LOG NO: 1020 RD.

ACTION:

FILE NO: 87-640-16298

ASSESSMENT REPORT

FOR THE

1987 DIAMOND DRILLING 7/88

ON

CERTIFIED MINING LEASE No. 1

OMINECA MINING DIVISION

NTS 93 L/1W

LATITUDE 54° ~~10'~~ 11'12" N

LONGITUDE 126° 15' 54" W

OWNED BY: EQUITY SILVER MINES LIMITED

WORK BY: EQUITY SILVER MINES LIMITED

REPORT BY: R. B. PEASE

OCTOBER 1987

FILMED

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,298

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FIGURES AND TABLES

INTRODUCTION

(i) Location and Access

The Equity Silver minesite is located 40 km southeast of the town of Houston, British Columbia (see Figure 1). The minesite lies in the gentle, and occasionally steep, hills of the Nechako Plateau physiographic region. Access is gained to the property by an all-weather gravel road from Houston (see Figure 2). The drillholes discussed in this report are located in the Main zone orebody (see Figure 3). Access to the drillsites is via existing Main zone access roads.

(ii) Claim Ownership and Status

The Equity minesite property consists of Certified Mining Lease # 1 and Mining Lease # 6 surrounded by a block of 289 two-post mineral claims, 7 fractional claims, and 3 modified grid claims (43 units). In addition, 19 two-post claims and one fraction are jointly held with Teck Corporation and Pioneer Metals Corporation.

The drilling was conducted on Certified Mining Lease No. 1. This lease is wholly owned by Equity Silver Mines Limited and is not subject to any vendor agreement. For the purpose of recording assessment, several adjoining claims have been grouped to form the 87-1 group.

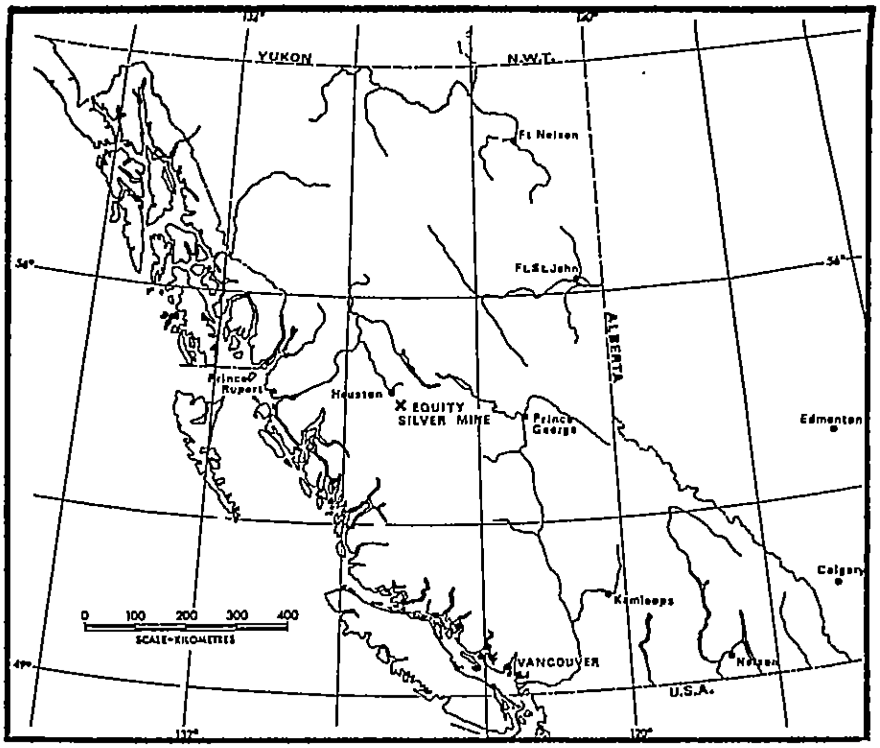


FIGURE 1 - MINESITE LOCATION

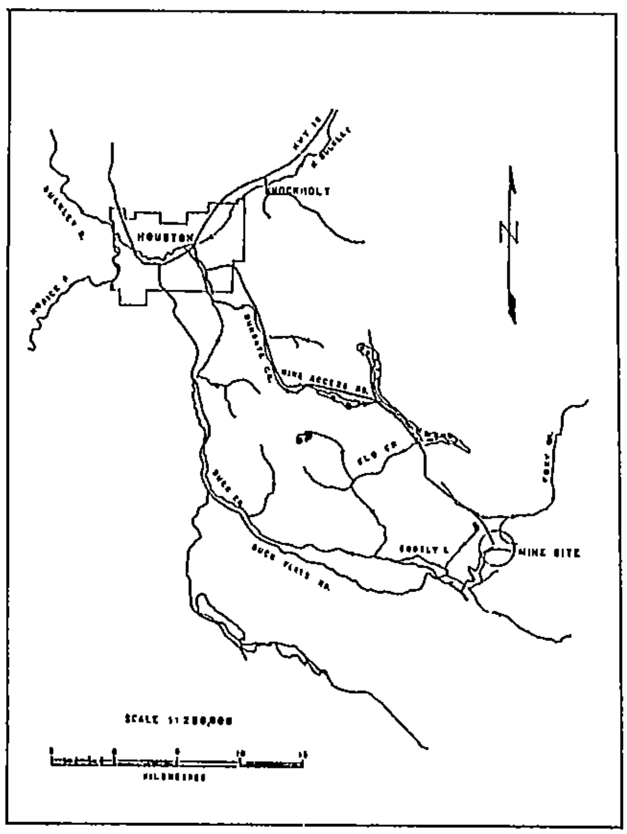


FIGURE 2 - MINESITE ACCESS

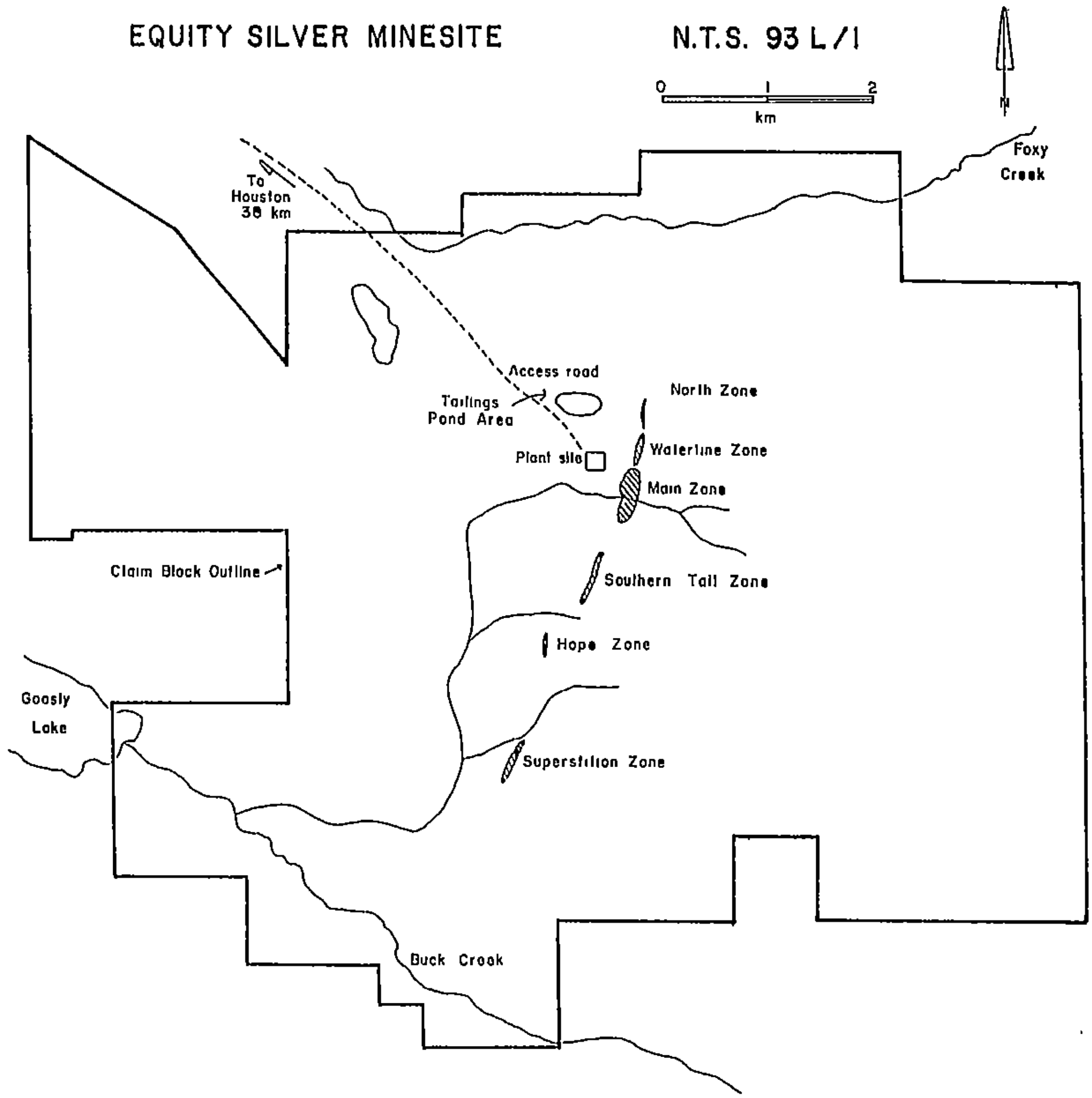


FIGURE 3 - PROPERTY LAYOUT

The company has been continuously operating a 5 500 tpd open pit mining and milling complex at this site since mid 1980. Production was increased to 10 000 tpd in mid 1986. Three ore deposits are known to occur on Certified Mining Lease # 1. The Southern Tail deposit has been mined out to the economic limit of an open pit. The Main Zone deposit is currently being mined by an open pit, and the Waterline deposit has yet to be developed. Proven ore reserves, as of January 1987, were approximately 18.3 million tonnes at a grade of 0.26 % copper, 85 g/t silver, and 1.03 g/t gold.

(iii) Purpose

Seven NQ size diamond drillholes, totalling 2,099.2 metres, were drilled in the Main zone to test possible extensions of the mineralized structure at depth. The potential intersections would be outside the current design of the main zone pit. High grade intersections could expand the pit boundaries and increase the mining reserve.

PROPERTY DESCRIPTION

(i) Geology

The geology of the Equity Silver property is briefly described below and illustrated on Figure 4. The reader is referenced to Cyr, et al. (1984) for a more detailed description.

The deposits occur in a homoclinal Upper Jurassic to Cretaceous inlier consisting of sedimentry, pyroclastic, and volcanic rocks flanked by intrusions and surrounded by younger, unconformable Tertiary andesitic to basaltic flows and flow breccias. Four stratigraphic conformable subdivisions, termed the Goosly Sequence, are recognized in the inlier and consist of a basal conglomerate and argillite (clastic division); intercalated sub-aerial tuffs and breccias (pyroclastic division); interbedded volcanic conglomerate, sandstone, and bedded tuff (sedimentry-volcanic division); and andesite and dacite flows (volcanic flow division). The Goosly sequence has an overall strike of 015 and dips generally to the west.

A quartz monzonite stock (58 m.y.) on the west, and a gabbro-monzonite complex (49 m.y.) to the east, intrude the Goosly sequence. Post-mineral andesite and quartz latite dykes (49 m.y.) crosscut the Goosly sequence and the gabbro-monzonite complex.

(ii) Mineralization

Economically significant Cu-Ag-Au mineralization occurs in three distinct zones designated the Main, Waterline, and Southern Tail orebodies (see Figure 4). Pyrite is the most abundant metallic mineral throughout the Goosly sequence regionally, and within the zones of Cu-Ag-Au mineralization in particular. The principal silver mineral is tetrahedrite with minor values contributed by a variety of argentiferous minerals. Chalcopyrite is the principal copper mineral and a smaller but significant portion is in tetrahedrite.

The ore minerals are generally restricted to tabular zones subconcordant to host rock stratigraphy. They occur as disseminations, veins, fracture fillings, and locally as massive pods and matrix material in breccia zones. The primary ore control is structural, since "economic" sulphides tend to be best concentrated in zones of intense fracturing and brecciation.

It is believed the Cu-Ag-Au mineralization is epigenetic in origin. Intrusive activity resulted in the introduction of hydrothermal metal-rich solutions into the pyroclastic division of the Goosly sequence. Sulphides introduced into the more competent and permeable ash and lapilli tuffs of the Main and Waterline zones formed as stringers and disseminations which grade randomly into zones of massive sulphide. In the Southern Tail Zone, sulphides formed as veins, fracture fillings, and breccia zones in the brittle, less permeable fine grained dust tuff. Emplacement of postmineral dykes into all types of sulphide-rich pyroclastic rocks resulted in remobilization and concentration of sulphides adjacent intrusive contacts. Remobilization, concentration, and contact metamorphism of sulphides occurred in the Main and Waterline zones at the contact with the postmineral gabbro-monzonite complex.

(iii) Alteration

Alteration assemblages in the Goosly sequence are characterized by minerals rich in alumina, boron, and phosphorous. The distribution of various alteration zones is illustrated on Figure 5. Four types of alteration are recognized and briefly described below. The reader is referenced to Wojdak and Sinclair (1984) for a more detailed discussion.

1. Aluminous alteration is characterized by a suite of aluminous minerals including analusite, corrundum, pyrophyllite, and scorzalite. These alteration zones show a systematic spatial relationship to areas of mineral deposits.

2. Boron-bearing minerals consisting of tourmaline and dumortierite occur within the ore zones and in the hangingwall section of the Goosly sequence.

3. Phosphorous-bearing minerals including scorzalite, apatite, augelite, and svanbergite occur in the hangingwall zone, immediately above and intimately associated with sulphide minerals - particularly in the Main and Waterline zones.

4. Phyllic alteration is characterized by weak to pervasive sericite-quartz replacement. It appears to envelope zones of intense fracturing, with or without chalcopyrite/tetrahedrite occurences, particularly in Unit 2 dust tuffs.

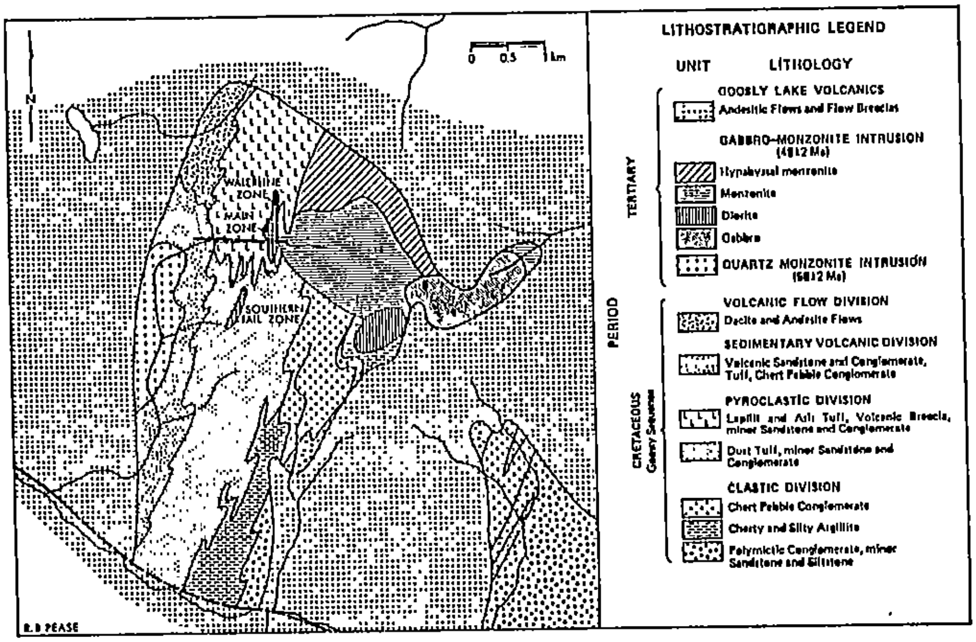


FIGURE 4 PROPERTY GEOLOGY

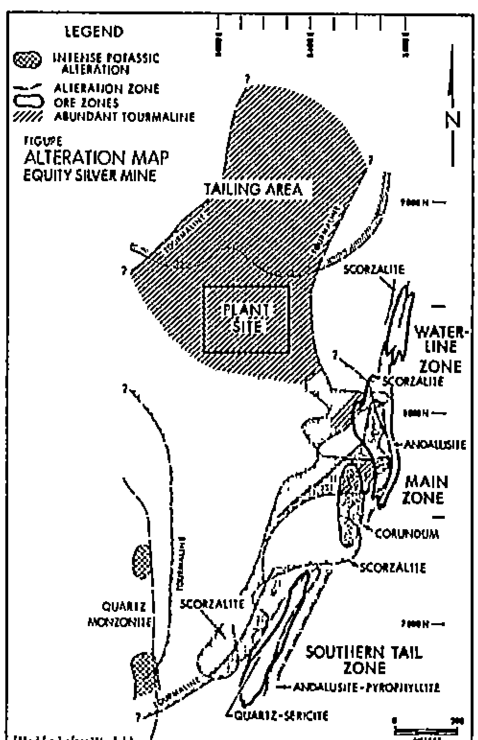


FIGURE 5 - PROPERTY ALTERATION

DRILLING PROGRAMME

The programme consisted of 2099.2 m of NQ wireline diamond drilling spread over seven (7) holes. The collar locations and surface projections of the drillholes are shown on Figure 6. The drillholes were inclined at angles of -60, -65, or -70 degrees, and orientated in an easterly direction. The drillholes were positioned intersect the potential down-dip extension of the Main zone mineralized structure 50 to 100 metres below the deepest existing drillhole intersection.

The drill setup pads and access roads were constructed prior to drill mobilization by Equity's D8 tractor. The drilling contractor was J. T. Thomas Diamond Drilling of Smithers, B.C. A skid-mounted Acker hydraulic wireline drill rig was utilized, and the contractor supplied a tractor to move and assist the drill. The drilling of hole X87CH310 commenced on April 27 and hole X87CH316 was finished on May 18. All of this core was logged and sampled by May 28.

The core was transported to the logging facilities at the minesite immediately following hole completion. The core was logged by the author, Mr. Daryl Hanson, and Mr. Darin Labrenz. Mr. Hanson, a geologist temporarily employed by Equity, has prevalent academic and practical training, holding a B.Sc. degree in geology and having over ten years experience in mineral exploration. Mr. Labrenz, also a geologist temporarily employed by Equity, recently obtained a B.Sc. degree in geology, and logged two holes under the supervision of the author and Mr. Hanson. The drillhole logs have been reproduced and are

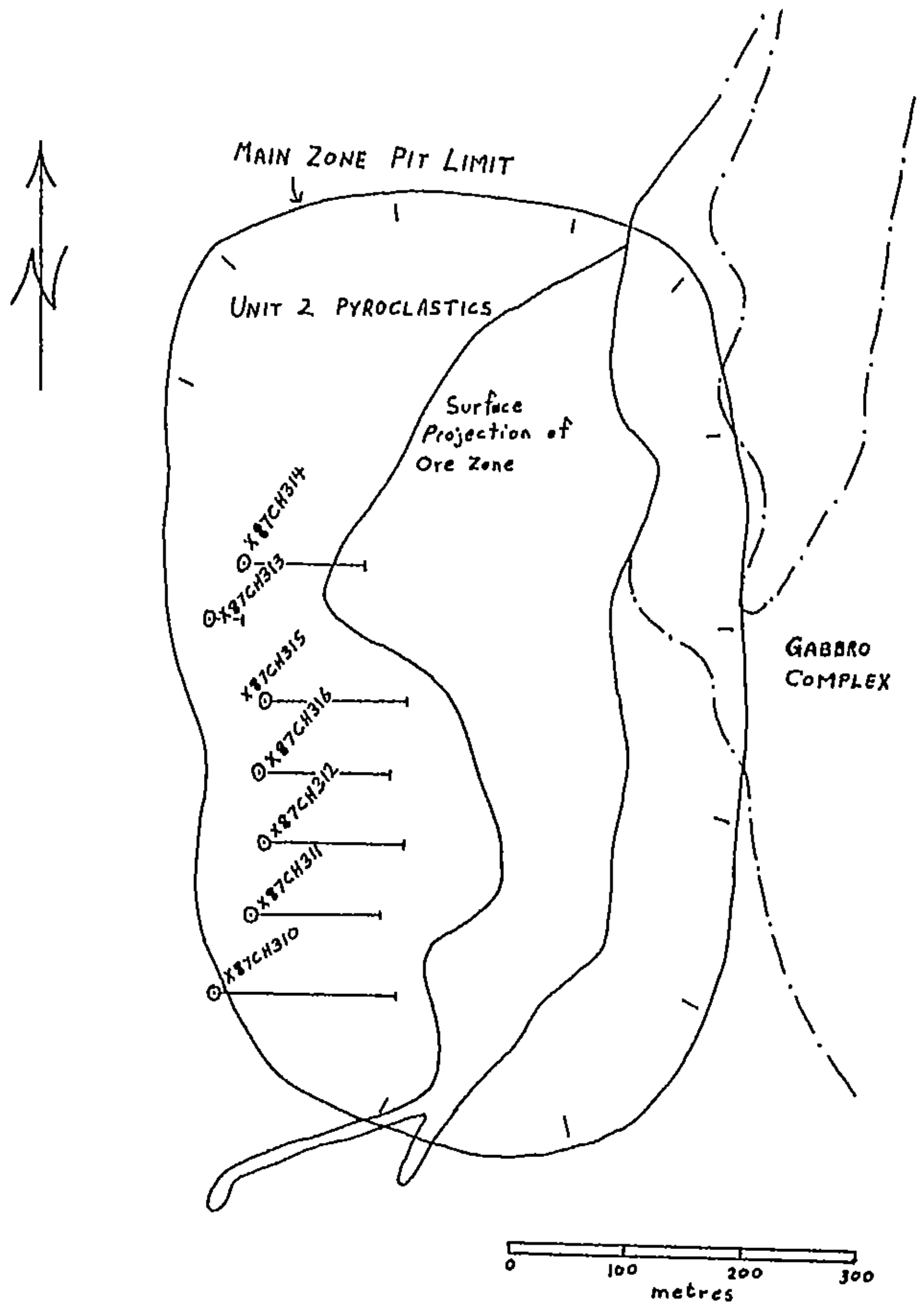


FIGURE 6 - DRILLHOLE LOCATIONS

included in this report as Appendix II. Assay results for the sampled intervals are recorded at the end of the logs. All assay results are recorded in percent, except silver and gold which are reported in grams/tonne.

A coded core logging system was utilized on this programme mainly to improve the measure of objectivity, consistency, measureability, and readability as compared to handwritten logs. The system allows geologic and assay data to be entered into formatted computer data files. These files can be accessed by programs which plot sections and plans, perform statistical analyses, and assist in reserve calculations. An explanation of the logging codes is provided in Appendix I.

The core was sampled generally top to bottom in approximately 3.0 metre intervals. Barren dyke intersections were generally omitted, as well as some of the weakly altered volcanics. Sampling was done by a hand operated core splitter. One half was placed in plastic sample bags and delivered to Equity's minesite laboratory for assay, and the other half was returned to the core box for permanent storage. The split core is stored in the facilities at the minesite.

The core samples were assayed for the metals Cu, Ag, Au, Sb, As, Fe, and Zn. In Equity's assay procedure, 1 gram of pulverized material is dissolved in 10 ml of nitric acid and 30 ml of hydrochloric acid. This solution is boiled for fifteen (15) minutes, after which 10 ml of 10% tartaric acid is added and the sample is returned to the hot plate for five (5) minutes. The solution is allowed to cool and quantitative analysis is done on an atomic absorption machine, except for Au which is fire assayed first.

RESULTS

The geology of the drilling area is restricted to Unit 2 of the Goosly sequence. These rocks are mainly lapilli, ash, and dust tuffs, with some volcanic breccia (which maybe a mylonite) and volcanic conglomerate. Numerous post-mineralization andesite and quartz latite dykes cut through the area. Some pre-mineral andesite dykes were also intersected generally deeper in the holes close to the gabbro-monzonite complex. The holes were drilled into the monzonite phase of the gabbro-monzonite complex before they were terminated.

