

87-405 - 15939

ASSESSMENT REPORT

on the

VILLALTA PROPERTY
in the
Nanaimo Mining Division
Latitude $49^{\circ} 09' 24''$ Longitude $124^{\circ} 28' 30''$
NTS Map# 92F/1W

for

Owner/Operator: CANAMIN RESOURCES LTD.
#220-145 Chadwick Court
North Vancouver, B.C. V7M 3K1

by

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(T.E. Lisle & Associates)
S.P. Quin B. Sc. ARSM
Southern Gold Resources Ltd.

FILMED

25 June 1987

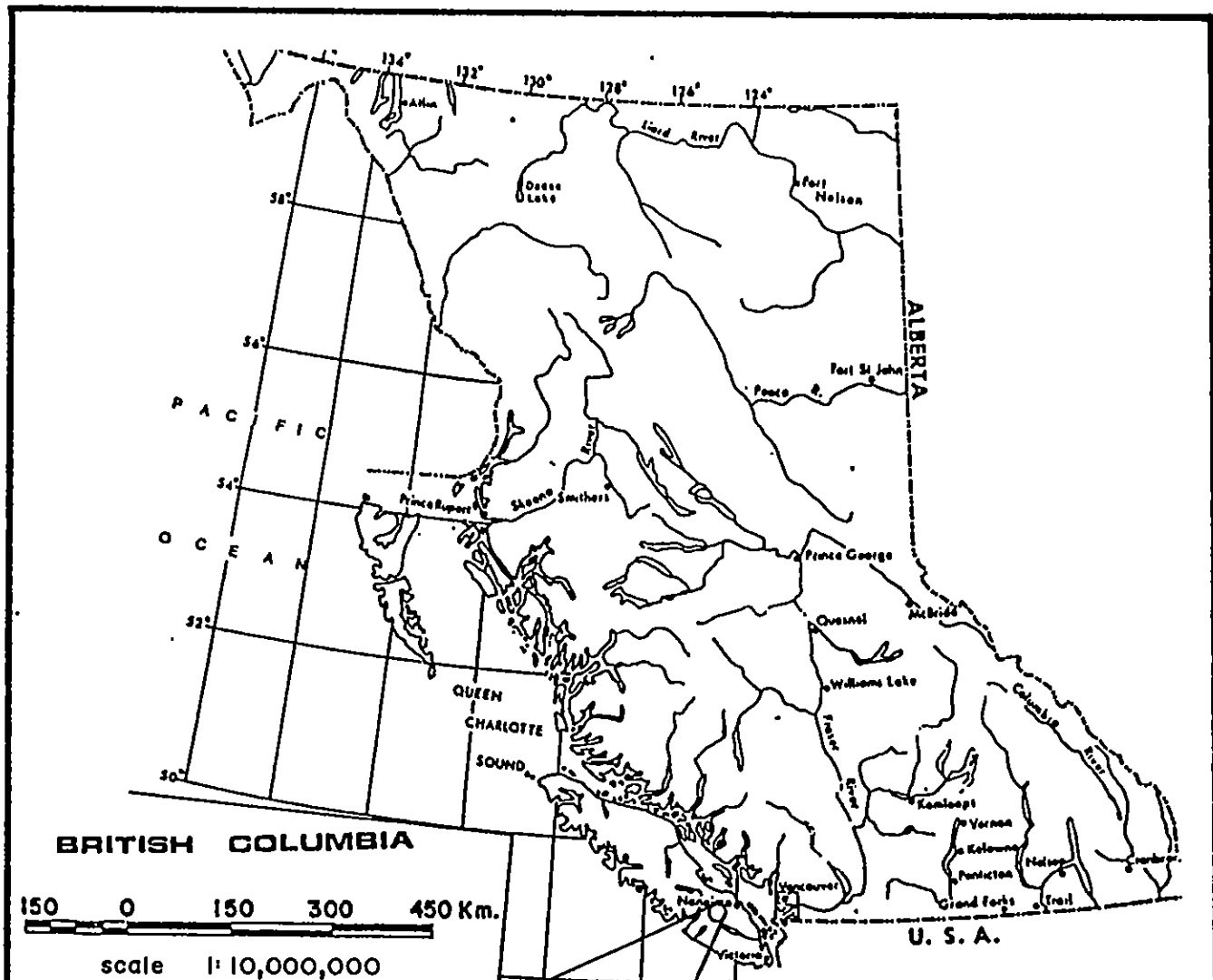
GEOLOGICAL BRANCH
ASSESSMENT REPORT

15,939

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CANAMIN RESOURCES LTD.	
VILLALTA PROJECT	
LOCATION MAP	
GEOLOGIST: S.P. QUINN/T. LISLE	BASED ON: SURVEY 1987
SCALE:	
DRAWN BY:	DATE: JUNE 1987
FIGURE: 1	

1. Introduction.

Between May 3 and June 18, 1987. the authors supervised a drilling program on the Villalta mineral claims, Nanaimo Mining Division, for CanaMin Resources Limited. T. Lisle supervised the drilling from 3 May to 10 June 1987 and S. Quin from 10 June to 18 June 1987.

The object of the drilling program was twofold:

- a) To outline the size, shape and grade of gold contained in the south exposed end of a hematite horizon and,
- b) To investigate the trace of hematite zone beneath the Nanaimo Group sedimentary rocks to the north.

2. Property

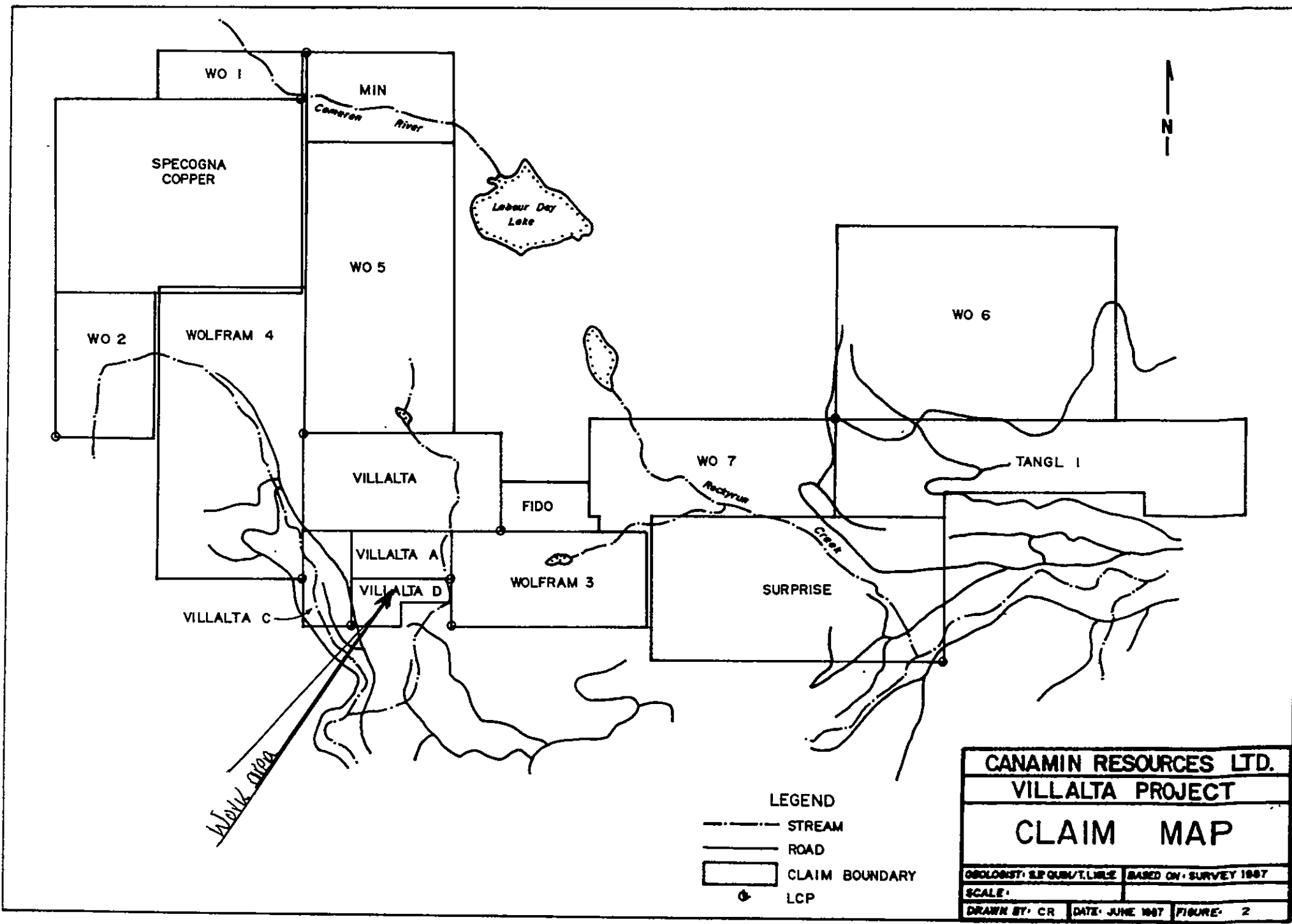
As presently constituted, the property comprises 16 modified grid claims aggregating 159 units as follows.

<u>Claim</u>	<u>Record.</u>	<u>Units</u>	<u>Group</u>	<u>Anniversary</u>
Min.	627 (5)	6	Waterfall	May. 30/95
Specogna Cu.	557 (3)	20	Waterfall	Mar. 17/95
WO 1	626 (5)	3	Waterfall	May. 30/95
WO 2	558 (3)	6	Waterfall	Mar. 17/95
Wolfram 3	344 (3)	8	Tangle	Mar. 9/95
Wolfram 4	1673 (3)	18	Waterfall	Mar. 28/95
WO 5	501 (12)	18	Waterfall	Dec. 31/87
WO 6	499 (12)	20	Tangle	Dec. 31/87
WO 7	500 (12)	10	Tangle	Dec. 31/87
Villalta	105 (9)	8	Waterfall	Sept. 15/87
Villalta A	104 (9)	2	Waterfall	Sept. 15/87
Villalta C	133 (1)	2	Tangle	Jan. 10/95
Villalta D	134 (1)	2	Tangle	Jan. 10/95
Fido	889 (6)	2	Tangle	Jun. 1/95
Tangl 1	786 (2)	16	Tangle	Feb. 25/95
Surprise	1058 (12)	18	Tangle	Dec. 29/87

See Figure 1

3. Location and Access.

The Villalta gold prospect is located about 48 kilometers by road west of Nanaimo on southern Vancouver Island; Latitude 49°06', Longitude 124°28"; NTS 92F/1W. The property is accessed by paved road along the Nanaimo River, then by about five kilometers of logging road to the northwest of Fourth Lake. (see Figure 1.)



CANAMIN RESOURCES LTD.	
VILLALTA PROJECT	
CLAIM MAP	
GEOLOGIST: S.P. QUINN	BASED ON: SURVEY 1987
SCALE:	
DRAWN BY: CR	DATE: JUNE 1987
FIGURE: 2	

4. Background

The Villalta prospect was staked by E. Specogna in 1976. It was optioned to Asarco in 1982 and subsequently to Falconbridge in 1984. Much of the geological, geochemical and geophysical data relative to the prospect was acquired during this period. Drill testing was also completed as follows:

1979	E. Specogna.	1 Winkie hole.	
1980	Canamin Resources.	6 NQ holes.	398.4 metres.
1981	Canamin Resources.	15 NQ holes.	2,008.2 metres.
1984*	Falconbridge.	4 NQ-BQ holes.	666.1 metres.
1986	Canamin Resources.	<u>9 Winkie holes.</u>	<u>51.3 metres.</u>
		<u>35</u>	<u>3,124.0 metres.</u>

* Three drill holes were completed in other areas of claims.

The results of preliminary test metallurgical work carried out between 1984 and 1986 are as follows.

- a) 78% of gold could be recovered from $\frac{1}{2}$ inch sized material; and 65% recovered from 1 inch sized material by cyanide leaching.
- b) Gravity concentration yielded poor results. (Bacon Donaldson).
- c) There is a free gold component to some of the hematitic mineralization, and refractory sulphide made for locally poor recovery. (Coastech).
- d) Best gold recovery in the 80% range was obtained by conventional milling-cyanidation. (Lakefield Research).

At the exposed south end of the hematite zone, drilling suggested a poorly defined reserve in the order of 30,000 to 35,000 short tons grading 0.126 opt gold in a near surface zone averaging 7.3 metres in thickness. (Carter, 1986). Better definition of the reserve and further metallurgical testing on bulk samples was recommended.

5. Geology.

The Villalta prospect occurs near a small exposure of Buttle Lake limestone close to a contact with volcanic and related sedimentary rocks of the Paleozoic Sicker Myra formation. The limestone is crinoidal and is marked by numerous sink holes. The presence of thin andesitic and tuffaceous horizons above the limestone similar to the underlying Myra rocks suggests contemporaneous deposition of carbonate and volcanic units.

Attention to the area was drawn to a hematite 'Iron formation' lying above the limestone and close to an unconformity with the overlying Cretaceous Nanaimo sedimentary group. The hematite layer is thought to have originated in or adjacent to a mafic volcanic centre. Only a small area at its south end is exposed, however its trace through drilling and geochemistry appears to be generally north-northeast. (Figure 2).

6. Mineralization

Two types of mineralization have been encountered and partly investigated:

- a) Massive fine to coarse grained pyrite with pyrrhotite and lesser sphalerite, chalcopyrite and galena is evident in steeply dipping discontinuous veins, and as crudely banded conformable lenses in the limestone near the iron formation. These occurrences locally carry important amounts of gold, silver, copper and zinc and tungsten, however they have not attracted detailed exploration.
- b) Because of the contained gold and potential size, the Iron formation has received much of the past attention. Belik reports the formation includes a variety of lithological types that form a gradational series from carbonate-rich facies at the base, to a basic to ultrabasic tuff facies at the top. Massive hematite occurs near the middle of the unit interlaminated with basic and calcareous basic tuff. In some areas the gold appears evenly distributed, in other areas better grades occur near the base and may relate to drilling angles relative to the formation. Some of the gold is indicated to be in native form.

Banding in the iron formation in drill holes 80 V2, V3, and V6 over a strike length of about 160 metres is in the order of $\pm 30^\circ$ to core axis. These holes appear to mark an eastern limit to the hematitic horizon, and areas of alteration, brecciation and shear and fault zones noted in drill holes further to the east may be part of a vent system at or close to the volcanic centre.

If the Iron formation was laid down on a paleoslope close to a volcanic centre; the nature of the surface (karsted limestone), and subsequent deformation would be significant features relative to its present distribution. In view of the apparent dip of the unit, the trace at depth may hold further potential that should be investigated.

7. 1987 Work Program.

In the 1987 program, forty-one short holes varying from 6.40 to 29.26 metres were completed over the south end of the hematite horizon. A longyear S-38 machine was used and HQ core recovered. Total drilling aggregated 648.60m (2127 feet) of which 581.45m were HQ core size and 67.15m were NQ.

Six holes varying from 54 metres to 96.6 metres were completed in the area further to the north. Total drilling aggregated 393.8 metres (1,292 feet), and NQ core was recovered.

The core from zones of interest were either sawed or split with conventional splitter for assay. A total of 445 core samples were sent for assay. All core samples were analysed for gold and silver by fire assay methods and also for 30 elements by the Induced Coupled Plasma (ICP) method. Some were checked for free gold by fire assay. All work was conducted by Acme Analytical Laboratories of Vancouver, B.C. A summary of the assay results is given in Appendix A, while the assay certificates are enclosed in Appendix B. The core was logged, and is stored in a core rack that was constructed in the area adjacent to the drilled area.

8. Program Results.

The hematite layer is associated with a green tuff-breccia above the Buttle Lake Limestone. The breccia commonly contains clasts of silicified limestone. In places this unit separates the hematite from the overlying Nanaimo Group conglomerate. In one area, the hematite has been eroded and is in direct contact with the conglomerate.

The hematite varies from black specular to earthy red in masses up to a few metres thick, or as breccia clasts up to 30 cm. in diameter in the surrounding tuff. The near surface material is commonly pitted, weathered and limonitic.

The southern exposure is marked by a strong northwest trend however the drill indicated trend along strike is about 030°.

The drilling program has shown a marked change in the geology of the southern exposure from that to the north. In the vicinity of drill hole 87-V-41 and 42, the limestone has been altered to a white marble, and a number of stringer type alteration and fracture zones, locally with hematite and scattered concentrations of pyritic sulphide, are evident.

At the southern exposure, both crinoidal and fine-grained limestone, and lesser amounts of dark grey rock (argillite?) have been silicified, subsequently brecciated, and incorporated into highly altered siliceous breccias that underlie the hematite. A number of dark green andesitic? dykes with silicified limestone clasts, and a small intercept of altered feldspar porphyry are also evident.

A large cut near drill hole 87-V-5 shows a distinct vertical 315° trend to limestone, chert, and the green dyke breccias beneath the relatively flat lying hematite layer at surface. Sink holes approximately 75 metres to the southeast along trend show silicified limestone clasts and dark grey chert clasts in a greenish tuff?.

Because of the proximity to the Tertiary intrusions, it seems possible that the siliceous breccias are related to the intrusions, and their development along a northwest trend coincidentally may have changed the attitude of the existing hematite zone.

All assays received to date are recorded in the logs accompanying appendices to this report. An economic evaluation is not attempted as part of this report.

9. STATEMENT OF COSTS

DRILLING

Mob/Demol	\$1,800.00	
Casing 78ft @ \$18/ft.	\$1,424.00	
Drilling (3345ft.@\$18.75/ft.)	\$62,718.00	
Man Hours (46 hours)	\$1,137.50	
Cat (82 Hours)	\$5,297.50	
Travel time (76 hours)	\$1,900.00	
Core bixes (212)	\$1,590.00	
Supplies (Additives, bits)	<u>\$15,615.80</u>	
	\$91,482.80	
Less 1% discount	<u>\$914.83</u>	
	\$90,567.97	\$90,567.97

ASSAYS \$11,796.25

FIELD SUPPLIES \$ 2,365.64


VEHICLE \$ 2,100.00

GEOLOGICAL SUPERVISION

T. Lisle (38d @ \$300/d)	\$11,400.00	
T. Lisle (Living expenses)	\$ 2,470.39	
S.P. Quin (19d @ \$200/d)	\$ 3,800.00	
Field Assistants (57 md @ \$125/d)	\$ 7,125.00	
Living Expenses	\$ 4,397.93	
	<u>\$29,193.32</u>	\$29,193.32
		<u>\$136,023.18</u>

REPORT, DRAFTING

	<u>4,000.00</u>
TOTAL	<u>\$140,023.18</u>



 S.P. QUIN 30 June 1987

10. References.

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VILLALTA PROJECT: ASSAY RESULTS (SOUTH AREA)

DDH #	From(Ft)	To(Ft)	Interval(Ft)	OPT AU	OPT AG	% FE	Block #
79-V-1			19.70	.180			18
80-V-2	2.00	35.98	33.98	.080	.23		29
80-V-3	26.99	39.98	12.99	.007	.25		3
86-V-1	0.00	23.00	23.00	.075			25
86-V-2	2.00	19.00	17.00	.175			24
86-V-3	1.00	6.00	5.00	.146			26
86-V-4	0.00	21.00	21.00	.125			21
86-V-5	0.00	21.50	21.50	.164			33
86-V-6	0.00	34.00	34.00	.125			31
86-V-8	0.00	27.00	27.00	.290			25
86-V-9	0.00	31.00	31.00	.061			29
87-V-1	1.00	13.20	12.20	.747	1.74	29.43	31
87-V-2	0.00	19.20	19.20	.045	.43	23.22	34
87-V-4	0.00	6.00	6.00	.047	.20	34.26	32
87-V-4A	0.00	6.00	6.00	.127	.12	36.31	32
87-V-5	2.00	19.00	17.00	.101	.14	30.22	33
87-V-5A	0.00	7.00	7.00	.082	.01	39.18	33
87-V-7	0.00	9.50	9.50	.016	.02	27.84	30
87-V-10	0.00	17.56	17.56	.265	2.12	26.00	26
87-V-11	0.00	27.60	27.60	.025	.16	34.24	28
87-V-12	4.00	36.10	32.10	.118	.26	38.63	25
87-V-13	0.00	15.00	15.00	.125	.71	33.14	24
87-V-15	0.00	27.80	27.80	.010	.10	25.91	27
87-V-17	0.00	6.00	6.00	.007	.24	35.80	23
87-V-18	0.00	11.60	11.60	.190	.47	27.23	22
87-V-19	4.00	14.50	10.50	.087	.05	22.85	19
87-V-23	0.00	4.00	4.00	.105	.03	10.28	NA
87-V-24	6.00	15.90	9.90	.037	.13	38.36	20
87-V-27	12.00	19.10	7.10	.009	.09	35.64	13
87-V-30	9.00	17.20	8.20	.162	.46	17.55	16
87-V-31	4.00	20.00	16.00	.274	.65	42.50	15
87-V-32	9.70	12.80	3.10	.228	.14	26.41	14
87-V-37	2.00	15.40	13.40	.005	.14	28.17	17
87-V-38	0.00	27.00	27.00	.017	.27	37.17	18
87-V-39	5.20	11.70	6.50	.060	.68	34.02	21
87-V-47	22.50	48.20	25.70	.163	.23	35.91	8
87-V-48	13.30	43.70	30.40	.064	.37	34.12	27
	Average		16.83	.119	.40	32.02	

(File: VILSUM4)

VILLALTA PROJECT: ASSAY RESULTS (NORTH AREA)

DDH #	From(Ft)	To(Ft)	Interval(Pt)	OPT AU	OPT AG	% FE
80-V-6	165.97	189.91	23.94	.081	.05	
81-V-8	194.96	217.96	23.00	.090		
84-V-24	96.43	107.78	11.35	.038		
84-V-25	103.22	129.63	26.41	.001		
87-V-41	179.00	214.00	35.00	.060	.29	27.89
87-V-42	150.80	156.00	5.20	.028	.10	30.28
87-V-43	99.80	114.20	14.40	.011	.06	29.48
87-V-44	138.70	145.50	6.80	.002	.09	29.45
	Average		18.26	.047	.22	28.64

(File: VILSUM3)

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VILLALTA-PROJECT--ASSAY RESULTS

WEIGHTED AVERAGES.....

DDH#	Sample#	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT-AU	OPT-AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT-AU	OPT-AG	% FE
87-V-1	8540	1.00	3.50	2.50	.30	1.07	.76	H	.675	2.05	29.46	1.00	13.20	12.20	.747	1.74	29.43
87-V-1	8541	3.50	6.00	2.50	1.07	1.83	.76	H	.592	1.07	29.29						
87-V-1	8542	6.00	9.28	3.28	1.83	2.83	1.00	H	1.644	2.66	23.09						
87-V-1	8543	9.28	13.20	3.92	2.83	4.02	1.20	H	.140	1.19	34.81						
87-V-1	8544	13.20	15.80	2.60	4.02	4.82	.79	C+B	.031	.51	9.06						
87-V-1	91501	15.80	18.00	2.20	4.82	5.49	.67	C+B	.001	.02	5.90						
87-V-1	91502	18.00	21.00	3.00	5.49	6.40	.91	C+B	.001	.04	6.27						
87-V-1	91523	21.00	24.28	3.28	6.40	7.40	1.00	C+B	.001	.69	25.57						
87-V-1	91524	24.28	27.56	3.28	7.40	8.40	1.00	C+B	.001	.53	22.96						
87-V-1	91525	27.56	31.30	3.74	8.40	9.54	1.14	C+B	.001	.38	18.46						
87-V-1	91503	31.30	35.00	3.70	9.54	10.67	1.13	C+B	.001	.29	8.57						
87-V-2	8545	0.00	6.00	6.00	.00	1.83	1.83	H	.005	.24	26.17	0.00	19.20	19.20	.045	.43	23.22
87-V-2	8546	6.00	9.00	3.00	1.83	2.74	.91	H	.027	.36	28.30						
87-V-2	91504	9.00	10.70	1.70	2.74	3.26	.52	C+H	.001	.01	9.40						
87-V-2	8547	10.70	11.20	.50	3.26	3.41	.15	T	.007	.06	32.63						
87-V-2	91505	11.20	16.20	5.00	3.41	4.94	1.52	C	.001	.03	16.70						
87-V-2	8548	16.20	19.20	3.00	4.94	5.85	.91	C	.248	1.86	29.39						
87-V-2	91506	19.20	22.00	2.80	5.85	6.71	.85	T	.001	.15	5.02						
87-V-2	91507	22.00	24.00	2.00	6.71	7.32	.61	T	.001	.07	5.77						
87-V-2	91508	24.00	26.40	2.40	7.32	8.05	.73	T	.001	.31	12.53						
87-V-2	91509	26.40	31.00	4.60	8.05	9.45	1.40	T+C	.001	.70	15.88						
87-V-2	91510	31.00	36.00	5.00	9.45	10.98	1.52	C	.001	.25	4.56						
87-V-2	91511	36.00	41.30	5.30	10.98	12.59	1.62	L	.001	.17	7.28						
87-V-3	91526	0.00	6.00	6.00	.00	1.83	1.83	CB	.001	.14	5.89						
87-V-3	91527	6.00	9.28	3.28	1.83	2.83	1.00	CB	.001	.27	7.55						
87-V-3	91528	9.28	12.56	3.28	2.83	3.83	1.00	CB	.001	.46	5.17						
87-V-3	91529	12.56	15.84	3.28	3.83	4.83	1.00	CB	.001	.33	3.91						
87-V-3	91530	15.84	19.12	3.28	4.83	5.83	1.00	CB	.001	.14	3.60						
87-V-4	8549	0.00	6.00	6.00	.00	1.83	1.83	H+T	.047	.20	34.26	0.00	6.00	6.00	.047	.20	34.26
87-V-4	91531	6.00	9.00	3.00	1.83	2.74	.91	T	.008	.17	30.36						
87-V-4	91532	9.00	12.00	3.00	2.74	3.66	.91	T	.004	.23	28.10						
87-V-4	91533	12.00	15.28	3.28	3.66	4.66	1.00	C	.002	.05	5.32						
87-V-4	91534	15.28	18.56	3.28	4.66	5.66	1.00	C	.001	.01	4.64						
87-V-4	91535	18.56	21.84	3.28	5.66	6.66	1.00	C	.001	.02	3.38						
87-V-4	91536	21.84	25.12	3.28	6.66	7.66	1.00	CB	.001	.02	6.88						
87-V-4	91537	25.12	28.40	3.28	7.66	8.66	1.00	CB	.044	.17	8.33						
87-V-4	91538	28.40	32.40	4.00	8.66	9.88	1.22	CB	.016	.54	12.84						
87-V-4	91539	41.00	46.00	5.00	12.50	14.02	1.52	C+CB	.002	.21	5.63						
87-V-4A	8550	0.00	3.50	3.50	.00	1.07	1.07	H	.212	.19	39.82	0.00	6.00	6.00	.127	.12	36.31
87-V-4A	8551	3.50	6.00	2.50	1.07	1.83	.76	H	.008	.01	31.39						
87-V-5	8554	0.00	2.00	2.00	.00	.61	.61	T	.002	.01	28.10						
87-V-5	8564	2.00	6.00	4.00	.61	1.83	1.22	T	.167	.04	33.30	2.00	19.00	17.00	.101	.14	30.22
87-V-5	8555	6.00	7.00	1.00	1.83	2.13	.30	T	.011	.04	37.63						
87-V-5	8556	7.00	10.70	3.70	2.13	3.26	1.13	T	.097	.11	36.94						
87-V-5	8557	10.70	14.40	3.70	3.26	4.39	1.13	T	.122	.16	38.62						
87-V-5	8558	14.40	16.50	2.10	4.39	5.03	.64	T	.024	.16	17.99						

CANAMIN RESOURCES LTD

VILLALTA PROJECT: ASSAY RESULTS

WEIGHTED AVERAGES.....

