GEOLOGICAL, GEOPHYSICAL AND GEOCHEMICAL REPORT

ON THE

MATSON PROPERTY

FOR

Owner/Operator: KELSO RESOURCES LTD.

LILLOOET MINING DIVISION
BRITISH COLUMBIA

NTS 92J 16E
WEST LONGITUDE: 122 DEG. ~~15~~ 12'24"
NORTH LATITUDE: 50 DEG. ~~45~~ 46'06"

BY

MOUNTAINSIDE MANAGEMENT LTD.

JOHN FAIRLEY, B.A.Sc., P. ENG
DARCY KROHMAN, B. SC., GEOL.

AUGUST 19, 1987

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SUMMARY

At the request of Kelso Resources Ltd., a first phase exploration program was completed on the Matson Claim Group by Mountainside Management Limited. The program was performed during June of 1987, and included geological, geochemical and geophysical surveys, and blasting and trenching. The purpose of the program was to define targets with potential for gold/silver mineralization.

The Matson Claim Group consists of 12 located 2-post mineral claims and 2 located 4-post mineral claims for a total of 38 units. The claim group is situated approximately 50 kilometers west of Lillooet, B.C. in the Lillooet Mining Division. A B.C. Hydro access road transects the property.

The Matson claim group lies near the Bralorne Mining Camp, which has been prospected since the 1890's. Development work consisting of a single adit and several pits was done on the Matson property during the 1940's. There is no history of production from the property.

The present exploration program was concentrated on a control grid established on the Matson property. Encouraging geological, geochemical, and geophysical results were obtained. An anomalous zone approximately 600 x 400 m's near the west central portion of the grid appears to be related to sulfide mineralization. Assays of rock chip samples from the old workings returned significant gold and silver values (from trace values to 0.179 oz/t Au and 8.36 oz/t Ag).

Signed at Vancouver, B.C.

John Fairley, P.Eng.
August 18, 1987

PART A

Introduction

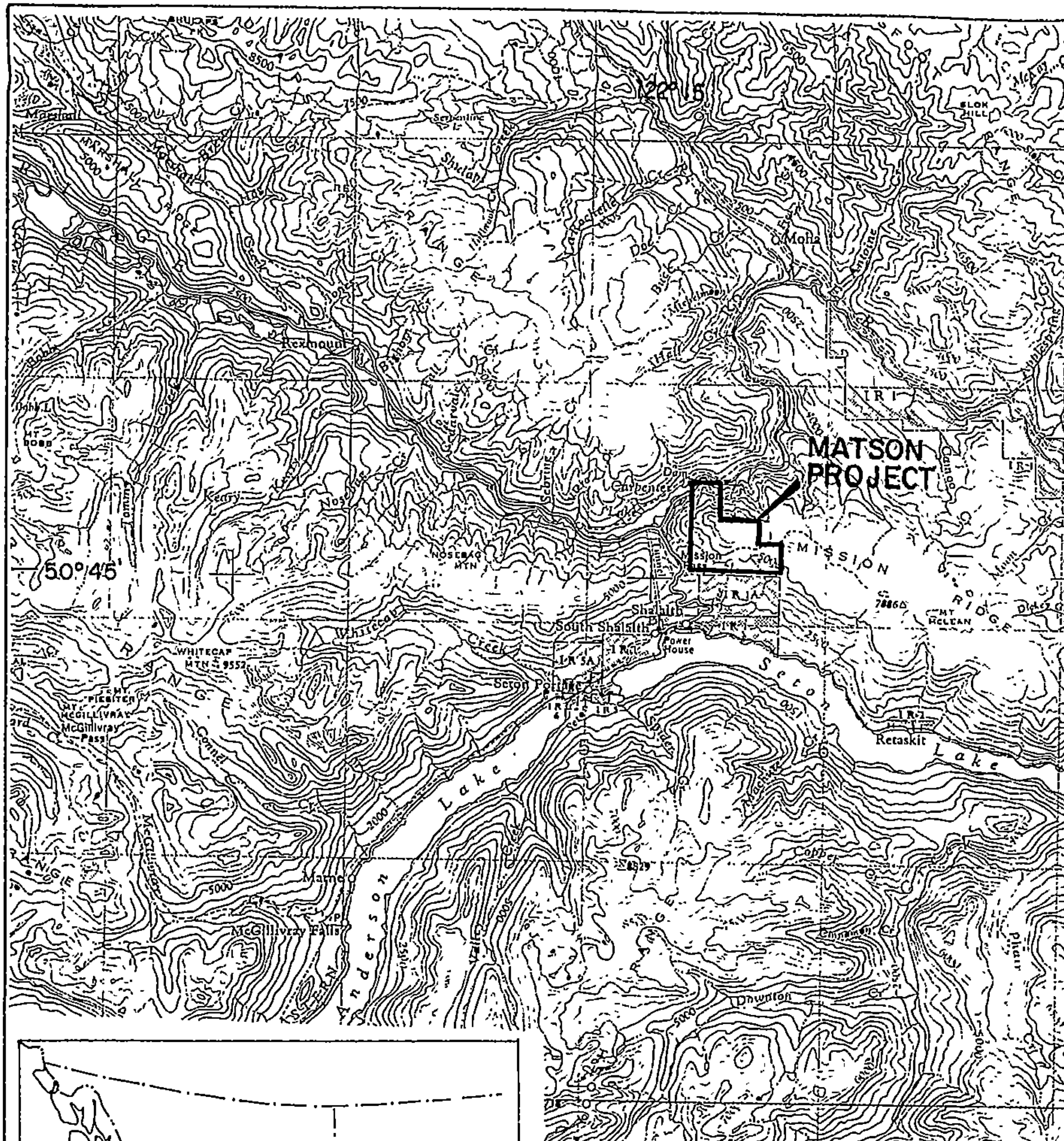
From June 1 to June 12, and from June 20 to June 24, 1987, Mountainside Management Limited conducted a first phase exploration program on the Matson property with the objective of defining targets with potential for precious metal deposition. The program consisted of grid establishment, geological mapping, and geochemical and geophysical surveys on the property, as well as some blasting and trenching. The exploration program was undertaken for Kelso Resources Ltd.

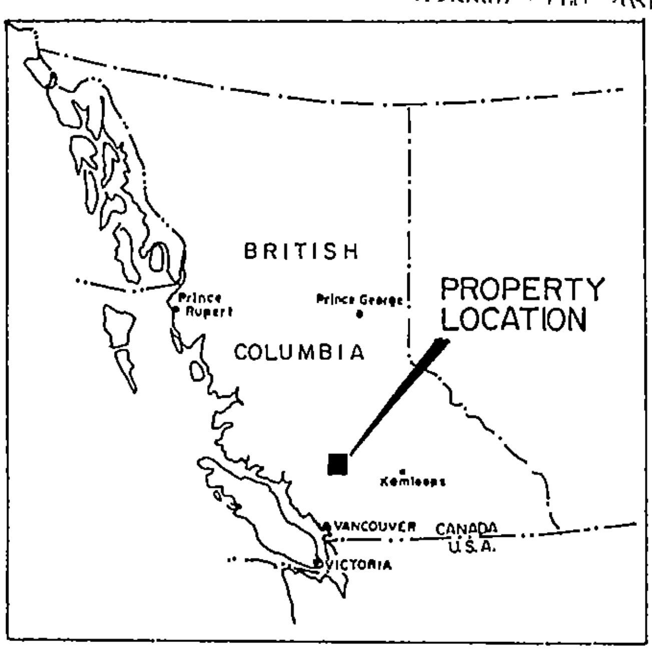
Location And Access

The Matson claim group is located approximately 45 km west of Lillooet approximately 20 km northeast of the community of Seton Portage (Fig. 1). Lillooet is 150 km north of Hope along the Fraser River, while Seton Portage is 130 km east of Pemberton between Anderson and Seton Lakes. The claim area is situated on the steep slopes of Mission Mountain, which separates the Bridge River and the Seton Lake valleys. The NTS map sheet which covers the area is 92J 16.

Access to the property is obtained by either of two ways. From Lillooet follow the Bridge River road approximately 40 km to BC Hydro's Carpenter Lake Dam, and proceed along the south shore of the lake until the road turns south and climbs to the summit of Mission Pass. At the summit a BC Hydro access road turns east; this road provides access to the property.

An alternate route provides quicker access from Vancouver. From Pemberton proceed east along Highway 99 for 80 km to the community of D'Arcy. From D'Arcy a secondary access road contours above the north shore of Anderson Lake for approximately





To accompany report by J. Fairley, B.A.Sc., P.Eng.

MATSON PROJECT

FOR: KELSO RESOURCES LTD.

BY: MOUNTAINSIDE MANAGEMENT LTD.

LOCATION MAP

LILLOOET M.D., B.C.

N.T.S. 92 J-16 E	DATE: JULY 1987
DRAWN BY: D.K.	FIGURE Nº. 1

40 km to Seton Portage. From Seton Portage continue east to Shalath and north to the summit of Mission Pass. At the summit the previously mentioned B.C. Hydro access road is reached. Proceeding east provides access to the property. Though generally well maintained by B.C. Hydro, many of the dirt roads are steep and require four-wheel drive vehicles.

The BC Railway line runs along the northern shore of Anderson and Seton Lakes through Shalath and Seton Portage and provides access to both Vancouver and the British Columbia interior.

Property Status

The Matson claim group consists of 14 located mineral claims in the Lillooet Mining Division of British Columbia. The claims are shown on the Department of Mines Mineral Claim map 92J 16E (Fig. 2). The claims are owned by Kelso Resources Ltd. A complete title search was not conducted for this report.

NAME	RECORD NO.	AREA (units)	EXPIRY dd/mm/yr	OWNER
MATSON 1	849 (7)	1	26/07/87	KELSO RES. LTD.
" 2	850 (7)	1	26/07/87	KELSO RES. LTD.
" 3	851 (7)	1	26/07/87	KELSO RES. LTD.
" 4	852 (7)	1	26/07/87	KELSO RES. LTD.
" 5	853 (7)	1	26/07/87	KELSO RES. LTD.
" 6	854 (7)	1	26/07/87	KELSO RES. LTD.
" 7	3757 (7)	1	*09/07/88	KELSO RES. LTD.
" 8	3758 (7)	1	*09/07/88	KELSO RES. LTD.
" 9	3759 (7)	1	*09/07/88	KELSO RES. LTD.
" 10	3760 (7)	1	*09/07/88	KELSO RES. LTD.
" 11	3761 (7)	1	*09/07/88	KELSO RES. LTD.
" 12	3762 (7)	1	*09/07/88	KELSO RES. LTD.

"	14	3683 (4)	14	24/04/88	KELSO RES. LTD.
"	15	3684 (4)	12	24/04/88	KELSO RES. LTD.

*The Matson 7 through 12 claims were restaked on July 8, 1987.

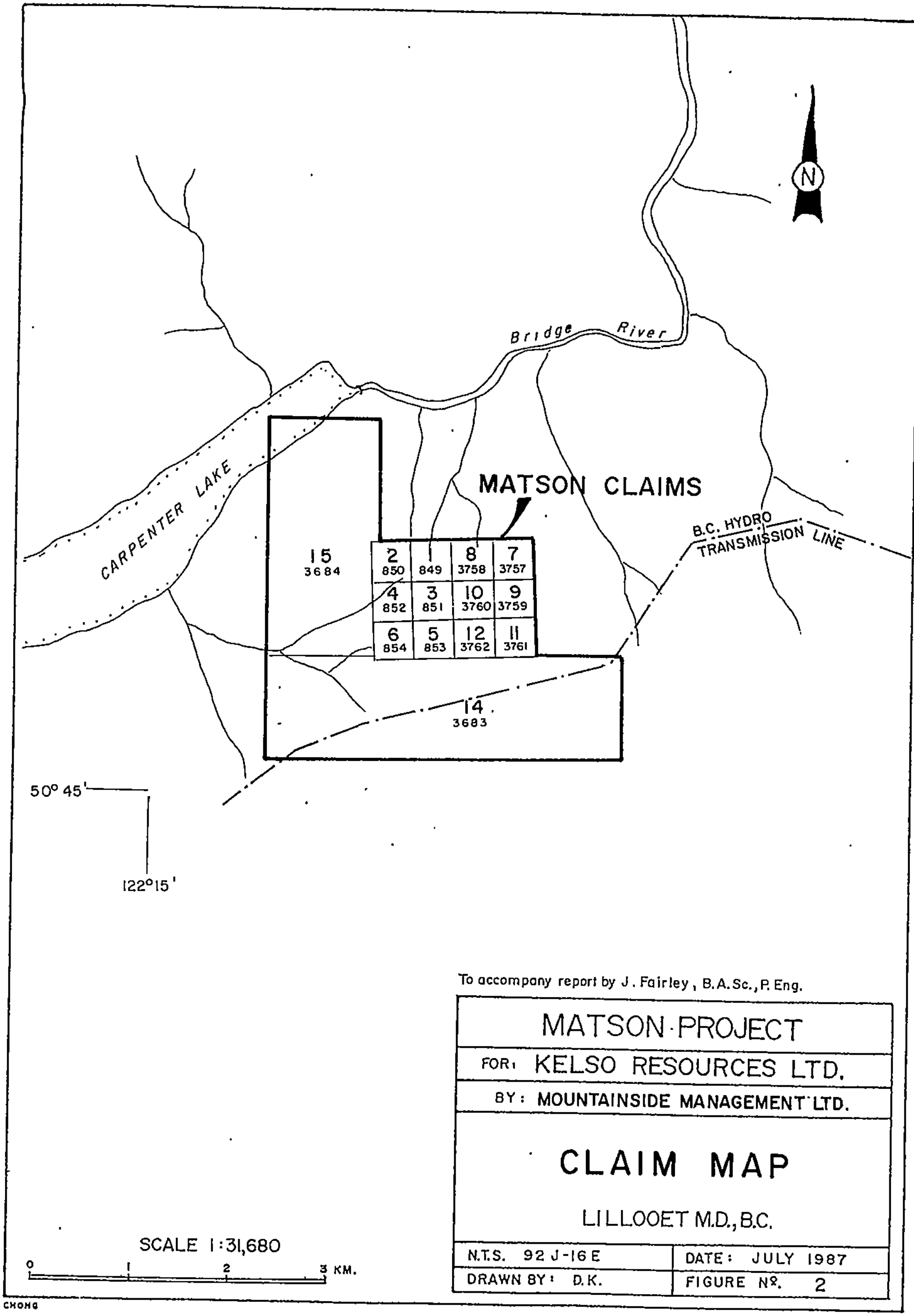
History

The Bridge River Area is one of British Columbia's oldest gold camps. Production from numerous hard rock and placer operations dates back to before the turn of the century. Placer mining commenced in 1858 when placer gold was recovered from the bed of the Bridge River near its confluence with the Fraser River. The placer gold deposition was followed for approximately 16 km upstream from the Fraser. In 1859 a second discovery was made on Gun Creek near its confluence with the Bridge River, close to the future site of the Minto Mine. Extensive placer operations were also initiated on Tyaughton and Hurley Rivers and on Cadwallader Creek.

It wasn't until the late 1800's, however, that an interest emerged in identifying the placer source. This lead to the discovery of the Bralorne and the Pioneer deposits near the turn of the century. The Bralorne Mine, the largest gold producer in the region, has yield over 2.8 million ounces of gold and over .7 million ounces of silver since 1900. The ore is reported to grade from 0.25 to 0.30 oz/ton gold.

The Pioneer Mine, south of the Bralorne Mine in the same greenstone belt, has produced over 1.3 million ounces of gold and .25 million ounces of silver since 1908.

Numerous smaller operations were scattered throughout the region. One of the larger of these operations was the Minto Mine, also known as the Congress Mine, located on the northern shore of Carpenter Lake near Bridge River. Production between



Bridge River
CARPENTER LAKE
MATSON CLAIMS
B.C. HYDRO TRANSMISSION LINE
N
15
3684
2
850
1
849
8
3758
7
3757
4
852
3
851
10
3760
9
3759
6
854
5
853
12
3762
11
3761
14
3683
50° 45'
122°15'
SCALE 1:31,680
0
1
2
3 KM.
CHONG
To accompany report by J. Fairley, B.A.Sc., P. Eng.
MATSON·PROJECT
FOR: KELSO RESOURCES LTD.
BY: MOUNTAINSIDE MANAGEMENT LTD.
CLAIM MAP
LILLOOET M.D., B.C.
N.T.S. 92 J-16 E
DATE: JULY 1987
DRAWN BY: D.K.
FIGURE Nº. 2

the years 1934 and 1940 totalled over 17,000 ounces of gold, 50,000 ounces of silver, and appreciable amounts of copper and lead. The deposit occurs in a fault fissure with mineralization consisting of stibnite, arsenopyrite, pyrite, pyrrhotite, sphalerite, galena and chalcopyrite. The showings on the Matson claims appear to be very similar to the Minto Deposit.

Other operations in the Bridge River camp include the Wayside Mine on the Bridge River a few miles upstream from the mouth of Gun Creek, the Pilot Mine situated near the center of the west shore of Gun Lake, and the Goldside Mine in the upper Taylor Creek Basin.

The showings on the present Matson group of claims were first discovered in the 1930's. At that time an adit and several pits were developed between the 5,100 and 5,800 foot elevations. A second phase of exploration was conducted by Benn Explorations Ltd. in 1966-67 on the claims, then known as the King Group. Benn Explorations isolated an anomalous area 500 x 300 m directly above and adjacent to the old workings by use of soil geochemistry. A short VLF-EM follow up program was conducted in 1977. The claims were subsequently dropped by Benn Explorations. The claims were restaked in 1979 and 1983 as the Matson Group.

In 1984 Odessa Explorations Inc. conducted an exploration program over the exposed mineralized zones. Encouraging magnetometer and soil geochemistry results were obtained. Odessa completed a second phase of sampling on the showing in July of 1985.

Physiography

Mission Mountain lies directly west of Mission Ridge in the Chilcotin Ranges on the eastern edge of the Coast Mountains. Elevations on the Matson Claim group range from 750 m (2,500 ft) to almost 2,000 m (6,500 ft.) above sea level. The majority of the property is heavily forested and steep. The northern extent of the claim group is precipitous, with cliffs of over 1,200 m (4,000 ft). The western portion of the property is generally densely forested and steep or precipitous in areas. The southern portion is also steep but is generally less formidable than the northern and western areas.

Outcrop exposure is abundant near the summit of Mission Mountain, but less abundant at lower elevations and virtually non-existent in many of the densely wooded areas. The best outcrop exposure at lower elevations is seen in the road cuts.

There are several deep cut valleys which appear to represent geological features. Very little water exists on the property. A small stream flowing down the south face of Mission Mountain provides the only water on the property and this would be dry at any time other than peak run off periods.

Because of the elevation and location of Mission Mountain, the climate varies dramatically. Snow remains on many of the north facing slopes year round and snow falls are not uncommon during the summer months. Conversely, the river and lake valleys of the area are the driest and warmest semi-arid regions in Canada.

PART B SURVEY SPECIFICATIONS

Grid Establishment

A single grid with a 1.9 km baseline was established over the Matson claim group (Fig. 3). A total of 29 km of grid was chained and flagged at 12.5 m spacings. Line intervals were 100 m except in areas of interest, where detail lines were established at 50 m intervals. Compasses, clinometers, and hip chains were used. Station locations were slope corrected.

Geological Mapping

Detailed geological mapping at 1:2500 scale was conducted on the grid. Reconnaissance traverses were conducted on the Matson 14 and 15 claims. Geological results are presented in Figs. 3-7, and Fig. 11.

Rock and Soil Geochemical Surveys

Soil samples were taken from the B horizon

A total of 118 rock samples and 904 soil samples was collected. Rock chip, grab, float and channel samples were collected from areas where signs of mineralization, alteration, and/or leaching were observed. The adit and veins uncovered by blasting and trenching were systematically sampled. Rock sample descriptions are found in the discussion of results and in Appendix C. Geochemical results are presented in Figs. 8a-h, and Fig. 11.

Ground VLF-EM Survey Method

The ground very low frequency electromagnetic (VLF-EM) survey was conducted using a Sabre Electronics Model 27 VLF Electromagnetometer. This instrument acts as a receiver only. It utilizes the primary electromagnetic fields generated by

United States Navy VLF marine communication stations. These stations operate at frequencies between 15 and 25 kHz, and have a vertical antenna current resulting in a horizontal primary magnetic field.

Secondary magnetic fields arise due to currents induced in conductors. The VLF-EM instrument measures the dip of the magnetic field resulting from the sum of the primary and secondary fields.

For maximum coupling, a transmitter station located in the direction of the geological strike and/or the strike of possible conductors is selected. At the Matson project area the transmitter located at Annapolis, Maryland was used.

Readings were taken at 12.5 m intervals along grid lines. The data was filtered as described by D.C. Fraser, Geophysics, Vol. 34, No. 6. This is essentially an averaging and differentiation filter technique applied to remove "DC" bias and attenuate long spatial wavelengths to increase resolution of local anomalies. VLF-EM conductors are indicated by positive values.

Ground VLF-EM survey results are presented in Fig. 9 and 11. A total of 29 line-km was surveyed.

Ground Magnetometer Survey Method

The magnetometer survey was conducted using an EDA OMNI IV Proton Precession magnetometer. This instrument measures the magnitude of the earth's total magnetic field to an accuracy of 0.5 gammas. Corrections for diurnal variation were made by an EDA PPM 337 proton precession base station magnetometer. The results are presented in Fig. 10 and 11.

Voluminous field (raw) data of geophysical surveys is at the Shangri-La Minerals Limited office, 200-675 W. Hastings St., Vancouver B.C. V6B 4Z1

PART C *GEOLOGY*

Regional

The geology of the Bridge River area consists of a very complex sequence of sedimentary, metasedimentary, intrusive and volcanic rocks located between the boundary of the Intermontane and the Coastal Crystalline Belts. The area is considered to be an anticlinorium with complicated folds on the southwest limb. In many areas the limb is pierced by intrusive bodies associated with the coastal batholith. The antiform is bounded on the southwest by the main mass of the Coast Crystalline Belt and on the north-west by the Yalakom Fault zone.

Sedimentary and volcanic rocks of the Triassic Bridge River Group are the most extensively exposed lithologies in the region. Along the southwestern flank of the antiform, the Bridge River Group is overlain by clastic and volcanic rocks of the Triassic Cadwallader Group. However, on the northeastern limb of the structure the Cadwallader is all but completely removed by the Yalakom Fault zone. Granodiorite and less common occurrences of diorite, gabbro and basalt are seen in the Bridge River area with the Bendor Pluton and the Rexmount Porphyry constituting two of the larger igneous bodies.

Lithology - Bridge River Group

The Bridge River Group, also known as the Fergusson Group, is the most prominent as well as the most important rock unit in the area, for it is the host rock of the mineralization on the Matson Claims. The group consists mainly of a thick sequence of thin-bedded chert, cherty argillite, and argillite intercalated with altered basaltic flows, peridotite, serpentinite and minor limestone. In many areas on the Matson claim group the argillites appear to have been altered by contact metamorphic *effects, which has produced hornfels facies. The process* involves recrystallization of the original sedimentary rock at high temperatures, but without shearing stresses. Dark altered argillite (hornfels), dark to light grey weathered chert and dark cherty argillite are the most abundant rock types. The chert commonly forms lensoid or nodular layers separated by thin films of argillite. Because of this characteristic, the rock is often referred to as ribbon-chert. The altered argillites (hornfels) are generally compact and massive, breaking with a splinting fracture into sharp angular pieces.

In many areas the sediments are so highly altered that the original lithology can not be clearly identified. The rock often resembles an andesite; the abundance of chert leads to the assumption that the rock is of sedimentary origin.

Pods or lens of light-grey weathered, recrystallized limestone are scattered throughout the Bridge River Group. Most are relatively thin (ie. less than 2 m) and discontinuous. One bed near BL 00/500 W, however, is approximately 25 m thick and traceable along strike for over 75 m. Although rare occurrences of skarn deposits in the Bridge River Group are documented, none were identified on the Matson claim group.

A basaltic flow striking northwest is exposed for over 1 km in the eastern portion of the property. The flow is generally more than 200 m wide. In many areas the flow exhibits pillow structures, indicating it was extruded in a marine environment. Although the flow appears to overlie the Rexmount unit, it is thought to be part of the older Bridge River Complex. The rock is a massive, medium to dark green chocolate brown weathered metabasalt. The principal mineralogy of the metabasalt consists of plagioclase, pyroxene and olivine. In areas the rock is broken into large, highly resistant boulder size blocks.

Along the western contact of the basalt, a lenticular body of serpentinite approximately 25 m wide outcrops for 150 m. Serpentinite float found 600 m to the south indicates that the serpentinite may be continuous along the full extent of the metabasalt contact with the Rexmount Porphyry. The serpentinite was probably formed by hydrothermal alteration of ultrabasic rocks in the area, such as peridotite. The serpentinite appears to be responsible for anomalous nickel and chromium values found in the soil survey.

In several areas an argillaceous quartzite is found in contact with the Rexmount Porphyry or the metabasalt. The quartzites are massive and black with a gossanous oxidized surface. They are generally found as small outcrops no more than 10 m across. However, near 50E/75S a large outcrop is found in contact with the trachyte along a well defined shear zone exposed for approximately 25 m. The Bridge River Group is considered to be of Triassic age.

Rexmount Porphyry

The Rexmount Porphyry is an intrusive body of granodiorite-quartz diorite, syenite, and their volcanic equivalents dacite and trachyte. Near the contact of the intrusive and the Bridge River Sediments, porphyritic trachyte is the dominant rock type. Well-formed phenocrysts of plagioclase in a light grey, feldspar-rich aphanitic groundmass characterize the unit. As the silica content increases in the rock at some distance from the contact, the rock grades to a dacite. A true granodiorite-quartz diorite is found in the northern and north eastern portion of the grid.

The granodiorite is medium to coarse grained with quartz and plagioclase forming the primary constituents of the rock. Minor components are hornblende, biotite and pyroxene.

Several aplite dykes associated with the Rexmount Porphyry cut the Bridge River Group on the property. The dykes are very fine grain felsic bodies generally greater than 25 m wide and often traceable for 100 m or more. Although not seen near the showings, it appears that these dykes may have provided a heat source for the mineralizing fluids. A Miocene age has been assigned to the Rexmount Porphyry.

Structure

The Matson Property lies on the northeast limb of a plunging anticline which is severed approximately 5 km to the northeast by the Yalakom Fault zone. The initial deformation of the sediments occurred during the Jurasside Revolution in late Jurassic time. Uplift and erosion followed until Tertiary time and the onset of the Laramide Orogeny. It was during the Laramide Orogeny that several of the plutonic bodies in the region, including the Rexmount Porphyry, were intruded.

The intrusion of the Rexmount Porphyry appears to have a very close genetic relationship with the mineralization on the property. The contact between the sediments and the intrusive runs northwest to southeast across the property. In most areas the contact is inferred due to lack of outcrop. However, from the road along Carpenter Lake the contact and interfingering dykes can be seen on the cliffs above. Several strata-cutting dykes were also identified on the portion of the property covered by grid. Because of the proximity of the exposed mineralization to the sediment/intrusive contact it appears that these dykes may have an important relationship to the sulfide mineralization.

Contact features associated with intrusive bodies are obvious throughout the property. The intrusive has a trachytic texture near the contact, while the sediments have been altered by contact metamorphic effects to the hornfels facies. The dykes are usually microcrystalline aplite.

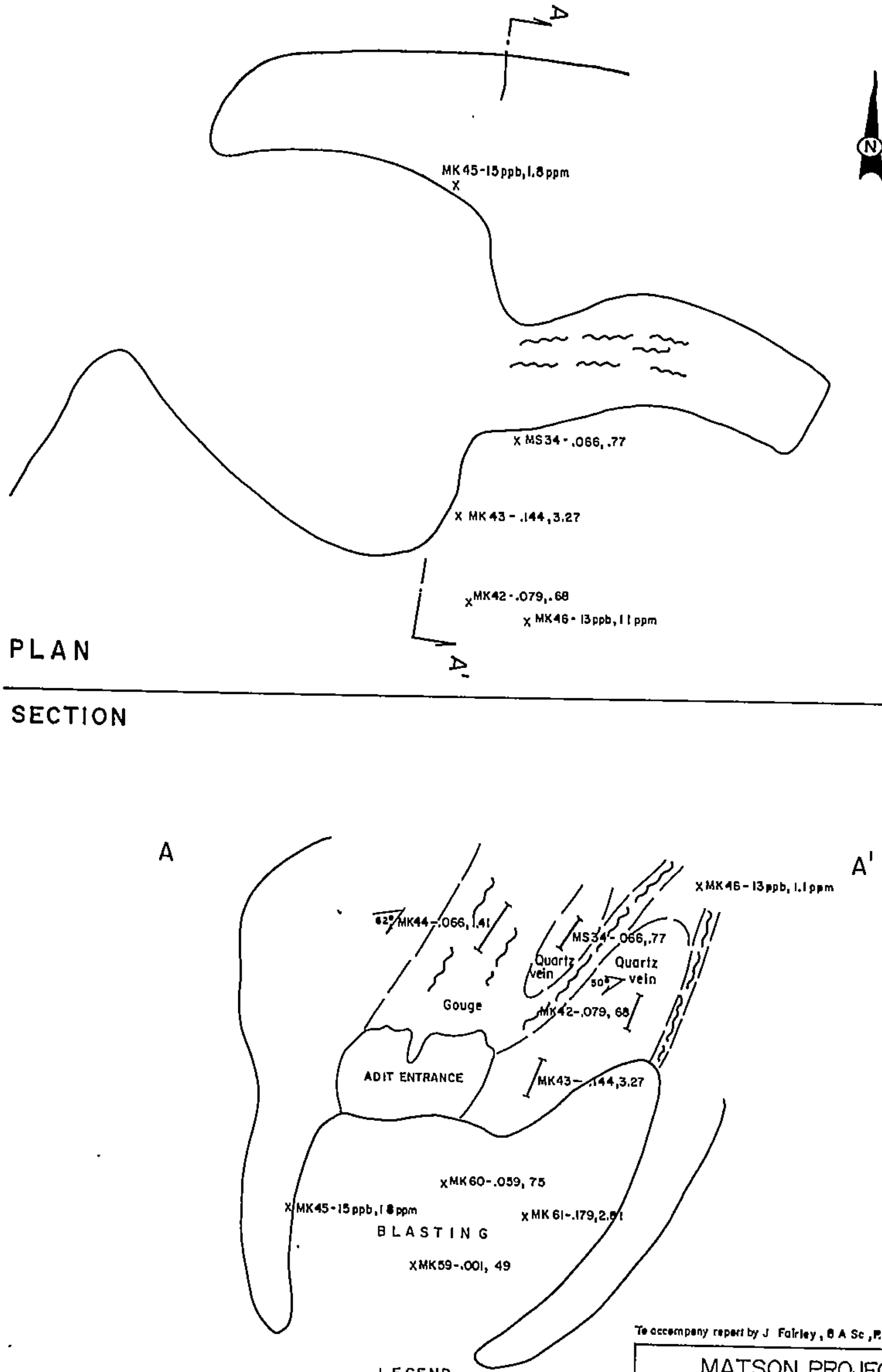
A major fault, striking 054 deg. and dipping steeply cuts the Bridge River Group approximately 100 m north of the adit. The fault is apparently normal, and the offset is unknown. The major shear zone which hosts the mineralization at the adit runs almost parallel to this fault, striking 051 deg., dipping 62 deg. NW. The attitudes of the other shear zones vary dramatically, with measured strikes ranging from 0 to 120 deg. Dips are generally very steep to the north west or vertical. Much of the exposed mineralization is found in quartz veins associated with these shear zones, thus making them important features with respect to the economics of the property. The shear zones (in particular those with mineralized quartz veins) often appear to be discontinuous and are difficult to trace on the surface for any substantial distances.

An extrusive flow of basalt, which has subsequently been altered to metabasalt/greenstone, has remnant pillow structures indicating it was deposited in a marine environment.

Alteration and Mineralization

Alteration and mineralization within the Matson project area is spatially associated with granodiorite and quartz diorite of the Rexmount Porphyry. The Bridge River Group, which forms the country rock in the region, has been recrystallized, metasomatized and silicified near the intrusion.

The mineralization on the Matson property consists mostly of arsenopyrite, galena, sphalerite, and marcasite with minor amounts of pyrite, chalcopyrite, pyrrhotite and magnetite. The geology and mineral assemblage of the showings seems to indicate that the deposit is a volcanic-associated vein and shear zone hydrothermal system. Deposits such as these appear to have a



LEGEND

MK01-.100,2.80	Sample No. - Au, Ag in oz/ton or otherwise indicated.
~~ ~~	Shear zone
MK01	Indicates channel sample
10	Strike / dip vein

SCALE 1:100

0 1 2 3 4 5 METRES

To accompany report by J. Fairley, B.A.Sc., P.Eng.

MATSON PROJECT

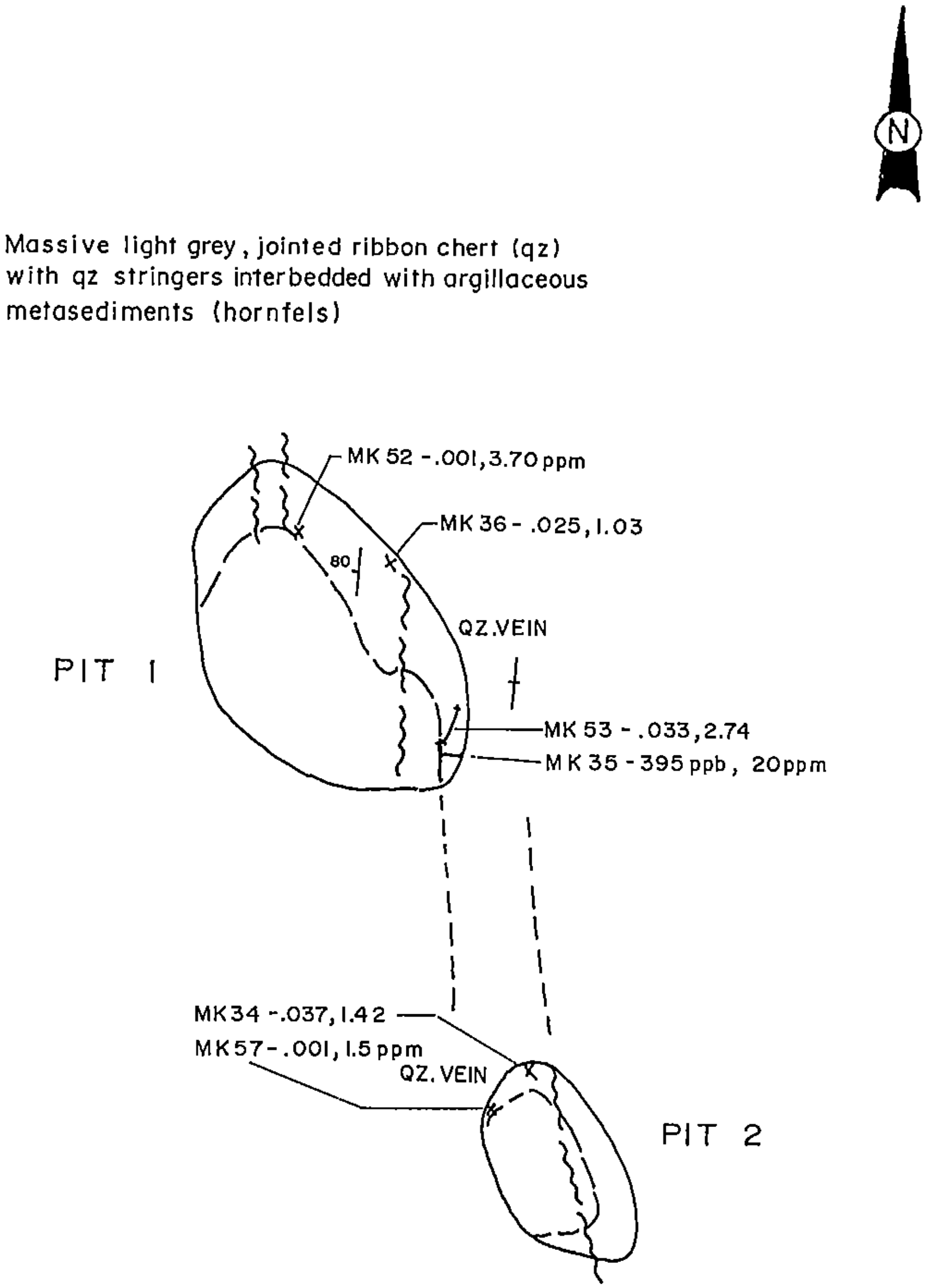
FOR: KELSO RESOURCES LTD.

BY: MOUNTAINSIDE MANAGEMENT LTD.

PLAN & SECTION
MATSON ADIT

LILLOOET M.D., B.C.

N.T.S. 92 J-16E	DATE: JULY 1987
DRAWN BY: D.K.	FIGURE No. 5



To accompany report by J. Fairley, B.A.Sc., P. Eng.

MATSON PROJECT

FOR: KELSO RESOURCES LTD.

BY: MOUNTAINSIDE MANAGEMENT LTD.

PLAN
PIT 1 & 2

LILLOOET M.D., B.C.

