

87-606-16265  
8/88

SOIL AND ROCK GEOCHEMICAL  
REPORT ON THE LUCKY AND  
LUCKY 2 CLAIMS, JURA AREA

SIMILKAMEEN M. D.  
BRITISH COLUMBIA

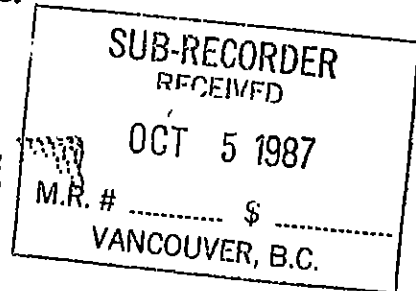
*Operator:* MINGOLD RESOURCES INC.

900A - 837 W. HASTINGS ST.

VANCOUVER, B. C.

*Owner(s): Mingold Resources Inc.  
Peter Peto*

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**



**16,265**

NTS: 92H9/W

Lat: 49°32'30"42"

Long: 120°26'00"

BY: K. J. TAYLOR

DATE: SEPT. 15, 1987

FILMED

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## INTRODUCTION

The Lucky claims were obtained under an option agreement between Mr. Peter Peto of Penticton, B. C. and Mingold Resources Inc.. These claims cover an area previously explored by Kenneco Exploration and Quintana Minerals for its porphyry copper potential. Mingold's interest in the ground was spurred by the presence of anomalous accessory gold values up to 420 ppb. Systematic rock and soil geochemical surveys were carried out by Mingold personnel from June 14-18, 20 and 23, 1987. Details and results of these surveys are elaborated on in the following report.

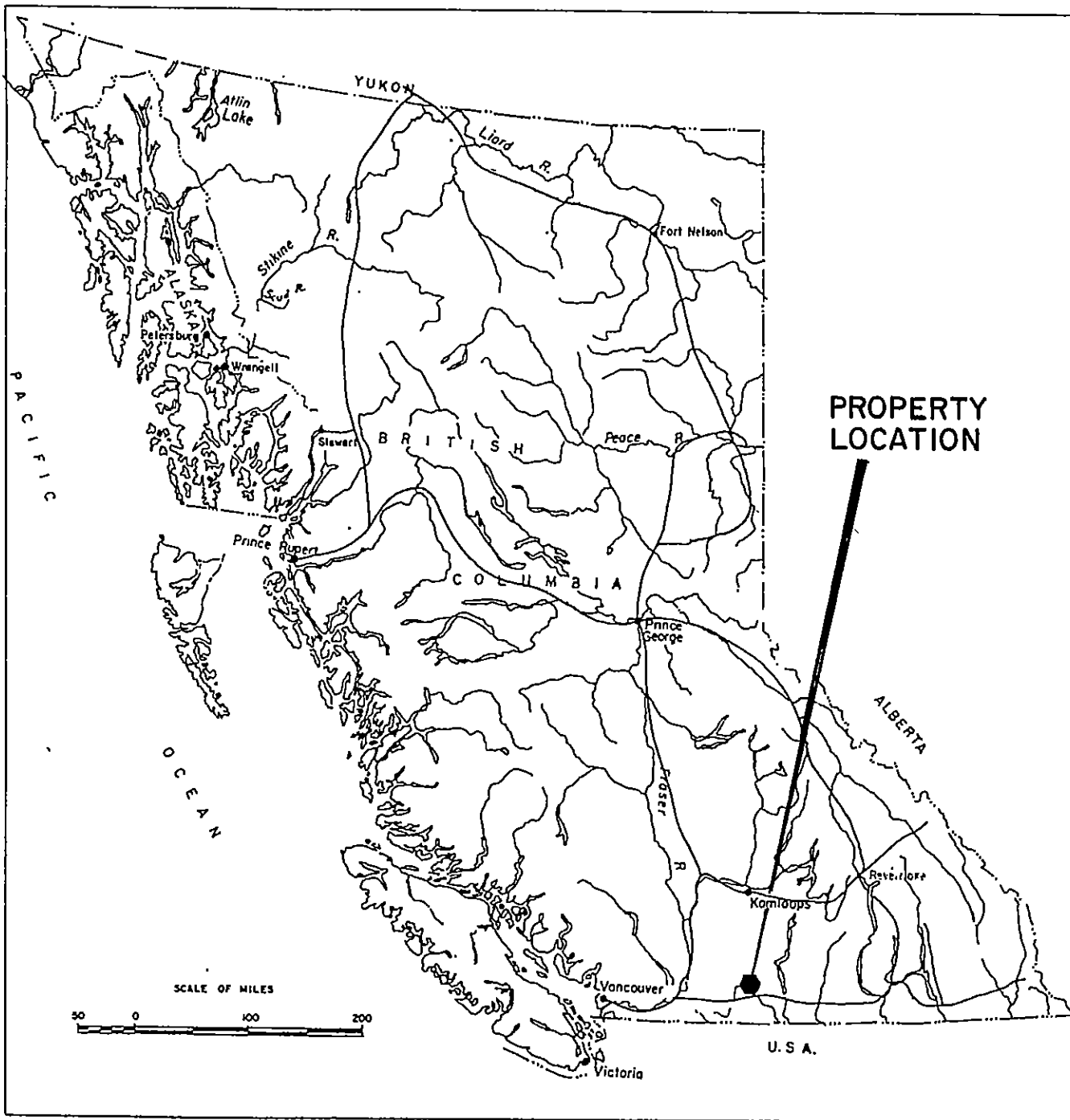
## LOCATION & ACCESS

The property straddles the Princeton-Summerland Highway near the Jura railway siding approximately 18 kilometers by road from Princeton. Hayes Creek lies along the eastern boundary of the claims and Christian Creek along the northern boundary. Topography slopes moderate to steeply to the east into the Hayes Creek Valley. Most of the area is devoid of trees, consisting of grassy rangeland.

## CLAIMS

The Lucky and Lucky 2 claims cover a 12 unit block staked under the modified grid system. The Lucky claims were staked by Mr. Peter Peto of Penticton, B. C. while the surrounding Lucky 2 claims were staked by Mingold Resources Inc.

| <u>Claim Name</u> | <u>No. of Units</u> | <u>Date of Record</u> | <u>Record No.</u> | <u>Expiry Date</u> |
|-------------------|---------------------|-----------------------|-------------------|--------------------|
| Lucky             | 4                   | August 20,1985        | 2435              | August 20,1987     |
| Lucky 2           | 12                  | April 29,1987         | 2896              | April 29,1988      |



MINGOLD RESOURCES INC.

VANCOUVER OFFICE

LUCKY PROPERTY  
LOCATION MAP

N.T.S. 92H-9W

SIMILKAMEEN M.D., B.C.

DRAWN BY: E.Y.

DATE: JULY 1987

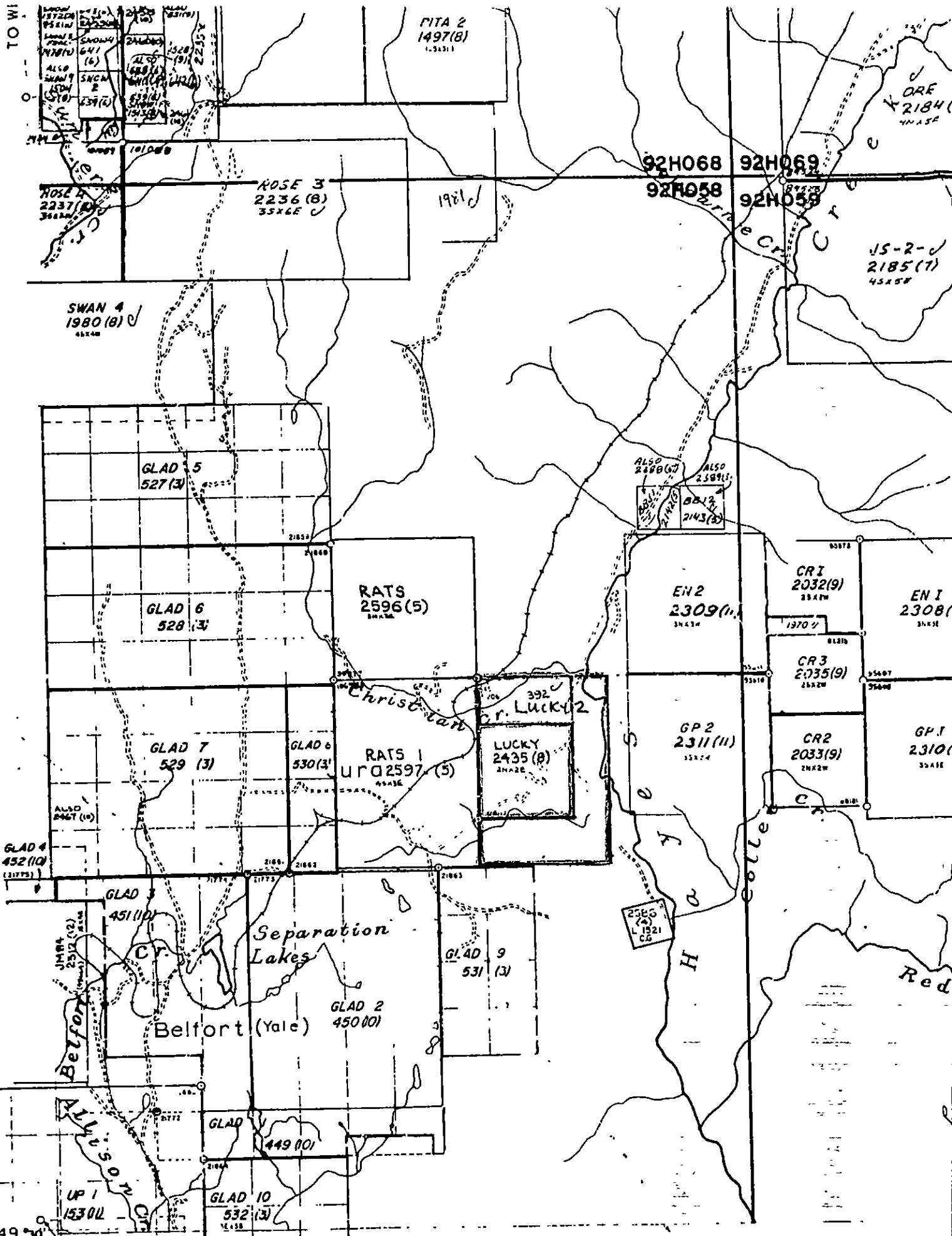
APPROVED BY:

BRITISH  
COLUMBIA

0 100 200 300 KM.

PLATE NO.

1



SIMILKAMEEN MINING DIVISION

DEPARTMENT OF MINES AND

## GEOLOGY & MINERALIZATION

The claims are underlain by altered dacites and andesites of the Upper Triassic Nicola Group. These rocks are intruded by the Middle Jurassic Osprey Lake Granodiorite which lies to the north and east of the property. The general trend of the rocks appears to be north-westerly, however, a combination of strong alteration (silicification, sericitization and pyritization) and shearing often masks any primary structures. A large part of the area is covered by a mantle of glacial and alluvial debris with outcrop essentially confined to roadcuts, trenches and creek gullies.

