

37-~~212~~. 214-16018

GEOCHEMICAL, GEOPHYSICAL REPORT  
ON THE  
CARIBOO 1-4, MOST LIKELY 3 AND 4  
SHORT STUFF 2 AND 3, AND SUN MINERAL CLAIMS

CARIBOO MINING DIVISION  
NTS 93A/12E  
52°~~41'~~'N      121°~~44'~~'W  
41'      42.3'

FILMED

For

*Owner/Operator:* E&B EXPLORATIONS INC.  
1440 - 800 West Pender Street  
Vancouver, B.C.  
V6C 2V6

SUB-RECORDER  
RECEIVED  
MAY 1987  
REG # \_\_\_\_\_  
VANCOUVER B.C.

February 15, 1987

Ken McNaughton, M.A.Sc., P. Eng.  
Project Geologist

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

**16,018**

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## SUMMARY AND RECOMMENDATIONS

The Phase II, 1986 exploration program was successful in outlining several coincident targets which warrant drilling for their gold potential.

The Cariboo Property is located along the north bank of the Quesnel River, approximately 4.5 km northwest of Quesnel Forks, 70 km north of Williams Lake in the Cariboo Mining Division. The property consists of 109 claim units totalling 2082 hectares. Access is by helicopter or along a good horse trail from a cable ferry crossing at Quesnel Forks.

The property geology consists of volcanic-sedimentary rocks that have been intruded by a series of syenite to monzonite stocks. Gold and copper mineralization is associated with this intrusive activity. Dome's QR deposit, contains stratabound gold mineralization in a brecciated augite basalt. The disseminated gold is micron sized and associated with epidote/chlorite/pyrite replacement. Present reserves are reported as 1,100,000 tons grading 0.210 oz Au/ton. Dome is activity exploring the property.

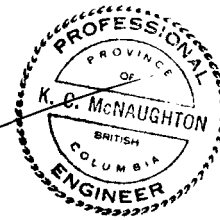
Six targets of coincident geochemical/geophysical anomalies have been identified. Three of the targets bear similarities to Dome's QR type gold mineralization. All six targets warrant further investigation.

A 10,000 foot reverse circulation rotary drill program is recommended to adequately test the targets. In addition, an I.P. survey is required to appraise two other coincident gold soil/magnetic anomalies.

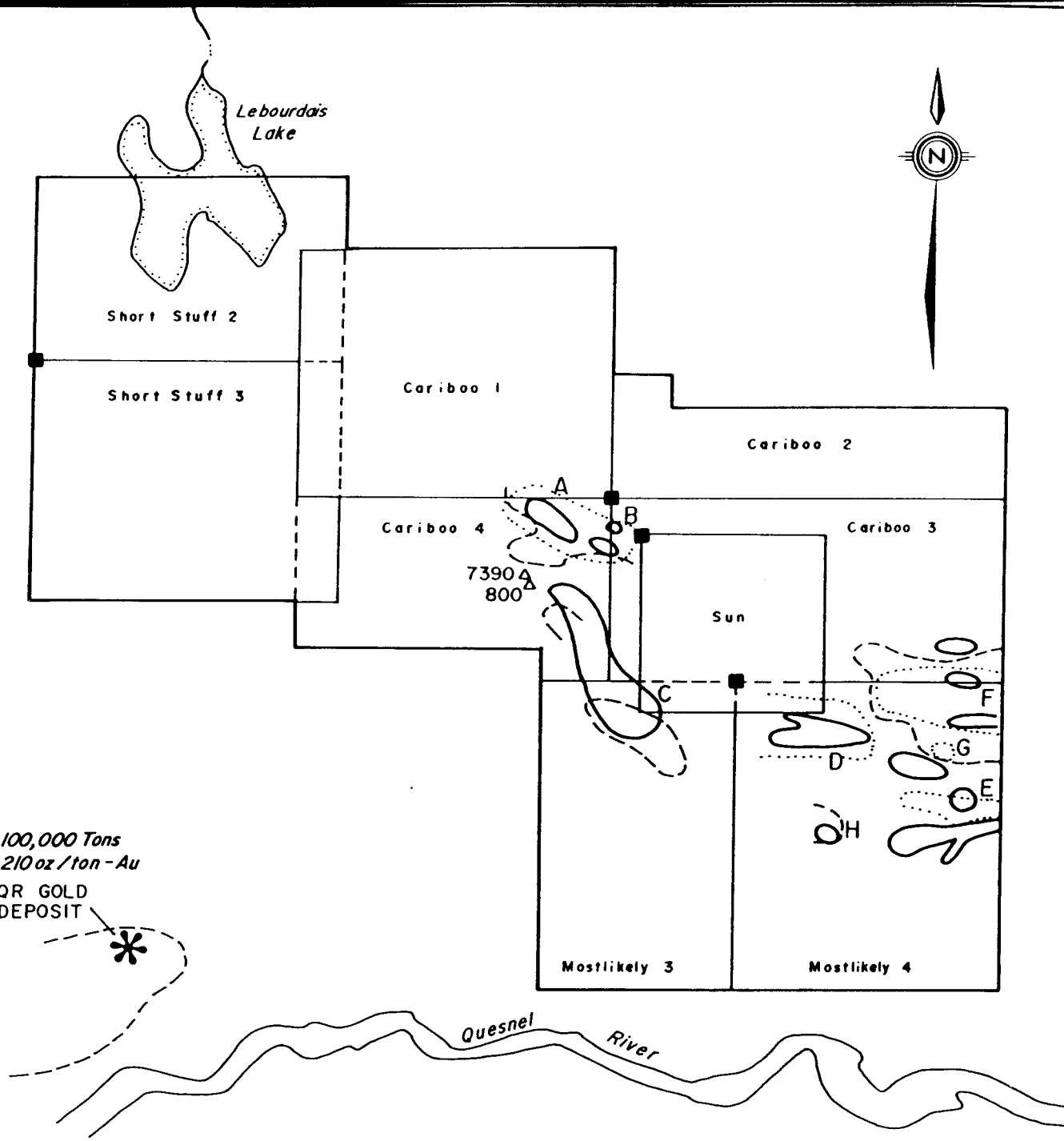
(ii)

The Phase III, 1987 exploration program is estimated to cost \$CDN 335,000 and will require three months to complete. Exploration activities are planned for early May, 1987. Contingent on the success of the above phase, a follow-up drill program will be undertaken. The anticipated program is to consist of 10,000 feet of diamond drilling and is estimated at a cost of \$CDN 690,000.

Respectfully submitted,



Ken McNaughton, P. Eng.  
Project Geologist



1,100,000 Tons  
0.210 oz/ton - Au  
OR GOLD  
DEPOSIT

LEGEND

- SIGNIFICANT SOIL ANOMALIES (Au, Ag, Cu)
- MAGNETIC HIGH
- ..... CHARGEABILITY HIGH
- B DRILL TARGETS
- Δ ROCK SAMPLE (ppb Au)

## 1.0 INTRODUCTION

The Cariboo property has been the subject of various exploration programs for six years. In that time, the property status has advanced from a single regional silt sample, to the present, pre-drilling phase.

The purpose of this program was to continue the soil sampling initiated in the spring program and geophysically study the existing grids. The aim was to develop significant targets which warranted a Phase III drill program.

High grade gold samples have been found on the property, but to date, only from narrow, restricted quartz veins. Barren QR deposit style of mineralization has been mapped on the property, and the potential remains high for such a zone to exist on the property which carries gold values.

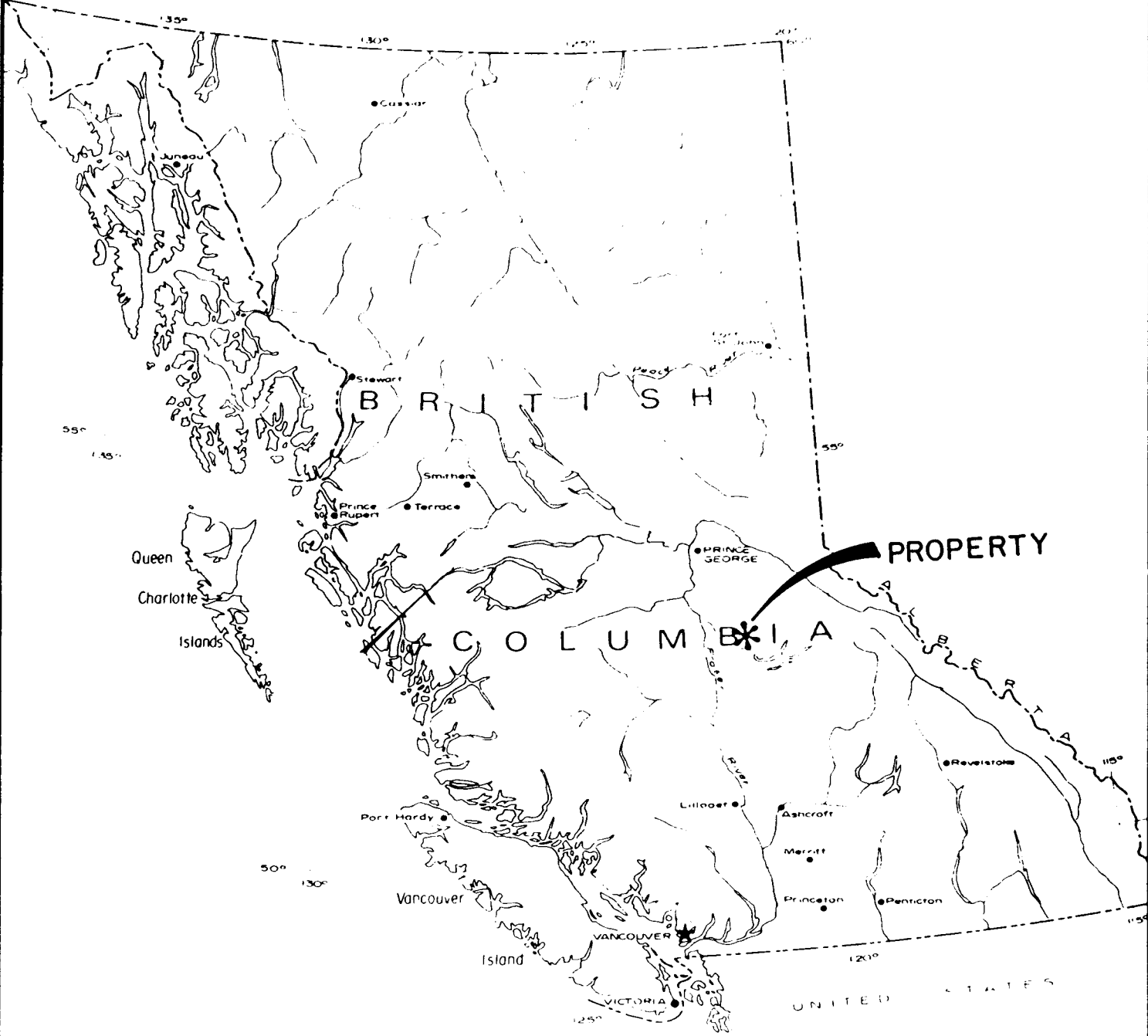
### 1.1 Location and Access

The claims are located along the north bank of the Quesnel River and are centered approximately 4 1/2 kilometers northwest of Quesnel Forks at 52°42' north latitude and 121°44' west longitude on NTS map sheet 93 A/12 (Figure 1).

Access to the property is by helicopter from either Quesnel, 35 kilometers to the northwest of Williams Lake, 70 kilometers to the south.

A logging road which accesses the western claims in the group runs 15 km before joining a good forestry road which terminates in Quesnel. A second forestry road is expected to be completed in the spring of 1987 and will end approximately 1 km northeast of the claim.

Access to the property can be made on foot along a good horse trail from the cable ferry crossing at Quesnel Forks.



# C A R I B O O P R O P E R T Y L O C A T I O N M A P

SCALE			
0	136 Mile		136 Mile
Mile : 136	0	136 Mile	136 Mile
Prepared by:	Date : Nov 1/73	NTS MAP AREA	DRAWING No. 1
Drawn by:	Revised:		

## 1.2 Claims and Ownership

The Cariboo Property consists of seven four post claims totalling 109 units. Title to the property is held by E&B Explorations Inc. of 1440-800 West Pender Street, Vancouver, B.C.

<u>Claim Name</u>	<u>Units</u>	<u>Record No.</u>	<u>Record Date</u>
Most Likely 3	20	3706(6)	24/06/81
Most Likely 4	20	3707(6)	24/06/81
Cariboo 1	20	3708(6)	24/06/81
Cariboo 2	12	3709(6)	24/06/81
Cariboo 3	18	3710(6)	24/06/81
Cariboo 4	15	3711(6)	24/06/81
Short Stuff 2	15	3712(6)	24/06/81
Short Stuff 3	20	3713(6)	24/06/81
Sun	9	7094(7)	19/07/85

## 1.3 Physiography

The property is characterized by rolling hills with moderate slopes and deeply incised stream valleys. Steep slopes and cliffs occur along the Quesnel River. Relief is approximately 2,200 feet about a mean elevation of 3,275 feet above sea level.

Vegetation consists primarily of lodgepole pine and spruce with stands of aspen, cottonwood and birch.

Outcrop on the property is sparse. Till thickness varies from a few feet to greater than 100 feet in scour channels. Ice movement during the last glacial episode was from the southeast to northwest.



#### 1.4 Geology

The property lies within the Quesnel Trough, a Mesozoic tectonic feature which lies between the Omineca Crystalline Belt to the east and the Cache Creek Group to the west (Bailey 1978).

The regional geology has been described by Bailey as "a sequence of Upper Triassic - Lower Jurassic volcanic and sedimentary rocks which have been intruded by comagmatic felsic plutons." The volcanic rocks comprise green-grey basalts which are analcite bearing towards the top of the sequence and grade upwards into maroon basalts of the same composition. The basaltic sequence is interbedded with thin units of siltstone and minor conglomerate and is overlain by a succession of felsic breccias which in turn are overlain by shallow water sedimentary rocks of Mid Jurassic age.

The volcanic-sedimentary pile is intruded by a series of syenite to monzonite stocks which are often related to copper or copper-gold mineralization.

In the vicinity of the Cariboo property, notable metal occurrences are E&B Explorations Inc.'s Cariboo-Bell copper porphyry south of Morehead Lake, and Dome Mines Ltd.'s QR gold deposit immediately southwest of the Cariboo claims.

Gold mineralization on the QR property is hosted by an augite basalt breccia unit peripheral to a diorite stock. The main gold zone on the QR is restricted to the augite basalt and as such is stratabound. Gold occurs as micron sized, disseminated free gold. Alteration associated with gold mineralization consists of moderate to intense epidote-chlorite replacement with several percent disseminated pyrite and minor chalcopyrite.

Geological mapping completed on the Cariboo property includes a sequence of pyroxene basalts and basalt breccias with subordinate siltstone horizons trending roughly S.E.-N.W. through the center of the property. The basalts are overlain by conglomerate to the south which in turn is overlain by siltstone. A diorite intrusive has been mapped in the northeast corner of the property.

Alteration similar to the QR property has been noted within the basaltic sequence on the Cariboo 4 claims along Le Bourdais Creek and a southwest flowing tributary to Maud Creek.

Along Le Bourdais Creek several narrow zones of variably silicified basalt with minor epidote-chlorite replacement are exposed. Pyrite is associated with the alteration as 2-10% disseminated blebs and rare veinlets.

Located near the center of the property is a mineralized quartz vein, 1-2 feet with subordinate veins and breccia zones.

### **1.5 Exploration History**

The property was staked in May 1981 to cover an arsenic anomaly detected on the west flowing tributary to Maud Creek by a Department of Energy, Mines and Petroleum Resources regional stream geochemistry program.

During the summer of 1982 reconnaissance scale mapping and soil geochemistry was completed along with soil geochemistry on a small grid placed in the south central portion of the claims. Localized, anomalous gold and arsenic values were returned from the sampling program prompting additional work in 1983.

Additional mapping and soil geochemistry was completed during the summer of 1983. Altered, pyritic basalt which locally returned anomalous gold and arsenic values from chip samples was identified in outcrop along Maud Creek and its southwest flowing tributary. Spotty anomalous gold values were also returned from the soil sampling program.

In June of 1984 an airborne geophysical survey consisting of magnetometer and two frequency VLF-EM surveys were completed over the property. A total of 370 line kilometers was flown covering an area of approximately 9,000 hectares. Flight line spacing was 250 meters.

The airborne survey detected two small areas of high magnetics and three weak VLF conductors on the property.

During 1985 an IP survey totalling 10.9 km was run over the area of pyritic basalts near Maud Creek. A geochemical grid was also established on the east central portion of the claims to cover one of the mag highs and two of the VLF-EM anomalies detected by the 1984 airborne survey.

The IP survey located three distinct chargeability anomalies. Soil sampling on the east grid returned several widely spaced gold anomalies with values to a maximum of 525 ppb. Additional mapping and rock sampling was also completed on the two grids at this time.

During the spring of 1986, detailed soil surveys were run over both the IP grid in the west and the soils grid in the east. Anomalous copper, silver and gold values were returned from both grids.

## 2.0 1986 EXPLORATION PROGRAM

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Field work for the Phase II program was conducted between July 24 and August 26.

Additional soil survey lines were laid out to expand both the east and west grids and fill-in areas over poorly defined anomalies. Reconnaissance soil surveys and prospecting were carried out to develop new exploration targets on the property.

Ground geophysical surveys, including VLF-EM and total field magnetics, were run over the existing grid lines and selected new lines. The east grid was further evaluated by an IP survey.

### 2.1 Geochemistry

Grid lines were flagged in using hip chain and compass, with 25 m station.

At each station, a mattock was used to collect a B-horizon soil sample. Samples were stored in kraft bags and sent to Acme Analytical Lab in Vancouver for a gold analysis as well as a 30 element ICP analysis. A total of 31 km of new line was set out, from which 1375 soils were collected.

Significant anomalies were detected in five areas in addition to numerous single sample or single line anomalies. The anomalies have been labelled A through E on Figures 3 to 5, with a brief description of each as follows:

- A - 600 m long, centered around 13+50N, 13+00E
  - strong Cu, Ag anomaly with Au locally coincident at the up ice end
  - mineralized quartz vein with up to 7390 ppb Au and breccia 400 m to the south

- B - 300 m long, centered around 12+00N, 21+50E
  - Au in soils up to 710 ppb Au
  - 400 m up ice from sol anomaly A
  
- C - 1700 m long, centered around 7+00N, 23+75E
  - strong Cu anomaly with locally coincident Ag, Au
  
- D - 600 m long, centered around 10+00N, 51+00E
  - coincident Au, Ag, Cu anomalies
  - follow topographic low down slope
  
- E - 600 m long, centered around 3+25N, 58+00E
  - narrow Au anomaly with values up to 745 ppb Au
  - locally coincident Ag, Cu anomaly

Three reconnaissance soil lines were run; 3+00W, 4+00W, being 300 and 600 m west respectively of the west grid and the third starting 800 m north of the east grid (Figure 6). Two samples on line 4+00W averaged 250 ppb Au. This was the only multiple sample gold anomaly detected in this portion of the program.

A broad silver anomaly was identified north of the east grid. (Figure 6).

Silt samples were collected from two creeks in the north half of the property. No anomalous values were detected in either of the creeks.

Prospecting uncovered another mineralized quartz-ankerite structure, between two known occurrences, in the area around 9+00N, 17+00E. Two samples, KR-86-093, 094 ran 1920 and 500 ppb Au respectively. Both are from 2 to 4 inch thick quartz veins. Sample, KR-86-095 ran 90 ppb Au, is from a 5 foot wide ankerite alteration zone which lies in the same locality as 093, 094 (Figure 6).

Anomalous gold values were not detected in any of the other rocks sampled.

## 2.2 Geophysics

VLF-EM and total field magnetic surveys were run over 38.4 km of existing grid. Three new lines, (27+50E, 30+00E, 32+50E) totalling 2.875 km, were covered by the magnetic survey. Readings were taken at every station. A compilation of the interpretation is shown on Figure 7, with the complete report in Appendix I.

### 2.2.1 East Grid

VLF-EM profiles indicate low to medium conductance for east-west trending conductors. The anomalies are irregular and discontinuous which implies a source in overburden or as short conductive structural features. An apparent offset in the conductors may be caused by a sub-parallel fault zone between lines 54+00E and 56+00E.

The entire grid is underlain by high background magnetic values. Intense magnetic highs are located in the northeast and southwest corners of the grid. The anomalies have been labelled F and G respectively on Figure 7. A sudden break in magnetic contours is evidence supporting the fault along line 54+00E.

Apparent chargeabilities values east of line 54+00E are believed to outline significant sulphide mineralization. Two peaks were located across lines 56+00E to 60+00E, the primary between 10+00N and 15+50N, the secondary from 3+00N to 7+50N. Both anomalies are situated at shallow to medium depths.

The primary zone correlates with higher magnetism and lower resistivities suggesting a presence of pyrrhotite and magnetite in an altered or weathered rock. The secondary zone correlates with non-anomalous magnetism and higher resistivities which could reflect non-magnetic sulphides within a silicified rock.

Chargeabilities west of line 54+00E are weak reflecting local increases in the amount of disseminated sulphides. Deep seated anomalies were detected on most of the lines at the lower detection limit of the survey. A horst and graben structure with the fault at line 54+00E is one interpretation to explain the data.

#### 2.2.2 West Grid

VLF-EM data showed a number of discontinuous, low conductance anomalies which are characteristic of those caused by an overburden response.

Magnetic results show an intense magnetic high and four secondary peaks on the grid. The intense high and one secondary peak are located between 10+00N and 15+00N on lines 12+50E, 15+00E and 17+50E.

Data from the 1985 IP survey was re-interpreted for correlation with the magnetic and VLF surveys.

The intense magnetic high and secondary peak occur in the vicinity of a significant apparent chargeability high. Much of the chargeability high falls within a zone of higher magnetism. Only the eastern extremity of the chargeability high is associated with higher resistivities. The remainder of the zone is flanking a more resistive region.

The resistivity highs correlate with intense magnetism implying magnetite mineralization. Interpretation suggests pyrrhotite and pyrite mineralization in an altered contact zone, as the cause of the anomaly on the whole.

A strong magnetic high was located between 3+00N and 5+00N on lines 27+50E to 32+50E. The anomaly increases in intensity to the east, however, the large line separation makes further interpretation tenuous.

### 2.3 Petrographic Studies

Petrographic studies were done on 15 rocks from around the property.

In summary, a diorite stock, thought to cover most of the north half of the property is in fact altered andesites. The area has been intruded by diorites and pyroxene rich gabbros with restricted areal extent.

As noted in the field, epidote and chlorite are the dominant alteration product. Accessory minerals include sphene, rutile and pyrite.

Whole rock analysis was performed on ten of the rocks. The results of this analysis are inconclusive.



### 3.0 CONCLUSIONS

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A compilation of data from Phase I and II of the 1986 exploration program identified six targets as having anomalous soil geochemistry associated with IP chargeability and magnetic highs. The targets are based solely on these surveys as the outcrop density is extremely sparse on the property.

The targets are listed in order of priority as follows:

<u>Target</u>	<u>Location</u>	<u>Description</u>
B	West grid	<ul style="list-style-type: none"><li>- strong gold in soils up to 710 ppb Au</li><li>- extrapolation of geophysical data yields coincident magnetic and chargeability highs</li></ul>
A	West grid	<ul style="list-style-type: none"><li>- coincident Cu, Ag, Au (up to 630 ppb) soil anomaly overlying magnetic high and intense chargeability high</li><li>- narrow quartz vein with up to 7390 ppb Au, 400 m south</li></ul>
E	East grid	<ul style="list-style-type: none"><li>- strong chargeability high peripheral to magnetic high</li><li>- strong soil anomaly immediately downslope, up to 745 ppb Au</li></ul>
H	East grid	<ul style="list-style-type: none"><li>- chargeability high on south flank of magnetic high</li><li>- coincident soil anomaly, up to 270 ppb Au</li></ul>
F	East grid	<ul style="list-style-type: none"><li>- intense chargeability and magnetic high</li><li>- locally coincident and geochemistry, up to 70 ppb Au</li></ul>
D	East Grid	<ul style="list-style-type: none"><li>- strong coincident soil anomaly, up to 525 ppb Au</li><li>- deep seated chargeability high</li></ul>

In addition to the above targets the two anomalies listed below require an IP survey before drilling can be recommended.

- |   |           |  |
|---|-----------|--|
| C | West Grid | - intense magnetic high underlies the up ice end of a strong copper anomaly (up to 1220 ppm Cu) with locally coincident Ag (up to 2.4 ppm Ag)                        |
| G | East Grid | - intense magnetic high underlies a restricted soil anomaly, up to 210 ppb Au<br>- shallow chargeability high detected 100 m east at the western limit of the survey |

A single sample, gold soil anomaly overlies an intense magnetic high at 16+25E, 10+25N. The soils are thin in this area, therefore the anomaly could be adequately explained by trenching.

Dome Mines Ltd. QR deposit lies 4.5 km southwest of the Cariboo property. Gold mineralization on the QR property is stratabound between silty sediments, within an augite basalt. Disseminated free gold is micron sized and associated with moderate-intense epidote/chlorite replacement with several percent disseminated pyrite and minor chalcopyrite.

Alteration similar to that observed on the QR deposit was found at the western end of the west grid. The alteration zone was mineralized with 5 to 7% pyrite but no substantial gold values. The presence of the zone demonstrates that QR deposit style of mineralization does exist on the property however poor bedrock exposure has prevented its discovery elsewhere.

Interpretation of the geophysical data on the Cariboo property, indicates that anomalies A, B, and H are similar to a QR deposit style of mineralization. The proximity of the anomalies to the QR and similarity of the geophysical characteristics implies a high probability for finding economic reserves on the Cariboo property.

#### 4.0 RECOMMENDATIONS

Drilling is warranted of six coincident geochemist-geophysical anomalies, of which, targets A, B and H have geochemical and geophysical properties similar to the QR deposit. A 10,000 foot, reverse circulation percussion drill program is required to adequately test the targets.

Anomalies C and G will require favourable results from an IP survey before drilling can be recommended.

A recently constructed forestry road ends 1 km east of the claims. A road onto the property, totalling 12 km, should be constructed and would greatly improve the access of the property as well as reduce the cost of future programs.

The Phase II geophysical/drill program requires a budget of \$CDN 310,000, which is outlined as follows:

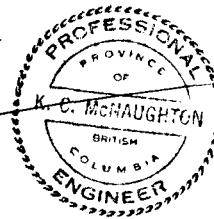
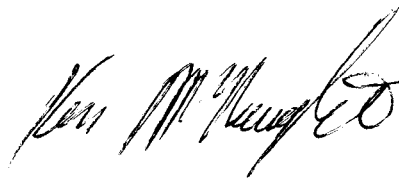
Analytical - 2000 rotary samples @ \$15.00	\$ 30,000
Drilling - 10,000 feet @ \$15.00	150,000
Drill Site Preparation and Construction	35,000
Drafting and Printing	5,000
Field Supplies	2,500
Geophysics - 10 km IP @ \$2000	20,000
Room and Board - 170 man days @ \$60.00 per day	10,200
Salaries - 1 geologist 70 days @ \$250.00	17,500
- 2 field assistants 50 days @ \$300.00	15,000
Shipping	1,000
Vehicle Rental and Operation	5,000
	<hr/>
Subtotal	291,200
Management Fee @ 15%	43,680
	<hr/>
TOTAL	\$334,880
SAY	\$335,000

Contingent on the success of Phase III, a follow-up drill program is anticipated, at a total cost of \$CDN 690,000.

Diamond Drilling - 10,000 ft. @ \$50.00	\$500,000
Drill Site Preparation, Road Upgrading	30,000
Personnel, 1 geologist, 2 field assistants	40,000
Field Supplies	5,000
Field Transportation	7,000
Management Fee @ 15%	90,000
	<hr/>
TOTAL	690,000

Work should begin in May of 1987 to allow sufficient time to undertake both programs.

Respectively submitted,



Ken McNaughton, P. Eng.

## LIST OF PERSONNEL

Ken McNaughton - Project Geologist  
July 22 to August 29 37 days  
1987 February 3 to February 12 10 days

Bob Bogusz - Field Assistant  
July 24 to August 9 17 days  
August 23 to August 29 7 days

Lorne Wilkinson - Field Assistant  
July 24 to August 9 17 days

### Interpretex Resources

Ed Rockel - Consulting Geophysicist  
July 25, 26 2 days  
August 12 - August 23 12 days

Tom Matich - Geophysicist  
July 25 - August 6 13 days

#### - Geophysical Technicians

John Martin - July 26 - August 6 13 days  
- August 12 - August 23 17 days

Grant McPherson  
Doug Sedgwick  
Terry Plant

All August 12 - August 23 17 days

### Renegade Exploration Services

#### - Linecutters

Andre Jette  
Craig Ellis  
John Cleaver  
Duan Theissan

All August 7 to August 9 3 days

**STATEMENT OF EXPENDITURES**

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Analytical	1375 soils @ \$11.00	\$15,125
	26 rocks @ \$14.00	364
Drafting and Printing		950
Geophysical Surveys		
	VLF & Mag 13 days @ \$ 550	6,825
	IP 17 days @ \$1,400	23,800
Linecutting	11.5 km @ \$243	2,790
Mascot Salaries	1 Geologist - 47 days @ \$140	6,580
	Field Assistants - 47 days @ \$100	4,700
Meals	198 man days @ \$15.50	3,069
Petrographic Studies	- 15 samples @ \$15.00	225
Shipping		147
Vehicle - Rental	- 1 month @ \$963	963
	- Operation	439
		<hr/>
	<b>TOTAL</b>	<b>\$65,977</b>
		<hr/> <hr/>

## STATEMENT OF QUALIFICATIONS

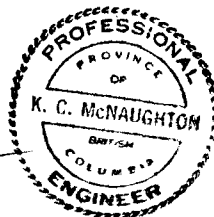
I, Ken McNaughton, of 265 Riverside Drive, North Vancouver, B.C. V7H 1V1 state that:

- 1) I am a 1981 graduate of the University of Windsor, Windsor, Ontario, with a B.A.Sc. Degree in Geological Engineering.
- 2) I am a 1983 graduate of the University of Windsor, Windsor, Ontario with a M.A.Sc. Degree in Geological Engineering.
- 3) I am a Professional Engineer, registered in the Province of British Columbia.
- 4) I have been employed in the mining industry prior to my graduation and that I have practiced my profession since April, 1983 as follows:  

1984 - 1987	Mascot Gold Mines Limited Vancouver, B.C.
1984	Borealis Exploration Ltd. Calgary, Alberta
1983	538162 Ontario Ltd. London, Ontario
- 5) I am presently employed as a Project Geologist with E&B Explorations Inc., 1440 - 800 West Pender Street, Vancouver, B.C. V6C 2V6.
- 6) That I am the author of this report which is based on public and property reports plus on site investigation.
- 7) That I was on site during the period from July 24 to August 29, 1986 to supervise ground geophysical and geochemical surveys which provide the basis for this report.
- 8) That I have no interest, direct or indirect, in the property discussed in this report or in the securities of E&B Explorations Inc. nor do I expect to receive any.
- 9) That this report may be used for the development of the property, provided that no portion may be used out of context in such a manner as to convey meanings different from that set out in the whole.
- 10) Consent is hereby given to E&B Explorations Inc. to reproduce this report or any part of it for the purposes of development of the property, or facts relating to the raising of funds by way of a prospectus and/or statement of material facts.

SIGNED AT VANCOUVER, BRITISH COLUMBIA  
THIS 15<sup>TH</sup> DAY OF FEBRUARY, 1987.

  
KEN McNAUGHTON, M.A.Sc., P. Eng.



**APPENDIX 1**

**GEOPHYSICAL REPORT**

**BY**

**ED ROCKEL**

**OF**

**INTERPRETEX RESOURCES**



CARIBOO GEOPHYSICAL INTERPRETATION  
OF  
VLF EM, MAGNETIC AND INDUCED POLARIZATION SURVEYS

1. SURVEY SPECIFICATIONS

1.1 Survey Parameters

- survey line separation - east grid - 100 and 200 meters
  - west grid - 125 meters for normal
  - as shown for fill-in
  - 250 meters for "extra"
- survey station spacing - 25 meters for VLF EM and magnetic survey in east grid
  - 50 meters for VLF EM and magnetic normal survey in west grid
  - 25 meters for VLF EM and magnetic fill-in survey in west grid
  - 25 meters for extra magnetic survey near west grid
  - 50 meters for induced polarization survey in east grid
  - 75 meters for 1985 induced polarization survey in west grid (by Walcott - see reference 5.)
- horizontal control - lines were surveyed by compass and hip chain with estimated slope corrections
  - semi-recoverable stations were located using felt pen markings on flagging tied to vegetation
  - grids tied in to base line 0+00N and to lakes
- baseline direction - east grid - east-west
  - west grid - Az. 300 degrees (N-60-W)
- survey lines were perpendicular to the base line
- readings from Cutler VLF transmitter were recorded on all lines
- induced polarization and resistivity survey was carried out in the east grid on lines 4600E, 4800E, 5000E, 5200E, 5400E, 5600E, 5800E & 6000E
- induced polarization and resistivity survey was carried out in the west grid during June, 1985 by Peter E. Walcott & Associates Limited on lines 250W, 00, 250E, 500E, 750E, 1000E, 1250E, 1500E and 1750E (data from line 250W was off the present grid and was therefore not used)
- survey totals:
  - East Grid
 

Induced Polarization	Magnetic	VLF EM
11.750 km.	13.550 km.	13.550 km.
  - West Grid
 

Induced Polarization	Magnetic	VLF EM
(by Walcott - see reference 5.)	27.725 km.	24.850 km.

1.2 Equipment Parameters

VLF Electromagnetic Survey

- Geonics EM-16 used for all survey
- transmitting station - Cutler, Maine
- in-phase (dip angle) and out-of-phase (quadrature) components measured in percent at each station
- direction faced: northerly

Total Field Magnetic Survey

- measured total magnetic field in gammas using EG & G G-816 proton precession magnetometer
- magnetic variations controlled by EG & G G-856 automatic magnetic base station recording every 30 seconds
- instrument accuracy +/- 1 gamma
- station repeatability better than +/- 3 gammas

Induced Polarization Survey

- Hunttec Mk II 7.5 kilowatt transmitter
- Hunttec Mk IV time domain receiver
- Interpretex Resources Ltd. 7.5 Kw. helicopter portable engine alternator system
- apparent chargeability measured in milliseconds
- primary voltage measured in millivolts
- apparent resistivity determined in ohm-meters
- dipole spacing a = 50 meters, n = 1 to 6
- pole-dipole method with pole southerly and dipole northerly

1.3 Equipment Specifications

- see appendix

2. DATA

2.1 Calculations

VLF Electromagnetic Survey

Fraser Filter values (after Fraser, 1969, reference 1.) were calculated for in-phase readings for all lines in the area.

Induced Polarization Survey

Apparent resistivity values were calculated using the formula;

$$Pa = 2n(n + 1)PI*a*(V/i)$$

- where: n = "n" value of 1 to 6
- PI = 3.14
- a = electrode separation (meters)
- V = observed voltage (millivolts)
- i = observed current (amps)
- \* = "multiplied by"

Metal Factor values were computed using the formula;

$$MF = (Ma/Pa)*1000$$

- where: Ma = apparent chargeability
- Pa = apparent resistivity
- \* = "multiplied by"

### Total Field Magnetic Survey

Total field magnetic readings were individually corrected for variations in the earth's magnetic field using magnetic base station values recorded at the same time. The effects of changes in magnetic content of operator's clothing or different batteries used in the magnetometer were controlled by re-occupying operator field base stations at the beginning and end of each day during the survey. An "operator adjust" correction was then applied where applicable.

### 2.2 Presentation

- VLF EM Fraser Filter values are presented as computer contours at a scale of approximately 1:7500 in the report and enlarged to 1:5000 in a map pocket
- total field magnetic values are presented as computer contours at a scale of approximately 1:7500 in the report and enlarged to 1:5000 in a map pocket
- apparent chargeability Fraser Filter values and apparent resistivity Fraser Filter values are presented as computer contours at a scale of approximately 1:7500 in the report and enlarged to 1:5000 in a map pocket
- apparent chargeability Fraser Filter values and magnetic readings are presented in the form of 3D plots for visual aids
- magnetic values for extra lines 2750E, 3000E and 3250E are presented in the report as contours at a scale of approximately 1:5000 and as computer profile plots for visual aids
- VLF EM in-phase readings plus calculated Fraser Filter values are presented in an appendix of this report in the form of tables showing values located with respect to line number and station number
- magnetic field and base station values are presented in the form of tables on "Total Field Magnetic Data Corrections Worksheets" in an appendix of this report
- IP data and calculated values are presented in an appendix of this report as "Induced Polarization Data Calculation Worksheets"
- IP data are presented as contoured pseudosections on pseudosection maps at a scale of 1:2500 (east grid only)
- IP anomalies are presented on the pseudosection maps and Geophysical Interpretation Maps as rectangles
- a geophysical interpretation is presented on grid plan maps as "Geophysical Interpretation Maps", for the east and west grids, at a scale of 1:5000
- VLF EM in-phase and out-of-phase readings are presented in profile form on grid plan maps at a scale of 1:5000.

### 3. INTERPRETATION

#### 3.1 Discussion of Results

On this project topography was mainly flat to moderate in slope thus little topographic effect was evident in VLF EM data. Both the filtered values and VLF EM profiles were used in this report to interpret the VLF EM data on all lines. Character matching and contours provided the means for continuing conductive trends. Overburden was not considered a problem in this region because of the shallow depth as evidenced by the prevalence of float boulders and some outcrop.

Magnetic data generally showed moderate magnetic variations in most of the two grid areas. Station to station variations were often of the order of 20 to 50 gammas or more and in some cases of the order of 200 gammas or more. Total field values ranged from around 56,600 gammas to over 59,000 gammas in magnetically active areas.

Extra magnetic survey (without VLF EM survey) was carried out on three lines (2750E, 3000E and 3250E) 750 meters east of the west grid. Values of these data fall within the range indicated above.

##### 3.1.1 East Grid

Induced polarization data in the east grid were noise free except in minor cases where poor contact reduced signal to noise ratio and required extra time and repeated readings in order to obtain reliable values. Chargeability readings ranged from less than 10 milliseconds to greater than 65 milliseconds with a general background in the area appearing to be between 10 and 20 milliseconds. Although values within the range of 15 to 20 may be construed as anomalous and may constitute background sulphide mineralization within bedrock, anomalous threshold has been set at 20 milliseconds with additional thresholds at 10 millisecond intervals in order to properly outline higher apparent chargeability levels within this anomalous area.

Apparent resistivity values ranged from under 300 ohm-meters to over 2,700 ohm-meters. Topographic influence was not readily apparent in resistivity data in this region.

Little use was made of metal factor values in the present interpretation because of the obvious relationship between apparent chargeability anomalies and apparent resistivity values. Metal factor calculations are designed to enhance the inverse relationship between apparent chargeability and apparent resistivity. In this case both the inverse and direct relationships were important.

##### 3.1.2 West Grid

Induced polarization and resistivity data analyzed in the west grid were obtained by Peter Walcott & Associates Limited in June, 1985 (Ref. #5.). The Walcott time domain IP survey was carried out using an electrode spacing of  $a = 75$  meters with  $n = 1$  and  $2$ . Apparent chargeability and apparent resistivity values for  $n = 1$  and  $n = 2$  were taken from contour maps, produced by Walcott, then Fraser Filtered and computer contoured in order to approximate the data sets and maps in the east grid.

Apparent chargeability readings varied from less than 4 to greater than 50 milliseconds. Background readings here were less than 10 milliseconds, in contrast with background values between 10 and 20 milliseconds in the east grid. The lower values can partly be attributed to the larger electrode spacing resulting in more averaging in the west grid. The anomaly threshold here has been placed at a different level than the east grid, for the same reasons. A threshold of 10 milliseconds and increments of 10 milliseconds were used in order to show various levels of anomalous apparent chargeability readings within the west grid. Apparent resistivity values ranged from less than 100 to more than 1000 ohm-meters. No topographic effect is believed to be present.

### 3.2 Conclusions

#### 3.2.1 East Grid

Geophysical surveys have delineated an area which is believed to contain anomalous amounts of disseminated sulphides. VLF EM Fraser Filter contours show east west trending conductors throughout the grid area. VLF EM profiles indicate low to medium conductance and in most cases anomaly profile character is not consistent from line to line. This suggests that the cause of conductivity is irregular and discontinuous, possibly due to overburden or short conductive structural features. An apparent offset of VLF EM Fraser Filter contour trends may reflect a fault zone sub-parallel to survey lines between line 5400E and 5600E. Support for some type of change in this region can also be found in magnetic and IP data. Magnetic contours seem to suggest a lineation, possibly caused by a fault, in the vicinity of line 5400E. Apparent resistivity contours show a slight resistivity low on line 5400E between two highs on adjacent lines. A weathered fault or contact could account for these lower apparent resistivity values. Apparent chargeability contours indicate that line 5400E represents an approximate boundary between more highly anomalous apparent chargeability readings to the east and less anomalous readings to the west. This would seem to support some sort of boundary condition, such as a fault or contact, in the vicinity of line 5400E.

Apparent chargeability values on parts of line 5400E, much of line 5600E, most of line 5800E and all of line 6000E are believed to outline significant amounts of disseminated sulphide mineralization. The highest values are seen on lines 5600E, 5800E and 6000E between approximately 1000N and 1550N. A secondary peak is evident on the same lines between approximately 300N and 750N. Both magnetic and apparent resistivity data seem to indicate that the two apparent chargeability peaks ("primary" from 1000N to 1550N and "secondary" from 300N to 750N) represent different types of mineralized targets. The primary zone correlates with higher magnetism and lower resistivities whereas the secondary zone correlates with background (non-anomalous) magnetism and higher resistivities. The conclusions would seem to be that the primary zone may represent disseminated sulphides containing appreciable amounts of magnetic pyrrhotite, possibly also with magnetite, and perhaps

altered or weathered, whereas the secondary zone could reflect non-magnetic sulphides, containing no magnetite, within rock which is harder, perhaps silicified.

Other weaker apparent chargeability anomalies seen on lines 5400E through 4600E probably reflect local increases in the amount of background disseminated sulphide mineralization. Much of the higher than background mineralization appears to be deep. The possibility exists, if the fault postulated above is real, that these deep, above background anomalies may reflect the top of more intensely mineralized occurrences that have been faulted down to nearly the detection limit of the IP survey employing electrode separations outlined above in section 1.2. Thus the background apparent chargeability values may represent a halo around more intense mineralization which is more deeply buried west of the interpreted fault.

### 3.2.2 West Grid

VLF EM data showed a number of short conductive features trending west to northwest. Profile character is not consistent from line to line in most cases suggesting an irregular causative body. VLF EM profiles also indicate moderate to low conductance throughout the west grid area. An obvious conclusion would be that the VLF EM anomalies are caused by conductive overburden.

Magnetic results show one "intense" (of the order of 1000 gammas) magnetic high anomaly and three secondary peaks within the west grid area. The intense anomaly and a nearby secondary peak occur in the vicinity of a significant apparent chargeability anomalous zone near the northeast ends of lines 1250E, 1500E and 1750E. The secondary magnetic peak nearly coincides with the apparent chargeability anomaly peak and much of the apparent chargeability anomalous zone falls within a zone of higher magnetism, suggesting that some chargeable material may be due to magnetic pyrrhotite. The intense magnetic anomaly seems to coincide with a zone of higher apparent resistivity, possibly indicating magnetite as the cause.

Apparent resistivity data indicate that only the eastern extremity of the apparent chargeability anomaly is associated with slightly higher resistivity values, whereas the majority of the chargeable zone corresponds with the flank of the more resistive region which drops off to lower resistivities. A possible conclusion is that the anomalous chargeability may be related to a mineralized zone near or in an altered contact.

A secondary apparent chargeability anomalous zone occurs near the south western ends of lines 750E, 1000E and 1250E. This weaker zone correlates with a slight resistivity high trending roughly northwest. This feature could be due to chargeable material such as sulphides in a silicified zone.

Extra magnetic survey carried out 750 meters to the east of the west grid show two magnetic high anomalies. A large line separation of 250 meters limits the validity and accuracy of line to line correlation of anomalies however data seems to suggest a trend roughly northwest. The larger high, between 300N and 500N, increases in amplitude towards the east and, as indicated by profile character, is near surface on line 3250E. Also, if the trend is valid across the wide separation between lines, the magnetic causative body seems to plunge westward.

#### 4. RECOMMENDATIONS

##### 4.1 East Grid

The apparent chargeability anomalous zones referred to as "primary" and "secondary" are both worthy of follow up exploration and constitute drill targets based on present information. Priorities for drilling the the zones should depend on the geologic model applied to this region, to geologic knowledge of the area and geochemical information from within the two anomalous zones.

An induced polarization survey, using electrode parameters providing maximum depth penetration, is recommended in the region of the east grid, (west of line 5400E) containing deeper "higher background" apparent chargeability values, in order to test the hypothesis that significant chargeable material may occur at depth. The deep IP survey should be carried out before drilling is considered in this region, unless other significant information can be used to produce a drill target.

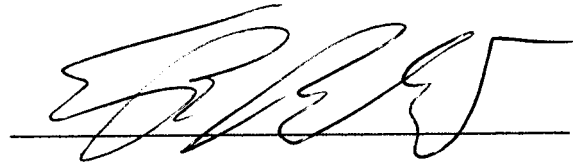
##### 4.2 West Grid

The induced polarization data gathered by Walcott in 1985 within the west grid is sufficient for the determination of drill targets. Although geochemical data should be used to support drill location, the IP results suggest that the highest apparent chargeability peaks should be tested first. Some attempt should be made to substantiate the cause of the intense magnetic anomaly near the anomalous IP zone and any possible relationship to mineralization. The secondary peak to the southwest should have geochemical and/or geological support before drilling is initiated.

Respectfully Submitted

INTERPRETEX RESOURCES LTD.

Vancouver, British Columbia

A handwritten signature in black ink, appearing to read 'E.R. ROCKEL', is written over a horizontal line. The signature is stylized and cursive.

E.R. ROCKEL

Consulting Geophysicist



CERTIFICATE

I, Edwin Ross Rockel, Geophysicist of Vancouver, British Columbia, Canada, hereby certify that:

1. I received a B.Sc. degree in Geophysics from the University of British Columbia in 1966.
2. I have been practising my profession since graduation.
3. I am a Professional Geophysicist registered in the Province of Alberta.
4. I am a Professional Engineer registered in the Province of Saskatchewan.
5. I hold no direct or indirect interest in, nor expect to receive any benefits from, the mineral property or properties described in this report.
6. This report may be used for the development of the property, provided that no portion will be used out of context in such a manner as to convey meanings different from that set out in the whole.
7. Consent is hereby given to the company for which this report was prepared to reproduce the report or any part of it for the purposes of development of the property, or facts relating to the raising of funds by way of a prospectus and/or statement of material facts.

Date:

Feb. 15/87

Signed:



Vancouver,  
British Columbia

Edwin Ross Rockel  
B.Sc., P.Geoph., P. Eng.

## REFERENCES

1. Fraser, D.C., 1969. Contouring of VLF EM Data, Geophysics, Vol. 34, No. 6, December, 1969, Tulsa, Oklahoma.
2. Sumner, J.S., 1976. Principals of Induced Polarization for Geophysical Exploration, Elsevier North-Holland Inc., New York, N.Y.
3. Sharma, P.V., 1976. Geophysical Methods in Geology, Elsevier Scientific Publishing Company, Amsterdam, The Netherlands
4. Telford, W.M., 1976. Applied Geophysics, Cambridge University Press, Cambridge, England
5. Walcott, P.E., August, 1985. A Report on an Induced Polarization Survey, Quesnel Area, British Columbia, Unpublished Report by Peter E. Walcott and Associates Limited, Vancouver, B.C.

## EQUIPMENT SPECIFICATIONS

Geonics Limited "EM-16" VLF EM Receiver

EG & G Canada "G-816" Portable Proton Magnetometer

EG & G Canada "G-856" Proton Precession  
Memory Magnetometer Base Station

Huntec "M-4" Induced Polarization Receiver

Huntec "M-2" 7.5 Kw. Induced Polarization Transmitter

Interpretex Resources Ltd. 7.5 Kilowatt Helicopter  
Portable Engine Driven Alternator

GEOPHYSICAL PERSONNEL

PERSONNEL

The following personnel worked on the property and/or were engaged in supervision for all or part of the days noted (includes mobilization and demobilization):

<u>Name</u>	<u>Position</u>	<u>Dates</u>
E.R. Rockel Richmond, B.C.	Consulting Geophysicist	July 25 & 26, 1986 Aug. 12 - 23, 1986
T.R. Matich Surrey, B.C.	Geophysicist	July 25 - Aug. 6, 1986
J.A. Martin Vancouver, B.C.	Geophysical Technician	July 25 - Aug. 6, 1986 Aug. 12 - 23, 1986
G.J. McPherson Surrey, B.C.	Geophysical Technician	Aug. 12 - 23, 1986
D.J. Sedgwick North Delta, B.C.	Geophysical Technician	Aug. 12 - 23, 1986
T.D. Plant Likely, B.C.	Geophysical Assistant	Aug. 12 - 23, 1986

The following personnel were involved in data preparation or reporting of the project for part or all of the days noted:

<u>Name</u>	<u>Position</u>	<u>Dates</u>
E.R. Rockel Richmond, B.C.	Consulting Geophysicist	Aug. 26 - 31, 1986 Sept. 1, 1986, Jan. 10 - 15, 17, 18, 20 - 23 & 26, 1987.

GEONICS LIMITED  
VLF EM 16

Source of Primary Field: VLF transmitting stations

Transmitting Stations Used: Any desired station frequency can be supplied with the instrument in the form of plug-in tuning units. Two tuning units can be plugged in at one time. A switch selects either station.

Operating Frequency Range: About 15-25 Hz

Parameters Measured: (1) The vertical in-phase component (tangent of the tilt angle of the polarization ellipsoid).  
(2) The vertical out-of-phase (quadrature) component (the short axis of the polarization ellipsoid compared to the long axis).

Method of Reading: In-phase from a mechanical inclinometer and quadrature from a calibrated dial. Nulling by audio tone.

Scale Range: In-phase  $\pm 150\%$ ; quadrature  $\pm 40\%$

Readability:  $\pm 1\%$

Reading Time: 10-40 seconds depending on signal strength

Operating Temperature Range:  $-40$  to  $50^{\circ}$  C.

Operating controls: ON-OFF switch, battery testing push button, station selector, switch, volume control, quadrature, dial  $\pm 40\%$ , inclinometer dial  $\pm 150\%$

Power Supply: 6 size AA (penlight) alkaline cells. Life about 200 hours

Dimensions: 42 x 14 x 9 cm (16 x 5.5 x 3.5 in)

Weight: 1.6 kg (3.5 lbs)

Instrument Supplied With: Monotonic speaker, carrying case, manual of operation, 3 station selector plug-in tuning units (additional frequencies are optional), set of batteries

Shipping Weight: 4.5 kg (10 lbs.)

Name and Address of Manufacturer: Geonics Limited  
1745 Meyerside Drive/Unit 8  
Mississauga, Ontario  
L5T 1C5

MODEL G-816

PORTABLE PROTON MAGNETOMETER

Sensitivity:  $\pm 1$  gamma throughout range

Range: 20,000 to 90,000 gammas (worldwide)

Tuning: Multi-position switch with signal amplitude indicator light on display

Gradient Tolerance: Exceeds 800 gammas/ft

Sampling Rate: Manual pushbutton, one reading each 6 seconds

Output: 5 digit numeric display with readout directly in gammas

Power Requirements: Twelve self-contained 1.5 volt "D" cell universally available flashlight-type batteries. Charge state or replacement signified by flashing indicator light on display.

Temperature Range: Console and sensor:  $-40^{\circ}$  to  $+85^{\circ}\text{C}$   
Battery pack:  $0^{\circ}$  to  $+50^{\circ}\text{C}$  (limited use to  $-15^{\circ}\text{C}$ ; lower temperature battery belt operation - optional)

Accuracy (Total Field):  $\pm 1$  gamma through  $0^{\circ}$  to  $\pm 50^{\circ}\text{C}$  temperature range

Sensor: High signal, noise cancelling, interchangeably mounted on separate staff or attached to back pack

Size: Console: 3.5 x 7 x 11 inches (9 x 18 x 28 cm)  
Sensor: 3.5 x 5 inches (9 x 13 cm)  
Staff: 1 inch diameter x 8 ft. length (3 cm x 2.5 m)

Weight: Console (w/batteries): 5.5lbs. 2.8kgs.  
Sensor and signal cable: 4.0lbs. 1.8kgs.  
Aluminum staff: 2.0lbs. 0.9kgs.  
Total Weight 11.5lbs. 5.2kgs.

EG & G Canada  
Exploranium/Geometrics Division  
Unit #1  
640 Hardwick Road  
Bolton, Ontario LOP 1A0

MODEL G-856

PROTON PRECESSION MEMORY MAGNETOMETER

Display	Six digit display of magnetic field to resolution of 0.1 gamma or time to nearest second. Additional three-digit display of station or day of year.
Resolution	Typically 0.1 gamma in average conditions. May degrade to lower resolution in weak fields, noisy conditions or high gradients.
Accuracy	One gamma, limited by remnant magnetism in sensor and crystal oscillator accuracy.
Clock	Julian clock with stability of 5 seconds per month at room temperature and 5 seconds per day over the temperature range of -20 to +50 degrees Celsius.
Tuning	Push button tuning from keyboard with current value displayed on request. Tuning range 20 to 90 kilogammas.
Gradient Tolerance	Tolerates gradients to 5000 gammas/meter. When high gradients truncate count interval, maintains partial reading to an accuracy consistent with data.
Cycle Time	Complete field measurement in three seconds in normal operation. Internal switch selection for faster cycle (1.5 seconds) at reduced resolution or longer cycles.
Manual Read	Takes reading on command. Will store data in memory on command at operator's discretion.
Self-Cycle	Internal switch will cause the instrument to self-cycle, storing automatically, for time dependent measurements. Available intervals are 5, 10 and 30 seconds, 1,2,5, and 10 minutes depending on switch position.
Memory	Stores 1,000 readings in portable mode, keeping track of time and station number. In base station operation, records last four digits of field at discrete intervals, allowing storage of over 2,500 readings.
Output	Plays data out in standard RS-232 format at selectable baud rates. Also outputs data in byte parallel, character serial BCD for use with digital recorders.
Inputs	Will accept an external sample command.
Special Functions	An internal switch allows adjustment of polarization time and count time to improve performance in marginal area or improve resolution or to speed operation.

cont'd



G-856 cont'd

Physical	Instrument console: 7 x 10½ x 3½ inches (18 x 27 x 9 cm) 6 lbs (2.7 kg) Sensor: 3½ x 5 inches (9 x 13 cm) 4 lbs (1.8 kg) Staff: 1 inch x 8 feet (3 cm x 2.5 m) 2 lbs (1 kg)
Environmental	Meets specifications from 0 to 40 degrees Celsius. Operates satisfactorily from -20 to 50 degrees Celsius. Weatherproof.
Power	Operates from 8 D-cell flashlight batteries (or 12 volts external power). May be operated at 18 volts external power to improve resolution. Power failure or replacement of batteries will not cause loss of data stored in memory.
Standard Accessories	Sensor Staff Chest Harness Two sets of batteries Operating Manual Applications Manual for Portable Magnetometers
Optional Accessories	RS-232 Interface Cable Rechargeable Battery Pack (mounts inside case in place of normal batteries) and Charger Cold weather battery belt Digital Tape Recorder with Interface Cables

EG & G Canada  
Exploranium/Geometrics Division  
Unit #1  
640 Hardwick Road  
Bolton, Ontario LOP 1A0

M-4 SERIES

M-4

# Induced Polarization Receiver

## DESCRIPTION

The Hunttec M-4 is a microprocessor based receiver for time and frequency domain IP and complex resistivity measurement. It is:

**Easy to operate.** One switch starts a measurement, of up to 33 quantities simultaneously. The optional Cassette DataLogger records them all in seconds. Calibration, gain setting and SP buckout are all automatic.

