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Shangri-La Minerals Limited

01/88

REPORT ON YUNIMAN 1986 PROJECT

(PHASE III EXPLORATION PROGRAM)

FOR

Operator: TOBY CREEK RESOURCES LTD.

Owner: John Hrabi

OSOYOOS MINING DIVISION

BRITISH COLUMBIA

NTS 82E/5W

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YUNIMAN PROJECT - 1986

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YUNIMAN PROJECT - 1986

INTRODUCTION AND SUMMARY

During the period July 24th through September 13th, 1986, a program of diamond drilling, hand, and backhoe trenching and sampling, EDM survey, geological mapping and an I.P. and airborne geophysical surveys were carried out on the Main showing of the Yuniman prospect of Toby Creek Resources.

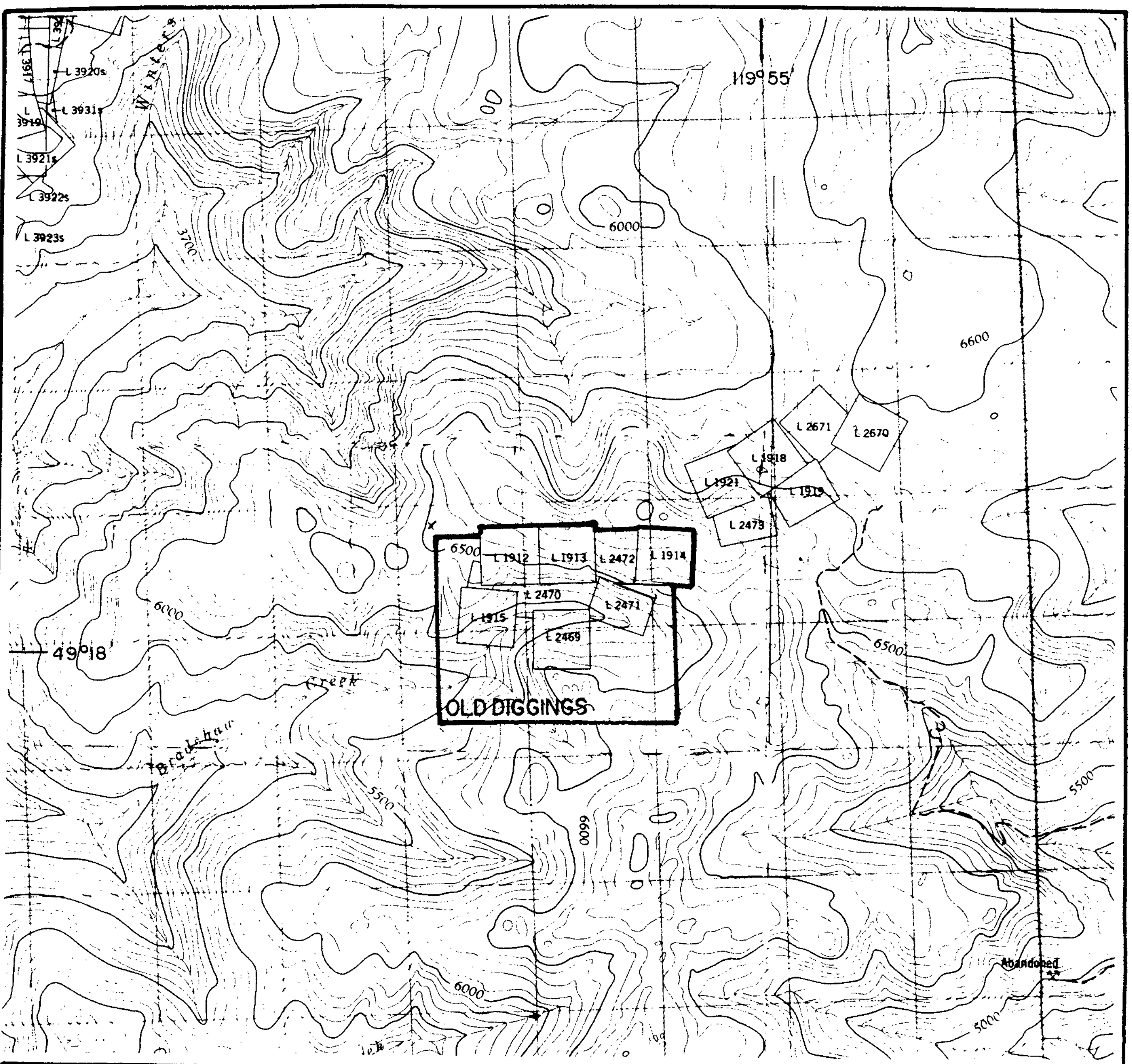
Narrow, NE to ENE - trending fractured sericitized zones within a diorite stock are veined by quartz-calcite-galena-sphalerite veins carrying gold values. Another type of mineralization consists of relatively wide zones of silicified sedimentary rocks, around the diorite stock, which carry veins and disseminations of pyrite, arsenopyrite and gold values.

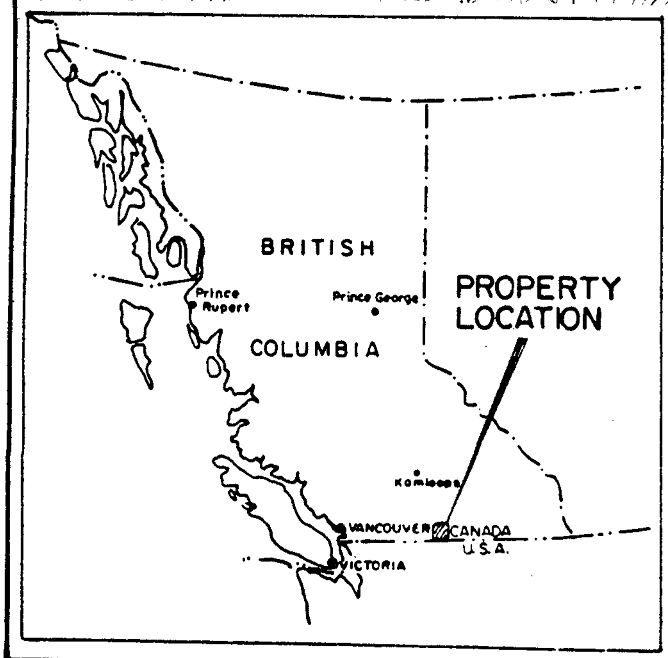
The high grade gold zone in diorite in the Bush Rat pit failed to carry through to depth as tested by drill holes Y86-1 and Y86-6, but the larger zones of low grade gold mineralization such as that in tunnel No 3 and the bottom of DDH Y86-5 could have economic potential, if present in significant tonnages. Further exploration is required to delimit and test the latter type mineralization to see if better grade zones can be found within it.

The zones of quartz replacement in chert carrying pyrite-arsenopyrite with gold values occur in a north-south trending zone near Tunnels 2 and 3. Further exploration of this zone, including detailed magnetic and I.P. surveys, and diamond drilling, is warranted to test the southward projection of the north-south mineralized zones in the valley of Bradshaw Creek. A separate geochemical and geophysical anomaly near 600S, 400E also deserves further work.

PROPERTY AND LOCATION

The claims are located on the crest and south slopes of Yuniman Ridge flanking the north side of Bradshaw Creek. Access is via good gravel roads from Ollala via Ollala Creek, a distance of 20 kilometers from Ollala. Figure No. 1 shows the claim location.





SCALE 1:50,000

0 1 2 3 KM

To accompany report by R.E. Gale, Ph.D., P. Eng.

YUNIMAN PROJECT 1986

FOR: TOBY CREEK RESOURCES LTD.

BY: SHANGRI-LA MINERALS LIMITED

LOCATION MAP

OSOYOOS M.D., B.C.

N.T.S. 82E-5W	DATE: OCT. 1986
DRAWN BY: R.G.	FIGURE No. 1

CHONG

The claims consist of seven reverted Crown Grant Claims, one escheated Crown Grant Claim and the Old Diggings located claim covering about 150 hectares. The claims are situated in the Osoyoos Mining Division. These claims are reported to belong to, or to be held under option by Toby Creek Resources Ltd. The status of the option agreements was not checked by the author.

Description of the claims is as follows:

Name	**Lot No.**	**Record No.**	**Anniversary**	**Area (Hectares)**
Black Pine	1912	(Escheated)	-	20.902
Bush Rat	1913	1163	16 July 1996	20.902
Black Jack	1914	1415	25 May 1996	20.902
Little Bessie	1915	2163	21 Jan 1996	20.902
Far West	2469	2165	21 Jan 1996	20.902
Hub Fraction	2470	2156	21 Jan 1996	16.431
Triune	2471	2155	21 Jan 1996	14.974
Blue Bell	2472	1416	25 May 1996	12.141
Old Diggings	-	2081	9 Aug 1996	450

The claims are located in the Osoyoos Mining Division of British Columbia.

HISTORY, PREVIOUS WORK

The Hedley area and the Yuniman Ridge have been prospected for almost one hundred years. The earliest records are of claim maps published in 1900 showing extensive holdings at the headwaters of Bradshaw Creek. The 1929 Minister of Mines Report states, "Two old cabins.....are in bad repair. The main workings, at an elevation of 6,600 feet, are nearly all caved..... The ore minerals are pyrite and arsenopyrite containing gold. Two dump samples of ore assayed: Gold, 4.30 oz to the ton; silver, 6.2 oz to the ton. And: gold 1.46 oz to the ton; silver 1 oz to the ton."

In 1934 the claims are known to have been owned by Hedley Yuniman Gold Fields Ltd. of Vancouver, B.C. Three adits, two shafts and five trenches are documented in the 1937 Minister of Mines Report by M.S. Hedley. He states that "the presence of a number of fractures in such a small area and the fact that high assays are obtainable is undoubtfully interesting".

An undated report (probably 1941) by Dr. Victor Dolmage states, "It is probable, that the cross veins in trenches 2 and 3 owe their high values to the fact that they are on or close to the long persistent shear which is shown in and between adits 1 and 3".

Regarding a trench found on the Black Pine claim, Dr. Dolmage reported the following gold values: 0.34, 0.59, 1.04, 2.06 and 2.45 ounces to the ton over widths varying from one to two feet.

Dr. Dolmage went on to say that: "The favourable features of this deposit are:

1) the high values found in some of the veins,
2) the large number of veins exposed by the small amount of work done,
3) the fact that the deposit is situated in a district known to have very large and rich gold deposits and,
4. the similarity of some of the diorites associated with the Yuniman deposit to those diorites associated with the rich neighbouring deposit on Nickel Plate Mountain. The unfavourable feature is the narrowness of some of the cross veins.

Mr. J.W. Gallagher, President of Hedley Yuniman Gold Fields Ltd., died in 1975 at the age of 92 years. It is believed that his holdings subsequently were abandoned and the Black Pine Crown Grant escheated while the rest reverted to the Crown.

The claims have changed owners several times since then with nothing but minor physical work reported on them.

In 1984 Toby Creek Resources Ltd. conducted a reconnaissance exploration program on the ground surrounding the Crown Grants. This survey located two test pits in the northwest claim area, one over a 2 m wide shear zone carrying low gold values and the other over a 3-4 m wide shear zone and 5-10 cm wide quartz vein. Samples of the vein returned values up to 0.092 oz of gold per ton. Grab samples collected from the Black Pine claim contained up to 2.81 oz of gold per ton. An anomalous geochemical zone was outlined in the central eastern area. Magnetometer results showed that dykes and small intrusives are associated with magnetic highs. A VLF-EM conductor at in the northwest corner of the property correlated with a geological contact.

The reverted Crown Grants were optioned by Toby Creek in 1985 and geological, geochemical and geographical surveys followed. In addition, the 4 old adits and numerous trenches and pits were cleaned out and sampled. Results indicated northwest trending gold-bearing arsenopyrite-pyrite quartz veins on surface and within adits on the Black Pine claim assaying up to 2.1 oz/ton Au and a northeast trending shear zone assaying up to 0.860 oz/ton Au over 90 cm on the Black Pine and Bush Rat claims. Soils anomalous in gold, silver, and arsenic were outlined on the Black Pine, Bush Rat, Blue Bell and Black Jack claims. Soils collected over the Far West claim were found to be anomalous in arsenic. Conductive zones interpreted from the horizontal loop electromagnetic survey were found to correlate with anomalous gold geochemistry values.

Results of the 1985 survey are presented in the November, 1985 report by F. Di Spirito, P. Eng., and Nigel Holme, B.Sc. The latter report recommended a program of trenching, sampling and drilling which was carried out during the period July 24th through September 13, 1986. The 1986 exploration program is the subject of this report.

REGIONAL GEOLOGY

The Hedley district is underlain by a series of Triassic and slightly older sedimentary and volcanic rocks of the Nicola Group which have been intruded by igneous rocks of Jurassic and/or younger ages. The intrusive rocks consist of large bodies of granite and granodiorite and of smaller stocks of diorite and gabbro with innumerable sill and dyke apophyses.

The Nicola Group rocks have been sub-divided by various authors; the most recent being the divisions as outlined by Bostock, 1940. The Triassic and older rocks of the region consist of the Bradshaw, Independence, Shoemaker, Old Tom, Redtop, Sunnyside, Hedley, Henry, and Wolf Creek Formations. These rocks form a large anticlinal fold whose axis strikes roughly north-south and whose continuity is broken by the bodies of igneous rocks. The Bradshaw, Independence, Shoemaker and Old Tom Formations comprise the east limb and dip moderately to the southeast. The west limb is formed by the younger Redtop, Sunnyside, Hedley, Henry and Wolfe Creek Formations. The Yuniman project area is situated on a portion of the east limb.

The Table of Formations for the Hedley Area is as follows:

TABLE OF FORMATIONS

Quaternary	Stream and glacial deposits.
Early Cretaceous Late Jurassic	Granite
	Granodiorite. Composing the batholith forming the base of Nickel Plate Mountain.
Jurassic	Diorite-gabbro Complex. Comprising stocks with innumerable sill and dyke apophyses.
Triassic	Wolfe Creek Formation. Consisting of andesite and basalt, breccia and tuff, and minor sediments.
	Henry Formation. Consisting of black argillite, tuff and impure limestones
	Hedley Formation. Consisting of massive limestone, argillite, breccia, and interbeds of limestone, quartzite, and argillite.
	Sunnyside Formation. Consisting of limestone and minor argillite-quartzite interbeds
	Redtop Formation. Consisting of interbedded argillite, limestone, and quartzite, volcanics, and minor breccia, resting on massive limestone.
Early Triassic or older	Old Tom Formation. Consisting of basalt, andesite, and minor chert.
	Shoemaker Formation. Cnsisting of chert, tuff, greenstone and limestone.
	Independence Formation. Consisting of chert, chert breccia, argillite, basalt, andesite, quartzite and limestone.
	Bradshaw Formation. Consisting of argillite, tuff, quartzite, breccia, andesite, and limestone.

GEOLOGY - YUNIMAN RIDGE AREA

The predominant rock type in the Bradshaw Creek - Yuniman Ridge area is chert which varies in color from dark brown to dark grey or white. This is a dense fine grained extremely hard rock which breaks with a conchoidal fracture. Most of the rock appears to be massive without any visible bedding, but on close inspection in a few areas, some thin beds (up to 0.3 meters wide) of chert pebble tuff or silt can be detected. In outcrops near the main zone of mineralization, chert beds trend northeast dipping steeply northwest. It is uncertain whether or not the latter orientation of chert beds is present throughout the whole area.

Chert beds are of probably more than one age and one formation. Cherts occur in both the Independence and Shoemaker Formations, both said to be Triassic or older in age. Cherts are in fault contact with andesitic volcanic rocks which are called the Old Tom Formation which is also said to be Triassic or older in age.

Diorite and gabbro intrusions of Mesozoic age cut the Triassic cherts and andesite, and these intrusions are probably associated with the time of alteration and mineralization of the sedimentary and volcanic rocks. Mineralized veins appear to be of two general types and orientations. Northeast to east-northeast trending quartz-calcite galena-sphalerite-gold-silver veins are probably somewhat older than the north to north 20° west trending quartz-calcite-pyrite-arsenopyrite-gold veins. Calcite replacement along small fractures is widespread in the andesite and diorite.

A late-stage white sugary quartz replacement of chert which is cut by quartz-pyrite-arsenopyrite veinlets carries low gold values in some zones and appears to be the most favourable type of mineralization having potential for sizeable gold deposits. A calcite-scapolite-garnet alteration of zones of limy andesite shows some patches of pyrite-gold values but has not been found to form sizeable zones in work done to date.

GEOLOGY - MAIN ZONE

GENERAL GEOLOGY

With reference to Figure No. 4 the four main rock types present in the area are, from west to east across the zone, dark grey argillaceous chert, dark green andesite, buff chert and chert breccia, and biotite-hornblende diorite intrusive rock. A number of relatively narrow light green post-mineral andesite dikes trend north-south through the western side of the zone, associated with late stage N20°W fracturing and faulting along the west side of the diorite stock.

A 5 to 15 meter-wide coarse grained biotite-hornbende breccia dike related to, but probably younger than the diorite stock, has intruded the N20°W fault zone west of the diorite stock. The breccia dike is bordered by an irregular zone of white sugary quartz replacement which is mineralized with small quartz-pyrite-arsenopyrite veinlets, carrying gold values. The dike itself is partly altered and mineralized, and along with the quartz replacement zone, forms the best target for further exploration for gold.

A) DARK GREY ARGILLACEOUS CHERT

The western side of the Main zone shows numerous outcrops of dark grey to black argillaceous chert which is strongly fractured and sheared in a northeasterly direction. The chert is in fault contact with dark green andesitic volcanic rock on its eastern margin.

Disseminated pyrite and arsenopyrite occur on fractures in the chert and low gold values occur within a 10cm wide zone of strong (4-5%) pyrite and arsenopyrite at sample point Y115. This chert was not tested by drilling in the present program, but a soil geochem target farther south within this zone, near 600S, 400E, should be considered for drilling in future work.

B) ANDESITIC VOLCANIC ROCKS

A 60 to 80 metre wide zone of dark green andesitic tuffs and flow rocks outcrops to the east of the dark grey argillaceous chert beds. Three different phases of andesitic to gabbroic rock are distinguishable within this zone. All 3 types show significant calcite content and are characterized by reaction with hydrochloric acid giving off CO_2.

The most common andesitic rock is a very fine grained massive looking tuff or amygdaloidal flow rock which is interbedded with coarser bands or zones of lapilli tuff or flow breccia. A third type of rock, into which the other 2 types may pass almost imperceptibly, is a medium grained crystalline gabbro which sometimes shows "graphic" interlocking texture of mineral grains. This gabbro may be a crystalline flow or more likely an intrusive phase of the andesite which is a slightly younger feeder phase to higher flows or tuffs in the volcanic sequence.

All phases of the andesite are cut by quartz-calcite-pyrite veinlets and widely scattered northerly trending 10 to 20 cm wide quartz-pyrite-arsenopyrite veins. The most concentrated zone of larger veins is explored by Tunnel No. 4.

At Y53 sample pit, a lenticular 1 metre wide zone of pyrite carrying gold replaces calcite-scapolite alteration in andesite. Patches of such alteration and mineralization were cut in drill hole No 4. but such zones appear to be too irregular and small in size to form mineable deposits, unless much wider zones exist somewhere within the area.

Some zones of fractured andesite with numerous very fine quartz-calcite-pyrite arsenopyrite veinlets carry low gold values in zones 0.5 to 2 metres wide. Samples YT57, 59, 61 grading 0.022 to 0.106 oz Au/ton in Tunnel No. 4 are an example of such low grade gold zones in andesite. If wider zones of such stockwork veinlets exist in the andesite, they could also be targets of interest for future work.

C) BUFF CHERT

Outcrops of buff chert are in fault contact with andesite across the east side of the main zone of mineralization. The fault contact runs north to north-northeast across the centre of the area. Along much of the fault zone and just to the east of it, the chert is intruded by a large northerly trending biotite-hornblende gabbro breccia dike and the main diorite stock, and the chert is variably replaced by white sugary quartz carrying elevated values of arsenic and gold.

Narrow 2-10 cm wide quartz-pyrite-arsenopyrite veins cut the chert and/or sugary replacement rocks on both margins of the breccia dike as in Tunnels No. 3 and No. 2 and at surface sample points Y94 and Y209A.

The zone of alteration and mineralization within buff chert surrounding the gabbro breccia dike is open to extension at depth and to the south of the main zone of mineralization. The geochemical data indicates that elevated values of gold and arsenic extend to the south within the chert. Along with the I.P. anomalies present here the geochem anomalies form viable drill targets for a large, low grade gold deposit south of the Tunnel No. 3 area.

D) DIORITE STOCK

A 100 metre by 50 metre stock of biotite-hornblende diorite is intruded into buff chert at the eastern side of the main zone on the Yuniman property. The diorite is relatively fresh but pervasively replaced by small calcite veinlets and several zones of sericite-quartz-pyrite-chlorite alteration along ENE and NE fractures. Some of the alteration zones may follow diorite porphyry dikes which cut the main stock.

Much of the diorite shows disseminated pyrite on fractures and in 2 - 3 different places the altered fracture zones are mineralized with quartz-calcite-pyrite-galena-sphalerite veins carrying gold and silver values. The Bush Rat pit exposes one such vein zone and 2 to 3 other vein zones were cut in DDH Y86-1 and Y86-6.

The Bush Rat vein, up to 1 metre wide, is one of the largest of such veins but based on the drill results it appears that the Bush Rat and the other veins in the diorite do not have good continuity along strike or at depth, and do not form mineable gold deposits.

The western side of the diorite stock may be cut by or merge with a gabbro breccia dike which has proved to be a favorable zone for low grade gold values in altered chert near the dike. The other diorite contacts were not intersected in the drilling, and may also be favorable for alteration and gold mineralization.

E) ALTERATION AND MINERALIZATION

A pervasive quartz-calcite-pyrite alteration affects both the andesitic rocks and the diorite intrusion. Much of the andesite shows marcasite and pyrite mineralization on fractures and pyrrhotite and some chalcopyrite replacing calcite amygdules in the andesite flows. A late phase of quartz-pyrite veins in andesite may carry significant arsenopyrite and often the best arsenopyrite seems to carry the best gold values. Mineralogical studies by C. Soux (Appendix I) point out the direct relationships between arsenopyrite and gold on the Yuniman prospect. In some rocks very fine gold occurs as inclusions in pyrite.

The best example of gold associated with arsenopyrite is the vein intersected in DDH Y86-4 at a depth of 56.77 metres. The latter intersection, about 0.3 metres true width, assayed 1.95% As and 2.77 ozAu/ton. High As almost invariably indicates that Au will be present, but the highest gold value does not necessarily correlate with the highest As value. The intersection in DDH Y86-4 may correlate with the arsenopyrite vein Y45 sampled at surface in 1985 which assayed 2.1 oz Au/ton over a width of 8 cms.

The diorite stock has early-formed marcasite, pyrite and pyrrhotite on fractures while later NE and ENE trending fractures replaced by sericite show quartz calcite-pyrite-galena-sphalerite veins and pods which carry gold-silver values. Some of the more basic phases of the diorite carry increased amounts of magnetite. The diorite stock in itself does not appear to be a good host rock for significant mineralization. The contact rocks on the west side of the stock appear to be favorable and it is possible that the contacts on the north, east and south sides of the diorite stock which are not well exposed, and have been only partly sampled at surface, may be favorable for gold mineralization.

The most significant alteration and mineralization is the north-south trending, white sugary quartz replacement zone along and near the gabbro breccia dike in the centre of the main zone of mineralization. The zone occupied by the breccia dike appears to be a major N to N20°W fault zone, with the dike being a feeder-dike to the diorite stock. Numerous small quartz veinlets with variable pyrite-arsenopyrite occur in this quartz replacement zone along with several northerly trending quartz-pyrite-arsenopyrite veins 1 cm to 10 cms wide.

Intersected in DDH Y86-5, the replacement zone extends from 153 to 217 metres and shows anomalous gold values for most of this interval. Four sections 3 metres or more wide assayed from 0.036 to 0.084 ozAu/ton. An interpretive cross section, Figure No. 5 (line A - A', Figure No. 4) shows the relationship of the altered mineralized zone to the gabbro-diorite dike and the western side of the diorite stock.

The zone as a whole is up to 40 meters wide extending from west of the west contact of the breccia dike east to Tunnel No. 2. Samples YT2 - 7, 9, 11, 13 and 16 in Tunnel No. 3 are within the zone of interest and show values across 2 metre intervals of 0.171, 0.105, 0.078, 0.365 and 0.041 oz Au/ton, respectively. True width of the zone, if it strikes north-south, is in the order of 5-10 metres.

1986 EXPLORATION PROGRAM

During the 1986 program, five diamond drill holes totalling approximately 626 metres, and 25 hand dug and backhoe trenches were excavated and sampled.

An EDM survey grid of 115 survey points was surveyed by Richard Chapman and Associates and maps of the main exploration area of the claims at scales of 1:2500 and 1:1000 have been drawn up (Figures No. 2 and No. 3). Description of survey points and surveyed co-ordinates are included as Appendix H.

Approximately 520 soil geochem samples collected in 1985, but not previously assayed were assayed in 1986 to give a more complete picture of the geochemistry of the area. Ten rock geochem samples were collected on the Far West claim.

Approximately 2,500 metres of reconnaissance I.P. and 12 line kilometres of airborne magnetics and E.M. was completed on the property.

1) SURFACE SAMPLING

Figures No. 6, 7, and 8 show the location of surface and underground sampling completed during the 1986 program and Appendix D, E and F list sample results. A total of 156 surface samples; Y56 through Y210, and 83 underground samples; YT1 - 61 in Tunnel No. 4, and YT2 1-22 in Tunnel No. 3, were collected during the project.

The sampling work emphasizes the localization of the better gold values to veins and sugary quartz replacement zones in the north-south zone in, and near Tunnels No. 2 and No. 3. The best gold values found are in Tunnel No. 3 in a zone which is at least 5-10 metres wide.

Rocks in the Eastern geochem anomaly area were mapped and sampled as shown in Figure 6a. Rock chip samples Y80 to 85, Y120 to 123, Y132 to 134 and Y197, 198 were collected here. Values in the rock run up to 1830 ppb Au (sample Y134) but represent only very narrow fracture zones in chert breccia which are too widespread to be significant.

Two long northwest trending trenches were dug using a backhoe in an area of strong I.P. response about 180 metres northwest of DDHY86-1. Samples Y143 to 149, and Y165 to Y183 taken here failed to show significant values in gold or base metals.

2) GEOPHYSICAL SURVEYS

A report by M. St. Pierre on his August 1986 I.P. survey of part of the Main Zone is included as Appendix A. This test proved that I.P. is a useful tool at Yuniman and picked up an anomalous response northwest of Tunnel No 1 and south, east and west of Tunnel No 3. The area NW of Tunnel No 1 was trenched by backhoe, but the trenching apparently failed to find the source of the I.P. anomaly.

Near Tunnel No. 3 on lines 4+50S and 4+75S St. Pierre's work showed anomalous chargeability at about 700E to 785E which corresponds fairly well with the zone of quartz replacement and mineralization in tunnels No 2 and 3.

A second zone of high chargeability on lines 4+50S and 4+75S was detected at about 530E to 595E. The latter area corresponds with the area of dark grey chert, west of the andesite, carrying disseminated pyrite and arsenopyrite.

Anomalous Au, As values are associated with the I.P. anomaly at 4+50S, 700E and another Au, As anomaly occurs at 600S, 400E, southwest of the I.P. anomaly at 530E to 595E, our lines 4+50 and 4+75S.

Further I.P. work should be done over the whole Main Zone, but the areas near 4+50S, 700E and 6+00S, 400E are of particular interest in an attempt to further define drill targets in the area of the known Au, As geochem anomalies.

The 1985 geophysical surveys indicate that the area just west of Tunnel No. 3 lies on the axis of a north-south E.M. conductor and the eastern edge of a north - south trending magnetic high. A magnetic high is also associated with the Au-As soil geochem anomaly at 600S, 400E. This earlier geophysical work emphasizes the newly-found I.P. and geochem anomalies at the two different points, and also suggests that more magnetic surveys could be useful in defining drill targets.

A 1986 airborne survey conducted by J.C. Graham shows similar magnetic trends and suggests some correlation with features of the E.M. data. Mr. Graham's interpretation is also included in Appendix A.

3) SOIL GEOCHEMISTRY

Soil samples taken with a cast iron mattock from the "B" horizon.

The 1985 soil geochemical values for Au and As were re-plotted and correlated with geological data to determine if the quartz replacement zone near Tunnel No 3 can be detected from the geochemistry results. Re-plotted data is shown in Figures No.9 (As in ppm), and No. 10 (Au in ppb).

The plot of the data for Au and As shows two north-south zones extending south, across Bradshaw Creek. The evidence indicates that the north-south trending altered and mineralized zone west of Tunnel No 3 does extend to the south and forms a significant target for further drilling.

The very high soil geochem results for As south of Bradshaw Creek on the Far West claim were confirmed by rock chip samples taken in 1986. Results are attached in Appendix K. The broad area of anomalous As in soild on the Far West claim should be explored by trenching and further mapping and sampling.

4) TRENCHING

Approximately 25 backhoe and hand-dug trenches were excavated in a number of covered areas in and around the Main Zone. The location of trenches is shown on Figure 4. Trenching to the north and northeast of Tunnel No. 1 was successful in uncovering the Bush Rat shear zone which was found to be gold-bearing, but too narrow to be mineable.

Based on future geophysical survey results in the area of the geochem anomalies south of Tunnels No. 2 and No. 3 further, backhoe and/or dozer trenching is warranted prior to diamond drilling to see if the source of the anomalous As, Au, and I.P. anomalous results can be determined by trenching.

5) DIAMOND DRILLING

The core is stored at a drill site on the property

Approximately 626 meters of NQ diamond drilling in 5 drill holes was completed during the course of the 1986 drill program. Recovery was excellent, being near 100% in most holes, but drilling was slow in the early drill holes because they were located in extremely hard chert and diorite.

DDH Y86-1 drilled southeasterly beneath the Bush Rat pit cut 5.1 metres of 0.122 oz Au/ton in the interval from 15.71 to 20.81 metres depth and 0.037 oz Au/ton in the 3.05 metre interval from 33.01 to 36.06 metres. The latter run also contained slightly elevated lead, zinc, silver and arsenic values and may represent a very low grade down dip extension of the Bush Rat structure, whose projected intersection had been at a depth of 30 to 40 metres.

Figure No. 11 shows DDH Y86-1 and Y86-6 in cross section.

DDH Y86-2 drilled from near the same site as Y86-1 but to the WNW, was designed to test the possible down dip extension of the 7 metre wide zone along the access road sampled as Y59 which assayed 0.08 oz Au/ton, and the pyritized zone which extends west for over 100 metres. No section comparable to sample Y59 was cut in the drill hole but a 21.48 metre long section from 64.85 to 86.33 metres was white quartz replacement alteration of chert carrying anomalous amounts of Au and As in the 50 - 300 ppb Au and 150 to 1000 ppm As range. A 1.83 metre long sample from 77.33 to 79.16 metres graded approximately 0.06 oz Au/ton.

Figure No. 12 shows DDH Y86-2 in cross section.

DDH Y86-3 was abandoned while still in overburden because of drilling problems, and **Y86-4** drilled south from the same site was drilled to test the

"Y53" showing and the zone of quartz veins in andesite south of drill site No Y86-4.

Narrow quartz veins were intersected in Y86-4 from 30.25 to 30.85 metres, 0.6 metres grading 0.193 oz Au/ton and from 37.55 to 38.22 metres, 0.67 metres grading 0.046 oz Au/ton. Low grade gold values occur with narrow quartz veins and pyritized andesite at 73.2 meters depth, 3.13 metres averaging 0.037 oz Au/ton and at 94.63 metres depth a 3.05 metre section of andesite assaying 0.030 oz Au/ton. The most significant vein intersection was 0.76 wide (true width of possibly 0.3 metres) and was cut from 56.77 to 57.53 metres depth. The latter vein contained appreciable arsenopyrite and scattered flakes of free gold and assayed 2.77 oz Au/ton and possibly correlates with the vein sampled at surface as Y45 in 1985. Two inclined drill holes to the west from near the DDH Y86-4 site could test the possible northwest extension of this narrow high grade vein which could have economic significance if it shows good continuity at depth and along strike. The drill holes here would also test the zone of dark grey chert west of the andesite. The chert carries disseminated pyrite and arsenopyrite, some of which has gold values associated with it.

Although scapolite-pyrite mineralization of the type seen in sample Y53 (1985 surface sample assaying 0.339 oz Au over 1 meter) was encountered in DDH Y86-4 no significant gold values occurred in the scapolite-type rock in the drill hole.

Figure No. 13 shows DDH Y86-4 in cross section.

In **DDH Y86-5**, drilled to the NE from near the same site as Y86-4, the andesite extends to a depth of 105 metres before passing into buff chert across a zone of brecciation. At 153 metres the zone of sugary white replacement quartz with anomalous amounts of Au and As was encountered, and this type rock continued to the bottom of the hole at 217 metres, except for the interval from 189 to 207 metres which was diorite-gabbro breccia dike.

The whole zone of quartz replacement shows arsenic values from 500 to 1900 ppm As and gold from 165 to 2940 ppb Au. Four, +3 metre long intervals assayed from 0.036 to 0.084 oz Au/ton, the highest grade interval of 4.25 metres of 0.084 oz Au/ton being at the bottom of the drill hole.

The zone of quartz replacement alteration and mineralization is the most significant gold mineralization encountered in the drilling program and warrants further exploration to determine if the zone may carry higher gold values at depth or along strike, especially to the south of the intersection in DDH Y86-5.

Figure No. 14 shows DDH Y86-5 in cross section.

The last hole drilled in the 1986 program, **DDH Y86-6**, was drilled to the NNW towards DDH Y86-1 at a point east of Tunnel No. 1, in order to further test the down-dip possibilities of the Bush Rat vein zone.

Two 0.6 metre wide quartz-calcite vein-zones containing sparse galena-sphalerite-arsenopyrite and very low gold values were cut at depths of 29 and 70 metres, the upper interval corresponding with a projected 60° dip to the south for the Bush Rat vein. It appears therefore that the gold values in the Bush Rat vein zone have decreased considerably at depth, or the vein sampled at surface has been faulted off and was not cut by either DDH Y86-1 or DDH Y86-6.

Figure No. 11 shows DDH Y86-1 and DDH Y86-6 in cross section.

COST BREAKDOWN FOR PHASE III OF THE YUNIMAN PROJECT

SITE PREPARATION	$ 4,844
DIRECT DIAMOND DRILLING COSTS	68,179
ANALYSIS AND ASSAY COSTS	11,360
STAFF CHARGES	53,248
VEHICLE CHARGES	6,221
CAMP COSTS AND EQUIPMENT RENTALS	21,577
INDUCED POLARIZATION AND LEGAL LAND SURVEYS	9,575
OFFICE AND RELATED CHARGES	1,609
REPORT PREPARATION	6,504
TOTAL COSTS FOR PHASE III	$ 183,117

CONCLUSIONS AND RECOMMENDATIONS

A significant zone of quartz replacement alteration carrying potentially economic amounts of low grade gold and scattered narrow higher grade gold-quartz veins appears to extend south under cover in the Main Zone of mineralization on the Yuniman claims. The gold-bearing potential of the quartz replacement zone in and around Tunnel No. 2 and No. 3 and south to Bradshaw Creek should be investigated by trenching, detailed I.P. and magnetic surveys and further diamond drilling. A detailed I.P. and magnetic survey and drilling is also recommended for the geochem anomaly area at 600S, 400E.

Nine kilometers of I.P. and magnetic surveying is recommended for the two zones of anomalous Au-As geochemistry on east-west lines spaced at 50 metre intervals within the general area from 400S to 900S and 300E to 1000E.

Prior to the recommended drilling program, a program of bulldozer and/or backhoe trenching, is warranted within the areas of I.P. and magnetic anomalies, and As, Au soil geochem anomalies, where overburden is shallow enough to use these trenching techniques. Trenching is especially necessary on the Far West claim where an extensive, strong arsenic anomaly has been outlined but is completely untested to date.

Modifying the pattern of drilling based on the geophysical and trenching results, a series of ten -50° - 100 metre deep drill holes should be drilled on the geochem anomalies at the points indicated on Figure No. 11. A 100 metre -70° hole and a 200 metre -50° hole drilled to the west are also warranted near DDH Y86-4 site to test for possible extension of the high grade vein in DDH Y86-4, and to test the Au-As geochem amomaly in dark grey chert west of the andesite. A 100 metre -50°, and a 250 metre -70° hole drilled west at a point 100 metres west of Tunnel No. 1 is recommended to find the eastern side of the mineralized zone cut in the bottom of DDH Y86-5. These proposed hole locations are shown on Figure No. 9.

The total amount of drilling in 14 drill holes in the initial phase of the recommended program is 1650 metres. The cherty rocks are very hard and expensive to drill but because the rocks core well, BQ drilling should be satisfactory. It is estimated that the initial phase of the trenching, geophysical and diamond drill work would take a minimum of 2 months to complete. Considering the steep slopes over which drill access would have to be made down to Bradshaw Creek, most of the area to be tested would best be explored during the summer months. If all or part of the recommended program is done during the winter, estimated costs could go higher if adverse weather conditions are encountered.

If the initial phase of geophysical work, trenching and drilling is successful in defining a potentially commercial zone of gold mineralization, then a second phase of 2,000 metres of fill-in drilling is warranted.

ESTIMATED COST

PHASE ONE

Geophysical Survey and Trenching

Planning and supervision	$ 2,000
3 man crew magnetic and I.P. survey 9 kms @ $1500/km	$ 13,500
Geological support 20 days @ $250.00/day	$ 5,000
Mobilization and demobilization	$ 3,000
Camp costs - 20 days @ $200/day	$ 4,000
Truck rentals and fuel	$ 4,000
20 days D-8 bulldozer trenching and/or backhoe trenching	$ 20,000
Assays - 300 samples @ $20.00/sample	$ 6,000
Engineering & interpretation 8 days @ $300.00/day	$ 2,400
Drafting and office costs	$ 3,000
Total	$ 62,900

Diamond Drilling

Planning and supervision	$ 5,000
Mobilization and demobilization	$ 10,000
1650 metres drilling - BQ @ $90/metre	$148,500
Road construction including drilling, blasting and D-8 cat rental, plus drill moves by cat, allow	$ 25,000
Camp equipment	$ 6,000
Camp costs - 8 man crew 60 days @ $400/day	$ 24,000
Sample costs - 500 samples @ $20/sample	$ 10,000
Geologist - supervision and geology 60 days @ $300/day	$ 18,000

Core splitter camp helper 60 days @ $150/day	$ 9,000
Cook - 60 days @ $150.00	$ 9,000
Travel expenses	$ 3,000
Truck rental - 2 trucks @ $4,000/mo Including fuel	$ 8,000
Engineering, interpretation, drafting, secretarial and office costs	$ 6,000
Minerology and petrography	$ 3,000
	$284,500
Total estimated cost- geophysics, trenching and drilling - phase one	$347,400

PHASE TWO

Diamond Drilling

Core shack construction	$ 10,000
Road construction and drill moves by cat	$ 15,000
2,000 metres drilling @ $90/metre	$180,000
Camp Costs - 8 man crew - 60 days	$ 24,000
Assay Costs - 600 samples @ $20/sample	$ 12,000
Geologist - supervision and geology 60 days @ $300/day	$ 18,000
Core splitter - camp helper 60 days @ $150/day	$ 9,000
Cook - 60 says @ $150/day	$ 9,000
Truck rental - 2 trucks - 2 months $2,000/mo. including fuel	$ 8,000

Engineering - interpretation, drafting and office costs	$ 10,000
Minerology and metallurgy	$ 5,000
Total Estimated Cost - Phase Two	$300,000
Grand Total Cost If Both Phase One And Two Are Implemented	$647,400

R E Gale

R.E. Gale, Ph.D., P.Eng.
December 5, 1986

REFERENCES

Bostock, H.S.	Map 628A - Olalla 1" = 1 mile, 1937
Di Spirito, F.	Report on Yuniman Crown Grants For Toby Creek Resources November 15, 1985
Dolmage, V.	Private Report for Hedley Yuniman Gold Fields, 1941
B.C. Minister of Mines	Reports, 1929, 1934, 1947.

APPENDIX A

GEOPHYSICAL SURVEYS

(1) INDUCED POLARIZATION SURVEY

A reconnaissance induced polarization survey was conducted on the Yuniman Project for Toby Creek Resources Ltd. Two sets of lines were surveyed (see Figs. 1a-b). One set is the old grid lines 4+50S and 4+75S which run due east-west. The second set runs north-northwest with line 0+00, station 00 at the "Bush Rat" pit and two more lines at 0+25E and 0+25W.

At each station, apparent resistivity (RHO), chargeability (Mt), and self potential (SP) were measured for a minimum of 2 dipole separations. The data are presented in three forms - plan contour maps (Figs. 1a, 1b), profiles (Figs. 2a, 2b), and pseudosections (Figs. 3a-b). Two details should be noted concerning the data presentation. First, in some places it was impossible to obtain a reading because of highly conductive ground. Therefore, there are some places where no data are shown. Second, on the pseudosection for line 0+25E, depths for the readings vary because the station spacing was not uniform on that line.

The zones considered to be anomalous (definite, probable, and possible) are indicated on the pseudosections. The chargeability data were the main consideration in the selection of anomalies. Factors considered were high amplitude, strong gradient, and areal extent. The survey area has a high concentration of pyrite, which has a high chargeability. Therefore, any value smaller than 30 msec was considered to be background. Anomalously high chargeability values presumably indicate an anomalously high concentration of mineralization.

ANOMALOUS ZONES ON LINES 4+50S AND 4+75S

A number of anomalous zones are observed, and seem to correlate well with the mineralization observed on the property.

The anomalous zone on line 4+75S extending from 700E to 750E (see Fig. 3b) corresponds to one on line 4+50S extending from 690E to 785E (Fig. 3a). This is an area of complex lithology, including a silicified breccia zone, and it is possible that the anomaly is due to mineralization associated with a fault zone. The anomaly on line 4+75S is narrower and more clearly associated with a resistivity contrast than the one on line 4+50S, perhaps indicating a more localized zone of alteration and/or mineralization.

A second anomalous zone which is indicated on lines 4+75S and 4+50S is a chargeability high with a related resistivity low and SP anomaly (Figs.2a,2b,3a,and 3b). On line 4+75S, this anomalous zone extends from 530E to 595E. On line 4+50S, it extends from 510E to 585E. This anomalous zone seems to be associated with pyrite mineralization in sheared black chert.

The contact of the black chert with the altered andesite is probably represented by the resistivity drop which occurs at about 600E on line 4+50S and 625E on line 4+75S.

ANOMALOUS ZONES ON LINES 0+25W, 0+00, AND 0+25E

The mineralized showing at the "Bush Rat" trench corresponds to a chargeability high at station 00, line 0+00 (Fig. 3d). An apparently related high occurs at station 5NW on line 0+25W (Fig. 3e). Also on line 0+25W, there is a definite anomaly extending from 60NW to 80NW. It is possibly related to the anomaly at 5NW, since there is a trend of high chargeability visible on the third separation (N=3). All these anomalous zones are underlain by diorite, and are presumably indicative of sulfide mineralization.

The northwest sections of lines 0+25E, 0+00, and 0+25W have high chargeability, low resistivity, and anomalous SP values (Figs. 2c-e, and 3c-e). The anomaly is weakest and narrowest on line 0+25W. On line 0+25E, the anomaly extends from 150 NW to 245 NW. On line 0+00 the anomaly is separated into 2 sections - one section is from 165 NW to 220 NW and the other from 235 NW to 265 NW. On line 0+25W, it extends from 170 NW to 200 NW. This area is underlain by intermediate volcanics with some interbedded chert. The rocks are extensively weathered, fractured, and stained. The chargeability high is probably related to pyrite mineralization.

On line 0+25 E, there is an anomalous zone from 35SE to 115SE. The chargeability increases and the resistivity decreases toward the SE. This may be an indication of increasingly massive mineralization. There is an apparently related, though weaker, anomaly which extends from 50SE on line 0+00.

Line 0+25E has an anomalous zone from 35 NW to 85 NW which does not seem to correlate clearly with the other lines (Fig. 3c). It is probably not related to the "Bush Rat" anomaly present on lines 0+00 and 0+25W, because it occurs in chert rather than diorite, and is probably due to pyrite.

J.C. Graham, B.Sc., M.Eng.

M. St.-Pierre, B.Sc.

December 5, 1986

APPENDIX A

(2) **AIRBORNE SURVEYS**

Magnetometer Survey

The total magnetic field strength results are presented in Fig. A4a. Values on the property range from less than 50 to greater than 500 gammas relative to a datum of 58,300 gammas. The magnetic field strength increases to the northwest, with a steepening gradient in the northwest indicating that the body responsible for the magnetic high is fairly near-surface in that region. Both the Independence and Old Tom Formations have mafic members (greenstone, andesite) which could be responsible for this high magnetic field strength area. There are outcroppings of andesite noted in the northwestern portion of the survey area.

Magnetic field readings could not be obtained in the southwest corner, probably due to a high gradient associated with a diorite/gabbro intrusive noted in the 1985 survey. This area is of particular interest since the VLF-EM results indicate it to be very conductive.

VLF-EM Survey

The VLF-EM survey results are presented in Figures A4b (Seattle) and A4c (Annapolis). Several anomalously high field strength areas are noted, which are indications of conductive zones. Faults, shears, and metalliferous zones are usually conductive, as are swamps.

The most striking VLF-EM anomalies are coincident with the area in the southwest of the survey area where magnetic data were unobtainable. Field strength readings are greater than 50% for the Seattle results and greater than 45% for the Annapolis results, relative to background levels of approximately 15%. These high values indicate a zone of quite high coductivity, possibly associated with mineralization related to the intrusive. The presence of sulphide minerals was noted in this area during the 1985 survey. A strong EM conductor noted in the southwestern corner (LY 1000S, 100E) of the 1985 survey grid is probably related to this anomaly.

Drill holes DDH Y86-4 and -5 are located in a region of high field strength - greater than 25% for Seattle, greater than 45% for Annapolis. The high field strength is probably related to the sulphide mineralization encountered in the drill holes. Another zone of high field strength is approximately 350 m to the west.

There is a northwesterly trending zone of moderately high field strength approximately 100 m east of DDH Y86-1, -2, and -6 which continues to the southeast some 200 m, possibly related to a shear zone.

There is a zone of field strength (> 45%) observed only on Line 2 and only for the Annapolis transmitter, just east of the center of the survey area. The conductivity here is quite possibly associated with wetness, however, as the area is swampy.

The northeastern corner of the survey area is a zone of very high field strength for both the Annapolis and Seattle results, indicating a very conductive zone. The geology of this area has not been mapped.

J. Campbell Graham, B.Sc., M.Eng.
5 December 1986.

APPENDIX B

CERTIFICATE

I, Robert E. Gale, of the City of North Vancouver in the Province of British Columbia, do hereby certify:

That I am a Consulting Geologist with the firm of Shangri-La Minerals Limited, based at 706-675 West Hastings Street, Vancouver, British Columbia, V6B 1N2.

I further certify that:

I) I am a graduate of Stanford University (1965) and hold a Ph.D. degree in Geology.

II) I am a registered member in good standing of the Association of Professional Engineers of British Columbia since 1966.

III) I have been practising my profession as a geologist for thirty-one years.

IV) This report and recommendations are based on my field work on the Yuniman property from July 24th through September 13, 1986, and the study of available data on the property.

V) I have no interest in the property directly or indirectly, or in Toby Creek Resources Ltd., nor do I expect to receive any such interest.

VI) Permission is granted to use this report and recommendations in a Prospectus or Statement of Material Facts.

Robert E Gale

Robert E. Gale, Ph.D., P.Eng.
5 December 1986.

CERTIFICATE

I, Nigel J. Hulme, do hereby certify:

I) I am a Consulting Geologist, with the firm of Shangri-La Minerals Limited at 706-675 West Hastings Street, Vancouver, B.C., V6B 1N2.

II) I graduated in 1982 from Carleton University, Ottawa, Ontario with an Honours B.Sc. in geology.

III) I have been involved in mineral exploration since 1979.

IV) This report is based on a field work carried out by this author and a Shangri-La Minerals Limited staff during the months July, August and September 1986.

V) I hold no direct interest or indirect interest in the property or any securities of Toby Creek Resources Ltd., nor do I expect to receive any.

VI) This report may be utilized by Toby Creek Resources Ltd. for inclusion in a Prospectus or Statement of Material Facts.

Respectfully submitted at Vancouver, B.C.

Nigel Hulme

Nigel J. Hulme, B.Sc.
5 December 1986

CERTIFICATE

I, James Campbell Graham of the City of Vancouver in the Province of British Columbia, do hereby certify:

I) I am a Consulting Geophysical Engineer with the firm of Shangri-La Minerals Limited at 706-675 West Hastings Street, Vancouver, B.C., V6B 1N2.

II) I graduated in 1985 with a M.Eng. degree in Geophysical Engineering and in 1982 with a B.Sc. in Geophysical Engineering from the Colorado School of Mines in Golden, Colorado.

III) I have been involved in numerous mineral exploration programs since 1975.

IV) This report is based upon field work carried out by a Shangri-La Minerals Limited crew in the months of July and August, 1986, and by myself and a Shangri-La Minerals Limited crew on September 5, 1986.

V) I hold no direct or indirect interest in the property described herein, or in any securities of Toby Creek Resources Ltd., or in any associated companies, nor do I expect to receive any.

VI) This report may be utilized by Toby Creek Resources Ltd., for inclusion in a Prospectus or Statement of Material Facts.

Respectfully submitted at Vancouver, B.C.

J C Graham

James Campbell Graham, B.Sc., M.Eng.
5 December 1986.

CERTIFICATE

I, Martin St. Pierre, of the City of Vancouver, in the Province of British Columbia, do hereby certify:

1) I am a Consulting Geophysicist with the firm of Shangri-La Minerals Limited at 706-675 West Hastings Street, Vancouver, British Columbia, V6B 1N2.

2) I graduated in 1984 from McGill University in Montreal with a B.Sc. in Geophysics.

3) I have been involved in mineral exploration since 1982.

4) This report is based upon fieldwork carried out by this author and a Shangri-La Minerals Limited staff during the months of July and August 1986.

5) I hold no direct or indirect interest in the property or in any securities of Toby Creek Resources Ltd., or in any associated companies, nor do I expect to receive any.

6) This report may be utilized by Toby Creek Resources Ltd. for inclusion in a Prospectus or Statement of Material Facts.

Respectfully submitted at Vancouver, B.C.

Martin St. Pierre, B.Sc.
5 December 1986.

CERTIFICATE

I Cristian L. Soux, of the City of Vancouver, in the Province of British Columbia, do hereby certify:

I) I am a Consulting Geologist with the firm of Shangri-La Minerals Limited at 706-675 West Hastings Street, Vancouver, British Columbia, V6B 1N2.

II) I graduated in 1972 from the University of British Columbia and hold a Bachelor of Science degree.

III) Since graduation I have been involved in numerous exploration programs in Canada, Bolivia, Malyasia, Indonesia, Thailand and Ethopia. During the period 1979-1984 I also worked as a consultant and technical adviser in Applied Mineralogy with the United Nations.

IV) This report is based on field work carried out by this author between September 20-24 and later research and laboratory analysis.

V) I hold no direct, nor indirect intertest in the property, or in any other securities of Toby Creek Resources Ltd., nor in any associated companies, nor do I expect receive any.

VI) This report may be utilized by Toby Creek Resources Ltd., for inclusion in a Prospectus or Statement of Material Facts.

Respectfully submitted at Vancouver, B.C.

Cristian L. Soux, B. Sc.
December 9, 1986

APPENDIX C

SURFACE SAMPLE DESCRIPTIONS - YUNIMAN PROJECT - 1986

Y56 **L500S 1430E** **Grab Sample**

Sample of pyritized dark grey chert. Fractures 070°/70°N.

Y57 **30 metres west of DDH 86-1** **Grab Sample**

Sample of pyritized andesite.

Y58 **Six metres northwest of DDH Y86-1** **Grab Sample**

Brecciated dark green volcanic rocks. Stringers of pyrite and trace chalcopyrite trend 050°.

Y59 **24 metres west of DDH Y86-1** **Chip Sample over 7 m**

Strongly shattered oxidized andesite, shatter zone 7 m wide. Fractures 035°/80°W.

Y60 **Located between Y58, Y59** **Chip Sample over 10 m**

Sample of silicified diorite. Pyrite mineralization on fracture planes. Chips at 50 cm intervals.

Y61 **Road to DDH Y86-1 site** **Chip Sample over 10 m**

Silicified, pyritized hornfels and diorite. Chips at 50 cm intervals.

Y62 **Road to DDH Y86-1 site** **Chip Sample over 1 m**

Andesite with carbonate alteration. Pyrite, arsenopyrite; also fine, dark grey mineral in the carbonate.

Y63 **Drill Site DDH Y86-4** **Grab Sample of Float**

Local origin, area of Drill Site #2. Black chert with quartz veinlets. Abundant bright yellow stain.

Y64 **Road to DDH Y86-4 site** **Chip Sample over 8 m**

Dark green basic tuff with abundant carbonate on fractures. Trace pyrite. Chips at 50 cm intervals.

Y65 **Road to DDH Y86-4 Site** **Chip Sample over 16m**

Dark green volcanic rock with 10% pyrite and possibly chalcopyrite.

Y66 **Road to DDH Y86-4 Site** **Chip Sample over 16 m**

Dark green andesitic tuff with abundant carbonate. Pyrite 1-5%. Chips at 50 cm intervals.

Y67	**Road to DDH Y86-4 site**	**Grab Sample**

Biotite-hornblende diorite. Fresh to moderately silicified. Disseminated pyrite on fractures. At contact with carbonate-rich andesite, also included in sample.

Y68	**Road to DDH Y86-4 site**	**Chip Sample over 3 m**

Contact zone between fine-grained silicified diorite on east and silicified andesite on west. Andesite is mineralized with pyrite and possibly chalcopyrite.

Y69	**3 metres to west of Y68**	**Grab Sample**

Silicified andesite with pyrite on fractures, as well as a few arsenopyrite needles. 50 cm northeast of brecciated zone.

Y70	**Road to DDH Y86-4 site**	**Chip Sample over 12 m**

Mixed outcrop and outcrop rubble. Dark green carbonate-rich andesite, white sugary quartz replacement, chert (silicified andesite?). All with trace to weak disseminated pyrite.

Y71	**Road to DDH Y86-4 site**	**Fragments over 8 m**

Rib of hard white silicified andesite with trace pyrite. Zone approximately 8 m wide. Vertical fractures trend 165° to 170°.

Y72	**Road to DDH Y86-4 site**	**Chip Sample over 7 m**

Silicified orange weathering rubbly andesite. Trace arsenopyrite and chalcopyrite in stringers.

Y73	**Road to DDH Y86-4 site**	**Grab Sample**

Green-yellow, clay-rich zone. Several fragments of dark green carbonate-rich andesite. Disseminated pyrite 10%+. Grey chert to west, trace pyrite. Wt: 3 kg.

Y74	**Adit 4 Dump**	**Grab Sample from Dump**

Pyritic dark green andesite, carbonate-rich. Disseminated pyrite, trace pyrrhotite. Wt: 3 kg.

Y75	**Adit 4- Underground**	**Chip Sample over 4.3 m**

West crosscut. Sample of green andesite situated between 2 quartz veins.

Y76	**Adit 4- Underground**	**Chip Sample over 60 cm**

East side of slash near 1985 Sample Y52. Green andesite with trace pyrite.

Y77	**15 m bearing 50° from LY450S, 575E**	**Chip Sample over 3 m**
	Sample is same type rock as Float Sample Y63. Black cherty rock with numerous fine quartz veins and lemon yellow stain on fractures. No visible sulphides. Fracture-quartz veinlets trend 50°.	
Y78	**10 m bearing 220° from LY450S, 575E**	**Chip Sample over 1 m**
	Similar to Y77 but traces of pyrite. Sample over 1 m plus few pieces from outcrop 10 m to southwest. Shears 050°/vertical.	
Y79	**20 m bearing 160° from LY450S, 575E**	**Chip Sample over 1 m**
	Dark chert with strongly pyritized patches.	
Y80	**30 m north of LY300S, 1075E**	**Grab Sample**
	Outcrop in creek bed. Black chert with quartz veinlets. Shearing fractures 165°/vertical.	
Y81	**30 m bearing 340° of 250S, 1125E**	**Grab Sample**
	Dark grey chert.	
Y82	**5 metres west of 200S, 1200E**	**Grab Sample**
	Black Chert	
Y83	**10 metres north of 300S, 1150E**	**Grab Sample**
	Dark grey chert with trace pyrite.	
Y84	**10 metres bearing 30° of 300S, 1150E**	**Chip Samples over 0.3 m in 3 different zones**
	Rusty outcrops - chert.	
Y85	**25 metres bearing 20° from 450S, 1150E**	**Chip Sample over 3 m square outcrop**
	Grey chert.	
Y86	**Southern backhoe trench west of andesite dike, Adit 4 area**	**Chip Sample over 0.3 m**
	Pyritized andesite.	
Y87	**Southern backhoe trench, Adit 4 area**	**Chip Sample over 1 m**
	Pyritized andesite.	