Mineralization consists of scattered chalcopyrite and minor bornite as disseminations and hairline fracture fillings. Weak pyrite is ubiquitous with greater concentrations (up to 20%) occurring in areas of more intense hydrothermal alteration. Anomalous gold values (up to 460 ppb in rock) occur in association with the better copper mineralization.

## GEOCHEMICAL SURVEYS

A systematic soil and rock sampling program was carried out over most of the Lucky claim and a portion of the Lucky 2 claim. Heavy overburden along the Hayes Creek Valley prevented the use of soil geochemistry over the eastern part of the Lucky 2 claim.

Soil sampling utilized a hipchain and compass grid which was put in concurrently with the sampling. A total of 233 samples (78 on Lucky 2,

155 on Lucky) were taken on grid lines spaced 100 meters apart with samples taken every 25 meters along them. Samples were collected at 15 - 25 cm depths, placed in gusseted Kraft envelopes and shipped to Acme Analytical Laboratories in Vancouver for analysis. Analysis was by ICP for a 30 element package. This technique uses a 0.5 gram sample which is digested with 3 ml. of 3-1-2 HCL-HNO<sub>3</sub>-H<sub>2</sub>O at 95° C for one hour. This is then diluted to 10 ml. with water and analysed by an ICP unit. Gold analysis was done separately using a 20 gram sample which is ignited at 600°C, digested with hot aqua regia and extracted by MIBK. This is then analysed using a graphite furnace AA unit. Mercury analysis uses the solution extracted during the ICP digestion. The aliquots of the extract are added to a stannous chloride-hydrochloric acid solution. The reduced mercury is swept out of the solution and passed into the mercury cell of a cold vapour AA using a F & J scientific mercury assembly.

A total of 95 rock samples (1 on Lucky 2, 94 on Lucky) were taken of selected outcrops generally at 2 metre intervals over the length of the exposure. A continuous sample of rock chips were collected in poly bags which were tagged and sent to Acme Analytical in Vancouver. There the samples are crushed to -<sup>3</sup>/<sub>16</sub>" then pulverized to -100 mesh. Analytical technique is then the same as that described above for soils.

#### DISCUSSION OF RESULTS

The geochemical results for gold and copper in soils are shown on

Plate No. 3 and No. 4. Anomalous levels of 25, 50 and 100 ppm for gold and 250, 500 and 750 ppm for copper were chosen by inspection. An obvious strong correlation exists between gold and copper anomalies with three main zones of interest outlined. The flat response of the soils along the west side of the highway may be partially a function of thicker overburden. It is not known what effect glaciation may have had in the area. The soils were a consistent gray colour suggesting a high till content, however no striae or other glacial features were noted. The close association between the gold and copper anomalies suggests that transport distances by glacial or hydromorphic dispersion have not been significant.

The rock sampling results are shown on Plate No. 5. The highest gold value obtained in the rock sampling was 470 ppb (0.014 oz/t) which coincided with the second highest copper value (7409 ppm or 0.7%). The highest copper value was 8215 ppm (0.82 %) which ran 460 ppb gold (.014 oz/t). In other samples the higher gold values were almost invariably associated with high copper values but many high copper values had very low accessory gold. The level of pyrite in the rocks appeared to have no bearing on the gold content. There seems to be good correlation generally between the soils and rocks although in some instances the rocks showed weak gold values where the soils were at background levels.

#### CONCLUSIONS & RECOMMENDATIONS

The soil and rock sampling has been effective in targetting several areas of gold-copper mineralization. The rock sampling suggests that



the concentrations of these metals at surface is probably not of economic interest. It is not known however, what influence surface oxidation and leaching may have had on the mineralization.

It is recommended that further soil sampling be carried out to the east and south of the area surveyed to try to close off the gold and copper anomalies. The valley to the east may present some problems due to excessive overburden. Reverse circulation drilling is also recommended on the known anomalies to determine if grades are improving with depth.

  
K. J. TAYLOR

APPENDIX 1

SOIL and ROCK GEOCHEMICAL ASSAY CERTIFICATES

GEOCHEMICAL ICP ANALYSIS

500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR NI FE CA P LA CR MG BA TI B W AND... LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPES: Rock Chips AU ANALYSIS BY AA FROM 10 EG-50 SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUNE 20 1987 DATE REPORT MAILED: *Jan 25/89* ASSAYER: *A. S. S. ...* DEAN TOYE, CERTIFIED B.C. ASSAYER

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Table with columns: SAMPLES, NO, PPM, CU, PB, ZN, NI, CO, MN, FE, AS, U, AU, TH, SR, CD, SB, BI, V, CA, P, LA, CR, MG, BA, TI, B, W, NA, K, MA, AL, S, NI, MO, HG. Rows include samples TL-92H-0988R through TL-92H-09105R and STD C/AU-R.

Table with columns: STD C/AU-R, TL-92H-09116R, TL-92H-09117R, TL-92H-09118R, TL-92H-09119R, TL-92H-09120R, TL-92H-09121R. Rows include sample numbers and corresponding PPM values for various elements.



