BEATY GEOLOGICAL LTD.
Consulting Geological Services

900-625 Howe Street
Vancouver, B.C., Canada V6C 2T6
Telephone (604) 684-5887

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ACTION:

FILE NO: 87-770-16367

REPORT ON A GEOCHEMICAL SURVEY OF THE TOMMY CREEK PROPERTY CONSISTING OF THE RAYMOND CLAIM, THE RAY #1 CLAIM AND THE RAY #2 CLAIM

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,367

Lillooet Mining Division

Longitude 122° 31'W

Latitude 55° ~~55'N~~ 49'30"

NTS Map 92J/15E

FILMED

SUB-RECORDER
RECEIVED
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M.R. # ..... $ .....
VANCOUVER, B.C.

OWNERS: Crack Resources Ltd.

OPERATORS: Vortex Resources Ltd.

CONSULTANTS: Beaty Geological Ltd.

AUTHORS: John L. Knox, B.Sc.
Douglas G. Leighton, B.Sc., F.G.A.C.

SUBMITTED: 11 November 1987

TABLE OF CONTENTS

LIST OF APPENDICES

LIST OF FIGURES

1. SUMMARY

The Tommy Creek property consists of three reverted crown granted claims (Raymond) and two overlapping 16 unit metric claims (Ray 1-2). These claims are located on the periphery of the Goldbridge-Bralorne gold mining camp.

The Tommy Creek property is held jointly by Equinox Resources Ltd. and Vortex Resources Ltd. under option from Crack Resources Ltd., all Vancouver based companies. A work program was carried out to assess the claims during May and June of 1987 by Beaty Geological Ltd. on behalf of Vortex and Equinox.

The area is underlain by rocks assigned to the Bridge River Group - an assemblage of greenstones, cherty argillites, limestone and dioritic intrusives. Regionally the sequence forms a broad anti-formal structure on an axis that passes through Shalath and Tyaughton Lakes. Age of the Bridge River group is uncertain but tentatively Middle Triassic.

The area of the Ray and Raymond claims is rugged and forest cover is dense with thick undergrowth. This, combined with poor access appears to have discouraged the intense prospecting which took place in other parts of the Bralorne Camp.

Survey results over the area tested are not encouraging. However, the upper and the most westerly section of the Raymond claim was not investigated due to adverse snow conditions at higher elevations, so there is still the possibility of locating exploration targets on the Tommy Creek property.

The present geochemical results do not indicate the presence of a significant mineralized structure extending towards the north from the Bristol Mines zone. However, further geochemical sampling should be carried out on the western slope of Tommy Creek on the Raymond claim to test the presence of a northerly extension of Benboe mineralization.

2. INTRODUCTION

During May and June a program of geochemical sampling and prospecting was carried out on the Tommy Creek prospect on the Ray and Raymond claims located south of Carpenter Lake, B.C. Work was carried out by Beaty Geological Ltd.

The property is immediately north of the adjoining Bristol and Benboe properties which were developed to a moderate extent between 1937 and 1947 but did not see production. Recent exploration success by Menika Mining Ltd. on its property to the west combined with untested geological potential prompted the present program on the Ray and Raymond claims.

This report summarizes the results of the 1987 work program.

3. PROPERTY

3.1 Location and Access (see Figure 1)

The property straddles Tommy Creek which flows into the south side of Carpenter Lake about 22 km east of Goldbridge, B.C. A good gravel highway connects Goldbridge to Lillooet, along the north side of Carpenter Lake. Access to the claims is accomplished via this highway to a point across the lake from the mouth of Tommy Creek, and then a lake crossing by boat or canoe.

There is an old road along the west side of Tommy Creek that leads to the Bristol Mine workings; this road ends near the south end of the Raymond claim.

Topographic relief varies from 650 m to about 2150 m. The claims should be relatively snow-free from mid-May to October and during this period the weather is normally fairly warm and dry.

3.2 Claims (see Figure 2)

The Tommy Creek property, owned by Crack Resources Ltd. of Vancouver B.C., consists of two sixteen unit claims and one claim made up from three reverted Crown Grants. The property is currently under option to Equinox Resources Ltd. and forms part of the Vortex-Equinox joint venture.

VORTEX-EQUINOX JOINT VENTURE	
TOMMY CREEK PROPERTY LOCATION MAP	
BEATY GEOLOGICAL LTD.	
SCALE As shown	DATE OCT. 1987
DRAWN	FIG No 1

Claim details are as follows:

Claim Name	Units	Record No.	Record Date	Expiry Date
Ray #1	16	3593	3 Nov. 1986	3 Nov. 1987
Ray #2	16	3594	3 Nov. 1986	3 Nov. 1987
Raymond*	1	3358	24 Sept. 1986	24 Sept. 1987

* The Raymond claim has been consolidated from three reverted crown granted mineral claims referred to as L7334, L7336, L7393.

4. HISTORY

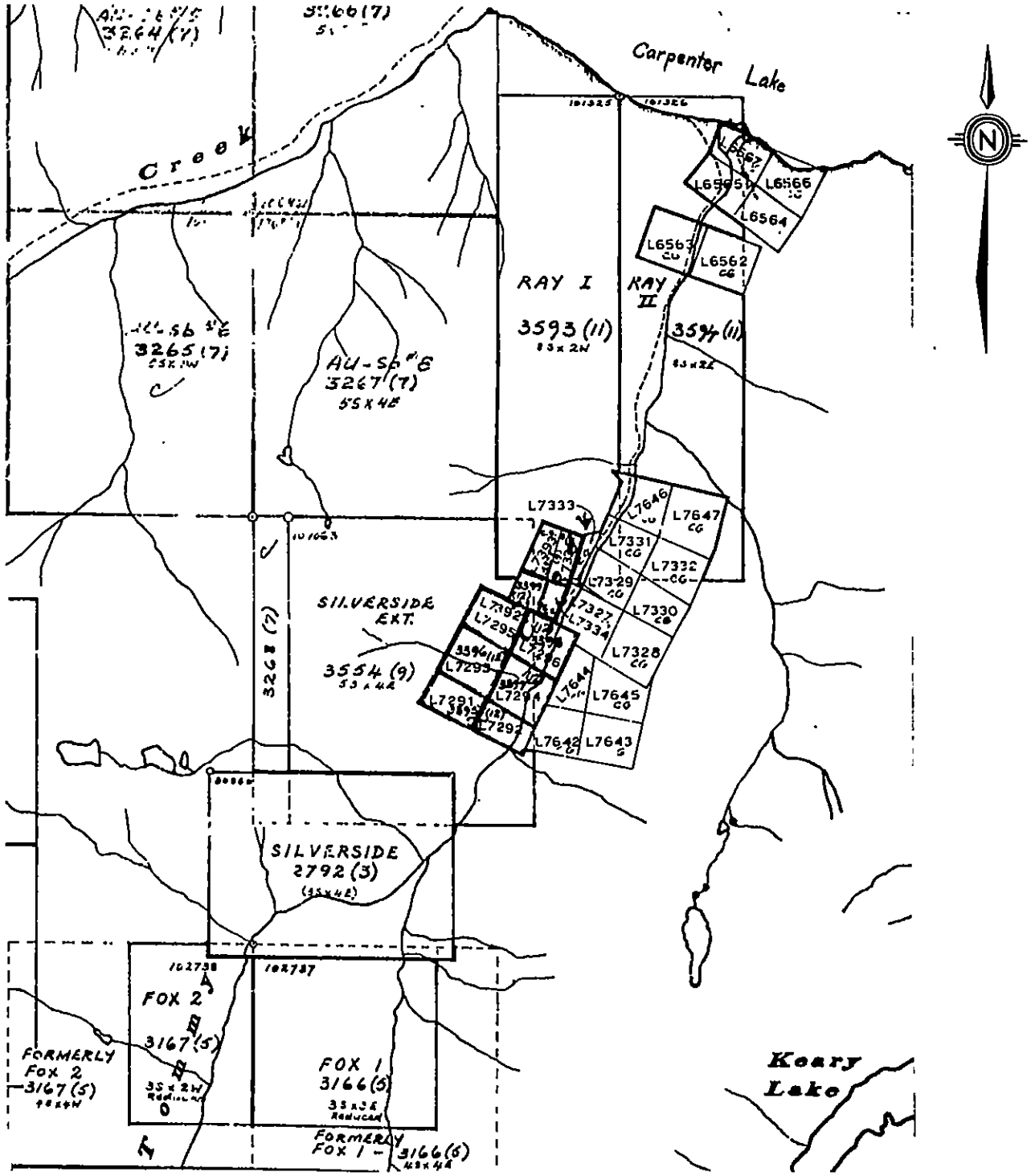
The following historical resume has been summarized from B.C. Minister of Mines reports on the claims that adjoin the Tommy Creek property on the south.

