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3/87

Assessment Report On The
Geological, Geochemical and Geophysical Surveys
on
LACY AND STOKES CLAIM GROUPS

in

Nanaimo and Alberni Mining Divisions, B.C.

for

Owner/Operator:

LODE RESOURCE CORPORATION
1020 - 475 Howe Street
Vancouver, B.C., V6C 2B3

by

FILMED

ASHWORTH EXPLORATIONS LIMITED
Mezzanine Floor - 744 West Hastings Street
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**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

16,138

Location: NTS 92F/7E, 7W 44'
49° 18' North / 124° 45' West
3-8 km NE of Port Alberni
Vancouver Island, British Columbia

Subject: Results of 1986 - 1987 Field Program and
Recommendations for Additional Exploration

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SUMMARY

The 9 claims of Lacy and Stokes Claim Groups (Esary 1, Lacy 1-4, and Stokes 1-4), totalling 110 units (27.5 km²) cover the northernmost end of the Paleozoic Cowichan Lake - Horne Lake Uplift area. This uplift, the largest of the 3 major uplifts on the Vancouver Island, comprises of Sicker Group volcanic and sedimentary rocks. The other two uplifts are the Buttle Lake Uplift (which contains the Western Mines Buttle Lake ore bodies), and Nanoose Uplift near Nanaimo. The Cowichan-Horne Lake Uplift, which extends from Horne Lake to Salt Spring Island, also contains a number of past producing mines, mainly in Mount Sicker area, and in China Creek - Mount McQuillan area south of Port Alberni. Typically, the ore bodies are the massive volcanogenic sulphide type, which may carry considerable gold and silver. In Mt. McQuillan - China Creek area vein type deposits of gold and silver, associated with copper-lead-zinc, are also common and some were past producers.

Although no economic deposits of either type have so far been found in the above claim groups area, several taconite type iron showings plus some magnetic anomalies were known here previously. There were also some geochemical Total Heavy Metal (Cu + Pb + Zn), anomalies located in the 1960's by Gunnex, and a few small copper occurrences on the property. Limestones, cherty sediments, argillite and volcanics of Sicker Group correlated by Muller (of G.S.C.) with Buttle Lake, Myra and Nitinat Formations, are found in the area of the claim groups.

Since the claims were considered to cover a mineralogically favourable area, a Phase I exploration program, comprising of prospecting and mapping, geochemistry and geophysics, was carried out during the winter 1986-1987 over the major part of the claims area. The results are the subject of this report.

Briefly, a number of geochemical soil anomalies, consisting of precious and base metals, and other associated or "pathfinder" metals, form several, distinct, NW to NNW trending geochemically anomalous zones, following the strike of regional geology. A narrow but persistent gold soil anomaly can be traced for some 5 km in NNW direction across the survey grid on the claims, with Au values up to 415 ppb. There are also several silver anomalies following a similar regional trend.

Geophysical surveys, VLF-EM and ground magnetics, also reveal a number of similarly trending anomalies, or zones consisting of several, closely parallel anomalies. Some of these are associated with geochemical soil anomalies, while others appear to be associated with fault zones (VLF and mag.) or mafic bodies (mag.).

Some massive sulphide type pyrite was observed and sampled in the railway cuts, associated with gabbroic rocks; samples taken here assayed up to 0.46 ounces/ton gold.

It is concluded that the claims warrant more exploration, both for base and precious metals, and a follow-up program is recommended. Work would consist of completing the survey coverage over the entire claim group area, then doing more detailed work in favorable selected areas, followed by trenching and drilling where warranted.

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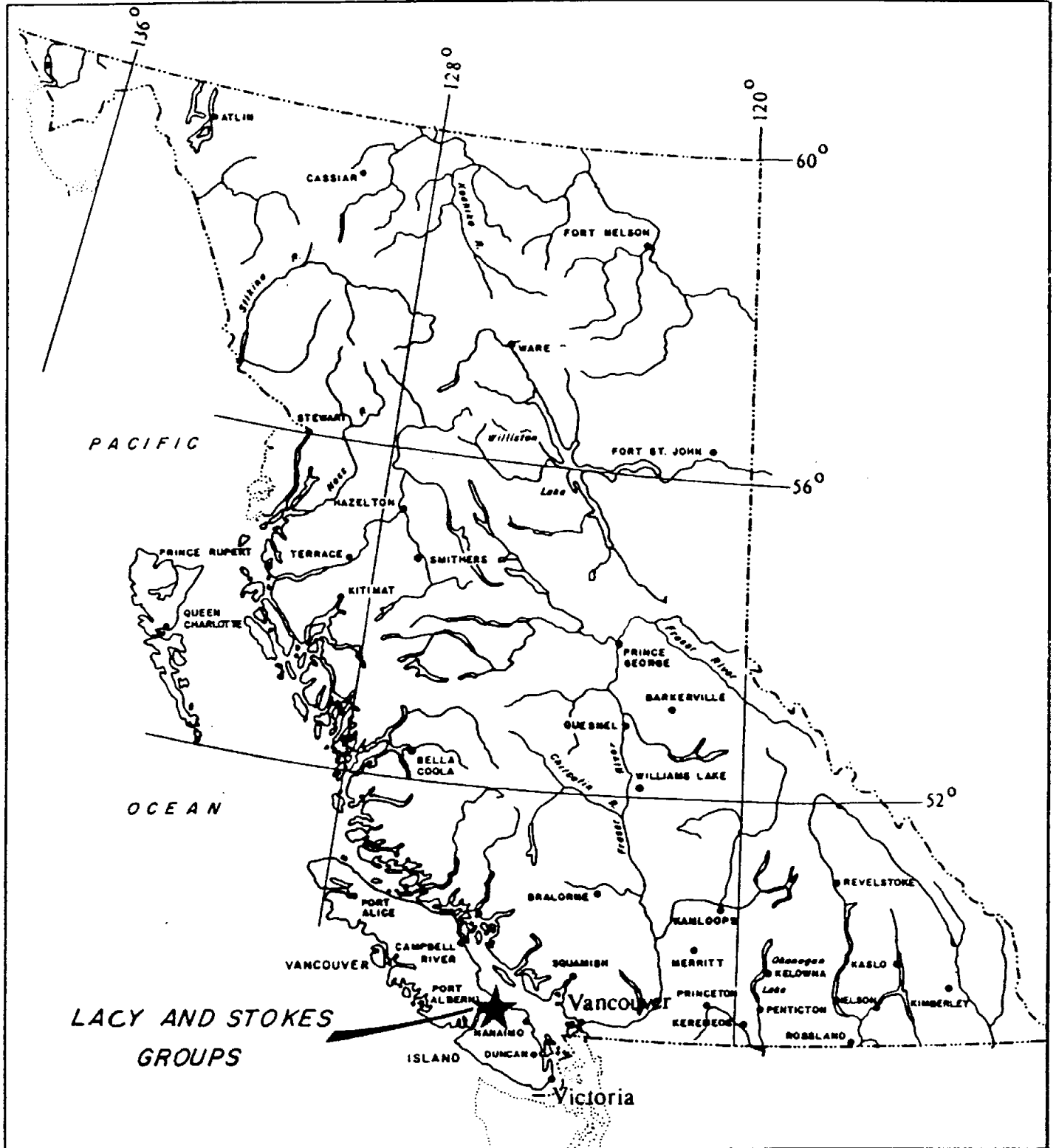
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GEOCHEMICAL ICP ANALYSIS - LAB DATA SHEETS

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LODE RESOURCE CORPORATION	
GENERAL LOCATION MAP	
LACY AND STOKES GROUPS	
NANAIMO AND ALBERNI MINING DIVISIONS	
Scale: 1 : 7 500 000	By: J. S.
Date: OCTOBER, 1986.	Figure 1
Ashworth Explorations Limited	

1. INTRODUCTION

This report was prepared at the request of Mr. T.F. Schorn, president of Lode Resource Corporation, to evaluate and describe the results of a reconnaissance type geological-geochemical-geophysical survey carried out during December, 1986, to February, 1987, on the Lacy-Stokes claim groups NE of Port Alberni, Vancouver Island, B.C. The field work was done by Ashworth Explorations Limited on behalf of Lode Resource Corporation, owner of the property. The report also briefly describes the regional geology, the past and recent exploration activity in the general area, and it outlines a further exploration program. A previous preliminary geological report on Lacy and Stokes claim group, by the author (Laanela, 1986) also summarizes the results of earlier work done in the property area.

These 9 contiguous claims were staked in early 1984 to cover a geologically favourable area underlain by Sicker Group volcanics and sediments. They also contain several exhalative type taconite (iron, with local manganese) occurrences, two airborne magnetic anomalies and two small copper showings, some of which were prospected during the 1960's by Gunnex Limited. Use is made of the information gathered by this author, and others, during the various 1962-1966 exploration programs in the area. The property geology was initially mapped by the author in early 1965, and in greater detail by Mr. Alan Hill in winter of 1986-1987.

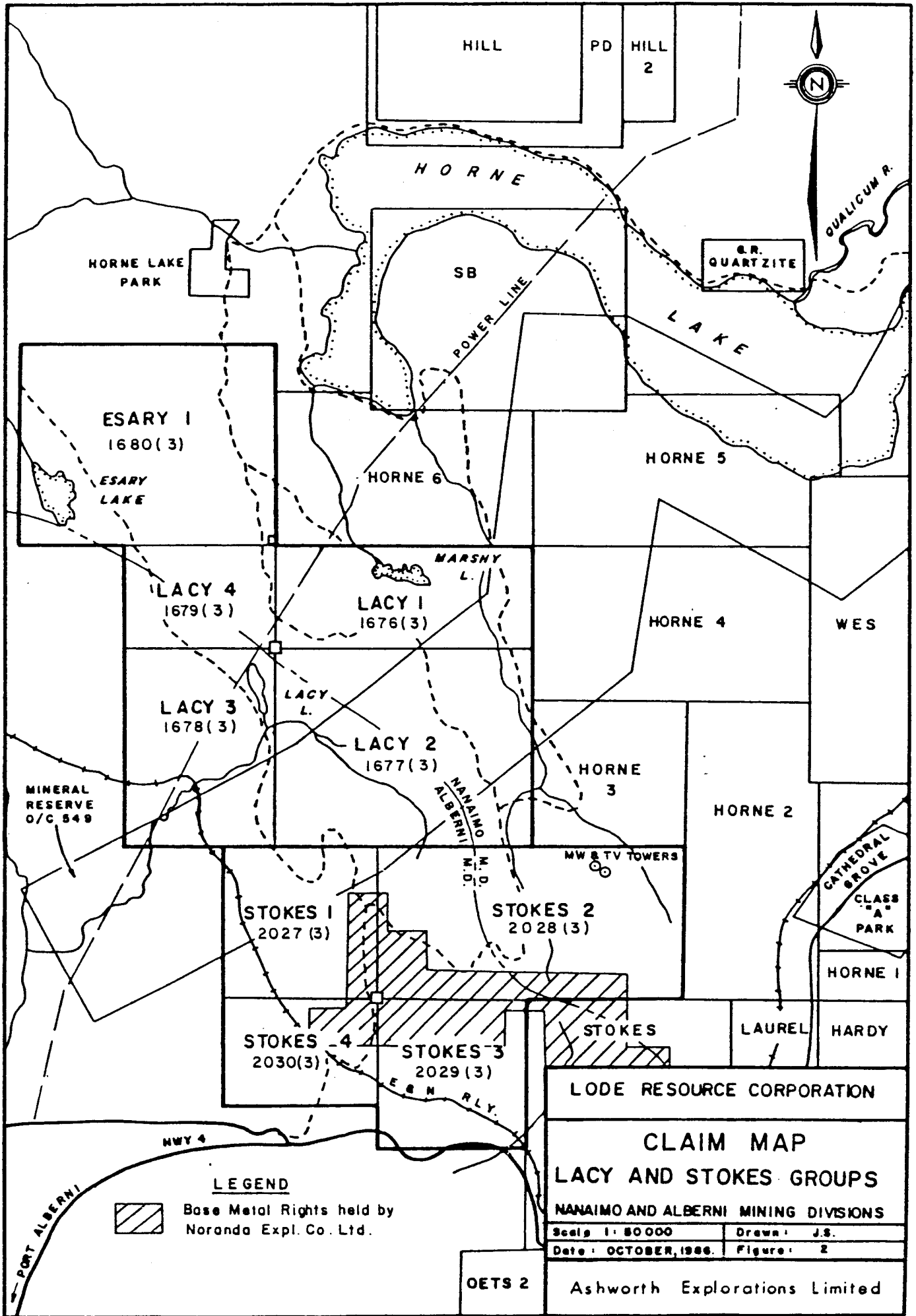
A line-grid was cut on the property in February, 1986, to fill assessment work requirements, but no surveys were then carried out. This grid forms the control of the work carried out here; it consists of 9 km base-line running at azimuth 330 degrees true through the property, and numerous cross-lines.

2. PROPERTY

The Lacy and Stokes Claim Groups consist of following 9 contiguous claims:

<u>Name</u>	<u>Record #</u>	<u>Units</u>	<u>Date Recorded</u>
Lacy Group:			
Lacy 1	1676 (3)	10	March 25, 1984
Lacy 2	1677 (3)	20	March 25, 1984
Lacy 3	1678 (3)	12	March 25, 1984
Lacy 4	1679 (3)	6	March 25, 1984
Esary 1	1680 (3)	20	March 24, 1984
Stokes Group:			
Stokes 1	2027 (3)	9	March 25, 1984
Stokes 2	2028 (3)	18	March 25, 1984
Stokes 3	2029 (3)	9	March 25, 1984
Stokes 4	2030 (3)	6	March 25, 1984

Total: 110 Units = 2,750 hectares = 27.5 km²



All claims are adjoining and the groups straddle the boundary between Nanaimo and Alberni Mining Divisions (see Figure 2).

Lacy 1 is wholly in Nanaimo, M.D.; Stokes 1, 3, and 4, and Lacy 3 are in Alberni M.D.; while Lacy 2 and 4, and Stokes 2 are on both sides of the boundary, Esary 1 is mostly in Nanaimo M.D.

These claims were staked during March, 1984, by Mr. Brent Schorn on behalf of Mrs. Mary Chatfield of Calgary, Alberta. They were sold to Lode Resource Corporation, the present owner, on August 23, 1985. They were grouped as Lacy and Stokes Group (see table above) on March 24, 1986.

Parts of Stokes 1 - 4 claims lie within an area where Noranda Explorations Co. Ltd. has base metal rights under option from MacMillan Bloedel Ltd. (see Figure 2).

The right-of-way for the proposed Vancouver Island Natural Gas Pipeline crosses the Lacy/Stokes property imposing certain conditions on the claim owners, but not disallowing exploration and mining activities (Order-in-Council 549), (see Figure 2).

3. LOCATION AND ACCESS

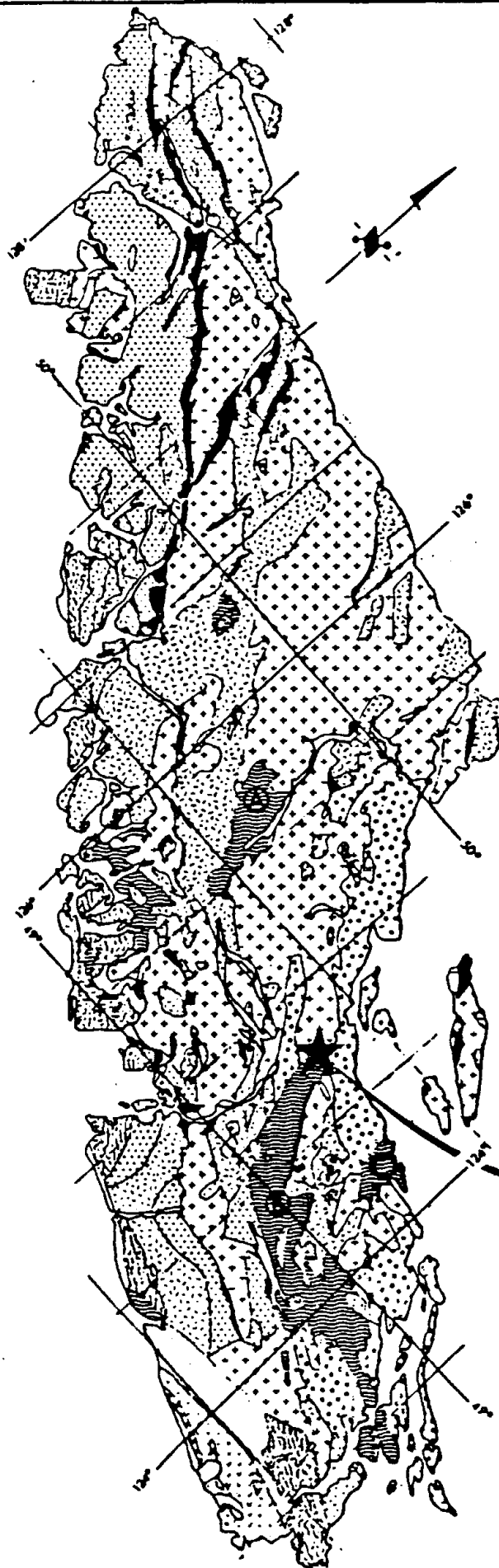
The area covered by Lacy and Stokes Claim Groups is situated between west end of Horne Lake and the Alberni Highway, within 3 - 8 km NE of Port Alberni and within similar distance west of Cameron Lake. CPR railway line passes through the southern end of the property.

The present access is via a gravel road which starts from the highway about 3/4 km east of Timberlodge Motel, crosses the railway track, and then branches in several directions on the property. The main access route crosses a powerline just north of Lacy Lake, connecting with the gravel highway along the north shore of Horne Lake; however, during the 1984 visit this alternate access from the north could not be used since the bridge across Qualicum River was out. Similarly, a third access road, crossing the railway track west of Bostock was also blocked by ditches and felled timber. The present condition of these two alternate access routes is not known to the writer. Many new roads are not shown on the present topographic maps. The use of 4-W-D is recommended, due to some steep hills with loose boulders and gravel.














4. PHYSIOGRAPHY

The claims are located in a rather hilly, forest covered terrain, where the relief ranges from 200 metres elevation in the Alberni Valley to about 550 metres above mean sea level (MSL), but being in the 300 - 450 metre range generally. About a 200m high escarpment trending SE and related to the Cameron River Fault System to the south, runs through the SW part of property; the CPR track descends along the flank of this escarpment into Alberni valley after crossing the mid-island divide between Cameron and Horne Lakes.

Geological sketch map of Vancouver Island.



LEGEND

-  CARMANAH GROUP MIDDLE TERTIARY
-  CATFACE INTRUSIONS EARLY TO MIDDLE TERTIARY
-  METCHOSIN VOLCANICS EARLY TERTIARY
-  NANAIMO GROUP LATE CRETACEOUS
-  QUEEN CHARLOTTE GROUP
KYUQUOT GROUP } LATE JURASSIC TO EARLY CRETACEOUS
-  LEECH RIVER FORMATION
PACIFIC RIM COMPLEX } EARLY CRETACEOUS
-  ISLAND INTRUSIONS EARLY AND (?) MIDDLE JURASSIC
-  BONANZA GROUP EARLY JURASSIC
-  VANCOUVER GROUP } LATE AND (?) MIDDLE TRIASSIC
-  PARSON BAY FORMATION
QUATSINO FORMATION } LATE AND (?) MIDDLE TRIASSIC
-  KARMUTSEN FORMATION } LATE AND (?) MIDDLE TRIASSIC
-  SICKER GROUP PALEOZOIC
-  METAMORPHIC COMPLEXES JURASSIC AND OLDER

- A — BUTTLE LAKE UPLIFT
- B — COWICHAN-HORNE LAKE UPLIFT
- C — NANOOSE UPLIFT

Geology from Muller, GSC, 1980.

LACY and STOKES CLAIM GROUPS



LODE RESOURCE CORPORATION	
REGIONAL GEOLOGY	
LACY AND STOKES GROUPS	
NANAIMO AND ALBERNI MINING DIVISIONS	
Scale	Drawn J.S.
Date: OCTOBER, 1986.	Figure: 3
Ashworth Explorations Limited	

Numerous other off-shoot and branch faults of the Cameron System, mostly trending NNW on the property, give the terrain a blocky, chopped-up appearance, with many locally steep-sided hills or ridges separated by gullies, several small lakes and swampy areas.

The area is generally densely forested. Most of the forest cover is of sizable second growth fir, hemlock and cedar, partly logged off, with old or new logging slash. Some of the "bush" is quite thick for traversing, with heavy chest-high underbrush.

Outcrops are exposed along ridges and in some roadcuts; in the lower parts they tend to be covered by underbrush. The numerous faults, mostly interpreted from airphotos, are generally buried under soil cover, stream sediments and swamps.

5. REGIONAL GEOLOGY

The Lacy-Stokes Claim Groups were staked to cover the northernmost end of the geologically favourable Cowichan - Horne Lake Uplift area of the Paleozoic Sicker Group volcanic and sedimentary sequence (see Muller, 1971, 1977 and 1980). Since this uplift area has become the focus of much exploration and mining activity on Vancouver Island by numerous companies during the past few years, it may be worthwhile to elucidate some points of the economic aspects of Vancouver Island geology here.

Regionally, the claims are located at the north end of one of the three main geologically most favourable and economically most promising areas on the Island. These areas consist of three uplifted Middle - Paleozoic volcanic - arc centres, namely (1) The Buttle Lake Uplift (which contains the Westmin's Buttle Lake massive sulphide deposits) to the north, (2) the smaller Nanoose Uplift, north of Nanaimo, and (3) the Cowichan - Horne Lake Uplift, in the south part of the Island. The latter one is the largest, being some 130 km long (from Horne Lake to Salt Spring Island) and 15-25 km wide, and containing the past base metal and gold producers in Mount Sicker and Mount McQuillan - China Creek areas. All are underlain by Sicker Group volcanics and associated sedimentary rocks, mostly of Devonian Age.

These Sicker Group rocks, consisting of the entire Paleozoic sequence on the Island, appear to be remnant of the Middle-Paleozoic island arc formed on the oceanic crust or possibly along the continental margin. They are now buried under the Mesozoic cover, except where they are now exposed in the above three major (and some smaller) uplift areas. These structural culminations, containing the host-rocks of exhalite type polymetallic deposits, are at present of prime interest in mining exploration on the Island. While the massive sulphides are close to or at the volcanic vents (eg. at Buttle Lake), the precious metal bearing quartz veins, such as those in Mount McQuillan area south of Port Alberni, appear to be more distal and originating over a longer time span, being related to various intrusive events.

The Sicker Group is the oldest rock unit on Vancouver Island and is equivalent to part of the Cache Creek Group on B.C. Mainland. The Sicker rocks are exposed in northerly and NW trending uplifted zones (or large horsts) formed prior to the late Cretaceous.

The lower and thicker part of the Sicker Group is mainly composed of greenstones derived from volcanic breccias and tuffs of intermediate composition. Generally, they occur in gently plunging NW trending open folds of regional extent, but locally they are isoclinally folded and converted to chloritic and sericitic schists. The upper part of the Sicker Group (occurring in Horne Lake area) consists largely of graywacke, argillite and minor conglomerate overlain by limestone and chert. The limestone near Buttle Lake and Horne Lake can be up to 1000 feet thick (Carson, 1973).

The Triassic volcanics of the Vancouver Group, the Karmutsen Formation, overlies the Sicker Group unconformably. In the Horne Lake area they are in fault-contact with Sicker Group, forming the boundaries of the uplifted area.

6. HISTORY AND PREVIOUS WORK

During the 1960's, Gunnex Limited, in partnership with Canadian Pacific Oil and Gas (CPOG), carried out various regional and detail surveys, mostly for base metals, on the E & N Railway Land Grant on Vancouver Island. As part of that program, the area south of Horne Lake, centered on the present Lacy Lake claims, was geologically mapped on 1": $\frac{1}{4}$ mile scale by the author during 1964-1966. Several taconite showings and airborne magnetic anomalies in the claim groups areas were also examined and described.

Subsequent regional mapping of Vancouver Island in 1970's by G.S.C. (Muller, 1971 - 1980) on a more general scale has resulted in revision of the Sicker Group nomenclature in the Cowichan-Horne Lake Uplift area, based on comparison with similar Sicker Group rocks in Buttle Lake area and elsewhere.

A geochemical regional sampling program by Gunnex Ltd. in 1960's for Total Heavy Metals (THM), mostly along roads, outlined several moderately anomalous areas, extending in a roughly outlined belt about 6 km long and up to several km wide, toward SE from the south end of Lacy lake. This larger anomalous area contains a number of clusters and "spot highs" of medium to high range values. To authors knowledge, these have not been followed-up so far.

Most and highest of these geochemical anomalies occurred in the SW half (diagonally) of Lacy 2 claim, extending into adjoining Lacy 3 and Stokes 2 claims.

A helicopter-borne magnetometer survey was carried out in 1962 by Hunting Survey Corporation Limited fro Department of National Resources of the C.P. Railway Company (Calgary), prior to the 1960's joint partnership program with Gunnex Limited on the E & N Railway Land Grant, between latitudes 40° N and 40° 20' N. The purpose of this survey was to locate magnetite bodies of economic size and grade and to assist in (preliminary)geological mapping of the Land Grant area. Only deposits containing high concentrations of magnetite would be detectable. The results of this survey are shown now on the G.S.C. aeromagnetic map 5323G, the Port Alberni Sheet (see References).

Among a number of magnetic anomalies detected by this survey, and later examined on the ground by Gunnex staff, two are located in Lacy and Stokes Claim Groups area.

The author also spent several days during September, 1984, doing reconnaissance geochemical sampling and prospecting on the Lacy-Stokes claims.

7. WINTER 1986 - 1987 PROGRAM

7.1 SCOPE AND PURPOSE

During December 10-21, 1986, January 7-12, February 4-14 and 24-27, 1987, a crew consisting of two geologists and four geotechnicians carried out a reconnaissance type geological-geochemical-geophysical survey over about two-thirds of the Lacy-Stokes claims area. The purpose of this program was:

a) To test by a "grassroots" survey all of the claims area for its mineral potential and to delineate the areas of "favourable" geology, i.e. Sicker Group rocks and particularly the areas underlain by Myra Formation.

b) At the same time, relocate, sample and re-examine several of the previously known taconite ("iron formation")—manganese and small Cu-Ag showings, as well as the aeromagnetic and geochemical "total heavy metal" anomalies (Laanela, 1965 - 1966, 1986).

7.2. METHODS AND PROCEDURES

A 7.2 km long base-line, at azimuth 330° extending diagonally through the property and paralleling the regional geological strike, had been laid out earlier in 1986 as a basis for the control-grid.

300 metre interval cross-lines were run from this base line by hip-chain and compass, across the regional strike.

Additional crosslines, at 100 metre line intervals were run on the South part of the grid, mainly on Stokes 3 and 4 grid, for more detailed surveys. A small 25 metre line interval grid was run in this area over a pyritic massive sulphide showing just north of the railway track, on Stokes 3 claim.

A total of 1,625 B-horizon soil samples were collected along all grid lines, using 50 metre sample intervals in most parts of the grid, and 25 metre intervals in detailed grid areas. The same grid was also used for control of geological mapping and prospecting.

VLF-EM and magnetic surveys were also run along these lines at 25 metre station intervals. Instruments used were VLF-2 EM receiver (tuned to Seattle, Washington, transmitter at 24.8 KHz) and Scintrex MP-2 proton precession magnetometer, respectively. In both cases, reliable readings could not be taken close to the power line due to strong interference from it. Only the in-phase readings were taken during the VLF-EM survey.

All soil samples were placed in marked Kraft-paper bags, field dried and then shipped to Acme Analytical Laboratories at 852 Hastings Street, Vancouver. There the soil samples were dried and sieved to -80 mesh size, then analyzed by Induced Coupled Plasma (ICP) method for a package of 30 elements. These elements included gold, silver, most of the common base metals (eg. Cu, Pb, Zn, etc.), various rock forming metals and a number of trace elements (see lab data sheets in Appendix for further details).

Eight of these elements, Ag, Cu, Pb, Zn, Au, Mo, Ni and Co, were plotted on 1:5,000 scale maps. Similarly, the VLF-EM and the magnetic survey results, along with geological mapping, were plotted on separate 1:5,000 scale sheets.

8. RESULTS

8.1. GEOLOGICAL MAPPING AND PROSPECTING

The property was mapped by Alan Hill, B.Sc. and L. Scroggins, B.Sc. (Hon) at a scale of 1:5,000 (except for the "detail grid area" which was mapped at 1:2,500). The following is from the field report by Mr. Hill.

8.1.1. Property Geology (See Maps 1-A, 1-B and 2)

The claims are underlain predominantly by northwest trending volcanic-volcaniclastic-sedimentary rocks of the Paleozoic Sicker Group, except for the margins of the property where the younger mafic volcanics of the Vancouver Group and sediments of the Nanaimo Group occur. The Sicker Group rocks form a "jigsaw puzzle" of fault blocks and display a very complex stratigraphy with numerous intercalations and rapid lateral facies changes. The rocks are commonly schistose in the vicinity of faults with associated carbonatization and silicification. Elsewhere they are relatively fresh with internal textures and fossils preserved. The stratigraphic nomenclature devised by the G.S.C. (Muller, 1980) was found to be inadequate for mapping at this scale, so a strictly lithological format was adopted. Attempts have been made, however, to place each lithological unit within Muller's succession. The units are described in roughly ascending order.

Unit 1 (oldest?) consists of basaltic to andesitic volcanic and volcanoclastic rocks which occur along the easternmost side of the property, and as a few thin members higher up in the sequence. Pillowed flow textures are common along with quartz and calcite filled amygdules and plagioclase/hornblende porphyritic textures. Clastic rocks are subordinate and range from fine tuffs and reworked tuffs, to coarse agglomeratic and pillow breccia horizons. Lenses of jasper-magnetite iron formation are present in two locations within this unit. The larger occurrence is known as the Cameron Lake Iron Showing and is discussed separately later in this report. Related to Muller's scheme this unit probably represents the uppermost Nitinat Formation.

Unit 2 on the property is the most widespread and also the most complex, displaying discontinuous individual lithologic units, and the most widespread facies changes. Lithologies include massive volcanoclastic "melange" containing clasts and blocks (up to 1m) of all types of volcanic rocks and chert in a poorly sorted wacke-like matrix. This grades laterally into thickly bedded mafic to intermediate lapilli tuff, chert, and chert breccia (containing rip-up clasts). Chemical sedimentary rocks are subordinate and include grey to green chert and lenses of pale red jasperoidal and manganiferous chert (especially north of Lacy Lake). Hematization has locally affected Unit 2, and to a lesser degree Unit 1, imparting to the rocks a streaky and patchy maroon coloured tinge. This alteration is believed to be diagenetic and unrelated to later faulting and fluid movement.

Unit 3 consists of agglomeratic rhyolite flows and felsic tuff, and is relatively uncommon on the property, occurring in the southeast as a single lense up to 150 metres thick. It is quartz and feldspar porphyritic, with minor sericitic tuffaceous beds, and contains numerous white pegmatitic quartz patches and veins. Agglomeratic phases contain clasts 5-15 cm in size, which are sub-rounded and display partially resorbed margins within a fine grained siliceous matrix. Finely disseminated pyrite is present in the matrix and in the clasts.

Unit 4 consists of a very distinctive white to green rhythmically laminated cherty tuff which occurs as lenses and interbeds mainly within Unit 2, and possibly as a lateral equivalent of Unit 3.

Unit 5 comprises dacitic to andesitic flows which underlie a large area in the southern portion of the map-area. These flows are plagioclase and hornblende porphyritic, with phenocrysts up to 5 mm. Minor tuffaceous, cherty, and fragmental beds are also present. Units 2 through 5 correlate with the main body of the Myra Formation of Muller's succession.

Unit 6 is comprised of distinctive calcareous sediments consisting predominantly of thickly bedded crinoidal limestone, with lesser dark grey to black chert and argillite. Minor chloritic tuffaceous material is also present locally, as are weakly jasperoidal chert beds near the (?) paraconformable contact with overlying Vancouver Group volcanics. This unit correlates with the Buttle Lake Formation, and also occurs as lenses within the Myra Formation. Caves, sinkholes and underground streams were encountered while mapping the limy members of this unit. Also, in the vicinity of diabase-gabbro intrusions contact metamorphism has converted the limestone to a cream-coloured marble, which has been quarried economically in the past on the property.

Unit 7 includes diabase and gabbro intrusions which are restricted to Units 2 through 6. The intrusions occur as dyke swarms, sills, and large bodies, and possibly are coeval with Vancouver Group-Karmutsen Formation volcanism. Muller (1980) included these diabase-gabbro intrusions in his "Sediment-Sill Unit" which is an informal division transitional between the Myra and Buttle Lake Formations. On the Lacy-Stokes property these intrusions are common at approximately this stratigraphic level, but also occur lower in Unit 2 as dyke swarms. These dykes display slightly elevated background base and precious metal levels, along with a distinctive high magnetic signature due to the presence of accessory sulphides and magnetite. The large gabbroic intrusion cut by the railway tracks in the south part of the property contains small pod-like bodies and seams of pyrite in the face of a blasted rock-cut. Grab samples here assayed up to 0.46 oz/T gold, and are described as the "main or railway showing" in a following section.

Unit 8 consists of prominently outcropping massive basaltic flows, along with lesser andesite and intrusive equivalents. This unit correlates with the Triassic Vancouver Group (Karmutsen Fm.) and occupies the northern and western margins of the property.

Unit 9 (youngest) is composed of the Cretaceous Nanaimo Group sediments consisting of mainly soft-weathering conglomerate, shale and greywacke, occupying the low-lying areas at the southernmost edge of the property.

8.1.2 Mineralization

Main "Railway" Showing

Located adjacent to the railway tracks between lines 7 + 00 S and 8 + 00 S, this showing contains coarse grained massive pyrite in seams and pods over an area 10 m x 7 m on a vertical rock-cut face. (There is **no** evidence of sulphide mineralization or alteration in original outcrop surfaces on top of the rock-cut.)

Individual sulphide pods are contorted and irregular in shape, up to about 10 cm x 100 cm x 50 cm, and do not express consistent strike direction or lineations, but rather suggest a complex infolding within the enclosing rocks. Grab samples, ranging from 25 - 80% pyrite assayed 14,900 ppb, 6320 ppb, 3580 ppb in gold (or 0.46, 0.19, and 0.11 ounces/ton gold). Host rock consists of fine to medium grained, multiphase, diabase-gabbro intrusions which are often magnetic in hand specimen due to primary accessory magnetite and pyrrhotite. This body of intrusive rock effectively explains the airborne magnetic anomaly detected here by Gunnex Ltd. in the 1960's (Laanela, 1965-66).

Alteration in the rocks is subtle, and not far-reaching and involves bleaching and the development of sericite adjacent to tiny quartz-carbonate-epidote veinlets. These veinlets are common throughout the host rock, but are most concentrated in the immediate vicinity of the pyrite pods. Malachite staining was found associated with these veinlets 10 metres east of the showing, where a grab sample assayed 1993 ppm copper and 25 ppb gold. A suite of three grab samples from the main showing were also analysed for Pt and Pd but returned background levels.

East Track Showing

This showing is about 50 m east of the point where the railway tracks cross the base line. Minor quartz veining and silicification is present within foliated dacite. Some of these veinlets are rusty and contain fine disseminations and blebs of pyrite. Sample LS86-43 contained 5% pyrite, 25% quartz and assayed 2320 ppb gold (0.07 ounces/ton Au). These veinlets occur within a zone 2 to 3 metres wide.

Old Au-Ag Showings

These two small copper-stained pits (about 1 m x 1 m) occur 130 m apart in silicified volcanics near the east end of the line 12 + 00 N, on the west shoulder of the road. The host rocks are porphyritic andesite (?), now somewhat bleached and cut by numerous quartz veinlets containing trace chalcopyrite, bornite, azurite and pyrite mineralization.

Past sampling, (Laanela, 1986), returned assays up to 2.22 oz/ton silver and 0.25 oz/ton silver respectively from the southern and northern pits. Sampling in this program returned only one notable sample assaying 0.50 oz/ton silver and 543 ppm copper from the southern pit. The systems of quartz veinlets controlling this mineralization appear to die out quickly, within a few metres of each blast pit.

Cameron Lake Showing

This showing is well described in previous reports by Laanela (1965-66 and 1986). It was relocated in a low-lying area now overgrown by thick "sala" underbrush at grid co-ordinates 9+00 S/1600 E. The showing consists of multiple contorted and crackle-brecciated jasper lenses ranging in thickness up to 3 metres, and exposed over a strike length of about 250 metres. The lenses are hosted by basaltic volcanics which display pillowed flow textures nearby. Magnetite seams 2-3 cm thick are present within the dark red jasper and are highly contorted. Crackle brecciation is expressed by angular open space infillings of white quartz which uncommonly contains traces of pyrite. Sampling of this material returned background base and precious metal values (sample no. LS86 - 1A and 1B). However, a similar 2 m thick lense of jasper was discovered at the east end of line 9400 N. Here quartz veinlets containing pyrite and malachite were noted and sample LS86 - 62 assayed 1217 ppm copper.

The Cameron Lake Iron showing and surrounding area was examined between 1963 - 1966 by Gunnex Ltd. personnel. An airborne magnetic anomaly occurs 300 metres west of the showing, in an area of little outcrop. This area was carefully prospected during this season's program, but the anomaly was not explained. Schistose and pyritic samples were collected between the showing and the airborne anomaly, but returned low values in all metals. The intensity of the airborne magnetic anomaly, however, suggests that buried lenses of magnetite-jasper iron formation may be responsible.

Lacy Lake Iron - Manganese Showings

These large lenses (up to 50 m thick) of pale jasperoidal chert were also previously examined by Gunnex in the 1960's. They differ markedly from the Cameron Lake Iron Showing in their notable lack of magnetite, and the paler pink to brick red colour of the jasperoidal chert. The manganese mineral pyrolusite was also identified locally, and in sample LS86 - 30 which assayed 4981 ppm Mn. Sulphides were not observed in these showings which, when sampled returned background levels in base and precious metals.

Notes on Manganese (By Alan Hill, B.Sc.)

- The high Mn values (up to 18,862 ppm!) in soils encountered sporadically may be attributable to the glacial dispersion of supergene enriched oxidized layer which once overlaid the Lacy Lake (or other?) Fe-Mn rich chert.

- Manganese has been mined at Hill 60 near Cowichan Lake. J.T. Fyles (1955) describes these upwardly enriched profiles in B.C.D.M. literature. These "laterites" are typically small and have been disturbed by glaciation.

ROCK SAMPLING HIGHLIGHTS

(See geology maps for locations)

Sample #	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Au ppb	Description
LS86-09	38	30	141	.5	86	quartz vein sample, 5% py.
LS86-14	409	24	101	.8	395	25% pyrite in small shear zone.
LS86-15	20	3	10	.1	81	10% coarse pyrite in 4 cm quartz vein; float sample along tracks.
LS86-16	1,993	5	62	.2	25	Malachite stained quartz vein and slickenside material; Main Showing.
LS86-17	21	15	13	.7	<u>6,320</u>	coarse, massive pyrite from 10 cm seam, Main Showing (0.19 oz/t gold).
LS86-18	39	5	65	.1	38	chloritic host rock, Main Showing.
LS86-20	64	6	32	.9	<u>14,900</u>	weathered, sericitic, 25% pyrite from cliff face, Main Showing (0.46 oz/t gold).
LS86-21	93	4	81	.1	29	trace py & magnetite in gabbro, corresponds to soil sample anomaly.
LS86-22	201	4	100	.1	54	0.3 m wide carbonated-filled shear.
LS86-23	77	6	58	.2	87	diabasic rock, 5% diss. po, quartz, and epidote veinlets, Main Showing.
LS86-25	42	7	59	.4	4,750	5 cm pyrite seam in float sample.
LS86-30	11	10	34	.1	22	4,981 ppm Manganese in pale jasper, Lacy Lake Showings.
LS87-33	543	64	157	<u>16.2</u>	3	trace py, cpy in silicified andesite (?), old Cu-Ag Showing (0.50 oz/t silver).
LS87-43	127	5	42	.3	<u>2,320</u>	5% py diss. in silicified dacite, East Track Showing (0.07 oz/t gold).
LS87-44	53	13	56	.1	520	silicified gabbro with quartz stringers, 10% py & po; Main Showing.
LS87-45	22	7	19	.1	<u>3,580</u>	80% pyrite from 1 m x 0.5 m x 0.1 m pod (0.11 oz/t gold); Main Showing.
LS86-62	1,217	6	79	.2	16	trace pyrite & malachite in quartz veinlets, adjacent to jasper lense.
LS86-65	600	28	984	.3	1	trace py, po in diabase dyke.
LS86-68	1,585	58	2,818	4.1	430	carbonatized shear 10 cm wide, 30% pyrite
LS87-78	11	5	3	.3	215	quartz vein float, trace sulphides.
LS87-80	35	2	89	.1	131	3% diss. pyrite in dacitic tuff.

8.2 GEOCHEMICAL SOIL SURVEY

8.2.1 Chalcophile Elements: Ag, Cu, Pb, Zn (See Maps 3A and 3B)

Chalcophile elements have an affinity for sulphur, hence they tend to be concentrated in sulphide minerals; they form covalent bonds with sulphur.

Maps show individual analytical values for silver, copper, lead and zinc. Statistical parameters for each element were calculated. On the maps, all values of "mean plus two standard deviations" or higher, which are normally taken as "anomalous", are underlined. Following is a description of individual elements and their anomalies.

Silver

Silver values of 0.4 ppm or higher are taken as anomalous. Aside from numerous "spot highs" scattered throughout the grid area, there are several noticeable anomalous zones, particularly south and SE of Lacy Lake, trending roughly NNW, parallel to regional geologic strike. The values range from 0.1 to 2.0 ppm Ag, with background in the 0.1 - 0.2 ppm range. Locally, there is some correlation between silver, zinc, copper and lead, and also with gold and some other elements.

Two of the most anomalous zones of silver are:

- just south of Lacy Lake, dimensions some 1300 metres long (and open northwards, toward the lake) and up to 200 - 300 metres wide; this zone has good correlation with gold anomalies also.
- starting a kilometer SE of Lacy Lake, then trending (intermittently) from Line 24N to Line 9S, over a total distance of about 3.5 km. This anomaly is generally quite narrow, usually consisting of one sample per line (i.e. less than 50 metres). A 2.0 ppm Ag value occurs on Line 18N, where the anomaly is about 3 sample intervals, i.e. 150 metres, wide.

Copper

Copper values range from 1 - 284 ppm, with the background in the 20 - 70 ppm range and values of 100 ppm and higher taken as anomalous. Copper anomalies are less extensive than silver; the best copper anomalies are associated with silver anomalies (see above) both south and SE of Lacy Lake. A significant copper anomaly, with a NW strike, length of about 400 metres, occurs along the railway track on the common boundary of Stokes 3 and 4 claims, where it is apparently associated with ultra-basic rocks and pyritic sulphide showings. Another copper anomaly occurs just SE of Esary Lake.

Lead

Lead values range from 2 - 112 ppm, with the background in the 4 - 14 ppm range and values of 20 ppm or higher taken as anomalous. Its anomalies tend to be largely "spot highs", having some lead correlation with copper and zinc.

Zinc

Zinc tends to be quite closely associated with silver; its values range from 14 to 564 ppm. Background is in the 40 - 140 ppm range, and values higher than 175 ppm can be considered as anomalous. The three best anomalous zones for zinc are:

- associated with the silver anomaly south of Lacy Lake;
- associated with silver and copper anomalies SE of Lacy Lake, in the centre of Lacy 2 claim;
- a cluster of small zinc anomalies associated with copper, silver and lead, SE of Esary Lake

8.2.2 Siderophile Elements: Au, Mo, Co, Ni (See Maps 4A and 4B)

Siderophile elements, which also include Fe, P and platinum group elements, are those having primarily an affinity for iron; they are concentrated in Earth's core. They normally prefer the metallic bond characteristics of metals and do not tend to form compounds with oxygen or sulphur, thus explaining why gold and platinum group metals commonly occur as native metals.

Gold

Aside from a number of small and "spot" anomalies present throughout the grid area, gold also forms a rather distinctly outlined NNW trending narrow anomalous zone which extends from the south boundary of the property (Line 14S on Stokes 3 claim) to east of Lacy Lake (Line 36N on Lacy 4 claim). This anomalous zone, or rather, a trend which often zig-zags and branches, has a total length of some 5 km, but for most part is only one-sample-width wide, i.e. 50 metres or less as defined by sample intervals.

The range of gold values in soils is from 1 to 415 ppb, with the background in the 1 - 2 ppb range; the "threshold" value is about 5 - 6 ppb, while the value of 9 ppb Au or higher is taken as anomalous.

The highest gold values, some in hundreds of ppb, occur in the detailed grid area (100 metre interval lines sampled at each 25 metres), on the west part of Stokes 3 claim and in the SW corner of Stokes 2 claim. The Au anomalies here, although part of the abovementioned trend, appear to be more irregularly shaped, perhaps due to more detailed sampling pattern here. A comparison with geology indicates that anomalies are associated with the mafic rocks (diabase and gabbro), also locally with some quartz veins and massive pyritic sulphide occurrences, such as in the "detail grid" area north of the railway track.

Gold shows some local correlation with silver just south of Lacy Lake.

Molybdenum

No significant Mo anomalies occur in the sampled grid area. The possible exemption is a anomalous area, some 300 metres across, on Lines 21 and 24 North, about 1.5 km SE of Lacy Lake, where Mo is also associated with silver, base metals and arsenic anomalies.

The range for "moly" is only 1 - 14 ppm, with a background of 1 ppm, and 3 ppm taken as anomalous.

Cobalt and Nickel

Both Co and Ni (along with Cr) are closely associated here and form similar anomalies. Two main anomalous trends here occur east of Esary Lake, north of Lacy Lake, on Lacy 4 and Esary claims. Other, small anomalous zones occur in the central parts of Stokes 1 and Stokes 3 claims, with some "spot highs" elsewhere on the grid.

Co, Ni (and Cr) are associated with ultrabasic rocks and can be used as pathfinders for platinum group metals (PGM). Since no soil samples so far have been analyzed here for Pt or Pd, it is suggested the samples high in Co-Ni-Cr be re-analyzed for these two PGM elements, particularly if they are already also "high" in other precious or base metals.

Ranges for Co and Ni are 1 - 65 and 1 - 565 ppm respectively. Respective background ranges are 5 - 20 and 10 - 50 ppm, while the above 27 ppm Co and 61 ppm Ni values can be taken as anomalous.

8.3 GEOPHYSICAL SURVEYS

8.3.1 VLF-EM Survey

(See Maps 5A, 5B and 6)

VLF-EM survey was run by taking the in-phase (dip angle) readings only, using the Seattle transmitter. The lack of out-of-phase readings considerably restricts the interpretation of significance of the conductive anomalies. Strong interference from the high-tension powerlines crossing the property, which varied according to atmospheric conditions, as well as the railway tracks, also restricted the information, particularly in some critically anomalous areas associated with massive pyritic sulphide occurrences on Stokes 3 claim.

Notwithstanding these shortcomings of the EM survey, a number of NW to NNW trending, generally parallel to sub-parallel EM conductive zones are present throughout the grid area. They tend to follow the regional geological strike (NW to NNW); several well defined "crossovers" appear to be associated with fault zones, according to geology maps. Similarly, the conductive zones run generally parallel to sub-parallel with the anomalous geochemical trends, although not always coinciding.

Of particular interest are the EM conductive zones close to or closely parallel to the geochemically anomalous zones in the following areas:

1. An about 0.5 km wide belt extending from Lacy Lake for about 2.5 - 3 km SSE in west half of Stokes 2 claim. It contains at least 3 sub-parallel EM conductors associated with Au and Ag geochemical anomalies, plus a zone of combined other geochemical anomalies [including antimony, strontium, manganese, barium, lanthanum (a Rare Earth element), and others].
2. On Lines 9N to 18N at the centre and in the SE quadrant of Lacy 2 claim: two conductive zones converge with a geochemically anomalous belt also containing anomalous silver and some gold values.

3. Another large belt centered east of Esary Lake and on Lacy 4 claim; of a number of EM conductors present, at least 3 appear to be associated with faults. Some small Au-Ag anomalies are present, as well a number of combined anomalies of other elements (mainly Sb, As, Mn, Ba and La). However, the correlation between EM and geochemical anomalies is not as noticeable as in the first example.

For better interpretation of the EM conductors at least some lines should be rerun by taking both in-phase and out-of-phase VLF readings, particularly in the abovementioned 3 areas. Fraser-filtering of the present data, particularly in the 3 blocks or areas discussed above, may also give new insights. Eventually some other, more advanced EM survey methods may have to be considered.

8.3.2 Magnetic Survey (See Maps 7A and 7B)

The readings of the ground magnetic survey, which was run with a proton precession magnetometer, were plotted as profiles because no diurnal corrections were made to allow correlations to be made between adjoining lines. As in the VLF-EM survey, there was strong interference from the powerline and railway tracks on the southern part of the property, hence any readings taken close to these sources of disturbances should be ignored.

The following observation can be made:

There are a large number of mainly NNW trending positive and negative anomalous zones, which, in most cases, tend to run fairly parallel over long distances.

These anomalous zones have the same regional strike as the geology, and geochemical and VLF-EM anomalies.

In some cases there is good to strong correlation between geochemical (eg. Au, Ag, et al), VLF-EM, and magnetic anomalies. Some more interesting examples are:

1. The anomalous zone trending SSE of Lacy Lake, particularly on Lines 12N to 24N (1.2 km strike length), where there is close correlation between magnetic, EM and geochemical anomalies, including gold and silver. Both EM and magnetic anomalies also appear to follow a fault zone in this area.
2. Area SE of Esary Lake where there is some correlation with the VLF-EM anomalies discussed previously, and some soil anomalies. This generally anomalous zone extends toward west side of Lacy Lake, and may in fact connect with the above-mentioned zone extending SSE of Lacy Lake (see Item 1 above); there is a gap in present survey coverage.

There appear to be numerous other, more local correlations between EM and magnetic anomalies, such as in the detail grid area toward south.

9. CONCLUSIONS

The Lacy-Stokes claim groups area appears to have very good potential for hosting both vein-type precious metals and volcanogenic-exhalative massive sulphide type base metal deposits. This opinion is based on the following:

1. Most of the claims area is underlain by geologically favourable Sicker Group rocks, particularly Myra Formation, which is host to a number of mines, both old and new, on Vancouver Island.
2. The presence of chert and taconite "iron formation" rocks on the property indicates a particularly favourable geological environment for exhalative type deposits.
3. A number of geochemical soil anomalies, following the regional NNW trending geological strike, occur on the property. A narrow but persistent gold anomaly extends across most of the grid area surveyed so far over a distance of 5 km. It is attended locally by silver and other metal anomalies, and also by VLF-EM conductors and magnetic anomalies. There are also several other significant silver anomalies.
4. There are also a number of VLF-EM conductors and magnetic anomalies, some of which are coinciding and also associated with geochemical anomalies, and following a general NW-NNW regional strike, similar to geology.
5. Pyritic massive sulphides have been observed just north of the railway track, on southern part of the property. More work has to be done in the detail grid area here to determine the significance of this occurrence.
6. The more "promising" anomalous zones toward north are so far been outlined by reconnaissance type survey lines at 300 metre (nearly 1000 feet) intervals, and at 50 metre (some 150 feet) sample spacings. Hence the details are lacking for the most anomalous areas. Additional surveys (geochemical, geophysical, mapping and prospecting) are still required in selected areas, using at least 100 metre, or even closer (50 or 25 metres?) control line intervals, with 25 to 10 metre stations or sample site spacings. Also, some anomalies and/or anomalous zones are still "open", particularly toward north of Esary Lake; south of Esary Lake, toward west side of Lacy Lake, there is a gap in the coverage in area that appears to be anomalous.

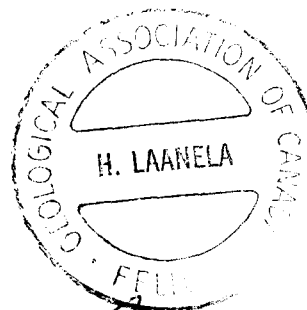
10. RECOMMENDATIONS

1. Complete the reconnaissance type coverage (at 300 metre line intervals) of the remainder of the property, particularly north and south of Esary Lake, and east and west of Lacy Lake. The work would involve soil sampling (using 300 x 50 metre spacing) and VLF-EM and magnetic surveys. Out-of-phase readings should be taken also during the VLF survey.
2. After adding the new data to the present maps, re-evaluate all data and select one or possibly several areas for "follow-up" work. Areas to be considered are the anomalous areas already discussed above, particularly those combining gold-silver anomalies, EM conductor and magnetic anomalies, eg. the area south of Lacy Lake, and others.
3. In the areas selected for "follow-up" work, which may be, say, up to $\frac{1}{2}$ km wide and possibly several km long, lay out additional lines of 100 metre (or locally at 50 metre) intervals, which should be soil sampled at least at 25 metre spacings, or closer where warranted. A VLF-EM survey should be run at 10 - 25 metre station intervals, taking both in-phase and out-of-phase readings. In-phase data should also be Fraser-filtered using several different station intervals (eg. from 10 to 50 metres), in order to differentiate between the local and regional effects. A mag survey should be run using similar station intervals (using smaller intervals in strongly anomalous areas), and all readings should be corrected for diurnal variations (using a base station); data should be contoured on maps. Consider also an S.P. Survey (run a test survey first).

4. The above areas selected for "follow-up" work should also be mapped in greater detail, and prospected. All outcrops should be checked, and if necessary, sampled for assay. All data should be plotted at a 1:2,000 or 1:2,500 scale, or on 1:1,000 scale if more detail is required.
5. After all data from the above surveys is evaluated fully, a program of trenching and more advanced geophysical methods (EM, IP) has to be considered for more limited, most anomalous or most favourable areas, eventually following by drilling of selected targets.

Respectfully submitted by

ASHWORTH EXPLORATIONS LIMITED



A handwritten signature in cursive script that reads "H. Laanela".

Hugo Laanela, F.G.A.C.

June 18, 1987
Vancouver, B.C.

PERSONNEL

The following persons were involved in carrying out the winter 1986 - 1987 Field Program on Lacy-Stokes Claim Group, near Port Alberni:

Alan Hill	Project Geologist/ Party Chief	Dec. 10-17, Jan. 7-12, Feb. 4 - 14
Elizabeth Scroggins	Field Geologist	Dec. 10-21, Jan. 7-12 Feb. 4-9
John Fleishman	Senior Geotechnician	Dec. 10-17, Jan. 7-12, Feb. 4-14, 24-27
Robert Paeseler	Geotechnician	Dec 10-21, Jan 7-12, Feb 4-14, 24-27
Ted Archibald	Geotechnician	Dec 10-21, Jan 7-12, Feb 4-7, 9-14, 24-27
Greg Brown	Geotechnician	Dec 10-21, Jan 7-12, Feb 4-11, 13-14, 24-27
Clive Ashworth	Manager/Supervisor	Dec 16-17, Feb 24-25
Hugo Laanela	Consulting Geologist	Dec 16-17, 1986

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CERTIFICATE

I, Alan R. Hill, residing at #1401 - 1601 Barclay Street, Vancouver, B.C. V6G 1J9, do hereby declare that:

1. I am a geologist, and graduated from the University of Western Ontario, London, Ontario in 1984 with a Bachelor of Science degree in Geology.
2. I have worked during the last 8 years in the geological field in the N.W. Territories, Ontario, Quebec and British Columbia.
3. I worked during December 10-17, 1986, January 7-12, and February 4-14, 1987, as a project geologist on the Lacy-Stokes Claim Groups, subject of this report, and also supervised field work.
4. I have no interest, nor do I expect to receive any interest, in the subject property of this report or in any shares of the company.

Dated at Vancouver, B.C. this 18th day of June, 1987.

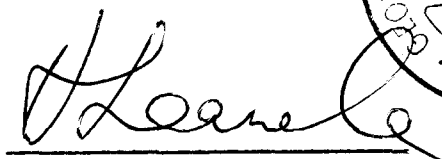
Alan R. Hill, B. Sc.

CERTIFICATE

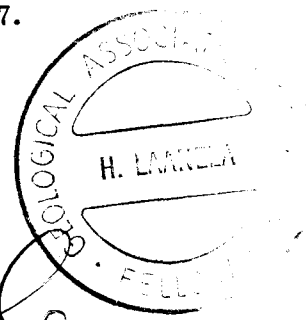
I, Hugo Laanela, of 3657 Ross Road, Nanaimo, B.C. V9T 2S3, do hereby declare that:

1. I am a geologist, graduate of the University of British Columbia, Vancouver, B.C., in 1961 with a B.A. degree in Geology.
2. I am a Fellow of the Geological Association of Canada, and a full member of the Association of Exploration Geochemists, The Canadian Institute of Mining and Metallurgy, and the Australasian Institute of Mining and Metallurgy.
3. I have practiced my profession as a mining exploration geologist since 1961 to 1966 and 1973 to present across Canada, and during 1966 to 1972 as a senior/regional exploration geologist in Australia.
4. During 1964 - 1966 I carried out regional geological mapping and numerous property evaluations on Vancouver Island, including the area discussed in this report. I also worked on the property in September, 1984, and again visited it in Winter, 1986 and in Spring, 1987.
5. The information, opinions and recommendations in this report are based on the field work carried out by myself or under my direct supervision during 1964 - 1966 and 1984, and my study of various survey data on the property.
6. I have no interest in any of the claims of the property, nor have I any shares in the company.
7. I consent to the use of this report in a prospectus or Statement of Material Facts by Lode Resource Corporation for the purpose of private or public financing.

Dated at Vancouver, British Columbia, this 18th day of June, 1987.



Hugo Laanela, F.G.A.C.



APPENDIX A

GEOCHEMICAL RESULTS

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, LL, SM, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: SOILS - BOMESH AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: DEC 22 1986 DATE REPORT MAILED: *Jan 5/87* ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER.

