	0.00000	-10 00	12 00		
)	1080-022 Y095-022	20211+22	30770+00	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	1454855 1910 - 1919		
	V005 022	20207+27	70770431	- 25.00	0.00000	0 00000	0.00000	0.00000	-70 00	<u> </u>	 	
	1080-072	28177+17	20220 71	-23:00	0.00000	0.00000	0.00000	0.00000	-30.00	విజి+నిమి కారా శిశ		
	1080-022	28170+20	30778+31		0.00000	0.00000	0.00000	0.00000	-40.00	12+18		
-	1000-V22	20102+31				<u></u>	0 00000			ు వచ+విలే కారా కారా		
	1000-002				0.00000	0+00000 A AAAAA				10 +7		
5	1680-022 VC05-022	201207+36 20120 /0	30770 37		0.00000	0.00000	0.00000	0.0000	-/0,00	12:13		
	10607022	<u>20104+04</u>	70770 00	<u> </u>	<u>0.00000</u>	0.00000	<u>0+00000</u>	<u> </u>		<u> </u>	 	
	1080-022	- 20190+0V	30770473	-00+00 _05 00	0+00000 0+00000	0.00000	0.00000	0.00000	*******	కళశమిమి కారా రాజు		
•,	1080-022	20140+00 20171 EX	- 39777+13 - マムマンローマム		0.00000	0.00000	0.00000	0.00000	-110.00	12+23 10 00		
÷'	1000-V22		70770 24					0+00000		10.00		
	10807032	20107 AD	20777401		0.00000	0.00000	0.00000	0.00000	- 120 - 00	14+22 10 00		
3	1000-022	. 20127+48	50//74/0	-120+00	0.00000	0.00000	0+00000	0.00000		1202		

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ſ		<u></u>									- w			
5	YG85-022	28120.45	30779,89	-135.00	0.00000	0,00000	0.00000	0.00000	-140.00	12,22				·
	1033-023													-
			•											
<u>`</u> }		<u></u>		ELEVATION								· · · · · · · · · · · · · · · · · · ·		
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	ытрты ор				
9	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE .				
	V000 407		74760 07	05 00					<b>6 6 6 6</b>	<b>—</b>				
)	YG85-023	28227+12	30759.93	25+00	0.00000	0.00000	0.00000	0.00000	20.00	5.51				
	YG85-023	28204.62	30759.09	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15.06				
$\mathbf{x}$	Y685-023	28193.38	30758.68	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	15.05				
/	1685-023 V095-027	28182.12	30/58,26	-15,00	0.00000	0,00000	0,00000		-20,00	15.06				
	Y685-023	28159.55	30757.46	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	15,10				
)	YG85-023	28148.26	30757.07	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	15.09				
	Y685-023	28136.96	30756.67	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	15,10				
- I ···			an an tha a finan and a sa ann ann an an tha ann an an an an ann an ann an	ELEVATION										
				OF MID										
) <u> </u>		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF				
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE				
5	YG85-024	28219.99	30759.84	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.09				
i	Y685-024	28213.20	30759.79	5.00	0.00000	0.00000	0.00000	0.00000	0,00	12.09				
·	YG85-024	28206.40	30759.75	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.09				
-	Y685-024	28199.61	<u>30759,70</u>	-15.00	0.00000	0.00000	0,00000	0,0000	-20.00	12.0?	`			
	Y685-024	28185,92	30739+70	-23,00	0.00000	0.00000	0.00000	0.00000	-30.00	12+11				
)	Y685-024	28178.92	30760.05	-45,00	0.00000	0.00000	0.00000		-50.00	12,26				
	Y685-024	28171.84	30760.38	-55.00	0.00000	0+00000	0.00000	0.00000	-60.00	12+26				
·,	Y685-024	28164.75	30760.72	-65.00	0.00000	0.00000	0,00000	0.00000	-70.00	12.26				
	Y685-024	28150.58	30761.39		0.00000	0.00000	0.00000	0.00000		12.24				
								· · · · · · · · · · · · · · · · · · ·	/ • • • • •	.1 <i>x</i> . + ∞, Q				
)														
				ELEVATION										
)		COMPOSITE	COMPOSITE	POINT OF					BASE OF	ытатн ог				
i	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE				
5														
1	1685-025	28163.80	30843.53	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.27				
	YG85-025	28141.73	30846.10	~5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.90				
)	Y685-025	28130.70	30847.46	-15+00	0.00000	0.00000	0.00000	0.00000	-20,00	14.95				
1	Y685-025	28119.67	30848.81	-25.00	0.00000	0.00000	0+00000	0.00000	-30.00	11.87				
)   -														
				ELEVATION		· · · · · · · · ·								
				OF MID										
2		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WINTH OF				
	HULE NU+	スールリロ民リ	T-CHIRD	CUMPUSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE				•
)	Y686-002	28308.65	30704.72	15,00	0.00000	0.00000	0.00000	0,00000	10.00	12.71				
	YG84-002	28300.86	30705.62	5.00	0.00000	0.00000	0.00000	0.00000	0.00	12.71			•	•
, ]	Y686-002	28293.06	30706.52	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.71				
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Y694-002	28285.24	30707.41	-15.00	0.00000	.0.00000	0.00000	0.00000	-20.00	19.79	
Y686-002	28203+26	30708.24	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.73	
Y686-002	28269.51	30709.09	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.83	
YG86-002	28261.51	30709.93	-45+00	0.00000	0.00000	0.00000	0.00000	-50.00	12.85	
YG86-002	28253.48	30710.78	-55.00	0.00000	0.00000	0,00000	0.00000	-60.00	12+85	
YG86-002	28245.46	30711.62	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.85	
YG86-002	28237.43	30712.46	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	12.86	· · ·
YG86-002	28229.35	30713.28	-85.00	0.00000	0,00000	0.00000	0.00000			
YG86-002	28221.23	30714.07	-95,00	0.00000	0.00000	0.00000	0.00000	-100.00	12.91	
Y686-002	28213.08	30714.84	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.94	
Y686-002	28204.84	30715.53	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	13.02	
Y684-002	28196+48	30/18+13	-120.00	0.00000	0.00000	0.00000	0.00000	-1.30.00	13+08	
1086-002	28188.03	30/10+07	-145.00	0.00000	0.00000	0.00000	0.00000	-150 00	13+14	
200-0001	20170 00	70717161	-155 00	0.00000	0.00000	0.00000	0.00000		17 07	
1086-002	20170+00	30719.09	-145.00	0.77997	0.75777	0.95759	3,72079	-170.00	10.20	
Y684-002	28153.26	30718.35	-175.00	0.00876	0.17735	0.02044	0.32018	-180.00	13.44	
Y084-002	28144.24	30718.49	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	17.49	
1000-002	20144+24 201	30710+47	199100	0+00000	0+00000		0.00000			
, .,	1911 - 1 T. J. S.	anna mar cann actor a rear y brown fan haitinn e	ELEVATION							
			OF MID							
	COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF	
HOLE NO.	X-000RD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE	
YG86-005	28310.61	30704.12	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.33	
Y686-005	28305.27	30704.21	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.33	
YG86-005	28299.94	30704.30	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.33	,
Y684-005	28294.60	30704.40	-15.00	000000	0.00000	0.00000	0.00000	-20.00	11.33	
Y686-005	28289.34	30704.48	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.27	
YG86-005	28284.17	30704.56	-35.00	0.00000	0.00000	0+00000	0.00000	-40.00	11,24	
YG86-005	28279.06	30704.61	-45.00	0.00000	0.00000	0.00000	0.00000	-50,00	11.22	
YG84-005	28273.97	30704.65	-55,00	0.00000	0.00000	0.00000	0.00000	-30.00	11.22	· .
Y686-005	28268.87	30704.70	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.22	
Y686-005	28263+76	30704+73	-/5+00	0.00000	0.00000	0.00000	0.00000	-30,00	11.24	
1686-005	28258.59	30/04./4	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	11.28	
1086-005	28253+38	30/04./4	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.27	
1030-003	20240.10	30704+74	-115 00	0.00000	1 47450	0.10000	7 66765	-110+00	11.428	
1000-000	- AGK4X+74 	30704+74	-125 00	0.00000	L+0-34-37	0+12724	3+00000	+70.00	11 70	
Y684-005	28232.41	30704.74	-135.00	0.00000	0.00000	0.00000	0.00000	-140 00	11+30	
Y686-005	28227.16	30704.74	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.30	
Y684-005	28221.90	30704.74	-155.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.29	
YG86-005	28216.60	30704.78	-165.00	0.03412	1.23601	0.10258	2.22384	-170.00	11.34	
Y686-005	28211.21	30704.85	-175.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.37	
Y686-005	28205.72	30704.97	-185.00	0.00000	0.00000	0.00000	0.00000	-190.00	11.45	
YG86-005	28200.13	30705.15	-195.00	0.00000	0.00000	0.00000	0.00000	-200.00	11.47	
Y686-005	28194.51	30705.34	-205.00	0.00000	0.00000	0.00000	0.00000	-210.00	11.48	
YG86-005	28188.87	30705.57	-215.00	0.11252	0.16762	0.02654	0.16889	-220.00	11.49	
Y686-005	28183.22	30705.84	-225.00	0.00000	0.00000	0,00000	0.00000	230.00	11.49	
YG86-005	28177.57	30706.11	-235.00	0.00000	0.00000	0+00000	0.00000	-240.00	10.53	
			FLEVATION	=						
			OF MID							
	COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF	
HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE	
	_ )								· · · · · · · · · · · · · · · · · · ·	
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	_MOZART\$I	UAO: [RESP]	NOZA.TELLJ	TNABENA58T.	REN 1	12-AUG-1986	16:03	Pase 15					
5	YG86-007 YG86-007	28311.89	30703.01	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.84			
	Y684-007	28303.65	30701.66	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.84			•
~	YG86-007	28299.54	30700,99	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.84			
. ' (	Y686-007	28295.35	30700.29	-25,00	0.00000	0.00000	0.00000	0.00000	-30.00	10.39			
[	Y686-007	28291.01	30677+00	-45.00	0.00000	0.00000	0.00000	0.24308	-50.00	11.04			
D	Y686-007	28281.88	30698.01	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	11.04			
	YG84-007	28277,28	30697.24	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.04	· ·		
$\sim$	YG86-007	28272.63	30696.48	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.07			
)	Y686-007	28267.86	30695.72	-85.00	0.02868	0.04374	0.26327	0.01864	-90.00	11,14			
	YG86-007	28263.00	30694.98	-95.00	0.00180	0.00152	0.15942	0.00000	-100.00	11.15			
2	YG86-007	28258.12	30694+25	-105.00	0+43907	5.68491	0.31855	9.71325	-110.00	11 + 10 11 + 17	•		
	1086-007	20233120	70407.05	-125.00	0.00000	0.00000	0.00000	0.00000	-170.00	11 19		· · ·	
	Y686-007	28240+27	30692160	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.17			
0	YG86-007	28238.39	30691.46	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	11.17			
İ	Y686-007	28233.46	30690.77	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.17			
-	YG86-007	28228.52	30690.07	-165.00	0+00000	0.00000	0.00000	0.00000	-170.00	6.51			
	· · · · · · · · · · · · · · · · · · ·			1997 - 19									
5				ELEVATION									
	···· ····	COMPOSITE	COMPORTE		······				PACE OF				
$\mathbf{a}$	HOLE NO.	X-COORD	Y-COORD	CONPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE			
	Y684-009	28313.09	30703.39	15.00	0.00000	0.00000	0.00000	0.00000	10.00	10.74			
	Y686-009	28310.46	30703.27	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.34			
) [	YG86-009	28307.82	30703.14	-5.00	0.00000	0.00000	0.00000	0.00000	-10,00	10.34			
ſ	Y684-009	28305.18	30703+02	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10.34			
.,	Y686-009	28302.54	30702.90	-25.00	0.00000	0.00000	0.00000	0.00000	-30,00	10.34			
. 1	Y686-009	28299.90	30702+78	-35,00	0.00000	0.00000	0.00000	0,00000	-40.00	10.34			
	Y686-009	28297.27	30702.65	-45.00	0.04469	0.00264	0.13988	0.00000	-50,00	10.34			
	YG86-009	28294.60	30702.51	-55.00	0,00000	0,00000	0.00000	0.00000	-30.00	10.36			
	YC94-009	20200 01	30702337	-75 00	0.00000	0,00000	0,00000	0,0000	-90.00	10+30			
	1000-007	20207+21	30702+23	-25.00	0.00000	0.00000	0.00000	0.00000	-80.00	10+30			
	YG86009	28283.72	30701.94	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.38			
	Y686-009	28280.95	30701.79	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.38			
	Y686-009	28278.18	30701.65	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	10.28			
	Y686-009	28275.41	30701.51	-125.00	0.00000	0.00000	0.00000	0,00000	-130.00	10.38			
	Y686-009	28272.64	30701.38	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.38			
	Y686-009	28269.87	30701.29	-145.00	0.00718	1.19843	0.12130	2.21700	-150.00	10.38			
1	Y686-009	28257.10	30701+23	-155.00	0,00000	0,00000	0.00000	0.00000	-140.00	10.38			
	1082-009	28264.32	30/03+19	-165+00	0.00000	0.00000	0.00000	0.00000	-170.00	5.86			
	-												
				ELEVATION									
_ ,		CONDOTIC	CONDOCTTO	OF MID						be not with them a be affected			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	STLVER	TRON S	FUE!	COMPOSITE			
,	V694-011	00707 70	70700 70	15 00	A AAAAA	0.00000	A 00000						
· · · [	Y684-011	2030/1/0	30/00+/0	00+00 20+00	0.0000	0.00000	0.00000	0.00000	10.00	14.33			
	Y686-011	28288.31	30694.11	-5.00	0.29733	0.35481	0.02144	0.35950	=10.00	14+33 14 77			
$\supset$	YG86-011	28278.58	30691.11	-15.00	0.00000	0.00000	0.00000	0.00000	-20,00	14.26			
ĺ	YG86-011	28268.85	30688.29	-25.00	0.00000	0,00000	0.00000	0,00000	-30.00	14.21			
. 1	YG86-011	28259.13	30685.57	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	14.20			