Bristol Mines adjoins the Ray #1 claim on its southeast corner and the Raymond claim on its eastern boundary. This property was under development from 1939 to 1941 by Bristol Mines Limited, a private company. During 1941 a third-level adit was started about 9 m above Tommy Creek, and 215 m of drifting and cross cutting was done. In 1946 the third level was extended in a southerly direction by 39 m and 118 m of drifting. During 1947 a 2743 m underground drilling program was carried out. This drilling was done from the third or lowest level to locate ore shoots similar to the one reported about 9 m below the second level.

The Benboe claims adjoin the Ray #1 claim on its extreme south boundary on the west side of Tommy Creek. The Benboe Deep Mines Syndicate commenced development in 1935. The vein investigated strikes at about 015° and dips 45 to 50° west and in 1937 it had been traced by a series of shallow cuts for a length of about 205 m. The vein extension beyond this length was covered with overburden. The gold assays varied from a low of 0.05 ounces per ton across 0.75 m to a high of 0.36 ounces per ton across 0.4 m. No reference was found that indicated any successful underground development was done on this structure.

5. GEOLOGY

The claim is mostly underlain by greenstones of the Middle Triassic Bridge River Group; these are locally sheared and schistose, or shattered. In places the greenstones are



CLAIMS

Ray I 3593
Ray II 3594
Raymond 1,2,4 3358

1000 500 0 1000 2000 3000 Metres
1 .5 0 1 2 3 Kilometres

VORTEX-EQUINOX JOINT VENTURE

TOMMY CREEK PROPERTY

CLAIM MAP

SCALE 1:50,000 | DATE OCTOBER 1987

FIGURE 2

interlayered with black argillite and less commonly limestone. Most of the observed shearing appears to have a northerly trend and the dips are mostly westerly or near vertical. Towards the head of the Tommy Creek valley the Bridge River Group has been intruded by the Benboe batholith. On the western bank of Tommy Creek, on the Raymond claim, much of the rock appears to be masked by a deep layer of overburden. The 1937 Minister of Mines report mentions that an adit driven on the Benboe Group encountered 14.6 m of overburden. However, in this same report, it is mentioned that the vein had been traced for about 200 m indicating the overburden is not consistently deep.

6. GEOCHEMICAL SAMPLING PROGRAM

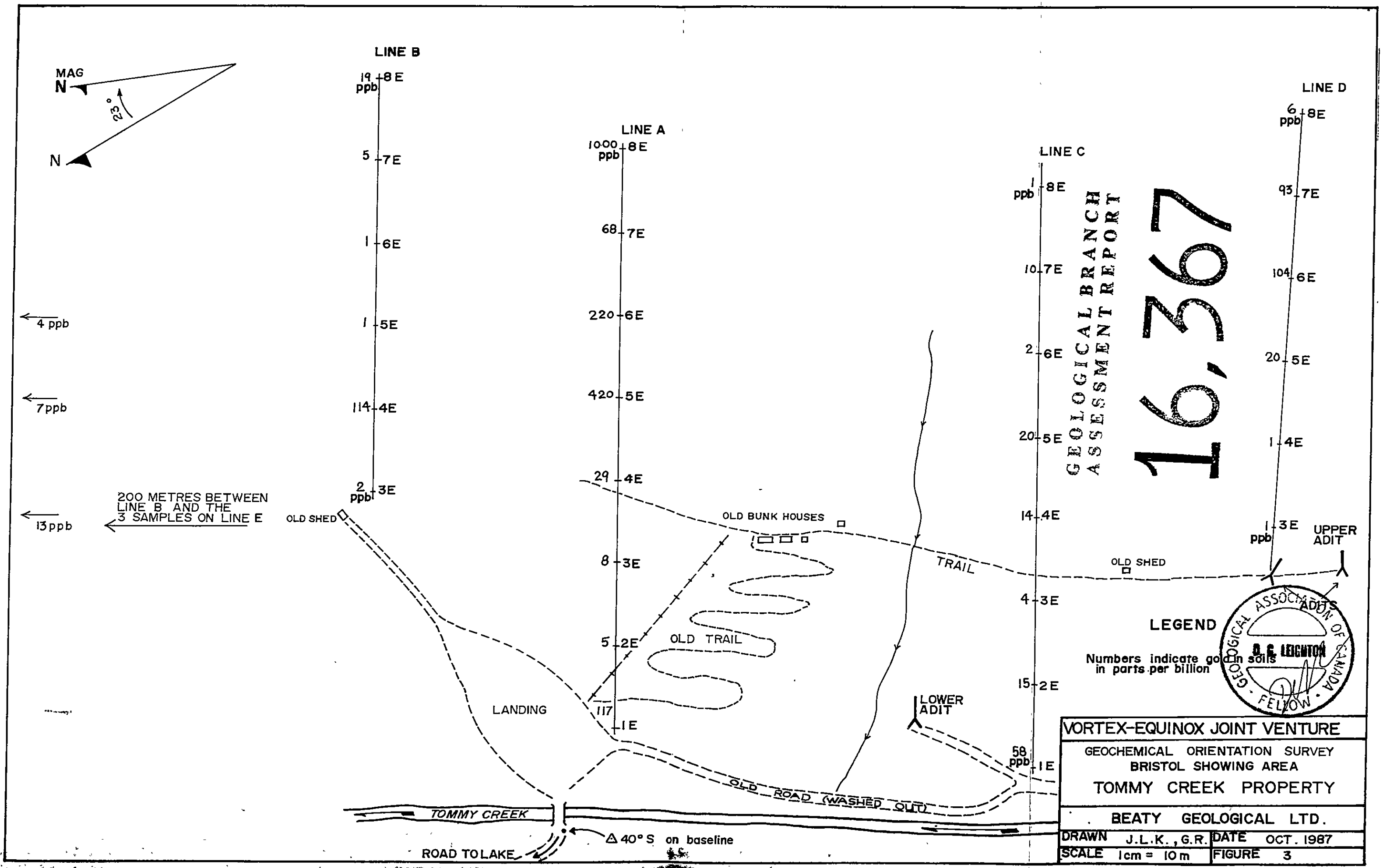
6.1 Field Work (see figures 3 and 4)

Much of the Tommy Creek property is covered by either rock, talus and/or debris slide material. This combined with partial snow cover limited the area which could be effectively tested. For ground control a north-south base line was established between the high water mark in Carpenter Lake and the Tommy Creek bridge - a distance of 4050 meters. Where practical cross lines were placed at 200 m intervals and soil samples were collected every 50 m. The sampling lines were extended until rock bluffs or talus were encountered. The program was restricted mainly to the west side of Tommy Creek. Whenever possible, soil was collected from the B horizon which occurs a few centimeters below surface on average. A number of samples were collected in the vicinity of known showings adjacent to the Tommy Creek property. Results of this orientation survey are shown on Figure 3. This was done to provide data which would help interpret any anomalous results encountered on the Tommy Creek property claims. In all 93 soil samples were collected.