**Reliable.** Using advanced digital signal processing techniques, the M-4 delivers consistently accurate data even in noisy, highly conductive areas. For mechanical reliability it is packaged in a rugged aluminum case for backpack or hand carrying.

**Versatile.** The operator may adjust delay and integration times, operating frequency and other measurement parameters to adapt to a wide range of survey conditions and requirements. An independent reference channel facilitates drillhole and underground work, and guarantees transmitter-receiver synchronization in high-noise conditions.

**Highly accurate.** With a frequency bandwidth of 100 Hz and noise-cancelling digital signal stacking, the M-4 delivers very precise results. The details are summarized in a table overleaf.



**Sensitive.** The same features that make the M-4 accurate allow detection of very weak signals. The Hunttec receiver requires lower transmitter power than any other, for a given set of operating conditions. Automatic correction for drifts in self-potential and gain allow long stacking times for significant signal-to-noise improvements.

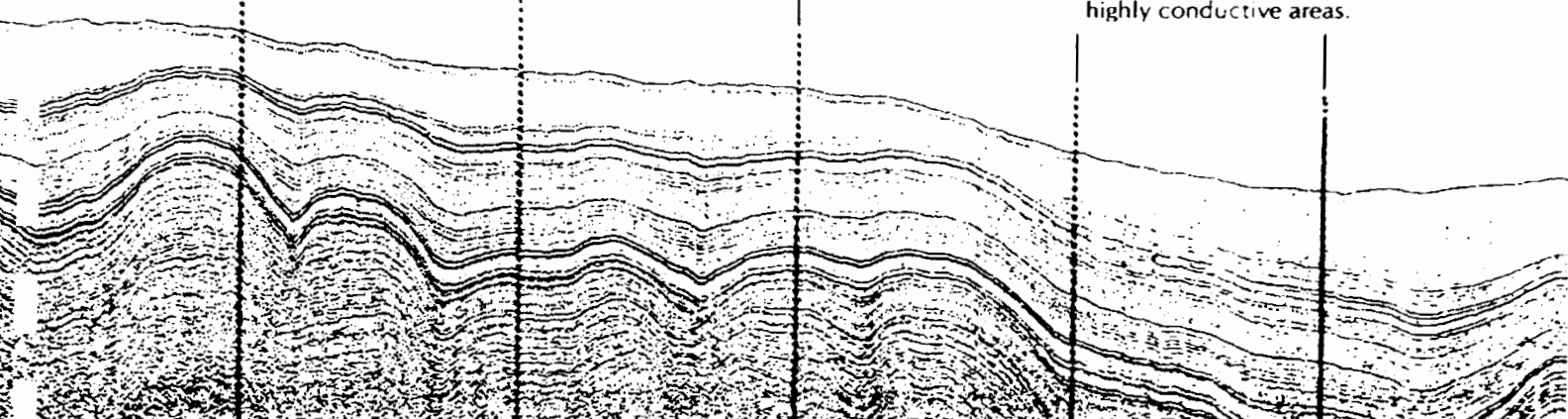
**Intelligent.** Under the control of a powerful 16-bit microprocessor, the M-4 calibrates and tests itself between measurements. Coded error messages, flashed onto the display, inform the operator of any malfunction.

The M-4 Receiver is complemented by Hunttec's new M-4 transmitters, which offer precisely timed constant-current output and both time and frequency domain waveforms, compatible with the receiver's accuracy and multi-mode measurement capabilities. The RL-2 Reference Isolator connects any IP transmitter to the receiver's reference channel.

Contact Hunttec for more information on the benefits offered by the M-4 product line.

## FEATURES

- Time and Frequency domain IP and Complex Resistivity operation.
- Simultaneous Time domain and Complex Resistivity measurement.
- Automatic calibration gain setting SP cancellation fault diagnosis filter tuning.
- Independent reference channel for drill-hole and underground work.
- 42 quantities, displayable on large 3½ digit low-temperature liquid-crystal read-out.
- Analogue meter for source resistance measurement.
- 10<sup>9</sup> ohms differential input resistance
- 8 hours continuous operation with replaceable, rechargeable nickel-cadmium battery pack (2 supplied).
- Optional Cassette DataLogger fits inside case, has read-after-write error checking. Up to 350 stations per tape.
- Conveniently packaged for backpacking or hand carrying.
- 100 Hz bandwidth, fine time-resolution.
- Advanced digital signal stacking.
- Delivers reliable, accurate data in noisy, highly conductive areas.



## SPECIFICATIONS

### INPUTS

#### Signal Channel

Range:  $5 \times 10^{-5}$  to 10 volts. Automatic ranging. Overload indication  
 Resistance: Greater than  $10^9$  ohms differential  
 Bandwidth: 100 Hz  
 P Cancellation: -5 to +5 volts (automatic)  
 Protection: Low-leakage diode clamps, gas discharge surge arrestors, replaceable fuses.

#### Reference Channel

Level: 500 mV minimum, 10 volts peak maximum, overload indication  
 Resistance:  $2 \times 10^9$  ohms differential

### CONTROLS AND FUNCTIONS

#### Operating Controls

Keypad: 16 keys, calculator format, function associated with each key.  
 Reference Registers: Keypad may be used to store up to ten  $3\frac{1}{2}$  digit numeric values with floating decimal point to represent station number, line number, operator, time, date, weather, transmitter current, etc. for recording on cassette.

#### Programming Controls

Sub-panel: All programming controls are on a covered sub-panel.  
 knob/wheel switches: Select delay time  $t_D$  in milliseconds chargeability window  $t_p$  in milliseconds; operating frequency; PFE frequency ratio.

#### Displayable Quantities

Time domain: Primary voltage; self-potential; chargeability (total or each of 10 windows of equal width); phases of odd harmonics 3 to 15; amplitudes of odd harmonics 1 to 15; cycle count; repeating display of polarization potential and total chargeability.  
 Frequency domain: Primary amplitude; Percent Frequency Effect; self-potential; cycle count.  
 Complex Resistivity: Phases of odd harmonics 3 to 15; amplitudes of odd harmonics 1 to 15; fundamental phase (with ref. input); cycle count.  
 Battery mode: Battery voltage, Frequency error.

### OUTPUTS

#### Displays

Digital Display:  $3\frac{1}{2}$  digit, low-temperature liquid crystal display. Indicates measurement results and diagnostic error messages.  
 Analogue Meter: Ohms scale for source resistance; also gives qualitative indication of signal-to-noise ratio.

### CASSETTE DATALOGGER (OPTIONAL)

Description: Accommodated within M-4 chassis. If not acquired with receiver, may be retrofitted by user at any time. Two recording modes:  
 Partial: All sub-panel settings, measurement results, and contents of reference registers are recorded (2 seconds recording time).  
 Full: As in partial mode, but also recorded is one cycle of averaged signal waveform (28 seconds recording time). If external reference is used, one cycle of reference waveform is also recorded (60 seconds recording time). Extra memory and software available to average and store the reference waveform for advanced offline resistivity computation.  
 Format: ANSI/ECMA/ISO standard for saturation recording: 80 bytes/record, all data recorded in ASCII code.  
 Verification: Read-after-write data verification (automatic).

### MECHANICAL

M-4 Receiver with battery pack: 45 cm x 33 cm x 14 cm, 10.0 kg.  
 M-4 Receiver with battery pack and Cassette DataLogger: Dimensions as above, 11.0 kg.  
 Replaceable Battery pack: 33 cm x 11 cm x 4.5 cm, 3 kg.

### ENVIRONMENTAL

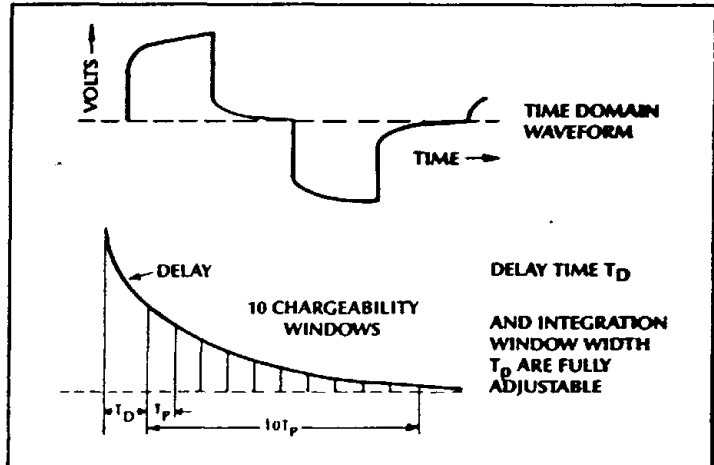
Temperature: Operation:  $-20^\circ\text{C}$  to  $+55^\circ\text{C}$ .  
 Storage:  $-40^\circ\text{C}$  to  $+70^\circ\text{C}$ .  
 Humidity: Moisture-proof, operable in light drizzle.  
 Altitude:  $-1,525$  m to  $+4,775$  m.  
 Shock, Vibration: Suitable for transport in bush vehicles.

### OUTPUT ACCURACY AND SENSITIVITY

	PHASES	AMPLITUDES	V <sub>p</sub>	SP	CHARGEABILITY	PFE
UNITS	milliradians	volts	volts	volts	seconds	%
ACCURACY	2milliradians(1)	1% to 40Hz 2% to 80Hz	$\pm 1\%$	$\pm 1\%$	0.1%(2)	0.1%(3) full scale
SENSITIVITY	0.01 milliradians	$10^{-6}$ volts	$10^{-3}$ volts	$10^{-3}$ volts	$10^{-6}$ seconds	0.001% full scale

- Frequency domain mode: at harmonic frequencies up to 15 Hz, increases to not more than 5 milliradians at 80 Hz.  
 Time domain mode: at harmonic frequencies up to 7.5 Hz, increases to not more than 5 milliradians at 30 Hz.
- of total OFF time
- Full scale defined as 100% PFE.  
 Cassette Data: recorded in ASCII, 9 digits with decimal point fixed for four decimal digits.  
 Display Data:  $3\frac{1}{2}$  digits, floating decimal point.  
 Resolution of averaged waveform limited by A/D converter to one part in  $4096 \times$  (square root of cycle count).  
 Resolution of reference waveform (not averaged) limited by available memory to one part in 256. Additional memory and averaging software available as option.

### CHARGEABILITY WINDOWS



HUNTEC  
 1750 Brimley Road, Scarborough  
 Ontario, Canada M1P 4X7  
 Phone: (416) 299-4100 Telex: 06-963640

HUNTEC (70) LIMITED  
1750 BRIMLEY ROAD  
SCARBOROUGH, ONTARIO  
M1P 4X7

7.5 Kw INDUCED POLARIZATION TRANSMITTER

SPECIFICATIONS

Output: 100 to 3250 volts in 10 steps. 16 amps maximum.

Input: 3 phase 400 Hz. 120/208 volts.

Cycling Rates: 2 sec. ON, 2 sec. OFF, or to suit customer requirements.  
SCR current on/off switching.

Temperature  
Range:  $-34^{\circ}\text{C}$  to  $+50^{\circ}\text{C}$

Current Output  
Meter: 2 ranges; 0 to 10 amp and 0 to 20 amp.

Ground Resis-  
tance Meter: 2 ranges; 0 to 10k ohms and 0 to 100k ohms.

Input  
Voltmeter: 0 to 150 volts A.C.

Dummy Load: 2 level; 2Kw and 6Kw. Switched in during OFF time to  
smooth generator load.

Over/Under  
Voltage  
Protection: Automatic shutdown for excessive input voltage  
changes.

Construction: Welded aluminum frame. All solid state circuits on  
removable printed circuit boards.

Size: 53.0 x 43.0 x 43.0 centimeters.

Weight: 34 kilograms.

INTERPRETEX RESOURCES LTD.  
BOX 48239 BENTALL P.O.  
VANCOUVER, B.C.  
V7X 1A1

---

HELICOPTER PORTABLE 7.5 KILOWATT ENGINE DRIVEN ALTERNATOR

SPECIFICATIONS

Output: 120 volts A.C. 400Hz. 3 phase 18KVA maximum.

Engine: 20 H.P. air cooled two cylinder Onan gasoline engine series CCKB mounted on a steel frame.

Fuel: regular grade leaded or non-leaded gasoline, tank capacity 25 liters (outboard motor tank) provides up to four hours continuous operation depending on load.

Alternator: Bendix Aviation AC Generator Type 28E01 belt driven, forced air cooled. External voltage regulator.

Construction: engine and alternator mounted on a steel frame suitable for helicopter sling transport.

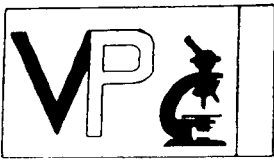
Speed  
Regulation: internal mechanical engine governor.

Size: approx. .75 meter x 1 meter x .50 meters

EAST GRID CONTOUR MAPS AND 3D PLOTS

**APPENDIX 2**

**PETROGRAPHIC REPORT**



# Vancouver Petrographics Ltd.

JAMES VINNELL, Manager  
JOHN G. PAYNE, Ph. D. Geologist

P.O. BOX 39  
8887 NASH STREET  
FORT LANGLEY, B.C.  
VOX 1J0

PHONE (604) 888-1323

September 22nd, 1986

Invoice #5961

Report for: Ken McNaughton,  
E and B Explorations,  
1440 - 800 West Pender St.,  
Vancouver, B.C.  
V6C 2V6

## Samples:

15 rock samples for thin sectioning and petrographic description. Samples (prefixed KR-86) are numbered 40A, 97 - 102, 104 - 106, 108 - 111 and 113.

## Summary:

The rocks of the suite mainly fall into 3 distinct groups: porphyritic volcanics; tuffs; and mafic intrusives.

### a) Porphyritic volcanics:

This group includes 3 samples: 40A, 98 and 111. Of these, sample 98 is a comparatively fresh rock of andesite composition, consisting of phenocrysts of pyroxene, plagioclase and an unidentifiable totally altered mafic, in a fine-grained groundmass of plagioclase, pyroxene and chlorite: it shows gradation to a chilled margin. Sample 40A is a rock of similar type, but strongly altered to chlorite, carbonate and epidote with disseminated pyrite. Sample 111 differs in having a groundmass containing K-spar and quartz, and phenocrysts dominantly of altered plagioclase (sericite/carbonate) and lesser altered biotite: it is classified as a dacite.

### b) Tuffs:

This group includes 6 samples: 99, 100, 102, 104, 105 and 106. Of these, samples 99 and 104 are andesitic lithic-crystal tuffs of rather coarse grain (up to 5.0mm), notably fresh and without fine matrix. Samples 105 and 106 are finer grained tuffs (clasts 0.1 - 0.5mm), the first of similar composition to 99 and 104, and the second with a higher content of K-spar and interlayers of much finer material. Sample 100 is a very fine ash-tuff of andesitic composition. Sample 102 is a specialized variety, consisting of clasts similar to those of 104 but embedded in a matrix of fine-grained carbonate.

### c) Mafic intrusives:

This group includes 4 samples: 101, 108, 109 and 113. Of these, sample 101



is essentially unaltered and consists of a medium to coarse-grained aggregate of clinopyroxene and lesser plagioclase. Sample 109 is of comparable grain size but is strongly altered; the plagioclase is converted to sericite and carbonate and the mafics are amphibole (secondary after pyroxene?) altering to carbonate. Sample 108 is a finer grained rock (0.2 - 2.0mm), in which partially sericitized plagioclase is intergrown with epidote, carbonate and chlorite - presumably representing totally altered mafics. Sample 113 is of similar grain size to 108; it contains very little plagioclase and the major constituents are a fibrous secondary amphibole and epidote.

These rocks appear to be more or less altered gabbros and microgabbros (possibly grading to diorites). They contain minor disseminated sulfides.

d) Others:

The remaining two rocks of the suite are #97, a coarse conglomerate of cherty and volcanic pebbles cemented and replaced by limonite; and #110, a rock of unknown affinities composed largely of fibrous, pale-coloured amphibole with minor chlorite and carbonate (but no feldspar).



J.F. Harris Ph.D.

## Estimated mode

Altered plagioclase	48
Quartz	7
Chlorite	15
Carbonate	14
Epidote	11
Secondary amphibole	3
Sphene )	1
Rutile )	1
Pyrite	1

This is a strongly altered, porphyritic rock. The groundmass is a mesh-work-textured aggregate of turbid plagioclase laths up to 0.15mm in size, with interstitial chlorite and quartz, disseminated granules of epidote, and minor fine-grained sub-opaques (sphene/rutile). Within this altered mass the shapes of coarser, prismatic feldspars, up to about 1.0mm in size, are sometimes distinguishable; these are extensively replaced by fine-grained chlorite and cloudy clay/sericite alteration.

Altered mafic phenocrysts make up some 15% of the rock. These are subhedral to euhedral in form and 0.1 - 2.5mm in size. They consist of various mixtures of carbonate, pale amphibole, chlorite and epidote. The amphibole may be remnants of the original grains or, more likely, secondary after pyroxene.

The rock is cut by irregular veinlets and replacement zones of carbonate and epidote. Epidote also forms more widespread, disseminated clumps throughout the rock. Carbonate veinlets with associated quartz appear to form a distinct phase of alteration following much the same zones but cross-cutting the carbonate-epidote veinlets.

Disseminated pyrite shows a clear association with the zone of strong veining but tends to occur marginal to the veinlets more than within them. It is also seen in dispersed form, randomly disseminated and associated with altered mafic phenocrysts.

This is a heterogenous conglomerate made up of rounded to sub-angular clasts of various rock types, ranging from 0.2mm - 40mm in size.

The largest pebble is a highly siliceous cherty rock composed of quartz of grain size 10 - 20 microns in microlenticular intergrowth with abundant micron-sized opaque dust. Other clasts are fine-grained quartzites and wackes, sheared (vein?) quartz and occasional altered volcanics.

The clasts are tightly cemented by compact, partly colloform limonite. This may be the original cement or totally replaces it. Limonite also fills occasional (post-formational) fractures in the constituent pebbles, and more or less strongly replaces others.

## Estimated mode

Plagioclase	35
Sericite	1
Pyroxene	42
Chlorite	13
Secondary amphibole	2
Carbonate	2
Sphene	4
Pyrite	1

This is a rather fresh andesite made up of approximately 15% phenocrysts set in a fine to very fine-grained, meshwork-textured groundmass.

The latter consists of a randomly-oriented aggregate of lathlike, fresh plagioclase and pyroxene, with interstitial chlorite and very fine-grained sphene. It appears to show a gradational change in overall grain size from approximately 0.1mm at one side of the slide to essentially cryptocrystalline or glassy at the other. This finest-grained zone contains numerous small xenoliths of a greywacke-like material and may represent a chilled margin or flow contact.

Phenocrysts range in size from 0.2 - 2.0mm and are of three different kinds. Most abundant (and coarsest) are euhedral crystals of fresh pyroxene. The other types are euhedral plagioclase, commonly more or less sericitized, and a totally altered type consisting of rather ragged-ended, equant/prismatic masses of fibrous secondary amphibole and/or chlorite. The latter are commonly rimmed by fine-grained disseminated sulfides (pyrite?).

Remarkably the fresh pyroxenes and the totally altered pseudomorphs (possibly after hornblende?) are quite often intimately associated in clumps.

Phenocrysts become smaller and less abundant in the chilled margin zone.

Carbonate forms occasional hairline microfracture fillings and small disseminated flecks.

This rock is a close-packed aggregate of lithic fragments up to 5mm in size, together with a proportion of crystal clasts.

The lithic fragments are of various kinds, mostly andesites with fine-grained to glassy-textured, K-rich groundmasses and abundant euhedral plagioclase and pyroxene phenocrysts. Some are amygdaloidal and have chlorite-filled vesicles. The rock appears to contain no quartz.

The disaggregated crystals are mainly euhedral pyroxenes, 0.1 - 2.0mm in size, sometimes broken.

All constituents are notably fresh and there is a total lack of alteration minerals such as sericite, carbonate, epidote etc.

The clasts are relatively homogenous in size and there is no matrix as such, the interstices between larger clasts simply being occupied by somewhat smaller ones. A few pockets of chlorite may be interstitial fillings of post-accumulation age.

This is a fine-grained feldspathic rock in which constituent proportions are difficult to estimate. Particles are mainly in the size range 0.02 - 0.05mm, and consist of rather diffuse crystal fragments of plagioclase in a turbid, ashy matrix flecked with chlorite, carbonate and sub-opaque dust.

Local lenses of slightly coarser sericitized plagioclase clasts (to 0.2mm) and minor quartz contribute to the streaky, ill-defined banded appearance.

Also the distribution of fine-grained, disseminated sulfides (pyrite?) tends to be concentrated in sub-parallel bands, though with no particular preference for the coarser clastic lenses. The sulfides are anhedral grains, 0.01 - 0.2mm in size, often forming intimate intergrowths and rim-structures with small patches of an unidentified, water-clear, low-relief mineral showing upper first-order polarization colours.

The slide includes a thin, sub-concordant zone of cherty silicification with a drusy limonitic core.

## Estimated mode

Pyroxene	62
Amphibole	12
Plagioclase	18
K-feldspar	5
Sericite	1
Chlorite	1
Sphene	1
Apatite	trace
Leucoxene	trace

This is a rather coarse-grained, intrusive-textured, mafic-rich rock composed dominantly of fresh, subhedral clino-pyroxene of grain size 1 - 7mm.

The pyroxene locally shows intergrowth with, or alteration to, amphibole. Some of the latter is a well-crystallized pale green to pale brown variety, but amphibole of obvious secondary type (fibrous, green to orange-brown material, as pockets and irregular networks) is also seen. Some of this material contains lamellar intergrowths of leucoxene.

Feldspars (mainly plagioclase with some intergrown K-spar) form an interstitial phase to the dominant mafics. They show local pervasive sericitization.

Sericite also occurs as occasional small concentrated pockets of felted material, sometimes associated with chlorite of similar mode.

Well-crystallized sphene is a disseminated accessory, together with rare small crystals of apatite. There is a surprising lack of opaque oxides or sulfides.

## Estimated mode

Lithic fragments	45
Crystal clasts	20
Carbonate	35

This is a rock of unusual type, composed of equant, angular lithic fragments, 0.2 - 2.0mm in size, and individual euhedral crystals of pyroxene and lesser plagioclase of slightly smaller size, 'floating' (without inter-clast contact) in a matrix of granular carbonate.

The lithic fragments are predominantly of the one general type - a porphyritic andesite with glassy to meshwork/microlitic groundmass, often with small amygdules of chlorite or carbonate, and more or less abundant euhedral phenocrysts of plagioclase and pyroxene.

Plagioclase phenocrysts, throughout the rock, show a consistent, rather strong, pervasive alteration to sericite, but pyroxene (whether in lithic fragments or as free mineral clasts) is totally fresh.

The outlines of the lithic fragments are often ragged and irregular, though well-defined; locally they appear to show marginal replacement by the carbonate cement, but are internally unaffected. Likewise the pyroxene crystal clasts, though generally retaining their euhedral form, or broken portions of it, are occasionally embayed and partially assimilated by the surrounding carbonate matrix.

The carbonate is an anhedral mosaic of rather homogenous grain size (0.02 - 0.15mm) which, judging from the moderate to strong reaction with dilute acid, is largely calcitic in composition. A striking feature is the total lack of small inclusions or replacement remnants in the carbonate matrix, which has the form of a homogenous continuum in which the separate, rather even-sized clasts are set. Likewise the lack of any vein-type or diffuse penetration of carbonate into the body of the clasts is remarkable.

The slide includes a localized sheeted vein or replacement zone of carbonate with associated albite.



This is a very similar type of rock to KR-86-99, though a little finer grained. It is a tuff composed of close-packed lithic and crystal clasts with little or no fine matrix. Lithic clasts from 1 - 4mm in size are distinguishable, but generally the grain size is mainly in the range 0.2 - 1.0mm, with crystals predominating over lithic clasts.

The composition is similar to the other tuffs of the suite, consisting of lithic fragments of porphyritic andesite (turbid cryptocrystalline to meshwork ground-masses, sometimes amygdaloidal and often potassic, with phenocrysts of plagioclase and pyroxene) and crystals of plagioclase and pyroxene. There is no quartz. Minimal interstitial or matrix material appears to be felsitic ash and/or fibrous chlorite, with rare traces of carbonate. In many areas it is difficult to tell whether the rock is made up of close-packed, randomly oriented disaggregated crystals or of abundantly porphyritic lithic clasts.

The pyroxene crystals are fresh and generally angular, subhedral in form. Plagioclase is generally also quite fresh, showing slight clouding and local weak sericitization. It sometimes shows partial replacement by (matrix?) chlorite.

This is another clean-looking, rather equigranular, non-foliated rock. It contains traces of disseminated pyrite.

This is a very similar type of rock to KR-86-104 but perceptibly finer grained.

It is an aggregate of plagioclase and pyroxene crystals and lesser lithic fragments of grain size 0.1 - 0.5mm, the interstices between which are packed with smaller clasts, about 0.05mm in size, of finer felsitic material and chlorite. Flecks and clumps of fine-grained carbonate are locally developed within this matrix component.

The proportion of plagioclase to pyroxene is notably higher in this rock than the previous one.

As in 104, the clasts are well-defined, angular/euhedral and fresh. The rock shows no foliation or recognizable layering on the thin section scale.

The content of disseminated pyrite is slightly higher than in 104. It occurs randomly and rather evenly distributed, as irregular-shaped grains, 0.05 - 0.2mm in size, clearly interstitial to, and moulded around, adjacent clasts.

This is another rock of very similar appearance to KR-86-105 under the microscope. The intensity of cobaltinitrite staining on the cut-off chip, however, indicates that K-feldspar is a more prominent constituent (probably making up about 30% of the rock).

It is a mixture of angular crystal and lesser lithic clasts in the size range 0.1 - 0.5mm (rarely to 1.0mm). The K-spar is partly in the form of turbid glassy groundmass material in the lithic clasts, but also occurs as recognizable individual mineral clasts and, rather extensively, as a felsitic aggregate interstitial to the coarser clasts.

Other constituents of the interstitial phase are chlorite and localized pervasive flecks and patches of carbonate.

The pyroxene and feldspars making up this rock are essentially fresh and unaltered throughout. Rare crystal clasts of hornblende are also present.

Some laminar segregation of K-spar is perceptible in the stained chip, producing a weak foliation.

The slide includes a somewhat irregular contact (soft-sediment scouring) with a similar but distinctly finer-grained rock type. In fact, there are two varieties present, one with a maximum clast size of 0.1mm and the other with clasts no more than 0.05mm in size. These variants still contain fresh angular crystals and crystal fragments of pyroxene and feldspars, but the proportion of very fine-grained interstitial chloritic/felsitic material becomes progressively greater in the finer aggregates. Also the ratios of pyroxene to feldspars and of K-spar to plagioclase appear progressively smaller.

## Estimated mode

Plagioclase	25
K-feldspar	1
Sericite	5
Carbonate	24
Quartz	3
Epidote	30
Chlorite	7
Sphene )	3
Rutile )	
Apatite	1
Pyrite	1

This is a strongly altered rock, possibly of related type to KR-86-101. Its original composition appears to have been dominantly a rather even-grained, subhedral to anhedral aggregate of plagioclase, 0.2 - 2.0mm in size, intergrown with mafics of indeterminate type.

It now has carbonate and epidote as major constituents, along with remnant plagioclase.

The epidote is largely in the form of well-crystallized prismatic masses, often with interstitial fine-grained quartz and minor carbonate. It is unclear whether this pseudomorphs original mafic silicates (of which no trace now survives) or whether it has developed by replacement of plagioclase. A few cases are seen where it appears to be developing as skeletal metacrysts within altered plagioclase.

Similar considerations apply to carbonate, of which the rock contains extensive patches, often with intimate, streaky/reticulate intergrowths of chlorite, speckled with fine-grained sphene, and irregular pools of quartz.

Probably both the above constituents mainly represent altered forms of original major constituent mafics. The plagioclase in the rock is typically quite strongly sericitized, but does not generally show either carbonate or epidote alteration.

Sphene, in well-crystallized form, occurs as scattered disseminated grains, as does apatite (as a few relatively coarse, prismatic grains). Rutile forms occasional skeletal clumps. Pyrite is relatively abundant, as random irregular grains interstitial to the granular fabric of the rock.

## Estimated mode

Plagioclase	10
Sericite	18
Amphibole	32
Carbonate	30
Chlorite	6
Quartz	2
Sphene )	1
Rutile )	
Pyrite	1

This is another intrusive-textured rock of similar general type to 101 and 108. Like 108 it is strongly altered, but in a somewhat different style. It contains abundant remnant mafics; however, these are hornblende (rather than the pyroxene of 101).

It is also a coarser rock than 108, consisting of an aggregate of anhedral-subhedral prismatic grains, mainly in the size range 1 - 5mm.

The major constituents are plagioclase, strongly and evenly altered to a mass of finely felted sericite and flecks and cleavage-controlled veinlets of carbonate; and amphibole (a pale olive-green variety), more or less extensively altered to carbonate via cleavages. In some cases the amphibole alteration includes patches of chlorite and tiny clumps of fine-grained sphene.

Chlorite also forms scattered interstitial, sometimes elongate pockets of compact felted material, and there are patches of acicular (secondary?) amphibole more or less pseudomorphed by carbonate.

Quartz forms randomly distributed, interstitial flecks and more extensive areas of apparent replacement, or small vein-like segregations with carbonates, often associated with clusters of pyrite grains.

The pyrite clusters occur indiscriminately interstitial to, and enclosed within, the coarse altered major constituents.

Estimated mode

Amphibole	80
Carbonate	8
Quartz	3
Chlorite	8
Pyrite	1

This is a heterogenous, totally altered rock of unknown origin.

It now consists largely of fine-grained, colourless to very pale green amphibole, ranging from ragged prismatic grains of 0.5mm in size, down through sub-oriented aggregates of small acicular crystals to extremely fine-grained, fibrous masses.

The amphibole aggregate tends to show a weak irregular foliation and, in some respects, looks like a sheared rock with fine-grained to fibrous aggregates swirling around kernels of coarser prismatic aggregate.

Chlorite is an accessory, locally occurring intimately intergrown as a matrix to the amphibole and as segregated diffuse streaks and veinlets.

Carbonate likewise occurs as a dispersed, fine-grained interstitial constituent and as irregular veinlets and replacement zones.

At one end of the slide there is an area of pervasive silicification, with granular or cherty quartz forming irregular impregnations and veinlet networks enclosing clumps of amphibole and chlorite. The cryptic breccia/fragmental structure which is faintly perceptible throughout the rock is most clearly developed in this area. This area of silicification is the locus of maximum concentration of disseminated pyrite. Pyrite also occurs scattered throughout, often (though not exclusively) associated with veinlets and pockets of chlorite, carbonate or quartz.

## Estimated mode

## Phenocrysts

Altered plagioclase	32
Altered mafics	8

## Groundmass

K-spar	28
Plagioclase	10
Quartz	10
Sericite	4
Carbonate	6
Limonite	2
Pyrite	trace
Apatite	trace

This rock is made up of approximately 40% phenocrysts, from 0.2 - 2.0mm in size, set in a felsitic groundmass of grain size 0.01 - 0.03mm.

The phenocrysts are of euhedral prismatic form and appear to have been largely plagioclase. They are now totally altered to fine-grained intergrowths of carbonate and felted sericite.

A proportion of the smaller phenocrysts are composed of interlaminated muscovite and leucoxene, or of limonite or limonitic carbonate with sericite. These are presumed to represent altered mafic silicates, probably mainly biotite.

Some of the altered phenocrysts contain small patches of quartz.

The groundmass is an intimate intergrowth of K-feldspar, plagioclase and quartz, possibly with minor interstitial mafics. It is pervasively flecked with sericite and limonitic carbonate, and dusted with micron-sized sub-opaques. However, the groundmass feldspars are essentially unaltered compared with the phenocrysts.

Disseminated pyrite (partially limonitized) occurs sparsely as clusters, showing no special association.

## Estimated mode

Pyroxene	14
Secondary amphibole	48
Remnant plagioclase	2
Epidote	20
Carbonate	6
Chlorite	5
Quartz	2
Sphene	1
Pyrite	2

This is another altered intrusive of similar general aspect to 101, 108 and 109. It appears closest to 101 as regards original rock type, being of mafic-rich (possibly even ultra-mafic) composition.

It is texturally and mineralogically strongly modified by alteration, but appears to have developed from a subhedral, granular aggregate of grain size 0.5 - 2.0mm.

It now consists of isolated masses of prismatic pyroxene, rimmed and veined by pale green amphibole, and more or less altered to carbonate, separated by extensive areas of felted or meshwork/acicular, darker green, secondary-type amphibole. The latter masses often include scattered, pockety segregations of chlorite.

Other components, in what is now a rather heterogenous aggregate, are areas composed largely of carbonate (sometimes with diffuse remnants of plagioclase), and irregular clumps and networks of coarsely granular epidote (locally seen to be developing from, and enveloping remnants of, any or all of the other constituents).

Quartz occurs as small interstitial pockets, especially associated with the epidote, and as occasional veinlets with intergrown carbonate.

Disseminated pyrite forms poikilitic/skeletal clusters and partial euhedra, 0.1 - 0.5mm in size, sometimes associated with pockets of quartz but generally random in its association.



**APPENDIX 3**  
**ASSAY CERTIFICATES**

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE 253-3158

DATA LINE 251-1011

## WHOLE ROCK ICP ANALYSIS

A .1000 GRAM SAMPLE IS FUSED WITH .60 GRAM OF LiBO<sub>2</sub> AND IS DISSOLVED IN 50 ML 5% HNO<sub>3</sub>.

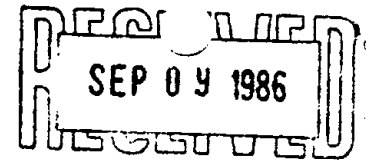
- SAMPLE TYPE:

DATE RECEIVED: 1 DATE REPORT MAILED: *Sept 9/86* ASSAYER: *D. J. J.* DEAN TOYE, CERTIFIED B.C. ASSAYER.

E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-2403

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SAMPLE#	SiO <sub>2</sub> %	Al <sub>2</sub> O <sub>3</sub> %	Fe <sub>2</sub> O <sub>3</sub> %	MgO %	CaO %	Na <sub>2</sub> O %	K <sub>2</sub> O %	TiO <sub>2</sub> %	P <sub>2</sub> O <sub>5</sub> %	MnO %	Cr <sub>2</sub> O <sub>3</sub> %	Ba PPM	Loi %	Sum
KR-86-040A	47.74	13.99	9.83	7.21	7.91	1.65	2.40	.69	.33	.17	.02	543	7.8	99.85
KR-86-098	49.74	14.19	10.52	6.84	8.14	2.65	2.45	.89	.38	.15	.05	1380	3.7	99.97
KR-86-099	49.49	14.28	10.98	7.09	6.78	2.95	2.25	1.10	.31	.15	.03	1642	4.2	99.93
KR-86-101	50.98	7.52	8.20	11.24	17.45	1.15	.70	.56	.15	.14	.15	138	1.7	99.97
KR-86-102	38.84	12.12	7.45	4.87	19.13	2.95	.85	.69	.27	.26	.04	242	12.4	99.92
KR-86-104	50.16	14.05	10.63	6.24	9.46	3.15	1.45	.99	.26	.15	.03	631	3.3	99.99
KR-86-105	51.58	15.00	9.87	4.79	8.18	4.20	1.45	1.03	.32	.15	.02	665	3.2	99.92
KR-86-106	51.05	15.45	9.80	4.93	7.92	3.15	2.80	.95	.30	.13	.02	1542	3.1	99.90
KR-86-108	46.28	14.30	11.20	5.77	11.70	1.25	1.35	.79	.06	.19	.04	218	6.8	99.77
KR-86-109	43.92	9.30	11.30	10.51	11.59	.30	.85	.67	.09	.16	.08	273	11.0	99.82
KR-86-110	49.78	6.68	10.46	13.04	11.30	.50	.20	.40	.20	.17	.18	102	6.9	99.83
KR-86-113	61.53	8.92	9.31	6.30	6.67	.20	.15	.46	.16	.23	.06	445	5.7	99.78
STD SO-4	68.09	10.07	3.37	.96	1.58	1.40	2.10	.53	.22	.07	.01	753	11.4	99.95



ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE 253-3158

DATA LINE 254-4911

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SN, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: SOILS - BOMESH AUI ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: SEPT 1 1986 DATE REPORT MAILED: *Sept 9/86* ASSAYER: *D. Toyne* DEAN TOYE, CERTIFIED B.C. ASSAYER.

E & B EXPLORATION PROJECT - 5055 FILE # 86-2403

PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au PPM
L4+00W 17+50N	1	25	9	96	.4	30	8	419	2.55	2	5	ND	3	17	1	4	2	56	.21	.064	12	47	.66	84	.05	2	1.71	.02	.07	1	2
L4+00W 17+25N	1	22	11	89	.3	20	9	317	2.56	2	5	ND	3	18	1	2	2	62	.22	.082	12	39	.43	84	.06	2	1.45	.02	.06	1	3
L4+00W 17+00N	1	33	10	96	.4	31	12	512	2.79	3	5	ND	2	23	1	4	2	63	.27	.059	11	45	.66	114	.05	7	1.75	.03	.08	1	2
L4+00W 16+75N	1	22	9	73	.3	25	6	206	2.01	2	5	ND	3	20	1	3	2	45	.20	.037	13	35	.59	60	.06	2	1.29	.02	.06	1	1
L4+00W 16+50N	2	45	12	106	.3	50	11	395	3.63	4	5	ND	5	24	1	5	2	64	.32	.066	16	64	.92	93	.07	2	1.85	.03	.08	1	1
L4+00W 16+25N	1	31	12	88	.2	42	9	319	3.10	2	5	ND	6	21	1	3	2	59	.28	.055	19	55	.86	75	.08	2	1.63	.03	.08	1	1
L4+00W 16+00N	1	28	11	98	.2	41	9	321	3.02	2	5	ND	5	22	1	5	2	58	.30	.058	22	54	.87	76	.09	2	1.63	.03	.07	1	9
L4+00W 15+75N	1	29	11	118	.3	34	8	270	2.68	2	5	ND	3	21	1	2	3	55	.26	.051	17	48	.68	103	.06	3	1.61	.03	.07	1	1
L4+00W 15+50N	2	32	10	124	.2	35	9	240	3.87	16	5	ND	4	32	1	2	2	72	.43	.087	18	44	.61	107	.05	4	1.47	.03	.05	1	1
L4+00W 15+25N	2	33	10	74	.1	34	10	272	3.11	11	5	ND	4	27	1	2	2	63	.52	.029	14	42	.60	99	.05	2	1.41	.03	.05	1	1
L4+00W 15+00N	2	39	11	90	.2	42	13	335	3.51	15	5	ND	4	24	1	7	2	73	.37	.038	13	50	.60	108	.06	2	1.55	.03	.06	1	1
L4+00W 14+50N	2	48	9	70	.6	38	9	431	2.83	10	5	ND	4	31	1	4	2	58	.42	.064	19	47	.61	88	.06	2	1.23	.03	.08	1	1
L4+00W 14+25N	2	36	10	120	.2	40	11	370	3.20	14	5	ND	5	29	1	4	2	61	.33	.079	18	45	.65	85	.07	4	1.25	.03	.08	1	2
L4+00W 14+00N	2	31	10	107	.2	35	9	315	2.98	11	5	ND	4	26	1	4	2	59	.33	.086	17	41	.61	98	.07	2	1.29	.03	.07	1	4
L4+00W 13+75N	1	37	9	126	.2	32	10	493	3.09	12	5	ND	2	32	1	2	2	71	.34	.075	17	43	.59	109	.06	4	1.30	.03	.07	1	2
L4+00W 13+50N	1	27	7	92	.2	35	8	358	2.56	2	5	ND	4	23	1	2	2	50	.31	.051	18	49	.72	80	.07	3	1.37	.03	.09	1	2
L4+00W 13+25N	1	23	12	96	.2	33	8	266	2.53	3	5	ND	4	22	1	2	2	53	.30	.044	19	47	.69	87	.07	3	1.37	.03	.08	1	1
L4+00W 13+00N	2	58	10	124	.3	47	12	740	3.36	3	5	ND	3	32	1	2	2	68	.40	.065	22	56	.76	128	.05	3	1.76	.03	.09	1	1
L4+00W 12+75N	3	72	13	118	.5	50	14	543	4.33	23	5	ND	4	28	1	3	2	96	.33	.129	13	54	.81	98	.07	2	1.78	.07	.10	1	3
L4+00W 12+50N	2	45	7	115	.2	36	10	343	3.59	14	5	ND	3	37	1	3	2	80	.34	.114	14	42	.69	99	.06	3	1.34	.03	.08	1	2
L4+00W 12+25N	2	33	6	77	.1	30	8	369	2.67	9	5	ND	3	30	1	2	2	61	.31	.058	14	42	.69	83	.06	3	1.36	.03	.07	1	1
L4+00W 12+00N	1	28	10	89	.1	37	9	316	2.77	5	5	ND	5	22	1	2	2	55	.28	.040	17	50	.89	73	.09	2	1.44	.03	.08	1	2
L4+00W 11+75N	1	23	8	90	.1	31	7	244	2.37	2	5	ND	4	21	1	4	2	48	.25	.036	18	43	.70	66	.07	2	1.31	.03	.07	1	4
L4+00W 11+50N	2	33	9	127	.3	37	9	264	3.31	11	5	ND	5	26	1	3	2	67	.32	.071	17	51	.73	77	.06	3	1.51	.03	.06	1	1
L4+00W 11+25N	1	46	11	92	.2	45	11	502	3.56	8	5	ND	6	23	1	5	3	65	.30	.068	16	61	.90	80	.08	2	1.63	.03	.10	1	3
L4+00W 11+00N	2	42	9	103	.4	33	10	385	3.34	6	5	ND	3	24	1	8	2	77	.31	.077	14	48	.68	95	.05	3	1.46	.03	.09	1	280
L4+00W 10+75N	2	51	11	115	.6	37	10	311	4.13	13	5	ND	3	27	1	8	2	87	.34	.093	17	52	.75	88	.05	2	1.87	.03	.09	1	220
L4+00W 10+50N	1	53	10	190	.3	33	12	339	4.60	17	5	ND	4	28	1	5	2	97	.30	.133	16	39	.65	146	.06	4	1.65	.03	.10	1	2
L4+00W 10+25N	2	70	8	127	.1	30	13	381	4.60	22	5	ND	3	32	1	6	2	110	.36	.137	12	37	.65	127	.06	5	1.53	.03	.10	1	6
L4+00W 10+00N	1	46	7	153	.2	40	12	385	4.09	17	5	ND	4	27	1	4	2	90	.37	.162	13	61	.75	123	.07	3	1.59	.03	.08	1	3
L4+00W 9+75N	1	40	6	132	.1	27	10	303	3.33	13	5	ND	3	30	1	7	2	76	.31	.084	12	36	.51	96	.06	2	1.17	.03	.09	1	2
L4+00W 9+50N	1	58	7	92	.2	29	14	521	3.75	16	5	ND	3	32	1	3	2	87	.38	.049	13	37	.64	87	.06	3	1.37	.03	.12	1	5
L4+00W 8+75N	2	62	6	114	.1	33	17	599	4.57	23	5	ND	3	32	1	3	2	101	.44	.089	19	44	.80	96	.09	4	1.47	.03	.15	1	2
L4+00W 8+50N	1	49	7	102	.2	34	12	414	3.42	10	5	ND	2	31	1	2	2	72	.44	.066	18	43	.66	102	.06	3	1.41	.03	.09	1	1
L4+00W 8+25N	2	63	12	80	.1	35	14	500	4.18	29	5	ND	3	30	1	2	2	86	.38	.076	12	47	.74	80	.07	3	1.40	.03	.11	1	5
L4+00W 7+75N	1	79	11	89	.1	41	16	626	4.25	19	5	ND	3	32	1	4	2	88	.43	.080	17	54	.81	83	.08	4	1.63	.03	.10	1	28
STD C/AU-0.5	20	59	47	137	7.2	71	29	1105	3.96	38	17	7	35	49	18	16	21	49	.48	.164	37	58	.88	183	.08	14	1.73	.09	.13	12	480

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-2400

PAGE 21

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	F %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	P PPM	Al %	Na %	K %	N PPM	Au2 PPM
L4+00W 7+50N	1	62	6	108	.2	36	14	780	3.51	14	5	ND	2	29	1	2	2	77	.32	.049	16	52	.68	108	.05	2	1.66	.02	.08	1	2
L4+00W 7+25N	1	60	9	102	.3	35	12	478	3.65	12	5	ND	2	27	1	2	2	79	.34	.060	15	53	.72	107	.06	2	1.72	.03	.08	1	1
L4+00W 7+00N	2	62	12	129	.4	42	16	1043	4.02	15	5	ND	2	26	1	7	2	83	.32	.076	17	67	.78	137	.05	2	2.04	.03	.10	2	2
L4+00W 6+75N	1	58	9	95	.6	38	13	549	3.55	16	5	ND	2	26	1	3	2	75	.36	.067	15	54	.69	113	.05	2	1.82	.03	.10	1	1
L4+00W 6+50N	1	71	9	113	.3	37	20	337	5.29	11	5	ND	2	37	1	3	2	106	.38	.197	14	68	.67	103	.06	2	1.64	.02	.07	1	5
L4+00W 6+25N	1	28	7	150	.2	28	10	307	3.32	14	5	ND	3	23	1	2	2	68	.33	.097	11	50	.60	73	.06	2	1.55	.03	.06	1	2
L4+00W 6+00N	2	52	9	158	.1	27	13	434	3.65	18	5	ND	3	21	1	4	2	79	.33	.050	14	45	.73	84	.06	2	1.56	.03	.07	1	190
L4+00W 5+75N	1	40	2	99	.1	34	11	307	3.66	14	5	ND	3	24	1	3	2	72	.28	.088	14	49	.72	76	.07	2	1.54	.03	.06	1	1
L4+00W 5+50N	1	32	7	95	.1	35	10	281	3.87	12	5	ND	4	27	1	2	2	75	.43	.170	17	57	.70	89	.07	2	1.62	.03	.07	1	2
L4+00W 5+25N	1	33	6	91	.2	25	10	288	3.55	29	6	ND	3	26	1	2	2	73	.26	.108	14	42	.49	86	.05	2	1.26	.03	.06	1	1
L4+00W 5+00N	1	25	6	98	.2	27	9	345	3.16	11	6	ND	3	23	1	2	2	64	.29	.124	14	39	.57	99	.06	2	1.35	.02	.07	1	1
L4+00W 4+75N	1	40	7	77	.3	29	9	407	3.25	13	5	ND	3	26	1	2	2	67	.26	.049	15	50	.73	82	.07	2	1.40	.03	.08	1	1
L4+00W 4+50N	1	36	6	72	.1	28	8	328	3.45	17	5	ND	2	25	1	3	2	70	.23	.071	12	46	.63	91	.05	2	1.30	.02	.07	1	3
L4+00W 4+25N	1	48	7	89	.2	34	10	379	3.62	19	5	ND	2	33	1	2	2	76	.28	.061	16	56	.78	111	.05	2	1.62	.03	.08	1	4
L4+00W 4+00N	1	43	7	87	.1	33	11	359	3.40	13	5	ND	3	30	1	2	2	67	.29	.065	17	53	.76	93	.06	4	1.53	.03	.07	1	2
L4+00W 3+75N	2	46	9	107	.2	33	10	326	3.85	14	6	ND	3	33	1	4	2	84	.24	.049	16	57	.78	93	.06	2	1.75	.03	.07	1	1
L4+00W 3+50N	2	47	10	101	.3	32	10	316	3.59	14	5	ND	3	42	1	3	2	77	.29	.080	15	52	.73	110	.06	2	1.47	.03	.06	1	1
L4+00W 3+25N	1	22	8	96	.2	18	8	404	2.44	7	5	ND	3	32	1	2	2	57	.27	.079	13	33	.38	110	.06	2	.95	.02	.07	1	19
L4+00W 3+00N	1	25	7	95	.1	22	8	280	2.77	13	5	ND	3	24	1	4	2	58	.27	.093	15	39	.50	90	.06	2	1.02	.02	.06	1	1
L4+00W 2+75N	1	14	7	94	.1	17	8	614	2.21	6	5	ND	2	23	1	2	2	50	.28	.050	14	37	.40	137	.05	2	1.00	.02	.07	1	2
L4+00W 2+50N	2	165	15	203	1.0	81	19	2588	5.35	24	5	ND	3	63	2	2	2	83	1.03	.101	25	87	.76	317	.05	3	2.73	.05	.13	2	1
L4+00W 2+25N	1	37	9	129	.3	36	12	709	3.30	16	5	ND	3	30	1	4	2	62	.38	.056	13	50	.61	134	.06	2	1.48	.03	.07	1	1
L4+00W 2+00N	1	15	8	82	.2	20	6	195	2.56	7	5	ND	4	20	1	2	2	48	.33	.082	16	36	.42	62	.06	2	1.03	.02	.07	1	1
L4+00W 1+75N	1	15	5	132	.1	25	8	273	2.66	9	5	ND	4	19	1	4	2	50	.27	.112	14	39	.50	106	.06	2	1.18	.02	.05	1	1
L4+00W 1+50N	1	18	8	86	.1	29	7	223	2.70	9	5	ND	4	18	1	2	3	49	.26	.077	18	42	.50	72	.07	4	1.22	.02	.07	1	97
L4+00W 1+25N	1	35	11	145	.3	33	13	629	3.89	12	5	ND	2	27	1	2	2	74	.36	.174	10	52	.56	128	.05	2	1.38	.03	.08	1	2
L4+00W 1+00N	2	33	8	68	.1	34	9	373	2.95	14	5	ND	6	21	1	3	2	51	.29	.065	17	44	.68	60	.07	2	1.20	.03	.08	1	2
L4+00W 0+75N	1	29	9	76	.2	35	10	466	2.69	4	7	ND	4	23	1	2	2	50	.37	.035	17	42	.62	82	.08	2	1.21	.03	.09	1	1
L4+00W 0+50N	1	34	11	80	.2	39	10	430	2.68	7	5	ND	4	23	1	4	2	51	.37	.035	23	45	.59	91	.07	2	1.32	.03	.09	2	6
L4+00W 0+25N	1	35	17	89	.3	46	11	556	3.13	11	6	ND	5	28	1	4	2	53	.46	.057	21	51	.77	92	.09	2	1.53	.03	.17	1	1
L4+00W 0+00	2	33	9	87	.3	44	11	463	3.02	10	5	ND	6	24	1	4	2	56	.32	.030	21	52	.70	85	.09	2	1.32	.03	.09	1	1
L3+00W 15+00N	2	30	9	119	.1	42	14	563	3.95	15	5	ND	2	24	1	2	2	76	.36	.074	13	65	.91	128	.05	2	1.87	.03	.07	1	4
L3+00W 14+75N	3	41	14	100	.2	54	16	889	3.42	13	6	ND	5	30	1	2	2	59	.50	.076	18	58	.83	97	.07	2	1.40	.04	.06	1	7
L3+00W 14+50N	2	41	9	174	.3	32	13	858	3.12	17	5	ND	2	33	1	6	2	65	.55	.148	9	47	.77	139	.05	2	1.34	.03	.09	1	1
L3+00W 14+00N	2	160	12	122	1.0	40	15	395	2.91	10	5	ND	1	38	1	2	2	79	.54	.111	18	68	.92	196	.03	2	2.37	.04	.11	1	3
L3+00W 13+75N	3	209	10	101	.5	38	40	884	4.27	18	5	ND	2	30	1	2	2	109	.38	.067	13	72	.99	197	.04	3	2.36	.04	.11	1	5
STD C/AU-0.5	22	59	39	139	7.3	71	29	1114	3.96	41	15	7	36	50	18	16	21	70	.48	.108	39	60	.88	187	.09	37	1.73	.09	.13	13	500