MINGOLD RESOURCES PROJECT - LUCKY FILE # 87-1901

| SAMPLES        | NO | CU  | PB | ZN  | AS  | FE | MN | CO   | NI   | CD | HW | AS | U  | AU | TH | SR | CD | SB | BI   | V    | CA | P  | LA  | CR  | MG  | BA | TI   | B   | AL  | HA | K  | M    | AUI | MG |
|----------------|----|-----|----|-----|-----|----|----|------|------|----|----|----|----|----|----|----|----|----|------|------|----|----|-----|-----|-----|----|------|-----|-----|----|----|------|-----|----|
| L58+00N 48+00E | 1  | 15  | 11 | 103 | .1  | 4  | 5  | 486  | 1.93 | 2  | 5  | MD | 3  | 35 | 1  | 2  | 2  | 39 | .43  | .079 | 9  | 13 | .24 | 145 | .08 | 3  | .99  | .03 | .13 | 1  | 1  | 40   |     |    |
| L58+00N 48+25E | 2  | 10  | 17 | 80  | .1  | 5  | 3  | 343  | 1.75 | 2  | 5  | MD | 3  | 26 | 1  | 2  | 2  | 37 | .30  | .059 | 7  | 12 | .20 | 146 | .08 | 2  | .84  | .02 | .09 | 1  | 25 | 50   |     |    |
| L58+00N 48+50E | 1  | 17  | 11 | 46  | .1  | 4  | 5  | 484  | 2.28 | 2  | 5  | MD | 4  | 31 | 1  | 2  | 2  | 47 | .33  | .024 | 13 | 14 | .24 | 154 | .10 | 2  | 1.09 | .02 | .12 | 1  | 1  | 10   |     |    |
| SID C/AU-S     | 19 | 58  | 40 | 131 | 6.9 | 66 | 27 | 982  | 3.90 | 40 | 15 | 8  | 34 | 47 | 17 | 15 | 21 | 62 | .47  | .099 | 36 | 56 | .84 | 171 | .08 | 35 | 1.70 | .07 | .14 | 13 | 49 | 1400 |     |    |
| L58+00N 48+75E | 1  | 10  | 4  | 63  | .1  | 7  | 4  | 305  | 2.08 | 2  | 5  | MD | 7  | 30 | 1  | 2  | 2  | 44 | .29  | .021 | 16 | 15 | .31 | 100 | .11 | 2  | 1.02 | .02 | .10 | 1  | 1  | 20   |     |    |
| L58+00N 49+00E | 1  | 7   | 5  | 74  | .1  | 4  | 4  | 287  | 1.72 | 2  | 5  | MD | 2  | 27 | 1  | 2  | 2  | 37 | .29  | .083 | 5  | 11 | .16 | 114 | .08 | 2  | .99  | .02 | .07 | 1  | 2  | 10   |     |    |
| L58+00N 49+25E | 1  | 10  | 4  | 99  | .1  | 5  | 5  | 244  | 1.87 | 2  | 5  | MD | 2  | 27 | 1  | 2  | 2  | 40 | .25  | .113 | 4  | 11 | .16 | 141 | .08 | 2  | 1.11 | .03 | .07 | 1  | 1  | 5    |     |    |
| L58+00N 49+50E | 1  | 32  | 10 | 48  | .1  | 6  | 6  | 238  | 3.01 | 2  | 6  | MD | 4  | 28 | 1  | 2  | 2  | 74 | .35  | .090 | 10 | 21 | .27 | 75  | .08 | 2  | .93  | .02 | .08 | 2  | 1  | 10   |     |    |
| L58+00N 49+75E | 1  | 58  | 9  | 91  | .1  | 6  | 9  | 792  | 3.59 | 6  | 5  | MD | 1  | 48 | 1  | 2  | 2  | 85 | .70  | .115 | 13 | 21 | .30 | 187 | .08 | 3  | 1.32 | .02 | .15 | 1  | 1  | 20   |     |    |
| L58+00N 50+00E | 1  | 55  | 10 | 94  | .1  | 9  | 8  | 737  | 3.38 | 3  | 5  | MD | 1  | 54 | 1  | 2  | 2  | 79 | .81  | .135 | 12 | 20 | .30 | 206 | .08 | 2  | 1.37 | .02 | .13 | 1  | 1  | 20   |     |    |
| L57+00N 48+00E | 2  | 22  | 9  | 129 | .2  | 7  | 4  | 1045 | 1.58 | 2  | 5  | MD | 1  | 43 | 1  | 2  | 2  | 32 | .48  | .124 | 4  | 10 | .19 | 248 | .07 | 2  | 1.25 | .03 | .09 | 1  | 1  | 10   |     |    |
| L57+00N 48+25E | 1  | 88  | 10 | 112 | .1  | 10 | 7  | 849  | 2.52 | 2  | 8  | MD | 1  | 55 | 1  | 2  | 2  | 58 | .75  | .121 | 9  | 18 | .33 | 192 | .08 | 4  | 1.44 | .02 | .17 | 1  | 1  | 20   |     |    |
| L57+00N 48+50E | 1  | 134 | 9  | 162 | .2  | 15 | 8  | 712  | 2.42 | 7  | 5  | MD | 1  | 47 | 1  | 2  | 2  | 34 | .57  | .214 | 9  | 23 | .43 | 226 | .11 | 3  | 1.97 | .04 | .13 | 1  | 1  | 30   |     |    |
| L57+00N 48+75E | 1  | 53  | 8  | 150 | .2  | 8  | 6  | 1011 | 2.33 | 3  | 5  | MD | 1  | 50 | 1  | 2  | 2  | 52 | .66  | .205 | 8  | 14 | .26 | 264 | .07 | 2  | 1.41 | .03 | .10 | 1  | 1  | 10   |     |    |
| L57+00N 49+00E | 1  | 30  | 6  | 86  | .1  | 7  | 6  | 633  | 2.67 | 2  | 5  | MD | 2  | 41 | 1  | 2  | 2  | 40 | .50  | .077 | 11 | 15 | .23 | 186 | .08 | 2  | 1.25 | .02 | .16 | 1  | 1  | 20   |     |    |
| L57+00N 49+25E | 1  | 40  | 8  | 76  | .1  | 6  | 7  | 528  | 3.01 | 3  | 5  | MD | 2  | 45 | 1  | 2  | 2  | 70 | .63  | .087 | 12 | 18 | .27 | 166 | .08 | 2  | 1.34 | .02 | .16 | 1  | 1  | 10   |     |    |
| L57+00N 49+50E | 1  | 50  | 13 | 84  | .1  | 9  | 7  | 576  | 3.19 | 6  | 5  | MD | 1  | 45 | 1  | 2  | 2  | 75 | .60  | .089 | 12 | 23 | .31 | 162 | .09 | 5  | 1.32 | .02 | .13 | 1  | 1  | 10   |     |    |
| L57+00N 49+75E | 1  | 60  | 12 | 89  | .1  | 9  | 7  | 554  | 3.13 | 6  | 5  | MD | 1  | 46 | 1  | 2  | 2  | 72 | .64  | .106 | 14 | 21 | .29 | 172 | .07 | 2  | 1.35 | .02 | .15 | 1  | 2  | 20   |     |    |
| L57+00N 50+00E | 1  | 45  | 18 | 124 | .1  | 9  | 7  | 688  | 2.72 | 4  | 5  | MD | 2  | 50 | 1  | 2  | 2  | 57 | .70  | .091 | 14 | 17 | .28 | 234 | .08 | 2  | 1.47 | .02 | .17 | 1  | 1  | 5    |     |    |
| L56+00N 48+00E | 1  | 37  | 5  | 61  | .1  | 7  | 6  | 503  | 2.75 | 2  | 5  | MD | 1  | 44 | 1  | 2  | 2  | 63 | .61  | .101 | 12 | 17 | .28 | 141 | .08 | 4  | 1.34 | .03 | .16 | 1  | 1  | 10   |     |    |
| L56+00N 48+25E | 1  | 26  | 7  | 76  | .1  | 6  | 5  | 543  | 2.17 | 2  | 5  | MD | 1  | 53 | 1  | 2  | 2  | 48 | .69  | .122 | 10 | 13 | .24 | 177 | .06 | 4  | 1.31 | .03 | .17 | 2  | 1  | 10   |     |    |
| L56+00N 48+50E | 1  | 25  | 6  | 78  | .1  | 6  | 5  | 540  | 2.10 | 2  | 5  | MD | 1  | 45 | 1  | 2  | 2  | 46 | .61  | .125 | 10 | 12 | .22 | 169 | .06 | 2  | 1.34 | .02 | .13 | 1  | 1  | 20   |     |    |
| L56+00N 48+75E | 1  | 28  | 7  | 87  | .1  | 4  | 5  | 602  | 2.15 | 2  | 5  | MD | 1  | 58 | 1  | 2  | 2  | 47 | .78  | .120 | 10 | 13 | .23 | 198 | .06 | 2  | 1.28 | .02 | .12 | 1  | 1  | 20   |     |    |
| L56+00N 49+00E | 1  | 27  | 11 | 84  | .1  | 4  | 6  | 605  | 2.15 | 3  | 5  | MD | 1  | 57 | 1  | 2  | 2  | 47 | .82  | .149 | 10 | 13 | .24 | 181 | .06 | 2  | 1.37 | .02 | .13 | 1  | 2  | 10   |     |    |
| L56+00N 49+25E | 1  | 25  | 6  | 63  | .1  | 6  | 5  | 528  | 2.31 | 2  | 5  | MD | 1  | 53 | 1  | 2  | 2  | 53 | .73  | .116 | 10 | 14 | .22 | 172 | .06 | 2  | 1.16 | .02 | .14 | 1  | 1  | 10   |     |    |
| L56+00N 49+50E | 1  | 25  | 3  | 104 | .1  | 6  | 6  | 632  | 2.12 | 3  | 5  | MD | 1  | 57 | 1  | 2  | 2  | 46 | .71  | .129 | 10 | 14 | .26 | 207 | .07 | 4  | 1.47 | .03 | .16 | 1  | 1  | 10   |     |    |
| L56+00N 49+75E | 1  | 27  | 4  | 107 | .1  | 6  | 5  | 718  | 1.99 | 2  | 5  | MD | 1  | 56 | 1  | 2  | 2  | 43 | .76  | .150 | 10 | 12 | .22 | 222 | .06 | 3  | 1.35 | .03 | .15 | 1  | 1  | 20   |     |    |
| L56+00N 50+00E | 1  | 139 | 9  | 144 | .1  | 13 | 7  | 1004 | 2.24 | 3  | 5  | MD | 1  | 43 | 1  | 2  | 2  | 50 | .94  | .137 | 9  | 22 | .44 | 229 | .07 | 2  | 1.69 | .03 | .19 | 1  | 1  | 30   |     |    |
| L55+00N 48+00E | 1  | 43  | 9  | 161 | .1  | 9  | 9  | 684  | 2.42 | 2  | 5  | MD | 1  | 40 | 1  | 2  | 2  | 52 | .92  | .135 | 11 | 15 | .33 | 154 | .09 | 3  | 1.77 | .03 | .25 | 1  | 3  | 20   |     |    |
| L55+00N 48+25E | 1  | 42  | 9  | 126 | .1  | 9  | 7  | 677  | 2.40 | 5  | 5  | MD | 1  | 61 | 1  | 2  | 2  | 43 | .95  | .144 | 11 | 14 | .30 | 202 | .08 | 2  | 1.49 | .02 | .19 | 1  | 2  | 20   |     |    |
| L55+00N 48+50E | 1  | 38  | 4  | 100 | .1  | 8  | 7  | 572  | 2.30 | 3  | 5  | MD | 1  | 55 | 1  | 2  | 2  | 50 | .79  | .137 | 12 | 14 | .27 | 183 | .07 | 3  | 1.49 | .03 | .15 | 1  | 1  | 30   |     |    |
| L55+00N 48+75E | 1  | 34  | 5  | 92  | .1  | 6  | 6  | 539  | 2.23 | 2  | 5  | MD | 1  | 56 | 1  | 2  | 2  | 47 | .75  | .132 | 11 | 12 | .26 | 164 | .07 | 2  | 1.54 | .03 | .13 | 1  | 1  | 10   |     |    |
| L55+00N 49+00E | 1  | 40  | 8  | 90  | .1  | 5  | 5  | 532  | 2.34 | 2  | 5  | MD | 1  | 52 | 1  | 2  | 2  | 52 | .83  | .105 | 11 | 14 | .29 | 161 | .08 | 2  | 1.45 | .03 | .15 | 1  | 1  | 20   |     |    |
| L55+00N 49+25E | 1  | 30  | 5  | 87  | .2  | 7  | 6  | 583  | 2.28 | 4  | 5  | MD | 1  | 51 | 1  | 2  | 2  | 48 | .74  | .155 | 11 | 13 | .25 | 178 | .07 | 2  | 1.73 | .03 | .16 | 1  | 1  | 10   |     |    |
| L55+00N 49+50E | 1  | 35  | 9  | 80  | .1  | 4  | 6  | 556  | 2.24 | 2  | 5  | MD | 1  | 57 | 1  | 2  | 2  | 49 | .95  | .116 | 10 | 13 | .25 | 171 | .07 | 2  | 1.39 | .03 | .14 | 1  | 1  | 20   |     |    |
| L55+00N 49+75E | 1  | 49  | 4  | 95  | .1  | 6  | 7  | 656  | 2.27 | 3  | 5  | MD | 1  | 65 | 1  | 2  | 2  | 47 | 1.25 | .137 | 11 | 13 | .31 | 234 | .08 | 3  | 1.59 | .03 | .17 | 1  | 2  | 20   |     |    |
| L55+00N 50+00E | 1  | 50  | 6  | 88  | .2  | 8  | 6  | 571  | 2.47 | 5  | 5  | MD | 1  | 64 | 1  | 2  | 2  | 55 | 1.05 | .153 | 12 | 15 | .34 | 169 | .07 | 3  | 1.46 | .03 | .19 | 1  | 1  | 30   |     |    |



MINGOLD RESOURCES PROJECT - LUCKY FILE # B7-1901

| SAMPLE         | NO | CU  | PB | ZN  | AS | FE | MN  | CO   | NI | MO | TI | CR | LA  | CA | V | BI | SB | SI   | CD   | SK | TN | AU  | IN  | MG  | BA | TE   | S   | AL  | MA | K  | W  | AU | MG |
|----------------|----|-----|----|-----|----|----|-----|------|----|----|----|----|-----|----|---|----|----|------|------|----|----|-----|-----|-----|----|------|-----|-----|----|----|----|----|----|
| L50+00M 48+00E | 2  | 406 | 12 | 111 | .5 | 9  | 520 | 3.15 | 4  | 5  | ND | 2  | 124 | 1  | 2 | 2  | 59 | 1.33 | .132 | 7  | 9  | .42 | 97  | .08 | 8  | 1.39 | .03 | .12 | 1  | 19 | 30 |    |    |
| L50+00M 48+25E | 2  | 130 | 16 | 88  | .5 | 7  | 732 | 4.65 | 9  | 5  | ND | 4  | 102 | 1  | 2 | 2  | 74 | .53  | .122 | 10 | 16 | .45 | 172 | .08 | 5  | 1.35 | .03 | .27 | 1  | 32 | 10 |    |    |
| L50+00M 48+50E | 1  | 72  | 9  | 75  | .1 | 9  | 478 | 2.72 | 3  | 5  | ND | 2  | 42  | 1  | 2 | 2  | 40 | .46  | .084 | 11 | 16 | .32 | 115 | .08 | 3  | 1.35 | .02 | .19 | 1  | 1  | 10 |    |    |
| L50+00M 48+75E | 1  | 46  | 6  | 91  | .1 | 7  | 861 | 2.56 | 5  | 5  | ND | 2  | 71  | 1  | 2 | 3  | 51 | .70  | .116 | 10 | 11 | .34 | 171 | .08 | 4  | 1.63 | .02 | .13 | 1  | 1  | 20 |    |    |
| L50+00M 49+00E | 2  | 155 | 12 | 103 | .3 | 11 | 925 | 2.50 | 7  | 5  | ND | 1  | 105 | 1  | 2 | 2  | 49 | 1.02 | .140 | 9  | 13 | .38 | 185 | .07 | 6  | 1.33 | .02 | .18 | 1  | 5  | 20 |    |    |
| L50+00M 49+25E | 1  | 134 | 11 | 120 | .1 | 13 | 902 | 2.48 | 4  | 6  | ND | 2  | 71  | 1  | 2 | 2  | 53 | .77  | .147 | 11 | 18 | .32 | 205 | .07 | 9  | 1.71 | .02 | .14 | 1  | 1  | 10 |    |    |
| L50+00M 49+50E | 1  | 119 | 10 | 126 | .1 | 12 | 789 | 2.10 | 2  | 5  | ND | 1  | 74  | 1  | 2 | 2  | 46 | .84  | .123 | 10 | 15 | .30 | 165 | .06 | 4  | 1.33 | .02 | .13 | 1  | 1  | 20 |    |    |
| L50+00M 49+75E | 1  | 70  | 14 | 117 | .1 | 9  | 641 | 2.18 | 4  | 5  | ND | 1  | 70  | 1  | 2 | 2  | 46 | .83  | .124 | 10 | 12 | .30 | 155 | .06 | 4  | 1.36 | .02 | .14 | 1  | 1  | 20 |    |    |
| L50+00M 50+00E | 1  | 80  | 6  | 127 | .1 | 8  | 633 | 2.19 | 2  | 5  | ND | 1  | 77  | 1  | 2 | 2  | 47 | .88  | .127 | 9  | 14 | .31 | 184 | .07 | 2  | 1.36 | .02 | .16 | 1  | 2  | 40 |    |    |

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEGC FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR NI FE CA P LA CR NI BA TI B AL NA K N AU H6 - SAMPLE TYPE: P1-5 SOILS PA-ROCKS AU ANALYSIS BY AA FROM 10 GRAM SAMPLE. MS ANALYSIS BY FLOWERS AA.