The Unit 2 rocks displayed generally only low grade alteration in the form of weak silicification and occasional patches of scorzalite. The assay results were discouraging since generally only low grade mineralization was intersected, even though it was intersected over widths of 10's of metres. "Low grade" means grades of generally less than 0.3 % Cu, 40 g/t Ag, and 0.5 g/t Au. Material of this grade is below Equity's current economic cut-off.

Therefore, the drilling had no impact on the mining reserve of the Main zone pit.

TABLE 1

STATEMENT OF EXPENDITURES

1.	Diamond Drilling 2099.2 metres @ 44.90/m	94 254.08
2.	Sample Assaying 510 samples @ 15.00/sample	7 650.00
3.	Salaries R. Pease, logging and supervision Apr. 27,28,29,30, May 1,5,6,7,8,11,12,13,19 13 days @ 185.00/day	2 405.00
	D. Hanson, logging and supervision May 5,6,7,8,13,14 6 days @ 165.00/day	990.00
	D. Labrenz, logging May 13,14,15,19,20,21,22,25,26,27 10 days @ 110.00/day	1 100.00
	T. Hallbaurer, splitting core May 4,6,8,11,13,15,19,20,22,25,26,28 12 days @ 125.00/day	1 500.00
4.	Vehicle Rental and Fuel 30 days @ 50.00/day	1 500.00
6.	Report Preparation	2 000.00
		$ 111 399.08

AUTHOR'S QUALIFICATIONS

I, Robert B. Pease, do hereby certify that:

1. I am a geologist residing at R. R. # 1, Kerr Road, Telkwa, British Columbia.

2. I am a 1981 graduate of the University of Waterloo, Waterloo, Ontario, with an Honours Bachelor of Science degree in Earth Sciences.

3. As a student, I spent some twenty (20) months employed in the mineral exploration field with several mining companies in various regions of Canada.

4. I was employed as an exploration geologist with Duval International Corporation in Vancouver from May 1981 to January 1982.

5. Since February of 1982, I have been continously employed as an exploration geologist with Equity Silver Mines Limited in Houston, British Columbia.

6. I am an Associate Member of the Geological Association of Canada, and a Member of the Canadian Institute of Mining and Metallurgy.

7. I personally supervised the work programmes as described in this report.

Respectfully submitted,

EQUITY SILVER MINES LIMITED

R. B. Pease, B.Sc.
Exploration Geologist

REFERENCES

Cyr, J. B.; Pease, R. B.; and Schroeter, T. G. (1984): Geology and Mineralization at Equity Silver Mine. Journal of Econ. Geol., Vol. 79, pp. 947-968.

Wojdak, P. J. and Sinclair, A. J. (1984): Equity Silver Ag-Cu-Au Deposit: Alteration and Fluid Inclusion Studies. Journal of Econ. Geol., Vol. 79, pp. 969-990.

APPENDIX I

Diamond Drillhole Logging Code Explanation

LOGGING CODE EXPLANATION

Column 1 is a key which indicates the type of data or information on each line.

I - Identity information/data
S - Survey data
/ - Upper tier geologic data
L - Lower tier geologic data
R - Free form remarks
A - Assay and analysis data

I DATA

The first line indicates:

Col. 17 to 24 - Drillhole Name
Col. 26 to 27 - Size of Core
Col. 29 to 35 - Day/Month/Year Logged
Col. 36 to 38 - Logger's Initials
Col. 39 to 41 - Helper's Initials (if any)
Col. 42 to 45 - Drilling Contractor
Col. 46 to 50 - Month/Year Hole Drilled
Col. 51 to 53 - Drill Rig Type
Col. 63 to 68 - Grid Azimuth (0.0 if True North)

The second line indicates:

Col. 5 to 45 - Company Name
Col. 46 to 80 - Zone and type of Geocode* used.

NOTE: * Equity uses two types of Geocodes, ST and MN. The ST geocode is used when a hole is drilled south of the Main Zone, and the MN geocode is used to the north of, and including, the Main Zone. This is done to reflect the differing host rock and style of mineralization/alteration between the northern and southern sections of the property.

S DATA

The S000 line is the collar survey data. Subsequent S lines (S001, S002, etc.) are down-the-hole surveys.

Col. 5 to 10 - From (a decimal point is inferred between column 8 and 9)
Col. 11 to 16 - To (a decimal point is inferred between column 14 and 15)
Col. 17 to 18 - Units; MT (metres), FT (feet)
Col. 20 to 26 - Total Length
Col. 27 to 32 - Azimuth
Col. 33 to 38 - Dip
Col. 51 to 60 - Northing
Col. 61 to 70 - Easting
Col. 71 to 80 - Elevation

/ AND L DATA

Disregard the /SCL and LSCL lines, they are only for computer processing. Two lines are available to describe a geologic interval, the upper line (/) and the lower line (L). The /NAM line defines the mineral fields for the upper line, and the LNAM defines the lower line. These mineral fields change according to the type of Geocode (ST or MN) used.

ST Geocode - upper (/NAM) line

Col. 57, 58 MS - Muscovite (sericite)
Col. 59, 60 CL - Chlorite
Col. 61, 62 QZ - Quartz
Col. 63, 64 PY - Pyrite
Col. 65, 66 CP - Chalcopyrite
Col. 67, 68 TT - Tetrahedrite
Col. 69, 70 AS - Arsenopyrite
Col. 71, 72 PR - Pyrrhotite

- lower (LNAM) line

Col. 57, 58 CB - Carbonate
Col. 59, 60 GY - Gypsum
Col. 63, 64 MG - Magnetite
Col. 65, 66 HE - Hematite
Col. 67, 68 SL - Sphalerite
Col. 69, 70 GL - Galena
Col. 71, 72 MO - Molybdenum

MN Geocode - upper (/) line

Col. 57, 58 QZ - Quartz
Col. 59, 60 SZ - Scorzalite
Col. 61, 62 TO - Tourmaline
Col. 63 to 72 - Same as ST Geocode
Col. 73 to 74 - Gypsum

- lower (L) line

Col. 57, 58 DM - Dumortierite
Col. 59, 60 CB - Carbonate
Col. 61, 62 CL - Chlorite
Col. 63 to 72 - Same as ST Geocode

Upper (/) Geologic Data

Col. 5 to 10 - From (decimal inferred between 8 and 9)
Col. 11 to 16 - To (decimal inferred between 14 and 15)
Col. 17 to 20 - Recovery in Metres (decimal inferred between 18 and 19)
Col. 24 to 27 - Rock Type Code - See Rock Type Chart
Col. 28 to 29 - Typifying Mineral 1 - see Mineral Chart
Col. 30 to 31 - Typifying Mineral 2 - see Mineral Chart
Col. 35 to 36 - Texture 1 - see Texture Chart
Col. 37 to 38 - Texture 2 - see Texture Chart
Col. 47 - Essentially always a "P" which stands for Principle Geologic Interval. If "D", it stands for Ditto Interval which means all of the above interval description applies, except as noted.
Col. 49 to 50 - Structure 1 - see Structure Chart
Col. 55 to 56 - Angle to Core Axis of Structure 1
Col. 57 - Mineral Field, Mode of Occurence - see How Chart
Col. 58 - Mineral Field, Amount of Occurence - see Amount Chart
Col. 59 to 72 - Mineral Fields, same pattern continues (ie. How, Amount) as in columns 57, 58.

Lower (L) Geologic Data

Col. 17 to 20 - RQD in Metres (decimal inferred between 18 and 19)
Col. 28 to 29 - Colour Code - see Colour Chart
Col. 35 to 36 - Typifying Mineral 3 - see Mineral Chart
Col. 37 to 38 - Typifying Mineral 4 - see Mineral Chart
Col. 43 - Count of Fractures at Steep Angle to Core Axis - See Amount Chart
Col. 44 - Count of Fractures at Medium Angle to Core Axis - See Amount Chart
Col. 45 - Count of Fractures at Low Angle to Core Axis - See Amount Chart
Col. 46 - Count of Total Fractures - See Amount Chart

NOTE: Columns 43 to 46 not always used

Col. 49 to 50 - Structure 2 - see Structure Chart
Col. 55 to 56 - Angle to Core Axis of Structure 2
Col. 57 to 72 - Mineral Fields, as in upper (/) Data

R DATA

These are free form remarks written by the logger to further describe the gelogic interval. Note that Rock Type Codes (see Rock Type Charts) are often used.

A DATA

This last type of data lists the assay information for the hole. Note that remarks are also used.

The first line, A001, defines a "set" of assay data. eg. A002 would define a different set, etc. The following lines describe and list the assay data.

ALAB Col. 17 to 80 - Define Laboratory
ATYP Col. 17 to 80 - Define Type of Determination
AMTH Col. 17 to 80 - Define Analytical Method
AUMM Col. 17 to 80 - Define Assay Fields
A001 Col. 5 to 10 - From (decimal inferred between 8 and 9)
Col. 11 to 16 - To (decimal inferred between 18 and 19)
Col. 23 to 26 - Sample Number
Col. 33 to 38 - Percent Copper
Col. 39 to 44 - Grams/Tonne Silver
Col. 45 to 50 - Grams/Tonne Gold
Col. 51 to 56 - Percent Antimony
Col. 57 to 62 - Percent Arsenic
Col. 63 to 68 - Percent Iron
Col. 69 to 74 - Percent Zinc

CHARTS

1. Rock Type Chart

A four digit code is used to describe rock types. The first and second digits are common to both ST and MN Geocodes. The first digit (number) defines stratigraphic unit, and the second digit (letter) defines a lithology unique to the stratigraphic unit. In the ST

Geocode, the third digit (number) defines the intensity of fracturing or brecciation, and the fourth digit (number) defines the type and intensity of alteration. In the MN Geocode, the third digit (number) defines the alteration, and the fourth digit (number) defines the mineralization.

One special code, OVBN, is used for overburden.

First Digit	Stratigraphic Unit	Second Digit	Lithology
1	Clastic Division	A	Polymictic Conglomerate
		B	Cherty or Silty Conglomerate
		C	Chert Pebble Conglomerate
		D	Quartz Sandstone
		E	Cherty Argillite
		F	Silty Argillite
2	Pyroclastic Division	A	Flow Breccia
		B	Ash Flow
		C	Dust Tuff
		D	Ash Tuff
		E	Lapilli Tuff
		F	Volcanic Breccia
		G	Volcanic Sandstone
		H	Volcanic Conglomerate
		I	Welded tuff
		J	Interbedded Dust and Ash Tuff
		K	Lahar
		L	Tuffaceous Siltsone
		M	Claystone
3	Sedimentry - Volcanic Division	A	Chert Pebble Conglomerate
		B	Quartz Sandstone
		C	Laminated Dust Tuff
		D	Volcanic Conglomerate
		E	Volcanic Sandstone
		F	Dust Tuff
		G	Ash Tuff
		H	Lapilli Tuff
		I	Volcanic Siltstone
		J	Interbedded Dust and Ash Tuff
		K	Silty Argillite
4	Volcanic Flow Division	A	Andesite Flow
		B	Dacite Flow
6	Quartz Monzonite	A	Fresh Quartz Monzonite
		B	Altered (Potassic) Quartz Monzonite

7	*Gabbro-Monzonite Complex*	A	*Gabbro*
		B	Diorite
		C	Monzonite
		D	Hypabyssal Monzonite Prophyry
		E	Gabbro - Monzonite Transition Phase
8	Property Dykes	A	Andesite
		B	Trachyandesite
		C	Quartz Latite
		D	Post-mineral Andesite
9	Tertiary Volcanics (Goosly Lake Fm)		
		A	Trachyandesite Flow
		B	Amygdaloidal Andesite Flow
		C	Flow Breccia
		D	Reddish-Purple Flow
		E	Massive Andesite Flow
		F	Quartz-eye Porphyry (Latite)
		G	Tuffaceous Sandstone/Siltstone

ST - Geocode

Third Digit	Intensity of Fracturing or Brecciation
0	No Fracturing
1	Weak Fracturing
2	Moderate Fracturing
3	Mod to Strong Fracturing
4	Strong Fracturing
5	Weak Brecciation
6	Weak to Mod Brecciation
7	Moderate Brecciation
8	Mod to Strong Brecciation
9	Strong Brecciation

Fourth Digit	Type and Intensity of Alteration
0	Unaltered
1	Weak Propylitic (CHL - CLAY)
2	Strong Propylitic
3	Weak Phyllic (QTZ - SER.)
4	Moderate Phyllic
5	Pervasive Phyllic
6	Advanced Argillic
7	Weak Potassic
8	Strong Potassic
9	Silicic (QTZ)

MN - Geocode

Third Digit	Alteration
0	Unaltered
1	Propylitic
2	Scorzalite Bearing/Argillic
3	Andalusite Bearing/Argillic
4	Moderate Silicification
5	Strong Silicification
6	Biotite Hornfels
7	Pyrite Porphyroblast Bearing
8	Phyllic (Quartz-Sericite)
9	Quartz - Tourmaline

Fourth Digit	Sulphide Mineralization
0	None
1	Disseminated Pyrite +/- Chalcopyrite
2	Pyrite - Magnetite Intergrowths
3	Sulphide Bearing (CP+/-PY+/-SL) Stringers
4	Sulphide Bearing (CP+/-PY) Patches
5	Massive Sulphide (CP+/-PY+/-TT+/-PO+/-SL) Replacements or Remobilized
6	Grey, "Dusty" Sulphides (fine grained mixture of sulphides and quartz)
7	Sulphides in Breccia Matrix (CP+/-PY+/-TT+/-SL)

2. Mineral Chart (ie. Mineral short-forms)

QZ	Quartz
CL	Chlorite
CY	Clay
CB	Carbonate
PY	Pyrite
MS	Muscovite
CP	Chalcopyrite
TT	Tetrahedrite
AS	Arsenopyrite
PR	Pyrrhotite
MG	Magnetite
HE	Hematite
SL	Sphalerite
GL	Galena
MO	Molybdenite
GY	Gypsum
EP	Epidote
FL	Feldspar
BI	Biotite

3. Texture Chart (ie. Texture Short-Forms)

<<	Micro Veins
MX	Massive
BR	Brecciated
P*	Porphyritic
A*	Amygdaloidal
TC	Trachytic
WP	Wispy
VU	Vugs
AD	Adherring/Pyroclastic
RC	Chilled Rind/Pyroclastic

4. Structure Chart (ie. Structure Short-Forms)

C/	Contact
BD	Bedding
V/	Vein
F/	Fault
BN	Banding
FB	Flow Banding
CU	Upper Contact
CL	Lower Contact
SH	Shear

5. How Chart

Symbol	Most Dominant Mode of Occurence
A	Amygdaloids, cavity fillings
B	Blebs
#	Breccia fillings
C	Coatings & encrustations
*	Clasts
D	Disseminations & scat.x'ls
E	Envelopes
F	Framework crystals
G	Gouge
H	Halos
I	Eyes, augen
J	Interstitial
K	Stockwork
L	Laminated/bedded
M	Massive
N	Nodules
O	Spots
Q	Patches, as in quilts
R	Rosettes & x'tls clusters
S	Selvages
$	Sheeting
T	Stainings, as in tarnish
U	Euhedral crystals

V	Veins
>	Macroveins
<	Microveins
W	Boxwork
X	Massive and/or laminated/bedding
Y	Dalmationite
Z	Fresh, primary rock
+	Flooding

6. Amount Chart

Code	Assigned Value	Range
X	100	100
9	90	85 to 99
8	80	75 to <85
7	70	65 to <75
6	60	55 to <65
5	50	45 to <55
4	40	35 to <45
3	30	25 to <35
2	20	15 to <25
1	10	7 to <15
=	5	4 to < 7
+	3	2 to < 4
)	1	.5 to < 2
*	.3	.2 to <.5
(	.1	.05 to <.2
–	.03	.02 to <.05
.	.01	Trace = <.02
0	0	Nil, Absent
/	.07	Present: Estimate impossible
?	0	Possibly Present

7. Colour Chart

The colour chart can be used in two ways. A lightness can be combined with a colour, or two colours can be combined.

eg. 3U – Dark Brown

or

RU – Reddish Brown

Lightness		Colour	
Symbol	Value	Symbol	Colour
9	palest	R	Red

8	*pale*
7	light
6	lighter
5	medium
4	darker
3	dark
2	very dark
1	darkest

U	brown (Umber)
O	Orange
T	Tan (khaki)
Y	Yellow
L	Lime (Y-G)
G	Green
Q	Aqua (B-P)
B	Blue
V	Violet (B-P)
P	Purple
M	Mauve (P-R)
W	White
A	Gray
N	Black (Noir)