DDH #	Sample #	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT AU	OPT AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT AU	OPT AG	% FE
87-V-5	91540	16.50	19.00	2.50	5.03	5.79	.76	C	.068	.33	10.20						
87-V-5	91541	19.00	22.80	3.80	5.79	6.95	1.16	C	.001	.02	7.16						
87-V-5	91542	22.80	26.00	3.20	6.95	7.93	.98	C	.001	.01	7.72						
87-V-5	91543	26.00	30.00	4.00	7.93	9.15	1.22	C	.002	.03	5.73						
87-V-5A	8552	0.00	3.50	3.50	.00	1.07	1.07	TB+H	.128	.01	37.26	0.00	7.00	7.00	.082	.01	39.18
87-V-5A	8553	3.50	7.00	3.50	1.07	2.13	1.07	TB+H	.036	.01	41.09						
87-V-6	8559	0.00	3.00	3.00	.00	.91	.91	CB+C	.004	.04	4.43						
87-V-6	8560	3.00	6.00	3.00	.91	1.83	.91	CB+C	.002	.05	3.55						
87-V-6	91512	6.00	9.28	3.28	1.83	2.83	1.00	CB+C	.001	.07	2.20						
87-V-6	91513	9.28	12.55	3.28	2.83	3.83	1.00	CB+C	.001	.08	1.25						
87-V-6	91514	12.55	15.84	3.28	3.83	4.83	1.00	CB+C	.002	.13	4.75						
87-V-6	91515	15.84	19.12	3.28	4.83	5.83	1.00	CB+C	.001	.07	10.57						
87-V-6	91516	19.12	22.40	3.28	5.83	6.83	1.00	CB+C	.001	.02	3.60						
87-V-6	91517	22.40	25.68	3.28	6.83	7.83	1.00	CB+C	.001	.05	8.51						
87-V-6	91518	25.68	28.96	3.28	7.83	8.83	1.00	CB+C	.001	.11	6.46						
87-V-6	91519	28.96	32.24	3.28	8.83	9.83	1.00	CB+C	.001	.11	6.79						
87-V-6	91520	32.24	35.52	3.28	9.83	10.83	1.00	CB+C	.001	.08	8.21						
87-V-6	91521	35.52	38.80	3.28	10.83	11.83	1.00	CB+C	.001	.13	7.00						
87-V-6	91522	38.80	41.00	2.20	11.83	12.50	.67	CB+C	.001	.06	4.71						
87-V-7	8561	0.00	3.50	3.50	.00	1.07	1.07	TB	.043	.01	12.57	0.00	9.50	9.50	.016	.02	27.84
87-V-7	8562	3.50	5.00	1.50	1.07	1.52	.46	TB	.001	.03	28.94						
87-V-7	8563	5.00	9.50	4.50	1.52	2.90	1.37	H	.001	.02	39.36						
87-V-7	91544	9.50	12.00	2.50	2.90	3.66	.76	TB	.003	.04	26.98						
87-V-7	91545	12.00	15.00	3.00	3.66	4.57	.91	TB	.047	.23	30.58						
87-V-7	8633	15.00	19.20	4.20	4.57	5.85	1.28	C+PY	.007	.27	29.50						
87-V-7	91546	19.20	22.48	3.28	5.85	6.85	1.00	CB	.002	.07	10.92						
87-V-7	91547	22.48	25.76	3.28	6.85	7.85	1.00	CB	.004	.27	9.99						
87-V-7	91548	25.76	29.04	3.28	7.85	8.85	1.00	CB	.011	.23	9.60						
87-V-7	91549	29.04	34.01	4.97	8.85	10.37	1.52	CB	.010	.12	4.13						
87-V-8	8501	0.00	4.00	4.00	.00	1.22	1.22	CB	.004	.22	12.65						
87-V-8	8502	4.00	7.28	3.28	1.22	2.22	1.00	CB	.002	.07	9.48						
87-V-8	8503	7.28	10.56	3.28	2.22	3.22	1.00	CB	.012	.18	7.69						
87-V-8	8504	10.56	13.50	2.94	3.22	4.12	.90	CB	.022	.47	8.54						
87-V-8	8680	13.50	16.78	3.28	4.12	5.12	1.00	L	.002	.01	.32						
87-V-8	8681	16.78	20.06	3.28	5.12	6.12	1.00	L	.001	.01	.19						
87-V-9	8682	0.00	6.00	6.00	.00	1.83	1.83	RUBBLE C?	.015	.18	19.54						
87-V-9	8505	6.00	8.50	2.50	1.83	2.59	.76	C+CB	.011	.09	8.77						
87-V-9	8506	8.50	11.78	3.28	2.59	3.59	1.00	C+CB	.001	.05	3.09						
87-V-9	8507	11.78	15.06	3.28	3.59	4.59	1.00	C+CB	.001	.03	4.85						
87-V-9	8508	15.06	18.34	3.28	4.59	5.59	1.00	C+CB	.001	.04	4.43						
87-V-9	8509	18.34	21.62	3.28	5.59	6.59	1.00	C+CB	.002	.04	1.55						
87-V-9	8510	21.62	24.90	3.28	6.59	7.59	1.00	C+CB	.001	.03	2.15						
87-V-9	8511	24.90	28.00	3.10	7.59	8.54	.95	C+CB	.001	.12	2.59						
87-V-10	8573	0.00	3.50	3.50	.00	1.07	1.07	T+H	.340	6.02	27.94	0.00	17.56	17.56	.265	2.12	26.00
87-V-10	8512	3.50	6.50	3.00	1.07	1.98	.91	TB	.601	3.17	34.02						
87-V-10	8574	6.50	7.50	1.00	1.98	2.29	.30	PY	.120	1.61	31.20						

CANAHIN RESOURCES LTD

VILLALTA-PROJECT--ASSAY-RESULTS

WEIGHTED AVERAGES.....

DDH #	Sample #	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT-AU	OPT-AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT-AU	OPT-AG	% FE
87-V-10	8575	7.50	11.00	3.50	2.29	3.35	1.07	H	.288	.37	30.77						
87-V-10	8513	11.00	14.28	3.28	3.35	4.35	1.00	TB	.008	.15	8.46						
87-V-10	8514	14.28	17.56	3.28	4.35	5.35	1.00	CB	.154	.99	27.44						
87-V-10	8515	17.56	21.00	3.44	5.35	6.40	1.05	CB	.024	.17	8.91						
87-V-10	8683	21.00	23.50	2.50	6.40	7.16	.76	LB	.002	.03	1.98						
87-V-10	8684	23.50	26.00	2.50	7.16	7.93	.76	LB	.001	.02	.40						
87-V-10	8516	26.00	29.28	3.28	7.93	8.93	1.00	CB	.002	.05	5.56						
87-V-10	8517	29.28	33.60	4.32	8.93	10.24	1.32	CB	.001	.09	4.27						
87-V-11	8565	0.00	5.00	5.00	.00	1.52	1.52	H	.021	.13	37.20	0.00	27.60	27.60	.025	.16	34.24
87-V-11	8566	5.00	9.00	4.00	1.52	2.74	1.22	H	.023	.21	38.34						
87-V-11	8567	9.00	12.28	3.28	2.74	3.74	1.00	H	.104	.43	34.05						
87-V-11	8568	12.28	15.56	3.28	3.74	4.74	1.00	H	.027	.10	35.91						
87-V-11	8569	15.56	18.84	3.28	4.74	5.74	1.00	H	.018	.10	30.29						
87-V-11	8570	18.84	22.12	3.28	5.74	6.74	1.00	H	.001	.07	30.22						
87-V-11	8571	22.12	25.40	3.28	6.74	7.74	1.00	H	.001	.08	32.21						
87-V-11	8572	25.40	27.60	2.20	7.74	8.41	.67	H	.001	.11	32.82						
87-V-11	8518	27.60	31.00	3.40	8.41	9.45	1.04	CB	.012	.20	14.18						
87-V-11	8519	31.00	34.28	3.28	9.45	10.45	1.00	CB	.001	.15	10.13						
87-V-11	8520	34.28	37.56	3.28	10.45	11.45	1.00	CB	.001	.11	7.31						
87-V-11	8521	37.56	40.84	3.28	11.45	12.45	1.00	CB	.001	.15	7.94						
87-V-11	8522	40.84	44.12	3.28	12.45	13.45	1.00	CB	.001	.03	6.13						
87-V-11	8523	44.12	46.60	2.48	13.45	14.21	.76	CB	.002	.10	7.51						
87-V-12	8576	0.00	4.00	4.00	.00	1.22	1.22	TB	.010	.07	33.45						
87-V-12	8577	4.00	7.28	3.28	1.22	2.22	1.00	H	.152	.12	39.32	4.00	36.10	32.10	.118	.26	38.63
87-V-12	8578	7.28	10.56	3.28	2.22	3.22	1.00	H	.228	.23	38.41						
87-V-12	8579	10.56	13.84	3.28	3.22	4.22	1.00	H	.044	.18	38.28						
87-V-12	8580	13.84	17.12	3.28	4.22	5.22	1.00	H	.134	.44	33.51						
87-V-12	8581	17.12	20.40	3.28	5.22	6.22	1.00	H	.376	.49	37.84						
87-V-12	8582	20.40	23.68	3.28	6.22	7.22	1.00	H	.025	.19	35.44						
87-V-12	8583	23.68	26.96	3.28	7.22	8.22	1.00	H	.096	.21	42.81						
87-V-12	8584	26.96	30.24	3.28	8.22	9.22	1.00	H	.095	.10	40.40						
87-V-12	8585	30.24	33.52	3.28	9.22	10.22	1.00	H	.001	.04	42.71						
87-V-12	8586	33.52	36.10	2.58	10.22	11.01	.79	H	.008	.74	37.30						
87-V-12	8524	36.10	39.00	2.90	11.01	11.89	.88	CB	.003	.25	12.85						
87-V-12	8525	39.00	41.00	2.00	11.89	12.50	.61	CB	.001	.11	8.24						
87-V-12	8685	41.00	43.75	2.75	12.50	13.34	.84	L	.004	.02	1.48						
87-V-12	8686	43.75	46.50	2.75	13.34	14.18	.84	L	.001	.01	.56						
87-V-12	8526	46.50	51.00	4.50	14.18	15.55	1.37	LB+CB	.023	.14	7.44						
87-V-12	8527	51.00	55.50	4.50	15.55	16.92	1.37	LB+CB	.011	.07	3.95						
87-V-13	8587	0.00	3.28	3.28	.00	1.00	1.00	H	.023	.08	27.15	0.00	15.00	15.00	.125	.71	33.14
87-V-13	8588	3.28	6.56	3.28	1.00	2.00	1.00	H	.015	.28	25.39						
87-V-13	8589	6.56	9.84	3.28	2.00	3.00	1.00	H+T	.438	.59	33.59						
87-V-13	8590	9.84	13.12	3.28	3.00	4.00	1.00	T+(H)	.087	2.10	42.51						
87-V-13	8591	13.12	15.00	1.88	4.00	4.57	.57	T+(H)	.012	.38	39.95						
87-V-13	8592	15.00	18.28	3.28	4.57	5.57	1.00	CB	.020	.52	20.51						
87-V-13	8593	18.28	21.56	3.28	5.57	6.57	1.00	CB	.002	.11	9.07						

CANAMIN RESOURCES LTD

VILLALTA PROJECT: ASSAY RESULTS

WEIGHTED AVERAGES.....

DDH #	Sample #	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT AU	OPT AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT AU	OPT AG	% FE
87-V-13	8687	21.56	23.20	1.64	6.57	7.07	.50	LB	.002	.05	8.35						
87-V-13	8688	23.20	26.48	3.28	7.07	8.07	1.00	L	.001	.02	.23						
87-V-14	8595	0.00	6.00	6.00	.00	1.83	1.83	RUBBLE	.005	.17	18.98						
87-V-14	8596	6.00	7.00	1.00	1.83	2.13	.30	TB	.010	.31	16.46						
87-V-14	8528	7.00	10.28	3.28	2.13	3.13	1.00	C	.003	.18	15.81						
87-V-14	8529	10.28	13.56	3.28	3.13	4.13	1.00	C	.001	.13	8.19						
87-V-14	8530	13.56	16.84	3.28	4.13	5.13	1.00	C	.003	.74	21.09						
87-V-14	8531	16.84	20.12	3.28	5.13	6.13	1.00	C	.001	.27	11.68						
87-V-14	8532	20.12	23.40	3.28	6.13	7.13	1.00	C	.001	.23	11.90						
87-V-14	8533	23.40	26.68	3.28	7.13	8.13	1.00	C+CB	.001	.05	2.86						
87-V-14	8534	26.68	31.00	4.32	8.13	9.45	1.32	CB	.001	.14	7.59						
87-V-14	8535	31.00	36.00	5.00	9.45	10.98	1.52	CB	.002	.07	6.54						
87-V-15	8603	0.00	3.00	3.00	.00	.91	.91	TB+H	.040	.10	28.70	0.00	27.80	27.80	.010	.10	25.91
87-V-15	8604	3.00	6.00	3.00	.91	1.83	.91	TB+H	.038	.18	22.20						
87-V-15	8536	6.00	10.00	4.00	1.83	3.05	1.22	TB	.004	.16	16.07						
87-V-15	8597	10.00	13.28	3.28	3.05	4.05	1.00	H	.001	.14	37.97						
87-V-15	8598	13.28	16.56	3.28	4.05	5.05	1.00	H	.008	.11	37.73						
87-V-15	8599	16.56	19.84	3.28	5.05	6.05	1.00	H	.001	.03	26.22						
87-V-15	8600	19.84	23.12	3.28	6.05	7.05	1.00	H	.001	.01	22.40						
87-V-15	8601	23.12	26.40	3.28	7.05	8.05	1.00	H	.001	.05	22.25						
87-V-15	8602	26.40	27.80	1.40	8.05	8.48	.43	H	.001	.06	16.08						
87-V-15	8537	27.80	32.80	5.00	8.48	10.00	1.52	CB	.001	.33	10.91						
87-V-15	8605	32.80	36.08	3.28	10.00	11.00	1.00	H	.002	.03	25.28						
87-V-15	8606	36.08	40.50	4.42	11.00	12.35	1.35	H	.001	.03	18.05						
87-V-15	8538	40.50	43.78	3.28	12.35	13.35	1.00	CB	.001	.09	8.86						
87-V-15	8539	43.78	47.00	3.22	13.35	14.33	.98	CB	.003	.08	5.48						
87-V-16	8607	0.00	4.00	4.00	.00	1.22	1.22	T, TB+(H)	.026	.38	21.49	0.00	7.28	7.28	.016	.35	18.71
87-V-16	8608	4.00	7.28	3.28	1.22	2.22	1.00	T, TB+(H)	.004	.31	15.31						
87-V-16	8689	7.28	10.56	3.28	2.22	3.22	1.00	MT	.003	.04	21.34						
87-V-16	8690	10.56	13.84	3.28	3.22	4.22	1.00	MT	.005	.09	16.05						
87-V-16	8691	13.84	15.72	1.88	4.22	4.79	.57	MT	.001	.01	21.33						
87-V-16	8609	15.72	19.00	3.28	4.79	5.79	1.00	CB	.011	.10	16.71						
87-V-16	8610	19.00	22.28	3.28	5.79	6.79	1.00	CB	.004	.04	9.72						
87-V-16	8692	22.28	22.56	.28	6.79	6.88	.09	CB	.002	.09	5.77						
87-V-16	8693	25.56	28.84	3.28	7.79	8.79	1.00	CB	.003	.06	3.66						
87-V-16	8694	28.84	32.12	3.28	8.79	9.79	1.00	CB	.001	.04	2.74						
87-V-16	8695	32.12	34.00	1.88	9.79	10.37	.57	CB	.002	.03	2.52						
87-V-17	8611	0.00	6.00	6.00	.00	1.83	1.83	H	.007	.24	35.80	0.00	6.00	6.00	.007	.24	35.80
87-V-17	8612	6.00	9.28	3.28	1.83	2.83	1.00	CB	.003	.28	9.02						
87-V-17	8613	9.28	12.56	3.28	2.83	3.83	1.00	C	.001	.01	3.19						
87-V-17	8614	12.56	15.84	3.28	3.83	4.83	1.00	C	.001	.02	1.93						
87-V-17	8615	15.84	19.12	3.28	4.83	5.83	1.00	C+T+CB	.004	.10	8.42						
87-V-17	8616	19.12	24.00	4.88	5.83	7.32	1.49	CB	.001	.10	5.12						
87-V-17	8696	24.00	26.50	2.50	7.32	8.08	.76	L	.001	.01	.55						
87-V-17	8697	26.50	28.71	2.21	8.08	8.75	.67	L	.001	.08	5.31						
87-V-18	8617	0.00	2.00	2.00	.00	.61	.61	H	.001	.03	27.15	0.00	11.60	11.60	.190	.47	27.23

CANAMIN RESOURCES LTD

VILLALTA-PROJECT--ASSAY-RESULTS

WEIGHTED AVERAGES.....

DDH #	Sample #	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT AU	OPT AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT AU	OPT AG	% FE
87-V-18	8618	2.00	5.28	3.28	.61	1.61	1.00	H	.017	1.34	31.78						
87-V-18	8619	5.28	8.56	3.28	1.61	2.61	1.00	H	.356	.16	25.83						
87-V-18	8620	8.56	11.60	3.04	2.61	3.54	.93	H	.322	.17	23.89						
87-V-18	8621	11.60	14.00	2.40	3.54	4.27	.73	C+LB	.009	.03	5.00						
87-V-18	8622	14.00	16.50	2.50	4.27	5.03	.76	LB	.003	.01	2.21						
87-V-18	8698	16.50	19.78	3.28	5.03	6.03	1.00	L	.001	.03	.29						
87-V-18	8699	19.78	22.00	2.22	6.03	6.71	.68	L	.001	.01	.14						
87-V-19	8623	0:00	4:00	4:00	.00	1.22	1.22	RUBBLE	.001	.01	5.43						
87-V-19	8624	4.00	7.50	3.50	1.22	2.29	1.07	H	.059	.04	21.99	4.00	14.50	10.50	.087	.05	22.85
87-V-19	8625	7.50	11.00	3.50	2.29	3.35	1.07	H	.190	.09	28.47						
87-V-19	8625	11.00	14.50	3.50	3.35	4.42	1.07	TB	.013	.02	18.10						
87-V-19	8627	14.50	18.00	3.50	4.42	5.49	1.07	C+(L)	.006	.01	3.45						
87-V-19	8700	18.00	21.28	3.28	5.49	6.49	1.00	L	.001	.04	2.01						
87-V-20	8628	0:00	4:50	4:50	.00	1.37	1.37	TB	.025	.02	31.17						
87-V-20	8629	4.50	8.00	3.50	1.37	2.44	1.07	TB	.002	.01	4.15						
87-V-20	8630	15.90	19.18	3.28	4.85	5.85	1.00	C	.003	.03	4.51						
87-V-20	8631	19.18	22.46	3.28	5.85	6.85	1.00	C	.001	.05	1.23						
87-V-20	8632	22.46	25.74	3.28	6.85	7.85	1.00	C	.003	.01	1.50						
87-V-21	8659	3.00	6.28	3.28	.91	1.91	1.00	CB	.001	.01	3.85						
87-V-21	8660	6.28	9.56	3.28	1.91	2.91	1.00	CB	.001	.17	12.04						
87-V-21	8661	9.56	12.84	3.28	2.91	3.91	1.00	CB	.001	.12	7.66						
87-V-21	8662	12.84	15.50	2.66	3.91	4.73	.81	CB	.001	.04	1.59						
87-V-22	8663	6:00	10:50	4:50	1.83	3.20	1.37	CB	.004	.01	10.17						
87-V-23	8664	0.00	4.00	4.00	.00	1.22	1.22	RUBBLE	.105	.03	10.28	0.00	4.00	4.00	.105	.03	10.28
87-V-23	8665	4.00	7.00	3.00	1.22	2.13	.91	RUBBLE	.001	.01	9.73						
87-V-23	8666	7.00	10.00	3.00	2.13	3.05	.91	RUBBLE & T	.029	.01	6.24						
87-V-24	8634	6.00	9.28	3.28	1.83	2.83	1.00	H	.004	.11	35.08	6.00	15.90	9.90	.037	.13	38.36
87-V-24	8635	9.28	12.56	3.28	2.83	3.83	1.00	H	.083	.15	40.84						
87-V-24	8636	12.56	14.60	2.04	3.83	4.45	.62	H	.023	.08	44.39						
87-V-24	8637	14.60	15.90	1.30	4.45	4.85	.40	H	.026	.18	30.90						
87-V-24	8638	15.90	19.18	3.28	4.85	5.85	1.00	CB	.001	.04	4.58						
87-V-24	8639	19.18	22.46	3.28	5.85	6.85	1.00	CB	.001	.02	2.74						
87-V-24	8640	22.46	25.74	3.28	6.85	7.85	1.00	CB	.002	.01	3.02						
87-V-24	8641	25.74	29.02	3.28	7.85	8.85	1.00	CB	.002	.01	2.81						
87-V-24	8642	29.02	32.30	3.28	8.85	9.85	1.00	CB	.001	.01	3.15						
87-V-24	8643	32.30	35.58	3.28	9.85	10.85	1.00	CB	.002	.01	2.18						
87-V-24	8644	35.58	40.00	4.42	10.85	12.20	1.35	CB	.001	.03	2.70						
87-V-26	8715	41.00	43.00	2.00	12.50	13.11	.61	TB	.002	.04	21.47						
87-V-26	8716	43.00	45.50	2.50	13.11	13.87	.76	TB	.002	.03	19.14						
87-V-26	8717	45.50	48.00	2.50	13.87	14.63	.76	TB	.002	.01	22.25						
87-V-26	8718	48.00	52.15	4.15	14.63	15.90	1.27	TB	.009	.05	27.37						
87-V-26	8719	52.15	54.40	2.25	15.90	16.59	.69	TB	.005	.12	25.03						
87-V-26	8720	57.68	60.96	3.28	17.59	18.59	1.00	T&CB	.011	.04	14.77						
87-V-26	8721	60.96	64.24	3.28	18.59	19.59	1.00	CB	.010	.23	8.09						
87-V-26	8722	64.24	67.52	3.28	19.59	20.59	1.00	CB&C	.028	.09	7.90						
87-V-27	8645	12.00	13.30	1.30	3.66	4.05	.40	T	.013	.09	26.91	12.00	19.10	7.10	.009	.09	35.64

CANAMIN RESOURCES LTD

VILLALTA PROJECT: ASSAY RESULTS

WEIGHTED AVERAGES.....

