87-258-16050



Operator: CARDINAL MINERAL CORP.

# GEOPHYSICAL REPORT on the MARINER PROPERTY

Owner: Mariner Explorations Inc.

KAMLOOP MINING DIVISION
CACHE CREEK, BRITISH COLUMBIA

N. Lat. 50° 48' 00" W. Long. 121° 20' 00"

NTS 92I/14W

by



M. JOHNSON, M.Sc.

STRATO GEOLOGICAL ENGINEERING LTD.
3566 KING GEORGE HIGHWAY
SURREY, BRITISH COLUMBIA
V4A 5B6

APRIL 4, 1987



STRATO GEOLOGICAL ENGINEERING LTD.

SUMMARY

The Mariner Claim comprises 20 units located at Cache Creek, British Columbia. Trans-Canada Highway 97 traverses the eastern sector of the ground.

Chromite was apparently discovered prior to 1938 and several drill tests and a magnetic survey were carried out prior to 1948. The next recorded exploration activity was conducted in 1982 when Mariner Explorations Inc. carried out trenching. Cardinal Mineral Corp. optioned the property in 1986 and carried out magnetic and gravimetric surveys which are the subject of this report.

A gravity anomaly of magnitude 0.2 to 0.55 milligals, associated a magnetic anamaly of 2000 gammas, is centered about L400S, 200E. The magnetic anomalies to the north which have previously been drilled and which intersected chromite have a gravity signature of at most 0.1 milligals. There is little evidence from the geophysical surveys of a large chromite body in this area. However, the possibility of small chromite pods has not been ruled out. Zone "B" is considered more promising than the area previously tested with drilling.

In light of the above, it is recommended that trenching be done in zone "B" at several locations between elevations 630 and 640 meters. Samples would be taken at regular intervals along the trenches, and density measurements taken prior to assaying. Should the results be encouraging, a detailed gravity survey at 5 meter spacing between Lines 200S and 550S for a distant of 200 meters on each line. The purpose would be to define drill targets and to better define the dip of the unit.

A tentative location for a drill test would be collared at L250S and 35E, with a bearing of 70 degrees and a dip of 60 degrees to a depth of at least 75 meters.

Respectfully submitted,
Strato Geological Engineering Ltd.

M. Johnson, M.Sc.
Geophysicist

April 4, 1987

STRATO GEOLOGICAL ENGINEERING LTD.

## TABLE OF CONTENTS



STRATO GEOLOGICAL ENGINEERING LTD.

## LIST OF APPENDICES



STRATO GEOLOGICAL ENGINEERING LTD.

## LIST OF FIGURES



STRATO GEOLOGICAL ENGINEERING LTD.

# 1. INTRODUCTION

## 1.1 Objectives

On the request of Cardinal Mineral Corporation, magnetic and gravitational surveys were undertaken by Strato Geological Engineering, Ltd. The purpose of the surveys was to better define the location and size of a chromite deposit known from previous drilling, geological exploration and magnetic surveys.

## 1.2 Location

| | |
|---|---|
| Province: | British Columbia |
| Mining District: | Kamloops, Ashcroft Division |
| Area: | Cache Creek |
| Property Name: | Mariner |
| Latitude: | North 50 degrees 48' |
| Longitude: | West 121 degrees 20' |
| Disposition Holders: | CARDINAL MINERAL CORP. |

The property lies immediately west of the community of Cache Creek, and 80 kilometers west of Kamloops.

## 1.3 Access

Access to the property is via the Trans-Canada Highway and several unimproved roads on the property itself.

## 1.4 Operations and Communications

The field crew had its lodging in Cache Creek, B.C., and commuted to the property by four wheel drive vehicle. Frequent communication was made with the office in Surrey, B.C. Transportation in town and on the property was not a problem.

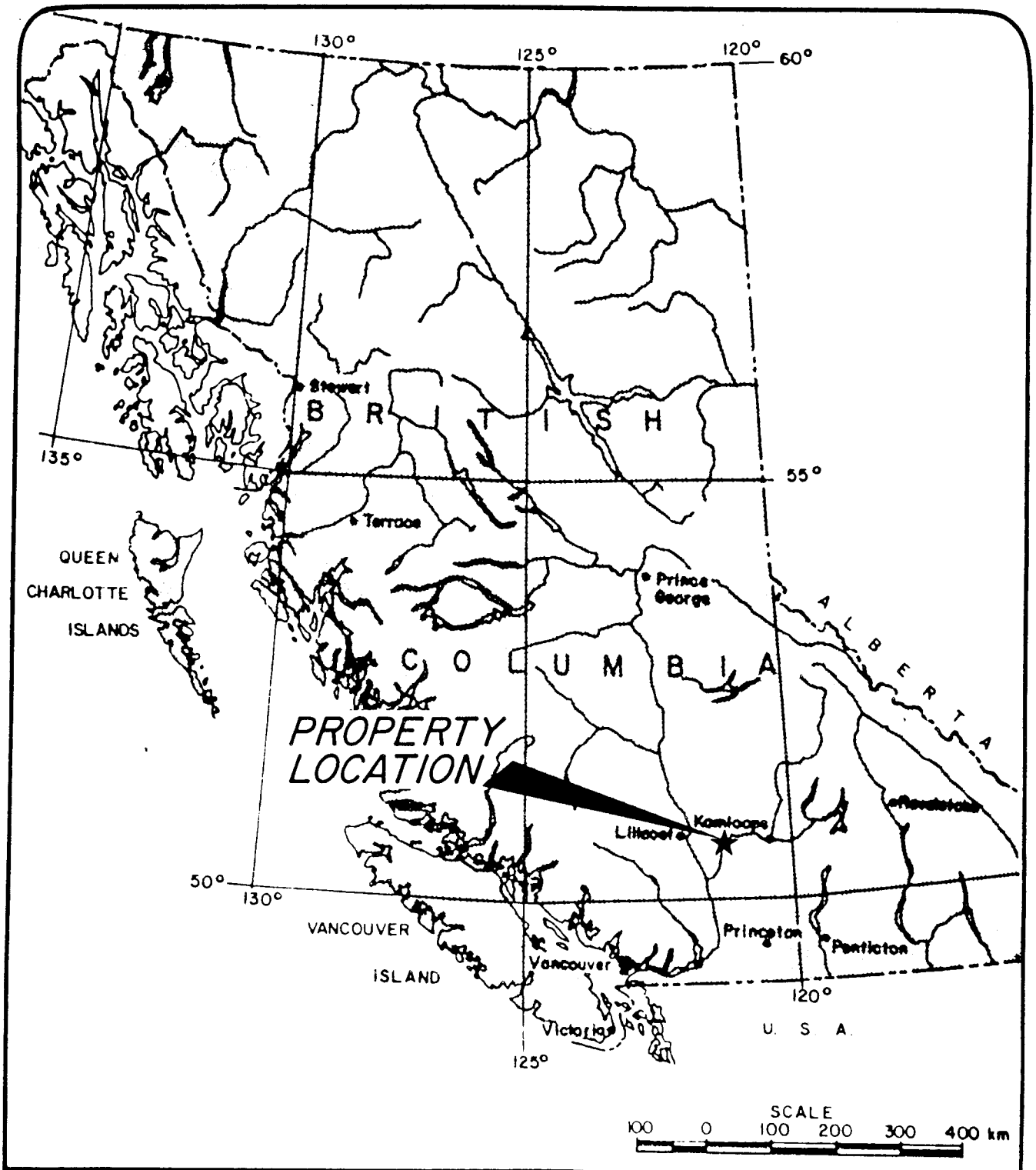



FIGURE 1

CARDINAL MINERAL CORP.

MARINER CLAIM GROUP

KAMLOOPS M.D. NTS 92 I/14 W

# LOCATION MAP

Feb. 1987

STRATO GEOLOGICAL ENGINEERING LTD.

## 1.5 Physiography

The terrain in the Cache Creek area is mountainous and is cut by several rivers and streams. Just west of the property the terrain rises steeply. The east side of the property is bounded by the Bonaparte River. Elevations on the property vary from 450 meters to 720 meters.

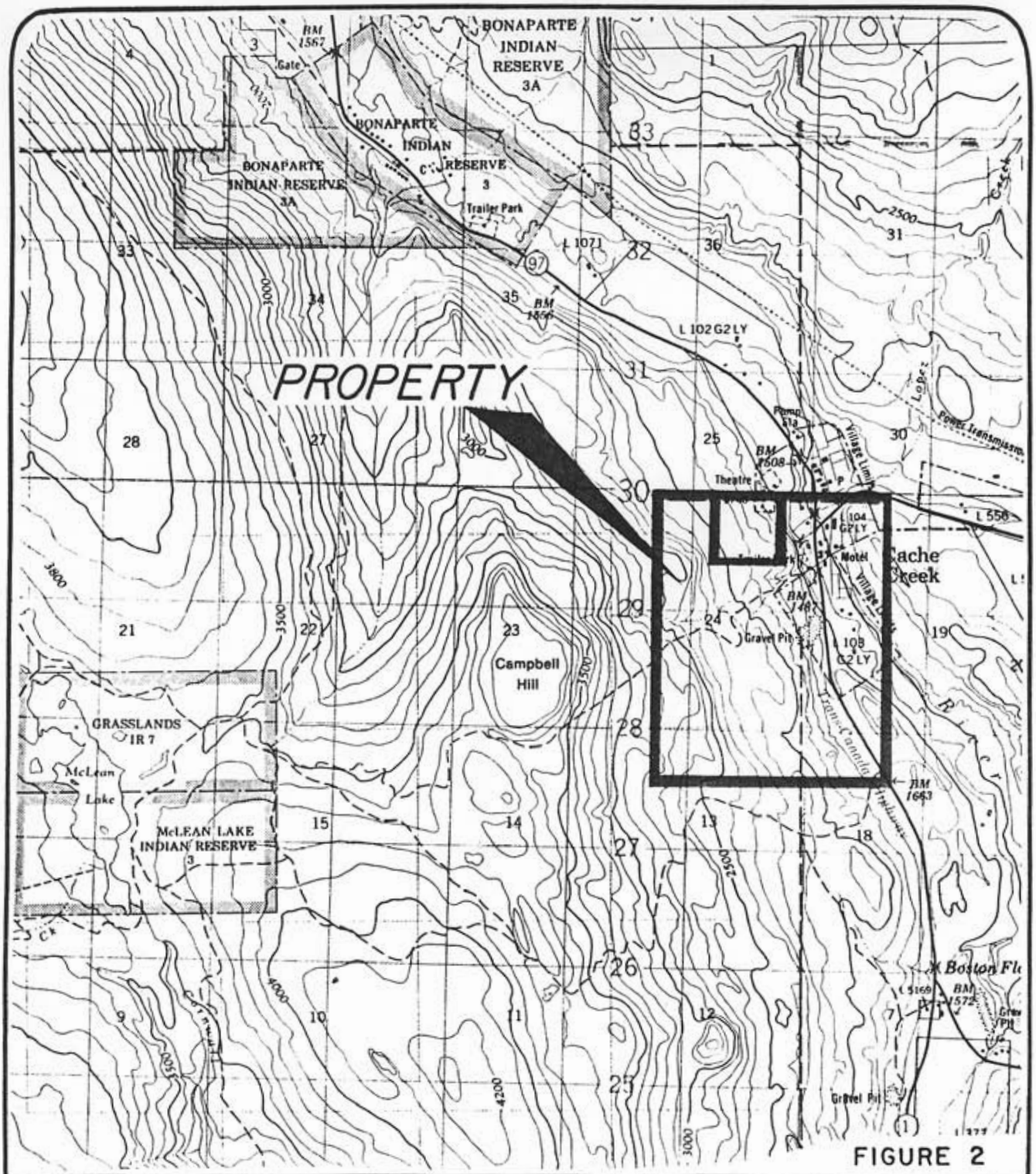
The area is considered to be "environmentally sensitive" because of its proximity to the community of Cache Creek.

## 1.6 Claims

Each claim unit is 500m by 500m, or 25 hectares in area. The number of claims is 20, giving a total claims area of 500 hectares or five square kilometers.

As of November 20, 1986 the following information was available at the Office of the Gold Commissioner, Court House, Kamloops, B.C.:

| | |
|---|---|
| Claim Name: | Mariner |
| Record Number: | 3963 (3) |
| Claim Units: | 5Nx4W (20) |
| Expiry Date: | March 1, 1987 |
| Recoded Holder: | Mariner Explorations Inc. |




AFTER
92 I/14
CACHE CREEK

Scale: 1: 50000

Metres 1000 0 1000 2000

CARDINAL MINERAL CORP.

MARINER CLAIM GROUP
KAMLOOPS M.D. NTS 92 I/14 W

# TOPOGRAPHIC MAP

Feb. 1987

STRATO GEOLOGICAL ENGINEERING LTD.

The property is located in Township 21, Ranges 24 and 25 in the Kamloops Land District.

Four claim units (2Nx2W) in the southeast corner of the claim area are the subject of negotiation between Mariner Explorations Inc. and the Village of Cache Creek for surface rights.

Within the claim area is one claim, the Everett (1) claim, not under record to Mariner Explorations Inc. Cardinal Mineral Corp. holds an option to earn a 100% interest in the Mariner Claim, subject to a 10% net profits interest, by completing exploration work on the property.

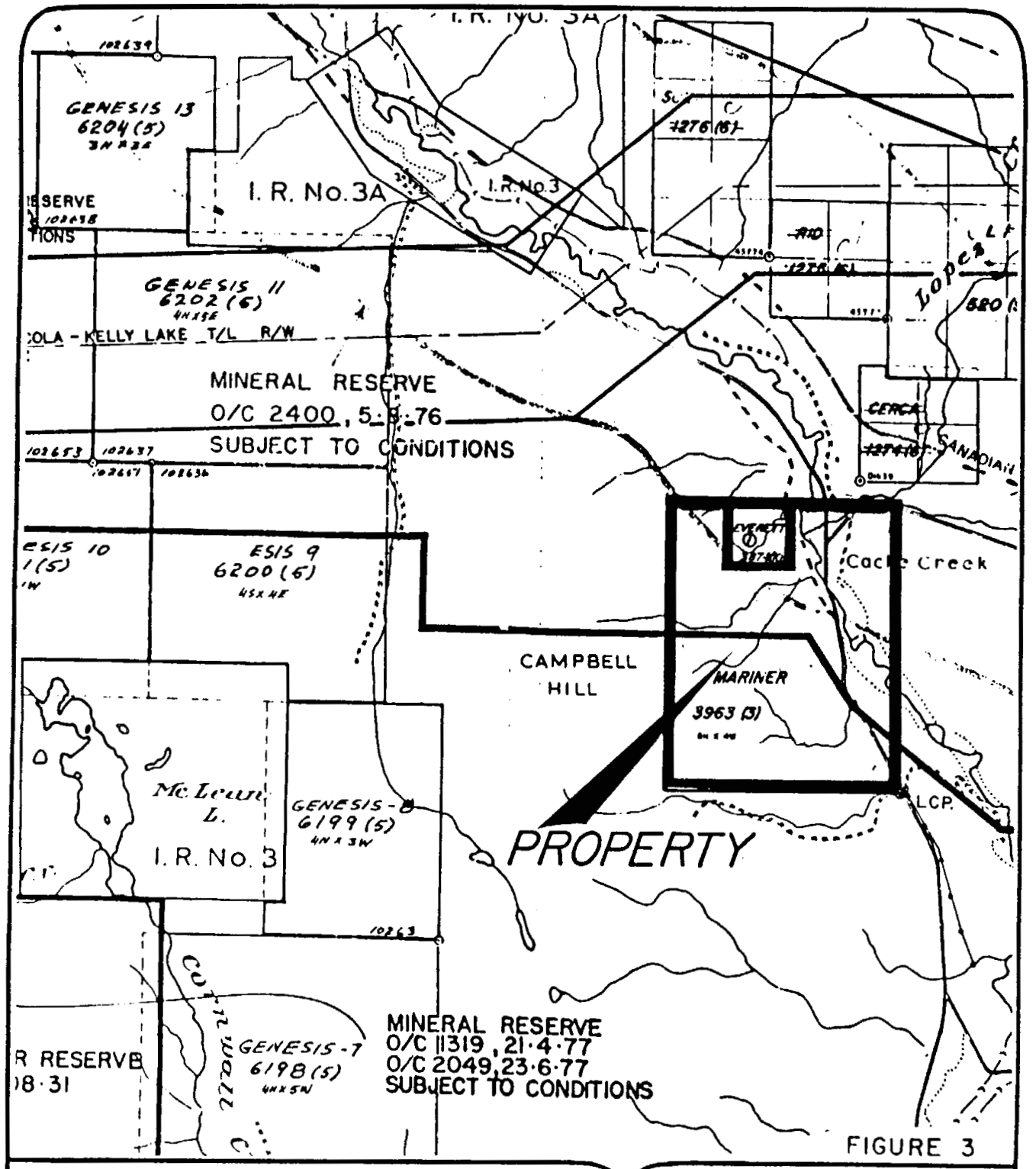



FIGURE 3

AFTER:
MINERAL CLAIM MAP
92 I/14W (M)

Scale 1:50,000

Metres 1000 0 1000 2000

CARDINAL MINERAL CORP.

MARINER CLAIM GROUP

KAMLOOPS M.D. NTS 92 I/14 W

# CLAIM MAP

Feb. 1987

STRATOS GEOLOGICAL ENGINEERING LTD.

## 2. HISTORY

The history of this property prior to 1947 is vague. Lester Starnes is reported to have had a chromite claim 4 1/2 miles west of Ashcroft, B. C., optioned to the Calgary Minerals Syndicate in 1938.

In 1947, the claims now held by Mariner were held as the Blue Rock claim group. J.W. Oakes of Vancouver held 11 claims and fractions at that time. The title of the claim group was then Dominion Chromium Property and was reported on by John C. Rogers. According to him, a magnetic survey had been done by the America Askania Corporation of Houston, Texas in 1939. Before this time at least five diamond drill holes had been drilled to test the indicated chromite deposits. Two of these drill holes were thought to have been shallow and three to have been deep tests. One of the deep drill holes was reported to have been lost in chromite mineralization in the area of anomaly "A" (Figure 4).

John C. Rogers examined the Dominion Chromium claims and his report is available in the geology report done by Mr. Don Tully of West Vancouver. He noted that the belt of serpentine and peridotite on the property were approximately 2,000 feet (600 meters) wide and trended south-southeasterly for more than one

mile (1.6 kilometers). He described a massive lenticular-shaped body of massive chromite measuring 15 feet (4.6 meters) long and four feet (1 meter) wide. He also reported "floats" of massive chromite in a ravine leading towards the Bonaparte River at the northern end of the property near the site of the original discovery of chromite on the claims. He also noted six mineral analyses of chromite samples in his report. These samples varied between 37.41 and 45.10 percent $Cr_2O_3$ and having a chrome/iron ratio between 2.81 and 3.03.

Mr. Rogers concluded that the grade of the chromite was adequate and that a detailed magnetometer survey ought to be implemented to target areas for diamond drill hole exploration of the chromite bodies.

In the summer of 1947, this magnetometer survey was carried out by H.L. Banting (Figure 3). The results of this survey disclosed three magnetic anomalies.

Mr. Banting concluded that the magnetite content, based on survey results and magnetic susceptibility tests on the serpentinized peridotite rock mass, was uniformly low. He also suggested that pods of chromite could occur in a manner directly related to the three magnetic anomalies and that the serpentinized mass was probably cross faulted.

Banting recommended that seven diamond drill holes be drilled to test the serpentine mass occuring within the 2,000 gamma contour interval horizons on the magnetic anomalies.

Mariner Explorations Inc., in 1982, trenched five pits. One of these exposed a mass of chromite that is open to the west. Estimated volume of earth and rock excavated during this work is calculated at 134 cubic meters.

A recent re-examination of these pits was done by Mr. Don Tully of West Vancouver, B.C. The assay values of the chromite samples taken in November 1986 were as follows:

| Sample No. | 613 | 614 |
|---|---|---|
| Mineral | (Chip) | (Boulder) |
| Chromite | 37.3 % | 36.7 % |
| Silica | 10.7 % | 10.1 % |
| Alumina | 15.2 % | 15.3 % |
| Lime | .77% | 1.15% |
| Magnesia | 20.1 % | 19.4 % |
| Iron Oxide | 8.1 % | 13.1 % |

Both samples also showed 0.005 Oz/st Platinum

Tully concludes that these grades are satisfactory for refractory grade chromite although the silica is slightly higher than the usual 5% that is required.

Mr. Tully expressed interest in the presence of gold and platinum in the samples taken. He recommended that a magnetometer and gravimetric survey be performed.

## 3. GEOLOGY

### 3.1 Regional Geology

The general geology of the claim area is shown on Geological Survey of Canada Map 1010A.

Paleozoic argillites, greenstone volcanics and a belt of limestone intruded by a mass of serpentinized ultrabasic rock of probable late Mesozioc age underlie the property.

A tentative geologic timetable from Tully is as follows:

| FORMATION | DESCRIPTION/EVENT | AGE |
|---|---|---|
| Sand, gravel, fluvial sediments and glacial debris | Unconsolidated | Quaternary |
| | (Erosional unconformity) | |
| Ultrabasic intrusives, mineralization including sparse pyrite, arsenopyrite(?), magnetite and chromite | Serpentinization Fine sulphides of iron, localized asbestos seams, (chromite considered to be magmatic segregation nized ultrabasic intrusive during emplacement) | (Probably late Jurassic or early Cretaceous |
| | (Faulting, folding, shearing and related tectonic activity) | |
| Cache Creek Group | Argillites, greenstone volcanics, chert beds and limestone horizons | Permian or earlier |

3.2 Property Geology

The geological formations on the property have been subjected to repeated folding and faulting events. There is a schistosity which has developed approximately parallel to the Bonaparte river. It has been postulated that the valley occupied by the river itself marks a major strike zone in the area which may have been very influential in the placement of the serpentinized ultrabasic which bears the chromite deposits.

The body of the peridotite is estimated to have a width at surface of 2,000 feet (0.6 kilometers). The strike is open at both the northern and southern ends of the property. The contact areas of the ultrabasic and Cache Creek Group have not been mapped to delineate the boundary.

The Geological Survey of Canada Aeromagnetic Map 5219g illustrates the trend of the basement geology which has been shown to correlate with the features of the geology at surface. A geological sketch map (After H.L. Banting, Oct. 1947) showing the serpentine outcrop in relation to the Cache Creek Formation is presented as Figure 6.

## 4. GEOPHYSICS: Magnetics

### 4.1 Station locations

The magnetometer survey was carried out on the property between January 5 and January 16, 1987, by technicians A. E. Hunter and Lucas Meyer. A total of 1149 stations were read.

The starting point for the survey was station OW,ON which is a local topographic high easily identifable from the topographic map. All lines were run with a compass and hip chain at a nominal spacing of 25 meters. The baseline has a bearing of 340 degrees, and was surveyed twice with the magnetometer to set up tie points for the crosslines. Crosslines were surveyed in loops and the values drifted as necessary to tie with the baseline values. Most lines tied within 10 gammas. Lines that did not tie to this accuracy were resurveyed.

### 4.2 Findings

The majority of the property has background values in the range of 57250 to 57500 gammas, with no significant gradients across the survey area. Two major features were located. Zone "A", a roughly circular feature with a diameter of 600 meters centered at 250N and 50E, has values about 250 gammas above background.

Within this area are four pod-like anomalies of 1000-1250 gammas above background. The two most northerly of these pods have loosely associated lows to the east, suggesting dipolar magnetic pods dipping to the west.

The second feature extends from 100S to 600S at a strike direction of 310 degrees, and is designated zone "B". It is characterized by values 1500 to 2500 gammas above background and is flanked to the east by a low area of similar magnitude. Profiles of this feature on lines 200S and 600S can be found in appendix VIII. The pattern on these profiles suggests a dipolar magnetic body with a dip of 45 degrees to the west and suboutcropping about 50 meters below surface. The most probable cause of this feature is magnetite within the serpentine unit which Banting noted as outcropping in this area.

The findings of this survey are similar to those of the survey reported by Banting in 1947. The main difference is that the older work did not establish a dip on the southern zone and the northern zone has been shown to be somewhat larger than originally indicated. Note that the absence of lows associated with the podlike highs suggests that dips are greater in the "A" zone.

## 5. GEOPHYSICS: Gravimetrics

### 5.1 Station Locations

Station locations were established using a Topcon Theodolite (see appendix I). The base station on the property was located by triangulation at a marked elevation point on the 1:50000 topographic map at coordinates 5629820N and 617260S. The baseline established for the magnetics was surveyed by transit from 1125 North to 800 South. Cross lines were generated by turning 90 degree angles from the baseline. Locations do not necessarily correspond to those for the magnetic survey, but were flagged as gravity stations. Loops were tied to the baseline values. Most loops closed positionally within five meters and had elevation closures of under two meters. Closure errors were corrected by linearly distributing the error around the loop. Two lines, 350S and 450S, had poor closures. Because these lines were surveyed on the last two days, it was not possible to redo the loops and they have been omitted from the results. Observations were extended beyond line 250N to the west along a powerline to establish the density of the Cache Creek volcanics which outcrop on Campbell Hill. A number of points along highway 1 and withinin the town of Cache Creek were also surveyed to establish background readings. Because of the steep terrain and slippery conditions when the survey was done, eight stations within the main grid were not surveyed.

## 5.2 Gravity Readings

The Lacoste-Romberg Gravimeter functioned well. Due to steep terrain and melting snow, it was necessary to prepare sites for the dish of the gravimeter. A base station was established at the motel in Cache Creek, which was read at the beginning and end of the survey day. All values were drifted to this station to eliminate diurnal drift. Lines were repeated if the misclosure at this station exceeded .05 milligals. The absolute accuracy of all gravity observations is calculated to be within .05 milligals of the true value.

## 5.3 Data Reduction of Transit Survey

The transit survey data was reduced using an HP41C programmable calculator using standard reduction formulas. Correspondence between the transit survey and the topographic map is generally good. However, in the extreme northwest and southeast corners of the property steep terrain caused elevation variations of up to 10 meters.

## 5.5 Density

A density of 2.67 gm/cc was used in the complete Bouguer calculations. This is the standard value used in gravity reduction. It is possible to estimate the density of the rock units by plotting the gravity values against elevations and

fitting a straight line to the resulting values by linear regression. This was done with two lines, 250S and 700S. The results of this analysis appear in Appendix VII. Density values of 2.79 and 2.68 gm/cc were found with this analysis, with excellent fit of all data to the line model. These results confirm that the chosen density for Bouguer reduction is reasonable, and that the entire survey area is one formation (except for surface variations). Note that in areas where two distinctly different density units existed, the gravity/elevation plot would have two slopes corresponding to the different densities.

5.6 Terrain corrections

Terrain corrections were done with custom software developed by Martin Johnson. The basic approach was to develop a grid of blocks over the property and the surrounding area which would closely represent the topography. The effect of each of these blocks was summed for each of the survey stations according to the formulas in Appendix III.

Within the survey area block elevations were established using the survey points. Since blocks were generated on a grid of 25 by 25 meters, it was necessary to interpolate results between survey lines. This was done by a program which looked for points

within a 150 meter by 150 meter area around the center of the block to be generated. Any point within the actual block was given a weighting of 8 in relation to points found in the surrounding area, and the average of the values found was taken to be the block elevation. This was checked visually against the existing topographic map for overall accuracy.

A commercial package called UNIRAS was also tried which uses a similar pattern with a circular search radius and polynomial smoothing, but this package would not yield satisfactory block elevations.

The remainder of the elevations were established by picking points off the 1:50000 government map of the area. Points within the coordinates 616500 E to 618500 E and 5627500 N to 5630000 N were picked on a 25 meter grid and the average of these values used to generate 25 meter by 25 meter blocks. Beyond this area, one kilometer block estimates were generated between 612500 E to 622500 E and 5624000 N and 5634000 N as shown in Figure 48 (appendix III).

The terrain corrections were done in two parts and the results for the outer zone of one kilometer blocks are listed seperately than those for the inner zone of 25 meter blocks as

defined above. The corrections due to the outer zone vary from 3.2 to 5.4 milligals. The main effect was to increase the values on the westerly end of the survey lines as the result of Campbell Hill which is centered about 1.25 kilometers west of the property and has an elevation of 1150 meters. The terrain corrections in the inner zone were more significant due to the steep slopes on the eastern half of the property. Elevations drop from the plateau value of 640 meters to under 520 meters, with slopes up to 40%. The inner zone terrain corrections vary from 1.2 to 1.8 milligals across the flat areas, and rise to over 4 milligals in places at and on the steep slopes.

Special attention was paid to the accuracy on the east side of the baseline between lines 300S and 650S to assure the best possible results. Difficulties were encountered in this area due to poor correspondence between the survey values and supplementary points used to generate block elevation estimates. The overall effect of this and other inaccuracies is a noise envelope of approximately .15 milligals in the Complete Bouguer values. Lines 350S and 450S were omitted from the final results because, although confirming a similar pattern to the other lines, the absolute gravity values could not be made to correspond with adjacent lines.

## 6. INTERPRETATION

### 6.1 Discussion of results

The complete Bouguer values are shown on Figure 6. The most important regional feature is an increase in the gravity values of 2.5 milligals from north to south across the property. This is characterized by a strong gradient from 650N to 100N and a shallower gradient to the south. The cause of this feature is interpreted as being variations in the basement rock depth which are not significant in the economic interpretation. To the west of the property, the values along the powerline rise steeply to a value more than 3 milligals higher than any in the main grid. The gradient is too steep to be due to a deep feature, and is more likely to be due to crossing into a denser rock unit.

East/west profiles show a strong gradient on the western side of the property from stations 400W to 175W. The gravimetric readings in this area have corrections of 1 to 2 milligals due to the extreme changes in elevation in this area.

The area bounded by 200W and 50E and between 150N and 400S is a gravity low which probably reflects Quaternary sediments. Higher values on the ends of the lines and to the south are interpreted as being due to serpentinized peridotite, with a thin

or non-existant covering of sediments. This shows on the plan map as the 11.75 milligal contour indicating the boundaries of the serpentine unit and the sediments.

The most significant gravity feature corresponds with the Magnetic Zone "B". It has a length of 350 meters and a width of up to 150 meters and anomolous gravity values from 0.2 to 0.55 milligals above background. This zone is on the eastern flank of the 2000 gamma magnetic anomaly in an area mapped by Banting (Figure 4) as having serpentine outcrops.

The serpentine outcrops located between 100N and 400N (Magnetic Zone "A") have little or no gravitational signature. Since this is an area which was previously drilled and holes were reported to have intersected chromite, it is concluded that the pods are too small or too deep in the northern area to be reflected in the gravity readings. This makes the area to the south of greater interest.

It is not clear that the 0.4 milligal anomaly in zone B is directly caused by Chromite mineralization. As the modeling will show, it is just as likely that that the anomaly is the result of an outcrop of serpentine surronded by a least dense unit. Nevertheless, economic mineralization can not be ruled out,

particularly since the Chromite to the north does not have a strong gravity signature. The presence of magnetite near this area is also an encouraging indication since chromite has been located within the magnetic anomalies to the north.

## 5.2 Modeling

The modeling method used was the Talwanic method, which gives the gravitational effect of a two-dimensional multi-sided polygon. This method has proved quite effective when the width of the ore zone is relatively constant, as in the present case. Four lines, 0N, 250S, 400S and 550S were modeled and the results appear in Appendix VI. The approach used was to create areas of different densities delineated as the vertices of polygons. The difference between the densities of the polygons rather than the absolute densities is the significant factor in determining the shape of the profiles generated. In this case density contrasts of 0.3 and 0.5 milligals were modeled. Although the sections show this as due to a sedimentary unit of density 2.2 or 2.4 gm/cc underlain by a denser unit of 2.7 gm/cc, the results would be the same for any combination where the density difference was the same.

The usual approach when attempting modeling is to start with a point at which the density of the underlieing rocks is known, as from drill results. Since this kind of information was not available, an assumption had to be made. It is known that the area has been glaciated, so it was postulated that the flat area at elevation 630 meters was the top of the glacial moraine. It was assumed that the denser unit (serpentine) would be at on near surface at the western end of the lines at elevation 650 meters. Figures 37, 38, and 40 show this type of model with a density contrast of 0.3 milligals. This model gives satisfactory results on lines 0N and 250S, with a suboutcrop of the serpentine at 20 meters and 4 meters respectively. However on line 400S this model did not fully account for the anomaly, particularly in the area from 200E to 300E. On line 550S it was necessary to assume a sedimentary cover on the western flank to fit the anomaly.

The second set of models put no constraints on the depth of sediments on the western flank and used a density contrast of 0.5 milligals. The depth to the sub-outcrop of the serpentine in the anomolous zone was kept constant. The main difference from the first model set is that the depth of sediments decreases from a central thickness of 200 meters to 130 meters on lines 0S , 250S and 400S, with a depth of 20 meters on the western flank. In light of the fact that the gravity values continue to increase sharply to the west, this model is believed to be more realistic.

On line 550S, a different approach was taken by establishing the sedimentary cover at 30 meters for both density contrasts. This resulted in maximum sediment thicknesses of 80 and 120 meters. In neither case was it possible to get a satisfactory fit to the high value at station 250E. Thus there is some evidence of a small zone of much higher density in this area.

Several general conclusions can be established from the modeling. Except for the anomalies on lines 400S and 550S, the rest of the anomalous zone can easily be accounted for by variations in the sedimentary cover. The magnetic values show a dip of 45 degrees to the west. The modeling generally confirms the westerly dip of the serpentine zone, although the dip may be steeper to the north and much shallower to the south. Secondly, even with the addition of a second polygon of higher density than the serpentine (see figure 40) it was not fully possible to explain the high values from 200 to 300E on lines 400S and 550S.

## 7. CONCLUSIONS AND RECOMMENDATIONS

An anomolous zone of magnitude 0.2 to 0.55 milligals was located about 50 meters to the west of a magnetic anomaly of 2000 gammas, and extending for 550 meters at a strike of 320 degrees. The magnetic anomalies to the north which had previously been drilled and which intersected chromite have a gravity signature of at most 0.1 milligal. There is little evidence from the geophysical surveys of a large chromite body in this area. However, the possibility of small chromite pods has not been ruled out. Magnetic Zone "B" is considered more promising than the area previously tested with drilling.

In light of the above, it is recommended that trenching be done in zone "B" at several locations between elevations 630 and 640 meters. Samples would be taken at regular intervals along the trenches, and density measurements taken prior to assaying. Should the results be encouraging, the next step would be a detailed gravity survey at 5 meter spacings between 200S and 550S for a distant of 200 meters on each line. The purpose would be to define drill targets and to better define the dip of the unit.

A tentative location for a drill hole is shown on figure 38. It should be collared at 250S and 35E, with a bearing of 70 degrees and a dip of 60 degrees to a depth of at least 75 meters.

Respectfully submitted,
Strato Geological Engineering Ltd.

M. Johnston, M.Sc.
Geophysicist

April 4, 1987



STRATO GEOLOGICAL ENGINEERING LTD.

## 8. REFERENCES


G.S.C. Paper 47-10, pp. 5-6

B.C. Annual Report of the Minister of Mines, 1947, p.130, 223

Tully, D. W. (July 4, 1982)
Private Report on the Dolly, Dominion, Mariner Mineral Claim Group, Kamloops M.D. for Mariner Explorations Inc.

Rogers, J. C. (May 12, 1947)
Report on Dominion Chromium Group, Ashcroft M.D., Kamloops District, B. C.

Banting, H. L. (October 15, 1947)
Report on a Magnetometer Survey on Port of the Property on the Dominion Chromium Property, Ashcroft M.D., Kamloops District, B. C.

Telford, W. M. (1976)
Applied Geophysics

Nagy, D. (1966)
The Gravitational Attraction of a Right Rectangular Prism, Geophysics Vol. XXXI, p. 362-371.

## 9. CERTIFICATE

I, MARTIN JOHNSON, of the City of Vancouver, Province of British Columbia, hereby certify that:

1) I am a geophysicist employed by Strato Geological Engineering Ltd. as a Consulting Geophysicist. My office is at 3566 King George Highway, Surrey, British Columbia, Canada, V4A 5B6

2) I obtained a Bachelor of Science degree in Mathematics and Physics from the University of British Columbia in 1966 and a Master of Science degree in Geophysics from the University of Utah, Salt Lake City in 1972.

3) I have been practising my profession as a geophysicist since 1972.

4) I have not received, nor do I expect to receive, any interests, direct or indirect, or contingent, in the securities or properties of Cardinal Mineral Corp., and that I am not an insider of any company having an interest in the Mariner Mineral Claim or any other properties in the area.

Dated at Surrey, this 4th day of April, 1987.

Martin Johnson, M.Sc.



STRATO GEOLOGICAL ENGINEERING LTD.

# APPENDIX I: Instrument Specifications

## Instrument Specifications

### MAGNETOMETER

| | |
|---|---|
| TYPE: | Scintrex |
| MODEL: | MP-2, Proton Magnetometer |
| FIELD: | Total |
| SENSITIVITY: | 1 gamma |
| RANGE: | 20,000 to 100,000 gammas |
| CAPABILITY: | 5000 gammas/meter on gradient |

### TRANSIT

| | |
|---|---|
| TYPE: | Topcon Theodolite |
| MODEL: | TL 20-DE |
| SERIAL NO.: | E32999 |
| OPTICAL SYSTEM: | Internal focusing analactic |
| ERECTING SYSTEM: | Porro-prism |
| MAGNIFICATION: | 30x |
| FIELD: | $1^{o}$ 20' |
| RESOLUTION: | 3" |
| STADIA RATIO: | 100 |
| STADIA CONSTANT: | 0 |
| OTHER: | Optical micrometer<br>Digital readout |

### GRAVIMETER

| | |
|---|---|
| TYPE: | Lacoste & Romberg<br>Land gravity meter |
| MODEL: | Model G #g199 |
| RANGE: | 7000 mgals |
| ACCURACY: | +0.01 mgals |
| DRIFT RATE: | $\overline{<}$1mgal/month |

# APPENDIX II: Time-Cost Distribution

## TIME - COST DISTRIBUTION

The claims toward which work is being applied with this report is the Mariner Claim held by under option by Cardinal Mineral Corp. Field work was completed by Strato Geological Engineering Ltd. during the period of January 5 through February 9, 1987. Office work was completed during February and March, 1987.

A listing of personnel and distribution of costs is as follows:

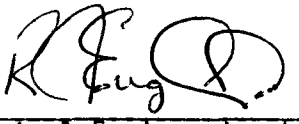
Personnel

| | |
|---|---|
| R. Englund, B.Sc. | Project Supervisor |
| M. Johnston, M.Sc. | Project Geophysicist |
| A.E. Hunter, B.A.Sc. | Geophysicist |
| L. Meyer, B.A.Sc. | Geophysicist, Gravimeter Operator |
| E. Ulmer, C.E.T. | Surveyor |
| R. Bunce | Field Assistant, Rod man |
| K. Pinksen | Field Assistant |

Cost Distribution

| | | |
|---|---|---|
| A. Hunter Jan. 5 - Feb. 4<br>L. Meyer Jan. 5 - Feb. 4<br>E. Ulmer, R. Bunce, K. Pinkson<br>Jan. 15 - Feb. 4<br>M. Johnston Jan. 16 - 19<br>R. Englund Jan. 4, 5, 16-19, 31 - Feb. 1<br>- 134 man days. | | $27,315.00 |
| Room and Board - 134 @ 55/day | | 7,370.00 |
| Vehicular - 4WD Trucks - 39 days @ 105/d<br>(incl. gas, oil, insurance, etc.) | | 4,095.00 |
| Field Equipment | | |
| - Proton magnetometer | 840.00 | |
| - LaCaste Romberg Gravity meter | 2,040.00 | |
| - Topcon TL 20DE | 600.00 | |
| - Computer and printer | 720.00 | |
| - Materials & supplies, etc. | 465.00 | 4,665.00 |

| | |
|---|---|
| Office Work | |
| - Gravity reduction, computer processing, programming, M. Johnston, A. Hunter, R.J. Englund | 7,100.00 |
| - Drafting, reproduction, typing, etc | 825.00 |
| - Geophysical Report | 1,600.00 |
| TOTAL | $52,970.00 |

Signed: 

Strato Geological Engineering Ltd.

# APPENDIX III: Terrain Correction Procedures

## APPENDIX III: Terrain Correction Procedure

The formula for gravitational attraction is:

$$\Delta F = G\rho \frac{\Delta v}{r^2}$$

where G= Gravitational constant, $\rho$ is the density, $\Delta v$ is the volume element and r is the distance to the mass.

This formula may be integrated by parts to solve for the vertical component, which in Cartesian coordinates gives the formula:

$$F_z = G\rho \int_{x_1}^{x_2} dx \int_{y_1}^{y_2} dy \int_{z_1}^{z_2} \frac{z\,dz}{R}$$

where $R = \sqrt{(x^2+y^2+z^2)^3}$

The solution of this integral for a right rectangular prism can take several forms. The solution given by Nagy (see references) is:

$$F_z = G\rho \left[ x \ln(y+r) + y \ln(x+r) - z \arcsin \frac{z^2+y^2+yr}{(y+r)\sqrt{y^2+z^2}} \right]$$

with the appropriate limits for x,y, and z (setting the axis of our coordinate system at the station at which we presently wish to determine the terrain correction. If the prism is completely contained within one of the xy quadrants and we establish the base of the prism at the height of the station (Z1=0 and Z2=Elevation difference between block and station), the solution takes the form:

F=X2(T1-T2)-X1(T3-T4)+Y2(T5-T6)-Y1(T7-T8)+Z2(T9-T10-T11+T12)

where the terms T1 to T8 take the form:

$$T = LN\left\{ \frac{U_K + \sqrt{U_I^2 + U_K^2}}{U_K \sqrt{U_I^2 + U_K^2 + Z_2^2}} \right\}$$

where U=Y in T1 to T4 and U=X in T5 to T8
V=X in T1 to T4 and V=Y in T5 to T8

and T1,T5- I=2,K=2 T2,T6- I=2,K=1
T3,T7- I=1,K=2 T4,T8- I=1,K=1

T9 to T12 take the form:

$$T= \text{ARCSIN}\left\{\frac{Y_K + Z_2^2 + Y_K\sqrt{X_I^2 + Y_K^2 + Z_2^2}}{(Y_K + \sqrt{X_I^2 + Y_K^2 + Z_2^2})\sqrt{Y_K^2 + Z_2^2}}\right\}$$

and T9- I=2,K=2 T10- I=1,K=2
T11- I=2,K=1 T12- I=1,K=1

Individual T terms may be large but since they come in pairs of opposite sign, ths sum result is small. As a result any program designed to calculate the effect must be written in double precision.

In the special case where the block under consideration straddles either the x or y axis, the form of the equation is:

F1=X2(T1-T2)-X1(T3-T4)+Y2(T5+T6-T7+T8)+Z2(T9-T10-T11+T12)
+T13+T14

where the terms T13 and T14 have the form:

$$T13= Y2\ LN\left\{\frac{Y_2}{Y_2 + Z_2}\right\} \qquad T14= Y1\ LN\left\{\frac{Y_1}{Y_1 + Z_2}\right\}$$

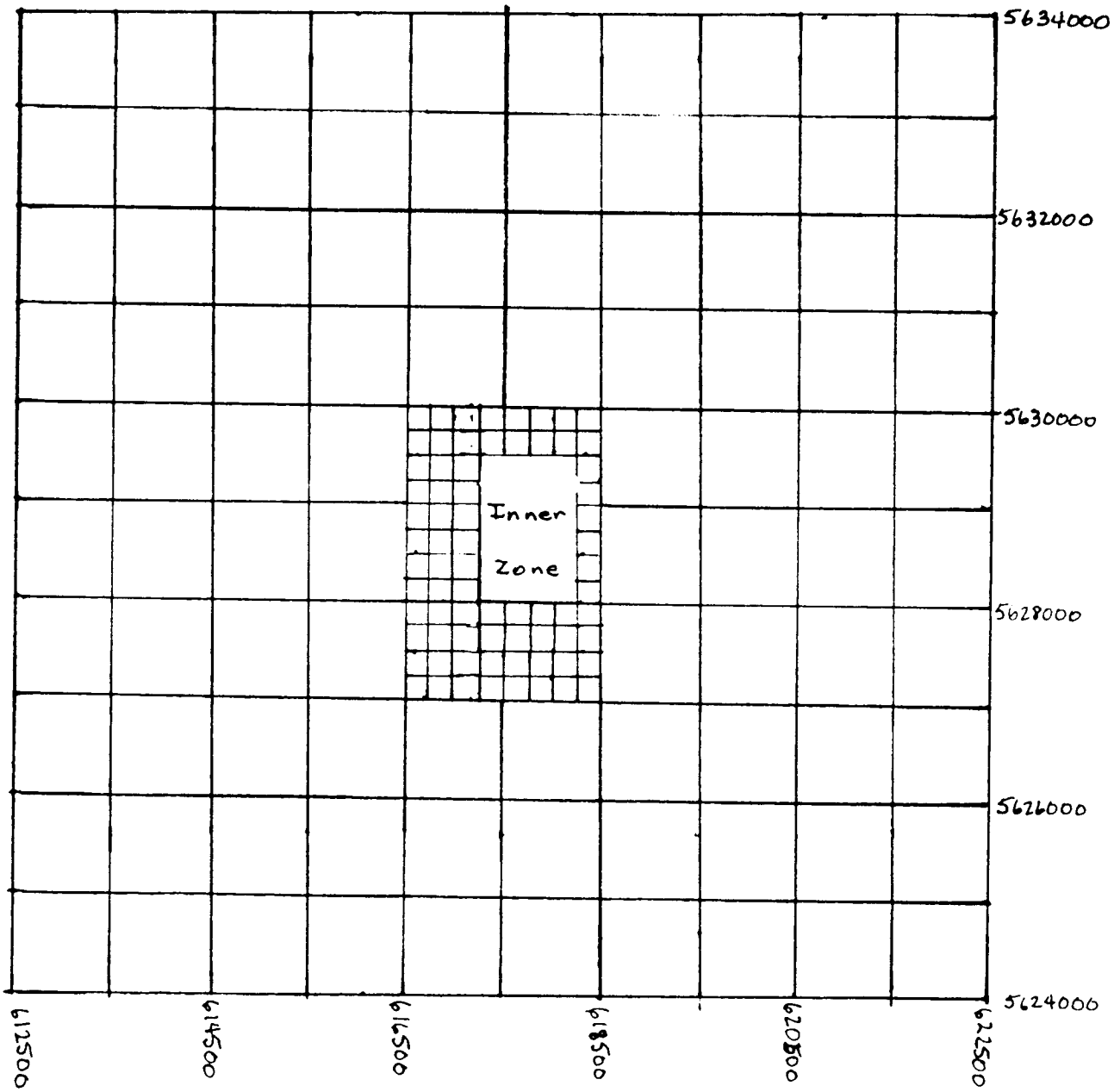
Note the difference in the signs of the T terms in equations for F and F1. The gravitational attraction in milligals is given by:

G=.0067 x 2.67 x F

The Fortran program to make the above calculations takes 5 seconds for a single block on a Kavpro II, and 5/100 of a second on an IBM AT computer. Running time for the calculations done for this project was 12 hours on the IBM-AT computer.

