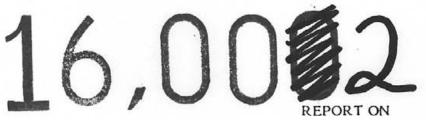
87-195-16002

GEOLOGICAL BRANCH **ASSESSMENT REPORT**



THE 1986 FIELD PROGRAM FOR THE MUSTANG MINERAL CLAIM GROUP:

MUSTANG 1, 2 AND 3 (4671, 4672, 4673)

YUZKLI AND MUSTANG CREEKS AREA CARIBOO MINING DIVISION, BRITISH COLUMBIA N.T.S. MAP AREA 93H/4W

11.5 LATITUDE 53 DEGREES 12 MINUTES LONGITUDE 121 DEGREES 46 MINUTES

Owner: G. Reidmann Operator: CANDORADO MINES LTD. 302 - 543 Granville Street Vancouver, B.C. **V6C 1X8**

SUE-RECORDER RECEIVED APR 24 1987 VANCOUVER, B.C.

Prepared by:

WAYNE ASH, P. Eng. ASH & ASSOCIATES MINING CONSULTANTS LTD. 811 - 543 Granville St. Vancouver, B.C. **V6C 1X8**

87-195-16002 RINCE GEORGE Province of Ministry of ASSESSMENT REPUBL British Columbia Energy, Mines and THE PAGE AND SUMMERY Petroleum Resources TYPE OF REPORT/SURVEY(S TOTAL COST GEOPHYSICAL; GEOCHEMICAL \$14425·63 AUTHORIS: Wayne Ash March 19, 1987 Kenneth Embree DATE STATEMENT OF EXPLORATION AND DEVELOPMENT FUED PROPERTY NAMELS COSALITE COMMODITIES PRESENT ... PD B.C. MINERAL INVENTORY NUMBERIS: IF KNOWN 93H 3Z 93 H/4W Cariboo / MINING DIVISION NTS LONGITUDE ATITUDE , NAMES and NUMBERS of all mineral tenures in good standing (when work was done) that form the property. (Examples - TAX 1-4, FIRE 2 [12 units): PHOENIX (Lot 1706), Mineral Lease M 123, Mining or Certified Mining Lease ML 12 (claims involved)): MUSTANG I (8 Units), MUSTANG Z(12 Units), MUSTANG 3 (10 Units) OWNER(S) REIDMANN GERHARD 111 MAILING ADDRESS 302-543 branville St. VancouverBe VGC IXB OPERATOR(S) (that is, Company paying for the work) Candorado Mines Ltd. (1) MAILING ADDRESS 302-543 Granville St. Vancouver, BC. VGC IXP SUMMARY GEOLOGY (lithology, age Four sequences (Devolian - Mississippian Mississippian - formian quartzites Mississippian - Permian quartzites Mississippian - Permian quartzites Mississippian - Permian diorike, basalt gabbro and serpentinite) were folded and thrust inth Post - Permian age and later metamorphosed, size, and attitude): Several phases of faulting provided channels for a gold-quartz veins generally, low is sulphides. with quantities of 12383 REFERENCES TO PREVIOUS WORK

	FENT OF WORK METRIC UNITS)	0	N WHICH CLAIMS		COST APPORTIONED
GEOLOGICAL (scale, area)					
Ground			···· · · · · · · · · · · · · · · · · ·		
> Photo					
GEOPHYSICAL (Ine kilometres)	-				
Ground MAGG 60.0 Electromagnetic EMGR. 14.	0 km 1 Km HLEM	Mustany 1,2, Mustang 1,2	3		12600.00 5460.00
Induced Polarization					
Radiometric					
Seismic					
Other	 , . 				
Airborne	••••••••••••••••••••••••••••••••••••••				
GEOCHEMICAL (number of samples enalysed for					
	b, Zn, As, As	Mustany 1, Z, 3			3575-00
Silt			•••••		
Rock	• • <i>• •</i> • • • • • • • • • • • • • • •	· · · · · · · · · · · · · · · · · · ·	• • • • • • • • • • • • • • • • • • • •		
Other			• • • • • • • • • • • • • • • • • • •		• • • • • •
DRILLING (total metres; number of holes, size)					
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RELATED TECHNICAL					
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Metallurgic					
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PREPARATORY/PHYSICAL	j j				
Legal surveys (scale, area)		••••••••••••••••••••••	· · · · · · · · · · · · · · · · · · ·	• • • • • • • • • • • • •	• • • • • • • • • • •
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Photogrammetric (scale, area) Line/grid (kilometres) LINE 83. Road, local access (kilometres) ROAD 2.	o km o km	Mustans 1, 2 Mustans 1,2	3	· · · · · · · · · · · · · · · · · ·	33000.00 / 16990.63
Trench (metres)					
Underground (metres)	, , , , , , , , , , , , , , , , , , ,				
Bala	nce-nil			TOTAL COST	\$74425.63
FOR MINISTRY USE ONLY	NAME OF PAC ACCOUNT	DEBIT CREDIT	REMARKS:		
Value work done (from report) . 196, 633.26				211	for results.
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Value claimed (from statement) . 30,000.00	CANDORADO MINES	2 La sar 13			ŀ
Value credited to PAC account 44,425.63	LTD	44,4256	about 2x	nor average	,
Value debited to PAC account	Hept. No. 87-195-16002	• • • • • • • • • • • • • • • • • • • •	Information Class (3)	0	

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SUMMARY

In November and December of 1986, Minore Mine Management Ltd. undertook a field exploration program of the Mustang Mineral Claim Group. During this period, a survey grid system, consisting of 83 km of base and grid line, was devised and installed. The baselines were installed at 1 km intervals, while the grid lines were installed at 200 m centres off the baselines. These lines were well flagged and marked with ribbon at 25 m stations, where samples or geophysical readings could be taken.

When the survey lines were in, soil sampling and geophysical testing was conducted. Some 134 soil samples were collected for geochemical analysis. A VLF-EM survey was conducted, but only 14.1 km of line were surveyed. Bad weather conditions, including deep snow and freezing temperatures, put an early end to the soil sampling and VLF-EM survey programs. An extensive magnetic survey was performed, but was called off just short of completion, due to weather and the approaching Christmas holiday.

The soil sampling and magnetic survey failed to locate any strongly anomalous zones. There were some high readings, but these were still too low for major concern. On the other hand, the VLF-EM survey discovered some highly anomalous areas. An examination of these anomalies indicated that, in some cases, they could be correlated from grid line to grid line, along the known strike of local geological features.

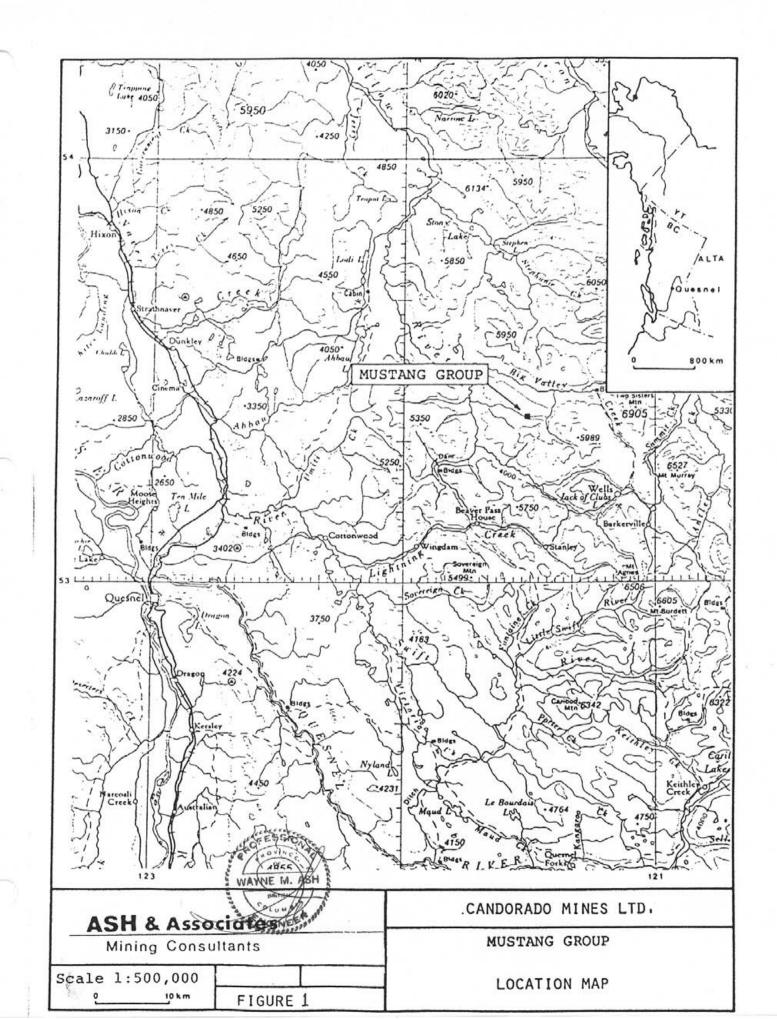
With the completion of the 1986 field program, several questions remained unanswered. In order to complete the work on the property, it is recommended that more exploration work be conducted in the summer of 1987. This proposal is in two phases. In Phase 1 it is proposed that the VLF-EM survey be continued and that it be accompanied by reconnaissance geological mapping. In Phase 2, it is proposed that trenching and sampling be conducted in the areas deemed interesting by Phase 1. The total cost of the proposals is estimated at \$44,550.00. This report was prepared at the request of the Directors of Candorado Mines Ltd., of 302 - 543 Granville Street, Vancouver, B.C. This request concerns assessment work carried out by Minore Mine Management Ltd. on the Mustang Mineral Claim Group.

The Mustang Claims are located northwest of Wells, B.C. and consist of three large claims totalling approximately 1,300 hectares of land area. During the fall of 1986, soil and geophysical surveys were conducted on these claims, the results of which are the subject of this report. The majority of the work was carried out after a layer of snow had fallen and therefore limited soil sampling and no geological reconnaissance mapping was under taken.

Due to adverse weather conditions the soil sampling and VLF surveys were curtailed and only the grid survey and magnetometer survey were completed. A recommendation for additional work totalling an expenditure of \$44,550.00 is proposed.

LOCATION AND ACCESS

The claims are situated 16 kilometers northwest of Wells, British Columbia (Figure 1), just south of Big Valley River, at approximately 53 degrees 12' latitude and 121 degrees 46' longitude. The National Topographic System map sheet for the area is 93H/4. The property is accessed on the east side by road near the confluence of Mustang and Sugar Creeks, $1\frac{1}{2}$ kilometers east of the property. Two roads can be used to reach this point, the better of these being the Beaver Pass route which branches northwest off Highway 26, the Quesnel-Barkerville Highway. The turn off is situated about 25 kilometers west of Wells. The access road, for the most part, is a gravelled logging road in very good condition which extends 40 kilometers north and east to a point where Sugar Creek joins Big Valley Creek. From this point a 4x4 bush road, which was roughed out many years ago and completed in 1983, follows Sugar and Mustang Creek to Yuzkli Lake in the north central part of the property.



There are several meadows in the valley of Yuzkli and Mustang Creeks where helicopters may land. Further, a float plane could land on Yuzkli Lake. An abandoned mining road also reaches Mustang Creek via Wells and Hardscrabble Creek. This route is about 15 kilometers long, but is presently not passable due to washouts.

PHYSIOGRAPHY AND CLIMATE

In general, the topography of the area is mountainous and the relief on the property ranges from 1,200 m to 1,625 m. Two major mountain ridges trending east-west pass through the property. The access road to the property is between the two ridges, the Mustang Creek Valley, on the central claim. Valley walls on the property slope steeply and in some localities approach 75% (or 37 degrees). The upland areas tend to be low in relief, making traversing in these locations relatively easy.

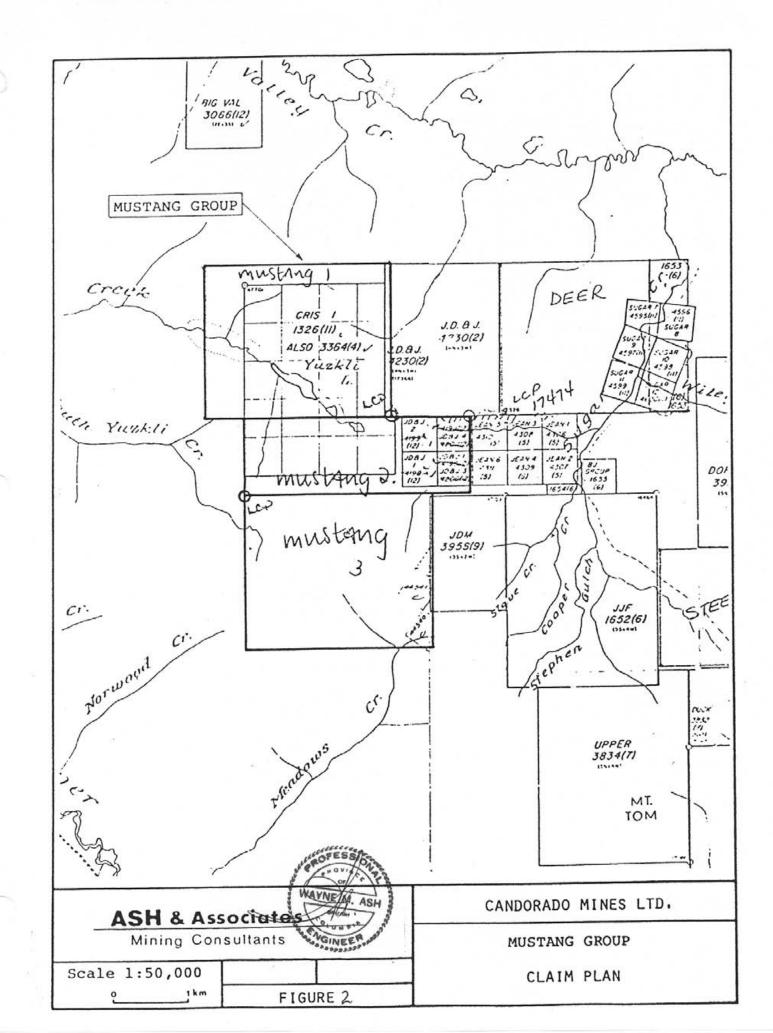
The property is totally covered by trees consisting primarily of pine and cedar varieties typical of the area. The annual precipitation is about 77 centimetres, the majority of which falls during autumn and spring. The average snowfall is about 305 centimetres and occurs from October to May. The mean annual temperature is 3 degrees (and varies from -25 degrees C to +45 degrees C).

OWNERSHIP

The property consists of three lode claims (Figure 2) that have been held by Candorado Mines Ltd. since 1983. A summary of the particulars of the claims is listed as follows and a notice to group the claims was recorded on March 14, 1983.

Claim Name	Record No.	Units	Recording Date	Registered Holder
Mustang 1	4671 (2)	20	Feb. 25, 1983	Candorado Mines Ltd.
Mustang 2	4672 (2)	12		Candorado Mines Ltd.
Mustang 3	4673 (2)	20		Candorado Mines Ltd.

The writer does not accept responsibility for the legal status of these claims.



HISTOR Y

The Cariboo district is one of the oldest gold mining camps in British Columbia, the first prospectors arriving in 1858. The early miners focused on placer deposits, but by the 1880's gold quartz veins were being mined.

The property lies at the northeast end of the Barkerville Gold Belt, a northwest alignment of gold-quartz veins, gold bearing pyrite ore bodies and placer deposits.

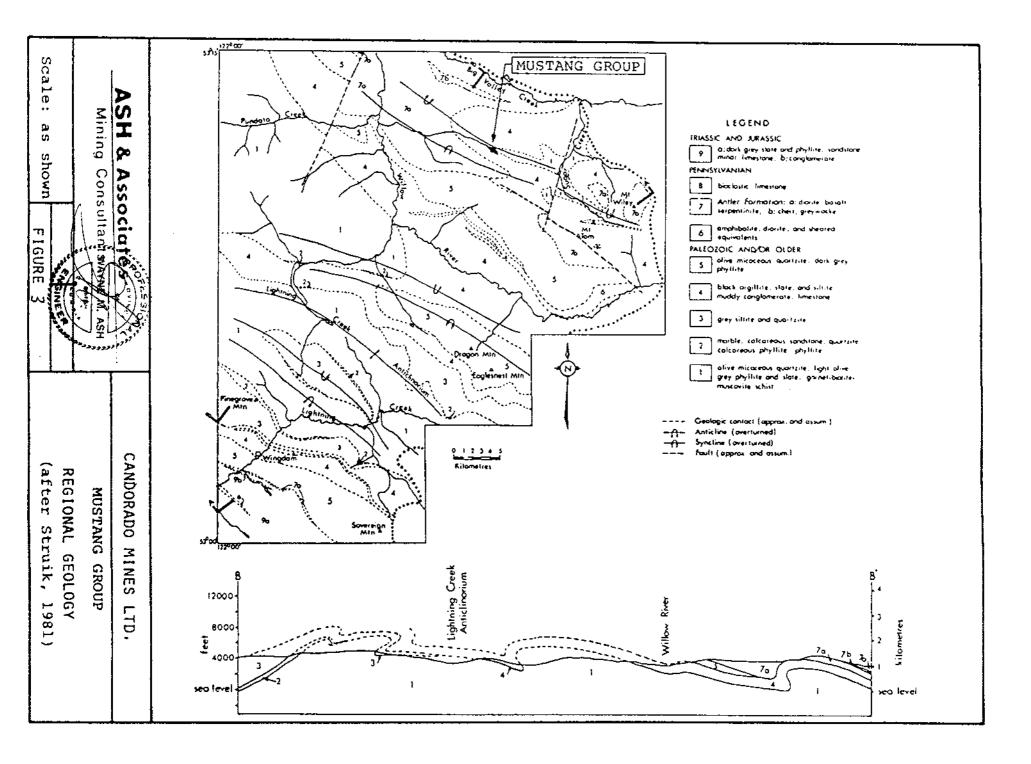
On the property there are two known gold occurrences that received some prospecting and surface development in the 1930's. The more developed of these is the Cosalite prospect (No. 1), $\frac{1}{2}$ kilometers north of Yuzkli lake. Quartz veins in quartzite ore were reported to have contained pyrite and galena bearing a trace of gold. There are at least four places where quartz veins were exposed by shallow surface workings. The veins are described as being from 9 inches to 4 feet wide and up to 100 feet in length.

The second known gold occurrence is at the headwater of South Yuzkli Creek. This occurrence (No. 3) is shown by Hanson (1938a) on his geological map of the area. The occurrence is summarized together with a number of other quartz vein prospects as being from a few inches to 10 feet wide and mineralized with pyrite and galena with low gold values.

GEOLOGY

a) Regional (from K.V. Campbell 1985)

Figure 3 illustrates an interpretation of the regional geology (Struik, 1981a) with the stratigraphy outlined in the legend. The area lies along the western part of the Omineca Tectonic Belt, known for its prevalence of gold and tungsten mineral occurrences. Two regional stratigraphic sequences are shown in Figure 3. These are (1) Upper Ordovician to Permian shale, dolstone, basalt, conglomerate and limestone (units 1 to 6 and 8, Figure 3) and (2) Permian and Pennsylvanian oceanic chert and mafic and ultramafic volcanic and intrusive rocks (unit 7, Figure 3). The



latter sequence, the Antler Formation, has been thrust from the west over the basinal sequence. A third stratigraphic sequence of Hadrynian to Cambrian quartzite, carbonate and shale, representing a continental terrace wedge, is exposed to the east of the area shown in Figure 3.

Eastward thrusting of the Antler Formation commenced in post-Permian time and predated the folding and regional metamorphism of Jura-Cretaceous age that affected all rock units in the area. The major folds, such as the Lightning Creek anticlinorium, 25 km southwest of Yuzkli Lake, are relatively open. The Mustang property straddles an overturned fold couplet whose axial planes dip nor theast.

The principal axis of the Barkerville Gold Belt, passing through Island Moutain and Barkerville, is located on the overturned limb of a northwest trending fold at or near the contact between Devonian-Mississippian black phyllites (unit 4, Figure 3) and micaceous quartzites containing limestone and dolomite (unit 1, Figure 3). The gold occurs mainly in pyrite or as free gold in quartz veins in the black metaclastic rocks. Gold also occurs in stratabound, massive, auriferous pyrite lenses and shoots, termed 'replacement ore', within and at the contacts of limestone beds in micaceous quartzite (Alldrick, 1983). Of critical importance to the mineral potential of the Mustang property is that this same structure passes through the claims area and affects the same rock units.

Several phases of faulting have affected the area. These are, listed from youngest to oldest, as follows (Struik, 1981b, 1982):

- (1) northerly and north-northeasterly right lateral strike slip faults,
- (2) transverse northeast trending normal faults,
- (3) east dipping high angle reverse and normal fault, and
- (4) east dipping thrust faults.

Quartz veins are common and widely distributed in the area. In general the sulphide content is low, but in certain areas they contain a fairly consistent quantity of pyrite with attendant gold (Sutherland Brown, 1957). Previous workers have all noted the pattern of occurrence of quartz veins. Four types of veins are recognized, as follows:

- transverse veins; northeast strike, smallest and most numerous type, at the Cariboo Gold Quartz Mine provided 60-75% of the Quartz ore,
- (2) diagonal veins; east-northeast strike, larger and fewer than transverse veins, at the Island Mountain Mine only the diagonal veins were mineable,
- (3) northerly veins; north-northeasterly strike, occur within faults, commonly crushed and difficult to mine, and
- (4) strike veins; northwest strike, subparallel to foliation, largest and fewest type, normally barren.

Earlier workers termed the strike veins 'A veins' and the transverse and diagonal veins 'B veins'.

Recently (Struik, 1981b), it has been recognized that the Paleozoic sedimentary units making up most of the area contain stratigraphic equivalents of the major divisions of the Selwyn basin; the Ordovivian to Devonian Road River Formation and the Devono-Mississippian Earn Group, informally called the "black clastics". Theses units are hosts for stratiform lead and zinc deposits in the northern Cordillera. In the Cariboo district the Black Stuart Formation (equivalent to unit 4 in Figure 3) and the Greenberry Limestone Member (unit 8 in Figure 3) are time and lithologic correlatives of the black clastic units in the northern Omineca and Mackenzie - Rocky Mountain belt. The recognition of this correlation gives the Mustang property the potential of having similar deposits.

b) Local Geology

Figure 4 illustrates the geology of the Mustang claims areas as mapped by Struik (1982). Table 1 provides an explanation of the rock units in Figure 4 and their correlation to those shown in the earlier work (Figure 3).

There are four rock units underlying the property: DMs - predominantly black phyllite; MPt - mostly olive gray micaceous quartzite, MPd - olive and gray micaceous quartzite, pllite and schist; and MPav (Antler Formation) - diorite, basalt, gabbro and serpentinite. Units DMs and MPd are the same units that host the majority, if not all, of the gold deposits along the Barkerville Gold Belt.

