87-655-16299
8/88

GEOLOGICAL, GEOPHYSICAL AND GEOCHEMICAL REPORT

ON THE

SADDLE-SHAKTI PROPERTY

FOR

Operator: WINSPEAR RESOURCES LTD.

Owner(s): M. Romero, G. Sinitsin, C. Baldys

SKEENA MINING DIVISION
BRITISH COLUMBIA

NTS 103P 12W
NORTH LATITUDE: 55° 37' ~~30"~~ 12"
WEST LONGITUDE: 129° ~~37' 30"~~ 50'42"

BY

FRANK DI SPIRITO, B.A.SC., P.ENG.
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J.C. GRAHAM, B.SC., M.ENG.
SHANGRI-LA MINERALS LIMITED

29 SEPTEMBER, 1987

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SUMMARY

At the request of Winspear Resources Ltd., a first phase exploration program was completed on the Saddle-Shakti claim group by Shangri-La Minerals Limited. The program was performed during July and August of 1987, and included geological, geochemical and geophysical surveys and blasting to open previous workings, and a mineralogical analysis. The purpose of the program was to define targets with potential for economic gold/silver mineralization.

The Saddle-Shakti claim group comprises 100 units, these being 5 located 4-post mineral claims and 8 Reverted Crown Granted mineral claims. The claim group is located in the Skeena Mining Division approximately 40 km southeast of Stewart, B.C., at the head of Hastings Arm. Access to the property is by helicopter from Stewart. A tramway (some traces of which can still be seen) was built from the Saddle Group workings on the Saddle-Shakti property to Hastings Arm to provide access to deep-sea shipping.

The Saddle-Shakti claim group lies near the Stewart Mining Camp, which has been prospected since the early 1900's. The Saddle-Shakti claim group includes two significant showings, one of which is a former producing property known as the Saddle Group. Underground development work and trenching on two well mineralized quartz veins was done on the Saddle Group during the late 1920's and early 1930's, and a small amount of high grade ore was shipped.

The second significant showing within the Saddle-Shakti claim group is at the Elkhorn Group workings, where "spectacular finely divided gold in streaks 1/4 to 1 inch wide..." was reported in 1929. The present program did not investigate the Elkhorn Group showing because of the steep topography there.

A preliminary evaluation of the property covered by the Saddle-Shakti claim group was conducted by Shangri-La Minerals Limited in September of 1986. Samples taken during 1986 from the Saddle Group vein system returned encouraging gold and silver values (from trace values to 0.296 oz/ton Au and 29.74 oz/ton Ag, and up to 42.40% Pb, 12.67% Zn). These results prompted the present exploration program.

The present exploration program was concentrated on the old Saddle Group workings. Encouraging geological, geochemical and geophysical results were obtained. Assays of channel and rock chip samples returned encouraging gold and silver values (from trace values to 0.322 oz/ton Au and 9.29 oz/ton Ag). As well, ground VLF-EM and soil geochemical results indicate a possible extension of the vein system to the northeast of the exposed mineralization. Mineralogical analysis shows the gold is 90% free milling at -1 mm, allowing easy recovery.

The geology of the Saddle-Shakti claim group is conducive to high-grade, low tonnage gold/silver mineralization. A second phase of exploration consisting of trenching and an induced polarization survey over the Saddle Group vein system is recommended in order to investigate the geometry and grade of the mineralization and to delineate additional targets. As well, the area of the old Elkhorn Group workings should be systematically sampled by a geologist skilled in technical climbing methods. The estimated cost of the proposed second phase program is $70,000.

Contingent upon favourable results from the recommended program, further work consisting of diamond drilling and additional trenching will be necessary in order to more fully evaluate the economic potential of the Saddle-Shakti property.

Signed at Vancouver, B.C.

PROFESSIONAL ENGINEER PROVINCE OF F. DISPIRITO BRITISH COLUMBIA

F. DiSpirito, B.A.Sc., P.Eng.
September 29, 1987

PART A

Introduction

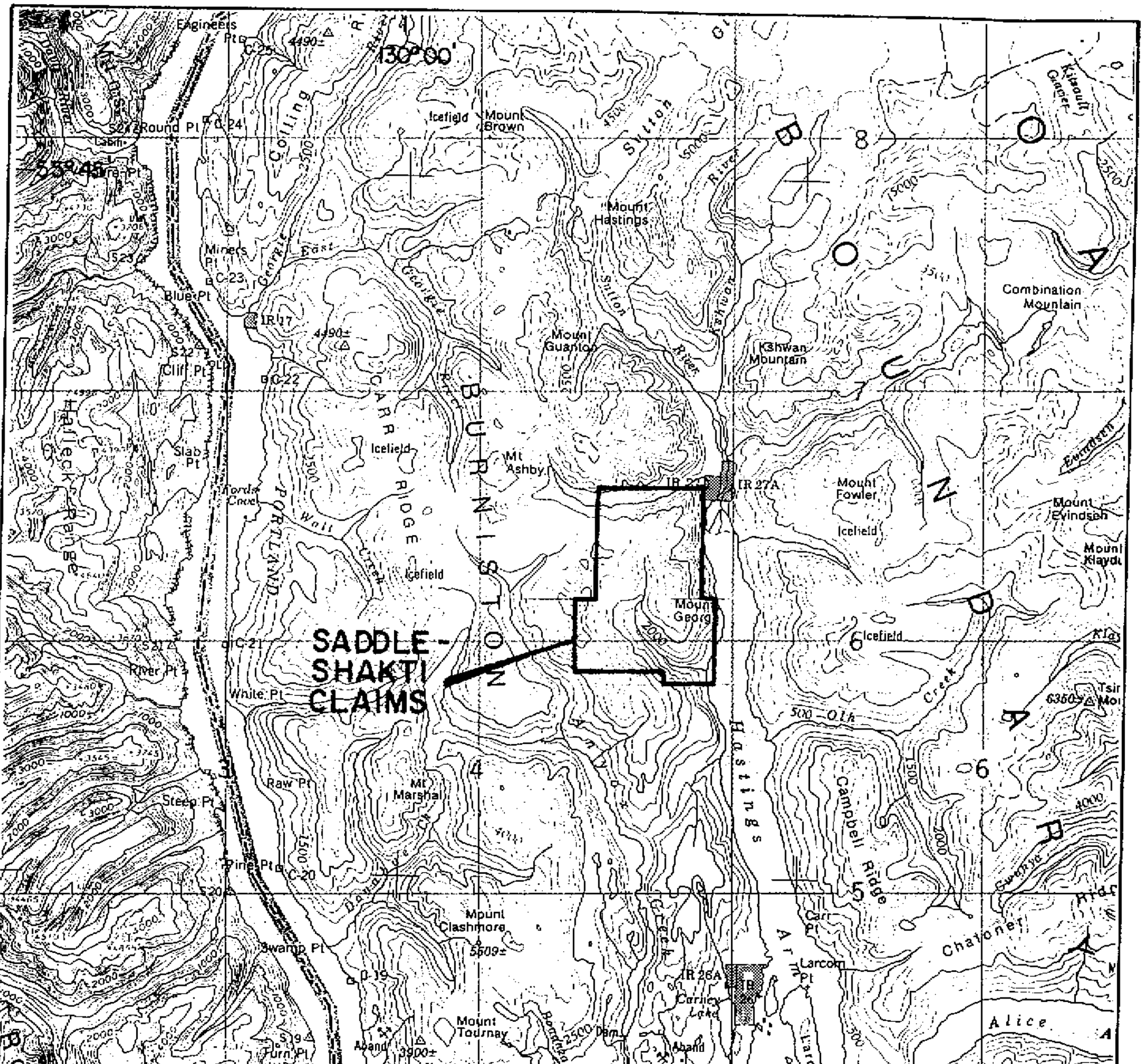
On July 3 and 4, and from August 10 to August 20, 1987, Shangri-La Minerals Limited conducted a first phase exploration program on the Saddle-Shakti property with the object of defining targets with potential for precious metal deposition. The program consisted of grid establishment, geological mapping, and geochemical, airborne and ground geophysical surveys, and a mineralogical analysis. The exploration program was undertaken for Winspear Resources Ltd.

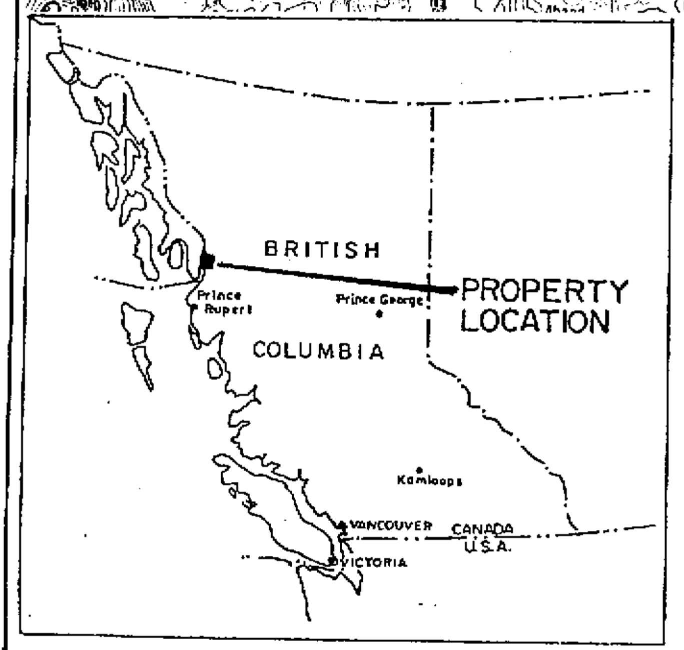
Location and Access

The Saddle-Shakti Claim group is located approximately 40 km southeast of Stewart, B.C., in the Skeena Mining Division, at N 55° 37' 30", W 129° 37' 30". Stewart is approximately 800 km north of Vancouver, lying near the B.C.-Alaska border. The claim area overlies Mt. George, which rises very steeply some 1,500 m from Hastings Arm. The NTS map sheet which covers the area is 103P 12W.

Stewart is served by scheduled air service from Terrace. From Stewart the property is reached by helicopter. Access may also be gained by boat from the community of Alice Arm (the location of the Kitsault Mine) up to the head of Hastings Arm. A steep trail rises from sea level to the Saddle Group workings on the property.

In the late 1920's, a tramway (some traces of which can still be seen) was built from the Saddle Group workings on the Saddle-Shakti property to Hastings Arm to provide access to deep-sea shipping.





SCALE 1:250,000

0 5 10 15 Km.

To accompany report by F. Di Spirito B.A.Sc., P.Eng.

SADDLE-SHAKTI CLAIMS

FOR: WINSPEAR RESOURCES LTD.

BY: SHANGRI-LA MINERALS LIMITED

LOCATION MAP

SKEENA M.D., B.C.

N.T.S. 103P-12W	DATE: SEPT. 1987
DRAWN BY: D.K.	FIGURE Nº. 1

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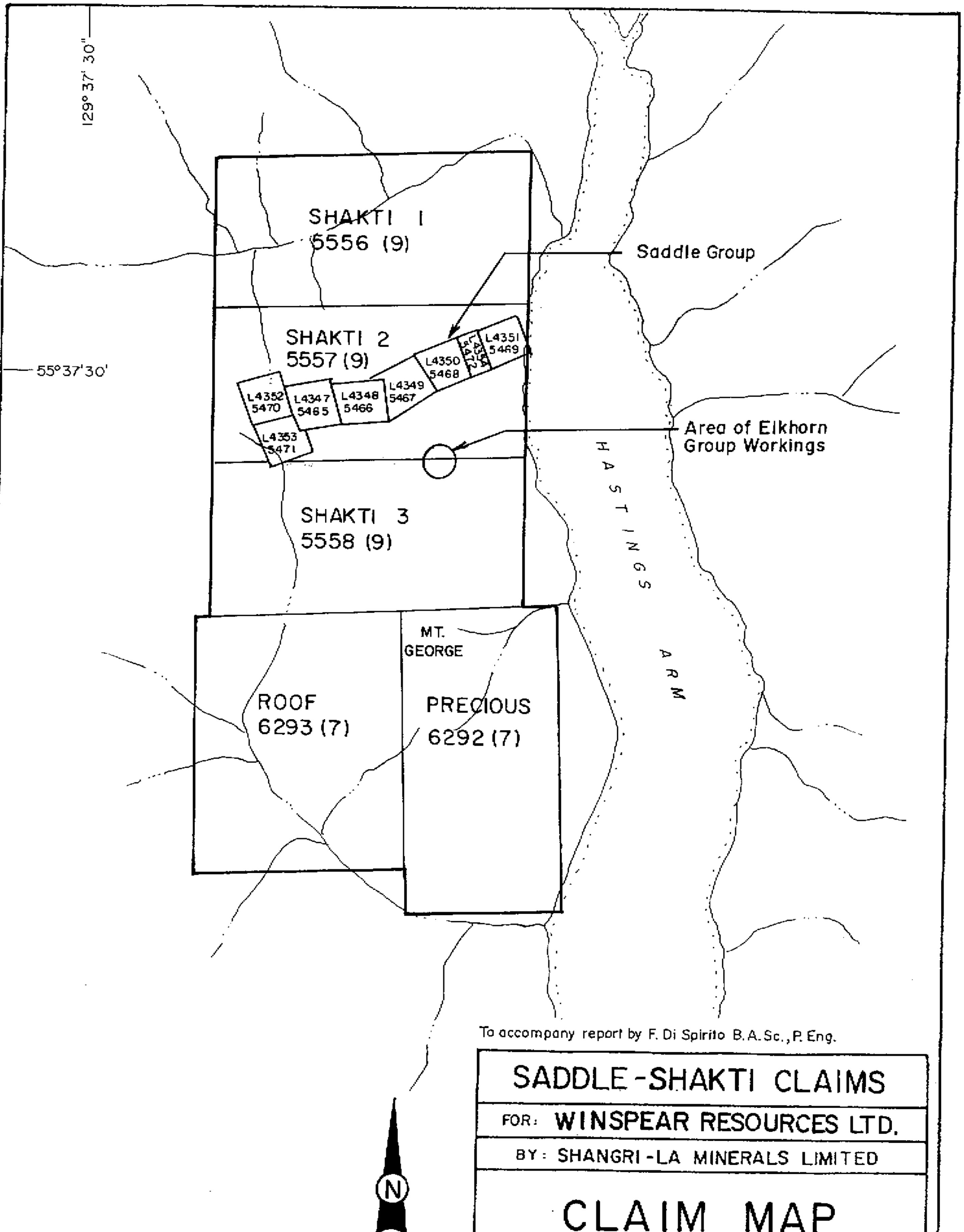
Property Status

The Saddle-Shakti claim group consists of 5 located mineral claims and 8 Reverted Crown Granted Mineral Claims in the Skeena Mining Division of British Columbia (Fig. 2). The claims are shown on the Department of Mines Mineral Claim Map 103P 12W. The claims are optioned to Winspear Resources Ltd.

NAME	REC. NO.	AREA (UNITS)	EXPIRY dd/mm/yr	OWNERS 70%	OWNERS 30%
SADDLE (L.4347)	5465	1	01/08/92	Sinitsin, G.	Baldys, C.
SADDLE No.1(L.4348)	5466	1	01/08/92	Sinitsin, G.	Baldys, C.
SADDLE No.2(L.4349)	5467	1	01/08/92	Sinitsin, G.	Baldys, C.
SADDLE No.3(L.4350)	5468	1	01/08/92	Sinitsin, G.	Baldys, C.
SADDLE No.4(L.4351)	5469	1	01/08/92	Sinitsin, G.	Baldys, C.
SADDLE No.5(L.4352)	5470	1	01/08/92	Sinitsin, G.	Baldys, C.
SADDLE No.6(L.4353)	5471	1	01/08/92	Sinitsin, G.	Baldys, C.
SADDLE Fr. (L.4354)	5472	1	01/08/92	Sinitsin, G.	Baldys, C.
SHAKTI No. 1	5556	18	10/09/91	Sinitsin, G.	Baldys, C.
No. 2	5557	18	10/09/92	Sinitsin, G.	Baldys, C.
No. 3	5558	18	10/09/92	Sinitsin, G.	Baldys, C.
PRECIOUS	6292	18	24/07/92	100% - Romero, M.	
ROOF	6293	20	24/07/92	100% - Romero, M.	

Physiography

The Saddle-Shakti claim group lies at the end of Hastings Arm on its western shoreline, along the eastern edge of the Burniston Range of the Coast Mountain System. Elevations on the property range from sea level to approximately 1,500 m at the summit of Mt. George. Most of the property is heavily forested and very steep, requiring technical climbing skills. Above 1,000 m much of the property continues to be steep but the vegetation becomes less dense and eventually gives way to an



To accompany report by F. Di Spirito B.A.Sc., P. Eng.

SADDLE-SHAKTI CLAIMS

FOR: **WINSPEAR RESOURCES LTD.**

BY: SHANGRI-LA MINERALS LIMITED

CLAIM MAP

SKEENA M.D., B.C.

N.T.S. 103P - 12W	DATE: SEPT. 1987
DRAWN BY: D.K.	FIGURE Nº. 2

SCALE 1:50,000

0 1 2 KM.

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alpine type environment. The summit of Mt. George and the unnamed summit immediately to the north are easily traversed.

Outcrop exposure is abundant in both the alpine and the precipitous lower elevations. There are several deep cut valleys which appear to represent large geological structures. Water is abundant on the project as snow rarely leaves the upper elevations on the north facing slopes. Armitage Creek flows southeasterly into Hastings Arm and represents an abundant supply of water.

The location of the Saddle-Shakti property with its proximity to the northern B.C./Alaska coast creates an unstable climate during the summer months and a harsh cold climate during the winter months. Snow is not uncommon during the short summers at this latitude.

History

As well as being one of British Columbia's oldest mining camps, the Stewart area has also been one of the largest producers of gold and silver in the province. Prospectors first came to the area during the Klondike gold rush in anticipation of recovering placer gold from the local creeks and rivers. Disappointing returns lead the prospectors to exploit the more obvious lode deposits. Several major producers including the Premier, Silbak Premier, Big Missouri, Dunwell, Indian, Scottie, and Prosperity and Porter Idaho Mines are located in the Stewart camp. The Premier and Silbak Premier Mines alone produced nearly 2 million ounces of gold, 41 million ounces of silver, 4 million pounds of copper, 60 million pounds of lead and 16 million pounds of zinc. The Premier and Silbak Premier mines and mill are currently being reopened and redeveloped by Westmin Resources Ltd.

There are 2 old claim groups included within the present Saddle-Shakti claim group. These are the Saddle Group and the Elkhorn Group.

The Saddle Group workings were developed during the 1920's by Silver Crest Mines Ltd. They sank three shafts and drove a 140 m adit. In 1928 an aerial tramway was constructed from the head of Hastings Arm to the adit entrance. In 1929 three tons of ore (yielding 84 oz silver, 44 kg copper and 1,436 kg lead) were shipped. Work was continued on the Saddle Group between 1934 and 1936 by the Saddle Mining Syndicate. In 1982 Norcon Exploration Ltd. of Vancouver acquired the property and carried out a surface mapping and sampling program. A preliminary evaluation of the property was conducted by Shangri-La Minerals in September of 1986. Encouraging assay results from the Saddle Group vein system (the 1986 assay results are included in Appendix D, and include gold and silver values from trace to 0.296 oz/ton and 29.74 oz/ton, respectively, and up to 42.40% Pb, 12.67% Zn) prompted the exploration program which is the subject of this report.

The Elkhorn Group showing was first discovered in 1929. Referring to the Elkhorn Group, the 1929 BCDM Annual Report states: "Spectacular finely divided gold in streaks 1/4 to 1 inch wide have been found in isolated patches. A sample taken from the small cut on this showing, and carefully scrutinized to avoid the presence of free gold, for the purpose of determining whether the sulphides carried gold, assayed: Gold, 0.16 oz. to the ton; silver, 0.5 oz. to the ton." No production is reported from the Elkhorn Group.

PART B SURVEY SPECIFICATIONS

Airborne VLF-EM and Magnetometer Survey Specifications

The survey system equipment simultaneously monitors and records the output signals from a proton precession magnetometer and two VLF-EM receivers installed in a bird which is towed over the survey area at an altitude of approximately 75 m by helicopter. The average flying speed while surveying is about 110 km/hr. Landmarks along the flight lines are plotted on aerial photographs as the lines are flown. This allows subsequent production of a flight line map on which to plot the survey results.

The two VLF-EM receivers respond to signals from two different transmitters - one near Seattle, Washington and one near Annapolis, Maryland. Conductors respond most strongly to the transmitter in the direction of their strike.

The three channels of geophysical data and one navigational marker channel are each digitized at a sample rate of approximately once every 1.6 seconds (resulting in a station spacing of approximately 50 m) using an 8 channel analog-to-digital converter. The data is then recorded digitally on one channel of a stereo cassette tape recorder, while the other channel records the operators' voice descriptions of landmarks, line identification, and other details. As well, the data is displayed on the screen of a TRS-80 Model 100 lap computer as it is recorded. Instrument specifications are detailed in Appendix G.

The flight lines run north-south. The line spacing is roughly 150 m. A total of 145 line-km was surveyed.

Control Grid Establishment

A single control grid with a 1.2 km baseline was established over a portion of the Saddle-Shakti claim group. A total of 11.1 km of grid was chained and flagged, with station locations every 12.5 m (slope corrected). The grid lines were established at intervals of 50 m.

Geological Mapping

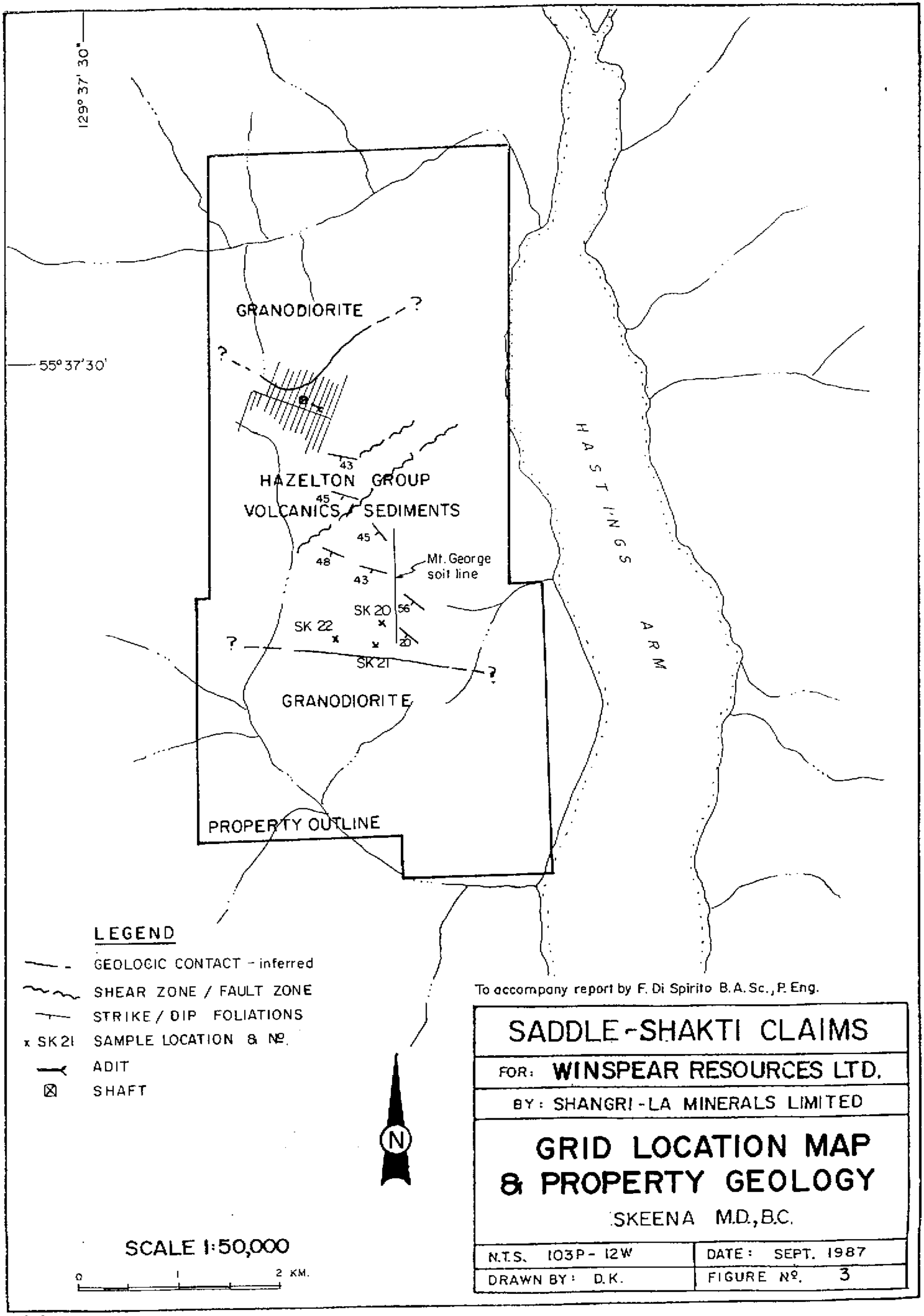
Detailed geological mapping at 1:2,500 scale was conducted on the grid. Reconnaissance traverses were conducted over Mt. George and other areas that were accessible.

Rock and Soil Geochemical Surveys

A total of 69 rock samples and 342 soil samples were collected. Rock chip, grab, float and channel samples were collected from areas where signs of mineralization, alteration, and/or leaching were observed. The adit and shaft uncovered by blasting were systematically sampled. Rock sample descriptions are found in the discussion of results and in Appendix C. Analytical results (including the 1986 assay results) are presented in Appendix D. The soil geochemical results were statistically analysed, and the results are presented in Appendix E.

Mineralogical Analysis

One mineralized hand specimen was analysed by Orex Laboratories in order to quantify the ore minerals present and to establish the paragenetic relationships among the ore minerals. The analysis and results are presented as Appendix F.


129° 37' 30"
55° 37' 30'
GRANODIORITE
HAZELTON GROUP
VOLCANICS / SEDIMENTS
Mt. George
soil line
SK 20
SK 22
SK 21
GRANODIORITE
PROPERTY OUTLINE
HASTINGS ARM
LEGEND
GEOLOGIC CONTACT - inferred
SHEAR ZONE / FAULT ZONE
STRIKE / DIP FOLIATIONS
x SK 21 SAMPLE LOCATION & №.
ADIT
SHAFT
N
SCALE 1:50,000
0 1 2 KM.
To accompany report by F. Di Spirito B.A.Sc., P. Eng.
SADDLE-SHAKTI CLAIMS
FOR: WINSPEAR RESOURCES LTD.
BY: SHANGRI-LA MINERALS LIMITED
GRID LOCATION MAP
& PROPERTY GEOLOGY
SKEENA M.D., B.C.
N.T.S. 103P - 12W
DATE: SEPT. 1987
DRAWN BY: D.K.
FIGURE №. 3

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Ground VLF-EM Survey Method

The ground very low frequency electromagnetic (VLF-EM) survey was conducted using a Sabre Electronics Model 27 VLF Electromagnetometer. This instrument acts as a receiver only. It utilizes the primary electromagnetic fields generated by United States Navy VLF marine communication stations. These stations operate at frequencies between 15 and 25 kHz, and have a vertical antenna current resulting in a horizontal primary magnetic field.

Secondary magnetic fields arise due to currents induced in conductors. The VLF-EM instrument measures the dip of the magnetic field resulting from the sum of the primary and secondary fields. For maximum coupling, a transmitter station located in the direction of the geological strike and/or the strike of possible conductors is selected. At the Saddle-Shakti project area the transmitter located at Annapolis, Maryland was used.

Readings were taken at 12.5 m intervals along grid lines. The data was filtered as described by D. C. Fraser, Geophysics, Vol. 34, No. 6. This is essentially an averaging and differentiation filter technique applied to remove "DC" bias and attenuate long spatial wavelengths to increase resolution of local anomalies. VLF-EM conductors appear as positive values. A total of 9.9 line-km was surveyed.

PART C GEOLOGY

Regional Geology

The Stewart camp lies adjacent to the east margin of the Coast Crystalline Belt near the northern end of the Stewart complex, a deformed belt of volcanic, sedimentary and metamorphic rocks which lies along the west edge of the Bowser Basin. The complex, which extends from Alice Arm on the south to the Iskut River on the north, includes major northerly trending structures which are complicated by complex plutonism. Regionally, the Stewart complex dips east under the Bowser sediments. The western contact of the Stewart complex is largely delineated by the contact of the Coast Crystalline Belt, while the eastern limits are masked by the overlying Bowser Assemblage.

Gold, silver, copper, lead and zinc have all been economically exploited in the area. Most of this mineralization has been hosted by the Stewart Complex. As a result, the importance of knowledge of the complex's geology and its association with the other assemblages cannot be overemphasized.

Property Geology

Lithologies - Stewart Complex

Although the volcanic and sedimentary rocks of the Saddle-Shakti property are considered to be part of the Stewart complex, they have never been assigned to a particular member of the formation. However lithologic similarities appear to indicate it is part of the Hazelton assemblage.

The Hazelton assemblage is the most prominent as well as the most important unit on the property, for it is the host rock for the mineralization. The group consists of three distinct lithologic units which form a roof pendant which outcrops over an area approximately 7 km by 4 km. The pendant has been intruded and altered by intrusives of the Coast Crystalline Belt. Massive and schistose, aphanitic, dark grey andesites dominate the surface exposure of the rock pendant. Locally well-formed plagioclase phenocrysts give the andesite a porphyritic texture and indicate a differential cooling for the extrusive. Aphanitic, green, welded tuff fragments of variable size are often found embedded in the andesite.

Also prominent on the property is a sequence of bedded or layered rocks which appear to have a sedimentary origin. Closer observation, however, indicates that this feature is actually metamorphic banding which can be easily misconstrued as relict bedding. These banded rocks are welded tuffs and clastic volcanics of andesite composition. Locally these banded tuffs and clastic volcanics have a foliated appearance and are marked by a submetallic greyish to greenish aspect in addition to the primary rock color. The foliation is variably developed, depending on the spatial proximity to the intrusive contacts and zones of shearing.

A well defined intermediate zone characterized by chloritic schists, minor ultramafics and xenoliths of andesitic composition, exists between the volcanic/intrusive contact. Many of these xenoliths are 25 m or more in diameter. The Hazelton formation is considered to be of Triassic age.

Lithologies - Intrusives

The intrusive body which encompasses the andesite roof pendant on the property varies in composition from diorite to granodiorite. The unit is generally coarse grained with well developed potassium feldspar, hornblende, pyroxene, biotite and quartz crystals in a plagioclase matrix. As mentioned earlier, the granodiorite often possesses xenoliths of altered andesite near the margin of the intrusive and the volcanics. Several later stage dykes cut the andesites of the Hazelton assemblage. A large quartz monzonite dyke over 75 m wide and several hundred m long, striking to the southeast, cuts the volcanics in the western portion of the grid. Numerous smaller dykes are found on the property. Most of these later phase intrusives are granodiorite to quartz diorite in composition, however fine grain, grey to brown lamprophyre dykes are also common. In the flat-lying banded clastic volcanics, the intrusive is often sill-like, lying along bedding or banding planes. The intrusive is considered to be Eocene in age.

Structure

The andesites and clastic volcanics which outcrop on the Saddle-Shakti property from a roof pendant approximately 7 km long and 4 km wide, in a mass of plutonic rocks associated with the Coast Crystalline Belt. The presumed sequence of events began with volcanic activity and the subsequent deposition of the andesites and tuffs. Erosional processes during this time lead to the formation of the clastic volcanics of andesitic composition. Intrusion of the Coastal Batholith followed during the Eocene. Several strata-cutting granitic dykes were emplaced at this time. Fracturing, shearing and folding accompanied by volcanic activity occurred during the Tertiary. The latest structural feature was the emplacement of quartz fissure veins and massive sulphide vein deposits which host the sulphide mineralization on the property.

Foliation and tight recumbent folding in the Hazelton rocks appears to be associated with plutonism in the region. Recrystallization by metasomatic processes has produced schists in these locations. The intrusion of the Coastal Batholith, however, does not appear to have a very close genetic relationship with the mineralization on the property. Numerous small dykes and sills are found near the contact of the volcanics and intrusives and in the vicinity of the showings.

The sills are intruded along "bedding planes" in the altered clastic volcanics and tuffs, apparent planes of weakness in the unit.

Regional metamorphic processes associated with the greenschist facies have affected isolated areas on the property. As well, contact metamorphic effects associated with the hornfels facies were reached along much of the exposed contacts.

Several creek valleys found on the Saddle-Shakti property represent fault zones. Three faults strike to the northeast while one strikes to the north. The north striking fault (which forms the Armitage Creek Valley) offsets a siliceous aplite dyke by approximately 50 m.

The fissures containing the mineralized quartz veins dip steeply to the southwest. This is consistent with the general trends of the banding and schistosity on the property.

Alteration and Mineralization

Elkhorn Group Showings

The Elkhorn Group showings are described in the 1929 BCDM Annual Report. The showing is of spectacular finely divided gold in streaks 1/4 to 1 inch wide which "occurs in a silicified zone carrying epidote and garnet in altered andesite and mica-schist, mineralized with fine-grained pyrite, pyrrhotite, some galena and zinc blende [i.e., sphalerite]. A small cut shows the zone to be about 3 1/2 feet wide, striking N. 45° W. (mag.) and dipping steeply into the abrupt mountain-slope."

Saddle Group Showings

The Saddle Group mineralization does not appear to share a close genetic relationship with the bulk mass of the Coastal Intrusive Complex. It does, however, seem to be associated with some smaller, later phase dyke and sill structures which were responsible for the circulating hydrothermally generated fluids. The mineralization occurs primarily in veins along fractures and fissures in a gangue of quartz. The vein deposits are clearly epigenetic.

The mineralization consists mostly of pyrite, galena, sphalerite and chalcopyrite with minor pyrrhotite. The mineralogical analysis (Appendix F) shows that the sequence (from earliest to latest) of deposition of the hypogene minerals is pyrite, chalcopyrite, sphalerite, galena, quartz(?), and finally(?) gold. The gold is 90% free at -1 mm, 10% inclusions in pyrite.

The geology and mineral assemblage of the showings implies that the deposit is a volcanic-associated vein and shear zone hydrothermal system. The precious metals and associated elements were probably scavenged from larger volumes of rocks by circulating hydrothermal fluids and deposited in fractures, faults and shear zones in the host rock.

Two sulphide rich veins (each greater than 50 m in length and between 0.3 and 1.2 m thick) comprise the main showings on the Saddle Group. The sulphides occupy the inner part of the veins as discontinuous lenses, pockets and streaks up to 0.6 m thick. The andesite wall rock also carries appreciable amounts of sulphide mineralization near the showings.

Silicification and chloritization has affected the country rock in varying degrees near the contact. Secondary mineralization of the sulphide laden veins, in the zone of oxidation, has produced cerussite (lead carbonate), smithsonite (zinc carbonate) and anglesite (lead sulphate).

The southeastern extension of the main vein is marked by a system of fractures, minor quartz vein and stringers accompanied by propylitic and chloritic alteration. A 195 m adit was drifted in this zone. Systematic sampling by this author failed to identify any particularly well mineralized zones within the adit.

A minor skarn showing was found near the summit of Mt. George. Well formed garnets and epidote crystals are found in the zone but no sulphide mineralization was seen.

PART D DISCUSSION OF GEOPHYSICAL RESULTS

Airborne Survey

The airborne magnetometer survey provides an effective method of reconnaissance mapping of lithology for rock types with differing magnetic mineral concentrations. Under favourable circumstances, small-scale features such as dykes and magnetic mineral deposits can be detected.

Airborne VLF-EM data are mainly used for the interpretation of large-scale geological features such as faults and conductive rock units, although under favourable circumstances smaller conductors (such as massive sulphide deposits) may be revealed. VLF-EM surveys are a cost-effective complement to airborne magnetic data. The airborne survey was undertaken primarily in order to delineate the extent of the roof pendant, which is relatively magnetic.

Airborne Magnetometer Survey

The results of the magnetic survey are presented in Fig. 6a, and the inferred extent of the roof pendant is indicated in that figure. Ground geological examination indicates that the actual extent of the roof pendant is probably greater than magnetically inferred.

Airborne VLF-EM Survey

The airborne VLF-EM results are presented in Figs. 6b and 6c. The results are dominated by topographic effects. Induced electrical currents are concentrated in topographic highs, which causes an increase in the measured field strength. The airborne VLF-EM method lacked the necessary spatial resolution to detect the mineralized zones on the Saddle property. The ground VLF-EM survey (discussed below) was apparently more successful.

Ground VLF-EM Survey

The ground VLF-EM survey results are presented in Fig. 7. The entire grid area is fairly conductive, probably because of the topographic structure of the property, and as well there are four localized anomalies. The two very strong anomalies in the eastern part of the grid are due to the presence of tramway cables.

The VLF-EM conductors which are thought to be significant are shown on the Compilation Map, Fig. 9. The conductors in the region of the showings are probably due to the exposed mineralization, and the one just north of the baseline on line 5+50E may be related to mineralization at depth. There is a weak VLF-EM conductor trending to the northeast from the exposed surface showings which may indicate an extension of the vein system. This inference is supported by the fact that the conductor leads to a geochemically anomalous zone.

PART E DISCUSSION OF GEOCHEMICAL RESULTS

Rock Geochemistry

A total of 69 rock samples were analysed by 30 element ICP analysis and atomic absorption for gold content at Acme Analytical Laboratories of Vancouver. Of the 69, 19 samples were also fire assayed for more accurate gold and silver values.

The best rock geochemical results were received from the showings and adit on the property. The mineralization, massive in much of the vein structure, consists mostly of pyrite, galena, sphalerite and chalcopyrite. Figures 4 and 5 show gold and silver assays from channel and rock chip samples from the adit and area of the showings.

Three samples assayed greater than 0.17 oz/ton gold (SK04 - 0.322 oz/ton Au; SK08 - 0.239 oz/ton Au; SK14 - 0.178 oz/ton Au). As well, 14 samples assayed greater than 1.00 oz/ton silver. Of these, three samples assayed greater than 6.00 oz/ton silver (SK04 - 6.71 oz/ton Ag; SK15 - 9.29 oz/ton Ag; SK35 - 8.57 oz/ton Ag).

Soil Geochemistry

The control grid lies in an area almost devoid of soil. The soils are almost all colluvial, and occur in small pockets on bedrock under the heather alpine tundra. The organic content of these soils is low, making them highly reliable indicators of bedrock mineralization.

On the upper part of the grid the erosional products were usually washed 2 to 3 m to settle in small pockets and accumulate. On the lower parts of the grid the soil is accumulating directly on the parent rock or falling to talus piles. It is thought that the rare alluvial soil sample has not moved much more than 20 m.

A total of 342 soil samples were collected and analysed by ICP for a 30 element suite, and atomic absorption for gold. The analyses were done by Acme Analytical Laboratories of Vancouver. The values for six separate pathfinder and indicator elements were plotted and contoured in order to establish geochemical trends.

A simple statistical analysis was performed on the geochemical data to isolate anomalous zones with a degree of probability. The anomaly threshold value for an element was taken to be its mean value plus two standard deviations. Appendix E lists all anomalous pathfinder and indicator elements, their maximum and minimum values, their mean, median and standard deviations.

A zone approximately 150x300 m between lines 500 and 800 E between stations 75 N and 225 N contains anomalous values for each of the pathfinder and indicator elements. This is the zone within which the mineralized quartz veins are exposed, and the anomalous soil values are undoubtedly due to weathering of the veins.

The anomalous zone has gold values ranging from 73 to 195 ppb (threshold value Au = 49 ppb) with the greatest gold value (195 ppb) being found at station 800 E/175 N. Anomalous silver values are also concentrated in the region. Values from 2.0 to 6.5 ppm silver are found in the zone (threshold value Ag = 1.6 ppm).

Anomalous values for the pathfinder elements arsenic, antimony, lead, zinc and copper are also found in the zone.

These moderately impressive values, coupled with the localized VLF-EM anomaly discussed above, suggest that the area warrants further subsurface investigation to isolate any portion of the vein system that may not outcrop. In an attempt to isolate new anomalies, a single soil line, consisting of 46 samples, was collected along the ridge on Mt. George. Values were generally low for both indicator and pathfinder elements and no geochemical trends could be established.

PART F DISCUSSION OF RESULTS

Correlation of the geological, geophysical and geochemical results obtained indicates at least 2 zones of interest on the grid area covering the Saddle Group workings. The most promising zone is associated with the adit and exposed vein system covered by the grid. VLF-EM and soil geochemical results indicates that the anomaly extends from approximately 80 N to 210 N concentrating near line 550 E. Several values for indicator and pathfinder elements are considered anomalous in this area.

Geochemical anomalies also exist along line 700 E between station 225 N and 300 N and between lines 700 E and 800 E and stations 150 N and 200 N. Values are high for both pathfinder and indicator elements. There is a weak VLF-EM conductor which leads from the main showings to this geochemically anomalous zone, suggesting the possibility of a vein extension. Further investigation is warranted.