N.T.S. 92 J-16 E	DATE: JULY 1987
DRAWN BY: D.K.	FIGURE Nº. 6

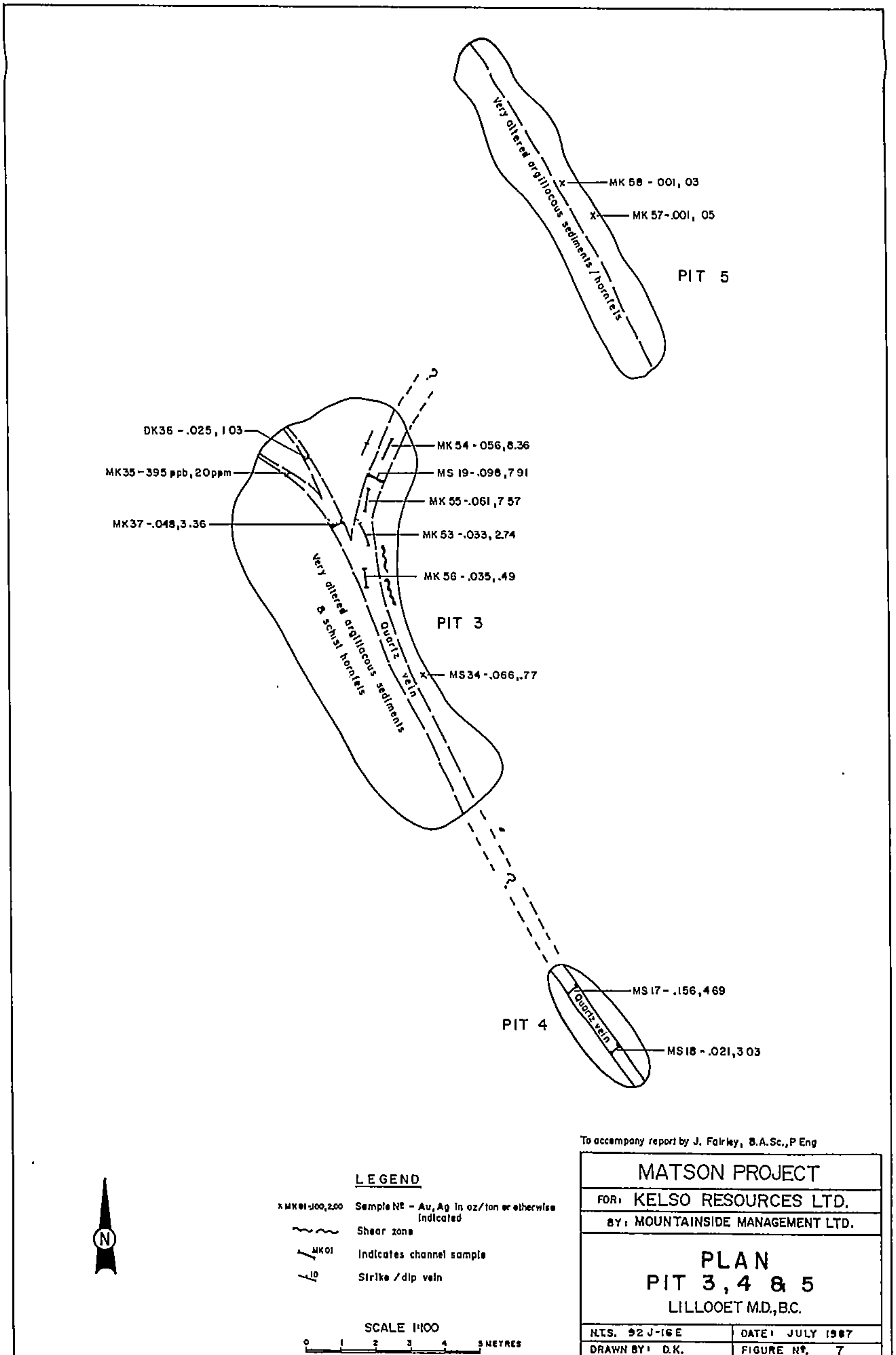
LEGEND

× MK01-.100, 2.00	Sample Nº. - Au, Ag in oz/ton or otherwise indicated.
~~ ~~	Shear zone
MK01	Indicates channel sample
10	Strike / dip vein

SCALE 1:100

0 1 2 3 4 5 METRES

CHONG


Very altered argillacous sediments / hornfels
MK 58 - .001, 03
MK 57-.001, 05
PIT 5
DK36 - .025, 1 03
MK35-395 ppb, 20ppm
MK37-.048,3.36
MK 54 - .056,8.36
MS 19-.098,7 91
MK 55-.061,7 57
MK 53 -.033, 2.74
MK 56 - .035, .49
Very altered argillacous sediments & schist hornfels
Quartz vein
PIT 3
MS34-.066,.77
MS 17- .156,469
Quartz vein
PIT 4
MS18-.021,3 03
LEGEND
x MK01-.100,2.00 Sample Nº - Au, Ag in oz/ton or otherwise indicated
Shear zone
MK01 Indicates channel sample
10 Strike / dip vein
SCALE 1:100
0 1 2 3 4 5 METRES
To accompany report by J. Fairley, B.A.Sc., P Eng
MATSON PROJECT
FOR: KELSO RESOURCES LTD.
BY: MOUNTAINSIDE MANAGEMENT LTD.
PLAN
PIT 3, 4 & 5
LILLOOET M.D., B.C.
N.T.S. 92 J-16E
DATE: JULY 1987
DRAWN BY: D.K.
FIGURE Nº. 7
CHONG

close genetic relationship with the associated intrusion. However it is not certain whether the intrusion and structures associated with the intrusion serve as a structurally and chemically favorable trap, or as a heat source responsible for the establishment of circulating hydrothermal generated fluids. The mineralization occurs primarily in veins along fractures and fault zones in highly sheared, schistose sediments, with a gangue of quartz and calcite.

Alteration in the mineralized zones is quite evident with cerrusite (lead carbonate), smithsonite (zinc carbonate) and anglesite (lead sulphate) all being common. Both cerrusite and anglesite are found as secondary minerals that generally form from galena in the zones of surface alteration. Smithsonite is found as a secondary mineral formed from the oxidation of sphalerite in similar deposits. Lime green arsenopyrite alteration is also abundant throughout the mineralized zones.

Pods or lenses of recrystallized limestone are abundant throughout the Bridge River Group. Although minor skarn occurrences in the Bridge River Group are documented none were identified on the Matson Property.

A band of serpentinite is exposed along the western contact of the metabasalt dyke/flow. Serpentinite is usually formed by alteration of ultrabasic rocks such as peridotite and is composed mostly of chrysotile and antigorite. Minor amounts of nickel and chromium in the serpentinite are thought to be responsible for anomalous values of those elements in the soils.

PART D DISCUSSION OF GEOPHYSICAL RESULTS

VLF-EM Survey

The VLF-EM Fraser filtered contoured data is presented on Figure 9.

The most obvious feature on this map is the strong high zone, starting in the west at 400 W/50 S and trending north-east to the baseline on line 400 E, then turning south-east up to 900 E/150 W. This feature is related to electric power lines used to supply the microwave transmission tower on the property.

In the immediate vicinity of the adit at 900 W/00, there are two parallel east-west trending anomalous areas. These anomalies are both centered on line 900 W. One is at station 30 N and the other at station 50 S. The anomaly to the north has maximum fraser filtered values between 15 deg. and 20 deg. and the one to the south between 20 deg. and 25 deg. Both anomalies have a strike length of at least 100 m. The two anomalies occur within a weaker anomalous area (greater than 5 deg.) which extends towards the west on the south side of the baseline between lines 600 W and 400 W near station 100 S. The anomalous zone has many values between 10 deg. and 15 deg. To the south of this anomaly on lines 500 W and 400 W at about 250 S there is another high with a maximum between 15 deg. and 20 deg.

In the southwestern section of the grid there are two anomalous areas which are roughly parallel. The northern most of the two is centered at about 500 S and trends from line 900 W to 600 W with maxima between 10 deg. and 15 deg.; it extends from 900 W to 700 W, with line 800 W having weaker values (between 0 deg. and 5 deg.).

On the northern portion of the grid, between lines 100 W and 200 W at station 100 N, there is a VLF peak running east-west with maximum values between 30 deg. and 35 deg. This peak is contained within a highly anomalous trend which strikes north-west up to 500 W/300 N. The north-west trend is roughly parallel to the contact between the Bridge River sediments to the west and the Rexmount Porphyry to the east. To the east of the peak the trend curves toward the east and extends up to 900 E/250 N. Within the eastward trending portion of this high there are a number of local peaks with two values greater than 20 deg. One is at 100 E/140 N and the other is at 700 E/200 N.

One other significant anomalous zone can be seen in the northern portion of the grid. It starts at 00/525 N and trends towards the east up to 900 E/500 N. Within this zone there are two peaks with values greater than to 20 deg. One is at 400 E/510 N and the other is at 600 E/485 N.

The VLF anomalies may represent mineralized zones or shearing in the rock. If the VLF trends observed in the immediate vicinity of the adit relate to mineralized zones, it is not surprising that the amplitude is relatively low. This is due to the presence of the non-conductive mineral sphalerite (zinc sulfide) seen in the adit. The conductive components of the mineralization would mostly be arsenopyrite (iron arsenic sulfide) and galena (lead sulfide). The east-west trending VLF anomalies could also reflect shearing in the rock, which crosscuts geological contacts.

Magnetometer Survey

The total field magnetic contoured data is presented in Figure 10. The background level for the grid area is between 56,350 and 56,450 gammas. Anomalous peaks in the vicinity of line 300 E and the base line cannot be trusted because of the presence of a power line.

In general the magnetic data trends to the north west, in the same general direction as the geological contacts.

There seems to be a recurrent relationship between some VLF and magnetic anomalies. For example, just to the north of the VLF high at 850 E/25 N (in the vicinity of the adit) there is a magnetic high flanking a VLF high. There is a similar situation in the southwest portion of the grid, where a magnetic high trends from 700 W/650 S to 1000 W/530 S. This magnetic trend consists of two distinct peaks which flank both VLF highs.

Another magnetic peak which flanks a VLF high can be seen at 300 W/150 N. The magnetic peak at 600 W/250 E does not flank a VLF high as clearly as the other peaks, but it is close (50 m) to the VLF trend which flanks the previously mentioned magnetic high.

There is one other magnetic high at 200 E/235 N which is flanked by a VLF high (Fig. 6, 7 and 8).

Magnetic peaks seen on lines 200 E and 300 E near the baseline are possibly related to localized enrichment of magnetite (iron oxide) and/or pyrrhotite (iron sulfide) in the metabasalt and serpentinite rock. It is difficult to be confident of this, however, because of the possible effect of the power line in this area.

The magnetic material which contributes to the anomaly in the vicinity of the adit, and possibly other magnetic peaks flanked by VLF highs, has not been positively identified. It is probably a local enrichment of magnetite. It is possible that the magnetic high is due to pyrrhotite, but this is thought unlikely since the high concentration necessary to produce an anomaly of this amplitude would be easily observed. It is also possible that the source is a combination of magnetite and pyrrhotite.

Assuming a vein type model for the source of these magnetic anomalies it appears that they are near vertically dipping formations. The two magnetic anomalies in the west of the grid, one just north of the baseline and the other at the southern tip, seem to have a depth within 25 m of the surface. The three other magnetic peaks (600 W/250 N, 300 W/150 N, and 100 E/135 N) seem to be within 10 m of the surface.

PART E DISCUSSION OF GEOCHEMICAL RESULTS

Rock Geochemistry

A total of 118 rock samples was analysed by 30 element ICP analysis at Acme Analytical Laboratories of Vancouver. Each sample was also analysed by atomic absorption for gold content. Of the 118, 27 samples with particularly high gold and silver values were reassayed by fire assay method to give a more accurate gold and silver content. As well, 10 samples were also assayed for platinum and palladium content from areas containing soils anomalous in nickel and chromium.

The best rock geochemical results were received from the three showings on the property and their extensions exposed by our own blasting and trenching program. Three samples assayed greater than .140 oz/ton gold (MK43 - .144 oz/ton Au; MS17 - .156 oz/ton Au; MK 61 - .179 oz/ton Au). As well, three samples assayed greater than 7.00 oz/t silver (MS19 - 7.91 oz/t Ag; MK54 - 8.36 oz/t Ag; MK55 - 7.57 oz/t Ag).

The best gold results received were from the adit area. The mineralization, massive in much of the vein structure, consists mostly of arsenopyrite, galena, sphalerite, pyrite and occasionally minor pyrrhotite. A mineralogical analysis of sample M-100 K from the adit vein system was done by Orex Labs of Vancouver. Chemical analysis of the lead indicated 0.085 oz/ton gold and 9 oz/ton silver. No gold or silver minerals were observed in polished section, however. Figure 5 shows all gold and silver assays from channel and rock chip samples from the adit area.

The best silver results received were from the vein system exposed by blasting and trenching near 750W/175N. Silver values from channel samples taken along the vein system ranged from 0.49 to 8.36 oz/ton Ag. The better results include values of 7.91, 7.57 and 4.69 oz/ton Ag. Good gold and silver results were also received from the vein system exposed near 650W/125N (Figures 6 and 7).

An area of anomalous nickel and chromium values was also isolated by the soil survey. Using the association of nickel and chromium with platinum, 10 rock chip samples of ultramafic and metabasaltic rocks were analyzed for both platinum and palladium in this area. Neither platinum nor palladium values of interest were observed.

Soil Geochemistry

A total of 904 soil samples was collected and analysed by ICP for a 30 element suite, and atomic absorption for gold by Acme Analytical Laboratories of Vancouver. The values for ten separate pathfinder and indicator elements were plotted and contoured in order to establish geochemical trends. Arsenic, cadmium, antimony, lead, zinc and copper are generally considered to be pathfinder elements for gold and silver mineralization in sulfide ore complexes such as those occurring on the Matson property.

A simple statistical analysis was performed on the geochemical data to determine anomalous zones with a degree of probability. The threshold value for an element was taken to be its mean value plus plus two standard deviations. Appendix E lists all anomalous pathfinder and indicator elements, their maximum and minimum analytical values, and their mean, median and standard deviations.

A zone approximately 400 x 600 m between lines 400 W and 1,000 W between stations 200 N and 200 S contains anomalous values for each of the pathfinder and indicator elements. This zone, which remains open ended to the west, has anomalous gold values ranging from 98 ppb to 765 ppb (threshold value Au = 87.2 ppb) with the greatest gold value - 765 ppb - being sampled at station 650 W/125 N, near remnants of past blasting and trenching. Anomalous silver values are also concentrated in the region. Values from 1.2 to 5.4 ppm and a single value of 28 ppm silver are found in the zone (threshold value Ag = 1.1 ppm).

Anomalous values for the pathfinder elements arsenic, cadmium, antimony, lead, zinc and copper are also found in the zone, indicating that the mineralization may be much more extensive than originally thought. Extremely high spot anomalies of arsenic, lead and zinc (20,697, 17,965 and 5,659 ppm respectively) occur within the zone. The arsenic source can be explained by the mineralization exposed by the trenching at station 650 W/125 N, however, the source of the lead and zinc values found at station 700 W/50 S remains unknown.

A second anomaly, smaller in magnitude and extent but which may indicate sulfide mineralization, occurs between lines 100 E and 200 E and stations 150 S and 175 N. Moderately high values in both indicator and pathfinder elements coupled with a magnetic high/low sequence makes this area a definite target. The fact that the anomalous values for each element are spread over several stations may be explained by the varying mobility of the elements within the soils.

Two areas, one in the southwestern and one in the northwestern portion of the grid, indicate anomalous zones of copper. Both zones correlate to identified magnetic and VLF-EM anomalies. Values from the northwest zone between lines 500 W and 750 W and stations 300 N and 550 N range from 194 to 870 ppm Cu (threshold value Cu = 191 ppm). Values from the southwest zone are not as impressive, but nonetheless indicate a zone of interest because of the correlation to the geophysical surveys.

A large volcanic flow and serpentinite body striking southeast near the center of the grid has produced very high chromite and nickel values. The zone is up to 300 m wide, extends for more than 1 km and is open to the southeast. From this zone, 24 nickel values and 23 chromium values were considered anomalous (threshold value Ni = 509, Cr = 334 ppm). Maximum values for nickel and chromium are 2,307 and 1,551 ppm respectively. The economic significance of these elements can also lie in their association with platinum. Rock assay results do not indicate that such a relationship exists in this case.

PART F TRENCHING PROGRAM

The most obvious showings on the property had been developed by an adit, and several trenches and pits. The present blasting and trenching program was used to help extend the strike length of the vein systems exposed by past programs. The most impressive results were received from the adit/portal area and the Pit No. 3 (Figures 5, 7, 8). Blasting on the face of the portal was used to give better exposure of the vein system near the adit, while blasting on the No. 3 Pit was used to increase the strike length of the main vein. We were able to extend this vein for approximately 5 m with an average width of .3 to .4 m. The vein, however, pinches to approximately .15 m near the surface. A second pit (Pit No. 5) was blasted 10 m north of Pit No. 3 in an attempt to locate the main vein along strike. The vein was not located.

Past reports have attempted to correlate the vein system exposed by Pits No. 1 and 2 with that exposed by Pits No 3 and 4. Due to the discontinuous nature of the exposed veins and the lack of geophysical evidence, correlation of the vein system over this distance (greater than 115 m) is not definitive. Blasting and trenching were also conducted on Pits No. 1 and 2 to give better exposure of the vein system.

PART G DISCUSSION OF RESULTS

Correlation of the geological, geophysical and geochemical results obtained indicate three main areas of interest on the Matson Property (Fig. 11). The most promising is a 600 x 400 m zone enclosing the old workings. This zone includes a VLF-EM conductor encompassing a magnetic high. Several values for indicator and pathfinder elements from this zone are considered anomalous.

A second conductive zone flanked by a magnetic high is situated in the extreme southwest corner of the grid area. Although anomalous gold and silver values were not observed in the soil samples, this second zone has similar VLF-EM and magnetic signatures to the zone noted above, suggesting a relationship may exist.

A third zone extends for approximately 700 m between 200 E and 500 W just north of the baseline, trending in a west/northwest direction. In this area three very conductive zones exist. Strong magnetic anomalies also exist over each of the VLF-EM anomalies. Anomalous gold and silver values were not observed in the soil samples, but slightly anomalous pathfinder elements (lead, zinc and arsenic) were found in the soils.

Anomalous copper values were found in two areas. The first appears to be associated with the magnetic and VLF-EM anomalies situated in the south western corner of the grid. The second occurs near the contact of the Bridge River Group and the Rexmount Porphyry between lines 500 W and 700 W in the northern portion of the grid.

Magnetic and VLF-EM anomalies occurred in many areas in the south central and south eastern portion of the survey area. However it is believed that these anomalies are due to the presence of BC Hydro transmission lines and the BC Telephone microwave tower located on Mission Mountain. Some transmission lines are buried, making accurate geophysical interpretations in this area difficult.

PART H CONCLUSIONS AND RECOMMENDATIONS

Encouraging geological, geochemical and geophysical results were obtained from the exploration program carried out on the Matson Property. The magnetic and VLF-EM survey outlined three distinct anomalous zones. The most promising area is located from 600 W to 1,000 W and 200 S to 200 N on the established grid and is open ended to the west. An IP survey is warranted over this zone to define the extent, depth and the sources of the anomalies. The IP survey should also be used to delineate targets in the other areas of interest.

The geology of the area is conducive to high-grade, low tonnage gold/silver mineralization hosted by shear zone controlled quartz veins. A second phase of exploration is recommended in order to further ascertain the sources of the geophysical and geochemical anomalies, to delineate additional targets, and to test for anomalous concentrations of sulfide mineralization at depth.

ESTIMATED COST OF PHASE II EXPLORATION PROGRAM

Grid Establishment	$ 7,000
Geological mapping and support	10,000
Soil geochemical survey	
say 300 samples @ $18/sample	5,400
(Incl. collection and analysis)	
Analysis of rock samples	
say 100 samples @ $15/sample	1,500
Induced Polarization survey	
(over selected areas) allow	25,000
Trenching and blasting	20,000
Engineering supervision and reports	8,500
Contingencies, allow approx. 15%	11,600
Estimated Total Cost for Phase II	$89,000

Contingent upon obtaining positive results from the proposed exploration program, a third phase consisting of road building, drill testing and additional trenching of specified targets may be necessary.

Signed at Vancouver, B.C.

____

John Fairley, P.Eng.
August 18, 1987

PROFESSIONAL
PROVINCE OF
JOHN F. FAIRLEY
BRITISH COLUMBIA
ENGINEER

REFERENCES

McCammon, J. W., 1938, The Geology and Mineral Deposits of The Bridge River District, British Columbia, B.A.Sc. Thesis University of B.C.

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AR 994, Assessment Work Report on The King Group of Mineral Claims, 1967

Woodsworth, G. I., 1977, GSC Open File Map 482, Pemberton (92J) Map Area

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COST BREAKDOWN FOR PHASE ONE OF THE MATSON PROPERTY

Geological mapping sampling and supervision	$11,550.00
Grid Emplacement:	
Baseline 1.9 kilometers @ $200.00/km	380.00
Crossline 29 kilometers @ $200.00/km	5,800.00
Geophysical surveys:	
VLF-EM 29 kilometers @ $200.00/km	5,800.00
Magnetometer 29 kilometers $200.00/km	5,800.00
Blasting and hand trenching (including blaster, geologist and supplies)	4,971.69
Geochemistry: (analysis and collection)	
904 soils @ $15.00	13,560.00
133 rocks @ $20.00	2,660.00
22 dual element fire assays	380.00
Computer plotting of geochem results	1,200.00
Mineralogical report	1,000.00
Camp costs, materials and vehicle	5,624.98
Analysis and report writing	6,000.00
Engineering, supervision and administration	3,500.00
Wordprocessing, printing, copying and binding	2,000.00
TOTAL COST FOR THIS PHASE	$70,226.67

CERTIFICATE

I, John Fairley, do hereby certify that;

I) I am a Consulting Engineer, residing at 3704 Mckechnie Ave., West Vancouver, B.C., V7W 2M8, for the firm of Mountainside Management Ltd. at 827 W. Pender Street, Vancouver, British Columbia.

II) I am a graduate of the University of British Columbia and hold a Bachelor of Applied Science in Geological Engineering.

III) I am a registered member, in good standing of the Association of Professional Engineers of British Columbia.

IV) Since graduation in 1963 I have been involved in numerous mineral exploration program, feasibility studies, and mining engineering throughout Canada, U.S.A., and Australia.

V) This report is based on a personal visit to the property, and an evaluation of information compiled by a Mountainside Management Ltd. crew on June 1 to June 12, 1987 and June 20 to June 24, 1987.

VI) I have no direct or indirect interest in the property described herein, or in any securities of Kelso Resources Limited, nor do I expect to receive any.

VII) This report may be utilized by Kelso Resources Limited for inclusion in a Prospectus or Statement of Material Facts.

Respectfully submitted at Vancouver, B.C.

PROFESSIONAL ENGINEER — PROVINCE OF BRITISH COLUMBIA — JOHN F. FAIRLEY

John Fairley, B.A.Sc., P.Eng.
August 18, 1987

CERTIFICATE

I, Darcy Krohman, do hereby certify that;

I) I am a Consulting Geologist to the firm of Mountainside Management Ltd. at 827 West Pender Street, Vancouver, British Columbia.

II) I graduated in 1985 from the University of British Columbia, Vancouver, B.C. with a B.Sc., in Geology.

III) I have been involved in mineral exploration since 1983.

IV) This report is based upon field work carried out by myself and a Mountainside Management crew under my supervision from June 1st to 12th and June 20th to 24th, 1987.

V) I have no direct or indirect interest in the property nor in Kelso Resources Ltd., nor do I expect to receive any.

VI) This report may be utilized by Kelso Resources Ltd. for inclusion in a Prospectus or Statement of Material Facts.

Respectfully submitted at Vancouver, B.C.

D. Krohman

Darcy Krohman, B.Sc.
August 19, 1987

MATSON PROPERTY ROCK SAMPLE DESCRIPTIONS

MK01	Very altered metasediments with massive mineralization consisting of arsenopyrite, galena, sphalerite, pyrite and minor chalcopyrite. Rock chip sample.
MK02	Granodiorite (Rexmount Porphyry). Rock chip sample.
MK03	Very mafic medium to fine grain metabasalt (greenstone). Rock chip sample.
MK04	Felsic trachyte. Fine grain off white ground mass w. prismatic Hornblende/Tremolite crystals. Rock chip sample.
MK05	Altered argillaceous siltstone (hornfel) with minor chert occurrence. Fine grain, very brittle and fractured. Original rock difficult to identify. Rock chip sample.
MK07	same of MK05
MK08	same of MK05
MK09	Fine to medium grain green siltstone with very thin calcite stringers. Very altered. Rock chip sample.
MK10	same as MK09
MK11	Very altered, easily fractured gossenous siltstone (hornfel). Original rock not identifiable. Rock chip sample.
MK12	Ribbon chert (quartz) with siliceous argillite. Very resistant grey microcrystalline quartz. Rock chip sample.
MK13	Massive, fine grain, dark grey, altered siltstone? (hornfel). Grab sample.
MK14	Massive microcrystalline grey chert with very minor pyrite mineralization in argillaceous siltstones. Iron stained. Grab sample.
MK15	same as MK14
MK16	Fine grain, argillaceous siltstones. Rock chip sample.
MK17	Dark green metabasalt (greenstone). Is generally very siliceous and is often calcareous with minor calcite stringers. Rock chip sample.

MK18 same as MK17.

MK19 same as MK17.

MK20 Very siliceous argillaceous siltstones grading to quartzites. Quartzites are black due to argillaceous material with a gossenous oxidized surface. Rock chip sample.

MK21 Serpentinite. Olivine, pyroxene rich with glassy sheen. Easily fractured along plane. Rock chip sample.

MK22 same as MK20

MK23 same as MK17

MK24 Argillaceous quartzite with quartz stringers. Black with gossenous weathered surface. Rock chip sample.

MK25 same as MK24

MK26 same as MK17

MK27 same as MK26

MK29 Massive microcrystalline white vein quartz. Gossenous on oxidized surface. Rock chip sample.

MK30 same as MK29

MK31 Light green, fine green altered siltstone (hornfel). Very siliceous in areas. Rock chip sample.

MK32 Siliceous foliated siltstone with abundant argillaceous material.

MK33 same as MK32

MK34 Vein quartz with abundant arsenopyrite galena, sphalerite. Anglesite, cerrusite alteration. Channel sample across .3m.

MK35 same as MK34

MK36 same as MK34

MK37 Grey argillaceous quartz with arsenopyrite, galena mineralization. Rock chip sample.

MK38	Very fine grain bleached intrusive from contact margin. Very siliceous and gossenous on weathered surface. Rock chip sample.
MK39	Very altered siltstone with black massive chert. Chloritized. Rock chip sample.
MK40	Very altered argillaceous sediments with interbedded massive black chert. Very fractured and gossenous. Rock chip sample.
MK42	Massive light grey vein quartz with abundant arsenopyrite, galena and pyrite mineralization. Channel sample across 1 m.
MK43	same as MK42
MK44	Gouge from shear zone. Very easily broken down to sand size grains. Gossenous in color with minor arsenopyrite and galena.
MK45	Very altered metasediment wall rock. Chloritized. Rock chip sample.
MK46	Metasediments with arsenopyrite, galena. Quartz stringers and silica replacement. Rock chip sample.
MK47	Massive, white, microcrystalline vein quartz. Vein 1 m wide. Channel sample across 1 m.
MK48	Aphanitic bleached siliceous aplite dyke. Rock chip sample.
MK49	Very altered vein quartz with abundant arsenopyrite. Grab sample.
MK50	Light grey colorless quartz with arsenopyrite mineralization. Gossenous on oxidized surface. Grab sample from blasting.
MK51	Massive light green and colorless quartz with minor pyrite mineralization gossenous. Grab sample from blasting.
MK52	Very altered gossenous schist. Minor arsenopyrite. Rock chip sample.
MK53	Very altered vein quartz with arsenopyrite channel sample across .5m.

MK54	Very altered medium grey vein quartz with abundant arsenopyrite and galena. Channel sample.
MK55	same as MK54
MK56	same as MK54
MK57	same as MK54
MK58	Very altered siltstone (Hornfel). Rock chip sample.
MK59	Massive microcrystalline medium grey vein quartz with quartz stringers. Abundant arsenopyrite, galena, sphalerite. Minor pyrite. Grab sample from blasting.
MK60	same as MK59
MK61	same as MK59
MS01	Metabasalt. Rock chip sample.
MS02	Aphanitic porphyritic trachyte. Plagioclase phenocrysts. Rock chip sample.
MS03	Metasediments (Hornfels). Very argillaceous. Rock chip sample.
MS05	Massive, dark green metabasalt. Rock chip sample.
MS06	same as MS02
MS07	same as MS05
MS08	Massive, white to colorless quartzite. Rock chip sample.
MS09	same as MS03
MS10	same as MS08
MS11	Phaneritic granodiorite with well formed quartz, plagioclase, hornblende crystals. Rock chip sample.
MS12	Massive, microcrystalline, white vein quartz. Rock chip sample.
MS13	same as MS12
MS14	Very siliceous phyllite. Chloritized. Rock chip sample.
MS15	same as MS03

MS16	Siliceous siltstone. Rock chip sample.
MS17	Vein quartz with arsenopyrite, galena, sphalerite mineralization. Channel sample across .1m.
MS18	same as MS17. Channel sample across .5m.
MS19	same as MS17. Channel sample across .1m.
MS20	Massive white quartzite. Rock chip sample.
MS21	Siliceous sandstone. Rock chip sample.
MS22	same as MS21
MS23	Siliceous aplite. Aphanitic and felsic. Rock chip sample.
MS24	Very fractured phyllite. Rock chip sample.
MS25	same as MS21
MS26	same as MS02
MS27	Massive, microcrystalline, black chert with sandstone. Rock chip sample.
MS28	Massive quartzite. Rock chip sample.
MS29	same as MS28
MS30	same as MS03
MS31	same as MS03
MS32	same as MS03
MS34	Vein quartz with arsenopyrite, galena, sphalerite mineralization. Rock chip sample.

MINERALOGRAPHIC REPORT

by C. L. Soux

For: Shangri La Minerals
Project: Matson
Sample: M-100K

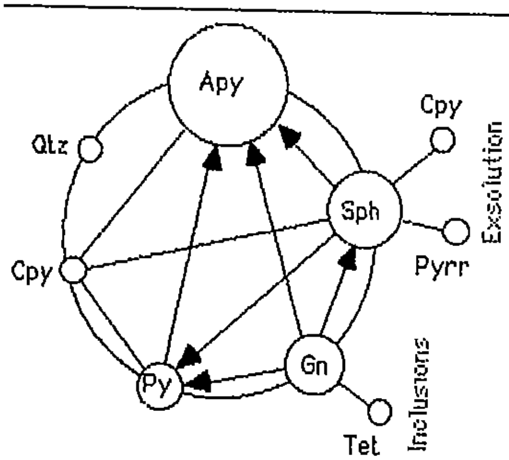
Location:
Collector:
Date Analyzed: July 31,1987

MACROSCOPIC DESCRIPTION:

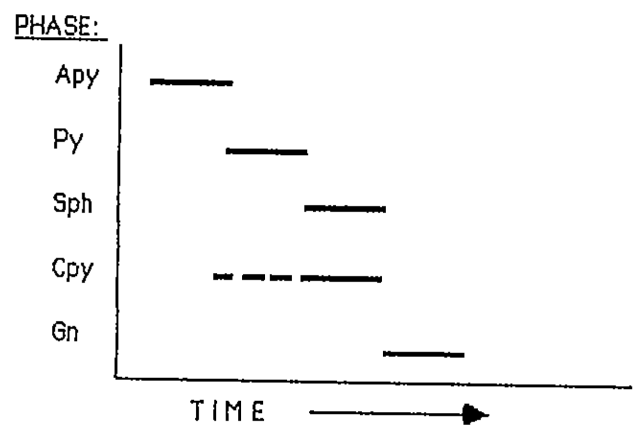
Pan concentrate of sample M-100 after crushing to 100% passing 5mm. A polished section of the concentrate product was prepared in order to carry out the microscopic analysis.

MICROSCOPIC ANALYSIS IN POLISHED SECTION

Abr.	Mineral	Chem. Formula	%	Description
Apy.	Arsenopyrite	Fe AS S	75	As free particles and in association with Gn. and Py.
Py.	Pyrite	Fe S2	5	Mainly as free particles
Gn.	Galena	Pb S	8	As free particles and in association with Apy., Sph. and Py.
Sph.	Sphalerite	Zn S	10	Contains inclusions of Cpy.
Cpy.	Chalcopyrite	Cu Fe S2	1	Mainly as inclusions in Sph.
Pyrr.	Pyrrhotite	Fe S	<<1	As exsolution blebs in Sph.
Qtz.	Quartz	Si 02	1	As free grains



Vandeveer Diagram



Tentative Paragenetic Sequence

TEXTURES AND DESCRIPTION:

Arsenopyrite is the most abundant mineral in the sample. It usually contains numerous narrow veinlets of galena and in a few cases chalcopyrite.

Sphalerite invariably contains exsolution bodies of chalcopyrite and in some cases pyrrhotite. Sphalerite replaces arsenopyrite and pyrite.

Galena appears to be the latest mineral in the paragenetic sequence. This mineral is almost completely devoid of inclusions. Only two grains were observed to contain inclusions of tetrahedrite. Galena replaces arsenopyrite, pyrite and sphalerite.

Chemical analyses of the head reported 0.085 oz/ton Au. and 9 oz/ton Ag. However, no gold or silver minerals were observed in polished section.

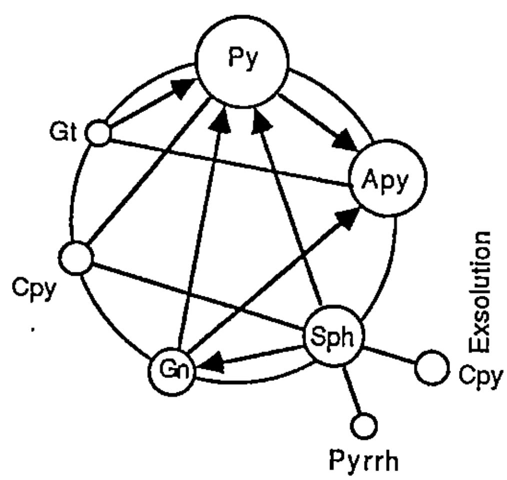
The silver values in the sample are probably tied up to tetrahedrite in part and argentiferous galena.

EXPLANATION ON THE USE OF THE
VANDEVEER DIAGRAM

A NEW DIAGRAMATIC SCHEME FOR PARAGENETIC RELATIONS OF THE ORE MINERALS

The ore minerals are arranged on the circumference of a circle and represented by smaller circles. Lines connect each pair of minerals which are observed to be in contact. An arrowhead points toward the mineral replaced where replacement textures are represented. The absence of arrows indicates simultaneous deposition. Minerals formed by exsolution are attached to the primary minerals by a line to the exsolution mineral point, which is outside the hypogene ore mineral circle. Supergene minerals are arranged on an outer arc and connected by lines to the hypogene minerals which are replaced. The density of the connecting lines in the diagram indicates semiquantitatively the relative replaceability of the host minerals.

After Forbes Robertson and Paul L. Vandeveer
Department of Geology,
Montana School of Mines,
October 16, 1951.



Example: (Above diagram)

Pyrite is replaced by sphalerite, galena and goethite. Arsenopyrite is replaced by galena and pyrite. Galena is replaced by sphalerite. Chalcopyrite is in contact with pyrite and sphalerite, but there is no evidence of replacement. Goethite and arsenopyrite are observed to be in contact. Sphalerite contains exsolution blebs of chalcopyrite and pyrrhotite:

MATSON GEOCHEMICAL STATISTICS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
COPPER	5.0	870.0	59.3	66.1	41.0
LEAD	2.0	5000.0	47.0	218.6	20.0
ZINC	27.0	5659.0	175.7	233.4	141.0
SILVER	0.1	28.0	0.2	1.0	0.1
NICKEL	10.0	2307.0	131.8	189.0	86.0
ARSENIC	2.0	5000.0	60.9	192.4	31.0
CADMIUM	1.0	100.0	1.6	3.9	1.0
ANTIMONY	2.0	28.0	2.4	1.7	2.0
CHROMIUM	17.0	1551.0	112.4	111.0	82.0
GOLD	1.0	765.0	7.4	39.9	1.0

TOTAL NUMBER OF SAMPLES = 904

SOME MAX VALUES HAVE BEEN REDUCED FOR STATISTICAL SIMPLICITY

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
COPPER	5.0	870.0	59.3	66.09	41.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-1000	-525	192
-1000	-625	205
-950	75	237
-900	-525	220
-800	-575	196
-700	475	518
-700	450	348
-700	425	579
-700	400	574
-700	375	287
-700	350	194
-700	225	246
-700	-50	534
-650	300	312
-650	125	366
-600	525	214
-600	500	649
-600	450	870
-600	425	195
-600	400	225
-500	350	227
-500	325	206
-500	275	213
-200	100	220
100	50	295
300	-275	197
500	-525	200
800	-425	320
800	-450	424

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
LEAD	2.0	5000.0	47.0	218.56	20.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-950	25	546
-850	-100	1038
-850	-125	627
-750	175	677
-750	150	637
-750	125	622
-750	100	907
-700	-50	17965
-650	125	3711

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
ZINC	27.0	5659.0	175.7	233.37	141.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-950	75	799
-950	25	674
-850	-100	867
-850	-125	725
-750	150	670
-750	125	772
-750	100	932
-750	75	709
-700	125	666
-700	100	725
-700	-50	5659
-650	125	3236
-600	125	809

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
SILVER	0.1	28.0	0.2	0.98	0.1

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-750	150	3
-700	-50	28
-650	125	4.9
-400	-75	5.4

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
NICKEL	10.0	2307.0	131.8	188.99	86.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
50	0	770
100	-100	542
200	125	1685
200	50	1483
200	-50	1270
200	-250	2307
300	100	623
300	0	1125
300	-25	697
300	-275	1450
300	-300	562
300	-625	535
400	25	517
400	-250	1309
400	-450	1025
400	-475	1044
400	-500	755
400	-575	669
400	-625	511
400	-650	939
500	-600	650
500	-650	587
600	-400	687
600	-575	1037
600	-600	1811
800	-450	822
900	0	1886

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
ARSENIC	2.0	5000.0	60.9	192.41	31.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-750	175	869
-750	150	739
-750	125	1166
-750	100	1397
-750	75	571
-700	125	631
-700	100	454
-700	-50	1079
-700	-200	597
-650	125	20607
200	-50	775

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
CADMIUM	1.0	100.0	1.6	3.88	1.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-950	75	11
-950	25	12
-900	-200	13
-750	100	15
-750	75	11
-700	100	12
-700	-50	48
-650	125	170
-400	25	10

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
ANTIMONY	2.0	28.0	2.4	1.70	2.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-950	87.5	6
-950	75	7
-950	-75	6
-850	-50	6
-800	25	7
-750	175	10
-700	225	9
-700	200	6
-700	-50	28
-700	-250	7
-650	125	10
-650	-75	6
-300	-50	12
50	0	7
100	50	7
200	-50	27
200	-250	11
300	-275	11
500	-525	25

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
CHROMIUM	17.0	1551.0	112.4	110.95	82.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-1000	-375	382
-900	-225	428
-900	-250	408
-800	-300	338
-700	-250	482
-600	-275	497
-400	375	379
-300	-50	527
50	0	468
100	-100	423
200	125	811
200	50	622
200	-50	709
200	-250	1551
300	0	611
300	-275	797
300	-325	374
400	25	336
400	-250	395
400	-450	744
400	-475	798
400	-500	530
400	-575	360
400	-650	565
500	-525	372
500	-600	461
500	-650	434
600	-400	428
600	-575	681
600	-600	915
800	-450	511
900	0	612

MATSON GEOCHEMICAL HIGHS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
GOLD	1.0	765.0	7.4	39.86	1.0

VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS
POSITIVE LINE NOS. SIGNIFY EAST, NEGATIVE LINE NOS. SIGNIFY WEST
POSITIVE STN. NOS. SIGNIFY NORTH, NEGATIVE STN. NOS. SIGNIFY SOUTH

LINE	STN	VALUE
-950	25	98
-750	50	225
-750	-75	265
-750	-125	215
-700	-175	133
-650	125	765
-600	25	395
-600	0	225
-500	-125	540
-400	-50	370

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P21 SOIL -80 MESH, P22-P24 ROCK AU* ANALYSIS BY AA FROM 20 GRAM SAMPLE.

