87-544 - 16218

6/88

GEOCHEMICAL REPORT

ON THE

ARLINGTON PROPERTY

GAM 1 AND 2 CLAIMS

SLOCAN MINING DIVISION

WESTERN KOOTENAY AREA

SOUTHEASTERN BRITISH COLUMBIA

NTS 82F /14W

49°48'12" 117°20'30"

FOR

Operator: **LIGHTNING CREEK MINES LTD.**

SUITE 13 - 1155 MELVILLE STREET

VANCOUVER, BRITISH COLUMBIA

V6E 4C4

Owner: Sveinson Way Mineral Services Ltd.

PREPARED BY

STILLWATER ENTERPRISES LTD.

2891 WEST 14TH AVENUE

VANCOUVER, BRITISH COLUMBIA

V6K 2X3

JOANNE C. FREEZE, F.G.A.C.

AUGUST, 1987

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INTRODUCTION

This reports discusses the geology and geochemistry of a silver occurrence in the Selkirk Mountains of Southeastern British Columbia. Mineralization was discovered in the area in 1861 and has been investigated by trenching, geophysics and diamond drilling. The claims are held by S. W. Resources Ltd. Lightning Creek Mines Ltd. has a joint venture agreement with S. W. Resources to earn a 50% interest in the property.

In June of 1987, J.F. Wetherill and W. Robb, geologists with Stetson Resource Management Corp. carried out a geochemical and geological program under the direction of the writer.

LOCATION AND ACCESS

The Birch Point Property is located 11 km east of Slocan City on the southeast shore of Slocan Lake at latitude 49° 48' and longitude 117° 21' on N.T.S. Map Sheet 82F/14W.

Access is via dirt road from Slocan City which is located on Highway 6 and extends from Silverton to Castlegar.

PHYSIOGRAPHY

The property covers steep topography which is covered by alders and jackpine at lower elevations and alpine scrubs and grass above 6232 feet (1900 metres). Elevations range from 4690 feet (1430 metres) to 6790 feet (2070 metres) above sea level. Snow cover lingers, limiting geological and geochemical exploration from June to mid October. Springer Creek drains the property to the southwest and Speculator Creek drains it to the south.

LIGHTNING CREEK MINES LTD.

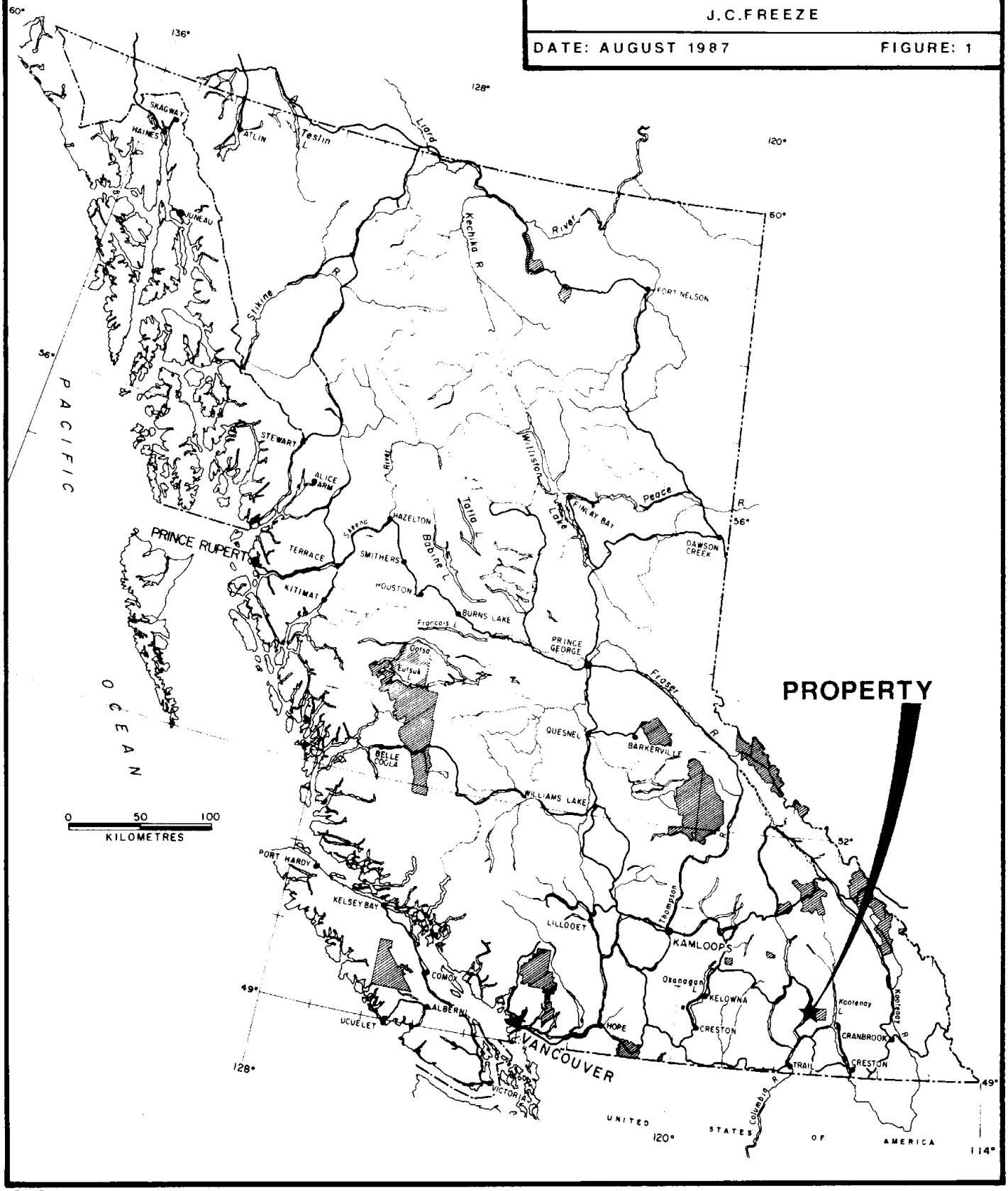
ARLINGTON PROPERTY

SLOCAN M.D., B.C. NTS: 82 F/14 W

LOCATION MAP

J.C.FREEZE

DATE: AUGUST 1987 FIGURE: 1



RWR

PROPERTY

The property comprises 6 contiguous claims and is situated in the Slocan Mining Division. Six (6) of the claims are crown grants, 3 are reverted crown grants , all of which are in mining leases, the rest are modified grid claims. All claims are held by S.W. Resources. Ltd.

Claim Name	Record No.	Lease No.	No. Units	Record Date	Expiry Date
Mineral Claims					
Gam 1	2552		8	06/06/81	1988
Gam 2	2553		18	06/05/81	1988
New Silver 1	4576		1	01/03/85	1988
New Silver 2	4577		1	01/03/85	1988
New Silver 3	4578		1	01/03/85	1988
New Silver 4	4579		1	01/03/85	1988
Crown Grants	Lot No.				
Silver Leaf No.2	5763		1		
Arlington No.2	2416		1		
Stephanite Fr.	2356		1		
Burlington No. 2	2417		1		
Speculator	2360		1		
Mineral Mt.	2362		1		
Reverted Crown Grants					
Speculator Fr.		M80	1	08/27/63	1987
Eda Fr.		M79	1	08/27/63	1987
Nancy		M79	1	08/27/63	1987

Lightning Creek Mines Ltd. has a joint venture agreement with S.W. Resources Ltd. to earn a 50% interest in the property.