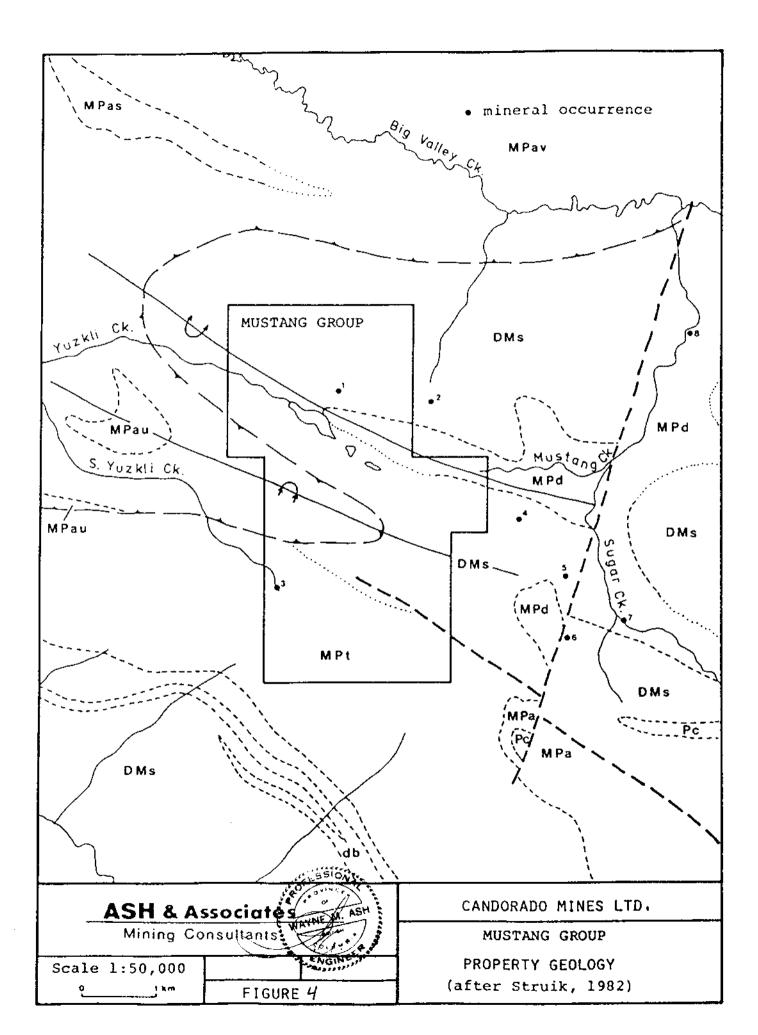


TABLE 1

Explanation of Figure 4 -- Property Geology

Rock U	nits Description	
PERMIAN		
Pc	 gray crinoidal limestone, minor gray cher t 	
and PERMIAN), PENNSYLVANIAN	
Antler For MPay		
MPas	 diorite, basalt, serpentine, gabbro olive and gray chert, black and green slate 	
MPau	- serpentine, sheared mafic rocks	
MISSISSIPPIAN	?) to PERMIAN(?)	
MPt	- Tom Creek Succession; olive gray micaceous guartzite, phyllite and schist	
MPd	 Downey Creek Succession; olive and gray micaceous quartzite, phyllite, gray olive and green slate, limestone, marble 	
MPa	- amphibolite	
db	- diabase	
DEVICINITANI(2)	nd MISSISSIPPIAN(?)	
DMs	- black siltite, phyllite, gray micaceous	
	quartzite, limestone	
	Fracture	
	Thrust fault	
	Geological contact (approximate, assumed)	
	Anticline, over turned	
\frown	Syncline, overturned	

Correlation to Figure 3:	Figure 3	Figure 4
	Unit 8	Pc
	Unit 7	MPav, MPas, MPau
	Unit 6	db
	Unit 5	MPt
	Unit 4	DMs
	Unit 1	MPd

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The foliation of most of the exposures dips northeasterly at moderate to steep angles. The claims are crossed by an overturned, northwest trending syncline and anticline, whose approximate locations are indicated in Figure 4. The general structure is shown in the geological section B-B' of Figure 3.

'Major faults in the area, as mapped by Struik, are the north-northeasterly fault in the lower course of Sugar Creek and the northwest fault that is projected into the south part of the claims group. A thrust fault marks the base of the Antler Formation. A characteristic of this fault is the flat lying shearing developed below it. Other fractures belong to the northwest and north-northeast fault and fracture sets. Recalling that many ore deposits in the region are controlled or spatially related to north-northeasterly faults (Sutherland Brown, 1957), fractures with the latter orientation should be prospected.

c) Geomorphology

The higher parts of the property, characterized by gently rolling hills, are remnants of a Tertiary plateau. The melting of a static ice sheet which covered this surface in the Pleistocene resulted in a lodgement till deeply cut by meltwater gullies. Many of these are today occupied by only small, intermittent streams. In a few places these gullies extend to bedrock. The depth to bedrock in areas underlain by the lodgement till is estimated to be up to 6 m.

A valley glacier occupied the northwest trending valley of Yuzkli and Mustang Creeks. Its stagnation and wasting resulted in moraine deposits and a kettled aspect along this valley. The depth to bedrock in the valley is estimated to be up to 30-40 m.

Several creeks on the Mustang Group have alignments parallel to the regional fracture sets, particularly those trending north-northeast, northeast and northwest.

d) Lithology

The property is mostly underlain by Paleozoic metasedimentary and metavolcanic rocks. The metasedimentary rocks are black phyllite and siltite and gray

micaceous quartzite. Quartz veining is widespread. These rocks are the host to most of the gold occurrences in the Cariboo district. The presence of limestone and dolomite on the Mustang group is suggested by abundant float of the same north and south of Yuzkli Creek.

The metasedimentary rocks are overthrust by basalt, gabbro and serpentine of the Antler Formation.

e) Stucture

The claims are crossed by a northwest trending anticline and syncline that are overturned to the southwest. The penetrative foliation of the rocks dips mostly north and northeast. Fractures trend northwest, north-northeast and northeast. At the base of the Antler Formation in the western part of the claims is a thrust fault below which the rocks are intensely sheared. Minor folding and complex cleavage and foliation relations can be expected throughout the area.

f) Mineralization

Previous work in the area focused on gold-quartz veins and there are two such known historical mineral occurrences on the property; (1) the Cosalite prospect north of Yuzkli Lake - a number of pyrite and galena-bearing quartz veins with low gold values, and (2) a similar occurrence on the south fork of Yuzkli Creek. Representative samples of vein quartz from both these locations were sampled in 1983. The sample from the Cosalite prospect assayed 0.52 oz/ton Ag, 0.001 oz/ton Au with 1.81% Pb. The sample collected from the south fork of Yuzkli Creek assayed 0.01 oz/ton Ag and 0.001 oz/ton Au. Such minimal values are to be expected where surface leaching of fractured quartz has removed precious metals.

Two types of gold mineralization are considered to be possible on the Mustang group; quartz vein mineralization and pyritic replacement in limestone. The claims lie at the northwest end of the Barkerville Gold Belt aligned along an overturned fold developed between black phyllite and gray micaceous quartzite. Gold-bearing pyritic replacement ore is found in a limestone member in the quartzite unit adjacent to its contact with the black phyllite. Gold-quartz veins are most common and best developed along north-northest trending faults.

The Mustang group has good potential for having deposits similar to those found to the southeast for the following reasons:

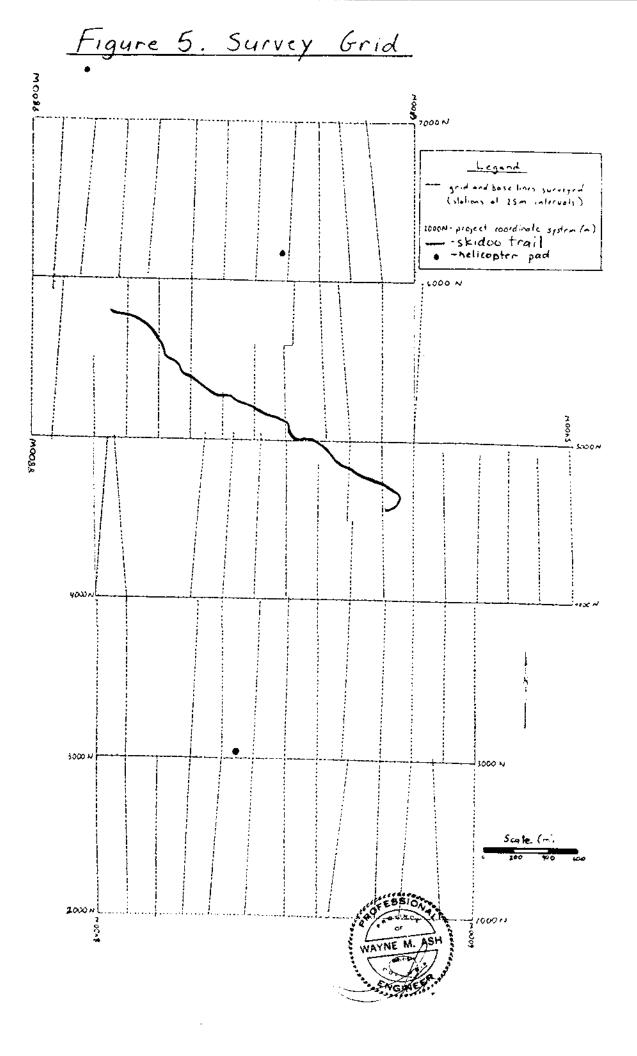
- (1) Continuity of lithology; presence of the same rock units that host gold deposits along the Barkerville Gold Belt.
- (2) Continuity of structure; the same fold structure that controls gold mineralization to the southeast extends across the property.
- (3) The presence of north-northeast and northeast trending fractures that localize gold-quartz veins along the Gold Belt.
- (4) The presence of several mineral occurrences on and near the property.

Reconnaissance geochemical silt sampling was performed in 1983 along the major drainageways. Analyses were made for arsenic, lead, silver and zinc. Virtually all the anomalies, a total of 14, are over the black phyllite and siltite unit. Half of these are located over the overturned fold limb that involves the critical geological contact of interest, that between units DMs and MPd. This lends further support to the view that there is a good potential of mineralization in the area between the traces of the two overturned fold axes. The other half of the anomalies have a close spatial relation to known mineral occurrences including sulphide-mineralized float. These are found over the black phyllite unit (DMs).

1986 FIELD EXPLORATION PROGRAM

The field work proposed for 1986 included geological mapping, geophysical surveys and soil sampling. Due to the late time of year for conducting the work, geological mapping could not be carried out and only geophysical surveys and soil sampling were undertaken.

Since the area is large and the topography rugged, the relief in some areas being very high, it was decided at the outset of the program to lay out baselines and section lines that would have closure documentation. Soil sampling was conducted



until the depth of snow and ground freezing did not permit effective sample taking. Likewise, the VLF surveys were discontinued half-way through the program due mainly to the difficulties encountered with negotiating the heavy equipment in deep snow. Some problems relating to malfunctioning of the equipment that resulted from cold weather also contributed to the decision to discontinue from VLF geophysical surveys. Magnetometer surveys and grid layout were carried out nearly to the end of the program when, again, inclement weather and the approaching Christmas holiday season shut down these activities.

Survey Grid

Approximately eighty-three (83) kilometers of Baselines and Closure section lines were installed (Figure 5). Stations where sampling or readings would be conducted were located at 25 meter centres. The lines were well marked with ribbon and the stations were labelled.

Table 2 shows the closures recorded and includes locations where closures were not documented. As the strike of the major geological features trended east-west, the baselines were installed east to west such that the grid lines would cross these features at approximately 90 degrees. Six baselines 1 kilometre apart were installed. The grid or section lines were installed at 200 metre centres, each having stations at 25 metre intervals. Baselines were installed using split chainage and slope corrections.

As the installation of the survey grid progressed, a skidoo trail was required to reach more remote areas of the property. The skidoo trail required three days and two men to construct it and was approximately 2 km long. When even more remote areas had to be accessed, a helicopter was used. Three helicopter pads were constructed on the property and one at the base camp. These pads required four days to build (Figure 5).

TABLE 2	

Survey Closures

Line	2000 - 3000	3000 - 4000	4000 - 5000	5000 - 6000	6000 - 7000
5400			5420, 4950	.	
5600			5625, 4930		
5800			5800, 4965		
6000	6075,2000	6020, 4000	5980, 4940		
6200	6260, 3020	N.A.	6215, 4955		
6400	6465, 2000	N.A.	OK met at swamp in middle	6350, 6000	6400, 7000
6600	6670, 2020	6575, 3985	6585, 4035	6600, 5990	6700, 7025
			6820, 4510		
6800	6915, 2030	6840, 3025	6780,4490	6880, 5980	687 <i>5</i> , 7035
7000	N.A.	7000, 3975	7000, 4850 (lake)	6950, 5025 7250, 5690	N.A.
7200	N.A.	7185, 4010	7200, 4000	7200, 5690	7150, 7000
7400	7450, 2015	7370, 3960	7340, 5060	7400, 5600	7360, 7020
7600	7675, 2000	N.A.	7525, 5075	OK meets in middle (lake)	7 <i>5</i> 75, 7030
7800	7840,2000	7760, 3960	7750, 5045	84	7770, 7030
8000	8015, 1968	line not in	line not in	et.	5070, 6040
8200	8180, 1967	N.A.	8280, 4000	N.A.	8255, 6000
8400	8400, 2000	8385, 3960	8325, 4995	8400, 5500 half way	8495, 6020
8600				8665, 5000	8670, 5920
8800				8800,6000	8800, 7000

NOTE: N.A. indicates closure notes are not available and a straight closed line for ploting purposes was assumed.

Soil Survey

During the first week of the field program some 134 soil samples were taken at 50 metre intervals in the locations shown on Figure 6. The samples were analyzed for copper, lead, zinc, silver and arsenic. The results are shown in Appendix I.

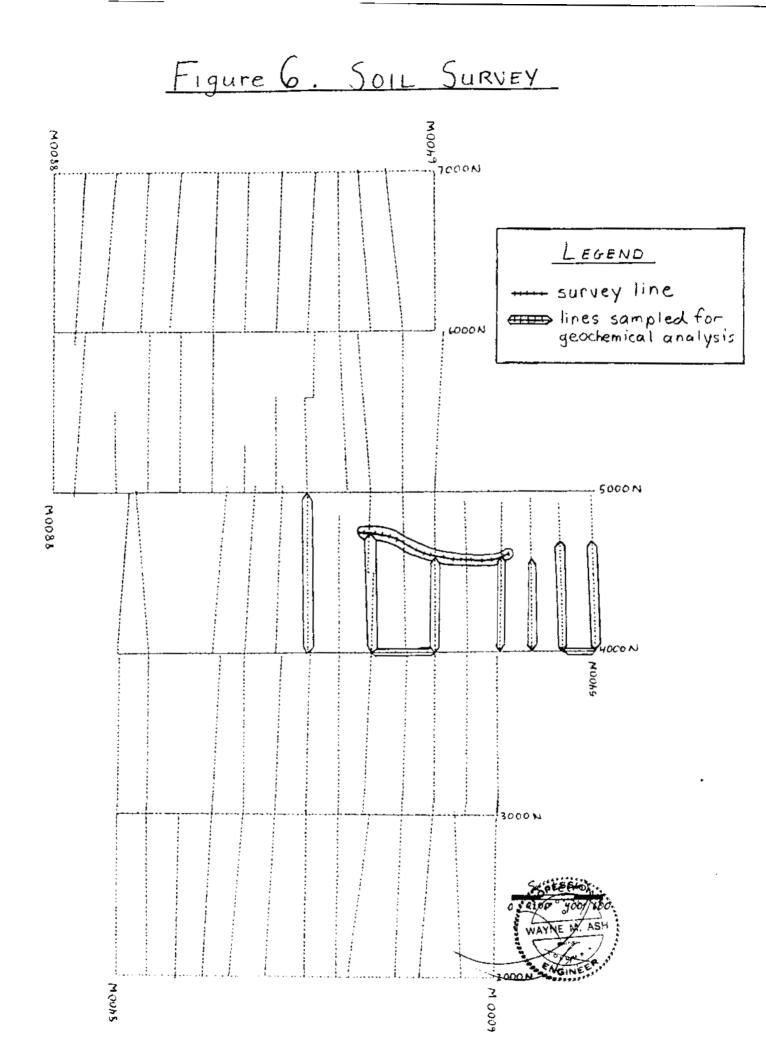
The area is an eluvial landscape where the soils are generally well drained and precipitation exceeds evaporation. Based on the Canadian system of soils classification, the soil in the area would be classified Podzolic.

The field personnel studied the soil and land form relationships in the area and concluded that the major portion of the soils are glacial till and the samples taken were for the most part not residual and therefore likely did not represent the mineral content of the subsurface rock formations. The depth of organic matter (except in muskegs) and the horizon of alluviation (leaching) are very thin in the areas surveyed. Therefore, the major portion of samples taken were from the horizon of illuviation (the horizon enriched in clay minerals). The basic statistics for these samples are as follows:

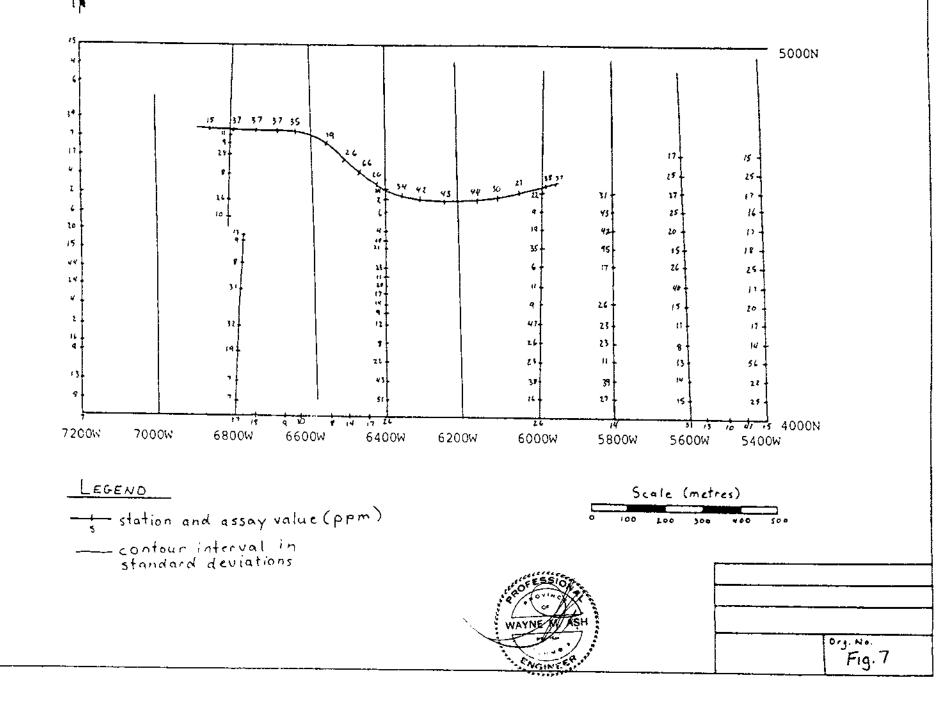
Metal Analyzed	No. of Samples	Mean ppm	Standard Deviation ppm	Lowest Value ppm	Highest Value ppm
Copper	134	21.6	3.19	2.0	95.0
Lead	134	23.2	1.81	2.0	103.0
Zinc	134	67.5	9.59	8.0	282.0
Silver	134	0.5	0.01	0.1	3.6
Arsenic	134	12.2	1.64	2.0	67.0

The mean, standard deviation and variances were calculated for each element, both normally and log-normally. This statistical analysis is located in Appendix II.

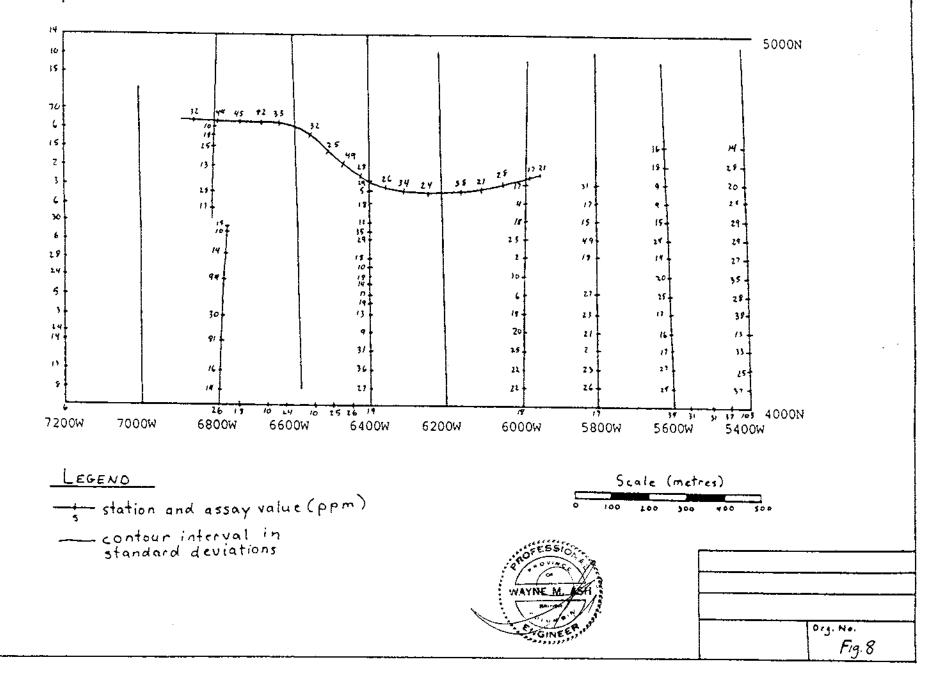
The locations of the survey points and results of the geochemical analysis for copper, lead, zinc, silver and arsenic are shown in Figures 7, 8, 9, 10 and 11, respectively. An inspection of the data reflected the east to west trend of the geological structures.