E & B EXPLORATION PROJECT - 5055 FILE # 86-2403

PAGE 7

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Pi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	Au#	
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPM	
L3+00W 13+50W	1	32	7	72	.1	13	7	378	2.44	9	5	ND	2	20	1	3	3	66	.29	.083	15	30	.36	153	.05	2	.99	.02	.06	1	1
L3+00W 13+25W	1	17	4	29	.1	5	3	67	1.23	2	5	ND	1	17	1	2	2	42	.16	.026	12	14	.14	122	.03	2	.77	.02	.04	1	1
L3+00W 12+75W	1	58	10	86	.3	27	8	314	3.16	12	5	ND	1	29	1	4	2	77	.36	.039	16	50	.66	140	.04	2	1.81	.03	.08	1	41
L3+00W 12+50W	2	59	12	125	.7	36	17	1054	3.73	18	5	ND	1	36	1	2	2	75	.51	.108	19	54	.73	202	.03	3	2.05	.03	.10	1	4
L3+00W 12+25W	1	18	8	57	.1	16	6	247	1.83	2	5	ND	2	21	1	2	2	47	.24	.027	15	29	.44	81	.04	2	1.23	.02	.05	1	1
L3+00W 12+00W	1	11	6	42	.1	9	3	203	1.43	5	5	ND	2	13	1	2	2	45	.17	.043	15	23	.20	60	.05	2	.78	.02	.04	1	5
L3+00W 11+75W	1	11	7	42	.2	13	4	125	1.42	2	5	ND	2	16	1	2	2	34	.19	.025	17	24	.39	55	.05	2	.95	.02	.05	1	2
L3+00W 11+50W	1	19	7	65	.1	18	6	249	2.42	5	5	ND	3	22	1	2	2	51	.24	.091	17	33	.44	75	.05	2	1.09	.02	.07	1	5
L3+00W 11+25W	1	25	8	80	.1	26	10	426	2.54	8	5	ND	2	29	1	5	2	51	.44	.057	16	36	.55	101	.04	2	1.29	.03	.07	1	1
L3+00W 11+00W	1	24	10	74	.3	25	8	218	2.81	11	5	ND	3	27	1	3	2	56	.19	.045	16	38	.50	82	.04	2	1.33	.02	.06	1	1
L3+00W 10+75W	1	21	3	66	.1	17	6	174	2.28	8	5	ND	2	30	1	3	2	61	.25	.053	12	31	.31	102	.05	2	.82	.02	.06	1	1
L3+00W 10+50W	2	42	15	115	.4	37	16	1164	3.17	11	5	ND	2	40	1	3	2	65	.56	.049	16	52	.55	151	.04	2	1.63	.03	.08	1	1
L3+00W 10+25W	1	58	14	90	.5	45	13	525	3.68	15	7	ND	3	46	1	2	2	75	.72	.055	22	57	.70	136	.05	3	1.89	.04	.08	1	1
L3+00W 9+00W	1	41	9	93	.3	32	9	320	2.74	8	5	ND	3	32	1	2	2	56	.40	.047	18	46	.67	121	.05	2	1.62	.03	.07	1	3
L3+00W 8+75W	3	116	21	152	.6	64	21	1229	5.08	22	8	ND	3	50	2	2	2	96	.66	.070	39	82	.90	231	.04	11	2.57	.04	.14	1	5
L3+00W 8+50W	2	48	9	94	.4	28	9	289	2.76	10	5	ND	2	31	1	2	2	63	.31	.044	20	39	.46	141	.03	2	1.39	.03	.08	1	1
L3+00W 8+25W	2	49	13	129	.5	39	11	553	3.21	13	5	ND	3	34	1	2	2	63	.44	.055	19	54	.75	151	.05	2	1.82	.03	.10	2	2
L3+00W 8+00W	1	22	10	86	.1	27	7	266	2.58	12	5	ND	3	21	1	2	2	50	.25	.031	20	41	.67	85	.05	2	1.33	.02	.07	1	13
L3+00W 7+75W	1	30	11	91	.2	34	8	304	3.13	9	5	ND	3	27	1	2	2	55	.28	.055	20	50	.83	94	.06	2	1.59	.03	.08	1	1
L3+00W 7+50W	2	39	8	117	.4	30	9	478	2.81	12	5	ND	2	30	1	2	2	64	.31	.043	15	44	.62	124	.04	2	1.59	.03	.08	1	1
L3+00W 7+25W	3	109	18	168	1.0	63	16	912	4.99	31	6	ND	3	54	2	2	2	106	.54	.084	18	67	.82	238	.04	4	2.58	.04	.15	2	2
L3+00W 7+00W	3	139	13	193	1.3	74	17	1054	5.25	35	6	ND	2	73	2	2	2	114	.92	.106	33	73	.84	287	.02	8	2.85	.05	.17	1	2
L3+00W 6+75W	1	30	12	76	.1	15	6	168	3.09	26	5	ND	2	26	1	4	2	82	.20	.084	13	29	.27	84	.04	2	.87	.02	.07	1	1
L3+00W 6+50W	1	68	15	101	.4	111	25	1021	4.84	9	5	ND	2	37	1	2	2	161	.94	.100	13	114	3.84	140	.21	10	2.90	.06	.07	1	1
L3+00W 6+25W	2	42	11	106	.2	23	8	219	3.70	24	5	ND	2	28	1	3	2	104	.32	.161	11	34	.40	107	.06	3	1.09	.03	.08	1	3
L3+00W 6+00W	1	16	10	149	.2	11	8	565	2.26	6	5	ND	2	24	1	2	3	61	.25	.057	12	27	.20	184	.06	3	.74	.02	.08	1	1
L3+00W 5+50W	1	29	7	62	.1	9	5	241	2.19	7	5	ND	2	34	1	5	2	75	.26	.052	10	18	.17	92	.05	3	.70	.02	.09	1	1
L3+00W 5+25W	1	23	7	83	.1	14	7	431	2.43	7	5	ND	2	25	1	3	2	66	.32	.080	13	25	.36	113	.06	2	.92	.02	.08	1	2
L3+00W 5+00W	1	20	9	71	.1	12	8	533	2.51	4	5	ND	1	20	1	5	2	75	.31	.087	10	28	.34	90	.08	2	.90	.02	.10	1	1
L3+00W 4+75W	1	18	7	64	.1	9	5	169	2.13	8	5	ND	1	20	1	2	2	63	.19	.073	9	20	.19	76	.04	2	.93	.02	.06	1	1
L3+00W 4+50W	1	38	6	82	.1	22	9	435	3.14	17	5	ND	2	25	1	5	3	72	.29	.100	11	29	.48	112	.05	2	1.09	.02	.11	1	2
L3+00W 4+25W	1	36	9	107	.1	17	10	853	3.40	21	6	ND	2	29	1	2	2	81	.31	.166	13	27	.34	214	.05	3	1.02	.02	.14	1	1
L3+00W 4+00W	1	29	7	122	.2	18	10	314	3.81	16	5	ND	2	25	1	2	2	89	.31	.137	10	34	.43	150	.05	2	1.46	.02	.10	1	8
L3+00W 3+75W	1	37	12	119	.6	24	11	280	4.38	23	5	ND	2	21	1	8	3	86	.24	.083	12	44	.50	109	.04	2	1.76	.02	.08	2	1
L3+00W 3+50W	1	13	7	51	.1	8	4	277	1.53	9	5	ND	1	26	1	2	2	47	.41	.040	11	20	.15	93	.06	2	.47	.02	.08	1	1
L3+00W 3+25W	1	16	5	97	.2	15	6	507	2.24	12	5	ND	2	22	1	2	2	52	.30	.083	12	29	.35	98	.06	2	.89	.02	.08	1	2
STD C/AU-0.5	22	58	37	136	7.0	69	28	1096	3.97	42	17	7	34	48	18	15	18	68	.48	.103	36	59	.89	182	.08	38	1.73	.09	.13	13	490

E & B EXPLORATION PROJECT 5055 FILE # 86-2403

PAGE 4

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Tl	F	Al	Na	I	K	Aut
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM	PPM
L3+00M 3+00M	1	10	6	81	.4	8	5	1492	1.28	5	5	ND	1	17	1	2	2	34	.16	.047	12	17	.15	139	.03	4	.55	.01	.07	1	2
L3+00M 2+75M	1	42	9	95	.1	25	11	673	3.77	44	5	ND	1	33	1	2	2	81	.25	.091	13	38	.48	118	.04	5	.99	.02	.08	1	7
L3+00M 2+50M	2	24	7	64	.2	13	5	295	2.30	29	5	ND	1	26	1	2	2	62	.18	.053	13	23	.15	82	.03	3	.53	.02	.06	1	1
L3+00M 2+25M	1	20	5	60	.2	13	6	212	2.40	21	5	ND	2	21	1	2	2	54	.13	.067	12	25	.23	57	.03	2	.82	.02	.06	1	1
L3+00M 2+00M	1	15	8	50	.1	8	4	297	1.75	18	5	ND	2	25	1	2	2	50	.19	.055	13	17	.12	104	.04	3	.46	.01	.06	1	3
L3+00M 1+75M	2	53	7	91	.2	21	10	393	3.78	31	5	ND	2	43	1	2	2	91	.24	.117	11	33	.38	108	.03	5	.97	.02	.07	1	13
L3+00M 1+50M	1	34	10	71	.2	17	10	1506	2.91	9	5	ND	1	29	1	2	2	74	.41	.056	10	30	.32	183	.04	5	.88	.02	.07	1	11
L3+00M 1+25M	1	16	7	34	.3	12	5	593	1.46	3	5	ND	2	22	1	2	3	39	.52	.042	8	22	.11	82	.05	2	.46	.02	.07	1	4
L3+00M 1+00M	1	20	8	54	.1	22	7	231	2.60	6	5	ND	3	24	1	2	2	57	.32	.055	11	32	.41	81	.05	3	.95	.02	.06	1	6
L7+50E 20+00M	1	79	7	159	.4	49	14	619	3.39	13	5	ND	3	30	1	2	2	77	.47	.051	15	77	1.10	109	.08	3	2.11	.04	.10	1	1
L7+50E 19+75M	1	42	7	96	.1	30	10	389	2.62	3	5	ND	4	29	1	2	2	66	.44	.040	16	58	.93	83	.08	4	1.66	.03	.07	1	5
L7+50E 19+50M	1	42	12	113	.2	36	12	474	2.87	9	5	ND	3	30	1	5	2	66	.45	.039	13	60	1.02	85	.08	4	1.71	.03	.08	1	1
L7+50E 18+50M	1	34	8	102	.1	34	10	348	2.46	8	5	ND	3	26	1	2	2	58	.47	.062	13	46	.90	79	.09	2	1.44	.03	.07	1	36
L7+50E 18+00M	2	83	9	87	.1	47	13	324	3.32	26	5	ND	5	32	1	2	2	69	.57	.076	19	59	.89	77	.08	5	1.56	.04	.09	1	21
L7+50E 17+50M	3	65	9	109	.6	50	14	455	3.42	25	5	ND	5	28	1	2	2	71	.51	.072	15	64	1.10	101	.08	3	1.77	.04	.10	1	12
L7+50E 17+25M	2	65	8	192	.4	54	12	609	3.26	13	5	ND	4	34	1	2	2	70	.55	.062	15	68	1.10	126	.08	5	2.06	.04	.09	2	18
L7+50E 17+00M	2	58	9	124	.3	50	11	384	3.06	13	5	ND	3	34	1	2	2	66	.57	.062	17	69	.97	104	.07	4	1.90	.04	.08	1	6
L7+50E 16+75M	1	34	9	159	.3	36	11	223	3.64	10	5	ND	4	17	1	2	2	81	.33	.114	10	65	.80	104	.06	3	2.00	.03	.06	1	25
L7+50E 16+50M	2	36	8	137	.1	42	13	235	3.91	15	5	ND	4	15	1	2	2	78	.25	.107	15	69	.81	82	.07	2	2.04	.03	.06	1	4
L7+50E 16+25M	1	56	8	224	.3	59	18	327	5.23	22	5	ND	3	20	1	2	2	104	.31	.097	11	95	1.19	118	.07	7	2.54	.04	.06	1	2
L7+50E 16+00M	2	48	8	101	.2	41	12	330	3.60	18	5	ND	3	17	1	3	2	87	.27	.038	10	74	1.00	90	.06	3	2.21	.03	.06	1	8
L7+50E 15+75M	2	60	9	105	.1	58	14	370	3.92	18	5	ND	3	22	1	2	2	94	.39	.040	10	92	1.23	85	.08	3	2.28	.04	.08	1	2
L7+50E 15+50M	2	44	11	85	.2	41	10	336	3.27	21	5	ND	2	23	1	3	2	83	.37	.035	10	71	1.11	99	.06	3	1.88	.03	.07	1	14
L7+50E 15+25M	2	71	13	122	.3	49	16	596	4.02	51	5	ND	3	22	1	2	2	86	.33	.060	10	82	1.19	108	.05	5	2.22	.03	.08	1	10
L7+50E 15+00M	2	65	9	91	.3	53	11	375	3.18	26	5	ND	4	27	1	5	2	72	.47	.030	16	80	1.20	94	.09	3	1.89	.04	.07	1	7
L10+00E 19+50M	1	44	6	116	.3	33	10	278	2.71	10	5	ND	3	29	1	2	2	64	.49	.030	11	53	.72	71	.07	2	1.59	.03	.07	1	6
L10+00E 19+25M	2	43	9	147	.1	38	11	374	2.81	7	5	ND	3	22	1	2	2	65	.37	.054	11	58	.81	80	.07	2	1.72	.03	.06	1	1
L10+00E 19+00M	2	29	8	93	.1	27	7	221	2.58	11	5	ND	2	18	1	3	3	67	.32	.041	11	51	.68	72	.06	2	1.58	.03	.06	1	1
L10+00E 18+75M	1	28	7	93	.1	25	9	321	2.54	8	5	ND	3	22	1	4	2	63	.36	.051	12	47	.71	78	.07	2	1.45	.03	.07	1	4
L10+00E 18+50M	2	44	6	91	.2	41	10	356	2.66	7	6	ND	4	27	1	2	2	62	.47	.044	15	62	.93	83	.09	2	1.72	.04	.08	1	6
L10+00E 18+25M	2	32	11	90	.1	33	10	372	2.69	14	5	ND	4	24	1	3	2	62	.43	.060	12	50	.81	61	.09	3	1.31	.03	.07	1	9
L10+00E 18+00M	3	37	8	164	.2	36	10	223	4.09	17	5	ND	3	18	1	2	2	86	.31	.135	10	56	.69	89	.06	3	1.99	.03	.06	1	4
L10+00E 17+75M	1	36	6	107	.1	30	9	301	2.75	8	5	ND	3	22	1	2	2	69	.38	.068	10	47	.76	98	.07	2	1.65	.03	.06	1	8
L10+00E 17+50M	2	35	10	129	.1	35	12	295	2.92	10	5	ND	3	22	1	5	2	75	.34	.034	10	48	.69	97	.07	3	1.84	.03	.06	1	4
L10+00E 17+25M	2	76	9	127	.2	51	15	634	3.20	18	5	ND	3	29	1	2	2	72	.43	.039	16	63	.81	119	.06	3	2.10	.03	.09	1	6
L10+00E 17+00M	2	25	13	224	.2	30	9	260	3.84	13	5	ND	3	19	1	2	2	90	.32	.214	10	51	.66	138	.06	4	1.84	.03	.05	1	2
STD C/AU-0.5	22	59	38	138	7.2	71	29	1109	3.96	37	19	7	36	49	18	15	22	69	.48	.105	37	58	.88	185	.09	36	1.73	.09	.13	12	500

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-2403

PAGE 5

SAMPLE#	Hg PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Er PPM	Mg %	Ba %	Ti %	F PPM	Al %	Na %	K %	W PPM	Agf PPM
L10+00E 16+75N	2	26	8	99	.2	24	8	319	2.95	17	5	ND	2	21	1	2	2	76	.37	.099	13	41	.56	77	.07	3	1.32	.02	.09	1	1
L10+00E 16+50N	2	63	18	115	.2	47	10	362	3.19	15	5	ND	3	27	1	2	2	68	.47	.049	22	62	.99	95	.07	3	1.97	.04	.09	1	2
L10+00E 16+25N	2	32	11	132	.1	25	9	205	3.37	15	5	ND	3	20	1	2	2	77	.35	.148	16	44	.60	84	.07	3	1.57	.02	.06	1	1
L10+00E 16+00N	2	86	13	126	.1	64	17	494	3.93	20	5	ND	4	32	1	2	2	82	.48	.039	17	83	1.27	84	.10	6	2.05	.04	.08	1	4
L10+00E 15+75N	1	41	7	151	.1	34	11	282	2.94	13	5	ND	3	22	1	2	2	71	.37	.040	13	47	.76	83	.08	4	1.60	.02	.08	1	5
L10+00E 15+50N	2	92	13	175	.2	69	20	732	4.18	23	5	ND	3	28	1	2	2	94	.48	.047	20	90	1.22	108	.07	4	2.44	.04	.09	1	1
L10+00E 15+25N	2	42	10	194	.2	38	13	314	4.91	23	5	ND	4	24	1	2	2	102	.43	.287	14	68	.86	108	.08	5	2.35	.02	.08	1	1
L10+00E 15+00N	2	102	16	112	.3	59	16	556	3.97	23	5	ND	3	29	1	2	2	88	.55	.038	19	79	1.20	90	.09	4	2.16	.04	.09	2	8
L20+60E 14+00N	2	31	11	183	.1	32	11	338	3.43	16	5	ND	2	20	1	2	2	81	.35	.125	12	52	.81	77	.08	4	1.64	.02	.08	1	1
L20+60E 13+75N	3	32	8	242	.1	41	15	532	3.29	15	5	ND	3	20	1	3	2	83	.37	.080	13	57	.79	117	.08	3	1.81	.03	.06	2	1
L20+60E 13+50N	5	64	8	197	.2	45	15	324	4.38	56	5	ND	2	22	1	3	2	111	.41	.037	10	70	1.03	75	.07	6	1.92	.02	.06	1	7
L20+60E 13+00N	2	45	13	197	.3	48	16	327	4.97	43	5	ND	3	18	1	3	2	92	.35	.099	16	118	1.17	88	.07	8	2.23	.03	.07	2	13
L20+60E 12+75N	1	35	7	149	.1	24	12	303	3.24	10	5	ND	2	15	1	2	2	80	.31	.084	7	54	.63	79	.07	3	1.66	.02	.06	1	1
L20+60E 12+50N	2	52	15	327	.7	30	16	311	4.68	47	5	ND	2	23	2	2	3	99	.42	.216	15	59	.63	119	.05	4	2.51	.03	.09	1	2
L20+60E 12+25N	1	30	15	500	.3	44	17	461	4.12	81	5	ND	3	26	1	2	2	82	.41	.188	12	51	.69	112	.09	5	2.51	.03	.07	1	134
L20+60E 12+00N	2	37	11	272	.1	30	14	651	3.26	32	5	ND	2	20	1	5	2	70	.33	.079	11	43	.66	111	.07	3	1.83	.03	.06	1	52
L20+60E 11+75N	2	74	20	110	.3	42	15	406	3.75	126	5	ND	3	20	1	2	2	77	.34	.049	15	62	1.03	69	.07	7	1.72	.03	.08	1	55
L20+60E 11+50N	2	33	6	124	.1	31	12	276	2.84	18	5	ND	3	17	1	2	2	63	.30	.035	12	41	.72	90	.07	3	1.68	.02	.08	1	3
L20+60E 11+25N	1	41	9	90	.1	30	12	282	3.09	13	5	ND	3	19	1	2	2	68	.28	.041	13	41	.72	75	.08	3	1.46	.03	.08	1	1
L20+60E 11+00N	2	35	7	74	.1	27	12	395	2.94	13	5	ND	3	22	1	2	2	68	.40	.047	10	45	.71	87	.07	4	1.37	.03	.08	2	2
L20+60E 10+75N	2	47	8	61	.1	26	11	333	3.22	19	5	ND	3	19	1	2	2	74	.34	.064	14	46	.72	67	.07	2	1.36	.03	.10	1	4
L20+60E 10+50N	2	38	10	67	.1	29	11	259	3.02	12	5	ND	4	16	1	2	2	66	.27	.045	13	45	.73	54	.09	3	1.35	.03	.09	1	10
L20+60E 10+25N	2	58	13	152	.1	39	16	793	3.87	18	5	ND	5	20	1	2	2	76	.31	.120	13	60	.79	120	.07	6	1.92	.03	.13	1	5
L20+60E 9+00N	2	68	11	91	.1	44	17	929	4.32	22	5	ND	3	25	1	2	2	78	.47	.060	17	63	.98	123	.07	4	2.09	.04	.11	1	4
L20+60E 8+75N	1	22	9	106	.4	16	10	545	2.55	6	5	ND	2	15	1	2	2	54	.26	.079	14	41	.53	106	.06	2	1.29	.02	.09	1	2
L20+60E 8+50N	3	802	22	223	2.5	117	24	1259	8.97	37	5	ND	6	49	3	2	2	120	.75	.095	27	122	1.49	542	.06	15	4.34	.06	.32	1	6
L20+60E 7+75N	2	257	13	85	.1	39	19	795	5.60	21	5	ND	4	47	1	2	2	116	.66	.113	20	62	1.36	158	.10	9	1.96	.04	.11	1	8
L20+60E 7+50N	2	190	12	91	.2	33	18	435	5.06	12	5	ND	3	42	1	2	3	119	.48	.072	10	56	1.13	168	.10	4	1.95	.04	.08	1	1
L20+60E 7+25N	3	204	9	68	.2	23	15	334	5.36	14	5	ND	3	37	1	8	2	113	.40	.069	13	37	.77	162	.05	5	1.78	.03	.07	2	2
L20+60E 7+00N	2	167	10	67	.2	25	15	361	4.38	15	5	ND	3	29	1	3	2	86	.30	.046	16	40	.75	150	.04	9	1.55	.03	.08	1	3
L20+60E 6+75N	2	51	10	80	.2	20	11	250	4.17	7	5	ND	3	23	1	2	2	91	.26	.081	13	36	.51	102	.05	4	1.44	.02	.06	1	1
L20+60E 6+50N	1	81	8	67	.2	29	12	401	3.82	13	5	ND	3	32	1	2	2	75	.39	.069	20	43	.80	113	.06	2	1.47	.03	.08	1	1
L20+60E 6+25N	2	78	11	84	.1	36	15	631	4.16	17	5	ND	4	40	1	2	2	78	.41	.077	20	50	.94	134	.07	2	1.63	.03	.10	1	2
L20+60E 6+00N	1	46	10	86	.2	27	10	377	3.44	6	5	ND	3	33	1	2	2	71	.37	.050	18	39	.69	148	.06	4	1.36	.03	.08	1	2
L21+90E 14+00N	3	170	13	313	1.0	75	23	1115	4.91	35	5	ND	3	77	5	2	2	88	1.66	.058	8	84	1.04	87	.05	6	2.20	.06	.08	1	1
L21+90E 13+75N	3	84	14	108	.5	54	27	914	4.93	22	5	ND	3	75	2	2	2	101	2.07	.065	10	92	1.67	71	.08	15	2.24	.06	.09	2	1
STD C/AU-0.5	21	57	40	131	6.9	67	27	1055	3.94	37	15	7	34	47	17	16	20	66	.48	.100	35	54	.88	175	.08	34	1.73	.09	.14	12	490

E & B EXPLORATION PROJECT - 5055 FILE # 86-2407

PAGE 5

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	F %	La PPM	Er PPM	Mg %	Ba PPM	Ti %	E PPM	Al %	Na %	K %	W PPM	AsI PPB
L21+90E 13+50N	4	136	12	202	.2	73	27	793	5.18	39	5	ND	4	33	1	2	2	114	.60	.039	19	82	1.41	77	.08	2	1.99	.05	.08	1	10
L21+90E 13+25N	4	51	12	229	.1	47	14	310	4.68	34	5	ND	1	33	2	2	2	133	.54	.037	16	81	.93	79	.05	5	1.88	.04	.08	2	5
L21+90E 13+00N	3	55	12	166	.2	32	15	405	3.86	27	5	ND	1	38	1	2	2	113	.77	.048	12	71	.66	57	.04	2	2.04	.04	.03	1	3
L21+90E 12+75N	1	29	4	109	.1	28	12	332	3.11	10	5	ND	2	16	1	5	2	79	.30	.088	9	56	.62	71	.06	7	1.34	.03	.07	1	490
L21+90E 12+25N	2	29	10	200	.2	32	18	1088	3.59	12	5	ND	2	25	1	3	2	95	.52	.120	11	62	.71	124	.06	4	1.57	.02	.10	1	2
L21+90E 12+00N	1	18	9	122	.1	17	10	1048	2.20	22	5	ND	1	17	1	2	2	61	.34	.059	12	32	.38	89	.07	2	1.06	.03	.07	1	102
L21+90E 11+75N	1	30	8	171	.2	27	17	2059	4.05	37	6	ND	2	29	1	2	2	103	.82	.141	9	52	1.22	135	.13	39	1.80	.08	.11	1	5
L21+90E 11+50N	1	71	102	336	.7	60	19	935	5.26	1957	5	ND	3	29	2	19	2	82	.41	.078	22	67	1.06	131	.03	8	2.46	.04	.09	1	55
L21+90E 11+00N	1	17	10	89	.1	20	10	421	2.06	36	5	ND	2	19	1	2	2	48	.34	.059	10	31	.47	97	.06	3	1.01	.03	.10	1	2
L21+90E 10+75N	2	36	9	123	.1	36	14	799	3.03	13	5	ND	2	35	1	2	2	72	.58	.071	12	43	.60	160	.07	4	1.52	.03	.14	1	2
L21+90E 10+50N	2	67	14	135	.2	40	19	1043	3.90	16	5	ND	2	21	1	5	2	79	.38	.101	12	50	.80	152	.06	4	1.62	.03	.11	1	1
L21+90E 10+25N	1	46	10	124	.1	31	15	500	3.74	17	5	ND	2	20	1	6	2	74	.35	.150	11	49	.74	105	.05	3	1.50	.03	.13	1	1
L21+90E 10+00N	8	69	13	96	.5	28	22	2494	4.60	32	5	ND	1	73	2	2	2	96	1.77	.090	9	64	.95	136	.04	16	1.68	.06	.10	1	1
L21+90E 9+75N	8	63	11	64	1.0	20	13	3242	2.59	38	5	ND	1	127	2	3	2	63	2.94	.162	9	33	.36	157	.02	3	1.14	.05	.09	1	3
L21+90E 9+50N	3	32	8	78	.1	26	12	584	3.19	15	5	ND	2	35	1	2	2	68	.63	.030	17	46	.63	74	.06	3	1.41	.03	.09	1	1
L21+90E 9+25N	2	78	11	98	.3	49	16	1453	3.63	19	5	ND	3	49	1	2	2	67	.95	.098	20	61	.93	177	.06	4	1.91	.04	.12	1	3
L21+90E 9+00N	2	114	16	132	.2	34	19	1897	4.24	23	5	ND	2	31	1	2	2	75	.55	.089	19	48	.74	248	.05	5	1.67	.04	.11	1	1
L21+90E 8+75N	2	183	19	177	.6	42	24	1508	6.33	20	5	ND	2	47	2	2	2	102	.87	.125	29	56	.78	332	.04	12	2.06	.05	.13	1	3
L21+90E 8+50N	1	155	14	107	.2	43	19	755	5.09	21	5	ND	3	40	1	2	2	85	.57	.081	22	59	1.05	220	.06	7	1.90	.04	.13	1	4
L21+90E 8+25N	2	175	13	136	.3	39	20	700	4.91	14	5	ND	3	42	1	2	2	88	.69	.077	19	52	.87	243	.05	7	1.80	.04	.11	1	2
L21+90E 8+00N	2	656	21	176	1.0	69	27	1401	7.06	22	7	ND	2	72	2	2	2	117	1.16	.120	42	83	1.27	508	.04	13	3.32	.06	.24	1	7
L21+90E 7+75N	1	797	12	143	1.5	81	21	873	6.98	13	5	ND	4	68	2	2	2	113	1.11	.122	41	88	1.44	570	.04	8	3.78	.06	.27	1	14
L21+90E 7+50N	3	693	16	110	.5	67	27	1356	6.69	19	7	ND	5	44	1	2	2	120	.61	.060	46	91	1.47	357	.06	7	2.95	.05	.21	1	9
L21+90E 7+25N	1	109	8	94	.1	21	13	320	4.27	11	5	ND	3	33	1	2	2	114	.38	.103	15	40	.63	165	.08	2	1.37	.03	.08	1	15
L21+90E 7+00N	3	204	12	62	.1	34	21	660	4.94	22	5	ND	4	35	1	9	2	103	.43	.111	21	48	.92	80	.09	4	1.42	.03	.08	1	9
L21+90E 6+75N	2	87	7	56	.2	18	10	209	3.87	8	5	ND	3	26	1	2	3	101	.32	.104	15	33	.49	92	.07	3	1.21	.03	.08	1	3
L21+90E 6+50N	2	117	5	72	.1	31	13	315	3.90	15	5	ND	3	25	1	2	2	83	.28	.059	18	43	.74	83	.06	5	1.45	.03	.07	1	4
L21+90E 6+25N	1	54	7	75	.1	18	9	203	3.24	8	5	ND	4	21	1	2	2	70	.25	.090	14	30	.46	90	.04	2	1.13	.02	.08	1	1
L21+90E 6+00N	2	75	8	82	.4	27	14	946	3.18	11	5	ND	2	34	1	5	2	72	.41	.073	19	40	.56	179	.04	3	1.52	.03	.10	1	4
L23+75E 14+00N	3	48	10	102	.2	26	9	220	3.46	14	5	ND	2	64	1	3	3	119	.48	.052	10	41	.53	52	.09	5	1.44	.03	.09	1	1
L23+75E 13+75N	5	1681	19	150	3.4	216	28	1502	6.88	37	11	ND	4	121	3	2	2	116	2.18	.060	66	128	.92	103	.07	8	3.24	.07	.10	1	4
L23+75E 13+50N	3	148	11	155	.2	72	18	448	4.38	29	5	ND	3	56	1	2	2	103	.67	.029	11	77	1.13	60	.08	3	2.05	.04	.08	1	22
L23+75E 13+25N	3	42	8	124	.1	37	14	357	3.45	21	5	ND	2	25	1	2	2	92	.44	.045	13	60	.72	43	.07	8	1.45	.03	.07	1	4
L23+75E 13+00N	1	31	8	130	.2	28	13	398	2.69	9	5	ND	2	22	1	2	2	71	.40	.039	10	50	.66	49	.05	2	1.27	.03	.07	1	4
L23+75E 12+50N	2	54	11	314	.1	52	21	650	4.46	13	5	ND	2	73	2	4	2	107	.47	.101	7	59	.85	111	.07	5	2.14	.04	.10	2	3
L23+75E 12+25N	5	119	13	301	.2	98	27	573	5.51	15	5	ND	3	53	2	2	2	166	.52	.079	12	98	1.20	80	.09	6	2.49	.04	.09	1	2
STD C/AU-0.5	20	60	42	139	7.3	71	29	1124	3.96	42	17	7	36	49	18	15	21	70	.48	.107	39	60	.88	185	.09	35	1.73	.09	.14	13	490



## E &amp; B EXPLORATION PROJECT - 5055 FILE # 06-2403

PAGE 7

SAMPLE#	Ag	Cu	Pb	Zn	As	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	Au	
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
L23+75E 11+75N	1	29	8	130	.2	34	11	308	2.86	13	5	ND	2	18	1	5	2	67	.35	.060	6	58	.77	66	.07	2	1.46	.04	.08	1	5
L23+75E 11+50N	2	22	6	124	.1	21	9	283	2.16	13	5	ND	2	19	1	6	2	69	.37	.043	8	36	.52	69	.09	2	1.24	.03	.06	1	12
L23+75E 11+25N	1	52	7	111	.1	37	15	273	3.81	17	5	ND	3	16	1	5	2	98	.31	.036	7	55	.82	71	.07	2	1.74	.03	.07	1	6
L23+75E 11+00N	3	83	14	121	.1	46	17	496	4.20	37	5	ND	3	21	1	2	2	92	.35	.046	10	58	.95	111	.04	2	2.02	.04	.09	1	3
L23+75E 10+75N	2	63	15	146	.2	47	17	621	3.86	32	5	ND	3	23	1	6	2	88	.40	.066	9	63	.98	110	.06	2	2.28	.04	.11	1	1
L23+75E 10+50N	3	76	14	181	.7	60	19	776	4.31	30	5	ND	4	28	1	7	2	89	.46	.109	8	66	1.01	143	.06	2	2.31	.04	.14	1	6
L23+75E 10+25N	2	42	14	181	.4	21	18	2178	3.12	15	5	ND	1	30	2	16	2	71	.52	.159	7	43	.35	185	.05	2	1.21	.03	.12	1	1
L23+75E 9+75N	3	239	13	100	1.2	74	19	952	4.57	37	5	ND	2	68	1	9	2	85	1.27	.093	16	87	.82	121	.04	2	2.11	.05	.09	1	6
L23+75E 9+25N	3	310	14	160	1.0	143	20	1023	4.58	29	5	ND	1	101	2	3	2	78	2.39	.131	8	82	1.01	91	.04	5	1.94	.06	.10	1	14
L23+75E 9+00N	3	100	14	106	.6	60	17	1333	4.04	27	5	ND	2	62	1	3	2	74	1.22	.094	17	69	1.02	218	.06	3	2.35	.05	.15	1	1
L23+75E 8+75N	1	60	9	97	.1	24	11	312	3.77	15	5	ND	2	26	1	7	2	79	.39	.076	11	38	.60	139	.05	3	1.30	.03	.09	1	4
L23+75E 8+50N	1	29	7	76	.1	13	6	158	2.42	10	6	ND	2	19	1	7	2	66	.32	.031	9	27	.38	83	.04	2	.90	.02	.08	1	1
L23+75E 8+25N	3	360	16	117	1.2	58	24	1562	6.76	22	5	ND	3	63	1	2	2	112	1.21	.095	26	77	1.03	555	.02	11	3.27	.06	.19	1	3
L23+75E 8+00N	2	62	10	61	.1	21	12	313	3.86	10	6	ND	2	23	1	3	2	85	.33	.051	10	39	.58	148	.04	2	1.24	.03	.09	1	2
L23+75E 7+75N	1	48	8	58	.1	16	9	367	2.69	4	5	ND	2	26	1	3	3	70	.37	.041	10	34	.43	183	.05	2	1.07	.03	.10	1	4
L23+75E 7+50N	1	38	6	37	.1	11	7	157	2.42	5	5	ND	1	24	1	2	3	70	.35	.041	10	27	.28	143	.05	2	.82	.03	.08	1	4
L23+75E 7+25N	2	241	10	78	.6	39	25	777	5.09	17	5	ND	2	45	1	7	2	104	.84	.067	14	61	.92	218	.06	5	1.94	.05	.11	1	4
L23+75E 7+00N	3	1231	19	86	2.0	72	26	1240	6.95	29	5	ND	3	73	1	3	2	117	1.43	.101	62	83	1.35	609	.04	11	3.82	.06	.19	1	8
L23+75E 6+75N	3	225	8	72	.3	27	17	355	6.50	20	6	ND	2	33	1	4	2	135	.36	.114	8	50	.87	147	.07	7	1.81	.04	.09	1	17
L23+75E 6+50N	1	117	10	51	.1	20	12	350	3.87	10	5	ND	2	36	1	2	2	97	.46	.073	10	34	.58	152	.06	2	1.26	.04	.08	1	1
L23+75E 6+25N	2	209	12	65	.3	27	17	647	4.83	17	5	ND	3	40	1	7	2	107	.53	.100	13	41	.80	195	.06	3	1.68	.04	.11	1	6
L23+75E 6+00N	2	146	7	63	.2	32	14	883	3.73	14	5	ND	3	31	1	9	2	81	.37	.063	14	50	.92	178	.04	5	2.00	.04	.10	1	4
SOIL 1	1	18	13	66	.1	24	5	181	2.72	8	5	ND	6	13	1	5	2	44	.24	.146	18	41	.56	90	.09	2	1.19	.02	.08	1	1
SOIL 2	1	17	8	112	.2	28	7	202	2.39	5	5	ND	3	20	1	5	2	36	.45	.069	17	40	.67	120	.06	2	1.29	.03	.07	1	1
SOIL 3	2	96	12	109	.4	40	21	1315	4.87	23	5	ND	3	35	1	6	2	114	.75	.059	11	70	1.11	179	.09	12	2.74	.05	.12	1	1
SOIL 4	3	53	13	115	.1	41	17	697	3.70	26	5	ND	4	24	1	4	2	69	.56	.049	7	35	.82	64	.11	5	1.63	.05	.08	1	1
SOIL 5	2	39	8	82	.2	32	10	319	4.02	14	5	ND	3	22	1	4	2	93	.47	.091	9	59	.92	77	.12	2	1.99	.04	.08	1	7
SOIL 6	1	16	9	70	.1	24	6	170	2.97	16	5	ND	5	13	1	4	2	41	.24	.164	14	43	.45	69	.05	2	1.29	.02	.10	1	1
SOIL 7	2	46	9	94	.1	34	12	327	3.93	14	5	ND	3	20	1	3	2	94	.49	.104	8	53	.89	95	.12	2	2.36	.04	.05	1	1
SOIL 8	1	29	11	143	.1	22	9	326	3.66	15	5	ND	3	18	1	2	2	83	.41	.205	9	44	.61	106	.10	2	1.86	.04	.07	2	1
SOIL 9	2	46	15	112	.2	40	11	1022	4.21	38	5	ND	2	12	1	7	3	42	.21	.079	8	17	.15	116	.03	6	.61	.03	.12	1	1
SOIL 10	5	69	18	248	.5	59	23	3151	4.59	20	5	ND	3	41	2	5	2	76	.64	.074	16	50	.53	255	.06	4	2.19	.04	.12	1	4
SOIL 11	1	28	8	95	.1	30	12	375	2.70	9	5	ND	3	28	1	2	2	63	.50	.036	12	44	.75	87	.09	2	1.65	.04	.09	1	4
SOIL 12	2	30	7	96	.1	33	9	387	2.46	7	5	ND	3	25	1	7	2	55	.46	.055	14	41	.72	73	.09	2	1.35	.03	.09	1	1
SOIL 13	2	32	9	120	.1	35	10	336	2.52	5	5	ND	4	19	1	2	2	51	.31	.048	15	40	.63	85	.07	2	1.60	.03	.09	1	5
SOIL 14	2	32	9	87	.1	29	13	449	3.17	13	5	ND	3	26	1	4	2	79	.52	.065	11	47	.85	95	.10	3	1.96	.04	.09	1	1
STD C/AU-0.5	22	59	39	136	7.0	70	28	1097	3.99	42	18	7	35	48	18	16	20	68	.48	.105	37	59	.88	181	.09	40	1.72	.09	.14	13	485

E & B EXPLORATION PROJECT - SOSE FILE # 82-2403

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	V	Au	Th	Sr	Co	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	Y	Al	Na	K	W	Pb
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	PPM	PPM	
SOIL 15	6	98	22	154	2.2	107	19	2725	3.69	9	5	ND	5	36	5	2	2	80	.69	.046	23	60	.81	222	.07	9	2.55	.04	.13	1	1
SOIL 16	2	31	4	232	.6	62	10	525	2.45	5	5	ND	4	27	11	2	2	56	.50	.031	17	40	.46	122	.07	4	1.49	.03	.08	1	2
SOIL 17	6	51	15	309	.7	53	14	1440	3.91	11	5	ND	3	17	4	2	2	85	.26	.050	17	53	.49	138	.06	7	1.76	.02	.07	1	6
SOIL 18	37	90	17	612	.4	141	21	605	6.62	35	5	ND	2	46	10	8	2	136	.65	.145	24	45	.89	165	.08	13	2.06	.04	.09	1	1
SOIL 19	9	58	10	209	.5	71	15	791	3.63	17	5	ND	5	33	2	2	2	79	.54	.056	24	73	1.01	141	.06	4	1.91	.02	.11	1	1
SOIL 20	2	27	8	92	.2	36	9	313	2.74	12	5	ND	3	27	1	4	2	73	.49	.026	20	49	.70	88	.10	4	1.59	.03	.07	1	3
SOIL 21	4	71	11	112	.3	56	15	906	3.69	20	5	ND	7	33	1	2	2	76	.55	.062	22	64	1.01	147	.12	10	1.99	.04	.18	1	2
SOIL 22	2	28	16	117	.5	25	10	635	2.26	10	5	ND	2	12	1	2	2	56	.19	.085	12	42	.50	84	.05	4	1.57	.02	.11	1	1
SOIL 23	1	17	8	115	.6	19	6	412	2.47	3	5	ND	3	15	1	2	2	58	.23	.100	16	35	.42	92	.07	4	1.44	.02	.08	1	1
SOIL 24	2	34	9	106	1.4	29	8	445	3.52	11	5	ND	4	19	1	2	2	74	.29	.094	18	42	.51	96	.08	3	1.46	.02	.09	1	3
SOIL 25	2	53	17	146	1.3	47	12	429	4.10	8	5	ND	2	31	1	2	2	76	.48	.080	13	51	.65	127	.06	7	2.14	.03	.08	1	1
SOIL 26	1	39	10	69	.2	36	11	580	3.72	11	5	ND	2	37	1	2	2	98	.55	.057	14	59	1.00	72	.15	6	2.04	.04	.09	1	1
SOIL 27	1	52	10	80	.3	49	13	649	3.65	11	5	ND	4	45	1	5	2	85	.63	.052	17	61	.97	109	.12	7	2.13	.04	.10	1	1
SOIL 28	1	24	9	45	.1	25	10	524	2.41	10	5	ND	4	26	1	5	2	57	.47	.041	16	42	.67	47	.12	2	1.29	.03	.08	2	2
SOIL 29	1	16	2	56	.2	19	5	207	2.19	7	5	ND	2	24	1	2	2	49	.41	.068	12	34	.50	67	.09	2	1.15	.02	.07	1	1
SOIL 30	1	11	8	85	.2	20	6	345	2.52	6	5	ND	2	23	1	2	2	59	.39	.090	12	38	.39	114	.10	2	1.11	.02	.08	1	1
SOIL 31	1	39	10	118	.4	36	9	356	3.85	20	5	ND	2	26	1	2	2	109	.44	.050	11	44	.71	41	.21	3	1.70	.03	.08	1	47
SOIL 32	1	16	9	78	.1	23	6	239	2.42	5	5	ND	5	24	1	2	3	56	.41	.092	16	38	.61	55	.11	2	1.43	.03	.07	1	1
SOIL 33	1	20	10	105	.4	27	10	394	2.63	7	5	ND	4	24	1	3	2	68	.43	.089	13	43	.70	72	.12	12	1.46	.03	.07	1	3
SOIL 34	1	18	9	49	.1	22	5	230	2.07	4	5	ND	5	13	1	8	2	40	.27	.072	15	41	.68	43	.10	2	1.14	.02	.08	1	3
SOIL 35	1	22	5	57	.1	22	6	254	2.13	7	5	ND	4	18	1	7	2	46	.30	.062	15	39	.64	58	.08	2	1.30	.02	.08	1	2
SOIL 36	1	28	13	75	.2	31	9	411	2.60	9	5	ND	4	19	1	2	2	53	.33	.086	17	47	.74	79	.09	4	1.56	.03	.11	1	2
SOIL 37	2	20	5	122	.1	27	9	325	2.60	13	5	ND	3	19	1	2	2	59	.33	.058	12	40	.60	92	.08	2	1.24	.02	.07	1	1
SOIL 38	2	58	12	285	2.1	60	16	1228	3.81	7	5	ND	3	25	3	3	2	104	.52	.113	12	47	.78	130	.12	9	1.72	.04	.09	1	4
SOIL 39	1	65	15	320	1.0	88	11	304	3.65	6	5	ND	4	18	2	2	2	94	.41	.026	14	50	.76	137	.12	3	2.06	.03	.06	1	1
SOIL 40	4	29	12	256	2.6	30	7	179	3.85	7	5	ND	4	13	1	6	2	96	.24	.103	15	47	.48	90	.09	2	1.93	.03	.05	1	3
SOIL 41	3	20	10	261	1.5	27	7	201	2.78	7	5	ND	3	13	1	2	2	76	.24	.053	9	29	.41	91	.06	2	1.47	.02	.06	1	1
SOIL 42	3	45	16	163	1.1	44	12	1776	3.31	11	5	ND	3	15	1	5	2	65	.24	.096	15	33	.60	115	.07	4	1.37	.03	.11	1	1
SOIL 43	1	21	7	95	1.4	35	7	217	2.47	8	5	ND	4	14	1	2	2	40	.28	.108	14	40	.60	83	.05	2	1.38	.02	.08	1	1
SOIL 44	2	241	20	242	2.4	162	19	1210	4.19	19	5	ND	8	27	3	6	2	77	.54	.037	32	62	1.06	233	.07	4	2.57	.04	.13	1	3
SOIL 45	1	43	9	99	.5	41	13	615	2.89	8	5	ND	3	33	1	2	3	68	.58	.046	12	51	.78	101	.09	2	1.69	.04	.09	1	2
STD C/AU-0.5	21	60	43	139	7.2	72	29	1115	3.97	43	18	7	36	49	18	16	20	69	.48	.107	33	58	.88	184	.09	33	1.73	.09	.13	12	480

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-2403

PAGE 9

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	K PPM	Al %	Na %	S %	W PPM	Au1 PPB
SILT 1	7	100	19	222	1.5	114	21	6244	5.67	38	5	ND	4	114	3	6	2	82	1.69	.140	41	86	.93	387	.06	9	3.42	.07	.26	1	2
SILT 2	5	31	16	120	.4	69	20	10671	3.73	26	5	ND	4	47	1	4	3	51	.78	.092	22	43	.68	267	.06	10	1.50	.04	.16	1	2
SILT 3	3	42	14	98	.4	60	13	1166	3.09	7	5	ND	3	58	1	4	2	69	.86	.070	19	61	.80	136	.11	5	2.06	.04	.17	1	1
SILT 4	3	44	13	95	.4	64	16	1310	3.65	11	5	ND	4	57	1	5	2	75	.89	.077	18	60	1.07	137	.11	5	2.14	.05	.18	1	1
SILT 5	3	42	18	93	.4	69	15	1077	3.31	8	5	ND	3	51	1	3	2	66	.80	.077	16	83	1.10	119	.10	6	1.94	.04	.16	1	1
SILT 6	3	38	16	88	.2	60	17	1192	3.50	13	5	ND	5	44	1	2	2	77	.71	.069	16	68	1.15	115	.14	10	1.86	.04	.15	1	1
SILT 7	4	40	15	91	.3	63	16	1282	3.33	13	5	ND	4	46	1	7	2	73	.76	.073	15	67	1.06	127	.11	11	1.84	.04	.16	1	1
SILT 8	3	38	17	90	.3	60	15	1209	3.31	12	5	ND	4	41	1	2	2	72	.67	.065	15	67	1.08	120	.11	11	1.84	.04	.16	1	1

E & B EXPLORATION PROJECT - 5055 FILE # 86-2400

PAGE 10A

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Ce PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	E PPM	Al %	Na %	K %	W PPM	Au# PPB
KR-86-0404	1	70	12	76	.3	30	1e	1130	5.02	2	5	ND	2	97	1	2	2	146	3.39	.116	4	77	3.99	16	.11	2	2.74	.09	.05	1	17
KR-86-097	1	49	15	97	.1	48	5	49	6.62	51	5	ND	3	173	1	5	3	132	.03	.094	8	32	.03	263	.01	2	.32	.02	.07	1	2
KR-86-09E	1	107	14	77	.1	94	23	858	5.40	9	5	ND	2	25	1	5	2	138	1.85	.132	5	143	2.57	36	.21	2	2.71	.08	.05	1	3
KR-86-099	1	86	13	97	.1	55	23	905	6.14	2	5	ND	1	23	1	2	2	188	1.17	.115	2	93	2.84	43	.39	5	2.77	.08	.04	1	1
KR-86-100	4	65	6	81	.1	47	16	537	4.41	2	5	ND	2	21	1	7	2	157	.74	.112	6	65	2.18	47	.20	2	2.07	.07	.11	1	2
KR-86-101	1	26	6	33	.1	32	11	369	1.73	2	5	ND	1	13	1	2	2	42	1.05	.055	2	112	1.43	16	.14	2	1.22	.06	.03	1	1
KR-86-102	1	77	7	59	.1	42	14	1717	3.35	3	5	ND	2	221	1	2	2	176	9.80	.097	5	36	1.26	37	.28	7	1.91	.09	.04	1	6
KR-86-103	1	6	2	3	.1	5	1	34	.28	6	5	ND	1	1	1	2	2	1	.01	.001	2	2	.01	4	.01	2	.02	.01	.01	1	2
KR-86-104	2	88	10	81	.1	40	22	791	5.53	2	5	ND	2	24	1	2	2	150	1.91	.093	2	45	1.91	15	.28	3	2.60	.08	.02	1	1
KR-86-105	1	103	9	87	.1	24	18	842	5.42	2	5	ND	2	30	1	4	2	162	2.33	.116	2	33	1.58	22	.41	8	2.40	.09	.02	1	1
KR-86-106	1	105	7	75	.2	30	19	789	5.46	2	5	ND	2	23	1	2	2	157	1.91	.102	4	60	1.68	19	.31	5	2.51	.08	.03	1	1
KR-86-107	5	70	6	137	.4	16	7	1165	4.89	14	8	ND	2	371	2	2	3	76	12.51	.046	6	11	3.00	129	.01	6	.35	.10	.08	1	2
KR-86-108	2	365	8	56	.5	34	20	1034	5.36	8	5	ND	2	136	1	3	2	86	3.98	.018	5	149	2.68	13	.11	2	2.15	.10	.05	1	8
KR-86-109	2	105	10	40	.1	103	23	951	5.38	5	5	ND	1	131	1	2	2	218	5.70	.027	5	229	4.65	61	.06	2	2.70	.10	.05	1	1
KR-86-110	5	225	9	48	.2	175	30	783	4.65	7	5	ND	1	65	1	2	2	84	3.63	.069	4	482	3.67	13	.13	2	1.92	.07	.03	1	3
KR-86-111	1	4	18	34	.1	10	5	811	1.73	13	5	ND	5	86	1	2	3	7	1.46	.054	13	9	.31	68	.01	4	.28	.07	.16	1	7
KR-86-112	1	48	144	39	2.9	15	3	481	.84	38	5	ND	1	70	1	18	2	5	4.49	.010	2	12	.46	18	.01	3	.06	.05	.01	1	37
KR-86-112A	2	143	13	83	.5	54	28	1499	6.75	27	5	ND	1	83	1	2	2	91	4.60	.098	5	81	1.95	57	.13	3	2.12	.23	.11	2	16
KR-86-113	2	11	14	86	.2	75	19	1713	5.09	25	5	ND	1	110	1	2	2	96	2.53	.056	2	242	3.88	51	.07	2	2.56	.06	.02	1	6
STD C/AU 0.5	22	60	41	140	7.0	72	29	1119	3.99	42	17	8	36	50	18	15	22	70	.48	.106	38	60	.88	188	.09	39	1.73	.09	.14	12	500

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE 253-3158

DATA LINE 251-1011

## GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO<sub>3</sub>-H<sub>2</sub>O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SM, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: SOILS -80 MESH AU: ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 2 1986

DATE REPORT MAILED:

Aug 6/86

ASSAYER:

D. J. ...

DEAN TOYE, CERTIFIED B.C. ASSAYER.

