87-184-15996

4/88

A GEOLOGICAL, GEOPHYSICAL AND GEOCHEMICAL REPORT

ON THE

WINDY 1-5 CLAIMS

NTS 93-J-13W

LAT. 54° ~~57'~~ 56.7'   LONG. 123° 50.6'

CARIBOO MINING DIVISION

FILMED

OWNER: RICHARD HASLINGER

OPERATOR: PLACER DEVELOPMENT LIMITED

GEOLOGICAL BRANCH ASSESSMENT REPORT

15,996

W. Pentland

R.W. Cannon, P. Eng.

Ian Thomson

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1.0 INTRODUCTION

This report describes the exploration program conducted by Placer Development Limited on the Windy property located on the Salmon River northeast of Fort St. James, B.C. during the period from September 1 - 12, 1986. Prospecting by the owner and reconnaissance sampling by Placer Development and other interested companies had indicated potential for copper, gold and palladium mineralization.

The program consisted of the following:

1. establishment of a line grid
2. soil sampling
3. magnetometer and VLF-EM surveys
4. mapping and sampling of outcrops and test pits.

The sector of the property explored with the present program is that thought to be the most favourable and represents about one-quarter of the ground held.

The region has no history of gold production, but gold prospects have been found in the general area of the Windy property. Placer gold has been found in the Salmon River although not in commercial amounts.

2.0 BACKGROUND

The history of the original prospecting activities in the area is unknown. One or two pits and signs of a cabin, all very old, were noted along the Salmon River. The present interest was started by Richard Haslinger of Fort St. James who located small amounts of chalcopyrite with low gold and silver values on the north bank of the Salmon River. These showings were examined by W. Pentland in May, 1985. The property was rejected with the suggestion that prospecting be extended in an effort to enlarge the area of interest.

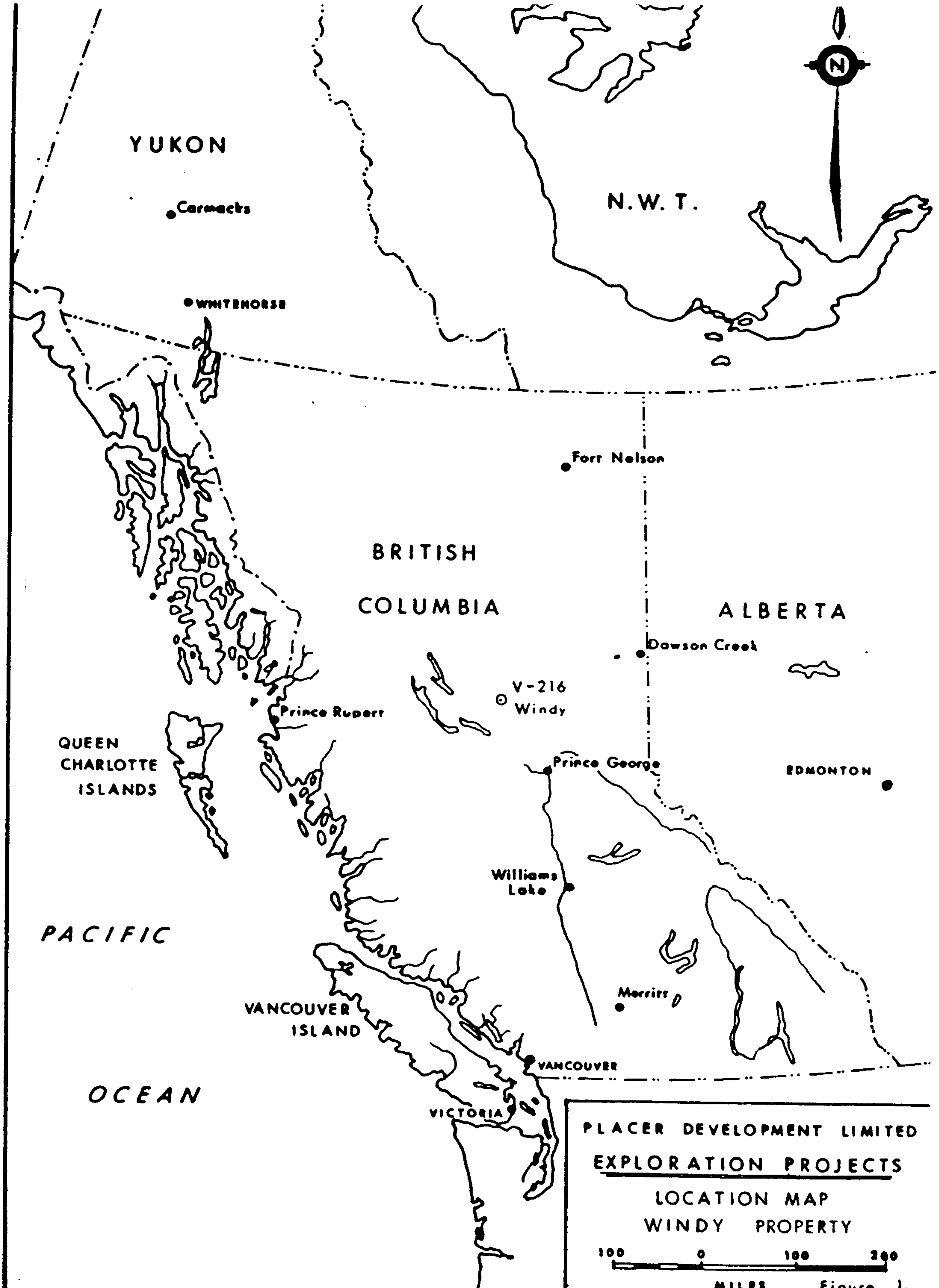
Additional pits containing somewhat higher gold and copper values were dug approximately 200 meters north of the initial discovery. Gold values ran to 0.10 oz/t and in addition it was found that palladium was present in the order of 0.50 grams/t.

In October 1985 Cassiar Mining Corporation (Brinco Mining Ltd.) soil sampled a small grid with lines at 400 meter intervals. Anomalous gold and copper were found and Cassiar concluded that rock types, alteration and mineralization were compatable with porphyry type mineralization. R. Haslinger dug more pits in an area of anomalous soils 800 meters northeast of the discovery pits and partially exposed a large quartz vein. Gold was panned from the overburden in the area.

In June 1986 the property was re-examined by R. Boyce for Placer Development. The check sampling and conclusions reached were favourable resulting in the property being optioned by Placer in August 1986.

3.0 LOCATION AND ACCESS (SEE FIGURE 1)

The Windy claims are located in Central British Columbia 65 kms north - northeast of the town of Fort St. James. The Salmon River traverses the southern part of the claims and Salmon Lake is located 7 kms to the south. Access is by helilcopter from either Fort St. James or MacKenzie which are


YUKON
Carmacks
WHITEHORSE
N.W.T.
N
Fort Nelson
BRITISH
COLUMBIA
ALBERTA
Dawson Creek
V-216
Windy
Prince Rupert
QUEEN
CHARLOTTE
ISLANDS
Prince George
EDMONTON
Williams
Lake
PACIFIC
Merritt
VANCOUVER
ISLAND
VANCOUVER
OCEAN
VICTORIA
PLACER DEVELOPMENT LIMITED
EXPLORATION PROJECTS
LOCATION MAP
WINDY PROPERTY
100
0
100
200
MILES
Figure 1.

equidistant from the property.

Access is also available by logging road to a point approximately 10 kms south of the claims and a forestry access road is projected to go through the property in the near future.

4.0 PROPERTY COMPOSITION (see figure 2)

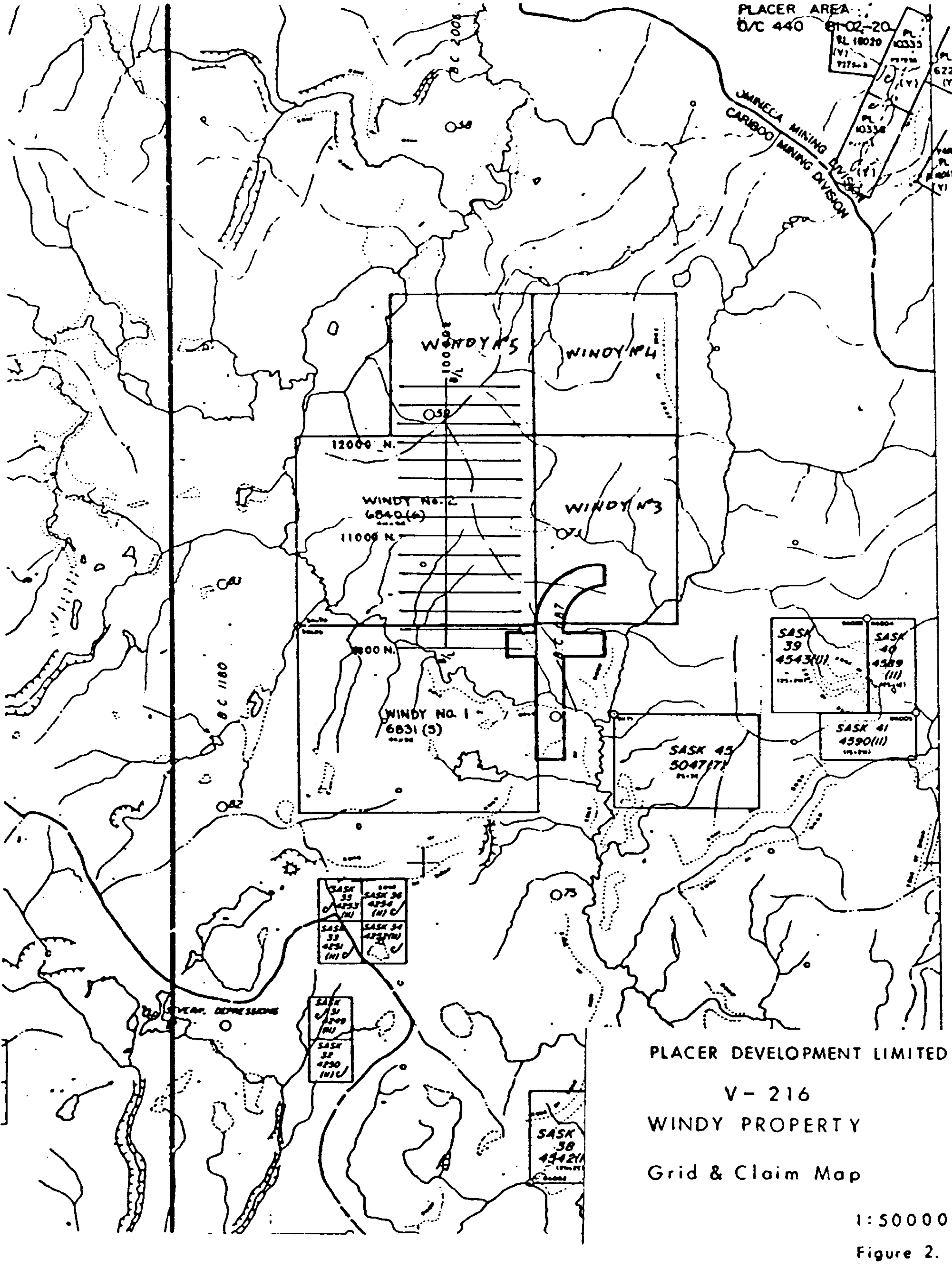
The Windy property is composed of 5 claims totaling 70 units. Claim status is as follows:

NAME	UNITS	EXPIRY DATE	RECORD NO.
Windy 1	20	May 16, 1987	6831
Windy 2	20	June 3, 1987	6840
Windy 3	12	July 9, 1987	7836
Windy 4	9	July 9, 1987	7837
Windy 5	9	July 9, 1987	7835

5.0 PHYSIOGRAPHY

The majority of the property is located on a topographic high with the ground surface sloping quite moderately in all directions from a maximum elevation of 3700' to a low of 3000' on the Salmon River in the southeast corner of the property.

The Salmon River flows southward along the western property boundary before angling southeast across the Windy No. 1 claim. A parallel tributary stream follows the east property boundary. The ground to the south of the Salmon River is generally flat with swampy areas.



PLACER DEVELOPMENT LIMITED

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WINDY PROPERTY

Grid & Claim Map

1:50000

Figure 2.

The grid on which the present program was done extends northward from the Salmon River to the topographic high in the north central sector of the property. The coniferous forest cover on the grid area is composed of spruce, balsam and lodgepole pine with the occasional fir. This is mixed with scattered and patchy poplar, tag alder, willows and occasional open meadows.

Outcrops are fairly common along and in the vicinity of the Salmon River. To the north however, in the area of the present grid, outcrop is rare. There are areas which appear to be underlain by sub-outcrop and in general the overburden appears to be quite thin. Glacial striae and oriented cobbles indicate that the direction of the last ice movement in this area was from the south towards N10°E.

6.0 WORK PROGRAM

The field program ran from September 1 - 12, 1986 for a total of 22 man days by Placer Development staff. Personnel involved were W. Pentland - geologist, R.W. Cannon - geophysicist, B. Ott and R. Hodgson. The line grid was put in by contractors and was comprised of 2.8 kms of cleared baseline and 19 kms of flagged cross lines at 200 m intervals with stations at 20 m intervals. An additional 2 kms of fill-in line at 100 m intervals was done later.

Magnetometer and VLF-EM ground geophysical surveys were done on the grid and a total of 560 soil samples collected. Outcrops and prospect pits were located and 26 rock samples collected.

Due to the short duration of the program the crew based in Fort St. James and travelled by helicopter to the property each day.

7.0 GEOLOGY

The property is located in the northwesterly trending belt of Takla Group rocks; Upper Triassic and/or Lower Jurassic in age and composed of andesitic and basaltic flows, tuffs and breccias. It is a northwesterly extension of the Quesnel Trough.

The Wolverine Complex lies a few kilometers to the east. It consists of granites, gneisses and schists in part derived from Lower Cambrian Caribou Group rocks. Metamorphism and granitization is placed from post - Lower Cambrian to Mesozoic in time.

The area of the Windy property has been mapped as having widespread overburden cover. Limited outcrop of Takla Group rocks are shown as occurring along the Salmon River and encroaching on the Windy property in the southeast corner.

7.1 PROPERTY GEOLOGY

Outcrop in the gridded area is very limited. Beyond the exposures along the Salmon River only half a dozen outcrops were found. Four additional exposures occur in pits and uprooted trees.

Information is particularly scarce on the northern half of the grid. One outcrop and considerable angular float were noted in the northwest corner of the grid leaving the strong impression of that sector being underlain by relatively unaltered diorite. Bedrock exposures in the southern half of the grid are more frequent particularly in the southwestern corner. All appear to be dioritic. A zone from 10,200 N to 10,300 N at 9,800 E contained several fairly angular boulders of lapilli tuff. These were originally thought to represent sub-outcrop but in hindsight are probably glacial till.

All specimens definitely originating from rock in place, ie outcrop or pits, appear to be dioritic in origin. They are fine to medium grained, unaltered to highly altered and variably sheared. Alteration consists of chlorite, epidote, carbonate and sericite. Shearing to some degree is apparent in most outcrops and in some cases is intense. Where measurable the strike is northeast.

Several specimens from the southwest area were submitted by Brinco Mining Ltd. to Vancouver Petrographics Ltd. for a thin section study. The following description is quoted from the summary of the report by Vancouver Petrographics Ltd.

"Alteration (or metamorphism) has occured under greenschist facies conditions with the development of actinolitic amphibole from original hornblende. The rocks could be called meta-diorites. There has clearly been some shearing but this was not so intense as to produce a strong foliated fabric. Rather there has been development of thin veinlets and diffuse shears zones around and partly within the plagioclase. The veinlets are filled with epidote while the shears are sericitic. As well as veinlets, a "disconnected patchy network" of epidote has developed around and partly within the plagioclase. Minor chlorite and sphene are alteration minerals."

At present there is no information as to where the diorite intrusion fits into the geological calendar. The most likely possibility is the Omineca intrusions of the Upper Jurassic to mid-Cretaceous age.

7.2 MINERALIZATION (see Figures 3 and 4)

Pyrite may be found in most specimens but in minor to trace amounts. The area of greatest interest is in the southwest corner of the grid from 9950 N, 9500 E to 10,200 N 9670 E. Pits and outcrops in this zone contain chalcopyrite and malachite with variable but low values in gold, silver and palladium.

The chalcopyrite, with minor pyrite, occurs as disseminations and veinlets in the diorite where it is associated with quartz and quartz-tourmaline veins. The latter situation occurs at 10,200N, 9660 E where a pit exposes quartz veining with black patches and sections of intergrown grains of tourmaline.

Assays from this southwest zone have ranged up to >1.00% Cu and 3.0 ppm Au but the average is much less. The maximum values obtained by Placer in the present program were .71% Cu and 1.35 ppm Au. The average for 5 samples from the zone was 0.36% Cu and 0.57 ppm Au. Palladium was found in several samples to a maximum of 1.25 ppm.

The second area of interest is located at 10,800 N, 10,150 E. Reconnaissance soil sampling by Brinco indicated high Au and As. R. Haslinger dug several pits in the area revealing sheared diorite at very shallow

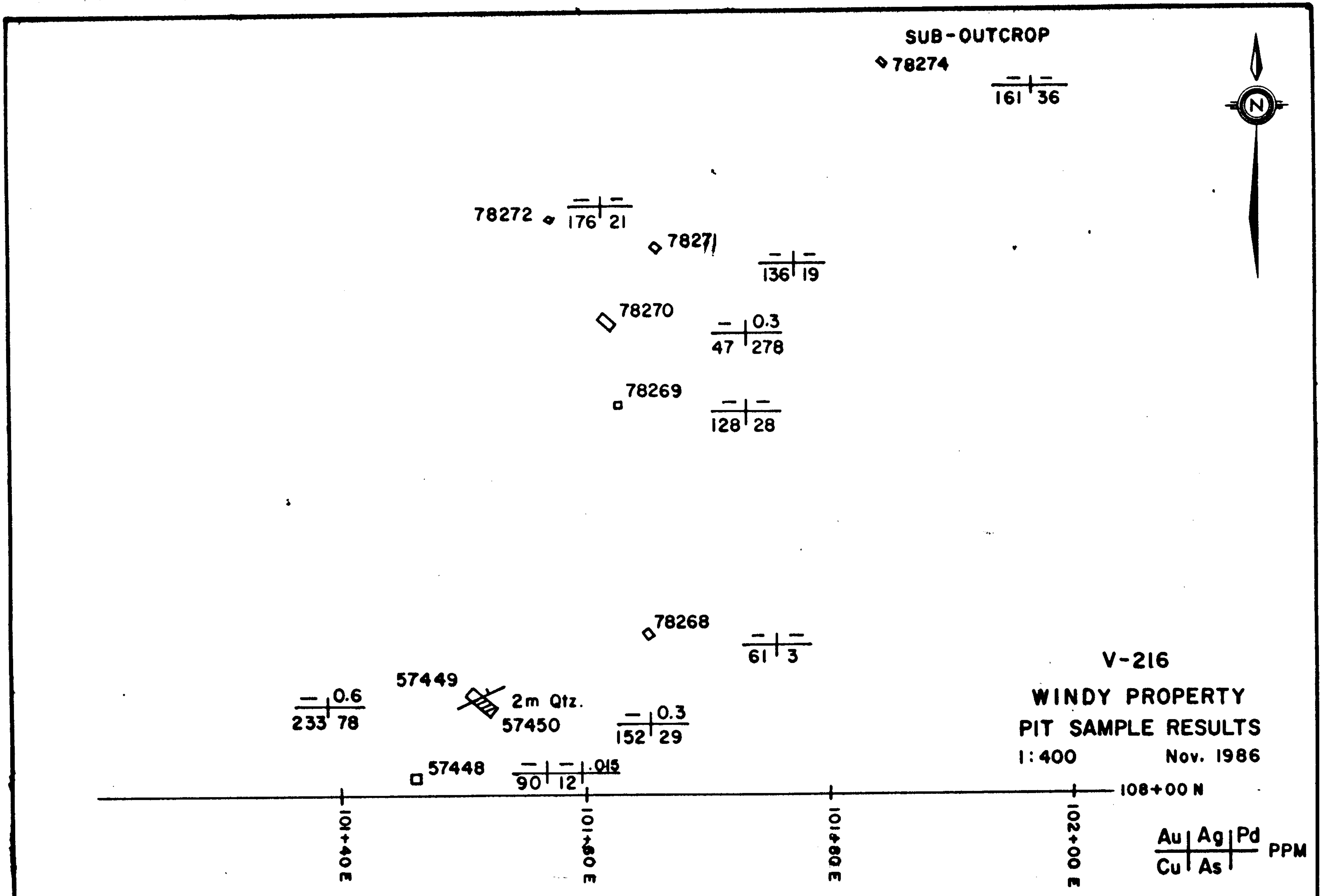
SUB-OUTCROP
78274
— | — 161 | 36
78272
— | — 176 | 21
78271
— | — 136 | 19
78270
— | 0.3 47 | 278
78269
— | — 128 | 28
78268
— | — 61 | 3
57449
2m Qtz.
57450
— | 0.6 233 | 78
— | 0.3 152 | 29
57448
— | — | .015 90 | 12
108+00 N
101+40 E
101+60 E
101+80 E
102+00 E
Au | Ag | Pd Cu | As PPM
V-216
WINDY PROPERTY
PIT SAMPLE RESULTS
1:400
Nov. 1986

FIG. 4

depth. A quartz vein (?) was partially exposed over two meters. No values were obtained from samples of the quartz. R. Haslinger was able to pan gold from overburden in the vicinity.