6.2 Analytical Procedure

The samples were sent to Acme Analytical Laboratories of 852 E. Hastings St., Vancouver, B.C. for geochemical ICP analysis. The laboratory method used by Acme is as follows:

A 0.500 gram sample is digested with 3 ml 3-1-2 $HCl-HNO_3-H_2O$ at 95°C for one hour and is diluted to 10 ml with water. This leach is partial for Ma, Fe, Ca, P, La, Cr, Mg, Ba, Ti, B, W, and limited for Na and K. Au detection limit by ICP is 3 ppm., so Au is analyzed by A.A. from a 10 gram sample.



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,367

VORTEX-EQUINOX JOINT VENTURE	
GEOCHEMICAL ORIENTATION SURVEY BRISTOL SHOWING AREA TOMMY CREEK PROPERTY	
BEATY GEOLOGICAL LTD.	
DRAWN J.L.K., G.R.	DATE OCT. 1987
SCALE 1cm = 10m	FIGURE 3

6.3 Results and Interpretation

Results of the sampling program on the Tommy Creek property and adjacent ground are shown on accompanying maps (see Figure 3-4) which show gold values in parts per billion. Additional analytical data appear in Appendix "A". The only anomalous samples encountered were those associated with old workings which have, as indicated earlier, already been evaluated. No new targets were identified. Exploration potential may exist in parts of the property not accessible during the course of this program.

7. CONCLUSIONS AND RECOMMENDATIONS

Exploration work carried out on the Tommy Creek prospect consisted of grid controlled geochemical sampling with complimentary geological-prospecting work. The exploration target is structurally controlled gold mineralization typical of the Goldbridge-Bralorne mining camp. The objective of the 1987 work was to trace potentially mineralized structures along strike from old nearby workings. A fault zone seems to extend north from the old Bristol Mines workings and another north from pits at the Benboe showings. No indication of mineralization was found north of the Bristol or the Raymond though the latter target zone was not adequately sampled due to snow cover.

The Goldbridge-Bralorne area is one of intensive exploration activity and mine development. While the results of work carried out on the Tommy Creek property do not merit follow-up at this time, it is recommended that the claims be maintained in good standing pending results of work being done on other nearby claims.

8. REFERENCES

B.C. Minister of Mines Annual Report (1939)
Benboe, pp. F12-13

B.C. Minister of Mines Annual Report (1946)
Bristol Mines (1946) Ltd., pp. A114-115

B.C. Minister of Mines Annual Report (1947)
Bristol Mines (1946) Ltd., pp. A135-136

9. STATEMENT OF QUALIFICATIONS

9.1 John L. Knox

I, John Knox of Box 1003, Kaslo, B.C. VOG IMO hereby state that:

1. I am a graduate (1970) of the University of British Columbia with a Bachelor of Science Degree in Geology.

2. I have worked as a prospector, exploration geologist and mine geologist mainly in British Columbia, the Yukon Territory and the Northwest Territories since 1964.

3. I have not written any other reports on the properties in the immediate vicinity of the Tommy Creek property.

4. This report is based on knowledge gained from working on the property in 1987 and from the study of published reports on claims in the Tommy creek Valley.

5. I do not have any interest direct or indirect in the Vortex Resources Ltd., Crack Resources Ltd. or Equinox Resources Ltd.

6. I do not have any interest in any other property within 10 kilometers of the Tommy Creek property.

Dated at Vancouver, British Columbia this 30th day of October, 1987.

John L. Knox, B.Sc.

9.2 Douglas G. Leighton

I, Douglas G. Leighton, do hereby certify that:

1. I am a professional geologist with offices at 900 - 625 Howe Street, Vancouver, B.C.

2. I am a graduate of the University of British Columbia, B.Sc., (1968).

3. I am a Fellow in the Geological Association of Canada.

4. I have practiced by profession as a geologist since 1968 mostly in British Columbia.

5. I personally examined the Tommy Creek property in 1987 for Equinox Resources Ltd. and Vortex Resources Ltd.

6. I have not received, nor do I expect to receive, any interest direct or indirect, in the Tommy Creek property, in the Vortex-Equinox joint venture, or in the securities of either Equinox Resources Ltd. or Vortex Resources Ltd.

7. I hereby consent to the publication of this report for purposes of a prospectus or a statement of material facts and to the use of my name therein.

Dated at Vancouver, British Columbia, this 30th day of October, 1987.

Douglas G. Leighton, B.Sc., F.G.A.C.

APPENDIX I

GEOCHEMICAL DATA

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-4 SOILS P5-ROCKS AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JUN 8 1987 DATE REPORT MAILED: June 11/87 ASSAYER. D. Toye ..DEAN TOYE. CERTIFIED B.C. ASSAYER