HISTORY

Silver, lead and zinc with minor gold and cadmium mineralization typifies the Slocan area. Mineralization was discovered in the Slocan area in 1861. Silver production from the area exceeds 74 million ounces (Henneberry, 1986). Silver mineralization occurs in veins, shears and replacements usually with lead and/or zinc mineralization. The veins extend over a few thousand metres along strike and over 500 metres down dip. The mineralization occurs either within the middle Jurassic Nelson Batholith or in the intruded Slocan Group.

The Arlington Property was originally staked in 1894 and put in to production in 1899. By 1903 three quarters of a million ounces of silver was mined. "Final production for the mine to 1980 is 1,010,606 ounces of silver from 22,643 tons of ore for an average grade of 44.6 ounces of silver per ton". (Henneberry, 1986)

In 1981, Sveinson Way Mineral Services acquired an option for 50% of the property from Western Arlington Silver Mines the predecessor to Lightning Creek Mines Ltd. A program of detailed surface and underground evaluation of the property was carried out. The program included soil sampling, geological mapping and underground data assessment. According to Henneberry (1986) the geochemistry and geophysics indicated the possible existence of a hanging wall structure either parallel to or splaying from the Arlington Shear.

In 1986, Lightning Creek Mines Ltd. carried out a soil sampling program to test for the possible existence of parallel structures. Coincident silver-lead-zinc anomalies were outlined, however, they are weak suggesting that the hanging wall structures may not be well mineralized.

GEOLOGY AND MINERALIZATION

The Arlington property is underlain by the middle Jurassic Nelson Batholith. The batholith comprises coarse grained hornblende granite to granodiorite. Dykes of coarse grained plagioclase feldspar crosscut the intrusive.

Mineralization consists of galena and sphalerite in association with disseminated stephanite, tetrahedrite and native silver. Pyrite and chalcopyrite are also present but not economically significant. The mineralization occurs as a crushed zone in both the hanging wall and the footwall of the Arlington Shear which strikes 034° and dips 65° to 70° easterly.

CURRENT WORK

Stetson Resource Management Corp. carried out a geochemical sampling program from May 29 to June 5, 1987.

'B' horizon soil sampling was carried out on lines extending the 1986 grid towards the north. This grid covers the hanging wall of the Arlington shear. Samples were collected at 25 metre intervals on lines trending 124° spaced 200 and 100 metres apart. A total of 193 soil samples and 5 rock samples were collected. All samples were collected from the 'B' soil horizon with the aid of a lightweight mattock and were sent to Acme Analytical Laboratory in Vancouver for analysis.

In the laboratory, samples were oven dried at 60° C. Subsamples, 30 grams in weight, were sieved to -80 mesh. A .5 gram sample was digested in HCl-HNO3-H20 at 95° C.

In assessing the soil geochemical results, graphical statistical methods were used to separate background from anomalous metal concentrations. Threshold and anomalous levels were determined at the mean plus two standard deviations (x+2s) and the mean plus three standard deviations (x+3s), respectively, from log probability plots prepared for each element. This data is given in Table 2. Sample locations and analytical results are shown on Map 3.

ELEMENT	N	MEAN(X)	THRESHOLD(X+2S)	ANOMALOUS(X+3S)
Ag	193	0.1 ppm	0.4 ppm	0.7 ppm
Pb	193	11 ppm	30 ppm	50 ppm
Zu	193	60 ppm	90 ppm	140 ppm

Anomalous silver and lead values coincide within a larger zone of anomalous zinc values at the south end of the grid. Towards the north half of the grid several zones of anomalous silver values outlined patterns somewhat paralleling the north Arlington Shear. These zones do not exceed 200 metre strike lengths. As was noted by Henneberry (1986), zinc has too wide a dispersion pattern to outline mineralized zones. The silver-lead and silver anomalies are weak to moderate indicating weakly mineralized structures.

CONCLUSIONS

Geochemical anomalies in the soils above the hanging wall of the Arlington Shear indicate the possible existence of mineralized structures paralleling or splaying from the main Arlington Shear.

Exploration in the hanging wall to date is limited. Additional 'B' horizon soil sampling as well as follow up geological mapping should be carried out.

Respectfully submitted,
STILLWATER ENTERPRISES LTD.

Joanne C. Freeze, F.G.A.C.

COST STATEMENT

GEOCHEMICAL ANALYSIS:	193 soils @ $6.75/sample	$ 1,302.75
	4 rocks @ $9.00/sample	$ 36.00
	1 rock @ $13.75/sample	13.75
FOOD:	12 man days @ $25/day	$ 300.00
ACCOMMODATION:	5 nights @ $40.00/nite	$ 200.00
VEHICLE:	4x4 truck 6 days @ $60/day	$ 360.00
	2300 kms. @ .18/km	414.00
	Fuel	223.98
MISCELLANEOUS:	Equipment Rental	$ 20.45
	Supplies	$ 522.67
REPORT WRITING, DRAFTING REPRODUCTION:		$ 448.14

PERSONNEL:

J.C. Freeze,	Geologist	2 days @ $300/day	$ 600.00
J.F. Wetherill	Geologist	6 days @ $225/day	$ 1,350.00
W.D. Robb	Geologist	7 days @ $175/day	$ 1,225.00
		SUB TOTAL	$ 7,016.70
ADMINISTRATION OVERHEAD @ 10%			$ 701.67
		TOTAL COST	$ 7,718.41

STATEMENT OF QUALIFICATIONS

NAME: Freeze, J. C. (nee Ridley), F.G.A.C.

PROFESSION: Consulting Geologist

EDUCATION: 1981 B.Sc. Geology - University of British Columbia.

1978 B.A. Geography
University of Western Ontario

PROFESSIONAL ASSOCIATIONS: Fellow of the Geological Association of Canada

EXPERIENCE: 1986 - present: Consulting Geologist and principal of Stillwater Enterprises Ltd. Consulting in mineral exploration programs in B.C., Yukon, Ontario.

1985 - 1986: Consulting Geologist with White Geophysical Inc.

Coordinating mineral exploration projects involving geology, geochemistry, geophysics and diamond drilling in B.C. and Yukon.

1981 - 1985: Project Geologist with Mark Management Ltd. Hughes-Long Group. Responsible for precious metals exploration programs involving geology, geochemistry, geophysics and diamond drilling in Western Canada and U.S.A.

1979 - 1981: Summer and part-time Geologist involved with coal exploration in N.E. B.C. with Utah Mines Ltd.

REFERENCES

Cairnes, C.E. 1935 — Descriptions of Properties, Slocan Mining Camp, British Columbia Memoir 184 Geological Survey of Canada.

Henneberry, R.J. 1986 — Gam 1 and Gam 2 Mineral Claims. Slocan Mining Division - Soil Geochemistry of the Arlington Shear hanging wall.