Several spot soil geochemical anomalies also exist on the grid. Although many of these values are extremely high, the varying mobility of the elements (and the lack of geophysical trends) makes accurate correlations difficult.

PART G CONCLUSIONS AND RECOMMENDATIONS

The present exploration program was concentrated on a control grid established over the old workings on the Saddle Group. Encouraging geological, geochemical and geophysical results were obtained. Assays of channel and rock chip samples from the Saddle Group workings returned encouraging gold and silver values (from trace values to 0.322 oz/ton Au and 9.29 oz/ton Ag). In addition, ground VLF-EM and soil geochemical results indicate a possible extension of the vein system to the northeast of the exposed mineralization. Mineralogical analysis of a mineralized hand specimen shows the gold to be 90% free milling at -1 mm, which allows easy recovery.

The geology of the Saddle-Shakti claim group is conducive to high-grade, low tonnage gold/silver mineralization. A second phase of exploration consisting of trenching and an induced polarization survey over the Saddle Group vein system is recommended in order to investigate the geometry and grade of the mineralization and to delineate additional targets. As well, the area of the old Elkhorn Group workings should be systematically sampled by a geologist skilled in technical climbing methods. The estimated cost of the proposed second phase program is $70,000.

ESTIMATED COST OF PHASE II EXPLORATION PROGRAM

Mob/Demob and logistical support	$ 8,000
IP survey	10,000
Trenching and blasting	20,000
Grid establishment	2,000
Geological support	9,000
Analysis of rock samples	5,000
Engineering supervision and reports	8,000
Contingencies	8,000
Estimated Total Cost For Phase II	$70,000

Contingent upon favourable results from the recommended program, further work consisting of diamond drilling and additional trenching will be necessary in order to more fully evaluate the economic potential of the Saddle-Shakti property.

Signed at Vancouver, B.C.

PROFESSIONAL
PROVINCE
OF
F. DISPIRITO
BRITISH
COLUMBIA
ENGINEER

F. Di Spirito, B.A.Sc., P.Eng.
September 29, 1987

REFERENCES

Grove, E. W., 1971	B.C. Dept. of Mines and Petroleum Resources; Bulletin No. 58; Geology and Mineral Deposits of the Stewart area, B.C.
AR 11076	Reconnaissance project of the "Saddle Claim Group" Skeena, M.D., Nor-con Exploration Ltd., 1983.
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APPENDIX A

COST BREAKDOWN

COST BREAKDOWN FOR PHASE ONE OF THE SADDLE PROJECT

Airborne VLF-EM and magnetometer Survey 145.45 kilometers @ $100.00 kilometer	$14,545.00
Geological Mapping and Sampling	10,000.00
Grid Emplacement 11.1 kilometers, 12.5 metre intervals 11.1 kilometers @ $500.00	5,600.00
VLF-EM Survey 11.1 kilometers @ $500.00	5,600.00
Blasting and Hand Trenching (Including materials)	9,000.00
Assays and analyses (including Collection costs)	
342 soils @ $25	8,550.00
69 rocks @ $30	2,070.00
Fire assays	309.00
Mineralogical analysis	1,035.00
Camp Costs	4,225.00
Interpretation, Report Writing and Office Costs	6,843.00
TOTAL COSTS FOR PHASE ONE	$67,777.00

APPENDIX B

CERTIFICATES

CERTIFICATE

I, Frank Di Spirito, of the City of Vancouver in the Province of British Columbia, do hereby certify:

I) I am a Consulting Engineer residing at 1319 Shorepine Walk, Vancouver, British Columbia, V6H 3T7 for Shangri-La Minerals Limited based at 706-675 West Hastings Street, Vancouver, British Columbia.

II) I am a graduate of the University of British Columbia (1974) and hold a Bachelor of Applied Science in Geological Engineering.

III) I am a registered member, in good standing, of the Association of Professional Engineers of British Columbia.

IV) Since graduation, I have been involved in numerous mineral exploration programs throughout Canada and the United States of America.

V) This report is based upon a field examination during September, 1986 and the results of an exploration program conducted by a Shangri-La Minerals Limited crew during July and August, 1987 for Winspear Resources Ltd.

VI) I hold no direct or indirect interest in the property, nor in any securities of Winspear Resources Ltd., or in any associated companies, nor do I expect to receive any.

Signed at Vancouver, B.C.

PROFESSIONAL ENGINEER PROVINCE OF BRITISH COLUMBIA F. DISPIRITO

Frank Di Spirito, B.A.Sc., P.Eng.
29 September, 1987

CERTIFICATE

I, Darcy Krohman, do hereby certify that;

I) I am a Consulting Geologist to the firm of Shangri-La Minerals Limited, #706-675 W. Hastings St., Vancouver, British Columbia.

II) I graduated in 1985 from the University of British Columbia, Vancouver, B.C. with a B.Sc., in Geology.

III) I have been involved in mineral exploration since 1983.

IV) This report is based upon field work carried out by myself and a Shangri-La Minerals crew during the month of August, 1987.

V) I have no direct or indirect interest in the property nor in Winspear Resources Ltd., nor do I expect to receive any.

VI) This report may be utilized by Winspear Resources Ltd. for inclusion in a Prospectus or Statement of Material Facts.

Respectfully submitted at Vancouver, B.C.

Darcy Krohman, B.Sc.
29 September, 1987

CERTIFICATE

I, J. Campbell Graham, of the City of Vancouver in the Province of British Columbia, do hereby certify:

I) I am a Consulting Geophysical Engineer for the firm of Shangri-La Minerals Limited at 706-675 West Hastings Street, Vancouver, B.C., V6B 1N2.

II) I graduated in 1985 with a M.Eng. degree in Geophysical Engineering and in 1982 with a B.Sc. in Geophysical Engineering from the Colorado School of Mines in Golden, Colorado.

III) I have been involved in numerous mineral exploration programs since 1975.

IV) This report is based upon field work carried out by myself during July, 1987, and a Shangri-La Minerals Limited crew during August, 1987.

V) I hold no direct or indirect interest in the property described herein, or in any securities of Winspear Resources Ltd., or in any associated companies, nor do I expect to receive any.

VI) This report may be utilized by Winspear Resources Ltd. for inclusion in a Prospectus or Statement of Material Facts.

Signed at Vancouver, B.C.

J. Campbell Graham, B.Sc., M.Eng.
29 September, 1987

APPENDIX C

SAMPLE DESCRIPTIONS

ROCK SAMPLE DESCRIPTIONS
SAMPLES FROM SHOWINGS SK01-SK19

SK01	Massive mineralized vein quartz. Pyrite, galena sphalerite, chalcopyrite. Gossenous alteration. Minor cerrucite, anglesite alteration. Channel sample across 0.4 m.
SK02	Same as SK01. Channel sample across 0.72 m
SK03	Same as SK01. Channel sample across 0.50 m
SK04	Same as SK01. Channel sample across 0.34 m
SK05	Same as SK01. Channel sample across 0.25 m
SK06	Same as SK01. Channel sample across 0.32 m
SK07	Same as SK01. Channel sample across 0.30 m
SK08	Same as SK01. Channel sample across 0.22 m
SK09	Same as SK01. Channel sample across 0.20 m
SK10	Same as SK01. Channel sample across 0.70 m
SK11	Same as SK01. Channel sample across 0.45 m
SK12	Same as SK01. Channel sample across 0.60 m
SK13	Same as SK01. Channel sample across 0.13 m
SK14	Same as SK01. Channel sample across 0.14 m
SK15	Mineralized vein quartz. Well formed pyrite crystals Gossenous Anglesite, cerrusite alteration.
SK16	Mineralized aphanitic andesite with galena, pyrite. Mineralization is both massive and disseminated. Grab sample.
SK17	Same as SK01. Channel sample across .30 m
SK18	Same as SK01. Channel sample across .28 m
SK19	Same as SK01. Channel sample across .75 m
SK20	Gossenous, white, massive quartz vein from contact zone. Chlorite schist host. Rock chip sample.
SK22	Aphanitic, chlorite schist from contact zone. 152/40° SW. Rock chip sample.

SK23 Massive, microcrystalline vein quartz in aphanitic andesite host. Grab sample.

SK24 Banded, aphanitic andesite with white quartz veining. Pyrite mineralization. Rock chip sample.

SK25 Same as SK24.

SK26 Massive white vein quartz in andesite and tuffs. Grab sample.

SK27 Siliceous dark grey andesite with massive white vein quartz (8 cm thick). Float sample from dump.

SK28 Same as SK27. Float sample from dump.

SK29 Dark grey aphanitic andesite with minor disseminated pyrite float sample from dump.

SK30 Same as SK29. Float sample from dump.

Samples from Adit SK31-SK46

SK31 Massive microcrystalline quartz (in andesite host) mineralized with sphalerite, galena, pyrite. Channel sample 10 m's in adit.

SK32 Aphanitic dark grey andesite with minor massive, white, microcrystalline vein quartz stringers. Sample 20 m's in adit.

SK33 Same as SK32. Sample 30 m's in adit.

SK34 Same as SK32. Sample 40 m's in adit.

SK35 Same as SK31. Sample 55 m's in adit.

SK36 Same as SK31. Sample 65 m's in adit.

SK37 Same as SK32. Sample 80 m's in adit.

SK38 Same as SK32. Sample 93 m's in adit.

SK39 Same as SK32. Sample 104 m's in adit.

SK40 Same as SK32. Sample 118 m's in adit.

SK41 Same as SK32. Sample 138 m's in adit.

SK42 Same as SK32. Sample 158 m's in adit.

SK43 Same as SK32. Sample 180 m's in adit.

SK44 Same as SK32. Sample 195 m's in adit.

SK45	Same as SK32. Sample 195 m's in adit.
SK46	Sample from adit entrance
SK48	Quartz monzonite. Crystalline quartz, pyroxene, hornblende, plag, biotite. Rock chip sample.
SK49	Aphanitic, welded tuff. Inclusion in andesite. Rock chip sample.
SK50	Aphanitic andesite. Abundant mafic minerals. Rock chip sample.
SK51	Massive, slightly mineralized vein quartz. Channel sample .75 m. From trench.
SK52	Altered andesite and tuff sheared hydrothermal alteration, recrystalized, tightly folded, banded and contorted. Quartz veins 3 to 5 cm thick present. Rock chip sample.
SK54	Altered, aphanitic andesite. Sample from contact zone. Rock chip sample.
SK55	Same as SK54.
SK56	Gossenous, massive white quartz vein in granodiorite host. Vein width varies from 0.5 to 1.5 m. Rock chip sample.
SK57	Medium grained granodiorite. Rock chip sample.
SK58	Altered andesite with siliceous veinlets and quartz stringers. Rock chip sample.
SK59	Very altered, tightly folded, contorted banded andesite and tuff. Weathers grey-green. Rock chip sample.
SK60	Very weathered, gossenous andesite from xenolith in granodiorite.
SK61	Altered, banded andesite. Recrystallized, light grey and fine grained. Rock chip sample.
SK62	Gossenous, altered andesite. Aphanitite. Rock chip sample.
SK63	Very siliceous felsic dyke cross cutting granodiorite .75 m wide. Rock chip sample.
SK64	Very altered, siliceous gossenous andesite from large xenolith in granodiorite. Rock chip sample.

SK65	Same as SK64.
SK66	Very mineralized quartz vein at showings. Pyrite, chalco, galena. Mineralization appears to be concentrated along contact between the quartz and granodiorite. Rock chip sample.
SK67	Massive, microcrystalline quartz vein mineralized with pyrite, phyrohotite. .10 m thick. 98°/30° NE. Rock chip sample.
SK68	Quartz monzonite dyke. Total thickness approximately 75 m's. Rock chip sample.
SK69	Altered aphanitic andesite from 7 m shaft drifted on vein "A". Channel sample across 2 m's.

APPENDIX D
ANALYTICAL RESULTS

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: OCT 16 1986
852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE: 251-1011 DATE REPORT MAILED: Oct 21/86

ASSAY CERTIFICATE

SAMPLE TYPE: PULP AU** AND AG** BY FIRE ASSAY

ASSAYER: D.Toye DEAN TOYE. CERTIFIED B.C. ASSAYER.

SHANGRI-LA MINERAL PROJECT-SADDLE FILE# 86-3062R PAGE 1

SAMPLE#	Pb %	Zn %	Ag** OZ/T	Au** OZ/T
86-SSR-01	2.12	-	-	-
86-SSR-02	1.27	-	2.50	-
86-AS-03	-	5.04	-	-
86-SSR-03	42.40	11.27	29.74	.062
86-SSR-04	-	-	3.05	-
86-SSR-06	12.27	12.62	11.16	.124
86-SSR-07	10.83	10.74	8.25	.102
86-SSR-08	-	7.13	1.82	-
86-SSR-10	2.80	5.73	2.60	-
86-SSR-11	13.03	12.67	5.99	.296

ACME ANALYTICAL LABORATORIES
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: SEPT 5 1987
DATE REPORT MAILED: Sept. 13/87..

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp AU** AND AG** BY FIRE ASSAY.

ASSAYER: .... DEAN TOYE, CERTIFIED B.C. ASSAYER

SHANGRI-LA File # 87-3689 R

SAMPLE#	PB %	ZN %	AG** OZ/T	AU** OZ/T
SK-01	1.52	1.57	.80	-
SK-02	1.64	4.75	1.39	.066
SK-03	-	5.31	1.22	-
SK-04	4.19	4.90	6.71	.322
SK-06	-	-	2.08	-
SK-07	-	-	-	.015
SK-08	-	-	1.03	.239
SK-09	-	-	-	.088
SK-10	2.33	1.45	1.42	-
SK-11	-	-	1.82	-
SK-12	4.34	5.36	3.39	.058
SK-14	1.67	-	2.35	.178
SK-15	5.07	8.53	9.29	.058
SK-17	-	-	2.02	.048
SK-18	-	-	-	.039
SK-19	5.05	-	2.21	-
SK-31	-	8.94	1.36	-
SK-35	4.66	-	8.57	-
SK-36	-	4.05	-	-

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 27 1987 DATE REPORT MAILED: Sept 4/87 ASSAYER. D. Toye. DEAN TOYE, CERTIFIED B.C. ASSAYER

SHANGRI-LA File # 87-3690 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SBG 00E+600N	1	40	12	103	.1	15	11	619	4.82	7	5	ND	5	10	1	2	2	117	.13	.038	9	45	1.44	75	.32	2	3.18	.04	.55	1	1
SBG 00E+575N	2	180	17	86	.3	12	14	615	5.26	9	5	ND	3	19	1	2	2	130	.30	.084	6	13	1.52	188	.27	2	3.04	.05	.52	1	3
SBG 00E+547N	1	125	10	97	.1	11	19	669	5.91	4	5	ND	1	12	1	2	2	178	.25	.064	3	8	2.40	364	.33	2	3.96	.06	.98	1	1
SBG 00E+525N	1	71	7	82	.1	12	14	556	5.36	8	5	ND	1	22	1	2	2	149	.20	.060	3	18	1.59	54	.26	2	5.83	.08	.59	2	1
SBG 00E+500N	2	44	17	78	.1	10	9	419	5.66	6	5	ND	6	13	1	2	2	121	.26	.077	11	22	1.22	95	.28	2	3.86	.06	.32	1	2
SBG 00E+475N	1	183	8	164	.2	50	44	1312	8.58	4	5	ND	2	32	1	2	5	257	.72	.094	4	107	4.08	500	.47	2	6.54	.04	.69	1	2
SBG 00E+450N	1	107	18	77	.3	13	13	535	5.96	8	5	ND	1	9	1	2	2	182	.19	.054	4	76	2.21	249	.38	5	3.92	.06	.87	1	1
SBG 00E+425N	1	75	17	84	.3	15	12	450	4.74	7	5	ND	3	31	1	2	2	115	.27	.084	8	23	1.48	235	.27	2	3.01	.04	.47	1	1
SBG 00E+400N	1	115	12	89	.3	16	17	511	5.50	6	5	ND	1	25	1	2	2	142	.33	.077	4	20	1.78	170	.31	2	3.99	.07	.53	1	6
SBG 00E+375N	1	72	37	89	.7	14	12	457	4.56	15	5	ND	4	23	1	2	2	111	.38	.100	8	21	1.59	180	.25	6	2.87	.05	.53	1	1
SBG 00E+350N	1	168	7	156	.4	27	31	1223	6.99	6	5	ND	4	74	1	2	4	202	.69	.109	12	47	3.04	243	.33	2	5.78	.10	.82	1	1
SBG 00E+335N	1	68	24	115	.4	23	15	646	4.98	7	5	ND	5	25	1	2	2	117	.40	.118	14	34	1.50	112	.27	2	3.44	.06	.28	1	2
SBG 00E+300N	1	83	14	104	.1	11	14	670	5.77	8	5	ND	1	13	1	2	2	147	.21	.078	6	23	1.77	235	.35	2	3.68	.04	.67	2	1
SBG 00E+275N	1	33	11	107	.1	6	16	947	6.41	6	5	ND	1	6	1	2	2	159	.13	.065	4	11	2.69	436	.40	2	3.95	.03	1.46	1	1
SBG 00E+250N	2	72	6	95	.2	6	11	715	6.06	3	5	ND	2	10	1	2	3	143	.21	.092	4	21	2.27	376	.38	2	3.52	.05	.92	1	1
SBG 00E+225N	1	25	7	116	.2	6	12	646	6.62	7	5	ND	1	47	1	4	2	143	.59	.169	5	18	2.63	308	.30	2	4.62	.13	.83	1	1
SBG 00E+200N	1	52	14	84	.2	7	9	627	6.31	4	5	ND	2	10	1	3	2	190	.19	.101	4	43	2.36	577	.42	2	3.08	.05	1.21	1	2
SBG 00E+175N	1	84	2	71	.3	27	12	389	5.29	8	5	ND	1	15	1	2	2	166	.20	.076	5	101	1.81	109	.39	2	5.71	.07	.32	1	1
SBG 00E+150N	1	39	8	89	.1	16	15	573	5.21	6	5	ND	2	15	1	2	2	138	.19	.055	5	37	2.00	234	.33	2	3.67	.04	.54	1	1
SBG 00E+125N	6	72	22	92	.4	18	9	415	4.25	12	5	ND	3	24	1	2	2	97	.30	.105	9	35	1.32	91	.24	5	2.90	.05	.26	1	1
SBG 00E+100N	3	47	17	72	.5	21	8	350	5.13	8	5	ND	3	13	1	2	2	120	.25	.085	11	54	1.23	119	.38	6	3.49	.05	.27	1	1
SBG 00E+75N	1	66	16	93	.2	34	14	539	5.43	8	5	ND	2	7	1	2	2	154	.20	.079	4	86	1.83	96	.29	2	4.28	.04	.69	1	1
SBG 00E+50N	3	66	8	100	.1	17	12	583	5.91	4	5	ND	2	8	1	2	2	188	.20	.073	4	48	1.89	192	.31	2	4.57	.04	.69	1	1
SBG 00E+25N	1	77	14	115	.3	18	16	742	5.77	8	5	ND	3	6	1	4	2	184	.29	.116	5	40	2.22	452	.34	2	3.53	.03	1.01	1	1
SBG 00E+00S	1	121	10	95	.3	26	10	606	5.96	3	5	ND	2	8	1	2	2	180	.19	.105	2	101	2.66	457	.37	2	3.66	.04	1.45	1	1
SBG 00E+26S	3	42	21	73	.2	12	7	434	3.64	5	5	ND	1	15	1	2	2	83	.11	.089	10	30	.87	34	.10	5	3.03	.02	.08	1	2
SBG 00E+50S	2	19	15	57	.2	3	5	258	3.49	4	5	ND	1	7	1	2	2	90	.11	.092	9	16	.64	19	.33	2	2.04	.04	.12	1	1
SBG 00E+75S	1	57	9	80	.2	8	12	425	5.72	7	5	ND	2	6	1	2	2	145	.13	.071	6	25	1.45	82	.25	2	4.98	.03	.32	1	1
SBG 00E+100S	2	49	11	83	.1	5	11	520	5.44	2	5	ND	1	4	1	2	2	143	.09	.067	4	9	1.60	159	.27	2	3.07	.03	.48	1	1
SBG 00E+125S	3	61	14	125	.3	16	15	835	6.66	7	5	ND	1	42	1	2	2	174	.58	.117	4	40	2.46	99	.35	2	5.60	.17	.92	1	2
SBG 00E+150S	4	55	16	91	.3	12	9	558	5.88	6	5	ND	3	12	1	2	2	153	.25	.095	6	42	1.96	156	.31	7	3.64	.04	.49	1	1
SBG 00E+175S	2	176	17	101	.4	20	16	558	6.01	7	6	ND	3	433	1	2	2	141	.64	.132	7	28	1.72	153	.25	2	3.45	.05	.70	1	1
SBG 00E+200S	2	82	19	106	.2	18	10	515	5.40	7	5	ND	6	36	1	2	2	124	.28	.097	8	43	1.75	135	.29	7	3.23	.05	.52	1	1
SBG 00E+225S	3	89	16	104	.3	23	12	528	4.97	6	5	ND	4	20	1	2	2	118	.29	.103	10	47	1.65	113	.27	5	3.98	.05	.36	1	2
SBG 00E+252S	2	90	27	88	.2	48	12	388	4.48	9	5	ND	2	26	1	2	2	95	.44	.105	10	114	1.72	96	.26	2	3.26	.05	.23	1	1
SBG 00E+274S	2	117	29	89	.4	54	12	388	4.23	14	5	ND	3	23	1	2	2	85	.38	.072	5	125	1.98	108	.19	2	2.60	.05	.31	4	2
STD C/AU-S	20	61	39	132	7.5	73	28	1056	4.07	39	21	8	38	52	18	18	20	59	.50	.093	38	61	.91	178	.08	34	1.92	.07	.14	13	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SBG 00E+300S	6	75	17	5	.4	60	11	339	4.72	12	6	ND	7	15	1	2	2	77	.22	.109	14	79	1.25	67	.22	2	3.44	.04	.15	1	1
SBG 00E+325S	1	32	11	45	.1	108	14	190	3.07	3	5	ND	1	8	1	2	2	76	.10	.032	3	216	2.29	104	.16	3	2.57	.03	.31	1	1
SBG 00E+350S	5	51	25	107	.3	30	10	351	6.57	10	5	ND	3	4	1	4	2	150	.05	.053	11	85	2.09	114	.33	2	3.57	.03	.26	1	2
SBG 00E+374S	2	60	17	87	.2	41	12	380	4.90	6	5	ND	3	15	1	2	2	95	.20	.065	8	93	1.53	58	.20	3	3.09	.03	.11	1	2
SBG 00E+400S	2	50	14	77	.2	37	11	410	3.78	4	5	ND	4	18	1	2	2	93	.22	.044	8	73	1.46	64	.20	2	3.04	.03	.09	2	9
SBG 00E+425S	4	42	13	71	.4	21	7	353	4.60	5	5	ND	5	9	1	2	2	80	.16	.076	13	47	1.11	54	.24	2	2.90	.04	.17	1	1
SBG 00E+450S	3	84	15	80	.3	47	12	486	4.67	3	5	ND	2	7	1	3	2	147	.22	.084	7	87	2.12	52	.29	2	3.26	.03	.32	1	1
SBG 00E+475S	2	24	32	51	.1	8	4	169	3.61	5	5	ND	3	9	1	2	2	66	.10	.139	12	20	.47	43	.23	2	2.55	.03	.06	1	1
SBG 00E+495S	2	28	18	53	.1	7	5	182	3.26	8	5	ND	2	9	1	2	2	65	.07	.077	7	11	.49	39	.14	2	1.98	.02	.06	1	2
SBG 00E+525S	1	9	15	29	.1	1	2	85	1.45	3	5	ND	1	65	1	2	3	45	.06	.053	5	5	.17	51	.13	2	1.20	.01	.03	1	1
SBG 00E+550S	4	21	18	44	.1	9	4	159	3.09	3	5	ND	1	36	1	2	2	65	.27	.072	8	23	.47	32	.14	2	2.38	.02	.07	1	4
STD C/AU-S	19	59	39	132	7.3	69	28	1055	4.04	42	23	7	37	50	19	18	21	58	.48	.090	37	58	.89	181	.08	37	1.87	.07	.12	13	52

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-8 SOIL P9-10 ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 27 1987 DATE REPORT MAILED: ASSAYER............DEAN TOYE, CERTIFIED B.C. ASSAYER

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 00E+25N	1	64	22	111	.3	7	11	529	5.00	13	5	ND	3	148	1	2	2	113	1.03	.104	6	22	1.52	75	.28	2	4.75	.03	.24	1	2
SA 00E+00	15	14	21	95	.4	11	5	5125	2.89	87	5	ND	1	667	1	2	7	75	6.09	.047	6	21	.95	34	.04	2	10.55	.01	.22	2	1
SA 00E+25S	1	81	18	133	.4	17	19	1133	7.99	4	5	ND	1	24	1	2	2	172	.40	.097	6	27	2.66	127	.34	2	4.84	.01	.80	3	3
SA 00E+50S	3	62	16	114	.1	30	17	861	6.95	15	5	ND	2	20	1	2	2	166	.20	.069	8	57	1.89	52	.32	2	3.66	.02	.27	1	76
SA 00E+75S	4	54	26	94	.3	18	12	548	6.11	13	5	ND	2	17	1	2	2	121	.19	.060	8	33	1.31	42	.30	11	3.32	.02	.21	2	3
SA 00E+110S	3	86	21	133	.2	32	18	1528	5.85	8	5	ND	1	123	1	2	2	150	1.13	.106	5	48	2.23	161	.28	2	5.12	.05	.43	4	3
SA 00E+125S	7	105	25	183	.5	11	18	1685	7.90	36	5	ND	1	149	1	2	4	177	.77	.131	5	20	2.20	164	.27	2	6.66	.04	.59	4	2
SA 00E+150S	9	71	20	181	.3	40	26	1774	8.05	41	5	ND	1	20	1	2	2	216	.38	.060	6	87	3.13	80	.38	3	7.26	.04	.22	4	2
SA 00E+175S	3	74	23	138	.4	17	22	1369	7.68	17	5	ND	3	17	1	2	2	200	.55	.095	5	39	2.56	244	.39	10	4.69	.06	.89	6	1
SA 00E+200S	4	30	58	57	.6	8	4	243	2.51	17	14	ND	8	10	1	2	4	38	.14	.054	10	13	.47	29	.12	2	1.37	.03	.11	1	1
SA 00E+250S	5	29	51	71	.1	12	5	301	4.87	16	5	ND	4	9	1	2	2	76	.09	.063	16	24	.71	27	.21	2	2.34	.02	.11	1	2
SA 00E+275S	8	57	25	72	.1	16	9	314	5.37	13	5	ND	3	10	1	2	2	82	.22	.044	13	21	.94	52	.29	2	3.38	.06	.17	3	1
SA 00E+300S	4	149	18	103	.3	26	19	608	6.46	8	5	ND	1	11	1	2	2	182	.29	.080	6	42	2.52	182	.35	4	3.86	.06	.65	1	2
SA 00E+325S	2	92	12	98	.3	35	20	708	5.71	13	5	ND	2	24	1	2	2	158	.88	.123	4	85	2.06	250	.42	6	2.63	.02	.73	1	1
SA 00E+360S	2	70	22	99	.5	14	20	810	6.42	15	5	ND	1	13	1	2	2	187	.32	.081	5	25	2.18	159	.40	2	3.58	.02	.98	2	1
SA 00E+375S	3	169	15	144	.4	29	26	990	7.70	6	5	ND	1	12	1	2	2	238	.33	.076	3	55	2.96	124	.36	2	4.92	.05	.81	3	1
SA 00E+400S	3	77	20	103	.4	23	19	688	6.19	10	5	ND	1	25	1	2	2	185	.28	.064	5	35	2.40	89	.35	2	4.14	.06	.90	3	2
SA 00E+425S	3	56	23	106	.1	11	12	586	4.85	10	5	ND	2	35	1	3	2	116	.27	.079	9	25	1.64	71	.25	8	2.75	.03	.49	1	1
SA 00E+450S	3	57	22	70	.1	15	8	393	3.85	18	5	ND	4	12	1	2	5	75	.21	.065	10	24	.94	27	.17	2	2.01	.01	.12	1	1
SA 00E+470S	2	36	23	64	.2	7	7	358	3.75	14	5	ND	4	12	1	2	2	72	.25	.077	11	22	.84	29	.14	2	2.11	.01	.11	4	5
SA 00E+500S	2	57	23	85	.1	21	19	696	5.87	5	5	ND	5	19	1	2	2	156	.27	.081	6	40	2.85	112	.33	5	3.49	.03	1.16	1	1
SA 00E+525S	1	233	18	113	.1	19	24	900	7.07	8	5	ND	1	12	1	2	2	175	.31	.090	3	19	2.75	180	.36	41	3.93	.03	1.06	2	1
SA 200E+75N	2	81	22	126	.4	17	16	774	5.76	7	5	ND	1	20	1	3	2	165	.40	.108	4	39	1.97	145	.29	2	4.27	.05	.50	1	1
SA 200E+50N	2	74	25	131	.7	23	14	751	6.41	18	5	ND	1	29	1	2	2	125	.44	.104	5	45	2.09	107	.28	2	5.51	.05	.43	1	1
SA 200E+25N	2	66	8	110	.3	10	14	731	6.48	9	5	ND	1	20	1	2	2	152	.33	.105	5	21	1.98	123	.29	2	3.89	.02	.57	2	1
SA 200E+00N	2	89	41	198	.6	13	14	739	6.04	19	5	ND	1	15	1	3	2	166	.34	.101	6	41	1.42	72	.30	4	3.70	.03	.45	2	2
SA 200E+25S	4	40	18	158	.3	7	14	832	8.44	20	5	ND	1	8	1	4	2	159	.13	.042	11	18	1.88	45	.31	6	4.11	.02	.36	4	1
SA 250E+75N	2	41	35	70	.4	8	7	304	5.23	22	5	ND	1	11	1	2	2	125	.14	.059	6	30	.90	43	.25	35	2.81	.03	.10	1	1
SA 250E+50N	2	42	17	83	.3	5	11	466	5.85	18	5	ND	1	6	1	3	2	144	.18	.075	5	18	1.52	125	.28	2	3.64	.02	.35	2	4
SA 250E+25N	2	65	51	137	.8	16	13	839	6.04	10	5	ND	1	17	1	3	2	155	.34	.094	5	39	1.76	81	.26	2	4.65	.05	.43	2	2
SA 250E+25S	3	47	27	131	.4	15	13	734	7.28	14	5	ND	1	10	1	2	2	179	.18	.063	8	47	1.76	65	.37	3	4.46	.03	.28	1	2
SA 250E+75S	4	29	48	120	.2	16	11	517	6.34	21	5	ND	2	11	1	2	2	122	.13	.034	10	44	1.23	45	.35	2	3.38	.02	.13	1	1
SA 250E+125S	2	85	24	163	.5	25	19	1293	6.57	22	5	ND	1	17	1	2	2	190	.50	.135	4	65	2.01	139	.29	2	3.82	.06	1.34	1	1
SA 300E+375N	3	35	58	107	.4	17	9	391	3.72	18	5	ND	2	41	1	3	9	61	.49	.159	10	28	1.21	116	.19	2	2.53	.03	.18	2	2
SA 300E+350N	7	35	122	156	1.4	19	10	395	4.49	16	5	ND	2	33	1	2	4	57	.41	.163	15	24	.99	100	.19	2	3.04	.05	.13	1	2
SA 300E+325N	6	67	247	233	.9	20	17	884	5.09	22	5	ND	7	42	1	2	2	86	.71	.231	12	26	1.37	192	.22	2	2.57	.04	.21	2	1
STD C/AU-S	20	60	41	133	7.5	69	29	1059	4.30	41	21	8	38	50	19	17	20	58	.52	.094	37	57	.94	181	.08	36	1.87	.06	.14	14	53

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 300E+300N	3	50	89	135	.5	20	12	457	4.42	15	5	ND	5	47	1	2	6	74	.42	.129	14	31	1.38	204	.24	7	3.06	.03	.26	3	25
SA 300E+287N	3	56	88	132	.6	18	13	568	5.37	14	5	ND	6	52	1	2	4	97	.51	.108	12	29	1.66	209	.25	2	2.95	.04	.31	5	3
SA 300E+262N	3	54	50	130	.4	19	13	603	5.36	7	5	ND	4	42	1	3	2	102	.51	.136	14	26	1.55	213	.26	5	3.53	.06	.42	3	5
SA 300E+200N	2	90	58	122	.5	18	18	942	6.96	21	5	ND	3	6	1	2	8	171	.16	.070	6	53	1.96	162	.32	2	3.03	.02	.60	3	10
SA 300E+175N	2	81	21	93	.4	13	16	839	6.65	8	5	ND	3	5	1	2	2	224	.15	.106	4	31	2.16	178	.37	2	3.02	.02	.77	1	1
SA 300E+125N	9	164	29	144	1.2	28	26	1622	8.05	43	5	ND	2	77	1	2	4	214	1.96	.158	3	48	2.77	117	.35	2	8.76	.31	.92	1	7
SA 300E+100N	6	93	19	157	1.3	23	20	1249	7.03	30	5	ND	1	32	1	2	2	192	.80	.105	4	54	2.00	71	.32	2	7.35	.10	.38	1	23
SA 300E+80N	1	94	13	175	.7	36	27	1317	7.41	2	5	ND	3	24	1	2	2	201	.67	.124	5	74	2.74	380	.35	2	4.68	.05	.67	1	2
SA 300E+50N	1	55	19	105	.4	26	14	481	6.99	2	5	ND	1	12	1	2	2	191	.16	.073	5	71	1.83	97	.29	4	4.73	.02	.22	1	19
SA 300E+25N	2	59	19	139	.5	15	13	596	6.60	2	5	ND	1	12	1	2	4	175	.18	.084	7	78	1.56	80	.30	2	4.11	.02	.25	1	6
SA 300E+00N	2	44	20	308	.3	11	12	641	6.05	8	5	ND	1	11	1	2	2	152	.22	.069	8	36	1.69	67	.26	3	3.71	.02	.20	1	1
SA 300E+25S	1	90	29	128	.5	22	21	1009	7.00	2	5	ND	2	17	1	2	2	190	.55	.111	4	54	2.55	115	.34	2	5.15	.09	.75	2	26
SA 300E+50S	1	22	12	87	.4	8	10	613	5.99	8	5	ND	1	7	1	2	2	174	.20	.082	5	31	1.42	48	.34	4	3.55	.03	.61	1	11
SA 300E+75S	2	58	27	120	.6	7	17	677	7.58	2	5	ND	3	8	1	2	2	191	.22	.093	7	13	1.95	217	.33	2	3.74	.03	.72	1	3
SA 300E+126S	11	59	29	87	.6	5	10	676	5.70	49	5	ND	2	4	1	2	2	131	.27	.150	4	5	1.16	61	.20	8	9.15	.01	.21	1	1
SA 350E+225N	1	149	8	161	.5	20	29	1251	7.88	3	5	ND	3	21	1	2	2	172	.57	.122	4	28	2.93	308	.28	2	4.75	.05	1.02	2	1
SA 350E+175N	6	25	44	96	.1	4	10	415	10.14	18	5	ND	3	4	1	2	2	94	.09	.047	17	19	.80	57	.24	2	2.53	.03	.18	2	5
SA 350E+150N	7	20	37	67	.1	7	5	235	7.52	11	5	ND	6	6	1	2	2	54	.06	.041	23	27	.40	24	.25	8	2.80	.03	.08	1	3
SA 350E+100N	2	39	20	77	.4	24	9	386	6.19	2	5	ND	3	14	1	2	2	102	.29	.155	15	29	1.11	63	.34	2	4.80	.03	.14	1	5
SA 350E+75N	3	39	34	84	.3	33	10	474	6.25	8	5	ND	2	13	1	2	2	125	.46	.087	9	43	1.40	42	.39	2	3.25	.03	.14	1	26
SA 350E+50N	2	39	17	107	.3	6	9	378	4.44	9	5	ND	1	6	1	2	2	126	.17	.056	7	33	1.02	84	.25	3	2.85	.02	.18	1	2
SA 350E+25N	1	53	19	113	.4	8	13	757	6.04	7	5	ND	2	10	1	2	2	152	.20	.084	6	19	1.67	150	.28	2	3.93	.02	.44	1	1
SA 350E+50S	1	59	2	108	.3	13	14	761	6.00	3	5	ND	1	18	1	2	2	156	.44	.122	5	10	1.82	123	.25	2	5.35	.06	.62	1	97
SA 350E+75S	1	25	6	147	.4	6	16	764	6.21	2	5	ND	2	12	1	2	2	161	.35	.127	7	8	1.94	121	.26	2	3.99	.03	.71	2	1
SA 450E+500N	4	17	25	102	.1	7	6	368	4.27	11	5	ND	9	16	1	2	2	46	.20	.119	19	15	.65	79	.19	5	2.33	.06	.18	1	1
SA 450E+475N	2	22	35	89	.2	8	4	352	3.38	13	5	ND	2	22	1	2	4	41	.17	.096	19	13	.65	68	.16	5	2.02	.02	.10	1	1
SA 450E+450N	4	47	12	107	.3	21	11	512	5.17	11	5	ND	8	25	1	2	2	93	.38	.115	14	31	1.19	132	.31	2	3.02	.08	.38	1	1
SA 450E+425N	9	42	21	80	.4	9	5	342	4.21	7	5	ND	4	16	1	3	2	98	.18	.100	14	30	1.01	100	.24	9	2.42	.03	.26	1	1
SA 450E+350N	3	39	34	151	.3	30	11	478	4.55	11	5	ND	9	50	1	2	2	62	.53	.139	20	29	1.28	190	.25	2	2.98	.05	.16	1	1
SA 450E+300N	2	39	63	121	.1	20	7	354	3.33	15	5	ND	3	30	1	2	2	57	.37	.121	17	27	.91	94	.18	5	2.39	.03	.09	1	1
SA 450E+200N	6	39	31	132	.2	18	8	342	5.24	5	5	ND	6	12	1	2	2	58	.19	.092	22	24	.70	70	.27	2	3.55	.06	.14	1	8
SA 450E+175N	4	47	31	121	.4	29	9	490	4.87	9	5	ND	12	18	1	2	2	64	.26	.110	17	27	.84	72	.21	4	2.71	.06	.15	1	17
SA 450E+150N	2	140	11	202	.5	18	27	1066	7.02	8	5	ND	2	19	1	2	2	177	.43	.126	4	30	2.44	210	.29	3	5.60	.06	.69	1	5
SA 450E+125N	1	165	10	216	.8	8	21	1344	9.41	2	5	ND	3	43	2	2	2	172	1.35	.160	4	8	3.50	409	.31	5	5.50	.09	1.06	2	1
SA 450E+100N	2	75	44	183	.3	17	11	513	4.65	11	5	ND	2	25	1	2	2	89	.36	.134	11	27	1.16	73	.22	2	3.42	.03	.17	1	1
SA 450E+75N	3	63	48	139	.1	11	9	475	5.67	14	5	ND	3	15	1	2	2	91	.17	.116	13	21	.94	47	.22	2	2.91	.03	.15	1	4
STD C/AU-S	20	60	39	130	7.5	71	29	1047	4.16	41	17	8	38	50	18	16	21	58	.51	.098	37	61	.93	180	.07	39	1.87	.06	.13	13	48