DDH #	Sample #	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT AU	OPT AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT AU	OPT AG	% FE
87-V-27	8646	13.30	16.20	2.90	4.05	4.94	.88	H	.015	.15	37.69						
87-V-27	8647	16.20	19.10	2.90	4.94	5.82	.88	H	.002	.04	37.50						
87-V-27	8648	19.10	22.38	3.28	5.82	6.82	1.00	CB	.002	.02	10.60						
87-V-28	8667	11.00	13.00	2.00	3.35	3.96	.61	TB	.001	.08	17.55						
87-V-28	8668	13.00	16.50	3.50	3.96	5.03	1.07	TB&LB	.001	.05	9.87						
87-V-29	8669	8.00	11.00	3.00	2.44	3.35	.91	LB	.002	.04	4.97						
87-V-29	8670	11.00	13.00	2.00	3.35	3.96	.61	LB	.006	.01	10.56						
87-V-29	8671	13.00	16.28	3.28	3.96	4.96	1.00	L	.001	.01	.33						
87-V-29	8672	16.28	19.56	3.28	4.96	5.96	1.00	L	.001	.03	.44						
87-V-30	8655	9.00	12.80	3.80	2.74	3.90	1.16	CB	.010	.10	10.10	9.00	17.20	8.20	.162	.46	17.55
87-V-30	8656	12.80	15.00	2.20	3.90	4.57	.67	HB	.490	.90	23.89						
87-V-30	8657	15.00	17.20	2.20	4.57	5.24	.67	H	.096	.66	24.09						
87-V-30	8658	17.20	20.48	3.28	5.24	6.24	1.00	CB	.001	.03	4.56						
87-V-30	8673	20.48	23.76	3.28	6.24	7.24	1.00	CB	.001	.07	4.62						
87-V-30	8674	23.76	27.04	3.28	7.24	8.24	1.00	CB	.001	.01	5.58						
87-V-31	8649	0.00	4.00	4.00	.00	1.22	1.22	H	.001	.07	36.08	0.00	20.00	20.00	.198	.53	41.22
87-V-31	8650	4.00	9.28	5.28	1.22	2.83	1.61	H	.042	.15	39.22						
87-V-31	8651	6.28	12.56	6.28	1.91	3.83	1.91	H	.018	.24	37.85						
87-V-31	8652	12.56	15.84	3.28	3.83	4.83	1.00	H	1.056	2.16	38.20						
87-V-31	8653	15.84	20.00	4.16	4.83	6.10	1.27	H	.038	.24	26.42						
87-V-31	8654	20.00	21.42	1.42	6.10	6.53	.43	CB	.010	.13	33.16						
87-V-31	8675	21.42	24.70	3.28	6.53	7.53	1.00	C	.001	.13	11.55						
87-V-31	8676	24.70	27.98	3.28	7.53	8.53	1.00	C	.002	.15	3.78						
87-V-31	8677	27.98	31.26	3.28	8.53	9.53	1.00	C	.002	.09	2.06						
87-V-31	8678	31.26	34.54	3.28	9.53	10.53	1.00	C	.001	.03	1.95						
87-V-31	8679	34.54	37.82	3.28	10.53	11.53	1.00	C	.001	.04	4.09						
87-V-31	8701	37.82	41.10	3.28	11.53	12.53	1.00	C	.001	.01	2.67						
87-V-31	8702	41.10	44.38	3.28	12.53	13.53	1.00	C	.001	.01	2.77						
87-V-31	8703	44.38	47.66	3.28	13.53	14.53	1.00	C (+PY)	.001	.03	3.90						
87-V-31	8704	47.66	50.94	3.28	14.53	15.53	1.00	C (+PY)	.001	.13	4.04						
87-V-31	8705	50.94	54.22	3.28	15.53	16.53	1.00	C (+PY)	.001	.19	5.16						
87-V-31	8706	54.22	56.00	1.78	16.53	17.07	.54	C (+PY)	.001	.14	3.55						
87-V-32	8707	7.00	9.70	2.70	2.13	2.96	.82	TB	.001	.04	18.15						
87-V-32	8708	9.70	12.80	3.10	2.96	3.90	.95	H	.228	.14	26.41	9.70	12.80	3.10	.228	.14	26.41
87-V-32	8709	12.85	16.00	3.15	3.92	4.88	.96	LB	.006	.06	5.89						
87-V-32	8710	16.00	19.28	3.28	4.88	5.88	1.00	LB	.001	.08	2.92						
87-V-32	8711	19.28	22.56	3.28	5.88	6.88	1.00	LB	.001	.05	1.51						
87-V-32	8712	22.56	25.84	3.28	6.88	7.88	1.00	C	.001	.02	1.49						
87-V-32	8713	25.84	30.76	4.92	7.88	9.38	1.50	C	.001	.03	1.35						
87-V-32	8714	30.76	35.30	4.54	9.38	10.76	1.38	C&LB	.001	.01	3.28						
87-V-33	8723	12.90	15.50	2.60	3.93	4.73	.79	TB	.031	.07	20.30						
87-V-33	8724	20.00	23.28	3.28	6.10	7.10	1.00	TB	.001	.06	8.70						
87-V-33	8725	23.28	26.56	3.28	7.10	8.10	1.00	C	.001	.01	2.06						
87-V-33	8726	26.56	29.84	3.28	8.10	9.10	1.00	C	.001	.01	1.22						
87-V-33	8727	29.84	34.10	4.26	9.10	10.40	1.30	C	.001	.01	1.15						
87-V-33	8728	39.94	43.22	3.28	12.18	13.18	1.00	T	.001	.02	3.23						

CANAMIN RESOURCES LTD

VILLALTA PROJECT- ASSAY RESULTS

WEIGHTED AVERAGES.....

DDH #	Sample #	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT AU	OPT AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT AU	OPT AG	% FE
87-V-33	8729	43.22	46.50	3.28	13.18	14.18	1.00	T	.001	.06	4.20						
87-V-34	8730	18.52	21.80	3.28	5.65	6.65	1.00	TB	.002	.10	9.07						
87-V-34	8731	21.80	25.08	3.28	6.65	7.65	1.00	C	.001	.02	1.15						
87-V-34	8732	25.08	28.36	3.28	7.65	8.65	1.00	C	.001	.05	.91						
87-V-34	8733	28.36	31.64	3.28	8.65	9.65	1.00	C	.001	.01	1.05						
87-V-34	8734	31.64	34.92	3.28	9.65	10.65	1.00	C	.001	.05	2.23						
87-V-35	8774	0	1.83	1.83	.00	.56	.56	TB	.099	.14	34.07						
87-V-35	8775	3.66	4.57	.91	1.12	1.39	.28	TB	.005	.12	6.61						
87-V-35	8776	4.57	5.57	1.00	1.39	1.70	.30	TB	.001	.04	1.4						
87-V-35	8777	5.57	6.57	1.00	1.70	2.00	.30	TB	.001	.02	1.02						
87-V-35	8778	6.57	7.31	.74	2.00	2.23	.23	TB	.001	.02	.98						
87-V-35	8779	7.31	7.92	.61	2.23	2.41	.19	TB	.001	.07	3.93						
87-V-37	8735	2.00	4.00	2.00	.61	1.22	.61	H	.001	.09	29.83	2.00	15.40	13.40	.005	.14	28.17
87-V-37	8736	4.00	6.00	2.00	1.22	1.83	.61	H	.003	.09	36.36						
87-V-37	8737	6.00	9.28	3.28	1.83	2.83	1.00	H	.004	.19	17.65						
87-V-37	8738	9.28	12.56	3.28	2.83	3.83	1.00	H	.007	.15	31.80						
87-V-37	8739	12.56	15.40	2.84	3.83	4.70	.87	H	.008	.14	29.19						
87-V-37	8766	4.69	5.69	1.00	1.43	1.73	.30	CB	.001	.06	3.3						
87-V-37	8767	5.69	6.4	.71	1.73	1.95	.22	CB	.001	.03	4.76						
87-V-37	8768	6.4	7.16	.76	1.95	2.18	.23	CB	.001	.01	8.66						
87-V-37	8769	7.16	8.16	1.00	2.18	2.49	.30	CB	.001	.02	1.96						
87-V-37	8770	8.16	9.16	1.00	2.49	2.79	.30	CB	.001	.01	1.67						
87-V-37	8771	9.16	10.16	1.00	2.79	3.10	.30	CB	.001	.01	2.37						
87-V-37	8772	10.16	10.97	.81	3.10	3.34	.25	CB	.001	.11	4.35						
87-V-37A	8751	2.00	4.00	2.00	.61	1.22	.61	H	.002	.10	35.14						
87-V-37A	8752	4.00	6.00	2.00	1.22	1.83	.61	H	.002	.16	38.20						
87-V-38	8740	0.00	3.00	3.00	.00	.91	.91	H	.004	.40	29.44	0.00	27.00	27.00	.017	.27	31.17
87-V-38	8741	3.00	6.00	3.00	.91	1.83	.91	H	.061	.08	29.37						
87-V-38	8742	6.00	9.28	3.28	1.83	2.83	1.00	H	.031	.22	31.83						
87-V-38	8743	9.28	12.56	3.28	2.83	3.83	1.00	H	.035	.27	35.88						
87-V-38	8744	12.56	15.84	3.28	3.83	4.83	1.00	H	.007	.43	36.73						
87-V-38	8745	15.84	19.12	3.28	4.83	5.83	1.00	H	.001	.62	36.88						
87-V-38	8746	19.12	22.40	3.28	5.83	6.83	1.00	H	.001	.15	24.36						
87-V-38	8747	22.40	25.68	3.28	6.83	7.83	1.00	H	.001	.06	26.07						
87-V-38	8748	25.68	27.00	1.32	7.83	8.23	.40	H	.001	.04	27.52						
87-V-38	8749	27.00	31.00	4.00	8.23	9.45	1.22	CB	.001	.04	7.27						
87-V-38	8764	31.00	33.50	2.50	9.45	10.21	.76	CB	.001	.19	5.21						
87-V-38	8765	43.50	46.00	2.50	13.26	14.02	.76	L	.001	.03	2.36						
87-V-39	8753	5.20	8.48	3.28	1.59	2.59	1.00	H	.081	.70	35.32	5.20	11.70	6.50	.060	.68	34.02
87-V-39	8754	8.48	11.70	3.22	2.59	3.57	.98	H	.039	.65	32.70						
87-V-39	8755	11.70	14.98	3.28	3.57	4.57	1.00	CB	.001	.05	4.91						
87-V-39	8756	14.98	18.26	3.28	4.57	5.57	1.00	CB	.001	.13	5.07						
87-V-39	8757	18.26	21.54	3.28	5.57	6.57	1.00	CB	.001	.03	2.57						
87-V-39	8758	21.54	24.82	3.28	6.57	7.57	1.00	CB	.001	.10	1.89						
87-V-39	8759	24.82	28.10	3.28	7.57	8.57	1.00	CB	.001	.08	1.82						
87-V-39	8760	28.10	31.38	3.28	8.57	9.57	1.00	CB	.001	.01	2.59						

CANAMIN RESOURCES LTD

VILLALTA PROJECT: ASSAY RESULTS

WEIGHTED AVERAGES.....

DDH#	Sample#	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT AU	OPT AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT AU	OPT AG	% FE
87-V-39	8761	31.38	34.66	3.28	9.57	10.57	1.00	CB	.001	.04	2.13						
87-V-39	8762	34.66	37.30	2.64	10.57	11.37	.80	CB	.001	.13	3.67						
87-V-39	8763	44.80	47.40	2.60	13.66	14.45	.79	L	.001	.03	1.92						
87-V-40	8773	13.00	14.50	1.50	3.96	4.42	.46	L	.001	.01	.58						
87-V-41	8791	175.72	179.00	3.28	53.57	54.57	1.00	TB	.013	.13	15.77						
87-V-41	8792	179.00	182.28	3.28	54.57	55.57	1.00	H	.016	.06	30.01	179.00	214.00	35.00	.060	.29	27.89
87-V-41	8793	182.28	185.56	3.28	55.57	56.57	1.00	H	.046	.09	28.20						
87-V-41	8794	185.56	188.84	3.28	56.57	57.57	1.00	H	.010	.12	29.37						
87-V-41	8795	188.84	192.12	3.28	57.57	58.57	1.00	H	.011	.05	29.43						
87-V-41	8796	192.12	195.40	3.28	58.57	59.57	1.00	H	.089	.07	30.31						
87-V-41	8797	195.40	198.68	3.28	59.57	60.57	1.00	H	.088	.16	26.86						
87-V-41	8798	198.68	201.96	3.28	60.57	61.57	1.00	H	.249	.65	25.50						
87-V-41	8799	201.96	205.24	3.28	61.57	62.57	1.00	H	.045	.55	29.62						
87-V-41	8800	205.24	208.52	3.28	62.57	63.57	1.00	H	.051	.50	23.98						
87-V-41	8801	208.52	211.80	3.28	63.57	64.57	1.00	H	.005	.51	27.93						
87-V-41	8802	211.80	214.00	2.20	64.57	65.24	.67	H	.052	.46	24.51						
87-V-41	8854	214.00	217.00	3.00	65.24	66.16	.91	L	.002	.24	22.21						
87-V-41	8865	245.00	249.00	4.00	74.70	75.91	1.22	T	.003	.05	33.27						
87-V-41	8835	249.00	252.28	3.28	75.91	76.91	1.00	TB	.005	.11	34.65						
87-V-41	8836	252.28	255.56	3.28	76.91	77.91	1.00	TB	.001	.02	29.85						
87-V-41	8837	255.56	258.84	3.28	77.91	78.91	1.00	TB	.002	.16	29.37						
87-V-41	8838	258.84	262.12	3.28	78.91	79.91	1.00	TB	.002	.07	27.05						
87-V-41	8839	262.12	264.50	2.38	79.91	80.64	.73	CB	.004	.01	12.38						
87-V-41	8840	264.50	268.00	3.50	80.64	81.71	1.07	CB	.002	.06	10.83						
87-V-41	8841	268.00	271.70	3.70	81.71	82.84	1.13	B	.009	.11	28.50						
87-V-41	8842	271.70	274.98	3.28	82.84	83.84	1.00	T	.004	.07	31.05						
87-V-41	8843	274.98	278.26	3.28	83.84	84.84	1.00	T	.006	.08	31.90						
87-V-41	8844	278.26	281.54	3.28	84.84	85.84	1.00	T	.007	.09	27.18						
87-V-41	8845	281.54	284.82	3.28	85.84	86.84	1.00	T	.001	.07	26.87						
87-V-41	8846	284.82	288.10	3.28	86.84	87.84	1.00	T	.001	.01	32.31						
87-V-41	8847	288.10	291.35	3.25	87.84	88.83	.99	T	.002	.05	19.79						
87-V-42	8803	147.51	150.80	3.29	44.97	45.98	1.00	TB	.019	.12	18.58						
87-V-42	8804	150.80	154.08	3.28	45.98	46.98	1.00	H	.004	.12	30.91	150.80	156.00	5.20	.028	.10	30.28
87-V-42	8805	154.08	156.00	1.92	46.98	47.56	.59	H	.068	.07	29.21						
87-V-42	8806	156.00	159.28	3.28	47.56	48.56	1.00	L	.020	.02	5.52						
87-V-42	8807	159.28	162.56	3.28	48.56	49.56	1.00	L	.027	.06	9.40						
87-V-42	8808	162.56	165.84	3.28	49.56	50.56	1.00	L	.013	.06	12.38						
87-V-42	8809	165.84	169.12	3.28	50.56	51.56	1.00	L	.001	.01	1.39						
87-V-42	8810	169.12	170.50	1.38	51.56	51.98	.42	L	.002	.03	7.05						
87-V-42	8811	170.50	173.78	3.28	51.98	52.98	1.00	L+PY	.052	.08	27.17						
87-V-42	8812	173.78	177.06	3.28	52.98	53.98	1.00	L+PY	.062	.32	30.76						
87-V-42	8813	177.06	179.70	2.64	53.98	54.79	.80	L+PY+MS	.022	.33	31.00						
87-V-42	8814	179.70	181.50	1.80	54.79	55.34	.55	L+PY	.005	.09	24.27						
87-V-42	8815	181.50	183.50	2.00	55.34	55.95	.61	B+L	.009	.04	13.11						
87-V-42	8816	183.50	186.78	3.28	55.95	56.95	1.00	L+PY	.004	.05	10.76						
87-V-42	8817	186.78	190.06	3.28	56.95	57.95	1.00	L+(PY)	.001	.01	2.77						

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VILLALTA PROJECT: ASSAY RESULTS

WEIGHTED AVERAGES.....

DDH #	Sample #	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT AU	OPT AG	% FE	From(Ft)	To(Ft)	Interval(Ft)	OPT AU	OPT AG	% FE
87-V-43	8818	99.80	103.08	3.28	30.43	31.43	1.00	B+H	.008	.03	27.56	99.80	114.20	14.40	.011	.06	29.48
87-V-43	8819	103.08	106.00	2.92	31.43	32.32	.89	B+H	.015	.05	24.26						
87-V-43	8820	106.00	109.28	3.28	32.32	33.32	1.00	H	.022	.06	28.08						
87-V-43	8821	109.28	112.56	3.28	33.32	34.32	1.00	H	.005	.05	34.71						
87-V-43	8822	112.56	114.20	1.64	34.32	34.82	.50	H	.002	.12	34.98						
87-V-43	8823	114.20	117.48	3.28	34.82	35.82	1.00	LB	.001	.06	9.05						
87-V-43	8824	117.48	120.76	3.28	35.82	36.82	1.00	LB+H	.005	.40	15.97						
87-V-43	8825	120.76	124.04	3.28	36.82	37.82	1.00	LB+H	.049	.33	17.46						
87-V-43	8826	124.04	127.32	3.28	37.82	38.82	1.00	LB+H	.030	.26	21.39						
87-V-43	8827	127.32	131.50	4.18	38.82	40.09	1.27	LB+H	.115	.17	20.53						
87-V-43	8750	161.67	164.67	3.00	49.29	50.20	.91	L+PY	.012	.15	2.50						
87-V-44	8828	138.70	140.45	1.75	42.29	42.82	.53	H	.002	.05	33.72	138.70	145.50	6.80	.002	.09	29.45
87-V-44	8829	140.45	143.50	3.05	42.82	43.75	.93	H	.001	.11	29.83						
87-V-44	8830	143.50	145.50	2.00	43.75	44.36	.61	H	.002	.08	25.15						
87-V-44	8831	145.50	148.20	2.70	44.36	45.18	.82	CHL+PY	.004	.11	28.04						
87-V-44	8832	148.20	149.45	1.25	45.18	45.56	.38	T	.003	.86	24.65						
87-V-44	8833	149.45	152.78	3.33	45.56	46.58	1.02	L	.001	.02	5.55						
87-V-44	8834	165.45	168.25	2.80	50.44	51.30	.85	L+PY	.001	.08	19.49						
87-V-45	8848	119.90	122.90	3.00	36.55	37.47	.91	CB	.012	.06	9.85						
87-V-45	8849	122.90	125.00	2.10	37.47	38.11	.64	CB+H	.037	.05	22.16						
87-V-45	8850	125.00	127.25	2.25	38.11	38.80	.69	CB+H	.001	.02	11.58						
87-V-45	8851	127.25	130.53	3.28	38.80	39.80	1.00	L+H	.005	.02	1.92						
87-V-45	8852	138.75	141.33	2.58	42.30	43.09	.79	CB+H	.007	.21	24.98						
87-V-45	8853	141.33	142.29	.96	43.09	43.38	.29	H	.014	.20	34.39						
87-V-45	8855	142.29	145.67	3.38	43.38	44.41	1.03	CB	.001	.21	28.54						
87-V-45	8856	145.67	148.77	3.10	44.41	45.36	.95	CB	.001	.15	23.68						
87-V-45	8857	148.77	150.10	1.33	45.36	45.76	.41	CB	.001	.08	13.79						
87-V-46	8858	98.70	103.00	4.30	30.09	31.40	1.31	REG	.001	.01	12.85						
87-V-46	8859	103.00	106.28	3.28	31.40	32.40	1.00	T	.001	.01	3.76						
87-V-46	8860	106.28	108.50	2.22	32.40	33.08	.68	T	.001	.10	10.81						
87-V-46	8861	108.50	110.80	2.30	33.08	33.78	.70	LB+H	.002	.05	7.00						
87-V-46	8862	110.80	112.80	2.00	33.78	34.39	.61	LB+H	.005	.15	13.02						
87-V-46	8863	112.80	116.08	3.28	34.39	35.39	1.00	L	.001	.01	.38						
87-V-46	8864	159.40	161.40	2.00	48.60	49.21	.61	L+HS	.005	.42	20.18						
87-V-47	8866	19.22	22.50	3.28	5.86	6.86	1.00	TB	.001	.01	26.44						
87-V-47	8867	22.50	25.78	3.28	6.86	7.86	1.00	H	.003	.12	38.82	22.50	48.20	25.70	.163	.23	35.91
87-V-47	8868	25.78	29.10	3.32	7.86	8.87	1.01	H	.001	.11	43.21						
87-V-47	8869	29.10	32.38	3.28	8.87	9.87	1.00	H	.001	.02	33.67						
87-V-47	8870	32.38	35.66	3.28	9.87	10.87	1.00	H	.039	.07	34.96						
87-V-47	8871	35.66	38.94	3.28	10.87	11.87	1.00	H	.025	.10	33.18						
87-V-47	8872	38.94	42.70	3.76	11.87	13.02	1.15	H	.017	.14	35.84						
87-V-47	8873	42.70	45.98	3.28	13.02	14.02	1.00	H	.640	.21	36.11						
87-V-47	8874	45.98	48.20	2.22	14.02	14.70	.68	H	.808	1.52	29.21						
87-V-47	8875	48.20	51.48	3.28	14.70	15.70	1.00	LB	.007	.38	5.92						
87-V-48	8876	9.00	11.00	2.00	2.74	3.35	.61	TB	.023	.24	35.24						
87-V-48	8877	11.00	13.30	2.30	3.35	4.05	.70	TB	.009	.17	31.30						

CAJAHIN RESOURCES LTD

VILLALTA-PROJECT--ASSAY-RESULTS

WEIGHTED AVERAGES.....

DDH#	Sample#	From(Ft)	To(Ft)	Interval(Ft)	From(m)	To(m)	Interval(m)	Rock	OPT-AU	OPT-AG	%FE	From(Ft)	To(Ft)	Interval(Ft)	OPT-AU	OPT-AG	%FE
87-V-48	8878	13.30	16.56	3.26	4.05	5.05	.99	H	.002	.14	34.64	13.30	43.70	30.40	.064	.37	34.12
87-V-48	8879	16.56	19.84	3.28	5.05	6.05	1.00	H	.009	.14	35.75						
87-V-48	8880	19.84	23.12	3.28	6.05	7.05	1.00	H	.028	.22	31.74						
87-V-48	8881	23.12	26.40	3.28	7.05	8.05	1.00	H	.005	.21	34.75						
87-V-48	8882	26.40	29.68	3.28	8.05	9.05	1.00	H	.001	.25	35.95						
87-V-48	8883	29.68	32.96	3.28	9.05	10.05	1.00	H	.005	.08	38.78						
87-V-48	8884	32.96	36.24	3.28	10.05	11.05	1.00	H	.020	.41	38.18						
87-V-48	8885	36.24	39.52	3.28	11.05	12.05	1.00	H	.192	.57	36.72						
87-V-48	8886	39.52	42.30	2.78	12.05	12.90	.85	H	.292	.94	24.04						
87-V-48	8887	42.30	43.70	1.40	12.90	13.32	.43	CB	.198	1.49	22.32						
87-V-48	8888	43.70	47.00	3.30	13.32	14.33	1.01	CB	.009	.14	9.75						
87-V-48	8889	47.00	51.30	4.30	14.33	15.64	1.31	CB	.008	.16	6.13						
87-V-48	8890	51.30	54.00	2.70	15.64	16.46	.82	CB	.002	.11	5.41						
87-V-48	8891	54.00	57.28	3.28	16.46	17.46	1.00	L	.001	.02	.60						
87-V-48	8892	57.28	60.56	3.28	17.46	18.46	1.00	L	.001	.02	.68						
87-V-48	8893	60.56	63.84	3.28	18.46	19.46	1.00	L+PY	.003	.03	.86						
87-V-48	8894	122.00	125.28	3.28	37.20	38.20	1.00	L+PY	.001	.05	.34						
87-V-48	8895	125.28	128.56	3.28	38.20	39.20	1.00	SST	.001	.19	.64						

GEOCHEMICAL/ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE CA P CR NG BA TI B AL NA K W SI ZR CE SH Y_ AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: Core AG# AU# BY FIRE ASSAY.

DATE RECEIVED: MAY 14 1987 DATE REPORT MAILED: *May 19/87* ASSAYER: *D. J. G.* DEAN TOYE, CERTIFIED B.C. ASSAYER

CANAMIN RESOURCES PROJECT - 87V File # 87-1287

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	NG	BA	TI	B	AL	NA	K	W	AG#	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	PPM	PPM	OZ/T	OZ/T
91501	2	949	16	808	1.7	22	9	2084	5.90	9	5	ND	1	2	3	2	7	48	.20	.015	3	13	.12	4	.01	4	.09	.01	.02	1	.02	.001
91502	1	1262	8	967	2.7	20	10	1225	6.27	3	5	ND	1	2	2	3	2	65	.12	.012	5	14	.09	5	.01	10	.13	.01	.01	1	.04	.001
91503	2	2742	14	1974	9.0	33	19	1488	8.57	2	5	ND	1	4	5	2	2	106	.37	.033	7	19	.38	4	.01	6	.15	.01	.01	1	.29	.001
91504	3	468	30	1265	1.4	9	13	3304	9.40	10	5	ND	1	4	2	2	10	52	.24	.074	5	27	.08	2	.01	6	.08	.01	.01	4	.01	.001
91505	3	638	27	2518	1.9	19	30	4450	16.70	22	5	ND	2	6	4	2	8	117	.57	.106	9	63	.33	5	.01	5	.14	.01	.01	9	.03	.001
91506	1	5574	25	504	5.3	5	12	1135	5.02	8	5	ND	1	3	1	3	2	266	.17	.072	4	19	.01	4	.01	2	.06	.01	.01	57	.15	.001
91507	2	2076	23	1074	2.4	13	37	4627	5.77	2	5	ND	1	5	4	2	2	89	.19	.059	5	22	.06	7	.01	2	.06	.01	.01	12	.07	.001
91508	3	7336	24	2666	10.9	22	56	5034	12.53	5	5	ND	1	9	6	2	2	228	.58	.169	20	33	.35	9	.01	2	.29	.01	.01	3	.31	.001
91509	4	7792	37	5333	22.4	27	56	2475	15.88	4	5	ND	1	8	3	2	2	156	.40	.072	12	18	.82	9	.01	7	2.27	.01	.01	1	.70	.001
91510	4	2499	18	3468	7.2	23	16	2319	4.56	5	5	ND	1	3	40	2	2	93	.21	.045	11	12	.25	2	.01	5	.15	.01	.01	1	.25	.001
91511	10	2695	363	3702	5.7	43	23	2291	7.28	78	5	ND	1	5	22	3	2	123	.32	.065	18	21	.58	5	.01	2	.75	.01	.01	1	.17	.001
91512	1	71	10	42	2.8	2	2	57	2.20	154	5	ND	1	1	1	2	2	150	.01	.009	3	7	.01	1	.01	3	.08	.01	.01	1	.07	.006
91513	1	185	8	30	1.9	3	3	90	1.25	96	5	ND	1	1	1	2	2	138	.01	.002	4	6	.01	1	.01	2	.04	.01	.01	3	.08	.001
91514	1	592	38	414	4.0	41	39	607	4.75	440	5	ND	1	1	6	5	2	207	.08	.019	7	11	.17	2	.01	6	.11	.01	.01	1	.13	.002
91515	3	166	100	1356	2.1	70	26	1038	10.57	123	5	ND	1	3	10	2	2	131	.29	.049	19	16	.54	4	.01	6	.27	.01	.01	1	.07	.001
91516	6	187	95	800	.6	25	8	558	3.40	92	5	ND	1	89	6	2	2	74	28.72	.055	12	7	.24	5	.01	2	.13	.01	.01	1	.02	.001
91517	8	567	472	3930	2.4	61	33	1247	8.51	397	5	ND	3	9	35	2	2	357	2.90	.059	11	15	.37	2	.01	2	.23	.01	.01	1	.05	.001
91518	2	482	145	4068	2.8	42	23	1440	6.46	360	6	ND	4	24	30	2	2	364	7.94	.069	18	14	.48	2	.01	4	.16	.01	.01	1	.11	.001
91519	1	357	175	2397	3.4	44	32	989	4.79	277	5	ND	1	3	16	2	2	277	.69	.038	6	12	.38	2	.01	5	.18	.01	.01	1	.11	.001
91520	1	190	184	2596	2.3	36	20	1132	8.21	288	5	ND	3	22	17	2	2	320	6.28	.042	13	11	.69	2	.01	5	.10	.01	.01	1	.08	.001
91521	1	857	153	2401	3.2	62	29	881	7.00	291	5	ND	1	10	14	2	2	348	2.34	.091	12	17	.41	2	.01	4	.23	.01	.01	1	.13	.001
91522	1	399	105	1487	1.6	52	16	1256	4.71	128	6	ND	4	39	10	2	2	298	11.41	.048	12	8	.99	4	.01	5	.15	.01	.01	1	.06	.001
91523	3	7539	46	2155	22.2	27	24	4872	27.57	23	5	ND	3	7	3	2	5	348	.31	.130	14	77	.03	11	.02	2	.15	.01	.01	50	.69	.004
91524	3	7248	44	1638	17.1	14	18	1449	22.96	38	5	ND	2	4	3	4	5	213	.18	.114	13	75	.02	14	.01	2	.08	.01	.02	65	.53	.001
91525	3	8124	38	1334	11.7	17	16	1213	18.46	25	5	ND	1	3	3	2	9	281	.22	.101	10	62	.04	10	.01	10	.11	.01	.01	97	.38	.001
91526	1	2051	10	1072	5.0	34	10	1004	5.89	2	5	ND	1	3	1	2	3	96	.20	.048	31	18	.21	5	.01	8	.16	.01	.01	1	.14	.001
91527	1	3091	14	1596	8.6	39	13	1586	7.55	2	5	ND	1	4	4	2	2	129	.21	.062	27	22	.26	8	.01	6	.24	.01	.01	1	.27	.001
91528	1	5866	21	1348	15.9	38	8	1933	5.17	2	5	ND	2	15	4	2	2	86	4.13	.060	23	15	.09	5	.01	5	.17	.01	.01	1	.46	.001
91529	1	3858	12	1139	10.6	31	6	1674	3.91	3	8	ND	4	43	3	2	2	67	15.92	.083	15	15	.19	3	.01	2	.14	.01	.01	1	.33	.001
STD C	19	58	40	134	6.8	65	28	994	3.86	40	18	8	33	47	17	14	18	60	.45	.091	35	59	.91	176	.08	37	1.73	.06	.14	13	-	-

GEOCHEMICAL/ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR NG BA TI B W AND LIMITED FOR RA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Core AGst AND AUst BY FIRE ASSAY.