Y88	**Southern backhoe trench, Adit 4 area**	**Chip Sample over 1 m**
	Pyritized andesite	
Y89	**Southern backhoe trench, Adit 4 area**	**Chip Sample over 30 cms**
	Pyritized andesite.	
Y90 cms.	**Southern backhoe trench, Adit 4 area**	**Chip Sample over 30**
	Pyritized andesite.	
Y91	**Southern backhoe trench, Adit 4 area**	**Chip Sample over 30 cms.**
	Pyritized andesite.	
Y92	**East end of southern backhoe trench, Adit 4 area**	**Grab Sample of Float**
	Pyritized andesite.	
Y93	**Pit northwest of Adit 2**	**Chip Sample over 1 m**
	Chert and 4 cm wide quartz arsenopyrite vein	
Y94	**Pit 50 metres northwest of Tunnel #2**	**Chips Sample over two 30 cm wide veins**
	Quartz veins with pyrite.	
Y95	**7 m from east end of northern backhoe trench, Adit 4 area**	**Chip Sample over 2.3 m**
	Silicified andesite or chert.	
Y96	**Northern backhoe trench west of Y95**	**Chip Sample over 2 m**
	Calcite-rich andesite.	
Y97	**Northern backhoe trench west of Y96**	**Chip Sample over 3 m**
	Pyritized - weakly altered andesite.	
Y98	**Northern backhoe trench west of Y97**	**Chip Sample over 3 m**
	Pyritized - weakly altered andesite.	
Y99	**Northern backhoe trench west end**	**Chip Sample over 1 m**
	Pyritized - weakly altered andesite	

Y100	**Northern backhoe trench east of andesite dike** Grey chert and weakly altered andesite.	**Chip Sample over 3 m**
Y101	**Northern backhoe trench east of smaller andesite dike** Pyritized andesite.	**Chip Sample over 5 m**
Y102	**50 metres north of DDH Y86-3 road** Pyritized andesite.	**Chip Sample over 1 m**
Y103	**7 m south of Y102** Pyritized andesite	**Grab Sample of Float**
Y104	**3 m south of 350S, 640E** Pyritized andesite	**Chip Sample over 1 m**
Y105	**East end of trench 20 m west of DDH Y86-3 site** Sheared grey chert, strong iron oxides	**Chip Sample over 2 m**
Y106	**450S, 850E** Pyritized andesite	**Chips across 1.3 m**
Y107	**10 m south of 825E, 425S** Pyritic chert.	**Grab Sample**
Y108	**Outcrops to north of 450S, 950E** Pyritic chert and pyritized andesite	**Grab Sample**
Y109	**Pit at 400S, 915E** Strongly oxidized chert breccia	**Chip Sample over 2 m**
Y110	**70-80 m southeast of Bush Rat Pit** Black chert with strong iron oxides	**Chip Sample over 2 m**
Y111	**5 m east of I.P.-1, Line 0+00, 1+60 N.W.** Graphitic quartz breccia	**Grab Sample of Float**

Y112 — **10 m bearing 140° from Line 1, 0+25E, 1+40N.W.** — **Grab Sample of Float**

Andesite with chalcopyrite

Y113 — **10 m west of I.P. Line 1 L0+00, 1+90 N.W.** — **Grab Sample of FLoat**

Heavy andesite rock.

Y114 — **40 M Northwest of DDH Y86-1** — **Chips Sample over 1 m**

Brecciated chert with disseminated arsenopyrite

Y115 — **30 m bearing 190° from 500S, 575E** — **Grab Sample**

Old pit with fractured chert - arsenopyrite, pyrite

Y116 — **10 m Southwest of Y115** — **Grab Sample**

White-grey chert with arsenopyrite-pyrite

Y117 — **5 m south of 500S, 550E in Creek bed** — **Grab Sample**

Phyllitic gougy chert

Y118 — **850S, 125E** — **Chip Sample over 1 m**

Chert breccia

Y119 — **Float 15 m north of LY100S, 725E** — **Grab Sample of Float**

Grey-green fine-graned andesite tuff. Carbonate filled fracture has malachite stains surrounding vugs. Weathered sulphides present in and around vugs. Fracture 1-2 mm wide. Pyrite, chalcopyrite.

Y120 — **Eastern geochem anomaly area** — **Chip Sample over 25 cm**

Fault breccia & fragments - argillaceous slightly silicified. Yellow and brown staining. <1 Py.

Y121 — **Eastern geochem anomaly area** — **Grab Sample of Float**

Mottled grey cherty rock. Rusty brown and yellow stains when broken open. Carbonatized, silicified, 3% pyrite less arsenopyrite.

Y122 — **Eastern geochem anomaly area** — **Grab Sample**

Altered volcanic. Minor silicification. Much manganese on fractures. <1% disseminated sulphides.

Y123 **Eastern geochem anomaly area** **Grab Sample**

Volcanic with <1 mm wide scoriaceous layers. Pyrite on some fracture surfaces.

Y124 **Trench south of L450S, 825E** **Chip Sample over 4.6 m**

Light grey chert. A few areas show quartz eyes in igneous ground mass. Light orange staining, manganese, >1% sulphides.

Y125 **Trench south of LY450S, 825E** **Chip Sample over 1.65 m**

Quartz eyes in igneous groundmass. Pockets of fine-grained powdery pyrite.

Y126 **Trench south of LY450S, 825E** **Chip Sample over 3.9 m**

Grey chert <1% pyrite. Fracture zone trends 020° with 5-10% pyrite within fracture.

Y127 **Trench south of LY450S, 825E** **Chip Sample over 5.6 m**

Light grey-green chert, with quartz eye bands. Microfractures, larger fractures rare. Manganese stains.

Y128 **Bush Rat Shear, Trench 1** **Chip Sample over 25 m**

Sheared diorite, very crumbly. Width varies from 35 m to 10 cm. Sample from east side of pit.

Y129 **Bus Rat Shear, Trench 1** **Chip Sample over 18 cm**

Sheared diorite, very crumbly. Sample from west side of pit.

Y130 **Bush Rat Shear, Trench 1** **Sample of 2 cm wide fracture**

Northerly trending fracture forms west wall of pit.
Orange gouge like coating on fracture.

Y131 **Bush Rat Shear, Trench 1** **Chip Sample over 10 cm**

Over closely spaced fractures east of Y130. Fractures are 5 cm apart.

Y132 **Eastern Geochem Anomaly Area** **Chip Sample over 50 cm**

50 cm pyrite-rich zone in cherty volcanics. Pyrite up to 10%. mainly along frctures. Grey cherty volcanic with yellow, yellow-green, orange stains. Presence of manganese.

Y133 **Eastern Geochem Anomaly Area.** **Chip Sample over 2 m**

Rusty stained grey and black chert. <1% disseminated pyrite.

Y134 **Eastern Geochem Anomaly Area** **Chip Sample over 15 cm**

Fault breccia in fracture. Grey, cherty volcanics stained rusty orange, rusty brown, yellow, yellow-green. 1-5% disseminated pyrite.

Y135 **Bush Rat Shear, Trench 2** **Chip Sample over 30 cm**

Sample from Floor and both walls of pit. Sheared diorite, some competent lenses, bleached white-green clots of pyrite.

Y136 **Approximately 40 m, N of LY450S, 900E** **Chip Sample over 1.5 cm**

Slightly cherty rock, rusty. Grey-green fresh surface. Manganese coatings, no visible sulphides.

Y137 **Approximately 40 m N of LY450S, 900E** **Chip Sample over 20 cm**

Fault gouge, breccia. Some quartz, slightly vuggy. Rusty stains, no visible sulphides. Manganese coatings.

Y138 **Approximately 40 m N of LY450S, 900E** **Chip Sample over 2 cm**

Rusty cherty volcanics. Grey fresh surface, rusty brown-purple weathered surface. Limonite stains, no visible sulpides. Abundant manganese.

Y139 **Hand trench 5 m N of L450S, 900E** **Chip Sample over 2 m**

Cherty green volcanics and green chert. Rusty staining 1-2% disseminated pyrite.

Y140 **Bush Rat Shear, Trench 3** **Chip Sample, 50 cm**

Rock to east of shear. Light colored chert, minor brecciation, orangy-rust weathering. No visible sulphides.

Y141 **Bush Rat Shear, Trench 3** **Chip Sample, 40 cm**

Breccia, small amount vuggy quartz, rusty brown gouge. (Shear zone).

Y142 **Bush Rat Shear, Trench 3** **Chip Sample over 50 cm**

To west of shear zone. Light colored chert, slightly rusty. No visible sulphides.

Y143 **IP Trench, L0+00 (begin from N end)** **Chip Sample over 5 m**

Grey volcanics, chert, breccia. Mainly rusty stained volcanics. Disseminated pyrite 1-3%, very fine-grained. Rare small blebs. Iridescent sulphide stains on fractures. Manganese.

Y144 **IP Trench, L0+00** **Chip Sample over 4.2 m**

Grey cherty volcanics, chert. Sulphides on fractures and lightly disseminated. Mainly in cherts. Mineralized fracture (pyrite) trends 068°.

Y145 **IP Trench, L0+00** **Chip Sample over 50 cm**

Fine-grained dyke appears to be striking 010°. Light green to grey, very hard, siliceous, disseminated pyrite <1%. Quartz blebs 1 mm wide. Weathered out pyrite.

Y146 **IP Trench, L0+00E** **Chip Sample over 4.7 cm**

Plagioclase phyric andesite. Minor carbonate.

Y148 **IP Trench L0+00** **Chip Sample over 5.3 cm**

Grey, dark grey aphanitic volcanics, some quartz eyes. Rusty stains, iridescent sulphide stains, <1% disseminated pyrite. Manganese coatings. Minor plagioclase phyric andesite.

Y149 **IP Trench L0+00** **Chip Sample over 5 m**

Grey, dark grey aphanitic volcanics. <1% disseminated pyrite, but iridescent sulphide stains, manganese coatings.

Y150 **Hand trench, northwest of 4+50S, 8+50S** **Chip Sample over 5 m**

Pyritized andesite and chert.

Y151 **Hand trench across gully from Y150** **Chip Sample over 6 m**

Chert.

Y152 **Hand trench as above** **Chips Sample over 0.5 m**

Dike rock.

Y153 **Hand trench as above** **Chips Sample over 8 m**

Chert and andesite.

Y154 **Hand trench south of Y53** **Chips Sample over 5.5 m**

Pyritized andesite.

Y155 **Hand trench south of Y53** **Chips Sample over 5.5 m**

Pyritized andesite.

Y156	**Hand trench south of Y53**	**Chips Sample over 8 m**
	Weakly mineralized andesite.	
Y157	**Hand trench south of Y53**	**Chips Sample over 4.2 m**
	Pyritized chert.	
Y158	**Hand trench south of Y53**	**Chips Sample over 8 m**
	Black, sheared chert with Fe oxides.	
Y159	**Hand trench south of Y53**	**Chip Sample over 5 m**
	Platy black chert.	
Y160	**Cut 5 m north of Y53 cut**	**Chip Sample over 2 m**
	Pyritized andesite.	
Y161	**Cut 5 m north of Y53 cut sample to west of Y160**	**Chip Sample over 2 m**
	Fresh andesite.	
Y162	**Cut 5 m N of Y160**	**Chip Sample over 3.7 m**
	Cut fractured, weakly altered andesite.	
Y163	**Same location as Sample Y102 50 m north of road to DDH Y86-3 site**	**Chip Sample over 2.9 m**
	Calcite-rich andesite with disseminated pyrite.	
Y164	**Trench 4 m NW of 350 S 675E**	**Chip Sample over 3.6 m**
	Weakly pyritized andesite.	
Y165	**IP Trench L0+00**	**Chip Sample over 5 m**
	Cherty volcanics, chert. Manganese, sulphide stains, <1% sulphides.	
Y166	IP Trench L0+00	Chip Sample over 5 m
	Pale chert, minor breccia. Rusty weathered surface, no visible sulphides.	

Y167 **IP Trench LO+00** **Chip Sample over 5 mm**

Green cherty volcanics. Brown, rusty stains. No visible sulphides.

Y168 **IP Trench LO+00** **Chip Sample over 5 m**

Grey volcanics. Limonite stains. Microfractures. No visible sulphides.

Y169 **IP Trench LO+00** **Chip Sample over 5 m**

Grey-green volcanics with rusty weathered surface. Manganese stains, no visible sulphides.

Y170 **IP Trench LO+25E** **Chip Sample over 5 m**

Minor rusty stained grey chert. Mainly plagioclase phyric dyke containing 2 mm equant plagioclase. Minor carbonate, no visible sulphides.

Y171 **IP Trench LO+25E** **Chip Sample over 5 m**

Purplish-grey vuggy volcanics, minor pale chert. Rusty brown weathered surfaces. No visible sulphides.

Y172 **IP Trench LO+25E** **Chip Sample over 5 m**

Grey volcanics with rusty weathered surfaces. Microfractures parallel to vague layering. No visible sulphides.

Y173 **IP Trench LO+25E** **Chip Sample over 5 m**

Grey, purplish volcanics. Chloritic surfaces. Rusty.

Y174 **IP Trench, LO+25E** **Chip Sample over 5**

Brown and grey-green silicic volcanics. No visible sulphides, yet rusty stained.

Y175 **IP Trench, LO+25E** **Chip Sample over 5 m**

Rusty-brown weathered volcanics. Manganese, 5% pyrite on fracture surfaces.

Y176 **IP Trench, LO+25E** **Chip Sample over 5 m**

Grey, purplish volcanics, few vugs. Manganese, no visible sulphides.

Y177 **IP Trench, L0+25E** **Chip Sample over 5 m**

Grey-green vuggy volcanics. Rusty stains. Manganese stains, no visible sulphides.

Y178 **IP Trench, L0+25E** **Chip Sample over 5 m**

Grey aphanitic volcanics. Rusty weathred surfaces. Pyrite in streaks along fractures.

Y178 **IP Trench, L0+25E** **Chip Sample over 5 m**

Grey volcanics. Rusty weathered surfaces, limonite stains. No visible sulphides.

Y180 **IP Trench, L0+25E** **Chip Sample over 5 m**

Green cherty volcanics. Slickensides, 5 mm quartz stringer. Rusty stains, no visible sulphides.

Y181 **IP Trench L0+25E** **Chip Sample over 5 m**

Dark grey to black cherty volcanics. <1% disseminated pyrite.

Y182 **IP Trench L0+25E** **Chip Sample over 5 m**

Soft, grey green volcanics. Rusty, yellow stains.

Y183 **IP Trench L0+00** **Chip Samples over 5 m**

Grey aphanitic volcanics, some chert. Rusty orange stains, pyrite disseminated and in clots.

Y184 **Bush Rat shear trench** **Chip Sample over 1 m**

Possible shear zone, cherty rock in muddy matrix.

Y185 **Hand trench above and to East of Adit 4** **Chip Sample over 2 m**

Dark and light green chert. Pyrite. Disseminated and pyrite cubes. Concentrated along and near fractures.

Y186 **Hand trench above and to East of Adit 4** **Chip Sample over 5 m**

Silicic, aphanitic, dark green volcanics. Chlorite along fractures. Pyrite, pyrrhotite 3%.

Y187	**Hand trench above and to East of Adit 4**	**Chip Sample over 2.7 m**
	Coarse-grained andesitic volcanics or offshoot of dyke. Plagioclase phyric. Lightly carbonatized pyrite <1%.	
Y188	**Hand trench above and to East of Adit 4**	**Chip Sample over 7.4 m**
	Highly fractured zone between dyke outcrops. Grey, purple-brown volcanics and cherty volcanics. Purple-brown rock shows wispy layering. Strong smell of H_2S with HCl from this rock - pyrrhotite.	
Y189	**Hand trench above and to East of Adit 4**	**Chip Sample over 3 m**
	Porphyritic dyke.	
Y190	**2nd Hand Trench above Y 53 pit.**	**Chip Sample over 5 m**
	Soft green to pale greeen mafic volcanics, weathers brown. No visible sulphides.	
Y191	**Trench 13 m West of 350S, 675E**	**Chip Sample over 1.3 m**
	Andesite with 4%-5% disseminated pyrite.	
Y192	**West side of Sample Y191** Hornblende andesite or trachyte dike.	**Chip Sample over 2.7 m**
Y193	**Strongly sericitized rock-gouge across back of Tunnel No. 2.**	**Chip Sample over 0.6 m**
	Some chert with pyrite.	
Y194	**No. 2 Tunnel Dump**	**Picked sample of high grade vein**
	(Picked sample of quartz-arsenopyrite vein material.)	
Y195	**Hand trench west of survey point No. 22**	**Chip Sample over 2 m**
	Oxidized chert.	
Y196	**Adjoining Y195 on east** Oxidized chert.	**Chip Sample over 2 m**
Y197	**Trench west from survey point 111**	**Chip Sample over 40 cms**
	Grey-black chert with disseminated pyrite.	
Y198	**Sample adjoining Y197 on west**	**Chip Sample over 10 cms**
	Fault zone in grey chert.	

Y199	**Trench NE of Tunnel No. 2 near survey point 44 at 3.75 m from west end of trench** Altered diorite porphyry dike?	**Chip Sample across 0.5 m**
Y200	**Old trench 1.8 m bearing 160° from survey point No. 45** Sugary quartz replacement of buff chert.	**Chip Sample across 4.7 m**
Y201	**Outcrop white sugary quartz replacement 8.5 m bearing 75° E from survey point 45** White sugary quartz replacement.	**Chip Sample across 2 m**
Y202	**Outcrop white sugary quartz replacement rock 5 m east of survey point 46** Sugary quartz replacement rock.	**Chip Sample across 3.6 m**
Y203	**Outcrop 6m bearing 125° for 6 m from Y202** East-west trending quartz arseno-pyrite vein.	**Picked Sample 10 cm wide vein**
Y204	**Float 10 m east of Y86-5 and Y86-6 roads intersection** Pyritized white sugary quartz replacement rock.	**Float material - blocks on road - sub outcroop**
Y205	**Trench west from survey point 44-2.2 m from west end.** (Quartz replacement in chert with pyrite.)	**Chip Sample 1 m across trench**
Y206	**Same trench as Y205, Y199,** Chert replaced by sugary quartz with disseminated pyrite.	**Chip Sample over 2.8 m**
Y207	**Same trench as Y199, 205, 206** Sample starts 3-75 m from west end white sugary quartz replacement rock	**Chip Sample over 3.75m**
Y208	**Trench west of survey point 51** Fractured chert	**Chip Sample across 6 m**

Y209	**Outcrop 30 m east of DDH Y86-6**	**Grab sample**
	Sugary quartz replacement in buff quartzite - disseminated pyrite and traces fuchsite.	
Y209A	**Trench between survey points 47 (west end) and 48.**	**Chip Sample across 10 cms**
	10 cm quartz vein with pyrite, iron oxides, 1 m from east end of trench.)	
Y210	**Same location as 209A - just west of Y209A**	**Chip Sample across 2.5 m**
	Coarse grained andesite	
Y211	**Same location as Y210 - just west of Y210**	**Chip Sample across 5 m**
	Green-purple aphanitic andesite - 5%. Pyrite and pyrrhotite.	

APPENDIX D - SURFACE SAMPLE ASSAY RESULTS

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM
Y 56	1	16	6	7	1.0	2	1	57	1.04	23	5	ND	2	7	1	6	2
Y 57	8	113	3	127	.1	73	16	716	3.80	7	5	ND	3	19	1	2	2
Y 58	12	1433	14	30	.5	61	40	594	19.09	125	5	ND	5	19	1	2	2
Y 59	3	69	717	280	8.3	44	14	1769	4.67	2225	5	2	3	11	4	2	2
Y-60	2	103	18	37	1.4	45	13	562	2.97	518	5	ND	4	10	1	2	2
Y-61	1	76	12	62	.4	53	22	1279	4.11	83	5	ND	2	25	1	2	2
Y-62	2	207	5	85	2.8	71	43	1701	7.51	283	11	ND	3	102	1	3	2
Y-63	1	16	11	18	.6	6	3	190	1.12	44	5	ND	1	7	1	3	2
Y 64	1	56	4	45	.1	38	19	450	3.05	23	6	ND	1	24	1	2	2
Y-65	1	826	14	24	.4	59	43	409	8.51	14	6	ND	1	25	1	2	3
Y-66	1	85	10	85	.5	73	25	539	4.19	47	5	ND	3	36	1	2	2
Y 67	1	55	3	64	.3	23	16	835	4.32	41	5	ND	2	59	1	2	2
Y 68	9	79	5	61	.8	30	18	656	3.00	408	5	ND	5	9	1	3	2
Y 69	1	84	13	94	.3	39	12	974	3.09	243	5	ND	2	14	1	2	2
Y 70	2	94	7	54	.6	74	17	1133	3.08	288	5	ND	2	9	1	2	2
Y-71	1	102	2	17	.1	24	13	397	2.22	121	5	ND	2	6	1	2	2
Y 72	11	124	11	30	.2	32	17	296	2.65	653	5	ND	2	3	1	2	2
Y 73	1	207	3	33	.3	47	31	621	4.03	247	5	ND	1	20	1	2	2
Y 74	1	133	6	44	.1	47	28	527	3.74	38	5	ND	1	29	1	2	2
Y-75	1	186	9	58	.3	50	32	680	3.94	300	7	ND	1	35	1	2	2
Y-76	1	113	16	41	.3	54	33	1017	4.74	44	13	ND	2	60	1	2	2
Y 77	5	60	15	140	1.0	24	8	332	2.72	61	5	ND	4	9	1	4	3
Y-78	1	44	9	42	.5	16	7	279	2.62	101	5	ND	3	14	1	2	2
Y 79	1	26	7	27	.6	9	4	203	2.02	452	5	ND	1	9	1	3	2
Y-80	6	53	23	44	1.7	74	9	1242	2.62	85	5	ND	2	20	1	5	3
Y 81	1	19	9	23	.1	8	3	268	1.68	4	5	ND	1	2	1	2	2
Y-82	1	37	7	18	.2	4	4	278	1.55	27	5	ND	2	4	1	3	2
Y-83	7	42	20	31	.7	16	6	883	2.25	58	5	ND	2	8	1	6	4
Y-84	2	64	2	48	.5	24	9	584	2.19	36	5	ND	2	24	1	4	2
Y 85	1	63	8	74	.1	26	15	1034	4.69	15	5	ND	2	14	1	2	2
Y 86	1	493	3	30	.3	39	50	431	6.03	115	6	ND	1	22	1	2	2
Y 87	1	74	5	59	.5	49	29	1488	5.62	211	5	ND	1	44	1	2	2
Y 88	1	250	9	50	1.4	33	39	805	7.01	301	5	ND	1	38	1	2	11
Y 89	1	179	7	28	2.7	15	25	446	3.86	705	5	ND	1	12	1	3	3
Y 90	1	105	6	48	.8	49	30	1237	5.55	2680	7	ND	1	104	1	13	2
Y 91	3	531	12	47	3.3	90	48	472	8.97	2810	5	ND	1	15	1	17	4
Y 92	1	571	9	29	.2	61	46	385	5.89	155	5	ND	1	17	1	2	2
Y 93	5	108	3	18	.5	32	16	593	2.83	638	5	ND	2	10	1	2	2
Y 94	3	156	6	25	.9	29	15	444	3.51	872	5	3	3	6	1	2	2
Y 95	1	166	2	31	.3	12	20	726	4.37	59	5	ND	2	49	1	2	2
Y 96	1	270	5	50	.5	54	34	1122	6.43	344	5	ND	1	26	1	2	2
Y 97	1	273	11	39	.5	64	33	709	6.22	64	5	ND	1	22	1	2	2
Y 98	1	198	8	4'	.3	42	37	767	5.07	132	5	ND	1	31	1	2	2
Y 99	1	436	4	28	.3	60	52	500	6.11	14	7	ND	1	23	1	2	2
Y 100	1	183	5	39	.2	37	31	658	4.96	54	7	ND	1	23	1	2	17
Y-101	1	173	2	41	.3	51	33	735	4.71	43	5	ND	1	44	1	2	2
Y 102	1	230	3	29	.3	51	35	515	4.53	34	7	ND	1	29	1	2	2
Y-103	1	225	4	37	.2	67	37	635	4.70	34	7	ND	1	30	1	2	2
Y 104	1	96	10	33	.1	35	22	475	3.70	30	5	ND	1	23	1	2	2
Y 105	1	167	7	71	1.6	78	42	1827	7.83	609	5	ND	1	26	1	4	4

SAMPLE#	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au** PPB	Au** OZ/T
Y 56	3	.01	.013	5	10	.01	114	.01	2	.06	.01	.07	14		.001
Y 57	190	.51	.119	9	89	1.25	63	.12	4	1.58	.12	.66	4		.001
Y 58	118	.55	.074	2	68	.50	20	.05	2	.92	.06	.11	3		.001
Y 59	46	.22	.097	10	36	.98	130	.01	4	1.10	.02	.15	7		.001
Y-60	92	.23	.078	13	56	.90	201	.03	2	1.22	.04	.20	6		.006
Y-61	76	.46	.094	11	62	1.17	338	.16	5	1.80	.08	.72	9		.001
Y-62	173	6.71	.042	4	195	4.53	32	.04	2	2.48	.03	.20	1		.001
Y-63	9	.03	.021	7	16	.05	358	.01	4	.20	.01	.08	15		.001
Y 64	81	1.81	.036	3	98	1.68	83	.28	3	1.83	.23	.21	4	1	
Y-65	167	1.02	.057	2	177	1.26	47	.38	2	2.15	.17	.10	2		.001
Y-66	116	.96	.320	41	98	1.74	309	.22	2	2.21	.12	1.02	5		.001
Y 67	123	1.49	.074	7	89	1.86	165	.10	2	2.32	.16	.26	3	11	
Y 68	39	.15	.050	18	34	.78	182	.05	4	1.16	.02	.35	5	120	
Y 69	311	.17	.026	11	38	.84	809	.06	5	1.00	.02	.31	5	46	
Y 70	61	.25	.040	11	37	.89	250	.06	2	1.04	.04	.24	7	105	
Y-71	32	.13	.042	9	30	.45	59	.03	2	.67	.02	.06	8		.001
Y 72	40	.09	.032	9	28	.34	55	.01	2	.50	.01	.05	8	95	
Y 73	105	.86	.087	8	76	1.90	145	.21	5	1.79	.09	.39	4	355	
Y 74	76	2.15	.033	3	107	1.96	87	.23	8	2.20	.24	.44	3	10	
Y-75	98	4.37	.038	2	122	2.04	48	.26	3	2.20	.27	.25	2		.001
Y-76	118	4.61	.036	2	134	2.19	95	.23	2	2.09	.21	.20	9		.001
Y 77	48	.05	.036	17	29	.23	490	.02	8	.56	.01	.23	7	150	
Y-78	24	.20	.032	13	22	.38	183	.02	5	.73	.02	.24	9		.001
Y 79	11	.08	.032	9	18	.12	92	.01	3	.28	.01	.08	8	36	
Y-80	33	.21	.043	10	30	.44	1151	.01	2	.72	.02	.14	11		.011
Y 81	11	.03	.016	8	22	.36	74	.01	3	.61	.01	.10	11	1	
Y-82	21	.03	.029	8	20	.32	212	.03	7	.68	.01	.26	10		.001
Y-83	9	.05	.020	13	17	.10	111	.01	4	.31	.01	.11	14		.001
Y-84	38	.34	.042	9	30	.43	302	.07	9	1.12	.08	.34	12		.001
Y 85	75	.33	.081	16	44	1.05	739	.20	6	2.12	.04	1.13	4	1	
Y 86	102	1.32	.048	2	88	1.10	31	.27	7	1.78	.20	.06	1	1	
Y 87	157	1.31	.035	2	164	3.17	208	.19	9	3.06	.14	.70	1	15	
Y 88	170	1.17	.061	2	84	2.68	113	.11	4	2.49	.10	.56	2	60	
Y 89	62	.39	.038	2	47	1.03	41	.04	5	1.19	.05	.15	5	145	
Y 90	144	3.60	.040	2	146	2.96	122	.09	6	2.02	.12	.35	2	1030	
Y 91	216	.29	.087	2	233	1.49	22	.10	7	1.87	.06	.36	1	1250	
Y 92	99	.67	.037	2	102	1.21	25	.23	2	1.54	.13	.14	1	12	
Y 93	25	.09	.057	11	34	.20	74	.01	4	.44	.01	.09	5	90	
Y 94	56	.12	.052	12	34	.97	137	.05	3	1.13	.02	.27	5	8200	
Y 95	111	1.14	.055	5	21	1.41	75	.08	3	2.01	.15	.23	4	37	
Y 96	151	.61	.050	4	141	2.12	220	.16	5	2.51	.11	.66	1	12	
Y 97	113	.49	.064	8	140	2.17	145	.20	4	2.78	.11	.93	2	15	
Y 98	117	.77	.044	4	117	2.06	121	.23	4	2.28	.15	.44	2	45	
Y 99	128	1.50	.050	2	104	.92	38	.35	4	1.67	.20	.06	2	10	
Y 100	110	.84	.043	2	100	1.95	261	.31	6	2.10	.13	.45	3	23	
Y-101	137	.87	.043	2	135	2.24	266	.31	3	2.36	.20	.39	3		.001
Y 102	0119	1.50	.047	2	102	1.65	49	.31	3	2.35	.26	.12	1	4	
Y-103	115	1.23	.042	2	123	1.98	110	.35	2	2.09	.23	.26	6		.001
Y 104	81	1.19	.039	2	88	1.51	105	.26	5	1.89	.20	.36	2	1	
Y 105	174	.67	.047	2	152	2.23	89	.02	6	2.34	.05	.18	1	80	

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au** PPB	Au** OZ/T
Y 106	1	136	3	169	.3	32	33	1598	5.91	92	7	ND	1	35	1	2	2	152	1.78	.077	2	55	2.40	83	.35	6	2.46	.15	.29	1	1	
Y 107	4	61	3	40	.8	34	13	847	2.06	415	5	ND	2	9	1	7	3	30	.19	.038	9	34	.41	117	.01	5	.55	.01	.12	6	115	
Y 108	6	61	19	50	.5	20	10	405	3.20	27	5	ND	2	9	1	2	2	75	.31	.079	6	42	.49	77	.08	5	.75	.03	.11	7	60	
Y 109	1	35	12	32	.9	9	6	456	1.79	59	5	ND	1	6	1	2	2	10	.02	.019	8	16	.12	274	.01	6	.20	.01	.08	9	56	
Y-110	?	18	15	21	3.2	4	3	208	1.63	114	5	ND	2	6	1	5	4	8	.02	.010	10	15	.03	71	.01	3	.15	.01	.09	13		.003
Y 111	5	26	15	10	.2	3	3	140	.77	3	5	ND	1	3	1	2	2	14	.03	.014	8	14	.15	78	.03	2	.20	.01	.17	6	12	
Y-112	1	737	3	81	.8	80	21	1009	2.70	37	5	ND	1	118	1	2	2	85	3.10	.015	2	172	2.27	220	.14	12	2.50	.36	.19	1		.001
Y 113	1	105	2	68	.3	42	32	747	3.68	34	7	ND	1	17	1	2	2	105	3.15	.048	2	153	.77	300	.29	2	1.44	.16	.56	1	2	
Y-114	1	64	14	67	.1	60	18	1045	3.60	16	5	ND	1	36	1	2	2	76	.55	.060	7	93	1.50	812	.21	2	2.35	.17	1.12	7		.001
Y-115	3	40	10	341	2.1	9	18	202	2.99	13324	5	ND	2	7	7	7	23	31	.11	.058	6	21	.38	120	.01	2	.53	.01	.09	8		.029
Y-116	3	41	11	130	.5	15	5	157	2.46	1021	5	ND	2	5	2	2	3	39	.02	.019	6	32	.40	118	.01	4	.56	.01	.10	10		.004
Y-117	3	44	4	81	.7	15	4	169	1.85	62	6	ND	3	7	1	2	2	30	.04	.018	18	40	.75	310	.01	2	.52	.01	.20	10		.001
Y-118	2	78	11	99	.5	91	21	661	3.76	30	12	ND	2	117	1	2	2	119	3.60	.267	8	143	1.33	67	.43	8	2.09	.18	.98	9		001
Y-119	1	1008	2	115	1.8	82	22	889	2.21	71	11	ND	1	102	2	2	13?	49	3.15	.014	2	118	1.45	161	.11	8	1.92	.34	.11	1	220	
Y-120	5	99	26	155	2.6	41	12	683	6.04	251	5	ND	3	41	1	12	2	44	.15	.240	15	22	.09	407	.01	5	.60	.03	.25	1	490	
Y-121	10	13	21	15	1.2	18	6	302	2.68	122	5	ND	3	20	1	4	2	7	.38	.055	7	6	.02	29	.01	7	.14	.02	.13	1	765	
Y-122	1	113	11	43	.2	15	8	1984	4.53	2	5	ND	2	6	1	3	2	45	.07	.024	15	17	.72	110	.05	2	1.54	.02	.24	2	8	
Y-123	1	101	2	207	.2	61	23	1437	10.43	18	5	ND	6	12	1	2	2	108	.55	.262	50	15	1.21	248	.43	2	3.68	.07	2.69	1	3	
Y-124	3	104	13	33	.8	27	10	677	2.86	271	5	ND	2	7	1	7	2	30	.07	.031	8	17	.30	139	.01	5	.48	.02	.10	1	60	
Y-125	2	93	15	43	1.1	33	16	713	2.79	109	5	ND	2	8	1	8	2	26	.14	.061	12	14	.30	115	.01	4	.53	.01	.13	1	35	
Y-126	2	59	6	31	.5	38	8	845	2.52	205	5	ND	3	9	1	8	2	36	.17	.056	12	30	.37	150	.02	5	.63	.03	.20	1	115	
Y-127	1	71	18	46	.1	75	11	715	1.58	65	5	ND	1	8	1	2	4	14	.13	.044	11	10	.75	235	.01	2	.41	.01	.10	1	50	
Y-128	1	100	164	103	10.4	6	13	944	3.01	909	5	4	3	10	2	5	4	32	.20	.067	14	7	.44	104	.01	3	.90	.03	.19	1	5620	
Y-129	2	119	1319	153	8.0	8	14	817	3.94	1920	5	3	2	9	2	7	2	13	.18	.058	13	5	.15	118	.01	2	.64	.02	.20	1	3830	
Y-130	1	78	13	47	.7	6	12	467	2.91	290	5	ND	3	9	1	2	5	42	.20	.059	12	10	.73	82	.01	3	1.29	.03	.14	1	445	
Y-131	1	68	4	49	.1	6	11	502	3.19	65	5	ND	2	17	1	2	4	69	.27	.066	8	12	1.00	186	.02	2	1.47	.06	.10	2	60	
Y-132	19	50	54	53	1.8	10	12	275	8.93	894	5	ND	2	33	1	10	5	23	.56	.309	21	2	.27	23	.06	5	.93	.01	.57	4	4100	
Y-133	4	40	12	38	.3	12	5	200	2.79	75	5	ND	1	5	1	3	2	22	.07	.053	15	20	.27	95	.09	4	.73	.01	.26	2	33?	
Y-134	62	44	140	176	2.0	14	8	204	4.75	249	5	ND	2	15	1	6	2	15	.03	.064	10	11	.09	214	.01	5	.42	.01	.21	1	1860	
Y-135	1	106	902	291	8.3	4	10	406	3.01	837	5	4	3	24	2	9	2	20	.10	.053	8	7	.27	145	.01	3	.66	.03	.20	1	4630	
Y-136	1	45	38	55	3.8	10	7	473	1.64	141	5	ND	2	14	1	3	2	4	.02	.029	8	4	.02	74	.01	3	.16	.01	.09	1	360	
Y-137	6	195	29	304	1.7	83	36	3036	8.17	127	5	ND	1	55	3	3	3	28	.06	.154	9	18	.04	268	.01	5	.40	.01	.15	1	225	
Y-138	1	85	28	83	1.6	20	11	785	5.18	164	5	ND	2	41	1	4	2	34	.20	.242	13	22	.03	332	.01	4	.32	.01	.11	1	65	
Y-139	2	67	14	106	.8	37	12	1230	3.42	59	5	ND	1	12	1	2	2	83	.20	.069	12	45	.74	615	.06	2	1.20	.02	.33	1	15	
Y-140	1	31	19	5	.4	3	1	65	.92	74	5	ND	1	8	1	4	2	6	.01	.025	6	8	.02	85	.01	4	.17	.01	.08	1	24	
Y-141	3	130	131	28	2.0	9	3	316	3.40	323	5	ND	3	22	1	11	2	21	.08	.113	13	10	.06	171	.01	5	.38	.01	.12	1	75	
Y-142	2	60	32	11	2.0	5	1	105	1.41	131	5	ND	1	10	1	6	2	6	.01	.033	6	6	.02	211	.01	4	.20	.01	.07	1	260	
Y-143	[illegible]	60	14	87	.4	26	12	1147	3.86	28.	5	ND	6	62	1	[illegible]	2	53	.64	.144	23	21	.94	430	.19	6	2.75	.16	.80	1	14	
Y-144	3	41	9	64	.7	21	5	377	2.55	48	5	ND	5	21	1	2	2	30	.22	.079	18	22	.50	323	.08	4	1.01	.03	.42	1	34	
Y-145	1	45	7	107	.3	52	25	1620	5.72	7	5	ND	2	67	1	3	2	167	1.34	.094	14	43	2.65	316	.02	2	3.13	.18	.12	1	1	
Y 146	1	69	14	132	.7	36	12	611	4.06	72	5	ND	3	20	1	3	3	43	.26	.117	17	17	.71	279	.05	4	1.47	.04	.27	1	55	
Y 147	4	98	10	200	.1	73	21	995	4.08	15	5	ND	1	42	1	2	2	119	.76	.095	12	32	1.91	201	.18	3	2.96	.12	.08	1	5	
Y 148	1	72	13	117	.7	37	12	834	3.90	159	5	ND	6	16	1	3	4	44	.14	.084	20	34	.71	442	.06	3	1.47	.01	.36	1	120	
Y 149	1	57	27	81	.5	32	12	782	3.25	63	5	ND	7	11	1	2	4	27	.12	.058	20	26	.55	253	.09	5	1.20	.01	.40	1	43	
Y-150	1	62	10	100	1.0	43	19	1096	4.37	69	5	ND	1	19	2	2	3	120	.62	.057	5	70	1.56	461	.25	2	1.97	.07	.42	1	35	
Y-151	1	41	8	54	.2	30	8	943	1.88	194	5	ND	2	9	1	9	2	18	.21	.038	9	19	.30	191	.01	5	.48	.02	.13	1	185	
Y-152	1	43	10	75	.5	11	19	2109	5.38	526	5	ND	2	70	1	2	2	124	2.69	.100	12	32	1.97	100	.03	4	1.74	.08	.22	1	55	
Y-153	1	50	13	134	.9	54	14	1142	2.56	182	5	ND	2	14	1	3	3	24	.21	.071	16	28	.08	260	.02	5	.80	.02	.17	1	75	
Y-154	1	139	5	45	.2	50	29	608	4.02	41	9	ND	1	33	1	2	2	134	2.26	.042	2	125	2.46	90	.32	2	2.78	.23	.31	2	235	
Y-155	1	59	2	57	.1	72	30	769	4.04	52	5	ND	1	27	1	2	4	137	1.14	.034	3	163	3.25	90	.30	2	2.72	.13	.38	1	15	
Y-156	1	104	8	70	.2	60	29	608	5.39	85	7	ND	1	29	1	2	4	150	1.10	.053	4	139	2.09	262	.34	2	2.68	.15	.52	1	34	
Y-157	2	96	9	85	.4	87	20	762	5.75	277	5	ND	1	37	1	2	4	149	.78	.173	19	139	2.46	456	.18	2	2.99	.08	.84	1	363	
Y-158	4	62	8	110	.5	50	16	1001	3.77	120	5	ND	3	11	1	3	3	54	.18	.070	17	57	.93	216	.04	5	1.27	.01	.36	1	39	
Y-159	7	60	9	165	.9	32	10	771	2.07	34	5	ND	2	9	1	4	2	54	.12	.071	15	19	.09	127	.01	3	.55	.01	.16	1	21	
Y-160	2	271	4	49	.3	69	43	656	5.99	132	8	ND	1	23	1	2	7	112	1.12	.112	7	113	2.76	173	.05	2	2.76	.15	1.16	2	50	

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	
Y-161	1	95	13	63	.2	82	36	769	5.52	50	6	ND	1	19	1	2	6	112	.96	.047	6	152	3.31	155	.45	5	2.05	.12	.89	1	25	
Y-162	1	129	15	46	.3	56	31	815	4.77	66	5	ND	1	22	1	2	6	132	1.13	.051	5	140	2.23	549	.42	2	2.19	.14	.59	2	34	
Y-163	1	243	7	35	.1	49	37	707	5.16	57	5	ND	1	31	1	2	2	143	1.51	.048	3	80	1.92	57	.20	2	2.56	.25	.10	1	31	
Y 164	1	105	7	46	.1	57	30	691	4.94	44	5	ND	1	27	1	2	2	119	1.17	.043	2	97	2.05	73	.20	2	2.20	.12	.54	1	17	
Y 165	2	68	13	86	.1	39	14	904	3.47	18	5	ND	9	8	1	2	4	37	.09	.046	24	31	.87	364	.13	2	1.93	.02	.61	1	3	
Y 166	1	43	14	79	.4	30	10	540	4.12	47	5	ND	7	16	1	4	2	31	.15	.062	24	20	.53	439	.07	4	1.22	.03	.45	1	17	
Y 167	1	33	29	99	.7	23	6	209	2.78	49	5	ND	5	11	1	2	2	23	.09	.066	16	16	.22	179	.01	3	.63	.01	.18	1	27	
Y 168	1	69	27	68	.2	20	10	942	2.49	17	5	ND	4	13	1	2	3	22	.09	.059	21	15	.36	240	.03	2	.87	.01	.23	1	3	
Y 169	1	47	21	90	.3	35	16	1130	3.33	30	5	ND	9	11	1	2	2	29	.12	.057	27	20	.60	214	.10	5	1.54	.02	.60	1	35	
Y 170	1	44	10	59	.1	29	9	443	2.43	28	5	ND	2	28	1	2	2	38	.39	.036	9	24	.68	295	.08	2	1.25	.08	.28	1	9	
Y 171	1	34	29	100	1.3	27	5	213	3.00	33	5	ND	3	8	1	4	2	18	.04	.035	15	15	.16	407	.01	5	.60	.01	.20	1	50	
Y 172	1	66	26	121	1.6	33	9	232	5.27	79	5	ND	2	17	1	3	3	65	.18	.143	14	61	.51	456	.07	4	1.27	.01	.47	1	80	
Y 173	4	43	12	55	.1	19	6	431	3.24	6	5	ND	5	18	1	2	3	46	.18	.085	23	35	.94	650	.12	3	2.08	.05	.71	1	4	
Y 174	1	45	3	71	.1	30	14	962	3.30	7	5	ND	6	11	1	2	2	48	.10	.052	18	26	.82	585	.13	4	1.60	.02	.57	1	3	
Y 175	3	49	16	103	.3	30	12	528	4.31	2	5	ND	1	16	1	2	2	117	.30	.148	11	54	1.78	550	.13	2	2.54	.03	.56	1	4	
Y 176	3	61	6	102	.3	37	14	940	4.45	11	5	ND	2	22	1	2	2	93	.34	.113	12	42	1.64	950	.21	2	2.66	.06	.64	1	13	
Y 177	1	73	11	59	.5	15	7	214	2.32	27	5	ND	2	9	1	2	2	32	.04	.032	10	31	.36	451	.01	3	.68	.01	.13	1	14	
Y 178	1	50	4	59	.3	16	6	244	1.91	10	5	ND	3	10	1	2	2	35	.06	.027	9	27	.47	579	.03	3	.91	.01	.20	1	5	
Y 179	2	54	11	51	.2	24	10	381	2.17	14	5	ND	2	15	1	2	2	44	.31	.055	10	44	.72	676	.09	6	1.06	.04	.22	1	35	
Y 181	3	50	7	107	.2	45	9	1139	3.44	17	5	ND	4	15	1	2	2	49	.16	.049	23	28	.81	684	.10	3	1.65	.01	.36	1	6	
Y 182	4	45	11	139	.3	44	13	1108	3.28	13	5	ND	1	45	1	2	2	128	.77	.155	15	51	1.16	604	.13	2	1.79	.08	.17	1	13	
Y 183	2	45	5	70	.1	51	12	1113	3.52	27	5	ND	4	21	1	2	2	60	.31	.064	19	74	1.52	489	.15	4	2.06	.08	.63	1	6	
Y-184	1	43	6	38	.2	22	7	454	2.25	27	5	ND	3	15	1	2	2	49	.34	.033	8	36	.66	280	.10	2	1.16	.08	.25	1	15	
Y-185	1	109	2	44	.2	29	16	932	2.16	42	7	ND	1	12	1	2	2	46	.18	.031	7	21	1.05	1590	.05	2	1.11	.03	.31	1	12	
Y-186	1	150	8	61	.3	61	31	910	4.35	104	5	ND	1	22	1	2	2	84	1.04	.048	2	98	1.76	161	.27	5	2.33	.19	.77	1	11	
Y-187	1	9	11	55	.3	5	8	848	3.38	157	9	ND	3	28	1	2	2	43	.90	.097	13	3	1.02	114	.04	4	1.49	.05	.08	1	6	
Y-188	1	120	2	50	.2	70	25	742	4.25	160	6	ND	1	19	1	2	2	68	.59	.082	6	74	1.62	170	.23	3	2.30	.14	.87	1	15	
Y-189	1	7	8	48	.1	8	8	809	3.04	19	5	ND	4	33	1	2	2	45	1.24	.098	24	4	.83	73	.01	2	1.06	.04	.13	1	1	
Y-190	1	110	4	50	.1	67	27	714	4.74	39	5	ND	1	19	1	2	2	133	1.10	.038	2	166	3.04	148	.46	2	2.68	.16	.14	1	4	
Y-191	2	938	14	38	.4	63	81	497	10.23	54	9	ND	1	15	1	2	9	54	.71	.087	6	54	1.62	15	.30	6	2.07	.09	.15	35	190	-
Y-192	1	19	16	73	.1	16	9	961	3.41	26	5	ND	4	37	1	2	4	46	1.20	.100	22	5	.93	89	.01	4	1.30	.04	.15	1	39	-
Y-193	3	92	273	50	2.2	22	12	553	2.33	2145	5	ND	2	6	2	2	3	11	.15	.039	9	11	.13	49	.01	8	.28	.01	.09	1	650	-
Y-194	2	256	39	54	13.1	18	26	82	3.81	14771	5	57	1	6	2	5	40	4	.08	.012	3	15	.04	26	.01	2	.09	.01	.04	1	27500	.895
Y-195	1	82	5	35	.1	60	21	577	3.42	321	5	ND	2	12	1	2	2	66	.19	.052	12	44	1.11	316	.10	5	1.62	.04	.60	1	6	
Y-196	1	46	4	41	.2	36	15	735	3.04	502	5	ND	2	8	1	2	2	46	.14	.038	12	22	1.04	218	.06	5	1.47	.03	.44	1	8	
Y-197	113	17	93	10	1.9	11	6	905	2.11	285	5	ND	2	7	1	6	2	5	.04	.021	7	3	.06	87	.01	3	.20	.01	.10	1	890	
Y-198	1	77	19	84	.7	37	31	633	6.30	7495	5	ND	2	23	1	12	2	70	.27	.138	10	60	1.14	140	.01	9	1.99	.01	.28	1	320	
Y-199	3	82	2	38	.1	14	14	504	4.22	63	5	ND	3	49	1	2	2	122	.74	.073	7	25	1.39	265	.11	2	2.38	.18	.40	1	14	
Y-200	1	93	3	21	.2	14	13	393	2.25	364	5	ND	2	5	1	2	3	19	.05	.034	9	12	.27	39	.01	2	.48	.01	.06	1	136	
Y-201	1	65	5	12	.2	7	6	172	2.11	158	5	ND	2	5	1	2	2	29	.06	.037	8	24	.54	74	.01	4	.71	.02	.08	1	150	
Y-202	3	45	2	17	.1	7	5	194	2.19	418	5	ND	3	5	1	2	2	37	.04	.030	10	27	.62	71	.01	2	.73	.01	.13	1	15	
Y-203	1	97	7	5	.6	7	15	115	1.76	8033	5	ND	1	4	1	2	4	11	.14	.002	2	11	.16	32	.01	2	.14	.01	.01	1	960	
Y-204	2	77	8	27	.2	33	11	453	2.35	194	5	ND	2	8	1	2	3	43	.13	.042	7	39	.66	186	.05	4	.84	.03	.31	1	101	
Y-205	19	323	16	273	.4	22	39	2736	36.53	18	29	ND	2	2	4	2	2	1	2.10	.033	66	5	.07	2	.01	2	.11	.01	.01	1	12	
Y-206	4	107	9	24	.2	28	14	323	3.13	372	5	ND	4	18	1	2	2	80	.30	.076	8	38	1.04	188	.03	5	1.40	.06	.23	1	820	
Y-207	4	89	10	29	.2	26	14	361	3.13	302	5	ND	3	31	1	2	2	93	.64	.075	10	37	1.01	176	.05	2	1.57	.09	.28	1	64	
Y-208	2	51	25	47	.9	33	10	886	2.28	123	6	ND	1	8	1	2	2	23	.12	.032	6	18	.38	171	.02	5	.61	.02	.13	1	80	-
Y-209	3	103	16	54	2.5	32	23	1092	4.19	299	5	ND	3	77	1	3	2	36	3.66	.059	4	18	1.44	50	.01	6	.38	.01	.19	1	100	
Y-209A	1	10	6	10	.9	10	2	353	.83	215	5	5	1	2	1	3	3	11	.04	.006	2	7	.40	16	.01	2	.33	.01	.01	1	11500	.391
Y-210	1	21	33	118	.1	40	11	972	3.50	41	5	ND	2	36	1	2	2	48	1.23	.148	18	42	1.66	327	.14	3	1.95	.06	.62	1	10	-
Y-211	2	175	4	46	.2	83	31	569	6.15	45	5	ND	1	26	1	2	2	90	.75	.078	2	101	2.07	97	.36	4	2.70	.14	.99	1	30	-

APPENDIX E

NO. 3 TUNNEL ASSAYS

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YT-2 1	1	48	5	24	.2	16	7	436	1.81	531	5	ND	2	2	1	2	2	14	.04	.024	9	22	.34	46	.01	3	.52	.01	.08	1	100
YT-2 2	4	54	2	23	.2	20	8	326	2.25	253	5	ND	2	2	1	2	5	24	.07	.041	10	33	.51	56	.01	3	.69	.01	.09	1	70
YT-2 3	2	49	2	21	.2	16	7	246	1.84	1128	5	ND	2	5	1	2	24	25	.13	.035	7	46	.56	63	.01	2	.64	.01	.09	1	185
YT-2 4	2	38	3	43	.3	9	8	511	2.40	499	5	ND	2	22	1	2	7	32	.85	.063	9	21	.67	66	.01	5	.93	.02	.10	1	135
YT-2 5	2	65	2	27	.2	20	9	376	2.13	2107	5	ND	2	24	1	2	3	24	.71	.049	6	28	.70	38	.01	2	.77	.01	.08	1	135
YT-2 6	7	74	2	17	.1	22	10	476	2.07	614	5	ND	2	25	1	2	3	25	1.08	.037	7	27	.66	46	.01	3	.52	.01	.07	1	70
YT-2 7	2	78	44	51	1.0	24	10	429	2.11	551	5	2	2	35	1	2	5	22	.97	.037	5	23	.73	30	.01	3	.54	.01	.08	1	3430
YT-2 8	1	147	4	21	.2	18	15	428	2.60	595	5	ND	1	38	1	2	2	46	1.34	.051	5	20	.88	105	.02	2	.95	.06	.16	1	675
YT-2 9	5	232	1588	4878	12.3	29	30	1708	6.67	2515	5	2	2	145	58	14	3	74	4.34	.058	2	62	2.34	20	.01	4	1.07	.03	.20	1	3630
YT-2 10	1	89	18	69	.8	27	22	1111	4.76	749	5	ND	2	120	1	2	3	118	4.17	.064	2	80	2.54	107	.06	2	1.90	.10	.31	1	150
YT-2 11	2	168	92	281	3.2	36	24	1550	4.69	3842	5	ND	2	177	4	9	2	74	4.89	.058	3	68	2.93	54	.01	3	1.16	.02	.17	1	2980
YT-2 12	2	105	32	80	1.1	27	23	1140	4.74	1112	5	ND	3	150	1	2	6	107	4.67	.063	4	76	2.64	74	.04	5	1.67	.08	.21	1	355
YT-2 13	2	58	6	72	1.1	11	17	969	4.48	57	5	7	2	96	1	2	35	100	3.54	.090	7	54	2.02	199	.03	2	2.06	.06	.19	1	14300
YT-2 14	2	115	9	66	.6	28	23	982	4.65	309	5	ND	2	114	1	2	4	149	4.00	.053	3	103	2.72	121	.09	4	2.19	.14	.33	1	275
YT-2 15	2	103	328	437	2.1	23	18	1432	4.25	3511	5	ND	2	125	5	6	2	64	3.57	.055	3	50	2.17	49	.01	4	1.04	.02	.15	1	385
YT-2 16	2	138	556	882	4.9	19	22	1706	4.89	6721	5	ND	2	145	11	8	3	53	4.27	.054	3	32	2.05	31	.01	4	.88	.03	.20	1	1350
YT-2 17	2	108	10	47	1.0	23	19	988	4.16	1660	6	ND	2	170	1	2	2	75	4.58	.049	4	52	2.51	56	.01	3	1.08	.03	.16	2	405
YT-2 18	5	100	13	27	.7	19	11	641	2.46	838	5	ND	2	78	1	2	5	15	2.30	.036	6	9	.76	45	.01	5	.34	.01	.10	1	325
YT-2 19	2	108	39	64	1.8	21	14	461	2.97	1679	5	3	2	41	1	2	6	21	1.01	.042	5	11	.48	59	.01	4	.53	.01	.13	1	515
YT-2 20	3	55	167	368	3.4	24	12	690	5.79	1322	5	ND	1	73	4	18	2	11	.34	.040	2	7	.16	51	.01	6	.31	.01	.11	1	625
YT-2 21	2	46	147	150	2.2	15	10	901	3.00	1483	5	ND	1	69	2	7	2	8	1.65	.033	4	7	.54	50	.01	3	.25	.01	.14	1	470
YT-2 22	2	126	146	299	4.6	27	20	1701	3.58	1648	7	ND	2	237	4	4	4	23	4.91	.049	3	16	2.02	44	.01	2	.43	.01	.20	1	970
STD C/AU-0.5	21	60	42	137	7.1	70	30	1105	3.93	40	22	8	32	47	17	16	22	62	.48	.109	34	60	.88	176	.08	37	1.73	.06	.13	13	515

APPENDIX F

NO. 4 TUNNEL ASSAYS

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YT 1	1	58	17	55	.2	40	13	1448	2.45	527	5	ND	1	7	1	2	3	32	.14	.037	11	17	.54	224	.02	4	.81	.02	.14	1	13
YT 2	1	63	13	54	.1	52	16	1166	2.85	272	5	ND	1	8	1	2	2	42	.16	.036	12	24	.87	197	.04	9	1.21	.03	.24	1	8
YT 3	2	77	8	73	.1	59	33	1471	6.69	263	5	ND	1	24	1	2	2	160	1.09	.039	8	197	3.54	278	.23	3	2.93	.09	.68	1	25
YT 4	1	99	3	47	.1	43	28	806	4.61	66	5	ND	1	25	1	3	2	115	1.77	.035	5	137	2.55	330	.27	3	2.23	.11	.56	64	145
YT 5	1	387	10	56	.4	43	44	814	4.66	46	5	ND	1	48	1	2	2	127	2.73	.039	7	152	2.45	411	.27	2	2.32	.16	.58	1	22
YT 6	1	168	4	48	.1	51	38	706	4.87	38	5	2	1	39	1	2	2	94	3.85	.027	5	130	2.41	92	.20	2	2.47	.16	.41	2	915
YT 7	2	208	11	68	.3	71	52	1011	7.44	53	5	3	2	74	1	3	8	135	5.45	.026	7	182	3.79	42	.06	2	3.00	.03	.18	1	3660
YT 8	2	78	5	78	.1	40	26	1349	6.08	23	5	ND	2	82	1	2	2	159	6.51	.034	7	181	3.46	57	.09	2	2.93	.05	.29	1	28
YT 9	2	172	8	56	.1	56	32	985	6.03	32	5	ND	2	56	1	2	6	126	4.36	.039	7	150	3.03	61	.22	2	2.77	.15	.57	1	695
YT 10	2	82	11	57	.7	51	27	1241	5.01	807	5	ND	2	74	1	2	2	125	4.01	.039	5	141	3.27	120	.14	7	2.44	.08	.52	1	65
YT 11	1	111	7	61	3.3	61	35	1500	6.03	1541	5	ND	2	88	1	5	3	115	4.90	.039	4	143	3.49	99	.16	2	2.50	.09	.57	1	120
YT 12	1	204	17	65	.1	81	45	893	6.98	97	5	ND	1	44	1	2	3	159	3.32	.040	4	181	3.26	41	.22	3	2.84	.11	.39	1	60
YT 13	1	162	3	38	.1	54	33	862	4.75	1046	5	ND	2	52	1	2	2	94	4.76	.035	2	116	1.92	49	.17	2	2.00	.14	.25	1	495
YT 14	2	141	6	53	.3	71	31	770	5.27	149	5	ND	1	46	1	2	2	129	3.48	.046	3	135	2.49	49	.22	4	2.39	.15	.32	1	30
YT 15	5	212	1353	2557	9.1	62	37	2456	7.18	9119	11	ND	3	171	29	42	2	105	6.65	.034	2	111	3.33	22	.02	3	1.86	.04	.16	1	870
YT 16	2	122	7	39	.1	54	31	753	4.92	48	5	ND	1	46	1	3	2	92	3.42	.033	3	121	2.50	80	.23	4	2.70	.22	.48	1	27
YT 17	1	31	12	23	.1	6	6	323	1.24	187	5	ND	1	20	1	2	2	21	3.09	.005	4	22	.64	6	.01	2	.47	.01	.01	7	270
YT 18	2	139	9	44	.1	56	32	677	5.16	50	5	ND	1	30	1	2	2	90	3.01	.034	2	119	2.77	52	.21	2	2.59	.14	.37	2	60
YT 19	1	63	8	35	.6	39	23	585	3.40	50	7	ND	1	36	1	2	2	81	3.66	.047	3	71	1.60	15	.21	5	1.97	.23	.06	3	10
YT 20	2	115	7	33	.1	38	25	559	4.16	32	5	ND	1	29	1	2	10	90	2.49	.041	3	85	1.81	31	.20	3	1.98	.17	.15	1	3150
YT 21	2	161	2	52	.1	45	32	609	5.17	47	5	ND	1	26	1	2	2	88	2.45	.036	2	112	2.52	58	.20	2	2.45	.15	.33	1	29
YT 22	1	240	4	57	.2	48	35	572	3.65	122	5	ND	1	31	1	2	2	78	3.40	.038	3	95	1.71	36	.19	2	1.85	.18	.19	1	70
YT 23	2	218	14	73	.4	57	36	863	5.17	627	5	ND	2	34	1	2	2	98	4.04	.035	2	130	3.05	56	.13	2	2.67	.11	.23	1	100
YT 24	2	206	10	52	.1	46	31	655	4.66	89	5	ND	1	33	1	2	2	101	3.02	.039	2	126	2.28	86	.22	2	2.31	.17	.40	2	18
YT 25	2	113	9	49	.1	47	29	665	4.84	590	5	ND	1	36	1	3	2	101	2.88	.038	2	124	2.78	107	.20	2	2.78	.18	.81	1	80
YT 26	2	111	6	86	.3	55	28	661	5.36	37	5	ND	1	21	1	2	2	90	2.60	.028	2	143	3.64	31	.24	2	3.04	.13	.23	1	5
YT 28	2	76	2	53	.1	42	24	650	3.91	39	5	ND	1	28	1	2	2	90	3.01	.033	2	117	2.27	21	.22	2	2.23	.19	.13	1	6
YT 29	2	252	5	52	.6	46	37	692	5.28	7217	5	ND	1	30	1	2	2	93	3.23	.034	2	133	2.46	35	.12	2	2.34	.16	.23	1	800
YT 30	2	191	10	57	.3	43	28	741	4.56	39	5	ND	2	40	1	2	2	107	4.11	.034	2	134	2.49	43	.21	5	2.20	.12	.23	1	22
YT 31	2	105	10	49	.2	41	27	760	4.82	1233	5	ND	1	33	1	2	2	98	3.07	.040	2	118	2.59	20	.12	3	2.41	.12	.11	1	15
YT 32	3	118	15	64	.2	54	32	1609	6.34	1023	7	ND	3	60	1	2	5	147	7.58	.046	2	177	3.69	33	.09	2	3.08	.08	.14	1	27
YT 33	3	255	2	55	.2	68	48	751	6.32	114	5	ND	1	26	1	2	3	101	2.75	.030	2	137	3.23	94	.22	2	2.84	.11	.71	1	60
YT 34	1	107	7	34	.1	45	30	513	3.79	43	5	ND	1	28	1	2	2	82	2.65	.043	4	99	1.68	33	.21	2	1.88	.19	.13	2	11