APPENDIX II

Diamond Drillhole Geologic Logs

and

Assay Data

NOTE: All Drillholes were logged using MN Geocode

```
IDEN6B0201       X87CH310 NQ   APR87RBP   JTT APR87ACK          0.0
IPRJ            EQUITY SILVER MINES LTD         MAIN ZONE - MN GEOCODE
S000   00   427 MT  368.7 090.0 -65.0                   7560.24   8409.74   1309.69
S001  427  1079     368.7 090.5 -64.0
S002 1079  1689     368.7 090.7 -63.0
S003 1689  2438     368.7 091.2 -64.5
S004 2438  3033     368.7 091.6 -64.5
S005 3033  3383     368.7 091.9 -65.0
S006 3383  3597     368.7 092.0 -65.75
S007 3597  3687     368.7 092.1 -65.0
/SCL          MT.2MT.2
LSCL              MT.2        LCTM
/NAM                                                          QZSZTOPYCPTTASPRGY
LNAM                                                          DMCBCLMGHESLGLMO
/       00    31          OVBN                 P
R                 :TRICONED - NO CORE
R                 :CASING THRU BROKEN ROCK TO 3.1, NO TILL
/       31    69  30     2C11        <<        P BN    55       <)
L                 00         AT                                    <(
R                 :LOC 2E
/       69   102  31     2E23     QZ <<        P CU    50  Q*   <+  <?
L                 10         AT                                    <)<(
R                 :LOC 2C & 2D, POSSIBLE TT.
/      102   132  29     2D23        <<        PP          Q(   <=  <?
L                 03         TA                                    <*<*
R                 :LOC 2C, RARE 2E. 0.2 M OF MASSIVE PY ABOVE DYKE BELOW
/      132   160  27     8A00        <<CM      P CU    30<<     D.
L                 15         BA                  CL    60    D*
R                 :RARE FELD LATHS
/      160   194  31     2D23        <<VU      P         V+Q-   <+  <*
L                 03         TA                                    <.
R                 :LOC 2C23 LARGE QTZ VEINS VUGGY. GOOD GRADE SILVER
/      194   225  28     2E23        <<        P BN    40<(     <*  <.
L                 03         BA                                     <-
R                 :LOC 2C & 2D
/      225   258  31     2C11        <<        P BD    55<(Q.   <(
L                 03         AT                                     <.
R                 :LOC 2E
/      258   315  53     2E11CL      <<BR      P         <-     <(
L                 10         GA                              <)  <-
/      315   325  10     2E83        <<BR      P                <*<.<?
L                 03         ga                              <*  <+<?
/      325   437 104     2E11CL      <<BR      P BD    50<.     <*
L                 31         TG                              <)  <(
R                 :LOC 2C, MINOR BR.
/      437   457  15     2E81CY      BR<<      P                ++
L                 00         TG
R                 :FAULT ZONE
/      457   482  23     2E11CL      <<RC      P         <-     <)
L                 06         GA                              <)
/      482   508  26     8A00        <<CM      P CU    70<*     D.
L                 18         GA                  CL    30    D)  <-
/      508   645 133     2E11CL      <<RC      P         <(     <*
L                 48         TG                              D+  <-
R                 :FEW CLAY SEAMS
```

```
/    645   685  37   2C11CL     <<         P           <*    <)
L               10      TA                                     <(
/    685   760  67   2E11CL     <<RC       P           <(    <*
L               15      AG                                <+  <-
/    760   794  32   2E13       <<BR       P           <+    <(  <.
L               03      GA                                <+    <-
R               :SOME CLAY GOUGE
/    794   826  31   2E13       <<BR       P           <)    D*  <.
L               18      GA                                <)
R               :POSSIBLE SILICIFIED
/    826   840  14   8B00       <<CM       P CU    30<*    D.
L               10      2A                   CL    35
R               :ABUN FELD PHENOS
/    840   870  30   2E11       BR<<       P           <*    D)
L               18      GT                                <(
R               :INTENSELY BR'X
/    870   894  24   2E11       BR<<       P           <*    D*
L               10      GT                                <(
R               :AS ABOVE
/    894   943  45   2D11       <<         P           <(    D*
L               08      AT                                <*
R               :LOC 2E11 MINOR OCC OF SOFT LIME GREEN MINERAL IN OPEN SPACE
R               :FILLINGS - POSSIBLY SERICITE
/    943   987  40   2C11       <<         P F/    65<-    D*
L               06      TG                                <)  <.
R               :ABUN SHARDS AT TOP OF INTERVAL WITH SOME 2D
/    987  1017  29   2E11       <<         P           <(    <*
L               15      GT                              <.<-  <-
/   1017  1047  28   2E23       <<         P           <(Q.  <)
L               10      TG                              <-<*<.<(<-
/   1047  1068  20   2E11       <<BR       P           <-    <*
L               06      AT                                <(
/   1068  1097  27   2F14       <<BR       P           <-    D*Q-
L               05      TG                                   D.
R               :CP IN PATCH AT 107.8 WITH PY/MG
/   1097  1113  15   2C11       <<         P           <-    <(
L               08      6G                              <.Q1  <.
R               :ABUN CL SPOTS
/   1113  1143  29   2E12       <<         P           .-    <)<.
L               11      AT                              <.<-<-<(
R               :PY/HE/MG PATCH AT 113.9
/   1143  1173  29   2E14       <<         P           <-    <*<-<?
L               08      TG                                <*  <-
/   1173  1198  24   2E11       <<BR       P           <-    <*
L               10      GA                              <-Q)<.
R               :SOME SHARDS
/   1198  1228  25   2E11       <<BR       P           <-    D(D?
L               00      GA
R               :AS ABOVE
/   1228  1252  23   8A00       <<         P CU    50M-    D.
L               05      5G                                Q*
/   1252  1341  83   2E11       <<RC       P F/    35<(    D*
L               20      BA                                <)  D-
/   1341  1400  56   2C11       <<         P           <-    <*
L               15      TA                                <)  <.
```

```
/   1400  1430  29    2C12       <<          P           <(     Q)
L               17          GT                                  <+D-Q*
R               :GYPSUM IN <<'S
/   1430  1458  27    2C21       <<          P           <-     Q)
L               10          GT                                  <+D-Q(Q?
R               :AS ABOVE
/   1458  1525  62    2C11CL     <<          P BD    50<-      <*
L               23          TG                                  <=<.<.
R               :LOC 2D11, GY IN <<'S
/   1525  1608  78    2C11CL     <<          P           <-     <*
L               32          TG                                  <=<.<-
R               :AS ABOVE, GY IN <<'S
/   1608  1661  50    2C81CL     <<          P                  <*
L               20          TG                                  <=  <.
/   1661  1780 115    2C11CL     <<          P BD    55<(      <*
L               36          TG                                  <=<-<-
R               :GYPSUM IN <<'S
/   1780  1810  30    2C41       <<          P BD    50<.      <+<.
L               18          TA                                  <-D.
R               :START OF ALTERNATION ZONE (SILICA)
/   1810  1840  29    2C42       <<          P           <-Q.  D+
L               13          AT                                  <)D*
/   1840  1870  28    2C42       <<BR        P           <-    D)
L               06          TA                                  <)D*
R               :GYP IN <<'S, SOME BR'X WITH SILICIFICATION
/   1870  1900  30    2C42       <<          P           <-    D)
L               18          TG                                  <+D*
R               :SOME SERICITE ALT'N
/   1900  1930  30    2C42       <<          P                 D+
L               12          TG                                  <(D*
R               :SOME SER. ALT'N, GYP IN <<'S
/   1930  1960  30    2C82       <<          P                 D*
L               12          TG                                  <*D-
R               :SOME SILIC. GYP IN <<'S
/   1960  1990  30    2C82       <<          P BD    35        D+
L               18          TG                                  <)D(<.
R               :AS ABOVE
/   1990  2020  30    2E42       <<          P                 D+
L               19          GA                                  Q)D)D-
R               :LAPILLI INDISTINCT IN STRONG SILIFICATION
R               :GYP IN <<'S, SMALL (0.2 M) 8B, GYP <<'S CROSS-CUT BOTH 8B + 2E
/   2020  2050  30    2E52       <<          P BN    50        D=
L               19          GA                                  Q*D)<(
R               :LOC 2C52, GYP IN <<'S
/   2050  2080  30    2C52       <<BR                          D+
L               21          TG                                  <)D)
R               :SOME MG BANDINGS, GYP IN <<'S
/   2080  2110  29    2C22       <<WP        P             Q-  D)
L               06          AT                                  <+D*
/   2110  2133  23    2C42       BR<<        P                 D+
L               09          TA                                  <)D)Q(
R               :STRONGLY BX'D. GYP IN <<'S
/   2133  2321 184    8C00       P*<<        P BN    40<(      D-
L              110          YW                 CU    50       <*
                :BOTTEM CONTACT GRAD
```

```
/   2321  2339  18    2E52      <<BR       P               D=
L               12       GA                              <*D)<(
/   2339  2358  19    8A00      <<CM       P CU    60<*
L               10       4G                  CL    50      D+<.
/   2358  2370  12    2E42      <<BR       P               <(D#<*
L               03       GA
/   2370  2376  06    8A00      <<CM       P CU    65<-
L               03       6G                                   D*
R               :UPPER C/ SHEARED.
/   2376  2385  09    2E52      BR<<       P               D)
L               03       GA                              D)
/   2385  2409  24    8A00      <<CM       P CU    60<.
L               15       6G                  CU    60
R               :TRACE GYP IN <<'S
/   2409  2440  30    2C42      <<BR       P F/    60      D+<.
L               06       AT                              <*D-<*
R               :LOC 2E42, UPPER C/ FAULT BR 0.2 M.
/   2440  2470  29    2E42      <<BR       P BD    40      D+
L               09       AG                                D-<(
R               :LOC 2D42
/   2470  2500  30    2D42      <<         P               D)
L               18       GA                              <)D-
R               :LOC 2E42
/   2500  2530  30    2E42      <<         P               D)
L               15       AG                              <)D.<-
R               :LAPILLI INDISTINCT
/   2530  2560  30    2E42      <<         P BD    35      D+
L               09       AG                              <)D*<-
R               :LOC INTERLEVELED 2D42
/   2560  2590  30    2E42      <<BR       PP              D)
L               11       AG                           <.<*D-<.
R               :LOC INTERLEV 2D42
/   2590  2614  23    2E42      <<BR       P         <-    D+<.
L               09       AG                              <)D-
/   2614  2625  11    8A00      <<         P CU    50
L               06       7G                                  <-
/   2625  2650  25    2E42      <<BR       P BD    55      D+
L               10       AG                              <)D*
/   2650  2673  22    2E42      <<BR       P         <-    D*
L               03       GA                              <)D.<.
R               :LOC 2D42
/   2673  2701  28    8A00      <<CM       P BN    50<-
L               20       5G                  CL    335     D.
/   2701  2740  37    2E51      <<BR       P         <-    D)
L               03       GA                              <*
R               :LAPILLI INDISTINCT
/   2740  2770  29    2E53      <<BR       P         <-    D)<-
L               03       GA                              <*D(
R               :LOC 2C
/   2770  2800  30    2E43      <<BR       P            <-  D+<(D?
L               18       GA                              <*D.
/   2800  2825  25    2E53      <<         P            <(  D+<-D?
L               19       GA                              <)D.
/   2825  2850  25    2E53      <<BR       P               D+<-
L               11       GA                              <*
```

```
/  2850 2877 27   2E53      <<        P         Q.  D+D-Q?
L            09       GA                              Q.
             :BOTTOM C/ TRANSITIONAL OVER 0.4 M
/  2877 2900 23   8D41      <<MX      P             D*
L            03       3G                  CL   30   D(<-
R            :STRANGE - POSSIBLY FG ANDESITE FLOW, PRE-MINERAL DYKE?
R            :ABUN. GYP IN <<'S, ABUN SHARDS AND SOME VOLC FRAGS
/  2900 2916 16   2E53      <<BR      P         Q.  D+D.
L            03       GA                           <*D(
/  2916 2955 38   8D41      <<MX      P             D)
L            24       GA                            D-<-
R            :ABUN GYP, IN <<'S, C/ TRANSITIONAL SHARDS?
/  2955 2984 28   8D41      <<MX      P             D)
L            10       GA                           Q)D-<-
R            :AS ABOVE, FRAGMENTS OF RELICT LAPILLI? REPLACED BY CL
/  2984 3000 15   2E41      <<        P             D*
L            00       GA                           <)
R            :LAPILLI INDISTINCT
/  3000 3013 13   8D41      <<MX      P             D*
L            06       5G                              Q-
R            :OCC LAPILLI
/  3013 3023 09   2E41      <<BR      P             D*
L            00       GA                           <+
/  3023 3053 30   8D41      <<MX      P             D)
L            12       4G                            D-
R            :POSSIBLE DYKE? GYP IN <<'S, SHARDS    D*
/  3053 3081 28   8D41      <<MX      P             D*
             15       6G                           Q)
R            :AS ABOVE, CL REPLACING LAPILLI?
/  3081 3110 28   2E54      <<        P             D+Q(     <*
L            11       GA                           <*D*  Q(
R            :SOME ASSIMILATED 8D
/  3110 3148 37   8D41      <<MX        CU   50     D+
L            21       GA                  CL   25  Q)D.<-
R            :GYP IN <<'S
/  3148 3172 24   2E41      <<        P             D)
L            11       AG                           <*
R            :LAPILLI INDISTINCT
/  3172 3197 24   2E41      <<        P             D+D.
L            06       AG                           <)
R            :AS ABOVE
/  3197 3223 25   8D41      <<MX      P             D+
L            09       3A                            D.
R            :GYP IN <.'S
/  3223 3248 25   2E51      <<        P             D=D.     D.
L            06       GA                           <)D.
R            :LOC 8D, LAPILLI INDISTINCT
/  3248 3280 31   2E51      <<BR      P             D+  D?
L            09       GA                           <+
/  3280 3310 30   2E51      <<BR      P             D=<.     D.
L            11       GA                           <+D-
/  3310 3334 24   2E51      <<BR      P             D+<-     <-
L            06       GA                           <)D.
   3334 3363 28   8D44      <<MX      P         <-  D+D.     Q-
L            16       2A                           <*D-
```

```
R                 :SULPHIDE O'S INCLUSIONS?
/     3363  3393  30     8D41         <<MX          P            <-     D=
                  19          2A                                      <*D-
R                 :LAPILLI INCLUSIONS
/     3393  3455  62     8B00         <<CM          P CU     20<-     D-
L                 34          6G      P*              CL     40     <*D-
R                 :A REAL DYKE?
/     3455  3480  24     2E41         <<            P                 D+
L                 09          GA                                    <)D.
R                 :MINOR ASSIMILATED 8B
/     3480  3510  30     2E52         <<BR          P              O-  D=
L                 11          GA                                    <*D(<-
/     3510  3539  28     2E54         <<BR          P           <*     D)O-<?
L                 09          GA                                    <*
/     3539  3571  32     8D41         <<MX          P           <-     D=
L                 10          3A                                    <*D-
R                 :CONTAINS LAPILLI FRAG
/     3571  3589  17     2E42         <<            P           <-     D+
L                 03          GA                                    <)D(
R                 :GRADES INTO 8D, THEN SHARP INTO GABBRO
/     3589  3687  97     7C01                       P                  D(
L                 63          7A                                       D-
R                 :TYPICAL COARSE GRAINED, BIOTITE/FELDSPAR MONZONITE
R                 :END OF HOLE AT 368.7
A001
ALAB               EQUITY MINESITE LABORATORY
ATYP               ASSAY
ATH                WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
ACOMM              RCOVSAMPLE   RQD % CU   G/TAG G/TAU % SB   % AS   % FE   % ZN
R       00     31 :TRICONED - NO CORE
R       31     69 :VOLC. - NO CORE
A001    69    102        9381          0.01    24.0 0.54  0.02  0.005 3.96  0.13
A001   102    132        9382          0.02    11.0 0.43  0.05  0.005 9.00  0.05
R      132    160 :DYKE - NO SAMPLE
A001   160    194        9383          0.03    35.0 1.17  0.04  0.01  5.55  0.32
A001   194    225        9384          0.03    11.0 0.38  0.03  0.01  2.63  0.07
A001   225    258        9385          0.02     9.0 0.19  0.03  0.005 3.81  0.06
R      258    315 :VOLC - NO SAMPLE
A001   315    325        9386          0.03    31.0 0.31  0.03  0.01  3.06  0.05
R      325    760 :VOLC - NO SAMPLE
A001   760    794        9387          0.01     5.0 0.12  0.03  0.01  3.07  0.17
A001   794    826        9388          0.02    10.0 0.11  0.03  0.01  3.12  0.03
R      826    840 :DYKE - NO SAMPLE
A001   840    870        9389          0.005    2.0 0.06  0.03  0.005 2.49  0.01
A001   870    894        9390          0.005    1.0 0.07  0.02  0.005 2.71  0.005
R      894    987 :VOLC - NO SAMPLE
A001   987   1017        9391          0.01     3.0 0.04  0.02  0.005 3.03  0.05
A001  1017   1047        9392          0.02    12.0 0.10  0.02  0.005 3.36  0.10
A001  1047   1068        9393          0.02     4.0 0.08  0.04  0.01  4.32  0.02
A001  1068   1097        9394          0.42    62.0 0.15  0.09  0.05  7.73  0.09
R     1097   1113 :VOLC - NO SAMPLE
A001  1113   1143        9395          0.03     7.0 0.08  0.03  0.01  3.92  0.04
A001  1143   1173        9396          0.05    25.0 0.18  0.06  0.06  7.45  0.04
A001  1173   1198        9397          0.06    95.0 0.90  0.05  0.01  3.81  0.03
A001  1198   1228        9398          0.04    53.0 0.52  0.04  0.001 2.83  0.03
```

R	1228	1252	:DYKE - NO SAMPLE							
R	1252	1400	:VOLC - NO SAMPLE							
A001	1400	1430	9399	0.04	19.0	0.28	0.03	0.02	3.86	0.08
A001	1430	1458	9400	0.04	24.0	0.49	0.03	0.02	4.19	0.65
R	1458	1780	:VOLC - NO SAMPLE							
A001	1780	1810	9401	0.17	10.0	0.36	0.04	0.01	6.26	0.04
A001	1810	1840	9402	0.02	13.0	0.21	0.02	0.01	3.45	0.01
A001	1840	1870	9403	0.02	6.0	0.10	0.03	0.01	2.98	0.02
A001	1870	1900	9404	0.01	7.0	0.20	0.03	0.01	3.65	0.01
A001	1900	1930	9405	0.07	10.0	0.25	0.04	0.02	4.72	0.05
A001	1930	1960	9406	0.04	10.0	0.18	0.03	0.01	3.44	0.05
A001	1960	1990	9407	0.02	13.0	0.13	0.03	0.02	3.08	0.04
A001	1990	2020	9408	0.07	6.0	0.10	0.04	0.02	5.68	0.03
A001	2020	2050	9409	0.17	10.0	0.15	0.05	0.02	6.33	0.05
A001	2050	2080	9410	0.13	5.0	0.07	0.02	0.005	4.64	0.01
A001	2080	2110	9411	0.01	7.0	0.55	0.01	0.01	1.49	0.01
A001	2110	2133	9412	0.15	21.0	0.27	0.03	0.01	5.41	0.03
R	2133	2321	:DYKE - NO SAMPLE							
A001	2321	2339	9413	0.13	5.0	0.15	0.02	0.01	7.96	0.10
R	2339	2358	:DYKE - NO SAMPLE							
A001	2358	2370	9414	0.14	40.0	0.47	0.01	0.01	5.61	0.05
R	2370	2376	:DYKE - NO SAMPLE							
A001	2376	2385	9415	0.10	24.0	0.43	0.01	0.01	4.14	0.19
R	2385	2409	:DYKE - NO SAMPLE							
A001	2409	2440	9416	0.28	9.0	0.53	0.01	0.01	4.75	0.02
A001	2440	2470	9417	0.19	28.0	0.40	0.02	0.01	5.30	0.06
A001	2470	2500	9418	0.17	32.0	0.54	0.03	0.03	4.68	0.03
A001	2500	2530	9419	0.18	27.0	0.48	0.03	0.03	4.89	0.04
A001	2530	2560	9420	0.26	26.0	0.61	0.03	0.02	6.01	0.15
A001	2560	2590	9621	0.34	25.0	0.55	0.04	0.03	4.15	0.04
A001	2590	2614	9622	0.33	16.0	0.35	0.02	0.01	5.67	0.05
R	2614	2625	:DYKE - NO SAMPLE							
A001	2625	2650	9623	0.20	8.0	0.32	0.01	0.005	3.45	0.04
A001	2650	2673	9624	0.21	16.0	0.38	0.02	0.005	3.40	0.08
R	2673	2701	:DYKE - NO SAMPLE							
A001	2701	2740	9625	0.34	39.0	0.77	0.04	0.02	4.21	0.04
A001	2740	2770	9626	0.34	26.0	0.61	0.02	0.03	2.63	0.04
A001	2770	2800	9627	0.49	23.0	0.84	0.03	0.10	4.98	0.16
A001	2800	2825	9628	0.40	30.0	5.51	0.04	0.09	5.00	0.05
A001	2825	2850	9629	0.46	64.0	1.80	0.07	0.10	4.75	0.07
A001	2850	2877	9630	0.37	66.0	1.48	0.06	0.06	4.54	0.09
A001	2877	2900	9631	0.17	61.0	1.46	0.06	0.02	3.57	0.08
A001	2900	2916	9632	0.27	37.0	0.98	0.03	0.02	5.17	0.45
A001	2916	2955	9633	0.03	12.0	0.31	0.03	0.01	3.54	0.03
A001	2955	2984	9634	0.04	13.0	0.33	0.02	0.02	4.15	0.06
A001	2984	3000	9635	0.15	24.0	0.42	0.02	0.005	4.04	0.23
A001	3000	3013	9636	0.05	12.0	0.30	0.01	0.005	3.85	0.05
A001	3013	3023	9637	0.12	22.0	0.25	0.02	0.005	2.49	0.37
A001	3023	3053	9638	0.03	17.0	0.30	0.02	0.01	4.28	0.03
A001	3053	3081	9639	0.005	4.0	0.04	0.005	0.001	4.12	0.03
A001	3081	3110	9640	0.17	13.0	0.34	0.005	0.03	6.45	0.70
A001	3110	3148	9641	0.02	2.0	0.02	0.005	0.001	4.10	0.05
A001	3148	3172	9642	0.12	9.0	0.07	0.005	0.005	3.62	0.17
A001	3172	3197	9643	0.10	12.0	0.11	0.005	0.02	3.94	0.11
A001	3197	3223	9644	0.02	9.0	0.05	0.005	0.001	4.18	0.03