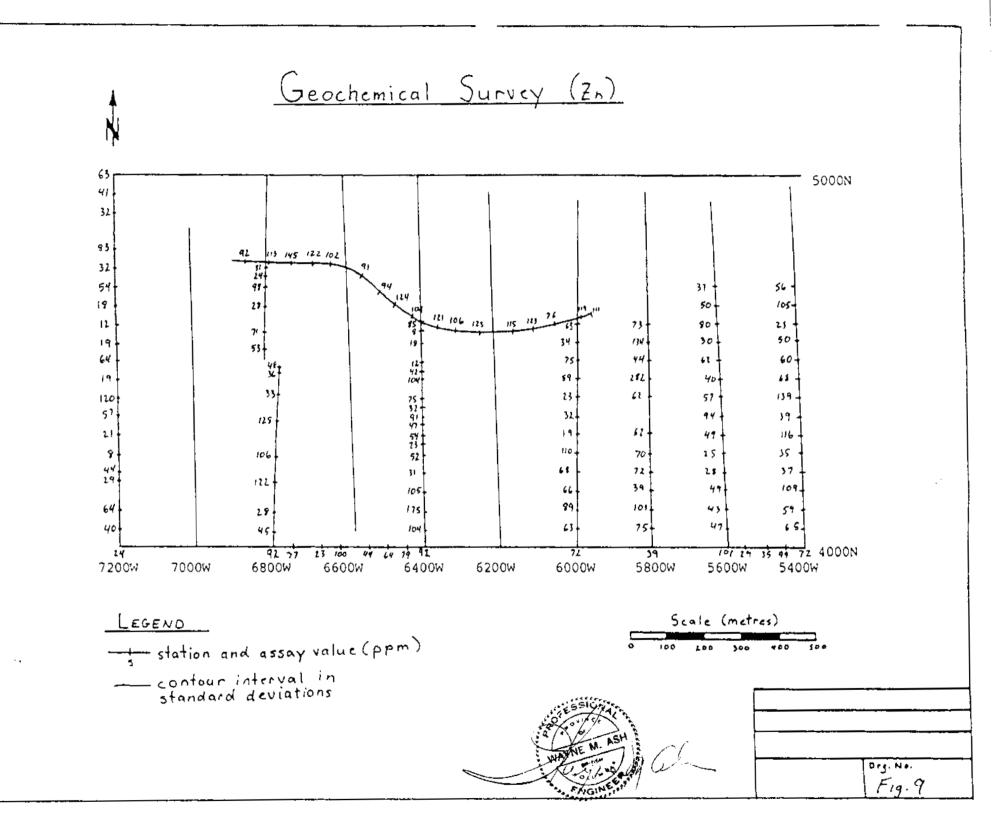


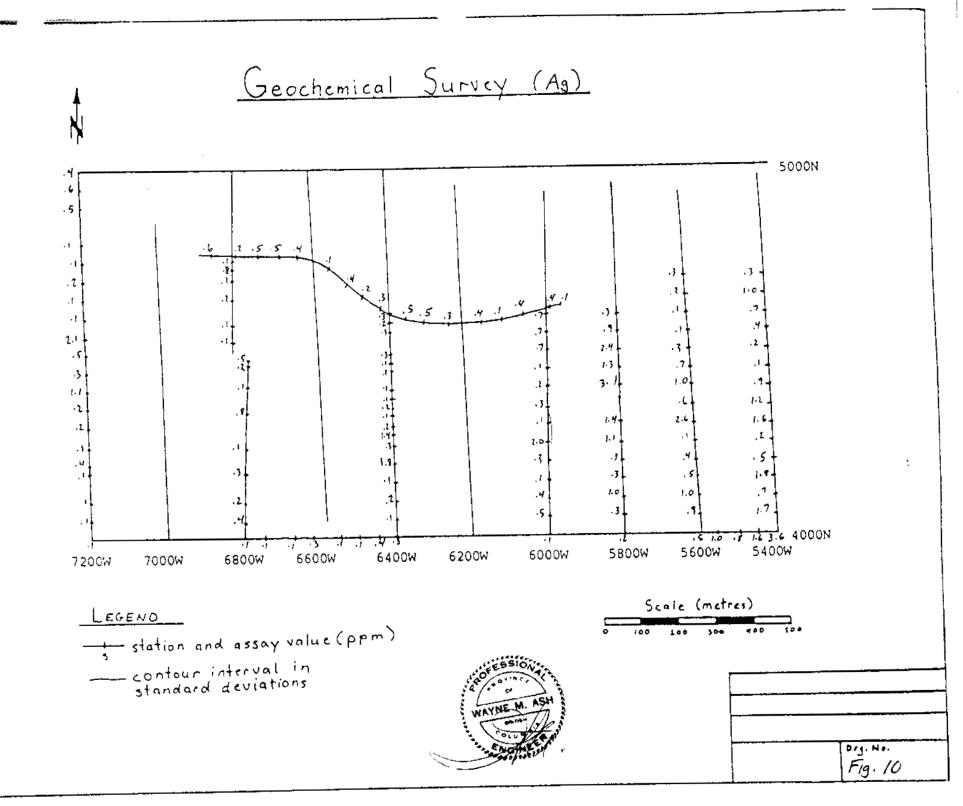
Geochemical Survey (Cu)



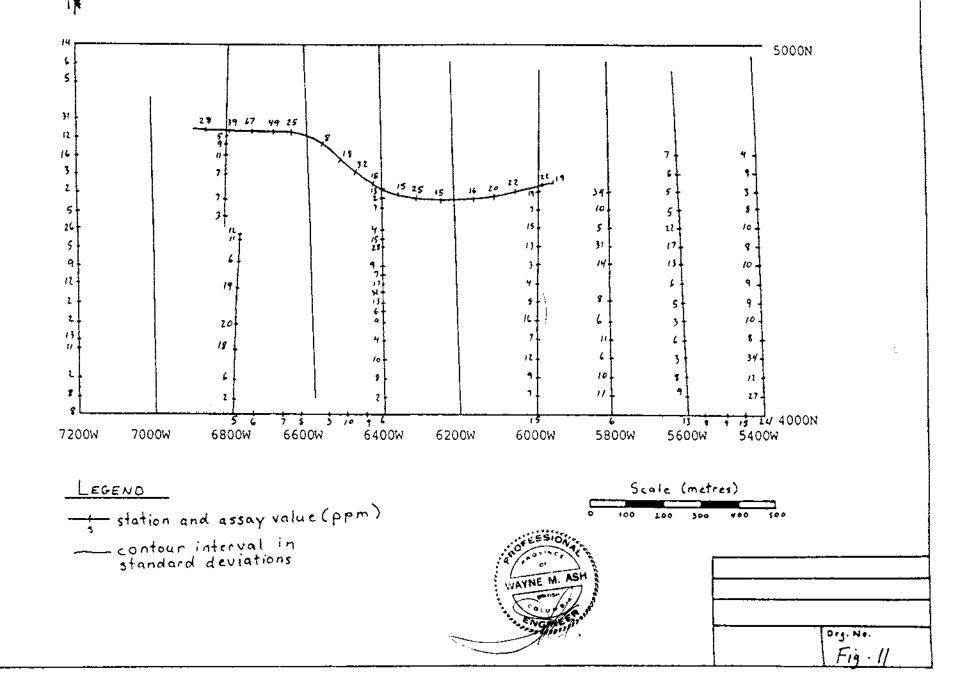
Geochemical Survey (Pb)







Geochemical Survey (As)



VLF-EM Geophysical Survey

Some 1,200 VLF-EM readings were taken at 12.5 metre intervals along the grid shown in Figure 12, respresenting 14.1 kilometres of grid line. The VLF-EM survey employed the SE-88 Genie electromagnetic system. This system is designed mainly for use in mineral prospecting for massive sulphide ore bodies. It is also useful for defecting faults or shear zones and for obtaining information about subsurface conductivity for geological mapping.

The system consists of a transmitter and receiver weighing 15 kg and 4 kg, respectively. It is designed for rapid two-person operation and minimizes geometrically derived errors. The measurements are based on the simultaneous transmission of two pre-selected, well separated frequencies and the comparisons of the amplitudes of the two signals at the receiver. The two transmitted frequencies are picked up by a single receiving coil, amplified and noise filtered. A proportional D.C. voltage is obtained from each signal, averaged over a selectable time period, and then the computed result x 100 is displayed in percent on the digital display with a resolution of 0.1%.

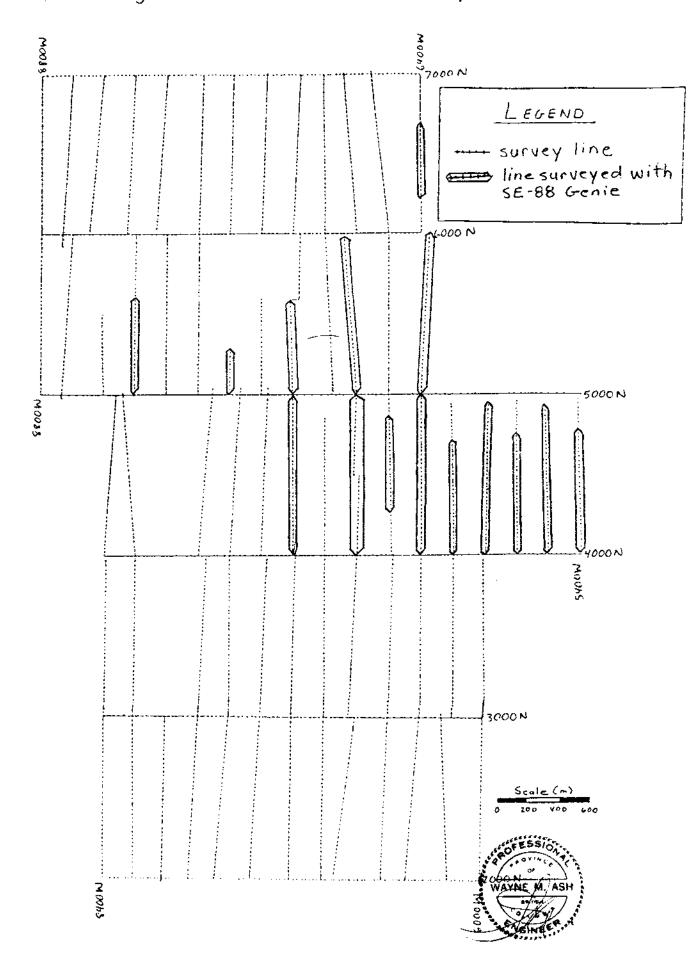
Under most field conditions, the system, whose sensitivity and repeatability are basically only limited by atmospheric noise, can detect amplitude ratio changes to better than 0.5%. Useful measurements may be made for a transmitter-receiver separation of 200 metres. Fifty (50) metres separation was used on the Mustang Property and readings were taken at 12.5 metre intervals along each grid line surveyed.

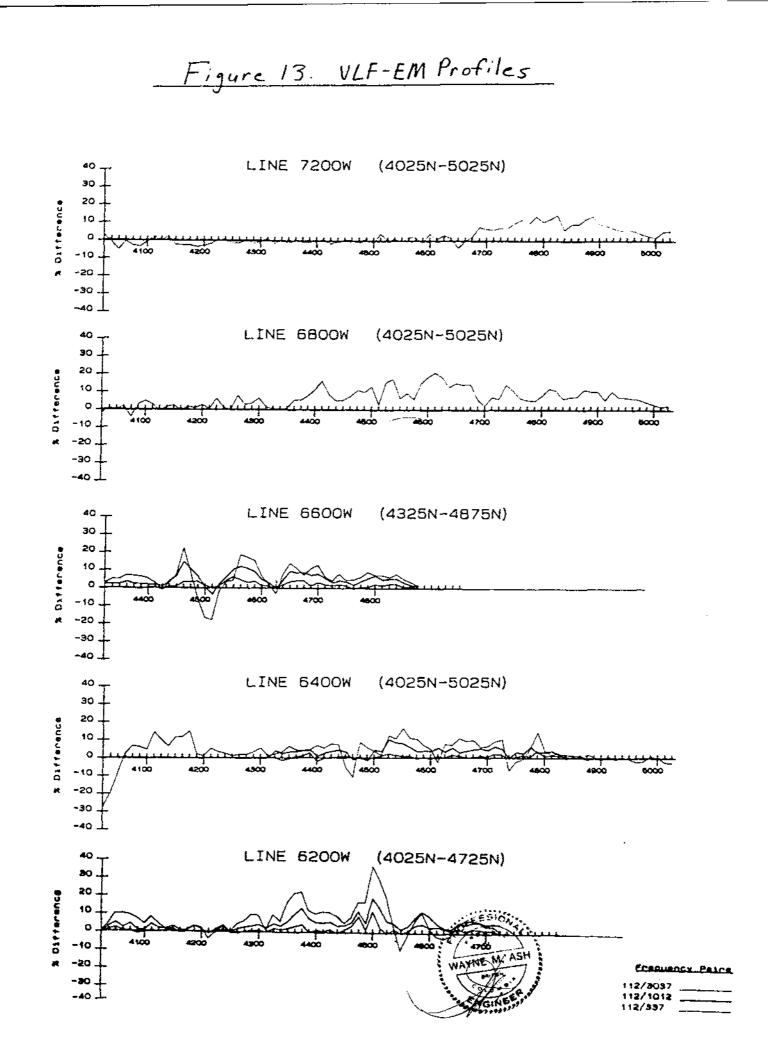
The frequency pairs used in the survey were 112 Hz / 3037 Hz, 112 Hz / 1012 Hz, and 112 Hz / 337 Hz. The field readings required no further filtering and were plotted directly. Since this system has, for the most part, eliminated all noise, the greater portion of readings taken show very little amplitude ratio change. The field operating strategy was as follows:

 To save time for the field crew, one set of readings was taken. The frequency pair used was 112 Hz / 3037 Hz, the frequencies that differ the most. This frequency pair shows the strongest amplitude ratio change.

Figure 12. VLF-EM Survey

N ---





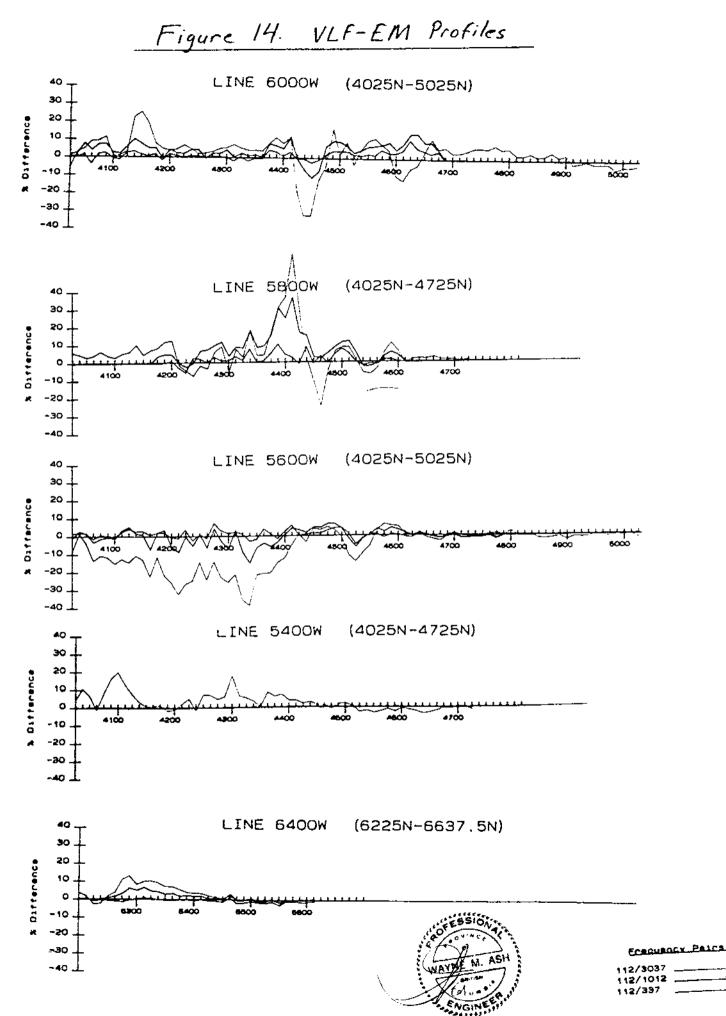
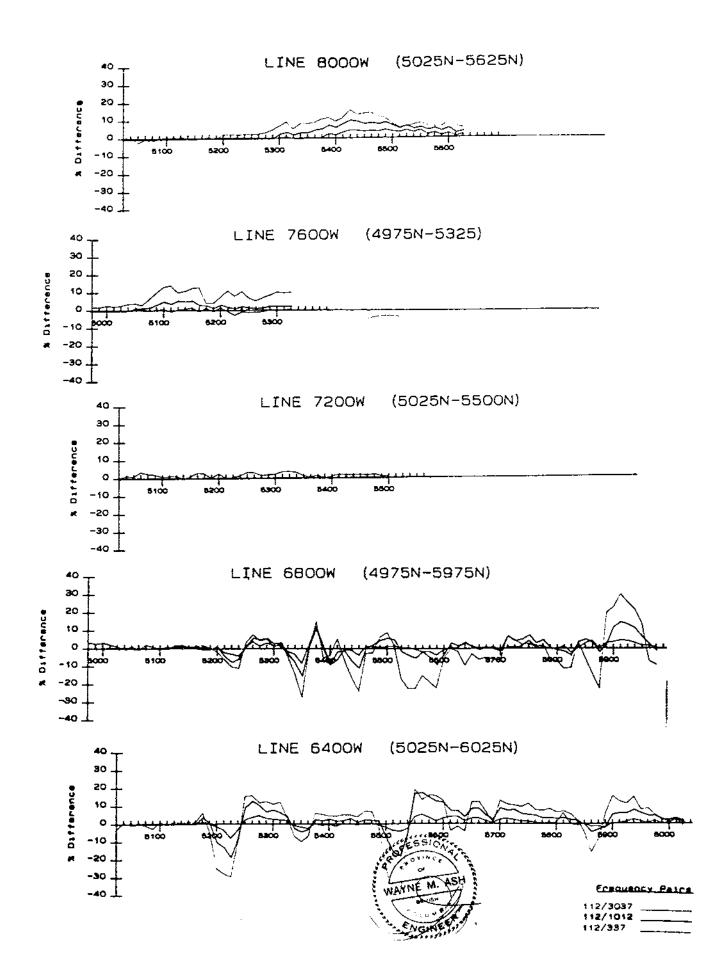


Figure 15. VLF-EM Profiles



2. When the first frequency pair shows a strong, anomalous amplitude ratio change, all three frequency pairs are used. As soon as the readings level off, the field crew returns to using the first frequency pair alone.

The field readings for the VLF-EM survey are in Appendix III. The plots of the data, showing anomalous readings, are in Figures 13, 14 and 15.

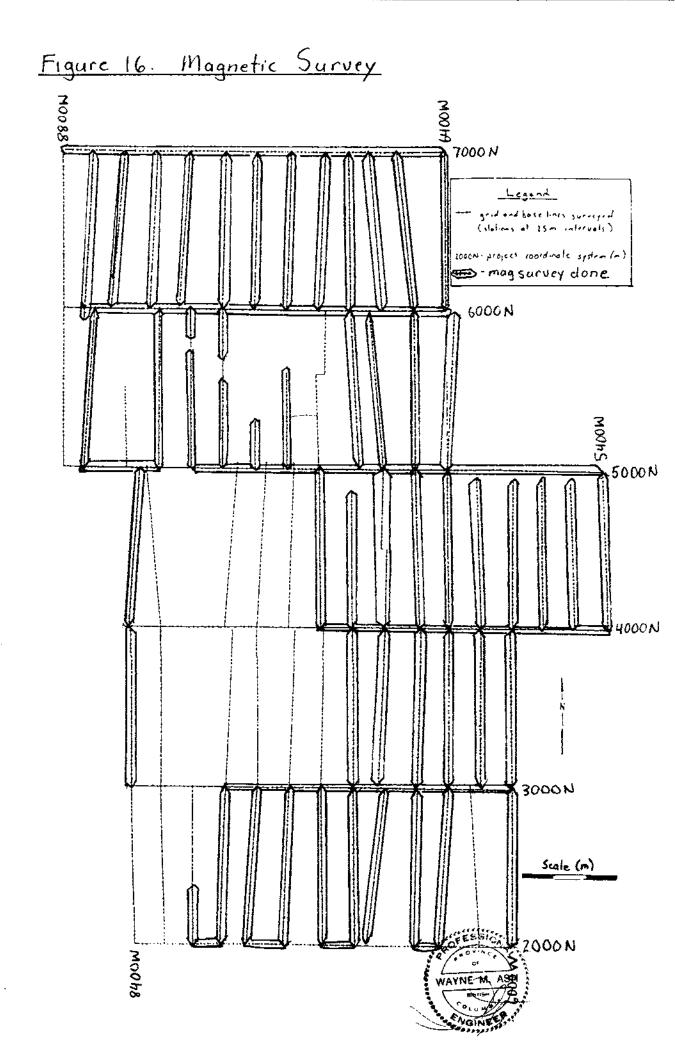
Magnetometer Geophysical Survey

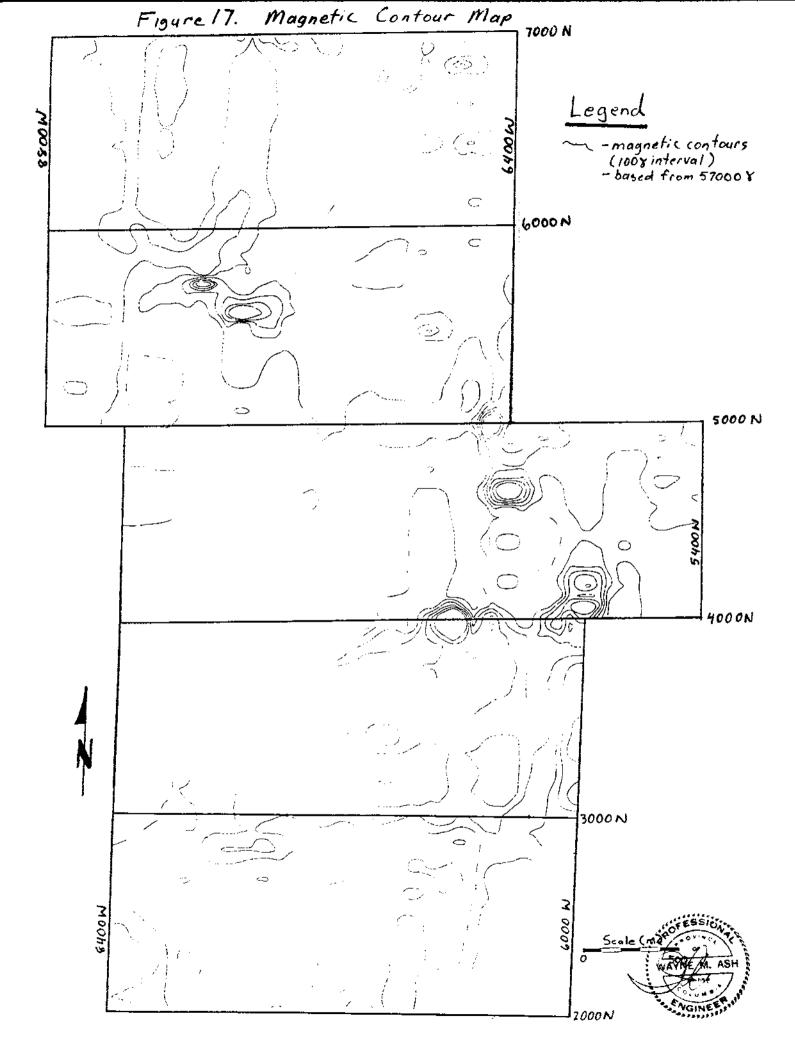
Some 1,200 stations representing 60 km of grid and base lines were surveyed (Figure 16). Two magnetometers were used, the first being the Scintrex MP-2. It is a proton precession magnetometer that measures the total intensity of the earth's magnetic field. The second magnetometer used was the Phoenix MV-1 fluxgate magnetometer. It measures the vertical component of the earth's magnetic field. Because two different magnetometers were used to complete the survey, a correlation factor had to be derived. This factor was determined by simultaneous measurements at the camp base station before and at the end of the day. The readings were as follows:

		Reading	Difference	
Date	Time	Magnetometer 1	Magnetometer 2	(gamma)
12/08/86	АМ	58140	-110	58250
	PM		-150	
12/09/86	AM	58174	-320	58494
	РМ		-190	
12/10/86	AM	58218	-260	58478
	РМ		-380	
12/11/86	AM		-280	58344
	PM	58164	-180	
12/12/86	АМ	58163	-320	58483
~~	PM	58167		

Note: Magnetometer I was the Scintrex MP-2 Proton Precession Magnetometer. It measures the total intensity of the earth's magnetic field.

Magnetometer 2 was the Phoenix MV-1 fluxgate magnetometer. It measures the vertical component of the earth's magnetic field.





Of the five sets of readings used to determine the correlation factor, only three were consistent. Consequently, the readings taken on 12/8/86 and 12/11/86 were ignored. The average difference of the three remaining sets of readings was 58485 gammas and this is the correlation factor that was used. For example, a reading from Magnetometer 2 of -280 gammas would be changed to (-280 + 58485 =) 58205 gammas. Thus, all readings from both magnetometers were correlated and were called the Total Field Intensity (Appendix IV). From this point, the data was corrected for diurnal variations.

The diurnal variations were determined by two methods. The first method consisted of surveying a closed loop in one working day. By doing so, a reading was taken at a known reference point at the beginning and end of each day. The difference in the readings, the diurnal variation, was then applied to the data. The second method of measuring diurnal variations involved measuring the magnetic intensity at the camp base station, again, at the beginning and end of each day. The diurnal variation was then applied to the data in the same manner. The diurnal variations and corrected total field are also listed in Appendix IV.

The results of the magnetic survey were presented in the form of a magnetic contour map (Figure 17). The corrected total field (gamma) was contoured from a base of 57000 gamma. This contour map enables local anomalies to be easily located.