DATE RECEIVED: JUNE 24 1987 DATE REPORT MAILED: June 30 1987 ASSAYER: A. J. DEAN TOYE, CERTIFIED B.C. ASSAYER

MINGOLD RESOURCES PROJECT-LUCKY File # 87-1966 Page 1

Table with columns: SAMPLE, NO, CU, PB, ZN, AG, NI, CO, MN, FE, AS, U, AU, TH, SR, CD, SB, BI, V, CA, P, LA, CR, NI, BA, TI, B, AL, NA, K, N, AU, H6. Rows list various sample IDs and their corresponding element concentrations in PPM.

LUCKY





MINGOLD RESOURCES PROJECT-LUCKY FILE # B7-1966

| SAMPLES       | NO  | CU   | FE  | AS  | U   | AU  | TH   | SR   | CO   | SB   | BI  | V   | CA  | P   | LA  | CR  | MG  | BA   | TI   | B    | AL  | WA  | K    | M   | AU  | HG   |      |     |     |      |      |      |
|---------------|-----|------|-----|-----|-----|-----|------|------|------|------|-----|-----|-----|-----|-----|-----|-----|------|------|------|-----|-----|------|-----|-----|------|------|-----|-----|------|------|------|
|               | PPH | PPH  | PPH | PPH | PPH | PPH | PPH  | PPH  | PPH  | PPH  | PPH | PPH | PPH | PPH | PPH | PPH | PPH | PPH  | PPH  | PPH  | PPH | PPH | PPH  | PPH | PPH | PPH  |      |     |     |      |      |      |
| 52+00M 52+00E | 4   | 72   | 315 | 5   | 7   | 10  | 1052 | 3.79 | 7    | 5    | MD  | 2   | 71  | 1   | 2   | 2   | 63  | .69  | .080 | 8    | 12  | .45 | 176  | .09 | 4   | 1.81 | .02  | .17 | 1   | 315  | 20   |      |
| 52+00M 52+25E | 3   | 382  | 36  | 381 | .2  | 7   | 12   | 1407 | 3.28 | 3    | 5   | MD  | 4   | 109 | 2   | 2   | 59  | 1.36 | .125 | 11   | 15  | .48 | 256  | .07 | 6   | 1.48 | .02  | .22 | 2   | (18) | 30   |      |
| 52+00M 52+50E | 2   | 289  | 26  | 328 | .1  | 7   | 9    | 1471 | 2.62 | 2    | 5   | MD  | 1   | 2   | 2   | 2   | 48  | 1.07 | .113 | 9    | 13  | .36 | 311  | .07 | 5   | 1.51 | .02  | .16 | 1   | 10   | 30   |      |
| 52+00M 52+75E | 4   | 534  | 12  | 192 | .2  | 9   | 9    | 1094 | 2.49 | 6    | 5   | MD  | 1   | 75  | 1   | 2   | 47  | .67  | .139 | 8    | 14  | .35 | 216  | .07 | 2   | 1.44 | .03  | .10 | 2   | 16   | 20   |      |
| 51+00M 50+50E | 7   | 486  | 18  | 134 | .4  | 5   | 7    | 632  | 2.94 | 2    | 5   | MD  | 1   | 147 | 1   | 2   | 30  | 1.08 | .124 | 8    | 9   | .33 | 214  | .09 | 7   | 1.33 | .03  | .18 | 1   | 1    | 30   |      |
| 51+00M 50+75E | 4   | 526  | 13  | 115 | .2  | 5   | 7    | 588  | 4.29 | 6    | 5   | MD  | 1   | 85  | 1   | 2   | 67  | .76  | .152 | 10   | 13  | .39 | 203  | .12 | 4   | 1.51 | .04  | .25 | 1   | 8    | 10   |      |
| 51+00M 51+00E | 5   | 91   | 15  | 108 | .4  | 4   | 5    | 594  | 4.30 | 7    | 5   | MD  | 1   | 238 | 1   | 2   | 72  | 1.13 | .162 | 8    | 12  | .53 | 194  | .12 | 5   | 1.40 | .04  | .27 | 1   | (13) | 10   |      |
| 51+00M 51+25E | 3   | 948  | 11  | 115 | .1  | 4   | 8    | 720  | 2.89 | 3    | 5   | MD  | 1   | 84  | 1   | 2   | 52  | .71  | .109 | 10   | 13  | .32 | 210  | .08 | 4   | 1.80 | .03  | .12 | 1   | 1    | 20   |      |
| 51+00M 51+50E | 5   | 242  | 9   | 62  | .5  | 4   | 6    | 23   | 463  | 4.84 | 2   | 5   | MD  | 4   | 44  | 1   | 4   | 76   | .29  | .135 | 14  | 20  | .34  | 123 | .09 | 3    | 3.25 | .02 | .11 | 2    | 37   | 110  |
| 51+00M 52+00E | 5   | 184  | 7   | 139 | .2  | 12  | 7    | 1028 | 2.37 | 2    | 5   | MD  | 1   | 105 | 1   | 2   | 3   | 41   | 1.19 | .127 | 9   | 15  | .44  | 229 | .07 | 4    | 1.54 | .02 | .21 | 1    | (10) | 30   |
| 51+00M 52+25E | 10  | 4382 | 9   | 103 | .2  | 14  | 8    | 716  | 3.95 | 3    | 5   | MD  | 1   | 242 | 1   | 3   | 2   | 76   | 1.12 | .116 | 9   | 30  | .71  | 199 | .13 | 5    | 1.69 | .04 | .26 | 1    | 20   | 10   |
| 51+00M 52+50E | 3   | 189  | 7   | 91  | .1  | 8   | 6    | 793  | 1.96 | 2    | 5   | MD  | 1   | 106 | 1   | 2   | 33  | 1.41 | .137 | 7    | 13  | .33 | 237  | .04 | 5   | 1.08 | .02  | .13 | 1   | 5    | 30   |      |
| 51+00M 52+75E | 1   | 487  | 14  | 102 | .1  | 20  | 11   | 1231 | 2.89 | 2    | 5   | MD  | 1   | 60  | 1   | 2   | 40  | 1.95 | .145 | 8    | 38  | .88 | 175  | .04 | 12  | 1.70 | .01  | .21 | 1   | 1    | 40   |      |
| 51+00M 53+00E | 1   | 299  | 12  | 112 | .1  | 17  | 9    | 1049 | 2.42 | 3    | 5   | MD  | 1   | 59  | 1   | 2   | 3   | 49   | 1.12 | .123 | 7   | 31  | .57  | 187 | .04 | 5    | 1.82 | .02 | .12 | 1    | 5    | 40   |
| 50+00M 50+50E | 4   | 428  | 19  | 127 | .3  | 6   | 7    | 625  | 3.30 | 6    | 5   | MD  | 1   | 130 | 1   | 2   | 2   | 54   | 1.07 | .138 | 9   | 13  | .37  | 251 | .08 | 6    | 1.34 | .03 | .21 | 1    | (13) | 30   |
| 50+00M 50+75E | 9   | 697  | 27  | 123 | 1.1 | 4   | 7    | 831  | 5.37 | 15   | 5   | MD  | 1   | 257 | 1   | 2   | 3   | 64   | .86  | .249 | 8   | 9   | .42  | 245 | .08 | 3    | 1.29 | .05 | .27 | 1    | 25   | 10   |
| 50+00M 51+00E | 4   | 71   | 7   | 91  | .1  | 4   | 4    | 692  | 2.57 | 4    | 5   | MD  | 1   | 152 | 1   | 2   | 2   | 42   | 1.00 | .105 | 6   | 8   | .34  | 184 | .06 | 4    | 1.07 | .02 | .18 | 1    | 4    | 30   |
| 50+00M 51+25E | 6   | 71   | 12  | 88  | .3  | 4   | 6    | 724  | 5.40 | 10   | 5   | MD  | 1   | 181 | 1   | 3   | 4   | 91   | .62  | .166 | 7   | 12  | .54  | 183 | .10 | 2    | 1.58 | .04 | .19 | 1    | 5    | 20   |
| 50+00M 51+50E | 1   | 819  | 15  | 96  | .1  | 6   | 9    | 815  | 2.94 | 5    | 5   | MD  | 1   | 58  | 1   | 2   | 2   | 59   | .59  | .095 | 9   | 14  | .29  | 153 | .07 | 4    | 1.43 | .02 | .09 | 1    | 1    | 40   |
| 50+00M 51+75E | 8   | 471  | 11  | 82  | .1  | 3   | 7    | 751  | 3.83 | 4    | 5   | MD  | 1   | 110 | 1   | 2   | 3   | 62   | .71  | .131 | 8   | 10  | .35  | 195 | .10 | 3    | 1.37 | .03 | .14 | 1    | 1    | 20   |
| 50+00M 52+00E | 1   | 1284 | 8   | 97  | .1  | 110 | 23   | 1053 | 4.00 | 5    | 5   | MD  | 2   | 116 | 1   | 2   | 2   | 96   | 2.38 | .059 | 11  | 189 | 3.06 | 100 | .22 | 2    | 2.74 | .01 | .20 | 1    | 1    | 30   |
| 50+00M 52+25E | 2   | 871  | 8   | 106 | .1  | 37  | 13   | 746  | 3.74 | 2    | 5   | MD  | 1   | 45  | 1   | 2   | 4   | 71   | .85  | .108 | 10  | 67  | 1.10 | 181 | .13 | 6    | 1.99 | .02 | .20 | 1    | 2    | 20   |
| 50+00M 52+75E | 1   | 138  | 7   | 137 | .1  | 8   | 6    | 1013 | 1.42 | 2    | 5   | MD  | 1   | 85  | 1   | 2   | 2   | 24   | 1.67 | .175 | 6   | 9   | .30  | 296 | .03 | 7    | 1.14 | .02 | .14 | 1    | 1    | 50   |
| 50+00M 53+00E | 2   | 575  | 11  | 122 | .1  | 10  | 13   | 893  | 2.46 | 2    | 5   | MD  | 1   | 61  | 1   | 2   | 2   | 50   | .71  | .072 | 11  | 15  | .41  | 202 | .07 | 6    | 1.95 | .02 | .15 | 1    | 1    | 20   |
| 49+00M 49+00E | 1   | 1647 | 10  | 87  | .1  | 10  | 11   | 784  | 3.78 | 5    | 5   | MD  | 2   | 50  | 1   | 2   | 2   | 67   | .54  | .083 | 11  | 17  | .42  | 143 | .11 | 2    | 1.76 | .02 | .19 | 1    | 2    | 10   |
| 49+00M 49+25E | 2   | 288  | 52  | 104 | .3  | 6   | 8    | 703  | 5.28 | 12   | 5   | MD  | 2   | 87  | 1   | 2   | 2   | 119  | .54  | .113 | 9   | 19  | .56  | 145 | .18 | 2    | 1.85 | .04 | .19 | 1    | 6    | 40   |
| 49+00M 49+50E | 17  | 478  | 24  | 96  | .8  | 5   | 4    | 634  | 4.97 | 11   | 5   | MD  | 2   | 1   | 1   | 4   | 2   | 91   | .66  | .132 | 10  | 13  | .51  | 204 | .17 | 2    | 2.07 | .06 | .19 | 1    | (14) | 20   |
| 49+00M 49+75E | 34  | 92   | 44  | 77  | 1.2 | 4   | 3    | 571  | 4.80 | 8    | 5   | MD  | 2   | 1   | 1   | 2   | 2   | 94   | .95  | .123 | 8   | 9   | .58  | 218 | .16 | 2    | 1.51 | .07 | .27 | 1    | 25   | 10   |
| 49+00M 50+00E | 18  | 1849 | 14  | 84  | .7  | 3   | 5    | 819  | 3.65 | 4    | 5   | MD  | 1   | 153 | 1   | 2   | 2   | 67   | .90  | .177 | 7   | 7   | .44  | 169 | .10 | 2    | 1.72 | .03 | .14 | 1    | (12) | 20   |
| 49+00M 50+25E | 5   | 595  | 15  | 140 | .3  | 10  | 14   | 907  | 3.90 | 9    | 5   | MD  | 1   | 89  | 1   | 2   | 2   | 68   | .91  | .137 | 9   | 15  | .69  | 173 | .12 | 2    | 1.93 | .03 | .17 | 1    | 20   | 30   |
| 49+00M 50+50E | 2   | 808  | 10  | 78  | .4  | 8   | 8    | 653  | 3.89 | 9    | 5   | MD  | 1   | 113 | 1   | 2   | 2   | 65   | .68  | .140 | 8   | 14  | .47  | 280 | .10 | 2    | 1.70 | .02 | .17 | 1    | 6    | 20   |
| 49+00M 50+75E | 2   | 243  | 9   | 84  | .2  | 6   | 6    | 875  | 2.91 | 8    | 5   | MD  | 1   | 138 | 1   | 2   | 2   | 49   | 1.14 | .143 | 7   | 8   | .42  | 279 | .07 | 2    | 1.44 | .02 | .11 | 2    | 2    | 30   |
| 49+00M 50+00E | 2   | 742  | 5   | 85  | .2  | 7   | 7    | 693  | 3.10 | 5    | 5   | MD  | 1   | 114 | 1   | 2   | 2   | 52   | 1.08 | .135 | 9   | 13  | .45  | 242 | .10 | 4    | 1.63 | .02 | .19 | 1    | 1    | 10   |
| 49+00M 50+50E | 2   | 940  | 9   | 83  | .1  | 5   | 8    | 646  | 2.70 | 6    | 5   | MD  | 1   | 80  | 1   | 2   | 2   | 47   | .87  | .125 | 9   | 13  | .33  | 187 | .04 | 5    | 1.38 | .02 | .15 | 1    | 1    | 20   |
| 49+00M 50+75E | 12  | 124  | 12  | 74  | .1  | 5   | 8    | 496  | 4.76 | 7    | 5   | MD  | 2   | 80  | 1   | 4   | 2   | 75   | .51  | .109 | 11  | 19  | .42  | 172 | .13 | 2    | 2.15 | .02 | .16 | 1    | 3    | 610  |
| 49+00M 51+00E | 4   | 904  | 10  | 81  | .1  | 5   | 7    | 1070 | 2.45 | 5    | 5   | MD  | 1   | 145 | 1   | 2   | 2   | 36   | 1.30 | .144 | 6   | 8   | .30  | 216 | .07 | 3    | 1.31 | .03 | .16 | 1    | 2    | 30   |
| STD C/AU-S    | 18  | 58   | 40  | 129 | 6.9 | 42  | 27   | 976  | 3.94 | 41   | 18  | 8   | 12  | 46  | 16  | 17  | 23  | 39   | .47  | .096 | 34  | 57  | .85  | 173 | .08 | 36   | 1.71 | .67 | .13 | 14   | 47   | 1300 |