APPENDIX F

NO. 4 TUNNEL ASSAYS

(continued)

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YT 35	2	205	4	54	.3	58	38	848	6.13	696	5	ND	1	33	1	2	5	114	3.18	.040	2	142	2.86	69	.17	3	2.61	.11	.38	1	42
YT 36	2	217	4	49	.2	55	42	641	4.53	58	5	ND	1	27	1	2	2	85	3.33	.042	3	105	2.17	30	.21	2	2.06	.17	.12	1	12
YT 37	1	362	13	29	.1	48	46	511	4.88	41	5	ND	1	33	1	2	2	85	3.79	.044	4	94	1.24	31	.23	2	1.67	.19	.14	1	10
YT 38	2	664	3	49	.5	60	75	963	9.31	460	5	ND	2	38	1	2	51	126	4.90	.033	3	146	2.08	13	.09	2	1.90	.05	.04	1	580
YT 39	1	184	2	43	.1	56	39	663	5.72	60	5	ND	1	47	1	2	2	125	3.31	.045	4	121	2.81	107	.24	5	3.15	.18	.64	1	9
YT 40	2	180	10	48	.3	55	39	686	5.77	186	5	ND	1	38	1	2	4	121	2.45	.043	3	128	2.85	92	.19	3	3.10	.20	.86	1	44
YT 41	2	99	39	67	.6	43	28	1095	7.53	31811	5	ND	1	42	1	3	4	154	3.01	.040	5	189	3.44	9	.02	2	2.89	.02	.03	1	1650
YT 42	2	225	9	31	.1	52	39	501	4.91	2	5	ND	1	30	1	2	5	71	2.27	.037	5	88	2.00	48	.18	2	2.27	.19	.35	1	9
YT 43	1	195	11	34	.1	51	37	567	4.98	72	5	ND	1	34	1	2	2	78	2.71	.040	3	105	2.16	44	.21	2	2.32	.19	.29	1	8
YT 44	1	162	2	34	.1	50	32	652	4.64	41	5	ND	1	36	1	2	2	90	2.87	.041	4	102	1.90	38	.22	2	1.98	.16	.15	2	10
YT 45	2	208	14	37	.1	64	35	664	5.08	44	5	ND	1	40	1	2	2	91	2.48	.036	4	101	2.12	89	.21	2	2.09	.13	.28	2	6
YT 46	6	693	22	49	.7	51	75	1041	10.95	236	5	ND	2	50	1	3	134	80	3.42	.048	11	75	1.61	25	.05	4	1.90	.05	.08	1	115
YT 47	2	661	5	42	.2	45	26	560	4.59	45	5	ND	1	37	1	2	2	91	1.60	.035	5	75	2.32	99	.27	5	2.39	.19	.68	1	28
YT 48	3	162	2	33	.1	45	32	622	4.50	35	5	ND	1	23	1	2	5	78	1.86	.037	4	85	1.77	36	.21	5	1.72	.13	.15	1	8
YT 49	4	181	7	32	.1	45	31	628	4.81	31	5	ND	1	20	1	2	2	90	1.79	.038	5	107	1.88	45	.24	4	1.69	.09	.14	1	10
YT 50	4	51	5	20	.1	22	12	481	2.60	12	5	ND	1	22	1	2	124	58	1.62	.016	2	67	1.24	69	.14	2	1.22	.08	.17	1	60
YT 51	2	205	11	46	.1	50	35	789	5.14	28	5	ND	1	39	1	2	7	115	2.37	.035	4	120	2.32	88	.28	4	2.10	.15	.17	1	7
YT 52	2	133	3	33	.1	47	29	608	4.15	35	5	ND	1	40	1	2	5	92	1.82	.036	2	93	1.72	90	.27	2	1.90	.18	.38	3	7
YT 53	3	263	10	57	.4	52	47.	1117	6.04	2027	5	ND	2	68	1	2	14	125	4.91	.034	3	123	2.70	47	.10	2	2.24	.07	.15	2	295
YT 54	12	212	8	44	.3	46	33	591	4.68	23	5	ND	1	27	1	2	5	105	1.48	.036	3	73	2.01	100	.22	3	2.10	.13	.57	3	22
YT 55	3	194	2	38	.3	41	31	794	4.36	61	5	ND	1	40	1	2	2	107	2.20	.031	3	88	1.97	95	.27	2	2.12	.15	.24	2	170
YT 56	1	27	6	53	.3	14	12	866	3.70	38	5	ND	3	65	1	2	2	71	3.02	.085	12	28	1.40	95	.07	2	1.57	.07	.15	1	9
YT 57	2	161	11	43	.5	37	28	1004	4.77	848	5	ND	1	82	1	2	6	121	4.68	.036	2	117	2.35	102	.18	4	2.33	.16	.26	5	3700
YT 58	2	242	6	62	.6	63	42	1144	5.67	2291	5	ND	2	86	1	2	19	105	3.31	.050	2	102	2.47	54	.13	2	2.23	.04	.63	2	335
YT 59	1	65	6	48	.3	37	16	953	2.89	1198	5	ND	2	19	1	2	3	53	1.48	.041	7	28	1.39	71	.04	2	1.35	.03	.20	1	1100
YT 60	1	81	8	54	.3	43	17	1087	3.74	2435	5	ND	2	17	1	2	4	57	.79	.046	7	36	1.35	46	.02	6	1.35	.03	.17	1	375
YT 61	1	76	2	38	.2	53	17	591	3.24	655	5	ND	2	12	1	2	2	62	.56	.048	6	38	1.19	73	.05	3	1.20	.04	.31	2	1130

APPENDIX H

ELECTRONIC DISTANCE MEASURING (EDM) SURVEY
SURVEY POINT DESCRIPTIONS

Chap.
1. Spike one foot east of L.C.P. of Old Diggings M.C.
2. Top of Old Angle Iron at N.W. corner Lot 1912 (Black Pine).
3. Top of Old Angle Iron at N.E. corner L1912.
4. 15 feet S.E. of S.E. end of IP Trench, L0+25E.
5. 10 feet N.W. of N.W. end of IP Trench, L0+25E.
6. 10 feet N.W. of N.W. end of Trench #2.
7. Point on line - East Boundary L1912.
8. Point on line - North Boundary L1913.
9. Point on line - North Boundary L1913
10. Top of old angle iron at N.E. corner Lot 1913 (Bush Rat).
11. 2 metres N.W. of N.W. end of Bush Rat Shear Trench 4.
12. S.E. end of Bush Rat Shear Trench 4.
13. Point on Line - East Boundary L1912.
14. Trig Point on cliff on south side of valley.
15. IP 2, L450S 620E.
16. Upper Y53 Trench.
17. 2.2 m bearing 23° from top of Y53 pit.
18. East end of lower Y53 Trench.
19. West end of lower Y53 Trench.
20. 4.2 m bearing 350° from Adit 4 portal.
21. Dyke to east of Adit 4.
22. East end of hand trench to east of Adit 4.
23. West end of hand trench to east of Adit 4.
24. Quartz vein in 1985 cross trench.
25. East side of dyke at west end of Y87 trench.
26. Dyke rubble at east end of Y87 trench.
27. LY450S 650E.
28. South end of 1985 backhoe trench.
29. 1985 backhoe trenches, intersection of cross trench and LY450S trench.
30. Y79 locale.
31. Y97 locale.
32. Dyke at east end of a 1985 backhoe trench.
33. Dyke to west of Adit 3.
34. Dyke at IP2 L475S 700E.
35. Same dyke, at lower elevation.
36. LY 500S 683E.
37. Dyke to west of Adit 3.
38. 1.6 m bearing 298° to same dyke.
39. IP 2 L475S 720E.
40. 4.4 m bearing 166° from portal of Adit 3.
41. LY 450S 725E.
42. 7 m bearing 171°
43. Pit above Adit 2
44. West end of old Trench to east of Adit 2 pit.
45. Northeast corner of cleaned out pit.
46. South end of pit at Y94.
47. West end of old trench south of LY 350S 700E.

48. East end of old trench south of LY 350S 700E.
49. Northeast corner of Y163 trench.
50. Y102 trench.
51. East end of old trench.
52. Main cat road, 3 m east of centre.
53. Main cat road, 3 m east of centre.
54. Main cat road, 3 m from centre.
55. Main cat road, 5 m north of centre.
56. Main cat road, centre.
57. Main cat road, 5 m from centre.
58. Main cat road, 2.5 m south of centre.
59. Main cat road, 3 m south of centre.
60. Cat road to DDH Y86-6, 2 m north of centre.
61. Cat road to DDH Y86-6, 2.5 m north of centre.
62. Cat road to DDH Y86-6, 2.5 m north of centre.
63. 3 m upslope of Adit I portal.
64. East side of Bush Rat Shear trench 1.
65. Bush Rat Pit.
66. Bush Rat trench road.
67. Bush Rat Shear trench 2, on shear.
68. Bush Rat trench road.
69. Bush Rat trench road.
70. East end of abandoned Bush Rat Shear trench.
71. South end of Bush Rat Shear trench 3.
72. Bush Rat Shear trench 3, on shear.
73. West end of Bush Rat Shear trench 3.
74. Intermediate sight near CL2E.
75. DDH Y86-2.
76. DDH Y86-4.
77. Point on line - east boundary L1912.
78. South side of main cat road at point of intersection (P.I.) of road centrelines.
79. North side of main cat road at P.I. of road centrelines.
80. North side of main cat road (approximate north boundary L1912).
81. South side of main cat road at P.I. of road centrelines.
82. Main cat road, 6 m west of centre.
83. Main cat road, northwest side.
84. Main cat road, 2.6 m north of centre.
85. Main cat road, at P.I. of road centrelines.
86. Main cat road, south side.
87. Main cat road, at P.I. of road centre lines.
88. Main cat road, 2.7 m north of centre.
89. 4.1 m from west end of cleaned out trench.
90. East end of trench 2.6 m bearing 330° from LY 450S 850E.
91. Eastern trench to north of LY 450S 825E, east side.
92. Western trench to north of LY 450S 825E, west side.
93. LY 450S 825E.
94. West end of trench to south of LY 450S 825E.
95. IP2 475S 830E.
96. IP1 L0+00 0+90SE.
97. IP1 L0+25E 1+20SE.

98. 1 m bearing 295° from LY450S 900E.
99. Y137 locale.
100. Y109 locale.
101. Intersection of CL1E and LY300S.
102. CL1E 325S.
103. Intersection of CL1E and LY350S.
104. Intersection of CL1E and LY400S.
105. Intersection of CL1E and LY450S.
106. LY450S 1125E.
107. Y134 locale.
108. Y133 locale.
109. LY400S 1150E.
110. Y132 locale.
111. Trench to north of Y132 locale.
112. LY300S 1175E.
113. Y120 locale.
114. Water trough.
115-125. No survey points.
126 Spike in ground near Yuniman LCP.

No tag number. Approximate location of northeast corner L1914.
No tag number. Yuniman 1 and Yuniman 2 Legal Corner Post.

△

YUNIMAN PROJECT.

APPENDIX H EDM SURVEY DATA

NOTES.

1) Origin of X, Y Co-ordinates:

Legal Corner Post of Old Diggings M.C., Record #2081,
Osoyoos Mining Division.
Assumed X = 10,000 (N) Y = 10,000 (E)

2) Bearings derived from north boundary of Lot 1912, Black Pine M.C. original plan bearing = 89°07'

3) Elevations derived from triangulation station #80H2774. Elevation = 2146.7M

COORDINATES.

	Northings X	Eastings Y.	Elevation Z.
CHAP. 1.	10,000.0.	10,000.3.	1993.0.
2.	9,941.9.	10,337.1.	2001.2.
3.	9,949.0.	10,794.0.	2051.5.
4.	9,842.4.	10,753.3.	2022.7.
5.	9,906.1.	10,712.4.	2030.7.
6.	9,886.8.	10,705.9.	2025.4.
7.	9,821.8.	10,795.9.	2018.6.
8.	9,951.0.	10,885.5.	2066.3.
9.	9,953.3.	10,982.9.	2070.3.
10.	9,959.2.	11,048.8.	2066.3.
11.	9,789.7.	11,018.4.	2021.5.
12.	9,765.1.	11,031.7.	2013.2.
13.	9,744.1.	10,797.1.	1986.5.
14.	8,886.5.	10,906.2.	1978.3.
15.	9,600.4.	10,643.8.	1921.7.
16.	9,577.6.	10,642.8.	1909.1.
17.	9,570.1.	10,642.0.	1904.0.
18.	9,552.0.	10,642.2.	1889.8.
19.	9,562.0.	10,606.0.	1888.8.
20.	9,564.0.	10,673.0.	1898.0.
21.	9,562.9.	10,686.7.	1896.2.
22.	9,578.0.	10,693.4.	1903.2.
23.	9,571.7.	10,572.1.	1902.6.
24.	9,590.2.	10,662.3.	1914.2.
25.	9,588.7.	10,669.5.	1914.1.
26.	9,592.3.	10,685.8.	1913.7.
27.	9,601.2.	10,675.0.	1920.8.
28.	9,594.4.	10,678.1.	1916.1.
29.	9,600.5.	10,655.4.	1918.8.
30.	9,617.4.	10,596.0.	1916.9.
31.	9,609.6.	10,704.1.	1920.9.
32.	9,610.2.	10,726.7.	1922.0.
33.	9,591.8.	10,729.7.	1909.8.
34.	9,572.4.	10,714.6.	1895.5.
35.	9,554.2.	10,710.1.	1881.7.
36.	9,538.2.	10,709.8.	1870.4.
37.	9,555.4.	10,739.3.	1877.5.
38.	9,563.5.	10,735.8.	1886.0.
39.	9,572.0.	10,735.8.	1892.5.
40.	9,596.9.	10,737.6.	1910.0.
41.	9,604.1.	10,749.3.	1913.8.
42.	9,617.5.	10,751.1.	1924.3.
43.	9,627.8.	10,747.5.	1931.3.

		Northings X.	Eastings Y.	Elevation Z.
CHAP.	44.	9,631.3.	10,758.4.	1931.7.
	45.	9,641.8.	10,708.5.	1940.5.
	46.	9,650.2.	10,727.6.	1946.0.
	47.	9,671.2.	10,710.6.	1955.2.
	48.	9,674.1.	10,720.8.	1957.0.
	49.	9,682.3.	10,691.4.	1957.5.
	50.	9,693.9.	10,695.1.	1963.8.
	51.	9,690.0.	10,718.3.	1963.8.
	52.	9,792.1.	10,651.3.	1989.4.
	53.	9,750.2.	10,676.1.	1982.0.
	54.	9,736.7.	10,692.1.	1979.4.
	55.	9,717.1.	10,768.2.	1973.7.
	56.	9,705.1.	10,797.7.	1965.5.
	57.	9,689.8.	10,769.2.	1960.7.
	58.	9,667.3.	10,735.7.	1954.3.
	59.	9,631.6.	10,679.4.	1934.9.
	60	9,663.4.	10,732.6.	1952.0.
	61.	9,650.4.	10,772.1.	1940.0.
	62.	9,642.6.	10,806.7.	1933.2.
	63.	9,652.6.	10,820.5.	1938.3.
	64.	9,664.0.	10,813.9.	1943.8.
	65.	9,674.1.	10,832.6.	1951.2.
	66.	9,677.9.	10,847.9.	1953.1.
	67.	9,683.4.	10,845.8.	1952.3.
	68.	9,691.5.	10,827.0.	1961.0.
	69.	9,695.6.	10,851.7.	1963.2.
	70.	9,689.4.	10,860.0.	1958.2.
	71.	9,693.0.	10,896.8.	1964.4.
	72.	9,700.9.	10,892.9.	1967.0.
	73.	9,701.1.	10,884.2.	1968.4.
	74.	9,700.0.	10,813.5.	1964.3.
	75.	9,606.2.	10,641.4.	1922,7.
	76.	9,791.2.	12,008.6.	2081.8.
	77.	9,625.5.	10,797.6.	1924.7.
	78.	9,845.0.	10,578.1.	1994.7.
	79.	9,902.3.	10,552.8.	2007.8.
	80.	9,946.2.	10,508.8.	2013.7.
	81.	9,982,7,	10,470.0.	2020.7.
	82.	10,022.4.	10,458.2.	2031.8.
	83.	10,062.2.	10,460.1.	2040.3.
	84.	10,082.7.	10,501.8.	2049.4.
	85.	10,076.9.	10,521.8.	2049.6.
	86.	10,094.0.	10,570.7.	2056.6.
	87.	10,108.3.	10,586.0.	2060.0.
	88.	10,114.6.	10,606.1.	2060.9.
	89.	9,661.1.	10,866.3.	1940.7.
	90.	9,610.1.	10,873.8.	1912.6.
	91.	9,615.7.	10,855.6.	1916.9.
	92.	9,615.7.	10,845.1.	1916.3.
	93.	9,607.7.	10,850.0.	1911.8.
	94.	9,599.2.	10,842.3.	1907.1.
	95.	9,578.5.	10,846.1.	1891.1.
	96.	9,577.2.	10,883.7.	1890.2.
	97.	9,573.2.	10,908.7.	1886.2.
	98.	9,611.4.	10,924.3.	1912.2.
	99.	9,657.3.	10,929.4.	1945.8.
	100.	9,671.6.	10,929.8.	1956.8.
	101.	9,735.5.	11,005.7.	1999.[illegible].
	102.	9.702.8.	11,005.1.	1985.6.
	103.	9,687.5.	11,007.0.	1971.8.
	104.	9,660.1.	11,009.8.	1956.0.

		Northings X.	Eastings Y.	Elevation Z.
CHAP.	105.	9,608.2.	11,012.1.	1920.0.
	106.	9,611.9.	11,149.3.	1918.8.
	107.	9,642.3.	11,163.1.	1943.4.
	108.	9,660.3.	11,164.1.	1955.4.
	109.	9,672.8.	11,157.6.	1958.4.
	110.	9,657.5.	11,199.1.	1967.0.
	111.	9,662.2.	11,205.2.	1971.6.
	112.	9,745.7.	11,191.4.	2002.7.
	113.	9,758.3.	11,095.6.	2005.4.
	114.	9,838.6.	11.205.2.	2037.3.
	115.-125 - No sample tag survey points assigned			
	126	9,896.5	12.018.6	2079.2
	N.E. Cor. L1914	9,924.8	12038.5	2081.5
	L.C.P. YUNIMAN 1 & 2	9,896.1	12017.3	2080.9

APPENDIX I

MINEROLOGICAL STUDY

A detailed minerological study was carried out on samples taken from sites where fairly high gold values are present.

The aim of the study was to identify and establish the paragenesis of the ore minerals present, the relationship of these minerals to gold mineralization, and to investigate the grain size distribution and liberation characteristics of gold.

The main conclusions to be drawn from the mineralogical analysis, are the following:

- In general and in order of abundance, the following ore minerals are present in the property: Arsenopyrite, pyrite, pyrrhotite, chalcopyrite, sphalerite, galena, Mn-oxides, Fe-hydroxides, gold and Au tellurides.
- The abundance of these minerals in different zones varies.
- There seem to be at least two stages of gold mineralization. In one, gold is closely associated with arsenopyrite, where the gold is fairly coarse (= 50 - 800u). In the second case, gold is present mainly as inclusions in pyrite. The size range of the gold grains in this case, however, is much smaller (= 60u - submicroscopic).
- Gold tellurides are closely associated with native gold.
- From the point of view of eventual recovery of the gold values from the mineralization, in zones where gold is associated with arsenopyrite, recovery should present no problems, but the recovery of gold associated with pyrite may be difficult.

MINERALOGICAL STUDY

1. Objectives

The main objectives of carrying out a detailed mineralogical study in the Yuniman property were:

- To identify and quantify all the ore minerals present in the different veins, shear zones and drill core where gold values are present
- To investigate the mode of occurrence of gold and its paragenetic relationship to other minerals
- To establish the size distribution and liberation characteristics of gold mineralization

2. Method

2.1. Sampling

The criteria for choosing sampling sites was based on the presence of fairly high gold values at the sites, since the main objective of the present study is to investigate the gold mineralogy in the property. The following table gives a description of the sampling sites and the method of sampling used:

Sample Nº	Type	Width cm.	Length m.	Description
MY-45A	vein	5-10	2	Continuous chip sample along strike. Contains abundant arsenopyrite
MYT-38	vein	5 - 15	15	Continuous chip sample along strike Contains sulphides
MYT-57	dyke	30-60	2	Sheared mafic dyke containing veinlets of quartz + sulphides
MYT-4058	core	1/4 split	3	Diorite containing quartz + sulphides in veinlets
MY-BR	shear	200	3	Limonitic shear zone (Bush rat) Contains some sulphides

Between 3kg and 5kg of material was collected from each sample site.

2.2. Sample Preparation

In order to carry out the mineralogical study, all samples were prepared in the following manner:

- Crush to 90% passing 3mm. This coarse grind was chosen to facilitate the study of ore mineral associations in fairly large particles and also to prevent gold losses to the slimes
- Sample homogenization
- Split of the heads submitted for chemical analyses
- Rest of the sample treated in a batea type of pan, in order to obtain a rough concentrate, where most of the ore minerals are present
- Preparation of polished sections of all concentrates and subsequent mineralogical study.

3. Discussion of Results and Conclusions

The results of the individual mineralographic studies are given in separate forms for each sample and are included at the end of the present report. While these reports show the type of associations and tentative paragenetic sequence of the ore minerals, it is difficult to draw conclusions on a general paragenetic sequence of deposition for the whole area. However, it seems that at least two sequences of gold deposition may have taken place.

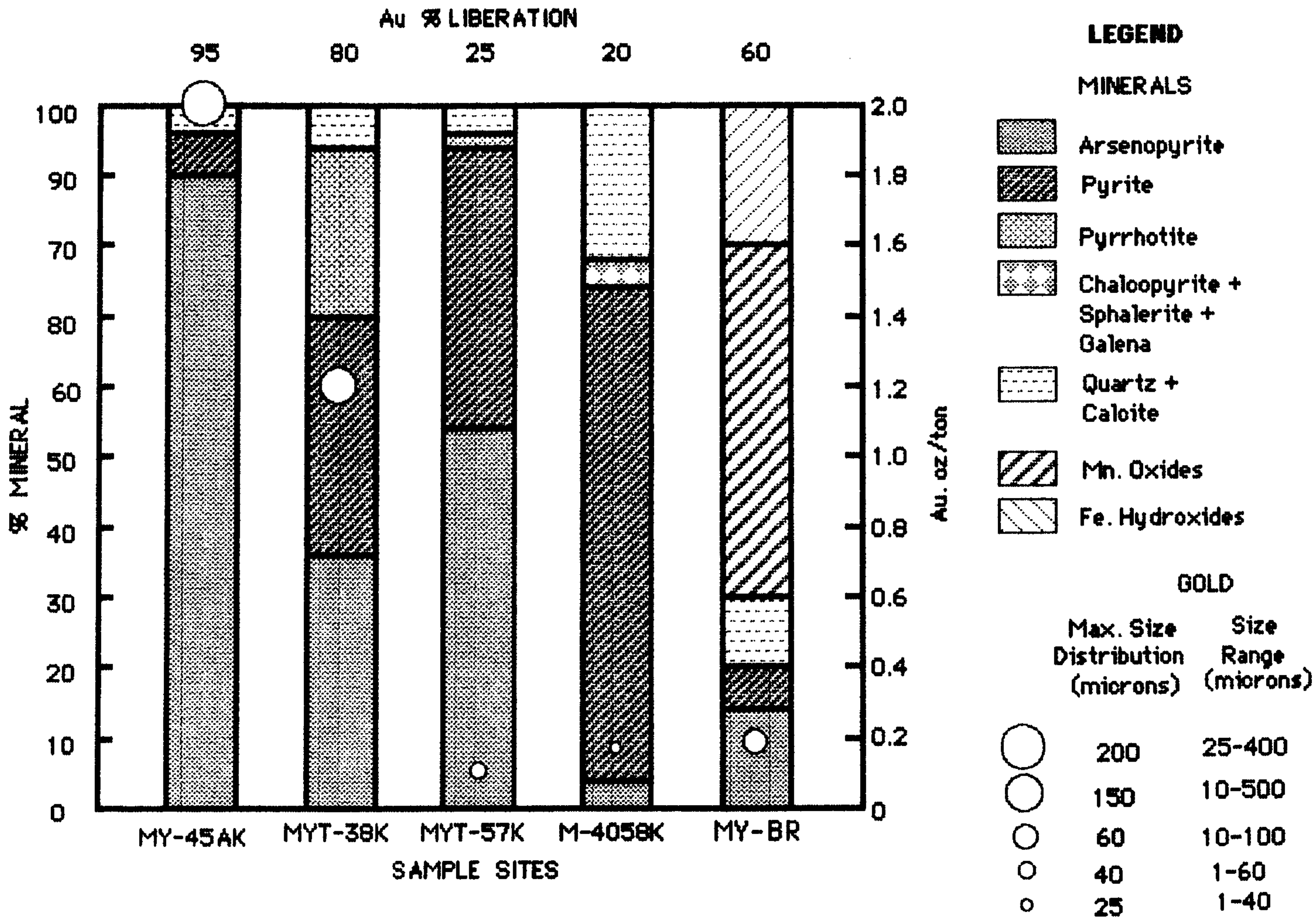
The chart on page 5 shows for each sample the mineralogy, gold content in the heads, maximum distribution and size range of particles, and degree of gold liberation in concentrates.

From the chart, the following conclusions can be drawn:

- In all cases, gold is present in the sample mainly as native gold and to a lesser extent as gold tellurides
- Samples MY-45AK and MYT-38K correspond to quartz calcite veins containing mainly sulphides, native gold and gold tellurides. It is evident that this two samples contain the highest gold values and have the coarsest gold.
- Sample MYT-57 was taken from a mineralized dyke close to the previous two samples. It is worth noting that the three samples mentioned above, contain fairly abundant arsenopyrite, which in turn is closely associated with gold occurrence as shown in the microscopic study
- SampleMY-BR was collected from the Bushrat shear zone, which is characterized by the presence of abundant Mn-oxides and Fe-hydroxides. Microscopic examination of this sample shows that the

Mn-oxides were formed at the expence of arsenopyrite, while pyrite is almost completely replaced by Fe-hydroxides.

- Sample M-4058 corresponds to a 10 ft. section of drill core (DDH-1, 58'-68'). The rock is a diorite with fine grained sulphides, disseminated and in veinlets. The microscopic study of this sample indicates that gold occurrs as minute inclusions in pyrite, with apparently no association with arsenopyrite, which is the case in the rest of the samples
- From the point of view of mineral processing, the graph shows that liberation of the gold from the vein and shear zone material, should not present any difficulties, while the gold values tied up in the country rock would require fine grinding in order to liberate a reasonable amount of gold.



Mineralogy, gold content in heads, maximum distribution and size range of gold particles, and degree of gold liberation in concentrates for different samples

MINERALOGRAPHIC REPORT

by C. L. Soux

For: Shangri La minerals
Project: Yuniman
Sample: MY-45AK

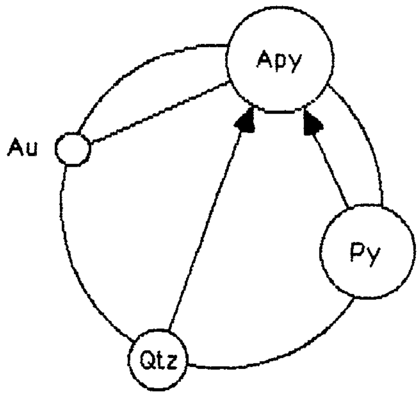
Location:
Collector: C. SOUX
Date Analyzed: Dec/2/86

MACROSCOPIC DESCRIPTION:

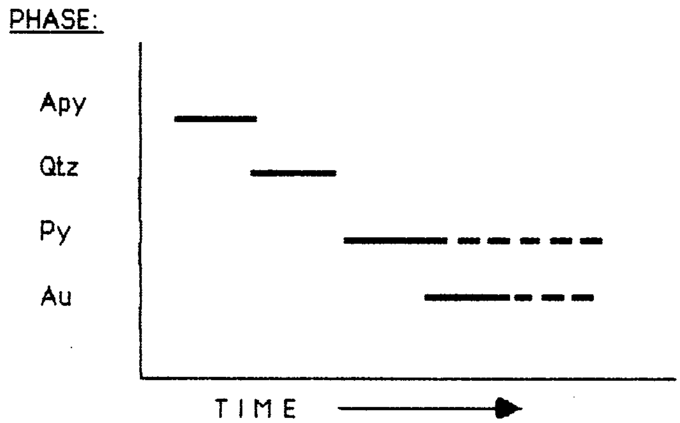
Concentrate of vein material. Continuous chip sample of vein (≈5-10cm wide) for 3m . Sample contains abundant arsenopyrite

MICROSCOPIC ANALYSIS IN POLISHED SECTION

Abr.	Mineral	Chem. Formula	%	Description
Apy	Arsenopyrite	Fe As S	90	Dicrete grains
Py	Pyrite	Fe S2	8	Discrete grains
Qtz	Quartz	Si O2	2	Mainly filling fractures in Apy
Au	Gold	Au	<1	As free grains and associated with Apy



Vandeveer Diagram



Tentative Paragenetic Sequence

TEXTURES AND DESCRIPTION:

Arsenopyrite occurs as discrete grains and contains veinlets of quartz.
Gold is present mainly as free grains (95% liberation) which are fairly coarse (around 200µ in size). The rest is closely associated with arsenopyrite. No association of gold with pyrite was observed.

MINERALOGRAPHIC REPORT

by C. L. Soux

For: Shangri La minerals
Project: Yuniman
Sample: MYT-38K

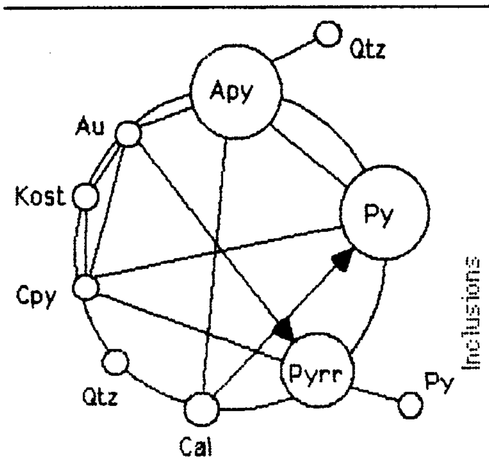
Location:
Collector: C. Soux
Date Analyzed: Dec/2/86

MACROSCOPIC DESCRIPTION:

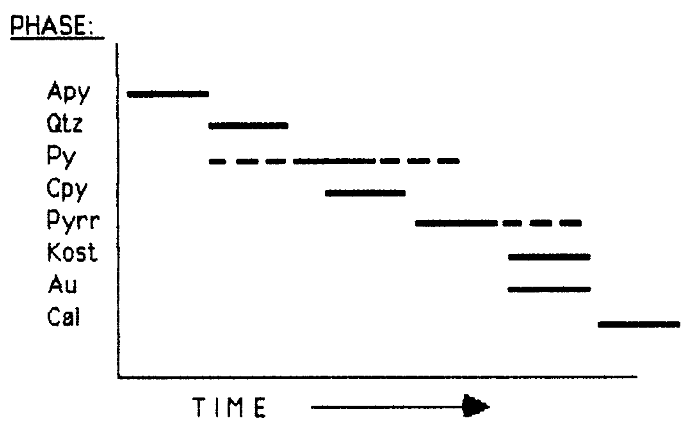
Concentrate of composite chip sample along strike of vein (5-15cm wide) for 15 m. Contains sulphides

MICROSCOPIC ANALYSIS IN POLISHED SECTION

Abr.	Mineral	Chem. Formula	%	Description
Apy	Arsenopyrite	Fe As S	35	Discrete grains
Py	Pyrite	Fe S2	35	Replaced in part by calcite
Pyrr	Pyrrhotite	Fe S	27	Contains inclusions of Py
Cpy	Chalcopyrite	Cu Fe S2	<1	Associated with Kos in Apy
Au	Gold	Au	<1	As free grains and associated with Kos in Apy
Kos	Kostovite	Au Cu Te4	<<1	Mainly associated with Au
Cal	Calcite	Ca C 03	2	Replaces Py



Vandeveer Diagram



Tentative Paragenetic Sequence

TEXTURES AND DESCRIPTION:

Gold in the sample occurs to a great extent as free grains. The liberation reaches 80%, the rest is present as inclusions in arsenopyrite intergrown with kostovite, chalcopyrite and to a minor extent with pyrrhotite. The grain size distribution of maximum frequency is 150µ and the total range 10 -500µ.

Kostovite is mainly associated to gold, but a few free particles were observed.

Calcite is seen filling late fractures and partly replacing pyrite.

Arsenopyrite occurs as discrete grains which are in some cases idiomorphic.

MINERALOGRAPHIC REPORT

by C. L. Soux

For: Shangri-La Minerals
Project: Yuniman
Sample: MYT-57K

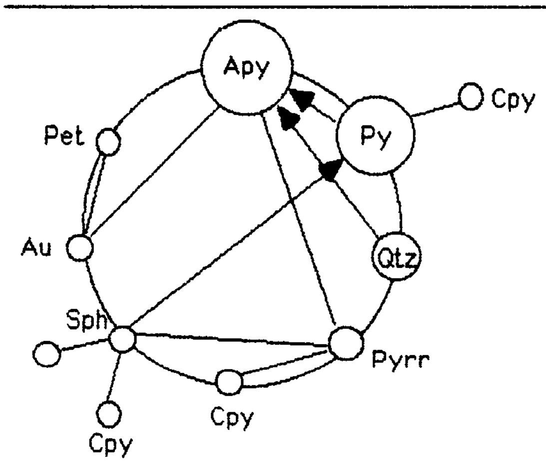
Location:
Collector: C. Soux
Date Analyzed: Dec/2/86

MACROSCOPIC DESCRIPTION:

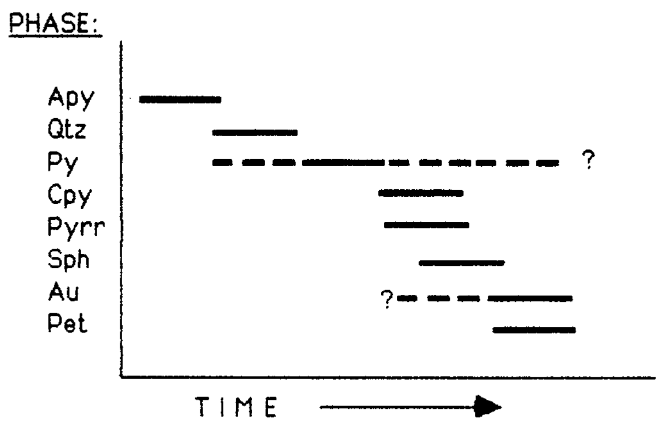
Concentrate of composite chip sample across 2 m. of sheared dyke in adit Nº 4

MICROSCOPIC ANALYSIS IN POLISHED SECTION

Abr.	Mineral	Chem. Formula	%	Description
Apy	Arsenopyrite	Fe As S	55	Contains Qtz and Au in veinlets and inclusions
Py	Pyrite	Fe S2	40	As discrete grains. Contains inclusions of Cpy
Qtz	Quartz	Si O2	3	Discrete grains and in veins in Apy
Pyrr	Pyrrhotite	Fe S	1	Discrete grains
Sph	Sphalerite	Zn S	<1	Contains inclusions of Cpy + Pyrr
Cpy	Chalcopyrite	Cu Fe S2	<1	Associated with Pyrr and Sph
Au	Gold	Au	<<1	In late fractures in Apy
Pet	Petzite	Ag3 Au Te2	<<1	Closely associated with Au



Vandeveer Diagram



Tentative Paragenetic Sequence

TEXTURES AND DESCRIPTION:

The sample is composed mainly of arsenopyrite and pyrite.

Gold mineralization seems closely associated to arsenopyrite. The liberation of the gold grains is poor. Only 25% is present as free grains which are, in average, around 40µ in size.

Most of the gold occurs as inclusions and in narrow veins in arsenopyrite closely associated with petzite. The overall size range of the gold grains is from 1 - 60µ.

Sphalerite contains exsolution blebs of chalcopyrite and pyrrhotite.

MINERALOGRAPHIC REPORT

by C. L. Soux

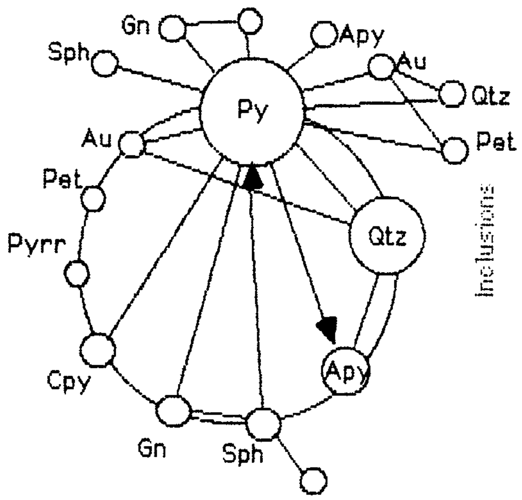
For:	Shangri La Minerals	**Location**:	
Project:	Yuniman	**Collector**:	C. Soux
Sample:	M-4058K	**Date Analyzed**:	Dec/3/86

MACROSCOPIC DESCRIPTION:

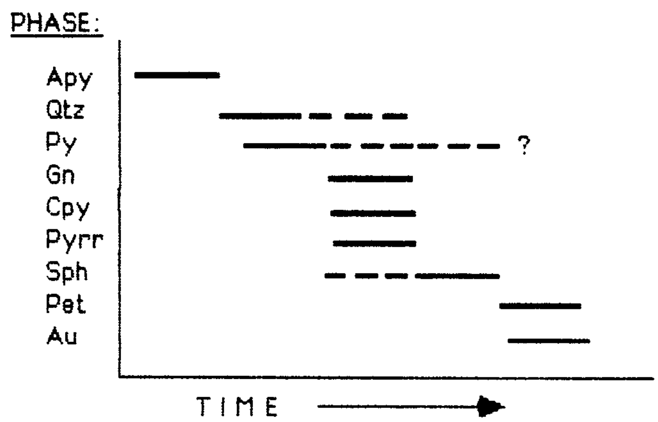
Concentrate of core sample containing abundant sulphides

MICROSCOPIC ANALYSIS IN POLISHED SECTION

Abr.	Mineral	Chem. Formula	%	Description
Py	Pyrite	$Fe S_2$	70	Contains numerous inclusions
Apy	Arsenopyrite	$Fe As S$	3	Mainly as idiomorphic grains
Qtz	Quartz	$Si O_2$	23	As discrete grains
Gn	Galena	$Pb S$	1	Replaced in part by Sph
Sph	Sphalerite	$Zn S$	1	Contains inclusions of Cpy
Cpy	Chalcopyrite	$Cu Fe S_2$	1	As inclusions in Py and Sph
Pyrr	Pyrrhotite	$Fe S$	<1	Mainly as inclusions in Py
Pet	Petzite	$Ag_3 Au Te_2$	<<1	In association with Au
Au	Gold	Au	<<1	Mainly as inclusions in Py



Vandeveer Diagram



Tentative Paragenetic Sequence

TEXTURES AND DESCRIPTION:

Pyrite is the major component in the sample and contains numerous inclusions of sphalerite, galena, arsenopyrite, chalcopyrite, quartz, petzite and gold.

Gold in the sample is very fine. The maximum grain size observed was 40µ. The gold liberation in the sample is very poor, only 20% of the total gold content is present as free particles. Most of the intergrown gold, which is almost entirely tied up with pyrite is very fine grained. The size ranges from ≈25µ to submicrscopic. Gold within pyrite is mainly associated with petzite and to a minor extent with quartz

MINERALOGRAPHIC REPORT

by C. L. Soux

For: Shangr-La Minerals
Project: Yuniman
Sample: My-BR

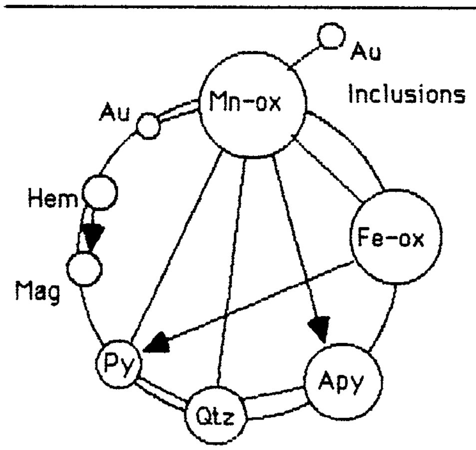
Location:
Collector: Nigel Hulme
Date Analyzed: Dec/2/86

MACROSCOPIC DESCRIPTION:

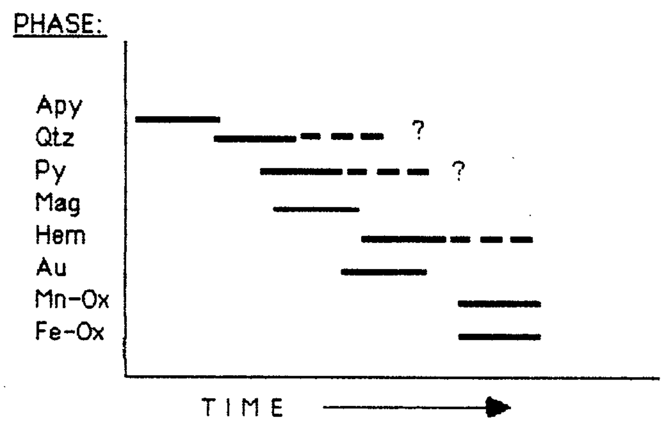
Concentrate of continuous chip sample in the Bush rat zone. Sample accross 2 m. Material is limonitic and contains some sulphides

MICROSCOPIC ANALYSIS IN POLISHED SECTION

Abr.	Mineral	Chem. Formula	%	Description
Apy	Arsenopyrite	$Fe\ As\ S$	12	Replaced by Mn-ox
Py	Pyrite	$Fe\ S_2$	8	Replaced by Fe-ox
Qtz	Quartz	$Si\ O_2$	10	Discrete grains
Mn-ox	Manganese oxides		50	Contains some Au inclusions
Fe-ox	Iron hydroxides		20	Replaces Py
Mag	Magnetite	$Fe\ Fe_2\ O_4$	1	Replaced by Hem
Hem	Hematite	$Fe_2\ O_3$	1	Replaces magnetite
Au	Gold	Au	<<1	As free and interlocked grains



Vandeveer Diagram



Tentative Paragenetic Sequence

TEXTURES AND DESCRIPTION:

The sample is composed mainly of Mn-ox. and Fe-ox.

Gold is present as free grains around 60µ in size. It also occurs as inclusions in Mn-ox. The size range of the gold grains varies from 10 to 100µ.

Arsenopyrite is replaced selectively by Mn-ox, while pyrite is mainly replaced by Fe-Ox (Goethite, lepidocrocite).

Hematite is found replacing magnetite in part (martitization)

APPENDIX J SOIL GEOCHEMICAL ANALYSIS RESULTS
(samples collected in 1985)

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL -80 MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JULY 16 1986 DATE REPORT MAILED: July 21/86 ASSAYER. D. Toye. DEAN TOYE. CERTIFIED B.C. ASSAYER.

SHANGRI-LA MINERALS PROJECT - YUNIMAN FILE # 86-1508 PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 225S 1025E	1	42	14	105	.3	33	13	1324	3.00	37	5	ND	1	26	1	2	2	54	.28	.086	9	30	.47	268	.09	4	1.90	.01	.12	1	44
YL 225S 1050E	1	41	10	96	.3	25	13	1553	3.02	30	5	ND	1	25	1	2	2	53	.20	.092	9	27	.45	275	.08	4	1.89	.01	.12	1	60
YL 225S 1075E	1	57	16	144	.4	44	16	1796	3.44	37	5	ND	1	23	1	2	3	58	.21	.112	14	35	.51	523	.07	2	1.90	.01	.13	1	17
YL 225S 1100E	1	63	16	128	.4	37	17	1627	3.46	44	5	ND	1	25	1	2	2	60	.24	.103	11	37	.54	343	.07	2	1.81	.01	.15	1	17
YL 225S 1125E	2	73	6	152	.6	44	17	2135	3.30	36	5	ND	1	37	1	2	2	57	.41	.102	16	38	.58	408	.10	6	2.02	.02	.15	1	22
YL 225S 1150E	1	58	11	149	.3	36	17	1591	3.60	40	5	ND	1	21	1	2	2	61	.22	.096	13	35	.55	224	.11	2	2.10	.01	.14	1	65
YL 225S 1175E	1	52	23	138	.5	39	18	1862	3.75	39	5	ND	1	36	1	2	2	61	.43	.121	14	38	.60	300	.10	2	2.21	.01	.20	1	50
YL 225S 1200E	1	48	14	90	.2	25	14	1233	3.44	40	5	ND	1	26	1	2	2	62	.26	.085	12	35	.50	258	.09	2	1.63	.01	.18	1	16
YL 225S 1225E	1	44	18	100	.3	24	15	2912	3.02	18	5	ND	1	19	1	2	2	55	.20	.099	8	24	.34	170	.10	3	1.69	.01	.09	1	10
YL 225S 1250E	1	41	11	83	.2	22	11	1311	2.90	22	5	ND	1	14	1	2	2	52	.13	.110	10	27	.42	164	.08	5	1.87	.01	.09	1	9
YL 225S 1275E	1	49	12	92	.3	26	14	1435	3.28	30	5	ND	1	15	1	2	2	55	.15	.079	11	30	.43	175	.10	5	1.96	.01	.11	1	19
YL 225S 1300E	1	52	18	109	.3	35	17	1760	3.78	36	5	ND	1	25	1	2	2	59	.22	.096	15	35	.51	252	.09	7	2.20	.01	.20	1	15
YL 225S 1325E	1	51	15	111	.1	34	18	1787	3.62	36	5	ND	1	23	1	2	2	56	.19	.091	13	34	.50	296	.09	6	2.06	.01	.25	1	19
YL 225S 1350E	1	54	10	116	.3	36	18	1836	3.55	34	5	ND	1	25	1	2	2	56	.24	.112	14	33	.52	371	.08	6	1.97	.01	.20	1	16
YL 225S 1375E	1	50	14	103	.1	33	17	1816	3.34	35	5	ND	1	32	1	2	2	56	.30	.107	12	34	.53	411	.09	6	1.88	.01	.19	1	14
YL 225S 1400E	1	54	8	104	.2	34	16	1611	3.42	38	5	ND	1	30	1	2	2	56	.30	.127	13	34	.55	370	.08	6	1.99	.01	.21	1	15
YL 225S 1425E	1	49	10	106	.2	31	15	1571	3.39	34	5	ND	1	24	1	2	2	56	.25	.122	12	34	.53	303	.07	3	1.87	.01	.21	1	25
YL 225S 1450E	1	50	18	104	.2	29	15	1575	3.49	35	5	ND	1	33	1	2	2	55	.31	.125	14	33	.49	371	.07	6	1.81	.01	.20	1	28
YL 225S 1475E	1	50	19	100	.1	32	16	1525	3.60	43	5	ND	1	22	1	2	2	59	.21	.129	13	38	.56	344	.09	4	1.73	.01	.28	1	16
YL 225S 1500E	1	51	21	126	.2	32	16	1517	3.80	55	5	ND	1	25	1	2	2	62	.22	.134	13	42	.58	334	.07	5	1.85	.01	.23	2	44
YL 225S 1525E	1	49	14	106	.2	29	16	1625	3.46	38	5	ND	1	18	1	2	2	58	.15	.122	12	34	.49	255	.08	4	1.83	.01	.18	1	31
YL 225S 1550E	1	52	9	131	.2	33	17	1748	3.49	31	5	ND	1	21	1	2	2	59	.18	.147	13	36	.54	254	.07	7	2.17	.01	.19	1	70
YL 225S 1575E	1	40	15	103	.2	25	14	1331	3.23	26	5	ND	1	17	1	2	2	58	.16	.111	10	32	.46	214	.10	2	1.91	.01	.11	1	36
YL 225S 1600E	2	44	9	108	.2	28	14	1675	3.06	26	5	ND	1	16	1	2	2	54	.15	.131	9	29	.43	221	.09	3	2.04	.01	.12	1	60
YL 225S 1625E	1	50	21	152	.2	34	15	2024	3.68	39	5	ND	1	19	1	2	2	63	.14	.090	11	29	.41	321	.12	3	2.19	.02	.10	1	46
YL 225S 1650E	2	53	25	134	.2	35	17	2030	3.76	43	5	ND	1	20	1	2	2	61	.14	.107	13	34	.44	312	.11	3	2.30	.02	.11	1	65
YL 225S 1675E	1	53	27	117	.3	28	15	1550	3.61	47	5	ND	1	19	1	3	2	59	.12	.109	13	32	.45	259	.09	6	2.21	.01	.12	1	130
YL 225S 1700E	2	58	26	149	.4	29	17	2011	3.67	77	5	ND	1	26	2	2	2	54	.20	.154	13	30	.43	290	.06	5	2.04	.01	.16	1	190
YL 225S 1725E	2	56	22	147	.5	34	16	1957	3.88	38	5	ND	1	26	1	2	2	64	.32	.130	14	40	.58	314	.11	2	2.31	.02	.18	1	65
YL 225S 1750E	1	44	14	96	.1	21	12	2315	3.05	21	5	ND	1	15	1	2	2	57	.10	.124	8	21	.31	156	.11	2	2.17	.02	.07	1	24
YL 225S 1775E	2	41	18	82	.5	23	12	1214	3.13	34	5	ND	1	12	1	2	2	53	.08	.088	10	27	.38	180	.09	3	1.94	.01	.08	2	50
YL 225S 1800E	2	46	22	94	.5	26	13	1395	3.31	35	5	ND	1	15	1	2	2	56	.11	.098	11	31	.40	222	.09	5	2.09	.01	.08	1	60
YL 225S 1825E	2	54	23	94	.5	28	15	1392	3.66	46	5	ND	1	18	1	2	2	58	.13	.092	12	35	.44	243	.08	2	1.95	.01	.12	1	135
YL 225S 1850E	1	51	18	136	.3	39	18	1387	3.93	38	5	ND	1	24	1	2	2	69	.27	.091	12	47	.67	234	.13	6	2.24	.02	.17	1	75
YL 225S 1875E	1	46	17	252	.4	51	18	1669	3.00	24	5	ND	1	13	2	2	2	52	.11	.065	11	33	.43	179	.11	3	2.04	.02	.09	1	60
YL 225S 1900E	1	37	16	104	.4	25	12	883	2.92	29	5	ND	1	16	1	2	2	49	.13	.068	10	31	.35	187	.08	2	1.75	.01	.09	1	31
STD C/AU 0.5	21	60	39	135	7.0	72	30	1160	3.95	36	18	8	35	50	18	15	21	65	.47	.109	40	61	.87	189	.09	36	1.72	.07	.14	15	495