DATE RECEIVED: JUNE 16 1987 DATE REPORT MAILED: June 22/87 ASSAYER. [signature] ..DEAN TOYE, CERTIFIED B.C. ASSAYER

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B1000W 125N	4	103	14	188	.1	110	31	1653	5.89	67	5	ND	2	28	2	2	2	110	.98	.101	18	108	2.26	86	.08	2	2.56	.02	.20	1	7
B1000W 100N	2	57	21	272	.1	74	22	1670	5.74	53	5	ND	2	21	3	2	2	116	.96	.146	16	81	2.08	66	.20	3	2.42	.02	.19	1	1
B1000W 75N	1	32	99	447	.2	133	27	1401	5.87	212	5	ND	2	23	6	2	2	133	.92	.103	12	167	3.34	59	.26	2	2.83	.03	.12	1	1
B1000W 50AN	1	46	211	404	.3	88	27	2613	6.83	144	5	ND	2	22	6	2	2	154	.84	.116	13	84	2.53	49	.20	2	2.76	.03	.11	1	20
B1000W 50BN	3	86	12	158	.4	90	31	1761	5.96	76	5	ND	2	45	2	2	2	112	2.28	.110	10	154	2.67	63	.03	2	2.83	.03	.25	1	9
B1000W 25N	1	65	70	203	.2	66	21	1660	5.13	49	5	ND	4	38	2	2	2	75	.38	.145	37	60	1.11	134	.02	2	2.16	.02	.16	1	7
B1000W 00N	4	54	271	638	.3	67	20	2888	4.03	79	5	ND	1	23	8	2	2	87	.51	.077	16	44	.73	148	.06	2	2.29	.02	.07	1	1
B1000W 50S	4	44	33	164	.1	95	22	1360	4.96	92	5	ND	2	16	1	3	3	109	.32	.038	12	89	1.23	116	.11	3	2.70	.02	.11	1	1
B1000W 75S	3	49	23	174	.1	66	22	2447	4.99	41	5	ND	1	25	2	2	2	101	.61	.076	14	52	.90	131	.08	2	2.25	.02	.11	1	1
B1000W 100S	3	86	67	288	.3	115	28	2756	5.75	94	5	ND	3	29	3	2	2	105	.37	.079	19	78	1.29	168	.09	2	2.76	.02	.16	1	12
B1000W 125S	3	109	66	190	.2	65	21	5177	4.83	32	5	ND	2	60	1	2	2	63	1.07	.115	33	54	.90	264	.04	2	2.07	.01	.26	1	7
B1000W 150S	3	123	39	183	.1	58	21	7547	3.27	27	5	ND	2	127	3	2	2	45	2.71	.183	17	38	.63	380	.03	8	1.45	.03	.18	1	1
B1000W 175S	2	89	25	208	.1	80	25	4142	3.94	29	5	ND	3	101	3	2	2	60	2.26	.141	33	58	.91	302	.03	8	1.81	.02	.27	1	22
B1000W 200S	2	70	15	175	.2	226	29	2619	4.38	27	5	ND	3	64	2	4	2	85	1.38	.129	15	246	2.19	195	.04	5	2.40	.02	.18	1	1
B1000W 225S	3	90	48	276	.3	138	28	3773	4.59	43	5	ND	2	86	3	2	2	80	1.61	.181	16	132	1.46	396	.04	6	2.30	.02	.18	1	1
B1000W 250S	5	107	53	262	.1	146	30	3814	5.26	56	5	ND	2	56	3	2	2	88	1.16	.183	20	122	1.44	267	.05	4	2.56	.02	.20	1	2
B1000W 275S	3	78	25	202	.2	123	24	4102	3.57	26	5	ND	1	83	3	2	2	62	1.82	.219	11	109	1.09	294	.04	4	1.89	.02	.11	1	1
B1000W 300S	2	42	55	276	.1	40	11	2266	2.13	10	5	ND	1	54	2	2	2	36	.97	.236	8	38	.45	212	.05	3	1.15	.02	.09	1	1
B1000W 325S	2	57	10	188	.2	96	12	1635	2.10	13	5	ND	1	192	2	2	2	37	14.81	.181	4	102	.80	265	.01	20	1.17	.07	.04	1	2
B1000W 350S	2	56	19	135	.2	78	19	1371	4.18	13	5	ND	2	54	1	2	2	75	1.54	.086	10	74	1.07	248	.02	5	2.09	.02	.17	2	1
B1000W 375S	3	78	8	184	.3	364	43	1544	7.96	23	5	ND	3	26	1	2	8	162	.54	.057	18	382	3.65	151	.04	4	4.39	.02	.11	1	2
B1000W 400S	2	113	2	120	.1	184	41	2195	8.53	2	5	ND	1	28	1	2	2	217	.76	.054	5	184	1.48	266	.01	10	3.22	.01	.27	1	4
B1000W 425S	1	77	4	110	.1	71	29	1732	7.08	7	5	ND	1	17	1	2	4	208	.56	.041	5	76	1.29	235	.07	6	2.85	.02	.14	1	1
B1000W 450S	3	124	7	133	.1	131	33	1819	7.14	10	5	ND	2	23	1	2	2	164	.73	.069	10	126	1.09	375	.02	6	2.59	.02	.20	1	1
B1000W 475S	1	144	3	127	.1	108	24	950	6.22	27	5	ND	2	14	1	3	4	162	.64	.040	8	99	1.06	487	.11	4	2.71	.02	.16	1	2
B1000W 500S	1	184	2	124	.2	114	41	1426	7.88	10	5	ND	1	14	1	2	2	219	1.09	.028	2	97	2.14	189	.24	11	3.29	.03	.22	1	1
B1000W 525S	1	192	5	99	.2	81	31	1622	5.84	11	5	ND	2	12	1	4	2	159	.60	.032	4	74	1.49	184	.15	6	2.63	.03	.14	1	1
B1000W 550S	10	110	8	409	.1	135	23	2563	4.78	35	5	ND	2	17	5	2	2	154	.71	.056	7	64	.71	289	.07	5	2.15	.02	.18	1	1
B1000W 575S	1	136	4	149	.2	92	34	1144	7.91	9	5	ND	2	15	1	2	2	241	.75	.047	5	101	2.02	157	.16	5	3.71	.02	.13	1	2
B1000W 600S	1	180	2	103	.1	133	39	2758	7.78	3	5	ND	2	16	1	2	2	190	1.00	.053	7	145	2.28	394	.04	8	3.30	.02	.29	1	8
B1000W 625S	1	205	7	112	.3	100	39	3269	7.70	18	5	ND	2	19	1	2	4	193	1.26	.072	10	95	2.15	483	.06	9	3.20	.02	.20	2	6
1000W 650S	1	157	2	109	.2	101	30	1570	6.72	4	5	ND	2	14	1	2	2	183	.72	.032	7	101	2.26	326	.15	7	3.99	.02	.09	1	1
B1000W 675S	1	148	4	112	.2	89	31	1481	7.68	15	5	ND	1	18	1	2	2	208	1.02	.038	5	98	1.77	271	.09	7	3.43	.02	.10	1	1
B1000W 700S	1	100	6	130	.1	99	30	1469	5.98	16	5	ND	2	24	1	2	2	181	.83	.117	7	104	1.70	138	.20	5	3.46	.02	.13	1	2
B950W 137.5N	2	100	37	385	.5	90	27	2078	6.64	156	5	ND	4	35	5	3	2	107	1.10	.152	27	71	1.97	100	.09	5	2.63	.02	.27	1	4
B950W 125N	1	93	24	314	.2	82	26	2347	6.55	107	5	ND	3	29	4	2	2	115	.90	.167	25	69	2.06	102	.13	4	2.62	.02	.29	1	1
STD C/AU-S	21	61	39	137	6.9	71	29	1043	3.92	39	18	7	35	49	18	15	20	66	.50	.102	37	59	.87	186	.09	38	1.68	.07	.14	14	48

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B950W 87.5N	11	87	102	426	.7	102	25	1481	6.04	160	5	ND	6	26	3	6	2	122	.41	.050	26	77	1.21	180	.02	4	2.66	.02	.12	1	3
B950W 75N	13	237	225	799	1.2	157	46	4345	9.54	310	5	ND	5	38	11	7	3	156	.57	.069	32	96	2.08	120	.04	7	3.12	.02	.11	1	46
B950W 25N	3	130	546	674	1.6	117	46	4296	9.60	367	5	ND	3	35	12	2	2	197	1.22	.140	19	65	3.30	42	.11	10	3.23	.02	.11	1	98
B950W 00N	2	53	62	192	.2	83	31	1639	8.29	89	5	ND	3	21	2	2	2	182	.97	.187	14	84	2.64	61	.29	7	3.00	.03	.19	1	5
B950W 25S	3	41	63	353	.4	70	18	1003	4.25	64	5	ND	3	20	4	2	3	78	.31	.152	16	65	.84	161	.04	4	2.07	.02	.11	1	1
B950W 50S	2	66	15	263	.2	123	22	855	5.01	40	5	ND	2	18	5	2	2	125	.46	.065	9	101	1.33	126	.15	5	2.80	.03	.08	1	2
B950W 75S	9	128	36	201	.9	126	41	3902	8.39	145	5	ND	3	28	2	6	2	119	.51	.080	27	74	1.39	164	.04	5	2.59	.01	.22	1	26
B950W 100S	5	129	35	236	.4	90	35	4995	6.97	104	5	ND	3	55	3	3	2	107	1.24	.118	25	52	1.03	213	.04	8	2.36	.01	.22	1	2
STD C/AU-S	20	58	38	132	7.0	69	29	1017	3.91	40	15	7	36	48	17	16	22	64	.46	.102	35	56	.87	170	.08	36	1.66	.07	.13	14	54
B950W 125S	5	117	55	242	.1	105	31	5700	6.02	57	5	ND	3	53	3	2	2	98	1.03	.131	21	64	1.09	249	.05	7	2.38	.02	.17	1	2
B950W 150S	5	95	56	276	.2	330	44	3720	6.13	106	5	ND	3	38	3	3	2	110	.79	.134	17	317	2.91	198	.04	7	3.18	.01	.13	1	1
B950W 175S	3	98	20	201	.1	236	40	3383	5.30	49	5	ND	3	56	2	2	2	92	1.30	.125	16	210	2.13	267	.04	7	2.63	.01	.12	1	1
B950W 200S	3	88	23	235	.1	265	39	2731	5.86	48	5	ND	3	57	2	2	4	96	.99	.145	18	248	2.38	266	.05	9	2.87	.01	.17	1	2
B900W 00S	5	114	181	412	.4	123	47	4188	9.48	307	5	ND	3	38	4	2	2	147	1.06	.078	20	63	2.08	105	.11	6	3.22	.01	.11	1	58
B900W 25S	2	51	19	158	.2	286	44	1075	7.80	124	5	ND	3	19	1	2	2	112	.54	.051	11	83	3.94	94	.14	6	3.53	.01	.08	1	2
B900W 50S	3	30	35	318	.1	84	20	2063	4.19	33	5	ND	2	26	5	2	3	82	.46	.104	10	68	.81	142	.11	5	1.93	.02	.08	1	3
B900W 75S	7	85	49	393	.7	172	28	1459	5.30	102	5	ND	4	42	6	2	2	87	.47	.078	20	112	1.43	211	.08	5	2.28	.02	.21	1	11
B900W 100S	9	132	128	440	1.1	205	30	1857	5.25	90	5	ND	4	53	5	3	2	75	.65	.090	23	102	1.20	212	.03	5	2.08	.02	.21	1	9
B900W 125S	8	78	63	334	.2	160	31	3667	4.25	76	5	ND	2	74	5	2	2	58	1.36	.174	13	93	1.06	345	.03	8	1.68	.01	.17	1	20
B900W 150S	4	90	76	281	.4	86	22	5167	4.28	51	5	ND	3	47	3	2	2	63	.86	.091	19	47	.75	281	.07	5	2.00	.02	.15	1	1
B900W 200S	4	113	271	581	.5	104	26	4538	3.09	77	5	ND	2	98	13	2	2	44	2.61	.209	12	54	.78	277	.03	13	1.35	.02	.16	1	2
B900W 225S	4	83	23	207	.3	442	40	1896	6.69	89	5	ND	3	28	1	2	2	120	.58	.081	18	428	3.35	134	.05	6	3.63	.02	.10	1	1
B900W 250S	2	89	20	222	.2	379	45	2533	6.11	46	5	ND	3	56	2	2	2	112	1.00	.127	17	408	3.66	227	.10	8	3.33	.01	.14	1	2
B900W 275S	3	83	26	239	.2	182	31	3085	4.62	34	5	ND	3	57	3	2	2	83	1.05	.134	16	174	1.68	303	.08	8	2.48	.02	.15	1	6
B900W 300S	3	76	39	291	.3	143	30	3546	4.30	49	5	ND	2	77	4	2	2	70	1.53	.268	12	149	1.50	366	.04	9	2.13	.01	.17	1	4
B900W 325S	7	77	15	121	.4	282	41	1649	7.37	40	5	ND	3	41	1	2	3	129	.55	.102	16	329	2.59	112	.04	6	3.34	.02	.06	1	2
B900W 350S	1	29	9	36	.3	53	7	529	1.57	10	11	ND	1	286	1	2	2	27	5.32	.084	4	60	.70	191	.02	26	.84	.05	.04	2	1
B900W 375S	2	33	10	183	.1	150	24	1064	4.66	30	5	ND	2	28	1	2	2	105	.38	.108	10	158	1.42	150	.08	5	2.34	.02	.09	1	1
B900W 400S	2	50	9	169	.1	260	29	870	6.28	25	5	ND	3	22	1	2	2	142	.53	.081	10	296	2.87	146	.17	7	3.08	.02	.09	1	1
B900W 425S	3	58	13	115	.1	73	19	1085	3.80	21	5	ND	2	81	2	2	2	69	1.02	.036	11	62	.81	233	.06	8	1.76	.02	.11	1	1
B900W 450S	4	30	8	64	.1	43	22	1251	7.17	17	5	ND	3	91	1	2	2	127	1.31	.078	10	48	.54	139	.05	9	2.65	.02	.09	1	1
B900W 475S	1	46	12	135	.3	92	24	2616	4.87	17	5	ND	2	32	1	2	2	114	.93	.135	9	72	.90	586	.06	10	2.15	.02	.17	1	2
B900W 500S	1	153	3	120	.1	59	30	873	7.96	10	5	ND	2	13	1	2	2	253	.61	.051	2	57	1.73	106	.11	8	3.30	.03	.06	2	1
B900W 525S	1	220	3	167	.1	60	40	1124	11.17	9	5	ND	2	16	1	2	2	327	1.21	.042	2	51	2.47	149	.18	7	4.25	.02	.06	1	1
B900W 550S	1	129	2	126	.1	251	42	1392	7.72	13	5	ND	2	10	1	2	2	193	.44	.033	4	176	3.63	181	.07	10	3.67	.02	.16	1	1
B900W 575S	1	109	3	122	.1	104	30	1304	6.69	12	5	ND	2	12	1	2	2	195	.62	.036	3	86	1.84	176	.13	7	3.11	.03	.12	1	2
B900W 600S	1	188	8	142	.1	147	39	2824	7.57	18	5	ND	2	22	1	2	2	197	1.13	.071	7	129	2.52	250	.14	9	3.51	.02	.27	1	1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B900W 625S	2	142	13	138	.1	75	34	1711	8.09	18	5	ND	1	25	1	2	3	190	1.44	.045	4	71	3.10	167	.06	5	3.30	.01	.13	1	4
B900W 650S	3	133	10	90	.2	56	25	2640	6.15	9	5	ND	1	26	1	2	2	165	1.75	.047	4	61	1.11	369	.04	6	2.27	.02	.16	1	1
B900W 675S	4	98	11	145	.1	78	31	2334	6.87	13	5	ND	2	21	1	2	2	142	.96	.058	16	82	1.55	177	.18	8	3.20	.02	.26	1	2
B900W 700S	3	115	6	161	.1	66	31	2744	6.62	2	5	ND	1	35	1	2	2	131	1.65	.087	10	71	1.40	108	.22	6	2.85	.02	.21	1	1
B850W 50N	5	96	32	162	.1	115	26	927	7.87	81	4	ND	3	16	1	5	4	150	.61	.050	16	120	2.39	81	.19	2	3.84	.01	.10	1	5
B850W 25N	5	45	77	293	.3	88	20	726	5.30	106	5	ND	2	9	1	2	2	104	.24	.064	12	91	1.31	86	.16	2	2.78	.02	.08	1	7
B850W 00N	4	22	57	185	.1	52	17	712	4.30	59	5	ND	1	18	1	2	2	91	.41	.047	8	53	.83	76	.13	2	2.20	.02	.05	1	1
B850W 25S	4	80	30	189	.2	70	34	1697	8.10	41	5	ND	2	28	1	3	5	142	1.04	.110	8	64	2.38	87	.26	2	3.56	.01	.14	1	1
B850W 50S	13	117	42	365	.9	119	31	1295	6.50	71	6	ND	5	42	3	6	2	87	.65	.057	25	65	1.75	138	.07	2	2.62	.01	.18	1	2
B850W 75AS	4	46	59	240	.1	96	24	1883	4.99	45	6	ND	1	31	3	2	2	78	.68	.089	12	59	1.76	141	.09	3	2.44	.01	.14	1	1
B850W 75BS	6	56	128	397	.3	104	22	1652	5.74	49	5	ND	3	26	5	2	2	100	.51	.112	17	66	1.30	130	.09	2	2.46	.01	.18	1	8
B850W 100S	12	179	1038	867	1.6	127	31	3820	5.78	227	5	ND	4	33	9	5	2	69	.78	.156	33	74	1.20	142	.04	4	2.34	.01	.16	1	22
B850W 125S	8	166	627	725	1.0	100	27	4657	5.03	177	5	ND	5	40	7	3	2	52	.75	.193	38	53	.99	285	.03	2	2.19	.01	.19	1	6
B850W 150S	9	139	176	482	.5	97	35	4377	6.63	215	5	ND	3	48	5	3	3	77	1.46	.177	19	51	1.32	173	.02	6	2.13	.01	.20	1	4
B850W 175S	4	66	53	239	.3	51	16	3325	2.66	44	5	ND	1	68	3	2	2	46	1.53	.135	13	36	.52	218	.06	4	1.45	.02	.10	1	4
B850W 200S	7	82	70	219	.1	128	27	3506	5.17	79	5	ND	2	50	2	2	2	87	1.33	.092	17	103	1.40	252	.09	3	2.56	.01	.15	1	3
B800W 200N	5	65	132	372	.2	77	21	1296	6.36	167	5	ND	2	14	2	2	3	119	.58	.149	16	74	2.30	62	.09	3	2.59	.01	.17	1	1
B800W 175N	4	67	187	472	.2	75	26	3181	6.32	195	5	ND	3	14	4	2	4	107	.29	.077	17	63	1.22	114	.09	2	2.59	.02	.12	1	1
B800W 50N	3	114	29	158	.3	67	27	1897	8.35	70	5	ND	3	18	1	2	4	147	.53	.060	25	62	1.91	62	.05	2	3.47	.01	.10	1	1
B800W 25N	3	57	28	178	.1	55	33	1960	8.38	97	5	ND	2	15	1	7	5	218	.82	.072	7	57	2.46	73	.31	5	3.41	.02	.08	2	1
B800W 0 N	5	58	48	241	.2	71	30	2567	6.56	68	5	ND	2	23	3	2	3	125	.42	.111	11	68	1.39	127	.13	2	2.95	.02	.09	1	1
B800W 25S	5	78	37	172	.4	104	22	2069	6.01	70	5	ND	2	21	2	2	2	111	.61	.042	13	89	1.46	111	.15	2	2.75	.01	.17	1	2
B800W 50S	7	41	94	298	.1	76	19	1713	4.69	54	5	ND	2	25	3	2	2	89	.72	.074	10	64	1.13	124	.12	2	2.34	.02	.13	1	1
B800W 75S	5	28	71	234	.1	46	18	2068	4.19	48	5	ND	1	18	3	2	2	81	.32	.048	8	40	.75	117	.10	4	1.98	.02	.08	1	4
B800W 125S	9	80	106	308	.6	104	30	4620	6.39	84	5	ND	3	116	3	2	2	102	2.14	.160	34	72	1.68	274	.10	9	2.59	.02	.18	1	4
B800W 150S	7	81	140	349	.1	118	32	3479	7.29	142	5	ND	4	37	3	2	2	119	.65	.133	36	97	1.85	152	.07	2	2.94	.01	.19	1	1
B800W 175S	6	52	118	307	.2	59	20	4078	3.52	49	5	ND	1	56	5	2	2	58	1.39	.128	12	43	.71	193	.05	4	1.53	.01	.15	2	2
B800W 200S	8	82	48	288	.2	122	31	3173	5.98	51	5	ND	2	33	2	2	2	85	.62	.116	18	96	1.53	210	.05	3	2.87	.01	.19	1	19
B800W 225S	6	65	32	236	.1	207	29	2191	5.59	46	5	ND	3	34	2	2	2	88	.68	.122	16	201	2.47	168	.04	3	3.08	.01	.14	1	1
B800W 250S	7	59	70	241	.2	124	25	2159	5.25	61	5	ND	2	31	2	2	2	91	.69	.101	16	113	1.40	154	.07	4	2.65	.02	.13	1	1
B800W 275S	8	83	109	300	.3	136	31	2592	6.51	81	5	ND	2	50	3	2	2	98	1.23	.239	16	118	1.82	152	.05	7	3.14	.01	.16	1	1
B800W 300S	8	111	23	159	.2	359	40	1123	7.56	88	5	ND	3	26	1	4	4	136	.40	.035	31	338	2.92	133	.04	3	3.77	.01	.06	1	1
B800W 325S	11	40	36	277	.1	125	23	712	5.69	78	5	ND	3	34	1	2	3	90	.58	.054	18	119	1.45	126	.03	2	2.83	.01	.11	1	1
B800W 350S	8	63	27	190	.1	122	24	1069	5.72	76	5	ND	2	46	1	3	2	107	.84	.057	14	124	1.89	126	.07	4	2.79	.01	.19	1	4
B800W 375S	6	56	17	135	.1	110	22	962	5.09	40	5	ND	2	23	1	2	2	109	.41	.063	9	106	1.35	108	.13	8	2.66	.02	.08	1	1
B800W 400S	6	28	11	127	.2	86	17	844	4.08	22	5	ND	1	25	1	2	2	84	.63	.065	10	97	1.00	283	.05	2	1.95	.01	.13	2	1
STD C/AU-S	21	54	37	126	7.0	64	26	941	3.90	43	15	6	31	44	16	18	20	59	.53	.092	33	55	.88	167	.08	34	1.71	.06	.12	13	50

SHANGRI-LA MINERALS PROJECT-MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B800W 425S	1	31	10	170	.1	51	17	1214	4.03	23	5	ND	2	19	1	2	2	73	.50	.161	13	53	.56	318	.04	2	1.86	.02	.11	1	7
B800W 450S	3	61	10	144	.1	66	23	1522	6.52	23	5	ND	2	12	1	2	2	113	.21	.081	20	64	1.08	184	.03	2	2.81	.02	.08	1	3
B800W 475S	3	87	17	133	.1	92	34	3710	6.54	30	5	ND	3	42	1	2	2	121	.90	.081	18	80	1.39	276	.06	3	2.87	.01	.14	1	4
B800W 500S	1	52	8	136	.1	127	28	1838	5.73	17	5	ND	1	23	1	2	2	134	.50	.070	11	146	1.70	179	.09	2	2.85	.02	.11	1	2
B800W 525S	1	68	13	96	.1	94	22	1034	4.79	20	5	ND	2	22	1	2	2	108	.59	.064	9	95	1.59	127	.03	4	2.52	.02	.17	1	1
B800W 550S	1	186	15	125	.1	80	36	1575	9.12	21	5	ND	1	11	1	2	2	269	.43	.075	3	79	1.39	214	.03	6	3.08	.02	.12	1	4
B800W 575S	1	196	11	152	.1	91	35	1577	8.91	16	5	ND	1	11	1	2	2	225	.55	.058	4	83	1.35	218	.04	7	2.81	.02	.23	1	1
B800W 600S	1	77	10	134	.1	99	30	1364	6.61	8	5	ND	1	11	1	2	2	168	.36	.041	5	97	1.55	140	.15	3	3.32	.03	.10	1	1
B800W 625S	1	138	9	104	.2	80	39	1857	8.48	19	5	ND	1	15	1	2	2	207	1.23	.025	2	91	2.32	144	.05	8	3.35	.02	.16	1	3
B800W 650S	1	147	7	100	.3	106	35	1733	8.24	12	5	ND	2	16	1	2	2	216	.95	.039	11	115	2.62	179	.29	5	3.60	.02	.20	1	2
B800W 675S	1	154	6	106	.1	160	42	2375	8.07	3	5	ND	2	23	1	2	2	189	1.42	.053	8	205	4.03	219	.32	7	3.65	.02	.15	1	3
B800W 700S	2	121	11	203	.3	218	44	2136	7.45	21	5	ND	2	21	1	2	2	187	.77	.084	14	261	3.24	184	.11	5	3.63	.02	.22	1	2
B750W 175N	6	138	677	621	2.1	113	45	4193	7.94	869	5	ND	2	25	9	10	2	117	.55	.094	21	80	1.62	110	.08	3	2.76	.02	.16	1	29
B750W 150N	3	103	637	670	3.0	86	29	1634	6.00	739	5	ND	3	16	5	3	2	108	.33	.059	19	77	1.38	105	.07	3	2.66	.02	.11	1	8
B750W 125N	1	88	622	772	1.0	89	27	2274	6.23	1166	5	ND	3	16	9	3	2	104	.28	.060	17	75	1.37	121	.10	2	2.66	.02	.10	1	9
B750W 100N	3	102	907	932	1.1	80	39	3588	7.95	1397	5	ND	2	18	15	2	2	145	.37	.087	16	65	1.74	111	.08	3	2.82	.02	.13	1	7
B750W 75N	7	79	457	709	.5	82	34	2894	6.93	571	5	ND	3	24	11	2	2	108	.39	.116	21	75	1.44	169	.06	3	2.61	.02	.14	1	15
B750W 50N	3	51	71	271	.1	60	27	2869	6.12	121	5	ND	1	19	2	2	2	134	.39	.084	12	54	1.12	111	.11	2	2.51	.02	.06	1	225
B750W 25N	2	49	44	258	.1	84	28	2982	5.63	124	5	ND	2	14	2	2	2	125	.29	.124	10	91	1.37	147	.16	3	2.80	.02	.10	1	8
B750W 0 N	2	69	32	182	.1	124	28	1860	5.90	84	5	ND	2	17	1	2	2	122	.44	.064	14	131	1.86	119	.17	2	3.01	.02	.13	1	3
B750W 25S	1	63	32	170	.2	115	23	1353	5.07	67	5	ND	3	27	1	2	2	106	.67	.065	13	117	1.65	124	.17	3	2.72	.02	.16	1	1
B750W 50S	3	61	67	194	.2	87	28	2570	5.78	63	5	ND	3	22	2	2	2	127	.56	.064	18	85	1.65	132	.11	2	2.99	.02	.11	1	4
B750W 75S	2	83	50	220	.1	88	33	3197	6.78	79	5	ND	3	28	2	2	2	137	.58	.105	21	70	1.65	140	.07	2	2.95	.02	.15	1	265
B750W 100S	3	64	47	219	.1	76	30	3436	5.23	76	5	ND	2	36	2	2	2	104	.76	.104	16	65	1.34	140	.05	2	2.42	.02	.13	1	2
B750W 125S	8	89	66	326	.4	107	33	2840	7.00	120	5	ND	3	37	3	2	2	119	.77	.141	20	66	1.57	122	.05	3	2.78	.01	.18	1	215
B750W 150AS	2	140	63	549	.6	105	34	3169	8.46	258	5	ND	4	36	8	2	2	122	.97	.136	34	73	2.28	93	.10	5	3.05	.01	.25	1	6
B750W 150BS	4	79	115	292	.5	83	32	4534	5.29	101	5	ND	3	41	5	2	2	98	.86	.136	16	67	1.14	171	.05	4	2.28	.02	.15	1	1
B700W 675N	3	105	48	232	.1	84	18	434	4.11	30	5	ND	4	10	1	2	2	87	.18	.028	7	86	1.11	87	.16	2	2.62	.02	.09	5	3
B700W 650N	7	126	35	226	.3	92	19	452	4.77	41	5	ND	3	10	1	2	2	103	.19	.035	7	98	1.26	78	.22	2	3.08	.02	.10	7	5
B700W 625N	3	79	30	154	.1	66	15	780	4.30	39	5	ND	2	7	1	2	2	86	.11	.075	8	87	1.03	69	.15	2	3.21	.02	.09	5	1
B700W 600N	2	87	17	107	.2	75	14	432	3.78	27	5	ND	2	9	1	2	2	79	.19	.092	7	83	1.13	54	.15	3	3.11	.03	.09	2	2
B700W 575N	3	77	12	119	.1	79	15	380	3.82	33	5	ND	2	10	1	2	2	80	.19	.059	6	81	1.15	60	.16	2	2.55	.02	.09	4	5
B700W 550N	3	123	15	158	.2	99	20	504	4.50	42	5	ND	3	15	1	2	2	85	.25	.047	7	88	1.15	99	.18	2	3.08	.02	.11	6	1
B700W 525N	3	114	24	179	.1	92	18	407	4.38	45	5	ND	4	9	1	2	2	88	.17	.055	8	97	1.27	83	.18	2	3.20	.03	.12	5	2
B700W 500N	3	88	27	206	.1	99	23	679	4.73	51	5	ND	3	15	1	2	4	99	.23	.073	7	99	1.27	118	.21	3	2.96	.03	.17	13	2
B700W 475N	2	518	19	146	.5	106	63	1401	6.00	53	5	ND	2	28	1	2	4	111	.50	.104	5	81	1.48	114	.27	2	2.87	.04	.42	50	12
STD C/AU-S	20	59	38	138	6.9	70	28	1019	3.92	44	17	7	34	48	18	17	18	64	.53	.103	36	59	.87	179	.08	35	1.71	.07	.13	14	50

SHANGRI-LA MINERALS PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B700W 450N	5	348	24	167	.5	164	39	1587	6.95	54	5	ND	2	28	1	2	15	154	.47	.073	6	174	2.44	156	.37	3	3.34	.04	.80	167	21
B700W 425N	14	579	21	177	.4	262	51	1173	7.19	77	5	ND	3	33	1	5	34	160	.50	.081	8	239	3.59	133	.32	3	3.63	.03	.97	105	26
B700W 400N	12	574	29	218	.3	106	47	1909	8.74	81	5	ND	5	29	1	3	31	227	.50	.069	11	95	2.22	181	.21	4	3.26	.04	.53	61	12
B700W 375N	12	287	98	281	.7	111	36	2274	5.53	111	5	ND	6	30	2	2	11	107	.81	.083	18	122	1.88	75	.07	5	2.56	.02	.24	10	45
B700W 350N	5	194	19	200	.3	231	40	1233	6.80	78	5	ND	3	25	1	2	5	152	.63	.046	13	304	3.80	97	.25	7	3.83	.04	.25	3	8
B700W 300N	3	67	30	214	.1	121	24	778	5.47	96	5	ND	2	11	1	2	2	108	.23	.070	15	125	1.83	113	.12	6	3.03	.02	.12	1	1
B700W 275N	7	94	29	176	.3	228	32	1038	7.04	129	5	ND	2	11	1	2	2	102	.16	.074	13	226	2.26	60	.04	5	2.87	.02	.09	1	2
B700W 250N	4	62	50	165	.1	152	32	1397	5.83	156	5	ND	2	11	1	2	2	102	.17	.122	13	197	1.96	66	.03	4	2.71	.02	.05	1	1
B700W 225N	8	246	40	167	.4	228	61	3475	11.52	139	7	ND	3	21	1	9	2	174	.64	.077	29	141	3.37	42	.05	7	3.72	.01	.05	1	2
B700W 200N	4	92	43	186	.5	84	37	2464	8.47	98	5	ND	2	22	2	6	2	144	.59	.081	22	63	1.95	79	.09	8	3.23	.02	.11	1	1
B700W 175N	2	68	55	198	.5	99	27	1323	5.47	117	5	ND	2	20	2	2	2	110	.42	.060	12	85	1.51	122	.13	7	3.03	.02	.10	1	1
B700W 150N	6	103	66	308	.3	114	27	1102	6.10	168	6	ND	3	15	2	4	2	106	.31	.057	22	94	1.51	122	.07	7	2.90	.02	.14	2	3
B700W 125N	6	133	353	666	.9	116	35	1633	9.23	631	5	ND	4	17	5	4	2	107	.33	.085	32	80	1.52	99	.07	9	2.96	.02	.19	1	12
B700W 100N	4	74	449	725	.5	81	29	3392	5.39	454	5	ND	2	21	12	2	2	86	.30	.092	17	48	1.07	136	.07	7	2.39	.02	.13	1	4
B700W 75N	4	84	116	461	.3	93	29	1601	6.15	179	5	ND	2	14	3	5	2	109	.28	.060	16	80	1.33	87	.08	7	3.11	.02	.08	1	8
B700W 50N	4	53	55	252	.1	73	22	1287	5.18	137	5	ND	2	15	1	2	2	105	.28	.065	13	70	1.14	104	.10	6	2.50	.02	.08	1	22
B700W 25N	3	78	30	184	.2	120	24	690	5.92	83	5	ND	3	9	1	2	2	120	.17	.056	10	122	1.87	68	.19	8	3.65	.02	.10	1	2
B700W 0 N	3	64	36	174	.3	92	28	1522	5.63	86	5	ND	2	12	1	2	2	115	.28	.062	10	90	1.54	98	.16	6	3.12	.02	.09	1	1
B700W 25S	3	76	46	204	.2	113	29	1799	6.36	106	5	ND	2	19	1	2	2	127	.39	.049	17	119	1.92	108	.17	6	3.33	.02	.12	1	1
B700W 50S	11	534	17965	5659	28.0	171	84	12910	13.28	1079	6	ND	4	17	48	28	2	150	.50	.120	21	165	3.34	40	.01	2	4.43	.01	.08	1	65
B700W 75S	5	124	276	361	.9	107	42	2668	8.90	175	5	ND	3	21	3	2	2	143	.61	.088	18	88	2.29	92	.07	6	3.46	.02	.15	1	18
B700W 100S	3	116	192	352	1.1	76	42	3946	7.33	135	5	ND	3	37	4	2	2	130	.74	.067	20	48	1.52	107	.06	7	2.94	.02	.12	1	10
B700W 125S	2	72	129	319	.4	54	33	3241	5.42	88	5	ND	2	32	3	2	2	110	.79	.061	15	39	1.09	71	.07	7	2.30	.02	.09	1	1
B700W 150S	4	101	131	266	1.0	69	32	3195	5.67	91	5	ND	3	32	4	2	2	115	.83	.080	18	51	1.23	105	.08	10	2.54	.02	.12	1	10
B700W 175S	3	102	139	324	.8	72	43	4982	6.78	138	5	ND	2	32	5	2	2	136	.90	.108	19	63	1.44	121	.08	8	3.03	.02	.12	1	133
B700W 200S	3	56	81	279	.3	46	22	2363	4.25	597	5	ND	2	39	3	2	2	89	1.23	.079	11	41	.86	98	.08	5	1.94	.02	.11	1	5
B700W 225S	6	87	72	279	.7	69	28	1936	6.62	122	5	ND	3	21	2	3	2	127	.51	.069	18	51	1.36	93	.07	9	2.64	.02	.15	1	58
B700W 250S	8	84	22	202	.1	436	41	893	7.40	50	5	ND	3	18	1	7	2	132	.28	.046	19	482	4.33	134	.03	4	4.04	.01	.08	2	5
B700W 275S	5	46	12	152	.1	225	30	1415	4.67	26	5	ND	1	17	1	2	2	99	.40	.052	12	261	2.24	133	.17	7	2.57	.02	.05	2	1
B700W 300S	3	59	37	253	.1	179	33	2331	5.30	53	5	ND	2	43	2	2	2	105	.96	.119	13	203	2.01	177	.08	8	2.67	.02	.12	1	1
B700W 325S	5	42	12	174	.1	111	23	752	5.14	30	5	ND	2	20	1	2	3	99	.31	.067	14	126	1.34	148	.04	3	2.74	.02	.10	1	1
B700W 350S	3	40	21	142	.1	143	22	975	4.78	36	5	ND	2	32	1	2	2	108	.43	.048	13	172	1.50	107	.06	2	2.46	.02	.06	1	1
B700W 375S	3	59	29	156	.1	124	22	1282	4.84	46	5	ND	2	27	1	2	2	95	.37	.058	13	126	1.56	226	.05	2	2.65	.02	.09	1	2
B700W 400S	2	23	15	143	.1	113	16	576	3.56	21	5	ND	2	12	1	2	2	78	.15	.074	10	115	1.12	175	.06	2	2.00	.02	.07	1	1
B700W 425S	1	31	19	132	.1	84	16	1478	3.74	24	7	ND	2	30	1	2	4	78	.40	.066	10	87	.99	224	.04	2	2.05	.02	.11	1	1
B700W 450S	4	33	15	132	.1	54	19	1725	4.19	16	5	ND	1	16	1	2	3	82	.39	.130	9	60	.87	270	.04	3	1.79	.02	.08	1	2
STD C/AU-S	20	56	36	134	6.7	69	28	997	3.93	44	16	7	32	47	17	15	19	63	.51	.099	35	58	.89	175	.08	35	1.71	.07	.15	12	50