A001	3223	3248		9645	0.07	9.0	0.11	0.005	0.005	4.39	0.07
A001	3248	3280		9646	0.07	6.0	0.14	0.005	0.005	2.28	0.03
A001	3280	3310		9647	0.11	8.0	0.20	0.005	0.005	2.43	0.04
A001	3310	3334		9648	0.07	6.0	0.15	0.005	0.005	1.82	0.04
A001	3334	3363		9649	0.005	0.5	0.03	0.005	0.005	2.47	0.02
A001	3363	3393		9650	0.02	0.5	0.03	0.005	0.005	3.39	0.03
R	3393	3455	:DYKE - NO SAMPLE								
A001	3455	3480		9651	0.05	5.0	0.25	0.005	0.005	3.92	0.03
A001	3480	3510		9652	0.04	3.0	0.20	0.005	0.005	3.57	0.08
A001	3510	3539		9653	0.07	0.5	0.16	0.005	0.005	2.91	0.12
A001	3539	3571		9654	0.02	0.5	0.02	0.005	0.001	1.81	0.02
A001	3571	3589		9655	0.02	0.5	0.03	0.005	0.001	2.45	0.02
R	3589	3687	:GABBRO - NO SAMPLE								
R			:END OF HOLE AT 368.7 M								

```
IDEN6B0201       X87CH311 NO   MAY87DJH   JTT MAY87ACK         0.0
IPRJ          EQUITY SILVER MINES LTD          MAIN ZONE - MN GEOCODE
S000   00    320 MT  324.6 090.0 -65.0               7630.15   8438.55   1270.00
S001  320  1006      324.6 090.5 -64.5
S002  1006 1783      324.6 090.9 -65.0
S003  1783 2487      324.6 091.8 -65.0
S004  2487 2944      324.6 092.4 -64.5
S005  2944 3178      324.6 092.5 -65.5
S006  3178 3246      324.6 092.6 -65.0
/SCL          MT.2MT.2
LSCL              MT.2        LCTM
/NAM                                                        QZSZTOPYCPTTASPRGY
LNAM                                                        DMCBCLMGHESLGLMO
/       00    31        OVBN                   P
R                 :TRICONED - NO CORE , BROKEN ROCK - NO TILL
/       31    60  22     2D23SZMS    <<          P              O.   <+
L                 02          6A                                  <(   <?
R                 :MASSIVE PY REPLACEMENT @ 5.0 - 5.1 M (40 % PY): LOC 2E
/       60    90  28     2D23SZMS    <<          P           <(O.   <+
L                 05          6A                                  <-
R                 :INTO 2C 6.8 - 7.3 M
/       90   120  29     2D83MS      <<BR        P           <(     <+
L                 06          6A                                  <-   <?<(<?
R                 :POSS HS (V. FINE GRANINED):V. WEAK LOC BXIA: MASS PY
R                 :REPLACEMENT 10.7 - 10.8 M
/      120   150  29     2D23SZ      <<BR        P              O-   <+
L                 08          GA                                       <?
R                 :V. WEAK LOC BXIA
/      150   169  19     2D23SZ      <<          P           <(O.   <+
L                 06          GA                                       <?
/      169   178  085    2D85PYMS                P           M1     M3
L                 07          6A                                       D?M+
R                 :PALE BROWN SL; PYROCLASTIC FRAGS BECOMING PROGRESSIVELY
R                 :FINER DOWN HOLE - NO LAPILLI
/      178   193  15     2D13        <<BR        P                  <+
L                 03          GA                                  <-
R                 :V. WEAK LOCAL BXIA W/VUGGY MATRIX
/      193   213  20     2D13CL      <<          P BD   040        <(
L                 09          GA                                  <-
R                 :V. WEAK MS ALT'N ENVS. AROUND PY <<: WEAK CL ALT'N
/      213   247  30     8D13CL      <<P*        P FB   038        <(
L                 00          GA                                  <-D-
R                 :CNT ATTITUDES NOT OBSERVED DUE TO HEAVY BROKEN CORE: FB//
R                 :TO CNT?: PRE-MINERAL DYKE
/      247   270  23     2E13CL      <<          P                  <-
L                 04          GA                                  <.
R                 :INTO 2D TOWARDS E.O.I.: WEAK MS ALT'N ENV. ON <<: V. WEAK
R                 :CL ALT'N
/      270   300  30     2D13CL      <<          P                  <-
L                 09          GA                                  <.
R                 :V. WEAK CL ALT'N: WEAK PATCHY MS ALT'N: INTO 2E TOWARDS EOI
/      300   330  27     2E13CL      <<          P                  <-
L                 15          GA                                  <.  <.
R                 :WEAK CL ALT'N
/      330   360  30     2E13CL      <<BR        P                  <-
```

```
L               08        GA                                      <.   <.
R              :WEAK LOCAL BRECCIA (TECTONIC): INTO 2E87 LOC
/    360   391  31      2E23SZMS    <<BR          P          <-0.   <(
L               11        6T                                           <.
R              :INTO 2D TOWARDS EOI: WEAK LOCAL TECTONIC BRECCIA
/    391   397  06      MSDEPY                    P          M1     M9
L               06
R              :VEIN? OR LENS
/    397   420  22      2E23SZMS    <<BR          P          <(0.   <(
L               06        6T
R              :INTO WEAK BXIA LOCALLY
/    420   450  29      2D13CL      <<            P          <+     <-0.
L               16        GA                                   <(<(
R              :INTO 2E LOCALLY AND TOWARDS EOI: INTO 2D8 LOC
/    450   480  28      2E13CL      <<            P          <(     <-
L               15        GA                                    <-
R              :INTO 2E8 LOC. - SOME FRAGS ARE MAGNETIC
/    480   497  17      2E13CL      <<            P                 <-
L               13        GA                                      <(  <-
R              :MS ALT'N ENVS. AROUND <<
/    497   515  17      2E23SZMS    <<            P          <-0.   <(
L               08        TG
/    515   533  17      2E13CL      <<            P                 <-
L               12        GA                                      <-  <.
/    533   540  07      8A10CL      P*            P CU   030
L               07        AG                        CL   028
R              :FLOW BANDED DYKE - LOOKS LIKE A FOLD: V. SMALL ALT'D
R              :PLAG PHENOS - LOOKS MORE LIKE A PRE-MIN DYKE BUT NO
R              :MINERALIZATION
/    540   570  29      2E13CL      <<            P                 <-
L               12        GA                                   <.<(  <-
R              :INTO 2D8 LOCALLY
/    570   591  18      2E13CL      <<            P                 <-
L               03        GA                                      <(  <.
R              :INTO 2D8 @ 58.0 TO EOI
/    591   661  70      8A13CL      <<P*          P CU   024      <.
L               47        AG                                           <.
R              :LOWER CNT SHARP & IRREGULAR: WEAKLY PORPH
/    661   680  19      8C80MS      P*            P
L               04        8G                                           D.
R              :LOWER CNT SHARP & IRREGULAR
/    680   711  30      8A13CL      P*<<          P                 <.
L               14        AG                        CL   045  <.<.  <.
R              :WEAK P* TEXT: GOOD SHARP "INTRUSIVE", LOWER CNT
/    711   738  27      2E13CL      <<            P                 <-
L               03        GA                                   <.<-D.<-
R              :DISSEM, MG IN ANDESITIC LAPILLI: ANDESITIC & DACITIC LAPILLI
R              :IN A DACITIC? MATRIX: INTO 2D LOC: MS ALT'N IN DACITE FRAGS
R              :ONLY: NO ALT'N ASSOC W/<<
/    738   756  18      2D83MS      <<            P                 <(
L               02        TA                                      <(
R              :INTO 2C LOCALLY: LOCALLY STRONG << TEXT (ASSOC W/6T COLOR)
/    756   780  23      2D83MS      <<            P                 <(
L               02        TA                                   <-<(  <(
R              :MASSIVE PY + MG 77.3-77.4 M W/<< OF CB + HS: TO 2C LOC
```

```
/     780   810  29    2E13CL     <<          P                <(
L                03         5G                             <-<(  <-
R               :INTO 2E83 LOC IN AREAS OF MORE INTENSE <<
/     810   840  29    2E13CL     <<          P          <-    <(
L                06         5G                             <-<(D-<.
R               :DISSEM MG IN ANDESITIC LAPILLI: INTO 2E83 LOC IN AREAS OF MORE
R               :INTENSE <<: OCCAS VOLC BXIA FRAGS
/     840   870  30    2E13CL     <<          P          <.    <-
L                08         5G                             <.<-  <-
R               :INTO 2D LOCALLY
/     870   900  30    2E23SZCL   <<          P             O-  Q)
L                09         GA                                Q)  <-
/     900   930  29    2E23SZCL   <<          P             O.  Q(
L                00         GA                                Q(  <-
R               :INTO 2D LOCALLY
/     930   960  29    2E212CL    <<          P                 Q)
L                09         AG                                Q(Q-
R               :INTO 2E8 LOC
/     960   990  30    2D12CL     <<BR        P             <.  <(<-      <-
L                06         GA                                <-  <-
R               :MASS PY + MG 38.8-38.9 M: V. WEAKLY BRECCIATED LOCALLY
R               :INTO 2E LOCALLY
/     990  1020        2E23SZCL   <<BR        P             Q(  <)
L                           GA                                <(  <-
R               :V. WEAK LOCAL BXIA (TECTONIC)
/    1020  1050  30    2D13CL     <<BR        P                <(           <+
L                14         GA                                <(<.<-
R               :8A DYKE 104.0-104.1: WEAK LOCAL BR TEXT: INTO 2E LOC
/    1050  1080  30    2D13CL     <<BR        P          <-    <(<.
L                19         GA                                <(<.<.
R               :INTO 2E LOC: WEAK LOCAL BR TEXT                             <-
/    1080  1089  15    2D13CL     <<BR        P                <(<.
L                10         GA                                <(
R               :WEAK LOCAL BXIA TEXT (TECTONIC): INTO 2E LOC
/    1089  1099  10    8A10CL     <<P*        P CU   020    <(              <)
L                08         AG                  CL   035
R               :WEAK P* TEXT
/    1099  1130  27    2E12CL     <<          P                 Q)          <(
L                09         GA                                <(Q)
/    1130  1160  29    2E13CL     <<          P                <-
L                22         GA                                <-
R               :LOCAL WEAK SILICIFICATION OF MATRIX (MS + QZ?)
/    1160  1190  30    2E23SZCL   <<          P             O-  <(
L                17         GA                                <-Q-<-
R               :LOCAL WEAK SILICIFICATION OF MATRIX (MS + QZ?)
/    1190  1220  29    2E23SZCL   <<          P             O.  <(<.
L                19         GA                                <-  <.
R               :INTO 2D LOCALLY
/    1220  1250  29    2E43QZCL   <<          P                 Q+          <-
L                18         GA                                <-Q.<.
R               :INTO 2D LOCALLY
/    1250  1280  28    2D23SZCL   <<          P          <-O.  <(
L                23         GA                                <(      <-
R               :INTO 2E LOC: MOD. SILICIFICATION LOCALLY
/    1280  1310  29    2E13CL     <<          P                <(
```

```
L                 17        GA                                    <(
R                :INTO 2C LOC: LOCAL STRON SILICIFICATION (QZ ONLY) - DARK
R                :GREEN COLOR
/   1310  1340   28     2E23SZCL    <<         P             O.  <(
L                 15        GA                                 #(<(  <.
R                :STRONG LOCAL SILICIFICATION
/   1340  1352   12     2D23MS      <<         P             O.  <)D(
L                 10        TA                                    <(
/   1352  1386   33     2C83MS      <<BR       P                   <)         <-
L                 14        5T                                    <)
R                :8A 137.5-137.9 M: WEAK LOCAL BXIA TEXT (TECT.)
/   1386  1410   24     2D23SZCL    <<         P           <(O.    <)         <-
L                 09        GA                                    <)
R                :INTO 2E LOCALLY
/   1410  1440   30     2D13CL      <<         P           <.      <)         <-
L                 18        GA                                 <.<)
R                :GY STRINGERS X-CUT ALL OTHER STRINGERS & FRACTURE FILLINGS
R                :POSSIBLE 8D DYKE 143.3-144.5
/   1440  1470   30     2D13CL      <<         P                   <+         <-
L                 21        GA                                    <)<-
/   1470  1500   30     2D83MS      <<         P                   <)         <-
L                 07        TA                                    <(<-<.
/   1500  1530   30     2D83MS      <<         P                   <)         <-
L                 19        TA                                    <(<-
R                :LOCAL MOD. SILICIFICATION
/   1530  1560   29     2D83MS      <<         P                   <)<-
L                 05        6T                                    <-<-
/   1560  1590   30     2D82MS      <<<<       P                   <)
L                 21        5T      BR                            <-<(
R                :LOCAL WEAK BXIA TEXT
/   1590  1620   30     2D23CL      <<         P             O-  <(           <.
L                 22        GA                                    <-<-
/   1620  1642   21     2D13CL      <<<<       P                   <(
L                 13        GA                                    <-<)<(
R                :INTO 2D1 LOC: << S/MS ALT'N ENVS.
/   1642  1730   85     8C80MS      P*         P CU   060          D.
L                 72        GW
R                :UPPER CNT SHARP & REGULAR: LOWER CNT GRAD OVER 0.05 M
R                :TYPICAL LATITE
/   1730  1752   22     8A10CL      A*         P
L                 15        4G
R                :LOWER CNT GRAD OVER 0.1 M
/   1752  1821   65     8C80MS      P*FB       P FB   060          D-
L                 47        6A                   CL   060
R                :2 XENOLITHS OF 2DE
/   1821  1850   28     2E12CL      <<<<       P                   O+         <.
L                 21        GA                                    <(O(<-
R                :LOCAL SILICIFICATION
/   1850  1878   28     2E12CL      <<<<       P                   <)<.       <-
L                 24        GA                                    <(<(<(
/   1878  1900   22     8D00        P*<<       P CU   030<.        <.
L                 17        VA                                       <?
R                :DACITE COMP?: MINOR MS ALT'N ENVS. ON <<.: UPPER CNT SHARP &
R                :REGULAR: LOWER CNT WEAKLY GRAD
/   1900  1915   15     8D83MS      <<P*       P                   <(         <-
```

```
L              17        5T     BR
R             :ALTERED DACITE (AS ABOVE): MINOR LOCAL BXIA: LOWER CNT
R             :GRAD OVER 0.05 M
/   1915 1940  25    8D00       P*<<        P                <.      <-
L              17        VA                            <-   <.
R             :AS ABOVE 187.8 - 190.0: INTO 8D8 LOC: MS ALT'N ENVS. OF <<
/   1940 1970  30    8D00       P*<<        P                <.      <-
L              19        VA                            <-   <.
R             :AS ABOVE W/MS ALT'N ENVS. AND INTO 8D8
/   1970 1994  24    8D00       P*<<        P         <-    <.       <.
L              19        VA                  CL   020 <.<.  <.
R             :AS ABOVE LOWER CNT SHARP & REGULAR: ANDESITE 198.8-199.4
/   1994 2020  26    2D87MS     BR<<        P         #1    #+#.     <-
L              03        6T                                 #(
/   2020 2052  31    2D13CL     <<BR        P               <(       <)
L              17        GA                            <-<-
R             :INTO 2D87 LOC: BA - 204.7-205.2 M
/   2052 2064  12    2D87MS     BR<<        P         #1    #(
L              04        6T                            <-
R             :INTO 2D13 LOC
/   2064 2195 131    BA10CLCB   P*          P CU  030
L             111        AG                                 D.
R             :UPPER CNT IRREG (FAIRLY SHARP): LOWER CNT OBSCURRED IN BROKEN
R             :CORE
/   2195 2225  30    2C23MS     <<<<        P           0-  <+
L              05        5T                            <(<-
/   2225 2255  30    2C27MS     BR<<        P        #10-  #+
L              05        AT                            <-
R             :INTO 2D23 LOC
/   2255 2285  30    2C83MS     <<<<        P               <
L              11        AT                            <(
/   2285 2316  30    2C87MS     BR<<        P         #1    #+
L              19        AT                            <+
/   2316 2346  30    2C87MS     BR<<        P         #1    #+
L              12        TA                            <+
R             :LOCAL SILICIFICATION
/   2346 2377  29    2C83MS     <<BR        P               <)
L              17        TA                          <(<)
R             :WEAK LOCAL BRECCIA: PATCHY MS ALT'N
/   2377 2407  30    2C13CL     <*BR        P        <-0?  <)
L              03        GA                          <.<(
R             :WEAK TO MED LOCAL BXIA
/   2407 2438  30    2C13CL     <<<<        P               <)<?
L              08        GA     BR                     <(
R             :V. WEAK LOCAL BXIA
/   2438 2468  30    2C17CL     <<BR        P         #1    #+<?
L              21        GA                            <(#(
R             :LOCAL BXIA TEXT W/QZ+PY+MG MATRIX - V. F. GRAINED
/   2468 2499  30    2C27MS     BR<<        P        #10-  #+<-
L              14        TA                            <(#(
R             :LOCAL BXIA TEXT W/QZ+P+MG MATRIX - V. F. GRAINED
/   2499 2529  30    2C17CL     BR<<        P         #1    #+<(
L              19        GA                            <(
R             :MINOR MS ALT'N: V. F. GRAINED MATRIX IN BXIA
/   2529 2560  30    2C27CL     BR<<        P        #10-  #+<(
```

```
L                18         GA                                    <-<(#-
R               :LOCAL BXIA TEXT W/F. GRAINED QZ+PY+MG MATRIX
/   2560  2590   29     2C27MS      BR<<         P               #-0-  #)<(
L                11         GT                                    <-
R               :WEAKER << LAST 0.5 M OF INT.
/   2590  2620   30     2C13CL      <<<<         P                     <)
L                15         GA                                      <)<-
/   2620  2651   30     2C13CL      <<<<         P                     <(
L                17         GA                                      <)
R               :INTO 2D LOCALLY: WEAK LOC BXIA
/   2651  2682   31     2C13CL      <<<<         P                     <(
L                24         GA                                    <(<)
R               :INTO 2D LOCALLY: WEAK LOC BXIA
/   2682  2712   30     2C13CL      <<<<         P                     <(
L                21         GA      BR                            <-<)
R               :INTO 2D LOC: V. WEAK LOCAL BXIA
/   2712  2743   30     2D13CL      <<<<         P                     <(
L                05         GA      BR                              <)
R               :V. WEAK LOC BXIA W/PY+CL MATRIX
/   2743  2779   36     2D13CL      <<<<         P                     <(
L                19         GA                                      <)
/   2779  2810   31     8D11CL      <<           P                     D)        <-
L                27         AG                                         D-
R               :SHARP IRREG. UPPER CNT.
/   2810  2840   29     8D11CL      <<P*         P             <.      D)
L                12         AG                                    <.   D-<.
R               :TWO SMALL TUFF XENOLITHS: PLAG PHENOS TO 10 X 3 MM
/   2840  2870   30     8D11CL      <<           P                     <(
L                25         AG                                    <.<(D-
/   2870  2900   30     8D11CL      <<           P                     <.
L                27         AG                                    <.<.D-
R               :V. WEAK <<TEXT
/   2900  2930   30     8D11CL      <<           P                     <.
L                17         AG                                    <-<.D-
R               :V. WEAK << TEXT
/   2930  2953   23     8D11CL      <<           P                     <.
L                11         AG                                      <.D-
R               :TR. EP ALT'N: V. WEAK << TEXT
/   2953  2980   27     2D11CL      <<<<         P                     <.
L                16         GA                                      <+<)
/   2980  3010   30     2D11CL      <<<<         P                     <.
L                15         GA                                      <+<)
/   3010  3031   21     2D13CL      <<<<         P                     <(
L                22         GA                                      <+
R               :MS ALT'N ENVS. ON <<
/   3031  3053   21     8D13CL      P*<<         P                     <-
L                09         AG                                    <-<-
R               :POSSIBLE 8A: CNTS V. IRREGULAR - FAIRLY SHARP
/   3053  3078   25     2D13CL      <<<<         P                     <(
L                13         GA                                    <-<+
/   3078  3108   30     2D13CL      <<<<         P                     <(
L                22         GA                                    <.<)
R               :MS ALT'N ENVS. ON <<
/   3108  3139   30     2D23CL      <<<<         P                 0-  <(
L                19         GA                                    <-<)
```

/ 3139 3165 26 2D13CL <<<< P <(
L 14 GA <-<)
/ 3165 3180 15 7C01 P D(
L 12 5A D-
R :TRANSITION ZONE: UPPER CNT INDISTINCT
/ 3180 3246 66 7C00 GT P
L 44 5A D(
R :GOOD COARSE GRAINED MONZONITE
R :EOH @ 324.6 M
A001
ALAB EQUITY MINESITE LABORATORY
ATYP ASSAY
AMTH WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

AUMM			RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	31	:TRICONED - NO CORE								
A001	31	60	9701		0.07	52.0	0.50	0.04	0.001	6.69	0.02
A001	60	90	9702		0.04	29.0	0.91	0.02	0.001	5.43	0.06
A001	90	120	9703		0.08	47.0	1.42	0.05	0.001	9.28	0.49
A001	120	150	9704		0.03	42.0	0.81	0.02	0.001	6.72	0.02
A001	150	169	9705		0.04	38.0	0.70	0.04	0.001	10.81	0.32
A001	169	178	9706		0.74	79.0	1.25	0.27	0.06	24.60	4.30
A001	178	193	9707		0.04	16.0	0.33	0.02	0.001	4.86	0.05
A001	193	213	9708		0.02	3.0	0.06	0.005	0.001	1.66	0.02
A001	213	247	9709		0.03	22.0	0.97	0.02	0.001	3.66	0.06
A001	247	270	9710		0.04	0.5	0.05	0.005	0.002	3.30	0.03
A001	270	300	9711		0.005	0.5	0.01	0.005	0.001	2.99	0.005
A001	300	330	9717		0.005	0.5	0.02	0.005	0.001	4.00	0.005
A001	330	360	9713		0.02	4.0	0.13	0.03	0.005	6.89	0.05
A001	360	391	9714		0.04	14.0	0.14	0.03	0.001	8.51	0.37
A001	391	397	9715		0.005	9.0	0.45	0.07	0.001	41.30	0.005
A001	397	420	9716		0.05	9.0	0.17	0.03	0.001	6.79	0.05
A001	420	450	9717		0.03	0.5	0.05	0.02	0.001	3.95	0.02
A001	450	480	9718		0.005	0.5	0.05	0.02	0.001	3.66	0.02
A001	480	497	9719		0.02	0.5	0.12	0.005	0.001	2.11	0.02
A001	497	515	9720		0.02	0.5	0.03	0.02	0.001	5.96	0.005
A001	515	533	9721		0.02	0.5	0.04	0.02	0.001	3.06	0.02
R	533	540	:DYKE - NO SAMPLE								
A001	540	570	9722		0.005	0.5	0.04	0.005	0.001	2.48	0.005
A001	570	591	9723		0.005	0.5	0.05	0.005	0.001	1.76	0.005
R	591	711	:DYKE - NO SAMPLE								
A001	711	738	9724		0.005	0.5	0.04	0.005	0.001	1.92	0.03
A001	738	756	9725		0.005	0.5	0.07	0.005	0.001	2.41	0.03
A001	756	780	9726		0.02	2.0	0.14	0.03	0.001	6.43	0.03
A001	780	810	9727		0.005	0.5	0.14	0.005	0.001	2.13	0.005
A001	810	840	9728		0.06	2.0	0.09	0.02	0.001	2.47	0.02
A001	840	870	9729		0.02	2.0	0.48	0.005	0.001	2.55	0.005
A001	870	900	9730		0.005	3.0	0.05	0.02	0.001	2.93	0.02
A001	900	930	9731		0.005	2.0	0.07	0.02	0.001	2.68	0.02
A001	930	960	9732		0.005	2.0	0.54	0.02	0.001	3.92	0.02
A001	960	990	9733		0.07	11.0	0.08	0.04	0.09	8.54	0.04
A001	990	1020	9734		0.005	2.0	0.11	0.02	0.03	4.05	0.02
A001	1020	1050	9735		0.03	24.0	0.30	0.03	0.005	4.42	0.03
A001	1050	1080	9736		0.06	74.0	0.49	0.04	0.005	4.22	0.04
A001	1080	1089	9737		0.13	139.0	0.79	0.08	0.03	4.54	0.03
R	1089	1099	:DYKE - NO SAMPLE								

A001	1099	1130	9738	0.15	69.0	0.38	0.07	0.04	7.55	0.04
A001	1130	1160	9799	0.06	100.0	0.57	0.04	0.005	2.97	0.03
A001	1160	1190	9740	0.07	110.0	0.76	0.05	0.03	4.12	0.04
A001	1190	1220	9741	0.11	95.0	0.60	0.05	0.005	3.35	0.05
A001	1220	1250	9742	0.12	110.0	0.62	0.03	0.005	3.74	0.19
A001	1250	1280	9743	0.08	47.0	0.62	0.03	0.04	4.90	0.50
A001	1280	1310	9744	0.05	14.0	0.59	0.02	0.02	4.71	0.07
A001	1310	1340	9745	0.05	22.0	0.55	0.02	0.001	3.02	0.07
A001	1340	1352	9746	0.31	19.0	0.40	0.03	0.02	4.40	0.06
A001	1352	1386	9747	0.06	6.0	0.12	0.02	0.005	2.56	0.02
A001	1386	1410	9748	0.02	6.0	3.10	0.005	0.005	2.45	0.03
A001	1410	1440	9749	0.04	36.0	0.35	0.02	0.005	2.43	0.04
A001	1440	1470	9750	0.04	8.0	0.18	0.02	0.005	3.80	0.05
A001	1470	1500	9751	0.03	10.0	0.37	0.02	0.005	2.44	0.02
A001	1500	1530	9752	0.06	17.0	18.80	0.02	0.006	3.17	0.05
A001	1530	1560	9753	0.11	9.0	1.15	0.02	0.02	4.42	0.10
A001	1560	1590	9759	0.10	39.0	0.57	0.005	0.005	2.50	0.07
A001	1590	1620	9755	0.06	20.0	0.43	0.02	0.02	3.27	0.04
A001	1620	1642	9756	0.08	40.0	1.05	0.02	0.02	2.53	0.04
R	1642	1821	:DYKE - NO SAMPLES							
A001	1821	1850	9757	0.03	11.0	0.10	0.005	0.02	4.32	0.10
A001	1850	1878	9758	0.02	8.0	0.13	0.005	0.005	3.60	0.03
A001	1878	1900	9759	0.005	0.5	0.03	0.005	0.001	1.91	0.01
A001	1900	1915	9760	0.005	2.0	0.10	0.005	0.005	3.29	0.01
A001	1915	1940	9761	0.005	1.0	0.01	0.005	0.005	2.07	0.01
A001	1940	1970	9762	0.005	1.0	0.03	0.005	0.001	1.78	0.01
A001	1970	1994	9763	0.005	0.5	0.02	0.005	0.005	1.92	0.01
A001	1994	2020	9764	0.05	5.0	0.08	0.005	0.005	2.98	0.02
A001	2020	2052	9765	0.04	8.0	0.06	0.02	0.01	4.17	0.04
A001	2052	2064	9766	0.08	5.0	0.12	0.005	0.01	3.47	0.01
R	2064	2195	:DYKE - NO SAMPLES							
A001	2195	2225	9767	0.08	3.0	0.07	0.005	0.005	1.82	0.02
A001	2225	2255	9768	0.10	7.0	0.11	0.005	0.01	2.90	0.03
A001	2255	2285	9769	0.14	11.0	0.16	0.01	0.05	5.40	0.03
A001	2285	2316	9770	0.14	7.0	0.24	0.005	0.04	3.50	0.01
A001	2316	2346	9771	0.33	12.0	0.36	0.02	0.03	4.25	0.03
A001	2346	2377	9772	0.12	5.0	0.16	0.005	0.02	3.88	0.01
A001	2377	2407	9773	0.22	97.0	2.35	0.02	0.03	4.33	0.07
A001	2407	2438	9774	0.20	27.0	0.29	0.03	0.04	3.86	0.03
A001	2438	2468	9775	0.10	5.0	0.11	0.005	0.04	4.35	0.01
A001	2468	2499	9776	0.30	9.0	0.17	0.005	0.06	4.62	0.02
A001	2499	2529	9777	0.38	15.0	0.36	0.02	0.07	4.98	0.02
A001	2529	2560	9778	0.30	12.0	0.24	0.02	0.11	3.98	0.02
A001	2560	2590	9779	0.34	49.0	1.44	0.04	0.14	3.86	0.04
A001	2590	2620	9780	0.25	33.0	0.66	0.04	0.11	3.85	0.02
A001	2620	2651	9821	0.08	28.0	0.33	0.03	0.04	2.40	0.02
A001	2651	2682	9822	0.04	34.0	0.42	0.005	0.02	2.51	0.02
A001	2682	2712	9823	0.03	18.0	0.23	0.005	0.02	3.44	0.02
A001	2712	2743	9824	0.16	32.0	0.48	0.005	0.03	3.02	0.02
A001	2743	2779	9825	0.11	13.0	0.21	0.005	0.04	3.63	0.02
A001	2779	2810	9826	0.22	50.0	0.62	0.005	0.005	2.35	0.02
A001	2810	2840	9827	0.0005	7.0	0.07	0.005	0.005	2.92	0.005
A001	2840	2870	9828	0.02	4.0	0.07	0.005	0.02	4.19	0.03
A001	2870	2900	9829	0.02	3.0	0.03	0.005	0.02	3.91	0.02
A001	2900	2930	9830	0.005	3.0	0.18	0.005	0.005	3.63	0.02