DATE RECEIVED: MAY 21 1987 DATE REPORT MAILED: *May 25/87* ASSAYER: *D. J. J.* DEAN TOYE, CERTIFIED B.C. ASSAYER

CANAMIN RESOURCES File # 87-1367 Page 1

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AGst	AUst	
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM	PPM	PPM
8501	1	368	89	1699	7.4	49	47	1789	12.65	117	5	ND	1	8	7	2	2	191	1.43	.051	13	21	.63	7	.01	2	2.09	.01	.01	1	.22	.004	
8502	2	328	190	904	2.9	17	13	1027	9.48	25	5	ND	1	5	1	2	3	70	.45	.015	4	27	.55	8	.01	2	.72	.01	.01	1	.07	.002	
8503	2	723	194	1466	6.2	41	9	975	7.69	32	5	ND	1	6	6	2	4	88	.53	.053	13	34	.64	6	.01	2	.50	.01	.01	1	.18	.012	
8504	1	1554	334	3816	15.7	85	13	1137	8.54	89	5	ND	1	15	22	2	16	239	2.10	.234	26	80	.90	9	.01	2	.89	.01	.01	1	.47	.022	
8505	2	312	64	2500	2.6	26	16	2158	8.77	46	5	ND	1	39	24	2	13	121	9.24	.067	13	13	.27	13	.01	2	.24	.04	.01	1	.09	.011	
8506	1	529	220	1097	1.5	29	7	572	3.09	125	5	ND	1	1	12	4	3	27	.08	.005	10	9	.11	5	.01	2	.10	.01	.01	1	.05	.001	
8507	1	633	157	663	1.6	24	18	750	4.85	107	5	ND	1	4	3	2	2	55	.43	.009	6	11	.48	2	.01	2	.11	.01	.01	1	.03	.001	
8508	4	871	98	670	1.1	32	18	790	4.43	64	5	ND	1	4	3	2	2	84	.36	.003	3	9	.58	2	.01	2	.15	.01	.01	1	.04	.001	
8509	1	766	44	545	1.1	23	5	675	1.55	61	5	ND	1	22	4	4	2	55	2.55	.004	11	9	.96	2	.01	2	.09	.01	.01	1	.04	.002	
8510	1	1522	27	704	1.3	34	6	869	2.15	25	5	ND	1	25	5	5	2	107	3.56	.005	16	10	1.21	3	.01	2	.21	.02	.01	1	.03	.001	
8511	5	2158	167	1043	4.6	61	12	1018	2.59	214	5	ND	1	26	7	7	2	73	3.78	.020	10	18	1.42	3	.01	2	.21	.02	.01	1	.12	.001	
8512	1	2471	2130	3468	94.7	36	46	3720	34.02	76	5	16	1	16	51	6	114	248	1.05	.186	11	50	.56	14	.01	2	.56	.01	.01	1	3.17	.601	
8513	1	400	1938	1338	4.7	55	52	1648	8.46	59	5	ND	1	4	16	3	3	192	.35	.017	5	10	.18	11	.01	2	.19	.01	.01	1	.15	.008	
8514	3	2318	2226	3848	31.9	77	54	3827	27.44	167	5	5	1	18	63	15	43	221	.88	.118	13	28	.52	52	.01	2	.45	.01	.01	8	.99	.154	
8515	3	1395	1153	2935	5.7	39	20	1257	8.91	565	5	ND	1	9	37	9	19	142	2.16	.028	6	20	.36	33	.01	2	.16	.01	.01	1	.17	.024	
8516	2	1011	124	1451	2.3	66	59	821	5.56	149	5	ND	1	8	7	2	3	78	.99	.062	20	18	.73	22	.01	2	.21	.01	.01	1	.05	.002	
8517	2	719	97	1354	3.2	48	31	792	4.27	78	5	ND	1	18	8	2	3	70	2.26	.237	26	18	.71	14	.01	2	.27	.01	.01	1	.09	.001	
8518	2	3044	19	2154	6.8	36	71	2216	14.18	21	5	ND	1	5	2	2	2	161	.52	.041	9	32	.42	14	.01	2	.23	.01	.01	10	.20	.012	
8519	1	2957	25	1480	5.1	25	42	1626	10.13	39	5	ND	1	3	3	2	3	98	.28	.040	12	17	.30	6	.01	2	.12	.01	.01	1	.15	.001	
8520	2	1196	93	2428	4.1	42	45	1053	7.31	17	5	ND	1	3	16	2	2	94	.25	.042	38	18	.47	6	.01	2	.18	.01	.01	1	.11	.001	
8521	1	1238	29	4259	4.4	59	19	1340	7.94	12	5	ND	1	6	39	2	2	101	.40	.096	36	20	.58	5	.01	2	.19	.01	.01	1	.15	.001	
8522	1	694	110	2734	1.5	31	11	1209	6.13	149	5	ND	1	4	23	6	2	70	.25	.046	31	14	.48	3	.01	2	.15	.01	.01	1	.03	.001	
8523	18	1524	841	4891	3.1	72	14	1392	7.51	145	5	ND	1	7	34	5	2	149	.54	.166	22	29	.71	4	.01	2	.63	.01	.01	1	.10	.002	
8524	1	3407	738	2816	8.6	27	44	1760	12.85	75	5	ND	1	5	31	5	5	210	.39	.044	5	28	.45	20	.01	4	.30	.01	.01	1	.25	.003	
8525	1	807	630	1870	3.7	25	39	1176	8.24	115	5	ND	1	5	20	6	4	77	.28	.026	25	15	.41	9	.01	4	.19	.01	.01	1	.11	.001	
8526	2	1299	660	3123	4.6	31	18	1354	7.44	159	5	ND	1	53	27	8	35	125	17.45	.184	18	27	.63	11	.01	2	.61	.04	.01	1	.14	.023	
8527	2	649	45	1635	1.9	33	7	713	3.95	101	5	ND	1	57	3	4	11	108	21.40	.134	25	20	.84	9	.01	2	.86	.04	.01	1	.07	.011	
8528	1	646	30	6831	6.2	70	24	2296	15.81	16	5	ND	2	7	43	2	3	164	.40	.104	34	12	.55	88	.01	4	.38	.01	.01	1	.18	.003	
8529	1	455	276	3654	3.7	32	17	1770	8.19	11	5	ND	1	4	27	2	5	113	.27	.037	28	18	.27	97	.01	4	.22	.01	.01	1	.13	.001	
8530	1	5500	42	4344	24.5	61	46	2937	21.09	10	5	ND	2	8	7	2	2	296	.44	.207	122	21	.36	123	.01	2	.27	.01	.01	1	.74	.003	
8531	1	2666	438	2836	9.3	33	27	1795	11.68	2	5	ND	1	6	6	2	2	157	.32	.052	53	25	.62	32	.01	2	.26	.01	.01	1	.27	.001	
8532	1	2219	87	5571	7.7	40	33	1918	11.90	18	5	ND	1	4	54	2	2	210	.26	.044	20	17	.50	22	.01	2	.18	.01	.01	1	.23	.001	
8533	1	481	24	2107	1.7	22	11	630	2.86	5	5	ND	1	2	26	2	2	88	.10	.032	18	10	.14	22	.01	2	.11	.01	.01	1	.05	.001	
8534	1	1583	34	5635	4.0	58	47	4895	7.59	28	5	ND	1	10	68	2	2	242	.20	.060	52	21	.31	109	.01	2	.20	.01	.01	1	.14	.001	
8535	1	960	68	3104	1.9	39	17	1563	6.54	183	5	ND	1	4	28	10	2	130	.28	.091	36	23	.36	6	.01	2	.17	.01	.01	1	.07	.002	
8536	1	738	20	3718	4.9	63	54	1074	16.07	20	5	ND	1	9	4	2	2	235	.47	.054	69	16	.46	20	.02	8	.31	.01	.01	1	.16	.004	
STD C	20	57	39	126	6.8	66	27	984	3.94	41	17	7	34	47	17	15	21	62	.48	.098	36	61	.88	177	.08	34	1.73	.07	.13	12	-	-	

CANAMIN RESOURCES FILE # 87-1367

Page 2

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA %	TI %	B PPM	AL %	NA %	K %	W PPM	AG#1 OZ/T	AU#1 OZ/T
8537	1	7169	13	2330	11.0	35	23	2742	10.91	18	5	ND	1	5	4	2	2	123	.60	.124	9	46	.45	5	.01	2	.19	.01	.01	3	.33	.001
8538	1	407	5	2952	2.9	29	32	1460	8.86	7	5	ND	1	5	16	2	2	99	.34	.038	10	17	.57	4	.01	3	.42	.01	.01	1	.09	.001
8539	1	895	194	2295	2.5	48	35	758	5.48	51	5	ND	1	3	8	2	2	121	.21	.061	32	28	.54	4	.01	2	.95	.01	.01	1	.08	.003
8540	1	6091	23	2040	60.6	13	43	3744	29.46	68	5	15	2	4	5	2	102	558	.28	.197	14	27	.11	4	.01	2	.21	.01	.01	6	2.05	.675
8541	1	3140	17	2119	31.6	10	30	2459	29.29	17	5	17	2	5	4	2	75	510	.40	.163	8	63	.13	3	.01	2	.16	.01	.01	4	1.07	.592
8544	1	3537	11	1187	16.2	26	10	1988	9.06	16	5	ND	1	3	4	2	116	142	.26	.055	10	55	.13	3	.01	2	.16	.01	.01	1	.51	.031
091530	1	1547	7	1199	4.7	32	6	1394	3.60	2	5	ND	1	50	3	2	2	62	17.82	.106	15	17	.17	3	.01	2	.14	.04	.01	1	.14	.001
091531	1	1166	14	3192	5.8	47	42	1908	30.36	6	5	ND	2	11	9	2	3	405	.80	.064	11	38	.66	4	.01	2	.38	.01	.01	1	.17	.008
091532	1	2374	487	3564	6.7	92	33	2167	28.10	29	5	ND	2	8	22	2	6	442	.74	.123	28	31	.72	4	.01	2	.33	.01	.01	1	.23	.004
091533	1	322	789	1016	2.3	42	7	503	5.32	9	5	ND	1	2	6	2	3	72	.13	.023	22	15	.19	2	.01	7	.16	.01	.01	1	.05	.002
091534	1	109	65	1327	.8	39	6	424	4.64	5	5	ND	1	2	18	2	2	58	.12	.039	18	15	.15	5	.01	2	.16	.01	.01	1	.01	.001
091535	1	61	15	948	.3	26	5	575	3.38	5	5	ND	1	2	10	2	4	45	.09	.038	20	7	.06	9	.01	3	.11	.01	.01	1	.02	.001
091536	1	122	37	2316	1.1	39	9	1477	6.98	7	5	ND	1	4	25	2	2	104	.21	.081	20	14	.18	86	.01	6	.17	.01	.01	1	.02	.001
091537	1	221	141	2809	5.5	42	10	1164	8.33	12	5	ND	1	3	32	2	3	167	.27	.054	12	19	.34	10	.01	2	.14	.01	.01	1	.17	.044
091538	1	1990	199	9509	17.5	78	18	2612	12.84	199	5	ND	2	5	162	23	23	400	.49	.076	24	23	.55	7	.01	2	.19	.01	.01	1	.54	.016
091539	1	1362	304	2389	7.4	46	12	1037	5.63	177	5	ND	1	3	16	2	3	108	.25	.051	18	18	.24	5	.01	5	.14	.01	.01	1	.21	.002
091540	1	217	58	493	10.3	13	10	1370	10.20	36	5	2	1	3	4	2	73	131	.29	.041	5	11	.15	6	.01	2	.11	.01	.01	47	.33	.068
091541	1	462	138	1177	1.1	19	15	2366	7.16	41	5	ND	1	2	29	2	2	260	.31	.040	7	6	.24	4	.01	2	.14	.01	.01	1	.02	.001
091542	1	130	7	555	.9	33	15	885	7.72	94	6	ND	1	1	1	2	3	104	.11	.008	3	6	.32	3	.01	2	.11	.01	.01	1	.01	.001
091543	1	344	129	2330	1.7	42	10	967	5.73	85	5	ND	1	2	21	2	2	101	.19	.040	11	17	.43	4	.01	2	.18	.01	.01	1	.03	.002
091544	1	662	2451	1276	1.5	16	14	2095	26.98	101	5	ND	1	14	17	15	4	318	1.10	.177	16	191	.54	19	.02	2	.48	.01	.01	1	.04	.003
091545	1	1860	1059	2699	7.1	22	35	2164	30.58	144	5	ND	1	13	18	2	59	343	.98	.151	14	85	.60	99	.01	2	1.29	.01	.01	1	.23	.047
091546	1	673	150	3592	2.2	33	28	1591	10.92	252	5	ND	1	3	39	2	2	151	.29	.023	6	16	.43	11	.01	2	.27	.01	.01	1	.07	.002
091547	1	1012	514	3094	8.4	28	25	1304	9.99	411	5	ND	1	3	22	2	2	124	.28	.028	16	12	.48	3	.01	2	.21	.01	.01	1	.27	.004
091548	1	1293	142	1678	7.3	32	12	965	9.60	369	6	ND	1	3	8	2	8	141	.33	.044	9	21	.48	3	.01	2	.22	.01	.01	1	.23	.011
091549	1	1403	101	2489	4.4	34	5	856	4.13	321	5	ND	1	31	15	2	8	74	11.73	.072	13	12	.20	5	.01	2	.16	.04	.01	1	.12	.010
STD C	20	56	39	127	6.8	68	27	979	4.02	41	13	7	34	47	17	18	20	63	.46	.098	35	58	.89	177	.08	34	1.73	.07	.13	15	-	-

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS, VANCOUVER B.C.
PH: (604) 253-3158 COMPUTER LINE: 251-1011

DATE RECEIVED JUNE 5 1987

DATE REPORTS MAILED

June 15/87

ASSAY CERTIFICATE

SAMPLE TYPE : REJECT
AU BY FIRE ASSAY
ND=None Detected

ASSAYER *Deane Toye* DEAN TOYE , CERTIFIED B.C. ASSAYER

CANAMIN RESOURCES LTD. FILE# 87-1367 R

PAGE# 1

SAMPLE	Sample wt. gm	Au-100 oz/t	Native Au mg	Average oz/t
8512	500	.661	.01	.662
8514	480	.199	ND	.199
8540	560	.466	ND	.466
8541	650	.751	ND	.751

GEOCHEMICAL/ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Core AGst BY FIRE ASSAY. AUst BY FIRE ASSAY

DATE RECEIVED: JUN 3 1987

DATE REPORT MAILED: June 10/87

ASSAYER: D. Toye DEAN TOYE, CERTIFIED B.C. ASSAYER

CANAMIN RESOURCES PROJECT - VA.

File # 87-1554A

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SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AGst	AUst	
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM	PPM	PPM
8603	1	306	75	3866	2.7	39	36	2217	28.70	25	5	ND	3	6	4	2	102	342	.10	.086	7	30	.28	19	.03	2	1.44	.01	.02	1	.10	.040	
8604	1	1957	62	4127	5.4	61	40	1643	22.20	9	5	ND	1	16	7	2	7	372	.90	.234	59	60	.52	10	.02	2	.58	.01	.02	1	.18	.038	
8657	1	3151	74	2571	17.1	22	25	3035	24.00	44	5	ND	6	50	11	2	38	746	10.40	.129	15	23	.62	6	.01	2	.00	.01	.01	34	.66	.096	
8658	1	837	23	1082	1.0	17	13	988	4.56	6	5	ND	1	53	9	2	2	77	3.83	.053	7	10	1.11	2	.01	2	.12	.01	.01	1	.03	.001	
8650	1	782	9	981	1.0	24	24	602	3.85	11	5	ND	1	3	1	2	2	59	.13	.024	53	7	.35	4	.01	2	.32	.01	.01	1	.01	.001	
8660	1	3076	51	3271	4.1	22	16	1412	12.04	8	5	ND	1	8	4	2	2	251	.49	.083	16	24	.70	8	.01	2	1.32	.01	.01	1	.17	.001	
8661	1	1953	106	2366	3.7	14	15	1019	7.66	8	5	ND	1	5	7	2	3	151	.40	.046	12	19	.57	5	.01	2	.75	.01	.02	1	.12	.001	
8662	1	315	33	411	1.5	21	4	482	1.59	12	5	ND	1	9	37	2	2	42	2.15	.008	15	10	.67	4	.01	2	.54	.01	.01	1	.04	.001	
8663	1	696	15	2134	.4	25	13	535	10.17	25	5	ND	1	5	6	2	14	48	.43	.073	22	7	.08	17	.01	2	.08	.01	.06	1	.01	.004	
8664	1	243	93	317	1.0	82	43	480	10.28	35	5	2	1	10	1	3	4	271	.29	.136	37	54	.26	117	.03	2	1.94	.01	.14	8	.03	.105	
8665	1	110	45	400	.2	85	53	673	9.73	8	5	ND	1	7	3	2	2	128	.23	.095	12	26	.23	130	.01	7	2.09	.01	.09	1	.01	.001	
8666	1	350	70	312	.4	38	33	587	6.24	4	5	ND	1	14	1	2	2	116	.75	.144	5	7	.21	160	.01	2	1.94	.01	.15	1	.01	.029	
8667	1	832	72	7646	1.8	112	41	3032	17.55	21	5	ND	4	31	43	2	2	648	5.91	.208	29	62	.75	61	.01	2	2.26	.01	.01	1	.08	.001	
8668	1	242	128	2866	.6	55	18	1761	9.87	17	5	ND	5	70	17	2	3	117	19.46	.120	17	25	.85	17	.01	2	2.28	.01	.01	1	.05	.001	
8669	1	436	75	1573	.7	57	37	1450	4.97	11	5	ND	3	77	16	2	2	291	10.38	.096	17	28	.77	15	.18	3	1.50	.03	.01	1	.04	.002	
8670	1	134	380	1650	.5	46	18	2055	10.56	16	5	ND	5	44	16	2	2	86	10.45	.114	31	27	1.01	24	.01	3	2.63	.01	.01	1	.01	.006	
8671	1	8	8	55	.1	5	3	935	.33	4	5	ND	3	95	2	3	7	5	26.24	.016	6	2	1.13	4	.01	3	.12	.01	.01	1	.01	.001	
8672	1	5	17	125	.2	4	1	1373	.44	4	5	ND	1	121	1	2	6	8	33.53	.022	9	3	.62	4	.01	2	.13	.01	.01	1	.03	.001	
8673	1	339	23	1208	1.5	21	10	884	4.62	6	5	ND	1	30	5	2	11	33	2.63	.062	6	10	.78	2	.01	2	.11	.01	.01	1	.07	.001	
8674	1	209	21	1510	.9	24	12	1097	5.58	5	5	ND	2	56	7	2	4	61	5.47	.071	10	9	1.26	5	.01	2	.16	.01	.01	1	.01	.001	
8675	2	2144	22	2193	4.2	21	46	1357	11.55	9	5	ND	2	11	2	2	2	59	.46	.048	4	9	.55	2	.01	2	.09	.01	.02	7	.13	.001	
8676	1	1679	20	1231	5.0	23	10	705	3.78	3	5	ND	1	34	5	2	2	29	2.06	.008	5	11	.68	2	.01	6	.00	.01	.01	1	.15	.002	
8677	1	983	253	837	3.8	18	5	448	2.06	2	5	ND	1	27	6	2	2	47	1.88	.034	13	5	.57	2	.01	7	.07	.01	.01	1	.09	.002	
8678	1	166	29	1039	.8	13	4	528	1.95	5	5	ND	1	27	9	2	2	28	3.99	.054	9	7	.64	2	.01	5	.09	.01	.01	1	.03	.001	
8679	2	834	79	2227	.7	44	11	685	4.09	65	5	ND	1	13	17	2	7	55	1.13	.044	9	9	.80	2	.01	2	.15	.01	.01	1	.04	.001	
8680	1	13	13	88	.4	4	1	661	.32	3	5	ND	1	120	1	2	5	2	38.07	.017	8	1	.14	4	.01	5	.02	.01	.01	1	.01	.002	
8681	1	3	11	26	.1	1	1	426	.10	3	5	ND	1	124	1	2	6	1	38.51	.014	6	1	.14	4	.01	5	.01	.01	.01	2	.01	.001	
8682	1	555	38	2146	4.9	85	59	1085	19.54	30	5	ND	1	20	1	2	2	268	.97	.077	26	82	.97	57	.11	6	4.15	.03	.05	1	.18	.015	
8683	1	127	55	470	.4	14	7	1005	1.98	36	5	ND	1	85	5	2	6	22	30.64	.064	16	3	.23	10	.01	2	.25	.01	.01	1	.03	.002	
8684	1	46	22	64	.4	4	1	515	.40	4	5	ND	1	111	1	2	7	4	36.16	.073	9	1	.17	24	.01	8	.05	.01	.01	1	.02	.001	
8685	1	226	117	530	.5	11	4	1138	1.48	68	5	ND	1	97	6	3	10	29	34.70	.055	14	3	.21	10	.01	2	.05	.01	.01	1	.02	.004	
8686	1	19	15	120	.2	4	3	765	.56	18	5	ND	1	117	1	2	6	9	37.48	.017	7	1	.22	4	.01	3	.01	.01	.01	2	.01	.001	
8687	7	761	653	2864	2.0	73	20	1343	8.35	159	5	ND	5	31	17	2	4	87	7.28	.333	29	10	.62	3	.01	2	.42	.01	.01	1	.05	.002	
8688	1	6	23	68	.3	2	1	481	.23	2	5	ND	1	115	1	2	7	1	38.34	.010	8	1	.17	4	.01	2	.01	.01	.01	1	.02	.001	
8689	1	241	87	3127	1.0	95	49	1642	21.34	18	5	ND	1	9	1	2	20	348	.32	.078	12	64	.85	32	.01	2	4.50	.01	.02	1	.04	.003	
8690	1	133	176	2093	2.3	92	30	1768	16.05	8	5	ND	1	7	2	2	4	196	.42	.035	11	68	.92	71	.01	2	3.80	.01	.14	1	.09	.005	
STD C	19	57	44	129	7.0	69	28	1012	3.88	42	10	8	33	48	17	18	10	62	.47	.101	35	57	.83	177	.08	37	1.60	.07	.13	12	2.94	-	