8.0 GEOPHYSICS

The results of an airborne magnetic survey done by the Geological Survey of Canada in 1961 are available. There is little variation in magnetic intensity with a maximum change of approximately 130 gammas on the property. The isomagnetic lines trend north-northeast appearing to parallel the lineation noted in the rocks. There is no airborne magnetic expression of the underlying intrusive as is clearly demonstrated on the "Tezzeron Creek" map a few kilometers to the west.

The present VLF-EM ground survey was carried out using the transmitting station at Jim Creek, Washington (Seattle). The direction to the station was 150 Az, therefore readings were taken facing 060 Az or 30 N of the line at 20 m intervals.

Magnetometer readings were taken at 10 m stations and correction for drift and diurnal changes were made by use of a base station recording magnetometer.

8.1 EQUIPMENT USED

The magnetometer survey was conducted using two Geometrics G-856A portable proton magnetometers (memory-mag). One was used in the field mode (Ser. No. 27503) while the other was used in a base station mode (Ser. No. 27502). The internal clocks were synchronized before commencement of the survey and subsequent daily readings were dumped out to floppy disc in a Kaypro I portable computer. The data from the two magnetometers were merged and corrected for diurnal drift from an established base station value. The corrected results were plotted as field profile and also stored on disc for eventual transfer to a Univac 1108 for final plotting.

The VLF-EM survey employed a geonics EM-16 (Ser. No. 25) which used the following transmitting station:

Jim Creek NLK 24.8 kHz

VLF readings were also entered only floppy disc in a Kaypro I computer and field profiles of In-Phase. Quadrature and Fraser Filter data were plotted. The stored data was tranferred to a Univac 1108 for final processing and plotting.

8.2 SURVEY RESULTS

The magnetometer survey results were plotted as plan maps of contoured and posted data at a scale of 1:5000 (see plates in folder at back of report).

The VLF-EM survey results were plotted as posted plan maps of In-Phase, Quadrature and Fraser Filter data and as a contoured Fraser Filter plan map at scales of 1:5000. The Fraser Filter data was calculated as per the method put forth by D.C. Fraser (1969, Contouring of VLF-EM data; Geophysics V.34 p.958-967). See plates in the folder at the back of report.

8.3 DISCUSSION OF RESULTS

8.3.1 MAGNETOMETER SURVEY

Weak magnetic anomalies were detected on lines 9800 through 10200 west of the 10000 E Baseline. Several of these anomalies could be traced from line to line and probably reflect changes in the underlying intrusive rocks. Several minor magnetic zones were detected on the northern most lines and appear to outline the edge of an intrusive.

8.3.2 VLF EM-16 SURVEY

Numerous weak conductor axes were outlined by the results of the VLF survey. No correlation has been attempted between lines as the line spacing of 200 m would make the connection of these weak anomalies speculative to say the least.

8.4 CONCLUSIONS AND RECOMMENDATIONS

It was concluded that the magnetometer survey could be of use in mapping the intrusive in areas of overburden cover. The VLF survey may be of more use in combination with the geochemical survey results in confirming any trends detected. No recommendation can be made on the property based solely on the geophysical results.

9.0 GEOCHEMISTRY

Reconnaissance soil sampling on the property by Cassiar Mining Corporations and Placer Development Limited had indicated that the method was satisfactory for copper, gold and arsenic. The procedure was therefore selected as the main exploration tool for the initial program.

9.1 SAMPLING PROCEDURES

A total of 560 soil samples were collected along the grid lines at 40 m intervals. The coverage was very good with only a few failures to obtain a sample; usually due to thick humus in swamps. Most of the samples were collected using hand augers which proved highly satisfactory since many of the samples were at considerable depth and unlikely to have been reached using a mattock. Sample depth varied from 10 cms to 110 cms with a considerable number in the 30 cm to 60 cm range. Notes were recorded on the material collected and on site conditions. The samples were collected in Kraft paper bags and sent to the Placer Development Laboratory in Vancouver for geochemical analysis for Au, Ag, Cu, Pb, Zn, Mo, As and Sb.

9.2 SAMPLING CONDITIONS

Samples were collected from the "B" soil horizon. In general the horizon is a light tan color with some variation from yellow to orange tone. A second characteristic is the high sand content. The size range varies from fine to coarse and there is usually some grit present. Occasional areas were quite gravelly with abundant pebbles.

It should be noted that the gravel content as recorded is probably low in many cases and is due to using an auger to obtain the samples. Some pebbles to 3 - 4 cm are picked up by the auger but larger clasts tend to be pushed aside. Very large clasts are immovable and block the auger necessitating a new hole. In rare severe cases the sample was collected using a mattock. In general the augering procedure had little trouble indicating a relatively low content of large clasts in the overburden.

The only area where soil conditions appeared to vary to any extent from the normal was in the extreme southwest corner of the grid on line 9800 - 10200 N where zones of silts and washed sands were encountered. These may represent old Salmon River stream channels.

9.3 RESULTS

The location and identification of the soil samples are shown in Figure 11 . Full listings of all soil geochemical data are provided in tabular form in Appendix 2 together with summary statistics and histograms for each element. The distribution of copper and arsenic in soils across the grid are shown in figures 12 and 13 respectively.

9.3.1 Element Distribution Patterns

Of the elements analysed only copper and arsenic display coherent, interpretable patterns of potential economic significance. Antimony and Mo are very largely undetected. Lead, Zn and Ag display broad amorphous patterns. Gold has a distinctive distribution that, while significant, is difficult to interpret.

Copper (Figure 12)

Copper displays a bimodel distribution which may be subdivided by contours selected at 75 and 150 ppm. The populations so defined have distinct aerial distributions and outline areas of potential intent.

In the south west part of the grid is an area extending from 9900N to 10800N and 9400E to 10000E with values of greater than 75 ppm ranging up to 820 ppm Cu. Peak values occur close to the point where bedrock samples are known to contain several thousand ppm Cu. Elsewhere in the zone other clusters of high values to the north and east suggest further areas of Cu rich bedrock or down ice dispersion of Cu rich rock debris.

To the north the central part of the grid is characterized by slightly elevated Cu values (75-120 ppm) which form an elongated zone east of line 10000E. This may indicate the presence of a distinctive rock type with a high background content of Cu beneath the grid throughout this area.

In the far north, Cu values increase to greater than 150 ppm at several scattered localities to form an irregular zone which is open to the north. A further area of bedrock with substantially elevated Cu concentration is inferred.

Arsenic (Figure 13)

Arsenic also displays a tendency towards a bimodel distribution which can be well seen when the data are contoured at 10 ppm and 20 ppm.

A well defined zone of elevated As values, elongated north-south, is found in the south central part of the grid extending from 10200N, 10200E to 11600N, 10400E. This zone encloses the area of pits at 10800N, 10150E where gold has been located. Peak values of 120 ppm As are found to the south within an area of +20 ppm As values. Arsenic values appear to decrease systematically from this point towards the north, a pattern which tends to suggest dilution due to down ice dispersion from a principle source in the southern part of the zone.

A second area of elevated As values occurs in the far north western part of the grid. This zone carries soils with up to 73 ppm As and is open to the north.

Gold

Gold is erratically distributed across the grid with a tendency for detectable concentration to be more frequently recorded in the southwest. The lack of any coherance or clear association with the areas of known gold in bedrock is discouraging. Further examination of the data, however, reveals that Au values closely approximate a poisson distribution which tends to indicate that gold occurs preferentially as free grams 0.150 mm or larger in diameter. The implication of this observation is that gold is coarse and free and poorly represented by the -80 mesh (-.177 mm) fraction used for analysis.

It is noteworthy that R. Hasslinger has successfully panned gold grains from the overburden in areas where the soils data show gold as largely undetected.

9.3.2 Discussions and Interpretation

Three geochemical anomalous zones are recognized on the grid and are shown on the interpretation map (Figure 11) accompanying this report. These anomalous zones may be described as follows:

Anomaly 1. This broad, elipitical feature is defined by anomalous Cu in soil and by Cu, Au and Pd in bedrock within the soil anomaly. A relatively large area of Cu rich bedrock is indicated which, by extrapolation, is inferred to carry Au and Pd. It is possible that the soil anomaly is developed on transported glacial material and thus larger than the bedrock sources. The geochemical signatures and observed geology is consistent with a body of porphyry mineralization.

Anomaly 2. This is a narrow, elongate As soil anomaly which encloses an area where pits and overburden samples contain free gold. The anomaly flanks, but is quite separate from Anomaly 1. A possible composite, zoned area of mineralization is suggested with Cu + Au + Pd (porphyry mineralization) flanked by As + Au (possible vein or stockwork or structurally controlled mineralization).

Anomaly 3

The far northern part of the grid is characterized by partly coincident zones of anomalous Cu and As in soil. The anomaly signature is different from Anomalies 1 and 2 and is open to the north. Absolute abundances are relatively low in the area sampled suggesting a lower intensity of mineralization or the flanks of a strong centre of mineralization outside the grid to the north.

9.4 CONCLUSIONS AND RECOMMENDATIONS

Three anomalous zones are recognized on the grid, two of which are spatially related to known gold showings but define much larger areas of potentially mineralized bedrock. The geochemical signature of the third anomaly is different from the other two and the feature is open to the north. The present geochemical procedure for determining gold in soils provides poor data due to the mode of occurrence of the gold and the size fraction selected for analysis.

On the basis of the geochemical data it is concluded that the potential for relatively large areas of mineralized bedrock containing gold exists on the grid and the following recommendations are made.

1. Extend the soil grid to the north to close off Anomaly 3.

2. Perform size fraction analysis of soils collected in the vicinity of the known gold showings to confirm the mode of occurrance and preferred size fraction of Au.

3. Based on the results of (2) above analyse the coarse fraction of soils for contained gold to provide more confident data on the distribution of Au on the property.

10.0 RECOMMENDATIONS FOR FURTHER EXPLORATION.

Gold has been found in bedrock on the property at two locations which also lie within two (Cu + Au, As + Au) distinct geochemical environments. Further information is required to describe the geology of the property, the character of the known mineralization and define the full extent of possible mineralization.

A positive relationship between Au and disseminated sulphides is noted about Anomaly 1. The sulphides can be mapped using an Induced Polarization geophysical survey. Such a survey would also aid identification of alteration and silicification which may be associated with gold mineralization.

Trenching to bedrock will permit mapping and sampling of the bedrock within the soil anomaly zones and across any geophysical features interpreted as significant. Soil anomaly C is open to the north and should be closed off.

Further exploration work is recommended as follows:

1. Extend the grid to 13000N and complete geochemical soil sampling (analysis for Cu, As, Au, Ag), mangetometer and VLF-EM surveys across this extension at the same density as the remainder of the grid.

2. Complete an Induced Polarization survey along the existing grid lines across the area defined by 10000N to 11000N and 9500E to 10400E.

3. Excavate trenches to bedrock across the focal points of Anomalies 1, 2 and 3 and extend these trenches in an up-ice direction to establish the bedrock sources. Bedrock should be mapped and sampled along the trenches. Profile samples should be taken through overburden in the walls of each trench to confirm the location of the principal sources of anomalous metals in bedrock.

4. Bulk soil samples collected at the known gold showings should be studied to confirm the mode of occurrence of Au in soils.

W. Pentland

W.S. Pentland

R.W. Cannon

R.W. Cannon

I. Thomson

RC/cs

03:31:87

REFERENCES

1. Results of an Examination on the Windy Property, B.C.
   Cassiar Mining Corporation
   By R.S. Hewton, P.Eng. 1985

2. Windy Property, Salmon Lake Area, B.C.
   Placer Development Limited
   By R.A. Boyce, July 1986

3. Map 1204 A
   Geology - McLeod Lake, B.C. 1:250,000
   Geological Survey of Canada 1968

4. Map 1572 G
   Airborne Magnetics - Salmon Lake, B.C. 1:50,000
   Geological Survey of Canada 1961

5. Topographic Map
   Salmon Lake, B.C. 1:50,000
   93-J-13
   Dept of Energy, Mines and Resources, 1979

STATEMENT OF QUALIFICATIONS

I, W.S. Pentland, with a business address in Vancouver, British Columbia, and a residential address in Delta, British Columbia, hereby certify that:

1. I am a geologist graduating from the University of British Columbia, Vancouver, British Columbia, with a B.A. in 1951.

2. From 1951 to 1986, I have worked in mineral exploration in various parts of Canada.

3. I personally examined the area and have assessed the results of the work.

W.S. Pentland

WSP/cs
03:31:878

STATEMENT OF QUALIFICATIONS

I, Richard W. Cannon, of the City of Vancouver, Province of British Columbia, hereby certify as follows:

1. I am a graduate of the University of British Columbia where I received a B.A. Sc. in Geological Engineering (Geophysics Option) in May 1966.

2. I am a member of the Association of Professional Engineers of British Columbia and have been so since 1968. Registration No. 6742.

3. I am a member of the Canadian Institute of Mining and Metallurgy, Society of Exploration Geophysicists, and B.C. Geophysical Society.

4. I have practised my profession since 1966.

R.W. Cannon, P. Eng.

STATEMENT OF QUALIFICATIONS

I, Ian Thomson, of the City of Vancouver, Province of British Columbia, do hereby certify that:

(1) I am a graduate of the University of London (England) where I received a B.Sc. (Honors) in Geology in 1967 and a Ph.D. in Applied Geochemistry in 1971.

(2) I am a member of the Association of Exploration Geochemists and the Canadian Institute of Mining and Metallurgy.

(3) I have practised as a geologist-geochemist and professional geochemist since 1971.

Ian Thomson

IT/cs
04:09:87

APPENDIX 1

STATEMENT OF EXPENDITURES

The following expenditures were incurred for a geological, geophpysical and geochemical exploration program on the Windy 1, 2 and 5 mineral claims located northeast of Fort St. James, B.C. during September, 1986. The expenditures are to be applied to the Windy 1 to 5 mineral claims.

1.	Labour * (Salaries and Benefits)	$8,325.00
2.	Motel and Meals	1,500.00
3.	Line Cutting (Contracted)	3,500.00
4.	Transportation	
	a. 2 airfares - Vancouver to Prince George	600.00
	b. U-drive car - 1 week	300.00
	c. 4 x 4 suburban - 1 week	500.00
	d. helicopter - 12.4 hours	6,479.00
5.	Assay Charges **	8,936.00
6.	Report Preparation	3,500.00
		$33,840.00

* Labour (Salaries and Benefits)
- W. Pentland - Geologist - 10 days @ $300/day
- R. Cannon - Geophysicist - 7 days @ $275/day
- R. Hodgson - Technician - 7 days @ $200/day
- B. Ott - Technician - 8 days @ $250/day

** Assay Charges

A. Soil Samples -

Preparation	$ .75
Digestion	2.00
Copper	.90
Lead	.90
Zinc	.90
Molybdenum	.90
Arsenic	.90
Silver	.90
Antimony	2.00
Gold	5.00
	$ 15.15

560 Soils =$8,484.00

B. Rock Samples -

Preparation	$ 3.00
Digestion	2.00
Copper	.90
Lead	.90
Zinc	.90
Molybdenum	.90
Arsenic	.90
Silver	.90
Antimony	2.00
Gold	5.00
	$ 17.40

26 Rocks = $ 452.00

APPENDIX 2

TABLE 1

EXTRACTION AND ANALYTICAL METHODS

Element	Units	Subsample Weight (grams)	Extraction Procedure Attack Used	Time	Analytical Method	Detection Range
Cu	ppm	0.5	Conc. $HClO_4/HNO_3$	4 hrs	Atomic Absorption	2-4000
Zn	ppm	0.5	Conc. $HN1O_4/HNO_3$	4 hrs	Atomic Absorption	2-3000
Pb	ppm	0.5	Conc. $HClO_4/HNO_3$	4 hrs	A. A. Background Corrected	2-3000
Ag	ppm	0.5	Conc. $HClO_4/HNO_3$	4 hrs	A. A. Background Corrected	0.2-20
Au	ppm	10.0	Aqua Regia	3 hrs	A. A. Solvent Extraction	0.02-4.00
As	ppm	0.5	Conc. $HClO_4$/HNO3	4 hrs	A. A. Background Corrected	2-1000
Sb	ppm	0.5	Conc. $HClO_4/HNO_3$	2 hrs	A. A. Background Corrected	2-1000
Mo	ppm	0.5	Conc. $HClO_4/HNO_3$	4 hrs	A. A. Nitrous Oxide	1-400

PLACER GEOCHEM ASSAY SYSTEM: DATA FROM V216 WINDY

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GRID	SAMPLE		PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L9800N	9520E	6245	<1	30	58	4	<0.2	<0.02	3	<2
93J13W	L9800N	9560E	6245	<1	30	49	5	<0.2	<0.02	4	<2
93J13W	L9800N	9600E	6245	<1	29	55	6	<0.2	<0.02	2	<2
93J13W	L9800N	9640E	6245	<1	36	62	5	<0.2	<0.02	5	<2
93J13W	L9800N	9680E	6245	<1	49	60	5	<0.2	<0.02	10	<2
93J13W	L9800N	9720E	6245	<1	15	87	5	<0.2	<0.02	4	<2
93J13W	L9800N	9760E	6245	<1	55	60	6	<0.2	<0.02	10	<2
93J13W	L9800N	9800E	6245	<1	35	45	5	<0.2	<0.02	6	<2
93J13W	L9800N	9840E	6245	<1	25	69	4	<0.2	<0.02	5	<2
test	STD P		6245	13	124	100	97	1.3		70	36
93J13W	L9800N	9880E	6245	<1	30	41	4	<0.2	<0.02	6	<2
93J13W	L9800N	9920E	6245	1	73	72	6	0.3	<0.02	6	<2
93J13W	L9800N	9960E	6245	<1	28	51	4	<0.2	<0.02	6	<2
93J13W	L9800N	10000E	6245	<1	33	44	3	<0.2	<0.02	<2	<2
93J13W	L9800N	10040E	6245	<1	31	48	6	<0.2	<0.02	4	<2
93J13W	L9800N	10080E	6245	<1	53	63	4	0.3	<0.02	9	<2
93J13W	L9800N	10120E	6245	<1	37	52	5	0.4	<0.02	5	<2
93J13W	L9800N	10160E	6245	<1	35	52	3	<0.2	<0.02	2	<2
93J13W	L9800N	10200E	6245	<1	43	62	4	0.5	<0.02	3	<2
test	STD P		6245	14	115	93	97	1.1		70	40
93J13W	L9800N	10240E	6245	1	58	83	8	<0.2	<0.02	4	<2
93J13W	L9800N	10280E	6245	<1	58	90	6	0.4	<0.02	2	<2
93J13W	L9800N	10320E	6245	<1	38	61	6	0.2	<0.02	7	<2
93J13W	L9800N	10360E	6245	<1	41	72	4	0.3	<0.02	2	<2
93J13W	L9800N	10400E	6245	<1	36	56	4	0.2	<0.02	3	<2
93J13W	L9800N	10440E	6245	<1	26	56	3	<0.2	<0.02	<2	<2
93J13W	L9800N	10480E	6245	<1	21	52	5	<0.2	<0.02	7	<2
93J13W	L9800N	10520E	6245	<1	22	53	5	<0.2	<0.02	2	<2
93J13W	L9800N	10560E	6245	<1	27	59	5	<0.2	<0.02	7	<2
93J13W	L9800N	10560E*	6245	<1	27	59	5	<0.2	<0.02	6	<2
93J13W	L9800N	10600E	6245	<1	26	58	6	<0.2	<0.02	3	<2
93J13W	L9800N	10640E	6245	<1	42	91	7	0.3	<0.02	3	<2
93J13W	L9800N	10680E	6245	<1	16	53	7	<0.2	<0.02	2	<2
93J13W	L9800N	10720E	6245	<1	19	57	6	<0.2	<0.02	5	<2
93J13W	L9800N	10760E	6245	<1	23	68	7	<0.2	<0.02	3	<2
93J13W	L9800N	10800E	6245	<1	22	64	4	<0.2	<0.02	5	<2
93J13W	L9900N	9840E	6245	<1	147	40	5	<0.2	<0.02	5	3
93J13W	L9900N	9880E	6245	<1	66	38	6	<0.2	<0.02	2	<2
93J13W	L9900N	9920E	6245	<1	35	34	4	0.4	<0.02	6	<2
93J13W	L9900N	9920E*	6245	<1	33	35	4	0.4	<0.02	6	<2
93J13W	L9900N	9960E	6245	<1	32	45	4	<0.2	<0.02	<2	2
93J13W	L9900N	10000E	6245	<1	37	42	3	0.2	<0.02	4	<2
93J13W	L10000N	9320E	6245	<1	41	62	3	0.3	0.03	5	<2
93J13W	L10000N	9360E	6245	<1	45	62	3	<0.2	<0.02	9	<2
93J13W	L10000N	9400E	6245	<1	30	60	5	<0.2	<0.02	5	<2
93J13W	L10000N	9440E	6245	<1	39	51	5	<0.2	<0.02	7	<2
93J13W	L10000N	9480E	6245	<1	404	45	4	<0.2	<0.02	4	<2
93J13W	L10000N	9520E	6245	<1	57	53	5	<0.2	<0.02	5	<2
93J13W	L10000N	9600E	6245	<1	27	53	5	<0.2	<0.02	4	<2
test	STD P		6245	14	118	87	95	1.4		63	40
93J13W	L10000N	9640E	6245	<1	17	55	5	0.4	<0.02	<2	<2
93J13W	L10000N	9680E	6245	<1	60	53	7	<0.2	<0.02	5	<2
93J13W	L10000N	9720E	6245	<1	26	64	7	<0.2	<0.02	2	<2
93J13W	L10000N	9760E	6245	<1	34	54	7	<0.2	<0.02	6	<2
93J13W	L10000N	9800E	6245	<1	88	55	5	<0.2	<0.02	8	<2
93J13W	L10000N	9840E	6245	<1	234	49	8	<0.2	<0.02	<2	<2
93J13W	L10000N	9880E	6245	<1	313	55	6	<0.2	<0.02	5	<2
93J13W	L10000N	9920E	6245	<1	240	64	4	<0.2	<0.02	2	<2
93J13W	L10000N	9960E	6245	<1	44	74	4	0.3	<0.02	5	<2
93J13W	L10000N	9960E*	6245	<1	46	73	5	0.2	<0.02	2	<2