SHANGRI-LA MINERALS PROJECT-MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B700W 475S	1	42	7	114	.1	74	20	826	5.57	14	5	ND	2	15	1	2	2	121	.28	.055	10	82	1.27	110	.06	2	2.64	.02	.06	1	2
B700W 500S	1	36	5	120	.1	78	16	591	3.97	9	5	ND	1	12	1	2	2	100	.28	.081	5	80	1.03	137	.08	5	1.93	.02	.06	1	1
B700W 525S	2	21	15	137	.1	61	16	1702	3.26	172	5	ND	1	27	1	2	2	74	.44	.074	7	60	.70	200	.11	5	1.67	.02	.09	1	1
B700W 550S	1	28	3	132	.1	80	17	637	3.83	5	5	ND	2	14	1	2	2	86	.33	.117	8	82	.94	162	.11	4	2.22	.02	.10	1	2
B700W 575S	2	34	3	107	.1	75	22	1262	3.86	20	5	ND	1	17	1	2	2	81	.39	.045	8	67	.82	127	.08	2	2.03	.02	.11	1	2
B700W 600S	2	48	8	118	.1	92	28	2539	4.95	14	5	ND	2	31	1	2	2	95	.65	.146	9	88	1.05	227	.08	4	2.55	.02	.12	2	1
B700W 625S	1	84	7	135	.1	136	35	2723	7.47	12	5	ND	3	32	1	2	2	151	.80	.071	16	122	2.18	146	.06	4	3.37	.02	.16	1	1
B700W 650S	1	79	8	114	.1	75	25	1662	5.26	3	5	ND	2	13	1	2	2	143	.65	.043	4	82	1.59	151	.18	6	2.77	.04	.12	1	3
B700W 675S	1	68	5	123	.1	96	24	1160	5.34	9	5	ND	2	12	1	3	2	137	.54	.030	5	100	1.48	134	.15	4	2.86	.02	.11	1	1
B700W 700S	1	160	2	148	.1	78	38	1903	8.89	2	5	ND	2	17	1	2	2	240	.99	.047	3	83	1.98	137	.16	3	3.75	.02	.07	1	1
B650W 300N	10	312	42	333	.2	171	51	3530	8.07	99	5	ND	7	27	2	2	6	143	.41	.093	18	125	2.60	116	.09	2	3.59	.03	.25	1	6
B650W 275N	7	24	42	151	.1	81	15	1470	3.53	70	5	ND	3	19	1	2	2	68	.34	.053	12	84	.74	127	.05	3	1.88	.02	.11	2	1
B650W 250N	4	36	37	211	.1	116	22	1897	4.33	56	5	ND	3	27	1	4	2	83	.39	.070	11	148	1.40	118	.05	4	2.45	.02	.13	1	2
B650W 225N	6	51	51	233	.2	117	29	2262	5.29	146	5	ND	1	11	1	2	2	104	.12	.091	14	150	1.45	131	.06	3	2.58	.02	.06	1	3
B650W 200N	3	63	41	276	.2	240	33	1527	6.03	178	5	ND	3	16	1	3	2	114	.26	.109	16	243	2.50	108	.08	3	3.20	.02	.09	1	2
B650W 175N	3	65	40	212	.5	156	30	1374	6.03	143	5	ND	3	27	1	4	2	120	.37	.056	16	148	1.80	103	.13	5	3.18	.02	.12	1	1
B650W 150N	3	50	52	206	.4	102	27	1850	5.15	116	5	ND	2	25	2	2	2	100	.37	.057	12	90	1.12	103	.12	4	2.29	.02	.10	1	1
B650W 125N	8	366	3711	3236	4.9	75	59	12156	14.55	20607	6	ND	6	18	170	10	5	60	.15	.103	50	54	.81	251	.03	3	1.79	.01	.12	1	765
B650W 100N	3	56	127	364	.3	69	25	2313	5.29	231	5	ND	2	28	4	2	2	105	.55	.094	13	68	1.08	112	.09	8	2.57	.02	.09	1	4
B650W 75N	3	69	33	207	.2	73	34	2858	6.28	56	5	ND	3	22	1	2	2	119	.65	.122	23	69	1.39	92	.28	6	2.72	.03	.10	1	2
B650W 50N	2	36	43	163	.1	55	23	2524	4.54	62	5	ND	2	25	1	2	2	108	.51	.067	8	53	.94	140	.15	5	2.10	.03	.06	1	1
B650W 00N	2	51	28	150	.1	79	24	2057	5.11	42	5	ND	2	20	1	2	2	120	.52	.058	9	79	1.33	122	.18	4	2.71	.02	.11	1	2
B650W 25S	2	63	40	188	.4	87	26	2061	5.48	66	5	ND	3	19	1	3	2	116	.43	.082	13	88	1.51	127	.17	4	2.79	.02	.14	1	4
B650W 75S	11	136	271	442	1.0	67	35	3506	6.59	79	5	ND	3	24	5	6	2	112	.52	.075	24	53	1.41	113	.06	4	2.59	.02	.14	1	52
B650W 100S	3	101	137	392	.4	72	37	4077	7.36	84	5	ND	3	22	4	2	2	131	.53	.103	23	59	1.59	137	.06	4	2.84	.02	.16	1	42
B650W 125S	4	91	94	257	.3	67	34	3544	7.04	70	5	ND	3	17	2	2	2	136	.32	.073	17	49	1.27	88	.10	4	2.58	.03	.10	1	82
B650W 150S	4	89	138	317	.4	63	34	2858	7.72	115	5	ND	3	18	3	4	2	153	.49	.091	14	55	1.78	107	.12	4	2.79	.02	.15	1	29
B650W 175S	3	63	31	177	.1	67	33	4306	5.26	50	5	ND	2	48	2	2	2	101	1.45	.106	13	57	1.16	127	.06	7	2.07	.02	.13	1	1
B650W 200S	4	69	49	229	.2	64	24	3562	4.24	71	5	ND	1	48	4	2	2	78	1.41	.149	11	63	.96	192	.06	8	1.90	.02	.16	4	4
B600W 650N	2	32	17	78	.1	28	7	345	2.56	12	5	ND	4	8	1	2	2	62	.12	.030	6	46	.49	57	.10	6	1.68	.03	.05	4	1
B600W 625N	2	67	16	152	.2	68	13	343	4.23	24	7	ND	4	9	1	2	2	85	.16	.047	6	79	1.02	72	.16	2	2.70	.02	.08	5	2
B600W 600N	8	56	20	177	.2	52	13	702	4.00	26	5	ND	3	10	1	4	2	88	.14	.044	8	68	.83	88	.15	3	2.47	.02	.08	6	1
B600W 575N	2	82	15	122	.1	59	12	557	3.70	31	5	ND	2	8	1	2	2	72	.12	.072	9	80	.98	49	.09	3	2.80	.02	.07	7	3
B600W 550N	6	126	63	240	1.1	67	20	1643	4.67	43	5	ND	2	9	1	2	2	94	.12	.066	12	76	1.02	78	.16	3	2.69	.03	.10	8	2
B600W 525N	5	214	50	283	.1	102	30	2173	5.97	47	5	ND	2	13	1	2	5	115	.26	.136	9	96	1.50	93	.16	2	2.81	.03	.27	14	4
B600W 500N	11	649	104	470	1.7	155	66	3986	9.59	51	5	ND	4	27	4	3	4	157	.68	.110	14	120	2.03	130	.29	2	3.35	.04	.63	84	14
STD C/AU-S	21	59	40	138	7.0	69	29	1027	3.92	43	16	7	34	48	18	15	20	65	.48	.103	36	62	.87	181	.08	35	1.71	.07	.13	13	50

SHANGRI-LA MINERALS PROJECT-MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B600W 450N	12	870	25	353	1.2	203	95	1846	10.68	26	5	ND	3	27	1	3	3	171	.70	.087	7	114	2.10	129	.42	3	4.03	.05	.44	25	27
B600W 425N	11	195	58	223	.3	116	35	1445	7.29	48	5	ND	3	18	1	2	4	140	.44	.090	11	105	2.02	100	.20	4	2.95	.03	.31	10	7
B600W 400N	6	225	38	219	.1	106	29	1703	6.26	54	5	ND	3	15	1	2	10	118	.38	.103	12	95	1.75	71	.14	4	2.61	.03	.19	27	12
B600W 350N	8	89	19	140	.1	42	17	634	3.99	28	5	ND	3	18	1	2	2	79	.26	.102	7	48	.80	110	.12	3	1.61	.03	.13	3	1
B600W 300N	5	164	49	207	.2	90	28	1045	5.87	65	5	ND	6	15	1	2	5	119	.37	.079	8	88	1.76	85	.17	2	2.85	.03	.24	36	4
B600W 275N	4	147	32	193	.1	215	31	949	5.45	101	5	ND	3	17	1	2	6	102	.37	.053	9	224	2.55	110	.21	4	3.29	.03	.14	5	5
B600W 250N	3	57	35	175	.2	137	21	1465	4.08	64	5	ND	3	20	1	2	2	86	.29	.044	7	146	1.51	160	.14	2	2.21	.03	.10	1	1
B600W 225N	3	53	39	225	.1	87	13	487	3.74	67	5	ND	3	22	1	3	3	63	.24	.043	13	84	1.11	93	.04	3	2.29	.02	.10	1	1
B600W 200N	4	33	67	249	.2	99	18	1079	3.87	113	5	ND	2	17	2	2	2	74	.23	.035	9	104	1.16	80	.09	3	2.07	.02	.09	1	2
B600W 175N	3	19	58	244	.3	64	18	725	3.71	75	5	ND	2	19	1	2	5	75	.20	.028	8	67	.82	80	.09	3	1.94	.02	.07	1	1
B600W 150N	3	64	163	338	.4	88	27	2514	5.48	152	5	ND	3	18	3	2	2	84	.42	.119	15	70	1.09	116	.07	3	2.28	.02	.14	1	40
B600W 125N	3	63	40	809	.7	153	23	1483	4.85	232	5	ND	2	45	8	2	2	85	.55	.053	15	103	1.42	83	.10	5	2.51	.02	.11	1	3
B600W 100N	2	55	69	277	.2	85	24	1688	5.57	125	5	ND	2	18	2	2	2	104	.26	.070	13	86	1.30	118	.08	4	2.84	.02	.09	1	4
B600W 75N	4	46	54	199	.1	39	18	2442	4.45	77	5	ND	1	12	2	2	2	85	.12	.095	11	46	.73	135	.04	3	2.19	.02	.08	1	1
B600W 50N	1	50	22	167	.1	97	18	958	4.41	56	5	ND	2	13	1	2	2	91	.24	.065	9	83	1.26	101	.14	5	2.51	.02	.08	1	1
B600W 25N	2	48	64	294	.3	63	38	3611	7.08	215	5	ND	3	17	3	2	2	154	.35	.085	9	57	1.60	84	.16	3	2.79	.02	.10	1	395
B600W 0 N	2	75	219	453	.2	53	36	1932	8.68	172	5	ND	2	18	2	2	2	177	.62	.069	6	42	1.92	75	.22	3	3.11	.02	.08	1	225
B600W 25S	2	75	159	269	.5	70	31	1662	7.06	149	5	ND	2	18	2	2	2	161	.42	.050	8	59	1.82	96	.18	3	2.97	.02	.07	1	7
B600W 50S	3	89	148	302	1.0	79	27	1374	6.49	380	5	ND	2	19	2	3	2	124	.39	.052	19	64	1.71	81	.11	3	2.78	.02	.09	1	20
B600W 75S	5	82	77	284	.7	52	24	1459	6.54	258	5	ND	2	19	1	2	2	106	.26	.063	20	40	1.19	113	.05	2	2.53	.02	.12	1	21
B600W 100S	7	65	57	235	.2	42	22	2319	5.14	164	5	ND	3	38	2	2	2	74	.81	.108	16	31	.87	151	.04	4	1.97	.01	.20	1	5
B600W 125S	3	83	55	212	.6	70	30	2743	5.98	161	5	ND	2	27	2	2	2	104	.79	.143	19	55	1.34	140	.09	6	2.77	.02	.16	1	4
B600W 150S	3	70	56	206	.1	56	26	3365	4.64	106	5	ND	2	34	3	2	2	77	.92	.192	15	42	.98	209	.09	10	2.00	.02	.18	1	5
B600W 175S	6	73	83	273	.4	57	32	3663	8.90	375	5	ND	3	27	1	2	2	108	.53	.112	19	50	1.34	98	.05	5	2.93	.02	.13	1	45
B600W 200S	7	48	33	236	.1	150	23	811	5.21	42	5	ND	2	34	2	2	2	111	.72	.062	16	192	1.61	88	.04	4	2.70	.02	.08	1	2
B600W 225S	2	25	16	80	.1	87	15	482	3.45	22	5	ND	1	39	1	2	2	78	.71	.028	9	113	.80	98	.09	5	2.21	.02	.05	1	1
B600W 250S	3	72	23	161	.1	230	29	891	5.66	58	5	ND	2	16	1	3	3	119	.39	.050	15	256	2.73	89	.05	5	3.08	.02	.08	1	1
B600W 275S	2	59	5	149	.1	420	39	1331	5.96	45	5	ND	3	19	1	2	3	122	.35	.057	16	497	4.46	118	.05	3	3.66	.02	.06	1	4
B600W 300S	2	35	10	135	.1	176	22	1076	4.31	23	5	ND	1	19	1	2	2	94	.39	.098	9	195	1.85	121	.08	2	2.45	.02	.09	1	3
B600W 325S	3	45	10	156	.1	173	22	1136	4.36	25	5	ND	2	16	1	2	2	89	.38	.104	15	178	1.73	154	.07	4	2.52	.02	.11	1	1
B600W 350S	3	24	13	129	.1	106	22	776	4.12	23	5	ND	1	15	1	2	2	93	.26	.066	10	134	1.15	119	.06	2	2.00	.02	.06	1	1
B600W 375S	4	37	20	147	.1	178	24	984	4.43	48	5	ND	2	14	1	2	2	97	.18	.046	11	203	1.59	111	.06	5	2.29	.02	.05	1	1
B600W 400S	4	39	10	131	.1	190	24	705	4.68	17	5	ND	2	9	1	2	3	109	.12	.053	17	234	2.16	117	.04	2	2.71	.02	.06	1	2
B600W 425S	2	38	10	108	.2	125	18	368	4.09	25	5	ND	3	10	1	2	2	91	.22	.046	9	116	1.46	78	.09	6	2.53	.02	.07	1	1
B600W 450S	1	25	10	91	.1	102	17	585	3.90	16	5	ND	1	14	1	2	2	88	.25	.042	6	101	1.54	100	.08	2	2.37	.02	.06	1	1
B600W 475S	2	45	11	126	.1	149	25	1777	5.71	33	5	ND	3	16	1	2	2	118	.28	.083	15	145	1.86	102	.07	3	2.80	.02	.09	1	1
STD C/AU-S	20	58	37	136	6.7	70	28	1007	3.93	43	19	7	34	48	17	18	20	64	.43	.100	36	57	.85	180	.08	35	1.71	.07	.13	12	50

SHANGRI-LA MINERALS PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B600W 500S	3	28	13	121	.1	48	17	2991	4.32	12	5	ND	3	26	1	2	2	90	.44	.097	12	43	.87	155	.09	2	2.06	.02	.08	1	1
B600W 525S	2	33	7	121	.1	86	17	1234	3.84	23	5	ND	2	15	1	3	2	87	.38	.084	6	78	1.05	127	.14	2	2.19	.02	.08	1	50
B600W 550S	3	43	15	135	.1	90	19	1104	4.47	39	5	ND	2	17	1	4	2	86	.38	.107	9	89	1.24	147	.09	3	2.27	.02	.11	1	3
B600W 575S	2	22	12	137	.1	69	15	1844	3.08	11	5	ND	1	21	1	2	2	61	.43	.179	5	62	.71	208	.10	3	1.72	.02	.11	1	1
B600W 600S	3	42	16	140	.1	110	20	1839	4.46	36	5	ND	2	16	1	2	2	89	.32	.081	8	97	1.16	171	.11	2	2.35	.02	.08	1	1
B600W 625S	2	33	10	131	.1	83	16	967	3.69	23	5	ND	1	12	1	2	2	74	.27	.098	6	75	.97	121	.11	3	1.96	.02	.07	1	2
B600W 650S	2	23	8	129	.1	71	14	736	3.21	16	5	ND	2	15	1	2	2	67	.26	.071	5	64	.80	120	.12	2	1.88	.02	.06	1	1
B600W 675S	2	25	10	126	.2	69	15	1198	3.31	17	5	ND	2	15	1	2	2	66	.29	.060	7	62	.78	130	.10	3	1.82	.02	.08	1	2
B600W 700S	2	36	6	159	.1	83	18	1152	3.96	15	5	ND	2	14	1	4	2	78	.25	.063	7	68	.87	155	.10	3	2.12	.02	.08	1	1
B500W 625N	8	46	18	96	.2	39	7	308	2.58	24	5	ND	4	8	1	2	2	53	.09	.037	7	53	.64	56	.06	2	1.91	.02	.06	4	1
B500W 600N	5	54	21	132	.1	47	9	432	3.07	24	5	ND	4	9	1	2	2	41	.11	.042	7	58	.74	67	.09	2	1.91	.02	.06	3	6
B500W 575N	2	35	25	112	.1	31	7	414	2.51	18	5	ND	5	8	1	2	2	49	.10	.030	7	36	.50	60	.07	2	1.40	.02	.06	1	1
B500W 550N	3	79	41	132	.1	46	11	507	2.99	31	5	ND	9	10	1	2	2	53	.14	.058	9	47	.66	84	.07	2	1.91	.02	.06	2	1
B500W 500N	3	100	52	107	.1	28	11	1372	2.53	29	5	ND	10	12	1	2	4	38	.16	.089	14	27	.46	74	.04	2	1.46	.02	.07	1	1
B500W 475N	2	65	42	149	.1	56	12	971	2.91	47	5	ND	7	17	1	2	2	52	.20	.053	8	57	.75	91	.08	2	1.74	.02	.08	4	1
B500W 450N	7	104	53	165	.1	77	16	774	3.75	66	5	ND	7	10	1	3	3	61	.16	.057	11	77	1.11	55	.06	2	2.15	.02	.10	3	2
B500W 400N	3	20	16	98	.2	37	8	299	2.24	23	5	ND	1	11	1	3	2	52	.15	.076	5	55	.55	84	.09	2	1.31	.03	.05	2	1
B500W 375N	3	153	43	175	.1	96	27	1038	6.07	40	5	ND	2	17	1	2	2	121	.54	.091	6	114	1.74	109	.20	2	3.14	.04	.18	13	3
B500W 350N	4	227	46	179	.7	88	27	1580	5.08	40	5	ND	2	12	1	2	2	96	.31	.101	8	91	1.44	71	.13	2	2.95	.03	.12	19	4
B500W 325N	2	206	35	154	.2	126	45	1673	7.22	29	5	ND	3	19	1	2	2	141	.67	.097	6	118	2.03	144	.33	2	3.51	.05	.31	9	12
B500W 300N	3	104	83	245	.1	89	26	3043	4.31	46	5	ND	3	28	2	2	3	83	.44	.085	7	86	1.13	201	.21	2	2.47	.04	.24	13	1
B500W 275N	4	213	51	229	.1	108	31	1224	5.80	90	5	ND	4	18	1	2	4	103	.28	.078	9	92	1.64	104	.17	2	3.39	.02	.15	14	6
B500W 250N	4	102	34	168	.1	96	20	1266	4.59	59	5	ND	4	14	1	2	2	93	.24	.057	9	93	1.37	101	.16	3	2.63	.02	.12	2	5
B500W 225N	2	70	26	166	.1	92	21	1623	4.05	53	5	ND	3	14	1	2	2	83	.27	.076	8	89	1.24	130	.17	2	2.40	.02	.12	10	1
B500W 200N	3	81	28	207	.1	83	22	2046	3.90	38	5	ND	3	20	2	4	2	77	.29	.096	8	80	1.07	155	.15	2	2.34	.02	.12	9	11
B500W 175N	3	45	24	178	.2	77	17	1686	3.43	72	5	ND	3	17	2	2	2	70	.30	.077	7	73	.91	137	.14	3	2.17	.03	.09	4	1
B500W 150N	3	26	33	181	.2	84	15	862	3.67	46	5	ND	3	19	1	2	2	77	.23	.045	8	90	.92	89	.13	2	2.00	.02	.08	1	1
B500W 125N	3	26	63	323	.3	77	18	2260	3.87	62	5	ND	2	20	3	3	2	76	.34	.102	8	93	.97	189	.10	3	2.02	.02	.10	1	1
B500W 100N	1	23	17	168	.1	42	13	1156	3.06	28	5	ND	2	13	1	2	2	63	.21	.089	7	50	.64	106	.09	3	1.67	.02	.05	1	1
B500W 75N	3	37	43	171	.3	63	18	1942	4.08	71	5	ND	2	10	1	3	2	79	.13	.053	9	62	.85	134	.10	2	2.00	.02	.06	1	1
B500W 50N	2	74	132	258	.4	79	35	4692	7.53	137	5	ND	3	22	3	2	2	149	.59	.132	22	75	1.70	113	.07	2	3.00	.02	.11	1	10
B500W 25N	2	65	32	165	.1	139	31	2290	6.50	62	5	ND	3	16	1	2	2	121	.40	.102	17	151	2.57	101	.11	3	3.00	.02	.13	1	1
B500W 0 N	2	76	44	189	.1	72	37	3122	8.59	54	5	ND	3	29	1	2	2	166	.87	.103	12	70	2.60	82	.32	4	3.29	.03	.17	1	16
B500W 25S	2	61	34	170	.1	57	29	2681	6.04	55	5	ND	2	35	1	2	2	124	1.10	.142	13	58	1.67	83	.25	5	2.73	.03	.12	1	1
B500W 50S	3	66	92	283	.2	57	30	3368	6.43	144	5	ND	3	25	3	2	2	138	.73	.115	15	58	1.51	104	.25	5	2.79	.02	.15	1	2
B500W 75S	3	52	81	286	.1	49	25	2737	5.60	137	5	ND	3	21	3	2	2	108	.54	.151	12	48	1.11	113	.14	3	2.47	.02	.14	1	3
B500W 100S	3	43	91	386	.3	47	21	3127	4.26	109	5	ND	3	28	7	2	2	71	.83	.205	11	41	.73	135	.07	4	1.90	.02	.16	1	5
STD C/AU-S	22	59	40	143	7.0	72	30	1055	3.93	42	19	7	36	49	19	14	21	60	.53	.105	36	61	.87	184	.09	33	1.71	.07	.13	14	50

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B500W 125S	1	87	34	180	.3	75	35	2403	7.51	171	5	ND	3	25	1	2	2	151	.64	.060	15	58	1.49	125	.15	5	3.08	.02	.10	1	540
B500W 150S	2	65	40	219	.2	64	29	2115	6.23	167	5	ND	3	25	2	2	2	134	.52	.085	10	53	1.37	108	.14	4	2.64	.02	.13	2	7
B500W 175S	1	41	61	209	.2	73	24	1401	5.17	175	5	ND	2	18	1	2	2	124	.39	.117	9	64	1.23	88	.11	3	2.35	.03	.12	1	8
B500W 200S	1	46	45	190	.1	76	23	2055	5.39	95	5	ND	1	23	2	2	2	108	.48	.071	11	69	1.15	122	.06	4	2.37	.02	.13	1	4
B500W 225S	1	53	26	185	.1	194	22	605	5.21	47	5	ND	2	10	1	2	2	104	.20	.083	13	214	2.24	81	.07	3	2.96	.02	.07	1	1
B500W 250S	2	28	23	170	.1	79	17	1436	3.68	28	5	ND	2	14	1	2	2	74	.22	.089	11	68	.92	152	.07	4	2.16	.02	.09	1	5
B500W 275S	2	29	15	139	.1	50	15	1716	3.22	23	5	ND	1	15	1	2	2	57	.22	.070	8	41	.62	165	.05	4	1.95	.03	.11	1	1
B500W 300S	1	29	35	165	.1	81	18	1391	3.49	22	5	ND	2	15	1	2	2	67	.23	.140	9	89	.87	152	.06	4	1.95	.02	.11	1	3
B500W 325S	1	50	17	191	.1	249	29	1404	5.70	73	5	ND	2	19	1	2	2	116	.33	.120	17	245	2.32	129	.04	2	2.97	.02	.08	1	2
B500W 350S	1	18	10	129	.1	74	16	951	3.29	15	5	ND	1	18	1	2	2	73	.28	.095	10	83	.78	158	.07	3	1.76	.03	.07	1	1
B500W 375S	1	53	20	138	.1	132	20	901	4.97	43	5	ND	3	18	1	2	2	104	.35	.109	13	121	1.68	180	.07	4	2.61	.02	.12	1	3
B500W 400S	1	37	21	138	.1	108	19	884	4.64	35	5	ND	2	14	1	2	2	99	.22	.079	11	101	1.28	168	.08	4	2.33	.02	.08	1	2
B500W 425S	1	21	10	97	.1	60	12	622	3.25	21	5	ND	2	11	1	2	2	72	.20	.093	9	65	.74	112	.09	2	1.57	.02	.07	2	10
B500W 450S	1	21	14	151	.1	59	13	811	3.14	19	5	ND	2	11	1	2	2	66	.21	.132	7	60	.73	112	.10	3	1.73	.02	.10	1	1
B500W 475S	1	19	12	166	.1	61	13	1356	3.08	17	5	ND	1	12	1	2	2	61	.23	.175	7	58	.72	127	.10	3	1.91	.02	.09	1	1
B500W 500S	1	18	15	192	.1	43	13	2577	3.03	8	5	ND	2	15	1	2	2	60	.23	.167	7	53	.58	270	.11	4	1.59	.02	.10	1	1
B500W 525S	1	79	23	150	.1	158	32	1840	6.71	41	5	ND	3	18	1	2	2	109	.33	.079	19	141	2.39	141	.08	5	3.19	.02	.08	2	3
B500W 550S	1	29	16	147	.1	77	17	1637	3.69	23	5	ND	1	19	1	2	2	76	.36	.142	8	70	.99	132	.10	4	2.07	.02	.08	1	1
B500W 575S	1	44	23	178	.1	104	21	2305	4.29	30	5	ND	1	26	2	2	2	84	.51	.163	12	95	1.23	186	.07	5	2.31	.02	.17	1	3
B500W 600S	1	31	11	143	.1	70	16	2190	3.71	16	5	ND	1	28	1	2	2	77	.47	.132	10	64	.90	207	.11	4	1.91	.03	.14	1	1
B500W 625S	1	48	13	157	.1	154	22	1725	4.92	27	5	ND	2	23	1	2	2	94	.34	.088	14	140	1.64	254	.07	4	2.65	.02	.11	1	2
B500W 650AS	1	45	13	118	.1	71	17	2602	3.34	23	5	ND	2	27	1	2	2	68	.48	.124	9	62	.78	208	.09	2	1.71	.02	.13	1	1
B500W 650BS	2	21	19	49	.1	18	3	196	2.21	18	5	ND	2	6	1	2	4	60	.07	.027	7	34	.35	41	.04	2	1.36	.02	.03	4	1
B500W 675S	1	19	11	135	.1	59	12	1094	2.93	11	5	ND	2	13	1	2	2	65	.26	.097	6	58	.70	112	.11	3	1.69	.02	.07	1	1
B500W 700S	1	39	9	137	.1	77	15	1136	3.69	23	5	ND	1	17	1	2	2	77	.35	.075	7	65	.99	136	.10	4	1.94	.02	.08	1	1
B400W 575N	1	29	21	71	.1	19	5	486	2.10	15	5	ND	3	6	1	2	3	49	.08	.034	8	25	.34	55	.05	2	1.26	.02	.04	2	1
B400W 550N	1	16	20	60	.1	12	3	277	1.54	9	5	ND	3	7	1	2	2	40	.08	.025	6	17	.23	51	.05	2	.92	.02	.05	2	1
B400W 500N	1	42	27	110	.1	28	8	618	2.44	26	5	ND	7	9	1	2	2	50	.12	.052	9	29	.48	82	.05	3	1.58	.02	.05	2	1
B400W 475N	2	91	34	115	.1	42	9	375	2.87	36	5	ND	10	7	1	2	4	46	.10	.039	14	42	.70	53	.04	2	1.97	.02	.07	4	1
B400W 424N	1	42	31	108	.1	34	8	707	2.66	30	5	ND	4	12	1	2	4	52	.17	.050	8	37	.58	83	.05	3	1.66	.02	.08	2	1
B400W 400N	3	29	19	99	.1	118	14	404	3.53	25	5	ND	3	20	1	3	2	98	.31	.041	7	195	1.67	180	.25	2	2.05	.03	.13	3	1
B400W 375N	4	77	45	179	.1	288	30	1337	4.72	34	5	ND	2	16	1	2	2	105	.25	.057	8	379	2.98	230	.22	2	2.99	.03	.14	3	1
B400W 350N	1	88	29	161	.1	197	32	1444	4.71	34	5	ND	1	17	1	2	3	108	.35	.095	7	265	2.53	88	.16	3	2.68	.03	.11	3	1
B400W 325N	1	31	22	53	.1	36	5	226	1.92	17	5	ND	1	7	1	2	2	49	.09	.045	6	54	.56	50	.05	2	1.36	.03	.04	1	1
B400W 300N	3	36	32	140	.3	53	12	1148	3.66	36	5	ND	1	8	1	5	2	78	.10	.054	7	68	.82	62	.11	4	2.05	.02	.05	3	1
B400W 275N	2	38	31	229	.2	52	15	1388	3.61	28	5	ND	1	17	1	2	2	76	.23	.083	7	58	.79	95	.10	4	1.94	.02	.11	1	2
STD C/AU-S	20	59	39	138	6.8	70	28	1020	3.97	40	14	8	34	48	18	15	20	65	.51	.102	36	59	.86	182	.08	37	1.69	.07	.14	13	47

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B400W 250N	3	44	43	236	.1	51	18	2793	3.84	27	5	ND	2	20	2	3	2	80	.26	.105	9	59	.76	144	.09	3	2.01	.02	.11	2	1
B400W 225N	1	42	21	139	.1	55	14	1463	3.31	17	5	ND	1	14	1	2	2	77	.25	.080	6	57	.89	115	.13	3	1.86	.02	.11	1	1
B400W 175N	1	41	22	159	.1	70	16	1377	3.24	22	5	ND	1	25	2	2	2	70	.33	.092	7	72	.98	219	.13	3	1.89	.02	.14	4	1
B400W 150N	1	72	16	173	.1	181	23	814	4.52	34	5	ND	2	13	1	2	2	95	.23	.061	8	169	1.84	97	.17	3	2.95	.02	.10	2	1
B400W 125N	2	40	18	145	.1	94	17	827	4.38	33	5	ND	1	15	1	2	2	96	.26	.057	8	90	1.17	94	.13	2	2.32	.02	.08	1	1
B400W 100N	2	52	18	190	.4	451	18	1685	3.48	325	5	ND	1	55	2	2	2	61	.81	.174	9	257	1.41	92	.06	7	2.33	.02	.06	1	4
B400W 75N	1	50	62	247	.1	147	24	1328	4.78	100	5	ND	1	24	2	2	2	87	.39	.110	10	167	1.66	126	.06	3	2.42	.02	.11	1	1
B400W 50N	1	44	40	369	.1	105	24	1534	5.16	81	5	ND	2	14	2	2	2	98	.21	.093	11	105	1.46	106	.10	3	2.62	.02	.12	1	2
B400W 25N	1	32	87	407	.1	73	21	3412	4.18	47	5	ND	1	41	10	2	2	79	.49	.135	10	71	.92	254	.09	3	2.06	.02	.15	1	1
B400W 00N	1	43	44	249	.1	101	23	1414	4.91	80	5	ND	2	26	1	2	2	92	.44	.099	10	102	1.37	130	.08	2	2.50	.02	.13	1	10
B400W 25S	1	53	55	195	.2	84	26	2380	5.44	108	5	ND	1	17	1	3	2	100	.34	.095	14	77	1.23	103	.07	4	2.55	.02	.12	1	18
B400W 50S	1	76	48	184	.4	89	36	3610	7.12	191	5	ND	2	21	1	2	2	158	.54	.126	15	105	2.23	104	.13	4	3.16	.02	.10	1	370
B400W 75S	4	72	191	563	5.4	103	24	4099	5.36	150	5	ND	2	58	2	4	2	58	.53	.114	16	71	1.08	285	.02	4	2.00	.02	.21	1	35
B400W 100S	2	43	44	191	.2	94	23	1963	4.85	66	5	ND	1	23	2	2	2	90	.48	.158	12	93	1.27	163	.08	3	2.28	.02	.14	1	2
B400W 125S	3	61	43	203	.2	70	31	3155	6.37	64	5	ND	2	22	1	3	2	124	.47	.154	17	59	1.62	152	.06	4	2.82	.02	.13	1	6
B400W 150S	1	70	51	195	.2	66	30	1873	7.99	77	5	ND	2	16	1	2	2	174	.33	.080	13	64	1.74	97	.07	2	3.13	.02	.10	1	34
B400W 175S	1	67	49	221	.1	60	26	1986	6.66	55	5	ND	3	24	1	2	2	133	.46	.100	15	57	1.46	126	.13	4	2.91	.02	.12	1	31
B400W 200AS	2	47	26	211	.1	62	17	1869	3.85	28	5	ND	1	20	1	2	2	82	.30	.100	7	58	.85	131	.12	4	2.28	.02	.11	3	1
B400W 200BS	2	73	241	376	.6	59	31	3269	7.14	234	5	ND	2	16	2	2	2	153	.35	.093	12	58	1.35	121	.11	3	2.97	.02	.12	1	19
B400W 225S	1	36	34	154	.3	48	20	1817	5.09	73	5	ND	1	16	1	2	2	106	.31	.076	9	44	.74	107	.06	3	2.07	.02	.07	1	26
B400W 250S	1	21	30	164	.1	32	19	1443	4.96	45	5	ND	1	13	1	2	2	114	.24	.094	7	34	.75	85	.09	2	2.00	.02	.07	1	3
B400W 275S	1	20	19	164	.1	52	13	1129	2.76	19	5	ND	1	13	2	2	2	58	.24	.089	7	50	.69	93	.09	3	1.77	.02	.08	1	1
B400W 300S	2	29	40	153	.1	52	15	1558	3.08	22	5	ND	1	14	1	2	2	61	.25	.093	9	47	.59	147	.09	5	1.63	.02	.08	1	1
B400W 325S	1	21	18	125	.1	68	12	537	3.22	19	5	ND	1	11	1	2	2	72	.21	.075	7	70	.77	99	.11	2	1.79	.02	.06	1	1
B400W 350S	1	19	13	130	.1	50	12	539	3.36	13	5	ND	1	14	1	2	2	69	.26	.115	7	57	.71	111	.11	3	1.77	.02	.07	1	1
B400W 375S	1	21	13	119	.1	83	17	1035	3.66	18	6	ND	2	13	1	2	3	81	.23	.089	8	95	.98	115	.12	4	1.80	.02	.08	1	1
B400W 400S	2	22	9	135	.1	65	14	2086	3.38	13	5	ND	1	14	1	2	3	68	.30	.112	5	65	.83	231	.10	2	1.68	.02	.07	1	1
B400W 425S	1	22	15	151	.1	57	14	1281	3.31	17	5	ND	1	13	1	2	6	69	.24	.109	8	60	.77	150	.09	2	1.84	.02	.06	1	3
B400W 450S	1	18	14	139	.1	57	14	1560	3.31	14	5	ND	1	14	1	2	2	69	.26	.107	6	63	.72	162	.09	2	1.58	.02	.09	1	1
B400W 475S	1	28	13	148	.1	63	15	1520	3.82	16	5	ND	1	13	1	2	3	76	.27	.128	9	62	.94	146	.11	4	2.03	.02	.10	1	1
B400W 500S	1	22	12	114	.1	55	16	1702	3.67	15	5	ND	1	16	1	2	2	72	.31	.136	8	50	.82	154	.11	3	1.86	.02	.13	1	2
B400W 525S	1	33	15	147	.1	89	18	1353	4.09	21	5	ND	1	20	1	2	2	79	.35	.150	9	82	1.13	168	.09	4	2.29	.02	.10	1	1
B400W 550S	1	48	14	128	.1	95	23	2170	4.54	18	5	ND	2	18	1	2	2	82	.38	.138	11	92	1.31	182	.08	4	2.36	.02	.14	1	1
B400W 575S	1	42	10	114	.1	76	22	2088	4.52	14	5	ND	1	23	1	2	2	86	.40	.152	10	84	1.14	177	.08	3	2.31	.02	.13	1	1
B400W 600S	2	44	17	147	.1	77	24	2980	4.63	18	5	ND	1	21	1	2	3	87	.34	.155	10	82	1.12	202	.08	4	2.55	.02	.11	1	1
B400W 625S	1	28	13	126	.1	51	17	2641	3.63	10	5	ND	1	28	1	2	2	69	.36	.150	8	54	.77	229	.09	3	1.89	.02	.13	1	1
B400W 650S	1	44	13	138	.1	104	21	1622	4.74	22	5	ND	1	16	1	2	2	96	.31	.117	10	105	1.33	143	.09	4	2.59	.02	.11	1	1
STD C/AU-S	19	58	41	138	7.1	69	29	1019	3.95	39	18	7	34	48	18	16	20	64	.48	.102	36	58	.91	180	.08	36	1.73	.07	.14	12	48