BEATY GEOLOGICAL PROJECT - 187 File # 87-1633 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
T 16S 450W	8	118	12	280	.4	68	24	2052	4.84	16	5	ND	3	75	3	4	2	57	1.44	.139	20	44	.95	287	.14	21	1.92	.02	.26	1	3
T 16S 400W	3	107	13	165	.4	81	29	1421	7.81	7	5	ND	4	69	1	2	2	110	2.34	.132	19	72	2.25	260	.50	58	3.08	.03	.20	1	1
T 16S 350W	4	166	16	234	.5	90	30	1347	7.09	12	6	ND	4	54	1	2	2	101	1.45	.091	25	68	2.00	968	.41	33	2.74	.02	.21	1	8
T 16S 300W	5	136	12	232	.4	84	27	1240	6.68	18	6	ND	4	51	1	2	2	87	1.05	.100	20	65	1.51	302	.30	16	2.41	.02	.25	1	5
T 16S 250W	2	130	13	186	.5	94	29	1373	7.05	20	5	ND	3	69	1	2	2	111	1.77	.064	18	89	1.97	280	.43	22	2.88	.03	.25	1	3
T 16S 200W	2	112	7	258	.3	108	32	1533	7.58	22	5	ND	3	69	1	2	3	112	1.71	.123	18	95	2.14	371	.39	30	3.26	.03	.28	1	1
T 16S 150W	2	102	13	275	.3	94	30	1282	7.18	14	5	ND	4	65	1	2	3	111	1.71	.123	18	87	1.95	378	.37	25	3.03	.03	.21	1	1
T 16S 100W	6	151	16	233	.4	87	30	1830	6.32	19	5	ND	3	98	1	2	2	82	2.49	.188	23	73	1.51	585	.25	45	2.39	.03	.19	1	4
T 16S 50W	5	134	15	245	.4	87	26	1223	6.48	12	5	ND	3	60	2	2	3	96	1.51	.092	23	76	1.62	550	.33	27	2.62	.03	.16	1	2
T 20S 550W	1	30	9	264	.1	44	12	1021	2.89	15	5	ND	2	35	1	2	2	49	.72	.184	11	40	.56	313	.17	8	1.53	.03	.14	1	2
T 20S 500W	2	26	8	240	.1	46	13	922	3.17	23	5	ND	2	30	1	2	2	54	.52	.217	9	44	.60	286	.18	9	1.70	.03	.14	1	1
T 20S 450W	1	28	10	165	.1	42	12	717	2.80	14	5	ND	2	24	1	2	3	51	.52	.117	9	39	.56	183	.19	6	1.58	.03	.11	1	1
T 20S 400W	2	45	7	209	.1	67	16	662	4.06	19	5	ND	2	34	1	2	2	69	.86	.115	12	56	.83	234	.29	10	2.26	.02	.18	1	3
T 20S 350W	2	74	11	227	.1	77	23	1021	5.21	41	5	ND	3	38	1	3	2	93	1.26	.134	14	78	1.09	209	.26	12	2.81	.02	.12	1	1
T 20S 300W	2	58	6	147	.2	70	19	802	5.49	17	5	ND	3	29	1	3	2	81	.68	.086	16	64	.96	123	.36	12	2.27	.03	.27	1	1
T 20S 250W	1	22	4	135	.1	40	9	392	2.27	14	5	ND	2	24	1	3	2	47	.42	.101	7	34	.46	101	.19	7	1.32	.03	.10	1	1
T 20S 200W	2	66	5	103	.1	68	16	536	4.08	29	5	ND	2	25	1	2	2	76	.70	.047	13	68	1.04	106	.34	9	1.89	.03	.25	1	2
T 20S 150W	1	117	7	151	.3	93	26	985	5.93	34	5	ND	3	45	1	2	2	93	1.54	.073	14	90	1.67	96	.39	17	2.62	.03	.23	1	4
T 20S 100W	3	138	14	165	.3	108	30	1107	7.06	36	5	ND	4	60	1	2	2	110	1.95	.109	17	105	2.07	95	.45	31	3.06	.03	.24	1	1
T 20S 50W	2	119	9	141	.3	106	30	1162	7.07	36	5	ND	4	67	1	2	3	108	2.28	.092	14	102	2.21	82	.46	23	3.05	.04	.23	1	1
T 22S 550W	1	21	7	173	.1	33	10	675	2.62	15	5	ND	2	30	1	2	2	46	.53	.230	7	36	.47	214	.16	7	1.32	.03	.09	1	1
T 22S 500W	3	41	8	177	.1	49	18	1439	3.87	32	5	ND	3	30	1	2	2	67	.68	.191	10	58	.61	298	.22	6	1.69	.02	.13	1	1
T 22S 450W	2	36	5	177	.1	71	18	1048	3.90	17	5	ND	2	27	1	2	2	64	.62	.159	9	72	.90	231	.21	8	2.06	.02	.11	1	1
T 22S 400W	1	39	4	128	.1	54	15	676	3.74	10	6	ND	3	22	1	2	2	62	.49	.058	7	44	.72	99	.31	7	1.44	.03	.12	2	1
T 22S 300W	1	28	3	185	.1	39	11	403	2.69	9	5	ND	2	30	1	2	2	44	.47	.198	6	37	.50	123	.18	7	1.24	.03	.14	1	1
T 22S 250W	1	89	2	190	.1	75	27	1089	6.46	9	5	ND	2	43	1	2	2	69	.78	.197	9	47	.74	130	.24	9	1.68	.02	.21	1	2
T 22S 200W	1	120	8	176	.1	87	32	966	7.43	9	5	ND	3	44	1	2	3	79	.91	.139	16	55	.85	77	.29	11	1.88	.02	.20	1	1
T 22S 100W	1	99	2	197	.3	83	27	1490	6.12	29	5	ND	3	57	1	2	2	77	1.14	.186	13	65	.97	168	.25	12	2.13	.02	.14	1	2
T 26S 700W	4	65	6	179	.1	86	25	1532	4.85	60	5	ND	3	50	2	2	2	86	.80	.060	11	106	1.45	148	.25	8	2.00	.03	.12	1	6
T 26S 650W	3	52	9	188	.1	75	21	1500	4.18	42	5	ND	2	37	2	2	2	75	.61	.095	10	85	1.14	150	.21	6	1.87	.03	.10	1	5
T 26S 600W	2	33	6	186	.1	57	16	1343	3.15	33	5	ND	3	45	1	2	3	58	.64	.190	8	63	.73	265	.17	7	1.60	.03	.11	1	6
T 26S 550W	1	12	8	161	.1	26	9	811	1.97	7	5	ND	2	29	1	2	2	41	.33	.147	4	30	.37	121	.14	4	1.01	.03	.09	1	1
T 26S 500W	1	19	8	182	.1	27	9	1347	2.16	23	5	ND	1	36	1	2	2	41	.47	.191	5	27	.34	201	.14	6	.97	.03	.11	1	1
T 26S 450W	1	13	5	87	.1	21	7	342	1.73	11	5	ND	1	15	1	2	2	37	.17	.194	3	22	.27	106	.11	3	.90	.03	.05	1	1
T 26S 400W	4	61	9	231	.2	149	25	1379	5.26	30	5	ND	3	22	1	2	2	88	.56	.210	8	179	1.98	180	.29	8	2.66	.02	.14	2	1
T 26S 350W	1	33	6	147	.1	39	12	880	2.75	23	5	ND	2	21	1	2	2	52	.39	.184	7	45	.46	133	.18	3	1.41	.03	.10	1	1
STD C/AU-S	21	59	41	132	6.8	68	28	1007	3.95	41	16	7	33	48	18	17	21	64	.45	.100	35	57	.86	180	.08	37	1.71	.07	.12	13	51