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
YL 225S 1925E	1	39	12	79	.3	23	12	746	3.17	33	5	ND	1	15	1	3	2	51	.12	.072	9	32	.41	190	.07	4	1.81	.01	.09	1	48
YL 225S 1950E	1	62	17	94	.4	57	17	925	3.53	34	5	ND	1	19	1	2	2	63	.36	.101	10	83	.64	242	.05	7	2.13	.01	.14	1	28
YL 225S 1975E	1	38	13	113	.2	26	11	896	2.85	24	5	ND	1	16	1	2	2	51	.17	.117	9	34	.39	184	.04	2	2.08	.02	.09	1	13
YL 225S 2000E	2	44	15	96	.4	25	10	610	3.21	31	5	ND	1	14	1	2	2	54	.11	.091	8	31	.39	165	.06	7	2.11	.02	.10	1	24
YL 250S 1000E	2	69	10	117	1.1	41	17	991	3.39	50	5	ND	1	11	1	2	2	60	.09	.072	9	34	.52	222	.09	5	2.10	.01	.10	1	18
YL 250S 1000E-A	1	63	14	117	1.6	33	19	1351	3.19	40	5	ND	1	14	1	2	2	59	.11	.088	10	32	.50	214	.10	3	2.48	.02	.08	1	6
YL 250S 1025E	2	48	14	122	.2	28	15	1546	3.06	33	5	ND	1	23	1	2	2	56	.24	.140	9	29	.49	220	.09	2	2.27	.02	.09	1	15
YL 250S 1050E	1	43	10	117	.2	30	15	1944	3.14	34	5	ND	1	20	1	2	4	60	.20	.132	8	31	.52	217	.10	2	2.53	.02	.11	1	11
YL 250S 1075E	2	47	14	134	.2	31	17	2131	3.24	33	5	ND	1	22	1	2	2	58	.22	.132	9	33	.53	267	.07	2	2.39	.02	.13	1	3
YL 250S 1100E	1	62	11	136	1.0	49	18	1281	4.18	57	5	ND	1	25	1	2	2	71	.26	.083	9	45	.70	245	.10	8	2.30	.02	.15	1	21
YL 250S 1125E	1	65	16	216	.4	47	19	1547	3.63	42	5	ND	1	33	1	2	2	59	.39	.132	13	39	.62	323	.08	6	2.20	.02	.18	1	12
YL 250S 1150E	2	60	38	231	.7	42	18	1861	4.02	79	5	ND	1	26	1	2	2	64	.29	.109	13	40	.61	252	.09	5	2.26	.02	.16	1	22
YL 250S 1175E	1	57	16	132	.5	38	17	1501	3.97	50	5	ND	1	25	1	2	2	67	.28	.089	14	40	.62	245	.09	8	2.44	.02	.16	1	23
YL 250S 1200E	1	74	11	128	.6	54	22	2168	4.70	47	5	ND	1	32	2	2	3	77	.37	.109	16	51	.83	297	.11	6	2.99	.02	.25	1	225
YL 250S 1225E	2	51	8	109	.2	24	13	2982	3.09	15	5	ND	1	17	1	2	2	55	.17	.138	9	20	.29	154	.13	8	3.40	.03	.06	1	3
YL 250S 1250E	1	53	16	96	.1	26	15	1698	3.25	25	5	ND	1	14	1	2	2	57	.12	.121	10	28	.43	144	.09	2	2.47	.02	.09	1	44
YL 250S 1275E	2	56	13	105	.1	29	16	1492	3.60	29	5	ND	1	12	1	2	2	65	.09	.115	10	33	.49	141	.09	6	2.31	.01	.09	1	24
YL 250S 1300E	1	48	13	114	.1	31	17	1750	3.65	32	5	ND	1	25	1	2	2	56	.23	.108	15	31	.50	282	.06	2	2.15	.02	.20	1	14
YL 250S 1325E	2	66	17	151	.2	43	20	1662	4.12	52	5	ND	1	28	1	2	2	62	.28	.122	15	39	.60	340	.08	6	2.46	.02	.26	1	10
YL 250S 1350E	1	53	9	127	.2	34	19	1808	3.69	37	5	ND	1	24	1	2	2	56	.22	.111	14	33	.53	346	.08	5	2.04	.02	.20	1	13
YL 250S 1375E	2	50	14	117	.3	37	17	1529	3.68	36	5	ND	1	21	1	2	2	59	.20	.102	12	33	.54	280	.10	7	2.06	.02	.17	1	7
YL 250S 1400E	2	51	7	107	.1	34	16	1386	3.61	39	5	ND	1	21	1	2	2	57	.20	.111	12	33	.51	279	.08	4	1.96	.02	.16	1	48
YL 250S 1425E	1	51	11	119	.1	32	17	1401	3.61	32	5	ND	1	21	1	2	2	58	.23	.111	12	35	.53	249	.09	6	2.26	.02	.15	1	22
YL 250S 1450E	2	50	10	127	.3	32	15	1452	3.39	29	5	ND	1	29	1	2	2	55	.32	.114	13	35	.53	318	.06	7	2.47	.02	.17	1	18
YL 250S 1475E	1	52	20	150	.5	35	15	1574	3.67	50	5	ND	1	31	2	2	2	61	.35	.153	15	41	.62	380	.05	8	2.33	.02	.24	2	20
YL 250S 1500E	2	66	27	157	.5	45	17	1546	4.07	53	5	ND	1	29	1	2	2	66	.28	.158	15	45	.64	362	.07	2	2.61	.02	.26	1	85
YL 250S 1525E	2	70	11	149	.4	44	17	1589	3.97	42	5	ND	1	28	1	2	3	67	.26	.156	15	44	.63	334	.07	6	2.67	.02	.20	1	19
YL 250S 1550E	1	43	11	115	.2	27	15	1598	3.33	25	5	ND	1	22	1	2	2	58	.27	.126	8	32	.51	233	.09	3	2.13	.02	.11	1	5
YL 250S 1575E	1	41	11	104	.1	27	13	1324	3.46	28	5	ND	1	15	1	2	2	59	.15	.092	9	33	.52	209	.10	2	2.41	.02	.11	1	15
YL 250S 1600E	1	39	14	104	.3	25	12	1526	3.04	23	5	ND	1	18	1	2	2	53	.20	.109	8	27	.45	197	.09	4	2.40	.02	.11	2	9
YL 250S 1625E	1	55	13	115	.3	29	17	1261	3.84	42	5	ND	1	15	1	2	2	66	.11	.090	12	32	.48	271	.11	2	2.23	.02	.11	1	50
YL 250S 1650E	2	50	18	123	.6	28	14	1161	3.74	48	5	ND	1	17	1	4	2	58	.14	.117	8	31	.41	189	.10	5	2.37	.02	.08	1	14
YL 250S 1675E	1	53	12	109	.1	34	16	1493	3.63	47	5	ND	1	20	1	2	2	60	.17	.095	11	35	.52	293	.08	4	2.20	.01	.12	1	38
YL 250S 1700E	2	65	40	196	.8	41	18	1830	3.97	46	5	ND	1	33	2	2	2	63	.51	.108	13	40	.60	278	.08	2	2.39	.02	.14	1	28
YL 250S 1725E	2	59	18	169	.2	37	18	1729	3.65	44	5	ND	1	20	1	2	2	59	.18	.099	10	33	.50	209	.09	7	2.40	.02	.17	1	865
YL 250S 1750E	2	56	17	121	.2	31	15	1295	3.56	42	5	ND	1	15	1	2	2	59	.10	.096	10	33	.50	214	.10	5	2.33	.02	.09	1	180
STD C/AU 0.5	20	59	37	132	7.0	70	30	1090	3.93	40	19	8	34	48	17	15	21	64	.48	.100	36	58	.88	179	.08	37	1.72	.07	.13	14	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 250S 1775E	2	46	19	137	.3	30	15	1084	3.39	49	5	ND	1	17	1	2	2	57	.20	.102	12	34	.47	203	.10	4	2.05	.02	.11	1	44
YL 250S 1800E	2	59	21	156	.7	34	17	1081	3.93	95	5	ND	1	13	1	2	4	58	.10	.082	13	36	.46	201	.09	5	2.17	.02	.11	1	110
YL 250S 1825E	2	49	18	115	.7	28	13	1203	3.63	54	5	ND	1	17	1	2	3	61	.16	.083	12	38	.48	202	.10	4	2.05	.02	.10	1	115
YL 250S 1850E	1	43	15	115	.3	28	13	1562	3.12	26	5	ND	1	18	1	2	2	59	.17	.097	8	37	.50	183	.11	2	2.34	.02	.08	1	37
YL 250S 1875E	2	69	24	79	.5	29	15	989	4.13	68	5	ND	1	15	1	2	2	59	.09	.079	15	44	.49	287	.07	3	1.82	.01	.19	1	90
YL 250S 1900E	2	63	21	226	.5	90	23	1127	4.20	51	5	ND	1	23	3	2	2	78	.34	.121	14	84	.74	349	.10	5	2.32	.02	.19	1	65
YL 250S 1925E	2	46	19	82	.7	27	12	529	3.27	30	5	ND	1	15	1	2	2	55	.12	.089	11	36	.42	179	.10	4	2.30	.02	.09	1	45
YL 250S 1950E	1	36	15	90	.4	20	11	931	2.69	17	5	ND	1	17	1	2	2	48	.15	.127	9	27	.33	162	.09	3	2.06	.02	.07	1	31
YL 250S 1975E	1	23	9	73	.3	14	7	563	2.58	9	5	ND	1	13	1	2	2	48	.11	.091	6	24	.28	107	.10	2	2.10	.02	.05	1	12
YL 250S 2000E	2	27	8	72	.8	16	9	1052	2.49	12	5	ND	1	12	1	2	2	45	.08	.086	9	24	.27	112	.07	3	2.24	.02	.06	1	27
YL 275S 1375E	1	54	13	137	.3	36	17	1888	3.59	35	5	ND	1	25	1	2	3	59	.22	.136	16	36	.53	334	.09	3	2.31	.02	.20	1	16
YL 275S 1400E	1	51	18	122	.2	33	16	1489	3.49	33	5	ND	1	22	1	2	2	58	.18	.124	15	36	.50	280	.11	2	2.34	.02	.15	1	7
YL 275S 1425E	1	42	14	107	.3	27	14	1214	3.27	25	5	ND	1	19	1	2	2	57	.17	.098	12	31	.43	218	.10	2	2.17	.02	.11	1	4
YL 275S 1450E	2	43	19	83	.8	31	12	1501	2.81	24	5	ND	1	48	1	2	2	53	.51	.098	16	34	.43	531	.06	7	2.55	.02	.13	2	8
YL 275S 1475E	2	58	30	131	.9	36	16	1459	3.89	57	5	ND	1	28	1	2	2	69	.26	.096	18	48	.62	394	.08	2	2.75	.02	.18	1	23
YL 275S 1500E	2	87	31	126	1.2	49	16	1179	4.24	55	5	ND	1	29	1	2	3	73	.25	.097	22	50	.61	461	.08	2	3.40	.02	.16	1	26
YL 275S 1525E	1	65	15	102	.3	37	17	1251	3.90	48	5	ND	1	28	1	2	2	65	.30	.110	16	43	.61	334	.08	2	2.03	.01	.25	1	18
YL 275S 1550E	1	53	13	107	.2	31	16	1274	3.69	35	5	ND	1	17	1	2	2	65	.19	.092	14	40	.56	259	.10	4	2.25	.02	.24	5	14
YL 275S 1575E	1	46	11	98	.3	29	14	1181	3.44	28	5	ND	1	16	1	2	2	62	.16	.087	13	34	.51	202	.12	5	2.49	.02	.11	1	9
YL 275S 1600E	1	43	11	99	.6	28	14	1018	3.36	28	5	ND	1	15	1	2	3	59	.16	.109	12	35	.49	194	.13	2	2.29	.02	.13	2	10
YL 275S 1625E	2	49	11	94	.4	25	12	1235	3.47	24	5	ND	1	12	1	2	2	63	.11	.107	10	33	.42	147	.10	5	2.18	.02	.09	1	21
YL 275S 1650E	1	46	15	103	.3	27	14	1497	3.19	25	5	ND	1	18	1	2	3	58	.15	.089	12	31	.45	270	.11	2	1.95	.02	.10	1	11
YL 275S 1675E	2	53	16	123	.4	33	18	1724	3.51	36	5	ND	1	20	1	2	3	63	.16	.082	13	37	.53	354	.12	3	2.12	.02	.12	1	26
YL 275S 1700E	1	43	14	117	.1	25	15	1329	3.28	29	5	ND	1	19	1	2	2	60	.15	.080	9	30	.43	213	.09	2	2.02	.02	.09	1	14
YL 275S 1725E	1	44	19	230	.4	31	14	1188	3.66	165	5	ND	1	31	1	2	2	62	.37	.073	12	38	.58	213	.12	4	2.25	.02	.11	1	21
YL 275S 1750E	3	63	21	162	.9	25	15	1610	3.79	75	5	ND	1	26	3	2	2	57	.21	.119	14	26	.36	198	.09	4	2.77	.02	.10	1	34
YL 275S 1775E	1	76	19	152	.4	53	17	600	4.61	63	5	ND	1	14	1	2	2	79	.13	.119	10	42	.99	162	.17	2	3.65	.02	.13	1	62
YL 275S 1800E	1	47	15	143	.2	29	12	502	3.50	36	5	ND	1	18	1	2	2	68	.23	.094	8	40	.57	128	.14	4	2.21	.02	.13	1	39
YL 275S 1825E	1	39	17	82	.2	26	12	665	3.16	14	5	ND	1	13	1	2	3	59	.10	.100	7	34	.43	94	.14	2	3.05	.02	.08	1	21
YL 275S 1850E	1	44	16	87	.6	28	13	823	3.22	28	5	ND	1	13	1	2	2	58	.10	.099	8	31	.39	104	.12	2	2.78	.02	.08	1	455
YL 275S 1875E	2	57	27	126	.8	33	16	1226	3.75	53	5	ND	1	21	2	3	2	58	.16	.117	15	39	.45	276	.07	5	2.15	.02	.14	1	75
YL 275S 1900E	2	63	25	119	.3	39	18	1505	3.97	53	5	ND	1	22	1	2	2	64	.23	.126	15	47	.55	345	.07	3	2.11	.01	.22	1	55
YL 275S 1925E	1	46	14	91	.4	34	15	644	3.58	33	5	ND	1	16	1	2	2	62	.11	.089	13	40	.48	199	.10	2	2.18	.02	.10	1	115
YL 275S 1950E	2	41	19	86	.6	24	12	692	3.15	28	5	ND	1	15	1	2	2	55	.12	.113	12	32	.38	161	.10	4	2.26	.02	.09	1	715
YL 275S 1975E	1	25	13	80	.6	14	9	738	2.38	12	5	ND	1	14	1	2	2	41	.11	.145	8	19	.21	104	.11	2	2.94	.03	.05	1	8
YL 275S 2000E	1	27	17	74	.5	18	7	618	2.58	19	5	ND	1	13	1	2	2	48	.11	.078	9	25	.26	122	.08	2	2.03	.02	.08	1	16
STD C/AU 0.5	21	62	37	136	7.0	70	30	1155	3.97	43	18	7	35	51	18	16	22	66	.48	.106	40	62	.88	189	.09	37	1.72	.07	.14	15	500

SHANGRI-LA MINERALS PROJECT - YUNIMAN FILE # 86-1508

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 600S 0E	2	41	14	141	.2	54	16	1350	3.95	39	5	ND	1	20	1	2	3	78	.19	.050	12	49	.61	232	.12	4	2.19	.02	.13	1	2
YL 600S 25E	2	71	9	186	.3	76	21	2006	4.05	37	5	ND	1	23	1	2	7	82	.16	.058	19	57	.72	285	.14	2	2.44	.02	.13	1	4
YL 600S 50E	2	48	9	204	.1	63	20	2102	3.64	57	5	ND	1	23	1	2	4	70	.22	.076	12	43	.60	284	.11	4	2.20	.02	.12	1	2
YL 600S 75E	2	48	9	143	.4	45	17	1834	3.36	54	5	ND	1	20	1	2	2	65	.17	.063	11	39	.54	247	.11	5	1.97	.02	.11	1	2
YL 600S 100E	1	42	15	169	.9	40	15	1707	3.22	137	5	ND	1	23	1	2	2	63	.22	.086	9	36	.49	246	.11	2	2.23	.02	.11	1	4
YL 600S 125E	2	46	13	122	.3	35	16	1379	3.65	84	5	ND	1	21	1	2	2	76	.18	.095	10	46	.60	275	.12	5	2.10	.02	.11	1	4
YL 600S 150E	2	44	9	134	.4	34	16	1748	3.37	74	5	ND	1	21	1	2	2	69	.18	.130	9	42	.55	266	.12	4	2.41	.02	.13	1	4
YL 600S 175E	2	47	8	159	.7	57	23	1508	3.74	196	5	ND	1	30	1	2	2	78	.27	.104	10	70	.78	431	.13	2	2.18	.02	.15	1	11
YL 600S 200E	3	72	55	179	1.4	58	22	1216	4.58	744	5	ND	1	32	1	3	6	100	.23	.142	11	84	.98	462	.13	3	2.60	.02	.15	1	65
YL 600S 225E	4	89	18	185	.6	54	26	1331	4.90	212	5	ND	1	49	1	2	3	125	.37	.207	11	91	1.02	701	.14	2	2.70	.01	.32	1	10
YL 600S 250E	3	85	15	195	.4	63	26	2426	4.28	136	5	ND	1	43	2	2	2	90	.33	.156	11	67	.80	591	.11	5	2.43	.01	.25	1	6
YL 600S 275E	3	77	33	236	.5	78	27	2064	4.73	116	5	ND	1	55	2	2	2	95	.43	.165	13	72	.87	646	.11	9	2.66	.02	.29	1	11
YL 600S 300E	4	69	25	206	.3	48	25	2045	4.66	157	5	ND	1	32	2	2	3	98	.24	.182	13	54	.72	559	.13	5	2.55	.02	.20	1	9
YL 600S 325E	3	122	67	388	.4	121	44	2561	4.95	161	5	ND	1	72	2	2	3	109	.70	.212	14	88	1.23	685	.16	7	2.99	.02	.34	1	8
YL 600S 350E	3	85	22	247	.3	63	27	2176	4.25	266	5	ND	1	54	2	2	3	86	.62	.203	10	48	.71	775	.09	10	2.43	.02	.21	1	30
YL 600S 375E	4	95	26	223	.5	66	31	2043	5.08	620	5	ND	1	40	2	3	3	106	.43	.198	14	71	.95	953	.09	3	2.71	.02	.27	1	160
YL 600S 400E	2	69	13	127	.5	34	18	1267	4.96	654	5	ND	1	45	1	2	2	95	.29	.131	14	52	.97	629	.09	2	2.56	.01	.29	1	175
YL 600S 425E	3	65	27	158	.5	33	18	1631	5.87	887	5	ND	1	48	1	2	2	107	.31	.179	16	59	.98	740	.08	2	2.73	.01	.29	1	285
YL 600S 450E	1	88	26	200	.3	65	33	1893	5.13	266	5	ND	1	55	1	2	5	103	.45	.119	12	71	1.15	943	.11	6	2.62	.01	.30	1	29
YL 600S 475E	1	122	9	134	.1	54	31	1548	5.68	47	5	ND	1	37	1	2	2	133	.44	.100	7	76	1.31	831	.09	4	2.18	.01	.40	1	13
YL 600S 500E	2	82	20	141	.2	53	23	2262	4.37	198	5	ND	1	26	1	2	2	76	.25	.109	14	56	.77	532	.06	3	1.87	.01	.23	1	20
YL 600S 525E	2	60	17	143	.4	44	18	1613	3.62	115	5	ND	1	32	1	2	3	68	.31	.124	12	48	.67	446	.08	5	1.87	.01	.22	1	16
YL 600S 550E	2	65	15	146	.3	46	20	1823	4.09	130	5	ND	1	30	1	2	2	67	.25	.129	15	47	.66	481	.07	3	1.75	.01	.24	1	18
YL 600S 575E	1	36	17	222	.2	32	16	1783	3.60	69	5	ND	1	24	1	2	2	65	.22	.115	10	33	.49	439	.07	4	2.14	.02	.10	1	10
YL 600S 600E	1	50	14	131	.1	34	16	1259	3.28	73	5	ND	1	28	1	2	2	59	.76	.105	11	46	.68	363	.08	5	1.59	.02	.22	1	9
YL 600S 625E	2	102	11	134	.3	57	25	1728	5.27	138	5	ND	1	35	1	2	2	89	.38	.112	17	66	.88	645	.07	2	1.95	.01	.31	1	16
YL 600S 650E	2	62	14	147	.3	48	20	1947	4.04	92	5	ND	1	29	1	2	2	68	.34	.125	17	48	.67	513	.07	2	1.84	.01	.25	1	15
YL 600S 675E	1	56	17	141	.1	37	20	2008	3.75	137	5	ND	1	30	1	2	2	68	.35	.110	11	42	.64	407	.10	7	2.00	.02	.14	1	14
YL 600S 700E	1	54	14	127	.1	36	17	1463	3.52	119	5	ND	1	23	1	2	2	65	.24	.100	11	40	.60	358	.12	2	2.04	.02	.13	1	18
YL 600S 725E	2	66	17	131	.1	41	21	1366	4.07	327	5	ND	1	22	1	2	2	73	.25	.071	13	46	.71	251	.13	2	2.42	.02	.11	1	85
YL 600S 750E	1	79	15	176	.3	46	19	1895	3.76	559	5	ND	1	43	1	2	2	62	.63	.059	11	44	.70	244	.11	2	2.12	.03	.13	1	50
YL 600S 775E	1	59	16	182	.2	42	19	1754	3.72	170	5	ND	1	35	1	2	2	65	.39	.139	11	41	.64	376	.10	4	2.18	.02	.15	1	55
YL 600S 800E	2	67	38	223	1.1	48	24	2873	3.85	202	5	ND	1	43	2	2	2	63	.54	.196	14	38	.59	397	.09	5	2.32	.02	.13	2	60
YL 600S 825E	3	98	52	352	1.1	101	41	7692	5.74	363	5	ND	1	36	4	3	2	58	.43	.158	14	34	.54	520	.07	7	2.00	.02	.15	1	185
YL 600S 850E	3	89	41	286	.6	87	34	5117	5.34	293	5	ND	1	30	1	2	2	63	.31	.100	14	39	.56	416	.09	2	2.07	.02	.15	1	75
YL 600S 875E	2	55	21	169	.4	41	19	1872	3.56	144	5	ND	1	29	1	2	2	61	.29	.106	13	38	.56	327	.10	4	2.07	.02	.12	1	36
YL 600S 900E	3	89	75	273	1.0	67	28	3295	4.46	180	5	ND	1	40	2	2	2	65	.33	.138	15	36	.46	565	.09	6	2.33	.02	.13	1	135
STD C/AU 0.5	21	61	39	136	7.0	72	31	1147	3.95	40	19	7	35	50	17	15	22	66	.48	.109	38	63	.88	189	.09	37	1.72	.07	.14	15	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au† PPB
YL 600S 925E	2	74	42	250	1.0	56	25	3820	4.28	144	5	ND	1	41	2	2	2	59	.45	.140	16	33	.48	486	.08	5	2.40	.02	.12	1	43
YL 600S 950E	2	52	30	179	.3	41	19	2758	3.82	131	5	ND	1	41	1	2	2	61	.38	.116	12	32	.53	389	.08	4	2.20	.02	.13	1	49
YL 600S 975E	3	58	37	257	.9	52	22	3397	4.16	139	5	ND	1	44	2	2	2	56	.42	.179	15	29	.45	496	.06	2	2.20	.02	.14	1	27
YL 600S 1000E	1	34	10	125	.2	30	14	1423	3.11	58	5	ND	1	22	1	2	2	53	.24	.103	10	30	.45	226	.11	3	2.25	.02	.08	1	13
YL 600S 1025E	1	37	10	123	.2	30	14	1315	2.74	37	5	ND	1	32	1	2	2	44	.37	.123	10	29	.47	276	.08	6	1.89	.02	.10	1	22
YL 600S 1050E	2	43	11	132	.1	35	17	1974	3.27	49	5	ND	1	36	1	2	2	54	.35	.142	12	33	.54	347	.11	3	2.17	.02	.11	1	170
YL 600S 1075E	2	52	19	199	.2	38	22	3989	3.84	56	5	ND	1	35	1	2	2	57	.41	.141	14	34	.50	393	.09	5	2.20	.02	.12	1	55
YL 600S 1100E	1	33	17	123	.3	27	16	2597	2.98	51	5	ND	1	32	1	2	2	45	.39	.105	10	25	.41	263	.07	3	1.74	.02	.13	1	95
YL 600S 1150E	2	56	14	133	.5	40	19	1970	3.55	66	5	ND	1	36	1	2	2	57	.39	.118	13	39	.61	361	.09	9	2.03	.02	.17	1	23
YL 600S 1175E	1	74	25	157	.3	41	23	2345	4.08	137	5	ND	1	34	1	2	2	64	.38	.159	15	43	.72	397	.08	4	2.23	.02	.19	1	315
YL 600S 1200E	2	73	23	160	.5	42	23	2329	4.04	132	5	ND	1	40	1	2	2	63	.47	.176	14	42	.74	395	.07	2	2.14	.01	.22	1	70
YL 600S 1225E	1	75	22	149	.6	42	23	2328	4.07	138	5	ND	1	34	1	2	2	64	.40	.157	15	43	.75	367	.07	8	2.19	.01	.21	1	54
YL 600S 1250E	1	61	20	120	.3	38	19	1737	3.62	109	5	ND	1	36	1	2	2	57	.40	.101	13	38	.63	318	.07	6	1.92	.01	.18	1	50
YL 600S 1275E	2	72	25	160	.3	46	23	2172	4.39	161	5	ND	1	33	1	2	2	65	.33	.122	18	43	.73	353	.08	6	2.17	.01	.21	2	55
YL 600S 1300E	2	65	15	146	.5	54	20	1402	4.10	84	5	ND	1	28	1	2	2	66	.30	.096	17	46	.70	347	.09	2	2.14	.02	.18	1	110
YL 600S 1325E	1	57	12	127	.1	43	19	1848	3.73	64	5	ND	1	25	1	2	2	62	.25	.112	14	41	.63	345	.10	2	2.12	.02	.16	1	36
YL 600S 1350E	2	51	16	115	.3	38	18	1694	3.24	58	5	ND	1	23	1	2	2	53	.24	.103	13	35	.57	314	.08	7	1.91	.02	.16	1	80
YL 600S 1375E	1	69	21	137	.2	47	23	1838	4.04	58	5	ND	1	27	1	2	2	74	.48	.133	13	60	1.01	324	.11	6	2.31	.02	.29	1	54
YL 600S 1400E	1	71	22	138	.2	45	23	1899	4.02	56	5	ND	1	29	1	2	2	74	.49	.135	14	61	1.02	346	.11	5	2.36	.02	.29	1	38
YL 600S 1425E	2	76	13	146	.4	52	25	2012	4.24	61	5	ND	1	33	1	2	2	77	.57	.145	13	63	1.09	380	.11	4	2.48	.02	.32	1	44
YL 600S 1450E	2	54	31	286	.8	44	21	3191	3.80	52	5	ND	1	46	2	2	2	53	.63	.232	15	31	.59	366	.10	7	2.60	.02	.22	1	49
YL 600S 1475E	2	88	25	411	.4	71	31	3712	5.30	68	5	ND	1	32	2	2	2	89	.47	.156	16	74	1.30	341	.14	3	2.94	.02	.39	1	50
YL 600S 1500E	1	106	18	220	.7	89	35	2350	6.26	54	5	ND	1	24	1	2	2	132	.49	.113	12	129	2.33	336	.22	4	3.52	.02	1.05	1	56
YL 600S 1525E	2	54	16	116	.3	41	19	1917	3.70	61	5	ND	1	40	1	2	2	63	.41	.092	14	41	.64	370	.10	3	2.04	.02	.18	1	43
YL 600S 1550E	2	54	13	108	.3	42	18	1411	3.69	70	5	ND	1	21	1	2	2	60	.19	.071	14	41	.63	265	.08	5	1.95	.01	.14	1	52
YL 600S 1575E	2	58	18	106	.2	40	17	1292	3.90	62	5	ND	1	17	1	2	2	65	.20	.081	14	42	.62	236	.10	5	2.14	.01	.12	1	57
YL 600S 1600E	2	64	19	122	.6	46	19	1556	4.07	74	5	ND	1	28	1	2	2	69	.32	.115	15	49	.74	380	.09	2	2.15	.01	.18	1	335
YL 600S 1625E	2	64	28	128	.3	44	20	1303	4.29	87	5	ND	1	24	1	2	2	67	.32	.070	15	46	.66	293	.08	2	2.24	.01	.15	1	70
YL 600S 1650E	2	47	19	103	.3	42	17	961	4.03	65	5	ND	1	19	1	2	2	70	.27	.058	12	46	.69	260	.11	3	2.15	.01	.12	1	65
YL 600S 1675E	2	51	26	150	.6	40	17	1115	3.95	93	5	ND	1	21	1	2	2	66	.26	.065	13	40	.61	238	.10	4	2.16	.02	.14	1	55
YL 600S 1700E	2	43	16	121	.2	34	15	1208	3.56	50	5	ND	1	17	1	2	2	62	.15	.074	12	37	.55	217	.11	3	2.27	.01	.08	1	32
YL 600S 1725E	2	49	60	223	.8	38	18	2350	3.97	258	5	ND	2	19	1	2	2	57	.15	.084	17	35	.51	273	.08	3	2.11	.01	.10	1	46
YL 600S 1750E	2	53	32	163	.4	42	17	1809	4.03	140	5	ND	1	18	1	2	2	64	.21	.093	15	41	.61	265	.09	3	2.21	.01	.12	1	50
YL 600S 1775E	2	72	32	237	.9	85	21	1426	4.38	95	5	ND	1	27	2	2	2	90	.45	.118	17	91	.93	394	.10	4	2.49	.02	.21	1	50
YL 600S 1800E	2	58	40	252	1.1	48	19	1731	4.08	332	5	ND	1	19	1	2	2	64	.20	.100	15	40	.60	253	.09	2	2.25	.01	.11	1	54
YL 600S 1825E	2	52	46	189	.9	41	16	1636	3.77	237	5	ND	1	23	1	2	2	56	.23	.101	16	36	.51	235	.06	4	1.85	.01	.11	1	165
STD C/AU 0.5	20	54	39	129	7.1	66	30	1082	3.93	38	20	8	33	48	17	17	21	62	.48	.101	36	58	.88	177	.08	38	1.72	.06	.13	14	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 600S 1850E	2	45	46	196	.8	41	16	2123	3.53	266	5	ND	1	20	1	2	2	54	.19	.111	12	32	.41	217	.07	4	1.70	.01	.09	1	60
YL 600S 1875E	2	45	36	166	.7	41	15	1232	3.46	145	5	ND	1	17	1	2	2	60	.13	.094	11	38	.42	205	.06	4	1.68	.01	.08	1	29
YL 600S 1900E	2	41	38	139	1.3	35	14	1376	3.35	121	5	ND	1	16	1	2	2	58	.11	.083	11	34	.43	190	.09	4	1.93	.01	.08	1	21
YL 600S 1925E	2	37	33	175	.8	37	12	1625	3.22	109	5	ND	1	22	1	2	2	53	.22	.098	10	32	.42	212	.07	5	1.65	.01	.09	1	75
YL 600S 1950E	2	47	29	181	.2	43	15	1086	3.72	150	5	ND	1	15	1	2	2	58	.12	.110	14	37	.54	176	.08	4	1.87	.01	.10	1	24
YL 600S 1975E	2	35	35	106	.8	26	11	693	3.01	119	5	ND	1	14	1	2	2	50	.12	.086	11	29	.34	145	.06	8	1.60	.01	.07	2	80
YL 600S 2000E	2	35	17	100	.6	28	11	953	2.85	62	5	ND	1	11	1	2	2	48	.09	.096	10	29	.32	148	.06	4	1.66	.01	.07	1	22
YL 650S 0E	2	45	13	185	.5	57	19	1398	3.82	218	5	ND	1	24	1	2	2	73	.19	.062	12	42	.63	268	.10	4	2.11	.01	.12	1	6
YL 650S 25E	3	52	17	234	.6	87	20	1306	3.98	153	5	ND	1	20	1	3	2	106	.18	.076	13	65	.91	296	.11	3	2.47	.01	.17	1	4
YL 650S 50E	4	46	14	166	.4	44	17	1821	3.37	53	5	ND	1	33	2	2	2	98	.32	.168	10	56	.60	519	.10	5	2.02	.02	.10	1	2
YL 650S 75E	3	47	10	117	.5	26	13	1433	3.02	78	5	ND	1	26	1	2	2	76	.17	.158	11	37	.49	310	.15	3	2.45	.02	.09	1	3
YL 650S 100E	2	78	15	152	.2	43	27	2910	4.32	101	5	ND	1	39	1	2	2	79	.22	.139	15	29	.51	329	.15	3	2.87	.02	.13	1	2
YL 650S 125E	3	79	16	210	1.0	57	24	1652	4.55	298	5	ND	3	44	2	2	2	80	.28	.117	21	38	.66	333	.14	2	2.45	.02	.21	1	7
YL 650S 150E	3	82	29	250	1.0	63	28	1994	6.48	627	5	ND	2	61	1	2	2	108	.33	.187	19	57	.81	622	.13	3	2.72	.02	.18	1	21
YL 650S 175E	2	70	16	212	.4	58	19	1582	3.48	211	5	ND	1	64	1	2	2	69	.51	.155	12	42	.63	613	.09	5	2.21	.02	.17	1	9
YL 650S 200E	1	89	20	308	.5	100	29	2095	4.40	207	5	ND	1	71	2	2	2	89	.47	.155	16	67	.84	734	.13	3	2.85	.02	.23	2	5
YL 650S 225E	2	69	18	195	.3	66	24	1598	4.20	244	5	ND	1	59	1	2	2	88	.38	.171	12	75	.95	722	.13	3	2.66	.02	.19	1	12
YL 650S 250E	2	135	15	184	.3	58	24	1714	4.11	197	5	ND	1	69	1	2	2	81	.42	.157	14	56	.75	703	.12	3	2.39	.02	.19	1	70
YL 650S 275E	3	86	15	184	.2	66	27	1771	4.52	189	5	ND	2	42	1	2	2	89	.20	.143	15	61	.81	517	.14	6	2.64	.01	.16	2	20
YL 650S 300E	1	94	36	307	.5	109	33	2044	4.59	200	5	ND	1	58	2	2	2	98	.58	.198	11	88	1.13	702	.15	8	3.09	.03	.27	1	75
YL 650S 325E	2	78	26	228	.4	73	28	2056	4.29	213	5	ND	1	61	1	2	2	89	.52	.153	12	74	1.05	574	.12	5	2.92	.02	.23	1	24
YL 650S 350E	2	56	31	312	.1	51	23	2332	2.60	64	5	ND	1	99	3	2	2	53	1.55	.286	8	41	.65	743	.09	6	1.99	.02	.22	1	5
YL 650S 375E	2	59	18	192	.3	49	20	2158	3.07	218	5	ND	1	52	1	2	2	59	.58	.191	10	38	.59	737	.08	8	1.94	.02	.13	1	24
YL 650S 400E	2	74	13	186	.3	56	22	2142	3.02	194	5	ND	1	68	2	2	2	56	.91	.218	11	39	.67	739	.05	6	1.86	.02	.17	1	31
YL 650S 425E	2	63	14	124	.3	34	17	1323	3.62	379	5	ND	1	53	1	2	2	70	.48	.174	10	44	.81	567	.06	4	2.08	.01	.25	1	635
YL 650S 450E	2	78	9	157	.3	39	25	1543	4.27	237	5	ND	1	54	1	2	2	85	.48	.171	10	60	1.02	607	.07	5	2.20	.02	.26	1	50
YL 650S 475E	1	79	11	156	.1	51	28	1755	4.58	129	5	ND	1	41	1	2	2	94	.37	.145	11	68	1.13	598	.11	3	2.30	.01	.22	1	75
YL 650S 500E	2	56	15	169	.3	57	22	2259	3.77	138	5	ND	1	29	1	2	2	70	.30	.107	10	52	.75	504	.08	3	1.94	.01	.14	1	13
YL 650S 525E	2	65	13	142	.1	49	20	1809	4.14	114	5	ND	1	28	1	2	2	69	.25	.110	14	47	.66	448	.09	5	1.69	.01	.19	1	12
YL 650S 550E	2	48	21	167	.1	32	18	1859	3.35	91	5	ND	1	33	1	2	2	59	.33	.191	11	39	.57	454	.09	6	1.96	.02	.13	1	8
YL 650S 575E	2	56	14	162	.2	47	21	1796	3.66	106	5	ND	1	27	1	2	2	72	.27	.108	12	48	.67	395	.10	4	2.12	.02	.12	1	12
YL 650S 600E	1	34	10	143	.3	28	15	2184	3.28	123	5	ND	1	18	1	2	2	60	.20	.149	8	31	.36	267	.08	6	1.94	.02	.09	1	24
YL 650S 625E	1	57	19	144	.2	40	19	1248	4.14	131	5	ND	1	18	1	2	2	75	.23	.096	13	49	.61	337	.07	3	2.05	.01	.12	1	27
YL 650S 650E	1	38	9	115	.2	34	14	1285	3.18	62	5	ND	1	18	1	2	2	60	.18	.108	11	37	.49	275	.11	4	1.93	.01	.09	1	85
YL 650S 675E	1	37	9	114	.3	35	14	1029	3.27	59	5	ND	1	18	1	2	2	64	.21	.138	11	38	.52	249	.11	5	2.11	.02	.07	1	5
YL 650S 700E	2	39	12	107	.1	35	15	1241	3.35	64	5	ND	1	18	1	2	2	68	.16	.089	12	41	.55	255	.12	6	2.10	.01	.09	1	9
STD C/AU 0.5	22	58	38	138	7.2	73	31	1161	3.96	42	19	8	35	51	19	16	20	67	.48	.111	40	61	.88	191	.09	38	1.72	.07	.13	15	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 650S 725E	1	41	15	115	.3	32	15	1538	3.06	133	5	ND	1	29	1	2	2	54	.36	.095	10	31	.47	302	.10	7	1.93	.02	.06	2	32
YL 650S 750E	1	57	23	175	.4	41	18	1358	3.55	372	5	ND	1	23	1	2	2	57	.21	.083	11	36	.52	256	.11	3	2.46	.02	.08	1	60
YL 650S 775E	1	34	15	114	.5	28	14	1531	3.01	137	5	ND	1	17	1	2	2	54	.16	.093	9	28	.39	202	.10	4	2.01	.02	.08	1	34
YL 650S 800E	1	40	31	121	.5	34	15	1026	3.30	148	5	ND	1	17	1	2	2	58	.16	.088	11	31	.43	209	.10	5	2.00	.01	.08	1	55
YL 650S 825E	2	53	29	161	.5	41	18	1640	3.53	165	5	ND	1	15	1	2	2	59	.16	.099	11	33	.44	211	.10	6	2.17	.02	.07	1	48
YL 650S 850E	3	74	54	283	1.3	82	32	3921	5.21	296	5	ND	1	17	2	3	2	56	.16	.104	14	29	.37	252	.10	8	2.40	.02	.08	1	130
YL 650S 875E	2	54	33	170	.7	41	19	1508	3.73	119	5	ND	1	21	1	2	2	60	.20	.109	12	32	.41	291	.08	4	2.06	.02	.09	1	115
YL 650S 900E	2	47	31	183	.8	35	18	2118	3.41	102	5	ND	1	26	1	2	2	53	.23	.172	10	27	.34	328	.08	8	2.00	.02	.08	1	23
YL 650S 925E	2	39	22	153	.5	30	14	1772	3.08	73	5	ND	1	24	1	2	2	53	.23	.137	8	26	.35	296	.08	4	2.10	.02	.07	1	17
YL 650S 950E	2	43	20	141	.6	33	16	1524	3.44	98	5	ND	1	19	1	2	4	58	.16	.137	10	27	.39	250	.09	6	2.21	.02	.10	1	30
YL 650S 975E	1	31	11	114	.6	26	13	1193	2.97	44	5	ND	1	16	1	2	2	52	.17	.136	9	26	.36	189	.09	3	2.15	.02	.10	1	26
YL 650S 1000E	2	32	11	111	.4	23	13	1124	3.19	45	5	ND	1	14	1	2	2	55	.11	.114	8	26	.36	171	.11	5	2.25	.02	.06	1	13
YL 700S 0E	3	84	20	196	.4	86	26	2516	3.87	46	5	ND	1	28	2	2	2	93	.23	.119	14	61	.83	445	.13	8	2.63	.02	.13	1	2
YL 700S 25E	2	50	19	124	.2	30	13	1886	3.18	41	5	ND	1	28	1	2	2	63	.24	.098	14	37	.58	341	.11	9	2.01	.02	.17	1	1
YL 700S 50E	2	50	25	123	.2	20	17	2857	4.46	40	5	ND	1	37	1	2	2	50	.28	.177	17	30	.50	324	.11	8	2.26	.02	.20	1	3
YL 700S 75E	2	59	18	201	.1	46	20	4325	3.46	40	5	ND	1	60	2	2	2	57	.44	.148	11	28	.46	416	.11	9	2.44	.02	.15	1	1
YL 700S 100E	3	59	15	236	.1	80	22	2165	3.39	84	5	ND	1	115	3	2	4	93	.91	.169	10	95	1.01	716	.10	11	2.48	.02	.29	1	1
YL 700S 125E	4	102	20	182	.8	49	25	2147	5.49	192	5	ND	2	51	1	3	2	87	.33	.155	17	44	.73	358	.14	7	2.85	.02	.20	1	3
YL 700S 150E	3	87	21	224	.6	70	21	1646	5.50	537	5	ND	2	72	2	3	2	96	.39	.135	17	61	.91	544	.15	6	2.94	.02	.27	1	10
YL 700S 175E	3	108	20	241	.9	82	31	1954	5.77	338	5	ND	1	57	2	2	2	105	.34	.194	17	72	.89	590	.16	7	3.29	.02	.21	1	13
YL 700S 200E	1	89	23	336	.5	108	30	2257	5.22	178	5	ND	1	89	2	2	2	90	.56	.207	15	64	.97	674	.14	8	3.03	.02	.30	1	23
YL 700S 225E	1	94	19	272	.6	91	25	1832	5.26	163	5	ND	1	81	1	2	2	91	.57	.181	15	80	1.03	649	.19	5	2.97	.02	.41	1	7
YL 700S 250E	2	78	18	231	.4	95	27	2040	4.82	184	5	ND	2	56	1	2	2	78	.33	.126	14	61	.89	578	.17	11	2.90	.02	.19	1	9
YL 700S 275E	3	129	32	301	.5	104	35	2118	5.82	704	5	ND	2	77	2	2	2	86	.73	.225	15	59	.95	667	.15	13	3.00	.02	.22	1	31
YL 700S 300E	2	107	26	291	.4	91	30	2449	4.72	337	5	ND	1	85	2	2	2	83	.85	.207	14	63	.95	742	.13	11	2.96	.03	.25	1	50
YL 700S 325E	2	116	34	329	.5	99	32	1910	5.35	165	5	ND	1	65	3	2	2	120	.80	.219	16	87	1.46	807	.17	11	3.42	.03	.52	1	11
YL 700S 350E	1	52	25	222	.2	35	16	1932	1.97	47	5	ND	1	80	2	2	2	35	1.44	.200	8	28	.44	708	.05	10	1.49	.02	.15	1	4
YL 700S 375E	2	63	19	178	.3	51	21	1862	3.32	207	5	ND	1	60	2	2	2	63	.64	.184	12	42	.68	645	.08	8	2.11	.02	.18	1	20
YL 700S 400E	2	57	16	165	.2	43	20	2233	3.15	127	5	ND	1	50	2	2	2	56	.61	.151	12	42	.66	598	.05	6	1.68	.01	.20	1	9
YL 700S 425E	2	61	14	153	.2	41	23	2026	3.64	264	5	ND	1	48	2	2	2	68	.48	.165	13	44	.76	528	.07	8	2.18	.02	.17	1	22
YL 700S 450E	2	72	20	154	.2	38	24	1730	4.11	248	5	ND	1	43	2	2	2	75	.41	.165	13	52	.94	558	.08	9	2.24	.01	.22	1	155
YL 700S 475E	2	68	20	156	.2	47	23	1871	3.96	110	5	ND	1	54	2	2	3	74	.58	.158	12	52	.93	593	.10	6	2.13	.01	.18	1	15
YL 700S 500E	2	57	20	199	.3	49	22	2662	3.82	109	5	ND	1	26	1	2	3	66	.29	.154	13	45	.67	487	.09	6	1.94	.01	.14	1	27
YL 700S 525E	2	63	18	172	.3	47	21	2199	4.45	126	5	ND	1	28	1	2	2	69	.27	.125	16	45	.67	468	.08	4	1.83	.01	.19	1	17
YL 700S 550E	2	52	10	161	.1	39	18	1512	3.88	120	5	ND	1	23	1	2	2	66	.23	.132	15	40	.59	401	.09	2	2.16	.02	.12	1	44
YL 700S 575E	2	47	11	137	.2	38	17	1513	3.44	97	5	ND	1	23	1	2	2	62	.21	.142	11	41	.58	337	.10	4	2.11	.02	.10	1	12
STD C/AU 0.5	21	57	37	133	7.1	70	30	1110	3.98	40	19	8	34	49	18	17	20	64	.48	.109	38	59	.88	184	.08	40	1.70	.07	.14	15	485

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 700S 600E	1	47	12	155	.3	39	16	1732	3.92	157	5	ND	1	18	1	2	2	69	.19	.107	12	39	.49	301	.10	5	2.24	.02	.09	1	70
YL 700S 625E	2	77	11	158	.6	47	20	1367	4.61	126	5	ND	1	22	1	2	2	77	.31	.110	17	55	.76	433	.08	6	2.18	.01	.17	1	32
YL 700S 650E	2	39	10	118	.3	40	14	1088	3.43	51	5	ND	1	20	1	2	2	62	.21	.112	12	40	.57	260	.10	7	2.15	.01	.08	1	19
YL 700S 675E	1	33	13	119	.3	33	13	1425	3.17	62	5	ND	1	21	1	2	2	57	.26	.155	11	34	.47	230	.10	7	2.19	.02	.07	1	10
YL 700S 700E	1	33	10	126	.4	33	13	1913	3.12	54	5	ND	1	19	1	2	2	58	.20	.162	11	34	.45	257	.10	8	2.02	.02	.07	1	16
YL 700S 725E	1	37	10	115	.5	29	12	878	3.28	174	5	ND	1	15	1	2	3	57	.19	.089	8	31	.42	174	.10	5	2.19	.02	.08	1	19
YL 700S 750E	1	31	16	116	.6	24	12	927	2.93	114	5	ND	1	15	1	2	2	53	.18	.099	9	29	.39	170	.09	2	1.88	.02	.06	1	21
YL 700S 775E	1	29	19	98	.3	24	10	727	2.51	75	5	ND	1	13	1	2	2	44	.14	.111	9	25	.33	161	.09	7	2.01	.02	.05	1	15
YL 700S 800E	1	38	19	118	.5	34	13	989	3.23	72	5	ND	1	26	1	2	2	60	.41	.103	11	40	.56	241	.08	6	1.77	.02	.11	1	18
YL 700S 825E	2	59	27	160	.5	43	17	2085	3.60	135	5	ND	1	22	1	2	2	60	.26	.123	10	38	.54	305	.07	5	1.74	.01	.10	1	65
YL 700S 850E	2	59	29	190	.7	61	21	1909	4.22	174	5	ND	1	19	1	2	2	65	.21	.076	13	48	.64	251	.09	9	2.19	.01	.10	1	46
YL 700S 875E	2	53	31	159	.5	53	15	1337	3.39	103	5	ND	1	26	1	2	2	54	.24	.131	11	36	.40	319	.08	6	2.52	.02	.08	1	30
YL 700S 900E	2	48	31	171	.9	38	16	1665	3.49	94	5	ND	1	26	1	2	2	58	.28	.134	9	31	.41	302	.07	3	2.04	.02	.09	1	50
YL 700S 925E	2	46	20	162	.8	34	16	1371	3.50	90	5	ND	1	20	1	2	2	61	.20	.140	9	31	.42	247	.07	5	2.05	.01	.09	1	55
YL 700S 950E	2	37	17	117	.7	26	12	1252	2.69	83	5	ND	1	24	1	2	2	47	.30	.126	8	24	.34	249	.05	6	1.69	.01	.06	1	25
YL 700S 975E	2	36	15	125	.7	30	13	1454	3.11	61	5	ND	1	24	1	2	2	54	.37	.131	8	32	.43	231	.08	7	2.24	.02	.13	1	50
YL 750S 0E	3	49	12	137	.2	38	15	2120	3.25	27	5	ND	1	50	1	2	2	65	.36	.109	14	36	.60	364	.11	2	2.34	.02	.18	2	2
YL 750S 25E	5	79	11	311	.4	89	23	2098	4.02	45	5	ND	1	92	2	2	2	138	.70	.142	15	111	1.14	700	.11	8	2.86	.01	.34	1	23
YL 750S 50E	3	81	15	166	.2	47	21	2474	4.14	38	5	ND	1	96	1	2	2	90	.72	.129	19	57	.91	510	.12	7	2.89	.02	.29	1	3
YL 750S 75E	2	60	15	184	.2	52	21	3159	3.41	50	5	ND	1	64	2	2	2	69	.47	.104	15	42	.68	486	.11	8	2.60	.02	.22	1	1
YL 750S 100E	3	91	15	174	.6	69	27	2217	4.62	69	5	ND	1	53	1	2	2	85	.30	.136	17	66	.84	307	.15	7	3.33	.02	.19	1	3
YL 750S 125E	3	121	19	200	.6	94	40	2671	4.63	63	5	ND	1	57	1	2	2	87	.31	.134	16	77	.95	392	.15	3	3.13	.01	.22	1	4
YL 750S 150E	4	122	13	209	.4	90	37	4076	5.20	77	5	ND	1	68	2	2	2	86	.46	.126	18	76	.92	449	.17	5	3.05	.02	.23	1	5
YL 750S 175E	2	103	9	151	.4	53	27	1666	4.55	52	5	ND	1	139	1	2	2	97	.72	.101	14	46	.92	422	.13	5	2.87	.02	.37	1	11
YL 750S 200E	1	62	6	134	.2	40	19	1421	4.12	39	5	ND	1	138	1	2	2	116	.90	.135	11	50	1.03	478	.12	6	2.64	.02	.37	1	3
YL 750S 225E	1	47	6	119	.1	33	15	1355	3.24	29	5	ND	1	62	1	2	2	76	.62	.112	10	30	.60	311	.14	2	2.84	.03	.22	1	1
YL 750S 250E	1	63	13	351	.3	50	24	3908	2.90	37	6	ND	1	113	3	2	2	51	2.20	.306	9	34	.57	1075	.07	10	1.88	.03	.21	1	10
YL 750S 275E	1	59	12	315	.1	99	19	1049	3.21	31	5	ND	1	41	1	2	2	60	.71	.319	10	34	.66	319	.17	5	2.28	.05	.10	1	9
YL 750S 300E	2	55	11	196	.3	49	17	1294	2.83	120	5	ND	1	54	2	2	3	56	.70	.157	9	41	.68	384	.06	4	1.82	.02	.18	1	34
YL 750S 325E	1	57	16	212	.4	51	19	1648	2.99	101	5	ND	1	66	2	2	2	55	.82	.171	11	42	.70	530	.06	4	2.10	.02	.19	1	17
YL 750S 350E	1	54	10	147	.1	50	20	1971	3.49	67	5	ND	1	47	1	2	2	67	.54	.138	12	47	.80	547	.10	5	2.27	.02	.21	1	6
YL 750S 375E	2	62	13	151	.3	51	21	2043	3.64	112	5	ND	1	42	1	2	2	73	.42	.118	13	51	.80	514	.10	3	2.41	.02	.15	1	9
YL 750S 400E	2	57	19	173	.2	48	20	2411	3.40	74	5	ND	1	60	2	2	2	66	.63	.148	12	49	.77	633	.08	3	2.13	.02	.18	1	6
YL 750S 425E	2	48	11	135	.3	49	19	1970	3.35	70	5	ND	1	33	1	2	5	64	.31	.131	11	45	.71	393	.09	6	2.11	.01	.18	1	3
YL 750S 450E	2	40	15	156	.3	42	17	1635	3.19	45	5	ND	1	31	1	2	2	58	.31	.146	12	38	.62	335	.09	6	2.13	.02	.10	1	5
YL 750S 475E	2	44	14	135	.2	47	17	1348	3.58	54	5	ND	1	20	1	2	2	67	.21	.107	12	48	.73	308	.10	5	2.07	.01	.12	1	7
STD C/AU 0.5	20	57	37	133	7.3	68	30	1121	3.96	37	18	8	34	49	17	17	21	64	.48	.105	36	59	.88	183	.08	37	1.72	.07	.13	14	505

SHANGRI-LA MINERALS PROJECT - YUNIMAN FILE # 86-1508

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au† PPB
YL 750S 500E	1	51	14	140	.3	58	20	1624	4.11	69	5	ND	1	47	1	2	2	76	.44	.092	15	58	.88	405	.10	3	2.12	.01	.14	1	16
YL 750S 525E	2	65	15	125	.5	64	22	1593	4.23	84	5	ND	1	31	1	2	2	80	.31	.085	15	58	.88	428	.12	5	2.25	.01	.19	1	26
YL 750S 550E	2	55	13	163	.2	74	20	2110	4.89	179	5	ND	1	27	1	2	2	82	.30	.098	12	53	.74	426	.08	5	2.11	.01	.14	1	41
YL 750S 575E	1	36	10	134	.8	33	13	1267	3.39	92	5	ND	1	18	1	2	2	60	.20	.120	10	33	.42	251	.09	6	2.02	.02	.08	1	11
YL 750S 600E	2	76	15	165	.6	60	23	2125	4.93	272	5	ND	1	27	1	2	2	73	.35	.081	16	52	.64	457	.06	6	2.07	.01	.14	1	40
YL 750S 625E	1	33	10	141	.9	34	13	1029	3.42	124	13	ND	2	24	1	2	2	61	.34	.088	9	37	.48	287	.07	6	1.98	.02	.09	2	45
YL 750S 650E	2	77	13	144	.4	52	19	1203	4.67	117	5	ND	3	17	1	2	2	75	.19	.093	17	53	.72	410	.09	4	1.91	.01	.19	1	16
YL 750S 675E	1	45	17	123	.8	42	13	443	3.29	62	5	ND	2	17	1	2	2	67	.20	.085	12	51	.65	273	.11	3	2.11	.02	.08	1	32
YL 750S 700E	2	30	18	115	.4	33	12	677	3.32	47	5	ND	1	25	1	2	2	62	.38	.050	12	42	.60	194	.10	3	2.33	.02	.06	1	19
YL 750S 725E	3	46	12	118	.7	43	11	536	3.44	70	5	ND	1	28	1	2	2	65	.53	.055	12	46	.70	252	.12	3	2.55	.02	.08	1	17
YL 750S 750E	3	12	14	49	.6	14	4	265	1.16	256	5	ND	1	28	1	2	2	25	.62	.091	4	8	.16	84	.21	4	2.70	.04	.03	1	2
YL 750S 775E	33	17	14	29	.4	16	8	13440	1.92	493	5	ND	1	28	1	2	5	48	.77	.105	7	10	.16	255	.09	4	1.96	.04	.02	2	1
YL 750S 800E	17	46	10	23	1.5	19	7	5885	1.91	75	5	ND	1	31	1	2	2	38	.83	.127	16	15	.15	144	.06	2	2.71	.04	.03	2	9
YL 750S 825E	1	31	12	98	.7	35	11	562	2.89	164	5	ND	1	30	1	2	3	63	.64	.062	11	46	.69	222	.13	5	2.30	.03	.06	1	1
YL 750S 850E	4	24	8	76	.7	17	6	270	1.21	487	5	ND	1	25	1	2	2	45	.67	.125	8	25	.35	72	.07	3	1.41	.04	.04	1	8
YL 750S 875E	23	33	6	64	.8	27	20	6435	4.94	2726	5	ND	1	40	2	2	2	73	1.39	.158	9	17	.19	160	.05	3	1.95	.03	.03	1	4
YL 750S 900E	2	35	10	25	2.4	16	4	315	1.71	45	5	ND	1	38	1	2	2	26	.89	.109	11	19	.17	112	.07	3	2.65	.03	.03	1	5
YL 750S 925E	1	26	12	84	.7	21	8	383	2.99	31	5	ND	1	14	1	2	2	61	.19	.086	9	36	.45	144	.08	3	1.94	.02	.06	1	13
YL 750S 950E	2	43	11	117	.9	39	11	792	3.03	49	5	ND	1	33	1	2	3	60	.66	.064	13	40	.62	209	.11	4	2.35	.03	.07	1	9
YL 750S 975E	1	26	11	72	.7	19	7	203	3.06	32	5	ND	1	13	1	2	2	64	.15	.088	10	35	.42	124	.12	5	1.97	.02	.05	1	3
YL 750S 1000E	2	79	15	82	2.0	34	13	1371	1.93	173	5	ND	1	79	2	2	2	32	2.44	.122	26	27	.44	214	.03	6	1.54	.02	.07	1	1
YL 800S 0E	3	53	13	145	.2	36	17	4539	2.57	39	5	ND	1	76	1	2	2	38	.85	.140	13	21	.40	393	.06	8	1.93	.02	.15	2	1
YL 800S 25E	2	67	8	135	.3	38	17	1940	3.93	43	5	ND	1	61	1	2	2	57	.47	.110	20	36	.77	342	.09	6	2.26	.02	.31	1	9
YL 800S 50E	5	76	22	165	.6	50	15	1627	4.28	41	5	ND	1	66	1	2	2	88	.48	.093	18	51	.90	418	.10	2	2.44	.01	.34	1	6
YL 800S 75E	3	84	17	157	.5	55	19	1775	5.05	39	5	ND	2	70	1	2	2	80	.44	.152	21	58	1.01	438	.14	7	3.12	.02	.42	1	4
YL 800S 100E	3	74	20	201	.5	72	25	2304	4.35	39	5	ND	1	80	1	2	2	96	.53	.151	12	80	1.07	612	.13	7	2.99	.02	.34	1	5
YL 800S 125E	2	49	15	165	.5	35	19	1911	4.01	29	5	ND	1	114	1	2	4	63	.56	.124	11	51	1.03	482	.16	6	2.89	.02	.41	1	1
YL 800S 150E	2	69	9	114	.5	41	15	1088	4.49	28	5	ND	2	84	1	2	2	97	.49	.129	10	88	1.27	594	.23	5	2.85	.02	.42	1	6
YL 800S 175E	2	63	17	180	.3	42	21	1984	4.13	26	5	ND	1	89	1	2	2	90	.53	.129	12	55	1.07	485	.18	7	2.86	.03	.42	2	5
YL 800S 200E	1	49	12	133	.2	37	18	1350	3.99	27	5	ND	1	89	1	2	2	110	.65	.148	10	48	.82	344	.14	6	2.56	.03	.30	1	4
YL 800S 225E	1	32	6	139	.2	23	13	2618	1.89	15	5	ND	1	69	1	2	2	35	.93	.232	4	21	.33	504	.06	7	1.46	.03	.15	1	2
YL 800S 250E	1	37	9	134	.2	39	13	1389	2.93	27	5	ND	1	69	1	2	2	71	.64	.116	6	36	.54	382	.11	7	1.93	.02	.13	1	1
YL 800S 275E	1	29	15	139	.1	31	11	1418	2.24	40	5	ND	1	50	1	2	2	41	.69	.346	7	21	.34	309	.10	8	2.98	.03	.09	1	1
YL 800S 300E	2	56	13	169	.2	50	18	1533	3.46	69	5	ND	1	37	1	2	2	75	.48	.120	10	48	.74	331	.11	4	2.13	.02	.17	1	6
YL 800S 325E	2	60	14	187	.4	54	20	1837	3.70	120	5	ND	1	50	2	2	2	76	.56	.117	11	49	.82	480	.11	4	2.30	.02	.18	1	12
YL 800S 350E	2	51	14	127	.3	46	17	1581	2.98	63	5	ND	1	46	1	2	2	59	.44	.108	9	42	.70	458	.10	5	2.05	.02	.16	1	8
STD C/AU 0.5	21	57	38	131	7.2	69	30	1099	3.94	41	16	8	34	49	16	16	20	63	.48	.103	37	59	.88	182	.08	37	1.72	.07	.13	14	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 800S 375E	2	48	13	135	.1	43	17	1804	3.14	69	5	ND	1	47	1	2	2	64	.49	.138	8	44	.73	464	.11	2	2.13	.02	.17	1	14
YL 800S 400E	2	45	5	130	.1	41	16	1877	3.10	60	5	ND	1	37	1	2	4	63	.39	.125	7	41	.65	447	.11	7	2.07	.02	.14	1	8
YL 800S 425E	2	51	17	141	.1	50	20	1766	3.68	63	5	ND	1	34	1	2	2	71	.33	.129	10	48	.79	424	.12	7	2.34	.02	.15	1	7
YL 800S 450E	2	56	16	132	.1	57	20	1458	3.92	66	5	ND	1	26	1	2	2	76	.27	.092	11	54	.86	372	.12	2	2.24	.02	.16	1	9
YL 800S 475E	2	60	19	159	.2	64	22	1594	4.21	63	5	ND	1	35	1	2	2	80	.39	.114	10	60	.94	452	.13	2	2.28	.02	.22	1	5
YL 800S 500E	2	65	6	146	.3	64	23	1384	4.29	62	5	ND	1	29	1	2	2	82	.28	.086	13	63	.95	448	.13	2	2.33	.02	.23	1	16
YL 800S 525E	2	71	16	148	.1	64	24	1561	4.25	63	5	ND	1	40	1	2	3	85	.44	.127	13	64	.98	496	.13	6	2.33	.02	.28	1	11
YL 800S 550E	2	77	15	224	.9	112	27	3332	5.18	180	5	ND	1	35	1	3	2	83	.43	.120	10	61	.81	712	.08	5	2.19	.01	.19	1	35
YL 800S 575E	2	68	26	163	.6	54	19	1281	4.63	150	5	ND	1	27	1	2	2	84	.44	.089	9	55	.74	373	.09	4	1.93	.02	.13	1	45
YL 800S 600E	2	52	20	152	.8	44	16	898	3.78	108	5	ND	1	27	1	2	3	73	.37	.090	10	51	.72	318	.09	3	2.14	.03	.10	1	32
YL 800S 625E	2	100	16	148	.4	57	25	1557	5.24	156	5	ND	1	22	1	2	2	92	.28	.092	11	63	.93	614	.08	2	2.07	.01	.20	1	38
YL 800S 650E	3	48	21	121	1.0	44	15	816	3.99	67	5	ND	1	28	1	3	2	74	.60	.091	8	56	.79	314	.12	5	2.40	.02	.14	1	53
YL 800S 675E	2	33	8	106	1.0	35	10	543	2.96	36	5	ND	1	33	1	2	2	58	.65	.070	6	40	.55	300	.10	3	2.54	.03	.07	1	6
YL 800S 700E	2	37	12	101	1.0	32	10	568	2.85	39	5	ND	1	26	1	2	4	59	.45	.075	12	36	.47	232	.09	2	2.62	.02	.07	1	6
YL 800S 725E	2	32	12	119	.4	26	11	842	2.74	31	5	ND	1	30	1	2	4	59	.48	.077	6	34	.53	222	.12	4	2.28	.03	.07	1	5
YL 800S 750E	4	67	8	34	2.6	18	7	573	1.33	51	5	ND	1	44	1	4	2	31	1.64	.181	15	17	.23	151	.03	3	1.66	.02	.04	2	10
YL 800S 775E	3	69	13	77	2.1	30	12	1000	2.55	183	5	ND	1	44	1	2	2	49	1.24	.116	26	33	.41	201	.07	2	2.37	.02	.06	1	10
YL 800S 800E	1	28	8	38	1.0	13	5	431	1.09	181	7	ND	1	66	1	2	2	25	3.48	.137	6	11	.15	125	.03	7	1.24	.04	.04	2	2
YL 800S 825E	2	33	8	40	1.6	14	7	505	1.50	46	7	ND	1	59	1	2	2	29	2.60	.114	7	16	.23	183	.04	3	1.18	.02	.03	3	5
YL 800S 850E	2	62	10	73	3.1	28	10	666	2.32	199	5	ND	1	39	1	2	2	48	1.03	.132	25	30	.42	160	.06	5	2.38	.03	.06	1	11
YL 800S 875E	4	86	19	198	.8	52	20	570	3.45	1099	7	ND	1	38	1	2	2	73	.89	.119	13	60	.85	189	.10	4	2.45	.03	.14	1	39
YL 800S 900E	1	30	6	66	1.5	19	8	794	2.37	329	5	ND	1	51	1	2	2	44	1.88	.131	8	26	.41	123	.06	5	1.82	.03	.05	1	9
YL 800S 925E	1	23	11	118	.2	29	12	825	3.11	45	5	ND	1	19	1	3	2	63	.27	.078	6	37	.54	144	.14	3	2.03	.02	.08	1	3
YL 800S 950E	1	41	12	102	.4	36	14	657	3.42	64	5	ND	1	21	1	2	2	69	.27	.090	8	42	.58	177	.13	2	2.20	.02	.07	1	7
YL 800S 975E	2	80	16	112	1.8	51	14	851	3.28	81	5	ND	1	38	1	2	3	65	.89	.088	18	47	.57	205	.09	2	2.53	.03	.09	1	18
YL 800S 1000E	2	64	16	118	1.1	47	15	628	3.29	208	5	ND	1	30	1	2	2	69	.58	.074	15	47	.66	163	.10	2	2.49	.03	.09	1	8
YL 800S 1025E	2	62	13	85	1.8	34	15	1096	3.16	68	5	ND	1	33	1	2	2	66	.54	.103	26	46	.64	190	.07	3	2.29	.02	.09	1	18
YL 800S 1050E	1	45	12	87	1.1	25	9	495	2.11	110	5	ND	1	42	1	2	2	43	.67	.068	16	30	.42	164	.09	2	1.75	.02	.06	1	6
YL 800S 1075E	4	63	13	78	.9	29	10	1853	2.22	634	5	ND	1	52	1	2	2	43	1.58	.139	11	26	.39	133	.04	2	1.56	.03	.06	1	9
YL 800S 1100E	3	94	12	90	1.0	45	12	471	2.50	208	5	ND	1	31	1	2	2	55	.61	.091	26	40	.62	172	.10	3	2.52	.03	.07	1	18
YL 800S 1125E	7	68	18	105	1.4	40	13	4635	2.27	910	5	ND	1	49	1	2	2	40	1.44	.151	12	24	.32	168	.06	2	2.24	.03	.06	1	8
YL 800S 1150E	5	60	6	34	1.8	23	8	2014	1.60	259	5	ND	1	43	1	2	2	33	1.50	.184	11	12	.17	99	.03	3	1.74	.03	.04	2	6
YL 800S 1175E	1	47	10	74	1.4	27	9	616	2.22	36	5	ND	1	40	1	2	2	44	1.40	.097	14	27	.40	130	.07	2	1.96	.03	.06	1	6
YL 800S 1200E	1	44	11	83	1.5	28	10	778	2.34	37	5	ND	1	44	1	2	2	46	1.46	.097	10	32	.41	202	.06	5	1.76	.02	.07	1	11
YL 850S 0E	28	201	56	163	3.6	45	19	981	8.28	288	5	ND	3	16	1	9	3	160	.10	.241	32	96	.72	454	.06	2	2.49	.01	.27	1	49
YL 850S 25E	6	125	29	269	.8	80	29	2065	5.42	118	5	ND	3	36	1	2	2	96	.19	.142	20	57	.78	736	.11	3	2.80	.02	.21	1	7
STD C/AU 0.5	21	57	40	136	7.1	68	31	1139	3.94	39	16	8	34	49	17	17	18	65	.48	.112	37	60	.88	185	.08	38	1.72	.07	.14	15	515