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6													
	Y686-011	28249.41	30682.88	-45.00	0.00000	0,00000	0.00000	0.00000	-50.00	14.20			
	Y686-011	28239.69	30680.28	-55,00	0.00000	0.00000	0.00000	0.00000	-60,00	14,17			
	Y686-011	28229.98	30677.85	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.14			•
	Y686-011	28220.24	30675.56	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.14			
	Y686-011	28210.46	30673.49	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	14.14			
	Y694-011	28200.45	30671.56	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14,14			
	Y006-011	20200000	70449 45	-105.00	0.00000	0.00000	0.00000	0.00000	~110.00	14.14			
1	YG94-011	20121 02	30337,00	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	14.14			
	1000-VII	20101+02	70445 97	-125 00	0 00000	0.00000	0.00000	0 00000	-170 00	4 47			
	1999-011	20171+21	-2400-1+03	- 120+00	0.00000	0+00000	V+0000V	V • V V V V V	100+00	0+07			
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′ ł	····	w		FLENATION									
		CONCRETTE	CONFORTE	00 01 05 00 01 05					BASE OF	11 TO TH OF			
'		CUNFUSITE	CONFOSILE	CONSCRIPT	A DOC 2117	000 0000	eti Hre	TOON C	1 6161	COMPOSITE			
1	HOLE NO.	X-000K0	Y-COORD	COMPUSICE	AKSENI	SULFHU	311.VER	UNUN 3	LEVEL	CUMPUSITE			
、								0 00000	40.00	10 77			
'	Y686-013	28309.60	30/01.34	15.00	0.00000	0.00000	0+00000	0.00000	10+00	1.2. + / /			
1	Y686-013	28302.11	30698.71	5.00	0.00000	0.00000	0.00000	0+00000	0.00	12+77			
	Y686-013	28294.61	30696.14	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.76			
, I	Y686-013	28286.98	30693.77	-15:00	0.20873	0.42131	0.10174	0,39013	<u>-</u> 20+00	12+85			
	Y686-013	28279.13	30691.55	-25.00	0.00000	0.00000	0.00000	0.00000	-30,00	12.96			
	Y686-013	28271.19	30689+36	-35.00	0.00000	0.00000	0+00000	0.00000	-40.00	12.96			
) [	Y686-013	28263.17	30687.22	-45.00	0.00000	0.00000	0.00000	0.00000	-50,00	13.03			
	YG34-013	28255.04	30685.23	-55.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.06	•		
	YG86-013	28246.84	30683,42	-65.00	0.00000	0.00000	0,00000	0.00000	-70.00	13.06			
)	Y686-013	28238.41	30481.77	-75.00	0.00000	0.00000	0+00000	0+00000	-30.00	13.06			
	Y686-013	28230.31	30680.27	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	13.10			
	Y686-013	28221.94	30678.90	-75.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.12			
	Y686-013	28213.55	30677.60	-105.00	0.00000	0.00000	0.00000	0.00000	-110,00	13,12			
ſ	Y686-013	28205.13	30676.33	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	13.15			
1	Y686-013	28196.68	30675.12	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	13.15			
) i	Y686-013	28188.23	30373.93	-1.45.00	0.00000	0.00000	0.00000	0.00000	-140.00	13.15			
	Y686-013	28179.78	30472.74	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	6.94			
1	1000 010	2.01//4/0		2 10 000									
				FIFUATION							· ·····		
ļ			•										
,		COMPOSITE	COMPOSITE	POINT OF					RASE OF	WINTH OF			
1		V COODD	V 00000	COMPOSITE	ADOCHT	euroun	CTI HED	TRONE	1 6461	COMPOSITE			
ļ	nu.m. Nu.	X-000800	1-00000	com ostre.	HIN OCH (	outrau	0.1.1. V C K	TUUM 9	LEVILL	CONFUSITE			
1	Y004-015	20711 44	20701 00	15 00	0.00000	0.00000	0.00000	0.00000	10.00	11 22			
		20311+04	<u>- 30701+88</u> 70100 07	1.0.00 E AA	0.00000	<u>0.00000</u>	<u>0.00000</u>	0 00000	10.00	11 00			
l	1086-015	20040402	30377+85	3+00	0.00000	0.00000	0+00000	0.00000	0.00	11 - 20 11 - 20			
, 1	1686-015	28302.00	30897+84	-5.00	0.00000	0.00000	0.00000	0.00000	-10+00	11+28			
1	1686-015	28297+10	30575.70			0,00000	0.00000	0.00000	O+00	11+40		1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	
į	Y686-015	28292.26	30694.09	-25.00	0.08352	0.50063	0.10/55	0.77040	30 + 00	11.28			
۰ I	YG86-015	28287+32	30692+35	-35.00	0.00000	0+00000	0.00000	0.00000	-40.00	11.29			
	Y686-015	28282.32	30690.65	-45,00	0,00000	0.00000	0.00000	0,00000	-50+00	11.32			
1	Y086-015	28277.30	30688.98	-55.00	0,00000	0.00000	0.00000	0.00000	-60.00	11.32			
	Y686-015	28272.25	30687.32	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.33			
1	YG84-015	28267.15	30685+69	-75,00	0.00000	0.00000	0.00000	0.+00000	-80.00	11.36			
	YG86-015	28261,95	.30684.10	-85.00	0.00000	0.00000	0.00000	0.00000	90.00	11.40			
. 1	Y886-015	28256.71	30682.55	-95.00	0.00000	0.00000	0.00000	. 0.0000	-100.00	11.39			
)	Y686-015	28251+47	30681.04	-105.00	0.00000	0.00000	0.00000	0.00000	-110,00	11.39			
	Y686-015	28246.24	30679.53	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	11.39			
	Y686-015	28241.01	30678.03	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	11.38			
2	YG86-015	28235,79	30676.54	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.37			
	Y686-015	28230.63	30675.05	-145.00	0.00000	0.00000	0.00000	0,00000	-150.00	11.34			
1	Y686-015	28225.50	30673.58	-155.00	0.00000	0.00000	0.00000	0.00000	-160.00	11.33			
)		· · · · · · · · · · · · · · · · · · ·											