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM
B400W 675S	1	34	7	119	.1	89	15	743	3.65	19	5	ND	2	15	1
B400W 700S	1	30	9	134	.1	92	16	864	3.48	18	5	ND	3	13	1
B350W 150S	1	39	37	167	.1	84	19	805	4.55	86	6	ND	3	12	1
B350W 175S	1	44	38	211	.1	100	30	1527	6.27	110	5	ND	3	15	1
B350W 200S	3	67	18	155	.1	74	26	1491	6.16	46	5	ND	3	15	1
B350W 225S	1	35	18	137	.1	66	18	988	4.21	51	5	ND	3	13	1
STD C/AU-S	19	57	39	134	6.7	67	28	988	3.73	42	18	7	35	46	17
B350W 250S	2	33	28	159	.2	48	24	1395	4.70	49	5	ND	3	15	1
B350W 275S	1	43	34	190	.3	84	20	1413	4.94	77	5	ND	3	16	1
B350W 300S	1	29	9	104	.1	43	16	1166	3.83	20	5	ND	1	16	1
B350W 325S	1	24	12	156	.1	57	14	1618	3.12	13	5	ND	2	16	2
B350W 350S	1	33	13	192	.2	51	14	1076	3.56	22	5	ND	2	13	1
B350W 375S	1	28	14	182	.2	66	14	1194	3.48	26	5	ND	2	13	1
B350W 400S	1	25	16	167	.1	66	15	1784	3.48	30	5	ND	2	13	1
B350W 425S	1	27	18	134	.1	79	17	1527	3.52	29	5	ND	2	21	1
B350W 450S	1	14	12	99	.1	27	9	1217	2.41	10	5	ND	1	10	1
B300W 575N	2	141	43	170	.1	17	7	480	2.11	35	5	ND	18	10	1
B300W 550N	2	69	42	268	.2	26	8	778	2.70	33	4	ND	11	8	1
B300W 525N	1	89	38	117	.2	15	7	1285	2.20	30	5	ND	15	6	1
B300W 500N	9	59	57	164	.1	66	18	1923	3.94	50	5	ND	6	13	1
B300W 475N	3	38	37	107	.5	40	9	597	3.45	42	5	ND	2	11	1
B300W 450N	1	28	14	78	.1	36	7	247	3.17	28	5	ND	1	9	1
B300W 425N	3	61	23	98	.1	59	12	696	4.15	42	5	ND	1	7	1
B300W 400N	2	71	17	120	.1	101	15	720	4.15	52	5	ND	2	8	1
B300W 375N	6	46	26	137	.1	148	14	640	4.45	40	5	ND	2	9	1
B300W 350N	1	26	16	83	.1	43	8	461	2.62	21	5	ND	1	9	1
B300W 325N	1	32	57	63	.8	35	5	218	2.01	18	5	ND	1	8	1
B300W 300N	4	40	26	94	.2	43	9	757	3.58	27	5	ND	1	8	1
B300W 275N	2	41	23	137	.5	43	9	385	3.75	27	5	ND	1	10	1
B300W 250N	5	103	28	226	.2	77	17	1208	4.35	41	5	ND	3	17	1
B300W 225AN	2	143	25	203	.1	84	18	992	4.24	33	5	ND	3	14	1
B300W 225BN	2	29	9	82	.1	103	11	333	2.75	13	5	ND	2	12	1
B300W 375S	3	37	13	195	.1	89	18	2883	4.19	15	5	ND	2	26	2
B250W 150S	1	24	13	120	.2	55	13	1358	3.98	28	5	ND	1	13	1
B250W 175S	1	18	15	147	.1	43	11	660	3.56	18	5	ND	1	10	1
B250W 200S	1	30	20	209	.1	82	14	1837	3.85	30	5	ND	1	20	2

SAMPLE#	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B400W 675S	2	2	75	.31	.150	7	91	1.15	124	.09	4	2.05	.02	.08	1	3
B400W 700S	2	2	83	.28	.183	10	100	1.10	110	.09	3	2.12	.02	.06	1	1
B350W 150S	2	2	97	.24	.116	10	84	1.27	83	.12	4	2.45	.02	.10	1	1
B350W 175S	2	2	124	.32	.112	8	88	1.57	150	.06	2	2.95	.02	.11	1	1
B350W 200S	2	2	118	.26	.076	19	58	1.41	105	.04	2	2.78	.02	.10	1	52
B350W 225S	2	2	93	.26	.063	9	62	.98	84	.11	2	2.10	.02	.09	1	1
STD C/AU-S	16	21	64	.45	.100	36	60	.84	171	.08	37	1.62	.07	.14	13	51
B350W 250S	2	2	110	.34	.077	6	53	.91	86	.15	3	2.00	.02	.08	1	1
B350W 275S	2	2	113	.32	.073	10	80	1.23	122	.12	5	2.58	.02	.09	1	5
B350W 300S	2	2	111	.27	.064	6	44	.80	88	.14	3	1.78	.02	.07	1	1
B350W 325S	2	2	66	.25	.092	8	53	.63	157	.10	3	1.64	.02	.08	1	1
B350W 350S	3	2	69	.25	.158	9	55	.78	150	.10	3	2.02	.02	.12	1	1
B350W 375S	2	2	74	.25	.118	8	67	.85	156	.10	4	2.03	.02	.10	1	1
B350W 400S	2	2	74	.24	.099	9	67	.82	188	.10	2	1.86	.02	.10	1	2
B350W 425S	2	2	77	.34	.107	8	77	.92	196	.11	3	1.82	.02	.11	1	9
B350W 450S	2	2	51	.14	.110	5	38	.39	97	.08	3	1.22	.02	.08	1	3
B300W 575N	2	6	31	.13	.053	21	17	.41	57	.01	3	1.56	.02	.09	1	1
B300W 550N	2	4	49	.11	.071	12	30	.52	51	.03	3	1.70	.02	.09	2	1
B300W 525N	2	5	31	.07	.041	20	17	.37	78	.01	3	1.46	.01	.10	1	1
B300W 500N	2	2	77	.20	.085	11	70	1.42	135	.06	4	2.30	.02	.19	1	1
B300W 475N	2	4	83	.10	.065	9	54	.74	78	.06	2	1.77	.02	.07	2	2
B300W 450N	2	2	81	.11	.053	7	41	.70	45	.09	2	1.63	.02	.04	1	1
B300W 425N	2	2	102	.09	.059	10	85	1.13	60	.08	2	2.25	.03	.07	1	1
B300W 400N	2	2	87	.12	.065	9	113	1.36	51	.11	2	2.64	.02	.06	1	1
B300W 375N	2	3	106	.12	.049	10	226	1.94	96	.15	3	2.77	.02	.07	1	1
B300W 350N	2	2	65	.11	.045	6	58	.62	60	.11	4	1.49	.03	.04	1	1
B300W 325N	2	3	59	.09	.043	6	54	.54	56	.08	3	1.39	.02	.04	1	1
B300W 300N	2	2	83	.10	.067	9	75	.78	59	.11	2	2.23	.02	.05	1	1
B300W 275N	2	2	90	.12	.060	10	58	.76	58	.10	2	2.06	.02	.05	3	6
B300W 250N	2	3	97	.21	.077	12	68	1.10	127	.10	2	2.50	.02	.10	4	2
B300W 225AN	2	3	91	.21	.080	10	72	1.15	90	.13	2	2.66	.02	.09	1	1
B300W 225BN	2	2	68	.14	.039	4	93	.83	76	.13	2	1.63	.03	.04	1	1
B300W 375S	2	3	80	.43	.175	11	95	1.04	244	.08	3	1.77	.02	.16	1	1
B250W 150S	2	2	77	.18	.083	8	65	.80	109	.06	3	2.09	.02	.07	2	7
B250W 175S	2	2	72	.18	.066	6	65	.64	93	.09	2	2.11	.02	.03	1	1
B250W 200S	2	2	75	.38	.186	9	81	1.06	202	.08	4	2.12	.02	.13	1	1

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B250W 225S	2	37	28	192	.1	65	17	2091	4.94	43	5	ND	1	19	1	2	2	96	.33	.242	11	75	1.03	158	.06	6	2.49	.02	.13	1	1
B250W 250S	1	23	21	182	.2	40	18	1915	4.33	35	5	ND	1	17	1	2	2	92	.34	.156	8	68	.91	175	.12	6	2.23	.02	.11	1	1
B250W 275S	2	46	22	149	.1	80	21	1781	5.25	62	5	ND	1	21	1	2	2	119	.41	.113	9	88	1.40	158	.13	6	2.70	.02	.11	1	4
B250W 300S	4	78	26	164	.4	79	41	2827	10.01	55	5	ND	1	21	1	3	2	218	.55	.074	12	78	2.40	171	.12	6	3.33	.02	.09	1	33
B250W 325S	1	32	19	157	.1	56	16	1916	3.95	29	5	ND	1	16	1	2	2	85	.32	.118	8	62	.90	162	.11	5	1.99	.02	.11	1	1
B250W 350S	1	28	21	143	.1	51	16	2340	3.84	27	5	ND	1	16	1	2	2	82	.29	.124	8	57	.83	168	.12	5	2.07	.02	.12	1	1
B200W 500N	6	68	79	258	.1	120	18	714	5.02	91	5	ND	2	17	1	2	2	108	.22	.052	15	143	1.60	110	.11	5	2.95	.02	.10	5	1
B200W 475N	5	43	29	239	.3	90	16	486	4.43	49	5	ND	1	14	1	2	2	89	.20	.074	11	104	1.26	80	.12	5	2.72	.02	.11	3	1
B200W 450N	8	47	21	182	.1	78	17	1323	3.97	39	5	ND	1	12	1	2	2	85	.16	.073	9	86	1.08	86	.11	6	2.18	.02	.11	1	1
B200W 425N	5	84	62	301	.2	94	20	2097	4.38	40	5	ND	1	18	1	2	2	93	.25	.084	11	98	1.25	170	.10	6	2.58	.02	.10	1	1
B200W 400N	4	16	17	89	.1	30	8	424	2.38	15	5	ND	1	15	1	2	2	59	.21	.053	4	39	.47	73	.12	5	1.06	.03	.05	1	1
B200W 375N	6	36	32	143	.1	79	14	837	3.93	38	5	ND	1	17	1	2	2	94	.23	.066	8	105	1.06	113	.10	4	1.92	.03	.09	1	1
B200W 350N	7	43	23	122	.3	67	17	1062	3.50	30	5	ND	1	10	1	2	2	79	.14	.074	9	77	.86	67	.09	4	2.33	.02	.06	1	1
STD C/AU-S	20	59	37	133	6.9	69	29	1025	3.85	41	17	7	33	48	17	15	20	65	.46	.103	36	61	.85	172	.09	38	1.70	.07	.13	13	47
B200W 325N	3	31	20	85	.2	45	8	307	3.80	27	5	ND	1	12	1	2	2	84	.16	.055	7	78	.78	54	.09	4	1.87	.02	.04	1	1
B200W 250N	2	9	10	28	.1	10	3	108	1.35	8	5	ND	1	7	1	2	2	39	.07	.055	3	18	.23	20	.07	6	.77	.02	.03	1	2
B200W 225N	4	36	36	72	.5	37	7	588	2.16	26	5	ND	1	19	1	2	2	56	.36	.075	7	49	.56	45	.06	5	1.83	.03	.04	2	2
B200W 125N	3	122	67	243	.4	113	19	1029	5.34	47	5	ND	1	14	1	2	2	120	.28	.108	13	133	1.86	93	.12	4	3.23	.02	.11	2	1
B200W 100N	4	220	47	175	.3	69	18	1247	5.08	48	5	ND	3	15	1	3	2	113	.27	.093	18	62	1.44	88	.06	5	2.54	.02	.12	1	4
B200W 75N	2	153	55	206	.1	120	21	1183	4.32	44	5	ND	3	15	1	2	2	96	.23	.068	12	106	1.40	97	.14	5	2.62	.03	.10	2	4
B200W 25N	6	62	40	204	.1	138	22	1704	3.89	66	5	ND	1	14	1	2	2	77	.18	.084	9	129	1.15	96	.08	6	2.22	.02	.09	1	1
B200W 0 N	2	32	16	155	.1	124	13	682	2.87	37	5	ND	1	18	1	2	2	58	.18	.065	10	119	.91	91	.07	5	1.90	.02	.07	1	1
B200W 25S	1	17	23	108	.2	65	9	780	2.54	23	5	ND	1	16	1	2	2	55	.14	.060	6	89	.84	115	.06	4	1.61	.02	.06	1	1
B200W 50S	1	33	33	178	.1	88	13	704	3.84	59	5	ND	1	12	1	2	2	75	.17	.145	7	96	1.06	92	.10	5	2.63	.02	.07	1	1
B200W 75S	1	17	19	192	.2	57	12	635	3.33	28	5	ND	1	16	1	2	2	69	.27	.106	8	69	.82	130	.09	7	2.08	.02	.10	1	1
B200W 100S	1	25	13	145	.1	66	16	1093	3.46	38	5	ND	1	15	1	2	2	71	.22	.122	10	65	.93	120	.09	5	2.03	.02	.13	1	2
B200W 125S	2	37	22	199	.2	89	18	878	4.58	46	5	ND	1	15	1	2	2	86	.28	.097	10	85	1.25	125	.09	6	2.47	.02	.10	1	1
B200W 150S	2	29	20	163	.1	92	15	514	3.82	30	5	ND	1	14	1	2	2	75	.26	.108	9	89	1.11	98	.09	7	2.22	.02	.07	1	1
B200W 175S	1	28	12	189	.2	87	15	884	3.91	31	5	ND	1	12	1	2	2	74	.23	.154	8	97	1.05	105	.07	3	2.31	.02	.09	1	1
B200W 200S	1	17	17	152	.1	32	9	1377	2.27	7	5	ND	1	9	1	2	2	50	.18	.168	6	40	.50	161	.09	5	1.37	.02	.06	1	3
B200W 225S	1	22	19	127	.1	40	11	1175	3.21	24	5	ND	1	13	1	2	2	69	.22	.109	7	49	.68	119	.10	5	1.70	.02	.07	1	1
B200W 250S	2	26	17	158	.1	55	14	1060	3.39	22	5	ND	1	12	1	2	2	75	.26	.097	8	57	.88	132	.11	5	2.13	.02	.09	1	2
B200W 275S	1	24	13	137	.1	53	14	1035	3.21	24	5	ND	1	12	1	2	2	76	.25	.094	6	55	.84	94	.12	6	2.20	.02	.09	1	1
B200W 300S	3	96	30	219	.6	78	46	4341	10.98	49	5	ND	1	27	1	2	3	240	.54	.072	15	76	2.55	171	.05	5	3.42	.02	.11	1	1
B200W 325S	3	30	20	157	.1	51	18	2027	4.10	27	5	ND	1	16	1	2	2	95	.31	.078	9	54	.88	130	.09	6	2.11	.02	.10	1	1
B200W 350S	1	28	8	129	.1	38	17	1511	4.14	16	5	ND	1	18	1	2	2	101	.37	.108	7	42	.79	124	.15	6	1.95	.03	.10	1	1
B200W 375S	2	48	32	144	.3	66	24	2321	5.43	46	5	ND	1	18	1	2	2	101	.41	.116	13	58	.95	122	.09	7	2.28	.02	.14	1	2

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B200W 400S	1	32	16	136	.1	65	19	1373	4.64	42	5	ND	2	19	1	2	5	90	.38	.115	9	63	1.00	134	.09	7	2.29	.02	.11	1	3
B200W 425S	1	20	16	143	.1	55	13	1329	3.22	21	5	ND	1	13	1	2	4	66	.24	.115	7	54	.74	133	.10	6	1.86	.02	.09	1	1
B200W 450S	1	27	20	144	.1	82	16	920	3.78	33	5	ND	2	13	1	3	2	77	.24	.122	8	76	.97	155	.10	6	2.21	.02	.07	1	1
B200W 475S	1	24	13	174	.1	70	15	1185	3.75	22	5	ND	2	15	1	2	2	75	.26	.113	7	70	.84	170	.12	7	2.27	.02	.08	1	4
B200W 500S	1	32	17	162	.1	102	17	990	4.12	28	5	ND	3	14	1	2	2	84	.25	.130	10	111	1.22	192	.11	7	2.41	.02	.07	1	1
B200W 525S	1	26	12	135	.1	68	14	1401	3.54	18	5	ND	1	14	1	2	2	72	.26	.104	7	77	.92	148	.09	6	2.07	.02	.09	1	1
B200W 550S	2	29	12	144	.1	76	15	1293	3.79	17	5	ND	1	13	1	3	2	77	.25	.106	8	85	1.01	132	.09	6	2.30	.02	.09	1	2
B200W 575S	1	25	14	130	.1	70	14	979	3.51	28	5	ND	2	15	1	2	2	72	.27	.120	9	74	.95	137	.09	6	2.00	.02	.08	1	1
B200W 600S	1	41	17	139	.1	97	18	994	4.33	45	5	ND	3	13	1	2	3	86	.26	.104	10	99	1.32	124	.10	6	2.36	.02	.07	1	10
B200W 625S	1	28	14	157	.1	90	16	2025	3.90	26	5	ND	2	17	1	2	2	78	.34	.140	10	93	1.09	208	.10	7	2.12	.02	.10	1	1
B200W 650S	1	34	13	133	.1	72	17	1732	3.80	19	5	ND	1	15	1	2	2	78	.28	.079	9	74	.93	146	.11	7	2.11	.02	.08	1	1
B200W 675S	1	33	10	156	.1	85	16	1108	3.89	25	5	ND	1	12	1	2	2	79	.24	.108	8	84	1.06	134	.09	6	2.20	.02	.07	1	1
B200W 700S	1	38	17	131	.2	102	17	670	4.45	27	5	ND	2	12	1	2	2	90	.26	.110	10	102	1.35	140	.08	7	2.54	.02	.07	1	2
STD C/AU-S	19	58	38	132	7.0	67	27	977	3.82	41	17	7	35	47	17	15	19	62	.46	.096	35	57	.84	172	.08	34	1.68	.07	.11	12	51
B150W 150S	1	43	20	157	.1	67	19	2064	5.98	42	5	ND	2	24	1	2	4	87	.53	.133	11	65	1.02	167	.06	5	2.22	.02	.12	1	1
B150W 175S	1	18	11	131	.1	46	12	818	3.18	17	5	ND	2	16	1	3	2	62	.27	.130	6	49	.76	102	.08	6	1.87	.02	.07	1	2
B150W 200S	1	22	20	180	.1	58	13	1503	3.52	22	5	ND	1	18	1	2	2	66	.29	.175	9	63	.86	172	.08	6	1.89	.02	.11	1	1
B150W 225S	1	20	15	121	.2	39	11	1070	3.33	18	5	ND	1	10	1	2	2	67	.13	.088	7	52	.68	104	.07	4	1.84	.02	.06	1	1
B150W 250S	1	32	29	155	.1	71	15	697	4.27	59	5	ND	2	18	1	2	2	88	.38	.138	8	75	1.15	113	.11	7	2.43	.02	.10	1	14
B150W 275S	1	19	11	137	.1	39	11	1527	3.05	12	5	ND	2	10	1	2	2	61	.19	.195	6	47	.62	134	.09	5	1.77	.02	.04	1	1
B150W 300S	1	25	17	147	.1	48	14	1260	3.74	35	5	ND	1	11	1	2	2	75	.20	.153	7	58	.88	115	.08	6	2.06	.02	.07	1	1
B150W 325S	1	36	22	151	.2	60	19	1900	4.88	39	5	ND	1	19	1	2	2	111	.48	.096	7	65	1.19	187	.11	6	2.47	.02	.07	1	1
B100W 525N	1	22	18	69	.2	24	4	271	2.39	22	5	ND	3	6	1	4	2	52	.06	.031	6	36	.45	35	.06	4	1.34	.02	.05	1	1
B100W 500N	1	63	25	77	.3	27	5	220	2.17	19	5	ND	1	6	1	2	5	49	.06	.056	8	47	.57	30	.05	6	1.70	.02	.05	1	1
B100W 475N	3	81	36	206	.2	69	14	976	4.18	39	5	ND	4	7	1	2	7	76	.09	.073	14	92	1.20	48	.07	6	2.94	.02	.08	1	3
B100W 450N	5	160	34	173	.1	71	14	1154	4.41	45	5	ND	4	11	1	2	7	80	.16	.107	11	87	1.24	97	.06	4	2.16	.02	.09	4	1
B100W 425N	3	73	25	172	.1	103	16	956	4.76	44	5	ND	2	8	1	2	4	91	.12	.082	10	117	1.52	66	.07	5	2.95	.02	.08	1	3
B100W 400N	3	73	40	266	.2	138	17	510	5.78	60	5	ND	2	9	1	2	6	111	.12	.070	11	158	1.96	66	.08	6	3.14	.02	.08	1	1
B100W 375N	3	42	18	134	.3	110	16	357	4.46	43	5	ND	2	15	1	4	3	104	.25	.053	8	117	1.46	71	.15	7	2.72	.02	.08	3	2
B100W 350N	1	38	19	131	.1	86	14	354	4.14	44	5	ND	2	13	1	2	6	98	.20	.043	8	104	1.38	63	.15	6	2.23	.02	.09	1	6
B100W 325N	3	44	14	122	.2	96	16	494	4.45	30	5	ND	2	11	1	2	3	94	.16	.042	7	102	1.35	57	.13	5	2.31	.02	.08	1	18
B100W 300N	1	48	24	138	.1	104	14	408	4.20	35	5	ND	2	11	1	2	4	93	.18	.048	8	110	1.39	70	.14	6	2.50	.02	.08	1	1
B100W 275N	2	41	23	113	1.1	84	14	890	3.79	18	5	ND	2	23	1	2	4	83	.30	.066	8	86	1.01	105	.10	6	1.76	.02	.10	1	2

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B100W 250N	5	62	23	134	.5	100	12	515	3.80	28	5	ND	1	20	1	2	2	89	.30	.067	9	96	1.24	134	.09	4	2.20	.02	.07	1	1
B100W 75N	1	56	24	143	.3	147	14	437	3.83	43	5	ND	1	12	1	2	2	80	.17	.061	9	132	1.49	79	.11	3	2.65	.02	.09	1	1
STD C/AU-S	21	60	39	136	7.2	73	30	1059	4.01	41	14	8	38	51	18	15	19	68	.49	.107	37	58	.89	177	.09	34	1.75	.07	.15	15	48
B100W 50N	1	31	18	122	.1	78	11	496	3.12	18	5	ND	1	12	1	2	2	71	.17	.057	7	86	.98	74	.13	3	1.98	.02	.06	1	1
B100W 25N	1	57	38	136	.1	87	15	1359	3.68	32	5	ND	3	21	1	2	2	81	.28	.088	11	88	1.20	198	.12	2	2.28	.03	.09	1	1
B100W 0 N	1	18	25	98	.1	84	12	955	2.46	17	5	ND	1	25	1	2	2	58	.29	.051	7	72	.73	132	.11	3	1.55	.03	.09	1	17
B100W 25S	1	26	25	131	.1	122	16	2010	2.58	20	5	ND	1	30	1	2	2	57	.39	.075	7	102	1.06	273	.10	3	1.62	.03	.11	1	1
B100W 50S	1	26	17	118	.1	115	12	467	2.64	20	5	ND	1	17	1	2	2	56	.22	.092	6	99	.93	117	.10	2	1.70	.02	.08	1	1
B100W 75S	1	21	18	129	.1	118	12	514	3.21	48	5	ND	1	17	1	2	2	65	.26	.088	7	120	1.12	100	.08	2	1.85	.02	.06	1	1
B100W 100S	1	20	15	158	.3	102	12	712	3.13	38	5	ND	1	13	1	3	2	64	.17	.130	8	119	1.09	106	.09	3	2.02	.02	.07	1	1
B100W 125S	1	21	18	121	.1	94	13	1002	3.13	35	5	ND	1	10	1	2	2	64	.13	.076	7	96	.93	100	.07	4	2.03	.02	.07	1	1
B100W 150S	1	23	25	156	.2	54	12	1562	3.24	28	5	ND	1	11	1	2	2	66	.13	.088	9	65	.76	114	.07	3	2.15	.02	.08	1	2
B100W 175S	1	26	14	180	.1	64	14	869	3.55	41	5	ND	1	14	1	2	4	71	.20	.110	10	66	.89	136	.11	4	2.41	.02	.07	1	1
B100W 200S	1	67	21	167	.1	83	27	1034	7.35	61	5	ND	3	13	1	2	2	171	.21	.101	10	85	1.89	154	.07	4	3.35	.02	.10	1	4
B100W 225S	1	22	11	160	.1	50	14	1858	3.38	16	5	ND	1	26	1	2	2	67	.41	.202	8	54	.78	277	.08	3	1.85	.02	.16	1	1
B100W 250S	1	25	21	159	.1	59	14	1637	3.72	21	5	ND	1	15	1	2	2	71	.26	.169	8	63	.88	140	.08	3	2.16	.02	.13	1	4
B100W 275S	1	23	16	152	.1	86	16	1019	3.74	26	5	ND	2	14	1	2	2	80	.24	.092	9	85	.99	127	.09	4	2.36	.02	.07	1	3
B100W 300S	2	30	22	167	.2	66	17	1809	4.23	42	5	ND	2	17	1	2	2	87	.32	.123	10	71	.95	180	.09	3	2.19	.02	.13	1	20
B100W 325S	1	22	12	156	.1	45	13	1594	3.33	19	5	ND	1	19	1	2	2	72	.30	.146	8	47	.68	163	.06	4	1.96	.02	.09	1	3
B100W 350S	2	36	18	164	.2	110	19	1779	4.17	33	5	ND	1	16	1	2	2	85	.32	.169	10	102	1.24	203	.10	4	2.42	.02	.13	1	1
B100W 375S	4	94	22	178	.1	246	37	1939	7.22	65	5	ND	3	18	1	3	2	123	.31	.105	24	222	2.86	160	.07	5	3.29	.02	.11	1	1
B100W 400S	1	28	13	171	.1	94	17	1544	3.64	21	5	ND	1	20	1	2	2	74	.36	.267	8	92	1.04	222	.10	5	2.24	.02	.13	1	1
B100W 425S	2	31	15	184	.1	81	18	2272	3.88	20	5	ND	1	17	1	2	2	79	.34	.184	9	82	1.00	246	.09	4	2.19	.02	.13	1	1
B100W 450S	1	39	10	126	.1	56	18	2679	3.67	12	5	ND	2	21	1	2	2	79	.38	.117	7	63	.87	231	.11	4	2.00	.02	.11	1	1
B100W 475S	2	39	16	157	.2	89	18	1448	4.16	29	5	ND	2	22	1	2	2	86	.39	.168	10	92	1.17	155	.09	4	2.40	.02	.11	1	1
B100W 500S	1	15	18	107	.1	134	14	1057	3.22	59	5	ND	1	17	1	2	2	63	.19	.083	6	128	.69	130	.09	2	1.54	.02	.07	1	1
B100W 525S	1	34	32	212	.1	79	14	840	4.24	69	5	ND	1	16	1	2	2	78	.18	.083	12	74	1.15	131	.07	2	2.46	.02	.12	1	1
B100W 550S	1	18	18	158	.1	55	13	614	3.11	34	5	ND	2	11	1	2	2	65	.16	.067	9	56	.81	110	.10	3	2.08	.02	.09	1	1
B100W 575S	1	22	10	138	.1	41	13	1028	3.38	18	5	ND	1	11	1	2	2	72	.19	.149	7	55	.75	120	.07	2	2.05	.02	.06	1	2
B100W 600S	1	42	22	148	.1	72	20	1138	4.93	51	5	ND	1	16	1	2	2	111	.32	.129	9	71	1.27	139	.13	3	2.53	.02	.11	1	1
B100W 625S	1	41	22	164	.1	80	20	1211	5.04	47	5	ND	1	16	1	2	3	108	.32	.158	11	84	1.33	175	.10	3	2.60	.02	.10	1	1
B100W 650S	1	31	20	190	.1	54	17	2342	4.16	31	5	ND	1	18	1	2	2	81	.31	.233	10	60	.87	196	.07	3	2.26	.03	.14	1	2
B100W 675S	2	73	62	251	.2	68	24	3209	6.35	48	5	ND	2	26	2	2	2	104	.63	.144	11	59	1.03	192	.08	3	2.42	.02	.14	1	1
B100W 700S	1	33	22	164	.1	76	19	2163	4.31	28	5	ND	1	26	1	2	2	83	.44	.119	11	69	.91	199	.09	3	2.06	.02	.12	1	3
B50W 150S	1	21	15	165	.1	64	14	1234	3.47	16	5	ND	1	14	1	2	2	73	.26	.166	8	61	.83	161	.11	4	2.03	.02	.09	1	2
B50W 175S	2	39	19	182	.2	96	19	2016	4.24	33	5	ND	2	17	1	2	2	84	.30	.149	10	86	1.08	214	.09	4	2.35	.02	.14	1	1
B50W 200S	1	26	17	168	.1	80	17	2152	3.58	21	5	ND	1	21	2	2	2	74	.37	.129	8	75	.90	285	.11	4	2.10	.02	.10	1	7

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B50W 225S	1	27	17	140	.1	63	13	897	3.97	35	5	ND	1	13	1	2	2	70	.23	.158	8	71	1.02	113	.05	2	2.10	.02	.08	1	2
B50W 250S	1	21	16	155	.1	51	11	1113	3.20	17	5	ND	1	11	1	2	2	59	.20	.142	7	56	.77	123	.06	5	1.95	.02	.07	1	1
B50W 275S	1	22	22	151	.3	64	13	1064	3.42	23	5	ND	2	11	1	2	2	65	.21	.097	8	65	.87	149	.09	3	2.05	.02	.06	1	4
B50W 300S	1	24	15	148	.1	64	14	1501	3.81	19	5	ND	1	13	1	2	2	71	.24	.156	7	71	.94	162	.07	2	2.14	.02	.09	1	2
B50W 325S	1	16	16	106	.1	32	11	1619	2.90	14	5	ND	1	12	1	2	2	61	.23	.092	5	44	.54	139	.05	2	1.67	.02	.05	1	1
B50W 350S	4	85	41	192	.4	144	29	1735	7.03	103	5	ND	3	15	1	2	2	99	.24	.098	24	116	1.83	135	.06	2	2.89	.02	.12	1	3
B50W 375S	2	26	17	148	.1	53	14	1030	3.88	30	5	ND	2	16	1	2	2	76	.33	.184	7	63	.89	144	.08	2	2.21	.02	.07	1	4
B50W 400S	1	27	13	137	.1	44	17	2184	4.28	21	5	ND	1	18	1	2	2	89	.34	.157	7	50	.89	190	.08	3	2.05	.02	.09	1	1
B50W 425S	1	30	23	154	.1	48	15	1544	3.95	34	5	ND	1	19	1	2	2	79	.42	.118	8	54	.85	171	.06	4	2.10	.02	.10	1	1
B50W 450S	1	21	15	149	.1	42	14	1614	3.68	20	5	ND	1	19	1	2	2	68	.37	.180	7	48	.76	180	.06	4	1.87	.02	.12	1	1
B50W 475S	1	37	28	173	.1	71	20	1195	5.03	55	5	ND	2	14	1	2	2	94	.33	.119	10	71	1.19	148	.07	3	2.53	.02	.14	1	1
B50W 500S	2	28	19	169	.2	64	17	1814	4.11	30	5	ND	2	16	1	2	2	78	.35	.206	9	66	.92	191	.09	3	2.18	.02	.11	1	1
B00 200N	2	44	23	109	.3	57	9	440	4.08	27	5	ND	1	12	1	3	4	88	.17	.060	7	79	1.04	77	.09	3	2.09	.02	.05	5	1
B00 175N	2	71	25	145	.6	82	12	531	4.90	26	6	ND	2	9	1	2	3	97	.14	.082	9	115	1.43	67	.08	2	3.05	.02	.06	3	1
B00 150N	1	24	21	74	.3	36	5	215	2.42	20	5	ND	1	7	1	2	2	59	.09	.052	6	65	.61	53	.06	2	1.57	.02	.03	2	3
B00 125N	1	27	22	90	.6	37	6	220	2.93	13	5	ND	1	8	1	2	2	58	.10	.051	7	63	.67	48	.05	2	1.96	.02	.04	1	1
B00 100N	2	74	32	148	.6	151	15	536	4.62	53	5	ND	2	15	1	2	9	88	.20	.057	8	162	1.92	62	.09	2	3.16	.02	.04	2	1
STD C/AU-S	21	60	40	141	7.1	70	29	1040	4.18	42	16	7	36	49	18	16	22	65	.50	.102	37	62	.92	186	.08	36	1.83	.07	.11	13	50
B00 75N	2	56	23	151	.5	157	15	610	4.66	55	5	ND	1	10	1	2	2	84	.15	.056	9	159	1.85	80	.10	4	2.78	.02	.06	1	1
B00 50N	1	19	22	114	.2	57	8	318	3.00	19	5	ND	2	19	1	2	2	67	.23	.053	6	68	.81	139	.10	2	1.88	.02	.05	1	1
B00 25N	2	59	47	150	.1	172	16	864	4.73	73	5	ND	1	11	1	2	2	84	.11	.060	11	143	1.84	145	.06	4	3.24	.02	.06	2	1
B00 0 N	1	30	25	130	.3	75	12	344	3.69	27	5	ND	1	11	1	2	2	78	.21	.064	8	87	1.18	74	.12	3	2.31	.02	.05	1	2
B00 25S	1	79	23	102	.1	214	21	370	4.26	46	5	ND	3	14	1	2	2	83	.25	.042	8	129	1.75	60	.14	3	2.75	.02	.06	1	1
B00 50S	4	102	159	251	.1	158	23	2255	4.22	32	5	ND	2	40	1	2	2	32	.60	.111	7	158	1.16	260	.02	2	1.57	.02	.09	1	1
B00 75S	1	21	23	94	.1	63	13	1552	2.90	16	5	ND	1	43	1	2	2	39	.48	.095	6	45	.69	289	.04	3	1.60	.02	.12	1	1
B00 100S	1	27	19	150	.1	124	13	581	3.26	24	5	ND	2	11	1	2	2	58	.17	.102	7	122	1.20	105	.08	3	2.17	.02	.07	1	1
B00 125S	1	25	28	139	.1	170	16	697	3.61	55	6	ND	2	11	1	2	2	64	.16	.093	7	158	1.30	126	.07	3	2.37	.02	.05	1	1
B00 150S	1	21	52	196	.3	82	11	1268	2.95	41	5	ND	1	10	1	2	2	54	.13	.078	8	95	.91	111	.06	3	2.36	.02	.04	1	1
B00 175S	1	23	18	132	.1	72	11	706	3.22	34	5	ND	1	13	1	2	2	56	.16	.132	7	81	1.07	111	.05	2	2.03	.02	.06	1	1
B00 200S	1	16	21	166	.4	90	11	793	3.13	39	5	ND	1	12	1	2	2	57	.13	.068	6	90	.82	140	.06	2	1.72	.02	.05	1	1
B00 225S	1	30	31	194	.1	77	16	1112	4.48	60	5	ND	1	15	1	2	2	80	.22	.092	11	79	1.16	118	.08	3	2.50	.02	.08	1	4
B00 250S	1	20	12	152	.1	42	12	1962	3.28	20	5	ND	1	18	1	2	2	57	.33	.163	6	47	.71	170	.04	2	1.81	.02	.09	1	1
B00 275S	1	22	15	161	.2	65	14	1169	3.73	28	5	ND	1	17	1	2	2	69	.29	.173	8	64	.96	148	.07	3	2.15	.02	.09	1	1
B00 300S	1	16	16	132	.2	50	12	919	3.32	19	5	ND	2	11	1	3	2	63	.20	.161	6	59	.76	137	.08	5	1.95	.02	.08	2	1
B00 325S	1	27	19	149	.2	76	15	979	3.90	28	8	ND	2	14	1	2	2	69	.30	.187	8	72	1.06	143	.07	6	2.32	.02	.08	1	1
B00 350S	2	29	17	141	.2	57	14	1161	3.81	29	5	ND	1	15	1	2	2	70	.23	.098	9	67	.88	145	.04	3	2.19	.02	.06	1	9
B00 375S	1	30	16	154	.1	51	16	1766	4.19	27	5	ND	2	17	1	2	2	76	.31	.177	9	55	.87	200	.06	9	2.16	.02	.09	1	1

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B00 400S	1	37	20	163	.2	62	18	1118	4.65	45	5	ND	1	14	1	2	2	97	.26	.092	12	65	1.10	140	.09	2	2.64	.02	.08	1	2
B00 425S	1	21	7	143	.1	46	14	1094	3.63	18	5	ND	1	14	1	2	2	74	.26	.139	7	51	.78	139	.09	3	2.12	.02	.08	1	1
B00 450S	2	28	12	139	.1	55	16	1005	4.09	30	5	ND	1	14	1	3	3	88	.30	.094	7	55	.96	173	.08	3	2.14	.02	.11	1	1
B00 475S	2	47	23	142	.1	70	17	863	4.70	46	5	ND	1	12	1	2	3	93	.26	.092	9	44	1.13	124	.08	3	2.49	.02	.12	1	3
B00 500S	1	33	19	133	.1	64	19	1487	4.29	26	5	ND	1	16	1	2	2	89	.33	.074	8	60	.98	146	.10	2	2.32	.02	.12	1	1
B00 525S	2	55	34	194	.1	108	25	1614	6.08	75	5	ND	1	13	1	2	3	110	.30	.124	13	97	1.47	161	.09	5	2.88	.02	.15	1	1
B00 550S	1	24	11	159	.1	62	16	1887	3.54	16	5	ND	1	20	1	2	3	68	.38	.163	7	60	.79	178	.09	4	1.81	.02	.13	1	1
B00 575S	1	26	17	184	.2	87	19	1818	4.19	17	5	ND	1	16	1	2	2	82	.28	.119	7	81	.95	208	.10	4	2.14	.02	.13	1	1
STD C/AU-S	20	57	36	137	6.8	70	29	1010	3.94	37	17	7	35	48	18	15	21	64	.48	.100	36	55	.91	172	.09	37	1.73	.07	.13	12	52
B00 600S	2	35	11	149	.1	113	19	1270	4.11	30	5	ND	1	15	1	2	2	86	.28	.085	8	94	1.16	158	.11	4	2.32	.02	.10	1	1
B00 625S	1	25	16	145	.1	74	16	1883	3.56	19	5	ND	1	19	1	2	2	72	.34	.170	8	72	.89	202	.10	3	1.96	.02	.10	1	2
B00 650S	2	42	19	170	.1	109	21	1942	4.50	29	5	ND	1	18	2	2	2	89	.36	.135	11	102	1.35	203	.09	4	2.38	.02	.14	1	1
B50E 300N	1	21	12	111	.1	118	17	904	3.51	9	5	ND	1	13	1	2	2	71	.23	.109	6	89	1.18	204	.08	6	2.38	.02	.09	1	2
B50E 250N	3	13	19	36	.1	23	3	140	2.08	16	5	ND	1	7	1	2	5	73	.09	.031	8	57	.48	41	.14	2	1.30	.02	.04	3	1
B50E 225N	2	12	11	32	.1	19	3	146	2.17	13	5	ND	1	7	1	3	5	69	.08	.040	5	40	.37	34	.10	2	.99	.02	.03	2	1
B50E 175N	2	48	19	112	.1	80	11	374	4.74	33	5	ND	1	8	1	2	3	97	.13	.049	9	101	1.33	76	.13	2	2.43	.02	.06	1	2
B50E 150N	2	80	20	114	.2	98	13	470	4.76	43	5	ND	1	8	1	2	2	93	.17	.133	11	117	1.59	50	.11	3	3.46	.02	.10	1	3
B50E 100N	1	15	17	27	.1	13	3	101	1.91	11	5	ND	1	8	1	2	3	47	.12	.055	6	32	.29	29	.09	2	1.33	.02	.03	1	12
B50E 75N	1	47	37	81	.4	61	15	1061	3.85	51	5	ND	2	20	1	2	2	43	.28	.075	17	56	1.15	109	.04	3	1.47	.02	.14	1	1
B50E 50N	1	36	41	97	.3	60	13	1857	2.75	35	5	ND	1	41	1	2	4	24	.43	.131	9	52	.63	158	.02	4	1.09	.02	.14	1	2
B50E 25N	1	31	27	122	.1	80	12	1238	3.48	27	5	ND	1	11	1	2	4	66	.16	.120	7	105	1.02	125	.07	2	1.96	.02	.07	1	1
B50E 0 N	2	65	34	133	.1	770	50	1514	5.24	196	5	ND	1	24	1	7	5	58	.19	.075	10	468	3.10	111	.05	4	2.48	.02	.09	1	7
B50E 25S	1	45	32	140	.1	189	18	1176	3.95	46	5	ND	1	19	1	2	2	67	.21	.088	10	157	1.49	192	.06	3	2.31	.02	.10	1	1
B50E 50S	1	48	24	108	.1	177	18	413	3.91	51	5	ND	1	19	1	2	5	78	.24	.061	8	131	1.53	91	.12	4	2.41	.02	.07	1	1
B50E 75S	1	32	18	117	.1	131	14	430	3.09	24	5	ND	1	23	1	3	2	41	.26	.069	7	107	1.17	132	.11	3	1.80	.02	.09	1	2
B50E 100S	2	73	60	178	.1	164	19	745	3.99	44	5	ND	2	16	1	2	2	44	.19	.081	9	138	1.45	138	.07	3	2.30	.02	.09	1	1
B50E 125S	1	17	20	121	.1	96	12	988	2.51	19	5	ND	1	21	1	3	2	52	.27	.131	6	94	.93	163	.11	4	1.69	.03	.08	1	1
B50E 150S	2	13	18	97	.1	84	11	1055	2.16	11	5	ND	1	17	1	2	2	47	.21	.103	5	75	.69	117	.09	2	1.43	.02	.06	1	1
B50E 175S	1	21	49	182	.1	146	15	947	3.09	89	5	ND	1	19	1	2	2	57	.21	.100	6	145	1.07	168	.06	2	1.88	.02	.07	1	1
B50E 200S	1	17	21	112	.1	81	10	451	2.94	31	5	ND	1	15	1	2	2	56	.16	.101	6	92	.82	99	.07	2	1.93	.02	.05	1	2
B50E 225S	1	20	20	143	.1	94	12	1071	3.21	30	5	ND	1	12	1	2	2	62	.16	.152	7	109	1.01	148	.05	2	2.19	.02	.06	1	1
B50E 250S	1	26	31	122	.2	80	11	818	2.96	39	5	ND	1	12	1	2	2	55	.20	.065	6	73	.79	84	.05	3	2.15	.02	.07	1	1
B50E 275S	1	25	25	179	.1	80	15	1305	3.73	48	5	ND	1	17	1	2	2	68	.23	.108	8	72	.95	159	.08	2	2.01	.02	.12	1	2
B50E 300S	1	15	16	113	.1	55	12	1230	2.79	14	5	ND	1	14	1	2	2	55	.22	.122	6	55	.66	143	.08	2	1.59	.02	.09	1	1
B50E 325S	2	16	14	124	.2	46	12	1451	3.08	11	5	ND	1	17	1	2	2	62	.29	.184	6	57	.67	213	.09	3	1.76	.02	.10	1	2