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GRID	SAMPLE		PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L10000N	10000E	6245	<1	35	70	6	0.4	<0.02	<2	<2
93J13W	L10000N	10040E	6245	<1	78	49	7	0.4	<0.02	2	<2
93J13W	L10000N	10080E	6245	<1	49	80	6	0.3	<0.02	5	<2
93J13W	L10000N	10120E	6245	<1	74	48	5	0.3	0.02	12	<2
93J13W	L10000N	10160E	6245	<1	67	56	5	0.3	<0.02	5	<2
93J13W	L10000N	10200E	6245	<1	34	54	5	<0.2	<0.02	<2	<2
93J13W	L10000N	10240E	6245	<1	50	65	5	0.4	<0.02	<2	<2
93J13W	L10000N	10280E	6245	<1	41	61	3	0.3	0.03	3	<2
93J13W	L10000N	10320E	6245	<1	42	59	4	<0.2	<0.02	7	<2
test	STD P		6245	13	130	96	97	1.3		68	45
93J13W	L10000N	10360E	6245	<1	32	60	7	<0.2	<0.02	3	<2
93J13W	L10000N	10400E	6245	<1	34	70	5	<0.2	<0.02	3	<2
93J13W	L10000N	10440E	6245	<1	36	57	4	<0.2	<0.02	5	<2
93J13W	L10000N	10480E	6245	<1	85	87	6	1.0	<0.02	5	<2
93J13W	L10000N	10520E	6245	<1	36	61	7	0.3	<0.02	2	<2
93J13W	L10000N	10560E	6245	<1	35	48	6	0.3	0.11	3	<2
93J13W	L10000N	10600E	6245	<1	38	71	6	<0.2	<0.02	<2	<2
93J13W	L10000N	10640E	6245	<1	49	81	5	0.3	<0.02	4	<2
93J13W	L10000N	10680E	6245	<1	34	56	4	0.4	<0.02	4	<2
93J13W	L10000N	10680E *	6245	<1	36	55	4	0.5	<0.02	6	<2
93J13W	L10000N	10720E	6245	1	37	73	3	0.9	<0.02	3	<2
93J13W	L10000N	10760E	6245	1	33	65	4	0.3	<0.02	8	<2
93J13W	L10000N	10800E	6245	1	46	70	4	0.7	<0.02	5	<2
93J13W	L10100N	9320E	6245	1	41	62	4	<0.2	<0.02	5	<2
93J13W	L10100N	9360E	6245	<1	34	63	5	<0.2	<0.02	2	<2
93J13W	L10100N	9400E	6245	1	31	64	5	<0.2	<0.02	<2	<2
93J13W	L10100N	9440E	6245	<1	35	70	6	<0.2	<0.02	6	<2
93J13W	L10100N	9480E	6245	<1	32	98	4	<0.2	<0.02	7	<2
93J13W	L10100N	9520E	6245	<1	28	68	5	<0.2	<0.02	4	<2
test	STD P		6245	13	118	99	98	1.0		70	44
93J13W	L10100N	9560E	6245	1	57	46	4	<0.2	<0.02	<2	<2
93J13W	L10100N	9600E	6245	<1	154	65	6	<0.2	<0.02	4	<2
93J13W	L10100N	9640E	6245	1	820	76	4	<0.2	0.03	8	<2
93J13W	L10100N	9680E	6245	1	38	59	5	<0.2	<0.02	3	<2
93J13W	L10100N	9720E	6245	<1	790	55	8	<0.2	0.08	11	<2
93J13W	L10100N	9800E	6245	<1	29	60	4	<0.2	<0.02	3	<2
93J13W	L10100N	9840E	6245	<1	25	51	3	<0.2	<0.02	5	<2
93J13W	L10100N	9880E	6245	1	63	56	5	<0.2	<0.02	3	<2
93J13W	L10100N	9920E	6245	1	30	45	5	<0.2	<0.02	5	<2
93J13W	L10100N	9920E *	6245	1	30	48	3	<0.2	<0.02	3	<2
93J13W	L10100N	9960E	6245	2	120	43	4	0.3	<0.02	<2	<2
93J13W	L10100N	10000E	6245	7	186	45	4	<0.2	<0.02	6	<2
93J13W	L10200N	9440E	6245	1	45	44	4	<0.2	<0.02	5	<2
93J13W	L10200N	9480E	6245	1	49	45	5	<0.2	<0.02	5	<2
93J13W	L10200N	9640E	6245	<1	160	77	7	<0.2	<0.02	15	<2
93J13W	L10200N	9760E	6245	1	38	56	3	<0.2	<0.02	3	<2
93J13W	L10200N	9800E	6245	1	53	50	4	<0.2	<0.02	3	<2
93J13W	L10200N	9840E	6245	1	66	91	5	<0.2	0.03	7	<2
93J13W	L10200N	9880E	6245	1	133	101	7	<0.2	<0.02	7	<2
93J13W	L10200N	9880E *	6245	1	130	96	7	<0.2	<0.02	7	<2
93J13W	L10200N	9920E	6245	2	70	53	5	<0.2	<0.02	5	<2
93J13W	L10200N	10000E	6245	1	83	108	31	0.4	<0.02	5	<2
93J13W	L10200N	10040E	6245	<1	40	42	3	<0.2	<0.02	7	<2
93J13W	L10200N	10080E	6245	<1	32	37	3	<0.2	<0.02	4	<2
93J13W	L10200N	10120E	6245	<1	44	42	4	<0.2	<0.02	9	<2
93J13W	L10200N	10160E	6245	<1	24	31	4	<0.2	<0.02	6	<2
93J13W	L10200N	10200E	6245	<1	54	41	3	<0.2	<0.02	15	<2
93J13W	L10200N	10240E	6245	<1	32	45	3	<0.2	<0.02	3	<2
93J13W	L10200N	10280E	6245	1	38	38	3	<0.2	<0.02	7	<2
test	STD P		6245	13	123	94	104	1.0		60	40

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GRID	SAMPLE		PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L10200N	10320E	6245	<1	56	40	5	<0.2	<0.02	8	<2
93J13W	L10200N	10360E	6245	<1	53	43	5	<0.2	<0.02	8	<2
93J13W	L10200N	10400E	6245	<1	36	53	5	<0.2	<0.02	7	<2
93J13W	L10200N	10440E	6245	<1	27	34	4	<0.2	<0.02	5	<2
93J13W	L10200N	10480E	6245	1	37	47	4	<0.2	<0.02	9	<2
93J13W	L10200N	10520E	6245	1	50	53	4	<0.2	<0.02	7	<2
93J13W	L10200N	10560E	6245	<1	53	60	4	<0.2	<0.02	3	<2
93J13W	L10200N	10600E	6245	<1	38	45	4	<0.2	<0.02	4	<2
93J13W	L10200N	10640E	6245	<1	59	50	5	<0.2	<0.02	8	<2
93J13W	L10200N	10640E•	6245	<1	59	49	4	<0.2	<0.02	9	<2
93J13W	L10200N	10680E	6245	<1	42	58	6	<0.2	<0.02	<2	<2
93J13W	L10200N	10720E	6245	<1	47	70	5	<0.2	0.06	<2	<2
93J13W	L10200N	10760E	6245	<1	68	85	5	<0.2	<0.02	4	<2
93J13W	L10200N	10800E	6245	<1	34	70	5	<0.2	<0.02	<2	<2
93J13W	L10300N	9720E	6245	<1	210	69	5	0.3	<0.02	5	<2
93J13W	L10300N	9760E	6245	1	177	53	6	0.5	<0.02	<2	<2
93J13W	L10300N	9800E	6245	1	90	70	6	<0.2	<0.02	2	<2
93J13W	L10300N	9840E	6245	<1	34	94	7	0.2	<0.02	<2	<2
93J13W	L10300N	9880E	6245	<1	33	80	7	0.2	<0.02	8	<2
test	STD P		6245	12	124	100	108	1.3		70	38
93J13W	L10300N	9920E	6245	<1	42	56	3	<0.2	<0.02	<2	<2
93J13W	L10300N	9960E	6245	<1	52	43	3	<0.2	<0.02	7	<2
93J13W	L10300N	10000E	6245	<1	69	45	5	<0.2	<0.02	9	<2
93J13W	L10400N	9600E	6245	1	139	63	6	0.3	<0.02	5	<2
93J13W	L10400N	9620E	6245	<1	72	55	6	0.3	<0.02	<2	<2
93J13W	L10400N	9640E	6245	<1	132	66	5	<0.2	<0.02	6	<2
93J13W	L10400N	9680E	6245	<1	52	64	5	<0.2	0.10	<2	<2
93J13W	L10400N	9720E	6245	<1	57	83	4	<0.2	<0.02	2	<2
93J13W	L10400N	9760E	6245	<1	150	56	4	<0.2	<0.02	<2	<2
test	STD P		6245	12	130	99	105	1.2		70	38
93J13W	L10400N	9800E	6245	<1	77	52	10	<0.2	<0.02	<2	<2
93J13W	L10400N	9920E	6245	5	156	59	7	<0.2	<0.02	5	<2
93J13W	L10400N	9960E	6245	4	580	58	6	<0.2	<0.02	8	<2
93J13W	L10400N	10000E	6245	1	109	48	5	0.2	<0.02	6	<2
93J13W	L10400N	10040E	6245	1	161	49	4	<0.2	<0.02	3	<2
93J13W	L10400N	10080E	6245	<1	52	74	4	<0.2	<0.02	<2	<2
93J13W	L10400N	10120E	6245	<1	36	40	6	<0.2	<0.02	<2	<2
93J13W	L10400N	10160E	6245	<1	70	76	4	<0.2	<0.02	4	<2
93J13W	L10400N	10200E	6245	<1	103	45	4	<0.2	<0.02	23	<2
93J13W	L10400N	10200E•	6245	<1	110	47	4	<0.2	<0.02	22	<2
93J13W	L10400N	10240E	6245	<1	96	63	4	<0.2	0.02	27	<2
93J13W	L10400N	10280E	6245	1	51	73	3	<0.2	<0.02	12	<2
93J13W	L10400N	10320E	6245	<1	36	55	4	<0.2	<0.02	4	<2
93J13W	L10400N	10360E	6245	1	45	54	4	<0.2	<0.02	5	<2
93J13W	L10400N	10400E	6245	<1	53	60	3	<0.2	<0.02	<2	<2
93J13W	L10400N	10440E	6245	1	40	45	4	<0.2	<0.02	<2	<2
93J13W	L10400N	10480E	6245	<1	39	56	3	<0.2	<0.02	4	<2
93J13W	L10400N	10520E	6245	<1	35	46	3	<0.2	<0.02	6	<2
93J13W	L10400N	10560E	6245	<1	49	53	4	<0.2	<0.02	6	<2
93J13W	L10400N	10560E*	6245	<1	48	53	4	<0.2	<0.02	7	<2
93J13W	L10400N	10600E	6245	1	49	44	5	<0.2	<0.02	8	<2
93J13W	L10400N	10640E	6245	<1	45	50	4	<0.2	<0.02	5	<2
93J13W	L10400N	10680E	6245	<1	42	61	4	<0.2	<0.02	<2	<2
93J13W	L10400N	10720E	6245	1	46	68	4	<0.2	<0.02	2	2
93J13W	L10400N	10760E	6245	<1	37	52	2	<0.2	<0.02	3	<2
93J13W	L10400N	10800E	6245	<1	37	47	2	<0.2	<0.02	3	<2
93J13W	L10500N	9520E	6245	<1	88	66	4	0.2	<0.02	7	<2
93J13W	L10500N	9560E	6245	<1	82	55	5	<0.2	<0.02	5	<2
93J13W	L10500N	9600E	6245	<1	64	47	2	<0.2	<0.02	3	<2
test	STD P		6245	13	130	89	97	1.4		62	45

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GRID	SAMPLE		PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L10500N	9640E	6245	1	56	43	3	0.2	0.17	3	<2
93J13W	L10500N	9680E	6245	1	62	82	4	0.2	<0.02	8	<2
93J13W	L10500N	9720E	6245	<1	115	74	5	0.2	<0.02	<2	2
93J13W	L10500N	9760E	6245	<1	170	68	6	0.2	<0.02	<2	<2
93J13W	L10500N	9800E	6245	<1	132	69	6	0.2	<0.02	<2	<2
93J13W	L10500N	9840E	6245	1	80	49	3	0.2	<0.02	3	<2
93J13W	L10500N	9880E	6245	<1	91	47	3	<0.2	<0.02	<2	<2
93J13W	L10500N	9920E	6245	<1	99	54	4	<0.2	<0.02	<2	2
93J13W	L10500N	10000E	6245	<1	163	49	4	<0.2	0.02	<2	<2
93J13W	L10500N	10000E *	6245	<1	160	46	2	0.2	NSS	<2	<2
93J13W	L10500N	10040E	6245	<1	60	76	6	0.2	<0.02	<2	<2
93J13W	L10500N	10080E	6245	<1	71	61	7	<0.2	<0.02	<2	<2
93J13W	L10500N	10120E	6245	1	60	47	8	<0.2	0.11	3	<2
93J13W	L10500N	10160E	6245	1	111	60	7	<0.2	<0.02	<2	<2
93J13W	L10500N	10200E	6245	1	118	46	6	0.4	<0.02	52	<2
93J13W	L10500N	10240E	6245	1	78	49	6	0.3	0.03	9	<2
93J13W	L10500N	10280E	6245	1	113	52	6	0.3	0.10	10	<2
93J13W	L10500N	10320E	6245	1	63	63	3	0.2	0.02	9	<2
93J13W	L10500N	10360E	6245	1	43	32	4	<0.2	0.03	4	<2
test	STD P		6245	12	130	88	99	1.4		60	40
93J13W	L10500N	10400E	6245	<1	47	48	7	<0.2	<0.02	4	<2
93J13W	L10600N	9520E	6245	<1	50	8	7	0.2	<0.02	3	<2
93J13W	L10600N	9560E	6245	<1	58	94	6	0.3	<0.02	2	<2
93J13W	L10600N	9600E	6245	<1	47	51	5	0.2	0.11	<2	<2
93J13W	L10600N	9640E	6245	<1	60	52	4	<0.2	<0.02	<2	<2
93J13W	L10600N	9680E	6245	<1	70	51	3	<0.2	<0.02	3	<2
93J13W	L10600N	9720E	6245	<1	373	100	9	<0.2	0.03	6	<2
93J13W	L10600N	9760E	6245	<1	193	70	7	0.2	<0.02	<2	2
93J13W	L10600N	9800E	6245	<1	158	65	5	0.3	0.18	2	<2
93J13W	L10600N	9800E ●	6245	<1	154	62	5	0.2	0.02	2	<2
93J13W	L10600N	9840E	6245	<1	133	72	5	<0.2	<0.02	<2	<2
93J13W	L10600N	9880E	6245	<1	140	66	5	0.2	<0.02	<2	<2
93J13W	L10600N	9920E	6245	<1	260	93	6	0.4	<0.02	4	<2
93J13W	L10600N	9960E	6245	<1	112	75	6	0.3	<0.02	2	<2
93J13W	L10600N	10000E	6245	<1	95	50	3	0.2	<0.02	2	<2
93J13W	L10600N	10040E	6245	<1	60	81	4	<0.2	<0.02	4	<2
93J13W	L10600N	10080E	6245	<1	65	85	4	0.2	<0.02	8	<2
93J13W	L10600N	10120E	6245	<1	92	88	4	0.3	<0.02	12	2
93J13W	L10600N	10160E	6245	<1	68	61	6	<0.2	0.02	120	<2
93J13W	L10600N	10160E *	6245	<1	68	58	5	<0.2	0.03	126	<2
93J13W	L10600N	10200E	6245	<1	79	57	6	<0.2	<0.02	17	<2
93J13W	L10600N	10240E	6245	<1	51	47	20	<0.2	<0.02	21	<2
93J13W	L10600N	10280E	6245	<1	47	57	6	<0.2	<0.02	12	<2
93J13W	L10600N	10320E	6245	<1	63	45	4	<0.2	<0.02	2	<2
93J13W	L10600N	10360E	6245	<1	48	56	4	<0.2	<0.02	5	<2
93J13W	L10600N	10400E	6245	<1	55	60	3	0.2	<0.02	5	<2
93J13W	L10600N	10440E	6245	<1	42	52	4	<0.2	<0.02	<2	<2
93J13W	L10600N	10480E	6245	<1	40	49	3	<0.2	0.19	<2	<2
93J13W	L10600N	10520E	6245	<1	46	45	4	0.2	<0.02	<2	<2
test	STD P		6245	12	126	87	100	1.1		56	40
93J13W	L10600N	10560E	6245	<1	35	49	5	0.2	<0.02	<2	<2
93J13W	L10600N	10600E	6245	<1	39	58	6	<0.2	0.03	<2	<2
93J13W	L10600N	10640E	6245	<1	40	62	5	0.4	<0.02	<2	<2
93J13W	L10600N	10680E	6245	<1	42	56	5	<0.2	<0.02	<2	<2
93J13W	L10600N	10720E	6245	<1	30	56	5	<0.2	<0.02	3	<2
93J13W	L10600N	10760E	6245	<1	60	82	6	<0.2	<0.02	<2	<2
93J13W	L10600N	10800E	6245	<1	70	60	3	<0.2	<0.02	<2	<2
93J13W	L10700N	10000E	6245	<1	40	68	5	<0.2	<0.02	<2	<2
93J13W	L10700N	10040E	6245	<1	95	70	3	<0.2	<0.02	<2	<2
test	STD P		6245	12		99	98			57	38