ASHWORTH EXPLORATION PROJECT - LACY STOKES FILE # 86-4052

PAGE 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mo	Ba	Ti	B	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM	PPM
LS86 L21N 0+00	1	27	3	75	.2	27	8	657	2.87	14	5	ND	1	10	1	2	2	77	.40	.050	6	30	.50	50	.08	3	1.63	.03	.03	1	1
LS86 L21N 0+50E	1	53	5	161	.3	47	18	555	5.08	.6	5	ND	2	15	1	2	2	141	.56	.148	4	58	.65	72	.36	3	3.98	.05	.03	1	2
LS86 L21N 1+00E	1	33	3	185	.2	36	15	2118	3.61	4	5	ND	1	16	1	2	2	100	.48	.132	4	38	.39	104	.26	3	2.72	.04	.03	1	1
LS86 L21N 1+50E	1	44	2	116	.2	25	13	798	3.48	7	5	ND	1	14	1	2	2	97	.41	.092	4	34	.34	60	.25	3	2.40	.04	.03	1	1
LS86 L21N 2+00E	3	93	5	95	.4	27	17	816	5.89	5	5	ND	2	13	1	2	2	128	.34	.093	6	46	.56	127	.24	2	4.25	.04	.04	2	11
LS86 L21N 2+50E	1	26	6	70	.2	17	8	296	4.70	2	5	ND	1	14	1	2	2	136	.33	.071	3	42	.25	56	.27	2	2.03	.03	.02	1	1
LS86 L21N 3+00E	2	71	2	88	.3	42	17	404	5.52	7	5	ND	2	13	1	2	2	155	.36	.041	4	56	.45	58	.33	3	3.92	.04	.02	1	2
LS86 L21N 3+50E	2	54	5	83	.1	29	13	1195	5.17	3	5	ND	2	14	1	2	2	147	.38	.042	5	47	.40	65	.32	2	3.04	.04	.02	1	1
LS86 L21N 4+00E	1	47	5	73	.5	34	16	2361	4.41	2	5	ND	2	18	1	2	2	120	.56	.035	8	65	.41	78	.28	2	3.04	.04	.02	1	1
LS86 L21N 4+50E	1	66	3	61	.3	36	14	303	5.56	7	5	ND	1	11	1	2	2	155	.37	.062	3	52	.53	49	.32	2	3.76	.04	.02	1	13
LS86 L21N 5+00E	3	52	4	49	.2	24	10	236	5.09	6	5	ND	2	13	1	2	2	157	.33	.035	4	49	.34	39	.32	2	2.78	.04	.02	2	1
LS86 L21N 5+50E	3	59	5	78	.4	27	13	330	5.66	6	5	ND	2	14	1	2	2	168	.41	.032	3	48	.40	68	.34	2	3.16	.04	.03	1	1
LS86 L21N 6+00E	1	41	3	48	.3	23	11	261	4.48	7	5	ND	1	13	1	2	2	135	.35	.028	7	37	.43	56	.25	2	2.63	.04	.01	1	7
LS86 L21N 6+50E	1	61	3	77	.2	34	14	269	6.34	30	5	ND	1	13	1	2	2	169	.34	.042	3	67	.53	60	.30	2	4.09	.04	.02	1	1
LS86 L21N 7+00E	2	81	4	71	.3	34	14	259	5.34	12	5	ND	2	12	1	2	2	157	.36	.023	3	52	.54	62	.30	3	3.49	.04	.03	1	3
LS86 L21N 7+50E	1	68	4	64	.3	31	12	225	5.24	3	5	ND	2	12	1	2	2	155	.33	.018	4	48	.54	64	.30	2	3.13	.04	.03	1	1
LS86 L21N 8+00E	1	24	2	40	.3	13	5	147	4.63	5	5	ND	1	13	1	2	2	152	.28	.025	3	35	.21	31	.26	2	1.74	.03	.02	1	3
LS86 L21N 8+50E	2	83	7	87	.1	18	11	924	6.28	3	5	ND	2	10	1	2	2	154	.23	.116	7	33	.44	61	.14	2	3.04	.03	.04	1	3
LS86 L21N 9+00E	2	56	7	83	.2	27	13	517	5.23	19	5	ND	2	10	1	2	2	133	.24	.077	4	55	.53	46	.19	2	4.47	.03	.03	1	2
LS86 L21N 9+50E	1	14	7	39	.1	10	4	173	3.64	9	5	ND	1	13	1	2	2	107	.24	.036	5	28	.23	27	.13	2	1.56	.03	.01	1	1
LS86 L21N 10+00E	2	41	6	93	.2	26	12	1232	4.44	7	5	ND	1	17	1	2	2	120	.46	.083	4	44	.48	79	.19	2	2.21	.04	.03	1	1
LS86 L21N 10+50E	1	5	2	44	.1	12	3	51	1.41	16	5	ND	1	1	1	2	3	27	.03	.020	2	4	.04	7	.01	5	.32	.01	.01	1	1
LS86 L21N 11+00E	3	28	4	88	.2	21	7	403	3.72	12	5	ND	1	11	1	2	2	101	.32	.059	3	35	.31	37	.13	2	2.07	.03	.02	1	1
LS86 L21N 11+50E	1	21	6	81	.2	15	7	301	3.37	12	5	ND	1	14	1	2	2	95	.33	.050	3	31	.25	33	.13	2	1.87	.03	.03	1	1
LS86 L21N 12+00E	1	25	2	70	.2	25	8	404	2.09	6	5	ND	1	7	1	2	2	48	.18	.036	2	24	.25	37	.04	4	1.98	.02	.02	1	1
LS86 L21N 12+50E	3	18	10	174	.1	30	7	752	2.70	15	5	ND	1	8	1	2	2	50	.24	.132	5	29	.25	49	.06	4	1.81	.02	.02	1	1
LS86 L21N 13+00E	2	34	4	95	.2	41	12	422	4.25	19	5	ND	2	12	1	2	2	109	.35	.066	4	48	.44	69	.15	3	3.02	.03	.03	1	1
LS86 L21N 13+50E	1	13	2	93	.1	26	8	386	2.46	5	5	ND	1	10	1	2	2	63	.24	.047	3	29	.71	36	.07	3	1.88	.03	.02	1	1
LS86 L21N 14+00E	2	31	5	84	.2	28	9	326	3.37	10	5	ND	1	9	1	2	2	82	.20	.043	6	31	.51	39	.12	2	2.19	.02	.02	1	1
LS86 L21N 14+50E	3	60	8	144	.4	38	13	773	4.68	22	5	ND	2	12	1	2	2	101	.24	.131	6	46	.56	55	.13	2	2.75	.03	.03	1	1
LS86 L21N 15+00E	9	38	4	98	.3	20	25	397	7.34	38	5	ND	2	19	1	2	2	215	.28	.079	8	53	.37	44	.27	2	4.33	.04	.03	2	2
LS86 L21N 15+50E	7	26	13	208	.5	5	24	1930	10.09	58	6	ND	2	21	1	2	2	91	.35	.320	15	11	.67	43	.71	7	2.79	.05	.07	1	1
LS86 L21N 16+00E	4	28	8	174	.5	6	20	1568	8.59	23	5	ND	2	22	1	2	2	120	.50	.324	10	10	1.36	38	.63	2	3.21	.05	.08	1	1
LS86 L21N 16+50E	6	36	10	187	.3	14	19	831	7.88	52	5	ND	2	24	1	2	2	146	.47	.273	6	27	.94	43	.71	2	3.13	.05	.05	1	1
LS86 L21N 17+00E	4	33	16	254	.3	16	23	1411	5.66	131	5	ND	1	24	1	2	2	119	.50	.111	6	36	.41	41	.37	2	2.14	.04	.04	1	1
LS86 L21N 17+50E	3	68	11	178	.3	21	14	552	6.42	18	5	ND	2	13	1	2	2	169	.22	.048	5	52	.41	50	.29	2	3.04	.03	.03	1	1
STD C/AU-S	21	58	39	134	7.2	68	28	1005	3.93	38	21	7	34	47	18	16	18	63	.48	.103	35	60	.88	177	.08	34	1.72	.09	.13	13	50

ASHWORTH EXPLORATION PROJECT - LACY STONES FILE # 86-4052

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SAMPLE#	Mc PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe I	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Ki PPM	V PPM	Ca I	P I	La PPM	Cr PPM	Mo I	Ba PPM	Ti I	F PPM	Al I	Na I	I I	W PPM	Au# PPB
LSB6 L21M 18+00E	2	140	13	117	.2	17	10	480	5.92	9	5	ND	1	19	1	2	2	153	.23	.095	4	39	.59	47	.19	2	3.74	.03	.03	1	8
LSB6 L21M 18+50E	1	36	10	89	.2	14	14	<u>1320</u>	3.84	2	5	ND	1	24	1	2	2	106	.41	.041	10	25	.29	97	.12	2	1.99	.03	.03	1	2
LSB6 L21M 19+00E	1	52	13	69	.1	19	9	390	6.53	12	5	ND	2	18	1	2	2	166	.36	.147	3	48	.63	32	.25	3	2.94	.04	.03	1	2
LSB6 L21M 19+50E	1	15	14	36	.1	5	5	286	6.76	4	5	ND	2	92	1	2	2	317	.51	.059	4	28	.45	16	.35	4	2.13	.04	.03	1	1
LSB6 L21M 20+00E	1	24	7	57	.2	5	18	716	2.73	2	5	ND	1	31	1	2	2	92	.28	.045	4	9	.45	44	.04	2	2.57	.03	.04	1	4
LSB6 L21M 20+50E	1	33	11	55	.1	12	6	275	4.41	2	5	ND	1	22	1	2	2	129	.30	.061	4	37	.37	35	.17	2	2.69	.03	.02	1	1
LSB6 L21M 21+00E	1	19	13	62	.1	14	11	527	5.61	3	5	ND	1	114	1	2	2	205	1.12	.035	5	57	.45	51	.19	3	2.37	.05	.02	1	13
LSB6 L21M 21+50E	1	18	10	50	.1	12	8	749	4.03	3	5	ND	1	39	1	2	2	148	.60	.027	4	36	.48	80	.19	4	1.86	.04	.03	1	1
LSB6 L21M 22+00E	1	15	9	67	.1	8	8	536	4.08	2	5	ND	1	21	1	2	2	126	.33	.077	4	28	.38	81	.10	2	2.00	.03	.02	1	1
LSB6 L21M 22+50E	1	64	11	83	.1	95	23	767	5.11	7	5	ND	1	19	1	2	2	168	.26	.040	5	320	2.31	72	.04	4	2.93	.04	.02	1	1
LSB6 L21M 23+00E	2	37	12	97	.2	24	18	907	5.32	2	5	ND	1	24	1	2	2	146	.49	.047	5	42	.57	74	.34	2	2.78	.04	.03	1	1
LSB6 L21M 23+50E	1	41	7	82	.2	25	11	<u>1326</u>	4.22	6	5	ND	1	16	1	2	2	121	.38	.066	4	42	.59	88	.17	5	2.34	.04	.03	1	1
LSB6 L21M 24+00E	1	28	12	75	.3	27	17	<u>1307</u>	4.58	5	5	ND	1	35	1	2	2	114	.69	.064	5	56	.77	89	.21	4	2.07	.05	.04	1	4
LSB6 L21M 24+50E	1	47	8	105	.2	33	12	723	4.46	7	5	ND	1	14	1	2	2	127	.34	.180	3	45	.60	70	.23	3	3.13	.04	.03	1	1
LSB6 L21M 25+00E	2	46	14	97	.9	34	12	525	5.10	14	5	ND	1	16	1	5	2	124	.35	.046	4	48	.42	115	.13	3	2.17	.03	.03	1	5
LSB6 L18M 0+00	1	75	7	66	.3	39	15	414	4.72	12	5	ND	2	18	1	2	2	132	.39	.021	5	56	.91	261	.22	3	3.54	.04	.04	1	4
LSB6 L18M 0+50E	1	56	9	87	.2	37	12	496	4.29	16	5	ND	1	12	1	2	2	121	.38	.075	3	46	.53	71	.17	5	3.09	.03	.03	1	6
LSB6 L18M 1+00E	1	19	9	208	.2	30	15	<u>1075</u>	5.20	12	5	ND	1	10	1	2	2	99	.22	.145	4	57	.25	82	.09	2	2.87	.03	.04	1	2
LSB6 L18M 1+50E	1	16	7	209	.8	36	10	<u>1314</u>	4.41	15	12	ND	2	8	1	2	2	84	.30	.122	29	49	.21	90	.01	2	2.07	.03	.04	1	4
LSB6 L18M 2+00E	1	15	15	423	1.1	37	9	<u>4507</u>	2.95	15	6	ND	2	19	3	2	2	53	.76	.172	33	35	.24	135	.03	7	2.12	.04	.06	1	2
LSB6 L18M 2+50E	1	44	6	119	.2	41	13	512	4.75	11	5	ND	1	13	1	2	2	131	.30	.072	4	55	.46	69	.21	3	3.12	.04	.02	1	3
LSB6 L18M 3+00E	1	42	15	130	.2	18	16	<u>1832</u>	5.34	7	5	ND	1	11	1	2	2	121	.26	.150	5	41	.24	111	.19	2	2.85	.03	.03	1	5
LSB6 L18M 3+50E	1	9	9	44	.2	6	5	898	2.62	5	5	ND	1	12	1	2	2	83	.17	.052	3	26	.22	75	.04	3	1.73	.02	.04	1	17
LSB6 L18M 4+00E	1	96	7	279	.4	43	20	766	6.60	17	7	ND	2	12	1	2	2	92	.31	.061	11	36	.65	97	.06	5	4.45	.04	.04	1	6
LSB6 L18M 4+50E	1	43	16	80	.2	12	9	<u>1798</u>	7.27	21	5	ND	1	12	1	2	2	112	.27	.107	9	32	.30	73	.17	3	3.02	.04	.03	1	9
LSB6 L18M 5+00E	1	28	16	119	.1	15	24	<u>1751</u>	6.73	12	5	ND	1	16	1	2	2	223	.33	.121	4	23	.75	121	.16	3	2.83	.04	.04	1	1
LSB6 L18M 5+50E	1	7	9	42	.1	3	12	<u>1371</u>	7.02	10	5	ND	1	5	1	2	2	185	.08	.056	8	3	.27	61	.01	2	1.58	.02	.03	1	2
LSB6 L18M 6+00E	1	56	9	78	.1	25	13	275	6.44	26	5	ND	1	11	1	2	2	177	.32	.028	4	44	.46	57	.29	2	2.76	.04	.02	1	5
LSB6 L18M 6+50E	1	40	15	84	.2	10	13	<u>1927</u>	5.03	10	5	ND	1	12	1	2	2	120	.26	.059	5	20	.55	127	.06	2	2.42	.04	.04	1	8
LSB6 L18M 7+00E	1	15	14	59	.1	9	9	<u>1843</u>	2.62	3	5	ND	1	14	1	2	2	84	.56	.040	7	22	.75	86	.01	2	1.86	.04	.05	1	1
LSB6 L18M 7+50E	1	35	11	75	.1	16	9	329	6.45	14	5	ND	1	13	1	2	2	175	.24	.120	3	40	.52	48	.14	2	2.74	.03	.02	1	1
LSB6 L18M 8+00E	1	68	11	96	.3	25	13	399	5.31	7	5	ND	1	16	1	3	2	152	.39	.068	4	47	.47	50	.22	2	2.95	.04	.03	1	1
LSB6 L18M 8+50E	1	75	10	89	.2	40	17	593	5.98	17	5	ND	2	11	1	2	2	147	.26	.059	5	65	.50	63	.19	2	4.33	.04	.03	1	1
LSB6 L18M 9+00E	1	59	18	117	.2	20	20	547	6.03	10	5	ND	2	9	1	3	2	109	.16	.095	8	31	.23	78	.06	2	3.57	.03	.05	1	1
LSB6 L18M 10+00E	2	55	8	110	.2	19	12	312	4.90	6	5	ND	1	16	1	2	2	132	.28	.060	5	39	.45	61	.18	2	2.81	.03	.03	1	1
LSB6 L18M 10+50E	1	43	10	90	.2	15	11	367	4.84	10	5	ND	1	14	1	2	2	127	.26	.044	5	31	.54	73	.08	2	2.51	.03	.03	1	9
STD C/AU-S	22	61	40	139	7.4	70	29	1035	3.97	39	23	8	34	48	18	16	18	65	.48	.106	36	59	.88	181	.08	33	1.72	.09	.14	12	53

ASHWORTH EXPLORATION PROJECT - LACY STORES FILE # 86-4050

PAGE 3

SAMPLE#	Mc	Cu	Pt	Zn	Ag	Ni	Co	Mn	Fe	As	U	Mo	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mo	Ba	Ti	B	Al	Mg	F	N	Au
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
LSB6 L18M 11+00E	1	60	11	60	.1	23	13	377	5.04	3	5	ND	2	19	1	2	2	147	.42	.029	4	45	.66	91	.17	2	2.85	.04	.03	1	1
LSB6 L18M 11+50E	1	32	10	115	.1	20	17	2670	5.47	4	5	ND	1	36	1	2	2	151	.61	.043	6	37	.84	132	.16	2	2.98	.04	.05	1	3
LSB6 L18M 12+00E	1	14	6	29	.1	8	4	136	3.83	2	5	ND	1	17	1	2	2	135	.30	.013	4	27	.25	30	.16	2	1.56	.03	.02	1	1
LSB6 L18M 12+50E	1	30	9	47	.1	12	5	166	4.23	2	5	ND	1	15	1	2	2	118	.21	.035	4	31	.35	25	.09	2	2.66	.03	.03	2	4
LSB6 L18M 13+00E	1	23	7	46	.1	9	4	145	3.44	5	5	ND	1	13	1	2	2	104	.23	.035	4	30	.22	24	.13	2	1.82	.03	.03	2	1
LSB6 L18M 13+50E	1	12	5	39	.1	7	4	331	2.02	2	5	ND	1	13	1	2	2	69	.25	.023	4	16	.16	32	.13	2	1.16	.02	.02	2	1
LSB6 L18M 14+00E	1	30	15	234	.5	47	16	1762	3.74	28	5	ND	1	17	1	2	2	73	.47	.114	13	39	.50	87	.06	2	2.22	.03	.04	1	1
LSB6 L18M 14+50E	1	49	38	307	2.0	85	28	6928	4.72	26	5	ND	2	65	3	2	2	76	1.73	.124	66	54	.43	255	.09	5	3.54	.06	.06	1	1
LSB6 L18M 15+00E	1	31	12	129	.5	28	10	268	5.14	13	5	ND	1	15	1	2	2	126	.25	.032	6	40	.47	67	.15	2	2.95	.03	.05	1	1
LSB6 L18M 15+50E	1	29	16	232	.4	110	40	6474	6.71	12	5	ND	2	22	2	2	2	114	.56	.102	11	136	3.12	133	.34	5	3.70	.06	.05	1	7
LSB6 L18M 16+00E	1	34	8	105	.2	14	9	535	5.39	34	5	ND	2	11	1	2	2	88	.20	.104	8	27	.43	30	.12	2	2.58	.03	.04	1	1
LSB6 L18M 16+50E	1	18	8	62	.1	30	11	413	4.43	28	5	ND	1	7	1	2	2	111	.11	.054	5	69	.32	45	.02	2	1.59	.02	.03	1	1
LSB6 L18M 17+00E	1	184	14	132	.1	14	40	3190	9.64	25	5	ND	1	19	1	2	2	210	.19	.157	4	52	1.27	95	.08	11	3.46	.04	.07	1	3
LSB6 L18M 17+50E	1	6	6	18	.1	3	2	144	1.85	2	5	ND	1	61	1	2	2	113	.72	.019	3	15	.21	10	.23	2	.89	.03	.02	1	1
LSB6 L18M 18+00E	1	50	15	50	.1	13	6	504	5.81	6	5	ND	2	28	1	2	2	162	.33	.054	3	41	.48	28	.22	2	3.18	.04	.03	1	1
LSB6 L18M 18+50E	1	87	7	71	.2	34	15	327	5.69	8	5	ND	2	11	1	2	2	173	.29	.039	6	61	.68	43	.31	4	4.35	.04	.04	2	1
LSB6 L18M 19+00E	1	69	11	72	.1	24	10	369	7.60	11	5	ND	2	15	1	2	2	225	.34	.179	4	51	.74	30	.31	8	3.10	.04	.03	1	1
LSB6 L18M 19+50E	1	50	13	56	.1	25	17	575	5.78	19	5	ND	1	10	1	2	2	187	.14	.039	4	50	.28	88	.02	3	2.56	.03	.05	1	4
LSB6 L18M 20+00E	1	20	16	79	.1	13	10	483	5.04	4	5	ND	1	20	1	2	2	183	.28	.084	3	58	.44	57	.26	3	1.60	.03	.03	1	1
LSB6 L18M 20+50E	1	63	24	118	.5	99	42	1770	5.31	74	5	ND	1	26	1	2	2	203	.64	.107	6	309	2.01	188	.18	12	2.92	.05	.03	1	1
LSB6 L18M 21+00E	1	48	12	52	.2	31	11	278	4.53	3	5	ND	1	12	1	2	2	131	.32	.036	3	59	.51	65	.22	2	2.62	.04	.03	1	1
LSB6 L18M 21+50E	1	54	19	242	.4	38	15	290	4.83	15	5	ND	1	13	1	2	2	127	.36	.060	4	63	.61	79	.22	2	2.81	.04	.03	1	2
LSB6 L18M 22+00E	1	54	12	113	.4	35	13	2151	3.89	8	5	ND	1	19	4	2	2	103	.68	.052	16	57	.64	219	.20	3	2.76	.05	.04	1	1
LSB6 L18M 22+50E	1	29	11	53	.2	15	6	236	4.10	4	5	ND	1	13	1	2	2	117	.25	.047	4	35	.35	30	.19	2	2.12	.03	.03	1	2
LSB6 L18M 23+00E	1	3	9	19	.1	9	2	108	1.86	2	5	ND	1	22	1	2	2	94	.29	.047	3	30	.13	11	.66	2	.54	.03	.01	1	1
LSB6 L18M 23+50E	1	11	9	48	.3	37	12	1143	2.86	2	5	ND	1	31	1	2	2	103	.31	.035	4	99	.87	30	.71	2	1.52	.04	.03	1	1
LSB6 L18M 24+00E	1	17	10	54	.1	20	7	328	3.95	3	5	ND	1	21	1	2	2	125	.32	.030	4	51	.37	53	.27	2	1.71	.03	.03	1	1
LSB6 L18M 24+50E	1	27	5	42	.1	19	7	145	5.52	5	5	ND	1	11	1	2	2	150	.20	.024	3	45	.47	44	.09	2	2.57	.03	.04	2	1
LSB6 L18M 25+00E	1	13	7	40	.1	12	4	171	3.05	2	5	ND	1	26	1	2	2	101	.31	.048	3	36	.26	25	.23	2	1.30	.03	.02	1	1
LSB6 L15M 0+00	1	63	8	85	.4	37	14	846	4.31	16	5	ND	2	15	1	2	2	116	.57	.062	8	45	.66	110	.22	2	2.67	.05	.04	1	1
LSB6 L15M 0+50E	1	19	3	113	.1	20	7	701	2.28	5	5	ND	1	7	1	2	2	59	.25	.051	5	22	.23	82	.07	2	1.76	.02	.03	1	1
LSB6 L15M 1+00E	1	21	13	56	.1	14	8	1700	3.52	2	5	ND	1	20	1	2	2	109	.45	.038	4	26	.27	112	.24	2	1.70	.03	.03	1	2
LSB6 L15M 1+50E	1	27	8	99	.1	71	26	333	9.47	347	5	ND	1	4	1	2	2	198	.07	.049	3	63	.15	99	.01	12	2.33	.02	.04	1	1
LSB6 L15M 2+00E	1	42	5	107	.2	39	19	1049	5.47	5	5	ND	1	13	1	2	2	150	.38	.079	6	54	.52	76	.29	4	3.99	.04	.03	1	1
LSB6 L15M 2+50E	1	11	24	110	.3	13	24	5928	4.86	2	5	ND	1	46	1	2	2	107	1.30	.112	5	17	.57	139	.14	2	1.60	.05	.08	1	1
LSB6 L15M 3+00E	1	10	9	61	.1	9	9	1368	5.72	5	5	ND	1	39	1	2	2	194	.47	.109	5	26	.48	48	.23	2	1.94	.04	.04	1	2
LSB6 L15M 3+50E	1	10	6	117	.2	20	8	1669	2.41	19	5	ND	1	16	1	2	2	45	.55	.084	12	24	.72	87	.01	5	1.96	.03	.07	1	1
STD CAU-5	20	59	39	136	7.2	70	28	1012	3.96	39	18	7	34	48	18	16	20	64	.48	.104	36	57	.88	179	.08	35	1.72	.09	.14	12	48

ASHWORTH EXPLORATION PROJECT - LACY STORES FILE # 86-4052

PAGE 4

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Pi	V	Ca	F	La	Cr	Mo	Ba	Ti	R	Al	Na	I	W	Au1
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	I	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	I	PPH	I	I	I	PPH	PPB
LSB6 L15M 4+00E	1	67	8	77	.3	43	14	393	4.61	7	5	ND	2	11	1	2	2	125	.33	.042	3	56	.71	90	.22	2	3.33	.04	.02	1	27
LSB6 L15M 4+50E	1	8	10	62	.1	10	10	1282	3.43	3	5	ND	1	10	1	2	2	105	.25	.073	4	17	.33	65	.06	2	1.15	.02	.04	1	1
LSB6 L15M 5+00E	1	9	8	68	.2	9	15	1945	3.59	3	5	ND	1	26	1	2	2	107	.32	.041	4	17	.27	58	.19	2	1.47	.03	.02	1	1
LSB6 L15M 5+50E	1	25	4	60	.2	15	11	587	3.46	4	5	ND	1	24	1	2	2	108	.30	.048	3	37	.48	56	.13	2	1.96	.03	.02	1	2
LSB6 L15M 6+00E	1	97	9	81	.1	16	19	1284	6.62	4	7	ND	2	10	1	2	2	160	.14	.092	7	31	1.64	81	.01	2	3.55	.03	.04	1	7
LSB6 L15M 6+50E	1	48	8	93	.2	29	15	351	5.48	6	5	ND	1	10	1	2	2	158	.28	.051	4	44	.35	76	.24	2	3.05	.03	.02	1	1
LSB6 L15M 7+00E	1	51	14	80	.2	24	13	995	4.38	4	5	ND	2	17	1	2	2	110	.51	.058	5	41	.50	108	.16	4	2.66	.04	.03	1	1
LSB6 L15M 7+50E	1	48	23	71	.1	17	10	3962	4.15	6	5	ND	1	18	1	2	2	118	.34	.066	5	33	.44	170	.13	2	2.49	.03	.04	1	1
LSB6 L15M 8+00E	1	37	8	53	.1	14	9	331	4.16	2	5	ND	1	12	1	2	2	123	.26	.032	4	38	.33	48	.16	2	2.03	.03	.02	1	1
LSB6 L15M 8+50E	1	7	11	30	.2	6	1	135	.91	3	5	ND	1	27	1	2	2	56	.48	.036	2	17	.14	27	.12	3	.63	.03	.02	1	9
LSB6 L15M 9+00E	1	14	9	76	.1	5	10	1203	2.81	3	5	ND	1	27	1	2	2	117	.53	.052	3	20	.37	56	.09	2	1.65	.03	.03	1	1
LSB6 L15M 9+50E	1	16	5	40	.1	9	8	250	4.02	4	5	ND	1	15	1	2	2	116	.29	.024	4	28	.40	38	.09	2	1.57	.03	.02	1	2
LSB6 L15M 10+00E	1	28	7	40	.2	9	5	291	2.74	4	5	ND	1	15	1	2	2	87	.47	.039	7	30	.18	64	.09	3	1.41	.03	.03	1	1
LSB6 L15M 10+50E	1	38	12	91	.2	20	13	985	4.54	5	5	ND	1	11	1	2	2	117	.25	.041	5	39	.32	118	.15	2	2.62	.03	.02	1	1
LSB6 L15M 11+00E	1	16	7	70	.1	8	7	441	4.20	6	5	ND	1	31	1	2	2	123	.28	.049	5	20	.36	58	.12	2	2.35	.03	.03	1	1
LSB6 L15M 11+50E	1	6	6	22	.1	5	3	289	2.32	2	5	ND	1	16	1	2	2	94	.24	.021	4	18	.14	35	.12	2	.83	.02	.01	1	1
LSB6 L15M 12+00E	1	76	8	55	.1	26	17	187	6.63	8	5	ND	1	11	1	2	3	180	.18	.028	4	54	.46	66	.08	3	3.92	.03	.02	1	1
LSB6 L15M 12+50E	1	77	6	69	.1	31	23	1782	4.02	3	5	ND	1	15	1	2	2	100	.33	.088	6	43	.49	80	.13	2	3.34	.03	.03	1	1
LSB6 L15M 13+00E	1	26	10	58	.2	10	15	598	5.03	2	5	ND	1	26	1	2	2	150	.42	.127	4	32	.51	37	.18	2	2.27	.03	.02	1	1
LSB6 L15M 13+50E	1	31	5	47	.1	21	10	272	4.50	7	3	ND	1	15	1	2	3	120	.33	.036	4	45	.49	49	.16	2	2.51	.03	.02	1	1
LSB6 L15M 14+00E	1	62	5	87	.3	40	14	896	4.75	11	5	ND	2	16	1	2	2	116	.45	.040	7	57	.88	114	.15	2	2.91	.04	.03	1	1
LSB6 L15M 14+50E	1	32	5	114	.3	22	12	352	4.60	7	5	ND	2	10	1	2	2	101	.17	.079	5	44	.51	37	.11	2	3.39	.03	.01	1	1
LSB6 L15M 15+00E	1	11	6	41	.1	10	4	502	1.93	5	5	ND	1	12	1	2	2	64	.21	.076	3	20	.16	47	.08	2	1.04	.02	.02	1	1
LSB6 L15M 15+50E	1	61	7	98	.2	47	14	377	4.43	8	5	ND	2	11	1	2	2	105	.29	.040	4	50	.78	68	.16	3	3.01	.04	.03	1	2
LSB6 L15M 16+00E	3	49	12	167	.7	41	13	402	5.97	19	5	ND	2	12	1	7	2	120	.24	.094	6	56	.49	63	.13	2	2.74	.03	.05	1	1
LSB6 L15M 16+50E	1	19	10	83	.2	33	18	863	5.85	2	5	ND	1	36	1	2	2	167	.94	.061	4	83	1.17	65	.32	4	2.55	.06	.04	1	2
LSB6 L15M 17+00E	1	95	9	118	.1	10	22	2460	4.77	4	5	ND	2	15	1	2	2	149	.34	.062	7	19	1.35	207	.01	2	3.25	.04	.09	1	2
LSB6 L15M 17+50E	1	39	8	65	.2	23	11	702	4.11	5	5	ND	2	13	1	2	2	114	.32	.039	5	39	.50	74	.16	2	2.44	.03	.03	1	1
LSB6 L15M 18+00E	1	26	14	104	.1	20	17	9150	4.85	2	5	ND	1	42	1	2	2	180	.78	.039	3	34	1.06	136	.22	4	1.76	.05	.03	1	1
LSB6 L15M 18+50E	1	21	11	66	.1	3	1	492	.89	2	5	ND	1	122	1	2	2	56	.65	.021	4	10	.06	34	.13	3	.86	.03	.01	1	4
LSB6 L15M 19+00E	1	5	8	21	.1	1	2	112	.96	2	5	ND	1	56	1	2	2	33	.29	.005	3	3	.15	31	.01	2	.94	.02	.01	1	2
LSB6 L15M 19+50E	1	3	6	19	.1	1	1	60	.46	2	5	ND	1	47	1	2	2	19	.23	.018	2	6	.02	36	.03	2	.48	.02	.02	1	1
LSB6 L15M 20+00E	1	66	5	69	.3	29	11	288	4.35	2	5	ND	2	12	1	2	2	122	.28	.048	4	46	.64	63	.20	2	3.33	.04	.04	1	1
LSB6 L15M 20+50E	1	38	6	49	.2	14	5	245	4.89	4	5	ND	2	11	1	2	3	147	.22	.051	3	44	.31	25	.20	2	2.78	.03	.02	1	1
LSB6 L15M 21+00E	1	20	12	49	.1	11	5	345	4.45	8	5	ND	1	16	1	2	2	129	.30	.122	4	39	.37	41	.16	2	2.08	.03	.04	1	1
LSB6 L15M 21+50E	1	6	8	25	.2	5	3	592	2.68	2	5	ND	1	15	1	2	3	85	.24	.029	5	21	.19	28	.11	2	1.28	.02	.01	1	1
STD C/AU-S	21	59	41	136	7.3	70	28	1012	3.96	37	17	7	34	48	18	16	20	64	.48	.105	36	58	.88	178	.08	34	1.72	.09	.13	13	47

ASHWORTH EXPLORATION PROJECT - LACY STONES FILE # 86-4052

PAGE 5

SAMPLE#	Hc PPH	Cu PPH	Pb PPH	Zn PPH	As PPH	Ni PPH	Co PPH	Mn PPH	Fe %	As PPH	U PPH	Au PPH	Th PPH	Sr PPH	Cd PPH	Sb PPH	Bi PPH	V PPH	Ca %	F %	La PPH	Cr PPH	Mo %	Ba PPH	Ti %	F PPH	Al %	Na %	K %	Aut PPH	Aut PPD
LS86 L15N 22+00E	1	41	14	109	.2	29	65	4936	4.19	4	5	ND	1	19	1	2	2	101	.34	.095	30	34	.33	131	.19	3	3.88	.04	.05	1	1
LS86 L15N 22+50E	1	7	13	31	.1	8	6	718	1.17	5	5	ND	1	14	1	2	2	34	.21	.013	8	14	.14	154	.06	3	1.39	.02	.99	2	270
LS86 L15N 23+00E	1	46	14	77	.1	27	12	542	4.18	5	5	ND	2	16	1	2	2	105	.34	.058	4	39	.54	49	.22	2	3.27	.03	.02	1	1
LS86 L15N 23+50E	1	58	9	61	.2	22	11	521	4.18	3	6	ND	2	18	1	2	2	117	.47	.051	5	40	.61	62	.21	2	2.34	.04	.04	1	1
LS86 L15N 24+00E	1	6	4	26	.1	14	3	78	2.64	2	5	ND	1	15	1	4	2	83	.19	.017	3	28	.17	30	.03	2	1.10	.02	.02	2	7
LS86 L15N 24+50E	1	39	10	87	.3	21	9	964	4.13	7	5	ND	2	21	1	2	3	107	.29	.111	4	43	.40	31	.21	2	2.80	.03	.02	1	1
LS86 L15N 25+00E	1	15	6	36	.2	14	5	218	2.09	2	5	ND	1	14	1	2	2	54	.19	.025	4	20	.16	47	.07	4	.95	.02	.03	2	1
LS86 L12N 0+00	1	55	5	61	.2	31	12	672	4.28	2	8	ND	2	14	1	2	2	129	.40	.038	5	60	.62	84	.29	2	2.83	.04	.02	2	1
LS86 L12N 0+50E	1	4	3	95	.1	10	3	386	1.05	4	5	ND	1	6	1	2	2	35	.16	.029	2	15	.12	38	.05	4	1.03	.01	.01	1	1
LS86 L12N 1+00E	1	27	5	93	.1	22	10	389	4.18	2	5	ND	1	19	1	2	2	116	.43	.057	6	36	.38	92	.28	2	2.39	.04	.03	2	4
LS86 L12N 1+50E	2	22	8	113	.1	16	15	2307	5.91	10	5	ND	2	25	1	2	2	134	.54	.178	5	31	.58	77	.21	2	2.27	.04	.03	1	1
LS86 L12N 2+00E	1	9	12	143	.1	11	4	1074	2.94	12	5	ND	1	4	1	4	2	27	.16	.098	19	16	.13	49	.01	3	1.03	.02	.05	1	1
LS86 L12N 2+50E	12	25	11	132	.1	43	11	248	3.95	25	5	ND	1	4	1	7	3	41	.11	.042	2	16	.10	27	.01	2	1.73	.02	.02	1	1
LS86 L12N 3+00E	1	25	7	136	.2	20	8	248	4.14	6	5	ND	2	10	1	2	2	94	.34	.166	4	37	.27	49	.11	2	2.47	.03	.03	1	1
LS86 L12N 3+50E	1	55	5	68	.2	34	13	240	4.72	5	5	ND	2	13	1	2	2	132	.34	.033	6	51	.55	74	.24	2	3.50	.04	.03	1	1
LS86 L12N 4+00E	1	85	3	53	.2	29	12	448	4.29	2	5	ND	2	14	1	2	2	116	.51	.024	4	49	.56	98	.23	3	2.67	.04	.03	1	1
LS86 L12N 4+50E	1	63	7	100	.3	24	13	999	5.33	5	5	ND	2	12	1	2	2	120	.30	.116	5	47	.67	126	.13	2	3.50	.04	.05	1	1
LS86 L12N 5+00E	1	55	15	149	.1	18	17	2156	6.33	7	5	ND	2	13	1	4	2	132	.30	.081	8	27	1.00	168	.08	2	3.75	.04	.06	1	40
LS86 L12N 5+50E	1	36	6	79	.1	8	11	892	3.81	2	5	ND	2	21	1	2	2	97	.18	.054	5	16	.59	120	.03	2	2.77	.03	.07	1	5
LS86 L12N 6+00E	1	80	17	82	.1	27	14	694	5.17	7	5	ND	2	12	1	2	2	123	.31	.037	7	42	.61	108	.16	2	2.92	.04	.03	1	1
LS86 L12N 6+50E	1	124	15	111	.2	31	23	1961	6.42	20	5	ND	2	12	1	8	2	108	.33	.060	11	40	.45	132	.07	3	2.61	.04	.04	1	1
LS86 L12N 7+00E	2	84	8	71	.2	31	17	1177	5.60	14	5	ND	2	16	1	2	2	124	.49	.035	11	57	.53	157	.19	2	3.95	.05	.04	1	1
LS86 L12N 7+50E	3	98	15	81	.2	22	23	2872	6.70	2	5	ND	2	18	1	2	2	137	.55	.060	10	56	.50	202	.08	2	4.60	.05	.05	1	1
LS86 L12N 8+00E	1	110	9	87	.3	29	14	1013	5.71	9	5	ND	2	14	1	2	2	140	.33	.189	6	58	.88	68	.16	2	4.05	.04	.04	1	1
LS86 L12N 8+50E	1	73	11	76	.1	29	13	521	5.30	5	5	ND	2	16	1	2	2	141	.32	.055	6	50	.65	73	.19	2	3.62	.04	.03	1	1
LS86 L12N 9+00E	1	54	7	56	.2	21	10	440	4.74	7	5	ND	2	22	1	2	2	133	.50	.054	5	42	.52	112	.19	2	2.88	.04	.03	1	1
LS86 L12N 9+50E	1	52	12	96	.2	27	15	885	5.54	2	5	ND	2	16	1	2	2	132	.42	.040	7	48	.53	100	.17	2	3.59	.04	.04	1	1
LS86 L12N 10+00E	1	51	11	67	.2	27	13	747	5.16	2	5	ND	2	19	1	2	2	129	.42	.039	8	43	.48	102	.20	2	3.07	.04	.03	2	1
LS86 L12N 10+50E	1	49	8	60	.3	21	15	1249	4.43	2	5	ND	2	20	1	2	2	111	.55	.034	9	32	.39	113	.16	2	2.65	.04	.03	1	1
LS86 L12N 11+00E	1	11	2	25	.1	9	3	102	3.13	3	5	ND	1	17	1	2	2	106	.20	.008	4	45	.19	22	.14	2	1.40	.03	.01	2	1
LS86 L12N 11+50E	1	102	6	60	.1	32	12	488	4.52	9	5	ND	3	12	1	2	2	125	.29	.053	4	50	.70	41	.23	2	4.27	.04	.04	3	2
LS86 L12N 12+00E	3	91	13	78	.1	8	10	409	6.37	7	5	ND	2	7	1	2	2	91	.09	.100	12	20	.63	75	.01	2	3.12	.03	.09	1	1
LS86 L12N 12+50E	1	51	10	56	.1	13	6	311	5.60	2	5	ND	2	21	1	2	2	147	.26	.096	4	43	.39	30	.21	2	3.14	.03	.03	1	1
LS86 L12N 13+00E	1	65	7	73	.2	19	12	822	5.59	2	5	ND	2	23	1	2	2	172	.37	.143	5	49	.79	75	.32	2	3.59	.05	.06	1	1
LS86 L12N 13+50E	1	113	7	97	.3	36	15	716	4.45	3	5	ND	2	14	1	2	2	116	.32	.096	4	53	.76	73	.21	2	4.33	.04	.04	1	1
LS86 L12N 14+00E	1	49	6	116	.2	29	13	887	3.93	5	5	ND	2	12	1	2	2	93	.29	.112	4	36	.38	52	.19	2	2.89	.03	.03	1	1
STD C/AU-S	21	59	38	131	6.8	65	27	972	3.94	38	18	7	32	46	17	15	17	61	.48	.100	34	57	.88	173	.08	35	1.71	.09	.12	12	47

ASHWORTH EXPLORATION PROJECT - LACY STORES FILE # B6-4052

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mp	Ba	Ti	F	Al	Na	I	M	Au1
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	I	%	PPH	PPH	I	PPH	I	PPH	I	I	I	PPH	PPB
LSB6 L12N 14+50E	2	154	18	564	.8	22	16	1237	5.36	21	5	ND	1	14	1	2	2	128	.39	.076	7	46	.55	89	.17	4	3.09	.04	.03	1	16
LSB6 L12N 15+00E	1	92	8	118	.4	29	17	514	5.44	8	5	ND	2	26	1	2	2	143	.33	.049	12	60	1.07	136	.13	4	3.86	.04	.04	1	1
LSB6 L12N 15+50E	1	129	10	115	.5	38	30	1876	6.13	12	5	ND	2	30	1	2	2	167	.34	.067	7	106	2.29	180	.03	5	4.10	.04	.06	1	19
LSB6 L12N 16+00E	1	72	3	73	.2	28	11	284	5.21	11	5	ND	2	12	1	2	2	128	.27	.088	7	59	.61	44	.25	3	4.03	.04	.05	1	1
LSB6 L12N 16+50E	1	14	7	43	.1	7	4	612	2.58	2	5	ND	1	34	1	2	2	93	.38	.031	3	21	.26	20	.18	2	1.49	.03	.02	1	1
LSB6 L12N 17+00E	1	8	6	48	.1	7	6	434	2.16	2	5	ND	1	16	1	2	2	88	.13	.026	3	23	.37	25	.03	2	1.59	.02	.02	1	1
LSB6 L12N 17+50E	1	164	12	74	1.1	39	16	300	4.31	8	5	ND	3	24	1	2	2	105	.55	.049	21	75	.49	406	.19	5	6.34	.05	.03	1	1
LSB6 L12N 18+00E	1	52	9	86	.2	25	10	287	5.06	7	5	ND	2	14	1	2	2	137	.29	.052	4	49	.51	87	.21	3	3.59	.04	.04	1	2
LSB6 L12N 18+50E	1	61	17	59	.2	14	7	244	3.61	4	5	ND	1	39	1	2	2	109	.37	.038	4	25	.46	50	.13	2	2.89	.03	.03	1	3
LSB6 L12N 19+00E	1	70	14	88	.1	25	9	279	5.15	5	5	ND	2	12	1	2	2	135	.24	.084	3	51	.49	41	.20	2	4.61	.03	.03	1	1
LSB6 L12N 19+50E	1	7	4	36	.2	4	6	356	1.37	2	5	ND	1	16	1	2	2	50	.27	.021	4	16	.13	35	.17	2	.94	.02	.01	1	1
LSB6 L12N 20+00E	1	42	8	108	.3	20	15	1191	4.21	2	5	ND	1	13	1	2	2	108	.27	.094	7	35	.55	72	.13	2	3.06	.03	.03	1	1
LSB6 L12N 20+50E	1	51	11	61	.1	15	7	264	4.89	4	5	ND	1	19	1	2	2	138	.29	.065	4	40	.43	44	.19	2	2.85	.03	.02	1	1
LSB6 L12N 21+00E	1	33	9	81	.1	17	14	1232	4.15	4	5	ND	1	35	1	2	2	137	.40	.051	4	39	1.18	108	.19	2	2.73	.04	.03	1	1
LSB6 L12N 21+50E	1	20	7	47	.1	8	5	250	2.43	2	5	ND	1	30	1	2	2	88	.35	.028	4	20	.42	29	.15	2	1.54	.03	.02	1	1
LSB6 L12N 22+00E	1	27	9	80	.1	14	7	212	4.55	4	5	ND	1	17	1	2	2	136	.34	.046	4	32	.45	56	.19	2	2.53	.03	.02	1	1
LSB6 L12N 22+50E	1	15	10	54	.1	9	4	127	4.67	6	5	ND	1	20	1	2	2	136	.30	.074	3	37	.28	20	.26	3	1.40	.03	.02	1	1
LSB6 L12N 23+00E	1	44	9	57	.8	21	9	489	3.41	5	5	ND	2	16	1	2	2	96	.27	.052	4	36	.41	27	.20	3	2.79	.03	.02	1	1
LSB6 L12N 23+50E	1	7	4	38	.3	39	8	207	1.99	2	5	ND	1	30	1	2	2	89	.41	.029	3	58	.58	20	.55	2	1.16	.03	.02	1	1
LSB6 L12N 24+00E	1	33	7	70	.1	19	8	256	4.48	2	5	ND	1	21	1	2	2	119	.27	.057	5	43	.34	62	.16	2	2.48	.03	.02	1	4
LSB6 L12N 24+50E	1	4	4	20	.1	2	1	60	.99	2	5	ND	1	11	1	2	2	48	.13	.014	13	18	.04	19	.07	2	.61	.01	.02	1	7
LSB6 L12N 25+00E	1	24	8	53	.1	22	8	393	3.61	2	5	ND	1	35	1	2	2	108	.41	.087	6	59	.43	41	.26	2	1.96	.03	.02	1	2
LSB6 L9N 4+50E	1	50	7	68	.1	23	13	261	6.12	11	5	ND	2	7	1	2	2	128	.12	.029	6	49	.24	94	.01	2	2.44	.02	.02	1	13
LSB6 L9N 5+00E	1	25	6	63	.1	25	12	426	5.08	3	5	ND	1	14	1	2	2	131	.34	.025	6	46	.64	115	.07	3	2.95	.04	.03	1	2
LSB6 L9N 5+50E	1	87	12	79	.2	32	14	557	5.59	8	5	ND	2	12	1	2	2	141	.31	.066	7	50	.54	83	.17	2	3.54	.04	.03	1	230
LSB6 L9N 6+00E	1	62	11	75	.2	42	16	436	5.50	6	5	ND	2	14	1	2	2	123	.36	.059	7	58	.66	81	.20	4	4.02	.04	.03	1	22
LSB6 L9N 6+50E	1	50	11	73	.4	29	16	603	5.74	4	5	ND	2	18	1	2	2	156	.51	.046	10	57	.51	97	.20	4	3.71	.05	.04	1	4
LSB6 L9N 7+00E	1	54	7	106	.1	30	14	1153	4.88	7	5	ND	1	13	1	2	2	122	.36	.090	6	46	.59	113	.21	3	3.34	.04	.04	1	2
LSB6 L9N 7+50E	1	41	21	107	.1	11	24	489	4.77	6	5	ND	1	15	1	2	2	100	.26	.055	8	24	.58	323	.03	2	2.68	.04	.05	1	1
LSB6 L9N 8+00E	1	72	14	71	.1	40	16	793	6.40	5	5	ND	2	15	1	2	2	165	.29	.063	7	98	.90	107	.14	4	3.73	.04	.04	1	1
LSB6 L9N 8+50E	1	81	9	76	.2	32	13	847	5.30	2	5	ND	2	13	1	2	2	143	.36	.078	5	59	.57	78	.24	5	3.91	.04	.04	1	1
LSB6 L9N 9+00E	1	42	9	97	.1	22	13	845	4.27	6	5	ND	1	13	1	2	2	114	.29	.083	4	43	.42	61	.17	2	3.03	.03	.02	1	1
LSB6 L9N 9+50E	1	45	11	109	.1	21	14	633	4.55	3	5	ND	1	15	1	2	2	120	.35	.138	4	39	.48	70	.18	2	2.62	.04	.03	1	5
LSB6 L9N 10+00E	1	46	11	72	.1	19	11	621	5.53	2	5	ND	1	24	1	2	2	170	.35	.040	4	50	.43	73	.23	2	2.71	.04	.02	1	2
LSB6 L9N 10+50E	1	44	5	64	.3	25	12	833	4.84	2	5	ND	1	16	1	2	2	134	.50	.037	5	46	.50	60	.24	3	2.44	.04	.02	1	4
LSB6 L9N 11+00E	1	48	8	56	.1	22	11	242	5.18	6	5	ND	1	14	1	2	2	134	.37	.029	4	41	.54	61	.22	3	2.83	.04	.03	1	1
STD C/AU-S	22	59	37	135	7.1	68	28	1012	3.96	39	18	7	34	48	18	16	19	63	.48	.105	36	57	.88	179	.08	33	1.72	.09	.13	13	50

ASHWORTH EXPLORATION PROJECT - LACY STONES FILE # 86-4052

PAGE 7

SAMPLE#	Mc	Cu	Pb	Zn	Ag	Ni	Cc	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mo	Ba	Ti	B	Al	Na	K	W	Au1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
LS86 L9N 11+50E	2	39	8	81	.1	26	10	429	3.70	4	5	ND	2	11	1	2	2	103	.27	.048	5	40	.63	45	.16	3	2.92	.03	.02	1	4
LS86 L9N 12+00E	1	35	4	68	.1	21	7	188	3.38	4	5	ND	1	11	1	2	2	97	.26	.043	5	32	.46	37	.15	4	2.49	.03	.02	1	5
LS86 L9N 12+50E	2	56	8	106	.2	35	14	308	5.01	11	5	ND	2	11	1	2	2	143	.28	.047	4	57	.48	64	.23	2	3.48	.03	.02	1	2
LS86 L9N 13+00E	2	53	6	66	.1	22	9	237	4.05	4	5	ND	1	13	1	2	2	122	.33	.031	3	37	.41	52	.22	2	2.58	.03	.02	1	5
LS86 L9N 13+50E	2	69	11	273	.4	27	16	4142	3.78	7	5	ND	2	20	1	2	2	103	.43	.051	12	37	.47	122	.20	3	3.20	.04	.04	1	6
LS86 L9N 14+00E	1	65	8	84	.1	4	15	1464	4.20	6	5	ND	2	6	1	2	3	108	.09	.044	10	2	.30	111	.01	2	2.85	.02	.09	1	1
LS86 L9N 14+50E	1	32	11	100	.2	17	10	398	3.49	5	5	ND	1	14	1	2	2	104	.27	.047	4	36	.36	54	.22	2	3.02	.03	.02	1	3
LS86 L9N 15+00E	2	30	11	59	.1	8	11	1751	3.46	2	5	ND	1	17	1	2	3	101	.41	.023	5	21	.32	99	.09	2	1.86	.03	.04	1	1
LS86 L9N 15+50E	1	27	3	39	.1	11	6	270	3.67	5	5	ND	1	18	1	2	2	125	.24	.020	4	30	.22	39	.16	2	2.23	.03	.02	1	2
LS86 L9N 16+00E	2	28	10	70	.1	15	7	202	4.03	8	5	ND	1	17	1	2	2	132	.25	.020	3	30	.31	94	.13	2	2.30	.03	.02	1	1
LS86 L9N 16+50E	1	29	7	63	.1	12	6	203	3.52	2	5	ND	1	17	1	2	2	102	.26	.038	4	30	.29	42	.17	2	2.65	.03	.03	1	2
LS86 L9N 17+00E	1	33	11	52	.1	6	3	193	3.85	2	5	ND	1	54	1	2	2	110	.39	.062	4	22	.19	32	.12	2	2.58	.03	.02	1	4
LS86 L9N 17+50E	1	91	3	70	.1	21	8	255	5.33	9	5	ND	2	15	1	2	2	143	.25	.079	4	57	.48	34	.24	2	4.81	.04	.03	1	3
LS86 L9N 18+00E	2	70	7	96	.1	17	8	475	4.90	12	5	ND	2	20	1	2	2	130	.29	.105	3	43	.48	61	.20	2	3.95	.04	.04	1	1
LS86 L9N 18+50E	1	15	15	58	.1	7	7	446	3.38	4	5	ND	1	19	1	2	5	88	.32	.032	5	19	.23	53	.11	2	1.53	.03	.03	1	1
LS86 L9N 19+00E	1	19	6	80	.1	9	6	397	3.96	3	5	ND	1	18	1	2	3	102	.31	.070	5	24	.24	51	.12	2	1.96	.03	.03	1	2
LS86 L9N 19+50E	1	46	15	71	.1	14	15	1940	4.64	2	5	ND	1	21	1	2	2	119	.37	.052	6	35	.49	172	.14	2	2.45	.04	.04	1	4
LS86 L9N 20+00E	1	37	7	76	.2	18	10	923	4.30	7	5	ND	1	21	1	2	3	117	.46	.055	5	34	.39	93	.18	2	2.16	.04	.02	1	1
LS86 L9N 20+50E	1	33	9	56	.1	12	5	191	3.52	6	5	ND	1	24	1	2	2	136	.48	.037	4	32	.30	98	.24	2	1.39	.04	.03	1	1
LS86 L9N 21+00E	1	7	4	38	.1	4	3	219	1.68	2	5	ND	2	21	1	2	2	53	.21	.034	5	14	.25	31	.03	3	1.81	.02	.03	1	1
LS86 L9N 21+50E	2	40	8	74	.1	115	23	343	5.80	9	5	ND	1	15	1	3	2	208	.18	.038	6	303	2.70	51	.02	2	3.13	.04	.03	1	1
LS86 L9N 22+00E	1	54	6	57	.2	26	10	230	4.38	3	5	ND	1	22	1	2	2	125	.36	.039	5	43	.56	51	.18	2	2.46	.04	.03	1	4
LS86 L9N 22+50E	1	46	6	135	.1	51	15	376	4.98	2	5	ND	1	18	1	2	2	120	.52	.058	6	53	.56	116	.19	2	3.31	.05	.03	1	1
LS86 L9N 23+00E	1	69	5	85	.1	40	16	436	4.45	2	5	ND	2	16	1	2	4	121	.30	.080	5	50	.49	66	.23	3	3.77	.04	.03	1	2
LS86 L9N 23+50E	1	11	6	35	.2	16	5	252	2.38	2	5	ND	1	55	1	2	2	87	.56	.042	6	47	.42	24	.18	3	1.67	.03	.03	1	1
LS86 L9N 23+75E	1	9	10	42	.1	9	4	269	3.79	2	5	ND	2	25	1	2	3	118	.30	.051	5	39	.18	27	.20	2	1.35	.03	.02	2	5
LS86 L9N 24+00E	1	62	11	70	.2	36	14	252	5.23	8	5	ND	2	16	1	2	2	135	.28	.080	4	62	.58	46	.26	2	3.63	.04	.03	1	1
LS86 L9N 24+25E	1	21	10	55	.2	16	6	179	4.57	2	5	ND	2	18	1	2	2	128	.28	.082	5	40	.33	36	.18	2	2.06	.03	.03	1	1
LS86 L9N 24+50E	1	11	9	43	.1	12	4	124	3.43	2	5	ND	1	26	1	2	2	106	.32	.040	5	36	.28	61	.12	2	1.47	.03	.03	1	1
LS86 L9N 24+75E	1	32	15	78	.1	36	9	234	5.17	3	5	ND	2	27	1	2	2	192	.38	.055	6	96	.84	68	.32	2	2.13	.04	.04	1	1
LS86 L6N 0+00	3	6	12	261	.3	17	7	3580	.95	10	5	ND	1	14	2	2	2	16	1.44	.150	9	11	.44	115	.02	7	.79	.04	.05	1	6
LS86 L6N 0+50E	1	25	7	100	.1	24	10	663	2.98	8	5	ND	1	14	1	2	3	88	.38	.077	4	34	.35	58	.17	3	2.24	.03	.03	1	1
LS86 L6N 1+00E	1	19	7	104	.1	34	12	758	2.66	19	5	ND	1	9	1	2	4	66	.24	.056	4	28	.23	69	.07	3	2.09	.02	.04	1	2
LS86 L6N 1+50E	1	39	7	56	.1	23	9	356	3.39	23	5	ND	1	10	1	3	2	68	.19	.043	6	23	.16	46	.04	3	1.28	.02	.03	1	1
LS86 L6N 2+00E	1	9	13	131	.4	21	7	1596	3.01	8	5	ND	2	5	1	2	2	42	.17	.094	15	30	.14	107	.01	3	1.49	.02	.04	1	3
LS86 L6N 2+50E	1	94	4	78	.3	37	16	700	4.55	14	5	ND	2	21	1	2	2	117	.74	.048	10	47	.75	111	.20	3	3.04	.05	.04	1	8
STD C/AU-S	21	60	40	139	7.3	70	29	1029	3.96	39	19	8	34	49	18	16	21	65	.48	.105	36	60	.88	183	.08	34	1.72	.09	.13	13	52

ASHWORTH EXPLORATION PROJECT - LACY STONES FILE # B6-4052

PAGE 8

SAMPLE#	Mc PPH	Cu PPH	Pb PPH	Zn PPH	Ag PPH	Ni PPH	Co PPH	Mn PPH	Fe %	As PPH	U PPH	Au PPH	Th PPH	Sr PPH	Cd PPH	Sb PPH	Bi PPH	V PPH	Ca %	P %	La PPH	Cr PPH	Mo %	Ba PPH	Ti %	F PPH	Al %	Na %	K %	W PPH	Au# PPB
LSB6 L&N 3+00E	1	27	13	62	.1	29	14	1208	3.29	4	5	ND	1	26	1	2	2	96	.73	.046	3	85	.91	78	.19	2	1.69	.04	.03	1	23
LSB6 L&N 3+50E	1	5	10	23	.1	3	2	231	1.46	2	5	ND	1	45	1	2	2	65	.42	.015	3	11	.12	29	.13	2	.88	.02	.02	1	28
LSB6 L&N 4+00E	1	40	10	97	.2	30	13	1176	4.07	4	5	ND	1	16	1	2	2	106	.34	.057	4	61	.52	88	.19	2	2.55	.03	.04	1	14
LSB6 L&N 4+50E	1	68	9	62	.2	39	14	325	4.69	9	5	ND	2	12	1	2	2	136	.32	.018	6	55	.79	119	.17	2	3.53	.04	.03	2	4
LSB6 L&N 5+00E	1	21	12	87	.2	21	12	2661	3.92	4	5	ND	1	21	1	2	2	100	.39	.082	3	70	.43	101	.18	2	2.04	.03	.02	1	2
LSB6 L&N 5+50E	2	82	14	81	.3	57	19	552	5.86	39	5	ND	2	17	1	10	2	130	.43	.036	9	69	.65	145	.12	2	3.16	.04	.07	1	1
LSB6 L&N 6+00E	1	85	17	97	.2	36	16	1156	5.95	12	5	ND	2	12	1	2	2	141	.30	.065	9	52	.76	121	.15	2	3.42	.04	.05	1	1
LSB6 L&N 6+50E	1	52	10	78	.1	29	13	918	4.35	7	5	ND	2	13	1	2	2	124	.33	.048	5	47	.50	87	.20	2	2.76	.04	.04	1	2
LSB6 L&N 7+00E	3	68	18	143	.6	29	16	10417	4.83	6	5	ND	2	29	1	2	2	98	.82	.103	23	41	.44	249	.15	2	3.64	.05	.05	1	1
LSB6 L&N 7+50E	1	77	17	92	.2	13	17	4879	5.75	8	5	ND	1	29	1	2	2	147	.50	.087	7	22	1.12	290	.09	2	3.58	.04	.06	1	1
LSB6 L&N 8+00E	1	37	11	84	.1	6	14	2532	5.20	5	5	ND	1	8	1	2	2	105	.16	.081	4	15	.59	75	.01	2	2.22	.03	.05	2	83
LSB6 L&N 8+50E	3	55	16	118	.4	28	22	9080	4.43	4	9	ND	3	17	1	3	2	105	.45	.092	14	40	.35	189	.19	2	3.41	.04	.04	1	31
LSB6 L&N 9+00E	1	65	14	114	.2	22	13	859	4.84	8	5	ND	2	15	1	2	2	115	.32	.158	5	37	.49	92	.15	2	3.45	.03	.06	1	10
LSB6 L&N 9+50E	2	80	13	79	.1	17	9	532	7.43	15	5	ND	2	11	1	2	3	179	.43	.188	3	53	.65	47	.17	2	5.07	.04	.02	1	4
LSB6 L&N 10+00E	1	5	10	19	.1	2	1	105	1.49	4	5	ND	1	26	1	3	2	78	.34	.027	3	26	.09	16	.17	4	.59	.02	.02	1	2
LSB6 L&N 10+50E	1	4	8	21	.1	4	3	157	1.32	2	5	ND	1	117	1	2	2	118	1.23	.018	3	19	.33	16	.11	3	1.40	.03	.03	2	3
LSB6 L&N 11+00E	1	15	7	28	.1	7	4	138	3.58	5	5	ND	1	19	1	2	2	125	.23	.014	3	25	.38	35	.11	2	1.76	.03	.03	2	3
LSB6 L&N 11+50E	1	8	6	31	.1	10	3	107	2.35	7	5	ND	1	10	1	2	3	71	.15	.018	3	21	.22	22	.05	2	1.17	.02	.02	2	1
LSB6 L&N 12+00E	2	43	11	78	.3	30	11	629	3.70	17	5	ND	2	15	1	3	3	98	.28	.049	5	43	.48	58	.12	2	2.72	.03	.03	1	1
LSB6 L&N 12+50E	1	53	7	65	.1	19	9	681	4.21	7	5	ND	1	26	1	2	2	115	.37	.124	3	50	.48	38	.16	2	3.15	.03	.04	1	1
LSB6 L&N 13+00E	1	66	11	133	.1	25	23	1139	4.43	11	5	ND	2	19	1	2	2	130	.32	.076	4	48	.81	58	.19	2	2.87	.04	.05	1	4
LSB6 L&N 13+50E	1	72	11	84	.1	4	12	1560	5.80	6	5	ND	1	9	1	2	2	175	.13	.069	4	14	.43	45	.05	2	2.99	.03	.06	1	3
LSB6 L&N 14+00E	1	81	11	75	.2	32	15	258	4.89	2	5	ND	2	14	1	2	2	133	.29	.063	4	57	.55	41	.25	2	3.72	.04	.03	1	1
LSB6 L&N 14+50E	1	2	6	14	.1	2	1	152	.70	2	5	ND	1	34	1	2	2	60	.61	.013	3	3	.20	11	.18	4	.86	.03	.01	2	1
LSB6 L&N 15+00E	1	44	10	55	.1	23	9	349	4.97	5	5	ND	2	14	1	2	3	142	.36	.069	4	47	.63	31	.22	2	2.85	.04	.04	1	1
LSB6 L&N 15+50E	2	22	8	52	.1	10	5	208	4.45	3	5	ND	1	23	1	2	3	138	.28	.037	4	35	.27	33	.13	2	2.32	.03	.02	1	8
LSB6 L&N 16+00E	1	51	11	79	.2	16	9	253	4.45	10	5	ND	2	30	1	2	2	123	.44	.052	4	33	.45	41	.17	2	3.33	.04	.03	2	16
LSB6 L&N 16+50E	1	57	12	90	.2	14	8	976	5.25	10	5	ND	2	17	1	2	4	135	.37	.077	4	31	.39	90	.18	2	2.99	.04	.04	1	2
LSB6 L&N 17+00E	1	53	9	90	.2	27	10	351	5.41	13	5	ND	2	11	1	2	2	147	.26	.056	3	55	.39	55	.23	19	4.07	.04	.02	2	1
LSB6 L&N 17+50E	3	77	14	75	.6	31	18	7516	4.35	11	11	ND	3	20	1	3	2	111	.31	.084	31	34	.30	187	.18	3	3.23	.04	.03	1	1
LSB6 L&N 18+00E	1	10	10	38	.1	5	4	344	1.61	2	5	ND	1	21	1	2	2	56	.26	.021	6	9	.11	128	.10	3	.95	.02	.02	1	1
LSB6 L&N 18+50E	1	131	10	97	.2	23	18	722	6.65	8	5	ND	2	21	1	2	2	137	.27	.161	10	38	1.04	180	.04	2	4.20	.04	.05	1	2
LSB6 L&N 19+00E	2	25	11	66	.2	35	22	1961	5.60	8	5	ND	1	32	1	2	2	151	.46	.073	4	79	.62	69	.58	2	1.84	.04	.01	1	3
LSB6 L&N 19+50E	2	16	10	54	.3	34	13	876	4.35	4	5	ND	1	33	1	2	2	128	.42	.094	4	73	.79	37	.44	2	2.26	.04	.02	1	7
LSB6 L&N 20+00E	1	17	6	34	.3	17	5	698	2.36	3	5	ND	1	24	1	2	2	69	.59	.054	3	40	.31	57	.27	2	.98	.03	.01	2	1
LSB6 L&N 20+50E	1	53	10	79	.1	30	14	293	4.01	4	5	ND	1	10	1	3	2	93	.27	.047	7	27	.26	67	.02	2	1.23	.03	.05	1	1
STD C/AU-S	21	58	41	135	7.2	68	28	1011	3.97	41	20	7	34	48	18	16	20	63	.48	.104	36	57	.88	179	.08	35	1.72	.09	.13	12	52