APPENDIX I

ANALYTICAL RESULTS

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-ROCK P2-7 SOILS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JUNE 8 1987 DATE REPORT MAILED: June 15/87 ASSAYER: D. Toye DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON RESOURCE File # 87-1641 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
ARLINTON A1	1	7	9	7	.2	1	1	104	.34	2	7	ND	12	17	1	2	2	1	.29	.001	2	1	.02	7	.01	2	.15	.05	.13	1	-
ARLINTON A2	2	5	8	53	.1	5	5	488	2.06	2	5	ND	12	18	1	2	2	37	.44	.089	13	45	.74	106	.18	4	.94	.10	.88	3	-
ARLINTON A3	2	165	8081	11215	407.1	2	4	3694	2.32	4	5	ND	3	71	60	13	2	2	2.35	.018	6	1	.28	80	.01	4	.23	.01	.18	1	-
ARLINTON A4	2	93	10854	11937	273.2	1	8	6946	9.21	4	5	ND	1	236	75	22	2	1	.32	.003	2	1	.36	40	.01	9	.01	.01	.01	1	-
SM-1	2	83	228	313	81.4	71	6	364	8.17	10	5	ND	7	34	1	2	2	10	.06	.083	13	6	.22	1124	.01	2	.52	.01	.20	1	5

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
N39 5+75E	3	19	18	88	.1	7	5	223	3.46	2	5	ND	7	8	1	2	2	48	.08	.170	8	26	.47	50	.23	3	5.07	.02	.10	1
N39 6+00E	3	14	12	115	.2	6	7	349	5.98	4	5	ND	3	9	1	2	7	71	.11	.093	12	26	.72	49	.12	3	2.66	.01	.09	1
N39 6+25E	41	12	15	23	.2	1	3	111	2.66	2	5	ND	1	5	1	2	2	35	.07	.052	6	6	.14	44	.16	2	1.42	.02	.06	1
N39 6+50E	1	13	27	63	.1	1	4	216	4.13	8	5	ND	3	7	1	2	2	61	.11	.053	8	15	.34	35	.20	2	2.21	.02	.07	1
N39 6+75E	1	10	11	40	.1	4	4	112	3.39	5	5	ND	6	4	1	2	2	36	.05	.114	8	9	.19	27	.13	2	5.40	.02	.04	2
N39 7+00E	1	12	18	85	.1	5	7	357	7.51	6	5	ND	21	7	1	2	2	72	.09	.169	32	15	.52	28	.20	2	2.75	.01	.10	1
N39 7+25E	1	12	22	19	.2	1	2	70	3.13	7	5	ND	4	3	1	4	2	34	.04	.066	6	8	.09	20	.15	4	3.67	.02	.03	1
N39 7+50E	1	11	12	54	.1	4	3	166	3.72	3	5	ND	7	6	1	3	2	37	.06	.077	12	10	.25	32	.15	2	4.69	.01	.06	1
N39 8+00E	1	9	13	45	.1	3	3	145	2.60	2	5	ND	3	6	1	2	2	33	.05	.047	19	6	.22	34	.08	3	1.73	.02	.05	2
N39 8+25E	1	8	18	37	.3	4	3	120	2.88	6	5	ND	3	5	1	2	2	33	.05	.055	8	7	.15	32	.16	2	2.84	.02	.05	1
N39 8+50E	1	6	16	62	.2	4	4	185	2.66	2	5	ND	7	7	1	2	2	32	.09	.078	13	7	.32	45	.13	8	1.86	.02	.09	1
N39 8+75E	1	9	6	20	.5	3	2	64	2.68	2	5	ND	4	5	1	2	3	32	.05	.075	7	7	.09	26	.15	2	4.17	.02	.02	1
N39 9+00E	1	6	16	85	.2	5	4	196	4.40	4	5	ND	7	6	1	2	2	43	.07	.139	20	10	.36	40	.07	2	1.93	.01	.10	1
N39 9+25E	1	8	23	63	.3	1	3	149	3.14	2	5	ND	1	16	1	2	2	29	.09	.046	14	6	.16	92	.07	2	1.38	.02	.04	1
N39 9+50E	1	11	11	73	.1	5	4	231	4.86	6	5	ND	12	8	1	2	2	52	.12	.069	25	10	.38	27	.18	5	2.46	.01	.08	1
N39 9+75E	1	8	18	10	.1	2	1	25	.90	2	5	ND	1	4	1	2	2	14	.02	.039	8	3	.04	20	.10	2	1.12	.02	.02	1
N39 10+00E	1	11	22	76	.2	7	5	276	5.48	9	5	ND	5	8	1	2	2	60	.08	.100	14	12	.44	40	.20	2	2.42	.01	.11	1
N39 10+25E	1	8	16	50	.2	5	3	218	3.58	2	5	ND	5	9	1	2	2	43	.11	.071	9	9	.28	30	.14	4	1.60	.01	.06	1
N39 10+50E	1	12	12	60	.4	6	6	281	3.32	4	5	ND	4	8	1	2	2	45	.05	.078	11	12	.35	63	.13	2	4.43	.02	.05	1
N39 10+75E	1	9	13	22	.4	3	2	77	2.00	2	5	ND	3	4	1	2	2	39	.04	.040	5	16	.11	36	.20	2	1.63	.02	.03	1
N39 11+00E	1	9	8	80	.1	7	4	219	3.21	2	5	ND	7	8	1	2	2	39	.07	.071	9	13	.35	39	.19	2	4.70	.02	.05	1
N39 11+25E	1	8	18	23	.1	4	2	68	1.60	5	5	ND	1	6	1	2	2	26	.05	.098	6	5	.09	22	.15	4	.86	.01	.04	1
N39 11+50E	1	17	20	76	.1	14	9	1405	2.74	2	7	ND	3	39	1	2	2	59	.31	.079	34	62	.68	122	.20	4	2.15	.03	.10	1
N39 11+75E	1	11	15	103	.1	9	7	338	4.61	2	5	ND	11	12	1	2	2	52	.26	.177	25	25	.76	78	.13	2	2.37	.02	.09	1
N39 12+00E	1	10	16	37	.1	3	4	364	1.91	2	5	ND	3	8	1	2	2	30	.05	.035	11	8	.14	65	.09	2	1.19	.02	.04	1
N39 12+25E	1	17	13	57	.2	16	6	225	3.91	2	5	ND	5	12	1	2	2	51	.15	.079	12	29	.49	75	.21	3	2.67	.02	.06	1
N39 12+50E	1	11	6	83	.2	4	5	456	3.90	2	5	ND	5	14	1	2	2	47	.28	.124	12	9	.48	79	.24	2	2.81	.03	.06	1
N39 12+75E	1	8	11	63	.2	6	5	204	3.09	5	5	ND	9	12	1	2	2	36	.13	.093	16	12	.37	39	.16	3	3.91	.02	.06	1
N38+75 5+75E	4	18	27	129	.2	8	8	417	4.60	7	5	ND	7	10	1	2	3	70	.14	.106	14	24	.71	66	.12	2	3.32	.01	.09	1
N38+75 7+75E	1	14	14	61	.1	2	5	199	5.26	2	5	ND	5	8	1	3	2	60	.11	.084	10	12	.33	40	.19	5	2.07	.01	.09	1
N38+75 12+75E	1	10	10	51	.1	2	4	212	2.92	2	5	ND	2	11	1	2	3	39	.18	.060	7	9	.35	45	.22	2	1.79	.02	.06	1
N38+50 5+75E	3	13	20	94	.1	8	5	315	3.58	3	5	ND	3	8	1	2	2	49	.09	.094	11	16	.39	43	.11	2	3.94	.02	.06	1
N38+50 7+75E	1	9	46	116	.1	3	6	257	4.91	3	5	ND	5	10	1	2	2	41	.14	.122	21	8	.44	61	.01	3	3.01	.01	.09	1
N38+50 12+75E	1	9	5	63	.1	6	6	258	3.42	2	5	ND	2	19	1	2	2	41	.29	.126	7	9	.43	81	.22	2	2.65	.02	.08	1
N38+25 5+75E	2	12	16	43	.1	1	4	176	4.41	4	5	ND	2	5	1	2	2	59	.05	.059	11	11	.12	42	.16	2	3.08	.02	.02	1
N38+25 7+75E	1	11	16	39	.2	4	3	146	2.98	7	5	ND	4	6	1	3	2	35	.05	.096	11	10	.18	35	.13	3	4.08	.02	.04	2
STD C/AU-S	19	60	35	123	7.4	64	26	922	3.93	37	15	6	32	43	16	18	20	55	.45	.086	37	53	.84	162	.08	38	1.70	.06	.12	14