A001	2930	2953	9831	0.005	0.5	0.10	0.005	0.005	3.90	0.02
A001	2953	2980	9832	0.005	0.5	0.02	0.005	0.005	4.60	0.005
A001	2980	3010	9833	0.005	0.5	0.02	0.005	0.005	4.37	0.005
A001	3010	3031	9834	0.005	3.0	0.03	0.005	0.005	4.83	0.005
A001	3031	3053	9835	0.005	3.0	0.03	0.005	0.005	4.35	0.02
A001	3053	3078	9836	0.005	2.0	0.47	0.005	0.005	4.23	0.02
A001	3078	3108	9837	0.005	5.0	0.06	0.005	0.005	3.96	0.03
A001	3108	3139	9838	0.02	2.0	0.03	0.005	0.005	2.72	0.03
A001	3139	3165	9839	0.04	7.0	0.07	0.005	0.005	3.30	0.02
A001	3165	3180	9840	0.06	4.0	0.33	0.005	0.005	4.51	0.02
R	3180	3246	:GABBRO - NO SAMPLES							

```
IDEN6B0201       X87CH312 NQ   MAY87RBP   JTT MAY87ACK              0.0
IPRJ            EQUITY SILVER MINES LTD          MAIN ZONE - MN GEOCODE
S000    00    216 MT   350.5 090.0 -70.5                7690.10   8448.30   1270.20
S001   216    625      350.5 090.9 -71.0
S002   625   1186      350.5 091.8 -71.0
S003  1186   1890      350.5 093.3 -70.5
S004  1890   2484      350.5 094.8 -70.5
S005  2484   3002      350.5 095.9 -70.0
S006  3002   3383      350.5 097.0 -69.5
S007  3383   3505      350.5 097.5 -69.5
/SCL           MT.2MT.2
LSCL               MT.2        LCTM
/NAM                                                            QZSZTOPYCPTTASPRGY
LNAM                                                            DMCBCLMGHESLGLMO
/       00     31          OVBN                   P
R                  :TRICONED - NO CORE : BROKEN ROCK TO 3.1, NO TILL
/       31     69  32     2E41        <<            P BD    50<-<-   D=
L                  03          AT
R                  :LOC 2C INTERLEVELED
/       69     94  26     2E41        <<BR          P          <-<-   <+
L                  06          7A
R                  :LOC 2C + 2F
/       94    111  16     2E41        BR            P          V5     V4
L                  03          YA
R                  :ESSENTIALLY ALL QTZ VEIN
/      111    145  32     2E41        <<BR          P          <-     D+  D?
L                  03          5A
R                  :FAULT GOUGE AT 12.6 M, LOC 2C41
/      145    177  31     2F41        <<BR          P          <-Q.   D+
L                  09          5A                                     D.Q(
/      177    206  28     2F41        <<BR          P          ~-Q-   Q+  <?
L                  09          TA                                     D(D*
/      206    221  14     2F41         BR           P            Q.   D(
L                  03          4A      BR
R                  :[illegible]
R                  :CONTACTS BROKEN
/      288    326  34     2E41        <<BR          P            Q-   D+  D?
L                  06          6A                                      D(
R                  :LOC 2D
/      326    357  30     2E41        <<BR          P                 D)  D?
L                  09          GA                                   #*D-D(
R                  :LOC 2D & 2F, F/ GOUGE AT 35.0 & 35.6
/      357    388  31     2F41        BR<<          P          #-Q.   D)
L                  09          GA                                <.#)  D-
R                  :LOC 2E41
/      388    425  35     2E41        <<BR          P          <-Q.   D)
L                  06          GA                                  D*  <(
R                  :SOME LAPILLI ALT'N TO SERICITE
/      425    456  15     8B00        P*            P                 D.
L                  03          AG                      CL      15   D+D.
/      456    484  28     2F11        BR<<          P BD    25<(      D*
L                  06          GA                                  <*
                   :LOC 2E11, 2C11
```

```
/    484   516  31     2E11        <<RC          P          <-     D)
L                06          GA                                  <)
R               :LOC 2E41
/    516   542  27     2E11        <<RC          P          <-     D)
L                04          AG                                  <)D.<(
R               :LOC 2E41, 2C11. SOME LAPILLI ALT'N TO SERICITE
/    542   571  29     2E11        <<RC          P          <-     D*
L                09          AG       AD                         <)  <(
R               :LOC 2C11, MINOR SILICIFICATION
/    571   604  33     2E12        <<BR          P F/     25<-     D)D.
L                09          AG                                  <(D-
R               :LOC 2D, 2C. F/AT 58.8
/    604   621  17     2E11        <<BR          P          <(     D+D.
L                03          TA                                  <(  D(D-
/    621   638         8B10        <<P*          P CU     20<*     D.
L                            AG                                  D+D.
R               :CL REPLACING FELD PHENOS
/    638   663  25     2F11        BR<<          P          <-     <)
L                06          TA                                    D.
/    663   697  30     2C41        <<            P          <*     <+
L                05          5A                                  <*  <-
R               :LOST CORE FROM 66.3 TO 66.7
/    697   719  22     2E41        <<            P          <-     <+
L                06          GA                                  <(  <*<-
R               :SOME LAPILLI ALT'N TO SERICITE
/    719   752  32     2F41        <<BR          P          <-     D)
L                03          GA                                  <*  <*<-
/    752   791  38     2E42        <<BR          P                 D)
L                09          TG                                    #*<*
/    791   821  28     2F42        BRBR          P          <-     <*
L                00          3A                  //                #(<-
R               :VERY BROKEN
/    821   851  29     2F42        BR            P          <*     D*
L                00          TA                                  #)#+#-
R               :LAPILLI ALT'D TO SERICITE
/    851   887  20     2E42        <<            P          <-     <*
L                00          5A                                  <)<(<-
R               :VERY BROKEN, FEW PIECES OF 8B
/    887   917  29     2F42        BR<<          P          <-     D*
L                03          GA                                  <)#2<-
R               :ESSENTIALLY MASSIVE MAGNETITE FROM 90.7 TO 90.9
/    917   948  31     2F42        BR<<          P                 <*            <(
L                12          AG                                  <(<+<(
/    948   978  30     2E42        <<BR          P BD     60       <*            <-
L                21          AG                                    <+<-
R               :LOC 2C42, MINOR BP'N
/    978  1008  30     2F42        BR<<          P             Q.  <)            <.
L                18          AG                                  <*<+<.
R               :SOME LAPILLI ALT'D TO SERICITE
/   1008  1035  27     2E42        BR<<          P             Q.  <)Q.Q?        <-
L                11          TG                                  <)<*
R               :LOC 2C42
/   1035  1037  02     8A00        CM            P CU     20<-
L                00          4G                    CL     35
/   1037  1067  30     2F42        BR<<          P             Q.  <+
```

```
                  12       GA                                        <+<(<-
1067  1098        31    2F42        BR<<          P
                  13       GA
                  :[illegible]

                  :AS ABOVE
1128  1158        30    2F54        BR<<          P
                  11       GA
                  :[illegible]

                  :MINOR BR'N
1188  1218        30    2F41        <<BR          P            <-0-  <+D.
                  09       GA                                    <)<-
1218  1248        30    2F41        <<BR          P            <-0.  <)<.     <(
                  13       GA                                    <*D-
1248  1278        30    2E41        <<BR          P            <-    <+       <(
                  15       GA                                    <)<.
                  :LAPILLI INDISTINCT
1278  1308        29    2F11        <<BR          P            <*    <)
                  09       AG                                    <+<.<(
1308  1337        27    2C42        <<BR          P            <-    0+       <-
                  06       AG                                    <+0*<-
                  :LOC 2F42
1337  1342        05    8A00        <<            P CU    80                 <*
                  03       6G                       CL    70     <*  <.
1342  1374        32    2F42        <<BR          P                           <*
                  16       GA                                    <)0*
                  :LOC 2E42
1374  1417        42    8B10        <<P*          P CU    35<-               <*
                  21       6G                       CL    30     D+D-
                  :FELDSPAR PHENOS ALT'D TO CL
1417  1439        21    2C11        BR<<          P                  <*       <-
                  03       GT                                    <+  <-
1439  1473        34    8A00        CM            P CU    20                 <*
                  19       6G                                      <(
1473  1503        30    2C42        <<            P            <-    0+       <-
                  09       GA                                    <)0*<-D-
                  :GRADES INTO 2D
1503  1540        36    2D42        <<            P            <-    <+D.
                  17       GA                                    <*<-<(<(
1540  1568        22    8A11        <<            P                  D(       <-
                  00       8G                                    <*
                  :VERY BROKEN, POOR RECOV.
1568  1603        33    8A11        <<CM          P CU    30          D-
                  14       TG                       CL    25     <+  <-
                  :BLEACHING ON <<'S
1603  1621        16    2D11        <<            P            <-    D*       <-
                  00       AG                                    <)  <(
1621  1635        13    8C01        <<CM          P                  D.
                  06       AW                       CL    60     <(
                  :UPPER C/ FAULTED
1635  1657        20    2D41        BR<<          P            <(    <*       <.
                  00       GA                                    <*  <-
```

```
R                  :ASSIMILATED 8C, BR'D
/   1657  1684  27    2D42        <<BR         P          <-    D+          <(
L               09        AG                                  <*D-
R               :MINOR BR'N
/   1684  1733  48    8A00        <<CM         P CU    55<-     D.          <-
L               32        5G                     CL    45     <(D.
R               :BOTH C/'S FAULTED
/   1733  1770  33    2D42        <<BR         P          <-Q.  D+          <-
L               09        GA                                  <*D-D(
/   1770  1803  33    2E52        <<BR         P             Q- D=          <-
L               11        AG                                  <(D*
/   1803  1895  90    8A00        <<           P CU    65       D.          <(
L               38        6G                                       <-
/   1895  1901  06    2F75        <<           P                D2D)     D=
L               03        4A                                    D1D+
R               :SUSPECT XENOLITH IN DYKE, ESSENTIALLY MASSIVE SULPHIDE
/   1901  1937  35    8A00        <<CM         P                            <*
L               06        6G                     CL    55
/   1937  1959  21    2E52        <<BR         P                Q+
L               09        4A                                  <-D(<-
/   1959  1993  33    2F52        <<BR         P             Q- D+  D?      <-
L               07        4A                                  <-D-
R               :LAST TWO INTERVALS SHOULD CARRY GOOD SILVER
/   1993  2021  28    2D51        <<BR         P                D)D.        <(
L               09        4A                                    D.
R               :GRADES INTO 2F51
/   2021  2045  24    2F52        <<BR         P             Q. D+          <(
                07        TA                                    D(  D.
R               :LOC 2F56
/   2045  2074  29    2E11        <<           P BD    60<-     D)          <(
L               11   GA                                       <*
R               :LOC 2D11
/   2074  2106  32    2E56        <<BR         P          <-    D+Q-        <(
L               12        GA                                  <*
R               :LOC 2D51, GRADES INTO 2F AT EOI
/   2106  2140  34    2D52        <<BR         P F/    35  Q.   D+          <-
L               20        GA                                  <(D-
R               :F/ GOUGE FROM 210.6 TO 210.9 LOC 2F52
/   2140  2164  24    8D42        <<           P BN    55       D+          <*
L               11        AG                                  <*D-<(
R               :SOME CL REPLACING PHENOS
/   2164  2186  22    2E52        <<BR         P          <-Q-  D+D.        <(
L               09        GA                                  <(D(<-
R               :MINOR ASSIMILATED 8B, LOC 2D52
/   2186  2257  72    8B00        <<CM         P CU    25<-     D.
L               49        4G                     CL    30     <-D.
/   2257  2272  15    2E51        <<           P          <-    D+
L               00        4A                                  <-D.
/   2272  2292  20    8A00        <<           P CU    40<-     D-          <(
L               06        5G                                  <*D.
R               :MINOR ASSIMILATED 2E?
/   2292  2322  30    2D52        <<           P          <-    D+D.        <-
L               06        4A                                  <(D(
                :LOC 2E52
/   2322  2353  31    2D53        <<           P          <*    <=<(     <*<.
```

```
L                 09       4A                                         <-<-
R                :LOC 2E53, SHOULD RUN GOOD SILVER
/    2353  2385  31     2D53       <<           P           <-    <+<.    <-
L                09        4A                                     <-<,  <-
R                :LOC 2C81 TOWARDS EOI
/    2385  2412  26     2C41       <<<<         P                 <)
L                00        TA                                     <)    <.
/    2412  2435  23     2D53       <<           P                 <+<*<?  <(<-
L                10        4A                                     <*    <-
R                :LOC 2E53, SHOULD BE GOOD GRADE
/    2435  2461  26     2E53       <<           P BN    40<(     <=Q*    <*
L                09        3A                                     <*<-<-D.
R                :LAPILLI INDISTINCT
/    2461  2484  23     2C51       <<<<         P           <(    D=
L                09        4A                                     <)
R                :MINOR 2D
/    2484  2491  06     8B00       <<           P           <-    D.
L                00        6G                                     <-D.
R                :CONTACTS NOT PRESERVED
/    2491  2511  20     2F53       <<           P           <-    <)
L                06        GA                                     <*    <(
/    2511  2533  22     2D53       <<BR         P             <+Q.  D+D-    D)
L                09        3A                                       D-  D-
/    2533  2557  24     2C51       <<           P             <(    <)<.
L                11        4A                                       <*
/    2557  2560  03     8B00       P*CM         P CU    40
L                03        3G                    CL     50        D-
/    2560  2567  06     2C51       <<           P             Q(  D)
L                00        3A
/    2567  2583  15     8B00       <<P*         P CU    30<-
L                00        6G       CM           CL     20       <)D-<-
/    2583  2613  29     2C51       <<BR         P                 <+,.      <-
L                03        3A                                     <*D.<.<-
R                :MINOR BR'N
/    2613  2630  10     8B10       P*           P                 D.
L                00        2G                                     D)D.
R                :VERY BROKEN, POOR RECOV. CL REPLACING FELDSPAR PHENOS
/    2630  2660  29     2C56       <<           P                 D+D-    D.
L                06        3A                                     D.  D.
/    2660  2694  32     2C53       <<           P           <-    D+D.    D.
L                16        3A                                     <*<-  D(
R                :LOC 2D53
/    2694  2728  33     2E53       <<BR         P           <(    D+<(    D*
L                12        3A                                     <*D.  <)
R                :8A FROM 271.2
/    2728  2761  32     2C51       <<                       <*    <+D.<.
L                18        4A      <<           P                 <*
R                :LOC 2E51
/    2761  2791  30     8A00       <<           P CU    10        D.
L                11        6G                    CL     10       <-D.
/    2791  2835  42     2C41       <<           P                 <)
L                18        4A                                     <)
R                :LOC 2E
/    2835  2865  29     2C41       <<           P           <-    <)
L                09        3A                                     <+<*
```

```
L                   09         4A                                                   <-<-
R                  :LOC 2E53, SHOULD RUN GOOD SILVER
/     2353   2385   31      2D53         <<             P            <-     <+<.     <-
L                   09         4A                                                   <-<.   <-
R                  :LOC 2C81 TOWARDS EOI
/     2385   2412   26      2C41         <<<<           P                   <)
L                   00         TA                                                   <)      <.
/     2412   2435   23      2D53         <<             P                   <+<*<?    <((<-
L                   10         4A                                                   <*      <-
R                  :LOC 2E53, SHOULD BE GOOD GRADE
/     2435   2461   26      2E53         <<             P BN     40<(    <=Q*      <*
L                   09         3A                                                   <*<-<-D.
R                  :LAPILLI INDISTINCT
/     2461   2484   23      2C51         <<<<           P            <(     D=
L                   09         4A                                                   <)
R                  :MINOR 2D
/     2484   2491   06      8B00                        P                   D.
L                   00         6G                                                   D.
L                  [illegible]
L                   05         6H
/     2511   2533   22      2D53         <<BR           P              <+Q.   D+D-      D)
L                   09         3A                                        D-   D-
/     2533   2557   24      2C51         <<             P              <(     <)<.
L                   11         4A                                           <*
/     2557   2560   03      8B00         P*CM           P CU     40
L                   03         3G                         CL     50         D-
/     2560   2567   06      2C51         <<             P             Q(   D)
L                   00         3A
/     2567   2583   15      8B00         <<P*           P CU     30<-
L                   00         6G           CM            CL     20     <)D-<-
/     2583   2613   29      2C51         <<BR           P                   <+,.          <-
L                   03         3A                                          <*D.<.<-
R                  :MINOR BR'N
/     2613   2630   10      8B10         P*             P                   D.
L                   00         2G                                          D)D.
R                  :VERY BROKEN, POOR RECOV. CL REPLACING FELDSPAR PHENOS
/     2630   2660   29      2C56         <<             P                   D+D-     D.
L                   06         3A                                           D.   D.
/     2660   2694   32      2C53         <<             P            <-     D+D.     D.
L                   16         3A                                          <*<-   D(
R                  :LOC 2D53
/     2694   2728   33      2E53         <<BR           P            <(     D+<(     D*
L                   12         3A                                          <*D.   <)
R                  :8A FROM 271.2
/     2728   2761   32      2C51         <<                           <*     <+D.<.
L                   18         4A        <<             P                  <*
R                  :LOC 2E51
/     2761   2791   30      8A00         <<             P CU     10         D.
L                   11         6G                         CL     10     <-D.
/     2791   2835   42      2C41         <<             P                   <)
L                   18         4A                                          <)
R                  :LOC 2E
/     2835   2865   29      2C41         <<             P            <-     <)
L                   09         3A                                          <+<*
```

```
R                     :STARTING HEAVY CL-MG <<'ING
/   2865  2895  30    2C41       <<          P                    <*
L               06         GA                                     [illegible]
R               :[illegible]
/   [illegible]
R               :[illegible]
/   2925  2955  30    2C41       <<<<        P          <-     <)
L               11         3A                                  <)<+
R               :AS ABOVE
/   2955  2985  30    2C41       <<<<        P          <*     <)<.      <-
L               11         3A                                  <)<+
R               :GRADES INTO 2D41
/   2985  3016  30    2D43       <<          P          <-     <+<.
L               15         GA                                  <)<*  <-
R               :GRADES INTO 2C41
/   3016  3046  30    2C56       <<          P          <*     D+<-      D*
L               12         3A                                  <(D.  <*
/   3046  3076  30    2E46       <<          P                 D+Q-      D*
L               15         3A                                  <(D*  <-
R               :GRADES INTO 2E41
/   3076  3106  30    2E53       <<          P          <-     D+<-      D(
L               16         3A                                  <(<-  <-
/   3106  3131  25    2D51       <<BR        P          <(     Q+D.      D-
L               11         4A                                  <)#1
R               :VERY BR'D
/   3131  3154  22    2D41       <<          P                 <)        <.
L               18         GA                                  <+D.
/   3154  3189  35    7C11       <<P*        P          <-     D*D.
L               21         GA                                  <(D.<-
R               :ASSIMILATION OF TUFF AND GABBRO
/   3189  3220  30    2E11       <<          P          <-     D)
L               19         AG                                  <)D.
R               :MINOR 7C11
/   3220  3245  25    2E11       <<          P          <-     D)
L               09         AG                                  <+D.
R               :AS ABOVE
/   3245  3277  31    2E41       <<          P          <(     <*
L               13         AG                                  <+
/   3277  3403 125    8A00       <<CM        P CU   060<-      D.
L               81         7G                  CL   040        D.<-
R               :MINOR XENOLITHS OF 2E11 AT 335.2 AND 339.8 M.
/   3403  3411  08    7C00       P*          P          <-
L               06         AG                                  D-
/   3411  3453  42    2E41       <<          P          <-     D*
L               28         AG                                  D-
R               :ASSIMILATION OF TUFF AND GABBRO - CONTACT HORNFELS
/   3453  3505  52    7C00       P*          P          <-
L               33         AG                                  D-
R               :TYPICAL MEDIUM GRAINED MONZONITE.
R               :END OF HOLE @ 350.5 M.
A001
ALAB            EQUITY MINESITE LABORATORY
ATYP            ASSAY
AMTH            WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
```

AUMM			RCOVSAMPLE	ROD % CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	31	:TRICONED - NO CORE, BROKEN ROCK - NO RECOVERY							
A001	31	69	9656	0.005	4.0	0.13	0.005	0.005	2.88	0.03
A001	69	94	9657	0.001	2.0	0.06	0.005	0.005	4.42	0.005
A001	94	111	9658	0.001	6.0	0.15	0.02	0.005	29.70	0.005
A001	111	145	9659	0.001	28.0	0.29	0.005	0.005	2.71	0.07
A001	145	177	9660	0.02	35.0	0.34	0.005	0.005	3.81	0.03
A001	177	206	9661	0.03	91.0	0.49	0.02	0.005	7.82	0.02
A001	206	221	9662	0.001	3.0	0.25	0.005	0.005	3.69	0.005
R	221	288	:DYKE - NO SAMPLES							
A001	288	326	9663	0.20	111.0	0.84	0.07	0.005	3.54	0.07
A001	326	357	9664	0.04	54.0	1.46	0.02	0.03	5.34	0.12
A001	357	388	9665	0.04	18.0	0.21	0.005	0.005	3.37	0.07
A001	388	425	9666	0.02	32.0	0.39	0.005	0.005	3.53	0.04
R	425	456	:DYKE - NO SAMPLES							
A001	456	484	9667	0.005	0.5	0.04	0.005	0.001	2.86	0.02
A001	484	516	9668	0.005	0.5	0.16	0.005	0.001	2.59	0.02
A001	516	542	9669	0.005	0.5	0.63	0.005	0.001	2.27	0.02
A001	542	571	9670	0.005	0.5	0.07	0.005	0.001	2.18	0.005
A001	571	604	9671	0.005	0.5	0.04	0.005	0.001	2.83	0.02
A001	604	621	9672	0.04	7.0	0.18	0.02	0.005	5.11	0.2
R	621	638	:DYKE - NO SAMPLES							
A001	638	663	9673	0.005	0.5	0.38	0.005	0.005	2.46	0.09
A001	663	697	9674	0.005	5.0	0.19	0.02	0.001	2.26	0.05
A001	697	719	9675	0.005	2.0	0.10	0.005	0.001	2.47	0.20
A001	719	752	9676	0.005	0.5	0.13	0.02	0.001	2.49	0.07
A001	752	791	9677	0.005	0.5	0.71	0.005	0.001	2.91	0.03
A001	791	821	9678	0.005	0.5	0.32	0.005	0.001	3.09	0.03
A001	821	851	9679	0.005	0.5	0.04	0.005	0.001	2.33	0.04
A001	851	887	9680	0.005	3.0	0.76	0.005	0.001	2.15	0.06
A001	887	917	9681	0.005	2.0	0.07	0.02	0.001	4.25	0.04
A001	917	948	9682	0.005	4.0	0.10	0.02	0.02	5.01	0.05
A001	948	978	9683	0.08	40.0	0.87	0.02	0.001	2.76	0.06
A001	978	1008	9684	0.03	8.0	0.12	0.02	0.001	3.14	0.07
A001	1008	1035	9685	0.03	16.0	0.12	0.02	0.001	2.72	0.05
R	1035	1037	:DYKE - NO SAMPLES							
A001	1037	1067	9686	0.005	5.0	0.30	0.02	0.005	3.45	0.04
A001	1067	1098	9687	0.10	35.0	0.27	0.02	0.02	5.82	0.09
A001	1098	1128	9688	0.14	46.0	0.35	0.03	0.005	4.08	0.07
A001	1128	1158	9689	0.07	32.0	0.53	0.03	0.03	4.87	0.09
A001	1158	1188	9690	0.09	29.0	0.17	0.03	0.03	4.94	0.09
A001	1188	1218	9691	0.13	39.0	0.27	0.02	0.09	5.42	0.04
A001	1218	1248	9692	0.08	44.0	0.24	0.02	0.005	3.45	0.37
A001	1248	1278	9693	0.12	31.0	0.32	0.02	0.005	3.85	0.05
A001	1278	1308	9694	0.02	17.0	0.24	0.005	0.005	2.94	0.08
A001	1308	1337	9695	0.14	84.0	1.37	0.005	0.005	4.83	0.18
R	1337	1342	:DYKE - NO SAMPLES							
A001	1342	1374	9696	0.15	46.0	0.26	0.005	0.005	3.66	0.03
R	1374	1417	:DYKE - NO SAMPLES							
A001	1417	1439	9697	0.005	4.0	0.14	0.005	0.005	1.79	0.005
R	1439	1473	:DYKE - NO SAMPLES							
A001	1473	1503	9698	0.14	48.0	1.30	0.005	0.005	2.57	0.19
A001	1503	1540	9699	0.58	80.0	0.30	0.03	0.05	5.79	1.02
R	1540	1603	:DYKE - NO SAMPLES							
A001	1603	1621	9700	0.03	10.0	0.49	0.001	0.005	2.40	0.03

R	1621	1635 :DYKE - NO SAMPLES								
A001	1635	1657	9781	0.02	9.0	0.20	0.005	0.005	2.54	0.03
A001	1657	1684	9782	0.02	8.0	0.12	0.005	0.005	3.10	0.03
R	1684	1733 :DYKE - NO SAMPLES								
A001	1733	1770	9783	0.001	3.0	0.40	0.005	0.02	4.57	0.06
A001	1770	1803	9784	0.005	4.0	0.14	0.005	0.03	4.46	0.05
R	1803	1895 :DYKE - NO SAMPLES								
A001	1895	1901	9785	0.03	5.0	0.60	0.02	0.23	25.40	0.04
R	1901	1937 :DYKE - NO SAMPLES								
A001	1937	1959	9786	0.005	9.0	0.78	0.005	0.02	5.64	0.04
A001	1959	1993	9787	0.005	5.0	0.16	0.005	0.005	2.78	0.04
A001	1993	2021	9788	0.005	6.0	0.52	0.005	0.005	3.16	0.02
A001	2021	2045	9789	0.03	13.0	0.45	0.005	0.005	3.93	0.02
A001	2045	2074	9790	0.02	4.0	0.06	0.005	0.005	3.23	0.06
A001	2074	2106	9791	0.39	9.0	0.38	0.02	0.02	4.98	0.11
A001	2106	2140	9792	0.13	8.0	0.26	0.02	0.05	4.17	0.04
A001	2140	2164	9793	0.03	3.0	0.02	0.02	0.001	2.90	0.02
A001	2164	2186	9794	0.13	10.0	0.23	0.02	0.005	4.35	0.03
R	2186	2257 :DYKE - NO SAMPLES								
A001	2257	2272	9795	0.29	87.0	3.86	0.05	0.07	4.94	0.02
R	2272	2292 :DYKE - NO SAMPLES								
A001	2292	2322	9796	0.08	5.0	0.95	0.03	0.001	2.87	0.04
A001	2322	2353	9797	0.26	9.0	0.31	0.04	0.03	4.25	0.02
A001	2353	2385	9798	0.16	9.0	0.17	0.03	0.005	3.05	0.04
A001	2385	2412	9799	0.12	26.0	0.48	0.02	0.005	2.11	0.05
A001	2412	2435	9800	0.26	38.0	0.21	0.03	0.03	4.12	0.11
A001	2435	2461	9801	0.34	26.0	1.34	0.03	0.04	4.78	0.04
A001	2461	2484	9802	0.27	30.0	4.55	0.05	0.02	4.08	0.05
R	2484	2491 :DYKE - NO SAMPLES								
A001	2491	2511	9803	0.08	8.0	0.36	0.02	0.005	2.14	0.09
A001	2511	2533	9804	0.29	8.0	0.67	0.03	0.07	6.39	0.12
A001	2533	2557	9805	0.09	2.0	0.07	0.005	0.04	2.86	0.02
R	2557	2560 :DYKE - NO SAMPLES								
A001	2560	2567	9806	0.37	25.0	0.89	0.03	0.05	3.37	0.07
R	2567	2583 :DYKE - NO SAMPLES								
A001	2583	2613	9807	0.26	6.0	0.21	0.02	0.03	3.31	0.05
R	2613	2630 :DYKE - NO SAMPLES								
A001	2630	2660	9808	0.25	3.0	0.10	0.02	0.005	3.60	0.03
A001	2660	2694	9809	0.17	5.0	0.07	0.005	0.03	4.04	0.06
A001	2694	2728	9810	0.08	11.0	0.07	0.03	0.02	4.42	0.75
A001	2728	2761	9811	0.06	10.0	0.05	0.02	0.05	4.07	0.04
R	2761	2791 :DYKE - NO SAMPLES								
A001	2791	2835	9812	0.03	9.0	0.03	0.02	.03	4.11	0.02
A001	2835	2865	9813	0.005	0.5	0.11	0.005	0.001	4.82	0.005
A001	2865	2895	9814	0.005	0.5	0.28	0.02	0.001	3.92	0.005
A001	2895	2925	9815	0.005	0.5	0.02	0.005	0.001	2.83	0.001
A001	2925	2955	9816	0.005	0.5	0.01	0.005	0.001	3.06	0.001
A001	2955	2985	9817	0.02	2.0	0.04	0.005	0.02	3.68	0.03
A001	2985	3016	9818	0.005	0.5	0.02	0.005	0.005	3.07	0.005
A001	3016	3046	9819	0.10	13.0	0.10	0.005	0.005	3.40	0.55
A001	3046	3076	9820	0.11	18.0	0.07	0.005	0.02	4.00	0.25
A001	3076	3106	9901	0.06	11.0	0.16	0.005	0.001	3.81	0.04
A001	3106	3131	9902	0.03	9.0	0.03	0.005	0.001	4.47	0.02
A001	3131	3154	9903	0.01	7.0	0.09	0.005	0.001	4.51	0.01
A001	3154	3189	9904	0.04	11.0	0.11	0.005	0.001	2.56	0.02