COST OF 1986 FIELD PROGRAM

Mobilization and demobilization	\$ 5,867.38
Road construction and maintenance	16,990.63
Site ground transportation	6,380.74
Helicopter and fixed wing air service (including helicopter preparation)	21,892.63
Baseline survey - 27 km at \$600km	16,200.00
Grid survey - 56 km at \$300km	16,800.00
Magnetometer survey - 60 km at \$210km	12,600.00
VLF-EM (Genie) survey - 14.1 km at \$600km	8,460.00
Soil sampling - 135 samples at \$25/sample	3,375.00
Supervision and administration	32,063.13
Report preparation	 6,003.75

Total Program

\$ 146,633.26

DISCUSSION AND CONCLUSIONS

In November and December of 1986, a field exploration program of the Mustang Mineral Claim Group was carried out by Minore Mine Management Ltd. The results of this program were the installation of 83 km of base and grid line, 134 soil geochemical samples, 14.1 km of VLF-EM survey, and 60 km of magnetic survey.

The soil samples were analyzed for copper, lead, zinc, silver and arsenic. The results, however, were disappointing as no significant anomalies were found. The quality of this sampling program was affected by weather conditions, though, as deep snow and freezing temperatures not only caused the program to be stopped, buy may have resulted in less than ideal samples to be taken.

The VLF-EM survey was considerably more successful, as several large anomalies were encountered. A brief examination of these anomalies indicated that, in some cases, they can be correlated, from grid line to grid line along the known strike of other local geological features. This would suggest that some geological features on the property are quite extensive.

Although the magnetic surey was the most extensive, it too failed to yield any significant anomalies. The Mustang Mineral Claim Group appears to be, in magnetic terms, rather quiet. The anomalies that are present, shown on the contoured map, are very small (up to 500 gammas) and, generally, the values do not vary more than 100 or 200 gammas. There was a significant area which was not covered by the magnetic survey, but the results from the rest of the property suggest that continuing the magnetic survey would not be beneficial.

PROPOSAL FOR FUTURE DEVELOPMENT

Phase 1

In the 1986 field program, the VLF-EM survey produced the only significant anomalies. The survey, however, was cut short and did not near completion. Consequently, it is proposed that the VLF-EM survey be continued. By continuing this program in the spring or summer, the problems encountered in the winter of 1986 would be avoided and the survey would progress more quickly. In order to continue this survey, two people would be required, one operator for the transmitter and one for the receiver. It is estimated that the survey could be completed in two weeks.

The areas that the VLF-EM survey show to be interesting should also be mapped. Reconnaissance geological mapping could be conducted by a geologist, who could work in conjunction with the VLF-EM operators. The reconnaissance mapping is necessary, as it could not be undertaken with a snow cover in the 1986 program.

The final step in Phase 1 involves data collection and report writing. Both the mapping and the VLF-EM survey results could be reported on by the geologist. The time required for this is estimated at five days.

Phase 2

Dependent upon Phase 1, the second phase of this proposal involves the trenching and sampling of the anomalous zones encountered by the VLF-EM survey and the reconnaissance mapping. The trenching would require a backhoe and its operator only. The sampling could be carried out by a geologist, alone. It is estimated that both the trenching and sampling could be completed in five days. After this, the final step, again, involves the writing of a report by the geologist. This is estimated to take three days.

COST OF PROPOSED PROGRAM

Phase 1

VLF-EM Survey: 25 km at \$450/km	\$ 11,250.00
Mapping: 10 days at \$300/day	3,000.00
Camp and Supplies: 14 days at \$100/day	1,400.00
Transportation: 14 days at \$50/day	700.00
Mob and demobilization: 1 day at \$400/day	400.00
Report Writing: 5 days at \$300/day	1,500.00
Total Phase I	\$ 18,250.00

Phase 2

Trenching: 2000 ft at \$10/ft	\$ 20,000.00
Sampling: 5 days at \$300/day	1,500.00
Camp and Supplies: 5 days at \$100/day	500.00
Transportation: 5 days at \$50/day	250.00
Backhoe Mob and Demobilization: 1 days at \$600/day	900.00
Report Writing: 3 days at \$300/day	900.00
Assays: 150 at \$15/sample	2,250.00
Total Phase 2	\$ 26,300.00
TOTAL COST PHASE 1 AND PHASE 2	\$ 44,550.00

REFERENCES

The following is a list of publications relevant to the area of the Mustang Group:

- Alldrick, D.J., 1983; The Mosquito Creek Mine, Cariboo Gold Belt, B.C. Ministry of Mines, Geological Fieldwork 1982.
- B.C. Minister of Mines Annual Report, 1934; pages 26, 27.
- B.C. Minister of Mines Annual Report, 1947; pages 117-123.
- Bowman, A., 1888; Report on the Geology of the Mining District of Cariboo, B.C., Geological Survey of Canada, Annual Report 1888, v. 3, pt. 1.
- Boyle, R.W., 1979; The Geochemistry of Gold and its Deposits, Geological Survey of Canada, Bulletin 280.
- Campbell, K.V.; Mustang Group, Cariboo Mining Division, Geology and Proposal for Gold Exploration, June 1985.
- Campbell, R.B., Mountjoy, E.W. and Young, F.G., 1973; Geology of the McBride Map Area, Geological Survey of Canada, Paper 72-35.

CERTIFICATE OF QUALIFICATIONS

I, Wayne M. Ash, P. Eng., of 401 - 1765 Duchess Street, West Vancouver, British Columbia, do hereby certify as follows:

1. I am a graduate of the Halleybury School of Mines (Ontario, 1965) and Michigan Technological University (Michigan, B. Sc. Mining Engineering, 1969).

2. I have been directly associated with the mining industry for the past twentysix years and have been a member of the Association of Professional Engineers of British Columbia since 1971 (Registration No. 7940).

3. I have no interest, either directly or indirectly in the property or securities of Candorado Mines Ltd., but may gain an interest in the future.

4. I inspected the property in November and December 1986, and co-ordinated field operations conducted in 1986.

5. I hereby grant permission to Candorado Mines Ltd. to use this report, or any portion of it, for any legal purposes normal to the business of the firm, so long as the portions used do not materially deviate from the intent of this report, as set out in the whole.

Dated at Vancouver, B.C., this 24th day of April, 1987.

Wayne M. Ash, P. Eng.

CERTIFICATE OF QUALIFICATIONS

I, Kenneth D.K. Embree, of 8588 Woodgrove Place, Burnaby, British Columbia, do hereby certify as follows:

- 1. I am a graduate of the University of Saskatchewan (B.Sc. Geological Engineering, 1986).
- 2. I have been directly associated with the mining industry for the past six months and have been a member of the Association of Professional Engineers of British Columbia, as an Engineer-In-Training, since 1986.
- 3. I acted as a supervisor and helped to carry out the field work on this project. I also helped in compiling all data and preparing this report.

Dated at Vancouver, B.C., this 24th day of April, 1987.

antimbre

Kenneth D.K. Embree

APPENDICES

APPENDIX I

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SOIL SURVEY RESULTS

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 DATA LINE 251-1011 PHONE 253-3158

1

DATE RECEIVED: MAR 3 1987

DATE REPORT MAILED: May 19/87.

ANALYSIS GEOCHEMICAL ICP

.500 GRAM SAMPLE IS DIGESTED WITH JWL 3-1-2 HCL-HN03-HZD AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MS.BA.TI.B.AL.NA.K.W.SI.IR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-4 SOILS -BO, WESH / 95 CYNIDE SOLUTION

ASSAYER: Men DEAN TOYE. CERTIFIED B.C. ASSAYER.

MINORE MINE	MANAGE	EMENT	FILE	E # 87-	-0559	FAGE	1
SAMPLE#			Zn FPM		As PPM		

			FPM	FFM	FPM	F'F'M	PPM
72+00W 72+00W 72+00W 72+00W 72+00W	49+50N 49+00N		15 4 6 39 7	14 10 15. 70 6	63 41 83 83 32	.4 .4 .5 .1 .1	14 6 5 31 12
72+00W 72+00W 72+00W 72+00W 72+00W	47+00N 46+50N 46+00N 45+50N 45+00N		17 4 2 6 20	15 2 3 6 30	54 18 12 19 64	.2 .1 .1 2.1 .5	16 3 2 5 26
72+00W 72+00W 72+00W 72+00W 72+00W	44+00N 43+50N		15 44 24 4 2	6 28 24 5 3	19 120 57 21 8	.3 1.1 .2 .2 .1	5 9 12 2 2 2
72+00W 72+00W 72+00W 72+00W 72+00W	41+75N		16 9 13 8 7	24 14 17 8 6	44 29 64 40 24	. 4 . 1 . 1 . 1 . 1	13 11 2 8 8
68+00W 68+00W 68+00W 68+00W	47+25N		11 9 28 8 26	10 18 25 13 28	31 24 98 28 71	.1 .8 .1 .2 .1	5 9 11 7 7
68+00W 68+00W 68+00W 68+00W 68+00W		A	10 13 9 8 31	17 15 10 14 94	53 48 36 33 128	.1 .5 .2 .1 .8	3 12 11 6 19
68+00W 68+00W 68+00W 68+00W 68+00W	42+50N 41+75N 41+00N 40+50N 40+00N		32 19 7 17 17	30 81 14 26	106 122 28 45 92	.1 .3 .2 .4 .1	20 18 6 2 5
64+00W STD C	46+00N		24 59	29 37	65 135	.3	13 39

M	INORE MINE	MANAC	SEMENT	FIL	E # 87	-0559
SAMPLE	••	Cu PPM	Fb FFM	Zn FFM	Ag FFM	As PPM
64+00W	45+75N	2	5	8	.2	2
64+00W	45+50N	6	18	18	.3	7
64+00W	45+00N	4	12	12	. 3	4
64+00W	44+75N	18	35	42	- 1	15
64+00W	44+50N	21	29	104	- 1	28
64+00W	44+00N	23	18	75	. 1	9
64+00W	43+75N	11	10	32	. 1	7
64+00W	43+50N	20	18	91	.2	17
64+00W	43+25N	17	14	47	. 1	32
64+00W	43+00N	14	17	54	.2	13
64+00W	42+75N	9	19	23	1.4	6
64+00W		12	13	52	.3	9
64+00W		8	9	31	1.8	4
64+00W		22	31	105	. 1	10
64+00W		4.3	36	175	.2	8
64+00W	40+50N	51	27	104	. 1	2
64+00W	40+00N	26	19	92	.3	6
60+00W	46+00N	22	17	63	.7	19
60+00W	45+50N	9	4	34	.7	7
60+00W	45+00N	19	18	75	.7	15
60+00W	44+50N	35	23	89	. 1	13
60+00W	44+00N	6	2	23	.2	3
60+00W	43+50N	11	10	32	.3	4
60+00W	43+00N	9	6	19	. 1	8
60+00W	42+50N	47	18	110	2.0	16
60+00W	42+00N	26	20	68	.3	7
60+00W	41+50N	23	25	66	. 1	12
60+00W	41+00N	38	22	89	. 4	9
	40+50N	16	22	63	.5	7
60+00W		26	18	72	. 1	15
58+00W	46+00N	31	31	73	.3	34
58+00W	45+50N	43	17	134	.9	10
58+00W	45+00N	42	15	44	2.4	5
58+00W		95	49	282	1.3	1 31
58+00W		17	18	62	3.1	14
58+00W	43+00N	26	12	62	1.4	8
STD C		58	36	131	6.8	41

MINORE MINE MANAGEMENT FILE # 87-0559

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PAGE

MINORE MIN	E MANAG	EMENT	FI	E # 87	7-0559
SAMPLE#	Cu	Pb	Zn	Ag	As
	FPM	FFM	F'F'M	F'F'M	PPM
58+00W 42+50N	23	27	70	1.1	6
58+00W 42+00N	23	23	72	.3	11
58+00W 41+50N	11	21	39	.3	6
58+00W 41+00N	39	23	101	1.0	10
58+00W 40+50N	27	26	75	.3	11
58+00W 40+00N	14	17	39	.2	6
56+00W 47+00N	17	16	37	.3	7
56+00W 46+50N	25	18	50	.2	6
56+00W 46+00N	37	9	80	- 1	5
56+00W 45+50N	25	9	20	. 1	5
56+00W 45+00N	20	15	62	.3	22
56+00W 44+50N	15	24	40	.7	17
56+00W 44+00N	26	14	57	1.0	13
56+00W 43+50N	4Ŏ	20	94	.6	6
56+00W 43+00N	15	25	49	2.6	5
56+00W 42+50N	11	12	25	. 1	3
56+00W 42+00N	8	16	28	.4	6
56+00W 41+50N	13	17	49	.5	3
56+00W 41+00N	14	27	43	1.0	8
56+00W 40+50N	15	24	47	.9	9
56+00W 40+00N	31	34	101	.5	13
54+00W 47+00N	15	14	56	.3	4
54+00W 46+30N	, 25	28	105	1.0	9
54+00W 46+00N	17	20	23	.7	3
54+00W 45+50N	16	25	50	. 4	8
54+00W 45+00N	17	29	60	. 2	10
54+00W 44+50N	18	29	68	. 1	8
54+00W 44+00N	25	27	139	. 9	10
54+00W 43+50N	17	35	39	1.2	9
54+00W 43+00N	20	28	116	1.6	9
54+00W 42+50N	17	38	35	.2	10
54+00W 42+00N	14	13	37	.5	8
54+00W 41+50N	56	33	109	1.8	34
54+00W 41+00N	22	25	59	- 7	12
54+00W 40+50N	25	37	65	1.7	27
54+00W 40+00N	15	103	72	3.6	24
STD C	58	38	133	6.9	41
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MINORE MINE MANAGEMENT FILE # 87-0559

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MINDRE MINE MANAGEMENT FILE # 87-0559

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SAMPLE#	Cu	РЬ	Zn	Ag	As
	PPM	РРМ	PPM	PPM	FFM
40+00N 67+50W	18	18	77	. 1	6
40+00N 66+75W	9	10	23	. 1	7
40+00N 66+25W	30	24	100	. 3	8
40+00N 65+50W	8	10	44	. 1	3
40+00N 65+00W	14	25	64	. 1	10
40+00N 64+50W	17	26	79	.4	9
40+00N 55+50W	13	31	29	1.0	8
40+00N 55+00W	10	31	35	.8	9
40+00N 54+50W	41	37	99	1.6	15
R1	15	32	92	.6	28
R2 R3 R4 R5 R6	37 37 35 19	44 45 82 33 32	113 145 122 102 91	.2 .5 .5 .4 .1	39 67 49 25 8
R7	26	25	94	.4	18
R8	66	49	124	.2	32
R9	26	28	104	.5	15
R10	34	26	121	5	15
R11	42	34	106		25
R13	43	24	123	. 3	15
R14	44	38	115	. 4	16
R15	30	21	123	. 1	20
R16	27	28	76	. 4	22
R17	38	17	119	. 4	22
R18	37	21	111	.1	19
STD C	59	38	135	6.8	41

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APPENDIX II

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SOIL SURVEY STATISTICS

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	ope^2 log^2
Cu(ppm) log 15 1.1768913	ppe^2 log^2 225 1.3831986
4 ,68285999	16 . 36247623
6 .77815125	36 68551937
39 1.5918646	1521 2.5314866
7.84509884	49 71419878
17 1.2304489	289 1.5148845
4 .69285999	161.36247623
.30103880	4 . 89861986
6 .77815125	36 .68551937
28 1.3818388	488 1.6926790
15 1.1760913	225 1.3831986
44 1.6434527	1936 2.7889367
24 1.3802112	576 1.9849831
4 .68285999	16 .36247623
. 39183988	4 . 89861986
16 1.2841288	256 1.4499849
9 .95424251	81 .91857877
13 1.1139434	169 1.2498698
8 .98388999	64 .81557152
7 ,84589884	49 71419878
11 1.0413927	121 1.0844987
9 .95424251	81 91857877
28 1.4471586	784:2.8942664
8 .99388999	64,.81557152
26 1.4149733	676 2.8821496
18 1	188 1
13 1.1139434	169 1.2408698
9 .95424251	81,91057077
8 .98388999	64 .B1557152
31 1,4913617	961 2.2241597
32 1.5851588	1824 2,2654765
19 1.2787536	361 1.6352108
7 .84589884	49 .71419272
17 1.2384489	289 1.5140045
17 1,2384489	289 1.5148845
24 1.3882112	576 1.9849831
38103889	
6,77815125	
4 .68285999	
	324 1.5757091
21 1.3222193	441 1.7482639
23 1.3617278	529 1.8543827
11:1.0413927	121 1.0844987
28 1.3010300	488 1.6926790
17.1.2304489	289 1.5148845
14 1.1451288	196 1.3136895
9 . 95424251	81.91057877
12 1.0791812	144 1.1646322
8,98388999	64 .81557152
22 1.3424227	484 1.8620987
43 1.6334685	1849 2.6682192
51 1.7875782	2681 2.9157959
26 1,4149733	676 2.0821496
22, 1, 3424227	484:1.8020907
9 . 95424251	81:.91857877
19 1.2787536	361 1.6352108
35 1.5440690	1225 2.3841461
677815125	36 .60551937

CuZ

11 1.8413927	121;1.0844987
9. 95424251	81 .91057877
47 1.6728979	2289 2.7959112
26 1.4149733	676 2,8821496
23 1.3617278	529 1.8543827
38, 1, 5797836	1444 2.4957162
16 1.2841288	256 1.4499849
	676 2.0821496
26 [.4]49733	
31 1.4913617	961 2.2241597
43 1.6334685 42 1.6232493	1849 2.6682192
42 1.6232493	1764 2.6349383
• 😒 1.9777236 👘	9825 j 3, 911398 7
17 1.2384489	289 1.5148845
26 1.4149733	676 2.8021496
23 1.3617278	529 1.8543827
23 1.3617278	529 1.8543827
11 1.8413927	121; 1.8844987
39 1.5910646	1521 2.5314866
27 1.4313638	729' 2. 64668822
	196 1.3136095
14-1.1461288	196 1.31380JJ
17 1.2384489	289 1.5140045
25 1.3979480	625 1.9542363
37 1.5682017	1369 2.4592566
25 1.3979488	625 1.9542363
28 1,3419360	488 1.6926798
15 1.1768913	225 1.3831986
26 1.4149733	676 2,8021495
48 1.6828688	1688 2.5665962
15 1.176 913	
13 1. 1. 1. 2027	225 1.3831986 121 1.8844987
11 1. 8413927	121, 1.007730/
8`.90386999	64 .81557152
13 1.1139434	169 1.2488698
14 1.1461280	19611.3136095
15 1.1760913	225 1.3831906
31 1.4913617	961 (2.2241597
15 1,1768913	225 1.3831986
25 1.3979400	625 1.9542363
17 1.2304489	289 1.5148845
16 1.2041200	256 1.4499849
17 1.2304489	289 1.5140045
	324 1.5757091
	625 1.9542363
25 1.3979468	
17 1.2384489	289 1.5148845
20 1.3810308	488 1 6926798
17 1.2384489	289-1.5148945
14 1.1461288	196 1.3136895
56 1.7481888	3136 3.8561614
22 1.3424227	484 1.8828987
25 1.3979400	625 1.9542363
15 1.1760913	225 1.3831986
18 1.2552725	324 1.5757891
9.95424251	81 .91057977
	908 2.1816872
38:1.4771213	
8.98308999	64 .81557152
14 1.1461288	196 1.3136895
17 1.2384489	289 1.5148845
13 1.1139434	169 1.2408690
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41 1.6127839	1681 2.6010718

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	. 2787536	361 1.6352108	
	1.4149733		
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	1,4149733		
		1156 2.3454277	
-		1764 2.6349383	
		1849 2.6682192	
44	1.6434527	1935 2.7889367	
38	1.4771213	900 2.1818872	
		729 2.8488822	
38	1.5797836	1444 2.4957162	
37	1.5682017	1369 2.4592566	
SUB	508	sun sun	
2988	166.37882	89324 219 12751	
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standard	standard		
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	: A ;: 9 !!	C (; D ;
	<u> </u>	ppe^2 log^2
5	14 1.1461288	196 1.3136895
3	18 1	188 1
4	15 1.1760913	225 1.3831986
5	78 1.8458988	4988 3.4843868
6	6.77815125	36 .68551937
7	15 1.1760913	225 1.3831986
8	. 38193080	4 .89861986
9	3.47712125	9.22764469
18	6.77815125	36 .68551937
11	38 1.4771213	908 2.1818872
12	6.77815125	36 .68551937
13	28 1.447158B	784 2.8942664
14	24 1.3802112	576 1.9049831
:5	5,59897888	25 .48855987
16	3 . 47712125	9.22764469
17	24 1.3882112	576 1.9849831
18	14 1.1461289	196 1.3136895
19	17 1.2384489	289 1.5140045
28	8 .98368999	64 .81557152
21	6.77815125	36 .60551937
22	18 1	108 1
23	18 1.2552725	324 1.5757891
24	25 1.3979480	625 1.9542363
25	13 1.1139434	169 1.2488698
26	28 1,4471580	784 2.8942564
27	17 1.2384489	289 1.5148845
28	15 1.1768913	225 1.3831986
29	18 1	188 1
38	14 1.1461288	196 1.3136095
31		8835 3.8932335
32	38 1.4771213	908 2.1816872
33	81 1.9884858	6561 3.6423151
34	16 1.2041280	256 1.4499849
35	14 1.1461288	196 1.3136095
36	26 1.4149733	676 2.9821496
37	29 1,4623988	841 2.1386879
38	5 .69897888	25 .48855907
39	18 1.2552725	324 1.5757891
48	12 1.6791812	144 1.1646322
41	35 1.5448688	1225 2.3841461
42	29 1.4623988	841 2.1386879
43	18 1.2552725	324 1.5757891
44	18 1	
45	18 1.2552725	324 1.5757891
45	14 1.1461280	196 1.3136895
47	17 1.2384489	289 1.5148845
48	19 1.2787536	361 1.6352188
49	13 1.1139434	169 1.2408598
50	9.95424251	81 .91857877
51	31 1.4913617	961 2.2241597
52	36 1.5563825	1296 2.4228775
53	27 1.431363B	729 2.8488822
54	19 1.2787536	361 1.6352189
55	17 1.2364489	289 1.5148045
56	4 .69285999	16 .36247623
57	18 1.2552725	324 1.5757091
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58	23 1.3617278	529 1.8543827
59	~	4 .89861986
52	1 8 I	180 5
61	6.77815125	36 .68551937
62	18 1.2552725	324 1.5757091
63	20 1.3818388	480 1.6926790
54	25 1.3979488	625 1.9542363
65	22 1.3424227	484 1.8820987
60 66	22 1.3424227	464 1.8020387
67	18 1.2552725	324 1.5757891
68	31 1.4913617	361 2.2241597
53	17 1.2384489	289 1.5148845
5 J 7 B	15 1.1768913	225 1.3831986
71	49 1.6981961	2481 2.8567628
72	10 1.2552725	324 1.5757091
73	12 1.8791812	144 1.1646322
74	27 1.4313638	729 2.8488022
75	23 1.3617278	529 1.8543027
76	21 1.3222193	441 1.7482639
71	23 1.3617278	529 1.8543027
	26 1.4149733	675 2,8021496
78	17 1.2384489	289 1.5140845
79	•• •• •• ••	256 1.4499849
88	16 1.2841280 18 1.2552725	324 1.5757891
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82	9.95424251	
83	9,95424251	81 .91857877
84	15 1.1768913	225 1.3831906
85	24 1.3802112	576 1.9849831
86	14 1.1451288	196 1.3136895
87	28 1.3010300	488 1.6926798
88	25 1.3979488	625 1.9542363
89	12 1.8791812	144 1.1646322
98	16 1.2841200	256 1.4499849
91	17 1.2384489	289 1.5140945
32	27 1.4313638	729 2.8488822
93	24 1.3892112	576 1.9849831
94	34 1.5314789	1156 2.3454277
95	14 1.1461288	196 1.3136895
96	28 1.4471580	784 2.8942664
97	20 1.3018300	488 1.6926798
98	25 1.397948#	625 1.9542363
99	29 1,4623988	841 2.1386879
108	29 1.4623980	841 2.1386879
111	27 1.4313638	729 2.8488822
182	35 1.5448688	1225 2.3841461
183	28 1.4471580	784 2.8942664
184	38 1.5797836	1444 2.4957162
185	13 1.1139434	169 1.2488698
186	33 1.5185139	1889 2.3858846
197	25 1.3979488	625 1.9542363
188	37 1.5682817	1369 2.4592566
189		18689 4.8515137
110	18 1.2552725	324 1.5757891
111	10 1	188 1
112	24 1.3882112	576 1.9849831
113	10 1	188 1
114	25 1.3979488	625 1.9542363
115	26 1.4149733	676 2.8821496
116	31 1.4913617	961 2.2241597
117	31 1.4913617	961 2.2241597
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118		7 1.5682017	1369 2	. 4592566		
119	31	2 1.5051500		.2654765		
128	4	4 1.6434527		.7889367		
121	43	5 1.6532125		.7331116		
122	8:	2 1.9138139		.6626835		
23	33	3 1.5185139	1689 2			
24	32	2 1.5851500		. 2654765		
25	25	1.3979400		.9542363		
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38		1.3802112	576 1.			
31		1.5797836				
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19 -						
2	sean.	hean				
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5 -					•	
6	variance	variance				
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9	standard	standard				
	deviation					