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
N38+25 12+75E	1	11	11	34	.2	4	3	147	3.24	6	5	ND	4	6	1	2	2	35	.11	.157	5	6	.16	24	.17	3	4.01	.02	.03	1
N38 5+50E	1	11	29	129	.1	4	5	302	5.46	6	5	ND	4	10	1	2	2	55	.11	.134	14	10	.33	44	.08	4	1.67	.01	.07	1
N38 7+50E	1	13	13	101	.1	6	4	365	3.61	8	5	ND	5	8	1	2	2	39	.08	.183	9	9	.46	58	.15	4	3.21	.02	.09	1
N38 12+50E	1	9	16	78	.1	3	4	211	3.57	2	5	ND	9	8	1	2	2	39	.13	.102	15	11	.40	35	.14	4	3.00	.01	.05	1
N37+75 5+50E	1	11	17	38	.1	4	3	101	3.29	4	5	ND	2	6	1	2	2	44	.03	.060	15	9	.15	32	.09	2	1.59	.01	.04	1
N37+75 7+50E	1	17	11	56	.1	4	3	192	3.53	9	5	ND	4	5	1	2	2	41	.06	.092	7	9	.29	34	.17	2	4.97	.02	.05	1
N37+75 12+50E	1	11	19	31	.1	3	2	110	3.31	2	5	ND	4	5	1	2	2	47	.06	.052	8	10	.17	29	.22	2	1.70	.01	.04	1
N37+50 5+50E	2	12	49	170	.1	9	6	305	3.90	7	5	ND	7	9	1	2	3	39	.08	.092	22	14	.47	45	.04	4	3.43	.01	.07	1
N37+50 7+50E	1	12	19	59	.1	6	4	164	4.91	6	5	ND	6	5	1	2	2	49	.06	.103	16	10	.26	29	.13	2	2.83	.01	.05	1
N37+50 12+50E	1	13	22	48	.1	3	4	130	3.47	6	5	ND	6	6	1	2	2	48	.06	.088	8	19	.29	30	.20	2	2.64	.01	.06	1
N37+25 5+50E	2	9	27	58	.2	6	4	165	3.22	5	5	ND	5	8	1	2	2	45	.05	.060	14	9	.20	42	.07	4	1.64	.01	.06	1
N37+25 7+50E	1	11	12	32	.2	2	2	88	2.64	2	5	ND	4	5	1	2	2	29	.04	.087	7	6	.14	25	.14	2	4.59	.02	.03	1
N37+25 12+50E	1	12	20	87	.1	6	6	243	5.05	2	5	ND	9	10	1	2	2	46	.12	.142	12	17	.46	30	.18	2	2.58	.01	.07	1
N37 5+50E	3	13	29	81	.5	6	4	240	3.18	2	5	ND	2	7	1	3	2	38	.06	.102	17	10	.30	44	.10	2	2.24	.01	.05	1
N37 5+75E	2	13	20	66	.1	4	3	346	4.34	8	5	ND	3	6	1	2	3	51	.06	.146	9	10	.26	44	.12	2	1.68	.01	.05	1
N37 6+00E	2	13	33	85	.1	8	5	246	3.86	3	5	ND	4	11	1	2	2	45	.09	.063	13	10	.32	69	.06	4	2.56	.01	.04	1
N37 6+25E	3	15	16	73	.1	7	5	251	3.24	2	5	ND	3	8	1	2	2	40	.07	.092	10	9	.31	60	.13	2	3.91	.02	.04	1
N37 6+50E	2	13	22	137	.1	6	9	543	4.80	3	5	ND	5	12	1	2	3	60	.17	.118	16	21	.81	89	.13	4	3.83	.01	.13	1
N37 6+75E	4	11	17	102	.2	8	6	487	3.88	6	5	ND	3	10	1	2	2	48	.15	.085	10	18	.60	58	.15	2	1.85	.02	.12	1
N37 7+00E	3	10	17	54	.1	4	4	164	3.87	5	5	ND	4	6	1	2	3	42	.10	.082	14	8	.32	38	.12	6	4.12	.01	.04	1
N37 7+25E	1	12	19	42	.1	2	4	184	3.72	3	5	ND	3	6	1	2	2	39	.05	.091	8	9	.18	42	.11	3	3.13	.01	.03	1
N37 7+50E	1	10	12	47	.1	3	3	138	3.17	2	5	ND	4	5	1	2	2	36	.06	.082	7	7	.19	30	.11	4	2.51	.02	.04	2
N37 7+75E	1	8	15	58	.2	4	5	211	4.39	4	5	ND	8	6	1	2	2	53	.06	.124	10	11	.29	32	.18	5	1.93	.01	.09	1
N37 8+00E	1	11	15	37	.1	4	3	130	2.56	7	5	ND	2	6	1	2	2	31	.06	.103	6	7	.13	30	.13	3	3.14	.02	.04	1
N37 8+25E	1	12	13	76	.5	4	4	152	3.63	5	5	ND	4	7	1	2	2	34	.06	.055	16	9	.20	53	.07	3	3.27	.02	.05	1
N37 8+50E	1	13	43	70	.6	6	4	231	3.99	5	5	ND	3	6	1	2	3	39	.05	.064	19	8	.28	35	.07	4	2.00	.01	.08	1
N37 8+75E	1	9	16	71	.1	8	5	223	3.95	4	5	ND	7	8	1	2	2	38	.11	.058	24	9	.41	37	.12	2	2.09	.01	.08	1
N37 9+25E	1	8	17	40	.1	3	3	142	2.77	4	5	ND	2	8	1	2	2	30	.06	.044	9	5	.13	46	.12	2	1.14	.02	.03	2
N37 9+50E	1	12	10	59	.1	5	4	260	2.95	6	5	ND	2	7	1	2	2	30	.06	.096	18	9	.28	38	.09	2	2.77	.01	.06	1
N37 9+75E	1	9	19	72	.3	5	5	341	3.30	4	5	ND	1	7	1	2	2	32	.09	.108	14	6	.29	52	.08	4	2.03	.02	.08	1
N37 10+00E	1	7	19	61	.2	4	4	154	2.72	2	5	ND	2	7	1	2	3	35	.04	.057	24	8	.24	62	.05	2	1.54	.01	.08	1
N37 10+25E	1	14	9	75	.1	6	6	247	3.63	6	5	ND	9	8	1	2	2	44	.12	.175	16	13	.44	37	.19	7	4.24	.02	.11	1
N37 10+50E	1	14	26	37	.1	4	3	106	2.50	3	5	ND	4	5	1	2	2	36	.05	.123	6	8	.13	46	.13	5	2.93	.02	.04	1
N37 10+75E	1	12	15	92	.1	6	5	258	4.60	3	5	ND	7	8	1	2	2	51	.09	.059	12	13	.45	31	.18	7	2.98	.01	.10	1
N37 11+00E	1	15	17	48	.2	6	4	141	2.88	3	5	ND	6	5	1	2	2	40	.06	.108	6	12	.25	25	.17	5	4.87	.02	.07	1
N37 11+25E	1	6	9	53	.1	4	3	135	2.53	2	5	ND	6	5	1	2	3	28	.05	.066	9	6	.26	25	.13	2	2.88	.01	.05	1
STD C/AU-S	17	58	36	133	6.8	66	28	910	3.93	40	15	7	32	43	15	18	21	54	.44	.091	35	51	.87	161	.07	37	1.71	.06	.11	14