A001	3189	3220	9905	0.05	15.0	0.05	0.005	0.001	3.87	0.04
A001	3220	3245	9906	0.06	8.0	0.06	0.005	0.001	3.44	0.04
A001	3245	3277	9907	0.02	5.0	0.03	0.005	0.001	4.16	0.03
R	3277	3403	:DYKE - NO SAMPLES							
R	3403	3411	:GABBRO - NO SAMPLES							
A001	3411	3453	9908	0.06	101.0	1.00	0.005	0.001	4.161	0.03
R	3453	3505	:GABBRO - NO SAMPLES							
R			:END OF HOLE @ 350.5							

```
IDEN6B0201      X87CH313 NQ   MAY87RBP   JTT MAY87ACK          0.0
IPRJ           EQUITY SILVER MINES LTD         MAIN ZONE - MN GEOCODE
S000   00     157 MT    52.7 090.0 -60.5                    7879.80   8386.70   1270.80
S001   157    527       52.7 090.0 -60.0
/SCL          MT.2MT.2
LSCL              MT.2        LCTM
/NAM                                                        QZSZTOPYCPTTASPRGY
LNAM                                                        DMCBCLMGHESLGLMO
/        00    30          OVBN             P
R                 :TRICONED - NO CORE, CASING THRU BROKEN ROCK
/        30    61          OVBN             P
R                 :CORED BOULDERS
/        61    91   25     2F43      BR<<   P              <)    #2#-
L                   00          GA                              <*     #+
/        91   127   31     2F43      BR<<   P              <)  D*<+
L                   06          GA                              <)     D-
R                 :POSSIBLE MYLONITE?
/       127   152   15     8C00      P*     P              <-    D.
L                   00          AW                              <-
R                 :NO CONTACTS PRESERVED
/       152   182   25     2F41      BR<<   P              #)    <+<.
L                   00          GA                              <*
/       182   212   25     2F41      BR<<   P              <-    D*
L                   00          4A                              <-
R                 :VERY BROKEN, CLAY GOUGE AT 18.9
/       212   242   27     2F41      BR<<   P              <*    D*
L                   00          6A
/       242   272   26     2F41      BR<<   P              <-  D?D*
L                   00          GA                              <(
R                 :TINY BLACK RECTANGLUAR PHENOS TO TO?
/       272   302   27     2F11      BR<<   P              <(    D*
L                   00          6A                              <*
/       302   338   31     2F41      BR<<   P              <-    D*
L                   00          5A                              <(
R                 :CLAY GOUGE AT 30.5 M
R                 :DRILLERS ADVANCED CASING TO 30.5 M
/       338   368   25     2F11      BR<<   P              <-    D*
L                   00          5A                              <(
R                 :LOC 2F41
/       368   396   25     2F11      BR<<   P              <(    D)
L                   00          4A                              <(
R                 :LOC 2F81
/       396   426   27     2F11      BR<<   P              <(    D)
L                   00          4A                              <(
R                 :LOC 2F81, CLAY GOUGE AT 41.1 M
/       426   457   20     2F11      BR<<   P              <-    D*
L                   00          6A                              <-
R                 :CLAY GOUGE AT 46.8 M
/       457   487   22     2F11      BR<<   P              <(    D*
L                   00          6A                                 <(
/       487   527   31     2F11      BR<<   P              <-    D*
L                   00          6A                              <(
R                 :LOC 2F41
R                 :DRILLERS ADVANCED CASING TO 45.7 M, BUT THE HOLE CONTINUED TO
R                 :SQUEEZE THE RODS. THEREFORE, HOLE ABANDONED AT 52.7 M
```

R			:END OF HOLE AT 52.7 M							
A001										
ALAB			EQUITY MINESITE LABORATORY							
ATYP			ASSAY							
AMTH			WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST							
AUMM			RCOVSAMPLE RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	30	:TRICONED - NO CORE, CASING THRU BROKEN ROCK							
R	30	61	:CORED BOULDERS, EXTREMELY POOR RECOVERY - NO SAMPLE							
A001	61	91	9909	0.08	75.0	0.40	0.005	0.001	4.55	21.00
A001	91	127	9910	0.005	15.0	0.15	0.005	0.001	4.54	0.15
R	127	152	:DYKE - NO SAMPLE							
A001	152	182	9911	0.05	208.0	0.10	0.03	0.001	5.21	0.06
A001	182	212	9912	0.005	5.0	0.02	0.005	0.001	1.75	0.05
A001	212	242	9913	0.005	3.0	0.32	0.005	0.001	1.44	0.04
A001	242	272	9914	0.005	2.0	0.15	0.005	0.001	1.63	0.06
A001	272	302	9915	0.005	0.5	0.03	0.005	0.001	2.29	0.04
A001	302	338	9916	0.005	2.0	0.04	0.005	0.001	1.34	0.05
A001	338	368	9917	0.005	2.0	0.04	0.005	0.001	1.68	0.03
A001	368	396	9918	0.005	3.0	0.10	0.005	0.001	1.64	0.02
A001	396	426	9919	0.005	0.5	0.05	0.005	0.001	1.93	0.03
A001	426	457	9920	0.005	2.0	0.02	0.005	0.001	1.73	0.40
A001	457	487	9921	0.005	3.0	0.05	0.005	0.001	1.70	0.02
A001	487	527	9922	0.005	2.0	0.05	0.005	0.001	1.65	0.05
R			:END OF HOLE @ 52.7 M							

```
IDEN6B0201       X87CH314 NQ   MAY87RDP    JTT MAY87ACK            0.0
IPRJ          EQUITY SILVER MINES LTD          MAIN ZONE - MN GEOCODE
S000   00    229 MT   320.0 090.0 -71.0                     7930.70   8434.00   1260.00
S001  229    625      320.0 090.0 -71.0
S002  625   1140      320.0 090.0 -71.0
S003 1140   1841      320.0 090.0 -72.5
S004 1841   2437      320.0 090.0 -71.0
S005 2437   2848      320.0 090.0 -72.0
S006 2848   3200      320.0 090.0 -71.0
/SCL         MT.2MT.2
LSCL              MT.2        LCTM
/NAM                                                           QZSZTOPYCPTTASPRGY
LNAM                                                           DMCBCLMGHESLGLMO
/       00     91         OVBN                     P
R                 :TRICONED - NO CORE, BROKEN ROCK - NO TILL
/       91    140  40     8B80        P*           P          <-
L                  00          5A
R                 :ALL FELDSPAR PHENOS ALT'D TO SERICITE
/      140    143  02     2F11        <<BR         P          <-     D*
L                  00          GA
/      143    183  00     NREC                     P
/      183    234  25     2F11        BR<<         P          <(     D(
R                 :CLAY GOUGE AT 20.5 M
/      234    260  20     2G01        <<           P                 D(
L                  00          TA
R                 :CLAY GOUGE AT 23.8 M
/      260    300  30     2H01        <<           P          <-     D*
L                  00          6A
/      300    354  32     2F01        <<BR         P          <-     D)
L                  00          4A
/      354    384  30     2H01        <<           P          <*     D*          <*
L                  06          GA                                  <-
R                 :LOC 2G11
/      384    414  28     2G01        <<           P          <(     D(          <*
L                  09          GA                                  <-
R                 :LOC 2G11
/      414    449  34     2H01        <<           P BD    40<(     D(          <)
L                  09          GA                                  <-
R                 :LOC 2G
/      449    480  30     2H01        <<           P BD    35<-     <*          <-
L                  14          4A                                  <-
R                 :LOC 2G
/      480    514  33     2H01        <<           P BD    35<-     <*          <(
L                  09          GA
R                 :LOC 2G
/      514    546  31     2H01        <<BR         PP BD   40<-     <(          <*
L                  11          GA                                  <*
R                 :LOC 2G, CONSIDERABLE BR'N
/      546    575  28     2E11        <<BR         P          <-     <)
L                  17          AG                                  <)
/      575    604  29     2E21        <<BR         P          <(<-   <+
L                  10          AG                                  <)
/      604    617  13     8B00        <<P*         P CU    70<-
L                  06          6G     CM            CL     75          D.
/      617    653  35     2E42        <<BR         P          <-Q.   D+          <-
```

```
L                   11       AG                                          <)D-D-
/    653    661     08      8B00           <<P*          P CU      50<-
                    05           6G        CM              CU      [illegible]    D.
/    661    691     30      [illegible]    [illegible]   P                 [illegible]    [illegible]

L                   09           AG                                          [illegible]
/    717    744     26      2E43           <<            P              <-    D+D(
L                   09           AG                                          <)D-D-<(
R                  :LOC 2C83
/    744    773     29      2E11           <<            P              <-    D+
L                   06           AG                                          <+  D*
/    773    800     27      2E11           <<BR          P              <-    D)        <-
L                   15           AG                                          <+
/    800    830     30      2F12           <<BR          P              <-    D)        <-
L                   12           AG                                          <+D-D-
/    830    860     30      2F12           BR<<          P              <(    D+        <-
L                   15           AG                                          <+D(<(
/    860    890     30      2E11           <<            P BN      55<-       D)        <(
L                   09           AG                                          <)
R                  :LOC 2H, 2G
/    890    920     30      2F11           BR<<          P              <(    <*        <(
L                   16           AG                                          <=
R                  :SOME FRAG UP TO 0.2 M DIAMETER
/    920    950     30      2F11           BR<<          P              <-    <+        <*
L                   12           AG                                          <)D.D-
R                  :LOC 2F42
/    950    983     32      2F11           BR<<          P              <-    D)        <(
L                   06           AG                                          <)D.
R                  :CONTAINS TWO 0.2 M 8A'S
R                  :FAULT GOUGE AT 97.4 M
/    983   1014     10      8A00                         P                    D.
L                   00           5G                                          D.
R                  :EXTREMELY BROKEN
/   1014   1043     27      2F11           BR<<          P              <-    D+        <-
L                   06           AG                                          <+D-D.
R                  :LOC 2F52
/   1043   1072     27      2F11           BR<<          P              <-    D)        <(
L                   09           GA                                          <)  D-
R                  :FAULT GOUGE AT 106.2 M
/   1072   1101     28      2F12           BR<<          PP             <-    <+        <-
L                   06           AG                                          <+<(<-
/   1101   1135     33      2F11           BR<<          P              <-    <+<.      <-
L                   11           AG                                          <)D-D-<(
R                  :PATCH OF 2F53 AT 112.8
/   1135   1170     34      2F12           BR<<          P              <)    D+D-
L                   06           GA                                          <)D(D(D.
R                  :LOC 2F42
/   1170   1197     20      8A00                         P              <-    D-
L                   00           6G                                          D.
R                  :EXTREMELY BROKEN
/   1197   1238     40      2F12           BR<<          P              <-    <+        <-
L                   11           GA                                          <*<(
R                  :LOC 2F42
/   1238   1421     81      8C00           P*CM          P CU      40         D.
```

```
L                35        GW                    CL    50
R               :WHITE PLAG PHENOS TO SOME ALT'D TO SERICITE
/    1421  1437  15    2411        <<          P              <-
L                03        GA                               <*
R               :MINOR BB INTERCLATED NEAR TOI
/    1437  1470  22    BB10        P*CM        P CU    45     D.
L                09        4G                    CL    50   D-
/    1470  1505  30    2E11        <<          P              D*
L                03        AG                               <*D.D-
R               :LOC 2E12, MINOR INTERCALATED BA, VERY BROKEN
/    1505  1524  15    2F12        <<BR        P              D)
L                00        AG                                 D*D(
R               :VERY BROKKEN, MOST PY-MG AT 150.9
/    1524  1554  20    2C11        <<          P              <*
L                00        TA                               <*
R               :EXTREMELY BROKEN
/    1554  1585  25    2F11        <<BR        P              <*
L                00        6A
R               :EXTREMELY BROKEN, INTERCALATED 8B, LOC 2F41
/    1585  1615  25    2F11        <<          P          <-  D)          <-
L                03        GA                               <*  0-
/    1615  1645  29    2C11        <<          P          <(  <*          <-
L                03        TA                               <)
/    1645  1681  35    2F42        <<BR        P          <-  <+
L                10        GA                               <)<*<(
/    1681  1691  10    8A00        <<          P BN    40<-
L                06        8G                    C/    40
/    1691  1737  43    2F12        <<BR        P          <(  0=          <(
L                11        GA                               <*0)0*
/    1737  1810  71    8C00        P*CM        P CU    40     D.
L                25        GW                    CL    50
/    1810  1832  20    8A00        <<CM        P CU    50     D-
L                05        5G                                 D.
/    1832  1862  30    2F12        <<BR        P          <-  <+          <-
L                09        AG                               <)<-<*
/    1862  1892  30    2E11        <<          P          <-  <)          <*
L                06        AG                               <+<.<*
R               :LOC 2D11
/    1892  1920  28    2F11        <<BR        P          <-  D*          <(
L                09        AG                               <+
R               :RELATIVELY COARSE GRAINED
/    1920  1958  37    2E11        <<BR        PP         <(  D*          <*
L                09        AG                               <+  <.
R               :LOC 2F11
/    1958  1984  25    2F11        <<BR        P          <-  D)          <)
L                06        AG                               <)<.
R               :INTERCALATED 8B, 50%
/    1984  2027  42    8A00        <<          P CU    50<-   D-          <-
L                21        5G                                 D.
R               :LOWER C/ BR'D
/    2027  2057  30    2F42        <<BR        P          <-  0+        0*<*
L                12        AG                               <)0-
R               :ALL PR IN Q AT 205.5 M.., SOME INTERCALATED 8A
/    2057  2089  31    2F42        <<BR        P          <(  0)          <-
L                15        AG                               <*0-
```

```
 /     2089  2119  30     2F11       <<BR        P          <-    Q+        <-
 L                 09        AG                                 <)
 /     2119  2150  31     2F11       <<BR        P          <-    D*        <-
 L                 15        AG                                 <)D.
 R                :INTERCALATED 8B, 20%
 /     2150  2183  31     2F42       <<BR        P          <-    Q+        <-
 L                 06        GA                                 <(Q(Q-
 R                :INTERCALATED 8B, 10%
 /     2183  2213  30     2E11       <<BR        P          <-    D(        <*
 L                 11        GA
 /     2213  2256  40     2F11       <<BR        P          <-    D*        <)
 L                 11        GA                                 <(
 /     2256  2286  30     2E12       <<          P                Q+        <*
 L                 12        AG                                 <*Q-Q(
 R                :LOC 2E42
 /     2286  2316  30     2F11       <<BR        P          <-    <*        <*
 L                 15        AG                                 <(
 R                :SOME ASSIMILATED 8B
 /     2316  2346  29     2E42       <<          P          <-    Q+        <*
 L                 13        AG                                 <*Q(
 /     2346  2372  26     2F41       <<BR        P BD    50M(Q.  <)         <*
 L                 11        AG                                 <(Q-
 R                :INTERLEVELED 2H
 /     2372  2392  20     2F54       <<BR        P                Q1Q)    Q)<(
 L                 11        4A                                   Q)
 R                :ALL CP & PR IN Q FROM 237.2 TO 237.6 M
 /     2392  2403  11     8A00       <<CM        P CU    50<(     D.        <-
 L                 11        6G                    CL    45       D.
 /     2403  2438  34     2F52       <<BR        P          <-Q.  Q1        <-
 L                 15        4A                                   Q*  Q(
 /     2438  2469  31     2E52       <<          P          <(    <+        <.
 L                 10        3A                                 <*<-
 /     2469  2504  33     2E52       <<          P          <-Q-  <+        <.
 L                 11        3A                                 <(<(
 /     2504  2535  31     2E52       <<BR        P BD    50       Q=Q(    Q*<.
 L                 09        3A                                   Q-
 /     2535  2569  33     2F52       <<BR        P          <-    Q+        <.
 L                 19        GA                                   Q-
 /     2569  2605  35     2E52       <<RC        P          <-Q-  <+<.
 L                 21        3A                                   <*
 /     2605  2634  29     8B00       <<P*        P CU    60<-     D.        <*
 L                 15        5A                    CL    55       D*
 /     2634  2664  30     2E52       <<BR        P          <*Q.  Q=Q.
 L                 17        3A                                   Q-
 /     2664  2687  22     2F53       <<BR        P          <(    <=      <)
 L                 06        3A                                   Q-
 /     2687  2694  06     8A00       <<          P CU    45<*
 L                 00        7G                    CL    30       D.
 /     2694  2725  30     2E42       <<          P          <*    Q+
 L                 09        GA                                 <*Q-
 /     2725  2830 102     8A00       <<          P          <-
 L                 59        7G                                   D.
 R                :C/BROKEN
 /     2830  2861  31     2E56       <<          P          <-    #2D.
 L                 12        2A                                   #2
```

```
R                    :LAPILLI INDISTINCT
/     2861  2886  25     8B00       <<P*          P          <-     D(         <*
L                 12         4G                                  <-D.
R                 :SOME ASSIMILATED TUFF
/     2886  2922  35     2E42       <<            P          <*     O+D.       <(
L                 09         GA                                  <(D+
/     2922  2955  35     2E42       <<            P          <(     D+
L                 12         GA                                  <(D*
/     2955  2994  37     2E42       <<            P          <(     O+         <.
L                 12         5G                                  <+O-
R                 :LOC 2D42
/     2994  3058  63     8B10       <<            P          <-     D-         <*
L                 24         6G                                <-   D.
R                 :XENOLITH OF 2E AT 3032
/     3058  3092  33     2E12       <<            P          <-     <*         <-
L                 03         AG                                     <*
/     3092  3113  21     7C00       <<            P                            <(
L                 06         AG                                     D.
/     3113  3141  26     8A00       <<CM          P CU     30                  <*
L                 06         7G                 CL     45           D-
/     3141  3200  57     7C00       <<            P          <-     D.         <(
L                 23         4A                                     D*
R                 :GRAIN SIZE VARIES FROM RELATIVELY FINE TO MEDIUM GRAINED
R                 :END OF HOLE AT 320.0 M
R                 :HOLE 10 FEET LONGER THAN DRILLERS THINK. CORE BLOCK MISTAKE
R                 :AT 900 FEET
A001
ALAB              EQUITY MINESITE LABORATORY
ATYP              ASSAY
AMTH              WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM              RCOVSAMPLE   ROD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R       00    91 :TRICONED - NO CORE
R       91   140 :DYKE - NO SAMPLE
R      140   143 :TUFF - NO SAMPLE
R      143   183 :NO RECOVERY
A001   183   234       9923       0.005    0.5 0.06  0.005 0.001 2.19  0.02
A001   234   260       9924       0.005    0.5 0.07  0.005 0.001 1.47  0.05
A001   260   300       9925       0.001    0.5 0.04  0.005 0.001 1.71  0.005
A001   300   354       9926       0.001    0.5 0.05  0.005 0.001 2.79  0.005
A001   354   384       9927       0.001    0.5 0.05  0.005 0.001 1.23  0.005
A001   384   414       9928       0.001    0.5 0.78  0.005 0.001 0.97  0.005
A001   414   449       9929       0.001    0.5 0.05  0.005 0.001 1.00  0.005
A001   449   480       9930       0.001    0.5 0.07  0.005 0.001 0.83  0.005
A001   480   514       9931       0.001    0.5 0.04  0.005 0.001 0.74  0.005
A001   514   546       9932       0.001    0.5 0.06  0.005 0.001 0.72  0.005
A001   546   575       9933       0.04    10.0 0.19  0.005 0.02  4.62  0.02
A001   575   604       9934       0.02     7.0 0.16  0.005 0.005 2.72  0.04
R      604   617 :DYKE - NO SAMPLE
A001   617   653       9935       0.001    6.0 0.52  0.005 0.005 3.47  0.02
R      653   661 :DYKE - NO SAMPLE
A001   661   691       9936       0.03    11.0 0.16  0.005 0.005 4.20  0.02
A001   691   717       9937       0.12    26.0 0.56  0.02  0.03  5.84  0.02
A001   717   744       9938       0.26    49.0 0.48  0.04  0.02  4.64  0.25
A001   744   773       9939       0.02    14.0 0.19  0.02  0.005 4.28  0.005
A001   773   800       9940       0.02     9.0 0.12  0.005 0.005 3.83  0.02
```

A001	800	830		9981	0.01	16.0	0.22	0.005	0.02	4.89	0.03
A001	830	860		9982	0.04	22.0	0.22	0.005	0.005	3.90	0.02
A001	860	890		9983	0.005	10.0	0.17	0.005	0.005	3.23	0.02
A001	890	920		9984	0.04	26.0	0.42	0.005	0.005	2.59	0.04
A001	920	950		9985	0.05	36.0	0.17	0.005	0.005	3.04	0.03
A001	950	983		9986	0.03	18.0	0.13	0.005	0.005	4.21	0.03
R	983	1014	:DYKE - NO SAMPLE								
A001	1014	1043		9987	0.005	5.0	0.12	0.005	0.005	3.17	0.10
A001	1043	1072		9988	0.03	8.0	0.16	0.005	0.005	4.03	0.12
A001	1072	1101		9989	0.07	65.0	0.44	0.02	0.005	4.06	0.06
A001	1101	1135		9990	0.21	38.0	0.49	0.02	0.005	7.39	2.20
A001	1135	1170		9991	0.20	70.0	0.39	0.03	0.02	5.16	0.09
R	1170	1197	:DYKE - NO SAMPLE								
A001	1197	1238		9992	0.09	73.0	0.48	0.02	0.02	4.09	0.09
R	1238	1421	:DYKE - NO SAMPLE								
A001	1421	1437		9993	0.02	42.0	0.19	0.005	0.005	3.05	0.02
R	1437	1470	:DYKE - NO SAMPLE								
A001	1470	1505		9994	0.005	4.0	0.07	0.005	0.005	3.29	0.005
A001	1505	1524		9995	0.05	6.0	0.22	0.005	0.01	8.40	0.21
A001	1524	1554		9996	0.005	0.5	0.06	0.005	0.005	1.35	0.03
A001	1554	1585		9997	0.005	1.0	0.07	0.005	0.005	2.37	0.04
A001	1585	1615		9998	0.005	0.5	0.04	0.005	0.005	1.11	0.02
A001	1615	1645		9999	0.005	0.5	0.05	0.005	0.005	0.59	0.005
A001	1645	1681		10000	0.01	2.0	0.05	0.005	0.005	4.40	0.01
R	1681	1691	:DYKE - NO SAMPLE								
A001	1691	1737		1602	0.005	4.0	0.06	0.005	0.02	4.76	0.01
R	1737	1832	:DYKE - NO SAMPLE								
A001	1832	1862		1603	0.02	10.0	0.15	0.005	0.01	2.83	0.01
A001	1862	1892		1604	0.01	4.0	0.08	0.005	0.005	2.10	0.01
A001	1892	1920		1605	0.01	3.0	0.09	0.005	0.005	1.51	0.01
A001	1920	1958		1606	0.005	2.0	0.05	0.005	0.005	1.87	0.005
A001	1958	1984		1607	0.005	4.0	0.73	0.005	0.005	2.89	0.01
R	1984	2027	:DYKE - NO SAMPLE								
A001	2027	2057		1608	0.05	10.0	0.21	0.005	0.21	7.82	0.05
A001	2057	2089		1609	0.005	6.0	0.10	0.005	0.02	3.90	0.02
A001	2089	2119		1610	0.005	2.0	0.55	0.001	0.005	3.00	0.03
A001	2119	2150		1611	0.005	3.0	0.12	0.005	0.03	4.17	0.03
A001	2150	2183		1612	0.02	5.0	0.18	0.005	0.01	2.95	0.02
A001	2183	2213		1613	0.005	2.0	0.11	0.005	0.005	1.12	0.02
A001	2213	2256		1614	0.005	3.0	0.08	0.005	0.005	1.96	0.06
A001	2256	2286		1615	0.005	5.0	0.06	0.005	0.005	1.72	0.08
A001	2286	2316		1616	0.04	25.0	0.20	0.03	0.005	1.87	0.005
A001	2316	2346		1617	0.02	10.0	0.08	0.02	0.01	1.92	0.005
A001	2346	2372		1618	0.03	8.0	0.08	0.01	0.01	2.02	0.005
A001	2372	2392		1619	1.37	270.0	2.25	0.19	0.10	9.48	0.58
R	2392	2403	:DYKE - NO SAMPLE								
A001	2403	2438		1620	0.02	7.0	0.49	0.03	0.02	3.17	0.10
A001	2438	2469		1621	0.02	15.0	0.09	0.03	0.005	2.93	0.09
A001	2469	2504		1622	0.08	26.0	0.24	0.02	0.02	4.41	0.04
A001	2504	2535		1623	0.03	12.0	0.28	0.01	0.02	5.78	0.07
A001	2535	2569		1624	0.005	2.0	0.11	0.005	0.005	2.73	0.01
A001	2569	2605		1625	0.10	35.0	0.49	0.01	0.02	5.93	0.06
R	2605	2634	:DYKE - NO SAMPLE								
A001	2634	2664		1626	0.11	34.0	0.46	0.005	0.10	8.59	0.06
A001	2664	2687		1627	0.20	42.0	3.34	0.01	0.32	15.50	0.12