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$\langle  $	YG84-015	28220.39	30672.11	-165.00	0.00000	0.00000	0.00000	0.00000	-170.00	11.33		
				and an Andrew Terk Terkana								•
5			· ·	ELEVATION							· .	
5	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	OF MID POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S.	BASE OF	WIDTH OF COMPOSITE		•
)	YG86-017 YG86-017	28309.27 28300.92	30698.64 30692.57	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.40		
	Y686-017	28292.55	30686.61	-5.00	1.01549	3.39980	0.10939	4.82248	-10.00	14.33	· · · · · · · · · · · · · · · · · · ·	
$\mathbf{x}$	Y686-017	28283.99	30680.78	-15.00	0.00000	0.00000	0.00000	0,00000	-20,00	14.48		
1	1086-017 V094-017	202/2+24	306/0+01	-75.00	0.00000	0.00000	0.00000	0.00000	-40,00	14.49	· · · ·	•
	Y684-017	28257.71	30663.49	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	14.49		
)	Y686-017	28248.83	30657.76	-55.00	0.00000	0.00000	0.00000	0.00000	-60,00	14.61		
	Y686-017	28239.79	30652.06	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	14.66		
	Y686-017	28230.70	30446.38	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.66		
'	Y686-017	28221.61	30640.70	-85.00	<u>+_000000</u>	0.00000	0.00000	0.00000		14.00		
)				ELEVATION								
				OF MID							·	:
)	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WINTH OF COMPOSITE		
	YG86-019	28311.00	30699.91	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.62		
)	YG86-019	28304.77	30695.38	5.00	0.00000	0.00000	0.,00000	0.00000	0.00	12.62		- 
	YG86-019	28298.52	30690.97	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.55		
	Y685-019	28292.20	30686.80	-15.00	0.17865	0.32697	4.11407	0,19826	-20.00	12,54		
	Y694-019	20203+70	30002+00	-35.00	0.00000	0.00000	0.00000	0.00000	-40,00	12:54		
	Y686-019	28272.74	30674.95	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.56		:
)	YG86-019	28266.24	30671.02	-55.00	0.00000	0.00000	0.00000	0,00000	-60.00	12.56		
i	Y686-019	28259+73	30667.09	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.56		
1	Y686-019	28253.22	30663.17	-75.00	0.00000	0.00000	0.00000	0.00000	-80,00	12.56		,
-	Y686-019	28246+72	30659+24	-95.00	0,00000	0.00000	0.00000	0.00000	-100.00	12+00. 10.54		
	Y684-019	28233.68	30651.57	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.52		
<u>)</u>	Y686-019	28227.16	30647.80	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.52		
	Y686-019	28220.63	30644.03	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	8,59		
1												
'				ELEVATION								
				OF MID								
' i	HOLE NO.	COMPOSITE X-COORD	Y-COORD	COMPOSICE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE		
									_			
.1	YG86-020	28285.11	30702.89	25,00	0,00000	0.00000	.0.00000	0,00000	20.00	. 6+22		
	Y686-020	28278+39	30702+36	15+00	0.00000	0+00000	0.00000	0.00000	-10.00	12+06		
	YG86-020	28264.94	30701.83	-5.00	0.47382	4.67757	1.83605	8.14552	-10.00	12+08		
	Y686-020	28258.22	30700.78	-15.00	0.17617	2.62369	5.62829	3.77765	-20.00	12.06		
	A089-050	28251.49	30700.24	-25.00	0.00837	0.00826	0.04479	0.00000	-30.00	12.06		
.)	Y686-020	28244.76	30699.72	-35,00	0.00004	0.00078	0.00272	0.00000	-40+00	12.07		
	Y684-020	28238+04	30699.19	-45.00	0.00000	0.00000	0.00000	0+00000	-50.00	12.06		