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
N37 11+50E	1	9	21	78	.3	6	4	238	3.36	4	8	ND	9	8	1	7	2	37	.12	.093	14	10	.43	39	.17	6	3.17	.01	.14	2
N37 11+75E	1	12	17	53	.1	4	3	185	3.59	3	5	ND	11	7	1	3	3	39	.11	.159	10	9	.27	34	.17	2	3.96	.02	.07	2
N37 12+00E	1	10	15	46	.2	5	4	156	3.30	2	5	ND	8	6	1	2	2	45	.09	.105	10	24	.32	31	.19	4	3.50	.01	.05	1
N37 12+25E	1	11	20	34	.3	3	3	112	3.71	8	5	ND	9	6	1	7	2	46	.05	.140	9	10	.19	31	.16	3	3.25	.01	.04	4
N37 12+50E	1	12	13	42	.1	6	3	131	4.71	4	5	ND	12	6	1	6	2	43	.06	.083	9	12	.23	26	.17	3	4.68	.01	.05	2
N36+75 7+50E	1	11	25	94	.1	6	6	539	5.29	4	5	ND	5	7	1	2	2	58	.05	.102	22	14	.40	46	.12	4	2.66	.01	.08	1
N36+50 7+50E	1	12	30	71	.4	5	4	321	3.28	9	6	ND	3	9	1	3	2	36	.08	.203	11	9	.30	54	.07	3	2.61	.01	.06	3
N36+25 7+50E	1	10	18	53	.2	5	3	161	3.34	2	5	ND	7	5	1	3	3	35	.05	.069	10	7	.28	34	.11	3	4.48	.01	.05	1
N36 7+25E	1	10	20	71	.1	5	4	215	5.39	6	5	ND	3	8	1	2	2	73	.08	.170	10	9	.40	41	.16	2	2.19	.01	.07	1
N35+75 7+25E	3	11	24	70	.3	4	5	229	3.23	5	7	ND	4	6	1	5	2	44	.06	.075	10	19	.35	51	.12	2	3.08	.01	.06	2
N35+50 7+25E	3	10	22	63	.1	3	4	274	3.67	2	5	ND	2	6	1	2	2	44	.06	.097	8	15	.26	57	.12	2	2.47	.02	.04	1
N35+25 7+25E	4	13	26	90	.1	3	5	351	6.14	5	5	ND	4	6	1	2	2	59	.06	.268	10	15	.37	57	.13	2	2.63	.02	.07	1
N35 6+25E	2	12	32	117	.4	13	7	679	4.06	4	7	ND	5	15	1	5	2	52	.09	.129	14	26	.44	136	.14	4	1.51	.02	.10	1
N35 6+50E	2	12	29	128	.1	11	9	619	4.91	4	5	ND	5	17	1	2	2	64	.13	.091	21	27	.64	129	.11	2	1.78	.02	.11	2
N35 6+75E	3	8	29	63	.3	4	4	191	2.91	3	6	ND	3	8	1	3	2	43	.10	.076	8	10	.23	56	.15	3	1.53	.02	.07	2
N35 7+00E A	3	10	31	90	.1	5	6	257	4.82	5	5	ND	6	8	1	2	2	59	.11	.151	12	21	.52	49	.11	4	2.45	.01	.10	2
N35 7+00E B	4	9	12	76	.1	7	5	250	4.58	3	5	ND	4	9	1	2	2	58	.10	.193	9	17	.39	53	.15	2	2.56	.02	.07	2
N35 7+25E	5	10	26	90	.6	4	5	277	3.60	2	5	ND	4	8	1	3	2	44	.11	.080	21	14	.44	58	.14	3	3.38	.02	.09	2
N35 7+50E	1	9	18	32	.3	3	2	106	3.40	5	6	ND	5	5	1	5	2	44	.04	.058	8	8	.13	34	.17	3	2.09	.01	.04	3
N35 7+75E	1	12	17	77	.1	5	7	296	4.64	4	5	ND	4	9	1	2	2	82	.20	.168	9	11	.74	61	.22	3	3.10	.02	.20	3
N35 8+00E	1	11	21	67	.6	6	4	256	3.44	2	5	ND	6	6	1	4	3	42	.10	.145	11	7	.33	43	.15	2	3.01	.02	.09	1
N35 8+25E	1	11	15	91	.1	5	5	314	5.21	4	5	ND	5	7	1	3	4	49	.06	.082	18	13	.41	41	.11	6	3.39	.01	.09	1
N35 8+50E	1	14	14	63	.1	5	4	234	3.47	3	5	ND	5	6	1	4	2	38	.05	.090	11	9	.27	37	.13	2	4.12	.01	.07	1
N35 8+75E	1	9	11	34	1.0	4	2	128	2.17	3	5	ND	4	6	1	3	2	31	.04	.048	13	6	.12	44	.08	3	1.44	.01	.04	3
N35 9+00E	2	11	24	65	1.6	4	3	191	2.64	2	5	ND	1	10	1	2	3	30	.09	.057	16	8	.28	88	.07	2	2.17	.02	.06	1
N35 9+25E	1	12	16	75	2.9	6	4	282	3.16	3	5	ND	1	12	1	4	2	34	.12	.084	17	9	.32	69	.09	2	2.76	.02	.07	1
N35 9+50E	1	10	14	43	.5	6	3	132	3.52	2	7	ND	7	5	1	5	2	38	.04	.138	7	10	.19	40	.14	2	3.80	.02	.05	3
N35 9+75E	1	10	12	45	.2	3	3	155	3.06	2	6	ND	5	5	1	4	3	29	.04	.100	11	9	.20	41	.09	4	3.91	.01	.04	3
N35 10+00E	1	11	16	66	.2	5	3	173	2.65	5	5	ND	8	7	1	6	2	31	.05	.085	10	10	.28	39	.12	3	4.10	.01	.07	3
N35 10+25E	1	9	15	67	.2	6	4	197	3.46	3	8	ND	20	7	1	4	4	40	.05	.110	13	11	.30	36	.15	3	3.82	.01	.08	2
N35 10+50E	1	8	9	90	.1	5	5	249	4.77	4	5	ND	18	10	1	2	2	51	.08	.105	20	13	.54	37	.17	2	3.20	.01	.13	1
N35 10+75E	1	9	16	65	.2	3	3	205	3.57	2	5	ND	27	9	1	3	3	40	.13	.168	27	10	.33	32	.13	6	4.14	.01	.08	1
N35 11+00E	1	8	16	47	.3	3	3	183	3.26	4	7	ND	10	7	1	4	2	39	.08	.140	12	8	.22	35	.17	4	3.50	.02	.06	3
N35 11+25E	1	11	13	80	.1	1	4	271	3.64	2	5	ND	13	11	1	2	3	41	.16	.161	25	8	.46	49	.17	4	3.10	.02	.13	1
N35 11+50E	1	9	15	91	.1	6	4	279	3.85	2	5	ND	19	9	1	2	2	40	.12	.166	18	9	.44	41	.16	5	3.90	.02	.12	1
N35 11+75E	1	11	14	78	.1	6	4	255	4.58	2	5	ND	10	8	1	2	2	48	.11	.147	15	11	.43	43	.19	3	3.22	.01	.11	2
STD C/AU-S	18	55	39	126	6.8	64	27	962	3.96	38	16	6	31	46	16	16	22	58	.43	.094	34	53	.85	172	.08	37	1.71	.06	.12	15