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	A	C (; D ;	
:	In(pps) log	pp=*2 log*2	
?	63 1.7993485	3969 3.2376264	
3	41 1.6127839	1681 2.6818718	
1	32 1.5051588	1024 2.2654765	
3	B3 1.9196781	6889 3.6828687	
5	32 1.5051500	1824 2.2654765	
ľ	54 1.7323938	2916 3.0811881	
3	18 1.2552725	324 1.5757091	
)	12 1.6791812	144 1.1646322	
.2	19 1.2787536	361 1.6352108	
.1	64 1.8861888	4895 3.2622861	
2	19 1.2787536	361 1.6352188	
3	128 2.6791812	14488 4.3229947	
4 5	57 1.7558749	3249 3.8838965	
	21 1.3222193	441 1.7482639	
6 7	.903889999 44 1.6434527	64 .81557152	
8		1936 2.7889367	
9	29 1,4623988 64 1.8861888	841 2.1386879	
		4896 3.2622861	
1 1	40 1.6820600 24 1.3802112	1688 2.5665962	
:1 ;2		576 1.9849831	
.2	31 1.4913617 24 1.3882112	961 2.2241597	
.4	98 1.9912261	576 1.9049831	
5		9684 3.9649813	
6	28 1.4471580 71 1.8512583	784 2.8942664	
7		5841 3.4271575	
ß	53 1.7242759 48 1.6012412	2899 2.9731273	
9 9	36 1.5563825	2384 2.8265721	
3	33 1.5185139	1295 2.4228775	
1	128 2.1972188	1889 2.3858846	
2	186 2.8253859	16384 4.4483339	
3	122 2.8863598	11236 4.1818638 14884 4.3528973	
4	26 1.4471582	784 2.8942664	
5	45 1.6532125	2825 2.7331116	
5 6	92 1.9637878	8464 3.8564626	
7	85 1.9294189	7225 3.7226574	
8	. 98368999	64 .81557152	
9	1B 1,2552725	324 1.5757891	
â	12 1.8791812	144 1.1645322	
1	42 1.6232493	1764 2.6349383	
2	184 2.0170333	10816 4.8684235	
3	75 1.9758613	5625 3.5158547	
6	32 1.5851588	1824 2.2654765	
5	91 1.9598414	8281 3.6378432	
5	47 1.6728979	2209 2.7959112	
7	54 1.7323938	2916 3.8811881	
3	23 1.3617278	529 1.8543027	
3	52 1.7168033	2784 2.9446675	
8	31 1.4913617	961 2.2241597	
1	105 2.0211893	11825 4.8852862	
2	175 2.2438388	38625 5.0312197	
3	164 2.0170333	18816 4.8684235	
4	92 1.9637878	8464 3.8564626	
5	63 1.7993485	3969 3.2376264	
ż	34 1.5314789	1156 2,3454277	
7	75 1.8758613	5625 3.5158547	

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Э	89 1.9493988	7921 3.8801214
3	23 1.3617278	529 1.8543827
ł	32 1.505;500	1024 2.2654765
1	19 1.2787536	361 1.6352198
2	112 2.0413927	12182 4.1672841
3	68 1.8325889	4624 3.3588889
\$	66 1.8195439	4356 3.3187401
5	89 1,9493900	7921 3.8001214
5	63 1.7933485	3969 3.2376264
7	72 1.8573325	5184 3.4496840
3	73 1.8633229	5329 3.4719721
9	134 2.1271848	17956 4. 5245748
à	44 1.6434527	1936 2.7889367
1	283, 2. 4582491	79524 6.0037207
2	62 1.7923917	3844 3.2126680
3	62 1.7923917	3544 3.2126680
4	78 1.8458388	
5	72	4968 3.4843858 5184 7.449484
76	39 1.5910646	5184 3.4496948
77		1521 2.5314866
78	161 2.6043214	10201 4.0173042
75	75 1.8758613	5625 3.5158547
	39 1.5918646	1521 2.5314866
80	37 1.5682917	1369 2.4592566
81	58 1.6989788	2589 2.8864991
82	80 1.9838988	6488 3.6217515
83	39 1.4771213	908 2.1810872
84	62 1.7923917	3844 3.2126680
85	48 1.5628588	1661 2.5655962
86	57 1.7558749	3249 3.8838965
87	94 1.9731279	8636 3.8932335
88	49 1.6981961	2481 2.8567629
89	25 1.3979400	625 1.9542363
96	28 1,4471588	784 2.0341654
91	49 1.6901961	2481 2.8567628
92	43 1.6334685	1849 2.5582192
93	47 1.6728979	2269 2.7959112
94	101 2.0043214	10281 4.0173842
95	56 1.7481888	3136 3.8561614
96	105 2.0211893	11025 4.0852862
97	23 1.3617278	529 1.8543027
98	50 1.6989780	2588 2.8864991
99	68 1.7781513	3688 3.1618219
108	68 1.8325889	4624 3.3589889
181	139 2.1438148	19321 4.5925124
102	39 1.5918646	1521 2.5314866
183	116 2.8644580	13456 4.2619868
184	35 1.5448688	1225 2.3841461
185	37 1.5582017	1369 2.4592566
186	189 2.8374265	11881 4.1511867
107	59 1.7788528	3481 3.1359168
188	55 1.8129134	4225 3.2866548
109	72 1.8573325	5184 3,4496840
118	77 1.8864987	5929 3.55BB473
111	23 1.3617278	529 1,8543827
112	188 2	10000 4
113	44 1.6434527	1936 2.7889367
1147	54 1.8061808	4896 3.2622861
115	79 1.897627:	6241 3.6809886
116	33 1 (FAR11)	

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118	99	1.9956352	9881	3.9825598
::9	92	1.9637878	8464	3.8564626
128	113	2.8538784	12769	4.2151311
12:	:45	2.1613688	21025	4.6715116
:22	122	2.8863595	14884	4,3528973
123	182	2.0006002	19484	4.8344747
124	91	1,95984:4	8281	3.8379432
125	94	1.9731279		3,8932335
126	124	2.8934217		4.3824144
127	184	2.0170333		4.0684235
126	121	2.2827854	14641	4.3379949
129	136	2,8253859		4.1818638
138	123	2.8899851		4,3677834
131	115	2.8686978	13225	4.2464756
132	123	2.0899851	15129	4.3677834
133	76	1.8888136	\$776	3, \$374598
134	119	2.0755470	14161	4.3878952
135	111	2.8453238	12321	4.1833461
136				
137	SUE	sue	SUB	Sum
138	9849	234,44965	823189	428.65798
129				
543	aean	aean		
141	67.529851	1.7496242		
142				• • • • • •
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145		• • • • • • • • • • • • •		•••••
146	variance	variance		
147	91.947761	.83121988		
143				
149	standard	standard		
158	deviation	deviation		
151	11.5881375	7668899		
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1	Ag(ppa) log	open2 10gn2
2 -	.4 3979488	.16 .15835625
2 3	.62218487	.36 .84921687
4	.53010300	.25 .89861986
5	.1 -1	.81 1
6	.1 -1	.01 1
7	,26989788	.84 .48855907
8	.1 -1	.81 1
9	.1 -1	.81 1
18	2.1 .32221929	4.41 .10382527
11	.53818388	.25 .09061986
12	.35228787	.89 .27340218
:3	1.1.84139269	1.21 .00171335
14	.26989788	.64 .48855967
15	.2 -,6989788	.84 .48855967
16	.1 -1	.81 i
:7	,439794 88	.15 .15835625
18	.1 -1	.81 1
19	.1 -1	. 8 1 i
28	.: -1	.61 1
21	.1 -1	.91 1
22	.1 -1	. 71 1
23	.88969188	.64 .88939155
24	.1 -1	.81 1
25	.26989788	.84 .48855967
26	.1 -1	.81 1
27	.1 -1	.#1 1
28	.53414388	.25 .89861986
29	.26989788	.84 .48855907
38	.1 -1	.61 1
31	.88969100	.64 .88339155
32	.1 -1	.61 1
33	.35228797	.09 .27348218
34	.26989788	.84 .48855987
35	.4 3979488	.16 .15835625
36	.1 -1	.01 1
37	.35228787	.89 .27348218
30	.26989708	.84 .48855987
39	.3 5228787	.89 .27348218
48	.3 5228787	.89 .27348218
41	.1 -1	.01 1
42	.1 -1	.01 1
43	.1 -1	, 9 1 I
44	.1 -1	.0E 1
45	.25989788	.84 .48855987
46	.1 -1	.81 1
47	.2 -,6989788	.84 .48855987
48	1.4 .14612884	1.95 .82135348
49	.3 5228787	.89 .27348218
58	1.8 .25527251	3.24 .86516405
51	.1 -1	. 21 1
52	.26989788	.64 .48855987
53	.1 -1	.01 i
54	.3 5228787	.89 .27348218
55	.7 1549828	.49 .82399462
56	.71549020	.49 .82399462
57	.7 1549020	.49 .82399462

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5ê	.1 -1	.61 1	
59	.26989788	.04 .48855987	
68	.35228787	.89 .27342218	
61	.1 -1	.01 1	
62	2 .38183888	4.09861986	
63	.35228787	.09 .27340218	
64	.1 -1	.01 1	
65	.4 3979488	.16 .15835625	
66	.53418388		
67		.25 .89861988	
	-1	.01 1	
66	.35228787	.09 .27340218	
69	.98457575	.81 .88289375	
7 e	2.4 .38821124	5.76 .14456859	•
7:	1.3 .11394335	1.69 .81298389	
72	3.1 .49136169	9.61 .24143631	
73	1.4 .14812804	1.36 .02135340	
74	1.1 .04139269	1.21 .08171335	
75	.35228787	.09 .27342218	
76	.35228787	.89 .27348218	
77	: 0	: 8	
73	.35228787	.89 .27340218	
79	.26989788	.84 .48855987	
38	.35228787	.83 .27348218	
3:	.26989788	.84 .48855907	
32	.1 -1	. 8 1 1	
33	.1 -1	.8: 1	
34	.35229787	. 39 . 27348218	
35	.71549828	.49 .02399462	
36	1 6	1 8	
37	.62218487	.36 .84921687	
38	2.6 .4:497335	6.76 .17228288	
39	.1 -1	.81 1	
78	.43979406	.16 .15835625	
31	.53818388	.25 .09061906	
3 2	; 8 '2 -'3etd399	1 0	
33	.98457575	.81 .08289375	
	.53910300	.25 .09061906	
34		.09 .27340218	
35 X	.35228787 1 8	1 0	
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37	.71549828	.49 .82399462	
38	.43979488	.16 .15835625	
39	.26989780	.84 .48855987	
188	.1 -1	.01 1	
181	.98457575	.81 .08289375	
:92	1.2 .07515175	1.44 .00626967	
183	1.6 .22411998	2.56 .04166497	
:84	.25989700	.84 .48855987	
105	.53010300	.25 .89061986	
: 86	1.8 .25527251	3.24 .06516405	
107	.71549828	.49 .82399462	
:86	1.7 .23844892	2.89 .05310671	
:09	. 55638258	12.96 .38947247	
:18	.1 -1	.91 1	
111	.t -!	.81 1	
:12	.35228787	.89 .27340218	
:13	.1 -t	.81 1	
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.15	.4 3979488	.16 .15835625	
.16	1 8	1 8	
.17	.80969100	.64 .08939155	

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.13	1.6 .20411998	2.36 .84166497	
. 15	.62218487	.36 .04921687	
28	.26989788	.84 .48855987	
:21	.53010382	.25 .09861986	
. 22	.5 3818382	. 25 . 89861985	
. 23	.4 3979422	-16 .15835625	
. 24	.1 -1	1 15.	
. 25	.4 3979422	.16 .15835625	
. 25	.26989728	.04 .48855387	
. 27	.3 5228787	.09 .27348218	
. 28	.5 3010300	- 25 . 89861986	
. 29	.53818380	.25 .09861986	
.38	.35228787	.89 ,27340218	
. 31	.4 3979428	.16 .15835625	
32	.1 -:	1.	
33	.4 3979422		
34	.4 3975422	.16 .: 5935625	
.35	-1	.16 .15835625	
.36		.81 1	
37	506 Sub		
38	71.1 -65.74326	SUA SUN	
35		d8.2/ 36.11/3/2	
. 4 8	Bean Gean		
41 .5	53059701 - 4905213		
42			
43	aedian secian		
44	accient accient		
45			
-	ariance variance		
- •	0007463 .82746269		
	tandard standard		
	viation deviation		
	8638684		

50=0.01

	A	
1	AS(DDA) ICQ	
: 2 3	14 1-1461262	<u>oge^2 log^2</u>
3	6 .77815125	196 1.3136895
4	5 .69897888	36 .60551937 25 .48855907
5	31 1.4913617	
6	12 1.8791812	961 2.2241597
7	16 1.2841280	144 1.1646322
9	3 .47712125	256 1.4499849 9 .22764469
9	4 .30163828	
18	5 .69897888	4 .09861986 25 .40855001
11	26 1.4149733	25 .48855987 676 2.0021496
12	5 .69897086	25 .48855967
13	9 .95424251	81 .91857877
14	12 1.8791812	144 1.1646322
15	38103000	4 .89851986
16	£ . 30183800	4 .89861986
17	13 1.1139434	169 1.2408698
18	11 1.8413927	121 1. 8844987
19	38103280	4.89861986
28	8 . 98388999	64 .81557152
2!	8 . 98388999	64 .81557152
22	5 .69897888	25 .48855987
23	9 .95424251	81 .91857877
24	11 1.8413927	121 1.9844987
25	7 .84509864	49 .71419878
26	7 84589884	49 .71419878
27	3 . 47712125	9 .22764469
28	12 1.8791812	144 1.1646322
29	11 1.0413927	121 1.0844987
38	6 .77815125	36 .68551937
31	19 1.2787536	361 1.63521#8
32	28 1.3818388	408 1.6926790
33	18 1.2552725	324 1.5757091
34	5 .77815125	36 .68551937
35	🍬 . 30183880	1 .89861986
36	5 .69897888	25 .48855987
37	13 1.1139434	169 1.2488698
38	4. . 38183088	4 .89861986
39	7 .04589684	49 .7141987B
48	4 .68285999	16 .36247623
41	15 1.1768913	225 1.3831986
42	29 1.4471580	784 2.8942664
43	9.95424251	61 .91857877
44	7 .84589884	49 .71419878
45	1.2384489	289 1.5148845
46	32 1.5851588	1824 2.2654765
47	13 1.1139434	169 1.2488698
48	6.77815125	36 .68551937
49	9 .95424251	81 .91857877
50	4 .68285999	16 .36247623
51	10 1	100 1
52	8 .90308999	64 .81557152
53	38183888	4 .09861986
54	6 .77815125	36 .68551937
55 57	19 1.2787536	361 1,6352108
56	7 .84589884	49 .71419878
57	15 1.1760913	225 1.3831986

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As 1

1

1

58	13 1.1139434	169 1.2488698
54 59	3 .47712125	9 .22764469
68	4 .68285999	16 .36247623
6:	8 .98388999	64 .81557152
62	16 1.2041200	256 1.4499849
63	7 .84589884	43 .71419070
64	12 1.8791812	144 1.1646322
65	9.95424251	81 . 91857877
66	7 .84589884	49 ,71419878
67	15 1.1768913	225 1.3831986
68	34 1.5314789	:156 2.3454277
69	18 1	128 1
78	5 .69897888	25 .48855987
71	31 1.4913617	961 2.2241597
72	14 1.1461288	196 1.3136835
73	8 .98388999	64 .81557152
74	5 .77815125	36 .68551937
75	11 1.8413927	121 1.8844987
76	6.77815125	36 .68551937
77	1 8 i	188 1
78	11 1.8413927	121 1.8844987
79	6.77815125	36 .68551937
88	7 .84509804	49 .71419078
81	6 .77815125	36 .68551937
62	5 .69897888	25 .48855907
83	5.69897082	25 .48855987
64	22 1.3424227	494 1.8828987
85	17 1.2384489	289 1.5148845
86	13 1.1139434	169 1.2488698
87	6.77815125	36 .68551937
88	5 .6989788%	25 .48855987
89	3.47712125	9.22764469
90	6.77815125	36 .68551937
91	3 .47712125	9.22764469
92	8.90388999	64 .81557152
93	9.95424251	81 .91057877
94	13 1.1139434	169 1.2488698
95	4 .68285999	16 .36247623
96	9.95424251	81 .91857877
97	3.47712125	9.22764469
98	8.98388999	64.81557152 189 1
99 1 0 9	18 1 B.98388999	188 1 64 .81557152
166		
101	18 i 9.95424251	81 .91957877
102 103	9.95424251	81 .91657877
184	18 1	198 1
185	8 .98368999	64 .81557152
196	34 1.5314789	1156 2.3454277
107	12 1.8791812	144 1.1646322
198	27 1.4313638	729 2.8488822
189	24 1.3882112	576 1.9849831
110	6.77815125	36 .68551937
111	7 .84599894	49 .71419878
112	8 .90388999	64 .81557152
113	3 .47712125	9 .22764469
114	18 1	100 1
115	- 9,95424251	01 .91857877
116	8.98368999	64 .81557152
117	9,95424251	81 .91857877
••*		

As 2

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i

118		1.1750913	275	1.3831986
118		1.4471580		2.0942664
120				2.5314866
		1.5918646		
121		1.8268748		
122		1.5981951		2.8567628
123		1.3979488		
124	-	.98388999	-	.81557152
125		1.2552725		1.5757091
126		1.5051500		2.2654765
127		1.1768913		:.3831906
126				:.3831986
125		1.3979488		
138		1.1768913		
131		1.2141280		1.4499849
132		1.3818388		1.6926790
133		1.3424227		
134	22	1.3424227	484	1.0020987
135	19	L.2787536	361	1.6352108
136				
137	544	SUR	504	sua
138	1635	130.36435	32739	148,24468
139				
14≇	#e30	wean		
	12.201493			
142				
143	wedi an	nedian		
144				
145				
146	variance	variance		
147		.2:222387		
	standard			
	deviation			

191.		**********		

5D=1.64

APPENDIX III

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VLF-EM SURVEY RESULTS

	Α	8]]	c	0	E
1			12\3037 113 (40258 5/		2/337
2 3	5400	INE 5400W 4025	(4025N-5) 4,9	02)N)	
4	5400	4037.5	11.1		
5	5400	4050	7		
6	5400	4062.5	9		
7	5400	4075	8.3		
8	5400	4087.5	16.5		
9	5400	4100 4112.5	20.4		
10 11	5400 5400	4112.5	1		
12	5400	4137.5	3.7		
13	5400	4150	1.1		
14	5400	4162.5	1.3		
15	5400	4175	1.8		
16	5400	4187.5	-1.4		
17	5400	4200	6		
18	5400	4212,5 4225	2.5 5.4		
19 20	5400 5400	4237.5	-1.3		
21	5400	4250	7.7		
22	5400	4262.5	7.4		
23	5400	4275	5.1		
24	5400	4287.5	6.6		
25	5400	4300	19.3		
26	5400	4312.5	6,8 5,7		
27 28	5400 5400	4325 4337.5	3.9		
29	5400	4350	.6		
30	5400	4362.5	8.8		
31	5400	4375	6.5		
32	5400	4387.5	7.6		
33	5400	4400	4.2		
34 35	5400	4412.5 4425	4.1 2.4		
36	5400 5400	4425	3.4		
37	5400	4450	1.5		
38	5400	4462.5	1.5		
39	5400	4475	5		
40	5400	4487.5	2,2		
41	5400	4500	2.6		
42	5400	4512.5	.8 -2,5		
43 44	5400 5400	4525 4537.5	-2.5		
45	5400	4550	-2.9		
46	5400	4562.5	-2		
47	5400	4575	7		
48	5400	4587.5	-2.2		
40	5400	4600			
50 51	5400 5400	4612.5 4625	-1.1 -1.8		
52	5400	4637.5	-3.3		
53	5400	4650	-2.6		
	5400	4662.5	-1.4		
55	5400	4675	5		
51,	5400	4687.5	. 4		
57	5400	4700	- 8		
5% 50	5400 5400	4712.5 4725	.8 -1.1		
60		NE 5600W	-1.1 (4025N-50	258)	
61	5600	4025	8.3	- 1,1	1,7
62	5600	4037.5	1.9	2.8	2.4

.