E &amp; B EXPLORATIONS PROJECT - 5055 FILE # 86-1803

PAGE 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	%	PPH	%	%	%	PPH	PPB
L15+00E 20+00N	2	138	21	183	.7	75	30	1462	4.98	27	5	ND	1	37	1	2	2	95	.61	.070	25	97	1.37	155	.06	4	3.06	.01	.19	1	1
L15+00E 19+75N	1	17	11	107	.2	15	7	297	1.89	6	5	ND	1	20	1	2	2	51	.37	.046	10	32	.37	61	.09	2	.96	.01	.06	1	1
L15+00E 19+50N	2	41	6	154	.2	27	12	820	3.46	20	5	ND	1	25	2	2	2	87	.50	.104	8	46	.60	110	.10	4	1.36	.01	.08	1	2
L15+00E 19+25N	1	20	6	158	.3	15	9	625	2.80	9	5	ND	1	24	1	3	2	79	.42	.091	9	40	.48	84	.10	2	1.12	.01	.07	1	1
L15+00E 19+00N	1	37	.8	179	.3	36	15	328	3.64	16	5	ND	2	19	1	2	2	74	.34	.147	10	56	.76	96	.07	2	1.75	.01	.07	1	1
L15+00E 18+75N	1	20	6	144	.2	17	11	406	2.49	7	5	ND	2	15	1	2	2	60	.29	.117	8	39	.44	66	.07	2	1.25	.01	.06	1	1
L15+00E 18+50N	1	38	9	125	.3	26	13	568	2.31	5	5	ND	1	23	1	2	2	59	.42	.033	12	48	.64	76	.08	3	1.40	.01	.07	1	1
L15+00E 18+25N	1	25	5	138	.2	22	16	638	2.76	7	5	ND	1	20	1	2	2	69	.41	.070	9	49	.60	84	.07	4	1.39	.01	.07	1	1
L15+00E 18+00N	1	22	10	98	.1	19	8	197	2.27	9	5	ND	2	18	1	2	2	59	.34	.057	10	39	.55	53	.08	4	1.07	.01	.06	1	1
L15+00E 17+75N	1	33	12	101	.1	24	15	483	2.11	6	5	ND	1	27	1	2	2	49	.50	.045	12	43	.59	76	.05	2	1.37	.01	.07	1	1
L15+00E 17+50N	1	44	17	137	.2	39	19	797	2.91	12	5	ND	1	32	1	2	2	71	.56	.055	11	57	.69	98	.05	2	1.75	.01	.09	1	1
L15+00E 17+25N	1	42	10	106	.1	31	14	624	2.42	8	5	ND	1	29	1	2	2	53	.49	.040	14	51	.71	82	.06	2	1.47	.01	.08	1	1
L15+00E 17+00N	2	58	14	167	.3	47	18	879	2.87	7	6	ND	1	31	1	2	2	62	.52	.062	13	62	.78	115	.05	4	1.84	.01	.10	1	1
L15+00E 16+75N	1	52	16	128	.1	39	16	501	2.88	10	5	ND	1	27	1	2	2	62	.44	.044	14	55	.73	81	.06	2	1.65	.01	.08	1	1
L15+00E 16+50N	2	30	8	100	.1	26	11	354	2.46	9	5	ND	1	27	1	2	2	63	.50	.049	8	46	.64	59	.08	4	1.13	.01	.09	1	1
L15+00E 16+25N	1	23	4	137	.2	23	11	262	2.78	3	5	ND	1	24	1	2	2	70	.44	.085	6	43	.55	67	.06	2	1.33	.01	.09	1	1
L15+00E 16+00N	1	40	13	134	.2	33	13	294	2.72	7	5	ND	1	25	1	2	2	65	.44	.049	9	54	.78	64	.07	2	1.41	.01	.06	1	1
L15+00E 15+75N	2	82	11	168	.2	49	22	819	3.39	13	5	ND	1	36	2	2	2	69	.57	.056	19	69	.86	127	.05	2	1.98	.01	.09	1	1
L15+00E 15+50N	2	80	15	179	.3	52	23	1011	3.72	15	5	ND	2	31	1	2	2	82	.56	.050	15	79	1.06	113	.08	6	2.03	.02	.10	1	1
L15+00E 15+25N	3	79	16	118	.3	51	19	805	3.32	15	5	ND	2	30	1	2	2	77	.56	.051	15	74	1.07	96	.09	3	1.94	.02	.11	1	6
L16+25E 20+00N	1	21	7	208	.3	20	12	342	2.85	9	5	ND	1	21	1	2	2	69	.39	.097	7	40	.48	72	.09	3	1.37	.01	.07	1	1
L16+25E 19+75N	1	16	10	159	.1	21	11	413	2.60	7	5	ND	1	20	1	2	2	64	.34	.066	9	38	.53	93	.09	2	1.25	.01	.06	1	3
L16+25E 19+50N	1	21	14	169	.1	18	15	2740	2.43	7	5	ND	1	21	2	2	2	63	.49	.071	6	44	.50	123	.11	2	1.02	.01	.09	1	1
L16+25E 19+25N	2	52	15	217	.2	39	42	2424	4.17	12	5	ND	1	23	2	2	2	109	.70	.114	5	67	1.14	99	.11	5	2.01	.02	.09	1	1
L16+25E 19+00N	1	29	5	132	.2	21	10	233	2.65	9	5	ND	2	19	1	2	2	69	.37	.058	8	41	.55	77	.09	2	1.47	.01	.06	1	1
L16+25E 18+75N	2	43	11	188	.1	31	17	419	3.56	11	5	ND	1	18	1	2	2	84	.33	.069	7	59	.64	81	.09	2	1.71	.01	.08	1	1
L16+25E 18+50N	1	51	17	158	.2	41	19	684	3.52	11	5	ND	1	28	1	2	2	93	.52	.057	8	64	.91	85	.09	2	1.94	.02	.07	1	1
L16+25E 18+25N	2	45	10	184	.2	42	20	1134	3.02	11	5	ND	1	31	2	2	2	74	.55	.051	7	66	.69	104	.07	3	1.66	.01	.08	1	1
L16+25E 18+00N	2	51	8	166	.2	43	17	475	2.90	10	5	ND	1	28	1	2	2	70	.43	.034	9	74	.92	81	.08	2	1.78	.01	.07	1	9
L16+25E 17+75N	1	35	5	93	.1	42	15	562	2.77	13	5	ND	1	29	1	2	2	64	.51	.053	11	93	1.23	69	.09	2	1.77	.01	.08	1	5
L16+25E 17+50N	2	85	12	145	.4	54	27	1146	3.30	10	5	ND	1	43	1	2	2	77	.66	.055	19	82	.96	112	.06	2	2.30	.02	.09	1	2
L16+25E 17+25N	1	21	10	98	.1	22	10	269	2.22	10	5	ND	1	22	1	2	2	61	.38	.055	8	46	.52	70	.07	2	1.08	.01	.07	1	1
L16+25E 17+00N	1	35	8	102	.1	31	13	309	2.49	7	5	ND	1	20	1	2	2	59	.33	.032	11	49	.68	73	.07	6	1.50	.01	.07	1	1
L16+25E 16+75N	1	52	7	124	.2	36	13	333	2.81	10	5	ND	1	34	1	2	2	69	.47	.042	16	51	.65	86	.07	3	1.58	.01	.08	1	1
L16+25E 16+50N	2	43	10	132	.3	29	15	716	2.97	7	5	ND	1	25	2	2	2	72	.41	.080	10	49	.58	101	.06	2	1.48	.01	.08	1	8
L16+25E 16+25N	3	74	12	187	.2	52	28	904	3.77	12	5	ND	2	30	1	2	2	84	.46	.060	12	74	1.00	105	.07	4	2.09	.01	.09	1	8
STD C/AU-0.5	21	58	41	137	7.1	69	31	1140	3.87	39	20	8	35	49	18	16	19	64	.50	.108	38	62	.87	184	.08	37	1.71	.07	.14	15	520

E & B EXPLORATION PROJECT - 5055 FILE # 86-1803

PAGE 2

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	R PPM	Al %	Na %	K %	W PPM	AuI PPB
L16+25E 16+00N	1	40	15	122	.4	49	21	713	3.75	16	7	ND	1	26	1	2	2	86	.54	.067	8	89	1.39	70	.08	4	1.78	.02	.08	1	1
L16+25E 15+75N	1	15	14	125	.3	17	9	377	2.27	11	5	ND	1	13	1	2	2	49	.26	.153	7	35	.34	88	.05	2	1.03	.01	.07	1	1
L16+25E 15+50N	1	24	12	113	.3	21	8	312	2.27	12	5	ND	1	15	1	2	2	55	.29	.067	8	38	.50	83	.06	4	1.10	.01	.06	1	8
L16+25E 15+25N	1	29	10	77	.2	26	10	529	2.08	11	5	ND	1	20	1	2	2	47	.35	.041	9	40	.56	72	.07	2	1.01	.01	.07	1	10
L17+50E 20+00N	1	23	13	216	.4	25	16	532	3.17	15	5	ND	2	18	1	2	2	68	.29	.185	7	45	.42	126	.06	4	1.65	.01	.06	1	21
L17+50E 19+75N	1	23	7	142	.1	25	10	592	2.41	12	5	ND	2	18	1	2	2	53	.34	.079	8	36	.50	123	.06	3	1.27	.01	.05	1	6
L17+50E 19+50N	1	23	12	139	.2	28	10	224	2.85	10	5	ND	2	16	1	2	2	64	.31	.078	7	41	.55	78	.07	2	1.50	.01	.06	1	7
L17+50E 19+25N	2	60	16	113	.3	41	15	473	3.60	22	5	ND	2	19	1	2	2	75	.35	.081	8	56	.86	78	.09	2	1.67	.01	.05	1	2
L17+50E 19+00N	1	20	14	139	.2	19	14	421	2.99	14	5	ND	1	19	1	2	2	71	.28	.095	8	37	.47	89	.07	2	1.41	.01	.05	1	1
L17+50E 18+75N	1	35	13	181	.2	35	15	688	3.30	10	5	ND	2	16	1	2	2	71	.32	.074	8	48	.63	93	.08	4	1.72	.01	.07	1	19
L17+50E 18+50N	1	23	10	131	.2	20	9	351	2.57	17	5	ND	1	18	1	2	2	67	.36	.058	8	36	.48	69	.08	2	1.15	.01	.06	1	3
L17+50E 18+25N	1	27	7	228	.2	27	13	602	3.43	15	5	ND	1	20	1	2	2	83	.34	.107	10	48	.61	97	.07	2	1.54	.01	.07	1	1
L17+50E 18+00N	2	52	14	172	.1	44	22	574	4.31	18	5	ND	2	16	2	2	2	87	.32	.148	9	63	.71	74	.07	3	1.86	.01	.07	1	5
L17+50E 17+75N	2	28	11	156	.2	22	19	510	3.76	17	5	ND	1	22	1	2	2	92	.32	.098	9	56	.63	75	.09	3	1.75	.01	.05	1	1
L17+50E 17+50N	2	53	8	144	.2	36	18	916	3.55	17	5	ND	1	31	1	2	2	87	.43	.068	9	60	.86	89	.09	2	1.42	.01	.07	1	3
L17+50E 17+25N	1	47	3	156	.1	36	14	533	3.17	14	5	ND	1	23	1	2	2	72	.42	.050	12	61	.85	69	.06	2	1.59	.01	.07	1	4
L17+50E 17+00N	1	120	15	165	1.0	67	22	967	4.57	26	5	ND	3	38	1	2	2	87	.70	.045	20	98	1.13	134	.09	4	2.50	.01	.11	1	4
L17+50E 16+75N	1	40	12	134	.1	43	13	374	3.37	14	5	ND	2	31	1	2	2	68	.48	.043	13	66	.94	78	.09	5	1.74	.01	.07	1	2
L17+50E 16+50N	2	89	19	177	.7	61	21	1997	4.33	15	5	ND	2	46	2	2	2	84	.92	.069	20	87	1.10	169	.06	2	2.68	.02	.11	1	1
L17+50E 16+25N	1	32	7	111	.1	28	10	426	2.20	7	5	ND	1	27	1	2	2	43	.50	.042	14	41	.58	77	.04	3	1.27	.01	.07	1	1
L17+50E 16+00N	1	51	10	121	.2	39	21	713	3.40	18	5	ND	2	23	1	2	2	65	.42	.080	15	52	.88	83	.05	2	1.76	.01	.09	1	3
L17+50E 15+75N	1	47	15	134	.1	35	12	293	3.51	14	5	ND	2	21	1	2	2	74	.28	.075	11	48	.77	57	.07	5	1.48	.01	.06	1	12
L17+50E 15+50N	3	105	10	151	.1	57	22	723	4.95	28	5	ND	2	23	1	2	2	90	.33	.126	11	70	1.12	82	.06	4	1.96	.01	.07	1	3
L17+50E 15+25N	2	27	4	127	.1	22	10	251	2.94	13	5	ND	1	19	1	2	2	73	.30	.078	10	42	.60	61	.07	4	1.19	.01	.06	1	2
L18+75E 19+75N	3	159	14	341	.2	78	29	507	7.27	22	5	ND	2	74	2	2	2	151	.37	.217	6	98	1.28	145	.11	5	3.08	.01	.06	1	2
L18+75E 19+25N	1	32	7	289	.3	30	13	330	3.92	12	5	ND	1	18	1	2	2	103	.37	.065	8	50	.79	104	.07	2	2.21	.01	.05	1	1
L18+75E 19+00N	1	33	9	152	.2	28	13	412	3.55	11	5	ND	2	17	1	2	2	83	.28	.075	7	48	.67	78	.08	2	1.85	.01	.05	1	1
L18+75E 18+75N	1	39	7	154	.1	23	13	841	3.48	9	5	ND	1	21	1	2	2	94	.60	.145	6	50	.83	107	.10	4	1.65	.01	.07	1	2
L18+75E 18+50N	1	31	10	300	.2	28	14	1105	2.67	11	5	ND	1	22	1	2	2	61	.40	.060	10	47	.67	120	.07	3	1.57	.01	.06	1	1
L18+75E 18+25N	1	21	11	115	.3	16	9	544	2.21	6	5	ND	1	20	1	2	2	60	.40	.047	7	36	.43	94	.08	2	1.03	.01	.06	1	1
L18+75E 18+00N	1	65	8	187	.2	51	18	442	3.66	15	5	ND	1	31	1	2	2	76	.57	.044	8	60	.70	86	.07	3	2.12	.01	.06	1	1
L18+75E 17+75N	1	58	8	203	.3	38	18	1579	3.21	13	5	ND	1	48	1	2	2	69	.80	.064	13	57	.63	137	.06	2	1.75	.01	.07	1	1
L18+75E 17+50N	1	55	12	143	.2	35	15	1282	3.04	16	5	ND	1	27	1	2	2	68	.51	.041	9	63	.76	85	.06	2	1.50	.01	.06	2	65
L18+75E 17+25N	1	45	14	124	.2	34	13	291	3.22	14	5	ND	2	19	1	2	2	70	.37	.066	7	53	.80	70	.07	2	1.66	.01	.06	1	2
L18+75E 17+00N	1	21	5	79	.2	19	8	272	2.29	5	5	ND	1	17	1	2	2	57	.34	.058	7	39	.49	73	.06	2	1.15	.01	.05	1	2
L18+75E 16+75N	1	20	7	120	.2	25	10	352	2.54	10	5	ND	1	16	1	2	2	62	.31	.080	6	49	.61	57	.07	3	1.23	.01	.05	1	1
STD C/AU-0.5	20	59	41	131	6.8	69	29	1089	3.93	41	19	7	34	48	17	15	19	62	.48	.104	37	59	.88	177	.08	37	1.73	.06	.13	14	510

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1803

PAGE 3

SAMPLE#	Mo PPM	Co PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	P PPM	Al %	Na %	K %	M PPM	Au PPM
L18+75E 16+50M	1	31	12	201	.1	31	18	584	3.60	6	5	ND	2	20	1	2	4	71	.39	.163	8	52	.71	81	.07	2	1.78	.01	.08	1	6
L18+75E 16+25N	1	23	7	244	.1	27	15	399	3.42	9	5	ND	1	21	1	2	2	63	.37	.120	11	47	.64	84	.08	5	1.76	.01	.08	1	2
L18+75E 16+00M	1	37	11	177	.2	34	14	245	3.69	12	5	ND	2	23	1	2	2	71	.27	.123	12	51	.71	64	.06	3	1.76	.01	.07	1	2
L18+75E 15+75N	1	45	15	129	.1	33	14	588	3.02	11	5	ND	1	19	1	2	2	59	.30	.048	9	45	.70	61	.07	3	1.44	.01	.06	1	12
L18+75E 15+50M	1	57	10	161	.1	36	18	426	3.90	20	5	ND	2	23	1	2	2	80	.38	.093	11	60	.91	80	.07	2	1.91	.01	.07	1	8
L18+75E 15+25M	1	46	6	144	.3	40	14	521	3.18	13	5	ND	1	29	1	2	2	66	.55	.054	11	62	.85	78	.06	3	1.78	.01	.06	1	5
L20+00E 20+00M	3	55	16	198	.2	15	16	908	6.10	7	5	ND	1	22	2	2	2	158	.56	.173	9	45	1.00	62	.18	6	1.97	.02	.06	1	3
L20+00E 19+50M	2	69	13	299	.2	48	27	1630	5.96	15	5	ND	1	22	1	2	4	150	.81	.127	8	104	1.48	76	.22	5	2.61	.02	.08	1	2
L20+00E 19+25N	1	21	10	349	.2	22	14	398	3.13	7	5	ND	1	25	1	2	4	84	.39	.126	9	41	.64	114	.09	2	2.23	.01	.08	1	1
L20+00E 19+00M	1	26	16	200	.3	21	15	1759	3.58	6	5	ND	1	26	1	2	2	91	.60	.131	8	47	.79	123	.11	2	2.00	.01	.08	1	1
L20+00E 18+75M	1	14	6	189	.2	14	13	577	2.45	2	5	ND	1	16	1	2	2	66	.38	.075	6	36	.50	53	.12	4	1.27	.01	.06	1	1
L20+00E 18+50M	1	22	13	285	.3	17	18	1922	2.59	9	5	ND	1	26	2	2	2	61	.53	.088	7	37	.50	121	.11	4	1.34	.01	.07	1	2
L20+00E 18+25M	1	19	8	162	.1	14	9	327	3.09	12	5	ND	1	19	1	2	2	85	.45	.137	9	42	.45	97	.10	2	1.69	.01	.06	1	15
L20+00E 18+00M	1	18	11	209	.1	15	17	2376	2.87	4	5	ND	1	32	2	2	5	81	.68	.096	8	40	.62	125	.12	4	1.50	.01	.09	1	2
L20+00E 17+75M	1	26	11	201	.1	22	15	435	3.23	11	5	ND	1	31	1	2	4	71	.56	.184	8	46	.67	119	.09	2	1.58	.01	.09	1	1
L20+00E 17+50M	1	28	11	193	.1	30	14	437	3.32	9	5	ND	1	31	1	2	3	79	.52	.090	9	49	.79	79	.10	3	1.77	.01	.08	1	42
L20+00E 17+25M	1	34	13	175	.1	27	16	555	3.80	12	5	ND	1	24	1	2	3	97	.45	.148	8	63	.74	69	.09	2	1.82	.01	.09	1	4
L20+00E 17+00M	1	25	5	204	.2	23	16	1017	2.82	10	5	ND	1	27	1	2	4	70	.48	.052	8	52	.68	98	.11	2	1.41	.01	.09	1	2
L20+00E 16+75M	1	19	9	172	.1	25	11	273	3.09	8	5	ND	1	20	1	3	3	68	.42	.124	7	61	.54	66	.09	4	1.38	.01	.06	1	1
L20+00E 16+50M	1	24	10	121	.1	27	11	355	3.08	9	5	ND	1	25	1	2	3	76	.48	.072	9	53	.68	93	.09	2	1.63	.01	.07	1	2
L20+00E 16+25M	1	34	8	177	.1	32	14	259	4.01	8	5	ND	1	25	1	3	2	98	.47	.134	8	64	.83	91	.09	2	1.87	.01	.08	1	2
L20+00E 16+00M	1	28	15	130	.1	26	12	323	3.00	5	5	ND	1	26	1	2	2	74	.50	.063	7	45	.64	84	.09	3	1.34	.01	.06	1	2
L20+00E 15+75M	1	33	11	152	.4	31	20	2100	3.02	6	5	ND	1	26	1	2	2	61	.44	.068	12	47	.65	136	.07	3	1.56	.01	.08	1	33
L20+00E 15+50M	1	42	10	189	.1	35	16	356	3.46	11	5	ND	2	23	1	2	2	74	.42	.077	11	54	.85	78	.09	2	1.82	.01	.08	1	3
L48E 0+25S	1	48	11	81	.3	23	9	476	2.32	7	5	ND	1	67	1	3	2	36	1.64	.058	9	32	.55	108	.04	2	1.26	.01	.05	1	3
L48E 0+50S	1	18	7	66	.1	12	4	741	1.42	5	5	ND	1	54	1	2	2	30	1.13	.075	7	19	.19	85	.04	2	.62	.01	.07	1	1
L48E 0+75S	1	20	8	75	.3	19	8	273	2.47	9	5	ND	1	28	1	2	2	40	.52	.084	13	31	.45	67	.04	2	1.13	.01	.05	1	15
L48E 1+00S	1	17	9	47	.3	10	4	177	1.55	5	5	ND	1	60	1	2	2	29	1.47	.045	8	19	.22	77	.04	2	.71	.01	.05	2	1
L48E 1+25S	1	78	19	104	.8	48	18	1086	4.47	22	6	ND	1	60	1	2	5	75	1.21	.073	21	61	.88	151	.06	3	2.34	.01	.12	1	8
L48E 1+50S	1	59	12	93	.7	36	15	581	3.36	15	7	ND	1	85	1	3	2	52	2.33	.109	26	43	.69	109	.04	4	1.81	.01	.10	1	3
L48E 1+75S	1	35	8	77	.3	28	12	386	3.14	13	5	ND	3	26	1	2	2	47	.44	.055	16	42	.65	58	.07	2	1.34	.01	.07	1	10
L48E 2+00S	1	140	29	159	1.5	96	28	1903	7.20	42	5	ND	3	58	1	2	2	103	.94	.108	22	98	1.27	271	.07	2	4.21	.02	.26	1	5
L48E 2+25S	1	28	9	71	.2	23	9	344	2.37	8	5	ND	2	21	1	2	2	37	.37	.055	19	32	.49	47	.06	2	1.05	.01	.08	1	135
L48E 2+50S	1	29	10	118	.3	30	16	1232	2.97	12	5	ND	1	41	1	2	2	46	.77	.061	14	41	.59	87	.05	2	1.47	.01	.10	1	2
L48E 2+75S	1	9	11	67	.2	11	5	165	1.89	2	5	ND	3	14	1	3	2	38	.18	.026	15	26	.31	25	.06	2	.72	.01	.06	1	1
L48E 3+00S	1	20	17	83	.3	23	12	287	3.22	18	5	ND	2	21	1	2	2	58	.24	.029	14	38	.45	54	.07	2	1.36	.01	.05	1	2
STD C/AU 0.5	19	55	40	127	6.8	67	29	1068	3.93	35	20	8	33	47	17	16	21	60	.48	.104	40	58	.88	173	.08	39	1.73	.06	.13	14	490

E & B EXPLORATION PROJECT - 5055 FILE # 86-1803

PAGE 4

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au†
	PPH	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
L48E 3+50S	1	67	19	95	.9	60	17	1231	4.42	16	5	ND	3	56	1	2	2	58	.97	.058	20	73	.84	216	.06	6	2.68	.02	.13	1	5
L48E 3+75S	1	18	10	76	.2	20	8	385	2.44	9	5	ND	1	13	1	2	2	36	.21	.058	14	32	.44	41	.05	7	.93	.01	.06	2	2
L48E 4+00S	1	20	14	76	.3	18	7	197	2.38	10	5	ND	1	16	1	2	2	38	.26	.060	14	30	.47	54	.04	4	1.20	.01	.05	1	13
L48E 4+25S	1	12	10	65	.1	14	6	238	1.72	8	5	ND	2	12	1	2	2	30	.20	.048	14	23	.37	49	.05	4	.85	.01	.04	1	2
L48E 4+50S	1	13	8	82	.3	16	6	255	1.86	2	5	ND	1	12	1	2	2	32	.19	.034	13	24	.43	54	.05	2	1.04	.01	.05	1	50
L48E 4+75S	1	13	5	57	.2	15	5	181	2.01	8	5	ND	1	14	1	2	2	34	.23	.065	14	26	.42	44	.05	3	.87	.01	.07	1	4
L48E 5+00S	1	11	9	64	.2	11	5	336	1.59	7	5	ND	1	12	1	2	2	32	.23	.073	11	22	.31	71	.05	2	.84	.01	.05	1	1
L49E 0+25S	1	19	8	57	.3	18	7	409	2.00	8	5	ND	1	30	1	2	2	30	.52	.039	11	26	.42	76	.03	2	.99	.01	.06	1	2
L49E 0+50S	1	35	11	117	.3	25	13	1940	2.49	10	5	ND	1	36	1	2	2	37	.69	.097	10	35	.46	178	.03	4	1.40	.01	.12	1	4
L49E 0+75S	1	12	6	52	.1	16	6	213	1.82	9	5	ND	2	13	1	2	2	30	.23	.035	11	24	.40	40	.05	3	.84	.01	.06	1	3
L49E 1+00S	1	27	8	61	.1	27	10	418	2.53	14	5	ND	3	19	1	2	3	38	.31	.052	13	33	.57	47	.06	4	1.08	.01	.08	1	13
L49E 1+25S	1	38	14	71	.4	32	11	495	2.66	13	5	ND	2	26	1	2	2	40	.45	.031	19	36	.56	75	.05	5	1.27	.01	.08	1	4
L49E 1+50S	1	299	24	91	1.5	70	25	1115	4.74	18	5	ND	4	72	1	2	2	61	1.18	.072	39	84	.82	372	.05	3	3.10	.05	.18	1	9
L49E 1+75S	1	54	16	82	.6	39	14	672	3.54	18	5	ND	2	40	1	2	2	50	.66	.033	13	45	.56	153	.05	3	1.71	.01	.09	1	4
L49E 2+00S	1	106	12	88	.9	46	13	421	3.38	17	5	ND	1	67	1	2	2	49	1.24	.045	17	42	.54	145	.04	6	1.66	.01	.09	1	2
L49E 2+50S	1	69	14	82	.4	35	14	619	3.04	20	5	ND	1	64	1	2	2	45	1.27	.048	12	40	.58	98	.04	7	1.36	.01	.09	1	7
L49E 2+75S	1	13	8	121	.1	15	5	324	1.91	9	5	ND	2	16	1	2	2	36	.21	.015	11	23	.33	59	.05	2	.72	.01	.05	1	8
L49E 3+25S	1	34	13	61	.4	29	11	390	2.78	19	5	ND	1	33	1	2	2	39	.50	.037	11	38	.52	78	.05	3	1.21	.01	.05	1	20
L49E 3+50S	1	16	7	53	.4	17	6	198	2.08	9	5	ND	1	31	1	2	2	36	.56	.024	10	26	.35	63	.04	3	1.05	.01	.05	1	2
L49E 3+75S	1	14	11	58	.2	14	6	138	2.03	8	5	ND	3	13	1	2	2	37	.21	.046	12	24	.35	37	.04	2	.85	.01	.05	1	3
L49E 4+00S	1	21	9	69	.1	24	10	229	2.69	13	5	ND	4	14	1	2	2	40	.22	.041	14	33	.53	37	.06	4	1.15	.01	.05	1	2
L49E 4+25S	1	14	9	79	.1	17	6	326	1.96	6	5	ND	3	18	1	2	2	33	.35	.054	14	26	.38	67	.05	3	1.05	.01	.06	1	10
L49E 4+50S	1	11	5	75	.2	16	6	171	2.34	8	5	ND	2	11	1	2	2	37	.17	.113	14	27	.39	57	.04	3	1.14	.01	.05	1	4
L49E 4+75S	1	16	10	64	.1	24	7	207	2.35	8	5	ND	2	21	1	2	2	32	.36	.034	14	30	.56	68	.05	2	1.15	.01	.06	1	5
L49E 5+00S	1	14	7	58	.1	20	7	169	2.33	12	5	ND	2	17	1	2	2	35	.26	.068	13	26	.46	53	.04	3	1.03	.01	.06	1	255
L50E 0+25S	1	34	9	60	.1	19	10	216	2.94	10	5	ND	2	12	1	3	2	38	.17	.064	14	25	.40	84	.03	2	.88	.01	.07	1	5
L50E 0+50S	1	33	5	113	.4	21	10	193	3.70	11	5	ND	1	13	1	2	2	49	.19	.102	12	31	.52	65	.02	2	1.16	.01	.06	1	2
L50E 0+75S	1	20	3	63	.1	12	9	896	2.10	8	5	ND	1	11	1	2	2	36	.17	.047	11	20	.28	171	.03	2	.77	.01	.08	1	3
L50E 1+00S	1	24	6	111	.2	21	11	986	2.73	8	5	ND	1	20	1	2	3	37	.32	.067	13	32	.43	144	.03	2	1.22	.01	.10	1	295
L50E 1+25S	1	73	12	72	.7	37	16	725	3.79	22	5	ND	3	38	1	2	2	52	.71	.038	16	49	.68	173	.06	5	1.63	.01	.08	1	14
L50E 1+50S	1	37	14	71	.6	26	12	846	2.95	13	5	ND	2	40	1	2	3	43	.73	.029	13	38	.44	188	.05	3	1.44	.01	.06	1	1
L50E 1+75S	1	27	7	81	.2	23	8	291	2.39	10	5	ND	2	22	1	2	2	40	.35	.018	13	29	.41	88	.05	2	.95	.01	.06	1	3
L50E 2+00S	1	73	21	88	.7	41	15	765	3.40	16	5	ND	2	49	1	2	2	45	.94	.038	18	47	.65	145	.05	4	1.61	.01	.09	1	2
L50E 2+25S	2	40	14	78	.5	42	11	440	2.96	16	5	ND	2	29	1	2	3	39	.50	.026	14	40	.59	96	.05	2	1.32	.01	.07	1	1
L50E 2+50S	1	102	17	136	.9	42	15	1222	2.99	16	5	ND	2	163	2	2	2	39	4.64	.121	13	49	.72	194	.05	10	1.56	.02	.11	1	4
L50E 2+75S	1	121	12	114	1.6	44	16	1240	2.78	14	5	ND	1	150	4	2	2	35	4.26	.090	12	50	.45	231	.05	4	1.55	.01	.07	1	1
STD C/AU 0.5	20	61	38	128	6.8	69	29	1073	3.93	41	19	7	33	47	17	15	18	61	.48	.102	37	58	.88	176	.08	40	1.73	.06	.13	15	495



## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1807

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SAMPLE#	Hg	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
L50E 3+00S	1	59	21	81	.5	11	15	320	3.53	20	5	ND	2	90	1	2	2	45	1.76	.043	14	53	.52	184	.05	3	2.19	.01	.07	1	1
L50E 3+25S	1	29	12	60	.1	26	13	488	2.89	14	5	ND	3	25	1	2	2	41	.40	.019	13	37	.58	81	.05	3	1.25	.01	.08	1	1
L50E 3+50S	1	21	9	61	.1	22	8	183	2.68	11	5	ND	3	16	1	2	2	41	.17	.018	13	33	.50	37	.05	2	1.20	.01	.05	1	4
L50E 3+75S	1	29	13	73	.4	35	12	213	3.64	23	5	ND	3	39	1	2	2	52	.66	.037	12	44	.53	95	.06	2	2.12	.01	.06	1	1
L50E 4+00S	1	15	6	64	.1	19	7	189	2.18	11	5	ND	2	16	1	2	2	33	.26	.061	14	26	.50	41	.05	3	1.02	.01	.08	1	4
L50E 4+25S	1	15	6	71	.1	21	9	188	3.09	12	5	ND	3	15	1	2	2	47	.21	.046	13	33	.57	46	.05	3	1.34	.01	.04	1	1
L50E 4+50S	1	11	5	57	.1	15	5	160	1.64	5	5	ND	2	11	1	2	2	31	.18	.030	12	22	.36	37	.05	2	.88	.01	.04	1	50
L50E 4+75S	1	27	9	61	.1	26	9	280	2.41	12	5	ND	2	16	1	2	2	38	.24	.050	15	32	.55	50	.05	2	1.28	.01	.05	1	110
L50E 5+00S	1	13	6	55	.1	18	7	166	2.16	6	5	ND	2	15	1	2	2	37	.23	.040	12	25	.43	44	.04	4	1.08	.01	.05	1	1
L51E 0+25S	1	17	8	65	.2	18	9	361	2.95	7	5	ND	1	13	1	2	2	41	.19	.057	11	29	.45	97	.02	3	1.07	.01	.07	1	1
L51E 0+50S	1	7	3	55	.1	10	8	684	1.98	4	5	ND	2	14	1	2	2	28	.21	.039	11	20	.25	170	.04	3	.62	.01	.06	1	1
L51E 0+75S	1	7	8	73	.1	9	8	1751	1.52	4	5	ND	1	18	1	2	4	30	.32	.047	9	20	.20	133	.04	3	.58	.01	.09	1	1
L51E 1+00S	1	39	9	48	.1	16	13	313	3.79	11	5	ND	2	16	1	4	2	47	.29	.047	8	21	.33	84	.01	4	1.11	.01	.07	1	1
L51E 1+25S	1	26	11	78	.5	22	12	1464	2.25	8	5	ND	1	26	1	2	2	36	.49	.065	13	34	.39	96	.04	2	1.27	.01	.10	1	1
L51E 1+50S	1	13	8	71	.1	21	10	454	2.62	11	5	ND	3	16	1	2	2	40	.29	.019	13	32	.52	88	.05	2	1.10	.01	.06	1	1
L51E 1+75S	1	19	9	57	.1	20	9	170	3.06	10	5	ND	2	13	1	2	2	48	.19	.018	9	30	.42	44	.03	2	1.14	.01	.05	1	1
L51E 2+00S	1	54	15	95	.9	32	15	626	3.27	11	5	ND	2	57	1	2	2	43	1.32	.030	14	44	.65	203	.05	2	1.74	.01	.08	1	1
L51E 3+50S	1	38	8	80	.3	37	13	555	2.96	14	5	ND	1	28	1	2	2	43	.47	.039	16	40	.60	83	.04	4	1.69	.01	.07	1	1
L51E 3+75S	1	14	6	65	.1	15	8	288	2.10	8	5	ND	1	19	1	2	2	35	.30	.039	12	27	.42	46	.04	2	.98	.01	.07	1	1
L51E 4+00S	1	18	8	86	.1	22	9	242	2.55	10	5	ND	2	15	1	2	3	39	.21	.038	15	34	.58	71	.05	2	1.31	.01	.06	1	1
L51E 4+25S	1	27	7	69	.2	27	11	394	2.92	12	5	ND	2	20	1	2	2	44	.29	.050	18	41	.67	75	.05	2	1.52	.01	.08	1	2
L51E 4+50S	1	52	13	79	.5	33	13	917	3.02	12	5	ND	1	33	1	2	2	47	.53	.052	36	41	.50	108	.04	2	1.71	.01	.10	1	1
L51E 4+75S	1	54	17	68	.3	36	15	785	3.30	17	5	ND	4	22	1	2	2	49	.34	.051	23	48	.68	72	.07	4	1.57	.01	.09	1	1
L51E 5+00S	2	129	19	89	.8	72	26	1809	5.56	36	5	ND	1	44	1	2	2	82	.56	.074	48	72	.73	199	.06	3	3.00	.01	.13	1	1
L52E 0+25S	2	16	6	74	.2	12	6	196	1.74	16	5	ND	1	23	1	2	2	41	.35	.064	9	25	.30	72	.04	2	.77	.01	.07	1	1
L52E 0+50S	1	13	3	78	.1	20	7	204	2.00	3	5	ND	2	14	1	2	3	30	.21	.041	16	28	.55	59	.05	2	1.17	.01	.05	1	1
L52E 0+75S	1	20	7	68	.1	22	8	223	2.39	11	5	ND	3	14	1	2	2	35	.22	.033	18	32	.56	47	.05	3	1.11	.01	.06	1	1
L52E 1+00S	1	16	14	78	.1	24	8	203	2.93	13	5	ND	4	20	1	2	2	43	.30	.109	17	35	.59	59	.05	2	1.37	.01	.07	1	1
L52E 1+25S	1	13	10	66	.1	20	8	198	2.60	10	5	ND	3	14	1	2	2	39	.25	.041	16	32	.53	51	.05	5	1.20	.01	.09	1	75
L52E 1+50S	1	7	9	58	.1	11	4	206	1.55	5	5	ND	1	17	1	2	2	29	.32	.034	12	20	.26	42	.04	3	.68	.01	.07	1	2
L52E 1+75S	1	27	17	91	.2	31	13	360	3.60	17	5	ND	2	27	1	2	2	52	.43	.047	12	43	.52	80	.04	2	1.74	.01	.08	1	1
L52E 2+50S	1	19	10	68	.1	23	8	219	2.74	9	5	ND	2	15	1	2	2	40	.18	.023	16	39	.69	54	.04	2	1.51	.01	.06	1	1
L52E 2+75S	1	6	10	58	.1	9	4	110	1.52	3	5	ND	2	10	1	2	2	30	.13	.018	13	19	.28	37	.04	2	.86	.01	.03	1	1
L52E 3+00S	1	18	10	77	.1	22	9	299	2.50	6	5	ND	3	17	1	2	2	38	.23	.048	16	36	.67	65	.05	2	1.47	.01	.06	1	1
L52E 3+25S	2	49	20	130	.6	41	16	763	4.12	15	5	ND	1	33	1	2	2	61	.42	.091	16	62	.87	169	.03	2	2.88	.01	.18	1	1
L52E 3+50S	1	22	10	76	.1	24	8	217	2.61	6	5	ND	3	15	1	2	2	38	.22	.045	17	34	.66	51	.05	2	1.36	.01	.06	1	1
STD C/AU 0.5	20	56	40	130	6.9	65	29	1080	3.93	40	20	B	34	48	17	16	18	61	.48	.104	38	57	.88	178	.08	37	1.73	.06	.13	15	505

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SAMPLE#	Mc PPH	Cu PPH	Pb PPH	Zn PPH	Ag PPH	Ni PPH	Co PPH	Mn PPH	Fe %	As PPH	U PPH	Au PPH	Th PPH	Sr PPH	Cd PPH	Sb PPH	Bi PPH	V PPH	Ca %	P %	La PPH	Cr PPH	Mg %	Ba PPH	Ti %	R PPH	Al %	Na %	K %	M PPH	Au# PPB
LS2E 3+75S	1	11	9	78	.2	17	6	153	2.29	6	5	ND	2	12	1	2	2	37	.18	.069	15	27	.45	55	.05	2	1.09	.01	.05	1	4
LS2E 4+00S	1	9	12	59	.1	14	6	430	1.64	6	5	ND	2	12	1	2	2	30	.18	.044	15	22	.36	85	.05	2	.86	.01	.05	1	1
LS2E 4+25S	1	12	5	74	.2	18	9	654	2.20	6	5	ND	1	17	1	2	2	36	.29	.055	15	27	.45	95	.05	2	1.12	.01	.09	1	1
LS2E 4+50S	1	17	10	70	.1	27	10	180	3.26	7	5	ND	3	12	1	2	2	43	.20	.085	14	38	.54	42	.05	2	1.61	.01	.06	1	1
LS2E 4+75S	1	30	10	78	.1	20	11	378	3.16	10	5	ND	3	16	1	2	2	57	.33	.090	13	35	.49	67	.06	2	1.21	.01	.07	1	135
LS2E 5+00S	1	22	11	65	.2	24	10	253	2.79	12	5	ND	3	15	1	2	2	40	.20	.067	16	35	.61	59	.06	2	1.20	.01	.06	1	1
LS3E 0+25S	4	67	9	187	.4	35	17	467	4.48	70	5	ND	2	16	1	5	2	102	.29	.118	5	52	.76	74	.03	4	1.66	.01	.08	1	2
LS3E 0+50S	3	65	11	95	.2	49	16	342	3.90	45	5	ND	2	16	1	3	2	71	.31	.100	8	51	.67	55	.04	3	1.61	.01	.07	1	3
LS3E 0+75S	1	29	11	70	.1	31	11	298	2.90	16	5	ND	4	16	1	2	2	40	.24	.038	17	38	.67	35	.07	2	1.21	.01	.07	1	2
LS3E 1+00S	1	49	15	93	.1	37	15	605	3.48	18	5	ND	5	19	1	2	2	43	.33	.053	18	43	.76	67	.06	3	1.41	.01	.10	1	3
LS3E 1+25S	1	48	11	166	.4	30	15	915	3.20	27	5	ND	1	32	1	2	2	55	.56	.059	10	40	.51	97	.04	2	1.37	.01	.08	1	2
LS3E 1+50S	1	18	9	55	.3	12	8	231	2.60	13	5	ND	1	24	1	2	2	50	.29	.050	8	27	.13	80	.03	2	.66	.01	.07	1	95
LS3E 1+75S	1	14	6	82	.1	16	8	315	2.50	13	5	ND	2	18	1	2	2	43	.31	.038	12	28	.39	59	.04	2	1.12	.01	.06	1	1
LS3E 2+00S	3	125	18	150	1.8	83	22	1211	5.80	46	11	ND	2	104	1	2	2	75	2.65	.129	34	88	.83	218	.05	3	3.74	.01	.16	1	4
LS3E 2+25S	1	18	8	72	.1	25	8	251	2.42	9	5	ND	2	14	1	2	2	34	.20	.044	15	35	.64	44	.05	5	1.31	.01	.06	1	105
LS3E 2+50S	1	24	14	72	.4	27	10	257	3.09	11	5	ND	3	16	1	2	2	41	.21	.060	14	40	.72	51	.05	3	1.52	.01	.06	1	1
LS3E 2+75S	1	25	8	86	.1	31	10	251	3.38	13	5	ND	4	14	1	2	2	43	.18	.087	15	41	.74	73	.05	2	1.55	.01	.06	1	3
LS3E 3+00S	1	9	8	85	.2	16	6	266	2.15	6	5	ND	2	14	1	2	2	33	.23	.060	13	27	.45	57	.04	2	1.04	.01	.05	1	1
LS3E 3+25S	1	14	10	117	.2	21	8	231	2.39	5	5	ND	3	15	1	2	2	35	.23	.046	15	32	.58	72	.05	2	1.31	.01	.05	1	2
LS3E 3+50S	1	10	10	93	.2	18	6	446	2.24	6	5	ND	1	31	1	2	2	38	.53	.104	10	27	.34	88	.04	2	1.03	.01	.11	1	13
LS3E 3+75S	1	14	9	83	.3	20	6	200	2.21	6	5	ND	3	14	1	2	2	33	.22	.058	16	29	.48	51	.05	2	1.12	.01	.06	1	1
LS3E 4+00S	1	16	6	75	.3	24	8	290	2.49	8	5	ND	2	17	1	2	2	34	.26	.060	17	35	.69	55	.05	2	1.38	.01	.07	1	1
LS3E 4+25S	1	64	15	136	1.3	54	18	1351	4.13	14	5	ND	1	31	1	2	2	54	.42	.134	27	60	.72	183	.04	2	2.60	.01	.15	1	4
LS3E 4+50S	1	30	4	73	.1	23	10	306	2.97	10	5	ND	2	14	1	2	2	52	.23	.089	14	32	.54	64	.05	2	1.16	.01	.07	1	1
LS3E 4+75S	1	12	8	104	.1	18	8	578	2.22	6	5	ND	2	16	1	2	2	32	.28	.129	12	27	.38	128	.05	2	.91	.01	.07	1	1
LS4E 5+00S	1	21	6	93	.2	27	10	239	3.11	9	5	ND	4	18	1	2	2	45	.32	.145	15	38	.64	99	.05	2	1.53	.01	.08	1	1
LS4E 0+25S	2	31	10	74	.1	20	10	253	2.79	34	5	ND	1	15	1	2	2	64	.29	.050	8	34	.42	74	.03	2	1.07	.01	.06	1	175
LS4E 0+50S	4	61	10	162	.1	41	16	285	4.49	60	5	ND	2	15	1	3	2	91	.28	.123	8	55	.61	64	.04	2	1.74	.01	.07	1	3
LS4E 0+75S	3	54	8	149	.1	49	16	306	4.31	42	5	ND	3	17	1	2	2	77	.30	.130	10	56	.73	75	.04	2	1.82	.01	.08	3	43
LS4E 1+00S	1	28	7	152	.4	32	10	278	2.58	15	5	ND	1	26	1	2	2	51	.42	.055	9	39	.51	79	.04	4	1.31	.01	.08	1	3
LS4E 2+00S	3	38	15	189	.4	26	14	1562	3.02	39	5	ND	1	23	1	2	2	70	.38	.091	8	41	.42	178	.04	2	1.07	.01	.06	1	1
LS4E 2+25S	1	28	7	118	.5	23	10	673	2.59	24	5	ND	1	23	1	2	2	57	.40	.069	10	39	.48	97	.05	2	.97	.01	.08	1	1
LS4E 2+50S	1	25	6	120	.1	19	10	460	3.04	32	5	ND	1	19	1	2	2	62	.34	.182	6	36	.36	129	.04	3	1.00	.01	.08	1	4
LS4E 2+75S	1	16	9	76	.3	24	8	286	2.14	9	5	ND	2	14	1	2	3	35	.24	.057	10	28	.42	52	.04	2	1.03	.01	.04	1	3
LS4E 3+00S	1	21	9	78	.2	29	9	268	2.58	7	5	ND	2	15	1	2	2	37	.24	.059	15	36	.64	53	.05	2	1.25	.01	.05	1	4
LS4E 3+25S	1	13	4	77	.3	25	8	225	2.38	7	5	ND	3	17	1	2	2	34	.24	.056	14	31	.58	55	.05	2	1.19	.01	.05	1	1
STD C/AU-0.5	21	59	42	136	7.0	69	31	1130	4.13	40	20	8	35	49	19	16	20	64	.50	.106	38	60	.91	182	.08	36	1.73	.07	.14	15	510

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
LS4E 3+50S	1	19	13	87	.2	24	7	252	2.42	9	5	ND	1	19	1	2	2	36	.32	.069	14	33	.59	66	.04	2	1.20	.01	.07	1	2
LS4E 3+75S	1	30	11	128	.2	30	10	392	3.26	22	5	ND	1	19	1	2	2	72	.29	.105	7	42	.49	102	.03	3	1.51	.01	.06	1	60
LS4E 4+00S	1	18	12	71	.2	25	8	252	2.66	8	5	ND	2	15	1	2	4	37	.20	.045	14	35	.66	60	.05	2	1.28	.01	.05	1	3
LS4E 4+25S	1	14	6	72	.3	19	6	149	2.19	6	5	ND	1	14	1	2	2	34	.20	.040	11	28	.43	52	.04	6	1.11	.01	.04	1	2
LS4E 4+50S	1	18	15	82	.2	24	8	218	2.76	10	5	ND	3	15	1	2	2	38	.20	.066	13	34	.59	53	.04	8	1.19	.01	.05	1	13
LS4E 4+75S	1	14	11	76	.1	22	6	242	2.20	4	5	ND	1	14	1	2	2	32	.19	.058	12	27	.52	49	.04	2	1.06	.01	.05	1	2
LS4E 5+00S	1	35	13	100	.2	20	10	345	3.00	10	5	ND	1	17	1	2	3	48	.24	.110	10	35	.54	80	.03	3	1.41	.01	.06	1	1
LS5E 0+25S	3	262	23	123	1.7	77	27	2755	3.85	54	5	ND	1	80	2	3	2	60	2.11	.112	22	72	.96	150	.03	8	1.69	.01	.09	1	20
LS5E 0+50S	1	199	19	130	1.1	46	18	329	3.76	46	5	ND	1	50	2	2	2	66	1.07	.040	14	70	.54	120	.05	7	1.70	.01	.04	1	7
LS5E 0+75S	1	93	16	138	.4	35	21	845	3.73	37	5	ND	1	47	2	2	2	54	.95	.037	11	54	.75	113	.04	5	1.59	.01	.06	2	5
LS5E 1+00S	3	176	20	234	1.0	44	23	1124	3.72	47	5	ND	1	84	4	3	2	66	2.19	.095	11	55	.57	148	.03	3	1.66	.01	.06	2	31
LS5E 1+25S	4	236	21	141	1.6	62	29	3422	3.41	42	6	ND	1	86	4	3	2	49	2.19	.074	13	48	.58	192	.04	5	1.64	.02	.05	1	11
LS5E 1+50S	2	49	11	159	.3	29	15	621	3.66	46	5	ND	1	39	1	4	2	66	.83	.039	6	44	.61	97	.04	5	1.46	.01	.05	2	14
LS5E 1+75S	1	20	8	96	.1	20	9	264	2.74	23	5	ND	1	16	1	2	2	59	.34	.052	8	33	.43	44	.03	4	1.03	.01	.05	1	34
LS5E 2+00S	1	34	14	120	.2	30	11	783	2.98	14	5	ND	2	21	1	2	2	41	.35	.053	11	39	.56	120	.04	3	1.39	.01	.08	1	5
LS5E 2+25S	1	35	20	182	.3	35	15	562	3.56	17	5	ND	2	20	1	2	2	56	.36	.067	9	46	.64	105	.04	3	1.65	.01	.08	1	7
LS5E 2+50S	1	90	11	89	.6	37	14	777	3.16	20	6	ND	1	63	1	2	2	39	1.55	.091	12	44	.67	135	.03	4	1.35	.01	.09	2	8
LS5E 2+75S	1	80	11	92	.6	30	13	973	2.98	19	7	ND	1	80	1	2	2	36	2.18	.098	9	40	.58	138	.02	7	1.20	.01	.08	1	5
LS5E 3+00S	1	149	19	99	.9	64	21	1184	4.84	34	5	ND	1	35	1	2	2	58	.53	.088	35	67	.77	170	.04	4	2.19	.01	.11	1	5
LS5E 3+25S	1	64	12	103	.5	40	14	520	3.71	38	5	ND	1	25	1	2	2	55	.42	.055	16	49	.66	85	.05	6	1.50	.01	.08	1	10
LS5E 3+50S	1	91	18	115	.4	47	18	670	3.86	39	5	ND	1	26	1	2	2	62	.35	.046	24	56	.76	84	.04	2	1.92	.01	.08	1	7
LS5E 3+75S	1	42	5	74	.3	31	10	204	2.95	26	5	ND	2	16	1	2	2	50	.22	.046	10	38	.62	45	.04	5	1.29	.01	.04	1	12
LS5E 4+00S	1	18	9	82	.3	18	8	186	2.04	11	5	ND	1	19	1	2	2	39	.26	.024	11	28	.41	50	.04	2	.97	.01	.06	1	12
LS5E 4+75S	1	174	29	133	1.6	90	25	1519	5.33	31	5	ND	1	48	1	2	2	74	.71	.079	47	78	.99	234	.05	3	3.13	.01	.15	1	7
LS6E 0+25S	2	76	15	214	.3	40	26	2130	4.93	51	5	ND	1	33	1	3	2	103	.65	.090	5	79	.76	160	.04	2	1.66	.01	.06	2	7
LS6E 0+50S	5	383	21	150	2.1	100	35	3773	4.37	44	5	ND	1	62	2	2	2	63	1.54	.070	42	74	.79	262	.04	5	2.29	.02	.09	1	19
LS6E 1+00S	3	92	11	169	.3	37	23	1309	4.28	32	5	ND	1	43	2	2	2	76	.97	.052	7	59	.57	135	.03	2	1.70	.01	.06	1	7
LS6E 1+25S	1	96	11	91	1.0	41	17	1048	3.46	29	5	ND	1	59	1	2	2	47	1.61	.054	10	48	.73	142	.04	4	1.63	.01	.07	1	6
LS6E 1+50S	7	135	18	128	.8	51	22	4288	3.51	29	6	ND	1	78	2	2	2	47	2.25	.075	13	49	.70	230	.04	4	1.65	.01	.09	1	5
LS6E 1+75S	1	86	14	85	.5	36	16	1221	3.05	27	5	ND	1	54	1	2	2	41	1.55	.071	12	42	.67	111	.03	5	1.36	.01	.06	1	6
LS6E 2+00S	1	49	18	111	.6	31	13	724	3.15	17	5	ND	2	44	1	2	2	40	1.08	.037	14	39	.63	121	.04	6	1.59	.01	.08	1	4
LS6E 2+50S	1	33	17	59	.1	25	10	280	2.55	14	5	ND	3	13	1	2	2	39	.24	.024	13	34	.57	66	.04	4	1.11	.01	.07	1	10
LS6E 4+25S	3	24	11	59	.4	18	15	11176	2.85	25	5	ND	1	86	1	2	5	49	1.38	.044	5	33	.49	257	.02	3	.94	.01	.04	1	4
LS6E 4+50S	1	32	14	148	.1	20	13	965	3.39	31	5	ND	1	22	1	3	5	62	.37	.095	10	35	.40	136	.04	3	1.00	.01	.08	1	130
LS6E 5+00S	1	8	10	53	.2	8	5	628	1.46	7	5	ND	1	12	1	2	2	39	.21	.034	8	22	.21	61	.05	2	.58	.01	.06	1	3
LS7E 0+25S	1	27	7	66	.1	31	11	420	2.51	18	5	ND	1	18	1	2	2	41	.35	.046	9	38	.60	63	.04	2	1.08	.01	.06	1	2
STD C/AU 0.5	20	59	46	135	7.1	69	30	1129	4.13	39	21	7	35	50	18	18	19	64	.50	.107	39	60	.93	184	.08	38	1.81	.07	.13	15	495

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1803

PAGE 8

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L57E 0+50S	2	46	13	92	.2	35	17	497	3.42	20	6	ND	1	31	1	2	2	63	.55	.058	10	49	.67	94	.05	9	1.58	.01	.10	1	4
L57E 0+75S	2	36	9	97	.1	28	13	327	3.55	18	5	ND	1	20	1	2	2	66	.32	.096	8	44	.52	67	.04	6	1.55	.01	.08	1	3
L57E 1+00S	2	117	12	101	.1	107	35	1399	5.73	61	5	ND	1	30	1	2	2	99	.64	.123	6	130	1.45	122	.07	7	1.87	.02	.12	1	1
L57E 1+25S	2	99	17	119	.2	52	22	811	4.38	38	5	ND	2	24	1	2	2	75	.39	.062	9	66	.78	147	.05	2	1.90	.01	.08	1	12
L57E 1+50S	3	87	13	91	.3	47	19	695	4.18	34	5	ND	2	26	1	2	3	84	.42	.039	9	63	.70	118	.05	2	1.84	.01	.08	1	3
L57E 1+75S	2	103	17	107	.7	50	23	1041	4.14	36	6	ND	2	71	1	2	3	63	1.66	.071	14	67	.91	137	.05	6	1.68	.01	.08	1	3
L57E 2+00S	3	40	12	71	.1	38	14	302	3.56	17	5	ND	4	22	1	2	2	51	.34	.022	15	48	.66	92	.06	3	1.72	.01	.06	1	1
L57E 2+25S	3	52	8	92	.1	41	16	338	3.92	35	5	ND	2	17	1	2	3	67	.30	.051	9	49	.61	62	.05	4	1.69	.01	.06	1	6
L57E 2+50S	2	49	8	87	.2	42	18	862	4.42	25	5	ND	1	31	1	2	3	99	.64	.080	7	84	1.12	100	.07	3	1.62	.02	.08	1	3
L57E 2+75S	4	27	7	56	.1	20	7	148	2.51	20	5	ND	1	25	1	2	2	70	.46	.040	8	28	.31	48	.02	2	.95	.01	.04	1	1
L57E 3+00S	2	20	5	46	.1	17	7	113	2.31	13	5	ND	2	10	1	2	3	46	.16	.024	10	27	.27	26	.05	3	.80	.01	.03	1	20
L57E 4+50S	2	14	8	55	.2	12	7	173	2.32	12	5	ND	1	15	1	2	5	77	.27	.019	8	32	.22	45	.04	4	.95	.01	.03	1	6
L57E 4+75S	2	92	13	111	.1	48	20	664	5.00	49	5	ND	1	28	1	2	3	98	.41	.146	9	62	.77	125	.04	2	1.80	.01	.08	1	12
L57E 5+00S	1	28	7	162	.2	30	16	383	4.01	18	5	ND	1	15	1	2	3	77	.21	.085	10	52	.46	100	.04	4	1.50	.01	.06	1	5
L58E 0+25S	2	29	7	86	.1	28	13	443	2.66	15	5	ND	1	17	1	2	2	63	.36	.066	9	47	.57	71	.05	2	1.20	.01	.08	1	2
L58E 0+50S	3	30	11	134	.2	28	16	2041	2.85	27	5	ND	1	27	2	2	2	69	.45	.104	7	40	.44	160	.04	2	1.11	.01	.08	1	1
L58E 0+75S	2	31	6	75	.2	20	11	672	2.40	20	5	ND	1	18	1	2	2	68	.37	.039	8	37	.44	68	.04	4	1.09	.01	.08	1	26
L58E 1+00S	1	23	8	82	.1	21	12	273	2.76	17	5	ND	1	17	1	2	2	71	.30	.055	9	39	.50	63	.04	4	1.31	.01	.05	1	3
L58E 1+25S	2	48	5	101	.1	34	15	401	3.70	34	5	ND	2	17	1	2	2	79	.32	.095	9	50	.66	70	.04	2	1.46	.01	.08	1	105
L58E 1+50S	2	75	8	124	.1	54	20	410	4.71	46	5	ND	2	17	1	2	2	89	.31	.081	11	73	.89	63	.05	2	1.99	.01	.08	1	20
L58E 1+75S	1	31	12	101	.1	24	12	485	2.87	15	5	ND	3	23	1	2	2	45	.44	.072	10	36	.60	79	.07	5	1.42	.01	.19	1	1
L58E 2+00S	1	15	9	61	.1	17	7	217	2.27	5	5	ND	2	20	1	2	2	40	.33	.030	12	28	.42	50	.04	4	1.08	.01	.05	1	1
L58E 2+25S	2	72	19	167	.1	37	23	2154	4.40	39	5	ND	1	35	1	2	2	71	.60	.181	10	50	.61	219	.03	10	1.68	.01	.12	1	1
L58E 2+50S	2	87	17	120	.2	54	24	814	5.28	51	5	ND	1	21	1	35	2	101	.46	.112	9	78	1.16	106	.06	3	1.83	.01	.08	1	5
L58E 2+75S	1	49	17	117	.1	30	20	1093	4.56	38	5	ND	1	31	1	3	2	84	.64	.112	7	51	.80	122	.06	11	1.45	.01	.12	1	1
L58E 3+00S	3	85	17	89	.2	46	23	806	4.29	40	5	ND	2	39	1	2	4	69	.77	.036	10	58	.68	107	.04	2	1.61	.01	.07	1	4
L58E 3+25S	4	210	19	190	1.1	63	30	2383	5.00	48	5	ND	1	54	1	2	2	69	.99	.054	19	69	.84	164	.05	5	1.95	.01	.07	1	335
L58E 3+50S	3	206	24	201	1.1	58	30	2288	4.45	43	5	ND	1	80	2	2	5	71	1.76	.068	23	53	.57	179	.04	5	1.86	.01	.07	1	2
L58E 3+75S	3	290	23	157	1.0	59	30	854	4.87	57	5	ND	1	67	1	3	3	74	1.42	.078	22	75	.81	131	.03	4	1.94	.01	.07	1	11
L58E 4+00S	2	75	7	95	.2	34	18	816	4.03	37	5	ND	1	55	1	2	2	61	1.49	.097	11	63	1.00	97	.03	4	1.46	.01	.07	1	260
L58E 4+50S	1	12	8	77	.1	11	7	366	2.60	13	5	ND	1	16	1	2	2	83	.27	.036	11	29	.27	66	.06	8	.94	.01	.04	1	2
L58E 5+00S	2	31	10	118	.3	24	13	440	3.80	29	5	ND	1	20	1	2	2	88	.29	.065	12	42	.46	105	.05	3	1.18	.01	.07	1	10
L59E 0+00S	6	134	33	86	.1	41	30	624	6.63	428	5	ND	2	15	1	28	2	58	.19	.031	10	44	.24	65	.01	3	.78	.01	.11	1	26
L59E 0+25S	5	202	20	138	.2	48	35	1423	6.91	53	5	ND	1	36	1	4	2	143	.74	.067	9	83	.71	172	.02	2	1.65	.01	.09	1	1
L59E 0+50S	2	37	10	99	.3	24	13	475	2.87	30	5	ND	1	19	1	2	2	70	.35	.052	8	35	.47	85	.03	2	1.21	.01	.10	1	21
L59E 0+75S	1	22	6	64	.1	22	9	438	2.36	13	5	ND	1	14	1	2	2	43	.24	.051	11	32	.47	70	.04	6	.98	.01	.07	1	24
STD C/AU-0.5	20	58	41	131	6.7	69	29	1091	3.93	37	21	8	34	48	18	15	20	62	.48	.106	38	59	.88	181	.08	39	1.73	.06	.13	14	490