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	B1	V	CA	P	LA	CR	MG	BA	TI	B	AL	MA	K	N	AG#4	AUT#		
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
8691	1	79	73	2532	.3	101	38	1718	21.33	7	5	ND	1	6	1	2	2	225	.15	.001	23	95	1.14	61	.01	2	5.49	.01	.04	1	.01	.001		
8707	1	229	48	1042	.6	48	29	1510	18.15	10	5	ND	3	10	1	2	10	185	.25	.034	9	51	.63	32	.01	18	3.16	.01	.06	2	.04	.001		
8708	1	1340	72	1731	4.0	19	22	1244	26.41	51	5	6	4	30	7	2	117	457	2.91	.107	11	32	.33	9	.02	2	.42	.01	.03	34	.14	.228		
8709	1	512	30	1064	1.4	16	9	996	5.89	7	5	ND	7	62	4	2	2	76	12.89	.108	11	9	.33	4	.01	2	.15	.01	.01	3	.06	.006		
8710	1	656	40	1573	1.3	23	6	1408	2.92	10	5	ND	7	77	11	2	5	87	13.91	.051	12	10	1.07	5	.01	2	.39	.01	.01	4	.08	.001		
8711	1	94	35	513	.5	13	4	911	1.51	2	5	ND	6	68	2	2	2	30	20.14	.045	13	11	.48	2	.01	2	.41	.01	.01	1	.05	.001		
8712	1	86	29	387	.3	25	3	1136	1.49	5	5	ND	8	47	2	2	2	29	12.08	.054	16	8	.92	5	.01	2	.29	.01	.01	1	.02	.001		
8713	1	66	17	439	.2	16	4	739	1.35	6	5	ND	5	32	1	2	2	15	6.37	.030	8	5	.79	6	.01	2	.10	.01	.02	1	.03	.001		
8714	1	170	32	951	.7	36	7	937	3.28	36	5	ND	5	80	4	2	2	127	23.20	.117	16	14	.88	7	.01	2	1.20	.01	.01	1	.01	.001		
8715	1	671	67	664	1.5	58	23	3071	21.47	43	5	ND	3	32	25	2	86	1374	1.44	.521	20	125	.27	320	.02	2	1.42	.01	.06	14	.04	.002		
8716	1	711	34	874	.8	29	24	1238	19.14	15	5	ND	1	9	7	2	11	156	.47	.027	6	54	.65	35	.01	10	1.34	.01	.11	2	.03	.002		
8717	1	447	58	1206	.6	51	45	1474	22.25	15	5	ND	3	15	2	2	16	253	.56	.099	10	71	.95	40	.01	7	3.03	.01	.07	1	.01	.002		
8718	1	1011	250	1217	1.6	58	29	2936	27.37	21	5	ND	3	26	9	2	6	869	1.58	.324	13	63	.81	13	.01	2	.55	.01	.03	5	.05	.009		
8719	1	547	2833	1720	3.4	96	29	1728	25.03	20	5	ND	3	19	13	2	15	886	1.16	.254	13	41	.82	20	.01	9	1.70	.01	.05	4	.12	.005		
8720	1	938	29	1016	1.3	39	23	1442	14.77	8	5	ND	1	9	1	2	9	263	.43	.095	30	17	.90	32	.01	6	2.65	.01	.12	1	.04	.011		
8721	1	1447	124	2452	4.9	60	19	855	8.09	14	5	ND	4	52	41	2	10	274	7.16	2.350	105	15	.53	14	.01	2	1.20	.01	.01	15	.23	.010		
8722	5	532	139	1844	2.2	35	9	682	7.90	51	5	2	1	17	22	2	11	161	1.84	.609	52	13	.60	9	.01	2	.85	.01	.03	6	.09	.028		
8735	1	1029	194	824	2.2	10	12	328	29.83	154	5	ND	3	5	3	20	8	409	.13	.072	8	1	.03	27	.01	19	.11	.01	.03	89	.09	.001		
8736	1	2845	101	4071	5.9	37	40	2056	36.36	89	5	ND	4	12	11	4	2	376	.52	.062	12	22	.49	20	.05	9	.62	.02	.04	38	.19	.003		
8737	2	2306	20	2486	3.8	56	28	2297	17.65	13	5	ND	2	10	6	2	2	203	.49	.084	12	16	.28	5	.01	6	.09	.01	.02	14	.15	.004		
8738	1	2313	53	4191	4.5	67	40	2926	31.80	29	5	ND	2	17	9	2	2	408	1.13	.087	21	33	.59	7	.01	2	.20	.01	.03	28	.14	.007		
8739	1	3241	66	4085	11.8	45	41	2707	29.19	17	5	ND	4	27	12	2	2	397	2.12	.098	20	18	.93	5	.01	8	.17	.01	.02	23	.40	.008		
8740	1	381	99	1186	3.4	10	16	489	29.44	30	5	ND	2	4	10	2	15	750	.13	.181	5	29	.04	18	.01	7	.08	.01	.02	14	.08	.004		
8741	1	480	108	1270	6.4	14	21	734	29.37	39	5	ND	3	11	5	2	66	1197	.26	.138	8	26	.16	11	.04	16	.20	.01	.02	16	.22	.041		
8742	1	675	111	1621	8.4	12	17	1611	31.83	44	5	ND	3	7	7	2	147	1387	.25	.086	3	16	.17	7	.01	14	.09	.01	.02	26	.27	.031		
8743	1	1428	90	3922	9.2	37	28	3148	35.88	39	5	ND	3	21	10	2	328	725	.63	.089	9	28	.70	9	.01	26	.30	.01	.08	16	.43	.035		
8744	2	3931	135	4018	18.3	24	22	2982	36.73	46	7	ND	3	28	12	2	31	406	.82	.088	7	22	.47	9	.03	18	.23	.01	.03	38	.62	.007		
8745	4	4030	89	5780	4.0	17	19	2509	36.88	45	5	ND	3	24	9	5	2	156	.71	.058	6	10	.74	9	.02	21	.33	.01	.03	66	.15	.001		
8746	3	1544	65	2759	2.0	12	20	1776	24.36	37	5	ND	2	12	4	2	3	148	.39	.023	4	13	.56	7	.03	4	.17	.01	.01	38	.06	.001		
8747	4	1284	50	6049	1.6	27	33	2941	26.07	21	5	ND	2	22	9	2	2	154	1.11	.027	7	12	1.14	7	.01	11	.12	.01	.03	51	.06	.001		
8751	1	2531	332	1802	3.0	7	19	446	35.14	164	5	ND	3	6	7	23	2	582	.04	.056	11	3	.03	37	.05	18	.17	.01	.02	74	.10	.002		
8752	1	3229	110	4209	4.1	41	36	2466	38.20	72	5	ND	3	12	15	13	2	471	.63	.064	11	22	.51	16	.02	22	.49	.01	.04	56	.16	.002		
8753	1	1551	265	2591	21.7	26	41	3824	35.32	55	5	3	3	14	16	2	226	665	.89	.099	9	21	.34	11	.01	11	.32	.01	.01	21	.70	.081		
8754	1	1850	217	1810	19.9	15	29	2770	32.70	74	5	ND	3	16	9	6	42	388	.91	.087	11	24	.46	14	.05	17	.39	.01	.03	44	.65	.039		
STD C	20	61	40	140	6.7	68	30	1031	3.92	42	15	8	33	49	18	17	22	64	.45	.096	36	57	.86	181	.08	33	1.75	.07	.14	13	-	-		

GEOCHEMICAL/ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR NA FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: Core AG# BY FIRE ASSAY. AU# BY FIRE ASSAY

DATE RECEIVED: JUN 11 1987 DATE REPORT MAILED: *June 15 1987* ASSAYER: *D. J. ...* DEAN TOYE, CERTIFIED B.C. ASSAYER

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SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AG#	AU#	
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	%	PPM	QZ/T	QZ/T
8692	1	828	532	3191	3.5	91	11	980	5.77	233	5	ND	1	3	19	2	2	96	.12	.008	20	24	.57	5	.01	3	.17	.01	.01	1	.09	.002	
8693	1	492	110	1884	1.2	65	8	1221	3.64	162	5	ND	1	8	7	2	2	75	.60	.011	29	18	.74	2	.01	2	.13	.01	.01	1	.06	.003	
8694	1	436	17	1672	1.6	59	7	879	2.74	41	5	ND	1	13	10	3	2	73	.86	.179	32	20	.49	8	.01	3	.24	.01	.01	1	.04	.001	
8695	1	410	16	1438	2.3	54	6	907	2.52	33	5	ND	1	9	5	16	2	63	.80	.160	32	17	.48	3	.01	2	.32	.01	.01	1	.03	.002	
8696	1	291	13	153	.4	11	1	385	.55	3	5	ND	1	113	1	2	9	11	44.93	.160	15	5	.28	3	.01	3	.05	.05	.01	4	.01	.001	
8697	1	659	65	1225	2.3	61	12	1137	5.31	66	5	ND	3	44	5	2	2	77	9.71	.343	33	16	1.32	3	.01	2	.48	.07	.01	1	.08	.001	
8698	1	13	12	67	.4	3	1	394	.29	5	5	ND	8	112	1	2	7	3	74.54	.032	8	2	.16	3	.01	4	.03	.31	.01	6	.03	.001	
8699	1	3	6	24	.3	1	1	328	.14	2	5	ND	6	118	1	2	8	1	74.38	.016	5	1	.15	2	.01	2	.01	.31	.01	6	.01	.001	
8700	1	382	12	1471	1.3	55	7	941	2.01	9	5	ND	1	74	4	2	3	49	25.38	.179	24	24	.61	4	.01	2	.79	.03	.01	1	.04	.001	
8701	1	226	104	1131	.1	28	5	519	2.67	83	5	ND	1	11	7	2	2	28	1.30	.031	7	6	.75	1	.01	2	.10	.01	.01	1	.01	.001	
8702	1	145	55	724	.3	28	5	588	2.77	47	5	ND	1	15	3	2	2	29	1.67	.043	5	14	.87	1	.01	2	.12	.01	.01	1	.01	.001	
8703	1	205	101	1253	1.1	36	6	870	3.90	110	5	ND	1	29	8	2	2	35	3.62	.083	8	12	1.21	3	.01	2	.22	.03	.02	1	.03	.001	
8704	1	457	110	1873	4.1	48	13	890	4.04	186	5	ND	1	35	9	2	2	341	4.47	.172	11	15	1.28	3	.01	2	.33	.04	.01	1	.13	.001	
8705	2	891	48	2512	5.4	82	16	842	5.16	116	5	ND	1	35	10	2	2	320	3.63	.180	14	21	1.19	3	.01	2	.45	.04	.01	1	.19	.001	
8706	3	559	78	1442	5.0	53	12	572	3.55	149	5	ND	1	27	7	2	2	139	3.85	.191	9	12	.81	4	.01	2	.27	.03	.03	1	.14	.001	
8723	1	1926	100	9216	2.7	156	188	4377	20.30	63	5	ND	2	11	27	2	2	359	.88	.166	32	40	.89	9	.01	2	1.92	.01	.01	1	.07	.031	
8724	1	305	255	1476	1.5	80	36	1028	8.70	87	5	ND	1	14	7	2	2	131	.47	.158	29	17	1.14	55	.02	12	3.43	.02	.19	1	.06	.001	
8725	1	59	29	544	.7	15	10	566	2.06	18	5	ND	1	4	6	2	2	24	.37	.012	2	5	.27	2	.01	2	.13	.01	.01	1	.01	.001	
8726	1	90	30	370	.1	9	7	477	1.22	44	5	ND	1	2	8	2	2	17	.11	.003	2	6	.13	44	.01	2	.13	.01	.01	1	.01	.001	
8727	1	37	22	415	.1	10	3	830	1.15	2	5	ND	1	9	6	2	2	16	.87	.003	2	7	.46	4	.01	2	.14	.01	.01	1	.01	.001	
8728	1	204	33	917	1.0	8	8	1425	3.23	1977	5	ND	3	49	4	16	2	42	1.55	.155	16	5	1.30	62	.01	8	1.95	.05	.12	1	.02	.001	
8729	5	245	30	1037	.8	3	7	1022	4.20	2199	5	ND	2	73	8	2	2	39	10.04	.115	9	4	1.01	62	.01	6	1.54	.11	.08	1	.06	.001	
8730	1	355	154	3897	2.5	289	21	1445	9.07	50	5	ND	2	7	4	2	2	269	.33	.130	89	57	1.72	91	.01	4	2.78	.02	.02	1	.10	.002	
8731	1	45	26	1016	.6	24	3	690	1.15	25	5	ND	1	15	2	2	2	19	1.81	.039	9	3	.47	9	.01	3	.15	.01	.02	1	.02	.001	
8732	1	41	17	478	.4	26	3	526	.91	10	5	ND	1	12	1	2	2	18	1.32	.012	15	8	.41	11	.01	3	.15	.01	.03	1	.05	.001	
8733	1	45	17	487	.3	31	4	472	1.05	19	5	ND	1	14	1	2	2	22	1.40	.005	9	10	.64	3	.01	2	.30	.01	.01	1	.01	.001	
8734	2	79	21	757	.9	28	5	908	2.23	35	5	ND	1	7	4	2	2	26	.53	.005	10	11	.59	11	.01	2	.72	.01	.01	1	.05	.001	
8748	2	672	104	2625	1.3	9	21	1484	27.52	59	5	ND	3	56	8	2	2	121	2.52	.038	9	1	.65	11	.01	2	.10	.02	.01	160	.04	.001	
8749	1	830	22	2680	1.9	21	28	2047	7.27	7	5	ND	2	95	10	2	2	90	6.19	.042	12	13	1.35	2	.01	2	.09	.05	.01	2	.04	.001	
8755	1	562	724	874	1.7	17	7	834	4.91	8	5	ND	1	3	5	2	3	30	.15	.009	2	7	.28	2	.01	3	.08	.01	.01	1	.05	.001	
8756	1	1292	412	2286	2.1	21	8	841	5.07	271	5	ND	1	10	32	8	2	57	.91	.023	25	10	.44	4	.01	3	.12	.01	.01	1	.13	.001	
8757	9	1404	615	1371	.6	22	6	657	2.57	320	5	ND	1	10	13	9	2	50	.81	.025	16	10	.29	9	.01	2	.08	.01	.01	1	.03	.001	
8758	3	1065	103	482	2.9	26	9	789	1.89	48	5	ND	1	23	3	2	2	58	3.14	.037	11	9	.83	2	.01	2	.14	.02	.01	1	.10	.001	
8759	2	763	47	409	1.7	19	4	576	1.82	44	5	ND	1	15	2	2	2	56	1.64	.045	12	8	.60	2	.01	3	.07	.01	.01	1	.08	.001	
8760	1	188	43	497	.3	31	3	756	2.59	3	5	ND	1	15	2	2	2	40	1.54	.073	16	11	.81	2	.01	2	.15	.01	.01	1	.01	.001	
8761	1	299	29	280	.5	34	3	626	2.13	12	5	ND	1	17	1	2	2	52	1.54	.101	9	10	.82	2	.01	2	.13	.01	.01	1	.04	.001	
STD C	20	59	40	142	7.0	71	29	1047	3.94	42	17	7	35	49	18	18	19	66	.47	.105	37	60	.83	185	.09	34	1.72	.07	.13	13	-	-	

CANAMIN RESOURCES FILE # 87-1704A

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	RI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AG11 OZ/T	AUX1 OZ/T
8762	2	1500	42	1427	4.2	75	14	875	3.67	37	5	ND	1	21	5	2	2	200	2.28	.204	21	27	1.25	4	.01	2	.63	.02	.01	1	.13	.001
8763	1	224	29	947	1.4	30	4	676	1.92	31	5	ND	2	39	6	2	2	37	19.51	.071	9	7	.82	3	.01	2	.99	.07	.01	1	.03	.001
8764	1	1703	25	2073	7.8	22	10	1063	5.21	4	5	ND	1	24	11	2	2	87	2.44	.103	14	14	.75	2	.01	2	.21	.02	.01	1	.19	.001
8765	1	31	28	285	1.0	13	3	991	2.35	118	5	ND	2	147	2	2	2	10	47.70	.030	7	5	.73	4	.01	2	.04	.06	.01	3	.03	.001
8766	1	581	750	799	1.8	20	5	464	3.30	7	5	ND	1	9	5	2	3	42	.71	.012	18	11	.30	1	.01	2	.07	.01	.02	1	.06	.001
8767	1	419	46	2496	1.6	41	19	1410	4.76	12	5	ND	1	26	23	2	2	95	2.53	.039	16	13	.94	1	.01	2	.19	.02	.01	1	.03	.001
8768	1	429	207	7757	.7	39	19	3300	8.00	69	5	ND	3	244	48	4	2	360	10.59	.079	14	15	2.02	4	.01	2	.12	.07	.01	1	.01	.001
8769	1	140	99	849	.1	31	5	789	1.96	13	5	ND	1	26	4	2	2	43	2.32	.043	9	9	.91	1	.01	2	.10	.02	.01	1	.02	.001
8770	1	180	36	889	.7	33	4	891	1.67	4	7	ND	1	24	3	2	2	56	3.25	.097	13	11	1.12	1	.01	2	.12	.03	.02	1	.01	.001
8771	1	144	30	991	1.0	29	5	689	2.37	16	5	ND	2	86	4	2	2	32	25.46	.097	12	8	.75	3	.01	2	.12	.04	.01	1	.01	.001
8772	1	238	36	1304	3.6	50	10	1048	4.35	62	5	ND	2	71	5	2	2	50	14.79	.114	9	15	1.45	3	.01	2	.20	.07	.01	1	.11	.001
8773	1	9	9	47	.5	6	1	335	.58	19	6	ND	1	111	1	2	3	24	23.65	.049	9	7	.52	2	.01	2	.19	.04	.02	2	.01	.001
8774	2	1226	363	2330	5.6	57	131	4354	34.07	128	5	ND	3	27	8	2	80	834	1.40	.309	18	124	.84	19	.01	2	3.25	.01	.02	1	.14	.099
8775	1	1299	223	3463	3.9	177	26	1575	6.61	18	5	ND	1	6	3	2	2	294	.60	.143	31	49	3.00	13	.01	2	2.69	.01	.02	1	.12	.005
8776	1	192	11	1695	1.1	70	4	817	1.40	12	5	ND	1	17	3	2	2	38	3.02	.115	23	14	.75	4	.01	2	.19	.02	.01	1	.04	.001
8777	1	64	8	301	.9	24	2	795	1.02	4	5	ND	1	15	1	2	2	19	2.46	.027	34	7	.86	2	.01	2	.11	.01	.01	1	.02	.001
8778	1	69	3	221	.5	19	2	461	.98	6	5	ND	1	9	1	2	2	21	.97	.021	33	9	.38	3	.01	2	.17	.01	.01	1	.02	.001
8779	1	273	23	2731	2.1	32	10	1543	3.93	21	5	ND	3	49	4	2	2	92	15.53	.165	32	22	1.84	36	.01	3	2.33	.07	.04	1	.07	.001
8780	1	279	34	1582	.2	44	15	782	25.76	27	5	ND	3	12	1	2	2	308	.47	.061	12	103	.72	69	.01	11	5.75	.01	.03	1	.01	.001
8781	6	2787	76	5285	6.8	42	47	2193	36.49	51	5	16	3	21	12	2	7	421	.95	.153	17	54	.70	20	.01	2	1.93	.01	.02	5	.11	.231
8782	1	651	49	1626	2.2	39	7	824	5.49	16	5	ND	1	7	10	2	2	163	.92	.134	28	27	.47	18	.01	2	.67	.01	.01	1	.08	.025
8783	1	91	59	527	1.1	21	3	1392	1.41	17	5	ND	3	71	2	2	2	34	18.56	.061	17	10	.52	7	.01	2	.18	.06	.01	1	.01	.001
8784	1	108	42	832	.8	59	6	562	1.80	14	5	ND	1	16	2	2	2	52	2.00	.092	11	11	.53	10	.01	2	.13	.01	.01	1	.03	.001
8785	1	163	26	1542	1.5	82	7	747	2.55	25	5	ND	1	17	4	2	2	58	1.58	.072	10	15	.91	2	.01	2	.14	.01	.01	1	.03	.001
8786	2	198	50	1467	2.6	57	8	803	2.34	24	5	ND	1	28	8	2	2	51	5.12	.199	16	16	.94	3	.01	2	.18	.04	.01	1	.07	.001
8787	1	90	22	767	1.8	36	5	1250	1.42	14	5	ND	3	60	3	2	2	29	18.11	.136	19	9	1.10	3	.01	2	.23	.06	.01	1	.05	.002
8788	3	158	30	1210	1.4	46	7	552	1.78	24	5	ND	1	27	5	2	2	40	5.88	.196	22	20	1.04	3	.01	2	.90	.05	.01	1	.03	.004
8789	1	1542	7	5346	9.1	64	25	2130	11.54	4	5	ND	1	4	41	2	2	153	.41	.036	15	24	.58	4	.01	3	.15	.01	.02	1	.28	.001
8790	2	1787	170	2946	7.4	71	14	2548	4.86	112	5	ND	1	13	74	2	2	87	3.59	.286	52	19	.55	14	.01	2	.91	.03	.01	1	.20	.002
STD C	20	57	38	138	6.9	71	29	1028	3.95	43	15	7	34	48	18	15	21	65	.47	.102	37	63	.84	181	.09	38	1.72	.07	.14	13	-	-

GEOCHEMICAL/ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: Core AG# BY FIRE ASSAY. AU# BY FIRE ASSAY

DATE RECEIVED: JUNE 15 1987 DATE REPORT MAILED: June 17/87 ASSAYER: D. Toye DEAN TOYE, CERTIFIED B.C. ASSAYER

CANAMIN RESOURCES File # 87-1785

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CP	MG	BA	TI	B	AL	NA	K	W	AG#	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	OZ/T	OZ/T
8750	2	354	86	343	3.4	1	4	3574	2.50	248	5	ND	1	127	3	2	11	2	34.08	.021	6	2	.28	4	.01	2	.07	.01	.01	1	.15	.012
8791	8	450	47	231	3.2	310	116	700	15.77	2339	5	ND	1	53	2	2	36	433	5.14	.454	25	18	.84	17	.01	3	2.52	.02	.01	4	.13	.013
8792	1	300	52	348	1.3	45	12	1338	30.01	761	5	ND	2	48	6	2	30	443	4.14	.259	9	6	.30	12	.01	2	.43	.01	.02	72	.06	.016
8793	55	229	165	102	2.3	11	12	965	28.20	150	5	ND	3	43	3	2	248	250	5.71	.244	5	2	.16	8	.03	2	.16	.01	.02	35	.09	.046
8794	15	121	114	150	3.2	37	16	1482	29.37	852	5	ND	2	26	3	2	56	409	2.44	.117	4	5	.35	8	.04	2	.37	.01	.02	23	.12	.010
8795	3	230	22	251	1.2	65	19	2613	29.43	245	5	ND	2	21	5	2	126	478	1.74	.177	7	7	.45	10	.04	2	.66	.01	.03	25	.05	.011
8796	8	222	59	262	2.2	12	12	791	30.31	89	5	ND	1	17	5	4	1058	290	1.41	.164	4	3	.24	12	.03	6	.25	.01	.02	79	.07	.089
8797	21	449	147	312	4.8	33	17	985	26.86	164	5	2	2	34	6	2	2627	332	3.58	.214	14	4	.25	6	.03	6	.29	.01	.02	76	.16	.088
8798	1	1466	78	456	15.7	90	28	2484	25.50	269	5	4	2	49	7	2	1264	477	3.74	.187	21	4	.42	93	.02	3	.43	.02	.03	65	.65	.249
8799	1	996	90	908	14.7	70	31	3105	29.62	214	5	ND	2	21	12	2	918	332	1.76	.172	13	4	.45	44	.01	2	.45	.02	.05	78	.55	.045
8800	1	977	300	1079	13.5	74	27	1593	23.98	290	5	ND	2	34	14	2	1114	371	3.26	.169	13	5	.26	16	.01	3	.21	.01	.02	77	.50	.051
8801	1	2153	33	979	13.5	186	101	6260	27.93	682	5	ND	2	38	8	2	30	937	3.34	.148	7	2	.64	14	.01	33	.40	.02	.02	40	.51	.005
8802	1	981	38	848	12.5	242	93	3173	24.51	753	5	ND	3	60	11	2	36	758	7.64	.090	4	2	.49	43	.01	38	.87	.03	.03	33	.46	.052
8805	1	752	31	502	1.7	29	16	1547	29.21	108	5	ND	2	64	6	2	23	553	3.91	.107	7	5	.21	10	.01	3	.21	.01	.02	61	.07	.068
8818	1	143	54	255	1.2	24	15	2222	27.56	96	5	ND	2	70	5	2	13	436	4.06	.130	4	42	.29	31	.06	4	.55	.02	.03	6	.03	.008
8819	3	301	27	374	1.4	10	11	3072	24.26	61	5	ND	2	78	7	2	146	433	5.49	.185	10	15	.21	14	.03	3	.24	.02	.03	4	.05	.015
8820	1	659	33	591	1.6	8	10	511	28.08	95	5	ND	1	26	6	4	202	565	1.96	.150	4	5	.11	12	.01	3	.18	.01	.02	32	.06	.022
8821	1	789	66	898	1.1	10	12	1486	34.71	163	5	ND	2	25	6	6	7	451	1.26	.136	5	9	.16	25	.02	28	.28	.02	.03	27	.05	.005
8822	1	813	63	1717	2.9	25	15	1403	34.98	104	5	ND	2	58	16	2	5	406	2.85	.124	14	12	.26	15	.01	7	.34	.03	.03	23	.12	.002
8827	1	2140	48	972	5.0	14	13	2263	20.53	479	5	ND	2	96	7	2	36	446	8.38	.105	14	8	.36	9	.01	4	.04	.02	.02	4	.17	.115
8834	2	4633	26	3045	1.6	49	44	1559	19.49	129	5	ND	2	57	28	2	7	108	8.63	.043	14	3	.85	6	.01	2	.22	.01	.08	9	.08	.001
8835	1	467	17	1548	3.0	63	31	2040	34.65	322	5	ND	2	29	5	3	3	245	.78	.118	11	4	.46	12	.01	41	.11	.03	.03	27	.11	.005
8836	1	293	24	1244	.9	20	29	2793	29.85	112	5	ND	2	13	7	2	6	175	1.06	.056	6	4	.55	6	.01	6	.01	.01	.03	9	.02	.001
8846	1	182	20	1070	.7	25	20	1368	32.31	47	5	ND	2	95	4	2	5	168	1.52	.091	8	4	.72	10	.01	3	.05	.01	.04	20	.01	.001
STD C	19	58	43	133	6.7	62	29	1007	3.93	43	18	8	33	48	16	17	23	61	.47	.100	36	57	.87	180	.08	35	1.72	.07	.14	14	-	-

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS, VANCOUVER B.C.
PH: (604) 253-3158 COMPUTER LINE: 251-1011

DATE RECEIVED JUNNE 5 1987

DATE REPORTS MAILED

June 24/87

ASSAY CERTIFICATE

SAMPLE TYPE : REJECT
AU BY FIRE ASSAY
ND=NONE DETECTED

ASSAYER *D. Toyer* DEAN TOYE . CERTIFIED B.C. ASSAYER

CANAMIN RESOURCES PROJECT VI FILE# 87-1456R

PAGE# 1

SAMPLE	Sample wt. gm	Au-100 oz/t	Native Au mg	Average oz/t
8542	580	1.680	ND	1.680
8543	520	.144	.02	.145
8548	520	.272	ND	.272
8550	510	.220	.02	.221
8552	470	.108	ND	.108
8557	530	.148	.02	.149
8564	250	.172	ND	.172
8567	500	.146	.03	.147
8573	170	.284	ND	.284
8574	580	.116	.01	.117
8575	620	.277	ND	.277
8577	550	.163	.02	.164
8578	540	.236	.01	.237
8580	580	.165	ND	.165
8581	600	.375	.03	.377
8589	560	.428	.06	.431
8619	480	.332	ND	.332
8620	520	.324	.02	.325
8625	490	.188	ND	.188
8652	450	1.084	ND	1.084
8656	570	.484	.02	.485

GEOCHEMICAL/ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Core AG** BY FIRE ASSAY. AU** BY FIRE ASSAY