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PLACER GEOCHEM ASSAY SYSTEM: DATA FROM V216 WINDY DATE

GRID	SAMPLE		PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L10700N	10080E	6245	2	62	48	5	<0.2	<0.02	<2	<2
93J13W	L10700N	10120E	6245	1	46	49	4	<0.2	<0.02	5	<2
93J13W	L10700N	10160E	6245	1	41	45	5	<0.2	<0.02	2	2
93J13W	L10700N	10200E	6245	1	60	50	6	0.3	0.02	16	<2
93J13W	L10700N	10240E	6245	<1	40	50	4	0.4	<0.02	14	<2
93J13W	L10700N	10280E	6245	<1	51	61	6	0.5	<0.02	30	<2
93J13W	L10700N	10320E	6245	1	40	46	6	<0.2	<0.02	2	<2
93J13W	L10700N	10360E	6245	1	70	55	6	<0.2	<0.02	5	<2
93J13W	L10700N	10400E	6245	1	44	54	6	<0.2	<0.02	<2	<2
test	STD P		6245	13	114	94	100	1.8		55	39
93J13W	L10800N	9520E	6245	1	46	73	6	<0.2	<0.02	<2	<2
93J13W	L10800N	9560E	6245	1	90	72	6	0.2	<0.02	<2	<2
93J13W	L10800N	9600E	6245	1	90	68	5	0.3	<0.02	<2	<2
93J13W	L10800N	9640E	6245	1	32	59	4	<0.2	<0.02	<2	<2
93J13W	L10800N	9680E	6245	1	45	52	3	<0.2	<0.02	<2	<2
93J13W	L10800N	9720E	6245	1	44	52	3	<0.2	0.02	3	<2
93J13W	L10800N	9760E	6245	1	57	58	3	<0.2	0.07	<2	<2
93J13W	L10800N	9800E	6245	1	94	60	4	<0.2	0.02	4	<2
93J13W	L10800N	9840E	6245	2	193	80	5	<0.2	<0.02	<2	<2
test	STD P		6245	12	135	87	100	1.8		62	42
93J13W	L10800N	9880E	6245	1	99	65	4	<0.2	<0.02	<2	<2
93J13W	L10800N	9920E	6245	1	147	78	6	<0.2	<0.02	<2	<2
93J13W	L10800N	9960E	6245	1	98	60	6	<0.2	<0.02	<2	<2
93J13W	L10800N	10000E	6245	<1	68	46	4	<0.2	<0.02	<2	<2
93J13W	L10800N	10040E	6245	2	61	43	6	<0.2	<0.02	<2	<2
93J13W	L10800N	10080E	6245	<1	58	46	4	<0.2	<0.02	4	<2
93J13W	L10800N	10120E	6245	1	58	60	6	<0.2	<0.02	9	<2
93J13W	L10800N	10160E	6245	2	136	65	5	<0.2	<0.02	17	<2
93J13W	L10800N	10200E	6245	2	66	46	5	<0.2	<0.02	17	<2
93J13W	L10800N	10200E*	6245	1	65	46	4	<0.2	<0.02	15	<2
93J13W	L10800N	10240E	6245	1	88	43	6	<0.2	<0.02	12	<2
93J13W	L10800N	10280E	6245	2	41	46	5	<0.2	<0.02	<2	<2
93J13W	L10800N	10320E	6245	1	41	41	6	<0.2	<0.02	<2	<2
93J13W	L10800N	10360E	6245	1	47	53	5	<0.2	<0.02	5	<2
93J13W	L10800N	10400E	6245	2	50	60	6	<0.2	<0.02	4	<2
93J13W	L10800N	10440E	6245	1	44	54	6	<0.2	<0.02	<2	<2
93J13W	L10800N	10480E	6245	1	42	43	5	<0.2	<0.02	<2	<2
93J13W	L10800N	10520E	6245	2	38	51	7	<0.2	0.08	<2	<2
93J13W	L10800N	10560E	6245	2	29	41	5	<0.2	<0.02	<2	<2
93J13W	L10800N	10560E*	6245	2	28	42	5	<0.2	<0.02	<2	<2
93J13W	L10800N	10600E	6245	1	28	40	6	0.4	<0.02	2	<2
93J13W	L10800N	10640E	6245	1	29	43	4	0.3	<0.02	<2	<2
93J13W	L10800N	10680E	6245	1	35	49	5	0.2	<0.02	<2	<2
93J13W	L10800N	10720E	6245	1	38	63	5	0.2	<0.02	5	<2
93J13W	L10800N	10760E	6245	1	27	54	4	0.2	<0.02	3	<2
93J13W	L10800N	10800E	6245	1	37	66	3	0.2	<0.02	<2	<2
93J13W	L10900N	10000E	6245	1	66	38	3	<0.2	<0.02	<2	<2
93J13W	L10900N	10040E	6245	<1	38	47	2	0.2	<0.02	<2	<2
93J13W	L10900N	10080E	6245	1	50	56	4	0.2	<0.02	3	5
test	STD P		6245	14	118	90	100	1.3		58	43
93J13W	L10900N	10120E	6245	<1	65	46	4	0.2	<0.02	4	<2
93J13W	L10900N	10160E	6245	1	57	80	3	<0.2	<0.02	12	<2
93J13W	L10900N	10200E	6245	1	47	50	3	0.3	<0.02	14	<2
93J13W	L10900N	10240E	6245	1	79	49	4	0.2	<0.02	40	<2
93J13W	L10900N	10280E	6245	1	45	48	3	<0.2	<0.02	13	<2
93J13W	L10900N	10320E	6245	1	43	43	5	<0.2	<0.02	<2	<2
93J13W	L10900N	10360E	6245	1	69	55	4	0.2	<0.02	14	<2
93J13W	L10900N	10400E	6245	1	90	83	5	0.2	<0.02	4	<2
93J13W	L10900N	10400E*	6245	1	91	80	5	0.2	<0.02	3	<2
test	STD AU		6245						0.33		

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GRID	SAMPLE		PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L1100N	9520E	6246	<1	35	72	8	<0.2	<0.02	3	<2
93J13W	L1100N	9560E	6246	<1	65	80	9	0.5	<0.02	4	3
93J13W	L1100N	9600E	6246	1	46	74	7	0.2	<0.02	6	4
93J13W	L1100N	9640E	6246	<1	33	57	5	<0.2	<0.02	4	<2
93J13W	L1100N	9680E	6246	<1	33	46	4	<0.2	<0.02	4	6
93J13W	L1100N	9720E	6246	1	26	45	4	<0.2	<0.02	<2	5
93J13W	L1100N	9760E	6246	1	38	38	4	<0.2	0.08	5	5
93J13W	L1100N	9800E	6246	<1	66	48	3	<0.2	<0.02	3	<2
93J13W	L1100N	9840E	6246	<1	56	38	5	<0.2	<0.02	8	4
test	STD P		6246	12	126	89	92	1.2		69-	40
93J13W	L1100N	9880E	6246	<1	68	62	8	<0.2	<0.02	10	4
93J13W	L1100N	9920E	6246	<1	61	37	5	<0.2	<0.02	5	2
93J13W	L1100N	9960E	6246	<1	53	91	6	<0.2	<0.02	5	3
93J13W	L1100N	10000E	6246	1	72	42	5	<0.2	<0.02	19	2
93J13W	L1100N	10040E	6246	<1	75	42	6	<0.2	<0.02	11	5
93J13W	L1100N	10080E	6246	<1	81	48	7	<0.2	<0.02	<2	5
93J13W	L1100N	10120E	6246	<1	73	39	6	<0.2	<0.02	<2	<2
93J13W	L1100N	10160E	6246	<1	43	26	5	<0.2	<0.02	<2	<2
93J13W	L1100N	10200E	6246	<1	49	29	6	<0.2	<0.02	2	3
test	STD P		6246	12	124	89	97	1.5		65	37
93J13W	L1100N	10240E	6246	<1	46	49	7	<0.2	<0.02	5	2
93J13W	L1100N	10280E	6246	<1	42	45	5	0.2	<0.02	13	<2
93J13W	L1100N	10320E	6246	1	99	43	6	<0.2	<0.02	25	2
93J13W	L1100N	10360E	6246	<1	90	61	6	0.3	<0.02	19	<2
93J13W	L1100N	10400E	6246	<1	87	65	7	<0.2	<0.02	13	<2
93J13W	L1100N	10440E	6246	1	49	52	6	<0.2	<0.02	10	<2
93J13W	L1100N	10480E	6246	1	38	51	6	<0.2	<0.02	12	<2
93J13W	L1100N	10520E	6246	<1	34	44	4	0.2	<0.02	6	<2
93J13W	L1100N	10560E	6246	<1	33	46	5	0.2	0.05	5	<2
93J13W	L1100N	10560E*	6246	<1	33	46	6	0.2	<0.02	5	<2
93J13W	L1100N	10600E	6246	<1	42	48	6	0.2	<0.02	7	<2
93J13W	L1100N	10640E	6246	<1	34	43	4	0.2	<0.02	4	3
93J13W	L1100N	10680E	6246	<1	32	49	5	0.2	<0.02	<2	4
93J13W	L1100N	10720E	6246	<1	37	59	7	<0.2	<0.02	9	2
93J13W	L1100N	10760E	6246	<1	39	63	4	0.5	<0.02	3	<2
93J13W	L1100N	10800E	6246	1	50	67	5	<0.2	<0.02	8	<2
93J13W	L11200N	9480E	6246	<1	41	58	6	<0.2	<0.02	<2	<2
93J13W	L11200N	9520E	6246	<1	35	75	6	0.3	<0.02	5	<2
93J13W	L11200N	9560E	6246	<1	29	54	6	0.2	<0.02	4	2
93J13W	L11200N	9560E*	6246	<1	29	52	4	0.4	<0.02	5	2
93J13W	L11200N	9600E	6246	<1	110	35	6	<0.2	0.02	10	<2
93J13W	L11200N	9640E	6246	<1	30	39	5	0.2	<0.02	4	6
93J13W	L11200N	9680E	6246	<1	41	58	4	<0.2	<0.02	4	2
93J13W	L11200N	9720E	6246	1	35	36	6	<0.2	<0.02	10	4
93J13W	L11200N	9760E	6246	1	60	68	7	<0.2	0.03	8	4
93J13W	L11200N	9800E	6246	1	50	45	5	<0.2	<0.02	3	2
93J13W	L11200N	9840E	6246	1	50	49	5	<0.2	0.08	5	2
93J13W	L11200N	9880E	6246	1	54	47	5	<0.2	<0.02	9	5
93J13W	L11200N	9920E	6246	1	49	44	4	<0.2	<0.02	4	3
test	STD P		6246	13	130	87	93	1.3		68-	45
93J13W	L11200N	9960E	6246	1	49	35	5	<0.2	0.03	6	<2
93J13W	L11200N	10000E	6246	1	73	48	4	<0.2	<0.02	9	<2
93J13W	L11200N	10040E	6246	2	87	42	4	<0.2	<0.02	11	<2
93J13W	L11200N	10080E	6246	1	74	57	4	<0.2	<0.02	4	5
93J13W	L11200N	10120E	6246	1	69	55	5	<0.2	0.02	8	3
93J13W	L11200N	10160E	6246	1	83	61	4	<0.2	<0.02	7	<2
93J13W	L11200N	10200E	6246	1	62	57	4	<0.2	<0.02	7	2
93J13W	L11200N	10240E	6246	1	92	41	4	<0.2	<0.02	4	3
93J13W	L11200N	10280E	6246	1	43	50	4	<0.2	<0.02	12	4
93J13W	L11200N	10280E*	6246	1	43	49	3	<0.2	<0.02	9	2

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GRID	SAMPLE		PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L11200N	10320E	6246	1	75	51	5	<0.2	0.03	13	2
93J13W	L11200N	10360E	6246	2	65	53	4	0.2	0.03	13	<2
93J13W	L11200N	10400E	6246	1	71	55	5	<0.2	<0.02	7	<2
93J13W	L11200N	10440E	6246	1	102	71	7	0.4	<0.02	22	3
93J13W	L11200N	10480E	6246	1	73	45	3	<0.2	<0.02	20	<2
93J13W	L11200N	10560E	6246	1	87	78	4	0.2	<0.02	20	<2
93J13W	L11200N	10760E	6246	1	61	71	6	<0.2	<0.02	7	5
93J13W	L11200N	10800E	6246	1	84	79	6	<0.2	<0.02	9	<2
93J13W	L11400N	9520E	6246	1	31	46	4	<0.2	0.05	2	2
test	STD P		6246	13	120	102	96	1.3		60	46
93J13W	L11400N	9560E	6246	1	33	45	4	<0.2	<0.02	9	<2
93J13W	L11400N	9600E	6246	<1	38	49	4	<0.2	<0.02	6	<2
93J13W	L11400N	9640E	6246	<1	31	47	4	<0.2	0.04	6	5
93J13W	L11400N	9680E	6246	<1	117	54	4	<0.2	0.03	14	4
93J13W	L11400N	9720E	6246	<1	46	53	4	<0.2	<0.02	4	2
93J13W	L11400N	9760E	6246	<1	23	40	4	0.2	0.06	4	<2
93J13W	L11400N	9800E	6246	<1	37	36	3	0.2	0.02	5	2
93J13W	L11400N	9840E	6246	<1	30	41	4	0.2	0.05	6	<2
93J13W	L11400N	9880E	6246	1	48	51	5	<0.2	<0.02	7	<2
93J13W	L11400N	9880E*	6246	1	47	49	5	<0.2	<0.02	7	<2
93J13W	L11400N	9920E	6246	<1	40	35	6	0.3	<0.02	8	<2
93J13W	L11400N	9960E	6246	1	47	43	8	0.2	<0.02	2	<2
93J13W	L11400N	10000E	6246	2	77	49	5	0.2	<0.02	9	2
93J13W	L11400N	10040E	6246	2	73	51	5	0.3	<0.02	5	<2
93J13W	L11400N	10080E	6246	2	139	65	5	0.4	<0.02	12	<2
93J13W	L11400N	10120E	6246	2	73	55	6	<0.2	<0.02	14	<2
93J13W	L11400N	10160E	6246	1	69	53	7	<0.2	<0.02	12	<2
93J13W	L11400N	10200E	6246	1	92	56	5	<0.2	<0.02	6	2
93J13W	L11400N	10240E	6246	1	66	35	6	<0.2	<0.02	3	<2
test	STD P		6246	13	124	90	8	1.4		57	44
93J13W	L11400N	10280E	6246	1	54	30	5	<0.2	0.26	3	<2
93J13W	L11400N	10320E	6246	1	61	38	4	<0.2	<0.02	7	<2
93J13W	L11400N	10360E	6246	1	74	49	6	<0.2	0.29	12	<2
93J13W	L11400N	10400E	6246	<1	48	49	5	<0.2	<0.02	9	3
93J13W	L11400N	10440E	6246	1	50	48	4	<0.2	<0.02	19	<2
93J13W	L11400N	10480E	6246	1	43	44	3	<0.2	0.02	15	<2
93J13W	L11400N	10520E	6246	1	70	47	6	<0.2	<0.02	19	2
93J13W	L11400N	10560E	6246	1	31	43	4	<0.2	<0.02	8	<2
93J13W	L11400N	10600E	6246	1	68	57	4	<0.2	<0.02	13	<2
93J13W	L11400N	10600E*	6246	1	71	59	3	<0.2	<0.02	10	<2
93J13W	L11400N	10640E	6246	1	67	57	3	0.4	<0.02	11	<2
93J13W	L11400N	10680E	6246	1	62	58	4	0.2	<0.02	7	<2
93J13W	L11400N	10720E	6246	1	79	64	4	0.4	<0.02	3	<2
93J13W	L11400N	10760E	6246	<1	46	53	3	<0.2	<0.02	7	2
93J13W	L11400N	10800E	6246	<1	37	62	3	<0.2	<0.02	4	3
93J13W	L11600N	9920E	6246	<1	44	46	3	0.3	<0.02	4	2
93J13W	L11600N	9960E	6246	1	42	36	6	0.2	0.04	8	<2
93J13W	L11600N	10000E	6246	<1	104	50	4	0.2	<0.02	9	<2
93J13W	L11600N	10040E	6246	<1	63	60	3	<0.2	0.02	2	2
93J13W	L11600N	10040E*	6246	<1	62	61	4	<0.2	<0.02	4	2
93J13W	L11600N	10080E	6246	2	183	79	6	0.4	<0.02	5	3
93J13W	L11600N	10120E	6246	1	91	64	6	0.2	0.03	12	<2
93J13W	L11600N	10160E	6246	<1	86	60	5	0.2	<0.02	14	<2
93J13W	L11600N	10200E	6246	1	79	54	6	<0.2	<0.02	6	5
93J13W	L11600N	10240E	6246	1	71	60	5	0.2	<0.02	8	<2
93J13W	L11600N	10280E	6246	1	178	63	5	0.4	<0.02	8	<2
93J13W	L11600N	10280EB	6246	1	102	46	4	<0.2	<0.02	2	4
93J13W	L11600N	10320E	6246	2	108	73	7	0.3	<0.02	7	<2
93J13W	L11600N	10360E	6246	1	55	55	5	0.2	<0.02	10	<2
test	STD P		6246	12	118	90	99	1.3		60	46

PLACER GEOCHEM ASSAY SYSTEM: DATA FROM V216 WINDY DATE:

GRID	SAMPLE	PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L11600N 10400E	6246	1	63	49	3	<0.2	0.03	15	<2
93J13W	L11600N 10440E	6246	1	43	50	4	0.2	<0.02	8	2
93J13W	L11600N 10480E	6246	1	64	53	6	<0.2	<0.02	8	<2
93J13W	L11600N 10520E	6246	2	116	69	5	0.2	<0.02	9	<2
93J13W	L11600N 10560E	6246	1	50	56	6	<0.2	<0.02	9	2
93J13W	L11600N 10600E	6246	1	67	65	8	<0.2	<0.02	4	<2
93J13W	L11600N 10640E	6246	2	75	74	6	0.2	<0.02	9	3
93J13W	L11600N 10680E	6246	1	52	89	5	<0.2	0.03	7	<2
93J13W	L11600N 10720E	6246	1	26	72	5	<0.2	<0.02	6	<2
93J13W	L11600N 10720E*	6246	1	24	70	5	<0.2	<0.02	5	<2
93J13W	L11600N 10760E	6246	2	79	96	6	0.3	<0.02	13	2
93J13W	L11600N 10800E	6246	1	50	52	5	0.2	<0.02	7	<2
93J13W	L11650N 9520E	6246	<1	35	54	6	<0.2	<0.02	2	<2
93J13W	L11650N 9560E	6246	1	33	43	6	0.3	<0.02	3	<2
93J13W	L11650N 9600E	6246	1	45	58	5	0.2	<0.02	3	<2
93J13W	L11650N 9640E	6246	2	30	57	5	<0.2	<0.02	2	<2
93J13W	L11650N 9680E	6246	1	35	53	5	<0.2	<0.02	3	<2
93J13W	L11650N 9720E	6246	1	35	45	4	<0.2	<0.02	2	<2
93J13W	L11650N 9760E	6246	1	50	52	4	<0.2	<0.02	5	<2
test	STD P	6246	13	111	95	100	1.0		62	42
93J13W	L11650N 9800E	6246	2	65	70	5	0.2	<0.02	3	<2
93J13W	L11650N 9840E	6246	1	55	67	4	<0.2	<0.02	4	<2
93J13W	L11650N 9840E-A	6246	2	50	53	3	<0.2	<0.02	2	<2
93J13W	L11650N 9880E	6246	1	50	56	3	<0.2	<0.02	4	<2
93J13W	L11800N 9520E	6246	1	36	46	6	<0.2	<0.02	3	<2
93J13W	L11800N 9560E	6246	1	27	56	4	<0.2	<0.02	<2	<2
93J13W	L11800N 9600E	6246	1	47	62	3	<0.2	<0.02	<2	<2
93J13W	L11800N 9640E	6246	1	35	52	3	<0.2	<0.02	5	<2
93J13W	L11800N 9680E	6246	1	30	59	2	<0.2	<0.02	2	<2
test	STD P	6246	12	125	0	90	1.5		69	44
93J13W	L11800N 9720E	6246	<1	40	65	2	0.4	<0.02	<2	<2
93J13W	L11800N 9760E	6246	1	74	78	3	0.4	<0.02	9	<2
93J13W	L11800N 9800E	6246	1	47	56	4	<0.2	<0.02	4	<2
93J13W	L11800N 9840E	6246	1	57	68	4	<0.2	<0.02	2	<2
93J13W	L11800N 9880E	6246	1	72	72	3	0.2	<0.02	4	<2
93J13W	L11800N 9920E	6246	1	44	50	3	0.3	<0.02	3	<2
93J13W	L11800N 9960E	6246	<1	50	41	3	<0.2	<0.02	5	<2
93J13W	L11800N 10000E	6246	<1	35	59	3	<0.2	0.03	3	<2
93J13W	L11800N 10040E	6246	1	90	77	2	<0.2	<0.02	7	<2
93J13W	L11800N 10040E*	6246	1	88	71	2	<0.2	<0.02	6	<2
93J13W	L11800N 10080E	6246	<1	86	92	6	<0.2	<0.02	8	<2
93J13W	L11800N 10120E	6246	<1	65	56	8	<0.2	<0.02	4	<2
93J13W	L11800N 10160E	6246	<1	78	49	6	<0.2	<0.02	7	<2
93J13W	L11800N 10200E	6246	<1	74	53	5	<0.2	<0.02	7	<2
93J13W	L11800N 10240E	6246	<1	75	60	6	<0.2	<0.02	4	<2
93J13W	L11800N 10280E	6246	<1	74	53	4	<0.2	<0.02	4	<2
93J13W	L11800N 10320E	6246	<1	35	62	6	<0.2	<0.02	3	<2
93J13W	L11800N 10360E	6246	<1	59	73	6	<0.2	<0.02	5	<2
93J13W	L11800N 10400E	6246	<1	71	96	6	<0.2	<0.02	6	<2
93J13W	L11800N 10400E*	6246	<1	72	103	6	<0.2	<0.02	4	<2
93J13W	L11800N 10440E	6246	<1	40	109	6	0.2	<0.02	3	<2
93J13W	L11800N 10480E	6246	<1	110	81	6	0.3	<0.02	11	<2
93J13W	L11800N 10520E	6246	<1	40	77	6	<0.2	<0.02	5	<2
93J13W	L11800N 10560E	6246	<1	56	46	4	<0.2	<0.02	10	<2
93J13W	L11800N 10600E	6246	<1	64	48	2	<0.2	<0.02	8	<2
93J13W	L11800N 10640E	6246	<1	54	58	3	<0.2	<0.02	6	<2
93J13W	L11800N 10680E	6246	<1	43	67	5	<0.2	<0.02	8	<2
93J13W	L11800N 10720E	6246	<1	47	59	6	<0.2	<0.02	11	<2
93J13W	L11800N 10760E	6246	<1	78	70	5	<0.2	<0.02	10	<2
test	STD P	6246	13	125	101	95	0.9		60	45