| SAMPLES       | ND | CU  | PB | ZN  | AG  | NI | CO | MR   | FE   | AS | U  | AU | TH | SR  | CD | SO | BI | V  | CA   | P     | LA | CR | MG  | BA  | TI   | B  | AL   | MA   | K   | N  | AUS  | MG   | PPB |
|---------------|----|-----|----|-----|-----|----|----|------|------|----|----|----|----|-----|----|----|----|----|------|-------|----|----|-----|-----|------|----|------|------|-----|----|------|------|-----|
| 47+00N 51+00E | 3  | 79  | 7  | 79  | -2  | 9  | 7  | 454  | 3.91 | 6  | 5  | ND | 1  | 118 | 1  | 2  | 2  | 69 | -54  | -0.65 | 11 | 15 | -41 | 238 | .13  | 2  | 2.27 | .04  | -15 | 1  | (11) | 10   |     |
| 47+00N 51+25E | 3  | 74  | 12 | 71  | -6  | 6  | 5  | 562  | 4.73 | 5  | 5  | ND | 1  | 258 | 1  | 2  | 2  | 64 | -66  | -0.92 | 11 | 11 | -32 | 248 | -15  | 2  | 1.26 | .07  | -21 | 1  | 21   | 20   |     |
| 47+00N 51+50E | 1  | 837 | 8  | 70  | -1  | 8  | 8  | 519  | 3.43 | 2  | 5  | ND | 2  | 135 | 1  | 2  | 4  | 56 | -59  | -0.60 | 11 | 18 | -32 | 144 | -.09 | 2  | 1.26 | .04  | -18 | 1  | 6    | 10   |     |
| 47+00N 51+75E | 1  | 835 | 10 | 59  | -3  | 8  | 7  | 493  | 2.83 | 6  | 5  | ND | 2  | 142 | 1  | 2  | 3  | 64 | -54  | -0.60 | 10 | 17 | -36 | 153 | -.11 | 3  | 1.33 | .04  | -15 | 1  | (12) | 10   |     |
| 47+00N 52+00E | 1  | 84  | 8  | 49  | -5  | 4  | 6  | 435  | 4.34 | 3  | 5  | ND | 2  | 153 | 1  | 2  | 2  | 62 | -31  | -0.72 | 9  | 13 | -33 | 159 | -.11 | 2  | 1.40 | .04  | -10 | 1  | (10) | 10   |     |
| 47+00N 52+25E | 1  | 870 | 10 | 91  | -3  | 15 | 11 | 1139 | 4.58 | 4  | 5  | ND | 1  | 132 | 1  | 2  | 2  | 65 | -69  | -0.96 | 10 | 17 | -58 | 183 | -.13 | 4  | 1.98 | .05  | -20 | 1  | (19) | 20   |     |
| 47+00N 52+50E | 1  | 887 | 14 | 434 | -7  | 12 | 16 | 1848 | 3.95 | 12 | 5  | ND | 1  | 54  | 2  | 2  | 2  | 44 | 1.24 | .057  | 10 | 11 | -96 | 215 | -.02 | 2  | 2.05 | -.01 | -35 | 1  | 110  | 240  |     |
| 47+00N 52+75E | 2  | 878 | 3  | 296 | -5  | 16 | 23 | 1892 | 4.14 | 9  | 5  | ND | 1  | 46  | 1  | 2  | 2  | 49 | -82  | -.041 | 10 | 11 | -74 | 244 | -.04 | 16 | 2.06 | -.02 | -33 | 1  | 33   | 30   |     |
| 47+00N 53+00E | 6  | 899 | 15 | 143 | -6  | 22 | 26 | 1656 | 4.94 | 11 | 5  | ND | 2  | 41  | 1  | 2  | 2  | 52 | -87  | -0.55 | 8  | 10 | -93 | 200 | -.05 | 3  | 2.07 | -.01 | -28 | 1  | 115  | 50   |     |
| STD C/AU-S    | 18 | 59  | 35 | 132 | 4.8 | 64 | 27 | 986  | 3.93 | 38 | 18 | 8  | 32 | 47  | 17 | 15 | 19 | 59 | -48  | -.060 | 35 | 56 | -88 | 177 | -.08 | 34 | 1.85 | -.07 | -64 | 11 | 52   | 1300 |     |