63	5600	4050	-3.9	1.4	1.7
64	5600	4062.5	-13.4	-3.5	-1.2
65	5600	4075	-10.5	-1.5	.8
66	5600	4087.5	-11.6	-,7	. 5
67	5600	4100	-15.1	-1.5	3
					2.6
68	5600	4112.5	-12.4	3.2	2.0
69	5600	4125	-14.3	5.3	4.5
70	5600	4137.5	-10,5	1.5	3
71	5600	4150	-12,9	.8	3,2
72	5600	4162.5	-22.3	-7.5	1.1
73	5600	4175	-11.3	1.8	2.1
74	5600	4187.5	-21.6	3,5	2,4
75	5600	4200	-25.7	-5.8	3
76	5600	4212.5	-32.4	-9.2	-1.1
77	5600	4225	-26.5	5	3,9
78	5600	4237.5	-24.6	-5.6	-2.4
79	5600	4250	-14.5	.9	1.2
80	5600	4262,5	-24,4	-6.6	-1,2
81	5600	4275	-14	4.1	7.5
82	5600	4287.5	-22,9	-3.1	3.2
83	5600	4300	-25.7	-7.3	1.8
84	5600	4312.5	-21,1	3.1	2.5
85	5600	4325	-35.5	-9	1.4
86	5600	4337,5	-38,7	-15.2	-2.8
87	5600	4350	-21.5	-6.7	-1.6
88	5600	4362,5	-20,7	-4.1	4.1
89	5600	4375	-20.5	-6.1	1,3
	5600	4387.5	-14.8	-3.6	-1.5
91	5600	4400	-12.3	.6	2.6
92	5600	4412.5	-5.2	4	6
93	5600	4425	1.1	3	. 4
94	5600	4437.5	-3.6	1.6	1.1
95	5600	4450	4	4.5	1.5
96	5600	4462.5	3.4	4.3	1.5
97	5600	4475	5.1	6.5	3.1
98	5600	4487.5	3.3	6.4	4.4
99	5600	4500	3	3.8	4.5
100				-2	1.3
	5600	4512.5	-10.8		
101	5600	4525	-14.5	-6.6	-4.8
102	5600	4537.5	-9.6	-1.8	-1.2
103	5600	4550	-5.4	.5	, 8
104	5600	4562.5	3.2	3.6	. 9
105	5600	4575	6.5	1.9	-1.2
106	5600	4587.5	5.6	4	.9
107	5600	4600	5,2	2.9	.5
108	5600	4612.5	1.4	1.2	8
109	5600	4625	4	2	-1.1
			 		1.2
110	5600	4637.5	2.1	.2	
111	5600	4650	. 4	5	-1.1
112	5600	4662.5	4	-1.1	-2.1
113	5600	4675	-1.3	-1.9	- 3
114	5600	4687.5	7	-,1	6
115	5600	4700	. 3	1	. 2
116	5600	4712.5	1.7	- • 5	-1,1
117	5600	4725	8	4	-1.5
118	5600	4737.5	9	5	-1
	5600				
119		4750	9	5	-1.2
120	5600	4762.5	5	. 5	. 2
121	5600	4775	-2.2	.9	-1.4
122	5600	4787.5	3		
123	5600	4800	2.7		
124	5600	4812.5	. 1		
125	5600	4825	-,5		
126	5600	4837.5	1		
127	5600	4850	-1.6		
128	5600	4862.5	-1.8		
120			-1.0		

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129	5600	4875	-1.3		
130	5600	4887.5	7		
131	5600	4900	-2.6		
132	5600	4912,5	9		
133	5600	4925	-1.3		
134	5600	4937.5	-1		
		4950	.4		
135	5600				
136	5600	4962.5	9		
137	5600	4975	-1.1		
138	5600	4987.5	- 1		
139	5600	5000	-,5		
140	5600	5012,5	.3		
141	5600	5025	-2		
142	LI		(4025N-4	4725N)	
143	5800	4025	6.1	-12.547	
144	5800	4037.5	5		
145	5800	4050	3.5		
146	5800	4062.5	4.5		
147	5800	4075	6,8		
148	5800	4087.5	4.4		
149	5800	4100	3.4		
150	5800	4112.5	5.6		
		4125	6.5		
151	5800				
152	5800	4137.5	10.5		
153	5800	4150	4.9		
154	5800	4162.5	7.3		
155	5800	4175	8,6	3.7	2
156	5800	4187.5	12.1	4.8	. I
157	5800	4200	12.7	4.6	1.3
158	5800	4212.5	-1.2	- 3	-2.7
159	5800	4225	-4.3	-2.4	-5,5
160	5800	4237.5	-7.3	3	2.9
161	5800	4250	-1.5	6.7	2.3
162	5800	4262.5	-3.2	7.4	.2
163	5800	4275	6.2	9,8	3.4
164	5800	4287.5	9.4	11.8	1.4
165	5800	4300	-5.4	3.7	1,3
166	5800	4312.5	7.7	8.8	3.6
167	5800	4325	3.2	8.2	1.4
168	5800	4337.5	17.9	18.3	
169	5800	4350	4.3	8.4	.7
170	5800	4362.5	4.4	9.5	1.3
171	5800	4375	17.4	15.6	5.3
172	5800	4387.5	30.9	30,5	10.4
173	5800	4400	36.5	24.7	4.7
174	5800	4412.5	61	36.3	2,9
175	5800	4425	29.3	16,6	9
176	5800	4437.5	2.8	15	8,8
177	5800	4450	-10.6	2.9	-,6
178	5800	4462.5	-24.7	2.4	3.8
179	5800	4475	-4.3	5.5	-,3
180	5800	4487.5	6.6	8.7	4.6
181	5800	4500	8.6	11.3	7.8
182	5800	4512.5	8.5	11.8	5.2
183	5800	4525	1.2	5,1	. 4
184	5800	4537.5	-5.7	-2.5	-1.7
				-2.2	8
185	5800	4550	-6.6	-2.2	
186	5800	4562.5	-3.3	9	7.6
187	5800	4575	5.7	3.5	1.7
188	5800	4587,5	10.8	5.6	1.6
189	5800	4600	6.3	3.8	.5
190	5800	4612.5	. 1		
191	5800	4625	1.7		
192	5800	4637.5	2,3		
193	5800	4650	1.9		
195	5900	40J0 8667 8	1.7		
			-		

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195	5800 4675	1.5		
196	5800 4675 5800 4687.5	1.2		
197	5800 4700	1.3		
198	5800 4712.5	.6		
199 200	5800 4725 LINE 6000W	1.2 (4025N-5025N)		
201	6000 4025	-4.8 1.8	.9	
202	6000 4037.5	3.4 2.6	.3	
203	6000 4050	5.2 8	2.1	
204 205	6000 4062.5 6000 4075	9.4 4.1 9.6 7.4	3,5 2	
205	6000 4087.5	9.6 7.4 11.8 7.6	2.9	
207	6000 4100	1.2 2.8	-, 2	
208	6000 4112,5	1.5 2.4	-1.1	
209 210	6000 4125 6000 4137.5	3.9 6.5	2.9	
210	6000 4137.5 6000 4150	22.8 10.2 25.6 7.8	3.7 1.9	
212	6000 4162.5	19.4 5.3	1	
213	6000 4175	8.2 5.2	2.1	
214	6000 4187.5	5.35	-1.5	
215 216	6000 4200 6000 4212,5	4.3 4.5 4.9 2.6	2.2	
210	6000 4212.5	7.2 2.3	.2	
218	6000 4237.5	5.3 4.4	1.2	
219	6000 4250	2.4 4.6	1.2	
220 221	6000 4262.5 6000 4275	32 3.7 2.6	.2.7	
222	6000 4287.5	5.5 2.5	1	
223	6000 4300	6 4.4	,5	
224	6000 4312.5	7.7.4	-1.7	
225 226	6000 4325 6000 4337.5	5.8 2.7 4.5 1.3	.7 -1.6	
227	6000 4337.3	4.6 1.7	-1.0 1	
228	6000 4362.5	4.2 .6	5	
229	6000 4375	8.6 8.1	4.5	
230 231	6000 4387.5 6000 4400	11.7 6.8 8.4 5.3	3.7 1.4	
232	6000 4412.5	11.8 11.8	3.6	
233	6000 4425	-18.2 -,6	- ,1	
234	6000 4437.5	-31.8 -6.6	3	
235	6000 4450	-31.9 -10.9	-2.2	
236 237	6000 4462.5 6000 4475	-12.4 $-7.3-4.4$ 6.8	2.1	
238	6000 4487.5	16.7 9.8	4.3	
239	6000 4500	2.3 9,5	4.4	
240	6000 4512.5	9.5 7.2	4.3	
241 242	6000 4525 6000 4537.5	-3.4 3.4 5.1 5.1	2.6	
243	6000 4550	10.3 6.8	2.8	
244	6000 4562.5	11.7 7.3	2.3	
245 246	6000 4575	8 7.9 5.1 9.4	5.3	
248	6000 4587.5 6000 4600	5.1 9.4 -9.5 5.2	3.5 3.4	
248	6000 4612,5	-11.8 8.5	4,9	
249	6000 4625	-5.4 14.3	10.9	
250 251	6000 4637.5 6000 4650	-3.4 14.2 4 9.3	6.3 4.7	
252	6000 4662.5	11.5 9.3	3.3	
253	6000 4675	6 5.1	4.4	
254	6000 4687.5	6.7		
255 256	6000 4700 6000 4712.5	3.6		
256	6000 4712.5	3.8 4.8		
258	6000 4737,5	6.5		
259	6000 4750	6.6		
240				
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200	0000	4102.3	0.0		
261	6000	4775	8.2		
262	6000	4787.5	5.9		
263	6000	4800	6.4		
264	6000	4812.5	2.7		
265	6000	4825	2.6		
266	6000	4837.5	3.9		
267	6000	4850	2.1		
268	6000	4862.5	2.5		
269	6000	4875	4.6		
270	6000	4887.5	1.9		
271	6000	4900	3.2		
272	6000	4912.5	-2.1		
273	6000	4925	-1.1		
274	6000	4937.5	6		
275	6000	4950	-1.8		
276	6000	4962.5	-1.6		
277	6000	4975	-1.7		
278	6000	4987.5	-4.6		
279	6000	5000	-3.1		
280	6000	5012.5	-3		
281	6000	5025	-2.3		
282	L	LNE 6200W	(4025N-4	725N)	
283	6200	4025	.3	r	
284	6200	4037.5	4.7	3.4	1.1
285	6200	4050	10.3	5.3	2.2
286	6200	4062.5	10.3	2.7	2.2
287	6200	4075	9.6	4.8	.2
288	6200	4087.5	7.7	1.5	-1.2
289	6200	4100	4.5	1.4	4
290	6200	4112.5	8.5	4.7	.7
291	6200	4125	4.7	2.2	5
292	6200	4137.5	1.8	2.1	.6
293	6200	4150	2.1	3.6	1.1
294	6200	4162.5	.3	1.2	5
295	6200	4175	1	1.7	-,1
296	6200	4187.5	3.8	3.7	.4
297	6200	4200	2.8	2	.3
298	6200	4212.5	-3.4	6	5
299	6200				
299		4225	1	2.1	3
300	6200	4237.5	3.3	4.2	1.4
301	6200	4250	- 4	.7	5
302	6200	4262.5	4.8	2.2	8
303	6200	4275	6.6	3.3	.6
304	6200	4287.5	10.3	3.8	.8
305	6200	4300	9.6	4.5	1
306	6200	4312.5	1,5	2.4	2
307	6200	4325	10	5.1	2.1
308	6200	4337.5	6.3	3.8	1.3
309	6200	4350	16.8	6.4	2.2
310	6200	4362.5	22,1	10.5	3.4
311	6200	4375	22.7	13.8	4.3
312	6200	4387.5	12.5	10.0	
					.1
313	6200	4400	10.6	5.9	1.2
314	6200	4412.5	11.8	5.7	.7
315	6200	4425	11.5	6.3	1.6
316	6200	4437.5	79.5	4	4
317	6200	4450	5.6	4.4	1.6
318	6200	4462.5	8.7	6	3.5
319	6200	4475	17.2	12.2	8,9
320	6200	4487.5	17.1	5.7	1.4
321	6200	4500	37.4	19.6	11.9
322	6200	4512.5	29.7	14.3	2.9
323	6200	4525	20.2	6.9	5
324	6200	4537.5	3.9	5,6	2.2
					4.4
325	6200	4550	-9.4	2.3	5
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320	0200	د . ∠بر ب	,	•. <i>></i>	د.ب
327	6200	4575	6.8	9.1	4.1
328	6200	4587.5	11.7	12.4	4.9
329	6200	4600	3.3	9.6	3.1
330	6200	4612.5	-1.4	5.8	3.4
331	6200	4625	-2.7	3.4	2.6
332	6200	4637.5	-1,2	2.7	1.2
333	6200	4650	5.7	5.6	2.7
334	6200	4662.5	7.1	5.4	1.1
335	6200	4675	7.6	6.4	2.4
336	6200	4687.5	6.5	6,7	2.3
337	6200	4700	4.1	5.4	1.5
338	6200	4712.5	4.2	5.8	1.7
339	6200	4725	1.6	5.2	3
340		INE 6400W	(4025N-5	025N)	
341	6400	4025	-27.1		
342	6400	4037.5	-19-4		
343	6400	4050	-8.4		
344	6400	4062.5	2.5	•	
345	6400	4075	7	•	
346	6400	4087.5	6.3		
347	6400	4100	4.9		
348	6400	4112.5	14.6		
349	6400	4125	10.3		
350	6400	4137.5	6.7		
351	6400	4150	11.7		
352	6400	4162.5	12.1		
353	6400	4175	15.4		
354	6400	4187.5	2.5		
355	6400	4200	1.5		
356	6400	4212.5	5.5		
357	6400	4225	3.6		
358	6400	4237.5	2.8		
359	6400	4250	1.5		
360	6400	4262.5	2.2		
361	6400	4275	2.3		
362	6400	4287.5	3.6		
363	6400	4300	5.8		
364	6400	4312.5	1.5		
365	6400	4325	2.5	4.1	. 2
366	6400	4337.5	3.6	2.7	-1.1
367	6400	4350	6.8	3.5	4
368	6400	4362.5	4.8	3.8	1.1
369	6400	4375	4,5	4.2	1,4
370	6400	4387.5	5	4.5	3.1
371	6400	4400	7,2	I	-1.7
372	6400	4412.5	5.7	2.9	-,3
373	6400	4425	8.2	3.8	.1
374	6400	4437.5	7.7	4.6	.8
37.5	6400	4450	-4.7	3.5	1.2
376	6400	4462.5	-10.6	-1.1	.3
377	6400	4475	9	.9	1
378	6400	4487.5	6.1	-1.4	8
379	6400	4500	4.1	4.6	. 7
380	6400	4512.5	1.6	3.9	1.4
381	6400	4525	12.8	10.6	2.7
382	6400	4537.5	11.1	8.7	1.9
383	6400	4550	16.8	8.2	1.1
384	6400	4562.5	11,2	6.1	1.5
385	6400	4575	10.9	3.8	3
386	6400	4587.5	7.4	4 1	.7
387	6400	4600	5,2	4	2
388	6400	4612.5	-2,2	5.8	1
389	6400	4625	7.9	3.5	. 4
390	6400	4637.5	7.3	5.7	1.7
391	6400	4650	11,1	3.1	1,2
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392	6400	4662.5	9.7	4	. 5
393	6400	4675	10,36	4.8	.6
394	6400	4687.5	6.3	5.4	1.3
395	6400	4700	6.9	4.5	1
396	6400	4712.5	9.4	6.4	2.4
397	6400	4725	10.6	5.1	2
398	6400	4737.5	+6.8		
399	6400	4750	-1.8	3.5	.7
400	6400	4762.5	5	2.7	1,8
401	6400	4775	5.7	6.4	.9
402	6400	4787.5	14.8	3.3	4.2
403	6400	4800	4.4	3.5	1.2
404	6400	4812.5	2.2	4.1	1.7
405	6400	4825	3.1	2.3	1.4
406	6400	4837.5	-,2	2	1.1
407	6400	4850	1.3	1.7	. 2
408	6400	4862.5	. 2	1.6	.9
409	6400	4875	2,5	4	5
410	6400	4887.5	1		
411	6400	4900	7		
412	6400	4912.5	1.3		
413	6400	4925	-,6		
414	6400	4937.5	. 7		
415	6400	4950	4		
416	6400	4962.5	-1.9		
417	6400	4975	-1.6		
418	6400	4987.5	1.3		
419	6400	5000	. 4		
420	6400	5012.5	-2.2		
421	6400	5025	-2.4		
422	L	INE 6400W	(5025N-6	025N)	
423	6400	5025	-2.4		
424	6400	5037.5	.8		
425	6400	5050	4		
426	6400	5062.5	. 5		
427	6400	5075	7		
428	6400	5087.5	-2.2		
429	6400	5100	1.4		
430	6400	5112.5	2		
431	6400	5125	1.6		
432	6400	5137.5	1		
433	6400	5150	1.6		
434	6400	5162,5	1.3		
435	6400	5175	6,5	3,9	1,2
436	6400	5187,5	-4.5	.6	. 4
437	6400	5200	-24.9	-10,4	-1,4
438	6400	5212.5	-27.7	-13.1	-3.2
439	6400	5225	-29,5	-18.9	-7.8
440	6400	5237.5	-9.4		-3,2
441	6400	5250	15.9	9.2	2.6
442	6400	5262.5	16.2	12.8	3.9
443	6400	5275	12.3	10.6	5
444	6400	5287.5	12.9	6.9	3.4
445	6400	5300	11.4	8	2.9
446	6400	5312.5	12.6	6.4	2.6
447	6400	5325	3.9	4.3	2.2
448	6400	5337.5	-6.5	-2.4	-,7
449	6400	5350	-9.6	-4.4	-1.6
450	6400	5362.5	-6.6		-2.3
451	6400	5375	6.4	2.7	.3
452	6400	5387.5	5.6	1.9	-,7
453	6400	5400	4,9	2.8	- 2
454	6400	5412.5	4.7	1.7	-1.1
455	6400	5425	5.5	1.8	-1.1
	6400	5437.5	2.2 5.3	3,2	.2
455			J_ 3	۰. ۲	
456 457	6400	5450	4 2	1	- 5

458	8 6400	5462.5	7.4	2.4	- 4	
459		5475 5487.5	7.1 -2.3	2.2	.5 5	
46		5500	-24,2	-7.4	-1.8	
46:		5512.5	-39.4	-15 9	-3.6	
46;		5525	-39.3	-18	-4.1	
464		5537.5	-3.9	-4.7	-2.5	
46		5550	19.6	16.8	4	
466		5562.5	13.6	17.5	5.4	
468		5575 5587.5	$16.3 \\ 15.8$	$\begin{array}{c}14.9\\12.6\end{array}$	3.8 1.6	
469		5600	13.2	12.1	3.2	
470		5612.5	-3.7	7.4	4.1	
471		5625	-1.3	7.4	4.3	
472		5637.5	-4.I	3.9	1.8	
472		5650	12.5	8.5	3.2	
474		5662.5 5675	12.7 6.9	8.7	3.4	
476		5687.5	1	4.8 2.5	1.9	
477		5700	13.2	8.9	2.7	
478		5712.5	11.3	7.6	3.1	
479		5725	10.7	8.1	2.4	
480		5737.5	9.9	5.8	1.7	
481 482		5750 5762.5	11.6	5.2	1.6	
482		5762.5	8.1 7.7	4.8 3.4	_9 _4	
484		5787.5	8.8	3.5	.9	
485		5800	6.8	3.1	.5	
486		5812.5	7.5	3.5	6.3	
. 487		5825	5.7	2.6	.3	
488		5837.5	2.36	1.9	8	
489 490		5850 5862,5	-4.6 -15.7	2	.1 -1.3	
491		5875	-8,5		-1.2	
492		5887.5	6.1	-1.6	-2.2	
493		5900	15.7		. 4	
494		5912.5	12.7	5.2 6 5.8	.6	
495 496		5925	11.5	5.8	1.2	
490		5937.5 5950	15.2 8.1	7,8 6	2.6 1.5	
498		5962,5	8.9	4.6	1.5	
499		5975	5,2	4.6	1.9	
500		5987.5	3.1	2.3	- 2	
501		6000	.9	2.4	.7	
502		6012.5	3.4	3.3	2,6	
503 504		6025 INE 6400W	2.2 (6225N-66	.4	9	
505		6200	3.8	, n		
506		6212.5	2.2			
507	6400	6225	-2.4	3	9	
508		6237.5	-2 2,2	. 2	-,6	
509		6250	2.2	.9	8	
510 511	6400 6400	6262.5 6275	4.3 11.4	1.7 3.4	-1.1 -1.4	
512	6400	6287.5	13.4	5.4	-1.4	
513		6300	8.7	5.1	.4	
514	6400	6312.5	10.3	6.6	.8	
515		6325	10.6	4.7	. 4	
516	6400	6337.5	2.5	4.2	3	
517 518	6400 6400	6350 6362 5	7.4	2.8	7	
518	6400	6362.5 6375	7.3 5.7	3.4 1.7	6 5	
520	6400	6387.5	4.2	2.3	5	
521	6400	6400	3.8	1.6	8	
522	6400	6412,5	3.7	1.8	-,3	
5.0.3	6400	61.75	7 5	5	1 T	

524	6400 6437.5	1.7	.9	-1-1
525	6400 6450		5	-1.5
526	6400 6462.5		3.2	1.1
527	6400 6475		5	-2.2
528 529	6400 6487.5 6400 6500		-3	-1_8 -1
530	6400 6512,5	-1.2	-1	-1,8
531	6400 6525		5	-2
532	6400 6537.5	.4	. 2	-1,2
533	6400 6550		-1.5	-3,1
534	6400 6562.5	1	4	-1
535	6400 6575	3	5	-1.2
536	6400 6587.5	-1.2		
537	6400 6600			
538	6400 6612.5	6		
539	LINE 6600			
540	6600 4325	3.3	2.4	1
541 542	6600 4337.5 6600 4350	5.5 5.3	$2.6 \\ 2.7$.3 .2
543	6600 4362.5	7.6	3.9	.1
544	6600 4375	7.2	2.6	1
545	6600 4387.5	6.9	2.6	3
546	6600 4400	Š.9	2,3	.7
547	6600 4412.5	3.2	2,2	.6
548	6600 4425	6	1.2	8
549	6600 4437.5	3.6	4 2	1.2
550	6600 4450	7.9	7_1	1.1
551	6600 4462.5	22.8	14.9	3.7
552	6600 4475	9.6	10.9	3.7
553	6600 4487.5 6600 4500	-5.3	7	, 4
555	6600 4500 6600 4512.5	-16.2 -17.5	.4 -3.4	1.7
556	6600 4525	-1,4	2.8	1.3
557	6600 4537,5	3.9	6.4	4.2
558	6600 4550	4.9	10.8	6.5
559	6600 4562.5	19.1	12.4	5
560	6600 4575	17.6	11.3	3.4
561	6600 4587.5	15.7	9.4	4.1
562	6600 4600	7.3	5	1.7
563	6600 4612.5	2.4	3.2	1.4
564	6600 4625	-2.6	.3	- 1
565 566	6600 4637.5 6600 4650	8.3	4.9 9.8	2.1
567	6600 4662.5	$14.4 \\ 11.5$	9.0 8.8	3.9 4.6
568	6600 4675	7.7	9	4 4
569	6600 4687.5	11.5	7.5	1.5
570	6600 4700	13.4	8.2	3.4
571	6600 4712.5	7	5.8	2.3
572	6600 4725	4.5	3.3	1.7
573	6600 4737.5	8,5	4.7	2.3
574	6600 4750	4.8	3.7	1.7
575	6600 4762,5	5,2	2	2
576	6600 4775	6.7	4.2	.9
577	6600 4787.5	9.5	5.8	.9
578	6600 4800	7.8	7.3	2.4
579	6600 4812.5	7.7	5.1	1.6
580	6600 4825	6.7	5.6	2.7
581	6600 4837.5	8.3	5.5	2.6
582 583	6600 4850 6600 4862.5	5.6	3.4	, 1
583 584	6600 4862.5 6600 4875	$3.9 \\ 2.1$	2 1.6	1.3
585	LINE 6800V			. >
586	6800 4025	-1.2		
587	6800 4037.5	1.3		
588	6800 4050	1. 5		
600	6000 10/FT-	. ,		