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 850S 50E	6	133	28	213	1.0	62	21	952	7.44	137	8	ND	6	59	1	3	9	103	.14	.148	11	60	.82	561	.10	4	2.99	.01	.19	1	21
YL 850S 75E	8	106	31	162	1.0	37	18	1701	7.32	124	5	ND	4	58	1	3	5	105	.31	.265	7	47	.66	525	.13	2	2.58	.02	.25	1	32
YL 850S 100E	5	108	17	202	.6	82	29	1964	5.38	73	5	ND	2	38	1	3	3	87	.24	.204	7	65	.89	421	.14	2	3.03	.02	.14	1	12
YL 850S 125E	5	95	17	212	.4	72	37	2357	4.65	47	6	ND	1	64	1	2	2	72	.38	.153	4	43	.75	335	.11	3	2.77	.02	.14	1	7
YL 850S 150E	3	73	14	271	.6	76	26	1575	4.01	31	5	ND	1	65	2	2	2	70	.74	.160	5	54	.93	456	.12	5	2.35	.03	.31	1	7
YL 850S 175E	2	41	15	118	.1	30	16	1122	3.00	10	5	ND	1	69	1	2	2	64	.76	.182	3	32	.78	377	.14	8	2.31	.04	.25	1	11
YL 850S 225E	2	49	9	125	.2	37	17	1180	3.06	33	5	ND	1	56	1	2	2	66	.50	.137	6	39	.66	351	.09	2	2.24	.02	.17	1	5
YL 850S 275E	2	44	5	106	.3	40	15	898	3.28	37	7	ND	1	44	1	2	2	84	.28	.082	3	43	.69	284	.12	4	2.24	.02	.13	1	3
YL 850S 300E	2	35	5	108	.2	33	13	1551	2.55	39	5	ND	1	39	1	2	2	56	.34	.106	4	32	.51	289	.10	2	1.89	.02	.09	1	5
YL 850S 325E	3	32	10	120	.2	36	14	786	2.95	54	7	ND	1	28	1	2	4	58	.27	.171	4	38	.56	282	.11	2	1.88	.02	.13	1	9
YL 850S 350E	2	27	13	108	.3	31	12	1438	2.47	55	5	ND	1	29	1	3	2	53	.26	.100	3	34	.43	271	.09	2	1.65	.02	.07	1	17
YL 850S 375E	2	35	14	110	.4	40	15	925	2.98	47	8	ND	1	26	1	3	2	57	.28	.092	5	38	.56	263	.10	3	1.89	.02	.09	1	11
YL 850S 400E	1	43	10	114	.3	48	16	1139	3.46	48	5	ND	1	40	1	2	2	68	.48	.072	6	49	.75	344	.12	3	2.12	.02	.17	1	255
YL 850S 450E	2	53	15	173	.6	60	19	1759	3.92	142	5	ND	1	24	1	2	2	67	.40	.092	7	51	.66	316	.08	3	1.92	.02	.10	1	33
YL 850S 475E	1	43	10	82	.5	35	12	484	3.10	42	5	ND	1	16	1	2	2	63	.20	.075	7	48	.62	207	.09	6	1.79	.02	.07	1	30
YL 850S 500E	1	30	10	72	.5	32	11	514	2.74	36	5	ND	1	16	1	2	2	54	.19	.101	5	35	.48	173	.09	2	1.67	.02	.06	1	13
YL 850S 525E	1	29	8	70	.3	28	11	657	2.81	46	5	ND	1	11	1	2	2	54	.14	.075	3	34	.42	146	.09	2	1.36	.01	.07	1	12
YL 850S 550E	1	33	3	78	.5	43	13	493	2.93	33	6	ND	2	14	1	2	2	56	.16	.112	5	48	.51	150	.11	3	2.05	.02	.07	1	10
YL 850S 575E	1	34	12	78	.4	29	12	489	3.11	32	5	ND	2	13	1	2	2	63	.14	.101	4	38	.51	152	.12	3	2.07	.01	.06	1	10
YL 850S 600E	1	27	9	80	.3	23	11	644	2.84	26	5	ND	2	13	1	2	2	57	.14	.120	5	31	.42	135	.12	2	2.22	.02	.05	1	5
YL 850S 625E	2	37	14	94	.4	30	13	702	3.10	31	5	ND	2	19	1	2	2	64	.21	.072	7	37	.59	185	.13	2	2.11	.02	.06	1	7
YL 850S 650E	1	29	7	104	.3	27	12	444	3.06	71	5	ND	1	16	1	2	2	63	.20	.057	5	38	.53	139	.13	2	1.91	.02	.06	1	12
YL 850S 675E	1	31	11	88	.4	28	12	423	3.07	40	5	ND	1	18	1	2	2	63	.23	.057	7	39	.57	147	.13	2	1.90	.02	.06	1	39
YL 850S 700E	1	33	9	101	.4	33	14	458	3.15	49	5	ND	1	15	1	2	2	65	.24	.065	4	40	.56	145	.14	3	2.05	.02	.07	1	2
YL 850S 725E	1	29	8	96	.7	26	11	440	2.87	43	5	ND	1	17	1	2	2	59	.24	.054	6	36	.50	154	.14	4	2.02	.02	.06	1	2
YL 850S 750E	1	34	12	106	.3	28	13	403	3.26	57	5	ND	1	16	1	2	2	65	.20	.073	7	39	.56	145	.13	4	2.22	.02	.08	1	7
YL 850S 775E	1	29	11	106	.4	24	11	318	2.77	131	5	ND	1	14	1	2	2	54	.18	.070	5	31	.43	116	.13	2	2.18	.02	.06	1	5
YL 850S 800E	1	20	10	69	.3	14	7	172	2.42	61	5	ND	1	10	1	2	2	51	.10	.092	3	23	.26	77	.11	2	1.79	.02	.05	1	6
YL 850S 825E	1	20	15	84	.7	15	8	180	2.36	239	5	ND	1	10	1	2	2	50	.12	.064	4	22	.26	90	.11	7	1.70	.02	.04	1	4
YL 850S 850E	1	23	10	79	.6	16	8	218	2.40	51	5	ND	1	10	1	2	2	51	.11	.096	4	26	.32	94	.12	2	1.65	.02	.05	1	3
YL 850S 875E	1	19	9	62	.3	15	7	217	2.27	54	5	ND	1	11	1	2	2	51	.12	.044	3	24	.28	82	.12	3	1.21	.02	.05	1	1
YL 850S 900E	1	49	9	66	2.0	29	10	687	2.57	626	5	ND	1	37	1	2	2	41	1.24	.086	10	38	.42	88	.04	4	1.68	.02	.07	1	8
YL 850S 925E	1	43	10	95	.4	33	14	642	3.40	78	5	ND	1	19	1	2	2	67	.22	.067	9	42	.59	171	.12	5	2.14	.02	.07	1	8
YL 850S 950E	1	30	13	92	.5	23	10	489	2.90	70	5	ND	1	16	1	2	2	59	.16	.066	5	29	.44	118	.11	4	1.82	.02	.06	1	3
YL 850S 975E	1	46	12	97	.6	37	15	669	3.46	144	5	ND	1	13	1	2	2	70	.16	.067	7	47	.69	167	.11	3	2.20	.02	.08	1	9
YL 850S 1000E	1	36	9	90	.5	31	13	422	3.09	103	5	ND	1	13	1	2	2	63	.18	.065	7	38	.55	140	.11	2	1.96	.02	.08	1	3
STD C/AU-0.5	21	57	38	132	7.1	68	31	1115	3.98	39	20	7	35	50	17	16	19	64	.48	.102	39	60	.88	186	.08	36	1.72	.07	.13	13	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 850S 1025E	2	44	17	100	.5	35	12	382	3.36	164	5	ND	2	16	1	2	2	66	.18	.063	10	38	.57	131	.14	2	2.18	.02	.08	2	5
YL 850S 1050E	1	46	14	93	.9	32	10	591	2.96	159	5	ND	1	27	1	2	2	62	.43	.068	11	40	.58	143	.10	4	1.97	.02	.08	2	390
YL 850S 1075E	2	70	15	107	1.4	41	13	851	2.94	405	5	ND	1	43	1	2	2	57	.76	.090	22	41	.61	185	.08	3	2.41	.02	.08	2	1
YL 850S 1100E	4	97	19	99	1.0	56	19	927	3.53	719	5	ND	1	34	1	2	2	67	.76	.091	16	48	.81	153	.10	2	2.12	.02	.13	1	13
YL 850S 1125E	3	81	23	139	1.5	56	15	1210	3.33	1190	5	ND	1	28	1	2	2	59	.54	.067	19	39	.57	155	.10	3	2.64	.03	.09	1	4
YL 850S 1150E	2	141	14	110	2.9	56	12	908	2.70	369	5	ND	1	53	1	2	2	41	2.01	.120	16	37	.41	143	.06	3	2.07	.03	.08	1	7
YL 850S 1175E	3	190	16	107	4.0	61	14	1005	2.91	410	9	ND	1	59	1	2	2	42	2.41	.150	21	43	.42	163	.05	2	2.22	.03	.09	1	10
YL 850S 1200E	2	43	11	99	.6	30	11	634	2.96	53	5	ND	1	19	1	2	2	59	.35	.065	8	34	.49	131	.14	2	2.10	.02	.07	1	8
YL 900S 0E	2	50	19	318	.6	35	18	2756	3.92	135	5	ND	1	79	1	2	2	60	.87	.289	10	30	.46	1559	.07	6	1.92	.04	.16	1	5
YL 900S 25E	1	53	14	317	.3	55	17	1145	3.30	42	5	ND	1	55	1	2	2	56	.68	.275	9	30	.48	629	.11	5	1.85	.04	.15	1	4
YL 900S 50E	1	41	19	333	.4	34	14	1959	3.36	25	5	ND	1	72	1	2	2	55	.82	.335	8	32	.50	867	.09	6	1.80	.03	.16	1	4
YL 900S 75E	4	103	26	217	.8	63	23	1354	6.89	227	5	ND	2	86	1	2	2	116	.60	.203	9	106	1.34	700	.18	2	3.35	.03	.39	2	14
YL 900S 100E	3	85	21	192	.6	59	21	1188	5.68	71	5	ND	1	72	1	2	2	102	.54	.159	8	102	1.31	749	.17	2	3.33	.02	.36	1	7
YL 900S 125E	2	49	20	293	.4	44	18	1765	3.48	16	5	ND	1	72	3	2	2	56	.98	.189	5	33	.66	420	.10	2	2.50	.04	.19	1	1
YL 900S 150E	2	54	13	212	.3	53	21	1308	3.54	21	5	ND	1	71	1	2	2	68	.84	.173	7	47	.81	481	.10	4	2.27	.03	.27	1	3
YL 900S 175E	2	58	11	191	.4	50	22	1382	3.71	32	5	ND	1	51	1	2	2	66	.54	.138	7	44	.79	405	.10	3	2.42	.03	.21	1	3
YL 900S 200E	2	49	9	175	.3	45	20	1752	2.93	31	5	ND	1	47	1	2	2	53	.50	.153	10	37	.64	356	.08	2	2.22	.02	.16	1	2
YL 900S 225E	2	48	11	137	.3	43	18	1432	3.35	32	5	ND	1	43	1	2	2	69	.41	.120	7	45	.74	364	.13	3	2.48	.02	.15	2	6
YL 900S 250E	1	38	11	112	.4	34	13	1093	3.00	35	5	ND	1	35	1	2	2	73	.30	.101	4	35	.53	244	.13	2	2.37	.02	.11	1	2
YL 900S 275E	1	36	12	132	.4	39	14	1328	3.15	47	5	ND	1	40	1	2	2	77	.28	.137	3	38	.59	285	.15	3	2.70	.03	.12	1	1
YL 900S 300E	2	41	8	128	.3	41	15	965	3.31	34	5	ND	2	26	1	2	2	69	.20	.112	6	42	.63	266	.14	2	2.33	.02	.09	1	6
YL 900S 325E	1	33	11	128	.4	36	13	849	3.02	40	5	ND	2	21	1	2	2	61	.18	.125	5	36	.50	226	.14	4	2.42	.02	.09	1	2
YL 900S 350E	1	44	13	126	.3	43	15	882	3.48	59	5	ND	2	19	1	2	2	67	.19	.108	6	43	.59	258	.13	3	2.16	.02	.11	1	17
YL 900S 375E	2	55	15	140	1.3	48	12	779	3.41	112	5	ND	1	37	1	2	2	68	.57	.089	10	62	.64	298	.09	2	2.16	.03	.10	1	20
YL 900S 400E	1	26	15	110	.8	27	11	293	2.92	49	5	ND	2	12	1	2	2	60	.13	.118	6	31	.39	155	.13	2	2.36	.02	.06	1	10
YL 900S 425E	1	24	12	111	.4	25	11	588	2.89	32	5	ND	1	15	1	2	2	58	.16	.127	4	31	.44	142	.15	2	2.30	.02	.07	1	140
YL 900S 450E	1	39	17	84	.3	31	11	493	3.19	50	5	ND	1	15	1	2	2	63	.15	.084	6	36	.49	180	.12	2	1.91	.02	.07	1	39
YL 900S 475E	1	38	12	90	.3	33	13	723	3.34	52	5	ND	1	15	1	2	2	65	.15	.091	8	37	.49	178	.13	5	2.05	.02	.08	1	20
YL 900S 500E	1	38	10	91	.4	32	12	331	3.29	47	5	ND	2	14	1	2	2	64	.13	.099	8	36	.48	167	.14	2	2.38	.02	.07	1	12
YL 900S 525E	1	31	15	96	.5	27	13	313	3.34	26	5	ND	2	18	1	2	2	68	.23	.114	8	33	.52	148	.18	2	2.63	.03	.08	1	13
YL 900S 550E	1	25	12	81	.3	23	10	287	2.90	24	5	ND	1	14	1	2	2	60	.16	.126	6	28	.39	103	.14	2	2.11	.02	.06	1	23
YL 900S 575E	1	39	7	94	.4	27	13	408	2.93	26	5	ND	2	14	1	2	2	62	.13	.137	6	32	.44	126	.18	2	2.15	.02	.06	1	2
YL 900S 625E	2	38	18	93	.5	39	17	1464	3.74	43	5	ND	1	21	1	2	2	80	.23	.045	10	48	.62	190	.17	2	2.60	.02	.06	1	2
YL 900S 650E	1	37	12	109	.2	37	16	855	3.61	67	5	ND	1	20	1	2	2	77	.26	.056	10	50	.70	161	.20	2	2.36	.02	.06	1	6
YL 900S 675E	1	36	12	120	.6	31	13	452	3.28	63	5	ND	1	14	1	2	2	67	.16	.078	9	42	.55	148	.17	2	2.24	.02	.07	1	5
YL 900S 700E	1	40	17	107	.4	32	14	489	3.43	71	5	ND	1	14	1	2	2	71	.15	.089	8	42	.54	149	.17	3	2.47	.02	.06	2	6
STD C/AU 0.5	21	59	42	136	7.2	70	30	1136	3.97	40	19	8	35	50	17	15	20	65	.48	.107	38	60	.88	186	.09	38	1.71	.07	.14	15	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 900S 725E	1	30	12	105	.1	28	11	310	2.94	69	5	ND	1	12	1	2	2	58	.13	.048	11	34	.44	111	.14	4	2.10	.02	.05	1	3
YL 900S 750E	1	14	12	63	.1	11	6	271	1.97	16	5	ND	1	10	1	2	2	39	.11	.111	7	15	.17	78	.13	2	1.76	.02	.03	1	1
YL 900S 775E	1	17	14	88	.2	12	7	226	2.23	28	5	ND	1	14	1	2	2	44	.10	.073	9	16	.21	90	.13	9	2.02	.02	.03	1	2
YL 900S 800E	1	30	14	79	.1	17	9	211	3.21	265	5	ND	1	22	1	2	2	55	.15	.049	11	22	.25	83	.14	2	2.53	.02	.05	1	11
YL 900S 825E	1	16	7	73	.1	10	9	323	2.42	66	5	ND	1	11	1	2	2	43	.09	.056	8	16	.16	65	.14	3	2.11	.02	.05	1	9
YL 900S 850E	1	26	26	251	2.0	23	13	350	2.61	251	5	ND	2	13	1	2	2	47	.09	.081	9	28	.30	109	.13	4	2.47	.02	.05	1	2
YL 900S 900E	1	19	12	67	.1	14	7	192	2.70	148	5	ND	1	13	1	2	2	55	.14	.085	8	28	.32	80	.17	6	2.01	.02	.06	1	4
YL 900S 925E	1	16	10	83	.4	11	6	238	2.71	75	5	ND	1	13	1	2	2	53	.12	.107	10	19	.20	73	.14	4	2.12	.02	.03	1	6
YL 900S 950E	1	22	14	60	.2	13	7	291	2.65	62	5	ND	1	11	1	2	2	52	.08	.110	9	21	.24	100	.13	3	1.71	.02	.04	1	4
YL 900S 975E	1	40	13	114	.1	44	17	427	3.54	160	5	ND	1	23	1	2	2	69	.13	.052	14	42	.69	251	.15	3	2.55	.02	.07	1	7
YL 900S 1000E	1	60	16	145	.5	73	23	651	4.93	360	5	ND	1	29	1	2	2	100	.52	.078	20	86	1.58	296	.23	6	3.10	.02	.24	1	13
YL 900S 1000E-A	1	37	7	103	.5	34	19	626	2.71	~~360~~	5	ND	1	20	1	2	2	51	.27	.060	15	35	.53	149	.14	3	2.00	.02	.09	1	46
YL 900S 1025E	1	81	25	224	1.8	58	17	1019	3.56	847	5	ND	1	31	1	2	2	58	.50	.084	23	43	.67	166	.08	6	2.89	.02	.10	1	31
YL 900S 1050E	1	40	15	113	.3	30	12	374	3.74	192	5	ND	1	16	1	2	2	73	.18	.060	17	41	.58	126	.14	3	2.28	.02	.07	1	4
YL 900S 1075E	1	90	21	159	.9	46	15	1030	3.93	716	5	ND	1	30	1	2	2	70	.46	.080	25	47	.67	193	.10	6	2.87	.02	.11	1	9
YL 900S 1100E	1	120	22	191	.7	63	26	953	4.67	934	5	ND	1	24	1	2	2	86	.48	.066	27	60	1.01	176	.11	5	2.77	.02	.14	1	6
YL 900S 1125E	1	38	19	128	.7	30	10	298	3.69	484	5	ND	1	18	1	2	2	66	.20	.073	16	35	.45	140	.14	2	2.34	.02	.07	1	12
YL 900S 1150E	1	30	10	97	.3	22	9	288	3.36	200	5	ND	1	11	1	2	2	63	.11	.078	14	32	.43	98	.12	2	2.41	.02	.05	1	10
YL 900S 1175E	1	45	15	89	.9	28	10	329	2.96	745	5	ND	1	21	1	2	2	56	.53	.063	16	31	.44	81	.10	2	2.11	.02	.06	1	7
YL 900S 1200E	1	41	16	97	.5	25	13	532	3.52	93	5	ND	1	14	1	2	2	70	.21	.052	15	37	.52	122	.13	2	2.10	.02	.07	1	9
YL 950S 25E	1	25	10	337	.2	41	12	1420	1.98	20	5	ND	1	56	3	2	2	31	.87	.265	10	21	.28	791	.07	5	1.45	.03	.12	1	2
YL 950S 50E	1	26	7	270	.2	22	9	1359	1.78	25	5	ND	1	88	2	2	2	30	1.37	.315	9	16	.26	845	.06	6	1.64	.03	.09	1	2
YL 950S 75E	1	24	10	255	.2	21	9	1336	1.69	28	5	ND	1	83	2	2	2	28	1.27	.312	9	15	.25	802	.06	5	1.57	.03	.09	1	1
YL 950S 100E	2	66	26	310	.2	79	27	1740	3.90	48	5	ND	1	44	3	2	2	65	.67	.172	20	60	.97	642	.06	2	2.06	.01	.26	1	4
YL 950S 125E	2	71	17	255	.3	63	24	1213	4.31	53	5	ND	1	51	2	2	2	79	.60	.135	20	68	1.09	668	.11	4	2.54	.02	.34	1	5
YL 950S 150E	1	64	19	256	.3	82	28	1332	4.87	34	5	ND	1	77	2	2	2	82	.85	.183	18	77	1.28	602	.16	2	2.89	.03	.50	1	4
YL 950S 175E	1	58	17	244	.2	79	26	1234	4.90	31	5	ND	1	82	2	2	3	81	.85	.172	18	81	1.28	577	.17	3	2.81	.03	.52	1	2
YL 950S 200E	1	55	16	164	.1	58	21	1444	3.63	28	5	ND	1	34	1	2	2	65	.42	.141	16	51	.87	341	.12	4	2.38	.02	.17	1	4
YL 950S 225E	1	41	9	141	.2	41	16	1297	3.13	25	5	ND	1	34	1	2	2	60	.42	.118	13	41	.63	291	.12	3	2.21	.02	.13	1	2
YL 950S 250E	1	31	12	175	.3	41	15	1100	3.22	22	5	ND	1	21	1	2	2	61	.25	.116	12	39	.59	246	.13	2	2.35	.02	.09	1	7
YL 950S 275E	1	27	9	148	.3	39	13	810	3.14	26	5	ND	1	23	1	2	2	65	.21	.134	10	36	.53	217	.13	2	2.31	.02	.08	1	4
YL 950S 300E	1	34	14	117	.3	36	12	806	3.10	33	5	ND	2	21	1	2	2	60	.19	.129	11	36	.51	215	.12	3	2.14	.02	.08	1	8
YL 950S 325E	1	64	13	101	.3	48	16	895	4.19	60	5	ND	2	27	1	2	2	75	.34	.078	19	57	.91	280	.13	2	1.85	.01	.17	1	14
YL 950S 350E	2	39	17	160	.7	44	14	931	3.77	99	6	ND	1	38	1	2	2	74	.71	.070	14	53	.77	273	.10	3	2.01	.02	.11	1	30
YL 950S 375E	1	23	13	98	.3	20	11	606	3.09	45	5	ND	1	12	1	2	2	61	.15	.138	9	33	.34	127	.11	3	1.78	.02	.06	1	28
YL 950S 400E	1	28	16	91	.3	28	12	459	3.24	46	5	ND	1	15	1	2	2	63	.19	.098	11	34	.44	153	.11	3	1.76	.02	.06	1	46
STD C/AU-0.5	21	57	40	134	6.9	70	29	1124	3.95	37	18	8	35	50	19	15	18	64	.48	.103	39	58	.88	184	.09	37	1.72	.07	.13	15	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 950S 425E	2	24	10	107	.1	30	12	920	3.00	40	5	ND	1	12	1	2	2	56	.17	.112	6	31	.45	103	.12	5	1.81	.02	.07	1	32
YL 950S 450E	2	29	2	89	.2	38	11	547	2.93	29	5	ND	1	19	1	2	2	57	.28	.058	6	35	.53	182	.14	3	2.09	.02	.07	1	6
YL 950S 475E	1	38	7	97	.2	39	14	410	3.44	38	5	ND	2	17	1	2	2	69	.21	.099	7	41	.62	161	.16	2	2.29	.02	.07	1	11
YL 950S 500E	1	35	8	96	.1	42	15	511	3.25	37	5	ND	2	15	1	2	2	66	.19	.091	5	42	.61	175	.18	3	2.34	.02	.07	1	3
YL 950S 525E	1	31	12	95	.2	34	13	400	2.85	42	5	ND	1	14	1	2	2	59	.16	.090	5	36	.49	140	.18	2	2.26	.02	.06	1	3
YL 950S 550E	3	85	6	115	.2	73	23	371	3.69	67	5	ND	2	15	1	2	2	75	.13	.060	5	78	1.02	164	.32	2	2.67	.02	.14	1	7
YL 950S 575E	2	46	13	92	.1	42	19	402	3.29	49	5	ND	2	14	1	2	2	66	.16	.055	9	43	.65	147	.20	2	2.24	.02	.07	1	8
YL 950S 600E	2	20	12	101	.1	27	15	613	3.03	57	5	ND	2	17	1	2	2	59	.21	.059	5	29	.40	157	.18	3	2.29	.03	.06	1	2
YL 950S 625E	1	32	11	92	.1	24	12	444	3.05	58	5	ND	1	13	1	2	2	64	.14	.070	2	31	.41	102	.19	2	2.09	.02	.05	1	1
YL 950S 650E	1	21	8	107	.2	18	10	390	2.43	74	5	ND	1	13	1	2	2	48	.14	.094	3	22	.29	90	.14	4	1.89	.02	.04	1	5
YL 950S 675E	1	21	15	126	.3	13	8	264	2.57	60	5	ND	1	11	1	2	2	47	.12	.083	2	17	.22	102	.17	4	1.48	.02	.05	1	3
~~YL 950S 750E~~	4	77	20	134	.2	33	23	967	4.48	62	6	ND	1	18	1	2	2	99	.17	.061	2	54	.61	237	.18	2	2.06	.02	.10	1	4
YL 950S 875E	2	44	18	115	.4	38	15	410	4.31	207	5	ND	2	21	1	2	2	90	.17	.041	5	50	.89	163	.24	2	2.52	.02	.08	1	14
YL 950S 900E	1	5	10	19	.1	3	1	72	.65	12	5	ND	1	9	1	2	2	21	.08	.014	3	6	.05	48	.10	2	.52	.02	.03	1	5
YL 950S 925E	2	25	11	74	.3	21	9	284	3.09	146	5	ND	2	15	1	2	2	61	.09	.049	3	31	.32	92	.16	2	2.23	.02	.05	1	11
YL 950S 950E	2	36	13	72	.1	31	9	275	3.64	199	5	ND	1	12	1	2	2	73	.08	.038	7	43	.53	124	.16	6	2.26	.02	.06	1	10
YL 950S 975E	2	37	20	80	.4	28	10	320	3.22	279	5	ND	1	15	1	2	2	62	.12	.041	7	36	.50	124	.14	2	2.05	.02	.07	1	20
YL 950S 1000E	2	38	15	112	.6	35	14	431	3.35	212	5	ND	1	13	1	2	2	62	.11	.073	8	37	.51	128	.13	3	2.48	.02	.06	1	20
YL 950S 1025E	1	35	14	121	.4	26	12	489	3.26	379	5	ND	1	17	1	2	2	60	.21	.068	8	36	.53	126	.14	4	2.24	.02	.07	1	17
YL 950S 1050E	1	48	21	100	.4	35	14	818	3.04	700	5	ND	1	22	1	2	2	57	.27	.055	10	38	.59	131	.11	2	2.25	.02	.07	1	14
YL 950S 1075E	1	43	17	101	.4	36	15	653	3.45	350	5	ND	1	27	1	2	2	65	.33	.051	11	41	.66	189	.14	4	2.36	.02	.08	1	15
YL 950S 1100E	1	40	14	107	.5	43	11	805	3.02	1626	5	ND	1	22	1	2	2	52	.39	.049	8	38	.56	155	.13	2	2.61	.02	.08	1	15
YL 950S 1125E	1	35	13	97	.5	34	14	561	3.50	283	5	ND	1	17	1	2	2	68	.20	.052	9	41	.64	160	.16	2	2.48	.02	.08	1	12
YL 950S 1150E	1	42	16	99	.5	36	15	627	3.57	213	5	ND	1	18	1	2	2	67	.21	.064	12	43	.67	189	.13	4	2.49	.02	.09	2	11
YL 950S 1175E	1	47	8	94	.5	43	15	715	3.59	446	5	ND	1	18	1	2	3	67	.24	.055	11	46	.69	186	.14	2	2.38	.02	.09	1	6
YL 950S 1200E	1	48	12	101	.5	43	14	873	3.66	229	5	ND	1	20	1	2	2	71	.38	.050	12	45	.71	208	.13	2	2.74	.02	.11	1	5
YL 1000S 0E	2	54	23	269	.2	53	17	1313	3.82	92	5	ND	1	82	2	2	2	59	.97	.212	14	37	.69	768	.08	4	2.25	.02	.22	1	3
YL 1000S 25E	1	48	15	210	.4	55	19	1264	2.95	42	5	ND	1	58	2	2	2	54	.86	.151	13	50	.77	519	.08	7	1.94	.02	.25	1	1
YL 1000S 50E	2	57	15	207	.3	67	24	1302	3.79	53	5	ND	1	52	1	2	2	67	.67	.167	15	63	.99	602	.09	2	2.20	.02	.34	1	4
YL 1000S 75E	2	66	20	258	.7	75	26	1408	4.11	70	6	ND	1	61	2	2	2	72	.81	.159	15	67	1.06	663	.09	2	2.36	.02	.31	1	5
YL 1000S 100E	1	58	18	182	.2	181	35	1814	4.33	29	5	ND	1	63	1	2	2	72	1.68	.204	8	161	1.89	407	.18	3	3.11	.03	.36	1	1
YL 1000S 125E	1	51	18	200	.1	95	25	1523	4.10	38	5	ND	1	36	1	2	2	70	.70	.167	14	86	1.16	413	.17	5	2.69	.02	.31	1	4
YL 1000S 150E	1	49	20	196	.1	95	26	1501	4.13	37	5	ND	1	33	1	2	2	70	.63	.172	13	83	1.13	386	.16	2	2.77	.02	.28	1	1
YL 1000S 175E	1	36	13	147	.3	43	16	1523	3.05	30	5	ND	1	31	1	2	2	53	.38	.118	9	40	.64	323	.12	3	2.20	.02	.11	1	1
YL 1000S 200E	1	31	8	146	.2	39	15	1235	2.86	25	5	ND	1	22	1	2	2	52	.25	.129	10	35	.54	254	.13	4	2.09	.02	.10	1	1
YL 1000S 225E	1	27	10	123	.8	62	10	753	2.63	21	5	ND	1	33	1	2	2	49	.69	.040	10	39	.52	359	.15	3	2.43	.03	.08	1	1
STD C/AU 0.5	21	57	39	132	7.2	69	30	1112	3.96	39	18	7	34	49	17	16	20	63	.48	.102	38	59	.88	183	.09	38	1.71	.07	.13	14	490

SHANGRI-LA MINERALS PROJECT - YUNIMAN FILE # 86-1508

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 1000S 250E	3	28	10	72	.8	33	6	620	1.78	17	5	ND	1	48	1	2	3	33	1.44	.108	3	19	.40	239	.05	5	1.50	.04	.05	1	4
YL 1000S 275E	2	19	12	105	.4	29	8	784	2.36	13	5	ND	1	32	1	2	2	45	.62	.041	5	28	.51	269	.11	4	2.12	.03	.06	1	1
YL 1000S 300E	1	19	11	103	.5	29	9	687	2.40	14	5	ND	1	30	1	2	2	45	.57	.041	4	28	.50	269	.11	3	2.19	.03	.06	1	1
YL 1000S 325E	1	35	11	96	.4	31	10	276	3.20	45	5	ND	1	13	1	2	4	58	.19	.124	5	34	.50	154	.11	2	1.79	.02	.06	1	28
YL 1000S 375E	1	38	15	82	.5	29	12	378	3.25	56	5	ND	1	10	1	2	2	60	.13	.071	5	33	.50	157	.11	2	1.84	.01	.07	1	13
YL 1000S 400E	1	33	17	98	.2	30	13	494	3.32	46	5	ND	1	12	1	2	2	60	.16	.143	5	31	.48	135	.11	2	1.99	.02	.07	1	90
YL 1000S 425E	1	33	12	78	.2	39	14	433	3.54	34	5	ND	1	17	1	2	2	71	.24	.070	5	40	.60	175	.16	2	2.47	.02	.07	1	4
YL 1000S 450E	1	32	13	91	.1	31	13	410	3.31	26	5	ND	2	16	1	2	2	66	.23	.088	6	35	.59	147	.14	2	2.26	.02	.08	1	5
YL 1000S 475E	1	31	11	97	.2	29	14	714	3.08	28	5	ND	1	16	1	2	2	63	.20	.095	6	31	.50	148	.16	2	2.23	.02	.07	1	3
YL 1000S 500E	2	46	18	106	.2	48	17	832	3.73	55	5	ND	2	18	1	2	2	79	.25	.067	8	50	.81	165	.21	2	2.34	.02	.08	1	2
YL 1000S 575E	1	29	15	76	.3	30	13	393	3.35	35	5	ND	2	16	1	2	2	71	.19	.056	10	37	.56	135	.18	2	2.13	.02	.06	1	3
YL 1000S 600E	2	37	19	135	.2	43	15	1381	3.14	428	5	ND	1	22	1	2	2	64	.34	.082	9	42	.64	128	.17	4	2.58	.03	.06	1	3
YL 1000S 625E	1	32	10	98	.2	27	11	265	2.46	426	5	ND	1	17	1	2	2	50	.27	.031	10	21	.40	157	.18	3	1.79	.02	.04	1	7
YL 1000S 650E	2	32	16	117	.5	20	12	371	3.34	159	5	ND	1	13	1	2	2	61	.11	.047	6	27	.36	93	.15	2	2.08	.02	.05	1	5
YL 1050S 750E	1	28	17	53	.1	17	6	176	2.58	29	5	ND	1	10	1	2	2	53	.09	.028	7	24	.28	95	.14	2	2.17	.02	.03	1	5
YL 1050S 775E	1	33	14	39	.1	8	4	194	2.40	12	5	ND	1	7	1	2	2	46	.07	.056	4	15	.13	65	.11	2	1.69	.01	.03	2	1
YL 1050S 800E	1	17	10	47	.4	11	6	309	2.11	133	5	ND	1	10	1	2	2	39	.09	.054	5	15	.18	65	.13	3	2.00	.02	.04	2	21
YL 1050S 825E	1	30	21	64	.4	17	7	241	3.46	53	5	ND	1	11	1	2	2	66	.09	.043	6	29	.34	90	.17	2	2.24	.02	.06	1	7
YL 1050S 850E	2	40	30	93	.7	27	10	280	3.39	62	5	ND	2	13	1	2	2	61	.09	.049	8	31	.42	105	.15	2	2.85	.02	.05	1	9
YL 1050S 875E	1	43	26	124	.8	37	17	684	3.89	83	5	ND	1	21	1	2	2	76	.19	.067	10	45	.69	141	.18	4	3.00	.02	.08	1	12
YL 1050S 900E	1	31	17	73	.5	35	12	281	2.94	171	5	ND	1	17	1	2	3	61	.13	.047	5	44	.67	147	.16	2	2.47	.02	.06	1	13
YL 1050S 925E	1	44	27	81	.6	30	10	315	3.64	429	5	ND	1	15	1	2	2	69	.12	.050	8	39	.55	130	.16	2	2.47	.02	.07	1	185
YL 1050S 950E	1	25	19	71	.3	19	8	252	2.84	140	5	ND	1	13	1	2	3	54	.11	.049	6	23	.33	94	.14	2	2.21	.02	.05	1	6
YL 1050S 975E	2	43	26	92	.6	31	14	351	3.79	264	5	ND	2	17	1	2	2	69	.15	.045	11	39	.60	141	.15	2	2.62	.02	.07	1	12
YL 1050S 1000E	2	46	29	109	.5	36	19	805	4.11	205	5	ND	1	20	1	2	2	74	.20	.041	11	43	.74	151	.16	2	2.59	.02	.08	1	12
YL 1050S 1025E	1	38	19	76	.3	27	12	372	3.46	97	5	ND	1	13	1	2	2	63	.12	.061	9	35	.53	110	.14	2	2.58	.02	.07	1	10
YL 1050S 1075E	1	32	26	83	.3	31	15	611	3.68	244	5	ND	1	23	1	2	2	72	.26	.044	10	39	.64	132	.13	2	2.36	.02	.09	1	14
YL 1050S 1100E	1	33	17	88	.5	28	11	321	3.59	235	5	ND	1	14	1	2	2	66	.13	.047	9	38	.57	112	.15	2	2.58	.02	.08	1	17
YL 1050S 1125E	1	49	25	99	.4	44	15	669	4.01	589	5	ND	1	24	1	2	2	73	.43	.037	12	47	.77	211	.15	2	3.08	.02	.11	1	13
YL 1050S 1150E	1	43	19	94	.4	39	15	514	3.97	248	5	ND	1	17	1	2	2	76	.30	.045	10	50	.78	147	.17	2	2.83	.02	.09	1	52
YL 1050S 1175E	1	42	24	67	.4	51	14	284	3.80	983	5	ND	1	22	1	2	2	65	.52	.044	7	48	.67	171	.16	2	3.79	.03	.09	1	12
YL 1100S 750E	1	37	28	89	.3	23	10	398	3.71	53	5	ND	1	13	1	2	2	69	.13	.052	8	36	.53	102	.19	2	2.47	.02	.05	1	8
YL 1100S 775E	1	35	19	109	.5	27	13	1174	3.61	39	5	ND	1	15	1	2	2	66	.16	.085	8	38	.58	118	.16	2	2.46	.02	.06	1	7
YL 1100S 800E	2	32	38	82	.8	20	8	287	3.05	53	5	ND	1	12	1	2	2	56	.10	.057	6	27	.36	88	.15	4	2.84	.02	.06	1	5
YL 1100S 825E	1	34	38	115	1.8	21	12	786	3.27	36	5	ND	1	14	1	2	2	59	.15	.065	7	31	.44	95	.15	2	2.65	.02	.05	1	4
YL 1100S 850E	4	67	44	127	1.3	44	27	703	3.93	71	5	ND	1	18	1	2	2	70	.14	.047	11	42	.57	159	.16	4	2.70	.02	.08	1	9
STD C/AU-0.5	20	57	39	126	7.3	66	29	1065	3.96	37	21	8	32	46	17	16	18	61	.48	.102	35	56	.88	176	.08	38	1.70	.06	.13	13	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 1100S 875E	1	25	9	61	1.2	14	7	162	3.01	31	5	ND	1	11	1	2	3	51	.10	.113	10	25	.26	77	.12	2	3.29	.02	.05	3	1
YL 1100S 900E	1	35	15	98	.8	37	10	243	3.51	431	8	ND	2	15	1	2	2	73	.11	.056	12	48	.69	125	.16	2	3.03	.02	.08	1	13
YL 1100S 925E	4	46	15	69	.2	22	9	268	3.50	516	5	ND	1	17	1	2	2	54	.08	.069	12	27	.38	95	.13	2	2.28	.02	.08	1	19
YL 1100S 950E	1	39	20	101	.8	32	13	554	3.24	81	5	ND	1	17	1	2	2	63	.14	.061	12	37	.52	171	.14	2	2.39	.02	.07	1	15
YL 1100S 975E	1	33	16	80	.7	18	10	439	2.67	113	5	ND	1	17	1	2	2	52	.16	.059	13	27	.39	108	.11	2	1.88	.02	.06	2	4
YL 1100S 1000E	1	22	9	44	.3	11	7	164	2.41	26	5	ND	1	10	1	2	2	41	.07	.065	9	19	.21	61	.13	2	3.27	.02	.04	1	1
YL 1100S 1025E	2	42	14	72	.5	26	10	312	3.25	77	5	ND	1	13	1	2	2	62	.09	.052	14	35	.47	97	.15	3	2.55	.02	.08	1	10
YL 1100S 1050E	1	36	11	74	.5	20	9	391	2.77	86	5	ND	1	17	1	2	4	53	.15	.081	13	28	.42	112	.11	2	2.12	.02	.07	1	9
YL 1100S 1075E	2	39	13	87	.5	26	9	336	3.56	99	5	ND	1	16	1	2	2	73	.12	.058	13	36	.53	127	.14	3	2.34	.02	.10	1	15
YL 1100S 1100E	1	49	13	92	.6	46	15	589	3.86	707	5	ND	1	27	1	2	2	73	.32	.090	16	54	.70	154	.12	2	2.78	.02	.13	1	21
YL 1100S 1125E	1	30	13	62	.5	22	8	303	3.18	119	5	ND	1	14	1	2	2	62	.15	.042	11	34	.48	113	.14	2	2.32	.02	.08	1	8
YL 1100S 1150E	1	36	17	128	.3	38	13	662	3.19	283	6	ND	1	22	1	2	2	62	.39	.029	14	46	.77	184	.14	2	2.31	.02	.11	1	17
YL 1100S 1175E	1	32	9	33	2.2	9	6	357	1.80	1637	5	ND	1	26	1	2	2	30	.91	.077	12	19	.19	57	.07	2	2.14	.04	.04	1	1
YL 1100S 1200E	1	37	6	32	.8	14	5	134	1.48	2369	7	ND	1	23	1	3	2	32	.63	.070	11	20	.25	42	.10	2	2.72	.05	.05	1	4
YL 1150S 750E	2	59	20	94	.9	42	15	418	3.85	72	6	ND	3	14	1	2	2	73	.14	.057	13	42	.69	164	.20	6	3.04	.02	.08	1	6
YL 1150S 775E	1	58	18	99	.5	55	19	551	4.52	41	5	ND	2	15	1	2	2	85	.21	.050	14	63	1.06	250	.23	3	2.74	.01	.10	1	7
YL 1150S 800E	1	34	9	90	.4	32	15	1127	3.48	23	5	ND	1	16	1	2	2	69	.23	.077	10	50	.72	123	.20	2	2.26	.02	.07	1	6
YL 1150S 825E	2	32	15	98	.4	24	11	724	3.26	44	5	ND	1	12	1	2	2	63	.11	.061	9	35	.48	118	.16	7	2.54	.02	.06	1	5
YL 1150S 850E	1	22	10	85	.6	15	8	753	2.52	23	5	ND	1	13	1	2	2	50	.10	.092	7	23	.30	86	.15	4	2.26	.02	.05	1	2
YL 1150S 900E	2	47	25	95	.7	29	9	314	2.93	160	5	ND	1	15	1	2	2	55	.08	.050	9	30	.42	87	.12	2	2.10	.02	.05	1	26
YL 1150S 925E	2	49	25	94	.5	32	12	389	3.34	113	5	ND	1	15	1	2	2	64	.09	.055	10	38	.53	146	.14	3	2.52	.02	.07	1	17
YL 1150S 950E	2	47	22	113	.8	32	17	632	3.36	98	5	ND	1	18	1	2	2	64	.13	.056	11	36	.51	135	.14	2	2.41	.02	.07	1	12
YL 1150S 975E	1	11	9	27	.3	5	4	126	2.09	14	5	ND	1	8	1	2	2	38	.06	.043	5	13	.12	50	.12	2	2.60	.02	.04	1	1
YL 1150S 1000E	2	39	22	71	.4	23	10	333	3.70	120	6	ND	2	15	1	2	2	66	.08	.049	13	34	.43	107	.15	2	2.84	.02	.08	2	14
YL 1150S 1025E	2	54	23	99	1.5	30	17	661	3.70	244	5	ND	1	17	1	2	2	63	.13	.057	13	39	.53	141	.14	2	2.77	.02	.10	2	10
YL 1150S 1050E	1	30	16	72	.5	17	10	293	2.96	83	5	ND	3	13	1	2	2	56	.10	.086	10	27	.34	95	.13	2	2.69	.02	.06	1	5
YL 1150S 1075E	2	36	13	88	.7	24	11	321	3.51	97	7	ND	2	13	1	3	2	68	.10	.067	11	37	.45	119	.16	3	2.85	.02	.08	1	9
YL 1150S 1100E	2	41	14	78	.7	27	13	346	3.37	138	5	ND	2	12	1	3	2	63	.08	.066	11	35	.47	126	.14	2	2.80	.02	.09	1	21
YL 1150S 1125E	2	39	20	137	1.0	30	14	452	3.48	219	5	ND	1	16	1	3	2	67	.15	.048	13	39	.58	137	.15	4	2.64	.02	.10	1	18
YL 1150S 1150E	1	32	16	83	.7	21	13	441	3.02	86	5	ND	2	11	1	2	2	58	.08	.060	10	32	.42	100	.14	2	2.67	.02	.07	1	11
YL 1150S 1175E	2	30	23	107	.6	19	10	358	3.02	112	5	ND	1	11	1	2	2	57	.09	.067	10	32	.41	98	.13	2	2.64	.02	.07	1	10
YL 1150S 1200E	1	29	16	101	.9	23	11	369	3.04	98	5	ND	1	12	1	2	2	57	.10	.055	9	31	.40	107	.13	2	2.45	.02	.08	1	17
YL 1200S 750E	2	78	52	147	.6	40	18	691	3.78	65	7	ND	3	24	1	3	2	75	.15	.077	11	35	.55	174	.19	2	2.82	.02	.08	1	13
YL 1200S 775E	2	75	68	144	.5	45	17	664	4.13	104	6	ND	2	14	1	3	2	81	.13	.095	13	43	.69	192	.19	2	3.16	.02	.09	1	15
YL 1200S 800E	2	57	22	116	.3	41	19	923	4.15	32	5	ND	2	20	1	2	2	85	.22	.067	11	45	.79	235	.20	2	2.76	.02	.07	1	11
YL 1200S 825E	1	22	13	85	.4	29	12	445	3.10	12	5	ND	1	17	1	2	2	65	.25	.067	8	43	.59	125	.21	2	1.98	.02	.07	1	6
STD C/AU 0.5	21	58	41	133	7.2	68	29	1100	3.96	38	18	8	34	49	17	16	19	64	.48	.103	38	58	.88	183	.08	39	1.72	.07	.14	13	485

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YL 1200S 850E	1	50	37	112	.3	32	13	633	3.34	73	5	ND	1	15	1	2	2	71	.11	.081	10	44	.57	145	.16	2	2.46	.02	.07	1	11
YL 1200S 875E	1	44	41	108	.1	32	12	851	3.39	69	5	ND	1	14	1	2	2	70	.12	.079	9	39	.52	142	.15	2	2.27	.02	.07	1	4
YL 1200S 900E	3	40	21	91	.7	24	14	436	2.98	90	7	ND	1	14	1	2	2	50	.09	.112	10	30	.37	99	.14	3	3.67	.02	.06	1	15
YL 1200S 925E	3	51	28	101	.3	29	14	770	3.35	89	5	ND	1	13	1	2	5	66	.09	.070	10	42	.47	102	.13	2	2.37	.02	.06	1	8
YL 1200S 950E	3	52	34	137	1.1	31	14	460	3.21	378	5	ND	1	16	1	2	4	60	.11	.063	12	37	.47	99	.13	2	2.44	.02	.07	1	11
YL 1200S 975E	3	25	21	59	.1	16	7	425	2.96	83	5	ND	1	11	1	2	3	61	.08	.058	9	28	.33	82	.14	2	2.05	.02	.06	1	7
YL 1200S 1000E	2	30	17	68	.5	23	9	344	3.28	89	5	ND	1	13	1	2	2	63	.10	.067	11	34	.46	96	.15	2	2.41	.02	.08	1	6
YL 1200S 1025E	2	21	12	67	.2	15	9	291	2.47	38	5	ND	1	10	1	2	2	48	.08	.056	7	19	.22	63	.14	2	2.38	.02	.05	1	2
YL 1200S 1050E	2	20	16	56	.3	16	7	267	2.63	37	5	ND	1	10	1	2	2	57	.08	.073	8	27	.31	76	.15	2	2.22	.02	.05	1	3
YL 1200S 1075E	2	25	17	62	.5	18	10	379	2.90	95	5	ND	1	10	1	2	2	59	.08	.078	10	28	.36	83	.13	2	2.41	.02	.06	1	5
YL 1200S 1100E	2	14	18	46	.5	11	7	235	2.51	43	5	ND	1	9	1	2	2	50	.07	.089	7	19	.20	66	.14	2	2.87	.03	.04	2	1
YL 1200S 1125E	2	29	21	87	.5	20	10	398	2.97	106	5	ND	1	11	1	2	2	61	.10	.066	10	32	.41	93	.15	2	2.29	.02	.07	1	7
YL 1200S 1150E	3	45	42	228	.8	32	15	570	3.37	169	5	ND	1	14	1	2	7	66	.10	.063	14	42	.57	124	.13	2	2.58	.02	.09	1	15
YL 1200S 1175E	2	31	28	88	.2	22	9	292	3.29	127	5	ND	1	11	1	2	2	63	.08	.071	11	33	.39	79	.15	2	2.44	.02	.05	1	13
YL 1200S 1200E	2	42	28	134	.9	37	14	473	3.55	113	5	ND	2	14	1	2	4	73	.11	.075	12	46	.62	142	.16	4	2.78	.02	.10	1	10
STD C/AU-0.5	22	59	40	136	7.0	72	31	1154	3.96	41	17	8	35	51	18	15	22	66	.48	.111	39	62	.87	190	.09	35	1.72	.07	.14	14	515

APPENDIX K ROCK GEOCHEMICAL ANALYSES - FAR WEST CLAIM

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H20 AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK CHIPS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 22 1986 DATE REPORT MAILED: Aug 26/86 ASSAYER. D. Toye .DEAN TOYE. CERTIFIED B.C. ASSAYER.

SHANGRI-LA MINERALS PROJECT - YUNIMAN-86 FILE # 86-2194 PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM
YC-01	1	96	35	71	2.1	47	27	701	6.15	13784	5	ND	2	19	1
YC-02	1	32	13	25	.4	13	6	501	2.94	10486	5	ND	1	8	1
YC-03	2	46	18	50	.4	61	24	603	5.23	26796	5	ND	2	13	1
YC-04	1	107	19	111	.2	150	41	1361	7.69	2046	5	ND	1	43	1
YC-05	1	159	15	54	.3	93	33	844	7.54	9840	5	ND	2	22	1
YC-06	1	138	53	70	.3	72	27	636	6.24	2495	5	ND	2	21	1
YC-07	1	117	10	46	.3	84	30	578	5.30	8577	5	ND	2	17	1
YC-08	1	96	9	65	.3	103	39	1120	7.83	2975	5	ND	2	9	1
YC-09	1	74	7	74	.1	76	26	1825	5.83	80	5	ND	2	6	1
STD C/AU 0.5	21	57	44	136	7.0	71	30	1093	3.93	44	21	8	32	47	17

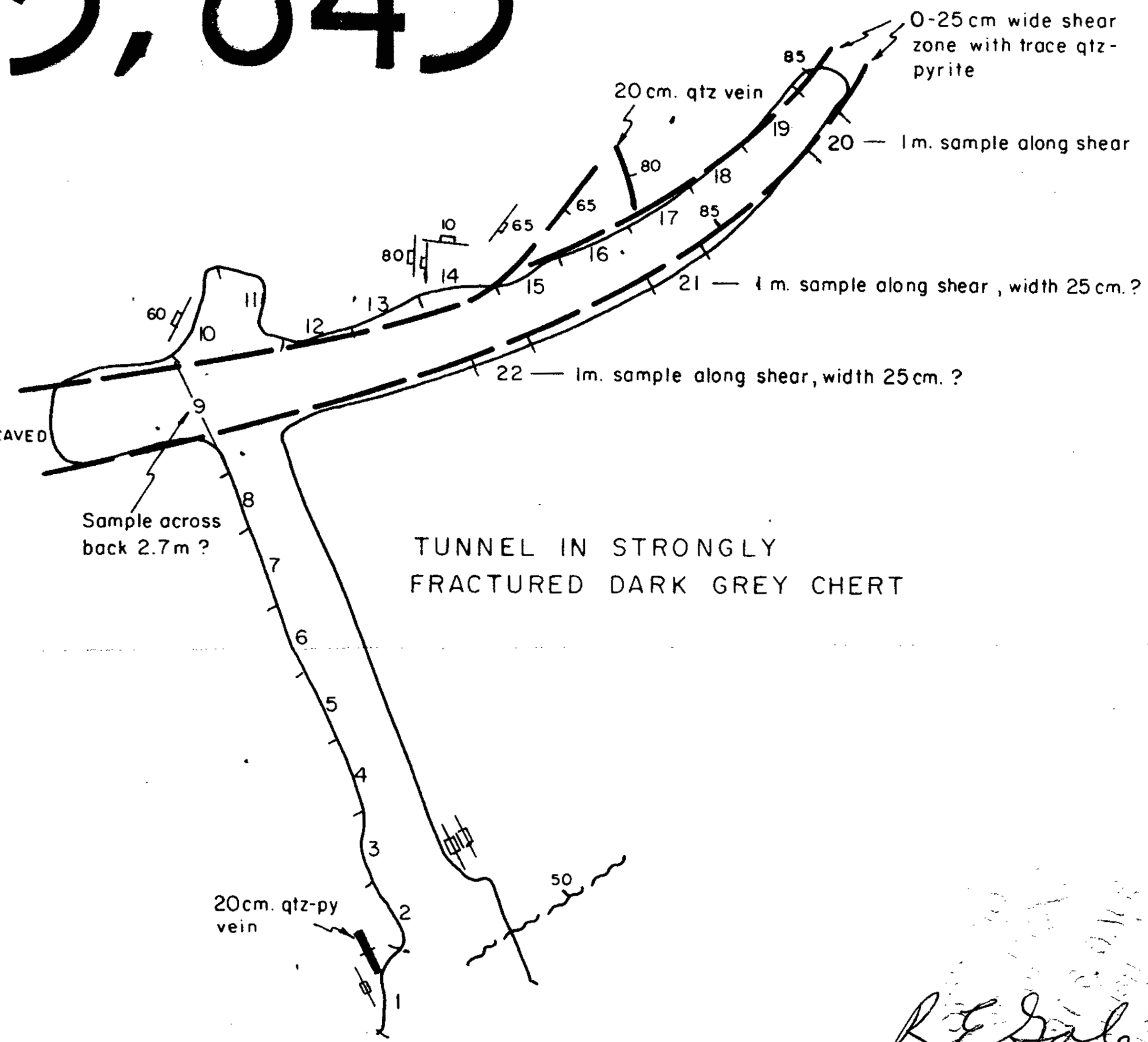
SAMPLE#	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
YC-01	6	2	46	.15	.143	21	69	1.06	131	.07	2	2.02	.03	.34	1	510
YC-02	6	3	42	.08	.025	8	23	.46	84	.03	2	.73	.05	.15	1	245
YC-03	8	2	78	.35	.105	14	71	1.25	83	.12	2	1.72	.06	.55	1	615
YC-04	2	2	139	.93	.107	13	213	3.92	71	.14	2	4.73	.25	.91	1	65
YC-05	4	5	105	.34	.099	12	137	2.03	62	.23	8	2.75	.09	1.36	1	295
YC-06	2	2	104	.26	.102	10	119	1.88	117	.24	3	2.61	.07	1.22	1	36
YC-07	3	2	108	.22	.075	9	108	1.64	91	.22	3	2.35	.06	1.12	1	275
YC-08	2	4	119	.44	.216	16	110	1.62	78	.37	4	3.12	.04	1.76	1	565
YC-09	2	4	87	.28	.092	16	82	1.57	301	.36	2	3.25	.03	1.70	1	10
STD C/AU 0.5	17	21	62	.48	.107	36	58	.88	175	.08	38	1.72	.08	.14	14	490

Cost Breakdown of Work on Escheated
Crown Grant Black Pine, L1912

Physical		
	Trenching and Drill Site Prepartion (prorated)	$ 4,278
Drilling		
	Drilling, Core Splitting, and Core Assays, Report, Office, Camp, Equipment and Vehicle Rental (prorated)	61,299
Geochemical		
	Soils	--------
Geophysical		
	Induced Polarization Survey (prorated)	2,098
Geological		
	Geology, Mineralogical Survey, Core Logging, Assays, Land Survey of Claim Posts and Geological Features, Report, Office, Camp Equipment and Vehicle Rental (prorated)	25,241
	Total	$ 92,916

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843



To accompany report by R. Gale, PhD., P. Eng.

2 m chip samples along walls except where noted differently.