DATE RECEIVED: JUN 18 1987

DATE REPORT MAILED: June 25/87

ASSAYER: *D. J. J.* DEAN TOYE, CERTIFIED B.C. ASSAYER

CANAMIN RESOURCES

File # 87-1867A

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SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AG**	AU**
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM	PPM	PPM
8803	21	131	33	190	2.9	114	13	1277	18.58	815	5	ND	2	36	2	2	17	431	1.81	.147	12	20	.82	22	.01	3	3.07	.02	.01	3	.12	.019
8804	1	180	36	250	1.9	26	10	2421	30.91	223	5	ND	2	67	3	2	2	1020	8.51	.139	12	7	.09	54	.02	50	.12	.01	.01	49	.12	.004
8806	1	150	2	178	.5	9	3	632	5.52	104	5	ND	1	137	2	2	2	81	35.91	.034	6	2	.22	4	.01	2	.98	.01	.01	16	.02	.020
8807	1	390	17	294	1.2	22	10	1008	9.40	345	5	ND	1	142	3	2	6	110	29.77	.062	13	4	.39	6	.01	2	.07	.01	.01	6	.04	.027
8808	1	225	7	373	.8	14	5	1371	12.38	36	5	ND	1	111	3	2	13	235	25.46	.070	8	5	.40	27	.01	2	.01	.01	.01	32	.06	.013
8809	1	30	2	60	.1	3	1	869	1.39	13	5	ND	1	151	1	2	2	25	40.14	.030	6	1	.20	2	.01	3	.01	.01	.01	1	.01	.001
8810	1	107	2	131	.4	1	2	2163	7.05	28	5	ND	1	119	1	2	2	39	32.51	.031	6	5	.30	2	.01	2	.01	.01	.01	1	.03	.002
8811	1	1617	30	368	2.3	4	12	4599	27.17	688	5	ND	1	40	4	2	6	357	7.17	.058	9	29	.47	2	.01	3	.01	.01	.01	4	.08	.052
8812	4	2779	106	349	8.2	2	16	4739	30.76	1779	5	ND	3	40	4	2	32	262	4.80	.050	12	22	.49	4	.01	4	.01	.01	.01	4	.32	.062
8813	22	1763	174	750	7.7	5	15	4801	31.00	8295	5	ND	4	29	6	8	9	92	3.22	.033	7	8	.43	3	.01	2	.01	.01	.02	4	.33	.022
8814	1	200	18	922	1.1	36	14	5536	24.27	157	5	ND	2	57	4	2	8	58	6.97	.149	17	12	.89	6	.01	2	.16	.01	.04	2	.09	.005
8815	17	120	9	850	2.1	88	12	3634	13.11	332	5	ND	1	66	3	2	5	36	10.05	.156	12	4	.64	6	.01	4	.27	.02	.07	2	.04	.009
8816	30	34	10	437	.9	3	5	3276	10.76	195	5	ND	1	99	2	2	2	20	22.98	.082	11	5	.45	4	.01	3	.01	.01	.01	2	.05	.004
8817	1	128	6	17	.1	1	1	2194	2.77	152	5	ND	1	145	1	2	2	1	37.52	.029	4	1	.24	4	.01	2	.01	.01	.01	1	.01	.001
8823	1	109	18	757	.8	17	8	1430	9.05	33	5	ND	1	123	6	2	2	61	26.76	.076	9	6	.22	5	.01	5	.08	.02	.01	1	.06	.001
8824	1	2706	114	1984	10.4	34	49	1873	15.97	496	5	ND	1	119	16	2	2	133	18.21	.241	17	10	.28	9	.01	9	.12	.03	.03	6	.40	.005
8825	1	4794	40	1275	8.0	29	43	3259	17.46	550	5	ND	1	135	9	2	2	173	18.42	.279	30	5	.25	56	.01	10	.10	.03	.02	5	.33	.049
8826	1	2033	36	732	6.6	19	19	3017	21.39	296	5	ND	1	127	5	2	25	274	12.73	.089	16	7	.22	71	.01	17	.05	.02	.02	1	.26	.030
8828	1	867	150	1175	1.3	50	13	2171	33.72	240	5	ND	3	122	15	2	2	743	7.43	.172	11	19	.26	28	.03	6	.33	.02	.03	60	.05	.002
8829	1	829	71	568	1.2	12	10	3364	29.83	102	5	ND	3	63	7	2	2	464	5.17	.108	4	9	.23	12	.01	5	.13	.01	.02	33	.11	.001
8830	1	1939	87	787	1.2	19	12	2603	25.15	231	5	ND	2	106	12	2	2	486	8.30	.142	16	18	.24	390	.01	9	.21	.01	.03	45	.08	.002
8831	1	1081	120	1266	2.1	51	14	639	28.04	84	5	ND	4	58	4	2	2	115	1.17	.058	8	10	.49	77	.01	29	4.45	.08	.03	5	.11	.004
8832	1	8101	242	1217	23.8	39	62	2600	24.65	226	5	ND	3	48	19	2	12	1329	5.55	.139	20	8	.30	16	.01	10	.29	.01	.04	12	.86	.003
8833	1	108	6	38	.1	1	1	1213	.55	5	5	ND	1	153	1	2	2	21	37.87	.016	4	1	.21	5	.01	2	.02	.01	.01	1	.02	.001
8837	1	599	29	1298	3.1	19	23	2232	29.37	1081	5	ND	4	20	6	2	9	222	1.89	.057	11	9	.70	5	.01	10	.03	.01	.02	8	.16	.002
8838	1	789	38	833	1.3	29	19	2848	27.05	90	5	ND	2	58	9	2	3	132	5.66	.062	15	8	.74	15	.01	2	.03	.01	.02	5	.07	.002
8839	1	61	7	552	.7	34	13	549	12.38	37	5	ND	2	33	15	2	3	117	1.89	.047	8	8	.83	14	.01	9	.24	.02	.03	3	.01	.004
8840	1	107	18	554	1.1	44	11	853	10.83	36	5	ND	2	34	2	2	5	160	3.36	.103	9	8	.79	8	.01	2	.14	.01	.01	3	.06	.002
8841	13	149	102	926	3.0	71	30	1005	28.50	589	5	ND	3	69	7	2	3	420	6.28	.106	14	14	.88	16	.01	11	.74	.01	.04	5	.11	.009
8842	1	218	37	1451	1.5	39	31	1944	31.05	164	6	ND	3	111	9	2	18	91	6.15	.045	10	8	.57	16	.01	30	.10	.01	.03	18	.07	.004
8843	1	116	27	1806	.6	25	25	1784	31.90	164	5	ND	2	62	7	2	2	161	6.01	.053	11	11	.30	9	.01	106	.10	.01	.01	21	.08	.006
8844	1	113	16	3664	2.2	40	28	1771	27.18	123	5	ND	3	87	26	2	2	160	7.62	.051	12	5	.46	6	.01	4	.04	.01	.06	9	.09	.007
8845	1	81	29	1406	2.1	16	15	1626	26.87	47	5	ND	2	114	7	2	4	147	8.19	.073	18	6	.57	8	.01	6	.02	.01	.04	9	.07	.001
8847	1	104	15	847	1.1	22	15	1309	19.79	42	5	ND	1	140	3	2	2	222	14.50	.064	8	4	.75	12	.01	6	.01	.01	.01	5	.05	.002
8848	1	244	14	1631	2.2	84	29	2760	9.85	31	5	ND	2	20	4	2	2	292	2.95	.157	24	10	.35	5	.01	2	.20	.01	.02	8	.06	.012
8849	1	73	34	1905	2.0	107	33	2458	22.16	81	5	ND	2	42	5	2	2	327	6.76	.165	14	1	.32	6	.01	2	.02	.01	.01	236	.05	.037
STD C	19	60	36	138	7.0	72	28	1022	3.87	43	17	8	34	48	17	17	22	63	.45	.104	36	58	.85	181	.08	39	1.72	.07	.14	12	-	-

CANAMIN RESOURCES FILE # 87-1867A

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SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	B1	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	ASLT	AUTZ
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	GT/T	GT/T
8850	1	22	15	538	.1	34	14	714	11.58	60	5	ND	3	14	2	2	191	2.90	.058	4	5	.09	3	.01	2	.01	.01	.01	142	.02	.001	
8851	1	74	9	308	.4	12	4	1061	1.92	20	5	ND	1	101	3	2	38	29.65	.038	5	3	.11	4	.01	2	.01	.01	.01	3	.02	.005	
8852	16	3577	44	26479	6.4	59	41	5420	24.98	121	5	ND	3	14	308	2	5	429	1.33	.102	10	16	.49	11	.01	2	.02	.01	.02	1	.21	.007
8853	1	1460	71	7807	4.4	68	56	2336	34.39	275	5	ND	3	22	55	2	11	1380	2.14	.108	13	8	.59	19	.01	2	.20	.01	.02	202	.20	.014
8854	1	749	35	1320	6.7	81	33	4085	22.21	322	5	ND	1	65	11	2	5	264	11.95	.095	19	5	.86	19	.01	15	.48	.04	.01	1	.24	.002
8855	3	2314	38	6243	5.8	60	54	1015	28.54	53	5	ND	3	29	38	2	2	180	1.00	.050	19	3	1.42	8	.01	4	.63	.01	.04	1	.21	.001
8856	1	1204	24	2128	3.8	98	78	6223	23.68	49	5	ND	3	38	6	2	2	372	4.13	.061	12	6	1.68	4	.01	2	.17	.01	.02	25	.15	.001
8857	1	657	10	1996	2.2	56	67	2701	13.79	47	5	ND	2	23	12	2	3	276	2.30	.052	9	6	1.12	3	.01	2	.14	.01	.01	2	.08	.001
8858	1	106	117	338	.1	103	59	1403	12.85	22	5	ND	2	39	1	2	2	228	1.07	.087	20	110	1.15	201	.05	18	2.88	.02	.39	1	.01	.001
8859	1	105	47	709	.7	52	25	695	3.76	7	5	ND	2	15	1	2	3	158	.36	.030	14	27	.66	137	.01	6	1.65	.01	.31	1	.01	.001
8860	1	135	254	1738	1.9	196	46	815	10.81	7	5	ND	2	16	1	2	4	228	.36	.072	26	32	1.18	253	.03	13	3.41	.01	.45	1	.10	.001
8861	1	264	46	3965	2.4	154	23	2063	7.00	20	5	ND	2	25	30	2	4	1023	3.82	.360	38	19	.30	24	.02	2	.30	.01	.04	1	.05	.002
8862	1	447	34	2277	5.5	146	27	2707	13.02	23	5	ND	1	50	7	2	3	548	10.40	.250	30	10	.39	11	.01	2	.24	.01	.01	3	.15	.005
8863	1	24	33	174	.3	5	1	978	.38	2	5	ND	1	147	1	2	2	14	36.95	.023	5	1	.19	5	.01	2	.01	.01	.01	1	.01	.001
8864	1	689	768	766	12.2	8	21	1397	20.18	11917	5	ND	1	41	6	2	7	19	10.08	.012	3	6	.95	5	.01	7	.10	.01	.01	1	.42	.005
8865	4	370	36	2805	1.0	55	21	2612	33.27	4743	5	ND	4	79	12	2	7	486	4.68	.127	32	6	.77	52	.01	140	.21	.07	.03	1	.05	.003
8866	1	372	42	5147	1.1	44	66	2774	26.44	56	5	ND	3	13	41	2	4	388	.75	.115	20	26	.72	10	.01	3	.99	.01	.07	1	.01	.001
8867	1	967	110	5135	2.9	21	86	2340	38.82	55	5	ND	3	13	16	2	5	661	.75	.164	12	11	.30	7	.01	2	.39	.01	.02	6	.12	.003
8868	1	2396	87	4853	5.1	20	42	2345	43.21	72	5	ND	5	16	13	4	62	771	.63	.097	8	16	.32	16	.01	2	.61	.01	.03	27	.11	.001
8869	2	800	47	6084	1.5	27	54	3658	33.67	58	5	ND	3	26	12	2	17	387	1.64	.081	11	16	.42	6	.01	2	.30	.01	.01	4	.02	.001
8870	2	1386	66	4425	2.7	21	31	3011	34.96	57	5	ND	5	18	5	2	42	480	1.50	.099	8	25	.37	7	.01	2	.26	.01	.03	23	.07	.039
8871	1	1619	50	5209	3.2	28	37	3312	33.18	46	5	ND	5	18	6	2	29	382	1.35	.097	10	19	.59	3	.01	2	.32	.01	.03	1	.10	.025
8872	1	1626	47	5473	4.2	26	45	3472	35.84	53	5	ND	4	13	7	2	89	462	.96	.109	7	22	.66	5	.01	2	.31	.01	.03	10	.14	.017
8873	1	2392	72	4634	7.6	21	67	3026	36.11	64	5	17	4	18	7	2	65	554	1.46	.114	8	36	.73	7	.02	2	.27	.01	.02	35	.21	.040
8874	3	3334	48	4340	49.3	26	39	2566	29.21	40	5	16	4	57	9	2	238	329	3.44	.107	12	13	.96	5	.01	2	.38	.01	.02	52	1.52	.888
8875	1	5538	26	2296	12.9	31	10	1361	5.92	13	5	ND	1	75	18	2	3	56	7.57	.062	12	13	1.24	4	.01	2	.28	.01	.01	1	.38	.007
8876	1	858	54	4426	8.1	41	54	4125	35.24	25	5	ND	3	12	8	2	7	252	.98	.141	17	35	.63	12	.01	2	.60	.01	.01	1	.24	.023
8877	2	1233	43	5393	5.3	47	47	1496	31.30	17	5	ND	2	12	5	2	13	211	.91	.157	176	19	.66	17	.01	2	.58	.01	.02	1	.17	.009
8878	1	985	65	3087	4.3	25	32	5303	34.44	59	5	ND	3	14	5	2	18	774	.47	.153	19	29	.16	112	.01	2	.40	.01	.02	36	.14	.002
8879	1	1129	47	4403	5.4	27	42	4699	35.75	31	5	ND	3	11	7	2	15	431	.82	.149	23	56	.43	161	.01	2	.54	.01	.02	1	.14	.009
8880	1	3941	64	1853	8.0	11	19	4477	31.74	58	5	ND	3	6	4	2	12	934	.55	.218	15	59	.15	115	.02	2	.30	.01	.02	19	.22	.028
8881	1	2048	93	1671	8.6	15	22	2386	34.75	82	5	ND	3	4	2	7	8	420	.43	.155	6	40	.17	62	.03	2	.34	.01	.02	36	.21	.005
8882	2	755	93	1283	7.8	17	23	2883	35.95	84	5	ND	4	5	2	2	13	301	.53	.113	9	48	.22	47	.05	2	.43	.01	.02	24	.25	.001
8883	1	1673	114	1524	2.7	20	31	2907	38.78	83	5	ND	3	6	3	2	48	401	.56	.094	8	52	.27	64	.08	2	.50	.01	.02	19	.08	.005
8884	1	3807	128	1401	14.9	17	40	4857	38.18	86	5	ND	4	8	3	2	49	549	.76	.142	11	43	.33	32	.08	2	.53	.01	.02	38	.41	.020
8885	1	904	155	1828	17.8	16	50	1957	36.72	93	5	3	4	10	5	2	107	510	.81	.180	10	52	.37	35	.12	2	.52	.01	.03	39	.57	.192
STD C	19	62	40	137	6.6	69	28	1014	3.79	44	17	8	33	47	17	17	22	63	.46	.099	35	58	.84	180	.08	38	1.74	.07	.13	13	-	-

CANAMIN RESOURCES FILE # 87-1867A

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SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AS#	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	PPM	%	%	%	PPM	OZ/T	OZ/T
8886	1	753	66	2877	30.4	27	74	5914	24.04	43	5	5	3	9	6	2	70	221	1.02	.124	6	26	.66	13	.01	2	.14	.01	.02	1	.94	.292
8887	1	2838	67	2394	47.7	30	51	5894	22.32	16	5	3	2	10	6	2	149	207	1.07	.119	9	28	.67	11	.01	4	.10	.01	.01	1	1.49	.198
8888	1	1090	169	2183	4.4	36	28	1590	9.75	107	5	ND	1	4	32	7	2	101	.33	.039	16	14	.41	4	.01	2	.08	.01	.01	1	.14	.009
8889	1	1123	142	1900	4.6	40	13	1290	6.13	236	5	ND	1	15	17	3	2	77	3.46	.199	17	11	.34	5	.01	2	.10	.01	.01	1	.16	.008
8890	2	456	394	1609	2.9	34	13	1879	5.41	316	5	ND	1	29	14	2	2	37	10.13	.170	16	9	.14	16	.01	2	.06	.01	.01	1	.11	.002
8891	1	19	9	122	.1	3	1	644	.60	52	5	ND	1	82	1	2	2	3	27.75	.023	9	1	.10	4	.01	2	.01	.01	.01	1	.02	.001
8892	1	25	9	107	.1	1	1	748	.68	79	5	ND	1	102	2	2	2	35.21	.010	.010	10	1	.07	5	.01	2	.01	.01	.01	1	.02	.001
8893	1	53	10	95	.5	2	1	522	.86	114	5	ND	1	85	1	2	2	4	34.00	.012	8	1	.07	5	.01	2	.01	.01	.01	1	.03	.003
8894	1	19	802	1911	.9	1	1	606	.34	25	5	ND	1	56	9	2	2	1	26.13	.015	5	1	.05	1	.01	2	.01	.01	.01	1	.05	.001
8895	4	25	3119	4331	4.4	1	1	1943	.64	139	5	ND	1	81	20	2	2	1	33.79	.015	8	1	.09	3	.01	2	.01	.01	.01	1	.19	.001
87-VR-1	1	7	22	274	.1	2	2	290	.25	7	5	ND	1	17	1	2	2	2	15.97	.007	2	1	.77	1	.01	127	.03	.01	.01	1	.01	.001
87-VR-2	1	127	28	226	.8	32	19	611	3.48	33	5	ND	1	9	5	2	2	26	.38	.161	12	1	.73	67	.01	5	1.16	.02	.06	1	.02	.001
87-VR-3	1	391	16	58	1.0	16	21	1018	6.01	7	5	ND	3	9	1	2	16	63	.39	.038	9	14	.04	113	.01	2	.40	.01	.03	1	.05	.001
87-VR-4	1	910	15	101	.5	59	46	818	9.93	8	5	ND	1	9	1	2	2	65	.32	.051	2	32	1.24	22	.01	6	2.08	.04	.04	1	.04	.002
87-VR-5	3	63119	1659	305	231.3	5	45	280	6.99	417	5	ND	5	3	3	38	3398	105	.18	.082	3	2	.16	18	.01	8	.40	.01	.09	1	8.24	.058
87-VR-6	1	38	2	399	.1	2	4	44	.14	4	5	ND	1	16	1	2	2	1	2.31	.012	2	1	.07	1	.01	670	.05	.01	.01	1	.01	.001
STD C	19	63	42	134	7.0	65	28	1024	3.96	42	19	9	34	49	17	15	22	63	.47	.103	36	60	.86	183	.09	37	1.73	.07	.14	12	-	-

✓ ASSAY REQUIRED FOR CORRECT RESULT -

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
2.89	4.57	Tuff Breccia.	91544	2.89	3.66	0.77			.003	.04	26.98		
(9.5	15.0)	- Mottled ^{cherty} green, local mafic clasts.	91545	3.66	4.57	0.91			.047	.23	30.58		
		- Traces pyrite & fine grained galena											
		- Core Recovery - 85%-90%											
		Highly broken 4.42-4.57 M											
4.57	4.88	* - Pyrite Zone.	8633	4.57	5.85	1.26			.007	.27	29.50		
(15.0	16.0)	- ± 80% Pyrite - Granular. Self-gouge											
		- Core Recovery + 80%											
4.88	5.85	Chert											
(16.0	19.2)	- Bluish-gray, brecciated, ± 10% Pyrite											
		- locally in steep fracture.											
		- Highly broken to 5.18.											
		- Core Recovery ~ 80%.											
5.85	10.36	Chert Breccia.	91546	5.85	6.85	1.0			.002	.07	10.92		
(19.2	34.0)	- Buff to green breccia. Py + Cp4.	91547	6.85	7.85	1.0			.004	.27	9.99		
		- 8.09-9.20 - limestone fragment	91548	7.85	8.85	1.0			.011	.23	9.60		
		- Possible intrusion (?).	91549	8.85	10.36	1.51			.010	.12	4.13		
		* Pyrite zone for sampling purposes is											
		taken to start at 4.57 M. Because of											
		highly broken and crushed nature the											
		zone may start lower, perhaps at 4.72 M.											
		T.E.L.											

CANAMIN RESOURCES LTD.

DIAMOND DRILL LOG

PROPERTY : VILLALTA HOLE No. : 87-V-12 CLAIM :

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____ SECTION : _____

DEPARTURE : _____ BEARING : _____

ELEVATION : _____ DIP : -90°DATE BEGUN : MAY 13/87 SHEET No : 1/2DATE FINISHED : MAY 14/87 LOGGED BY : T. LISLETOTAL DEPTH : 18.57 (61.0') DATE : MAY 19/87CORE SIZE : HQ

METERS

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
0	0.91	Surface Rubble.	8576	0	1.22	1.22			.010	.07	33.45		
(0	3.0')	Core Recovery = ±10%											
0.91	1.22	Tuff Breccia (weathered).											
(3.0'	4.0')	Green, minor limonite, trace Hematite.											
		- Core Recovery ~ 90%											
1.22	11.00	Hematite Zone.	8577	1.22	2.22	1.00			.152	.12	39.32		
(4.0	36.1')	Porous, pitted, Non-banded, locally limonite.	8578	2.22	3.22	1.00			.228	.23	38.41		
		Core Recovery 93% except at 1.22-1.83 = 50%	8579	3.22	4.22	1.00			.044	.18	38.28		
		- 1.22 - 5.00M - 50%-70% hematite + Tuff.	8580	4.22	5.22	1.00			.134	.44	33.51		
		- 5.00 - 9.75M - 25% hematite mainly as	8581	5.22	6.22	1.00			.376	.49	37.84		
		fragments, Commonly Red, locally black.	8582	6.22	7.22	1.00			.025	.19	35.44		
		in Tuff Breccia	8583	7.22	8.22	1.00			.096	.21	42.81		
		- 9.75 - 10.82 - 70% Hematite.	8584	8.22	9.22	1.00			.095	.10	40.40		
		- 10.82 - 11.00 - Hematitic Tuff Breccia.	8585	9.22	10.22	1.00			.001	.04	42.71		
			8586	10.22	11.00	0.78			.008	.74	37.30		

CANAMIN RESOURCES LTD.

DIAMOND DRILL LOG

PROPERTY : VILLALTA HOLE No. : 87-U-14 CLAIM : _____

HOLE SURVEY		
FOOTAGE	BEARINGS	DIP

COLLAR SURVEY :

LATITUDE : _____ SECTION : _____

DEPARTURE : _____ BEARING : _____

ELEVATION : _____ DIP : - 90°DATE BEGUN : MAY 14/87 SHEET No. : 1/2DATE FINISHED : MAY 15/87 LOGGED BY : T. LISLETOTAL DEPTH 13.41 (44.0') DATE : MAY 19/87CORE SIZE : HQ

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
0	1.83	RUBBLE - Dark green tuff. 10% C.R.	8595	0.0	1.82	1.82			.005	.17	18.98		
(0	6.0')		8596	1.82	2.13	0.31			.010	.31	16.46		
1.83	2.44	Tuff Breccia.											
(6.0'	8.0')	- layering locally at 40° - Green Fragments in pale green matrix. - Broken, limonitic - Core Recovery 80%	8528	2.13	3.13	1.00			.003	.18	15.81		
2.44	7.31	CHERT.											
(8.0'	24.0')	- Mottled, pale green to buff, limonitic. - Spongy limonitic ^{manganese} fragments. 0°-10° to C.A. - Upper contact with tuff steep. - Core Recovery = 83% - 3.9-4.78 Tuff. Friable, clay altered? local chert fragments	8529	3.13	4.13	1.00			.001	.13	8.19		
			8530	4.13	5.13	1.00			.003	.74	21.09		
			8531	5.13	6.13	1.00			.001	.27	11.68		
			8532	6.13	7.13	1.00			.001	.23	11.90		
			8533	7.13	8.13	1.00			.001	.05	2.86		

CANAMIN RESOURCES LTD.

DIAMOND DRILL LOG

PROPERTY : VILLOLTA HOLE No. : 87-U-15 CLAIM : _____

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____ SECTION : _____

DEPARTURE : _____ BEARING : _____

ELEVATION : _____ DIP : -90°DATE BEGUN : MAY 15 / 87 SHEET No. : 1/3DATE FINISHED : MAY 15 / 87 LOGGED BY : LJSLBTOTAL DEPTH : 15.54 (61.0') DATE : MAY / 87CORE SIZE : NQ.

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
C	1.52	CASING - Rubble.	8603	0.0	0.91	0.91			.040	.10	28.70		
(0	5.0')	- Mixed hematite and Tuff Breccia	8604	0.91	1.92	0.92			.038	.18	22.20		
		- (Probably did not core until ~ 3.0' or 4.0' feet) to L.											
1.52	3.05	TUFF BRECCIA.	8536.	1.83	3.05	1.22			.004	.16	16.07		
(5.0'	10.0')	- 1% small hematite clasts from 1.83 M.											
		- 15% chert clasts to 1.83											
		- Core Recovery = 75% to 1.83, then 90%											
3.05	8.47	HEMATITE ZONE	8597	3.05	4.05	1.00			.001	.14	37.97		
(10.0'	27.8')	- Core Recovery 95%	8598	4.05	5.05	1.00			.008	.11	37.73		
		- 3.05 - 4.88 M - 65% hematite, 35% Tuff Br, 5% chert.	8599	5.05	6.05	1.00			.001	.03	26.22		
		P.Hed., limonitic, manganeseous with trace Py.	8600	6.05	7.05	1.00			.001	.01	22.40		
		Mud (Red) seam @ 8.47 M.	8601	7.05	8.05	1.00			.001	.05	22.25		
			8602	8.05	8.47	0.42			.001	.06	16.08		

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
3.05	8.47	Cont. 4.88 to 8.47 - Approximately 30% chert. Crude banding at 60° to 80° - Tuffaceous at bottom.											
8.47	10.0	CHERT BRECCIA.	8537	8.47	10.00	1.53			.001	.33	10.91		
(27.8	32.8)	- Chert clasts in tuff matrix - Traces VFC sulphide? - Hematitic at bottom. - Core Recovery = 95%											
10.0	12.34	HEMATITE ZONE (As 305-847)	8605	10.00	11.00	1.00			.002	.03	25.28		
(32.8	40.5)	40% Hematite, 55% chert + minor tuff. Chert occurs as breccia fragments. - 45°-55° crude banding in cherty tuff @ 11.28M - Core Recovery = 95%	8606	11.00	12.34	1.34			.001	.03	18.05		
12.34	14.32	CHERT BRECCIA -	8538	12.34	13.34	1.00			.001	.09	8.86		
(20.5	47.0)	Buff. epidote green grading @ 13.2 M to dark green chlorite-rich breccia that includes volcanic fragments. - Minor Jasper @ 12.65M, traces of pyrite - Core Recovery = 90%	8539	13.34	14.32	0.98			.003	.08	5.48		

CANAMIN RESOURCES LTD. :

DIAMOND DRILL LOGPROPERTY : VILLALTA HOLE No. : 87-V-17 CLAIM : _____

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____ SECTION : _____

DEPARTURE : _____ BEARING : _____

ELEVATION : _____ DIP : -90°DATE BEGUN : May 16/87. SHEET No. : 1/2DATE FINISHED : May 16/87 LOGGED BY : LISLGTOTAL DEPTH : 10.97 (36.0') DATE : May 21/87.CORE SIZE : HQ

METRES

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
0	1.83	HEMATITE ZONE	8611	0.0	1.83	1.83			.007	.24	35.80		
(0	6.0')	- 20% hematite, locally as fragments in fuff breccia - Crude banding at 45° - 20% Core Recovery (Solid core) - (Hole likely started to core ~4.0') T.C.L.											
1.83	2.28	CHERT BRECCIA	8612	1.83	2.83	1.00			.003	.28	9.02		
(6.0'	7.5)	- CHERT FRAGMENTS (Silicified limestone) in mauve brown fuff. limonite. - Well defined bottom contact @ 40° - 100% Recovery = 100%											
2.28	5.18	CHERT	8613	2.83	3.83	1.00			.001	.01	3.19		
(7.5'	17.0')	- Gray, locally well fractured, brecciated, limonite.	8614	3.83	4.83	1.00			.001	.02	1.93		

CANAMIN RESOURCES LTD.