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B50E 350S	1	22	18	135	.1	74	14	1112	3.46	19	5	ND	1	17	1	2	2	69	.25	.112	8	79	.90	148	.07	3	2.05	.02	.11	1	7
B50E 375S	1	15	6	124	.1	44	12	1774	2.88	9	5	ND	1	14	1	3	3	62	.23	.110	5	53	.65	197	.09	2	1.71	.02	.06	1	1
B50E 400S	1	19	12	127	.1	45	13	994	3.24	10	5	ND	1	11	1	2	4	72	.18	.097	6	64	.71	135	.09	3	1.96	.02	.06	1	1
B50E 425S	1	22	13	144	.1	53	15	1544	3.40	24	5	ND	1	21	1	2	2	76	.36	.135	7	40	.80	176	.07	2	2.02	.02	.08	1	2
B50E 450S	1	34	16	138	.1	55	22	3086	4.72	23	5	ND	1	19	1	2	2	100	.31	.188	10	58	.99	215	.09	3	2.36	.02	.13	1	2
B50E 475S	1	29	17	130	.1	49	19	1766	4.45	20	5	ND	1	17	1	2	2	92	.32	.141	7	46	.79	166	.10	2	1.96	.02	.10	1	1
B50E 500S	1	26	10	134	.3	58	18	1473	4.40	27	5	ND	1	16	1	2	2	92	.32	.148	8	53	.88	129	.11	3	2.20	.02	.11	1	4
B100E 150N	1	68	22	116	.1	128	19	670	4.48	39	5	ND	2	8	1	2	2	93	.17	.068	11	143	1.88	48	.15	3	3.15	.02	.06	3	4
B100E 125N	1	13	8	58	.2	31	5	183	1.88	5	5	ND	1	10	1	2	2	54	.13	.029	5	43	.45	54	.11	2	1.23	.02	.03	1	1
B100E 100N	1	17	16	40	.2	28	4	186	1.81	12	5	ND	1	7	1	2	2	50	.08	.063	6	59	.41	50	.05	2	1.49	.02	.02	3	1
STD C/AU-S	19	57	39	134	7.0	72	29	1021	3.79	39	16	7	36	48	17	16	20	66	.45	.099	35	60	.83	175	.09	36	1.69	.07	.12	14	49
B100E 75N	1	34	27	94	.2	57	13	1166	3.98	32	5	ND	2	15	1	2	2	45	.13	.106	14	67	.89	88	.02	2	1.93	.02	.09	1	1
B100E 50N	3	295	16	52	1.0	78	12	812	2.42	125	5	ND	3	26	1	7	2	11	.15	.069	21	36	.71	101	.01	3	1.26	.01	.14	1	4
B100E 25N	1	74	53	178	.1	187	24	1183	4.78	98	5	ND	3	19	1	2	2	92	.26	.124	12	174	2.07	136	.11	4	2.85	.02	.09	2	8
B100E 0 N	1	33	16	78	.2	68	9	545	2.71	24	5	ND	1	18	1	3	2	58	.21	.084	8	87	.83	91	.07	2	1.82	.02	.04	1	1
B100E 25S	1	51	29	145	.2	218	23	1267	4.53	100	5	ND	2	20	1	2	2	83	.24	.086	10	201	1.85	147	.09	4	2.76	.02	.11	1	2
B100E 50S	1	32	26	122	.2	115	16	1260	3.30	22	5	ND	2	23	1	2	2	63	.26	.112	7	107	1.11	309	.07	3	2.14	.02	.09	1	1
B100E 75S	1	33	40	135	.1	204	21	1267	4.28	27	5	ND	1	33	1	2	2	55	.32	.098	10	161	1.49	343	.04	3	2.15	.02	.09	1	5
B100E 100S	1	92	54	146	.2	542	38	1212	6.30	64	5	ND	5	18	1	2	2	114	.14	.032	13	423	3.20	139	.07	3	3.25	.02	.08	1	6
B100E 150S	1	76	21	54	.1	59	7	307	1.79	27	5	ND	2	15	1	4	2	14	.12	.043	13	32	.48	80	.01	2	1.07	.01	.11	1	1
B100E 175S	1	74	365	390	.2	124	23	3298	3.91	33	5	ND	2	76	3	2	2	62	.50	.129	13	114	1.68	311	.03	3	2.23	.02	.12	1	2
B100E 200S	1	34	24	121	.1	175	15	875	3.20	40	5	ND	2	16	1	2	2	63	.22	.108	9	158	1.29	119	.08	2	2.05	.02	.07	1	1
B100E 225S	1	32	112	225	.3	257	21	893	3.95	154	5	ND	2	14	1	2	2	69	.13	.098	8	256	1.51	158	.04	2	2.33	.02	.05	1	2
B100E 250S	1	21	13	123	.2	60	11	704	3.39	22	5	ND	1	9	1	2	2	69	.13	.080	6	75	.81	89	.07	2	2.33	.02	.04	1	1
B100E 275S	1	29	16	144	.2	116	16	1219	3.85	42	5	ND	1	10	1	2	2	72	.11	.080	9	121	.92	99	.07	3	2.38	.02	.06	1	2
B100E 300S	2	27	27	254	.1	52	12	1817	3.68	27	5	ND	2	14	1	2	2	72	.20	.193	6	58	.73	188	.07	5	2.14	.02	.09	1	1
B100E 325S	2	41	31	187	.1	148	18	1367	4.24	42	5	ND	1	15	1	2	2	73	.21	.103	9	118	1.11	158	.07	3	2.31	.02	.11	1	16
B100E 350S	1	27	19	183	.2	59	15	2198	3.57	16	5	ND	1	26	1	2	2	71	.35	.200	8	61	.77	270	.06	2	1.95	.02	.09	1	1
B100E 375S	1	33	20	203	.1	110	19	1210	4.32	35	5	ND	2	17	1	2	2	83	.29	.177	11	107	1.25	218	.08	3	2.49	.02	.10	1	1
B100E 400S	2	36	15	169	.1	93	17	1260	4.05	27	5	ND	1	18	1	2	2	81	.29	.140	9	84	1.07	199	.08	3	2.44	.02	.09	1	2
B100E 425S	3	31	13	234	.2	60	17	2057	4.14	19	5	ND	1	14	3	2	2	79	.24	.236	8	68	.88	184	.07	3	2.23	.02	.09	1	1
B100E 450S	2	32	15	148	.1	57	16	1656	4.05	23	5	ND	1	15	1	2	2	83	.23	.137	9	62	.83	179	.07	2	2.23	.02	.10	1	1
B100E 475S	3	50	18	143	.2	92	36	2343	8.57	57	5	ND	2	18	1	4	2	124	.30	.173	14	62	1.38	182	.05	5	2.76	.02	.14	2	1
B100E 500S	3	62	17	161	.3	84	37	2944	7.94	43	5	ND	3	16	1	2	2	144	.32	.151	15	65	1.26	158	.07	2	2.92	.02	.12	1	2
B100E 525S	2	50	13	153	.3	62	25	2501	5.36	33	5	ND	2	23	1	2	2	103	.37	.163	13	55	1.02	176	.07	3	2.62	.02	.13	1	1
B100E 550S	1	35	17	166	.2	59	20	1676	4.46	21	5	ND	2	17	1	2	2	94	.29	.202	9	60	.91	145	.10	3	2.29	.03	.11	1	1
B100E 575S	2	45	22	165	.1	74	21	1786	5.02	37	5	ND	2	15	1	2	2	104	.27	.150	10	73	1.09	167	.10	8	2.50	.02	.14	1	1

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B100E 600S	3	51	21	173	.1	79	24	1570	8.08	39	5	ND	2	13	1	2	2	108	.27	.093	15	72	1.09	108	.05	2	2.30	.02	.11	1	1
B100E 625S	2	45	14	193	.1	54	21	2824	5.61	25	5	ND	2	31	1	2	2	95	.51	.166	12	53	.97	214	.09	4	2.09	.02	.14	1	2
B100E 650S	3	50	9	138	.1	162	24	1092	5.18	31	5	ND	2	18	1	2	2	111	.33	.078	11	177	1.89	143	.09	2	2.65	.02	.09	1	1
B150E 225N	4	25	10	71	.2	50	8	248	3.76	21	5	ND	1	10	1	2	2	86	.15	.064	5	78	.83	37	.12	2	1.72	.02	.04	1	1
B150E 200N	3	21	9	66	.2	54	7	203	3.41	18	5	ND	1	9	1	2	2	74	.13	.045	6	78	.78	53	.11	2	1.88	.02	.04	1	1
B150E 175N	1	13	15	29	.1	18	3	95	1.31	4	5	ND	1	7	1	2	2	43	.08	.028	6	44	.34	36	.08	5	1.34	.02	.02	1	1
B150E 150N	2	20	16	68	.1	43	7	306	2.81	15	5	ND	1	8	1	2	2	71	.13	.041	6	65	.72	67	.12	2	1.55	.02	.04	1	1
B150E 125N	1	47	24	113	.1	157	20	589	4.43	34	5	ND	2	14	1	2	2	90	.25	.060	9	138	2.07	93	.16	4	2.59	.02	.08	1	2
B150E 100N	1	32	15	95	.3	62	13	643	3.70	20	5	ND	1	8	1	2	2	72	.14	.064	8	92	1.08	57	.09	3	2.49	.02	.05	1	1
B150E 75N	1	83	38	96	.2	126	24	1722	4.40	51	5	ND	3	34	1	2	2	56	.32	.107	13	114	1.88	100	.01	2	2.01	.02	.10	1	5
B150E 50N	1	44	22	75	.1	91	15	1445	3.46	73	5	ND	1	26	1	2	2	29	.30	.113	13	93	.83	136	.01	2	1.42	.02	.10	1	3
B150E 25N	2	80	35	125	.1	159	20	1393	4.24	102	5	ND	2	17	1	2	2	70	.19	.096	11	141	1.63	116	.06	2	2.26	.02	.11	1	4
B150E 0 N	1	22	60	120	.1	28	8	1033	2.21	37	5	ND	1	28	1	2	2	25	.32	.120	7	29	.39	114	.02	2	.88	.02	.09	1	2
B200E 175N	1	38	11	113	.2	113	14	310	4.06	26	5	ND	2	9	1	2	2	83	.17	.055	7	114	1.43	62	.14	3	2.63	.02	.06	1	1
B200E 150N	2	103	25	136	.1	169	23	567	5.21	53	5	ND	3	11	1	2	2	110	.23	.041	10	156	2.27	79	.16	4	3.22	.03	.07	2	2
B200E 125N	1	31	2	114	.1	1685	144	2891	7.00	14	5	ND	2	8	1	2	6	53	.11	.039	7	811	17.80	50	.03	18	2.23	.01	.02	1	1
B200E 100N	2	69	28	118	.2	213	26	798	4.97	58	5	ND	3	17	1	2	2	103	.55	.031	13	203	2.98	95	.23	6	2.69	.03	.06	1	2
B200E 75N	2	49	14	118	.1	191	22	952	4.40	21	5	ND	2	32	1	2	2	99	.88	.066	8	167	3.62	87	.29	8	2.10	.03	.08	1	2
B200E 50N	1	35	8	72	.1	1493	87	1161	5.85	23	8	ND	1	9	1	2	4	53	.13	.043	4	622	19.88	40	.03	59	1.58	.01	.05	1	1
B200E 25N	1	31	14	82	.2	42	8	431	2.55	24	5	ND	1	22	1	2	2	53	.23	.118	6	50	.62	81	.08	2	1.48	.03	.05	1	1
B200E 0 N	1	20	15	87	.1	54	8	486	2.78	48	5	ND	1	25	1	2	2	31	.25	.197	7	61	.60	107	.02	2	1.81	.02	.08	1	1
B200E 25S	1	50	12	71	.1	24	7	489	2.31	21	5	ND	2	20	1	2	2	19	.22	.080	10	24	.44	66	.01	2	.79	.02	.11	1	41
B200E 50S	2	74	179	253	1.4	1270	79	2385	6.56	775	5	ND	3	247	1	27	2	80	.86	.075	12	709	7.44	71	.01	2	3.75	.01	.04	1	13
B200E 75S	1	45	38	109	.5	237	20	1648	3.57	185	5	ND	3	34	1	3	2	27	.26	.072	15	203	1.36	111	.01	3	1.42	.02	.08	1	1
B200E 100S	1	23	16	108	.1	93	11	830	2.45	36	5	ND	1	19	1	2	2	45	.15	.043	5	85	.67	145	.06	2	1.36	.03	.04	1	1
B200E 125S	1	8	5	51	.1	16	4	255	1.58	8	5	ND	1	18	1	2	2	39	.17	.031	3	19	.25	65	.08	2	.75	.03	.04	1	1
B200E 150S	1	15	19	127	.2	40	10	1395	2.21	6	5	ND	1	24	1	2	2	39	.24	.051	5	40	.60	173	.04	4	1.10	.02	.07	1	1
B200E 175S	1	18	12	153	.1	218	13	843	3.53	85	5	ND	1	28	1	2	2	53	.21	.092	4	295	1.04	157	.05	2	1.84	.02	.05	1	2
B200E 200S	1	37	18	111	.1	157	13	295	3.60	29	5	ND	2	9	1	2	2	66	.14	.069	6	126	1.30	76	.09	3	2.34	.02	.06	1	1
B200E 225S	1	37	28	148	.1	411	25	648	5.02	55	5	ND	1	55	1	2	2	75	.36	.106	6	315	2.52	163	.04	2	2.83	.02	.07	1	1
B200E 250S	1	43	21	102	.1	2307	94	2011	12.18	41	5	ND	2	29	1	11	2	46	.18	.114	6	1551	6.93	138	.03	19	2.19	.01	.03	3	1
B200E 275S	1	28	17	125	.1	280	23	747	4.02	43	5	ND	2	19	1	2	2	68	.21	.080	6	235	1.32	117	.09	3	2.06	.02	.07	1	2
B200E 300S	2	30	34	162	.1	198	19	710	3.53	69	5	ND	3	20	1	2	2	63	.20	.074	9	174	1.51	143	.06	3	2.41	.02	.09	1	1
B200E 325S	1	31	17	88	.1	43	11	672	2.89	11	5	ND	2	24	1	2	2	39	.26	.094	11	36	1.13	71	.02	2	1.42	.02	.10	1	1
B200E 350S	1	25	70	130	.1	132	12	912	2.41	23	5	ND	4	28	1	2	2	36	.25	.102	20	134	1.38	110	.01	4	1.73	.02	.11	1	1
B200E 375S	3	24	20	147	.3	77	15	1681	3.07	20	5	ND	1	35	1	2	2	59	.44	.095	7	71	.78	260	.05	5	1.65	.02	.12	1	2
STD C/AU-S	20	59	37	137	6.9	69	28	1014	3.97	38	16	7	34	48	18	16	18	65	.46	.099	36	59	.88	182	.08	37	1.65	.07	.13	13	51

SHANGRI-LA MINERALS FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B200E 400S	3	46	14	170	.1	147	19	816	4.77	39	5	ND	1	16	1	2	2	88	.29	.109	10	140	1.46	177	.04	2	2.59	.01	.12	1	4
B200E 425S	4	46	20	176	.1	247	28	1376	5.18	50	5	ND	2	24	1	2	2	90	.36	.143	16	226	2.00	219	.04	2	2.74	.01	.17	1	3
B200E 450S	1	32	21	162	.1	110	20	1801	3.88	31	5	ND	1	35	1	2	2	68	.42	.180	9	109	1.12	421	.04	2	2.08	.01	.17	1	1
B200E 475S	2	47	26	202	.1	97	24	1802	5.05	30	5	ND	3	28	1	2	2	83	.30	.163	20	85	1.09	322	.02	2	2.49	.01	.19	1	1
B200E 500S	4	95	15	201	.3	146	34	2065	7.81	52	5	ND	3	29	1	2	2	102	.45	.177	15	118	1.54	222	.02	2	2.89	.01	.20	1	1
B200E 525S	6	67	28	207	.1	210	29	1755	5.35	74	5	ND	4	30	1	2	2	84	.38	.138	18	179	1.68	269	.02	2	2.68	.01	.19	1	1
B200E 550S	1	23	22	148	.1	60	15	1684	3.11	16	5	ND	1	35	1	2	2	54	.40	.109	8	59	.82	320	.04	2	1.88	.01	.19	1	1
B200E 575S	2	32	14	141	.1	48	17	2414	3.73	12	5	ND	1	36	1	2	2	68	.56	.155	8	45	.76	338	.06	2	1.79	.01	.17	1	1
B200E 600S	3	72	8	137	.1	90	34	2258	7.72	11	5	ND	1	49	1	2	2	170	1.85	.145	12	98	2.49	189	.13	5	2.94	.01	.10	1	1
B200E 625S	3	58	18	189	.1	83	29	2177	6.51	27	5	ND	2	23	1	2	2	131	.55	.163	11	80	1.28	220	.08	3	3.08	.01	.13	1	2
B200E 650S	2	55	9	152	.1	59	36	2286	9.84	2	5	ND	3	40	1	2	2	197	1.34	.190	18	61	2.90	158	.34	6	3.38	.01	.12	1	1
B300E 250N	2	73	18	136	.1	164	17	404	4.63	36	5	ND	2	9	1	2	2	94	.15	.050	8	138	1.58	63	.12	2	2.85	.02	.08	1	2
B300E 200N	4	35	17	100	.2	70	11	737	3.63	25	5	ND	1	11	1	2	2	81	.15	.057	6	89	1.03	92	.09	2	1.79	.02	.08	1	1
B300E 175N	1	25	15	72	.2	49	7	216	2.70	16	5	ND	1	7	1	2	2	63	.11	.043	6	67	.71	56	.06	2	1.88	.02	.05	2	4
B300E 150N	2	81	29	125	.1	192	24	1158	4.62	44	5	ND	2	18	1	2	2	97	.30	.082	14	162	2.00	134	.12	2	2.75	.02	.10	4	4
B300E 125N	2	47	23	117	.1	240	29	1095	5.05	39	5	ND	1	24	1	2	2	98	.39	.117	9	215	2.64	158	.06	5	2.44	.01	.08	1	1
B300E 100N	2	38	14	97	.1	623	37	1409	4.60	18	5	ND	1	12	1	2	2	73	.18	.071	6	299	1.81	141	.08	2	2.10	.02	.04	1	1
B300E 75N	1	20	10	92	.1	71	12	416	3.13	16	5	ND	1	14	1	2	2	68	.25	.054	6	67	.94	91	.09	2	2.04	.02	.08	1	1
B300E 25N	1	23	6	137	.1	61	17	1342	4.39	7	5	ND	3	27	1	2	2	100	.47	.115	8	75	1.57	177	.19	3	2.50	.03	.10	1	2
B300E 0 N	1	27	5	56	.1	1125	67	894	4.52	8	5	ND	1	11	1	5	6	39	.21	.037	3	611	18.13	103	.06	84	1.26	.01	.02	1	5
B300E 25S	1	35	10	83	.1	697	45	1004	4.26	30	5	ND	1	18	1	3	4	59	.19	.037	8	316	8.32	91	.04	19	1.70	.01	.06	1	4
B300E 50S	1	45	14	118	.1	129	18	596	3.93	28	5	ND	2	16	1	2	2	81	.27	.057	9	111	1.53	122	.10	3	3.12	.02	.07	1	2
B300E 100S	1	53	18	95	.1	267	23	896	3.89	35	7	ND	2	21	1	2	2	63	.34	.077	11	181	3.47	106	.08	5	2.05	.02	.11	1	3
B300E 125S	1	37	19	129	.1	53	13	2279	2.62	18	5	ND	1	48	1	2	2	42	.62	.109	8	43	1.32	337	.01	3	1.49	.01	.11	1	2
B300E 150S	4	73	23	132	.2	110	12	758	2.93	35	5	ND	2	26	1	2	2	29	.24	.066	9	86	1.23	126	.01	2	1.47	.02	.10	1	1
B300E 175S	1	16	21	85	.3	19	6	660	2.14	14	5	ND	1	13	1	2	2	36	.13	.070	7	21	.37	109	.02	2	1.21	.02	.08	1	1
B300E 200S	1	29	18	96	.1	56	8	644	2.77	34	5	ND	2	21	1	2	2	50	.21	.084	8	59	.74	108	.04	2	1.46	.02	.10	1	2
B300E 225S	1	25	21	116	.1	66	8	490	2.75	33	5	ND	1	22	1	3	2	44	.31	.113	8	62	.81	109	.03	2	1.54	.01	.14	2	1
B300E 250S	1	19	27	210	.2	76	9	622	2.67	58	8	ND	1	50	1	2	2	28	.31	.077	5	48	.68	120	.01	2	1.69	.01	.11	1	1
B300E 275S	2	197	30	147	.3	1450	70	1872	6.51	232	5	ND	1	55	1	11	5	85	.27	.075	5	797	8.48	181	.01	4	3.41	.01	.07	1	2
B300E 300S	1	45	12	77	.3	562	30	1061	3.09	53	5	ND	1	58	1	2	2	26	.27	.072	5	305	1.94	124	.01	2	1.22	.02	.11	1	2
B300E 325S	2	21	22	135	.1	455	26	836	3.88	158	8	ND	2	37	1	4	2	53	.27	.100	6	374	1.81	128	.05	4	1.81	.02	.08	1	1
B300E 375S	1	19	26	107	.1	54	10	1038	2.32	15	5	ND	1	40	1	2	2	39	.30	.070	8	53	.64	242	.04	2	1.44	.02	.11	1	2
STD C/AU-S	21	58	40	139	6.9	71	29	1031	3.96	43	18	7	35	49	18	17	19	66	.43	.102	37	60	.85	183	.08	35	1.72	.06	.15	13	47

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B300E 400S	1	14	20	119	.1	44	9	885	2.13	7	5	ND	1	35	1	2	2	34	.45	.085	4	48	.63	208	.04	6	1.21	.02	.10	1	3
B300E 425S	1	5	8	56	.1	30	6	997	1.32	4	5	ND	1	23	1	2	2	12	.24	.059	4	20	.45	149	.01	6	.63	.02	.11	1	2
B300E 450S	1	39	27	180	.1	190	16	935	3.29	42	5	ND	1	51	1	3	2	42	.43	.107	6	155	1.27	258	.03	6	1.81	.01	.12	1	1
B300E 475S	1	18	22	211	.1	142	15	945	3.05	27	5	ND	1	28	1	2	2	53	.26	.064	5	109	1.00	190	.06	6	1.70	.02	.10	1	1
B300E 500S	2	16	21	173	.3	162	17	1237	3.06	17	5	ND	1	25	1	2	2	50	.28	.080	5	127	.78	278	.06	4	1.68	.02	.07	1	1
B300E 525S	2	20	21	125	.1	41	9	2083	2.18	8	5	ND	1	36	1	3	2	35	.35	.075	6	39	.51	319	.05	7	1.23	.02	.09	1	1
B300E 550S	1	13	11	104	.1	86	11	798	2.45	13	5	ND	1	23	1	2	3	47	.22	.045	4	65	.66	313	.05	5	1.50	.02	.08	1	2
B300E 575S	1	17	19	113	.1	115	13	815	2.92	18	5	ND	2	23	1	2	2	48	.24	.086	5	86	.84	177	.05	5	1.73	.02	.10	1	1
B300E 600S	2	39	31	157	.2	260	23	1471	3.74	71	5	ND	2	42	1	2	2	48	.43	.113	7	194	1.78	292	.05	6	1.87	.02	.15	1	2
B300E 625S	4	68	35	200	.1	535	45	1982	5.06	66	5	ND	1	92	1	5	6	62	1.08	.122	8	330	5.60	210	.09	14	2.20	.01	.11	1	1
B300E 650S	4	88	35	257	.1	357	30	2312	4.25	60	5	ND	1	135	2	2	2	65	1.49	.097	10	192	2.51	319	.13	11	1.97	.01	.10	1	1
B400E 250N	2	35	9	93	.1	193	14	338	3.81	14	5	ND	1	13	1	2	2	66	.19	.042	5	110	1.11	82	.09	5	2.05	.02	.04	1	37
B400E 225N	3	23	11	116	.1	97	10	283	3.71	12	5	ND	1	9	1	2	2	64	.15	.052	4	75	.90	77	.08	6	2.11	.02	.06	1	1
B400E 200N	3	26	11	104	.3	61	10	791	3.17	8	5	ND	1	10	1	2	2	65	.16	.046	4	57	.82	116	.09	6	1.75	.02	.04	1	1
B400E 175N	7	54	16	112	.1	97	11	338	4.21	30	5	ND	1	8	1	2	2	75	.13	.066	7	86	1.26	69	.08	6	2.54	.02	.06	1	1
B400E 150N	2	29	11	105	.1	65	10	626	3.56	23	5	ND	1	8	1	2	2	68	.13	.069	6	65	.92	81	.07	4	2.14	.02	.04	1	1
B400E 100N	2	46	12	114	.1	280	21	875	4.52	27	5	ND	2	14	1	2	2	77	.26	.063	7	144	1.82	130	.12	8	2.69	.02	.08	1	2
B400E 75N	2	39	14	103	.1	202	18	542	4.53	36	5	ND	1	15	1	2	2	81	.28	.066	7	139	2.07	104	.14	8	2.48	.02	.06	1	21
B400E 50N	1	25	16	88	.1	131	17	789	3.48	20	5	ND	1	25	1	2	2	67	.36	.074	6	110	1.53	158	.09	8	1.91	.02	.11	2	1
B400E 25N	2	40	19	95	.1	517	36	1073	4.65	35	5	ND	1	22	1	2	2	71	.29	.073	6	336	2.63	145	.03	7	2.19	.02	.06	2	1
B500E 300N	2	40	15	114	.3	143	14	633	3.95	22	5	ND	2	10	1	2	2	71	.16	.062	7	109	1.25	112	.09	6	2.35	.02	.05	1	1
B500E 275N	2	24	5	75	.1	169	12	356	3.27	13	5	ND	1	16	1	2	2	59	.21	.043	4	107	.92	98	.08	6	1.71	.02	.05	1	1
B500E 250N	2	21	11	108	.1	151	12	366	3.59	11	5	ND	1	13	1	2	2	62	.23	.046	4	97	.86	80	.09	7	2.00	.02	.07	1	1
B500E 225N	2	26	8	96	.2	75	10	587	3.38	15	5	ND	1	10	1	2	2	67	.15	.048	5	68	.79	87	.10	6	1.87	.02	.04	1	1
B500E 200N	2	46	14	97	.3	72	11	409	3.23	21	5	ND	1	11	1	2	2	67	.17	.045	11	65	.96	52	.11	5	2.03	.02	.05	2	2
B500E 175N	1	36	14	106	.1	100	12	393	3.92	29	5	ND	1	11	1	2	2	74	.21	.064	6	84	1.20	81	.11	4	2.10	.02	.08	1	1
B500E 150N	1	26	12	104	.1	129	12	435	3.11	21	5	ND	1	11	1	2	2	59	.19	.046	5	109	1.11	86	.09	6	2.09	.02	.05	1	1
B500E 125N	2	23	11	87	.1	50	7	317	3.28	13	5	ND	1	6	1	2	2	63	.11	.058	5	59	.74	44	.07	6	2.03	.02	.04	1	1
STD C/AU-S	19	57	38	135	7.0	70	26	922	3.81	41	15	6	32	42	16	15	19	57	.44	.091	36	52	.84	168	.07	35	1.62	.06	.12	13	53
B500E 75N	2	34	13	118	.1	95	15	1182	3.93	15	5	ND	1	13	1	2	2	71	.16	.070	7	89	1.15	119	.08	7	2.50	.02	.06	1	1
B500E 50N	2	24	12	98	.2	86	11	570	3.32	20	5	ND	1	10	1	2	2	63	.17	.075	5	71	1.01	94	.08	7	2.02	.02	.07	1	1
B500E 25N	1	23	8	98	.1	99	13	704	3.15	19	5	ND	2	18	1	2	2	61	.28	.056	5	77	1.07	126	.10	6	1.97	.02	.09	1	53
B600E 225N	2	35	10	101	.1	129	13	362	3.66	20	5	ND	2	10	1	2	2	67	.19	.052	6	89	1.28	100	.10	5	2.31	.02	.06	1	1
B600E 175N	2	23	14	93	.2	96	11	341	3.43	18	5	ND	1	11	1	2	2	65	.19	.056	5	82	1.11	82	.11	4	2.01	.02	.07	1	1
B600E 150N	1	24	8	77	.1	124	13	476	3.24	13	5	ND	1	12	1	2	2	61	.18	.046	6	88	1.09	102	.08	7	1.83	.02	.06	1	1
B600E 125N	2	27	8	88	.1	151	13	285	3.58	22	5	ND	1	10	1	2	2	66	.17	.045	5	94	1.21	68	.09	8	2.21	.02	.07	1	2

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B600E 100N	2	28	10	83	.1	106	11	449	3.39	25	5	ND	1	16	1	2	2	70	.20	.085	6	99	1.08	99	.07	9	1.95	.02	.08	1	2
B600E 50S	4	35	10	112	.1	82	13	1405	3.32	34	5	ND	1	11	1	2	2	69	.15	.081	7	79	.90	95	.06	6	2.15	.02	.05	1	1
B600E 75S	5	16	10	85	.1	87	10	324	2.68	33	5	ND	2	12	1	3	2	61	.18	.054	6	77	.70	77	.09	5	1.58	.02	.06	1	1
B600E 100S	2	20	15	92	.1	75	12	506	2.88	28	5	ND	1	19	1	2	2	62	.25	.084	6	73	.86	94	.10	6	1.68	.02	.08	2	2
B700E 200N	2	29	10	123	.1	121	16	820	3.66	22	5	ND	2	15	1	2	2	77	.24	.073	7	98	1.16	130	.12	6	2.15	.02	.07	1	3
B700E 175N	3	38	15	108	.1	137	15	488	4.60	40	5	ND	1	10	1	2	2	92	.15	.065	8	140	1.70	68	.12	10	2.49	.02	.04	2	4
B700E 150N	4	31	13	87	.1	136	11	598	3.99	23	5	ND	1	9	1	2	2	76	.12	.088	6	122	.99	62	.07	7	2.11	.02	.03	2	3
B700E 125N	2	19	8	69	.1	69	10	690	2.93	17	5	ND	1	10	1	2	4	65	.13	.054	6	72	.62	99	.08	5	1.67	.02	.04	1	1
B700E 100N	1	25	9	74	.1	106	15	849	2.91	23	5	ND	1	25	1	2	2	62	.35	.056	7	91	.94	136	.08	5	1.71	.02	.07	1	3
B700E 75N	1	25	14	72	.1	101	13	700	2.85	23	5	ND	2	19	1	2	2	60	.23	.056	7	81	.92	117	.09	9	1.76	.02	.06	1	1
B700E 50N	1	32	12	71	.1	130	15	542	3.09	27	5	ND	2	20	1	2	2	41	.24	.055	7	89	1.06	113	.08	11	1.78	.02	.07	1	2
B700E 25N	2	23	8	80	.1	92	11	307	3.60	24	5	ND	2	14	1	2	2	75	.20	.090	5	82	.81	119	.08	6	1.76	.02	.06	1	1
B700E 0 N	2	15	7	60	.3	30	5	200	2.68	17	5	ND	1	8	1	2	2	69	.11	.064	4	55	.54	45	.06	5	1.42	.02	.03	1	1
B700E 25S	3	18	10	49	.3	28	5	198	3.33	20	5	ND	1	9	1	2	3	89	.10	.054	5	50	.48	67	.08	4	1.46	.02	.02	2	1
B700E 125S	3	42	13	117	.2	86	13	340	4.26	47	5	ND	1	11	1	2	2	91	.17	.094	8	90	1.23	70	.10	7	2.50	.02	.06	1	2
B800E 25S	2	30	17	100	.1	99	12	286	3.68	41	5	ND	2	9	1	2	2	77	.14	.056	7	89	1.05	68	.09	6	2.11	.02	.04	1	3
B800E 100S	2	31	17	100	.1	103	11	281	3.60	43	5	ND	1	11	1	2	2	70	.14	.058	7	99	1.11	85	.06	5	2.28	.02	.05	1	1
B800E 150S	3	32	21	116	.1	82	12	625	3.19	37	5	ND	1	11	1	2	2	65	.15	.073	7	79	.91	95	.06	6	1.99	.02	.05	1	4
B800E 175S	3	37	20	95	.1	109	13	448	3.17	46	5	ND	2	14	1	2	2	62	.17	.064	9	116	1.17	85	.06	6	1.86	.02	.09	2	5
B900E 100S	2	26	14	79	.1	72	9	359	3.02	23	5	ND	1	11	1	2	2	46	.15	.051	6	75	.82	82	.06	5	1.85	.02	.04	2	1
STD C/AU-S	21	58	38	136	6.7	70	29	1015	3.75	41	17	7	34	47	18	18	19	64	.44	.100	37	56	.83	171	.08	37	1.61	.07	.11	15	46
B900E 125S	1	13	9	46	.1	25	4	139	2.27	11	5	ND	1	8	1	2	2	63	.11	.042	5	48	.42	48	.06	4	1.41	.02	.03	2	2
B900E 150S	2	15	11	65	.1	34	6	203	2.78	15	5	ND	1	9	1	2	2	70	.13	.057	5	51	.55	56	.06	5	1.70	.02	.04	1	1
NO NUMBER A	4	51	17	161	.1	54	28	1776	6.07	42	5	ND	2	13	1	3	2	148	.28	.082	7	51	1.24	84	.21	8	2.47	.03	.06	1	1
NO NUMBER B	8	107	75	299	.8	98	33	2738	7.22	89	5	ND	3	22	2	2	2	132	.34	.066	22	75	1.52	116	.10	6	3.01	.02	.10	1	34