A drawing showing the blocks used in the above calculations follows on the next page.

Outer Zone - 1 Kilometer + 250 meter blocks
Inner Zone - 25 meter blocks
(See Columns in Gravity Listings)




TERRAIN CORRECTION
BLOCKS

Figure 48

# APPENDIX IV: Complete Bouguer Gravity Listings

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 650N | 300 | 617113.7 | 629262.0 | 651.87 | 4174.54 | 0.54 | 5.41 | 2.16 | 4310.87 |
| 650N | 275 | 617136.5 | 629270.6 | 644.84 | 4176.04 | 0.44 | 5.25 | 2.07 | 4310.64 |
| 650N | 250 | 617161.2 | 629280.0 | 639.31 | 4177.52 | 0.43 | 5.10 | 1.77 | 4310.57 |
| 650N | 225 | 617184.5 | 629288.8 | 639.38 | 4177.81 | 0.42 | 4.84 | 1.50 | 4310.34 |
| 650N | 200 | 617209.7 | 629298.4 | 640.25 | 4177.87 | 0.42 | 4.55 | 1.42 | 4310.20 |
| 650N | 175 | 617233.0 | 629307.2 | 638.82 | 4178.01 | 0.41 | 4.37 | 1.53 | 4309.98 |
| 650N | 150 | 617255.0 | 629315.5 | 630.48 | 4179.35 | 0.40 | 4.40 | 1.67 | 4309.84 |
| 650N | 125 | 617278.0 | 629324.2 | 618.35 | 4181.71 | 0.39 | 4.42 | 1.71 | 4309.86 |
| 650N | 100 | 617300.5 | 629332.7 | 612.62 | 4182.96 | 0.39 | 4.35 | 1.51 | 4309.71 |
| 650N | 75 | 617324.5 | 629341.8 | 609.29 | 4183.80 | 0.38 | 4.24 | 1.38 | 4309.64 |
| 650N | 50 | 617348.7 | 629351.0 | 608.06 | 4184.19 | 0.37 | 4.10 | 1.33 | 4309.60 |
| 650N | 25 | 617373.0 | 629360.2 | 607.03 | 4184.51 | 0.37 | 3.97 | 1.32 | 4309.58 |
| 650N | 0 | 617398.4 | 629369.8 | 602.00 | 4185.56 | 0.36 | 3.91 | 1.38 | 4309.62 |
| 650N | -25 | 617424.7 | 629379.7 | 596.36 | 4186.64 | 0.35 | 3.86 | 1.45 | 4309.60 |
| 650N | -50 | 617446.5 | 629388.0 | 589.52 | 4187.92 | 0.34 | 3.85 | 1.33 | 4309.40 |
| 650N | -75 | 617470.0 | 629396.9 | 582.48 | 4189.28 | 0.34 | 3.85 | 1.32 | 4309.36 |
| 650N | -100 | 617493.0 | 629405.6 | 575.44 | 4190.63 | 0.33 | 3.85 | 1.38 | 4309.38 |
| 650N | -125 | 617515.1 | 629414.0 | 568.70 | 4191.95 | 0.32 | 3.85 | 1.38 | 4309.36 |
| 650N | -150 | 617538.8 | 629422.9 | 564.96 | 4192.76 | 0.32 | 3.81 | 1.39 | 4309.40 |
| 650N | -175 | 617564.4 | 629432.6 | 559.02 | 4193.91 | 0.31 | 3.79 | 1.45 | 4309.41 |
| 650N | -200 | 617589.1 | 629441.9 | 556.78 | 4194.48 | 0.30 | 3.72 | 1.37 | 4309.39 |
| 650N | -225 | 617615.6 | 629452.0 | 556.14 | 4194.74 | 0.29 | 3.63 | 1.43 | 4309.49 |
| 650N | -250 | 617642.0 | 629462.0 | 556.30 | 4194.80 | 0.29 | 3.54 | 1.45 | 4309.51 |
| 650N | -275 | 617666.0 | 629471.1 | 562.86 | 4193.47 | 0.28 | 3.39 | 1.63 | 4309.49 |
| 650N | -300 | 617692.0 | 629480.9 | 570.92 | 4191.75 | 0.27 | 3.25 | 1.96 | 4309.53 |
| 650N | -325 | 617714.7 | 629489.5 | 575.08 | 4190.64 | 0.26 | 3.19 | 2.48 | 4309.69 |
| 650N | -350 | 617729.4 | 629495.0 | 576.24 | 4190.09 | 0.26 | 3.16 | 2.89 | 4309.74 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 550N | 400 | 617065.1 | 629160.6 | 687.60 | 4167.53 | 0.53 | 5.20 | 1.99 | 4310.50 |
| 550N | 375 | 617086.2 | 629167.3 | 678.84 | 4169.23 | 0.52 | 5.20 | 1.99 | 4310.47 |
| 550N | 350 | 617108.5 | 629174.2 | 667.28 | 4171.56 | 0.51 | 5.24 | 1.98 | 4310.54 |
| 550N | 325 | 617127.6 | 629180.3 | 656.13 | 4173.65 | 0.51 | 5.32 | 2.06 | 4310.60 |
| 550N | 300 | 617146.7 | 629186.2 | 643.37 | 4176.28 | 0.51 | 5.46 | 1.78 | 4310.58 |
| 550N | 275 | 617169.9 | 629193.6 | 637.31 | 4177.62 | 0.50 | 5.31 | 1.74 | 4310.53 |
| 550N | 250 | 617193.6 | 629200.9 | 632.95 | 4178.59 | 0.49 | 5.13 | 1.61 | 4310.32 |
| 550N | 225 | 617218.0 | 629208.7 | 629.09 | 4179.42 | 0.49 | 4.95 | 1.49 | 4310.09 |
| 550N | 200 | 617243.4 | 629216.6 | 624.74 | 4180.25 | 0.48 | 4.80 | 1.44 | 4309.86 |
| 550N | 175 | 617269.0 | 629224.7 | 621.28 | 4180.97 | 0.48 | 4.64 | 1.40 | 4309.69 |
| 550N | 150 | 617294.1 | 629232.4 | 619.52 | 4181.43 | 0.47 | 4.46 | 1.30 | 4309.52 |
| 550N | 125 | 617318.8 | 629240.2 | 615.46 | 4182.22 | 0.46 | 4.36 | 1.34 | 4309.44 |
| 550N | 100 | 617341.4 | 629247.3 | 607.10 | 4183.93 | 0.46 | 4.30 | 1.30 | 4309.41 |
| 550N | 75 | 617366.5 | 629255.2 | 604.55 | 4184.50 | 0.45 | 4.24 | 1.28 | 4309.39 |
| 550N | 50 | 617391.9 | 629263.1 | 602.39 | 4185.03 | 0.45 | 4.11 | 1.22 | 4309.29 |
| 550N | 25 | 617419.1 | 629271.7 | 601.33 | 4185.30 | 0.44 | 3.97 | 1.33 | 4309.33 |
| 550N | 0 | 617433.8 | 629276.3 | 601.30 | 4185.47 | 0.42 | 3.86 | 1.38 | 4309.41 |
| 550N | -25 | 617456.4 | 629286.7 | 597.50 | 4186.36 | 0.42 | 3.83 | 1.31 | 4309.45 |
| 550N | -50 | 617479.3 | 629297.2 | 592.60 | 4187.29 | 0.41 | 3.79 | 1.37 | 4309.43 |
| 550N | -75 | 617503.3 | 629308.2 | 588.50 | 4188.11 | 0.41 | 3.73 | 1.45 | 4309.46 |
| 550N | -100 | 617528.9 | 629320.0 | 577.40 | 4190.31 | 0.40 | 3.78 | 1.48 | 4309.55 |
| 550N | -125 | 617558.1 | 629333.4 | 567.70 | 4192.06 | 0.39 | 3.80 | 1.61 | 4309.53 |
| 550N | -150 | 617585.9 | 629346.2 | 571.90 | 4191.25 | 0.38 | 3.71 | 1.64 | 4309.47 |
| 550N | -175 | 617608.9 | 629356.8 | 569.70 | 4191.76 | 0.37 | 3.55 | 1.67 | 4309.41 |
| 550N | -200 | 617634.3 | 629368.4 | 568.10 | 4192.01 | 0.36 | 3.47 | 1.81 | 4309.40 |
| 550N | -225 | 617656.6 | 629378.7 | 563.80 | 4193.02 | 0.35 | 3.45 | 1.89 | 4309.59 |
| 550N | -250 | 617679.6 | 629389.3 | 560.10 | 4193.77 | 0.34 | 3.42 | 2.03 | 4309.63 |
| 550N | -275 | 617703.5 | 629400.2 | 559.40 | 4193.88 | 0.33 | 3.35 | 2.13 | 4309.73 |
| 550N | -300 | 617726.2 | 629410.7 | 558.10 | 4193.99 | 0.33 | 3.30 | 2.26 | 4309.66 |
| 550N | -325 | 617750.1 | 629421.7 | 560.00 | 4193.47 | 0.32 | 3.22 | 2.60 | 4309.76 |
| 550N | -350 | 617770.1 | 629430.9 | 561.00 | 4192.99 | 0.31 | 3.16 | 3.06 | 4309.87 |
| 550N | -375 | 617786.0 | 629440.0 | 558.20 | 4193.39 | 0.30 | 3.15 | 3.22 | 4309.86 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 500N | 400 | 617079.4 | 629113.0 | 684.30 | 4168.15 | 0.56 | 5.21 | 2.37 | 4310.89 |
| 500N | 375 | 617102.2 | 629120.2 | 677.76 | 4169.44 | 0.56 | 5.08 | 2.24 | 4310.64 |
| 500N | 350 | 617127.6 | 629128.1 | 671.51 | 4170.73 | 0.55 | 4.93 | 2.32 | 4310.61 |
| 500N | 325 | 617145.7 | 629133.7 | 656.87 | 4173.59 | 0.55 | 5.16 | 2.03 | 4310.54 |
| 500N | 300 | 617169.6 | 629141.2 | 644.92 | 4176.07 | 0.54 | 5.11 | 1.90 | 4310.48 |
| 500N | 275 | 617196.5 | 629148.7 | 638.28 | 4177.47 | 0.53 | 5.07 | 1.89 | 4310.51 |
| 500N | 250 | 617216.6 | 629155.9 | 634.14 | 4178.27 | 0.53 | 4.96 | 1.79 | 4310.28 |
| 500N | 225 | 617241.4 | 629163.6 | 626.99 | 4179.69 | 0.52 | 4.89 | 1.63 | 4310.06 |
| 500N | 200 | 617264.4 | 629170.8 | 623.05 | 4180.44 | 0.52 | 4.76 | 1.49 | 4309.77 |
| 500N | 175 | 617288.7 | 629178.4 | 619.60 | 4181.10 | 0.51 | 4.62 | 1.33 | 4309.44 |
| 500N | 150 | 617312.0 | 629185.7 | 616.36 | 4181.83 | 0.50 | 4.50 | 1.30 | 4309.37 |
| 500N | 125 | 617336.4 | 629193.3 | 615.52 | 4182.05 | 0.50 | 4.33 | 1.32 | 4309.27 |
| 500N | 100 | 617360.2 | 629200.8 | 611.27 | 4182.85 | 0.49 | 4.25 | 1.36 | 4309.19 |
| 500N | 75 | 617385.3 | 629208.6 | 603.83 | 4184.32 | 0.49 | 4.22 | 1.29 | 4309.09 |
| 500N | 50 | 617408.8 | 629215.9 | 601.98 | 4184.78 | 0.48 | 4.11 | 1.26 | 4309.04 |
| 500N | 25 | 617431.2 | 629222.9 | 599.04 | 4185.37 | 0.47 | 4.06 | 1.31 | 4309.04 |
| 500N | 0 | 617454.8 | 629230.3 | 592.90 | 4186.69 | 0.47 | 4.00 | 1.32 | 4309.10 |
| 500N | -25 | 617477.0 | 629237.3 | 585.40 | 4188.32 | 0.46 | 4.01 | 1.42 | 4309.36 |
| 500N | -50 | 617502.5 | 629245.3 | 579.20 | 4189.59 | 0.46 | 3.98 | 1.56 | 4309.52 |
| 500N | -75 | 617527.3 | 629253.0 | 578.40 | 4189.87 | 0.45 | 3.87 | 1.67 | 4309.62 |
| 500N | -100 | 617554.1 | 629261.4 | 577.40 | 4190.08 | 0.44 | 3.76 | 1.69 | 4309.54 |
| 500N | -125 | 617577.3 | 629268.7 | 576.50 | 4190.20 | 0.44 | 3.78 | 1.83 | 4309.65 |
| 500N | -175 | 617619.8 | 629282.0 | 553.60 | 4194.44 | 0.43 | 3.85 | 2.08 | 4309.69 |
| 500N | -200 | 617642.9 | 629289.2 | 542.50 | 4196.25 | 0.42 | 3.95 | 2.44 | 4309.77 |
| 500N | -225 | 617668.4 | 629297.2 | 529.50 | 4198.66 | 0.42 | 3.99 | 2.55 | 4309.87 |
| 500N | -250 | 617695.4 | 629305.6 | 522.90 | 4200.11 | 0.41 | 3.95 | 2.63 | 4309.95 |
| 500N | -275 | 617722.6 | 629314.1 | 515.00 | 4201.25 | 0.40 | 4.00 | 3.03 | 4309.97 |
| 500N | -300 | 617746.1 | 629321.5 | 509.60 | 4202.33 | 0.44 | 4.00 | 2.96 | 4310.00 |
| 500N | -325 | 617770.5 | 629329.1 | 504.80 | 4203.23 | 0.39 | 3.95 | 3.07 | 4309.03 |
| 500N | -350 | 617794.0 | 629337.4 | 499.40 | 4204.22 | 0.38 | 3.97 | 3.11 | 4309.91 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 450N | 400 | 617079.2 | 629063.3 | 684.75 | 4169.12 | 0.60 | 5.22 | 1.72 | 4311.36 |
| 450N | 375 | 617103.9 | 629071.3 | 680.56 | 4169.78 | 0.60 | 5.18 | 1.72 | 4311.14 |
| 450N | 350 | 617130.2 | 629079.9 | 670.27 | 4171.60 | 0.59 | 5.15 | 1.77 | 4310.95 |
| 450N | 325 | 617150.4 | 629086.4 | 656.48 | 4174.22 | 0.58 | 5.19 | 1.67 | 4310.79 |
| 450N | 300 | 617170.6 | 629092.9 | 647.19 | 4176.05 | 0.58 | 5.15 | 1.58 | 4310.67 |
| 450N | 275 | 617192.1 | 629099.9 | 638.90 | 4177.67 | 0.57 | 5.17 | 1.50 | 4310.58 |
| 450N | 250 | 617216.0 | 629107.7 | 633.21 | 4178.75 | 0.57 | 5.11 | 1.44 | 4310.42 |
| 450N | 225 | 617239.7 | 629115.4 | 627.22 | 4179.92 | 0.56 | 5.01 | 1.45 | 4310.31 |
| 450N | 200 | 617263.7 | 629123.2 | 621.62 | 4180.98 | 0.56 | 4.91 | 1.56 | 4310.28 |
| 450N | 175 | 617290.9 | 629132.0 | 618.63 | 4181.62 | 0.55 | 4.73 | 1.58 | 4310.16 |
| 450N | 150 | 617314.2 | 629139.6 | 615.84 | 4182.12 | 0.54 | 4.67 | 1.49 | 4309.96 |
| 450N | 125 | 617338.9 | 629147.7 | 613.05 | 4182.74 | 0.54 | 4.46 | 1.42 | 4309.75 |
| 450N | 100 | 617362.4 | 629155.2 | 607.86 | 4183.78 | 0.53 | 4.43 | 1.41 | 4309.72 |
| 450N | 75 | 617387.6 | 629163.4 | 602.47 | 4184.78 | 0.52 | 4.37 | 1.44 | 4309.62 |
| 450N | 50 | 617411.4 | 629171.2 | 598.68 | 4185.59 | 0.52 | 4.29 | 1.43 | 4309.59 |
| 450N | 25 | 617436.1 | 629179.2 | 595.89 | 4186.16 | 0.52 | 4.23 | 1.45 | 4309.58 |
| 450N | 0 | 617469.8 | 629181.0 | 589.00 | 4187.53 | 0.50 | 4.08 | 1.64 | 4309.61 |
| 450N | -25 | 617495.1 | 629189.1 | 592.65 | 4187.25 | 0.50 | 3.87 | 1.40 | 4309.59 |
| 450N | -50 | 617518.8 | 629196.7 | 596.91 | 4186.50 | 0.50 | 3.69 | 1.61 | 4309.71 |
| 450N | -75 | 617542.0 | 629204.1 | 592.37 | 4187.49 | 0.49 | 3.65 | 1.64 | 4309.79 |
| 450N | -100 | 617566.3 | 629211.9 | 586.63 | 4188.56 | 0.48 | 3.63 | 1.70 | 4309.76 |
| 450N | -125 | 617587.7 | 629218.8 | 578.59 | 4190.09 | 0.48 | 3.66 | 1.71 | 4309.74 |
| 450N | -150 | 617611.4 | 629226.4 | 573.85 | 4191.05 | 0.47 | 3.63 | 1.75 | 4309.78 |
| 450N | -175 | 617635.4 | 629234.1 | 570.11 | 4191.49 | 0.47 | 3.68 | 1.96 | 4309.74 |
| 450N | -200 | 617656.1 | 629240.7 | 557.27 | 4193.95 | 0.46 | 3.70 | 2.04 | 4309.76 |
| 450N | -225 | 617676.5 | 629247.2 | 547.23 | 4195.85 | 0.46 | 3.76 | 2.22 | 4309.93 |
| 450N | -250 | 617700.7 | 629255.0 | 539.39 | 4197.24 | 0.45 | 3.82 | 2.26 | 4309.87 |
| 450N | -275 | 617728.1 | 629263.8 | 538.85 | 4197.45 | 0.44 | 3.72 | 2.21 | 4309.81 |
| 450N | -350 | 617794.3 | 629274.7 | 507.03 | 4203.00 | 0.43 | 3.93 | 2.57 | 4309.85 |
| 450N | -375 | 617810.6 | 629288.6 | 500.79 | 4204.03 | 0.42 | 3.94 | 2.90 | 4309.80 |
| 450N | -400 | 617838.2 | 629287.4 | 506.05 | 4203.35 | 0.42 | 3.92 | 2.56 | 4309.79 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 400N | 400 | 617095.1 | 629014.0 | 689.15 | 4168.53 | 0.64 | 5.05 | 1.68 | 4311.46 |
| 400N | 375 | 617119.4 | 629021.7 | 685.44 | 4169.10 | 0.63 | 4.84 | 1.84 | 4311.24 |
| 400N | 350 | 617143.9 | 629029.4 | 676.33 | 4170.71 | 0.63 | 4.83 | 1.75 | 4310.96 |
| 400N | 325 | 617167.8 | 629037.0 | 665.12 | 4172.73 | 0.62 | 4.88 | 1.75 | 4310.81 |
| 400N | 300 | 617191.1 | 629044.3 | 655.61 | 4174.53 | 0.62 | 4.90 | 1.68 | 4310.69 |
| 400N | 275 | 617215.8 | 629052.1 | 645.80 | 4176.53 | 0.61 | 4.86 | 1.63 | 4310.65 |
| 400N | 250 | 617239.6 | 629059.6 | 639.79 | 4177.70 | 0.60 | 4.82 | 1.56 | 4310.53 |
| 400N | 225 | 617263.9 | 629067.4 | 633.48 | 4178.82 | 0.60 | 4.76 | 1.60 | 4310.42 |
| 400N | 200 | 617287.4 | 629074.7 | 624.38 | 4180.40 | 0.59 | 4.75 | 1.75 | 4310.41 |
| 400N | 175 | 617311.7 | 629082.4 | 616.07 | 4181.98 | 0.59 | 4.73 | 1.82 | 4310.30 |
| 400N | 150 | 617335.0 | 629089.8 | 612.16 | 4182.80 | 0.58 | 4.63 | 1.76 | 4310.18 |
| 400N | 125 | 617358.4 | 629097.2 | 609.95 | 4183.35 | 0.57 | 4.49 | 1.60 | 4309.99 |
| 400N | 100 | 617383.1 | 629104.9 | 607.74 | 4183.78 | 0.57 | 4.36 | 1.56 | 4309.81 |
| 400N | 50 | 617433.3 | 629120.9 | 602.82 | 4184.99 | 0.56 | 4.12 | 1.38 | 4309.62 |
| 400N | 25 | 617459.2 | 629129.1 | 598.11 | 4185.99 | 0.55 | 4.05 | 1.46 | 4309.70 |
| 400N | 0 | 617483.9 | 629137.0 | 604.00 | 4184.78 | 0.55 | 3.88 | 1.54 | 4309.56 |
| 400N | -25 | 617513.6 | 629133.2 | 602.75 | 4184.95 | 0.55 | 3.73 | 1.59 | 4309.38 |
| 400N | -50 | 617534.9 | 629140.0 | 599.99 | 4185.55 | 0.54 | 3.65 | 1.63 | 4309.39 |
| 400N | -75 | 617559.2 | 629147.9 | 596.83 | 4186.24 | 0.53 | 3.59 | 1.84 | 4309.60 |
| 400N | -100 | 617582.2 | 629155.2 | 592.37 | 4187.00 | 0.53 | 3.55 | 1.88 | 4309.48 |
| 400N | -125 | 617605.8 | 629162.8 | 585.01 | 4188.42 | 0.52 | 3.56 | 1.87 | 4309.44 |
| 400N | -150 | 617628.4 | 629170.0 | 573.65 | 4190.65 | 0.52 | 3.64 | 1.88 | 4309.53 |
| 400N | -175 | 617651.4 | 629177.4 | 565.39 | 4192.31 | 0.51 | 3.67 | 1.91 | 4309.61 |
| 400N | -200 | 617675.9 | 629185.2 | 563.23 | 4192.74 | 0.50 | 3.60 | 1.89 | 4309.51 |
| 400N | -275 | 617746.0 | 629207.7 | 549.95 | 4195.34 | 0.49 | 3.53 | 2.13 | 4309.67 |
| 400N | -300 | 617766.7 | 629214.3 | 545.09 | 4196.16 | 0.49 | 3.53 | 2.16 | 4309.56 |
| 400N | -325 | 617792.7 | 629222.7 | 535.13 | 4198.05 | 0.48 | 3.61 | 2.16 | 4309.56 |
| 400N | -350 | 617813.0 | 629229.2 | 528.97 | 4199.23 | 0.47 | 3.63 | 2.21 | 4309.59 |
| 400N | -375 | 617838.8 | 629237.4 | 523.01 | 4200.46 | 0.46 | 3.65 | 2.26 | 4309.71 |
| 400N | -400 | 617861.6 | 629244.7 | 529.55 | 4199.07 | 0.46 | 3.45 | 2.63 | 4309.77 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 350N | 400 | 617130.1 | 628913.2 | 679.20 | 4170.57 | 0.68 | 5.25 | 1.39 | 4311.48 |
| 350N | 375 | 617153.9 | 628968.7 | 673.70 | 4171.68 | 0.68 | 4.97 | 1.42 | 4311.27 |
| 350N | 350 | 617178.1 | 628977.0 | 672.60 | 4171.85 | 0.67 | 4.72 | 1.63 | 4311.17 |
| 350N | 325 | 617200.9 | 628984.9 | 663.30 | 4173.60 | 0.66 | 4.74 | 1.55 | 4311.02 |
| 350N | 300 | 617226.2 | 628993.6 | 656.60 | 4174.82 | 0.66 | 4.63 | 1.68 | 4310.94 |
| 350N | 275 | 617248.0 | 629001.1 | 646.00 | 4176.82 | 0.65 | 4.64 | 1.70 | 4310.88 |
| 350N | 250 | 617271.6 | 629009.2 | 644.40 | 4177.21 | 0.64 | 4.55 | 1.56 | 4310.72 |
| 350N | 225 | 617295.7 | 629017.5 | 642.80 | 4177.49 | 0.64 | 4.39 | 1.68 | 4310.64 |
| 350N | 200 | 617318.4 | 629025.3 | 636.00 | 4178.64 | 0.63 | 4.36 | 1.62 | 4310.35 |
| 350N | 175 | 617341.5 | 629033.3 | 628.80 | 4179.89 | 0.62 | 4.36 | 1.65 | 4310.20 |
| 350N | 150 | 617362.3 | 629040.4 | 620.20 | 4181.51 | 0.62 | 4.36 | 1.67 | 4310.15 |
| 350N | 125 | 617385.4 | 629048.4 | 614.90 | 4182.65 | 0.61 | 4.31 | 1.66 | 4310.19 |
| 350N | 100 | 617409.0 | 629056.5 | 614.70 | 4182.73 | 0.60 | 4.15 | 1.50 | 4309.89 |
| 350N | 75 | 617432.6 | 629064.6 | 612.40 | 4183.27 | 0.60 | 4.05 | 1.46 | 4309.84 |
| 350N | 50 | 617456.1 | 629072.7 | 610.80 | 4183.67 | 0.59 | 3.94 | 1.51 | 4309.85 |
| 350N | 25 | 617479.6 | 629080.8 | 609.30 | 4184.02 | 0.58 | 3.83 | 1.48 | 4309.76 |
| 350N | 0 | 617503.1 | 629088.9 | 607.80 | 4184.30 | 0.58 | 3.74 | 1.58 | 4309.75 |
| 350N | -25 | 617531.0 | 629097.0 | 603.00 | 4185.21 | 0.57 | 3.68 | 1.62 | 4309.69 |
| 350N | -50 | 617554.0 | 629105.0 | 598.11 | 4186.13 | 0.56 | 3.65 | 1.61 | 4309.60 |
| 350N | -75 | 617578.0 | 629114.0 | 591.91 | 4187.19 | 0.56 | 3.69 | 1.79 | 4309.64 |
| 350N | -100 | 617601.0 | 629121.0 | 580.82 | 4189.33 | 0.55 | 3.70 | 1.90 | 4309.73 |
| 350N | -125 | 617624.0 | 629129.0 | 572.13 | 4190.89 | 0.54 | 3.73 | 2.03 | 4309.73 |
| 350N | -150 | 617647.0 | 629137.0 | 568.93 | 4191.64 | 0.54 | 3.68 | 1.92 | 4309.75 |
| 350N | -175 | 617670.0 | 629145.0 | 558.34 | 4193.67 | 0.53 | 3.76 | 2.07 | 4309.86 |
| 350N | -200 | 617694.0 | 629153.0 | 556.35 | 4194.25 | 0.52 | 3.69 | 2.01 | 4309.90 |
| 350N | -225 | 617718.0 | 629162.0 | 560.15 | 4193.64 | 0.51 | 3.53 | 1.96 | 4309.82 |
| 350N | -250 | 617742.0 | 629170.0 | 555.06 | 4194.45 | 0.50 | 3.50 | 2.01 | 4309.67 |
| 350N | -275 | 617767.0 | 629178.0 | 547.77 | 4195.96 | 0.49 | 3.53 | 1.95 | 4309.68 |
| 350N | -300 | 617790.0 | 629187.0 | 545.37 | 4196.26 | 0.49 | 3.50 | 2.10 | 4309.63 |
| 350N | -325 | 617813.0 | 629194.0 | 541.78 | 4196.84 | 0.48 | 3.56 | 2.15 | 4309.60 |
| 350N | -350 | 617836.0 | 629202.0 | 535.89 | 4198.00 | 0.47 | 3.57 | 2.21 | 4309.66 |
| 350N | -375 | 617860.0 | 629211.0 | 532.29 | 4198.65 | 0.46 | 3.58 | 2.27 | 4309.66 |
| 350N | -400 | 617884.0 | 629219.0 | 528.00 | 4199.27 | 0.46 | 3.62 | 2.49 | 4309.72 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 300N | 400 | 617146.2 | 628913.2 | 678.65 | 4170.61 | 0.72 | 5.07 | 1.64 | 4311.53 |
| 300N | 375 | 617170.3 | 628921.5 | 674.12 | 4171.48 | 0.71 | 4.92 | 1.72 | 4311.43 |
| 300N | 350 | 617192.1 | 628929.0 | 660.48 | 4174.04 | 0.71 | 5.06 | 1.75 | 4311.48 |
| 300N | 325 | 617216.8 | 628937.5 | 655.85 | 4175.05 | 0.70 | 4.91 | 1.67 | 4311.33 |
| 300N | 300 | 617242.8 | 628946.5 | 651.01 | 4175.93 | 0.69 | 4.78 | 1.80 | 4311.25 |
| 300N | 275 | 617271.3 | 628956.3 | 655.58 | 4174.93 | 0.69 | 4.71 | 1.66 | 4310.94 |
| 300N | 250 | 617294.8 | 628964.4 | 649.44 | 4176.36 | 0.68 | 4.46 | 1.54 | 4310.79 |
| 300N | 225 | 617319.2 | 628972.8 | 647.41 | 4176.72 | 0.67 | 4.22 | 1.64 | 4310.59 |
| 300N | 200 | 617343.2 | 628981.0 | 642.27 | 4177.53 | 0.67 | 4.15 | 1.60 | 4310.28 |
| 300N | 175 | 617367.2 | 628989.3 | 636.34 | 4178.72 | 0.66 | 4.11 | 1.62 | 4310.27 |
| 300N | 150 | 617391.1 | 628997.5 | 630.60 | 4179.77 | 0.65 | 4.06 | 1.64 | 4310.16 |
| 300N | 125 | 617413.8 | 629005.3 | 623.87 | 4181.09 | 0.65 | 4.04 | 1.63 | 4310.13 |
| 300N | 100 | 617438.4 | 629013.8 | 619.73 | 4181.95 | 0.64 | 3.97 | 1.57 | 4310.03 |
| 300N | 75 | 617462.3 | 629022.0 | 613.40 | 4183.15 | 0.63 | 3.94 | 1.57 | 4309.94 |
| 300N | 50 | 617487.2 | 629030.6 | 609.66 | 4183.89 | 0.63 | 3.87 | 1.62 | 4309.93 |
| 300N | 25 | 617501.1 | 629035.4 | 606.33 | 4184.46 | 0.62 | 3.85 | 1.72 | 4309.91 |
| 300N | 0 | 617520.1 | 629040.7 | 601.60 | 4185.38 | 0.62 | 3.83 | 1.68 | 4309.84 |
| 300N | -25 | 617544.0 | 629049.0 | 598.39 | 4186.08 | 0.61 | 3.76 | 1.76 | 4309.92 |
| 300N | -50 | 617567.0 | 629057.0 | 591.58 | 4187.34 | 0.60 | 3.76 | 1.94 | 4310.00 |
| 300N | -75 | 617592.0 | 629065.0 | 580.08 | 4189.40 | 0.60 | 3.73 | 2.20 | 4310.04 |
| 300N | -100 | 617616.0 | 629074.0 | 585.57 | 4188.60 | 0.59 | 3.63 | 1.99 | 4309.99 |
| 300N | -125 | 617640.0 | 629082.0 | 586.67 | 4188.43 | 0.58 | 3.58 | 1.99 | 4309.97 |
| 300N | -150 | 617665.0 | 629091.0 | 579.46 | 4189.92 | 0.57 | 3.57 | 1.97 | 4310.03 |
| 300N | -175 | 617688.0 | 629098.0 | 572.65 | 4191.35 | 0.56 | 3.52 | 1.95 | 4310.02 |
| 300N | -200 | 617708.0 | 629105.0 | 564.15 | 4193.14 | 0.56 | 3.47 | 1.92 | 4310.09 |
| 300N | -225 | 617732.0 | 629114.0 | 558.24 | 4194.44 | 0.55 | 3.46 | 1.90 | 4310.15 |
| 300N | -250 | 617757.0 | 629122.0 | 556.64 | 4194.83 | 0.54 | 3.39 | 1.93 | 4310.18 |
| 300N | -275 | 617782.0 | 629131.0 | 551.33 | 4195.78 | 0.53 | 3.38 | 1.90 | 4310.04 |
| 300N | -300 | 617806.0 | 629139.0 | 547.42 | 4196.78 | 0.52 | 3.32 | 1.79 | 4310.09 |
| 300N | -325 | 617830.0 | 629149.0 | 544.32 | 4197.39 | 0.52 | 3.31 | 1.87 | 4310.16 |
| 300N | -350 | 617852.0 | 629155.0 | 537.61 | 4198.69 | 0.51 | 3.34 | 1.95 | 4310.24 |
| 300N | -375 | 617877.0 | 629163.0 | 533.51 | 4199.22 | 0.50 | 3.33 | 2.13 | 4310.12 |
| 300N | -400 | 617896.0 | 629170.0 | 521.20 | 4201.59 | 0.49 | 3.41 | 2.07 | 4310.07 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 250N | 400 | 617154.0 | 628868.0 | 677.10 | 4171.27 | 0.75 | 5.18 | 1.40 | 4311.78 |
| 250N | 375 | 617178.0 | 628875.0 | 674.17 | 4171.96 | 0.74 | 4.97 | 1.38 | 4311.66 |
| 250N | 350 | 617202.0 | 628883.0 | 672.64 | 4172.29 | 0.74 | 4.79 | 1.38 | 4311.51 |
| 250N | 325 | 617226.0 | 628891.0 | 669.61 | 4172.96 | 0.73 | 4.60 | 1.40 | 4311.41 |
| 250N | 300 | 617249.0 | 628898.0 | 664.47 | 4173.94 | 0.73 | 4.51 | 1.41 | 4311.29 |
| 250N | 275 | 617273.0 | 628906.0 | 659.64 | 4174.91 | 0.72 | 4.42 | 1.43 | 4311.23 |
| 250N | 250 | 617297.0 | 628913.0 | 660.01 | 4174.86 | 0.72 | 4.23 | 1.53 | 4311.16 |
| 250N | 225 | 617321.0 | 628921.0 | 656.38 | 4175.49 | 0.71 | 4.13 | 1.57 | 4311.01 |
| 250N | 200 | 617345.0 | 628928.0 | 652.25 | 4176.28 | 0.71 | 4.05 | 1.58 | 4310.92 |
| 250N | 175 | 617368.0 | 628936.0 | 647.02 | 4177.28 | 0.70 | 4.00 | 1.56 | 4310.81 |
| 250N | 150 | 617392.0 | 628943.0 | 643.49 | 4177.89 | 0.69 | 3.92 | 1.64 | 4310.71 |
| 250N | 125 | 617418.0 | 628952.0 | 639.66 | 4178.47 | 0.69 | 3.84 | 1.77 | 4310.59 |
| 250N | 100 | 617442.0 | 628959.0 | 629.52 | 4180.36 | 0.68 | 3.87 | 1.65 | 4310.38 |
| 250N | 75 | 617466.0 | 628967.0 | 626.49 | 4181.00 | 0.68 | 3.80 | 1.65 | 4310.36 |
| 250N | 50 | 617490.0 | 628976.0 | 623.76 | 4181.41 | 0.67 | 3.71 | 1.70 | 4310.19 |
| 250N | 25 | 617513.0 | 628982.0 | 611.33 | 4183.46 | 0.66 | 3.80 | 1.84 | 4310.01 |
| 250N | 0 | 617538.9 | 628990.0 | 602.40 | 4185.16 | 0.66 | 3.81 | 1.91 | 4310.03 |
| 250N | -25 | 617568.9 | 629000.3 | 598.45 | 4185.96 | 0.66 | 3.73 | 2.01 | 4310.08 |
| 250N | -50 | 617593.7 | 629008.2 | 602.09 | 4185.46 | 0.65 | 3.56 | 1.93 | 4310.03 |
| 250N | -75 | 617617.4 | 629016.1 | 601.72 | 4185.56 | 0.64 | 3.46 | 2.14 | 4310.16 |
| 250N | -100 | 617641.2 | 629023.0 | 596.76 | 4186.59 | 0.64 | 3.44 | 2.22 | 4310.27 |
| 250N | -125 | 617664.9 | 629030.9 | 592.00 | 4187.42 | 0.63 | 3.41 | 2.21 | 4310.11 |
| 250N | -150 | 617687.7 | 629037.8 | 583.63 | 4189.04 | 0.63 | 3.44 | 2.18 | 4310.09 |
| 250N | -175 | 617711.4 | 629045.7 | 576.27 | 4190.48 | 0.62 | 3.45 | 2.15 | 4310.05 |
| 250N | -200 | 617734.2 | 629053.6 | 568.01 | 4192.10 | 0.62 | 3.48 | 2.12 | 4310.05 |
| 250N | -225 | 617757.0 | 629060.5 | 558.14 | 4194.06 | 0.62 | 3.54 | 2.11 | 4310.12 |
| 250N | -250 | 617779.7 | 629067.4 | 551.58 | 4195.37 | 0.61 | 3.56 | 2.15 | 4310.19 |
| 250N | -275 | 617803.5 | 629075.3 | 547.42 | 4196.39 | 0.60 | 3.54 | 2.01 | 4310.20 |
| 250N | -300 | 617829.2 | 629083.2 | 542.55 | 4197.33 | 0.59 | 3.52 | 2.00 | 4310.16 |
| 250N | -325 | 617853.0 | 629091.1 | 536.59 | 4198.54 | 0.59 | 3.53 | 2.00 | 4310.18 |
| 250N | -350 | 617877.7 | 629099.0 | 534.53 | 4198.95 | 0.58 | 3.48 | 2.06 | 4310.21 |
| 250N | -375 | 617900.6 | 629105.9 | 533.26 | 4199.16 | 0.58 | 3.42 | 2.22 | 4310.27 |
| 250N | -400 | 617925.3 | 629113.8 | 531.20 | 4199.40 | 0.57 | 3.37 | 2.48 | 4310.31 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 200N | 400 | 617172.4 | 628821.3 | 679.00 | 4170.99 | 0.77 | 5.07 | 1.48 | 4311.87 |
| 200N | 375 | 617195.6 | 628828.4 | 674.97 | 4171.90 | 0.78 | 4.91 | 1.40 | 4311.76 |
| 200N | 350 | 617218.7 | 628836.4 | 671.64 | 4172.62 | 0.78 | 4.76 | 1.36 | 4311.63 |
| 200N | 325 | 617244.9 | 628844.5 | 667.91 | 4173.44 | 0.77 | 4.60 | 1.33 | 4311.52 |
| 200N | 300 | 617268.1 | 628851.6 | 665.57 | 4173.97 | 0.77 | 4.45 | 1.39 | 4311.50 |
| 200N | 275 | 617292.3 | 628859.7 | 663.74 | 4174.34 | 0.76 | 4.30 | 1.38 | 4311.34 |
| 200N | 250 | 617317.5 | 628867.7 | 662.71 | 4174.66 | 0.75 | 4.14 | 1.24 | 4311.29 |
| 200N | 225 | 617340.7 | 628874.8 | 659.08 | 4175.21 | 0.75 | 4.05 | 1.54 | 4311.19 |
| 200N | 200 | 617365.9 | 628882.9 | 654.15 | 4176.25 | 0.74 | 3.98 | 1.40 | 4311.04 |
| 200N | 175 | 617390.1 | 628890.9 | 649.02 | 4177.22 | 0.73 | 3.93 | 1.39 | 4310.93 |
| 200N | 150 | 617415.2 | 628899.1 | 644.69 | 4178.00 | 0.73 | 3.86 | 1.43 | 4310.83 |
| 200N | 125 | 617440.4 | 628907.1 | 644.76 | 4177.89 | 0.72 | 3.72 | 1.65 | 4310.80 |
| 200N | 100 | 617464.6 | 628914.2 | 641.32 | 4178.41 | 0.72 | 3.65 | 1.80 | 4310.73 |
| 200N | 75 | 617487.8 | 628922.2 | 630.79 | 4180.55 | 0.71 | 3.70 | 1.70 | 4310.74 |
| 200N | 50 | 617512.0 | 628930.3 | 615.76 | 4183.21 | 0.71 | 3.71 | 1.99 | 4310.70 |
| 200N | 25 | 617546.2 | 628940.4 | 622.73 | 4181.91 | 0.70 | 3.54 | 1.98 | 4310.62 |
| 200N | 0 | 617552.8 | 628942.2 | 624.60 | 4181.13 | 0.70 | 3.49 | 2.33 | 4310.51 |
| 200N | -25 | 617576.0 | 628950.0 | 621.55 | 4181.87 | 0.69 | 3.43 | 2.24 | 4310.49 |
| 200N | -50 | 617591.2 | 628954.1 | 614.12 | 4183.06 | 0.69 | 3.47 | 2.54 | 4310.45 |
| 200N | -75 | 617624.5 | 628965.2 | 604.88 | 4184.98 | 0.68 | 3.46 | 2.40 | 4310.50 |
| 200N | -100 | 617648.7 | 628973.3 | 593.85 | 4187.13 | 0.68 | 3.51 | 2.38 | 4310.51 |
| 200N | -125 | 617675.0 | 628981.4 | 585.41 | 4188.73 | 0.67 | 3.53 | 2.35 | 4310.43 |
| 200N | -150 | 617696.2 | 628988.6 | 576.48 | 4190.43 | 0.67 | 3.57 | 2.39 | 4310.45 |
| 200N | -175 | 617722.5 | 628996.6 | 567.24 | 4191.97 | 0.66 | 3.61 | 2.66 | 4310.48 |
| 200N | -200 | 617746.7 | 629003.7 | 564.11 | 4192.79 | 0.65 | 3.56 | 2.50 | 4310.46 |
| 200N | -225 | 617770.0 | 629011.9 | 558.17 | 4193.98 | 0.65 | 3.56 | 2.43 | 4310.43 |
| 200N | -250 | 617792.2 | 629018.9 | 550.64 | 4195.62 | 0.64 | 3.59 | 2.30 | 4310.46 |
| 200N | -275 | 617817.6 | 629026.1 | 546.71 | 4196.56 | 0.64 | 3.56 | 2.31 | 4310.48 |
| 200N | -300 | 617839.8 | 629034.2 | 543.77 | 4197.32 | 0.63 | 3.52 | 2.04 | 4310.46 |
| 200N | -325 | 617865.1 | 629042.2 | 540.74 | 4197.98 | 0.63 | 3.48 | 1.98 | 4310.43 |
| 200N | -350 | 617888.3 | 629049.4 | 535.50 | 4198.99 | 0.62 | 3.48 | 2.04 | 4310.46 |
| 200N | -375 | 617914.6 | 629057.5 | 534.07 | 4199.30 | 0.62 | 3.42 | 2.03 | 4310.42 |
| 200N | -400 | 617939.8 | 629065.6 | 533.33 | 4199.47 | 0.61 | 3.35 | 2.24 | 4310.58 |
| 200N | -425 | 617961.0 | 629072.0 | 532.70 | 4199.21 | 0.60 | 3.29 | 2.67 | 4310.55 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 150N | 400 | 617183.2 | 628745.8 | 682.65 | 4170.17 | 0.85 | 5.02 | 1.56 | 4311.90 |
| 150N | 375 | 617207.1 | 628754.6 | 678.13 | 4171.13 | 0.84 | 4.93 | 1.58 | 4311.87 |
| 150N | 350 | 617231.0 | 628763.5 | 674.32 | 4171.94 | 0.84 | 4.77 | 1.51 | 4311.70 |
| 150N | 300 | 617278.0 | 628780.9 | 667.49 | 4173.49 | 0.82 | 4.50 | 1.45 | 4311.55 |
| 150N | 275 | 617301.2 | 628789.5 | 664.67 | 4174.09 | 0.82 | 4.37 | 1.45 | 4311.47 |
| 150N | 250 | 617324.2 | 628798.0 | 662.33 | 4174.55 | 0.81 | 4.24 | 1.37 | 4311.25 |
| 150N | 225 | 617347.6 | 628806.7 | 660.74 | 4174.87 | 0.80 | 4.11 | 1.42 | 4311.17 |
| 150N | 200 | 617371.8 | 628815.6 | 658.43 | 4175.34 | 0.80 | 3.99 | 1.48 | 4311.12 |
| 150N | 175 | 617395.1 | 628824.3 | 653.41 | 4176.29 | 0.79 | 3.94 | 1.42 | 4310.96 |
| 150N | 150 | 617418.1 | 628832.8 | 648.80 | 4177.23 | 0.78 | 3.84 | 1.40 | 4310.84 |
| 150N | 125 | 617441.9 | 628841.6 | 645.68 | 4177.75 | 0.78 | 3.80 | 1.45 | 4310.78 |
| 150N | 100 | 617465.6 | 628850.4 | 643.27 | 4178.14 | 0.77 | 3.71 | 1.56 | 4310.71 |
| 150N | 75 | 617488.1 | 628858.7 | 636.65 | 4179.27 | 0.76 | 3.70 | 1.77 | 4310.73 |
| 150N | 50 | 617514.9 | 628868.7 | 628.34 | 4180.85 | 0.76 | 3.69 | 1.84 | 4310.73 |
| 150N | 25 | 617541.4 | 628878.5 | 631.62 | 4180.20 | 0.75 | 3.52 | 1.94 | 4310.65 |
| 150N | 0 | 617564.2 | 628886.9 | 638.10 | 4178.94 | 0.74 | 3.35 | 2.18 | 4310.73 |
| 150N | -25 | 617587.0 | 628896.0 | 636.32 | 4179.39 | 0.74 | 3.28 | 2.18 | 4310.76 |
| 150N | -50 | 617609.2 | 628904.4 | 629.88 | 4180.56 | 0.73 | 3.27 | 2.34 | 4310.79 |
| 150N | -75 | 617631.5 | 628912.7 | 622.45 | 4181.96 | 0.73 | 3.28 | 2.35 | 4310.76 |
| 150N | -100 | 617653.7 | 628921.1 | 614.31 | 4183.37 | 0.72 | 3.29 | 2.50 | 4310.72 |
| 150N | -125 | 617676.0 | 628929.4 | 607.08 | 4184.67 | 0.71 | 3.30 | 2.51 | 4310.61 |
| 150N | -150 | 617698.2 | 628937.7 | 595.34 | 4187.03 | 0.71 | 3.36 | 2.47 | 4310.67 |
| 150N | -175 | 617721.5 | 628947.1 | 586.51 | 4188.73 | 0.70 | 3.39 | 2.37 | 4310.55 |
| 150N | -200 | 617744.7 | 628955.5 | 577.17 | 4190.43 | 0.70 | 3.43 | 2.40 | 4310.49 |
| 150N | -225 | 617766.0 | 628963.8 | 567.63 | 4192.35 | 0.69 | 3.49 | 2.38 | 4310.56 |
| 150N | -250 | 617790.2 | 628973.2 | 557.90 | 4194.35 | 0.68 | 3.50 | 2.32 | 4310.59 |
| 150N | -275 | 617813.6 | 628981.6 | 549.96 | 4196.10 | 0.68 | 3.54 | 2.12 | 4310.61 |
| 150N | -300 | 617837.8 | 628990.9 | 543.83 | 4197.42 | 0.67 | 3.52 | 2.02 | 4310.62 |
| 150N | -325 | 617862.1 | 629000.2 | 540.79 | 4197.99 | 0.67 | 3.54 | 2.05 | 4310.63 |
| 150N | -350 | 617886.3 | 629009.6 | 540.16 | 4198.14 | 0.66 | 3.46 | 2.10 | 4310.61 |
| 150N | -375 | 617910.6 | 629018.9 | 533.82 | 4199.51 | 0.65 | 3.48 | 2.03 | 4310.67 |
| 150N | -400 | 617936.8 | 629028.3 | 533.69 | 4199.56 | 0.65 | 3.39 | 2.07 | 4310.65 |
| 150N | -425 | 617956.0 | 629032.0 | 533.35 | 4199.55 | 0.64 | 3.33 | 2.20 | 4310.63 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 100N | 400 | 617200.5 | 628699.1 | 687.70 | 4169.18 | 0.89 | 4.91 | 1.69 | 4311.94 |
| 100N | 375 | 617223.4 | 628707.6 | 679.10 | 4170.98 | 0.88 | 4.88 | 1.61 | 4311.93 |
| 100N | 350 | 617245.8 | 628715.9 | 674.10 | 4172.06 | 0.88 | 4.77 | 1.51 | 4311.81 |
| 100N | 325 | 617269.7 | 628724.7 | 670.00 | 4173.00 | 0.87 | 4.64 | 1.43 | 4311.73 |
| 100N | 300 | 617293.1 | 628733.4 | 667.40 | 4173.65 | 0.86 | 4.49 | 1.45 | 4311.73 |
| 100N | 275 | 617316.2 | 628741.9 | 665.20 | 4174.06 | 0.86 | 4.35 | 1.38 | 4311.50 |
| 100N | 250 | 617340.2 | 628750.8 | 662.60 | 4174.67 | 0.85 | 4.23 | 1.36 | 4311.44 |
| 100N | 225 | 617363.3 | 628759.4 | 659.40 | 4175.28 | 0.84 | 4.13 | 1.34 | 4311.30 |
| 100N | 200 | 617386.6 | 628768.0 | 657.00 | 4175.80 | 0.83 | 4.02 | 1.36 | 4311.24 |
| 100N | 175 | 617410.6 | 628776.9 | 654.50 | 4176.23 | 0.83 | 3.92 | 1.38 | 4311.10 |
| 100N | 150 | 617434.5 | 628785.7 | 649.40 | 4177.22 | 0.82 | 3.86 | 1.38 | 4311.02 |
| 100N | 125 | 617458.8 | 628794.7 | 645.40 | 4177.98 | 0.81 | 3.79 | 1.40 | 4310.93 |
| 100N | 100 | 617482.4 | 628803.5 | 642.20 | 4178.58 | 0.81 | 3.70 | 1.48 | 4310.81 |
| 100N | 75 | 617508.7 | 628813.2 | 635.90 | 4179.75 | 0.80 | 3.58 | 1.68 | 4310.89 |
| 100N | 50 | 617534.7 | 628822.9 | 645.60 | 4177.89 | 0.79 | 3.44 | 1.78 | 4310.89 |
| 100N | 25 | 617558.1 | 628831.5 | 646.80 | 4177.57 | 0.78 | 3.33 | 2.02 | 4310.92 |
| 100N | 0 | 617581.5 | 628840.2 | 645.00 | 4177.90 | 0.78 | 3.27 | 2.24 | 4311.06 |
| 100N | -25 | 617617.8 | 628862.8 | 635.72 | 4179.57 | 0.78 | 3.23 | 2.41 | 4311.04 |
| 100N | -50 | 617641.6 | 628870.4 | 628.64 | 4180.95 | 0.77 | 3.22 | 2.54 | 4311.13 |
| 100N | -75 | 617685.3 | 628887.1 | 621.76 | 4182.08 | 0.76 | 3.15 | 2.87 | 4311.16 |
| 100N | -100 | 617707.1 | 628894.8 | 613.08 | 4183.73 | 0.75 | 3.17 | 2.86 | 4311.11 |
| 100N | -125 | 617726.8 | 628901.4 | 602.20 | 4185.78 | 0.75 | 3.23 | 2.78 | 4310.99 |
| 100N | -150 | 617749.6 | 628910.1 | 592.63 | 4187.60 | 0.74 | 3.26 | 2.70 | 4310.85 |
| 100N | -175 | 617774.4 | 628918.8 | 586.25 | 4188.83 | 0.74 | 3.25 | 2.67 | 4310.80 |
| 100N | -225 | 617818.9 | 628935.1 | 569.79 | 4192.03 | 0.72 | 3.31 | 2.51 | 4310.64 |
| 100N | -250 | 617841.6 | 628942.8 | 558.21 | 4194.29 | 0.72 | 3.40 | 2.47 | 4310.64 |
| 100N | -275 | 617864.4 | 628951.4 | 549.33 | 4196.09 | 0.71 | 3.45 | 2.30 | 4310.60 |
| 100N | -300 | 617887.2 | 628959.1 | 550.35 | 4196.05 | 0.71 | 3.35 | 2.22 | 4310.58 |
| 100N | -325 | 617909.9 | 628967.8 | 542.57 | 4197.25 | 0.70 | 3.39 | 2.48 | 4310.55 |
| 100N | -350 | 617934.7 | 628976.4 | 535.59 | 4198.84 | 0.69 | 3.42 | 2.27 | 4310.57 |
| 100N | -375 | 617957.4 | 628985.1 | 528.62 | 4200.33 | 0.69 | 3.41 | 2.20 | 4310.60 |
| 100N | -400 | 617981.2 | 628992.8 | 527.64 | 4200.78 | 0.68 | 3.35 | 2.02 | 4310.62 |
| 100N | -425 | 618000.0 | 628996.0 | 527.26 | 4200.79 | 0.67 | 3.35 | 2.20 | 4310.83 |
| 100N | -450 | 618019.0 | 629003.0 | 523.28 | 4201.43 | 0.67 | 3.35 | 2.36 | 4311.74 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 50N | 400 | 617216.8 | 628640.0 | 689.74 | 4168.78 | 0.93 | 4.85 | 1.79 | 4312.01 |
| 50N | 375 | 617239.9 | 628649.4 | 681.57 | 4170.40 | 0.92 | 4.81 | 1.74 | 4311.93 |
| 50N | 350 | 617264.3 | 628659.4 | 674.00 | 4171.99 | 0.91 | 4.75 | 1.64 | 4311.87 |
| 50N | 325 | 617288.8 | 628669.4 | 670.32 | 4172.84 | 0.91 | 4.61 | 1.60 | 4311.82 |
| 50N | 300 | 617312.5 | 628679.1 | 667.35 | 4173.50 | 0.90 | 4.47 | 1.50 | 4311.64 |
| 50N | 275 | 617336.2 | 628688.8 | 664.18 | 4174.23 | 0.90 | 4.34 | 1.41 | 4311.53 |
| 50N | 250 | 617359.0 | 628698.1 | 661.31 | 4174.83 | 0.89 | 4.23 | 1.37 | 4311.40 |
| 50N | 225 | 617382.9 | 628707.8 | 658.64 | 4175.43 | 0.87 | 4.12 | 1.33 | 4311.31 |
| 50N | 200 | 617407.4 | 628717.8 | 655.96 | 4175.92 | 0.87 | 4.01 | 1.34 | 4311.16 |
| 50N | 175 | 617432.6 | 628728.1 | 652.49 | 4176.58 | 0.86 | 3.91 | 1.35 | 4311.04 |
| 50N | 150 | 617457.1 | 628738.0 | 648.12 | 4177.51 | 0.85 | 3.85 | 1.38 | 4311.07 |
| 50N | 125 | 617481.1 | 628748.7 | 646.95 | 4177.78 | 0.85 | 3.73 | 1.37 | 4310.99 |
| 50N | 100 | 617505.8 | 628758.0 | 644.08 | 4178.32 | 0.84 | 3.65 | 1.49 | 4310.99 |
| 50N | 75 | 617529.7 | 628767.7 | 647.40 | 4177.73 | 0.83 | 3.50 | 1.54 | 4310.94 |
| 50N | 50 | 617553.5 | 628777.4 | 650.63 | 4177.01 | 0.83 | 3.36 | 1.83 | 4311.01 |
| 50N | 25 | 617577.3 | 628787.2 | 652.96 | 4176.40 | 0.82 | 3.25 | 2.19 | 4311.10 |
| 50N | 0 | 617600.4 | 628796.6 | 652.30 | 4176.39 | 0.81 | 3.18 | 2.54 | 4311.23 |
| 50N | -25 | 617621.1 | 628805.6 | 642.72 | 4178.27 | 0.80 | 3.20 | 2.38 | 4311.08 |
| 50N | -50 | 617644.4 | 628816.1 | 631.58 | 4180.40 | 0.80 | 3.24 | 2.37 | 4311.04 |