DIAMOND DRILL LOGPROPERTY : VILLALTA HOLE No. : 87-U-18 CLAIM :

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____

SECTION : _____

DEPARTURE : _____

BEARING : _____

ELEVATION : _____

DIP : -90°DATE BEGUN : May 17/87SHEET No. : 1/2DATE FINISHED : May 17/87LOGGED BY : T. LisleTOTAL DEPTH : 6.71 (22'0")DATE : MAY 22/87CORE SIZE : HQ

METRES. (FEET IN BRACKETS)

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	As 02/17	Ag 02/17	Fe %	Pb %	Zn %
FROM	TO												
0	3.50	HEMATITE ZONE	8617	0.0	0.61	0.61			.001	.03	27.15		
(0	11.5')	- Est. ±80% hematite - luggy and pitted.	8618	0.61	1.61	1.00			.017	1.34	31.78		
		- Red hematite to 2.13 then black	8619	1.61	2.61	1.00			.356	.16	25.83		
		- Bottom contact @ 40°	8620	2.61	3.54	0.93			.322	.17	23.89		
		- Core Recovery - 0 - 0.61 = +50% 0.61 - 1.83 = 87% 1.83 - 3.50M = 100%											
3.50	3.81	SILICEOUS, CHERTY ZONE.	8621	3.54	4.27	0.73			.009	.03	5.00		
(11.5'	12.5')	- Chloritic and limonitic.											
		- C.R. = ~95%											
3.81	5.03	LIMESTONE BRACCIÀ											
(12.5'	16.5')	- Bottom contact @ 70°	8622	4.27	5.03	0.76			.003	.01	2.21		
		- Section is limestone that has been fractured and altered by a) chlorite or b) Pale, epidote green quartz-rock breccia shungers.	8698	5.03	6.03	1.00			.001	.03	.29		
			8699	6.03	6.71	0.66			.001	.01	.14		

87-U-30 1/2

CANAMIN RESOURCES LTD.

DIAMOND DRILL LOG

PROPERTY : VILLALTA HOLE No. : 87-U-30 CLAIM : _____

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____ SECTION : _____
 DEPARTURE : _____ BEARING : _____
 ELEVATION : _____ DIP : -90°

DATE BEGUN : May 26 / 87

SHEET No. : 1/2

DATE FINISHED : May 26 / 87

LOGGED BY : T. LISCE

TOTAL DEPTH : 10.97 (36.0')

DATE : May 29 / 87

CORE SIZE : H.O.

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
0	2.74	OVERBURDEN											
10	9.01												
2.74	3.90	TOP BRECCIA											
9.01	12.81	- Fragments mainly pale siliceous limestone minor dark grey chert. Tuffaceous matrix green and altered (chlorite, epidote?) - Core Recovery = 95%	B655	2.74	3.90	1.16			.010	.10	10.10		
			B656	3.90	4.57	0.67			.490	.90	23.89		
3.90	5.24	HEMATITE ZONE											
12.81	17.21	- Well broken and pitted. Limestone clasts from 4.57 to 4.88 m. with local conch 70° bedding - Approximately 70% hematite - Core Recovery to 4.57 = 75% 4.57 to 4.88 = 100%; 4.88 to 5.24 = 50%	B657	4.57	5.24	0.67			.096	.66	24.09		
			B658	5.24	6.24	1.00			.001	.03	4.56		

CANAMIN RESOURCES LTD.

DIAMOND DRILL LOG

PROPERTY : VILLALTA.

HOLE No. : 87-U-32 CLAIM :

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____

SECTION : _____

DEPARTURE : _____

BEARING : _____

ELEVATION : _____

DIP : -90°

DATE BEGUN : May 27/87

SHEET No. : 1/72

DATE FINISHED : May 27/87

LOGGED BY T. LISLE

TOTAL DEPTH : 1554 (510')

DATE : May 31/87

CORE SIZE : HQ

METERS (FEET IN BRACKETS)

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
0'	2.13	OVERBURDEN											
(0'	7.0')												
2.13	2.99	Tuff Breccia	8707	2.13	2.96	0.83			.001	.04	18.15		
(7.0'	9.8')	- Dark green, 15% pale siliceous limestone clasts mainly at top.	8708	2.96	3.92	0.96			.228	.14	26.41		
		- Minor hematite at bottom.	8709	3.92	4.88	0.96			.006	.06	5.89		
		- Core Recovery = 90%	8710	4.88	5.88	1.00			.001	.08	2.92		
			8711	5.88	6.88	1.00			.001	.05	1.51		
			8712	6.88	7.88	1.00			.001	.02	1.49		
2.99	3.92	HEMATITE ZONE											
(9.8'	12.85')	- Approximately 70% red hematite in altered tuff breccia. Non-banded.											
		- Core Recovery = 95%	8713	7.88	9.37	1.49			.001	.03	1.35		
			8714	9.37	10.76	1.39			.001	.01	3.28		

87-V-33

CANAMIN RESOURCES LTD. :

DIAMOND DRILL LOG

PROPERTY : WILLALTA. HOLE No. : 87-V-33 CLAIM : _____

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____ SECTION : _____

DEPARTURE : _____ BEARING : _____

ELEVATION : _____ DIP : -90°

DATE BEGUN : Aug 27/87 SHEET No. : 1/3

DATE FINISHED : Aug 28/87 LOGGED BY : LISLIE

TOTAL DEPTH : 1707 (560') DATE : June 1/87

CORE SIZE : H.9

METRES (FEET IN BRACKETS)

FOOTAGE		DESCRIPTION	SAMPLE NO	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
0	1.83	OVERBURDEN.											
(0'	6.0')												
1.83	7.07	TUFF BRECCIA.	8723	3.93	4.72	0.79			.031	.07	20.30		
(6.0	23.2')	- Dark green, Non calcareous.											
		- 10% - 20% siliceified limestone clasts											
		- Local dark grey chert and green volcanic clasts also present.	8724	6.10	7.10	1.00			.001	.06	8.70		
		- Section locally resembles andesite.	8725	7.10	8.10	1.00			.001	.01	2.06		
		- 3.96 - 4.72m - Chloritic; minor hematite.	8726	8.10	9.10	1.00			.001	.01	1.22		
		- 6.10 - 7.07m - Strong chlorite section, pale green with pyrite.	8727	9.10	10.39	1.29			.001	.01	1.15		
		- Traces pyrite											
		- Core Recovery = 95%, Badly broken in places.	8728	12.17	13.17	1.00			.001	.02	3.23		
			8729	13.17	14.17	1.00			.001	.06	4.20		

CANAMIN RESOURCES LTD.

DIAMOND DRILL LOG

PROPERTY : _____ HOLE No. : 87-U-34 CLAIM : _____

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____ SECTION : _____

DEPARTURE : _____ BEARING : _____

ELEVATION : _____ DIP : - 90°DATE BEGUN : MAY 28, 1987 SHEET No. : 1/2DATE FINISHED : MAY 28, 1987 LOGGED BY : LISLETOTAL DEPTH : 1463 (480') DATE : JUNE 1, 1987CORE SIZE : HQ

METRES (FEET IN BRACKETS)

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV	SULPHIDES	AU OPT	AG OPT	Fe %		
FROM	TO												
0	1.83	SURFACE RUBBLE											
(0'	6.0')	(INCLUDES CONGLOMERATE & FELDSPAR PARTS)											
1.83	6.64	TUFF BRECCIA.											
6.0'	21.8'	- Dark green, as in 87-U-33 and includes black to dark green chloritic tuff clasts	8730	5.64	6.64	1.00			.002	.10	9.07		
		- 5.79 - 6.64 Pale green chloritic zone weathered with traces of pyrite.	8731	6.64	7.64	1.00			.001	.02	1.15		
		- Core Recovery = ± 95%	8732	7.64	8.64	1.00			.001	.05	.91		
6.64	10.67	CHERT.	8733	8.64	9.64	1.00			.001	.01	1.05		
(21.8	35.0')	- Pale grey, partly limonitic & luggy. - 9.4 - 10.67, Pale green chloritic chert with up to 1% disseminated pyrite.	8734	9.64	10.64	1.00			.001	.05	2.23		

CANAMIN RESOURCES LTD. :

DIAMOND DRILL LOGPROPERTY : VILLALTA HOLE No. : 87-V-39 CLAIM : _____

HOLE SURVEY		
FOOTAGE	BEARING	DIP

COLLAR SURVEY :

LATITUDE : _____

SECTION : _____

DEPARTURE : _____

BEARING : 135°

ELEVATION : _____

DIP : -87°DATE BEGUN : JUNE 1/87SHEET No : 1/2DATE FINISHED : JUNE 2/87LOGGED BY : T. LISLETOTAL DEPTH 15.54M (51.0')DATE : JUNE /87.CORE SIZE : HQ

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
0	1.22	Overburden.											
1.22	1.58	Robble. Mainly Feldspar porphyry.											
(4.0'	5.2')												
1.58	3.53	HEMATITE ZONE	8753	1.58	2.58	1.00			.081	.70	35.32		
(5.2	11.6')	- Mainly red hematite. Approx. 35%	8754	2.58	3.57	0.98			.039	.65	32.70		
		in grey-green fult breccia.	8755	3.57	4.57	1.00			.001	.05	4.91		
		- Section locally well banded @ 50° to 60°	8756	4.57	5.57	1.00			.001	.13	5.07		
		Steeper at bottom.	8757	5.57	6.57	1.00			.001	.03	2.57		
		- Bottom contact at 33°	8758	6.37	7.37	1.00			.001	.10	1.89		
		- Core Recovery = ± 95%	8759	7.37	8.37	1.00			.001	.08	1.82		
			8760	8.37	9.37	1.00			.001	.01	2.59		
			8761	9.37	10.37	1.00			.001	.04	2.13		
			8762	10.37	11.17	0.80			.001	.13	3.67		

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
38.40	41.45	TUFF											
(126-d)	(136-d)	- Hematized, non-calcareous. - Shale zone? well broken 40%-50% C.R.											
41.45	45.96	TUFF											
(136-d)	(150-d)	- Grading to Breccia with increase in chert (silicified limestone) content. - Host rock changes at 43.59 from a coarse grained volcanic sandstone with pink rhodonite? or hematite stained layers at 50' to a dark green fine grained chloritic tuff - Bottom contact area highly siliceous - Core Recovery = +80%	8803	44.96	45.96	1.00			.019	.12	18.58		
45.96	47.55	HEMATITE ZONE											
(150-d)	(156-d)	- Hematite occurs in dark green tuff breccia similar to 87-V-41 - Estimate ± 30% hematite - DK blue! Red. - Core Recovery = +95%	8804	45.96	46.96	1.00			.004	.12	30.91		
			8805	46.96	47.55	0.59			.068	.07	29.21		

FOOTAGE		DESCRIPTION	SAMPLE NO	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
30.42	30.55	- Boundary between conglomerate	8818	30.42	31.42	1.00			.008	.03	27.56		
99.8'	100.25	and hematite. limonite - Assumed correct.											
30.55	34.81	HEMATITE ZONE											
100.25	114.2	- 30.55 - 32.31, ~20% hematite in tuff breccia with limestone clasts.	8819	31.42	32.31	0.89			.015	.05	24.26		
			8820	32.31	33.31	1.00			.022	.06	28.08		
		- 32.31 - 34.20, ~70% black and red hematite Coarse banding at 75°.	8821	33.31	34.31	1.00			.005	.05	34.71		
		- 34.20 - 34.81 Approx 30% Red hematite with very strong 5 cm chloritic zone at 35° at 34.29 m. ; chloritic to bottom.	8822	34.31	34.81	0.50			.002	.12	34.98		
		- Core Recovery = 95%.											
34.81	40.08	LIMESTONE BRECCIA											
114.2	131.5	- Large irregular clasts of limestone in yellowish-green alteration zone with local strong concentrations of hematite. ^{with traces of chalcopryrite.} zones are apparently related to steep 0°-15° fracture system.	8823	34.81	35.81	1.00			.001	.06	9.05		
			8824	35.81	36.81	1.00			.005	.40	15.97		
			8825	36.81	37.81	1.00			.049	.33	17.46		
			8826	37.81	38.81	1.00			.030	.26	21.39		
		Bottom Contact chloritic at 20° - Core Recovery = 95%	8827	38.81	40.08	1.27			.115	.17	20.53		

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
		eg. 40.84 - 41.07. Lower contact irregular but clear @ 75-90° to CA.											
42.28	44.35	HAEMATITE ZONE overall 50-60% Haematite	8828	42.28	42.81	0.53			.002	.05	33.72		
(135.7 - 145.5)		locally very massive & banded @ 65° to CA.	8829	42.81	43.74	0.93			.001	.11	29.83		
		42.28 - 42.81 red haematite, 30-40% in matrix	8830	43.74	44.35	0.61			.002	.08	25.15		
		with clasts of Est frags upto 0.5" (unidentified)											
		with msc Galena? (<0.5%)											
		42.81 - 43.74 Massive grey specular haematite, very fine grained, locally magnetic (Pyrite?) 1-2%											
		Rare blebs of Pyrite <0.5%. Matrix filling of 4-5% calcite blebs. Local banding @ 45-60° to CA.											
		43.74 - 44.35 Haematite breccia with upto 1cm frags of reddish haem. in buffaceous matrix. Banding @ 45-55° to CA. 1-2% fine pyrite No pyrrhotite. Matrix haematitic. Total haematite 20-25%.											
44.35	45.17	chlorite - siliceous shear zone.	8831	44.35	45.17	0.82			.004	.11	28.04		
(145.5)		Intensely chloritized with cherty zones @	8832	45.17	45.55	0.38			.003	.86	24.65		
		44.65 - 44.81 + 44.96 - 45.17. Rest is 80-90% chlorite, intensely sheared with chalcopyrite smeared	8833	45.55	46.55	1.00			.001	.02	.55		

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV	SULPHIDES	Au OPT	Ag OPT	Fe %		
FROM	TO												
		@ 14.97-17.07 Conglomerate with rare haematite partings in matrix + minor alteration of selected clasts.											
		@ 21.84-22.23 Unconsolidated haematite mudstone band (cf hole 87-V-44 @ 29.16-31.24)											
		@ 24.84-29.46 Rare haematite all'n of matrix + selected clasts, possibly related to fractures.											
29.46	33.28	SANDSTONE - upper section highly altered + sheared.											
(26.67-109.28)		Heterolithic clasts < 0.1 cm, rarely upto 3cm clasts, clasts rounded. Banding @ 50° to ca. Pervasive chlorite all'n giving green colour.											
		29.46-29.87 Intensely silicified cherty section											
		29.87-30.14 Shear zone or highly altered mudstone, sericitic alteration.											
		30.14-33.28 Pervasive irregular chlorite all'n of matrix											
33.28	37.46	CONGLOMERATE: heterolithic but with predominance of angular cherty clasts (reluct. cross-bedded bit?) upto 3cm.											
(109.28-122.9)		36.54-37.46 Matrix pervasively altered to siderite + calcite. Lower contact @ 10° to ca.	8848	36.54	37.46	0.92			.012	.06	9.85		

FOOTAGE		DESCRIPTION	SAMPLE NO.	FROM	TO	WIDTH	RECOV.	SULPHIDES	Au	Ag	Fe		
FROM	TO								OPT	OPT	%		
		lower 0.6m. Possible banding @ 45° to CA.	8885	11.05	12.05	1.00			.192	.57	36.72		
			8886	12.05	12.89	0.84			.292	.94	24.04		
12.84	16.46	CHERT BRECCIA. clast supported breccia of angular cherty clasts.											
(42.3-54.0)		12.84-13.32 weathered breccia, clasts (2cm) len	8887	12.84	13.32	0.43			.198	1.49	22.32		
		cherty but not carbonate matrix fine disseminated	8888	13.32	14.32	1.00			.009	.14	9.75		
		kaenolite + white carbonate alteration noted	8889	14.32	15.64	1.32			.008	.16	6.13		
		at surface. Minor kaenolite clasts. silicification	8890	15.64	16.46	0.81			.002	.11	5.41		
		increases with depth. some evidence for banding @ 30° to CA. Fine disseminated sulphides throughout, 1-2% Pyrite ± 20.1% Galena.											
		15.64-16.46 Less intensely silicified. some clasts respond to HCl. 3-5% disseminated sulphides 2-3% Pyrite, minor Galena + possible minor barite.											
16.46	43.68	LIMESTONE: Crinoidal, massive light grey Lst.,	8891	16.46	17.46	1.00			.001	.02	.60		
(54.0-143.3)		locally well preserved crinoids especially in partially silicified sections + below 30.5m.	8892	17.46	18.46	1.00			.001	.02	.68		
		16.46-18.90 Lst. fractured with minor associated pyrite (1-2%) + limonitic staining. Partial silicification related to fracturing + in bands upto 30cm @ 45° to CA 16.25m (1cm), 28.96-29.14 21.47-21.87, 30.24(3cm), 30.75-30.88 etc.	8893	18.46	19.46	1.00			.003	.03	.86		

I, Stephen Paul Quin, of #207 - 1455 Robson Street, Vancouver, British Columbia, do certify that:

I am a geologist with Southern Gold Resources Ltd. and have practised my profession for the past 6 years.

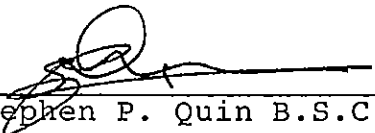
I am a member in good standing of the Canadian Institute of Mining and Metallurgy.

I supervised the drill program described in this report on the Villalta Property, Nanaimo Mining Division, between 10 June and 18 June, 1987.

I prepared the drill logs of drill holes 87-V-44 to 87-V-48 that accompany this report.

I am a director and shareholder of Southern Gold Resources Ltd. Which owns approximately 25% of the issued capital of CanaMin Resources Ltd. and that I am a director and shareholder of CanaMin Resources Ltd.

Dated this 25 day of June 1987


Stephen P. Quin B.S.C.

T.E. LISLE & ASSOCIATES LTD.
GEOLOGICAL SERVICES

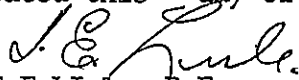
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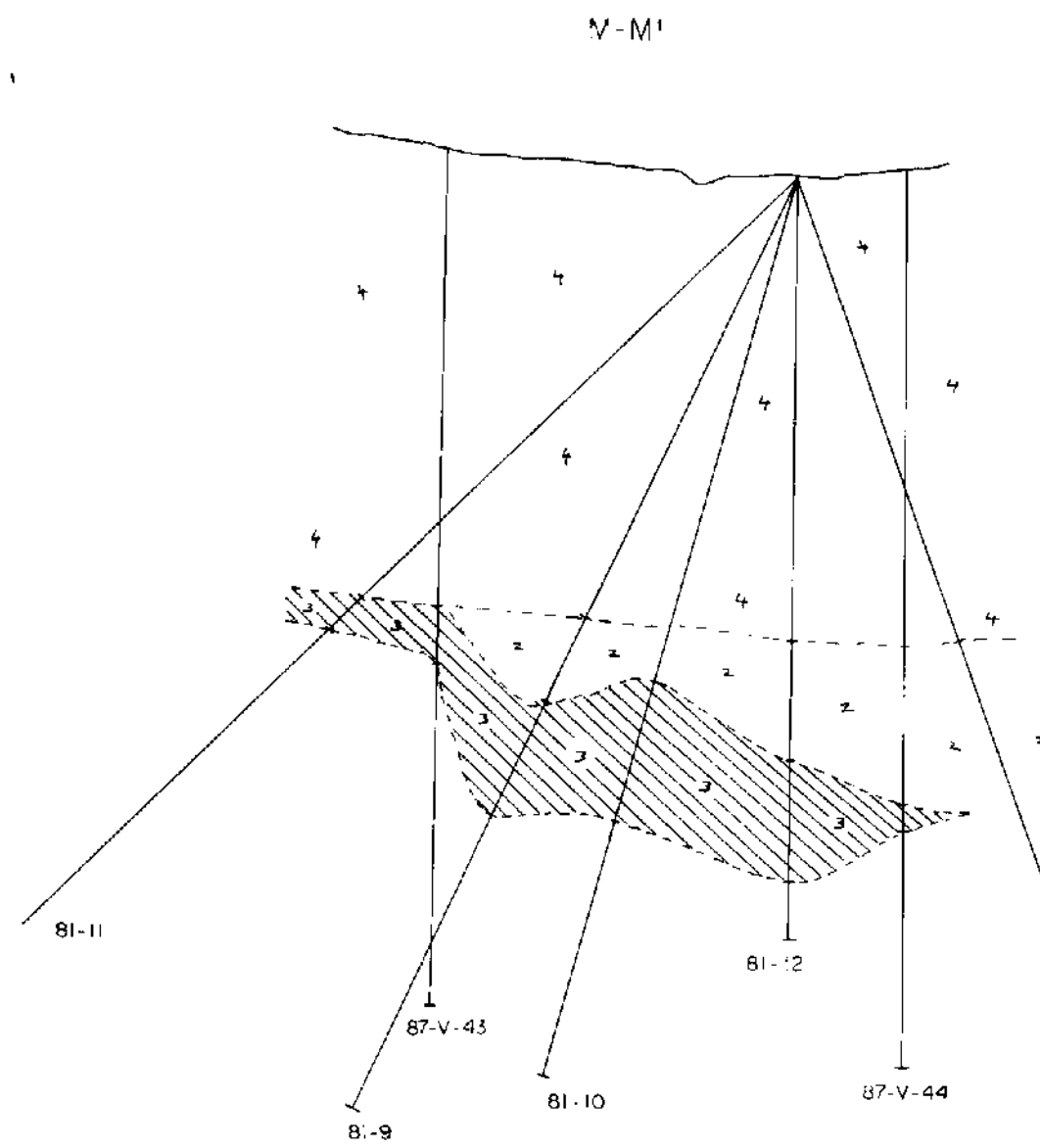
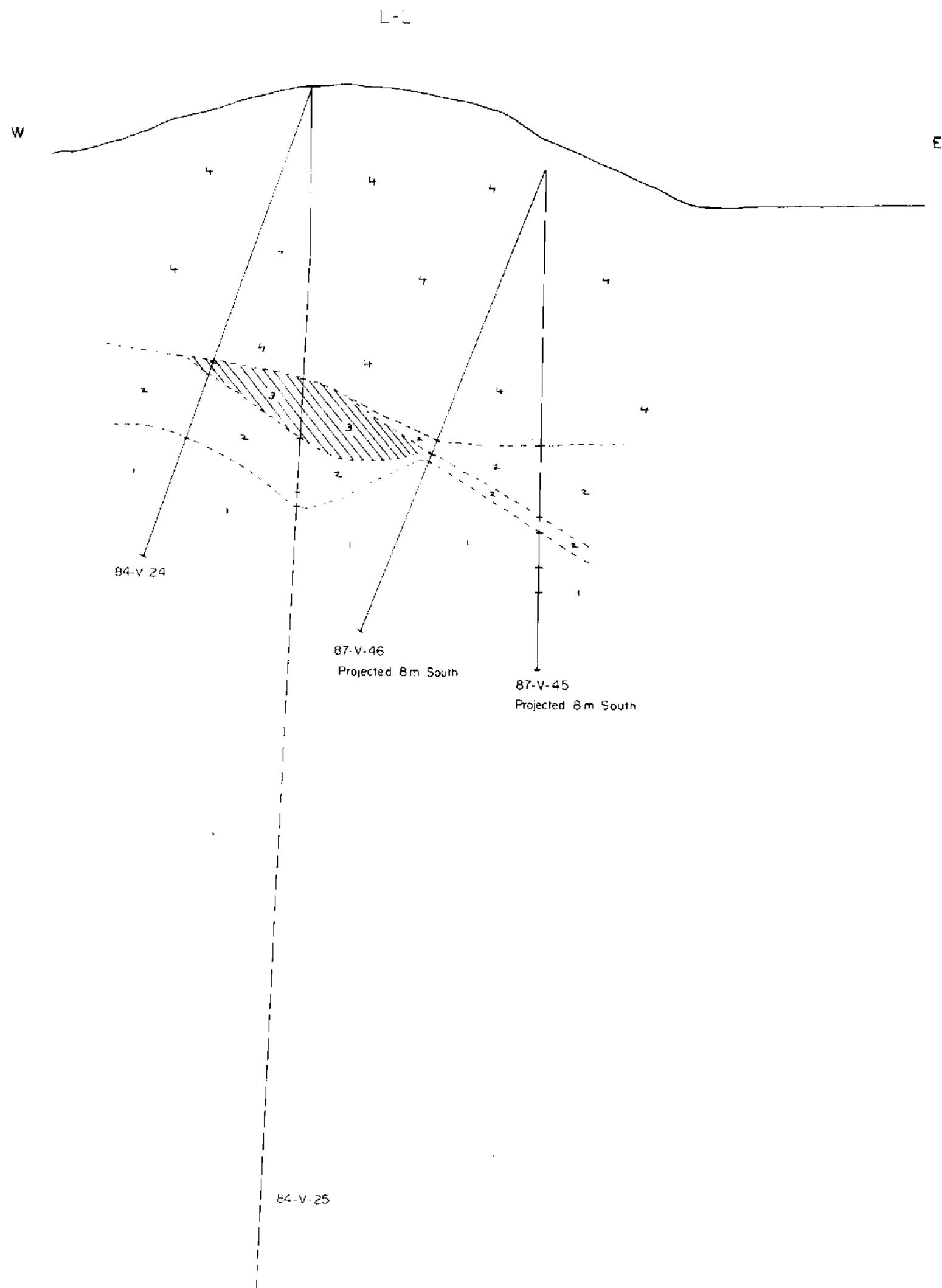
Telephone 604-987-0821

I, Thomas, E. Lisle, of the above address in the District of North Vancouver, British Columbia, Canada do hereby declare:

- 1) That I am a geologist with business at the above address.
- 2) That I am a member in good standing of the Geological Association of Canada, and the Association of Professional Engineers of British Columbia.
- 3) That I supervised the drilling program described in this report on the Villalta Mining Property, Nanaimo Mining Division, between May 3 and June 10, 1987.
- 4) That I prepared the drill logs of drill holes 87-V-1 to 87-V-43 that accompany this report
- 5) That I have no interest in the property described in this report, or in the securities of Canamin Resources Limited or related companies.