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1803

PAGE 9

SAMPLER	Hc PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Cc PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Rb PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS9E 1+00E	1	23	11	76	.2	25	9	279	2.45	13	5	ND	1	16	1	2	4	45	.30	.060	11	31	.46	74	.03	7	1.11	.01	.07	1	4
LS9E 1+25E	1	15	10	66	.1	19	8	415	2.23	10	5	ND	1	17	1	2	2	39	.34	.057	9	26	.45	70	.05	4	1.01	.01	.07	1	1
LS9E 1+50E	1	12	7	61	.3	14	7	539	1.62	7	5	ND	1	20	1	2	3	31	.38	.055	7	21	.27	84	.04	3	.67	.01	.06	1	6
LS9E 1+75E	2	59	8	53	.5	15	2	158	.40	3	5	ND	3	207	1	2	4	4	20.67	.111	2	38	.30	111	.01	12	.19	.01	.04	1	1
LS9E 2+00E	3	30	11	162	.2	30	14	497	3.38	21	5	ND	2	21	1	2	2	55	.41	.061	8	45	.61	121	.04	5	1.52	.01	.07	1	55
LS9E 2+25E	2	63	12	119	.1	36	18	701	4.03	33	5	ND	1	20	1	2	2	69	.36	.072	5	47	.59	101	.03	3	1.40	.01	.07	1	55
LS9E 2+50E	1	54	17	116	.1	37	24	1036	5.57	29	5	ND	1	22	1	2	2	113	.46	.104	3	95	.65	85	.05	2	1.09	.01	.08	2	3
LS9E 2+75E	1	31	12	136	.2	23	13	2223	2.40	16	5	ND	1	33	1	2	2	44	.68	.048	4	32	.38	218	.04	5	.90	.01	.07	1	6
LS9E 3+00E	4	22	7	38	.4	11	4	124	1.46	15	5	ND	1	45	1	2	2	39	1.08	.059	2	16	.13	90	.03	5	.39	.01	.07	1	1
LS9E 3+25E	3	34	9	94	.4	19	10	590	2.79	25	5	ND	1	36	1	2	2	71	.82	.049	3	36	.33	86	.05	5	.87	.01	.06	1	5
LS9E 3+50E	3	148	10	100	.7	39	9	1032	1.24	12	7	ND	2	153	3	4	3	21	10.55	.130	5	41	.45	118	.01	16	.64	.01	.07	1	1
LS9E 4+00E	2	132	16	125	.9	32	16	730	2.89	22	6	ND	1	89	1	2	2	38	2.48	.079	7	70	.46	132	.05	8	1.62	.01	.06	1	2
LS9E 4+25E	2	104	18	130	.5	32	21	1297	3.37	39	5	ND	1	67	1	2	2	47	1.90	.042	4	58	.62	139	.05	9	1.42	.01	.07	1	1
LS9E 4+75E	1	30	12	80	.2	17	9	256	3.47	26	5	ND	1	18	1	2	2	87	.32	.037	3	37	.30	63	.06	5	.99	.01	.04	1	3
LS9E 5+00E	1	26	9	100	.3	23	11	283	3.16	18	5	ND	2	16	1	2	2	54	.23	.111	8	35	.40	79	.05	3	1.24	.01	.05	1	18
L60E 0+25E	2	40	13	151	.3	35	19	3296	3.15	25	5	ND	1	36	1	2	2	71	.68	.128	3	45	.48	311	.03	2	1.42	.01	.09	1	2
L60E 0+50E	2	29	9	94	.2	25	15	1579	2.50	20	5	ND	1	27	1	2	2	53	.54	.083	6	33	.43	137	.05	3	1.09	.01	.08	1	3
L60E 0+75E	2	58	5	115	.2	53	17	491	3.39	42	5	ND	2	27	1	2	2	63	.38	.070	8	55	.84	87	.05	4	1.44	.02	.09	1	10
L60E 1+00E	3	61	13	99	.2	45	17	651	4.16	60	5	ND	1	15	1	5	2	73	.28	.074	8	47	.61	85	.04	3	1.47	.01	.09	1	6
L60E 1+25E	1	21	7	56	.1	20	8	325	2.29	16	5	ND	2	19	1	2	2	52	.24	.050	10	35	.41	74	.03	3	1.01	.01	.06	1	2
L60E 1+50E	2	21	7	79	.1	28	12	413	2.72	11	5	ND	1	15	1	2	2	54	.30	.063	8	48	.55	108	.04	3	1.11	.01	.07	1	3
L60E 1+75E	1	21	10	70	.1	18	10	238	2.56	11	5	ND	1	10	1	2	2	48	.20	.040	10	31	.48	80	.05	2	1.27	.01	.04	1	5
L60E 2+00E	1	26	11	59	.1	22	10	391	2.65	15	5	ND	2	16	1	2	2	44	.32	.053	11	34	.55	60	.05	5	1.23	.01	.08	1	13
L60E 2+25E	1	24	7	124	.1	18	12	1983	2.28	12	5	ND	1	17	1	2	2	38	.29	.092	9	28	.36	196	.04	2	1.07	.01	.05	1	3
L60E 2+50E	8	117	17	140	2.1	69	22	5170	4.75	32	5	ND	1	68	2	2	2	63	1.49	.069	12	90	.76	316	.06	8	2.36	.01	.14	1	7
L60E 2+75E	1	29	7	79	.2	23	10	457	2.72	12	5	ND	3	18	1	2	2	42	.29	.053	14	35	.63	72	.07	2	1.11	.01	.08	1	9
L60E 3+00E	1	14	9	74	.2	17	8	500	2.38	11	5	ND	1	18	1	2	2	39	.27	.064	9	27	.38	72	.05	2	.93	.01	.06	1	19
L60E 3+25E	1	21	13	75	.1	22	11	290	2.71	11	5	ND	3	15	1	2	2	44	.22	.107	12	34	.47	63	.05	3	1.25	.01	.06	1	4
L60E 3+50E	1	17	12	63	.1	21	9	218	2.36	6	5	ND	2	13	1	2	2	35	.21	.052	14	30	.52	45	.06	2	1.05	.01	.06	1	6
L60E 3+75E	1	11	4	53	.1	15	8	429	2.09	7	5	ND	2	10	1	2	2	30	.17	.041	11	26	.40	35	.05	2	.89	.01	.05	1	5
L60E 4+00E	2	26	13	72	.1	23	12	443	3.08	16	5	ND	2	18	1	3	2	46	.32	.045	8	33	.42	67	.04	2	1.17	.01	.06	1	125
L60E 4+25E	2	47	14	86	.2	25	13	317	3.85	28	5	ND	1	37	1	2	2	70	.70	.047	9	38	.46	79	.04	3	1.50	.01	.06	1	8
L60E 4+50E	1	25	12	97	.1	22	11	230	3.28	29	5	ND	2	12	1	2	2	56	.22	.073	8	33	.46	35	.05	2	1.11	.01	.04	1	51
L60E 4+75E	2	36	9	119	.1	28	13	282	3.88	36	5	ND	2	25	1	2	2	75	.48	.043	7	41	.48	80	.06	7	1.36	.01	.07	1	11
L61E 0+25E	5	211	9	206	.4	118	25	338	5.75	271	5	ND	3	12	1	30	2	43	.18	.085	12	33	.43	42	.02	4	.90	.01	.07	1	14
L61E 0+50E	3	113	5	107	.1	42	22	616	4.10	39	5	ND	1	22	1	2	2	91	.72	.173	3	64	1.14	76	.08	4	2.04	.01	.07	1	33
STD C/AU-C. E	20	58	40	130	6.9	66	29	1078	3.92	40	19	7	33	46	16	16	19	61	.48	.103	35	58	.88	173	.08	36	1.73	.06	.13	14	490

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1907

PAGE 10

SAMPLE#	Mc	Cu	Pb	Zn	Ag	Mi	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L61E 0+75E	1	41	10	201	.3	37	23	599	3.90	32	5	ND	1	21	1	2	3	84	.38	.250	8	52	.52	96	.05	2	1.74	.01	.08	2	3
L61E 1+00E	1	17	9	84	.1	16	10	770	2.17	17	5	ND	1	14	1	2	2	39	.23	.074	11	30	.35	91	.04	3	.80	.01	.08	1	2
L61E 1+25E	2	52	6	114	.1	36	16	1071	2.99	32	5	ND	1	22	1	2	2	55	.39	.082	11	46	.55	188	.04	4	1.12	.01	.07	1	24
L61E 1+50E	1	26	7	138	.3	35	14	819	2.87	16	5	ND	1	21	1	2	4	62	.41	.081	10	64	.60	138	.04	3	1.26	.01	.09	1	2
L61E 1+75E	2	61	10	114	.2	50	16	479	3.68	31	5	ND	2	14	1	2	2	71	.23	.069	11	52	.64	107	.05	3	1.72	.01	.07	2	8
L61E 2+00E	3	53	13	85	.1	45	13	230	3.22	33	5	ND	1	16	1	3	2	59	.28	.075	10	44	.62	49	.04	5	1.31	.01	.05	1	6
L61E 2+25E	2	55	7	101	.2	45	18	1260	3.08	32	5	ND	1	20	1	9	3	59	.34	.071	9	46	.50	117	.04	3	1.18	.01	.06	1	45
L61E 2+50E	2	70	7	79	.2	36	15	373	3.47	40	5	ND	2	16	1	2	3	56	.27	.088	11	48	.52	52	.03	3	1.17	.01	.07	1	15
L61E 2+75E	1	12	11	84	.1	15	9	1553	1.66	9	5	ND	1	21	1	2	2	30	.35	.071	9	23	.27	140	.04	3	.68	.01	.08	1	1
L61E 3+00E	1	30	9	111	.1	27	13	247	4.26	28	5	ND	1	15	1	2	4	78	.24	.161	11	46	.48	71	.05	6	1.56	.01	.07	1	8
L61E 3+25E	1	24	9	58	.1	24	9	231	2.54	15	5	ND	2	15	1	2	2	42	.25	.068	12	33	.50	47	.05	3	1.11	.01	.06	1	7
L61E 3+50E	1	16	2	76	.1	17	9	393	2.44	19	5	ND	2	15	1	2	2	42	.25	.096	10	28	.36	65	.05	2	.97	.01	.06	1	6
L61E 3+75E	1	32	12	64	.1	26	12	303	2.87	17	5	ND	3	18	1	2	2	47	.29	.071	11	38	.58	52	.05	4	1.21	.01	.06	1	9
L61E 4+00E	1	16	6	78	.1	19	10	214	3.01	18	5	ND	2	16	1	2	2	52	.31	.072	8	33	.40	46	.04	4	1.23	.01	.07	1	1
L61E 4+25E	1	15	16	62	.1	23	10	201	2.57	12	5	ND	3	12	1	2	3	39	.19	.028	11	34	.51	40	.05	3	1.19	.01	.05	1	6
L61E 4+50E	1	37	13	80	.5	32	13	1440	2.90	16	5	ND	1	25	1	2	3	45	.46	.050	13	43	.51	101	.04	5	1.46	.01	.08	1	5
L61E 4+75E	1	17	13	51	.1	18	8	190	2.41	19	5	ND	3	13	1	2	4	41	.20	.020	9	30	.43	32	.06	3	.91	.01	.04	1	4
L61E 5+00E	3	150	15	64	1.2	39	24	2162	3.18	33	5	ND	1	69	2	2	2	43	1.52	.065	11	42	.36	140	.06	2	1.45	.01	.06	1	34
STD C/AU 0.5	21	57	42	134	7.0	70	30	1118	3.94	42	19	8	34	49	18	15	21	63	.48	.112	37	61	.88	181	.08	36	1.73	.07	.13	14	510

alt  
K. McLaughlin

RECEIVED  
AUG 22 1986  
REGISTERED

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
THIS LEACH IS PARTIAL FOR MM.FE.CA.P.CR.MG.BA.TI.B.AL.WA.K.W.SI.ZR.CE.SM.Y.ND AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.  
- SAMPLE TYPE: SOILS -BOMESH AU8 ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 16 1986 DATE REPORT MAILED: Aug 20/86 ASSAYER: D. Jones DEAN TOYE. CERTIFIED B.C. ASSAYER.

E & B EXPLORATION PROJECT - 5055 FILE # 86-2093 need from here PAGE 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
44E 15+50N	1	167	16	140	1.0	52	24	2298	4.87	68	5	ND	2	45	2	2	119	.90	.070	23	86	1.16	189	.05	2	2.31	.06	.13	1	7	
44E 15+25N	1	69	9	87	.1	35	16	655	3.62	50	5	ND	2	27	1	2	90	.50	.040	10	56	.85	107	.04	4	1.53	.04	.07	1	7	
44E 15+00N	1	35	7	61	.2	18	11	455	2.51	25	5	ND	1	31	1	2	79	.47	.035	10	36	.31	85	.04	3	1.05	.03	.06	1	2	
44E 14+75N	1	22	7	52	.1	14	7	161	2.08	20	5	ND	1	19	1	2	72	.30	.029	10	29	.27	60	.04	2	.81	.02	.07	1	1	
44E 14+50W	1	34	8	88	.2	23	10	383	3.16	41	5	ND	2	17	1	2	86	.29	.111	11	44	.37	94	.03	3	1.17	.03	.08	1	1	
44E 14+25N	1	27	8	84	.1	19	10	253	2.67	22	5	ND	2	14	1	2	67	.26	.089	11	42	.49	86	.04	5	1.29	.03	.07	1	13	
44E 14+00N	1	23	4	59	.1	19	7	169	2.15	22	5	ND	3	12	1	2	65	.22	.038	12	34	.42	69	.06	3	1.01	.03	.07	1	10	
44E 13+75N	1	30	9	70	.2	22	8	220	2.78	21	5	ND	3	15	1	2	81	.25	.082	11	41	.53	58	.06	3	1.21	.03	.06	1	46	
44E 13+50N	1	41	8	89	.1	30	11	266	3.24	27	5	ND	3	17	1	2	80	.31	.088	13	47	.67	71	.05	3	1.44	.03	.07	1	9	
44E 13+25N	1	13	2	60	.1	14	8	337	1.70	6	5	ND	2	13	1	3	51	.25	.028	10	30	.35	74	.05	2	.80	.02	.06	1	1	
44E 13+00N	1	28	6	71	.1	20	10	411	2.58	14	5	ND	3	12	1	2	68	.23	.062	11	35	.46	75	.05	4	1.03	.03	.09	1	1	
44E 12+75N	1	49	8	66	.1	30	11	228	3.12	19	5	ND	3	13	1	2	66	.25	.051	12	42	.62	78	.04	4	1.37	.03	.07	1	13	
44E 12+50N	1	42	10	60	.1	28	13	256	3.65	18	5	ND	3	12	1	3	88	.22	.081	13	47	.60	112	.03	4	1.54	.03	.08	1	14	
44E 12+25N	1	29	6	66	.1	25	10	319	2.66	12	5	ND	3	15	1	3	69	.29	.040	11	40	.57	101	.06	3	1.07	.03	.08	1	23	
44E 12+00N	1	37	8	79	.1	28	13	713	3.13	15	5	ND	2	17	1	2	81	.33	.044	12	45	.62	207	.05	3	1.45	.03	.10	1	11	
44E 11+75N	1	27	8	53	.1	15	8	212	2.65	12	5	ND	2	19	1	3	66	.38	.057	13	29	.35	115	.03	3	1.06	.03	.10	1	4	
44E 11+50N	1	51	9	59	.1	30	12	416	2.92	18	5	ND	4	19	1	2	67	.34	.038	14	46	.65	99	.06	2	1.39	.03	.08	1	9	
44E 11+00N	1	129	16	66	2.0	41	13	680	3.65	21	5	ND	2	93	2	2	81	2.38	.061	16	59	.59	242	.04	5	1.99	.06	.11	1	7	
44E 10+00N	1	37	7	62	.1	21	11	322	3.77	12	5	ND	3	19	1	2	84	.24	.065	14	37	.59	133	.03	2	1.41	.03	.09	1	2	
44E 9+75N	1	39	11	69	.1	33	12	342	3.80	9	5	ND	3	13	1	2	80	.20	.064	11	43	.57	103	.03	2	1.35	.02	.08	1	1	
44E 9+50N	1	25	7	50	.1	15	7	256	2.48	14	5	ND	3	14	1	2	54	.21	.077	13	29	.36	97	.03	3	.93	.02	.08	1	62	
44E 9+25N	1	64	11	68	.1	24	14	393	4.20	26	5	ND	3	14	1	3	89	.18	.058	12	46	.77	115	.02	3	1.61	.03	.07	1	7	
44E 9+00N	1	32	5	58	.1	16	9	245	3.03	11	5	ND	3	11	1	2	62	.16	.070	12	31	.44	92	.03	2	1.20	.02	.08	1	3	
44E 8+75N	1	8	5	26	.1	6	4	298	1.13	2	5	ND	2	13	1	2	34	.19	.031	11	16	.14	87	.04	2	.45	.02	.10	1	1	
44E 8+50N	1	34	5	53	.1	18	8	205	2.62	8	5	ND	3	13	1	2	54	.16	.058	13	33	.45	90	.03	4	1.03	.02	.10	1	4	
44E 8+25N	1	24	10	54	.1	20	9	193	3.11	10	5	ND	3	12	1	2	61	.17	.059	15	34	.45	83	.03	4	1.13	.02	.10	1	2	
44E 8+00N	1	39	9	46	.1	21	12	283	3.30	16	5	ND	4	12	1	4	67	.16	.027	15	39	.52	73	.03	3	1.29	.02	.11	2	1	
44E 6+75N	1	90	10	64	.3	31	15	525	3.28	11	5	ND	3	29	1	2	63	.50	.041	17	44	.93	221	.04	3	1.60	.04	.10	1	8	
44E 6+50N	1	90	13	68	.3	28	16	583	4.02	18	5	ND	4	26	1	3	77	.44	.031	16	48	.87	304	.03	2	1.62	.04	.09	1	6	
44E 6+00N	3	648	16	115	2.5	96	21	1375	7.95	37	5	ND	6	84	2	4	2	101	1.32	.146	58	79	.71	632	.06	2	3.21	.06	.21	1	20
44E 5+75N	1	313	14	108	.9	55	21	922	6.09	30	5	ND	3	77	1	2	95	1.37	.093	33	67	.88	478	.03	2	2.46	.06	.17	1	16	
44E 5+50N	1	156	7	82	.3	42	17	918	4.39	19	5	ND	3	41	1	6	2	76	.61	.074	25	55	.93	304	.03	4	2.16	.04	.13	1	10
44E 5+25N	1	37	10	69	.1	22	10	260	3.45	14	5	ND	2	18	1	2	78	.26	.081	14	36	.61	132	.03	3	1.25	.03	.09	1	8	
44E 5+00N	1	58	9	70	.1	26	10	248	3.61	20	5	ND	2	17	1	3	2	81	.27	.084	13	42	.64	88	.03	4	1.42	.03	.11	1	10
44E 4+75N	1	36	8	54	.1	16	9	263	2.66	11	5	ND	2	19	1	2	70	.29	.047	13	30	.40	164	.03	4	.88	.03	.12	1	1	
44E 4+50N	1	69	9	65	.1	29	11	295	3.56	20	5	ND	4	17	1	2	66	.24	.053	15	42	.68	118	.04	4	1.45	.03	.09	1	32	
STD C/AU-0.5	20	62	42	137	7.0	74	30	1175	3.97	38	15	8	38	51	19	17	20	72	.48	.110	40	60	.88	182	.09	36	1.73	.10	.14	12	510

E & B EXPLORATION PROJECT -- 5055 FILE # 86-2093

PAGE 2

SAMPLE#	Mc	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	E	Al	Na	K	W	Au
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
44E 4+25N	1	143	12	84	.4	44	18	579	4.85	11	5	ND	3	43	1	2	2	101	.56	.065	28	66	1.42	372	.03	7	2.57	.04	.12	1	15
44E 3+00N	1	83	20	78	.7	38	14	485	3.38	18	5	ND	2	60	1	5	2	64	1.27	.038	13	47	.46	145	.04	5	1.72	.04	.09	1	9
44E 2+75N	1	23	12	81	.1	31	13	619	3.02	8	5	ND	5	29	1	5	2	54	.41	.029	16	44	.63	107	.05	6	1.56	.03	.07	1	10
44E 2+50N	1	29	10	75	.1	31	12	287	2.96	13	5	ND	4	23	1	3	2	54	.34	.041	16	44	.57	112	.05	8	1.45	.03	.07	1	7
44E 2+25N	1	23	12	93	.2	15	12	1741	2.00	6	5	ND	3	17	1	3	2	41	.26	.080	12	31	.30	154	.06	7	.76	.02	.08	1	12
44E 2+00N	1	14	6	60	.3	17	6	369	1.92	7	5	ND	4	17	1	2	2	38	.26	.083	14	27	.41	69	.06	4	.85	.02	.07	1	6
44E 1+75N	1	49	11	92	.6	34	13	1215	2.86	9	5	ND	2	25	1	2	2	54	.39	.051	17	45	.53	131	.04	7	1.51	.03	.09	1	23
44E 1+50N	1	55	13	109	.6	33	13	1336	3.14	10	5	ND	3	31	1	2	2	58	.43	.108	19	47	.60	158	.04	7	1.72	.03	.12	1	4
44E 1+25N	1	15	6	82	.2	14	7	496	1.72	3	5	ND	2	19	1	3	2	36	.30	.078	13	25	.38	103	.04	4	.83	.02	.09	1	6
44E 1+00N	1	12	6	64	.1	15	5	197	1.80	6	5	ND	5	16	1	2	2	41	.28	.051	15	27	.37	84	.06	6	.79	.02	.07	1	2
44E 0+75N	1	3	6	32	.2	5	2	115	.80	2	5	ND	4	13	1	2	2	24	.21	.022	14	15	.16	48	.06	4	.46	.01	.06	1	1
44E 0+50N	1	26	8	66	.1	27	9	380	2.73	12	5	ND	5	25	1	2	2	52	.37	.074	17	40	.63	67	.06	5	1.22	.03	.07	1	4
44E 0+25N	1	26	13	96	.2	33	12	562	3.13	16	5	ND	4	27	1	9	2	57	.47	.039	15	44	.67	103	.06	6	1.58	.03	.11	1	1
45E 17+00N	4	40	12	83	.1	21	9	251	3.96	57	5	ND	2	21	1	8	2	135	.30	.028	9	54	.52	86	.04	5	1.53	.03	.07	1	1
45E 16+75N	2	48	11	133	.5	25	14	1639	3.40	46	5	ND	2	25	1	2	2	100	.37	.070	7	50	.60	170	.05	6	1.16	.03	.09	1	15
45E 16+50N	2	105	18	110	.3	46	25	1157	4.45	94	5	ND	4	30	1	7	2	93	.51	.086	13	68	1.12	102	.07	7	1.65	.04	.13	1	9
45E 15+75N	2	26	8	54	.3	15	7	308	1.99	25	5	ND	2	18	1	8	2	64	.34	.036	9	33	.38	60	.06	6	.79	.02	.10	1	1
45E 15+50N	1	28	9	56	.1	24	7	231	2.32	15	5	ND	3	16	1	2	2	50	.30	.064	11	40	.54	41	.06	4	1.07	.02	.07	1	4
45E 15+25N	1	41	7	103	.1	28	10	241	3.15	38	5	ND	2	15	1	3	2	84	.29	.062	10	55	.66	59	.05	5	1.61	.03	.07	1	13
45E 15+00N	1	43	10	86	.2	25	12	311	2.91	32	5	ND	2	13	1	3	3	89	.25	.059	8	75	.53	62	.05	6	1.30	.03	.06	1	3
45E 14+75N	1	27	7	93	.1	18	9	431	2.30	20	5	ND	1	23	1	5	2	71	.40	.070	9	39	.48	83	.05	5	1.12	.03	.11	1	4
45E 14+50N	1	30	8	84	.1	18	9	409	2.42	45	5	ND	2	22	1	3	2	74	.37	.072	10	38	.48	99	.05	6	1.13	.03	.10	1	3
45E 14+25N	1	41	5	97	.2	26	13	448	3.40	45	5	ND	2	17	1	5	2	98	.26	.116	9	52	.57	79	.04	5	1.48	.03	.07	1	2
45E 13+75N	1	64	7	138	.3	28	21	1440	4.89	6	5	ND	2	21	1	2	2	112	.42	.113	7	70	2.06	114	.06	7	2.62	.04	.19	1	6
45E 13+25N	1	75	11	150	.3	20	19	2193	5.43	10	5	ND	1	32	1	3	2	132	.50	.175	8	53	.93	288	.03	5	1.82	.04	.13	1	2
45E 13+00N	2	47	11	64	.1	29	11	293	2.87	27	5	ND	3	20	1	4	2	74	.31	.029	10	45	.72	71	.09	5	1.33	.03	.08	1	1
45E 12+75N	1	49	7	71	.1	30	11	253	3.52	30	5	ND	3	17	1	6	2	84	.25	.099	10	50	.63	95	.04	8	1.48	.03	.08	1	2
45E 12+50N	1	50	9	60	.1	29	11	285	2.99	21	5	ND	4	18	1	4	2	70	.28	.041	11	45	.63	66	.06	6	1.29	.03	.09	1	1
45E 12+25N	1	60	11	113	.1	22	12	332	3.97	20	5	ND	2	19	1	7	3	106	.27	.091	9	44	.61	118	.01	7	1.69	.03	.11	1	1
45E 12+00N	1	29	7	43	.1	17	8	287	2.66	20	5	ND	2	20	1	3	2	92	.36	.058	7	32	.38	79	.03	6	1.00	.03	.12	1	7
45E 11+75N	2	56	8	75	.1	31	13	294	3.86	28	5	ND	4	16	1	5	2	95	.28	.064	11	52	.73	75	.05	5	1.67	.03	.08	1	5
45E 11+00N	1	58	15	117	.2	40	30	1932	5.69	15	5	ND	2	23	1	2	2	149	.32	.092	9	119	1.18	187	.02	5	1.84	.04	.11	1	1
45E 10+75N	2	219	13	102	.9	51	21	746	6.00	52	5	ND	4	38	1	4	2	126	.59	.047	11	84	1.08	234	.01	6	2.70	.04	.13	1	4
45E 10+00N	1	64	13	222	.3	45	20	560	3.81	33	5	ND	2	50	2	2	2	99	.94	.118	8	59	.97	156	.09	6	2.00	.06	.12	1	1
45E 9+75N	2	50	8	120	.2	33	15	670	3.66	28	5	ND	2	22	1	5	2	109	.43	.052	9	55	.77	117	.09	5	1.54	.03	.10	1	5
45E 9+50N	4	100	13	125	.2	37	28	383	6.41	19	5	ND	3	31	1	4	2	107	.35	.093	7	47	.69	100	.06	4	2.13	.03	.08	1	6
STD C/AU 0.5	20	63	41	144	7.1	74	30	1175	3.99	42	18	8	37	51	19	16	22	72	.48	.111	41	63	.89	192	.09	39	1.73	.10	.14	12	500



## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-2093

PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Tl PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	F PPM	Al %	Na %	K %	W PPM	Aut PPB
45E 9+25N	2	128	21	198	1.0	52	21	3058	4.46	31	5	ND	2	40	1	2	2	85	.78	.077	16	70	.60	297	.06	3	2.52	.05	.16	1	1
45E 9+00N	2	54	11	92	.1	31	14	457	3.70	23	5	ND	2	26	1	6	2	93	.46	.065	9	47	.75	105	.06	3	1.54	.04	.10	1	10
45E 8+75N	1	16	10	74	.1	14	9	667	2.07	10	5	ND	2	17	1	2	2	66	.28	.042	9	30	.34	107	.09	2	.91	.02	.11	1	1
45E 8+50N	1	19	10	83	.1	22	8	358	2.65	18	5	ND	2	16	1	2	2	62	.25	.091	9	33	.46	81	.06	2	1.20	.02	.07	1	2
45E 8+25N	1	23	10	149	.1	23	11	288	2.86	14	5	ND	2	20	1	3	2	90	.35	.075	6	41	.57	82	.08	3	1.62	.03	.09	1	1
45E 8+00N	1	13	9	32	.1	8	5	130	1.51	6	5	ND	1	15	1	2	2	64	.28	.029	8	26	.20	72	.09	3	.72	.03	.11	1	1
45E 7+75N	1	14	8	36	.2	9	4	202	1.40	5	5	ND	2	21	1	2	2	51	.42	.019	8	22	.27	110	.03	2	.82	.03	.09	3	1
45E 7+50N	2	222	15	73	.7	37	16	2251	3.56	32	5	ND	1	65	1	2	2	69	1.12	.056	9	52	.65	349	.03	3	2.00	.05	.09	1	2
45E 6+50N	1	87	15	80	.1	28	16	708	4.01	20	5	ND	3	19	1	2	2	70	.32	.096	14	43	.77	205	.04	2	1.39	.03	.11	1	14
45E 6+25N	1	35	13	70	.1	14	9	185	3.44	9	5	ND	2	11	1	2	2	88	.16	.064	9	30	.34	96	.04	2	1.03	.02	.09	1	1
45E 6+00N	1	33	9	93	.2	18	11	385	3.33	12	5	ND	2	14	1	2	2	68	.25	.087	9	33	.47	127	.03	4	1.20	.03	.11	1	3
45E 5+75N	2	60	11	92	.2	26	12	321	4.17	13	5	ND	4	16	1	2	2	75	.22	.081	12	45	.64	218	.03	2	1.59	.03	.08	1	2
45E 5+50N	1	55	10	84	.2	24	11	675	2.71	12	5	ND	3	21	1	2	2	35	.37	.044	14	35	.47	175	.05	2	1.13	.03	.12	1	4
45E 5+25N	2	143	17	94	.4	44	17	1147	4.74	21	5	ND	3	24	1	3	2	92	.39	.066	19	68	1.14	313	.05	2	2.37	.04	.15	1	125
45E 5+00N	1	27	10	98	.1	24	9	272	3.38	15	5	ND	3	16	1	2	2	68	.22	.084	14	38	.56	157	.05	2	1.35	.03	.08	1	225
45E 4+75N	1	16	10	68	.1	18	7	304	2.38	8	5	ND	4	16	1	2	2	46	.21	.071	16	29	.46	148	.06	3	.95	.02	.10	1	41
45E 4+50N	1	99	12	68	.3	35	13	601	3.89	21	5	ND	4	35	1	2	2	64	.46	.041	13	46	.84	193	.05	2	1.67	.04	.12	1	9
45E 4+25N	1	57	10	87	.1	25	14	638	3.35	13	5	ND	3	26	1	2	2	69	.30	.021	11	39	.53	183	.04	2	1.62	.03	.06	1	2
45E 4+00N	2	51	11	97	.1	29	10	489	3.56	23	5	ND	3	15	1	2	2	78	.25	.091	10	45	.69	176	.05	3	1.40	.03	.09	1	10
45E 3+75N	1	18	8	68	.2	11	8	928	2.00	6	5	ND	1	21	1	2	2	47	.30	.045	11	19	.22	416	.03	2	.63	.02	.09	1	1
45E 3+50N	1	16	7	45	.1	11	8	196	2.39	11	5	ND	2	16	1	2	2	57	.20	.057	11	24	.27	112	.03	2	.77	.02	.09	2	1
45E 3+25N	1	32	8	61	.1	20	12	264	3.55	15	5	ND	4	19	1	2	2	72	.29	.050	12	38	.51	142	.04	3	1.27	.03	.13	1	39
45E 3+00N	1	15	8	49	.1	13	6	324	2.19	10	5	ND	3	22	1	2	3	61	.30	.024	12	27	.28	148	.06	2	.89	.02	.08	1	10
45E 1+25N	1	66	16	82	.4	43	15	581	4.14	35	5	ND	4	47	1	2	2	83	.98	.051	17	52	.93	144	.08	3	1.88	.05	.12	1	3
45E 1+00N	1	23	11	63	.2	19	7	194	2.55	10	5	ND	3	23	1	2	2	60	.38	.022	12	34	.40	94	.05	2	1.20	.03	.07	1	5
45E 0+75N	1	31	9	72	.5	22	7	259	2.04	7	5	ND	2	40	1	2	2	41	.83	.047	12	33	.41	97	.04	2	1.20	.03	.06	1	11
45E 0+50N	1	23	13	69	.2	24	11	850	2.57	11	5	ND	3	35	1	2	2	55	.62	.032	11	39	.50	119	.05	2	1.41	.03	.07	1	1
45E 0+25N	1	18	9	90	.3	20	10	854	2.12	6	5	ND	2	21	1	2	2	42	.32	.044	13	32	.46	94	.05	2	1.23	.02	.09	1	4
46E 17+00N	5	439	24	166	2.0	91	23	1273	5.89	113	7	ND	3	90	2	2	2	110	1.77	.105	17	100	1.06	219	.05	2	2.83	.06	.18	1	23
46E 16+50N	3	79	15	80	.1	36	15	620	4.01	80	5	ND	2	25	1	2	2	100	.45	.063	9	58	.84	81	.06	4	1.48	.04	.13	1	6
46E 16+25N	3	83	12	92	.3	39	17	713	3.87	61	5	ND	3	24	1	3	2	88	.40	.051	13	63	.85	94	.06	2	1.59	.04	.09	1	4
46E 16+00N	2	31	11	106	.1	23	10	373	2.97	35	5	ND	2	20	1	2	2	93	.38	.036	9	48	.64	79	.06	3	1.22	.04	.08	1	1
46E 15+75N	2	28	8	73	.2	19	11	442	2.65	37	5	ND	2	18	1	2	2	91	.31	.027	9	39	.42	65	.05	4	1.02	.03	.10	1	4
46E 15+50N	3	46	13	103	.3	29	11	852	3.40	49	5	ND	2	22	1	4	2	88	.39	.052	11	51	.67	149	.05	3	1.37	.03	.09	1	2
46E 15+25N	2	54	9	105	.1	27	12	630	3.32	54	5	ND	3	16	1	4	2	95	.26	.075	10	47	.68	68	.06	6	1.33	.03	.09	1	30
46E 15+00N	1	45	5	111	.1	20	13	1429	2.78	50	5	ND	1	18	1	3	2	82	.35	.058	8	44	.56	129	.05	4	1.09	.03	.11	1	75
STD C/AU 0.5	20	62	42	142	6.7	73	30	1154	3.96	39	15	8	37	50	19	16	19	71	.48	.108	38	62	.88	188	.09	36	1.73	.10	.15	12	500

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-2093

PAGE 4

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Tl	F	Al	Na	K	W	Ag#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
46E 14+75N	2	28	7	108	.1	21	11	268	2.67	25	5	ND	1	19	1	3	2	78	.34	.072	9	40	.58	72	.05	8	1.20	.03	.09	1	5
46E 14+50N	2	30	7	109	.1	22	10	506	2.82	33	5	ND	2	17	1	2	2	77	.31	.087	9	43	.49	73	.06	9	1.24	.03	.09	2	6
46E 14+25N	2	32	7	121	.1	25	11	293	2.93	25	5	ND	1	17	1	2	2	84	.33	.066	8	49	.70	90	.05	11	1.58	.03	.08	1	25
46E 14+00N	1	33	3	80	.1	17	10	554	2.45	18	5	ND	2	20	1	2	2	79	.31	.062	6	38	.46	87	.05	8	1.31	.03	.10	1	3
46E 13+75N	1	43	13	85	.1	19	9	208	2.88	26	5	ND	2	18	1	2	2	88	.31	.055	7	44	.49	74	.06	9	1.36	.03	.07	1	2
46E 13+50N	2	74	10	117	.3	36	16	1275	3.66	47	5	ND	1	26	1	3	2	97	.54	.051	11	65	.66	131	.04	11	1.93	.04	.08	2	12
46E 13+25N	3	85	6	86	.1	40	17	300	4.62	71	5	ND	1	20	1	3	2	119	.34	.062	8	66	.88	69	.03	12	1.89	.04	.07	2	16
46E 13+00N	2	52	9	70	.4	25	11	337	3.65	32	5	ND	1	17	1	2	2	97	.28	.091	7	43	.55	99	.03	11	1.38	.03	.07	1	13
46E 12+75N	3	36	12	79	.1	25	13	369	3.39	38	5	ND	2	22	1	4	2	101	.44	.033	7	42	.33	110	.04	10	1.52	.03	.05	1	3
46E 12+50N	1	28	6	86	.1	15	10	539	2.60	12	5	ND	1	19	1	3	2	70	.34	.091	8	39	.38	119	.05	9	1.09	.02	.06	1	25
46E 12+25N	2	28	6	83	.1	24	11	371	2.72	20	5	ND	2	16	1	3	2	79	.31	.053	9	42	.55	83	.06	10	1.40	.03	.06	1	3
46E 12+00N	2	26	5	61	.1	20	7	189	2.60	19	5	ND	2	16	1	6	2	84	.28	.045	10	38	.48	82	.06	9	1.28	.03	.07	1	15
46E 11+75N	3	42	8	79	.1	26	9	240	3.75	29	5	ND	2	17	1	2	2	102	.30	.103	8	49	.59	65	.04	12	1.50	.03	.09	1	13
46E 11+50N	2	41	5	92	.1	19	12	641	3.42	22	5	ND	2	21	1	2	2	95	.31	.053	6	41	.54	137	.02	10	1.40	.03	.10	1	4
46E 11+25N	3	52	11	134	.1	25	17	414	5.21	29	5	ND	2	19	1	5	2	130	.27	.110	6	55	.71	86	.02	14	1.92	.03	.12	1	1
46E 11+00N	3	43	10	67	.1	19	10	269	4.12	26	5	ND	1	24	1	2	2	142	.46	.051	6	39	.49	88	.03	10	1.34	.03	.10	1	1
46E 10+75N	3	53	10	72	.2	25	12	217	4.12	29	5	ND	1	25	1	5	2	121	.50	.046	8	44	.47	105	.02	12	1.86	.03	.04	2	8
46E 10+50N	2	81	9	74	.1	42	16	366	3.97	30	5	ND	2	15	1	2	2	88	.30	.047	10	62	.80	77	.06	11	1.98	.03	.08	1	16
46E 10+00N	3	23	8	60	.1	16	6	183	2.67	28	5	ND	2	15	1	2	2	111	.27	.048	8	32	.32	72	.09	9	1.03	.02	.04	1	9
46E 9+75N	2	22	10	98	.1	23	9	275	3.54	16	5	ND	2	17	1	2	2	104	.37	.080	6	42	.51	73	.07	10	1.49	.03	.07	4	13
46E 9+50N	2	18	9	111	.1	18	8	307	3.27	13	5	ND	2	19	1	2	2	101	.38	.151	8	42	.51	71	.09	11	1.57	.03	.07	1	2
46E 9+25N	2	17	9	80	.1	16	7	192	2.49	15	5	ND	1	16	1	2	2	96	.33	.052	7	34	.42	63	.08	7	1.31	.03	.07	1	1
46E 9+00N	4	60	11	88	.1	34	15	522	3.93	28	5	ND	1	22	1	5	2	137	.48	.057	6	58	.75	87	.10	10	1.61	.04	.08	1	42
46E 8+50N	2	56	7	87	.1	37	12	430	2.78	36	5	ND	2	18	1	2	2	75	.41	.073	5	40	.59	77	.09	9	1.30	.03	.08	1	7
46E 8+25N	3	65	12	110	.1	31	14	687	3.62	28	5	ND	1	21	1	2	2	96	.42	.101	7	51	.67	108	.06	12	1.47	.03	.11	1	11
46E 8+00N	2	39	12	203	.3	38	17	602	4.57	27	5	ND	2	18	1	2	2	118	.32	.136	6	59	.81	143	.09	12	2.06	.03	.11	1	1
46E 7+00N	4	144	13	129	1.0	57	19	1893	5.72	57	5	ND	2	79	1	2	2	89	1.43	.081	11	70	.91	323	.04	14	2.45	.05	.15	1	10
46E 6+75N	1	43	9	55	.3	15	6	158	2.01	8	5	ND	1	21	1	2	2	57	.34	.026	9	38	.23	181	.03	7	.81	.02	.06	1	2
46E 6+50N	1	43	9	97	.2	18	12	543	2.78	3	5	ND	1	19	1	2	2	65	.31	.043	10	34	.28	174	.03	11	1.09	.02	.08	1	1
46E 6+25N	1	72	11	101	.3	28	14	622	3.27	12	5	ND	3	20	1	2	2	59	.34	.037	16	41	.63	208	.04	12	1.46	.03	.09	1	3
46E 6+00N	1	47	11	71	.1	20	11	244	3.11	7	5	ND	4	16	1	2	2	61	.24	.053	15	33	.51	149	.04	9	1.00	.02	.08	1	48
46E 5+75N	1	19	8	61	.3	11	8	214	2.25	4	5	ND	2	13	1	2	2	55	.19	.041	13	20	.26	164	.03	9	.78	.02	.08	1	11
46E 5+50N	1	25	6	62	.1	13	7	259	1.96	4	5	ND	3	12	1	2	2	45	.23	.040	13	25	.33	115	.05	7	.74	.02	.09	1	2
46E 5+25N	2	53	12	94	.1	23	11	197	4.14	20	5	ND	3	13	1	2	2	81	.23	.149	11	41	.60	94	.03	13	1.41	.03	.06	1	17
46E 5+00N	1	45	11	81	.1	19	9	216	3.01	11	5	ND	2	12	1	2	2	61	.20	.060	10	36	.52	84	.03	10	1.25	.02	.06	1	3
46E 4+75N	1	18	8	54	.1	13	7	262	2.19	5	5	ND	3	13	1	5	2	45	.24	.059	14	24	.35	95	.04	7	.83	.02	.07	1	27
STD C/AU 0.5	22	61	41	140	7.1	73	30	1143	3.96	40	18	8	36	50	18	15	20	70	.48	.109	39	59	.88	186	.09	43	1.73	.09	.14	14	505

E & B EXPLORATION PROJECT - 5055 FILE # 86-2093

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au1 PPM
47E 11+25N	1	29	8	82	.2	19	10	378	3.56	28	5	ND	2	18	1	2	2	107	.33	.076	8	39	.44	75	.04	4	1.29	.03	.10	1	5
47E 11+00N	1	16	5	44	.1	9	6	191	1.94	11	5	ND	1	15	1	2	2	77	.22	.036	7	26	.20	56	.04	2	.74	.02	.07	2	3
47E 10+75N	1	63	13	85	.1	33	15	456	3.47	44	5	ND	2	22	1	2	2	101	.39	.051	11	51	.71	119	.04	4	1.72	.03	.09	1	15
47E 10+50N	1	89	13	97	.6	55	15	514	3.82	48	5	ND	3	35	1	2	2	94	.54	.041	18	70	.92	138	.05	4	2.18	.04	.11	1	13
47E 10+00N	6	341	16	162	1.4	125	22	956	8.20	63	5	ND	7	68	1	2	2	158	.93	.102	34	145	1.53	388	.05	7	5.43	.06	.27	1	11
47E 9+75N	1	50	9	79	.1	33	11	321	3.62	25	5	ND	3	19	1	2	3	89	.33	.093	11	58	.79	100	.06	5	1.74	.03	.07	1	31
47E 9+50N	2	33	10	67	.1	26	8	215	3.81	18	5	ND	3	16	1	2	2	98	.27	.135	13	49	.57	78	.06	3	1.46	.03	.07	1	11
47E 9+25N	1	44	9	67	.1	27	9	245	3.44	20	5	ND	3	18	1	2	2	88	.33	.107	12	49	.71	65	.05	6	1.51	.03	.07	1	8
47E 9+00N	2	41	9	85	.1	33	10	224	3.56	20	5	ND	4	16	1	2	2	90	.28	.127	11	55	.66	69	.07	4	1.66	.03	.06	1	19
47E 8+75N	1	26	7	58	.1	28	8	214	2.57	15	5	ND	4	17	1	2	2	56	.29	.064	10	40	.50	60	.06	4	1.21	.02	.07	1	39
47E 8+50N	2	210	14	110	1.0	78	25	2122	4.85	34	5	ND	3	63	2	2	2	105	.93	.071	55	90	1.16	272	.05	5	3.12	.05	.17	1	5
47E 8+25N	3	240	15	103	1.5	81	22	1233	5.21	40	5	ND	5	73	1	5	2	110	.83	.061	49	98	1.12	257	.07	5	3.19	.05	.17	1	6
47E 8+00N	1	28	6	51	.1	16	9	271	2.34	10	5	ND	1	14	1	2	2	81	.25	.035	8	31	.36	60	.05	3	1.07	.02	.06	1	4
47E 7+75N	1	36	8	80	.1	28	10	280	2.94	13	5	ND	3	18	1	3	2	66	.29	.073	14	48	.67	88	.05	6	1.45	.03	.08	1	15
47E 7+50N	1	29	5	102	.1	21	10	586	2.32	11	5	ND	3	17	1	2	2	64	.29	.064	13	38	.43	90	.05	5	1.12	.03	.08	1	2
47E 7+25N	1	22	10	127	.1	18	13	530	3.65	17	5	ND	2	20	1	2	3	110	.33	.165	7	48	.38	117	.06	8	1.69	.03	.08	1	2
47E 7+00N	1	20	9	100	.1	17	10	334	3.10	17	5	ND	2	19	1	2	2	112	.36	.088	7	39	.44	68	.07	4	1.36	.03	.08	1	11
47E 6+75N	1	38	9	94	.3	23	13	846	2.58	13	5	ND	2	24	1	2	2	78	.42	.049	10	39	.51	143	.05	5	1.41	.03	.09	1	5
47E 6+50N	2	39	9	146	.2	30	15	445	4.39	31	5	ND	2	22	1	2	2	127	.41	.165	6	53	.67	132	.07	6	1.76	.03	.10	1	2
47E 6+00N	2	386	19	133	2.1	93	24	1513	6.20	29	5	ND	4	46	2	2	2	92	.91	.080	33	85	.97	500	.04	8	3.04	.05	.21	1	12
47E 5+75N	1	38	7	82	.1	29	11	384	2.93	16	5	ND	5	16	1	3	2	53	.30	.050	16	43	.67	98	.06	4	1.24	.03	.08	1	7
47E 5+50N	1	56	11	80	.2	27	14	990	2.97	13	5	ND	2	23	1	2	2	57	.48	.053	9	37	.56	169	.02	5	1.37	.03	.08	1	9
47E 5+25N	1	51	8	91	.4	19	13	274	4.30	10	5	ND	3	13	1	3	2	74	.17	.112	13	37	.44	124	.02	9	1.22	.02	.08	1	5
47E 5+00N	2	154	10	96	.1	16	17	1184	6.00	7	5	ND	1	27	1	6	2	57	.73	.136	11	21	.19	443	.01	6	.69	.03	.20	1	2
47E 4+75N	1	27	9	78	.1	15	10	433	2.87	10	5	ND	3	14	1	2	3	68	.26	.090	12	30	.35	127	.02	6	1.05	.02	.09	1	3
47E 4+50N	1	117	7	117	.2	19	23	1084	6.23	7	5	ND	2	16	1	2	2	88	.36	.129	7	20	.61	268	.01	5	1.30	.03	.17	1	2
47E 4+25N	1	13	3	38	.1	8	5	125	1.69	2	5	ND	3	11	1	2	2	41	.15	.034	16	15	.16	123	.03	4	.64	.01	.12	1	7
47E 4+00N	1	24	9	86	.1	12	12	2237	1.98	5	5	ND	2	23	1	2	2	53	.44	.075	11	24	.36	507	.03	3	.86	.02	.10	1	2
47E 3+75N	1	31	8	81	.1	20	10	213	3.08	12	5	ND	3	16	1	2	2	65	.20	.109	13	34	.52	138	.03	5	1.21	.02	.06	1	3
47E 3+50N	1	17	8	49	.1	13	5	133	2.03	13	5	ND	3	11	1	2	2	47	.13	.062	16	26	.31	92	.03	6	.83	.02	.08	1	6
47E 3+25N	1	45	11	72	.1	27	11	1019	3.36	16	5	ND	4	19	1	6	2	59	.26	.046	16	37	.68	194	.04	4	1.37	.03	.10	1	11
47E 3+00N	1	12	6	44	.1	9	4	135	1.65	3	5	ND	3	11	1	2	2	42	.14	.029	16	21	.24	94	.04	3	.81	.02	.07	1	3
47E 2+75N	1	70	6	122	.1	26	13	355	4.05	6	5	ND	4	18	1	4	2	79	.32	.086	13	37	.81	310	.02	5	1.77	.03	.11	1	2
47E 2+50N	1	21	6	41	.1	13	7	367	2.27	3	5	ND	3	13	1	2	2	62	.15	.024	12	26	.24	111	.03	4	.93	.02	.08	1	2
47E 2+25N	1	12	6	91	.1	17	7	345	1.86	4	5	ND	4	18	1	2	2	38	.25	.059	14	27	.42	78	.05	4	.96	.02	.06	1	1
47E 0+50N	1	21	8	85	.2	16	6	162	3.10	9	5	ND	4	15	1	2	2	62	.24	.140	11	32	.37	106	.05	6	1.15	.02	.07	1	1
47E 0+25N	1	41	4	67	.1	16	6	192	2.32	11	5	ND	4	18	1	2	2	48	.24	.077	14	27	.37	64	.04	5	.80	.02	.07	1	6
STD C/AU-0.5	21	62	41	138	7.1	74	31	1192	3.99	40	17	8	39	52	19	17	20	74	.48	.111	38	63	.89	186	.09	38	1.72	.10	.14	14	495



## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Ti %	K PPM	Al %	Na %	K %	W PPM	Au1 PPB
L11+85E 9+00N	1	15	2	41	.2	12	6	175	1.68	9	5	ND	1	21	1	2	2	50	.32	.029	10	30	.34	54	.07	4	1.01	.01	.04	2	4
L11+85E 8+75N	2	195	9	106	.2	53	25	306	4.97	42	5	ND	2	20	1	3	2	87	.32	.115	6	70	.92	87	.06	6	2.29	.01	.05	1	25
L11+85E 8+50N	1	31	3	81	.1	17	11	720	2.53	13	5	ND	1	26	1	2	4	67	.39	.095	7	39	.48	111	.07	6	1.21	.01	.06	1	1
L11+85E 8+25N	1	105	3	96	.3	36	20	1110	4.15	16	5	ND	2	35	1	2	2	86	.49	.105	11	68	1.12	220	.08	3	1.72	.01	.10	1	5
L11+85E 8+00N	2	106	3	115	.8	29	17	2485	3.24	15	5	ND	1	37	1	2	2	69	.72	.051	10	53	.68	270	.05	6	1.70	.01	.07	1	3
L11+85E 7+75N	1	55	4	123	.3	30	15	338	3.86	16	5	ND	2	26	1	2	4	71	.44	.112	10	56	.79	149	.06	2	1.69	.01	.07	1	50
L11+85E 7+50N	1	77	7	115	.4	33	15	565	3.34	14	5	ND	1	32	1	2	3	69	.63	.070	10	53	.86	147	.05	6	1.71	.01	.07	1	10
L11+85E 7+25N	1	28	2	91	.5	25	9	268	2.48	13	5	ND	1	25	1	2	2	47	.41	.055	13	41	.67	92	.06	6	1.30	.01	.07	1	6
L11+85E 7+00N	2	145	19	172	1.7	69	21	1253	5.05	28	5	ND	1	49	2	2	2	80	1.11	.125	19	86	1.05	281	.05	8	2.85	.01	.16	1	9
L11+85E 6+75N	1	13	6	119	.2	18	6	239	2.29	5	5	ND	2	18	1	2	2	44	.23	.099	15	32	.43	150	.06	4	1.08	.01	.06	1	4
L11+85E 6+50N	1	21	6	102	.4	26	8	233	2.84	11	5	ND	2	21	1	2	2	50	.29	.104	14	37	.53	94	.06	6	1.29	.01	.06	1	1
L12+50E 20+00N	4	308	17	239	2.3	138	41	989	7.86	44	10	ND	4	65	1	2	3	131	.82	.114	36	140	1.71	275	.06	4	5.57	.02	.32	1	7
L12+50E 19+75N	3	344	21	253	2.9	140	36	875	7.39	38	12	ND	3	77	3	2	2	114	1.11	.111	48	134	1.54	299	.07	3	4.92	.02	.32	1	6
L12+50E 19+50N	3	298	22	309	2.0	130	44	1068	8.30	50	5	ND	4	58	2	2	2	143	.84	.081	25	167	1.81	252	.08	5	4.84	.02	.30	2	5
L12+50E 19+25N	2	350	22	324	3.2	157	37	406	8.08	43	8	ND	6	60	2	2	3	127	.81	.172	20	192	1.58	330	.07	9	6.57	.03	.34	1	11
L12+50E 19+00N	3	204	25	248	1.5	104	38	1662	7.42	43	5	ND	3	56	3	2	2	134	.79	.090	22	140	1.56	267	.07	5	4.27	.02	.29	1	4
L12+50E 18+75N	3	248	24	218	1.8	99	34	1273	6.31	33	5	ND	2	65	2	2	2	104	1.18	.080	30	133	1.45	259	.06	6	3.82	.02	.25	1	6
L12+50E 18+50N	2	86	15	238	.6	73	28	1288	4.96	19	5	ND	1	34	1	2	2	97	.58	.076	12	141	1.49	144	.07	5	3.11	.02	.14	1	2
L12+50E 18+25N	1	25	3	89	.2	23	9	231	2.27	7	5	ND	2	21	1	2	2	55	.35	.027	12	43	.73	53	.09	2	1.48	.01	.05	1	2
L12+50E 18+00N	1	24	6	82	.1	21	8	262	2.52	11	5	ND	2	19	1	3	2	66	.33	.064	12	41	.56	65	.08	3	1.28	.01	.06	1	1
L12+50E 17+75N	1	31	13	116	.2	28	11	430	2.38	6	5	ND	1	20	1	2	4	55	.36	.030	13	48	.70	77	.07	3	1.52	.01	.08	1	4
L12+50E 17+50N	1	19	7	76	.4	17	7	353	2.13	7	5	ND	1	22	1	2	3	65	.45	.045	9	37	.40	76	.09	2	1.05	.01	.06	1	2
L12+50E 17+25N	1	23	7	108	.2	21	8	199	2.09	9	5	ND	2	19	1	2	2	52	.36	.027	13	37	.58	60	.08	2	1.36	.01	.06	1	3
L12+50E 17+00N	2	118	12	172	.7	87	25	1009	4.71	27	6	ND	2	35	1	2	2	88	.53	.063	22	99	1.35	192	.06	2	3.23	.01	.17	1	4
L12+50E 16+75N	1	48	5	121	.3	38	12	405	2.65	10	5	ND	1	28	1	2	2	57	.51	.038	14	51	.66	97	.06	5	1.66	.01	.09	1	1
L12+50E 16+50N	1	14	4	41	.1	13	5	124	.89	7	5	ND	1	8	1	2	4	19	.15	.009	6	18	.26	24	.03	2	.51	.01	.02	3	4
L12+50E 16+25N	2	65	12	116	.4	48	17	654	3.17	15	5	ND	2	28	1	2	2	62	.48	.037	20	59	.90	100	.08	2	1.71	.01	.09	1	5
L12+50E 16+00N	1	93	10	135	.6	51	18	461	3.24	15	5	ND	2	31	1	2	2	63	.52	.038	16	63	.79	110	.06	2	1.93	.01	.10	1	2
L12+50E 15+75N	2	27	6	23	.1	13	7	190	1.05	14	5	ND	1	5	1	4	4	24	.12	.014	9	20	.20	19	.01	3	.38	.01	.02	4	6
L12+50E 15+50N	2	108	11	111	.6	53	17	564	3.10	14	7	ND	2	27	1	2	5	53	.47	.042	12	62	.75	97	.03	2	1.71	.01	.09	1	8
L12+50E 15+25N	2	101	12	110	.6	51	15	593	2.94	19	5	ND	1	21	1	2	2	51	.39	.035	11	60	.69	95	.03	2	1.69	.01	.10	1	8
L13+10E 12+50N	4	184	16	205	1.5	87	25	894	5.56	48	7	ND	2	37	1	2	2	84	.61	.067	10	94	.96	184	.04	2	2.72	.01	.17	1	6
L13+10E 12+25N	4	468	29	337	4.3	156	44	1190	9.23	90	8	ND	4	81	5	3	2	124	1.29	.153	21	149	1.32	367	.06	4	4.77	.02	.28	1	9
L13+10E 12+00N	4	344	26	346	3.6	149	40	1188	9.12	76	5	ND	5	65	3	3	2	127	.95	.133	14	153	1.32	336	.07	3	4.78	.02	.28	1	20
L13+10E 11+75N	3	138	20	220	.8	78	31	1376	5.52	59	5	ND	2	45	1	2	2	98	.79	.074	9	97	1.48	181	.07	2	2.81	.02	.14	1	6
L13+10E 11+50N	2	84	12	187	.6	68	26	919	4.55	41	5	ND	2	45	1	2	2	86	.65	.048	9	93	1.36	139	.07	5	2.30	.02	.11	1	11
STD C/AU-0.5	20	59	38	130	6.9	69	30	1096	3.93	40	20	8	34	48	16	16	19	62	.48	.106	36	59	.88	180	.08	40	1.73	.07	.13	13	500