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203	0000	4004.5	4.4
590 591	6800 6800	4075 4087,5	-3.8 3.4
592	6800	4100	5.4
593	6800	4112.5	3.3
594 595	6800 6800	4125 4137,5	4 1.9
596	6800	4150	2.9
597	6800	4162.5	3
598 599	6800 6800	4175 4187.5	2.2 1.4
600	6800	4200	3.1
601	6800	4212.5	.7
602 603	6800 6800	4225 4237.5	6.6 1.6
604	6800	4250	.3
605 606	6800 6800	4262.5 4275	8.3 3.4
607	6800	4287.5	3.9
608	6800	4300	6.9
609	6800	4312,5	1.9
$\begin{array}{c} 610 \\ 611 \end{array}$	6800 6800	4325 4337,5	1_1 .8
612	6800	4350	1.5
613	6800	4362.5	5.8
614 615	6800 6800	4375 4387.5	5.9 8.3
616	6800	4400	11,8
617	6800 6800	4412.5	16.5
$\begin{array}{c} 618 \\ 619 \end{array}$	6800 6800	4425 4437.5	8.9 5.5
620	6800	4450	5.9
621 622	6800 6800	4462.5	7.8
623	6800	4475 4487.5	11.3 10.3
624	6800	4500	13.5
625 626	6800 6800	4512.5 4525	3.4 15.7
627	6800	4537.5	17,9
628	6800	4550	6.8
629 630	6800 6800	4562.5 4575	9.8 6.3
631	6800	4587.5	15.1
632	6800	4600	18.8
633 634	6800 6800	4612.5 4625	$21.3 \\ 18.8$
635	6800	4637.5	13.1
636	6800	4650	15.3
637 638	6800 6800	4662,5 4675	14.5 14.8
639	6800	4687.5	6.3
640	6800	4700	2.6
641 642	6800 6800	4712.5 4725	7.5 6.4
643	6800	4737.5	14.6
644	6800	4750	11.1
645 646	6800 6800	4762.5 4775	6.8 5.8
647	6800	4787.5	5.4
648 640	6800	4800	8.1
649 650	6800 6800	$ 4812.5 \\ 4825 $	12.1 11.2
651	6800	4837.5	6.6
652 652	6800 6800	4850	7.5
653 654	6800 6800	4862.5 4875	7.8 11.7
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655	6800	4887.5	10.6		
656	6800	4900	10.6		
657	6800	4912.5	5.8		
658	6800	4925	10.6		
659 660	6800	4937.5 4950	7.4 7.2		
660 661	6800 6800	4962.5	6.7		
662	6800	4902.5	6		
663	6800	4987.5	4.6		
664	6800	5000	3.3		
665	6800	5012.5	2.3		
666	6800	5025	2.8		
667	L	INE 6800W	(4975N-S	975N)	
668	6800	4975	3.6		
669	6800	4987.5	3.1		
670	6800	5000	3.6		
671	6800	5012.5	2.6		
672	6800	5025	1.4		
673 674	6800	5037,5 5050	.4 1.7		
675	6800 6800	5062,5	2		
676	6800	5075	2.6		
677	6800	5087.5	1.4		
678	6800	5100	.4		
679	6800	5112.5	1.6		
680	6800	5125	1	1.4	1.8
681	6800	5137.5	1.5	2.4	2,2
682	6800	5150	1.5	.8	.3
683	6800	5162.5	1.8	.9	. 2
684	6800	5175	2.5	1.3	5
685	6800	5187.5	.8	.2	5
686 687	6800 6800	5200 5212.5	-1.5 -5.7	.8 -3.9	$1.3 \\ -2.1$
688	6800	5225	-9.7	-7.3	-2.8
689	6800	5237.5	-10.5	-5.4	-3.9
690	6800	5250	3.8	1.5	.4
691	6800	5262.5	8.4	6.2	4.3
692	6800	5275	4.8	5.4	1.6
693	6800	5287.5	5.8	6.1	3.4
694	6800	5300	1.5	3	1.9
695	6800	5312.5	3.2	3.7	1,7
696	6800	5325	-4.2	-2.7	-1.4
697	6800	5337.5	-14	-7.6	-2.9
698 699	6800 6800	5350	-26.6	-15.1	-8.1
700	6800	5362,5 5375	.4 15.6	11,7	1.8 12,2
701	6800	5387.5	-4.7	1.9	.8
702	6800	5400	-3.2	-8.3	-9.1
703	6800	5412.5	6.1	-1.4	-6.4
704	6800	\$425	-6,3	-1.1	-15
705	6800	5437.5	-15.8	-6.8	8
706	6800	5450	-23.2	-10.6	-3.6
707	6800	5462.5	-2.3	.6	1.3
708	6800	5475	- 2	2.5	1.4
709	6800	5487.5	6.9	4.9	.8
710	6800	5500	9.4	6	1.3
711	6800	5512.5	2.1	5.1	1.6
712 713	6800	5525	-16.5	-1.4	.6
714	6800 6800	5537.5 5550	-21.9 -21.8	-3.6 -5.1	.7
715	6800	5562.5	-14.6	-1.6	-1.7
716	6800	5575	-18.2	-4.7	-1.5
717	6800	5587.5	-21.7	-8.9	-3.5
718	6800	5600	-5.3	-3.2	6
719	6800	5612.5	. 3	3.5	.8
720	6800	5625	-1.3	1,7	. 6

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721	6800 5637.5	0 1 2 0	a 1	
		-9.1 3.8	3.1	
722	6800 5650	-2.6 1	1.5	
723	6800 5662.5	-5.84	.5	
724	6800 5675	-4.5 .9	1_1	
725	6800 5687.5	-5,5 1,2	0	
726	6800 5700	-6.29	-1,5	
727	6800 5712.5	7.3 7.2	1.2	
			1.2	
728	6800 5725	5.1 4.6	.8	
729	6800 5737,5	2.7 5.3	1.4	
730	6800 5750	3.1 7.7	4.4	
731	6800 5762.5	.8 3.2	1.3	
732	6800 5775	3.1 5.1	1.3	
733	6800 5787.5	-5.6 .6	2	
734	6800 5800	-78	3	
735	6800 5812.5			
		-11 -1.5	1.6	
736	6800 5825	-10.5 -3.8	-2.3	
737	6800 5837.5	4.3 3.8	. 1	
738	6800 5850	-5.2 5.3	2.9	
739	6800 5862.5	-13.7 3.5	4.4	
740	6800 5875	-22 -2	.2	
741	6800 5887.5	20.5 2.7	3.1	
742	6800 5900	23.3 12.1		
743			3.7	
	6800 5912.5	30.7 14.9	4.6	
744	6800 5925	25.8 13.5	4.3	
745	6800 5937.5	22.1 11.5	3.2	
746	6800 5950	14.2 6.6	1.8	
747	6800 5962.5	-6.7 2.6	1.7	
748	6800 5975	-8.79	.8	
749	LINE 7200W	(4025N-5025N)	••	
750	7200 4025	3.3		
751		3		
		3		
752	7200 4050	-4.8		
753	7200 4062.5	-,2		
754	7200 4075	-2.5		
755	7200 4087.5	-3.2		
756	7200 4100	- 4		
757	7200 4112.5	2.6		
758	7200 4125	.1		
759		, , ,		
		2.8		
760	7200 4150	-2,1		
761	7200 4162.5	-2.3		
762	7200 4175	-2.4		
763	7200 4187.5	-3.2		
764	7200 4200	-2.6		
765	7200 4212.5	-1.6		
766	7200 4225	.6		
767	7200 4237.5	.u I		
768	7200 425715	-1.2		
769		-1.6		
		-1.1		
770	7200 4275	.5		
771	7200 4287.5	-1.3		
772	7200 4300	5		
773	7200 4312.5	1,6		
774	7200 4325	-1.3		
775	7200 4337.5	.7		
776	7200 4350	-1.1		
777	7200 4362.5	.5		
778	7200 4302.5			
		-,6		
779	7200 4387.5	5		
780	7200 4400	, 3		
781	7200 4412.5	.9		
782	7200 4425	-1.4		
783	7200 4437.5	- <u>-</u> 4		
- 784	7200 4450	1.1		
785	7200 4462.5	. 6		
786	7200 4475	_1 1		
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787	7200	4487,5	2.3
788	7200	4500	- 7
789 790	7200 7200	4512.5 4525	4.4 .6
791	7200	4537.5	1.6
792	7200	4550	I
793 794	7200 7200	4562.5 4575	2.4 2.2
795	7200	4587.5	7
796	7200	4600	4.4
797 798	7200 7200	$4612.5 \\ 4625$	1.2 3.4
799	7200	4637.5	1.7
800 801	7200 7200	4650 4662.5	-3.6
802	7200	4675	2.7
803	7200	4687.5	8.1
804 805	7200 7200	4700 4712,5	6.9 6.5
806	7200	4725	7.5
807	7200 7200	4737.5 4750	7.6
808 809	7200	4762.5	10.2
810	7200	4775	10.1
811 812	7200 7200	4787.5 4800	13.9 10.8
813	7200	4812.5	12.5
814 815	7200 7200	4825 4837.5	15 6.5
816	7200	4850	9.6
817	7200	4862.5	9.7
818 819	7200 7200	4875 4887.5	12.5 14.3
820	7200	4900	9.7
821 822	7200 7200	4912.5 4925	8.8 7.4
823	7200	4937.5	6.1
824	7200	4950	6.7
825 826	7200 7200	4962.5 4975	5.7 4.1
827	7200	4987.5	3.1
828 829	7200 7200	5000 5012.5	2 5.4
830	7200	5025	5.9
831 832	7200 1		(5025N-5500N)
833	7200	5025 5037.5	.7 1.7
834	7200	5050	1.3
835 836	7200 7200	5062.5 5075	3.8 3
837	7200	5087.5	2.4
838 839	7200 7200	5100 5112,5	1.3 1.6
840	7200	512.5	1.9
841	7200	5137.5	, 2
842 843	7200 7200	5150 5162.5	1.4 3.4
844	7200	5175	3.1
845 846	7200 7200	5187.5 5200	.4 3.1
847	7200	5212.5	.5
848 849	7200 7200	5225 5237.5	.9 1.8
850	7200	5250	3.6
851	7200	5262.5	3.5

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240	1200	2212	1.0		
853	7200	5287.5	2.3		
854	7200	5300	2.5		
855	7200	5312.5	3.9		
856	7200	5325	4		
857	7200	5337.5	3.5		
858					
	7200	5350	1.6		
859	7200	5362.5	- 8		
860	7200	5375	1.9		
861	7200	5387.5	. 3		
862	7200	5400	1.5		
863	7200	5412.5	2.2		
864	7200	5425	2		
865	7200	5437.5	2		
866	7200	5450	2.3		
867	7200	\$462.5	1.8		
868	7200	5475	2.5		
869	7200	5487.5	1.2		
870	7200	5500	1.4		
871	Т. Т	NE 7600W	(4975N-5325	3	
872	7600	4975	2,1	/	
873	7600	4987.5	2.2		
874	7600	5000	3.1		
875	7600	5012.5	2.5		
876	7600	5025	3.1		
877	7600	5037.5	4		
878	7600	5050	4.2	1.7	.6
879	7600	5062.5	3.5	1.7	.9
880	7600	5075	6.8	2	- , 2
881					
	7600	5087.5	10.4	3.6	. 5
882	7600	5100	13.6	5.4	.8
883	7600	5112.5	14.5	4	6
864	7600	5125	10.5	5.9	.3
885	7600	5137,5	11.3	5.4	1
886	7600	5150	12.9	5.9	1.6
887	7600	5162.5	13,5	3.3	8
888	7600	5175	4.6		
				3.1	1.4
889	7600	5187.5	4.5	1.6	7
890	7600	5200	7.9	3.5	1.6
891	7600	5212.5	11_4	2.1	7
892	7600	5225	8.4	1.4	-2.7
893	7600	5237.5	11.1	2.6	8
894	7600	5250	7.3	1.7	-1.2
895	7600	5262.5	5.7	1.5	-1.1
896	7600	5275	7.5		
			7.5	1.8	9
897	7600	5287.5	8.9	2.8	- 4
898	7600	5300	10.5	2.6	1
899	7600	5312.5	10.2	2,6	. 1
900	7600	5325	10.4	2.6	•6
901	LI	NE 8000W	(5025N-5625	N)	
902	8000	5025	.7		
903	8000	5037.5	1_7		
904	8000	5050	~2		
905	8000	5062.5	2		
906	8000	5075	-1,2		
907	8000	5087.5	.5		
908	8000	5100	1.3		
909		5112.5	1		
	8000				
			1.4		
910	8000	5125			
910 911	8000 8000	5125 5137.5	. 2		
910 911 912	8000 8000 8000	5125 5137.5 5150	.2		
910 911 912 913	8000 8000 8000 8000	5125 5137.5 5150 5162.5	.2 5 .6		
910 911 912 913 914	8000 8000 8000 8000 8000	5125 5137.5 5150 5162.5 5175	.2 5 .6 .7		
910 911 912 913 914 915	8000 8000 8000 8000 8000 8000	5125 5137.5 5150 5162.5 5175 5187.5	.2 5 .6 .7 3		
910 911 912 913 914 915 916	8000 8000 8000 8000 8000 8000 8000	5125 5137.5 5150 5162.5 5175 5187.5 5200	.2 5 .6 .7 3 2.3		·
910 911 912 913 914 915	8000 8000 8000 8000 8000 8000	5125 5137.5 5150 5162.5 5175 5187.5	.2 5 .6 .7 3		

	918	8000	5225	2		
	919	8000	5237.5	2.7		
	920	8000	5250	2.4		
	921	8000	5262.5	2.7		
	922	8000	5275	3.4		
	923	8000	5287.5	4.9		
	924	8000	\$300	7.1	2.7	, 2
	925	8000	5312.5	9.4	3.7	.8
	926	8000	5325	5.5	2.3	3
	927	8000	5337.5	8.5	3.5	-,6
	928	8000	5350	8.4	3.5	. 6
	929	8000	5362.5	9.2	4.9	3
	930	8000	5375	11.1	5.6	.4
	931	8000	5387.5	11.9	7.7	2.6
	932	8000	5400	9.9	6.4	1.7
	933	8000	5412.5	11.7	8.5	3.4
	934	8000	5425	16.2	10.4	4.4
	935	8000	5437.5	13.7	9.8	4.3
	936	8000	5450	14.3	8.4	3.7
	937	8000	5462.5	14.6	9	4
	938	8000	5475	12.4	8,2	3.7
	939	8000	5487.5	11.6	9.2	4.7 3.7 3.2
	940	8000	5500	8.6	7.5	3.7
	941	8000	5512,5	6.6	5.7	3.2
	942	8000	5525	6.7	7.2	4.3
	943	8000	5537.5	7.6	5.5	3.1
	944	8000	5550	8.7	6.3	4.3
	945	8000	5562.5	7.I	4.7	1.8 2.8
	946	8000	5575	6.6	5.6	2.8
	947	8000	5587.5	6.4	4.1	1.2
•	948	8000	5600	9.1	5.9	2.4
	949	8000	5612.5	6.7	3.1	. 7
	950	8000	5625	5.8	3.9	1.8

APPENDIX IV

MAGNETIC SURVEY RESULTS

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	600.05.0	ATEC (-)	Magnetometer #1		weter #2 Consolated	Total Ciald	Niur na 1	Corrected
	LOUKSIN	IALES (B)	Total Field					Total Field
DATE	Hest	North	(gannas)	(gannas)	(ganwas)	(ganhas)	(gannas)	(gannas)
11\4\66	8553	5080	35295			58895		58835
•	5388	4958	58185			58105		58105
								58086 Selen
								58103 59872
								58122
•								58886
		4658	52836			56896		5B 89 6
•	6888	4608	58155			58155		58155
•	6883	4558	58133					58133
•						58128		58128
				!!! /1/:!!!!!!	***********			
								58160 58191
	0366	9144	20131			4 0131	•	30171
:1/5/86	6827	5022	58126					58128
				. بـ				58120 50245
								58285 58173
•								5816B
								58283
		3888						58129
•	7152	5200	59151				-8	58143
•	720B	5886	38124			58184	-10	58:74
1\5\86	7280	5078	58184			58184	-10	58174
•	7260	4958	59 88 3			58883	-11	58072
•	7268	4988	58885					58073
		4956	58887					58874
								58865 58863
								58071
								58868
								58219
•	7288	4558	58893				-21	53873
,	7268	4588	56859					SB437
	7268	4450	58855					58833
								38861
								58851 50040
								58846 58837
								58872
•		4158	58101					58871
11\5\86			58893			58893		58062
•	7288	4858	59894			58894	-32	58862
•	7288	4688	38886			58886	-33	56853
:1\5\86	7299	4893	56886			58886	-33	58853
r	7156	4836	58113			58:13	-35	56878
		4602	58114			58114	-36	58878
								58866
								58649 58878
۲								58031
•								58453
•	6886	4688	58139					58895
	111/4/66 111/4/66 111/5/66 111/5/86 111/5/86 111/5/86	DATE Hest 13\\4\66 6288 - 6388 - 6888 - 7888 - 7288 - 7288 - 7288 - 7288 - 7288 - 7288 - 7288 - 7288 - 7288	11\4\66 6228 588 - 5302 4558 - 6620 4900 - 6628 4858 - 6628 4858 - 6628 4768 - 6628 4768 - 6628 4768 - 6828 4668 - 6828 4668 - 6828 4668 - 6828 4688 - 6828 4688 - 6828 4588 - 6828 4588 - 6828 4588 - 6828 4588 - 6828 5828 - 6828 5828 - 6828 5828 - 7288 5828 - 7288 5828 - 7288 4358 - 7288 4358 - 7288 4588	DATE Hest North (gammas) 11\\4\56 6228 5882 5225 5382 4958 56185 6680 4908 58826 6688 4928 55872 6688 4928 58826 6688 4928 58826 6688 4558 58226 6688 458 58235 6688 458 58235 6688 458 58235 6688 458 58122 6688 458 58123 6688 4584 58123 11\5\66 6388 5828 6688 5828 58123 11\5\66 6388 5828 6698 5828 58123 11\5\66 6388 5828 11\5\66 6388 5828 11\5\66 5888 58131 11\5\66 5888 58131 7288 5888 58131 <t< td=""><td>DATE Hest North Gamma S Gamma S 111/4/66 6288 5982 55235 (gamma S) 111/4/66 6288 4956 55235 (gamma S) - 5388 4956 55812 (gamma S) - 6688 4956 55812 (gamma S) - 6688 4956 58123 (gamma S) - 6688 4988 58123 (gamma S) - 6688 4988 58123 (gamma S) - 6688 4588 58123 (gamma S) - 6688 58125 (gamma S) (gamma S) - 6688 58126 (gamma S) (gamma S) -</td><td>DATE Hest North Total Field Reading (gamas) Reading (gamas) 1114166 6280 5080 5225 (gamas) (gamas) (gamas) 1114166 6280 4968 56825 56125 (gamas) (gamas) 1114166 6280 4968 58826 (gamas) (gamas) 11166 6280 4968 588122 (gamas) (gamas) 11166 6280 4788 58896 (gamas) (gamas) 11156 6880 4586 58123 (gamas) (gamas) 11156 6880 4586 58128 (gamas) (gamas) 11156 6880 58128 58133 (gamas) (gamas) 11156 6880 58128 58128 58128 (gamas) (gamas) 11156 6888 58848 58128 58128 58121 (gamas) (gamas) 111576 5888 58826 58121 (gamas) (gamas)<!--</td--><td>DATE Horth Total Frid Reading Reading Intensity JATE Worth (gamas) (gamas) (gamas) (gamas) 1114166 GG28 5082 5225 50835 50855 - GG28 5082 50825 50825 50825 - GG28 4968 50825 50827 50827 - GG28 4968 50825 50825 50825 - GG28 4958 50825 50825 50825 - GG28 4968 50825 50825 50825 - GG28 4688 50123 50123 50123 - GG28 4588 50126 50128 50128 - GG28 4588 50128 50128 50128 - GG28 50245 50235 50128 50128 - GG28 50245 50235 50128 50128 - GG2</td><td>DATE Hest North Cgamash Gpamash Ggamash Ggamas</td></td></t<>	DATE Hest North Gamma S Gamma S 111/4/66 6288 5982 55235 (gamma S) 111/4/66 6288 4956 55235 (gamma S) - 5388 4956 55812 (gamma S) - 6688 4956 55812 (gamma S) - 6688 4956 58123 (gamma S) - 6688 4988 58123 (gamma S) - 6688 4988 58123 (gamma S) - 6688 4588 58123 (gamma S) - 6688 58125 (gamma S) (gamma S) - 6688 58126 (gamma S) (gamma S) -	DATE Hest North Total Field Reading (gamas) Reading (gamas) 1114166 6280 5080 5225 (gamas) (gamas) (gamas) 1114166 6280 4968 56825 56125 (gamas) (gamas) 1114166 6280 4968 58826 (gamas) (gamas) 11166 6280 4968 588122 (gamas) (gamas) 11166 6280 4788 58896 (gamas) (gamas) 11156 6880 4586 58123 (gamas) (gamas) 11156 6880 4586 58128 (gamas) (gamas) 11156 6880 58128 58133 (gamas) (gamas) 11156 6880 58128 58128 58128 (gamas) (gamas) 11156 6888 58848 58128 58128 58121 (gamas) (gamas) 111576 5888 58826 58121 (gamas) (gamas) </td <td>DATE Horth Total Frid Reading Reading Intensity JATE Worth (gamas) (gamas) (gamas) (gamas) 1114166 GG28 5082 5225 50835 50855 - GG28 5082 50825 50825 50825 - GG28 4968 50825 50827 50827 - GG28 4968 50825 50825 50825 - GG28 4958 50825 50825 50825 - GG28 4968 50825 50825 50825 - GG28 4688 50123 50123 50123 - GG28 4588 50126 50128 50128 - GG28 4588 50128 50128 50128 - GG28 50245 50235 50128 50128 - GG28 50245 50235 50128 50128 - GG2</td> <td>DATE Hest North Cgamash Gpamash Ggamash Ggamas</td>	DATE Horth Total Frid Reading Reading Intensity JATE Worth (gamas) (gamas) (gamas) (gamas) 1114166 GG28 5082 5225 50835 50855 - GG28 5082 50825 50825 50825 - GG28 4968 50825 50827 50827 - GG28 4968 50825 50825 50825 - GG28 4958 50825 50825 50825 - GG28 4968 50825 50825 50825 - GG28 4688 50123 50123 50123 - GG28 4588 50126 50128 50128 - GG28 4588 50128 50128 50128 - GG28 50245 50235 50128 50128 - GG28 50245 50235 50128 50128 - GG2	DATE Hest North Cgamash Gpamash Ggamash Ggamas