Dated this day of June, 1987.


T.E. Lisle, P.Eng.

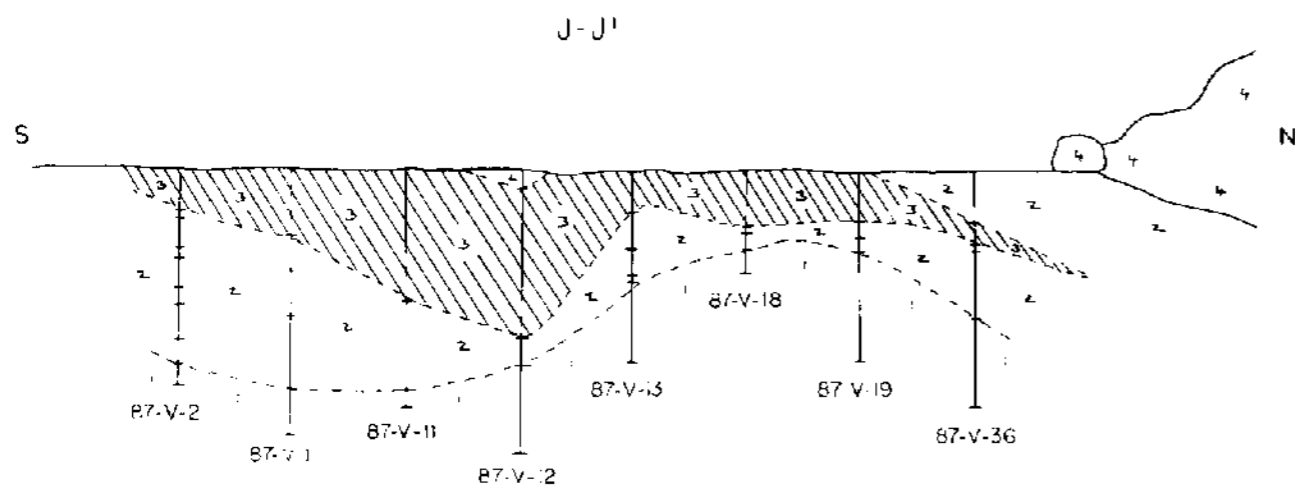
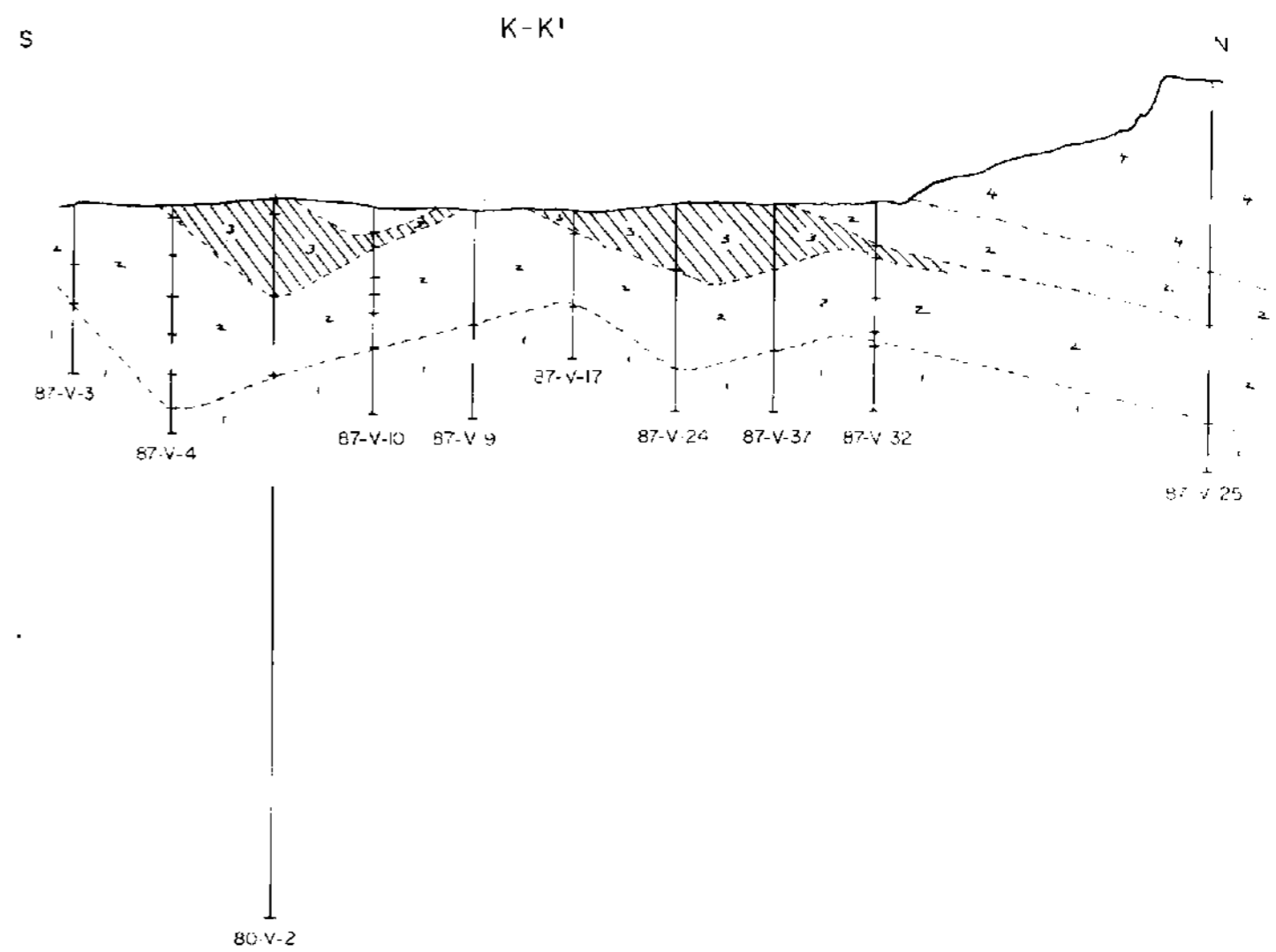
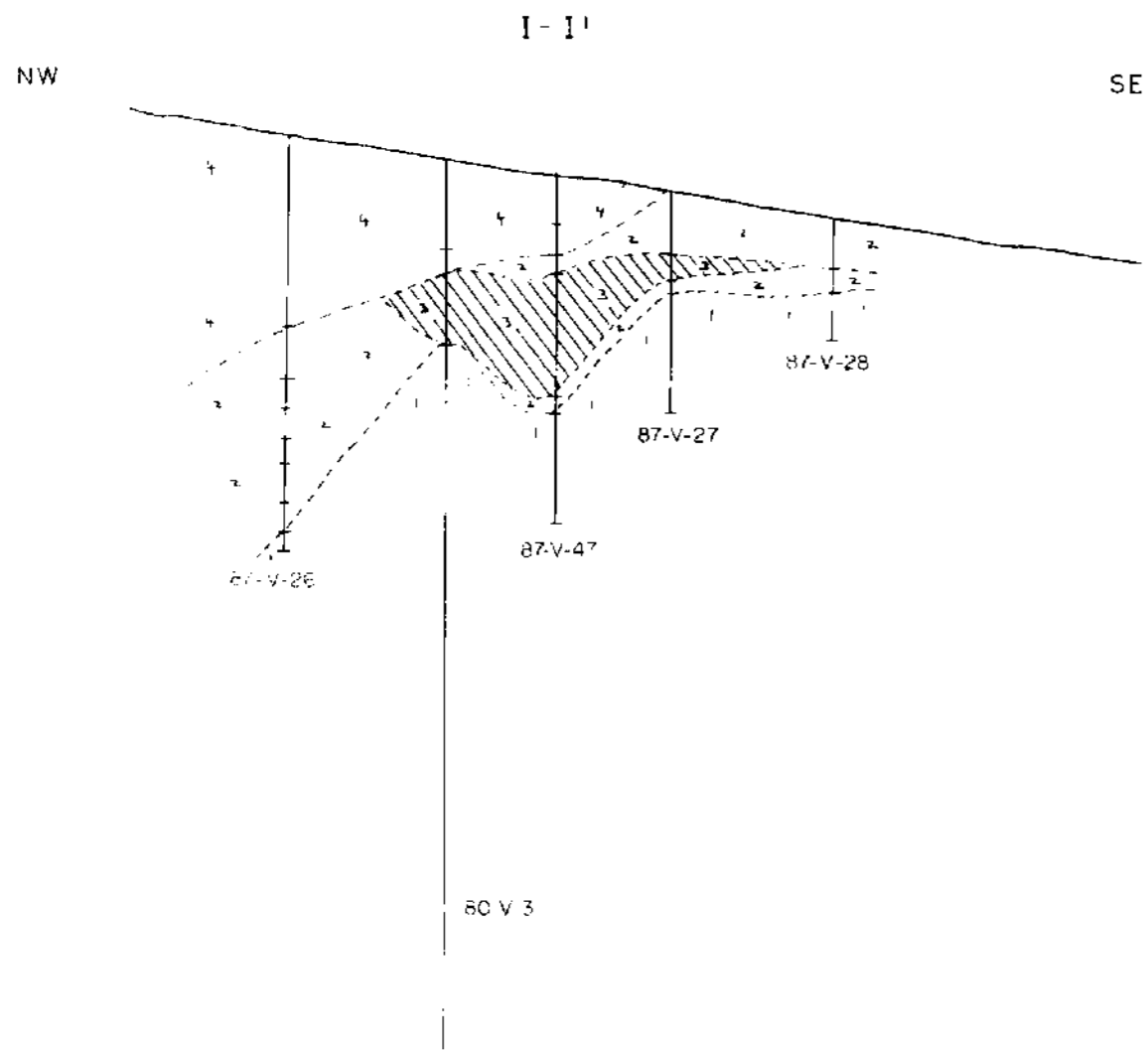


**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

15,939

LEGEND	
⊥	DRILL HOLE
---	GEOLOGICAL CONTACT
4	NANAIMO GROUP SEDIMENTS
3	HAEMATITE ZONE
2	TUFFS & BRECCIAS
1	BUTTE LAKE LIMESTONE

CANAMIN RESOURCES LTD.	
VILLALTA PROJECT	
CROSS SECTIONS L-L', M-M'	
GEOLOGIST: S.P. QUINN/T. LISLE	BASED ON SURVEY 1987
SCALE: 1:500	
DRAWN BY: D.R.	DATE: JUNE 1987
	FIGURE: 6



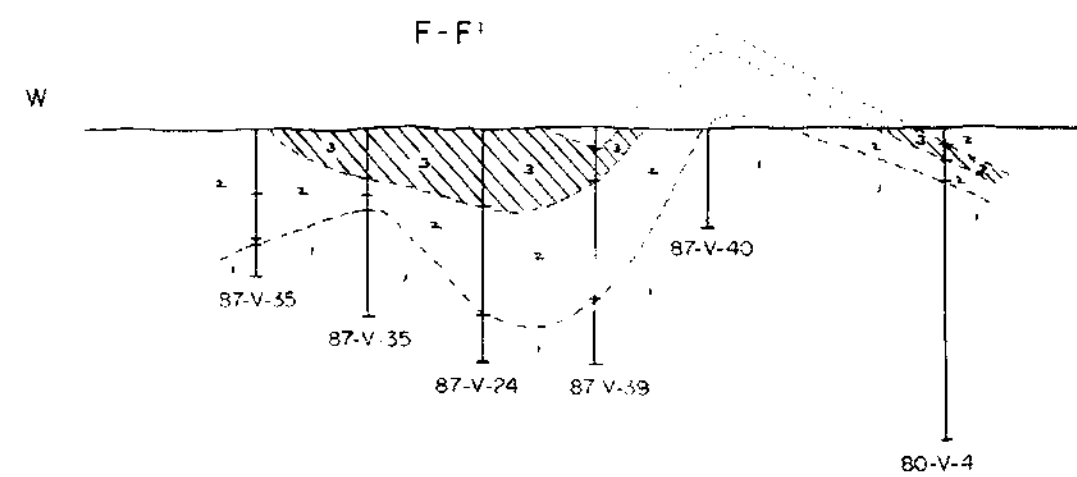
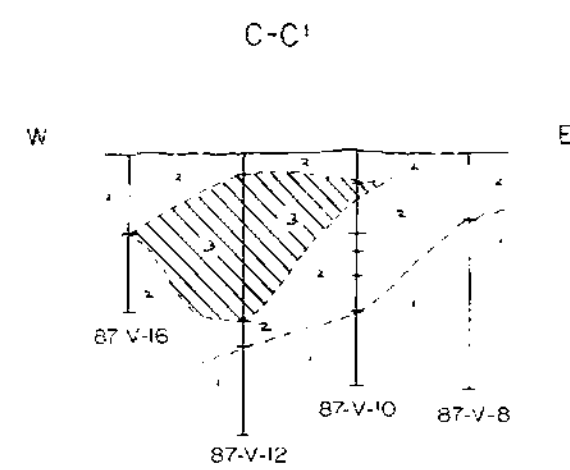
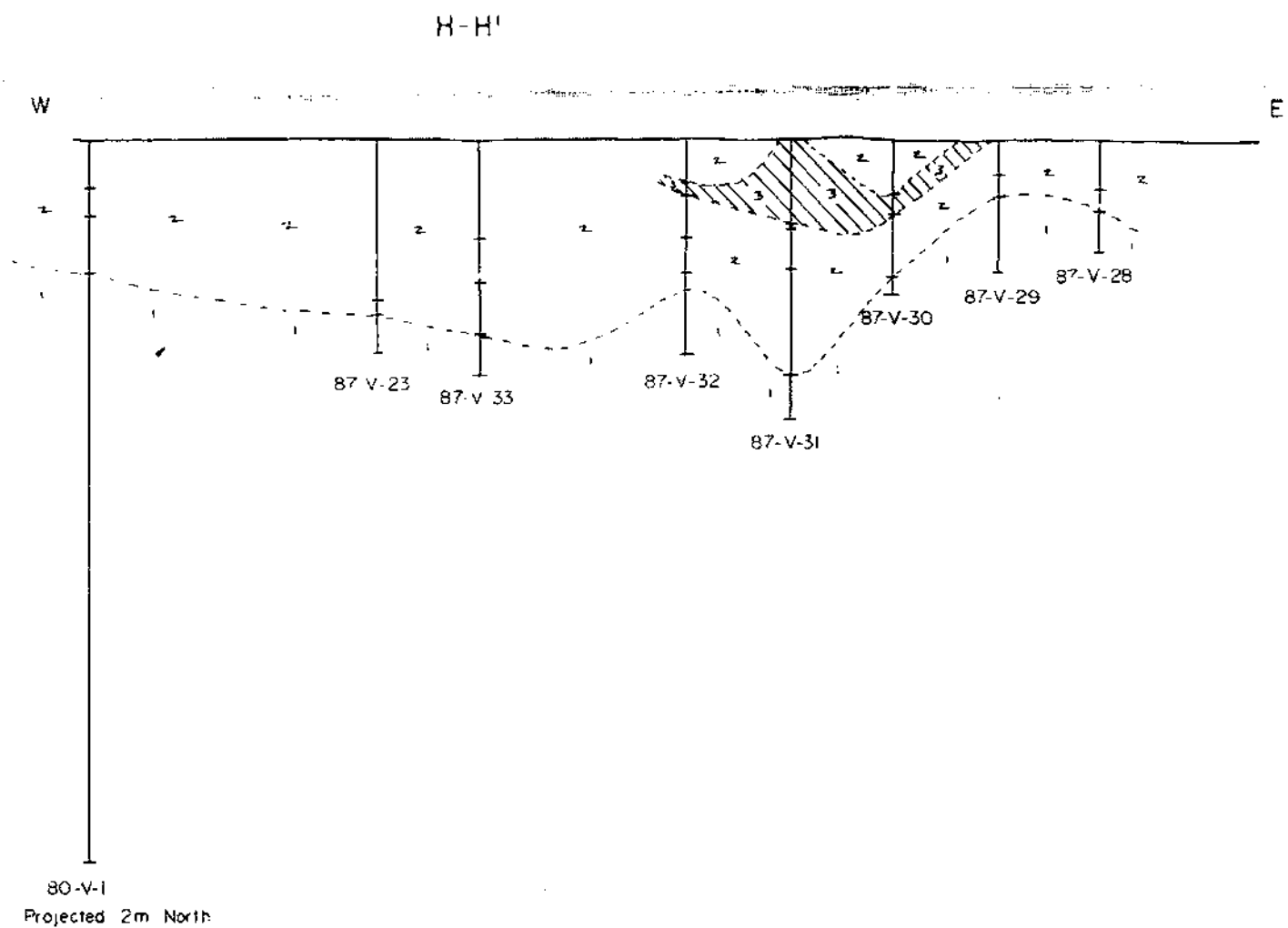
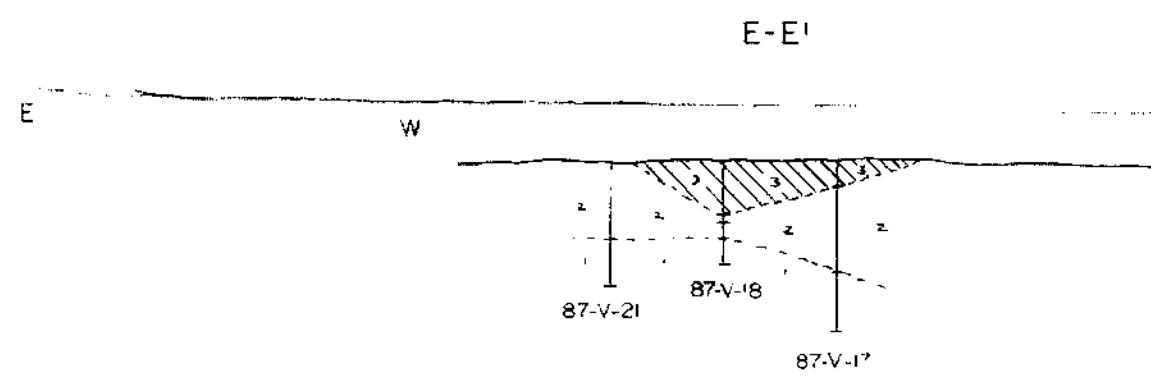
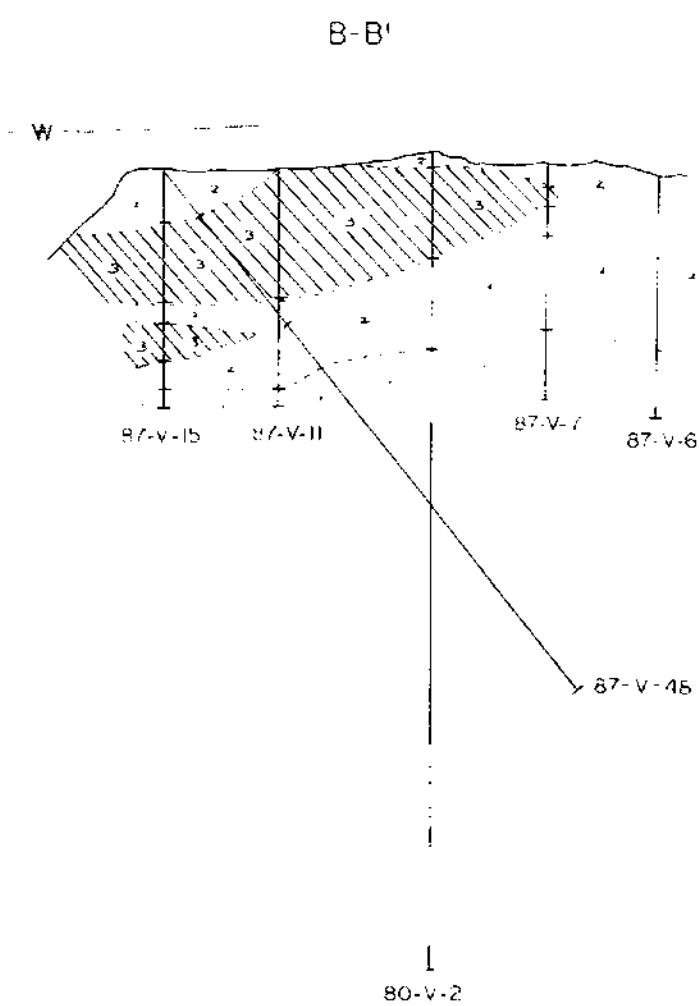
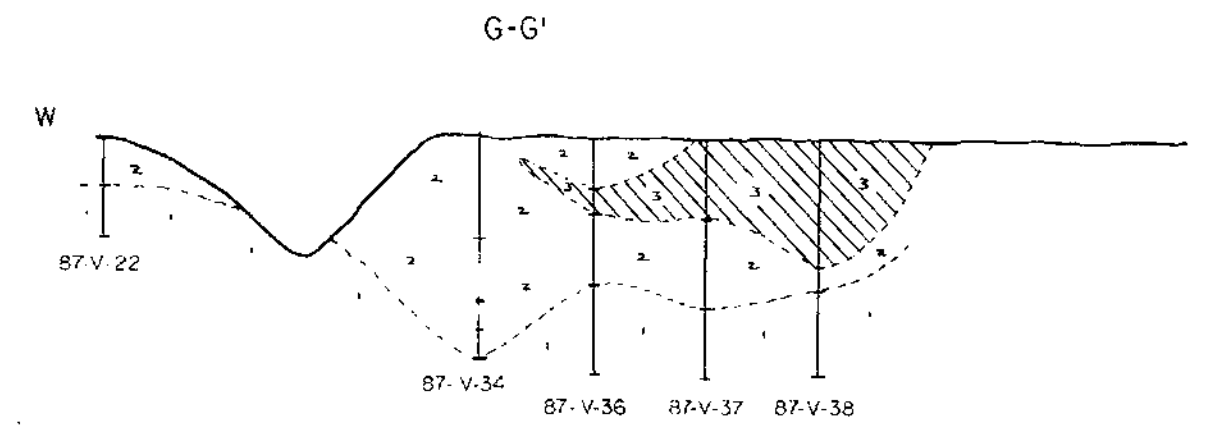
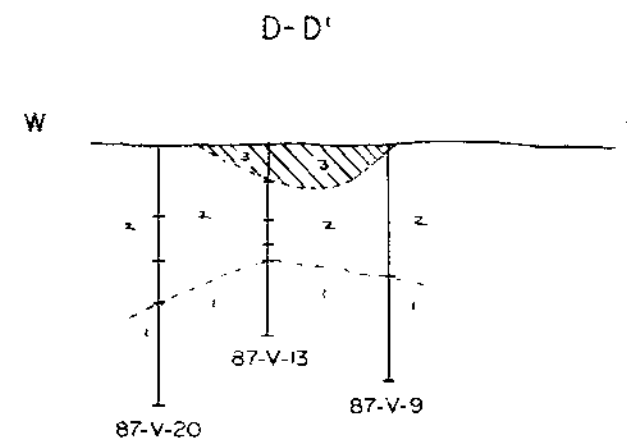
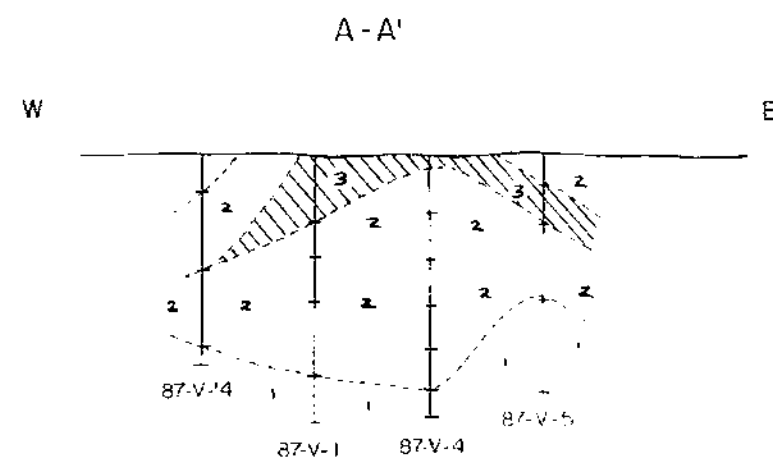
**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

15,939

LEGEND

- DRILL HOLE
- GEOLOGICAL CONTACT
- 4 NANAIMO GROUP SEDIMENTS
- 3 HAEMATITE ZONE
- 2 TUFFS & BRECCIAS
- 1 BUTTLE LAKE LIMESTONE

CANAMIN RESOURCES LTD.	
VILLALTA PROJECT	
CROSS SECTIONS I-I' to K-K'	
GEOLOGIST: S.P. QUINN/T. LISLE	BASED ON: SURVEY 1987
SCALE: 1:500	
DRAWN BY: DR	DATE: JUNE 1987
FIGURE: 5	



LEGEND

- ↓ DRILL HOLE
- GEOLOGICAL CONTACT
- 4 NANAIMO GROUP SEDIMENTS
- 3 HAEMATITE ZONE
- 2 TUFFS & BRECCIAS
- 1 BUTTLE LAKE LIMESTONE

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

15,939

CANAMIN RESOURCES LTD.	
VILLALTA PROJECT	
CROSS SECTIONS A-A' to H-H'	
GEOLOGIST: S.P. QUINN/T. LISLE	BASED ON: SURVEY 1987
SCALE: 1:500	
DRAWN BY: DR	DATE: JUNE 1987
FIGURE: 4	