GRID	SAMPLE	PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L11800N 10800E	6246	<1	74	67	7	0.3	<0.02	14	<2
93J13W	L12000N 9520E	6246	<1	25	62	6	0.2	<0.02	<2	<2
93J13W	L12000N 9560E	6246	<1	28	50	6	<0.2	<0.02	<2	<2
93J13W	L12000N 9600E	6246	<1	38	68	5	<0.2	<0.02	3	<2
93J13W	L12000N 9640E	6246	<1	37	64	7	<0.2	<0.02	<2	<2
93J13W	L12000N 9680E	6246	<1	25	57	6	<0.2	<0.02	2	<2
93J13W	L12000N 9720E	6246	<1	62	74	6	0.3	<0.02	4	<2
93J13W	L12000N 9760E	6246	<1	38	70	8	<0.2	<0.02	5	<2
93J13W	L12000N 9800E	6246	<1	44	82	7	<0.2	<0.02	<2	<2
93J13W	L12000N 9800E*	6246	NSS	42	NSS	NSS	<0.2	<0.02	<2	NSS
93J13W	L12000N 9840E	6246	<1	37	60	5	<0.2	<0.02	2	<2
93J13W	L12000N 9880E	6246	<1	33	52	6	<0.2	<0.02	5	<2
93J13W	L12000N 9920E	6246	<1	45	61	6	<0.2	<0.02	5	<2
93J13W	L12000N 9960E	6246	<1	49	53	6	<0.2	<0.02	6	<2
93J13W	L12000N 10000E	6246	<1	90	99	7	<0.2	<0.02	7	<2
93J13W	L12000N 10040E	6246	<1	46	86	8	<0.2	<0.02	4	<2
93J13W	L12000N 10080E	6246	<1	94	73	6	<0.2	<0.02	5	<2
93J13W	L12000N 10120E	6246	<1	78	48	7	<0.2	<0.02	2	<2
93J13W	L12000N 10160E	6246	<1	68	79	8	<0.2	<0.02	<2	<2
test	STD P	6246	13	133	92	110	1.0		69	42
93J13W	L12000N 10200E	6246	<1	131	58	7	0.2	<0.02	2	<2
93J13W	L12010N 10240E	6246	<1	93	64	12	0.2	<0.02	3	<2
93J13W	L12010N 10280E	6246	<1	130	85	7	<0.2	<0.02	<2	<2
93J13W	L12010N 10320E	6246	<1	70	87	8	<0.2	<0.02	<2	<2
93J13W	L12010N 10360E	6246	<1	131	70	9	0.3	0.06	<2	<2
93J13W	L12010N 10400E	6246	<1	122	79	10	0.4	<0.02	3	<2
93J13W	L12010N 10440E	6246	<1	124	70	9	<0.2	<0.02	<2	<2
93J13W	L12010N 10480E	6246	<1	189	63	9	0.2	<0.02	<2	<2
93J13W	L12010N 10520E	6246	<1	101	71	9	0.3	<0.02	6	<2
93J13W	L12010N 10520E*	6246	<1	94	70	10	0.2	<0.02	6	<2
93J13W	L12010N 10560E	6246	<1	53	50	6	<0.2	<0.02	5	<2
93J13W	L12010N 10600E	6246	<1	90	59	6	<0.2	<0.02	6	<2
93J13W	L12010N 10640E	6246	<1	40	64	6	0.3	<0.02	4	<2
93J13W	L12010N 10680E	6246	<1	36	47	7	0.2	<0.02	5	<2
93J13W	L12010N 10720E	6246	<1	51	50	6	<0.2	<0.02	<2	<2
93J13W	L12010N 10760E	6246	<1	62	57	4	<0.2	<0.02	6	<2
93J13W	L12010N 10800E	6246	<1	86	64	4	0.3	<0.02	2	<2
93J13W	L12200N 9520E	6246	<1	42	50	8	<0.2	<0.02	<2	<2
93J13W	L12200N 9560E	6246	<1	43	55	9	<0.2	<0.02	<2	<2
93J13W	L12200N 9560E*	6246	<1	43	58	8	<0.2	<0.02	<2	<2
93J13W	L12200N 9600E	6246	<1	78	99	6	1.0	0.02	<2	<2
93J13W	L12200N 9640E	6246	<1	46	55	6	<0.2	<0.02	<2	<2
93J13W	L12200N 9680E	6246	<1	75	90	7	0.7	<0.02	<2	<2
93J13W	L12200N 9720E	6246	<1	27	57	7	0.3	<0.02	<2	<2
93J13W	L12200N 9760E	6246	<1	27	63	6	0.2	<0.02	<2	<2
93J13W	L12200N 9800E	6246	<1	45	68	7	<0.2	<0.02	<2	<2
93J13W	L12200N 9840E	6246	<1	47	59	7	0.4	<0.02	<2	<2
93J13W	L12200N 9880E	6246	<1	32	51	8	0.2	<0.02	<2	<2
93J13W	L12200N 9920E	6246	<1	34	58	7	<0.2	<0.02	<2	<2
test	STD P	6246	12	130	97	101	1.0		66	42
93J13W	L12200N 9960E	6246	<1	29	45	5	0.2	<0.02	<2	<2
93J13W	L12200N 10000E	6246	<1	35	57	5	<0.2	<0.02	<2	<2
93J13W	L12200N 10040E	6246	<1	59	76	7	0.4	<0.02	<2	<2
93J13W	L12200N 10080E	6246	<1	34	70	6	0.2	<0.02	<2	<2
93J13W	L12200N 10120E	6246	<1	52	60	6	<0.2	<0.02	<2	<2
93J13W	L12200N 10160E	6246	<1	91	60	7	<0.2	<0.02	<2	<2
93J13W	L12200N 10200E	6246	<1	83	70	9	<0.2	0.03	<2	<2
93J13W	L12200N 10240E	6246	<1	78	45	6	<0.2	<0.02	3	<2
93J13W	L12200N 10280E	6246	<1	82	62	8	<0.2	<0.02	<2	<2
test	STD P	6246	12	125	100	111	0.9		61	44

PLACER GEOCHEM ASSAY SYSTEM: DATA FROM V216 WINDY DATE:

GRID	SAMPLE	PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L12200N 10320E	6246	<1	64	50	5	0.2	<0.02	6	<2
93J13W	L12200N 10360E	6246	<1	129	77	4	<0.2	<0.02	9	<2
93J13W	L12200N 10400E	6246	<1	104	83	6	0.2	<0.02	16	<2
93J13W	L12200N 10440E	6246	<1	50	52	6	0.3	<0.02	10	<2
93J13W	L12200N 10480E	6246	<1	52	64	6	0.3	<0.02	7	3
93J13W	L12200N 10520E	6246	<1	61	57	7	<0.2	<0.02	7	3
93J13W	L12200N 10560E	6246	<1	53	61	5	<0.2	<0.02	13	<2
93J13W	L12200N 10600E	6246	<1	34	46	6	<0.2	<0.02	7	3
93J13W	L12200N 10760E	6246	<1	40	45	5	0.2	<0.02	5	2
test	STD P	6246	12	138	98	105	1.5		55	38
93J13W	L12200N 10800E	6246	<1	57	47	7	0.2	<0.02	9	<2
93J13W	L12400N 9520E	6246	<1	42	52	8	0.3	<0.02	41	<2
93J13W	L12400N 9560E	6246	<1	60	102	8	0.2	<0.02	10	<2
93J13W	L12400N 9600E	6246	<1	65	69	10	0.9	<0.02	21	<2
93J13W	L12400N 9640E	6246	<1	32	53	6	0.2	<0.02	6	<2
93J13W	L12400N 9680E	6246	<1	43	70	6	1.3	<0.02	28	3
93J13W	L12400N 9720E	6246	<1	32	50	4	0.3	<0.02	4	<2
93J13W	L12400N 9760E	6246	<1	44	51	6	<0.2	<0.02	3	<2
93J13W	L12400N 9800E	6246	<1	62	58	6	0.3	<0.02	<2	<2
test	STD P	6246	12	109	88	105	1.5		54	39
93J13W	L12400N 9840E	6246	<1	40	47	5	0.2	<0.02	<2	<2
93J13W	L12400N 9880E	6246	<1	68	71	6	0.2	<0.02	28	<2
93J13W	L12400N 9920E	6246	<1	34	60	6	<0.2	<0.02	28	<2
93J13W	L12400N 9960E	6246	<1	34	50	6	<0.2	<0.02	5	<2
93J13W	L12400N 10000E	6246	<1	152	66	6	<0.2	<0.02	73	<2
93J13W	L12400N 10040E	6246	<1	40	60	5	<0.2	<0.02	4	<2
93J13W	L12400N 10080E	6246	<1	58	54	7	0.2	0.10	18	<2
93J13W	L12400N 10120E	6246	<1	43	56	6	<0.2	<0.02	8	<2
93J13W	L12400N 10160E	6246	<1	51	48	7	<0.2	<0.02	8	<2
93J13W	L12400N 10160E*	6246	<1	50	47	6	<0.2	<0.02	6	<2
93J13W	L12400N 10200E	6246	<1	61	49	5	<0.2	<0.02	4	<2
93J13W	L12400N 10240E	6246	<1	59	43	4	<0.2	<0.02	4	<2
93J13W	L12400N 10280E	6246	<1	77	59	4	<0.2	<0.02	5	<2
93J13W	L12400N 10320E	6246	<1	137	50	3	<0.2	<0.02	<2	<2
93J13W	L12400N 10360E	6246	<1	256	76	8	0.3	<0.02	12	<2
93J13W	L12400N 10400E	6246	<1	182	59	6	0.3	<0.02	9	<2
93J13W	L12400N 10440E	6246	<1	106	60	6	<0.2	<0.02	7	<2
93J13W	L12400N 10480E	6246	<1	80	79	4	0.2	0.56	20	<2
93J13W	L12400N 10520E	6246	<1	49	60	5	<0.2	<0.02	7	<2
93J13W	L12400N 10520E*	6246	<1	48	59	5	<0.2	<0.02	6	<2
93J13W	L12400N 10560E	6246	<1	43	53	4	<0.2	<0.02	8	2
93J13W	L12400N 10600E	6246	<1	37	48	4	<0.2	<0.02	9	<2
93J13W	L12400N 10640E	6246	<1	36	50	4	<0.2	<0.02	4	3
93J13W	L12400N 10680E	6246	<1	42	59	5	<0.2	<0.02	6	<2
93J13W	L12400N 10720E	6246	<1	100	123	4	<0.2	<0.02	8	6
93J13W	L12400N 10800E	6246	<1	36	37	5	<0.2	<0.02	5	<2
93J13W	L12600N 9520E	6246	<1	44	50	4	<0.2	<0.02	6	<2
93J13W	L12600N 9560E	6246	<1	73	52	5	<0.2	<0.02	12	4
93J13W	L12600N 9600E	6246	<1	67	83	7	0.2	<0.02	13	2
test	STD P	6246	12	125	93	95	1.0		70	45
93J13W	L12600N 9640E	6246	<1	47	70	5	0.3	<0.02	21	<2
93J13W	L12600N 9680E	6246	<1	129	56	6	0.2	<0.02	11	<2
93J13W	L12600N 9720E	6246	<1	54	56	6	<0.2	<0.02	16	<2
93J13W	L12600N 9760E	6246	<1	66	38	5	0.2	<0.02	18	<2
93J13W	L12600N 9800E	6246	<1	72	45	6	<0.2	<0.02	20	<2
93J13W	L12600N 9840E	6246	<1	94	59	5	0.2	<0.02	17	<2
93J13W	L12600N 9880E	6246	<1	940	60	4	0.7	<0.02	10	<2
93J13W	L12600N 9920E	6246	<1	60	65	5	<0.2	<0.02	6	<2
93J13W	L12600N 9960E	6246	<1	135	89	7	0.2	<0.02	16	3
93J13W	L12600N 9960E*	6246	<1	139	86	7	0.2	<0.02	17	2

PLACER GEOCHEM ASSAY SYSTEM: DATA FROM V216 WINDY

DATE

GRID	SAMPLE		PROJECT	MO	CU	ZN	PB	AG	AU	AS	SB
93J13W	L12600N	10000E	6246	<1	33	49	6	0.2	<0.02	8	<2
93J13W	L12600N	10040E	6246	<1	82	49	6	<0.2	<0.02	14	<2
93J13W	L12600N	10080E	6246	<1	53	63	8	<0.2	<0.02	12	<2
93J13W	L12600N	10120E	6246	<1	161	51	6	0.5	<0.02	13	<2
93J13W	L12600N	10160E	6246	<1	142	51	6	0.5	<0.02	11	<2
93J13W	L12600N	10200E	6246	<1	120	41	6	0.4	<0.02	8	<2
93J13W	L12600N	10240E	6246	<1	63	55	6	<0.2	<0.02	23	<2
93J13W	L12600N	10280E	6246	<1	76	65	9	<0.2	<0.02	9	<2
93J13W	L12600N	10320E	6246	<1	56	55	7	0.2	<0.02	7	<2
test	STD P		6246	13	123	98	110			64	44
93J13W	L12600N	10360E	6246	<1	65	52	6	<0.2	<0.02	5	<2
93J13W	L12600N	10400E	6246	<1	80	84	5	0.6	<0.02	13	<2
93J13W	L12600N	10440E	6246	<1	53	49	7	<0.2	<0.02	7	<2
93J13W	L12600N	10480E	6246	<1	54	50	6	0.2	0.21	4	<2
93J13W	L12600N	10520E	6246	<1	66	60	7	0.3	<0.02	10	<2
93J13W	L12600N	10560E	6246	<1	54	49	6	0.2	0.08	5	2
93J13W	L12600N	10600E	6246	<1	52	56	7	<0.2	<0.02	<2	<2
93J13W	L12600N	10640E	6246	<1	39	34	8	<0.2	<0.02	3	<2
93J13W	L12600N	10680E	6246	<1	45	51	6	<0.2	<0.02	2	<2
93J13W	L12600N	10680E*	6246	<1	45	46	6	<0.2	<0.02	3	<2
93J13W	L12600N	10720E	6246	1	40	46	5	<0.2	<0.02	5	<2
93J13W	L12600N	10760E	6246	<1	43	43	6	<0.2	<0.02	2	<2
93J13W	L12600N	10800E	6246	1	42	49	5	<0.2	<0.02	5	<2
93J13W	L12600N	10800E*	6246	1	42	44	4	<0.2	<0.02	5	<2
test	STD AU		6246						0.25		
test	STD AU		6246						0.20		
test	STD AU		6246						0.40		
test	STD AU		6246						0.26		
test	STD AU		6246						0.24		
test	STD AU		6246						0.22		
test	STD AU		6246						0.36		
test	STD AU		6246						0.22		
test	STD AU		6246						0.35		
test	STD AU		6246						0.20		
test	STD AU		6246						0.23		
test	STD AU		6246						0.20		
test	STD AU		6246						0.23		
test	STD AU		6246						0.36		