| WELL         | NO  | CU   | PB  | ZK  | 46  | NI  | CO  | MI   | FE   | AS  | U   | AU  | TH  | SR  | CO  | SB  | BI  | V   | CA   | P    | LA  | CR  | MG   | BA  | TI  | B   | AL   | MA  | K   | M   | RUC | HS   |     |
|--------------|-----|------|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|-----|------|-----|
|              | PPH | PPH  | PPH | PPH | PPH | PPH | PPH | PPH  | PPH  | PPH | PPH | PPH | PPH | PPH | PPH | PPH | PPH | PPH | PPH  | PPH  | PPH | PPH | PPH  | PPH | PPH | PPH | PPH  | PPH | PPH | PPH | PPH | PPH  | PPH |
| TL92H-09153R | 12  | 5742 | 11  | 118 | 2.0 | 6   | 15  | 474  | 3.75 | 11  | 5   | ND  | 3   | 49  | 1   | 2   | 2   | 107 | .48  | .100 | 6   | 10  | 1.38 | 27  | .14 | 4   | 1.44 | .04 | .25 | 4   | 250 | 5    |     |
| TL92H-09154P | 10  | 1520 | 7   | 82  | 1.1 | 6   | 8   | 315  | 3.14 | 7   | 5   | ND  | 2   | 49  | 1   | 2   | 3   | 129 | .48  | .082 | 3   | 9   | 1.20 | 27  | .23 | 9   | 1.54 | .04 | .35 | 1   | 220 | 5    |     |
| TL92H-09155R | 11  | 2148 | 12  | 46  | 1.3 | 4   | 7   | 232  | 4.62 | 10  | 5   | ND  | 3   | 41  | 1   | 2   | 2   | 132 | .34  | .096 | 5   | 9   | .89  | 27  | .15 | 5   | 1.24 | .03 | .22 | 2   | 340 | 5    |     |
| TL92H-09154H | 35  | 474  | 13  | 77  | 1.9 | 7   | 4   | 229  | 3.02 | 10  | 5   | ND  | 2   | 70  | 1   | 2   | 2   | 115 | .29  | .085 | 4   | 8   | 1.19 | 25  | .20 | 7   | 1.42 | .04 | .35 | 1   | 350 | 5    |     |
| TL92H-09157R | 5   | 496  | 4   | 70  | .4  | 6   | 8   | 480  | 3.55 | 7   | 5   | ND  | 2   | 90  | 1   | 2   | 2   | 111 | .61  | .101 | 4   | 9   | 1.34 | 27  | .25 | 7   | 1.82 | .04 | .20 | 2   | 133 | 5    |     |
| TL92H-09158R | 20  | 463  | 11  | 58  | 1.3 | 6   | 5   | 259  | 3.44 | 12  | 5   | ND  | 3   | 62  | 1   | 2   | 2   | 138 | .52  | .104 | 4   | 11  | 1.30 | 34  | .28 | 6   | 1.56 | .05 | .34 | 1   | 145 | 5    |     |
| TL92H-09159R | 34  | 8215 | 18  | 123 | 3.5 | 4   | 8   | 612  | 4.78 | 31  | 5   | ND  | 2   | 39  | 1   | 2   | 2   | 66  | .55  | .110 | 4   | 4   | .81  | 27  | .09 | 10  | 1.76 | .02 | .21 | 6   | 460 | 5    |     |
| TL92H-09160P | 22  | 7409 | 16  | 125 | 3.7 | 3   | 9   | 647  | 4.59 | 32  | 5   | ND  | 2   | 27  | 1   | 2   | 2   | 69  | .38  | .105 | 4   | 4   | .85  | 22  | .05 | 8   | 1.50 | .03 | .20 | 5   | 470 | 5    |     |
| TL92H-09161R | 19  | 1441 | 9   | 82  | 1.0 | 4   | 10  | 523  | 3.20 | 5   | 5   | ND  | 2   | 69  | 1   | 2   | 3   | 103 | .70  | .100 | 5   | 8   | .97  | 33  | .21 | 6   | 1.58 | .04 | .17 | 1   | 360 | 5    |     |
| TL92H-09162R | 17  | 1021 | 9   | 117 | .6  | 4   | 12  | 1143 | 3.08 | 8   | 5   | ND  | 1   | 56  | 1   | 2   | 2   | 93  | .60  | .097 | 5   | 8   | .97  | 25  | .18 | 5   | 1.55 | .03 | .14 | 2   | 350 | 10   |     |
| TL92H-09163R | 12  | 1514 | 10  | 118 | .4  | 5   | 12  | 1212 | 2.88 | 3   | 5   | ND  | 2   | 54  | 1   | 2   | 3   | 89  | .59  | .094 | 4   | 8   | .89  | 23  | .19 | 5   | 1.42 | .03 | .13 | 2   | 230 | 5    |     |
| TL92H-09164R | 4   | 270  | 36  | 180 | .8  | 6   | 8   | 778  | 6.45 | 11  | 5   | ND  | 4   | 61  | 1   | 2   | 2   | 181 | .55  | .116 | 6   | 18  | .88  | 38  | .26 | 4   | 1.60 | .05 | .14 | 1   | 52  | 80   |     |
| TL92H-09165R | 26  | 2368 | 14  | 86  | 1.4 | 5   | 14  | 424  | 3.62 | 19  | 5   | ND  | 1   | 270 | 1   | 2   | 2   | 85  | 3.96 | .085 | 3   | 6   | 1.16 | 29  | .19 | 5   | 1.25 | .03 | .15 | 2   | 280 | 10   |     |
| TL92H-09171R | 3   | 359  | 12  | 52  | .3  | 6   | 7   | 349  | 4.87 | 33  | 5   | ND  | 2   | 121 | 1   | 2   | 2   | 92  | 1.61 | .108 | 3   | 7   | .88  | 39  | .22 | 2   | 1.07 | .05 | .21 | 1   | 42  | 40   |     |
| TL92H-09172R | 2   | 406  | 10  | 50  | .6  | 5   | 10  | 343  | 4.70 | 33  | 5   | ND  | 3   | 102 | 1   | 2   | 2   | 76  | 1.36 | .095 | 2   | 7   | .85  | 34  | .20 | 6   | .95  | .04 | .18 | 1   | 43  | 30   |     |
| TL92H-09173R | 3   | 270  | 14  | 45  | .4  | 1   | 5   | 353  | 4.54 | 27  | 5   | ND  | 3   | 170 | 1   | 2   | 2   | 79  | 2.00 | .111 | 3   | 9   | .91  | 46  | .18 | 5   | 1.04 | .08 | .25 | 1   | 55  | 40   |     |
| TL92H-09174R | 3   | 189  | 17  | 60  | .3  | 2   | 6   | 403  | 4.96 | 40  | 5   | ND  | 3   | 101 | 1   | 2   | 2   | 91  | 1.10 | .113 | 3   | 9   | .88  | 48  | .20 | 6   | 1.11 | .06 | .22 | 1   | 65  | 50   |     |
| TL92H-09175P | 4   | 488  | 12  | 65  | .4  | 6   | 8   | 405  | 5.46 | 38  | 5   | ND  | 3   | 125 | 1   | 2   | 2   | 96  | 1.65 | .124 | 3   | 8   | .89  | 43  | .20 | 8   | 1.13 | .05 | .20 | 1   | 54  | 40   |     |
| TL92H-09176R | 2   | 438  | 15  | 46  | .6  | 5   | 8   | 384  | 5.44 | 28  | 5   | ND  | 3   | 207 | 1   | 2   | 2   | 91  | 1.83 | .124 | 3   | 9   | .98  | 41  | .18 | 8   | 1.09 | .06 | .23 | 1   | 75  | 50   |     |
| TL92H-09177R | 1   | 806  | 16  | 136 | .3  | 17  | 14  | 549  | 4.89 | 18  | 5   | ND  | 2   | 149 | 1   | 2   | 2   | 107 | 2.54 | .133 | 7   | 18  | 1.53 | 38  | .29 | 8   | 1.57 | .03 | .12 | 1   | 60  | 40   |     |
| TL92H-09178R | 1   | 839  | 11  | 113 | .5  | 7   | 7   | 509  | 4.58 | 16  | 5   | ND  | 2   | 123 | 1   | 2   | 2   | 116 | 1.29 | .126 | 3   | 12  | 1.49 | 45  | .22 | 4   | 1.65 | .03 | .12 | 2   | 78  | 20   |     |
| TL92H-09179R | 1   | 1904 | 11  | 137 | .2  | 11  | 21  | 839  | 3.88 | 12  | 5   | ND  | 2   | 107 | 1   | 2   | 2   | 128 | 1.07 | .119 | 4   | 11  | 2.02 | 37  | .23 | 5   | 2.35 | .03 | .09 | 2   | 36  | 5    |     |
| TL92H-09180R | 1   | 1751 | 12  | 112 | .4  | 10  | 17  | 892  | 4.40 | 12  | 5   | ND  | 2   | 104 | 1   | 2   | 2   | 135 | 1.18 | .122 | 4   | 13  | 2.14 | 48  | .27 | 2   | 2.45 | .03 | .12 | 2   | 60  | 5    |     |
| TL92H-09181R | 1   | 4677 | 14  | 279 | .5  | 54  | 36  | 1029 | 5.19 | 18  | 5   | ND  | 2   | 44  | 1   | 2   | 2   | 133 | 1.88 | .135 | 12  | 39  | 2.54 | 57  | .33 | 10  | 3.15 | .03 | .12 | 3   | 55  | 5    |     |
| TL92H-09182R | 10  | 456  | 10  | 29  | 1.5 | 3   | 4   | 180  | 3.88 | 10  | 5   | ND  | 2   | 79  | 1   | 2   | 2   | 62  | .31  | .083 | 3   | 5   | .40  | 38  | .14 | 3   | .78  | .05 | .19 | 1   | 152 | 10   |     |
| TL92H-09183R | 44  | 307  | 10  | 57  | .5  | 5   | 2   | 344  | 3.96 | 8   | 5   | ND  | 2   | 69  | 1   | 2   | 2   | 120 | .33  | .105 | 4   | 9   | .80  | 24  | .19 | 4   | 1.02 | .05 | .21 | 1   | 210 | 20   |     |
| TL92H-09184R | 17  | 906  | 7   | 67  | 1.3 | 3   | 5   | 629  | 2.75 | 5   | 5   | ND  | 2   | 47  | 1   | 2   | 2   | 74  | .34  | .077 | 5   | 6   | .76  | 48  | .08 | 8   | 1.02 | .05 | .18 | 1   | 220 | 10   |     |
| TL92H-09185R | 18  | 646  | 10  | 42  | 1.4 | 3   | 4   | 206  | 4.41 | 18  | 5   | ND  | 3   | 122 | 1   | 2   | 2   | 56  | .14  | .079 | 4   | 5   | .38  | 88  | .06 | 6   | .77  | .12 | .34 | 2   | 310 | 10   |     |
| STD C/ML-R   | 21  | 68   | 42  | 144 | 7.3 | 71  | 30  | 1088 | 3.95 | 46  | 13  | 8   | 37  | 52  | 18  | 16  | 21  | 66  | .48  | .089 | 39  | 63  | .88  | 193 | .09 | 36  | 1.85 | .07 | .15 | 14  | 480 | 1400 |     |

APPENDIX II a

STATEMENT OF EXPENDITURES - LUCKY CLAIM

Personnel: Ken Taylor, Proj. Supervisor \$ 150.00/day  
 John Nicholson, Geologist 100.00/day

Dates: June 14 (1/2 day) - established baseline  
 June 16 - 18 - soil sampled lines west of baseline  
 and rock sampled roadcuts.  
 June 20 (1 man) - rock sampled old trenches  
 June 23 - soil sampled lines east of baseline

Total Samples: 155 soil samples (13 no samples)  
 94 rock samples

Cost Breakdown:

|   |              |
|---|--------------|
| 4 1/2 man days at \$100.00/day                  | 450.00       |
| 5 1/2 man days at \$150.00/day                  | 825.00       |
| 5 days truck rental at \$65.00/day (incl. fuel) | 325.00       |
| 5 nights accommodation at \$38.88/night         | 194.40       |
| 10 man days of meals at \$25.00/man day         | 250.00       |
| Supplies (flagging, thread, bags etc.)          | 120.00       |
| 155 analysis of soils at 11.75/sample           | 1821.25      |
| 94 analysis of rocks at 14.00/sample            | 1316.00      |
| Report (1 day at \$150.00/day)                  | 150.00       |
| Drafting (6 hrs at \$15.00/hr)                  | <u>90.00</u> |
|   | \$5541.65    |

APPENDIX II b

STATEMENT OF EXPENDITURES - LUCKY 2 CLAIM

|            |                              |               |
|------------|------------------------------|---------------|
| Personnel: | Ken Taylor, Proj. Supervisor | \$ 150.00/day |
|            | John Nicholson, Geologist    | 100.00/day    |

|        |  |
|--------|--|
| Dates: | June 14 (1/2 day) - established baseline         |
|        | June 15 - soil sampled lines west of baseline    |
|        | June 20 (1 man) - sampled lines east of baseline |