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
T 26S 300W	1	71	3	186	.1	67	21	1017	4.53	12	5	ND	1	29	1	2	2	67	.54	.147	8	68	.81	182	.28	8	1.90	.03	.17	1	45
T 26S 250W	1	109	4	165	.2	89	29	1075	6.65	11	5	ND	3	29	1	2	2	88	.70	.109	13	82	1.24	108	.38	9	2.20	.03	.19	1	4
T 26S 200W	1	122	3	167	.1	86	29	968	6.36	7	5	ND	3	35	1	2	2	79	.67	.122	10	90	1.14	100	.38	11	2.07	.03	.25	1	1
T 26S 150W	2	176	9	195	.2	115	37	1492	7.66	11	5	ND	3	47	1	2	2	85	1.95	.215	18	106	1.20	137	.26	14	2.39	.03	.26	1	1
T 26S 100W	3	89	5	170	.2	76	30	1709	8.12	14	5	ND	4	50	1	2	2	89	1.43	.186	24	75	1.65	105	.31	15	2.66	.02	.22	1	2
T 26S 50W	4	90	8	170	.1	117	36	1491	7.40	8	6	ND	6	90	1	2	2	102	3.13	.139	40	111	1.87	66	.32	16	2.94	.03	.22	1	1
T 30S 700W	4	36	8	238	.1	47	13	559	3.64	135	5	ND	2	21	1	2	2	57	.31	.123	8	45	.55	89	.13	11	1.55	.03	.10	1	2
T 30S 650W	3	32	9	350	.1	52	15	1088	3.57	87	5	ND	2	31	2	2	2	58	.45	.171	8	51	.57	164	.14	7	1.76	.03	.11	1	3
T 30S 600W	2	39	7	155	.1	63	14	685	3.65	111	5	ND	3	26	1	2	2	62	.38	.122	9	59	.75	130	.16	8	1.77	.03	.15	1	2
T 30S 550W	4	70	8	171	.1	136	33	1695	5.06	63	5	ND	2	42	1	2	2	96	.75	.140	10	155	1.77	139	.25	8	2.28	.02	.17	1	1
T 30S 500W	5	86	10	191	.1	154	39	2086	5.41	64	5	ND	3	57	2	2	2	91	.96	.163	12	164	1.90	166	.25	11	2.43	.02	.16	1	12
T 30S 400W	1	16	6	157	.1	33	10	955	2.37	29	5	ND	2	34	1	2	3	47	.41	.195	5	42	.43	126	.15	5	1.05	.03	.09	1	1
T 30S 300W	2	48	5	123	.1	76	18	706	4.19	55	5	ND	2	25	1	2	2	77	.54	.100	9	78	1.10	112	.20	9	1.88	.03	.23	1	1
T 30S 250W	3	68	6	153	.1	108	20	774	5.01	111	5	ND	4	22	1	2	2	86	.52	.085	11	113	1.44	97	.32	9	2.19	.03	.19	1	4
T 30S 200W	2	41	9	115	.1	72	17	853	3.51	93	5	ND	3	24	1	2	4	66	.44	.125	8	74	.95	153	.20	6	1.60	.04	.22	1	8
T 32SS 450W	4	89	5	142	.4	110	23	1078	5.19	325	5	ND	3	34	1	2	2	86	.73	.110	14	105	1.66	153	.21	8	2.08	.04	.43	3	18
T 32SS 400W	6	107	8	159	.3	143	27	1176	5.60	161	5	ND	3	37	1	2	3	87	.82	.117	14	137	1.92	150	.19	10	2.20	.03	.36	1	8
T 32SS 350W	3	102	13	131	.3	169	28	954	5.61	252	6	ND	4	39	1	2	2	110	.77	.100	11	180	2.42	233	.27	7	2.81	.08	.51	1	10
T 32SS 300W	3	95	5	140	.5	124	26	1035	5.69	572	5	ND	4	36	1	3	2	100	.89	.112	14	124	1.96	181	.23	6	2.46	.06	.42	2	25
STD C/AU-S	21	58	38	133	7.0	69	28	1013	3.87	39	16	7	36	47	18	15	20	64	.46	.102	36	60	.86	176	.08	36	1.69	.07	.12	14	49
T 32SS 250W	4	110	11	159	.4	135	26	1203	5.48	247	5	ND	4	33	1	2	2	88	.78	.120	17	136	2.13	205	.20	7	2.45	.04	.42	1	41
T 32SS 200W	5	109	7	161	.4	160	27	1122	5.87	198	5	ND	4	37	1	2	2	93	.85	.119	15	168	2.23	184	.19	7	2.55	.05	.40	1	32
T 32SS 150W	6	111	8	167	.3	167	27	1178	5.74	181	5	ND	3	35	1	2	2	91	.67	.104	15	165	2.13	174	.20	7	2.43	.04	.37	1	10
T 32SS 100W	5	95	15	161	.5	159	25	1024	5.31	148	5	ND	3	36	1	2	2	88	.72	.128	14	164	2.10	172	.19	7	2.31	.04	.44	1	10
T 32SS 50W	6	105	10	158	.2	156	28	1311	5.28	146	5	ND	3	36	1	2	2	96	.77	.119	13	155	2.00	173	.18	8	2.28	.04	.36	1	6
T 34SS 450W	2	72	6	140	.1	96	27	664	6.69	143	5	ND	2	17	1	2	2	107	.55	.091	9	98	2.07	68	.50	6	2.99	.03	.29	1	5
T 34SS 400W	2	46	2	128	.3	64	17	991	4.79	98	5	ND	4	30	1	2	2	71	.54	.118	17	63	1.31	136	.19	8	2.39	.03	.26	1	1
T 34SS 350W	1	58	8	177	.1	72	17	737	4.07	61	5	ND	4	26	1	2	2	73	.44	.105	16	81	1.76	125	.18	4	2.33	.03	.15	1	1
T 34SS 300W	3	44	8	422	.1	72	19	1019	3.97	67	5	ND	2	24	2	3	2	62	.37	.103	11	57	.94	160	.14	6	2.18	.03	.12	1	4
T 34SS 250W	1	17	3	154	.1	34	8	325	1.96	26	5	ND	1	19	1	3	2	41	.33	.092	6	34	.52	79	.13	5	1.11	.03	.08	1	1
T 34SS 200W	1	15	8	182	.1	35	9	427	2.07	26	5	ND	2	20	1	2	2	46	.34	.137	6	37	.46	110	.13	3	1.15	.03	.06	1	1
T 34SS 150W	1	55	4	113	.1	75	16	412	3.40	70	5	ND	3	18	1	2	2	74	.39	.094	6	69	1.02	115	.21	4	1.87	.03	.16	1	1
T 34SS 100W	1	56	2	129	.1	81	17	480	3.53	67	5	ND	4	17	1	2	2	71	.38	.100	6	80	1.18	129	.21	5	1.90	.04	.17	1	2
T 34SS 50W	1	20	2	94	.1	36	9	387	2.06	29	5	ND	2	15	1	2	4	44	.27	.090	5	37	.52	128	.14	2	1.14	.04	.08	1	4
T 36S 250W	1	24	4	84	.1	39	10	265	2.37	60	5	ND	2	23	1	2	2	46	.37	.104	6	32	.57	76	.16	7	1.22	.04	.09	1	1
T 36S 200W	3	74	5	142	.2	92	23	840	6.14	433	5	ND	3	27	1	3	2	94	.50	.088	16	84	1.37	123	.23	9	2.32	.02	.28	1	13
T 36S 150W	2	58	6	121	.1	75	17	499	4.37	257	5	ND	4	26	1	4	2	71	.47	.071	13	71	1.10	126	.19	6	1.89	.03	.24	1	4