R	2687	2694	:DYKE - NO SAMPLE								
A001	2694	2725		1628	0.07	23.0	0.58	0.005	0.01	5.66	0.06
	2725	2830	:DYKE - NO SAMPLE								
A001	2830	2861		1629	0.02	4.0	0.22	0.005	0.09	10.99	0.04
R	2861	2886	:DYKE - NO SAMPLE								
A001	2886	2922		1630	0.02	6.0	0.20	0.005	0.05	4.05	0.03
A001	2922	2955		1631	0.03	8.0	0.13	0.005	0.01	2.44	0.005
A001	2955	2994		1632	0.04	11.0	0.17	0.005	0.005	2.50	0.01
R	2994	3058	:DYKE - NO SAMPLE								
A001	3058	3092		1633	0.06	35.0	0.35	0.005	0.005	2.08	0.07
R	3092	3113	:GABBRO - NO SAMPLE								
R	3113	3141	:DYKE - NO SAMPLE								
R	3141	3200	:GABBRO - NO SAMPLE								
R			:END OF HOLE AT 320.0 M								

```
IDEN6B0201        X87CH315 NQ   MAY87DMLDJHJTT MAY87ACK              0.0
IPRJ          EQUITY SILVER MINES LTD           MAIN ZONE - MN GEOCODE
S000   00    411 MT   353.5 090.0 -70.0                   7812.00   8446.50   1260.00
S001  411   1295      353.5 090.8 -70.0
S002 1295   2149      353.5 091.6 -70.0
S003 2149   2880      353.5 092.3 -70.0
S004 2880   3383      353.5 093.0 -71.0
S005 3383   3535      353.5 093.2 -71.0
/SCL          MT.2MT.2
LSCL              MT.2        LCTM
/NAM                                                        QZSZTOPYCPTTASPRGY
LNAM                                                        DMCBCLMGHESLGLMO
/       00     37          OVBN                   P
R                 :TRICONED - NO CORE
/       37     68  26      2D83MS     <<          P         >(     <)
L                  00          6T
/       68     91  16      2D31MS                 P                <(
L                  02          5A
R                 :.1 M 2D54: CLAY OUGE @ 8.9 M
/       91    122  09      2D31MS                 P                <(
L                  00          5A
R                 :0.2 M CLAY GOUGE: INTO 2E LOC
/      122    194  67      8C01PL     P*          P                D-
L                  16          AW                   CL   055
R                 :CU OBSCURRED IN BROKEN CORE; 4 CM CLAY GOUGE @ 18.0 M
/      194    225  21      2D31MS     BR          P                <-
L                  00          5A
R                 :POST-MIN (FAULT/) BRECCIA W/GOUGE
/      225    252  21      8A00PL     P*          P                <.
L                  02          5A
R                 :A FEW XENOLITHS OF 2D31 BXIA: CNTS OBSCURRED IN BROKEN CORE
R                 :DACITE?
/      252    305  39      8A00CL     P*          P                D.
L                  09          GA                              <-
R                 :0.4 M 2D XENOLITH: INTO 8A AS ABOVE 22.5-25.2 M: LOWER CNT
R                 :OBSCURRED IN BROKEN CORE
/      305    341  36      2D43MSQZ   <<          P         <(     <=
L                  13          4A                                <(  <(<-
R                 :INTO 2D33 LOC.
/      341    417  65      8A00CL     P*          P CU   050       D.
L                  85          GA
R                 :CL OBSCURRED IN BROKEN CORE
/      417    435  25      2D33MS     <<          P                D(
L                  02          5A
/      435    472  36      8C01PL     P*          P                D.
L                  06          AW                   CL   040
R                 :CU OBSCURRED IN BROKEN CORE
/      472    527  50      2D31MS                 P
L                  00          5A
R                 :INTO 2E81 (APPROX. .3 M)
/      527    533  05      8A00CL     P*          P                D.
L                  00          GA
R                 :CNT OBSCURRED IN BROKEN CORE
/      533    538  04      2D31MS                 P                <-
L                  00          5A
```

```
/    538   563  29    2D13CL                   P                <)
L               05        5G                                 <(
R               :IN PARTS IS CLOSER TO 2E13
/    563   592  27    2D33MS                   P                <)
L               07        5A                                           ?.
R               :CNT 0.5 M OF 2C10
/    592   622  27    2D41MS                   P                <)         <)
L               20        5A                                           ?.
R               :CONTAINS OL4 M OF 2D51, CONTAINING ROUNDED FRAGMENTS
/    622   652  28    2D31MS                   P                <(         <)
L               16        5A
/    652   679  27    2D31MS                   P                <(         <(
L               06        5A
R               :INTO 2E31 IN PLACES
/    679   694  15    2D81MS     <(            P                <+
L               08        GT                                    <(<(
R               :CONTAINS 0.5 M OF 2D33
/    694   716  22    2D31MS                   P                <+
L               17        5A                                    <(<(
/    716   745  29    2D31MS                   P                <)         <)
L               09        5A                                    <-
R               :CONTAINS 2C81 IN PLACES & ALSO SECONDARY
R               :(<--FELDSPAR IN PLACES)
/    745   771  23    2D11MS                   P                <(         <)
L               19        5A                                    <-<.
R               :CONTAINS SMALL AMOUNT  2C11
/    771   876  94    8A00PL     P*            P CU   060       D.         <(
L               10        7G
R               :CONTAINS 2 XENOLITHS APPROX. 0.3 M EACH OF 2D20 CONT. PY, HE
R               :SZ, MG: LOWER CONTACT IRREGULAR
/    876   906  25    2D41MSQZ   BR            P          <(    D(
L               60        5A
R               :CONT. .15 M OF 8A00 @ 89.3, BR OCCURS @ 90.4 M
/    906   939  31    2D41MSQZ                 P          <)    <)         <(
L               15        4A
/    939   969  28    2E41MSQZ   AD            P          <(    B)
L               18        5A
R               :CONTAINS MINOR 2D41 IN PLACES
/    969   999  27    2E31                     P          <)    D(         <-
L               17        6A
R               :INTO 2E41 W/COLOR = 5A
/    999  1022  23    2E51MSQZ                 P          <+    <)
L               08        4A
R               :COLOR TO 5A, SILICIFICATION PREFERENTIALLY OCCURS BETWN GRAINS
/   1022  1048  24    2D11CL                   P          <(    D)
L               07        5G                                  B1
R               :COLOR TO 6G
/   1048  1068  16    2D11CLMS                 P          <*    D)
L               12        6G                                  B=  >(
R               :MINOR SILICIFICATION AS WELL AS PHYLLIC ALTERATION
/   1068  1097  25    2E21SZCL   AD            P          <(B)  B+
L               20        5G                                  B=      <.
R               :GRADES TO 2E23
/   1097  1122  24    2E21SZCL   AD            P          <(B*  B)
L               18        5G                                  B=
```

```
R                :SILICIFICATION OCCURRING INTERSTITIALLY<(B-  B-
/    1122  1148  25    2D81MS                P             B)<)<-
                 15       5T
R                :LOCALLY 2581
/    1148  1167  16    2C81MS                P               D-
L                09       6T                                 D.
/    1167  1189  21    2D21SZMS              P           B-  D*
L                09       AT                               B(
R                :LOCALLY TO 2C81 AS ABOVE
/    1189  1211  22    2D11CLMS              P               <+
L                11       5G                               D-    ?-
/    1211  1239  27    2C83MS     <<         P               <+
R                15       5T                                 <-
/    1239  1268  28    2C83MS     <<         P               <+
L                12       GT                               B)
/    1268  1298  24    2D13CL     <<MX       P         <)    QZ      <(
L                11       4G                               Q1<(
/    1298  1331  28    2C83MS     <<         P         <)    Q1
L                19       AT                               B)<(
/    1331  1359  27    2C83MS     <<MX       P               Q1      <)
L                19       5T                               B)<(<*
/    1359  1389  29    2D51QZ     <<         P         <2B-  Q=      <(
L                19       GA                               Q)<(D-?)
/    1389  1419  28    2D41QZ     <<<<       P         <1    Q=      >(
L                23       5A                               Q)<=
/    1419  1433  14    2D51QZCL   <<         P         Q2D-  <=
L                11       4G                               Q1Q=
L    1433  1455  22    2C11CL     <<         P               D.        <)
L                19       5G                               Q1<-
R                :GYPSUM - MAJOR COMPONENT OF MICROVEINS, APPEARANCE OF UNIT
R                :SIMILAR TO 8D
/    1455  1478  21    2C11CL                P               D.
L                19       5G      <<                   <)    D-        <)
/    1478  1514  34    2D41QZCL              P             Q1
L                27       GA      <<                   Q2    <=
/    1514  1546  29    2C11CL                P             <1<)
L                19       5G                                 D.
R                :SIMILAR TO INTERVAL 143.3 - 145.5        D2  <-
/    1546  1635  81    8C00PL     P*           CU   033
L                32       8G
R                :LOWER CONTACT OBSCURRED IN BROKEN CORE: CLAY GOUGE @
R                :167.5 TO 168.5
/    1635  1670  30    8D11MS                P               D-        <-
L                13       7T                               <-
R                :CONTAINS 1.0 M OF 2D81: CHLORITE ALTERATION OCCURS
R                :PREFERENTIALLY AROUND MICROVEINS
/    1670  1682  11    2D11CLMS              P               D(
L                04       5G                               Q=  <-  ?.
R                :CONTAINS 0.4 M OF 8D81 TO HIGH ALTERATION AROUND VEINS
/    1682  1705  23    8D11MSCL              P               D.
L                08       7T                                   <-  ?.
R                :CONTAINS 0.7 M OF 2D11
/    1705  1731        8A00PL                  CU   020
                 02       5G
R                :CONTAINS 0.2 M OF 2D81: LOWER CONTACT IRREGULAR
```

```
/   1731  1761  29    2D31MS                      P                 <(
L                 09        5A                                      <1  <-       <-
3                 :BRECCIATED AND DEFORMED NEAR CONTACT WITH DYKE
/   1761  1791  28    2E41QZ                      P          Q2     B(
L                 15        5A                                      <(           <(
/   1791  1821  29    2E41QZ                      P          Q1     D-
L                 16        5A                                      <(           <-
/   1821  1850  27    2D41QZ                      P          Q1     D-
L                 14        5A                                      <)           <(
/   1850  1880  29    2D41QZ                      P          Q=     D-
L                 06        5A                                        <(         <(
/   1880  1911  30    8A00PL        P*            P CU   040        D-
L                 09        5G                                      B1           <(
R                 :LOWER CONTACT OBSCURRED BY BROKEN CORE
/   1911  1948  36    2D81CLQZ      P                               <=           <1
L                 19        5G                                        <-<.
/   1948  1971  23    8A00PL        P*            P
L                 18        6G                                                   <)
R                 :UPPER CONTACT IRREGULAR: CONTAINS 2C XENOLITH OF APPROX. .15 M
/   1971  2198 219    8A00PL        P*            P CU   070
L                 73        6G                      CL   045
/   2198  2228  28    2D21SZCL                    P          Q1<.  <)
L                 07        5G                                      <=           <(
/   2228  2258  29    2D41QZCL                    P          Q1<.  <)
L                 14        5A                                      <=           <(
/   2258  2288  26    2D41QZCL                    P          Q1     D)
L                 13        5A                                      <=<(<(       <-
                  :CONTAINS .20 M OF MX, PY, MG, HE
/   2288  2318  29    2D41QZCL                    P          Q=     <=
L                 20        4A                                      <=<-<-       <-
/   2318  2348  30    2D11CL                      P          Q)     <*
L                 22        4G                                      <1           <)
R                 :CONTAINS 0.3 M OF INTENSELY << 2C81
/   2348  2378  28    2D41QZ                      P          Q1     <)
L                 12        5A                                      <)<-<-       <)
R                 :CONTAINS 0.3 M OF CHLORITIZED ANDESITE DYKE
/   2378  2413  32    2D41QZ                      P          Q1     D-
L                 20        5A                                      <)<-
/   2413  2425  11    8A00PL        P*            P CU   035        D.
L                 10        5G                      CL   040
/   2425  2451  26    2D11CLQZ                    P          Q1     B)
L                 18                                                Q2<)
R                 :ZONE SHOWS ALSO MODERATE TO STRONG SILICIFICATION
/   2451  2588 130    8A00DL        P*            P CU   030        D-
L                 43        5G                                      01D=
R                 :LOWER CONTACT NOT WELL DEFINED, PHENOCRYSTS HAVE
R                 :RECRYSTALIZED & MINERALIZED
/   2588  2618  29    2D11CLQZ                    P          Q*     D*
L                 20        5G                                      Q1<-<-       <-
/   2618  2643  24    2D11C;QZ                    P          Q1     D*
L                 10        5G                                    <(<1<)         <-
R                 :CONTAINS FRAGMENTS OF 8D11
/   2643  2661  16    8D11CL                      P                 <)
                  06        4G                                    <(<1<(
R                 :SHOWS MINOR SILICIFICATION: CONTACTS OBSCURRED: CONTAINS
```

[illegible]

L 169 8G

R :CL OBSCURRED BY BROKEN CORE; DYKE SHOWS CHLORITE ALTERATION

R :NEAR CONTACTS

/	3019	3048	28	8D51QZPL	P*	P	B3	D-
L			07	6V				<) <-
/	3048	3078	30	8D41QZPL	P*	P	B2	D.
L			06	GV				<= <(
/	3078	3094	16	8D41QZ	P*	P	B2	<(
L			04	GV				<) <-
/	3094	3116	21	8D41QZCL	P*	P	B2	D-
L			00	7G				<= <(
/	3116	3146	30	8D41QZ	P*	P	B2	D(
L			03	7V				<(
/	3146	3176	28	8D51QZ	P*	P	B2	D.
L			05	5V				B1
/	3176	3206	30	8D51QZ	P*	P	B2	D.
L			00	6V				B1
/	3206	3229	23	8D51QZ	P*	P	B2	D.
L			16	60				B= <-
/	3229	3259	25	8D51QZ	P*	P	B3	
L			07	7V				
/	3259	3385	124	8D51QZ	P*	P	B1	D.
L			41	5V				B1D=

R :CONTAINS NUMEROUS XENOLITHS OF 7E

/	3385	3535	146	7E00PL		P	01	
			70					B1D=

R :CONTACT NOT SEEN, ABOUT 1/2 OF THE SECTION IS SIMILAR TO 8D51

R :END OF HOLE

A001

ALAB EQUITY MINESITE LABORATORY

ATYP ASSAY

AMTH WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST

AUMM			RCOVSAMPLE	ROD % CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	37	:TRICONED - NO CORE							
A001	37	68	9841	0.005	2.0	0.63	0.005	0.005	5.19	0.02
A001	68	91	9842	0.005	1.0	0.06	0.005	0.005	4.10	0.02
A001	91	122	9843	0.005	0.5	0.03	0.005	0.005	1.40	0.02
R	122	194	:DYKE - NO SAMPLE							
A001	194	225	9844	0.005	1.0	0.04	0.005	0.005	2.29	0.07
A001	225	252	9845	0.005	0.5	0.05	0.005	0.005	1.41	0.02
R	252	305	:DYKE - NO SAMPLES							
A001	305	341	9846	0.005	2.0	0.97	0.005	0.005	4.36	0.06
R	341	417	:DYKE - NO SAMPLES							
A001	417	435	9847	0.01	0.5	0.42	0.005	0.005	1.85	0.02
R	435	472	:DYKE - NO SAMPLES							
A001	472	500	9848	0.005	0.5	0.06	0.005	0.005	1.51	0.01
A001	500	527	9849	0.005	0.5	0.05	0.005	0.005	1.89	0.01
A001	527	538	9850	0.005	0.5	0.05	0.005	0.005	3.01	0.02
A001	538	563	9851	0.005	0.5	0.06	0.005	0.01	2.52	0.02
A001	563	592	9852	0.005	0.5	0.06	0.005	0.005	1.81	0.04
A001	592	622	9853	0.005	0.4	0.04	0.005	0.001	1.99	0.07
A001	622	652	9854	0.005	0.5	0.05	0.005	0.005	2.06	0.11
A001	652	679	9855	0.005	2.0	0.06	0.005	0.005	2.10	0.10

A001	679	694	9856	0.005	3.0	0.08	0.005	0.005	3.02	0.13
A001	694	716	9857	0.005	9.0	0.12	0.02	0.005	2.21	0.06
A001	716	745	9858	0.005	5.0	0.03	0.005	0.005	1.92	0.05
A001	745	771	9859	0.005	3.0	0.17	0.005	0.005	1.43	0.09
R	771	876	:DYKE - NO SAMPLES							
A001	876	906	9860	0.005	5.0	0.05	0.005	0.005	1.89	0.12
A001	906	939	1634	0.03	24.0	0.22	0.06	0.02	2.78	0.09
A001	939	969	1635	0.02	25.0	0.23	0.05	0.01	1.82	0.02
A001	969	999	1636	0.01	2.0	0.03	0.005	0.01	1.92	0.05
A001	999	1022	1637	0.005	3.0	0.09	0.005	0.005	2.76	0.02
A001	1022	1048	1638	0.005	2.0	0.07	0.005	0.005	3.65	0.12
A001	1048	1068	1639	0.02	4.0	0.09	0.005	0.005	3.57	0.19
A001	1068	1097	1640	0.03	8.0	0.26	0.005	0.03	5.52	0.07
A001	1097	1122	2001	0.02	17.0	0.24	0.005	0.09	4.11	0.25
A001	1122	1148	2002	0.01	15.0	0.80	0.005	0.005	3.93	0.03
A001	1148	1167	2003	0.02	3.0	2.10	0.005	0.005	2.34	0.005
A001	1167	1189	2004	0.02	9.0	0.29	0.005	0.01	3.97	0.01
A001	1189	1211	2005	0.01	13.0	0.67	0.005	0.11	6.63	0.02
A001	1211	1239	2006	0.01	9.0	0.50	0.005	0.04	8.80	0.01
A001	1239	1268	2007	0.02	15.0	0.53	0.005	0.06	8.52	0.09
A001	1268	1298	2008	0.04	13.0	0.53	0.02	0.06	17.10	0.02
A001	1298	1331	2009	0.03	49.0	3.64	0.02	0.04	14.5	0.07
A001	1331	1359	2010	0.05	36.0	2.20	0.03	0.05	12.06	0.02
A001	1359	1389	2011	0.04	32.0	1.22	0.005	0.03	10.62	0.02
A001	1389	1419	2012	0.03	26.0	0.97	0.005	0.03	12.65	0.02
A001	1419	1433	2013	0.05	15.0	0.16	0.005	0.05	13.70	0.03
A001	1433	1455	2014	0.005	3.0	0.09	0.005	0.005	3.18	0.01
A001	1455	1478	2015	0.005	3.0	0.05	0.005	0.005	4.01	0.02
A001	1478	1514	2016	0.05	44.0	1.08	0.005	0.005	5.34	0.11
A001	1514	1546	2017	0.005	3.0	0.01	0.005	0.005	3.84	0.02
R	1546	1635	:DYKE - NO SAMPLES							
A001	1635	1670	2018	0.01	7.0	0.14	0.005	0.02	4.40	0.02
A001	1670	1682	2019	0.03	11.0	0.08	0.005	0.02	4.28	0.03
A001	1682	1705	2020	0.005	6.0	0.11	0.005	0.005	3.46	0.02
R	1705	1731	:DYKE - NO SAMPLES							
A001	1731	1761	2021	0.02	5.0	0.08	0.005	0.005	2.31	0.03
A001	1761	1791	2022	0.005	1.0	0.05	0.005	0.005	1.82	0.02
A001	1791	1821	2023	0.005	0.0	0.05	0.005	0.005	1.46	0.02
A001	1821	1850	2024	0.005	0.0	0.04	0.005	0.005	1.07	0.02
A001	1850	1880	2025	0.01	3.0	0.09	0.005	0.01	1.57	0.02
R	1880	1910	:DYKE - NO SAMPLES							
A001	1910	1948	2026	0.11	61.0	3.33	0.03	0.03	3.99	0.15
A001	1948	1971	2027	0.005	3.0	0.11	0.005	0.005	2.89	0.03
R	1971	2198	:DYKE - NO SAMPLES							
A001	2198	2228	2028	0.16	20.0	0.87	0.05	0.01	3.29	0.37
A001	2228	2258	2029	0.13	42.0	1.58	0.03	0.01	2.41	0.33
A001	2258	2288	2030	0.04	7.0	0.57	0.01	0.005	2.68	0.47
A001	2288	2318	2031	0.03	6.0	0.33	0.01	0.005	3.05	0.27
A001	2318	2348	2032	0.05	27.0	0.70	0.01	0.005	2.74	0.24
A001	2348	2378	2033	0.02	20.0	0.57	0.01	0.005	2.45	0.22
A001	2378	2425	1680	0.07	46.0	0.74	0.02	0.005	2.73	0.15
A001	2425	2451	2034	0.19	93.0	0.70	0.09	0.04	3.59	0.10
R	2451	2588	:DYKE - NO SAMPLES							
A001	2588	2618	2035	0.07	17.0	0.28	0.02	0.005	3.37	0.14
A001	2618	2643	2036	0.08	21.0	0.27	0.02	0.005	4.18	0.14