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		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF			
)	HOLE NO.	Y-008D	Y	COMPOSITE	ARSENI	SHI PHD	STIUER	TRON S	I EUEI	COMPOSITE			
		<u></u>	1 300103	0011 00210				CIXOR 5	Inter Viela			 	
	Y684-021	28313.24	30701.52	15.00	0.0000	0.00000	0.00000	0.00000	10.00	10 74		· .	
)	Y686-021	28310.08	30699.13	5.00	0.00000	0.00000	0.00000	0.00000	0.00	10.76	,		
	Y684-021	28706.90	30696.75	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.76			
	Y684-021	28303.70	30694.38	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	10 77			
)	Y686-021	28300.46	30692.03	-25.00	0.04674	0.22246	0.04083	0.27737	-30.00	10.78			
	Y686-021	28297.17	30489.49	-35,00	0.00000	0.00000	0.00000	0.00000	-40.00	10.79		 	
	Y684-021	28293.83	30487.35	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.80			
)	Y686-021	28290.49	30685.01	-55.00	0.00000	0.00000	0.00000	0.00000	-60.00	10180			
	Y686-021	28287.14	30682.66	-45.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.80			
	Y694-021	28287.77	30480.30	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	10.82			
)	Y686-021	28280.34	30677.91	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.84			
	Y684-021	28276.92	30475.51	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.84		 	
	Y686-021	28273.48	30673.11	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	10.84			
	Y686-021	28270.05	30470.70	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	10.84			
	Y686-021	28244.40	30448.29	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.84			
	Y684-021	28244.13	30445.84	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.84			
)	Y684-021	28259.45	30663.42	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	10.86			
Ì	Y686-021	28256.18	30660.99	-155.00	0,00000	0.00000	0.00000	0.00000	-160.00	9,84		 //	
	10.0.0	7	(100001111	4.0070.0		000000	0100000	0100000		7400			
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i				0F MID									
)		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	STLVER	IRON S	LEVEL	COMPOSITE		 	
				•									
)	Y686-022	28284.63	30702.86	25.00	0.00000	0.00000	0.00000	0.00000	20,00	7.94			
	Y686-022	28274.28	30702+59	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.40			
	YG86-022	28263.93	30702.32	5.00	0.01248	0.16411	0,07577	0.23118	0.00	14.39			
)	¥686-022	28253.58	30702.04	-5.00	0.29257	0.74008	1.01892	0.91762	-10.00	14.40		 	
Í	Y686-022	28243.23	30701.77	-15.00	0.62072	0.20478	1,36645	0.00000	-20,00	14,10			
:													
)								11. M					
				ELEVATION									
.				OF MID									
)		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WINTH OF		 	
1	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE			
)	Y686-023	28288+66	30724+25	15.00	0.00000	0.00000	_0.00000	0.00000	10.00	15.24			
	YG86-023	28279+48	30717.32	5.00	0.00000	0.00000	0.0000	0.00000	0.00	15.24			
.	Y686-023	28270.24	30710,47	-5,00	0.00000	0.00000	0,00000	0,00000	-10.00	15.25			
)	YG86-023	28260.90	30703.75	-15.00	0.05974	0.01037	0.50433	0.00000	-20.00	15.24		 	
ļ	Y686-023	28251.54	30697.16	-25.00	0.00665	0.00158	0.02613	0.00000	-30,00	15.16			
	Y686-023	28242+21	30690.62	-35,00	0.00000	0.00000	0+00000	0.00000	-40.00	15.15			
1	Y686-023	28232.90	30684,10	-45.00	0.00000	0.00000	0.0000	0.+00000	-50+00	15.12			
	YG86-023	28223.60	30677.60	-55,00	0100000	0.00000	0.00000	0.00000	-60.00	15,12			
	YG86-023	28214.31	30671+09	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	15.12			
)	Y686-023	28205.04	30664.60	-75,00	0.00000	0.00000	0.00000	0.00000	-80,00	15+09		 	

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2	_MOZART\$	DUAO:ERESP	INOZA, TELLI	ITNABENA58T.	BEN;1	12-AUG-198	6 16:03	Pase 19					
5	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	I.E.VEL	COMPOSITE	 • •		
)	YG86-024 YG86-024 YG86-024	28273.13 28266.14 28259.15	30714.01 30707.72 30701.42	25.00 15.00 5.00	0.00000 0.00376 0.00000	0.00000 0.02385 0.00000	0.00000 0.01009 0.00000	0.00000 0.02064 0.00000	20.00 10.00 0.00	7.87 13.73 13.73			
7	YG86-024 YG86-024	28252.16 28245.18	30695.13 30688.85	-5.00 -15.00	0.00000	0,00000	0.00000	0.00000	-10.00	13.73 13.69		· .	
)				ELEVATION OF MID									•
)	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WIDTH OF COMPOSITE			
)	YG86-025 YG86-025 YG86-025	28290.29 28283.43 28276.53	30725.62 30720.73 30715.91	15.00 5.00 -5.00	0.00000	0.00000 0.00000 0.00000	0.00000 0.00000 0.00000	0.00000 0.00000 0.00000	10.00 0.00 -10.00	13.08 13.08 13.05			·
5	Y684-025 Y684-025 Y684-025	28269.60 28262.65 28255.69	30711.18 30706.48 30701.79	-15.00 -25.00 -35.00	0.00000 0.00000 0.08924	0.00000 0.00000 0.02134	0.00000 0.00000 0.61747	0.00000 0.00000 0.00000	-20.00 -30.00 -40.00	13.06 13.05 13.06			
	Y686-025 Y686-025 Y686-025	28248.73 28241.80 28234.92	30697.10 30692.46 30687.90	-45.00 -55.00 -65.00	0.00000	0.00000	0.00000	0.00000	-50.00 -60.00 -70.00	13.05 13.00 12.74			
<b>^</b> }	Y686-025 Y686-025 Y686-025	28228.07 28221.22 28214.40	30683+38 30678+88 30674+42	-75.00 -85.00 - <u>95.00</u> _	0.00000 0.00000 0.00000	0.00000 0.00000 0.00000	0+00000 0+00000 0+00000	0.00000 0.00000 0.00000	-80.00 -90.00 -100.00	12.94 12.93 12.87			na an an an Anna a San a San anna ann
)	YG86-025 YG86-025	28207.61 28200.82	30670.01 30665.59	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00 -120.00	12.87	 		
)				ELEVATION OF MID									
)	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	POINT OF Composite	ARSENI	SULPHU	SILVER	IRON S	BASE OF LEVEL	WINTH OF COMPOSITE			
4	Y686-026 Y686-026 Y686-026 Y686-026	28273.36 28269.07 28264.78 28260.49	30714.18 30710.31 30706.45 30702.59	25.00 15.00 5.00 -5.00	0.00000 0.00000 0.00000 0.53762	0.00000 0.00000 0.00000 0.24569	0.00000 0.00000 0.00000 1.12008	0.00000 0.00000 0.00000 0.01041	20.00 10.00 0.00 -10.00	7.46 11.55 11.55 11.55			
1				ELEVATION	· · · · · · · · · · · · · · · · · · ·						 		
2	HOLE NO.	COMPOSITE X-COORD	COMPOSITE Y-COORD	OF MID POINT OF COMPOSITE	ARSENI	ទារា.គមា	STLVER	IRON S	BASE OF	WIDTH OF COMPOSITE			
	Y686-027 Y686-027	28291.73	30727.02	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11.39	 ······································		
3	Y686-027 Y686-027 Y686-027	28282.35 28277.66 28272.96	30721.49 30718.72 30715.96	-5.00 -15.00 -25.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.39 11.39 11.39			
)	Y686-027 Y686-027 Y686-027	28268+27 28263+59 28258-91	30713.19 30710.49 30707.84	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.39 <u>11.35</u>	 		
)	Y686-027 Y686-027 Y686-027	28254.25 28249.58 28244.87	30705.18 30702.52 30699.85	-65.00 -75.00 -85.00	0.00000	0.00000 0.00000 1.48112	0.00000	0.00000 0.00000 2.58161	-70.00	11.34 11.34 11.36 11.39			
)	YG86-027	28240.07	30697.17	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11.43			