ASHWORTH EXPLORATION PROJECT - LACY STORES FILE# 86-4052

PAGE 9

SAMPLE#	Mc	Cu	Pb	Zn	Ag	Ni	Cc	Mn	Fe	As	U	Au	Tn	Sr	Cd	St	Et	V	Ca	P	La	Cr	Mo	Ba	Ti	B	Al	Na	I	K	Au1
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	%	PPH	%	%	%	PPH	PPH
LS86 L6N 21+00E	1	36	11	62	.1	27	10	183	4.71	3	5	ND	1	20	1	2	2	136	.55	.031	5	43	.47	91	.13	2	2.03	.04	.03	1	1
LS86 L6N 21+50E	1	18	6	55	.1	11	6	205	4.20	2	5	ND	2	18	1	2	2	129	.25	.049	5	30	.21	68	.17	2	1.99	.03	.02	1	1
LS86 L6N 22+00E	1	13	9	45	.1	32	6	323	2.74	4	5	ND	1	26	1	2	2	106	.33	.037	6	82	.76	63	.24	2	1.69	.03	.02	1	1
LS86 L6N 22+50E	14	72	29	59	.5	29	11	493	4.84	17	6	ND	3	7	1	6	2	91	.18	.138	35	35	.31	91	.01	2	1.07	.02	.07	1	1
LS86 L6N 23+00E	1	39	8	48	.1	22	9	129	4.52	5	5	ND	2	21	1	2	2	131	.29	.035	5	55	.39	43	.26	2	2.67	.03	.03	1	1
LS86 L3N 0+00	1	42	8	78	.1	35	13	532	3.94	4	5	ND	1	14	1	2	2	112	.35	.046	4	53	.66	82	.15	4	3.09	.04	.03	1	1
LS86 L3N 0+50E	2	15	29	386	1.0	43	12	3342	3.87	17	5	ND	2	16	2	2	4	54	.61	.142	44	40	.25	148	.01	4	3.00	.03	.03	1	1
LS86 L3N 1+00E	1	66	11	121	.2	40	14	1445	5.63	11	5	ND	2	20	1	2	2	157	.58	.086	8	72	.62	182	.28	2	3.35	.06	.08	1	2
LS86 L3N 1+50E	1	41	10	118	.1	33	26	3475	4.44	6	5	ND	1	33	1	2	2	109	.55	.114	5	76	.76	122	.28	2	2.39	.04	.03	1	12
LS86 L3N 2+00E	1	25	11	115	.1	17	9	705	4.87	5	5	ND	1	14	1	2	2	108	.31	.326	4	49	.28	65	.18	2	2.77	.03	.04	1	1
LS86 L3N 2+50E	1	33	7	75	.1	25	11	1015	3.84	3	5	ND	1	17	1	2	2	108	.39	.043	4	44	.51	84	.17	3	2.31	.04	.03	1	1
LS86 L3N 3+00E	1	90	6	111	.1	87	24	987	7.79	58	5	ND	1	10	1	5	2	192	.23	.062	6	235	.96	157	.01	3	1.90	.03	.03	1	1
LS86 L3N 3+50E	1	45	9	84	.1	38	14	1104	4.71	4	5	ND	1	14	1	2	2	130	.32	.045	4	59	.58	97	.20	2	2.73	.04	.03	1	8
LS86 L3N 4+00E	1	25	7	106	.1	28	13	1542	4.56	2	5	ND	1	22	1	2	2	117	.37	.094	3	98	.48	67	.25	2	2.14	.04	.02	1	1
LS86 L3N 4+50E	1	16	4	49	.1	24	9	315	3.42	4	5	ND	1	28	1	2	2	120	.35	.018	4	92	.73	39	.21	2	1.61	.03	.02	1	1
LS86 L3N 5+00E	1	60	7	87	.1	49	16	443	5.17	7	5	ND	2	14	1	2	2	141	.35	.045	3	61	.59	81	.28	2	3.53	.04	.04	1	1
LS86 L3N 5+50E	2	56	8	106	.1	37	14	573	4.86	6	5	ND	2	13	1	2	2	131	.33	.073	4	58	.65	76	.22	3	3.17	.04	.03	1	1
LS86 L3N 6+00E	1	47	4	66	.2	30	13	477	4.38	12	5	ND	1	14	1	2	2	124	.40	.033	6	54	.55	106	.20	3	2.74	.04	.02	1	1
LS86 L3N 6+50E	2	74	9	119	.2	55	23	544	5.92	9	5	ND	2	39	1	2	2	151	.39	.048	4	147	.94	95	.37	2	3.34	.04	.03	1	1
LS86 L3N 7+00E	1	36	9	118	.1	28	14	987	4.52	9	5	ND	2	14	1	2	2	118	.35	.108	4	51	.46	98	.20	2	2.71	.04	.03	1	1
LS86 L3N 7+50E	2	64	19	77	.1	27	23	3669	6.42	19	5	ND	1	15	1	2	2	159	.25	.039	7	83	1.10	340	.01	2	2.93	.04	.05	1	1
LS86 L3N 8+00E	1	116	6	63	.1	39	17	1377	5.87	6	5	ND	2	15	1	2	2	170	.29	.055	6	81	.67	122	.22	2	3.97	.04	.04	1	1
LS86 L3N 8+50E	1	90	10	79	.2	41	17	748	5.22	9	5	ND	3	18	1	2	2	142	.41	.047	7	73	.85	130	.22	2	4.03	.04	.06	1	1
LS86 L3N 9+00E	1	40	9	69	.2	20	14	1214	3.95	5	5	ND	1	29	1	2	2	124	.42	.064	4	59	1.04	79	.19	2	2.13	.04	.03	1	1
LS86 L3N 9+50E	1	49	12	107	.2	25	15	3575	4.29	2	5	ND	1	18	1	2	2	119	.33	.084	5	47	.59	167	.15	2	3.16	.04	.04	1	1
LS86 L3N 10+00E	1	79	9	79	.4	41	21	589	5.44	11	5	ND	2	31	1	2	2	137	.70	.041	14	60	.54	260	.15	2	3.48	.05	.04	1	2
LS86 L3N 10+50E	1	55	10	119	.3	18	22	1924	6.10	8	5	ND	1	38	1	2	2	158	.59	.347	4	53	1.45	69	.28	2	3.64	.05	.04	1	1
LS86 L3N 11+00E	2	63	7	84	.1	24	11	557	4.84	12	5	ND	1	15	1	2	2	134	.26	.128	4	52	.43	71	.21	2	4.31	.03	.03	1	1
LS86 L3N 11+50E	1	17	8	101	.2	25	19	3686	7.11	9	5	ND	1	19	1	2	2	173	1.35	.160	4	81	1.01	61	.34	4	2.97	.06	.03	1	2
LS86 L3N 12+00E	1	32	6	81	.1	23	12	794	3.89	2	5	ND	1	17	1	2	2	109	.34	.076	3	41	.43	75	.17	2	2.69	.03	.03	1	1
LS86 L3N 12+50E	1	20	8	53	.2	15	8	453	3.60	2	5	ND	1	19	1	2	2	109	.32	.030	4	34	.32	44	.20	2	2.15	.03	.03	1	1
LS86 L3N 13+00E	2	81	6	34	.1	29	12	182	5.52	4	5	ND	1	15	1	2	2	160	.32	.021	5	55	.37	46	.23	2	3.15	.04	.03	1	5
LS86 L3N 13+50E	1	119	7	79	.1	23	13	711	5.06	4	5	ND	1	14	1	2	2	138	.30	.099	3	47	.62	59	.19	2	3.21	.04	.03	1	15
LS86 L3N 14+00E	1	51	13	97	.1	17	7	496	5.53	11	5	ND	2	13	1	2	2	145	.27	.232	3	54	.41	60	.18	2	3.73	.03	.04	1	1
LS86 L3N 14+50E	1	26	23	59	.5	15	9	1521	3.57	7	5	ND	1	13	1	2	2	154	.62	.111	4	48	.26	67	.29	9	1.25	.04	.04	1	1
LS86 L3N 15+00E	1	41	7	135	.2	16	19	2989	4.96	5	5	ND	1	21	1	2	2	139	.36	.079	4	40	.56	141	.14	2	2.76	.04	.04	1	1
STD C/AU-S	21	59	38	137	7.2	69	28	1023	3.96	38	18	7	34	48	18	16	20	64	.48	.107	36	59	.88	180	.08	33	1.72	.09	.14	13	49

ASHWORTH EXPLORATION PROJECT - LACY STOKES FILE# 86-4052

SAMPLE#	Mc	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	In	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mo	Ba	Ti	F	Al	Na	K	W	Au
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	I	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	I	I	PPH	PPH	I	PPH	I	PPH	I	I	I	PPH	PPB
LS86 L3N 15+50E	1	57	8	56	.1	24	11	229	5.03	5	5	ND	1	12	1	2	2	153	.32	.034	3	45	.49	52	.27	3	2.95	.04	.02	1	1
LS86 L3N 16+00E	1	23	10	73	.2	8	14	1556	3.36	2	5	ND	1	33	1	2	2	95	.44	.043	5	23	.42	97	.10	3	1.78	.03	.03	1	1
LS86 L3N 16+50E	1	44	13	91	.2	16	16	1864	4.78	3	5	ND	2	33	1	2	2	117	1.08	.025	10	35	.49	186	.15	2	2.25	.05	.03	1	1
LS86 L3N 17+00E	1	53	8	69	.2	28	12	253	5.77	2	5	ND	1	13	1	2	2	152	.34	.057	5	42	.60	74	.20	2	2.63	.04	.03	1	2
LS86 L3N 17+50E	1	19	6	51	.1	12	5	219	2.04	2	5	ND	1	18	1	2	2	64	.53	.043	2	21	.37	45	.16	6	.93	.03	.04	1	1
LS86 L3N 18+00E	1	65	6	70	.1	32	14	293	5.57	9	5	ND	1	16	1	2	2	153	.28	.038	5	49	.43	69	.17	3	2.73	.03	.02	1	3
LS86 L3N 18+50E	3	139	23	193	1.2	36	21	8325	3.79	2	5	ND	2	44	3	2	2	73	1.70	.223	43	54	.40	262	.12	8	4.66	.06	.05	1	2
LS86 L3N 19+00E	1	54	12	58	.1	41	14	651	4.02	10	5	ND	2	23	1	2	2	108	.67	.075	5	57	.94	56	.23	6	2.02	.05	.03	1	5
LS86 L3N 19+50E	1	25	7	56	.2	32	9	183	5.05	4	5	ND	1	19	1	2	2	137	.31	.050	3	45	.46	44	.15	2	1.87	.03	.03	1	1
LS86 L3N 20+00E	1	2	7	24	.1	11	4	97	2.08	2	5	ND	1	24	1	2	2	86	.29	.022	3	33	.30	23	.08	4	1.10	.02	.03	1	2
LS86 L3N 20+50E	1	20	8	32	.1	12	5	133	3.86	2	5	ND	1	17	1	2	2	118	.29	.023	3	29	.35	25	.19	2	2.17	.03	.01	1	1
LS86 L3N 21+00E	1	20	8	42	.1	17	6	130	4.07	2	5	ND	1	21	1	2	2	134	.24	.071	4	49	.37	24	.30	3	1.91	.03	.02	1	1
LS86 L3N 21+50E	1	30	10	50	.1	12	5	269	3.85	2	5	ND	1	20	1	2	2	108	.34	.087	4	40	.26	37	.20	3	1.57	.03	.02	1	1
LS86 L3N 22+00E	2	18	7	30	.1	16	5	96	4.14	2	5	ND	1	27	1	2	2	150	.31	.020	11	44	.41	59	.05	2	2.08	.03	.04	1	2
LS86 L3N 22+50E	1	49	13	66	.2	36	11	192	4.97	4	5	ND	2	15	1	2	2	127	.30	.104	5	72	.69	48	.26	4	3.22	.04	.03	1	1
LS86 L3N 23+00E	1	5	13	32	.1	12	4	98	2.46	3	5	ND	1	24	1	2	2	107	.32	.023	5	33	.32	26	.26	3	1.21	.03	.02	1	1
LS86 L3N 23+50E	1	47	11	54	.1	49	12	676	4.49	2	5	ND	1	22	1	2	2	126	.31	.047	5	103	.69	92	.17	2	2.45	.03	.03	1	1
LS86 L3N 24+00E	1	10	6	31	.1	13	5	110	2.81	2	5	ND	1	29	1	2	2	80	.29	.030	6	28	.27	97	.06	3	1.56	.02	.03	1	1
LS86 L3N 24+50E	1	8	13	58	.1	13	10	2323	4.11	2	5	ND	1	55	1	2	2	117	.52	.102	4	53	.28	62	.16	2	1.82	.03	.02	1	1
LS86 L3N 25+00E	1	48	13	111	.1	37	11	639	4.19	3	5	ND	1	21	1	2	2	103	.39	.125	4	62	.61	130	.20	2	2.55	.04	.03	1	1
LS86 L0 0+00	1	43	10	116	.4	38	13	416	4.05	3	5	ND	2	13	1	2	2	104	.33	.062	5	54	.70	93	.17	5	3.38	.04	.05	1	2
LS86 L0 0+50E	1	53	9	78	.2	28	11	601	3.69	7	5	ND	2	12	1	2	2	102	.29	.071	5	46	.53	82	.16	3	2.75	.03	.04	1	2
LS86 L0 1+00E	1	72	12	68	.2	39	14	521	4.24	2	5	ND	2	15	1	2	2	117	.50	.067	3	58	1.01	52	.21	3	3.11	.05	.04	1	1
LS86 L0 1+50E	1	73	11	70	.2	38	12	726	4.85	7	5	ND	2	13	1	2	2	137	.33	.084	5	82	.60	71	.22	3	3.88	.04	.04	1	8
LS86 L0 2+00E	1	45	6	70	.1	25	9	767	3.36	3	5	ND	1	11	1	2	2	96	.32	.065	3	37	.44	81	.17	4	2.54	.03	.03	1	1
LS86 L0 2+50E	1	56	10	101	.3	18	11	1673	5.16	2	5	ND	1	47	1	2	2	117	.39	.155	5	60	.47	73	.20	2	2.74	.04	.03	1	2
LS86 L0 3+00E	1	66	13	70	.1	43	12	637	5.14	10	5	ND	2	16	1	2	2	145	.36	.064	4	76	.69	99	.27	2	3.98	.04	.04	1	1
LS86 L0 3+50E	1	18	112	81	.3	14	10	2635	3.89	2	5	ND	1	22	1	2	2	110	.38	.067	5	32	.36	132	.15	2	1.92	.03	.03	1	1
LS86 L0 4+00E	1	15	10	60	.1	6	4	317	3.09	2	5	ND	1	23	1	2	2	81	.26	.134	4	18	.19	64	.05	2	1.87	.02	.06	1	250
LS86 L0 4+50E	1	21	9	64	.1	16	8	608	2.65	4	5	ND	1	15	1	2	2	74	.33	.083	3	33	.35	49	.18	4	2.07	.03	.03	1	2
LS86 L0 5+00E	1	26	9	49	.1	14	6	700	2.52	5	5	ND	1	15	1	2	2	79	.24	.049	3	25	.24	74	.15	5	1.76	.02	.03	1	1
LS86 L0 5+50E	1	25	12	59	.1	4	13	361	5.97	2	5	ND	2	30	1	2	2	134	.33	.030	7	3	.85	117	.03	2	3.49	.04	.06	1	12
LS86 L0 6+50E	1	11	7	41	.2	16	7	327	3.02	2	5	ND	1	19	1	2	2	91	.25	.020	4	53	.51	97	.06	3	1.52	.03	.03	1	1
LS86 L0 7+00E	1	34	12	84	.2	21	11	2190	4.72	4	5	ND	1	19	1	2	2	121	.30	.105	4	54	.29	123	.21	2	2.45	.03	.03	1	1
LS86 L0 7+50E	1	34	9	101	.2	40	16	796	4.81	7	5	ND	1	32	1	2	2	131	.43	.076	4	106	1.26	103	.27	2	2.67	.04	.03	1	2
LS86 L0 8+00E	1	12	11	67	.1	25	12	500	4.23	2	5	ND	1	21	1	2	2	172	.24	.051	3	70	1.85	50	.19	2	2.69	.03	.03	1	1
STD C/AU-5	21	60	41	137	7.3	70	28	1029	3.96	41	17	8	34	48	18	16	19	64	.48	.105	36	59	.88	182	.08	33	1.72	.09	.13	13	49

ASHWORTH EXPLORATION PROJECT - LACY STONES FILE# 86-4052

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	P	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mo	Ba	Ti	F	Al	Na	I	W	Au#
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH
LS86 L0 8+50E	1	34	9	74	.1	36	19	359	5.32	2	5	ND	1	12	1	2	2	167	.11	.031	3	104	1.85	58	.04	2	3.85	.02	.04	1	1
LS86 L0 9+00E	1	36	8	91	.1	32	14	796	3.98	2	5	ND	1	12	1	2	2	117	.22	.136	3	86	.82	78	.03	2	2.92	.04	.03	1	1
LS86 L0 9+50E	1	26	9	80	.1	14	17	536	6.07	2	5	ND	1	19	1	2	2	196	.17	.037	2	33	1.76	90	.01	2	3.47	.04	.04	1	31
LS86 L0 10+00E	1	76	13	109	.1	31	16	508	5.66	5	5	ND	2	12	1	2	2	150	.25	.111	3	79	.56	53	.19	2	4.98	.03	.04	1	1
LS86 L0 10+50E	1	17	5	59	.1	9	9	794	3.06	3	5	ND	1	21	1	2	2	103	.23	.039	4	28	.65	49	.07	2	2.63	.03	.04	1	1
LS86 L0 11+00E	1	82	8	55	.1	34	14	293	5.34	5	5	ND	2	13	1	2	2	164	.34	.028	4	56	.54	83	.27	2	3.26	.04	.03	1	1
LS86 L0 11+50E	1	26	7	78	.4	32	9	179	3.44	7	5	ND	1	12	1	2	2	95	.23	.022	5	38	.34	51	.12	2	2.37	.03	.02	1	1
LS86 L0 12+00E	1	41	10	107	.6	28	10	237	4.49	5	5	ND	1	13	1	2	2	120	.25	.050	5	41	.30	59	.15	2	2.64	.03	.03	1	1
LS86 L0 12+50E	1	35	12	105	.2	72	26	327	5.99	4	5	ND	2	17	1	2	2	151	.39	.042	5	89	.70	60	.26	2	3.21	.04	.03	1	1
LS86 L0 13+00E	2	106	22	77	.4	12	19	<u>9937</u>	2.36	7	5	ND	1	48	1	2	2	101	1.11	.056	3	15	.67	268	.09	3	1.47	.05	.04	1	320
LS86 L0 13+50E	1	48	4	39	.1	10	14	254	4.17	2	5	ND	1	11	1	2	2	139	.16	.032	4	20	1.07	67	.01	2	3.00	.03	.03	1	1
LS86 L0 14+00E	1	64	11	73	.1	16	57	<u>2811</u>	4.31	2	5	ND	1	20	1	2	2	162	.38	.069	2	26	1.67	172	.04	2	2.30	.04	.04	1	1
LS86 L0 14+50E	1	10	12	36	.1	4	2	561	2.37	2	5	ND	1	42	1	2	2	70	.29	.044	4	12	.15	38	.07	3	1.47	.02	.04	1	1
LS86 L0 15+00E	1	36	15	62	.2	6	15	1532	3.17	2	5	ND	1	41	1	2	2	93	.47	.044	4	19	.47	118	.09	2	2.10	.03	.04	1	2
LS86 L0 15+50E	1	21	7	45	.1	13	4	105	3.80	2	5	ND	1	14	1	2	2	120	.19	.030	4	34	.23	30	.11	2	2.24	.03	.02	1	6
LS86 L0 16+00E	1	7	5	24	.1	8	2	51	.69	3	5	ND	1	27	1	2	2	62	.27	.020	3	42	.13	23	.19	7	.41	.03	.03	2	1
LS86 L0 16+50E	1	3	7	23	.1	5	1	82	1.20	3	5	ND	1	20	1	2	2	73	.27	.024	3	18	.13	18	.32	4	.54	.02	.02	1	2
LS86 L0 17+00E	1	14	7	48	.1	10	4	114	2.68	5	5	ND	1	18	1	2	2	99	.28	.017	4	31	.31	40	.17	2	1.26	.03	.02	2	1
LS86 L0 17+50E	1	30	14	93	.1	35	11	244	4.07	2	5	ND	1	20	1	2	2	111	.31	.059	4	54	.56	83	.28	2	2.65	.04	.03	1	1
LS86 L0 18+00E	1	4	10	28	.1	7	3	236	1.25	2	5	ND	1	50	1	2	2	78	.46	.021	3	21	.21	25	.35	4	.93	.03	.03	1	1
LS86 L0 18+50E	1	16	20	149	.1	33	24	<u>3709</u>	3.97	2	5	ND	1	29	1	2	2	115	.96	.044	4	53	.65	121	.54	2	1.76	.06	.08	1	1
LS86 L0 19+00E	1	12	7	37	.1	11	4	150	3.17	2	5	ND	1	18	1	2	2	129	.31	.025	4	28	.35	35	.26	2	1.37	.03	.02	2	2
LS86 L0 19+50E	1	17	7	58	.1	13	5	148	3.57	2	5	ND	1	29	1	2	2	112	.31	.048	4	31	.26	31	.27	2	1.74	.03	.02	1	1
LS86 L0 20+00E	1	22	13	62	.1	20	6	274	3.36	2	5	ND	1	30	1	2	2	100	.39	.066	4	45	.40	32	.35	2	1.94	.03	.03	1	1
LS86 L0 20+50E	1	14	5	28	.1	11	3	139	1.77	2	5	ND	1	27	1	2	2	75	.46	.015	5	29	.11	49	.31	4	.88	.03	.02	1	1
LS86 L0 21+00E	1	8	9	43	.1	19	7	472	2.90	2	5	ND	1	34	1	2	2	88	.41	.042	4	39	.48	25	.24	2	1.42	.03	.03	1	2
LS86 L0 21+50E	1	19	8	60	.1	19	7	431	3.02	2	5	ND	1	26	1	2	2	89	.41	.060	4	39	.35	47	.23	2	1.68	.03	.03	1	1
LS86 L0 22+00E	1	29	7	47	.2	23	8	223	4.04	2	5	ND	2	18	1	2	2	120	.29	.052	4	41	.41	48	.25	2	2.21	.03	.03	2	1
LS86 L0 22+50E	1	23	11	75	.1	28	11	509	4.39	2	5	ND	2	18	1	2	2	117	.33	.110	4	55	.54	52	.37	2	2.38	.04	.03	1	1
LS86 L0 23+00E	1	29	13	74	.3	33	10	754	2.83	4	10	ND	1	25	1	2	2	66	1.57	.035	5	45	.62	47	.18	5	1.47	.05	.04	1	1
LS86 L0 23+50E	1	10	10	49	.1	12	5	308	3.05	2	5	ND	1	30	1	2	2	108	.38	.041	5	36	.26	64	.24	2	1.29	.03	.02	2	1
LS86 L0 24+00E	1	16	6	39	.1	14	5	327	2.78	2	5	ND	1	41	1	2	2	87	.37	.063	4	36	.27	30	.19	2	1.44	.03	.02	1	1
LS86 L3S 0+00	1	125	16	66	.1	51	15	739	4.14	4	5	ND	2	14	1	2	2	115	.44	.129	3	74	.91	99	.20	3	3.97	.04	.03	1	1
LS86 L3S 0+50E	2	30	15	103	.2	25	19	<u>18862</u>	3.14	5	5	ND	1	29	1	2	2	73	.39	.159	3	83	.45	221	.11	2	1.43	.04	.05	1	1
LS86 L3S 1+00E	1	57	7	94	.1	32	11	<u>828</u>	3.98	4	5	ND	2	13	1	2	3	116	.31	.209	3	49	.47	80	.22	2	3.50	.03	.04	1	1
LS86 L3S 1+50E	1	74	9	66	.4	38	14	446	4.48	3	5	ND	2	16	1	2	2	135	.39	.039	6	64	.77	120	.25	2	3.40	.04	.04	1	1
STD C/AU-5	22	61	39	140	7.3	71	29	1045	3.97	38	16	8	35	49	19	16	22	66	.48	.106	37	59	.88	185	.08	36	1.72	.09	.13	13	51

ASHWORTH EXPLORATION PROJECT - LACY STORES FILE# 86-4052

SAMPLE#	Mc	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mo	Ba	Ti	B	Al	Na	F	W	Au1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
LS86 L3S 2+00E	1	51	11	73	.1	29	11	679	4.38	3	5	ND	2	13	1	2	2	122	.36	.070	4	49	.40	64	.27	2	2.67	.03	.02	1	1
LS86 L3S 2+50E	1	63	10	79	.1	32	12	496	4.49	3	5	ND	1	12	1	2	2	136	.48	.061	3	49	.60	71	.30	2	2.97	.04	.02	1	1
LS86 L3S 3+00E	1	39	12	83	.1	24	11	313	4.89	8	5	ND	1	15	1	2	2	136	.38	.038	4	46	.41	80	.20	2	2.55	.04	.03	1	1
LS86 L3S 3+50E	2	41	14	71	.2	19	12	784	5.27	5	5	ND	2	21	1	3	2	148	.39	.029	6	36	.27	126	.23	2	2.52	.04	.04	1	2
LS86 L3S 4+00E	1	65	8	114	.1	36	14	756	4.81	8	5	ND	2	15	1	2	2	129	.38	.098	5	47	.52	108	.23	2	3.32	.04	.04	1	1
LS86 L3S 4+50E	2	34	12	51	.1	14	8	231	5.05	120	5	ND	1	9	1	7	3	97	.15	.081	4	20	.19	49	.04	4	1.96	.02	.03	1	1
LS86 L3S 5+00E	1	9	9	74	.1	4	8	2475	2.55	5	5	ND	1	10	1	2	2	60	.19	.056	11	9	.28	121	.02	2	1.33	.02	.04	1	7
LS86 L3S 5+50E	1	73	8	92	.1	89	20	490	5.20	32	5	ND	2	12	1	12	2	99	.28	.088	4	83	.46	245	.04	3	2.72	.03	.07	1	86
LS86 L3S 6+00E	2	31	8	49	.1	38	13	271	4.78	8	5	ND	1	27	1	3	2	135	.43	.029	5	128	.64	75	.16	2	2.26	.04	.03	2	1
LS86 L3S 6+50E	2	65	11	71	.1	47	15	421	5.01	14	5	ND	2	13	1	2	2	129	.29	.049	6	82	.71	92	.14	2	2.88	.04	.04	1	1
LS86 L3S 7+00E	1	26	15	71	.1	22	14	3206	3.60	4	5	ND	1	34	1	2	2	99	.32	.117	4	71	.74	108	.19	2	1.99	.03	.03	1	4
LS86 L3S 7+50E	3	120	17	349	.3	66	41	7376	6.76	19	5	ND	3	18	1	2	2	131	.30	.213	12	103	.62	94	.19	4	4.79	.04	.04	1	1
LS86 L3S 8+00E	1	62	12	91	.1	51	18	825	4.95	8	5	ND	2	19	1	2	2	125	.29	.103	4	101	1.06	59	.14	2	3.05	.04	.03	1	1
LS86 L3S 8+50E	1	11	5	43	.1	24	8	260	2.90	5	5	ND	1	28	1	2	2	102	.27	.024	5	72	.79	23	.13	2	1.77	.03	.01	2	2
LS86 L3S 9+00E	1	25	8	59	.1	26	12	308	3.96	4	5	ND	2	21	1	3	2	113	.26	.050	4	74	.50	58	.09	2	2.22	.03	.02	1	2
LS86 L3S 9+50E	2	52	5	79	.1	24	10	191	2.66	13	5	ND	1	5	1	4	2	43	.10	.029	3	28	.24	53	.03	2	1.52	.02	.02	1	6
LS86 L3S 10+50E	3	27	8	126	.3	27	12	204	3.44	7	5	ND	1	6	1	2	2	67	.20	.032	9	25	.38	47	.04	2	2.16	.02	.02	1	1
LS86 L3S 11+00E	2	60	10	87	.4	48	14	620	4.45	14	5	ND	2	16	1	2	2	96	.51	.045	15	57	.67	79	.18	2	3.07	.04	.04	1	2
LS86 L3S 11+50E	3	83	16	78	.1	39	28	383	5.76	10	5	ND	2	16	1	3	2	144	.33	.043	5	61	.51	95	.26	3	2.93	.04	.03	1	1
LS86 L3S 12+00E	1	17	11	60	.1	6	6	1191	3.18	8	5	ND	1	10	1	2	2	93	.27	.049	3	22	.27	90	.05	2	2.19	.02	.04	1	7
LS86 L3S 12+50E	1	73	8	73	.1	17	8	293	3.78	8	5	ND	1	18	1	2	2	98	.30	.105	4	41	.50	39	.18	2	3.24	.03	.03	1	9
LS86 L3S 13+00E	1	24	7	50	.1	5	3	301	2.62	2	5	ND	1	18	1	2	2	77	.26	.043	3	21	.13	43	.09	3	1.57	.02	.01	1	5
LS86 L3S 13+50E	2	51	9	51	.2	24	10	319	3.60	3	5	ND	2	15	1	2	2	100	.38	.061	5	44	.57	49	.21	2	2.82	.04	.03	1	6
LS86 L3S 14+00E	1	25	10	48	.1	11	7	212	4.07	6	5	ND	1	13	1	2	2	116	.31	.033	5	28	.31	51	.15	3	1.84	.03	.02	2	5
LS86 L3S 14+50E	1	25	10	43	.1	15	9	351	5.25	4	5	ND	1	19	1	2	2	157	.35	.024	5	37	.44	66	.23	2	2.56	.04	.02	1	5
LS86 L3S 15+00E	2	43	5	60	.1	21	10	488	3.98	8	5	ND	1	17	1	2	2	115	.42	.062	4	44	.52	54	.22	2	2.61	.04	.03	1	3
LS86 L3S 15+50E	1	16	10	45	.1	10	4	309	4.51	2	5	ND	1	21	1	2	2	126	.25	.050	5	43	.27	22	.15	2	2.28	.03	.02	2	1
LS86 L3S 16+00E	1	17	14	49	.1	14	5	346	3.77	7	5	ND	1	21	1	2	2	109	.23	.062	4	50	.40	33	.18	2	2.34	.03	.03	2	3
LS86 L3S 16+50E	1	16	14	48	.1	8	3	1003	1.90	2	5	ND	1	14	1	2	2	55	.26	.057	4	20	.20	35	.11	2	1.43	.02	.02	2	1
LS86 L3S 17+00E	1	4	8	21	.1	2	2	113	1.45	4	5	ND	1	30	1	2	2	65	.35	.016	4	10	.11	21	.10	2	.85	.02	.02	1	1
LS86 L3S 17+50E	2	47	11	81	.2	19	7	247	5.21	6	5	ND	2	13	1	2	2	125	.26	.099	6	47	.45	40	.26	4	3.89	.03	.03	1	2
LS86 L3S 18+00E	1	10	9	40	.1	7	3	87	3.96	2	5	ND	1	18	1	2	2	124	.24	.015	4	35	.19	24	.19	2	1.47	.03	.02	2	5
LS86 L3S 19+00E	1	15	9	36	.1	10	4	154	4.15	3	5	ND	1	15	1	2	2	142	.28	.067	4	33	.27	27	.26	3	1.75	.03	.02	1	15
LS86 L3S 19+50E	1	4	7	22	.1	4	1	166	1.49	2	5	ND	1	16	1	3	3	75	.25	.024	3	12	.08	11	.26	2	.57	.02	.02	1	2
LS86 L3S 20+00E	1	4	6	28	.1	4	2	147	1.15	2	5	ND	1	27	1	2	2	96	.33	.019	3	19	.15	28	.36	2	.55	.03	.01	2	1
LS86 L3S 20+50E	1	10	6	44	.2	20	6	164	2.71	4	5	ND	1	17	1	2	2	84	.37	.017	3	37	.25	35	.20	2	1.19	.03	.02	2	1
STD C/AU-S	22	60	38	136	7.2	70	28	1014	3.97	38	20	7	34	48	18	16	21	64	.48	.105	35	58	.88	178	.08	35	1.72	.09	.13	12	46

ASHWORTH EXPLORATION PROJECT - LACY STONES FILE# 86-4052

SAMPLE#	Hc	Cu	Pb	Zn	As	Ni	Co	Mn	Fe	Ks	U	Au	Tl	Sr	Cd	Sb	Bi	V	Ca	F	La	Cr	Mo	Ba	Ti	B	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
LSB6 L3S 21+00E	1	18	8	53	.1	16	5	147	3.27	5	5	ND	1	14	1	2	2	87	.25	.095	4	34	.26	27	.22	2	2.41	.03	.02	1	1
LSB6 L3S 21+50E	1	29	7	73	.1	32	9	232	4.35	3	5	ND	1	19	1	2	2	113	.27	.054	4	63	.41	38	.22	2	2.83	.03	.02	1	1
LSB6 L3S 22+00E	1	29	8	59	.1	27	7	458	3.26	4	5	ND	1	17	1	2	2	82	.29	.082	4	52	.45	35	.19	2	2.10	.03	.02	1	1
LSB6 L3S 22+50E	1	3	6	21	.1	7	3	287	1.60	3	7	ND	1	19	1	2	2	61	.30	.025	3	21	.14	23	.33	2	.54	.03	.01	1	1
LSB6 L3S 23+00E	1	21	6	49	.1	17	6	238	3.67	2	5	ND	1	15	1	2	2	112	.31	.034	4	39	.25	56	.22	2	1.82	.03	.02	1	3
LSB6 L3S 23+50E	1	46	7	43	.4	34	11	342	3.28	6	5	ND	1	16	1	2	2	90	.39	.044	14	54	.42	107	.20	2	2.77	.04	.03	1	1
LSB6 L3S 24+00E	1	71	35	115	.1	24	19	1182	5.03	15	5	ND	1	20	1	2	2	115	.54	.139	8	49	.52	89	.19	2	1.88	.04	.04	1	2
LSB6 L6S 10+00W	1	53	7	87	.1	44	13	790	4.42	6	5	ND	2	17	1	2	2	131	.38	.062	8	57	.61	183	.22	2	3.54	.04	.04	1	1
LSB6 L6S 9+50W	1	58	5	79	.1	42	14	492	4.55	2	5	ND	2	17	1	2	2	131	.38	.047	9	61	.63	107	.21	2	3.66	.04	.03	1	1
LSB6 L6S 9+00W	1	55	8	115	.2	45	13	4070	4.51	2	5	ND	1	32	1	2	2	112	.74	.055	22	58	.44	208	.20	2	3.72	.05	.04	1	1
LSB6 L6S 8+50W	1	52	7	72	.1	39	14	759	4.43	6	5	ND	1	22	1	2	2	131	.47	.034	8	62	.62	112	.19	2	3.22	.04	.03	1	1
LSB6 L6S 8+00W	1	37	6	65	.3	27	11	1624	3.49	6	5	ND	1	40	1	2	2	109	1.38	.044	9	75	.40	129	.15	5	2.42	.05	.03	1	11
LSB6 L6S 7+50W	1	54	5	59	.1	35	12	393	4.04	10	5	ND	1	20	1	2	2	126	.48	.018	6	54	.74	63	.20	2	3.01	.04	.02	1	6
LSB6 L6S 7+00W	1	23	9	73	.1	29	13	801	4.01	2	5	ND	1	25	1	3	2	123	.60	.023	6	44	.39	110	.22	2	2.61	.04	.02	1	1
LSB6 L6S 6+50W	1	52	12	102	.1	37	14	1882	4.38	6	5	ND	2	16	1	2	2	124	.41	.131	5	50	.64	127	.22	3	3.09	.04	.03	1	1
LSB6 L6S 6+00W	1	41	8	105	.1	33	13	2181	3.90	9	5	ND	1	21	1	2	2	105	.48	.172	6	41	.57	290	.20	3	2.98	.04	.04	1	2
LSB6 L6S 5+50W	1	38	13	86	.1	35	17	1863	5.19	6	5	ND	1	29	1	2	2	145	.41	.128	8	59	.64	449	.34	3	3.24	.04	.04	1	10
LSB6 L6S 5+00W	1	49	10	94	.1	38	12	738	3.50	2	5	ND	1	17	1	2	2	102	.39	.064	5	40	.42	160	.21	2	2.44	.03	.03	1	1
LSB6 L6S 4+50W	1	45	11	140	.1	28	14	3446	3.77	6	5	ND	1	19	1	2	2	98	.54	.323	6	37	.55	226	.17	3	2.47	.04	.05	1	1
LSB6 L6S 4+00W	1	117	10	100	.1	55	21	853	5.15	6	5	ND	1	29	1	2	2	137	.40	.154	5	109	1.24	105	.27	3	3.15	.05	.05	1	28
LSB6 L6S 3+50W	1	65	12	72	.1	33	13	870	4.37	3	5	ND	3	14	1	2	2	137	.33	.083	4	56	.55	90	.27	2	3.94	.04	.03	1	1
LSB6 L6S 3+00W	1	47	3	40	.1	16	10	439	3.04	2	5	ND	1	18	1	2	2	94	.40	.029	3	25	.49	58	.07	2	1.91	.03	.03	1	185
LSB6 L6S 2+50W	1	78	9	74	.1	39	17	453	5.08	7	5	ND	2	19	1	2	2	149	.37	.051	8	57	.50	97	.30	2	3.70	.04	.03	1	26-
LSB6 L6S 2+00W	1	86	8	84	.1	31	14	1000	5.89	4	5	ND	2	14	1	2	2	165	.31	.119	5	50	.43	120	.24	3	3.77	.04	.04	1	33-
LSB6 L6S 1+50W	1	58	7	119	.2	42	19	2754	4.22	9	5	ND	2	20	1	2	2	122	.46	.069	10	54	.60	137	.21	2	4.10	.04	.04	1	3
LSB6 L6S 1+00W	1	31	10	127	.1	35	13	1719	4.47	4	5	ND	1	15	1	2	2	129	.35	.172	5	49	.39	163	.29	2	3.17	.04	.04	1	1
LSB6 L6S 0+50W	1	49	11	90	.1	35	14	800	4.65	10	5	ND	1	15	1	2	2	138	.36	.148	4	56	.50	128	.25	2	3.31	.04	.03	1	8
LSB6 L6S 0+00	1	18	9	71	.1	23	8	506	2.81	6	5	ND	1	25	1	2	2	89	.49	.076	3	79	.82	44	.20	2	1.73	.03	.03	1	1
LSB6 L6S 0+50E	1	47	8	110	.1	40	13	696	4.56	7	5	ND	1	19	1	2	2	117	.38	.142	4	69	.56	101	.23	2	2.82	.04	.03	1	1
LSB6 L6S 1+00E	2	21	11	58	.1	20	9	260	4.46	2	5	ND	1	22	1	2	2	126	.40	.046	4	38	.39	64	.20	2	2.09	.04	.03	1	30
LSB6 L6S 1+50E	1	23	11	133	.2	15	22	4482	4.67	3	5	ND	1	54	1	2	2	90	.88	.159	7	22	.64	153	.18	2	2.32	.05	.10	1	1
LSB6 L6S 2+00E	2	39	9	68	.1	22	9	295	5.29	7	5	ND	2	15	1	2	2	138	.27	.083	4	42	.33	72	.22	2	3.38	.03	.04	1	1
LSB6 L6S 2+50E	1	17	8	75	.1	14	7	746	4.70	2	5	ND	2	24	1	2	2	129	.33	.077	4	32	.30	86	.16	2	2.36	.03	.03	1	1
LSB6 L6S 3+00E	2	54	10	100	.1	34	14	730	4.88	3	5	ND	2	14	1	2	2	129	.30	.122	5	53	.46	78	.23	2	3.96	.03	.04	1	1
LSB6 L6S 3+50E	1	26	11	74	.1	18	11	854	4.07	3	5	ND	2	21	1	2	2	109	.37	.092	5	34	.43	65	.19	2	2.29	.03	.04	1	1
LSB6 L6S 4+00E	1	34	13	72	.1	20	9	951	3.43	3	5	ND	2	19	1	2	2	102	.40	.086	5	38	.37	69	.18	2	2.24	.03	.04	1	1
STD C/AU-E	21	61	38	139	7.3	71	29	1041	3.97	40	16	8	35	49	18	16	18	65	.48	.108	37	60	.88	184	.08	36	1.72	.09	.13	13	53

ASHWORTH EXPLORATION PROJECT - LACY STORES FILE# B6-4052

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mo	Ba	Ti	B	Al	Na	F	M	AuI
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
LSB6 L6S 4+50E	1	31	7	57	.1	22	8	230	3.99	2	5	ND	1	12	1	2	2	115	.36	.040	3	33	.37	61	.23	5	2.51	.03	.03	1	2
LSB6 L6S 5+00E	2	32	12	94	.1	20	13	371	5.01	7	8	ND	1	11	1	5	2	104	.22	.061	9	26	.26	95	.02	2	2.30	.03	.04	1	1
LSB6 L6S 5+50E	1	69	9	77	.2	63	15	353	4.64	5	5	ND	1	12	1	2	2	121	.27	.071	4	58	.50	82	.13	2	2.65	.03	.02	1	1
LSB6 L6S 6+00E	1	64	7	80	.1	101	22	507	5.51	62	5	ND	1	8	1	10	2	103	.10	.054	4	128	.37	103	.01	2	1.98	.03	.06	1	2
LSB6 L6S 6+50E	1	42	10	68	.1	50	20	676	4.43	4	7	ND	1	9	1	2	2	127	.18	.034	5	141	1.41	63	.05	2	2.73	.03	.02	1	1
LSB6 L6S 7+00E	1	67	9	67	.2	39	15	376	4.47	9	5	ND	2	19	1	2	2	117	.54	.042	5	55	.71	77	.19	3	3.77	.04	.03	1	1
LSB6 L6S 7+50E	1	42	11	77	.2	48	15	1331	4.15	2	5	ND	1	23	1	2	2	99	.46	.111	6	120	.89	79	.20	2	2.63	.04	.04	1	1
LSB6 L6S 8+00E	2	160	8	71	.1	42	16	514	5.87	15	5	ND	2	29	1	2	2	161	.32	.090	4	112	1.55	35	.27	3	3.37	.04	.04	1	3
LSB6 L6S 8+50E	1	90	11	77	.2	41	16	530	4.65	19	6	ND	2	13	1	4	2	122	.31	.109	3	68	.71	59	.23	2	3.89	.04	.04	1	1
LSB6 L6S 9+00E	1	41	9	50	.1	26	10	274	4.21	12	5	ND	1	22	1	2	2	122	.42	.053	3	59	.62	36	.25	2	2.32	.04	.02	1	2
LSB6 L6S 9+50E	1	34	12	62	.1	18	9	229	4.23	2	5	ND	1	11	1	2	2	116	.25	.046	3	32	.32	43	.19	2	2.38	.03	.03	1	1
LSB6 L6S 10+00E	1	7	4	105	.1	34	7	455	.98	3	5	ND	1	4	1	2	2	17	.09	.058	4	10	.27	34	.02	2	.84	.01	.02	1	1
LSB6 L6S 10+50E	1	13	8	105	.2	21	7	392	2.56	5	5	ND	1	13	1	2	2	68	.23	.072	3	28	.38	61	.09	2	1.89	.03	.03	1	1
LSB6 L6S 11+00E	4	75	9	182	.4	17	20	1172	3.46	2	5	ND	1	13	1	2	2	68	.36	.212	13	32	.23	217	.13	3	2.98	.03	.04	1	1
LSB6 L6S 11+50E	1	25	7	41	.1	10	7	398	3.37	2	5	ND	1	16	1	2	2	97	.31	.033	4	23	.27	82	.09	2	1.66	.03	.02	2	1
LSB6 L6S 12+00E	1	22	11	59	.1	8	7	358	3.29	2	5	ND	1	57	1	2	2	99	.40	.048	3	26	.58	40	.10	2	1.71	.03	.02	1	1
LSB6 L6S 12+50E	1	49	10	78	.1	13	6	649	4.66	5	5	ND	2	12	1	2	2	105	.22	.216	4	37	.33	49	.16	2	2.87	.03	.03	1	1
LSB6 L6S 13+00E	1	19	10	80	.1	15	10	292	3.69	2	5	ND	1	14	1	2	4	100	.28	.037	5	31	.27	58	.21	2	2.21	.03	.02	1	2
LSB6 L6S 13+25E	1	41	9	68	.1	18	7	272	4.09	2	5	ND	1	14	1	2	2	114	.30	.061	3	36	.40	46	.19	2	2.32	.03	.03	1	1
LSB6 L6S 13+50E	1	20	7	78	.2	13	6	528	4.39	4	5	ND	1	28	1	2	2	132	.40	.071	3	33	.34	85	.23	2	1.86	.03	.03	1	1
LSB6 L6S 13+75E	1	35	8	60	.1	19	7	455	3.53	2	5	ND	1	15	1	2	2	100	.30	.069	4	39	.41	45	.21	2	2.96	.03	.03	1	5
LSB6 L6S 14+00E	3	25	13	74	.1	11	6	794	6.08	3	7	ND	2	13	1	2	2	115	.26	.272	5	39	.32	43	.24	3	3.83	.03	.03	1	1
LSB6 L6S 14+25E	1	10	9	35	.1	9	6	405	3.35	2	5	ND	1	16	1	2	2	87	.31	.058	4	25	.29	43	.16	2	1.34	.03	.02	1	3
LSB6 L6S 14+50E	1	36	8	65	.3	20	19	369	3.50	5	5	ND	2	11	1	2	2	98	.38	.107	6	25	.51	34	.20	2	3.37	.04	.02	1	4
LSB6 L6S 14+75E	1	40	10	77	.3	21	14	809	4.37	3	5	ND	2	13	1	2	2	120	.36	.057	6	34	.56	55	.29	3	2.54	.04	.02	1	1
LSB6 L6S 15+00E	1	13	6	52	.1	10	8	757	2.85	3	5	ND	1	18	1	2	3	91	.35	.041	3	26	.29	39	.18	2	1.24	.03	.02	1	1
LSB6 L6S 15+50E	2	30	10	58	.2	19	8	455	3.77	3	5	ND	1	16	1	2	2	114	.43	.037	3	37	.43	51	.21	2	2.00	.03	.02	1	3
LSB6 L6S 16+00E	2	31	11	74	.1	19	7	202	4.73	2	5	ND	1	17	1	2	2	133	.31	.048	3	43	.31	50	.27	2	2.37	.03	.02	1	6
LSB6 L6S 16+50E	1	65	10	41	.4	18	10	642	2.80	2	5	ND	1	9	1	2	3	81	.35	.053	21	34	.25	54	.15	2	2.86	.03	.02	1	1
LSB6 L6S 17+00E	1	58	6	56	.1	31	11	268	4.05	9	5	ND	2	11	1	2	2	109	.28	.049	4	44	.55	41	.21	2	3.67	.03	.03	1	3
LSB6 L6S 17+50E	1	16	8	35	.1	9	4	321	2.24	2	5	ND	1	12	1	2	2	67	.21	.032	4	21	.26	23	.11	2	1.29	.02	.03	1	3
LSB6 L6S 18+00E	2	15	16	77	.1	12	12	739	5.69	2	5	ND	2	12	1	2	2	95	.22	.104	6	30	.26	53	.11	2	3.67	.03	.02	1	3
LSB6 L6S 18+50E	1	16	11	63	.1	24	9	613	3.95	2	5	ND	1	12	1	2	2	96	.25	.101	3	50	.44	50	.19	2	1.87	.03	.02	2	4
LSB6 L6S 19+00E	3	23	16	67	.2	20	8	396	5.12	17	5	ND	1	11	1	2	2	142	.34	.083	4	57	.64	63	.39	2	1.65	.04	.02	1	1
LSB6 L6S 19+50E	1	7	8	29	.1	6	2	94	2.54	2	5	ND	1	12	1	2	2	89	.20	.026	3	19	.13	19	.17	2	.90	.02	.02	2	1
LSB6 L6S 20+00E	1	28	11	69	.2	21	7	207	4.50	3	5	ND	2	10	1	2	2	114	.22	.049	3	45	.28	34	.24	2	2.61	.03	.02	1	3
STD C/AU-S	22	60	39	136	7.2	70	28	1020	3.95	38	19	8	34	48	18	16	18	64	.48	.103	36	55	.88	180	.08	35	1.72	.09	.14	12	49

ASHWORTH EXPLORATION PROJECT - LACY STOKES FILE# 86-4052

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	I		J		Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	F PPM	Al %	Na %	K %	W PPM	Aut PPB
						Mi PPM	Co PPM	Mn PPM	Ni PPM																							
LSB6 L9S 7+00W	1	48	12	57	.1	20	11	963	4.13	2	5	ND	1	23	1	2	2	122	.40	.024	8	34	.33	237	.18	3	2.36	.04	.03	1	1	
LSB6 L9S 6+50W	1	27	21	66	.3	25	10	1031	3.83	4	5	ND	1	30	1	2	2	110	1.22	.030	8	36	.28	70	.20	3	2.47	.05	.02	1	1	
LSB6 L9S 6+00W	1	21	10	50	.2	27	10	305	4.10	4	5	ND	1	22	1	3	2	121	.71	.022	4	39	.38	53	.23	3	2.76	.04	.03	1	1	
LSB6 L9S 5+50W	1	49	9	75	.2	33	11	633	3.78	6	5	ND	2	25	1	2	2	112	.44	.085	5	44	.60	171	.20	3	3.00	.04	.04	2	1	
LSB6 L9S 5+00W	1	50	9	91	.2	45	13	646	4.06	11	5	ND	1	25	1	2	2	120	.39	.050	6	48	.59	132	.20	3	3.48	.04	.04	1	1	
LSB6 L9S 4+50W	1	29	6	79	.2	25	10	1579	3.24	3	5	ND	1	30	1	2	2	92	.37	.073	10	34	.41	192	.18	2	2.40	.03	.04	1	1	
LSB6 L9S 4+00W	1	39	7	120	.1	25	10	2624	3.44	6	5	ND	1	15	1	2	2	87	.34	.275	5	36	.45	289	.16	3	2.57	.03	.04	1	1	
LSB6 L9S 3+50W	1	76	10	68	.2	19	11	2901	4.15	2	5	ND	1	22	1	2	2	116	.36	.104	5	33	.40	167	.22	2	2.32	.03	.04	1	1	
LSB6 L9S 3+00W	1	76	7	66	.2	33	12	435	4.81	2	5	ND	2	16	1	3	2	141	.33	.050	5	48	.57	134	.26	3	3.75	.04	.04	1	2	
LSB6 L9S 2+50W	1	59	11	88	.2	24	12	1671	4.71	2	5	ND	1	21	1	2	2	127	.37	.139	4	40	.47	198	.22	2	2.48	.04	.04	1	3	
LSB6 L9S 2+00W	1	77	7	76	.2	35	16	988	4.25	9	5	ND	1	30	1	2	2	111	.76	.055	6	45	.72	96	.21	2	2.13	.05	.07	1	1	
LSB6 L9S 1+50W	1	41	7	46	.1	26	12	497	4.18	2	5	ND	1	18	1	2	2	129	.38	.020	5	46	.31	174	.19	2	2.52	.03	.03	2	1	
LSB6 L9S 1+00W	1	89	7	57	.1	29	10	327	3.65	10	5	ND	2	15	1	2	2	109	.34	.042	4	41	.62	114	.18	3	2.98	.04	.03	1	5	
LSB6 L9S 0+50W	1	51	9	65	.1	38	13	746	4.76	4	5	ND	1	21	1	2	2	137	.47	.043	5	56	.48	121	.18	3	3.28	.04	.04	1	3	
LSB6 L9S 0+00	1	42	10	63	.1	35	11	269	5.11	2	5	ND	2	17	1	3	2	145	.29	.043	5	56	.44	97	.21	3	3.76	.04	.03	1	1	
LSB6 L9S 0+50E	1	30	13	104	.1	8	9	2143	4.01	2	5	ND	1	44	1	2	2	101	.40	.124	6	16	.26	226	.10	2	2.55	.03	.08	1	4	
LSB6 L9S 1+00E	1	56	14	58	.1	24	9	670	4.82	4	5	ND	2	14	1	3	2	142	.28	.072	5	51	.45	71	.25	4	4.05	.03	.03	2	1	
LSB6 L9S 1+50E	1	56	13	121	.1	30	15	1866	4.54	2	5	ND	2	23	1	2	2	120	.33	.142	5	42	.29	178	.23	4	2.84	.04	.04	1	8	
LSB6 L9S 2+00E	1	42	10	116	.2	17	23	2704	4.13	2	5	ND	1	27	1	2	2	78	.37	.185	5	39	.21	84	.20	2	2.42	.03	.02	1	20	
LSB6 L9S 2+50E	1	45	9	73	.1	30	11	342	4.28	4	5	ND	1	15	1	2	2	123	.34	.057	4	43	.47	75	.22	2	2.95	.04	.04	1	1	
LSB6 L9S 3+00E	1	39	9	77	.1	20	9	746	2.93	2	5	ND	1	20	1	2	2	85	.32	.082	5	33	.45	116	.14	2	2.24	.03	.03	1	1	
LSB6 L9S 3+50E	1	27	5	83	.1	21	9	464	3.40	2	5	ND	1	16	1	2	2	95	.34	.118	4	28	.36	82	.18	2	2.40	.03	.03	1	1	
LSB6 L9S 4+00E	1	49	10	59	.2	27	10	416	3.81	2	5	ND	1	15	1	2	2	109	.30	.060	5	42	.56	88	.20	3	3.38	.03	.03	2	1	
LSB6 L9S 4+50E	1	35	10	51	.1	24	13	233	4.54	5	5	ND	1	12	1	3	2	105	.26	.034	5	30	.41	79	.13	2	2.93	.03	.03	1	2	
LSB6 L9S 5+00E	1	45	7	76	.1	26	10	712	3.75	2	5	ND	2	13	1	2	2	102	.34	.121	5	36	.46	91	.17	2	2.85	.03	.03	2	1	
LSB6 L9S 5+50E	1	29	14	124	.1	21	12	686	4.05	3	5	ND	1	15	1	2	2	108	.35	.183	5	34	.34	104	.15	2	2.39	.03	.04	1	1	
LSB6 L9S 6+00E	1	90	8	77	.1	76	25	1712	5.61	204	5	ND	1	15	1	17	2	148	.23	.084	5	173	.52	191	.01	5	2.24	.03	.04	1	1	
LSB6 L9S 6+50E	1	18	10	82	.1	23	15	2231	3.50	4	5	ND	1	32	1	2	2	101	.42	.101	5	82	.53	62	.19	2	1.84	.03	.02	1	1	
LSB6 L9S 7+00E	1	28	6	42	.1	27	9	301	3.06	2	5	ND	1	25	1	2	2	95	.37	.027	5	77	.71	53	.15	3	1.77	.03	.02	2	1	
LSB6 L9S 7+50E	1	39	8	113	.1	23	11	410	3.88	4	5	ND	2	14	1	2	2	103	.29	.109	4	38	.43	65	.13	2	2.32	.03	.03	1	1	
LSB6 L9S 8+00E	1	129	4	91	.7	42	15	2250	3.99	12	5	ND	1	29	2	2	2	86	1.12	.061	19	72	.79	115	.10	3	2.53	.05	.03	1	1	
LSB6 L9S 8+50E	1	35	8	72	.1	33	17	547	4.64	2	5	ND	1	14	1	2	2	160	.19	.040	4	117	1.71	93	.11	2	3.55	.03	.04	2	1	
LSB6 L9S 9+00E	1	24	6	66	.1	62	19	559	3.76	2	6	ND	1	29	1	2	2	112	.30	.026	3	213	1.50	38	.26	2	2.09	.03	.02	1	3	
LSB6 L9S 9+50E	1	54	7	71	.2	23	18	1074	5.53	6	6	ND	2	17	1	2	2	149	.35	.058	8	44	1.03	128	.06	3	3.93	.04	.04	2	1	
LSB6 L9S 10+00E	1	24	9	106	.2	28	10	706	4.61	10	6	ND	2	11	1	2	2	79	.26	.064	8	37	.27	70	.07	4	2.50	.03	.04	2	1	
LSB6 L9S 10+50E	1	9	12	121	.1	21	8	1758	2.91	10	5	ND	1	14	1	2	2	59	.30	.120	7	25	.18	113	.03	3	1.83	.02	.03	1	1	
STD C/AU-S	21	60	41	138	7.4	70	29	1033	3.97	39	19	8	35	49	18	15	18	66	.48	.105	37	58	.88	183	.08	36	1.72	.09	.13	12	53	

ASHWORTH EXPLORATION PROJECT - LACY STOKES FILE# 86-4052

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	P	Al	Na	F	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
LS86 11+00E	1	13	8	105	.1	22	8	313	2.99	8	5	ND	1	14	1	2	3	81	.32	.045	4	31	.52	54	.09	2	2.36	.03	.02	1	1
LS86 11+50E	1	13	8	118	.1	18	10	1126	3.27	3	5	ND	1	18	1	2	2	84	.38	.220	5	34	.39	109	.14	2	2.09	.03	.04	1	1
LS86 12+00E	1	35	9	41	.1	12	6	213	4.04	2	5	ND	1	19	1	2	2	120	.31	.035	6	34	.28	53	.14	2	2.55	.03	.02	8	1
LS86 12+50E	1	56	12	67	.1	15	7	604	4.44	5	5	ND	2	15	1	2	4	111	.30	.181	4	40	.39	41	.22	2	3.26	.04	.04	1	1
LS86 13+00E	1	101	12	84	.1	12	12	362	5.57	2	7	ND	2	12	1	3	3	117	.12	.184	7	39	.63	89	.04	2	5.70	.03	.04	1	1
LS86 13+50E	1	17	11	133	.1	14	16	1215	5.47	2	5	ND	1	20	1	2	2	117	.35	.138	5	23	.41	133	.22	2	2.46	.03	.03	1	1
LS86 14+00E	3	66	13	100	.3	29	39	4923	4.72	6	12	ND	3	16	1	2	2	104	.37	.092	13	38	.45	97	.16	8	3.88	.04	.04	1	1
LS86 14+50E	1	23	8	48	.1	12	9	442	4.58	2	5	ND	1	16	1	2	2	111	.26	.043	5	27	.52	84	.09	2	2.06	.03	.03	11	1
LS86 15+00E	1	61	9	60	.1	15	10	334	4.78	6	5	ND	1	11	1	2	2	102	.21	.046	4	29	.64	57	.06	2	2.26	.03	.02	1	1
LS86 15+50E	1	54	10	50	.2	26	10	193	4.62	2	5	ND	2	13	1	2	2	114	.25	.027	5	47	.41	56	.18	2	3.24	.03	.02	1	2
LS86 16+00E	1	31	8	58	.1	38	16	1025	4.21	2	5	ND	2	18	1	2	2	91	.48	.038	7	43	.33	82	.23	2	2.80	.04	.03	1	1
LS86 16+50E	1	10	8	22	.1	7	3	93	2.88	2	5	ND	1	14	1	2	3	87	.24	.015	4	22	.14	27	.13	2	1.19	.02	.02	4	2
LS86 17+00E	1	22	10	47	.1	20	8	316	2.95	6	5	ND	1	14	1	2	2	73	.26	.040	4	27	.33	49	.19	2	2.78	.03	.03	10	1
LS86 17+50E	1	40	5	51	.1	20	8	422	3.53	3	5	ND	1	13	1	2	2	93	.27	.061	5	39	.39	38	.21	2	2.53	.03	.03	1	2
LS86 18+00E	1	31	10	48	.1	14	8	331	4.17	2	5	ND	2	11	1	2	2	111	.25	.093	4	34	.29	35	.21	2	2.84	.03	.03	10	2
LS86 18+50E	1	16	11	93	.1	17	14	834	3.94	2	5	ND	1	11	1	2	2	81	.29	.124	5	25	.30	51	.15	2	2.03	.03	.03	1	1
LS86 19+00E	1	22	6	66	.1	18	7	264	4.42	2	5	ND	1	12	1	2	2	115	.22	.092	4	40	.29	43	.19	2	2.76	.03	.02	1	1
LS86 19+50E	2	45	4	70	.1	19	8	333	4.09	5	5	ND	2	11	1	2	2	90	.24	.161	4	46	.42	31	.22	2	3.87	.03	.02	1	1
LS86 20+00E	1	38	5	66	.2	25	9	278	4.85	3	5	ND	2	14	1	2	2	106	.28	.204	4	49	.53	34	.30	2	3.54	.04	.03	1	1
LS86 20+50E	2	36	10	66	.1	58	17	327	5.18	5	5	ND	1	31	1	2	2	138	.39	.072	4	90	1.04	33	.59	2	2.64	.04	.03	1	1
STD C/AU-S	21	57	39	135	7.1	69	28	1003	3.95	37	20	7	33	47	18	16	19	63	.47	.102	35	57	.88	177	.08	36	1.72	.09	.13	13	50

Lacy Klock 57
IA

ASHWORTH EXPLORATION PROJECT - LACY STORES FILE# 86-4052

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Ti	B	Al	Na	K	M	Au11
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
LSB6 01 A	2	38	16	119	.2	31	6	271	15.77	6	5	ND	4	8	2	4	2	93	.26	.086	10	40	.88	12	.02	19	2.04	.05	.02	2	5
LSB6 01 B	2	9	13	36	.1	19	4	117	3.18	7	5	ND	2	71	1	2	2	47	.87	.269	4	15	.31	22	.04	2	.87	.04	.04	1	8
LSB6 02	1	5	11	26	.2	3	6	178	1.67	2	5	ND	5	32	1	2	2	6	.64	.050	16	3	.18	71	.05	7	.44	.06	.14	1	5
LSB6 03	2	11	4	27	.1	14	6	117	2.69	2	5	ND	2	10	1	2	2	13	.13	.047	11	11	.58	95	.02	4	.85	.03	.14	1	4
LSB6 04	1	57	8	49	.1	22	15	718	4.02	2	5	ND	3	34	1	2	2	43	2.24	.129	3	12	1.89	74	.01	2	2.11	.08	.13	5	1
LSB6 05	1	5	2	18	.1	8	5	341	1.54	2	5	ND	1	6	1	2	2	54	.14	.014	2	10	.42	24	.03	4	.57	.02	.05	1	2
LSB6 06	2	73	8	69	.3	12	11	837	4.55	6	5	ND	2	11	1	2	2	50	.49	.043	4	13	1.40	70	.21	2	1.99	.06	.10	3	2
LSB6 07	1	66	8	59	.2	20	17	1315	4.74	3	5	ND	7	233	1	5	4	79	11.54	.038	5	69	3.40	34	.01	2	2.00	.09	.08	3	1
LSB6 08	1	2	9	93	.1	57	16	291	6.39	2	5	ND	4	44	1	2	2	132	3.45	.119	7	21	.76	121	.02	9	.56	.08	.18	1	2
LSB6 09	29	38	30	141	.5	4	8	1244	10.34	442	5	ND	2	9	2	3	2	52	.92	.094	5	2	1.05	23	.19	12	2.02	.05	.28	3	86
LSB6 10	1	114	3	94	.1	55	25	957	5.88	34	5	ND	5	87	1	30	2	92	5.02	.080	4	50	1.49	33	.01	7	.50	.06	.11	1	6
LSB6 11	1	19	3	75	.1	15	9	235	2.08	36	5	ND	5	65	1	2	2	15	5.39	.019	4	7	.51	13	.01	8	.30	.07	.11	1	4
LSB6 12	2	82	17	90	.3	28	28	534	8.84	7	5	ND	2	19	1	2	2	51	.90	.107	5	11	.82	50	.01	5	1.70	.08	.12	2	11
LSB6 13	2	76	17	57	.3	38	20	1034	6.29	10	5	ND	5	55	1	2	2	37	5.78	.098	2	14	1.00	27	.01	2	1.18	.11	.11	2	1
LSB6 14	7	409	24	101	.8	14	15	1253	17.76	376	5	ND	2	4	2	9	5	168	.12	.077	4	53	3.39	13	.01	21	3.89	.06	.12	5	395
LSB6 15	1	20	3	19	.1	4	32	189	6.11	2	5	ND	1	3	1	2	2	26	.10	.058	2	2	.61	33	.01	2	.73	.03	.11	2	81
LSB6 16	1	1993	5	62	.2	7	13	628	3.82	2	5	ND	1	31	1	2	2	94	.75	.083	3	2	1.67	19	.13	2	1.77	.06	.07	1	25
LSB6 17	13	21	15	13	.7	10	109	233	19.52	6	5	5	1	17	2	5	2	32	.18	.041	3	1	.63	9	.06	20	.71	.05	.11	2	6320
LSB6 18	4	39	5	65	.1	8	27	745	7.31	3	5	ND	3	51	2	3	2	118	2.17	.155	5	9	2.09	38	.24	2	2.20	.09	.14	4	38
LSB6 50	1	7	4	44	.1	3	18	619	5.87	67	5	ND	1	15	1	2	3	44	.36	.152	6	1	.87	39	.04	2	1.57	.05	.16	1	55
LSB6 51	1	13	2	11	.1	1	2	362	1.01	2	5	ND	1	25	1	2	2	21	.39	.037	2	1	.10	24	.06	5	.50	.02	.11	1	1
LSB6 52	1	3	2	8	.1	4	1	235	.68	2	5	ND	1	4	1	2	2	11	.20	.004	2	7	.11	6	.01	6	.20	.01	.03	1	8
LSB6 53	1	8	5	51	.1	12	12	657	2.53	5	5	ND	1	78	1	2	2	53	1.12	.041	4	31	1.37	58	.18	4	1.56	.06	.01	1	1
LSB6 54	1	45	8	167	.1	113	34	872	6.83	5	5	ND	1	22	1	2	2	89	1.05	.116	6	128	3.76	125	.49	2	3.84	.06	.17	1	2
LSB6 55	1	30	6	85	.1	1	14	920	5.74	2	5	ND	3	77	1	2	2	122	1.62	.211	11	3	1.63	13	.39	2	2.39	.08	.03	1	1
LSB6 57	1	35	6	77	.7	28	4	135	2.84	17	5	ND	1	2	1	2	2	28	.05	.024	3	21	1.03	34	.01	3	1.20	.02	.09	1	4
LSB6 58	1	27	4	27	.1	3	5	433	1.93	2	5	ND	1	113	1	2	2	43	.71	.016	2	1	.74	36	.09	9	1.32	.06	.07	1	1
LSB6 60	5	36	3	82	.1	3	12	685	4.69	5	5	ND	2	69	1	2	2	69	1.46	.182	12	1	1.18	65	.14	2	2.14	.07	.16	1	8
LSB6 61 A	1	73	6	91	.1	44	29	942	6.83	9	5	ND	1	37	1	2	2	156	1.31	.183	8	46	3.13	39	.74	3	3.13	.08	.02	1	2
LSB6 61 B	1	47	6	89	.1	42	28	862	6.42	10	5	ND	1	35	1	2	2	127	1.22	.168	7	30	2.93	21	.60	2	2.90	.07	.03	1	1
LSB6 62	1	1217	6	79	.2	28	10	371	8.24	3	5	ND	2	32	1	2	2	106	1.92	.821	8	46	1.39	758	.02	2	2.33	.05	.01	1	16
LSB6 63	1	6	8	106	.1	28	9	267	6.73	6	5	ND	3	52	1	2	2	42	3.03	.260	9	34	.84	90	.04	14	.59	.08	.20	1	1
LSB6 64	1	49	3	35	.1	6	7	307	2.11	2	5	ND	2	21	1	2	3	21	.69	.077	16	7	.76	69	.03	2	.91	.07	.06	1	1
LSB6 65	2	600	28	984	.3	11	24	2166	6.61	8	5	ND	1	13	3	2	2	85	.93	.107	5	4	2.61	108	.01	2	3.01	.05	.22	1	1
LSB6 66	1	17	2	22	.1	2	1	779	1.29	14	5	ND	1	1	1	2	2	14	.04	.010	2	1	.24	21	.01	4	.39	.02	.03	2	1
LSB6 67	1	39	19	443	.7	191	42	900	8.22	2	5	ND	1	13	2	2	2	61	.47	.141	5	114	2.74	40	.03	4	3.65	.04	.14	1	1
LSB6 68	2	1585	58	2818	4.1	7	30	1135	15.95	468	5	ND	1	2	10	7	2	63	.29	.075	3	6	1.89	6	.01	19	2.10	.05	.16	1	430
STD C/AU-S	20	57	40	133	7.1	69	28	1028	3.93	38	18	7	33	47	17	15	21	64	.48	.105	36	57	.88	182	.09	37	1.72	.09	.13	13	505

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1007 N
Rocks
1 E

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK CHIPS AU88 ANALYSIS BY FA+AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JAN 14 1987 DATE REPORT MAILED: Jan 22/87 ASSAYER: D. Toy... DEAN TOYE. CERTIFIED B.C. ASSAYER.