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

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SAMPLE#	Hc PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	E PPM	Al %	Na %	K %	W PPM	Au# PPB
L13+10E 11+25N	1	41	8	223	.4	28	22	478	3.82	13	5	ND	1	30	2	2	2	75	.48	.081	9	49	.76	137	.08	2	1.47	.01	.09	1	4
L13+10E 11+00N	1	73	7	127	.2	27	17	307	3.72	28	5	ND	1	20	1	2	2	69	.29	.053	13	50	.80	90	.07	2	1.50	.01	.08	1	7
L13+10E 10+75N	1	62	7	137	.4	30	20	510	3.89	19	5	ND	1	21	1	2	2	79	.36	.054	12	56	.74	127	.05	2	1.71	.01	.08	1	16
L13+10E 10+25N	1	19	7	71	.3	13	8	282	1.90	9	5	ND	1	21	1	2	2	54	.34	.055	9	39	.28	143	.06	3	.85	.01	.06	1	3
L13+10E 10+00N	1	46	12	120	.3	28	16	683	4.00	23	5	ND	1	26	1	3	2	99	.45	.109	13	71	1.19	190	.10	3	1.82	.02	.12	1	10
L13+10E 9+50N	1	57	29	116	.2	40	25	2143	4.20	13	5	ND	1	35	1	2	2	90	.77	.131	9	81	1.28	227	.11	6	2.05	.02	.11	1	2
L13+10E 9+25N	1	42	4	147	.3	25	16	680	3.84	16	5	ND	2	31	1	2	2	75	.43	.133	15	58	.83	191	.06	2	2.10	.01	.10	1	3
L13+10E 9+00N	1	32	7	76	.1	24	13	241	3.58	20	5	ND	1	17	1	2	2	81	.31	.135	11	60	.77	98	.06	6	1.67	.01	.08	1	8
L13+10E 8+75N	1	39	6	96	.1	21	15	460	3.28	10	5	ND	1	29	1	2	2	77	.50	.103	10	46	.58	90	.09	2	1.75	.01	.07	1	2
L13+10E 8+50N	1	60	8	64	.1	27	15	393	3.59	11	5	ND	2	44	1	2	2	84	.53	.075	13	50	.81	133	.08	4	2.16	.01	.08	1	4
L13+10E 8+25N	1	44	7	43	.1	13	10	187	2.34	7	5	ND	1	32	1	2	2	66	.39	.043	11	30	.49	71	.09	3	1.04	.01	.07	1	3
L13+10E 8+00N	1	34	4	75	.2	13	10	154	3.71	15	5	ND	2	24	1	2	2	78	.31	.248	14	35	.43	168	.05	4	1.62	.01	.07	1	4
L13+10E 7+75N	1	121	11	75	.1	31	21	604	3.89	24	5	ND	2	31	1	3	2	62	.57	.090	16	46	.79	144	.06	5	1.47	.01	.15	1	10
L13+10E 7+50N	1	71	10	73	.1	31	16	463	3.56	21	5	ND	4	26	1	2	2	60	.47	.078	17	54	.93	101	.09	3	1.49	.01	.13	1	8
L13+75E 20+00N	2	58	17	182	.4	41	30	2734	4.11	18	5	ND	1	39	2	2	2	95	.76	.080	16	68	1.04	150	.11	6	2.42	.01	.12	1	2
L13+75E 19+75N	1	19	4	120	.2	17	8	232	2.48	9	5	ND	1	27	1	2	2	63	.51	.057	11	39	.49	71	.09	4	1.32	.01	.09	1	115
L13+75E 19+50N	1	30	10	119	.1	21	9	232	3.09	14	5	ND	2	27	1	3	2	83	.53	.052	11	44	.57	79	.12	4	1.43	.01	.07	1	3
L13+75E 19+25N	2	155	25	230	.9	79	32	1288	5.79	24	5	ND	2	50	1	2	2	110	.92	.076	26	124	1.54	177	.10	3	3.47	.02	.18	1	2
L13+75E 18+75N	1	82	12	163	.4	55	24	845	4.59	18	5	ND	2	36	1	2	2	101	.69	.054	15	99	1.62	99	.13	3	2.51	.01	.10	1	170
L13+75E 18+50N	1	42	11	147	.1	35	19	594	4.12	25	5	ND	2	31	1	3	2	77	.46	.083	16	62	1.03	93	.09	6	1.89	.01	.13	1	5
L13+75E 18+25N	1	34	4	143	.1	29	12	312	3.19	13	5	ND	1	26	1	2	2	74	.44	.038	14	54	.78	71	.09	4	1.66	.01	.07	1	7
L13+75E 18+00N	2	103	10	165	.9	56	20	981	4.05	24	5	ND	1	41	1	2	2	84	.75	.064	24	83	.86	138	.07	2	2.56	.01	.12	1	2
L13+75E 17+75N	1	24	9	174	.3	21	11	278	3.49	10	5	ND	2	20	1	2	2	76	.39	.098	11	58	.58	65	.10	3	1.81	.01	.05	1	4
L13+75E 17+50N	1	20	9	144	.1	24	9	316	3.04	8	5	ND	2	19	1	2	2	62	.37	.085	14	47	.60	74	.08	3	1.56	.01	.07	1	3
L13+75E 17+25N	1	29	7	95	.1	22	12	415	2.16	9	5	ND	1	25	1	2	2	52	.46	.040	13	39	.50	72	.06	3	1.29	.01	.07	1	4
L13+75E 17+00N	1	24	4	129	.1	26	10	211	3.33	12	10	ND	2	20	1	2	2	74	.36	.074	14	50	.67	84	.09	2	1.71	.01	.07	1	1
L13+75E 16+75N	1	14	4	77	.1	15	6	212	1.87	5	5	ND	1	16	1	2	3	49	.31	.037	11	29	.36	51	.08	2	1.04	.01	.05	1	1
L13+75E 16+50N	1	46	9	110	.1	36	14	543	2.86	10	5	ND	2	22	1	2	4	63	.39	.033	16	56	.81	92	.08	7	1.86	.01	.08	1	12
L13+75E 16+25N	1	16	4	84	.1	16	6	152	2.18	8	5	ND	2	17	1	2	2	62	.29	.042	12	34	.44	46	.10	2	1.13	7.36	.05	1	4
L13+75E 16+00N	1	56	11	143	.4	42	21	1316	3.40	15	5	ND	1	31	1	2	2	69	.48	.069	18	65	.76	136	.07	3	2.24	.01	.10	1	4
L13+75E 15+75N	1	24	12	81	.1	19	7	208	2.27	8	5	ND	1	22	1	2	2	55	.40	.035	13	40	.49	62	.08	2	1.36	.01	.07	1	5
L13+75E 15+50N	1	67	12	134	.3	52	16	757	3.47	22	5	ND	2	31	1	2	2	67	.51	.045	17	70	1.00	105	.08	3	2.13	.01	.10	1	3
L13+75E 15+25N	2	267	22	186	1.1	103	34	1309	6.20	40	6	ND	3	63	2	2	2	106	.96	.074	43	125	1.58	243	.07	7	4.18	.02	.24	2	4
L14+30E 17+50N	2	26	5	91	.1	23	10	408	2.71	15	5	ND	2	23	1	2	2	68	.44	.044	12	44	.65	61	.10	2	1.18	.01	.08	1	1
L14+30E 17+25N	1	33	10	125	.2	28	15	721	2.71	13	5	ND	1	25	1	2	2	63	.49	.037	13	51	.63	83	.08	6	1.65	.01	.08	1	6
L14+30E 17+00N	1	31	8	81	.1	22	24	988	2.24	9	5	ND	1	23	1	2	2	53	.44	.053	15	44	.52	89	.08	3	1.34	.01	.09	1	3
STD C/AU 0.5	20	56	38	128	6.8	62	29	1072	3.92	38	20	7	33	47	17	17	19	61	.48	.101	37	58	.88	176	.08	38	1.73	.06	.13	12	510

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

PAGE 4

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Aut PPB
L14+30E 16+75N	1	14	9	76	.2	15	6	258	1.90	3	5	ND	1	16	1	2	2	52	.29	.067	9	29	.31	61	.07	2	.90	.01	.06	1	15
L14+30E 16+50N	1	68	11	137	.2	42	22	1067	3.26	9	5	ND	1	24	1	2	2	69	.37	.059	13	61	.86	106	.06	2	2.09	.01	.10	1	1
L14+30E 16+25N	1	14	7	64	.1	17	5	177	1.29	5	5	ND	1	15	1	2	2	41	.30	.025	8	35	.34	49	.08	2	.83	.01	.04	1	1
L14+30E 16+00N	2	86	10	169	.6	61	20	713	3.84	17	5	ND	2	31	1	2	2	74	.45	.062	13	75	1.02	106	.06	2	2.32	.01	.11	1	4
L14+30E 15+75N	2	76	13	139	.3	54	20	896	3.61	16	5	ND	2	33	1	2	2	74	.51	.048	12	72	1.07	107	.07	3	2.16	.01	.09	1	1
L14+30E 15+50N	1	80	10	140	.4	52	20	811	3.31	15	5	ND	2	30	1	2	2	67	.49	.052	18	67	.82	105	.06	3	2.04	.01	.09	1	2
L14+30E 15+25N	1	58	6	110	.2	42	14	386	2.72	14	5	ND	2	25	1	2	2	58	.43	.034	14	53	.79	70	.08	5	1.52	.01	.08	1	1
L14+30E 15+00N	1	49	8	163	.1	41	16	468	3.03	10	5	ND	2	24	1	2	2	65	.45	.046	11	60	.89	82	.09	2	1.66	.01	.08	1	6
L14+30E 14+75N	2	112	13	165	.6	65	24	815	4.06	18	5	ND	2	35	1	2	2	76	.59	.055	20	85	1.12	124	.07	3	2.20	.01	.11	1	21
L14+30E 14+50N	1	47	4	103	.1	38	16	384	2.91	13	5	ND	2	23	1	2	2	64	.44	.038	12	61	.91	69	.09	2	1.52	.01	.08	1	3
STD C/AU 0.5	20	58	36	130	6.9	65	29	1087	3.91	40	22	7	34	48	17	16	22	62	.48	.107	36	58	.88	179	.08	37	1.72	.07	.13	13	490

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

PAGE 5

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au PPB
L14+30E 14+25N	3	372	23	267	2.2	154	40	1291	6.85	35	5	ND	3	65	2	2	2	108	.99	.109	42	147	1.72	273	.05	2	4.61	.02	.25	1	10
L14+30E 14+00N	3	404	25	270	2.5	163	42	1147	7.99	41	5	ND	4	61	2	2	2	124	.89	.083	28	160	1.77	310	.06	7	5.04	.02	.27	1	7
L14+30E 13+75N	3	215	17	244	1.1	108	33	991	6.07	32	7	ND	2	66	2	2	2	99	.95	.065	23	122	1.28	212	.06	2	3.45	.02	.18	1	2
L14+30E 13+50N	4	412	35	281	3.1	156	41	1091	8.37	54	11	ND	5	78	3	2	2	118	1.04	.080	27	162	1.64	329	.06	2	5.05	.02	.27	1	1
L14+30E 13+25N	4	334	29	302	2.5	149	36	1070	7.81	55	8	ND	4	81	3	2	2	112	1.14	.095	22	156	1.54	294	.06	6	4.95	.02	.27	1	13
L14+30E 13+00N	5	285	35	237	2.1	113	33	1034	6.75	83	6	ND	2	73	1	3	2	103	1.17	.116	26	127	1.37	229	.05	5	3.87	.02	.21	1	12
L14+30E 12+75N	3	91	20	151	.5	54	20	799	4.50	70	5	ND	2	36	1	2	2	80	.57	.058	13	77	1.14	113	.07	2	2.05	.01	.12	1	9
L14+30E 12+50N	6	108	19	329	1.2	41	22	6606	3.40	36	5	ND	1	33	4	3	2	69	.43	.130	7	41	.55	506	.05	4	1.28	.01	.11	1	25
L14+30E 12+25N	1	14	6	76	.4	14	6	220	2.27	14	5	ND	1	12	1	2	3	44	.20	.163	9	28	.32	101	.04	2	.88	.01	.06	1	2
L14+30E 12+00N	2	30	14	169	.3	23	15	789	2.95	20	5	ND	1	20	1	3	3	84	.36	.032	7	43	.67	124	.06	4	1.42	.01	.10	1	1
L14+30E 11+75N	3	436	18	255	3.1	117	32	1239	4.73	44	5	ND	1	43	3	2	2	75	.73	.065	37	83	.96	193	.04	5	2.66	.01	.13	1	12
L14+30E 11+50N	2	28	14	156	.4	26	12	263	3.07	33	5	ND	1	16	1	3	2	73	.27	.085	6	42	.57	72	.05	2	1.31	.01	.08	1	3
L14+30E 11+25N	1	42	13	391	.5	32	16	375	5.11	29	5	ND	2	22	1	2	2	95	.34	.199	4	64	.90	152	.06	2	2.52	.01	.12	1	1
L14+30E 11+00N	1	49	8	126	.3	22	19	1116	3.75	17	5	ND	1	27	1	2	2	83	.49	.094	5	44	.72	198	.05	2	1.60	.01	.10	1	75
L14+30E 10+75N	1	22	12	72	.2	12	11	621	2.66	7	5	ND	1	17	1	2	2	67	.35	.077	4	45	.40	118	.04	2	1.02	.01	.10	1	1
L14+30E 10+50N	2	156	15	103	.3	57	26	1345	4.51	23	5	ND	1	40	1	2	2	84	1.25	.044	3	95	.99	216	.05	4	2.65	.01	.08	1	1
L14+30E 10+25N	1	31	11	135	.3	35	16	419	3.20	11	5	ND	1	24	1	2	2	73	.38	.072	6	65	.98	109	.10	3	1.49	.01	.10	1	2
L14+30E 10+00N	1	27	9	173	.3	22	16	1922	2.64	10	5	ND	1	25	1	2	2	64	.51	.073	5	55	.64	202	.07	4	1.31	.02	.09	1	1
L14+30E 9+75N	1	99	13	140	.3	41	24	749	4.93	45	5	ND	1	39	1	2	2	101	.50	.170	4	74	1.36	304	.06	5	2.55	.02	.09	1	11
L14+30E 9+50N	1	111	16	132	.2	56	26	499	4.83	28	5	ND	2	32	1	2	2	106	.42	.067	6	81	1.49	231	.09	8	2.88	.02	.07	1	6
L14+30E 9+25N	1	25	14	101	.2	27	14	429	2.91	10	5	ND	1	25	1	2	2	72	.42	.104	6	58	.79	122	.09	2	1.65	.02	.09	1	3
L14+30E 9+00N	1	45	11	103	.2	35	17	570	3.84	31	5	ND	1	26	1	2	2	88	.45	.097	7	60	.86	157	.06	4	1.96	.02	.10	1	8
L14+30E 8+75N	1	22	8	54	.1	16	10	287	2.19	8	5	ND	1	22	1	2	2	53	.34	.045	8	35	.51	102	.07	2	1.16	.01	.06	1	6
L14+30E 8+50N	1	59	5	61	.1	27	15	311	3.40	6	5	ND	2	30	1	2	3	80	.48	.040	10	49	.79	89	.08	3	1.83	.01	.08	1	1
L14+30E 8+25N	1	74	7	64	.2	22	17	438	3.37	5	5	ND	2	27	1	2	2	82	.40	.048	10	37	.71	160	.07	4	1.67	.01	.08	1	1
L14+30E 8+00N	1	86	10	77	.3	38	15	337	3.72	11	5	ND	4	22	1	2	2	55	.38	.037	17	52	.85	76	.06	3	1.54	.01	.08	1	13
L14+30E 7+75N	1	48	12	81	.1	36	14	392	3.40	13	5	ND	4	21	1	2	2	46	.35	.084	17	45	.80	73	.07	2	1.35	.01	.10	1	21
L14+30E 7+50N	1	75	9	85	.5	42	16	473	3.64	18	5	ND	3	32	1	2	2	55	.60	.054	15	53	.89	115	.07	7	1.63	.01	.10	1	3
L15+6SE 17+50N	1	31	6	94	.1	27	11	293	2.52	7	5	ND	2	23	1	2	3	59	.40	.032	11	49	.80	62	.09	2	1.53	.01	.06	1	51
L15+6SE 17+25N	1	22	13	115	.1	23	9	215	3.02	9	5	ND	1	18	1	2	2	68	.36	.071	9	48	.59	59	.08	3	1.47	.01	.07	1	1
L15+6SE 17+00N	1	28	5	72	.1	26	10	308	2.56	13	5	ND	2	20	1	2	2	54	.36	.049	10	49	.82	54	.09	5	1.38	.01	.07	1	8
L15+6SE 16+75N	1	20	12	85	.2	21	8	192	2.25	8	5	ND	1	21	1	2	2	55	.38	.041	11	40	.54	62	.08	2	1.22	.01	.07	1	1
L15+6SE 16+50N	1	42	8	125	.1	35	15	402	2.58	8	5	ND	2	25	1	2	2	55	.41	.039	12	49	.67	74	.08	5	1.45	.01	.07	1	6
L15+6SE 16+25N	1	90	18	126	.4	56	19	784	3.39	11	5	ND	2	32	1	2	2	66	.52	.039	18	69	.87	110	.06	6	2.18	.01	.10	1	4
L15+6SE 16+00N	1	77	10	143	.5	49	17	669	2.98	10	5	ND	1	36	1	2	2	65	.64	.053	17	59	.75	101	.06	2	1.90	.01	.09	1	4
L15+6SE 15+75N	1	27	11	111	.2	25	14	545	2.83	11	5	ND	1	20	1	2	2	77	.40	.054	7	47	.65	79	.08	3	1.41	.01	.08	1	3
STD C/AU 0.5	20	56	37	128	6.8	68	29	1075	3.91	40	22	7	33	47	16	15	19	61	.48	.100	35	57	.88	176	.08	37	1.72	.06	.13	13	510



SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	R PPM	Al %	Na %	K %	W PPM	Au# PPB
L15+6SE 15+50M	1	35	13	126	.1	32	11	288	2.51	6	5	ND	2	24	1	2	3	55	.40	.031	12	46	.75	69	.08	4	1.50	.01	.06	1	44
L15+6SE 15+25M	2	56	8	104	.2	42	15	476	3.19	10	5	ND	2	27	1	2	2	67	.46	.034	14	60	.98	79	.08	2	1.71	.01	.08	1	70
L15+6SE 15+00M	2	84	13	144	.3	49	21	735	3.22	14	5	ND	1	33	1	2	2	66	.54	.051	22	64	.95	107	.07	3	1.88	.01	.10	1	4
L15+6SE 14+75M	2	47	9	120	.1	39	14	359	3.43	15	5	ND	2	24	1	2	2	73	.45	.170	11	61	.90	101	.07	3	1.68	.01	.09	1	14
L15+6SE 14+50M	3	289	30	202	.7	114	37	1236	5.28	25	5	ND	1	51	2	2	2	96	.79	.095	45	115	1.55	185	.05	2	3.58	.02	.17	1	2
L15+6SE 14+25M	3	257	31	223	1.0	114	40	1728	5.98	34	5	ND	2	56	3	2	2	103	.88	.097	48	136	1.76	210	.05	2	3.72	.02	.18	1	1
L15+6SE 14+00M	3	332	21	237	2.4	128	33	1226	5.79	34	5	ND	1	95	4	2	2	88	1.61	.107	55	127	1.25	281	.05	3	3.97	.01	.21	1	4
L15+6SE 13+75M	3	322	22	249	2.8	116	29	867	5.40	42	5	ND	1	116	4	2	2	82	2.35	.117	31	112	1.03	227	.04	4	3.34	.01	.18	1	6
L15+6SE 13+50M	9	289	16	166	2.3	97	26	1087	5.20	52	15	ND	1	144	2	2	2	82	2.62	.161	24	106	1.04	184	.04	3	3.22	.01	.17	1	10
L15+6SE 13+25M	4	117	26	340	1.1	69	24	1157	4.23	34	5	ND	1	92	2	2	2	64	1.72	.082	16	82	1.17	149	.05	3	2.43	.02	.13	1	3
L15+6SE 13+00M	5	264	29	224	3.5	112	29	799	6.93	80	13	ND	2	104	2	2	4	103	2.01	.146	37	142	1.31	246	.04	5	4.37	.02	.26	1	15
L15+6SE 12+75M	5	406	54	242	2.7	121	41	1105	7.69	96	5	ND	3	70	3	3	2	114	1.15	.083	33	117	.94	231	.07	2	3.21	.02	.14	1	630
L15+6SE 12+50M	3	110	23	384	1.9	40	23	2962	3.50	32	5	ND	1	72	4	2	4	72	1.34	.132	15	51	.51	224	.05	4	1.38	.01	.10	1	1
L15+6SE 12+25M	2	72	19	207	.3	36	19	1319	4.31	61	5	ND	1	25	2	4	2	67	.46	.120	15	42	.60	175	.04	4	1.28	.01	.11	1	9
L15+6SE 12+00M	2	38	12	124	.3	20	11	240	3.79	18	5	ND	2	15	1	2	2	74	.23	.075	12	40	.62	82	.04	3	1.68	.01	.05	1	1
L15+6SE 11+75M	1	22	10	97	.4	13	9	321	1.79	17	5	ND	1	22	1	2	2	53	.32	.038	9	28	.30	113	.04	3	.76	.01	.06	1	3
L15+6SE 11+50M	4	1123	49	472	4.5	221	29	1199	7.76	105	8	ND	5	77	3	4	3	107	1.41	.057	44	151	1.47	307	.05	3	3.90	.02	.23	1	26
L15+6SE 11+25M	6	795	38	433	3.9	184	25	2102	7.40	99	5	ND	3	88	5	3	2	108	1.72	.098	48	127	1.11	360	.05	5	3.87	.02	.20	1	18
L15+6SE 11+00M	1	28	11	123	.2	18	15	545	2.77	10	5	ND	1	22	1	2	3	66	.39	.084	8	41	.57	82	.06	3	1.16	.01	.09	1	1
L15+6SE 10+75M	1	68	14	182	.3	34	20	820	4.09	16	5	ND	1	26	1	2	2	83	.39	.101	12	51	.79	172	.05	4	1.76	.01	.12	1	1
L15+6SE 10+50M	2	83	15	138	.2	37	21	814	3.88	28	5	ND	1	34	2	2	4	73	.75	.113	9	58	1.00	113	.05	6	1.63	.01	.14	1	7
L15+6SE 10+25M	2	48	10	147	.4	38	15	1269	2.33	8	5	ND	1	46	3	2	2	45	1.26	.089	5	68	1.25	106	.05	6	1.10	.01	.09	1	1
L15+6SE 10+00M	1	45	10	140	.2	60	19	578	3.70	14	5	ND	2	32	1	2	3	79	.47	.126	12	102	1.58	234	.12	4	1.99	.02	.09	1	1
L15+6SE 9+75M	1	21	15	91	.2	34	18	1174	2.52	6	5	ND	1	21	1	2	2	64	.42	.054	8	79	.77	137	.07	3	1.14	.02	.08	1	1
L15+6SE 9+50M	1	94	16	100	.2	47	22	682	4.14	22	5	ND	2	28	1	2	2	85	.43	.062	14	83	1.43	153	.08	5	2.05	.01	.10	1	2
L15+6SE 9+25M	1	53	14	150	.2	45	23	807	3.76	8	5	ND	1	30	1	2	4	83	.40	.068	12	85	1.52	248	.15	2	2.09	.02	.11	1	1
L15+6SE 8+75M	1	101	24	112	.1	56	25	546	5.10	90	5	ND	2	28	1	2	2	106	.42	.052	14	80	1.52	141	.11	6	2.42	.01	.13	1	14
L15+6SE 8+50M	1	105	12	91	.2	61	26	783	5.00	44	5	ND	3	42	1	2	5	89	.55	.034	16	92	1.59	196	.06	4	2.36	.01	.12	1	27
L15+6SE 8+25M	1	349	19	90	.5	65	50	2771	6.90	86	5	ND	3	125	1	2	2	153	1.60	.068	28	76	1.76	586	.04	6	2.93	.01	.17	1	16
L15+6SE 8+00M	1	225	12	71	.2	45	32	679	5.13	33	5	ND	3	48	1	2	3	94	.54	.069	17	60	1.02	196	.07	3	2.28	.01	.12	1	11
L16+90E 17+50M	1	42	11	110	.1	34	13	329	2.93	8	5	ND	2	24	1	2	2	67	.41	.038	12	55	.86	64	.09	2	1.55	.01	.05	1	3
L16+90E 17+25M	2	60	20	111	.3	36	29	1145	3.19	10	5	ND	1	35	1	2	3	74	.62	.055	19	67	.86	109	.06	2	2.11	.01	.08	1	1
L16+90E 17+00M	1	54	18	117	.3	31	26	1149	2.68	7	5	ND	1	25	1	2	4	60	.48	.045	17	63	.71	90	.06	2	1.74	.01	.08	1	1
L16+90E 16+75M	1	33	12	95	.1	26	11	280	2.50	6	5	ND	1	25	1	2	2	61	.43	.028	13	48	.69	65	.08	2	1.43	.01	.05	1	1
L16+90E 16+50M	1	32	14	116	.3	25	11	339	2.66	7	5	ND	1	24	1	2	2	59	.42	.033	12	44	.61	67	.07	3	1.35	.01	.07	1	1
L16+90E 16+25M	1	27	10	77	.1	23	9	298	2.62	10	5	ND	3	20	1	2	2	59	.35	.043	13	42	.62	63	.09	2	1.21	.01	.08	1	2
STD C/AU-0.5	20	58	36	130	6.9	69	29	1089	3.93	37	22	8	34	47	16	16	20	62	.48	.106	39	58	.88	176	.08	38	1.72	.06	.13	14	480

## E &amp; B EXPLORATION PROJECT - 5055 FILE # B6-1917

PAGE 7

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Aut
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM	PPM	
L16+90E 16+00N	1	29	8	156	.2	28	11	481	2.53	6	5	ND	1	31	1	2	3	54	.52	.055	9	40	.47	95	.07	3	1.37	.01	.08	1	1
L16+90E 15+75N	1	116	19	141	1.2	73	24	1001	4.63	21	5	ND	2	52	1	2	2	89	.98	.058	21	104	1.25	140	.09	2	2.69	.02	.14	1	2
L16+90E 15+50N	2	122	11	147	.5	65	24	935	4.36	24	5	ND	3	58	1	2	5	83	.94	.051	25	90	1.16	112	.08	2	2.36	.01	.12	1	5
L16+90E 15+25N	1	72	5	176	.5	52	18	516	3.59	17	5	ND	2	38	1	2	2	73	.61	.039	15	72	1.00	82	.08	4	1.96	.02	.08	1	8
L16+90E 15+00N	2	111	11	164	.7	64	23	1010	3.85	12	5	ND	1	46	1	2	4	73	.81	.061	18	77	.85	130	.05	3	2.43	.01	.12	1	1
L16+90E 14+75N	1	13	9	140	.1	20	9	267	2.47	8	5	ND	1	20	1	2	2	64	.39	.104	8	43	.43	73	.07	2	1.07	.01	.08	1	1
L16+90E 14+50N	2	43	6	110	.1	36	14	274	2.73	9	5	ND	2	23	1	2	4	61	.40	.065	12	52	.73	60	.08	2	1.38	.01	.06	1	1
L16+90E 14+25N	2	43	4	138	.1	35	13	362	3.18	14	5	ND	2	21	1	2	3	66	.36	.067	12	58	.81	72	.07	4	1.41	.01	.07	1	2
L16+90E 14+00N	2	34	9	147	.2	27	14	321	3.27	14	5	ND	1	23	1	2	2	74	.38	.050	11	56	.65	64	.07	4	1.31	.01	.12	1	1
L16+90E 13+50N	3	106	15	225	1.2	76	25	1387	4.23	27	5	ND	1	76	2	2	2	77	1.49	.060	14	114	1.20	136	.06	3	2.18	.03	.09	1	1
L16+90E 13+25N	1	49	12	212	.8	36	16	610	3.66	42	5	ND	1	41	1	2	2	65	.79	.045	14	58	.68	102	.05	3	1.82	.01	.07	1	26
L16+90E 13+00N	2	603	27	316	4.0	158	25	1974	7.00	71	5	ND	3	92	5	4	2	102	1.74	.082	70	148	1.11	293	.05	2	3.78	.02	.16	1	12
L16+90E 12+75N	3	62	7	148	.2	38	21	387	4.09	45	5	ND	1	32	1	3	2	88	.65	.087	12	69	.92	98	.04	2	1.96	.01	.07	1	6
L16+90E 12+50N	4	26	14	304	.5	20	14	4014	2.37	29	5	ND	1	35	6	2	3	59	.70	.070	9	36	.33	288	.05	4	.92	.01	.09	1	10
L16+90E 12+25N	3	326	21	168	3.1	112	29	1444	5.11	95	5	ND	1	125	2	3	3	83	3.07	.096	35	116	.84	217	.03	3	2.71	.01	.14	1	8
L16+90E 12+00N	2	262	13	336	1.4	105	31	1356	5.75	78	5	ND	2	40	3	3	4	104	.61	.156	28	129	1.08	292	.06	4	3.10	.02	.17	1	12
L16+90E 11+75N	6	41	14	279	.2	28	25	980	4.25	39	5	ND	1	19	1	3	4	113	.33	.188	11	56	.74	146	.06	3	1.69	.01	.10	1	1
L16+90E 11+25N	2	31	10	214	.1	25	12	223	3.47	40	5	ND	1	20	1	2	2	75	.32	.076	10	46	.61	79	.05	2	1.53	.01	.07	1	5
L16+90E 11+00N	2	38	9	162	.4	31	11	434	2.68	40	5	ND	1	27	1	2	4	61	.46	.031	11	41	.42	105	.05	3	1.38	.01	.05	1	1
L16+90E 10+75N	1	51	10	174	.3	36	15	286	3.71	32	5	ND	1	27	1	2	3	82	.34	.153	10	70	1.02	99	.06	5	2.02	.02	.11	1	1
L16+90E 10+50N	1	35	7	102	.2	25	11	263	2.72	15	5	ND	2	25	1	2	3	57	.35	.056	11	41	.64	97	.05	2	1.48	.01	.06	1	8
L16+90E 10+25N	1	88	5	94	.4	40	27	827	4.89	27	5	ND	1	25	1	2	2	120	.50	.049	6	100	1.24	177	.06	4	2.16	.01	.12	1	1
L16+90E 9+75N	1	82	5	79	.1	71	31	581	4.03	19	5	ND	1	39	1	2	2	90	.60	.044	3	93	2.27	129	.10	2	2.45	.03	.07	1	1
L16+90E 9+50N	1	88	7	99	.1	69	27	394	4.22	22	5	ND	1	36	1	2	2	100	.46	.036	5	115	1.73	156	.07	2	2.57	.02	.09	1	1
L16+90E 9+25N	1	73	7	83	.1	47	27	1292	3.64	16	5	ND	1	33	1	2	2	83	.95	.072	5	95	1.59	233	.08	5	1.91	.02	.10	1	1
L16+90E 9+00N	1	218	11	71	.4	65	35	824	4.57	51	5	ND	2	39	1	2	2	84	.85	.067	10	100	1.68	173	.08	2	1.84	.02	.11	1	12
L16+90E 8+75N	1	154	13	65	.3	73	33	823	4.08	39	5	ND	2	46	1	3	2	70	1.57	.066	8	97	2.15	203	.07	2	1.78	.02	.10	1	8
L21+25E 20+00N	1	26	7	198	.1	25	14	621	3.73	9	5	ND	1	25	1	2	2	100	.59	.117	10	50	.94	87	.14	2	1.87	.01	.08	1	1
L21+25E 19+75N	1	37	9	128	.3	29	12	323	2.61	9	5	ND	1	20	1	2	2	59	.36	.065	10	37	.63	61	.06	3	1.55	.01	.06	1	1
L21+25E 19+50N	1	41	5	288	.3	26	21	1403	3.90	10	5	ND	1	25	1	2	2	86	.55	.109	10	43	.90	98	.11	4	1.98	.01	.09	1	1
L21+25E 19+25N	1	55	9	206	.2	51	20	287	4.04	14	5	ND	2	38	1	2	2	88	.41	.094	11	55	.79	118	.09	4	2.43	.01	.07	1	1
L21+25E 18+75N	3	38	13	345	.4	24	9	330	4.79	15	5	ND	2	17	2	4	2	96	.21	.106	10	36	.59	82	.10	4	1.67	.01	.10	1	1
L21+25E 18+50N	1	62	14	156	.2	18	14	812	5.18	10	5	ND	1	27	2	2	2	134	.86	.142	10	36	1.06	81	.17	2	2.03	.02	.08	1	1
L21+25E 18+25N	1	25	5	103	.2	23	9	350	2.21	5	5	ND	1	26	1	2	2	57	.59	.028	11	36	.55	57	.10	4	1.54	.01	.05	1	1
L21+25E 18+00N	1	29	9	214	.3	22	13	562	3.59	7	5	ND	1	26	1	2	2	93	.52	.141	7	39	.80	88	.14	3	1.64	.01	.08	1	1
L21+25E 17+75N	1	32	5	256	.4	43	15	297	3.89	14	5	ND	2	21	1	2	2	79	.38	.139	9	56	.73	86	.09	4	2.19	.01	.07	1	6
STD C/AU 0.5	20	57	35	129	6.8	68	29	1088	3.92	42	21	8	34	49	17	15	18	62	.48	.104	38	58	.88	183	.08	38	1.72	.07	.13	12	495

E & B EXPLORATION PROJECT - 5055 FILE # 86-1917

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Tl PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	K PPM	Al %	Na %	K %	M PPM	Au PPM
L21+2SE 17+50N	1	20	10	195	.2	16	10	787	2.45	6	5	ND	1	21	1	2	2	65	.40	.069	9	40	.57	77	.10	5	1.30	.01	.08	1	4
L21+2SE 17+25N	1	21	3	205	.2	21	12	469	2.97	14	5	ND	1	25	1	2	2	74	.43	.107	9	45	.57	106	.09	7	1.67	.01	.06	1	2
L21+2SE 17+00N	1	23	6	161	.1	20	12	544	2.50	9	5	ND	1	26	1	2	2	65	.49	.093	6	40	.57	87	.09	2	1.37	.01	.07	1	2
L21+2SE 16+75N	2	41	2	200	.3	37	15	378	3.72	17	5	ND	1	30	1	2	2	86	.43	.081	8	65	.95	77	.10	5	1.91	.01	.07	1	85
L21+2SE 16+50N	2	69	10	358	.7	63	26	304	5.48	40	5	ND	2	30	1	2	2	109	.44	.146	7	93	.85	107	.08	2	3.15	.01	.08	1	3
L21+2SE 16+25N	1	19	5	167	.1	18	10	261	2.57	7	5	ND	1	23	1	2	2	73	.43	.078	7	53	.56	83	.11	4	1.36	.01	.06	1	2
L21+2SE 16+00N	1	42	11	180	.2	34	15	333	3.76	23	5	ND	1	30	1	2	2	82	.44	.149	6	84	1.00	83	.09	5	1.85	.01	.07	1	4
L21+2SE 15+75N	1	132	13	168	.8	65	18	301	4.08	24	5	ND	2	55	1	2	2	79	1.06	.074	6	102	1.07	122	.08	3	3.19	.02	.09	1	21
L21+2SE 15+50N	1	40	8	142	.2	33	15	443	3.46	16	5	ND	1	23	1	2	2	81	.42	.081	5	56	.86	62	.10	3	1.74	.01	.07	1	2
L21+2SE 15+25N	1	32	11	141	.2	20	13	870	2.53	13	5	ND	1	29	1	2	2	71	.48	.067	7	39	.40	121	.08	6	1.19	.01	.08	1	4
L21+2SE 15+00N	2	47	6	158	.2	29	14	295	3.79	17	5	ND	2	22	1	2	2	93	.38	.095	6	59	.80	57	.09	5	1.95	.01	.06	1	4
L21+2SE 14+75N	1	17	3	147	.1	15	12	735	2.08	8	5	ND	1	24	1	2	3	65	.39	.064	5	35	.38	85	.08	2	1.19	.01	.08	1	2
L21+2SE 14+50N	1	21	7	121	.1	17	8	175	2.27	12	5	ND	1	23	1	2	2	67	.41	.040	7	33	.40	38	.08	2	1.04	.01	.07	1	4
L21+2SE 14+25N	1	22	6	173	.2	21	12	468	2.62	11	5	ND	1	29	1	3	2	66	.43	.058	7	42	.51	61	.07	4	1.21	.01	.06	1	2
L21+2SE 13+75N	2	81	9	110	.5	54	20	738	3.70	23	5	ND	3	41	1	2	2	72	.75	.032	9	73	1.03	79	.09	5	1.93	.01	.10	1	5
L21+2SE 13+50N	2	149	10	200	1.6	63	19	441	3.30	19	6	ND	1	102	3	2	2	66	2.46	.078	10	77	.75	105	.04	2	2.08	.01	.10	1	1
L21+2SE 13+25N	2	32	9	275	.2	24	14	1105	2.79	15	5	ND	1	36	4	3	2	75	.81	.054	4	55	.42	78	.05	4	1.06	.01	.09	1	1
L21+2SE 13+00N	1	49	17	148	.1	36	14	297	3.57	33	5	ND	1	25	1	2	2	77	.45	.046	6	72	.88	87	.05	5	1.91	.01	.07	1	8
L21+2SE 12+75N	1	30	7	147	.1	28	16	362	3.43	16	5	ND	2	16	1	3	2	75	.30	.047	7	53	.70	74	.05	5	1.58	.01	.06	1	1
L21+2SE 12+50N	1	21	9	110	.1	69	21	765	3.16	13	5	ND	1	17	1	2	2	60	.49	.039	3	122	2.11	58	.08	6	2.16	.02	.05	1	1
L21+2SE 12+25N	1	18	6	103	.1	17	10	1106	2.15	14	5	ND	1	21	1	2	2	58	.46	.062	8	34	.48	119	.10	4	.98	.01	.09	1	1
L21+2SE 12+00N	1	54	15	139	.2	34	15	287	3.97	72	5	ND	2	18	1	3	2	84	.28	.136	8	53	.76	86	.04	4	1.91	.01	.07	1	85
L21+2SE 11+75N	1	35	6	125	.3	34	14	435	3.21	92	5	ND	1	21	1	3	2	74	.35	.063	7	51	.65	77	.06	5	1.64	.01	.07	1	175
L21+2SE 11+50N	1	32	14	175	.1	40	16	569	3.13	41	5	ND	2	26	1	2	2	63	.41	.055	9	54	.74	109	.07	4	1.70	.01	.09	1	75
L21+2SE 11+25N	1	30	9	217	.1	34	14	486	2.99	23	5	ND	2	24	1	2	2	59	.40	.064	9	49	.79	80	.07	4	1.54	.01	.08	1	5
L21+2SE 11+00N	1	25	12	113	.2	23	13	491	2.57	11	5	ND	2	19	1	2	2	52	.34	.060	9	38	.59	95	.06	5	1.28	.01	.09	1	2
L21+2SE 10+75N	2	57	7	85	.1	32	15	341	3.68	22	5	ND	2	19	1	2	2	76	.32	.070	10	53	.81	80	.06	3	1.69	.01	.09	1	1
L21+2SE 10+50N	1	44	9	76	.1	30	14	400	2.90	17	5	ND	2	18	1	2	2	60	.36	.060	10	48	.80	90	.07	4	1.28	.01	.08	1	17
L21+2SE 10+25N	1	47	9	189	.4	28	17	1999	3.35	13	5	ND	1	44	2	2	2	61	.81	.181	7	43	.69	321	.04	3	1.48	.01	.15	1	6
L21+2SE 10+00N	2	14	9	112	.2	13	11	639	1.91	5	5	ND	1	21	1	2	2	50	.44	.051	6	29	.27	101	.05	3	.93	.01	.09	1	1
L21+2SE 9+75N	2	26	9	100	.4	17	11	981	2.26	13	5	ND	1	20	1	3	2	52	.37	.071	8	36	.39	144	.06	4	.99	.01	.09	1	1
L21+2SE 9+50N	1	56	17	118	.4	44	15	1023	3.74	18	5	ND	2	28	1	2	2	66	.53	.072	8	65	.83	148	.06	7	2.05	.01	.13	1	5
L21+2SE 9+25N	2	222	19	103	.9	58	26	1376	4.23	23	5	ND	1	41	1	2	2	66	.79	.099	30	67	.98	302	.05	5	2.45	.01	.14	1	19
L21+2SE 9+00N	1	21	13	88	.4	25	11	527	2.76	12	5	ND	1	23	1	2	2	51	.41	.103	10	44	.69	92	.06	2	1.32	.01	.10	1	4
L21+2SE 8+75N	1	44	10	83	.4	21	15	1472	3.13	11	5	ND	1	25	1	2	2	58	.44	.072	10	44	.61	196	.06	4	1.37	.01	.10	1	2
STD C/AU 0.5	20	58	39	128	6.8	66	29	1080	3.92	37	21	7	34	48	17	16	18	61	.48	.102	35	58	.89	179	.08	38	1.73	.07	.13	13	490

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

PAGE 9

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Ti	B	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L21+25E 8+50M	2	602	7	123	1.4	61	19	802	5.83	22	9	ND	1	72	2	4	4	85	1.21	.129	37	72	1.07	418	.03	6	3.01	.01	.22	1	8
L21+25E 8+25M	1	372	20	130	.9	51	36	975	5.37	23	5	ND	1	46	1	2	4	84	.65	.079	25	69	1.08	277	.05	3	2.26	.01	.15	1	6
L21+25E 8+00M	2	708	19	136	1.8	75	26	1096	7.44	34	5	ND	3	64	1	4	3	114	.98	.089	28	93	1.37	502	.04	2	3.74	.02	.27	1	12
L21+25E 7+75M	2	643	13	113	1.6	68	29	1283	6.70	23	6	ND	2	64	1	3	2	110	.96	.098	31	83	1.46	437	.04	2	3.58	.02	.23	1	11
L21+25E 7+50M	1	170	8	75	.4	29	25	590	4.88	20	5	ND	2	41	1	2	3	105	.56	.104	11	50	.90	158	.06	5	1.63	.02	.13	1	8
L22+50E 20+00M	2	43	15	213	.4	35	20	614	4.27	21	5	ND	1	44	1	3	2	90	.60	.147	7	48	.62	80	.08	2	1.67	.01	.06	1	2
L22+50E 19+50M	1	26	11	277	.3	14	17	3206	2.34	7	5	ND	1	47	6	2	2	64	.77	.092	6	27	.37	177	.08	2	1.21	.02	.11	1	1
L22+50E 19+00M	2	187	5	225	1.1	70	33	1161	5.66	22	5	ND	2	55	2	2	5	122	.99	.077	15	91	1.67	112	.13	2	2.98	.02	.10	1	1
L22+50E 18+75M	2	47	11	240	.5	29	20	2490	2.91	10	5	ND	1	49	3	2	4	63	1.00	.061	6	41	.41	106	.08	2	1.53	.01	.08	1	1
L22+50E 18+50M	1	49	6	230	.4	29	16	661	3.11	12	5	ND	1	33	1	2	2	75	.57	.074	9	43	.51	86	.09	2	1.67	.01	.09	1	1
L22+50E 18+25M	2	29	10	183	.3	18	13	661	2.46	9	5	ND	1	33	2	2	2	66	.60	.065	6	36	.37	81	.09	2	1.03	.01	.07	1	95
L22+50E 18+00M	1	40	12	279	.4	33	15	540	3.04	10	5	ND	2	33	1	2	3	66	.48	.050	10	48	.66	69	.09	2	1.67	.01	.06	1	15
L22+50E 17+75M	2	37	2	131	.4	24	10	324	2.94	14	5	ND	1	29	1	2	2	70	.36	.073	11	44	.64	54	.09	2	1.29	.01	.07	1	28
L22+50E 17+50M	2	55	12	257	.4	32	17	335	4.83	19	5	ND	2	33	1	3	2	111	.34	.171	8	59	.88	88	.10	7	2.06	.01	.08	1	1
L22+50E 17+25M	1	44	10	130	.3	32	14	374	3.23	11	5	ND	1	31	1	2	2	83	.49	.035	9	54	.63	64	.08	3	1.70	.01	.07	1	1
L22+50E 17+00M	1	27	6	180	.2	23	14	565	3.14	15	5	ND	2	27	1	2	3	76	.45	.075	8	43	.63	77	.10	6	1.42	.01	.09	1	3
L22+50E 16+75M	2	54	7	180	.3	40	16	295	4.26	27	5	ND	1	34	1	2	2	104	.44	.040	7	66	.79	71	.12	2	1.92	.01	.06	1	1
L22+50E 16+50M	3	87	7	261	.3	67	25	518	5.27	49	5	ND	1	36	1	2	4	113	.45	.166	6	85	1.54	95	.10	2	2.64	.01	.08	1	1
L22+50E 16+25M	1	23	11	170	.2	22	16	808	3.08	12	5	ND	1	28	1	2	4	80	.45	.109	7	54	.55	101	.09	2	1.37	.01	.09	1	1
L22+50E 16+00M	2	43	7	153	.5	28	16	595	3.00	21	5	ND	1	38	1	3	3	86	.64	.049	7	72	.59	89	.08	2	1.68	.01	.07	1	1
L22+50E 15+75M	1	63	9	240	.7	38	17	851	3.14	12	5	ND	1	41	1	2	2	67	.76	.052	13	76	.68	107	.08	3	1.79	.01	.08	1	8
L22+50E 15+50M	3	147	9	187	1.1	69	28	1177	5.62	33	5	ND	3	45	1	2	4	128	.88	.074	12	120	1.60	116	.12	4	3.14	.02	.13	1	2
L22+50E 15+25M	1	39	12	202	.4	39	18	1104	3.47	16	5	ND	1	34	1	2	8	78	.62	.076	7	71	.01	91	.09	3	2.11	.01	.06	1	1
L22+50E 15+00M	2	167	9	160	.9	69	25	1199	4.05	20	5	ND	1	50	2	2	2	86	.85	.066	16	91	1.09	87	.07	2	2.52	.02	.09	1	1
L22+50E 14+75M	1	84	5	150	.5	44	21	1503	3.75	13	5	ND	1	32	1	2	2	78	.53	.054	15	63	.68	100	.07	2	2.13	.01	.09	1	1
L22+50E 14+50M	3	216	17	181	1.2	87	29	1285	5.42	33	5	ND	2	68	2	2	4	101	1.22	.074	21	118	1.10	156	.06	2	3.41	.02	.13	1	1
L22+50E 14+25M	1	41	12	125	.2	27	17	513	3.09	12	5	ND	1	36	2	2	2	78	.62	.066	9	53	.54	75	.08	2	1.40	.01	.08	1	1
L22+50E 14+00M	2	111	13	228	.3	58	27	638	4.96	29	5	ND	1	41	1	2	4	108	.45	.127	6	71	1.04	97	.07	2	2.36	.01	.08	1	1
L22+50E 13+75M	2	53	10	106	.1	42	17	303	3.58	19	5	ND	1	32	1	2	2	90	.38	.067	8	67	1.01	66	.07	6	1.74	.01	.07	1	2
L22+50E 13+50M	1	17	9	115	.1	16	9	363	1.92	10	5	ND	1	22	1	2	2	64	.37	.042	8	37	.34	75	.07	2	1.07	.01	.06	1	1
L22+50E 13+25M	3	119	7	238	.3	73	27	396	4.71	25	5	ND	2	23	2	2	2	94	.32	.065	7	87	1.32	95	.06	5	2.55	.01	.06	1	1
L22+50E 13+00M	4	26	12	167	.4	22	13	334	4.08	20	5	ND	1	19	2	2	2	149	.45	.046	6	52	.53	78	.06	3	1.50	.01	.08	1	1
L22+50E 12+75M	5	93	7	348	.6	83	30	626	5.87	14	5	ND	1	13	2	2	5	131	.35	.132	4	152	2.01	61	.08	4	2.92	.01	.06	1	1
L22+50E 12+50M	1	49	2	149	.2	36	16	363	3.59	18	5	ND	1	19	1	3	2	86	.31	.075	9	65	.93	62	.06	2	1.63	.01	.07	1	1
L22+50E 12+25M	1	28	15	288	.5	31	17	1425	3.15	16	5	ND	1	26	3	2	2	72	.49	.076	7	59	.77	111	.07	2	1.66	.01	.08	1	710
L22+50E 12+00M	2	48	24	430	.5	45	22	868	4.11	20	5	ND	1	24	2	2	3	89	.49	.114	8	69	1.03	98	.08	5	2.03	.01	.09	1	1
STD C/AU-0.5	20	59	37	130	6.8	69	30	1092	3.92	42	21	7	34	48	18	16	19	62	.48	.105	37	59	.88	179	.08	36	1.72	.07	.13	13	510

E & B EXPLORATION PROJECT - 5055 FILE # 86-1917

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Ti	B	Al	Na	K	W	Aut
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L22+50E 11+75N	2	45	9	161	.2	35	16	538	3.78	50	5	ND	1	20	1	2	2	77	.36	.124	9	60	.82	114	.05	4	1.80	.01	.08	1	26
L22+50E 11+50N	1	29	9	136	.1	31	13	629	2.78	15	5	ND	2	22	1	2	2	60	.36	.069	10	51	.68	107	.06	3	1.48	.01	.09	1	4
L22+50E 11+25N	1	54	36	170	.4	45	18	752	3.70	50	5	ND	2	40	1	6	2	80	.48	.047	9	61	.94	126	.06	4	2.03	.01	.09	1	13
L22+50E 11+00N	2	69	41	229	.4	60	20	988	4.24	132	5	ND	2	36	1	8	2	74	.43	.064	8	64	.98	133	.05	4	2.16	.01	.10	1	10
L22+50E 10+75N	2	37	38	256	.3	46	19	1921	3.36	34	5	ND	1	43	2	4	2	62	.68	.107	8	51	.74	181	.05	8	2.01	.01	.12	1	3
L22+50E 10+25N	2	59	17	169	.2	45	17	949	3.69	32	5	ND	2	33	2	4	2	68	.55	.089	8	55	.93	149	.05	6	1.59	.01	.10	1	4
L22+50E 9+75N	2	29	19	129	.3	26	12	359	3.42	25	5	ND	1	30	1	2	2	73	.55	.054	8	49	.58	107	.05	3	1.60	.01	.06	1	4
L22+50E 9+25N	2	67	10	92	.3	49	18	793	3.62	18	6	ND	1	39	1	2	2	64	.79	.071	16	64	.90	145	.05	4	2.09	.01	.11	1	3
L22+50E 8+75N	4	828	25	142	2.4	87	29	1159	10.07	46	5	ND	3	63	1	4	2	138	.97	.123	28	106	1.27	615	.04	4	4.01	.02	.30	1	16
L22+50E 8+50N	3	772	17	127	1.7	80	24	1197	7.37	25	5	ND	2	66	1	2	2	103	1.15	.119	34	86	1.24	546	.03	3	3.54	.01	.26	1	14
L22+50E 8+25N	1	417	18	104	.9	48	32	783	6.98	19	7	ND	1	71	1	2	2	74	1.47	.085	27	61	.92	350	.03	4	2.31	.01	.16	1	10
L22+50E 8+00N	2	426	21	113	.6	54	40	1194	6.62	27	5	ND	3	42	1	2	2	102	.68	.085	19	74	1.31	312	.05	5	2.78	.02	.20	1	25
L22+50E 7+75N	2	489	24	143	1.0	64	28	1320	7.28	24	5	ND	3	49	1	2	2	118	.76	.086	23	85	1.35	406	.05	3	3.19	.02	.23	1	9
L22+50E 7+50N	3	537	18	120	.7	66	30	1709	7.13	19	5	ND	3	42	1	2	4	114	.50	.077	16	87	1.55	510	.05	5	3.56	.02	.28	1	8
L25+00E 20+00N	1	31	10	180	.1	33	11	285	2.86	9	5	ND	1	21	1	2	2	81	.46	.083	8	46	.62	62	.10	2	1.76	.01	.06	1	2
L25+00E 19+50N	2	30	6	224	.4	24	14	1112	3.09	8	5	ND	1	28	2	2	2	87	.55	.081	7	49	.76	111	.12	3	1.82	.01	.08	1	2
L25+00E 19+25N	1	62	11	141	.2	33	20	1421	4.61	18	5	ND	1	25	1	2	2	121	.67	.101	6	59	1.41	94	.16	2	2.12	.02	.10	1	2
L25+00E 19+00N	2	22	8	149	.2	23	10	369	2.70	9	5	ND	2	20	1	2	2	71	.35	.044	9	37	.60	75	.10	2	1.54	.01	.07	1	1
L25+00E 18+75N	1	37	9	192	.2	32	16	495	3.84	11	5	ND	1	77	1	3	2	98	.52	.107	7	48	.61	105	.10	4	1.88	.01	.07	1	4
L25+00E 18+25N	1	22	8	95	.1	21	8	225	2.44	4	5	ND	2	24	1	2	2	67	.46	.033	9	35	.56	34	.10	2	1.58	.01	.04	1	3
L25+00E 18+00N	1	22	8	201	.1	19	13	1214	2.39	6	5	ND	1	31	1	2	2	73	.51	.053	7	35	.54	97	.11	4	1.48	.01	.06	1	1
L25+00E 17+75N	3	41	14	138	.2	37	17	356	3.35	9	5	ND	2	23	1	2	2	77	.32	.050	8	43	.61	58	.10	2	1.71	.01	.06	1	8
L25+00E 17+50N	1	26	2	216	.1	19	12	444	3.11	7	5	ND	2	51	2	2	3	90	.42	.070	7	36	.39	76	.15	2	1.49	.01	.05	1	1
L25+00E 17+00N	2	39	10	142	.1	41	13	284	3.59	17	5	ND	3	24	1	2	2	86	.28	.060	10	60	.84	63	.09	3	1.97	.01	.06	1	42
L25+00E 16+75N	3	41	10	388	.2	38	14	335	3.97	14	5	ND	1	26	2	2	3	96	.35	.098	9	58	.83	83	.09	2	2.03	.01	.07	1	2
L25+00E 16+50N	3	49	10	224	.2	40	16	412	3.95	13	5	ND	2	39	1	2	2	94	.35	.072	9	58	.90	94	.09	4	1.94	.01	.06	1	2
L25+00E 16+25N	2	19	8	146	.2	15	9	521	2.77	10	5	ND	1	29	1	2	2	72	.39	.084	7	31	.39	95	.11	2	1.25	.01	.08	1	5
L25+00E 16+00N	2	38	3	188	.1	32	13	333	3.35	16	5	ND	2	29	1	2	2	78	.35	.069	10	50	.78	73	.08	2	1.65	.01	.07	1	2
L25+00E 15+75N	2	57	16	199	.2	40	16	366	4.21	17	5	ND	2	33	1	2	2	107	.39	.049	9	64	.92	83	.10	2	2.03	.01	.05	1	2
L25+00E 15+50N	2	54	10	385	.2	56	23	1592	4.37	14	5	ND	1	45	2	2	2	101	.59	.095	8	79	.97	214	.10	4	2.31	.01	.11	1	2
L25+00E 15+25N	2	31	9	210	.2	34	14	447	3.19	13	5	ND	1	32	1	2	2	84	.40	.058	8	55	.74	66	.09	3	1.54	.01	.07	1	24
L25+00E 15+00N	1	46	9	232	.3	45	18	623	3.40	10	5	ND	1	40	1	2	3	83	.66	.053	8	73	.77	55	.10	2	1.91	.01	.06	1	2
L25+00E 14+50N	1	37	4	133	.3	39	18	1076	2.75	8	5	ND	1	35	1	2	2	70	.64	.045	7	97	.88	64	.08	3	1.85	.01	.06	1	1
L25+00E 14+25N	1	14	6	74	.2	21	10	393	2.46	10	5	ND	1	22	1	2	3	76	.50	.049	7	54	.62	63	.10	2	1.31	.01	.05	1	1
L25+00E 14+00N	2	31	12	79	.1	32	13	502	2.77	16	5	ND	1	23	1	2	2	72	.40	.045	8	57	.72	63	.08	3	1.58	.01	.05	1	6
L25+00E 13+75N	2	29	9	112	.2	25	12	211	3.30	16	5	ND	2	21	1	2	3	82	.32	.054	8	47	.59	53	.08	2	1.39	.01	.07	1	5
STD C/AU 0.5	21	57	36	130	6.8	68	29	1089	3.92	38	23	7	34	48	16	16	21	62	.48	.107	37	59	.88	181	.08	36	1.72	.07	.13	12	505