SCALE 1:200

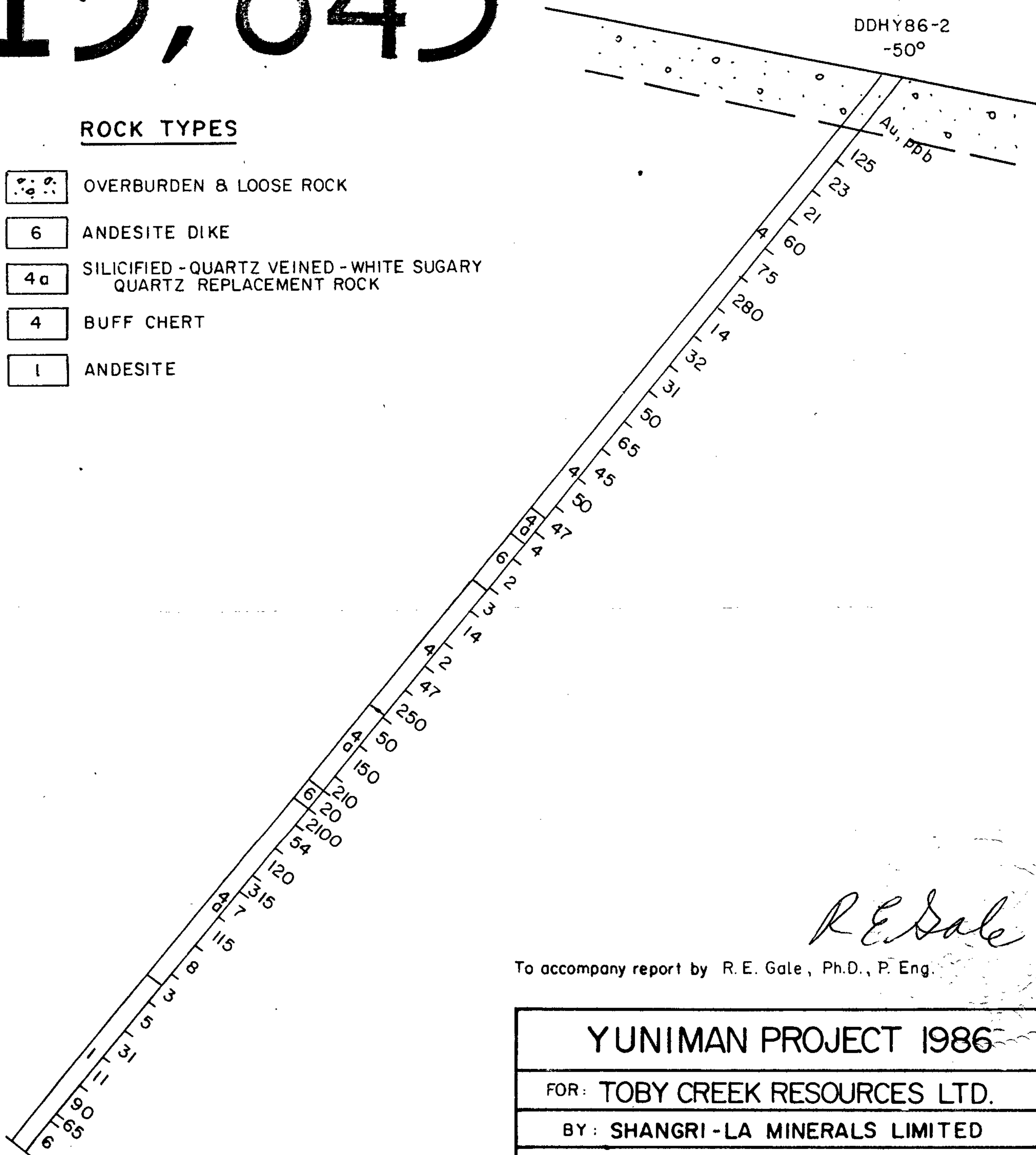
0 5 10 METRES

YUNIMAN PROJECT 1986	
FOR: TOBY CREEK RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LIMITED	
SAMPLE LOCATIONS TUNNEL No. 3 OSOYOOS M.D., B.C.	
N.T.S. 82E / 5W	DATE: OCT. 1986
DRAWN BY: R. G.	FIGURE No. 8

CHONG

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843



ROCK TYPES

(symbol)	OVERBURDEN & LOOSE ROCK
6	ANDESITE DIKE
4a	SILICIFIED - QUARTZ VEINED - WHITE SUGARY QUARTZ REPLACEMENT ROCK
4	BUFF CHERT
1	ANDESITE

R E Gale

To accompany report by R. E. Gale, Ph.D., P. Eng.

YUNIMAN PROJECT 1986	
FOR: TOBY CREEK RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LIMITED	
SECTION Y86-2 LOOKING NE MAIN ZONE OSOYOOS M.D., B.C.	
N.T.S. 82E / 5W	DATE: OCT. 1986
DRAWN BY: R.G.	FIGURE Nº. 12

CHONG

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843

APPENDIX G

DDH Y86-1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au† PPB	DEPTH (m)
4051	1	87	78	36	.7	6	12	235	2.62	347	5	ND	3	21	1	2	5	50	.26	.055	8	18	.81	154	.03	3	1.35	.08	.19	8	.001	3.8 - 5.33
4052	1	103	2	20	.3	10	12	254	2.67	59	5	ND	3	16	1	2	5	44	.24	.052	6	16	.75	135	.01	2	1.23	.07	.14	5	.001	5.33 - 8.38
4053	1	103	5	25	.3	4	12	310	2.75	323	5	ND	2	27	1	2	2	41	.63	.056	6	16	.69	83	.02	2	1.10	.08	.17	7	.001	8.38 - 9.91
4054	1	92	10	46	.3	5	8	243	2.86	156	5	ND	3	32	1	2	2	56	1.18	.050	5	14	.85	80	.04	2	1.28	.12	.15	1	70	9.91 - 13.06
4055	1	66	14	24	.6	4	7	206	2.26	482	5	ND	3	44	1	2	2	39	1.59	.047	5	11	.70	75	.02	3	1.01	.10	.16	1	265	13.06 - 15.71
4056	1	379	2706	2952	21.0	4	8	397	3.65	1140	5	4	3	48	38	13	2	6	1.43	.040	4	4	.45	41	.01	3	.33	.06	.17	1	2100	15.71 - 16.86
4057	1	141	113	337	11.0	4	9	465	2.82	1545	5	2	2	68	4	4	2	16	1.98	.048	4	4	.66	53	.01	4	.55	.08	.16	1	1250	16.86 - 17.76
4058	1	94	95	115	13.3	5	7	632	2.88	1106	5	2	3	71	1	6	2	25	2.30	.069	7	8	.72	64	.01	5	.86	.09	.15	1	6050	17.76 - 20.81
4059	1	62	8	26	.7	4	6	342	2.88	334	5	ND	3	51	1	2	2	43	1.54	.049	5	10	.77	99	.02	3	1.27	.13	.13	1	105	20.81 - 23.86
4060	1	61	8	20	.4	4	7	423	2.73	330	5	ND	3	49	1	2	2	49	1.75	.048	5	12	.82	171	.02	3	1.20	.11	.13	1	100	23.86 - 26.91
4061	1	71	6	47	.3	3	7	697	2.88	32	5	ND	3	70	1	2	2	31	2.89	.082	9	6	.78	233	.01	3	1.14	.10	.13	1	12	26.91 - 29.96
4062	1	65	6	31	.2	4	6	517	2.74	12	5	ND	3	58	1	2	2	35	2.23	.064	7	9	.74	207	.01	7	1.17	.11	.13	1	9	29.96 - 33.01
4063	1	58	64	161	2.5	4	6	432	2.79	302	5	6	4	52	2	3	2	44	1.64	.046	5	10	.75	162	.04	4	1.21	.11	.25	1	2200	33.01 - 36.06
4064	1	140	5	13	.3	3	8	289	2.87	96	5	ND	3	40	1	2	2	46	2.56	.050	5	12	.77	47	.02	6	1.24	.11	.12	1	150	36.06 - 39.11
4065	1	98	2	17	.1	4	6	240	2.82	13	5	ND	3	25	1	2	2	59	1.11	.048	3	12	.86	73	.10	3	1.30	.13	.13	2	11	39.11 - 42.16
4066	1	76	5	19	.1	4	7	298	2.76	16	5	ND	3	27	1	2	2	57	1.17	.050	4	14	.85	99	.10	5	1.35	.14	.21	1	17	42.16 - 45.21
4067	1	99	39	31	.7	5	6	676	2.94	95	5	ND	3	64	1	2	2	48	2.36	.048	5	15	.79	126	.04	6	1.21	.11	.24	1	125	45.21 - 48.26
4068	1	103	25	21	1.3	3	5	502	2.56	622	5	ND	3	76	1	2	2	34	2.76	.046	5	11	.70	94	.01	3	.98	.09	.14	1	285	48.26 - 51.31
4069	1	154	6	20	.8	4	7	444	2.81	28	5	ND	3	48	1	2	2	46	2.10	.047	6	13	.76	118	.01	5	1.16	.10	.13	1	36	51.31 - 54.36
4070	1	65	6	13	.4	13	12	264	2.29	402	10	ND	4	64	1	2	2	42	3.05	.051	5	11	.71	39	.01	8	.95	.08	.10	1	315	54.36 - 57.41
4071	1	94	4	15	.1	4	7	228	2.79	75	5	ND	4	35	1	2	2	54	1.67	.051	6	9	.81	67	.04	8	1.19	.11	.11	1	26	57.41 - 60.46
4072	1	65	2	13	.1	4	5	226	2.52	84	5	ND	3	31	1	2	2	53	2.03	.053	5	12	.83	53	.05	8	1.12	.10	.09	1	80	60.46 - 63.51
4073	1	77	6	12	.1	4	7	212	2.66	165	5	ND	4	27	1	2	2	57	1.63	.052	5	10	.86	60	.06	8	1.15	.10	.10	1	90	63.51 - 66.56
4074	1	122	3	10	.1	5	8	248	2.84	366	5	ND	4	30	1	2	2	50	1.82	.053	6	11	.82	95	.05	8	1.13	.10	.12	1	235	66.56 - 69.61
4075	1	59	6	22	.1	5	6	414	2.91	89	5	ND	4	36	1	2	2	64	1.37	.053	5	14	.93	226	.13	8	1.38	.14	.45	1	110	69.61 - 72.66
4076	1	124	6	23	.3	6	6	451	3.15	77	5	ND	3	58	1	2	2	73	2.11	.061	4	20	1.06	184	.08	8	1.75	.18	.24	1	25	72.66 - 75.71
4077	1	32	2	27	.1	19	10	474	2.83	150	7	ND	2	144	1	2	2	93	4.03	.059	2	64	1.25	151	.12	9	3.21	.33	.15	1	60	75.71 - 78.79
STD C/AU-0.5	19	59	38	137	7.2	71	29	1132	3.96	40	16	7	36	49	18	15	22	70	.48	.103	36	59	.88	184	.08	37	1.72	.09	.13	12	515	

DDH Y86-2

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au** PPB	Depth (m)
4078	3	51	5	29	.5	25	7	301	2.06	150	5	ND	3	6	1	2	2	36	.17	.041	8	75	.49	82	.01	8	.68	.03	.12	1	125	5.49 - 8.54
4079	4	50	8	16	.2	21	5	324	1.54	258	5	ND	3	16	1	2	2	20	.59	.023	6	14	.47	82	.01	7	.42	.03	.08	1	23	8.54 - 11.59
4080	4	39	2	12	.1	17	4	287	1.37	91	5	ND	2	16	1	2	2	17	.56	.023	5	13	.43	44	.01	6	.36	.03	.06	1	21	11.59 - 14.64
4081	8	71	2	18	.1	33	7	333	1.74	337	5	ND	2	16	1	3	2	26	.52	.013	4	27	.42	35	.01	5	.36	.03	.06	1	60	14.64 - 17.69
4082	3	51	3	28	.1	19	6	519	2.09	230	5	ND	3	21	1	3	2	48	.56	.032	6	34	.77	59	.02	7	.71	.04	.10	1	75	17.69 - 20.74
4083	6	91	11	90	2.4	60	17	1198	4.28	122	5	ND	3	62	1	2	2	91	1.44	.005	8	80	1.84	145	.11	10	1.73	.08	.42	1	208	20.74 - 23.79
4084	3	157	5	40	.1	38	13	1021	3.27	47	5	ND	2	21	1	2	2	67	1.08	.043	6	51	1.01	57	.08	9	1.11	.08	.33	1	14	23.79 - 26.84
4085	1	78	3	47	.2	23	8	991	2.37	156	5	ND	3	18	1	2	2	60	.56	.039	7	29	.81	208	.04	7	.87	.05	.17	1	32	26.84 - 29.89
4086	1	89	7	58	.2	45	13	1193	3.31	224	5	ND	3	23	1	2	2	67	.70	.038	7	56	1.14	88	.08	10	1.20	.05	.40	1	31	29.89 - 32.94
4087	1	46	5	41	.3	26	7	703	2.14	183	5	ND	3	32	1	2	2	31	1.44	.017	5	28	1.03	37	.01	9	.70	.04	.09	1	50	32.94 - 35.99
4088	2	37	6	40	.3	41	11	1154	2.49	92	5	ND	3	107	1	2	2	30	2.50	.055	8	37	1.51	148	.06	2	.88	.04	.31	2	65	35.99 - 39.04
4089	2	89	8	54	.1	66	21	1482	3.85	95	5	ND	2	38	1	2	2	98	.98	.072	10	82	1.90	224	.20	2	1.82	.04	.08	1	45	39.04 - 42.09
4090	1	58	4	83	.2	48	16	1259	2.99	158	5	ND	2	23	1	2	2	54	.84	.058	10	55	1.24	168	.07	2	1.30	.02	.31	1	50	42.09 - 45.14
4091	2	66	3	71	.1	45	14	863	2.81	282	5	ND	2	19	1	2	3	46	.80	.045	9	47	1.14	162	.07	2	1.30	.03	.32	1	47	45.14 - 47.60
4092	1	16	2	73	.1	12	13	1027	4.08	9	8	ND	1	101	1	2	3	80	3.55	.114	13	21	1.52	452	.01	7	1.93	.10	.11	1	4	47.60 - 50.65
4093	1	17	8	79	.1	12	14	1080	4.67	3	5	ND	1	105	1	2	6	111	3.47	.109	12	23	1.99	305	.01	3	2.36	.14	.08	1	2	50.65 - 53.70
4094	1	13	4	75	.1	9	11	1068	4.24	5	5	ND	1	104	1	2	2	80	3.06	.120	11	12	1.56	200	.02	5	1.99	.12	.09	1	3	53.70 - 55.96
4095	2	46	6	66	.3	35	15	897	3.14	67	5	ND	6	17	1	2	2	39	.87	.083	20	37	.94	117	.04	6	1.48	.03	.29	1	14	55.96 - 59.46
4096	1	12	10	75	.1	11	12	1120	4.09	9	6	ND	1	93	1	2	2	71	3.08	.118	13	14	1.42	200	.01	2	1.91	.11	.12	1	2	59.46 - 61.90
4097	2	67	7	68	.1	34	14	902	3.15	158	5	ND	10	12	1	5	2	31	.43	.029	21	30	.80	83	.07	5	1.32	.04	.52	1	47	61.90 - 64.55
4098	1	70	11	91	.2	45	21	2022	4.89	1184	5	ND	10	10	1	7	2	37	.20	.018	18	45	1.21	73	.13	4	1.83	.04	.95	1	250	64.55 - 67.60
4099	1	72	20	90	.4	25	9	911	2.25	192	5	ND	5	30	1	4	2	21	.47	.014	14	16	.77	100	.05	6	.93	.03	.41	1	50	67.60 - 70.65
4100	6	58	9	63	.3	29	11	1186	2.79	293	5	ND	7	30	1	2	2	27	.77	.072	19	18	.74	113	.04	5	1.04	.05	.38	1	150	70.65 - 73.70
4101	15	90	51	198	1.6	57	15	1381	3.23	454	5	ND	4	85	2	2	2	34	2.38	.041	10	15	.98	33	.01	6	.67	.05	.21	1	210	70.70 - 75.20
4102	2	29	12	82	.2	4	12	1213	4.18	16	5	ND	2	92	1	2	2	68	3.72	.121	17	7	1.28	255	.01	5	1.58	.10	.18	1	20	75.20 - 77.03
4103	1	174	170	333	2.3	58	31	5034	6.71	1065	6	ND	1	179	3	2	2	155	5.66	.036	8	134	2.83	39	.13	2	2.26	.18	.60	1	2100	77.03 - 78.86
4104	2	187	14	81	.6	68	32	6955	5.49	37	5	ND	1	94	1	2	2	154	4.37	.063	11	121	2.19	52	.17	4	2.53	.32	.37	1	54	78.86 - 81.30
STD C/FA AU	20	62	44	143	7.0	73	30	1165	3.97	34	17	8	38	51	19	16	22	72	.48	.111	41	62	.88	186	.09	36	1.73	.10	.13	13	49	

DDH Y86-2 (CONT.)

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au** PPB	Depth (m)
4105	1	97	6	92	.8	91	7	1174	1.31	794	5	ND	2	51	1	3	2	6	1.38	.217	10	17	.42	174	.01	9	.24	.04	.07	1	120	81.30 - 84.35
4106	1	140	26	80	2.0	34	26	3169	6.39	424	9	ND	2	140	1	3	2	116	4.15	.066	3	51	2.31	50	.05	2	1.41	.08	.25	1	315	84.35 - 86.03
4107	1	149	6	49	.3	58	29	854	4.68	15	5	ND	1	48	1	3	2	127	2.37	.035	2	105	2.84	55	.24	11	2.71	.28	.58	1	7	86.03 - 88.88
4108	1	109	68	190	1.1	74	28	1652	5.74	364	12	ND	2	118	2	3	2	127	4.78	.038	3	91	3.07	51	.13	5	2.14	.15	.63	1	115	88.88 - 91.93
4109	1	124	6	79	.3	65	23	1192	4.41	13	5	ND	2	51	1	2	2	114	2.70	.051	6	96	2.41	382	.26	4	2.56	.21	.98	1	8	91.93 - 94.98
4110	1	125	10	55	.3	57	26	749	4.21	17	5	ND	1	42	1	3	2	118	2.85	.033	2	126	2.94	74	.20	10	2.28	.22	.16	1	3	94.98 - 98.03
4111	1	120	4	53	.3	46	19	726	3.19	12	5	ND	1	29	1	3	2	90	2.52	.034	2	84	1.92	120	.25	12	1.79	.34	.19	1	5	98.03 - 101.08
4112	1	116	8	64	.3	67	23	919	4.15	596	5	ND	2	59	1	2	2	125	3.48	.040	4	92	1.93	48	.10	4	1.57	.14	.15	1	31	101.08 - 104.13
4113	1	60	6	55	.3	40	21	866	3.98	17	9	ND	2	47	1	2	2	120	3.95	.031	3	121	2.42	127	.27	11	2.01	.27	.35	1	11	104.13 - 107.18
4114	1	84	10	66	.6	54	24	1396	5.05	109	9	ND	2	98	1	2	2	148	5.72	.031	3	129	3.12	67	.17	6	1.99	.14	.42	1	90	107.18 - 110.50
4115	2	1541	22	159	6.6	57	59	1683	10.48	261	13	ND	2	126	2	2	2	166	4.92	.025	7	159	2.96	20	.05	2	1.69	.10	.25	1	65	110.50 - 111.72
4116	1	82	6	65	.3	50	24	987	5.37	24	5	ND	1	52	1	2	2	141	3.47	.029	2	152	3.19	101	.26	6	2.59	.15	.51	1	6	111.72 - 114.47

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DDH Y86-4

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au** PPB	Au** OZ/T	DEPTH (m)
4117	1	152	4	41	.2	49	22	735	4.87	15	5	ND	2	47	1	2	2	155	4.18	.039	3	130	2.40	26	.40	5	2.06	.24	.16	1	10		12.50 - 15.55
4118	1	101	8	42	.2	53	24	673	5.33	17	5	ND	2	31	1	2	3	163	2.65	.041	3	109	2.09	48	.41	2	2.14	.27	.30	2	6		15.55 - 18.60
4119	1	156	2	42	.4	58	29	701	5.06	54	5	ND	2	34	1	2	2	174	2.60	.043	3	130	2.42	124	.44	7	2.37	.20	.60	1	16		18.60 - 21.65
4120	1	73	2	37	.2	57	22	625	4.65	26	5	ND	2	26	1	2	2	137	2.18	.038	2	135	2.31	117	.40	2	2.24	.22	.62	1	7		21.65 - 24.70
4121	1	67	6	32	.1	50	25	609	3.85	41	5	ND	1	30	1	2	2	126	2.51	.034	2	126	1.86	60	.35	2	1.87	.23	.31	1	17		24.70 - 27.75
4122	1	110	140	32	1.1	53	24	619	4.17	75	5	ND	2	42	1	2	2	128	2.89	.039	3	120	1.84	119	.38	4	2.19	.27	.62	1	720		27.75 - 30.25
4123	1	1476	23	70	7.5	118	129	1082	12.74	30621	12	6	3	66	2	13	5	47	6.75	.007	2	40	.92	13	.02	2	.78	.08	.02	1	6000		30.25 - 30.85
4124	1	103	27	39	.6	55	22	680	4.68	19	5	ND	1	32	1	2	2	140	2.57	.041	2	139	2.35	97	.41	3	2.24	.19	.49	1	39		30.85 - 33.65
4125	1	94	53	32	.5	54	24	577	4.01	174	5	ND	1	36	1	2	2	114	2.28	.039	2	117	1.90	143	.36	3	2.06	.23	.78	1	160		33.65 - 37.55
4126	1	1387	13	89	3.9	57	150	894	12.78	12243	11	ND	2	46	2	2	3	83	3.80	.015	2	88	1.80	8	.03	2	1.42	.08	.02	1	1390		37.55 - 38.22
4127	1	124	8	37	.4	61	29	793	5.14	122	5	ND	2	50	1	2	2	146	3.38	.041	3	148	2.40	113	.35	4	2.34	.22	.56	1	120		38.22 - 41.27
4128	2	121	4	35	.3	60	25	655	4.68	51	5	ND	1	40	1	3	2	134	2.14	.036	3	137	2.39	208	.36	4	2.48	.22	1.06	1	14		41.27 - 44.32
4129	1	128	5	53	.3	41	26	532	4.13	148	5	ND	1	31	1	2	2	147	2.43	.041	2	57	2.00	83	.30	2	2.07	.21	.70	1	29	-	44.32 - 47.37
4130	2	240	10	74	.3	74	36	807	5.65	69	5	ND	1	28	1	2	2	129	2.11	.031	5	147	3.34	66	.25	5	2.70	.14	.50	1	18	-	47.37 - 50.42
4131	1	133	5	55	.3	55	29	810	4.39	486	5	ND	1	45	1	2	2	121	3.20	.031	2	145	2.48	69	.23	6	2.14	.17	.55	1	290	-	50.42 - 53.47
4132	1	103	12	45	.3	56	30	818	4.21	91	5	ND	1	47	1	2	2	126	3.04	.033	3	140	2.63	77	.24	3	2.20	.17	.60	1	31	-	53.47 - 54.97
4133	2	148	12	72	.5	61	31	1188	6.08	2670	5	ND	1	71	1	3	2	180	4.23	.033	2	182	4.38	71	.10	2	3.19	.15	.53	1	97	-	54.97 - 56.77
4134	1	1042	11	80	19.7	28	55	841	6.66	19548	10	94	1	111	2	47	7	54	3.92	.008	2	48	1.19	9	.01	2	.85	.06	.04	2	105000	2.770	56.77 - 57.53
4135	1	151	11	57	.9	41	24	1055	5.36	671	9	ND	1	128	1	2	2	156	5.08	.048	2	117	3.05	36	.05	3	2.42	.08	.28	1	190	-	57.53 - 58.90
4136	1	82	11	86	.6	67	34	1107	5.99	628	5	ND	1	79	1	2	2	209	4.02	.037	5	197	4.03	28	.12	4	2.94	.10	.19	1	121	-	58.90 - 60.40
4137	2	62	5	46	.3	15	11	1563	3.39	1172	18	ND	2	326	1	2	2	96	9.02	.048	4	38	2.25	4	.01	3	1.64	.08	.01	2	85	-	60.40 - 61.00
4138	2	144	9	69	.4	61	30	871	5.16	184	5	ND	1	53	1	2	2	149	3.17	.035	2	150	3.23	43	.25	6	2.52	.15	.29	2	32	-	61.00 - 64.05

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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DDH Y86-4 (CONT)

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au**	Au**	Depth (m)
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB	OZ/T	
4139	2	68	10	76	.2	51	27	749	4.96	46	5	ND	1	46	1	2	2	142	2.75	.036	2	155	3.05	68	.25	8	2.53	.15	.53	1	10	-	64.05 - 67.10
4140	1	55	7	65	.2	46	26	822	4.21	73	5	ND	1	69	1	2	2	130	4.09	.031	2	128	2.54	31	.19	5	2.07	.15	.19	1	51	-	67.10 - 70.15
4141	1	73	6	60	.2	48	25	530	3.48	40	5	ND	1	30	1	2	2	107	2.17	.040	2	80	2.01	48	.21	4	1.74	.17	.30	1	30	-	70.15 - 73.20
4142	1	126	13	56	.5	56	28	767	4.89	862	5	ND	1	42	1	2	2	121	2.77	.037	2	116	2.63	91	.21	4	2.39	.18	.54	1	1150	.035	73.20 - 76.03
4143	3	1713	26	38	2.4	96	176	976	14.97	520	7	ND	1	26	1	2	78	58	2.48	.013	2	35	1.09	15	.03	4	1.00	.07	.06	1	2450	.058	76.03 - 76.33
4144	1	215	10	53	.5	41	35	854	6.11	836	5	ND	1	45	1	2	4	157	2.87	.047	4	50	2.20	85	.18	5	2.15	.13	.55	1	310	-	76.33 - 79.38
4145	1	182	9	34	.4	32	26	743	5.02	6752	5	ND	1	39	1	2	2	126	2.96	.044	4	23	1.65	54	.12	6	1.58	.14	.24	1	540	-	79.38 - 82.43
4146	1	260	6	33	.3	33	33	701	5.18	32	5	ND	1	31	1	2	8	130	2.24	.048	2	31	1.63	58	.25	4	1.69	.16	.25	1	450	-	82.43 - 85.48
4147	1	198	2	27	.2	29	28	606	4.35	48	5	ND	1	27	1	2	2	106	1.95	.046	3	12	1.30	40	.21	5	1.53	.17	.17	1	34	-	85.48 - 88.53
4148	2	237	7	30	.3	28	32	679	4.97	166	5	ND	1	28	1	2	2	124	2.13	.055	3	10	1.33	36	.23	7	1.61	.18	.15	1	78	-	88.53 - 91.58
4149	1	208	11	29	.4	33	29	694	4.58	816	5	ND	1	45	1	2	2	115	3.06	.046	2	29	1.56	39	.16	6	1.72	.19	.16	1	83	-	91.58 - 94.63
4150	1	206	14	37	2.2	35	33	883	5.47	5649	5	ND	1	87	1	7	7	136	4.19	.047	2	45	1.92	21	.08	3	1.86	.15	.12	1	1050	.030	94.63 - 97.68
4151	1	368	13	32	1.9	41	64	651	5.44	4754	5	ND	1	49	1	2	9	86	3.56	.036	2	31	1.37	21	.08	3	1.63	.18	.08	1	600	-	97.68 - 100.73
4152	1	143	22	30	.6	41	31	584	3.70	400	5	ND	1	49	1	2	2	75	3.82	.035	3	47	1.36	17	.15	11	2.05	.22	.05	1	45	-	100.73 - 103.78
4153	1	104	18	34	.1	49	33	519	3.53	63	7	ND	1	66	1	2	2	73	3.13	.043	3	71	1.64	20	.18	4	2.27	.28	.07	2	19	-	103.78 - 106.83
4154	1	114	9	33	.4	43	32	687	3.85	45	9	ND	2	67	1	3	2	85	4.02	.036	3	87	1.83	37	.20	2	2.20	.23	.08	2	8	-	106.83 - 109.88
4155	1	98	17	30	.3	37	29	569	3.41	873	5	ND	1	51	1	2	2	74	3.19	.044	3	54	1.49	18	.15	6	1.84	.20	.05	2	27	-	109.88 - 112.93
4156	1	114	5	36	.2	39	27	551	3.26	426	5	ND	2	51	1	3	2	80	3.66	.041	3	67	1.52	18	.17	7	2.03	.23	.05	1	11	-	112.93 - 115.98
4157	1	147	17	40	.3	41	34	521	3.67	298	5	ND	2	49	1	2	2	80	3.02	.042	2	48	1.48	22	.18	5	1.90	.19	.05	1	190	-	115.98 - 119.03
4158	1	116	3	34	.3	31	28	609	3.76	837	10	ND	1	52	1	2	2	92	3.60	.037	4	45	1.65	22	.17	6	1.87	.16	.06	1	168	-	119.03 - 122.08
4159	1	122	10	28	.3	39	30	484	3.32	100	5	ND	1	47	1	2	2	85	2.77	.044	3	47	1.21	17	.19	4	1.62	.20	.05	1	21	-	122.08 - 125.13
4160	1	125	12	41	.3	47	30	458	3.17	157	5	ND	1	48	1	2	2	76	3.12	.042	2	67	1.52	22	.18	5	1.83	.21	.05	1	11	-	125.13 - 128.18
4161	1	149	11	49	.3	45	34	509	3.58	1380	5	ND	1	51	1	2	2	76	2.70	.041	4	59	1.55	22	.16	3	1.80	.21	.05	1	109	-	128.18 - 130.01
STD C/FA-AU	20	61	43	141	7.1	74	30	1140	3.97	42	16	8	36	50	19	17	19	70	.48	.110	36	61	.89	187	.09	34	1.73	.09	.15	12	52	-	

DDH Y86-5

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Depth (m)
4162	1	109	14	36	.2	33	20	528	3.01	15	10	ND	2	27	1	2	4	93	3.97	.039	2	89	1.67	19	.27	2	1.49	.16	.15	1	12	7.60 - 10.65
4163	1	182	10	50	.3	43	27	461	3.51	49	5	ND	1	26	2	2	2	105	2.31	.036	3	112	1.96	31	.25	3	1.80	.17	.22	1	24	10.65 - 13.70
4164	1	147	8	53	.4	44	25	522	3.79	31	5	ND	1	24	1	2	3	113	2.16	.041	4	114	1.93	15	.24	6	1.80	.18	.11	1	4	13.70 - 16.75
4165	2	118	8	53	.2	50	29	698	4.85	56	7	ND	1	39	1	2	9	130	3.29	.047	3	129	2.58	62	.27	5	2.26	.13	.46	1	2050	16.70 - 19.80
4166	2	169	20	59	.4	54	32	583	4.65	666	5	ND	1	28	1	2	4	122	2.10	.044	2	128	2.62	82	.26	6	2.35	.19	.65	1	55	19.80 - 22.85
4167	1	140	2	62	.2	54	37	554	4.44	61	5	ND	1	29	1	2	4	114	1.89	.041	2	138	2.64	85	.28	2	2.29	.13	.63	1	16	22.85 - 25.90
4168	2	355	10	71	.4	60	46	625	5.01	67	7	ND	1	30	2	2	2	114	2.50	.045	2	122	2.60	47	.25	10	2.39	.16	.31	1	30	25.90 - 28.95
4169	1	225	3	56	.4	60	37	522	4.03	49	5	ND	1	28	1	2	2	104	2.43	.034	3	142	2.81	25	.27	8	2.57	.21	.17	1	5	28.95 - 32.00
4170	1	139	21	47	.1	42	29	429	3.62	40	5	ND	1	26	1	2	2	91	2.52	.039	2	107	2.24	12	.23	4	2.26	.22	.06	1	4	32.00 - 35.05
4171	2	234	7	50	.4	58	37	540	3.95	56	5	ND	1	29	1	2	2	106	2.96	.038	3	127	2.12	53	.25	6	2.21	.23	.35	3	10	35.05 - 38.10
4172	1	77	3	41	.2	46	25	568	3.45	37	5	ND	1	29	1	2	4	90	3.15	.041	4	108	1.79	19	.24	5	1.84	.21	.12	1	2	38.10 - 41.15
4173	1	180	10	46	.3	50	35	553	3.72	50	5	ND	1	24	1	2	2	93	2.39	.038	3	110	1.83	35	.25	5	1.76	.18	.22	1	7	41.15 - 44.20
4174	2	157	15	52	.3	61	33	898	5.36	70	7	ND	2	58	1	2	3	107	4.75	.027	5	136	3.08	101	.20	5	2.45	.10	.67	4	180	44.20 - 47.25
4175	2	188	2	40	.2	44	38	703	5.11	164	9	ND	1	36	1	2	2	94	2.88	.045	5	120	2.76	50	.23	2	2.38	.15	.31	2	16	47.25 - 50.30
4176	2	62	14	37	.1	59	28	629	4.11	39	5	ND	1	36	1	2	3	93	2.33	.043	5	127	2.62	73	.28	7	2.39	.18	.46	3	3	50.30 - 53.35
4177	2	68	3	34	.1	44	24	517	3.69	19	5	ND	1	42	1	2	2	82	1.84	.037	3	107	2.27	111	.27	10	2.26	.21	.75	3	1	53.35 - 56.40
4178	1	64	2	34	.3	46	24	604	3.85	26	6	ND	1	40	1	2	3	93	2.91	.032	3	115	2.52	53	.25	9	2.27	.17	.43	3	7	56.40 - 59.45
4179	2	48	11	32	.1	42	23	522	3.52	18	5	ND	1	29	1	2	3	76	2.12	.035	2	111	2.21	49	.24	3	2.02	.14	.31	3	2	59.45 - 62.50
4180	1	106	5	27	.1	34	22	453	3.05	15	5	ND	1	31	1	2	2	67	2.10	.039	2	80	1.43	19	.23	7	1.42	.17	.09	7	34	62.50 - 65.80
4181	1	75	7	31	.1	36	20	474	3.21	23	5	ND	1	34	1	2	6	78	1.89	.037	3	94	1.66	45	.27	7	1.59	.17	.25	1	13	65.80 - 68.85
4182	1	163	10	31	.3	49	32	529	4.23	22	5	ND	1	36	1	2	2	82	1.92	.036	3	105	1.97	80	.26	5	1.99	.18	.47	3	200	68.85 - 71.90
4183	1	232	9	44	.1	62	40	626	5.55	25	5	ND	1	28	1	2	2	114	2.04	.038	2	132	3.27	95	.28	3	2.72	.12	.67	1	39	71.90 - 74.95
4184	1	197	4	44	.1	54	38	592	5.19	151	5	ND	1	27	1	2	6	117	1.77	.033	4	144	2.78	120	.27	2	2.53	.12	1.00	2	810	74.95 - 78.00
4185	1	319	16	35	.4	55	48	473	5.33	24	10	ND	1	27	1	5	2	100	1.44	.040	2	121	2.26	78	.29	5	2.34	.20	.71	3	7	78.00 - 81.05
4186	1	262	10	39	.1	61	38	512	4.98	19	7	ND	1	34	1	2	2	102	1.88	.037	4	118	2.49	88	.27	3	2.58	.21	.72	1	2	81.05 - 84.10
4187	1	378	7	31	.1	53	53	426	4.97	18	5	ND	1	25	1	2	2	78	1.49	.034	4	97	2.00	58	.24	2	1.90	.14	.49	1	5	84.10 - 87.15
4188	1	279	7	31	.1	51	38	423	4.30	18	5	ND	1	25	1	2	2	84	1.42	.038	5	94	2.02	62	.25	2	2.02	.19	.49	1	1	87.15 - 90.20
4189	1	165	7	34	.1	50	31	445	4.01	20	5	ND	1	28	1	2	2	81	1.55	.036	3	106	2.13	56	.24	2	2.05	.16	.46	1	2	90.20 - 93.25
4190	1	210	9	42	.2	57	36	566	4.93	27	6	ND	1	29	1	2	2	112	2.08	.034	3	129	2.58	59	.30	3	2.22	.15	.42	1	4	93.25 - 96.30
4191	2	230	15	49	.2	64	41	672	5.58	47	7	ND	1	33	1	2	5	118	2.18	.041	3	136	2.93	86	.29	2	2.51	.13	.60	2	11	96.30 - 99.35
4192	2	259	12	63	.1	62	42	702	5.84	29	7	ND	1	33	1	2	2	130	2.21	.045	6	144	2.42	76	.31	4	2.28	.12	.40	1	13	99.35 - 102.40
4193	1	39	12	72	.1	19	14	870	3.82	15	6	ND	2	64	1	2	3	56	3.08	.089	14	32	1.40	89	.08	2	2.07	.10	.15	1	2	102.40 - 105.45
STD C/FA-AU	21	60	38	134	7.0	67	29	1090	3.96	41	21	8	33	47	17	.15	18	62	.47	.109	39	58	.88	176	.08	34	1.72	.06	.13	12	52	

DDH Y86-5 (continued)

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au** PPB	Depth (m)
4194	1	13	12	75	.2	1	8	1011	3.78	3	5	ND	2	84	1	2	3	43	3.43	.110	14	1	1.13	127	.01	4	2.15	.13	.14	1	2	105.45 - 108.50
4195	1	2	9	65	.1	2	6	946	3.24	4	5	ND	5	83	1	2	3	45	2.72	.099	17	3	1.00	156	.01	3	1.28	.07	.10	1	1	108.50 - 111.55
4196	1	2	5	67	.1	2	7	946	3.27	2	5	ND	5	86	1	2	4	44	2.78	.100	17	2	.99	124	.01	2	1.26	.06	.11	1	1	111.55 - 114.60
4197	1	6	11	63	.2	4	7	905	3.21	3	5	ND	4	78	1	2	3	44	2.59	.097	20	2	.98	103	.01	2	1.27	.07	.12	1	1	114.60 - 117.65
4198	2	6	12	55	.1	3	6	915	3.14	2	5	ND	4	73	1	2	2	46	2.94	.097	23	4	.93	83	.01	2	1.22	.06	.11	1	1	117.65 - 121.00
4199	2	47	11	57	.1	56	25	784	4.76	28	7	ND	1	45	1	2	5	106	2.44	.037	2	139	3.27	50	.28	5	2.62	.12	.16	1	1	121.00 - 124.05
4200	2	74	16	49	.2	53	26	775	4.78	32	5	ND	1	34	1	2	2	99	1.87	.038	2	132	3.16	61	.28	2	2.55	.11	.35	2	9	124.05 - 127.10
4201	1	137	8	54	.2	60	31	905	5.57	43	5	ND	1	37	1	2	3	127	2.83	.037	2	151	3.26	44	.26	4	2.66	.08	.26	1	22	127.10 - 130.15
4202	2	74	11	66	.3	42	21	1204	5.16	70	5	ND	2	78	1	2	2	127	3.76	.048	5	130	2.79	154	.15	2	2.52	.09	.22	1	5	130.15 - 133.20
4203	1	33	26	77	.3	8	9	1057	3.44	41	5	ND	1	54	1	2	3	55	2.70	.084	12	30	1.21	65	.04	5	1.57	.07	.13	1	9	133.20 - 136.25
4204	1	73	14	64	.2	24	16	913	3.78	35	5	ND	1	45	1	2	2	61	2.37	.072	9	51	1.40	102	.12	2	1.65	.08	.24	1	14	136.25 - 139.30
4205	1	163	11	60	.3	60	31	885	5.56	116	7	ND	1	46	1	2	2	120	2.96	.030	2	133	2.65	92	.21	3	2.28	.07	.36	1	180	139.30 - 142.35
4206	2	110	7	44	.2	52.	22	763	4.55	39	5	ND	1	50	1	2	2	112	2.72	.042	2	116	2.29	139	.26	2	2.26	.13	.51	5	15	142.35 - 145.40
4207	2	160	14	51	.2	56	28	835	5.10	51	6	ND	2	47	1	3	2	115	2.88	.042	4	115	2.63	117	.27	3	2.30	.08	.47	1	42	145.40 - 147.45
4208	1	116	9	58	.1	58	29	896	5.57	50	5	ND	1	69	1	2	2	138	2.61	.042	3	124	3.10	145	.28	2	2.97	.15	.64	1	4	147.45 - 150.50
STD C/FA-AU	21	60	38	134	7.0	67	29	1090	3.96	41	21	8	33	47	17	15	18	62	.47	.109	39	58	.88	176	.08	34	1.72	.06	.13	12	49	

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DDH Y86-5 (continued)

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Au** OZ/T	Depth (m)
4209	1	35	5	67	.1	27	18	881	4.87	8	5	ND	1	90	1	2	2	130	3.06	.083	5	34	2.31	121	.16	2	2.46	.14	.05	1	5	-	150.50 – 153.53
4210	1	180	15	64	.9	7	26	865	5.30	559	5	ND	2	85	1	2	4	112	3.02	.085	6	10	1.60	55	.10	3	2.40	.13	.27	1	910	-	153.53 – 156.58
4211	1	95	22	129	1.1	67	29	1509	5.56	1132	5	ND	1	68	1	5	2	99	2.25	.061	5	82	2.30	60	.04	3	2.05	.03	.20	1	165	-	156.58 – 159.63
4212	1	92	34	62	1.4	24	16	1290	3.50	1825	5	ND	1	90	1	4	2	25	3.19	.052	5	15	1.63	50	.01	4	.62	.01	.15	1	515	-	159.63 – 162.68
4213	1	70	9	58	.6	35	14	932	3.06	570	5	ND	3	42	1	4	4	38	1.09	.056	9	29	1.08	85	.02	2	.99	.03	.19	1	215	-	162.68 – 165.73
4214	2	89	17	34	1.4	32	14	524	2.78	1902	5	ND	2	36	1	4	4	27	1.14	.046	8	22	.89	48	.01	2	.70	.02	.11	1	840	-	165.73 – 168.78
4215	8	74	39	114	2.4	27	13	609	2.52	1519	5	ND	1	28	1	5	4	21	.77	.028	6	24	.57	31	.01	2	.50	.01	.07	1	1440	.049	168.78 – 171.83
4216	1	131	9	52	2.3	33	15	764	2.48	1389	5	ND	2	46	1	4	2	29	1.12	.045	5	23	.89	35	.01	3	.65	.02	.07	1	690	-	171.83 – 174.88
4217	2	134	7	64	1.2	34	15	558	2.50	1266	5	ND	2	33	1	2	4	32	.91	.054	6	27	.77	58	.01	2	.65	.02	.11	1	375	-	174.88 – 177.93
4218	1	128	5	32	1.7	35	16	546	2.54	1604	5	ND	2	34	1	3	2	27	.93	.040	5	24	.73	42	.01	2	.60	.01	.09	1	1100	.036	177.93 – 180.98
4219	1	137	16	57	1.3	25	16	642	3.08	1661	5	ND	2	55	1	2	3	49	1.64	.053	4	26	1.02	70	.03	3	1.00	.05	.15	1	305	-	180.98 – 184.03
4220	1	116	4	35	.7	25	21	585	3.53	508	5	ND	1	72	1	2	3	100	2.85	.050	2	64	1.67	93	.08	2	1.66	.12	.24	1	295	-	184.03 – 187.08
4221	1	80	9	30	.2	33	19	568	3.38	156	5	ND	1	76	1	2	2	132	3.43	.044	2	87	1.91	81	.10	3	1.85	.14	.27	1	170	-	187.08 – 190.13
4222	1	75	13	35	.1	35	21	637	3.43	57	5	ND	1	79	1	2	2	131	3.74	.043	2	98	2.10	76	.10	3	1.85	.12	.19	1	33	-	190.13 – 193.18
4223	1	78	24	59	.2	33	22	1104	3.57	100	5	ND	1	70	1	2	2	138	3.78	.043	3	111	2.28	32	.09	2	1.73	.07	.11	1	102	-	193.18 – 196.23
4224	1	95	37	142	.6	31	24	1108	4.51	98	5	ND	2	107	2	4	2	174	5.12	.047	2	132	3.21	36	.07	2	2.17	.06	.23	272	170	-	196.23 – 199.28
4225	6	82	12	49	.6	34	24	1599	4.71	276	5	ND	2	106	1	3	2	141	5.10	.039	2	111	3.15	74	.08	3	1.89	.06	.43	1	255	-	199.28 – 202.33
4226	3	51	30	58	4.5	39	18	1455	4.14	623	5	3	2	89	1	6	2	14	3.56	.083	5	9	1.40	24	.01	2	.26	.01	.13	2	2460	.063	202.33 – 205.38
4227	1	137	22	34	2.7	4	22	1232	4.93	1264	5	ND	2	101	1	5	2	35	3.63	.087	3	4	1.58	38	.01	5	.82	.02	.21	1	650	-	205.38 – 208.43
4228	1	89	12	78	.7	5	19	990	5.03	1232	5	ND	1	82	1	3	2	87	2.91	.088	3	5	1.53	56	.04	2	1.55	.05	.29	1	275	-	208.43 – 211.43
4229	1	117	28	99	2.6	5	20	1114	4.80	710	5	ND	1	92	1	5	2	63	3.16	.083	2	4	1.38	40	.03	3	1.14	.05	.27	1	2940	.084	211.48 – 215.73
STD C/AU-R	19	55	41	140	7.0	74	31	1119	3.97	40	20	8	30	47	18	17	21	63	.48	.109	37	58	.88	173	.08	37	1.73	.06	.12	13	485	-	

GEOLOGICAL BRANCH ASSESSMENT REPORT

15,843

DDH Y86-6

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Depth (m)
4230	1	61	4	36	.2	12	15	892	3.97	26	8	ND	3	80	1	2	2	120	2.52	.068	3	48	1.66	203	.12	3	2.52	.25	.28	1	28	6.10 – 9.15
4231	1	97	7	31	.1	16	16	748	3.69	12	6	ND	3	65	1	2	2	108	2.51	.065	3	65	1.86	134	.12	3	2.20	.17	.18	1	5	9.15 – 12.20
4232	1	75	5	26	.1	18	15	558	3.18	9	5	ND	3	71	1	2	2	90	2.15	.066	3	60	1.43	120	.14	5	2.12	.22	.17	1	15	12.20 – 15.25
4233	1	98	10	28	.2	16	16	663	3.49	8	6	ND	3	72	1	2	2	103	2.46	.065	3	66	1.66	110	.13	4	2.21	.20	.14	2	24	15.25 – 18.30
4234	1	79	5	28	.1	16	15	563	3.42	15	5	ND	3	75	1	2	2	107	2.74	.068	3	69	1.61	63	.12	4	2.13	.17	.14	1	8	18.30 – 21.35
4235	1	65	10	31	.2	19	14	646	3.70	38	7	ND	3	101	1	2	2	118	3.49	.065	2	73	1.83	51	.11	6	2.33	.16	.15	1	350	21.35 – 24.40
4236	1	52	6	22	.1	16	11	505	3.00	54	5	ND	2	105	1	2	2	96	3.66	.054	3	56	1.35	88	.10	4	2.60	.18	.11	56	39	24.40 – 27.45
4237	1	37	49	89	1.1	24	11	733	3.37	1591	8	ND	2	96	1	5	2	87	3.44	.049	2	56	1.65	156	.05	4	2.01	.08	.29	2	580	27.45 – 28.81
4238	1	31	214	137	1.4	16	8	1043	2.66	635	6	ND	3	163	2	3	2	48	3.86	.048	2	37	1.21	86	.01	5	1.25	.02	.23	1	150	28.81 – 29.44
4239	1	95	2	18	.3	4	10	357	2.95	52	5	ND	3	36	1	2	2	60	1.33	.055	6	19	1.00	161	.08	2	1.40	.09	.26	1	33	29.44 – 32.02
4240	1	90	14	17	.2	3	10	286	2.76	34	5	ND	3	30	1	2	2	55	1.32	.052	5	17	.93	134	.09	4	1.27	.08	.23	2	50	32.02 – 35.07
4241	1	76	7	25	.1	5	8	236	2.62	39	5	ND	3	29	1	2	2	50	1.61	.049	5	16	.82	104	.08	2	1.17	.08	.18	1	44	35.07 – 38.12
4242	1	97	9	15	.1	5	9	206	2.82	49	3	ND	3	30	1	2	2	50	1.45	.051	4	17	.84	68	.07	4	1.24	.09	.16	1	32	38.12 – 41.17
4243	1	143	2	30	.2	3	11	297	2.90	104	5	ND	3	36	1	2	2	49	1.38	.051	4	15	.87	136	.05	3	1.27	.09	.22	1	2o	41.17 – 44.22
4244	1	134	5	15	.5	4	11	358	2 75	217	5	ND	3	49	1	2	2	38	1.86	.051	4	13	.77	108	.03	4	1.11	.07	.17	1	39	44.22 – 47.27
4245	1	130	57	22	.5	5	11	262	2.76	397	5	ND	3	36	1	2	3	48	1.40	.051	3	15	.81	86	.06	2	1.17	.09	.20	1	153	47.27 – 50.32
4246	1	128	5	14	.1	4	10	229	2.71	19	5	ND	3	29	1	2	2	47	1.17	.049	3	15	.78	97	.07	5	1.20	.09	.19	2	5	50.32 – 53.37
4247	1	137	6	17	.5	5	11	251	2.74	84	5	ND	3	36	1	2	2	42	1.52	.048	3	15	.76	59	.04	4	1.07	.06	.12	1	87	53.37 – 56.42
4248	1	107	4	21	.8	2	9	314	2.47	312	5	ND	3	62	1	2	2	35	2.17	.047	4	11	.72	58	.01	2	1.03	.05	.10	1	490	56.42 – 58.25
4249	1	13	2	71	.1	1	6	853	3.47	9	5	ND	3	90	1	2	3	19	2.92	.145	14	3	.87	92	.01	2	1.41	.04	.13	1	5	58.25 – 59.47
4250	1	16	9	66	.1	1	7	901	3.23	7	5	ND	3	100	1	2	3	17	3.12	.143	14	1	.86	166	.01	5	1.28	.04	.13	1	2	59.47 – 60.69
4251	1	127	3	17	.1	3	11	221	2.80	28	5	ND	3	45	1	2	2	39	1.47	.049	3	12	.76	71	.02	4	1.15	.06	.12	1	7	60.69 – 64.04
4252	1	120	11	16	.4	5	9	307	2.75	70	5	ND	3	57	1	2	2	41	1.89	.047	3	14	.79	76	.02	2	1.14	.06	.14	1	23	64.04 – 67.09
4253	1	50	7	21	.2	6	7	312	2.59	166	5	ND	2	37	1	2	2	43	1.25	.047	2	13	.77	124	.06	2	1.11	.07	.24	1	25	67.09 – 69.53
4254	1	39	114	299	3.0	3	5	386	2.22	927	5	ND	2	83	6	5	2	8	2.10	.036	2	3	.51	50	.01	3	.37	.02	.13	1	605	69.53 – 70.13
4255	1	67	6	13	.1	4	8	236	2.75	24	5	ND	3	38	1	2	2	46	1.47	.050	4	15	.80	83	.03	2	1.26	.08	.18	1	1	70.13 – 73.18
4256	1	60	5	14	.2	5	8	286	2.52	100	5	ND	3	50	1	2	2	40	1.93	.047	4	13	.74	45	.02	3	1.12	.06	.11	1	72	73.18 – 76.23
4257	1	63	6	14	.1	5	8	312	2.51	79	5	ND	3	56	1	2	2	39	2.15	.047	3	11	.74	42	.02	7	1.07	.05	.10	1	35	76.23 – 79.28
4258	1	65	9	32	.2	5	8	375	2.91	18	5	ND	3	45	1	2	2	36	1.68	.072	7	10	.79	61	.04	2	1.20	.06	.12	1	13	79.28 – 80.78
4259	1	57	7	37	.1	3	8	425	2.90	15	5	ND	3	49	1	2	2	33	1.76	.081	7	8	.79	57	.03	2	1.20	.06	.12	1	5	80.78 – 83.83
4260	1	69	6	27	.1	4	8	400	2.70	40	5	ND	2	42	1	2	2	35	1.35	.063	5	10	.79	239	.01	2	1.16	.04	.10	1	27	83.83 – 86.88

GEOLOGICAL BRANCH ASSESSMENT REPORT

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TO ACCOMPANY REPORT BY R.E. Gale

LEGEND

SURVEY POINT WITH Nº. & ELEVATION IN METRES

CREEK

YUNIMAN PROJECT	
FOR: TOBY CREEK RESOURCES LTD.	
BY: SHANGRI - LA MINERALS LIMITED	
SURVEY PLAN	
OSOYOOS M.D., B.C.	
N.T.S. 82E / 5W	DATE : OCTOBER 1986
DRAWN BY :	FIGURE Nº. 2

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

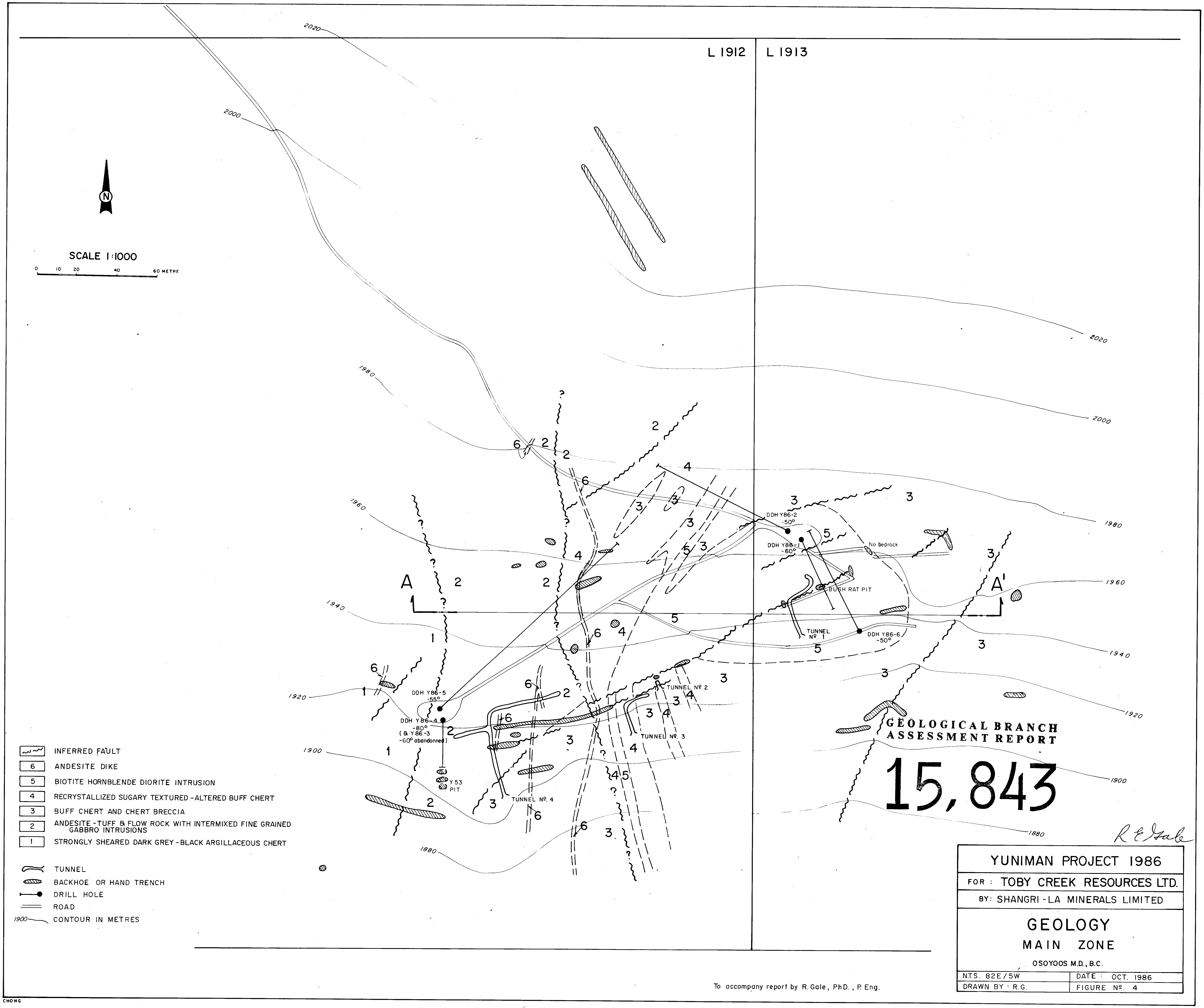
BY: SHANGRI - LA MINERALS LIMITED

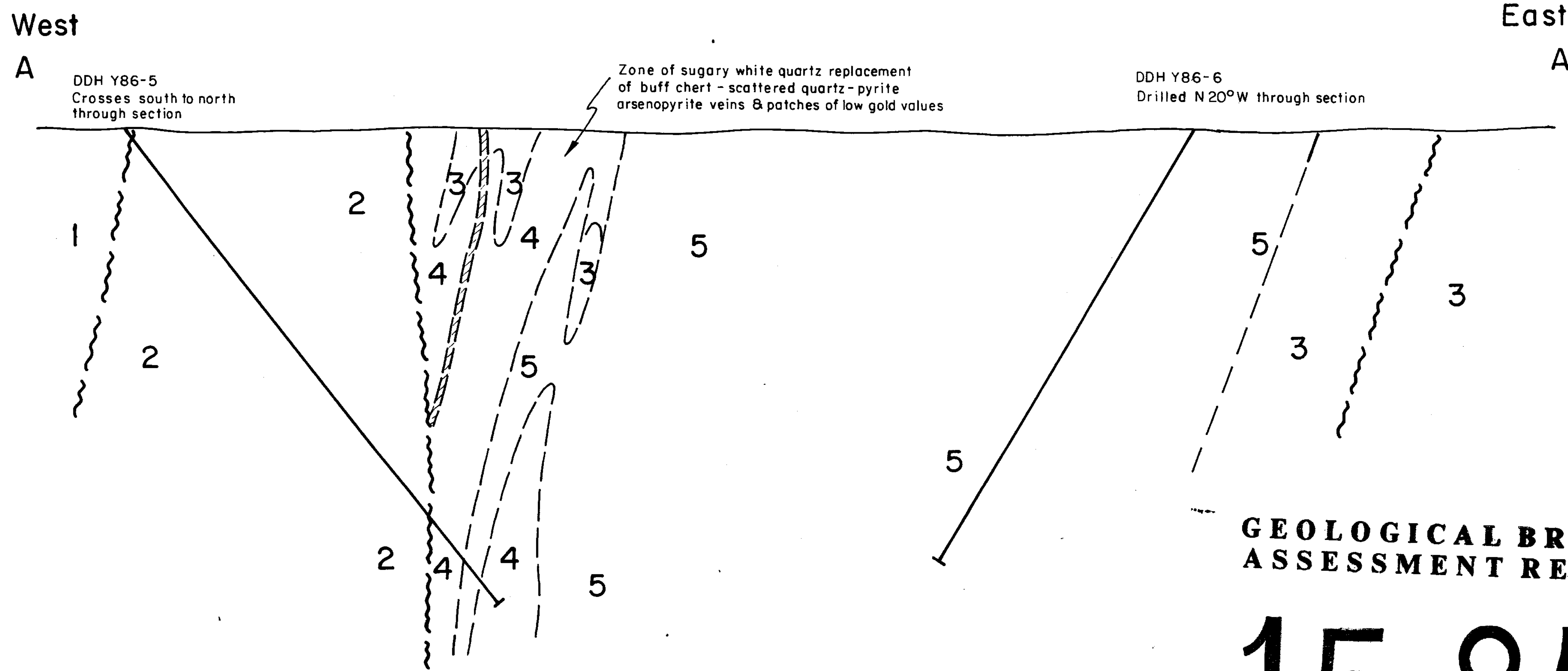
SURVEY PLAN

OSOYOOS M.D., B.C.