| 50N | -75 | 617670.9 | 628827.9 | 628.44 | 4180.76 | 0.79 | 3.18 | 2.65 | 4311.00 |
| 50N | -100 | 617689.6 | 628836.2 | 618.02 | 4182.74 | 0.78 | 3.23 | 2.66 | 4310.98 |
| 50N | -125 | 617708.7 | 628844.9 | 607.38 | 4184.96 | 0.77 | 3.28 | 2.43 | 4310.91 |
| 50N | -150 | 617732.9 | 628855.8 | 596.94 | 4186.93 | 0.77 | 3.32 | 2.42 | 4310.85 |
| 50N | -175 | 617756.9 | 628866.6 | 589.90 | 4188.16 | 0.76 | 3.32 | 2.47 | 4310.74 |
| 50N | -200 | 617781.7 | 628877.6 | 580.46 | 4189.98 | 0.75 | 3.35 | 2.53 | 4310.79 |
| 50N | -225 | 617805.1 | 628888.2 | 574.54 | 4191.22 | 0.74 | 3.35 | 2.44 | 4310.76 |
| 50N | -250 | 617827.6 | 628898.2 | 567.20 | 4192.67 | 0.73 | 3.37 | 2.38 | 4310.71 |
| 50N | -275 | 617851.6 | 628909.0 | 563.16 | 4193.41 | 0.73 | 3.33 | 2.46 | 4310.70 |
| 50N | -300 | 617876.3 | 628920.1 | 559.72 | 4193.93 | 0.72 | 3.30 | 2.64 | 4310.68 |
| 50N | -325 | 617896.8 | 628929.3 | 550.88 | 4195.70 | 0.71 | 3.35 | 2.53 | 4310.65 |
| 50N | -350 | 617917.1 | 628938.4 | 539.66 | 4197.90 | 0.70 | 3.45 | 2.42 | 4310.62 |
| 50N | -375 | 617939.7 | 628948.6 | 531.22 | 4199.49 | 0.70 | 3.51 | 2.51 | 4310.70 |
| 50N | -400 | 617961.4 | 628958.2 | 521.98 | 4201.37 | 0.67 | 3.59 | 2.42 | 4310.73 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0 | 350 | 617288.7 | 628599.6 | 674.10 | 4172.11 | 0.97 | 4.68 | 1.65 | 4312.01 |
| 0 | 325 | 617312.1 | 628610.0 | 670.81 | 4172.82 | 0.96 | 4.54 | 1.53 | 4311.80 |
| 0 | 300 | 617335.6 | 628620.6 | 668.73 | 4173.31 | 0.95 | 4.39 | 1.49 | 4311.67 |
| 0 | 275 | 617357.9 | 628630.6 | 664.94 | 4174.15 | 0.94 | 4.29 | 1.40 | 4311.58 |
| 0 | 250 | 617382.3 | 628641.5 | 663.16 | 4174.53 | 0.93 | 4.15 | 1.38 | 4311.44 |
| 0 | 225 | 617405.6 | 628654.0 | 660.07 | 4175.16 | 0.93 | 4.05 | 1.34 | 4311.32 |
| 0 | 200 | 617429.8 | 628662.8 | 656.59 | 4175.92 | 0.92 | 3.96 | 1.34 | 4311.29 |
| 0 | 175 | 617453.3 | 628673.3 | 653.80 | 4176.54 | 0.91 | 3.87 | 1.35 | 4311.28 |
| 0 | 150 | 617479.2 | 628684.9 | 650.92 | 4177.24 | 0.90 | 3.78 | 1.33 | 4311.29 |
| 0 | 125 | 617503.3 | 628695.7 | 648.33 | 4177.77 | 0.89 | 3.69 | 1.40 | 4311.28 |
| 0 | 100 | 617527.2 | 628706.4 | 649.05 | 4177.62 | 0.88 | 3.57 | 1.44 | 4311.17 |
| 0 | 50 | 617573.4 | 628727.1 | 653.88 | 4176.66 | 0.87 | 3.32 | 1.81 | 4311.28 |
| 0 | 25 | 617597.1 | 628737.7 | 655.79 | 4176.11 | 0.86 | 3.21 | 2.21 | 4311.39 |
| 0 | 0 | 617620.2 | 628748.1 | 660.50 | 4174.68 | 0.85 | 3.10 | 2.86 | 4311.40 |
| 0 | -25 | 617645.2 | 628757.4 | 646.31 | 4177.33 | 0.84 | 3.15 | 2.87 | 4311.32 |
| 0 | -50 | 617665.3 | 628766.4 | 633.01 | 4180.06 | 0.84 | 3.21 | 2.61 | 4311.24 |
| 0 | -75 | 617688.3 | 628776.7 | 622.02 | 4182.21 | 0.83 | 3.25 | 2.66 | 4311.30 |
| 0 | -100 | 617711.1 | 628787.1 | 612.12 | 4184.09 | 0.82 | 3.28 | 2.52 | 4311.12 |
| 0 | -125 | 617733.1 | 628797.0 | 604.32 | 4185.51 | 0.81 | 3.29 | 2.57 | 4311.05 |
| 0 | -150 | 617753.9 | 628806.4 | 595.43 | 4187.35 | 0.80 | 3.33 | 2.37 | 4310.97 |
| 0 | -175 | 617777.0 | 628816.9 | 589.53 | 4188.50 | 0.80 | 3.32 | 2.40 | 4310.98 |
| 0 | -200 | 617799.0 | 628826.8 | 585.13 | 4189.34 | 0.79 | 3.29 | 2.44 | 4310.95 |
| 0 | -225 | 617819.6 | 628836.1 | 578.53 | 4190.63 | 0.78 | 3.31 | 2.38 | 4310.90 |
| 0 | -250 | 617843.8 | 628847.1 | 571.04 | 4192.19 | 0.77 | 3.32 | 2.29 | 4310.81 |
| 0 | -275 | 617865.4 | 628856.7 | 568.14 | 4192.69 | 0.77 | 3.28 | 2.33 | 4310.83 |
| 0 | -300 | 617889.6 | 628867.7 | 562.14 | 4193.81 | 0.76 | 3.28 | 2.39 | 4310.80 |
| 0 | -325 | 617910.2 | 628876.9 | 553.15 | 4195.51 | 0.76 | 3.34 | 2.45 | 4310.87 |
| 0 | -350 | 617930.7 | 628886.2 | 541.25 | 4197.71 | 0.75 | 3.44 | 2.54 | 4310.90 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 50S | 350 | 617309.4 | 628553.4 | 671.60 | 4172.44 | 1.00 | 4.66 | 1.78 | 4311.98 |
| 50S | 325 | 617333.0 | 628564.0 | 668.79 | 4173.43 | 1.00 | 4.52 | 1.43 | 4311.96 |
| 50S | 300 | 617355.7 | 628574.2 | 667.97 | 4173.68 | 0.99 | 4.35 | 1.43 | 4311.84 |
| 50S | 275 | 617378.4 | 628584.4 | 664.96 | 4174.32 | 0.98 | 4.24 | 1.33 | 4311.67 |
| 50S | 250 | 617401.0 | 628594.5 | 662.34 | 4174.97 | 0.97 | 4.14 | 1.24 | 4311.61 |
| 50S | 225 | 617423.6 | 628604.6 | 659.53 | 4175.59 | 0.96 | 4.04 | 1.20 | 4311.51 |
| 50S | 200 | 617446.2 | 628614.7 | 656.91 | 4176.22 | 0.96 | 3.95 | 1.13 | 4311.47 |
| 50S | 175 | 617469.7 | 628625.3 | 654.30 | 4176.86 | 0.95 | 3.86 | 1.07 | 4311.44 |
| 50S | 150 | 617492.2 | 628635.4 | 652.38 | 4177.34 | 0.94 | 3.76 | 1.03 | 4311.39 |
| 50S | 125 | 617515.9 | 628646.0 | 650.57 | 4177.66 | 0.93 | 3.67 | 1.14 | 4311.37 |
| 50S | 100 | 617540.5 | 628657.0 | 649.25 | 4178.02 | 0.92 | 3.57 | 1.16 | 4311.38 |
| 50S | 75 | 617565.7 | 628668.3 | 652.24 | 4177.39 | 0.91 | 3.46 | 1.29 | 4311.34 |
| 50S | 50 | 617589.2 | 628678.8 | 655.22 | 4176.82 | 0.90 | 3.30 | 1.45 | 4311.36 |
| 50S | 25 | 617612.8 | 628689.4 | 655.11 | 4176.79 | 0.90 | 3.22 | 1.77 | 4311.54 |
| 50S | 0 | 617640.9 | 628701.9 | 656.40 | 4175.82 | 0.89 | 3.12 | 2.59 | 4311.53 |
| 50S | -25 | 617664.7 | 628712.6 | 649.50 | 4176.83 | 0.88 | 3.24 | 2.80 | 4311.51 |
| 50S | -50 | 617680.7 | 628719.8 | 639.00 | 4178.91 | 0.87 | 3.22 | 2.68 | 4311.37 |
| 50S | -75 | 617700.1 | 628728.4 | 625.89 | 4181.42 | 0.87 | 3.24 | 2.69 | 4311.33 |
| 50S | -100 | 617719.2 | 628737.0 | 615.39 | 4183.62 | 0.86 | 3.27 | 2.47 | 4311.27 |
| 50S | -125 | 617742.3 | 628747.3 | 605.98 | 4185.44 | 0.85 | 3.30 | 2.47 | 4311.26 |
| 50S | -150 | 617765.6 | 628758.8 | 597.18 | 4187.09 | 0.84 | 3.32 | 2.48 | 4311.20 |
| 50S | -175 | 617788.2 | 628767.9 | 590.08 | 4188.46 | 0.83 | 3.33 | 2.44 | 4311.13 |
| 50S | -200 | 617811.0 | 628778.1 | 584.67 | 4189.61 | 0.83 | 3.32 | 2.32 | 4311.12 |
| 50S | -225 | 617835.4 | 628789.1 | 583.47 | 4189.78 | 0.82 | 3.25 | 2.44 | 4311.06 |
| 50S | -250 | 617858.1 | 628799.2 | 579.37 | 4190.55 | 0.81 | 3.22 | 2.49 | 4311.03 |
| 50S | -275 | 617878.5 | 628808.3 | 568.86 | 4192.58 | 0.80 | 3.29 | 2.41 | 4310.98 |
| 50S | -300 | 617902.6 | 628819.2 | 558.76 | 4194.56 | 0.79 | 3.34 | 2.43 | 4311.04 |
| 50S | -325 | 617924.1 | 628828.8 | 550.75 | 4196.07 | 0.79 | 3.38 | 2.47 | 4311.05 |
| 50S | -350 | 617948.2 | 628839.6 | 543.35 | 4197.47 | 0.78 | 3.41 | 2.53 | 4311.07 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 100S | 350 | 617325.0 | 628528.8 | 668.10 | 4173.27 | 0.98 | 4.66 | 1.76 | 4312.08 |
| 100S | 325 | 617349.0 | 628534.9 | 664.40 | 4174.20 | 0.97 | 4.55 | 1.59 | 4312.00 |
| 100S | 300 | 617372.4 | 628544.7 | 663.50 | 4174.47 | 0.97 | 4.38 | 1.54 | 4311.87 |
| 100S | 275 | 617397.5 | 628553.2 | 662.30 | 4174.68 | 0.96 | 4.23 | 1.53 | 4311.68 |
| 100S | 250 | 617430.6 | 628562.0 | 659.90 | 4175.17 | 0.96 | 4.26 | 1.52 | 4311.67 |
| 100S | 225 | 617444.6 | 628571.1 | 657.20 | 4175.87 | 0.96 | 4.02 | 1.45 | 4311.57 |
| 100S | 200 | 617467.8 | 628579.9 | 655.00 | 4176.36 | 0.95 | 3.92 | 1.46 | 4311.53 |
| 100S | 175 | 617491.1 | 628588.7 | 652.80 | 4176.82 | 0.95 | 3.83 | 1.44 | 4311.47 |
| 100S | 125 | 617539.9 | 628607.1 | 650.30 | 4177.43 | 0.94 | 3.63 | 1.49 | 4311.41 |
| 100S | 100 | 617564.2 | 628616.3 | 650.50 | 4177.37 | 0.94 | 3.52 | 1.53 | 4311.31 |
| 100S | 75 | 617588.5 | 628625.5 | 650.80 | 4177.34 | 0.94 | 3.41 | 1.64 | 4311.34 |
| 100S | 50 | 617612.8 | 628634.0 | 652.80 | 4176.94 | 0.93 | 3.30 | 1.79 | 4311.37 |
| 100S | 25 | 617637.0 | 628643.9 | 653.90 | 4176.57 | 0.93 | 3.21 | 2.10 | 4311.43 |
| 100S | 0 | 617660.3 | 628652.7 | 652.30 | 4176.70 | 0.92 | 3.15 | 2.41 | 4311.49 |
| 100S | -25 | 617682.5 | 628661.1 | 643.68 | 4178.19 | 0.92 | 3.20 | 2.58 | 4311.50 |
| 100S | -50 | 617702.0 | 628668.5 | 631.46 | 4180.63 | 0.92 | 3.24 | 2.50 | 4311.49 |
| 100S | -75 | 617724.3 | 628676.9 | 619.05 | 4182.64 | 0.92 | 3.29 | 2.69 | 4311.30 |
| 100S | -100 | 617747.7 | 628685.6 | 609.63 | 4184.64 | 0.91 | 3.31 | 2.50 | 4311.28 |
| 100S | -125 | 617771.8 | 628694.9 | 604.31 | 4185.66 | 0.91 | 3.29 | 2.46 | 4311.19 |
| 100S | -150 | 617795.5 | 628703.9 | 597.20 | 4186.98 | 0.91 | 3.29 | 2.51 | 4311.16 |
| 100S | -175 | 617817.6 | 628712.2 | 587.58 | 4189.02 | 0.90 | 3.29 | 2.39 | 4311.24 |
| 100S | -200 | 617841.3 | 628721.2 | 581.67 | 4190.04 | 0.90 | 3.33 | 2.54 | 4311.21 |
| 100S | -225 | 617866.7 | 628730.8 | 579.75 | 4190.31 | 0.90 | 3.30 | 2.60 | 4311.17 |
| 100S | -250 | 617890.3 | 628739.8 | 569.03 | 4192.21 | 0.89 | 3.36 | 2.68 | 4311.08 |
| 100S | -275 | 617915.0 | 628749.1 | 562.52 | 4193.59 | 0.89 | 3.36 | 2.61 | 4311.09 |
| 100S | -300 | 617939.5 | 628758.4 | 554.50 | 4195.11 | 0.89 | 3.40 | 2.66 | 4311.12 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 150S | 350 | 617343.0 | 628479.0 | 661.35 | 4174.47 | 1.00 | 4.67 | 1.95 | 4312.18 |
| 150S | 325 | 617366.0 | 628488.0 | 659.65 | 4175.03 | 1.00 | 4.61 | 1.70 | 4312.10 |
| 150S | 300 | 617390.0 | 628497.0 | 657.84 | 4175.49 | 1.00 | 4.46 | 1.61 | 4311.96 |
| 150S | 275 | 617414.0 | 628506.0 | 656.64 | 4175.82 | 1.00 | 4.31 | 1.53 | 4311.83 |
| 150S | 250 | 617439.0 | 628515.0 | 655.24 | 4176.18 | 0.99 | 4.17 | 1.46 | 4311.67 |
| 150S | 225 | 617463.0 | 628525.0 | 653.23 | 4176.69 | 0.99 | 4.06 | 1.40 | 4311.61 |
| 150S | 200 | 617486.0 | 628533.0 | 651.63 | 4177.16 | 0.99 | 3.95 | 1.34 | 4311.62 |
| 150S | 175 | 617510.0 | 628542.0 | 650.63 | 4177.38 | 0.99 | 3.84 | 1.32 | 4311.51 |
| 150S | 150 | 617533.0 | 628551.0 | 650.42 | 4177.51 | 0.98 | 3.73 | 1.31 | 4311.47 |
| 150S | 125 | 617556.0 | 628560.0 | 650.72 | 4177.46 | 0.98 | 3.61 | 1.32 | 4311.37 |
| 150S | 100 | 617580.0 | 628569.0 | 651.21 | 4177.35 | 0.98 | 3.51 | 1.39 | 4311.32 |
| 150S | 75 | 617603.0 | 628578.0 | 651.51 | 4177.22 | 0.97 | 3.43 | 1.52 | 4311.30 |
| 150S | 50 | 617627.0 | 628586.0 | 650.11 | 4177.53 | 0.97 | 3.34 | 1.59 | 4311.31 |
| 150S | 25 | 617650.0 | 628595.0 | 651.60 | 4177.15 | 0.97 | 3.24 | 1.88 | 4311.41 |
| 150S | 0 | 617678.0 | 628606.0 | 647.90 | 4177.76 | 0.96 | 3.19 | 2.07 | 4311.42 |
| 150S | -25 | 617704.8 | 628621.2 | 635.52 | 4180.02 | 0.96 | 3.22 | 2.21 | 4311.41 |
| 150S | -50 | 617727.7 | 628629.4 | 629.24 | 4181.23 | 0.96 | 3.21 | 2.36 | 4311.53 |
| 150S | -75 | 617750.4 | 628638.1 | 623.25 | 4182.21 | 0.95 | 3.20 | 2.53 | 4311.48 |
| 150S | -100 | 617774.2 | 628646.9 | 613.97 | 4183.96 | 0.95 | 3.22 | 2.47 | 4311.36 |
| 150S | -125 | 617796.9 | 628655.7 | 610.69 | 4184.64 | 0.95 | 3.17 | 2.42 | 4311.31 |
| 150S | -150 | 617822.7 | 628665.4 | 603.90 | 4185.59 | 0.94 | 3.20 | 2.72 | 4311.24 |
| 150S | -175 | 617845.5 | 628673.2 | 593.62 | 4187.56 | 0.94 | 3.22 | 2.74 | 4311.22 |
| 150S | -200 | 617867.2 | 628682.0 | 583.03 | 4189.55 | 0.94 | 3.26 | 2.77 | 4311.21 |
| 150S | -250 | 617911.7 | 628697.6 | 560.60 | 4193.57 | 0.93 | 3.43 | 2.96 | 4311.16 |
| 150S | -275 | 617934.6 | 628706.3 | 550.40 | 4195.48 | 0.93 | 3.45 | 3.05 | 4311.18 |
| 150S | -300 | 617960.3 | 628716.1 | 543.90 | 4196.94 | 0.93 | 3.46 | 3.00 | 4311.21 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 200S | 350 | 617382.1 | 628398.3 | 663.50 | 4174.16 | 1.13 | 4.57 | 1.90 | 4312.27 |
| 200S | 325 | 617404.9 | 628409.3 | 658.91 | 4175.23 | 1.12 | 4.49 | 1.67 | 4312.12 |
| 200S | 300 | 617427.7 | 628420.4 | 654.72 | 4176.14 | 1.11 | 4.41 | 1.54 | 4311.99 |
| 200S | 275 | 617450.4 | 628431.4 | 651.12 | 4177.02 | 1.10 | 4.32 | 1.48 | 4312.01 |
| 200S | 250 | 617473.1 | 628442.4 | 649.03 | 4177.45 | 1.09 | 4.21 | 1.35 | 4311.75 |
| 200S | 225 | 617495.5 | 628453.3 | 647.54 | 4177.85 | 1.08 | 4.09 | 1.20 | 4311.68 |
| 200S | 200 | 617519.3 | 628464.8 | 646.95 | 4178.07 | 1.07 | 3.96 | 1.24 | 4311.61 |
| 200S | 175 | 617542.0 | 628475.9 | 648.25 | 4177.93 | 1.07 | 3.82 | 1.24 | 4311.56 |
| 200S | 150 | 617564.5 | 628486.8 | 649.36 | 4177.78 | 1.06 | 3.69 | 1.24 | 4311.51 |
| 200S | 125 | 617586.9 | 628497.7 | 649.87 | 4177.75 | 1.05 | 3.48 | 1.32 | 4311.43 |
| 200S | 75 | 617633.7 | 628520.4 | 648.98 | 4177.79 | 1.03 | 3.40 | 1.45 | 4311.32 |
| 200S | 50 | 617656.2 | 628531.4 | 648.59 | 4177.86 | 1.02 | 3.32 | 1.56 | 4311.33 |
| 200S | 25 | 617678.7 | 628542.3 | 648.70 | 4177.82 | 1.01 | 3.21 | 1.70 | 4311.34 |
| 200S | 0 | 617700.4 | 628552.9 | 647.60 | 4177.78 | 1.00 | 3.18 | 1.96 | 4311.30 |
| 200S | -25 | 617723.6 | 628564.0 | 644.87 | 4178.15 | 1.00 | 3.14 | 2.29 | 4311.42 |
| 200S | -50 | 617747.7 | 628575.5 | 640.14 | 4179.03 | 0.99 | 3.11 | 2.46 | 4311.50 |
| 200S | -75 | 617770.4 | 628586.4 | 632.61 | 4180.37 | 0.98 | 3.11 | 2.53 | 4311.43 |
| 200S | -100 | 617791.5 | 628596.5 | 626.18 | 4181.52 | 0.97 | 3.11 | 2.64 | 4311.41 |
| 200S | -125 | 617814.4 | 628607.4 | 617.65 | 4183.11 | 0.96 | 3.12 | 2.66 | 4311.34 |
| 200S | -150 | 617837.6 | 628618.5 | 612.52 | 4183.84 | 0.95 | 3.10 | 2.92 | 4311.30 |
| 200S | -175 | 617855.8 | 628627.2 | 602.00 | 4185.84 | 0.95 | 3.15 | 2.90 | 4311.25 |
| 200S | -200 | 617877.0 | 628637.4 | 593.47 | 4187.30 | 0.94 | 3.18 | 2.98 | 4311.19 |
| 200S | -225 | 617896.4 | 628646.6 | 581.44 | 4189.48 | 0.93 | 3.28 | 3.03 | 4311.17 |
| 200S | -250 | 617916.1 | 628656.1 | 570.01 | 4191.67 | 0.92 | 3.36 | 3.08 | 4311.15 |
| 200S | -275 | 617941.9 | 628668.4 | 561.28 | 4193.16 | 0.91 | 3.46 | 3.24 | 4311.18 |
| 200S | -300 | 617960.6 | 628677.4 | 547.55 | 4195.80 | 0.91 | 3.48 | 3.34 | 4311.23 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 250S | 350 | 617405.6 | 628349.7 | 662.10 | 4174.47 | 1.16 | 4.52 | 1.98 | 4312.36 |
| 250S | 325 | 617429.5 | 628361.3 | 657.39 | 4175.52 | 1.16 | 4.44 | 1.76 | 4312.18 |
| 250S | 300 | 617452.6 | 628372.5 | 653.99 | 4176.33 | 1.15 | 4.34 | 1.63 | 4312.09 |
| 250S | 275 | 617475.8 | 628383.8 | 650.18 | 4177.13 | 1.14 | 4.26 | 1.55 | 4311.97 |
| 250S | 250 | 617498.2 | 628394.7 | 647.17 | 4177.87 | 1.13 | 4.17 | 1.42 | 4311.89 |
| 250S | 225 | 617520.8 | 628405.6 | 644.97 | 4178.35 | 1.12 | 4.08 | 1.38 | 4311.80 |
| 250S | 200 | 617544.2 | 628417.0 | 644.96 | 4178.45 | 1.11 | 3.94 | 1.31 | 4311.68 |
| 250S | 175 | 617566.6 | 628427.9 | 645.55 | 4178.44 | 1.10 | 3.82 | 1.28 | 4311.62 |
| 250S | 150 | 617589.1 | 628438.8 | 647.64 | 4178.10 | 1.09 | 3.68 | 1.30 | 4311.56 |
| 250S | 125 | 617611.6 | 628449.7 | 646.94 | 4178.26 | 1.09 | 3.59 | 1.31 | 4311.50 |
| 250S | 100 | 617634.0 | 628460.6 | 647.13 | 4178.23 | 1.08 | 3.49 | 1.37 | 4311.46 |
| 250S | 75 | 617656.5 | 628471.5 | 646.72 | 4178.23 | 1.07 | 3.41 | 1.43 | 4311.35 |
| 250S | 50 | 617679.0 | 628482.5 | 647.82 | 4177.93 | 1.06 | 3.31 | 1.56 | 4311.29 |
| 250S | 25 | 617701.5 | 628493.4 | 647.51 | 4177.96 | 1.05 | 3.24 | 1.70 | 4311.31 |
| 250S | 0 | 617724.0 | 628504.3 | 647.60 | 4177.90 | 1.05 | 3.17 | 1.90 | 4311.41 |
| 250S | -25 | 617756.7 | 628527.2 | 644.13 | 4178.47 | 1.03 | 3.10 | 2.25 | 4311.55 |
| 250S | -50 | 617778.8 | 628537.7 | 639.56 | 4179.35 | 1.02 | 3.08 | 2.45 | 4311.70 |
| 250S | -75 | 617802.5 | 628549.0 | 633.09 | 4180.45 | 1.01 | 3.07 | 2.79 | 4311.85 |
| 250S | -100 | 617822.1 | 628558.2 | 624.92 | 4182.04 | 1.00 | 3.08 | 2.79 | 4311.83 |
| 250S | -125 | 617843.1 | 628568.2 | 617.55 | 4183.35 | 0.99 | 3.09 | 2.84 | 4311.74 |
| 250S | -150 | 617866.2 | 628579.2 | 609.88 | 4184.73 | 0.99 | 3.09 | 3.05 | 4311.82 |
| 250S | -175 | 617888.8 | 628589.9 | 599.90 | 4186.46 | 0.98 | 3.13 | 3.20 | 4311.77 |
| 250S | -200 | 617908.1 | 628599.2 | 590.03 | 4187.99 | 0.97 | 3.17 | 3.48 | 4311.67 |
| 250S | -225 | 617927.6 | 628608.4 | 576.76 | 4190.29 | 0.96 | 3.27 | 3.42 | 4311.39 |
| 250S | -250 | 617945.6 | 628616.9 | 564.39 | 4192.52 | 0.96 | 3.37 | 3.39 | 4311.25 |
| 250S | -275 | 617963.2 | 628625.4 | 552.02 | 4194.79 | 0.96 | 3.49 | 3.37 | 4311.19 |
| 250S | -300 | 617984.5 | 628635.4 | 544.65 | 4196.23 | 0.94 | 3.52 | 3.34 | 4311.17 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 300S | 300 | 617468.5 | 628337.5 | 653.00 | 4176.47 | 1.17 | 4.32 | 1.63 | 4312.03 |
| 300S | 275 | 617491.4 | 628347.0 | 649.70 | 4177.27 | 1.17 | 4.24 | 1.52 | 4311.99 |
| 300S | 250 | 617514.1 | 628356.5 | 646.30 | 4178.00 | 1.16 | 4.16 | 1.42 | 4311.86 |
| 300S | 225 | 617537.8 | 628366.4 | 643.60 | 4178.66 | 1.15 | 4.07 | 1.38 | 4311.86 |
| 300S | 200 | 617561.7 | 628376.3 | 642.40 | 4178.95 | 1.14 | 3.96 | 1.36 | 4311.77 |
| 300S | 175 | 617585.3 | 628386.2 | 643.60 | 4178.84 | 1.14 | 3.82 | 1.27 | 4311.67 |
| 300S | 150 | 617608.5 | 628395.8 | 644.90 | 4178.59 | 1.13 | 3.69 | 1.27 | 4311.53 |
| 300S | 125 | 617631.5 | 628405.4 | 644.60 | 4178.65 | 1.12 | 3.64 | 1.29 | 4311.50 |
| 300S | 100 | 617654.6 | 628415.1 | 644.20 | 4178.72 | 1.11 | 3.55 | 1.34 | 4311.44 |
| 300S | 75 | 617677.7 | 628424.7 | 644.40 | 4178.64 | 1.11 | 3.46 | 1.51 | 4311.47 |
| 300S | 50 | 617701.6 | 628434.6 | 648.10 | 4177.84 | 1.10 | 3.34 | 1.60 | 4311.36 |
| 300S | 0 | 617743.8 | 628457.4 | 649.50 | 4177.52 | 1.08 | 3.15 | 1.96 | 4311.47 |
| 300S | -25 | 617766.9 | 628467.0 | 648.83 | 4177.56 | 1.07 | 3.12 | 2.24 | 4311.61 |
| 300S | -50 | 617790.1 | 628476.7 | 643.45 | 4178.70 | 1.06 | 3.10 | 2.29 | 4311.72 |
| 300S | -75 | 617813.2 | 628486.3 | 637.37 | 4179.86 | 1.06 | 3.09 | 2.41 | 4311.79 |
| 300S | -100 | 617837.5 | 628496.4 | 632.80 | 4180.66 | 1.05 | 3.07 | 2.71 | 4311.96 |
| 300S | -125 | 617860.9 | 628506.2 | 629.62 | 4180.97 | 1.04 | 3.01 | 3.00 | 4311.89 |
| 300S | -150 | 617884.1 | 628515.9 | 623.15 | 4181.72 | 1.03 | 3.00 | 3.38 | 4311.71 |
| 300S | -175 | 617905.2 | 628524.7 | 609.57 | 4184.27 | 1.03 | 3.03 | 3.61 | 4311.74 |
| 300S | -200 | 617926.3 | 628533.3 | 596.60 | 4186.73 | 1.02 | 3.08 | 3.60 | 4311.75 |
| 300S | -225 | 617949.5 | 628543.1 | 583.73 | 4189.24 | 1.01 | 3.13 | 3.64 | 4311.84 |
| 300S | -250 | 617972.3 | 628552.6 | 570.85 | 4191.57 | 1.00 | 3.20 | 3.76 | 4311.79 |
| 300S | -275 | 617997.4 | 628563.1 | 558.77 | 4193.85 | 1.00 | 3.26 | 3.77 | 4311.79 |
| 300S | -300 | 618019.0 | 628572.1 | 545.90 | 4196.06 | 0.99 | 3.38 | 3.84 | 4311.64 |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 400S | 300 | 617507.0 | 628245.2 | 652.00 | 4176.67 | 1.25 | 4.27 | 1.59 | 4312.03 |
| 400S | 250 | 617529.5 | 628254.6 | 648.00 | 4177.51 | 1.24 | 4.21 | 1.48 | 4311.90 |
| 400S | 250 | 617553.1 | 628264.4 | 644.80 | 4178.32 | 1.23 | 4.13 | 1.42 | 4311.93 |
| 400S | 225 | 617575.8 | 628273.9 | 641.60 | 4178.97 | 1.22 | 4.06 | 1.44 | 4311.89 |
| 400S | 200 | 617598.7 | 628283.4 | 639.20 | 4179.51 | 1.22 | 3.98 | 1.34 | 4311.78 |
| 400S | 175 | 617621.9 | 628293.1 | 638.10 | 4179.83 | 1.21 | 3.88 | 1.32 | 4311.75 |
| 400S | 150 | 617645.0 | 628302.7 | 637.90 | 4179.91 | 1.20 | 3.77 | 1.30 | 4311.65 |
| 400S | 125 | 617668.0 | 628312.3 | 639.50 | 4179.68 | 1.19 | 3.65 | 1.26 | 4311.57 |
| 400S | 100 | 617691.1 | 628321.9 | 640.40 | 4179.52 | 1.19 | 3.54 | 1.31 | 4311.53 |
| 400S | 75 | 617715.3 | 628332.0 | 640.50 | 4179.46 | 1.18 | 3.45 | 1.37 | 4311.45 |
| 400S | 50 | 617738.0 | 628341.5 | 643.70 | 4178.74 | 1.17 | 3.36 | 1.49 | 4311.37 |
| 400S | 25 | 617761.0 | 628351.1 | 644.60 | 4178.56 | 1.16 | 3.26 | 1.62 | 4311.39 |
| 400S | 0 | 617784.1 | 628360.7 | 644.10 | 4178.59 | 1.16 | 3.20 | 1.77 | 4311.41 |
| 400S | -25 | 617799.7 | 628368.1 | 642.97 | 4178.86 | 1.15 | 3.16 | 1.91 | 4311.55 |
| 400S | -50 | 617822.4 | 628377.7 | 643.35 | 4178.73 | 1.14 | 3.10 | 2.13 | 4311.65 |
| 400S | -75 | 617845.2 | 628387.4 | 642.82 | 4178.75 | 1.14 | 3.05 | 2.45 | 4311.83 |
| 400S | -125 | 617894.7 | 628408.2 | 632.97 | 4180.41 | 1.12 | 3.01 | 2.93 | 4311.97 |
| 400S | -150 | 617917.9 | 628418.0 | 630.05 | 4180.54 | 1.11 | 2.98 | 3.55 | 4312.11 |
| 400S | -175 | 617947.2 | 628430.2 | 617.22 | 4182.68 | 1.10 | 3.01 | 4.02 | 4312.22 |
| 400S | -200 | 617968.9 | 628439.5 | 601.50 | 4185.51 | 1.09 | 3.08 | 3.89 | 4311.89 |
| 400S | -225 | 617988.6 | 628447.7 | 586.77 | 4188.38 | 1.09 | 3.17 | 3.79 | 4311.85 |
| 400S | -250 | 618013.9 | 628458.4 | 568.35 | 4191.77 | 1.08 | 3.31 | 3.82 | 4311.77 |
| 400S | -275 | 618037.2 | 628468.3 | 551.92 | 4194.98 | 1.07 | 3.47 | 3.77 | 4311.85 |
| 400S | -300 | 618063.2 | 628479.2 | 534.60 | 4198.11 | 1.06 | 3.65 | 3.73 | 4311.71 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 500S | 300 | 617549.7 | 628154.2 | 653.85 | 4176.67 | 1.31 | 4.16 | 1.59 | 4312.34 |
| 500S | 275 | 617572.2 | 628163.3 | 648.90 | 4177.74 | 1.30 | 4.12 | 1.45 | 4312.25 |
| 500S | 250 | 617595.6 | 628172.8 | 644.34 | 4178.66 | 1.30 | 4.08 | 1.37 | 4312.16 |
| 500S | 225 | 617618.8 | 628182.0 | 642.09 | 4179.17 | 1.30 | 4.00 | 1.32 | 4312.09 |
| 500S | 200 | 617644.2 | 628192.2 | 637.63 | 4180.12 | 1.29 | 3.95 | 1.29 | 4312.07 |
| 500S | 175 | 617667.3 | 628201.4 | 635.38 | 4180.61 | 1.28 | 3.87 | 1.27 | 4311.99 |
| 500S | 150 | 617690.5 | 628210.8 | 634.72 | 4180.82 | 1.27 | 3.78 | 1.25 | 4311.97 |
| 500S | 125 | 617713.7 | 628220.1 | 635.97 | 4180.62 | 1.27 | 3.66 | 1.24 | 4311.88 |
| 500S | 100 | 617736.8 | 628229.4 | 635.91 | 4180.66 | 1.26 | 3.57 | 1.28 | 4311.85 |
| 500S | 75 | 617760.0 | 628238.7 | 636.16 | 4180.54 | 1.25 | 3.48 | 1.35 | 4311.75 |
| 500S | 50 | 617784.4 | 628248.4 | 638.50 | 4179.98 | 1.24 | 3.37 | 1.52 | 4311.70 |
| 500S | 25 | 617806.2 | 628257.2 | 640.95 | 4179.35 | 1.24 | 3.28 | 1.65 | 4311.59 |
| 500S | 0 | 617827.2 | 628267.2 | 640.30 | 4179.38 | 1.23 | 3.23 | 1.79 | 4311.58 |
| 500S | -25 | 617850.4 | 628276.5 | 639.33 | 4179.40 | 1.22 | 3.18 | 2.07 | 4311.63 |
| 500S | -50 | 617874.1 | 628285.9 | 638.35 | 4179.47 | 1.22 | 3.13 | 2.48 | 4311.87 |
| 500S | -75 | 617897.9 | 628295.4 | 632.86 | 4180.38 | 1.21 | 3.12 | 2.68 | 4311.87 |
| 500S | -100 | 617922.1 | 628305.2 | 626.68 | 4181.37 | 1.20 | 3.11 | 3.01 | 4311.96 |
| 500S | -125 | 617945.3 | 628314.4 | 618.69 | 4182.65 | 1.19 | 3.12 | 3.24 | 4311.89 |
| 500S | -150 | 617966.4 | 628322.7 | 607.51 | 4184.89 | 1.19 | 3.16 | 3.27 | 4312.01 |
| 500S | -175 | 617987.8 | 628331.3 | 599.32 | 4186.44 | 1.18 | 3.18 | 3.30 | 4311.99 |
| 500S | -200 | 618011.5 | 628340.8 | 590.24 | 4187.94 | 1.17 | 3.21 | 3.48 | 4311.90 |
| 500S | -250 | 618052.5 | 628357.2 | 561.87 | 4193.18 | 1.16 | 3.43 | 3.39 | 4311.68 |
| 500S | -275 | 618070.7 | 628364.5 | 546.88 | 4195.84 | 1.15 | 3.59 | 3.56 | 4311.71 |
| 500S | -300 | 618090.5 | 628372.3 | 532.60 | 4198.35 | 1.14 | 3.76 | 3.66 | 4311.68 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 550S | 300 | 617551.3 | 628111.9 | 654.60 | 4176.39 | 1.35 | 4.21 | 1.58 | 4312.29 |
| 550S | 275 | 617575.2 | 628120.6 | 651.18 | 4177.13 | 1.35 | 4.14 | 1.47 | 4312.18 |
| 550S | 250 | 617599.5 | 628129.3 | 648.57 | 4177.69 | 1.34 | 4.06 | 1.49 | 4312.15 |
| 550S | 225 | 617621.4 | 628137.3 | 642.85 | 4178.90 | 1.33 | 4.05 | 1.35 | 4312.07 |
| 550S | 200 | 617647.0 | 628146.5 | 640.43 | 4179.45 | 1.33 | 3.96 | 1.29 | 4312.00 |
| 550S | 175 | 617672.1 | 628155.6 | 637.22 | 4180.10 | 1.32 | 3.90 | 1.25 | 4311.92 |
| 550S | 150 | 617697.1 | 628164.6 | 633.70 | 4180.78 | 1.31 | 3.84 | 1.25 | 4311.83 |
| 550S | 125 | 617723.3 | 628174.1 | 631.09 | 4181.39 | 1.30 | 3.77 | 1.26 | 4311.85 |
| 550S | 100 | 617748.9 | 628183.3 | 634.87 | 4180.70 | 1.29 | 3.61 | 1.26 | 4311.74 |
| 550S | 75 | 617774.4 | 628192.6 | 634.55 | 4180.74 | 1.29 | 3.52 | 1.41 | 4311.78 |
| 550S | 50 | 617798.8 | 628201.4 | 635.44 | 4180.55 | 1.28 | 3.43 | 1.46 | 4311.71 |
| 550S | 25 | 617822.3 | 628209.9 | 636.92 | 4180.11 | 1.28 | 3.34 | 1.61 | 4311.62 |
| 550S | 0 | 617851.6 | 628208.0 | 637.40 | 4179.92 | 1.28 | 3.27 | 1.85 | 4311.69 |
| 550S | -25 | 617871.1 | 628227.9 | 634.65 | 4180.41 | 1.27 | 3.23 | 2.01 | 4311.76 |
| 550S | -50 | 617894.5 | 628236.4 | 632.70 | 4180.61 | 1.26 | 3.19 | 2.35 | 4311.86 |
| 550S | -75 | 617919.3 | 628245.3 | 626.35 | 4181.77 | 1.26 | 3.18 | 2.60 | 4312.01 |
| 550S | -100 | 617944.2 | 628254.3 | 620.10 | 4182.72 | 1.25 | 3.17 | 2.92 | 4312.03 |
| 550S | -125 | 617965.0 | 628261.9 | 610.15 | 4184.65 | 1.24 | 3.21 | 2.90 | 4312.02 |
| 550S | -150 | 617986.8 | 628269.7 | 600.40 | 4186.49 | 1.24 | 3.25 | 2.95 | 4312.03 |
| 550S | -175 | 618005.8 | 628276.6 | 591.55 | 4188.08 | 1.23 | 3.29 | 3.02 | 4311.98 |
| 550S | -200 | 618026.7 | 628284.2 | 580.50 | 4190.20 | 1.23 | 3.36 | 3.07 | 4312.04 |
| 550S | -225 | 618048.8 | 628292.1 | 569.95 | 4192.12 | 1.22 | 3.42 | 3.21 | 4312.08 |
| 550S | -250 | 618072.4 | 628300.7 | 559.80 | 4194.12 | 1.21 | 3.48 | 3.35 | 4312.28 |
| 550S | -275 | 618097.4 | 628309.7 | 549.35 | 4195.95 | 1.21 | 3.56 | 3.35 | 4312.13 |
| 550S | -300 | 618114.6 | 628315.9 | 545.70 | 4196.30 | 1.20 | 3.55 | 3.46 | 4311.85 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 600S | 300 | 617587.0 | 628061.4 | 653.15 | 4176.91 | 1.39 | 4.16 | 1.46 | 4312.40 |
| 600S | 275 | 617609.7 | 628070.5 | 649.70 | 4177.70 | 1.39 | 4.10 | 1.39 | 4312.38 |
| 600S | 250 | 617633.3 | 628080.0 | 646.06 | 4178.48 | 1.38 | 4.04 | 1.35 | 4312.33 |
| 600S | 225 | 617656.1 | 628089.2 | 642.71 | 4179.23 | 1.37 | 3.97 | 1.29 | 4312.28 |
| 600S | 200 | 617679.1 | 628098.4 | 639.77 | 4179.89 | 1.36 | 3.92 | 1.24 | 4312.26 |
| 600S | 175 | 617702.1 | 628107.7 | 636.82 | 4180.38 | 1.36 | 3.84 | 1.22 | 4312.06 |
| 600S | 150 | 617726.1 | 628117.3 | 633.18 | 4181.21 | 1.35 | 3.78 | 1.22 | 4312.10 |
| 600S | 125 | 617749.5 | 628126.7 | 630.63 | 4181.67 | 1.34 | 3.70 | 1.25 | 4312.01 |
| 600S | 100 | 617773.1 | 628136.2 | 629.59 | 4182.01 | 1.33 | 3.62 | 1.24 | 4312.04 |
| 600S | 75 | 617795.7 | 628145.3 | 634.04 | 4181.16 | 1.33 | 3.47 | 1.25 | 4311.92 |
| 600S | 50 | 617818.8 | 628154.5 | 635.40 | 4180.85 | 1.32 | 3.39 | 1.41 | 4311.93 |
| 600S | 25 | 617842.0 | 628163.9 | 635.75 | 4180.66 | 1.31 | 3.34 | 1.61 | 4311.97 |
| 600S | 0 | 617865.0 | 628173.1 | 632.20 | 4181.06 | 1.30 | 3.33 | 1.83 | 4311.87 |
| 600S | -25 | 617874.3 | 628178.1 | 631.39 | 4181.20 | 1.30 | 3.31 | 1.94 | 4311.94 |
| 600S | -50 | 617896.3 | 628187.1 | 628.07 | 4181.76 | 1.30 | 3.28 | 2.10 | 4311.98 |
| 600S | -75 | 617919.7 | 628196.6 | 624.76 | 4182.24 | 1.28 | 3.25 | 2.43 | 4312.09 |
| 600S | -100 | 617941.0 | 628205.2 | 619.44 | 4183.19 | 1.28 | 3.25 | 2.62 | 4312.18 |
| 600S | -125 | 617963.3 | 628214.1 | 607.92 | 4185.00 | 1.27 | 3.30 | 2.79 | 4311.94 |
| 600S | -150 | 617985.4 | 628223.1 | 599.90 | 4186.52 | 1.27 | 3.32 | 2.82 | 4311.93 |
| 600S | -175 | 618009.9 | 628233.1 | 590.89 | 4188.19 | 1.26 | 3.35 | 2.82 | 4311.85 |
| 600S | -200 | 618032.2 | 628242.0 | 580.57 | 4190.11 | 1.25 | 3.40 | 2.95 | 4311.91 |
| 600S | -225 | 618054.0 | 628250.8 | 570.05 | 4192.11 | 1.24 | 3.47 | 3.17 | 4312.12 |
| 600S | -250 | 618077.9 | 628260.6 | 557.93 | 4194.17 | 1.24 | 3.56 | 3.12 | 4311.83 |
| 600S | -275 | 618105.6 | 628271.7 | 550.02 | 4195.80 | 1.23 | 3.58 | 3.14 | 4311.94 |
| 600S | -300 | 618129.0 | 628281.1 | 541.90 | 4197.27 | 1.22 | 3.63 | 3.19 | 4311.90 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 650S | 300 | 617585.3 | 628017.9 | 653.70 | 4176.56 | 1.43 | 4.25 | 1.53 | 4312.35 |
| 650S | 275 | 617610.2 | 628026.9 | 649.42 | 4177.53 | 1.42 | 4.20 | 1.42 | 4312.31 |
| 650S | 250 | 617635.0 | 628035.9 | 646.43 | 4178.17 | 1.41 | 4.12 | 1.36 | 4312.21 |
| 650S | 225 | 617660.1 | 628044.9 | 644.55 | 4178.63 | 1.41 | 4.03 | 1.38 | 4312.23 |
| 650S | 200 | 617687.6 | 628054.9 | 639.47 | 4179.70 | 1.40 | 3.98 | 1.27 | 4312.14 |
| 650S | 175 | 617711.0 | 628063.3 | 637.48 | 4180.15 | 1.39 | 3.91 | 1.25 | 4312.09 |
| 650S | 150 | 617735.3 | 628072.1 | 635.30 | 4180.61 | 1.38 | 3.83 | 1.28 | 4312.07 |
| 650S | 125 | 617760.6 | 628081.3 | 632.81 | 4181.10 | 1.38 | 3.77 | 1.25 | 4311.98 |
| 650S | 100 | 617787.0 | 628090.8 | 624.83 | 4182.59 | 1.37 | 3.78 | 1.33 | 4311.98 |
| 650S | 75 | 617810.9 | 628099.5 | 626.45 | 4182.48 | 1.36 | 3.62 | 1.30 | 4312.00 |
| 650S | 50 | 617834.9 | 628108.1 | 631.96 | 4181.34 | 1.36 | 3.50 | 1.44 | 4311.94 |
| 650S | 25 | 617858.3 | 628116.6 | 632.38 | 4181.22 | 1.35 | 3.42 | 1.61 | 4311.99 |
| 650S | 0 | 617881.6 | 628125.0 | 629.60 | 4181.70 | 1.34 | 3.38 | 1.74 | 4312.00 |
| 650S | -25 | 617899.3 | 628133.3 | 627.90 | 4181.85 | 1.35 | 3.35 | 2.12 | 4312.18 |
| 650S | -50 | 617920.8 | 628144.9 | 623.85 | 4182.40 | 1.34 | 3.33 | 2.33 | 4312.11 |
| 650S | -75 | 617945.9 | 628148.9 | 612.01 | 4184.65 | 1.33 | 3.39 | 2.35 | 4312.10 |
| 650S | -100 | 617971.9 | 628158.3 | 599.16 | 4187.04 | 1.32 | 3.46 | 2.40 | 4312.07 |
| 650S | -125 | 617997.7 | 628167.6 | 592.52 | 4188.26 | 1.32 | 3.46 | 2.47 | 4312.06 |
| 650S | -150 | 618020.3 | 628175.8 | 588.87 | 4188.85 | 1.31 | 3.43 | 2.78 | 4312.20 |
| 650S | -175 | 618042.8 | 628184.0 | 577.93 | 4190.86 | 1.30 | 3.50 | 2.86 | 4312.20 |
| 650S | -200 | 618065.4 | 628192.1 | 565.78 | 4192.96 | 1.30 | 3.60 | 2.96 | 4312.11 |
| 650S | -225 | 618084.6 | 628199.1 | 550.94 | 4195.45 | 1.29 | 3.81 | 3.11 | 4312.04 |
| 650S | -250 | 618103.1 | 628205.7 | 535.89 | 4198.13 | 1.29 | 3.97 | 3.28 | 4312.08 |
| 650S | -275 | 618125.3 | 628213.8 | 528.35 | 4199.61 | 1.28 | 4.03 | 3.17 | 4312.02 |
| 650S | -300 | 618148.5 | 628222.2 | 522.30 | 4201.01 | 1.27 | 4.06 | 2.94 | 4312.01 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 700S | 300 | 617619.8 | 627960.3 | 650.80 | 4177.30 | 1.47 | 4.30 | 1.40 | 4312.49 |
| 700S | 275 | 617643.5 | 627970.3 | 649.20 | 4177.69 | 1.46 | 4.19 | 1.43 | 4312.47 |
| 700S | 250 | 617667.2 | 627980.3 | 646.30 | 4178.27 | 1.46 | 4.11 | 1.36 | 4312.32 |
| 700S | 225 | 617689.2 | 627989.8 | 640.40 | 4179.40 | 1.45 | 4.11 | 1.31 | 4312.24 |
| 700S | 200 | 617712.0 | 627999.1 | 630.40 | 4181.30 | 1.44 | 4.19 | 1.29 | 4312.22 |
| 700S | 175 | 617735.8 | 628009.1 | 626.70 | 4182.14 | 1.43 | 4.14 | 1.21 | 4312.20 |
| 700S | 150 | 617758.8 | 628018.8 | 627.40 | 4182.20 | 1.43 | 4.00 | 1.10 | 4312.14 |
| 700S | 125 | 617782.8 | 628028.9 | 628.60 | 4182.03 | 1.42 | 3.86 | 1.20 | 4312.15 |
| 700S | 100 | 617804.3 | 628037.9 | 621.50 | 4183.30 | 1.41 | 3.89 | 1.28 | 4312.13 |
| 700S | 75 | 617830.0 | 628048.7 | 620.60 | 4183.58 | 1.40 | 3.79 | 1.31 | 4312.15 |
| 700S | 50 | 617852.1 | 628058.0 | 627.80 | 4182.21 | 1.40 | 3.59 | 1.40 | 4312.09 |
| 700S | 25 | 617875.9 | 628068.0 | 626.60 | 4182.42 | 1.39 | 3.52 | 1.48 | 4312.06 |
| 700S | 0 | 617900.6 | 628078.4 | 623.80 | 4182.92 | 1.39 | 3.48 | 1.51 | 4312.01 |
| 700S | -25 | 617922.9 | 628087.8 | 619.70 | 4183.68 | 1.37 | 3.45 | 1.60 | 4312.00 |
| 700S | -50 | 617945.5 | 628097.0 | 615.20 | 4184.45 | 1.36 | 3.43 | 1.76 | 4312.02 |
| 700S | -75 | 617969.7 | 628106.9 | 611.90 | 4184.93 | 1.36 | 3.40 | 2.07 | 4312.12 |
| 700S | -100 | 617994.1 | 628116.9 | 605.10 | 4186.12 | 1.35 | 3.40 | 2.22 | 4312.11 |
| 700S | -125 | 618014.5 | 628125.1 | 593.70 | 4188.41 | 1.34 | 3.47 | 2.14 | 4312.14 |
| 700S | -150 | 618036.1 | 628134.0 | 584.00 | 4190.17 | 1.33 | 3.53 | 2.18 | 4312.08 |
| 700S | -175 | 618061.6 | 628144.5 | 573.80 | 4192.02 | 1.33 | 3.58 | 2.29 | 4312.09 |
| 700S | -200 | 618083.7 | 628153.4 | 563.40 | 4193.99 | 1.32 | 3.65 | 2.29 | 4312.07 |
| 700S | -225 | 618106.5 | 628162.8 | 553.00 | 4195.79 | 1.31 | 3.73 | 2.46 | 4312.09 |
| 700S | -250 | 618128.7 | 628171.9 | 542.90 | 4197.79 | 1.30 | 3.82 | 2.50 | 4312.19 |
| 700S | -275 | 618154.6 | 628182.4 | 534.20 | 4199.24 | 1.30 | 3.88 | 2.57 | 4312.17 |
| 700S | -300 | 618176.2 | 628191.3 | 522.70 | 4201.38 | 1.29 | 4.02 | 2.74 | 4312.24 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 G | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 800S | 300 | 617658.6 | 627862.0 | 649.70 | 4177.74 | 1.55 | 4.53 | 1.17 | 4312.72 |
| 800S | 275 | 617681.9 | 627877.8 | 645.88 | 4178.41 | 1.53 | 4.43 | 1.12 | 4312.53 |
| 800S | 250 | 617705.5 | 627887.7 | 642.37 | 4179.16 | 1.53 | 4.35 | 1.09 | 4312.48 |
| 800S | 225 | 617730.0 | 627898.0 | 638.75 | 4179.92 | 1.52 | 4.28 | 1.12 | 4312.48 |
| 800S | 200 | 617752.2 | 627907.6 | 635.63 | 4180.60 | 1.51 | 4.21 | 1.08 | 4312.43 |
| 800S | 175 | 617776.2 | 627917.5 | 631.92 | 4181.40 | 1.51 | 4.15 | 1.15 | 4312.50 |
| 800S | 125 | 617826.7 | 627938.7 | 626.59 | 4182.49 | 1.49 | 3.99 | 1.21 | 4312.43 |
| 800S | 100 | 617848.6 | 627947.9 | 620.57 | 4183.47 | 1.48 | 3.99 | 1.44 | 4312.45 |
| 800S | 75 | 617866.7 | 627955.5 | 609.60 | 4185.57 | 1.48 | 4.12 | 1.23 | 4312.31 |
| 800S | 50 | 617871.7 | 627966.0 | 605.04 | 4186.38 | 1.47 | 4.16 | 1.27 | 4312.29 |
| 800S | 25 | 617914.4 | 627975.6 | 598.92 | 4187.50 | 1.46 | 4.08 | 1.36 | 4312.21 |
| 800S | 0 | 617940.0 | 627984.7 | 608.20 | 4185.84 | 1.46 | 3.78 | 1.40 | 4312.11 |
| 800S | -25 | 617966.3 | 627986.5 | 606.12 | 4186.26 | 1.45 | 3.73 | 1.46 | 4312.12 |
| 800S | -50 | 617991.4 | 627997.2 | 602.14 | 4187.11 | 1.44 | 3.68 | 1.55 | 4312.22 |
| 800S | -75 | 618008.1 | 628007.4 | 596.85 | 4188.11 | 1.43 | 3.69 | 1.61 | 4312.24 |
| 800S | -100 | 618038.8 | 628017.7 | 593.27 | 4188.83 | 1.42 | 3.63 | 1.73 | 4312.30 |
| 800S | -125 | 618061.3 | 628027.4 | 588.99 | 4189.67 | 1.42 | 3.60 | 1.85 | 4312.39 |
| 800S | -175 | 618107.5 | 628047.4 | 575.72 | 4191.94 | 1.40 | 3.62 | 2.29 | 4312.49 |
| 800S | -200 | 618130.2 | 628057.2 | 566.93 | 4193.56 | 1.39 | 3.66 | 2.33 | 4312.45 |
| 800S | -225 | 618153.3 | 628067.1 | 559.15 | 4194.73 | 1.39 | 3.69 | 2.56 | 4312.36 |
| 800S | -250 | 618174.2 | 628076.1 | 545.77 | 4197.04 | 1.38 | 3.84 | 2.69 | 4312.30 |
| 800S | -275 | 618197.6 | 628086.2 | 532.48 | 4199.47 | 1.37 | 3.99 | 2.74 | 4312.31 |
| 800S | -300 | 618217.5 | 628094.9 | 520.00 | 4201.74 | 1.36 | 4.17 | 2.79 | 4312.34 |
| | | 9999 | | | | | | | |