END OF LISTING - 338 RECORDS PRINTED
GCLIST RUN AT: 12:50:52

APPENDIX 3

```
 File: EXPL*IT.WINDY              Field name: CU       LOG = 1  REPVAL =     .00100
  560 SAMPLES WITH CU    MINIMUM:    15.0000              MAXIMUM:  940.000
  560 VALUES PLOTTED:      0 NOT IN RANGE   15.0000      to  940.000
     GEOMETRIC MEAN:            56.5805         DISPERSION: 32.6566      98.0309
   SCALE OF HISTOGRAM IS    2.00 COUNTS /PRINT POSITION    # = 5,50,95%
   N    MIDPOINT   PERCENT 0         20        40        60        80
                           I---------I---------I---------I---------I
   1     15.000        .18 I*                                        I
   2     16.635        .36 I*                                        I
   1     18.448        .18 I*                                        I
   1     20.458        .18 I*                                        I
   4     22.688        .71 I**                                       I
  10     25.161       1.79 I*****                                    I
  17     27.903     #  3.04 I*********                                I
  25     30.944       4.46 I*************                            I
  54     34.316       9.64 I***************************              I
  48     38.056       8.57 I************************                 I
  47     42.204       8.39 I************************                 I
  48     46.803       8.57 I************************                 I
  45     51.904     #  8.04 I***********************                  I
  36     57.561       6.43 I******************                       I
  43     63.834       7.68 I**********************                   I
  40     70.791       7.14 I********************                     I
  28     78.507       5.00 I**************                           I
  25     87.063       4.46 I*************                            I
  16     96.551       2.86 I********                                 I
  12     107.07       2.14 I******                                   I
   9     118.74       1.61 I*****                                    I
  13     131.68       2.32 I*******                                  I
   8     146.04     #  1.43 I****                                     I
   8     161.95       1.43 I****                                     I
   5     179.60        .89 I***                                      I
   2     199.18        .36 I*                                        I
   1     220.88        .18 I*                                        I
   3     244.96        .54 I**                                       I
   1     271.65        .18 I*                                        I
   1     301.26        .18 I*                                        I
   0     334.09        .00 I                                         I
   1     370.51        .18 I*                                        I
   1     410.89        .18 I*                                        I
   0     455.67        .00 I                                         I
   0     505.33        .00 I                                         I
   1     560.40        .18 I*                                        I
   0     621.48        .00 I                                         I
   0     689.21        .00 I                                         I
   1     764.32        .18 I*                                        I
   1     847.62        .18 I*                                        I
   1     940.00        .18 I*                                        I
-----                      I---------I---------I---------I---------I
 560                       0         20        40        60        80
```

```
File: EXPL*IT.WINDY              Field name: PB       LOG = 1  REPVAL =     .00100
 560 SAMPLES WITH PB    MINIMUM:    2.00000              MAXIMUM:  31.0000
 560 VALUES PLOTTED:      0 NOT IN RANGE   2.00000      to  31.0000
    GEOMETRIC MEAN:          4.98988         DISPERSION: 3.64527     6.83046
  SCALE OF HISTOGRAM IS   4.00 COUNTS /PRINT POSITION    # = 5,50,95%

  N    MIDPOINT  PERCENT 0         40        80        120       160
                         I---------I---------I---------I---------I
  8     2.0000     1.43  I**                                       I
  0     2.1418      .00  I                                         I
  0     2.2938      .00  I                                         I
  0     2.4564      .00  I                                         I
  0     2.6307      .00  I                                         I
  0     2.8172      .00  I                                         I
 60     3.0170   # 10.71 I***************                          I
  0     3.2310      .00  I                                         I
  0     3.4602      .00  I                                         I
  0     3.7056      .00  I                                         I
130     3.9684    23.21  I*********************************        I
  0     4.2498      .00  I                                         I
  0     4.5512      .00  I                                         I
129     4.8740   # 23.04 I********************************         I
  0     5.2197      .00  I                                         I
  0     5.5899      .00  I                                         I
142     5.9864    25.36  I************************************     I
  0     6.4109      .00  I                                         I
 54     6.8656     9.64  I**************                           I
  0     7.3525      .00  I                                         I
 22     7.8740   #  3.93 I******                                   I
  0     8.4325      .00  I                                         I
  9     9.0305     1.61  I**                                       I
  3     9.6710      .54  I*                                        I
  0     10.357      .00  I                                         I
  0     11.091      .00  I                                         I
  1     11.878      .18  I                                         I
  0     12.720      .00  I                                         I
  0     13.623      .00  I                                         I
  0     14.589      .00  I                                         I
  0     15.624      .00  I                                         I
  0     16.732      .00  I                                         I
  0     17.918      .00  I                                         I
  0     19.189      .00  I                                         I
  1     20.550      .18  I                                         I
  0     22.007      .00  I                                         I
  0     23.568      .00  I                                         I
  0     25.240      .00  I                                         I
  0     27.030      .00  I                                         I
  0     28.947      .00  I                                         I
  1     31.000      .18  I                                         I
----                     I---------I---------I---------I---------I
560                      0         40        80        120       160
```

```
File: EXPL*IT.WINDY              Field name: ZN      LOG = 1  REPVAL =     .00100
 560 SAMPLES WITH ZN     MINIMUM:    8.00000             MAXIMUM:  123.000
 560 VALUES PLOTTED:      0 NOT IN RANGE   8.00000     to  123.000
    GEOMETRIC MEAN:          56.2494          DISPERSION: 43.9721      71.9545
  SCALE OF HISTOGRAM IS   4.00 COUNTS /PRINT POSITION    # = 5,50,95%

  N    MIDPOINT   PERCENT 0         40        80        120       160
                          I---------I---------I---------I---------I
  1     8.0000       .18  I                                         I
  0     8.5657       .00  I                                         I
  0     9.1713       .00  I                                         I
  0     9.8198       .00  I                                         I
  0     10.514       .00  I                                         I
  0     11.257       .00  I                                         I
  0     12.053       .00  I                                         I
  0     12.906       .00  I                                         I
  0     13.818       .00  I                                         I
  0     14.795       .00  I                                         I
  0     15.841       .00  I                                         I
  0     16.961       .00  I                                         I
  0     18.161       .00  I                                         I
  0     19.445       .00  I                                         I
  0     20.820       .00  I                                         I
  0     22.292       .00  I                                         I
  0     23.868       .00  I                                         I
  1     25.556       .18  I                                         I
  0     27.363       .00  I                                         I
  2     29.297       .36  I*                                        I
  2     31.369       .36  I*                                        I
  3     33.587       .54  I*                                        I
 10     35.962      1.79  I***                                      I
  9     38.504      1.61  I**                                       I
 19     41.227   #  3.39  I*****                                    I
 46     44.142      8.21  I************                             I
 47     47.263      8.39  I************                             I
 83     50.605     14.82  I*********************                    I
 75     54.183   # 13.39  I*******************                      I
 72     58.014     12.86  I******************                       I
 46     62.116      8.21  I************                             I
 31     66.508      5.54  I********                                 I
 41     71.210      7.32  I**********                               I
 20     76.245      3.57  I*****                                    I
 22     81.636      3.93  I******                                   I
 12     87.408   #  2.14  I***                                      I
  9     93.589      1.61  I**                                       I
  6     100.21      1.07  I**                                       I
  2     107.29       .36  I*                                        I
  0     114.88       .00  I                                         I
  1     123.00       .18  I                                         I
-----                     I---------I---------I---------I---------I
 560                      0         40        80        120       160
```

```
File: EXPL*IT.WINDY            Field name: AS       LOG = 1  REPVAL =      .00100
 560 SAMPLES WITH AS     MINIMUM:    1.00000              MAXIMUM:  120.000
 560 VALUES PLOTTED:      0 NOT IN RANGE    1.00000       to  120.000
    GEOMETRIC MEAN:           4.05415          DISPERSION: 1.57629      10.4271
  SCALE OF HISTOGRAM IS   4.00 COUNTS /PRINT POSITION    # = 5,50,95%
  N    MIDPOINT   PERCENT 0         40        80        120       160
                          I---------I---------I---------I---------I
121    1.0000    # 21.61  I******************************          I
  0    1.1271       .00   I                                        I
  0    1.2705       .00   I                                        I
  0    1.4320       .00   I                                        I
  0    1.6141       .00   I                                        I
  0    1.8193       .00   I                                        I
 41    2.0506      7.32   I**********                              I
  0    2.3113       .00   I                                        I
  0    2.6052       .00   I                                        I
 53    2.9364      9.46   I*************                           I
  0    3.3098       .00   I                                        I
  0    3.7306       .00   I                                        I
 57    4.2049     10.18   I**************                          I
 66    4.7395    # 11.79  I*****************                       I
  0    5.3421       .00   I                                        I
 34    6.0213      6.07   I*********                               I
 37    6.7869      6.61   I*********                               I
 31    7.6498      5.54   I********                                I
 25    8.6225      4.46   I******                                  I
 14    9.7188      2.50   I****                                    I
  8    10.954      1.43   I**                                      I
 26    12.347      4.64   I*******                                 I
  8    13.917      1.43   I**                                      I
  8    15.687      1.43   I**                                      I
  6    17.681    #  1.07  I**                                      I
 11    19.929      1.96   I***                                     I
  3    22.463       .54   I*                                       I
  1    25.319       .18   I                                        I
  5    28.538       .89   I*                                       I
  0    32.167       .00   I                                        I
  0    36.256       .00   I                                        I
  2    40.866       .36   I*                                       I
  0    46.062       .00   I                                        I
  1    51.919       .18   I                                        I
  0    58.520       .00   I                                        I
  0    65.960       .00   I                                        I
  1    74.347       .18   I                                        I
  0    83.800       .00   I                                        I
  0    94.454       .00   I                                        I
  0    106.46       .00   I                                        I
  1    120.00       .18   I                                        I
-----                     I---------I---------I---------I---------I
560                       0         40        80        120       160
```

AUTOVALU

```
File: EXPL*IT.WINDY              Field name: AU       LOG = 1  REPVAL =     .00100
 560 SAMPLES WITH AU    MINIMUM:    .100000-001         MAXIMUM:  .560000
 560 VALUES PLOTTED:       0 NOT IN RANGE    .100000-001 to  .560000
    GEOMETRIC MEAN:          .117700-001      DISPERSION: .682667-002 .202930-001
  SCALE OF HISTOGRAM IS  20.00 COUNTS /PRINT POSITION    # = 5,50,95%
    N    MIDPOINT  PERCENT 0         200       400       600       800
                           I---------I---------I---------I---------I
  501  .10000-001# 89.46 I*************************                  I
    0  .11059-001    .00 I                                          I
    0  .12230-001    .00 I                                          I
    0  .13524-001    .00 I                                          I
    0  .14956-001    .00 I                                          I
    0  .16540-001    .00 I                                          I
    0  .18291-001    .00 I                                          I
   14  .20227-001   2.50 I*                                         I
    0  .22369-001    .00 I                                          I
    0  .24737-001    .00 I                                          I
    0  .27356-001    .00 I                                          I
   18  .30252-001#  3.21 I*                                         I
    0  .33455-001    .00 I                                          I
    0  .36997-001    .00 I                                          I
    2  .40913-001    .36 I                                          I
    0  .45245-001    .00 I                                          I
    3  .50035-001    .54 I                                          I
    0  .55332-001    .00 I                                          I
    3  .61191-001    .54 I                                          I
    1  .67669-001    .18 I                                          I
    0  .74833-001    .00 I                                          I
    5  .82756-001    .89 I                                          I
    0  .91517-001    .00 I                                          I
    3  .10121        .54 I                                          I
    3  .11192        .54 I                                          I
    0  .12377        .00 I                                          I
    0  .13687        .00 I                                          I
    0  .15137        .00 I                                          I
    1  .16739        .18 I                                          I
    2  .18511        .36 I                                          I
    1  .20471        .18 I                                          I
    0  .22638        .00 I                                          I
    1  .25035        .18 I                                          I
    1  .27686        .18 I                                          I
    0  .30617        .00 I                                          I
    0  .33858        .00 I                                          I
    0  .37443        .00 I                                          I
    0  .41407        .00 I                                          I
    0  .45791        .00 I                                          I
    0  .50639        .00 I                                          I
    1  .56000        .18 I                                          I
 ----                    I---------I---------I---------I---------I
  560                    0         200       400       600       800
```

AUTOVALU

```
File: EXPL*IT.WINDY               Field name: AG       LOG = 1  REPVAL =     .00100
 560 SAMPLES WITH AG    MINIMUM:    .100000+000        MAXIMUM:  1.30000
 560 VALUES PLOTTED:      0 NOT IN RANGE    .100000+000 to  1.30000
   GEOMETRIC MEAN:          .140642          DISPERSION: .831071-001 .238007
  SCALE OF HISTOGRAM IS  10.00 COUNTS /PRINT POSITION    # = 5,50,95%
  N    MIDPOINT  PERCENT 0       100       200       300       400
                         I---------I---------I---------I---------I
370  .10000+000#  66.07 I*************************************     I
  0   .10662        .00 I                                         I
  0   .11368        .00 I                                         I
  0   .12121        .00 I                                         I
  0   .12924        .00 I                                         I
  0   .13780        .00 I                                         I
  0   .14692        .00 I                                         I
  0   .15665        .00 I                                         I
  0   .16703        .00 I                                         I
  0   .17809        .00 I                                         I
  0   .18988        .00 I                                         I
 94   .20246      16.79 I*********                                I
  0   .21587        .00 I                                         I
  0   .23016        .00 I                                         I
  0   .24540        .00 I                                         I
  0   .26165        .00 I                                         I
  0   .27898        .00 I                                         I
 54   .29746       9.64 I*****                                    I
  0   .31716        .00 I                                         I
  0   .33816        .00 I                                         I
  0   .36056        .00 I                                         I
  0   .38443        .00 I                                         I
 26   .40989    #  4.64 I***                                      I
  0   .43704        .00 I                                         I
  0   .46598        .00 I                                         I
  7   .49684       1.25 I*                                        I
  0   .52974        .00 I                                         I
  0   .56482        .00 I                                         I
  1   .60223        .18 I                                         I
  0   .64211        .00 I                                         I
  3   .68463        .54 I                                         I
  0   .72997        .00 I                                         I
  0   .77831        .00 I                                         I
  0   .82986        .00 I                                         I
  2   .88481        .36 I                                         I
  0   .94341        .00 I                                         I
  2   1.0059        .36 I                                         I
  0   1.0725        .00 I                                         I
  0   1.1435        .00 I                                         I
  0   1.2193        .00 I                                         I
  1   1.3000        .18 I                                         I
-----                   I---------I---------I---------I---------I
 560                    0       100       200       300       400
```

AUTOVALU

```
File: EXPL*IT.WINDY              Field name: MO      LOG = 1  REPVAL =     .00100
 560 SAMPLES WITH MO    MINIMUM:    .500000              MAXIMUM:  7.00000
 560 VALUES PLOTTED:     0 NOT IN RANGE    .500000      to  7.00000
    GEOMETRIC MEAN:          .658228        DISPERSION: .431086     1.00505
  SCALE OF HISTOGRAM IS  10.00 COUNTS /PRINT POSITION    # = 5,50,95%
    N    MIDPOINT  PERCENT 0        100       200       300       400
                           I---------I---------I---------I---------I
  370    .50000    # 66.07 I*************************************    I
    0    .53410        .00 I                                         I
    0    .57053        .00 I                                         I
    0    .60944        .00 I                                         I
    0    .65100        .00 I                                         I
    0    .69540        .00 I                                         I
    0    .74283        .00 I                                         I
    0    .79349        .00 I                                         I
    0    .84761        .00 I                                         I
    0    .90542        .00 I                                         I
    0    .96717        .00 I                                         I
  162   1.0331       28.93 I****************                         I
    0   1.1036         .00 I                                         I
    0   1.1789         .00 I                                         I
    0   1.2593         .00 I                                         I
    0   1.3451         .00 I                                         I
    0   1.4369         .00 I                                         I
    0   1.5349         .00 I                                         I
    0   1.6396         .00 I                                         I
    0   1.7514         .00 I                                         I
    0   1.8708         .00 I                                         I
   25   1.9984     #  4.46 I**                                       I
    0   2.1347         .00 I                                         I
    0   2.2803         .00 I                                         I
    0   2.4358         .00 I                                         I
    0   2.6020         .00 I                                         I
    0   2.7794         .00 I                                         I
    0   2.9690         .00 I                                         I
    0   3.1715         .00 I                                         I
    0   3.3878         .00 I                                         I
    0   3.6188         .00 I                                         I
    0   3.8656         .00 I                                         I
    1   4.1293         .18 I                                         I
    0   4.4109         .00 I                                         I
    0   4.7117         .00 I                                         I
    1   5.0331         .18 I                                         I
    0   5.3763         .00 I                                         I
    0   5.7430         .00 I                                         I
    0   6.1347         .00 I                                         I
    0   6.5531         .00 I                                         I
    1   7.0000         .18 I                                         I
-----                      I---------I---------I---------I---------I
  560                      0        100       200       300       400
```

AUTOVALU

```
File: EXPL*IT.WINDY              Field name: SB       LOG = 1  REPVAL =     .00100
 560 SAMPLES WITH SB    MINIMUM:    1.00000           MAXIMUM:  6.00000
 560 VALUES PLOTTED:      0 NOT IN RANGE   1.00000      to  6.00000
   GEOMETRIC MEAN:          1.15310        DISPERSION: .784995     1.69381
  SCALE OF HISTOGRAM IS  20.00 COUNTS /PRINT POSITION   # = 5,50,95%
  N    MIDPOINT   PERCENT 0       200       400       600       800
                          I---------I---------I---------I---------I
484    1.0000    # 86.43 I************************                 I
  0    1.0458        .00 I                                         I
  0    1.0937        .00 I                                         I
  0    1.1438        .00 I                                         I
  0    1.1962        .00 I                                         I
  0    1.2510        .00 I                                         I
  0    1.3083        .00 I                                         I
  0    1.3683        .00 I                                         I
  0    1.4310        .00 I                                         I
  0    1.4965        .00 I                                         I
  0    1.5651        .00 I                                         I
  0    1.6368        .00 I                                         I
  0    1.7118        .00 I                                         I
  0    1.7902        .00 I                                         I
  0    1.8722        .00 I                                         I
 34    1.9580       6.07 I**                                       I
  0    2.0477        .00 I                                         I
  0    2.1415        .00 I                                         I
  0    2.2396        .00 I                                         I
  0    2.3422        .00 I                                         I
  0    2.4495        .00 I                                         I
  0    2.5617        .00 I                                         I
  0    2.6791        .00 I                                         I
  0    2.8018        .00 I                                         I
  0    2.9302        .00 I                                         I
 19    3.0644    #  3.39 I*                                        I
  0    3.2048        .00 I                                         I
  0    3.3516        .00 I                                         I
  0    3.5051        .00 I                                         I
  0    3.6657        .00 I                                         I
  0    3.8337        .00 I                                         I
 10    4.0093       1.79 I                                         I
  0    4.1930        .00 I                                         I
  0    4.3851        .00 I                                         I
  0    4.5859        .00 I                                         I
  0    4.7960        .00 I                                         I
 10    5.0158       1.79 I                                         I
  0    5.2455        .00 I                                         I
  0    5.4858        .00 I                                         I
  0    5.7372        .00 I                                         I
  3    6.0000        .54 I                                         I
----                     I---------I---------I---------I---------I
560                      0       200       400       600       800
```

AUTOVALU

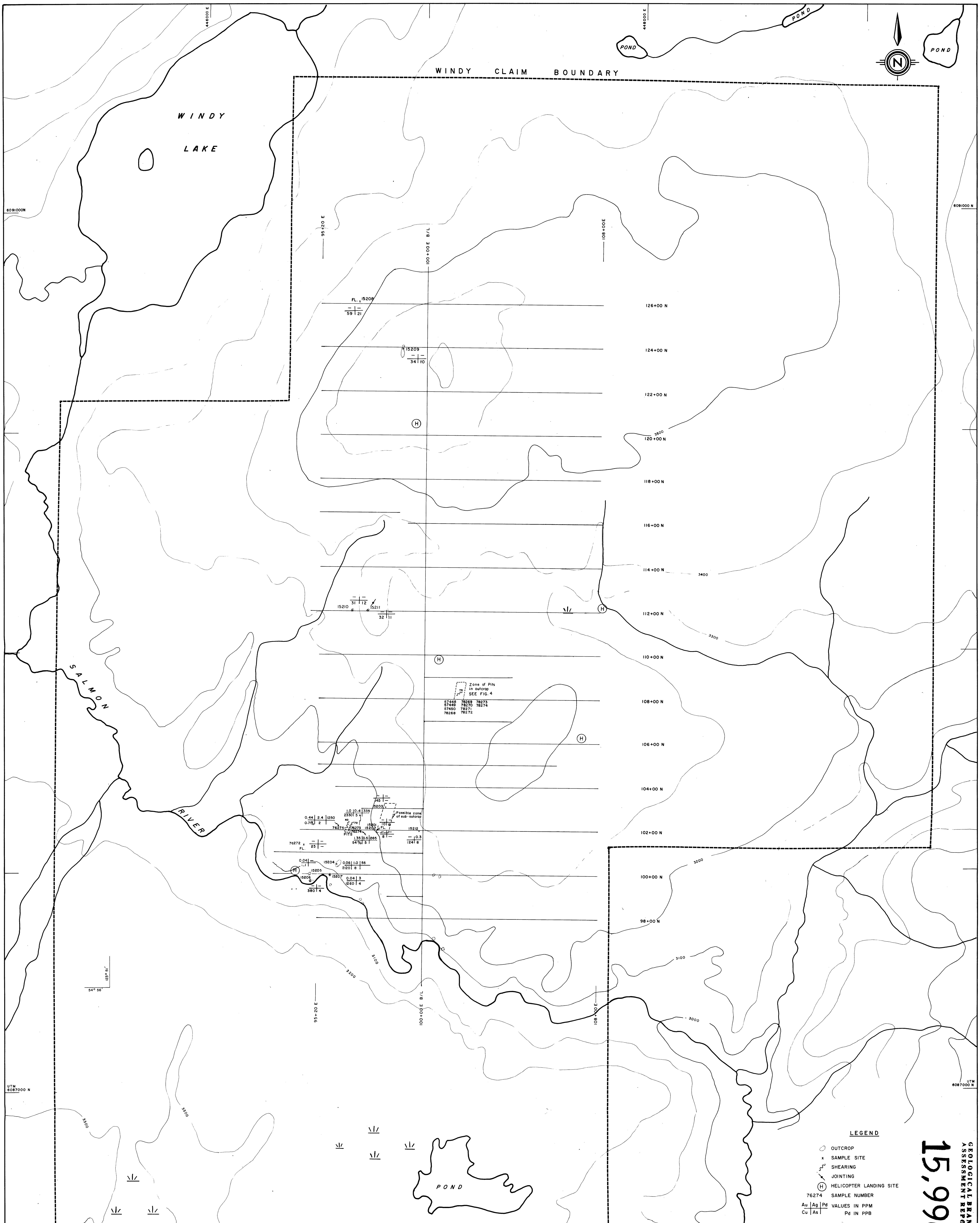
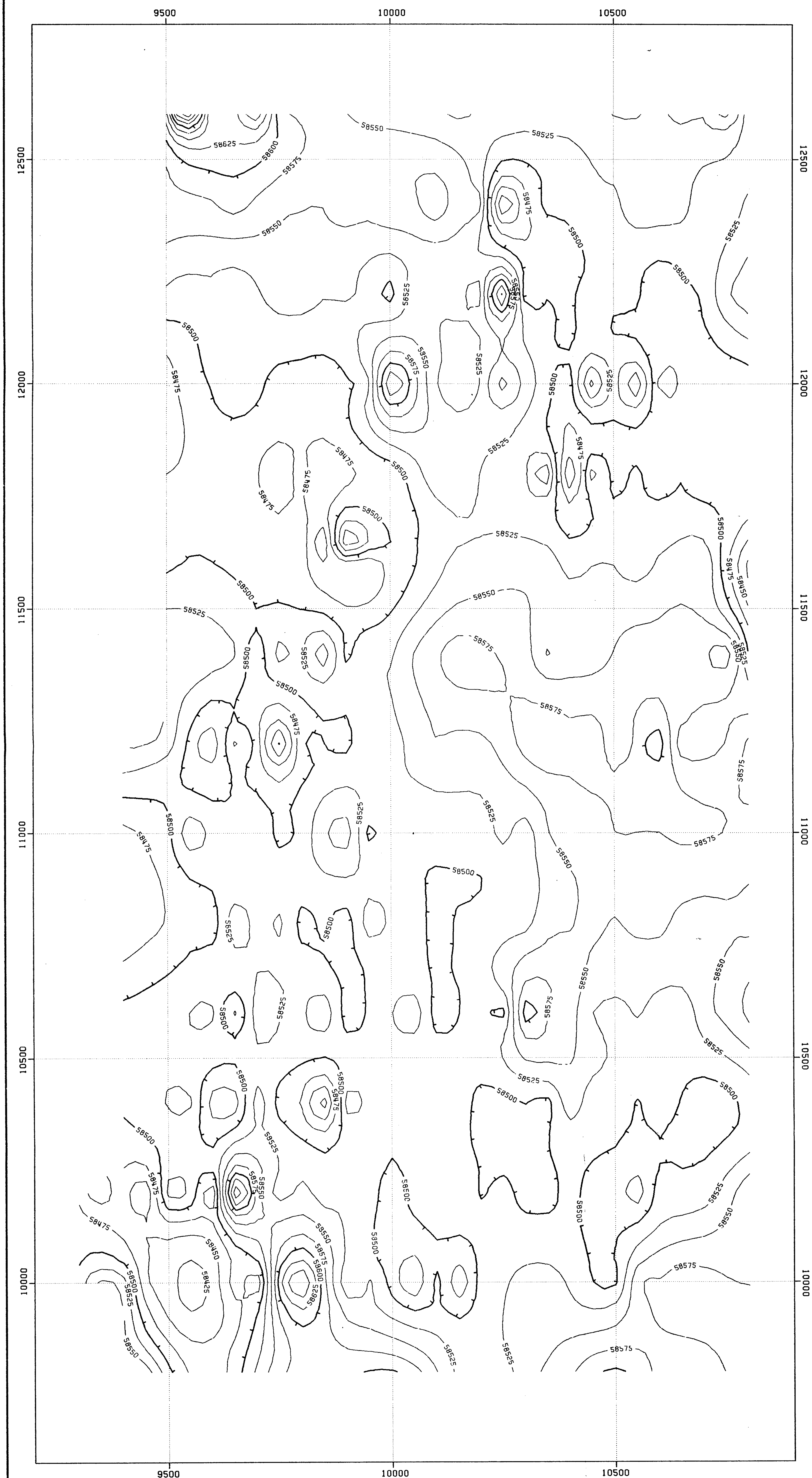


Figure 3.