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
N35 12+00E	2	12	23	63	.3	5	5	206	3.59	2	5	ND	8	7	1	2	2	45	.09	.116	12	11	.31	47	.19	2	3.71	.02	.09	1
N34+75 7+25E	4	11	31	111	.3	7	7	324	4.94	4	5	ND	10	11	1	2	2	64	.15	.075	18	19	.74	100	.15	2	2.97	.02	.13	1
N34+75 12+00E	2	12	21	74	.1	8	4	231	3.76	3	5	ND	9	8	1	2	2	43	.09	.135	14	11	.36	42	.17	2	3.35	.01	.09	1
N34+50 7+25E	3	12	72	98	.2	12	8	355	4.60	6	5	ND	6	42	1	2	2	69	.49	.256	25	28	.91	137	.19	2	2.06	.02	.17	1
N34+50 12+00E	1	9	19	96	.3	8	6	415	3.22	2	5	ND	15	8	1	2	2	39	.12	.102	22	10	.46	47	.14	2	3.36	.01	.14	1
N34+25 7+25E	3	16	23	133	.6	8	7	598	4.21	2	5	ND	4	12	1	2	2	67	.18	.103	12	28	.73	87	.21	2	2.20	.02	.12	1
N34+25 12+00E	2	11	17	99	.1	5	6	307	4.35	2	5	ND	15	8	1	2	2	52	.11	.138	21	14	.53	50	.18	3	4.47	.02	.17	1
N34 7+00E	3	14	82	429	.7	12	8	532	4.53	4	5	ND	5	20	1	2	2	59	.27	.092	21	25	.88	108	.17	2	2.41	.02	.15	1
N34 11+75E	2	10	19	69	.3	7	5	276	3.17	2	5	ND	12	9	1	2	2	40	.09	.100	16	10	.44	49	.15	2	3.93	.02	.13	1
N33+75 7+00E	3	11	22	74	.7	6	4	214	4.55	4	5	ND	3	12	1	3	2	53	.08	.148	12	15	.25	59	.14	2	1.51	.01	.05	1
N33+75 11+75E	1	11	24	88	.3	5	6	256	3.37	5	5	ND	10	10	1	2	2	49	.15	.095	13	18	.55	45	.18	2	2.43	.02	.14	1
N33+50 7+00E	3	18	33	79	.7	22	8	360	4.40	3	5	ND	3	30	1	4	2	70	.21	.146	24	49	.76	120	.22	2	1.95	.02	.07	1
N33+50 11+75E	1	8	22	84	.1	7	5	278	3.29	2	5	ND	10	10	1	2	2	42	.12	.098	13	11	.44	52	.15	2	2.76	.02	.12	1
N33+25 7+00E	3	13	27	97	.3	7	5	260	4.19	3	5	ND	4	10	1	3	2	53	.09	.146	14	18	.37	57	.11	2	2.66	.01	.07	1
N33+25 11+75E	1	8	11	83	.2	7	5	431	2.79	2	5	ND	10	10	1	2	2	36	.12	.089	13	8	.36	56	.13	2	2.28	.01	.11	1
N33 6+00E	3	9	24	80	1.4	6	3	305	2.36	4	5	ND	1	19	1	2	2	30	.20	.093	25	11	.25	77	.05	2	1.90	.03	.07	1
N33 6+25E	2	10	22	81	.1	7	5	253	5.00	2	5	ND	2	11	1	2	2	65	.14	.136	13	15	.40	48	.10	2	2.21	.01	.07	1
N33 6+50E	2	6	26	36	.2	4	3	187	3.00	3	5	ND	1	7	1	2	2	47	.06	.078	8	10	.17	44	.15	2	1.47	.02	.04	1
N33 6+75E A	2	12	19	78	.5	8	4	403	3.61	2	5	ND	2	11	1	2	2	47	.10	.120	12	15	.32	65	.13	2	2.05	.02	.06	1
N33 6+75E B	2	8	20	108	.3	6	6	321	3.90	2	5	ND	4	18	1	2	2	57	.21	.072	12	11	.55	103	.16	2	2.50	.02	.11	1
N33 7+00E	4	11	27	82	.9	8	5	292	3.63	2	5	ND	4	11	1	2	2	56	.09	.099	13	20	.38	61	.17	2	2.94	.02	.06	1
N33 7+25E	4	12	18	66	.2	8	4	235	3.84	2	5	ND	3	8	1	2	2	64	.08	.065	8	18	.35	46	.18	2	2.19	.01	.06	1
N33 7+50E	3	10	25	84	.2	6	5	235	3.97	3	5	ND	3	8	1	2	2	55	.08	.059	11	13	.37	50	.12	2	1.95	.01	.08	2
N33 7+75E	3	9	26	38	.6	3	3	331	3.41	3	5	ND	1	5	1	2	2	43	.05	.132	8	6	.14	35	.15	2	1.76	.02	.04	1
N33 8+00E	3	10	19	48	.2	3	3	201	2.36	2	5	ND	1	6	1	2	2	31	.05	.064	9	6	.16	43	.11	2	2.56	.02	.04	1
N33 8+25E	6	11	15	82	.1	5	4	582	2.79	2	5	ND	3	9	1	2	2	38	.09	.078	15	13	.31	62	.14	2	2.40	.02	.08	1
N33 8+50E	3	6	27	129	.2	5	5	361	3.88	6	5	ND	10	9	1	2	2	41	.17	.136	22	10	.49	63	.11	2	2.58	.01	.12	1
N33 8+75E	4	8	17	31	.2	3	2	100	2.39	2	5	ND	3	4	1	2	2	27	.04	.048	8	7	.15	32	.09	2	2.26	.01	.04	1
N33 9+00E	3	10	22	68	.2	6	4	209	3.74	2	5	ND	5	7	1	2	2	42	.08	.106	15	11	.30	48	.12	3	3.39	.01	.08	1
N33 9+25E	2	9	17	66	.5	6	4	218	3.63	2	5	ND	5	7	1	2	2	48	.10	.080	11	17	.40	47	.18	2	3.29	.02	.08	1
N33 9+50E	1	7	26	88	2.8	6	5	254	3.34	2	5	ND	4	12	1	2	4	39	.11	.054	24	9	.42	68	.10	2	2.71	.02	.10	1
N33 9+75E	1	7	15	79	.3	4	3	208	3.34	2	5	ND	7	6	1	2	2	36	.07	.107	12	9	.29	52	.11	2	3.22	.01	.07	1
N33 10+00E	2	11	27	54	.1	5	3	177	3.72	2	5	ND	11	6	1	2	2	41	.07	.076	12	13	.23	36	.16	2	4.32	.01	.06	1
N33 10+25E	1	12	19	82	.1	16	6	228	3.04	2	5	ND	10	17	1	2	2	42	.09	.109	19	18	.56	124	.17	4	3.99	.02	.10	1
N33 10+50E	1	8	16	88	.1	7	4	218	2.97	2	5	ND	6	9	1	2	2	35	.07	.090	11	9	.34	49	.12	2	2.84	.01	.09	1
N33 10+75E	1	8	13	84	.1	6	4	254	3.09	2	5	ND	12	10	1	2	2	34	.10	.085	12	9	.36	49	.11	3	3.00	.02	.09	1
STD C/AU-S	19	58	39	130	6.8	65	27	972	3.94	38	17	6	32	45	16	16	18	59	.46	.092	34	55	.85	172	.08	35	1.67	.06	.13	13