BEATY GEOLOGICAL PROJECT - 187 FILE # 87-1633

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
T 34S 100W	1	57	6	159	.1	86	20	579	4.77	139	5	ND	1	28	1	2	2	77	.45	.109	8	76	1.32	100	.26	5	2.18	.03	.20	1	4
T 36S 50W	1	44	10	140	.1	70	19	1004	4.07	102	5	ND	1	46	1	2	2	65	.53	.181	8	64	1.07	159	.21	5	1.86	.03	.22	1	1
T 38S 250W	2	53	8	218	.1	119	24	739	4.52	124	5	ND	2	28	1	4	2	78	.44	.082	9	88	1.30	155	.28	5	2.36	.03	.22	1	4
T 38S 200W	1	36	9	206	.1	87	19	770	3.54	67	5	ND	1	32	1	2	2	67	.43	.176	7	74	1.11	196	.21	5	2.06	.04	.15	1	1
T 38S 150W	1	71	6	142	.1	107	21	713	4.87	209	5	ND	3	25	1	9	2	88	.42	.057	11	112	1.49	162	.26	5	2.25	.04	.41	1	30
T 38S 100W	1	68	11	226	.2	120	25	1085	5.32	200	5	ND	3	32	1	11	2	92	.63	.106	13	128	1.66	273	.25	6	2.37	.04	.26	1	16
T 38S 50W	1	67	4	156	.1	105	22	675	4.75	128	5	ND	2	30	1	5	2	92	.61	.155	11	114	1.65	180	.23	3	2.25	.05	.27	1	12
STD C/AU-S	20	58	38	131	7.2	71	30	1072	4.00	38	15	7	35	50	17	16	19	66	.46	.107	35	63	.92	179	.08	36	1.70	.07	.12	13	48
TOM LA 1E	2	83	13	198	.5	93	24	1095	5.07	645	5	ND	1	55	1	6	2	87	1.52	.105	11	97	1.24	226	.18	5	2.14	.05	.30	2	117
TOM LA 2E	1	48	7	203	.4	66	20	1661	3.67	129	5	ND	2	34	2	3	2	70	.58	.244	5	72	.83	529	.17	3	1.70	.03	.16	1	5
TOM LA 3E	1	65	7	178	.1	85	22	876	4.31	194	5	ND	2	35	1	2	2	85	.49	.223	6	82	1.11	250	.19	2	2.13	.04	.20	1	8
TOM LA 4E	1	40	10	137	.2	49	17	840	3.55	402	5	ND	2	32	1	2	2	62	.46	.096	9	51	.65	103	.13	3	1.51	.03	.09	1	29
TOM LA 5E	3	127	14	189	.9	82	28	1319	6.82	2246	5	ND	2	55	1	12	2	69	.94	.102	26	72	.91	147	.06	6	1.57	.02	.10	1	420
TOM LA 6E	3	151	10	229	1.0	86	27	1002	6.87	1707	5	ND	3	81	1	13	3	65	1.65	.115	23	69	.89	120	.06	7	1.48	.02	.14	1	220
TOM LA 7E	4	131	9	240	.8	90	29	1040	6.87	1629	5	ND	3	41	2	9	2	70	1.59	.126	21	87	1.00	109	.05	9	1.52	.02	.15	1	68
TOM LA 8E	2	104	8	210	.6	107	36	1354	7.96	4820	5	ND	3	80	1	19	2	85	1.37	.134	28	121	1.50	141	.07	9	2.08	.02	.18	1	1000
TOM LB 3E	1	59	5	159	.1	52	16	1081	3.32	99	5	ND	2	28	1	2	2	63	.49	.126	12	48	.66	134	.15	4	1.63	.03	.10	1	2
TOM LB 4E	1	68	11	179	.1	67	21	1296	4.31	175	5	ND	1	32	1	2	2	73	.59	.169	10	73	.95	113	.15	3	1.79	.03	.19	2	114
TOM LB 5E	1	47	7	266	.1	46	16	1100	2.47	50	5	ND	1	35	1	2	3	42	.49	.230	9	26	.35	120	.11	2	1.22	.03	.08	1	1
TOM LB 6E	3	102	11	231	.1	78	24	1598	4.12	135	5	ND	2	41	1	3	2	69	.76	.133	17	85	.98	114	.11	2	1.95	.02	.09	1	1
TOM LB 7E	4	177	14	267	.1	132	41	2110	6.06	188	5	ND	3	55	1	4	2	97	.86	.094	28	194	1.71	135	.13	5	2.57	.02	.17	1	5
TOM LB 8E	5	117	10	322	.3	93	28	2507	5.08	443	5	ND	3	59	1	6	2	59	1.00	.156	21	59	.78	153	.08	6	1.85	.02	.16	1	19
TOM LC 1E	4	110	7	196	.1	121	32	1235	6.22	470	5	ND	2	47	1	2	2	103	.98	.153	10	106	1.73	277	.24	2	2.58	.05	.50	2	58
TOM LC 2E	1	67	6	151	.1	69	21	1147	4.32	128	5	ND	1	47	1	3	2	77	1.28	.136	9	60	1.18	150	.18	5	2.07	.03	.26	1	15
TOM LC 3E	1	56	8	165	.1	70	19	479	4.26	107	5	ND	1	33	1	2	2	82	.83	.077	7	67	.98	81	.18	5	1.99	.03	.09	1	4
TOM LC 4E	1	66	10	224	.4	64	21	2018	5.30	154	5	ND	2	40	2	2	2	92	1.22	.168	11	61	.96	204	.18	6	2.40	.03	.19	1	14
TOM LC 5E	1	86	13	359	.1	97	37	1527	5.49	179	5	ND	3	34	2	2	2	121	.68	.162	10	143	2.09	146	.21	4	2.81	.03	.19	1	20
TOM LC 6E	1	19	9	101	.1	28	10	541	2.22	74	5	ND	1	27	1	2	2	49	.45	.153	4	29	.45	124	.17	3	1.12	.03	.06	1	2
TOM LC 7E	2	66	9	292	.1	81	27	1346	5.13	223	5	ND	2	27	1	3	2	92	.56	.201	9	87	1.12	144	.21	5	2.54	.03	.16	1	10
TOM LC 8E	2	40	11	146	.1	43	17	917	3.60	187	5	ND	2	22	1	2	2	63	.37	.121	9	36	.51	76	.16	4	1.54	.03	.09	1	1
TOM LD 3E	1	41	7	46	.3	30	5	196	1.37	115	5	ND	1	396	1	2	4	24	23.15	.051	2	19	.65	80	.07	25	.60	.06	.08	4	1
TOM LD 4E	1	64	7	46	.1	35	10	321	2.35	255	5	ND	1	247	1	2	2	41	17.94	.079	5	36	.70	70	.07	25	.98	.06	.12	2	1
TOM LD 5E	3	72	8	124	.4	60	23	673	5.47	458	5	ND	1	239	1	9	2	98	13.64	.201	17	47	.92	83	.08	12	1.40	.08	.23	2	20
TOM LD 6E	1	83	3	90	.1	82	23	709	5.33	432	5	ND	1	79	1	5	2	109	2.47	.085	10	83	1.67	91	.30	9	2.36	.05	.37	1	104
TOM LD 7E	1	90	4	101	.1	88	27	823	5.93	506	5	ND	2	28	1	3	2	126	.78	.107	11	108	1.92	94	.35	4	2.63	.05	.37	1	93
TOM LD 8E	1	129	7	131	.1	106	31	1099	5.88	258	5	ND	2	27	1	2	2	126	.55	.116	8	143	1.71	111	.30	8	2.87	.04	.28	1	6
TOM LE 1E	2	100	10	220	.3	81	24	1255	4.53	220	5	ND	2	34	1	3	2	77	.78	.201	13	81	1.03	169	.16	3	2.02	.03	.21	1	13