ASHWORTH EXPLORATION FILE # 87-0066

PAGE 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Pi	V	Ca	P	La	Cr	Mo	Ba	Ti	B	Al	Na	K	W	Au88
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
LS-86-19	1	7	5	50	.1	38	7	669	2.79	2	5	ND	1	13	1	2	2	11	.34	.022	5	7	.50	220	.01	6	.54	.02	.09	1	3
LS-86-20	1	64	6	32	.9	7	60	333	13.62	9	5	13	2	17	1	2	2	73	.39	.154	3	3	.89	37	.25	3	1.30	.01	.25	2	14900
LS-86-21	1	93	4	81	.1	11	24	967	5.95	6	5	ND	1	60	1	2	2	157	1.10	.119	5	10	2.62	65	.26	6	2.87	.03	.10	1	29
LS-86-22	1	201	4	100	.1	17	22	1266	5.32	20	5	ND	1	10	1	61	2	78	.50	.184	4	23	.09	72	.01	9	.80	.01	.16	1	54
LS-86-23	18	77	6	58	.2	5	24	1047	4.88	4	5	ND	4	48	1	131	2	96	5.43	.151	5	5	1.70	31	.16	9	1.91	.03	.12	1	87
LS-86-24	1	20	5	47	.2	51	17	888	3.87	19	5	ND	6	260	1	2	4	72	13.18	.036	3	119	2.85	79	.01	3	1.05	.01	.09	1	6
LS-86-25	3	42	7	59	.4	9	45	637	9.57	8	5	5	1	37	1	14	2	122	.63	.154	5	6	1.90	35	.24	4	2.02	.03	.13	1	4750
LS-86-26	1	16	9	80	.1	1	14	686	8.18	170	5	ND	1	17	1	2	2	10	.75	.217	9	2	1.34	58	.01	5	2.30	.03	.08	1	17
LS-86-30	2	11	10	34	.1	80	16	4981	2.00	3	5	ND	1	16	1	44	2	17	.14	.029	10	3	.20	146	.03	4	.29	.01	.07	1	22
LS-86-31	1	6	6	23	.1	24	6	328	1.38	2	5	ND	1	4	1	3	2	11	.20	.027	9	8	.16	40	.01	2	.29	.01	.08	1	1
LS-86-32	9	16	35	53	.4	7	6	88	4.57	48	5	ND	4	3	1	6	2	3	.04	.031	57	2	.46	24	.01	5	.79	.01	.16	1	4
LS-86-69	1	30	16	63	.1	15	10	327	3.68	6	5	ND	1	17	1	2	2	25	.34	.063	6	14	.98	41	.12	4	1.02	.03	.09	1	20
LS-86-70	1	35	10	73	.2	13	10	519	3.57	21	5	ND	2	52	1	8	2	28	1.16	.078	16	10	1.03	99	.01	9	.84	.03	.17	1	3
LS-86-71	2	17	9	17	.3	7	5	53	2.53	7	5	ND	1	7	1	5	2	36	.60	.157	20	17	.15	13	.39	2	.29	.07	.04	1	2
LS-86-72	1	8	10	136	.1	40	13	903	4.62	9	5	ND	1	17	1	2	2	48	.58	.174	6	26	2.08	74	.20	5	1.51	.03	.17	1	3
LS-86-73	1	7	2	73	.1	18	15	820	4.17	12	6	ND	2	43	1	2	2	76	2.90	.089	6	28	2.37	167	.01	5	2.12	.03	.11	1	1
STD C/AU-R	19	58	35	128	6.9	65	27	961	3.97	39	19	8	32	46	16	17	20	61	.48	.100	34	55	.88	177	.08	38	1.72	.06	.14	12	505

Loay S... UK IB

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-MND3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SN, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM. SAMPLE TYPE: SOILS - BOMESH AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JAN 14 1987 DATE REPORT MAILED: Jan 16/87 ASSAYER: N. Jeps. DEAN TOYE, CERTIFIED B.C. ASSAYER.

ASHWORTH EXPLORATION FILE # 87-0067

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Table with columns: SAMPLE#, Mo, Cu, Pb, Zn, As, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mo, Ba, Ti, B, Al, Na, K, W, Au. Rows list various sample IDs like LS-86 57N 1+00E and their corresponding element concentrations in PPM.

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
LS-86 54N-B 9+00E	1	30	7	80	.1	18	10	701	5.29	9	5	ND	1	12	1	2	2	143	.24	.098	4	48	.31	49	.27	3	2.12	.01	.01	1	1
LS-86 54N-B 9+50E	1	65	8	88	.2	31	19	612	6.39	15	5	ND	1	21	1	10	2	162	.30	.045	9	43	.84	184	.15	2	3.56	.01	.04	1	1
LS-86 54N-B 10+00E	1	44	9	98	.1	20	15	912	5.61	15	5	ND	1	15	1	36	2	145	.25	.074	4	28	.62	120	.08	4	3.22	.01	.03	1	1
LS-86 54N-B 10+50E	1	18	7	56	.1	7	7	598	4.33	2	5	ND	1	13	1	2	2	114	.19	.059	5	25	.11	57	.19	2	1.30	.01	.01	1	2
LS-86 54N-B 11+00E	1	54	13	111	.1	32	20	900	6.31	20	5	ND	1	11	1	36	2	163	.29	.054	9	53	.62	76	.30	3	3.09	.01	.03	1	1
LS-86 54N-B 11+50E	1	81	16	128	.1	40	22	765	6.47	13	5	ND	1	13	1	2	2	172	.35	.082	7	66	.63	83	.36	5	3.55	.01	.04	1	1
LS-86 54N-B 12+00E	3	70	17	90	.2	22	16	836	9.49	9	5	ND	1	30	1	9	2	304	.57	.078	4	55	.64	65	.80	2	2.53	.01	.03	1	8
LS-86 54N-B 12+50E	1	92	16	65	.1	36	13	218	6.47	9	5	ND	1	14	1	2	2	183	.28	.052	3	63	.55	35	.37	2	4.42	.01	.03	1	1
LS-86 54N-B 13+00E	1	53	7	95	.1	23	19	1764	7.78	2	5	ND	1	61	1	27	2	261	.66	.067	4	60	.60	65	.70	2	2.63	.01	.03	1	2
LS-86 54N-B 13+50E	1	70	15	86	.1	22	14	785	7.56	6	5	ND	2	19	1	9	2	220	.32	.137	4	55	.38	45	.48	2	2.96	.01	.02	1	1
LS-86 54N-B 14+00E	1	80	9	78	.1	27	14	528	5.67	3	5	ND	1	11	1	2	2	152	.30	.199	4	47	.39	37	.35	4	3.78	.01	.02	1	1
LS-86 54N-B 14+50E	1	69	15	97	.1	27	18	919	9.42	3	5	ND	1	13	1	2	4	253	.37	.096	4	55	.40	74	.61	2	3.17	.01	.04	1	1
LS-86 54N-B 15+00E	2	91	20	204	.3	29	44	7876	7.85	7	5	ND	1	23	1	20	2	206	.84	.082	7	62	.43	250	.61	2	2.33	.01	.03	1	1
LS-86 51N 0+00E	1	88	8	97	.1	49	21	1205	5.82	12	5	ND	1	14	1	7	2	162	.59	.058	7	65	.74	159	.38	4	3.60	.01	.03	1	1
LS-86 51N 0+50E	2	115	12	101	.1	65	22	833	6.05	25	5	ND	1	10	1	8	2	146	.45	.110	6	80	1.45	198	.25	8	3.43	.01	.06	1	1
LS-86 51N 1+00E	3	81	21	282	.4	59	27	10467	4.65	21	5	ND	1	48	2	16	2	83	1.66	.122	12	54	.62	643	.20	4	3.14	.02	.05	1	1
LS-86 51N 1+50E	1	73	19	135	.1	106	20	646	6.55	9	5	ND	1	10	1	2	3	119	.38	.075	38	105	2.01	186	.05	6	4.28	.01	.10	1	1
LS-86 51N 2+00E	1	40	12	90	.1	275	35	788	6.05	17	5	ND	1	6	1	21	2	65	.15	.054	5	317	1.54	110	.03	2	3.28	.01	.09	1	4
LS-86 51N 2+50E	1	35	7	88	.3	40	11	869	3.19	9	5	ND	1	10	1	2	2	82	.27	.065	5	55	.52	54	.18	4	2.01	.01	.03	1	1
LS-86 51N 3+00E	1	27	10	108	.1	28	12	1602	3.67	13	5	ND	1	10	1	2	2	89	.34	.137	5	44	.46	50	.23	2	1.95	.01	.02	1	1
LS-86 51N 3+50E	3	47	18	160	.4	45	15	1031	3.71	34	5	ND	1	7	1	2	2	59	.22	.071	34	43	.94	32	.08	2	1.98	.01	.04	1	1
LS-86 51N 4+00E	3	36	12	86	.4	25	11	305	4.15	8	5	ND	1	16	1	2	2	108	.32	.054	7	38	.49	38	.24	2	2.43	.01	.04	1	1
LS-86 51N 4+50E	1	23	12	111	.2	6	17	1514	6.94	2	5	ND	1	19	1	2	2	85	.30	.135	11	17	.65	49	.41	3	1.90	.01	.03	1	3
LS-86 51N 5+00E	2	34	14	118	.1	16	18	1519	6.44	7	5	ND	1	14	1	36	2	85	.30	.124	9	30	.91	49	.36	2	3.12	.01	.04	1	1
LS-86 51N 5+50E	1	86	12	114	.3	52	22	558	4.91	12	5	ND	1	13	1	30	2	127	.38	.080	7	61	.94	54	.31	5	3.25	.01	.03	1	1
LS-86 51N 6+00E	1	59	8	91	.1	44	14	225	3.58	11	5	ND	1	9	1	2	2	90	.24	.043	5	42	.57	43	.20	3	2.59	.01	.02	1	1
LS-86 51N 6+50E	1	67	12	90	.1	44	14	487	4.00	14	5	ND	1	13	1	2	3	106	.34	.041	6	50	.68	75	.19	5	2.76	.01	.03	1	1
LS-86 51N 7+00E	1	17	4	137	.2	26	9	539	3.05	15	5	ND	1	8	1	2	2	61	.25	.147	3	24	.17	45	.07	2	1.68	.01	.02	1	1
LS-86 51N 7+50E	1	34	5	111	.1	29	12	467	4.00	13	5	ND	1	11	1	2	2	102	.33	.073	3	44	.44	42	.17	2	2.29	.01	.02	1	1
LS-86 51N 8+00E	2	7	6	41	.1	10	5	304	1.60	16	5	ND	1	5	1	3	2	35	.11	.019	2	16	.09	94	.01	2	.84	.01	.01	1	2
LS-86 51N 8+50E	1	65	5	49	.1	17	10	270	4.34	3	5	ND	1	9	1	2	2	141	.18	.031	12	52	.56	243	.07	5	1.92	.01	.03	1	3
LS-86 51N 9+00E	1	19	6	57	.1	15	11	449	4.06	3	5	ND	1	36	1	2	2	118	.44	.030	5	43	.32	128	.27	2	1.34	.01	.02	1	1
LS-86 51N 9+50E	3	12	58	57	.2	8	9	8155	2.33	2	5	ND	1	47	1	2	2	81	.78	.085	6	16	.16	239	.24	3	.95	.01	.06	1	1
LS-86 51N 10+00E	1	62	21	129	.2	20	21	4538	5.20	5	5	ND	1	34	1	2	2	138	.38	.092	10	53	.90	641	.17	2	2.64	.01	.06	1	1
LS-86 51N 10+50E	1	240	10	116	.1	23	15	504	5.30	20	5	ND	1	3	1	96	2	77	.05	.069	16	31	.18	121	.01	4	1.55	.01	.07	1	10
LS-86 51N 11+00E	1	24	11	66	.1	11	10	1561	3.76	3	5	ND	1	16	1	2	2	107	.27	.039	5	30	.25	77	.23	2	1.48	.01	.03	1	1
STD C/AU-S	21	61	37	133	7.1	68	28	995	3.95	37	22	8	34	49	17	15	19	63	.48	.100	35	56	.98	182	.98	37	1.71	.06	.15	14	52

ASHWORTH EXPLORATION FILE # 87-0067

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	F	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
LS-86 51N 11+50E	1	23	11	72	.1	13	9	1293	3.97	2	5	ND	1	15	1	2	2	104	.27	.043	4	29	.42	67	.22	2	1.65	.01	.03	1	1
LS-86 51N 12+00E	1	17	14	87	.1	12	10	2575	5.40	3	5	ND	1	12	1	2	2	115	.29	.093	5	35	.23	90	.26	2	1.82	.01	.03	1	1
LS-86 51N 12+50E	2	39	12	124	.1	21	29	2051	7.16	13	5	ND	1	20	1	2	2	208	.48	.131	5	47	1.76	287	.07	7	4.26	.01	.09	1	2
LS-86 51N 13+00E	1	21	6	80	.1	11	20	1396	4.95	2	5	ND	1	11	1	2	3	141	.20	.069	6	24	.75	155	.06	5	2.47	.01	.04	1	1
LS-86 51N 13+50E	3	31	8	82	.1	19	16	1040	5.52	21	5	ND	1	9	1	2	2	124	.24	.066	7	22	.39	103	.04	4	1.85	.01	.04	1	1
LS-86 51N 14+00E	1	47	5	145	.1	25	10	341	3.83	10	5	ND	1	7	1	7	2	87	.24	.074	3	33	.35	85	.05	3	2.63	.01	.04	1	1
LS-86 48N 0+00E	1	56	7	96	.3	53	17	1222	5.15	11	5	ND	1	11	1	27	2	123	.32	.089	5	82	.64	116	.22	4	3.18	.01	.05	1	1
LS-86 48N 0+50E	2	60	14	165	.1	96	24	1944	6.01	11	5	ND	1	17	1	2	4	100	.52	.060	19	81	.81	194	.23	3	4.84	.02	.06	1	1
LS-86 48N 1+00E	1	37	17	127	.1	85	24	1363	6.87	31	5	ND	1	7	1	11	2	47	.16	.065	11	81	.96	246	.01	5	3.15	.01	.09	1	1
LS-86 48N 1+50E	2	34	6	150	.2	39	13	884	3.21	13	5	ND	1	11	1	2	3	83	.26	.043	6	41	.96	68	.14	2	2.34	.01	.03	1	1
LS-86 48N 2+00E	2	42	12	264	.3	118	37	2418	6.20	22	5	ND	1	11	1	2	2	161	.27	.066	7	210	2.78	91	.11	8	3.67	.01	.04	1	1
LS-86 48N 2+50E	1	16	9	66	.2	9	12	797	4.94	4	5	ND	1	18	1	2	2	144	.26	.067	5	33	.41	41	.25	2	1.55	.01	.02	1	1
LS-86 48N 3+00E	1	36	13	87	.1	21	15	506	8.18	8	5	ND	1	15	1	7	3	219	.31	.094	6	56	.40	55	.34	2	2.81	.01	.02	1	2
LS-86 48N 3+50E	2	21	2	108	.1	31	10	159	2.96	19	5	ND	1	5	1	2	2	65	.16	.045	3	29	.20	42	.04	3	2.11	.01	.02	1	1
LS-86 48N 4+00E	1	28	8	80	.1	24	11	251	3.54	16	5	ND	1	9	1	2	2	84	.29	.058	3	35	.34	47	.07	5	2.17	.01	.02	1	2
LS-86 48N 4+50E	1	34	8	92	.1	29	14	448	5.35	7	5	ND	1	11	1	2	2	151	.40	.046	3	45	.32	53	.28	3	2.80	.01	.02	1	1
LS-86 48N 5+50E	1	59	10	150	.1	53	16	540	4.78	17	5	ND	1	11	1	28	2	119	.39	.039	9	48	.40	60	.21	5	3.32	.01	.02	1	1
LS-86 48N 6+00E	2	1	6	247	.1	32	5	450	1.06	10	5	ND	1	4	1	2	2	10	.15	.043	7	6	.85	35	.01	2	.81	.01	.01	1	1
LS-86 48N 6+50E	1	28	6	128	.1	44	11	344	3.32	9	5	ND	1	9	1	2	2	74	.32	.040	8	31	.30	51	.12	4	2.37	.01	.02	1	1
LS-86 48N 7+00E	1	17	8	78	.1	19	5	244	2.38	9	5	ND	1	6	1	2	2	50	.15	.050	2	18	.13	27	.07	2	1.27	.01	.01	1	4
LS-86 48N 7+50E	1	3	4	30	.3	6	2	87	1.02	7	5	ND	1	6	1	2	2	34	.13	.015	2	8	.06	23	.02	3	.88	.01	.02	2	1
LS-86 48N 8+00E	1	9	3	114	.1	18	7	226	2.07	12	5	ND	1	5	1	2	2	40	.09	.032	8	18	.40	52	.01	6	1.57	.01	.02	1	1
LS-86 48N 8+50E	1	69	21	182	.1	46	23	1423	4.99	11	5	ND	1	12	1	26	2	114	.40	.209	5	46	.45	137	.26	6	3.20	.01	.04	1	1
LS-86 48N 9+00E	1	16	13	69	.2	8	8	1640	5.16	3	5	ND	1	22	1	2	2	114	.39	.093	5	32	.12	57	.28	3	1.41	.01	.02	1	8
LS-86 48N 9+50E	1	29	7	141	.1	19	16	1150	6.44	7	5	ND	1	12	1	2	2	160	.32	.072	4	42	.19	106	.35	2	2.14	.01	.02	1	1
LS-86 48N 10+00E	1	11	15	57	.1	4	11	2018	3.65	2	5	ND	1	67	1	2	2	85	.36	.052	7	19	.09	92	.26	2	.99	.01	.02	1	1
LS-86 48N 10+50E	1	15	9	64	.1	13	9	586	4.01	3	5	ND	1	13	1	2	2	117	.29	.052	4	35	.28	90	.21	2	1.47	.01	.03	2	1
LS-86 48N 11+00E	1	10	8	147	.1	84	29	1785	5.04	2	5	ND	1	7	1	2	2	43	.49	.024	5	93	.97	286	.45	7	1.92	.01	.22	1	2
LS-86 48N 11+50E	1	22	20	90	.1	18	15	1675	5.08	9	5	ND	1	17	1	2	2	149	.48	.063	9	52	.30	260	.29	4	1.63	.01	.05	1	1
LS-86 48N 12+00E	1	75	5	65	.1	38	17	401	4.83	7	7	ND	1	13	1	14	2	137	.47	.046	5	52	.61	121	.32	9	3.26	.01	.03	1	1
LS-86 48N 12+50E	1	13	8	31	.1	17	6	128	5.87	2	5	ND	1	18	1	2	2	112	.25	.013	8	65	.44	75	.37	2	.94	.01	.04	1	1
LS-86 45N 0+00E	1	66	13	96	.1	62	22	670	6.21	9	5	ND	1	12	1	2	2	157	.44	.054	8	81	.78	92	.33	2	3.90	.01	.05	1	2
LS-86 45N 0+50E	3	186	14	152	.3	35	37	841	10.05	12	5	ND	2	11	1	2	9	230	.27	.123	17	42	.78	120	.02	5	6.37	.01	.06	1	1
LS-86 45N 1+00E	1	1	2	20	.3	4	2	180	.68	3	5	ND	1	4	1	2	2	24	.09	.014	5	8	.05	14	.03	2	.43	.01	.01	1	1
LS-86 45N 1+50E	1	34	13	96	.2	28	12	401	5.55	9	5	ND	1	10	1	2	2	142	.27	.040	6	71	.50	48	.18	7	2.52	.01	.04	1	1
LS-86 45N 2+50E	1	25	7	44	.2	15	7	167	3.70	6	5	ND	1	11	1	2	2	112	.30	.016	4	34	.26	30	.23	4	1.55	.01	.02	2	1
STD C/AU-S	21	61	39	133	6.9	69	29	989	3.95	38	17	8	32	47	17	15	18	62	.48	.097	35	57	.88	183	.09	37	1.71	.06	.15	13	50

ASHWORTH EXPLORATION FILE # 87-0067

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS-86 45N 3+00E	1	68	9	103	.2	36	17	703	5.80	15	6	ND	1	12	1	36	2	167	.44	.057	5	55	.53	67	.39	5	3.25	.01	.03	1	1
LS-86 45N 3+50E	1	31	10	89	.1	23	11	308	3.60	8	5	ND	1	9	1	2	2	92	.21	.057	4	31	.46	53	.15	2	2.22	.01	.01	1	1
LS-86 45N 4+00E	2	20	11	145	.3	28	12	958	4.01	29	10	ND	1	6	1	3	2	64	.22	.069	7	25	.21	85	.01	2	2.30	.01	.04	1	1
LS-86 45N 4+50E	1	71	14	97	.1	37	16	413	5.91	16	5	ND	2	10	1	29	2	151	.47	.060	12	56	.63	60	.21	2	3.18	.01	.04	1	2
LS-86 45N 5+00E	1	109	15	89	.2	36	21	896	4.89	14	8	ND	1	21	1	2	2	135	.74	.144	7	48	.87	42	.29	2	4.24	.07	.04	2	5
LS-86 45N 5+50E	1	49	7	119	.1	26	16	503	6.47	18	5	ND	1	12	1	15	2	186	.41	.081	3	50	.39	53	.39	3	2.58	.01	.02	1	2
LS-86 45N 6+00E	1	75	10	114	.1	36	15	725	4.44	13	5	ND	1	20	1	2	2	115	.77	.059	8	51	.45	77	.20	5	2.87	.01	.02	1	8
LS-86 45N 6+50E	1	90	8	90	.3	46	17	420	4.83	19	5	ND	1	12	1	36	2	127	.42	.031	7	68	.71	104	.25	5	3.46	.01	.03	1	2
LS-86 45N 7+00E	2	11	3	66	.1	20	5	419	1.19	7	5	ND	1	3	1	2	2	23	.11	.028	4	9	.05	24	.02	2	.67	.01	.02	1	1
LS-86 45N 7+50E	2	29	13	117	.3	35	12	3237	2.93	37	5	ND	1	15	1	5	2	61	.51	.095	10	39	.15	110	.02	5	1.68	.01	.06	1	1
LS-86 45N 8+00E	1	58	17	96	.1	565	57	670	10.14	1169	5	ND	1	6	1	54	5	155	.86	.057	5	820	.10	31	.01	4	1.41	.01	.01	3	4
LS-86 45N 9+00E	1	41	14	63	.1	21	10	278	5.12	11	5	ND	1	13	1	27	2	149	.29	.067	3	54	.38	56	.30	2	3.58	.01	.03	2	3
LS-86 45N 9+50E	1	56	16	80	.1	21	13	294	6.30	9	5	ND	1	23	1	9	2	168	.34	.094	4	51	.45	59	.34	4	3.48	.01	.03	1	1
LS-86 45N 10+00E	1	28	7	93	.1	17	16	818	5.64	6	5	ND	1	29	1	2	2	164	.34	.070	6	42	1.13	180	.17	2	2.82	.01	.05	1	1
LS-86 45N 10+50E	1	22	10	91	.1	35	18	2119	5.07	7	5	ND	1	68	1	25	2	122	1.47	.057	4	95	2.59	167	.28	9	3.76	.01	.11	1	4
LS-86 45N 11+00E	1	38	11	91	.1	22	16	357	6.58	4	5	ND	1	11	1	29	2	187	.27	.039	8	65	.48	107	.18	2	2.97	.01	.05	1	1
LS-86 45N 11+50E	1	24	9	70	.3	17	10	275	4.94	6	5	ND	1	17	1	2	2	163	.38	.043	4	49	.49	77	.29	5	2.08	.01	.03	1	1
LS-86 45N 12+00E	1	37	11	139	.1	71	28	1783	6.09	4	5	ND	1	14	1	2	2	100	.52	.062	6	97	1.47	239	.46	4	2.77	.01	.31	1	2
LS-86 45N 12+50E	1	28	9	92	.1	73	27	1276	6.07	4	5	ND	1	27	1	26	2	105	.73	.071	10	148	3.41	193	.59	5	3.06	.01	.17	1	3
LS-86 45N 13+00E	1	59	9	71	.3	41	16	299	5.19	15	5	ND	1	13	1	28	2	138	.35	.056	6	68	.77	105	.27	5	3.26	.01	.03	1	1
LS-86 45N 13+50E	1	72	9	80	.1	38	15	657	4.84	12	5	ND	1	13	1	2	2	128	.31	.080	4	61	.77	72	.26	8	2.97	.01	.04	1	1
LS-86 45N 14+00E	1	16	4	49	.1	19	8	203	5.00	2	5	ND	1	25	1	2	2	113	.27	.038	6	63	.64	62	.35	5	1.39	.01	.02	1	1
LS-86 45N 14+50E	1	37	9	49	.1	29	12	187	5.70	2	5	ND	1	13	1	2	2	161	.25	.022	5	76	.78	54	.28	6	2.73	.01	.02	1	1
LS-86 45N 15+00E	1	42	7	61	.3	60	18	548	5.16	4	5	ND	1	15	1	2	2	142	.54	.040	9	118	2.17	162	.49	3	2.88	.01	.07	1	1
LS-86 42N 0+00E	1	25	7	115	.2	67	26	4014	6.39	7	5	ND	1	10	1	5	2	160	.38	.071	7	200	1.85	78	.60	5	2.69	.01	.09	1	3
LS-86 42N 0+50E	1	50	9	108	.2	30	14	672	4.56	8	5	ND	1	29	1	2	2	101	1.27	.050	6	62	.45	67	.30	7	3.14	.02	.02	1	2
LS-86 42N 1+00E	1	158	10	91	.3	39	21	1606	5.51	14	5	ND	1	15	1	34	2	142	.40	.059	8	55	.74	82	.25	3	3.43	.01	.03	1	1
LS-86 42N 1+50E	1	79	13	80	.2	30	16	396	6.35	10	5	ND	1	15	1	27	2	174	.35	.057	4	52	.46	74	.33	4	2.95	.01	.04	1	8
LS-86 42N 2+00E	1	47	12	96	.1	35	14	1143	3.21	16	5	ND	1	11	1	2	2	60	.36	.024	16	26	.55	46	.09	6	1.92	.01	.02	1	3
LS-86 42N 2+50E	1	77	8	119	.4	38	16	1470	5.24	11	5	ND	1	14	1	21	2	141	.34	.050	4	49	.52	75	.31	4	3.21	.01	.03	1	2
LS-86 42N 3+00E	1	37	9	140	.1	41	16	393	5.45	20	5	ND	1	10	1	2	2	128	.31	.064	4	49	.50	58	.12	6	3.81	.01	.03	1	4
LS-86 42N 3+50E	1	24	19	102	.1	25	10	315	2.63	7	5	ND	1	7	1	2	2	58	.18	.034	7	22	.38	44	.06	2	1.88	.01	.02	1	1
LS-86 42N 4+00E	3	13	6	101	.1	16	9	694	3.88	15	5	ND	1	10	1	2	2	85	.36	.104	4	27	.17	52	.08	3	1.50	.01	.02	1	1
LS-86 42N 4+50E	1	25	9	188	.1	48	13	650	2.59	6	5	ND	1	7	1	2	2	54	.32	.154	5	23	.24	32	.09	2	1.53	.01	.02	1	1
LS-86 42N 5+00E	3	12	8	90	.1	14	7	539	2.13	8	5	ND	1	5	1	2	2	48	.14	.073	3	21	.11	20	.08	2	1.12	.01	.01	1	1
LS-86 42N 5+50E	3	6	4	76	.2	23	4	517	1.27	11	5	ND	1	3	1	2	2	14	.08	.029	7	11	.04	37	.01	2	.50	.01	.02	1	2
LS-86 42N 6+00E	1	53	2	134	.2	31	14	1575	5.20	10	5	ND	1	11	1	2	2	146	.35	.089	6	46	.35	58	.32	2	2.96	.01	.02	1	51
STD C/AU-S	20	60	36	133	7.0	65	27	987	3.94	37	20	8	33	48	16	15	21	62	.48	.098	35	57	.88	182	.09	36	1.71	.06	.15	13	48

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
LS-86 42N 6+25E	1	74	2	120	.4	41	18	587	5.44	19	5	ND	1	12	1	28	2	137	.40	.102	15	52	.53	45	.23	5	3.54	.01	.02	1	1
LS-86 42N 6+50E	1	27	7	103	.1	28	12	330	3.63	16	5	ND	2	8	1	2	2	86	.21	.056	10	33	.20	32	.17	2	2.26	.01	.02	1	1
LS-86 42N 6+75E	1	67	2	84	.1	40	13	482	5.10	23	5	ND	2	12	1	2	2	124	.28	.050	10	71	.73	106	.13	5	3.05	.01	.03	1	1
LS-86 42N 7+00E	1	62	6	94	.1	30	15	696	4.52	15	5	ND	1	10	1	2	2	117	.35	.086	11	44	.45	46	.19	7	2.56	.01	.02	1	1
LS-86 42N 7+25E	1	39	7	132	.2	30	16	1652	4.08	14	5	ND	1	14	1	2	2	99	.38	.082	10	48	.31	74	.19	2	2.67	.01	.04	1	1
LS-86 42N 7+50E	1	40	4	132	.1	31	16	548	4.45	14	5	ND	1	13	1	2	2	95	.22	.046	9	53	.26	137	.05	2	2.59	.01	.03	1	1
LS-86 42N 7+75E	2	34	6	102	.1	29	14	800	3.80	25	5	ND	1	12	1	2	2	83	.28	.074	8	34	.26	90	.06	3	2.20	.01	.03	1	4
LS-86 42N 8+00E	2	35	7	111	.1	92	20	1807	3.54	24	5	ND	1	17	1	2	2	57	.40	.063	10	100	1.22	100	.11	5	2.11	.01	.08	1	1
LS-86 42N 8+25E	1	81	10	100	.2	130	31	3472	5.09	9	5	ND	2	42	1	2	2	124	1.17	.070	16	187	2.78	232	.38	9	3.09	.01	.07	1	3
LS-86 42N 8+50E	1	34	3	85	.2	29	13	381	4.07	10	5	ND	1	14	1	2	2	93	.30	.078	8	49	.34	68	.15	2	2.48	.01	.03	1	1
LS-86 42N 8+75E	1	20	7	117	.1	75	22	1906	5.12	9	5	ND	1	13	1	2	2	117	.37	.132	16	134	1.40	110	.18	2	2.83	.01	.05	1	1
LS-86 42N 9+00E	1	14	6	38	.1	19	8	414	3.83	7	5	ND	1	15	1	2	2	92	.27	.033	12	51	.38	72	.12	2	1.47	.01	.03	1	1
LS-86 42N 9+25E	3	45	28	119	.1	11	16	16269	6.83	41	6	ND	2	10	1	2	3	134	.15	.230	21	35	.16	322	.13	2	1.76	.01	.09	1	1
LS-86 42N 9+50E	1	59	8	106	.2	54	19	2185	5.18	17	5	ND	1	16	1	2	2	122	.42	.100	16	74	.95	125	.16	3	3.01	.01	.05	1	1
LS-86 42N 9+75E	1	49	6	81	.1	38	14	454	5.95	21	5	ND	2	14	1	30	2	150	.28	.232	11	79	.60	72	.16	7	3.28	.01	.04	1	2
LS-86 42N 10+00E	1	13	10	50	.1	57	12	1411	3.40	3	5	ND	1	49	1	2	2	123	.78	.052	9	118	1.38	75	.18	2	1.73	.01	.03	1	1
LS-86 42N 10+25E	1	22	13	113	.1	42	19	2955	5.36	10	5	ND	2	26	1	2	2	140	.38	.148	13	99	1.13	100	.24	6	2.60	.01	.05	1	1
LS-86 42N 10+50E	1	21	7	79	.1	19	14	1937	4.57	5	5	ND	1	20	1	2	2	137	.26	.080	11	59	.68	110	.15	5	2.10	.01	.05	1	3
LS-86 42N 10+75E	1	34	7	89	.1	28	20	4140	5.06	6	5	ND	1	37	1	2	2	142	.36	.082	11	63	1.66	119	.11	2	2.83	.01	.08	1	3
LS-86 42N 11+00E	1	10	2	48	.1	10	7	1720	2.48	2	5	ND	1	7	1	2	2	94	.10	.035	13	40	.42	107	.04	2	1.71	.01	.05	1	1
LS-86 42N 11+50E	1	33	5	81	.2	26	14	1070	4.09	9	5	ND	1	13	1	2	2	106	.21	.064	11	57	.44	72	.12	2	2.43	.01	.03	1	1
LS-86 42N 12+00E	2	140	2	107	.1	45	18	470	5.72	25	5	ND	2	10	1	2	2	143	.31	.178	11	82	.84	47	.19	5	4.35	.01	.05	1	1
LS-86 42N 12+50E	2	101	4	90	.2	53	21	496	5.59	20	5	ND	2	12	1	2	2	144	.35	.071	14	72	.85	108	.21	6	4.83	.01	.03	1	2
LS-86 42N 13+00E	1	85	4	80	.3	40	19	863	5.34	24	5	ND	2	13	1	2	2	131	.42	.134	13	63	.74	79	.21	5	3.19	.01	.04	1	1
LS-86 42N 13+50E	1	60	4	119	.1	59	23	504	5.91	15	5	ND	2	13	1	2	2	136	.32	.114	13	99	1.14	73	.23	2	4.05	.01	.05	1	1
LS-86 42N 14+00E	1	18	4	60	.4	35	15	539	5.07	5	5	ND	1	160	1	2	2	145	.87	.051	15	110	1.32	39	.52	3	2.28	.01	.02	1	1
LS-86 42N 14+50E	1	45	5	59	.3	33	13	301	7.05	13	5	ND	2	31	1	2	2	160	.36	.052	14	114	.78	36	.20	5	2.10	.01	.02	1	2
LS-86 42N 15+00E	1	83	2	67	.1	50	19	357	4.49	12	5	ND	1	14	1	2	2	131	.37	.029	12	71	.95	88	.23	2	3.20	.01	.03	1	1
LS-86 39N 0+00E	1	34	5	83	.1	23	14	336	6.33	12	5	ND	2	12	1	2	2	182	.37	.053	11	54	.32	60	.41	3	2.45	.01	.02	1	1
LS-86 39N 0+50E	1	35	6	75	.2	22	13	322	5.89	16	5	ND	2	14	1	2	2	170	.39	.038	11	49	.32	69	.29	2	2.16	.01	.03	1	1
LS-86 39N 1+00E	2	29	3	181	.1	42	14	1184	4.93	35	5	ND	2	12	1	22	2	93	1.65	.042	21	49	.68	42	.22	27	3.51	.01	.02	1	1
LS-86 39N 1+50E	1	71	4	78	.1	29	16	992	4.93	13	5	ND	2	13	1	29	2	135	.37	.087	9	48	.44	38	.27	3	3.51	.01	.02	1	3
LS-86 39N 2+00E	1	21	6	85	.2	12	13	498	6.33	8	5	ND	1	19	1	2	2	172	.41	.045	11	41	.23	39	.25	2	1.84	.01	.03	1	2
LS-86 39N 2+50E	1	6	8	27	.1	6	4	599	1.64	4	5	ND	1	7	1	2	2	43	.11	.020	7	13	.13	19	.02	2	.88	.01	.01	1	1
LS-86 39N 3+00E	1	8	3	52	.1	15	6	180	1.68	8	5	ND	1	9	1	2	2	42	.25	.015	7	13	.22	41	.01	2	1.38	.01	.03	1	1
LS-86 39N 3+50E	1	41	2	102	.4	35	16	321	5.38	14	5	ND	2	13	1	30	2	131	.25	.050	10	53	.41	70	.19	2	3.59	.01	.03	1	1
STD C/AU-S	20	59	37	128	6.8	69	28	1040	3.97	40	19	7	32	49	16	15	21	60	.48	.092	39	61	.88	177	.07	37	1.71	.06	.15	13	52

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cl PPM	Sb PPM	Ri PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	Y %	W PPM	Au# PPB
LS-86 39N 4+00E	1	57	12	113	.2	35	15	1381	4.59	15	5	ND	1	13	1	2	2	124	.33	.101	4	46	.42	63	.22	5	3.20	.01	.02	1	1
LS-86 39N 4+50E	1	55	7	102	.1	35	16	305	4.99	14	5	ND	1	14	1	8	2	145	.30	.078	4	52	.36	50	.20	2	3.47	.01	.02	1	1
LS-86 39N 5+00E	1	25	8	66	.1	15	8	248	3.91	10	5	ND	1	13	1	2	2	120	.28	.075	4	32	.25	34	.15	2	1.92	.01	.01	1	2
LS-86 39N 5+50E	2	8	3	74	.1	10	5	116	1.63	12	5	ND	1	3	1	2	2	35	.08	.038	2	13	.06	15	.01	2	.98	.01	.01	1	1
LS-86 39N 6+00E	1	20	5	197	.1	25	15	231	3.13	12	5	ND	1	6	1	2	2	70	.19	.074	5	41	.18	34	.07	2	3.09	.01	.03	1	1
LS-86 39N 6+25E	1	27	12	85	.1	16	8	583	2.93	18	5	ND	1	11	1	2	2	82	.21	.106	5	25	.16	51	.08	3	1.74	.01	.04	1	1
LS-86 39N 6+50E	2	13	2	133	.3	26	7	64	2.68	29	5	ND	1	3	1	3	2	43	.06	.047	2	21	.10	24	.01	2	1.88	.01	.02	1	1
LS-86 39N 6+75E	4	17	26	166	.1	42	13	8085	6.59	40	5	ND	1	23	2	4	2	63	1.09	.209	31	39	.38	150	.01	2	1.19	.01	.05	1	2
LS-86 39N 7+00E	1	67	11	131	.1	31	17	574	6.17	18	5	ND	1	12	1	2	2	129	.31	.093	7	43	.40	71	.17	4	2.86	.01	.03	1	2
LS-86 39N 7+25E	1	62	9	124	.2	19	20	1461	5.65	12	5	ND	1	32	1	2	2	169	.53	.076	3	44	.52	80	.23	5	3.09	.01	.04	1	1
LS-86 39N 7+50E	1	39	7	58	.1	17	9	304	4.28	9	5	ND	1	13	1	2	2	134	.29	.054	4	44	.35	35	.26	3	2.60	.01	.02	1	1
LS-86 39N 7+75E	1	33	8	51	.1	18	8	225	4.81	10	5	ND	1	62	1	2	2	169	.50	.062	4	51	.55	27	.28	2	2.27	.01	.03	1	1
LS-86 39N 8+00E	1	16	35	40	.1	24	7	144	3.24	7	5	ND	1	7	1	2	2	101	.12	.035	8	62	.51	29	.01	2	1.60	.01	.03	1	2
LS-86 39N 8+25E	1	22	4	48	.1	14	7	127	3.03	24	5	ND	1	6	1	4	2	66	.10	.042	3	20	.17	30	.02	3	1.32	.01	.02	1	1
LS-86 39N 8+50E	1	98	9	173	.2	50	25	565	7.31	30	5	ND	2	11	1	2	2	178	.29	.166	4	89	.58	75	.30	7	6.15	.01	.04	1	1
LS-86 39N 8+75E	1	58	6	126	.1	32	15	606	4.37	14	5	ND	1	12	1	2	2	121	.37	.085	4	44	.48	58	.22	2	3.05	.01	.02	1	1
LS-86 39N 9+00E	1	28	4	66	.1	14	9	853	2.83	10	5	ND	1	16	1	2	2	88	.31	.074	4	29	.46	45	.12	4	1.85	.01	.02	1	6
LS-86 39N 9+25E	1	72	5	77	.1	59	17	346	4.37	14	5	ND	1	16	1	32	2	117	.33	.070	5	67	.78	68	.24	2	3.81	.01	.03	1	4
LS-86 39N 9+50E	1	13	7	48	.1	22	7	408	3.76	4	5	ND	1	46	1	2	2	106	.55	.045	5	49	.39	48	.34	3	1.27	.01	.03	1	2
LS-86 39N 9+75E	1	9	10	46	.1	48	12	330	5.85	2	5	ND	1	75	1	2	2	151	1.25	.036	8	170	.80	22	.56	11	1.47	.01	.04	2	1
LS-86 39N 10+00E	1	98	4	86	.2	57	17	1403	4.58	3	5	ND	1	28	1	6	2	124	.81	.091	27	115	.52	327	.30	8	3.53	.02	.04	1	1
LS-86 39N 10+25E	1	22	5	68	.1	29	10	1352	5.02	5	5	ND	1	15	1	2	2	133	.37	.114	5	74	.47	70	.28	4	1.84	.01	.03	1	2
LS-86 39N 10+50E	1	43	11	87	.1	49	18	1340	5.05	6	5	ND	1	29	1	2	2	136	.45	.087	6	101	.73	65	.43	4	2.17	.01	.02	1	114
LS-86 39N 10+75E	1	44	14	75	.1	31	12	969	3.85	11	5	ND	1	17	1	2	2	112	.48	.086	4	49	.55	77	.23	4	1.98	.01	.04	1	1
LS-86 39N 11+00E	1	57	8	86	.1	31	16	732	4.88	9	5	ND	1	14	1	2	2	139	.34	.067	4	43	.49	97	.25	3	2.58	.01	.03	1	3
LS-86 39N 11+50E	1	46	10	106	.2	18	12	701	4.79	9	5	ND	1	14	1	2	2	119	.30	.160	5	44	.27	81	.23	3	2.69	.01	.03	1	1
LS-86 39N 12+00E	1	85	5	72	.1	42	19	426	5.51	13	5	ND	1	14	1	32	2	155	.35	.044	6	59	.58	94	.30	4	3.58	.01	.03	1	2
LS-86 39N 12+50E	1	78	6	116	.1	41	18	1211	5.53	10	5	ND	1	14	1	24	2	140	.36	.112	7	63	.69	88	.29	6	3.44	.01	.06	1	1
LS-86 39N 13+00E	1	58	7	98	.1	44	21	519	6.20	9	5	ND	1	13	1	2	2	157	.36	.085	5	95	1.13	94	.34	2	3.86	.01	.04	1	2
LS-86 39N 13+50E	1	34	10	60	.1	16	9	266	5.47	7	5	ND	1	19	1	2	2	147	.38	.121	5	56	.44	44	.37	4	2.21	.01	.03	1	3
LS-86 39N 14+00E	1	17	8	44	.1	16	10	414	7.79	3	5	ND	1	16	1	2	2	142	.38	.026	12	82	.95	67	.60	7	1.69	.01	.05	1	1
LS-86 39N 14+50E	1	86	3	75	.1	42	19	364	5.41	14	5	ND	1	17	1	25	2	152	.48	.074	4	66	.84	59	.35	4	3.41	.01	.02	1	2
LS-86 39N 15+00E	1	84	3	83	.2	38	18	460	5.30	14	5	ND	1	14	1	2	2	147	.42	.082	3	56	.68	47	.33	2	3.20	.01	.02	1	2
LS-86 27N 0+00E	1	61	5	98	.1	33	14	525	4.50	15	5	ND	1	15	1	2	2	134	.45	.078	3	42	.53	85	.27	6	3.23	.01	.02	1	3
LS-86 27N 0+50E	1	40	5	114	.1	52	14	710	3.97	17	5	ND	1	17	1	2	4	107	.38	.073	5	50	.61	99	.13	3	3.48	.01	.03	1	1
LS-86 27N 1+00E	1	16	4	100	.1	20	10	502	2.27	10	5	ND	1	8	1	2	2	59	.19	.077	2	21	.15	57	.11	2	1.95	.01	.02	1	1
STD C/AU-S	21	62	36	136	7.1	69	30	1022	3.95	40	17	7	34	49	17	16	18	65	.48	.106	36	57	.88	186	.09	35	1.71	.07	.15	12	53

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SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
LS-86 27N 1+50E	1	46	9	97	.1	31	14	473	4.78	16	5	ND	1	14	1	2	3	137	.42	.093	3	47	.46	66	.32	4	3.32	.01	.02	1	1
LS-86 27N 2+00E	1	16	8	68	.2	11	7	779	2.76	12	5	ND	1	12	1	2	2	68	.28	.086	3	21	.11	55	.15	2	1.24	.01	.02	1	89
LS-86 27N 2+50E	1	12	13	47	.1	8	6	1364	4.27	6	5	ND	1	18	1	2	2	126	.52	.050	3	24	.15	54	.23	2	1.49	.01	.03	2	5
LS-86 27N 3+00E	1	4	12	25	.1	4	2	399	.61	4	5	ND	1	27	1	2	2	28	.22	.031	2	5	.04	30	.05	2	.62	.01	.03	2	2
LS-86 27N 3+50E	1	167	13	70	.4	28	24	1744	5.56	13	5	ND	1	15	1	24	4	139	.41	.080	8	42	.82	105	.18	5	3.35	.01	.03	1	11
LS-86 27N 4+50E	2	52	21	142	.1	14	12	4778	1.73	10	5	ND	1	82	1	2	2	30	4.45	.108	9	11	.29	238	.03	12	.76	.01	.06	1	1
LS-86 27N 5+00E	1	68	13	54	.2	26	13	1125	4.26	11	5	ND	1	24	1	2	2	129	.83	.044	5	40	.42	93	.26	2	2.50	.01	.03	1	1
LS-86 27N 5+50E	1	77	17	119	.1	43	20	952	6.06	12	5	ND	1	14	1	39	4	158	.38	.097	4	60	.54	90	.34	2	3.61	.01	.03	1	3
LS-86 27N 6+00E	2	31	20	95	.1	17	21	7632	5.19	9	5	ND	1	26	1	4	6	144	.60	.092	5	44	.59	214	.02	2	2.20	.02	.07	1	27
LS-86 27N 6+50E	1	39	10	97	.4	24	14	1226	5.04	11	5	ND	1	15	1	2	4	144	.47	.107	3	40	.33	75	.32	2	2.40	.01	.02	1	6
LS-86 27N 7+00E	1	64	7	98	.1	32	17	828	5.72	10	5	ND	1	13	1	6	5	167	.44	.079	4	50	.45	51	.40	6	3.26	.01	.02	1	9
LS-86 27N 7+50E	1	20	7	66	.2	15	8	1130	3.71	4	5	ND	1	21	1	2	2	94	.74	.044	4	29	.21	41	.29	2	1.22	.01	.02	1	1
LS-86 27N 8+00E	1	26	11	59	.2	11	7	225	5.76	10	5	ND	1	8	1	2	3	166	.21	.085	5	32	.20	26	.19	2	2.18	.01	.02	1	3
LS-86 27N 8+50E	1	26	6	63	.2	14	8	192	4.86	7	5	ND	1	12	1	2	2	157	.30	.102	3	36	.26	32	.28	2	1.89	.01	.02	1	1
LS-86 27N 9+00E	2	47	15	161	.2	36	14	2707	3.71	20	5	ND	1	20	1	2	2	71	.63	.075	19	36	.44	134	.07	2	2.05	.01	.04	1	1
LS-86 27N 9+50E	1	6	7	67	.1	15	5	125	1.91	16	5	ND	1	5	1	2	2	40	.09	.070	2	13	.11	29	.01	2	.98	.01	.01	1	2
LS-86 27N 10+00E	2	35	9	104	.1	54	16	383	4.04	18	5	ND	1	15	1	2	2	101	.41	.054	8	63	.58	92	.09	2	2.25	.01	.04	1	1
LS-86 27N 10+50E	2	64	11	137	.3	41	18	1756	3.76	8	5	ND	1	20	1	2	2	105	.60	.102	13	52	.60	85	.30	5	3.55	.01	.04	1	2
LS-86 27N 11+00E	1	52	10	62	.2	63	19	196	7.46	7	5	ND	1	6	1	39	7	110	.12	.062	11	113	.88	49	.01	4	3.05	.01	.15	1	1
LS-86 27N 11+50E	1	17	9	48	.2	11	7	364	4.42	2	5	ND	1	19	1	2	2	115	.34	.070	4	46	.23	34	.33	2	1.29	.01	.02	1	1
LS-86 27N 12+00E	2	96	8	98	.2	44	20	634	6.45	17	5	ND	1	12	1	8	3	130	.31	.054	5	55	.52	55	.26	3	3.67	.01	.02	1	2
LS-86 27N 12+50E	1	23	12	42	.2	12	6	165	4.35	3	5	ND	1	14	1	2	2	149	.29	.030	3	39	.27	30	.33	2	1.56	.02	.02	1	1
LS-86 27N 13+00E	1	30	12	46	.1	15	7	112	5.51	2	5	ND	1	18	1	2	2	175	.25	.020	3	51	.23	26	.28	2	1.99	.01	.02	2	1
LS-86 27N 13+50E	1	74	11	58	.1	37	14	196	5.57	12	5	ND	1	13	1	2	2	166	.38	.039	4	57	.55	50	.36	3	2.88	.01	.03	1	4
LS-86 27N 14+00E	1	45	5	52	.2	23	9	169	5.15	9	5	ND	1	14	1	2	2	173	.31	.031	3	57	.42	27	.37	3	2.51	.01	.02	1	1
LS-86 27N 14+50E	2	82	3	72	.2	39	15	213	5.49	14	5	ND	1	12	1	37	3	162	.30	.037	8	65	.56	34	.36	3	3.62	.01	.02	1	39
LS-86 27N 15+00E	1	36	9	76	.1	21	10	227	5.50	8	5	ND	1	16	1	2	2	161	.36	.030	3	46	.28	41	.32	2	2.31	.01	.02	1	2
LS-86 27N 15+50E	1	25	14	113	.3	12	8	1259	4.63	11	5	ND	1	18	1	2	2	124	.31	.097	4	35	.13	74	.23	2	1.56	.01	.03	1	11
LS-86 27N 16+00E	1	6	7	32	.6	6	1	62	.71	3	5	ND	1	7	1	2	2	31	.18	.026	17	7	.05	43	.02	3	.52	.01	.07	2	5
LS-86 27N 16+50E	1	13	8	76	.1	9	6	651	3.33	2	5	ND	1	15	1	2	2	94	.41	.038	3	24	.24	36	.22	2	.98	.01	.01	1	3
LS-86 27N 17+00E	1	3	2	19	.1	7	2	37	1.03	13	5	ND	1	3	1	2	2	28	.04	.016	2	3	.03	6	.02	3	.34	.01	.01	1	2
LS-86 27N 17+50E	1	28	12	114	.2	26	10	217	4.23	8	5	ND	1	10	1	2	3	111	.21	.048	4	38	.60	34	.19	2	2.63	.01	.01	1	1
LS-86 27N 18+00E	1	35	6	94	.1	26	12	620	4.20	7	5	ND	1	12	1	2	2	115	.30	.070	3	38	.42	34	.25	3	2.23	.01	.02	1	1
LS-86 27N 18+50E	1	15	8	67	.1	18	8	780	3.67	11	5	ND	1	5	1	2	3	70	.10	.062	3	20	.78	22	.06	2	1.76	.01	.01	1	3
LS-86 27N 19+00E	1	7	5	53	.1	13	4	49	2.45	13	5	ND	1	3	1	2	2	50	.04	.033	2	14	.14	10	.03	2	.93	.01	.01	1	2
LS-86 27N 19+50E	1	14	8	91	.1	24	8	153	2.70	16	5	ND	1	5	1	2	2	59	.11	.020	7	21	.31	23	.07	2	1.28	.01	.01	1	1
STD C/AU-S	21	62	39	133	7.1	70	28	998	3.96	37	19	8	33	48	17	15	23	63	.48	.105	35	56	.88	184	.09	36	1.71	.06	.15	13	48

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
LS-86 27N 20+00E	1	51	8	119	.1	31	18	1314	4.82	5	5	ND	1	13	1	2	2	127	.31	.074	5	43	.64	76	.26	4	2.78	.01	.03	1	1
LS-86 27N 20+50E	1	75	9	96	.1	23	17	680	7.72	12	5	ND	3	12	1	2	2	205	.27	.129	5	54	.52	64	.34	2	4.24	.01	.04	1	1
LS-86 27N 21+00E	1	34	12	58	.1	17	9	352	4.49	7	5	ND	1	15	1	2	2	141	.28	.036	4	38	.31	39	.22	3	2.25	.01	.02	1	10
LS-86 27N 21+50E	1	60	13	64	.1	20	16	715	6.21	7	5	ND	1	21	1	2	2	164	.30	.073	5	50	.33	73	.24	2	4.13	.01	.04	1	2
LS-86 27N 22+00E	2	17	8	46	.1	4	8	4185	2.72	2	5	ND	1	17	1	2	3	112	.27	.056	3	14	.39	71	.05	3	1.76	.01	.04	1	1
LS-86 27N 22+50E	2	27	18	98	.2	33	16	4260	4.64	5	5	ND	1	20	1	2	5	130	.48	.099	4	58	.56	187	.23	2	2.33	.01	.04	1	1
LS-86 27N 23+00E	1	13	9	41	.1	9	6	594	3.74	5	5	ND	1	15	1	3	2	112	.31	.058	4	27	.22	35	.18	2	1.13	.01	.03	1	3
LS-86 27N 23+50E	1	17	5	47	.2	7	6	423	3.15	5	5	ND	1	19	1	2	2	102	.35	.033	4	26	.25	49	.18	2	1.27	.01	.03	1	1
LS-86 27N 24+00E	1	86	12	69	.1	30	16	1065	4.81	13	5	ND	1	16	1	8	2	123	.33	.066	8	51	.84	116	.08	5	2.55	.01	.05	1	2
LS-86 27N 24+50E	1	10	13	44	.1	12	6	461	3.65	3	5	ND	1	126	1	2	2	114	.65	.065	4	47	.37	67	.26	2	1.61	.01	.03	2	1
LS-86 24N 0+00E	1	41	13	105	.1	22	15	734	4.72	5	5	ND	1	19	1	2	2	131	.42	.072	4	35	.27	106	.35	5	2.44	.01	.02	1	1
LS-86 24N 0+50E	1	59	7	89	.1	65	23	876	5.47	11	5	ND	1	12	1	9	2	108	.34	.059	13	60	1.09	99	.10	2	3.26	.01	.06	1	7
LS-86 24N 1+00E	2	34	12	108	.1	48	14	1526	3.06	25	5	ND	1	7	1	4	2	54	.23	.062	19	45	.11	109	.01	2	1.47	.01	.04	1	3
LS-86 24N 1+50E	2	94	11	89	.2	27	18	921	5.31	16	6	ND	2	15	1	2	2	138	.43	.057	6	41	.47	123	.27	3	3.18	.01	.04	1	1
LS-86 24N 2+00E	1	110	12	101	.1	27	23	1081	6.43	7	5	ND	1	17	1	2	2	159	.35	.084	6	41	.54	113	.25	2	3.89	.01	.04	1	4
LS-86 24N 2+50E	1	39	13	124	.1	20	16	630	5.42	2	5	ND	1	15	1	2	2	151	.32	.035	4	43	.22	67	.29	2	2.65	.01	.03	1	2
LS-86 24N 3+00E	1	85	9	106	.4	30	16	859	5.48	15	6	ND	2	15	1	31	2	153	.37	.099	7	52	.43	64	.36	2	3.45	.01	.03	1	1
LS-86 24N 3+50E	1	98	10	143	.4	41	20	1050	5.13	8	5	ND	2	18	1	38	2	140	.48	.072	6	55	.61	126	.34	4	3.84	.02	.04	1	13
LS-86 24N 4+00E	1	41	7	76	.1	19	12	631	5.14	6	5	ND	1	15	1	2	3	166	.36	.041	5	44	.28	62	.34	2	2.19	.01	.02	1	1
LS-86 24N 4+50E	1	37	7	63	.3	23	13	341	6.00	12	5	ND	1	13	1	4	2	182	.32	.088	4	48	.35	73	.30	4	2.83	.01	.03	1	1
LS-86 24N 5+00E	1	52	6	92	.2	22	14	1289	4.30	7	5	ND	1	13	1	2	2	124	.32	.077	4	38	.29	62	.27	2	2.62	.01	.02	1	1
LS-86 24N 5+50E	1	74	8	102	.1	37	20	676	5.36	11	5	ND	2	16	1	2	2	152	.41	.049	5	53	.54	95	.31	8	4.13	.02	.03	1	1
LS-86 24N 6+00E	1	77	5	92	.3	36	16	556	5.00	9	5	ND	1	14	1	31	2	145	.35	.071	4	50	.49	77	.31	3	3.55	.01	.04	1	1
LS-86 24N 6+50E	1	60	8	78	.3	20	11	512	5.26	5	6	ND	2	13	1	32	2	151	.28	.094	5	49	.31	41	.30	5	3.43	.01	.03	1	2
LS-86 24N 7+00E	1	69	7	64	.2	32	18	277	5.91	9	5	ND	1	13	1	21	2	174	.34	.046	4	52	.43	46	.34	4	3.66	.01	.02	1	3
LS-86 24N 7+50E	1	102	11	93	.3	29	18	535	5.70	12	5	ND	2	11	1	2	2	162	.32	.106	4	51	.48	42	.34	2	4.45	.01	.03	1	1
LS-86 24N 8+00E	1	60	7	72	.1	18	13	748	4.90	4	5	ND	1	12	1	2	2	149	.33	.062	4	38	.36	52	.31	4	2.70	.01	.02	1	2
LS-86 24N 8+50E	1	36	6	62	.3	12	7	226	4.10	7	5	ND	1	12	1	2	2	128	.25	.055	4	32	.22	31	.29	7	2.22	.01	.02	1	3
LS-86 24N 9+00E	1	40	5	96	.1	25	13	228	4.73	17	5	ND	1	11	1	2	2	138	.28	.031	3	38	.36	61	.18	3	2.28	.01	.02	1	1
LS-86 24N 9+50E	1	41	7	137	.4	29	14	399	4.34	20	5	ND	2	15	1	2	3	114	.24	.067	4	53	.39	58	.16	4	2.80	.01	.03	1	1
LS-86 24N 10+00E	1	99	2	82	.1	43	16	332	4.41	12	5	ND	1	13	1	2	2	130	.41	.034	4	48	.73	54	.31	2	2.81	.01	.02	1	1
LS-86 24N 10+50E	1	62	6	100	.1	31	13	411	3.44	9	5	ND	1	11	1	2	2	100	.34	.054	3	34	.44	47	.24	2	2.86	.01	.02	1	1
LS-86 24N 11+00E	2	20	7	88	.2	40	17	1044	4.46	34	5	ND	1	14	1	2	2	134	.31	.037	7	78	1.14	100	.06	4	2.21	.01	.04	1	60
LS-86 24N 11+50E	1	86	5	92	.2	46	18	492	5.52	12	5	ND	1	13	1	2	2	168	.36	.070	3	63	.67	54	.35	8	4.36	.01	.03	1	3
LS-86 24N 12+00E	1	79	13	165	.6	161	37	1183	7.22	13	5	ND	2	55	1	2	2	163	.45	.626	7	336	2.58	57	.52	2	6.28	.01	.05	1	1
LS-86 24N 12+50E	1	62	4	100	.2	37	17	518	4.05	9	5	ND	1	15	1	2	2	115	.41	.071	4	41	.49	63	.30	4	2.79	.01	.03	1	1
STD C/AU-S	22	60	39	134	7.1	69	29	1123	3.94	39	16	8	33	48	17	15	21	64	.48	.104	36	57	.88	185	.09	37	1.71	.07	.15	12	48

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	F PPM	Al %	Na %	K %	W PPM	Au# PPB
LS-86 24N 13+00E	1	42	4	81	.1	13	9	313	5.36	8	5	ND	1	16	1	8	2	142	.28	.106	4	45	.18	33	.29	5	3.01	.01	.03	1	1
LS-86 24N 13+50E	1	74	7	89	.1	35	17	374	5.45	12	6	ND	2	14	1	2	2	153	.34	.065	4	55	.63	49	.30	5	3.85	.01	.04	1	3
LS-86 24N 14+00E	1	62	9	142	.2	34	16	615	5.44	16	5	ND	2	12	1	12	2	141	.27	.139	4	54	.46	57	.26	8	3.65	.01	.04	1	1
LS-86 24N 14+50E	1	51	5	178	.2	38	16	501	5.33	409	5	ND	1	13	1	31	2	136	.32	.071	6	50	.44	48	.25	8	3.27	.01	.03	1	3
LS-86 24N 15+00E	1	68	7	174	.3	35	18	479	6.00	30	5	ND	2	15	1	11	2	172	.31	.044	8	55	.41	47	.33	4	3.40	.01	.03	2	1
LS-86 24N 15+50E	9	54	8	144	.1	31	23	540	5.27	201	5	ND	1	16	1	2	2	158	.40	.036	5	42	.44	40	.35	8	2.64	.01	.03	1	3
LS-86 24N 16+00E	1	28	6	64	.1	14	8	327	4.94	13	5	ND	1	15	1	2	2	149	.43	.100	4	54	.35	29	.37	3	2.17	.01	.03	1	1
LS-86 24N 16+50E	2	25	6	98	.2	79	26	710	6.09	5	5	ND	2	17	1	2	2	106	.25	.054	5	122	1.41	51	.35	4	2.44	.01	.02	1	1
LS-86 24N 17+00E	1	87	4	95	.1	34	17	601	5.45	17	5	ND	2	11	1	2	2	147	.28	.105	3	62	.64	37	.28	8	4.24	.01	.03	1	1
LS-86 24N 17+50E	1	56	5	91	.1	51	23	411	5.38	13	5	ND	1	14	1	2	2	145	.37	.045	4	95	.88	51	.38	8	2.77	.01	.03	2	4
LS-86 24N 18+00E	1	97	12	158	.1	39	17	286	5.77	9	5	ND	1	15	1	7	2	155	.36	.039	6	93	.67	33	.37	5	2.92	.01	.02	1	4
LS-86 24N 18+50E	1	55	10	301	.1	64	19	314	6.45	14	5	ND	1	13	1	2	2	162	.31	.100	3	150	.94	39	.38	9	4.33	.01	.03	2	5
LS-86 24N 19+00E	1	65	3	141	.1	62	42	615	5.17	8	5	ND	1	17	1	2	2	130	.35	.070	5	77	.95	71	.29	7	4.03	.01	.04	1	1
LS-86 24N 19+50E	1	89	12	131	.1	34	20	476	6.87	10	6	ND	2	12	1	2	2	168	.23	.283	6	111	.62	35	.27	2	5.52	.01	.04	2	1
LS-86 24N 20+00E	1	32	7	68	.1	14	9	324	4.53	2	5	ND	1	31	1	2	3	151	.32	.040	4	45	.53	33	.22	2	2.46	.01	.03	1	1
LS-86 24N 20+50E	1	51	4	54	.1	23	11	247	4.65	5	5	ND	1	20	1	2	2	157	.30	.028	3	51	.55	37	.33	4	2.42	.01	.02	1	1
LS-86 24N 21+00E	1	51	12	71	.1	20	10	214	4.65	3	5	ND	1	34	1	2	2	142	.39	.037	4	47	.45	58	.19	6	2.90	.01	.04	1	1
LS-86 24N 21+50E	1	47	9	51	.1	14	8	256	6.51	8	5	ND	2	37	1	2	2	199	.44	.099	4	48	.37	27	.30	4	3.69	.01	.04	1	4
LS-86 24N 22+00E	1	24	7	58	.1	11	10	1087	4.40	2	5	ND	1	39	1	2	2	135	.84	.077	5	49	.49	62	.23	6	2.03	.01	.02	1	1
LS-86 24N 22+50E	1	54	8	129	.1	20	19	2446	4.78	3	5	ND	1	29	1	2	2	140	.50	.100	7	42	.56	211	.22	3	2.88	.01	.04	1	1
LS-86 24N 23+00E	1	65	12	67	.1	25	18	1144	5.66	8	5	ND	1	22	1	38	2	156	.47	.048	14	51	.56	140	.18	8	3.41	.01	.04	1	5
LS-86 24N 23+50E	1	68	6	64	.1	29	13	388	3.99	8	5	ND	1	15	1	2	2	116	.63	.030	4	41	.85	56	.27	11	2.48	.02	.03	1	1
LS-86 24N 24+00E	1	41	9	131	.1	26	17	1414	4.38	3	5	ND	1	13	1	2	2	130	.24	.071	4	63	1.40	86	.05	4	2.55	.01	.04	1	1
LS-86 24N 24+50E	1	17	7	76	.1	10	8	555	2.81	3	5	ND	1	20	1	2	2	91	.26	.039	9	24	.45	67	.07	4	1.74	.01	.03	1	2
LS-86 24N 25+00E	1	14	10	69	.1	7	7	494	2.55	5	5	ND	1	16	1	2	2	67	.21	.031	15	17	.24	112	.03	5	1.83	.01	.04	1	1
STD C	20	62	38	134	7.1	65	29	1008	3.96	40	17	8	34	49	16	15	19	64	.48	.101	36	58	.88	186	.09	36	1.71	.07	.15	13	47

LOW PHASE
(II) IC

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE 253-3158

DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GFAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN, FE, CA, F, CR, MG, BA, TI, B, AL, NA, K, M, SI, ZR, CE, SN, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: F1-20 SOILS -80 MESH P21 ROCKS AUXIL ANALYSIS BY FA-AAA FROM 10 GFAM SAMPLE.