N.T.S. 82E / 5W	DATE : OCTOBER 1986
DRAWN BY :	FIGURE No. 3

R E Gale


L 1912
L 1913
SCALE 1:1000
0 10 20 40 60 METRE
N
2020
2000
1980
1960
1940
1920
1900
1880
A
A'
DDH Y86-2 -50°
DDH Y86-1 -60°
DDH Y86-5 -55°
DDH Y86-4 -80° (& Y86-3 -60° abandonned)
DDH Y86-6 -50°
No bedrock
BUSH RAT PIT
TUNNEL Nº. 1
TUNNEL Nº. 2
TUNNEL Nº. 3
TUNNEL Nº. 4
Y53 PIT
INFERRED FAULT
6 ANDESITE DIKE
5 BIOTITE HORNBLENDE DIORITE INTRUSION
4 RECRYSTALLIZED SUGARY TEXTURED - ALTERED BUFF CHERT
3 BUFF CHERT AND CHERT BRECCIA
2 ANDESITE - TUFF & FLOW ROCK WITH INTERMIXED FINE GRAINED GABBRO INTRUSIONS
1 STRONGLY SHEARED DARK GREY - BLACK ARGILLACEOUS CHERT
TUNNEL
BACKHOE OR HAND TRENCH
DRILL HOLE
ROAD
1900 CONTOUR IN METRES
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,843
R E Gale
YUNIMAN PROJECT 1986
FOR: TOBY CREEK RESOURCES LTD.
BY: SHANGRI-LA MINERALS LIMITED
GEOLOGY
MAIN ZONE
OSOYOOS M.D., B.C.
N.T.S. 82E/5W
DATE: OCT. 1986
DRAWN BY: R.G.
FIGURE Nº. 4
To accompany report by R. Gale, PhD., P. Eng.
CHONG



- INFERRED FAULT
- ANDESITE DIKE
- 5 BIOTITE - HORNBLENDE DIORITE INTRUSIVE STOCK
- 4 RECRYSTALLIZED - SUGARY TEXTURED ALTERED BUFF CHERT
- 3 BUFF CHERT AND CHERT BRECCIA
- 2 ANDESITE - TUFF & FLOW ROCK WITH INTERMIXED FINED GRAINED GABBRO INTRUSIONS.
- 1 STRONG SHEARED DARK GREY TO BLACK ARGILLACEOUS CHERTY
- DRILL HOLE CUTTING SECTION

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TO ACCOMPANY REPORT BY R.E. GALE, PhD., P. ENG.

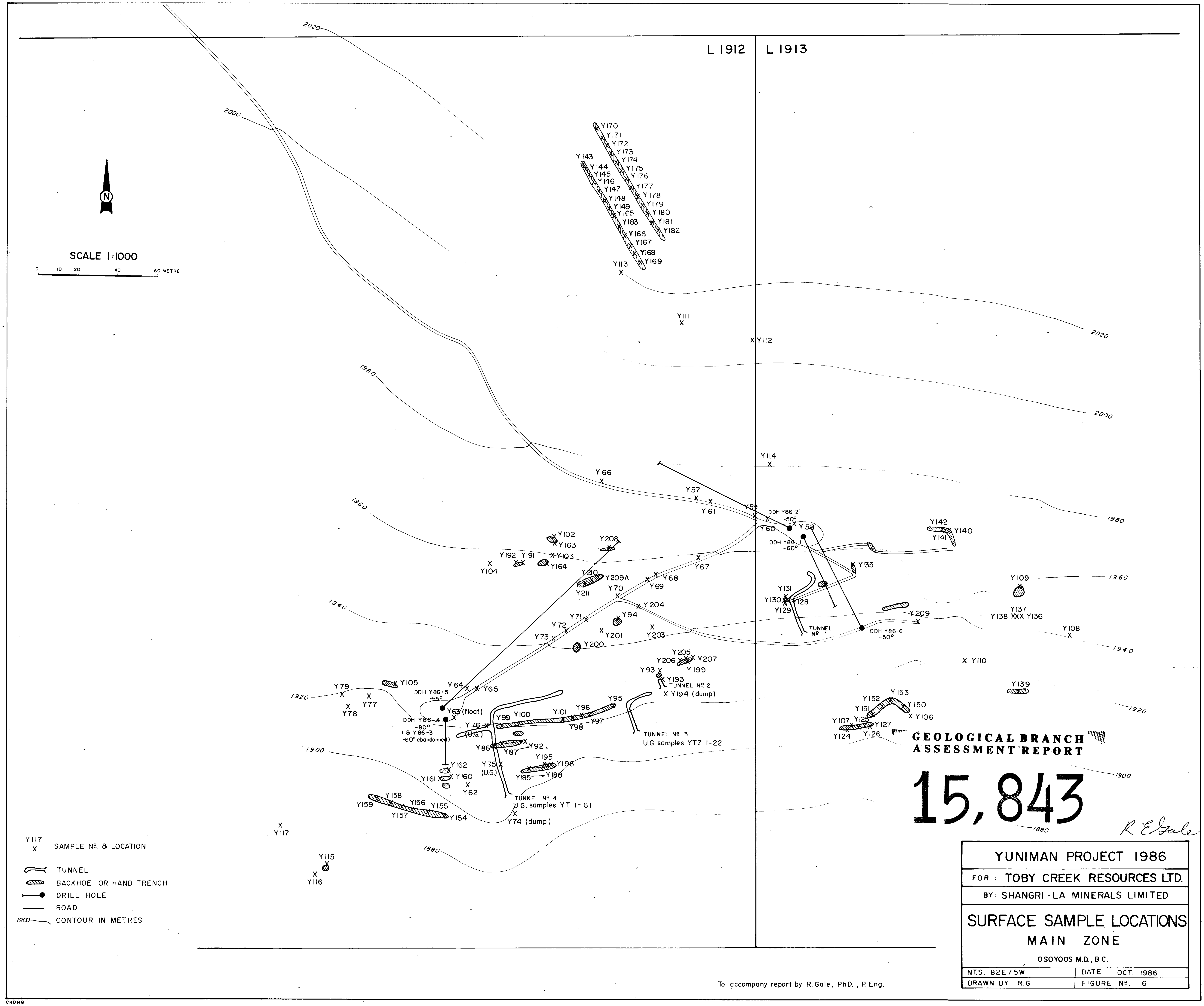
SCALE 1:1000

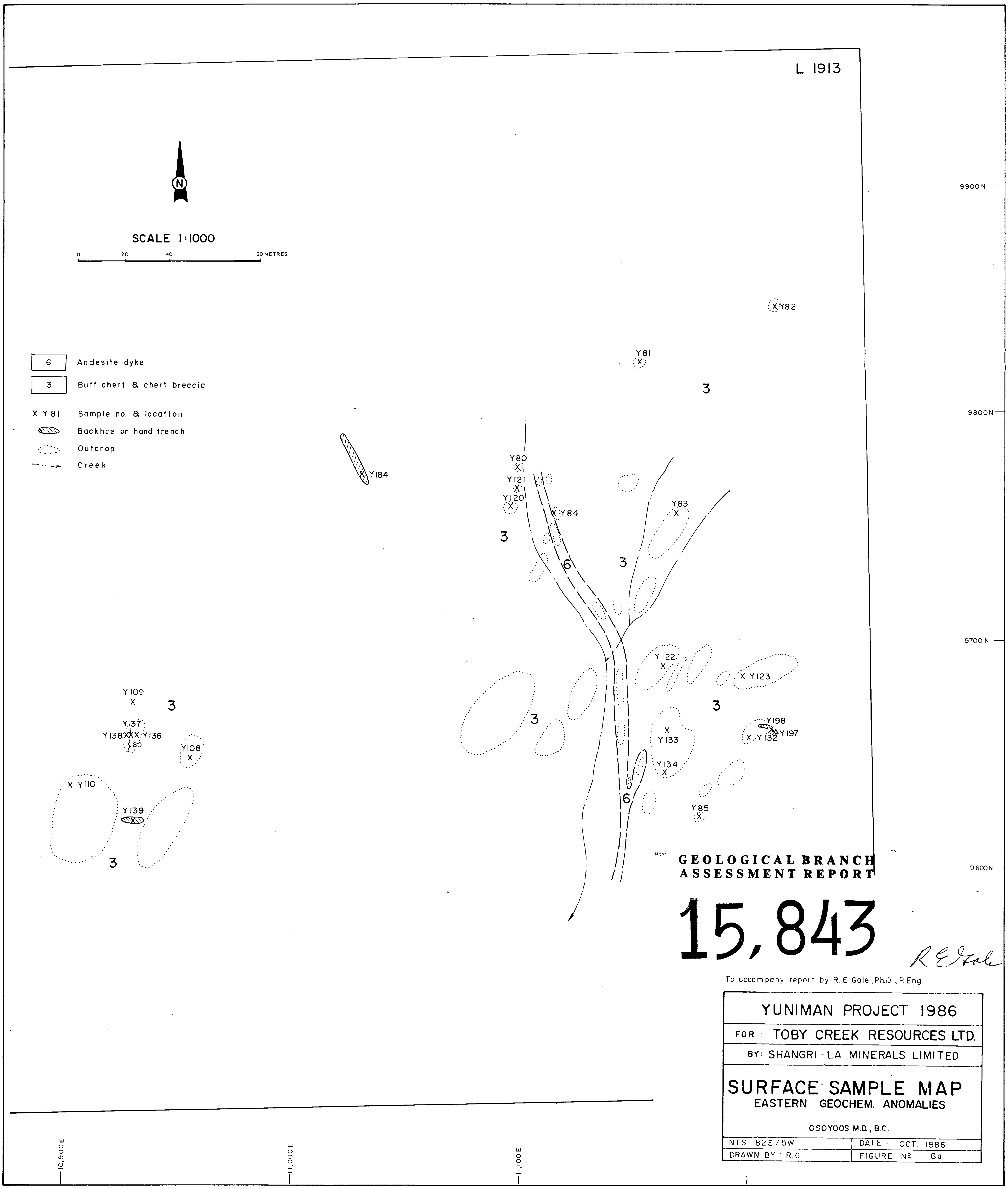
0 10 20 50 METRES

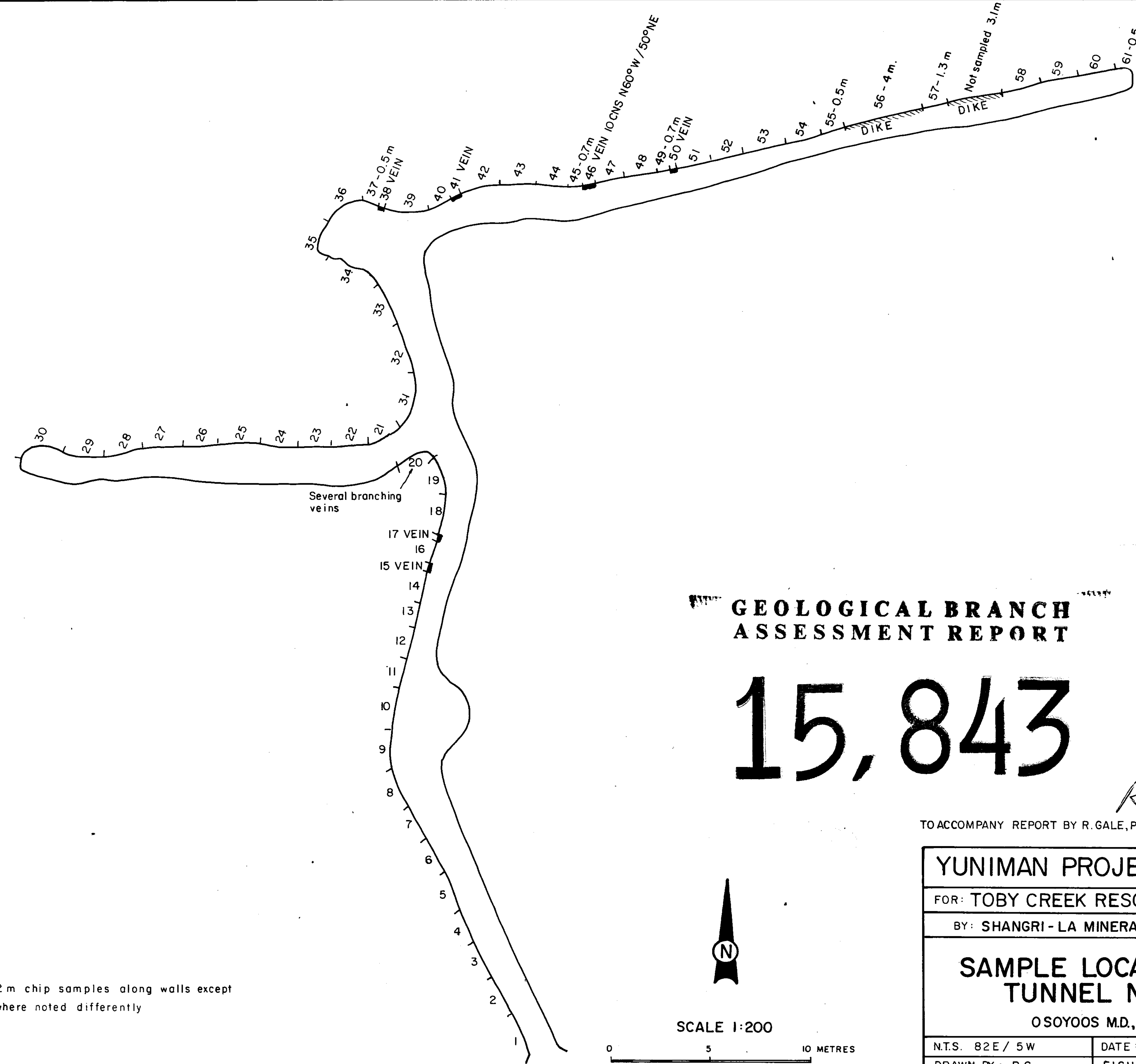
YUNIMAN PROJECT 1986	
FOR: TOBY CREEK RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LIMITED	
DIAGRAMMATIC CROSS-SECTION (MAIN ZONE) OSOYOOS M.D., B.C.	
N.T.S. 82 E / 5 W	DATE: OCT. 1986
DRAWN BY: R. G.	FIGURE Nº. 5

CHONG

R E Gale


L 1912
L 1913
SCALE 1:1000
0 10 20 40 60 METRE
N
Y117 X SAMPLE No. & LOCATION
TUNNEL
BACKHOE OR HAND TRENCH
DRILL HOLE
ROAD
1900 CONTOUR IN METRES
GEOLOGICAL BRANCH ASSESSMENT REPORT
15,843
R E Gale
YUNIMAN PROJECT 1986
FOR: TOBY CREEK RESOURCES LTD.
BY: SHANGRI-LA MINERALS LIMITED
SURFACE SAMPLE LOCATIONS
MAIN ZONE
OSOYOOS M.D., B.C.
N.T.S. 82E/5W
DATE OCT. 1986
DRAWN BY RG
FIGURE No. 6
To accompany report by R. Gale, PhD., P. Eng.
TUNNEL No. 1
TUNNEL No. 2
TUNNEL No. 3 U.G. samples YTZ 1-22
TUNNEL No. 4 U.G. samples YT 1-61
DDH Y86-1 -60°
DDH Y86-2 -50°
DDH Y86-4 -80° (& Y86-3 -60° abandoned)
DDH Y86-5 -55°
DDH Y86-6 -50°
Y63 (float)
X Y194 (dump)
Y74 (dump)
CHONG


L 1913
N
SCALE 1:1000
0 20 40 80 METRES
6 Andesite dyke
3 Buff chert & chert breccia
X Y81 Sample no. & location
Backhce or hand trench
Outcrop
Creek
Y82
Y81
Y184
Y80
Y121
Y120
Y84
Y83
Y122
Y123
Y198
Y197
Y132
Y133
Y134
Y85
Y109
Y137
Y138
Y136
80
Y108
Y110
Y139
9900 N
9800 N
9700 N
9600 N
10,900 E
11,000 E
11,100 E
GEOLOGICAL BRANCH
ASSESSMENT REPORT
15,843
To accompany report by R. E. Gale, Ph.D., P.Eng.
YUNIMAN PROJECT 1986
FOR: TOBY CREEK RESOURCES LTD.
BY: SHANGRI-LA MINERALS LIMITED
SURFACE SAMPLE MAP
EASTERN GEOCHEM. ANOMALIES
OSOYOOS M.D., B.C.
N.T.S. 82E/5W
DATE: OCT. 1986
DRAWN BY: R.G.
FIGURE Nº 6a



2 m chip samples along walls except where noted differently

GEOLOGICAL BRANCH ASSESSMENT REPORT

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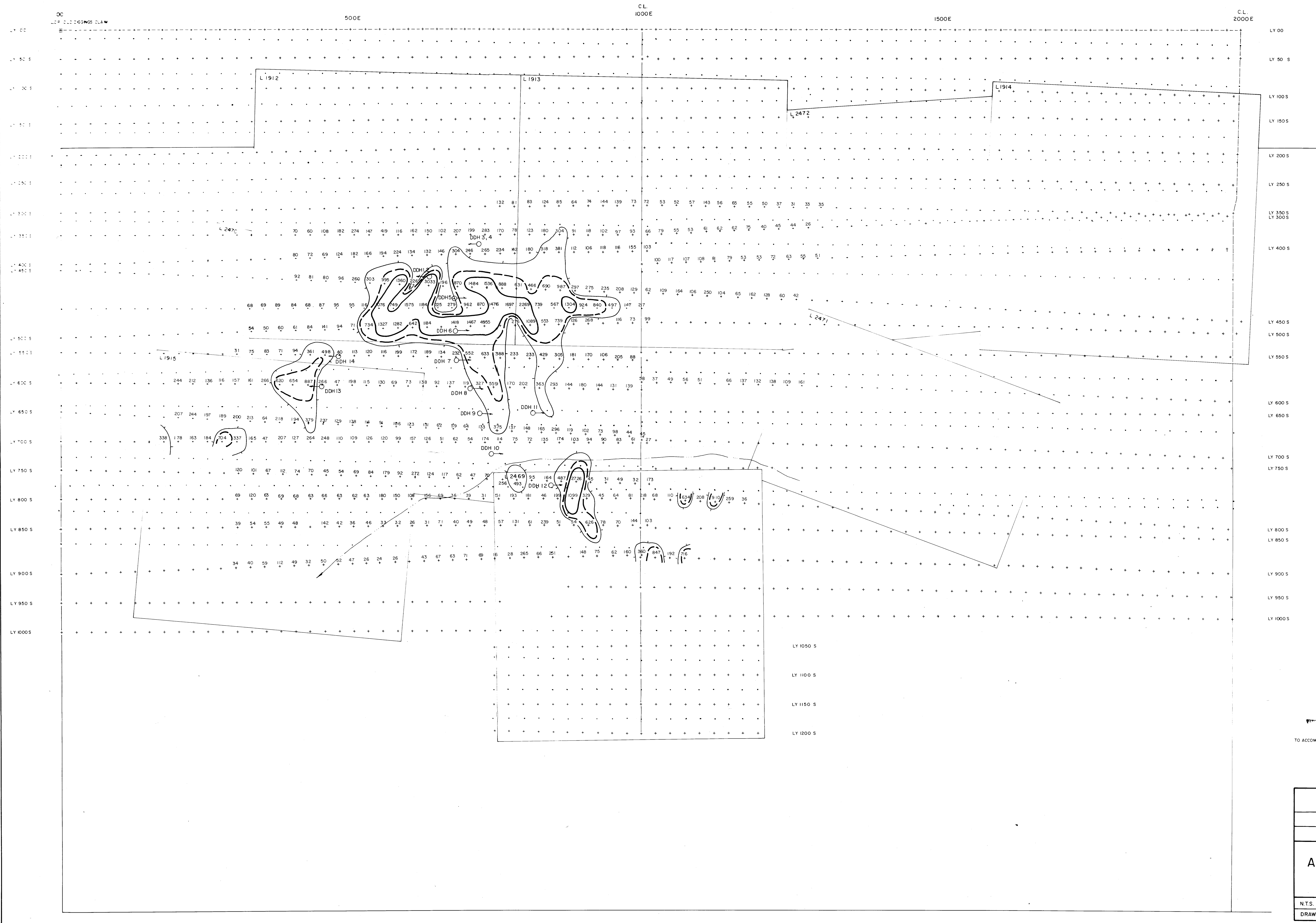
TO ACCOMPANY REPORT BY R. GALE, PhD., P. ENG.

YUNIMAN PROJECT 1986	
FOR: TOBY CREEK RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LIMITED	
SAMPLE LOCATIONS TUNNEL No. 4 OSOYOOS M.D., B.C.	
N.T.S. 82E/5W	DATE: OCT. 1986
DRAWN BY: R.G.	FIGURE No. 7

CHONG



PROPOSED DRILL HOLES

DDH 1, 2 – Near DDH Y86-4, to be drilled at -50°, -70° for 200 m. & 100 m.

DDH 3, 4 – West of tunnel Nº. 1, to be drilled at -50°, -70° for 100m & 200 m.

DDH 5 to 14 – To be drilled at -50° for 100m to test I.P. &/or geochem. anomalies.

300 ppm As
500 " "
1000 " "

BASED ON 1985 SOIL SAMPLE RESULTS

N

SCALE 1:2500

0 50 100 200 METRES

GEOLOGICAL BRANCH
ASSESSMENT REPORT

TO ACCOMPANY REPORT BY R. GALE, PhD, P.ENG.

15,843

YUNIMAN PROJECT 1986

FOR TOBY CREEK RESOURCES LTD.

BY SHANGRI-LA MINERALS LIMITED

ARSENIC GEOCHEMISTRY

OSOYOOS M.D., B.C.

N.T.S. 82E/5W	DATE: OCT. 1986
DRAWN BY: R.G.	FIGURE Nº. 9

GEOLOGICAL BRANCH ASSESSMENT REPORT

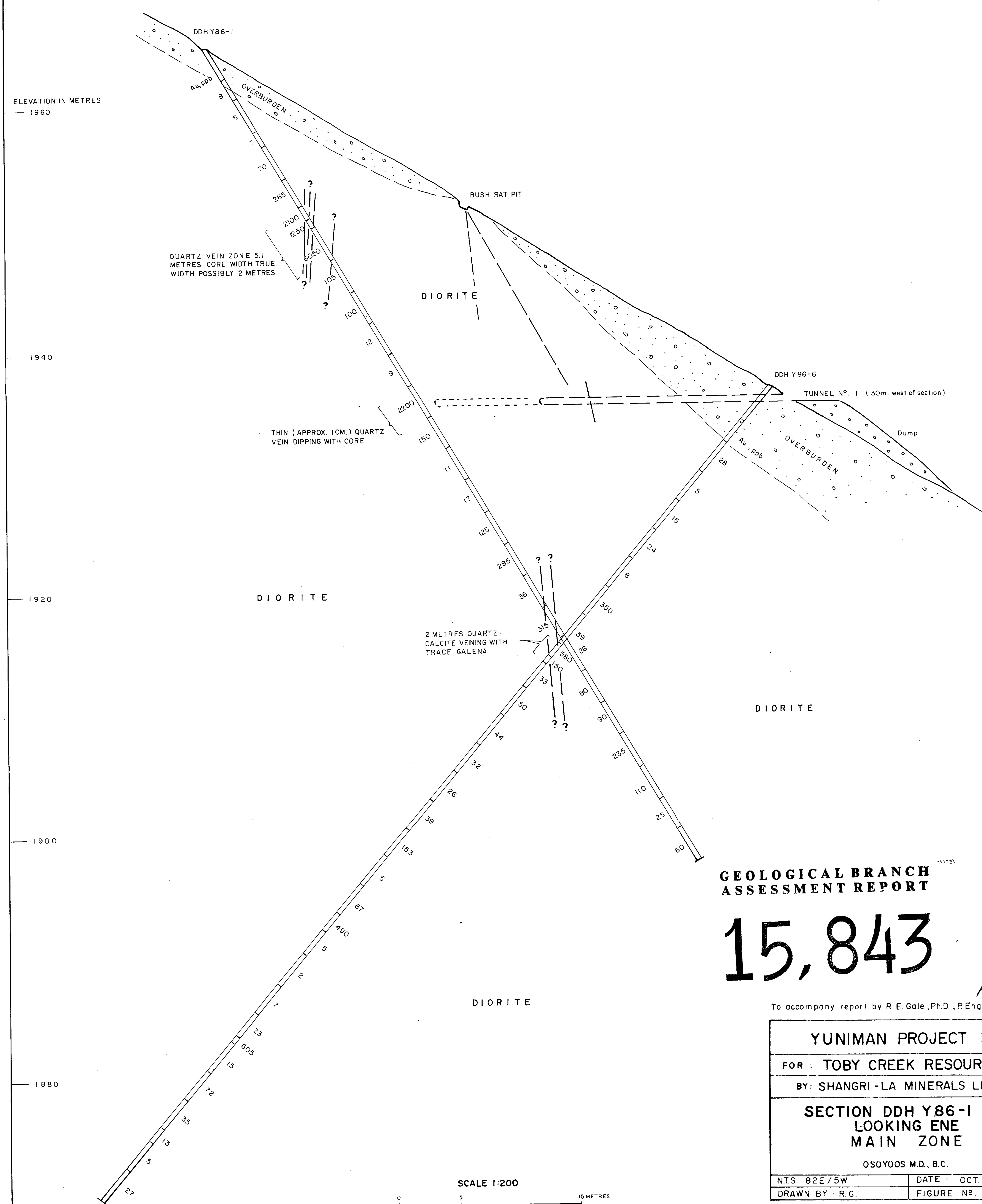
15,843

TO ACCOMPANY REPORT BY

R E Gale

YUNIMAN PROJECT 1986	
FOR TOBY CREEK RESOURCES LTD.	
BY SHANGRI-LA MINERALS LIMITED	
GOLD GEOCHEMISTRY OSOYOOS M.D., B.C.	
N.T.S. 82E/5W	DATE: OCT. 1986
DRAWN BY: R.G.	FIGURE No. 10

CHONG



GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843

R.E. Gale

To accompany report by R. E. Gale, Ph.D., P.Eng

YUNIMAN PROJECT 1986

FOR: TOBY CREEK RESOURCES LTD.

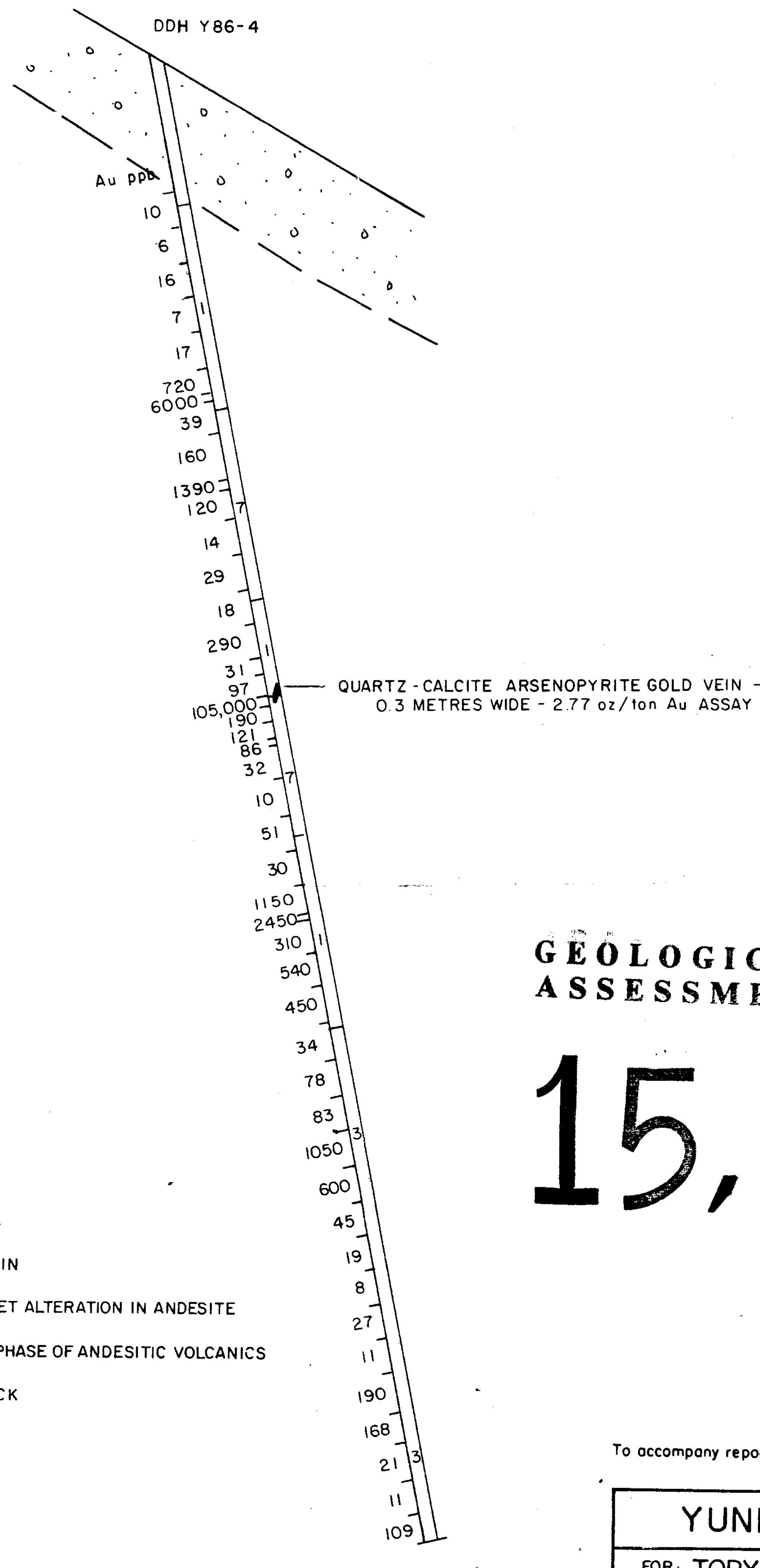
BY: SHANGRI-LA MINERALS LIMITED

SECTION DDH Y86-1 & 6
LOOKING ENE
MAIN ZONE

OSOYOOS M.D., B.C.

N.T.S. 82E/5W	DATE: OCT. 1986
DRAWN BY: R.G.	FIGURE No. 11

CHONG



GEOLOGICAL BRANCH ASSESSMENT REPORT

15,843

ROCK TYPES

- OVERBURDEN - LOOSE ROCK
- GOLD - BEARING QUARTZ VEIN
- 7 SCAPOLITE ? - CALCITE - GARNET ALTERATION IN ANDESITE
- 3 GABBROIC - MEDIUM GRAINED PHASE OF ANDESITIC VOLCANICS
- 1 ANDESITE TUFF & FLOW ROCK

R E Gale

To accompany report by R. E. Gale, Ph.D., P. Eng.

SCALE 1:500

0 10 20 30 METRES

YUNIMAN PROJECT 1986

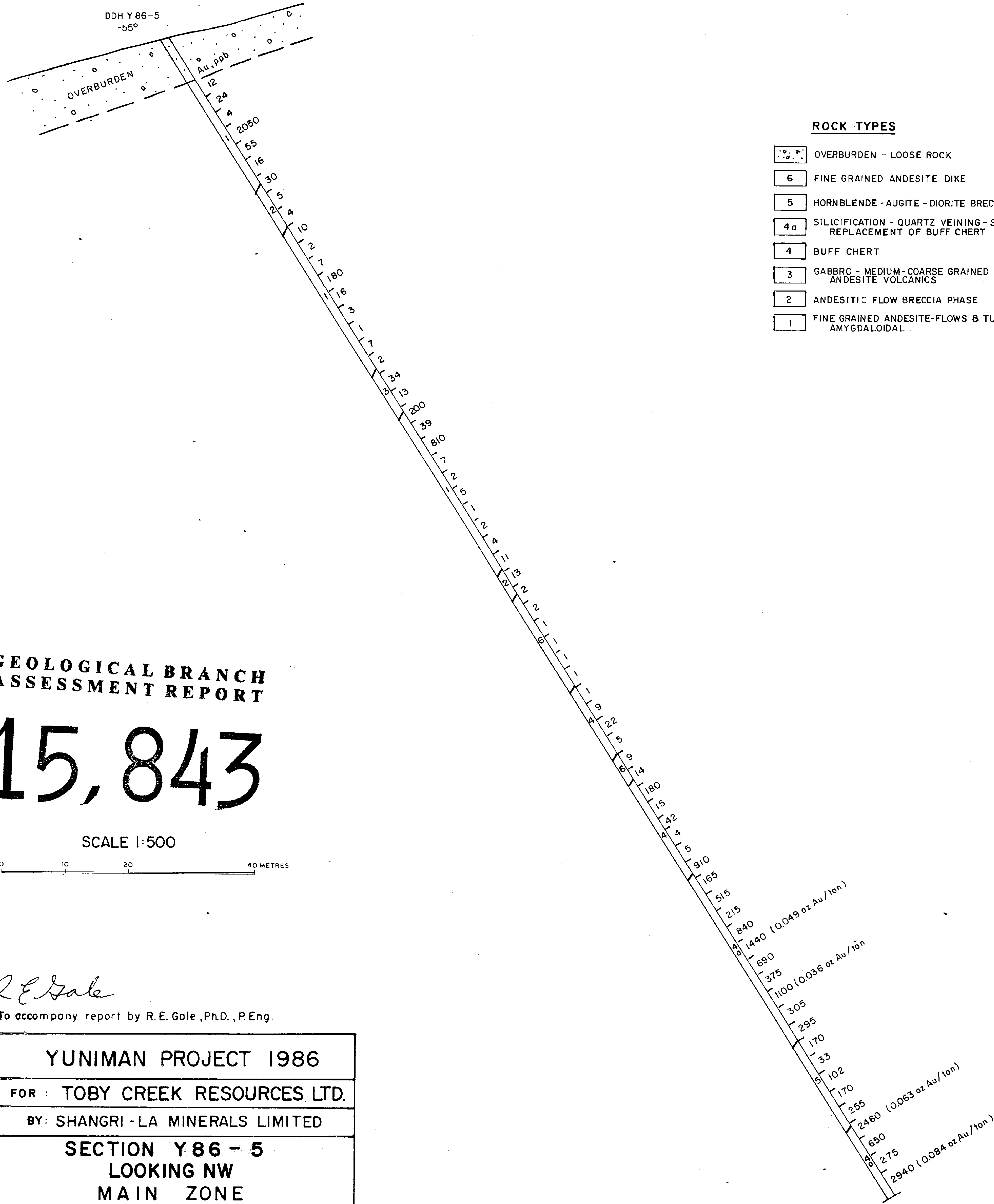
FOR: TOBY CREEK RESOURCES LTD.

BY: SHANGRI - LA MINERALS LIMITED

SECTION Y86 - 4
LOOKING EAST
MAIN ZONE
OSOYOOS M.D., B.C.

N.T.S. 82E / 5W	DATE: OCT. 1986
DRAWN BY: R. G.	FIGURE Nº. 13

CHONG



ROCK TYPES

(symbol)	OVERBURDEN - LOOSE ROCK
6	FINE GRAINED ANDESITE DIKE
5	HORNBLENDE - AUGITE - DIORITE BRECCIA DIKE
4a	SILICIFICATION - QUARTZ VEINING - SUGARY QUARTZ REPLACEMENT OF BUFF CHERT
4	BUFF CHERT
3	GABBRO - MEDIUM - COARSE GRAINED PHASE OF ANDESITE VOLCANICS
2	ANDESITIC FLOW BRECCIA PHASE
1	FINE GRAINED ANDESITE-FLOWS & TUFFS OFTEN AMYGDALOIDAL .

SCALE 1:500

0 10 20 40 METRES

R E Gale

To accompany report by R. E. Gale, Ph.D., P. Eng.

YUNIMAN PROJECT 1986

FOR : TOBY CREEK RESOURCES LTD.

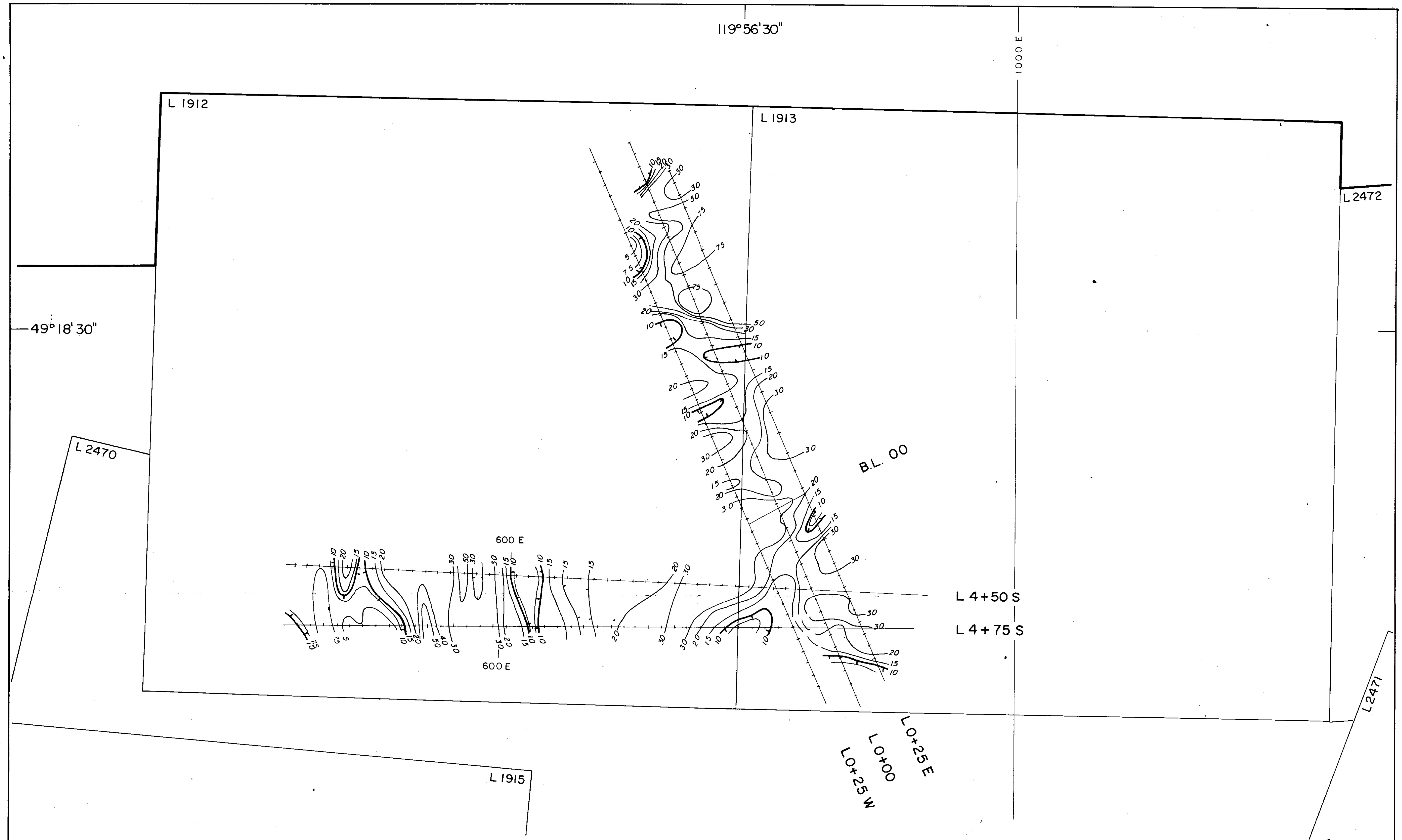
BY: SHANGRI - LA MINERALS LIMITED

SECTION Y86 - 5
LOOKING NW
MAIN ZONE

OSOYOOS M.D., B.C.

N.T.S. 82E / 5W	DATE : OCT. 1986
DRAWN BY : R.G.	FIGURE Nº 14

CHONG



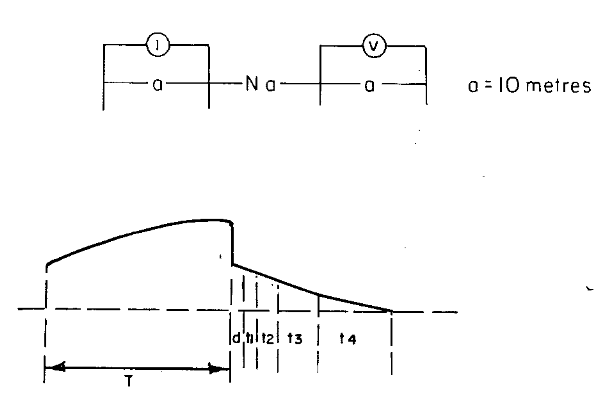
TO ACCOMPANY REPORT BY R.E. GALE, Ph.D., P. ENG.

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843

SCALE 1:25.00

0 50 100 150 METRES



T Pulse duration	d Delay time	Window widths (msec) t1	t2	t3	t4
2000 msec	120 msec	120	220	420	820

YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

BY: SHANGRI-LA MINERALS LIMITED

I.P. TEST SURVEY
N = 1
CHARGEABILITY Mt(msec.)

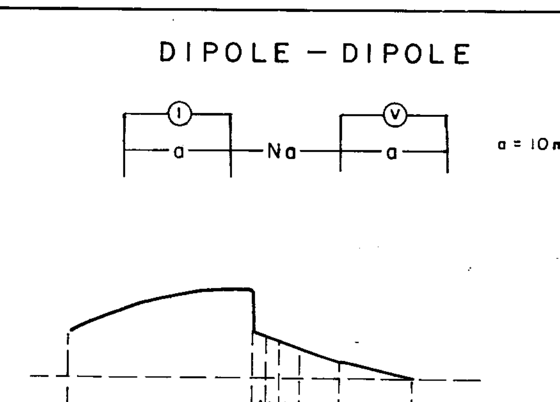
OSOYOOS M.D., B.C.

N.T.S. 82E/5W	DATE: AUGUST 1986
DRAWN BY: M.S.	FIGURE Nº. A1a

CHONG

R E Gale

TO ACCOMPANY REPORT BY R.E. GALE, Ph.D., P. ENG.



T Pulse duration	d Delay time	Window widths (msec) t1	t2	t3	t4
2000 msec	120 msec	120	220	420	820

SCALE 1:2500

0 50 100 150 METRES

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

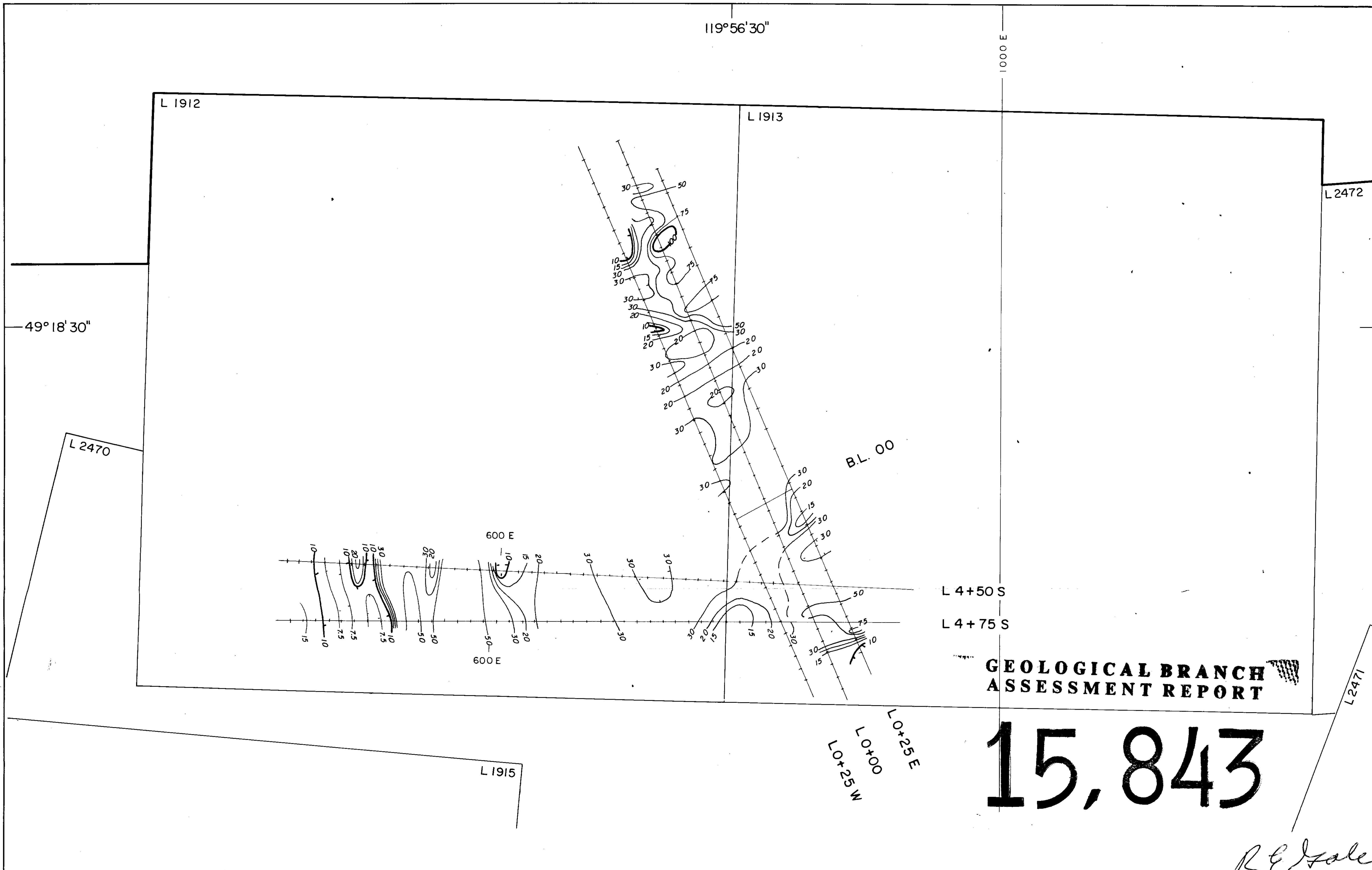
BY: SHANGRI-LA MINERALS LIMITED

I.P. TEST SURVEY
N = 1
APPARENT RESISTIVITY RHO (KΩ-m)

OSOYOOS M.D., B.C.

N.T.S. 82E/5W	DATE: AUGUST 1986
DRAWN BY: M.S.	FIGURE Nº. A1b

CHONG

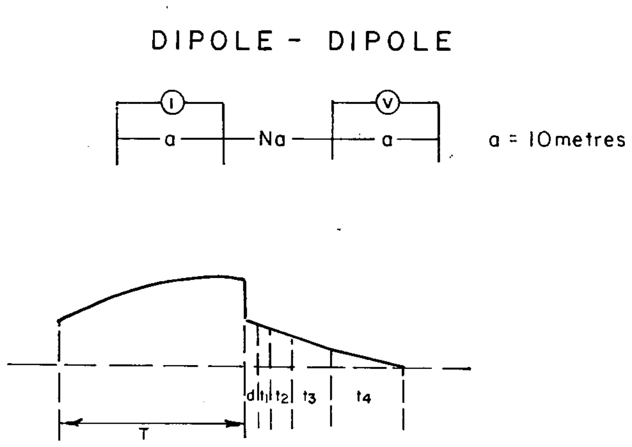


R E Gale

TO ACCOMPANY REPORT BY R.E. GALE, Ph.D., P. ENG.

SCALE 1:25.00

0 50 100 150 METRES



T	d	Window widths (msec)			
Pulse duration	Delay time	t1	t2	t3	t4
2000 msec	120msec	120	220	420	820

YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

BY: SHANGRI - LA MINERALS LIMITED

I.P. TEST SURVEY
N = 2
CHARGEABILITY Mt (msec.)

OSOYOOS M.D., B.C.

N.T.S. 82E/5W	DATE : AUGUST 1986
DRAWN BY : M.S.	FIGURE Nº. A1c

CHONG

TO ACCOMPANY REPORT BY R. E. GALE, Ph. D., P. ENG.

R.E. Gale

SCALE 1:2500

0 50 100 150 METRES

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843

DIPOLE - DIPOLE

a = 10 metres

T Pulse duration	d Delay time	Window widths (msec) t1	t2	t3	t4
2000 msec	120 msec	120	220	420	820

YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

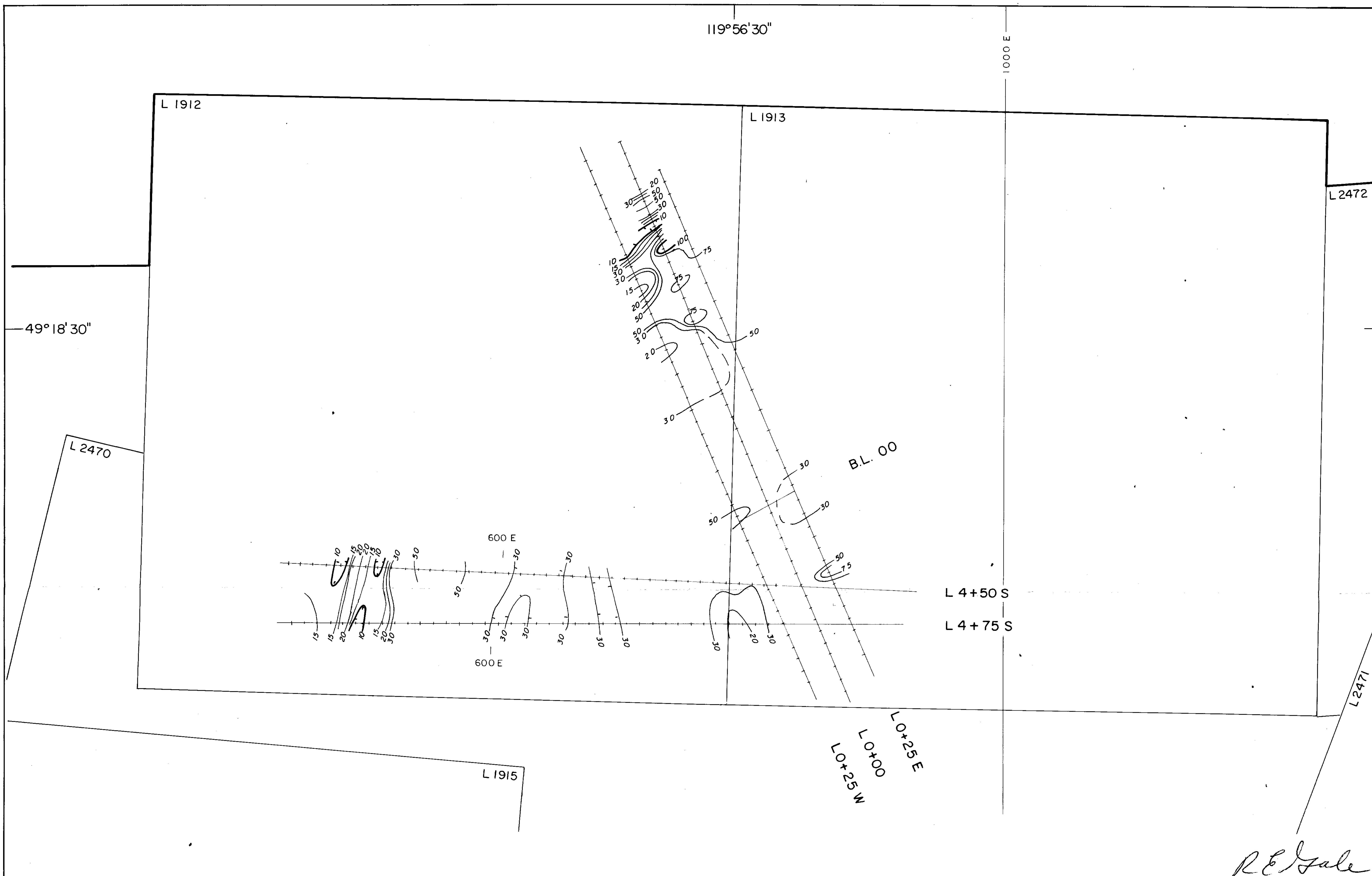
BY: SHANGRI - LA MINERALS LIMITED

I.P. TEST SURVEY
N = 2
APPARENT RESISTIVITY RHO (KΩ-m)

OSOYOOS M.D., B.C.

N.T.S. 82E/5W	DATE: AUGUST 1986
DRAWN BY: M.S.	FIGURE No. A1d

CHONG



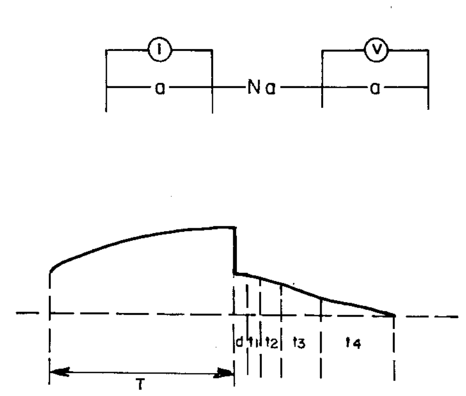
TO ACCOMPANY REPORT BY R.E. GALE, Ph.D., P. ENG.

R.E. Gale

SCALE 1:2500

0 50 100 150 METRES

DIPOLE - DIPOLE



T Pulse duration	d Delay time	Window widths (msec) t1	t2	t3	t4
2000 msec	120 msec	120	220	420	820

YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

BY: SHANGRI - LA MINERALS LIMITED

I.P. TEST SURVEY
N = 3
CHARGEABILITY Mt (msec.)

OSOYOOS M.D., B.C.

N.T.S. 82E/5W	DATE: AUGUST 1986
DRAWN BY: M.S.	FIGURE No. A1e

CHONG

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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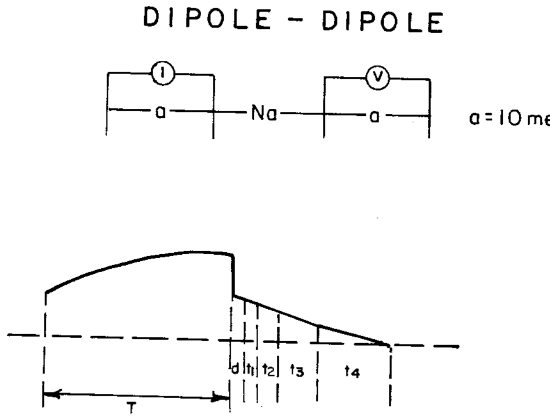
R E Gale

TO ACCOMPANY REPORT BY R.E. GALE, Ph.D., P. ENG.

DIPOLE – DIPOLE



T Pulse duration	d Delay time	Window widths (msec) t1	t2	t3	t4
2000 msec	120 msec	120	220	420	820

YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

BY: SHANGRI-LA MINERALS LIMITED

I.P. TEST SURVEY
N = 3
APPARENT RESISTIVITY RHO (KΩ-m)

OSOYOOS M.D., B.C.