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
MK-01	1	599	22862	8338	87.1	35	30	295	22.33	41927	5	3	3	103	234	112	5	72	.08	.027	4	105	.65	4	.01	2	1.29	.02	.04	1	1260
MK-02	1	6	189	39	.1	12	4	279	1.58	119	5	ND	7	29	1	2	2	23	.53	.035	11	8	.50	42	.01	2	.74	.07	.09	1	3
MK-03	1	18	1391	154	1.7	1957	72	623	4.64	1023	5	ND	1	2	4	11	8	5	.04	.005	2	102	22.22	2	.01	7	.06	.01	.01	1	17
MK-04	1	41	14	31	.1	12	3	271	1.43	12	5	ND	3	17	1	2	2	16	.29	.032	11	9	.41	57	.01	2	.68	.07	.16	1	1
MK-05	1	47	89	91	.3	118	29	1026	6.70	69	5	ND	3	147	1	3	2	194	3.76	.155	13	178	4.88	119	.02	7	2.66	.05	.09	1	1
MK-06	3	65	11	55	.1	15	14	426	4.54	75	5	ND	1	12	1	2	2	76	.29	.039	5	22	1.01	73	.01	3	1.45	.05	.16	1	64
MK-08	1	44	30	56	.2	33	17	575	4.23	17	5	ND	1	24	1	2	2	164	2.70	.049	2	55	2.03	9	.43	7	2.83	.08	.04	1	1
MK-09	1	41	2	72	.1	27	21	682	5.33	2	5	ND	1	45	1	2	4	185	1.66	.066	2	36	2.17	63	.54	6	2.19	.08	.05	1	1
MK-10	1	15	29	45	.2	37	15	465	3.42	22	5	ND	1	51	1	2	2	99	2.05	.041	2	57	1.57	3	.49	5	2.12	.11	.02	1	1
MK-12	1	26	6	65	.4	33	9	1761	2.87	7	5	ND	4	328	1	2	2	54	10.88	.066	11	30	1.15	111	.13	2	1.40	.11	.36	1	1
MK-13	1	35	31	87	.1	26	11	558	4.56	31	5	ND	2	20	1	2	3	86	.32	.074	7	28	1.59	132	.06	4	2.32	.08	.26	1	1
MK-14	1	25	4	114	.2	18	5	357	2.59	2	5	ND	2	12	1	2	2	74	.42	.037	7	18	1.13	29	.21	2	1.02	.08	.04	1	1
MK-15	1	3	47	25	.3	1202	46	568	2.73	35	5	ND	1	110	1	10	9	10	1.88	.009	2	353	15.89	12	.01	24	.11	.01	.02	1	1
MK-16	1	39	6	100	.2	27	11	694	4.50	11	5	ND	3	21	1	2	2	98	1.13	.055	9	29	1.74	68	.39	9	2.04	.05	.16	1	1
MK-17	1	43	12	94	.2	89	28	1046	6.97	10	5	ND	3	118	1	2	2	180	4.89	.188	15	110	3.03	73	.07	6	2.72	.17	.07	1	1
MK-18	1	29	2	67	.2	25	12	709	4.08	2	5	ND	3	27	1	2	2	117	1.16	.056	8	36	1.64	72	.36	6	1.80	.06	.10	1	1
MK-19	1	29	12	68	.1	21	10	603	3.48	3	5	ND	3	31	1	2	2	90	1.57	.051	8	25	1.92	42	.30	102	1.84	.05	.10	1	1
MK-20	1	6	5	28	.2	626	27	1053	3.15	37	5	ND	1	1113	1	11	7	16	5.82	.004	2	488	12.15	60	.01	2	.35	.02	.01	1	1
MK-21	1	11	9	38	.1	1795	70	535	4.84	7	5	ND	1	1	1	10	5	23	.09	.008	2	871	23.21	1	.01	181	.25	.01	.01	2	3
MK-22	1	5	2	24	.2	1186	46	813	3.87	3	6	ND	1	489	1	5	8	15	7.62	.004	2	533	14.39	21	.01	8	.16	.03	.01	1	1
MK-23	1	29	14	79	.1	39	13	754	3.86	10	5	ND	2	42	1	2	2	82	3.44	.054	8	36	1.71	47	.14	14	1.76	.06	.10	1	1
MK-24	1	6	3	17	.2	1067	47	589	3.29	6	5	ND	1	109	1	11	8	13	1.25	.004	2	500	17.25	7	.01	19	.18	.01	.01	1	1
MK-25	1	10	8	17	.5	980	48	633	4.28	31	5	ND	2	42	1	8	8	16	.26	.006	2	695	20.29	26	.01	5	.24	.01	.02	1	1
MK-25A	2	463	9705	3424	19.3	16	3	138	2.35	8583	5	ND	1	7	65	11	7	9	.03	.011	2	11	.30	11	.01	3	.31	.01	.05	1	38
MK-26	1	28	5	93	.1	30	13	767	4.53	4	5	ND	3	24	1	2	2	102	.80	.050	8	30	1.59	97	.26	6	2.07	.05	.15	1	1
MK-27	1	17	69	60	.3	8	3	119	1.20	42	5	ND	2	8	1	2	2	9	.10	.033	10	9	.44	39	.01	6	.67	.05	.17	1	1
MK-30	2	117	66	69	.6	14	5	522	1.23	43	5	ND	1	1	1	2	5	12	.02	.009	4	6	.19	7	.01	2	.27	.01	.03	1	1
MK-31	1	17	25	39	.1	22	3	291	1.07	12	5	ND	7	7	1	2	2	8	.07	.016	20	11	.42	55	.01	2	.59	.06	.11	1	1
MK-32	1	145	43	80	.3	24	7	451	2.31	47	5	ND	2	40	1	2	2	56	.96	.054	12	20	.60	35	.01	3	1.02	.02	.13	1	1
MK-33	1	63	4	77	.1	40	21	769	5.63	5	5	ND	3	59	1	2	3	184	5.34	.087	7	94	2.15	30	1.01	28	3.12	.10	.05	1	1
MK-34	6	45	25232	6765	46.1	1	2	130	10.25	41566	5	2	3	19	207	75	5	1	.01	.004	5	2	.02	28	.01	2	.18	.01	.17	1	1350
MK-35	2	169	13173	600	20.0	3	2	145	3.07	18722	5	ND	5	11	23	19	4	6	.13	.014	16	7	.13	49	.01	3	.49	.02	.25	1	395
MK-36	1	297	5620	1361	33.4	13	16	77	13.01	41279	5	ND	2	10	37	67	7	6	.02	.009	2	1	.11	20	.01	2	.23	.01	.10	1	995
STD C/AU-R	21	59	39	137	7.1	72	29	1023	3.86	41	16	8	35	48	18	17	18	65	.46	.103	37	63	.86	176	.09	35	1.67	.07	.13	15	510
MK-36A	7	210	1794	20829	10.7	24	57	859	6.68	14169	5	ND	1	6	344	8	8	37	.21	.041	4	14	.72	23	.01	2	1.09	.01	.12	1	450
MK-37	13	2183	21806	56013	105.8	8	22	60	14.06	41209	5	2	2	8	915	99	18	3	.01	.004	2	1	.04	14	.01	2	.07	.01	.02	1	1560
MK-38	1	4	39	125	.1	2	1	30	.45	219	5	ND	2	1	1	2	2	1	.01	.001	3	2	.01	20	.01	8	.24	.04	.16	1	1

Pb As saturates at 10,000 PPM
Zn ✓ at 20,000 PPM
Ag ✓ at 35 PPM

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
MK-39	1	41	120	313	.8	167	33	1288	7.37	339	5	ND	2	73	5	2	2	135	6.66	.105	12	173	4.21	52	.01	6	3.19	.07	.06	1	3
MK-40	1	54	8	86	.2	124	25	931	6.51	11	6	ND	2	117	1	2	2	168	5.79	.178	15	110	2.76	82	.30	9	2.11	.07	.32	1	1
MK-41	1	56	66	121	.1	23	4	255	1.59	95	5	ND	2	4	1	2	2	12	.11	.017	8	8	.55	36	.01	4	.72	.01	.12	1	1
MK-41A	1	47	6	94	.1	113	22	707	5.66	8	5	ND	1	22	1	2	2	104	.97	.106	10	109	3.22	58	.28	7	2.78	.03	.10	1	1
MK-42	5	49	12821	11012	20.6	58	25	2496	16.10	35973	10	3	1	60	191	80	2	63	2.65	.043	3	48	1.76	12	.01	2	2.00	.02	.05	1	2940
MK-43	6	29	16823	14902	109.1	50	39	1378	21.51	35168	9	5	2	15	264	172	2	48	.63	.041	2	35	1.46	12	.01	5	1.48	.01	.07	1	5090
MK-44	8	337	20308	18895	43.8	123	91	3665	18.69	36597	12	3	1	296	513	55	2	96	.48	.049	4	161	2.90	19	.01	4	2.79	.01	.02	1	2460
MK-45	2	152	503	1213	1.8	21	15	4582	8.59	809	5	ND	3	62	18	2	2	225	4.74	.128	11	1	3.68	19	.01	3	3.88	.04	.13	1	15
MK-46	1	48	167	149	1.1	84	27	1010	6.51	514	9	ND	3	111	2	2	2	174	10.56	.092	7	109	2.78	52	.45	8	2.71	.10	.22	1	13
MK-47	1	31	38	49	.1	6	1	227	.68	146	5	ND	1	2	1	2	3	7	.06	.004	2	4	.20	4	.01	7	.19	.01	.01	1	1
MK-48	3	29	46	58	.1	3	2	184	1.13	145	5	ND	7	4	1	2	3	3	.17	.004	7	3	.06	14	.01	5	.33	.05	.11	1	2
MS-01	1	29	15	83	.2	23	12	671	4.15	24	5	ND	1	32	1	2	2	108	2.00	.051	7	30	1.68	49	.29	7	1.71	.05	.07	1	1
MS-02	1	6	8	44	.1	24	5	181	1.32	20	5	ND	1	91	1	2	2	15	1.04	.045	5	17	.67	147	.01	4	.72	.04	.10	1	1
MS-03	1	3	8	37	.1	562	27	1002	3.49	120	5	ND	1	2335	1	9	6	11	10.64	.003	2	377	14.27	21	.01	4	.28	.04	.01	1	1
MS-04	1	27	10	57	.1	42	12	354	2.70	15	9	ND	1	304	1	2	2	52	2.69	.084	10	32	2.03	163	.01	3	1.61	.06	.12	1	1
MS-05	2	41	11	70	.2	51	19	843	5.52	3	9	ND	2	88	1	2	2	152	7.42	.079	8	100	2.72	45	.83	37	3.52	.10	.02	1	1
MS-06	1	19	8	43	.1	6	4	97	1.49	13	5	ND	1	24	1	2	2	10	.39	.061	8	9	.39	33	.01	5	.63	.05	.15	2	2
MS-07	1	26	7	101	.1	24	15	902	5.24	5	5	ND	2	33	1	2	2	141	1.79	.057	8	33	2.11	54	.42	10	2.20	.05	.07	1	3
MS-08	1	10	13	37	.1	4	2	276	1.27	6	5	ND	7	7	1	2	2	11	.07	.029	14	1	.23	39	.01	5	.52	.05	.15	1	1
MS-09	3	75	51	103	.2	48	7	432	3.99	167	7	ND	2	192	1	2	2	67	1.02	.062	9	39	1.72	150	.05	6	1.63	.05	.14	1	7
MS-10	1	91	3	19	.2	1432	61	704	4.76	5	8	ND	1	14	1	8	9	10	.17	.004	2	261	20.54	18	.01	61	.15	.01	.01	1	1
MS-11	6	21	13	20	.1	4	1	158	1.26	20	5	ND	10	6	1	2	2	16	.11	.020	6	2	.21	26	.08	5	.48	.06	.21	4	1
MS-12	248	14	8	7	.1	12	1	36	.54	13	5	ND	1	3	1	2	2	2	.01	.004	2	3	.11	6	.01	5	.07	.01	.03	6	2
MS-13	3	8	13	14	.1	4	1	105	.46	18	5	ND	19	2	1	2	2	2	.01	.003	2	2	.04	9	.01	5	.18	.05	.07	1	1
MS-14	1	36	526	440	.7	84	25	405	5.53	863	5	ND	1	14	10	2	2	129	.91	.219	4	119	1.36	189	.41	3	2.10	.09	1.49	1	28
MS-15	1	109	109	136	.1	45	9	355	3.05	164	5	ND	4	8	2	2	3	74	.12	.038	13	48	1.00	119	.03	4	1.54	.04	.29	1	6
MS-16	5	19	46	38	.5	19	4	361	1.63	22	5	ND	3	3	1	2	2	19	.07	.020	9	8	.62	16	.01	10	.80	.02	.08	1	1
MS-17	1	1741	20510	1478	152.8	3	11	25	15.62	36146	5	3	1	24	39	147	2	5	.01	.008	2	1	.03	18	.01	4	.13	.01	.11	1	5490
MS-18	1	571	21940	683	97.3	12	5	124	7.40	36527	5	ND	1	17	10	63	4	8	.02	.010	3	5	.28	37	.01	4	.42	.01	.09	1	795
MS-19	1	3867	20249	2519	262.8	1	1	13	14.86	35742	5	3	2	10	51	245	2	2	.01	.002	2	1	.02	20	.01	5	.02	.01	.04	1	3150
MS-19A	1	13	443	66	1.1	2	1	51	.52	817	5	ND	3	1	1	4	2	1	.01	.001	3	1	.01	31	.01	7	.25	.04	.18	1	14
MS-20	1	118	2389	107	8.6	1	1	84	.78	4107	5	ND	3	1	2	8	2	1	.01	.003	2	1	.01	16	.01	7	.18	.03	.15	1	97
MS-21	2	73	43	109	.6	34	30	1108	9.30	55	6	ND	1	46	1	2	2	300	3.08	.068	4	35	3.20	558	.89	15	3.17	.07	.06	1	1
MS-22	1	32	44	64	.3	209	34	885	5.96	90	7	ND	1	249	1	2	2	115	4.66	.064	7	203	6.03	195	.01	7	2.98	.11	.18	1	1
MS-23	1	27	36	50	.1	20	9	2418	3.28	65	5	ND	1	11	1	2	2	23	.24	.034	9	5	.47	54	.02	5	.71	.01	.03	1	1
MS-24	3	59	38	134	.4	15	7	271	3.50	85	5	ND	1	11	1	2	2	32	.19	.049	12	11	.47	63	.01	6	1.24	.03	.21	2	3
STD C/AU-R	21	59	41	138	6.9	69	28	1019	4.06	38	16	7	34	48	18	16	21	65	.50	.102	36	57	.92	182	.08	33	1.77	.07	.15	13	505

SHANGRI-LA PROJECT - MATSON FILE # 87-1809

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
MS-25	1	40	5	118	.1	13	14	912	4.76	26	5	ND	3	31	1	2	2	75	.81	.144	16	6	1.13	148	.01	4	1.84	.04	.18	1	3
MS-26	1	15	10	38	.1	30	5	213	1.32	4	5	ND	1	12	1	2	2	9	.13	.051	5	25	.43	47	.01	4	.64	.05	.17	2	2
MS-27	1	50	5	84	.1	46	21	851	6.28	2	5	ND	3	138	1	2	2	133	7.38	.114	9	90	1.85	156	.05	6	1.54	.09	.13	2	1
MS-28	1	36	8	39	.1	21	4	245	1.34	6	5	ND	2	4	1	2	2	10	.04	.012	10	11	.35	40	.01	4	.47	.01	.09	1	4
MS-29	1	20	58	39	.1	1	1	61	.50	16	5	ND	4	3	1	2	2	1	.04	.001	4	1	.02	35	.01	6	.31	.04	.21	1	39
MS-29A	36	70	121	72	3.6	2	1	79	.59	15	5	ND	6	2	1	3	15	3	.01	.003	2	3	.05	8	.01	4	.22	.04	.07	1	3
MS-30	1	47	8	82	.3	35	24	1957	6.80	34	5	ND	3	111	1	2	2	182	8.31	.044	3	65	2.25	25	.01	5	2.29	.07	.06	2	4
MS-31	1	30	2	60	.1	67	22	861	5.19	3	5	ND	2	137	1	2	2	118	3.52	.056	7	81	3.51	162	.01	5	2.18	.05	.14	1	3
MS-32	1	62	7	101	.2	77	29	779	7.15	9	5	ND	3	80	1	2	2	138	3.99	.182	15	65	2.21	73	.01	8	2.70	.06	.17	1	2
MS-33	1	53	13	97	.1	74	21	782	5.67	14	5	ND	1	38	1	2	2	116	1.10	.154	12	74	2.39	148	.01	7	2.43	.03	.14	1	1
MS-34	3	81	13855	9806	26.9	48	20	3838	11.47	37220	5	ND	1	154	185	60	2	63	5.78	.046	4	62	1.83	10	.01	2	1.99	.04	.04	1	1820
MS-35	1	73	2	1034	1.4	24	4	328	2.45	127	5	ND	2	6	4	2	2	16	.04	.013	13	14	.84	44	.01	7	1.08	.01	.15	1	3
MS-36	1	22	58	214	.4	18	4	725	1.36	148	5	ND	2	4	8	2	2	8	.11	.031	8	7	.62	12	.01	5	.67	.01	.06	1	2
MS-37	1	36	6	48	.1	15	11	265	2.82	245	5	ND	1	6	1	2	2	104	1.11	.086	2	14	.74	14	.19	4	.98	.12	.04	1	1
MS-38	1	44	10	26	.2	18	2	374	1.09	13	5	ND	1	40	1	2	3	25	1.27	.005	3	20	.41	2	.01	3	.45	.01	.01	1	1
STD C/AU-R	21	58	39	136	6.8	67	29	1012	3.92	38	14	7	34	46	18	15	20	62	.45	.099	35	57	.85	163	.07	36	1.67	.06	.12	14	510
MS-39	5	81	8	7	.2	2	1	44	.76	40	5	ND	6	6	1	2	4	1	.02	.004	12	2	.02	37	.01	5	.18	.06	.09	2	2
RSC-02	4	151	5	87	.2	22	49	1057	7.93	33	5	ND	2	59	1	2	2	64	7.06	.027	2	6	1.40	56	.01	2	1.27	.08	.03	1	1
RSC-03	22	35	6	565	.1	46	5	539	2.09	17	5	ND	2	76	6	2	4	15	20.88	.041	2	3	.14	26	.01	2	.19	.06	.05	1	1
RSC-04	3	86	4	92	.1	10	24	1321	6.10	5	5	ND	2	32	1	2	2	22	6.86	.037	2	1	1.62	31	.01	3	.55	.09	.05	1	1
L5-TS 175W 600S	1	14	5	108	.1	14	16	685	4.91	2	5	ND	2	21	1	2	2	76	.43	.136	18	8	1.53	101	.02	9	1.84	.05	.08	1	2
TS 125W 600S	1	36	6	97	.1	40	14	603	4.79	13	5	ND	1	18	1	2	2	91	.66	.063	7	56	1.64	58	.01	6	1.84	.06	.06	1	1
JDK-11	1	63	2	73	.1	80	21	670	5.21	2	5	ND	1	23	1	2	2	166	3.04	.046	3	90	2.43	23	.55	30	2.94	.08	.01	1	1
100W-50N	1	10	3	36	.1	1886	74	817	5.03	5	9	ND	1	1	1	4	3	15	.09	.004	2	612	21.08	1	.01	21	.18	.01	.01	1	1
CONTACT REXMT. PORPHORY	1	11	11	26	.1	11	2	106	.76	2	5	ND	2	10	1	2	2	3	.08	.033	7	5	.21	36	.01	5	.38	.05	.13	1	1
LOC.MK-40 THIN SECTION	1	53	4	84	.1	34	20	690	6.92	2	5	ND	2	66	1	2	2	173	4.23	.180	16	65	1.75	56	.32	13	1.88	.07	.41	1	1
PERIDOTITE	1	2	6	39	.2	1829	75	753	4.94	3	9	ND	1	8	1	3	6	23	.14	.004	2	745	21.45	9	.01	766	.25	.01	.01	1	1
CARPENTER LK	1	42	2	37	.1	16	5	689	1.90	7	5	ND	3	18	1	2	3	37	.38	.044	7	8	.57	88	.13	6	.81	.05	.32	2	1
APLITE	1	3	17	16	.3	8	1	374	.23	4	5	ND	1	243	1	2	9	1	32.02	.007	2	5	.19	8	.01	11	.01	.01	.01	5	1
NO NUMBER 1	249	172	13	23	.1	4	2	50	2.30	9	5	ND	4	3	1	2	6	6	.01	.009	3	4	.03	8	.01	5	.29	.02	.06	5	1
NO NUMBER 2	8	81	23683	9230	50.7	3	2	307	10.05	37300	5	ND	4	21	240	67	6	1	.01	.006	5	4	.05	29	.01	7	.18	.01	.17	1	945
NO NUMBER 3	1	43	25	78	.1	46	23	989	6.17	34	5	ND	1	73	1	2	3	199	3.52	.072	8	61	2.37	43	.18	9	2.37	.06	.05	1	3

ACME ANALYTICAL LABORATORIES
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: JULY 4 1987

DATE REPORT MAILED: July 14/87.

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp AU** AND AG** BY FIRE ASSAY.

ASSAYER: D. Toye. DEAN TOYE, CERTIFIED B.C. ASSAYER

SHANGRI-LA MINERALS PROJECT-MATSON File # 87-1809 R

SAMPLE#	AG** OZ/T	AU** OZ/T
MK-01	2.69	.035
MK-25A	.57	.001
MK-34	1.42	.037
MK-36	1.03	.025
MK-37	3.36	.048
MK-42	.68	.079
MK-43	3.27	.144
MK-44	1.41	.066
MS-17	4.69	.156
MS-18	3.03	.021
MS-19	7.91	.098
MS-34	.77	.066

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS, VANCOUVER B.C.
PH:(604)253-3158 COMPUTER LINE:251-1011

RECEIVED 1987 JUL 20

DATE RECEIVED JULY 14 1987
DATE REPORTS MAILED July 17/87

ASSAY CERTIFICATE

SAMPLE TYPE : PULP
PT** & PD** BY FIRE ASSAY

ASSAYER ____ DEAN TOYE , CERTIFIED B.C. ASSAYER

SHANGRI - LA MINERALS PROJECT MATSON FILE# 87-1809 R PAGE# 1

SAMPLE	Pt** oz/t	Pd** oz/t
MK-03	.001	.001
MK-15	.001	.001
MK-20	.001	.001
MK-21	.001	.001
MK-22	.001	.001
MK-24	.001	.001
MK-25	.001	.001
MS-03	.001	.001
MS-10	.001	.001
100W-50N	.001	.001

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL/ASSAY CERTIFICATE

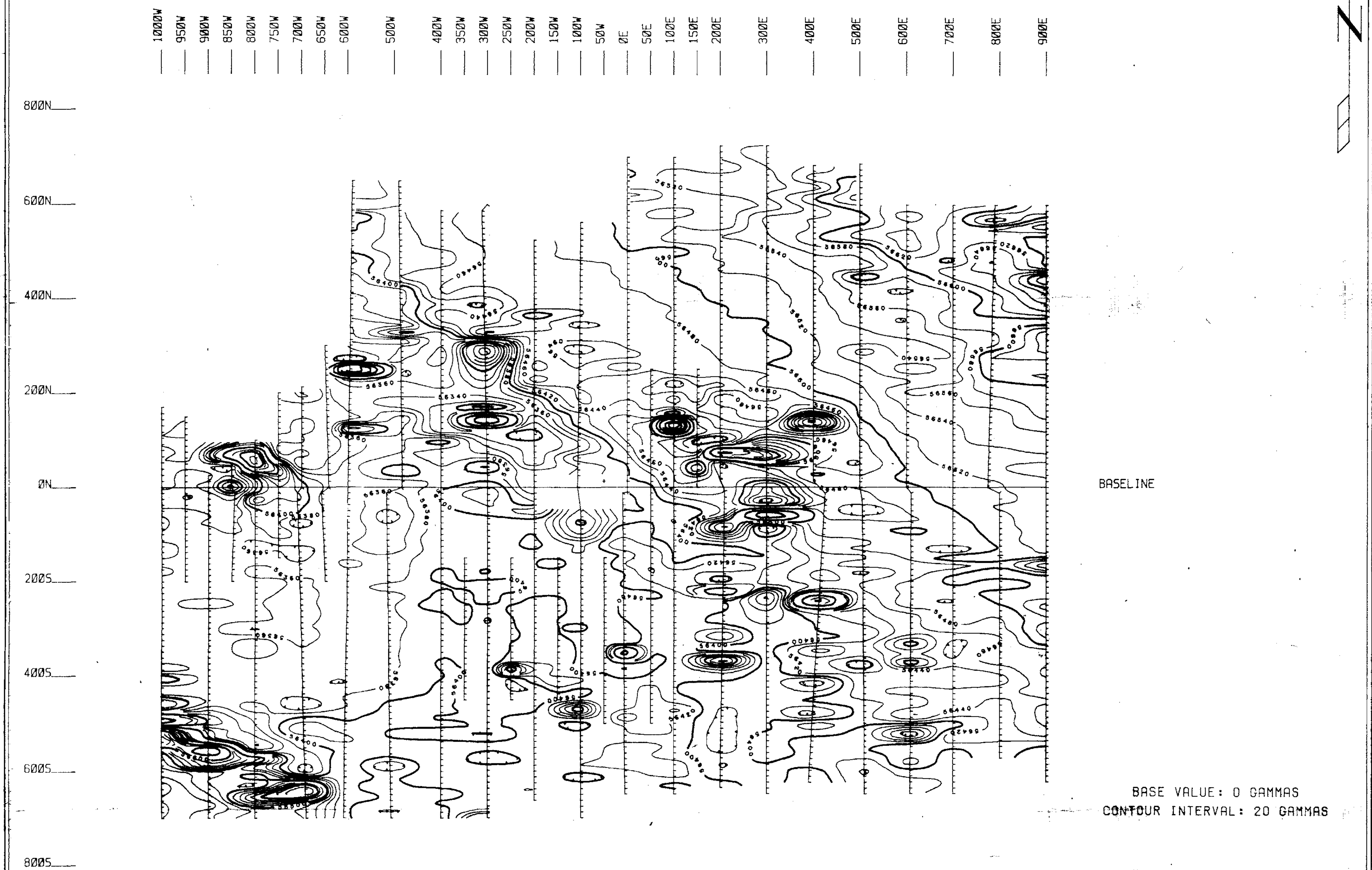
.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Rock Chips

DATE RECEIVED: JUNE 26 1987 DATE REPORT MAILED: July 13/87 ASSAYER. D. Toye. DEAN TOYE. CERTIFIED B.C. ASSAYER

SHANGRI-LA MINERALS PROJECT - MATSON File # 87-2010

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AG OZ/T	AU OZ/T
MK49	8	195	27610	7843	213.8	8	12	94	26.12	99999	5	2	4	34	116	314	2	15	.01	.020	3	3	.02	21	.01	5	.37	.01	.05	1	6.01	.089
MK50	19	124	24934	26858	106.9	8	38	125	24.90	99999	5	ND	4	14	388	182	3	5	.01	.006	2	1	.03	10	.01	11	.08	.01	.05	1	2.86	.059
MK51	2	42	356	205	1.3	2	2	123	1.47	731	9	ND	4	2	4	3	2	3	.01	.015	18	4	.08	24	.01	2	.38	.04	.18	1	.04	.001
MK52	5	101	766	329	3.7	32	12	554	4.74	239	5	ND	2	8	2	2	2	44	.13	.076	10	39	.92	29	.01	2	1.37	.01	.15	1	.14	.001
MK53A	17	1608	27197	22125	96.8	22	18	239	17.50	99999	5	ND	4	22	329	100	3	12	.02	.021	2	3	.16	20	.01	4	.33	.01	.07	1	2.74	.033
MK53B	1	42	4194	511	12.6	1	2	113	4.99	47892	5	ND	3	3	15	31	2	1	.01	.012	13	1	.01	44	.01	2	.29	.02	.19	1	.40	.029
MK54	14	1413	25525	17128	287.9	2	8	135	24.89	99999	5	ND	3	35	247	389	2	12	.01	.021	2	1	.03	19	.01	6	.14	.01	.09	1	8.36	.056
MK55	44	4300	22569	77263	295.6	10	20	214	25.94	99999	5	ND	4	7	1057	263	40	7	.04	.005	2	1	.07	11	.01	13	.10	.01	.04	1	7.57	.061
MK56	4	48	3895	5075	16.1	4	20	72	15.33	99999	5	2	1	5	85	69	3	3	.01	.005	2	1	.04	7	.01	8	.05	.01	.03	1	.49	.035
MK57	5	35	361	119	1.5	1	1	181	1.27	482	5	ND	4	9	3	2	2	1	.15	.008	18	1	.02	36	.01	5	.28	.04	.16	1	.05	.001
MK58	3	98	266	552	1.4	42	15	521	3.29	292	5	ND	2	12	10	2	11	39	.12	.078	8	36	1.08	28	.01	2	1.42	.02	.16	1	.03	.001
MK59A	9	66	5007	10408	18.1	73	8	5881	4.66	894	5	ND	1	110	146	9	5	50	7.98	.069	9	49	1.79	16	.01	2	1.97	.01	.09	1	.49	.001
MK59B	3	117	741	699	3.1	28	6	1063	2.36	89	5	ND	1	3	13	2	7	20	.07	.016	5	10	.86	23	.01	2	1.05	.01	.08	1	.12	.001
MK60	8	43	6360	10621	24.5	50	30	5695	10.95	74809	5	ND	1	119	157	65	2	46	8.48	.067	8	40	1.46	19	.01	2	1.60	.01	.10	1	.75	.059
MK61	10	29	26612	10813	99.2	28	70	1240	26.48	99999	5	4	4	26	174	321	3	26	.96	.024	2	13	.67	10	.01	10	.76	.01	.07	1	2.81	179
STD C	22	65	36	134	7.2	72	31	1097	4.08	42	19	9	38	52	19	18	22	63	.44	.095	39	64	.85	186	.09	35	1.82	.07	.15	13	-	-

ASSAY REQUIRED FOR Pb, As >10,000 ppm
Zn >20,000 ppm
Ag >35 ppm



BASE VALUE: 0 GAMMAS

CONTOUR INTERVAL: 20 GAMMAS

SCALE 1:5000

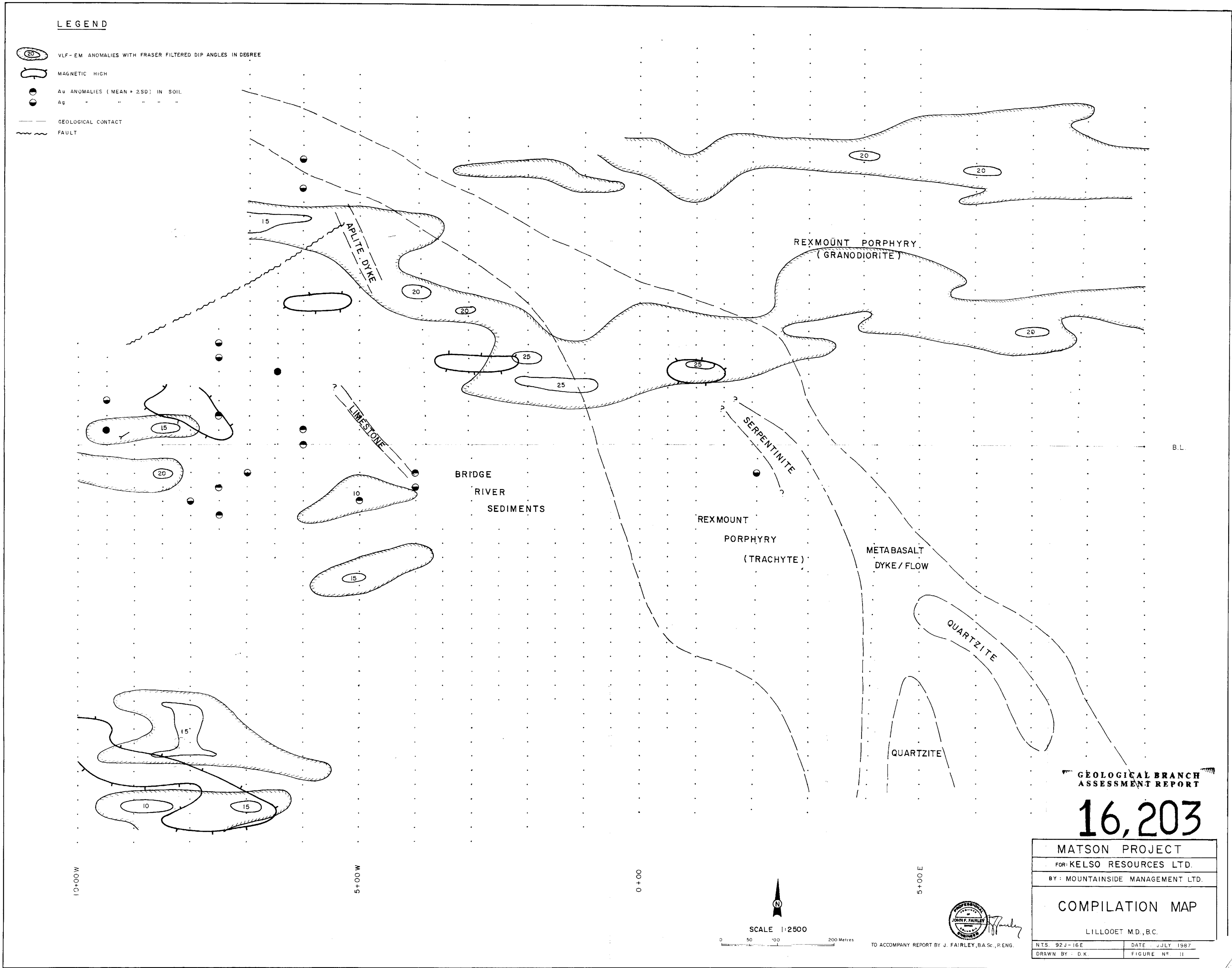
100 0 100 200 300

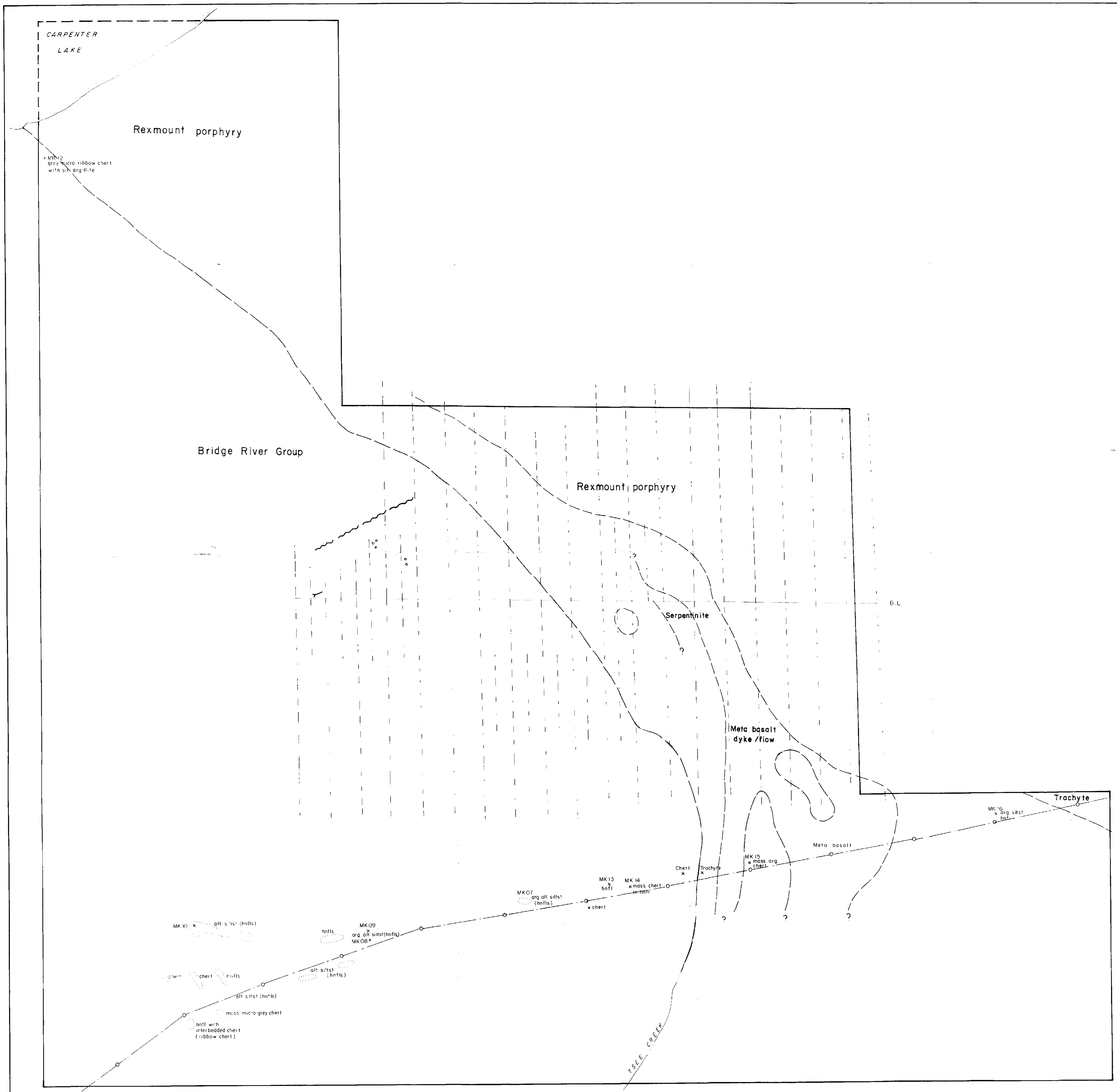
METERS

TO ACCOMPANY REPORT BY
JOHN FAIRLEY, P.ENG.