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
N33 11+00E	1	9	15	77	.1	6	5	238	2.82	4	5	ND	14	9	1	2	2	33	.08	.069	13	8	.40	44	.13	2	3.42	.02	.08	1
N33 11+25E	1	8	27	110	.3	5	4	301	3.20	6	5	ND	16	8	1	3	2	39	.08	.104	13	10	.37	47	.15	5	3.75	.02	.10	2
N33 11+50E	1	9	12	76	.1	5	4	342	2.65	5	5	ND	8	8	1	2	2	34	.10	.139	11	7	.30	61	.14	2	2.25	.02	.10	1
N33 11+75E	1	9	16	94	.2	5	5	271	3.41	4	5	ND	10	9	1	2	2	40	.10	.105	12	10	.36	48	.18	3	3.28	.02	.11	2
N32+75 6+75E	1	12	22	86	.5	5	6	721	3.53	6	5	ND	3	10	1	2	2	53	.12	.088	13	10	.46	74	.11	4	1.76	.02	.11	1
N32+50 6+75E	2	11	18	55	.4	5	4	197	3.09	4	5	ND	4	11	1	2	2	39	.10	.169	11	10	.24	51	.12	4	3.15	.02	.05	2
N32+25 6+75E	1	11	21	31	.4	2	2	122	3.14	4	5	ND	3	6	1	3	2	38	.06	.075	10	9	.10	34	.13	2	2.76	.02	.03	4
N32 6+50E	1	12	23	62	.1	5	4	206	4.28	4	5	ND	5	8	1	2	2	51	.10	.191	12	15	.34	51	.13	3	3.14	.02	.07	2
N31+75 6+50E	1	11	23	75	.1	6	5	250	3.59	2	5	ND	1	11	1	2	2	47	.15	.127	17	12	.45	63	.08	2	2.18	.02	.08	1
N31+50 6+50E	1	10	23	60	.5	3	3	300	2.69	3	5	ND	3	7	1	2	2	33	.08	.175	10	10	.17	40	.10	2	3.44	.02	.03	1
N31+25 6+50E	1	7	34	101	.6	5	6	1171	3.11	3	5	ND	2	11	1	2	2	38	.13	.132	22	10	.40	72	.05	2	1.99	.01	.09	2
N28 6+25E	1	9	16	72	.3	6	4	249	3.21	2	5	ND	1	15	1	2	2	39	.17	.084	17	11	.41	69	.08	2	1.95	.02	.10	1
N28 7+00E	1	11	35	196	1.3	7	5	319	2.73	2	5	ND	1	27	1	2	2	45	.26	.088	42	19	.46	107	.09	3	2.75	.02	.12	1
N28 7+25E	1	6	26	97	.3	4	5	310	2.83	4	5	ND	3	17	1	2	2	35	.26	.082	16	9	.46	98	.10	2	1.62	.02	.14	1
N28 7+50E	1	10	22	79	.3	5	6	312	3.07	2	5	ND	1	11	1	2	2	35	.15	.076	20	11	.36	72	.11	2	1.77	.02	.08	1
N28 7+75E	1	11	90	47	6.4	6	4	222	2.71	88	5	ND	2	10	1	586	2	33	.10	.085	15	10	.26	62	.14	2	2.30	.02	.05	3
N28 8+00E	1	7	246	67	.4	4	4	242	2.76	11	5	ND	4	8	1	2	2	40	.12	.114	12	11	.30	45	.11	2	1.76	.02	.06	1
N28 8+25E	1	6	19	59	.1	5	4	288	3.06	7	5	ND	3	9	1	2	2	47	.08	.081	11	11	.26	53	.11	6	1.27	.02	.06	1
N28 8+50E	1	9	24	105	.1	6	6	391	3.52	6	5	ND	8	11	1	2	2	47	.12	.154	12	15	.42	62	.13	5	3.18	.02	.09	2
N28 8+75E	1	7	25	132	.2	8	8	495	4.26	3	5	ND	5	17	1	2	2	55	.20	.157	25	24	.49	113	.14	5	2.37	.02	.10	1
N28 9+00E	1	7	26	87	.5	4	6	243	3.91	3	5	ND	5	9	1	2	2	61	.11	.088	13	17	.42	68	.14	6	1.97	.02	.09	1
N28 9+25E	1	11	34	151	.8	18	9	785	3.62	6	5	ND	6	24	1	2	3	51	.29	.191	18	24	.80	141	.15	8	2.33	.02	.14	1
N28 9+50E	1	11	19	123	.1	26	11	1619	4.08	3	5	ND	5	25	1	2	2	62	.25	.172	23	46	.94	194	.16	8	2.38	.02	.12	1
N28 9+75E	1	16	22	143	.2	49	14	695	4.95	4	6	ND	10	43	1	2	2	79	.45	.213	25	47	1.56	338	.35	4	3.03	.02	.21	1
N28 10+00E	1	14	15	130	.1	22	11	579	4.20	2	5	ND	8	26	1	2	2	79	.32	.154	20	35	1.19	201	.23	6	2.62	.02	.20	1
N28 10+25E	1	8	33	164	.2	12	10	932	4.59	2	5	ND	13	24	1	2	2	70	.27	.189	23	34	1.04	181	.14	8	3.03	.02	.15	1
N28 10+50E	1	9	23	156	.1	6	7	719	3.73	3	5	ND	7	19	1	2	2	48	.32	.331	18	21	.61	134	.16	3	2.28	.02	.14	1
N28 10+75E	1	6	27	128	.1	3	6	308	3.48	2	5	ND	10	16	1	2	2	35	.22	.164	28	10	.58	159	.01	5	2.27	.01	.15	1
N28 11+00E	2	9	27	93	.1	16	9	1260	3.42	2	16	ND	7	102	1	2	2	44	.83	.128	48	40	.65	157	.05	5	1.66	.01	.15	1
N28 11+25E	1	6	13	79	.1	4	6	322	3.24	2	5	ND	5	18	1	2	2	46	.27	.091	21	14	.55	63	.10	9	1.51	.02	.13	1
N26 6+50E	1	7	25	89	.1	2	4	201	3.78	5	5	ND	2	20	1	2	2	45	.15	.151	9	10	.23	110	.14	4	1.96	.02	.05	1
N26 6+75E	1	5	12	138	.1	3	9	643	4.67	2	5	ND	2	34	1	2	2	64	.37	.051	15	14	.89	127	.12	5	2.12	.02	.11	1
N26 7+00E	2	7	26	114	.2	5	7	1177	3.24	6	5	ND	3	37	1	2	2	45	.35	.040	19	15	.47	120	.12	4	1.96	.02	.09	1
N26 7+25E	1	6	21	90	.1	5	5	445	2.67	4	5	ND	3	14	1	2	2	43	.13	.060	11	12	.26	136	.13	6	1.07	.02	.07	1
N26 7+50E	1	9	22	87	.1	6	5	210	3.85	3	5	ND	8	10	1	2	2	49	.11	.230	13	16	.33	51	.12	8	3.01	.02	.06	1
N26 7+75E	1	8	18	66	.4	6	4	176	2.40	6	5	ND	5	8	1	2	2	33	.06	.095	11	16	.27	47	.14	3	3.89	.02	.03	1
STD C/AU-S	18	56	42	128	7.1	63	27	969	3.84	40	16	6	32	46	16	17	19	59	.46	.099	34	56	.93	170	.08	34	1.71	.06	.13	13