| LINE | STN | UTM (long) | UTM (lat) | ELEV (m) | OBS G | LAT G | TER1 G | TER2 B | CB GRAV (mgal) |
|---|---|---|---|---|---|---|---|---|---|
| 0 | 600 | 617419.6 | 629321.2 | 602.20 | 4185.31 | 0.40 | 3.88 | 1.35 | 4309.39 |
| 0 | 575 | 617427.8 | 629300.7 | 602.20 | 4185.33 | 0.41 | 3.87 | 1.39 | 4309.45 |
| 0 | 525 | 617444.6 | 629252.8 | 598.30 | 4185.96 | 0.45 | 3.92 | 1.33 | 4309.34 |
| 0 | 475 | 617461.3 | 629206.2 | 588.80 | 4187.76 | 0.49 | 4.08 | 1.51 | 4309.66 |
| 0 | 425 | 617477.5 | 629158.9 | 594.00 | 4186.83 | 0.53 | 3.98 | 1.51 | 4309.69 |
| 0 | 375 | 617492.5 | 629111.5 | 605.60 | 4184.67 | 0.56 | 3.79 | 1.50 | 4309.64 |
| 0 | 325 | 617511.5 | 629064.5 | 607.50 | 4184.23 | 0.60 | 3.74 | 1.55 | 4309.62 |
| 0 | 275 | 617531.3 | 629015.6 | 610.80 | 4183.63 | 0.64 | 3.67 | 1.70 | 4309.78 |
| 0 | 225 | 617546.8 | 628962.9 | 611.40 | 4183.45 | 0.67 | 3.67 | 1.94 | 4309.99 |
| 0 | 175 | 617555.6 | 628922.5 | 629.90 | 4180.00 | 0.72 | 3.44 | 2.11 | 4310.17 |
| 0 | 125 | 617570.7 | 628865.3 | 641.90 | 4178.41 | 0.76 | 3.31 | 2.27 | 4311.02 |
| 0 | 75 | 617590.1 | 628817.2 | 648.00 | 4177.46 | 0.80 | 3.23 | 2.30 | 4311.25 |
| 0 | 25 | 617610.2 | 628772.5 | 657.70 | 4175.28 | 0.83 | 3.13 | 3.11 | 4311.72 |
| 0 | -25 | 617630.4 | 628724.5 | 658.20 | 4175.40 | 0.87 | 3.11 | 3.15 | 4312.00 |
| 0 | -75 | 617652.2 | 628676.4 | 654.10 | 4176.35 | 0.91 | 3.14 | 2.72 | 4311.78 |
| 0 | -125 | 617671.7 | 628630.7 | 649.90 | 4177.24 | 0.94 | 3.17 | 2.35 | 4311.54 |
| 0 | -175 | 617689.4 | 628577.6 | 646.30 | 4178.10 | 0.98 | 3.20 | 1.90 | 4311.31 |
| 0 | -225 | 617710.7 | 628529.1 | 647.70 | 4177.85 | 1.02 | 3.18 | 1.89 | 4311.34 |
| 0 | -275 | 617732.9 | 628483.3 | 647.80 | 4177.82 | 1.06 | 3.17 | 1.85 | 4311.33 |
| 0 | -325 | 617753.7 | 628435.6 | 648.90 | 4177.59 | 1.10 | 3.15 | 1.90 | 4311.38 |
| 0 | -375 | 617774.1 | 628387.8 | 646.30 | 4178.10 | 1.14 | 3.17 | 1.81 | 4311.35 |
| 0 | -425 | 617795.4 | 628339.5 | 643.00 | 4178.77 | 1.18 | 3.20 | 1.71 | 4311.33 |
| 0 | -475 | 617816.4 | 628290.8 | 642.00 | 4178.98 | 1.21 | 3.21 | 1.75 | 4311.44 |
| 0 | -525 | 617843.5 | 628244.5 | 638.70 | 4179.67 | 1.25 | 3.23 | 1.81 | 4311.59 |
| 0 | -575 | 617856.7 | 628196.5 | 635.20 | 4180.40 | 1.29 | 3.29 | 1.71 | 4311.63 |
| 0 | -625 | 617874.0 | 628147.7 | 630.40 | 4181.49 | 1.32 | 3.36 | 1.68 | 4311.85 |
| 0 | -675 | 617891.5 | 628101.1 | 626.60 | 4182.27 | 1.36 | 3.43 | 1.73 | 4312.04 |
| 0 | -725 | 617909.3 | 628054.2 | 620.00 | 4183.60 | 1.40 | 3.54 | 1.59 | 4312.08 |
| 0 | -750 | 617919.1 | 628031.0 | 615.60 | 4184.51 | 1.42 | 3.62 | 1.50 | 4312.13 |
| 0 | -775 | 617930.2 | 628007.7 | 612.90 | 4185.01 | 1.44 | 3.68 | 1.45 | 4312.13 |
| 10000 | 1 | 617912.0 | 629590.0 | 457.40 | 4212.03 | 0.18 | 4.66 | 2.58 | 4309.42 |
| 10000 | 2 | 617883.0 | 629697.0 | 459.00 | 4211.83 | 0.10 | 4.74 | 1.86 | 4308.81 |
| 10000 | 3 | 617984.0 | 629474.0 | 455.70 | 4212.22 | 0.28 | 4.54 | 1.91 | 4308.58 |
| 10000 | 5 | 617998.0 | 629244.0 | 453.80 | 4212.58 | 0.46 | 4.74 | 3.63 | 4310.67 |
| 10000 | 6 | 618047.0 | 629199.0 | 454.10 | 4212.44 | 0.52 | 4.64 | 3.07 | 4309.99 |
| 10000 | 7 | 618082.0 | 629114.0 | 454.60 | 4212.27 | 0.56 | 4.62 | 3.51 | 4310.38 |
| 10000 | 8 | 618148.0 | 629124.0 | 454.40 | 4213.30 | 0.55 | 4.48 | 2.05 | 4309.76 |
| 10000 | 10 | 618106.0 | 629278.0 | 454.40 | 4213.27 | 0.43 | 4.43 | 1.67 | 4309.18 |
| 10000 | 11 | 618079.0 | 629447.0 | 456.00 | 4213.30 | 0.30 | 4.33 | 1.31 | 4308.93 |
| 10000 | 12 | 618082.0 | 629542.0 | 457.60 | 4213.11 | 0.22 | 4.24 | 1.08 | 4308.66 |
| 10000 | 13 | 618091.0 | 629656.0 | 460.10 | 4212.57 | 0.13 | 4.13 | 0.85 | 4308.18 |
| 10000 | 14 | 618082.0 | 629781.0 | 463.50 | 4211.82 | 0.03 | 4.06 | 0.61 | 4307.69 |
| 10000 | 15 | 618074.0 | 629957.0 | 466.00 | 4211.65 | -0.11 | 4.49 | 0.40 | 4308.09 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 250W | 450 | 617104.0 | 628887.0 | 678.50 | 4169.10 | 0.74 | 5.77 | 1.76 | 4310.83 |
| 250W | 500 | 617062.0 | 628840.0 | 706.60 | 4165.35 | 0.78 | 5.56 | 1.71 | 4312.39 |
| 250W | 550 | 617020.0 | 628818.0 | 723.10 | 4162.21 | 0.80 | 5.85 | 1.89 | 4312.99 |
| 250W | 600 | 616975.0 | 628794.0 | 731.20 | 4160.50 | 0.81 | 5.96 | 1.50 | 4312.59 |
| 250W | 650 | 616932.0 | 628771.0 | 754.30 | 4155.74 | 0.83 | 6.08 | 1.78 | 4312.80 |
| 250W | 700 | 616893.0 | 628749.0 | 774.60 | 4151.83 | 0.85 | 6.33 | 1.94 | 4313.32 |
| 250W | 750 | 616846.0 | 628725.0 | 790.20 | 4149.00 | 0.87 | 6.35 | 1.88 | 4313.54 |
| 250W | 800 | 616807.0 | 628697.0 | 804.10 | 4146.32 | 0.89 | 6.53 | 1.86 | 4313.76 |
| 250W | 850 | 616769.0 | 628669.0 | 820.80 | 4142.96 | 0.91 | 6.95 | 1.90 | 4314.17 |
| 250W | 900 | 616725.0 | 628641.0 | 838.20 | 4139.81 | 0.93 | 7.28 | 1.91 | 4314.80 |
| 250W | 950 | 616679.0 | 628610.0 | 852.60 | 4137.19 | 0.96 | 7.40 | 1.85 | 4315.11 |
| 250W | 1000 | 616636.0 | 628581.0 | 864.40 | 4134.96 | 0.98 | 7.87 | 1.78 | 4315.62 |
| | | 9999 | | | | | | | |

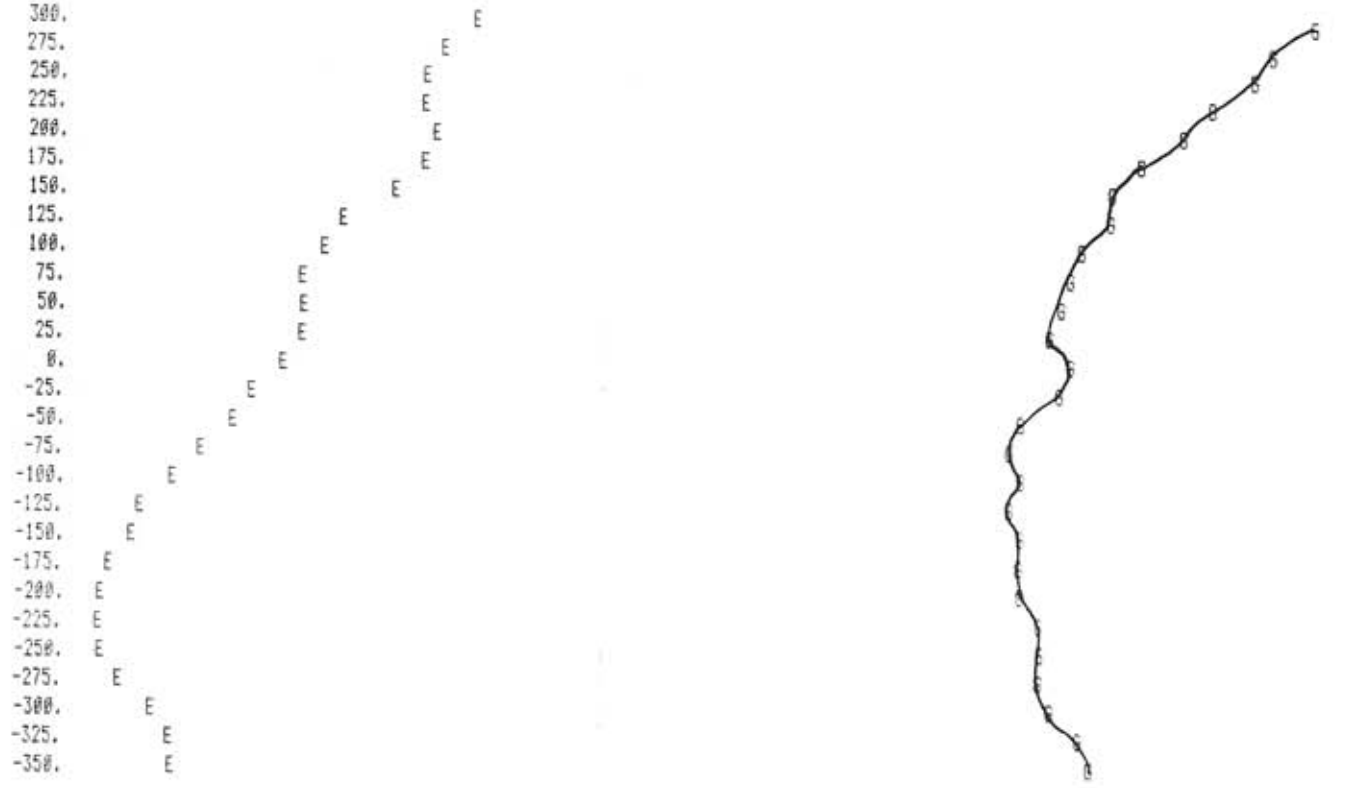
# APPENDIX V: Gravity Profiles

PROFILE OF LINE L650N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1824 | 1906 | 1988 | 2073 | 2155 | 2240 | 2322 | 2404 | 2490 | 2572 | 2657 | 2739 | 2821 |
| ELEV M | 556 | 581 | 606 | 632 | 657 | 683 | 708 | 733 | 759 | 784 | 810 | 835 | 860 |
| MGAL | 4304.9 | 4305.4 | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 |





| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1824 | 1906 | 1988 | 2073 | 2155 | 2240 | 2322 | 2404 | 2490 | 2572 | 2657 | 2739 | 2821 |
| ELEV M | 556 | 581 | 606 | 632 | 657 | 683 | 708 | 733 | 759 | 784 | 810 | 835 | 860 |
| MGAL | 4304.9 | 4305.4 | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 |

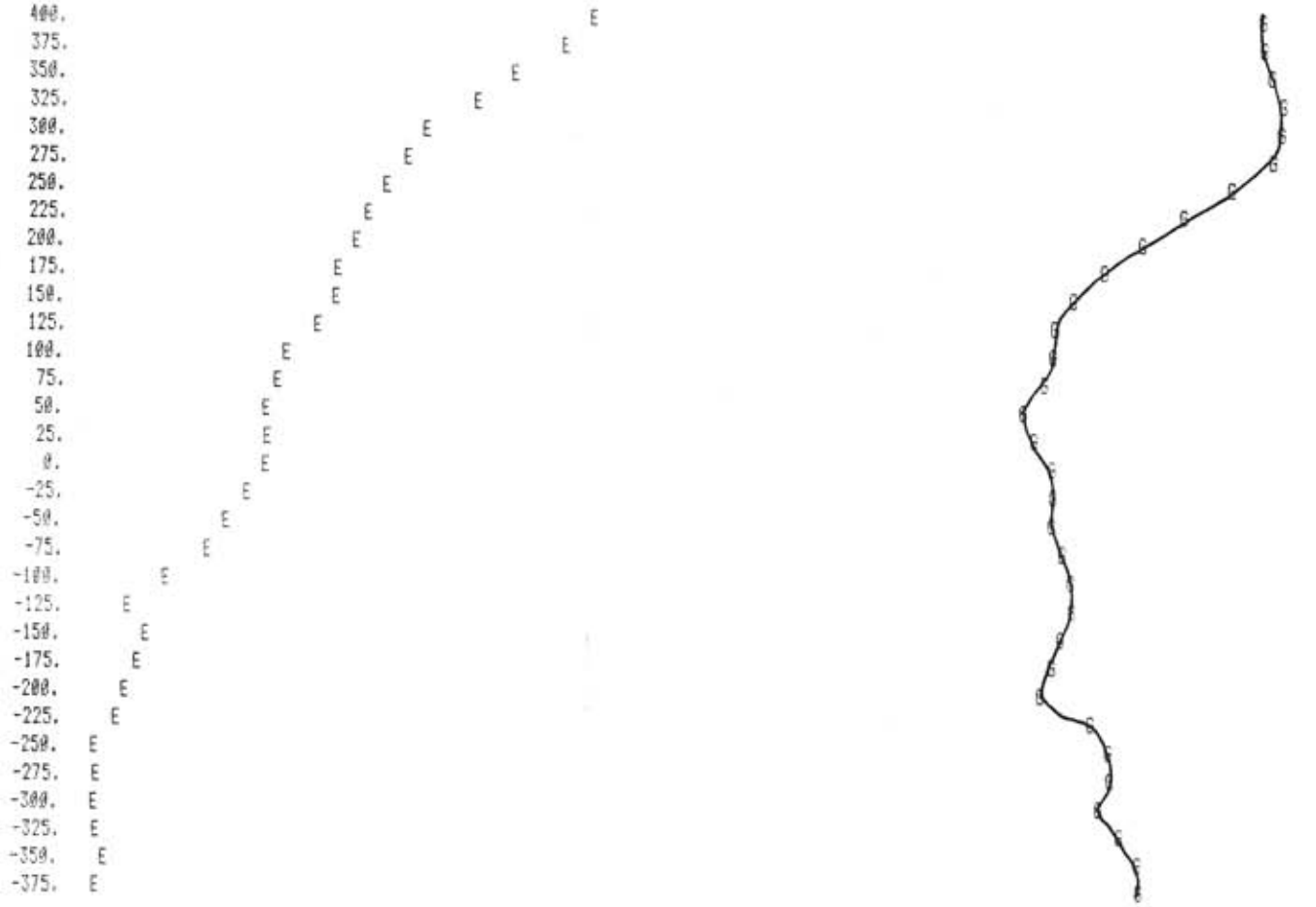

Figure 7

PROFILE OF LINE L550N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1830 | 1912 | 1994 | 2080 | 2162 | 2247 | 2329 | 2411 | 2496 | 2578 | 2664 | 2746 | 2828 |
| ELEV M | 558 | 583 | 608 | 634 | 659 | 685 | 710 | 735 | 761 | 786 | 812 | 837 | 862 |
| MGAL | 4304.6 | 4305.1 | 4305.6 | 4306.1 | 4306.6 | 4307.1 | 4307.6 | 4308.1 | 4308.6 | 4309.1 | 4309.6 | 4310.1 | 4310.6 |





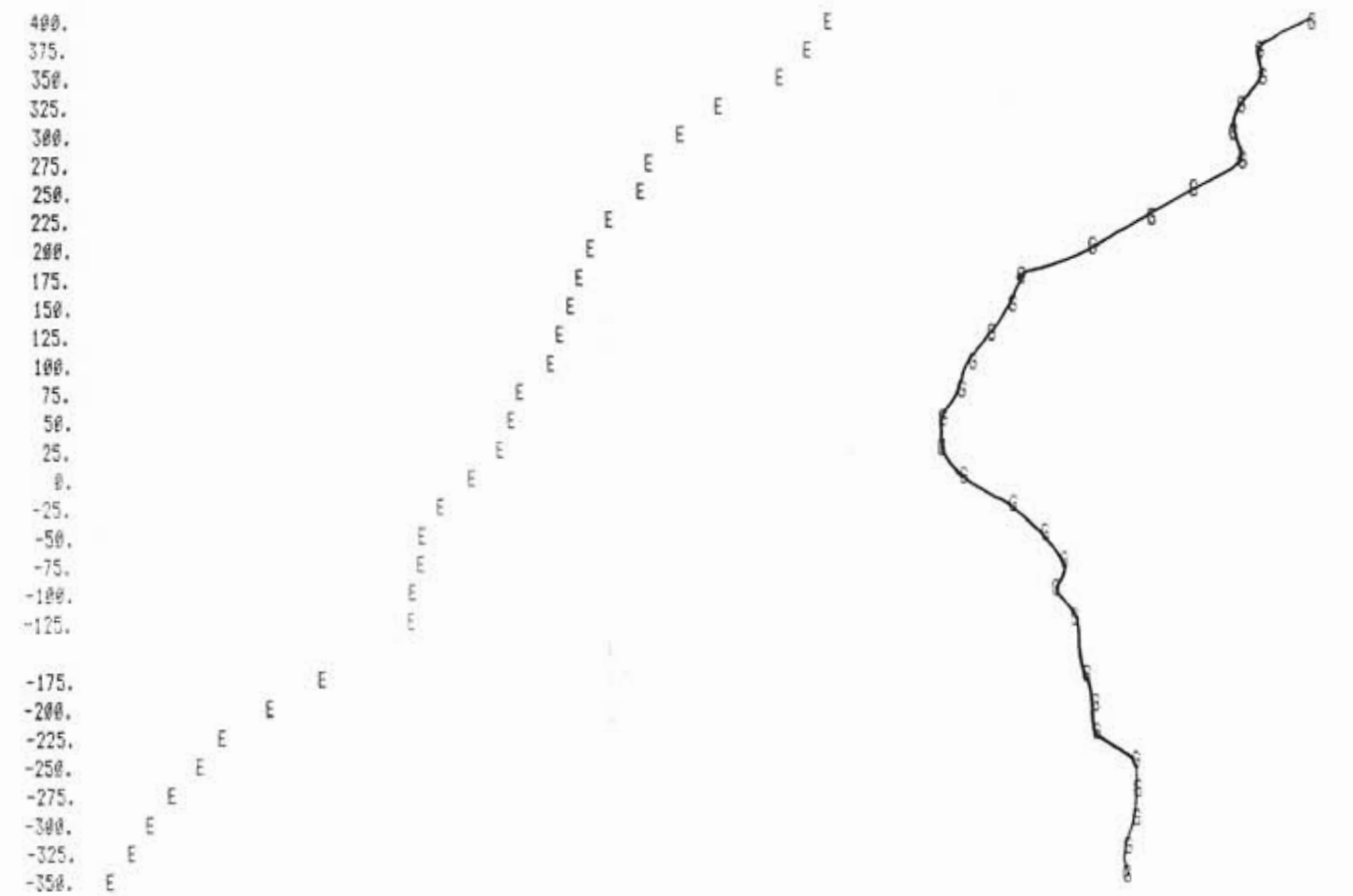
| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1830 | 1912 | 1994 | 2080 | 2162 | 2247 | 2329 | 2411 | 2496 | 2578 | 2664 | 2746 | 2828 |
| ELEV M | 558 | 583 | 608 | 634 | 659 | 685 | 710 | 735 | 761 | 786 | 812 | 837 | 862 |
| MGAL | 4304.6 | 4305.1 | 4305.6 | 4306.1 | 4306.6 | 4307.1 | 4307.6 | 4308.1 | 4308.6 | 4309.1 | 4309.6 | 4310.1 | 4310.6 |


Figure 8

PROFILE OF LINE L500N

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967
G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1637 | 1719 | 1804 | 1886 | 1971 | 2053 | 2135 | 2221 | 2303 | 2388 | 2470 | 2552 | 2637 |
| ELEV M | 499 | 524 | 550 | 575 | 601 | 626 | 651 | 677 | 702 | 728 | 753 | 778 | 804 |
| MGAL | 4304.9 | 4305.4 | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 |





| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1637 | 1719 | 1804 | 1886 | 1971 | 2053 | 2135 | 2221 | 2303 | 2388 | 2470 | 2552 | 2637 |
| ELEV M | 499 | 524 | 550 | 575 | 601 | 626 | 651 | 677 | 702 | 728 | 753 | 778 | 804 |
| MGAL | 4304.9 | 4305.4 | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 |

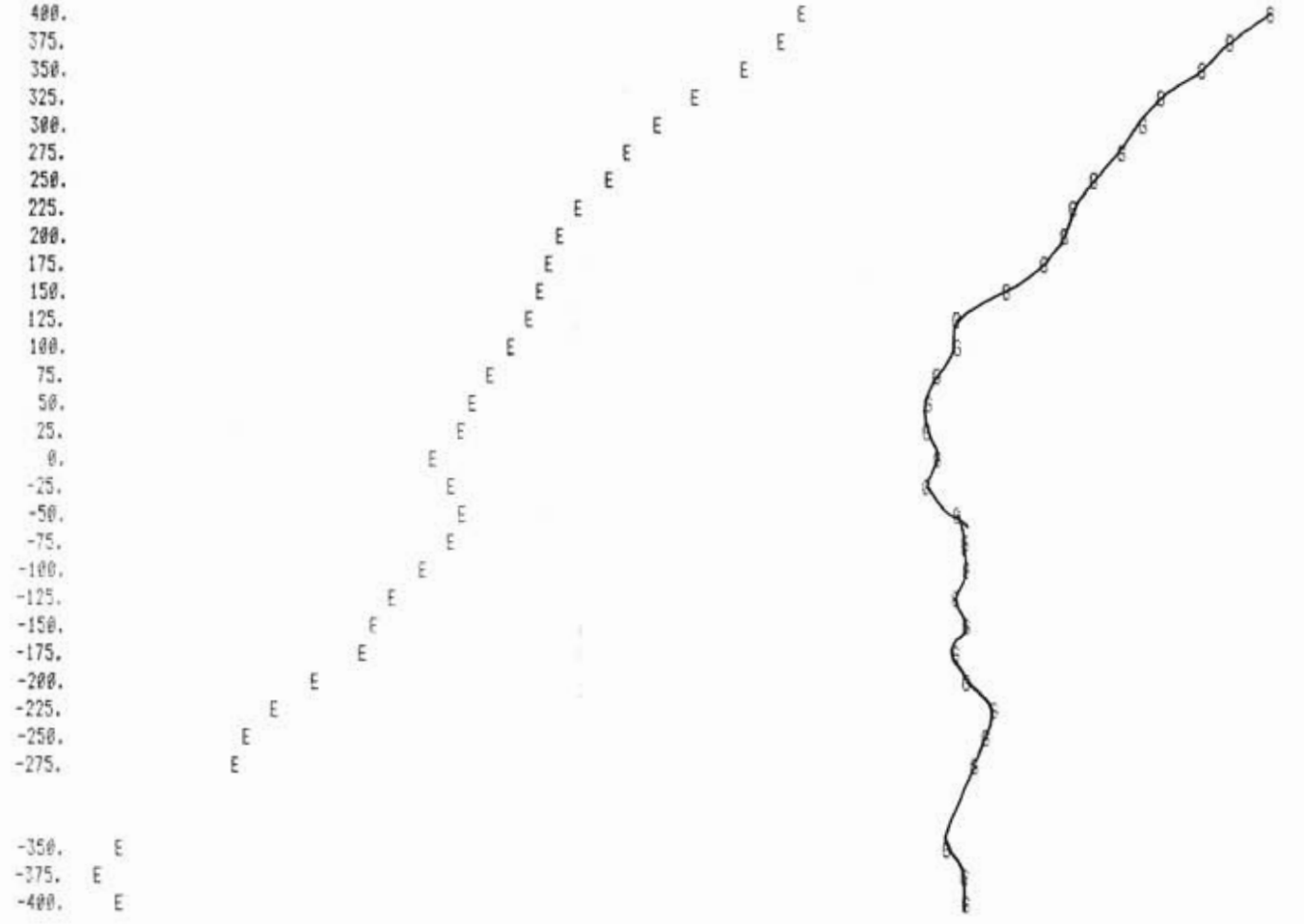

Figure 9

PROFILE OF LINE L450N

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967

G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1640 | 1725 | 1807 | 1889 | 1975 | 2057 | 2142 | 2224 | 2306 | 2391 | 2473 | 2559 | 2641 |
| ELEV M | 500 | 526 | 551 | 576 | 602 | 627 | 653 | 678 | 703 | 729 | 754 | 780 | 805 |
| MGAL | 4305.4 | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 |





| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1640 | 1725 | 1807 | 1889 | 1975 | 2057 | 2142 | 2224 | 2306 | 2391 | 2473 | 2559 | 2641 |
| ELEV M | 500 | 526 | 551 | 576 | 602 | 627 | 653 | 678 | 703 | 729 | 754 | 780 | 805 |
| MGAL | 4305.4 | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 |