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Y686-02.	/ 28235.24	30694+48	-105.00	0+00000	0.00000	0.00000	0.00000	-110.00	11+43			
1086-02	/ <u>20230+37</u>	30671+80	105.00	0+00000	0.00000	0.00000	0.00000	-120.00				
1086-02	/ <8223+33	30689+11	-125.00	0.00000	0.00000	0.00000	0.00000	-130,00	11+43			
Y686-02.	/ 28220+/1	30886+42	-135.00	0.00000	0+00000	0+00000	0.00000	-140.00	7.13		<u> </u>	
			CI CUATION									
			OF MID									·.
	COMPOSITE	COMPOSITE				·····		DAGE DE	HYBTH OF			
	. Y-COORD	Y~COORD	COMPOSITE	ARCENT	SHI PUH	GTINED	TOON C	DHSE UP	COMPOSITE			
HOLL ROA			60m 661 FG	PINOL RY		0 E L. V E. K		I. E. V F. C.	COMPOSITE			
YG86-028	8 28284.95	30731.77	15.00	0.00000	0.0000	0.00000	0.00000	10.00	15.50		· · ·	
1086-020	3 X3X/0+50 0 00017 01	30/23+32	5.00	0.00000	0.00000	0.00000	0.00000	0.00	15+50			
1000-020	0 2020/+70	30714400	-3.00	0.00000	0.00000	0+00000	0.00000	-10.00	13+24			
1086-020	3 <u>20200+7</u> 3	30/08+30	-15.00	0.00000	0+00000	0+00000	0.00000	-20.00	16+02			
1086-028	3 20247+42	30678+21	-23.00	0.00000	0.00000	0.00000	0.00000	-30.00	15.96			
Y684-020	3 28270 A0	30620+14	-45 00	0.00000	0.00000	0.00000	0.00000		15 00			
Y684-020	2 2020V+47 2 2020A 04	202002+20 20278 88		0.00000	0.00000	0.00000	0.00000	-40.00	10+07			
- 7000-020 - 7684-0020	3 28211.30	30444.44	-45.00	0.00000	0.00000	0.00000	0.00000	-70.00	15.00			
Y684-029	2 28201.79	30458.85	-75.00	0.00000	0.00000	0.00000	0,0000	-80.00	15.20			
Y68A-029	3 28192.09	30451.20	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	15.29			
Y684-028	3 28182.34	30643.59	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	9.85			
							·			***************************************		
			ELEVATION									
			OF MID									
	COMPOSITE	COMPOSITE	POINT OF					BASE OF	WINTH OF			
HOLE NO	+ X-COORD	Y-COORD	COMPOSITE	ARSENI	SULFHU	SILVER	IRON S	LEVEL	COMPOSITE			
Y686-029	28287+62	30734.41	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.06			
YG86-029	7 28282.98	30729.52	5.00	0.00000	0,00000	0.00000	0.00000	0.00	12,06			
YG86-029	28278.34	30724.63	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	12.06			
Y686-029	9 28273+69	-30719.73	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12.06			
Y686-029	28269.04	30714.84	-25.00	0.00000	0.00000	0.00000	0,00000	-30.00	12.06			
Y686-029	7 28264.40	30709.95	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.06			
Y686-029	7 28259.76	30705.06	-45.00	0.00000	0.00000	0.00000	0.00000	-50,00	12.06			
YG34-029	28255.12	30700.16	-55.00	0+35803	0.05180	0+10140	0.00000	-60,00	12.06			
Y686-029	28250.48	30695.27	-65.00	0.51516	0.07446	0.47160	0.02578	-70.00	12.07			
YG84-029	9 28245.83	30690.38	-75,00	0+00000	0.00000	0.00000	0.00000	-80.00	12.06			
Y686-029	28241.19	30685.48	-85,00	0.00000	0.00000	0.00000	0.00000	-90.00	12.06			
Y086-029	28236+54	30680.59	-95.00	0+00000	0.00000	0.00000	0.00000	-100.00	12.06			
Y686-029	28231.90	30675+69	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	12.06			
YG86-029	7 28227.26	30670.80	-115.00	0.00000	0.00000	0.00000	0+00000	-130.00	12.06			
Y686-029	7 28222+62	30665.91	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	12.07			
Y684-029	9 28217.98	30661.02	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	12.06			
		·····										
			ELEVATION									
	COMPOSITE	COMPOSITE	POINT OF			n a 1 a 11a 11a		BASE OF	итртн ог			
HOLE NO.	- X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE			
Y684-07/	78780 14	30775.77	15.00	0.00000	0.00000	0.00000	0 00000	10 00	10 Q.			
Y084-030	2 20207+10 ) 28284.40	30733473	10.00	0.00000	0.00000	0.00000	0.00000	10+00	10.02			
- 1050-030 - Y686-030	/ 28283.82	30729.13	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.84			
Y684-67	N 28281.15	20705.02	-15.00	0.00000	0.00000	0.00000	<u></u>	-20 00	10 02			
1000-000	/ 20201+10 \ 20202 AD	20720+00 20700 SA	-25 AA	0.00000	0.00000	0.00000		-70 00	10 02			
1000-030	1 20278+47	39722+34	-20+00	V+00000	0.00000	0.00000	0+00000	-30.00	10,80			

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	Y684-030	28275,80	30719.24	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	10.84		
<b>)</b>	Y684-030		30715.94	-45.00	0.00000	0,00000	0,00000	0.00000		1.0 . 86		
	YG86-030	28270.46	30712.64	-55.00	0+00000	0.00000	0.00000	0.00000	-60.00	10.86		
	Y684-030	28267.79	30709.34	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	10.86		
	$- \frac{1686-030}{200}$	28263+12	30708.04	-73+00	0.00000	0.00000	0.00000	0.00000	-80.00	10,86		
	Y686-030	28259.77	30/02+/4	-85.00	0.00000	0.00000	0.00000	0.00000	-100.00	10.86		
)	YG86-030	28257.10	30696.14	-105.00	0.36847	1.86245	0.44185	2.87831	-110.00	10.86		
	Y686-030	28254.43	30692.85	-115,00	0.12535	1.27796	0.02978	1.51268	-120.00	10.86	- ··· · ·	• •
	YG86-030	28251.76	30689.55	-125.00	0.00000	0.00000	0.00000	0.00000	-130.00	10.50		
/		····-	······									
				ELEVATION							· · · · ·	
)			· · · · · · · · · · · · · · · · · · ·	OF MID	and the contract of the Party			a easier the manufacture				
		COMPOSITE	COMPOSITE	FOINT OF					BASE OF	WIDTH OF		
$\mathbf{r}$	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE		
	Y684-031	28277.72	30745.70	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13,80	· · · · · · · · · · · · · · · · · · ·	
	Y686-031	28270+34	30739.70	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.80		
)	YG86-031	28262.96	30733.71	-5.00	0.00000	0.00000	0.00000	0.0000	-10.00	13.80		
	Y686-031	28255+58	30727+71	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	13.80		
$^{1}$	YG86-031	28248.20	30721.71	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	13.80		
7	<u>Y684-031</u>	28240.75	30715+78	-35.00	0.00000	0.00000	0.00000	0+00000	-40.00	13.82		
1	Y686-031	28233.18	30709+96	~45.00	1.06910	1.02653	0+15387	1.00/34	-50.00	13.86		
)	1686-931 Vrok=071	28220+43	30704+24	-55.00	0.00000	0.00000	0.00000	0.00000	-20.00	13+38		
	Y686-031	28209.86	30693.17	~75.00	0.00000	0.00000	0.00000	0.00000	-80.00	13.81	• • • • • • • • • • • • • • • • • • • •	
Ì	YG86-031	28202.08	30687.68	-85.00	0.00000	0.00000	0.00000	0.00000	-70,00	13.81		
) (	Y686-031	28194.29	30682,19	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	13.81		
-												
-												
			· · · · · · · · · · · · · · · · · · ·	ELEVATION								
		COMPOSITE	CONDOCITE	UF MIU						UNDER OF		
	HOLE NO.	Y-COORD	Y-CORRD	COMPOSITE	ARGENT	SUL PHU	STIUFR	TRON S	SADE UF	COMPOSITE		
	110/12/2 / 10/4	<u> </u>			<u>////////////////////////////////</u>				inte i saita			
	Y686-032	28279.17	30747.09	15.00	0,00000	0.00000	0.00000	0.00000	10.00	11.88		
)	Y686-032	28274.04	30743.24	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.88		
	Y686-032	28268.90	30739.39	-5.00	0.00000	0.00000	0.00000	0+00000	-10.00	11.88		
,	Y684-032	28263.77	30735.55	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.88		
1	<u>Y686-032</u>	28258.64	30731.71	-25.00	0.00000	0,0000	0.00000	0,00000	-30.00	11.88		· · · · · · · · · · · · · · · · · · ·
ĺ	Y686-932	28253+51	30/2/+86	-35+00	0.00000	0.00000	0.00000	0.00000	-40.00	11.88		
)	1080-032	20240+37	30724+02	-40.00	0.00000	0.00000	0.00000	0.00000	-50.00	11,88		
	Y686-032	28237.98	30716.45	-45.00	0.00000	0.00000	0.00000	0.00000	-70.00	11.00		
	Y986-032	28232.54	30712.89	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	11.94		
) [	Y684-032	28226.98	30709.44	-85.00	0.00000	0.00000	0.00000	0.00000	-90,00	11.96		
Í	Y686-032	28221+35	30706.05	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	11+97		
,	Y686-032	28215.69	30702+68	-105.00	0.00000	0.00000	0.00000	0+00000	-110.00	6.27		
1												
				FLEUATION								
				OF MID								
Î		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF		
	HOLE NO.	X-COORD	Y-COORD	COMPOSIFE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE		
		00000	70740 0-		A A6447	0 0 0 0 0 0						
	1686-033	28280,42	30/48+03	15,00	0.00000	0+00000	0.00000	0.00000	10.00	10.79		
) [	1000-033	282//+21	30740+36	0+00	0.00000	0+00000	0.00000	0+00000	0.00	10./9		