SHANGRI-LA FILE # 87-3689

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 450E+50N	3	54	2	149	.3	8	16	834	9.81	2	5	ND	6	6	1	2	2	163	.16	.077	14	4	2.05	119	.36	2	3.86	.02	.82	1	1
SA 450E+25N	2	83	50	148	.1	7	20	1215	8.18	25	5	ND	3	23	1	2	2	178	.36	.118	10	12	2.29	168	.40	3	4.30	.04	.74	2	1
SA 450E+25S	2	125	46	147	.3	8	18	925	6.67	9	5	ND	4	34	1	2	2	143	.39	.113	9	11	2.00	120	.33	4	3.70	.04	.73	3	2
SA 450E+50S	3	83	7	211	.1	5	25	1607	8.69	3	5	ND	1	16	1	2	2	207	.29	.044	19	5	2.99	97	.44	2	4.42	.02	.50	1	1
SA 450E+75S	3	109	14	112	.2	22	13	570	6.75	13	5	ND	5	19	1	2	2	114	.31	.100	12	25	1.39	73	.30	6	3.60	.04	.26	2	9
SA 450E+100S	2	58	13	114	.1	1	9	1197	7.64	4	5	ND	1	9	1	2	2	208	.22	.138	6	17	2.70	505	.43	2	3.43	.02	1.39	1	2
SA 450E+125S	5	41	19	152	.1	8	20	1431	7.01	8	5	ND	3	32	1	2	2	136	.49	.088	12	10	1.75	96	.29	2	5.74	.10	.63	1	2
SA 450E+150S	4	46	25	85	.1	7	8	520	6.87	8	5	ND	1	15	1	2	2	130	.21	.066	10	25	1.29	40	.29	2	3.08	.04	.18	1	2
SA 450E+175S	6	37	31	96	.1	7	11	446	9.49	2	5	ND	2	7	1	2	3	161	.15	.050	11	42	.75	30	.49	4	3.14	.02	.09	1	2
SA 450E+200S	2	19	20	50	.3	3	7	313	3.57	8	5	ND	1	8	1	2	2	96	.21	.040	5	18	.67	40	.31	3	1.98	.03	.13	1	1
SA 500E+425N	4	46	13	75	.1	10	6	461	5.41	3	5	ND	3	15	1	2	2	109	.19	.085	9	21	1.28	109	.24	3	2.16	.03	.39	1	2
SA 500E+400N	3	59	23	102	.1	20	11	438	4.24	9	5	ND	6	40	1	2	2	78	.44	.130	17	36	1.00	134	.23	7	2.52	.03	.20	1	2
SA 500E+340N	3	28	28	152	.1	22	14	444	4.97	7	5	ND	7	97	1	2	2	82	.90	.195	24	27	1.35	190	.29	6	3.28	.06	.15	1	2
SA 500E+300N	5	127	1712	676	3.1	21	9	357	4.25	13	5	ND	4	162	1	2	4	87	.95	.168	15	36	.99	71	.24	4	3.72	.04	.11	3	2
SA 500E+275N	2	60	137	143	.6	22	11	392	4.48	17	6	ND	5	54	1	2	2	72	.80	.241	16	30	1.31	242	.24	6	2.87	.04	.27	1	4
SA 500E+225N	4	49	102	141	.2	24	9	404	4.69	14	5	ND	12	30	1	2	2	58	.36	.114	15	25	.86	58	.13	2	2.24	.02	.10	2	9
SA 500E+212N	3	67	335	191	.2	20	10	474	4.37	17	5	ND	10	31	1	2	2	63	.41	.119	17	24	.95	60	.16	4	2.51	.02	.11	1	4
SA 500E+150N	4	64	343	238	.5	17	9	436	4.97	17	5	ND	6	20	1	2	2	79	.33	.110	13	26	1.00	49	.16	2	2.24	.02	.13	1	9
SA 500E+125N	6	49	43	132	.4	17	11	474	5.98	13	5	ND	7	14	1	2	2	69	.15	.096	18	22	.87	66	.20	8	3.83	.05	.16	3	4
SA 500E+100N	2	80	39	112	.3	15	11	499	5.77	17	5	ND	4	25	1	2	2	100	.23	.113	13	22	1.26	113	.24	7	2.99	.02	.22	1	9
SA 500E+75N	3	54	26	124	.1	13	11	576	5.62	10	5	ND	3	16	1	2	2	112	.28	.102	11	21	1.38	80	.25	3	3.19	.02	.32	1	3
SA 500E+50N	2	39	24	115	.2	22	12	679	4.30	14	5	ND	10	27	1	2	2	72	.49	.129	16	24	1.10	85	.19	2	2.51	.02	.15	1	1
SA 500E+25N	3	61	26	87	.1	8	9	594	6.52	8	5	ND	2	18	1	2	2	137	.20	.104	9	13	1.62	107	.30	4	2.83	.02	.50	1	4
SA 500E+00N	4	68	24	105	.4	13	10	603	6.78	15	5	ND	2	17	1	2	2	120	.22	.110	9	29	1.55	116	.26	2	3.23	.02	.51	1	7
SA 500E+25S	6	61	17	102	.3	8	9	684	5.66	10	5	ND	2	27	1	2	2	129	.14	.083	7	16	1.62	92	.30	5	2.52	.02	.59	1	4
SA 500E+50S	3	53	3	96	.2	10	11	589	6.73	15	5	ND	2	12	1	2	2	177	.18	.096	8	36	1.81	186	.35	2	3.38	.02	.58	2	2
SA 500E+75S	3	74	6	127	.4	10	11	670	6.94	15	5	ND	1	46	1	2	2	162	.31	.097	6	22	1.77	218	.31	2	4.27	.03	.75	3	6
SA 500E+100S	4	104	11	108	.4	2	12	670	6.71	18	5	ND	3	11	1	2	2	143	.41	.132	5	7	1.34	45	.23	13	5.72	.03	.39	2	4
SA 500E+125S	4	86	9	80	.3	3	13	681	5.60	10	5	ND	1	10	1	2	6	172	.40	.157	8	5	1.07	50	.24	11	2.57	.03	.32	1	2
SA 500E+150S	3	52	2	104	.1	6	18	721	6.52	9	5	ND	1	6	1	2	2	157	.31	.098	8	4	1.92	74	.33	6	3.29	.02	.52	1	2
SA 500E+175S	2	76	24	111	.1	4	21	854	6.92	14	5	ND	4	9	1	2	2	186	.37	.125	4	6	2.40	250	.37	7	3.19	.02	1.04	1	1
SA 500E+200S	10	32	40	88	.1	6	8	364	9.47	22	5	ND	4	6	1	2	2	63	.10	.065	21	27	.67	26	.20	2	3.25	.04	.16	1	2
SA 500E+225S	3	51	24	86	.2	22	13	420	7.56	10	5	ND	2	6	1	2	2	180	.16	.041	8	72	1.51	108	.40	2	3.76	.03	.36	1	1
SA 550E+450N	2	31	42	134	.1	16	8	600	4.61	8	5	ND	10	66	1	2	2	63	.67	.156	21	28	1.04	121	.26	9	2.93	.04	.18	1	2
SA 550E+425N	2	36	24	105	.2	15	8	424	4.39	8	5	ND	9	59	1	2	2	64	.64	.168	15	37	1.04	129	.32	5	3.03	.05	.18	1	7
SA 550E+400N	2	30	20	86	.1	12	6	309	3.62	12	5	ND	4	59	1	2	2	67	.58	.120	17	29	.88	89	.23	4	2.74	.03	.11	1	2
STD C/AU-S	19	59	42	127	6.9	66	28	1013	4.15	39	19	7	35	48	18	17	21	56	.50	.089	37	61	.91	174	.08	37	1.84	.06	.13	13	48

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 550E+375N	3	28	16	136	.2	19	8	384	4.08	14	5	ND	5	35	1	2	2	53	.31	.141	31	26	.76	258	.27	3	3.24	.06	.18	2	4
SA 550E+350N	2	27	18	108	.1	14	8	376	3.45	10	5	ND	5	29	1	2	2	46	.37	.139	19	21	.63	97	.20	5	2.51	.03	.11	1	1
SA 550E+325N	3	39	14	96	.1	16	8	297	3.69	6	5	ND	3	40	1	2	2	70	.60	.188	13	39	1.01	227	.33	2	3.28	.04	.18	5	2
SA 550E+300N	5	19	17	92	.1	9	6	295	3.95	10	5	ND	3	36	1	2	2	48	.36	.132	18	17	.64	101	.19	2	2.61	.04	.11	1	5
SA 550E+275N	4	40	34	95	.1	13	8	361	4.44	21	5	ND	3	26	1	2	2	72	.36	.153	16	19	.93	110	.24	7	2.65	.03	.16	1	2
SA 550E+200N	2	59	83	154	.2	11	9	608	4.50	13	5	ND	6	49	1	2	3	79	.46	.114	13	15	1.18	53	.21	2	2.89	.02	.28	2	4
SA 550E+175N	3	362	1533	953	6.5	9	8	619	5.49	10	5	ND	2	15	3	2	2	97	.40	.148	10	12	1.32	33	.27	2	2.79	.03	.32	3	55
SA 550E+150N	3	40	140	352	.6	8	7	436	4.06	13	5	ND	1	15	2	2	2	80	.20	.074	15	16	.88	43	.19	2	2.43	.02	.10	1	151
SA 550E+125N	3	73	1224	588	4.4	9	6	401	4.00	15	5	ND	1	18	1	2	2	79	.20	.106	12	23	.96	38	.05	2	3.32	.01	.13	1	7
SA 550E+100N	3	62	46	113	.1	18	8	467	6.14	11	5	ND	1	17	1	2	2	100	.34	.129	11	48	.96	43	.17	17	3.29	.02	.15	6	4
SA 550E+75N	2	44	13	73	.1	5	10	379	6.61	11	5	ND	1	7	1	2	2	131	.15	.070	8	10	.89	55	.26	7	2.78	.02	.14	1	4
SA 550E+50N	1	112	9	106	.1	4	15	554	6.00	7	5	ND	1	12	1	2	3	149	.39	.124	6	7	1.38	192	.29	2	3.57	.04	.30	1	1
SA 550E+25N	1	20	5	45	.1	5	4	199	4.51	8	5	ND	1	10	1	6	2	156	.13	.065	5	26	.46	22	.42	8	1.94	.01	.04	1	1
SA 550E+00N	3	54	15	102	.2	18	10	409	4.96	11	5	ND	2	27	1	2	3	104	.28	.113	9	26	1.38	153	.22	4	2.95	.03	.43	1	3
SA 550E+25S	2	94	17	115	.6	18	22	842	6.81	10	5	ND	2	19	1	2	2	189	.30	.087	5	54	2.74	376	.39	2	4.08	.03	1.02	1	2
SA 550E+75S	2	87	3	117	.5	15	12	522	5.63	16	5	ND	1	18	1	2	2	119	.28	.126	5	29	1.07	56	.26	4	5.91	.03	.29	7	6
SA 550E+100S	1	75	7	109	.7	10	10	658	6.21	10	5	ND	1	8	1	2	2	167	.17	.106	4	36	1.37	95	.29	2	4.94	.03	.49	1	6
SA 550E+175S	1	52	3	117	.2	9	15	872	6.38	6	5	ND	2	3	1	2	2	134	.21	.090	6	21	1.98	223	.29	2	3.49	.01	.99	1	1
SA 550E+200S	5	66	2	173	.6	19	20	862	7.70	6	5	ND	2	21	1	2	2	211	.56	.092	6	61	2.60	129	.35	6	6.67	.06	.86	1	1
SA 600E+500N	3	22	20	109	.1	12	5	368	3.37	12	5	ND	6	20	1	2	2	42	.26	.106	21	20	.70	73	.19	3	2.01	.03	.11	2	17
SA 600E+475N	3	44	77	109	.6	14	9	475	4.26	19	5	ND	9	38	1	2	2	59	.33	.130	19	26	1.00	147	.23	5	2.61	.04	.18	29	6
SA 600E+450N	3	41	40	91	.3	18	8	313	4.05	16	5	ND	9	31	1	2	4	58	.40	.151	17	31	.77	136	.27	2	2.30	.06	.15	1	1
SA 600E+425N	5	23	16	80	.1	11	7	303	3.89	7	5	ND	4	20	1	2	2	57	.24	.122	21	28	.76	110	.26	2	2.72	.03	.12	18	2
SA 600E+400N	2	30	29	93	.1	17	7	322	3.84	7	5	ND	5	38	1	3	2	57	.50	.186	15	33	.97	168	.21	2	2.31	.03	.17	1	48
SA 600E+375N	4	34	26	98	.1	14	6	327	3.77	13	5	ND	4	32	1	2	3	51	.32	.130	20	24	.74	113	.20	3	2.37	.03	.14	1	1
SA 600E+300N	3	26	28	106	.1	15	7	365	3.66	10	5	ND	6	35	1	2	2	48	.29	.107	19	23	.77	90	.22	2	2.43	.04	.15	1	3
SA 600E+275N	1	51	23	132	.3	9	15	1028	6.88	2	5	ND	3	26	1	2	2	138	.36	.125	6	9	2.29	203	.32	2	3.80	.02	.83	1	3
SA 600E+250N	3	56	93	137	.4	10	8	481	3.73	17	5	ND	3	41	1	2	2	63	.39	.112	13	18	1.06	84	.22	3	2.49	.03	.32	1	2
SA 600E+225N	2	79	222	286	2.0	7	8	651	5.22	6	5	ND	3	32	1	2	2	102	.41	.105	9	15	1.42	55	.27	2	3.01	.05	.31	1	6
SA 600E+200N	12	17	94	118	.1	1	4	489	7.39	24	5	ND	14	3	1	2	4	15	.07	.023	29	8	.18	13	.17	11	2.33	.12	.12	1	4
SA 600E+175N	2	28	135	143	.3	6	14	769	7.54	3	5	ND	3	5	1	2	3	136	.17	.079	12	14	1.85	219	.30	4	3.73	.01	.37	1	1
SA 600E+150N	5	44	343	158	.4	5	8	384	5.83	15	5	ND	2	10	1	2	8	74	.18	.077	15	17	.73	51	.22	2	2.89	.03	.12	1	3
SA 600E+125N	4	27	225	91	.4	4	6	391	5.99	8	5	ND	3	7	1	2	2	89	.17	.070	14	19	.89	62	.27	3	2.93	.03	.25	1	1
SA 600E+100N	1	53	21	115	.1	12	7	401	4.67	9	5	ND	7	12	1	2	3	72	.19	.074	11	13	.89	34	.16	5	2.22	.01	.13	1	3
SA 600E+75N	2	70	326	146	.6	16	8	464	4.66	19	5	ND	7	32	1	2	3	94	.36	.099	10	27	1.31	105	.24	3	3.04	.03	.39	1	5
SA 600E+50N	1	37	13	115	.4	7	14	698	6.41	6	5	ND	1	11	1	2	2	154	.17	.082	9	21	1.56	163	.38	4	3.84	.02	.33	2	1
STD C/AU-S	19	61	42	130	7.1	67	27	1040	4.13	43	16	7	37	49	18	17	23	56	.51	.088	37	61	.91	174	.08	34	1.85	.06	.12	12	51

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 600E+25N	1	44	27	81	.5	1	6	586	6.95	12	5	ND	1	10	1	3	2	168	.20	.094	6	13	1.60	85	.36	3	3.26	.03	.35	1	1
SA 600E+00S	8	26	34	112	.1	2	6	395	7.68	27	5	ND	6	3	1	2	2	35	.09	.047	27	15	.34	33	.22	2	3.16	.06	.11	1	1
SA 600E+25S	2	39	19	84	.4	12	12	502	6.13	15	5	ND	4	12	1	6	2	125	.19	.057	8	37	1.54	85	.32	2	3.35	.02	.43	2	1
SA 600E+50S	20	63	20	90	.9	3	6	573	6.75	16	5	ND	1	12	1	5	2	172	.11	.088	7	43	2.07	188	.38	2	3.69	.03	.83	2	3
SA 600E+75S	14	69	16	77	.7	3	5	595	6.32	8	5	ND	1	22	1	4	2	162	.09	.092	5	35	1.97	103	.35	10	3.39	.03	.82	1	6
SA 600E+100S	4	67	27	88	.7	12	8	583	7.64	13	5	ND	2	9	1	2	2	176	.14	.117	8	55	1.71	130	.40	6	3.50	.02	.55	1	1
SA 600E+125S	5	63	24	138	.5	28	15	868	7.61	8	5	ND	1	7	1	2	5	141	.15	.056	6	84	1.71	62	.29	2	6.18	.01	.21	1	1
SA 600E+150S	3	45	13	91	.6	13	9	539	5.41	17	5	ND	1	10	1	5	2	149	.15	.077	4	52	1.53	71	.27	3	3.37	.02	.21	1	5
SA 600E+175S	7	20	43	90	.3	3	6	312	6.27	13	5	ND	3	7	1	2	2	56	.10	.089	18	19	.46	24	.24	2	3.37	.04	.10	2	1
SA 600E+200S	2	81	24	99	.6	14	12	415	6.87	7	5	ND	1	7	1	2	2	170	.16	.074	10	37	1.55	84	.31	2	4.98	.01	.28	2	2
SA 600E+225S	2	66	29	146	.9	15	19	773	6.96	18	5	ND	1	13	1	2	7	199	.29	.062	4	31	2.15	132	.38	2	6.36	.06	.43	4	2
SA 600E+300S	1	68	34	88	.7	18	13	423	7.09	3	5	ND	1	6	1	2	2	230	.18	.071	5	64	1.40	80	.38	8	4.84	.02	.19	1	3
SA 600E+325S	1	96	21	87	.7	13	13	654	6.36	11	5	ND	1	6	1	2	2	187	.17	.087	6	41	1.97	62	.36	2	3.81	.02	.42	1	3
SA 650E+500N	2	26	43	145	.6	22	9	519	4.13	16	6	ND	5	42	1	4	2	50	.31	.110	29	25	.72	115	.25	6	3.06	.06	.13	2	2
SA 650E+475N	1	27	28	123	.6	17	8	464	3.55	15	5	ND	21	24	1	4	4	45	.27	.118	16	21	.67	54	.13	10	1.86	.02	.07	4	6
SA 650E+450N	3	33	27	106	.6	14	10	373	4.67	10	5	ND	6	48	1	2	5	75	.55	.200	14	41	1.26	329	.26	5	2.68	.03	.29	8	2
SA 650E+425N	2	26	32	79	.5	11	6	251	3.22	7	5	ND	1	24	1	2	6	64	.19	.086	16	39	.71	85	.27	2	3.28	.02	.08	9	3
SA 650E+350N	1	31	16	92	.4	29	8	279	3.82	11	5	ND	1	28	1	2	2	68	.30	.113	15	36	1.03	94	.35	2	3.44	.03	.09	2	4
SA 650E+300N	3	42	71	120	.5	11	10	552	5.59	16	5	ND	3	18	1	3	3	101	.27	.108	13	21	1.23	87	.29	5	3.15	.03	.22	1	2
SA 650E+275N	2	33	39	73	.3	10	7	380	4.60	18	5	ND	2	11	1	3	2	88	.13	.067	11	25	.82	53	.30	2	2.29	.02	.13	1	3
SA 650E+250N	3	74	44	117	.8	15	8	506	5.69	22	5	ND	1	46	1	3	2	111	.50	.167	10	35	1.13	75	.25	8	4.00	.03	.26	4	8
SA 650E+225N	3	99	25	75	1.0	9	5	463	5.39	5	5	ND	1	17	1	2	2	128	.21	.118	7	50	1.27	60	.25	3	3.85	.02	.38	3	1
SA 650E+200N	1	77	189	232	.6	17	9	513	5.25	18	5	ND	4	23	1	2	2	95	.31	.126	12	34	1.14	60	.24	2	2.79	.02	.21	1	73
SA 650E+175N	7	19	57	103	.2	7	8	376	8.24	20	5	ND	9	9	2	2	3	68	.13	.078	20	33	.62	29	.27	2	3.20	.04	.12	1	2
SA 650E+150N	1	36	25	99	.5	14	10	619	5.05	14	7	ND	13	17	1	5	2	91	.24	.098	10	21	1.15	42	.25	2	2.29	.01	.18	1	3
SA 650E+100N	1	29	38	61	.5	6	6	291	4.36	11	5	ND	1	9	1	2	2	102	.19	.058	5	23	.62	21	.35	5	2.29	.02	.08	1	1
SA 650E+75N	6	2	57	83	.1	2	3	254	6.36	15	5	ND	3	2	1	2	2	14	.06	.041	52	10	.10	10	.16	9	4.02	.06	.06	2	1
SA 650E+50N	1	43	67	142	.3	11	8	506	4.89	16	5	ND	3	9	1	3	2	79	.23	.088	11	16	1.04	24	.22	4	2.50	.01	.14	1	4
SA 650E+00N	1	66	15	146	.4	2	14	790	6.71	2	5	ND	1	6	1	2	2	151	.20	.085	7	9	1.84	60	.33	9	5.03	.02	.24	1	1
SA 650E+25S	1	63	11	166	.6	14	18	951	7.58	5	5	ND	1	8	1	2	2	177	.16	.070	5	21	2.41	278	.45	4	5.02	.02	.52	2	1
SA 650E+50S	2	83	12	53	.6	25	10	253	4.30	5	5	ND	1	17	1	5	2	108	.16	.098	3	78	.95	87	.17	2	5.71	.03	.18	1	4
SA 650E+75S	1	58	3	60	.4	10	8	231	5.37	5	5	ND	1	5	1	2	2	165	.13	.082	3	98	1.85	245	.38	2	3.34	.02	.49	1	2
SA 650E+100S	1	65	17	125	.5	25	15	474	5.27	19	5	ND	1	18	1	5	2	155	.28	.110	8	89	1.93	193	.30	3	4.29	.03	.34	1	3
SA 650E+125S	1	47	27	129	.4	14	9	476	4.44	16	5	ND	3	21	1	2	2	102	.31	.091	10	38	1.36	73	.21	3	2.87	.02	.15	1	1
SA 650E+150S	3	33	27	115	.2	12	7	374	5.38	8	5	ND	3	11	1	4	2	98	.12	.083	16	37	1.10	86	.29	3	4.00	.04	.17	1	2
SA 650E+175S	1	52	25	118	.4	21	9	634	4.45	11	5	ND	7	21	1	2	2	82	.27	.104	14	26	1.03	65	.20	3	2.68	.02	.13	1	5
STD C/AU-S	18	59	39	133	7.5	73	29	1116	4.27	42	26	7	37	51	19	16	21	59	.51	.095	37	64	.93	183	.09	35	1.93	.06	.13	12	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 650E+200S	4	59	13	131	.1	23	12	578	4.81	20	5	ND	5	22	1	2	2	117	.31	.129	15	35	1.40	93	.27	2	3.66	.03	.28	2	1
SA 650E+225S	5	54	27	134	.1	18	12	761	5.45	11	5	ND	9	13	1	4	2	113	.15	.074	17	27	1.32	68	.24	2	3.19	.02	.22	1	1
SA 650E+262.5S	4	93	21	99	.1	21	20	771	6.41	16	6	ND	2	7	1	2	2	190	.15	.070	10	39	2.25	227	.36	8	3.84	.02	.66	2	1
SA 650E+275S	4	73	9	99	.1	23	20	462	6.11	13	5	ND	2	7	1	2	2	191	.15	.059	6	75	2.35	143	.37	4	3.92	.03	.79	2	1
SA 650E+300S	6	39	22	86	.1	14	8	410	5.02	17	5	ND	3	12	1	2	2	76	.14	.056	14	30	.73	33	.23	3	2.71	.02	.10	3	1
SA 650E+325S	4	104	2	104	.1	19	21	667	7.05	9	5	ND	1	5	1	2	6	198	.14	.045	5	42	2.31	171	.37	4	5.19	.03	.79	3	1
SA 650E+350S	3	59	15	94	.1	16	13	463	4.54	16	5	ND	1	16	1	2	2	126	.30	.072	7	27	1.48	102	.25	2	3.12	.03	.33	2	94
SA 650E+400S	5	47	12	84	.1	14	15	610	6.83	15	6	ND	1	4	1	2	2	204	.08	.026	6	43	1.73	63	.39	13	3.64	.02	.28	1	1
SA 650E+425S	4	57	14	66	.1	17	12	404	4.97	10	5	ND	2	9	1	2	2	124	.31	.064	8	50	1.07	45	.30	4	2.89	.03	.15	1	2
SA 650E+450S	3	51	2	99	.1	10	20	947	7.00	5	5	ND	1	7	1	2	2	202	.33	.132	6	10	2.38	77	.39	8	3.76	.03	1.19	1	1
SA 650E+475S	4	53	10	106	.1	13	15	690	7.00	8	6	ND	1	5	1	2	2	186	.09	.028	7	35	1.75	52	.37	7	3.70	.02	.34	1	1
SA 650E+500S	4	95	57	459	.4	18	15	828	5.39	18	5	ND	1	28	1	2	3	166	.31	.104	5	49	1.78	55	.25	7	4.09	.06	.40	5	2
SA 700E+500N	3	22	9	79	.1	18	8	302	3.83	18	5	ND	5	90	1	32	8	72	.75	.216	16	35	.74	131	.22	6	2.80	.05	.11	1	1
SA 700E+475N	6	25	17	94	.1	16	6	372	3.98	13	5	ND	9	30	1	2	2	48	.25	.099	21	24	.55	47	.18	2	2.55	.05	.10	5	1
SA 700E+445N	3	38	27	116	.1	19	9	384	3.50	15	5	ND	5	38	1	2	2	64	.39	.142	15	41	1.09	243	.21	5	2.38	.02	.18	1	1
SA 700E+395N	4	25	17	100	.2	17	6	324	3.40	13	5	ND	3	52	1	2	2	64	.39	.158	21	36	.87	114	.24	7	3.25	.03	.15	5	1
SA 700E+375N	5	29	5	100	.3	15	10	307	3.90	14	7	ND	1	129	1	2	2	51	.76	.124	14	21	.69	72	.10	2	3.47	.03	.11	14	1
SA 700E+350N	6	15	18	74	.1	8	5	230	3.52	19	5	ND	1	46	1	2	2	59	.33	.117	19	22	.54	89	.22	7	2.97	.04	.09	1	1
SA 700E+325N	5	82	20	115	.8	19	10	471	4.04	42	5	ND	2	244	1	2	2	75	1.35	.104	8	31	.74	59	.14	4	4.88	.02	.16	2	9
SA 700E+300N	7	106	40	128	1.0	22	11	519	6.23	50	5	ND	3	119	1	2	2	101	.78	.146	8	39	.95	56	.14	7	3.87	.03	.21	4	8
SA 700E+270N	63	277	196	263	.9	76	72	2921	22.04	692	6	ND	5	17	2	4	2	45	.09	.279	13	14	.41	24	.05	7	1.91	.01	.09	5	25
SA 700E+250N	16	152	55	175	.9	26	18	926	7.91	144	5	ND	3	65	1	2	2	98	.34	.212	13	26	.95	76	.11	3	3.50	.02	.17	3	5
SA 700E+225N	6	73	10	127	.1	10	10	752	4.99	17	5	ND	1	40	1	2	2	113	.32	.120	8	25	1.20	57	.25	6	4.80	.03	.18	5	1
SA 700E+200N	3	23	8	54	.1	6	6	265	3.98	15	5	ND	2	7	1	2	2	112	.12	.054	6	38	.72	21	.31	2	2.40	.02	.11	1	1
SA 700E+175N	5	72	202	223	.2	16	12	594	5.33	29	5	ND	2	21	1	2	2	125	.29	.121	13	41	1.27	90	.26	14	3.56	.04	.32	4	7
SA 700E+150N	2	45	8	101	.4	8	15	1482	5.16	10	5	ND	1	25	1	2	2	149	.15	.069	6	23	1.16	89	.25	12	3.24	.02	.24	2	6
SA 700E+125N	3	47	13	73	.1	11	10	510	4.99	6	5	ND	1	17	1	2	2	104	.11	.058	8	39	.98	48	.21	7	3.14	.02	.14	2	1
SA 700E+100N	4	42	9	112	.1	6	13	775	6.18	11	5	ND	6	15	1	4	2	140	.24	.096	9	14	1.44	40	.31	3	3.39	.02	.30	3	1
SA 700E+75N	3	55	356	111	.3	10	8	444	4.18	18	5	ND	3	15	1	2	2	89	.25	.087	11	17	.85	28	.26	3	2.31	.03	.16	1	31
SA 700E+50N	3	58	17	101	.1	3	13	928	5.77	7	5	ND	2	7	1	2	2	128	.14	.080	10	10	1.47	35	.29	2	3.51	.03	.40	1	1
SA 700E+25N	3	112	41	103	.3	3	13	924	5.39	14	5	ND	2	42	1	2	2	99	.30	.122	6	6	.86	15	.15	2	4.77	.03	.12	2	34
SA 700E+00N	3	54	21	88	.4	10	7	444	4.44	19	5	ND	1	22	1	2	2	129	.23	.119	7	33	1.04	75	.24	2	3.65	.03	.34	1	3
SA 700E+25S	8	38	16	157	.1	8	11	814	8.20	22	5	ND	2	8	1	2	2	119	.07	.070	14	39	.98	46	.25	2	3.93	.02	.16	6	1
SA 700E+50S	18	145	46	147	.7	29	22	1453	6.90	35	5	ND	1	52	1	2	2	141	.19	.165	9	45	.96	105	.14	3	3.24	.02	.24	2	3
SA 700E+75S	7	54	22	99	.3	12	10	552	7.31	15	5	ND	5	11	1	5	2	118	.13	.076	13	45	1.13	55	.31	2	4.00	.05	.22	4	2
SA 700E+100S	3	41	8	100	.1	12	10	602	5.68	10	5	ND	8	14	1	2	2	147	.16	.077	5	34	1.66	88	.31	3	3.40	.03	.50	1	2
STD C/AU-S	20	59	38	130	7.3	68	29	1088	3.82	38	18	7	41	51	17	17	20	58	.47	.091	39	62	.84	181	.08	36	1.81	.06	.14	14	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 700E+125S	2	85	27	136	.3	12	19	767	6.53	2	5	ND	2	24	1	2	2	213	.32	.072	4	32	2.30	125	.33	3	4.78	.05	.43	1	8
SA 700E+150S	1	68	54	164	.4	13	9	461	4.33	10	5	ND	4	18	1	2	2	94	.35	.113	11	23	1.07	67	.17	2	2.66	.02	.16	2	5
SA 700E+175S	2	51	23	97	.2	7	12	430	5.21	6	5	ND	2	8	1	2	2	141	.14	.061	7	23	1.29	58	.26	3	3.38	.02	.21	1	1
SA 700E+200S	1	125	24	150	.3	12	12	495	5.83	7	5	ND	9	14	1	2	2	136	.26	.084	11	23	1.76	139	.23	3	3.01	.03	.44	1	1
SA 700E+225S	2	87	29	86	.2	8	14	490	6.89	2	5	ND	1	8	1	2	2	150	.33	.070	7	21	1.50	79	.30	3	4.51	.06	.23	1	1
SA 700E+250S	3	106	3	157	.2	11	19	698	7.63	2	5	ND	2	7	1	2	2	195	.15	.050	6	33	2.51	100	.35	11	5.25	.03	.33	1	1
SA 700E+250SA	2	37	22	51	.5	1	3	123	3.97	5	5	ND	1	10	1	4	2	139	.09	.079	5	23	.24	16	.17	5	2.92	.01	.03	1	1
SA 700E+275S	2	48	29	116	.2	9	10	462	4.42	3	5	ND	1	13	1	2	2	128	.13	.049	7	31	1.33	50	.24	4	3.10	.02	.22	4	3
SA 700E+300S	2	79	35	138	.4	27	24	1577	6.09	21	5	ND	1	16	1	2	2	125	.24	.092	9	60	1.98	89	.21	7	3.49	.03	.37	1	1
SA 700E+325S	3	76	24	64	.2	6	8	330	6.20	5	5	ND	1	8	1	2	2	156	.17	.106	8	33	1.04	44	.34	36	3.12	.04	.19	1	1
SA 700E+350S	2	49	22	54	.1	9	8	286	3.73	6	5	ND	1	8	1	3	2	103	.12	.065	7	40	.86	24	.24	11	2.45	.03	.22	1	1
SA 700E+375S	2	77	31	83	.4	9	8	432	4.92	4	5	ND	1	13	1	2	2	129	.19	.105	9	41	1.32	43	.30	7	3.17	.04	.37	1	3
SA 700E+400S	1	84	27	166	.4	12	25	1218	8.07	2	5	ND	2	8	1	2	2	209	.26	.084	6	21	2.89	608	.39	2	4.22	.02	.84	1	1
SA 700E+425S	2	44	6	76	.1	9	6	277	4.06	6	5	ND	1	5	1	3	2	107	.11	.089	16	18	.70	37	.23	2	3.51	.04	.20	1	3
SA 700E+450S	1	126	17	146	.5	19	21	986	6.84	7	5	ND	2	12	1	2	2	193	.24	.084	5	54	2.40	144	.37	2	3.79	.04	1.03	1	2
SA 700E+475S	1	95	16	172	.5	11	24	1218	6.88	2	5	ND	2	23	1	2	2	189	.80	.101	4	28	2.47	161	.37	2	3.38	.06	1.11	1	1
SA 700E+500S	2	84	26	124	.1	21	14	697	5.70	23	5	ND	3	19	1	2	2	123	.29	.096	8	45	1.84	91	.30	7	3.43	.04	.61	1	4
SA 800E+500N	3	17	24	57	.3	2	4	192	4.54	10	5	ND	1	24	1	2	3	47	.13	.096	16	18	.39	49	.16	3	2.12	.02	.06	9	1
SA 800E+475N	3	45	15	102	.1	6	7	431	8.07	2	5	ND	2	46	1	2	6	101	.55	.245	7	25	1.51	290	.30	45	4.09	.04	.70	96	1
SA 800E+450N	7	10	24	74	.1	1	4	233	7.12	8	5	ND	4	10	1	2	5	28	.06	.046	24	21	.23	28	.16	32	2.93	.05	.07	1	2
SA 800E+425N	1	23	21	79	.1	14	7	322	3.21	11	5	ND	3	95	1	2	2	45	.68	.079	12	18	.64	55	.10	3	2.63	.02	.07	5	1
SA 800E+400N	4	30	19	62	.1	10	5	267	3.10	6	5	ND	2	55	1	3	2	49	.35	.088	14	20	.65	66	.11	2	2.19	.02	.05	7	3
SA 800E+375N	2	30	10	90	.4	12	6	388	4.14	7	5	ND	4	39	1	2	2	74	.43	.107	10	22	.87	69	.16	29	3.77	.07	.17	2	1
SA 800E+350N	7	19	45	75	.1	3	5	333	7.25	18	5	ND	3	20	1	2	2	61	.11	.073	22	18	.49	49	.24	4	3.04	.03	.13	1	4
SA 800E+325N	2	22	19	78	.2	12	7	392	4.34	2	5	ND	2	36	1	2	2	73	.32	.119	12	22	.83	82	.24	7	3.37	.03	.13	1	1
SA 800E+300N	2	55	46	86	1.0	3	7	500	6.85	11	5	ND	1	33	1	2	2	85	.30	.109	7	16	.69	58	.18	2	3.98	.02	.16	2	7
SA 800E+275N	2	37	33	95	.5	3	8	634	4.95	5	5	ND	2	48	1	2	2	110	.47	.094	9	11	1.18	164	.26	4	3.66	.07	.38	3	165
SA 800E+250N	3	26	17	107	.2	14	8	429	4.10	13	5	ND	5	17	1	2	2	59	.18	.050	12	18	.78	47	.17	3	2.42	.02	.08	4	1
SA 800E+225N	4	29	25	81	.5	11	10	666	5.94	21	5	ND	2	25	1	4	3	82	.20	.093	10	19	.84	48	.18	5	2.37	.02	.10	1	1
SA 800E+200N	7	15	20	91	.2	1	8	937	5.64	14	5	ND	2	14	1	2	2	100	.19	.047	13	15	.82	55	.27	36	3.17	.03	.16	1	1
SA 800E+175N	17	215	210	166	4.8	1	23	60016	15.57	69	9	ND	1	5	4	3	11	42	.05	.096	25	18	.24	79	.05	2	6.54	.01	.03	1	195
SA 800E+150N	15	34	17	144	.3	6	10	631	6.91	13	5	ND	1	11	1	2	2	157	.20	.069	8	30	1.05	44	.30	4	3.94	.02	.20	1	5
SA 800E+125N	10	43	30	87	.6	4	8	2167	5.94	15	5	ND	1	12	1	2	3	118	.22	.084	7	30	.91	40	.28	2	3.74	.02	.12	3	3
SA 800E+100N	16	20	14	79	.4	2	6	525	5.92	21	5	ND	1	7	1	2	5	100	.07	.052	18	22	.42	21	.18	3	3.43	.02	.09	1	1
SA 800E+75N	3	21	48	106	.4	5	12	652	7.32	10	5	ND	1	8	1	3	5	242	.21	.057	6	33	1.60	72	.48	2	3.44	.02	.39	1	1
SA 800E+50N	5	24	27	98	.3	2	7	369	5.22	23	5	ND	1	7	1	2	2	112	.16	.075	6	13	.65	21	.20	3	3.38	.02	.05	1	1
STD C/AU-S	19	59	38	128	7.4	70	28	1031	4.14	38	19	7	36	48	18	17	25	55	.51	.088	36	61	.91	171	.08	37	1.83	.06	.13	13	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 800E+25N	9	31	19	146	.1	3	10	614	5.52	25	5	ND	2	8	1	6	9	119	.19	.067	8	10	1.20	42	.24	2	3.63	.02	.20	1	2
SA 800E+00N	9	58	9	159	.1	6	15	862	6.26	39	5	ND	3	19	1	2	4	159	.45	.084	6	14	1.56	50	.29	4	4.15	.03	.27	1	3
SA 800E+00	7	97	162	124	.3	6	9	583	4.51	18	5	ND	1	14	1	2	18	105	.31	.120	9	10	1.03	42	.16	2	4.88	.02	.23	1	1
SA 800E+75S	6	42	4	109	.1	3	9	793	5.41	17	5	ND	1	8	1	2	2	153	.13	.074	5	24	1.44	107	.23	2	3.86	.04	.48	1	1
SA 800E+100S	5	48	5	83	.2	3	6	593	5.93	14	5	ND	1	6	1	2	2	147	.11	.067	6	12	1.41	139	.28	2	3.76	.02	.49	1	2
SA 800E+125S	6	42	3	74	.1	4	5	613	5.22	21	5	ND	1	7	1	3	2	150	.15	.079	6	18	1.45	87	.27	2	3.41	.04	.50	1	2
SA 800E+150S	4	48	13	2125	.1	12	19	1149	6.37	65	5	ND	1	24	2	2	11	214	.72	.090	6	34	1.71	83	.23	2	4.73	.04	.22	1	4
SA 800E+175S	6	136	8	374	.1	26	74	2718	5.79	13	5	ND	2	25	3	2	2	129	.50	.168	8	27	1.21	107	.18	2	6.60	.03	.30	1	1
SA 800E+200S	2	100	13	173	.1	26	24	858	9.64	7	5	ND	1	14	1	2	2	275	.21	.064	5	61	3.23	406	.46	6	6.30	.05	1.02	1	22
SA 800E+225S	7	16	16	98	.1	6	6	617	8.10	17	5	ND	1	6	1	2	2	61	.07	.074	21	34	.35	19	.15	7	3.38	.03	.05	1	1
SA 800E+250S	3	95	11	96	.1	9	10	262	6.03	14	5	ND	1	10	1	2	3	180	.15	.053	6	50	.60	26	.64	2	2.81	.01	.05	1	2
SA 800E+275S	1	36	8	95	.1	8	19	976	7.59	2	5	ND	1	5	1	2	2	215	.18	.072	3	8	2.85	98	.37	9	5.22	.02	1.34	1	1
SA 800E+300S	4	41	18	78	.1	8	10	521	6.60	13	5	ND	2	6	1	2	9	160	.11	.047	7	41	1.11	53	.42	2	3.60	.02	.20	1	1
SA 800E+325S	4	38	15	76	.1	19	10	477	6.90	13	5	ND	1	5	1	2	2	149	.04	.045	7	61	1.00	30	.33	2	3.83	.01	.17	1	1
SA 800E+350S	9	17	24	115	.1	9	9	695	8.83	13	5	ND	3	5	1	2	2	101	.07	.053	20	34	.97	42	.27	2	4.52	.04	.27	1	1
SA 800E+375S	5	40	20	76	.2	14	8	384	6.63	21	5	ND	4	7	1	2	2	82	.09	.058	13	34	.78	47	.27	3	4.07	.03	.17	1	44
SA 800E+400S	2	85	20	410	.1	16	15	727	5.45	2	5	ND	1	19	1	2	2	130	.39	.097	5	49	1.62	35	.29	2	5.73	.09	.54	1	1
SA 800E+425S	4	65	11	98	.1	23	12	671	5.87	9	5	ND	1	6	1	2	8	140	.08	.054	7	50	1.81	50	.32	2	4.24	.02	.45	1	3
SA 800E+450S	4	61	9	71	.1	39	8	378	4.72	23	5	ND	1	9	1	2	2	116	.14	.071	7	121	1.14	31	.37	2	3.53	.03	.29	1	1
SA 800E+475S	8	32	5	98	.1	17	8	401	5.29	16	5	ND	3	8	1	2	2	69	.13	.073	14	24	.82	36	.23	2	3.54	.03	.18	1	2
SA 800E+500S	2	65	5	122	.1	53	19	840	6.99	16	5	ND	2	6	1	2	2	170	.17	.083	6	122	2.62	127	.40	3	4.67	.02	1.13	1	1
STD C/AU-S	21	61	42	132	7.4	67	29	1052	3.97	39	17	8	39	51	19	16	21	60	.47	.092	39	58	.87	179	.08	37	1.95	.06	.12	13	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-01	21	778	15219	15806	30.8	2	13	1553	4.67	20	5	ND	2	4	184	2	18	56	.21	.061	2	1	1.11	11	.01	2	1.90	.02	.13	1	9
SK-02	34	1252	16291	48142	53.2	8	36	969	4.56	38	5	ND	7	10	729	7	2	11	.57	.028	3	1	.23	27	.01	10	.67	.02	.22	1	2405
SK-03	32	3524	3754	52463	44.0	4	32	1838	6.43	16	5	ND	3	24	671	2	2	69	.94	.092	3	2	1.34	26	.01	3	2.53	.01	.19	1	18
SK-04	36	4856	24058	48332	238.9	3	25	524	3.78	21	5	9	1	1	627	30	20	26	.07	.037	2	1	.40	15	.01	2	.91	.01	.12	1	15500
SK-05	5	192	1832	1130	14.3	2	8	1035	5.47	20	5	ND	1	3	7	2	5	75	.19	.110	3	1	1.09	33	.01	2	2.15	.01	.23	1	42
SK-06	41	388	733	1212	76.6	2	2	55	2.15	8	5	ND	1	1	15	2	13	4	.01	.005	2	1	.02	4	.01	2	.13	.01	.03	1	880
SK-07	4	281	3276	1591	11.0	4	4	362	2.04	8	5	ND	1	1	19	2	7	17	.06	.028	2	1	.32	11	.01	2	.70	.01	.10	1	1380
SK-08	5	271	992	434	45.0	2	3	210	1.62	11	5	15	1	1	4	2	12	12	.01	.009	2	2	.17	3	.01	2	.36	.01	.03	1	8850
SK-09	17	240	1282	1071	15.9	1	2	90	1.39	7	5	ND	14	1	14	2	5	4	.02	.013	3	1	.13	27	.01	3	.44	.01	.21	1	1500
SK-10	18	573	20892	14161	55.7	16	61	75	16.72	14	5	ND	3	1	209	9	2	4	.01	.007	2	1	.02	4	.01	2	.01	.01	.05	1	330
SK-11	28	516	9958	1669	70.7	3	5	469	3.59	16	5	ND	1	1	21	10	10	26	.03	.021	2	1	.40	7	.01	22	.80	.01	.05	1	164
SK-12	42	4661	24974	55768	113.7	3	13	94	2.04	11	5	ND	1	1	880	36	2	3	.01	.002	2	1	.02	2	.01	2	.07	.01	.01	1	1650
SK-13	3	80	4897	69	24.4	5	2	83	1.18	4	5	ND	1	1	1	4	14	4	.01	.006	2	1	.04	2	.01	2	.11	.01	.01	1	350
SK-14	6	414	18321	2658	96.9	2	6	240	2.67	22	5	3	1	1	41	21	19	15	.01	.008	2	2	.19	5	.01	2	.40	.01	.03	1	6320
SK-15	48	7798	23896	84062	322.2	3	39	274	3.05	24	5	ND	1	1	1040	37	5	8	.02	.016	2	1	.08	8	.01	2	.29	.01	.07	1	1320
SK-16	4	134	3362	504	11.8	3	10	1749	7.77	16	5	ND	2	5	3	2	2	110	.25	.126	3	1	1.83	38	.03	3	3.30	.01	.22	1	720
SK-17	4	354	2891	688	71.7	6	5	400	3.23	12	5	ND	1	1	7	2	11	21	.06	.034	2	2	.34	12	.01	2	.77	.01	.11	1	1990
SK-18	129	25	383	164	7.7	4	1	122	1.16	4	5	7	1	1	1	4	5	8	.01	.008	2	1	.08	6	.01	2	.23	.01	.07	1	1050
SK-19	10	420	25699	1863	83.3	3	2	58	2.79	7	5	ND	1	1	27	14	19	5	.01	.008	2	2	.02	7	.01	2	.17	.01	.05	1	74
SK-20	10	115	214	33	.6	10	11	159	3.79	6	5	ND	2	43	1	2	7	70	1.10	.086	5	17	.26	23	.18	7	1.39	.18	.07	4	1
SK-21	3	38	668	50	1.4	8	3	197	2.04	5	5	ND	2	17	1	4	6	56	.18	.030	2	5	.25	216	.08	2	.66	.04	.32	1	2
SK-22	2	64	110	34	.4	200	19	175	2.09	12	5	ND	1	154	1	2	2	37	2.28	.121	3	327	1.34	9	.07	4	2.61	.14	.05	1	7
SK-23	9	20	265	166	1.1	6	3	304	1.88	6	5	ND	1	9	1	2	5	24	.27	.024	2	4	.41	18	.02	6	.93	.03	.10	1	1
SK-23A	2	31	15	69	.1	9	9	792	4.04	14	5	ND	3	11	1	2	2	98	.30	.081	7	26	1.56	113	.30	2	1.88	.07	1.41	1	2
SK-24	2	40	29	93	.2	16	7	723	4.12	12	5	ND	3	108	1	2	2	91	1.78	.079	3	36	1.44	37	.17	6	4.20	.30	.39	4	1
SK-25	3	68	9	69	.3	11	9	505	3.51	14	5	ND	3	75	1	2	3	54	2.22	.103	4	14	.87	23	.15	2	3.64	.18	.15	1	1
SK-26	3	85	102	956	1.0	4	7	535	1.92	12	5	ND	1	91	11	2	7	42	6.39	.098	2	1	.51	32	.10	2	1.34	.03	.05	1	1
SK-27	14	34	221	604	1.2	2	4	141	.76	5	5	ND	1	1	2	2	3	4	.01	.004	2	2	.07	8	.01	2	.18	.01	.04	2	1
SK-28	1	61	14	71	.4	3	10	638	3.64	13	5	ND	2	87	1	2	6	85	2.84	.101	3	1	1.29	136	.10	4	2.19	.09	.53	1	5
SK-29	4	10	27	683	.7	5	3	314	.99	4	5	ND	1	1	5	2	6	6	.18	.004	2	1	.15	5	.01	2	.25	.01	.03	1	1
SK-30	13	169	291	3981	5.4	3	4	136	.82	4	5	ND	1	1	48	2	3	6	.01	.004	2	2	.09	3	.01	10	.17	.01	.01	1	11
SK-31	54	4171	5681	95264	50.3	7	48	601	3.54	17	5	ND	1	37	1172	2	2	58	.53	.023	2	5	.29	13	.01	2	1.55	.01	.10	1	250
SK-32	6	34	99	473	.1	12	8	548	2.40	22	5	ND	1	1	1	2	3	30	.08	.034	2	12	.43	21	.01	2	1.01	.01	.16	1	1
SK-33	49	232	690	4488	2.1	7	12	856	3.27	22	6	ND	2	25	8	2	2	124	.34	.060	4	14	.81	21	.01	2	1.94	.01	.21	1	8
SK-34	39	126	741	3969	1.0	8	9	868	3.11	27	5	ND	1	24	7	2	6	70	.30	.049	4	6	.70	16	.01	8	1.58	.01	.18	1	3
SK-35	1889	247	25198	8609	327.4	6	10	352	1.88	49	9	ND	1	10	12	8	419	33	.16	.013	2	4	.37	11	.01	2	.83	.01	.08	17	620
STD C/AU-R	19	60	38	132	7.0	67	27	1034	3.72	41	19	7	37	49	18	18	22	56	.48	.087	36	59	.88	173	.08	37	1.85	.06	.14	12	490