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

PAGE 11

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	R	Al	Na	K	W	Au1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L25+00E 13+50N	1	23	14	135	.2	19	15	731	3.04	12	5	ND	1	20	1	2	3	76	.32	.073	8	37	.39	83	.06	2	1.39	.01	.06	1	21
L25+00E 13+25N	4	137	20	208	.3	37	25	804	8.18	698	5	ND	2	21	1	4	6	113	.25	.085	7	39	.53	93	.01	2	1.99	.01	.10	1	16
L25+00E 13+00N	4	69	17	214	.1	47	16	581	2.94	24	5	ND	1	26	1	2	2	66	.45	.037	7	51	.57	65	.05	2	1.81	.01	.06	1	6
L25+00E 12+75N	1	25	11	110	.2	40	15	759	3.18	16	5	ND	1	17	1	2	2	83	.31	.054	7	59	.72	88	.06	2	1.63	.01	.06	1	2
L25+00E 12+50N	2	21	5	87	.1	29	12	571	2.65	16	5	ND	1	17	1	2	2	68	.32	.046	7	47	.58	70	.06	3	1.37	.01	.05	1	4
L25+00E 12+25N	2	45	9	92	.1	54	17	255	3.54	21	5	ND	1	19	1	2	2	72	.30	.056	8	72	.94	62	.04	2	1.74	.01	.07	1	8
L25+00E 12+00N	1	41	7	101	.1	25	15	450	3.56	18	5	ND	1	17	1	2	3	78	.29	.047	8	46	.75	61	.05	2	1.66	.01	.06	1	1
L25+00E 11+75N	1	37	10	188	.1	31	16	434	3.45	45	5	ND	1	19	1	2	2	77	.40	.064	8	47	.71	75	.06	2	1.84	.01	.06	1	4
L25+00E 11+50N	1	79	7	191	.2	69	23	360	3.98	21	5	ND	1	21	1	3	2	84	.36	.054	6	86	1.03	63	.08	3	2.04	.01	.07	1	1
L25+00E 11+00N	1	49	4	104	.1	52	19	358	3.93	25	5	ND	2	14	1	3	2	71	.27	.093	6	74	1.02	56	.05	2	1.77	.01	.08	1	4
L25+00E 10+75N	3	88	10	139	.3	49	25	578	4.73	20	5	ND	1	24	1	2	2	103	.48	.088	4	62	.94	99	.05	2	2.05	.01	.08	1	7
L25+00E 10+50N	2	95	16	141	.1	54	25	474	4.79	25	5	ND	2	19	1	2	2	95	.39	.077	4	78	1.11	85	.06	2	2.06	.01	.10	1	1
L25+00E 10+25N	2	49	12	153	.1	33	22	1207	4.21	18	5	ND	1	26	1	2	2	81	.57	.224	5	59	.72	184	.04	4	1.73	.01	.13	1	1
L25+00E 10+00N	2	29	11	93	.1	19	13	273	3.66	18	5	ND	1	16	1	2	3	80	.31	.083	6	41	.43	74	.03	3	1.49	.01	.07	1	1
L25+00E 9+75N	1	37	16	93	.3	20	11	366	3.24	18	5	ND	1	32	1	2	2	61	.78	.059	8	36	.42	131	.04	3	1.43	.01	.07	1	3
L25+00E 9+50N	1	64	13	96	.4	26	16	428	3.31	18	5	ND	1	31	1	2	2	65	.78	.056	9	41	.52	183	.03	3	1.59	.01	.08	1	8
L25+00E 9+25N	1	53	12	81	.2	23	15	291	3.99	21	5	ND	2	18	1	2	2	72	.28	.094	11	45	.71	99	.04	3	1.51	.01	.08	1	4
L25+00E 9+00N	1	52	10	69	.2	24	14	533	3.47	23	5	ND	1	21	1	2	2	66	.33	.075	13	38	.61	170	.04	2	1.21	.01	.12	1	5
L25+00E 8+75N	2	164	12	104	1.4	65	24	1913	4.63	26	5	ND	2	41	3	2	2	72	.88	.083	20	75	.97	296	.06	2	2.46	.01	.16	1	6
L25+00E 8+50N	1	168	14	78	.3	39	23	681	4.39	24	5	ND	2	33	1	2	2	66	.63	.075	19	53	.90	226	.04	2	1.65	.01	.10	1	12
L25+00E 8+25N	1	150	13	72	.4	34	20	704	4.05	25	5	ND	2	34	1	2	2	62	.68	.096	22	50	.88	192	.04	4	1.57	.01	.10	1	14
L25+00E 8+00N	1	135	12	85	.3	35	22	792	4.22	19	5	ND	2	28	1	2	3	68	.49	.056	15	54	.90	232	.04	2	1.81	.01	.10	1	8
L25+00E 7+75N	1	82	8	71	.1	27	19	428	3.96	17	5	ND	2	20	1	2	3	68	.27	.057	11	45	.69	151	.04	2	1.49	.01	.08	1	5
L25+00E 7+50N	1	81	7	61	.1	25	17	404	4.20	17	5	ND	1	22	1	2	2	82	.34	.061	12	46	.69	133	.04	2	1.45	.01	.09	1	4
L27+50E 8+75N	1	25	9	51	.1	25	9	225	2.14	13	5	ND	2	20	1	2	2	43	.37	.050	13	41	.59	81	.07	2	1.25	.01	.08	1	7
L27+50E 8+00N	1	88	11	76	.3	26	17	357	4.03	22	5	ND	1	28	1	2	2	76	.37	.052	12	44	.58	234	.03	2	1.52	.01	.09	2	17
L27+50E 7+75N	1	65	9	72	.2	24	13	414	3.30	13	5	ND	1	19	1	2	2	58	.27	.063	12	36	.60	196	.03	2	1.24	.01	.08	1	5
L27+50E 7+50N	1	69	8	83	.3	21	15	530	3.30	13	5	ND	2	18	1	2	2	60	.26	.075	10	35	.49	156	.04	3	1.19	.01	.09	1	9
L27+50E 7+25N	1	56	7	71	.1	21	13	499	2.66	10	5	ND	1	18	1	2	2	51	.26	.050	13	35	.61	183	.03	2	1.36	.01	.08	1	20
L27+50E 7+00N	1	219	10	76	.6	36	23	729	4.39	22	5	ND	1	38	1	2	2	76	.53	.074	16	62	.88	306	.03	2	2.36	.01	.11	1	5
L27+50E 6+75N	1	68	2	50	.1	17	12	213	2.92	12	5	ND	1	29	1	2	2	63	.40	.046	9	31	.46	196	.02	2	1.06	.01	.06	2	2
L27+50E 6+50N	1	51	4	65	.2	17	13	259	3.67	12	5	ND	1	23	1	3	2	79	.34	.072	7	38	.53	135	.04	2	1.20	.01	.07	1	19
L27+50E 6+25N	1	132	3	71	.3	26	18	640	3.55	10	5	ND	1	32	1	2	3	84	.47	.065	9	50	.65	229	.04	2	1.96	.01	.10	1	10
L27+50E 6+00N	1	56	5	63	.1	15	13	1125	2.73	11	5	ND	1	24	1	2	2	77	.36	.066	7	36	.39	143	.06	2	1.21	.01	.07	1	7
L27+50E 5+75N	1	135	2	52	.1	19	12	231	2.46	8	5	ND	1	29	1	2	2	76	.43	.050	9	46	.87	124	.05	2	2.05	.01	.06	1	8
L27+50E 5+50N	2	198	12	73	.3	25	20	318	5.69	22	5	ND	2	29	1	2	2	127	.37	.116	4	56	.98	115	.06	2	2.13	.01	.06	1	7
STD C/AU-0.5	20	57	38	130	6.8	68	29	1086	3.91	40	21	7	33	47	16	17	19	62	.48	.105	35	58	.89	174	.08	38	1.72	.07	.13	12	480

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

PAGE 12

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	P	Al	Na	K	W	Au
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	I	I	I	I	PPM	PPB
L27+50E 4+50N	2	170	15	80	.6	36	22	553	4.28	13	5	ND	1	43	1	2	2	82	.70	.088	15	45	.62	261	.02	2	1.82	.01	.13	1	2
L27+50E 4+25N	2	160	17	92	.6	39	25	1076	4.97	17	5	ND	1	34	1	2	2	91	.44	.091	17	60	.86	249	.03	2	2.25	.01	.13	1	6
L27+50E 4+00N	2	129	13	84	.6	46	22	998	4.11	13	5	ND	1	38	1	2	2	79	.49	.077	24	54	.89	224	.04	5	2.04	.01	.11	1	3
L27+50E 3+75N	1	25	13	59	.2	12	7	196	2.14	5	5	ND	1	29	1	2	2	52	.25	.055	13	24	.20	117	.06	2	.61	.01	.06	1	1
L27+50E 3+50N	1	51	13	81	.1	31	12	253	4.16	12	5	ND	2	33	1	2	2	78	.18	.084	13	49	.47	118	.05	2	1.30	.01	.05	1	1
L27+50E 3+25N	1	21	9	73	.2	20	7	294	2.12	4	5	ND	1	43	1	2	2	41	.18	.076	13	30	.34	159	.04	4	.90	.01	.08	1	1
L27+50E 3+00N	1	21	9	64	.4	20	7	156	2.78	4	5	ND	2	41	1	2	2	52	.26	.068	16	31	.40	124	.05	2	1.09	.01	.06	1	1
L27+50E 2+75N	1	31	9	98	.4	24	12	371	2.89	9	5	ND	1	39	1	2	2	59	.35	.127	12	36	.38	192	.05	8	1.26	.01	.05	1	2
L27+50E 2+50N	1	15	7	67	.5	14	6	365	2.01	6	5	ND	1	35	1	2	2	43	.20	.074	14	27	.31	113	.04	3	.86	.01	.05	1	1
L27+50E 2+25N	1	19	5	53	.2	13	5	610	1.62	7	5	ND	1	46	1	2	2	42	.27	.043	10	18	.10	145	.04	3	.37	.01	.07	1	1
L27+50E 2+00N	1	32	14	130	.1	30	12	284	3.63	21	5	ND	3	31	1	2	3	63	.24	.189	12	40	.49	137	.05	3	1.44	.01	.06	1	2
L27+50E 1+75N	1	16	9	49	.1	14	6	139	1.64	11	5	ND	2	38	1	2	2	40	.18	.052	13	22	.20	93	.05	2	.56	.01	.06	1	1
L27+50E 1+50N	1	33	9	108	.4	30	11	328	3.43	16	5	ND	2	39	1	2	2	60	.24	.086	12	37	.39	115	.04	4	1.24	.01	.07	1	3
L27+50E 1+25N	1	15	8	54	.3	13	6	371	1.53	10	5	ND	1	51	1	2	2	38	.17	.037	12	18	.08	110	.04	2	.41	.01	.05	1	1
L27+50E 1+00N	1	36	11	73	.2	31	11	393	3.37	18	5	ND	3	37	1	2	2	63	.26	.072	14	42	.51	89	.05	5	1.14	.01	.07	1	2
L27+50E 0+75N	1	15	9	44	.2	14	6	556	1.56	9	5	ND	1	38	1	2	2	42	.22	.039	12	22	.10	121	.05	2	.49	.01	.06	1	1
L27+50E 0+50N	1	25	8	63	.1	20	8	226	2.64	8	5	ND	1	24	1	2	2	58	.29	.080	12	38	.54	82	.05	3	1.24	.01	.06	1	2
L27+50E 0+25N	1	15	3	92	.1	13	7	165	2.31	7	5	ND	2	16	1	2	2	50	.25	.103	10	31	.34	88	.07	2	1.09	.01	.05	1	3
L27+50E 0+00N	1	24	11	73	.1	19	8	220	2.71	6	5	ND	1	20	1	2	2	57	.27	.090	12	37	.42	90	.07	3	1.07	.01	.07	1	1
L30+00E 10+00N	2	113	15	136	.7	36	25	830	5.66	34	5	ND	2	34	1	7	2	104	.69	.053	14	69	.82	231	.02	2	2.45	.01	.11	1	2
L30+00E 9+75N	2	84	20	110	.2	40	25	880	5.20	33	5	ND	2	27	1	3	2	90	.60	.054	10	78	1.34	193	.04	2	2.08	.01	.11	1	1
L30+00E 9+50N	1	29	9	70	.2	12	11	219	3.57	5	5	ND	1	17	1	2	2	82	.23	.055	10	34	.33	98	.03	2	1.04	.01	.10	1	1
L30+00E 9+25N	1	21	4	54	.1	9	7	198	1.96	4	5	ND	1	14	1	2	2	57	.22	.036	11	24	.31	91	.05	2	.92	.01	.07	1	1
L30+00E 9+00N	2	90	11	80	.1	31	18	550	4.28	27	5	ND	2	21	1	2	2	75	.43	.082	11	54	1.05	130	.05	2	1.68	.01	.09	1	7
L30+00E 8+75N	1	14	9	74	.2	10	8	553	1.86	5	5	ND	1	18	1	2	2	48	.32	.053	9	23	.28	169	.04	2	.85	.01	.08	1	1
L30+00E 8+50N	1	18	14	119	.1	11	8	1201	1.84	7	5	ND	1	20	1	2	3	40	.41	.055	9	27	.37	305	.04	2	.82	.01	.10	1	15
L30+00E 8+25N	1	25	5	124	.3	10	12	612	3.31	8	5	ND	1	15	1	2	2	74	.26	.082	8	33	.43	186	.03	4	1.49	.01	.10	1	1
L30+00E 8+00N	1	68	14	92	.2	27	16	418	4.20	20	5	ND	1	18	1	2	3	77	.32	.101	8	54	.83	158	.03	2	1.65	.01	.08	1	5
L30+00E 7+75N	1	52	4	89	.1	20	15	485	3.58	18	5	ND	1	21	1	2	2	69	.33	.052	9	43	.70	142	.05	3	1.29	.01	.09	1	2
L30+00E 7+25N	1	258	15	107	.7	49	29	784	4.97	25	5	ND	1	41	1	2	2	77	.71	.067	24	56	.85	353	.03	2	2.10	.01	.13	1	6
L30+00E 7+00N	1	74	10	78	.2	28	16	306	4.31	20	5	ND	1	19	1	2	2	66	.28	.101	8	42	.74	129	.03	2	1.61	.01	.07	1	4
L30+00E 6+75N	1	49	4	91	.1	19	14	505	3.15	9	5	ND	2	19	1	2	2	54	.29	.100	10	30	.52	138	.04	2	.98	.01	.09	1	1
L30+00E 4+75N	3	334	12	68	.1	30	35	791	5.99	22	5	ND	1	32	1	2	2	116	.44	.137	6	50	1.25	211	.06	2	1.78	.01	.08	1	7
L30+00E 4+25N	2	281	4	59	.2	24	28	305	6.07	15	5	ND	1	38	1	2	2	150	.44	.143	5	49	1.00	164	.07	2	1.91	.01	.08	1	6
L30+00E 4+00N	1	60	8	69	.2	14	13	185	3.93	14	5	ND	2	19	1	2	2	72	.22	.155	9	28	.48	118	.04	3	1.41	.01	.07	1	2
L30+00E 3+75N	2	221	8	66	.3	20	22	296	4.51	19	5	ND	2	17	1	5	2	61	.18	.094	8	30	.53	130	.03	2	1.37	.01	.07	1	4
STD C/AU-0.5	21	58	40	130	6.9	70	29	1090	3.92	42	21	7	34	47	16	15	21	62	.48	.105	37	57	.89	177	.08	36	1.72	.07	.13	14	480

E & B EXPLORATION PROJECT - 5055 FILE # 86-1917

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au PPB
L30+00E 3+50N	1	22	4	38	.3	8	9	292	2.18	3	5	ND	1	35	1	2	2	63	.27	.059	12	18	.23	93	.08	3	.77	.01	.09	1	2
L30+00E 3+25N	1	74	11	79	.2	19	16	356	4.30	15	5	ND	2	22	1	2	2	71	.30	.147	12	31	.55	194	.03	6	1.28	.01	.09	1	5
L30+00E 2+75N	1	85	12	87	.4	31	17	1075	3.86	17	5	ND	1	38	1	2	2	72	.51	.054	19	54	.82	207	.06	2	1.70	.01	.10	1	3
L30+00E 2+50N	1	50	7	67	.2	20	17	564	2.36	9	5	ND	1	23	1	2	3	53	.29	.042	17	38	.47	156	.07	2	.99	.01	.08	1	8
L30+00E 2+25N	1	20	2	62	.2	13	8	454	2.05	6	5	ND	2	21	1	2	2	39	.31	.047	12	27	.35	227	.06	4	.69	.01	.08	1	2
L30+00E 2+00N	1	17	5	79	.2	14	7	541	1.86	6	5	ND	1	17	1	2	2	38	.29	.042	14	24	.34	230	.06	5	.83	.01	.08	1	1
L30+00E 1+75N	1	7	2	46	.2	10	4	221	1.37	6	5	ND	1	15	1	2	2	31	.23	.045	15	20	.24	127	.07	2	.61	.01	.06	1	1
L30+00E 1+50N	1	7	7	108	.3	12	5	312	1.86	7	5	ND	1	15	1	2	2	35	.21	.101	12	27	.28	108	.05	3	.94	.01	.07	1	1
L30+00E 1+25N	1	20	3	97	.3	17	10	3780	2.13	12	5	ND	1	32	1	2	2	44	.34	.078	10	29	.26	234	.04	2	.83	.01	.07	1	3
L30+00E 1+00N	1	22	9	77	.1	18	9	351	2.62	11	5	ND	2	17	1	2	2	52	.19	.067	13	34	.38	61	.05	3	1.08	.01	.06	1	5
L30+00E 0+50N	1	19	6	69	.2	23	11	594	2.41	28	5	ND	2	39	1	2	2	53	.28	.081	10	34	.29	206	.05	5	1.17	.01	.08	1	2
L30+00E 0+25N	1	28	11	96	.2	27	11	509	2.69	28	5	ND	2	73	1	2	2	63	.25	.133	10	38	.25	318	.03	7	1.19	.01	.09	1	1
L30+00E 0+00N	1	20	8	139	.1	18	10	477	2.65	20	5	ND	1	44	1	2	2	55	.31	.142	9	43	.23	255	.04	6	1.05	.01	.09	1	6
L32+50E 10+00N	1	71	5	82	.3	28	16	390	4.01	47	5	ND	2	16	1	4	3	76	.29	.084	9	50	.76	90	.04	4	1.53	.01	.09	1	7
L32+50E 9+75N	1	38	4	70	.3	16	8	188	2.62	19	5	ND	1	14	1	2	2	69	.20	.061	9	39	.52	91	.02	2	1.84	.01	.07	1	18
L32+50E 9+50N	1	30	5	61	.3	16	11	305	2.72	10	5	ND	1	13	1	2	2	74	.20	.042	8	36	.36	78	.04	2	.94	.01	.06	1	1
L32+50E 9+25N	1	58	8	76	.1	29	13	280	4.00	25	5	ND	2	13	1	3	2	70	.22	.058	9	52	.73	66	.04	3	1.58	.01	.08	1	5
L32+50E 9+00N	1	24	8	71	.4	17	12	729	3.14	13	5	ND	1	19	1	2	2	75	.32	.062	10	42	.47	157	.02	2	1.21	.01	.08	1	1
L32+50E 8+75N	2	56	12	87	.3	36	18	554	5.94	19	5	ND	2	24	1	2	2	88	.28	.076	10	86	1.28	124	.02	2	1.95	.01	.12	1	2
L32+50E 6+75N	1	52	13	90	.2	21	13	296	3.62	13	5	ND	1	16	1	2	2	62	.23	.054	13	39	.61	110	.04	2	1.36	.01	.08	1	6
L32+50E 6+50N	1	92	10	83	.3	27	16	339	4.45	20	5	ND	2	18	1	2	2	74	.25	.083	14	53	.91	125	.03	2	1.96	.01	.09	1	8
L32+50E 6+25N	1	60	4	72	.2	21	12	514	2.65	11	5	ND	1	17	1	2	2	55	.26	.056	14	44	.71	183	.03	2	1.85	.01	.12	1	4
L32+50E 6+00N	1	105	8	70	.1	22	18	566	4.07	17	5	ND	1	18	1	2	2	72	.27	.053	15	39	.76	184	.03	5	1.50	.01	.13	1	8
L32+50E 5+75N	1	47	4	82	.2	18	15	413	3.40	7	5	ND	1	20	1	2	2	64	.23	.069	12	33	.48	131	.04	4	1.07	.01	.09	1	4
L32+50E 5+50N	1	307	13	168	.9	50	42	2149	4.94	18	5	ND	1	42	2	2	3	74	.59	.125	26	56	.84	590	.02	2	2.41	.01	.20	1	8
L32+50E 4+75N	1	23	2	59	.3	13	10	274	2.94	7	5	ND	1	21	1	2	2	64	.27	.051	10	32	.47	118	.05	3	1.02	.01	.08	1	4
L32+50E 4+50N	1	30	10	69	.2	13	14	363	3.45	6	5	ND	1	26	1	2	2	79	.36	.081	11	26	.47	186	.05	4	1.03	.01	.12	1	6
L32+50E 3+75N	1	36	5	77	.3	40	20	1331	3.67	10	5	ND	1	82	1	2	2	92	.58	.083	11	100	.75	883	.11	3	1.20	.02	.14	1	20
L32+50E 3+25N	1	122	4	68	.3	18	18	294	4.71	11	5	ND	1	38	1	2	2	100	.42	.127	9	37	.81	139	.06	5	1.71	.01	.09	1	3
L32+50E 3+00N	1	22	5	52	.2	7	8	802	1.77	4	5	ND	1	35	1	2	3	49	.49	.058	12	23	.28	228	.07	5	.85	.01	.08	1	1
L32+50E 2+75N	1	58	7	67	.1	17	14	296	3.59	10	5	ND	3	25	1	2	2	60	.30	.094	10	29	.53	142	.05	5	1.24	.01	.08	1	5
L32+50E 2+50N	2	78	7	131	.5	24	18	3724	3.39	12	5	ND	1	39	1	3	2	61	.98	.139	10	30	.41	543	.04	6	1.55	.01	.12	1	3
L32+50E 2+25N	1	21	7	82	.3	19	10	248	3.04	11	5	ND	2	16	1	2	2	59	.24	.134	10	35	.41	99	.05	3	1.14	.01	.07	1	4
L32+50E 2+00N	1	36	5	60	.3	20	11	473	2.84	12	5	ND	3	19	1	2	2	53	.29	.065	12	36	.56	79	.07	3	1.16	.01	.07	1	8
L32+50E 1+75N	1	195	13	77	.9	40	24	987	4.34	23	7	ND	2	43	1	2	2	71	1.20	.070	13	58	.78	211	.05	9	2.12	.01	.11	1	7
L32+50E 1+50N	1	17	4	50	.3	12	5	286	2.35	7	5	ND	1	21	1	2	2	56	.35	.040	11	28	.33	91	.06	2	.77	.01	.08	1	1
STD C/AU-0.5	20	58	42	130	6.9	69	29	1090	3.92	41	21	7	34	48	17	15	20	62	.48	.107	36	59	.89	178	.08	36	1.72	.07	.14	12	515



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Ti	R	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	I	PPM	PPB
L32+50E 1+25M	1	27	6	71	.1	13	10	979	2.32	7	5	ND	1	17	1	2	43	.23	.080	12	30	.34	185	.05	7	.98	.01	.11	1	3	
L32+50E 1+00M	1	27	7	85	.2	21	10	266	2.93	11	5	ND	3	17	1	3	2	56	.22	.087	14	32	.44	96	.05	3	1.07	.01	.06	1	2
L32+50E 0+75M	1	21	8	164	.4	14	9	2075	1.72	8	5	ND	1	31	2	2	2	40	.48	.216	9	22	.17	494	.05	6	.75	.01	.13	1	1
L32+50E 0+50M	1	32	11	74	.2	20	11	239	3.02	11	5	ND	2	15	1	3	2	56	.19	.097	14	36	.42	80	.05	3	1.04	.01	.07	1	5
L32+50E 0+25M	1	19	3	102	.2	19	10	480	2.43	8	5	ND	2	20	1	2	2	46	.28	.086	13	33	.40	177	.06	4	1.12	.01	.08	1	1
L32+50E 0+00M	1	20	9	90	.2	21	9	247	2.52	6	5	ND	2	23	1	2	2	48	.35	.122	12	33	.43	97	.06	6	1.06	.01	.09	1	1
L44+00E 0+00S	1	13	11	114	.3	18	8	225	2.67	8	5	ND	3	18	1	2	2	44	.30	.099	14	34	.47	71	.07	2	1.12	.01	.07	1	1
L44+00E 0+25S	1	34	15	211	1.1	27	12	1207	3.21	19	5	ND	2	37	2	2	2	51	.77	.127	13	38	.53	134	.05	4	1.26	.01	.09	1	5
L44+00E 0+50S	1	16	7	91	.3	18	7	559	2.34	9	5	ND	2	20	1	2	2	38	.30	.178	14	28	.37	108	.06	4	.96	.01	.06	1	1
L44+00E 0+75S	1	9	8	76	.2	16	6	266	1.97	7	5	ND	2	13	1	2	2	34	.21	.106	15	27	.36	75	.05	2	.99	.01	.06	1	1
L44+00E 1+00S	1	11	10	101	.3	13	7	351	2.06	6	5	ND	1	14	1	2	2	36	.24	.089	14	27	.36	71	.05	3	.93	.01	.08	1	4
L44+00E 1+25S	1	20	7	79	.3	17	8	244	2.42	10	5	ND	1	16	1	2	2	46	.25	.102	14	31	.41	90	.05	5	1.10	.01	.07	1	2
L44+00E 1+50S	1	14	10	85	.3	15	6	479	2.04	6	5	ND	1	23	1	2	2	39	.44	.120	12	26	.34	85	.05	6	.96	.01	.09	1	1
L44+00E 1+75S	1	23	10	168	.4	21	15	4356	2.46	9	5	ND	1	22	1	2	2	49	.35	.088	11	34	.35	239	.05	6	1.05	.01	.11	1	2
L44+00E 2+00S	1	21	8	71	.2	18	10	506	2.69	9	5	ND	1	22	1	2	2	59	.41	.077	11	33	.36	72	.06	3	.82	.01	.09	1	1
L44+00E 2+25S	1	29	8	100	.1	28	12	261	3.63	12	5	ND	3	18	1	2	2	64	.30	.206	13	45	.63	93	.07	2	1.68	.01	.07	1	1
L44+00E 2+50S	1	35	16	94	.3	32	12	730	2.93	6	5	ND	2	19	1	2	2	55	.38	.063	17	44	.66	83	.07	5	1.70	.01	.08	1	3
L44+00E 2+75S	1	21	5	106	.2	22	11	405	2.69	8	5	ND	2	20	1	2	2	54	.40	.078	12	36	.46	88	.07	5	1.20	.01	.08	1	1
L44+00E 3+00S	1	14	5	79	.2	10	7	451	2.12	4	5	ND	1	15	1	3	2	51	.32	.051	10	27	.32	96	.08	5	.80	.01	.08	1	1
L44+00E 3+25S	1	65	14	117	.6	30	18	1295	3.84	10	5	ND	1	33	1	2	2	75	.63	.103	23	52	.67	129	.07	5	1.93	.01	.09	1	1
L44+00E 3+50S	1	40	14	85	.5	26	12	655	3.03	10	5	ND	1	27	1	2	3	60	.56	.046	16	45	.56	98	.07	7	1.74	.01	.08	1	2
L44+00E 3+75S	1	14	6	68	.2	14	10	468	2.24	7	5	ND	1	17	1	2	2	52	.30	.049	12	31	.39	72	.08	3	1.00	.01	.07	1	1
L44+00E 4+25S	1	60	8	99	.2	45	19	671	4.22	17	5	ND	2	22	1	2	2	77	.40	.098	11	65	.85	139	.07	2	1.89	.01	.08	1	10
L44+00E 4+50S	1	14	11	53	.2	13	5	178	1.80	5	5	ND	1	16	1	2	2	41	.28	.062	13	27	.30	41	.07	3	.78	.01	.06	1	1
L44+00E 4+75S	1	16	2	99	.2	17	9	353	2.27	4	5	ND	2	18	1	3	2	47	.26	.076	12	30	.39	72	.05	6	1.03	.01	.07	1	1
L44+00E 5+00S	1	34	13	76	.2	24	10	227	2.90	15	5	ND	3	19	1	3	3	51	.27	.062	14	36	.53	51	.05	4	1.10	.01	.06	1	6
L45+00E 0+00S	1	17	7	97	.3	18	9	303	1.87	9	5	ND	2	24	1	2	2	32	.38	.056	15	26	.38	105	.06	3	.84	.01	.07	1	11
L45+00E 0+25S	1	31	11	66	.3	28	9	398	2.47	10	5	ND	1	42	1	2	2	40	.84	.088	13	41	.62	85	.05	4	1.26	.01	.08	1	7
L45+00E 0+50S	1	18	8	87	.2	21	8	231	2.59	14	5	ND	1	16	1	2	2	43	.27	.086	14	33	.51	62	.05	4	1.15	.01	.07	1	1
L45+00E 0+75S	1	16	8	93	.4	18	8	308	2.76	10	5	ND	1	13	1	2	2	45	.22	.119	12	34	.43	67	.05	4	1.22	.01	.07	1	1
L45+00E 1+00S	1	13	8	70	.3	17	6	340	1.99	8	5	ND	1	14	1	2	2	36	.23	.060	13	26	.36	66	.04	3	.91	.01	.05	1	2
L45+00E 1+25S	1	5	4	32	.1	3	2	114	.74	2	5	ND	1	12	1	2	2	20	.21	.032	13	13	.13	42	.06	2	1.38	.01	.06	2	1
L45+00E 1+50S	1	38	12	78	.3	24	10	207	3.19	14	5	ND	1	14	1	2	2	59	.20	.079	14	35	.48	53	.03	3	1.08	.01	.06	1	6
L45+00E 1+75S	1	9	5	61	.2	13	6	217	1.55	5	5	ND	1	14	1	2	3	32	.23	.044	12	22	.30	65	.06	4	.78	.02	.07	1	1
L45+00E 2+00S	1	21	8	79	.3	26	9	212	3.20	13	5	ND	2	14	1	2	2	54	.21	.086	15	38	.58	70	.06	2	1.39	.01	.08	1	1
L45+00E 2+25S	1	14	6	87	.5	13	8	505	2.14	11	5	ND	1	18	1	2	2	43	.30	.099	11	30	.27	117	.04	2	1.14	.01	.08	1	155
STD C/AU-0.5	21	58	40	131	6.9	67	29	1100	3.94	41	22	8	35	49	17	16	20	63	.48	.106	38	59	.88	183	.08	36	1.73	.07	.14	12	505

SAMPLE#	Mo PPH	Cu PPH	Pb PPH	Zn PPH	Ag PPH	Ni PPH	Co PPH	Mn PPH	Fe %	As PPH	U PPH	Au PPH	Th PPH	Sr PPH	Cd PPH	Sb PPH	Bi PPH	V PPH	Ca %	P %	La PPH	Cr PPH	Hg %	Ba PPH	Ti %	B PPH	Al %	Na %	K %	M PPH	AuI PPB
L45+00E 2+50S	1	33	3	100	.2	20	14	949	3.31	12	5	ND	1	15	1	2	2	68	.20	.135	12	41	.35	120	.04	5	1.20	.01	.06	1	3
L45+00E 2+75S	1	7	2	49	.3	9	4	179	1.39	4	5	ND	1	14	1	2	2	35	.25	.052	10	19	.21	64	.06	2	.67	.01	.05	2	2
L45+00E 3+00S	1	14	5	97	.2	21	9	323	2.83	9	5	ND	1	15	1	2	2	53	.27	.092	13	35	.46	99	.06	4	1.32	.01	.09	1	4
L45+00E 3+25S	1	12	4	94	.2	12	7	183	2.08	3	5	ND	2	14	1	2	2	47	.25	.055	13	28	.38	59	.08	2	1.03	.01	.07	1	1
L45+00E 3+50S	1	22	5	88	.2	14	10	379	2.20	6	5	ND	1	20	1	2	2	47	.41	.063	16	28	.36	73	.07	6	1.06	.01	.07	1	1
L45+00E 3+75S	1	133	7	135	1.2	55	24	1584	5.25	13	5	ND	2	45	1	2	2	95	1.11	.097	34	80	.91	177	.07	7	3.13	.02	.15	1	3
L45+00E 4+00S	1	38	7	99	.4	33	15	498	3.73	9	5	ND	3	28	1	2	2	69	.54	.041	12	49	.72	102	.08	7	1.88	.02	.07	1	1
L45+00E 4+25S	1	24	8	125	.2	26	13	338	3.73	10	5	ND	3	18	1	2	2	66	.32	.177	11	48	.56	69	.08	2	1.52	.01	.06	1	1
L45+00E 4+50S	1	13	2	100	.2	15	9	401	2.34	6	5	ND	1	18	1	2	2	49	.34	.098	10	35	.42	81	.08	3	1.12	.01	.07	1	46
L45+00E 4+75S	1	12	2	93	.2	15	8	244	1.92	3	5	ND	1	16	1	2	2	43	.31	.066	9	36	.32	95	.06	2	.91	.01	.09	1	1
L45+00E 5+00S	1	22	7	100	.4	20	10	741	2.59	9	5	ND	1	23	1	2	3	56	.36	.039	8	38	.43	119	.06	4	1.09	.01	.07	1	10
L46+00E 0+00S	1	19	4	88	.1	24	9	277	2.68	12	5	ND	3	15	1	2	2	41	.22	.060	15	35	.57	63	.06	3	1.21	.01	.06	1	8
L46+00E 0+25S	1	28	9	74	.1	25	10	243	3.07	15	5	ND	4	18	1	2	2	52	.32	.093	14	38	.61	47	.06	4	1.24	.01	.06	1	6
L46+00E 0+50S	1	22	7	79	.2	24	10	399	2.55	9	5	ND	2	21	1	2	2	40	.35	.031	17	38	.54	71	.05	4	1.24	.01	.07	1	2
L46+00E 1+25S	1	30	11	87	.3	20	12	727	2.03	8	5	ND	1	25	1	2	2	39	.42	.028	15	31	.33	80	.05	3	1.05	.01	.10	1	1
L46+00E 1+50S	1	28	5	126	.5	27	10	242	3.36	13	5	ND	1	20	1	2	2	53	.32	.122	14	39	.58	67	.05	4	1.44	.01	.07	1	11
L46+00E 1+75S	1	33	6	74	.2	22	11	443	2.97	12	5	ND	3	15	1	3	3	54	.20	.061	16	33	.40	75	.06	4	.84	.01	.08	1	38
L46+00E 2+00S	1	14	8	97	.3	19	7	912	2.19	6	5	ND	1	18	1	2	3	37	.30	.088	15	29	.48	86	.06	6	1.11	.01	.07	1	1
L46+00E 2+25S	1	88	6	84	.2	39	20	335	4.93	17	5	ND	2	16	1	2	2	90	.23	.100	11	50	.47	35	.02	5	1.39	.01	.08	1	6
L46+00E 2+50S	1	21	12	76	.2	24	8	236	2.86	11	5	ND	2	18	1	2	2	46	.32	.123	15	32	.51	82	.05	3	1.20	.01	.08	1	3
L46+00E 2+75S	1	11	4	97	.1	14	7	228	2.17	6	5	ND	3	18	1	2	2	39	.26	.112	13	27	.32	113	.06	4	1.01	.01	.08	1	2
L46+00E 3+00S	1	16	11	81	.2	17	9	529	2.23	8	5	ND	2	20	1	2	2	42	.31	.075	13	27	.35	75	.07	4	1.07	.01	.09	1	1
L46+00E 3+50S	1	30	11	60	.6	24	11	514	2.79	7	5	ND	3	37	1	2	2	44	.50	.022	14	54	.50	138	.07	6	1.66	.01	.07	1	1
L46+00E 3+75S	1	33	11	96	.5	23	11	597	2.60	10	5	ND	2	44	1	2	2	45	.68	.042	13	36	.60	101	.07	8	1.32	.01	.07	1	2
L46+00E 4+00S	1	16	7	89	.1	20	10	241	2.83	9	5	ND	3	14	1	2	2	55	.21	.045	17	33	.51	48	.08	4	1.15	.01	.05	1	5
L46+00E 4+25S	1	32	6	101	.1	19	14	459	3.54	7	5	ND	3	15	1	2	2	72	.26	.118	12	40	.48	75	.06	6	1.22	.01	.07	1	1
L46+00E 4+50S	1	43	5	123	.1	31	15	376	3.95	10	5	ND	2	22	1	2	2	80	.45	.135	10	47	.80	82	.09	6	1.69	.01	.09	1	2
L46+00E 4+75S	1	15	5	86	.1	16	9	291	2.35	7	5	ND	2	17	1	2	2	48	.26	.066	12	36	.44	73	.07	5	1.04	.01	.05	1	1
L46+00E 5+00S	1	23	9	92	.2	21	10	268	3.07	7	5	ND	3	20	1	2	2	61	.31	.103	11	39	.53	79	.08	2	1.35	.01	.07	1	1
L47+00E 0+00S	1	13	5	79	.1	17	7	207	1.92	10	5	ND	2	16	1	2	2	35	.28	.034	15	28	.43	59	.06	3	1.00	.01	.06	1	8
L47+00E 0+25S	1	40	9	85	.3	34	14	569	3.26	14	5	ND	3	30	1	2	2	51	.50	.038	17	44	.65	99	.06	4	1.61	.01	.12	1	1
L47+00E 0+50S	1	73	13	88	.7	57	18	3363	4.37	23	5	ND	2	63	1	2	2	59	1.01	.083	20	60	.78	291	.06	6	2.29	.01	.12	1	11
L47+00E 0+75S	1	40	11	108	.2	38	14	745	3.48	20	5	ND	4	28	1	2	2	53	.43	.042	16	48	.69	113	.07	5	1.70	.01	.11	1	7
L47+00E 1+00S	1	18	6	96	.3	29	11	311	2.70	10	5	ND	3	24	1	2	2	42	.38	.039	13	39	.57	79	.06	4	1.38	.01	.07	1	2
L47+00E 1+25S	1	18	12	83	.2	19	8	279	2.36	11	5	ND	1	25	1	2	2	42	.43	.055	13	31	.51	54	.05	4	1.18	.01	.07	1	8
L47+00E 1+50S	1	18	8	73	.1	17	8	281	2.06	8	5	ND	1	20	1	2	2	38	.32	.039	13	29	.37	64	.06	2	.97	.01	.07	1	21
STD C/AU-0.5	20	58	40	129	6.8	68	29	1085	3.92	40	21	8	34	48	17	16	21	62	.48	.107	37	58	.89	179	.08	39	1.73	.07	.13	14	500

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

PAGE 16

SAMPLED	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	AuI PPB
L47+00E 1+7SS	1	60	10	75	.7	47	15	559	3.92	12	5	ND	3	29	1	2	2	58	.44	.030	21	61	.62	141	.05	3	2.30	.01	.09	1	3
L47+00E 2+00S	1	23	12	62	.1	23	9	375	2.69	12	5	ND	3	17	1	2	2	43	.29	.043	17	36	.64	49	.07	2	1.25	.01	.07	1	6
L47+00E 2+2SS	1	48	13	91	.5	30	17	1132	3.40	14	5	ND	1	32	1	2	2	59	.54	.055	16	46	.62	107	.04	2	1.84	.01	.10	1	1
L47+00E 2+50S	1	17	7	68	.1	21	9	208	2.66	10	5	ND	3	18	1	2	2	46	.25	.027	14	34	.53	43	.06	2	1.22	.01	.05	1	9
L47+00E 2+7SS	1	17	7	70	.2	16	9	636	2.22	9	5	ND	2	30	1	2	2	39	.33	.043	12	28	.34	86	.05	6	1.11	.01	.07	1	1
L47+00E 3+00S	1	36	18	81	.3	28	15	587	3.81	18	5	ND	3	50	1	2	2	52	.75	.031	13	41	.68	100	.06	6	1.52	.01	.08	1	7
L47+00E 3+2SS	1	23	6	64	.3	25	13	712	2.91	11	5	ND	3	29	1	2	2	48	.35	.020	14	39	.59	82	.06	6	1.32	.01	.06	1	42
L47+00E 3+50S	1	19	9	94	.3	22	11	1067	2.51	8	5	ND	1	31	1	2	2	43	.44	.036	15	35	.59	97	.05	2	1.38	.01	.07	1	1
L47+00E 3+7SS	1	10	6	88	.2	11	6	194	1.94	6	5	ND	2	13	1	2	2	37	.16	.104	15	24	.30	79	.05	2	1.03	.01	.05	1	1
L47+00E 4+00S	1	11	3	66	.2	13	5	163	2.01	8	5	ND	2	13	1	2	3	40	.20	.061	15	25	.38	59	.06	2	.96	.01	.05	1	5
L47+00E 4+2SS	1	24	7	72	.1	23	10	267	2.83	8	5	ND	2	18	1	2	2	47	.32	.104	15	34	.59	73	.05	5	1.29	.01	.07	1	5
L47+00E 4+50S	1	16	9	86	.2	18	9	253	2.61	4	5	ND	3	14	1	2	2	47	.28	.080	14	32	.44	69	.06	5	1.34	.01	.06	1	3
L47+00E 4+7SS	1	15	9	98	.1	13	8	1094	2.03	4	5	ND	1	17	1	2	2	45	.34	.065	12	28	.34	105	.07	4	.98	.01	.06	1	1
L47+00E 5+00S	1	15	6	72	.1	15	6	193	2.17	5	5	ND	2	15	1	2	2	46	.27	.062	13	26	.38	62	.07	2	1.06	.01	.06	1	3
STD C/AU 0.5	20	58	37	128	6.8	66	28	1076	3.93	39	22	8	34	48	17	15	19	61	.48	.104	38	58	.89	177	.08	36	1.72	.06	.13	12	495

## E &amp; B EXPLORATION PROJECT - 5055 FILE # 86-1917

PAGE 17

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Tl	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Ant	Aut
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB	DTAT
KR-86-090	2	136	661	89	2.3	5	7	803	1.12	114	5	ND	1	74	1	30	7	8	5.95	.013	2	4	.15	26	.01	2	.04	.01	.02	1	25	-
KR-86-091	12	57	107	89	.9	27	20	783	3.35	81	5	ND	2	56	1	6	2	40	5.70	.090	10	21	.35	106	.01	5	.65	.02	.21	1	34	-
KR-86-092	1	67	10	53	.2	21	27	1377	5.78	52	5	ND	3	89	1	2	2	124	7.78	.092	12	37	1.88	59	.01	4	2.13	.02	.15	1	7	-
KR-86-093	2	55	37	27	1.8	9	9	882	3.30	557	5	ND	3	141	1	12	2	13	10.18	.033	5	3	.74	32	.01	2	.16	.01	.08	1	1920	.053
KR-86-094	2	8	2	17	.2	5	4	824	1.51	321	5	ND	2	126	1	2	3	6	7.04	.008	3	3	.47	27	.01	3	.07	.01	.04	1	500	-
KR-86-095	2	74	5	681	.8	22	10	751	2.58	79	5	ND	2	237	1	2	2	19	8.01	.025	3	19	2.29	14	.01	2	.22	.01	.09	1	90	-
KR-86-096	1	82	7	54	.3	42	22	1322	4.42	262	5	ND	3	202	1	5	2	65	9.70	.095	5	71	2.63	28	.01	4	1.26	.01	.12	1	24	-
STD C/AU-0.5	20	57	41	130	6.8	67	29	1083	3.92	40	22	7	33	47	16	15	18	61	.48	.104	37	58	.89	175	.08	41	1.72	.06	.13	12	505	-

E & B EXPLORATIONS INC.

CARIBOO PROJECT  
I.P. PSEUDOSECTION

TO ACCOMPANY REPORT BY E.R. ROCKEL

IR INTERPRETEX PROJECT 86616 DATE OCT/86  
RESOURCES LTD. NTS DRAWN BY

INDUCED POLARIZATION AND RESISTIVITY SURVEY

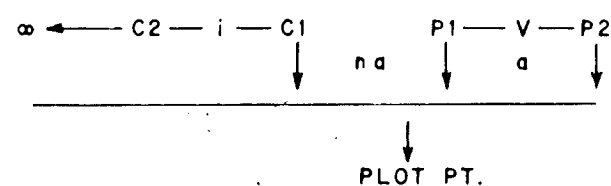
POLE - DIPOLE ARRAY PSEUDOSECTION

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

LEGEND

- PSEUDOSECTION CONTOURS (Intervals as Indicated)
- Ma GREATER THAN 40 ms.
- Ma 30.1 ms. TO 40 ms.
- Ma 20 ms. TO 30 ms.

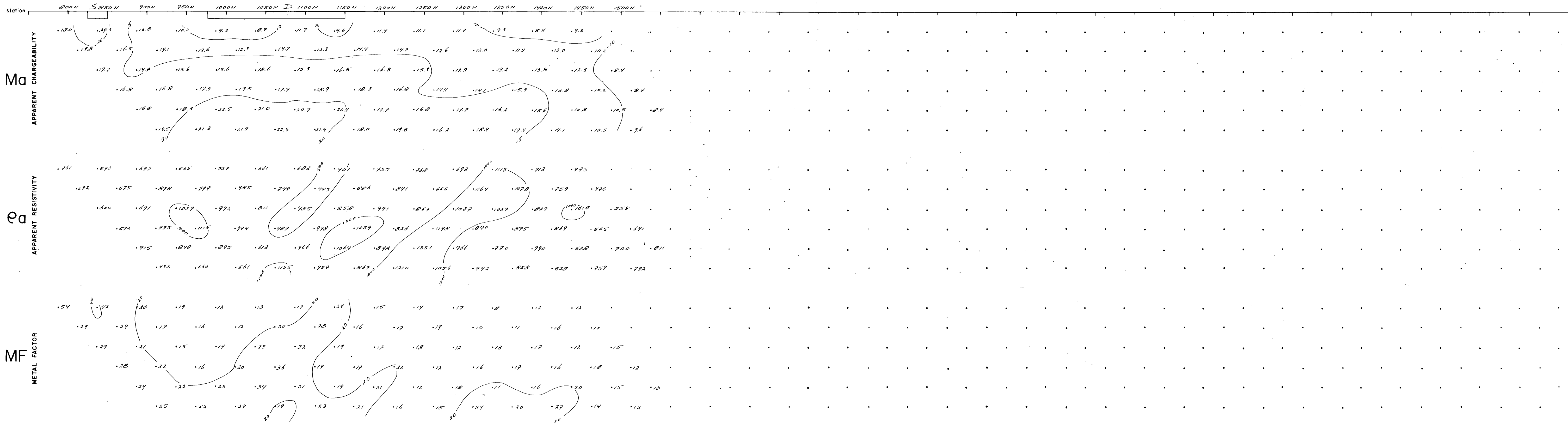
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# 16,018

LINE NO. \_\_\_\_\_

LINE NO. 46 E



E & B EXPLORATIONS INC.

CARIBOO PROJECT  
I.P. PSEUDOSECTION

TO ACCOMPANY REPORT BY E.R. ROCKEL

IR INTERPRETEX  
RESOURCES LTD. SCALE 1:2500 DATE OCT./86  
PROJECT 86616 FIGURE NO. NTS DRAWN BY

INDUCED POLARIZATION AND RESISTIVITY SURVEY

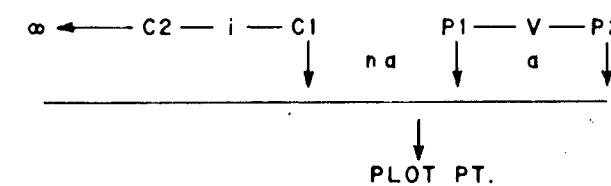
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GEOLOGICAL BRANCH  
ASSESSMENT REPORT

LEGEND

- PSEUDOSECTION CONTOURS (Intervals as Indicated)
- Ma GREATER THAN 40 ms.
- Ma 30.1 ms. TO 40 ms.
- Ma 20 ms. TO 30 ms.

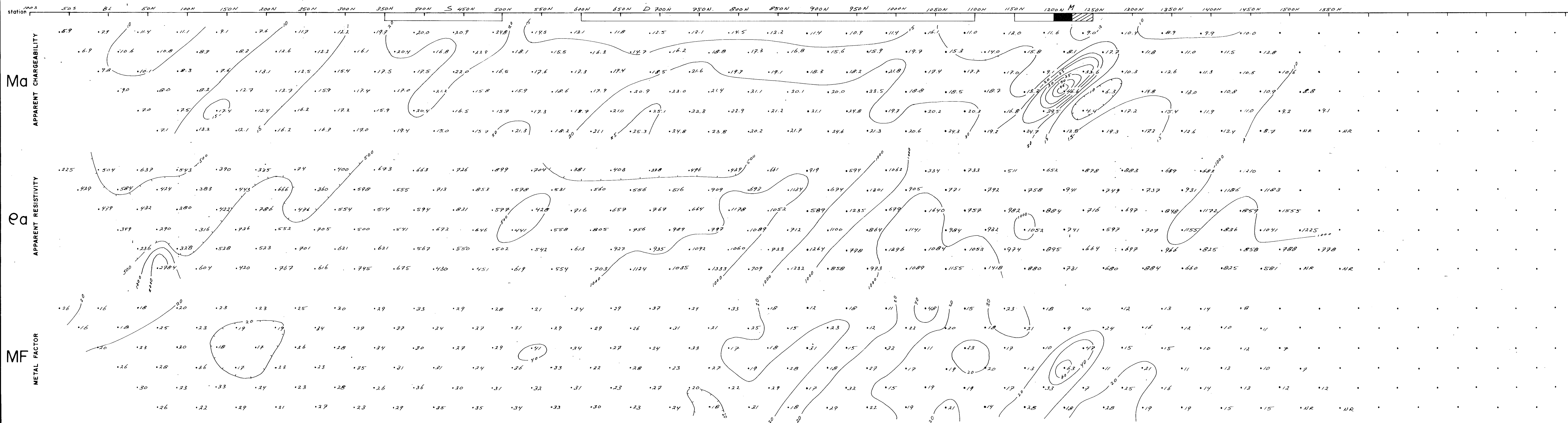
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LINE NO. \_\_\_\_\_

# 16,018

LINE NO. 48 E



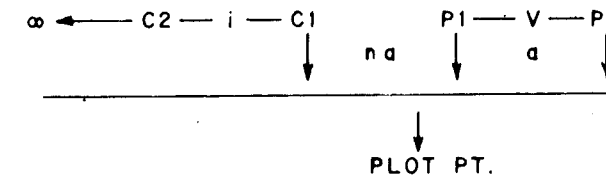
E & B EXPLORATIONS INC.  
 CARIBOO PROJECT  
 I.P. PSEUDOSECTION  
 TO ACCOMPANY REPORT BY E.R. ROCKEL  
 IR INTERPRETEX RESOURCES LTD  
 SCALE 1:2500  
 PROJECT 86616  
 DATE OCT. 7 86  
 FIGURE NO.  
 DRAWN BY

INDUCED POLARIZATION AND RESISTIVITY SURVEY

POLE-DIPOLE ARRAY PSEUDOSECTION

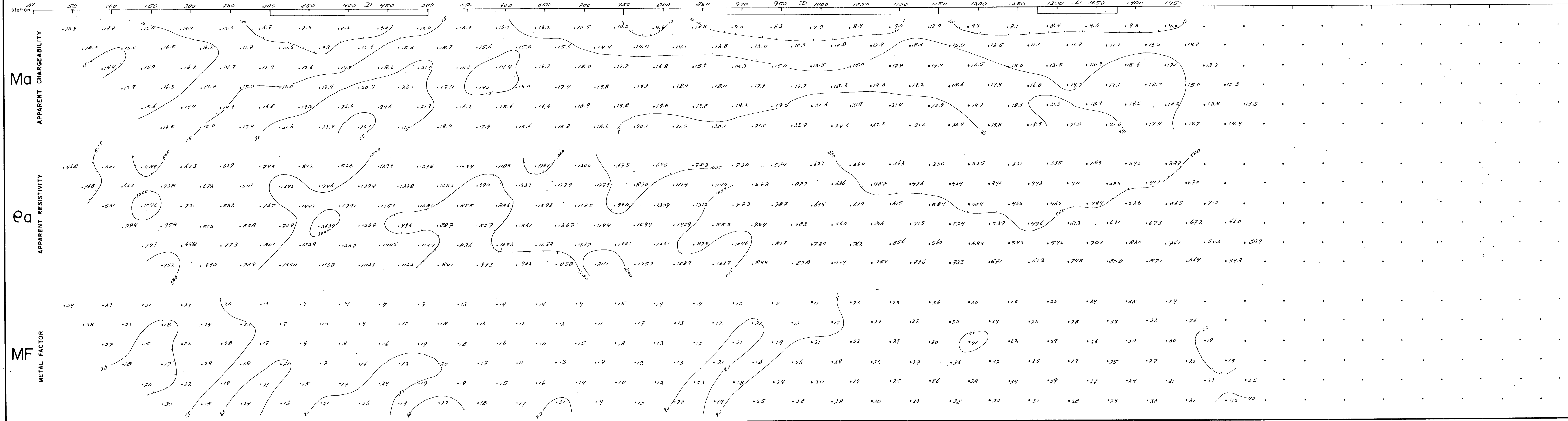
GEOLOGICAL BRANCH ASSESSMENT REPORT

**LEGEND**  
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 Ma GREATER THAN 40 ms.  
 Ma 30.1 ms. TO 40 ms.  
 Ma 20 ms. TO 30 ms.



LINE NO. 16,018

LINE NO. 52 E



E & B EXPLORATIONS INC.

CARIBOO PROJECT  
I.P. PSEUDOSECTION

TO ACCOMPANY REPORT BY E.R. ROCKEL

IR INTERPRETEX  
RESOURCES LTD

SCALE 1:2500  
PROJECT B6616  
FIGURE NO. NTS

DATE OCT/86  
DRAWN BY

INDUCED POLARIZATION AND RESISTIVITY SURVEY

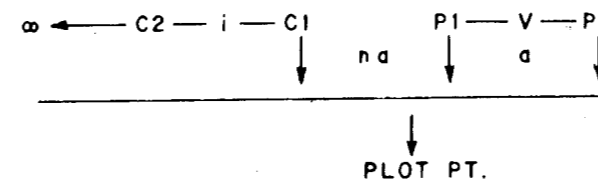
POLE - DIPOLE ARRAY PSEUDOSECTION

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

LEGEND

- PSEUDOSECTION CONTOURS (intervals as indicated)
- Ma GREATER THAN 40 ms.
- Ma 30.1 ms. TO 40 ms.
- Ma 20 ms. TO 30 ms.