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2	Y686-033	28274.00	30743.08	-3.00	0.00000	0.00000	0.00000	0.00000	-10.00	10.79		
9	1686-033	28270+79	30/40.61	-15,00	0.00000	0.00000	0.00000	0.00000	-20.00	10.79	and the second second second second second second second second second second second second second second second	
	1085-033	28207+38	30/38+14	-20+00	0.00000	0.00000	0.00000	0.00000	-30.00	10+79		
01	Y684-033	28261.13	30733.21	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	10.79		
$\sim$	Y686-033	28257.93	30730.77	-55.00	0.00000	0.00000	0,00000	0.00000	-60.00	10.79		
	Y686-033	28254.71	30728.33	-65+00	0.00000	0.00000	0.00000	0.00000	-70.00	10.79		
9	Y686-033	28251.48	30725.90	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	1.0 + 7,9	• •	
	YG86-033	28248+22	30723.52	-85.00	0.00000	0.00000	0.00000	0.00000	-90.00	10.79		
2	Y686-033	28244.92	30721.18	-95.00	0.00000	0.00000	0,00000	0.0000	-100.00	10.78		
'  -	<u>Y686-033</u>	28241.62	30/18+85	-105.00	0+00000	0,00000	0.00000	0,0000	-110.00	10.79		
	1686-033	28238.32	30716+02	-125.00	0.00000	0.00000	0.00000	0.00000	-120.00	10+79		
01	Y686-033	28231.68	30711.91	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	10.79		
	Y686-033	28228.34	30709.45	-145.00	0.00000	0.00000	0.00000	0.00000	-150.00	10.79		
	Y686-033	28224.99	30707.39	-155.00	0.00000	0.00000	0.00000	0,00000	-160,00	10.78		
$\odot$								. <u></u>				
				FLEVATION								
$\Box$				OF MID								
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF	· · · ·	
$\sim$	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	IRDN S	LEVEL	COMFOSITE		
	Y684-034	28261.03	30723.11	25.00	0.00000	0.00000	0.00000	0.0000	20.00	7.70		•
	Y686-034	28253.63	30716.90	15.00	0.00000	0.00000	0.00000	0.00000	10.00	13.90		
)	YG86-034	28246.24	30710.69	5.00	0.00000	0.00000	0.00000	0.00000	0.00	13.90		
1	YG86-034	28238.84	30704.49	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	13.90		
_	YG86-034	28231.44	30698.28	-15.00	1.10547	3,31534	2,37040	4.88795	-20.00	13.90		
(1) L	YG86-034	28224.05	30692.07	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	1.2.58		
ł												
0				ELEVATION								
				OF MID								
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF		
×. [	HOLE NO.	X-COORD	Y-COURD	COMPOSITE	ARSENI	SULPHU	STLVER	IRON S	<u>I.EVEL</u>	COMPOSITE		
l	Y686-035	28266+73	30756.79	15.00	0.00000	0.00000	0.00000	0.00000	10.00	14.63		
	YG84-035	28258.36	30750.16	5.00	0.00000	0.00000	0.00000	0.00000	0.00	14.63		
	Y686-035	28249,99	30743.53	-5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.63		
. ]	YG84-035	28241.62	30736.90	-13.00	0+00000	0.00000	0.00000	0.00000	-50,00	14.63		
	Y686-035	28233.24	30730.28	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	14+63		
l	Y686-035	28224+76	30723+84	-35.00	0.00000	0,00000	0.00000	0.00000	-40.00	14.60		
	1086-033	28218+11	30/1/./0	-45.00	0.00000	0.78390	0.03899	0./9033	-50.00	14.06		
	Y604-033	20100.44	30705 82		0.00000	0 00000	0.00000	0.00000	-70.00	14404		
	Y684-035	28189.92	30499.93	-75.00	0.00000	0.00000	0.00000	0.00000	-80.00	14.53		
ļ	Y686-035	28181.18	30694.03	-85,00	0.00000	0.00000	0.00000	0.00000	-90.00	14.53		
-	Y686-035	28172.45	30688.14	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	14.53	ана "Маллон ток му на селата — организация станција, <u>— о</u> 2000 вело селатурија се "Далан и и — око 20 Малија осеру (1999 вели	
	Y686-035	28163.71	30682.24	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	14.53		
	й - Ш										and the second second second second second second second second second second second second second second second	
and the second second				ELEVATION								
! 1		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WINTH OF		
l	HOLE NO.	X-COORD	Y-COORD	COMPOSITE	ARSENI	SULPHU	SILVER	TRON S	LEVEL	COMPOSITE		
· · [			an an ann an an an an an									
l	YG86-036	28268.54	30758.47	15.00	0.00000	0.00000	0.00000	0.00000	10.00	12.36		
	Y686-036	28262+67	30/04.20	5.00	0.00000	0+00000	0.00000	0.00000	0.00	12.36		

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О	_MOZART\$	DUAO:[RESP]	NOZA . TELL J	TNABENA58T	BEN:1	12-AUG-1986	16:03	Pase23				 	
	Y684-034	28254.80	30749.93	-5.00	0.0000	0.00000	0.00000		-10.00	12.74			
0	Y686-036	28250.93	30745.66	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	12,36			
	Y686-036	28245.05	30741.39	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	12.36			
_	Y686-036	28239.18	30737.12	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	12.36			
D (	YG86-036	28233.31	30732+84	-45.00	0.00000	0.00000	0.00000	0.00000	-50.00	12.36			
(	Y686-036	28227.44	30728.57	-55.00	0+00000	0.00000	0.00000	0.00000	-60,00	12.36			
	Y686-036	28221.56	30724.30	-65.00	0.00000	0.00000	0.00000	0.00000	-70.00	12.36			
0	Y686-036	28215.60	30720.15	-75.00	0.00000	0,00000	0.00000	0.00000	-80.00	12.36			
	YG86-036	28209.53	30716.14	-85.00	0.01603	0.03448	0.01779	0.04493	-90.00	12,36			۰.
~	YG86-036	28203.24	30712.22	-95.00	0.00000	0.00000	0.00000	0.00000	-100.00	12.54			
." {	Y684-036	28196.73	30708+35	-105.00	0.00000	0+00000	0+00000	0.00000	-110.00	12.54		 	
	YG86-036	28190.22	30704.48	-115.00	0.00000	0.00000	0.00000	0.00000	-120.00	12.54			
2	Y685-036	28183.72	30700+62	-125.00	0,00000	0.00000	0+00000	0.00000	-130.00	12,54			
. /	1086-038	28177+21	30696+73	-130+00	0.00000	0+00000	0.00000		-140.00	12:54	· · · · · ·		
	1085-036	281/0.70	30672+88	-145+00	0.00000	0.00000	0.00000	0.00000	-150.00	12+54			
5	1686-036	28164+19	30689.02	-155.00	0.00000	0,0000	0.00000	0.00000	-160.00	12.54			
	1000000	20107+07	30800+10	-100+00	0+00000	0+00000	0.00000	0.00000	-1/0.00	/.01		 	
	"			ELEVATION		1 an - 1 101 a 10 a 10 10							
		COMPOSITE	COMPORTE	OF MID						UNDER OF			
5	UDIE NO.	V-COOPD	Y-COOSD	FUINE OF	ARGENT	SHI DUH	STI HED	TDOM C	BASE OF	WINIH UP			
	1101.1_ 11014	<u></u>	1 00000	00x10.	PHYSILITE	0.501110	<u> </u>		1. he ¥ 1. he	CONTRACT		 	
	Y686-037	28269.90	30759.49	15.00	0.00000	0.00000	0.00000	0.0000	10.00	11.25			
1	YG86-037	28265.78	30756.40	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.25			
	Y686-037	28261.66	30753.31	~5.00	0.00000	0.00000	0.00000	0.00000	-10.00	11.25			
	Y686-037	28257.54	30750.22	-15.00	0.00000	0.00000	0.00000	0.00000	-20.00	11.25			
)	Y686-037	28253.43	30747.13	-25.00	0.00000	0.00000	0.00000	0.00000	-30.00	11.25			
1	Y684-037	28249.31	30744.04	-35.00	0.00000	0.00000	0.00000	0.00000	-40.00	11.25		 	
	Y686-037	28245.19	30740.95	-45,00	0.00000	0.00000	0,00000	0.00000	-50.00	11.25			
	YG86-037	28241.07	30737.85	-55+00	0.00000	0.00000	0,00000	0.00000	-60.00	11.25			
i	Y686-037	28236,95	30734.76	-65,00	0.00000	0.00000	0.00000	0.00000	-70.00	11.25			
1	YG86-037	28232.83	30731.67	-75.00	0.00000	0.00000	0.00000	0.00000	-80+00	11.25			
	Y <u>686-037</u>	28228.71	30728,58	-85,00	0.00000	0.00000	0.00000	0,00000	-90.00	11.25		 	
	YG86-037	28224.59	30725+49	-95.00	0.00000	0.00000	0.00000	0.00000	-100+00	11,25			
	Y686-037	28220+47	30722,40	-105.00	0.00000	0.00000	0.00000	0.00000	-110.00	11.25			
	Y686-037	28216+31	30719.34	-115,00	0.00000	0.00000	0.00000	0.00000	-120.00	11,27			
	Y686-037	28211.99	30716.35	-125+00	0.00000	0.00000	0.00000	0.00000	-130.00	11.33			
	Y686-037	28207.54	30713.43	-135.00	0.00000	0.00000	0.00000	0.00000	-140.00	11.33			
	1686-037	28203.09	30/10+52	-145.00	0.00000	0.00000	0.00000	0,00000	-150.00	11.33		 	
	Y686-037	28198+63	30707.63	-135.00	0.00000	0+00000	0.00000	0,00000	-160.00	11+33			
	Y686-037	28194.17	30704+73	-165+00	0.00000	0.00000	0.00000	0.00000	-170.00	11.33			
1	1000-007	20107471	30/01+03			0+00000	0.00000	0.00000	-180.00	11+33			
				ELEVATION									
1				OF MID								 	
		COMPOSITE	COMPOSITE	POINT OF					BASE OF	WIDTH OF			
	HOLE NO.	X-COORD	Y-COORD	COMPOSITE.	ARSENI	SULPHU	SILVER,	IRON S	LEVEL	COMPOSITE			
!	Y684-038	28261.36	30723.38	25.00	0.00000	0.00000	0.00000	0.00000	20.00	4.59			
·	1686-038	28257.07	30/19+51	15.00	0.00000	0.00000	0.00000	0.00000	10.00	11,55		 	
	Y686-038	28252.78	30/15.65	5.00	0.00000	0.00000	0.00000	0.00000	0.00	11.55			
1	1036-938	28248+48 28277 10	30/11+/9	-5+00	0.00000	0+00000	0.00000	0.00000	-10,00	11.55			
	1000-V38	- 494744J7 - 90770 04	20204 01	-10+00 Se AA	0100000	0+00000 A AAAAA	0.00000						
	1000-000	20207+7V 20275 /4	30704+98	ニマロ・ワワ		4 07004	0.00000	0.0000	50+00	11+22			
$\rightarrow$ (	1000-030	20203+01	30700+20		0.4//14	3+97284	0+38727	V+8/86/	-40+00	11+04			