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-36	183	654	1558	41211 ✓	9.8	13	25	516	3.58	30	5	ND	2	24	518	2	3	23	.45	.052	2	6	.69	18	.01	3	1.32	.01	.18	1	35
SK-37	80	59	6691	630	3.4	4	3	99	.54	5	5	ND	1	2	4	2	5	2	.01	.001	2	2	.03	[illegible]	.01	2	.07	.01	.02	1	6
SK-38	58	20	846	622	1.0	4	4	139	.75	2	8	ND	1	1	2	5	3	8	.04	.009	2	1	.09	6	.01	2	.18	.01	.06	1	1
SK-39	2	44	48	119	.6	15	8	328	2.21	10	5	ND	3	136	1	2	6	45	2.94	.077	4	13	.54	22	.12	10	3.12	.10	.16	1	1
SK-40	3	71	405	814	.5	12	6	920	2.70	5	5	ND	3	63	12	2	2	55	2.54	.056	6	9	.63	16	.01	2	1.68	.01	.22	1	1
SK-41	10	30	18	144	.2	13	4	457	3.63	4	5	ND	3	64	2	5	6	54	1.16	.038	5	13	.93	48	.16	3	2.22	.09	.44	1	1
SK-42	2	49	31	97	.1	131	24	663	5.07	12	5	ND	3	188	1	2	4	82	2.96	.174	26	35	3.61	331	.55	2	3.23	.32	.15	1	1
SK-44	1	51	28	72	.2	1	12	808	4.51	2	5	ND	3	67	1	2	5	85	2.97	.123	4	3	1.12	206	.18	8	2.57	.13	.63	1	1
SK-45	3	8	18	336	.1	8	3	622	1.33	4	5	ND	1	18	11	2	2	12	1.10	.012	2	2	.28	14	.02	2	.43	.01	.04	1	1
SK-46	57	66	1335	507	2.1	2	4	303	1.98	6	5	ND	1	1	1	2	3	15	.04	.019	2	5	.26	11	.01	6	.52	.01	.11	1	1
SK-47	5	31	9	146	.2	21	6	278	2.70	4	5	ND	2	82	2	2	3	76	1.71	.061	2	23	.52	30	.12	2	2.06	.10	.26	1	1
SK-48	1	21	302	235	.3	4	4	487	2.23	2	5	ND	11	15	1	3	3	20	.20	.046	15	3	.44	98	.08	2	.79	.04	.15	1	3
SK-49	1	16	17	65	.1	2	6	640	2.13	4	6	ND	2	130	1	2	2	37	2.13	.128	4	1	.31	20	.12	2	1.30	.01	.02	1	2
SK-50	1	53	30	122	.5	3	15	1068	5.93	5	5	ND	3	16	1	2	4	127	.68	.181	5	3	1.71	132	.24	13	2.20	.05	.83	1	1
SK-51	5	360	1362	1956	5.6	6	9	412	2.60	5	5	ND	2	9	18	2	4	29	.16	.018	2	2	.52	10	.01	2	.91	.01	.08	3	57
SK-52	2	68	27	81	.4	18	10	183	2.09	10	5	ND	3	56	1	3	2	48	2.29	.095	4	24	.30	25	.12	5	2.73	.19	.12	1	2
SK-53	3	36	30	112	.1	79	24	936	6.21	2	5	ND	1	108	1	2	4	89	3.38	.160	19	97	3.53	159	.28	6	2.67	.14	.22	1	2
SK-54	4	94	20	54	.5	17	14	362	6.13	2	5	ND	3	125	1	2	5	91	1.51	.194	4	27	1.34	79	.19	2	3.08	.24	.42	2	9
SK-55	1	44	32	22	.3	3	4	289	1.99	4	5	ND	2	232	1	2	2	48	2.34	.117	4	3	.19	6	.12	2	1.76	.09	.05	1	1
SK-56	1	7	5	7	.1	1	1	72	.53	2	5	ND	17	1	1	3	2	2	.01	.002	5	1	.02	4	.01	2	.15	.04	.06	1	1
SK-57	1	5	23	70	.1	7	7	276	2.10	2	5	ND	11	25	1	2	5	19	.34	.058	14	6	.56	30	.09	2	.93	.04	.10	1	2
SK-58	1	54	11	65	.3	7	11	657	4.09	4	5	ND	3	26	1	2	2	79	.90	.115	4	10	1.13	64	.21	2	1.54	.08	.48	1	1
SK-59	5	87	18	96	.5	17	14	910	5.83	9	5	ND	5	20	1	2	2	140	.91	.146	4	44	1.84	50	.24	2	2.92	.04	.82	1	1
SK-60	10	57	7	71	.3	6	9	655	4.64	2	5	ND	4	60	1	2	2	103	2.42	.097	4	14	1.36	79	.24	3	4.14	.20	.75	1	1
SK-61	1	55	9	80	.5	12	12	983	5.15	7	5	ND	3	65	1	2	5	123	1.18	.105	4	25	1.85	202	.25	11	3.54	.26	1.13	1	3
SK-62	2	80	9	42	.7	9	10	403	4.53	20	5	ND	4	96	1	2	2	101	1.42	.105	5	36	.95	26	.15	4	2.52	.19	.18	1	1
SK-63	1	3	2	11	.1	2	1	261	.43	2	5	ND	15	2	1	2	2	2	.01	.001	6	1	.02	2	.01	2	.14	.05	.05	1	2
SK-64	9	49	10	83	.5	17	9	678	5.25	13	5	ND	4	19	1	2	2	169	.69	.087	3	32	1.79	40	.27	12	2.71	.10	.96	1	1
SK-65	7	80	20	96	.6	29	14	352	4.93	6	5	ND	3	87	1	2	4	119	2.96	.090	4	35	1.23	24	.18	2	4.39	.13	.42	2	2
SK-66	10	7921	17183 ✓	10579	101.7 ✓	4	47	103	4.31	78	5	ND	1	1	127	2	2	3	.01	.004	2	1	.05	7	.01	7	.12	.01	.04	9	220
SK-67	13	28	15	7	.2	4	5	42	1.11	2	5	ND	1	2	1	4	2	4	.01	.001	2	2	.04	3	.01	8	.08	.01	.01	35	1
SK-68	1	7	4	37	.1	3	1	166	.63	2	5	ND	18	2	1	2	2	3	.02	.001	11	1	.03	2	.03	8	.21	.04	.06	2	3
SK-69	20	158	621	5270	6.5	3	7	581	2.48	4	5	ND	2	21	85	2	2	22	.94	.043	2	2	.42	19	.01	6	.77	.01	.15	4	36
STD C/AU-R	19	59	40	132	7.2	71	28	1050	4.32	38	18	8	40	51	19	18	20	58	.52	.087	38	60	.90	182	.08	35	1.80	.06	.14	13	510

ASSAY REQUIRED FOR ✓

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 27 1987 DATE REPORT MAILED: Sept 4/87 ASSAYER. D. Toye. DEAN TOYE, CERTIFIED B.C. ASSAYER

SHANGRI-LA File # 87-3690 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SBG 00E+600N	1	40	12	103	.1	15	11	619	4.82	7	5	ND	5	10	1	2	2	117	.13	.038	9	45	1.44	75	.32	2	3.18	.04	.55	1	1
SBG 00E+575N	2	180	17	86	.3	12	14	615	5.26	9	5	ND	3	19	1	2	2	130	.30	.084	6	13	1.52	188	.27	2	3.04	.05	.52	1	3
SBG 00E+547N	1	125	10	97	.1	11	19	669	5.91	4	5	ND	1	12	1	2	2	178	.25	.064	3	8	2.40	364	.33	2	3.96	.06	.98	1	1
SBG 00E+525N	1	71	7	82	.1	12	14	556	5.36	8	5	ND	1	22	1	2	2	149	.20	.060	3	18	1.59	54	.26	2	5.83	.08	.59	2	1
SBG 00E+500N	2	44	17	76	.1	10	9	419	5.66	6	5	ND	6	13	1	2	2	121	.26	.077	11	22	1.22	95	.28	2	3.86	.06	.32	1	2
SBG 00E+475N	1	183	8	164	.2	50	44	1312	8.58	4	5	ND	2	32	1	2	5	257	.72	.094	4	107	4.08	500	.47	2	6.54	.04	.69	1	2
SBG 00E+450N	1	107	18	77	.3	13	13	535	5.96	8	5	ND	1	9	1	2	2	182	.19	.054	4	76	2.21	249	.38	5	3.92	.06	.87	1	1
SBG 00E+425N	1	75	17	84	.3	15	12	450	4.74	7	5	ND	3	31	1	2	2	115	.27	.084	8	23	1.48	235	.27	2	3.01	.04	.47	1	1
SBG 00E+400N	1	115	12	89	.3	16	17	511	5.50	6	5	ND	1	25	1	2	2	142	.33	.077	4	20	1.78	170	.31	2	3.99	.07	.53	1	6
SBG 00E+375N	1	72	37	89	.7	14	12	457	4.56	15	5	ND	4	23	1	2	2	111	.38	.100	8	21	1.59	180	.25	6	2.87	.05	.53	1	1
SBG 00E+350N	1	168	7	156	.4	27	31	1223	6.99	6	5	ND	4	74	1	2	4	202	.69	.109	12	47	3.04	243	.33	2	5.78	.10	.82	1	1
SBG 00E+335N	1	68	24	115	.4	23	15	646	4.98	7	5	ND	5	25	1	2	2	117	.40	.118	14	34	1.50	112	.27	2	3.44	.06	.28	1	2
SBG 00E+300N	1	83	14	104	.1	11	14	670	5.77	8	5	ND	1	13	1	2	2	147	.21	.078	6	23	1.77	235	.35	2	3.68	.04	.67	2	1
SBG 00E+275N	1	33	11	107	.1	6	16	947	6.41	6	5	ND	1	6	1	2	2	159	.13	.065	4	11	2.69	436	.40	2	3.95	.03	1.46	1	1
SBG 00E+250N	2	72	6	95	.2	6	11	715	6.06	3	5	ND	2	10	1	2	3	143	.21	.092	4	21	2.27	376	.38	2	3.52	.05	.92	1	1
SBG 00E+225N	1	25	7	116	.2	6	12	646	6.62	7	5	ND	1	47	1	4	2	143	.59	.169	5	18	2.63	308	.30	2	4.62	.13	.83	1	1
SBG 00E+200N	1	52	14	84	.2	7	9	527	6.31	4	5	ND	3	10	1	3	2	190	.19	.101	4	43	2.36	577	.42	2	3.08	.05	1.21	1	2
SBG 00E+175N	1	84	2	71	.3	27	12	389	5.29	8	5	ND	1	15	1	2	2	166	.20	.076	5	101	1.81	109	.39	2	5.71	.07	.32	1	1
SBG 00E+150N	1	39	8	89	.1	16	15	573	5.21	6	5	ND	2	15	1	2	2	138	.19	.055	5	37	2.00	234	.33	2	3.67	.04	.54	1	1
SBG 00E+125N	6	72	22	92	.4	18	9	415	4.25	12	5	ND	3	24	1	2	2	97	.30	.105	9	35	1.32	91	.24	5	2.90	.05	.26	1	1
SBG 00E+100N	3	47	17	72	.5	21	8	350	5.13	8	5	ND	3	13	1	2	2	120	.25	.085	11	54	1.23	119	.38	6	3.49	.05	.27	1	1
SBG 00E+75N	1	66	16	93	.2	34	14	539	5.43	8	5	ND	2	7	1	2	2	154	.20	.079	4	86	1.83	96	.29	2	4.28	.04	.69	1	1
SBG 00E+50N	3	66	8	100	.1	17	12	583	5.91	4	5	ND	2	8	1	2	2	188	.20	.073	4	48	1.89	192	.31	2	4.57	.04	.69	1	1
SBG 00E+25N	1	77	14	115	.3	18	16	742	5.77	8	5	ND	3	6	1	4	2	184	.29	.116	5	40	2.22	452	.34	2	3.53	.03	1.01	1	1
SBG 00E+00S	1	121	10	95	.3	26	10	606	5.96	3	5	ND	2	8	1	2	2	180	.19	.105	2	101	2.66	457	.37	2	3.66	.04	1.45	1	1
SBG 00E+26S	3	42	21	73	.2	12	7	434	3.64	5	5	ND	1	15	1	2	2	83	.11	.089	10	30	.87	34	.10	5	3.03	.02	.08	1	2
SBG 00E+50S	2	19	15	57	.2	3	5	258	3.49	4	5	ND	1	7	1	2	2	90	.11	.092	9	16	.64	19	.33	2	2.04	.04	.12	1	1
SBG 00E+75S	1	57	9	80	.2	8	12	425	5.72	7	5	ND	2	6	1	2	2	145	.13	.071	6	25	1.45	82	.25	2	4.98	.03	.32	1	1
SBG 00E+100S	2	49	11	83	.1	5	11	520	5.44	2	5	ND	1	4	1	2	2	143	.09	.067	4	9	1.60	159	.27	2	3.07	.03	.48	1	1
SBG 00E+125S	3	61	14	125	.3	16	15	835	6.66	7	5	ND	1	42	1	2	2	174	.58	.117	4	40	2.46	99	.35	2	5.60	.17	.92	1	2
SBG 00E+150S	4	55	16	91	.3	12	9	558	5.88	6	5	ND	3	12	1	2	2	153	.25	.095	6	42	1.96	156	.31	7	3.64	.04	.49	1	1
SBG 00E+175S	2	176	17	101	.4	20	16	558	6.01	7	6	ND	3	433	1	2	2	141	.64	.132	7	28	1.72	153	.25	2	3.45	.05	.70	1	1
SBG 00E+200S	2	82	19	106	.2	18	10	515	5.40	7	5	ND	6	36	1	2	2	124	.28	.097	8	43	1.75	135	.29	7	3.23	.05	.52	1	1
SBG 00E+225S	3	89	16	104	.3	23	12	528	4.97	6	5	ND	4	20	1	2	2	118	.29	.103	10	47	1.65	113	.27	5	3.98	.05	.36	1	2
SBG 00E+252S	2	90	27	88	.2	48	12	388	4.48	9	5	ND	2	26	1	2	2	95	.44	.105	10	114	1.72	96	.26	2	3.26	.05	.23	1	1
SBG 00E+274S	2	117	29	89	.4	54	12	388	4.23	14	5	ND	3	23	1	2	2	85	.38	.072	5	125	1.98	108	.19	2	2.60	.05	.31	4	2
STD C/AU-S	20	61	39	132	7.5	73	28	1056	4.07	39	21	8	38	52	18	18	20	59	.50	.093	38	61	.91	178	.08	34	1.92	.07	.14	13	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SBG 00E+300S	6	75	17	5	.4	60	11	339	4.72	12	6	ND	7	15	1	2	2	77	.22	.109	14	79	1.25	67	.22	2	3.44	.04	.15	1	1
SBG 00E+325S	1	32	11	45	.1	108	14	190	3.07	3	5	ND	1	8	1	2	2	76	.10	.032	3	216	2.29	104	.16	3	2.57	.03	.31	1	1
SBG 00E+350S	5	51	25	107	.3	30	10	351	6.57	10	5	ND	3	4	1	4	2	150	.05	.053	11	85	2.09	114	.33	2	3.57	.03	.26	1	2
SBG 00E+374S	2	60	17	87	.2	41	12	380	4.90	6	5	ND	3	15	1	2	2	95	.20	.065	6	93	1.53	58	.20	3	3.09	.03	.11	1	2
SBG 00E+400S	2	50	14	77	.2	37	11	410	3.78	4	5	ND	4	18	1	2	2	93	.22	.044	8	73	1.46	64	.20	2	3.04	.03	.09	2	9
SBG 00E+425S	4	42	13	71	.4	21	7	353	4.60	5	5	ND	5	9	1	2	2	80	.16	.076	13	47	1.11	54	.24	2	2.90	.04	.17	1	1
SBG 00E+450S	3	84	15	80	.3	47	12	486	4.67	3	5	ND	2	7	1	3	2	147	.22	.084	7	87	2.12	52	.29	2	3.26	.03	.32	1	1
SBG 00E+475S	2	24	32	51	.1	8	4	169	3.61	5	5	ND	3	9	1	2	2	66	.10	.139	12	20	.47	43	.23	2	2.55	.03	.06	1	1
SBG 00E+495S	2	28	18	53	.1	7	5	182	3.26	8	5	ND	2	9	1	2	2	65	.07	.077	7	11	.49	39	.14	2	1.98	.02	.06	1	2
SBG 00E+525S	1	9	15	29	.1	1	2	85	1.45	3	5	ND	1	65	1	2	3	45	.06	.053	5	5	.17	51	.13	2	1.20	.01	.03	1	1
SBG 00E+550S	4	21	18	44	.1	9	4	159	3.09	3	5	ND	1	36	1	2	2	65	.27	.072	8	23	.47	32	.14	2	2.38	.02	.07	1	4
STD C/AU-S	19	59	39	132	7.3	69	28	1055	4.04	42	23	7	37	50	19	18	21	58	.48	.090	37	58	.89	181	.08	37	1.87	.07	.12	13	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-01	21	778	15219	15806	30.8	2	13	1553	4.67	20	5	ND	2	4	184	2	18	56	.21	.061	2	1	1.11	11	.01	2	1.90	.02	.13	1	9
SK-02	34	1252	16291	48142	53.2	8	36	969	4.56	38	5	ND	7	10	729	7	2	11	.57	.028	3	1	.23	27	.01	10	.67	.02	.22	1	2405
SK-03	32	3524	3754	52463	44.0	4	32	1838	6.43	16	5	ND	3	24	671	2	2	69	.94	.092	3	2	1.34	26	.01	3	2.53	.01	.19	1	18
SK-04	36	4856	24058	48332	238.9	3	25	524	3.78	21	5	9	1	1	627	30	20	26	.07	.037	2	1	.40	15	.01	2	.91	.01	.12	1	15500
SK-05	5	192	1832	1130	14.3	2	8	1035	5.47	20	5	ND	1	3	7	2	5	75	.19	.110	3	1	1.09	33	.01	2	2.15	.01	.23	1	42
SK-06	41	388	733	1212	76.6	2	2	55	2.15	8	5	ND	1	1	15	2	13	4	.01	.005	2	1	.02	4	.01	2	.13	.01	.03	1	880
SK-07	4	281	3276	1591	11.0	4	4	362	2.04	8	5	ND	1	1	19	2	7	17	.06	.028	2	1	.32	11	.01	2	.70	.01	.10	1	1380
SK-08	5	271	992	434	45.0	2	3	210	1.62	11	5	15	1	1	4	2	12	12	.01	.009	2	2	.17	3	.01	2	.36	.01	.03	1	8850
SK-09	17	240	1282	1071	15.9	1	2	90	1.39	7	5	ND	14	1	14	2	5	4	.02	.013	3	1	.13	27	.01	3	.44	.01	.21	1	1500
SK-10	18	573	20892	14161	55.7	16	61	75	16.72	14	5	ND	3	1	209	9	2	4	.01	.007	2	1	.02	4	.01	2	.01	.01	.05	1	330
SK-11	28	516	9958	1669	70.7	3	5	469	3.59	16	5	ND	1	1	21	10	10	26	.03	.021	2	1	.40	7	.01	22	.80	.01	.05	1	164
SK-12	42	4661	24974	55768	113.7	3	13	94	2.04	11	5	ND	1	1	880	36	2	3	.01	.002	2	1	.02	2	.01	2	.07	.01	.01	1	1650
SK-13	3	80	4897	69	24.4	5	2	83	1.18	4	5	ND	1	1	1	4	14	4	.01	.006	2	1	.04	2	.01	2	.11	.01	.01	1	350
SK-14	6	414	18321	2858	96.9	2	6	240	2.67	22	5	3	1	1	41	21	19	15	.01	.008	2	2	.19	5	.01	2	.40	.01	.03	1	6320
SK-15	48	7798	23896	84062	322.2	3	39	274	3.05	24	5	ND	1	1	1040	37	5	8	.02	.016	2	1	.08	8	.01	2	.29	.01	.07	1	1320
SK-16	4	134	3362	504	11.8	3	10	1749	7.77	16	5	ND	2	5	3	2	2	110	.25	.126	3	1	1.83	38	.03	3	3.30	.01	.22	1	720
SK-17	4	354	2891	688	71.7	6	5	400	3.23	12	5	ND	1	1	7	2	11	21	.06	.034	2	2	.34	12	.01	2	.77	.01	.11	1	1990
SK-18	129	25	383	164	7.7	4	1	122	1.16	4	5	7	1	1	1	4	5	8	.01	.008	2	1	.08	6	.01	2	.23	.01	.07	1	1050
SK-19	10	420	25699	1863	83.3	3	2	58	2.79	7	5	ND	1	1	27	14	19	5	.01	.008	2	2	.02	7	.01	2	.17	.01	.05	1	74
SK-20	10	115	214	33	.6	10	11	159	3.79	6	5	ND	2	43	1	2	7	70	1.10	.086	5	17	.26	23	.18	7	1.39	.18	.07	4	1
SK-21	3	38	668	50	1.4	8	3	187	2.04	5	5	ND	2	17	1	4	6	56	.18	.030	2	5	.25	216	.08	2	.66	.04	.32	1	2
SK-22	2	64	110	34	.4	200	19	175	2.09	12	5	ND	1	154	1	2	2	37	2.28	.121	3	327	1.34	9	.07	4	2.61	.14	.05	1	7
SK-23	9	20	265	166	1.1	6	3	304	1.88	6	5	ND	1	9	1	2	5	24	.27	.024	2	4	.41	18	.02	6	.93	.03	.10	1	1
SK-23A	2	31	15	69	.1	9	9	792	4.04	14	5	ND	3	11	1	2	2	98	.30	.081	7	26	1.56	113	.30	2	1.88	.07	1.41	1	2
SK-24	2	40	29	93	.2	16	7	723	4.12	12	5	ND	3	108	1	2	2	91	1.78	.079	3	36	1.44	37	.17	6	4.20	.30	.39	4	1
SK-25	3	68	9	69	.3	11	9	505	3.51	14	5	ND	3	75	1	2	3	54	2.22	.103	4	14	.87	23	.15	2	3.64	.18	.15	1	1
SK-26	3	85	102	956	1.0	4	7	535	1.92	12	5	ND	1	91	11	2	7	42	6.39	.098	2	1	.51	32	.10	2	1.34	.03	.05	1	1
SK-27	14	34	221	604	1.2	2	4	141	.76	5	5	ND	1	1	2	2	3	4	.01	.004	2	2	.07	8	.01	2	.18	.01	.04	2	1
SK-28	1	61	14	71	.4	3	10	638	3.64	13	5	ND	2	87	1	2	6	85	2.84	.101	3	1	1.29	136	.10	4	2.19	.09	.53	1	5
SK-29	4	10	27	683	.7	5	3	314	.99	4	5	ND	1	1	5	2	6	6	.18	.004	2	1	.15	5	.01	2	.25	.01	.03	1	1
SK-30	13	169	291	3981	5.4	3	4	136	.82	4	5	ND	1	1	48	2	3	6	.01	.004	2	2	.09	3	.01	10	.17	.01	.01	1	11
SK-31	54	4171	5681	95264	50.3	7	48	601	3.54	17	5	ND	1	37	1172	2	2	58	.53	.023	2	5	.29	13	.01	2	1.55	.01	.10	1	250
SK-32	6	34	99	473	.1	12	8	548	2.40	22	5	ND	1	1	1	2	3	30	.08	.034	2	12	.43	21	.01	2	1.01	.01	.16	1	1
SK-33	49	232	690	4488	2.1	7	12	856	3.27	22	6	ND	2	25	8	2	2	124	.34	.060	4	14	.81	21	.01	2	1.94	.01	.21	1	8
SK-34	39	126	741	3969	1.0	8	9	868	3.11	27	5	ND	1	24	7	2	6	70	.30	.049	4	6	.70	16	.01	8	1.58	.01	.18	1	3
SK-35	1889	247	25198	8609	327.4	6	10	352	1.88	49	9	ND	1	10	12	8	419	33	.16	.013	2	4	.37	11	.01	2	.83	.01	.08	17	620
STD C/AU-R	19	60	38	132	7.0	67	27	1034	3.72	41	19	7	37	49	18	18	22	56	.48	.087	36	59	.88	173	.08	37	1.85	.06	.14	12	490

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-36	183	654	1558	41211	9.8	13	25	516	3.58	30	5	ND	2	24	518	2	3	23	.45	.052	2	6	.69	18	.01	3	1.32	.01	.18	1	35
SK-37	80	59	6691	630	3.4	4	3	99	.54	5	5	ND	1	2	4	2	5	2	.01	.001	2	2	.03	2	.01	2	.07	.01	.02	1	6
SK-38	58	20	846	622	1.0	4	4	139	.75	2	8	ND	1	1	2	5	3	8	.04	.009	2	1	.09	6	.01	2	.18	.01	.06	1	1
SK-39	2	44	48	119	.6	15	8	328	2.21	10	5	ND	3	136	1	2	6	45	2.94	.077	4	13	.54	22	.12	10	3.12	.10	.16	1	1
SK-40	3	71	405	814	.5	12	6	920	2.70	5	5	ND	3	63	12	2	2	55	2.54	.056	6	9	.63	16	.01	2	1.68	.01	.22	1	1
SK-41	10	30	18	144	.2	13	4	457	3.63	4	5	ND	2	64	2	5	6	54	1.16	.038	5	13	.93	48	.16	3	2.22	.09	.44	1	1
SK-42	2	49	31	97	.1	131	24	663	5.07	12	5	ND	3	188	1	2	4	82	2.96	.174	26	35	3.61	331	.55	2	3.23	.32	.15	1	1
SK-44	1	51	28	72	.2	1	12	808	4.51	2	5	ND	3	67	1	2	5	85	2.97	.123	4	3	1.12	206	.18	8	2.57	.13	.63	1	1
SK-45	3	8	18	336	.1	8	3	622	1.33	4	5	ND	1	18	11	2	2	12	1.10	.012	2	2	.28	14	.02	2	.43	.01	.04	1	1
SK-46	57	66	1335	507	2.1	2	4	303	1.98	6	5	ND	1	1	2	2	3	15	.04	.019	2	5	.26	11	.01	6	.52	.01	.11	1	1
SK-47	5	31	9	146	.2	21	6	278	2.70	4	5	ND	2	82	2	2	3	76	1.71	.061	2	23	.52	30	.12	2	2.06	.10	.26	1	1
SK-48	1	21	202	235	.3	4	4	487	2.23	2	5	ND	11	15	1	3	3	20	.20	.046	15	3	.44	98	.08	2	.79	.04	.15	1	3
SK-49	1	16	17	65	.1	2	6	640	2.13	4	6	ND	2	120	1	2	2	37	2.13	.128	4	1	.31	20	.12	2	1.30	.01	.02	1	2
SK-50	1	53	30	122	.5	3	15	1066	5.93	5	5	ND	3	16	1	2	4	127	.68	.181	5	3	1.71	132	.24	13	2.20	.05	.83	1	1
SK-51	5	360	1362	1956	5.6	6	9	412	2.60	5	5	ND	2	9	18	2	4	29	.16	.018	2	2	.52	10	.01	2	.91	.01	.08	3	57
SK-52	2	68	27	81	.4	18	10	183	2.09	10	5	ND	3	56	1	2	2	48	2.29	.095	4	24	.30	25	.12	5	2.73	.15	.12	1	2
SK-53	3	36	30	112	.1	79	24	935	6.21	2	5	ND	1	108	1	2	4	89	3.38	.160	19	97	3.53	159	.28	6	2.67	.14	.22	1	2
SK-54	4	94	20	54	.5	17	14	362	6.13	2	5	ND	3	125	1	2	5	91	1.51	.194	4	27	1.34	79	.19	2	3.08	.24	.42	2	9
SK-55	1	44	32	22	.3	3	4	289	1.99	4	5	ND	2	232	1	2	2	48	2.34	.117	4	3	.19	6	.12	2	1.76	.09	.05	1	1
SK-56	1	7	5	7	.1	1	1	72	.53	2	5	ND	17	1	1	3	2	2	.01	.002	5	1	.03	4	.01	2	.15	.04	.06	1	1
SK-57	1	5	23	70	.1	7	7	276	2.10	2	5	ND	11	25	1	2	5	19	.34	.058	14	6	.56	30	.09	2	.93	.04	.10	1	2
SK-58	1	54	11	65	.3	7	11	657	4.09	4	5	ND	3	26	1	2	2	79	.90	.115	4	10	1.13	64	.21	2	1.54	.06	.48	1	1
SK-59	5	87	18	96	.5	17	14	910	5.83	9	5	ND	5	20	1	2	2	140	.91	.146	4	44	1.84	50	.24	2	2.92	.04	.82	1	1
SK-60	10	57	7	71	.3	6	9	655	4.64	2	5	ND	4	60	1	2	2	103	2.42	.097	4	14	1.36	79	.24	3	4.14	.20	.75	1	1
SK-61	1	55	9	80	.5	12	12	983	5.15	7	5	ND	3	65	1	2	5	123	1.18	.105	4	25	1.85	202	.25	11	3.54	.26	1.13	1	3
SK-62	2	80	9	42	.7	9	10	403	4.53	20	5	ND	4	96	1	2	2	101	1.42	.105	5	36	.95	26	.15	4	2.52	.19	.18	1	1
SK-63	1	3	2	11	.1	2	1	261	.43	2	5	ND	15	2	1	2	2	2	.01	.001	6	1	.02	2	.01	2	.14	.05	.05	1	2
SK-64	9	49	10	83	.5	17	9	678	5.25	13	5	ND	4	19	1	2	2	169	.69	.087	3	32	1.79	40	.27	12	2.71	.10	.96	1	1
SK-65	7	80	20	96	.6	29	14	352	4.93	6	5	ND	3	87	1	2	4	119	2.96	.090	4	35	1.23	24	.18	2	4.39	.13	.42	2	2
SK-66	10	7921	17183	10579	101.7	4	47	103	4.31	78	5	ND	1	1	127	2	2	3	.01	.004	2	1	.05	7	.01	7	.12	.01	.04	9	220
SK-67	13	28	15	7	.2	4	5	42	1.11	2	5	ND	1	2	1	4	2	4	.01	.001	2	2	.04	3	.01	8	.08	.01	.01	35	1
SK-68	1	7	4	37	.1	3	1	166	.63	2	5	ND	18	2	1	2	2	3	.02	.001	11	1	.03	2	.03	8	.21	.04	.06	2	3
SK-69	20	158	621	5270	6.5	3	7	581	2.48	4	5	ND	2	21	85	2	2	22	.94	.043	2	2	.42	19	.01	6	.77	.01	.15	4	36
STD C/AU-R	19	59	40	132	7.2	71	28	1050	4.32	38	18	8	40	51	19	18	20	58	.52	.087	38	60	.90	182	.08	35	1.80	.06	.14	13	510

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-01	21	778	15219	15806	30.8	2	13	1553	4.67	20	5	ND	2	4	184	2	18	56	.21	.061	2	1	1.11	11	.01	2	1.90	.02	.13	1	9
SK-02	34	1252	16291	48142	53.2	8	36	969	4.56	38	5	ND	7	10	729	7	2	11	.57	.028	3	1	.23	27	.01	10	.67	.02	.22	1	2405
SK-03	32	3524	3754	52463	44.0	4	32	1838	6.43	16	5	ND	3	24	671	2	2	69	.94	.092	3	2	1.34	26	.01	3	2.53	.01	.19	1	18
SK-04	36	4856	24058	48332	238.9	3	25	524	3.78	21	5	9	1	1	627	30	20	26	.07	.037	2	1	.40	15	.01	2	.91	.01	.12	1	15500
SK-05	5	192	1832	1130	14.3	2	8	1035	5.47	20	5	ND	1	3	7	2	5	75	.19	.110	3	1	1.09	33	.01	2	2.15	.01	.23	1	42
SK-06	41	388	733	1212	76.6	2	2	55	2.15	8	5	ND	1	1	15	2	13	4	.01	.005	2	1	.02	4	.01	2	.13	.01	.03	1	880
SK-07	4	281	3276	1591	11.0	4	4	362	2.04	8	5	ND	1	1	19	2	7	17	.06	.028	2	1	.32	11	.01	2	.70	.01	.10	1	1380
SK-08	5	271	992	434	45.0	2	3	210	1.62	11	5	15	1	1	4	2	12	12	.01	.009	2	2	.17	3	.01	2	.36	.01	.03	1	8850
SK-09	17	240	1282	1071	15.9	1	2	90	1.39	7	5	ND	14	1	14	2	5	4	.02	.013	3	1	.13	27	.01	3	.44	.01	.21	1	1500
SK-10	18	573	20892	14161	55.7	16	61	75	16.72	14	5	ND	3	1	209	9	2	4	.01	.007	2	1	.02	4	.01	2	.01	.01	.05	1	330
SK-11	28	516	9958	1669	70.7	3	5	469	3.59	16	5	ND	1	1	21	10	10	26	.03	.021	2	1	.40	7	.01	22	.80	.01	.05	1	164
SK-12	42	4661	24974	55768	113.7	3	13	94	2.04	11	5	ND	1	1	880	36	2	3	.01	.002	2	1	.02	2	.01	2	.07	.01	.01	1	1650
SK-13	3	80	4897	69	24.4	5	2	83	1.18	4	5	ND	1	1	1	4	14	4	.01	.006	2	1	.04	2	.01	2	.11	.01	.01	1	350
SK-14	6	414	18321	2858	96.9	2	6	240	2.67	22	5	3	1	1	41	21	19	15	.01	.008	2	2	.19	5	.01	2	.40	.01	.03	1	6320
SK-15	48	7798	23896	84062	322.2	3	39	274	3.05	24	5	ND	1	1	1040	37	5	8	.02	.016	2	1	.08	8	.01	2	.29	.01	.07	1	1320
SK-16	4	134	3362	504	11.8	3	10	1749	7.77	16	5	ND	2	5	3	2	2	110	.25	.126	3	1	1.83	38	.03	3	3.30	.01	.22	1	720
SK-17	4	354	2891	688	71.7	6	5	400	3.23	12	5	ND	1	1	7	2	11	21	.06	.034	2	2	.34	12	.01	2	.77	.01	.11	1	1990
SK-18	129	25	383	164	7.7	4	1	122	1.16	4	5	7	1	1	1	4	5	8	.01	.008	2	1	.08	6	.01	2	.23	.01	.07	1	1050
SK-19	10	420	25699	1863	83.3	3	2	58	2.79	7	5	ND	1	1	27	14	19	5	.01	.008	2	2	.02	7	.01	2	.17	.01	.05	1	74
SK-20	10	115	214	33	.6	10	11	159	3.79	6	5	ND	2	43	1	2	7	70	1.10	.086	5	17	.26	23	.18	7	1.39	.18	.07	4	1
SK-21	3	38	668	50	1.4	8	3	187	2.04	5	5	ND	2	17	1	4	6	56	.18	.030	2	5	.25	216	.08	2	.66	.04	.32	1	2
SK-22	2	64	110	34	.4	200	19	175	2.09	12	5	ND	1	154	1	2	2	37	2.28	.121	3	327	1.34	9	.07	4	2.61	.14	.05	1	7
SK-23	9	20	265	166	1.1	6	3	304	1.88	6	5	ND	1	9	1	2	5	24	.27	.024	2	4	.41	18	.02	6	.93	.03	.10	1	1
SK-23A	2	31	15	69	.1	9	9	792	4.04	14	5	ND	3	11	1	2	2	98	.30	.081	7	26	1.56	113	.30	2	1.88	.07	1.41	1	2
SK-24	2	40	29	93	.2	16	7	723	4.12	12	5	ND	3	108	1	2	2	91	1.78	.079	3	36	1.44	37	.17	6	4.20	.30	.39	4	1
SK-25	3	68	9	69	.3	11	9	505	3.51	14	5	ND	3	75	1	2	3	54	2.22	.103	4	14	.87	23	.15	2	3.64	.18	.15	1	1
SK-26	3	85	102	956	1.0	4	7	535	1.92	12	5	ND	1	91	11	2	7	42	6.39	.098	2	1	.51	32	.10	2	1.34	.03	.05	1	1
SK-27	14	34	221	604	1.2	2	4	141	.76	5	5	ND	1	1	2	2	3	4	.01	.004	2	2	.07	8	.01	2	.18	.01	.04	2	1
SK-28	1	61	14	71	.4	3	10	638	3.64	13	5	ND	2	97	1	2	6	85	2.84	.101	3	1	1.29	136	.10	4	2.19	.09	.53	1	5
SK-29	4	10	27	683	.7	5	3	314	.99	4	5	ND	1	1	5	2	6	6	.18	.004	2	1	.15	5	.01	2	.25	.01	.03	1	1
SK-30	13	169	291	3981	5.4	3	4	136	.82	4	5	ND	1	1	48	2	3	6	.01	.004	2	2	.09	3	.01	10	.17	.01	.01	1	11
SK-31	54	4171	5681	95264	50.3	7	48	601	3.54	17	5	ND	1	37	1172	2	2	58	.53	.023	2	5	.29	13	.01	2	1.55	.01	.10	1	250
SK-32	6	34	99	473	.1	12	8	548	2.40	22	5	ND	1	1	1	2	3	30	.08	.034	2	12	.43	21	.01	2	1.01	.01	.16	1	1
SK-33	49	232	690	4488	2.1	7	12	856	3.27	22	6	ND	2	25	8	2	2	124	.34	.060	4	14	.81	21	.01	2	1.94	.01	.21	1	8
SK-34	39	126	741	3969	1.0	8	9	868	3.11	27	5	ND	1	24	7	2	6	70	.30	.049	4	6	.70	16	.01	8	1.58	.01	.18	1	3
SK-35	1889	247	25198	8609	327.4	6	10	352	1.88	49	9	ND	1	10	12	8	419	33	.16	.013	2	4	.37	11	.01	2	.83	.01	.08	17	620
STD C/AU-R	19	60	38	132	7.0	67	27	1034	3.72	41	19	7	37	49	18	18	22	56	.48	.087	36	59	.88	173	.08	37	1.85	.06	.14	12	490