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
N26 8+00E	1	11	17	123	.6	9	7	513	3.61	7	5	ND	9	16	1	4	2	50	.18	.137	16	21	.43	90	.14	2	3.42	.03	.11	1
N26 8+25E	1	4	25	97	.2	10	5	349	3.38	4	5	ND	6	12	1	2	2	48	.15	.125	14	15	.34	94	.15	2	2.45	.02	.09	1
N26 8+50E	1	5	18	130	.2	9	6	824	2.98	3	5	ND	5	14	1	2	2	44	.14	.150	11	19	.28	145	.17	2	2.58	.02	.09	1
N26 8+75E	1	4	24	133	.3	9	7	352	3.55	8	5	ND	9	17	1	2	3	50	.21	.115	19	19	.47	109	.12	2	2.31	.02	.16	1
N26 9+00E	1	4	66	142	.2	5	6	590	3.50	7	5	ND	8	18	1	2	2	32	.14	.079	28	12	.30	147	.03	2	1.99	.01	.21	1
N26 9+25E	1	9	54	226	.3	9	9	1325	4.19	3	6	ND	14	18	1	3	3	40	.11	.160	34	14	.36	212	.08	2	2.85	.01	.22	1
N26 9+50E	1	7	52	226	.1	6	7	1164	3.86	2	5	ND	8	20	1	2	2	36	.16	.200	27	14	.30	172	.06	2	2.35	.01	.17	1
N26 9+75E	1	11	61	262	.5	5	8	2523	3.17	6	6	ND	7	23	1	2	2	35	.18	.142	20	11	.25	358	.07	2	2.00	.02	.12	1
N26 10+00E	1	8	55	281	1.4	12	9	1229	4.33	5	5	ND	13	45	1	2	2	51	.37	.156	31	21	.70	327	.14	2	2.81	.02	.22	1
N26 10+25E	1	8	35	223	.5	11	9	579	4.25	3	5	ND	11	23	1	2	2	52	.25	.218	21	22	.70	181	.16	4	2.82	.02	.21	1
N26 10+50E	1	11	24	153	.8	8	8	624	3.71	6	5	ND	10	15	1	3	2	50	.17	.240	17	16	.46	161	.14	2	3.06	.02	.16	1
N26 10+75E	1	7	24	107	.4	8	6	463	3.31	3	5	ND	8	19	1	2	2	43	.27	.180	25	16	.52	97	.11	2	2.27	.02	.14	1
N26 11+00E	1	9	33	161	1.0	11	7	561	3.73	2	5	ND	6	21	1	2	2	50	.21	.106	27	23	.56	186	.07	2	2.95	.02	.15	1
STD C/AU-S	19	59	38	132	6.7	65	28	990	3.97	42	17	7	32	47	17	16	19	61	.48	.095	35	56	.91	176	.08	36	1.73	.07	.14	13

473600 474000 474400 474800

N

ABANDONED MINE

CREEK

EDA FRACTION 2363

MINERAL MOUNTAIN 2362

MINERAL LEASE 80

SPECULATOR 2360

NANCY 5259

SHAFT A-1

ADIT A-3

GAM2

GAM 1

BURLINGTON 2417

NEW SILVER 4 4579

STEPHANITE FR. 2356

ARLINGTON Nº 2 2416

NEW SILVER 3 4578

NEW SILVER 2 4577

SILVER LEAF 5763

NEW SIVER 1 4576

400E 500E

L 39+00 N

L 37+00 N

L 35+00 N

L 33+00 N

L 31+00 N

L 29+00 N

L 28+00 N

L 27+00 N

L 26+00 N

L 25+00 N

ARLINGTON BASIN

ABANDONED MINE

LCP LCP

LEGEND:

1.4, 581, 65 SILVER, ZINC, LEAD RESULTS IN P.P.M.

GEOCHEM. CONTOUR INTERVALS

SILVER 0.4 & 0.7 PPM

ZINC 70 & 140 P.P.M.

LEAD 30 & 50 P.P.M.

CONTOUR INTERVAL - 10 m COMPILED FROM 1:54 000 SCALE PHOTOGRAPHY (BC820351) PRODUCED BY PACIFIC INTERNATIONAL MAPPING CORP.

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,218

0 100 200 300 400 500
SCALE 1:5000

LIGHTNING CREEK MINES LTD.

ARLINGTON PROPERTY
GAM CLAIMS

SLOCAN M.D., B.C. NTS: 82 F/14 W

GEOCHEMICAL SURVEY

Ag, Zn & Pb RESULTS

BY: J.C.F.

DATE: AUGUST 1987

FIGURE: 2