DATE RECEIVED: FEB 16 1987 DATE REPORT MAILED: Feb 20/87 ASSAYER: J. J. J. IDENT TOYEL. CERTIFIED B.C. ASSAYER.

ASHWORTH EXPLORATION PROJECT - LACY-STONES FILE # 87-0355

PAGE 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM	
LS-87 12N 7+00W	1	61	9	61	.1	29	16	324	5.39	69	6	ND	1	18	1	2	168	.37	.042	7	60	.55	92	.36	6	4.14	.01	.04	1	3	
LS-87 12N 6+50W	1	37	10	73	.1	42	19	1092	5.61	60	5	ND	1	16	1	2	151	.47	.043	7	62	.54	124	.32	4	3.98	.02	.04	1	5	
LS-87 12N 6+00W	1	37	9	67	.1	47	19	1021	5.57	146	7	ND	1	29	1	4	2	155	.71	.035	9	69	.50	161	.32	4	4.08	.02	.04	1	1
LS-87 12N 5+50W	1	87	7	76	.1	41	21	471	5.56	20	6	ND	1	16	1	2	170	.42	.049	7	64	.68	107	.35	2	4.20	.01	.04	1	1	
LS-87 12N 5+00W	1	43	11	107	.3	39	19	1739	5.22	19	7	ND	1	15	1	3	2	135	.34	.114	6	41	.32	136	.28	2	3.42	.01	.03	1	3
LS-87 12N 4+50W	1	47	8	88	.1	24	12	566	5.72	15	5	ND	2	12	1	2	2	138	.31	.449	4	42	.42	54	.26	5	3.87	.01	.03	1	2
LS-87 12N 4+00W	1	28	9	103	.2	32	14	985	4.82	106	5	ND	1	14	1	2	5	128	.35	.076	4	37	.41	169	.22	4	2.38	.01	.03	1	2
LS-87 12N 3+50W	1	40	11	141	.1	32	23	3601	5.70	3	6	ND	1	20	1	2	2	123	.55	.106	7	47	.42	295	.32	8	3.34	.02	.05	1	1
LS-87 12N 3+00W	1	66	7	79	.1	41	18	438	5.49	3	5	ND	1	14	1	2	2	159	.41	.064	5	58	.67	111	.34	4	4.00	.02	.04	1	21
LS-87 12N 2+50W	1	38	2	116	.2	34	17	590	5.66	4	5	ND	1	16	1	2	2	145	.33	.107	4	52	.35	120	.34	2	3.53	.01	.03	1	3
LS-87 12N 2+00W	1	62	4	85	.1	44	18	504	5.28	2	5	ND	1	13	1	2	2	149	.36	.075	5	58	.66	158	.33	2	4.46	.01	.04	1	4
LS-87 12N 1+50W	1	39	15	161	.2	26	27	8884	6.25	3	6	ND	1	34	1	2	2	120	.45	.197	9	80	.78	367	.29	2	2.68	.01	.04	1	2
LS-87 12N 1+00W	1	97	5	88	.1	96	29	683	5.08	3	5	ND	1	10	1	2	7	91	.25	.060	11	73	.95	94	.11	5	2.61	.01	.05	1	1
LS-87 12N 0+50W	1	31	8	87	.1	25	7	362	2.48	3	5	ND	1	8	1	2	4	56	.27	.034	7	25	.36	37	.09	5	1.47	.01	.02	1	4
LS-87 9N 7+00W	1	42	12	85	.1	34	18	354	5.32	3	7	ND	1	24	1	3	2	148	.56	.040	10	53	.47	163	.32	7	3.65	.02	.05	1	2
LS-87 9N 6+50W	1	73	11	79	.2	37	16	424	4.87	8	5	ND	1	18	1	2	2	151	.42	.044	6	58	.67	112	.28	5	3.89	.01	.04	1	1
LS-87 9N 6+00W	1	46	6	84	.2	39	17	899	5.50	4	9	ND	2	19	1	2	2	153	.45	.061	5	51	.53	149	.34	4	3.76	.02	.04	1	1
LS-87 9N 5+50W	1	54	17	106	.1	41	18	589	5.22	8	6	ND	1	18	1	2	2	141	.47	.061	12	66	.85	156	.32	4	4.34	.02	.05	1	1
LS-87 9N 5+00W	1	63	11	71	.1	40	18	463	5.55	8	7	ND	1	16	1	2	2	172	.37	.067	9	64	.67	76	.34	2	4.34	.01	.04	1	1
LS-87 9N 4+50W	1	19	15	213	.1	11	19	4119	6.29	2	8	ND	1	21	1	2	2	113	.24	.140	6	17	.13	105	.47	2	1.32	.01	.06	1	1
LS-87 9N 4+00W	1	90	4	99	.1	97	26	968	5.62	9	6	ND	1	14	1	2	2	120	.39	.066	12	100	1.12	159	.24	2	3.90	.01	.04	1	2
LS-87 9N 3+50W	1	62	10	92	.2	65	22	492	5.64	10	5	ND	1	15	1	2	2	157	.36	.054	6	71	.72	109	.31	6	3.90	.01	.05	1	1
LS-87 9N 3+00W	1	28	11	77	.1	15	14	1206	4.01	2	5	ND	1	16	1	2	2	110	.36	.062	5	27	.29	111	.22	2	2.02	.01	.03	1	2
LS-87 9N 2+50W	1	67	10	88	.2	41	17	722	4.79	3	7	ND	1	13	1	2	2	138	.32	.065	3	58	.83	70	.26	6	4.29	.01	.04	1	5
LS-87 9N 2+00W	1	27	4	74	.2	21	13	343	3.40	2	5	ND	1	14	1	2	2	93	.31	.041	3	32	.34	62	.17	2	2.17	.01	.03	1	4
LS-87 9N 1+50W	1	53	6	162	.4	48	16	1159	4.03	4	5	ND	1	13	1	2	2	100	.30	.098	5	54	.57	98	.21	3	4.29	.01	.04	1	1
LS-87 9N 1+00W	1	33	5	131	.1	26	14	753	3.54	6	5	ND	1	11	1	3	3	96	.36	.119	3	35	.38	50	.19	4	2.81	.01	.03	1	1
LS-87 9N 0+50W	1	20	6	90	.1	29	10	289	3.44	6	5	ND	1	9	1	2	3	85	.43	.046	7	48	.41	35	.07	2	2.57	.01	.04	1	1
LS-87 6N 7+50W	1	56	2	94	.1	32	19	707	5.06	2	5	ND	1	17	1	2	2	130	.33	.060	18	53	.48	148	.33	4	3.66	.02	.06	1	3
LS-87 6N 7+00W	1	16	21	64	.1	20	13	5827	2.98	2	5	ND	1	32	1	2	3	76	.61	.109	6	26	.29	294	.15	2	1.55	.01	.04	1	1
LS-87 6N 6+50W	1	35	12	92	.1	31	16	2196	4.58	2	5	ND	1	20	1	2	2	123	.37	.123	6	45	.40	217	.27	4	2.81	.01	.04	1	1
LS-87 6N 6+00W	1	33	2	74	.1	35	14	1006	4.48	4	5	ND	1	21	1	2	2	132	.36	.042	5	47	.54	143	.29	2	3.28	.01	.04	1	1
LS-87 6N 5+50W	1	33	11	94	.1	31	16	3278	4.38	3	5	ND	1	20	1	2	2	112	.37	.065	8	41	.40	253	.26	2	2.92	.01	.05	1	1
LS-87 6N 5+00W	1	28	8	105	.1	31	15	2405	3.84	2	5	ND	1	16	1	2	2	100	.34	.112	5	40	.40	184	.21	2	2.74	.01	.05	1	1
LS-87 6N 4+50W	1	26	16	117	.1	28	17	2747	4.94	3	5	ND	1	21	1	2	2	132	.44	.058	7	42	.33	331	.27	2	2.41	.01	.04	2	1
LS-87 6N 4+00W	1	40	4	90	.1	29	16	911	4.12	3	5	ND	1	16	1	2	2	115	.34	.066	6	43	.46	136	.22	3	3.15	.01	.04	1	2
STD Cr/Au-S	20	60	37	136	6.9	69	30	1018	3.95	36	15	8	33	49	17	15	20	63	.48	.107	35	58	.88	182	.08	37	1.71	.07	.14	13	49

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE # 87-0355

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Ni PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au#1 PPB
LS-87 6N 3+50W	1	41	5	121	.1	35	15	1306	4.57	6	5	ND	1	14	1	2	2	115	.33	.252	4	50	.45	180	.21	5	3.31	.01	.03	1	1
LS-87 6N 3+00W	1	15	7	56	.1	14	8	354	3.30	4	5	ND	1	18	1	2	2	101	.37	.032	5	30	.26	100	.17	2	1.69	.01	.03	1	2
LS-87 6N 2+50W	1	35	3	94	.2	25	11	407	3.53	5	5	ND	1	14	1	2	2	98	.34	.079	3	37	.46	80	.16	5	2.33	.01	.03	1	2
LS-87 6N 2+00W	1	43	2	95	.3	27	13	703	4.21	3	5	ND	1	13	1	2	2	115	.30	.088	4	54	.49	65	.20	7	2.66	.01	.03	2	5
LS-87 6N 1+50W	1	24	7	74	.3	19	9	540	3.16	3	5	ND	1	13	1	2	2	93	.31	.078	3	35	.32	45	.18	5	2.15	.01	.03	1	1
LS-87 6N 1+00W	1	17	4	103	.1	17	8	458	2.54	7	5	ND	1	7	1	2	2	60	.17	.074	3	23	.16	46	.08	2	1.72	.01	.02	1	1
LS-87 6N 0+50W	1	35	18	129	.5	35	12	740	3.21	18	5	ND	1	11	1	2	2	90	.29	.115	4	38	.33	65	.15	4	2.90	.01	.03	1	1
LS-87 3N 7+50W	1	34	6	90	.1	22	16	993	5.21	3	5	ND	1	19	1	2	2	139	.39	.071	6	44	.38	111	.23	8	3.02	.02	.04	2	4
LS-87 3N 7+00W	1	32	7	54	.2	21	10	324	5.47	7	5	ND	1	15	1	3	2	161	.29	.060	4	44	.33	67	.27	7	3.03	.01	.04	1	1
LS-87 3N 6+50W	1	47	2	110	.1	29	17	1842	4.65	2	5	ND	1	19	1	2	2	118	.41	.210	5	48	.38	165	.24	3	3.22	.02	.05	1	1
LS-87 3N 6+00W	1	41	5	100	.1	33	15	1413	4.16	3	5	ND	1	13	1	2	2	117	.30	.093	5	50	.46	130	.23	4	3.27	.01	.04	1	1
LS-87 3N 5+50W	1	42	5	82	.1	34	15	793	4.64	3	5	ND	1	13	1	2	2	129	.30	.052	7	53	.45	157	.25	5	3.21	.01	.04	1	2
LS-87 3N 5+00W	1	46	2	112	.1	28	17	1180	5.14	3	5	ND	1	19	1	2	2	144	.58	.079	6	45	.41	139	.32	3	2.76	.01	.04	2	1
LS-87 3N 4+50W	1	64	5	96	.1	118	42	668	6.34	8	5	ND	1	23	1	2	3	127	.71	.077	17	127	.91	180	.13	5	5.03	.01	.04	1	1
LS-87 3N 4+00W	1	29	7	93	.2	30	12	945	3.98	4	5	ND	1	15	1	2	2	114	.37	.027	4	44	.47	117	.15	2	2.29	.01	.03	2	4
LS-87 3N 3+50W	1	58	6	169	.1	55	22	1414	5.44	6	5	ND	1	12	1	2	2	107	.25	.153	8	61	.51	133	.16	5	2.90	.01	.05	1	1
LS-87 3N 3+00W	1	33	5	60	.4	20	10	394	3.40	3	5	ND	1	13	1	2	2	100	.29	.067	4	38	.39	68	.14	5	2.33	.01	.04	1	3
LS-87 3N 2+50W	1	23	6	52	.3	19	9	406	3.92	3	5	ND	1	13	1	2	2	122	.32	.026	3	37	.33	50	.18	2	2.18	.01	.02	1	1
LS-87 3N 2+00W	1	14	5	179	.1	63	20	1073	4.64	5	5	ND	1	5	1	2	2	93	.11	.054	13	46	2.27	95	.01	4	3.54	.01	.08	1	1
LS-87 3N 1+50W	1	14	3	78	.1	19	8	1000	2.39	5	5	ND	1	12	1	2	2	64	.32	.073	4	29	.36	51	.09	2	1.68	.01	.02	2	1
LS-87 3N 1+00W	1	38	7	109	.3	27	12	758	3.23	7	5	ND	1	13	1	2	2	86	.31	.109	5	37	.40	85	.14	2	2.46	.01	.03	1	2
LS-87 3N 0+50W	1	24	4	120	.2	28	11	476	3.23	4	5	ND	1	12	1	2	2	82	.31	.111	4	35	.35	69	.14	5	2.63	.01	.03	2	1
LS-87 0N 15+00W	1	47	23	128	.2	48	18	1536	4.83	6	5	ND	1	29	1	2	2	125	.65	.093	6	58	.75	205	.16	10	3.02	.02	.06	2	4
LS-87 0N 14+50W	1	47	12	153	.2	48	18	2344	4.55	4	5	ND	1	30	1	2	2	107	.56	.135	7	59	.67	357	.15	6	2.99	.02	.05	1	1
LS-87 0N 14+00W	1	52	2	96	.1	41	15	932	4.37	5	5	ND	1	21	1	2	3	131	.41	.064	7	59	.71	212	.20	7	3.24	.01	.04	1	1
LS-87 0N 13+50W	1	78	8	87	.1	34	16	1076	4.40	7	5	ND	1	18	1	2	2	141	.47	.096	4	51	.63	97	.32	11	3.41	.02	.04	1	1
LS-87 0N 13+00W	1	27	7	100	.2	32	13	1508	3.30	4	5	ND	1	24	1	2	2	91	.48	.096	4	37	.43	156	.24	2	2.67	.01	.03	2	3
LS-87 0N 12+50W	1	77	2	56	.1	39	18	532	4.51	8	5	ND	1	30	1	2	2	153	.39	.028	7	69	.79	123	.30	4	3.87	.01	.04	2	1
LS-87 0N 12+00W	1	54	11	88	.1	46	15	1788	4.16	7	5	ND	1	28	1	2	2	120	.56	.042	15	61	.56	137	.21	8	3.39	.02	.03	2	1
LS-87 0N 11+50W	1	77	2	81	.1	37	16	636	4.50	7	5	ND	1	23	1	2	2	142	.54	.055	7	56	.73	125	.29	10	3.40	.02	.04	1	2
LS-87 0N 11+00W	1	34	4	78	.1	31	14	485	4.63	3	5	ND	1	22	1	2	2	131	.46	.048	8	47	.43	140	.34	10	2.71	.01	.04	1	1
LS-87 0N 10+50W	1	67	2	92	.1	47	19	634	5.79	5	5	ND	2	19	1	2	4	170	.34	.050	9	74	.64	118	.32	8	4.48	.02	.05	1	3
LS-87 0N 10+00W	1	66	2	100	.1	44	17	915	5.00	7	5	ND	1	27	1	2	2	157	.44	.083	9	64	.62	151	.32	7	3.96	.02	.05	1	1
LS-87 0N 9+50W	1	67	2	90	.1	45	16	519	5.13	7	5	ND	1	27	1	2	2	167	.40	.040	8	73	.81	132	.30	8	4.32	.02	.06	1	4
LS-87 0N 9+00W	1	66	2	119	.1	45	18	1587	5.15	2	5	ND	1	27	1	2	2	145	.41	.064	16	65	.63	232	.31	6	3.96	.02	.09	1	1
LS-87 0N 8+50W	1	38	11	108	.1	37	15	1476	4.82	5	5	ND	1	28	1	2	2	133	.41	.057	11	53	.53	215	.31	6	3.47	.02	.06	1	1
STD C/AU-S	21	61	36	136	7.2	67	29	1021	3.95	40	14	8	34	49	17	16	20	63	.48	.105	36	60	.88	182	.08	34	1.70	.07	.14	13	52

ASHWORTH EXPLORATION PROJECT - LACY-STONES FILE # 87-0355

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS-87 ON 8+00W	1	25	9	98	.1	28	12	869	4.15	2	5	ND	1	16	1	2	3	109	.35	.074	5	37	.47	134	.22	2	2.62	.01	.05	1	1
LS-87 ON 7+50W	1	19	9	100	.1	20	13	2032	3.75	2	5	ND	1	16	1	2	2	93	.37	.098	5	31	.34	162	.21	2	2.15	.01	.05	1	1
LS-87 ON 7+00W	1	61	16	112	.1	28	16	1138	4.59	2	5	ND	1	15	1	2	2	118	.37	.080	12	42	.45	176	.24	2	3.05	.01	.05	1	2
LS-87 ON 6+50W	1	48	7	112	.1	30	16	3626	4.40	2	5	ND	1	17	1	2	5	111	.35	.115	10	43	.41	324	.22	9	3.10	.01	.04	1	1
LS-87 ON 6+00W	1	71	10	-99	.1	35	16	747	4.41	4	5	ND	1	12	1	2	2	120	.36	.109	5	47	.69	172	.21	2	3.38	.01	.04	1	1
LS-87 ON 5+00W	1	19	6	175	.1	16	20	3044	6.19	2	5	ND	1	27	1	2	2	105	.35	.116	5	35	.15	155	.28	2	1.59	.01	.04	1	1
LS-87 ON 4+50W	1	44	5	103	.1	26	17	782	5.13	4	5	ND	2	16	1	2	8	137	.33	.136	8	47	.51	95	.27	2	3.78	.02	.05	2	1
LS-87 ON 4+00W	1	90	11	125	.1	49	24	2996	5.19	3	5	ND	2	11	1	2	4	121	.30	.139	7	44	.49	263	.21	3	3.39	.01	.05	1	7
LS-87 ON 3+50W	1	19	5	74	.1	24	12	2054	3.18	2	5	ND	1	12	1	2	4	72	.34	.088	7	41	.39	103	.15	3	1.71	.01	.03	1	1
LS-87 ON 3+00W	1	47	6	92	.1	29	12	1188	3.47	4	5	ND	1	12	1	2	2	94	.38	.116	4	37	.55	85	.18	4	2.63	.01	.03	1	1
LS-87 ON 2+50W	1	34	9	133	.2	32	15	630	3.95	8	5	ND	1	11	1	2	2	100	.31	.116	4	41	.47	62	.18	2	3.11	.01	.03	1	1
LS-87 ON 2+00W	1	11	8	120	.1	36	9	669	1.42	19	5	ND	1	5	1	2	2	29	.12	.109	5	12	.08	37	.05	3	1.15	.01	.02	1	1
LS-87 ON 1+50W	1	36	7	91	.1	28	11	1095	3.13	5	5	ND	1	11	1	2	2	90	.37	.091	5	32	.42	74	.13	2	2.49	.01	.03	1	2
LS-87 ON 1+00W	1	43	6	133	.1	29	14	680	3.95	4	5	ND	1	12	1	2	2	105	.32	.153	4	41	.42	69	.18	2	3.04	.01	.03	1	1
LS-87 ON 0+50W	1	82	8	102	.2	36	15	572	4.19	5	5	ND	2	12	1	2	2	116	.50	.130	3	40	.70	79	.23	3	3.16	.02	.04	1	1
LS-87 ON 0+25E	1	43	10	76	.2	32	12	879	3.26	5	5	ND	1	11	1	2	4	83	.28	.072	4	32	.49	90	.14	2	2.64	.01	.03	2	1
LS-87 ON 0+75E	1	64	6	79	.1	28	15	622	4.03	2	5	ND	1	14	1	2	3	107	.30	.084	5	57	.63	96	.18	2	3.14	.01	.04	1	2
LS-87 ON 1+25E	1	82	11	55	.1	35	14	269	4.69	5	5	ND	1	12	1	2	2	130	.29	.072	5	67	.59	47	.25	2	3.60	.01	.03	1	1
LS-87 ON 1+75E	1	63	12	86	.1	27	13	726	4.42	2	5	ND	2	13	1	2	2	119	.32	.113	3	41	.40	73	.24	5	3.50	.01	.04	1	1
LS-87 ON 2+25E	1	63	9	74	.2	29	13	293	4.15	5	5	ND	1	11	1	2	2	110	.29	.056	3	48	.51	86	.20	7	3.60	.01	.03	1	1
LS-87 ON 2+75E	1	36	8	58	.3	28	10	483	5.35	2	5	ND	1	30	1	2	2	148	.33	.077	4	75	.70	52	.27	6	2.69	.01	.03	1	2
LS-87 ON 3+25E	1	81	10	65	.1	37	16	316	4.67	5	5	ND	1	16	1	2	2	127	.34	.038	5	70	.73	75	.25	6	4.22	.01	.05	1	1
LS-87 ON 3+75E	2	55	70	62	.2	27	14	506	4.99	4	5	ND	2	15	1	2	2	134	.31	.051	5	56	.53	78	.24	2	3.27	.01	.03	1	12
LS-87 ON 4+25E	1	53	10	75	.2	23	12	864	3.92	3	5	ND	1	12	1	2	2	104	.29	.122	4	45	.36	53	.20	5	3.19	.01	.03	1	1
LS-87 ON 4+75E	1	80	7	68	.1	24	11	325	4.53	2	5	ND	2	12	1	2	2	120	.26	.089	3	65	.47	39	.26	6	5.12	.01	.04	1	1
LS-87 1S 3+50W	1	51	8	95	.1	55	15	698	4.47	2	5	ND	2	12	1	2	2	108	.33	.082	6	59	.67	140	.19	7	3.54	.01	.04	1	3
LS-87 1S 3+25W	1	8	7	102	.2	59	23	2794	5.14	2	5	ND	1	6	1	2	2	63	.17	.040	11	142	.58	187	.05	2	2.01	.01	.08	1	1
LS-87 1S 3+00W	1	8	10	73	.2	27	11	559	2.99	3	5	ND	1	6	1	2	2	60	.14	.036	8	76	.41	60	.07	5	1.45	.01	.04	1	3
LS-87 1S 2+75W	1	15	7	105	.2	24	8	1130	1.98	8	5	ND	1	11	1	2	2	56	.29	.063	4	21	.24	71	.09	2	1.48	.01	.03	1	1
LS-87 1S 2+50W	1	19	11	121	.5	25	10	1068	2.93	9	5	ND	1	11	1	2	2	75	.32	.110	3	30	.34	72	.15	4	2.32	.01	.04	1	1
LS-87 1S 2+25W	4	12	10	183	.1	69	12	956	2.56	24	5	ND	1	12	1	2	2	54	.45	.072	10	18	.19	72	.09	3	1.54	.01	.03	1	1
LS-87 1S 2+00W	1	6	4	64	.1	18	5	225	.87	4	5	ND	1	5	1	2	4	24	.12	.025	2	8	.13	32	.03	5	.78	.01	.02	1	1
LS-87 1S 1+75W	1	25	7	75	.1	24	10	462	2.53	4	5	ND	1	12	1	2	4	73	.37	.044	3	26	.44	67	.14	3	1.98	.01	.02	1	1
LS-87 1S 1+50W	1	26	13	123	.1	29	11	739	3.12	7	5	ND	1	11	1	2	2	83	.29	.107	3	34	.36	85	.15	2	2.69	.01	.03	1	4
LS-87 1S 1+25W	1	10	12	140	.1	25	8	1454	2.53	3	5	ND	1	12	1	2	2	61	.46	.145	8	30	.28	100	.11	6	1.98	.01	.03	1	1
LS-87 1S 1+00W	1	29	11	121	.2	25	11	941	3.38	4	5	ND	1	13	1	2	2	85	.42	.130	7	35	.32	84	.19	3	2.45	.01	.03	1	1
STD C/AU-S	20	58	38	133	6.8	64	29	1002	3.94	38	17	8	33	47	17	15	19	62	.48	.100	35	56	.88	178	.08	34	1.71	.07	.14	13	47

ASHWORTH EXPLORATION PROJECT - LACUF-STOPES FILE # 87-0255

PAGE 4

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Tl	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
LS-87 1S 0+75W	1	37	7	103	.2	28	12	933	3.35	10	7	ND	2	11	1	2	2	87	.35	.085	4	36	.63	73	.16	5	2.60	.01	.04	1	1
LS-87 1S 0+50W	1	57	21	95	.2	28	15	914	4.23	11	7	ND	2	19	1	2	2	100	.58	.060	7	39	.93	67	.20	9	1.94	.02	.05	1	1
LS-87 1S 0+25W	1	64	22	156	.1	31	14	2242	3.71	8	5	ND	2	14	1	2	2	96	.35	.115	6	34	.53	123	.14	2	2.62	.01	.06	1	2
LS-87 1S 0+00W	1	51	11	109	.3	32	14	1781	3.59	6	5	ND	2	12	1	2	3	96	.28	.038	8	38	.48	120	.14	3	2.63	.01	.03	1	1
LS-87 1S 0+25E	1	46	14	81	.1	20	12	581	3.25	3	5	ND	1	15	1	2	2	93	.31	.033	5	39	.53	67	.14	3	1.94	.01	.03	1	2
LS-87 1S 0+50E	1	64	12	63	.2	31	12	414	2.59	6	5	ND	2	10	1	2	2	63	.23	.020	8	30	.47	52	.08	4	1.71	.01	.03	1	1
LS-87 1S 0+75E	1	18	4	86	.1	21	12	1908	2.55	3	5	ND	1	19	1	2	2	67	.34	.113	4	50	.48	107	.13	2	1.71	.01	.02	1	1
LS-87 1S 1+00E	1	19	6	57	.1	26	9	563	2.48	3	5	ND	1	41	1	2	2	71	.40	.066	3	77	.71	49	.16	2	1.74	.01	.02	1	1
LS-87 1S 1+25E	1	34	6	62	.2	31	11	321	3.45	3	5	ND	1	19	1	2	2	98	.30	.040	4	74	.79	52	.21	6	2.57	.01	.03	1	4
LS-87 1S 1+50E	1	61	12	84	.1	27	13	446	4.18	4	5	ND	2	14	1	2	2	113	.27	.094	4	54	.44	64	.20	5	3.17	.01	.03	1	1
LS-87 1S 1+75E	1	39	4	65	.2	22	10	572	3.36	2	5	ND	1	15	1	2	2	90	.27	.074	3	57	.56	58	.15	3	2.29	.01	.03	1	2
LS-87 1S 2+00E	1	15	3	55	.2	11	9	1286	2.49	2	5	ND	1	12	1	2	2	71	.28	.035	4	23	.22	69	.13	3	1.42	.01	.02	1	1
LS-87 1S 2+25E	1	64	7	82	.1	33	15	1660	4.06	7	5	ND	2	16	1	2	2	113	.38	.059	6	63	.73	131	.22	9	2.85	.01	.05	1	25
LS-87 1S 2+50E	1	16	11	50	.3	19	8	958	2.78	2	5	ND	1	20	1	2	2	79	.37	.050	4	40	.37	98	.18	3	1.61	.01	.03	1	3
LS-87 1S 2+75E	1	64	10	105	.1	32	38	1421	4.67	5	5	ND	1	19	1	2	2	99	.30	.094	12	39	.40	131	.20	5	3.30	.01	.05	1	40
LS-87 1S 3+00E	1	37	3	76	.1	23	11	508	4.09	5	5	ND	2	15	1	2	2	105	.28	.129	4	39	.35	81	.17	5	3.22	.01	.04	1	24
LS-87 1S 3+25E	1	47	6	65	.1	15	10	320	3.63	5	5	ND	1	17	1	2	2	90	.25	.073	4	30	.29	55	.12	3	2.65	.01	.03	1	2
LS-87 1S 3+50E	1	17	8	70	.1	8	6	2818	3.10	5	5	ND	1	19	1	2	2	82	.29	.148	3	21	.19	91	.13	2	1.64	.01	.03	1	31
LS-87 1S 3+75E	1	38	13	81	.2	19	12	669	2.94	5	5	ND	1	15	1	2	2	81	.31	.092	4	33	.43	58	.15	5	2.69	.01	.04	1	1
LS-87 1S 4+00E	1	29	6	80	.1	14	13	1874	3.12	6	5	ND	1	15	1	2	2	80	.27	.092	5	22	.24	116	.11	5	2.32	.01	.04	1	32
LS-87 1S 4+25E	3	24	6	72	.1	5	12	262	4.77	16	5	ND	1	14	1	10	2	108	.31	.036	3	7	.14	90	.01	4	1.77	.01	.05	1	1
LS-87 1S 4+50E	1	31	13	70	.1	18	12	491	4.64	5	5	ND	1	17	1	2	2	124	.39	.046	7	38	.34	82	.19	6	2.23	.01	.03	1	2
LS-87 1S 4+75E	1	21	13	83	.1	8	9	2107	3.46	4	5	ND	1	19	1	2	2	87	.30	.072	5	19	.32	115	.11	4	2.05	.01	.05	1	1
LS-87 1S 5+00E	1	30	12	96	.2	24	14	779	4.13	7	5	ND	1	15	1	2	2	101	.32	.087	5	36	.32	118	.20	4	2.28	.01	.04	1	1
LS-87 1S 5+50E	1	57	17	63	.1	34	15	365	4.31	5	5	ND	1	13	1	2	2	115	.29	.084	4	48	.53	91	.20	2	3.45	.01	.04	1	1
LS-87 1S 6+00E	1	22	14	53	.1	17	10	1724	3.26	4	5	ND	1	20	1	2	2	90	.34	.075	3	65	.51	75	.18	4	1.53	.01	.03	1	2
LS-87 1S 6+50E	1	8	2	28	.1	10	6	951	1.49	2	5	ND	1	18	1	2	3	49	.19	.023	2	44	.35	42	.06	2	.80	.01	.01	1	1
LS-87 1S 7+00E	1	35	2	69	.1	18	9	425	4.58	6	5	ND	1	12	1	2	2	127	.26	.122	3	53	.39	41	.20	9	3.47	.01	.03	1	1
LS-87 1S 7+50E	1	20	14	51	.1	15	6	226	3.59	5	5	ND	1	12	1	2	2	101	.27	.083	3	34	.27	43	.18	2	1.58	.01	.02	1	1
LS-87 1S 8+00E	1	87	11	69	.1	29	16	439	4.12	7	5	ND	2	13	1	2	2	108	.27	.090	5	66	.63	40	.21	5	3.11	.01	.03	1	1
LS-87 2S 3+00W	1	21	12	127	.2	20	11	2193	2.83	5	5	ND	1	12	1	2	2	72	.33	.135	5	30	.27	89	.15	6	2.24	.01	.02	1	1
LS-87 2S 2+75W	1	35	10	151	.1	25	12	1170	2.86	5	5	ND	1	13	1	2	2	81	.43	.137	4	29	.40	96	.15	10	2.33	.01	.03	1	1
LS-87 2S 2+50W	1	30	5	101	.1	27	11	1052	2.98	5	5	ND	1	13	1	2	2	82	.35	.081	4	33	.36	79	.17	5	2.34	.01	.02	1	45
LS-87 2S 2+25W	1	18	9	211	.5	46	12	966	3.08	6	5	ND	1	11	1	2	2	71	.29	.144	6	34	.42	95	.14	2	2.74	.01	.04	1	1
LS-87 2S 2+00W	1	48	8	160	.1	35	14	1192	3.24	6	5	ND	1	13	1	2	2	82	.41	.111	3	33	.44	81	.15	5	2.62	.01	.03	1	1
LS-87 2S 1+75W	1	16	9	99	.1	33	10	781	2.57	10	5	ND	1	8	1	2	2	57	.19	.042	6	24	.31	80	.07	5	1.75	.01	.03	1	2
STD C/AU-S	21	60	40	135	7.0	67	28	1019	3.95	38	16	8	33	49	17	16	21	63	.48	.097	36	58	.88	180	.08	36	1.71	.07	.14	12	50

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE # 87-0355

PAGE 5

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS-87 2S 1+50W	1	73	8	110	.1	33	14	775	4.32	12	5	ND	1	13	1	2	2	108	.42	.113	5	44	.61	83	.20	4	2.89	.01	.03	1	1
LS-87 2S 1+25W	2	51	9	106	.1	32	13	528	3.48	10	5	ND	1	10	1	2	2	83	.30	.089	6	38	.39	66	.16	5	2.67	.01	.02	1	3
LS-87 2S 1+00W	1	246	11	77	.1	38	21	622	4.78	10	5	ND	2	18	1	2	2	120	.57	.046	5	53	.94	160	.20	6	3.39	.02	.04	1	4
LS-87 2S 0+75W	1	82	13	75	.1	31	16	1653	4.50	6	5	ND	1	15	1	2	2	127	.46	.118	4	51	.57	131	.22	3	3.26	.01	.05	1	2
LS-87 2S 0+50W	1	75	9	86	.3	32	14	439	3.80	9	5	ND	1	12	1	2	3	103	.35	.060	4	42	.58	93	.18	4	2.92	.01	.03	1	1
LS-87 2S 0+25W	1	71	12	70	.1	36	17	2203	4.31	5	5	ND	1	20	1	2	2	111	.61	.075	16	63	.64	104	.21	2	3.46	.01	.04	1	3
LS-87 2S 0+00W	2	71	11	72	.1	41	16	366	5.05	5	5	ND	1	15	1	2	2	141	.34	.056	4	68	.65	77	.29	6	3.82	.01	.04	1	11
LS-87 2S 0+25E	1	24	2	78	.1	21	11	1573	3.26	5	5	ND	1	18	1	2	2	96	.36	.060	4	66	.79	144	.08	4	2.53	.01	.04	1	1
LS-87 2S 0+50E	1	30	8	78	.1	22	11	978	3.90	3	5	ND	1	15	1	2	2	108	.39	.042	4	37	.32	108	.25	2	2.18	.01	.03	1	4
LS-87 2S 0+75E	1	80	9	77	.1	37	17	544	4.94	8	5	ND	1	13	1	2	2	140	.35	.036	7	59	.55	114	.28	8	3.81	.01	.04	1	1
LS-87 2S 1+00E	1	72	11	73	.1	32	14	419	4.37	7	5	ND	2	15	1	2	2	122	.43	.039	4	46	.69	68	.26	3	3.06	.01	.03	1	1
LS-87 2S 1+25E	1	104	5	69	.1	34	17	408	4.90	10	5	ND	2	15	1	2	2	145	.42	.030	5	61	.92	146	.28	6	3.94	.02	.04	1	5
LS-87 2S 1+50E	2	58	7	74	.1	35	15	418	5.25	3	5	ND	1	14	1	2	2	147	.36	.044	4	55	.47	84	.28	2	3.66	.01	.04	1	1
LS-87 2S 1+75E	1	55	14	69	.1	32	15	673	4.65	5	5	ND	1	13	1	2	2	131	.33	.036	5	49	.43	105	.26	9	3.01	.01	.03	1	1
LS-87 2S 2+00E	2	52	9	78	.2	38	15	351	4.68	11	5	ND	2	12	1	2	2	123	.29	.035	4	56	.65	84	.23	7	3.49	.01	.03	1	1
LS-87 2S 2+25E	2	14	7	48	.1	11	8	934	2.77	2	5	ND	1	16	1	2	2	84	.36	.027	4	31	.27	80	.16	2	1.17	.01	.03	1	1
LS-87 2S 2+50E	1	78	13	102	.2	29	18	740	4.20	7	6	ND	2	18	1	2	2	106	.41	.090	7	44	.66	119	.21	6	2.97	.01	.06	1	2
LS-87 2S 2+75E	1	41	10	70	.1	23	13	1491	3.54	2	5	ND	1	14	1	2	2	92	.35	.094	4	39	.40	119	.20	2	2.41	.01	.03	1	1
LS-87 2S 3+00E	1	59	11	76	.1	29	13	521	4.52	7	5	ND	1	12	1	2	2	122	.31	.113	5	52	.40	72	.25	3	4.09	.01	.04	1	5
LS-87 2S 3+25E	1	49	16	81	.1	29	12	413	4.52	6	5	ND	1	12	1	2	3	113	.28	.139	4	45	.41	77	.22	2	4.14	.01	.04	1	1
LS-87 2S 3+50E	2	58	6	78	.1	18	14	771	4.14	6	5	ND	2	15	1	2	2	104	.29	.146	8	35	.34	52	.17	5	3.45	.01	.04	1	8
LS-87 2S 3+75E	1	47	9	96	.1	22	12	383	4.59	4	5	ND	2	13	1	2	2	117	.33	.148	4	37	.47	85	.20	8	3.52	.01	.03	1	3
LS-87 2S 4+00E	1	44	4	119	.1	19	13	888	5.25	7	5	ND	1	14	1	4	2	119	.34	.156	4	33	.37	146	.13	4	2.79	.01	.04	1	1
LS-87 2S 4+25E	1	85	2	72	.1	37	15	382	4.84	8	5	ND	1	12	1	2	2	143	.38	.054	3	56	.73	106	.25	5	4.04	.01	.03	1	1
LS-87 2S 4+50E	1	41	6	78	.2	24	14	886	4.30	2	5	ND	2	16	1	2	4	111	.37	.050	5	39	.37	102	.23	6	2.59	.01	.04	1	2
LS-87 2S 4+75E	1	55	9	82	.1	33	15	654	4.55	7	5	ND	2	12	1	2	2	122	.33	.079	5	47	.54	84	.26	5	3.55	.01	.04	1	1
LS-87 2S 5+00E	1	58	5	96	.2	33	14	775	4.51	4	5	ND	2	13	1	2	2	117	.38	.160	4	51	.47	103	.27	2	3.31	.01	.04	1	9
LS-87 2S 5+50E	2	22	7	45	.1	17	7	254	3.51	3	5	ND	1	18	1	2	3	102	.37	.013	4	30	.41	78	.16	4	1.82	.01	.03	1	2
LS-87 2S 6+00E	1	61	8	78	.1	57	21	1004	4.53	7	5	ND	1	52	1	2	2	117	.58	.069	4	189	1.98	70	.29	4	3.07	.01	.03	1	1
LS-87 2S 6+50E	1	42	13	46	.3	24	9	320	5.90	6	5	ND	2	30	1	2	2	171	.35	.062	4	109	.60	30	.27	3	2.56	.01	.03	1	1
LS-87 2S 7+00E	1	71	3	80	.1	34	17	380	5.17	8	5	ND	1	12	1	2	3	140	.33	.065	6	63	.56	66	.25	2	3.35	.01	.03	1	1
LS-87 2S 7+50E	1	83	13	68	.2	56	19	534	4.16	8	5	ND	1	12	1	2	4	117	.36	.046	5	104	1.25	60	.14	8	3.28	.01	.03	1	8
LS-87 2S 8+00E	1	106	9	75	.3	51	20	304	5.16	7	5	ND	2	12	1	3	3	140	.30	.037	7	77	.81	72	.24	2	4.12	.01	.04	1	1
LS-87 3S 15+00W	1	34	7	89	.1	33	13	517	4.92	6	5	ND	1	16	1	2	2	127	.39	.034	4	56	.47	116	.27	2	2.84	.01	.04	1	1
LS-87 3S 14+50W	1	43	16	89	.3	37	14	1263	4.48	5	5	ND	1	24	1	2	2	121	.49	.047	8	58	.52	161	.22	6	3.07	.02	.05	1	1
LS-87 3S 14+00W	1	62	6	98	.3	40	15	554	4.53	7	5	ND	1	21	1	2	4	120	.49	.081	9	54	.61	125	.26	7	3.25	.01	.04	1	2
STD C/AU-S	21	58	38	129	6.9	67	28	977	3.94	37	17	7	33	47	17	16	20	61	.48	.098	35	57	.88	176	.08	36	1.71	.07	.13	12	49

ASHWORTH EXPLORATION PROJECT - LACY-STONES FILE # 87-0355

PAGE 6

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS-87 3S 13+50W	1	32	5	134	.2	33	13	1433	4.33	11	5	ND	1	17	1	2	2	101	.43	.141	8	42	.48	170	.23	8	2.72	.01	.04	1	1
LS-87 3S 13+00W	1	43	8	62	.1	38	13	516	3.87	8	5	ND	1	20	1	2	2	107	.48	.028	5	46	.77	141	.20	5	2.52	.01	.02	1	1
LS-87 3S 12+50W	1	44	3	92	.1	37	14	1080	4.16	9	5	ND	1	20	1	2	2	99	.42	.092	8	50	.57	167	.19	2	3.12	.01	.03	1	29
LS-87 3S 12+00W	1	57	2	77	.1	34	15	393	4.19	7	5	ND	1	20	1	2	2	125	.41	.065	8	48	.50	88	.24	6	3.22	.01	.02	1	1
LS-87 3S 11+50W	1	34	4	-72	.2	28	12	1359	3.74	6	5	ND	1	19	1	2	3	99	.45	.049	5	45	.53	104	.16	2	2.46	.01	.02	1	14
LS-87 3S 11+00W	1	58	7	57	.1	35	14	336	4.68	7	5	ND	1	13	1	2	2	141	.34	.035	5	54	.62	48	.29	8	3.31	.01	.02	1	8
LS-87 3S 10+50W	1	50	6	98	.2	40	15	424	5.18	9	8	ND	1	16	1	2	3	146	.30	.074	8	57	.44	117	.27	5	4.20	.01	.03	1	2
LS-87 3S 10+00W	1	29	4	86	.2	34	13	541	4.68	6	5	ND	1	15	1	2	3	125	.32	.055	4	44	.42	114	.25	2	2.83	.01	.03	1	1
LS-87 3S 9+50W	1	42	5	55	.1	33	15	373	3.97	5	5	ND	1	16	1	2	2	112	.33	.031	4	47	.56	70	.17	2	2.67	.01	.02	1	1
LS-87 3S 9+00W	1	32	5	62	.1	26	13	852	3.43	8	5	ND	1	17	1	2	2	95	.48	.026	7	42	.56	69	.17	8	2.22	.01	.01	1	1
LS-87 3S 8+50W	1	26	4	66	.1	22	14	567	3.40	2	5	ND	1	16	1	2	2	96	.43	.028	6	37	.38	50	.15	3	2.28	.01	.02	1	1
LS-87 3S 8+00W	1	29	5	68	.1	28	13	1026	3.56	4	5	ND	1	26	1	2	2	100	.60	.030	11	45	.47	99	.15	3	2.42	.01	.03	1	3
LS-87 3S 7+50W	1	40	7	69	.3	34	15	732	4.71	8	5	ND	1	16	1	2	2	136	.55	.037	6	48	.53	103	.25	5	2.72	.01	.03	1	4
LS-87 3S 7+00W	1	27	8	82	.1	22	12	1209	3.72	4	5	ND	1	27	1	2	2	104	.67	.042	7	46	.46	105	.18	2	2.07	.01	.05	1	1
LS-87 3S 6+50W	1	30	14	191	.1	21	15	2726	4.35	5	5	ND	1	31	1	2	2	83	.54	.160	10	37	.39	252	.20	6	2.44	.01	.06	1	1
LS-87 3S 6+00W	1	60	22	74	.1	33	17	720	4.43	8	5	ND	1	21	1	2	3	120	.65	.052	6	46	1.11	85	.29	6	2.17	.02	.05	1	1
LS-87 3S 2+25W	1	48	18	85	.2	23	15	1035	3.79	5	5	ND	1	20	1	2	2	107	.66	.057	6	38	.75	77	.22	3	2.21	.02	.04	1	1
LS-87 3S 1+75W	1	37	18	134	.1	19	12	1541	3.84	7	5	ND	1	12	1	2	2	98	.35	.119	3	37	.42	130	.17	2	2.04	.01	.02	1	6
LS-87 3S 1+25W	2	66	20	143	.1	21	14	1388	3.78	7	5	ND	1	14	1	2	2	90	.49	.074	5	33	.49	109	.15	2	2.37	.01	.03	1	2
LS-87 3S 0+75W	1	108	9	74	.1	30	20	966	5.06	4	6	ND	1	18	1	2	2	122	.46	.046	9	72	1.10	134	.13	4	3.41	.01	.05	1	17
LS-87 3S 0+25W	1	43	3	106	.1	39	29	2834	5.22	5	5	ND	1	57	1	2	2	122	.81	.089	6	123	1.63	130	.13	4	3.38	.01	.04	1	31
LS-87 3S 0+25E	1	15	2	94	.1	14	9	1008	4.06	2	5	ND	1	16	1	2	2	92	.30	.173	3	45	.28	67	.20	2	1.86	.01	.02	1	1
LS-87 3S 0+75E	1	45	13	78	.1	19	11	1833	3.31	5	5	ND	1	15	1	2	2	87	.30	.155	4	46	.51	90	.16	3	2.79	.01	.03	1	1
LS-87 3S 1+25E	1	28	9	90	.2	24	12	1196	3.35	2	5	ND	1	13	1	2	2	86	.33	.117	4	33	.32	102	.20	2	2.12	.01	.02	1	3
LS-87 3S 1+75E	1	49	14	60	.1	32	14	971	4.18	5	5	ND	1	12	1	2	2	113	.46	.052	5	49	.54	82	.22	2	2.99	.01	.02	1	1
LS-87 3S 2+25E	1	62	4	68	.1	32	14	433	4.71	5	5	ND	1	10	1	2	3	131	.38	.062	3	53	.55	51	.31	2	3.07	.01	.01	1	2
LS-87 3S 2+75E	1	19	7	71	.1	15	10	1112	3.75	3	5	ND	1	11	1	2	2	99	.31	.045	3	33	.21	87	.19	2	1.82	.01	.02	1	3
LS-87 3S 3+25E	1	47	6	75	.2	26	12	539	4.11	9	5	ND	1	12	1	2	2	111	.38	.039	4	40	.51	79	.22	2	2.39	.01	.02	1	1
LS-87 3S 3+75E	1	39	6	79	.1	24	16	823	4.79	6	5	ND	1	13	1	2	2	125	.41	.049	4	39	.40	119	.25	6	2.42	.01	.02	1	2
LS-87 3S 4+25E	2	45	7	80	.1	19	14	437	4.15	7	5	ND	1	15	1	2	2	103	.30	.077	3	34	.54	77	.15	2	2.65	.01	.03	1	1
LS-87 3S 4+75E	1	34	9	70	.2	25	13	321	4.85	7	5	ND	1	11	1	2	2	105	.28	.073	5	39	.42	89	.13	2	3.34	.01	.04	1	4
LS-87 3S 5+25E	1	43	12	85	.1	33	13	368	4.82	5	5	ND	1	12	1	2	3	112	.37	.053	4	40	.48	95	.21	2	3.08	.01	.03	1	2
LS-87 3S 5+75E	1	30	8	87	.2	33	14	494	4.03	7	5	ND	1	11	1	2	2	83	.29	.158	4	61	.36	113	.09	2	2.71	.01	.03	1	1
LS-87 4S 7+00W	1	29	7	128	.1	27	14	3256	4.01	6	5	ND	1	34	1	2	2	84	.81	.110	9	37	.43	251	.17	4	2.38	.01	.09	1	1
LS-87 4S 6+75W	1	45	9	103	.1	33	14	1460	4.26	7	5	ND	1	20	1	2	2	103	.43	.188	7	45	.66	217	.17	6	2.88	.01	.05	1	1
LS-87 4S 6+50W	1	36	11	109	.1	26	14	2286	4.06	5	5	ND	1	20	1	2	2	95	.30	.243	8	42	.45	218	.18	2	2.71	.01	.04	1	1
STD C/AU-S	21	56	37	130	6.9	66	29	980	3.94	38	14	7	31	47	16	15	22	61	.48	.096	35	57	.88	176	.08	36	1.71	.07	.12	13	51

ASHWORTH EXPLORATION PROJECT - LACY-STONES FILE # 87-0255

PAGE 7

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Aut#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
LS-87 4S 6+25W	1	41	9	118	.2	27	14	2532	4.09	10	5	ND	1	24	1	2	2	101	.36	.236	12	37	.35	248	.20	3	3.01	.01	.05	1	1
LS-87 4S 6+00W	1	94	16	80	.1	37	20	1184	4.77	13	5	ND	1	22	1	2	2	133	.66	.082	9	50	.98	154	.28	4	3.01	.02	.07	1	1
LS-87 4S 5+75N	1	41	13	111	.2	34	15	2565	4.36	7	5	ND	2	25	1	2	2	106	.38	.119	19	40	.50	273	.24	3	3.34	.02	.06	1	1
LS-87 4S 5+50W	1	47	13	101	.1	31	15	1359	4.88	7	5	ND	1	21	1	2	2	125	.41	.079	7	44	.58	242	.25	2	3.43	.01	.05	1	8
LS-87 4S 5+25W	1	52	18	103	.1	29	18	1441	5.66	10	5	ND	1	19	1	2	4	146	.33	.135	9	47	.43	224	.16	3	3.58	.01	.04	1	1
LS-87 4S 5+00W	1	73	16	78	.1	35	15	690	5.01	10	5	ND	1	16	1	2	2	145	.36	.074	6	54	.63	143	.27	2	4.02	.01	.04	1	1
LS-87 4S 4+75W	1	42	14	87	.2	35	14	1503	4.51	8	5	ND	2	14	1	4	2	122	.41	.120	5	46	.54	205	.27	3	3.28	.01	.04	1	1
LS-87 4S 4+50W	1	73	13	97	.2	63	21	1456	4.93	15	5	ND	1	12	1	2	4	87	.30	.063	8	58	.61	240	.09	2	2.75	.01	.08	1	1
LS-87 4S 4+25W	1	57	22	113	.1	44	18	2588	4.66	13	5	ND	1	16	1	2	2	116	.40	.119	10	46	.47	267	.23	5	3.47	.02	.05	1	1
LS-87 4S 4+00W	1	86	13	79	.1	58	18	835	4.39	7	5	ND	1	15	1	2	4	83	.36	.027	12	61	1.35	117	.13	3	2.61	.02	.06	1	12
LS-87 4S 3+75W	1	29	11	95	.2	17	10	608	2.99	6	5	ND	1	16	1	2	2	83	.55	.049	3	25	.42	73	.17	4	1.84	.01	.03	1	1
LS-87 4S 3+50W	1	48	17	99	.1	22	11	1359	2.95	7	5	ND	1	12	1	2	2	80	.37	.110	4	31	.44	88	.15	3	2.10	.01	.03	1	1
LS-87 4S 3+25W	1	35	17	229	.3	24	16	1253	4.18	9	5	ND	1	15	1	2	2	109	.43	.158	4	36	.40	77	.23	6	3.06	.01	.04	1	1
LS-87 4S 3+00W	1	60	17	124	.2	25	16	1695	4.29	8	5	ND	1	26	1	2	2	108	.84	.162	5	39	.69	108	.24	3	2.96	.02	.04	1	1
LS-87 4S 2+75W	1	46	18	107	.1	27	15	1632	3.93	8	5	ND	1	15	1	3	2	100	.41	.109	4	36	.44	123	.22	3	2.61	.01	.04	1	2
LS-87 4S 2+50W	1	85	19	88	.2	25	15	803	4.57	5	5	ND	1	14	1	2	2	123	.35	.099	5	42	.44	90	.24	4	3.01	.01	.03	1	105
LS-87 4S 2+25W	1	80	17	89	.1	23	16	2831	3.95	5	5	ND	1	14	1	2	2	103	.36	.112	11	37	.45	104	.21	2	3.12	.01	.03	1	1
LS-87 4S 2+00W	1	31	7	62	.2	16	8	963	2.82	6	5	ND	1	14	1	2	3	77	.37	.084	3	24	.27	74	.17	3	1.63	.01	.03	1	6
LS-87 4S 1+75W	1	65	8	87	.1	31	14	727	4.33	6	5	ND	1	15	1	2	2	112	.33	.077	4	40	.51	103	.23	7	3.40	.01	.03	1	1
LS-87 4S 1+50W	1	72	13	88	.2	32	15	486	4.55	10	5	ND	1	17	1	2	3	125	.44	.061	6	48	.63	124	.23	4	3.38	.01	.03	1	1
LS-87 4S 1+25W	1	137	16	102	.1	31	21	2590	5.47	9	5	ND	1	26	1	2	2	145	.44	.156	6	45	.65	248	.24	3	3.32	.01	.05	1	5
LS-87 4S 1+00W	1	104	16	111	.3	25	21	1410	5.57	6	5	ND	1	34	1	2	2	144	.87	.154	5	41	.70	177	.19	4	3.10	.01	.04	1	1
LS-87 4S 0+75W	1	78	13	143	.1	41	21	5128	5.09	9	5	ND	1	34	1	2	2	127	.82	.068	25	62	.61	367	.21	10	4.35	.02	.04	1	4
LS-87 4S 0+50W	1	65	19	87	.1	37	17	673	5.10	7	5	ND	1	17	1	2	4	140	.35	.069	5	60	.59	142	.25	5	3.70	.01	.04	1	1
LS-87 4S 0+25W	1	57	14	73	.1	31	14	1104	4.49	7	5	ND	1	14	1	2	2	124	.35	.075	6	56	.55	99	.24	5	3.24	.01	.03	1	1
LS-87 4S 0+00W	1	57	18	90	.1	46	18	790	5.23	6	5	ND	1	17	1	2	2	134	.54	.082	7	71	.48	92	.23	2	4.22	.02	.02	1	1
LS-87 4S 0+25E	1	72	16	68	.2	36	15	275	4.99	7	5	ND	1	14	1	2	2	139	.32	.052	5	67	.63	51	.25	4	3.67	.01	.03	1	2
LS-87 4S 0+50E	1	75	21	85	.3	30	15	868	4.77	5	5	ND	1	14	1	2	2	121	.28	.143	4	68	.43	71	.25	3	3.75	.01	.03	1	1
LS-87 4S 0+75E	1	46	18	106	.1	29	14	1271	5.28	8	5	ND	1	13	1	2	2	124	.31	.201	4	59	.35	98	.26	2	3.41	.01	.03	1	1
LS-87 4S 1+00E	1	89	15	77	.1	30	14	503	4.94	11	5	ND	1	12	1	2	4	133	.31	.140	4	73	.64	48	.25	6	4.07	.01	.03	1	2
LS-87 4S 1+25E	1	49	10	97	.4	24	11	711	3.36	4	5	ND	1	23	1	2	2	82	.46	.170	3	77	.59	65	.19	4	2.27	.01	.03	1	1
LS-87 4S 1+50E	1	52	11	74	.2	32	13	338	4.04	8	5	ND	1	13	1	2	2	118	.34	.048	5	53	.52	88	.24	3	3.38	.01	.04	1	1
LS-87 4S 1+75E	1	55	13	88	.1	27	13	1207	4.60	6	5	ND	1	13	1	2	4	101	.33	.361	5	76	.59	79	.21	4	3.40	.01	.03	1	1
LS-87 4S 2+00E	1	26	8	110	.1	18	12	1497	2.97	2	5	ND	1	15	1	2	2	71	.36	.158	4	30	.28	112	.19	4	2.03	.01	.03	1	1
LS-87 4S 2+25E	1	41	13	88	.1	18	9	1647	2.93	4	5	ND	1	21	1	2	2	75	.39	.085	3	50	.52	80	.15	3	2.06	.01	.03	1	2
LS-87 4S 2+50E	1	66	14	100	.1	36	15	1022	4.35	5	5	ND	1	15	1	2	2	114	.36	.126	4	50	.54	100	.20	7	3.61	.01	.03	1	2
STD C/AU-S	21	59	38	131	6.8	62	28	988	3.95	41	17	7	32	47	16	15	19	61	.48	.103	35	55	.88	175	.08	37	1.71	.07	.13	13	47