11\5\66	68 9 0	4000	58139		58139	-43	58896	m (2
•	6888	4958	58166		59168	-45	58123	- 146
•	6888	4188	58154		\$3154	-46	28183	
•	6888	4156	58184		58184	-47	58137	
• •	6888	4228	58156		58156	-48	58188	
•	8528	4258	18172		58222	-49	58173	
•	6395	4308	58225		58225	-58	58175	
	55 83	4358	58284		58204	-52	58152	
н	6822	4488	58216		53216	-53	58163	
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11/6/66	6302	5222	56;:::		58112	8	58112	
4	6758	5888	5614:		58141	8	58141	
۰	6732	5888	58142		58148	1	58141	
•	6657	5882	52164		\$8164	1	58165	
•	6502	5328	55.40		58:43	1	58144	
•	6558	5888	59802		58888	2	58862	
•	6588	5888	59288		59288	2	59282	
•	6458	5886	56648		58646	2	58658	
•	6438	5882	55532		58532	2	58534	
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44 10.00	5480	4958	58151		58161	3	58164	
	5488 5488	4988	58535		58596	3	58593	
	5466 5488	4858	58317		58317	3	58324	
			55483		56483	4	56487	
•	64 89 6403	4820			38983 58141	4	58145	
-	6402	4752	58:43					
-	64 8 8	4768	59489		58486	4	58484 50421	
	6488	4658	59426		53426	5	59431	
	6468	4689	58849		58849	5	58854	
	6408	4558	58132		58132	5	58137	
	64 8 8	4538	58896		59096	5	58181	
•	6488	4458	58885		58985	6	58691	
	6488	4488	58751		58751	6	58757	
•	5488	4350	56869		58669	6	58875	
•	64 0 0	4388	58183		58183	7	58118	
•	6488	4258	58991	•	58892	7	56899	
•	6488	4288	58678	•	5867 8	7	58677	
•	6460	4158	56897	1	59897	8	5618S	
11\5\86	6488	4188	36105		58165	8	56113	
	5428	4858	59184		59184	8	58112	
•	6488	4086	58258		58238	Û	59698	
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11\6\86	6400	4060	58898		58098	8	58698	
	5458	4888	58739		58739	9	58748	
•	6588	4668	58232		58535	9	58544	
•	6558	4828	58441		58441	9	58458	
•	68 8	4868	58160		58168	10	58178	
Ľ	6650	4828	68834		68894	18	£2:34	
•	6788	4202	58674		58574	18	56624	
	6758	4888	59346		59346	11	59357	
•	6888	4038	\$9771	:	59771	11	58782	
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11\6\86	6488	4880	56032		56898	8	58898	
•	635 4	4808	Saito		58146	11	58157	
•	6388	4288	59163		58163	11	58114	
•	6258	4222	59:33		58133	12	58145	
•	6288	4828	38832		58632	12	58844	
*	6159	4806	59235		59285	12	59217	
۲	6198	4880	55:48		58:48	13	5\$153	
۲	6858	4896	56194		53294	13	59387	
¢	6083	4868	53616	:	58616	13	58629	
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•	6888	4388	58213					
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•	6883	4488	58215		58215	16	58231	
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		4488	58153		58153	1	58153	
					56196	3	58201	
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•			36722		38222		30728	
•							-	
•	6828	4782	58215					
•	6868	4758	58226			21	58247	
•	6836	4922	58248		56248	24	58264	
					58248	27	58273	
•	6868	2868	58266		55266	20	28381	
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	•	6552	5888	58118	58119	-23	58687
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	•	7288	505B	58275	58279	8	58279
	•	7288	6182	58238	58238	8	5BZ38
	•	7286	6158	58194	58194	1	58195
	•	7200	6208	58215	58215	i	58216
	•	7228	£ 25£	56123	53289	:	38218
		7280	6322	52224	58224	:	5B225
	•	7238	6358	58223	58239	:	58249
		7183	5428	56117	59222	2	58222
	•	21.22	8432	53144	56244	2	59246
	•	7122	6562	58243	59243	2	5624 <u>5</u>
	•	7288	6558	58231	58231	î	\$8233
	•	7286	£6 88	58225	58225	2	56227
	-	7288	6658	58215	58215	3	58218
	•	7288	6708	58214	58214	3	58217
	•	7282	6758	58228	58228	3	58231
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	•	7288	6954	58264	58234	ý	58268
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	1215136	5262	7200	58285	58265	4	58283
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		7488	6658	58188	58186	6	58185
	•	7488	6688	58154	58184	7	58191
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	•	7436	5853	38174	58174	9	58183
	•	7462	6608	58160	58169	9	56169
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	1215186	7488	8668	38:68	55168	÷	55:63
	•	7358	6888	58230	58238	3	58259
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	•	6488	6189	58229	58228	1	58221
		6488	6158	59238	58238	2	58232
	•	5488	5288	58201	58221	3	58284
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	:	64 88 64 88	6250 6300	58232 58225			58232 58225	4	58229
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	•	£480	6652	59128			58125	18	56138
	•	6408	6788	58234			53234	13	58244
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	•	6488	6658	53236			58288	13	58221
	,	6408	\$388	58228			58228	13	58241
	•	6480	£95a	58221			52221	14	56235
		6488	7622	56175			56175	15	58198
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	1217186	6428	7362	58175			38281	15	38277
	•	645 8	7062	58263					
	•	\$580	7228	58281			58281	16	5B237
	-	6558	7883	58195			56195	17	59212
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	•	668 8	685B	58224			58224	28	58244
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	•	5668	6758	58237			59237	<u>.</u>	
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-	٠	6638	665B	\$8217			55217	23	55248
	-	6669	5689	58316			53316	24	5334 8
		8966	6556	58226			58226	24	56258
	•	6688	6588	58215			58215	25	58242
		6688	6450	58177			58177	26	582 8 3
	-	6688	6488	\$7958			57938	27	58625
		5600	6358	58214			58214	27	58241
		5638	5328	56237			19137	23	58265
							58251	29	56264
		5582	6258	58251				52	52179
		5682	6228	58143			53145		
	•	55 86	8153	53155			58165	32	56215
	•	5622	5169	5815 2			58152	31	58181
	-	6688	6652	58186			58188	32	58212
	•	6668	6808a	58151			58151	33	58184
	12\7\86	6808	5888	58283			58289	33	58242
		6808	6252	58208			53296	34	58242
		5888	6136	56234			58234	35	58265
	3						58228	36	58264
		6306	6158 7 107	S8228			56213	36	58249
	-	5688	6202	56213 581/05					58232
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	•	6866	6306	53212			58215	36	58253
	•	6336	635B	58238			56234	39	58269
	•	1968	6138	58354			58354	42	56394
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		5402	3:33		-10	58475	58475	1	53476
		6426	3158		õ	56485	58485	2	58497
					-22	53465	58465	3	56468
		64 8 7	0208				58488	4	58484
		64 88	3250		-5	5946 8			
	•	6488	3388		-15	58478	58478	4	58474
	•	5488	3353		-28	56465	58465	5	58470
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		6488	3458		-90	\$8395	56395	7	55482
		6488	3502		- 30	58395	58395	7	58482
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•	6483	3652		-88	58485	58485	1 B	58415 111 (11
•	6466	3768		-88	58405	58485	1 6	58415
	6498	3758		-48	58445	58445	н	58456
	6488	3836		-78	58415	5841S	12	58427
	6400	3658		-110	\$8375	58375	13	56068
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,	5688	3388		-50	55435	58435	13	38454
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				-82	58485	58485	22	56:27
-	1522	3758		-38	38465 58465	58485	22	58427
	55C2	3788					23	5842B
	56 32	3552		-88	58485	584 8 5		
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•	6688	3558		-52	58485	58485	25	58438
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,	6688	3158		-90	58395	58395	31	58425
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	6628	3836		-148	58345	58345	\$3	58378
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•	1750	3668		~148	5B345	56345	34	56384
-	5388	3888		-1-8	58345	58345	48	58385
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	6868	6588	5822B			58228	1	58229
•	6668	6558	58231			58231	i	55232
	3688	6638	58174			58274	2	58276
	5866 68 66	6658	58237			58237	3	58240
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•	6686	- 986	SSIBB			5818B	6	58194
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•	6958	7200	58195			58:35	:2	5828;	
•	7888	7888	58283			58203	12	56215	
•	7858	7800	53193			58193	13	56286	
,	7138	7288	58173			58;7B	13	58191	
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•	293	6995	58135			58235	16	56251	
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	5567						10		
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•	528	5 52 5	58293			58233	27	53322	
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•	7522	6263	58238			58233	32		
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	7532	5658	58160				36 20		
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1	6368	3122		-22	58465	594\$5	1	58467	
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•	6338	3450		-92	58395	SB 395	8	58483	
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	•	6888	3698		-128				
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		6888	3860		-92	56295	58395	14	53429
	•	£32 6	3858		-168	58325	58325	15	56348
	•	6382	33 86		- 188	18361	58385	16	58481
		6828	3358		-92	58395	58395	17	58412
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	12/3/36	6636	4838		-62	58425	55425	:7	
	•	£828	4888		-178	58315	58315	18	5B333
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	•	7228	3758		-148	53345	58345	25	58376
	*	5387	3788		-162	58385	58305	26	59331
		7888	3654		-178	55315	58315	27	58342
	-					50315			
	-	7638	3688		-138	56385	58385	26	58033
		7992	3556		-172	28315	58315	29	58344
		7965	3566		-288	58265	58265	36	56315
		1228	3459		-248	56245	58245	33	58275
						58175	58175	31	58286
		7232	3468		-318	JU./J			
	•	7838	3351		-,52	56335	58335	32	58367
		7838	3382		-12	10465	58465	33	58468
	•	7868	3258		-88	1 58485	58485	34	58439
		7888	3248		3	53485	56485	35	5852
									58581
	•	782B	3150		-28	58465	58465	36	
	•	7888	3100		-58	56415	58425	37	58462
								20	58443
	•	7808	3056		-92	58485	58485	38	
	•	7808 7808	3858 3888		-83 -118 `	58405 58375	58485 58375	38 39	58414
	•								
	1 - 1714)(86	7808	3888		-118	58375	58375	39	58414
	- 1218186	7808 6958	3888 3888	******	-118 ×	58375 58375	58375 58375	39 48	58414 58415
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	12\8\86 :: !!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!</td <td>7888 6958 *******</td> <td>3888 3888 11111111 6888</td> <td>58287</td> <td>-118 ×</td> <td>58375 58375</td> <td>58375 58375 ************ 58267</td> <td>39 40 111111111</td> <td>58414 58415 1111111111111111111111111111</td>	7888 6958 *******	3888 3888 11111111 6888	58287	-118 ×	58375 58375	58375 58375 ************ 58267	39 40 111111111	58414 58415 1111111111111111111111111111
	**********************	7808 6954 ******* 7680 7600	3088 3088 \$\$\$\$\$\$ 6088 6050	58287 58197	-118 ×	58375 58375	58375 58375 ************ 58267 58197	39 48 ********** # -2	58414 58415 59287 59287 58195
	**********************	7888 6958 *******	3888 3888 11111111 6888	58287	-118 ×	58375 58375	58375 58375 +1+++++++++++ 58267 58197 58228	39 48 ********* # -2 -5	58414 58415 59207 58195 58283
	**********************	7808 6954 ******** 7680 7600 7608	3888 3888 ********* 6885 6850 6188	58287 58197 58288	-118 ×	58375 58375	58375 58375 +1+++++++++++ 58267 58197 58228	39 48 ********** # -2	58414 58415 59287 59287 58195
	**********************	7808 6958 ******** 7688 7698 7698 7598	3888 3888 5888 5885 6850 5198 5150	58287 58197 58288 58237	-118 ×	58375 58375	58375 58375 ************* 58267 58197 58228 58237	39 48 48 48 -2 -2 -5 -7	58414 58415 59207 58195 58283 58238
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	**********************	7808 6958 ********* 7688 7688 7688 7688 7688 768	3899 3899 ************ 6839 6850 6199 6199 6150 6290 6259	58287 58197 58288 58237 58239 58255	-118 ×	58375 58375	58375 58375 ************** 58287 58197 58228 58237 58239 58239 58265	39 48 ********************** # -2 -5 -7 -9 -11	58414 58415 59207 58195 58283 58238 58238 58238
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		7688	7038	58266			58266	-55	58211
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	-	7782	7889	58536			58544	-62	58482
	r	7752 782 8	7290 7308	56544 53564			56364	-64	58582
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	12, 31, 26	7680	7389	58564			56564	- 64	58582
		7922	£95 2	53246			58246	-66	13:80
		7668	6908	58237			56237	-GE	66169
		7302	885 2	58254			58154	-7	59183
		182B	1823	58222			55218	-75	58:47
	•	7368	6753	58222			58118	-75	39145
	•	7888	6728	58286			58286	-78	58128
	•	7862	\$657	S6245			58245	- 53	58165
	•	7886	6606	36232			56132	-31	5615#
	-	7888	6558	58222			56212	-64	58139
		7882	6588	58241			58241	- 67	58154
	:	7882	6458	58217			58217	-85	58128
		7823	6482	58223			56223	-31	56132
	•	7866	6358 6358	56226			56226	-34	58134
	-	. 346					38233	-96	58137
	-	7680	53 88	58233			20122	- 75	
		2636	825 8	58203			58283	-38	13125
	•	7388	6208	55283			56223	- 126	53123
	•	7838	6153	58191			58191	-193	58883
	-	7689	6188	58197			58:37	- 125	58892
		7888	6656	58222			58282	-187	58895
	•	7622	6888	56188			56196	-169	58879
	121,91,85	7632	6282	58188			53183	-183	58879
	12,3.00	7958	6888	58173			56173	-112	58861
	•	7932	6888	58:68			58168	-114	58854
		7358	6986	58163			58163	-116	58847
		6888	6382	58:67			58167	-119	\$6848
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	121/91/86	5860	6293	56167			58167	-115	58848
	-	3238	595 8	\$\$147			58147	-122	38825
	•	9623	5988	52197			58197	-125	56872
	*	3626	3358	52155			33155	-128	58827
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	,	64 80	2958		- 178	58315	58315	-2	56313
	•	6488	2988		-198	58295	58295	-4	58291
		6488	2858		-222	58285	58285	-6	58279
		6488	2886		-228	58265	58265	-8	58257
		6482	2759		-125	58355	58355	-18	58345
					-128	38365 58365	58365	-12	58353
	-	64 88	2788		-110	10404 50005	58335	-14	56321
		6428	2658		-158	58335	10220		58389
	-	5400	2688		-168	55015	53325	-16	
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	•	6182	25 8 0		- 93	\$8395	58395	-28	58375
	•	54 83	2458		-128	58355	S6355	-22	58023
		6483	2400		-138	55085	28365	-24	58361
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	•		2168		-198	56295	58295	-35	58268
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-					53145	58145	-73	53 8 72	
-	5522	2658		-340					
•	6£ 3 8	2728		-518	55175	5B175	-75	53166	
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:	6628	2382		-238	58055	58255	-73	58:76	
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	6688	2388		-348	58145	5B145	-83	58 8 62	
						58195	-85	58118	
•	6688	2958		-292	58195				
۵	6638	3882		-178	58315	58315	-37	56228	
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•	6888	2958		-248	58245	58245	-91	58154	
,		2303		-228	58265	58265	-93	58172	
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•	88 2 2	2825		-208	58285	58285	-95		
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•	6883	2763		-288	58285	58285	-121	58134	
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-				-328	53165	58165	-185	58850	
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			58275			58275	8	56279	
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	7952	7622	58296			58296	5	55331	
•	2626	7863	58263			58263	7	5629 8	
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•	8228	2683	58214			55214	47	58231	
•	8296	6758	58259			58259	19	58278	
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,	6358	6650	53243			58243	24	59267	
						55247	26	5B273	
_	532C	6688	50247						
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	3868	5588	58241			26241	3[58271	
*	2626	6450	58241			58241	34	58275	
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	*	3122	5223	56161			53165	72	58035
		3222	07 52	53227			58257	74	56311
		5222	5722	03173				77	56352
	•	3226	5652	56187			53227	79	58286
	•	5235	5233	50252			53151	62	58334
	•	3222	655B	58285			58205	84	58289
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	•	3282	6458	58221			53221	d i	58318
	•	\$132	8422	58221	-	•	53221	91	58312
		3122	\$352	58188			55283	34	58294
	•	82 8 2	6322	58283			56263	36	58233
		3222	6258	58:35			56195	33	58293
	•	3020	6283	36.38			SE198	121	58299
	•	32 88	6158	SE:76			55176	183	58275
		3225	6198	53167			58157	186	58273
	,	5528	5258	53183			55:83	163	58291
	•	8163	5662	58286			58288	118	58318
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	•	0158	6862	58287			58287	113	58320
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	•	9528	6865	5821B			58212	118	58336
	•	8838	6888	58221			58221	128	58341
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	•	6288	3888		- 288	58265	58265	9	53214
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		0040	3024		2,0			••	8
	:21:20:56	6886	3030		-278	58215	58215	18	58233
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	,	6888			~558	57935	57935	25	57968
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		6869	3233				58055	2 B	53685
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	•	6868	3402		-536	57955	57955	37	57532
	•	6292	3452		-618	57985	57885	25	57324
	•	6201	3223		- 532	57955	\$7955	42	57997
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	•	6666	3654		-528	57965	57965	49	58814
	•	5965	3762		-53 0	57953	57955	31	58226
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		6882	3866		-480			55	
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	-	6004	3980		- 32	53285	58285	60	58345 M(17
		6383	3958		-258	58235	58235	62	58297
	-					58345	53345	65	58418
	•	6888	4638		-:42	10347	19949	64	3
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	•	6288	1332		-288	58235	53285	74	58359
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		62 98	3950		-178	58015	58315	75	58391
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	•	6228	3488		-122 .	56225	58285	: 32	58387
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		6280	3368		-386	58185	56185	106	58291
	•				-338	58155	58155	189	58264
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	•	6206	3208		-320	58:65	58165	111	
	·	6288	315 2		-358	58135	58135	113	58248
	•	6208	3139		-388	58185	59185	115	58221
		6288	3858		-378	58115	58:15	118	58233
		6232	3883		-352	58135	58135	128	56255
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	1.111100						58152	-2	58158
		8258	7868	56152					
		93 88	7922	58195			53185	-3	58182
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	•	5428	7002	58158			58138	-7	5815:
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	12/11/85	2438	7062	58158			59158	-7	56151
	•	84 32	6958	58135			58135	-8	58127
	•	S422	5982	58162			55122	-12	53172
	•	8432	6550	58151			59151	-12	58139
							58147	-14	58133
	-	64 88	6888	58147					
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	•	8422	6658	58128			58128	-19	55181
	•	5488	6688	58129			56129	-28	\$8189
	3	8468	6554	56(24			58128	-22	58898
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		3482	65 88	58187			561 07		
	•	9408	6458	58119			56119	-25	38894
	•	3422	£436	58137			58137	-27	5811B
	•	8468	6358	58:04			56184	-25	58875
		8486	6308	58183			58183	-51	58872
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							5B111	-34	56877
		8490	82 28	58111					
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	•	8428	6144	58129			SB126	-37	58892
	•	8428	6850	58143			58143	-39	56184
	¥ .	342B	6888	58128			56128	-41	58887
	12\11\96	8488	6888	58128			58128	-41	58887
	•	635B	6888	58124			5B124	-42	588B2
		8396	6980	58074			58874	-44	58032
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	8288	5958	58:33		58139	-49	58839
•	52 88	5982	58129		58129	-51	52278
,	8280	5850	58152		\$9152	-53	56803
	8280	5888	58118		59118	-54	58064
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,	8528	7808	58285		58285	- 58	58147
•	8558	7888	58195		58195	-59	58136
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	3522	565 6	52143		56143	-73	56076
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	8628	6:32	\$3.11		58114	- 92	58819
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,				-118 58275	58275	-4	58271
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r	[32]	2453		-310 58175	53175	-15	58169
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	7889	2350		-306 58185	58185	-18	58167
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- V				-236 58285	58295	-21	58(64
· ·	7888	2258				-22	56133
	7888	1208		-332 58155	58155	-21	56141
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	-	1368	2662		-128	22682	58385	-31	58234	
	•	7558	2082		-180	55 38 5	56385	-93	56012	
	12111186	7358	3898		-:02	58585	56585	- 54	55134	
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	•	7158	3008		-72	56415	58415	-128	59315	
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	,	8428	3168	58125			58(25	4	58129	
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	•	8428	2368	58123			58123	11	55134	
	•	5248	3358	58122			38122	13	58135	
	•	5486	3488	58188			56168	15	55115	
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•	8498	3750	58148			58140	27	58167
•	8488	3868	58130			56136	23	58159
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	3420	33 98	58121			58121 52104	33 25	58154
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	0400	4852	58155			58155 58139	38 48	58195 58179
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•	8480 3:32	4158 4288	58148 58142			58140	44	58186
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٢	5488	4458	56;22			58122	53	58175
•	1100	4588	SB183			53153	55	58206
	6422	4502	10135			58161	57	58218
	5423	4632	56134			58134	59	58193
•	3400	4852	58143			58143	68	58283
•	5423	- 225	58143			58143	62	58265
•	8482	4758	52134	-		52134	64	58156
•	5566	628	58141			58141	66	58287
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	8238	5464	58829			56488	95	58183
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,	3232	5558	58896			56895	18)	58197
•	8289	5688	53899			58899	102	58291
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12\12\8		3866		-268	58225	16125	8	58225
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•	3567	29 82		-486	28285	58855	3	58886
•	7688	2859		118	59595	58595	4	58599
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		7608	2458	-352	58135	58135	14	53149 M(21)
				-348	58145	58145	15	58162
		7688	2488					
	•	7528	2350	-388	58123	58185	17	58122
	•	7628	2378	-330	50155	58155	13	58173
	•	7620	2258	- 378	53115	58115	19	58134
	-	7680	2288	- 35B	58135	55135	21	58156
	-	7528	2:32	-328	22:22	58165	22	58187
	-	7600	2128	-302	53185	58165	13	562 26
		75.32	2858	-34 Z	58:45	58145	15	55:72
		2823	2000	-272	58:15	58115	26	11.11
			2000	212				
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	44.16.166 *			-512	19165	58165	17	58:32
		7659	1828			58135		52:53
		7786	2082	-358	58135		28	
	•	7753	2885	-310	58165	58165	38	58195
	•	7321	5852	-368	58125	58125	31	58156
	11,11,28	2885	2888	- 368	55125	58125	31	53156
		601	2858	-368	\$8125	58125	32	58:57
		7388	2100	-358	58135	53135	34	58169
		1388	2:50	-368	58125	58125	35	53:52
					53425	53425	36	58461
	-	7522	2288	-68				50101
		7388	225B	-400	58685	58885	37	58(22
	•	7688	2338	-378 -	58:15	56115	39	58154
	-*	2825	2358	-368	58185	58185	43	58145
	ĸ	7888	2408	-366	56165	58185	41	58145
	•	7828	2458	-368	58125	56125	43	58168
	•	7528	2580	-360	58115	58125	44	58169
		7888	2550	-278	58215	58215	:5	58269
		7680	2693	-380	56185	58185	46	58231
						58825	49	58073
		7300	2650	-468	58825			
	ł	7838	2798	-398	58865	58835	49	58144
		7822	2758	-388	58185	56165	52	58155
	•	7828	2868	-228	55265	36265	50	56317
	x	7368	2858	-188	55385	56385	53	55353
	•	7680	2988	-386	58185	58;25	54	58159
	,	7808	2956	-408	58835	55985	55	58148
		7622	3696	-380	53105	58185	57	56162
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	12\12\86	7800	3888	-388	58:05	58185	57	58162
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		7856	3880	-380				
		7388	3868	-408	58885	S8885	59	58144
	•	795D	3002	-354	56135	58135	61	58196
	•	8888	3988	-338	59155	56155	62	58217
	12\12\86	8389	3040	-338	56155	58155	62	58217
	•	8888	2958	-328	\$8165	58:65	63	59223
	,	8888	2988	-398	56835	58095	65	58166
		3625	285B	-388	59185	58125	66	58171
								58172
	-	6288	2888	-368	58185	58185	£7	501/2
	·	3686	2758	-428	Sa682	58085	68	58153
	•	6986	2708	-348	58145	53145	70	59115
	•	3282	2658	-368	58125	58125	71	58136
		3033	2508	-388	56165	58185	72	56177
		8226	2550	-438	13855	68922	74	56:29
	-	8338	2538	55	53235	59265	75	55168
		3823	2458	-478	53211	58215	76	53891
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		8020	24 8 8	-428	56865	58865	77	56142
		8988	2350	-468	55625	58825	79	58184
	7	5626	2362	-498	57635	57995	86	58675
	,	9886	2258	-458	58835	58835	81	58115
- k.	•	8689	2288	-428	56865	58865	B\$	56146
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	3536	2032	-413	56865	58865	55	58:53	\sim
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12/12/186	8203	2882	-422	58265	56665	õõ.	58155	29
12112100	3252	2000	- 388	58185	S8185	89	18194	
		2388	-378	58115	58115	33	58285	
	8:31	2286	-358	58135	56135	92	58727	
	3152	-	- 202	58285	58285	35	58578	
•	8203	2038		30100				
		1377	-200	58285	58285	Ťŝ	55073	
12\12\86	32 62	2023	-368	55125	58:25	94	38219	
,	3023	2858	-278	55215	58215	95	58318	
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•	8122	2158	202			96 96	56293	
	3362	1088	-198	58195	5B195			
	8222	2256	-138	58385	58305	39	58404	
-	8133	2382	-282	58285	58285	161	56366	
-	6123	1352	-312	58:75	53(75	182	58277	
	8288	2488	-328	58165	56165	183	56265	
12\12\36	7362	3282	-362	58:85	56185	:84	56229	
12112.00	7750	3888	-538	58155	58155	126	3E26:	
	7720	3000	-378	\$8115	38:15	187	56222	
,		3822	-280	55265	58285	:08	58313	
	7658		-350	58135	58135	118	58245	
•	7685	3869						

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 $(1,1,2,\dots,n_{n-1}) \in \mathbb{R}^{n-1} \times \mathbb{R}^{n-1$

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