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-36	183	654	1558	41211	9.8	13	25	516	3.58	30	5	ND	2	24	518	2	3	23	.45	.052	2	6	.69	18	.01	3	1.32	.01	.18	1	35
SK-37	80	59	6691	630	3.4	4	3	99	.54	5	5	ND	1	2	4	2	5	2	.01	.001	2	2	.03	2	.01	2	.07	.01	.02	1	6
SK-38	58	20	846	622	1.0	4	4	139	.75	2	8	ND	1	1	2	5	3	8	.04	.009	2	1	.09	6	.01	2	.18	.01	.06	1	1
SK-39	2	44	48	119	.6	15	8	328	2.21	10	5	ND	3	136	1	2	6	45	2.94	.077	4	13	.54	22	.12	10	3.12	.10	.16	1	1
SK-40	3	71	405	814	.5	12	6	920	2.70	5	5	ND	3	63	12	2	2	55	2.54	.056	6	9	.63	16	.01	2	1.68	.01	.22	1	1
SK-41	10	30	18	144	.2	13	4	457	3.63	4	5	ND	3	64	2	5	6	54	1.16	.038	5	13	.93	48	.16	3	2.22	.09	.44	1	1
SK-42	2	49	31	97	.1	131	24	663	5.07	12	5	ND	3	188	1	2	4	82	2.96	.174	26	35	3.61	331	.55	2	3.23	.32	.15	1	1
SK-44	1	51	28	72	.2	1	12	808	4.51	2	5	ND	3	67	1	2	5	85	2.97	.123	4	3	1.12	206	.18	8	2.57	.13	.63	1	1
SK-45	3	8	18	336	.1	8	3	622	1.33	4	5	ND	1	18	11	2	2	12	1.10	.012	2	2	.28	14	.02	2	.43	.01	.04	1	1
SK-46	57	66	1335	507	2.1	2	4	303	1.98	6	5	ND	1	1	1	2	3	15	.04	.013	2	5	.26	11	.01	6	.52	.01	.11	1	1
SK-47	5	31	9	146	.2	21	6	278	2.70	4	5	ND	2	82	2	2	3	76	1.71	.061	2	23	.52	30	.12	2	2.06	.10	.26	1	1
SK-48	1	21	302	235	.3	4	4	487	2.23	2	5	ND	11	15	1	3	3	20	.20	.046	15	3	.44	98	.08	2	.79	.04	.15	1	3
SK-49	1	16	17	65	.1	2	6	640	2.13	4	6	ND	2	130	1	2	2	37	2.13	.128	4	1	.31	20	.12	2	1.30	.01	.02	1	2
SK-50	1	53	30	122	.5	3	15	1068	5.93	5	5	ND	3	16	1	2	4	127	.68	.181	5	3	1.71	132	.24	13	2.30	.05	.83	1	1
SK-51	5	360	1362	1956	5.6	6	9	412	2.60	5	5	ND	2	9	18	2	4	29	.16	.018	2	2	.52	10	.01	2	.91	.01	.08	3	57
SK-52	2	68	27	81	.4	18	10	183	2.09	10	5	ND	3	56	1	3	2	48	2.29	.095	4	24	.30	25	.12	5	2.73	.19	.12	1	2
SK-53	3	36	30	112	.1	79	24	936	6.21	2	5	ND	1	108	1	2	4	89	3.38	.160	19	97	3.53	159	.28	6	2.67	.14	.22	1	2
SK-54	4	94	20	54	.5	17	14	362	6.13	2	5	ND	3	125	1	2	5	91	1.51	.194	4	27	1.34	79	.19	2	3.08	.24	.42	2	3
SK-55	1	44	32	22	.3	3	4	289	1.99	4	5	ND	2	232	1	2	2	48	2.34	.117	4	3	.19	6	.12	2	1.76	.09	.05	1	1
SK-56	1	7	5	7	.1	1	1	72	.53	2	5	ND	17	1	1	3	2	2	.01	.002	3	1	.03	4	.01	2	.15	.04	.06	1	1
SK-57	1	5	23	70	.1	7	7	276	2.10	2	5	ND	11	25	1	2	5	19	.34	.058	14	6	.56	30	.09	2	.93	.04	.10	1	2
SK-58	1	54	11	65	.3	7	11	657	4.09	4	5	ND	3	26	1	2	2	79	.90	.115	4	10	1.13	64	.21	2	1.54	.08	.48	1	1
SK-59	5	87	18	96	.5	17	14	910	5.83	9	5	ND	5	20	1	2	2	140	.91	.146	4	44	1.84	50	.24	2	2.92	.04	.82	1	1
SK-60	10	57	7	71	.3	6	9	655	4.64	2	5	ND	4	60	1	2	2	103	2.42	.097	4	14	1.36	79	.24	3	4.14	.20	.75	1	1
SK-61	1	55	9	80	.5	12	12	983	5.15	7	5	ND	3	65	1	2	5	123	1.18	.105	4	25	1.85	202	.25	11	3.54	.26	1.13	1	3
SK-62	2	80	9	42	.7	9	10	403	4.53	20	5	ND	4	96	1	2	2	101	1.42	.105	5	36	.95	26	.15	4	2.52	.19	.18	1	1
SK-63	1	3	2	11	.1	2	1	261	.43	2	5	ND	15	2	1	2	2	2	.01	.001	6	1	.02	2	.01	2	.14	.05	.05	1	2
SK-64	9	49	10	83	.5	17	9	678	5.25	13	5	ND	4	19	1	2	2	169	.69	.087	3	32	1.79	40	.27	12	2.71	.10	.96	1	1
SK-65	7	80	20	96	.6	29	14	352	4.93	6	5	ND	3	87	1	2	4	119	2.96	.090	4	35	1.23	24	.18	2	4.39	.13	.42	2	2
SK-66	10	7921	17163	10579	101.7	4	47	103	4.31	78	5	ND	1	1	127	2	2	3	.01	.004	2	1	.05	7	.01	7	.12	.01	.04	9	220
SK-67	13	28	15	7	.2	4	5	42	1.11	2	5	ND	1	2	1	4	2	4	.01	.001	2	2	.04	3	.01	8	.08	.01	.01	35	1
SK-68	1	7	4	37	.1	3	1	166	.63	2	5	ND	18	2	1	2	2	3	.02	.001	11	1	.03	2	.03	8	.21	.04	.06	2	3
SK-69	20	158	621	5270	6.5	3	7	581	2.48	4	5	ND	2	21	85	2	2	22	.94	.043	2	2	.42	19	.01	6	.77	.01	.15	4	36
STD C/AU-R	19	59	40	132	7.2	71	28	1050	4.32	38	18	8	40	51	19	18	20	58	.52	.087	38	60	.90	182	.08	35	1.80	.06	.14	13	510

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SP PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-36	183	654	1558	41211	9.8	13	25	516	3.58	30	5	ND	2	24	518	2	3	23	.45	.052	2	6	.69	18	.01	3	1.32	.01	.18	1	35
SK-37	80	59	6691	630	3.4	4	3	99	.54	5	5	ND	1	2	4	2	5	2	.01	.001	2	2	.03	2	.01	2	.07	.01	.02	1	6
SK-38	58	20	846	622	1.0	4	4	139	.75	2	8	ND	1	1	2	5	3	8	.04	.009	2	1	.09	6	.01	2	.18	.01	.06	1	1
SK-39	2	44	48	113	.6	15	8	328	2.21	10	5	ND	3	136	1	2	6	45	2.94	.077	4	13	.54	22	.12	10	3.12	.10	.16	1	1
SK-40	3	71	405	814	.5	12	6	920	2.70	5	5	ND	3	63	12	2	2	55	2.54	.056	6	9	.63	16	.01	2	1.68	.01	.22	1	1
SK-41	10	30	18	144	.2	13	4	457	3.63	4	5	ND	3	64	2	5	6	54	1.16	.039	5	13	.93	48	.16	3	2.22	.09	.44	1	1
SK-42	2	45	31	97	.1	131	24	663	5.07	12	5	ND	3	188	1	2	4	82	2.96	.174	26	35	3.61	331	.55	2	3.23	.32	.15	1	1
SK-44	1	51	28	72	.2	1	12	808	4.51	2	5	ND	3	67	1	2	5	85	2.97	.123	4	3	1.12	206	.18	8	2.57	.13	.63	1	1
SK-45	3	8	18	336	.1	8	3	622	1.33	4	5	ND	1	18	11	2	2	12	1.10	.012	2	2	.28	14	.02	2	.43	.01	.04	1	1
SK-46	57	66	1335	507	2.1	2	4	303	1.98	6	5	ND	1	1	1	2	3	15	.04	.019	2	5	.26	11	.01	6	.52	.01	.11	1	1
SK-47	5	31	9	146	.2	21	6	278	2.70	4	5	ND	2	82	2	2	3	76	1.71	.061	2	23	.52	30	.12	2	2.06	.10	.26	1	1
SK-48	1	21	302	235	.3	4	4	487	2.23	2	5	ND	11	15	1	3	3	20	.20	.046	15	3	.44	98	.08	2	.79	.04	.15	1	3
SK-49	1	16	17	65	.1	2	6	640	2.13	4	6	ND	2	130	1	2	2	37	2.13	.128	4	1	.31	20	.12	2	1.30	.01	.02	1	2
SK-50	1	53	30	122	.5	3	15	1068	5.93	5	5	ND	3	16	1	2	4	127	.68	.181	5	3	1.71	132	.24	13	2.20	.05	.83	1	1
SK-51	5	360	1362	1956	5.6	6	9	412	2.60	5	5	ND	2	9	18	2	4	29	.16	.018	2	2	.52	10	.01	2	.91	.01	.08	3	57
SK-52	2	68	27	81	.4	18	10	183	2.09	10	5	ND	3	56	1	2	2	48	2.29	.095	4	24	.30	25	.12	5	2.73	.19	.12	1	2
SK-53	3	36	30	112	.1	79	24	936	6.21	2	5	ND	1	108	1	2	4	89	3.38	.160	19	97	3.53	159	.28	6	2.67	.14	.22	1	2
SK-54	4	94	20	54	.5	17	14	362	6.13	2	5	ND	3	125	1	2	5	91	1.51	.194	4	27	1.34	79	.19	2	3.08	.24	.42	2	9
SK-55	1	44	32	22	.3	3	4	289	1.99	4	5	ND	2	232	1	2	2	48	2.34	.117	4	3	.19	6	.12	2	1.76	.09	.05	1	1
SK-56	1	7	5	7	.1	1	1	72	.53	2	5	ND	17	1	1	3	2	2	.01	.002	3	1	.03	4	.01	2	.15	.04	.06	1	1
SK-57	1	5	23	70	.1	7	7	276	2.10	2	5	ND	11	25	1	2	5	19	.34	.058	14	6	.56	30	.09	2	.93	.04	.10	1	2
SK-58	1	54	11	65	.3	7	11	657	4.09	4	5	ND	3	26	1	2	2	79	.90	.115	4	10	1.13	64	.21	2	1.54	.08	.48	1	1
SK-59	5	87	18	96	.5	17	14	910	5.83	9	5	ND	5	20	1	2	2	140	.91	.146	4	44	1.84	50	.24	2	2.92	.04	.82	1	1
SK-60	10	57	7	71	.3	6	9	655	4.64	2	5	ND	4	60	1	2	2	103	2.42	.097	4	14	1.36	79	.24	3	4.14	.20	.75	1	1
SK-61	1	55	9	80	.5	12	12	983	5.15	7	5	ND	3	65	1	2	5	123	1.18	.105	4	25	1.85	202	.25	11	3.54	.26	1.13	1	3
SK-62	2	80	9	42	.7	9	10	403	4.53	20	5	ND	4	96	1	2	2	101	1.42	.105	5	36	.95	26	.15	4	2.52	.19	.18	1	1
SK-63	1	3	2	11	.1	2	1	261	.43	2	5	ND	15	2	1	2	2	2	.01	.001	6	1	.02	2	.01	2	.14	.05	.05	1	2
SK-64	9	49	10	83	.5	17	9	678	5.25	13	5	ND	4	19	1	2	2	169	.69	.087	3	32	1.79	40	.27	12	2.71	.10	.96	1	1
SK-65	7	80	20	96	.6	29	14	352	4.93	6	5	ND	3	87	1	2	4	119	2.96	.090	4	35	1.23	24	.18	2	4.39	.13	.42	2	2
SK-66	10	7921	17163	10579	101.7	4	47	103	4.31	78	5	ND	1	1	127	2	2	3	.01	.004	2	1	.05	7	.01	7	.12	.01	.04	9	220
SK-67	13	28	15	7	.2	4	5	42	1.11	2	5	ND	1	2	1	4	2	4	.01	.001	2	2	.04	3	.01	8	.08	.01	.01	35	1
SK-68	1	7	4	37	.1	3	1	166	.63	2	5	ND	18	2	1	2	2	3	.02	.001	11	1	.03	2	.03	8	.21	.04	.06	2	3
SK-69	20	158	621	5270	6.5	3	7	581	2.48	4	5	ND	2	21	85	2	2	22	.94	.043	2	2	.42	19	.01	6	.77	.01	.15	4	36
STD C/AU-R	19	59	40	132	7.2	71	28	1050	4.32	38	18	8	40	51	19	18	20	58	.52	.087	38	60	.90	182	.08	35	1.80	.06	.14	13	510

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-01	21	778	15219	15806	30.8	2	13	1553	4.67	20	5	ND	2	4	184	2	18	56	.21	.061	2	1	1.11	11	.01	2	1.90	.02	.13	1	9
SK-02	34	1252	16291	48142	53.2	8	36	969	4.56	38	5	ND	7	10	729	7	2	11	.57	.028	3	1	.23	27	.01	10	.67	.02	.22	1	2405
SK-03	32	3524	3754	52463	44.0	4	32	1838	6.43	16	5	ND	3	24	671	2	2	69	.94	.092	3	2	1.34	26	.01	3	2.53	.01	.19	1	18
SK-04	36	4856	24058	48332	238.9	3	25	524	3.78	21	5	9	1	1	627	30	20	26	.07	.037	2	1	.40	15	.01	2	.91	.01	.12	1	15500
SK-05	5	192	1832	1130	14.3	2	8	1035	5.47	20	5	ND	1	3	7	2	5	75	.19	.110	3	1	1.09	33	.01	2	2.15	.01	.23	1	42
SK-06	41	388	733	1212	76.6	2	2	55	2.15	8	5	ND	1	1	15	2	13	4	.01	.005	2	1	.02	4	.01	2	.13	.01	.03	1	880
SK-07	4	281	3276	1591	11.0	4	4	362	2.04	8	5	ND	1	1	19	2	7	17	.06	.028	2	1	.32	11	.01	2	.70	.01	.10	1	1380
SK-08	5	271	992	434	45.0	2	3	210	1.62	11	5	15	1	1	4	2	12	12	.01	.009	2	2	.17	3	.01	2	.36	.01	.03	1	8850
SK-09	17	240	1282	1071	15.9	1	2	90	1.39	7	5	ND	14	1	14	2	5	4	.02	.013	3	1	.13	27	.01	3	.44	.01	.21	1	1500
SK-10	18	573	20892	14161	55.7	16	61	75	16.72	14	5	ND	3	1	209	9	2	4	.01	.007	2	1	.02	4	.01	2	.01	.01	.05	1	330
SK-11	28	516	9958	1669	70.7	3	5	469	3.59	16	5	ND	1	1	21	10	10	26	.03	.021	2	1	.40	7	.01	22	.80	.01	.05	1	164
SK-12	42	4661	24974	55768	113.7	3	13	94	2.04	11	5	ND	1	1	880	36	2	3	.01	.002	2	1	.02	2	.01	2	.07	.01	.01	1	1650
SK-13	3	80	4897	69	24.4	5	2	83	1.18	4	5	ND	1	1	1	4	14	4	.01	.006	2	1	.04	2	.01	2	.11	.01	.01	1	350
SK-14	6	414	18321	2858	96.9	2	6	240	2.67	22	5	3	1	1	41	21	19	15	.01	.008	2	2	.19	5	.01	2	.40	.01	.03	1	6320
SK-15	48	7798	23896	84062	322.2	3	39	274	3.05	24	5	ND	1	1	1040	37	5	8	.02	.016	2	1	.08	8	.01	2	.29	.01	.07	1	1320
SK-16	4	134	3362	504	11.8	3	10	1749	7.77	16	5	ND	2	5	3	2	2	110	.25	.126	3	1	1.83	38	.03	3	3.30	.01	.22	1	720
SK-17	4	354	2891	688	71.7	6	5	400	3.23	12	5	ND	1	1	7	2	11	21	.06	.034	2	2	.34	12	.01	2	.77	.01	.11	1	1990
SK-18	129	25	383	164	7.7	4	1	122	1.16	4	5	7	1	1	1	4	5	8	.01	.008	2	1	.08	6	.01	2	.23	.01	.07	1	1050
SK-19	10	420	25699	1863	83.3	3	2	58	2.79	7	5	ND	1	1	27	14	19	5	.01	.008	2	2	.02	7	.01	2	.17	.01	.05	1	74
SK-20	10	115	214	33	.6	10	11	159	3.79	6	5	ND	2	43	1	2	7	70	1.10	.086	5	17	.26	23	.18	7	1.39	.18	.07	4	1
SK-21	3	38	668	50	1.4	8	3	187	2.04	5	5	ND	2	17	1	4	6	56	.18	.030	2	5	.25	216	.08	2	.66	.04	.32	1	2
SK-22	2	64	110	34	.4	200	19	175	2.09	12	5	ND	1	154	1	2	2	37	2.28	.121	3	327	1.34	9	.07	4	2.61	.14	.05	1	7
SK-23	9	20	265	166	1.1	6	3	304	1.88	6	5	ND	1	9	1	2	5	24	.27	.024	2	4	.41	18	.02	6	.93	.03	.10	1	1
SK-23A	2	31	15	69	.1	9	9	792	4.04	14	5	ND	3	11	1	2	2	98	.30	.081	7	26	1.56	113	.30	2	1.88	.07	1.41	1	2
SK-24	2	40	29	93	.2	16	7	723	4.12	12	5	ND	3	108	1	2	2	91	1.78	.079	3	36	1.44	37	.17	6	4.20	.30	.39	4	1
SK-25	3	68	9	69	.3	11	9	505	3.51	14	5	ND	3	75	1	2	3	54	2.22	.103	4	14	.87	23	.15	2	3.64	.18	.15	1	1
SK-26	3	85	102	956	1.0	4	7	535	1.92	12	5	ND	1	91	11	2	7	42	6.39	.098	2	1	.51	32	.10	2	1.34	.03	.05	1	1
SK-27	14	34	221	604	1.2	2	4	141	.76	5	5	ND	1	1	2	2	3	4	.01	.004	2	2	.07	8	.01	2	.18	.01	.04	2	1
SK-28	1	61	14	71	.4	3	10	638	3.64	13	5	ND	2	97	1	2	6	85	2.84	.101	3	1	1.29	136	.10	4	2.19	.09	.53	1	5
SK-29	4	10	27	683	.7	5	3	314	.99	4	5	ND	1	1	5	2	6	6	.18	.004	2	1	.15	5	.01	2	.25	.01	.03	1	1
SK-30	13	169	291	3981	5.4	3	4	136	.82	4	5	ND	1	1	48	2	3	6	.01	.004	2	2	.09	3	.01	10	.17	.01	.01	1	11
SK-31	54	4171	5681	95264	50.3	7	48	601	3.54	17	5	ND	1	37	1172	2	2	58	.53	.023	2	5	.29	13	.01	2	1.55	.01	.10	1	250
SK-32	6	34	99	473	.1	12	8	548	2.40	22	5	ND	1	1	1	2	3	30	.08	.034	2	12	.43	21	.01	2	1.01	.01	.16	1	1
SK-33	49	232	690	4488	2.1	7	12	856	3.27	22	6	ND	2	25	8	2	2	124	.34	.060	4	14	.81	21	.01	2	1.94	.01	.21	1	8
SK-34	39	126	741	3969	1.0	8	9	868	3.11	27	5	ND	1	24	7	2	6	70	.30	.049	4	6	.70	16	.01	8	1.58	.01	.18	1	3
SK-35	1889	247	25198	8609	327.4	6	10	352	1.88	49	9	ND	1	10	12	8	419	33	.16	.013	2	4	.37	11	.01	2	.83	.01	.08	17	620
STD C/AU-R	19	60	38	132	7.0	67	27	1034	3.72	41	19	7	37	49	18	18	22	56	.48	.087	36	59	.88	173	.08	37	1.85	.06	.14	12	490

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-36	183	654	1558	41211	9.8	13	25	516	3.58	30	5	ND	2	24	518	2	3	23	.45	.052	2	6	.69	18	.01	3	1.32	.01	.18	1	35
SK-37	80	59	6691	630	3.4	4	3	99	.54	5	5	ND	1	2	4	2	5	2	.01	.001	2	2	.03	2	.01	2	.07	.01	.02	1	6
SK-38	58	20	846	622	1.0	4	4	139	.75	2	8	ND	1	1	2	5	3	8	.04	.009	2	1	.09	6	.01	2	.18	.01	.06	1	1
SK-39	2	44	48	119	.6	15	8	328	2.21	10	5	ND	3	136	1	2	6	45	2.94	.077	4	13	.54	22	.12	10	3.12	.10	.16	1	1
SK-40	3	71	405	814	.5	12	6	920	2.70	5	5	ND	3	63	12	2	2	55	2.54	.056	6	9	.63	16	.01	2	1.68	.01	.22	1	1
SK-41	10	30	18	144	.2	13	4	457	3.63	4	5	ND	3	64	2	5	6	54	1.16	.038	5	13	.93	48	.16	3	2.22	.09	.44	1	1
SK-42	2	49	31	97	.1	131	24	663	5.07	12	5	ND	3	188	1	2	4	82	2.96	.174	26	35	3.61	331	.55	2	3.23	.32	.15	1	1
SK-44	1	51	28	72	.2	1	12	808	4.51	2	5	ND	3	67	1	2	5	85	2.97	.123	4	3	1.12	206	.18	8	2.57	.13	.63	1	1
SK-45	3	8	18	336	.1	8	3	622	1.33	4	5	ND	1	18	11	2	7	12	1.10	.012	2	2	.28	14	.02	2	.43	.01	.04	1	1
SK-46	57	66	1335	507	2.1	2	4	303	1.98	6	5	ND	1	1	1	2	3	15	.04	.013	2	5	.26	11	.01	6	.52	.01	.11	1	1
SK-47	5	31	9	146	.2	21	6	278	2.70	4	5	ND	2	82	2	2	3	76	1.71	.061	2	23	.52	30	.12	2	2.06	.10	.26	1	1
SK-48	1	21	302	235	.3	4	4	487	2.23	2	5	ND	11	15	1	3	3	20	.20	.046	15	3	.44	98	.08	2	.79	.04	.15	1	3
SK-49	1	16	17	65	.1	2	6	640	2.13	4	6	ND	2	130	1	2	2	37	2.13	.128	4	1	.31	20	.12	2	1.30	.01	.02	1	2
SK-50	1	53	30	122	.5	3	15	1068	5.93	5	5	ND	3	16	1	2	4	127	.68	.181	5	3	1.71	132	.24	13	2.20	.05	.83	1	1
SK-51	5	360	1362	1956	5.6	6	9	412	2.60	5	5	ND	2	9	18	2	4	29	.16	.018	2	2	.52	10	.01	2	.91	.01	.08	3	57
SK-52	2	68	27	81	.4	18	10	183	2.09	10	5	ND	3	56	1	2	2	48	2.29	.095	4	24	.30	25	.12	5	2.73	.19	.12	1	2
SK-53	3	36	30	112	.1	79	24	936	6.21	2	5	ND	1	108	1	2	4	89	3.38	.160	19	97	3.53	159	.28	6	2.67	.14	.22	1	2
SK-54	4	94	20	54	.5	17	14	362	6.13	2	5	ND	3	125	1	2	5	91	1.51	.194	4	27	1.34	79	.19	2	3.08	.24	.42	2	9
SK-55	1	44	32	22	.3	3	4	289	1.99	4	5	ND	2	232	1	2	2	48	2.34	.117	4	3	.19	6	.12	2	1.76	.09	.05	1	1
SK-56	1	7	5	7	.1	1	1	72	.53	2	5	ND	17	1	1	3	2	2	.01	.002	3	1	.03	4	.01	2	.15	.04	.06	1	1
SK-57	1	5	23	70	.1	7	7	276	2.10	2	5	ND	11	25	1	2	5	19	.34	.058	14	6	.56	30	.09	2	.93	.04	.10	1	2
SK-58	1	54	11	65	.3	7	11	657	4.09	4	5	ND	3	26	1	2	2	79	.90	.115	4	10	1.13	64	.21	2	1.54	.08	.48	1	1
SK-59	5	87	18	96	.5	17	14	910	5.83	9	5	ND	5	20	1	2	2	140	.91	.146	4	44	1.84	50	.24	2	2.92	.04	.87	1	1
SK-60	10	57	7	71	.3	6	9	655	4.64	2	5	ND	4	60	1	2	2	103	2.42	.097	4	14	1.36	79	.24	3	4.14	.20	.75	1	1
SK-61	1	55	9	80	.5	12	12	983	5.15	7	5	ND	3	65	1	2	5	123	1.18	.105	4	25	1.85	202	.25	11	3.54	.26	1.13	1	3
SK-62	2	80	9	42	.7	9	10	403	4.53	20	5	ND	4	96	1	2	2	101	1.42	.105	5	36	.95	26	.15	4	2.52	.19	.18	1	1
SK-63	1	3	2	11	.1	2	1	261	.43	2	5	ND	15	2	1	2	2	2	.01	.001	6	1	.02	2	.01	2	.14	.05	.05	1	2
SK-64	9	49	10	83	.5	17	9	678	5.25	13	5	ND	4	19	1	2	2	169	.69	.087	3	32	1.79	40	.27	12	2.71	.10	.96	1	1
SK-65	7	80	20	96	.6	29	14	352	4.93	6	5	ND	3	87	1	2	4	119	2.96	.090	4	35	1.23	24	.18	2	4.39	.13	.42	2	2
SK-66	10	7921	17163	10579	101.7	4	47	103	4.31	78	5	ND	1	1	127	2	2	3	.01	.004	2	1	.05	7	.01	7	.12	.01	.04	9	220
SK-67	13	28	15	7	.2	4	5	42	1.11	2	5	ND	1	2	1	4	2	4	.01	.001	2	2	.04	3	.01	8	.08	.01	.01	35	1
SK-68	1	7	4	37	.1	3	1	166	.63	2	5	ND	18	2	1	2	2	3	.02	.001	11	1	.03	2	.03	8	.21	.04	.06	2	3
SK-69	20	158	621	5270	6.5	3	7	581	2.48	4	5	ND	2	21	85	2	2	22	.94	.043	2	2	.42	19	.01	6	.77	.01	.15	4	36
STD C/AU-R	19	59	40	132	7.2	71	28	1050	4.32	38	18	8	40	51	19	18	20	58	.52	.087	38	60	.90	182	.08	35	1.80	.06	.14	13	510

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-8 SOIL P9-10 ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 27 1987 DATE REPORT MAILED: ASSAYER............DEAN TOYE, CERTIFIED B.C. ASSAYER

SHANGRI-LA File # 87-3689 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 00E+25N	1	64	22	111	.3	7	11	529	5.00	13	5	ND	3	148	1	2	2	113	1.03	.104	6	22	1.52	75	.28	2	4.75	.03	.24	1	2
SA 00E+00	15	14	21	95	.4	11	5	5125	2.89	87	5	ND	1	667	1	2	7	75	6.09	.047	6	21	.95	34	.04	2	10.58	.01	.22	2	1
SA 00E+25S	1	81	18	133	.4	17	19	1133	7.99	4	5	ND	1	24	1	2	2	172	.40	.097	6	27	2.66	127	.34	2	4.84	.01	.80	3	3
SA 00E+50S	3	62	16	114	.1	30	17	861	6.95	15	5	ND	2	20	1	2	2	166	.20	.069	8	57	1.89	52	.32	2	3.66	.02	.27	1	76
SA 00E+75S	4	54	26	94	.3	18	12	548	6.11	13	5	ND	2	17	1	2	2	121	.19	.060	8	33	1.31	42	.30	11	3.32	.02	.21	2	3
SA 00E+110S	3	86	21	133	.3	32	18	1528	5.85	8	5	ND	1	123	1	2	2	150	1.13	.106	5	48	2.23	161	.28	2	5.12	.05	.43	4	3
SA 00E+125S	7	105	25	183	.5	11	18	1685	7.90	36	5	ND	1	149	1	2	4	177	.77	.131	5	20	2.20	164	.27	2	6.66	.04	.59	4	2
SA 00E+150S	9	71	20	181	.3	40	26	1774	8.05	41	5	ND	1	20	1	2	2	216	.38	.060	6	87	3.13	80	.38	3	7.26	.04	.22	4	2
SA 00E+175S	3	74	23	138	.4	17	22	1369	7.68	17	5	ND	3	17	1	2	2	200	.55	.095	5	39	2.56	244	.39	10	4.69	.06	.89	6	1
SA 00E+200S	4	30	58	57	.6	8	4	243	2.51	17	14	ND	8	10	1	2	4	38	.14	.054	10	13	.47	29	.12	2	1.37	.03	.11	1	1
SA 00E+250S	5	29	51	71	.1	12	5	301	4.87	16	5	ND	4	9	1	2	2	76	.09	.063	16	24	.71	27	.21	2	2.34	.02	.11	1	2
SA 00E+275S	8	57	25	72	.1	16	9	314	5.37	13	5	ND	3	10	1	2	2	82	.22	.044	13	21	.94	52	.29	2	3.38	.06	.17	3	1
SA 00E+300S	4	149	18	103	.3	26	19	608	6.46	8	5	ND	1	11	1	2	2	182	.29	.080	6	42	2.52	182	.35	4	3.86	.06	.65	1	2
SA 00E+325S	2	92	12	98	.3	35	20	708	5.71	13	5	ND	2	24	1	2	2	158	.88	.123	4	85	2.06	250	.42	6	2.63	.02	.73	1	1
SA 00E+360S	2	70	22	99	.5	14	20	810	6.42	15	5	ND	1	13	1	2	2	187	.32	.081	5	25	2.18	159	.40	2	3.58	.02	.98	2	1
SA 00E+375S	3	169	15	144	.4	29	26	990	7.70	6	5	ND	1	12	1	2	2	238	.33	.076	3	55	2.96	124	.36	2	4.92	.05	.81	3	1
SA 00E+400S	3	77	20	103	.4	23	19	688	6.19	10	5	ND	1	25	1	2	2	185	.28	.064	5	35	2.40	89	.35	2	4.14	.06	.90	3	2
SA 00E+425S	3	56	23	106	.1	11	12	586	4.85	10	5	ND	2	35	1	3	2	116	.27	.079	9	25	1.64	71	.25	8	2.75	.03	.49	1	1
SA 00E+450S	3	57	22	70	.1	15	8	393	3.85	18	5	ND	4	12	1	2	5	75	.21	.065	10	24	.94	27	.17	2	2.01	.01	.12	1	1
SA 00E+470S	2	36	23	64	.2	7	7	358	3.75	14	5	ND	4	12	1	2	2	72	.25	.077	11	22	.84	29	.14	2	2.11	.01	.11	4	5
SA 00E+500S	2	57	23	85	.1	21	19	696	5.87	5	5	ND	5	19	1	2	2	156	.27	.081	6	40	2.85	112	.33	5	3.49	.03	1.16	1	1
SA 00E+525S	1	233	18	113	.1	19	24	900	7.07	8	5	ND	1	12	1	2	2	175	.31	.090	3	19	2.75	180	.36	41	3.93	.03	1.06	2	1
SA 200E+75N	2	81	22	126	.4	17	16	774	5.76	7	5	ND	1	20	1	3	2	165	.40	.108	4	39	1.97	145	.29	2	4.27	.05	.50	1	1
SA 200E+50N	2	74	25	131	.7	23	14	751	6.41	18	5	ND	1	29	1	2	2	125	.44	.104	5	45	2.09	107	.28	2	5.51	.05	.43	1	1
SA 200E+25N	2	66	8	110	.3	10	14	731	6.48	9	5	ND	1	20	1	2	2	152	.33	.105	5	21	1.98	123	.29	2	3.89	.02	.57	2	1
SA 200E+00N	2	89	41	198	.6	13	14	739	6.04	19	5	ND	1	15	1	3	2	166	.34	.101	6	41	1.42	72	.30	4	3.70	.03	.45	2	2
SA 200E+25S	4	40	18	158	.3	7	14	832	8.44	20	5	ND	1	8	1	4	2	159	.13	.042	11	18	1.88	45	.31	6	4.11	.02	.36	4	1
SA 250E+75N	2	41	35	70	.4	8	7	304	5.23	22	5	ND	1	11	1	2	2	125	.14	.059	6	30	.90	43	.25	35	2.61	.03	.10	1	1
SA 250E+50N	2	42	17	83	.3	5	11	466	5.85	18	5	ND	1	6	1	3	2	144	.18	.075	5	18	1.52	125	.28	2	3.64	.02	.35	2	4
SA 250E+25N	2	65	51	137	.8	16	13	839	6.04	10	5	ND	1	17	1	3	2	155	.34	.094	5	39	1.76	81	.26	2	4.65	.05	.43	2	2
SA 250E+25S	3	47	27	131	.4	15	13	734	7.28	14	5	ND	1	10	1	2	2	179	.18	.063	8	47	1.76	65	.37	3	4.46	.03	.28	1	2
SA 250E+75S	4	29	48	120	.2	16	11	517	6.34	21	5	ND	2	11	1	2	2	122	.13	.034	10	44	1.23	45	.35	2	3.38	.02	.13	1	1
SA 250E+125S	2	85	24	163	.5	25	19	1293	6.57	22	5	ND	1	17	1	2	2	190	.50	.135	4	65	3.01	139	.29	2	3.82	.06	1.34	1	1
SA 300E+375N	3	35	58	107	.4	17	9	391	3.72	18	5	ND	2	41	1	3	9	61	.49	.159	10	28	1.21	116	.19	2	2.53	.03	.18	2	2
SA 300E+350N	7	35	122	156	1.4	19	10	395	4.49	16	5	ND	2	33	1	2	4	57	.41	.163	15	24	.99	100	.19	2	3.04	.05	.13	1	2
SA 300E+325N	6	67	247	233	.9	20	17	884	5.09	22	5	ND	7	42	1	2	2	86	.71	.231	12	26	1.37	192	.22	2	2.57	.04	.21	2	1
STD C/AU-S	20	60	41	133	7.5	69	29	1059	4.30	41	21	8	38	50	19	17	20	58	.52	.094	37	57	.94	181	.08	36	1.87	.06	.14	14	53