Total Samples: 78 soil samples ( 6 no samples)  
1 rock sample

Cost Breakdown:

|   |           |
|---|-----------|
| 2 1/2 man days at \$100.00/day                    | 250.00    |
| 1 1/2 man days at \$150.00/day                    | 225.00    |
| 2 days truck rental at \$65.00/day ( incl. fuel ) | 130.00    |
| 2 nights accommodation at \$38.88/night           | 77.76     |
| 4 man days of meals at \$25.00/man day            | 100.00    |
| Supplies (flagging, thread, bags etc.)            | 30.00     |
| 78 analysis of soils at 11.75/sample              | 916.50    |
| 1 analysis of rock at 14.00/sample                | 14.00     |
| Report (1/2 day at \$150.00/day)                  | 75.00     |
| Drafting (2 hrs. at 15.00/hr)                     | 30.00     |
|   | <hr/>     |
|   | \$1848.26 |

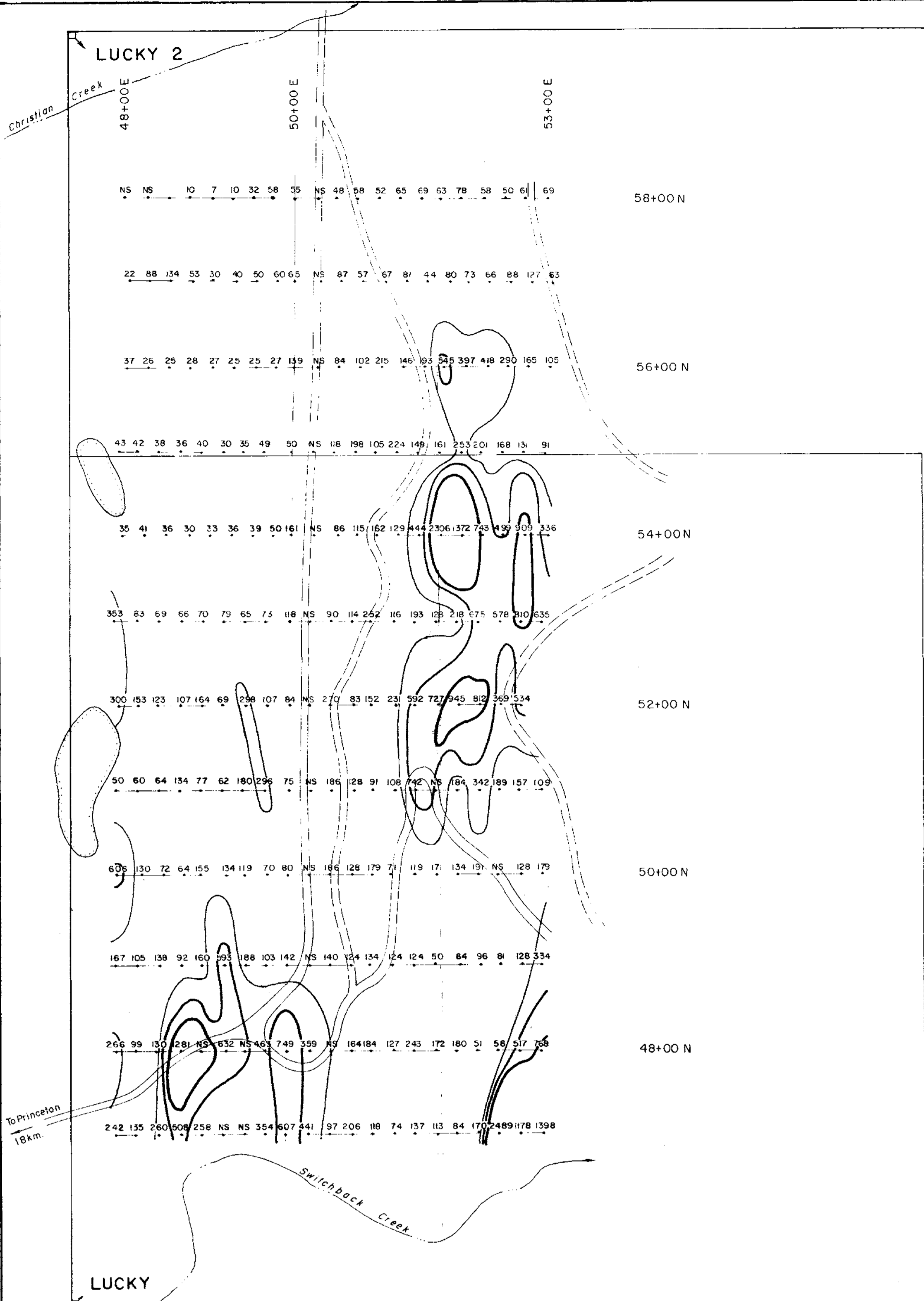
APPENDIX III

STATEMENT OF QUALIFICATION

I, Kenneth James Taylor of Surrey, British Columbia do hereby certify that:

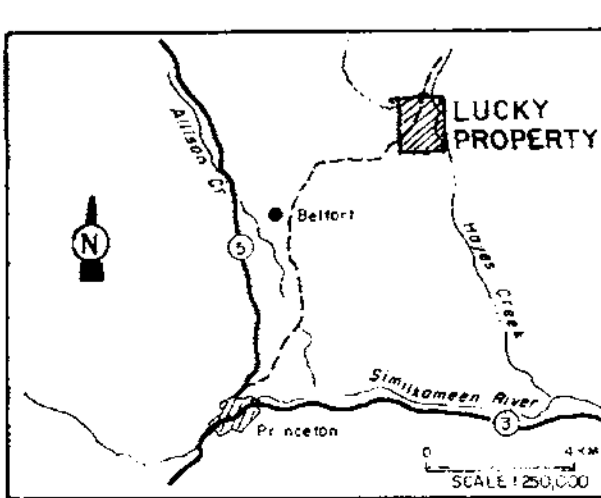
1. I am a geologist employed on a contract basis with Mingold Resources Inc. of 900A - 837 W. Hastings St., Vancouver, British Columbia.
2. I am a graduate from the University of British Columbia with a B.Sc. in Geology (1973).
3. I have been practising my profession for the past 14 years.
4. I am a Fellow in the Geological Association of Canada.
5. I supervised and coexecuted the work being applied for assessment on the Lucky and Lucky 2 claims in the Princeton area, British Columbia.





**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

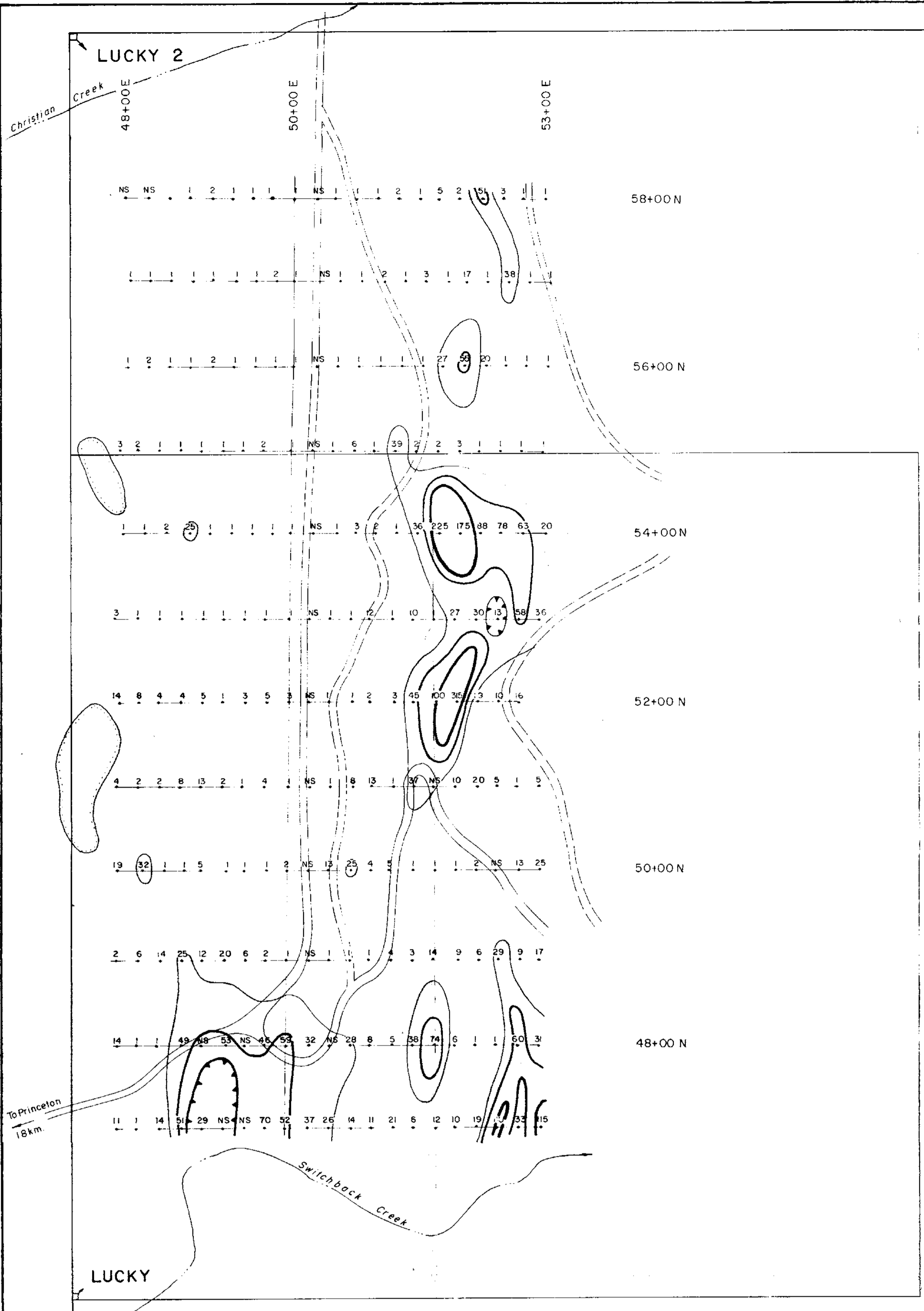
**16,265**



- LEGEND**
- Road
  - Creek
  - Lake
  - Sample location
  - Legal corner post
  - 180 Cu in ppm
- CONTOURS**
- 250-499
  - 500-749
  - ≥ 750

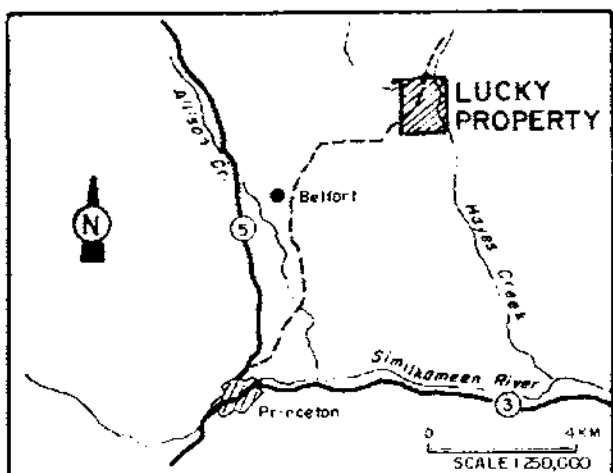


|   |                        |                |
|---|------------------------|----------------|
| <b>MINGOLD RESOURCES INC.</b><br>VANCOUVER OFFICE |                        |                |
| <b>LUCKY PROPERTY<br/>COPPER GEOCHEMISTRY</b>     |                        |                |
| NTS. 92H-9W                                       | SIMILKAMEEN M.D., B.C. |                |
| DRAWN BY E.Y.                                     | DATE: JULY 1987        | APPROVED BY:   |
| PRINCETON AREA                                    |                        | PLATE NO.<br>3 |