PLACER DEVELOPMENT LIMITED	
DRAWN - H.R.G.	V-216 WINDY PROPERTY
DATE - NOV. 1986	OUTCROP MAP WITH ROCK SAMPLE LOCATIONS & ANALYTICAL RESULTS
SCALE - 1:5000	
REVISED -	NO.



WINDY PROPERTY
CONTOURED MAGNETIC DATA

CONTOUR INTERVAL - 25 NT

DATA PLOTTED ON THIS MAP:

FIELD FILE
CONTOURS: MAG EXPL*V-216.GRMG

DIRECTION OF NORTH AT CENTRE OF MAP

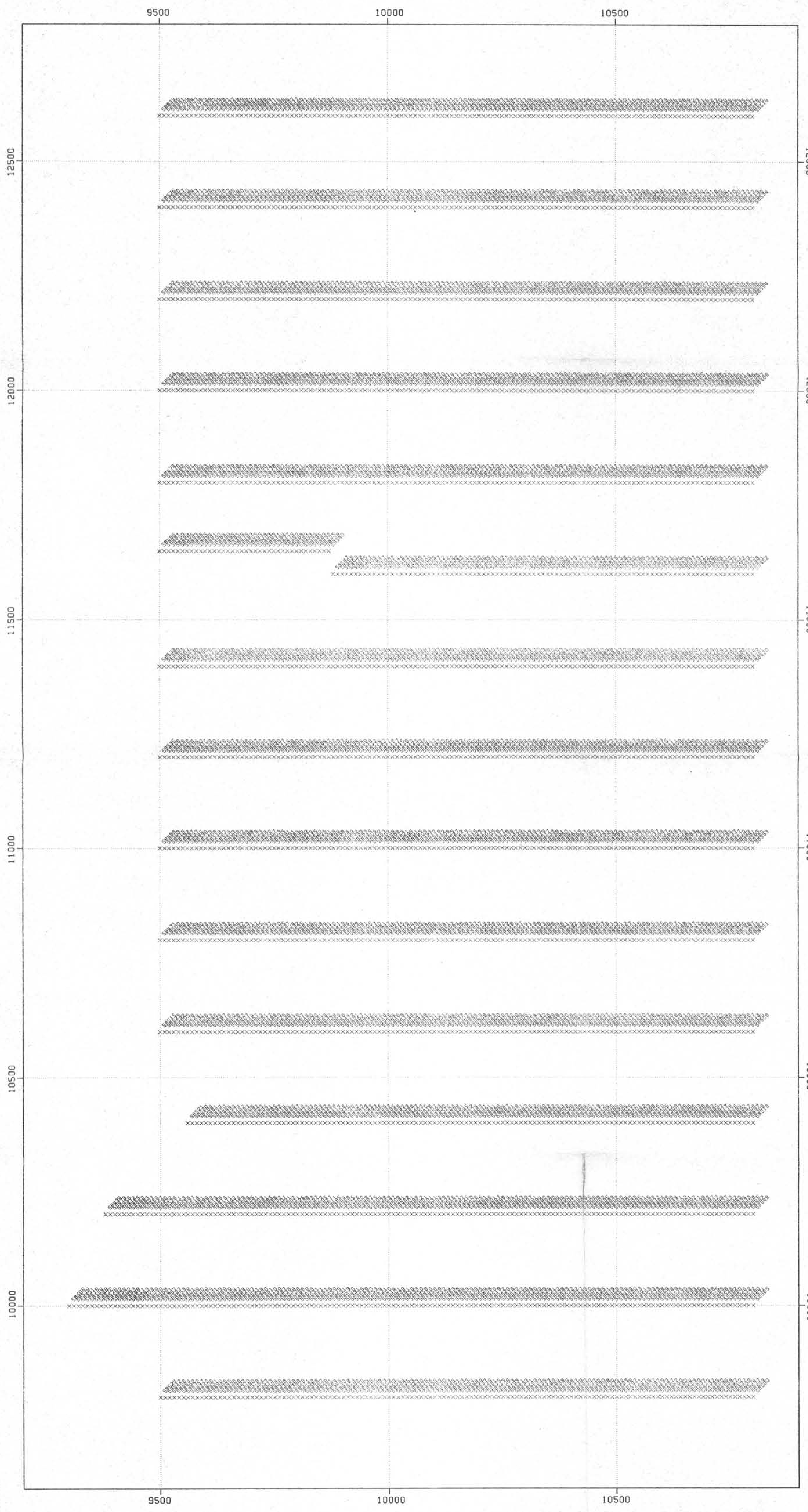
0 125 250 375 500
METRES

15,996

GEOLOGICAL BRANCH
ASSESSMENT REPORT

Figure 5.

PLACER DEVELOPMENT LIMITED	
DRAWN RC DATE 87/03/11 SCALE 1:5000	WINDY PROPERTY CONTOURED MAGNETIC DATA
NO.	PLATE



WINDY PROPERTY
POSTED MAGNETIC DATA

VALUES IN NANOTESLAS

DATA PLOTTED ON THIS MAP:

	FIELD	FILE
× POINTS:	MAG	EXPL×V-216.MAGS

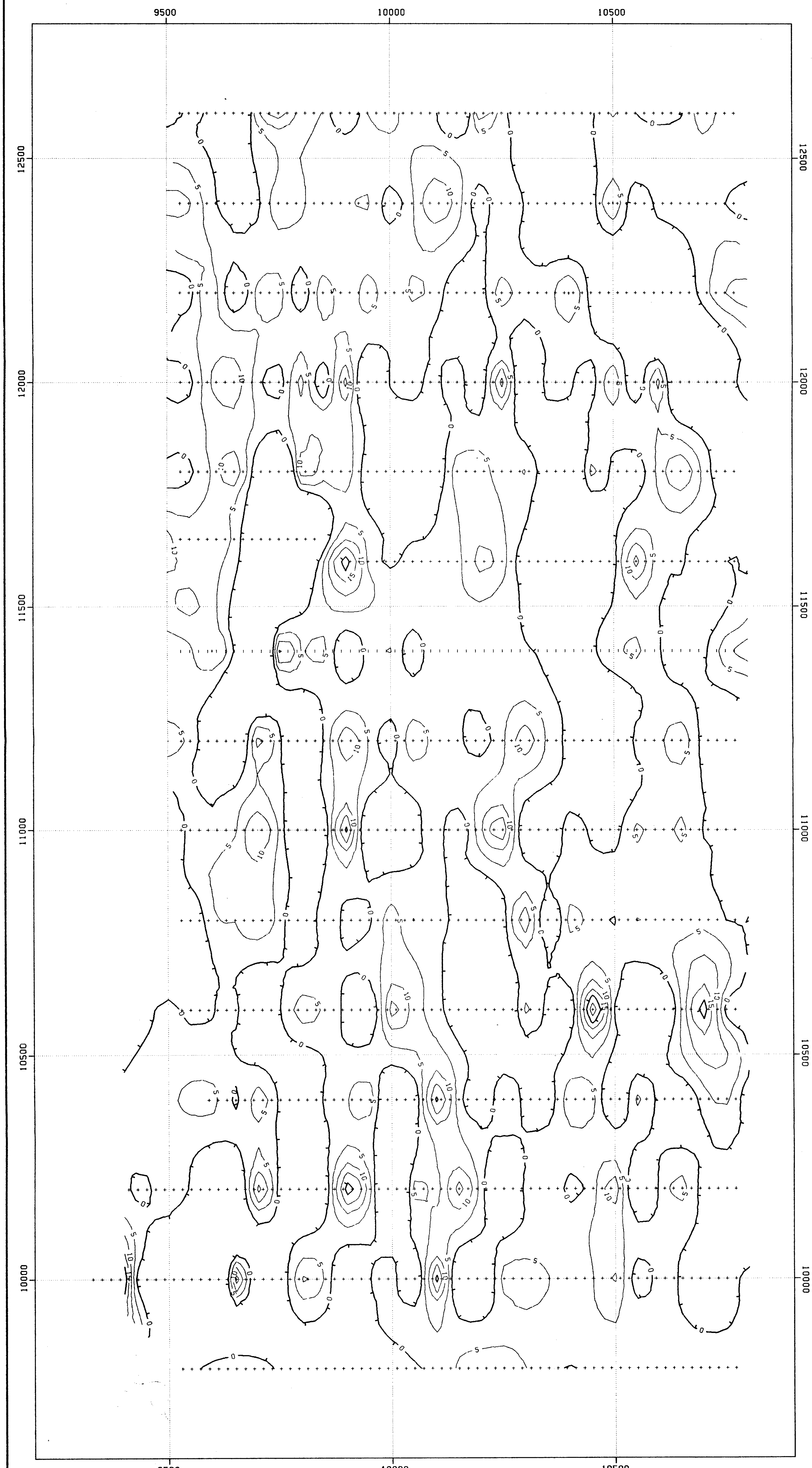
DIRECTION OF NORTH AT CENTRE OF MAP

N

0 125 250 375 500
METRES

Figure 6.

PLACER DEVELOPMENT LIMITED	
DRAWN RC	WINDY PROPERTY
DATE 87/03/06	POSTED MAGNETIC DATA
SCALE 1:5000	
	NO. PLATE



DATA PLOTTED ON THIS MAP:

FIELD FILE

+ CONTOURS: FF EXPL*V-216.FFS

DIRECTION OF NORTH AT CENTRE OF MAP

0 125 250 375 500

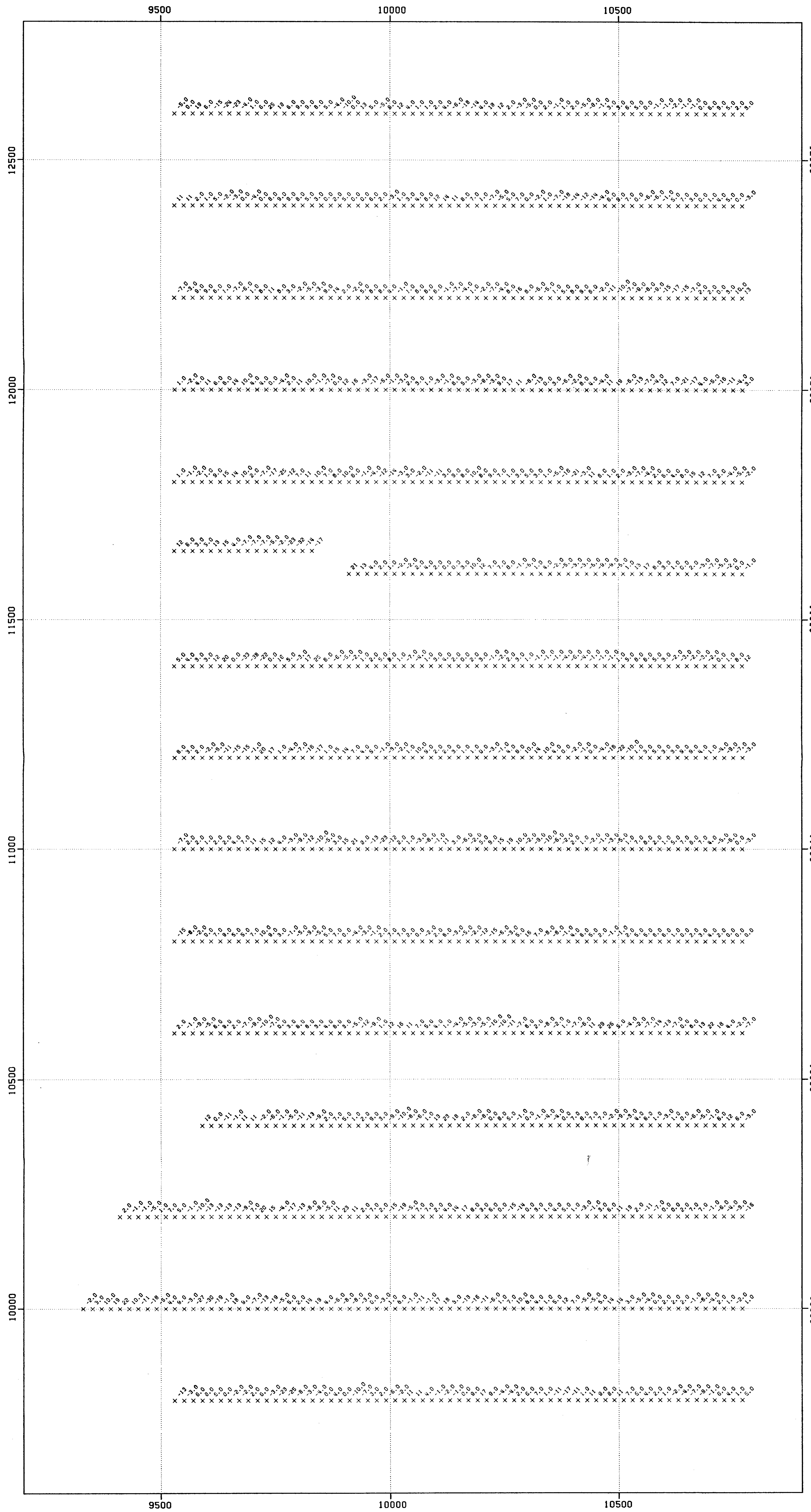
METRES

15,996

GEOLOGICAL BRANCH
ASSESSMENT REPORT

Figure 7

PLACER DEVELOPMENT LIMITED	
DRAWN RC	WINDY PROPERTY
DATE 87/03/10	CONTOURED FRASER FILTER DATA
SCALE 1:5000	
	NO. PLATE



DATA PLOTTED ON THIS MAP:

	FIELD	FILE
× POINTS:	FF	EXPL×V-216.FFS

DIRECTION OF NORTH AT CENTRE OF MAP

0 125 250 375 500
METRES

15,996

GEOLOGICAL BRANCH
ASSESSMENT REPORT

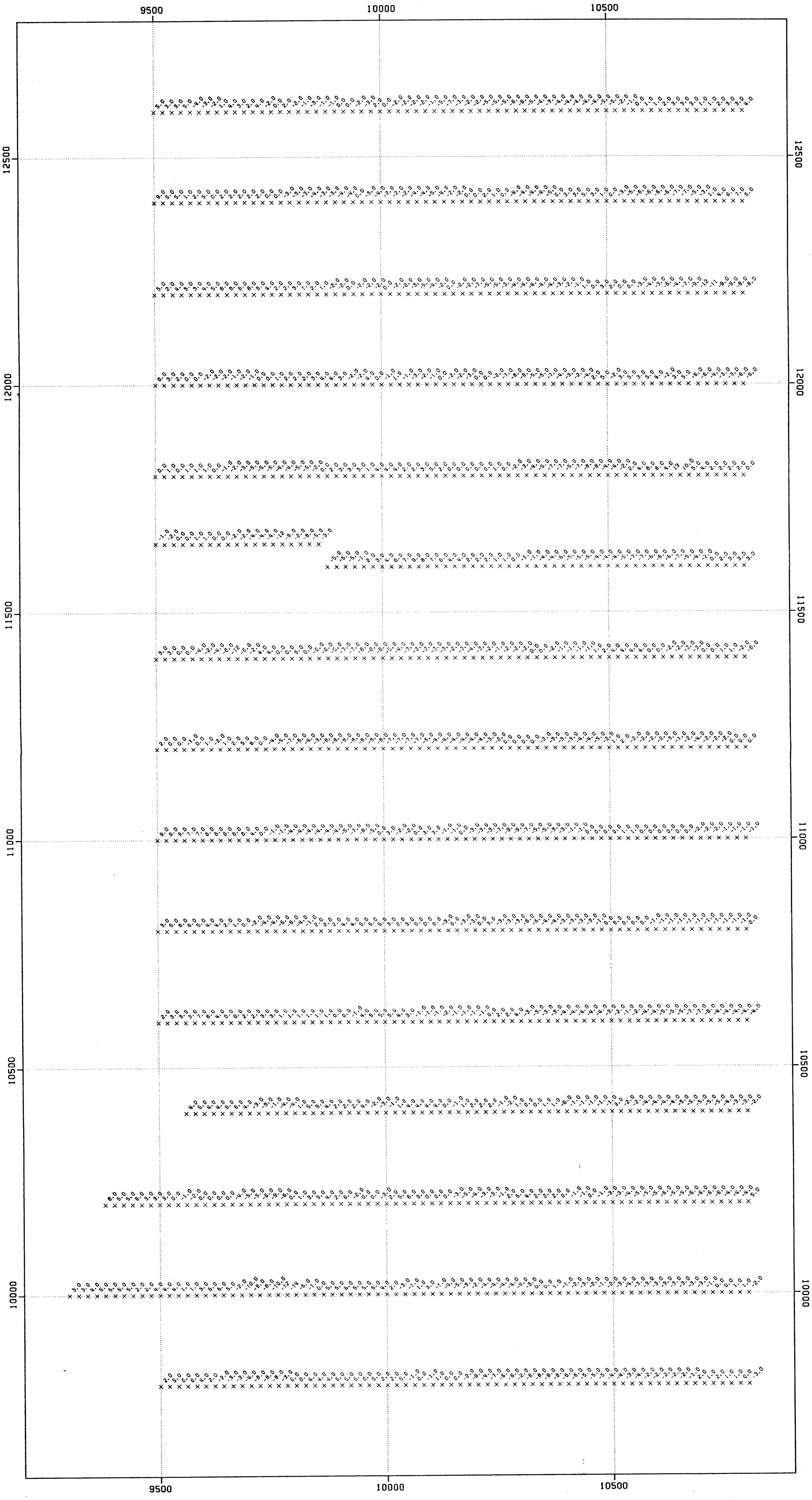
Figure 8.