PROFESSIONAL ENGINEER — JOHN F. FAIRLEY — PROVINCE OF BRITISH COLUMBIA

MATSON PROJECT	
FOR: KELSO RESOURCES LTD.	
BY: MOUNTAINSIDE MANAGEMENT LTD.	
PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.	
TOTAL FIELD MAGNETICS CONTOUR MAP LILLOET M.D., B.C.	
N.T.S.: 92J 15E	DATE: JULY 1987
PLOTTED BY: R.P.M.	FIGURE NO. 10


LEGEND
VLF-EM ANOMALIES WITH FRASER FILTERED DIP ANGLES IN DEGREE
MAGNETIC HIGH
Au ANOMALIES (MEAN + 2SD) IN SOIL
Ag " " " " "
GEOLOGICAL CONTACT
FAULT
APLITE DYKE
REXMOUNT PORPHYRY
(GRANODIORITE)
LIMESTONE
BRIDGE
RIVER
SEDIMENTS
SERPENTINITE
REXMOUNT
PORPHYRY
(TRACHYTE)
METABASALT
DYKE / FLOW
QUARTZITE
QUARTZITE
B.L.
10+00W
5+00W
0+00
5+00E
SCALE 1:2500
0 50 100 200 Metres
TO ACCOMPANY REPORT BY J. FAIRLEY, B.A.Sc., P.ENG.
GEOLOGICAL BRANCH
ASSESSMENT REPORT
16,203
MATSON PROJECT
FOR: KELSO RESOURCES LTD.
BY: MOUNTAINSIDE MANAGEMENT LTD.
COMPILATION MAP
LILLOOET M.D., B.C.
N.T.S. 92J-16E
DATE: JULY 1987
DRAWN BY: D.K.
FIGURE Nº 11



LEGEND

x MK 14	SAMPLE LOCATION & Nº.
•	TRENCH / PIT
≻—	ADIT
—— ——	GEOLOGIC CONTACT
∿∿ ∿∿	FAULT / SHEAR ZONE
—·—o— · —	B.C. HYDRO TRANSMISSION LINE & TOWER

N

SCALE 1:5000

0 100 200 400 metres

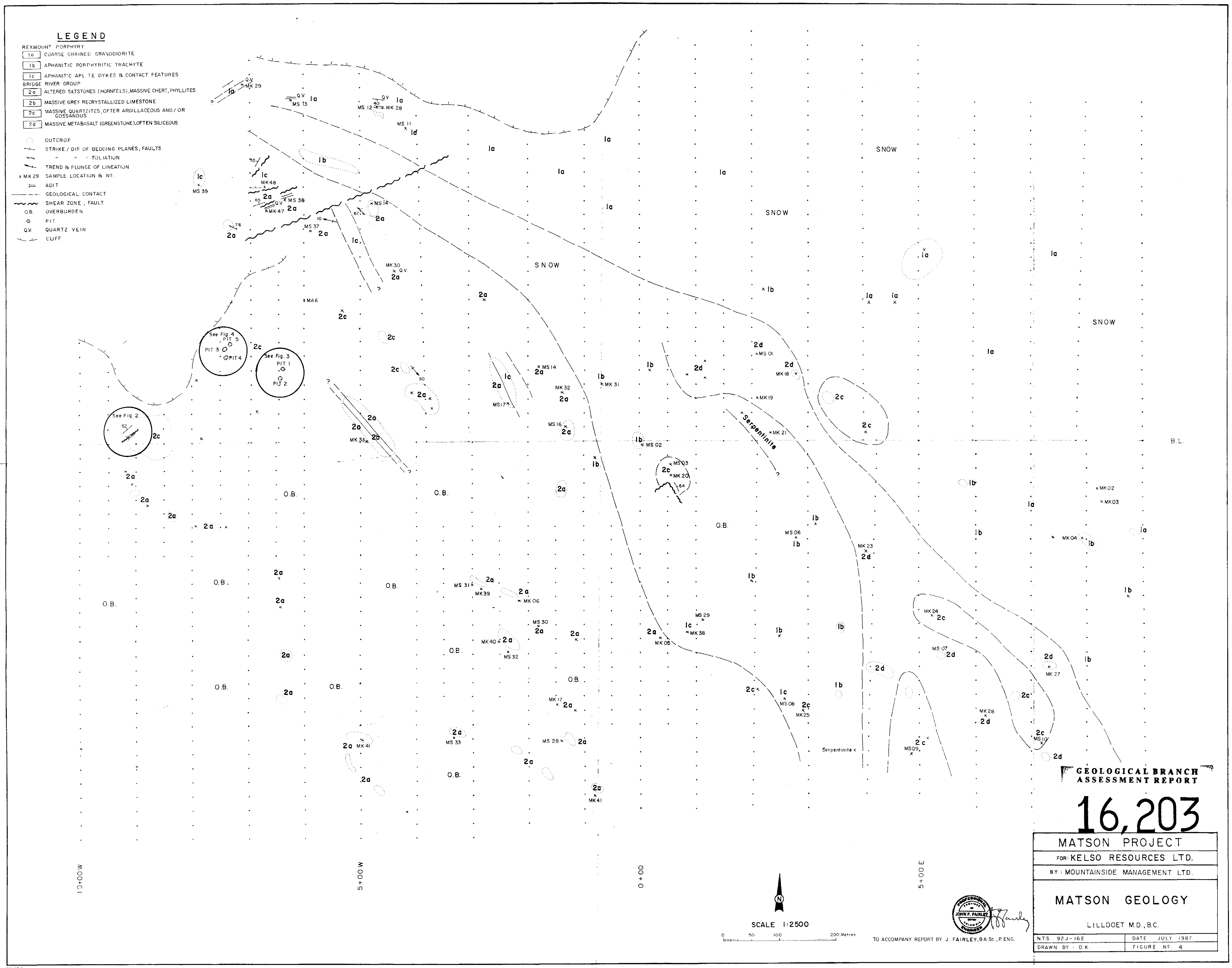
GEOLOGICAL BRANCH
ASSESSMENT REPORT

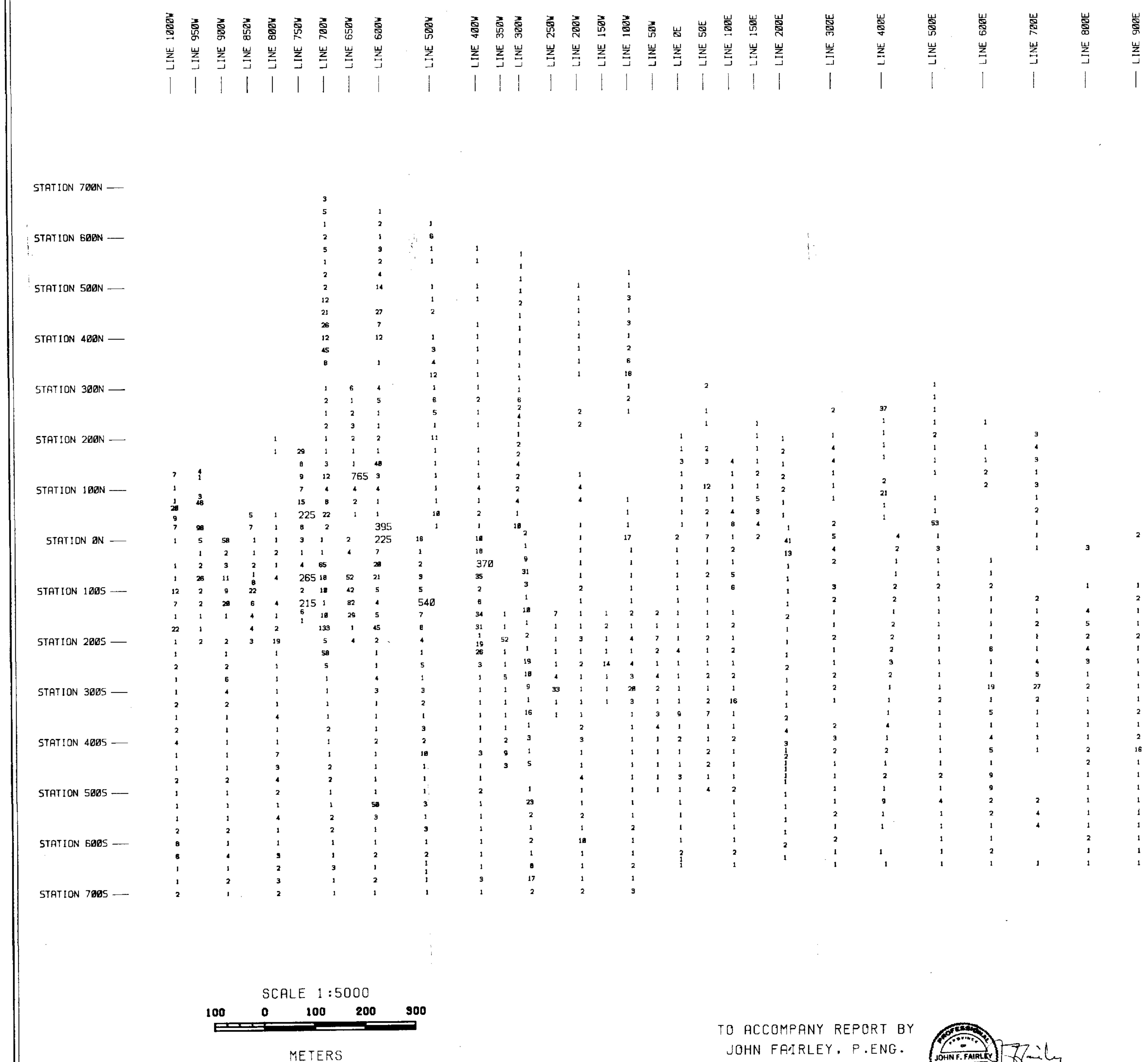
16,203

PROFESSIONAL ENGINEER — PROVINCE OF BRITISH COLUMBIA — JOHN F. FAIRLEY

TO ACCOMPANY REPORT BY J. FAIRLEY, B.A. Sc., P. ENG.

MATSON PROJECT	
FOR: KELSO RESOURCES LTD.	
BY: MOUNTAINSIDE MANAGEMENT LTD.	
MATSON GEOLOGY (OFF GRID) LILLOOET M.D., B.C.	
N.T.S. 92J-16E	DATE JULY 1987
DRAWN BY D.K	FIGURE Nº. 3


LEGEND
REXMOUNT PORPHYRY
1a COARSE GRAINED GRANODIORITE
1b APHANITIC PORPHYRITIC TRACHYTE
1c APHANITIC APLITE DYKES & CONTACT FEATURES
BRIDGE RIVER GROUP
2a ALTERED SILTSTONES (HORNFELS), MASSIVE CHERT, PHYLLITES
2b MASSIVE GREY RECRYSTALLIZED LIMESTONE
2c MASSIVE QUARTZITES, OFTER ARGILLACEOUS AND / OR GOSSANOUS
2d MASSIVE METABASALT (GREENSTONE), OFTEN SILICEOUS
OUTCROP
STRIKE / DIP OF BEDDING PLANES, FAULTS
" " FOLIATION
TREND & PLUNGE OF LINEATION
x MK 29 SAMPLE LOCATION & Nº.
ADIT
GEOLOGICAL CONTACT
SHEAR ZONE, FAULT
O.B. OVERBURDEN
PIT
Q.V. QUARTZ VEIN
CLIFF
SNOW
See Fig. 2
See Fig. 3
See Fig. 4
Serpentinite
B.L.
10+00W
5+00W
0+00
5+00E
SCALE 1:2500
0 50 100 200 Metres
TO ACCOMPANY REPORT BY J. FAIRLEY, B.A.Sc., P.ENG.
GEOLOGICAL BRANCH ASSESSMENT REPORT
16,203
MATSON PROJECT
FOR: KELSO RESOURCES LTD.
BY: MOUNTAINSIDE MANAGEMENT LTD.
MATSON GEOLOGY
LILLOOET M.D., B.C.
N.T.S. 92J-16E
DATE: JULY 1987
DRAWN BY: D.K.
FIGURE Nº 4



VALUES IN PPB

VALUES OVER 200 PPB IN LARGE CHARACTERS

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PROFESSIONAL ENGINEER — JOHN F. FAIRLEY

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PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.	
GOLD GEOCHEMISTRY	
LILLOET M.D., B.C.	
N.T.S.: 92J 16E	DATE: JULY 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8A

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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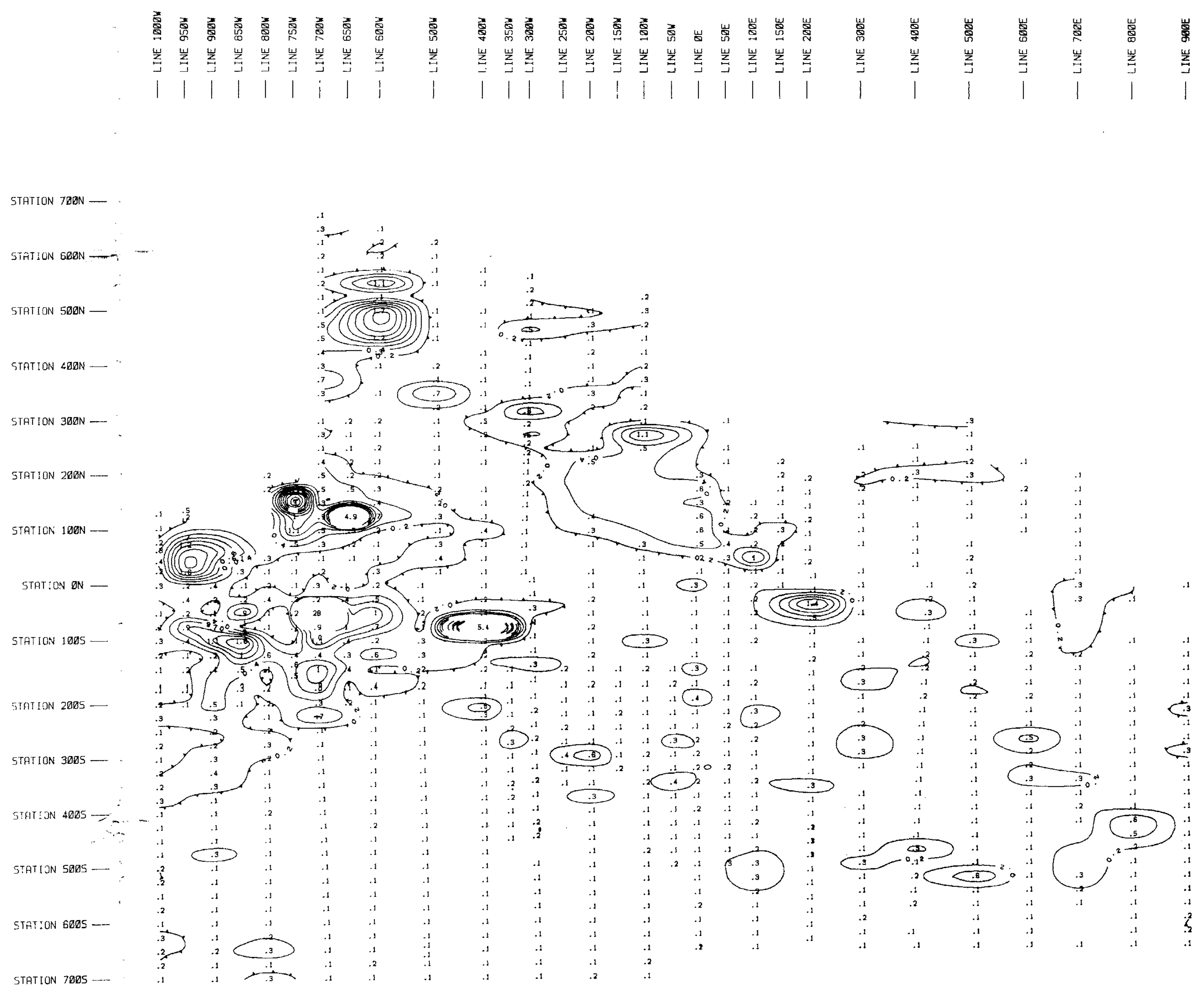

CONTOUR INTERVAL: 0.2 PPM

SCALE 1:5000

100 0 100 200 300

METERS

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SILVER GEOCHEMISTRY

VALUES IN PPM

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GEOLOGICAL BRANCH
ASSESSMENT REPORT

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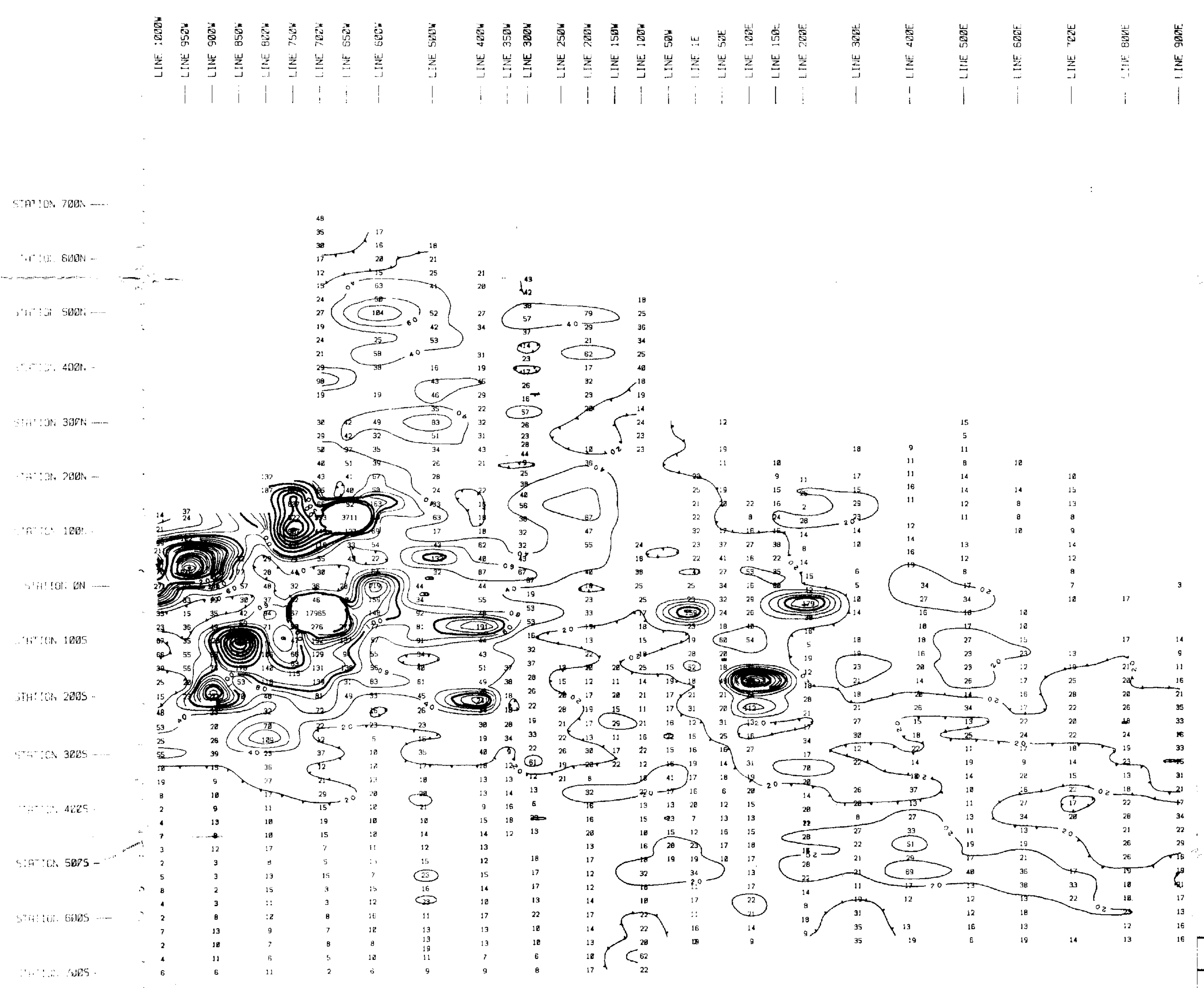

CONTOUR INTERVAL: 20 PPM

SCALE 1:5000

100 0 100 200 300

METERS

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LEAD GEOCHEMISTRY

VALUES IN PPM

LILLOET M.D., B.C.

N.T.S.: 92J 16E	DATE: JULY 1987
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ASSESSMENT REPORT

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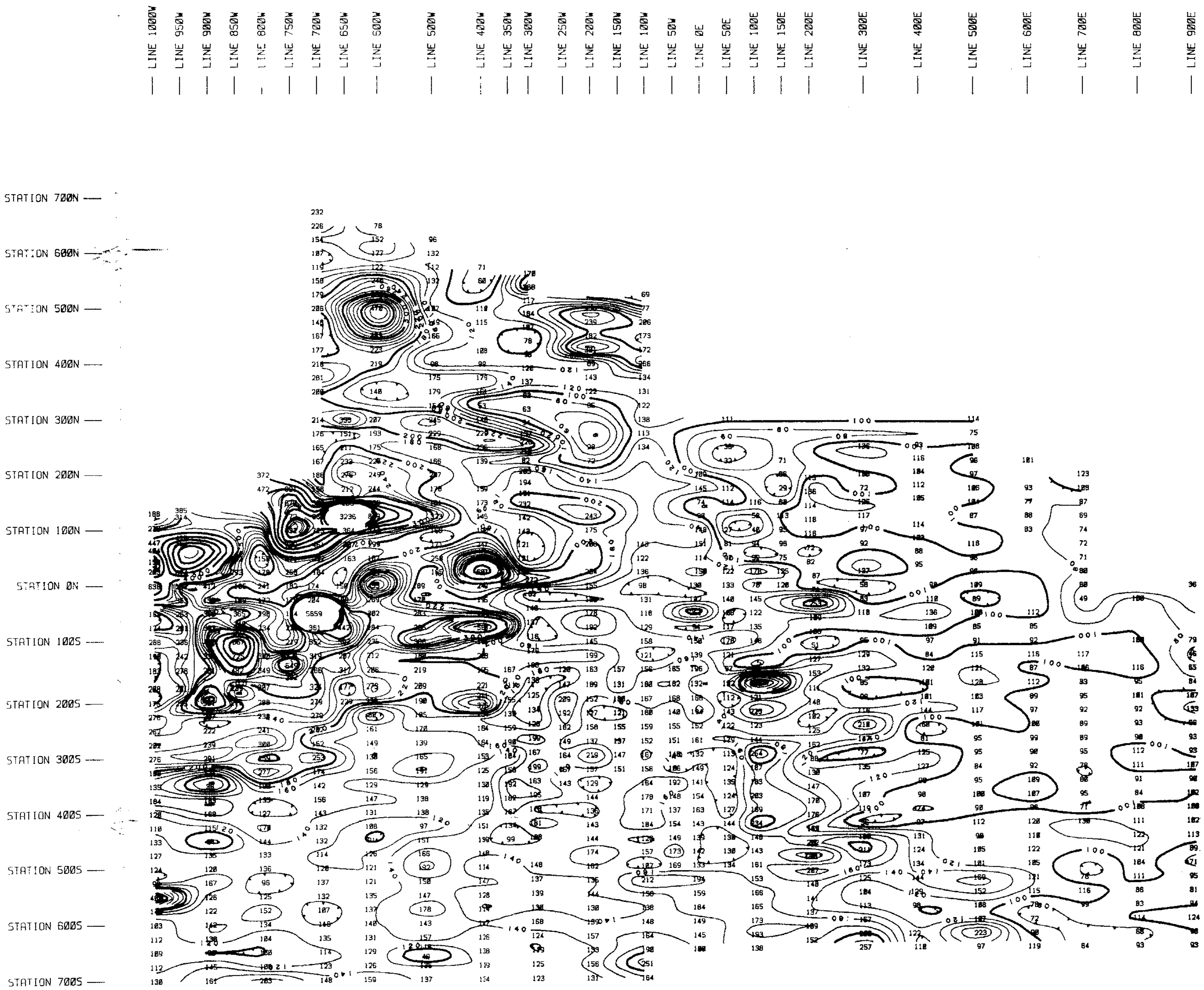

CONTOUR INTERVAL: 20 PPM

SCALE 1:5000

100 0 100 200 300

METERS

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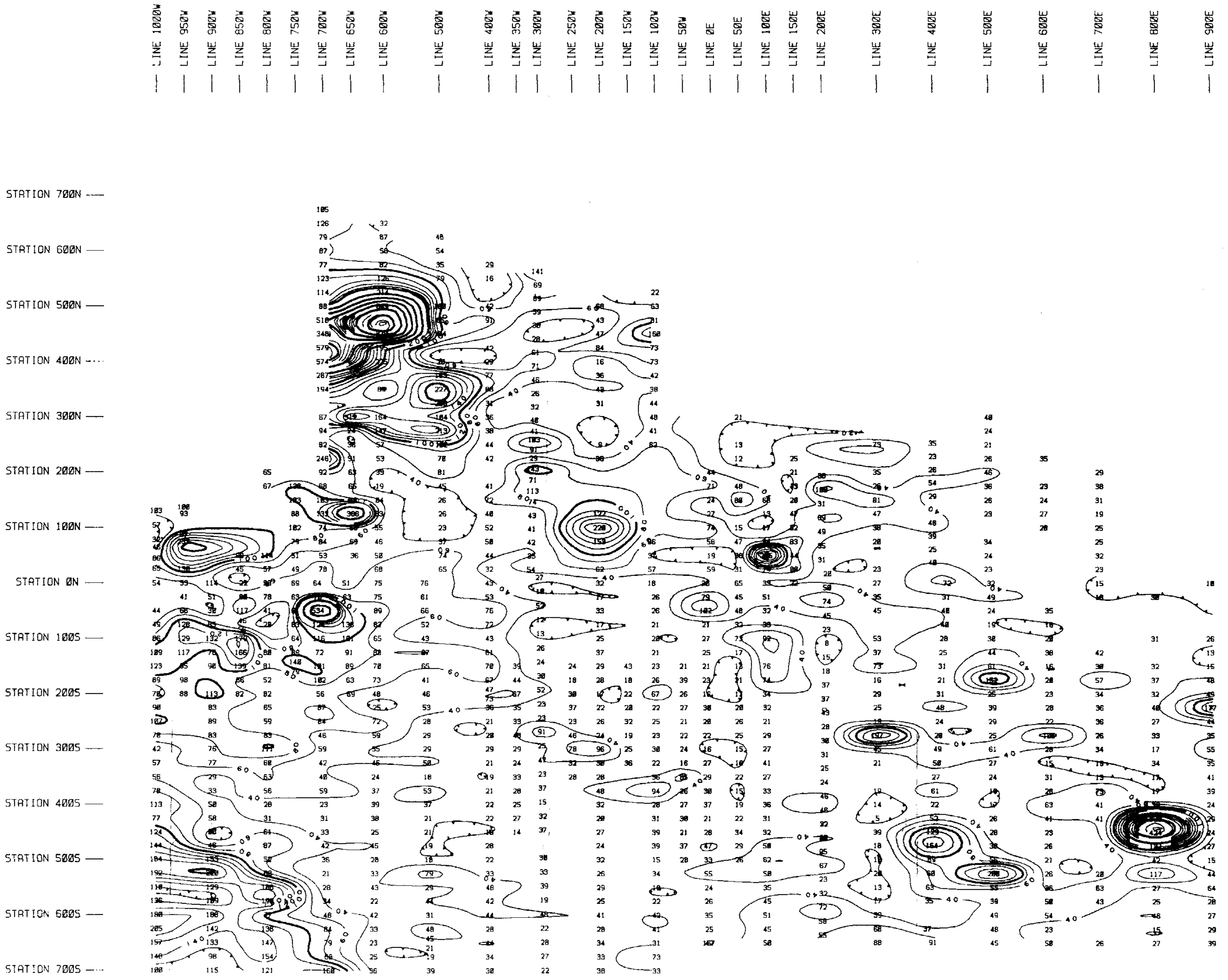
ZINC GEOCHEMISTRY

VALUES IN PPM

LILLOET M.D., B.C.

N.T.S.: 92J 16E	DATE: JULY 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8E



SCALE 1:5000

100 0 100 200 300

METERS

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,203

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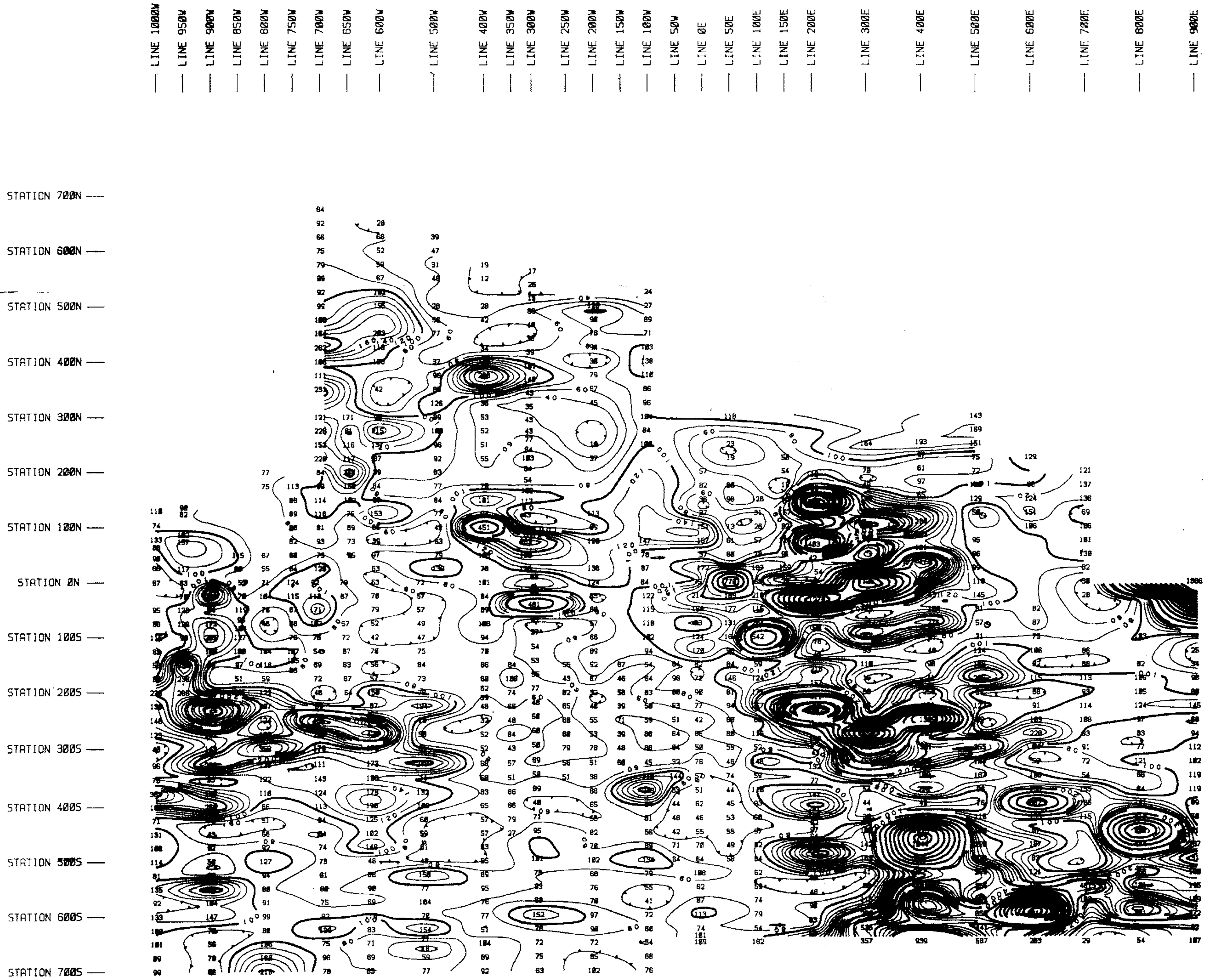
COPPER GEOCHEMISTRY VALUES IN PPM LILLOET M.D., B.C.	
N.T.S.: 92J 16E	DATE: JULY 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8F



CONTOUR INTERVAL: 20 PPM

SCALE 1:5000

100 0 100 200 300

METERS

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MATSON PROJECT

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NICKEL GEOCHEMISTRY

VALUES IN PPM

LILLOET M.D., B.C.

N.T.S.: 92J 16E	DATE: JULY 1987
PLOTTED BY: R.P.M.	FIGURE NO. 80

GEOLOGICAL BRANCH ASSESSMENT REPORT

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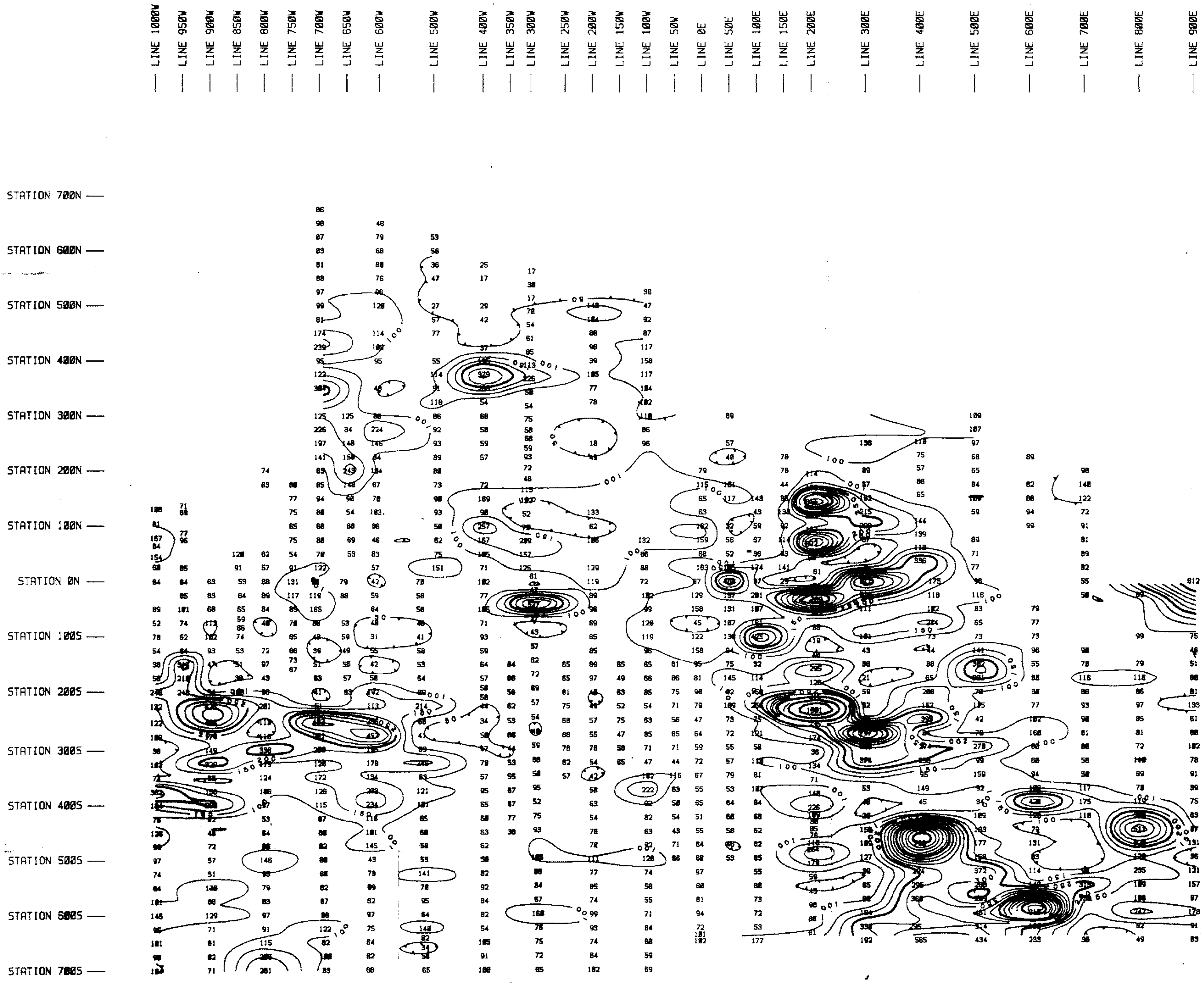

CONTOUR INTERVAL: 50 PPM

SCALE 1:5000

100 0 100 200 300

METERS

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PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.	
CHROMIUM GEOCHEMISTRY VALUES IN PPM LILLOET M.D., B.C.	
N.T.S.: 92J 10E	DATE: JULY 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8H

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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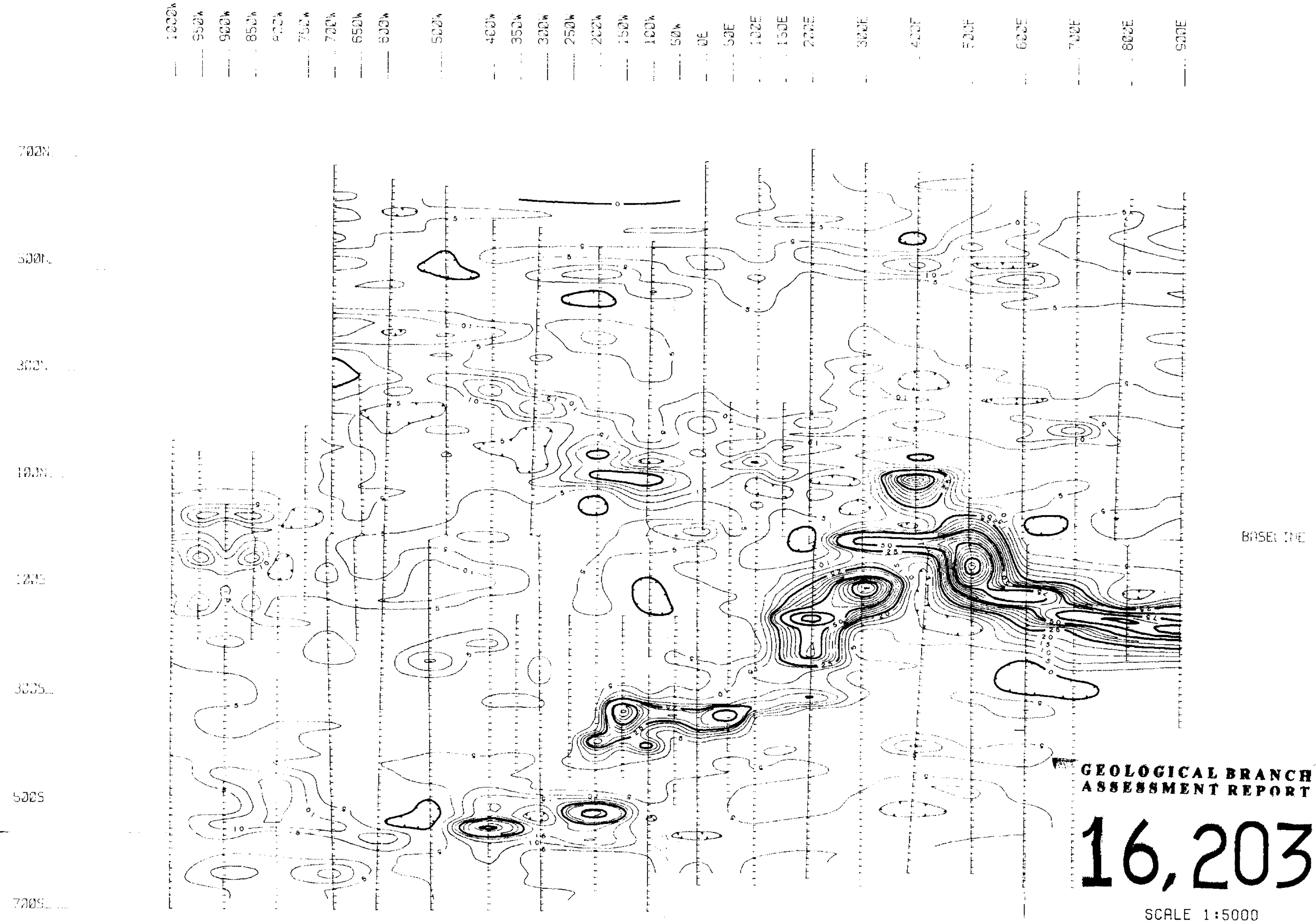

GEOLOGICAL BRANCH ASSESSMENT REPORT

16,203

SCALE 1:5000

100 0 100 200 300

METERS

MATSON PROJECT
FOR: KELSO RESOURCES LTD.
BY: MOUNTAINSIDE MANAGEMENT LIMITED
PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.
VLF-EM FRASER FILTERED CONTOUR MAP LILLOET M.D., B.C.

N.T.S.: 92J / 18E	DATE: AUGUST 1987
PLOTTED BY: R.P.M.	FIGURE NO. 9

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CONTOUR INTERVAL: 5 PERCENT