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE #87-0355

PAGE 8

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au#1 PPB
LS-87 4S 2+75E	1	49	5	79	.4	32	12	688	4.15	8	5	ND	1	14	1	2	2	110	.33	.061	3	50	.48	72	.23	4	3.06	.01	.02	1	1
LS-87 4S 3+00E	1	17	5	66	.1	8	6	669	3.55	7	5	ND	1	13	1	2	2	84	.30	.119	3	30	.23	56	.15	2	1.73	.01	.02	1	1
LS-87 4S 3+25E	1	15	7	68	.2	15	8	424	3.12	6	5	ND	1	14	1	2	2	76	.29	.103	3	29	.27	70	.16	5	1.49	.01	.02	2	1
LS-87 4S 3+50E	1	52	5	75	.2	36	16	273	5.33	9	5	ND	1	12	1	2	2	141	.29	.038	3	54	.51	81	.26	2	3.38	.01	.03	2	1
LS-87 4S 3+75E	1	55	2	113	.4	32	14	824	3.95	6	5	ND	1	11	1	2	2	97	.28	.119	4	44	.44	72	.18	2	3.35	.01	.03	2	1
LS-87 4S 4+00E	1	51	9	70	.3	21	10	534	3.34	2	5	ND	1	11	1	4	2	82	.28	.133	4	30	.46	52	.15	4	2.86	.01	.04	2	2
LS-87 4S 4+25E	2	28	4	80	.1	25	12	652	3.67	3	5	ND	1	12	1	2	2	91	.31	.054	4	35	.33	68	.19	5	2.58	.01	.03	1	1
LS-87 4S 4+50E	1	45	5	72	.3	19	12	962	3.97	5	5	ND	1	15	1	3	2	103	.32	.099	5	33	.40	101	.14	2	2.67	.01	.04	1	33
LS-87 4S 4+75E	1	17	4	79	.3	10	7	394	2.99	6	5	ND	1	14	1	2	2	67	.25	.065	6	19	.21	147	.02	5	2.34	.01	.04	1	1
LS-87 4S 5+00E	1	39	6	115	.1	15	13	1229	4.54	3	5	ND	1	17	1	2	2	83	.37	.089	7	24	.36	213	.04	2	2.30	.01	.05	1	1
LS-87 4S 5+25E	1	61	4	104	.1	76	24	3660	5.99	24	5	ND	1	28	1	7	3	98	1.00	.064	15	111	.30	377	.01	3	2.41	.02	.06	1	1
LS-87 4S 5+50E	1	38	2	69	.1	72	23	1190	4.82	17	5	ND	1	13	1	4	3	106	.17	.099	4	123	.23	289	.01	2	2.08	.02	.05	2	1
LS-87 4S 5+75E	1	122	4	82	.4	91	31	704	6.43	44	5	ND	1	10	1	9	4	133	.08	.088	4	134	.27	143	.01	2	1.65	.02	.05	1	1
LS-87 4S 6+00E	1	35	5	70	.1	75	23	520	4.90	6	5	ND	1	10	1	2	3	110	.15	.059	5	120	.66	146	.01	2	2.32	.02	.05	1	1
LS-87 4S 6+50E	1	83	8	68	.2	66	25	545	5.54	8	5	ND	1	5	1	2	2	96	.08	.045	7	162	2.09	71	.01	5	2.96	.01	.04	1	1
LS-87 4S 7+00E	1	28	6	97	.1	33	14	3496	3.55	5	5	ND	1	17	1	2	2	83	.33	.129	5	55	.41	186	.12	2	2.26	.01	.04	1	1
LS-87 4S 7+50E	1	30	5	73	.1	23	11	472	7.43	17	5	ND	1	16	1	2	2	146	.27	.631	4	103	.66	58	.21	2	3.17	.01	.04	1	2
LS-87 4S 8+00E	1	15	6	41	.2	9	6	360	2.56	3	5	ND	1	16	1	2	2	75	.33	.079	3	30	.31	32	.16	2	1.24	.01	.02	2	1
LS-87 5S 8+50W	1	39	8	86	.2	31	13	951	4.27	3	5	ND	1	27	1	3	2	117	.76	.040	8	49	.58	109	.18	4	2.78	.01	.04	1	1
LS-87 5S 8+00W	1	22	10	66	.2	21	10	1198	3.05	4	5	ND	1	31	1	2	2	88	1.13	.032	5	72	.39	87	.14	3	2.10	.01	.03	1	1
LS-87 5S 7+50W	1	11	2	52	.1	18	12	565	5.81	8	5	ND	1	17	1	2	3	136	.53	.034	3	42	.37	78	.15	3	2.11	.01	.02	1	1
LS-87 5S 7+00W	1	41	7	128	.1	24	13	2200	3.96	5	5	ND	1	19	1	2	4	89	.52	.212	6	33	.46	157	.18	7	2.44	.01	.04	1	2
LS-87 5S 6+75W	1	43	2	84	.3	32	13	628	4.21	6	5	ND	1	16	1	3	6	112	.40	.104	9	43	.55	131	.22	6	2.98	.01	.05	2	1
LS-87 5S 6+50W	1	41	5	89	.3	30	14	898	4.15	5	5	ND	1	15	1	2	2	114	.38	.107	6	44	.55	145	.21	3	3.09	.01	.05	1	1
LS-87 5S 6+25W	1	27	6	102	.1	23	12	2257	3.34	5	5	ND	1	16	1	2	2	83	.41	.063	7	34	.39	257	.15	2	2.23	.01	.04	1	1
LS-87 5S 6+00W	1	34	5	105	.1	27	19	1673	5.46	7	5	ND	1	25	1	2	2	119	.41	.110	9	42	.51	445	.28	2	2.97	.01	.07	1	2
LS-87 5S 5+75W	2	39	18	84	.1	19	17	3423	3.18	2	5	ND	1	30	1	2	2	69	.63	.113	7	34	.42	309	.10	2	1.80	.01	.04	1	1
LS-87 5S 5+50W	1	84	7	80	.1	35	21	868	4.62	10	5	ND	1	23	1	2	2	127	.40	.059	7	83	1.26	160	.25	4	3.49	.01	.05	1	1
LS-87 5S 5+25W	1	78	15	88	.1	30	24	1644	5.01	6	5	ND	1	25	1	2	2	128	.52	.043	8	52	1.11	284	.23	6	3.11	.01	.05	1	1
LS-87 5S 5+00W	1	1233	43	127	.1	73	25	1089	7.56	12	5	ND	1	22	1	3	5	86	.33	.072	14	39	.76	385	.14	2	3.25	.02	.07	1	2
LS-87 5S 4+75W	1	57	13	94	.3	35	16	1730	4.28	5	5	ND	1	14	1	5	2	112	.41	.081	9	48	.50	249	.20	8	3.32	.01	.05	1	1
LS-87 5S 4+50W	2	109	18	137	.2	17	29	5003	6.03	18	5	ND	1	14	1	2	8	53	.25	.127	13	12	.51	316	.01	2	2.18	.01	.10	1	1
LS-87 5S 4+25W	1	22	2	150	.1	34	11	1892	2.74	9	5	ND	1	12	1	2	2	48	.25	.081	11	26	1.06	194	.05	2	2.17	.01	.03	1	1
LS-87 5S 4+00W	1	17	8	104	.4	20	11	3028	3.07	4	5	ND	1	17	1	3	2	75	.40	.117	6	27	.27	136	.18	4	1.86	.01	.03	1	1
LS-87 5S 3+75W	1	74	4	77	.1	32	15	991	4.82	5	5	ND	1	12	1	2	5	148	.37	.135	4	52	.62	113	.28	3	4.05	.01	.02	1	2
LS-87 5S 3+50W	1	68	2	77	.1	41	18	330	5.46	6	5	ND	1	14	1	2	5	160	.40	.041	4	54	.64	81	.30	2	3.94	.02	.05	1	1
STD C/AU-S	22	59	39	134	7.1	69	29	1014	3.91	39	11	7	34	49	18	16	20	63	.50	.101	36	58	.92	184	.08	38	1.72	.07	.14	12	52

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE #87-0355

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Ni PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS-87 SS 3+25W	1	45	2	59	.2	23	15	860	4.55	3	5	ND	1	19	1	2	2	128	.45	.030	7	40	.32	107	.28	6	2.48	.01	.03	1	2
LS-87 SS 3+00W	1	53	6	71	.1	26	15	1221	4.02	7	5	ND	1	16	1	2	2	115	.42	.071	4	41	.45	114	.23	2	2.71	.01	.03	1	3
LS-87 SS 2+75W	1	59	2	69	.1	19	21	1801	4.95	5	5	ND	1	33	1	2	2	139	.69	.049	10	30	.59	122	.24	7	2.47	.01	.02	1	8
LS-87 SS 2+50W	1	31	7	30	.3	2	4	272	2.10	2	5	ND	1	60	1	2	2	73	.63	.030	3	14	.10	44	.11	2	.59	.01	.02	1	23
LS-87 SS 2+25W	1	51	7	64	.1	24	16	770	4.40	6	5	ND	1	17	1	2	4	123	.43	.047	7	39	.40	68	.23	2	3.04	.01	.02	1	4
LS-87 SS 2+00W	1	77	7	80	.1	30	16	815	4.75	4	5	ND	1	16	1	2	2	131	.41	.101	5	46	.54	100	.26	4	3.54	.01	.04	1	1
LS-87 SS 1+75W	1	54	8	78	.1	29	15	1245	4.40	6	5	ND	1	16	1	2	2	123	.39	.089	4	47	.46	120	.24	5	3.27	.01	.04	1	2
LS-87 SS 1+50W	1	54	6	64	.1	24	14	1159	4.22	6	5	ND	1	15	1	2	2	122	.39	.068	4	40	.44	99	.22	3	2.95	.01	.03	1	1
LS-87 SS 1+25W	1	83	9	183	.3	17	13	4587	3.86	11	5	ND	1	27	1	2	2	83	.40	.369	4	34	.25	214	.10	2	2.13	.01	.04	1	1
LS-87 SS 1+00W	1	85	7	80	.2	39	19	410	5.16	338	5	ND	1	13	1	14	2	107	.29	.037	5	51	.56	137	.07	2	3.00	.01	.04	1	1
LS-87 SS 0+75W	1	55	6	69	.1	36	14	1365	4.13	8	5	ND	1	17	1	2	2	121	.43	.096	4	51	.56	171	.22	9	3.24	.01	.04	1	3
LS-87 SS 0+50W	1	57	5	94	.1	32	15	1342	4.26	7	5	ND	1	17	1	2	2	116	.33	.095	5	50	.42	137	.25	2	3.24	.01	.04	1	2
LS-87 SS 0+25W	1	60	13	138	.1	28	22	6448	4.77	5	5	ND	1	19	1	2	2	113	.33	.131	7	81	.55	184	.23	5	3.26	.01	.04	1	1
LS-87 SS 0+00W	1	29	10	57	.1	17	21	2222	3.16	6	5	ND	1	23	1	2	2	81	.41	.099	4	41	.29	97	.12	3	1.65	.01	.02	1	2
LS-87 SS 0+25E	1	32	10	68	.1	20	13	2027	4.22	7	5	ND	1	17	1	2	2	108	.30	.156	4	50	.45	78	.22	3	2.65	.01	.03	1	1
LS-87 SS 0+50E	1	15	2	46	.2	39	11	1670	2.55	2	5	ND	1	57	1	2	2	76	.53	.046	3	132	1.04	40	.16	2	1.64	.01	.02	1	1
LS-87 SS 0+75E	1	63	2	71	.1	26	13	567	4.17	3	5	ND	1	19	1	2	4	117	.34	.087	4	57	.48	103	.21	6	2.89	.01	.02	1	1
LS-87 SS 1+00E	1	60	5	68	.2	50	18	361	5.45	8	5	ND	1	21	1	2	3	157	.36	.047	6	102	.82	126	.30	2	3.97	.01	.04	1	1
LS-87 SS 1+25E	1	65	10	88	.1	33	15	1173	4.51	5	5	ND	1	20	1	2	2	124	.46	.161	4	63	.54	112	.22	5	3.50	.01	.05	1	2
LS-87 SS 1+50E	1	30	7	108	.1	21	15	2001	3.52	3	5	ND	1	29	1	2	2	84	.40	.128	4	51	.39	95	.21	2	2.16	.01	.03	1	1
LS-87 SS 1+75E	1	48	13	97	.1	24	14	1137	3.66	8	5	ND	1	18	1	2	2	91	.40	.128	4	44	.47	97	.18	3	2.73	.01	.03	1	1
LS-87 SS 2+00E	1	16	3	58	.1	26	11	247	2.58	4	5	ND	1	25	1	2	2	119	.44	.026	4	85	.89	29	.17	2	1.80	.01	.01	1	1
LS-87 SS 2+25E	1	48	7	95	.2	32	13	565	4.66	6	5	ND	1	15	1	2	2	124	.35	.166	3	49	.43	69	.21	6	3.37	.01	.04	1	1
LS-87 SS 2+50E	1	53	8	48	.1	25	12	204	4.89	6	5	ND	1	14	1	2	2	141	.28	.034	5	49	.46	45	.23	5	3.43	.01	.02	1	1
LS-87 SS 2+75E	1	20	14	66	.1	5	15	1411	3.70	5	5	ND	1	34	1	2	2	102	.33	.052	7	9	.34	128	.10	2	2.79	.01	.08	1	1
LS-87 SS 3+00E	2	16	12	88	.1	9	8	2930	2.65	2	5	ND	1	27	1	2	2	76	.38	.104	5	17	.22	172	.12	4	1.77	.01	.08	1	2
LS-87 SS 3+25E	1	18	10	52	.1	9	8	664	4.93	3	5	ND	1	18	1	2	2	127	.30	.074	4	32	.31	51	.17	2	2.21	.01	.06	1	9
LS-87 SS 3+50E	1	50	14	85	.1	15	11	736	3.65	5	5	ND	1	18	1	2	2	94	.34	.156	5	32	.42	64	.17	2	2.97	.01	.05	1	1
LS-87 SS 3+75E	1	19	13	72	.2	9	7	578	2.64	2	5	ND	1	19	1	2	2	72	.34	.086	4	19	.27	55	.12	2	1.88	.01	.04	1	1
LS-87 SS 4+00E	1	27	3	61	.2	12	9	262	3.85	2	5	ND	1	17	1	2	4	94	.30	.045	4	28	.26	63	.18	2	2.12	.01	.03	1	1
LS-87 SS 4+25E	3	51	5	63	.2	21	16	345	5.87	9	5	ND	1	14	1	2	5	139	.27	.033	5	38	.41	61	.17	3	3.37	.01	.03	1	1
LS-87 SS 4+75E	1	45	5	67	.1	25	15	147	5.14	10	5	ND	1	11	1	7	2	109	.21	.031	5	34	.22	83	.03	2	2.74	.01	.03	1	1
LS-87 SS 5+00E	1	43	12	57	.1	32	14	241	4.56	7	5	ND	1	13	1	2	2	125	.36	.030	8	44	.48	60	.22	3	3.21	.01	.03	1	5
LS-87 SS 5+25E	1	17	3	69	.1	32	12	586	3.00	4	5	ND	1	13	1	2	2	83	.30	.049	4	45	.30	106	.09	2	1.87	.01	.03	1	1
LS-87 SS 5+50E	1	30	7	81	.2	16	12	1311	3.14	3	5	ND	1	13	1	2	2	84	.37	.179	3	31	.33	67	.15	2	1.88	.01	.02	1	2
LS-87 SS 5+75E	1	31	5	58	.2	33	13	785	3.14	5	5	ND	1	14	1	2	2	82	.26	.059	4	50	.31	67	.05	4	1.88	.01	.03	1	1
STD C/AU-R	21	57	36	133	7.0	63	30	997	3.96	38	16	7	33	48	17	16	20	62	.48	.098	36	58	.88	178	.08	34	1.71	.07	.14	13	52

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE #87-0355

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
LS-87 5S 6+00E	1	85	9	73	.2	85	24	791	4.97	6	5	ND	1	12	1	2	5	126	.25	.068	5	233	2.16	52	.06	5	3.16	.01	.03	1	1
LS-87 5S 6+50E	2	193	11	79	.1	86	30	1083	6.94	8	5	ND	1	8	1	2	4	120	.10	.100	4	222	2.16	37	.01	5	3.12	.01	.03	1	1
LS-87 5S 7+00E	1	63	8	91	.1	41	70	2740	4.32	3	5	ND	1	30	1	2	4	91	.50	.076	6	101	.89	78	.22	5	2.48	.01	.02	1	1
LS-87 5S 7+50E	1	61	2	68	.1	33	15	1080	3.47	53	5	ND	1	12	1	2	2	88	.32	.185	3	64	.65	60	.14	3	2.57	.01	.03	1	1
LS-87 5S 8+00E	1	20	10	-73	.2	11	11	1221	3.28	2	5	ND	1	12	1	2	2	73	.25	.134	4	38	.26	62	.13	2	1.57	.01	.03	1	16
LS-87 6S 6+75W	1	43	5	48	.1	27	13	369	3.63	4	5	ND	1	13	1	2	2	106	.31	.021	7	46	.36	51	.18	3	2.83	.01	.03	1	3
LS-87 6S 6+25W	1	40	5	76	.1	35	12	563	3.78	4	5	ND	1	13	1	2	2	107	.32	.049	4	48	.63	186	.17	3	3.21	.01	.03	1	2
LS-87 6S 5+75W	1	22	8	90	.1	17	11	1331	2.56	3	5	ND	1	21	1	2	5	69	.42	.082	8	27	.42	288	.15	4	1.81	.01	.04	1	1
LS-87 6S 5+25W	1	42	19	96	.1	22	19	1019	5.77	2	5	ND	1	20	1	2	8	127	.29	.123	6	59	.65	259	.23	3	2.66	.01	.04	1	3
LS-87 6S 4+75W	2	49	4	95	.1	25	12	2452	3.16	6	5	ND	1	14	1	2	8	80	.45	.151	5	32	.49	146	.13	4	2.33	.01	.04	1	7
LS-87 6S 4+25W	1	92	10	79	.3	32	17	893	4.16	10	5	ND	1	18	1	2	9	108	.46	.083	6	46	.90	109	.20	5	2.59	.01	.05	1	8
LS-87 6S 3+75W	1	284	13	85	.1	14	33	2346	5.58	6	5	ND	1	55	1	2	4	133	.70	.154	7	26	2.10	66	.18	4	2.98	.01	.08	1	74
LS-87 6S 3+25W	1	19	7	38	.1	17	10	529	3.40	2	5	ND	1	13	1	2	4	91	.28	.023	5	30	.31	74	.13	2	1.74	.01	.02	1	13
LS-87 6S 2+75W	1	67	5	71	.2	27	16	538	4.54	4	5	ND	1	12	1	2	3	115	.31	.059	4	41	.46	76	.23	5	3.28	.01	.03	1	6
LS-87 6S 2+25W	1	93	7	64	.1	30	16	449	4.49	5	5	ND	1	11	1	2	5	127	.30	.062	5	49	.61	59	.25	4	3.65	.01	.03	1	2
LS-87 6S 1+75W	1	94	6	71	.1	22	14	1190	4.05	4	5	ND	1	12	1	2	2	109	.29	.106	4	41	.45	92	.18	2	3.33	.01	.04	1	4
LS-87 6S 1+25W	1	17	2	53	.2	16	10	358	4.02	2	5	ND	1	14	1	2	2	111	.35	.033	4	33	.29	93	.17	3	1.81	.01	.03	1	1
LS-87 6S 0+75W	1	63	2	72	.1	38	16	315	5.14	5	5	ND	1	12	1	2	2	135	.40	.059	3	57	.56	88	.25	6	3.73	.01	.02	1	10
LS-87 6S 0+25W	1	17	4	44	.1	16	9	246	3.15	2	5	ND	1	13	1	2	2	89	.37	.029	3	29	.32	54	.16	3	1.61	.01	.01	1	1
LS-87 6S 0+25E	1	41	6	103	.2	25	12	632	3.77	7	5	ND	1	14	1	2	2	75	.34	.219	3	72	.49	61	.15	5	2.91	.01	.03	1	3
LS-87 6S 0+75E	1	23	4	64	.1	22	10	847	3.09	2	5	ND	1	16	1	2	5	80	.42	.056	3	55	.46	73	.15	4	1.62	.01	.03	1	1
LS-87 6S 1+25E	1	38	11	102	.1	20	14	1974	4.33	2	5	ND	1	27	1	2	2	95	.43	.130	5	31	.38	99	.21	2	2.63	.01	.04	1	7
LS-87 6S 1+75E	1	46	9	75	.2	13	9	812	4.33	4	5	ND	1	13	1	2	4	91	.27	.179	5	32	.40	62	.15	2	3.04	.01	.03	1	1
LS-87 6S 2+25E	1	53	7	72	.2	24	14	401	4.64	2	5	ND	2	12	1	2	2	116	.25	.078	5	40	.36	62	.21	2	3.58	.01	.04	1	6
LS-87 6S 2+75E	1	41	7	67	.2	12	9	495	4.19	2	5	ND	1	14	1	2	2	99	.21	.096	4	28	.20	53	.13	4	2.87	.01	.03	1	1
LS-87 6S 3+25E	1	20	2	49	.1	8	7	333	3.14	2	5	ND	1	14	1	2	2	79	.28	.041	3	23	.27	44	.13	2	1.65	.01	.02	1	4
LS-87 6S 3+75E	1	26	9	83	.1	10	10	383	4.04	2	5	ND	1	12	1	2	2	91	.24	.150	4	30	.23	41	.15	3	2.46	.01	.03	1	1
LS-87 6S 4+25E	1	40	3	89	.1	17	10	1555	3.71	2	5	ND	1	13	1	2	2	82	.33	.318	3	34	.40	78	.16	4	2.29	.01	.02	1	49
LS-87 6S 4+75E	1	23	11	63	.4	41	15	324	4.62	2	6	ND	2	9	1	2	2	110	.17	.037	6	89	1.36	55	.01	4	2.30	.01	.03	1	1
LS-87 6S 5+25E	1	50	2	79	.1	44	16	1798	3.93	2	5	ND	1	11	1	2	2	101	.30	.094	4	50	.48	442	.13	4	2.68	.01	.04	1	3
LS-87 6S 5+75E	1	86	3	89	.1	99	24	252	6.79	17	5	ND	1	5	1	11	2	93	.05	.077	4	109	.19	42	.01	3	1.30	.01	.02	1	7
LS-87 7S 8+00W	1	49	8	77	.1	31	13	666	4.29	5	5	ND	1	13	1	2	2	127	.35	.101	4	52	.60	104	.27	5	3.64	.01	.04	1	7
LS-87 7S 7+50W	1	23	16	80	.2	21	13	1555	3.27	4	5	ND	1	14	1	2	2	84	.33	.063	10	33	.32	131	.22	2	2.43	.01	.03	1	1
LS-87 7S 7+00W	1	18	5	90	.1	24	11	616	3.92	4	5	ND	1	13	1	2	2	106	.35	.093	3	37	.41	130	.23	5	2.77	.01	.03	1	5
LS-87 7S 6+75W	1	55	9	80	.1	27	13	1083	3.81	8	5	ND	1	12	1	2	2	106	.42	.105	4	34	.52	124	.22	5	2.48	.01	.03	1	1
LS-87 7S 6+50W	1	22	5	98	.2	17	14	2760	4.07	7	5	ND	1	12	1	2	2	91	.32	.147	4	29	.32	198	.15	2	1.87	.01	.03	1	5
STD C/AU-S	19	59	41	132	7.0	64	29	979	3.93	38	15	7	32	47	16	15	19	60	.48	.096	35	57	.88	174	.08	37	1.72	.07	.14	12	49

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE #87-0355

PAGE 11

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS-87 7S 6+25W	2	72	2	61	.1	23	11	1019	2.08	8	5	ND	1	5	1	3	2	58	.12	.069	6	20	.33	57	.08	2	1.62	.01	.02	1	1
LS-87 7S 6+00W	1	51	55	90	.1	28	14	2004	3.29	7	5	ND	1	13	1	2	3	84	.36	.096	5	37	.42	111	.14	16	2.21	.01	.02	1	1
LS-87 7S 5+75W	1	65	5	95	.1	33	14	1045	3.76	10	5	ND	1	12	1	2	2	104	.34	.125	4	46	.54	81	.17	4	3.01	.01	.02	2	1
LS-87 7S 5+50W	1	34	4	128	.1	37	13	1759	3.72	3	5	ND	1	17	1	2	2	96	.45	.106	5	40	.48	125	.18	2	2.44	.01	.03	1	2
LS-87 7S 5+25W	1	28	10	123	.4	33	14	848	3.19	5	5	ND	1	15	1	3	7	73	.34	.085	10	31	.56	141	.10	3	2.33	.01	.04	1	1
LS-87 7S 5+00W	1	57	9	101	.3	62	17	444	4.34	12	5	ND	1	13	1	2	2	108	.30	.066	8	51	.54	85	.18	3	3.44	.01	.04	1	1
LS-87 7S 4+75W	1	19	3	113	.2	16	10	1057	2.59	4	5	ND	1	14	1	2	2	66	.38	.143	4	26	.28	105	.12	2	1.61	.01	.03	1	1
LS-87 7S 4+50W	1	27	2	131	.1	22	12	2095	2.72	4	5	ND	1	14	1	2	3	69	.34	.126	6	29	.33	116	.15	2	2.01	.01	.03	1	1
LS-87 7S 4+25W	1	66	19	104	.1	22	15	3649	3.83	2	5	ND	1	14	1	2	2	88	.26	.252	8	37	.39	221	.18	6	2.67	.01	.04	1	2
LS-87 7S 4+00W	1	109	2	74	.1	33	16	944	4.53	4	5	ND	1	15	1	2	4	136	.32	.125	5	53	.62	100	.23	6	3.76	.01	.04	1	1
LS-87 7S 3+75W	1	48	7	111	.1	20	15	6360	4.14	2	5	ND	1	17	1	2	2	94	.33	.278	4	43	.38	190	.15	2	2.48	.01	.03	1	1
LS-87 7S 3+50W	1	76	2	62	.1	27	15	596	4.32	2	5	ND	1	16	1	2	2	113	.31	.060	4	40	.45	95	.20	2	2.79	.01	.04	1	1
LS-87 7S 3+25W	1	98	3	58	.1	32	16	314	4.68	3	5	ND	2	14	1	2	2	131	.30	.025	6	52	.70	73	.21	9	3.86	.01	.04	2	16
LS-87 7S 3+00W	1	84	2	61	.1	26	16	372	4.60	2	5	ND	1	14	1	2	3	121	.30	.050	7	47	.50	57	.21	5	3.42	.01	.03	1	1
LS-87 7S 2+75W	1	69	4	68	.1	34	16	743	4.64	8	5	ND	1	12	1	2	2	121	.38	.065	6	49	.60	83	.23	5	3.20	.01	.04	3	1
LS-87 7S 2+50W	1	65	4	64	.1	34	15	366	5.16	5	5	ND	2	13	1	2	2	138	.27	.048	5	57	.59	108	.29	6	4.46	.01	.04	2	2
LS-87 7S 2+25W	1	46	2	76	.1	7	14	1273	5.74	3	5	ND	1	15	1	2	2	120	.26	.230	4	30	.42	91	.15	7	1.82	.01	.04	1	1
LS-87 7S 2+00W	1	56	4	60	.2	18	15	979	4.41	2	5	ND	1	12	1	2	4	106	.28	.151	9	45	.42	77	.19	2	3.65	.01	.04	2	1
LS-87 7S 1+75W	1	87	9	122	.1	16	19	2573	6.27	7	5	ND	1	28	1	2	3	146	.33	.087	4	45	.81	96	.25	5	2.59	.01	.04	1	8
LS-87 7S 1+50W	1	36	4	78	.1	27	14	491	4.50	2	5	ND	1	16	1	2	2	119	.28	.062	5	48	.52	145	.23	5	3.27	.01	.03	1	1
LS-87 7S 1+25W	1	52	2	73	.1	34	15	401	4.98	2	5	ND	2	13	1	2	2	136	.26	.054	5	59	.62	130	.25	6	4.02	.01	.04	1	1
LS-87 7S 1+00W	1	33	6	76	.3	26	12	803	3.66	2	5	ND	1	13	1	2	2	96	.36	.094	4	44	.38	140	.18	2	2.26	.01	.04	1	1
LS-87 7S 0+75W	1	48	4	101	.4	55	18	1791	4.58	25	5	ND	1	11	1	6	3	102	.29	.127	4	83	.54	169	.09	5	2.69	.01	.04	1	2
LS-87 7S 0+50W	1	69	5	78	.1	30	15	893	4.70	5	5	ND	1	15	1	2	3	112	.38	.146	4	65	.61	68	.21	3	3.05	.01	.04	1	1
LS-87 7S 0+25W	1	45	4	86	.2	24	14	2610	3.92	2	5	ND	1	13	1	2	2	94	.33	.103	5	41	.35	158	.18	2	2.62	.01	.02	1	1
LS-87 7S 0+00W	1	68	6	52	.2	30	13	430	4.23	2	5	ND	1	12	1	2	2	117	.30	.028	4	48	.56	86	.20	3	3.18	.01	.03	1	2
LS-87 7S 0+25E	1	77	4	61	.1	31	16	382	3.91	5	5	ND	1	14	1	2	2	108	.32	.032	7	56	.73	107	.19	2	3.53	.01	.05	2	2
LS-87 7S 0+50E	1	57	8	72	.1	33	15	700	4.31	4	5	ND	1	13	1	2	3	112	.32	.047	5	52	.58	123	.21	5	3.42	.01	.03	1	1
LS-87 7S 0+75E	2	40	12	105	.1	20	15	2669	3.13	2	5	ND	1	21	1	2	2	69	.33	.338	8	37	.32	205	.12	3	3.29	.01	.05	2	1
LS-87 7S 1+00E	1	38	12	122	.1	26	25	2302	3.75	3	5	ND	1	21	1	2	2	69	.30	.167	9	33	.25	131	.17	2	2.84	.01	.04	1	38
LS-87 7S 1+25E	1	39	6	90	.1	19	14	1038	5.75	2	5	ND	1	18	1	3	2	112	.24	.166	8	46	.32	130	.09	2	3.21	.01	.07	2	7
LS-87 7S 1+50E	1	38	9	63	.3	16	13	815	5.59	3	5	ND	2	11	1	3	2	117	.22	.129	7	39	.41	87	.20	2	3.57	.01	.04	2	2
LS-87 7S 1+75E	1	68	9	54	.1	26	13	418	3.92	3	5	ND	1	15	1	2	2	110	.30	.057	4	49	.61	60	.21	2	3.63	.01	.05	1	2
LS-87 7S 2+00E	2	31	5	48	.1	18	11	230	3.77	2	5	ND	1	16	1	2	2	100	.31	.049	6	37	.44	55	.20	5	2.96	.01	.03	1	3
LS-87 7S 2+25E	1	49	7	73	.1	33	13	547	4.30	4	5	ND	1	15	1	2	2	115	.34	.077	3	48	.51	97	.21	3	3.91	.01	.05	1	3
LS-87 7S 2+50E	1	44	8	83	.2	24	12	858	3.91	2	5	ND	1	18	1	2	5	84	.39	.202	5	40	.40	91	.17	5	2.92	.01	.05	2	1
STD C/AU-S	21	57	38	133	7.1	66	29	993	3.95	40	15	8	33	48	17	14	22	61	.48	.102	35	59	.88	178	.08	35	1.71	.07	.14	12	47

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE #87-0355

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mi PPM	Co PPM	Mn PPM	Fe I PPM	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca I PPM	P I PPM	La PPM	Cr PPM	Mg I PPM	Ba PPM	Ti I PPM	B PPM	Al I PPM	Na I PPM	K I PPM	M PPM	Au#1 PPB
LS-87 7+25S 3+50M	1	166	7	108	.2	22	20	1330	5.34	4	5	ND	1	27	1	3	2	129	.36	.074	4	32	.48	107	.24	5	2.77	.01	.05	1	63
LS-87 7+25S 3+25M	1	134	15	75	.3	40	18	484	5.63	4	5	ND	2	15	1	5	2	156	.39	.063	5	58	.64	104	.25	2	4.52	.01	.05	1	1
LS-87 7+25S 3+00M	1	82	7	75	.1	35	16	488	4.98	5	5	ND	1	14	1	3	2	143	.36	.053	5	52	.55	83	.27	2	3.75	.01	.04	1	4
LS-87 7+25S 2+75M	1	51	10	94	.1	26	15	3729	3.81	6	5	ND	1	18	1	2	2	97	.43	.125	5	41	.57	182	.18	5	2.92	.01	.04	1	1
LS-87 7+25S 2+50M	1	94	9	78	.1	36	17	500	5.12	7	5	ND	2	15	1	3	2	150	.33	.061	7	58	.70	88	.27	11	4.18	.01	.05	2	4
LS-87 7+25S 2+25M	1	92	11	96	.2	31	18	1043	5.75	6	5	ND	2	16	1	4	2	149	.32	.164	6	46	.50	114	.22	2	3.92	.01	.04	2	7
LS-87 7+25S 2+00M	1	261	4	92	.1	40	24	747	5.43	2	5	ND	1	23	1	3	2	157	.42	.137	6	84	.84	84	.25	6	3.60	.01	.05	2	3
LS-87 7+50S 3+25M	1	94	8	119	.1	15	19	2009	4.77	3	5	ND	1	28	1	3	2	96	.32	.173	4	35	.37	130	.18	7	2.47	.01	.05	1	12
LS-87 7+50S 3+00M	1	92	7	80	.1	25	14	405	4.83	2	5	ND	1	16	1	2	2	130	.29	.091	4	47	.48	86	.24	3	3.81	.01	.04	1	2
LS-87 7+50S 2+75M	1	105	10	66	.1	30	15	740	4.03	6	5	ND	1	17	1	2	2	117	.38	.062	7	56	.72	85	.22	5	3.99	.01	.05	1	1
LS-87 7+50S 2+50M	1	48	10	81	.2	25	15	785	4.79	4	5	ND	1	19	1	3	2	131	.38	.113	4	38	.68	111	.21	4	3.52	.01	.07	2	14
LS-87 7+50S 2+25M	1	107	10	77	.2	35	17	513	5.42	7	5	ND	2	20	1	5	2	164	.35	.057	4	61	.86	95	.31	3	4.30	.01	.05	2	4
LS-87 7+50S 2+00M	1	41	7	67	.1	16	11	509	3.17	4	5	ND	1	23	1	2	4	88	.40	.084	4	31	.48	85	.16	6	1.80	.01	.02	1	4
LS-87 7+75S 3+25M	1	88	13	77	.2	34	15	474	4.98	11	5	ND	2	15	1	5	2	144	.31	.077	5	58	.74	80	.25	6	4.53	.01	.05	1	1
LS-87 7+75S 3+00M	1	94	15	65	.1	38	17	536	5.22	8	5	ND	2	17	1	3	2	150	.32	.047	7	57	.67	102	.25	4	4.28	.01	.05	1	10
LS-87 7+75S 2+75M	1	25	6	57	.1	19	9	569	3.31	2	5	ND	1	18	1	2	2	93	.32	.039	4	31	.37	96	.19	3	2.04	.01	.03	1	1
LS-87 7+75S 2+50M	1	30	10	64	.1	19	12	1139	3.28	5	5	ND	1	19	1	2	2	96	.38	.058	4	29	.40	107	.19	5	2.16	.01	.04	1	1
LS-87 7+75S 2+25M	1	30	8	69	.1	11	14	2458	2.96	3	5	ND	1	60	1	2	3	99	.48	.038	2	43	1.42	66	.14	5	1.64	.01	.04	1	8
LS-87 7+75S 2+00M	1	22	11	78	.2	3	12	1888	3.54	3	5	ND	1	66	1	2	3	108	.49	.068	3	23	.37	91	.18	7	1.23	.01	.05	1	1
LS-87 8S 6+75M	1	33	15	130	.1	24	14	2948	4.16	4	5	ND	1	16	1	2	2	103	.46	.264	5	36	.38	243	.22	4	2.26	.01	.05	1	2
LS-87 8S 6+50M	1	44	6	83	.1	19	14	1085	4.57	2	5	ND	1	18	1	2	2	142	.49	.051	4	33	.54	145	.19	9	2.56	.01	.05	1	1
LS-87 8S 6+25M	1	56	15	70	.1	36	15	647	4.24	21	5	ND	1	13	1	3	2	104	.36	.025	6	49	.73	111	.11	4	2.81	.01	.03	1	4
LS-87 8S 6+00M	1	27	9	97	.2	24	13	1143	3.97	8	5	ND	1	15	1	2	2	106	.32	.044	4	35	.37	147	.19	8	2.31	.01	.04	1	1
LS-87 8S 5+75M	2	32	9	120	.1	25	15	2869	3.41	30	5	ND	1	19	1	3	2	58	.23	.083	10	21	.40	281	.01	3	2.33	.01	.06	1	1
LS-87 8S 5+50M	1	9	9	66	.4	17	7	1440	1.64	8	5	ND	1	16	1	3	2	42	.28	.029	5	15	.29	109	.03	5	1.25	.01	.03	1	3
LS-87 8S 5+25M	1	6	11	123	.2	16	7	2164	1.78	3	5	ND	1	13	1	2	5	48	.26	.046	5	22	1.05	95	.05	7	1.81	.01	.03	1	1
LS-87 8S 5+00M	1	40	10	87	.4	30	12	917	3.42	3	5	ND	1	15	1	5	3	97	.35	.060	7	37	.60	94	.14	2	2.82	.01	.03	1	1
LS-87 8S 4+75M	1	22	6	123	.1	21	10	3155	2.81	3	5	ND	1	21	1	2	2	72	.45	.148	6	28	.36	162	.15	2	1.90	.01	.03	1	1
LS-87 8S 4+50M	1	23	12	142	.1	27	12	2171	3.17	8	5	ND	1	15	1	3	2	76	.43	.226	6	31	.44	110	.13	9	2.05	.01	.03	1	1
LS-87 8S 4+25M	1	90	11	108	.5	37	19	676	5.31	5	5	ND	2	18	1	3	2	140	.34	.140	20	63	.45	105	.25	8	4.38	.02	.06	1	1
LS-87 8S 4+00M	1	246	16	70	.1	34	25	1542	4.92	8	5	ND	1	20	1	2	2	138	.51	.099	7	63	.95	94	.23	7	3.53	.01	.05	1	2
LS-87 8S 3+75M	1	97	8	86	.1	35	19	1527	4.86	2	5	ND	1	21	1	3	2	129	.41	.059	8	54	.85	100	.25	6	3.58	.01	.05	1	2
LS-87 8S 3+50M	1	757	14	102	.1	27	22	2475	5.98	2	5	ND	1	91	1	2	2	154	1.05	.147	7	42	2.65	72	.22	4	3.24	.01	.08	1	109
LS-87 8S 3+25M	2	154	95	69	.2	28	23	1303	7.86	13	5	ND	1	33	1	8	2	123	.69	.091	6	59	.85	71	.21	9	2.36	.03	.06	1	22
LS-87 8S 3+00M	2	127	15	61	.1	28	18	2351	4.79	5	5	ND	1	23	1	2	2	137	.58	.052	12	53	.70	102	.21	7	3.65	.01	.04	1	1
LS-87 8S 2+75M	1	49	8	68	.1	27	15	2258	4.17	5	5	ND	1	22	1	2	2	116	.45	.064	5	42	.58	137	.21	5	3.12	.01	.05	1	1
STD C/AU-S	20	58	41	135	6.8	65	29	1013	3.93	39	16	7	32	47	18	16	21	62	.48	.106	35	59	.88	175	.08	38	1.71	.07	.14	12	50

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	N PPM	Au#1 PPB
LS-87 8S 2+50W	1	47	4	53	.1	28	13	369	4.87	8	5	ND	1	12	1	2	5	137	.27	.039	4	47	.50	107	.24	4	3.33	.01	.04	1	8
LS-87 8S 2+25W	1	56	12	65	.1	26	14	1314	4.61	8	5	ND	1	15	1	2	2	125	.30	.084	3	45	.51	135	.25	3	3.26	.01	.04	1	1
LS-87 8S 2+00W	1	45	6	57	.2	21	10	932	3.20	6	5	ND	2	11	1	2	2	88	.23	.094	4	35	.35	111	.17	5	2.40	.01	.03	1	3
LS-87 8S 1+75W	1	51	8	60	.2	27	14	561	4.43	7	5	ND	1	19	1	2	2	120	.40	.037	7	49	.57	147	.21	5	3.12	.01	.04	1	1
LS-87 8S 1+50W	1	120	2	63	.1	39	20	738	5.16	8	5	ND	1	15	1	2	4	138	.36	.040	5	64	.62	148	.20	3	4.11	.01	.05	1	1
LS-87 8S 1+25W	1	45	5	69	.2	36	15	879	4.83	8	5	ND	1	13	1	2	5	124	.28	.068	4	59	.55	157	.22	3	3.11	.01	.05	2	1
LS-87 8S 1+00W	1	78	7	62	.3	41	17	683	4.11	12	5	ND	1	12	1	2	2	113	.34	.034	4	68	.80	184	.13	2	3.42	.01	.04	1	2
LS-87 8S 0+75W	1	52	4	71	.3	30	15	1260	4.39	8	5	ND	1	17	1	2	4	116	.52	.070	4	49	.54	141	.19	5	3.11	.01	.05	1	1
LS-87 8S 0+50W	2	43	7	96	.1	35	24	7512	2.61	6	5	ND	1	34	1	2	2	59	.79	.064	3	162	.69	202	.16	3	1.18	.01	.04	1	3
LS-87 8S 0+25W	1	73	9	64	.1	44	22	1239	5.07	7	5	ND	1	34	1	2	2	126	.88	.043	7	142	1.00	104	.22	3	3.40	.01	.04	1	1
LS-87 8S 0+00W	1	55	12	48	.1	38	17	542	5.62	7	5	ND	1	29	1	2	3	136	.72	.040	14	129	.46	73	.26	2	3.06	.01	.03	3	3
LS-87 8S 0+25E	3	39	12	171	.1	15	16	13765	3.59	2	5	ND	1	28	1	2	2	52	.37	.263	5	24	.15	426	.10	3	2.05	.01	.07	1	1
LS-87 8S 0+50E	1	14	11	94	.1	10	11	1722	4.09	2	5	ND	1	25	1	2	2	79	.29	.145	4	30	.23	95	.12	2	2.34	.01	.05	1	1
LS-87 8S 0+75E	1	76	10	58	.1	30	15	356	4.20	7	5	ND	1	14	1	2	5	116	.29	.054	7	54	.59	72	.18	3	3.88	.01	.04	1	1
LS-87 8S 1+00E	4	49	6	56	.1	34	15	282	5.43	9	5	ND	1	20	1	2	3	138	.58	.046	8	54	.55	62	.20	6	3.80	.01	.04	2	1
LS-87 8S 1+25E	2	60	4	69	.1	36	16	500	5.09	7	5	ND	1	16	1	2	5	125	.37	.057	4	48	.64	95	.21	6	3.90	.01	.04	2	1
LS-87 8S 1+50E	2	13	8	67	.2	6	10	654	3.56	4	5	ND	1	24	1	2	4	98	.31	.040	6	9	.23	63	.11	2	2.22	.01	.05	2	1
LS-87 8S 1+75E	1	20	11	37	.2	7	6	499	2.68	2	5	ND	1	20	1	2	3	58	.23	.051	5	11	.15	94	.11	6	1.08	.01	.04	1	40
LS-87 8S 2+00E	1	33	12	58	.1	12	12	809	4.78	8	5	ND	1	18	1	2	2	115	.27	.087	4	26	.39	72	.15	3	2.41	.01	.04	1	37
LS-87 8S 2+25E	2	16	19	90	.1	9	10	7282	2.57	3	5	ND	1	43	1	2	2	60	.63	.140	4	15	.19	234	.09	5	1.27	.01	.07	1	4
LS-87 8S 2+50E	1	29	5	77	.2	29	14	1482	3.32	3	5	ND	1	20	1	2	2	93	.44	.086	3	53	.74	74	.18	4	2.71	.01	.05	1	1
LS-87 9S 6+75W	1	51	6	113	.2	29	13	749	4.00	8	5	ND	1	13	1	2	4	95	.31	.129	5	38	.54	189	.13	5	2.96	.01	.05	1	2
LS-87 9S 6+25W	1	27	14	52	.1	21	11	478	3.80	4	5	ND	1	28	1	2	2	104	1.31	.030	5	40	.35	53	.19	5	2.39	.01	.02	1	1
LS-87 9S 5+75W	1	24	7	71	.1	33	12	763	3.79	7	5	ND	1	16	1	2	2	88	.34	.023	5	36	.63	81	.12	2	2.35	.01	.03	1	1
LS-87 9S 5+25W	1	36	2	70	.1	25	11	1342	3.22	8	5	ND	1	19	1	2	2	89	.36	.073	8	35	.45	171	.17	2	2.52	.01	.03	1	1
LS-87 9S 4+75W	1	26	10	119	.1	31	13	3164	3.55	3	5	ND	1	19	1	2	3	80	.32	.102	9	35	.37	189	.17	2	2.52	.01	.06	1	1
LS-87 9S 4+25W	1	19	4	58	.1	19	10	650	2.63	5	5	ND	1	16	1	2	4	71	.32	.060	3	27	.36	104	.14	2	2.09	.01	.04	1	1
LS-87 9S 3+75W	1	102	2	98	.1	10	16	5316	2.87	2	5	ND	1	19	1	2	2	140	.24	.072	7	10	.47	440	.04	2	3.01	.01	.10	1	1
LS-87 9S 3+25W	1	58	11	58	.2	25	13	1118	3.90	5	5	ND	1	21	1	2	2	104	.59	.079	5	37	.50	123	.17	5	2.84	.01	.04	2	1
LS-87 9S 2+75W	1	48	2	117	.2	6	12	1076	3.69	3	5	ND	1	37	1	2	2	107	.46	.104	3	15	.54	231	.13	2	2.28	.01	.04	1	1
LS-87 9S 2+25W	1	28	7	49	.1	24	11	531	4.21	4	5	ND	1	19	1	2	3	116	.40	.033	3	36	.43	157	.17	3	2.28	.01	.04	3	1
LS-87 9S 1+75W	1	44	8	63	.1	23	12	822	4.18	7	5	ND	1	14	1	2	2	114	.31	.067	4	37	.31	170	.19	3	2.54	.01	.03	2	1
LS-87 9S 1+25W	1	33	2	58	.1	56	18	552	4.79	5	5	ND	1	11	1	2	4	122	.23	.026	4	135	.95	183	.02	2	2.69	.01	.04	1	1
LS-87 9S 0+75W	1	72	9	65	.1	41	17	702	4.89	13	5	ND	1	18	1	2	2	129	.43	.041	8	79	.65	188	.13	5	4.19	.02	.04	1	1
LS-87 9S 0+25W	1	45	14	64	.1	31	13	1790	3.74	3	5	ND	1	28	1	2	2	87	.89	.057	7	51	.52	98	.15	4	2.92	.01	.04	2	1
LS-87 9S 0+25E	1	29	2	65	.2	26	12	1118	4.02	6	5	ND	1	16	1	2	2	101	.42	.056	5	37	.40	146	.17	4	2.48	.01	.04	1	1
STD C/AU-S	21	58	37	131	6.9	64	28	988	3.94	37	19	7	33	47	17	16	20	61	.48	.098	35	56	.88	175	.08	36	1.71	.07	.13	13	49

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
LS-87 9S 0+75E	2	14	4	31	.1	5	6	1490	1.81	4	5	ND	1	7	1	2	4	51	.07	.059	3	6	.08	58	.02	2	.95	.01	.04	1	1
LS-87 9S 1+25E	2	40	2	61	.1	25	14	687	4.51	4	5	ND	1	18	1	2	4	130	.37	.066	4	47	.54	87	.26	4	3.08	.01	.02	1	13
LS-87 9S 1+75E	1	61	9	68	.1	32	16	1058	4.66	5	5	ND	1	19	1	2	2	125	.34	.112	5	45	.44	94	.22	2	2.97	.01	.05	1	5
LS-87 9S 2+25E	1	29	3	50	.1	22	11	1011	3.39	5	5	ND	1	18	1	2	2	94	.39	.037	5	37	.45	134	.13	2	2.07	.01	.02	1	1
LS-87 10S 6+50W	1	45	18	62	.1	28	16	515	4.32	8	5	ND	1	19	1	2	2	122	.54	.027	5	50	.60	109	.22	2	2.74	.02	.03	1	1
LS-87 10S 6+25W	1	40	17	98	.1	25	13	926	3.89	5	5	ND	1	21	1	2	2	104	.44	.057	7	41	.45	171	.23	2	3.10	.02	.05	1	1
LS-87 10S 6+00W	1	38	2	94	.3	36	15	666	4.28	11	5	ND	1	19	1	3	2	123	.39	.081	5	47	.54	152	.24	3	3.37	.01	.05	1	4
LS-87 10S 5+75W	1	35	8	93	.1	29	14	1227	3.79	3	5	ND	1	22	1	2	2	99	.43	.103	7	39	.43	183	.20	2	2.90	.01	.06	1	52
LS-87 10S 5+50W	1	24	27	164	.1	18	13	8201	3.19	4	5	ND	1	36	1	2	2	69	.69	.279	7	26	.34	775	.08	2	2.12	.01	.11	1	1
LS-87 10S 5+25W	1	29	17	98	.2	19	10	2412	3.49	3	5	ND	1	14	1	2	2	84	.29	.198	6	28	.27	264	.10	4	2.20	.01	.05	1	1
LS-87 10S 5+00W	1	32	7	112	.2	33	12	931	3.35	8	5	ND	1	13	1	2	2	90	.28	.118	4	34	.40	153	.15	2	3.16	.01	.05	1	1
LS-87 10S 4+75W	1	24	7	70	.2	28	10	407	2.92	8	5	ND	1	14	1	2	2	78	.25	.042	4	28	.38	123	.13	4	2.33	.01	.04	1	1
LS-87 10S 4+50W	1	22	7	88	.2	27	9	1852	3.16	5	5	ND	1	13	1	2	2	77	.24	.093	5	29	.28	180	.13	2	2.30	.01	.04	1	2
LS-87 10S 4+25W	1	58	3	63	.1	32	13	452	3.69	7	5	ND	1	13	1	2	2	105	.31	.047	3	38	.61	151	.17	3	3.07	.01	.04	1	1
LS-87 10S 4+00W	1	57	10	97	.1	19	15	2446	3.71	6	5	ND	1	21	1	2	2	94	.35	.112	5	29	.42	288	.09	3	2.76	.01	.06	1	4
LS-87 10S 3+75W	1	67	2	66	.2	30	15	745	4.38	10	5	ND	1	14	1	2	2	124	.33	.067	6	49	.64	163	.21	4	3.56	.01	.05	1	2
LS-87 10S 3+50W	1	34	6	71	.1	27	12	511	3.46	4	5	ND	1	18	1	2	2	97	.30	.033	4	34	.49	151	.11	3	2.75	.01	.04	1	1
LS-87 10S 3+25W	1	51	10	61	.1	26	13	512	4.07	5	5	ND	1	17	1	2	2	112	.36	.031	4	36	.54	185	.14	2	2.76	.01	.03	1	1
LS-87 10S 3+00W	1	92	9	82	.1	33	17	1351	4.94	17	5	ND	1	32	1	2	2	114	.76	.097	10	56	.78	330	.15	4	3.90	.02	.06	1	3
LS-87 10S 2+75W	1	40	7	65	.1	26	14	1472	4.44	6	5	ND	1	24	1	2	2	112	.71	.056	8	40	.47	209	.19	5	2.45	.01	.04	1	1
LS-87 10S 2+50W	1	60	6	82	.1	41	19	1004	5.69	11	5	ND	1	16	1	2	2	147	.37	.092	4	77	.90	154	.23	3	3.91	.01	.04	1	1
LS-87 10S 2+25W	1	68	3	84	.2	38	18	742	5.26	11	5	ND	1	18	1	2	2	138	.27	.054	7	76	1.16	165	.06	3	3.69	.01	.05	1	2
LS-87 10S 2+00W	1	43	6	90	.1	40	18	2106	5.08	8	5	ND	1	22	1	2	2	118	.61	.041	9	78	.83	275	.20	4	3.62	.02	.05	1	1
LS-87 10S 1+75W	1	32	5	62	.2	55	19	361	6.27	28	5	ND	1	9	1	8	2	155	.15	.033	2	160	.85	203	.01	2	2.74	.01	.06	2	3
LS-87 10S 1+50W	1	28	12	39	.3	33	13	442	4.96	15	5	ND	1	26	1	3	2	128	.77	.027	6	77	.48	155	.12	2	3.13	.02	.02	1	1
LS-87 10S 1+25W	1	44	9	89	.1	37	20	2533	5.04	12	5	ND	1	25	1	2	2	130	.40	.075	5	78	.42	196	.16	2	2.70	.01	.06	1	1
LS-87 10S 1+00W	1	60	10	98	.1	39	18	2635	4.95	10	5	ND	1	22	1	2	2	122	.44	.086	7	61	.59	257	.20	3	3.53	.02	.08	1	6
LS-87 10S 0+75W	1	34	12	88	.2	25	13	3140	3.89	6	5	ND	1	16	1	2	2	101	.31	.121	4	48	.41	188	.19	2	2.59	.01	.06	1	1
LS-87 10S 0+50W	1	33	7	52	.1	22	11	686	3.66	2	5	ND	1	19	1	2	2	103	.38	.040	4	37	.48	96	.18	2	2.30	.01	.03	1	2
LS-87 10S 0+25W	1	35	8	75	.1	18	12	1281	3.57	2	5	ND	1	29	1	2	4	100	.37	.048	4	34	.41	147	.14	2	2.15	.01	.05	1	2
LS-87 10S 0+00W	1	43	6	59	.4	13	12	278	4.50	5	5	ND	1	27	1	2	2	86	.21	.055	5	21	.53	71	.07	2	2.30	.01	.07	1	6
LS-87 10S 0+25E	1	24	9	90	.2	18	17	6438	4.83	6	5	ND	1	29	1	2	3	114	.47	.062	7	38	.36	224	.17	6	2.87	.01	.07	1	1
LS-87 10S 0+50E	1	32	8	82	.1	18	13	2186	3.96	4	5	ND	1	17	1	2	2	93	.32	.127	10	27	.33	286	.11	2	2.68	.01	.06	1	1
LS-87 10S 0+75E	1	44	3	78	.1	14	10	538	3.83	6	5	ND	1	15	1	2	2	90	.29	.122	6	29	.37	99	.17	2	2.76	.01	.04	1	13
LS-87 10S 1+00E	1	30	7	68	.1	18	11	613	3.52	2	5	ND	1	24	1	2	2	88	.39	.121	4	35	.65	87	.15	2	2.39	.01	.04	1	1
LS-87 10S 1+25E	1	36	2	86	.1	26	12	966	3.25	3	5	ND	1	13	1	2	2	88	.43	.131	3	31	.44	106	.13	5	2.29	.01	.03	1	1
STD C/AU-S	21	58	39	135	6.9	67	30	995	3.96	40	16	7	32	47	17	16	20	61	.48	.097	35	56	.88	176	.08	34	1.71	.07	.14	13	53

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE #87-0355

PAGE 15

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS-87 10S 1+50E	1	59	2	88	.1	29	14	652	3.54	2	5	ND	1	31	1	2	2	91	.54	.132	4	52	.92	87	.16	2	2.77	.01	.03	1	48
LS-87 10S 1+75E	1	16	4	49	.2	15	9	668	3.36	2	5	ND	1	22	1	2	2	101	.51	.031	4	32	.39	69	.19	4	1.77	.01	.02	1	1
LS-87 10S 2+00E	2	27	6	54	.2	22	11	333	3.89	2	5	ND	1	19	1	2	2	112	.34	.038	4	43	.44	74	.16	2	2.54	.01	.03	1	1
LS-87 10S 2+25E	1	30	13	93	.1	21	12	1036	4.28	2	5	ND	1	16	1	2	2	103	.31	.233	4	46	.37	102	.15	2	3.02	.01	.03	1	2
LS-87 10S 2+50E	1	14	5	79	.2	10	8	914	3.19	2	5	ND	1	22	1	2	3	82	.39	.136	4	30	.32	83	.13	2	2.01	.01	.03	1	8
LS-87 11S 5+50W	1	52	32	74	.3	19	14	758	4.46	2	5	ND	1	16	1	2	3	128	.32	.039	7	34	.59	195	.05	4	3.23	.01	.06	1	1
LS-87 11S 5+25W	1	28	8	141	.1	18	12	2474	3.69	2	5	ND	1	17	1	2	2	95	.36	.121	4	28	.40	339	.06	3	2.42	.01	.05	1	8
LS-87 11S 5+00W	1	38	14	111	.1	22	13	3156	3.82	3	5	ND	1	21	1	2	2	101	.57	.116	4	37	.38	241	.17	7	2.62	.01	.03	1	6
LS-87 11S 4+75W	1	32	9	213	.1	15	16	4015	4.22	2	5	ND	1	17	1	2	2	92	.31	.314	4	31	.20	279	.10	5	2.66	.01	.05	1	2
LS-87 11S 4+50W	1	32	3	88	.1	37	15	1186	4.29	4	5	ND	1	18	1	2	2	113	.38	.043	5	44	.50	227	.08	7	2.83	.01	.03	1	4
LS-87 11S 4+25W	1	24	10	176	.3	24	18	3101	5.10	3	5	ND	1	14	1	2	2	103	.21	.177	6	43	.27	304	.06	5	3.01	.01	.06	1	2
LS-87 11S 4+00W	1	16	13	67	.1	15	12	6497	3.36	2	5	ND	1	16	1	2	2	73	.16	.113	4	36	.20	213	.02	3	1.67	.01	.06	1	1
LS-87 11S 3+75W	1	58	14	104	.1	32	16	1348	5.20	7	5	ND	1	15	1	2	2	138	.29	.161	6	61	.35	155	.18	8	4.46	.01	.04	1	13
LS-87 11S 3+50W	1	52	5	98	.1	33	16	1045	4.67	2	5	ND	1	13	1	2	2	120	.27	.091	7	55	.50	152	.14	8	4.03	.01	.04	1	1
LS-87 11S 3+25W	1	35	2	74	.1	30	13	998	3.80	2	5	ND	1	15	1	2	2	101	.28	.075	4	47	.49	136	.12	3	3.55	.01	.05	1	1
LS-87 11S 3+00W	1	37	9	103	.1	29	14	2360	4.18	3	5	ND	1	16	1	2	3	104	.30	.198	4	47	.44	177	.13	4	3.35	.01	.04	1	1
LS-87 11S 2+75W	1	29	3	58	.2	26	13	321	4.53	2	5	ND	1	15	1	2	2	125	.32	.027	4	42	.44	112	.13	3	2.60	.01	.02	1	1
LS-87 11S 2+50W	2	88	2	75	.2	35	17	545	4.49	12	5	ND	1	16	1	12	2	151	.22	.061	6	95	.86	125	.01	4	3.98	.01	.05	1	9
LS-87 11S 2+25W	1	43	2	116	.1	51	27	4449	5.06	11	5	ND	1	9	1	16	2	133	.15	.102	4	144	1.42	278	.01	2	3.31	.01	.05	1	1
LS-87 11S 2+00W	1	51	7	80	.2	39	16	1935	4.31	2	5	ND	1	20	1	2	2	112	.36	.109	5	74	.57	200	.17	3	3.20	.01	.04	1	1
LS-87 11S 1+75W	1	65	12	75	.3	54	20	885	5.02	3	5	ND	1	16	1	4	2	132	.26	.078	5	91	.59	177	.11	5	3.31	.01	.05	1	1
LS-87 11S 1+50W	1	54	6	80	.1	30	16	1096	5.11	2	5	ND	1	15	1	2	2	134	.27	.117	7	79	.34	157	.20	2	4.05	.01	.04	1	8
LS-87 11S 1+25W	1	37	7	61	.1	25	11	531	3.64	2	5	ND	1	16	1	2	3	102	.33	.042	4	47	.46	143	.16	2	3.20	.01	.03	1	1
LS-87 11S 1+00W	1	56	10	106	.1	29	14	1065	4.57	5	5	ND	1	31	1	2	2	119	.46	.161	6	76	.41	138	.19	5	2.97	.01	.05	1	1
LS-87 11S 0+75W	1	108	15	115	.1	30	20	1460	4.35	2	5	ND	1	21	1	2	4	156	.38	.140	10	47	.75	209	.08	7	3.54	.01	.07	1	2
LS-87 11S 0+50W	1	47	5	86	.1	52	15	525	4.11	7	5	ND	1	16	1	6	2	103	.41	.105	6	71	.42	230	.05	3	3.34	.01	.05	1	360
LS-87 11S 0+25W	1	35	15	94	.2	13	16	4404	4.30	4	5	ND	1	20	1	2	2	94	.30	.103	6	28	.55	283	.05	6	2.24	.01	.10	1	51
LS-87 11S 0+00W	1	88	12	61	.1	4	22	731	5.91	24	5	ND	1	19	1	2	3	116	.21	.105	12	9	.50	132	.01	2	3.25	.01	.09	1	7
LS-87 11S 0+25E	1	40	6	100	.1	21	13	5564	4.05	3	5	ND	1	47	1	2	2	73	1.13	.113	27	36	.35	175	.10	5	3.05	.01	.06	1	47
LS-87 11S 0+50E	1	67	7	58	.2	20	14	414	4.20	2	6	ND	2	16	1	2	2	111	.39	.071	5	36	.53	69	.14	5	3.20	.01	.04	1	15
LS-87 11S 0+75E	1	38	12	42	.1	21	14	357	4.24	2	5	ND	1	21	1	2	2	126	.38	.024	5	43	.37	90	.18	3	2.65	.01	.04	1	18
LS-87 11S 1+00E	1	105	27	78	.1	27	17	881	4.88	8	5	ND	1	34	1	2	4	124	.66	.067	8	50	.75	91	.21	4	3.09	.02	.05	1	10
LS-87 11S 1+25E	1	66	3	58	.1	29	17	672	4.72	2	5	ND	1	24	1	2	3	127	.55	.053	7	55	.63	96	.16	6	3.25	.01	.05	1	8
LS-87 11S 1+50E	1	65	6	57	.2	26	16	538	5.44	5	5	ND	1	15	1	2	2	150	.29	.036	7	56	.35	100	.19	2	3.85	.01	.04	1	9
LS-87 11S 1+75E	1	59	8	67	.2	30	15	671	4.41	4	5	ND	1	23	1	2	3	119	.53	.054	7	51	.66	88	.14	6	3.22	.01	.05	1	11
LS-87 11S 2+00E	1	138	12	107	.1	34	30	2373	4.89	6	5	ND	1	49	1	2	2	105	1.06	.126	12	64	1.65	101	.19	4	2.86	.02	.09	1	56
STD C/AU-S	21	58	41	133	6.9	65	29	999	3.92	37	16	8	33	47	17	16	19	62	.48	.104	36	60	.88	179	.08	34	1.71	.07	.13	13	51