1000 000	28231.32	30696.34	-45.00	0.46027	2.05652	0.60952	3.33599	-50.00	11.55			
		a construction and the second s	ELEVATION		- H - Herre - America -				· · · ·	·		at a manadat
	COMPOSITE	COMEDETTE	OF MID									
HOLE NO.	X-COORD	Y-COURD	COMPOSITE	ARSENI	SULPHU	SILVER	IRON S	LEVEL	COMPOSITE			· · ·
YG86-039 YG86-039	28248,94 28240,81	30731.65 30724.95	25.00 15.00	0.00000	0.00000	0.00000	0.00000	20.00 10.00	9.88 14.53			
Y686-039 Y686-039	28232.68	30718.25	5.00	0.00000	0.00000	0.00000	0.00000	-10.00	14.53		·····	
Y686-039	28216.41	30704+84	-15.00	0.17970	0.10234	0.05371	0.00000	-20.00	14.53			
1006-037	20290+20	20020+14		V • C & 7 S C	V 4 / 7 40 /	<u> </u>		<u>30+00</u>	0,21			
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# APPENDIX III

EXPENDITURES JUNE, 1986 TO FEBRUARY, 1987

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#### NOTES

- (1) The June, 1986 E-SCAN Geophysical Program was an experimental program, therefore the rates charged by Premier Geophysics were lower than normal. Regular rates were charged for the October-December, 1986 program.
- (2) Since several projects were underway on Banks Island at the time of the projects listed here, transportation costs are apportioned from the total amount incurred during each time period.
- (3) Two boats & motors were purchased to transport crews on site during the field projects. The cost has been apportioned as a rate per day used.

## APPENDIX III

GEOPHYSICAL SURVEY PERIOD OF FIELD WORK: JUNE 3 - JUNE 22, 1986

(1) Linecutting & grid	preparation	
Wages K. Burton Jur	ne 6 1 day <b>e</b> 169.71/day	169.71
P. Huxley Jur	ne 6 1 days <b>e</b> 146.57/day	146.57
Equipment Rental EDM S	Survey Equip. 1 day @ 15/day	15.00
Field Supplies Chair	ı Saw, gas & oil	20.00
Camp/Costs 2 ma	n dava <b>a \$</b> 40/dav	80.00
	11 uuyo e 940/uuy	80.00
Transportation Boat &	Motor 1 day <b>@ \$</b> 46.80/day	46.80
•		

Tatal \$558.08 \$ 478.08

#### (2) PREMIER GEOPHYSICS INC.

Wages	G.Shore	June 3–22	12 days @ \$360/day	\$4320.00
	A.Ryder	June 3-22	11.4 days @ \$285/day	3249.00
	B.Pielak	June 3-9,14	.,22 9.6 days @ \$240/day	2304.00
	M.Marchan	t Ĵune 11-22	2 7.2 days <b>@ \$</b> 285/day	2052.00

Equipment Renta	1 E-SCAN System 11 days @ \$1140/da	y \$12540.00	
Field Supplies		- 1346.61	27951-72
MOB/DEMOB COSTS	-	- 16,026.72	28671.19 = 28,429.80
CAMP/COSTS Wages J.Bu	58 Man days @ \$40/day rton(cook) 15 days @ \$108/day	2320.00 1620.00	
TRANSPORTATION	Airfare J.Burton Vanc-Pr Rupert Float Plane 1.1 Flights @ 392/flt Helicopter 3.58 hrs @ \$495.00/hr	286.77 435.00 1774.31	
	Boat & Motor 12 days @ \$46.80	561.60	
COMMUNICATIONS		230.00	7227.68 🗸
REPORT PREPARATIO	Ν		
G.Shore J	une 30,July 14,31,1986 3 days @ \$360	/day 1080.00	
Computer	Costs 12.81 hours @ \$60/hour	608.81	,

TOTAL

608.81 37587.68 7 L 1 737, 346.29

GEOLOGICAL SURVEY PERIOD OF FIELD WORK: JUNE 10-20, 1986	
CONTROL SURVEY	
K. Burton June 9–17, 8 days @ \$169.71/day	1357.68
P. Huxley June 9,14,16,17 4 days @ \$146.57/day	586.78
A. Helfors June 10–13 4 days @ \$114.75/day	459.00
EQUIPMENT RENTAL EDM EQUIPMENT 8 days @ \$15/day	120.00
GEOLOGICAL SURVEY	
J. Shearer June 10–20 10 days <b>@ \$</b> 216.00/day	2160.00
A. Freeze June 10–17 8 days <b>e \$</b> 216.00/day	<u>1728.00</u>

6411.46 🗸

CAMP COSTS	42 Man Days @ \$40/day	1760.00
Wages J.	Burton(cook) 8 days @ \$108/day	756.00
TRANSPORTATION	AIRFARE -J. Shearer	284.90
	FLOAT PLANE 1.1 Flights @ 392/flt	435.00
	BOAT & MOTOR 11 days @ \$46.80/day	514.80
COMMUNICATIONS		150.00

3900.70 🗸

REPORT Wages	PREPARATION J. Shearer July 3–8,1986 5 days @ \$216.00	1080.00
	J. Michell Jan 14,Feb 23, 1987 @ days @ 270.00	540.00
	S. Gardiner Aug 14,feb 19–20 4 days @ 182.25	729.00
	I. Korec Sept 24,29,1986 10 hours @ \$15/Hour	150.00
	C. Mantik July 7,8,1986,Feb20,1986 3 days @ \$135/day	405.00
	S. Johnson Feb 24,25 2 days @ 135/day	270.00

REPRODUCTION

150.00

3324.00	/
\$13636.16	/-

TOTAL

COMPUTERIZATION OF ASSAY RESULTS PERIOD OF DATA PROCESSING: July 3-Aug21, 1986

H.A. SIMONS (INTERNATIONAL) LTD.