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 300E+300N	3	50	89	135	.5	20	12	457	4.42	15	5	ND	5	47	1	2	6	74	.42	.129	14	31	1.38	204	.24	7	3.06	.03	.26	3	25
SA 300E+287N	3	56	88	132	.6	18	13	568	5.37	14	5	ND	6	52	1	2	4	97	.51	.108	12	29	1.66	209	.25	2	2.95	.04	.31	5	3
SA 300E+262N	3	54	50	130	.4	19	13	603	5.36	7	5	ND	4	42	1	3	2	102	.51	.136	14	26	1.55	213	.26	5	3.53	.06	.42	3	5
SA 300E+200N	2	90	58	122	.5	18	18	942	6.96	21	5	ND	3	6	1	2	8	171	.16	.070	6	53	1.96	162	.32	2	3.03	.02	.60	3	10
SA 300E+175N	2	81	21	93	.4	13	16	839	6.65	8	5	ND	3	5	1	2	2	224	.15	.106	4	31	2.16	178	.37	2	3.02	.02	.77	1	1
SA 300E+125N	9	164	29	144	1.2	28	26	1622	8.05	43	5	ND	2	77	1	2	4	214	1.96	.158	3	48	2.77	117	.35	2	8.76	.31	.92	1	7
SA 300E+100N	6	93	19	157	1.3	23	20	1249	7.03	30	5	ND	1	32	1	2	2	192	.80	.105	4	54	2.00	71	.32	2	7.35	.10	.38	1	23
SA 300E+80N	1	94	13	175	.7	36	27	1317	7.41	2	5	ND	3	24	1	2	2	201	.67	.124	5	74	2.74	380	.35	2	4.66	.05	.67	1	2
SA 300E+50N	1	55	19	105	.4	26	14	481	6.99	2	5	ND	1	12	1	2	2	191	.16	.073	5	71	1.83	97	.29	4	4.73	.02	.22	1	19
SA 300E+25N	2	59	19	139	.5	15	13	596	6.60	2	5	ND	1	12	1	2	4	175	.18	.084	7	78	1.56	80	.30	2	4.11	.02	.25	1	6
SA 300E+00N	2	44	20	308	.3	11	12	641	6.05	8	5	ND	1	11	1	2	2	152	.22	.069	8	36	1.69	67	.26	3	3.71	.03	.20	1	1
SA 300E+25S	1	90	29	128	.5	22	21	1009	7.00	2	5	ND	2	17	1	2	2	190	.55	.111	4	54	2.55	115	.34	2	5.15	.09	.75	2	26
SA 300E+50S	1	22	12	87	.4	8	10	613	5.99	8	5	ND	1	7	1	2	2	174	.20	.082	5	31	1.42	48	.34	4	3.55	.03	.61	1	11
SA 300E+75S	2	58	27	120	.6	7	17	677	7.58	2	5	ND	3	8	1	2	2	191	.23	.093	7	13	1.95	217	.33	2	3.74	.03	.72	1	3
SA 300E+126S	11	59	29	87	.6	5	10	676	5.78	49	5	ND	2	4	1	2	2	131	.27	.150	4	5	1.16	61	.20	8	9.15	.01	.21	1	1
SA 350E+225N	1	149	8	161	.5	20	29	1251	7.88	3	5	ND	3	21	1	2	2	172	.57	.122	4	28	2.93	308	.28	2	4.75	.05	1.02	2	1
SA 350E+175N	6	25	44	96	.1	4	10	415	10.14	18	5	ND	3	4	1	2	2	94	.09	.047	17	19	.80	57	.24	2	2.53	.03	.18	2	5
SA 350E+150N	7	20	37	67	.1	7	5	235	7.52	11	5	ND	6	6	1	2	2	54	.06	.041	23	27	.40	24	.25	8	2.80	.03	.06	1	3
SA 350E+100N	2	39	20	77	.4	24	9	386	6.19	2	5	ND	3	14	1	2	2	102	.29	.155	15	29	1.11	63	.34	2	4.80	.03	.14	1	5
SA 350E+75N	3	39	34	84	.3	33	10	474	6.25	8	5	ND	2	13	1	2	2	125	.46	.087	9	43	1.40	42	.39	2	3.25	.03	.14	1	26
SA 350E+50N	2	39	17	107	.3	6	9	378	4.44	9	5	ND	1	6	1	2	2	126	.17	.056	7	33	1.02	84	.25	3	2.85	.02	.18	1	2
SA 350E+25N	1	53	19	113	.4	8	13	757	6.04	7	5	ND	2	10	1	2	2	152	.20	.084	6	19	1.67	150	.28	2	3.93	.02	.44	1	1
SA 350E+50S	1	59	2	108	.3	13	14	761	6.00	3	5	ND	1	18	1	2	2	156	.44	.122	5	10	1.82	123	.25	2	5.35	.06	.62	1	97
SA 350E+75S	1	25	6	147	.4	6	16	764	6.21	2	5	ND	2	12	1	2	2	161	.35	.127	7	8	1.94	121	.26	2	3.99	.03	.71	2	1
SA 450E+500N	4	17	25	102	.1	7	6	368	4.27	11	5	ND	9	16	1	2	2	46	.20	.119	19	15	.65	79	.19	5	2.33	.06	.18	1	1
SA 450E+475N	2	22	35	89	.2	8	4	352	3.38	13	5	ND	2	22	1	2	4	41	.17	.096	19	13	.65	68	.16	5	2.02	.02	.10	1	1
SA 450E+450N	4	47	12	107	.3	21	11	512	5.17	11	5	ND	8	25	1	2	2	93	.38	.115	14	31	1.19	132	.31	2	3.02	.08	.38	1	1
SA 450E+425N	9	42	21	80	.4	9	5	342	4.21	7	5	ND	4	16	1	3	2	98	.18	.100	14	30	1.01	100	.24	9	2.42	.03	.26	1	1
SA 450E+350N	3	39	34	151	.3	30	11	478	4.55	11	5	ND	9	50	1	2	2	62	.53	.139	20	29	1.28	190	.25	2	2.98	.05	.16	1	1
SA 450E+300N	2	39	63	121	.1	20	7	354	3.33	15	5	ND	3	30	1	2	2	57	.37	.121	17	27	.91	94	.18	5	2.39	.03	.09	1	1
SA 450E+200N	6	39	31	132	.2	18	8	342	5.24	5	5	ND	6	12	1	2	2	58	.19	.092	22	24	.70	70	.27	2	3.55	.06	.14	1	8
SA 450E+175N	4	47	31	121	.4	29	9	490	4.87	9	5	ND	12	18	1	2	2	64	.26	.110	17	27	.84	72	.21	4	2.71	.06	.15	1	17
SA 450E+150N	2	140	11	202	.5	18	27	1066	7.02	8	5	ND	2	19	1	2	2	177	.43	.126	4	30	2.44	210	.29	3	5.60	.06	.69	1	5
SA 450E+125N	1	165	10	216	.8	8	21	1344	9.41	2	5	ND	3	43	2	2	2	172	1.35	.160	4	8	3.50	409	.31	5	5.50	.09	1.06	2	1
SA 450E+100N	2	75	44	183	.3	17	11	513	4.65	11	5	ND	2	25	1	2	2	89	.36	.134	11	27	1.16	73	.22	2	3.42	.03	.17	1	1
SA 450E+75N	3	63	48	139	.1	11	9	475	5.67	14	5	ND	3	15	1	2	2	91	.17	.116	13	21	.94	47	.22	2	2.91	.03	.15	1	4
STD C/AU-S	20	60	39	130	7.5	71	29	1047	4.16	41	17	8	38	50	18	16	21	58	.51	.098	37	61	.93	180	.07	39	1.87	.06	.13	13	48

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 450E+50N	3	54	2	149	.3	8	16	834	9.81	2	5	ND	6	6	1	2	2	163	.16	.077	14	4	2.05	119	.36	2	3.86	.02	.82	1	1
SA 450E+25N	2	83	50	148	.1	7	20	1215	8.18	25	5	ND	3	23	1	2	2	178	.36	.118	10	12	2.29	168	.40	3	4.30	.04	.74	2	1
SA 450E+25S	2	125	46	147	.3	8	18	925	6.67	9	5	ND	4	34	1	2	2	143	.39	.113	9	11	2.00	120	.33	4	3.70	.04	.73	3	2
SA 450E+50S	3	83	7	211	.1	5	25	1607	8.69	3	5	ND	1	16	1	2	2	207	.29	.044	19	5	2.99	97	.44	2	4.42	.02	.50	1	1
SA 450E+75S	3	109	14	112	.2	22	13	570	6.75	13	5	ND	5	19	1	2	2	114	.31	.100	12	25	1.39	73	.30	6	3.60	.04	.26	2	9
SA 450E+100S	2	58	13	114	.1	1	9	1197	7.64	4	5	ND	1	9	1	2	2	208	.22	.138	6	17	2.70	505	.43	2	3.43	.02	1.39	1	2
SA 450E+125S	5	41	19	152	.1	8	20	1431	7.01	8	5	ND	3	32	1	2	2	136	.49	.088	12	10	1.75	96	.29	2	5.74	.10	.63	1	2
SA 450E+150S	4	46	25	85	.1	7	8	520	6.87	8	5	ND	1	15	1	2	2	130	.21	.066	10	25	1.29	40	.29	2	3.08	.04	.18	1	2
SA 450E+175S	6	37	31	95	.1	7	11	448	9.49	2	5	ND	2	7	1	2	3	161	.15	.050	11	42	.75	30	.49	4	3.14	.02	.09	1	2
SA 450E+200S	2	19	20	50	.3	3	7	313	3.57	8	5	ND	1	8	1	2	2	96	.21	.040	5	18	.67	40	.31	3	1.98	.03	.13	1	1
SA 500E+425N	4	46	13	75	.1	10	6	461	5.41	3	5	ND	3	15	1	2	2	109	.19	.085	9	21	1.28	109	.24	3	2.18	.03	.39	1	2
SA 500E+400N	3	59	23	102	.1	20	11	438	4.24	9	5	ND	6	40	1	2	2	78	.44	.130	17	36	1.00	134	.23	7	2.52	.03	.20	1	2
SA 500E+340N	3	28	28	152	.1	22	14	444	4.97	7	5	ND	7	97	1	2	2	82	.90	.195	24	27	1.35	190	.29	6	3.28	.06	.15	1	2
SA 500E+300N	5	127	1712	676	3.1	21	9	357	4.25	13	5	ND	4	162	1	2	4	87	.95	.168	15	36	.99	71	.24	4	3.72	.04	.11	3	2
SA 500E+275N	2	60	137	143	.6	22	11	392	4.48	17	6	ND	5	54	1	2	2	72	.80	.241	16	30	1.31	243	.24	6	2.87	.04	.27	1	4
SA 500E+225N	4	49	102	141	.2	24	9	404	4.69	14	5	ND	12	30	1	2	2	58	.36	.114	15	25	.86	58	.13	2	2.24	.02	.10	2	9
SA 500E+212N	3	67	335	191	.2	20	10	474	4.37	17	5	ND	10	31	1	2	2	63	.41	.119	17	24	.95	60	.16	4	2.51	.02	.11	1	4
SA 500E+150N	4	64	343	238	.5	17	9	436	4.97	17	5	ND	6	20	1	2	2	79	.33	.110	13	26	1.00	49	.16	2	2.24	.02	.13	1	9
SA 500E+125N	6	49	43	132	.4	17	11	474	5.98	13	5	ND	7	14	1	2	2	69	.15	.096	18	22	.87	68	.20	8	3.83	.05	.16	3	4
SA 500E+100N	2	80	39	112	.3	15	11	499	5.77	17	5	ND	4	25	1	2	2	100	.23	.113	13	22	1.26	113	.24	7	2.99	.02	.22	1	9
SA 500E+75N	3	54	26	124	.1	13	11	576	5.62	10	5	ND	3	16	1	2	2	112	.28	.102	11	21	1.38	80	.25	3	3.19	.02	.32	1	3
SA 500E+50N	2	39	24	115	.2	22	12	679	4.30	14	5	ND	10	27	1	2	2	72	.49	.129	16	24	1.10	85	.19	2	2.51	.02	.15	1	1
SA 500E+25N	3	61	26	87	.1	8	9	594	6.52	8	5	ND	2	18	1	2	2	137	.20	.104	9	13	1.62	107	.30	4	2.83	.02	.50	1	4
SA 500E+00N	4	68	24	105	.4	13	10	603	6.78	15	5	ND	2	17	1	2	2	120	.22	.110	9	29	1.55	116	.26	2	3.23	.02	.51	1	7
SA 500E+25S	6	61	17	102	.3	8	9	684	5.66	10	5	ND	2	27	1	2	2	129	.14	.083	7	16	1.62	92	.30	5	2.52	.02	.59	1	4
SA 500E+50S	3	53	3	96	.2	10	11	589	6.73	15	5	ND	2	12	1	2	2	177	.18	.096	8	36	1.81	186	.35	2	3.38	.02	.58	2	2
SA 500E+75S	3	74	6	127	.4	10	11	670	6.94	15	5	ND	1	46	1	2	2	162	.31	.097	6	22	1.77	218	.31	2	4.27	.03	.75	3	6
SA 500E+100S	4	104	11	108	.4	2	12	670	6.71	18	5	ND	3	11	1	2	2	143	.41	.132	5	7	1.34	45	.23	13	5.72	.03	.39	2	4
SA 500E+125S	4	86	9	80	.3	3	13	681	5.60	10	5	ND	1	10	1	2	6	172	.40	.157	8	5	1.07	50	.24	11	2.57	.03	.32	1	2
SA 500E+150S	3	52	2	104	.1	6	18	721	6.52	9	5	ND	1	6	1	2	2	157	.31	.098	8	4	1.92	74	.33	6	3.29	.02	.52	1	2
SA 500E+175S	2	76	24	111	.1	4	21	854	6.92	14	5	ND	4	9	1	2	2	186	.37	.125	4	6	2.40	250	.37	7	3.19	.02	1.04	1	1
SA 500E+200S	10	32	40	88	.1	6	8	364	9.47	22	5	ND	4	6	1	2	2	63	.10	.065	21	27	.67	26	.20	2	3.25	.04	.16	1	2
SA 500E+225S	3	51	24	86	.2	22	13	420	7.56	10	5	ND	2	6	1	2	2	180	.16	.041	8	72	1.51	100	.40	2	3.76	.03	.36	1	1
SA 550E+450N	2	31	42	134	.1	16	8	600	4.61	8	5	ND	10	66	1	2	2	63	.67	.156	21	28	1.04	121	.26	9	2.93	.04	.18	1	2
SA 550E+425N	2	36	24	105	.2	15	8	424	4.39	8	5	ND	9	59	1	2	2	64	.64	.168	15	37	1.04	129	.32	5	3.03	.05	.18	1	7
SA 550E+400N	2	30	20	86	.1	12	6	309	3.62	12	5	ND	4	59	1	2	2	67	.58	.120	17	29	.88	89	.23	4	2.74	.03	.11	1	2
STD C/AU-S	19	59	42	127	6.9	66	28	1013	4.15	39	19	7	35	48	18	17	21	56	.50	.089	37	61	.91	174	.08	37	1.84	.06	.13	13	48

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 550E+375N	3	28	16	136	.2	19	8	384	4.08	14	5	ND	5	35	1	2	2	53	.31	.141	31	26	.76	258	.27	3	3.24	.06	.18	2	4
SA 550E+350N	2	27	18	108	.1	14	8	376	3.45	10	5	ND	5	29	1	2	2	46	.37	.139	19	21	.63	97	.20	5	2.51	.03	.11	1	1
SA 550E+325N	3	39	14	96	.1	16	8	297	3.69	6	5	ND	3	40	1	2	2	70	.60	.188	13	39	1.01	227	.33	2	3.28	.04	.18	5	2
SA 550E+300N	5	19	17	92	.1	9	6	295	3.95	10	5	ND	3	36	1	2	2	48	.36	.132	18	17	.64	101	.19	2	2.61	.04	.11	1	5
SA 550E+275N	4	40	34	95	.1	13	8	361	4.44	21	5	ND	3	26	1	2	2	72	.36	.153	16	19	.93	110	.24	7	2.65	.03	.16	1	2
SA 550E+200N	2	59	83	154	.2	11	9	608	4.50	13	5	ND	6	49	1	2	3	79	.46	.114	13	15	1.18	53	.21	2	2.89	.02	.28	2	4
SA 550E+175N	3	362	1533	953	6.5	9	8	619	5.49	10	5	ND	2	15	3	2	2	97	.40	.148	10	12	1.32	33	.27	2	2.79	.03	.32	3	55
SA 550E+150N	3	40	140	352	.6	8	7	436	4.06	13	5	ND	1	15	2	2	2	80	.20	.074	15	16	.88	43	.19	2	2.43	.02	.10	1	151
SA 550E+125N	3	73	1224	588	4.4	9	6	401	4.00	15	5	ND	1	18	1	2	2	79	.20	.106	12	23	.96	38	.05	2	3.32	.01	.13	1	7
SA 550E+100N	3	62	46	113	.1	18	8	467	6.14	11	5	ND	1	17	1	2	2	100	.34	.129	11	48	.96	43	.17	17	3.29	.02	.15	6	4
SA 550E+75N	2	44	13	73	.1	5	10	379	6.61	11	5	ND	1	7	1	2	2	131	.15	.070	8	10	.89	55	.26	7	2.78	.02	.14	1	4
SA 550E+50N	1	112	9	106	.1	4	15	554	6.00	7	5	ND	1	12	1	2	3	149	.39	.124	6	7	1.38	192	.29	2	3.57	.04	.30	1	1
SA 550E+25N	1	20	5	45	.1	5	4	199	4.51	8	5	ND	1	10	1	6	2	156	.13	.065	5	26	.46	22	.42	8	1.94	.01	.04	1	1
SA 550E+00N	3	54	15	102	.2	18	10	409	4.96	11	5	ND	2	27	1	2	3	104	.28	.113	9	26	1.38	153	.22	4	2.95	.03	.43	1	3
SA 550E+25S	2	94	17	115	.6	18	22	842	6.81	10	5	ND	2	19	1	2	2	189	.30	.087	5	54	2.74	376	.39	2	4.08	.03	1.02	1	2
SA 550E+75S	2	87	3	117	.5	15	12	522	5.63	16	5	ND	1	18	1	2	2	119	.28	.126	5	29	1.07	56	.26	4	5.91	.03	.29	7	6
SA 550E+100S	1	75	7	109	.7	10	10	658	6.21	10	5	ND	1	8	1	2	2	167	.17	.106	4	36	1.37	95	.29	2	4.94	.03	.49	1	6
SA 550E+175S	1	52	3	117	.2	9	15	872	6.38	6	5	ND	2	3	1	2	2	134	.21	.090	6	21	1.98	223	.29	2	3.49	.01	.99	1	1
SA 550E+200S	5	66	2	173	.6	19	20	862	7.70	6	5	ND	2	21	1	2	2	211	.56	.092	6	61	2.60	129	.35	6	6.67	.06	.86	1	1
SA 600E+500N	3	22	20	109	.1	12	5	368	3.37	12	5	ND	6	20	1	2	2	42	.26	.106	21	20	.70	73	.19	3	2.01	.03	.11	2	17
SA 600E+475N	3	44	77	109	.6	14	9	475	4.26	19	5	ND	9	38	1	2	2	59	.33	.130	19	26	1.00	147	.23	5	2.61	.04	.18	29	6
SA 600E+450N	3	41	40	91	.3	18	8	313	4.05	16	5	ND	9	31	1	2	4	58	.40	.151	17	31	.77	136	.27	2	2.30	.06	.15	1	1
SA 600E+425N	5	23	16	80	.1	11	7	303	3.89	7	5	ND	4	20	1	2	2	57	.24	.122	21	28	.76	110	.26	2	2.72	.03	.12	18	2
SA 600E+400N	2	30	29	93	.1	17	7	322	3.84	7	5	ND	5	38	1	3	2	57	.50	.186	15	33	.97	168	.21	2	2.31	.03	.17	1	48
SA 600E+375N	4	34	26	98	.1	14	6	327	3.77	13	5	ND	4	32	1	2	3	51	.32	.130	20	24	.74	113	.20	3	2.37	.03	.14	1	1
SA 600E+300N	3	26	28	106	.1	15	7	365	3.66	10	5	ND	6	35	1	2	2	48	.29	.107	19	23	.77	90	.22	2	2.43	.04	.15	1	3
SA 600E+275N	1	51	23	132	.3	9	15	1028	6.88	2	5	ND	3	26	1	2	2	138	.36	.125	6	9	2.29	203	.32	2	3.80	.02	.83	1	3
SA 600E+250N	3	56	93	137	.4	10	8	481	3.73	17	5	ND	3	41	1	2	2	63	.39	.112	13	18	1.06	84	.22	3	2.49	.03	.32	1	2
SA 600E+225N	2	79	222	286	2.0	7	8	651	5.22	6	5	ND	3	32	1	2	2	102	.41	.105	9	15	1.42	55	.27	2	3.01	.05	.31	1	6
SA 600E+200N	12	17	94	118	.1	1	4	489	7.39	24	5	ND	14	3	1	2	4	15	.07	.023	29	8	.18	13	.17	11	2.33	.12	.12	1	4
SA 600E+175N	2	28	135	143	.3	6	14	769	7.54	3	5	ND	3	5	1	2	3	136	.17	.079	12	14	1.85	219	.30	4	3.73	.01	.37	1	1
SA 600E+150N	5	44	343	158	.4	5	8	384	5.83	15	5	ND	2	10	1	2	8	74	.18	.077	15	17	.73	51	.22	2	2.89	.03	.12	1	3
SA 600E+125N	4	27	225	91	.4	4	6	391	5.99	8	5	ND	3	7	1	2	2	89	.17	.070	14	19	.89	62	.27	3	2.93	.03	.25	1	1
SA 600E+100N	1	53	21	115	.1	12	7	401	4.67	9	5	ND	7	12	1	2	3	72	.19	.074	11	13	.89	34	.16	5	2.22	.01	.13	1	3
SA 600E+75N	2	70	326	146	.6	16	8	464	4.66	19	5	ND	7	32	1	2	3	94	.36	.099	10	27	1.31	105	.24	3	3.04	.03	.39	1	5
SA 600E+50N	1	37	13	115	.4	7	14	698	6.41	6	5	ND	1	11	1	2	2	154	.17	.082	9	21	1.56	163	.38	4	3.84	.02	.33	2	1
STD C/AU-S	19	61	42	130	7.1	67	27	1040	4.13	43	16	7	37	49	18	17	23	56	.51	.088	37	61	.91	174	.08	34	1.85	.06	.12	12	51

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 600E+25N	1	44	27	81	.5	1	6	586	6.95	12	5	ND	1	10	1	3	2	168	.20	.094	6	13	1.60	85	.36	3	3.26	.03	.35	1	1
SA 600E+00S	8	26	34	112	.1	2	6	395	7.68	27	5	ND	6	3	1	2	2	35	.09	.047	27	15	.34	33	.22	2	3.16	.06	.11	1	1
SA 600E+25S	2	39	19	84	.4	12	12	502	6.13	15	5	ND	4	12	1	6	2	125	.19	.057	8	37	1.54	85	.32	2	3.35	.02	.43	2	1
SA 600E+50S	20	63	20	90	.9	3	6	573	6.75	16	5	ND	1	12	1	5	2	172	.11	.088	7	43	2.07	188	.38	2	3.69	.03	.83	2	3
SA 600E+75S	14	69	16	77	.7	3	5	595	6.32	8	5	ND	1	22	1	4	2	162	.09	.092	5	35	1.97	103	.35	10	3.39	.03	.82	1	6
SA 600E+100S	4	67	27	88	.7	12	8	583	7.64	13	5	ND	2	9	1	2	2	176	.14	.117	8	55	1.71	130	.40	6	3.50	.02	.55	1	1
SA 600E+125S	5	63	24	138	.5	28	15	868	7.61	8	5	ND	1	7	1	2	5	141	.15	.056	6	84	1.71	62	.29	2	6.18	.01	.21	1	1
SA 600E+150S	3	45	13	91	.6	13	9	539	5.41	17	5	ND	1	10	1	5	2	149	.15	.077	4	52	1.53	71	.27	3	3.37	.02	.21	1	5
SA 600E+175S	7	20	43	90	.3	3	6	312	6.27	13	5	ND	3	7	1	2	2	56	.10	.089	18	19	.46	24	.24	2	3.37	.04	.10	2	1
SA 600E+200S	2	81	24	99	.6	14	12	415	6.87	7	5	ND	1	7	1	2	2	170	.16	.074	10	37	1.55	84	.31	2	4.98	.01	.28	2	2
SA 600E+225S	2	66	29	146	.9	15	19	773	6.96	18	5	ND	1	13	1	2	7	199	.29	.062	4	31	2.15	132	.38	2	6.36	.06	.43	4	2
SA 600E+300S	1	68	34	88	.7	18	13	423	7.09	3	5	ND	1	6	1	2	2	230	.18	.071	5	64	1.40	80	.38	8	4.84	.02	.19	1	3
SA 600E+325S	1	96	21	87	.7	13	13	654	6.36	11	5	ND	1	6	1	2	2	187	.17	.087	6	41	1.97	62	.36	2	3.81	.02	.42	1	3
SA 650E+500N	2	26	43	145	.6	22	9	519	4.13	16	6	ND	5	42	1	4	2	50	.31	.110	29	25	.72	115	.25	6	3.06	.06	.13	2	2
SA 650E+475N	1	27	28	123	.6	17	8	464	3.55	15	5	ND	21	24	1	4	4	45	.27	.118	16	21	.67	54	.13	10	1.86	.02	.07	4	6
SA 650E+450N	3	33	27	106	.6	14	10	373	4.67	10	5	ND	6	48	1	2	5	75	.55	.200	14	41	1.26	329	.26	5	2.68	.03	.29	8	2
SA 650E+425N	2	26	32	79	.5	11	6	251	3.22	7	5	ND	1	24	1	2	6	64	.19	.086	16	39	.71	85	.27	2	3.28	.02	.08	9	3
SA 650E+350N	1	31	16	92	.4	29	8	279	3.82	11	5	ND	1	28	1	2	2	68	.30	.113	15	36	1.03	94	.35	2	3.44	.03	.09	2	4
SA 650E+300N	3	42	71	120	.5	11	10	552	5.59	16	5	ND	3	18	1	3	3	101	.27	.108	13	21	1.23	87	.29	5	3.15	.03	.22	1	2
SA 650E+275N	2	33	39	73	.3	10	7	380	4.60	18	5	ND	2	11	1	3	2	88	.13	.067	11	25	.82	53	.30	2	2.29	.02	.13	1	3
SA 650E+250N	3	74	44	117	.8	15	8	506	5.69	22	5	ND	1	46	1	3	2	111	.50	.167	10	35	1.13	75	.25	8	4.00	.03	.26	4	8
SA 650E+225N	3	99	25	75	1.0	9	5	463	5.39	5	5	ND	1	17	1	2	2	128	.21	.118	7	50	1.27	60	.25	3	3.85	.02	.38	3	1
SA 650E+200N	1	77	189	232	.6	17	9	513	5.25	18	5	ND	4	23	1	2	2	95	.31	.126	12	34	1.14	60	.24	2	2.79	.02	.21	1	73
SA 650E+175N	7	19	57	103	.2	7	8	376	8.24	20	5	ND	9	9	2	2	3	68	.13	.078	20	33	.62	29	.27	2	3.20	.04	.12	1	2
SA 650E+150N	1	36	25	99	.5	14	10	619	5.05	14	7	ND	13	17	1	5	2	91	.24	.098	10	21	1.15	42	.25	2	2.29	.01	.18	1	3
SA 650E+100N	1	29	38	61	.5	6	6	291	4.36	11	5	ND	1	9	1	2	2	102	.19	.058	5	23	.62	21	.35	5	2.29	.02	.08	1	1
SA 650E+75N	6	2	57	83	.1	2	3	254	6.36	15	5	ND	3	2	1	2	2	14	.06	.041	52	10	.10	10	.16	9	4.02	.06	.06	2	1
SA 650E+50N	1	43	67	142	.3	11	8	506	4.89	16	5	ND	3	9	1	3	2	79	.23	.088	11	16	1.04	24	.22	4	2.50	.01	.14	1	4
SA 650E+00N	1	66	15	146	.4	2	14	790	6.71	2	5	ND	1	6	1	2	2	151	.20	.085	7	9	1.84	60	.33	9	5.03	.02	.24	1	1
SA 650E+25S	1	63	11	166	.6	14	18	951	7.58	5	5	ND	1	8	1	2	2	177	.16	.070	5	21	2.41	278	.45	4	5.02	.02	.52	2	1
SA 650E+50S	2	83	12	53	.6	25	10	253	4.30	5	5	ND	1	17	1	5	2	108	.16	.098	3	78	.95	87	.17	2	5.71	.03	.18	1	4
SA 650E+75S	1	58	3	60	.4	10	8	231	5.37	5	5	ND	1	5	1	2	2	165	.13	.082	3	98	1.85	245	.38	2	3.34	.02	.49	1	2
SA 650E+100S	1	65	17	125	.5	25	15	474	5.27	19	5	ND	1	18	1	5	2	155	.28	.110	8	89	1.93	193	.30	3	4.29	.03	.34	1	3
SA 650E+125S	1	47	27	129	.4	14	9	476	4.44	16	5	ND	3	21	1	2	2	102	.31	.091	10	38	1.36	73	.21	3	2.87	.02	.15	1	1
SA 650E+150S	3	33	27	115	.2	12	7	374	5.38	8	5	ND	3	11	1	4	2	98	.12	.083	16	37	1.10	86	.29	3	4.00	.04	.17	1	2
SA 650E+175S	1	52	25	118	.4	21	9	634	4.45	11	5	ND	7	21	1	2	2	82	.27	.104	14	26	1.03	65	.20	3	2.68	.02	.13	1	5
STD C/AU-S	18	59	39	133	7.5	73	29	1116	4.27	42	26	7	37	51	19	16	21	59	.51	.095	37	64	.93	183	.09	35	1.93	.06	.13	12	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 650E+200S	4	59	13	131	.1	23	12	578	4.81	20	5	ND	5	22	1	2	2	117	.31	.129	15	35	1.40	93	.27	2	3.66	.03	.28	2	1
SA 650E+225S	5	54	27	134	.1	18	12	761	5.45	11	5	ND	9	13	1	4	2	113	.15	.074	17	27	1.32	68	.24	2	3.19	.02	.22	1	1
SA 650E+262.5S	4	93	21	99	.1	21	20	771	6.41	16	6	ND	2	7	1	2	2	190	.15	.070	10	39	2.25	227	.36	8	3.84	.02	.66	2	1
SA 650E+275S	4	73	9	99	.1	23	20	462	6.11	13	5	ND	2	7	1	2	2	191	.15	.059	6	75	2.35	143	.37	4	3.92	.03	.79	2	1
SA 650E+300S	6	39	22	86	.1	14	8	410	5.02	17	5	ND	3	12	1	2	2	76	.14	.056	14	30	.73	33	.23	3	2.71	.02	.10	3	1
SA 650E+325S	4	104	2	104	.1	19	21	667	7.05	9	5	ND	1	5	1	2	6	198	.14	.045	5	42	2.31	171	.37	4	5.19	.03	.79	3	1
SA 650E+350S	3	59	15	94	.1	16	13	463	4.54	16	5	ND	1	16	1	2	2	126	.30	.072	7	27	1.48	102	.25	2	3.12	.03	.33	2	94
SA 650E+400S	5	47	12	84	.1	14	15	610	6.83	15	6	ND	1	4	1	2	2	204	.08	.026	6	43	1.73	63	.39	13	3.64	.02	.28	1	1
SA 650E+425S	4	57	14	66	.1	17	12	404	4.97	10	5	ND	2	3	1	2	2	124	.31	.064	8	50	1.07	45	.30	4	2.89	.03	.15	1	2
SA 650E+450S	3	51	2	99	.1	10	20	947	7.00	5	5	ND	1	7	1	2	2	202	.33	.132	6	10	2.38	77	.39	8	3.76	.03	1.19	1	1
SA 650E+475S	4	53	10	106	.1	13	15	690	7.00	8	6	ND	1	5	1	2	2	186	.09	.038	7	35	1.75	52	.37	7	3.70	.02	.34	1	1
SA 650E+500S	4	95	57	459	.4	18	15	828	5.39	18	5	ND	1	28	1	2	3	166	.31	.104	5	49	1.78	55	.25	7	4.09	.06	.40	5	2
SA 700E+500N	3	22	9	79	.1	18	8	302	3.83	18	5	ND	5	90	1	32	8	72	.75	.216	16	35	.74	131	.22	6	2.80	.05	.11	1	1
SA 700E+475N	6	25	17	94	.1	16	6	372	3.98	13	5	ND	9	30	1	2	2	48	.25	.099	21	24	.55	47	.18	2	2.55	.05	.10	5	1
SA 700E+445N	3	38	27	116	.1	19	9	384	3.50	15	5	ND	5	38	1	2	2	64	.39	.142	15	41	1.09	243	.21	5	2.38	.02	.18	1	1
SA 700E+395N	4	25	17	100	.2	17	6	324	3.40	13	5	ND	3	52	1	2	2	64	.39	.158	21	36	.87	114	.24	7	3.25	.03	.15	5	1
SA 700E+375N	5	29	5	100	.3	15	10	307	3.90	14	7	ND	1	129	1	2	2	51	.76	.124	14	21	.69	72	.10	2	3.47	.03	.11	14	1
SA 700E+350N	6	15	18	74	.1	8	5	230	3.52	19	5	ND	1	46	1	2	2	59	.33	.117	19	22	.54	89	.22	7	2.97	.04	.09	1	1
SA 700E+325N	5	82	20	115	.8	19	10	471	4.04	42	5	ND	2	244	1	2	2	75	1.35	.104	9	31	.74	59	.14	4	4.88	.02	.16	2	9
SA 700E+300N	7	106	40	128	1.0	22	11	519	6.23	50	5	ND	3	119	1	2	2	101	.78	.146	8	39	.95	56	.14	7	3.87	.03	.21	4	8
SA 700E+270N	63	277	196	263	.9	76	72	2921	22.04	692	6	ND	5	17	2	4	2	45	.09	.279	13	14	.41	24	.05	7	1.91	.01	.09	5	25
SA 700E+250N	16	152	55	175	.9	26	18	926	7.91	144	5	ND	3	65	1	2	2	98	.34	.212	13	26	.95	76	.11	3	3.50	.02	.17	3	5
SA 700E+225N	6	73	10	127	.1	10	10	752	4.99	17	5	ND	1	40	1	2	2	113	.32	.120	8	25	1.20	57	.25	6	4.80	.03	.18	5	1
SA 700E+200N	3	23	8	54	.1	6	6	265	3.98	15	5	ND	2	7	1	2	2	112	.12	.054	6	38	.72	21	.31	2	2.40	.02	.11	1	1
SA 700E+175N	5	72	202	223	.2	16	12	594	5.33	29	5	ND	2	21	1	2	2	125	.29	.121	13	41	1.27	90	.26	14	3.56	.04	.32	4	7
SA 700E+150N	2	45	8	101	.4	8	15	1482	5.16	10	5	ND	1	25	1	2	2	149	.15	.069	6	23	1.16	89	.25	12	3.24	.02	.24	2	6
SA 700E+125N	3	47	13	73	.1	11	10	510	4.99	6	5	ND	1	17	1	2	2	104	.11	.058	8	39	.98	48	.21	7	3.14	.02	.14	2	1
SA 700E+100N	4	42	9	112	.1	6	13	775	6.18	11	5	ND	6	15	1	4	2	140	.24	.096	9	14	1.44	40	.31	3	3.39	.02	.30	3	1
SA 700E+75N	3	55	356	111	.3	10	8	444	4.18	18	5	ND	3	15	1	2	2	89	.25	.087	11	17	.85	28	.26	3	2.31	.03	.16	1	31
SA 700E+50N	3	58	17	101	.1	3	13	928	5.77	7	5	ND	2	7	1	2	2	128	.14	.080	10	10	1.47	35	.29	2	3.51	.03	.40	1	1
SA 700E+25N	3	112	41	103	.3	3	13	924	5.39	14	5	ND	2	42	1	2	2	99	.30	.122	6	6	.86	15	.15	2	4.77	.03	.12	2	34
SA 700E+00N	3	54	21	88	.4	10	7	444	4.44	19	5	ND	1	22	1	2	2	129	.23	.119	7	33	1.04	75	.24	2	3.65	.03	.34	1	3
SA 700E+25S	8	38	16	157	.1	8	11	814	8.20	22	5	ND	2	8	1	2	2	119	.07	.070	14	39	.98	46	.25	2	3.93	.02	.16	6	1
SA 700E+50S	18	145	46	147	.7	29	22	1453	6.90	35	5	ND	1	52	1	2	2	141	.19	.165	9	45	.96	105	.14	3	3.24	.02	.24	2	3
SA 700E+75S	7	54	22	99	.3	12	10	552	7.31	15	5	ND	5	11	1	5	2	118	.13	.076	13	45	1.13	55	.31	2	4.00	.05	.22	4	2
SA 700E+100S	3	41	8	100	.1	12	10	602	5.68	10	5	ND	8	14	1	2	2	147	.16	.077	5	34	1.66	88	.31	3	3.40	.03	.50	1	2
STD C/AU-S	20	59	38	130	7.3	68	29	1088	3.82	38	18	7	41	51	17	17	20	58	.47	.091	39	62	.84	181	.08	36	1.81	.06	.14	14	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SA 700E+125S	2	85	27	136	.3	12	19	767	6.53	2	5	ND	2	24	1	2	2	213	.32	.072	4	32	2.30	125	.33	3	4.78	.05	.43	1	8
SA 700E+150S	1	68	54	164	.4	13	9	461	4.33	10	5	ND	4	18	1	2	2	94	.35	.113	11	23	1.07	67	.17	2	2.66	.02	.16	2	5
SA 700E+175S	2	51	23	97	.2	7	12	430	5.21	6	5	ND	2	8	1	2	2	141	.14	.061	7	23	1.29	58	.26	3	3.38	.02	.21	1	1
SA 700E+200S	1	125	24	150	.3	12	12	495	5.83	7	5	ND	3	14	1	2	2	136	.26	.084	11	23	1.76	139	.23	3	3.01	.03	.44	1	1
SA 700E+225S	2	87	29	86	.2	8	14	490	6.89	2	5	ND	1	8	1	2	2	150	.33	.070	7	21	1.50	79	.30	3	4.51	.06	.23	1	1
SA 700E+250S	3	106	3	157	.2	11	19	698	7.63	2	5	ND	2	7	1	2	2	195	.15	.050	6	33	2.51	100	.35	11	5.25	.03	.33	1	1
SA 700E+250SA	2	37	22	51	.5	1	3	123	3.97	5	5	ND	1	10	1	4	2	139	.09	.079	5	23	.24	16	.17	5	2.92	.01	.03	1	1
SA 700E+275S	2	48	29	116	.2	9	10	462	4.42	3	5	ND	1	13	1	2	2	128	.13	.049	7	31	1.33	50	.24	4	3.10	.02	.22	4	3
SA 700E+300S	2	79	35	138	.4	27	24	1577	6.09	21	5	ND	1	16	1	2	2	125	.24	.092	9	60	1.98	89	.21	7	3.49	.03	.37	1	1
SA 700E+325S	3	76	24	64	.2	6	8	330	6.20	5	5	ND	1	6	1	2	2	156	.17	.106	8	33	1.04	44	.34	36	3.12	.04	.19	1	1
SA 700E+350S	2	49	22	54	.1	9	8	286	3.73	6	5	ND	1	8	1	3	2	103	.12	.065	7	40	.86	24	.24	11	2.45	.03	.22	1	1
SA 700E+375S	2	77	31	83	.4	9	8	432	4.92	4	5	ND	1	13	1	2	2	129	.19	.105	9	41	1.32	43	.30	7	3.17	.04	.37	1	3
SA 700E+400S	1	84	27	166	.4	12	25	1218	8.07	2	5	ND	2	8	1	2	2	209	.26	.084	6	21	2.89	608	.39	2	4.22	.02	.84	1	1
SA 700E+425S	2	44	6	76	.1	9	6	277	4.06	6	5	ND	1	5	1	3	2	107	.11	.089	16	18	.70	37	.23	2	3.51	.04	.20	1	3
SA 700E+450S	1	126	17	146	.5	19	21	986	6.84	7	5	ND	2	12	1	2	2	193	.24	.084	5	54	2.40	144	.37	2	3.79	.04	1.03	1	2
SA 700E+475S	1	95	16	172	.5	11	24	1218	6.88	2	5	ND	2	23	1	2	2	189	.80	.101	4	28	2.47	161	.37	2	3.38	.06	1.11	1	1
SA 700E+500S	2	84	26	124	.1	21	14	697	5.70	23	5	ND	3	19	1	2	2	123	.29	.096	6	45	1.84	91	.30	7	3.43	.04	.61	1	4
SA 800E+500N	3	17	24	57	.3	2	4	192	4.54	10	5	ND	1	24	1	2	3	47	.13	.096	16	18	.39	49	.16	3	2.12	.02	.06	9	1
SA 800E+475N	3	45	15	102	.1	6	7	431	8.07	2	5	ND	2	46	1	2	6	101	.55	.245	7	25	1.51	290	.30	45	4.09	.04	.70	96	1
SA 800E+450N	7	10	24	74	.1	1	4	233	7.12	8	5	ND	4	10	1	2	5	28	.06	.046	24	21	.23	28	.16	32	2.93	.05	.07	1	2
SA 800E+425N	1	23	21	79	.1	14	7	322	3.21	11	5	ND	3	95	1	2	2	45	.68	.079	12	18	.64	55	.10	3	2.63	.02	.07	5	1
SA 800E+400N	4	30	19	62	.1	10	5	267	3.10	6	5	ND	2	55	1	3	2	49	.35	.088	14	20	.65	66	.11	2	2.19	.02	.05	7	3
SA 800E+375N	2	30	10	90	.4	12	6	388	4.14	7	5	ND	4	39	1	2	2	74	.43	.107	10	22	.87	69	.16	29	3.77	.07	.17	2	1
SA 800E+350N	7	19	45	75	.1	3	5	333	7.25	18	5	ND	3	20	1	2	2	61	.11	.073	22	18	.49	49	.24	4	3.04	.03	.13	1	4
SA 800E+325N	2	22	19	78	.2	12	7	392	4.34	2	5	ND	2	36	1	2	2	73	.32	.119	12	22	.83	82	.24	7	3.37	.03	.13	1	1
SA 800E+300N	2	55	46	86	1.0	3	7	500	6.85	11	5	ND	1	33	1	2	2	85	.30	.109	7	16	.69	58	.18	2	3.58	.02	.16	2	7
SA 800E+275N	2	37	33	95	.5	3	8	634	4.95	5	5	ND	2	48	1	2	2	110	.47	.094	9	11	1.18	164	.26	4	3.66	.07	.38	3	165
SA 800E+250N	3	26	17	107	.2	14	8	429	4.10	13	5	ND	5	17	1	2	2	59	.18	.050	12	18	.78	47	.17	3	2.42	.02	.08	4	1
SA 800E+225N	4	29	25	81	.5	11	10	666	5.94	21	5	ND	2	25	1	4	3	82	.20	.093	10	19	.84	48	.18	5	2.37	.02	.10	1	1
SA 800E+200N	7	15	20	91	.2	1	8	937	5.64	14	5	ND	2	14	1	2	2	100	.19	.047	13	15	.82	55	.27	36	3.17	.03	.16	1	1
SA 800E+175N	17	215	210	166	4.8	1	23	60016	15.57	69	9	ND	1	5	4	3	11	42	.05	.096	25	18	.24	79	.05	2	6.54	.01	.03	1	195
SA 800E+150N	15	34	17	144	.3	6	10	631	6.91	13	5	ND	1	11	1	2	2	157	.20	.069	8	30	1.05	44	.30	4	3.94	.02	.20	1	5
SA 800E+125N	10	43	30	87	.6	4	8	2167	5.94	15	5	ND	1	12	1	2	3	118	.22	.084	7	30	.91	40	.28	2	3.74	.02	.12	3	3
SA 800E+100N	16	20	14	79	.4	2	6	525	5.92	21	5	ND	1	7	1	2	5	100	.07	.052	18	22	.42	21	.18	3	3.43	.02	.09	1	1
SA 800E+75N	3	21	48	106	.4	5	12	652	7.32	10	5	ND	1	8	1	3	5	242	.21	.057	6	33	1.60	72	.48	2	3.44	.02	.39	1	1
SA 800E+50N	5	24	27	98	.3	2	7	369	5.22	23	5	ND	1	7	1	2	2	112	.16	.075	6	13	.65	21	.20	3	3.38	.02	.05	1	1
STD C/AU-S	19	59	38	128	7.4	70	28	1031	4.14	38	19	7	36	48	18	17	25	55	.51	.088	36	61	.91	171	.08	37	1.83	.06	.13	13	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
SK-36	183	654	1558	41211	9.8	13	25	516	3.58	30	5	ND	2	24	518	2	3	23	.45	.052	2	6	.69	18	.01	3	1.37	.01	.18	1	35
SK-37	80	59	6691	630	3.4	4	3	99	.54	5	5	ND	1	2	4	7	5	2	.01	.001	2	2	.03	2	.01	2	.07	.01	.02	1	6
SK-38	58	20	846	622	1.0	4	4	139	.75	2	8	ND	1	1	2	5	3	8	.04	.009	2	1	.09	6	.01	2	.18	.01	.06	1	1
SK-39	2	44	48	119	.6	15	8	328	2.21	10	5	ND	3	136	1	2	6	45	2.94	.077	4	13	.54	22	.12	10	3.12	.10	.16	1	1
SK-40	3	71	405	814	.5	12	6	920	2.70	5	5	ND	3	62	12	2	2	55	2.54	.056	6	9	.63	16	.01	2	1.68	.01	.22	1	1
SK-41	10	30	18	144	.2	13	4	457	3.63	4	5	ND	3	64	2	5	6	54	1.16	.038	5	13	.93	48	.16	3	2.22	.09	.44	1	1
SK-42	2	49	31	97	.1	131	24	663	5.07	12	5	ND	3	188	1	2	4	82	2.96	.174	26	35	3.61	331	.55	2	3.23	.32	.15	1	1
SK-44	1	51	28	72	.2	1	12	808	4.51	2	5	ND	3	67	1	2	5	85	2.97	.123	4	3	1.12	206	.18	8	2.57	.13	.63	1	1
SK-45	3	8	18	336	.1	8	3	622	1.33	4	5	ND	1	18	11	2	2	12	1.10	.012	2	2	.28	14	.02	2	.43	.01	.04	1	1
SK-46	57	66	1335	507	2.1	2	4	303	1.98	6	5	ND	1	1	1	2	3	15	.04	.019	2	5	.26	11	.01	6	.52	.01	.11	1	1
SK-47	5	31	9	146	.2	21	6	278	2.70	4	5	ND	2	92	2	2	3	76	1.71	.061	2	23	.52	30	.12	2	2.06	.10	.26	1	1
SK-48	1	21	302	235	.3	4	4	487	2.23	2	5	ND	11	15	1	3	3	20	.20	.045	15	3	.44	98	.08	2	.79	.04	.15	1	3
SK-49	1	16	17	65	.1	2	6	640	2.13	4	6	ND	2	120	1	2	2	37	2.13	.128	4	1	.31	20	.12	2	1.30	.01	.02	1	2
SK-50	1	53	30	122	.5	3	15	1068	5.93	5	5	ND	3	16	1	2	4	127	.68	.181	5	3	1.71	132	.24	13	2.20	.05	.83	1	1
SK-51	5	360	1362	1956	5.6	6	9	412	2.60	5	5	ND	2	9	18	2	4	29	.16	.018	2	2	.52	10	.01	2	.91	.01	.08	3	57
SK-52	2	68	27	81	.4	18	10	183	2.09	10	5	ND	3	56	1	2	2	48	2.29	.095	4	24	.30	25	.12	5	2.73	.19	.12	1	2
SK-53	3	36	30	112	.1	79	24	936	6.21	2	5	ND	1	108	1	2	4	89	3.38	.160	19	97	3.53	159	.28	6	2.67	.14	.22	1	2
SK-54	4	94	20	54	.5	17	14	362	6.13	2	5	ND	3	125	1	2	5	91	1.51	.194	4	27	1.34	79	.19	2	3.08	.24	.42	2	9
SK-55	1	44	32	22	.3	3	4	289	1.99	4	5	ND	2	232	1	2	2	48	2.34	.117	4	3	.19	6	.12	2	1.76	.09	.05	1	1
SK-56	1	7	5	7	.1	1	1	72	.53	2	5	ND	17	1	1	3	2	2	.01	.002	5	1	.03	4	.01	2	.15	.04	.06	1	1
SK-57	1	5	23	70	.1	7	7	276	2.10	2	5	ND	11	25	1	2	5	19	.34	.058	14	6	.56	30	.09	2	.93	.04	.10	1	2
SK-58	1	54	11	65	.3	7	11	657	4.09	4	5	ND	3	26	1	2	2	79	.90	.115	4	10	1.13	64	.21	2	1.54	.08	.48	1	1
SK-59	5	87	18	96	.5	17	14	910	5.83	9	5	ND	5	20	1	2	2	140	.91	.146	4	44	1.84	50	.24	2	2.92	.04	.87	1	1
SK-60	10	57	7	71	.3	6	9	655	4.64	2	5	ND	4	60	1	2	2	103	2.42	.097	4	14	1.36	79	.24	3	4.14	.20	.75	1	1
SK-61	1	55	9	80	.5	12	12	983	5.15	7	5	ND	3	65	1	2	5	123	1.18	.105	4	25	1.85	202	.25	11	3.54	.26	1.13	1	3
SK-62	2	80	9	42	.7	9	10	403	4.53	20	5	ND	4	96	1	2	2	101	1.42	.105	5	36	.95	26	.15	4	2.52	.19	.18	1	1
SK-63	1	3	2	11	.1	2	1	261	.43	2	5	ND	15	2	1	2	2	2	.01	.001	6	1	.02	2	.01	2	.14	.05	.05	1	2
SK-64	9	49	10	83	.5	17	9	678	5.25	13	5	ND	4	19	1	2	2	169	.69	.087	3	32	1.79	40	.27	12	2.71	.10	.96	1	1
SK-65	7	80	20	96	.6	29	14	352	4.93	6	5	ND	3	87	1	2	4	119	2.96	.090	4	35	1.23	24	.18	2	4.39	.13	.42	2	2
SK-66	10	7921	17183	10579	101.7	4	47	103	4.31	78	5	ND	1	1	127	2	2	3	.01	.004	2	1	.05	7	.01	7	.12	.01	.04	9	220
SK-67	13	28	15	7	.2	4	5	42	1.11	2	5	ND	1	2	1	4	2	4	.01	.001	2	2	.04	3	.01	8	.08	.01	.01	35	1
SK-68	1	7	4	37	.1	3	1	166	.63	2	5	ND	18	2	1	2	2	3	.02	.001	11	1	.03	2	.03	8	.21	.04	.06	2	3
SK-69	20	158	621	5270	6.5	3	7	581	2.48	4	5	ND	2	21	85	2	2	22	.94	.043	2	2	.42	19	.01	6	.77	.01	.15	4	36
STD C/AU-R	19	59	40	132	7.2	71	28	1050	4.32	38	18	8	40	51	19	18	20	58	.52	.087	38	60	.90	182	.06	35	1.80	.06	.14	13	510