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE# 87-0355

PAGE 16

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
LS-87 11S 2+2SE	1	59	11	69	.1	17	15	788	3.50	4	5	ND	1	20	1	2	2	90	.28	.077	7	46	.96	99	.02	2	3.18	.01	.04	1	5
LS-87 11S 2+50E	1	26	10	64	.1	17	9	478	3.16	2	5	ND	1	13	1	2	3	80	.32	.102	3	33	.43	87	.07	3	2.04	.01	.03	1	4
LS-87 12S 5+50W	1	38	13	129	.1	16	15	2641	3.81	2	5	ND	1	20	1	2	5	87	.30	.137	7	28	.46	380	.06	9	2.69	.01	.05	1	6
LS-87 12S 5+25W	1	36	13	114	.5	17	14	1450	3.95	5	6	ND	1	13	1	2	2	97	.23	.044	8	31	.23	164	.10	5	2.89	.01	.03	3	1
LS-87 12S 5+00W	1	42	11	-69	.3	25	13	316	4.10	2	5	ND	1	11	1	2	2	106	.27	.029	4	42	.63	132	.09	4	2.94	.01	.03	1	4
LS-87 12S 4+75W	1	18	3	93	.3	16	12	1826	3.20	2	5	ND	1	15	1	2	7	76	.27	.024	4	29	.25	263	.06	2	1.91	.01	.02	1	6
LS-87 12S 4+50W	1	60	5	111	.1	35	16	1580	5.28	5	5	ND	1	13	1	2	2	133	.36	.217	4	57	.62	256	.19	7	3.91	.01	.04	1	1
LS-87 12S 4+25W	1	39	7	108	.1	29	15	1810	4.27	5	5	ND	1	18	1	2	2	99	.41	.103	5	40	.50	242	.10	2	3.01	.02	.05	1	3
LS-87 12S 4+00W	1	48	13	109	.1	27	15	771	4.91	2	5	ND	1	17	1	2	2	122	.33	.088	10	45	.40	153	.24	2	3.68	.02	.04	1	2
LS-87 12S 3+75W	1	41	7	116	.1	24	12	1147	4.54	2	5	ND	1	14	1	2	2	108	.33	.177	5	48	.43	177	.14	2	3.80	.01	.04	1	4
LS-87 12S 3+50W	1	53	8	91	.2	27	14	575	5.71	6	6	ND	1	13	1	2	2	140	.27	.164	6	66	.50	96	.18	3	4.10	.01	.05	2	1
LS-87 12S 3+25W	1	38	13	160	.1	19	20	5550	5.09	2	5	ND	1	26	1	2	3	91	.42	.304	7	46	.23	370	.12	2	2.78	.01	.06	1	1
LS-87 12S 3+00W	1	78	10	89	.1	39	18	2445	5.01	8	5	ND	1	32	1	2	2	109	1.18	.060	14	99	.65	252	.03	6	2.92	.01	.05	1	1
LS-87 12S 2+75W	1	78	10	78	.1	42	16	542	5.05	8	5	ND	1	13	1	2	2	126	.40	.036	5	62	.71	203	.09	5	3.15	.01	.04	1	6
LS-87 12S 2+50W	1	58	3	100	.3	52	21	1210	5.44	3	6	ND	1	17	1	2	2	147	.37	.066	6	153	1.58	267	.01	7	3.62	.01	.06	2	1
LS-87 12S 2+25W	1	67	17	97	.2	50	18	976	5.66	6	5	ND	1	13	1	2	2	137	.27	.179	5	108	.95	279	.10	3	4.00	.01	.05	1	3
LS-87 12S 2+00W	1	71	3	73	.1	45	18	1063	5.32	4	5	ND	1	11	1	2	2	133	.25	.086	6	93	.74	152	.07	3	4.29	.01	.06	2	1
LS-87 12S 1+75W	1	116	7	82	.1	72	26	243	7.33	11	5	ND	1	9	1	2	5	135	.15	.046	3	104	.88	75	.01	5	2.56	.01	.03	1	1
LS-87 12S 1+50W	1	61	13	105	.3	88	24	322	6.08	4	6	ND	1	7	1	5	2	114	.09	.046	4	116	1.06	95	.01	5	2.41	.01	.04	1	1
LS-87 12S 1+25W	1	31	11	145	.1	21	16	6652	4.26	3	5	ND	1	26	1	2	2	83	.55	.186	19	30	.32	421	.05	7	2.95	.01	.08	1	6
LS-87 12S 1+00W	1	90	12	133	.1	9	18	2154	5.31	9	5	ND	1	24	1	2	2	114	.32	.159	13	13	.36	303	.04	4	4.14	.01	.10	1	415
LS-87 12S 0+75W	1	42	7	108	.1	9	13	1536	3.39	2	5	ND	1	29	1	2	3	98	.74	.166	3	18	.72	296	.10	2	3.36	.01	.09	1	1
LS-87 12S 0+50W	1	33	3	89	.1	15	11	1534	3.33	2	5	ND	1	17	1	2	2	91	.43	.115	4	26	.44	263	.08	4	2.94	.01	.04	1	2
LS-87 12S 0+25W	1	34	13	125	.1	24	13	1235	4.41	2	5	ND	1	15	1	2	3	96	.40	.237	4	43	.60	253	.07	8	3.33	.01	.06	1	1
LS-87 12S 0+00W	1	44	5	84	.3	13	14	856	3.81	3	5	ND	1	19	1	2	4	101	.35	.085	4	19	.64	278	.01	4	3.81	.01	.06	2	4
LS-87 12S 0+25E	1	33	4	76	.1	20	12	1114	3.61	2	5	ND	1	16	1	2	2	92	.50	.067	8	36	.46	83	.16	5	2.53	.01	.03	1	1
LS-87 12S 0+50E	3	33	5	99	.1	25	12	2568	3.98	2	5	ND	1	20	1	2	3	93	.73	.083	9	42	.50	150	.13	6	2.73	.02	.03	1	3
LS-87 12S 0+75E	1	30	9	74	.2	23	11	577	4.04	4	5	ND	1	16	1	3	2	102	.48	.061	3	35	.43	79	.15	5	2.46	.01	.03	2	9
LS-87 12S 1+00E	1	29	9	104	.2	15	14	2482	4.10	5	5	ND	1	15	1	2	2	92	.46	.197	4	32	.31	237	.13	3	2.12	.01	.04	1	3
LS-87 12S 1+25E	1	73	7	74	.1	30	15	531	5.10	4	5	ND	1	18	1	2	2	120	.36	.074	5	52	.72	173	.03	6	3.71	.01	.06	1	4
LS-87 12S 1+50E	1	50	7	94	.1	32	17	1605	5.23	4	5	ND	1	20	1	2	2	125	.32	.074	8	68	.54	252	.01	5	3.87	.01	.06	1	3
LS-87 12S 1+75E	1	76	15	82	.4	33	26	1278	4.96	5	6	ND	1	25	1	3	2	105	.47	.060	9	83	.72	207	.01	6	2.96	.01	.09	2	5
LS-87 12S 2+00E	1	70	18	80	.1	32	23	1155	4.25	4	5	ND	1	77	1	2	2	110	.73	.065	10	78	.68	216	.03	2	2.53	.01	.05	1	11
LS-87 12S 2+25E	1	61	11	102	.2	35	16	750	5.11	8	5	ND	1	13	1	2	2	134	.25	.133	5	79	.47	151	.09	10	4.22	.01	.05	1	5
LS-87 12S 2+50E	1	58	5	62	.1	30	15	781	4.32	3	5	ND	1	18	1	2	2	107	.34	.062	6	64	.68	132	.12	5	3.02	.01	.04	1	2
LS-87 12S 2+75E	1	59	2	53	.1	25	12	586	3.70	3	5	ND	1	34	1	2	2	93	.72	.062	6	45	.67	96	.21	2	2.07	.02	.03	1	1
STD C/AU-S	21	61	38	133	7.3	62	28	992	3.91	40	17	7	34	49	16	15	21	62	.50	.100	36	58	.92	184	.08	36	1.80	.07	.14	14	52

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE# 87-0255

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au#1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
LS-87 12S 3+00E	1	50	5	64	.2	32	14	296	4.59	2	5	ND	1	18	1	2	2	115	.31	.046	4	52	.60	106	.04	6	3.52	.01	.05	1	1
LS-87 12S 3+50E	1	44	2	72	.1	38	18	475	5.21	3	5	ND	1	19	1	2	3	119	.36	.039	5	73	.73	121	.06	2	3.68	.01	.05	1	1
LS-87 12S 4+00E	1	41	8	133	.1	35	16	1144	5.08	2	5	ND	1	30	1	2	3	109	.85	.119	9	60	.61	187	.12	6	3.65	.02	.06	1	1
LS-87 12S 4+50E	1	65	9	102	.1	102	27	842	5.56	2	5	ND	1	13	1	2	3	107	.15	.093	4	205	1.42	180	.01	3	3.22	.02	.07	1	1
LS-87 12S 5+00E	2	63	4	.61	.1	30	16	478	4.01	8	5	ND	1	17	1	2	4	98	.40	.098	5	56	.66	82	.14	3	3.42	.01	.05	1	2
LS-87 12S 5+50E	1	69	9	76	.1	34	21	1107	4.45	8	5	ND	1	20	1	2	5	98	.41	.089	11	78	.58	187	.19	3	4.52	.02	.05	1	1
LS-87 12S 6+00E	1	23	3	35	.2	18	9	223	4.08	2	5	ND	1	32	1	2	3	121	.40	.027	4	62	.54	65	.15	2	2.05	.01	.03	1	3
LS-87 12S 6+50E	1	86	12	82	.1	43	22	523	6.15	2	5	ND	1	32	1	2	2	151	.41	.092	5	132	.72	66	.31	2	3.77	.01	.03	1	4
LS-87 12S 7+00E	1	59	8	63	.1	29	14	377	4.19	7	5	ND	1	17	1	2	3	117	.36	.131	4	61	.48	60	.22	5	3.92	.01	.02	1	1
LS-87 12S 7+50E	1	51	4	88	.1	26	13	1783	4.16	8	5	ND	1	22	1	2	2	109	.41	.371	4	59	.57	130	.20	2	3.61	.02	.04	1	1
LS-87 12S 8+00E	1	57	9	91	.3	30	15	914	4.33	2	5	ND	2	22	1	2	3	107	.37	.175	5	60	.37	126	.23	5	3.59	.02	.05	1	1
LS-87 12S 8+50E	1	26	3	58	.1	17	10	475	3.23	2	5	ND	1	19	1	2	2	87	.35	.048	4	36	.35	86	.16	2	2.39	.01	.02	1	23
LS-87 12S 9+00E	1	61	5	45	.1	26	15	228	4.60	13	5	ND	1	17	1	2	3	127	.37	.045	5	59	.51	53	.25	3	3.45	.01	.02	1	2
LS-87 12S 9+50E	1	24	7	49	.1	14	8	234	4.76	2	5	ND	1	20	1	2	2	137	.32	.027	4	46	.27	74	.18	2	1.95	.01	.02	1	3
LS-87 13S 5+75W	1	32	11	128	.4	29	13	909	2.80	2	5	ND	1	18	1	2	2	69	.34	.051	5	33	.48	257	.07	4	2.79	.01	.05	1	1
LS-87 13S 5+50W	2	17	2	85	.1	19	11	1745	2.59	3	5	ND	1	19	1	2	2	67	.41	.055	4	28	.44	210	.06	4	2.10	.01	.03	1	1
LS-87 13S 5+25W	1	46	9	98	.3	33	15	939	4.22	2	5	ND	1	15	1	2	4	110	.31	.048	6	47	.68	159	.12	6	3.30	.01	.05	1	1
LS-87 13S 5+00W	1	44	5	119	.1	31	15	975	4.50	5	5	ND	1	16	1	2	3	116	.33	.070	5	47	.47	221	.18	5	4.18	.01	.06	1	1
LS-87 13S 4+75W	1	47	6	115	.1	33	15	862	4.49	4	5	ND	1	14	1	2	4	116	.28	.103	4	50	.58	183	.12	5	4.64	.01	.05	1	1
LS-87 13S 4+50W	1	65	10	94	.1	35	17	560	5.34	6	5	ND	1	13	1	2	2	141	.28	.075	3	63	.59	155	.18	8	5.09	.01	.05	1	3
LS-87 13S 4+25W	2	45	7	108	.1	27	16	3093	4.13	7	5	ND	1	17	1	2	2	105	.29	.105	5	39	.45	226	.09	2	3.53	.01	.05	1	1
LS-87 13S 4+00W	1	36	7	77	.1	24	14	370	4.75	4	5	ND	1	16	1	2	4	122	.25	.054	4	41	.47	159	.06	8	3.88	.01	.05	1	3
LS-87 13S 3+75W	1	25	2	126	.1	18	10	538	5.53	2	5	ND	1	12	1	2	3	152	.21	.135	3	42	.24	124	.07	4	3.52	.01	.04	1	1
LS-87 13S 3+50W	1	24	5	130	.1	18	20	3333	5.75	3	5	ND	1	8	1	2	5	128	.17	.140	6	34	.68	262	.01	3	2.97	.01	.09	1	1
LS-87 13S 3+25W	2	22	2	155	.2	19	15	3188	3.29	2	5	ND	1	14	1	2	2	94	.26	.062	5	58	.35	221	.02	3	2.44	.01	.05	1	1
LS-87 13S 3+00W	2	34	9	94	.2	39	14	407	4.91	6	5	ND	1	17	1	2	2	115	.28	.034	4	52	.41	207	.11	5	3.40	.01	.05	1	1
LS-87 13S 2+25W	2	119	9	77	.2	8	20	914	4.82	5	5	ND	2	8	1	11	3	67	.14	.065	6	11	.09	144	.01	2	1.29	.01	.12	1	225
LS-87 13S 2+00W	1	63	6	178	.1	18	16	2066	4.37	4	5	ND	1	19	1	2	4	117	.32	.224	9	28	.55	328	.02	4	4.16	.01	.13	1	2
LS-87 13S 1+75W	1	55	3	117	.2	25	16	940	4.25	3	5	ND	1	15	1	2	3	105	.28	.169	7	40	.60	149	.05	7	3.75	.01	.07	1	11
LS-87 13S 1+50W	1	43	2	115	.4	13	12	529	3.30	2	5	ND	1	23	1	2	2	89	.31	.082	6	18	.45	204	.01	2	4.31	.01	.08	1	1
LS-87 13S 1+25W	1	20	5	75	.3	14	11	470	2.76	4	5	ND	1	24	1	2	2	89	.41	.040	4	22	.35	139	.03	6	2.91	.01	.06	1	1
LS-87 13S 1+00W	1	22	4	68	.3	23	11	487	3.59	2	5	ND	1	16	1	2	2	96	.42	.057	5	37	.41	174	.13	4	2.72	.01	.04	1	3
LS-87 13S 0+75W	1	42	10	98	.4	29	15	988	4.53	3	5	ND	1	22	1	2	2	121	.60	.076	4	44	.66	180	.09	2	2.76	.01	.06	1	1
LS-87 13S 0+50W	2	24	5	127	.1	11	16	4957	2.96	2	5	ND	1	35	1	2	2	83	.56	.178	4	22	.40	343	.03	2	2.61	.01	.10	1	1
LS-87 13S 0+25W	1	61	2	65	.1	22	12	530	5.55	5	5	ND	1	15	1	2	2	164	.49	.112	5	46	.54	90	.17	5	2.64	.02	.04	1	2
LS-87 13S 0+00W	2	30	2	129	.2	11	13	4263	3.18	2	5	ND	1	14	1	2	4	80	.26	.195	6	22	.26	326	.01	3	3.50	.01	.11	1	1
STD C/AU-S	20	59	35	135	7.2	67	30	1026	3.93	41	16	8	35	49	17	15	19	64	.50	.103	36	61	.93	184	.08	2	1.80	.07	.14	13	50

ASHWORTH EXPLORATION PROJECT - LADY-STONES FILE# 87-0355

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Na PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au88 PPB
LS-87 13S 0+25E	2	27	2	155	.2	14	12	2485	2.98	5	5	ND	1	18	1	2	3	76	.35	.269	5	32	.30	305	.02	4	2.97	.01	.05	1	1
LS-87 13S 0+50E	1	25	3	150	.2	18	14	1939	3.06	3	5	ND	1	20	1	5	2	73	.34	.142	3	34	.31	257	.01	2	2.45	.01	.06	1	67
LS-87 13S 0+75E	1	45	10	124	.3	26	13	522	3.83	3	5	ND	1	15	1	2	2	90	.32	.123	5	41	.53	130	.04	7	2.76	.01	.06	1	3
LS-87 13S 1+00E	1	57	2	95	.2	25	15	954	3.91	2	5	ND	1	14	1	3	3	89	.26	.105	6	45	.46	165	.03	2	3.11	.01	.05	1	1
LS-87 13S 1+25E	1	41	4	142	.2	19	16	2846	4.16	3	5	ND	1	14	1	2	2	89	.27	.325	5	45	.27	213	.06	5	3.41	.01	.05	1	1
LS-87 13S 1+50E	1	49	5	93	.1	26	16	1126	4.20	4	5	ND	1	13	1	3	2	98	.31	.112	4	46	.52	131	.04	2	3.44	.01	.04	1	1
LS-87 13S 1+75E	1	54	3	104	.1	33	15	1582	4.85	2	5	ND	1	12	1	2	2	110	.28	.150	4	59	.56	177	.11	2	4.12	.01	.05	1	3
LS-87 13S 2+00E	1	45	2	77	.1	28	13	815	3.89	2	5	ND	1	14	1	2	2	99	.32	.102	4	46	.57	136	.10	2	3.50	.01	.04	1	1
LS-87 13S 2+25E	1	47	9	93	.1	29	16	841	4.90	2	5	ND	1	15	1	3	2	118	.30	.073	5	56	.63	110	.14	2	3.69	.01	.05	1	4
LS-87 14S 5+25W	1	57	2	97	.2	34	16	448	5.36	5	5	ND	1	16	1	2	4	139	.29	.046	5	52	.59	324	.12	5	3.90	.01	.05	1	3
LS-87 14S 5+00W	1	38	11	110	.1	22	13	2460	4.00	4	5	ND	1	12	1	2	2	97	.27	.218	4	34	.47	286	.06	3	2.99	.01	.05	1	1
LS-87 14S 4+75W	1	32	15	103	.1	30	12	881	3.38	2	5	ND	1	11	1	2	4	88	.24	.050	5	39	.41	202	.08	2	3.63	.01	.04	1	3
LS-87 14S 4+50W	1	34	3	124	.1	24	13	1571	3.77	2	5	ND	1	11	1	2	2	92	.21	.134	4	33	.36	210	.05	2	3.26	.01	.05	1	69
LS-87 14S 4+25W	1	33	5	89	.1	23	11	774	3.38	2	5	ND	1	10	1	2	2	89	.21	.064	4	37	.45	163	.07	2	3.51	.01	.04	1	6
LS-87 14S 4+00W	1	20	5	122	.2	19	11	979	3.15	2	5	ND	1	11	1	3	3	76	.23	.099	4	29	.38	151	.04	2	2.63	.01	.04	1	6
LS-87 14S 3+75W	1	21	4	41	.1	17	9	151	2.98	6	5	ND	1	12	1	2	2	82	.28	.019	4	34	.32	114	.08	2	2.11	.01	.02	1	4
LS-87 14S 3+50W	1	22	4	86	.2	16	11	831	4.37	2	5	ND	1	9	1	2	2	104	.17	.031	3	31	.27	245	.01	2	2.21	.01	.04	1	2
LS-87 14S 3+25W	1	25	9	160	.1	11	13	4987	3.94	3	5	ND	1	8	1	2	5	77	.14	.116	9	28	.25	502	.01	2	2.15	.01	.07	1	1
LS-87 14S 3+00W	1	18	12	64	.1	20	9	528	3.30	3	5	ND	1	12	1	2	2	89	.33	.078	3	31	.28	97	.12	2	2.43	.01	.03	1	3
LS-87 14S 2+75W	1	57	7	127	.1	40	18	978	5.25	4	5	ND	1	10	1	3	2	138	.19	.110	5	64	.44	205	.05	2	4.49	.01	.06	1	345
LS-87 14S 2+50W	1	33	7	97	.1	24	15	1128	4.51	2	5	ND	1	11	1	2	2	110	.19	.053	4	49	.45	215	.01	2	2.67	.01	.05	1	27
LS-87 14S 2+25W	1	16	6	48	.1	3	7	203	3.51	2	5	ND	1	19	1	2	2	90	.24	.029	3	13	.25	148	.01	2	2.60	.01	.05	1	1
LS-87 14S 2+00W	1	39	4	173	.1	10	11	1368	3.07	2	5	ND	1	19	1	2	2	66	.22	.451	4	22	.23	244	.02	2	3.12	.01	.06	1	2
LS-87 14S 1+75W	1	61	7	125	.2	13	14	912	3.83	2	5	ND	1	16	1	2	2	77	.26	.309	5	19	.50	170	.01	2	3.27	.01	.07	1	1
LS-87 14S 1+50W	2	34	7	170	.1	18	16	2858	3.52	6	5	ND	1	28	1	2	2	72	.58	.365	4	33	.41	326	.05	3	2.74	.01	.05	1	1
LS-87 14S 1+25W	1	33	6	73	.1	19	11	680	3.96	2	5	ND	1	14	1	2	2	87	.45	.057	7	37	.39	124	.10	3	2.35	.01	.04	1	1
LS-87 14S 1+00W	1	56	7	99	.1	17	12	703	4.16	6	5	ND	1	14	1	2	2	94	.35	.356	4	33	.41	172	.07	3	3.05	.01	.06	1	3
LS-87 14S 0+75W	1	41	13	96	.1	13	14	586	5.07	2	5	ND	1	30	1	2	2	108	.58	.366	4	15	.65	262	.01	2	3.97	.01	.15	1	1
LS-87 14S 0+50W	1	60	4	86	.1	19	16	853	4.56	2	5	ND	1	21	1	2	4	101	.29	.083	8	32	.54	243	.01	4	3.74	.01	.09	1	1
LS-87 14S 0+25W	1	60	7	116	.1	15	17	2282	4.18	2	5	ND	1	18	1	2	2	97	.28	.179	7	29	.41	303	.01	4	3.42	.01	.09	1	4
LS-87 14S 0+00W	1	37	15	117	.1	22	15	1004	3.45	2	5	ND	1	14	1	2	2	99	.35	.308	4	39	.48	167	.07	6	2.58	.01	.05	1	1
LS-87 14S 0+25E	1	30	8	115	.1	22	12	472	3.65	3	5	ND	1	12	1	2	2	91	.34	.113	4	33	.36	113	.15	4	2.85	.01	.04	1	1
LS-87 14S 0+50E	1	27	7	72	.1	16	10	739	3.02	2	5	ND	1	17	1	2	2	77	.29	.073	4	28	.37	108	.03	2	2.48	.01	.04	1	1
LS-87 14S 0+75E	1	10	7	53	.1	8	6	291	2.43	2	5	ND	1	18	1	2	2	69	.28	.024	4	19	.25	125	.04	2	1.61	.01	.02	1	5
LS-87 14S 1+00E	1	46	8	57	.1	25	13	264	3.66	4	5	ND	1	18	1	2	2	95	.32	.029	5	43	.49	98	.04	2	2.70	.01	.03	1	1
LS-87 14S 1+25E	1	33	13	107	.1	20	15	1170	4.80	4	5	ND	1	16	1	2	3	104	.26	.110	4	42	.39	164	.07	2	3.41	.01	.05	1	1
STD C/AU-5	21	59	38	131	6.8	66	28	983	3.94	40	18	7	32	47	17	15	20	61	.48	.102	35	59	.88	176	.08	34	1.71	.07	.15	12	49

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE# 87-0355

PAGE 19

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au# PPB
LS-87 14S 1+50E	1	46	13	84	.1	22	15	533	5.41	6	5	ND	1	11	1	2	2	119	.21	.110	4	54	.57	90	.08	2	4.10	.01	.04	1	1
LS-87 14S 1+75E	1	54	6	82	.1	31	17	400	5.19	3	5	ND	2	13	1	2	5	122	.23	.065	4	59	.62	98	.10	5	4.60	.01	.05	1	1
LS-87 14S 2+00E	1	47	7	81	.1	26	14	1165	4.65	6	5	ND	1	12	1	2	2	117	.22	.104	4	51	.51	112	.12	6	4.30	.01	.03	1	1
LS-87 14S 2+25E	1	42	10	68	1.6	22	13	967	4.84	5	5	ND	1	11	1	2	5	118	.23	.092	4	49	.45	77	.11	9	3.44	.01	.03	1	1
LS-87 14S 2+50E	1	36	16	89	.1	18	13	1573	5.29	6	5	ND	1	10	1	2	3	124	.18	.176	4	52	.29	113	.07	7	3.15	.01	.03	1	2
LS-87 14S 2+75E	1	39	2	75	.1	19	14	616	4.44	3	5	ND	1	11	1	2	5	109	.23	.102	3	61	.43	96	.11	5	4.55	.01	.03	1	1
LS-87 14S 3+00E	1	47	7	79	.1	24	16	1474	4.52	4	5	ND	1	13	1	2	5	112	.25	.097	5	59	.48	92	.14	4	3.25	.01	.04	1	3
LS-87 15S 4+50W	1	12	6	43	.1	10	6	275	2.83	3	5	ND	1	12	1	2	2	78	.21	.023	3	20	.26	96	.03	4	1.49	.01	.02	1	1
LS-87 15S 4+25W	1	53	6	76	.1	23	16	410	5.06	4	5	ND	2	11	1	2	5	117	.18	.037	5	44	.81	137	.05	7	3.48	.01	.07	1	1
LS-87 15S 4+00W	1	54	8	88	.1	26	17	536	5.67	4	5	ND	1	10	1	2	6	123	.16	.049	4	41	.80	156	.01	5	3.63	.01	.07	1	1
LS-87 15S 3+75W	1	46	15	88	.1	26	16	406	4.66	7	5	ND	1	11	1	2	2	120	.25	.039	9	50	.71	131	.09	9	3.21	.01	.07	1	1
LS-87 15S 3+50W	1	22	6	64	.1	16	13	299	5.18	2	5	ND	1	11	1	2	3	132	.27	.031	4	34	.22	157	.12	3	2.16	.01	.03	1	1
LS-87 15S 3+25W	1	52	2	78	.2	27	14	304	4.83	5	5	ND	1	10	1	2	2	129	.26	.056	4	51	.52	122	.16	3	3.87	.01	.04	1	1
LS-87 15S 3+00W	1	35	7	60	.1	34	16	900	4.22	4	5	ND	1	16	1	2	4	103	.27	.032	8	52	.42	469	.11	2	3.40	.01	.04	1	1
LS-87 15S 2+75W	1	29	8	63	.2	22	13	688	4.48	6	5	ND	1	10	1	2	2	109	.25	.057	4	43	.47	220	.09	6	3.13	.01	.04	1	1
LS-87 15S 2+50W	1	19	8	134	.1	11	11	2390	3.28	2	5	ND	1	8	1	2	2	89	.18	.166	4	28	.22	194	.02	2	2.45	.01	.04	1	1
LS-87 15S 2+25W	1	22	11	126	.1	14	11	2165	3.80	3	5	ND	1	9	1	2	2	86	.23	.159	3	26	.25	372	.02	5	1.93	.01	.03	1	1
LS-87 15S 2+00W	1	49	5	121	.3	21	15	637	4.54	5	5	ND	1	9	1	3	2	114	.18	.205	4	40	.31	195	.04	3	3.11	.01	.04	1	1
LS-87 15S 1+75W	1	49	3	100	.2	29	16	612	4.77	6	5	ND	1	12	1	2	2	117	.25	.048	4	43	.57	236	.03	4	3.10	.01	.05	1	1
LS-87 15S 1+50W	2	59	6	62	.1	24	17	954	4.53	11	5	ND	1	20	1	4	2	101	.54	.037	15	55	.54	177	.01	4	2.53	.01	.04	1	4
LS-87 15S 1+25W	1	62	4	79	.1	23	18	829	4.01	3	5	ND	1	47	1	2	2	100	1.02	.065	8	56	.60	225	.01	3	2.95	.01	.07	1	1
LS-87 15S 1+00W	1	83	13	74	.2	51	24	645	5.15	3	5	ND	1	26	1	2	2	92	.41	.084	9	86	1.00	122	.01	5	2.60	.01	.09	1	1
LS-87 15S 0+75W	1	20	3	129	.3	19	14	1326	3.09	2	5	ND	1	15	1	2	2	71	.30	.169	4	31	.29	143	.06	4	2.43	.01	.04	1	1
LS-87 15S 0+50W	1	30	5	165	.1	28	19	5607	4.53	4	5	ND	1	18	1	2	2	92	.27	.212	5	63	.27	326	.01	7	2.53	.01	.05	1	1
LS-87 15S 0+00W	1	24	7	57	.3	15	11	695	3.30	4	5	ND	1	21	1	2	2	78	.42	.042	4	33	.29	109	.03	2	2.07	.01	.03	1	1
LS-87 15S 0+25E	1	27	4	66	.2	19	13	697	2.71	3	5	ND	1	16	1	2	2	67	.31	.044	3	29	.38	104	.04	2	2.24	.01	.03	1	1
LS-87 15S 0+50E	1	23	4	157	.1	18	12	2657	2.79	3	5	ND	1	15	1	2	2	61	.29	.176	4	29	.29	180	.05	4	2.43	.01	.03	1	1
LS-87 15S 0+75E	1	35	7	86	.1	26	16	2769	3.68	2	5	ND	1	26	1	2	2	84	.60	.076	9	56	.42	166	.07	2	2.60	.01	.04	1	1
LS-87 15S 1+00E	1	27	6	62	.2	21	12	572	3.40	5	5	ND	1	21	1	2	2	86	.45	.048	6	51	.41	112	.06	4	2.28	.01	.02	1	1
LS-87 15S 1+25E	1	31	11	63	.4	25	14	400	2.94	2	5	ND	1	17	1	2	2	75	.39	.023	4	38	.38	83	.07	8	1.93	.01	.02	1	1
LS-87 15S 1+50E	1	30	6	115	.2	28	14	1203	4.20	2	5	ND	2	11	1	2	4	102	.23	.238	3	47	.34	181	.08	2	3.57	.01	.05	1	1
LS-87 15S 1+75E	1	42	7	96	.1	23	15	1440	3.46	2	5	ND	1	13	1	2	2	81	.27	.232	3	52	.37	148	.05	4	2.81	.01	.03	1	1
LS-87 15S 2+00E	1	24	10	72	.2	16	12	266	4.08	5	5	ND	1	12	1	2	2	100	.22	.047	3	44	.34	106	.08	4	3.00	.01	.03	1	1
LS-87 15S 2+25E	1	50	6	76	.1	21	14	455	5.48	8	5	ND	2	10	1	2	2	127	.20	.114	5	74	.44	65	.09	3	3.91	.01	.03	2	1
LS-87 15S 2+50E	1	39	2	123	.1	22	17	1976	3.85	5	5	ND	1	13	1	2	2	109	.21	.184	5	59	.20	157	.03	4	3.77	.01	.03	1	2
LS-87 15S 2+75E	1	59	2	58	.1	25	16	508	4.09	2	5	ND	1	12	1	2	2	110	.24	.059	5	64	.53	67	.11	2	3.88	.01	.03	1	1
STD C/AU-S	2	59	38	132	6.9	66	29	995	3.94	41	15	7	33	48	17	15	20	62	.48	.102	35	59	.88	179	.08	36	1.71	.07	.13	13	46

ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE# 87-0355

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au11 PPB
LS-87 15S 3+00E	1	19	11	60	.3	18	13	1258	3.02	3	5	ND	1	14	1	2	2	75	.26	.087	4	42	.32	100	.04	2	2.61	.01	.04	1	5
LS-87 15S 3+25E	1	34	5	130	.1	31	16	2966	3.81	5	5	ND	1	15	1	2	2	87	.27	.132	5	53	.26	204	.07	8	2.93	.01	.03	1	1
LS-87 15S 3+50E	1	28	5	55	.1	21	14	443	3.70	8	5	ND	1	19	1	6	2	80	.28	.040	4	26	.34	171	.03	14	2.20	.01	.05	1	1
LS-87 15S 4+00E	1	24	2	40	.1	24	11	722	3.67	2	5	ND	1	18	1	2	6	87	.40	.039	8	44	.39	92	.09	5	2.49	.01	.02	1	1
LS-87 15S 4+50E	1	26	5	39	.1	25	10	567	3.21	4	5	ND	1	18	1	2	2	88	.46	.038	4	43	.49	129	.09	3	2.10	.01	.03	1	1
LS-87 15S 5+00E	1	40	4	71	.1	27	20	2309	3.69	3	5	ND	1	22	1	2	2	76	.41	.119	9	55	.45	130	.13	5	3.07	.01	.03	1	2
LS-87 15S 5+50E	1	28	4	66	.1	25	13	910	4.09	2	5	ND	1	22	1	2	3	79	.51	.125	4	56	.48	173	.16	24	2.81	.02	.04	1	1
LS-87 15S 6+00E	1	33	5	58	.1	31	15	1890	4.11	2	5	ND	1	19	1	2	2	108	.52	.050	10	49	.59	133	.15	20	3.04	.01	.04	1	1
LS-87 15S 6+50E	1	27	5	53	.1	33	13	535	4.43	2	5	ND	1	14	1	2	2	115	.32	.045	3	52	.48	113	.17	6	3.39	.01	.03	1	119
LS-87 15S 7+00E	1	33	5	53	.1	34	14	752	4.24	5	5	ND	1	23	1	2	2	116	.68	.055	6	67	.57	85	.16	6	3.50	.01	.03	1	10
LS-87 15S 7+50E	1	30	4	58	.1	28	14	457	4.85	2	5	ND	1	19	1	2	2	121	.37	.046	4	61	.54	115	.16	5	3.10	.01	.03	1	1
LS-87 15S 8+00E	1	29	2	58	.2	31	12	516	4.13	2	5	ND	1	16	1	2	2	112	.35	.049	4	52	.50	105	.15	2	2.67	.01	.03	1	4
LS-87 15S 8+50E	1	38	2	69	.1	35	16	1386	4.26	2	5	ND	1	20	1	2	2	111	.40	.071	4	68	.63	140	.18	7	3.10	.01	.03	1	1
LS-87 15S 9+00E	1	46	2	60	.1	29	14	398	4.65	3	5	ND	1	15	1	3	2	125	.35	.048	4	56	.49	90	.22	4	3.31	.01	.03	1	1
LS-87 15S 9+50E	1	41	2	39	.1	18	10	298	4.12	3	5	ND	1	15	1	2	2	115	.32	.038	3	46	.50	62	.16	6	2.18	.01	.02	1	1
LS-87 15S 10+00E	1	28	5	44	.1	20	9	192	4.64	2	5	ND	1	16	1	2	2	124	.25	.033	5	46	.59	69	.07	2	2.36	.01	.02	1	1
LS-87 SOIL "A"	1	38	16	91	.1	540	59	938	10.43	991	5	ND	1	8	1	22	5	153	.12	.063	5	757	.10	44	.01	8	1.48	.01	.02	1	1
STD C/AU-S	20	59	38	129	6.9	69	29	978	3.95	37	16	7	32	47	17	16	22	61	.48	.097	34	56	.88	175	.08	34	1.72	.07	.14	12	51

resamp? 45N 8100E o.f.v

LC-1 K¹⁻⁵ plate II
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ASHWORTH EXPLORATION PROJECT - LACY-STOKES FILE # 87-0355

SAMPLE#	No	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	M	Au#1	Pt#1	Pd#1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
LS-87-33	2	543	64	157	16.2	52	16	403	2.72	2	5	ND	1	57	6	2	2	32	3.84	.102	5	33	.57	60	.05	7	1.44	.01	.29	1	3	-	-
LS-87-34	1	189	2	66	.1	3	10	605	3.76	16	5	ND	3	110	1	3	2	7	4.15	.065	10	2	1.48	127	.01	12	.92	.02	.16	1	1	-	-
LS-87-35	1	202	8	267	.1	11	27	1593	5.81	10	5	ND	2	39	1	2	2	208	1.61	.152	8	16	3.50	32	.26	5	3.19	.05	.12	1	6	-	-
LS-87-36	3	11	3	35	.3	6	5	67	1.66	6	5	ND	1	5	1	2	2	18	.20	.046	16	21	.08	7	.15	2	.18	.08	.03	1	1	-	-
LS-87-37	1	100	6	17	.1	32	17	257	3.22	8	5	ND	1	47	1	2	2	69	1.52	.035	2	50	.90	6	.38	2	1.51	.10	.03	1	1	-	-
LS-87-38	2	47	4	82	.1	2	14	992	4.40	2	8	ND	3	130	1	3	2	25	7.33	.168	7	4	.72	137	.01	3	.44	.03	.17	1	1	-	-
LS-87-39	1	36	4	36	.1	3	10	767	3.17	6	5	ND	1	86	1	7	2	24	3.06	.122	9	3	.17	60	.01	6	.34	.05	.09	1	3	-	-
LS-87-40	1	13	2	55	.1	3	7	701	2.89	3	6	ND	2	150	1	2	3	43	3.82	.144	9	3	1.01	127	.01	9	.36	.07	.06	1	1	-	-
LS-87-41	1	4	2	5	.1	1	2	181	.68	2	5	ND	1	3	1	2	2	4	.03	.003	2	3	.09	7	.01	2	.15	.01	.01	1	1	-	-
LS-87-42	1	15	2	59	.1	41	10	1183	2.20	2	5	ND	1	12	1	2	4	32	.55	.047	9	19	1.68	145	.02	2	1.08	.02	.07	1	2	-	-
LS-87-43	1	127	5	42	.3	2	18	700	4.32	16	5	2	2	85	1	3	2	46	5.14	.158	12	2	.44	48	.11	3	1.22	.05	.24	1	2320	2	2
LS-87-44	17	53	13	56	.1	6	61	1064	13.90	5	5	ND	2	26	1	2	6	98	3.24	.128	3	5	2.03	54	.22	12	2.36	.03	.41	1	520	2	6
LS-87-45	3	22	7	19	.2	10	127	153	20.75	7	5	ND	1	9	1	2	9	12	.07	.004	2	1	.21	9	.01	8	.22	.01	.04	1	3580	2	10
LS-87-74	1	76	8	88	.1	9	25	1047	7.16	11	7	ND	3	136	1	2	2	204	6.22	.071	11	6	2.21	70	.17	6	2.62	.05	.11	1	5	-	-
LS-87-75	1	25	2	48	.1	161	26	1171	4.08	333	7	ND	5	400	1	8	2	49	16.98	.058	4	311	3.77	37	.01	3	.28	.01	.05	1	1	-	-
LS-87-77	1	52	2	67	.1	31	17	491	3.54	2	5	ND	1	35	1	2	2	72	1.17	.087	5	35	1.66	132	.14	7	2.04	.18	.19	1	1	-	-
LS-87-78	1	11	5	3	.3	2	2	100	.47	4	5	ND	1	4	1	4	3	10	.12	.003	2	6	.04	18	.01	3	.13	.01	.08	1	215	-	-
LS-87-79	1	56	3	96	.1	3	16	860	5.41	3	5	ND	1	30	1	2	2	106	.95	.147	7	6	1.38	45	.26	5	2.23	.07	.13	1	3	-	-
LS-87-80	1	35	2	89	.1	2	14	749	5.42	4	5	ND	1	71	1	2	2	93	1.29	.190	17	5	1.46	67	.14	3	2.39	.07	.34	1	131	-	-
LS-87-81	5	63	10	120	.1	8	14	616	4.73	6	5	ND	1	48	1	2	2	80	1.26	.143	8	8	1.24	33	.38	10	1.97	.12	.10	1	2	-	-
LO 3490M	1	9	2	34	.1	9	9	272	2.52	2	5	ND	1	25	1	2	2	87	.57	.035	4	15	.53	368	.35	2	.64	.03	.07	1	4	-	-
STD C/FA 5X	20	58	42	135	6.9	65	29	1003	3.95	38	16	8	33	49	17	15	19	62	.48	.102	36	58	.88	179	.08	35	1.72	.07	.14	12	102	97	103

Cu - Ag showing
no. counting

trx / E
main sig.

→
→

ASHWORTH EXPLORATION PROJECT - LACY FILE # 87-0535

PAGE 2

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Tl	B	Al	Na	K	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
1612 LS-87 30N 14+50E	1	30	5	60	.1	59	15	188	5.47	2	5	ND	1	14	1	2	2	105	.14	.023	7	128	1.13	40	.02	4	2.97	.01	.03	1	1
1613 LS-87 30N 15+00E	1	11	11	73	.1	15	25	2457	6.46	5	5	ND	1	16	1	2	2	156	.68	.097	3	67	.54	35	.29	2	1.65	.01	.03	1	1
1614 LS-87 30N 15+50E	1	20	6	60	.1	15	14	1124	6.60	5	5	ND	1	32	1	2	2	174	.69	.059	3	62	.73	38	.27	2	1.97	.01	.02	1	22
1615 LS-87 30N 16+00E	1	9	9	40	.1	11	7	747	4.33	2	5	ND	1	11	1	2	2	132	.63	.052	3	48	.43	23	.26	2	1.21	.01	.02	1	1
1616 LS-87 30N 16+50E	1	13	8	66	.1	45	14	468	4.31	4	5	ND	1	22	1	2	2	108	1.06	.042	3	83	1.59	27	.23	2	2.31	.02	.02	1	1
1617 LS-87 30N 17+00E	3	46	12	184	.1	45	25	2846	6.56	23	5	ND	1	16	1	2	2	102	.48	.052	27	76	.61	68	.14	6	2.86	.01	.03	1	1
1618 LS-87 30N 17+50E	1	36	7	93	.1	25	12	250	4.63	8	5	ND	1	9	1	2	2	119	.29	.027	3	47	.49	36	.25	2	2.42	.01	.02	1	1
1619 LS-87 30N 18+00E	2	14	12	305	.1	41	14	3248	3.89	8	5	ND	1	9	2	2	5	47	.42	.095	28	31	.55	91	.05	2	2.16	.01	.03	1	2
1620 LS-87 30N 18+50E	1	5	11	24	.1	9	3	81	2.79	7	5	ND	1	4	1	2	2	92	.12	.010	2	14	.04	9	.15	2	.37	.01	.01	1	1
1621 LS-87 30N 19+00E	1	7	12	28	.1	2	2	248	1.25	2	5	ND	1	29	1	2	2	70	.31	.018	2	8	.11	24	.07	3	.78	.01	.02	1	1
1622 LS-87 30N 19+50E	1	40	11	32	.1	14	8	111	5.25	2	5	ND	1	9	1	2	2	138	.25	.021	4	45	.25	35	.29	2	2.43	.01	.02	1	2
1623 LS-87 30N 20+00E	1	71	11	65	.1	29	10	215	4.95	6	5	ND	1	10	1	2	2	125	.24	.032	4	50	.66	40	.22	2	3.32	.01	.03	1	3
1624 LS-87 30N 20+50E	2	55	10	284	.1	40	29	7894	6.43	10	5	ND	1	23	1	2	2	110	.68	.114	12	57	.40	229	.22	6	4.88	.02	.06	2	1
1625 LS-87 30N 21+00E	1	52	10	63	.1	30	14	557	5.00	9	5	ND	2	11	1	2	2	127	.42	.047	5	46	.60	48	.28	3	2.87	.01	.03	1	1
STD C/AU-S	20	58	37	133	7.1	64	27	943	3.93	40	17	7	31	46	17	16	20	58	.48	.096	34	54	.88	171	.08	37	1.72	.07	.14	13	53

107-25
1000

ASHWORTH EXPLORATION PROJECT - LACY FILE # 87-0535

PAGE 3

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Aut1 PPB
LS-87 R-101	1	145	5	53	.1	7	13	620	3.41	2	5	ND	1	69	1	2	2	77	1.43	.092	3	3	1.57	18	.14	3	1.70	.03	.06	1	38
LS-87 R-120	29	34	11	61	.1	4	12	351	7.83	12	5	ND	1	9	1	6	2	29	.37	.164	6	3	.46	28	.01	3	1.13	.02	.16	1	8

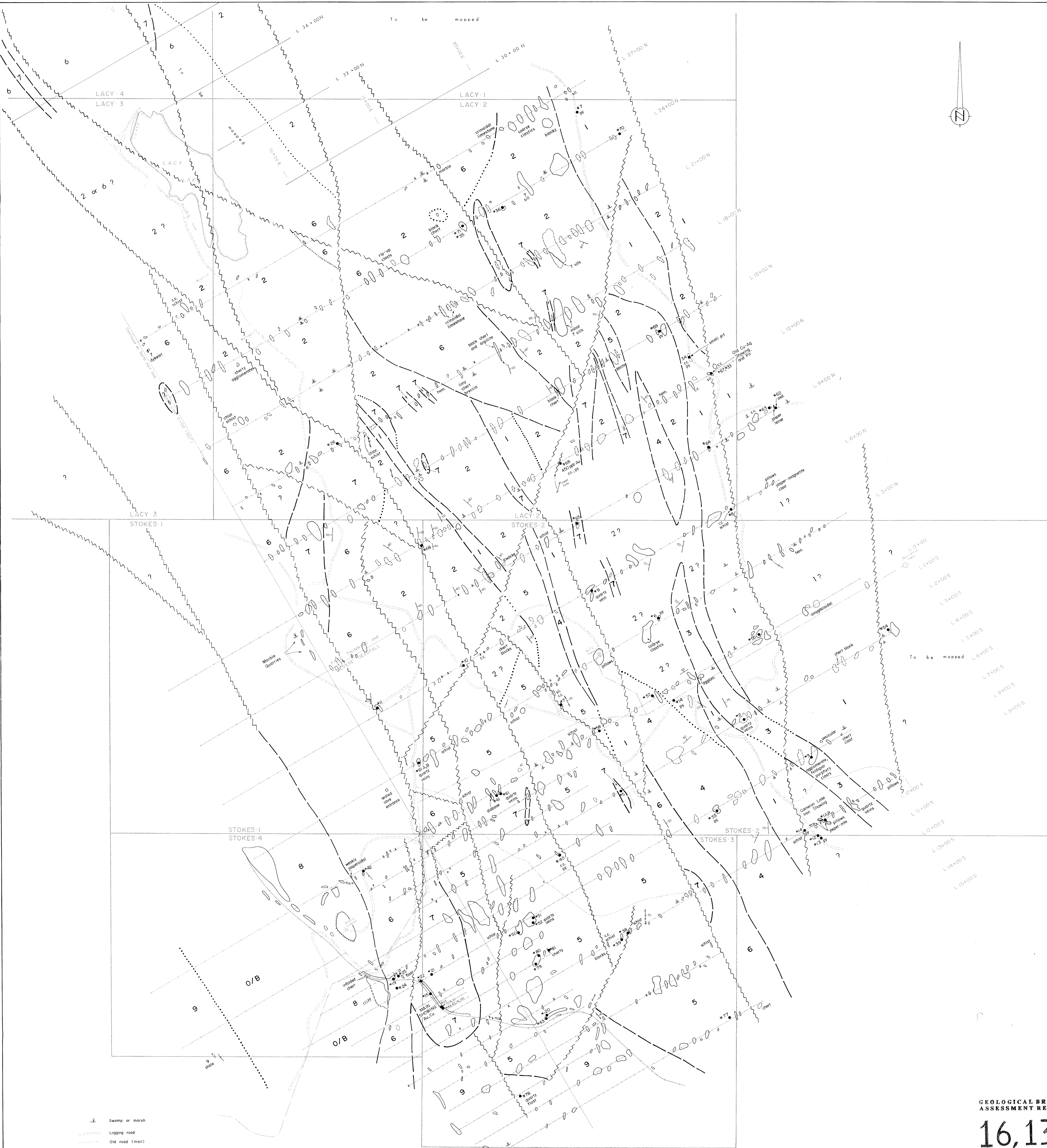
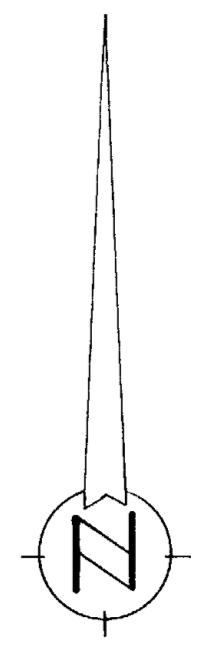
APPENDIX B

ITEMIZED COST STATEMENT

ITEMIZED COST STATEMENT

LACY-STOKES, ALBERNI MINING DIVISION,
VANCOUVER ISLAND, B.C.
PHASES IA, IB, IC, ID

PROJECT PREPARATION - all Phases	\$ 3,700	
MOB/DEMOB	<u>11,100</u>	\$ 14,800.00
PROJECT GEOLOGIST @ \$350/day x 36days	\$ 12,600	
FIELD GEOLOGIST @ \$275/day x 32days	8,800	
GEOPHYSICAL OPERATOR @ \$225/day x 36 x 2	16,200	
GEOTECHNICIANS @ \$190/day x 77mandays	<u>14,630</u>	\$ 52,230.00
LAB ANALYSIS (30 element analysis)		
1625 SOILS @ \$10.75/sample	\$ 17,468.75	
75 ROCK @ \$14.50/sample	<u>1,087.50</u>	
		\$ 18,556.25
INSTRUMENT RENTALS, including start-up CHECKS AND INSURANCE PROTON PRECESSION MAGNETOMETER PHOENIX VLF-2 @ \$150/day x 40 days	\$ 6,000	
DRILL RENTAL (plugger) \$750/mo.	1,500	
TRUCK RENTALS, including gas & mileage 2-4X4'S @ \$125/day x 36days	9,000	
COMMUNICATIONS @ \$50/day x 37days	1,850	
ROOM & BOARD @ \$70/day x 20mandays	15,400	
FIELD SUPPLIES \$100/day x 37 days	<u>3,700</u>	\$ 37,450.00
SUPERVISION @ \$450/day x 30days		\$ 13,500.00
CONSULTING & REPORTING (F.G.A.C.) (with field visits) @ \$450/day x 39	\$ 17,550.00	
CONSULTANT (4 days & disbursements)	1,579.17	
OFFICE SUPPORT (staff geologist) \$250/day x 23mandays	5,750.00	
SUB-CONTRACTS	2,400.00	
DRAFTING & MAPS	4,800.00	
COPYING, WORD PROCESSING, & BINDING	<u>1,600.00</u>	
		\$ 33,679.17
SUB-TOTAL		\$170,215.42
ADMINISTRATION 15%		<u>25,532.31</u>
TOTAL ALL PHASES		<u>\$195,747.73</u>

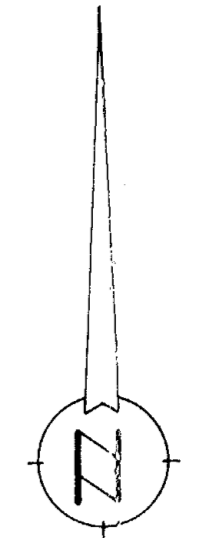


GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,138

Scale: 1:5000
Date: APRIL 1987
By: A.H. E.S. Drawn:
Map: J.A.
Ashworth Explorations Limited

LODE RESOURCE CORPORATION	
LACY & STOKES CLAIM GROUP	
ALBERNI and NANAIMO MINING DIVISIONS	
SOUTHERN HALF	
Geology and Rock Sampling	
Scale: 1:5000	By: A.H. E.S. Drawn:
Date: APRIL 1987	Map: J.A.
Ashworth Explorations Limited	



- Powerline
- Logging road
- Old road (trail)
- Flagged grid line
- Swamp or marsh
- Rock outcropping (large, small)
- Geological contact (assumed, approximate)
- Fault (assumed, probable)
- Schistosity, bedding
- Rock sample location and sample number (prefix LS-86 or LS-87)
- Sil - Silicification
- c.c. - Carbonatization
- mal. - Malachite
- py. - Pyrite
- hem. - Hematization

- TRIASSIC and (?) JURASSIC
- 8 Vancouver Group: basalt, andesite, and intrusive equivalent.
- PERMIAN and (?) EARLIER
- Sicker Group:
- 7 diabase dykes and sills, gabbro.
 - 6 limestone, commonly crinoidal, dark grey to black chert and argillite, minor tuff and pale jasper.
 - 4 laminated chert and cherty tuff, green to light green.
 - 2 mafic to intermediate volcanics and tuff, massive to thickly bedded, containing blocks and clasts of chert and volcanic rock, pale jasper and chert lenses.
 - 1 basaltic to andesitic volcanic and volcanoclastic rocks pillowed flows, tuff, agglomerate, pillow breccia and lenses of jasper-magnetite iron formation.

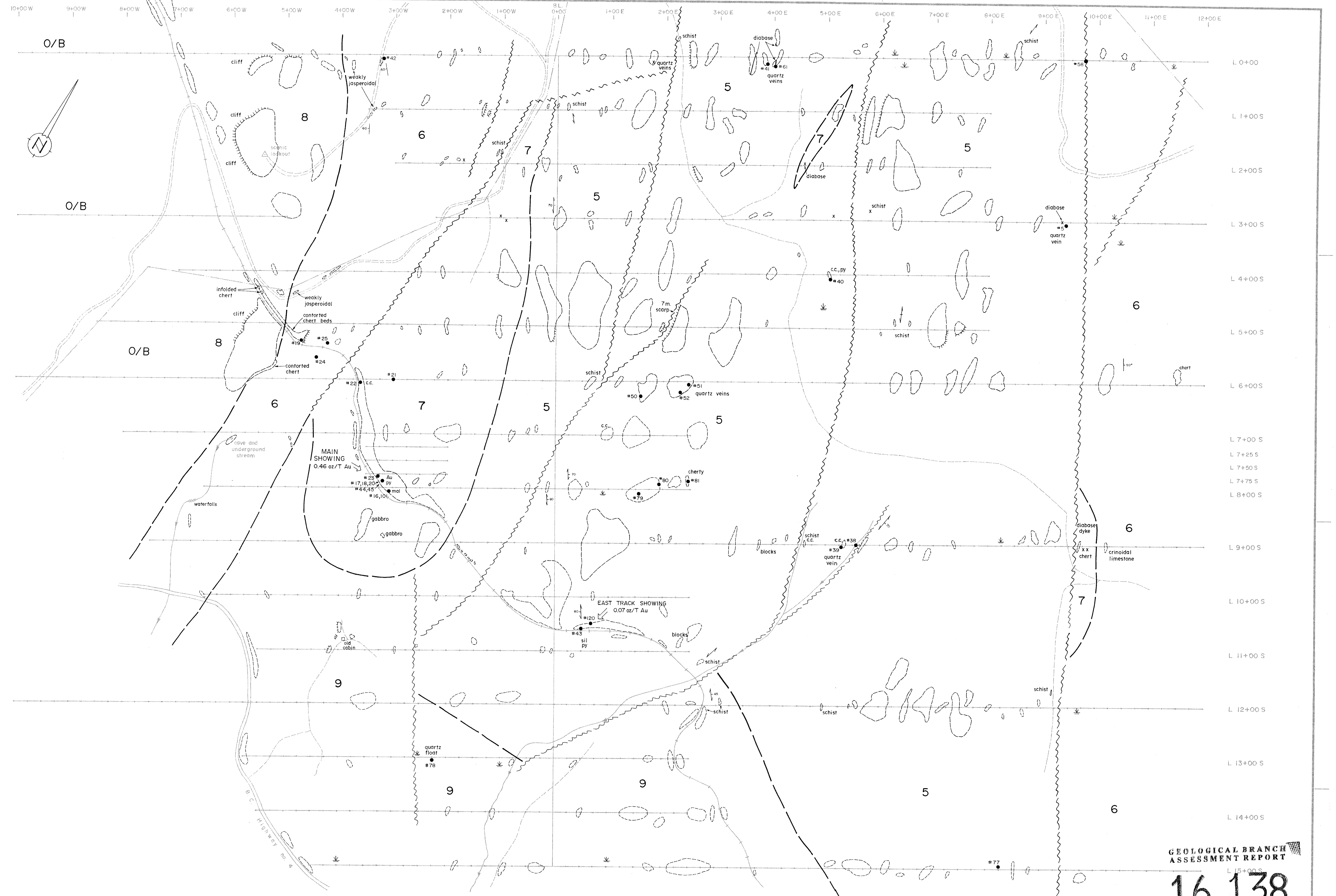


**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

16,138

0 50 100 200 300 400 500 metres

LODE RESOURCE CORPORATION	
LACY & STOKES CLAIM GROUP	
ALBERNI and NANAIMO MINING DIVISIONS	
NORTHERN HALF	
Geology and Rock Sampling	
Scale: 1:5000	By: A. H. E. S. Drawn:
Date: APRIL 1987	Map: 1 B
Ashworth Explorations Limited	

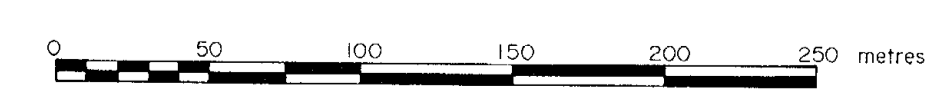


- Flagged grid line
- Powerline
- Highway
- Logging road
- Old road (trail)
- Creek
- Swamp or marsh

- x Rock outcropping (large, small)
- Geological contact
- Schistosity, bedding
- Faults (assumed, probable)
- Rock sample location and sample number (prefix LS 86 or LS 87)

- PLEISTOCENE and RECENT**
- sil. silicification
 - c.c. carbonatization
 - mal. malachite
 - py pyrite
 - hem. hematization
- CRETACEOUS**
- 9 Nanaimo group: mostly conglomerate, lesser shale and graywacke.
- TRIASSIC and (?) JURASSIC**
- 8 Vancouver group: basalt, andesite, and intrusive equivalents.

- PERMIAN and (?) EARLIER**
- Sicker group:
- 7 Diabase dykes and sills, gabbro.
 - 6 limestone, commonly crinoidal, dark grey to black chert and argillite, minor tuff and pale jasper.
 - 5 dacite and andesite flows, minor chert and tuff, agglomerate, breccia.