**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

**16,265**

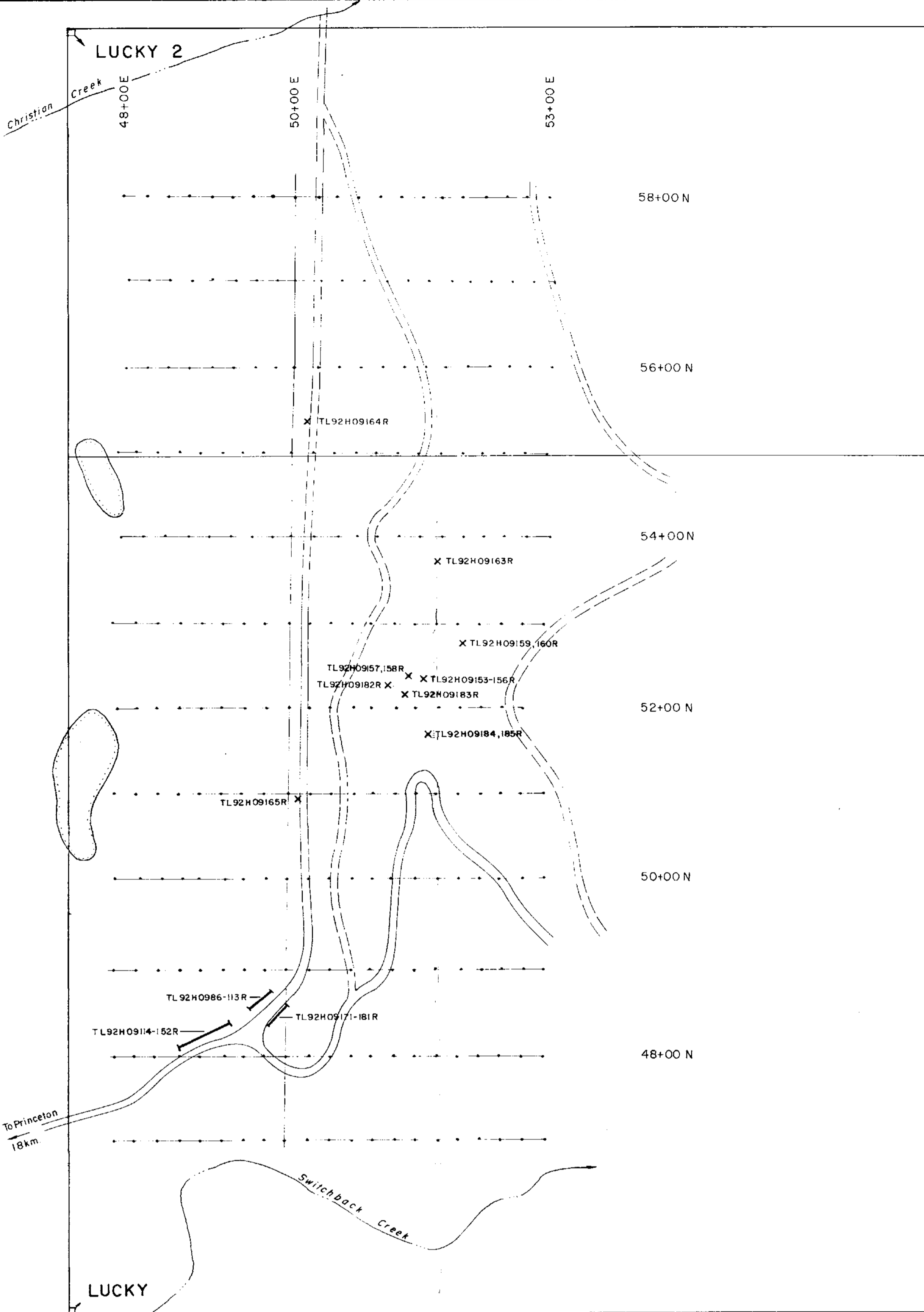


- LEGEND**
- Road
  - ~~~ Creek
  - Lake
  - Sample location
  - └┘ Legal corner post
  - 21 Au in ppb

- CONTOURS**
- 25-49
  - 50-99
  - ≥100



|   |                        |              |
|---|------------------------|--------------|
| <b>MINGOLD RESOURCES INC.</b><br>VANCOUVER OFFICE |                        |              |
| <b>LUCKY PROPERTY<br/>GOLD GEOCHEMISTRY</b>       |                        |              |
| NTS. 92H-9W                                       | SIMILKAMEEN M.D., B.C. |              |
| DRAWN BY E.Y.                                     | DATE: JULY 1987        | APPROVED BY: |
| PRINCETON AREA                                    | 0 50 100 150 metres    | PLATE NO. 4  |



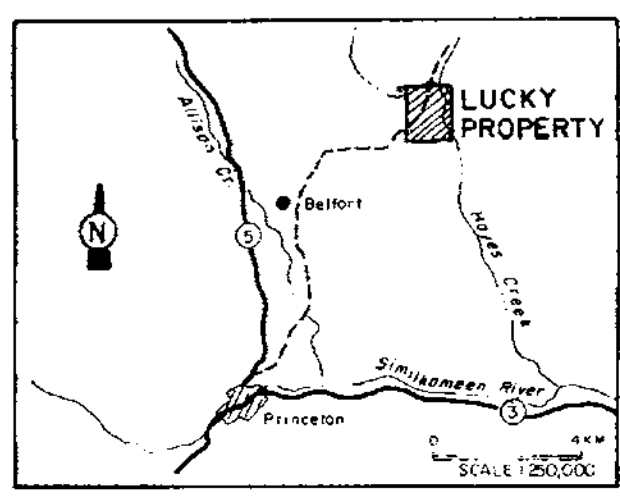
ROCK SAMPLE RESULTS

(All values continuous unless otherwise noted)

| Sample No. | Cu (ppm) | Ag (ppb) | Width (m)          |
|------------|----------|----------|--------------------|
| TL92H0906R | 315      | 41       | 2.0                |
| 07R        | 341      | 27       | 2.0                |
| 08R        | 632      | 40       | 2.0                |
| 09R        | 639      | 21       | 2.0                |
| 90R        | 514      | 23       | 2.0                |
| 91R        | 491      | 21       | 2.0                |
| 92R        | 927      | 26       | 2.0                |
| 93R        | 386      | 17       | 2.0                |
| 94R        | 321      | 14       | 2.0                |
| 95R        | 327      | 25       | 2.0                |
| 96R        | 525      | 22       | 2.0                |
| 97R        | 197      | 10       | 2.0                |
| 98R        | 142      | 8        | 2.0                |
| 99R        | 267      | 5        | 2.0                |
| 100R       | 415      | 6        | 2.0                |
| 101R       | 116      | 7        | 2.0                |
| 102R       | 156      | 5        | 2.0                |
| 103R       | 439      | 10       | 2.0                |
| 104R       | 197      | 21       | 2.0                |
| 105R       | 490      | 20       | 2.0                |
| 106R       | 136      | 15       | 2.0                |
| 107R       | 979      | 30       | 2.0                |
| 108R       | 364      | 26       | 2.0                |
| 109R       | 134      | 35       | 2.0                |
| 110R       | 101      | 44       | 2.0                |
| 111R       | 320      | 55       | 2.0                |
| 112R       | 323      | 70       | 2.0                |
| 113R       | 230      | 25       | 2.0                |
| 114R       | 221      | 19       | 2.0                |
| 115R       | 213      | 16       | 2.0                |
| 116R       | 300      | 10       | 2.0                |
| 117R       | 573      | 12       | 2.0                |
| 118R       | 933      | 37       | 2.0                |
| 119R       | 1852     | 44       | 2.0                |
| 120R       | 964      | 40       | 2.0                |
| 121R       | 1147     | 60       | 2.0                |
| 122R       | 860      | 40       | 2.0                |
| 123R       | 366      | 39       | 2.0                |
| 124R       | 467      | 16       | 2.0                |
| 125R       | 70       | 25       | 2.0                |
| 126R       | 49       | 27       | 2.0                |
| 127R       | 54       | 15       | 2.0                |
| 128R       | 70       | 20       | 2.0                |
| 129R       | 100      | 16       | 2.0                |
| 130R       | 89       | 18       | 2.0                |
| 131R       | 51       | 22       | 2.0                |
| 132R       | 54       | 12       | 2.0                |
| 133R       | 52       | 15       | 2.0                |
| 134R       | 65       | 15       | 2.0                |
| 135R       | 45       | 22       | 2.0                |
| 136R       | 140      | 20       | 2.0                |
| 137R       | 161      | 16       | 2.0                |
| 138R       | 295      | 13       | 2.0                |
| 139R       | 210      | 18       | 2.0                |
| 140R       | 297      | 21       | 2.0                |
| 141R       | 250      | 13       | 2.0                |
| 142R       | 290      | 8        | 2.0                |
| 143R       | 542      | 21       | 2.0                |
| 144R       | 630      | 15       | 2.0                |
| 145R       | 737      | 43       | 2.0                |
| 146R       | 1084     | 35       | 2.0                |
| 147R       | 362      | 19       | 2.0                |
| 148R       | 329      | 52       | 2.0                |
| 149R       | 463      | 22       | 2.0                |
| 150R       | 346      | 20       | 2.0                |
| 151R       | 393      | 34       | 2.0                |
| 152R       | 228      | 31       | 2.0                |
| 153R       | 5742     | 250      | 2.0                |
| 154R       | 1520     | 220      | 2.0                |
| 155R       | 2168     | 360      | 1.0                |
| 156R       | 674      | 350      | 2.0                |
| 157R       | 496      | 133      | 2.0                |
| 158R       | 463      | 165      | 2.0                |
| 159R       | 8215     | 460      | 2.0                |
| 160R       | 7409     | 470      | 1.0                |
| 161R       | 1641     | 360      | 2.0                |
| 162R       | 1021     | 350      | 2.0                |
| 163R       | 1514     | 230      | 2.0                |
| 164R       | 270      | 52       | 50.0 (random chit) |
| 165R       | 2368     | 280      | 4.0                |

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

**16,265**



- LEGEND**
- Road
  - Creek
  - Lake
  - Sample location
  - Legal corner post
  - X Rock sample location



**MINGOLD RESOURCES INC.**  
VANCOUVER OFFICE

**LUCKY PROPERTY  
ROCK SAMPLE MAP**

N.T.S. 92H-9W SIMILKAMEEN M.D., B.C.

|                |                    |              |
|----------------|--------------------|--------------|
| DRAWN BY: E.Y. | DATE: JULY 1987    | APPROVED BY: |
| PRINCETON AREA | 0 50 100 150metres | PLATE NO. 5  |