APPENDIX E

GEOCHEMICAL STATISTICAL RESULTS

SADDLE-SHAKTI GRID GEOCHEMICAL STATISTICS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
COPPER	2.0	362.0	60.3	40.4	53.0
LEAD	2.0	1712.0	53.8	163.0	23.0
ZINC	45.0	2125.0	133.3	147.6	108.0
SILVER	0.1	6.5	0.4	0.6	0.3
ARSENIC	2.0	692.0	16.3	43.0	13.0
CHROMIUM	4.0	122.0	30.6	18.2	27.0
GOLD	1.0	195.0	6.9	21.1	2.0

TOTAL NUMBER OF SAMPLES = 273

MT. GEORGE SOIL LINE GEOCHEMICAL STATISTICS (ALL IN PPM EXCEPT AU (PPB))

ELEMENT	MIN	MAX	MEAN	STD DEV	MEDIAN
COPPER	9.0	183.0	72.3	42.3	66.0
LEAD	2.0	37.0	15.4	6.9	15.0
ZINC	5.0	164.0	87.2	27.8	89.0
SILVER	0.1	0.7	0.2	0.1	0.2
ARSENIC	2.0	15.0	6.6	2.8	6.0
CHROMIUM	5.0	216.0	49.1	40.5	40.0
GOLD	1.0	9.0	1.6	1.4	1.0

TOTAL NUMBER OF SAMPLES = 47

SADDLE-SHAKTI GRID VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
COPPER	2.0	362.0	60.3	40.4	53.0

LINE	STATION	PPM
0E	300S	149.0
0E	375S	169.0
0E	525S	233.0
300E	125N	164.0
350E	225N	149.0
450E	125N	165.0
550E	175N	362.0
700E	270N	277.0
700E	250N	152.0
700E	50S	145.0
800E	175N	215.0

SADDLE-SHAKTI GRID VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
LEAD	2.0	1712.0	53.8	163.0	23.0

LINE	STATION	PPM
500E	300N	1712.0
550E	175N	1533.0
550E	125N	1224.0

SADDLE-SHAKTI GRID VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
ZINC	45.0	2125.0	133.3	147.6	108.0

LINE	STATION	PPM
500E	300N	676.0
550E	175N	953.0
550E	125N	588.0
650E	500S	459.0
800E	150S	2125.0

SADDLE-SHAKTI GRID VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
SILVER	0.1	6.5	0.4	0.6	0.3

LINE	STATION	PPM
500E	300N	3.1
550E	175N	6.5
550E	125N	4.4
600E	225N	2.0
800E	175N	4.8

SADDLE-SHAKTI GRID VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
ARSENIC	2.0	692.0	16.3	43.0	13.0

LINE	STATION	PPM
700E	270N	692.0
700E	250N	144.0

SADDLE-SHAKTI GRID VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
CHROMIUM	4.0	122.0	30.6	18.2	27.0

LINE	STATION	PPM
0E	150S	87.0
0E	325S	85.0
300E	80N	74.0
300E	50N	71.0
300E	25N	78.0
500E	225S	72.0
600E	125S	84.0
650E	50S	78.0
650E	75S	98.0
650E	100S	89.0
650E	275S	75.0
800E	450S	121.0
800E	500S	122.0

SADDLE-SHAKTI GRID VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
GOLD	1.0	195.0	6.9	21.1	2.0

LINE	STATION	PPB
0E	50S	76.0
350E	50S	97.0
550E	175N	55.0
550E	150N	151.0
650E	200N	73.0
650E	350S	94.0
800E	275N	165.0
800E	175N	195.0

SADDLE-MT. GEORGE VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
COPPER	9.0	183.0	72.3	42.3	66.0

LINE	STATION	PPM
0E	575N	180.0
0E	475N	183.0
0E	350N	168.0
0E	175S	176.0

SADDLE-MT. GEORGE VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
LEAD	2.0	37.0	15.4	6.9	15.0

LINE	STATION	PPM
0E	375N	37.0
0E	475S	32.0

SADDLE-MT. GEORGE VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
ZINC	5.0	164.0	87.2	27.8	89.0

LINE	STATION	PPM
0E	475N	164.0
0E	350N	156.0

SADDLE-MT. GEORGE VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
SILVER	0.1	0.7	0.2	0.1	0.2

LINE	STATION	PPM
0E	375N	0.7

SADDLE-MT. GEORGE VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
ARSENIC	2.0	15.0	6.6	2.8	6.0

LINE	STATION	PPM
0E	375N	15.0
0E	274S	14.0

SADDLE-MT. GEORGE VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
CHROMIUM	5.0	216.0	49.1	40.5	40.0

LINE	STATION	PPM
0E	325S	216.0

SADDLE-MT. GEORGE VALUES ABOVE MEAN + 2 STANDARD DEVIATIONS

ELEMENT	MINIMUM	MAXIMUM	MEAN	STD. DEV.	MEDIAN
GOLD	1.0	9.0	1.6	1.4	1.0

LINE	STATION	PPB
0E	400N	6.0
0E	400S	9.0

APPENDIX F

MINERALOGICAL ANALYSIS

MINERALOGICAL ANALYSIS OF A SAMPLE FROM THE SADDLE PROPERTY

BY
C.L. Soux, B.Sc.

OREX LABORATORIES Ltd.

1. Introduction

A mineralized hand specimen from the saddle property was delivered to Orex Laboratories by Shangri La Minerals for thr purpose of carrying out a complete mineralogical analysis.

The purpose of the present study is to quantify the ore minerals present and to establish the paragenetic relationships among the ore minerals.

2. Sample Preparation

In order to obtain a representative mineralogical composition of the ore, the original sample was subjected to the following treatment:

- The sample was crushed to 100% passing 1 mm and then panned in a batea type of pan. Three gravity products were obtained: Concentrate, middlings and tailings.
- The three different products were then dried and weighed.
- Since most of the ore minerals report in the concentrate and middlings, representative quantities of these two products were prepared into briquettes and then polished.
- The mineralogical analysis was carried out by microscopic observation of the two polished sections.

3. Results

The detailed mineralogical study of the concentrate and middlings products of the sample are given in separate sheets which form part of this report.

The mineralogical composition of the whole sample is given below:

PHASE	% WEIGHT
Chalcopyrite	17
Pyrite	15
Galena	5
Sphalerite	3
Goethite	3
Cerussite	<1
Covellite	<1
Gold	<<1
Gangue	47
TOTAL	100

The tentative paragenetic sequence of deposition of the different hypogene minerals is as follows:

Pyrite
Chalcopyrite
Sphalerite
Galena
Quartz ?
Gold ?

At the original grind of 100% passing 1mm, about 90% of the total gold in the sample was liberated. The rest of the gold (10%) is tied up with pyrite and occurs as small inclusions in this mineral. The size of these inclusions vary between 2 microns and 10 microns.

MINERALOGRAPHIC REPORT

by C. L. Soux

For: Shangri La Minerals
Project: Saddle
Sample: SDL-K
Location: Stewart, B.C.
Collector:
Date Analyzed: Sep/25/87

MACROSCOPIC DESCRIPTION:

Hand specimen ground to 100% passing 1 mm, followed by gravity separation. The concentrate product was then mounted and polished. The microscopic analysis was carried out using a reflected light polarizing microscope

MICROSCOPIC ANALYSIS IN POLISHED SECTION

Abr.	Mineral	Chem. Formula	%	Description
Py.	Pyrite	Fe S2	12	Mainly as free grains. Some alteration to Gt.
Gn.	Galena	Pb S	80	Mainly as free grains
Cpy.	Chalcopyrite	Cu Fe S2	3	As free grains and as inclusions in Sph.
Sph.	Sphalerite	Zn S	2	Contains inclusions of Cpy.
Gt.	Goethite	H Fe O2	<1	Alteration product of Py.
Cov.	Covellite	Cu S	<<1	Close association with Cer.
Cer.	Cerussite	Pb CO3	<1	Alteration product of Gn.
Qtz.	Quartz	Si O2	3	Mainly as free grains
Au.	Gold	Au	<<1	As free particles and small inclusions in Py.

TEXTURES AND DESCRIPTION:

This product is composed mainly of galena which is present mainly as free particles. Some grains show incipient alteration to cerussite and covellite.

Chalcopyrite occurs as free particles and also as inclusions in sphalerite.

Sphalerite contains fairly abundant inclusions of chalcopyrite.

Pyrite shows incipient alteration to goethite. A few inclusions of gold in pyrite were observed. These inclusions vary in size from 2 microns to ≈ 10 microns.

Although some of the gold is intergrown with pyrite, over 90% of the distribution of gold in the sample is as free particles in the size range 50 microns to 100 microns. No other associations of gold with other minerals were observed.

MINERALOGRAPHIC REPORT

by C. L. Soux

For: Shangri La Minerals
Project: Saddle
Sample: SDL-M
Location: Stewart, B.C.
Collector:
Date Analyzed: Sep/25/87

MACROSCOPIC DESCRIPTION:
Hand specimen ground to 100% passing 1mm, followed by gravity concentration. The middlings product was mounted and polished. The microscopic analysis of this product was carried out using a reflected light polarizing microscope

MICROSCOPIC ANALYSIS IN POLISHED SECTION

Abr.	Mineral	Chem. Formula	%	Description
Py.	Pyrite	Fe S2	30	Mainly as free grains. Some grains altered to Gt.
Gn.	Galena	Pb S	3	Replaces Cpy. and Sph.
Cpy.	Chalcopyrite	Cu Fe S2	35	As free grains and as inclusions in Sph.
Sph.	Sphalerite	Zn S	6	Contains inclusions of Cpy. Replaced by Gn.
Gt.	Goethite	H Fe O2	6	Alteration product of Py.
Cov.	Covellite	Cu S	<1	Replaces Cpy. and Gn.
Qtz.	Quartz	Si O2	20	Contains inclusions of other minerals

TEXTURES AND DESCRIPTION:
Pyrite is present mainly as free particles. Some inclusions of Gn., Cpy. and Sph. were observed. Some pyrite grains show alteration to goethite.
Sphalerite, invariably contains inclusions of chalcopyrite.
Chalcopyrite occurs as discrete particles and also as inclusions in sphalerite.
Galena replaces chalcopyrite, sphalerite and to a minor extent pyrite. It appears to be the latest hypogene mineral in the paragenetic sequence.
Covellite is an alteration product of chalcopyrite.

APPENDIX G

AIRBORNE SYSTEM SPECIFICATIONS

SPECIFICATIONS: SABRE AIRBORNE VLF-EM SYSTEM

Antenna System: 2 separate omnidirectional arrays, housed in same bird as proton magnetometer detector.

Parameters Measured: Horizontal field strength on 2 stations simultaneously (Seattle and Annapolis). Designed for use in steep terrain where dip angle information is confusing and often useless.

Type of Readout: 2 analog meters, one for each station, and 2 analog outputs at rear of console. These analog outputs, along with those of the proton magnetometer and a marker channel, were digitized by a CCC-Maron Remote Monitoring and logging system (an 8 channel, 8 bit analog to digital converter custom manufactured by Maron Engineering Ltd., Burnaby, B.C.) and stored in multiplex format on one channel of a conventional stereo cassette tape deck.

Receiver Console: 2 separate receiver channels, both housed in 30 x 10 x 25 cm case.

Operating Temperature Range:

Instrument console:	-10 C to +50 C
Antenna System:	-10 c to +50 C

Power Source:

Receiver Console:	8 alkaline penlite cells with life of 100 hours.
Instrument console:	2 9V transistor batteries

Manufacturer: Sabre Electronic Instruments Ltd., Burnaby, B.C.

SPECIFICATIONS: SABRE AIRBORNE MAGNETOMETER

Type: Proton Precession

Range: 20,000 to 75,000 gammas

Repetition Rate: Approximately 1.6 seconds

Output: Analog meter on instrument console, 0-100 mV analog output on rear of console. Full scale deflection can be either 1000, 2500, or 5000 gammas, this being measured from a zero value selected by instrument operator depending on background field in survey area. Zero value for this survey was 57,000 gammas, with 1000 gammas full scale deflection. The analog output on the rear of the console was digitized with the CCC-Maron Remote Monitoring and Logging System and stored on one channel of a conventional stereo cassette tape deck along with the VLF-EM data and the navigational·marker channel.

Resolution: Resolution of instrument itself is better than 1 gamma, but recorded resolution is limited to about 4 gammas (1000 gamma full scale deflection is resolved to one part in 255 with the 8 bit CCC-Maron analog to digital converter).

Detector: Kerosene-filled coil, 9 cm long x 8 cm diameter. Inductance 60 millihenries, resistance 7.5 ohms, weight 2.2 kilograms.

Operating Temperature:

Instrument: -10 C to + 60 C
Detector: -40 C to + 60 C

Dimensions:

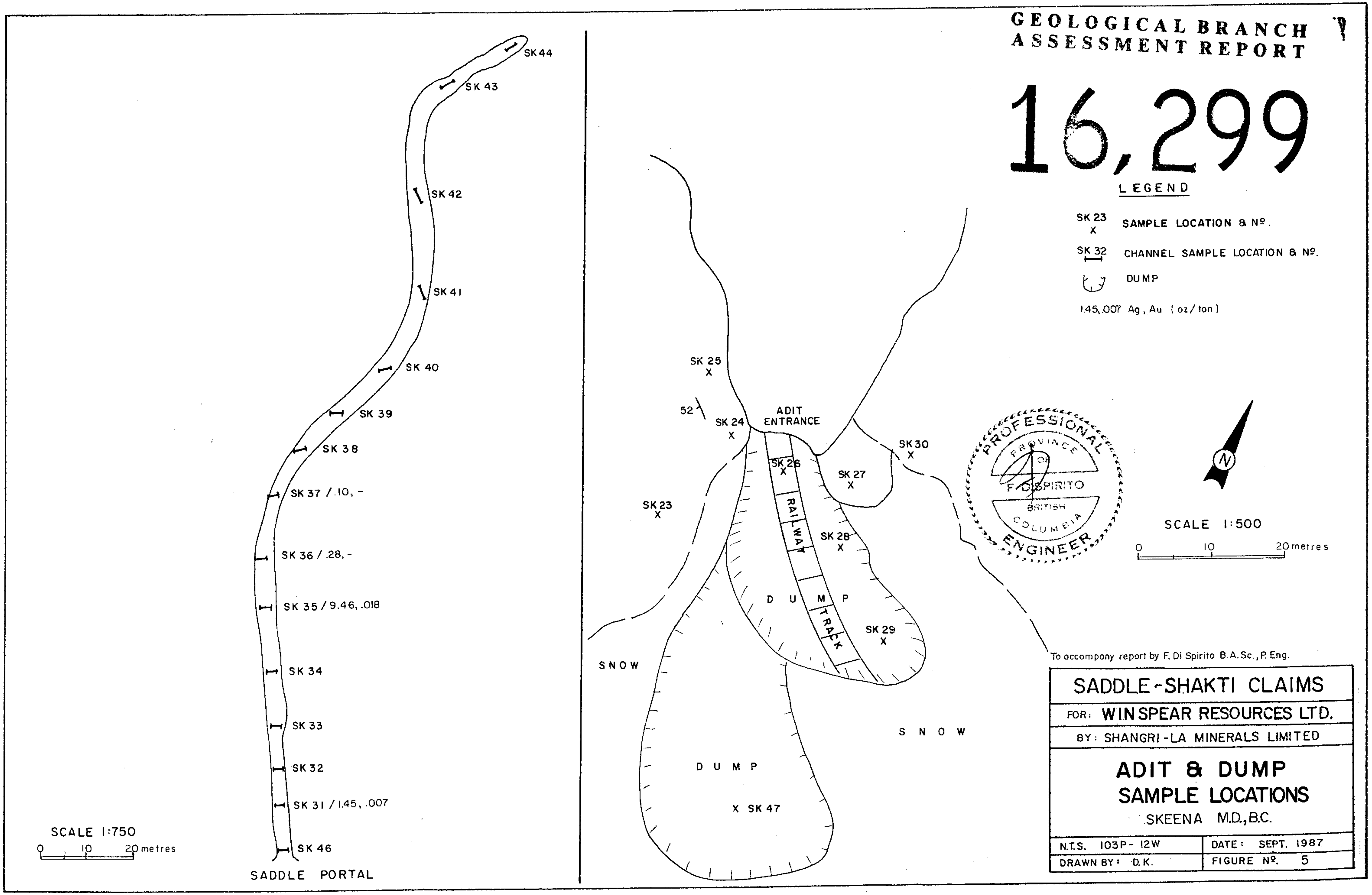
Instrument console: 30 x 10 x 25 cm, weight 3.5 kg.
Towed bird: 1.7 m x 21 cm diameter, weight 30 kg.
(VLF-EM antenna system is housed in bird along with mag detector).

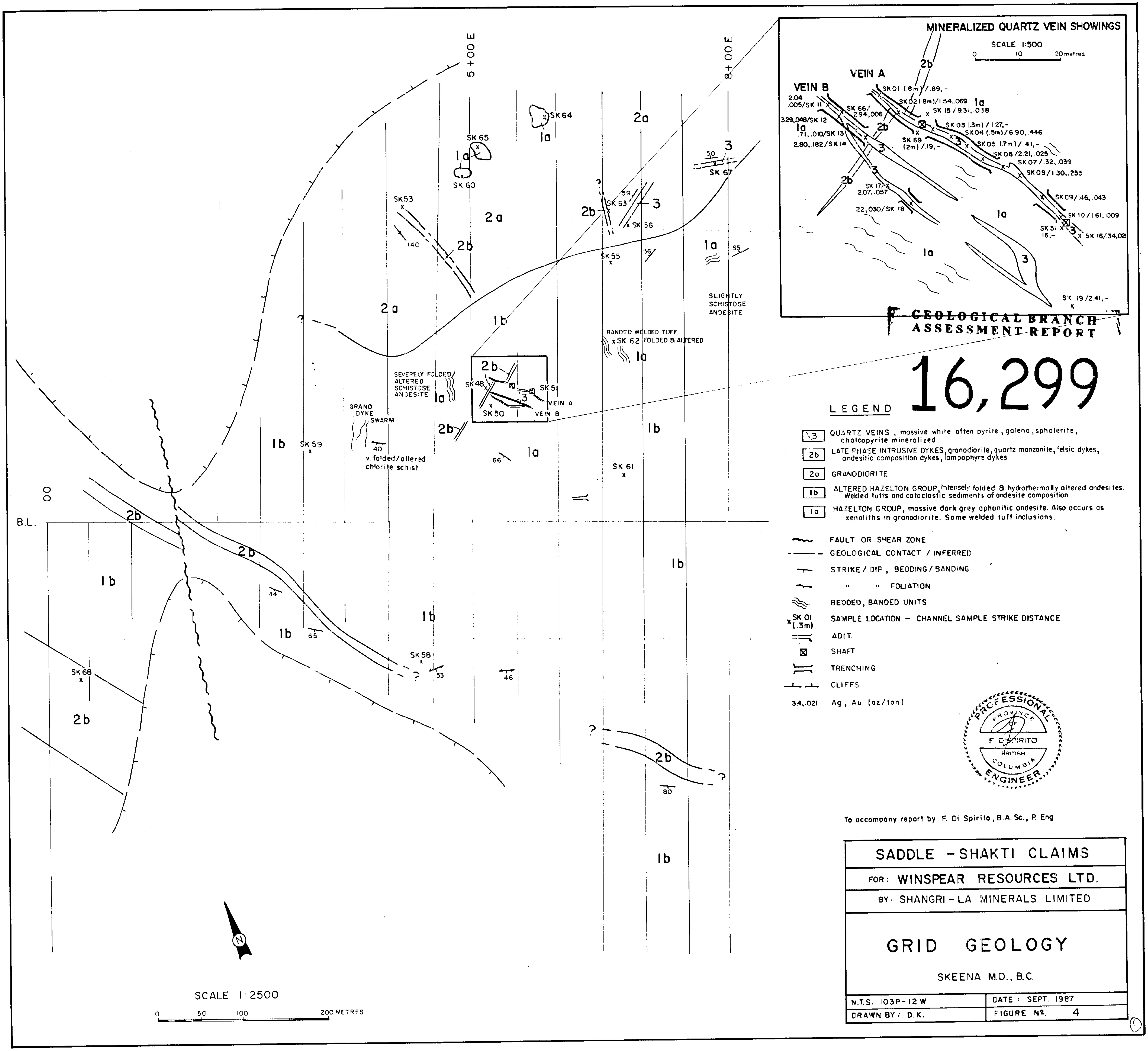
Power Source:

2 12V 20 AH lead-acid batteries.

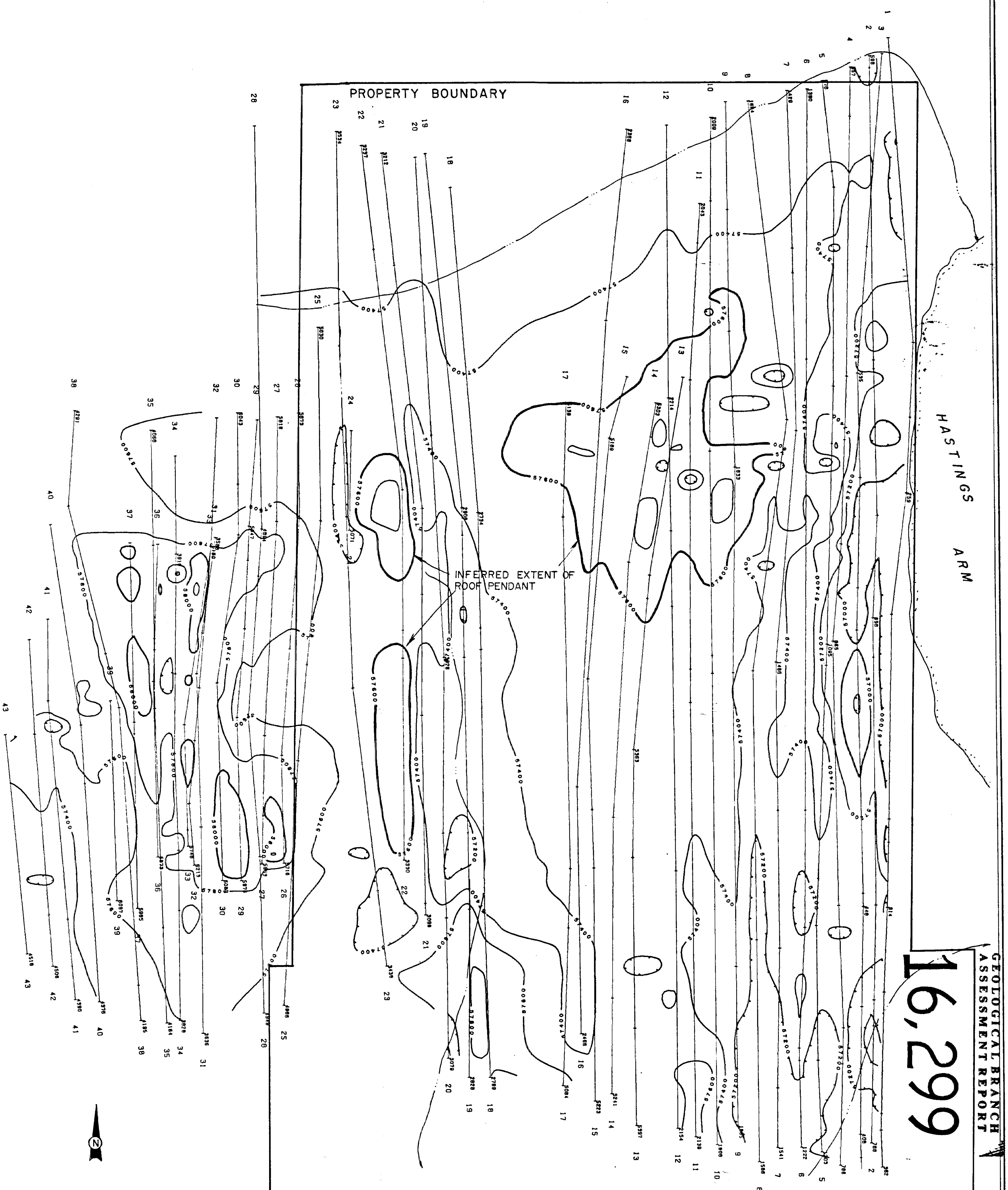
Manufacturer:

Sabre Electronics Ltd., Burnaby, B.C.


GEOLOGICAL BRANCH ASSESSMENT REPORT
16,299
LEGEND
SK 23 X SAMPLE LOCATION & Nº.
SK 32 CHANNEL SAMPLE LOCATION & Nº.
DUMP
1.45, .007 Ag, Au (oz/ton)
SK 44
SK 43
SK 42
SK 41
SK 40
SK 39
SK 38
SK 37 / .10, -
SK 36 / .28, -
SK 35 / 9.46, .018
SK 34
SK 33
SK 32
SK 31 / 1.45, .007
SK 46
SADDLE PORTAL
SCALE 1:750
0 10 20 metres
SK 25 X
52
SK 24 X
ADIT ENTRANCE
SK 26 X
SK 27 X
SK 30 X
SK 23 X
RAILWAY
SK 28 X
D U M P
TRACK
SK 29 X
SNOW
S N O W
D U M P
X SK 47
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
F. DI SPIRITO
N
SCALE 1:500
0 10 20 metres
To accompany report by F. Di Spirito B.A.Sc., P. Eng.
SADDLE-SHAKTI CLAIMS
FOR: WINSPEAR RESOURCES LTD.
BY: SHANGRI-LA MINERALS LIMITED
ADIT & DUMP
SAMPLE LOCATIONS
SKEENA M.D., B.C.
N.T.S. 103P-12W
DATE: SEPT. 1987
DRAWN BY: D.K.
FIGURE Nº. 5
CHONG



MINERALIZED QUARTZ VEIN SHOWINGS
SCALE 1:500
0 10 20 metres
VEIN A
VEIN B
SK 01 (.8m) / .89, -
SK 02 (.8m) / 1.54, .069
SK 15 / 9.31, .038
SK 03 (.3m) / 1.27, -
SK 04 (.5m) / 6.90, .446
SK 05 (.7m) / .41, -
SK 06 / 2.21, .025
SK 07 / .32, .039
SK 08 / 1.30, .255
SK 09 / 46, .043
SK 10 / 1.61, .009
SK 16 / 34, .02
SK 19 / 2.41, -
SK 66 / 2.94, .006
SK 69 (2m) / .19, -
SK 17 / 2.07, .057
.22, .030 / SK 18
2.04 .005 / SK 11
329, .048 / SK 12
.71, .010 / SK 13
2.80, .182 / SK 14
SK 51 .16, -
GEOLOGICAL BRANCH
ASSESSMENT REPORT
16,299
5+00 E
8+00 E
B.L.
00
SK 64
SK 65
SK 60
SK 53
SK 63
SK 56
SK 67
SK 55
SK 62
SK 48
SK 51
SK 50
SK 59
SK 61
SK 58
SK 68
VEIN A
VEIN B
SLIGHTLY SCHISTOSE ANDESITE
BANDED WELDED TUFF
FOLDED & ALTERED
SEVERELY FOLDED/ ALTERED SCHISTOSE ANDESITE
GRANO DYKE SWARM
v. folded/altered chlorite schist
LEGEND
QUARTZ VEINS, massive white often pyrite, galena, sphalerite, chalcopyrite mineralized
LATE PHASE INTRUSIVE DYKES, granodiorite, quartz monzonite, felsic dykes, andesitic composition dykes, lampophyre dykes
GRANODIORITE
ALTERED HAZELTON GROUP, intensely folded & hydrothermally altered andesites. Welded tuffs and cataclastic sediments of andesite composition
HAZELTON GROUP, massive dark grey aphanitic andesite. Also occurs as xenoliths in granodiorite. Some welded tuff inclusions.
FAULT OR SHEAR ZONE
GEOLOGICAL CONTACT / INFERRED
STRIKE / DIP, BEDDING / BANDING
" " FOLIATION
BEDDED, BANDED UNITS
SAMPLE LOCATION – CHANNEL SAMPLE STRIKE DISTANCE
ADIT
SHAFT
TRENCHING
CLIFFS
3.4, .021 Ag, Au (oz/ton)
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
F. DI SPIRITO
To accompany report by F. Di Spirito, B.A. Sc., P. Eng.
SADDLE – SHAKTI CLAIMS
FOR: WINSPEAR RESOURCES LTD.
BY: SHANGRI-LA MINERALS LIMITED
GRID GEOLOGY
SKEENA M.D., B.C.
N.T.S. 103P-12W
DATE: SEPT. 1987
DRAWN BY: D.K.
FIGURE No. 4
SCALE 1:2500
0 50 100 200 METRES



TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

SADDLE - SHAKTI CLAIMS

FOR: WINSPEAR RESOURCES LTD.

BY: SHANGRI-LA MINERALS LTD.

PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.

AIRBORNE SURVEY
MAGNETIC FIELD STRENGTH

SKEENA M.D., B.C.