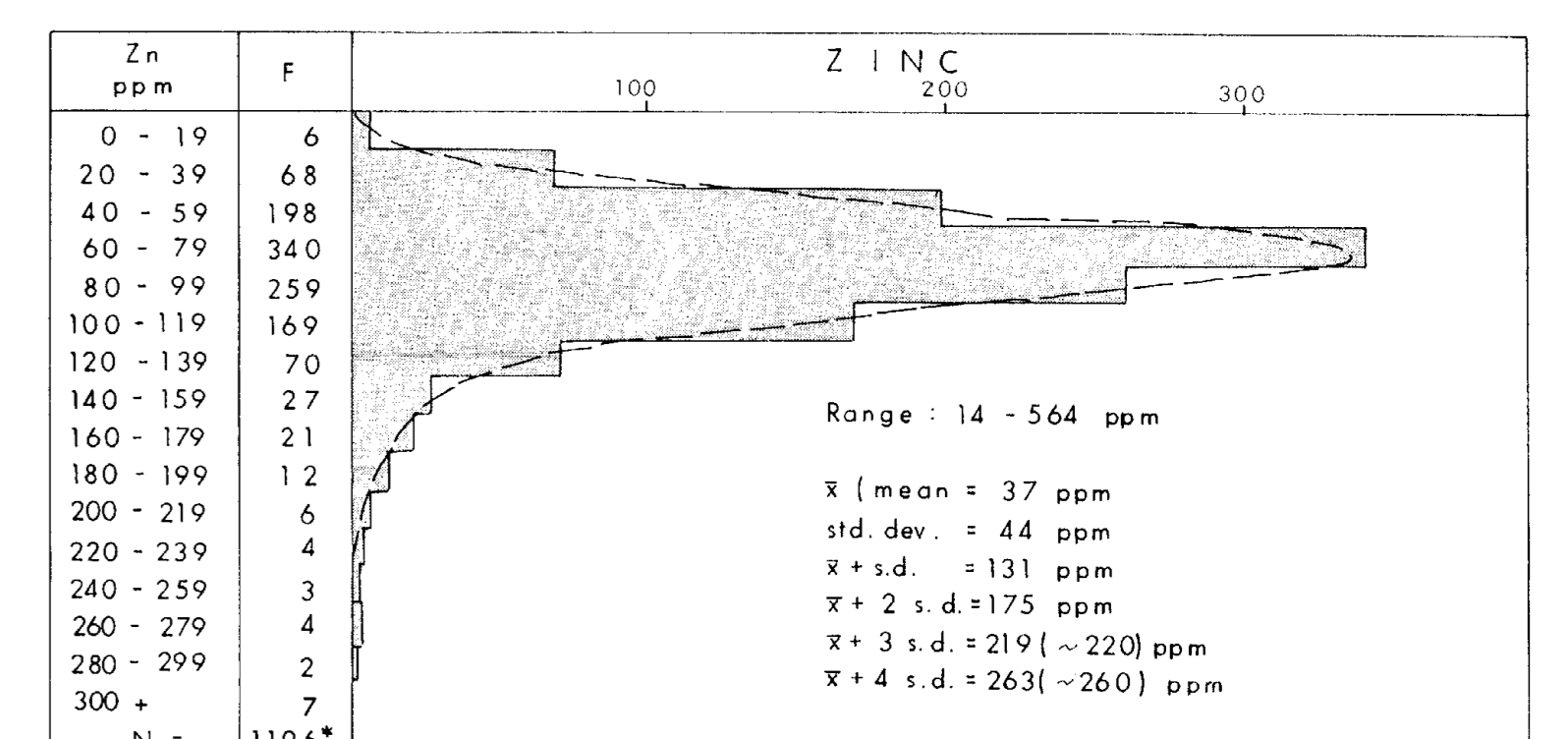
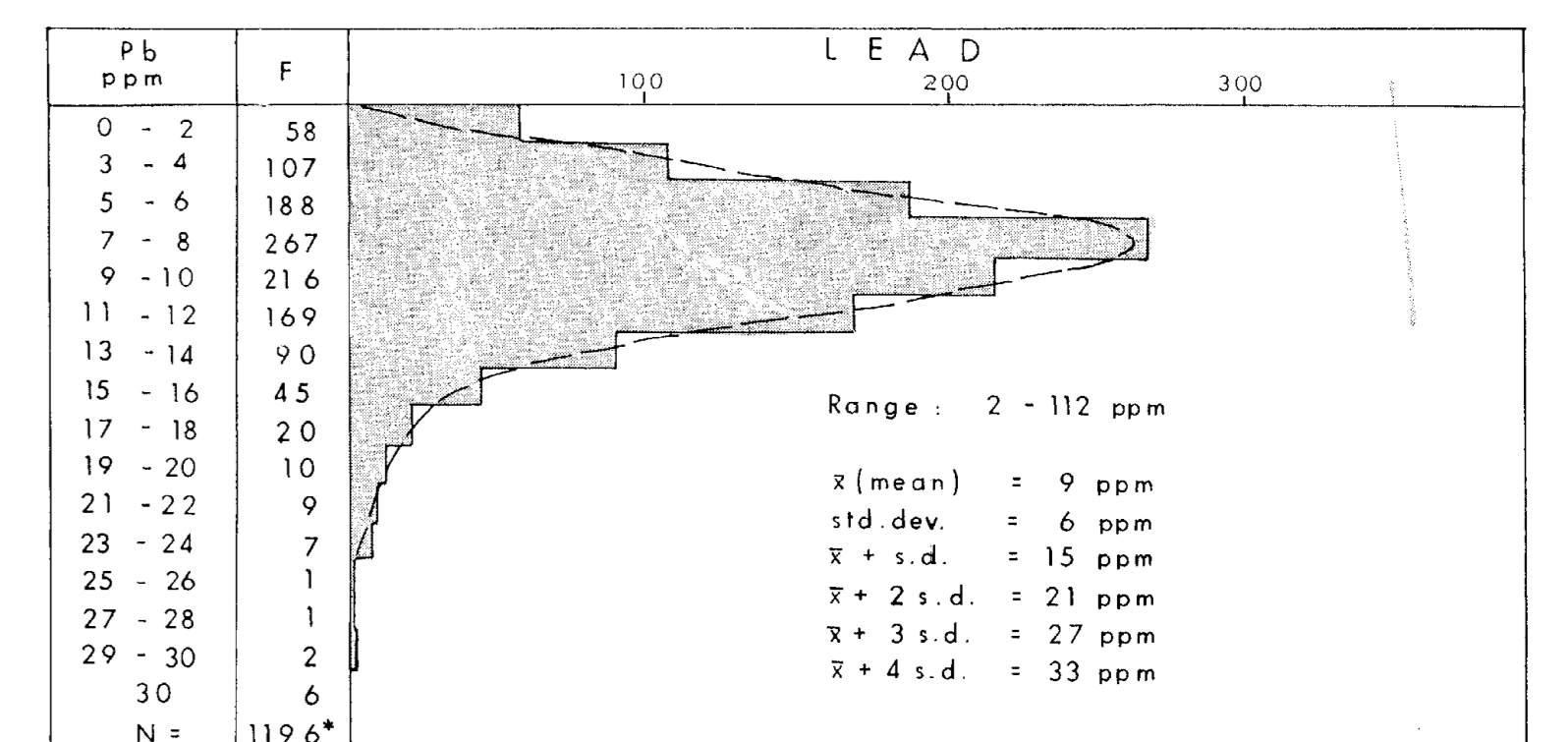
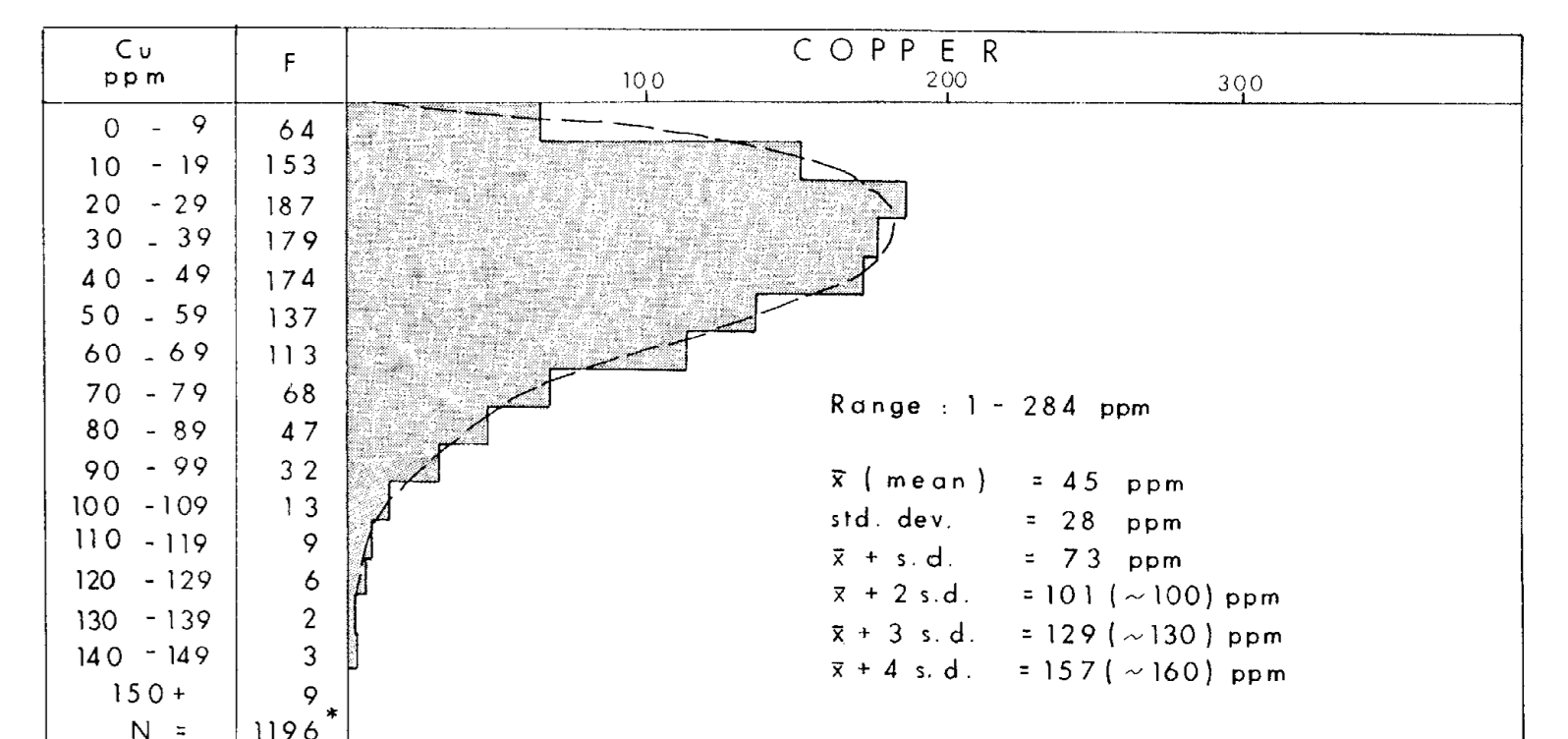
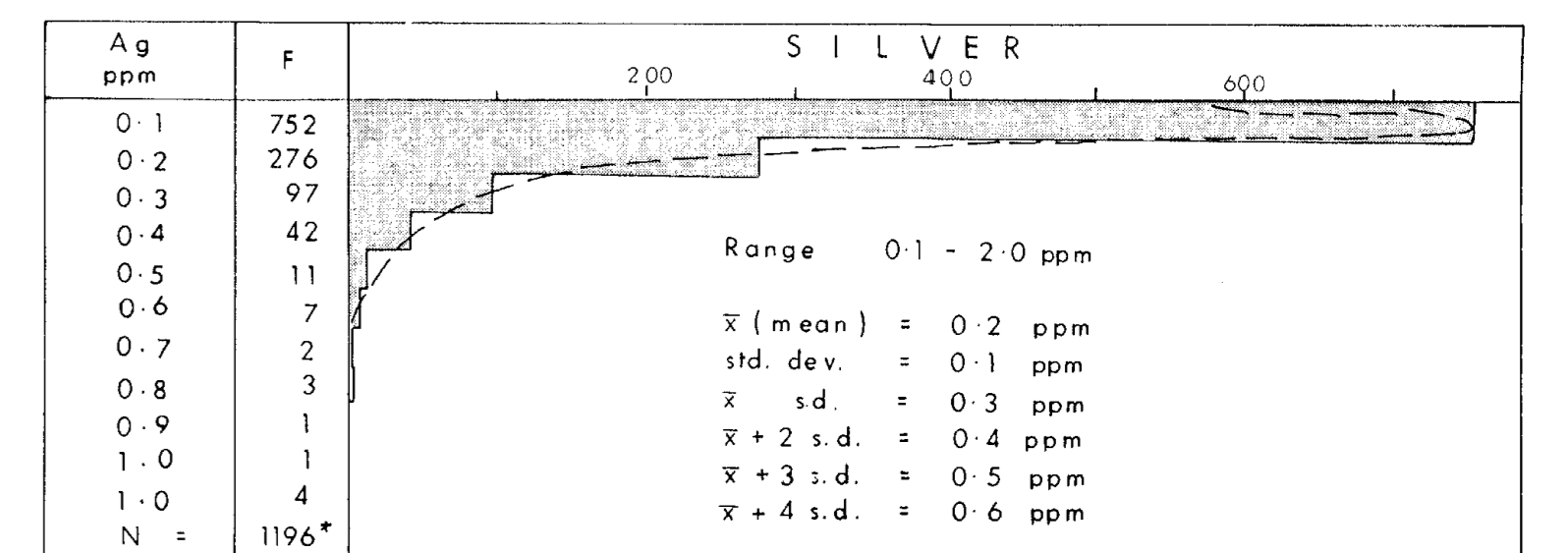


GEOLOGICAL BRANCH ASSESSMENT REPORT

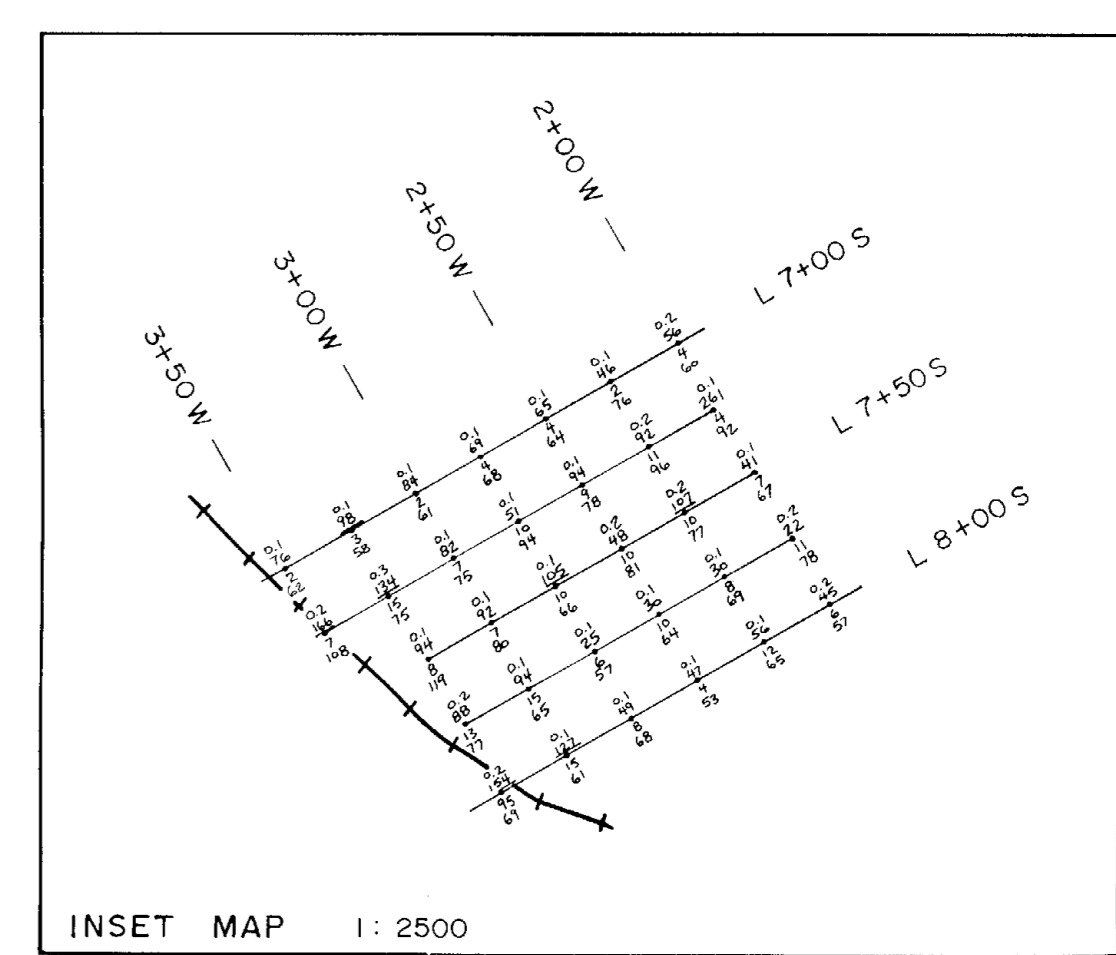
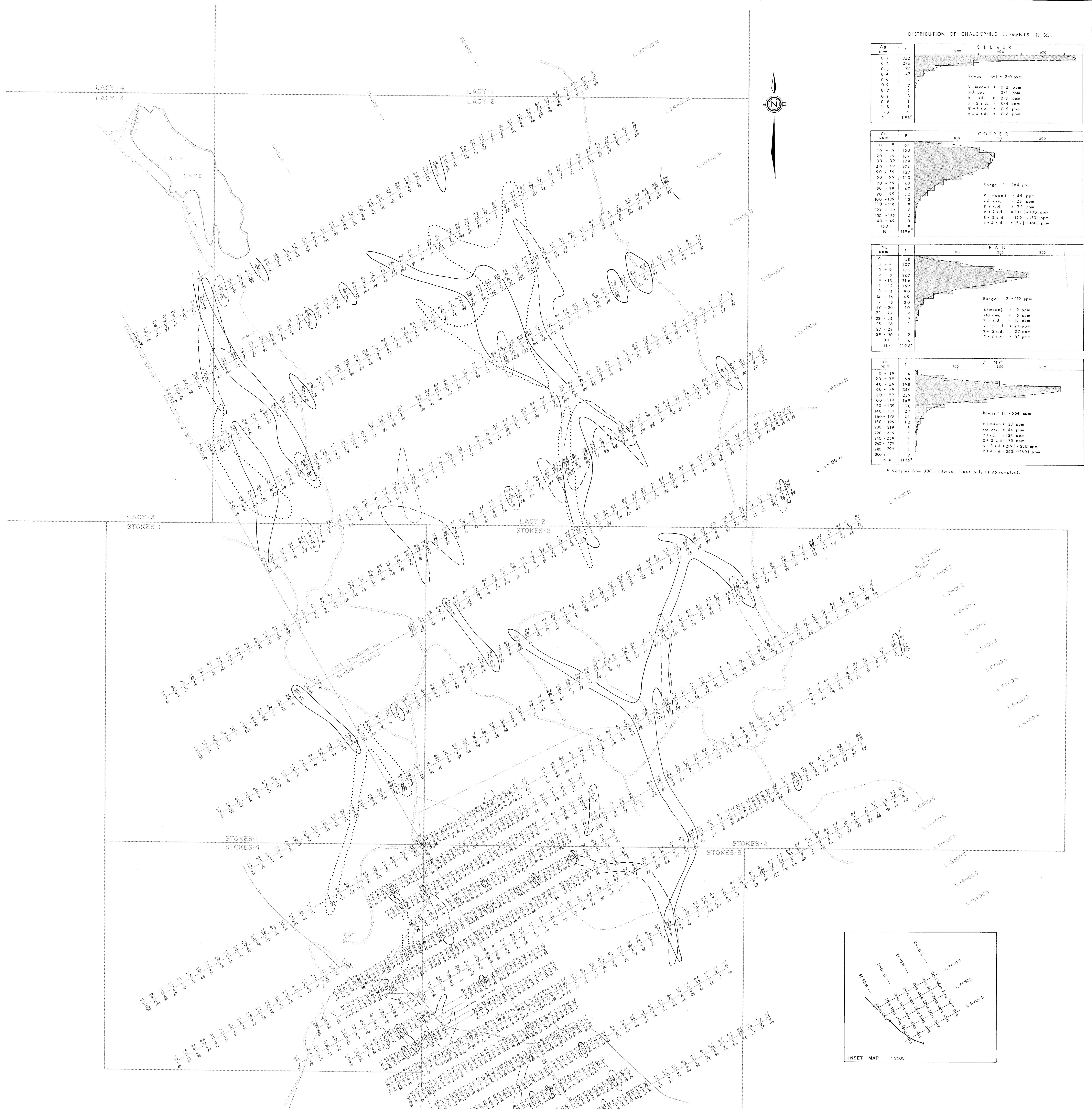
16,138

LODE RESOURCE CORPORATION	
LACY & STOKES CLAIM GROUP	
ALBERNI and NANAIMO MINING DIVISIONS	
SOUTHERN HALF DETAIL GRID	
DETAIL GRID AREA	
Geology and Rock Sampling	
Scale: 1:2500	By: A.H., E.S. Drawn:
Date: APRIL 1987	Map: 2
Ashworth Explorations Limited	

DISTRIBUTION OF CHALCOPHILE ELEMENTS IN SOIL



* Samples from 300 m interval lines only (1196 samples).



LEGEND

- Logging road
- Old road (trail)
- Railway tracks
- Powerline
- Flagged grid lines, sample locations, and geochemical soil sample results

- >0.4 ppm Ag underlined (anomalous)
- >100 ppm Cu underlined (anomalous)
- >20 ppm Pb underlined (anomalous)
- >175 ppm Zn underlined (anomalous)

MAIN ANOMALOUS TRENDS

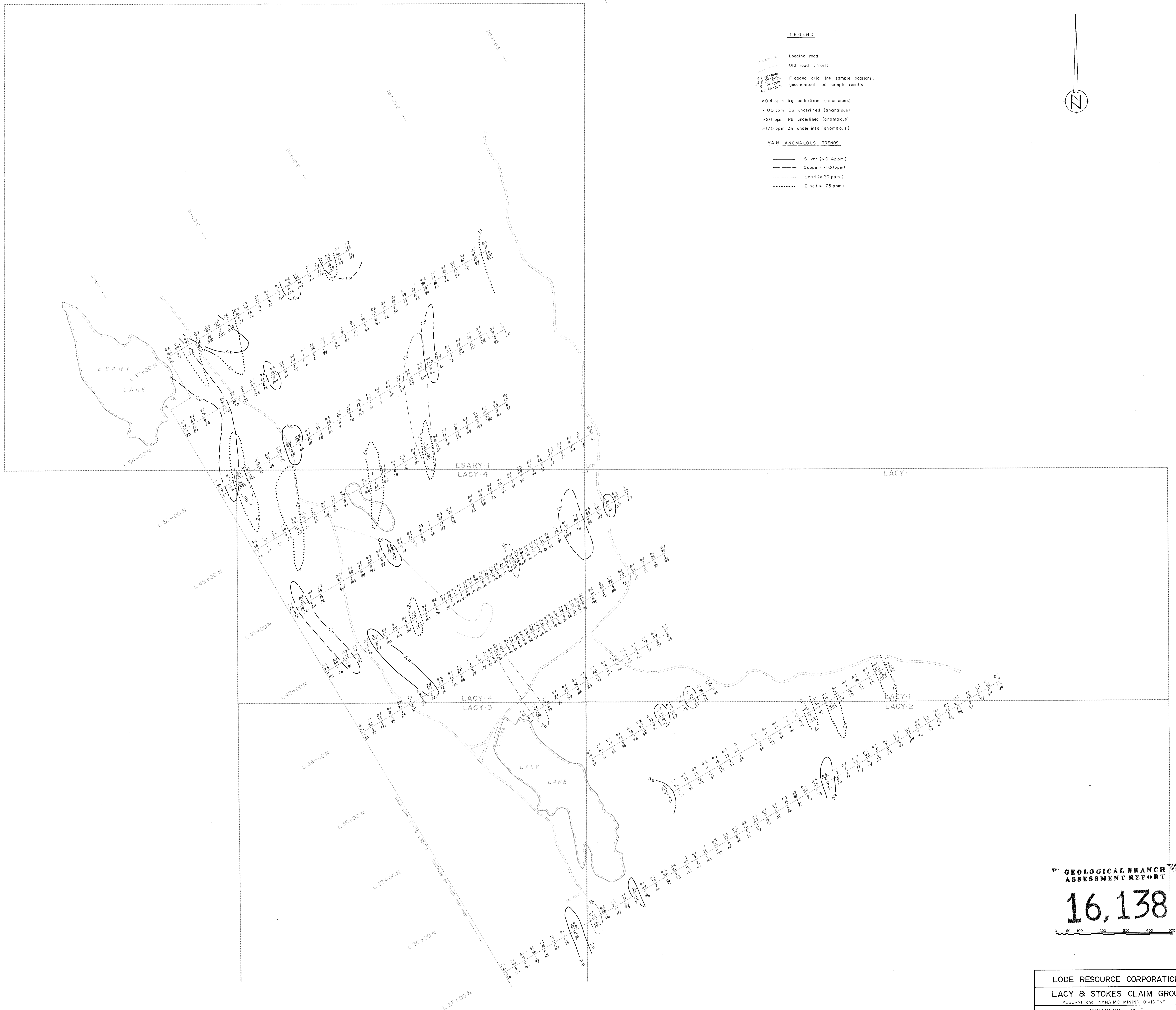
- Silver (>0.4 ppm)
- Copper (>100ppm)
- Lead (>20ppm)
- Zinc (>175 ppm)

GEOLOGICAL BRANCH ASSESSMENT REPORT

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Scale: 1:5000 Date: APRIL 1987

LODE RESOURCE CORPORATION
 LACY & STOKES CLAIM GROUP
 ALBERNI and NANAIMO MINING DIVISIONS
 SOUTHERN HALF
 GEOCHEMICAL SURVEY
 Silver, Copper, Lead and Zinc
 in Soils
 By: H. L. Drawn:
 Map: 3 A
 Ashworth Explorations Limited



LEGEND

Logging road
 Old road (trail)

Flagged grid line, sample locations,
 geochemical soil sample results

>0.4 ppm Ag underlined (anomalous)
 >100 ppm Cu underlined (anomalous)
 >20 ppm Pb underlined (anomalous)
 >175 ppm Zn underlined (anomalous)

MAIN ANOMALOUS TRENDS:

— Silver (>0.4 ppm)
 - - - Copper (>100 ppm)
 . . . Lead (>20 ppm)
 - . . . Zinc (>175 ppm)

**GEOLOGICAL BRANCH
 ASSESSMENT REPORT**

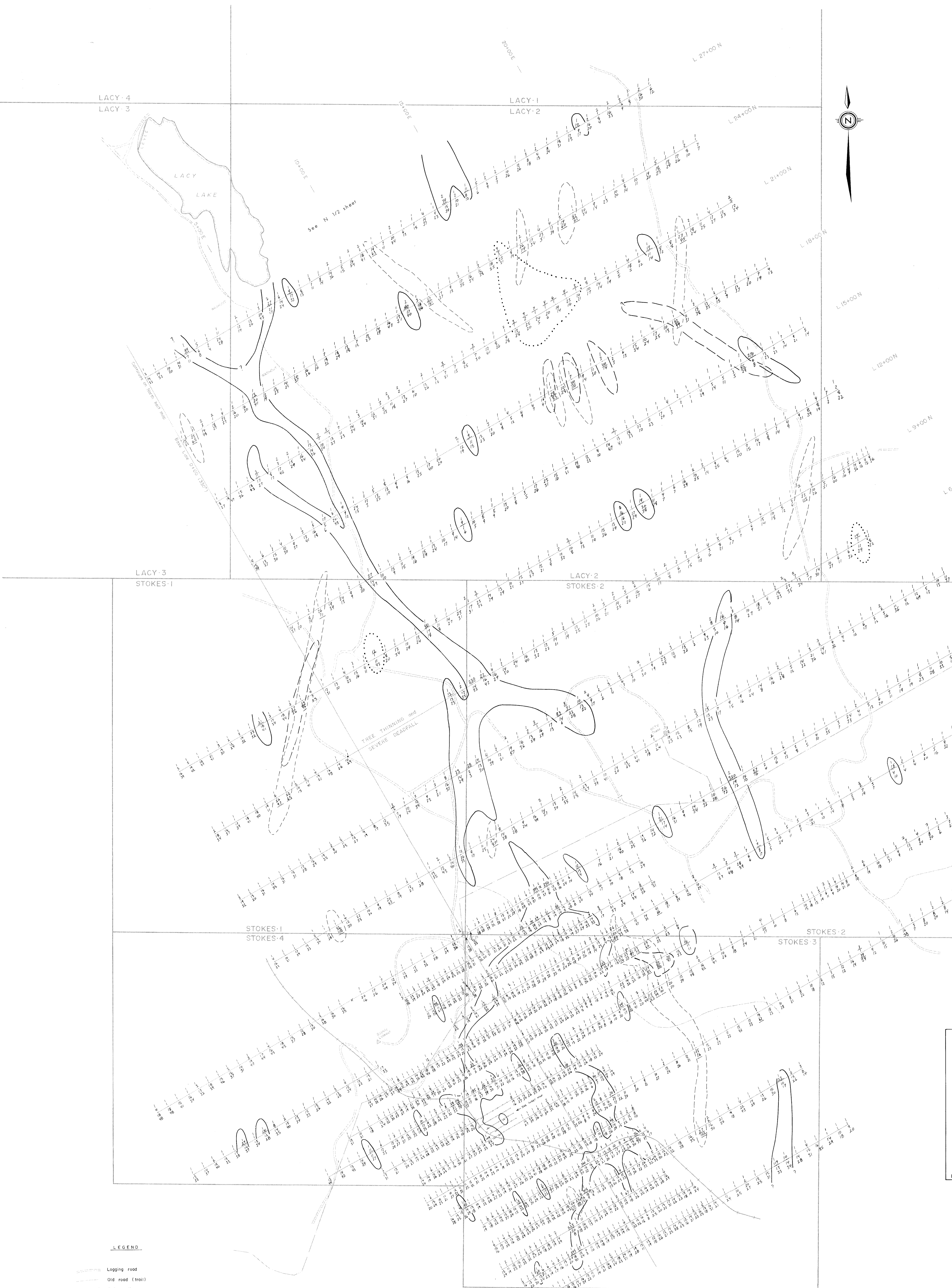
16,138

0 50 100 200 300 400 500 metres

LODE RESOURCE CORPORATION
 LACY & STOKES CLAIM GROUP
 ALBERNI and NANAIMO MINING DIVISIONS
 NORTHERN HALF
 GEOCHEMICAL SURVEY
 Silver, Copper, Lead and Zinc
 in Soils

Scale: 1 : 5000 By: H. L. Drawn:
 Date: APRIL 1987 Map: 3 B

Ashworth Explorations Limited



DISTRIBUTION OF SIDEROPHILE ELEMENTS IN SOIL

Au ppm	F	100	500	1000
1 - 2	914			
3 - 4	134			
5 - 6	47			
7 - 8	27			
9 - 10	12			
11 - 12	9			
13 - 14	8			
15 - 16	4			
17 - 18	2			
19 - 20	2			
21 - 22	3			
23 - 24	3			
25 - 26	1			
27 - 28	2			
29 - 30	2			
>30	2			
N:	1196*			

Range : 1 - 415 ppb
 Calculated at 30 ppb cutoff (N = 1172):
 Z (mean) = 2.35 ppm
 std. dev. = 3.38 ppb
 X + s.d. = 5.73 (6) ppb
 X - 2 s.d. = 9.11 (9) ppb
 X + 3 s.d. = 12.49 (12) ppb
 X - 4 s.d. = 15.87 (16) ppb

Mo ppm	F	100	500	1000
1	1051			
2	101			
3	34			
4	4			
5	-			
6	1			
7	1			
8	-			
9	2			
10	2			
N:	1196*			

Range : 1 - 14 ppm
 Z (mean) = 1 ppm
 std. dev. = 1 ppm
 X + s.d. = 2 ppm
 X - 2 s.d. = 3 ppm
 X + 3 s.d. = 4 ppm
 X - 4 s.d. = 5 ppm

Co ppm	F	100	200	300
1 - 4	101			
5 - 8	206			
9 - 12	336			
13 - 16	335			
17 - 20	123			
21 - 24	54			
25 - 28	22			
29 - 32	3			
33 - 36	5			
37 - 40	3			
41 - 44	5			
45	3			
N:	1196*			

Range : 1 - 65 ppm
 Z (mean) = 1.3 ppm
 std. dev. = 7 ppm
 X + s.d. = 20 ppm
 X - 2 s.d. = 27 ppm
 X + 3 s.d. = 34 ppm
 X - 4 s.d. = 41 ppm

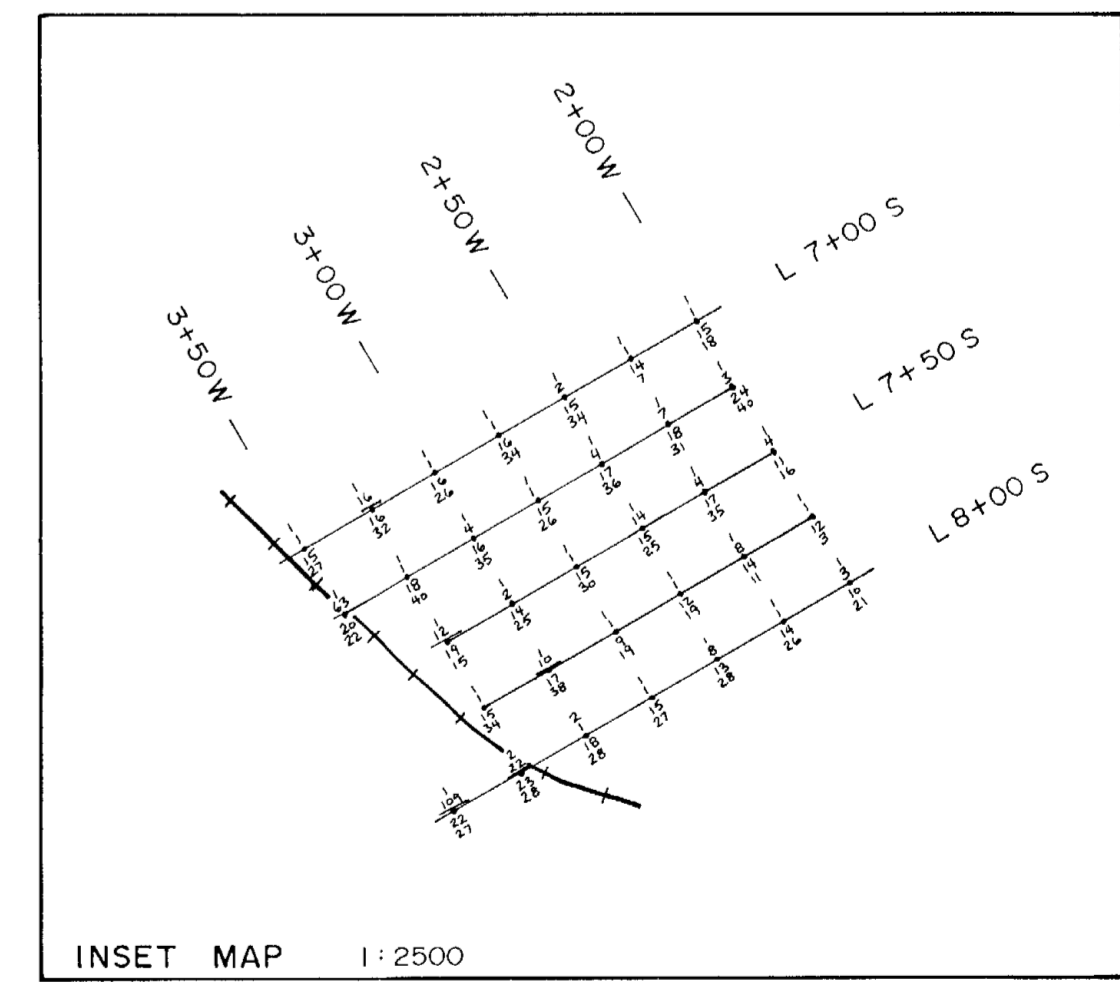
Ni ppm	F	100	200	300
0 - 9	102			
10 - 19	203			
20 - 29	361			
30 - 39	261			
40 - 49	110			
50 - 59	37			
60 - 69	18			
70 - 79	9			
80 - 89	6			
90 - 99	7			
100 - 109	3			
110 - 119	4			
120 - 129	1			
130 -	4			
N:	1196*			

Range : 1 - 565 ppm
 Calculated at 125 ppm cutoff (N = 1192):
 Z (mean) = 26 ppm
 std. dev. = 16 ppm
 X + s.d. = 44 ppm
 X - 2 s.d. = 61 ppm
 X + 3 s.d. = 77 ppm
 X - 4 s.d. = 94 ppm

* Samples from 300m interval lines only (1196 samples)

LEGEND

- Logging road
- Old road (trail)
- Railway line
- Powerline
- Flogged grid line, sample locations, geochemical soil sample results.
- > 3 ppm Mo underlined (anomalous)
- > 9 ppb Au underlined (anomalous)
- > 27 ppm Co underlined (anomalous)
- > 6 ppm Ni underlined (anomalous)
- MAIN ANOMALOUS TRENDS**
- Gold (> 9 ppb)
- Molybdenum (> 3 ppm)
- Cobalt (> 27 ppm)
- Nickel (> 6 ppm)



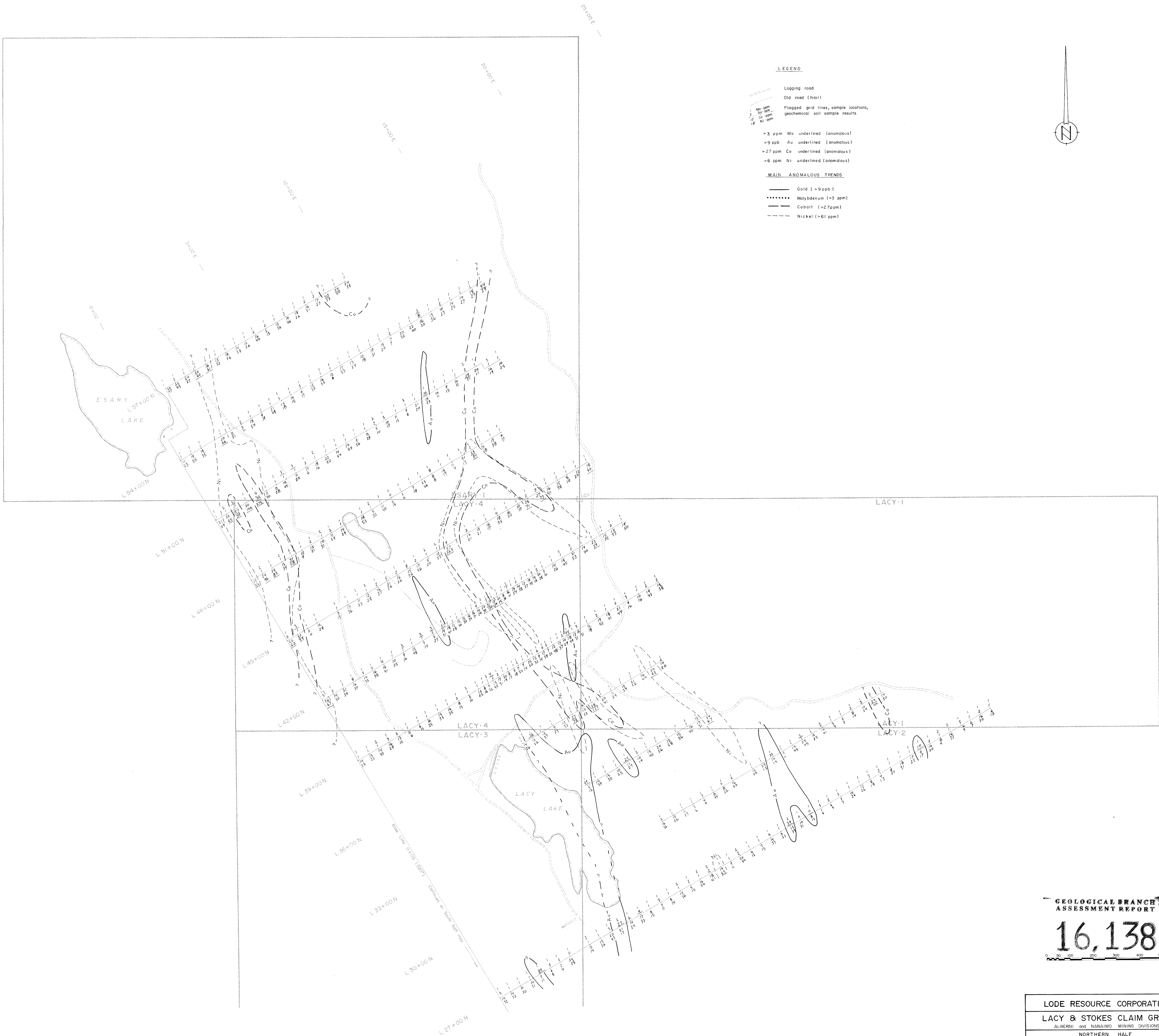
GEOLOGICAL BRANCH
 ASSESSMENT REPORT

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Scale: 1:5000 By: H. L. Drawn:
 Date: APRIL 1987 Map: 4.A

ASHORTH EXPLORATIONS LIMITED

LODE RESOURCE CORPORATION
 LACY & STOKES CLAIM GROUP
 ALBERNI and NANAIMO MINING DIVISIONS
 SOUTHERN HALF
 GEOCHEMICAL SURVEY
 Molybdenum, Gold, Cobalt and Nickel
 in Soils



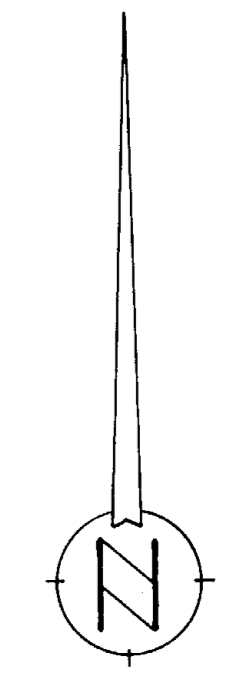
LEGEND

Logging road
 Old road (trail)
 Flagged grid lines, sample locations,
 geochemical soil sample results

> 3 ppm Mo underlined (anomalous)
 > 9 ppb Au underlined (anomalous)
 > 27 ppm Co underlined (anomalous)
 > 6 ppm Ni underlined (anomalous)

MAIN ANOMALOUS TRENDS

Gold (> 9 ppb)
 Molybdenum (> 3 ppm)
 Cobalt (> 27 ppm)
 Nickel (> 6 ppm)

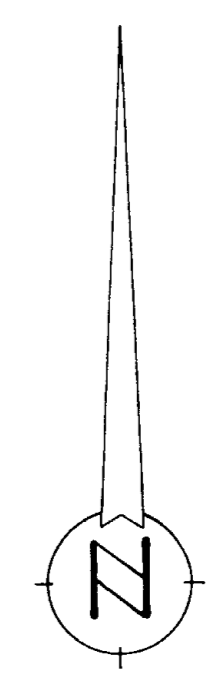


**GEOLOGICAL BRANCH
 ASSESSMENT REPORT**

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0 50 100 200 300 400 500 metres

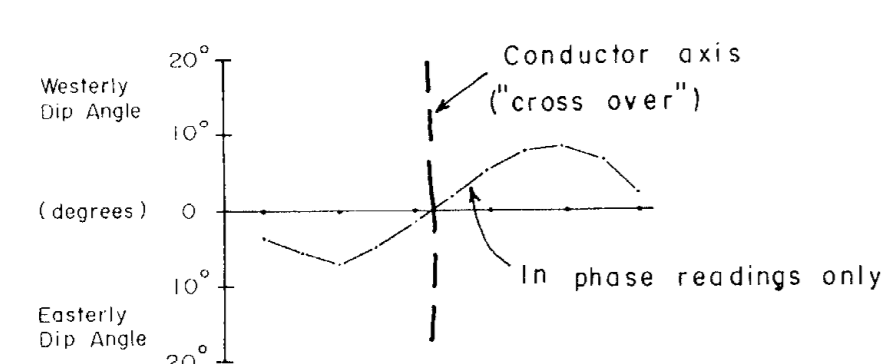
LODE RESOURCE CORPORATION	
LACY & STOKES CLAIM GROUP	
ALBERNI and NANAIMO MINING DIVISIONS	
NORTHERN HALF	
GEOCHEMICAL SURVEY	
Gold, Molybdenum, Cobalt and Nickel in Soils	
Scale: 1:5000	By: H.L. Drawn:
Date: APRIL 1987	Map: 4 J
Ashworth Explorations Limited	



LEGEND

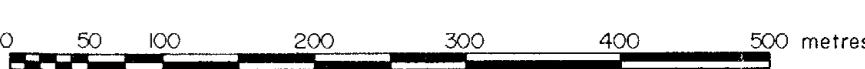
- Logging road
- Old road (trail)
- Railway tracks
- Powerline
- Flogged grid line

Instrument: PHOENIX VLF-2
 Transmitter station: SEATTLE, WASHINGTON
 24.8 KHZ

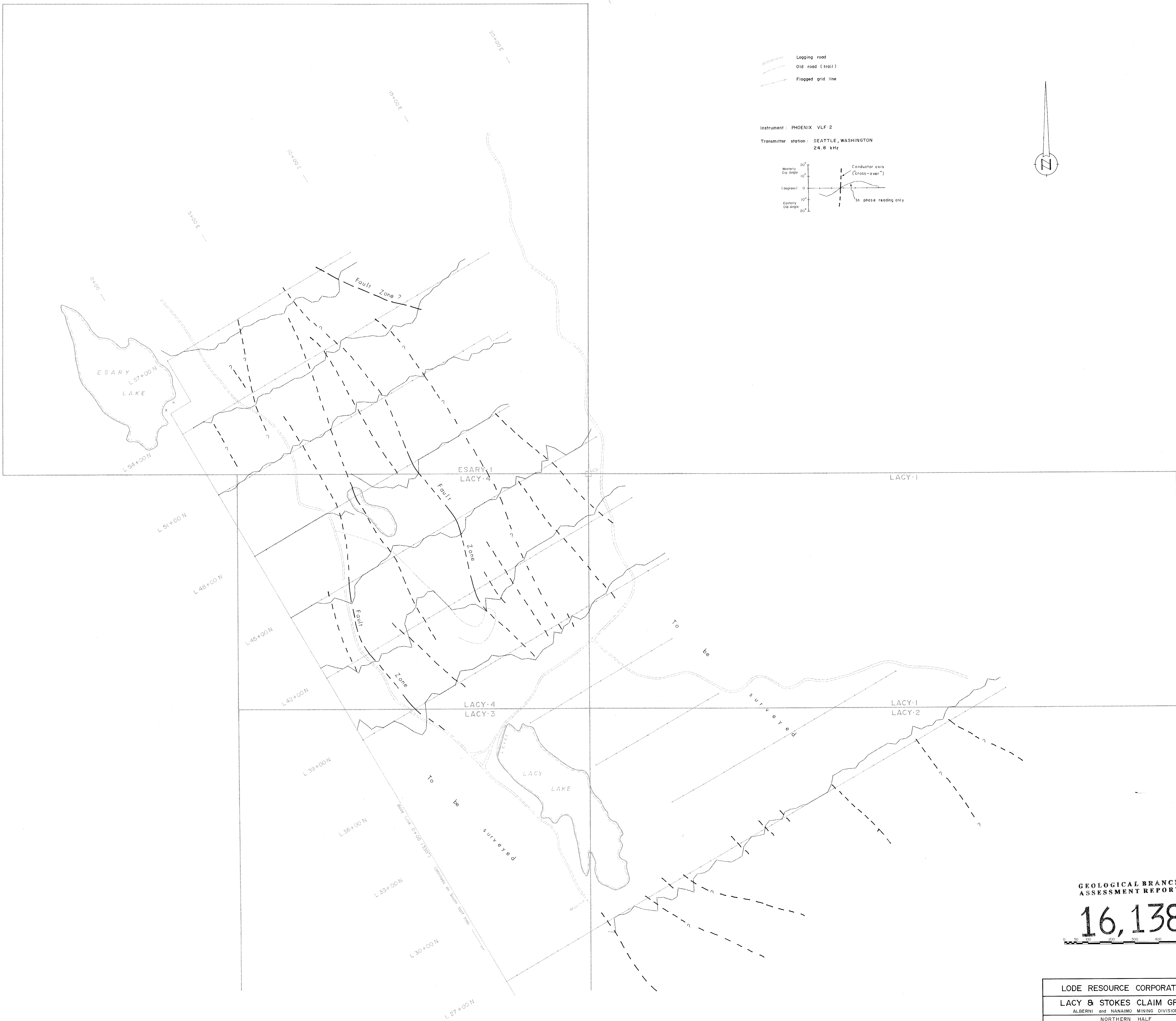


**GEOLOGICAL BRANCH
 ASSESSMENT REPORT**

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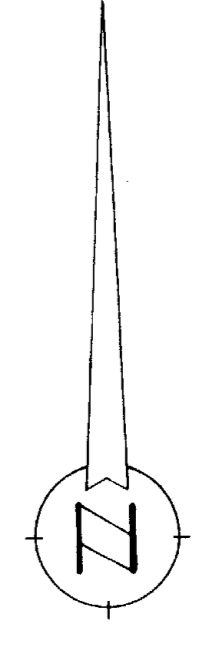
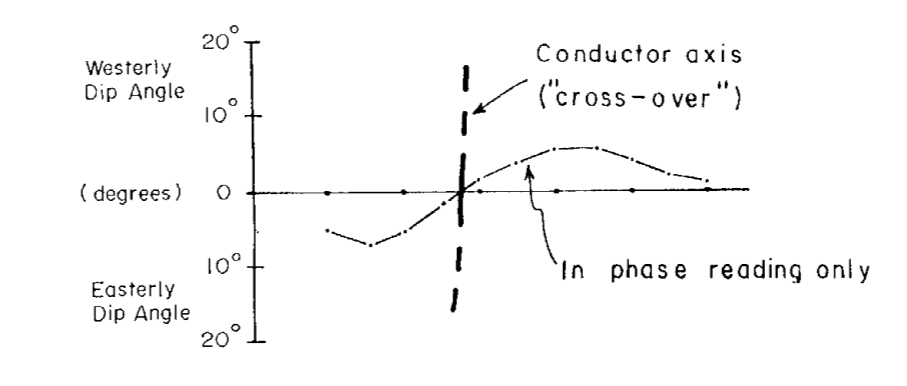


LODE RESOURCE CORPORATION	
LACY & STOKES CLAIM GROUP	
ALBERNI and NANAIMO MINING DIVISIONS	
SOUTHERN HALF	
VLF-EM SURVEY	
Scale: 1:5000	By: H. L. Drawn:
Date: APRIL 1987	Map: 5.A
Ashworth Explorations Limited	



- Logging road
- Old road (trail)
- Flagged grid line

Instrument: PHOENIX VLF-2
 Transmitter station: SEATTLE, WASHINGTON
 24.8 kHz



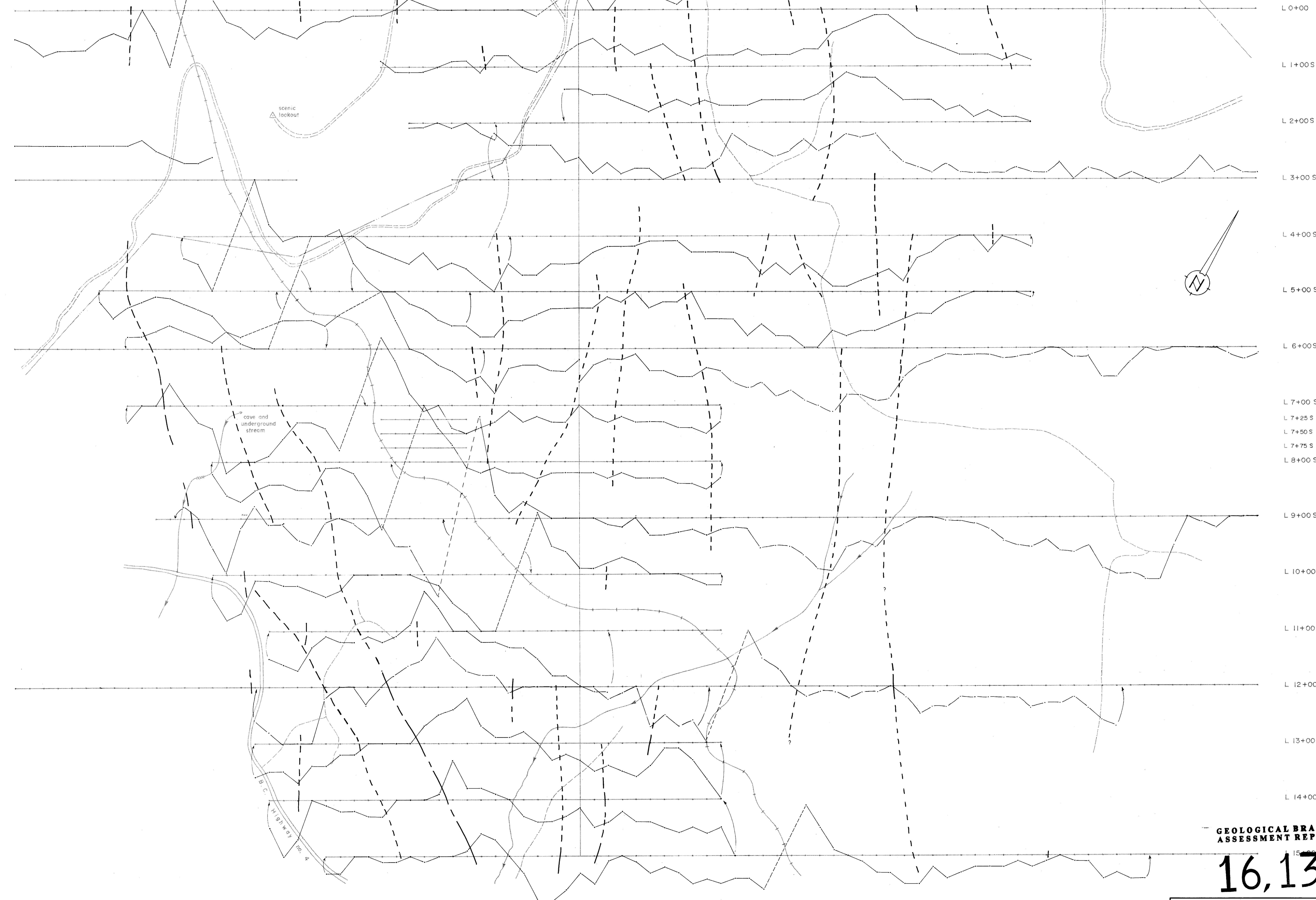
GEOLOGICAL BRANCH
 ASSESSMENT REPORT

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LODE RESOURCE CORPORATION	
LACY & STOKES CLAIM GROUP	
ALBERNI and NANAIMO MINING DIVISIONS	
NORTHERN HALF	
VLF-EM SURVEY	
Scale: 1:5000	By: H.L. Drawn:
Date: APRIL 1987	Map: 5 B
Ashworth Explorations Limited	

10+00W 9+00W 8+00W 7+00W 6+00W 5+00W 4+00W 3+00W 2+00W 1+00W BL 0+00 1+00E 2+00E 3+00E 4+00E 5+00E 6+00E 7+00E 8+00E 9+00E 10+00E 11+00E 12+00E



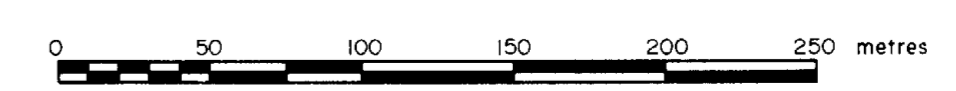
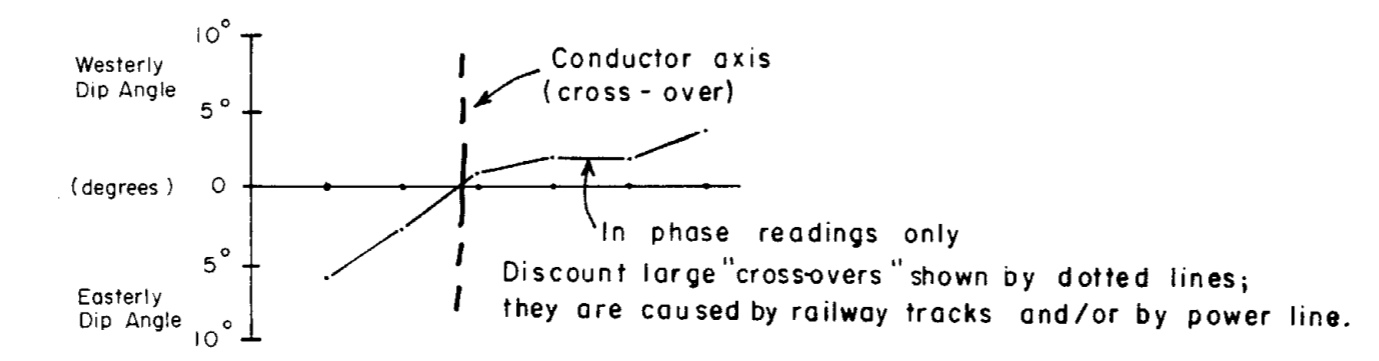
scenic lockout

cave and underground stream

B.C. HIGHWAY No. 4

- Flagged grid line
- Powerline
- Highway
- Logging road
- Old road (trail)
- Creek
- Railway tracks

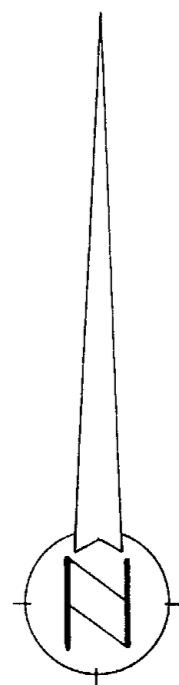
Instrument: PHOENIX VLF-2
 Transmitter station: SEATTLE, WASHINGTON
 24.8 kHz



GEOLOGICAL BRANCH ASSESSMENT REPORT

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LODE RESOURCE CORPORATION		
LACY & STOKES CLAIM GROUP		
ALBERNI and NANAIMO MINING DIVISIONS		
SOUTHERN HALF DETAIL GRID		
DETAIL GRID AREA		
VLF-EM SURVEY		
Scale: 1:2500	By: H.L.	Drawn:
Date: APRIL 1987	Map: 6	
Ashworth Explorations Limited		



LACY-4
LACY-3

LACY-1
LACY-2



LACY-3
STOKES-1

LACY-2
STOKES-2

STOKES-1
STOKES-4

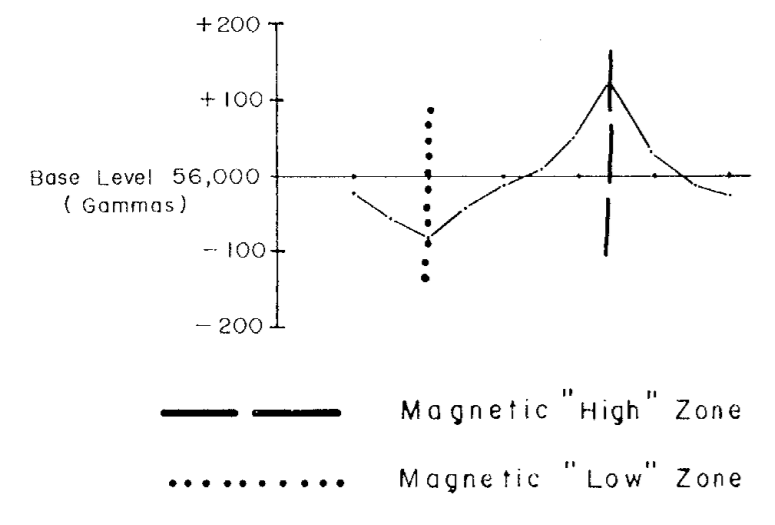
STOKES-3

L 0+00
L 1+00 S
L 2+00 S
L 3+00 S
L 4+00 S
L 5+00 S
L 6+00 S
L 7+00 S
L 8+00 S
L 9+00 S

LEGEND

- Logging road
- Old road (trail)
- Railway tracks
- Powerline
- Flogged grid line

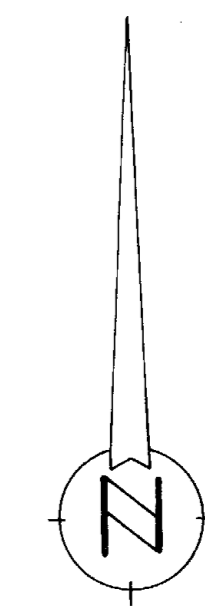
Instrument: SCINTREX MP-2



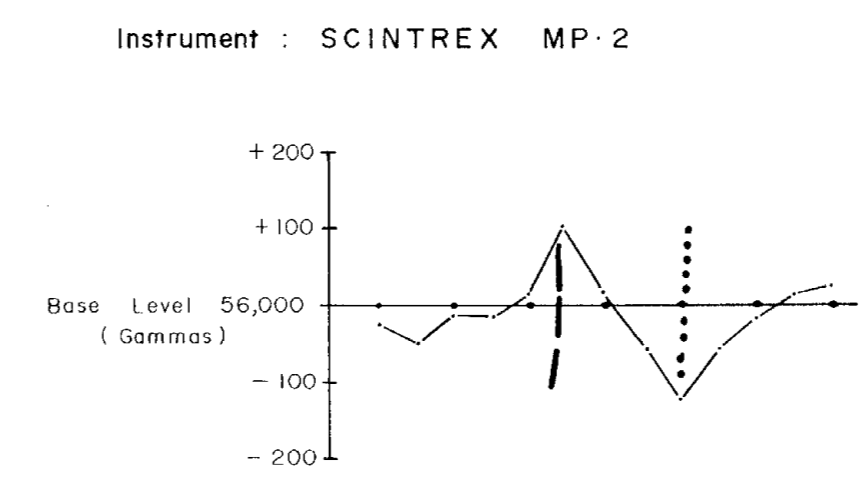
GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,138

LODE RESOURCE CORPORATION	
LACY & STOKES CLAIM GROUP	
ALBERNI and NANAIMO MINING DIVISIONS	
SOUTHERN HALF (includes DETAIL AREA)	
Magnetometer Survey	
Scale: 1:5000	By: H.L. Drawn:
Date: APRIL 1987	Map: 7.A
Ashworth Explorations Limited	



LEGEND
Logging road
Old road (trail)
Flagged grid line

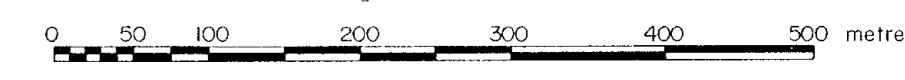


--- Magnetic "High" Zone
..... Magnetic "Low" Zone



**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

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LODE RESOURCE CORPORATION		
LACY & STOKES CLAIM GROUP		
ALBERNI and NANAIMO MINING DIVISIONS		
NORTHERN HALF		
Magnetometer Survey		
Scale: 1:5000	By: H.L.	Drawn:
Date: APRIL 1987	Map: 7.B	
Ashworth Explorations Limited		