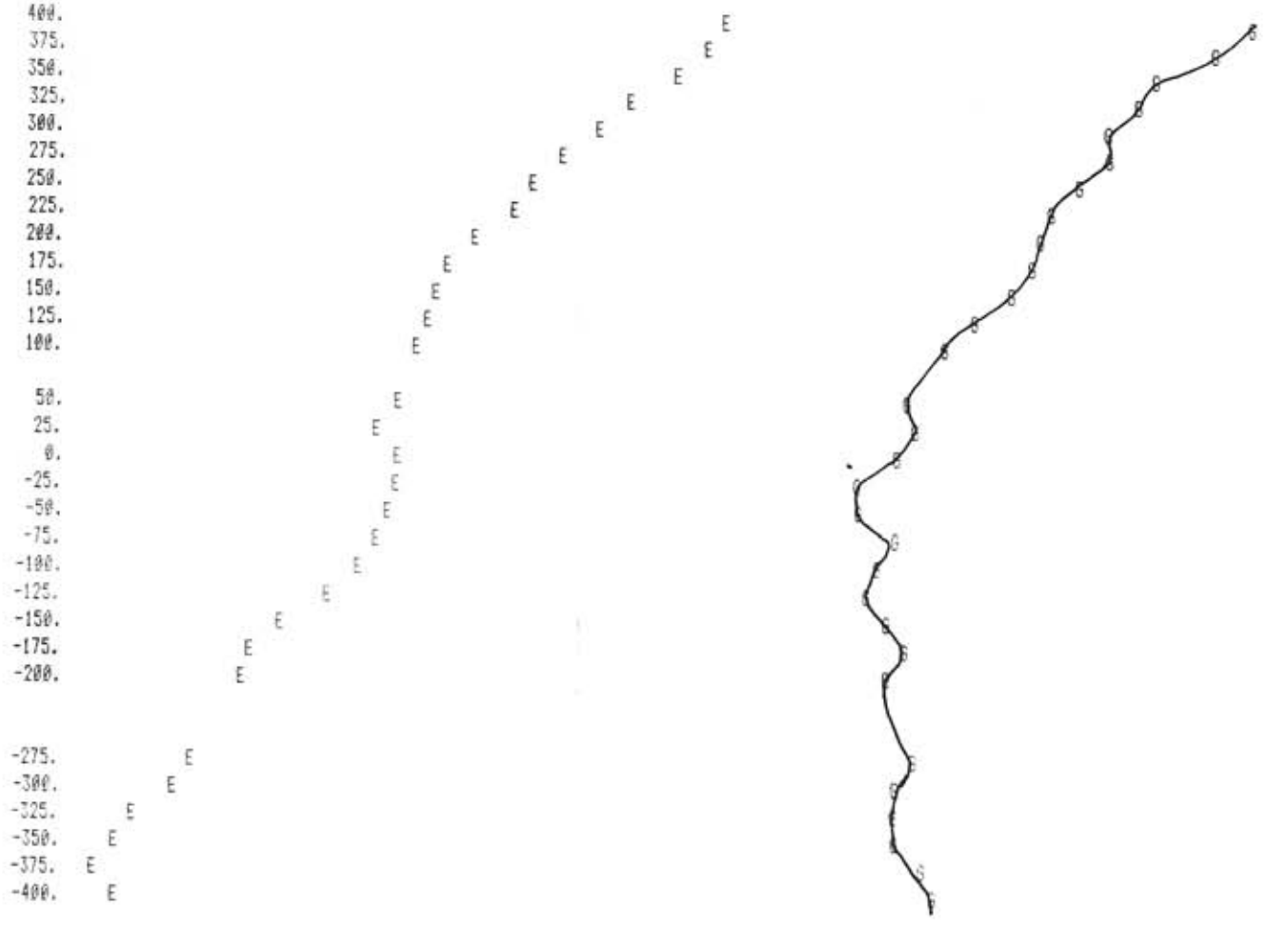

Figure 10

PROFILE OF LINE L400N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1715 | 1797 | 1879 | 1965 | 2047 | 2132 | 2214 | 2296 | 2381 | 2463 | 2549 | 2631 | 2713 |
| ELEV M | 523 | 548 | 573 | 599 | 624 | 650 | 675 | 700 | 726 | 751 | 777 | 802 | 827 |
| MGAL | 4305.5 | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 |




| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1715 | 1797 | 1879 | 1965 | 2047 | 2132 | 2214 | 2296 | 2381 | 2463 | 2549 | 2631 | 2713 |
| ELEV M | 523 | 548 | 573 | 599 | 624 | 650 | 675 | 700 | 726 | 751 | 777 | 802 | 827 |
| MGAL | 4305.5 | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 |

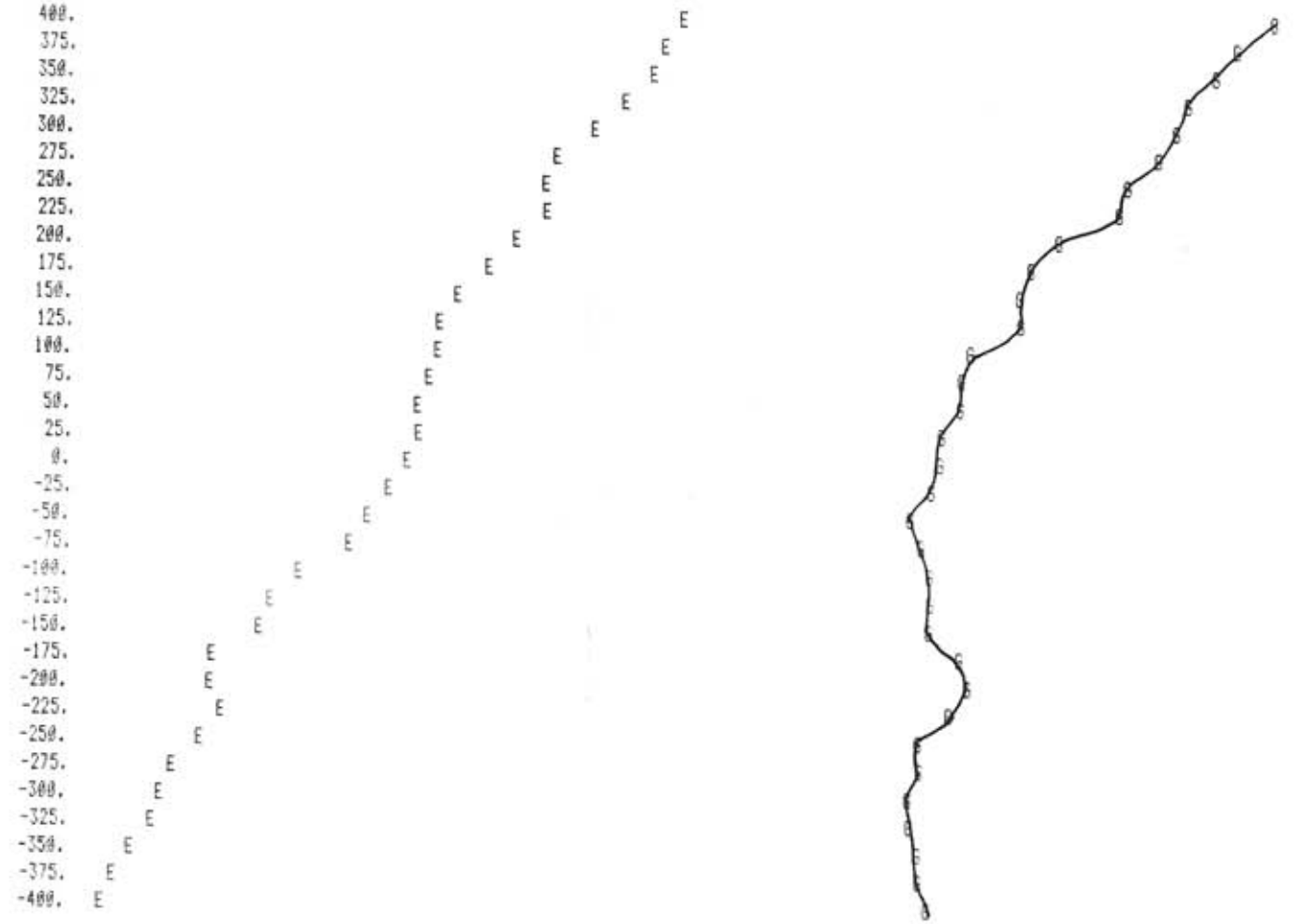
Figure 11

PROFILE OF LINE L350N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1732 | 1814 | 1896 | 1981 | 2063 | 2148 | 2230 | 2312 | 2398 | 2480 | 2565 | 2647 | 2729 |
| ELEV M | 528 | 553 | 578 | 604 | 629 | 655 | 680 | 705 | 731 | 756 | 782 | 807 | 832 |
| MGAL | 4305.5 | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1732 | 1814 | 1896 | 1981 | 2063 | 2148 | 2230 | 2312 | 2398 | 2480 | 2565 | 2647 | 2729 |
| ELEV M | 528 | 553 | 578 | 604 | 629 | 655 | 680 | 705 | 731 | 756 | 782 | 807 | 832 |
| MGAL | 4305.5 | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 |

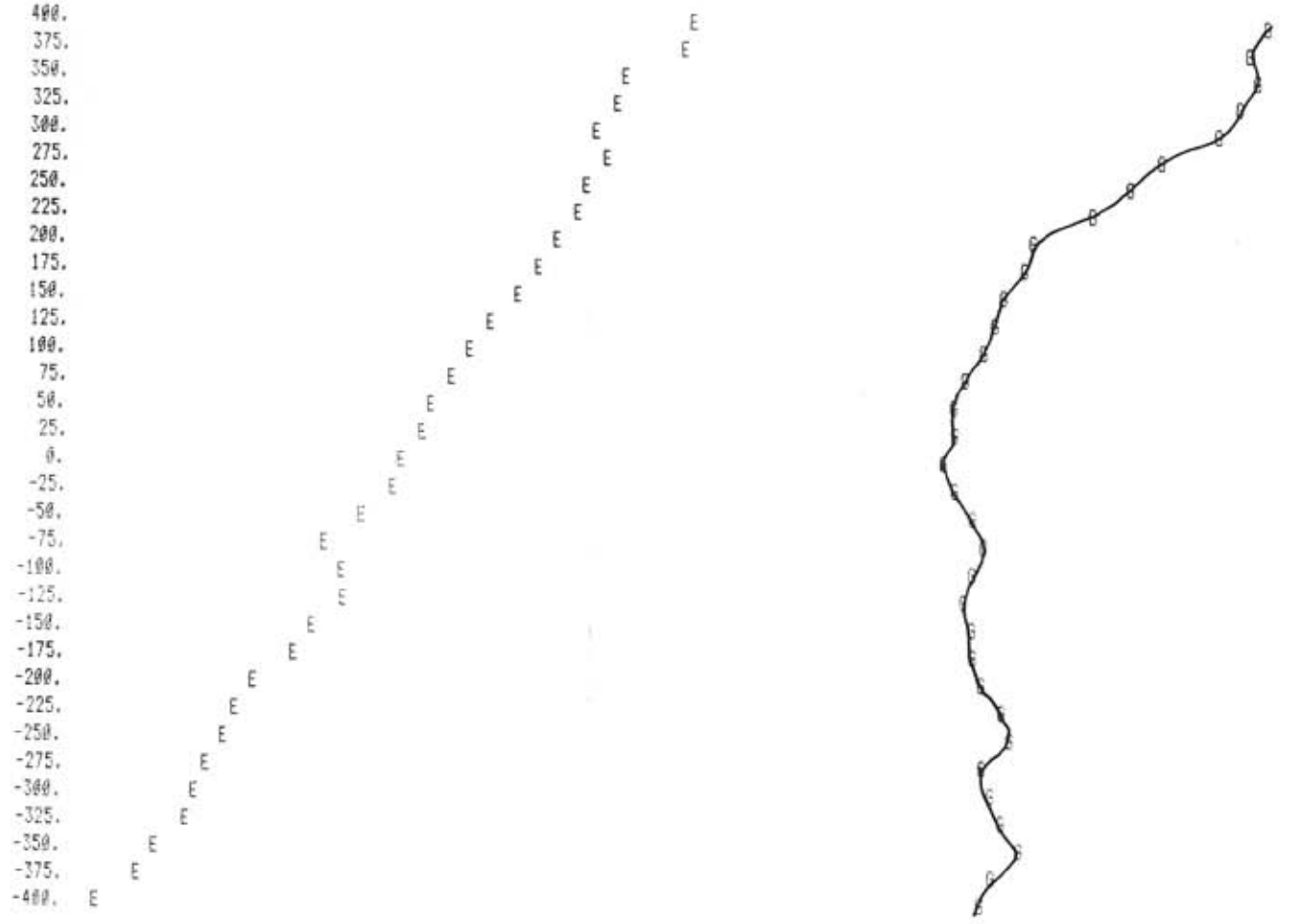
Figure 12

PROFILE OF LINE L300N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1709 | 1791 | 1876 | 1958 | 2040 | 2125 | 2208 | 2293 | 2375 | 2457 | 2542 | 2624 | 2709 |
| ELEV M | 521 | 546 | 572 | 597 | 622 | 648 | 673 | 699 | 724 | 749 | 775 | 800 | 826 |
| MGAL | 4305.5 | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 |





| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1709 | 1791 | 1876 | 1958 | 2040 | 2125 | 2208 | 2293 | 2375 | 2457 | 2542 | 2624 | 2709 |
| ELEV M | 521 | 546 | 572 | 597 | 622 | 648 | 673 | 699 | 724 | 749 | 775 | 800 | 826 |
| MGAL | 4305.5 | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 |

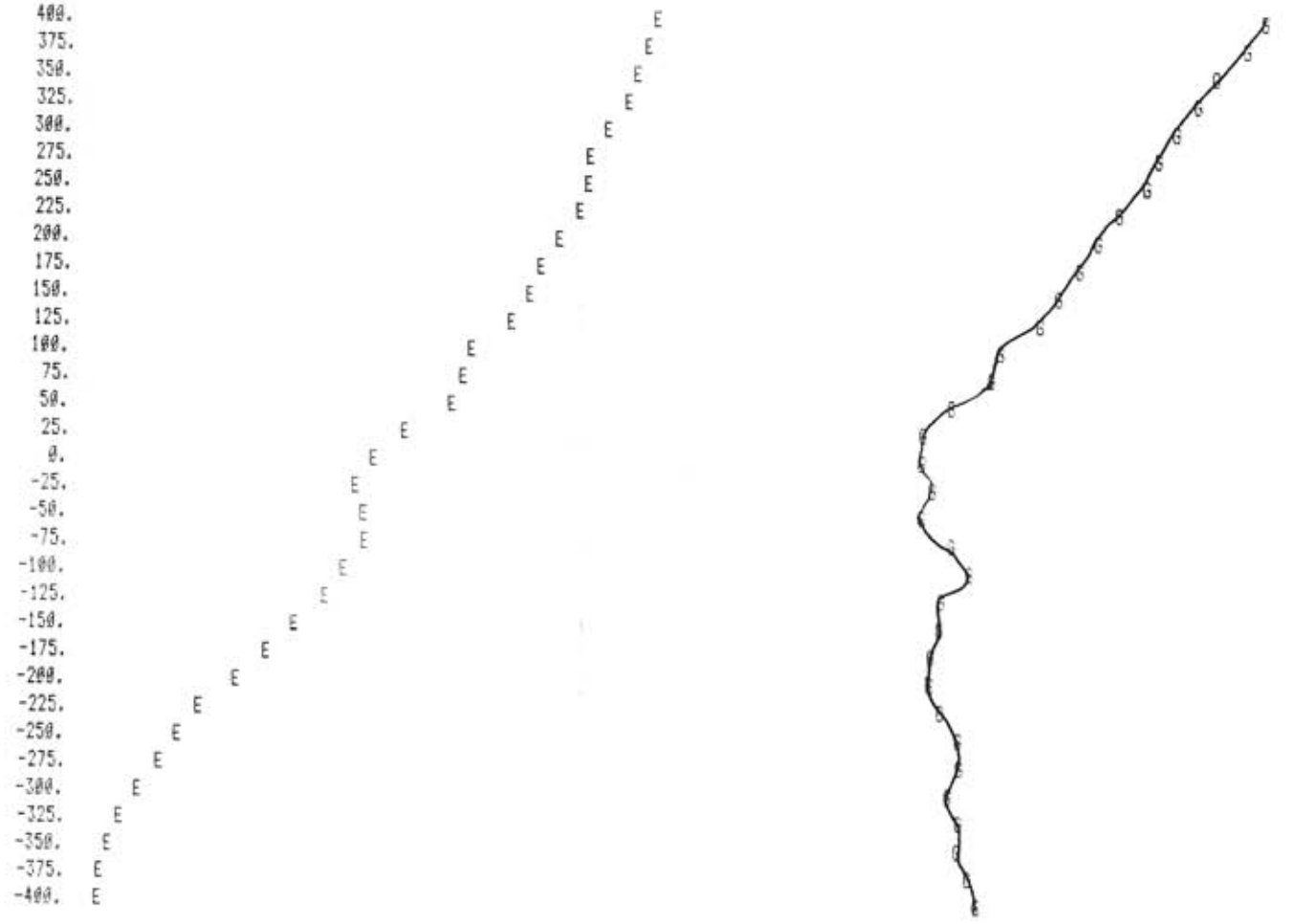

Figure 13

PROFILE OF LINE L250N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1742 | 1824 | 1909 | 1991 | 2073 | 2158 | 2240 | 2326 | 2408 | 2490 | 2575 | 2657 | 2742 |
| ELEV M | 531 | 556 | 582 | 607 | 632 | 658 | 683 | 709 | 734 | 759 | 785 | 810 | 836 |
| MGAL | 4305.8 | 4306.3 | 4306.8 | 4307.3 | 4307.8 | 4308.3 | 4308.8 | 4309.3 | 4309.8 | 4310.3 | 4310.8 | 4311.3 | 4311.8 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1742 | 1824 | 1909 | 1991 | 2073 | 2158 | 2240 | 2326 | 2408 | 2490 | 2575 | 2657 | 2742 |
| ELEV M | 531 | 556 | 582 | 607 | 632 | 658 | 683 | 709 | 734 | 759 | 785 | 810 | 836 |
| MGAL | 4305.8 | 4306.3 | 4306.8 | 4307.3 | 4307.8 | 4308.3 | 4308.8 | 4309.3 | 4309.8 | 4310.3 | 4310.8 | 4311.3 | 4311.8 |

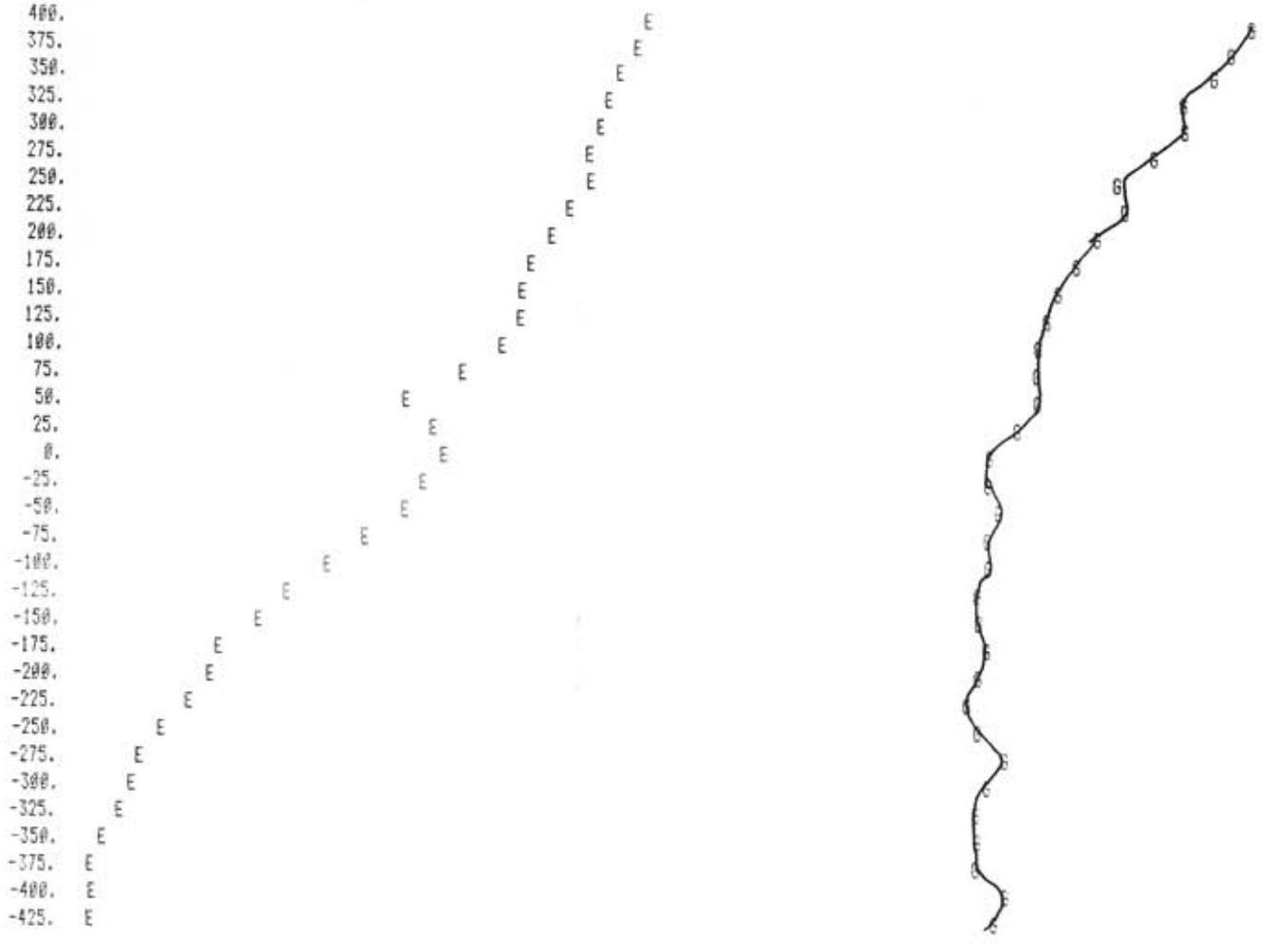
Figure 14

PROFILE OF LINE L200N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1745 | 1830 | 1912 | 1994 | 2080 | 2162 | 2247 | 2329 | 2411 | 2496 | 2578 | 2664 | 2746 |
| ELEV M | 532 | 558 | 583 | 608 | 634 | 659 | 685 | 710 | 735 | 761 | 786 | 812 | 837 |
| MGAL | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 |





| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1745 | 1830 | 1912 | 1994 | 2080 | 2162 | 2247 | 2329 | 2411 | 2496 | 2578 | 2664 | 2746 |
| ELEV M | 532 | 558 | 583 | 608 | 634 | 659 | 685 | 710 | 735 | 761 | 786 | 812 | 837 |
| MGAL | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 |

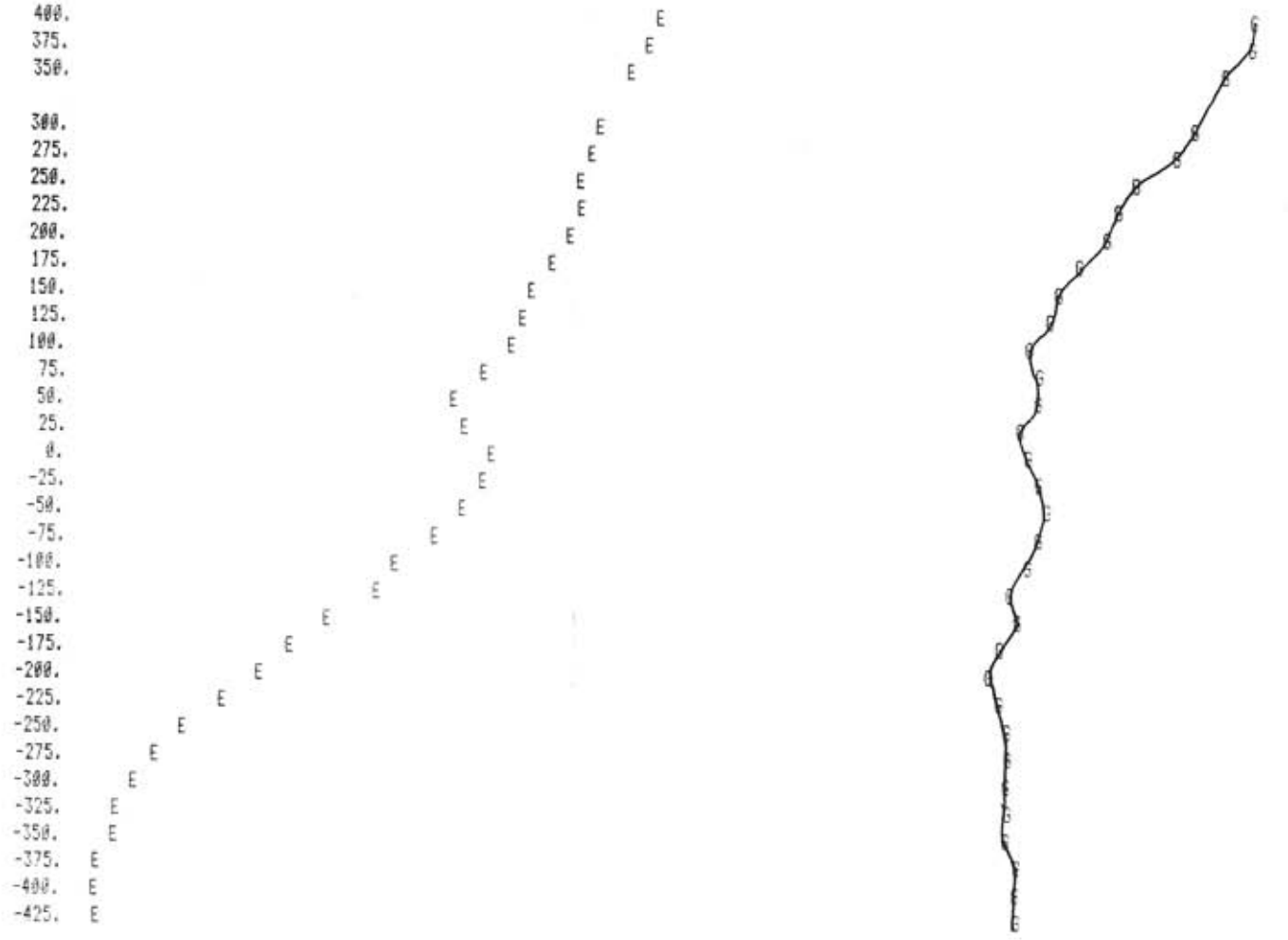

Figure 15

PROFILE OF LINE L150N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1748 | 1830 | 1916 | 1998 | 2080 | 2165 | 2247 | 2332 | 2414 | 2496 | 2582 | 2664 | 2749 |
| ELEV M | 533 | 558 | 584 | 609 | 634 | 660 | 685 | 711 | 736 | 761 | 787 | 812 | 838 |
| MGAL | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 |





| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1748 | 1830 | 1916 | 1998 | 2080 | 2165 | 2247 | 2332 | 2414 | 2496 | 2582 | 2664 | 2749 |
| ELEV M | 533 | 558 | 584 | 609 | 634 | 660 | 685 | 711 | 736 | 761 | 787 | 812 | 838 |
| MGAL | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 |

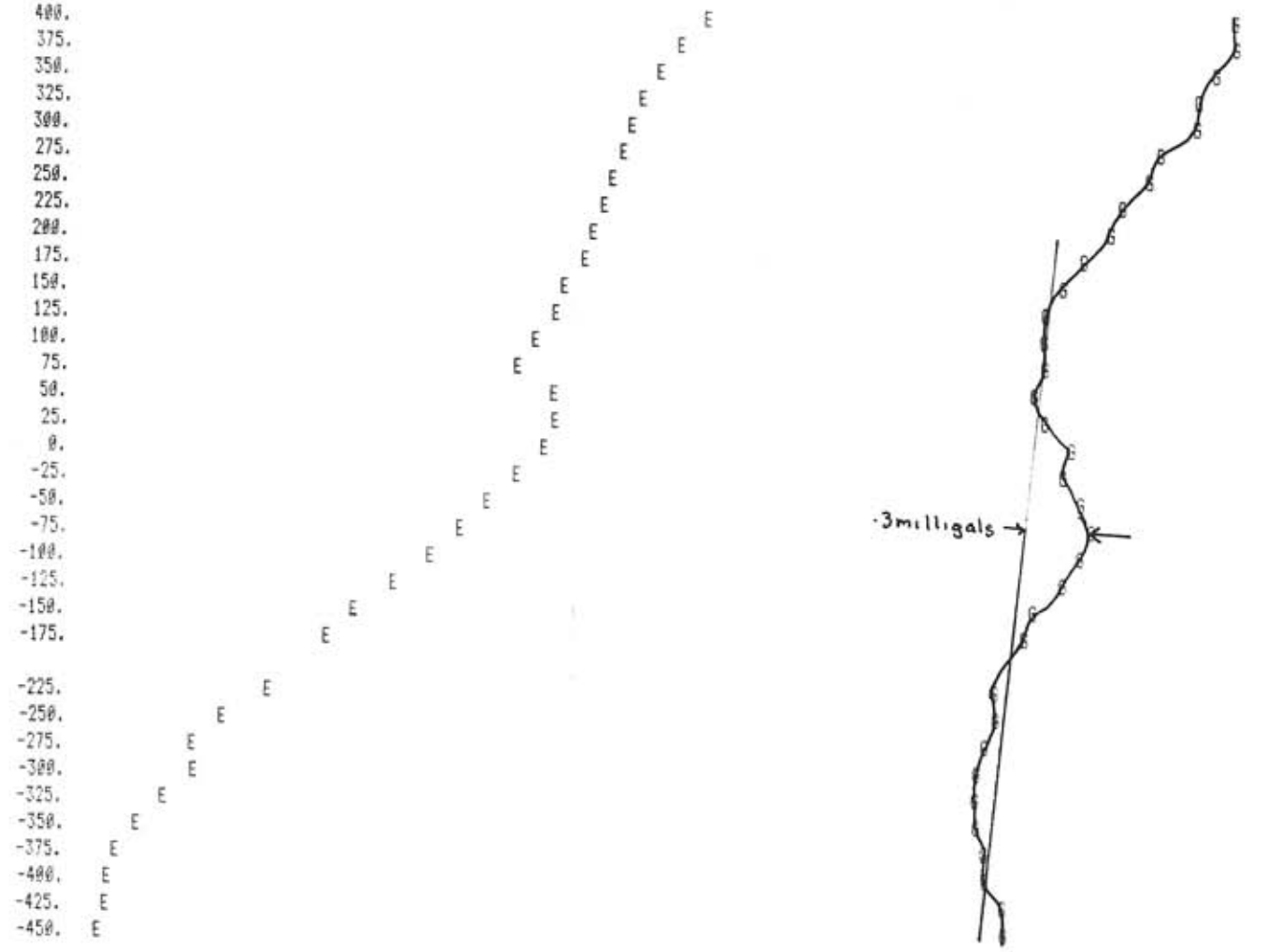

Figure 16

PROFILE OF LINE L100N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1715 | 1797 | 1883 | 1965 | 2047 | 2132 | 2214 | 2299 | 2381 | 2463 | 2549 | 2631 | 2716 |
| ELEV M | 523 | 548 | 574 | 599 | 624 | 650 | 675 | 701 | 726 | 751 | 777 | 802 | 828 |
| MGAL | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1715 | 1797 | 1883 | 1965 | 2047 | 2132 | 2214 | 2299 | 2381 | 2463 | 2549 | 2631 | 2716 |
| ELEV M | 523 | 548 | 574 | 599 | 624 | 650 | 675 | 701 | 726 | 751 | 777 | 802 | 828 |
| MGAL | 4305.9 | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 |

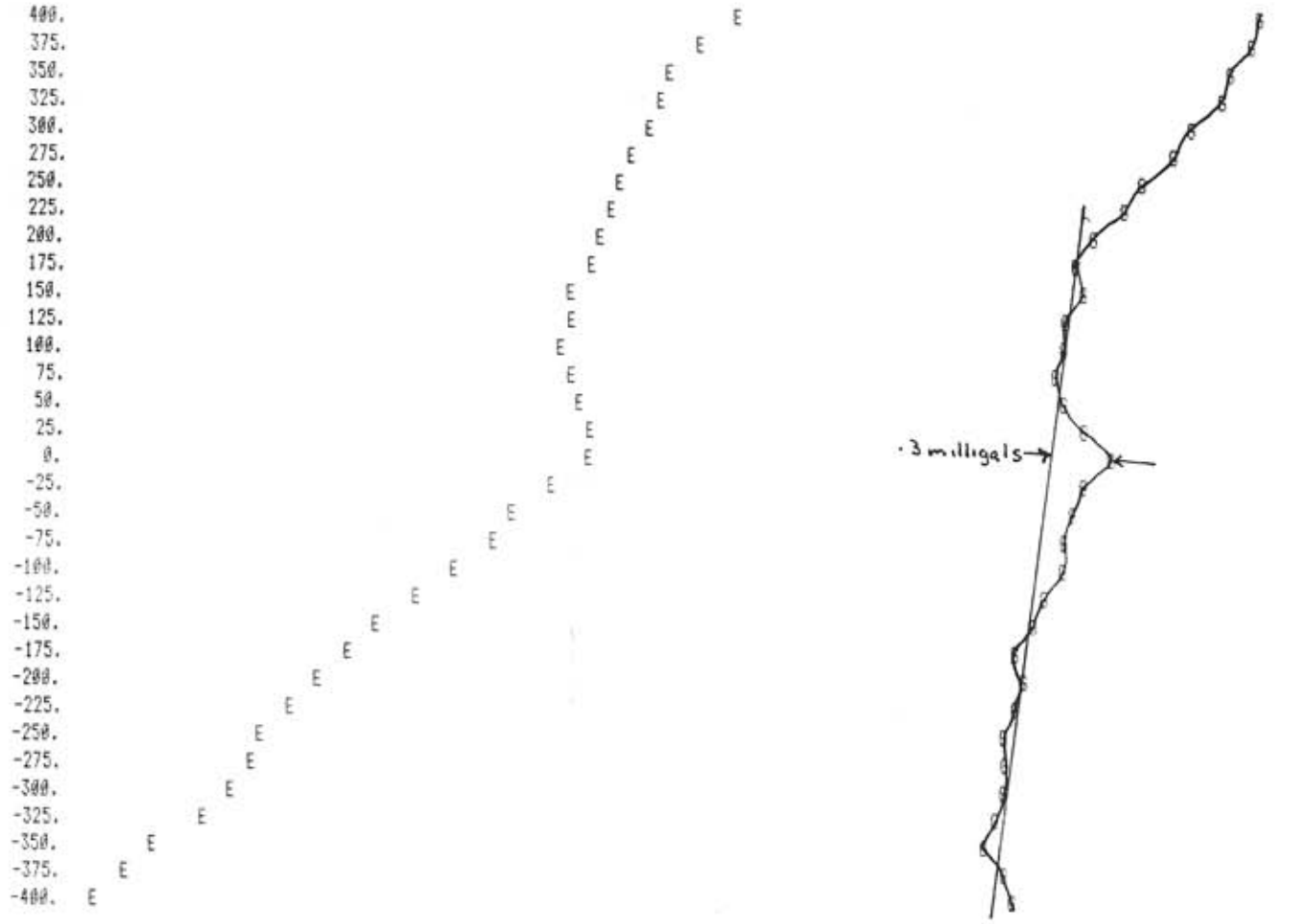
Figure 17

PROFILE OF LINE L50N

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967

G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1709 | 1794 | 1876 | 1961 | 2043 | 2125 | 2211 | 2293 | 2378 | 2460 | 2542 | 2627 | 2709 |
| ELEV M | 521 | 547 | 572 | 598 | 623 | 648 | 674 | 699 | 725 | 750 | 775 | 801 | 826 |
| MGAL | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |





| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1709 | 1794 | 1876 | 1961 | 2043 | 2125 | 2211 | 2293 | 2378 | 2460 | 2542 | 2627 | 2709 |
| ELEV M | 521 | 547 | 572 | 598 | 623 | 648 | 674 | 699 | 725 | 750 | 775 | 801 | 826 |
| MGAL | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 |

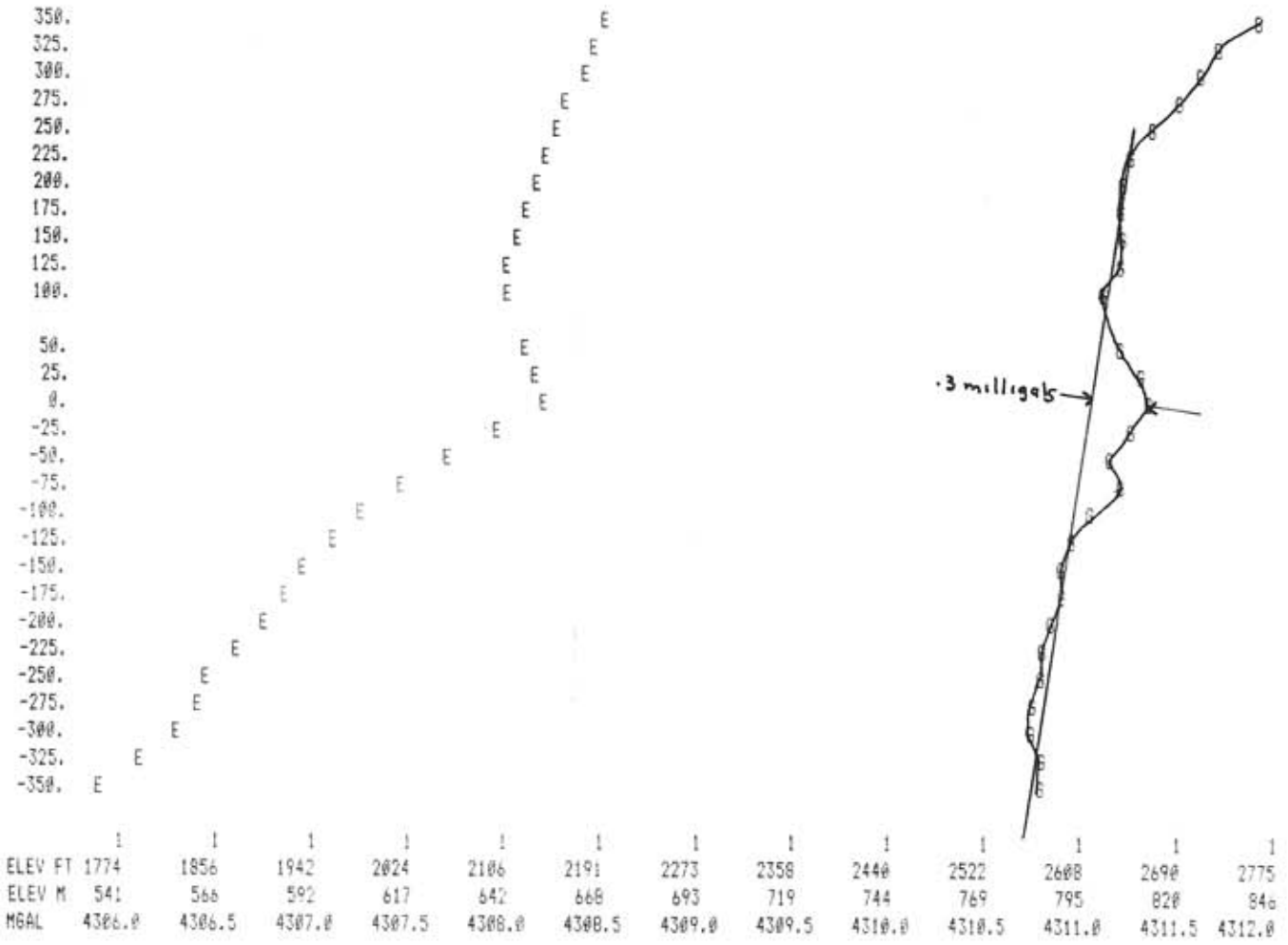

Figure 18

PROFILE OF LINE L00N

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1774 | 1856 | 1942 | 2024 | 2106 | 2191 | 2273 | 2358 | 2440 | 2522 | 2608 | 2690 | 2775 |
| ELEV M | 541 | 566 | 592 | 617 | 642 | 668 | 693 | 719 | 744 | 769 | 795 | 820 | 846 |
| MGAL | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1774 | 1856 | 1942 | 2024 | 2106 | 2191 | 2273 | 2358 | 2440 | 2522 | 2608 | 2690 | 2775 |
| ELEV M | 541 | 566 | 592 | 617 | 642 | 668 | 693 | 719 | 744 | 769 | 795 | 820 | 846 |
| MGAL | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 |

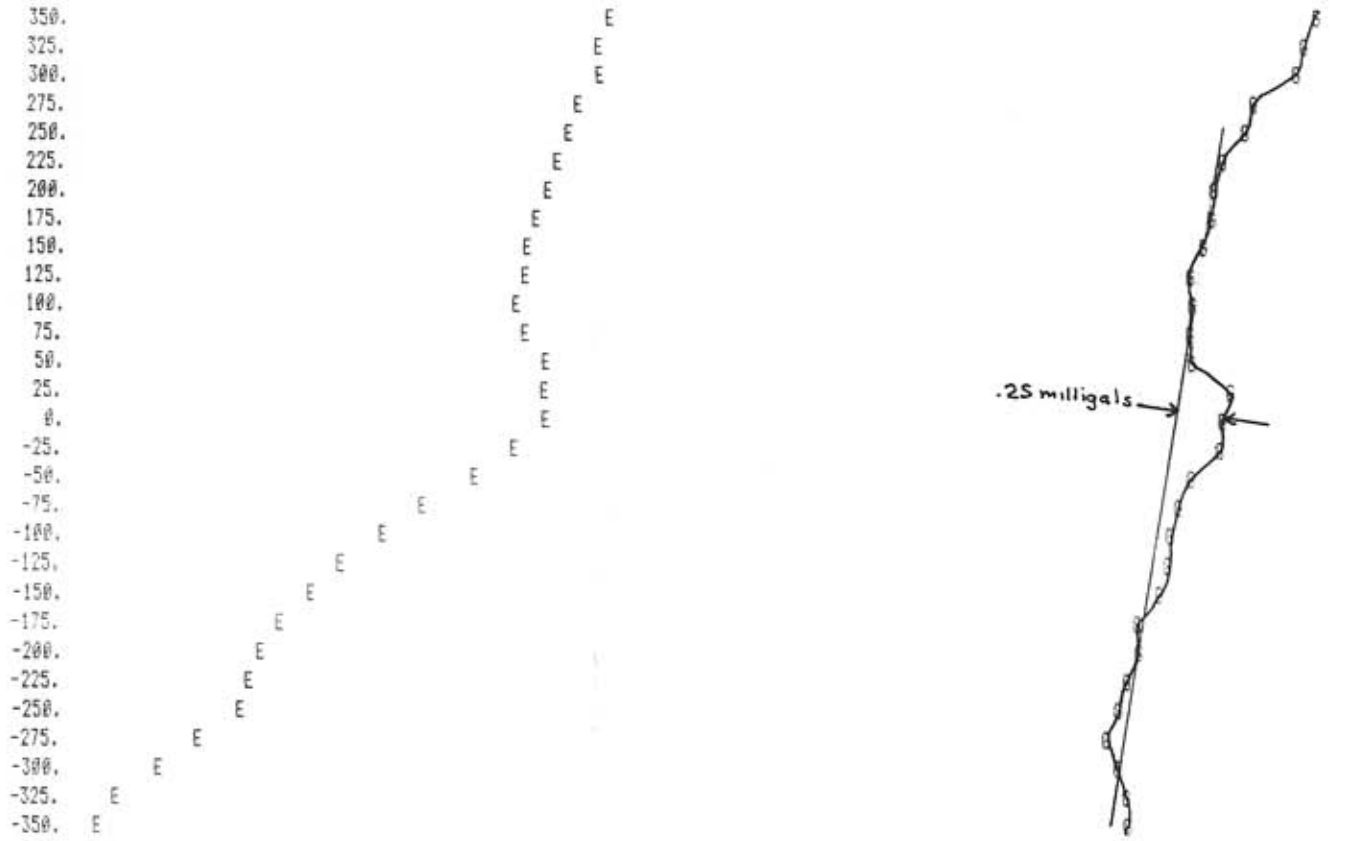
Figure 19

PROFILE OF LINE L50S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967

G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1781 | 1863 | 1948 | 2030 | 2112 | 2198 | 2280 | 2365 | 2447 | 2529 | 2614 | 2696 | 2782 |
| ELEV M | 543 | 568 | 594 | 619 | 644 | 670 | 695 | 721 | 746 | 771 | 797 | 822 | 848 |
| MGAL | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 |