Wages O. Syberg July 3-23,A	ug 8-21 27 days @ \$320/day	\$8640.00	
Computer Charges	27 days @ \$50/day	1350.00	
Plotting	35 plans @25.29/plan	885.00	

\$10,875.00 V

REPORT PREPARATION

J. Shearer July 2,24 1 day @ 216/day	216.00
S. Gardiner Feb 10,19,22,23 4 days @ 182.25/day	\$729.00
S. Skermer Feb 21 6 Hours @ \$15/Hour	90.00
Reproduction	250.00 2185.00 × 1285 00
TOTAL	\$12160.00

GEOPHYSICAL SURVEY PERIOD OF FIELD WORK: OCT 20-DEC 10,1986

 (1) LINECUTTING & GRID PREPARATION Wages K.Burton Nov8,10,11 3 days @ \$169.71/day \$848.55 A.Helfors Nov5,8,11 3 days @ 131.14/day 393.42
Equipment Rental EDM Equipment 1 day @\$15/day 15.00 Walkie Talkie 2 days @\$5/day 15.00
Field Supplies Chainsaw,Gas & Oil 115.00
Camp Accomodation 9 Man days @ \$40/day 240.00

Transportation Boat & Motor 5 days @\$46.80/day

140.40 lot 1427.95 ×

•	(2) PREMIER GEOPHYSICS Waaes	
	G.Shore Oct24-28,31,Nov1-16,Dec7 21 days @\$486/day 1	0206.00
	M.Marchant Oct24-31,Nov1,2,4-16 21.66 days @\$386/day	8360.00
	B.Pielak Oct24–31,Nov1–5,7–10,13,14,18.32 days @\$310/day Dec7,8,	4129.20
	T.Gee Oct24,31,Nov1-6,8-15,Dec7,8 21.32 days @\$310/day	6609.20
	B.Smith Oct24-31,Nov1-4,6-10,Dec7,8 16.32 days @\$244/day	3982.08
	Equipment Rental 23 1/3 days @ \$1776.00/day 4	1434.08

Field Supplies

Mob/Demob

<u>2410.46</u> 77857.63

726.81

-29,625°

33 CAMP/COSTS 123 1/3 Man day @ \$40/day \$4933.20 Wages J.Burton(cook) 26 2/3 days @\$123.43 3331.80 3291.47-? Split Charter J & K Burton Transportation 296.00 Float Plane 4.79 Flights @ \$392/flt 1876.71 Helicopter 3.25 hrs @\$495/hr 1609.84 13458.65 X = 13472.65 Boat & Motor 21 days @\$46.80/day 982.80 ÷ Communications 482.50 Report Preparation G.Shore Feb 9-18 7.94 days @ \$480/day 3810.00

G.Shore Feb 9–18 7.94 days @ \$480/day Computer Costs 68.5 hours @ \$50/hour S.Gardiner Aug 13,Dec 11,Feb 18,22 4 days @ 182.25

 $\begin{array}{c} 3310.00\\ 3424.00\\ \underline{729.00}\\ \$99279.28\\ z_{1}, 435_{-}65 \end{array}$ 

166, 353 97 + 1766-97 + 168, 319-

TOTAL

# APPENDIX IV

# PERSONNEL AND DAYS WORKED

# APPENDIX IV

# Personnel & Days Worked

# Trader Resource Corp

J. Shearer	Geologist/Project Manager	June10-20,July3-8, 1986
A. Freeze	Geologist	June10-17,1986
J.Michell	Mining Engineer/Fame Project Supervisor	Jan14, Feb23, 1987
S.Gardiner	Geologist/Fame Project Geologist	Aug 14, Dec, 11, 1986 February 13-21, 1987
K.Burton	Surveyor/Field Supervisor	June6,Nov8,10, 11,1986
P.Huxley	Camp Manager/Labourer	June 6,1986
A.Helfors	Labourer	Nov,8,11,1986
J.Burton	Camp Cook	June3-22,0ct23-31, Nov1-16,1986
I.Korec	Draughtsman	
S.Skermer	Draughtsman	February 21,1986
C.Mantik	Secretary	July 7,8,1986,
	·	February 20, 1987
S.Johnson	Secretary	Feb. 24,25,1987
Premier Geoph	nysics Inc.	

G.Shore	Geophysicist/Crew Chief	June3-22,0ct24-22, Nov1-16,DEc 7,1986
A.Ryder	Geologist/Geophysical Technition IV	June 3-22,1986
M.Marchant	Engineer/Crew Chief/ Geophysical Operator	June11-22,0ct24-31 Nov1.2.4.16.1986
B.Pielak	Crew Chief/Geophysical Operator	June3-9,14-22,0ct 24-31,Nov1-5,1-10, 13.14.Dec7.8
T.Gee	Geophysical Technition IV/ Field Supervisor	Oct24-31,Nov1-6,8, -15,Dec 7,8,1986
B.Smith	Geophysical Technition II	Oct24-31,Nov1-4, 6-10,Dec7,8,1986

H.A. Simon (International) Ltd.

0.Syberg	Engineer	July3-23,Aug8-21,
_	_	1986

APPENDIX V

# STATEMENTS OF QUALIFICATIONS

## STATEMENT OF QUALIFICATIONS

I, Johan T. Shearer of the City of Port Coquitlam, in the Province of British Columbia, do hereby certify:

- 1. I graduated in Honours Geology (B.Sc. 1973) from the University of British Columbia and the University of London, Imperial College (M.Sc. 1977).
- 2. I have practiced my profession as an Exploration Geologist continuously since graduation and have been employed by such mining companies as McIntyre Mines Ltd., J.C. Stephen Explorations Ltd. and Carolin Mines Ltd. I am presently employed by TRM Engineering Ltd.
- 3. I am a fellow of the Geological Association of Canada. I am also a member of the Canadian Institute of Mining and Metallurgy, the Geological Society of London and the Mineralogical Association of Canada.
- 4. I have personally conducted detail geological mapping, logged all diamond core and supervised general exploration field work on the Tel Deposit, Banks Island. This report is an interpretation of the data obtained.

Vancouver, B.C. July 8, 1986

## STATEMENT OF QUALIFICATIONS

I, Sharon L. Gardiner, of the District of North Vancouver, in thr Province of British Columbia, do hereby certify:

- 1. I graduated with a Bachelor of Science, Honours Degree in Earth Sciences (cooperative program) from the University of Waterloo in May, 1979.
- 2. I have practiced my profession continuously since graduation.
- 3. I am a Fellow of the Geological Association of Canada.
- 4. I compiled this summary using reports written by J. Shearer, G. Shore, and data from H.A. Simon Ltd.

Dated at Vancouver this 25th day of February, 1986.

A Saidiner

VICTORIA FAME REPORT (E161) 15759 Chowince of Min Stry Of Energy Millivis and British Columbia Patroleum Resources 113 TYPE OF REPORT/SURVEY(S GEOPHYSICAL; GEOLOGICAL 164,649.15 LUTHORIS J.T. Shearer, G.A. Shore, SIGNATLRE .. S.L. Gardiner CAPE CTATEMENT OF EXPLORATION AND DEVELOPMENT FILED FEb. 26 /87. YEAR C. W. . 1986 PROPERTY NAME/SI .... YELLOW GIANT ........... COMMODITIES PRESENT . A4, A9, Z1, Pb, C4. MINING DIVISION SKEENA 103G/8E STITUDE 53°ZI'57" LONGITUDE 130°9'38" NAMES and NUMBERS of all momens, tanunes in goud standing (when work eval donor the origination of origin). In Clanus' PHORNIX Flow 1706, Minner Lesse & 122, Minner Dent Fran Minner Leart Fill (1) parts ravo vari Yellow Giant 3 OWNER(S) Trader Resource Corp. MAILING ADDREES OFERATORIS' I that is, Company paying for the work as above . . . . . . . . . . . . . . . . . . MAILING ADDRESS SUMMARY GEOLOGY (ithology, age, structure, alteration, minerelitation, size, and attitude) SLAWARY SEOLOGY intrology, are enclosed and stated and stated and stated and stated by narrow, but On the west flank of the Coast Plutonic Complex, northwest trending granitic bodies are separated by narrow, but persistent belts of sedimentary rocks. The Tel Deposit belongs to a series of high grade veins that are controlled by faults and replacement zones within the metasedimentary rock. The section is cut by many faults and shears. The main host REFERENCES TO PREVIOUS WORK in the unaltered and altered slates. A.R. 12719, 14171

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