A001	2643	2661		2037	0.07	10.0	0.15	0.01	0.005	3.64	0.08
R	2661	3019	:DYKE - NO SAMPLES								
A001	3019	3048		2038	0.005	0.5	0.04	0.01	0.005	2.23	0.06
A001	3048	3078		2039	0.005	2.0	0.03	0.01	0.005	2.04	0.06
A001	3078	3094		2040	0.005	0.5	0.03	0.005	0.005	2.47	0.06
A001	3094	3116		1641	0.01	8.0	0.04	0.005	0.005	3.01	0.05
A001	3116	3146		1642	0.005	6.0	0.02	0.005	0.005	2.58	0.05
A001	3146	3176		1643	0.005	9.0	0.01	0.005	0.005	2.15	0.04
R	3176	3535	:MIXED DYKE & GABBRO - NO SAMPLES								
R			:END OF HOLE								

```
IDEN6B0201        X87CH316 NO   MAY87DML    JTT MAY87ACK            0.0
IPRJ            EQUITY SILVER MINES LTD          MAIN ZONE - MN GEOCODE
S000   00    457 MT  329.2 090.0 -70.0                        7751.0    8445.5    1260.0
S001  457   1295     329.2 090.0 -70.0
S002 1295   2073     329.2 090.0 -70.0
S003 2073   2743     329.2 090.0 -70.0
S004 2743   3292     329.2 090.0 -70.0
/SCL            MT.2MT.2
LSCL                MT.2        LCTM
/NAM                                                          QZSZTQPYCPTTASPRGY
LNAM                                                          DMCBCLMGHESLGLMO
/        00     91          OVBN                    P
R                   :TRICONED - NO CORE
/        91    188  90      8A00PL      P*          P
L                   17          6G                     CL    055     B(
R                   :CU NOT VISIBLE, LOWER CONTACT ALTERED - DYKE SHOWS QTZ-SERICITE ALT. NE
CTCTS.
/       188    213  25      2D13MS                  P                  D(
L                   00          6A                                   B)
R                   :CONTAINS SOME 2C81
/       213    244  30      2D31                    P                  B+
L                   05          5A                                   <(   <)
R                   :CONTAINS 0.4 M OF 8A00 (CONTACT OBSCURRED)
/       244    267  23      2D81MS                  P            <(    B+
L                   06          5T                                      <-
/       267    288  19      8A00CL      P*          P CU   040         D)
L                   00          7G                     CL    025     B*
R                   :CONTAINS 0.2 M OF 2D31 CONTAINING PY AND HE
/       288    313  22      2D41QZ                  P                  <=
L                   00          6A                                     <(<-
/       313    330  17      2E31MS                  P                  <(
L                   07          6A6A
/       330    348  18      8A00PL     P*           P CU   060         <(
L                   02          7G                     CL    060
/       348    384  27      2D31                    P                  <+
L                   00          5A                                     <-<)
R                   :CLAY GOUGE @ 37.7 M
/       384    406  22      8A00CL      P*          P                  D.
L                   02          GA                     CL    050     <)
R                   :CONTAINS SMALL XENOLITHS OF 2D31: UPPER CONTACT OBSCURRED
R                   :BY BROKEN CORE
/       406    440  31      2D21SZMS                P             B-  <)
L                   10          5A                                <(    <(
/       440    474  34      2D21SZ                  P                  <)
L                   06          5A                                   <(   <*
/       474    507  31      2D81MS                  P                  <+<.
L                   21          GT                                   <(<(<)   <-
R                   :INTO 2E81
/       507    514  07      8A00PL      P*          P CU   070         <-
L                   02          7G                     CL    010
/       514    539  25      2D81MS                  P             B.  <+
L                   07           GT                                    <(<-
/       539    560  19      2C83SZMS    <<MX        P             B.  >2
L                   06          5T                                     <(<.
/       560    589  28      2D21SZ      <<MX        P             B-  <1
L                   16          5A
```

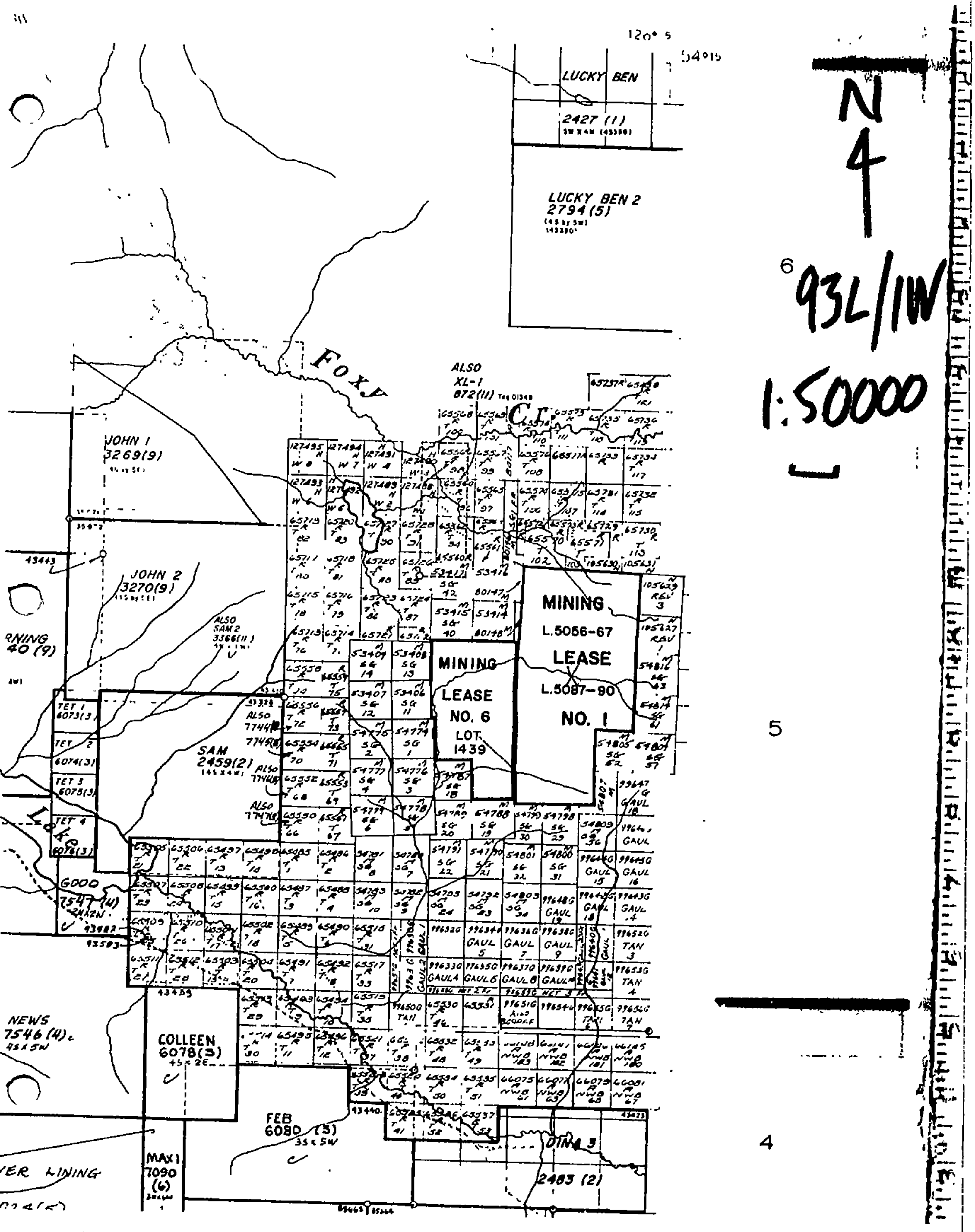
```
 /     589    615  20     2C81MSSZ                    P              B.   D)
 L                 00          6T
 R                :CONTAINS SOME 2D21 WITH PY STRINGERS & SZ
 /     615    645  30     2D21SZ                      P              B-   <=
 L                 04          5A
 /     645    675  30     2D31MS                      P                   <+
 L                 11          5A                                    <-
 R                :CONTAINS 0.2 M OF 8A00
 /     675    705  30     2D21SZ                      P              B.   <+
 L                 10
 R                :CONTAINS 0.2 M OF 8A00: INTO 2E21 IN PLACES
 /     705    731  24     2D31MS                      P                   <)
 L                 08           5A                                   <-
 /     731    765  34     8D81CL        P*            P                   <*          <+
 L                 24          6G                                      Q2
 R                :CONTACTS OBSCURRED THROUGH ALTERATION
 /     765    785  19     2D41QZ                      P                   <+          <(
 L                 19          GA                                      <+
 R                :MAY IN PART BE COMPOSED OF 8D81
 /     785    817  31     2D31MS                      P                   <=
 L                 12          6A                                      <(
 R                :LOCALLY INTO 2C31, & LOCALLY SHOWS <<
 /     817    847  29     2D81CL                      P                   B+          <)
 L                 18          6G                                      B1  <(
 /     847    877         2E41                        P
 /     877    898  20     2E41QZCL                    P                   B*B.
 L                 15          GA                                      B=  <-         <+
 /     898    926  28     2D81CL                      P                   <(
 L                 15          GA                                      D=
 R                :CONTAINS 0.3 M OF 8A00: LOC INTO 2E81
 /     926    958  31     2D41QZ                      P              <)   <?<)        <=
 L                 19          6A                                          <(
 R                :LOC INTO 2E41 (ROCKS MAY BE 2D91)
 /     958    980  19     2D41QZ                      P              <*   <?B*        <)
 L                 15          6A                                      <-
 R                :LOCALLY INTO 2E81: ROCKS MAY POSSIBLY BE 2D91
 /     980   1010  30     2C81MS                      P                   <)        <-<(
 L                 24          GT                                       <-<-
 R                :LOC. INTO 2D41
 /    1010   1040  26     2D41QZ                      P              Q=    <(         <*
 L                 14          5A                                      B)
 /    1040   1070  29     2D41QZ                      P                    <(         <(
 L                 16          VA
 /    1070   1100  30     2D41QZ                      P              <(    <*         <(
 L                 08          5G                                      <)<-<-
 R                :LOCALLY INTO 2C41
 /    1100   1130  30     2D41QZ                      P                    <*         <(
 L                 22          5G                                      <)<-<.
 R                :CONTAINS 0.8 M OF 8A00 FROM 110.5 TO 111.3
 /    1130   1160  30     2D41QZCL                    P                    <+         <*
 L                 22          6G                                      <=<(<-
 /    1160   1189  29     2D51QZCL                    P                    <)         <)
 L                 15          5G                                      <=<*<-
 /    1189   1201  11     8A00PL        P*               CU   050                     <(
 L                 09          5G                        CL   070          D*
```

```
/   1201  1223  22    2D41QZCL             P                <)        <(
L               06      GA                               <)  <(
/   1223  1266  43    8A00PL     P*        P                D-
L               27      5G                               <)D)
R              :CONTACT OBSCURRED BY ALTERATION: CONTAINS 0.2M XENOLITH OF 2D41
/   1266  1293  26    2D41QZCL   BR        P                <(        <+
L               16      GA                               <+
/   1293  1310  17    2D41QZ               P                <(        <*
L               09      5A                               <(  <-
/   1310  1322  12    2D41QZCL   BR        P                <(        <(
L               10      7G                               <=
/   1322  1334  12    8A00PL               P CU   070       D-        <*
L               10      5G                   CL   070
/   1334  1355  20    2D41QZCL             P                B(        <*
L               13      5G                               <)
R              :LOC INTO 8A00
/   1355  1374  19    2D41QZ               P                <(        <(
L               17      5A                               <)  <(
/   1374  1469  92    8A00PL     P*        P                          <(
L               51      4G                   CL   065       D)
R              :UPPER CONTACT OBSCURRED BY BROKEN CORE
/   1469  1500  31    2D21SZMG             P           <(<(  <=      <-
L               06      3N                               <*<+<(
R              :ALSO SHOWS STRONG SILICIFICATION
/   1500  1529  29    2D21SZ               P             O-  <*
L               06      5A                               <(<.
R              :SHOWS MODERATE SILICIFICATION
/   1529  1552  21    2D31MS               P                <+
L               19      5A                               <-<-<.
/   1552  1576  23    2D11CL               P                <(        <)
L               18      5G                               <=
/   1576  1591  14    2D11CL               P                <(
L               08      5G                               <=
R              :CONTAINS 0.4 M OF 8A00
/   1591  1620  24    2D31MS               P                <(        <-
L               02      6A                               <+
/   1620  1764 138    8C00PL     P*        P CU   025       D.
L               51      7G
R              :LOWER CONTACT OBSCURRED BY BROKEN CORE: INTO 8A00 NEAR CNTS
/   1764  1786  20    2D41QZ               P                <*        <(
L               03      6A                               <*  <(
/   1786  1812  26    2D31MS               P                <*        <-
L               07      5A                               <)
R              :SHOWS MNR SILICIFICATION: LOC INTO 2E31
/   1812  1842  30    2D41QZ               P                B+        <-
L               12      5A
R              :INTO LOC 2C41
/   1842  1872  30    2D41QZ               P                <)<.      <(
L               03      GA                            <-      <(
R              :CONTAINS 0.3 M XENOLITH OF 8A00
/   1872  1902  30    2D41QZ     <<        P                <)        <(
L               03      5A                                  <+
/   1902  1932  29    2D41QZ     <<        P                <(        <(
L               06      5A
/   1932  1962  28    2D41QZ               P                <-<.
```

			04	4A						<*	
/	1962	1997	34	2D41QZ		P				<+	<-
L			11	4A						<(	
/	1997	2032	32	2D41QZ		P				<*	
L			10	4A						<(	
/	2032	2059	29	2D51QZ	<<	P				<)<)	
L			19	3N						<)	
/	2059	2086	27	2D51QZ	<<	P				<*<(	
L			11	4N						<(	
R			:CONTAINS 0.3 M OF 8A00								
/	2086	2146	60	8A00PL	P*	P	CU	025		D-	<)
L			13	5G			CL	070		D(	
R			:CONTAINS 2 XENOLITHS OF 2D41 EACH 0.5 M								
/	2146	2177	28	2D81MS		P				<)	
L			05	6A					<+		
/	2177	2203	26	2D41QZ		P				<)	
L			15	5A						<)	
/	2203	2223	15	8A00PL	P*	P				D-	
L			00	5G						D-	
R			:CONTACTS OBSCURRED BY BROKEN CORE								
/	2223	2253	30	2D51QZCL	<<	P			<(	<(	
L			18	4N						<*<(	
/	2253	2284	31	2D41QZCL		P				<(	
L			14	4N						<)<.	
/	2284	2314	28	2D41QZ	BR	P				<*<.	
L			21	4N						<)<-	
/	2314	2344	30	2D51QZMG	<<	P				<(<.<(	<-
L			20	4N						<(<+	
/	2344	2374	30	2D51QZMG	<<	P				<*<*	
L			10	4A						<+ <(	
/	2374	2408	33	2D51QZ,G	<<	P				<*<(	
L			12	4A						<* <-	
/	2408	2485	77	8A00PL	P*	P	CU	080		D.	
L			38	4G			CL	055		D.	
/	2485	2517	29	2D51QZ	<<	P				<(	
L			06	5A						<)<(<(	
/	2517	2536	23	2D51QZ	<<	P				<*<.	
L			13	4N						<)<* <)	
/	2536	2555	13	2D51QZ	<<	P				<(<.	
L			08	5N						<(<(<)	
/	2555	2575	21	2C41QZ		P				<(	<(
L			14	3N						<(	
/	2575	2596	20	2C51QZ		P				B(	
L			16	2N						<(	
/	2596	2631	31	2D51QZ		P				<(	
L			11	4A						<-<(<.	
/	2631	2647	16	8A00PL	P*	P				D.	
L			02	6A							
/	2647	2682	35	2D51QZ	<<	P				<*<.	
L			08	5N						<(<.	
/	2682	2717	35	2D41QZSZ		P			B.	<(	
L			13	4A						<(	
/	2717	2749	29	2D41QZSZ		P			B.	<(	
L			06	5N						<(	
/	2749	2827	75	8A00PL	P*	P	CU	055		D.	<(

```
L                    53        5G                          CL    068
/     2827   2857   28      2D510Z      <<          P                         <(     <-
L                    24        4N                                             <)   <-
/     2857   2887   30      2D510ZMG    <<          P                         <*        <(
L                    24        4N                                             <+
/     2887   2917   30      2D510ZMG    <<          P                         <*<.
L                    14        4N                                             <+   <+
/     2917   2947   30      2D510ZMG    <<          P                         <(
L                    23        4N                                             <+   <.
/     2947   2977   29      2D510ZMG    <<          P                         <(
L                    22        4N                                             <+   <(
/     2977   3007   30      2D510ZMG    <<          P                         <(        <(
L                    20        5N                                             <+   <-
/     3007   3037   30      2D510ZMG    <<          P                 <.      <*
L                    27        5N                                             <)
/     3037   3067   30      2D410Z      <<          P                         <(        <-
L                    20        5N                                             <+   <-
R                  :CONTAINS 0.35 M OF 8A00
/     3067   3097   29      2D410Z      BR          P                         <(<.      <-
L                    23        5N                                           <(<*   <.
R                  :HYDROTHERMAL ALTERATION PREFERENTIAL ALONG BRECCIATION
R                  :FRACTURES: CLAY GOUGE @ 309.5
/     3097   3124   26      2D510Z      BR          PP                        <(        <-
L                    20        5N                                           <(<*   <.
/     3124   3154   30      2D510Z      BR          P               <(      <(        <-
L                    28        5A                                           <(<(
/     3154   3184   27      2D510Z      BR          P                       <*<(      <-
L                    22        5A                                             <(   <-
/     3184   3214   30      2D510Z      BR          P                         <(        <-
L                    26        5A                                             <-   <(
/     3214   3236   21      2D510Z      BR          P                         <(
L                    15        5A                                             <-   <(
/     3236   3256   14      7C00PL                  P                         D.
L                    07        7V
R                  :FINER GRAINED THAN TYPICAL MONZONITE
/     3256   3292   36      8C00PL      P*          P                         D.
L                    15        8G
R                  :END OF HOLE
A001
ALAB               EQUITY MINESITE LABORATORY
ATYP               ASSAY
AMTH               WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM               RCOVSAMPLE   ROD % CU   G/TAG G/TAU % SB   % AS   % FE   % ZN
R        00     91 :TRICONED - NO CORE
R        91    188 :DYKE - NO SAMPLES
A001    188    213        1644        0.005    0.5 0.04  0.005 0.005 1.79  0.03
A001    213    244        1645        0.005    0.5 0.07  0.005 0.01  2.77  0.03
A001    244    267        1646        0.005    0.5 0.06  0.005 0.005 2.43  0.02
R       267    288 :DYKE - NO SAMPLES
A001    288    313        1647        0.005    4.0 0.11  0.005 0.02  4.80  0.14
A001    313    330        1648        0.005    4.0 0.04  0.005 0.005 2.83  0.05
R       330    348 :DYKE - NO SAMPLES
A001    348    384        1649        0.02    17.0 0.31  0.005 0.04  8.03  0.30
R       384    406 :DYKE - NO SAMPLES
A001    406    440        1650        0.005    3.0 0.10  0.005 0.01  3.55  0.03
```

A001	440	474		1651	0.001	4.0	0.11	0.005	0.02	4.00	0.03
A001	474	507		1652	0.005	20.0	0.44	0.005	0.005	5.59	0.18
R	507	514	:DYKE - NO SAMPLES								
A001	514	539		1653	0.03	22.0	0.33	0.005	0.005	3.61	0.06
A001	539	560		1654	0.03	20.0	0.50	0.03	0.20	29.10	0.29
A001	560	589		1655	0.005	12.0	1.55	0.03	0.00521.10		0.03
A001	589	615		1656	0.005	6.0	0.10	0.005	0.001	2.69	0.005
A001	615	645		1657	0.005	8.0	0.37	0.005	0.001	3.36	0.02
A001	645	675		1658	0.005	3.0	0.19	0.005	0.001	4.69	0.005
A001	675	705		1659	0.005	2.0	0.04	0.005	0.001	3.41	0.02
A001	705	731		1660	0.005	2.0	0.13	0.005	0.001	4.64	0.02
A001	731	765		1661	0.005	2.0	0.06	0.005	0.001	3.15	0.02
A001	765	785		1662	0.005	0.5	0.01	0.005	0.001	2.04	0.03
A001	785	817		1663	0.005	4.0	0.02	0.005	0.001	2.20	0.19
A001	817	847		1664	0.005	0.5	0.02	0.005	0.001	1.57	0.02
A001	847	877		1665	0.005	2.0	0.03	0.005	0.001	2.36	0.02
A001	877	898		1666	0.005	0.5	0.02	0.005	0.005	1.41	0.01
A001	898	926		1667	0.005	0.5	0.09	0.005	0.005	1.93	0.03
A001	926	959		1668	0.01	1.0	0.14	0.005	0.005	2.10	0.01
A001	959	980		1669	0.005	0.5	0.11	0.005	0.005	1.41	0.01
A001	980	1010		1670	0.005	0.5	0.09	0.005	0.005	2.03	0.005
A001	1010	1040		1671	0.005	0.5	0.03	0.005	0.005	1.75	0.005
A001	1040	1070		1672	0.005	0.5	0.13	0.005	0.01	1.90	0.005
A001	1070	1100		1673	0.005	0.5	0.04	0.005	0.02	1.79	0.005
A001	1100	1130		1674	0.005	2.0	0.03	0.005	0.005	2.19	0.02
A001	1130	1160		1675	0.005	2.0	0.03	0.005	0.001	2.74	0.005
A001	1160	1189		1676	0.005	0.5	0.02	0.005	0.001	2.10	0.005
R	1189	1201	:DYKE - NO SAMPLES								
A001	1201	1223		1677	0.005	0.5	0.03	0.005	0.001	2.33	0.03
R	1223	1266	:DYKE - NO SAMPLES								
A001	1266	1293		1678	0.005	0.5	0.47	0.005	0.001	1.50	0.005
A001	1293	1310		1679	0.005	3.0	0.87	0.005	0.005	1.72	0.005
A001	1310	1322		1761	0.005	0.5	0.05	0.005	0.005	1.66	0.005
R	1322	1334	:DYKE - NO SAMPLES								
A001	1334	1355		1762	0.005	0.5	0.07	0.005	0.005	1.49	0.005
A001	1355	1374		1763	0.005	2.0	0.03	0.005	0.005	1.85	0.005
R	1374	1469	:DYKE - NO SAMPLES								
A001	1469	1500		1764	0.10	39.0	0.21	0.005	0.04	5.48	0.02
A001	1500	1529		1765	0.06	23.0	0.19	0.005	0.03	2.73	0.04
A001	1529	1552		1766	0.06	81.0	0.59	0.02	0.04	4.36	0.03
A001	1552	1576		1767	0.11	43.0	0.55	0.02	0.005	4.12	0.06
A001	1576	1591		1768	0.10	26.0	0.23	0.005	0.005	3.22	0.03
A001	1591	1620		1769	0.06	7.0	0.21	0.005	0.005	2.56	0.08
R	1620	1764	:DYKE - NO SAMPLES								
A001	1764	1786		1770	0.07	10.0	0.11	0.005	0.03	3.69	0.03
A001	1786	1812		1771	0.08	12.0	0.21	0.005	0.02	3.15	0.02
A001	1812	1842		1772	0.34	10.0	0.34	0.005	0.09	3.75	0.04
A001	1842	1872		1773	0.17	13.0	0.31	0.005	0.02	3.29	0.02
A001	1872	1902		1774	0.08	19.0	0.66	0.02	0.005	2.76	0.02
A001	1902	1932		1775	0.19	15.0	0.02	0.02	0.07	3.19	0.03
A001	1932	1962		1776	0.18	14.0	0.41	0.03	0.24	7.35	0.06
A001	1962	1997		1777	0.02	5.0	0.12	0.01	0.005	3.40	0.03
A001	1997	2032		1778	0.18	11.0	0.31	0.03	0.01	5.70	0.04
A001	2032	2059		1771	0.80	13.0	0.36	0.02	0.01	6.60	0.08
A001	2059	2086		1780	1.07	15.0	0.46	0.04	0.01	5.60	0.15



120° 5
LUCKY BEN
2427 (1)
LUCKY BEN 2
2794 (5)
N
4
93L/1W
1:50000
Foxy Cr.
ALSO
XL-1
872(11)
JOHN 1
3269(9)
JOHN 2
3270(9)
ALSO
SAM 2
3366(11)
SAM
2459(2)
MINING
L.5056-67
LEASE
L.5087-90
NO. 1
MINING
LEASE
NO. 6
LOT
1439
TET 1
6073(3)
TET 2
6074(3)
TET 3
6075(3)
TET 4
6076(3)
GOOD
7547(4)
NEWS
7546 (4)
COLLEEN
6078(3)
FEB
6080 (3)
MAX 1
7090
(6)
DINA 3
2483 (2)
6
5
4