BEATY GEOLOGICAL PROJECT - 187 FILE # 87-1633

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
TOM LE 2E	3	80	11	215	.2	63	20	1117	3.81	131	5	ND	2	58	1	2	2	59	.95	.180	15	49	.73	107	.12	5	1.71	.03	.12	1	7
TOM LE 3E	2	56	7	215	.1	49	19	1539	3.13	87	5	ND	1	66	1	2	2	50	1.30	.201	8	45	.57	154	.11	7	1.34	.02	.13	3	4
TOM LF 1	1	20	7	136	.1	29	8	883	2.58	5	5	ND	2	46	1	2	2	50	.59	.148	11	27	.52	201	.12	7	1.27	.03	.12	1	3
TOM LF 2	2	65	11	137	.1	64	19	712	6.69	15	5	ND	3	51	1	2	2	125	.70	.086	26	65	1.49	273	.17	10	3.27	.02	.22	1	1
TOM LF 3	1	7	4	119	.2	16	5	239	1.62	2	5	ND	1	22	1	2	2	43	.23	.077	4	14	.27	135	.12	4	.77	.03	.05	1	2
TOM LF 4	1	19	8	266	.1	32	11	653	3.08	10	5	ND	3	73	1	2	2	53	.69	.150	11	30	.59	197	.11	14	1.61	.03	.17	1	1
TOM LF 5	1	10	10	100	.1	18	7	845	2.09	7	5	ND	2	70	1	2	2	39	.40	.047	8	21	.35	139	.11	11	1.11	.04	.08	1	1
TOM LF 6	2	18	5	82	.1	24	9	867	3.25	3	5	ND	1	145	1	2	2	59	1.12	.057	16	38	.55	187	.14	21	1.32	.03	.09	1	1
STD C/AU-S	22	61	37	137	7.2	73	29	1050	4.09	41	17	8	37	49	18	16	19	65	.48	.106	39	58	.90	177	.08	37	1.75	.07	.13	14	48
TOM LF 7	1	7	6	89	.1	16	6	261	1.78	4	5	ND	2	37	1	2	2	40	.21	.045	7	16	.28	88	.11	8	.83	.03	.09	1	1
TOM LF 8	1	7	4	97	.1	14	5	253	1.74	3	5	ND	2	17	1	2	2	40	.21	.069	5	13	.25	70	.11	4	.77	.03	.08	1	1
TOM LG 1	2	24	6	129	.1	33	10	720	3.16	14	5	ND	1	46	1	2	2	52	.59	.162	12	28	.57	252	.10	8	1.50	.03	.15	1	1
TOM LG 2	4	60	5	163	.1	55	19	597	6.84	15	5	ND	3	32	1	2	2	88	.44	.095	24	42	1.10	258	.08	7	2.59	.02	.28	2	1
TOM LG 3	1	43	5	140	.1	51	18	461	7.22	11	5	ND	3	42	1	2	2	111	.71	.093	24	56	2.00	199	.24	7	3.32	.03	.21	1	1
TOM LG 4	1	28	5	111	.1	34	14	477	5.16	7	5	ND	3	36	1	2	2	85	.51	.078	19	31	1.11	157	.13	7	2.38	.03	.19	1	1
TOM LG 5	1	16	5	77	.1	20	8	300	2.90	4	5	ND	2	25	1	2	2	63	.34	.034	11	18	.54	84	.13	5	1.36	.04	.09	1	1
TOM LG 6	1	15	8	109	.1	24	8	427	2.29	4	5	ND	2	39	1	2	2	49	.51	.091	12	23	.44	114	.12	7	1.14	.03	.10	1	1
TOM LG 7	4	59	5	133	.1	41	19	734	7.52	10	5	ND	4	62	1	2	2	107	.65	.060	46	50	1.73	128	.15	20	3.14	.02	.35	1	3
TOM LG 8	5	94	6	178	.1	76	25	823	8.03	16	5	ND	4	56	1	2	2	95	.56	.080	34	62	1.35	188	.04	23	3.01	.02	.40	1	2
TOM LG 9	1	12	9	132	.1	33	9	475	2.66	7	5	ND	2	20	1	2	2	53	.28	.083	9	26	.45	127	.12	6	1.40	.03	.18	1	2
TOM LG 10	6	66	2	152	.1	55	16	444	6.24	19	5	ND	3	25	1	2	2	69	.54	.102	26	38	.69	124	.11	7	1.89	.02	.19	2	2
T 16S 400W	2	160	9	155	.1	135	45	2006	7.91	25	5	ND	3	73	1	2	2	119	2.17	.086	13	99	2.56	127	.47	59	3.50	.04	.22	1	6
T 16S 550W	2	101	17	188	.1	93	27	1555	5.34	35	5	ND	2	84	1	2	2	81	1.81	.277	13	69	1.25	238	.24	34	2.52	.03	.16	1	1
T 16S 500W	5	109	11	261	.2	83	24	1695	5.92	29	5	ND	2	56	1	2	2	88	1.14	.078	19	62	1.17	264	.34	17	2.64	.03	.30	1	4
T 17SS 550W	18	191	17	515	1.4	104	34	2879	7.44	29	5	ND	4	32	4	6	2	49	.60	.066	29	22	.43	308	.01	7	1.27	.01	.16	1	7
T 17SS 500W	4	58	8	218	.1	52	14	1024	4.17	21	5	ND	3	30	1	2	2	66	.50	.062	13	36	.57	225	.17	8	1.71	.02	.17	3	1
T 17SS 450W	4	52	10	177	.1	47	13	772	3.82	23	5	ND	2	40	1	2	2	64	.69	.061	10	41	.52	145	.19	11	1.50	.02	.17	1	1
T 17SS 400W	4	82	13	184	.1	83	24	1251	5.68	27	5	ND	3	52	1	2	2	78	1.05	.106	15	82	1.10	194	.23	18	2.02	.02	.26	2	1
T 17SS 350W	2	93	4	132	.1	86	22	820	5.67	29	5	ND	3	35	1	2	2	106	1.18	.061	11	86	1.36	141	.48	10	2.91	.03	.15	1	3
T 17SS 300W	1	36	5	108	.1	50	12	748	2.98	30	5	ND	2	57	1	2	2	59	1.03	.153	8	47	.61	156	.19	10	1.42	.03	.15	1	3
T 17SS 250W	1	37	5	224	.1	45	13	1532	2.93	23	5	ND	2	67	1	2	2	53	1.12	.216	8	48	.57	275	.16	10	1.44	.03	.17	1	2
T 17SS 200W	1	24	7	104	.1	39	10	449	2.49	19	5	ND	2	25	1	2	2	53	.40	.094	6	30	.51	137	.19	6	1.23	.04	.12	2	2
T 17SS 150W	2	55	8	107	.1	72	16	623	4.27	40	5	ND	2	29	1	2	2	76	.73	.085	9	71	1.28	104	.28	11	1.80	.04	.24	2	5

BEATY GEOLOGICAL PROJECT - 187 FILE # 87-1633

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
J187 TOM 1R	4	32	2	197	.4	94	22	765	8.11	161	5	ND	5	135	1	3	2	71	5.75	.905	18	137	1.85	64	.05	8	2.38	.09	.40	1	8
J187 TOM 2R	1	46	2	70	.5	80	18	771	4.37	2785	5	ND	2	236	1	8	2	24	10.82	.074	2	37	2.90	22	.01	10	.58	.06	.17	1	64
J187 TOM 3R	2	5	2	163	.3	137	32	876	6.95	42	5	ND	4	137	1	2	2	88	6.15	.589	15	196	2.84	78	.06	7	2.90	.08	.59	1	2
J187 TOM 4R	1	37	2	112	.3	118	26	962	5.00	198	5	ND	3	177	1	6	2	33	8.17	.170	5	88	3.00	1	.01	11	.74	.06	.20	1	1
J187 TOM 5R	2	22	5	97	.6	13	8	732	3.69	57	5	ND	3	294	1	2	2	22	16.22	.081	5	7	1.29	64	.01	17	.39	.07	.16	1	1
J187 TOM 6R	2	55	2	73	.4	36	18	991	5.90	5932	5	ND	4	363	1	13	2	50	9.59	.143	7	22	2.86	28	.01	23	.45	.06	.18	1	2380
J187 TOM 7R	2	45	2	85	4.8	56	19	1298	5.28	13754	5	4	3	185	1	62	2	32	7.25	.131	5	15	2.19	21	.01	16	.53	.05	.18	3	11140
J187 TOM 8R	2	51	3	81	3.1	75	24	981	5.73	19434	5	7	4	203	1	120	2	37	5.96	.115	5	22	1.19	21	.01	16	.73	.04	.21	1281	14520
J187 TOM 9R	3	39	4	110	6.4	42	18	827	5.97	21411	5	6	4	147	1	85	2	51	7.42	.284	8	24	1.40	44	.03	15	1.09	.05	.32	5	8380
J187 TOM 10R	1	4	6	9	.6	3	1	24	.20	107	5	ND	1	878	1	2	.5	2	36.03	.005	2	3	.47	84	.01	9	.05	.01	.01	13	9
J187 TOM 12R	5	55	5	96	.2	17	5	439	1.92	7	5	ND	2	68	1	2	2	26	3.22	.038	9	10	.50	65	.03	10	.74	.02	.15	1	4
J187 TOM 13R	2	76	2	101	.1	92	26	1132	6.69	13	5	ND	4	134	1	3	2	189	4.38	.196	14	221	4.40	95	.48	7	3.07	.10	.07	2	1
J187 TOM 14R	1	25	2	77	.1	61	21	671	5.73	12	5	ND	4	149	1	2	2	68	11.51	.188	12	43	.82	34	.50	20	1.50	.10	.37	2	1
J187 TOM 15R	6	46	4	104	.1	17	5	919	2.33	10	5	ND	2	109	1	2	2	26	5.50	.039	6	12	.37	192	.01	9	.78	.04	.13	1	2
J187 TOM 16R	7	22	2	79	.3	8	2	1934	1.88	6	5	ND	2	277	1	3	4	12	13.64	.029	4	3	.31	74	.01	6	.39	.06	.05	1	1
J187 TOM 17R	6	59	6	102	.3	19	7	472	2.64	11	5	ND	1	24	1	2	2	34	.81	.052	8	13	.35	233	.01	10	.84	.02	.17	1	8
J187 TOM 18R	1	29	7	29	.2	10	8	61	.94	68	5	ND	2	121	1	2	2	15	.80	.031	4	3	.40	27985	.05	4	2.89	.16	.61	1	29
MAC187 TOM 1R	1	4	9	12	.4	2	1	11	.14	8	5	ND	1	1001	1	2	4	1	35.30	.007	2	1	.47	378	.01	15	.04	.01	.01	3	1
STD C/AU-R	20	58	38	132	6.9	70	28	1006	3.97	40	16	7	33	47	17	16	18	63	.46	.102	36	60	.90	180	.08	37	1.72	.07	.14	12	485