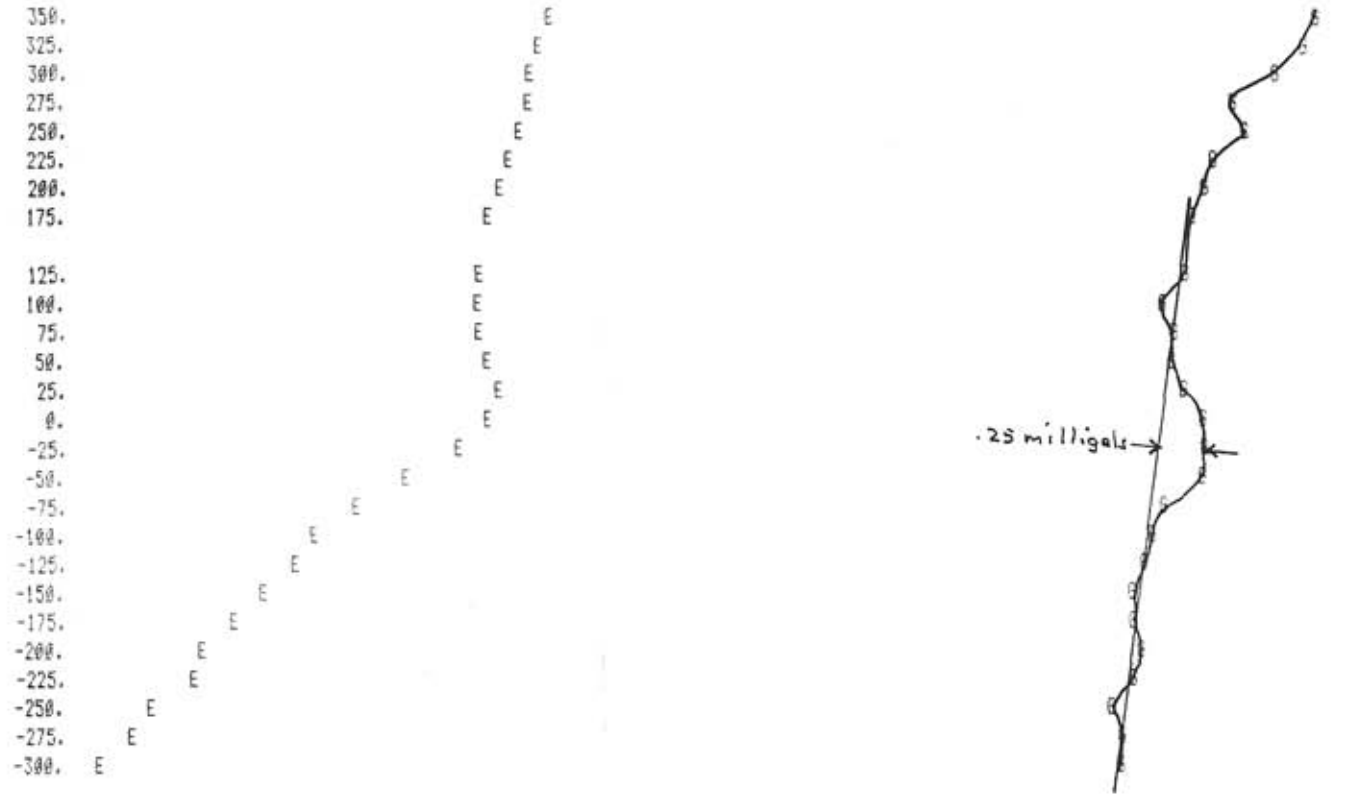

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1781 | 1863 | 1948 | 2030 | 2112 | 2198 | 2280 | 2365 | 2447 | 2529 | 2614 | 2696 | 2782 |
| ELEV M | 543 | 568 | 594 | 619 | 644 | 670 | 695 | 721 | 746 | 771 | 797 | 822 | 848 |
| MGAL | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 |

Figure 20

PROFILE OF LINE L100S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967
G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1817 | 1899 | 1984 | 2066 | 2152 | 2234 | 2316 | 2401 | 2483 | 2568 | 2650 | 2732 | 2818 |
| ELEV M | 554 | 579 | 605 | 630 | 656 | 681 | 706 | 732 | 757 | 783 | 808 | 833 | 859 |
| MGAL | 4306.1 | 4306.6 | 4307.1 | 4307.6 | 4308.1 | 4308.6 | 4309.1 | 4309.6 | 4310.1 | 4310.6 | 4311.1 | 4311.6 | 4312.1 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |




| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1817 | 1899 | 1984 | 2066 | 2152 | 2234 | 2316 | 2401 | 2483 | 2568 | 2650 | 2732 | 2818 |
| ELEV M | 554 | 579 | 605 | 630 | 656 | 681 | 706 | 732 | 757 | 783 | 808 | 833 | 859 |
| MGAL | 4306.1 | 4306.6 | 4307.1 | 4307.6 | 4308.1 | 4308.6 | 4309.1 | 4309.6 | 4310.1 | 4310.6 | 4311.1 | 4311.6 | 4312.1 |

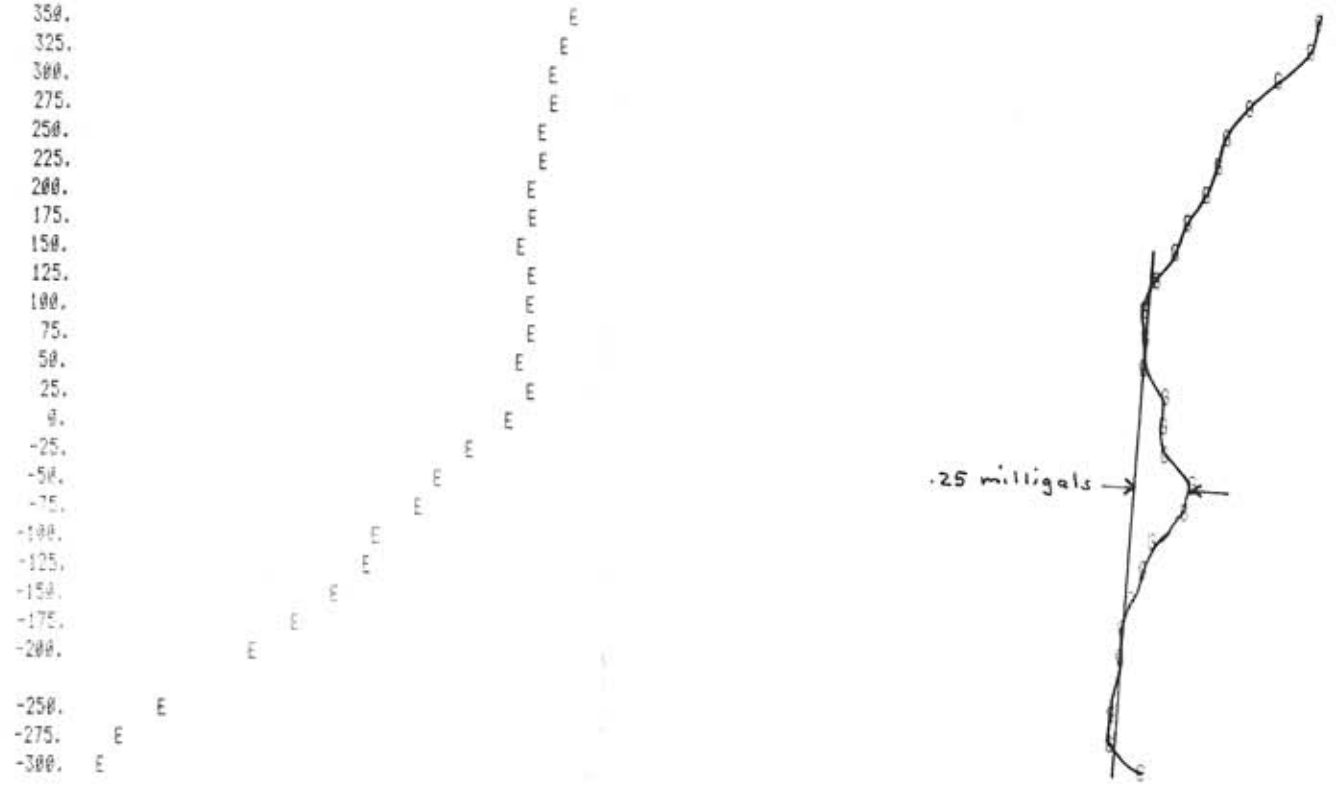
Figure 21

PROFILE OF LINE L150S

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1781 | 1866 | 1948 | 2034 | 2116 | 2198 | 2283 | 2365 | 2450 | 2532 | 2614 | 2700 | 2782 |
| ELEV M | 543 | 569 | 594 | 620 | 645 | 670 | 696 | 721 | 747 | 772 | 797 | 823 | 848 |
| MGAL | 4306.2 | 4306.7 | 4307.2 | 4307.7 | 4308.2 | 4308.7 | 4309.2 | 4309.7 | 4310.2 | 4310.7 | 4311.2 | 4311.7 | 4312.2 |




| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1781 | 1866 | 1948 | 2034 | 2116 | 2198 | 2283 | 2365 | 2450 | 2532 | 2614 | 2700 | 2782 |
| ELEV M | 543 | 569 | 594 | 620 | 645 | 670 | 696 | 721 | 747 | 772 | 797 | 823 | 848 |
| MGAL | 4306.2 | 4306.7 | 4307.2 | 4307.7 | 4308.2 | 4308.7 | 4309.2 | 4309.7 | 4310.2 | 4310.7 | 4311.2 | 4311.7 | 4312.2 |

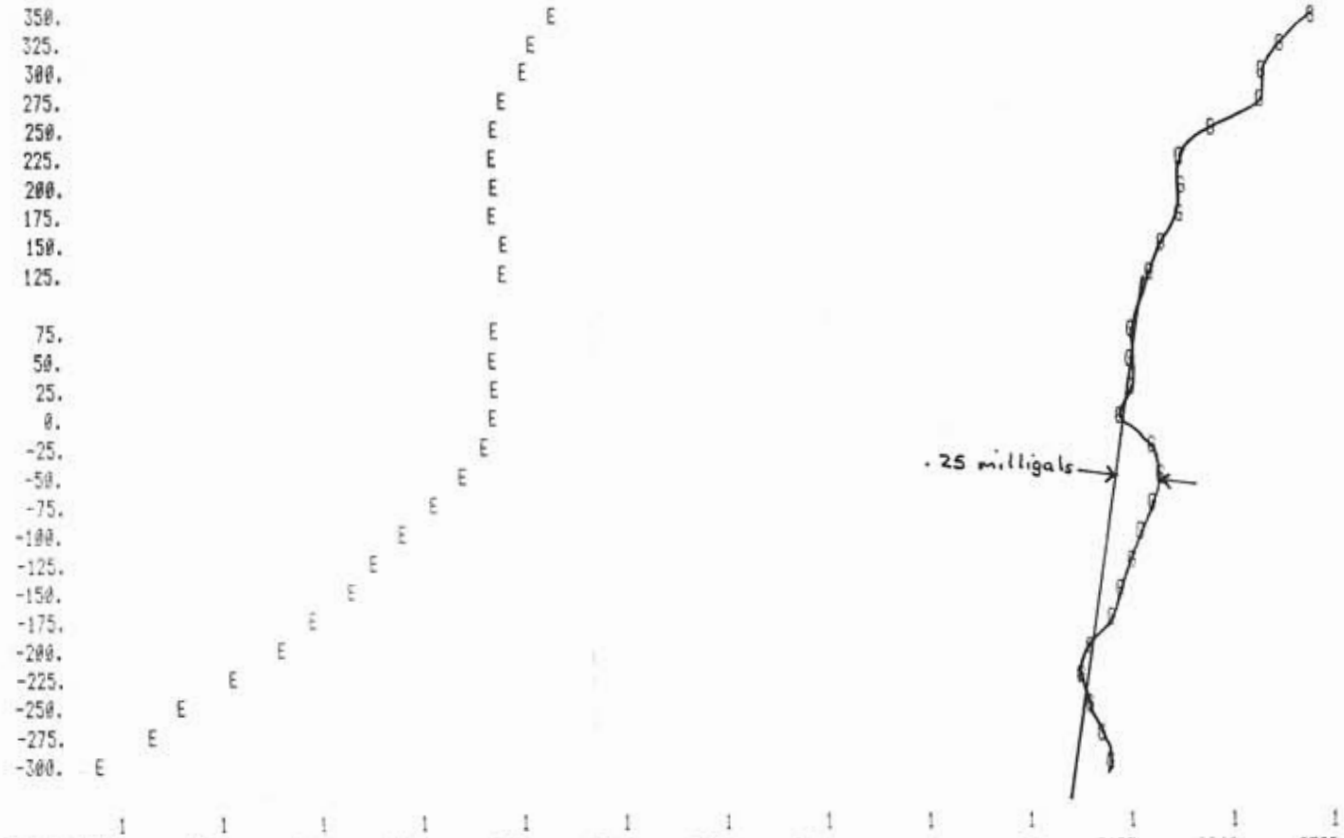
Figure 22

PROFILE OF LINE L200S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967

G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1794 | 1876 | 1961 | 2043 | 2129 | 2211 | 2293 | 2378 | 2460 | 2545 | 2627 | 2709 | 2795 |
| ELEV M | 547 | 572 | 598 | 623 | 649 | 674 | 699 | 725 | 750 | 776 | 801 | 826 | 852 |
| MGAL | 4306.3 | 4306.8 | 4307.3 | 4307.8 | 4308.3 | 4308.8 | 4309.3 | 4309.8 | 4310.3 | 4310.8 | 4311.3 | 4311.8 | 4312.3 |




| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1794 | 1876 | 1961 | 2043 | 2129 | 2211 | 2293 | 2378 | 2460 | 2545 | 2627 | 2709 | 2795 |
| ELEV M | 547 | 572 | 598 | 623 | 649 | 674 | 699 | 725 | 750 | 776 | 801 | 826 | 852 |
| MGAL | 4306.3 | 4306.8 | 4307.3 | 4307.8 | 4308.3 | 4308.8 | 4309.3 | 4309.8 | 4310.3 | 4310.8 | 4311.3 | 4311.8 | 4312.3 |

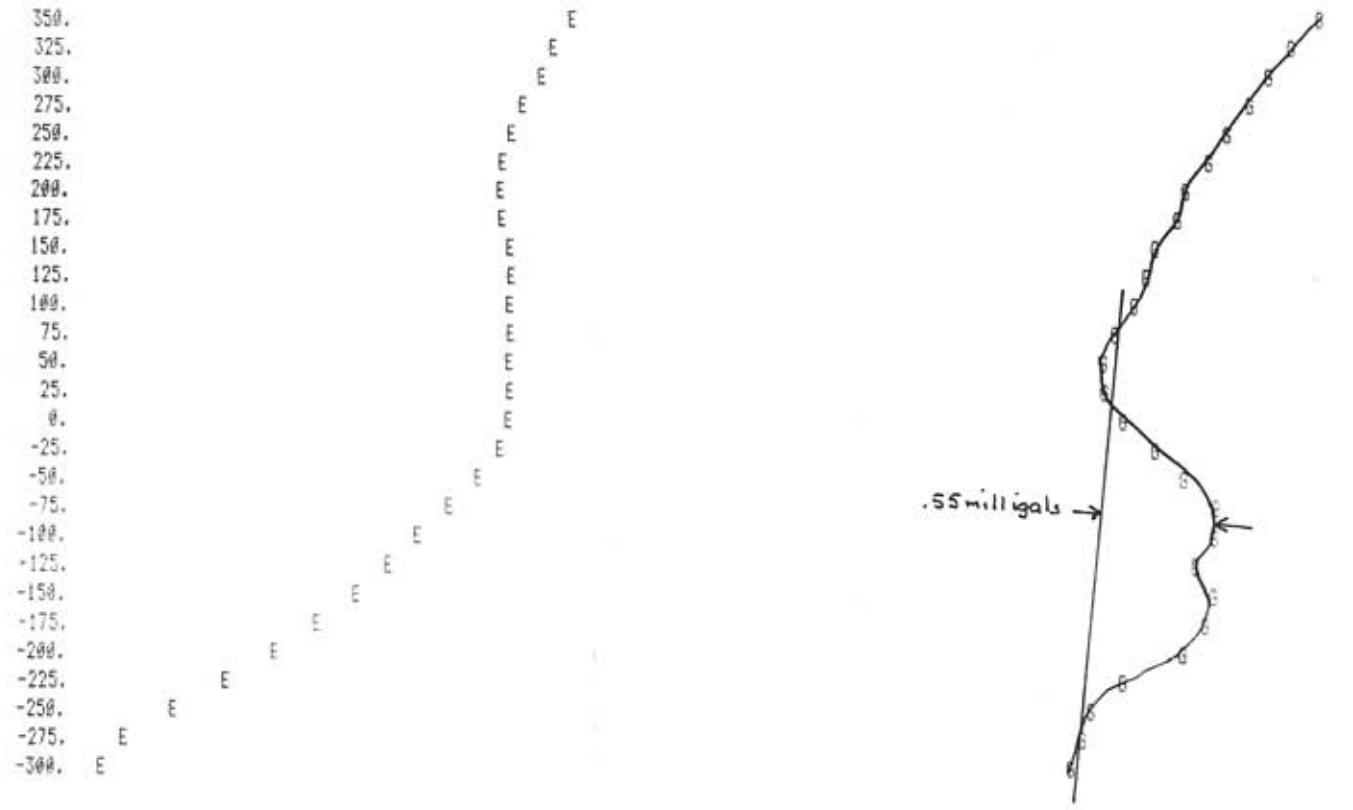
Figure 23

PROFILE OF LINE L250S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967

G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1784 | 1870 | 1952 | 2034 | 2119 | 2201 | 2286 | 2368 | 2450 | 2536 | 2618 | 2703 | 2785 |
| ELEV M | 544 | 570 | 595 | 620 | 646 | 671 | 697 | 722 | 747 | 773 | 798 | 824 | 849 |
| MGAL | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 | 4312.4 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1784 | 1870 | 1952 | 2034 | 2119 | 2201 | 2286 | 2368 | 2450 | 2536 | 2618 | 2703 | 2785 |
| ELEV M | 544 | 570 | 595 | 620 | 646 | 671 | 697 | 722 | 747 | 773 | 798 | 824 | 849 |
| MGAL | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 | 4312.4 |

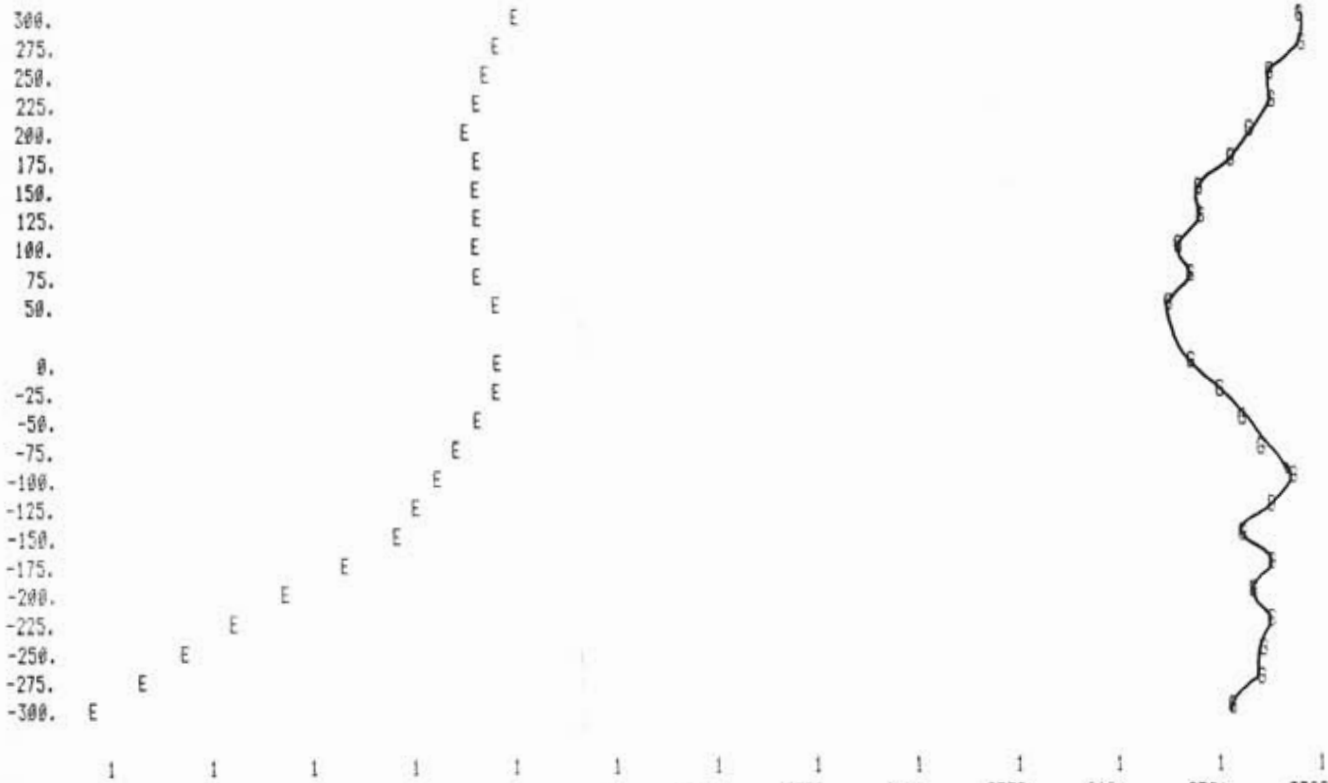
Figure 24

PROFILE OF LINE L300S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967

G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1788 | 1873 | 1955 | 2040 | 2122 | 2204 | 2290 | 2372 | 2457 | 2539 | 2621 | 2706 | 2788 |
| ELEV M | 545 | 571 | 596 | 622 | 647 | 672 | 698 | 723 | 749 | 774 | 799 | 825 | 850 |
| MGAL | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |





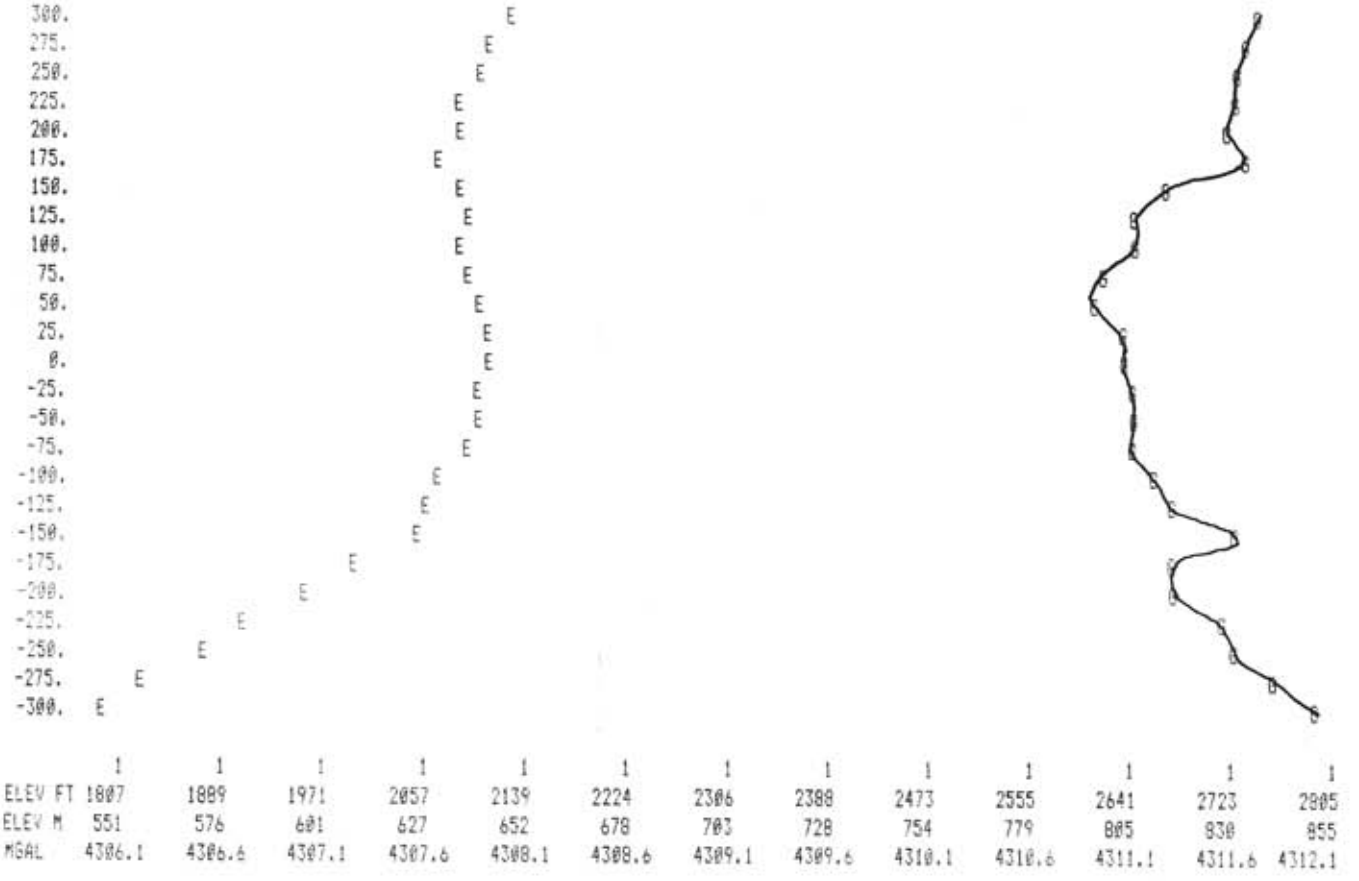
| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1788 | 1873 | 1955 | 2040 | 2122 | 2204 | 2290 | 2372 | 2457 | 2539 | 2621 | 2706 | 2788 |
| ELEV M | 545 | 571 | 596 | 622 | 647 | 672 | 698 | 723 | 749 | 774 | 799 | 825 | 850 |
| MGAL | 4306.0 | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 |


Figure 25

PROFILE OF LINE L350S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967
G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1807 | 1889 | 1971 | 2057 | 2139 | 2224 | 2306 | 2388 | 2473 | 2555 | 2641 | 2723 | 2805 |
| ELEV M | 551 | 576 | 601 | 627 | 652 | 678 | 703 | 728 | 754 | 779 | 805 | 830 | 855 |
| MGAL | 4306.1 | 4306.6 | 4307.1 | 4307.6 | 4308.1 | 4308.6 | 4309.1 | 4309.6 | 4310.1 | 4310.6 | 4311.1 | 4311.6 | 4312.1 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1807 | 1889 | 1971 | 2057 | 2139 | 2224 | 2306 | 2388 | 2473 | 2555 | 2641 | 2723 | 2805 |
| ELEV M | 551 | 576 | 601 | 627 | 652 | 678 | 703 | 728 | 754 | 779 | 805 | 830 | 855 |
| MGAL | 4306.1 | 4306.6 | 4307.1 | 4307.6 | 4308.1 | 4308.6 | 4309.1 | 4309.6 | 4310.1 | 4310.6 | 4311.1 | 4311.6 | 4312.1 |

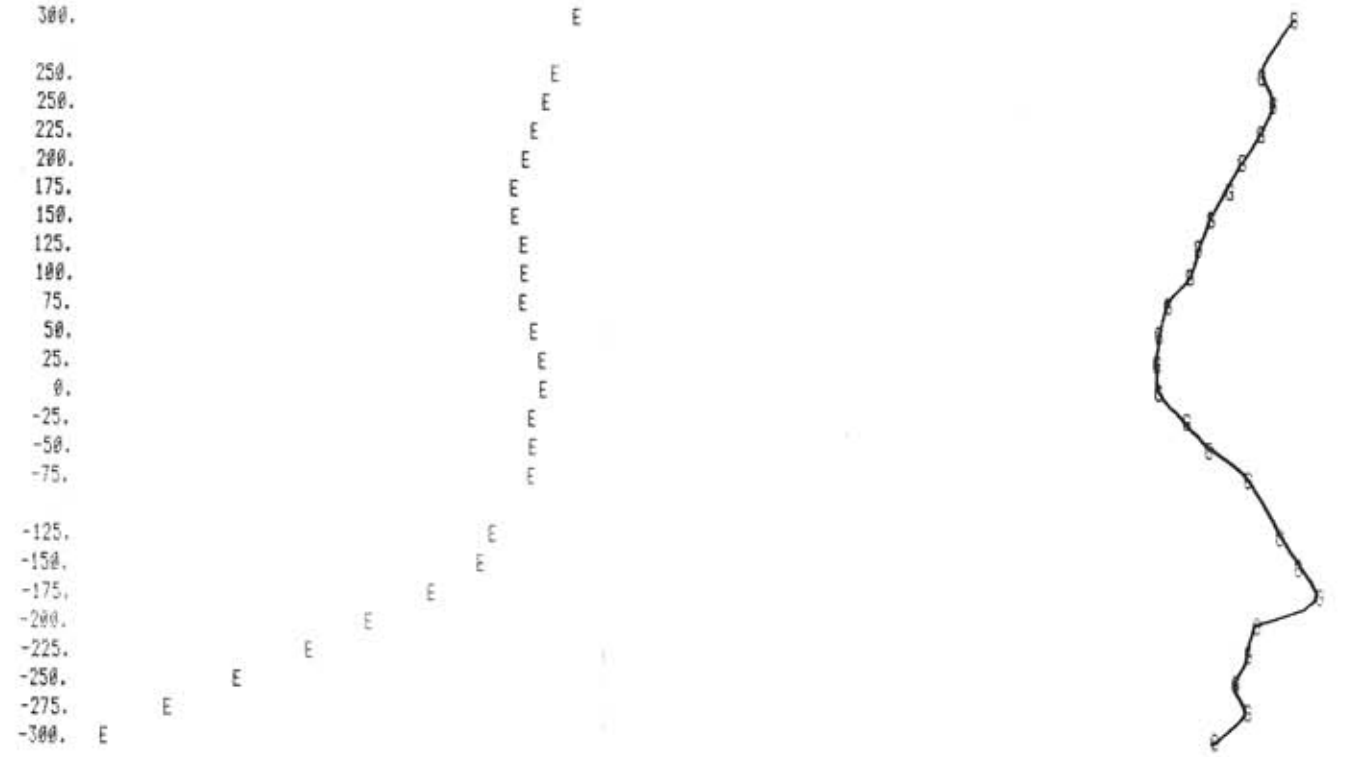
Figure 26

PROFILE OF LINE L400S

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1751 | 1837 | 1919 | 2001 | 2086 | 2168 | 2253 | 2335 | 2417 | 2503 | 2585 | 2670 | 2752 |
| ELEV M | 534 | 560 | 585 | 610 | 636 | 661 | 687 | 712 | 737 | 763 | 788 | 814 | 839 |
| MGAL | 4306.2 | 4306.7 | 4307.2 | 4307.7 | 4308.2 | 4308.7 | 4309.2 | 4309.7 | 4310.2 | 4310.7 | 4311.2 | 4311.7 | 4312.2 |





| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1751 | 1837 | 1919 | 2001 | 2086 | 2168 | 2253 | 2335 | 2417 | 2503 | 2585 | 2670 | 2752 |
| ELEV M | 534 | 560 | 585 | 610 | 636 | 661 | 687 | 712 | 737 | 763 | 788 | 814 | 839 |
| MGAL | 4306.2 | 4306.7 | 4307.2 | 4307.7 | 4308.2 | 4308.7 | 4309.2 | 4309.7 | 4310.2 | 4310.7 | 4311.2 | 4311.7 | 4312.2 |

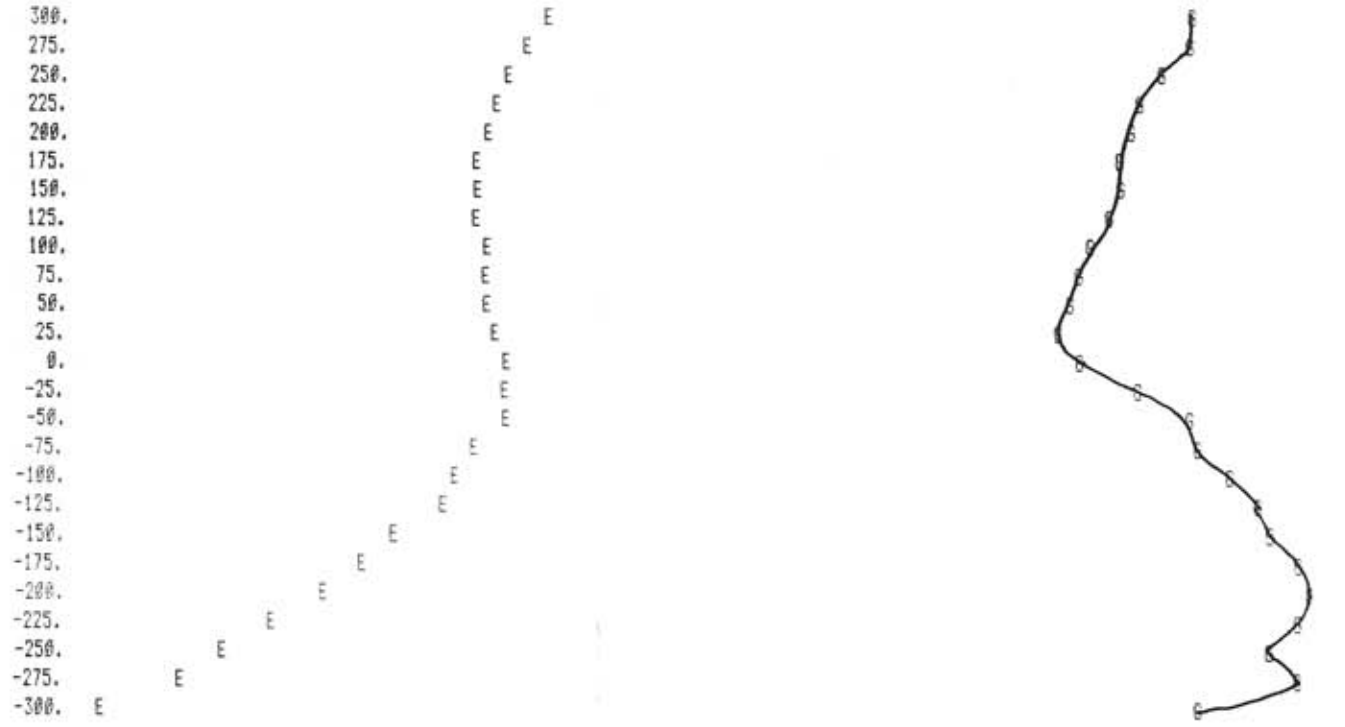

Figure 27

PROFILE OF LINE L450S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967

G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1774 | 1856 | 1942 | 2024 | 2109 | 2191 | 2273 | 2358 | 2440 | 2526 | 2608 | 2690 | 2775 |
| ELEV M | 541 | 566 | 592 | 617 | 643 | 668 | 693 | 719 | 744 | 770 | 795 | 820 | 846 |
| MGAL | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 | 4312.5 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1774 | 1856 | 1942 | 2024 | 2109 | 2191 | 2273 | 2358 | 2440 | 2526 | 2608 | 2690 | 2775 |
| ELEV M | 541 | 566 | 592 | 617 | 643 | 668 | 693 | 719 | 744 | 770 | 795 | 820 | 846 |
| MGAL | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 | 4312.5 |

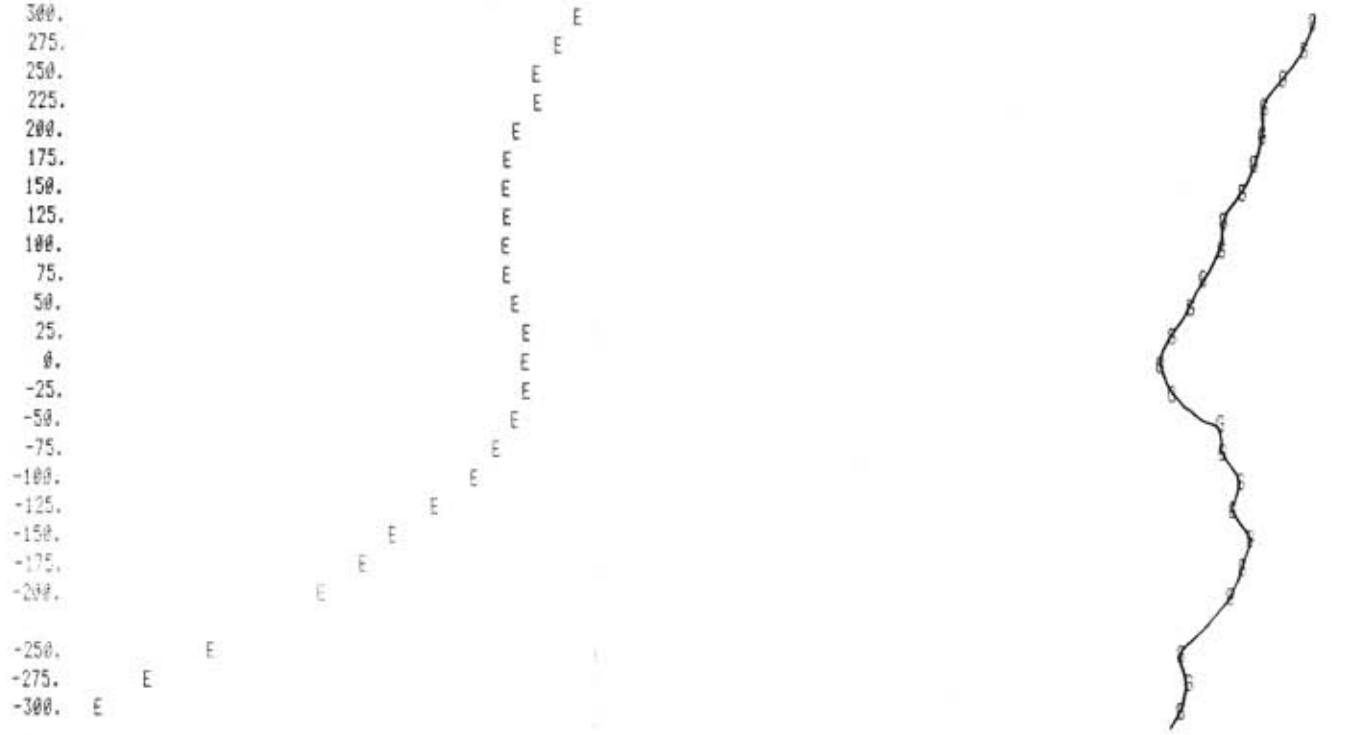
Figure 28

PROFILE OF LINE L500S

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1745 | 1830 | 1912 | 1994 | 2080 | 2162 | 2247 | 2329 | 2411 | 2496 | 2578 | 2664 | 2746 |
| ELEV M | 532 | 558 | 583 | 608 | 634 | 659 | 685 | 710 | 735 | 761 | 786 | 812 | 837 |
| MGAL | 4306.3 | 4306.8 | 4307.3 | 4307.8 | 4308.3 | 4308.8 | 4309.3 | 4309.8 | 4310.3 | 4310.8 | 4311.3 | 4311.8 | 4312.3 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1745 | 1830 | 1912 | 1994 | 2080 | 2162 | 2247 | 2329 | 2411 | 2496 | 2578 | 2664 | 2746 |
| ELEV M | 532 | 558 | 583 | 608 | 634 | 659 | 685 | 710 | 735 | 761 | 786 | 812 | 837 |
| MGAL | 4306.3 | 4306.8 | 4307.3 | 4307.8 | 4308.3 | 4308.8 | 4309.3 | 4309.8 | 4310.3 | 4310.8 | 4311.3 | 4311.8 | 4312.3 |

Figure 29

PROFILE OF LINE L550S

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1788 | 1873 | 1955 | 2037 | 2122 | 2204 | 2290 | 2372 | 2454 | 2539 | 2621 | 2706 | 2788 |
| ELEV M | 545 | 571 | 596 | 621 | 647 | 672 | 698 | 723 | 748 | 774 | 799 | 825 | 850 |
| MGAL | 4306.3 | 4306.8 | 4307.3 | 4307.8 | 4308.3 | 4308.8 | 4309.3 | 4309.8 | 4310.3 | 4310.8 | 4311.3 | 4311.8 | 4312.3 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

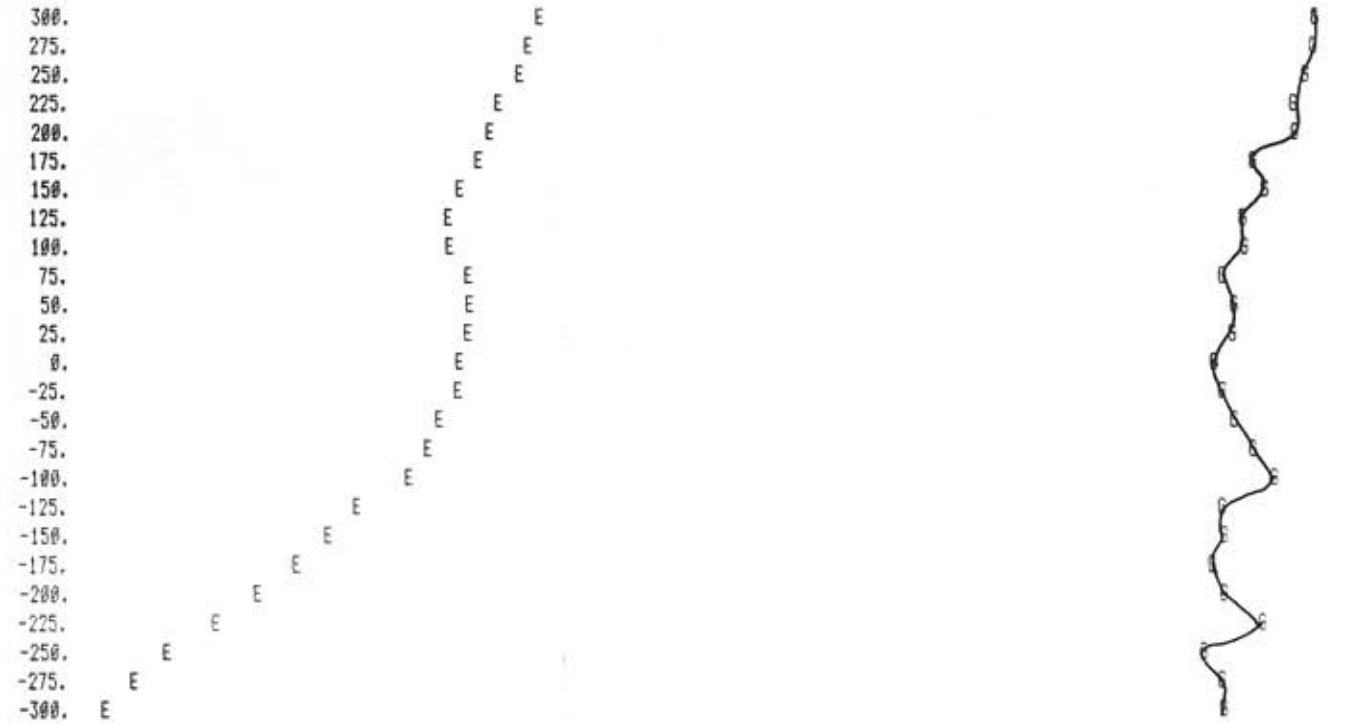

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1788 | 1873 | 1955 | 2037 | 2122 | 2204 | 2290 | 2372 | 2454 | 2539 | 2621 | 2706 | 2788 |
| ELEV M | 545 | 571 | 596 | 621 | 647 | 672 | 698 | 723 | 748 | 774 | 799 | 825 | 850 |
| MGAL | 4306.3 | 4306.8 | 4307.3 | 4307.8 | 4308.3 | 4308.8 | 4309.3 | 4309.8 | 4310.3 | 4310.8 | 4311.3 | 4311.8 | 4312.3 |

Figure 30

PROFILE OF LINE L600S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967
G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1774 | 1860 | 1942 | 2027 | 2109 | 2191 | 2276 | 2358 | 2444 | 2526 | 2608 | 2693 | 2775 |
| ELEV M | 541 | 567 | 592 | 618 | 643 | 668 | 694 | 719 | 745 | 770 | 795 | 821 | 846 |
| MGAL | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 | 4312.4 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |



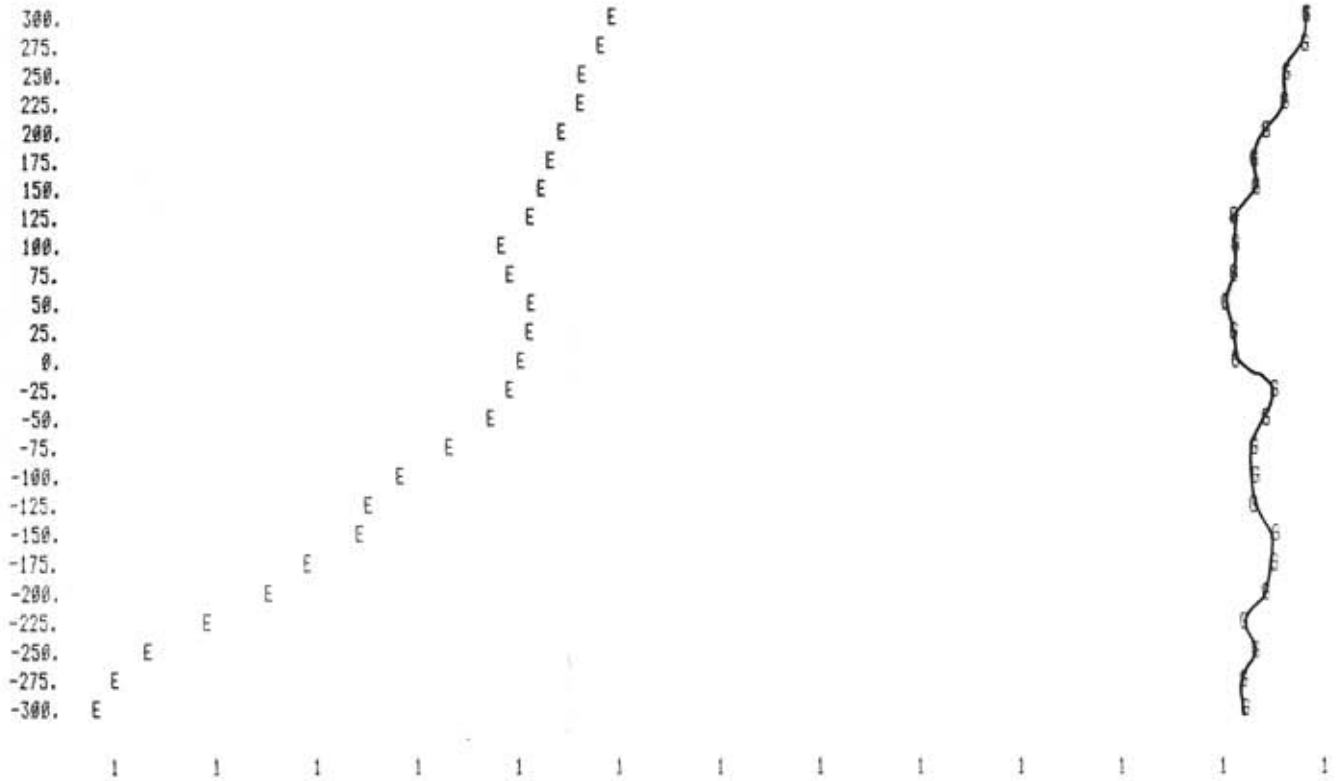

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1774 | 1860 | 1942 | 2027 | 2109 | 2191 | 2276 | 2358 | 2444 | 2526 | 2608 | 2693 | 2775 |
| ELEV M | 541 | 567 | 592 | 618 | 643 | 668 | 694 | 719 | 745 | 770 | 795 | 821 | 846 |
| MGAL | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 | 4312.4 |