N.T.S.: 103P / 12W — DATE: SEPTEMBER 1987

PLOTTED BY: R.P.M. — FIGURE NO. 6 a

SCALE 1:10000

200 0 200 400 600

METERS

BASE VALUE: 0 GAMMAS
CONTOUR INTERVAL: 200 GAMMAS

②

TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

SADDLE - SHAKTI CLAIMS	
FOR: WINSPEAR RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LTD.	
PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.	
AIRBORNE SURVEY VLF-EM (SEATTLE)	
SKEENA M.D., B.C.	
N.T.S.: 103P / 12W	DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.	FIGURE NO. 6 b

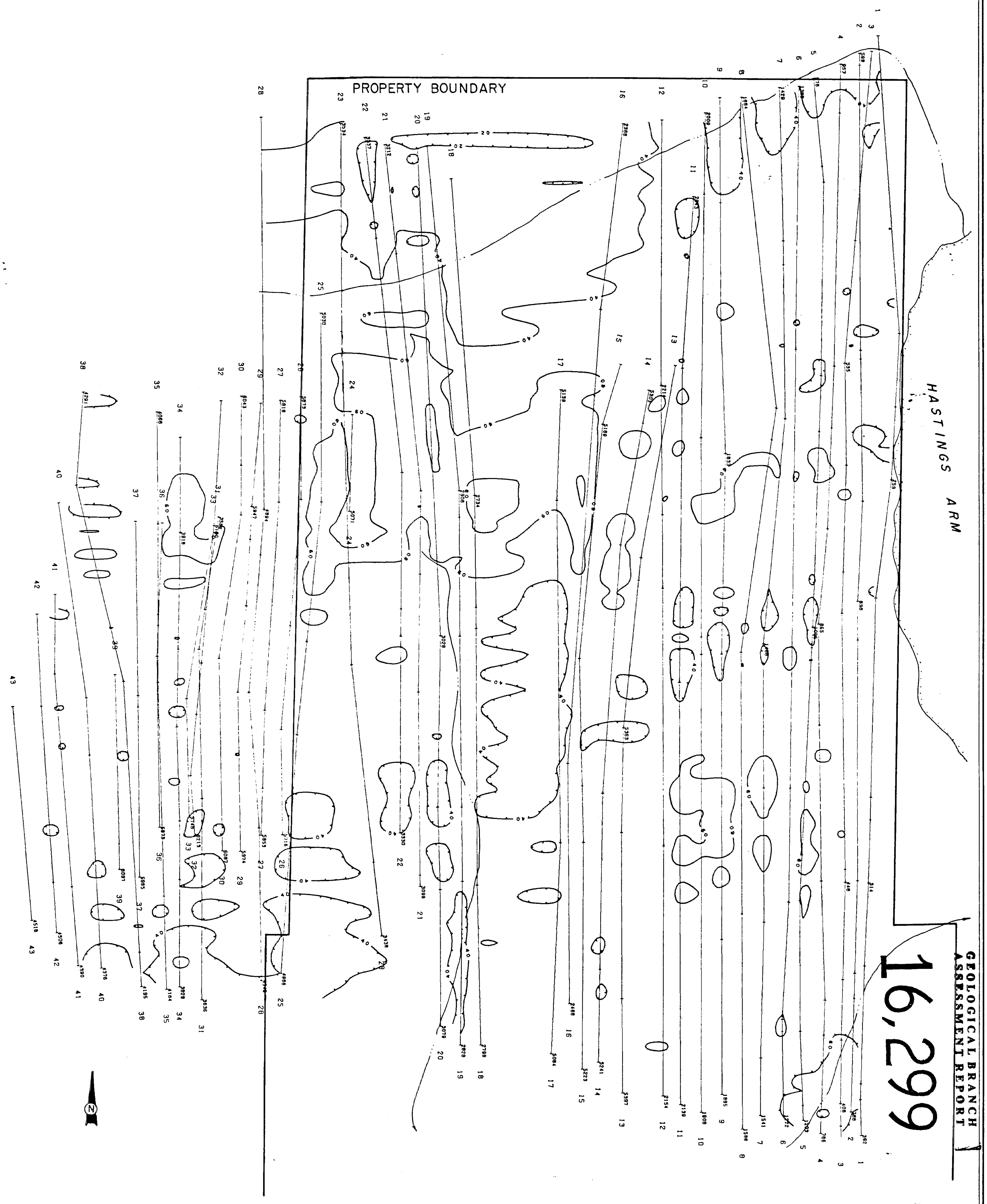
SCALE 1:10000

200 0 200 400 600

METERS

CONTOUR INTERVAL: 10 PERCENT

(3)



TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

SADDLE - SHAKTI CLAIMS	
FOR: WINSPEAR RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LTD.	
PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.	
AIRBORNE SURVEY VLF-EM (ANNAPOLIS)	
SKEENA M.D., B.C.	
N.T.S.: 103P / 12W	DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.	FIGURE NO. 6c

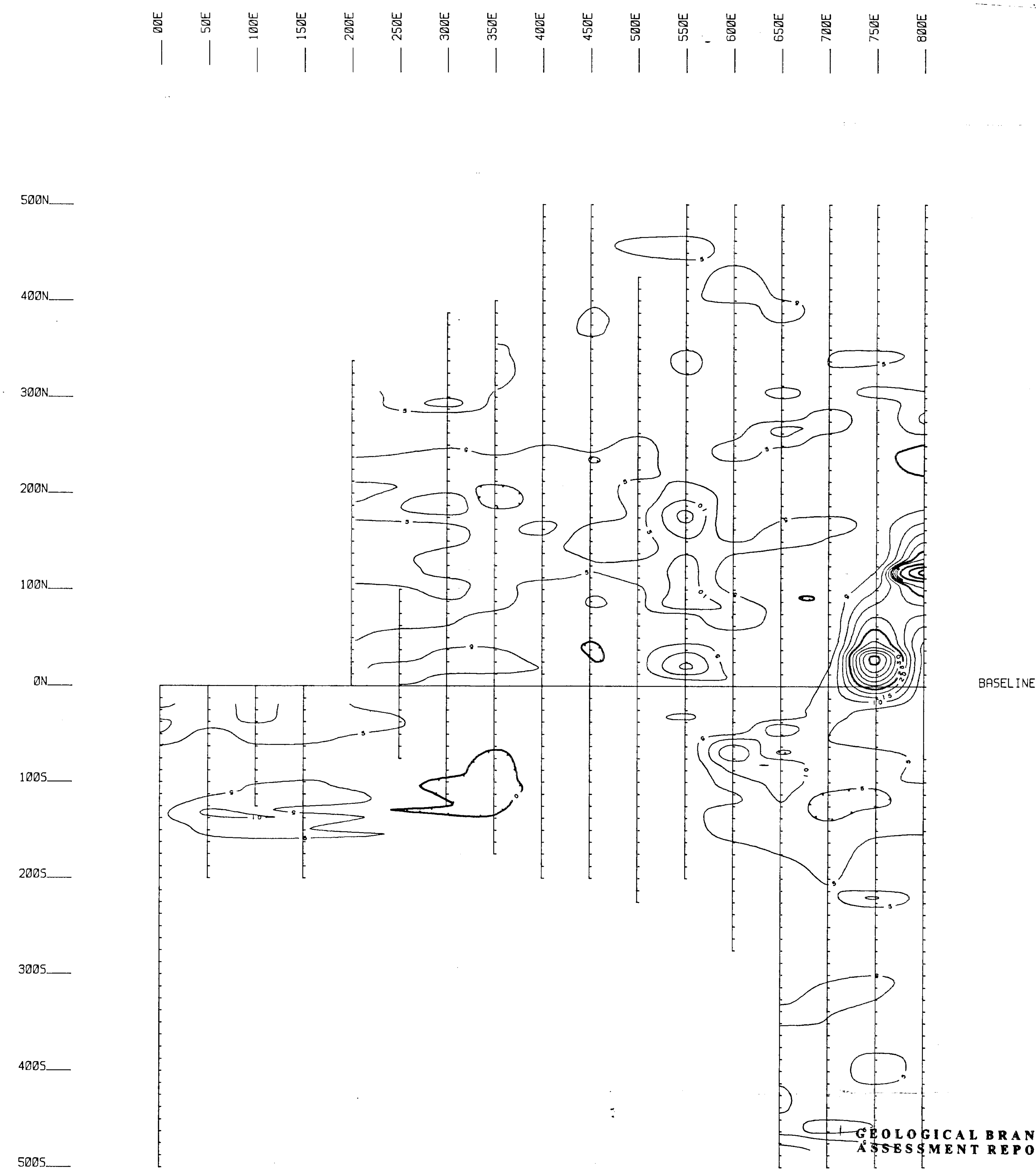
SCALE 1:10000

200 0 200 400 600

METERS

CONTOUR INTERVAL: 20 PERCENT

4



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,299

TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

PROFESSIONAL ENGINEER — PROVINCE OF BRITISH COLUMBIA — F. DI SPIRITO

SCALE 1:2500

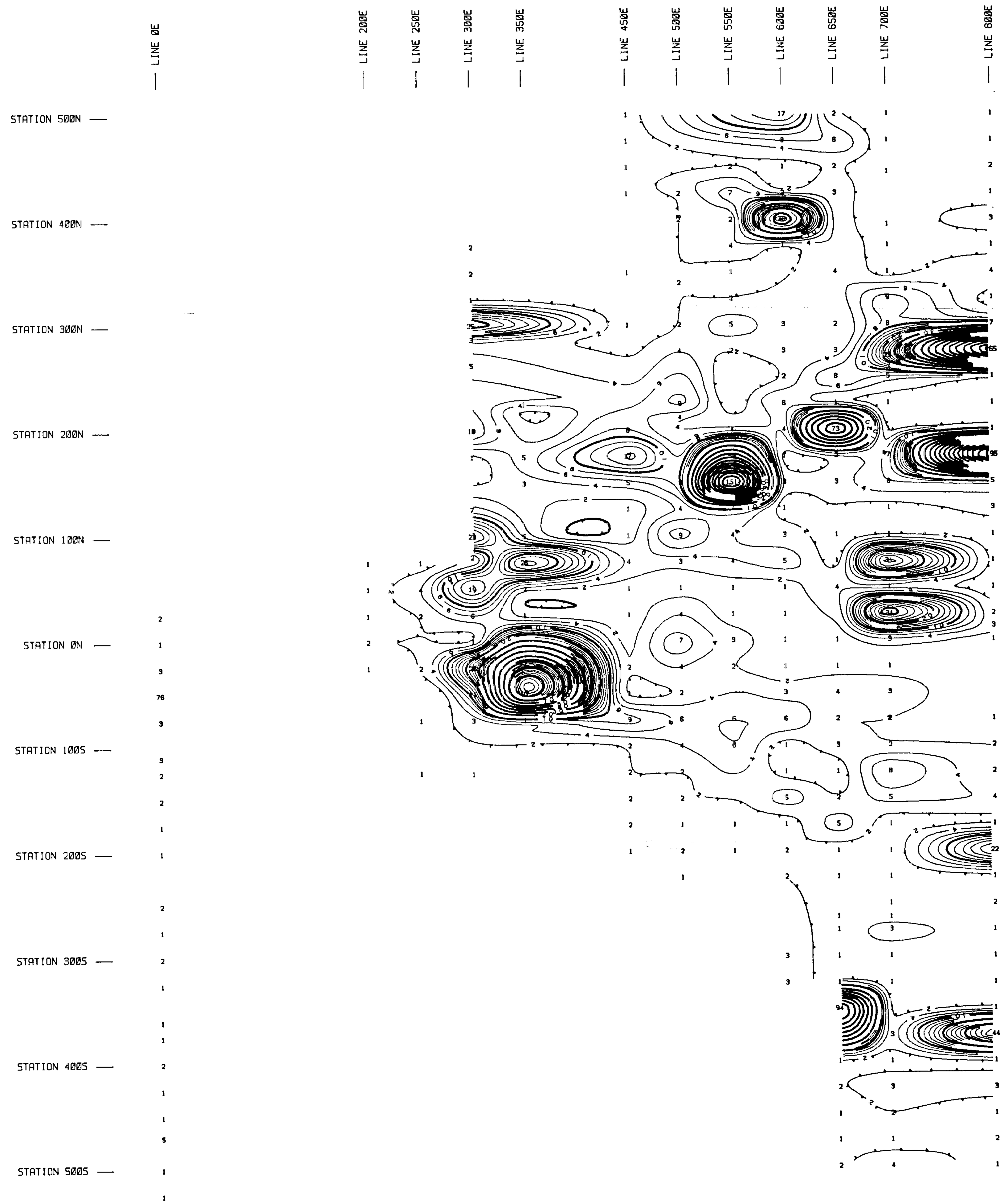
50 0 50 100 150

METERS

CONTOUR INTERVAL: 5 PERCENT

SADDLE - SHAKTI CLAIMS	
FOR: WINSPEAR RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LTD.	
PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.	
VLF-EM (SEATTLE) FRASER FILTERED CONTOUR MAP	
SKEENA M.D., B.C.	
N.T.S.: 103P / 12W	DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.	FIGURE NO. 7

(5)



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,299

CONTOUR INTERVAL: 2 PPB

N

SCALE 1:2500

50 0 50 100 150

METERS

TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

PROFESSIONAL ENGINEER, PROVINCE OF BRITISH COLUMBIA, F. DI SPIRITO

SADDLE - SHAKTI CLAIMS

FOR: WINSPEAR RESOURCES LTD.

BY: SHANGRI-LA MINERALS LTD.

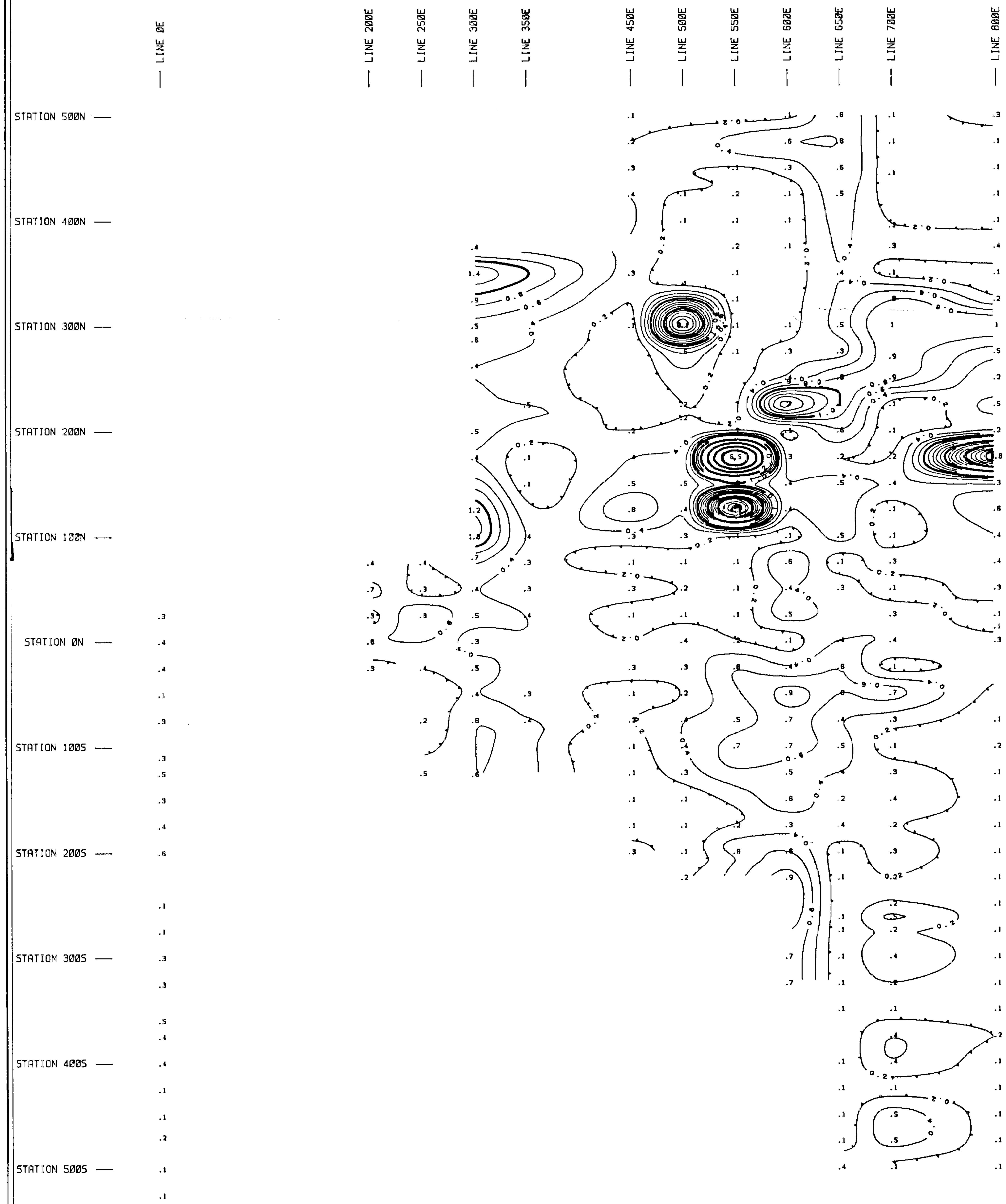
PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.

AU GEOCHEMISTRY

SKEENA M.D., B.C.

N.T.S.: 103P / 12W	DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8a

6



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,299

CONTOUR INTERVAL: 0.2 PPM

N

SCALE 1:2500

50 0 50 100 150

METERS

TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
F. DI SPIRITO

SADDLE - SHAKTI CLAIMS

FOR: WINSPEAR RESOURCES LTD.

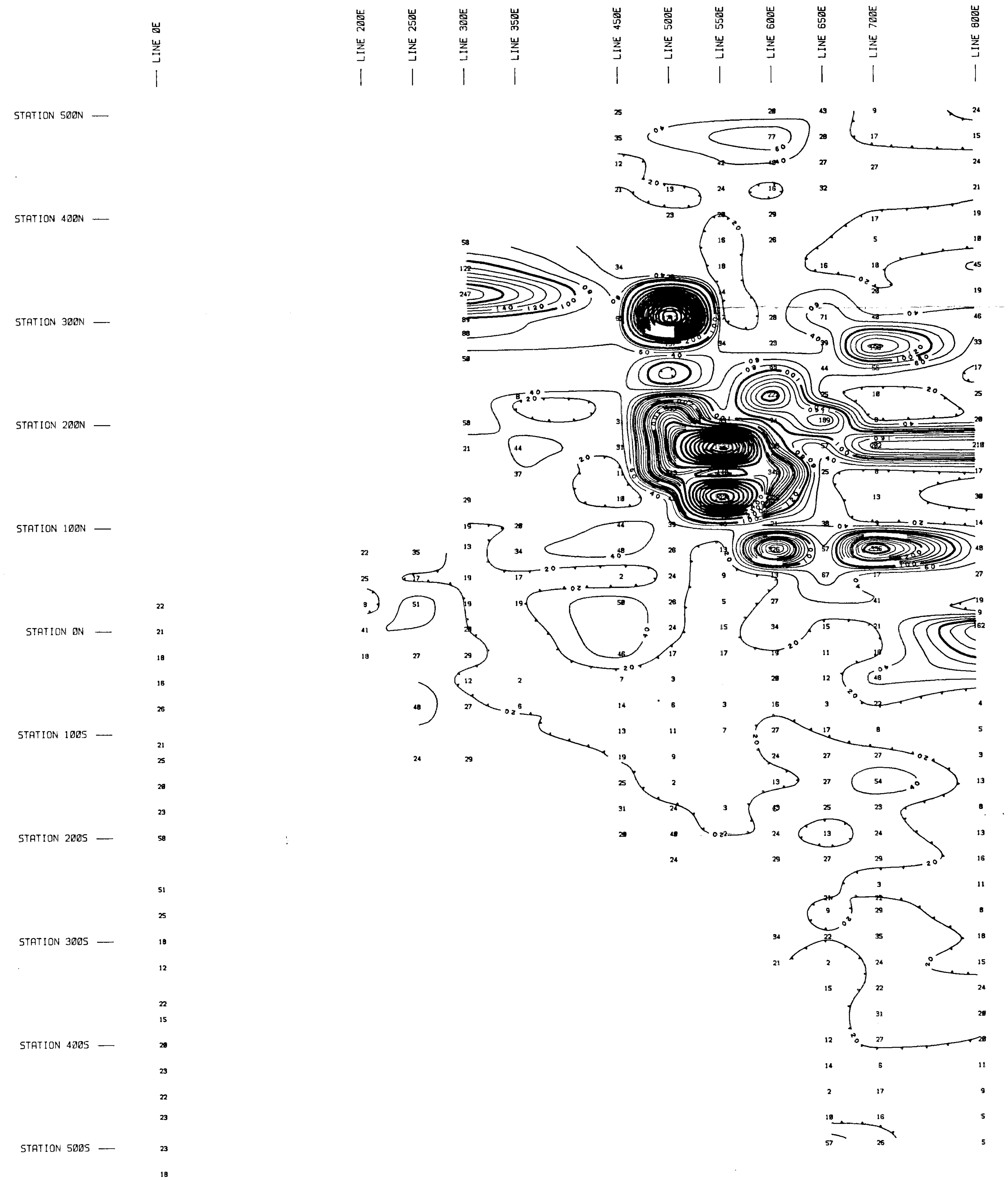
BY: SHANGRI-LA MINERALS LTD.

PLOTTED BY: RPM MAPPING
AND COMPUTER SERVICES LTD.

AG GEOCHEMISTRY

SKEENA M.D., B.C.

N.T.S.: 103P / 12W	DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8 b



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,299

CONTOUR INTERVAL: 20 PPM

SCALE 1:2500

50 0 50 100 150

METERS

TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

SADDLE - SHAKTI CLAIMS

FOR: WINSPEAR RESOURCES LTD.

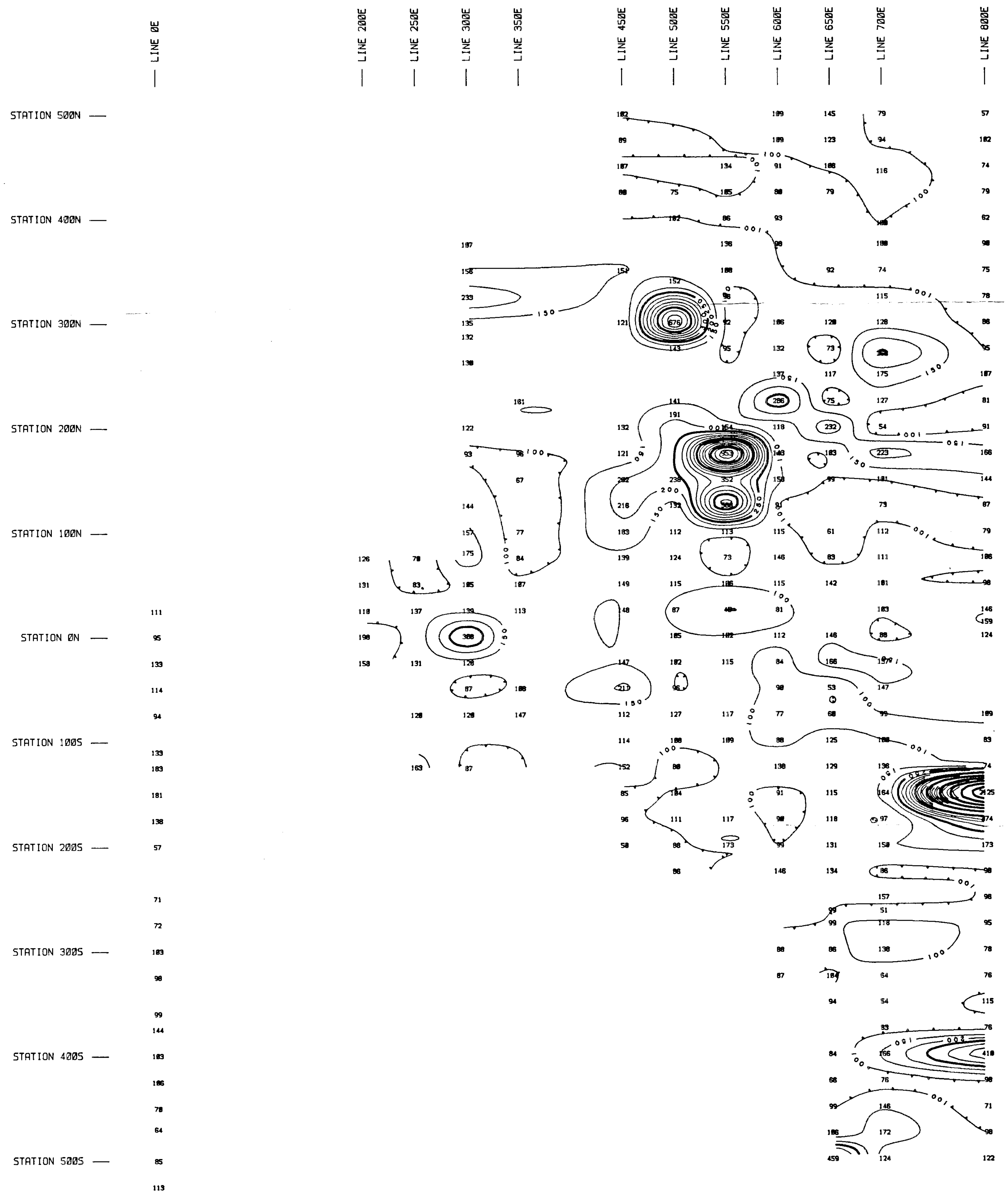
BY: SHANGRI-LA MINERALS LTD.

PLOTTED BY: RPM MAPPING
AND COMPUTER SERVICES LTD.

PB GEOCHEMISTRY

SKEENA M.D., B.C.

N.T.S.: 103P / 12W	DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8 c



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,299

CONTOUR INTERVAL: 50 PPM

SCALE 1:2500

50 0 50 100 150

METERS

TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
F. DISPIRITO

SADDLE - SHAKTI CLAIMS

FOR: WINSPEAR RESOURCES LTD.

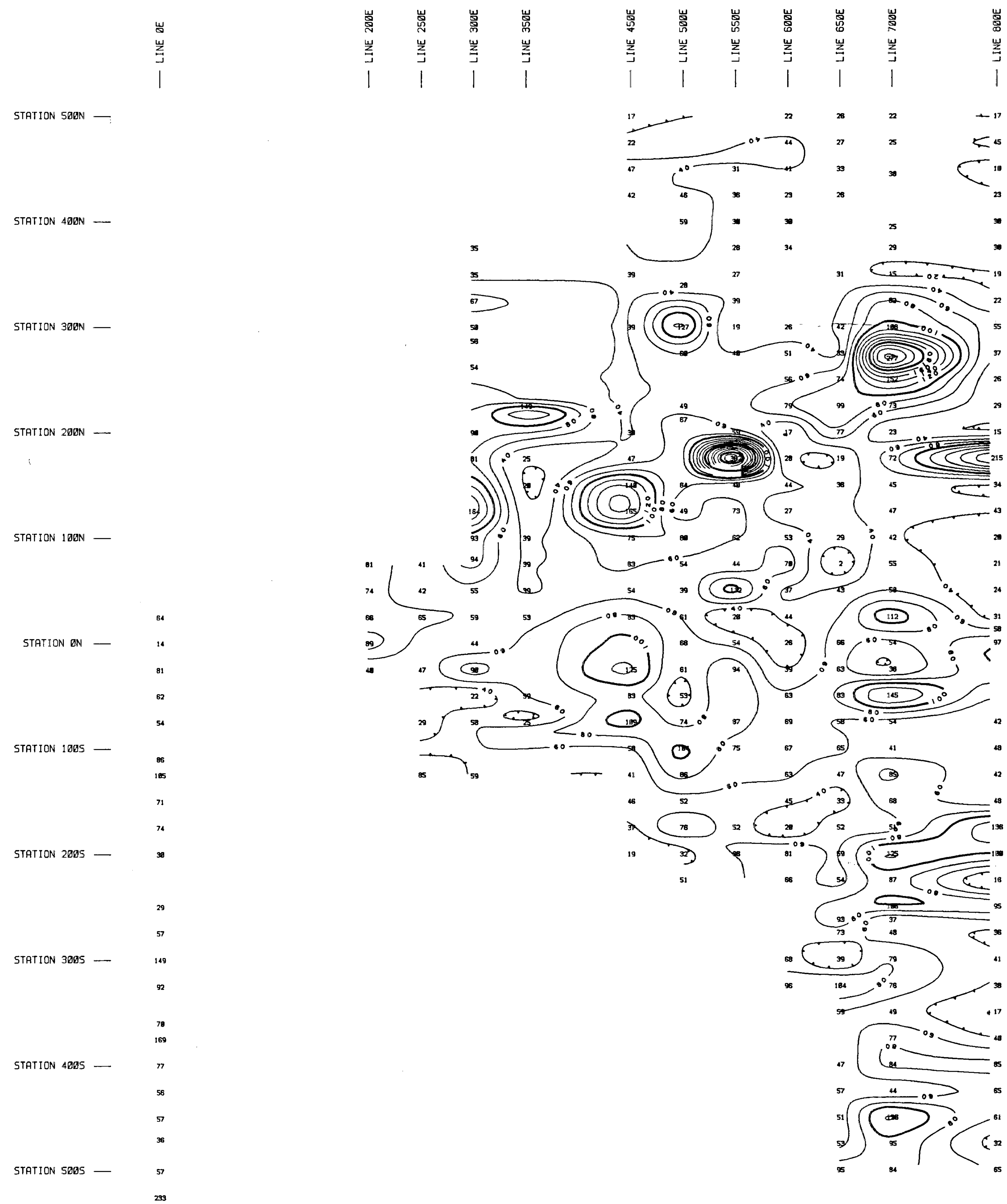
BY: SHANGRI-LA MINERALS LTD.

PLOTTED BY: RPM MAPPING
AND COMPUTER SERVICES LTD.

ZN GEOCHEMISTRY

SKEENA M.D., B.C.

N.T.S.: 103P / 12W	DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8 d



CONTOUR INTERVAL: 20 PPM

N

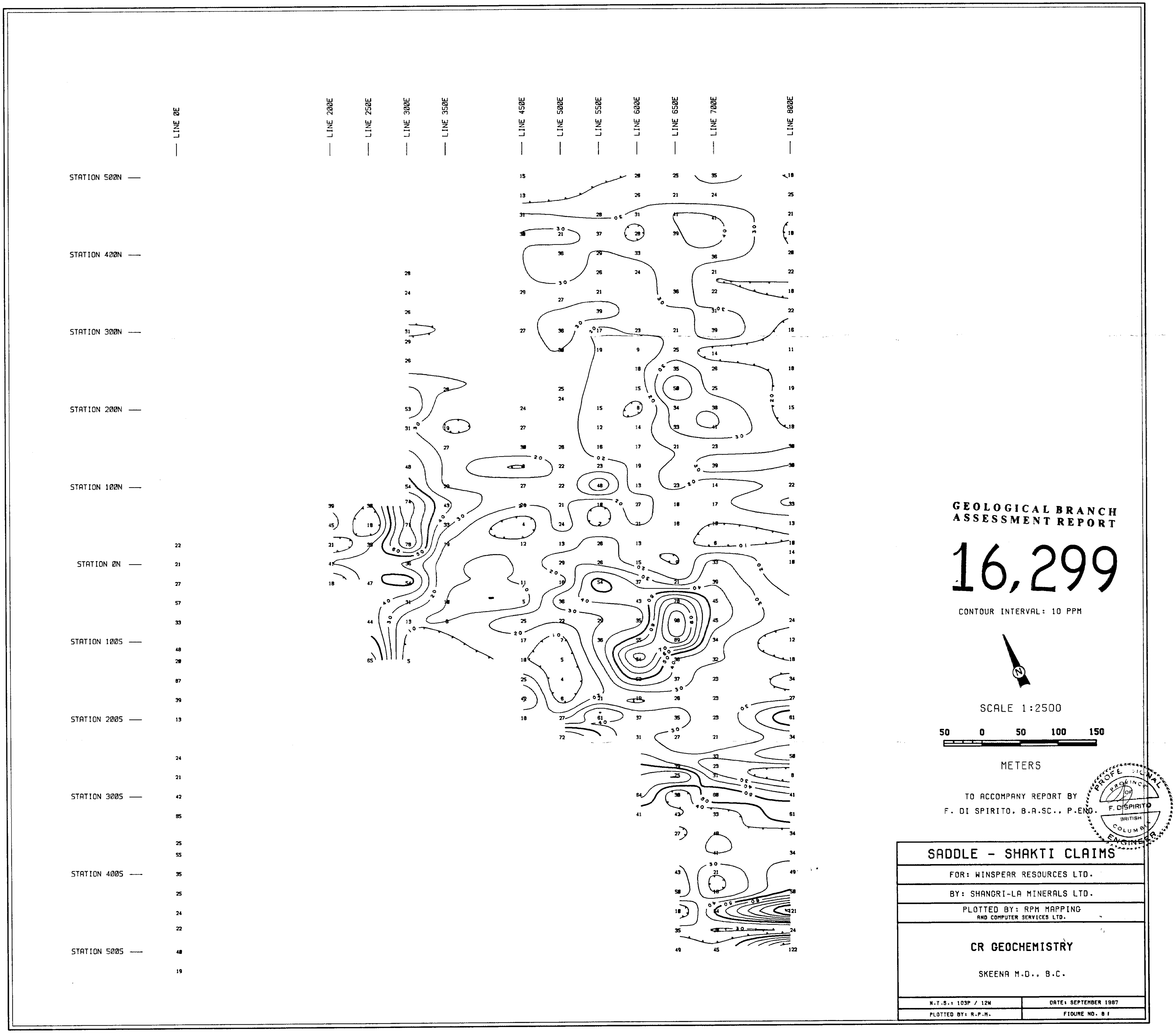
SCALE 1:2500

50 0 50 100 150

METERS

TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.

SADDLE - SHAKTI CLAIMS	
FOR: WINSPEAR RESOURCES LTD.	
BY: SHANGRI-LA MINERALS LTD.	
PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.	
CU GEOCHEMISTRY SKEENA M.D., B.C.	
N.T.S.: 103P / 12W	DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.	FIGURE NO. 8 c


LINE 0E
LINE 200E
LINE 250E
LINE 300E
LINE 350E
LINE 450E
LINE 500E
LINE 550E
LINE 600E
LINE 650E
LINE 700E
LINE 800E
STATION 500N
STATION 400N
STATION 300N
STATION 200N
STATION 100N
STATION 0N
STATION 100S
STATION 200S
STATION 300S
STATION 400S
STATION 500S
GEOLOGICAL BRANCH
ASSESSMENT REPORT
16,299
CONTOUR INTERVAL: 10 PPM
N
SCALE 1:2500
50 0 50 100 150
METERS
TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.
F. DI SPIRITO
SADDLE - SHAKTI CLAIMS
FOR: WINSPEAR RESOURCES LTD.
BY: SHANGRI-LA MINERALS LTD.
PLOTTED BY: RPM MAPPING
AND COMPUTER SERVICES LTD.
CR GEOCHEMISTRY
SKEENA M.D., B.C.
N.T.S.: 103P / 12W
DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.
FIGURE NO. 8 I

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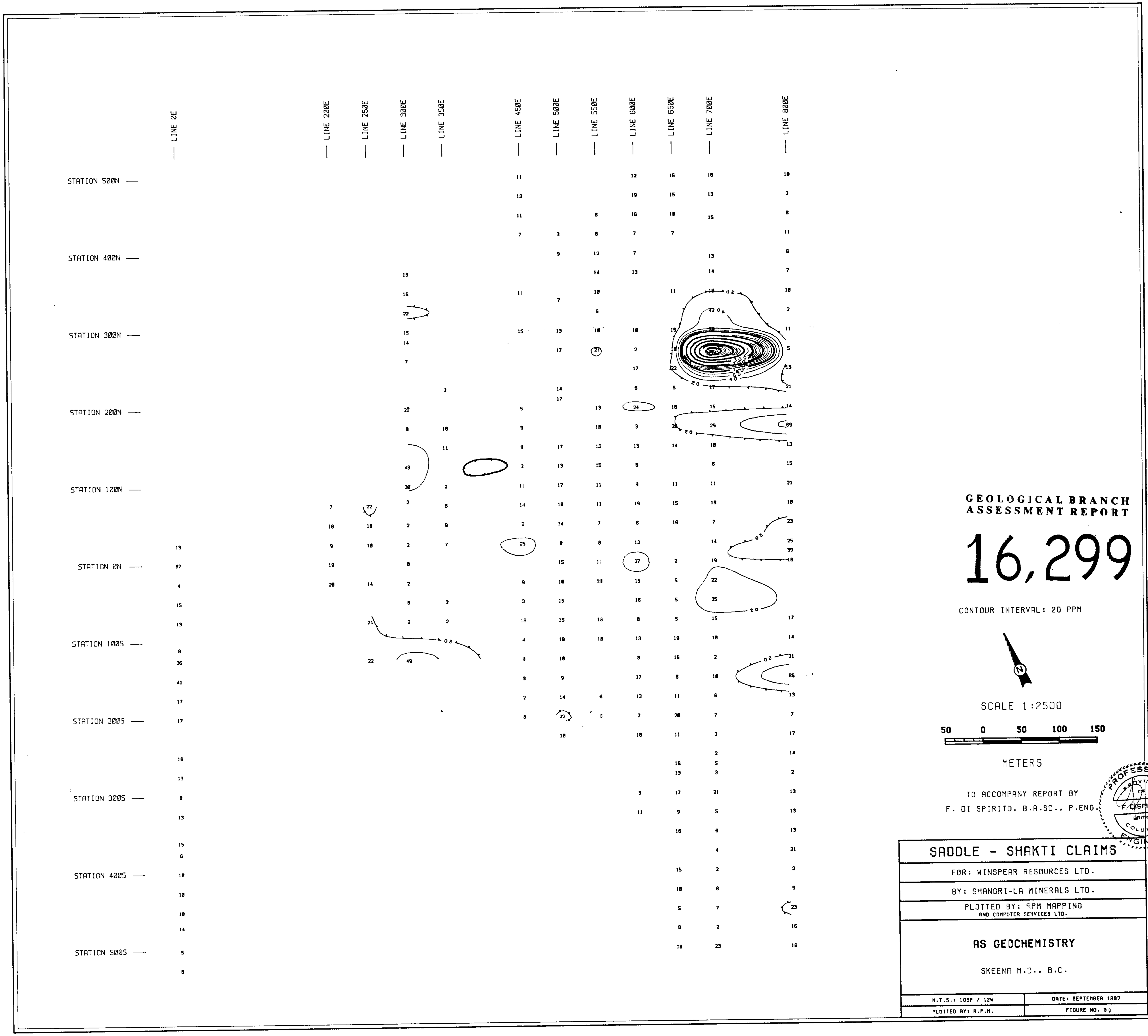
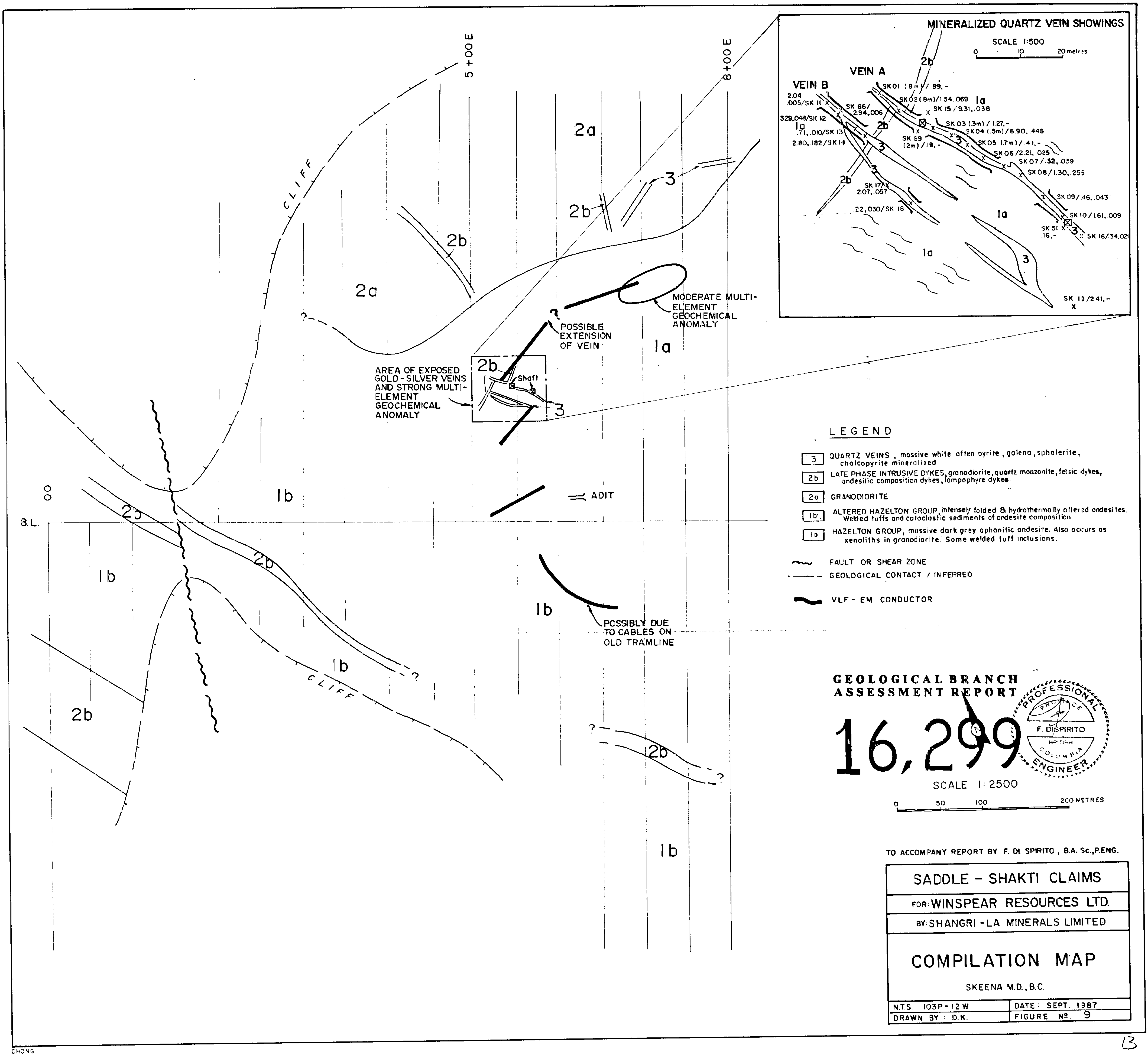


LINE 0E
LINE 200E
LINE 250E
LINE 300E
LINE 350E
LINE 450E
LINE 500E
LINE 550E
LINE 600E
LINE 650E
LINE 700E
LINE 800E
STATION 500N
STATION 400N
STATION 300N
STATION 200N
STATION 100N
STATION 0N
STATION 100S
STATION 200S
STATION 300S
STATION 400S
STATION 500S
GEOLOGICAL BRANCH
ASSESSMENT REPORT
16,299
CONTOUR INTERVAL: 20 PPM
N
SCALE 1:2500
50 0 50 100 150
METERS
TO ACCOMPANY REPORT BY
F. DI SPIRITO, B.A.SC., P.ENG.
SADDLE - SHAKTI CLAIMS
FOR: WINSPEAR RESOURCES LTD.
BY: SHANGRI-LA MINERALS LTD.
PLOTTED BY: RPM MAPPING AND COMPUTER SERVICES LTD.
AS GEOCHEMISTRY
SKEENA M.D., B.C.
N.T.S.: 103P / 12W
DATE: SEPTEMBER 1987
PLOTTED BY: R.P.M.
FIGURE NO. 8g



MINERALIZED QUARTZ VEIN SHOWINGS
SCALE 1:500
0 10 20 metres
VEIN A
VEIN B
SK 01 (.8m)/.89, -
SK 02 (.8m)/1.54,.069
SK 15 / 9.31, .038
2.04 .005/SK 11
SK 66/ 2.94,.006
329,.048/SK 12
.71, .010/SK 13
2.80, .182/SK 14
SK 03 (.3m) / 1.27, -
SK 04 (.5m)/6.90, .446
SK 69 (2m) /.19, -
SK 05 (.7m) / .41, -
SK 06 /2.21, .025
SK 07 / .32, .039
SK 08 / 1.30, .255
SK 17/ 2.07, .057
.22, .030/SK 18
SK 09 / .46, .043
SK 10 / 1.61, .009
SK 51 .16, -
SK 16/34,.021
SK 19 /2.41, -
5+00 E
8+00 E
CLIFF
POSSIBLE EXTENSION OF VEIN
MODERATE MULTI-ELEMENT GEOCHEMICAL ANOMALY
AREA OF EXPOSED GOLD-SILVER VEINS AND STRONG MULTI-ELEMENT GEOCHEMICAL ANOMALY
Shaft
ADIT
B.L.
00
POSSIBLY DUE TO CABLES ON OLD TRAMLINE
LEGEND
3 QUARTZ VEINS, massive white often pyrite, galena, sphalerite, chalcopyrite mineralized
2b LATE PHASE INTRUSIVE DYKES, granodiorite, quartz monzonite, felsic dykes, andesitic composition dykes, lamprophyre dykes
2a GRANODIORITE
1b ALTERED HAZELTON GROUP, intensely folded & hydrothermally altered andesites. Welded tuffs and cataclastic sediments of andesite composition
1a HAZELTON GROUP, massive dark grey aphanitic andesite. Also occurs as xenoliths in granodiorite. Some welded tuff inclusions.
FAULT OR SHEAR ZONE
GEOLOGICAL CONTACT / INFERRED
VLF - EM CONDUCTOR
GEOLOGICAL BRANCH
ASSESSMENT REPORT
16,299
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
F. DISPIRITO
SCALE 1: 2500
0 50 100 200 METRES
TO ACCOMPANY REPORT BY F. DI SPIRITO, B.A. Sc., P.ENG.
SADDLE - SHAKTI CLAIMS
FOR: WINSPEAR RESOURCES LTD.
BY: SHANGRI-LA MINERALS LIMITED
COMPILATION MAP
SKEENA M.D., B.C.
N.T.S. 103P-12W
DATE: SEPT. 1987
DRAWN BY: D.K.
FIGURE No. 9

CHONG

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