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL/ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JUNE 10 1987 DATE REPORT MAILED: June 16/87 ASSAYER. D. Toye .DEAN TOYE. CERTIFIED B.C. ASSAYER

BEATY GEOLOGICAL PROJECT - 187 File # 87-1679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
T BL 12+00S	3	126	7	177	.2	73	26	981	5.82	31	5	ND	3	77	1	2	2	95	3.91	.084	12	67	1.45	114	.30	115	2.26	.06	.15	1	1
T BL 14+00S	2	54	6	125	.1	57	15	636	3.59	43	5	ND	2	23	1	2	2	67	.46	.089	11	54	.78	175	.20	5	1.79	.03	.13	1	4
T BL 16+00S	5	137	11	210	.2	86	29	1277	6.41	12	5	ND	3	.65	1	2	2	90	1.68	.104	20	69	1.71	567	.34	42	2.38	.03	.15	1	7
T BL 18+00S	2	86	8	130	.1	90	20	801	4.74	60	5	ND	3	39	1	2	2	84	1.11	.081	12	90	1.56	134	.26	9	1.99	.04	.28	1	10
T BL 20+00S	1	86	10	125	.1	88	22	815	4.87	72	5	ND	3	52	1	2	2	84	1.90	.100	11	85	1.55	113	.26	10	1.98	.04	.24	1	9
T BL 22+00S	3	73	10	151	.1	160	26	1173	4.94	28	5	ND	2	32	1	2	2	80	.79	.147	11	173	1.97	172	.21	6	2.43	.02	.13	3	1
T BL 26+00S	2	86	4	141	.1	78	26	995	5.77	27	5	ND	3	64	1	2	2	76	2.27	.170	13	76	1.13	98	.21	11	1.82	.03	.21	1	3
T BL 28+00S	8	215	19	230	.1	109	24	1534	5.87	14	5	ND	3	34	1	2	4	40	.54	.066	20	37	.52	244	.06	4	.80	.01	.09	1	8
T BL 30+00S	1	58	5	78	.1	76	16	410	3.35	146	5	ND	2	27	1	2	2	71	1.09	.080	7	80	1.09	124	.15	2	1.41	.05	.33	2	35
T BL 32+00S	2	68	6	128	.1	113	20	935	3.92	145	5	ND	1	26	1	2	2	71	.51	.086	10	105	1.29	149	.15	2	1.97	.03	.24	1	6
T BL 34+00S	1	70	6	145	.1	98	20	534	4.48	82	5	ND	2	23	1	2	2	86	.54	.087	10	99	1.59	151	.26	4	2.28	.04	.24	1	3
T BL 36+00S	1	53	6	93	.1	55	13	478	3.15	153	5	ND	2	19	1	4	2	61	.39	.067	10	59	.84	116	.16	2	1.52	.04	.20	1	8
T BL 38+00S	1	68	4	107	.1	83	19	647	3.75	137	5	ND	3	29	1	2	2	81	.66	.083	9	85	1.35	169	.21	2	1.81	.06	.47	3	18
T BL 40+00S	1	90	9	132	.1	123	26	911	5.28	360	5	ND	4	33	1	3	3	112	.83	.107	11	143	2.21	230	.25	2	2.53	.06	.67	5	106

APPENDIX II

STATEMENT OF COSTS

STATEMENT OF COSTS

* A work schedule breakdown follows on page 18.

Salaries:				
D. Leighton	4	days @ $250	$1,000.00	
E. MacKenzie	8	days @ $130	1,040.00	
J. Knox	8	days @ $130	1,040.00	
D. Howard	8	days @ $130	1,040.00	
25% contract expenses (WCB, CPP, UIC)			1,030.00	$ 5,150.00
Disbursements:				
Supplies (Neville Crosby)			$ 805.49	
(Deakin)			176.49	
Geochemical Analysis (Acme)			2,003.75	
Expense accounts (mainly groceries, meals and accommodation)				
D. Leighton	$1,020.57			
E. MacKenzie	413.31			
J. Knox	1,191.88		5,034.94	
Truck rental			500.00	
Telephone			4.93	
Accounting			125.00	
Photocopies and postage			76.50	
Drafting and report preparation			500.00	6,817.92
				$11,967.92

NAME	RATE	MONTH	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Time Total
Eric MacKenzie	$130/day	May 87																					X	X	X	X	X	X	X	X				8D
John L. Knox	$130/day	May 87																					X	X	X	X	X	X	X	X				8D
David Howard	$130/day	May 87																							X	X	X	X	X	X	X	X		8D
D.G. Leighton	$250/day	May 87																						/	X	X	X	/						4D
Total chargeable																																		

Total paid_____ Prepared by_____ Authorized by_____

Cheque no._____ Date_____

CARPENTER LAKE

C.P.
C.P.

RAY I CLAIM

RAY II CLAIM

LINE OS

1S
2S
3S
4S
5S
6S
7S
8S
9S
10S
11S
12S
13S
14S
15S
16S
17S
18S
19S
20S
21S
22S
23S
24S
25S
26S
27S
28S
29S
30S
31S
32S
33S
34S
35S
36S
37S
38S
39S
40S

CABIN

CABIN

LINE G

LINE F

APPROXIMATE LIMIT TO ROCK BLUFF AND TALUS

BRISTOL FRACTURE ZONE—LOCATION APPROXIMATE

BENBOE FRACTURE ZONE —LOCATION APPROXIMATE

RAYMOND CLAIM

LINE E

LINE B

LINE A

LINE C

LINE D

BENBOE WORKINGS

BRISTOL WORKINGS

AREA OF BRISTOL ORIENTATION SURVEY -SEE FIGURE 3

N

LEGEND

PERIMETER TO TOMMY CREEK PROPERTY

PORTAL

GRID LINE WITH SAMPLE SITE (number corresponds to gold in soil in ppb)

14S

ACCESS ROAD

PROJECTED BRISTOL FAULT STRUCTURE BASED IN PART ON AIRPHOTO INTERPRETATION

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,367

GEOLOGICAL ASSOCIATION OF CANADA
D. S. LEIGHTON
FELLOW

SCALE

0 100 200 300 400 500 metres

VORTEX-EQUINOX JOINT VENTURE

GEOCHEMICAL SURVEY RESULTS
GOLD IN SOILS
TOMMY CREEK PROPERTY

BEATY GEOLOGICAL LTD.

DRAWN J.L.K., G.R.	DATE OCT. 1987
SCALE 1 5000	FIGURE 4