PLACER DEVELOPMENT LIMITED

DRAWN RC
DATE 87/03/06
SCALE 1:5000

WINDY PROPERTY
POSTED FRASER FILTER DATA

NO. PLATE



WINDY PROPERTY
POSTED QUADRATURE DATA

VALUES ARE % OF PRIMARY FIELD

DATA PLOTTED ON THIS MAP:

	FIELD	FILE
× POINTS:	QD	EXPL×V-216.QDS

DIRECTION OF NORTH AT CENTRE OF MAP

0 125 250 375 500
METRES

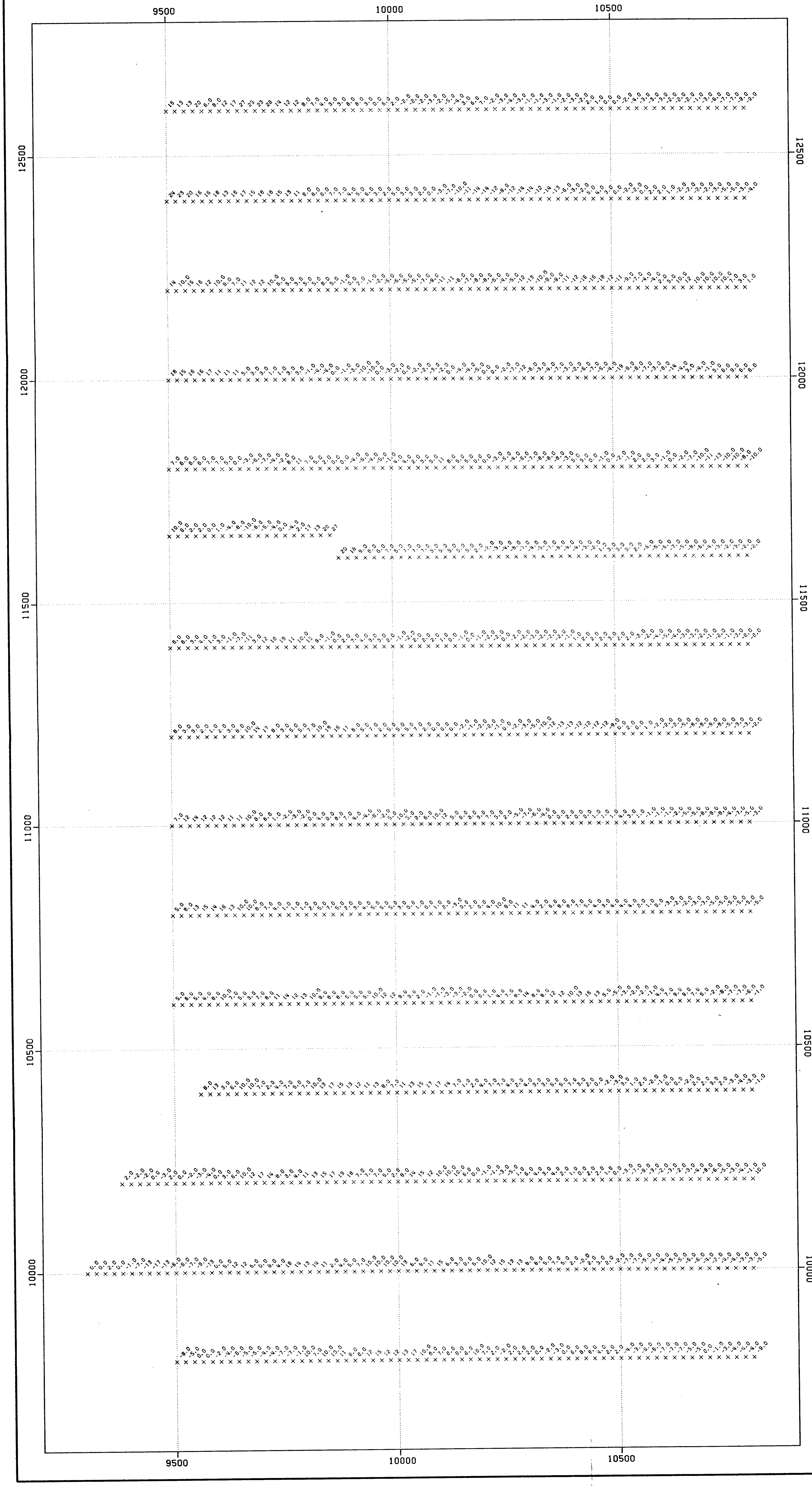
15,996

GEOLOGICAL BRANCH
ASSESSMENT REPORT

Figure 9.

PLACER DEVELOPMENT LIMITED

DRAWN RC	WINDY PROPERTY
DATE 87/03/06	POSTED QUADRATURE DATA
SCALE 1:5000	
	NO. PLATE



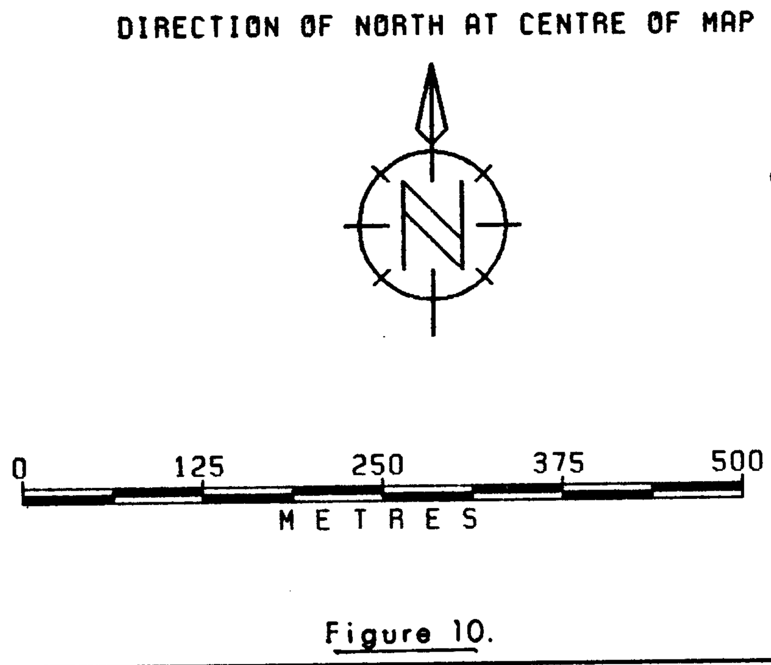
WINDY PROPERTY
POSTED IN-PHASE DATA

VALUES IN % OF PRIMARY FIELD

DATA PLOTTED ON THIS MAP:

	FIELD	FILE
× POINTS:	IP	EXPL*V-216.IPS

DIRECTION OF NORTH AT CENTRE OF MAP



15,996

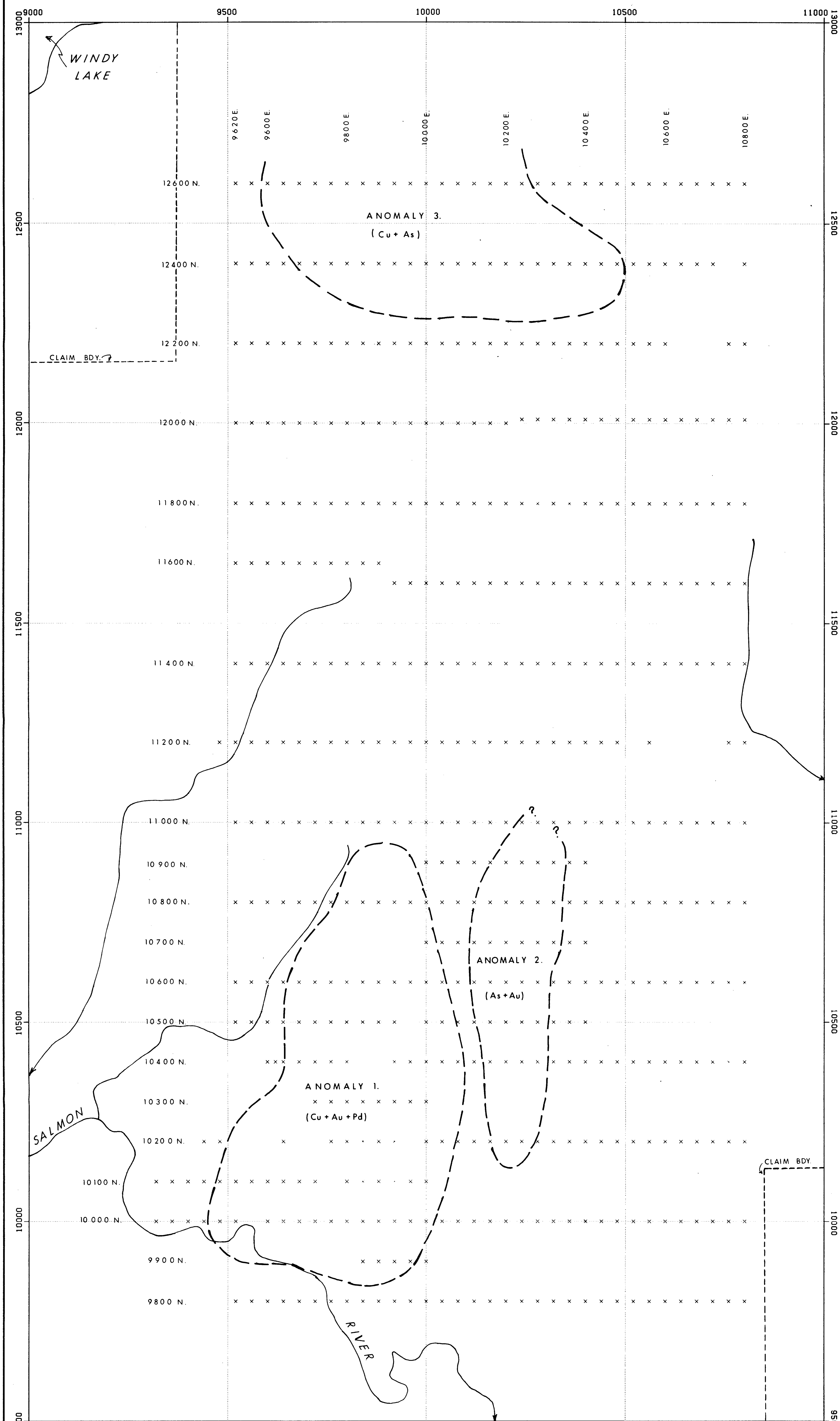
GEOLOGICAL BRANCH
ASSESSMENT REPORT

Figure 10.

PLACER DEVELOPMENT LIMITED

DRAWN RC	WINDY PROPERTY
DATE 87/03/06	POSTED IN-PHASE DATA
SCALE 1:5000	
NO.	PLATE

V-216 WINDY CLAIMS
SAMPLE LOCATIONS



DATA PLOTTED ON THIS MAP:

FIELD FILE
× POINTS: EXPL×V-216.GEOCHEM

MAP LIMITS:	X	Y
MAX:	11000.000	13000.000
MIN:	9000.000	9500.000

DIRECTION OF NORTH AT CENTRE OF MAP

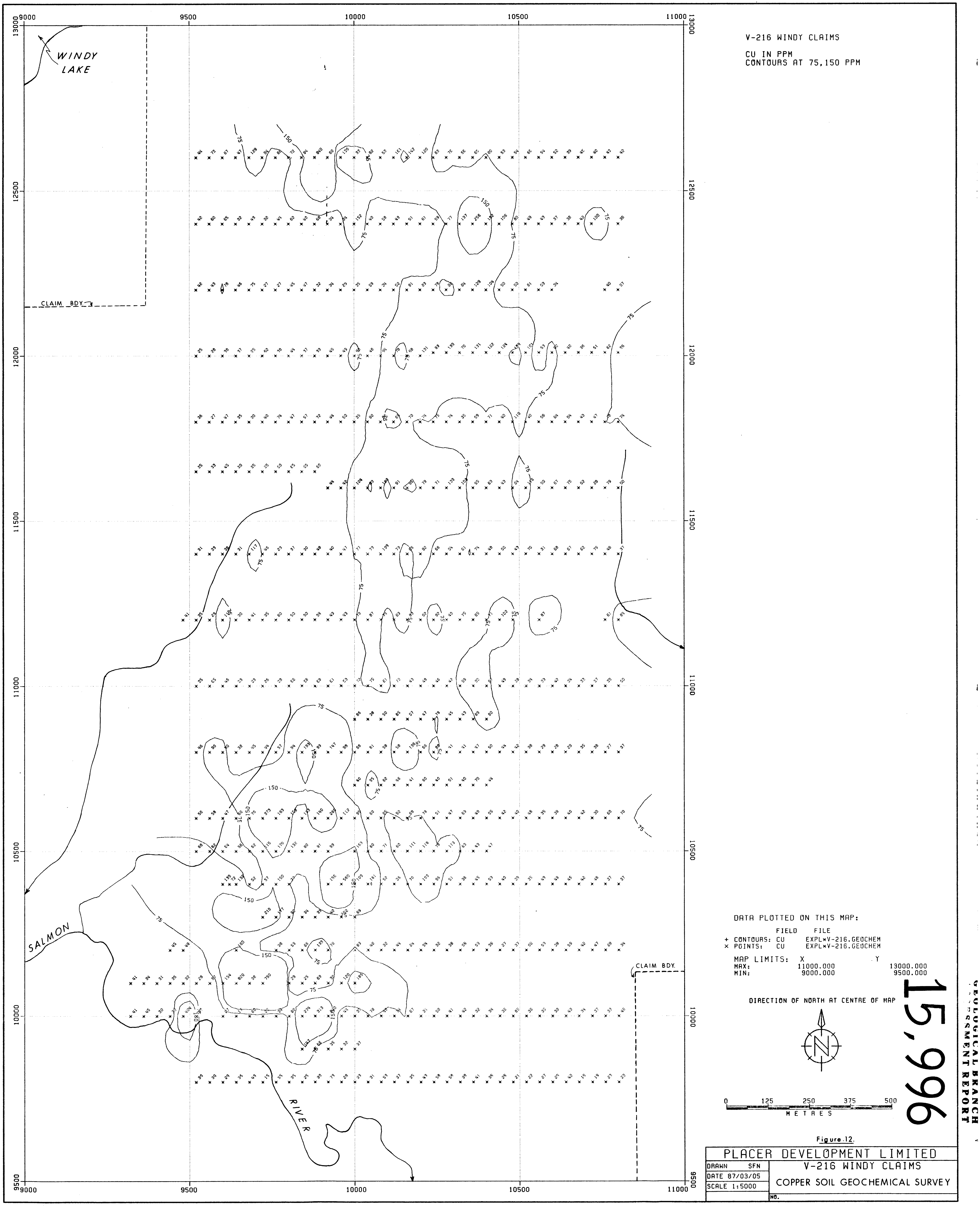
0 125 250 375 500
METRES

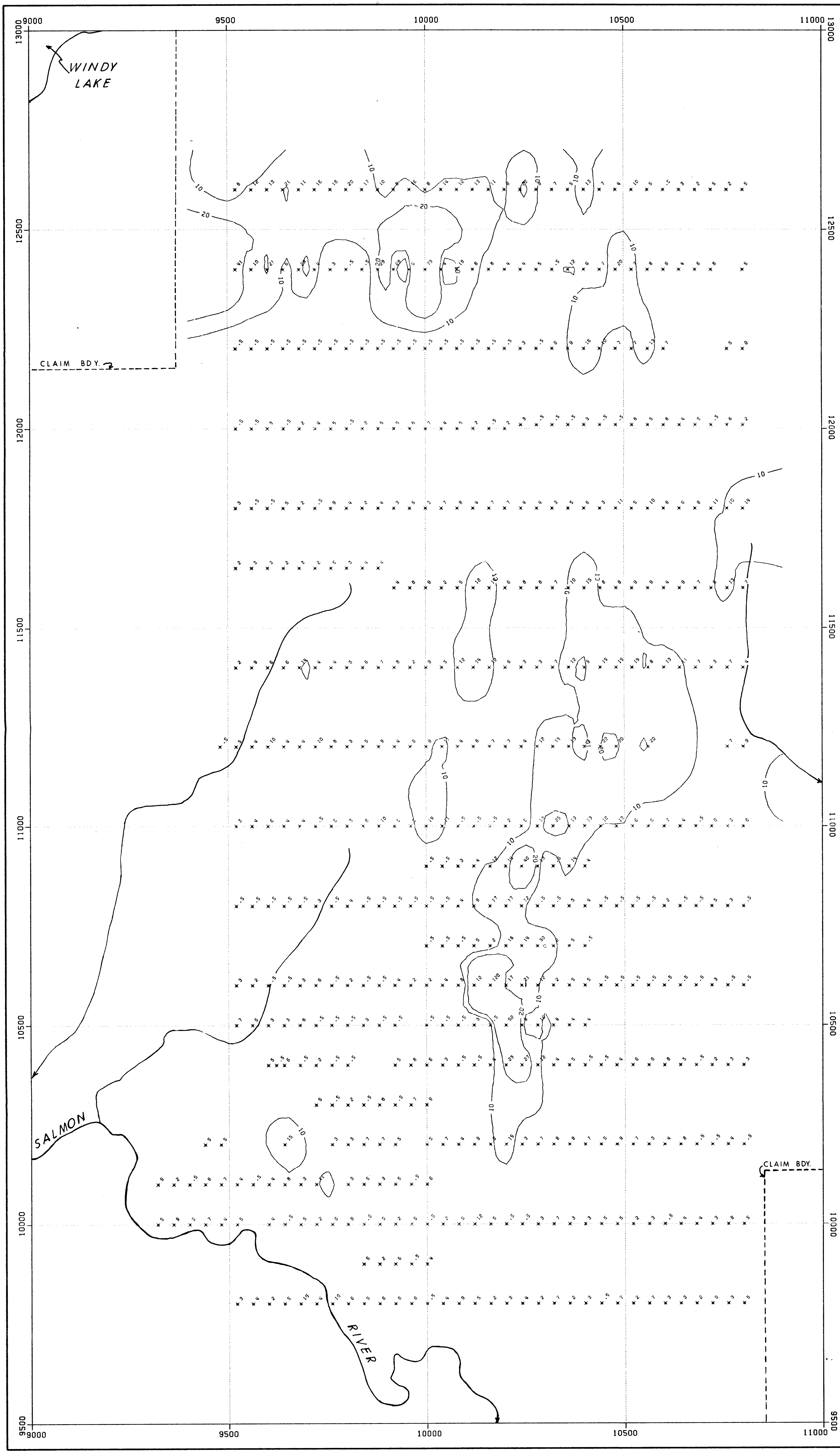
Figure 11.

PLACER DEVELOPMENT LIMITED

DRAWN SFN	V-216 WINDY CLAIMS
DATE 87/03/03	SOIL SAMPLE LOCATION AND
SCALE 1:5000	GEOCHEMICAL INTERPRETATION MAP
	NO.

15,996


V-216 WINDY CLAIMS
CU IN PPM
CONTOURS AT 75,150 PPM
WINDY LAKE
CLAIM BDY
SALMON
RIVER
CLAIM BDY.
DATA PLOTTED ON THIS MAP:
FIELD FILE
+ CONTOURS: CU EXPL×V-216.GEOCHEM
× POINTS: CU EXPL×V-216.GEOCHEM
MAP LIMITS: X Y
MAX: 11000.000 13000.000
MIN: 9000.000 9500.000
DIRECTION OF NORTH AT CENTRE OF MAP
0 125 250 375 500
METRES
Figure 12.
PLACER DEVELOPMENT LIMITED
DRAWN SFN
DATE 87/03/05
SCALE 1:5000
V-216 WINDY CLAIMS
COPPER SOIL GEOCHEMICAL SURVEY
NO.
15,996
GEOLOGICAL BRANCH
ASSESSMENT REPORT



V-216 WINDY CLAIMS

AS IN PPM
CONTOURS AT 10,20 PPM

DATA PLOTTED ON THIS MAP:

	FIELD	FILE
+ CONTOURS:	AS	EXPL*V-216.GEOCHEM
× POINTS:	AS	EXPL*V-216.GEOCHEM

MAP LIMITS:	X	Y
MAX:	11000.000	13000.000
MIN:	9000.000	9500.000

DIRECTION OF NORTH AT CENTRE OF MAP

0 125 250 375 500
METRES

Figure 13.

PLACER DEVELOPMENT LIMITED

DRAWN SFN	V-216 WINDY CLAIMS
DATE 87/03/05	ARSENIC SOIL GEOCHEMICAL SURVEY
SCALE 1:5000	NO.