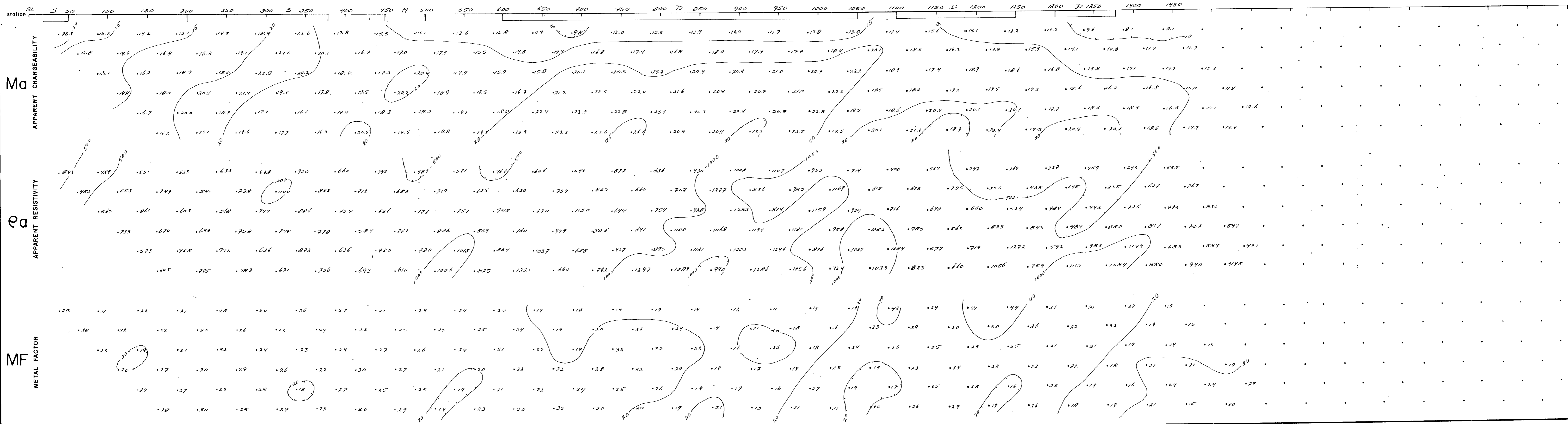
SCALE 1:2500



LINE NO. \_\_\_\_\_

# 16,018

LINE NO. 50E





E & B EXPLORATIONS INC.

CARIBOO PROJECT  
I.P. PSEUDOSECTION

TO ACCOMPANY REPORT BY E.R. ROCKEL

IR INTERPRETEX  
RESOURCES LTD

SCALE 1:2500  
PROJECT 86616  
NTS

DATE OCT. 7 86  
FIGURE NO.  
DRAWN BY

INDUCED POLARIZATION AND RESISTIVITY SURVEY

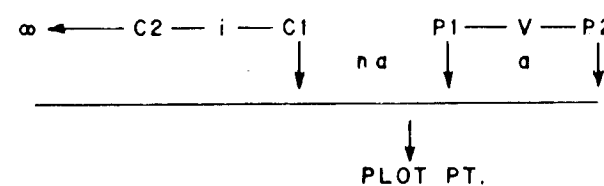
POLE-DIPOLE ARRAY PSEUDOSECTION

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

LEGEND

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- Ma GREATER THAN 40 mS.
- Ma 30.1 mS. TO 40 mS.
- Ma 20 mS. TO 30 mS.

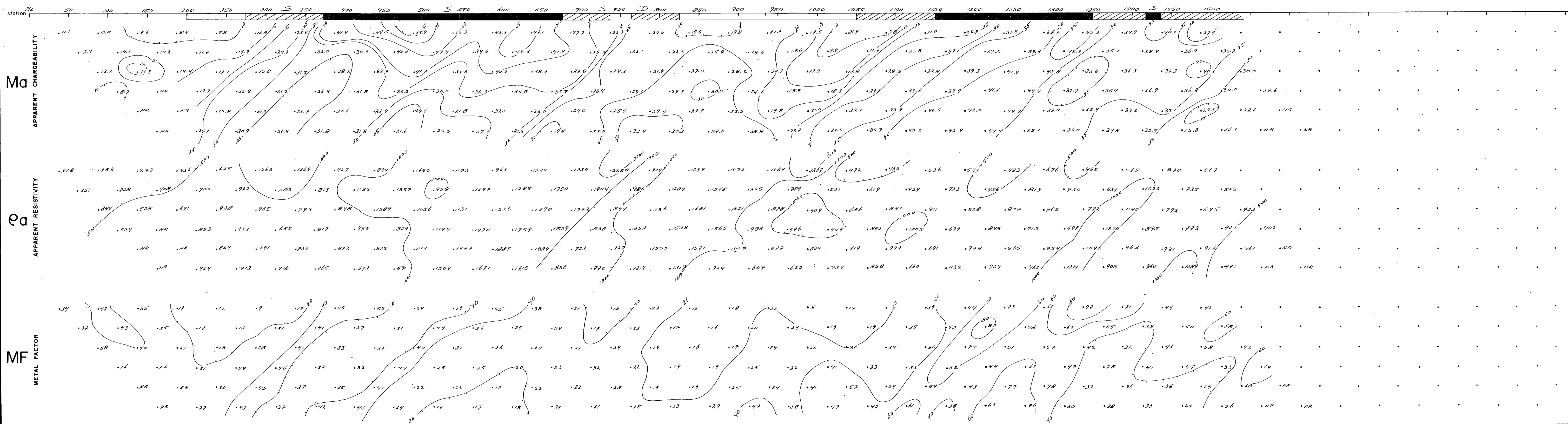
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LINE NO. \_\_\_\_\_

# 16,018

LINE NO. 56 E



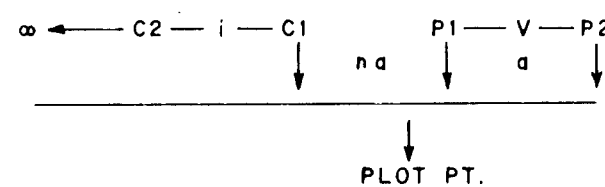
E & B EXPLORATIONS INC.  
 CARIBOO PROJECT  
 I.P. PSEUDOSECTION  
 TO ACCOMPANY REPORT BY E.R. RÖCKEL  
 IR INTERPRETEX RESOURCES LTD. SCALE 1:2500 DATE OCT. 86 PROJECT 86616 FIGURE NO. NTS DRAWN BY

INDUCED POLARIZATION AND RESISTIVITY SURVEY

POLE - DIPOLE ARRAY PSEUDOSECTION

GEOLOGICAL BRANCH ASSESSMENT REPORT

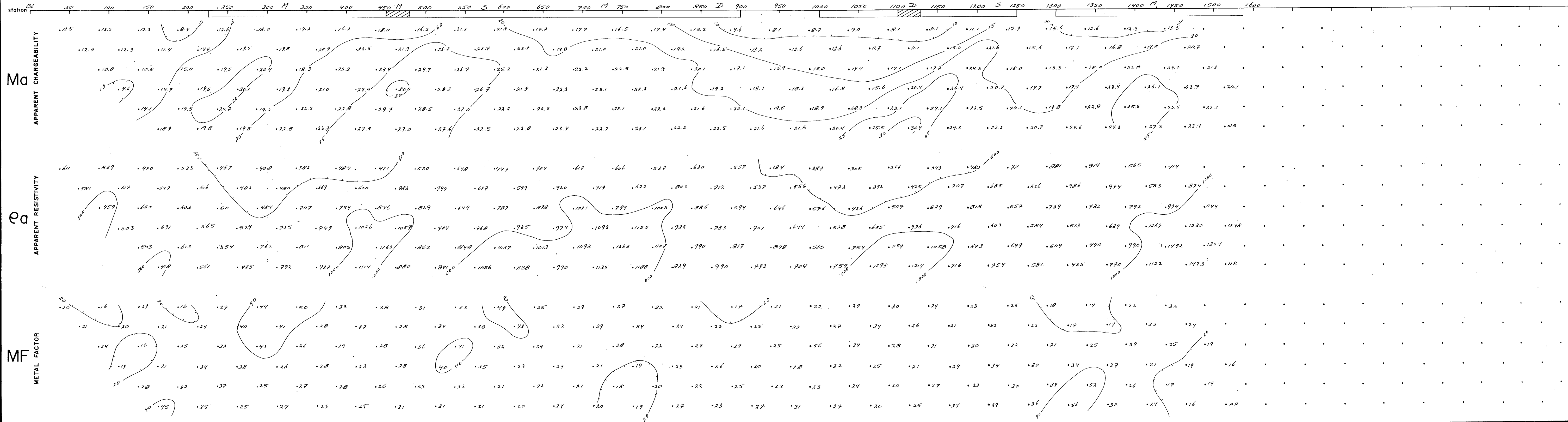
**LEGEND**  
 PSEUDOSECTION CONTOURS (Intervals as Indicated)  
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 Ma 30.1 ms. TO 40 ms.  
 Ma 20 ms. TO 30 ms.



16,018

LINE NO. \_\_\_\_\_

LINE NO. 54E



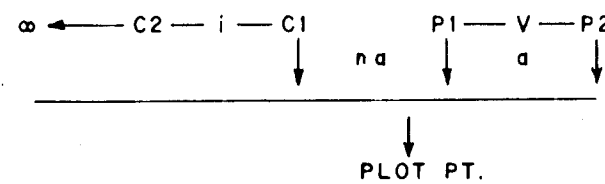
E & B EXPLORATIONS INC.  
 CARIBOO PROJECT  
 I.P. PSEUDOSECTION  
 TO ACCOMPANY REPORT BY E.R. ROCKEL  
 IR INTERPRETEX RESOURCES LTD. SCALE 1:2500 DATE OCT./86 PROJECT 86616 FIGURE NO. NTS DRAWN BY

INDUCED POLARIZATION AND RESISTIVITY SURVEY

POLE-DIPOLE ARRAY PSEUDOSECTION

GEOLOGICAL BRANCH ASSESSMENT REPORT

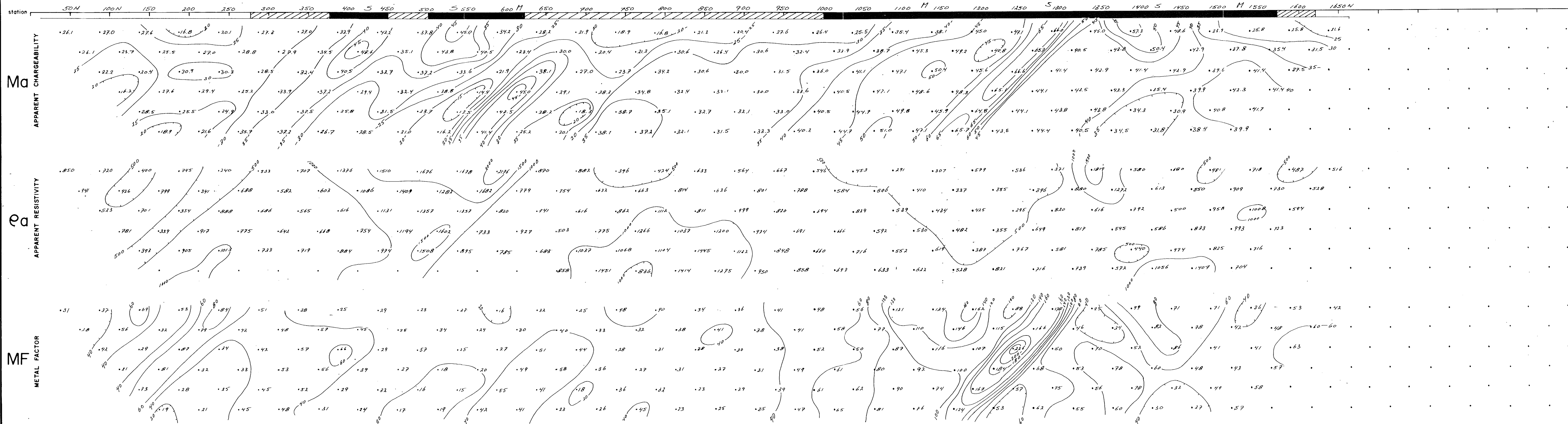
**LEGEND**  
 PSEUDOSECTION CONTOURS (Intervals as Indicated)  
 Ma GREATER THAN 40 ms.  
 Ma 30.1 ms. TO 40 ms.  
 Ma 20 ms. TO 30 ms.



16,018

LINE NO. \_\_\_\_\_

LINE NO. 60E



E & B EXPLORATIONS INC.

CARIBOO PROJECT  
I.P. PSEUDOSECTION

TO ACCOMPANY REPORT BY E.R. ROCKEL

IR INTERPRETEX  
RESOURCES LTD

SCALE 1:2500  
PROJECT 66616  
DATE OCT. / 86  
FIGURE NO.  
DRAWN BY

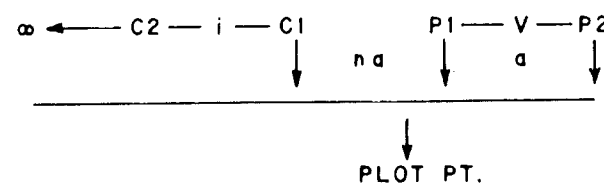
INDUCED POLARIZATION AND RESISTIVITY SURVEY

LEGEND

- PSEUDOSECTION CONTOURS (Intervals as indicated)
- Ma GREATER THAN 40 mS.
- Ma 30.1 mS. TO 40 mS.
- Ma 20 mS. TO 30 mS.

SCALE: 1:2500

POLE-DIPOLE ARRAY PSEUDOSECTION

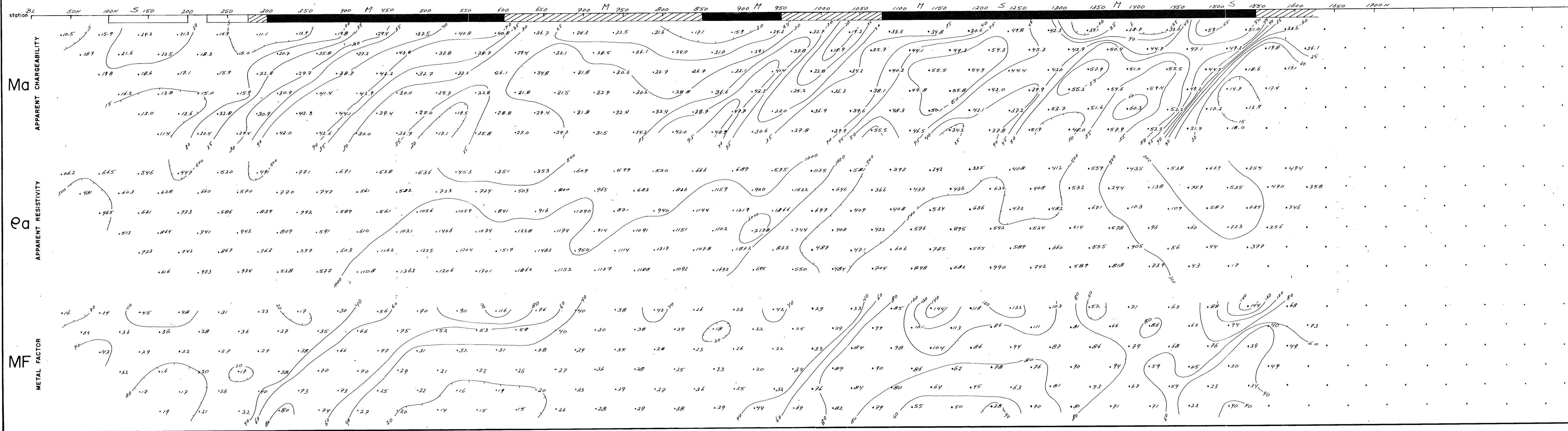


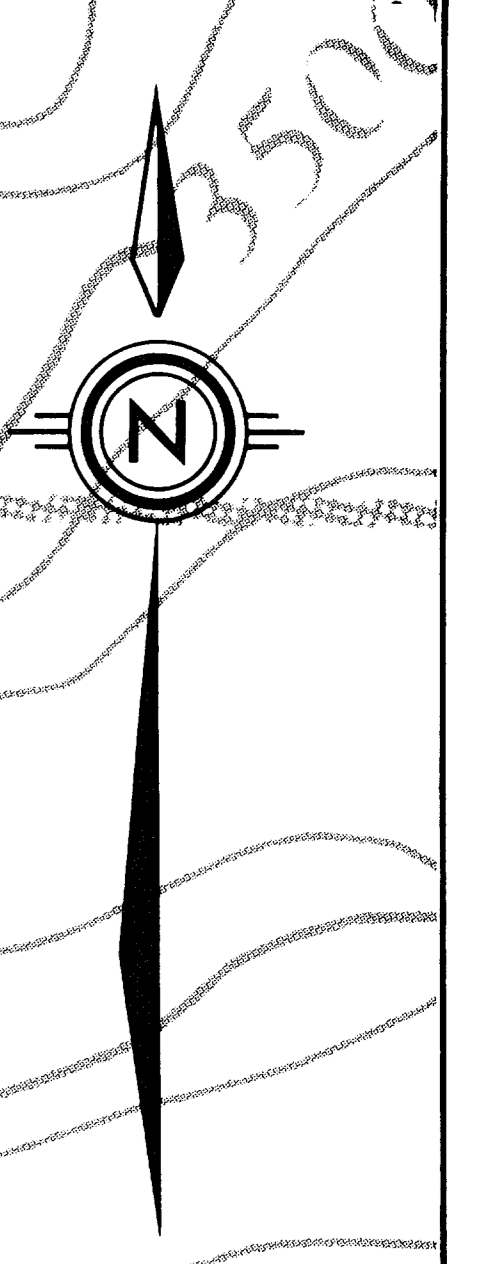
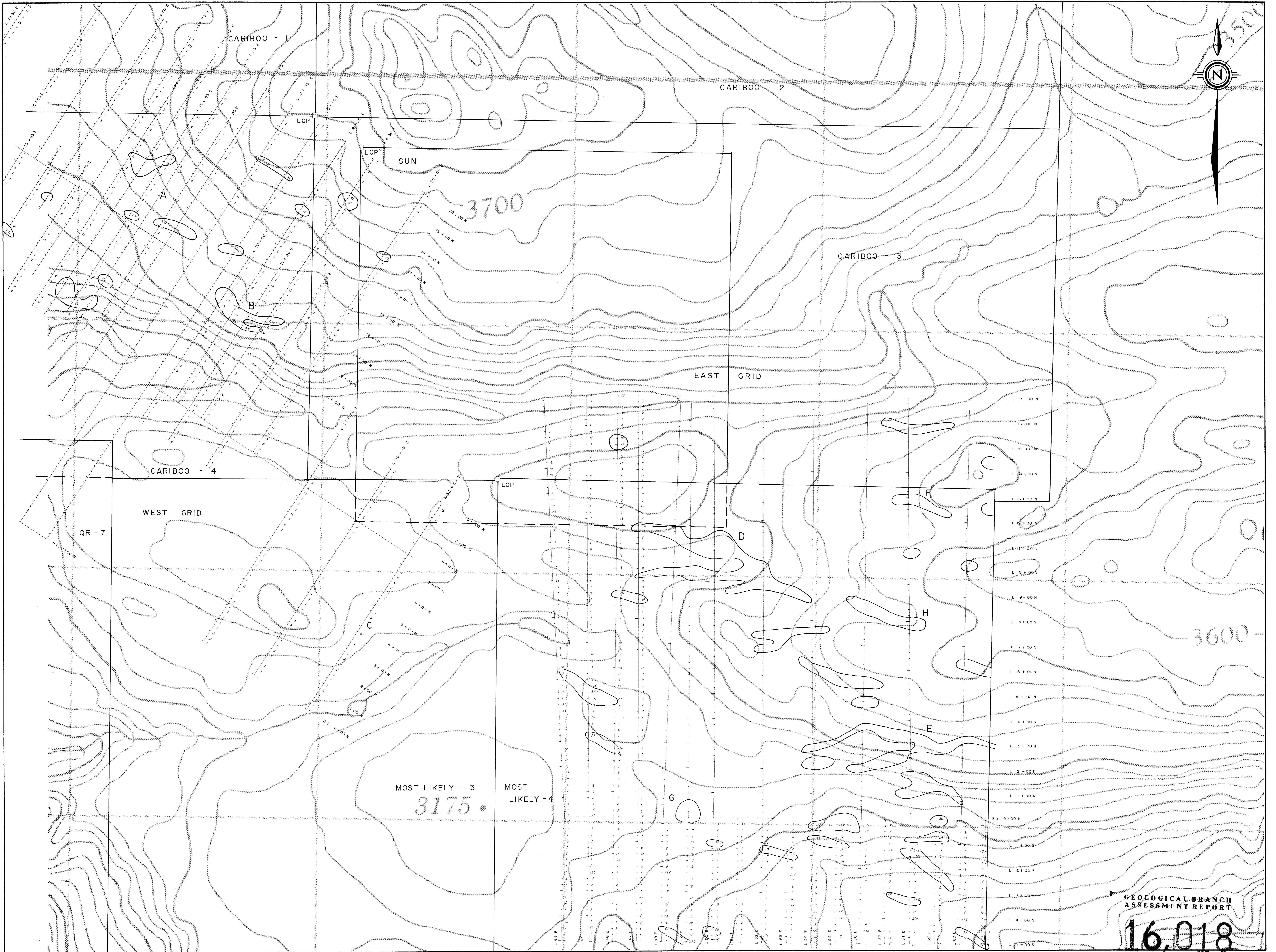
GEOLOGICAL BRANCH  
ASSESSMENT REPORT

# 16,018

LINE NO. \_\_\_\_\_

LINE NO. 58 E



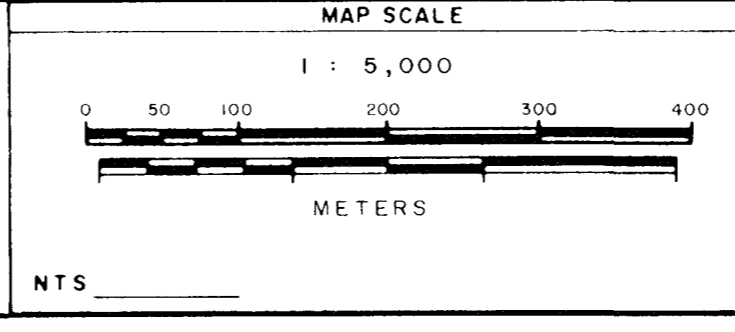


GEOLOGICAL BRANCH  
ASSESSMENT REPORT

**16,018**

**LEGEND**

○	SAMPLE LOCATION, GOLD ASSAY PPB
—	> 20 ppb Au

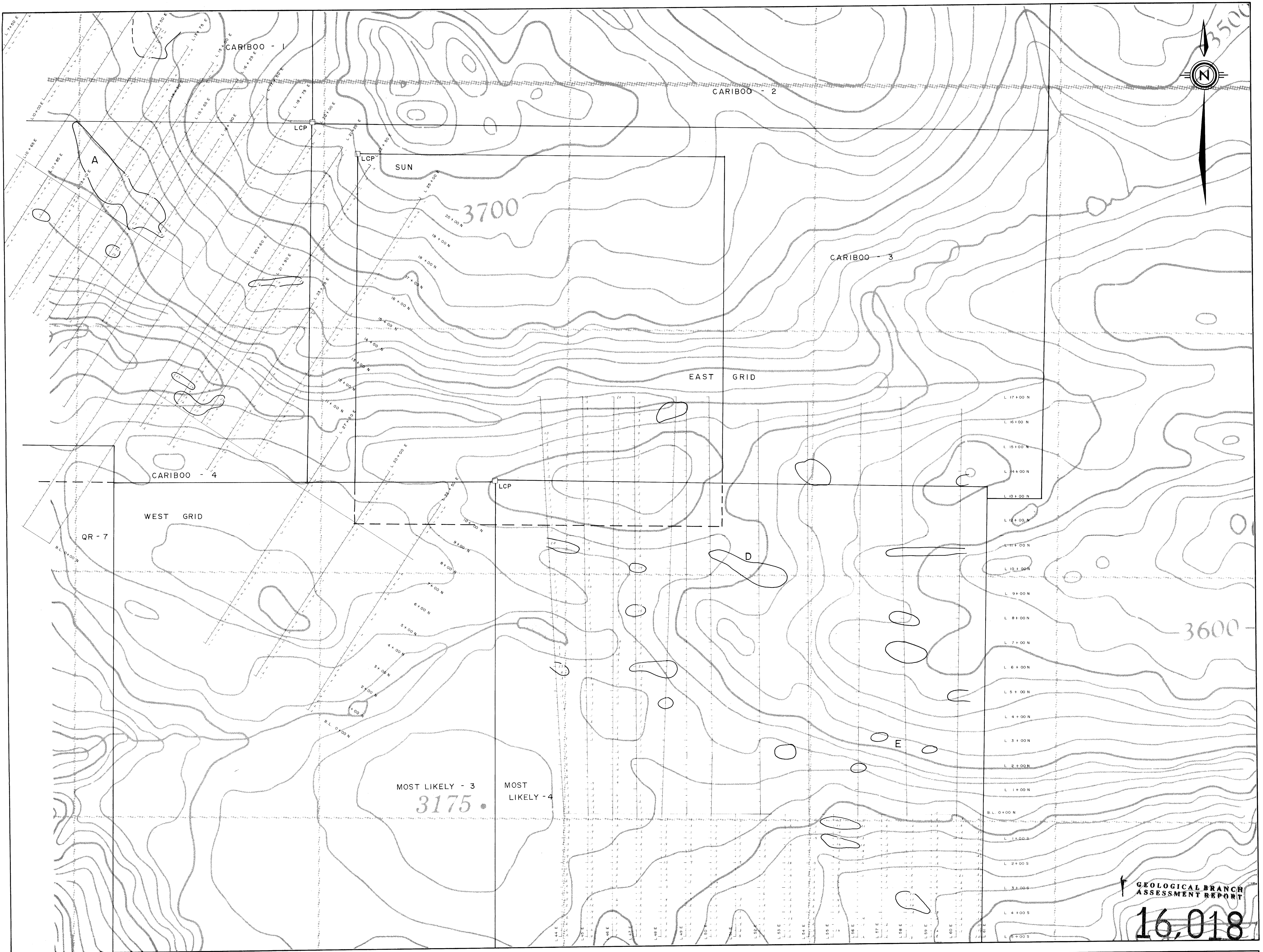


NO	DATE	DRW	MADE BY	DESCRIPTION
1				
2				
3				
4				

DATE	DRAWN BY	CHECKED	APPROVED	OFFICE	DEPARTMENT
	T.W. SHERIDAN DRAFTING				

CARIBOO BELL PROJECT			
SOIL GEOCHEMISTRY			
GOLD			
MAP INDEX NUMBER	SCALE	DRAWING NUMBER	
	1 : 5,000	2	

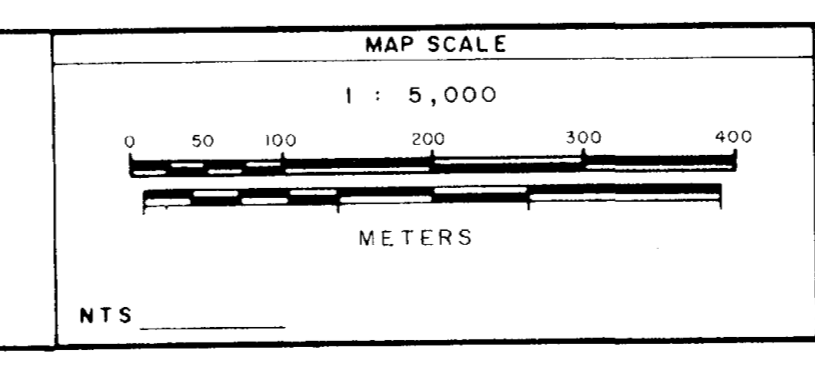
MARCH 2005



**LEGEND**

SAMPLE LOCATION, SILVER ASSAY PPM

> 1.0 ppm Ag



NO.	DATE	BY	DESCRIPTION
1			
2			
3			
4			
5			

DATE	DRAWN BY	CHECKED	APPROVED	OFFICE	DEPARTMENT
	F. W. SHERIDAN				

**CARIBOO BELL PROJECT**

SOIL GEOCHEMISTRY

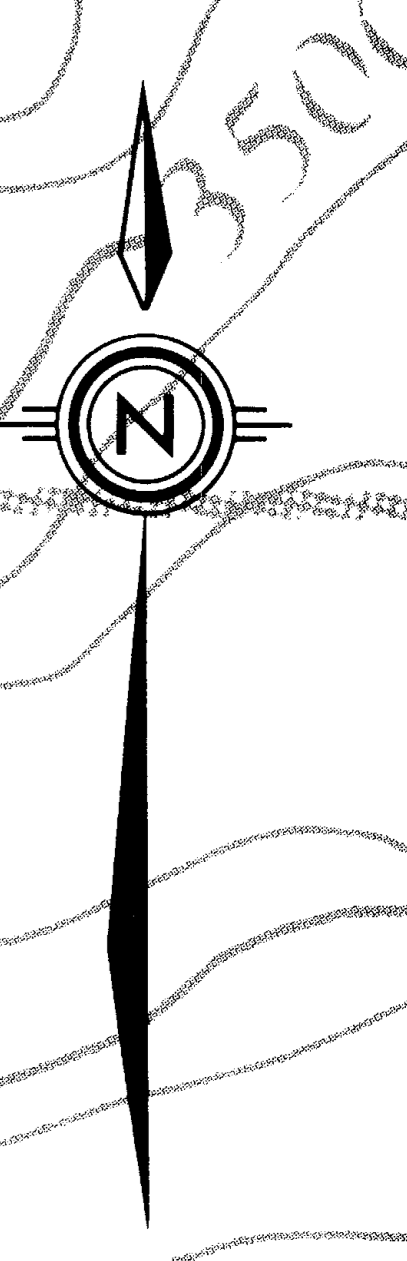
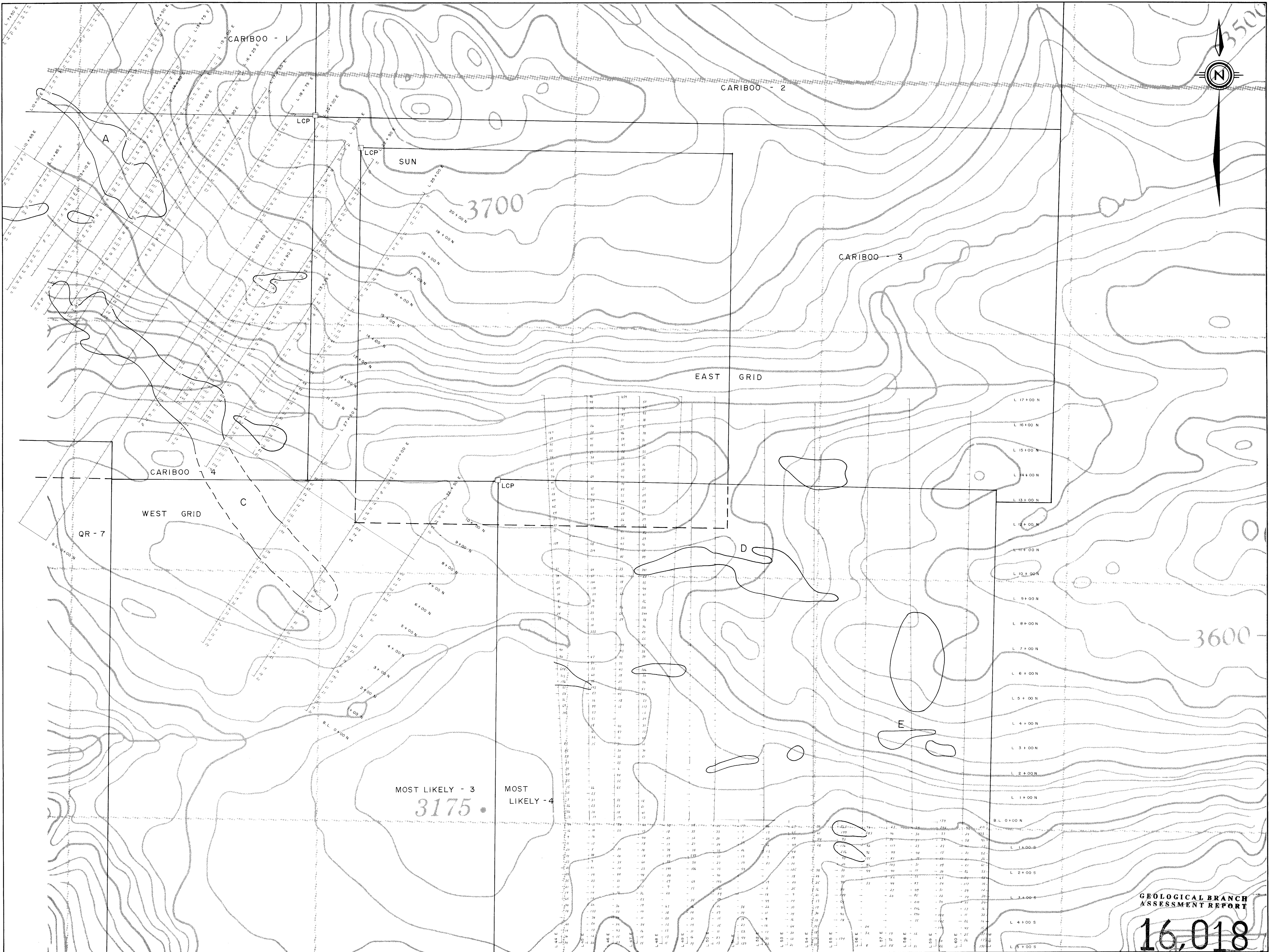
SILVER

MAP INDEX NUMBER: SCALE: 1 : 5,000 DRAWING NUMBER: 3

**GEOLOGICAL BRANCH**

ASSESSMENT REPORT

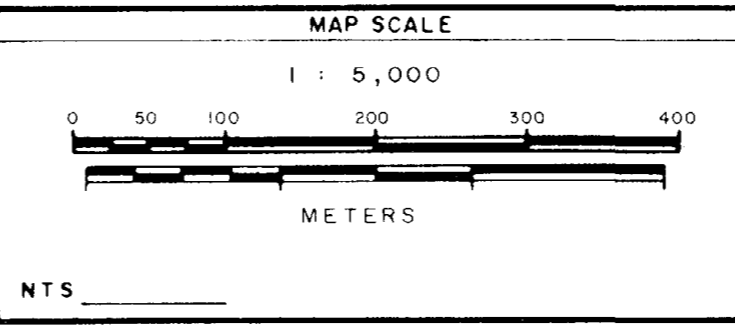
**16,018**



GEOLOGICAL BRANCH  
ASSESSMENT REPORT

16,018

LEGEND	
	SAMPLE LOCATION, COPPER ASSAY PPM
	> 130 ppm Cu



NO	DATE	MADE BY	DESCRIPTION
1			
2			
3			
4			

DATE	DRAWN BY	CHECKED	APPROVED	OFFICE	DEPARTMENT

CARIBOO BELL PROJECT			
SOIL GEOCHEMISTRY			
COPPER			
MAP INDEX NUMBER	SCALE	DRAWING NUMBER	
	1 : 5,000	4	

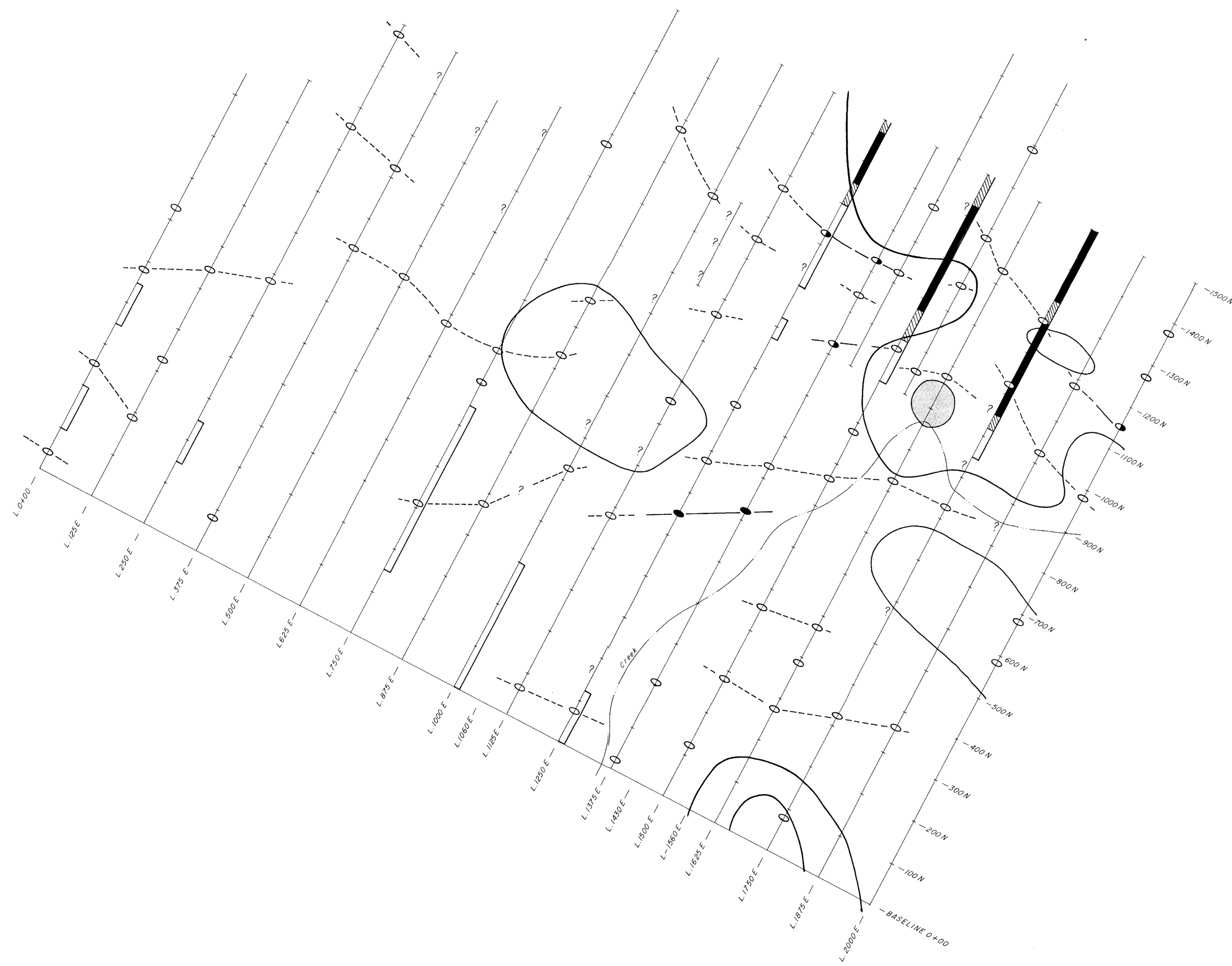
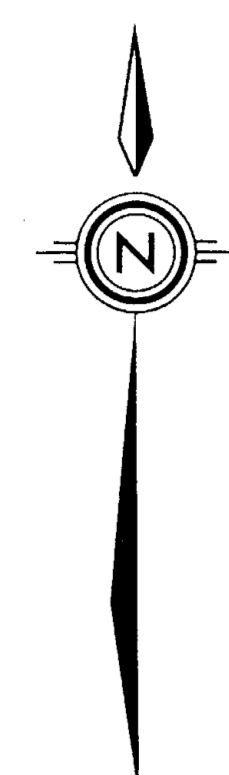


GEOLOGICAL BRANCH  
ASSESSMENT REPORT

**16,018**

<p> <input type="checkbox"/> SILT SAMPLE (ppb Au, ppm Ag)  <input type="checkbox"/> ROCK SAMPLE (500) ppb Au  <input type="checkbox"/> OLD SAMPLE LOCATION  <input type="checkbox"/> SOIL SAMPLE (ppb Au, ppm Ag)         </p>	<p>MAP SCALE</p> <p>NTS: 93A/11</p>	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>REV</th> <th>DATE</th> <th>BY</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td>1</td> <td></td> <td></td> <td></td> </tr> <tr> <td>2</td> <td></td> <td></td> <td></td> </tr> <tr> <td>3</td> <td></td> <td></td> <td></td> </tr> <tr> <td>4</td> <td></td> <td></td> <td></td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> </tr> </tbody> </table>	REV	DATE	BY	DESCRIPTION	1				2				3				4				5				<p><b>E &amp; B Explorations Inc.</b></p>	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>DATE</th> <th>DRAWN BY</th> <th>CHECKED</th> <th>APPROVED</th> </tr> </thead> <tbody> <tr> <td>FEB 1987</td> <td></td> <td></td> <td></td> </tr> </tbody> </table>	DATE	DRAWN BY	CHECKED	APPROVED	FEB 1987			
REV	DATE	BY	DESCRIPTION																																	
1																																				
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DATE	DRAWN BY	CHECKED	APPROVED																																	
FEB 1987																																				
				<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>OFFICE</th> <th>DEPARTMENT</th> <th>MAP. INDEX NUMBER</th> <th>SCALE</th> <th>DRAWING NUMBER</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td>93A/11</td> <td>1:10,000</td> <td>6</td> </tr> </tbody> </table>	OFFICE	DEPARTMENT	MAP. INDEX NUMBER	SCALE	DRAWING NUMBER			93A/11	1:10,000	6																						
OFFICE	DEPARTMENT	MAP. INDEX NUMBER	SCALE	DRAWING NUMBER																																
		93A/11	1:10,000	6																																

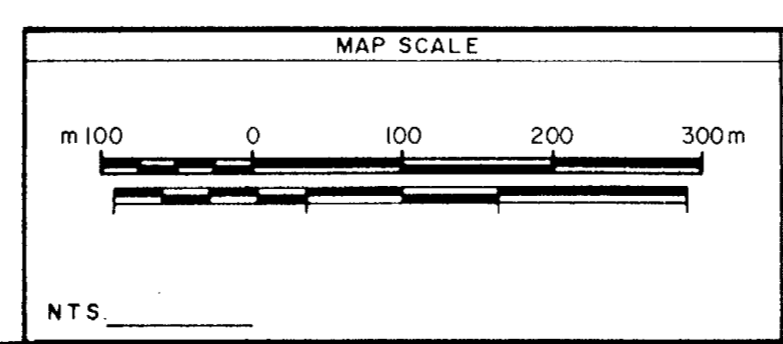




- LEGEND**
- VLF-EM ANOMALY (WEAK, MODERATE, STRONG)
  - INTERPRETED VLF-EM CONDUCTOR AXIS (WEAK, MODERATE, STRONG)
  - APPARENT CHARGEABILITY ANOMALY (WEAK, MEDIUM, STRONG)
  - MAGNETIC HIGH OUTLINE
  - INTENSE MAGNETIC HIGH

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

**16,018**



No	Date	MADE BY	DESCRIPTION
1			
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3			
4			
5			

DATE	DRAWN BY	CHECKED	APPROVED
FEB /1987			



OFFICE	DEPARTMENT

CARIBOO PROJECT		
WEST GRID		
GEOPHYSICAL INTERPRETATION MAP		
MAP INDEX NUMBER	SCALE	DRAWING NUMBER
	1: 5000	5A

MANCAL 12841

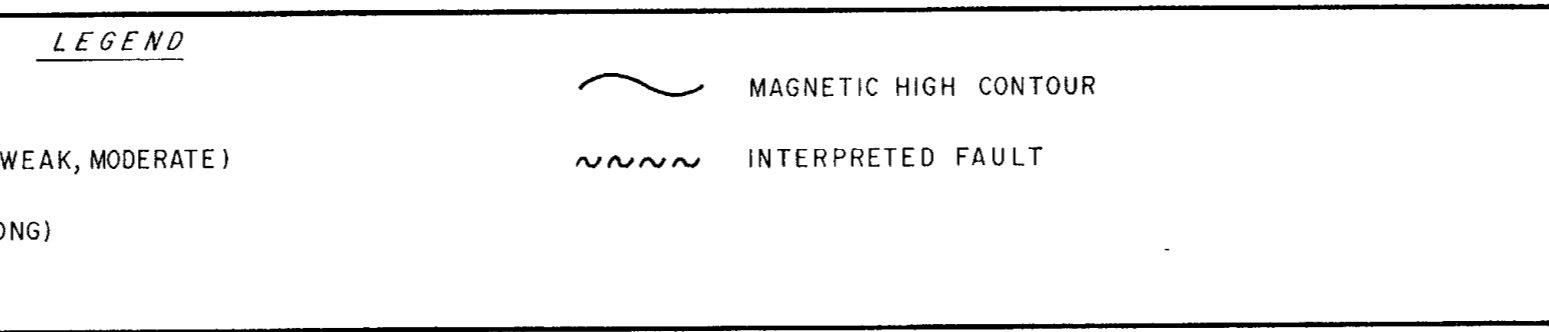


GEOLOGICAL BRANCH  
ASSESSMENT REPORT

16,018

**LEGEND**

	VLF-EM ANOMALY (QUESTIONABLE, WEAK, MODERATE)		MAGNETIC HIGH CONTOUR
	INTERPRETED VLF-EM CONDUCTOR AXIS (QUESTIONABLE, WEAK, MODERATE)		INTERPRETED FAULT
	APPARENT CHARGEABILITY ANOMALY (WEAK, MEDIUM, STRONG)		
	DEPTH ESTIMATE (SHALLOW, MODERATE, DEEP)		



No.	Date	MADE BY	DESCRIPTION

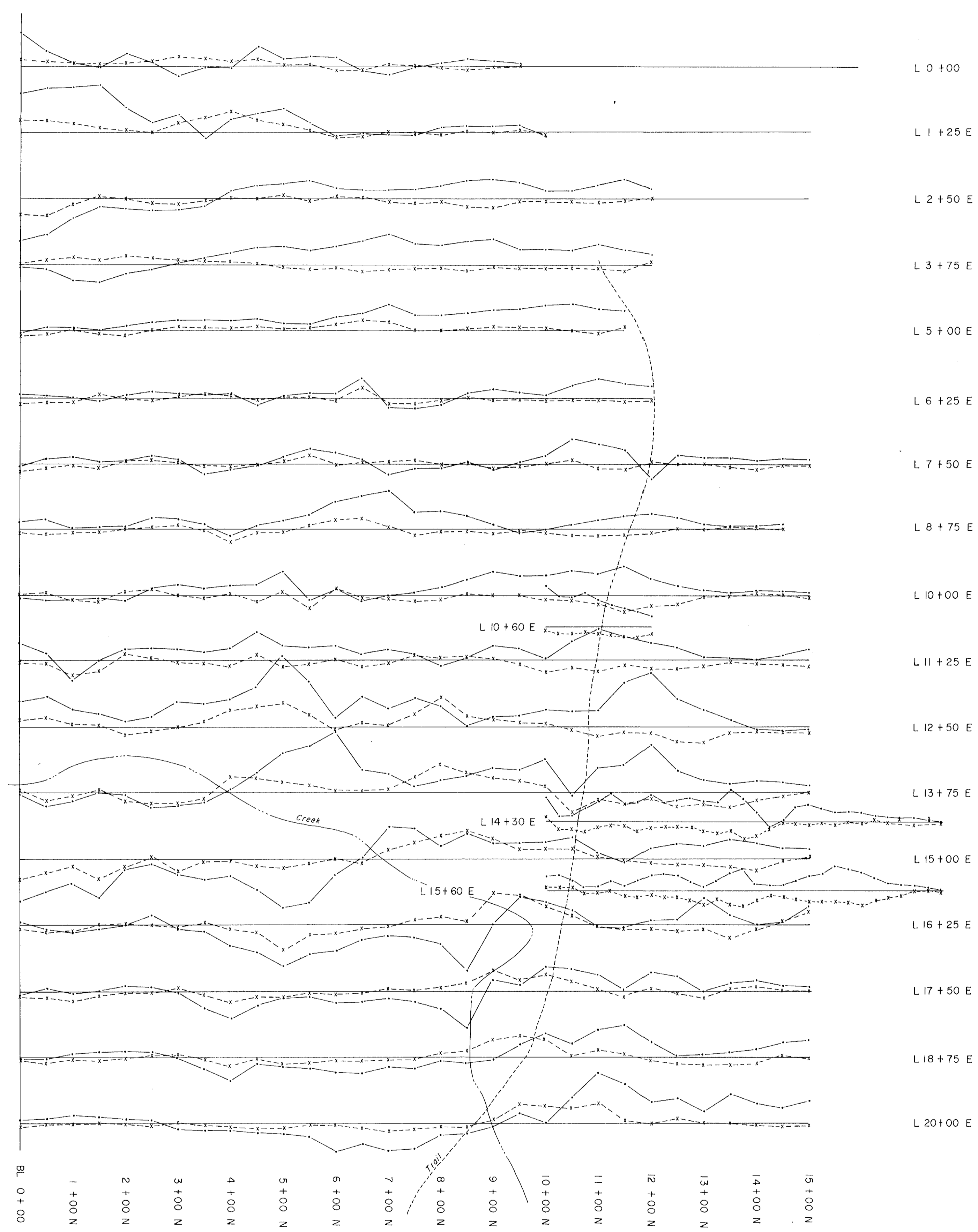
  

DATE	DRAWN BY	CHECKED	APPROVED

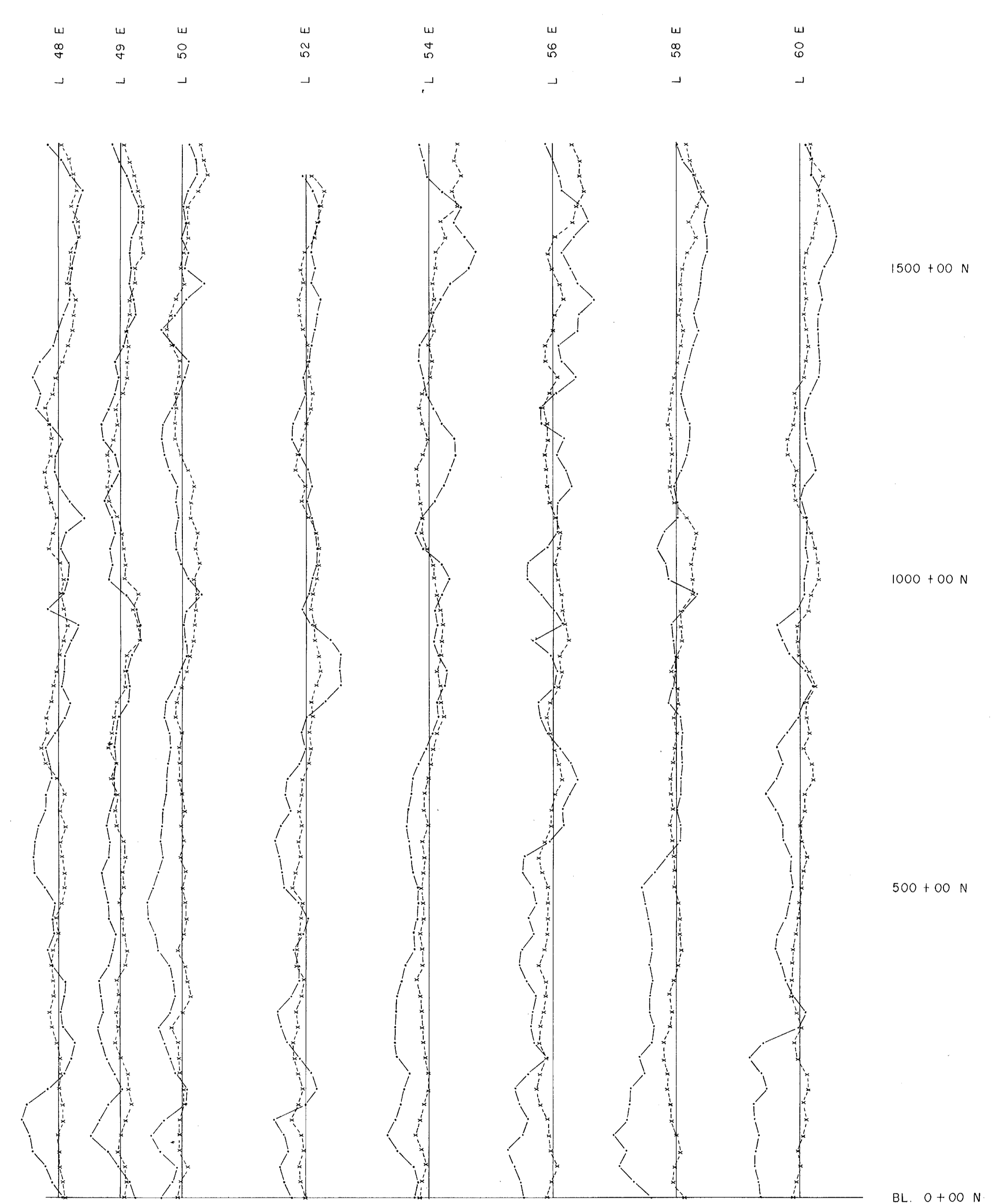
**E & B Explorations Inc.**

OFFICE	DEPARTMENT

CARIBOO PROJECT		
GEOLOGICAL INTERPRETATION MAP		
MAP INDEX NUMBER	SCALE	DRAWING NUMBER
	1 : 5,000	5



WEST GRID

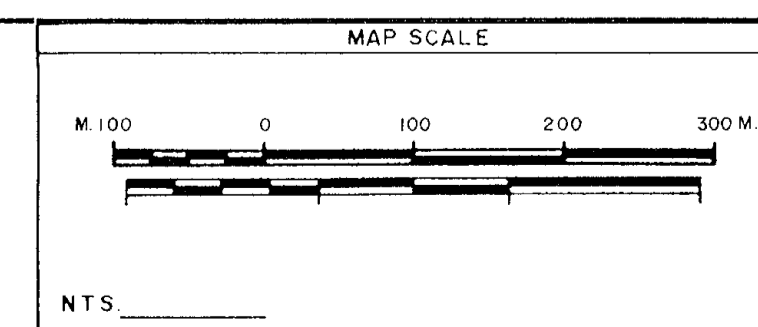
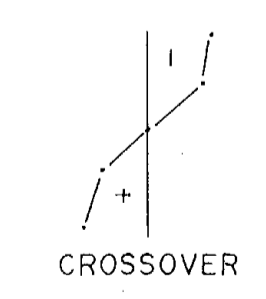
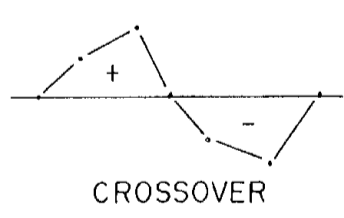
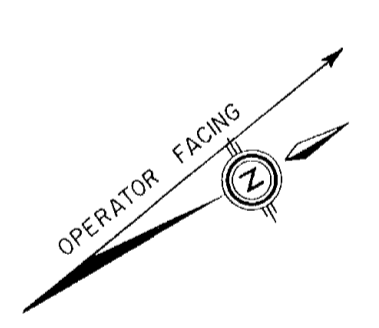


EAST GRID

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

16,018

**LEGEND**  
 - - - INPHASE  
 - - - QUADRATURE  
 ICM = 20 %  
 NAA CUTLER, MAINE  
 24.0 KHz



REVISIONS	No.	Date	MADE BY	DESCRIPTION
1				
2				
3				
4				
5				

DATE	DRAWN BY	CHECKED	APPROVED	OFFICE	DEPARTMENT
FEB 1986					



CARIBOO PROJECT		
VLF SURVEY		
MAP INDEX NUMBER	SCALE	DRAWING NUMBER
	1:5000	7

MAGNETIC