N.T.S. 82E/5W	DATE: AUGUST 1986
DRAWN BY: M.S.	FIGURE No. A1f

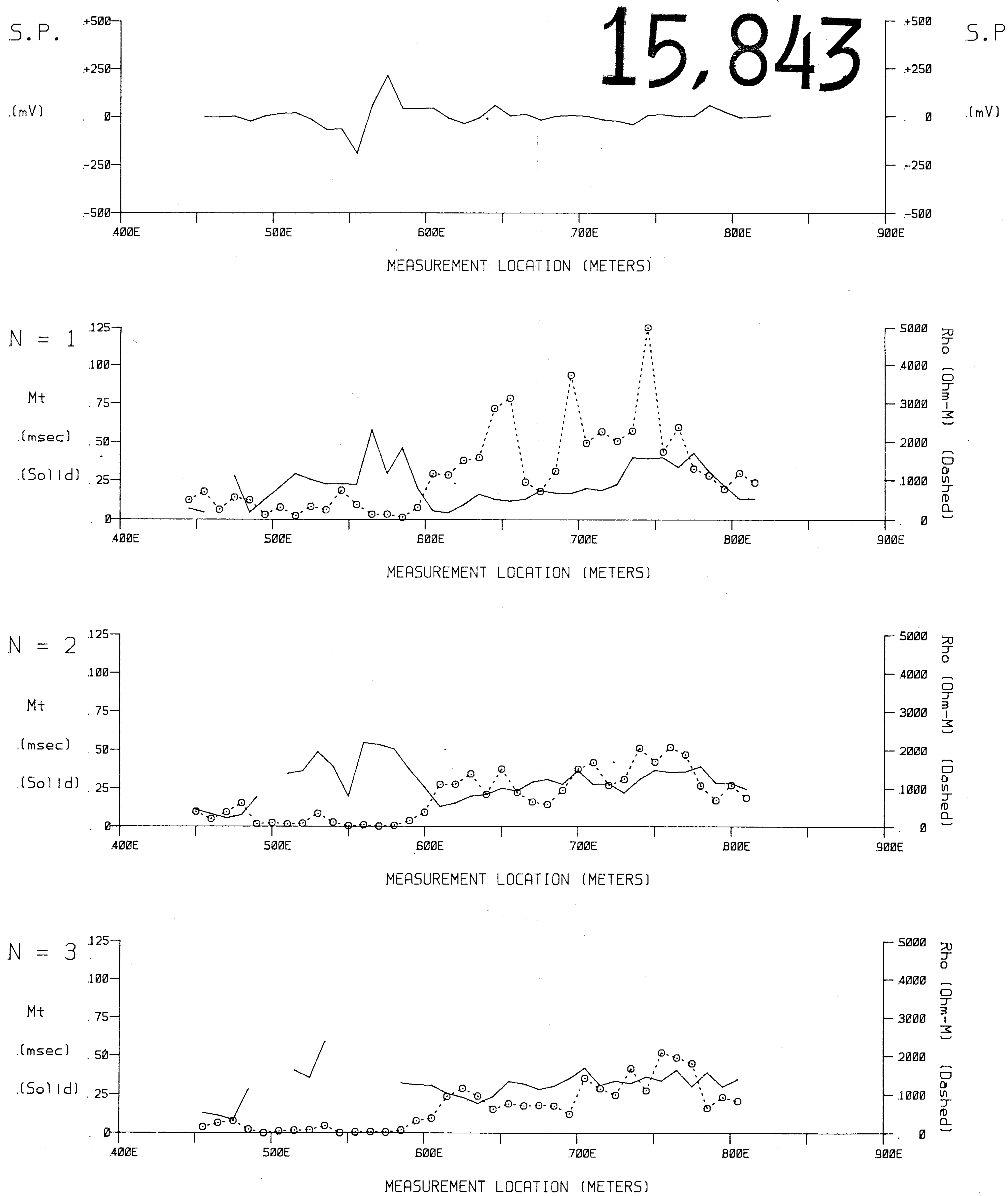
CHONG

YUNIMAN PROJECT FIG. NO.:A2a

FOR: TOBY CREEK RESOURCES LTD. BY: SHANGRI-LA MINERALS LIMITED DATE: SEPTEMBER 1986

SELF POTENTIAL, INDUCED POLARIZATION AND RESISTIVITY PROFILES

LINE 4+50S



YUNIMAN PROJECT FIG. NO.: A2 b

R E Gale

FOR: TOBY CREEK RESOURCES LTD. BY: SHANGRI-LA MINERALS LIMITED DATE: SEPTEMBER 1986

SELF POTENTIAL, INDUCED POLARIZATION AND RESISTIVITY PROFILES

LINE 4+75S

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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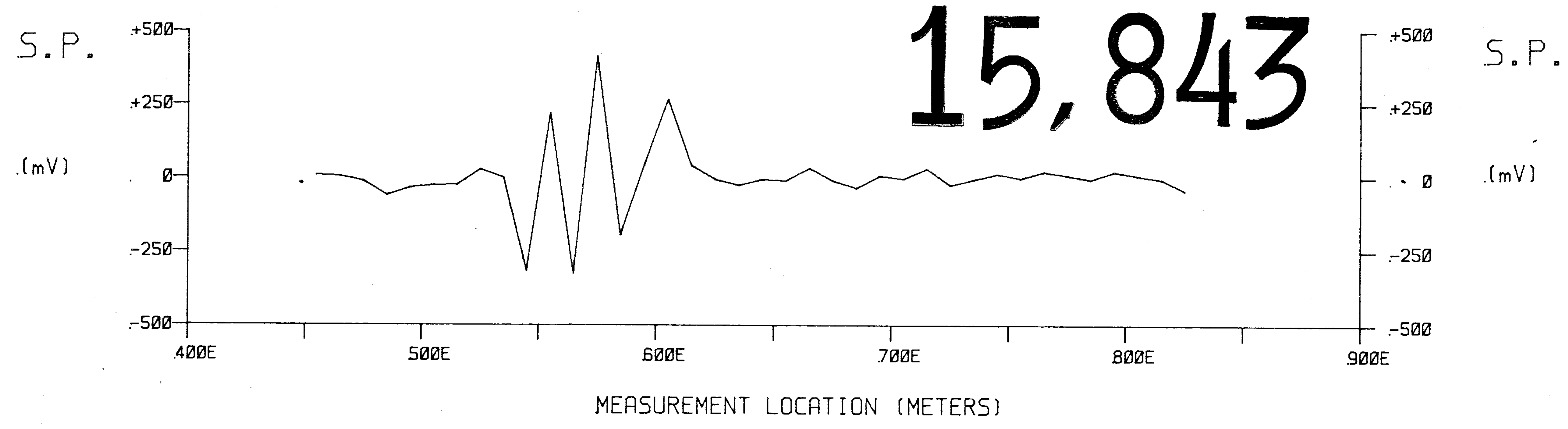

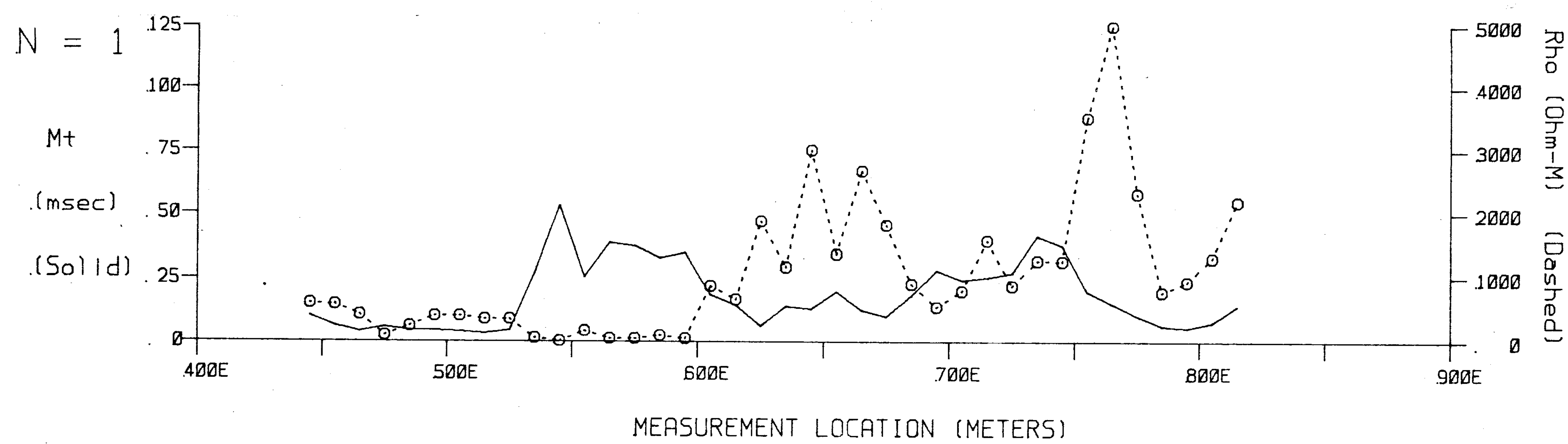

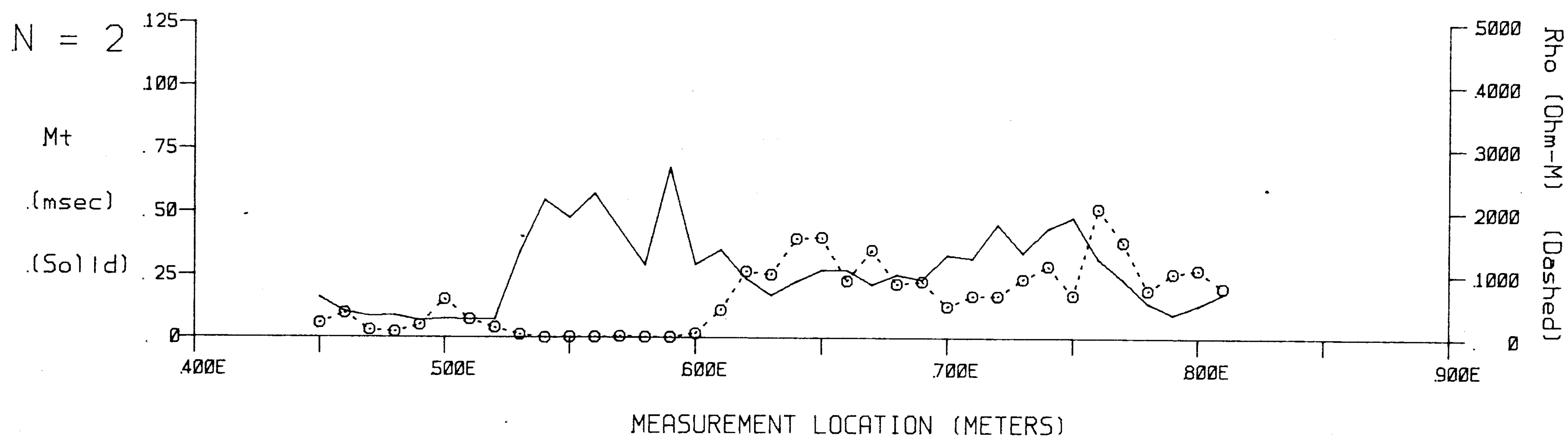

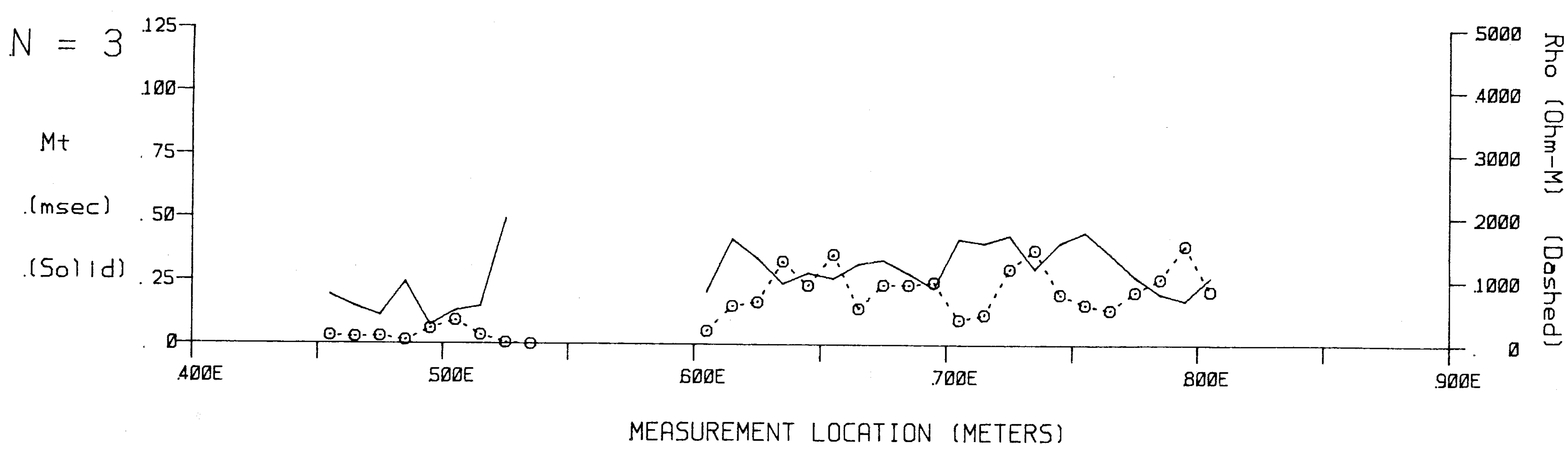

YUNIMAN PROJECT FIG. NO.: A2c *R E Gale*

FOR: TOBY CREEK RESOURCES LTD. BY: SHANGRI-LA MINERALS LIMITED DATE: AUGUST 1986

SELF POTENTIAL, INDUCED POLARIZATION AND RESISTIVITY PROFILES

LINE Ø+25E

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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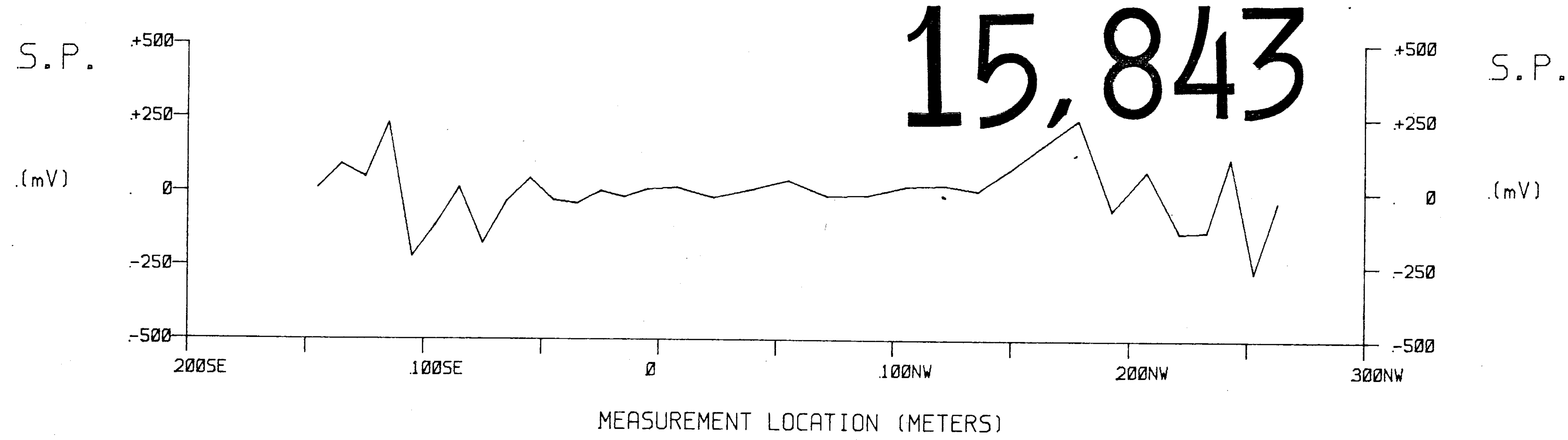

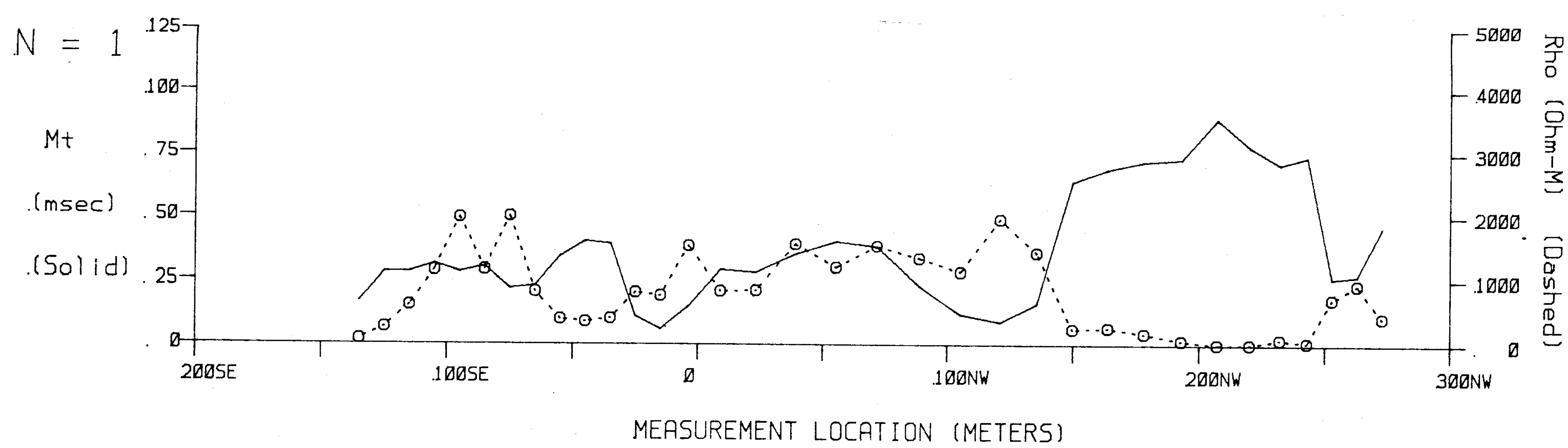

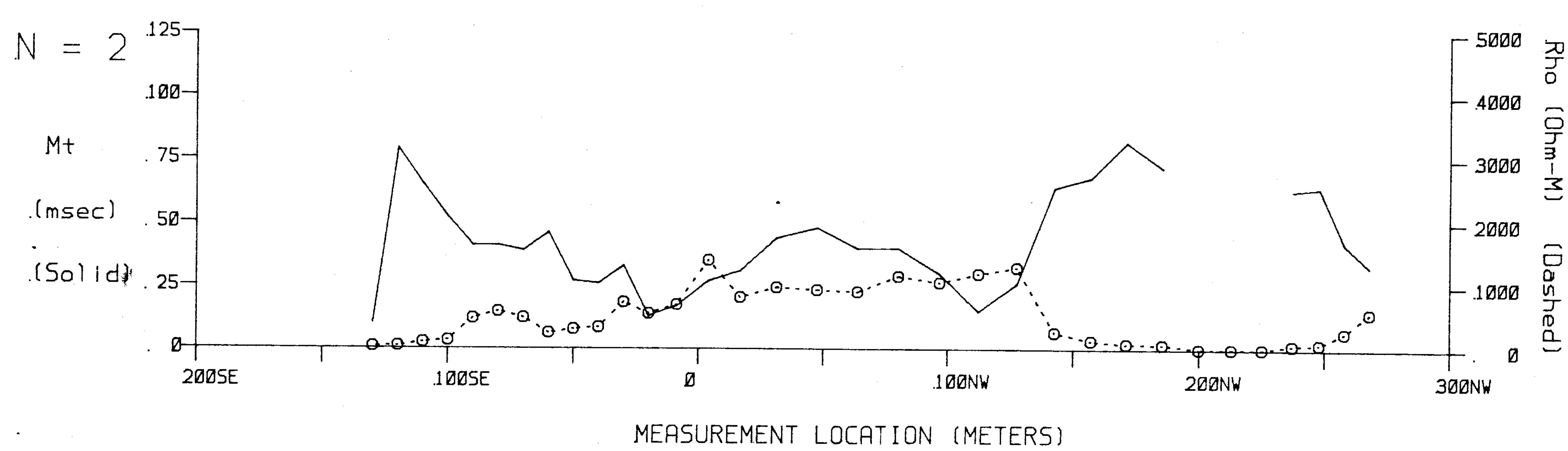

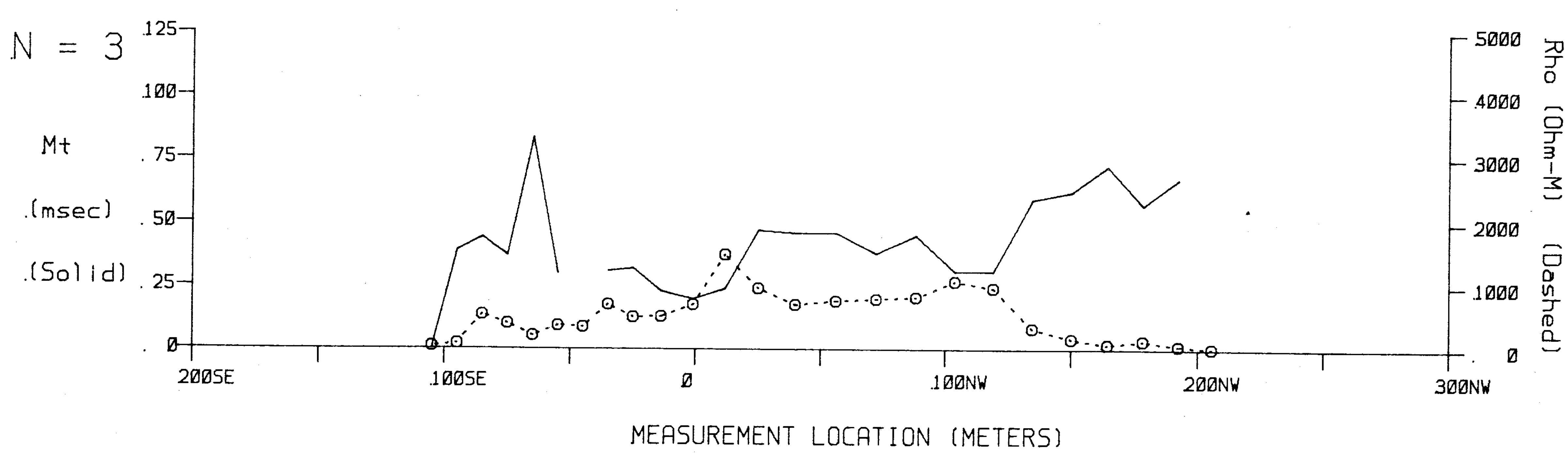

YUNIMAN PROJECT FIG. NO.: A2d R E Gale

FOR: TOBY CREEK RESOURCES LTD. BY: SHANGRI-LA MINERALS LIMITED DATE: AUGUST 1986

SELF POTENTIAL, INDUCED POLARIZATION AND RESISTIVITY PROFILES

LINE 0+00

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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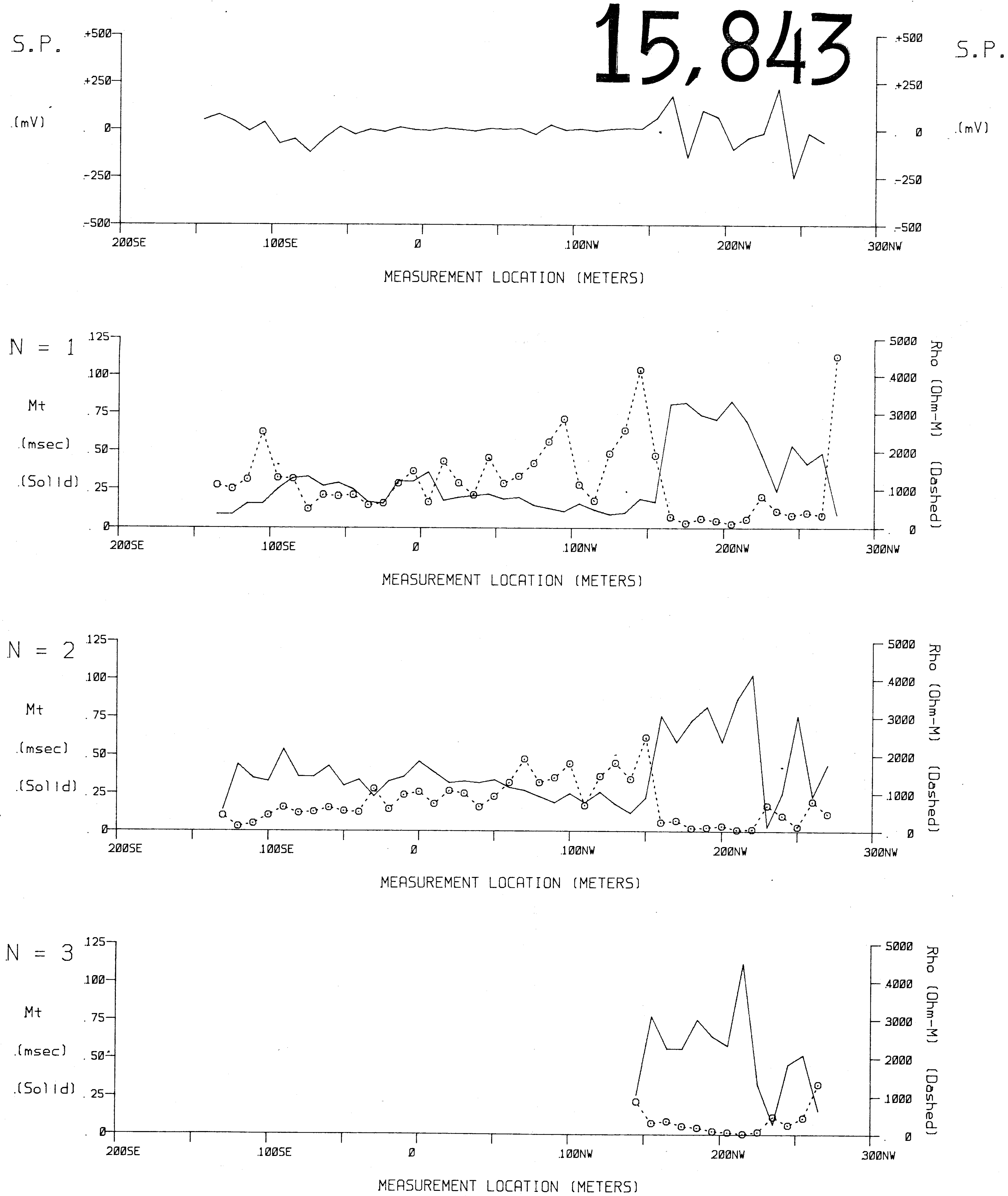

YUNIMAN PROJECT

FIG. NO.: A2e

FOR: TOBY CREEK RESOURCES LTD. BY: SHANGRI-LA MINERALS LIMITED DATE: AUGUST 1986

SELF POTENTIAL, INDUCED POLARIZATION AND RESISTIVITY PROFILES

LINE 0+25W

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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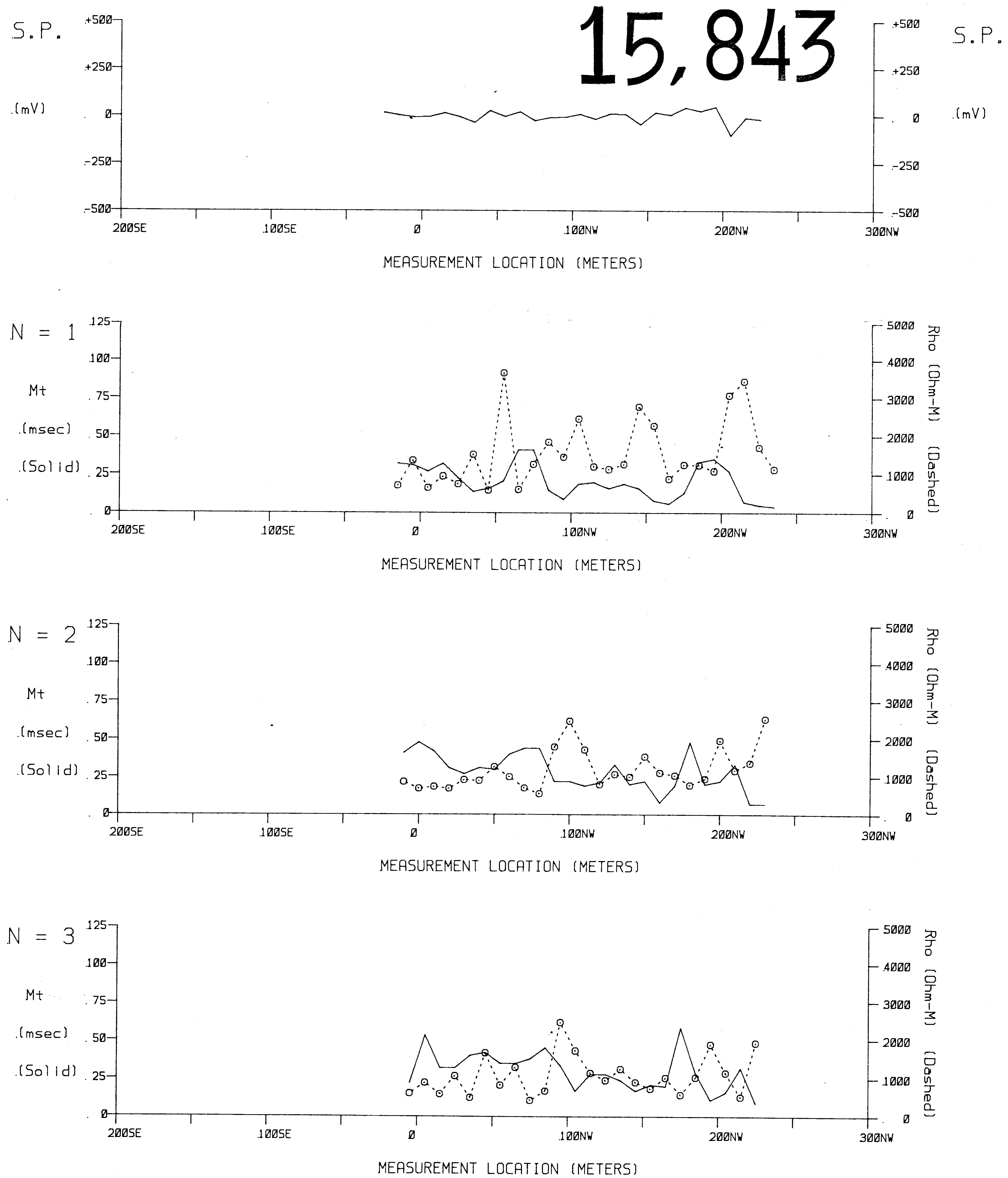


R E Gale

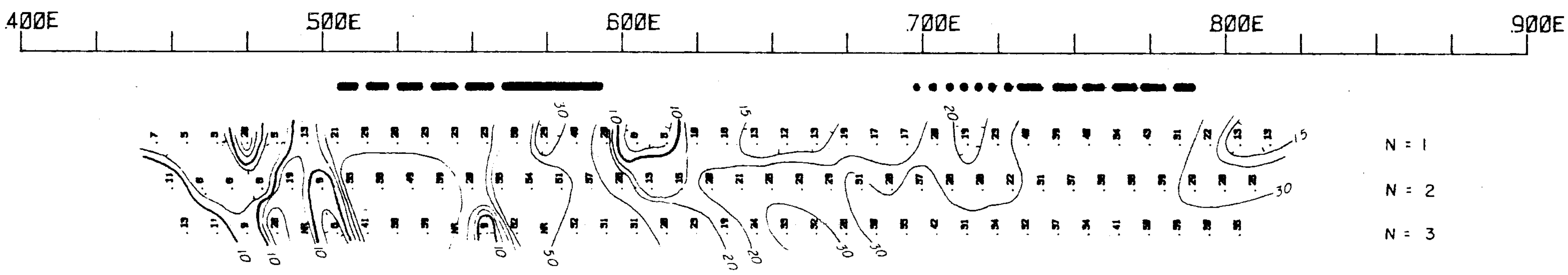
YUNIMAN PROJECT FIG. NO.: A3a

FOR: TOBY CREEK RESOURCES LTD. BY: SHANGRI-LA MINERALS LIMITED DATE: AUGUST 1986

INDUCED POLARIZATION AND RESISTIVITY PSEUDO-SECTIONS
LINE 4+50S

Mt (msec): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3

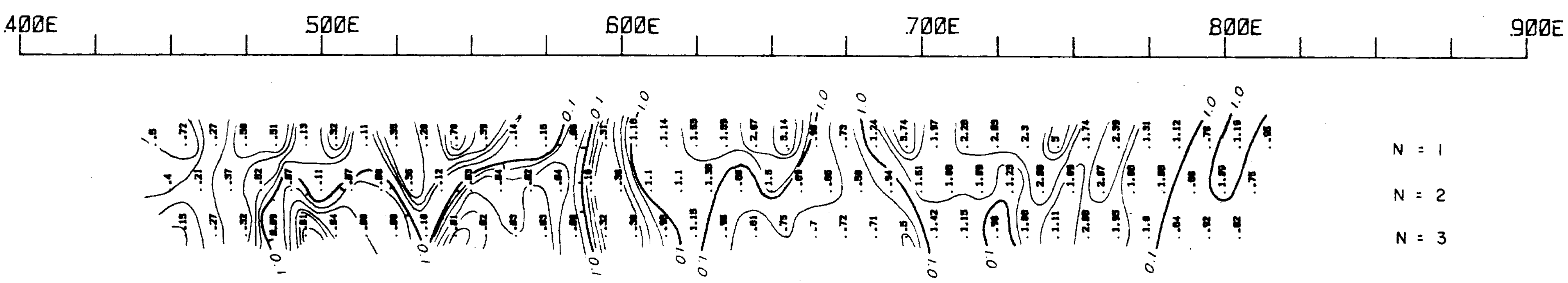


LOGARITHMIC CONTOUR : 1, 1.5, 2, 3, 5, 7.5, 10

DEFINITE ANOMALY
PROBABLE "
POSSIBLE "
EXPLANATION OF SELECTION CRITERIA IN TEXT

Rho (KOhm-M): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3



To accompany report by R. E. Gale, Ph.D., P. Eng.

R E Gale

YUNIMAN PROJECT   FIG. NO.: A3 b

FOR: TOBY CREEK RESOURCES LTD.   BY: SHANGRI-LA MINERALS LIMITED   DATE: AUGUST 1986

INDUCED POLARIZATION AND RESISTIVITY PSEUDO-SECTIONS
LINE 4+75S

GEOLOGICAL BRANCH
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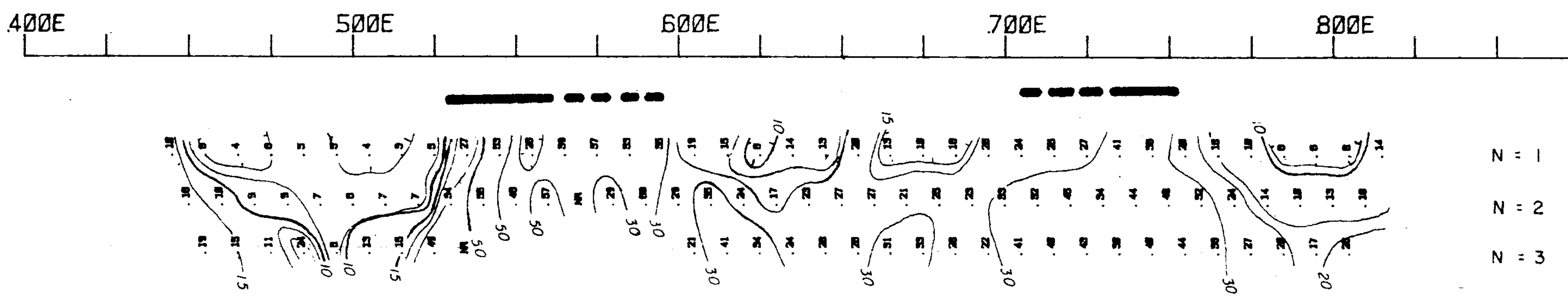
Mt (msec): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3

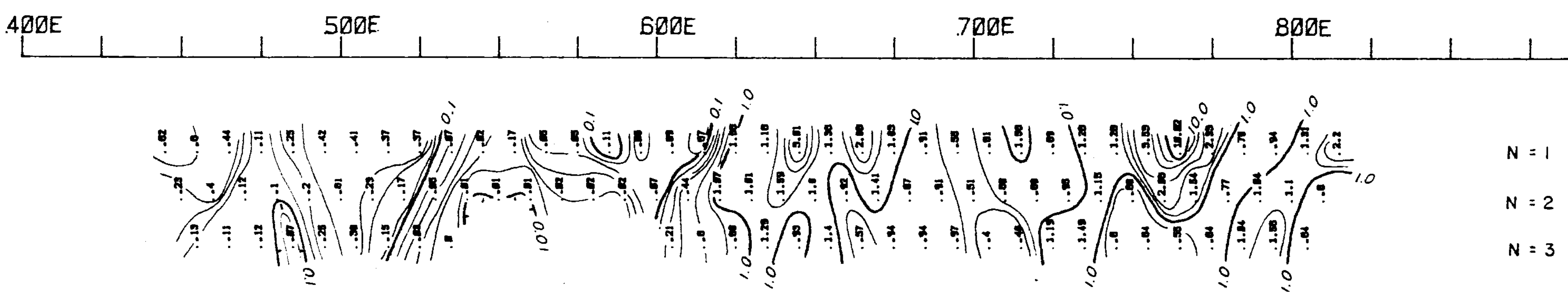


LOGARITHMIC CONTOUR : 1, 1.5, 2, 3, 5, 7.5, 10

DEFINITE ANOMALY
PROBABLE "
POSSIBLE "
EXPLANATION OF SELECTION CRITERIA IN TEXT

Rho (KOhm-M): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3



To accompany report by R.E. Gale, Ph.D., P. Eng.

R E Gale

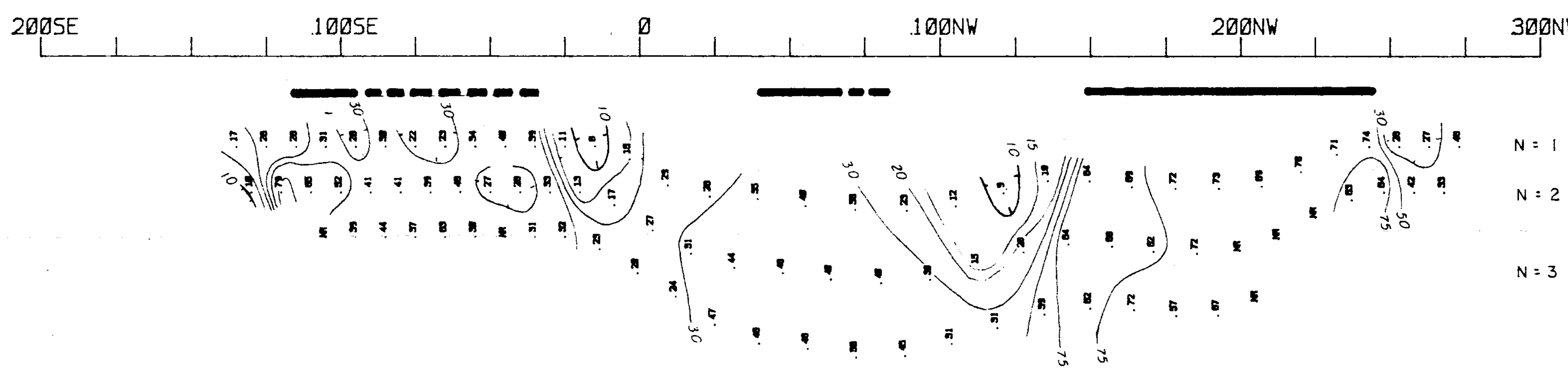
YUNIMAN PROJECT   FIG. NO.: A3 c

FOR: TOBY CREEK RESOURCES LTD.   BY: SHANGRI-LA MINERALS LIMITED   DATE: AUGUST 1986

INDUCED POLARIZATION AND RESISTIVITY PSEUDO-SECTIONS
LINE 0+25E

Mt (msec): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3



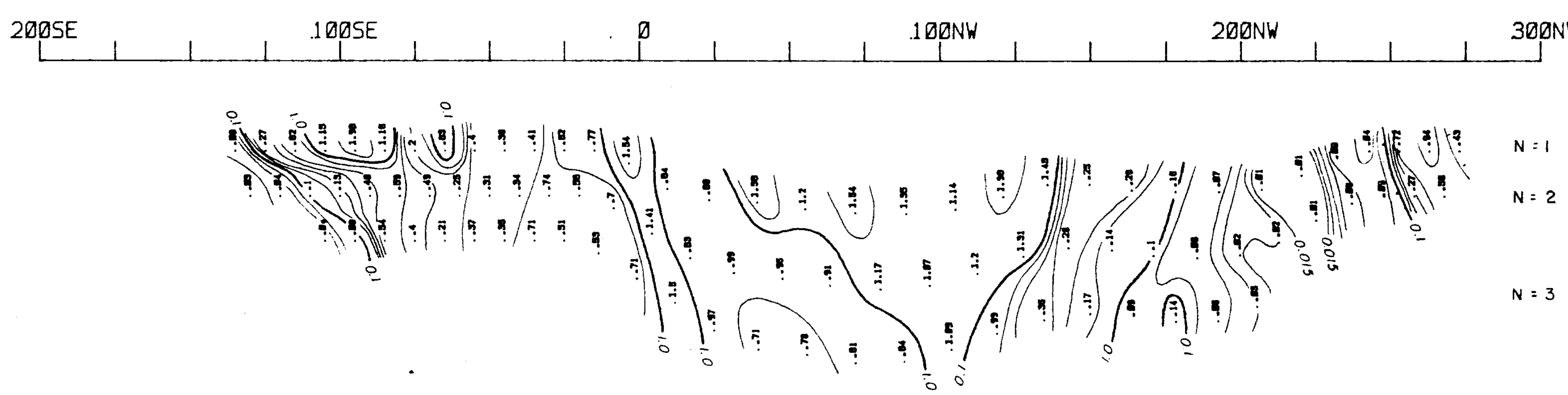
LOGARITHMIC CONTOUR 1, 1.5, 2, 3, 5, 7.5, 10

DEFINITE ANOMALY
PROBABLE "
POSSIBLE "

EXPLANATION OF SELECTION CRITERIA IN TEXT

Rho (KOhm-M): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3



To accompany report by R.E. Gale, Ph.D., P.Eng

R E Gale

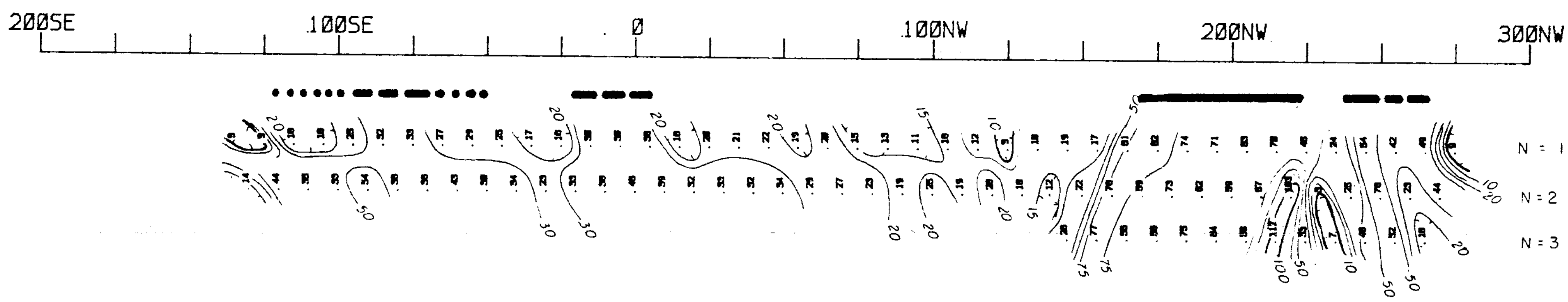
YUNIMAN PROJECT FIG. NO.: A3d

FOR: TOBY CREEK RESOURCES LTD. BY: SHANGRI-LA MINERALS LIMITED DATE: AUGUST 1986

INDUCED POLARIZATION AND RESISTIVITY PSEUDO-SECTIONS
LINE 0+00

Mt (msec): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3



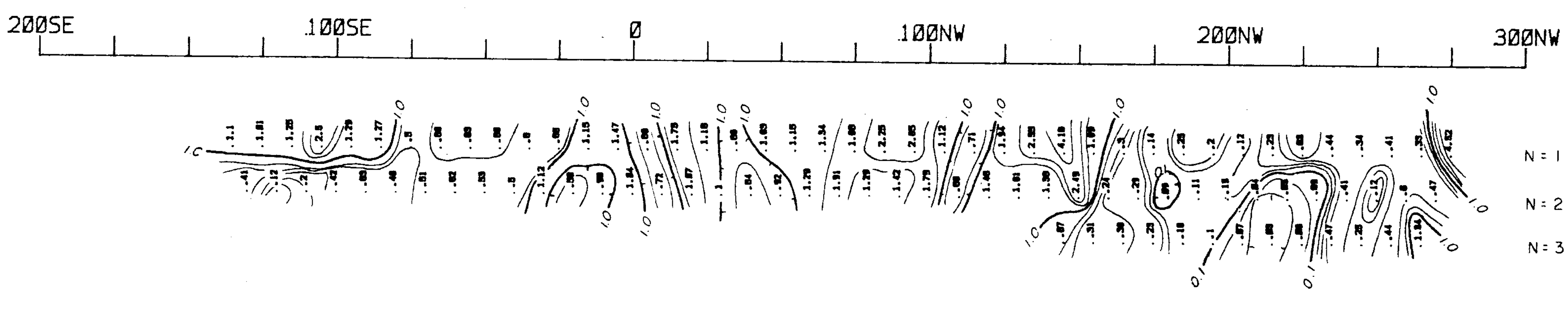
LOGARITHMIC CONTOUR : 1, 1.5, 2, 3, 5, 7.5, 10

- DEFINITE ANOMALY
- PROBABLE "
- POSSIBLE "

} EXPLANATION OF SELECTION CRITERIA IN TEXT

Rho (KOhm-M): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3



To accompany report by R.E. Gale, Ph.D., P. Eng.

GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843

R E Gale

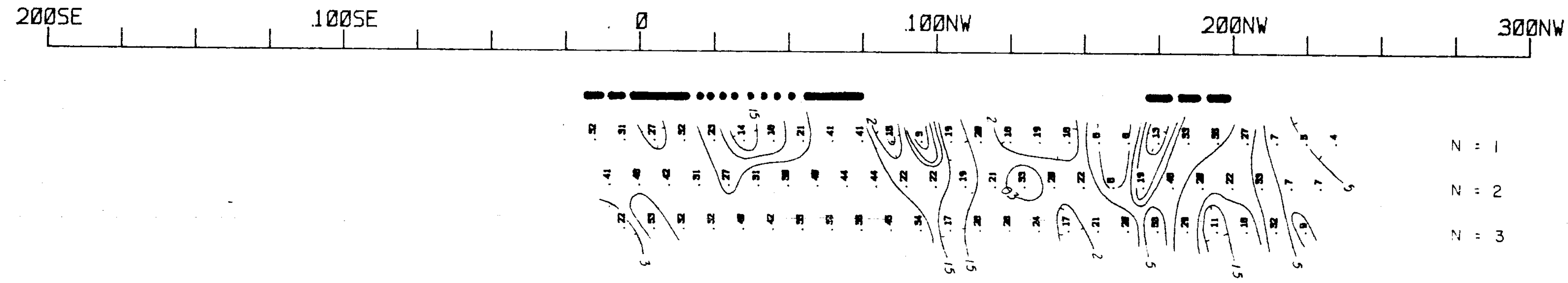
YUNIMAN PROJECT FIG. NO.: A3e

FOR: TOBY CREEK RESOURCES LTD. BY: SHANGRI-LA MINERALS LIMITED DATE: AUGUST 1986

INDUCED POLARIZATION AND RESISTIVITY PSEUDO-SECTIONS
LINE Ø+25W

Mt (msec): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3

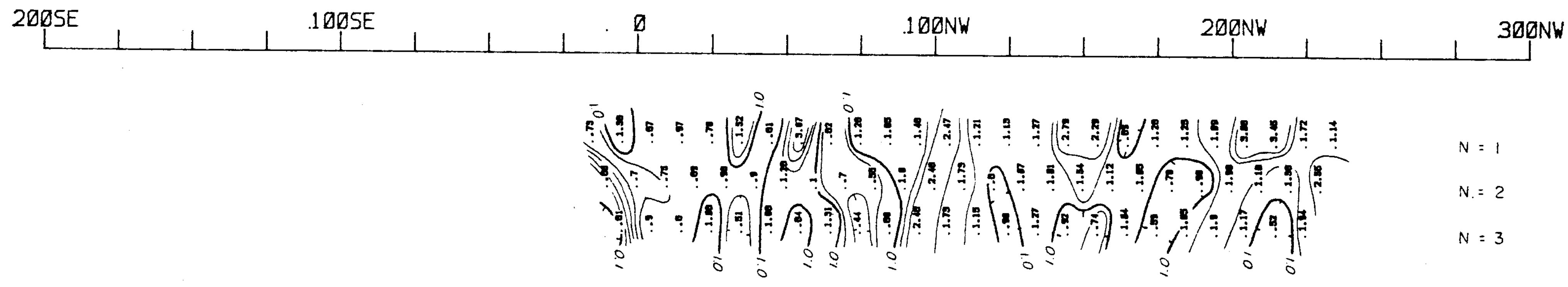


LOGARITHMIC CONTOUR : 1, 1.5, 2, 3, 5, 7.5, 10

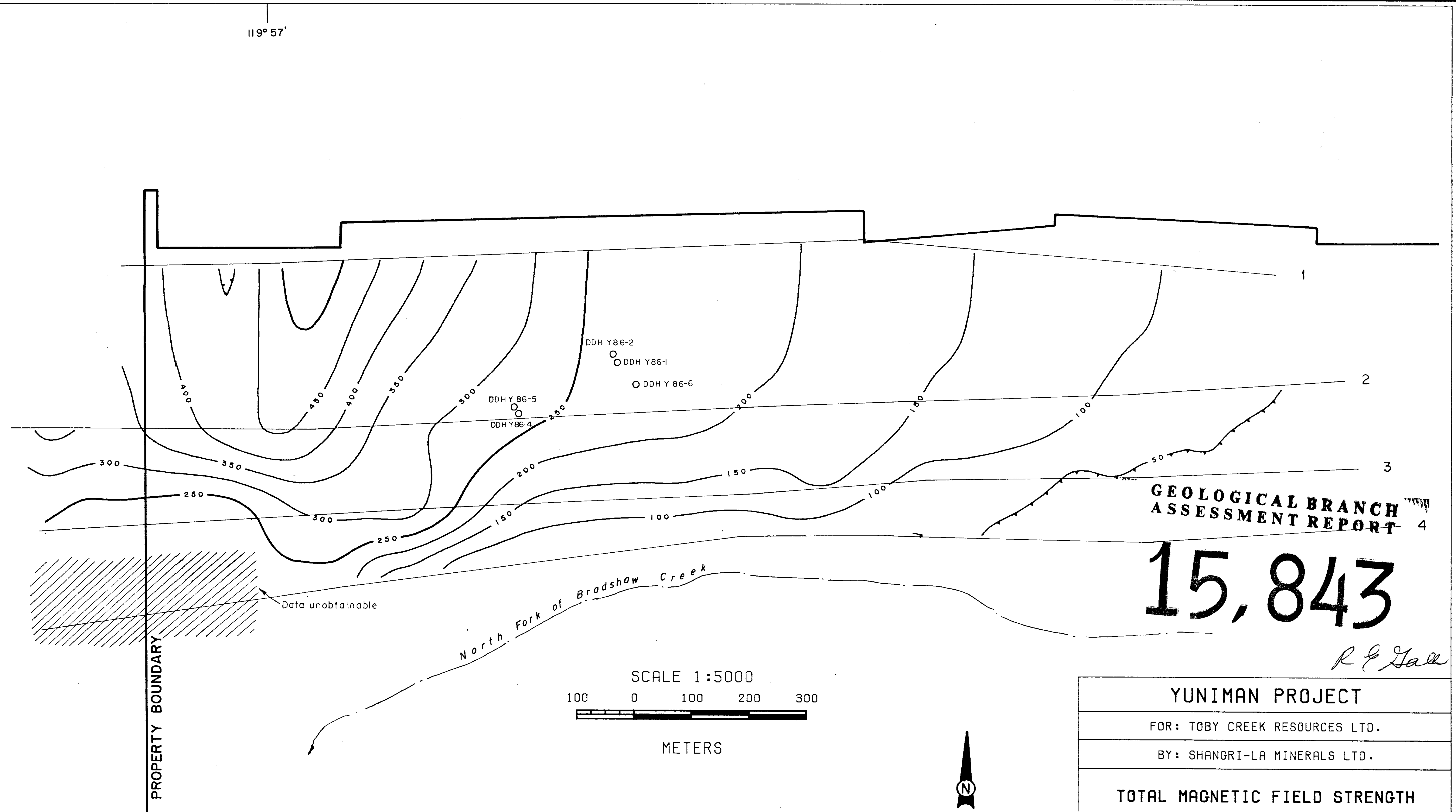
DEFINITE ANOMALY
PROBABLE "
POSSIBLE "
EXPLANATION OF SELECTION CRITERIA IN TEXT

Rho (KOhm-M): N = 1 UPPER, N = 2 CENTER, N = 3 BOTTOM

MEASUREMENT LOCATION (METERS) - DEPTH OF VALUES ILLUSTRATED EXAGGERATED BY FACTOR OF 3



To accompany report by R.E. Gale, Ph.D., P.Eng.



GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843

R E Gale

BASE VALUE: 58,300 GAMMAS
CONTOUR INTERVAL: 50 GAMMAS

TO ACCOMPANY REPORT BY
R. GALE, PH.D., P.ENG.

YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

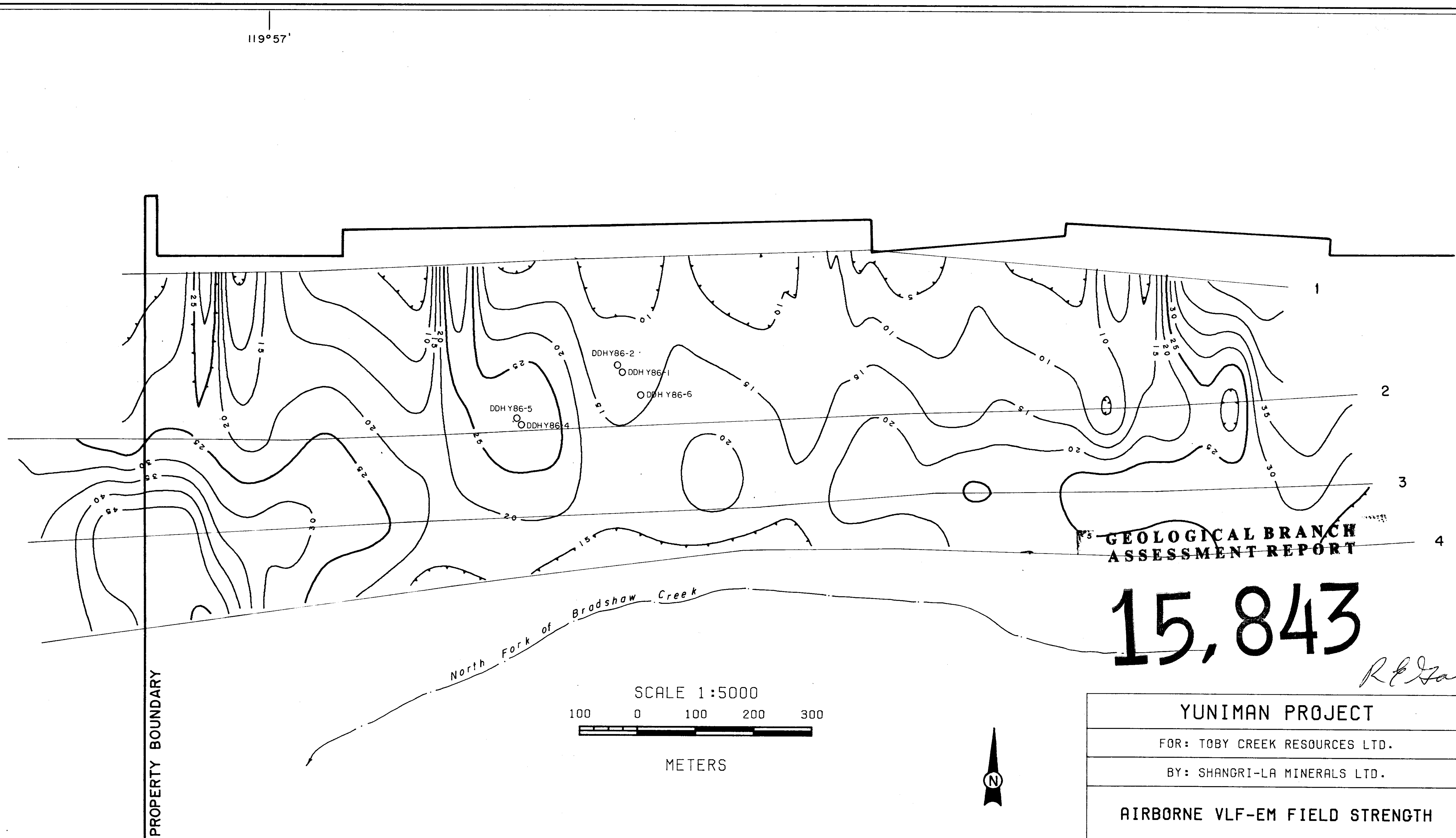
BY: SHANGRI-LA MINERALS LTD.

TOTAL MAGNETIC FIELD STRENGTH

AIRBORNE SURVEY

OSOYOOS M.D., B.C.

N.T.S.: 82 E/5	DATE: OCTOBER 1986
PLOTTED BY: R.P.M.	FIGURE NO.: A4a



CONTOUR INTERVAL: 5 PERCENT

TO ACCOMPANY REPORT BY
R. GALE, PH.D., P.ENG.

R E Gale

YUNIMAN PROJECT

FOR: TOBY CREEK RESOURCES LTD.

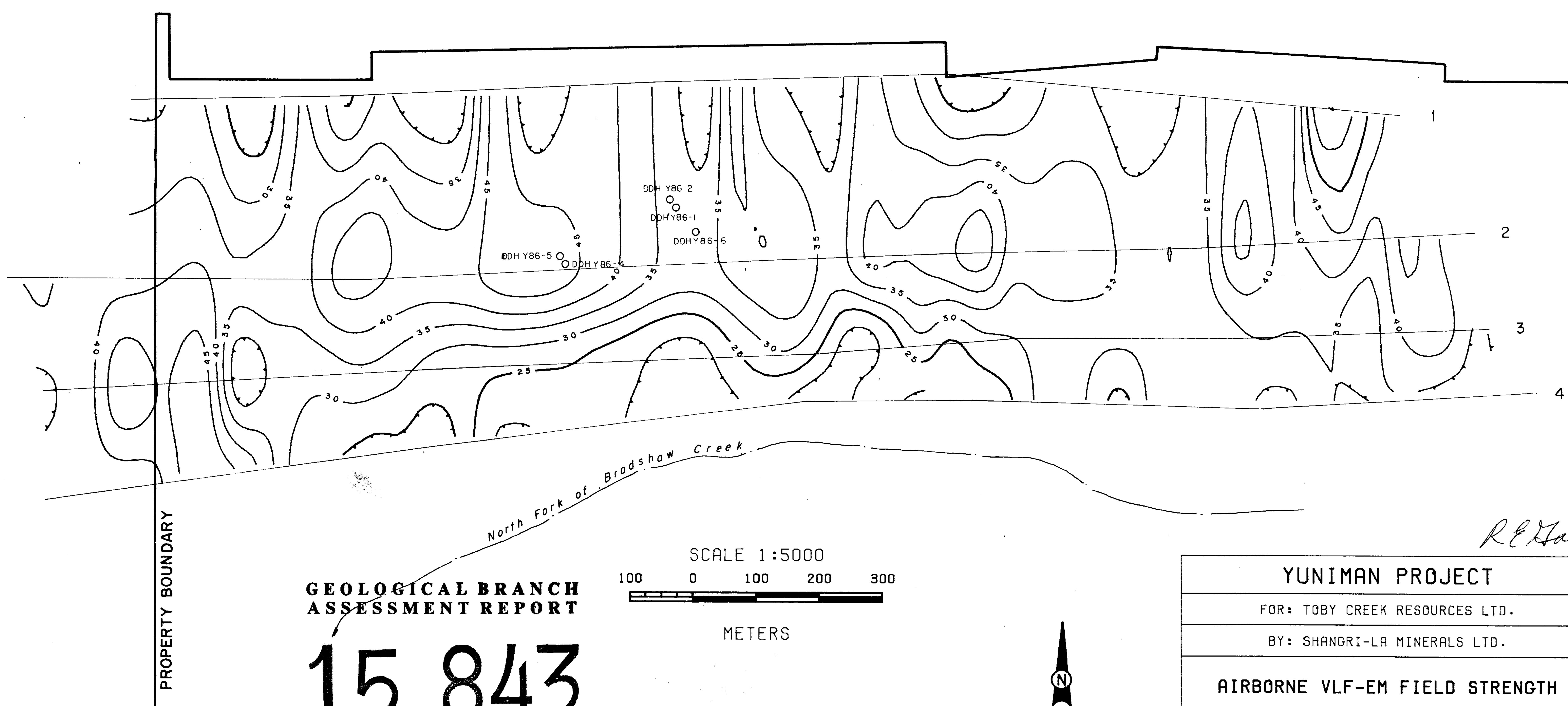
BY: SHANGRI-LA MINERALS LTD.

AIRBORNE VLF-EM FIELD STRENGTH

SEATTLE

OSOYOOS M.D., B.C.

N.T.S.: 82 E/5	DATE: OCTOBER 1986
PLOTTED BY: R.P.M.	FIGURE NO.: A 4b



GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,843

CONTOUR INTERVAL: 5 PERCENT

SCALE 1:5000

100 0 100 200 300

METERS

TO ACCOMPANY REPORT BY
R. GALE, PH.D., P.ENG.

R E Gale

YUNIMAN PROJECT	
FOR: TOBY CREEK RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LTD.	
AIRBORNE VLF-EM FIELD STRENGTH ANNAPOLIS OSOYOOS M.D., B.C.	
N.T.S.: 82 E/5	DATE: OCTOBER 1986
PLOTTED BY: R.P.M.	FIGURE NO.: A4c