Figure 31

PROFILE OF LINE L650S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967
G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1712 | 1794 | 1879 | 1961 | 2043 | 2129 | 2211 | 2296 | 2378 | 2460 | 2545 | 2627 | 2713 |
| ELEV M | 522 | 547 | 573 | 598 | 623 | 649 | 674 | 700 | 725 | 750 | 776 | 801 | 827 |
| MGAL | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 | 4312.4 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1712 | 1794 | 1879 | 1961 | 2043 | 2129 | 2211 | 2296 | 2378 | 2460 | 2545 | 2627 | 2713 |
| ELEV M | 522 | 547 | 573 | 598 | 623 | 649 | 674 | 700 | 725 | 750 | 776 | 801 | 827 |
| MGAL | 4306.4 | 4306.9 | 4307.4 | 4307.9 | 4308.4 | 4308.9 | 4309.4 | 4309.9 | 4310.4 | 4310.9 | 4311.4 | 4311.9 | 4312.4 |

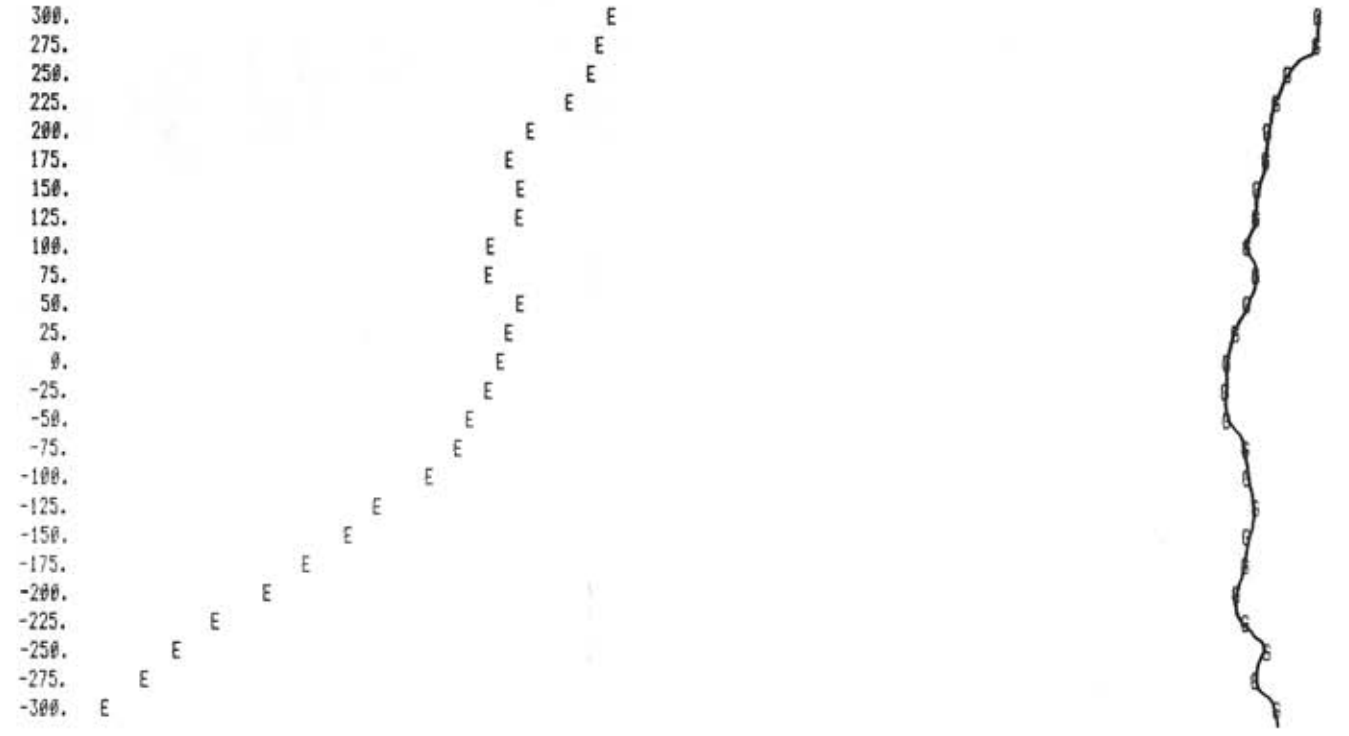
Figure 32

PROFILE OF LINE L700S

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967

G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1712 | 1797 | 1879 | 1961 | 2047 | 2129 | 2214 | 2296 | 2378 | 2463 | 2545 | 2631 | 2713 |
| ELEV M | 522 | 548 | 573 | 598 | 624 | 649 | 675 | 700 | 725 | 751 | 776 | 802 | 827 |
| MGAL | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 | 4312.5 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1712 | 1797 | 1879 | 1961 | 2047 | 2129 | 2214 | 2296 | 2378 | 2463 | 2545 | 2631 | 2713 |
| ELEV M | 522 | 548 | 573 | 598 | 624 | 649 | 675 | 700 | 725 | 751 | 776 | 802 | 827 |
| MGAL | 4306.5 | 4307.0 | 4307.5 | 4308.0 | 4308.5 | 4309.0 | 4309.5 | 4310.0 | 4310.5 | 4311.0 | 4311.5 | 4312.0 | 4312.5 |

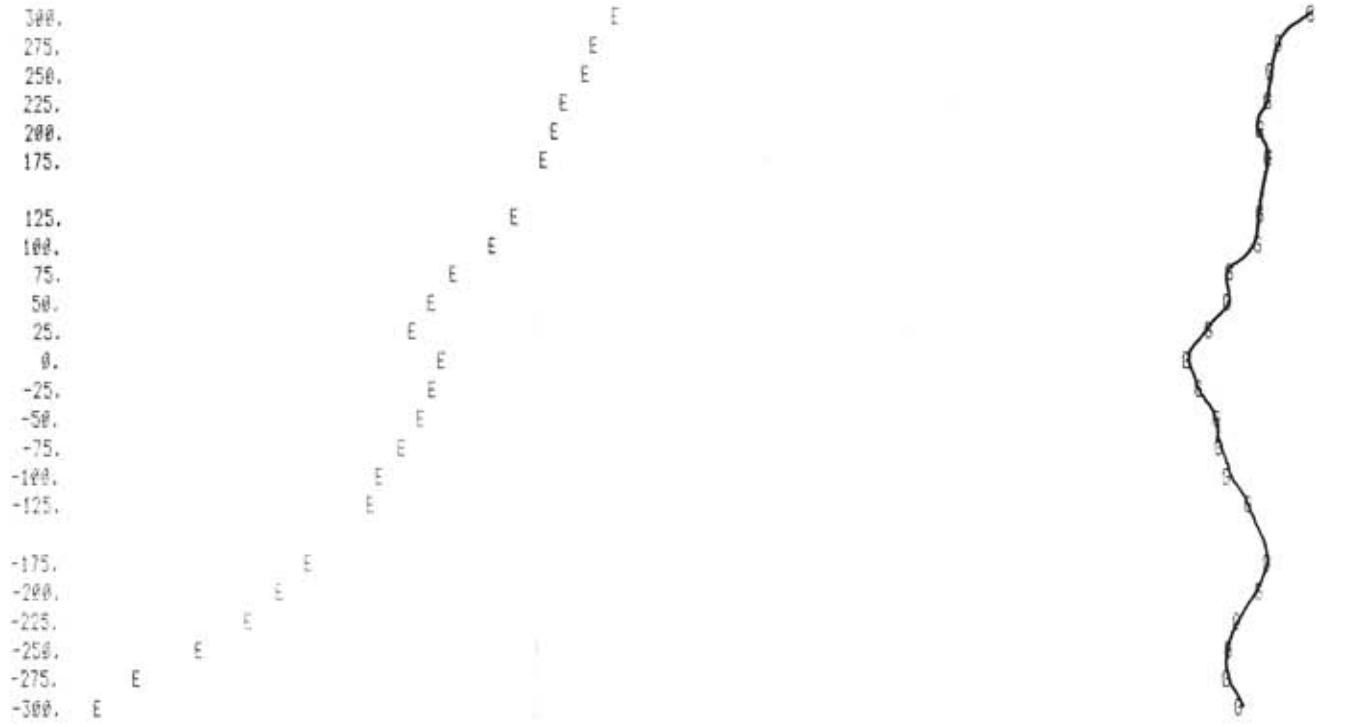
Figure 33

PROFILE OF LINE 800 S

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1706 | 1788 | 1870 | 1955 | 2037 | 2122 | 2204 | 2286 | 2372 | 2454 | 2539 | 2621 | 2703 |
| ELEV M | 520 | 545 | 570 | 596 | 621 | 647 | 672 | 697 | 723 | 748 | 774 | 799 | 824 |
| MGAL | 4306.7 | 4307.2 | 4307.7 | 4308.2 | 4308.7 | 4309.2 | 4309.7 | 4310.2 | 4310.7 | 4311.2 | 4311.7 | 4312.2 | 4312.7 |





| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1706 | 1788 | 1870 | 1955 | 2037 | 2122 | 2204 | 2286 | 2372 | 2454 | 2539 | 2621 | 2703 |
| ELEV M | 520 | 545 | 570 | 596 | 621 | 647 | 672 | 697 | 723 | 748 | 774 | 799 | 824 |
| MGAL | 4306.7 | 4307.2 | 4307.7 | 4308.2 | 4308.7 | 4309.2 | 4309.7 | 4310.2 | 4310.7 | 4311.2 | 4311.7 | 4312.2 | 4312.7 |

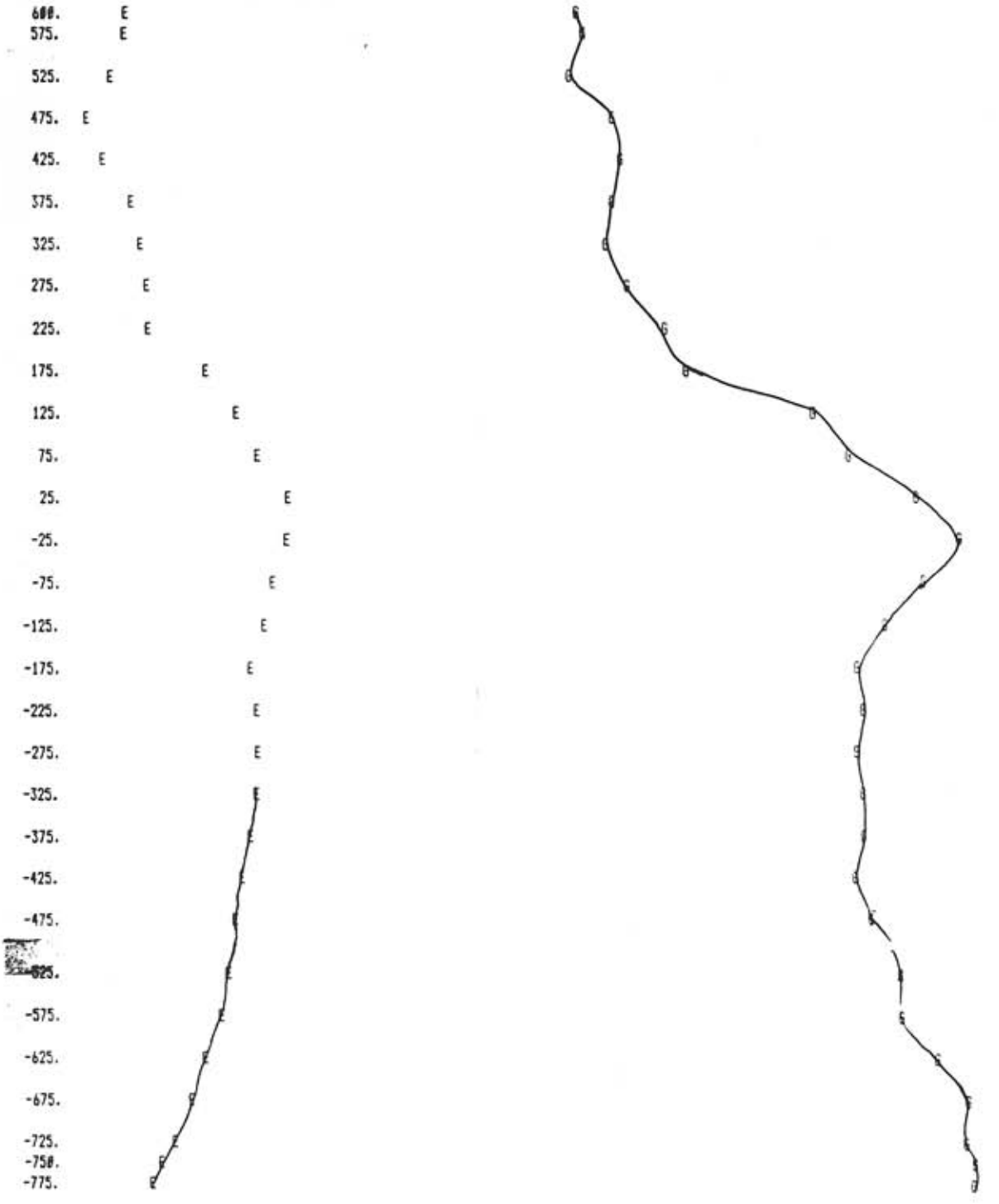

Figure 34

PROFILE OF LINE BASELINE

DENSITY= 2.67
G=GRAVITY READING

BOUGUER CORRECTION PER METER .1967
E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 1929 | 2014 | 2096 | 2181 | 2263 | 2345 | 2431 | 2513 | 2598 | 2680 | 2762 | 2847 | 2929 |
| ELEV M | 588 | 614 | 639 | 665 | 690 | 715 | 741 | 766 | 792 | 817 | 842 | 868 | 893 |
| MGAL | 4306.1 | 4306.6 | 4307.1 | 4307.6 | 4308.1 | 4308.6 | 4309.1 | 4309.6 | 4310.1 | 4310.6 | 4311.1 | 4311.6 | 4312.1 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |



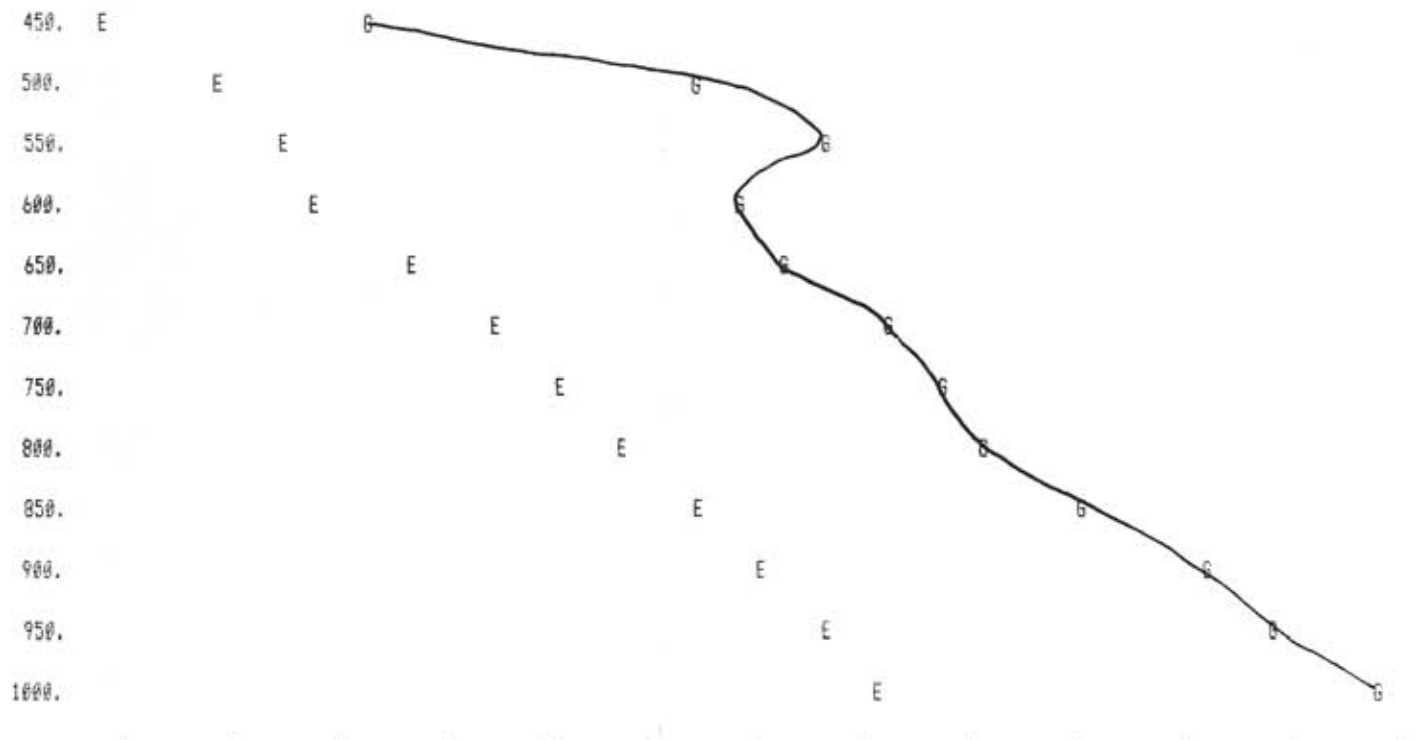

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 1929 | 2014 | 2096 | 2181 | 2263 | 2345 | 2431 | 2513 | 2598 | 2680 | 2762 | 2847 | 2929 |
| ELEV M | 588 | 614 | 639 | 665 | 690 | 715 | 741 | 766 | 792 | 817 | 842 | 868 | 893 |
| MGAL | 4306.1 | 4306.6 | 4307.1 | 4307.6 | 4308.1 | 4308.6 | 4309.1 | 4309.6 | 4310.1 | 4310.6 | 4311.1 | 4311.6 | 4312.1 |

Figure 35

PROFILE OF LINE POWERLINE

DENSITY= 2.67 BOUGUER CORRECTION PER METER .1967
G=GRAVITY READING E=ELEVATION READING

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| ELEV FT | 2224 | 2306 | 2391 | 2473 | 2559 | 2641 | 2723 | 2808 | 2890 | 2975 | 3057 | 3139 | 3225 |
| ELEV M | 678 | 703 | 729 | 754 | 780 | 805 | 830 | 856 | 881 | 907 | 932 | 957 | 983 |
| MGAL | 4309.6 | 4310.1 | 4310.6 | 4311.1 | 4311.6 | 4312.1 | 4312.6 | 4313.1 | 4313.6 | 4314.1 | 4314.6 | 4315.1 | 4315.6 |
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |




| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| ELEV FT | 2224 | 2306 | 2391 | 2473 | 2559 | 2641 | 2723 | 2808 | 2890 | 2975 | 3057 | 3139 | 3225 |
| ELEV M | 678 | 703 | 729 | 754 | 780 | 805 | 830 | 856 | 881 | 907 | 932 | 957 | 983 |
| MGAL | 4309.6 | 4310.1 | 4310.6 | 4311.1 | 4311.6 | 4312.1 | 4312.6 | 4313.1 | 4313.6 | 4314.1 | 4314.6 | 4315.1 | 4315.6 |

Figure 36

# APPENDIX VI: Gravity Modeling

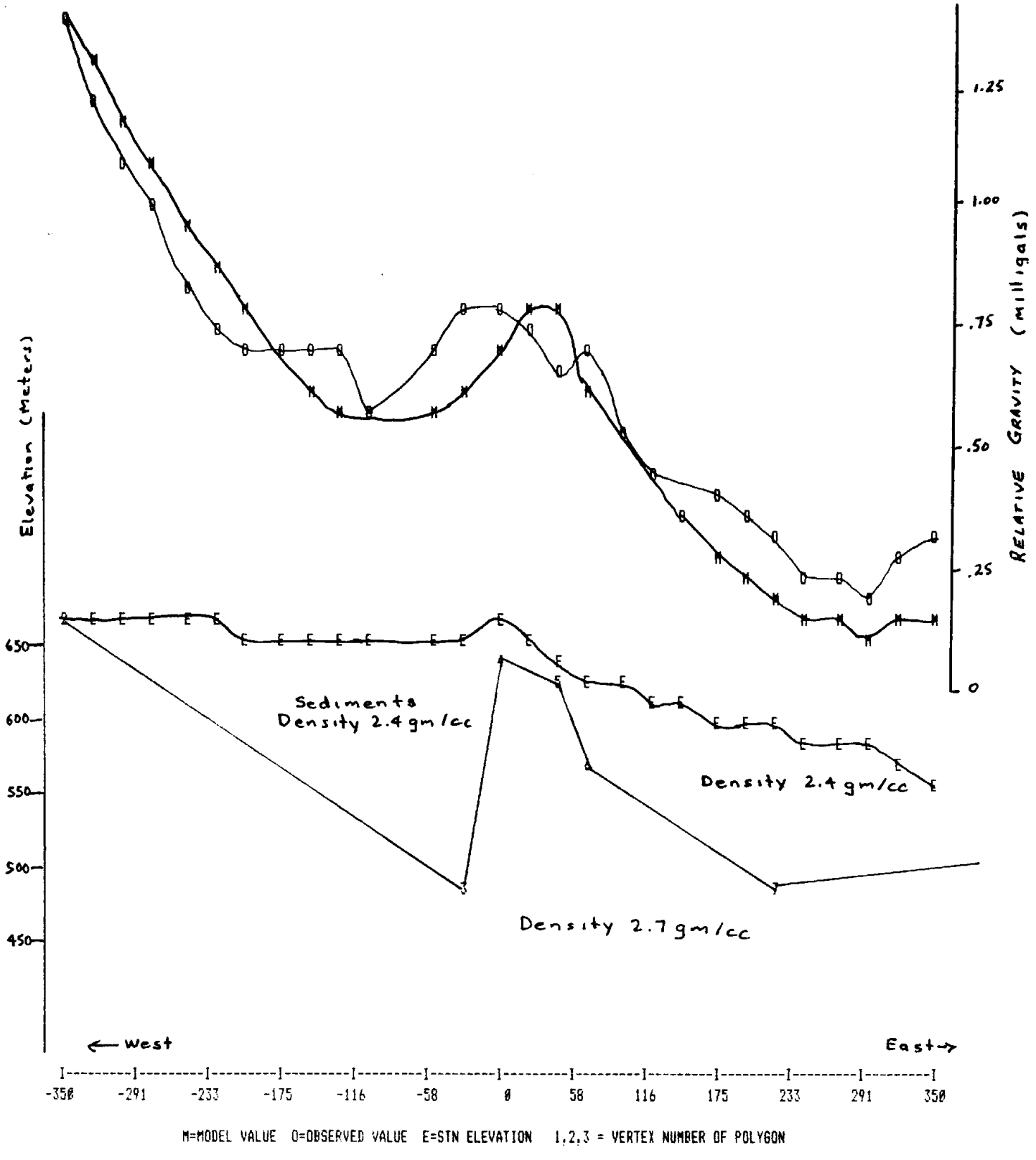



Figure 37 - LINE ON

LINE ØØN WITH MODEL FOR 25ØS MOVED TO WEST

FILE NAME FØØN  MODEL NAME MODØØN

FOR POLYGON 1  DENSITY CONTRAST = .3ØØØ

| VERTEX | X-COORD | Z-COORD |
|---|---|---|
| 1 | -1ØØØ.ØØ | 87Ø.ØØ |
| 2 | -35Ø.ØØ | 66Ø.ØØ |
| 3 | -25.ØØ | 45Ø.ØØ |
| 4 | Ø.ØØ | 64Ø.ØØ |
| 5 | 5Ø.ØØ | 62Ø.ØØ |
| 6 | 75.ØØ | 55Ø.ØØ |
| 7 | 225.ØØ | 45Ø.ØØ |
| 8 | 5ØØ.ØØ | 5ØØ.ØØ |
| 9 | 1ØØØ.ØØ | 65Ø.ØØ |
| 1Ø | 1ØØØ.ØØ | Ø.ØØ |
| 11 | -1ØØØ.ØØ | Ø.ØØ |

| STATION | ELEV | OBS.GRAVITY | MODEL GRAVITY | DIFFERENCE |
|---|---|---|---|---|
| -35Ø. | 674.1Ø | 1.21ØØ | 1.21ØØ | Ø.ØØØØ |
| -325. | 67Ø.81 | 1.ØØØØ | 1.1ØØ8 | -.1ØØ8 |
| -3ØØ. | 668.73 | .87Ø1 | .9775 | -.1Ø74 |
| -275. | 664.94 | .78Ø3 | .8691 | -.ØØ88 |
| -25Ø. | 663.16 | .64Ø1 | .7626 | -.1225 |
| -225. | 66Ø.Ø7 | .52ØØ | .6692 | -.1492 |
| -2ØØ. | 656.59 | .49Ø2 | .5729 | -.ØØ27 |
| -175. | 653.8Ø | .48ØØ | .492Ø | -.Ø12Ø |
| -15Ø. | 65Ø.92 | .49Ø2 | .4256 | .Ø646 |
| -125. | 648.33 | .48ØØ | .3763 | .1Ø37 |
| -1ØØ. | 649.Ø5 | .37Ø1 | .3512 | .Ø189 |
| -5Ø. | 653.88 | .48ØØ | .3717 | .1ØØ2 |
| -25. | 655.79 | .59Ø3 | .4228 | .1675 |
| Ø. | 66Ø.5Ø | .6ØØ1 | .477Ø | .1231 |
| 25. | 646.31 | .52ØØ | .5885 | -.Ø685 |
| 5Ø. | 633.Ø1 | .44Ø4 | .5628 | -.1224 |
| 75. | 622.Ø2 | .5ØØØ | .4265 | .Ø735 |
| 1ØØ. | 612.12 | .32Ø3 | .3119 | .ØØ85 |
| 125. | 6Ø4.32 | .25ØØ | .2237 | .Ø263 |
| 15Ø. | 595.43 | .17Ø4 | .15Ø3 | .Ø2Ø1 |
| 175. | 589.53 | .18Ø2 | .Ø822 | .Ø98Ø |
| 2ØØ. | 585.13 | .15Ø4 | .Ø227 | .1277 |
| 225. | 578.53 | .1ØØ1 | -.Ø234 | .1235 |
| 25Ø. | 571.Ø4 | .Ø1Ø3 | -.Ø56Ø | .Ø662 |
| 275. | 568.14 | .Ø3Ø3 | -.Ø784 | .1Ø86 |
| 3ØØ. | 562.14 | Ø.ØØØØ | -.Ø857 | .Ø857 |
| 325. | 553.15 | .Ø7Ø3 | -.Ø773 | .1476 |
| 35Ø. | 541.25 | .1ØØ1 | -.Ø533 | .1534 |

THE SUM OF THE SQUARE OF THE DIFFERENCES= .28Ø3

Figure 37a

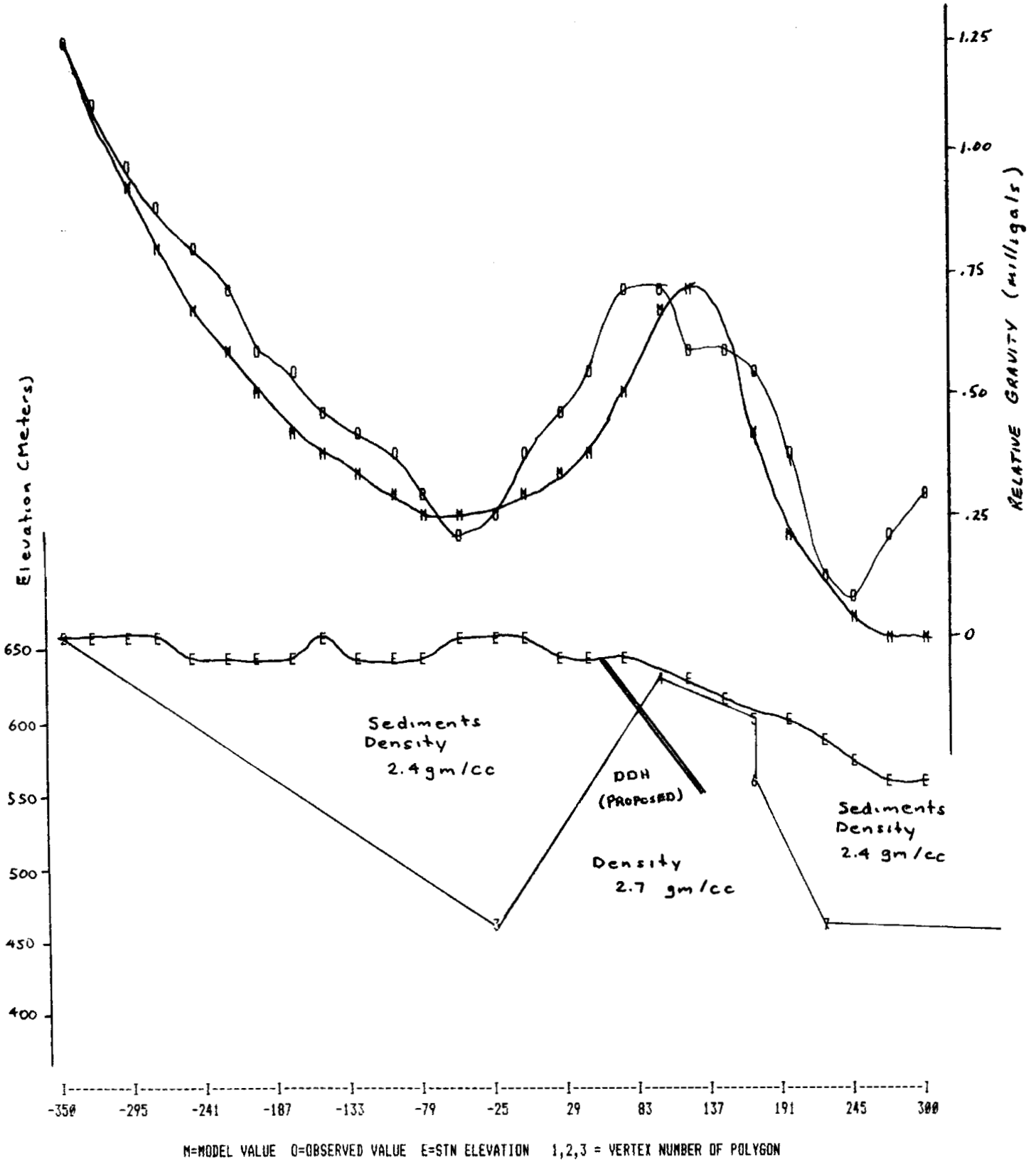



Figure 38 - LINE 250S

LINE 250S MODEL 3

FILE NAME F250S MODEL NAME MOD2503

FOR POLYGON 1 DENSITY CONTRAST = .3000

| VERTEX | X-COORD | Z-COORD |
|---|---|---|
| 1 | -1000.00 | 870.00 |
| 2 | -350.00 | 660.00 |
| 3 | -25.00 | 450.00 |
| 4 | 100.00 | 620.00 |
| 5 | 175.00 | 596.00 |
| 6 | 170.00 | 550.00 |
| 7 | 225.00 | 450.00 |
| 8 | 500.00 | 500.00 |
| 9 | 1000.00 | 650.00 |
| 10 | 1000.00 | 0.00 |
| 11 | -1000.00 | 0.00 |

| STATION | ELEV | OBS.GRAVITY | MODEL GRAVITY | DIFFERENCE |
|---|---|---|---|---|
| -350. | 662.10 | 1.2300 | 1.2300 | 0.0000 |
| -325. | 657.39 | 1.0503 | 1.0562 | -.0059 |
| -300. | 653.99 | .9502 | .8966 | .0536 |
| -275. | 650.18 | .8301 | .7569 | .0732 |
| -250. | 647.17 | .7500 | .6352 | .1148 |
| -225. | 644.97 | .6499 | .5288 | .1211 |
| -200. | 644.96 | .5303 | .4391 | .0912 |
| -175. | 645.55 | .4702 | .3615 | .1087 |
| -150. | 647.64 | .4102 | .2979 | .1123 |
| -125. | 646.94 | .3501 | .2414 | .1087 |
| -100. | 647.13 | .3003 | .2000 | .1003 |
| -75. | 646.72 | .2002 | .1724 | .0278 |
| -50. | 647.82 | .1299 | .1622 | -.0323 |
| -25. | 647.51 | .1499 | .1674 | -.0175 |
| 0. | 647.60 | .3003 | .1903 | .1099 |
| 25. | 644.13 | .3901 | .2342 | .1559 |
| 50. | 639.56 | .5000 | .3052 | .1948 |
| 75. | 633.09 | .6699 | .4163 | .2536 |
| 100. | 624.92 | .6602 | .6011 | .0591 |
| 125. | 617.55 | .5400 | .6390 | -.0990 |
| 150. | 609.88 | .5400 | .5363 | .0038 |
| 175. | 599.90 | .4902 | .3604 | .1299 |
| 200. | 590.03 | .2900 | .1335 | .1566 |
| 225. | 576.76 | .0303 | .0105 | .0198 |
| 250. | 564.39 | 0.0000 | -.0690 | .0690 |
| 275. | 552.02 | .1001 | -.1148 | .2149 |
| 300. | 544.65 | .2100 | -.1345 | .3445 |

THE SUM OF THE SQUARE OF THE DIFFERENCES= .4562

Figure 38a

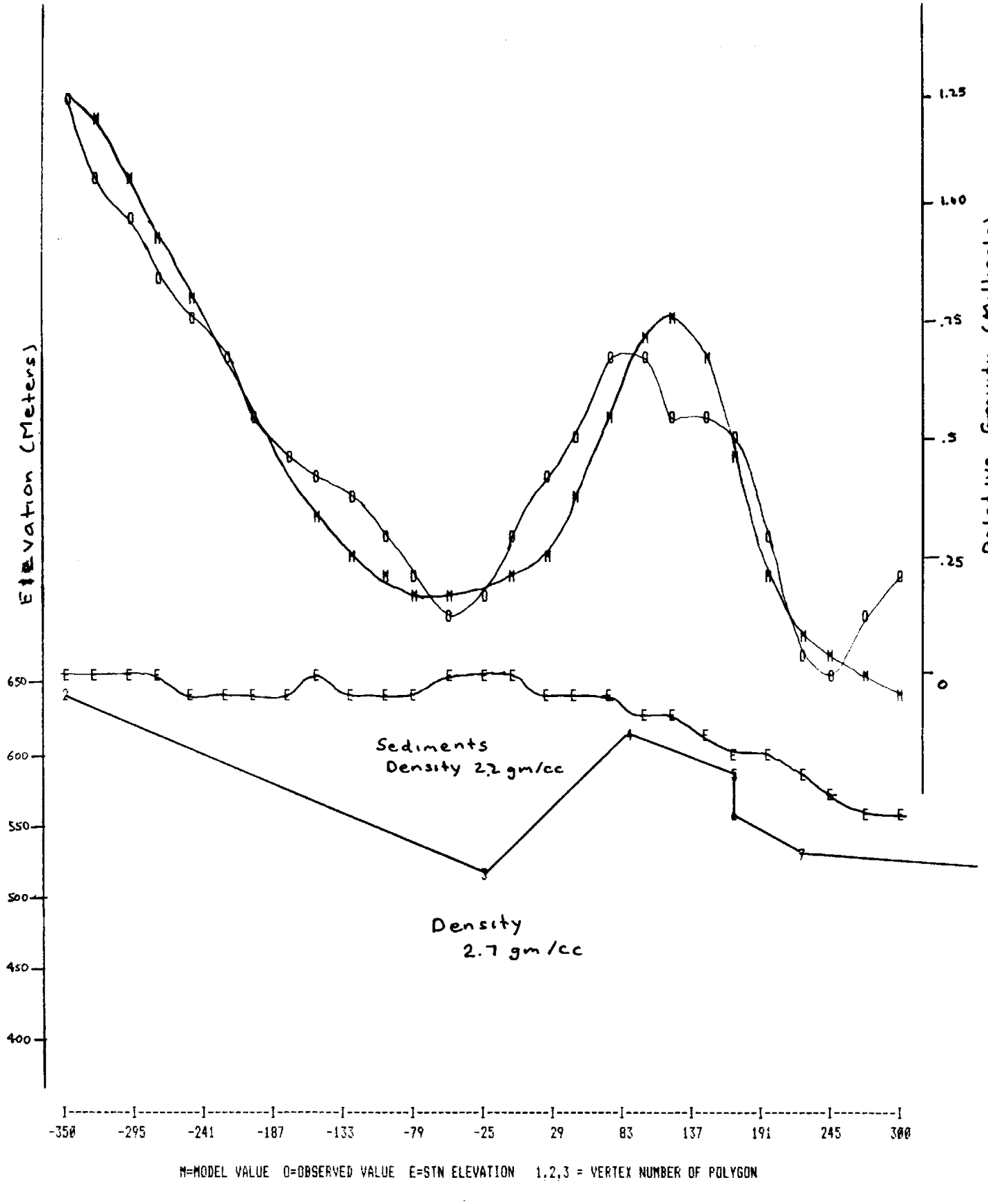



Figure 39 - LINE 250S

LINE 250S WITH DENSITY VARIATIONS

FILE NAME F250S  MODEL NAME MOD250

FOR POLYGON 1  DENSITY CONTRAST = .5000

| VERTEX | X-COORD | Z-COORD |
|---|---|---|
| 1 | -1000.00 | 870.00 |
| 2 | -350.00 | 640.00 |
| 3 | -25.00 | 500.00 |
| 4 | 90.00 | 608.00 |
| 5 | 175.00 | 586.00 |
| 6 | 170.00 | 550.00 |
| 7 | 225.00 | 520.00 |
| 8 | 500.00 | 500.00 |
| 9 | 1000.00 | 650.00 |
| 10 | 1000.00 | 0.00 |
| 11 | -1000.00 | 0.00 |

| STATION | ELEV | OBS.GRAVITY | MODEL GRAVITY | DIFFERENCE |
|---|---|---|---|---|
| -350. | 662.10 | 1.2300 | 1.2300 | 0.0000 |
| -325. | 657.39 | 1.0503 | 1.1543 | -.1040 |
| -300. | 653.99 | .9502 | 1.0379 | -.0877 |
| -275. | 650.18 | .8301 | .9207 | -.0906 |
| -250. | 647.17 | .7500 | .7997 | -.0497 |
| -225. | 644.97 | .6499 | .6793 | -.0294 |
| -200. | 644.96 | .5303 | .5568 | -.0265 |
| -175. | 645.55 | .4702 | .4439 | .0263 |
| -150. | 647.64 | .4102 | .3405 | .0697 |
| -125. | 646.94 | .3501 | .2615 | .0886 |
| -100. | 647.13 | .3003 | .1980 | .1023 |
| -75. | 646.72 | .2002 | .1567 | .0435 |
| -50. | 647.82 | .1299 | .1365 | -.0067 |
| -25. | 647.51 | .1499 | .1456 | .0043 |
| 0. | 647.60 | .3003 | .1809 | .1193 |
| 25. | 644.13 | .3901 | .2566 | .1335 |
| 50. | 639.56 | .5000 | .3701 | .1299 |
| 75. | 633.09 | .6699 | .5258 | .1441 |
| 100. | 624.92 | .6602 | .7011 | -.0410 |
| 125. | 617.55 | .5400 | .7408 | -.2008 |
| 150. | 609.88 | .5400 | .6590 | -.1190 |
| 175. | 599.90 | .4902 | .4557 | .0345 |
| 200. | 590.03 | .2900 | .2119 | .0781 |
| 225. | 576.76 | .0303 | .0856 | -.0553 |
| 250. | 564.39 | 0.0000 | .0208 | -.0208 |
| 275. | 552.02 | .1001 | -.0038 | .1039 |
| 300. | 544.65 | .2100 | -.0318 | .2418 |

THE SUM OF THE SQUARE OF THE DIFFERENCES= .2625

Figure 39a

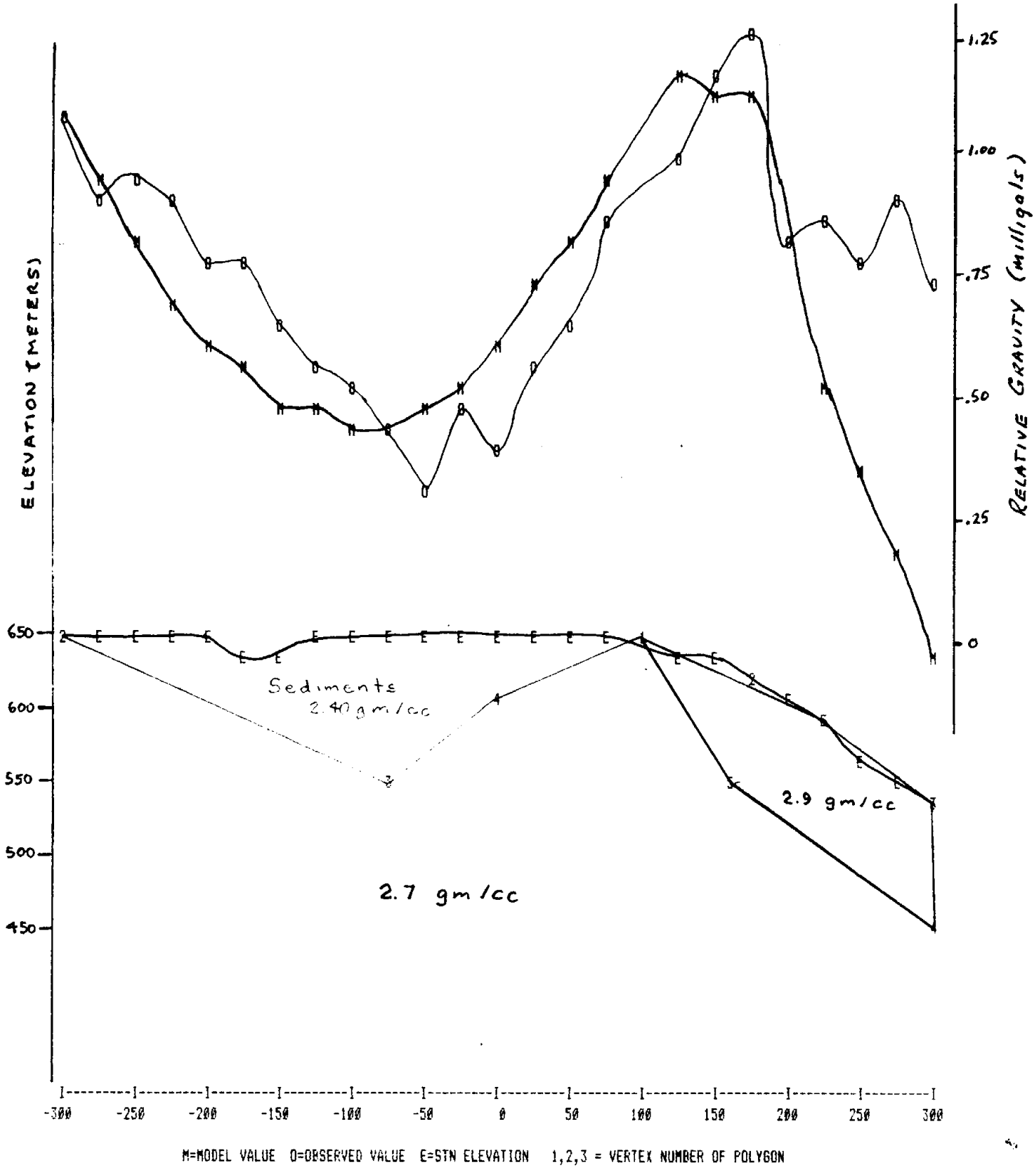



Figure 40- LINE 400S

LINE 400S WITH TWO DENSITY ZONES

FILE NAME F400S MODEL NAME \ _ MOD 400S

FOR POLYGON 1 DENSITY CONTRAST = .3000

| VERTEX | X-COORD | Z-COORD |
|---|---|---|
| 1 | -1000.00 | 870.00 |
| 2 | -300.00 | 650.00 |
| 3 | -75.00 | 550.00 |
| 4 | 0.00 | 600.00 |
| 5 | 100.00 | 640.00 |
| 6 | 160.00 | 550.00 |
| 7 | 300.00 | 450.00 |
| 8 | 500.00 | 500.00 |
| 9 | 1000.00 | 650.00 |
| 10 | 1000.00 | 0.00 |
| 11 | -1000.00 | 0.00 |

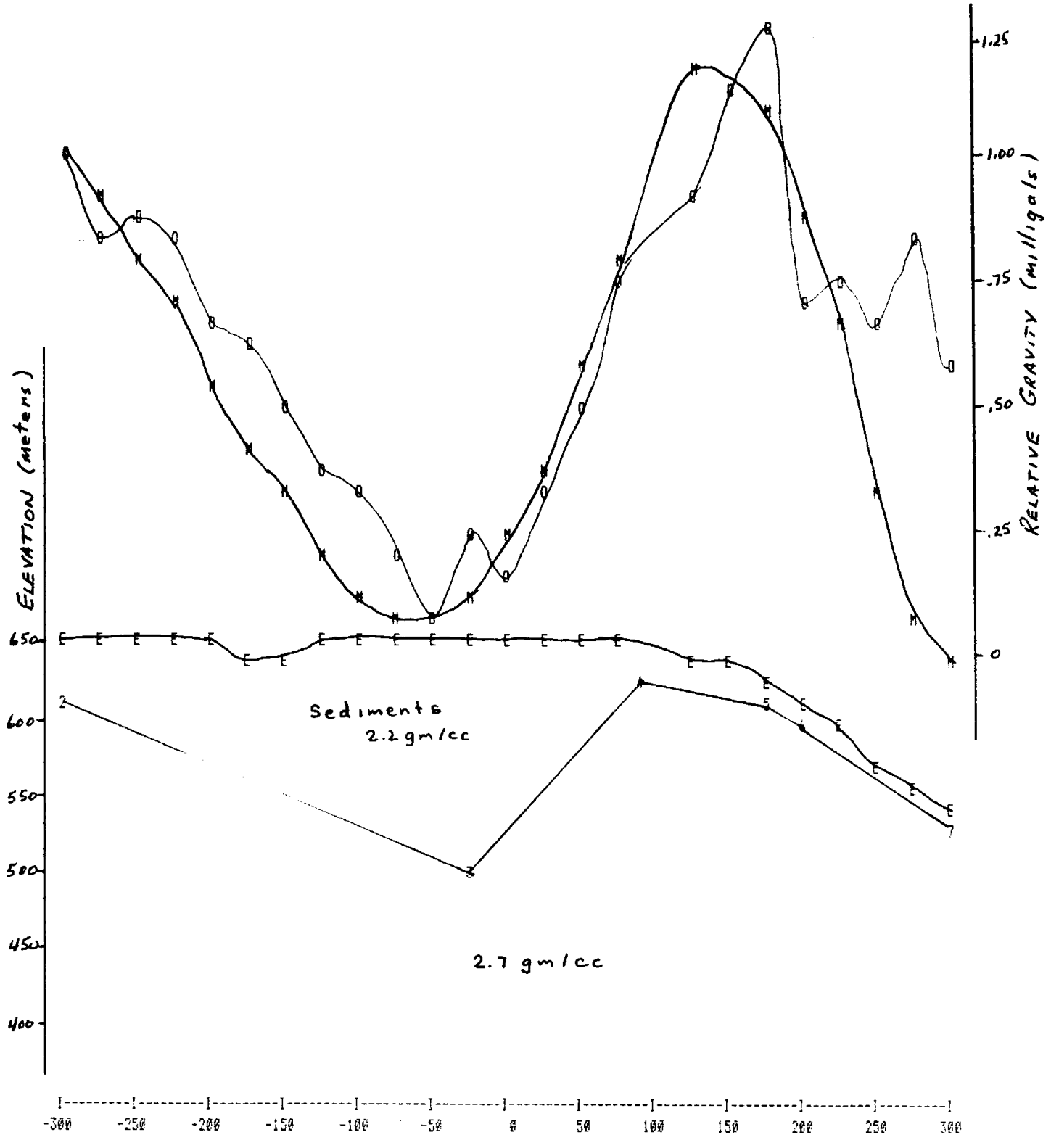
FOR POLYGON 2 DENSITY CONTRAST = .5000

| VERTEX | X-COORD | Z-COORD |
|---|---|---|
| 1 | 100.00 | 640.00 |
| 2 | 175.00 | 615.00 |
| 3 | 300.00 | 532.00 |
| 4 | 300.00 | 450.00 |
| 5 | 160.00 | 550.00 |

| STATION | ELEV | OBS.GRAVITY | MODEL GRAVITY | DIFFERENCE |
|---|---|---|---|---|
| -300. | 652.00 | .6797 | .6797 | 0.0000 |
| -275. | 648.00 | .5498 | .5651 | -.0152 |
| -250. | 644.80 | .5801 | .4521 | .1280 |
| -225. | 641.60 | .5400 | .3558 | .1843 |
| -200. | 639.20 | .4297 | .2749 | .1548 |
| -175. | 638.10 | .3999 | .2084 | .1915 |
| -150. | 637.90 | .2998 | .1556 | .1442 |
| -125. | 639.50 | .2197 | .1196 | .1001 |
| -100. | 640.40 | .1797 | .1018 | .0779 |
| -75. | 640.50 | .1001 | .1071 | -.0070 |
| -50. | 643.70 | 0.0000 | .1380 | -.1380 |
| -25. | 644.60 | .1201 | .1920 | -.0719 |
| 0. | 644.10 | .0601 | .2676 | -.2075 |
| 25. | 642.97 | .1997 | .3594 | -.1597 |
| 50. | 643.35 | .2998 | .4560 | -.1562 |
| 75. | 642.82 | .4800 | .5706 | -.0906 |
| 125. | 632.97 | .6201 | .7603 | -.1402 |
| 150. | 630.05 | .7598 | .7149 | .0449 |
| 175. | 617.22 | .8701 | .7430 | .1271 |
| 200. | 601.50 | .4600 | .4396 | .0204 |
| 225. | 586.77 | .5000 | .1944 | .3056 |
| 250. | 568.35 | .4199 | .0096 | .4103 |
| 275. | 551.92 | .5498 | -.1295 | .6793 |
| 300. | 534.60 | .3599 | -.3157 | .6756 |

THE SUM OF THE SQUARE OF THE DIFFERENCES= 1.4913

Figure 40a -




M=MODEL VALUE O=OBSERVED VALUE E=STN ELEVATION 1,2,3 = VERTEX NUMBER OF POLYGON
LINE 400S WITH DENSITY CONTRAST OF .5 MILLIGALS

Figure 41 - LINE 400S

LINE 400S WITH DENSITY CONTRAST OF .5 MILLIGALS

FILE NAME F400S MODEL NAME MOD 400.SV

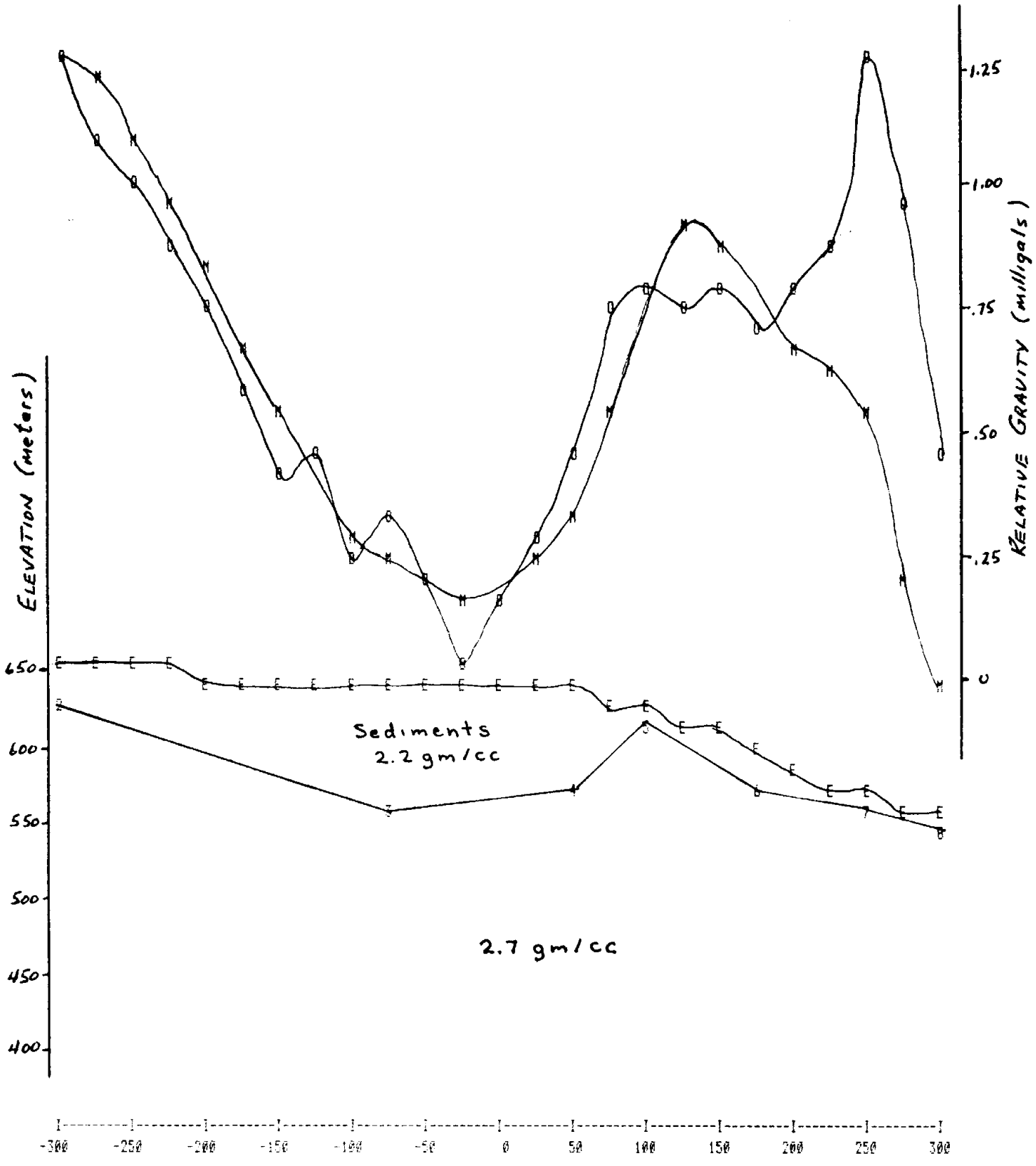
FOR POLYGON 1 DENSITY CONTRAST = .5000

| VERTEX | X-COORD | Z-COORD |
|---|---|---|
| 1 | -1000.00 | 870.00 |
| 2 | -300.00 | 610.00 |
| 3 | -25.00 | 500.00 |
| 4 | 90.00 | 620.00 |
| 5 | 175.00 | 605.00 |
| 6 | 200.00 | 585.00 |
| 7 | 300.00 | 520.00 |
| 8 | 500.00 | 500.00 |
| 9 | 1000.00 | 650.00 |
| 10 | 1000.00 | 0.00 |
| 11 | -1000.00 | 0.00 |

| STATION | ELEV | OBS.GRAVITY | MODEL GRAVITY | DIFFERENCE |
|---|---|---|---|---|
| -300. | 652.00 | .6797 | .6797 | 0.0000 |
| -275. | 648.00 | .5498 | .6222 | -.0723 |
| -250. | 644.80 | .5801 | .5390 | .0410 |
| -225. | 641.60 | .5400 | .4491 | .0910 |
| -200. | 639.20 | .4297 | .3557 | .0740 |
| -175. | 638.10 | .3999 | .2631 | .1368 |
| -150. | 637.90 | .2998 | .1784 | .1214 |
| -125. | 639.50 | .2197 | .1045 | .1152 |
| -100. | 640.40 | .1797 | .0525 | .1271 |
| -75. | 640.50 | .1001 | .0254 | .0747 |
| -50. | 643.70 | 0.0000 | .0213 | -.0213 |
| -25. | 644.60 | .1201 | .0516 | .0685 |
| 0. | 644.10 | .0601 | .1186 | -.0585 |
| 25. | 642.97 | .1997 | .2248 | -.0251 |
| 50. | 643.35 | .2998 | .3614 | -.0616 |
| 75. | 642.82 | .4800 | .5273 | -.0473 |
| 125. | 632.97 | .6201 | .8020 | -.1819 |
| 150. | 630.05 | .7598 | .7546 | .0052 |
| 175. | 617.22 | .8701 | .7447 | .1254 |
| 200. | 601.50 | .4600 | .5978 | -.1379 |
| 225. | 586.77 | .5000 | .4338 | .0662 |
| 250. | 563.35 | .4199 | .1832 | .2367 |
| 275. | 551.92 | .5498 | .0226 | .5272 |
| 300. | 534.60 | .3599 | -.0327 | .3926 |

THE SUM OF THE SQUARE OF THE DIFFERENCES= .6647

Figure 41a




M=MODEL VALUE O=OBSERVED VALUE E=STN ELEVATION 1,2,3 = VERTEX NUMBER OF POLYGON
LINE 550S WITH DENSITY CONTRAST OF .5 MILLIGALS

Figure 42- LINE 550S

LINE 550S WITH DENSITY CONTRAST OF .5 MILLIGALS

FILE NAME L550S  MODEL NAME MOD550S

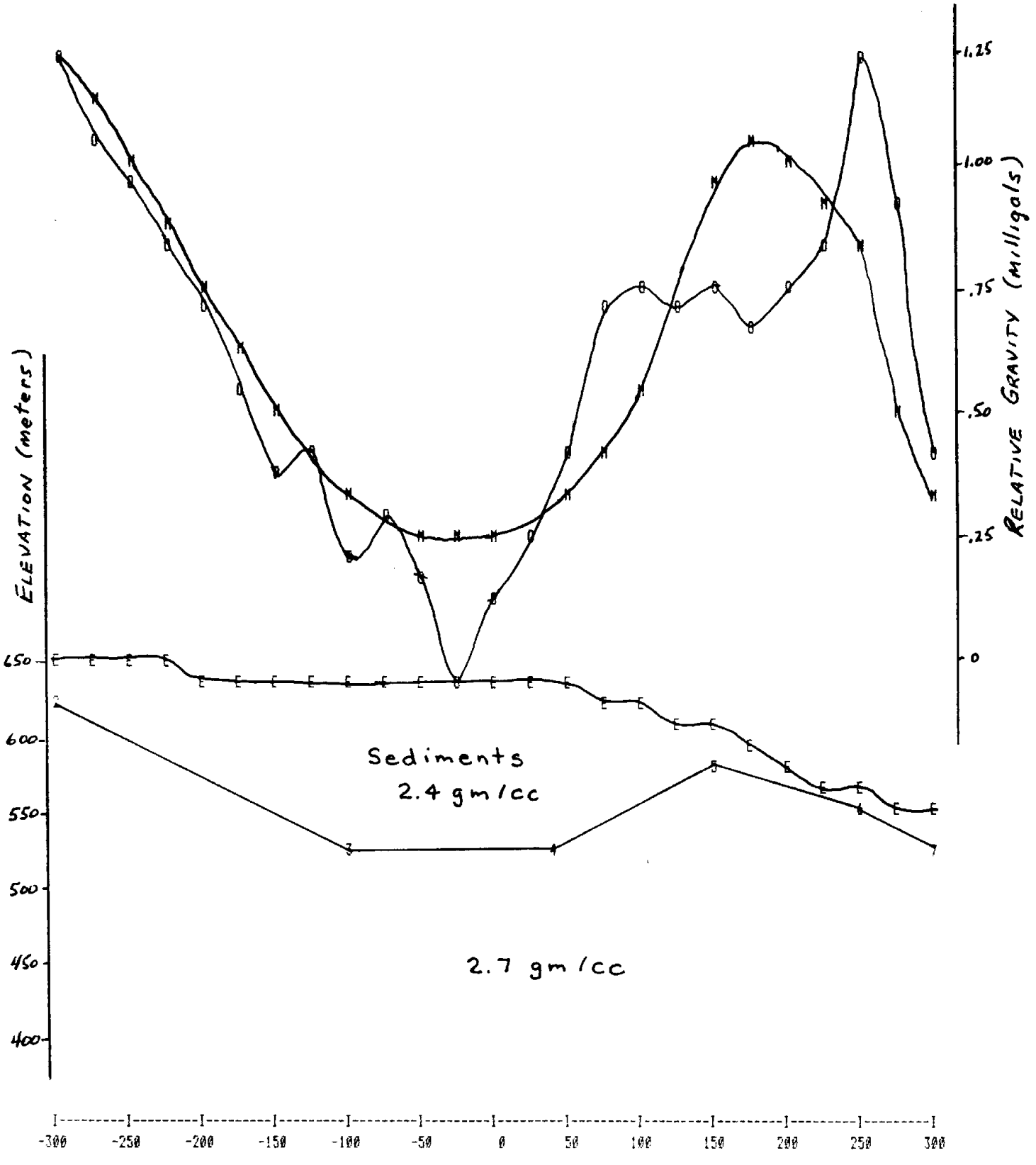
FOR POLYGON 1  DENSITY CONTRAST = .5000

| VERTEX | X-COORD | Z-COORD |
|---|---|---|
| 1 | -1000.00 | 870.00 |
| 2 | -300.00 | 620.00 |
| 3 | -75.00 | 550.00 |
| 4 | 50.00 | 560.00 |
| 5 | 100.00 | 600.00 |
| 6 | 175.00 | 570.00 |
| 7 | 250.00 | 558.00 |
| 8 | 300.00 | 540.00 |
| 9 | 500.00 | 500.00 |
| 10 | 1000.00 | 650.00 |
| 11 | 1000.00 | 0.00 |
| 12 | -1000.00 | 0.00 |

| STATION | ELEV | OBS.GRAVITY | MODEL GRAVITY | DIFFERENCE |
|---|---|---|---|---|
| -300. | 654.60 | .6699 | .6699 | 0.0000 |
| -275. | 651.18 | .5601 | .6273 | -.0673 |
| -250. | 648.57 | .5298 | .5594 | -.0296 |
| -225. | 642.85 | .4497 | .5052 | -.0555 |
| -200. | 640.43 | .3799 | .4266 | -.0467 |
| -175. | 637.22 | .2998 | .3549 | -.0551 |
| -150. | 633.70 | .2100 | .2892 | -.0792 |
| -125. | 631.09 | .2300 | .2272 | .0028 |
| -100. | 634.87 | .1201 | .1545 | -.0344 |
| -75. | 634.55 | .1597 | .1153 | .0443 |
| -50. | 635.44 | .0898 | .0899 | -.0000 |
| -25. | 636.92 | 0.0000 | .0786 | -.0786 |
| 0. | 637.40 | .0698 | .0856 | -.0158 |
| 25. | 634.65 | .1396 | .1227 | .0169 |
| 50. | 632.70 | .2397 | .1762 | .0635 |
| 75. | 626.35 | .3896 | .2830 | .1066 |
| 100. | 620.10 | .4097 | .4068 | .0029 |
| 125. | 610.15 | .3999 | .4867 | -.0868 |
| 150. | 600.40 | .4097 | .4516 | -.0419 |
| 175. | 591.55 | .3599 | .3659 | -.0060 |
| 200. | 580.50 | .4199 | .3404 | .0795 |
| 225. | 569.95 | .4600 | .3193 | .1407 |
| 250. | 559.80 | .6597 | .2815 | .3782 |
| 275. | 549.35 | .5098 | .0994 | .4104 |
| 300. | 545.70 | .2300 | -.0005 | .2305 |

THE SUM OF THE SQUARE OF THE DIFFERENCES= .4453

Figure 42a




M=MODEL VALUE O=OBSERVED VALUE E=STN ELEVATION 1,2,3 = VERTEX NUMBER OF POLYGON
LINE 550S WITH DENSITY CONTRAST OF .3 MILLIGALS

Figure 43- LINE 550S

LINE 550S WITH DENSITY CONTRAST OF .3 MILLIGALS

FILE NAME L550S  MODEL NAME 550SMOD3

FOR POLYGON 1  DENSITY CONTRAST = .3000

| VERTEX | X-COORD | Z-COORD |
|---|---|---|
| 1 | -1000.00 | 870.00 |
| 2 | -300.00 | 620.00 |
| 3 | -100.00 | 520.00 |
| 4 | 40.00 | 520.00 |
| 5 | 150.00 | 585.00 |
| 6 | 250.00 | 558.00 |
| 7 | 300.00 | 520.00 |
| 8 | 500.00 | 500.00 |
| 9 | 1000.00 | 650.00 |
| 10 | 1000.00 | 0.00 |
| 11 | -1000.00 | 0.00 |

| STATION | ELEV | OBS.GRAVITY | MODEL GRAVITY | DIFFERENCE |
|---|---|---|---|---|
| -300. | 654.60 | .6699 | .6699 | 0.0000 |
| -275. | 651.18 | .5601 | .6148 | -.0548 |
| -250. | 648.57 | .5298 | .5429 | -.0131 |
| -225. | 642.85 | .4497 | .4796 | -.0299 |
| -200. | 640.43 | .3799 | .4077 | -.0278 |
| -175. | 637.22 | .2998 | .3439 | -.0441 |
| -150. | 633.70 | .2100 | .2882 | -.0782 |
| -125. | 631.09 | .2300 | .2401 | -.0102 |
| -100. | 634.87 | .1201 | .1945 | -.0744 |
| -75. | 634.55 | .1597 | .1665 | -.0068 |
| -50. | 635.44 | .0898 | .1476 | -.0578 |
| -25. | 636.92 | 0.0000 | .1379 | -.1379 |
| 0. | 637.40 | .0698 | .1389 | -.0691 |
| 25. | 634.65 | .1396 | .1554 | -.0158 |
| 50. | 632.70 | .2397 | .1815 | .0583 |
| 75. | 626.35 | .3896 | .2308 | .1588 |
| 100. | 620.10 | .4097 | .2961 | .1136 |
| 125. | 610.15 | .3999 | .3953 | .0046 |
| 150. | 600.40 | .4097 | .5137 | -.1040 |
| 175. | 591.55 | .3599 | .5690 | -.2091 |
| 200. | 580.50 | .4199 | .5463 | -.1263 |
| 225. | 569.95 | .4600 | .4974 | -.0375 |
| 250. | 559.80 | .6597 | .4666 | .1931 |
| 275. | 549.35 | .5098 | .2879 | .2219 |
| 300. | 545.70 | .2300 | .1849 | .0451 |

THE SUM OF THE SQUARE OF THE DIFFERENCES= .2480

Figure 43a

# APPENDIX VII: Density Analysis

# PLOT OF GRAVITY VERSUS ELEVATION

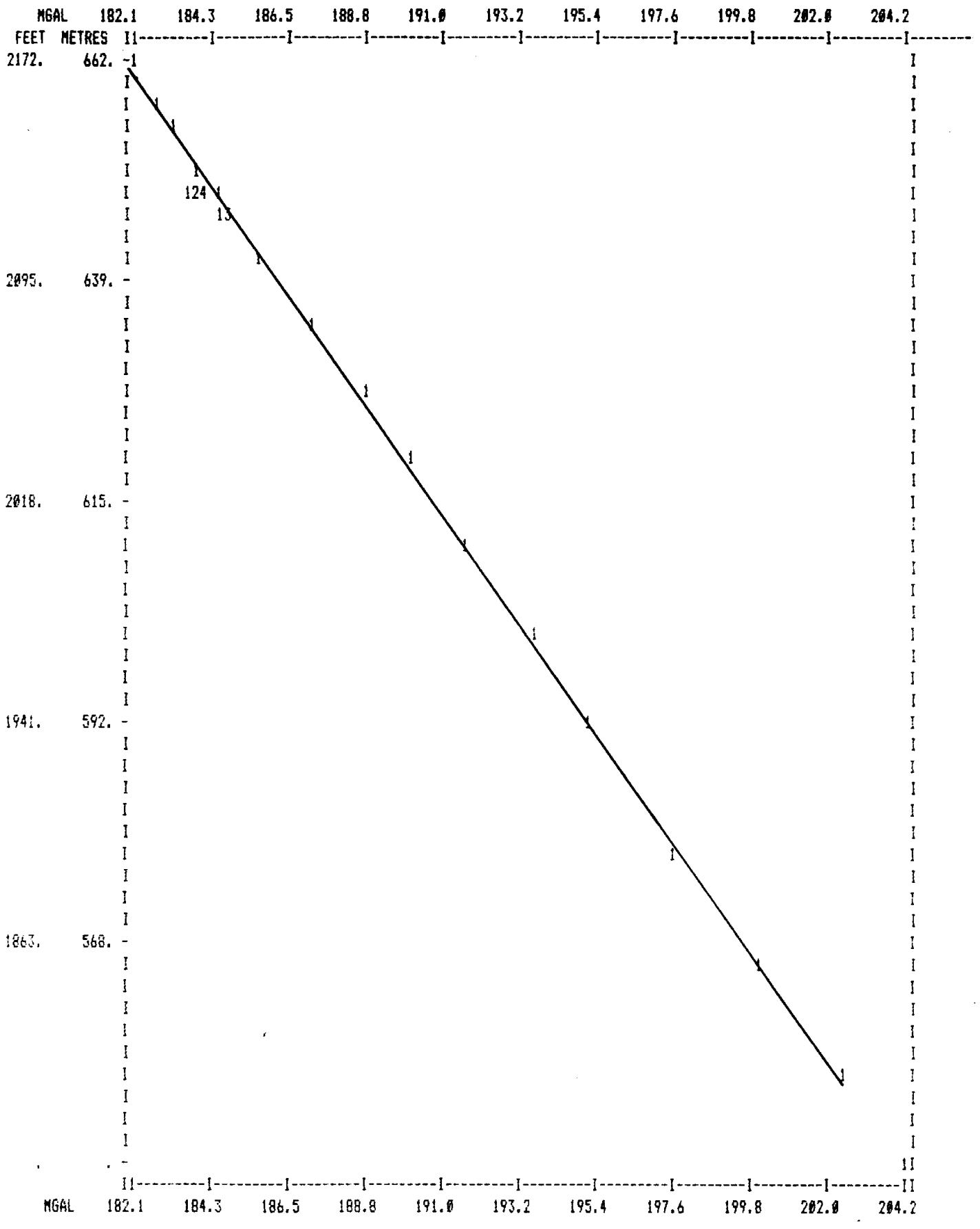



Figure 44- LINE 250S

# LINE 250S

NUMBER OF OBSERVATIONS= 27

THE PARAMETERS OF THE REGRESSION EQUATION GRAV=A + B*ELEV ARE
A= 308.3814 B= -.1916 FOR ELEVATION IN METRES
A= 1011.4989 B= -.6283 FOR ELEVATION IN FEET
THE TOTAL SUM OF SQUARES= 1085.9375
SUMS OF SQUARES DUE TO REGRESSION= 1083.6250
THE SUM OF SQUARES DUE TO DEVIATION= 2.3125
THE CORRELATION COEFFICIENT = .9989

DENSITY= 2.7925

THE POINTS OUTSIDE OF 1.6157 UNITS FROM THE LINE Y= 308.3814 + -.1916 * X ARE IGNORED

NUMBER OF OBSERVATIONS= 27

THE PARAMETERS OF THE REGRESSION EQUATION GRAV=A + B*ELEV ARE
A= 308.3814 B= -.1916 FOR ELEVATION IN METRES
A= 1011.4989 B= -.6283 FOR ELEVATION IN FEET
THE TOTAL SUM OF SQUARES= 1085.9375
SUMS OF SQUARES DUE TO REGRESSION= 1083.6250
THE SUM OF SQUARES DUE TO DEVIATION= 2.3125
THE CORRELATION COEFFICIENT = .9989

Figure 44a

# GRAVITY/ELEVATION

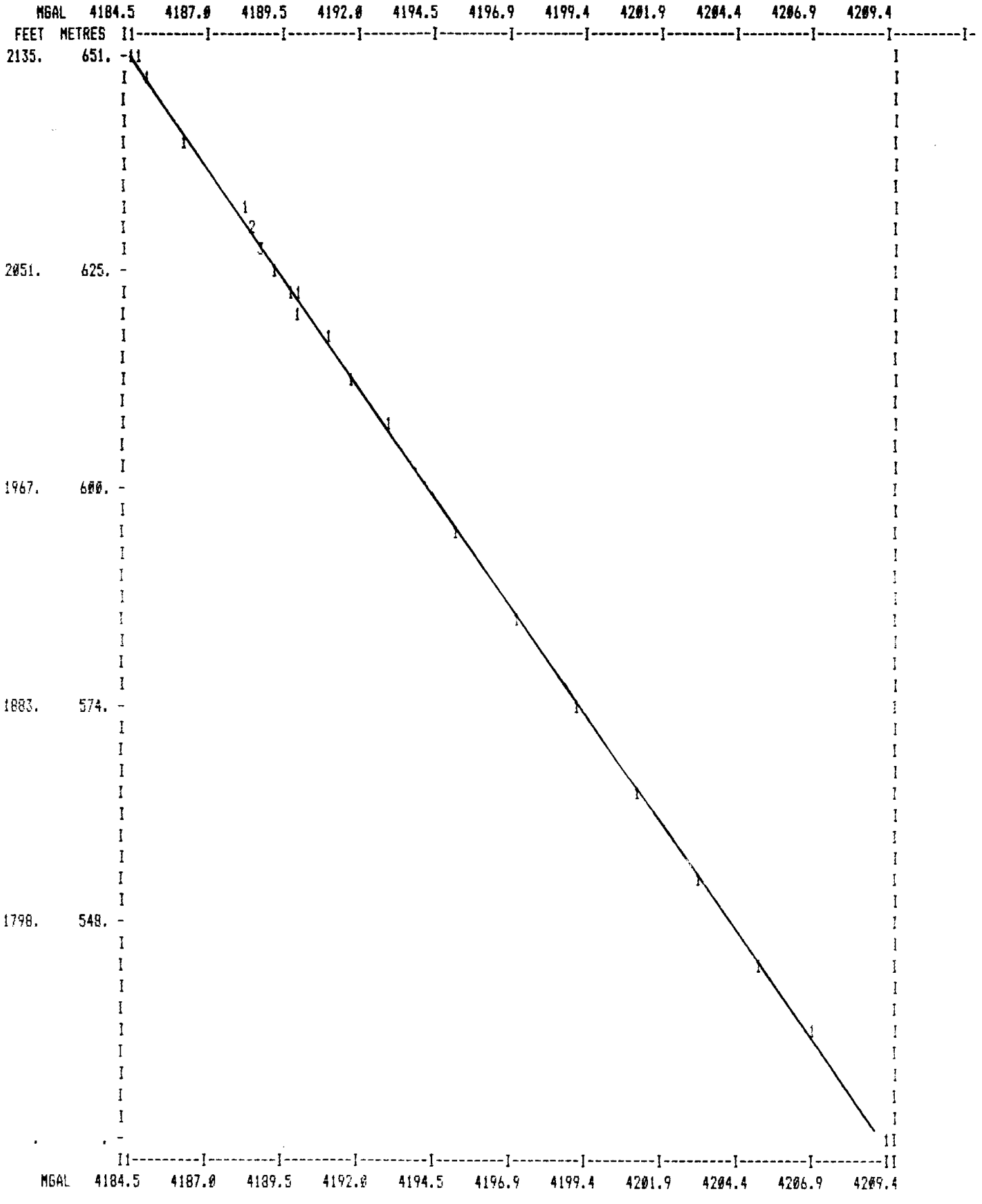



Figure 45 - LINE 700S

```
 NUMBER OF OBSERVATIONS=   25

THE PARAMETERS OF THE REGRESSION EQUATION GRAV=A + B*ELEV ARE
                  A=  4311.8984 B=     -.1963 FOR ELEVATION IN METRES
                 A= 14143.0264 B=     -.6438 FOR ELEVATION IN FEET
THE TOTAL SUM OF SQUARES=  1152.0000
SUMS OF SQUARES DUE TO REGRESSION=  1280.0000
THE SUM OF SQUARES DUE TO DEVIATION=  -128.0000
THE CORRELATION COEFFICIENT  =    1.0541

DENSITY=     2.6803

THE POINTS OUTSIDE OF     1.7321 UNITS FROM THE LINE Y= 4311.8984 +    -.1963 * X ARE IGNORED


 NUMBER OF OBSERVATIONS=   25

THE PARAMETERS OF THE REGRESSION EQUATION GRAV=A + B*ELEV ARE
                  A=  4311.8984 B=     -.1963 FOR ELEVATION IN METRES
                 A= 14143.0264 B=     -.6438 FOR ELEVATION IN FEET
THE TOTAL SUM OF SQUARES=  1152.0000
SUMS OF SQUARES DUE TO REGRESSION=  1280.0000
THE SUM OF SQUARES DUE TO DEVIATION=  -128.0000
THE CORRELATION COEFFICIENT  =    1.0541
```

Figure 45a

# APPENDIX VIII: Magnetic Cross sections

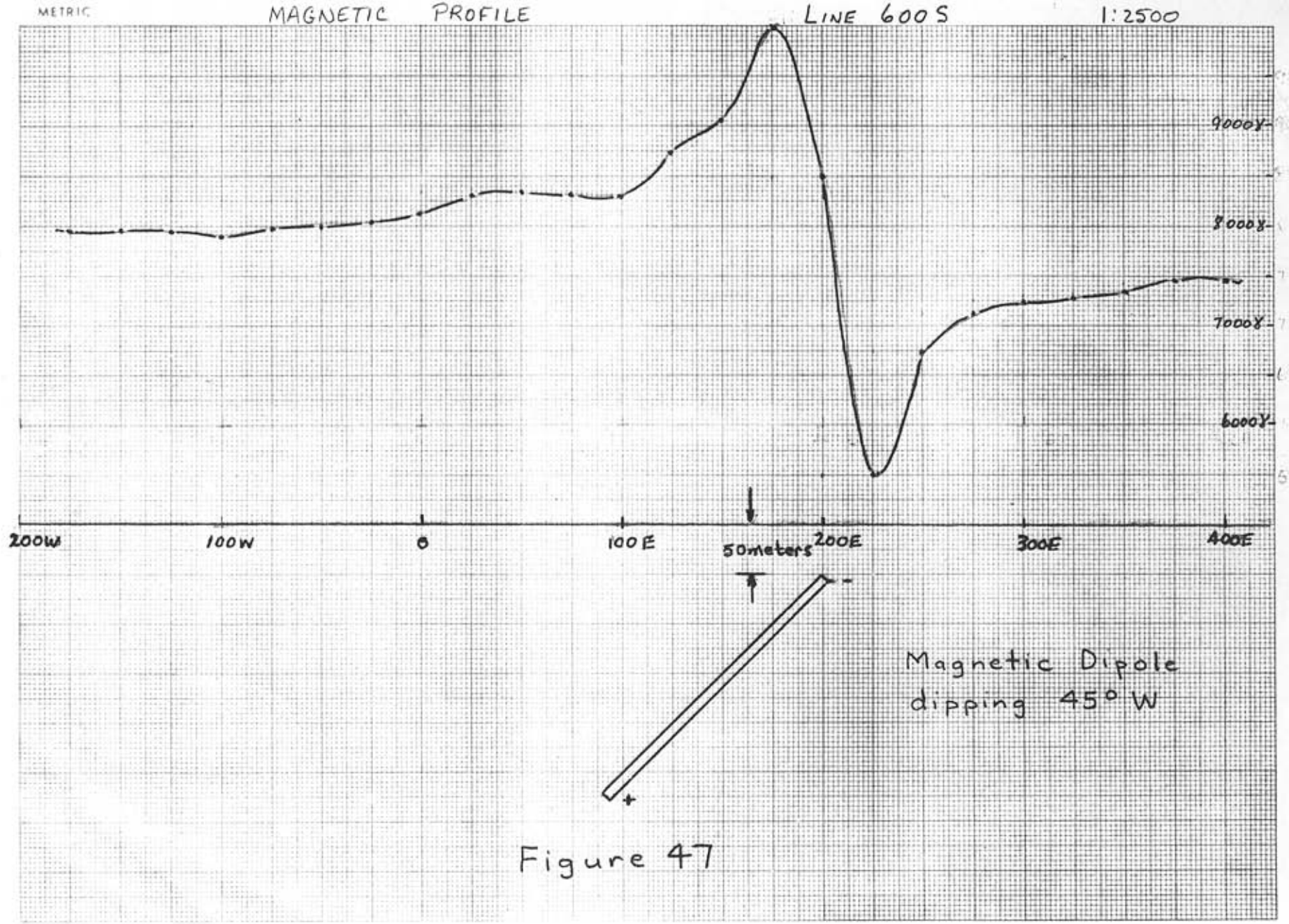

METRIC
MAGNETIC PROFILE
LINE 600S
1:2500
9000γ
8000γ
7000γ
6000γ
200W
100W
0
100E
50meters
200E
300E
400E
Magnetic Dipole
dipping 45° W
+

Figure 47

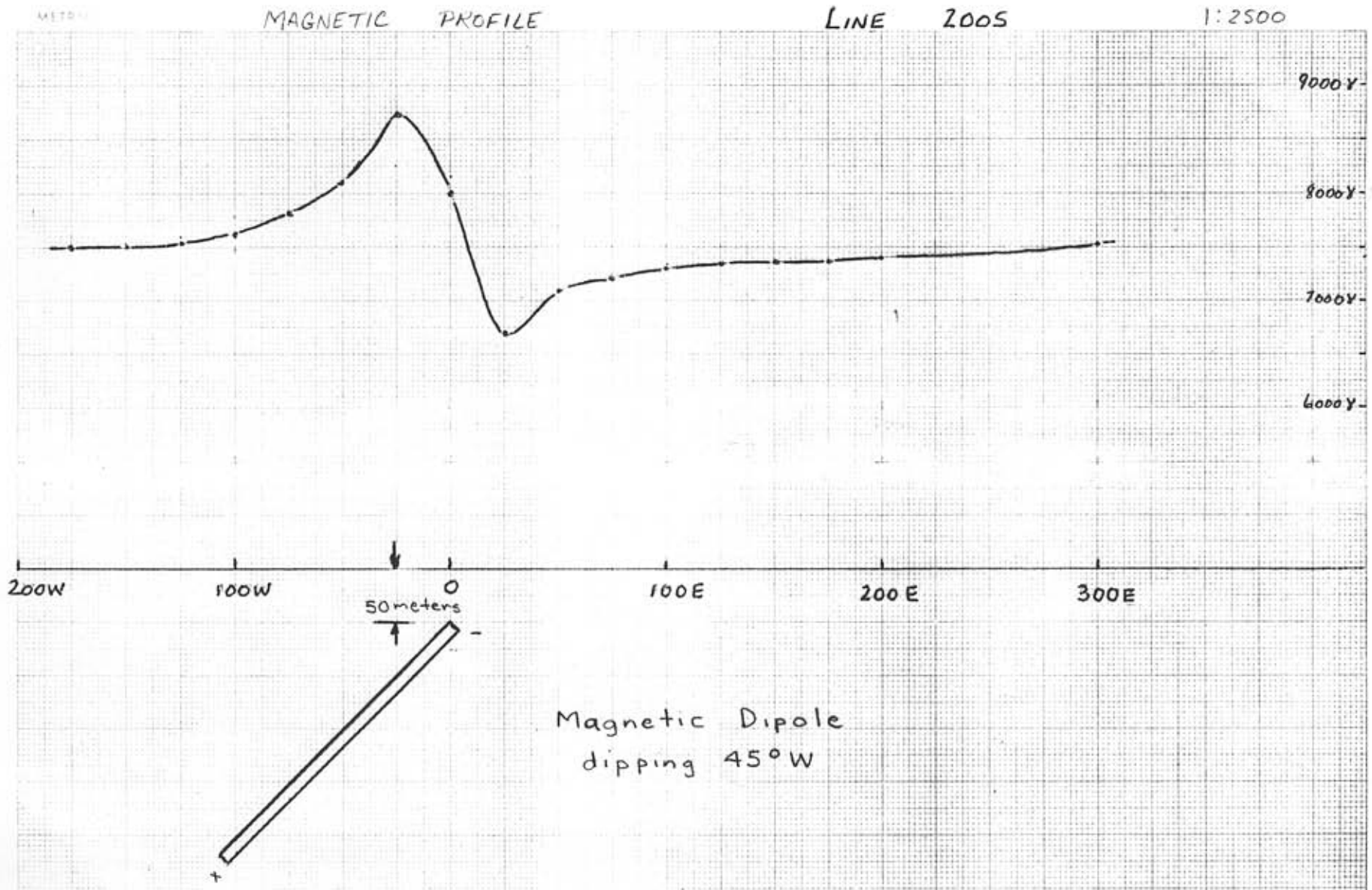
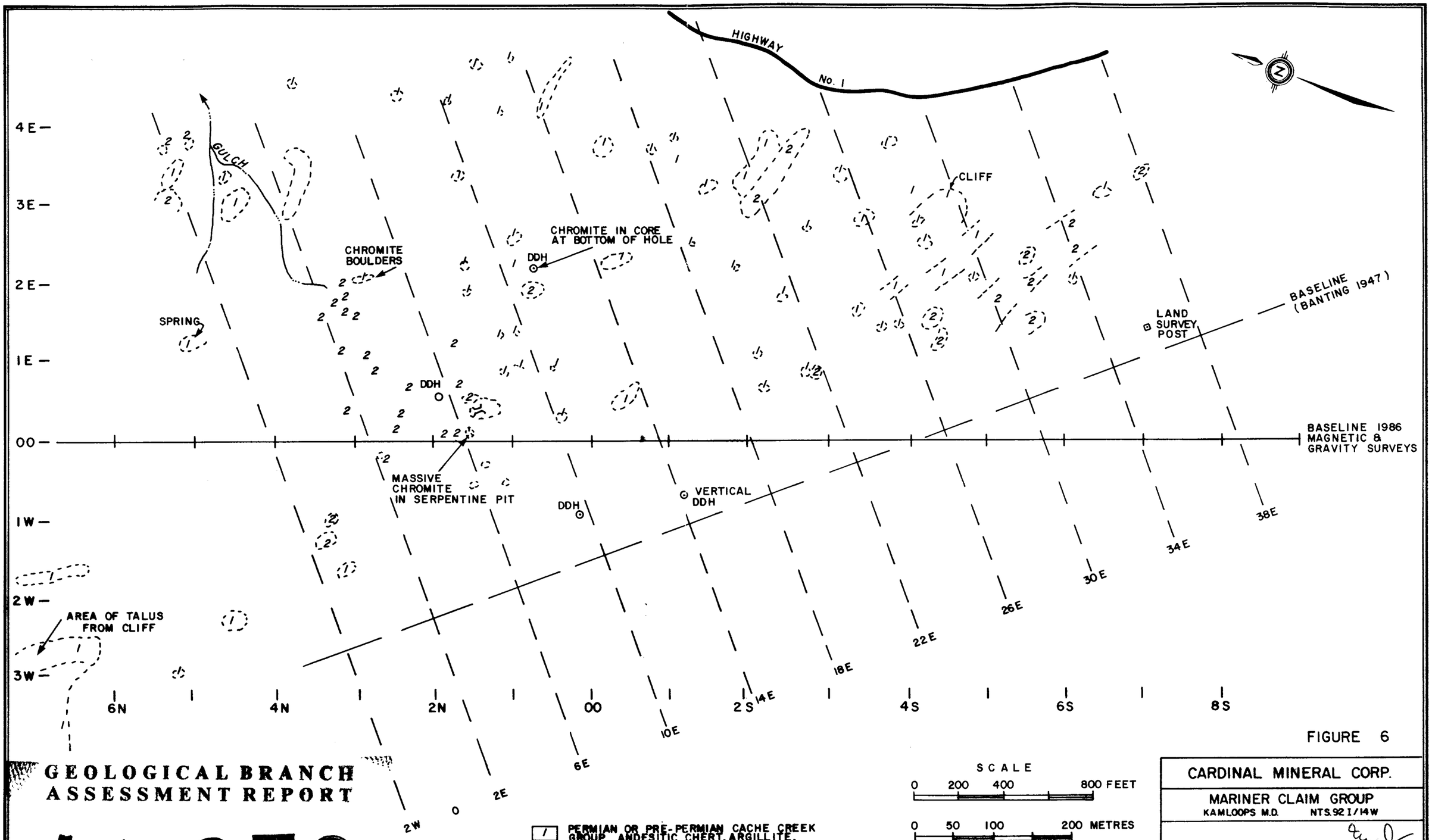

MAGNETIC PROFILE
LINE 2005
1:2500
9000γ
8000γ
7000γ
6000γ
200W
100W
0
100E
200E
300E
50 meters
+
-
Magnetic Dipole
dipping 45° W

Figure 46




GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,050

1 PERMIAN OR PRE-PERMIAN CACHE CREEK GROUP ANDESITIC CHERT, ARGILLITE, QUARTZITE AND LIMESTONE

2 INTRUSIVE CRETACEOUS OR LATER SERPENTINE

SCALE
0 200 400 800 FEET
0 50 100 200 METRES

NOTE:
AFTER H.L. BANTING, OCT. 15, 1947
GEOLOGICAL SKETCH MAP - SHOWING DISTRIBUTION OF SERPENTINE OUTCROPS TO THE CACHE CREEK FORMATION.

FIGURE 6

CARDINAL MINERAL CORP.

MARINER CLAIM GROUP
KAMLOOPS M.D. NTS 92 I/14W

GEOLOGICAL SKETCH MAP

To accompany a report by:
M. Johnson, M. Sc.

Drawn by: GT
Date: March 1987

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,050

# CARDINAL MINERAL CORP.

MARINER CLAIM GROUP
KAMLOOPS M.D. NTS 92 I/14 W

# MAGNETIC PLAN MAP

To accompany a report by:
M. Johnson, M. Sc.

Drawn by: MJ / GT
Date: March, 1987

STRATO GEOLOGICAL ENGINEERING LTD.

FIGURE 4

CLAIM BOUNDARY
BASELINE
12+00N
11+00N
10+00N
9+00N
8+00N
7+00N
6+00N
5+00N
4+00N
3+00N
2+00N
1+00N
0+00
1+00S
2+00S
3+00S
4+00S
5+00S
6+00S
7+00S
8+00S
9+00S
10+00S
11+00S
12+00S
13+00S
14+00S
CACHE CREEK
Bonaparte River
HIGHWAY No. 1
SURVEY POST
C.P. C. MARLOW
May 1986
A
B
10W
8W
6W
4W
2W
2E
4E

1431 — TOTAL FIELD MAGNETOMETER READINGS IN GAMMAS – DATUM 56000 gammas.

—1000— MAGNETIC FIELD STRENGTH CONTOURS IN GAMMAS. CONTOUR INTERVAL 250gammas.

POWER LINE

DRAINAGE GULLY

TRENCH

ROAD

N

CACHE CREEK

Bonaparte River

OLD CARIBOO ROAD

HIGHWAY No. 1

DITCH

DITCH

00 BASELINE

100 W

200 W

300 W

400 W

200 E

300 E

400 E

650 N

550 N

500 N

450 N

400 N

350 N

300 N

250 N

200 N

150 N

100 N

50 N

0

50 S

100 S

150 S

200 S

250 S

300 S

350 S

400 S

450 S

500 S

550 S

600 S

650 S

700 S

800 S

629 500 E

629 000 E

628 000 E

617 000 N

617 500 N

618 000 N

618 500 N

619 000 N

619 500 N

9.5

9.75

10.0

10.25

10.5

10.75

11.00

11.25

11.5

11.75

12.0

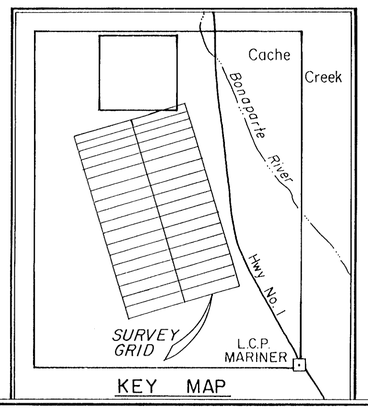
12.25

SCALE 1 2500

0 50 100 150 200 250 Metres

FIGURE 5

KEY MAP




Legend

CREEK

ROAD

Notes:

Instrument: La Coste Rhomberg Gravity Meter
Serial No. G199

Contour Interval : - 0.25 m.gal
- DATUM 4300 m.gal.

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,050

CARDINAL MINERAL CORP.

MARINER CLAIM GROUP
KAMLOOPS M.D. NTS 92 I/14W

# COMPLETE BOUGUER GRAVITY

To accompany a report by :
M. Johnson, M. Sc.

Drawn by AH / GT

Date : March , 1987

STRATOTH GEOLOGICAL ENGINEERING LTD.