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GEOPHYSICAL SURVEYS

BAY PROPERTY (BAY 1, 2, 5-7, 11-16)

KAMLOOPS MINING DIVISION,

BRITISH COLUMBIA

NTS 82M/4₩

FILMED

51° 06 1/2 N, 119° 46'W.

Owners: COMINCO LTD. and WESTMIN RESOURCES LIMITED, KIDOCBEEK MINES LTD.

Operator: KIDD CREEK MINES LTD.

September 4, 1987.

G.A. Hendrickson, P.Geoph.

GEOLOGICAL BRANCH ASSESSMENT REPORT

16,564

TABLE OF CONTENTS

Introduction	• •	Page 1.
Location Map, (Fig. 1)	• •	Page 2.
Personnel	• •	Page 3.
Equipment	••	Page 3.
Data Presentation	• •	Page 4.
Survey Procedures	• •	Page 5.
Discussion of the Data	••	Pages 6, 7, 8.
Conclusion and Recommendations	••	Page 9.
Statement of Qualification	••	Page 10.
Cost Statement	••	Page 11.
Certification	••	Page 12.
APPENDIX:		
Grid Outline, (Fig. 2)	••	Pocket 1.
H.L.E.M. 3555 Hz Plan (Fig. 3	••	Pocket 2.
H.L.E.M. 888 Hz Plan (Fig. 4)	••	Pocket 3.
Filtered V.L.F. Plan (Fig. 5)	••	Pocket 4.
Total Field Magnetic Profiles Plan (Fig. 6)	• •	Pocket 5.
Total Field Magnetic Contour Plan (Fig. 7)	• •	Pocket 6.
Gradiometer Profile Plan (fig. 8)	• •	Pocket 7.
Filtered V.L.F. Sections (Cross Lines)	• •	Pockets 8, 9 & 10.
Filtered V.L.F. Sections (Tie Lines)	• •	Pocket 11.

Introduction

On behalf of Kidd Creek Mines Ltd., a division of Falconbridge Limited, Delta Geoscience Ltd. conducted ground geophysical surveys on the Bay property. This property is located in the Adams Plateau area of south central B.C., approximately 65 kms. northeast of Kamloops (fig. 1). The nearest settlement is Barriere, approximately 26 km. west of the survey area.

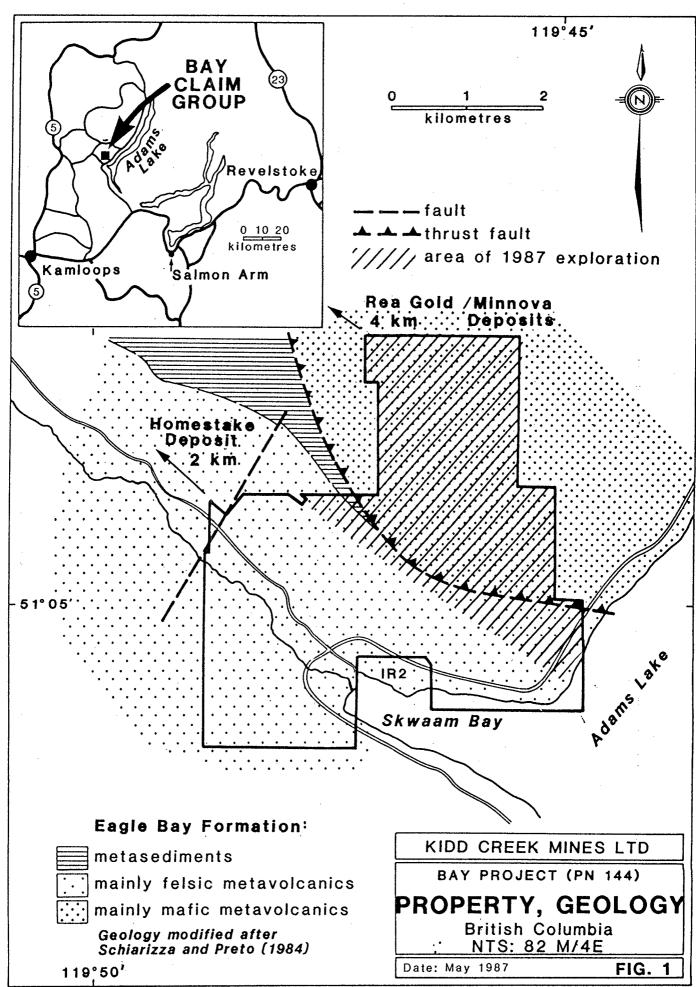
The geology of the survey area is described in preliminary map #56 produced by the B.C. Ministry of Energy, Mines and Petroleum Resources. This map shows the survey area to be underlain by rocks of the Eagle Bay formation. The rocks are described as being "medium to dark green calcarious chlorite schist and fragmented schist derived largely from mafic to intermediate volcanic rocks; lesser amounts of limestone and dolostone, minor amounts of quartzite, grey phyllite and sericite quartz phyllite." General geology underlying the Bay property is shown on Fig. 1.

The exploration target is volcanogenic massive sulphide deposits.

Ground geophysical techniques included horizontal coplaner loop electromagnetics, V.L.F., magnetic and gradiometer surveys. Approximately 70 kms. of grid lines were surveyed during the period July 4 to July 23, 1987, (Fig. 2).

Frank Hassard, a senior geologist for Falconbridge Ltd., was the client representative. Grant Hendrickson, a senior geophysicist for Delta Geoscience Ltd., supervised the survey.

Room and board for the crew was obtained at the fishing camp located on the west end of Johnson Lake, which is situated near the north side of the survey area.



Personnel - Delta Geoscience Ltd.

Robert Wilson-Smith - Junior Geophysicist Dean Truant '- Junior Geophysicist Eric Hards - Junior Geophysicist (Crew Chief) Grant Hendrickson - Senior Geophysicist (Supervisor)

Equipment

- 2 Apex Parametrics Maxmin 1+ Electromagnetic Systems
- 1 Scintrex I.G.S. system configured as a VLF/MAG/GRAD.
- 1 Scintrex MP-3 base station magnetometer
- 1 4x4 truck
- 1 H.P.110 field computer, complete with disc drive and printer.

Data Presentation

Stacked profile plans of the filtered V.L.F., magnetics, horizontal co-planer loop electromagnetics and gradiometer data are presented at a scale of 1:5000.

The magnetic data is also presented as a contoured plan with the contour interval at 50 nanotesla.

Separate profile sections of the V.L.F. data are also given with the Fraser and Hjelt filtered values posted below the profiles. The scale of these sections is 1:2000.

Fig.#3 - H.L.E.M. 3555Hz. Plan. Fig.#4 - H.L.E.M. 888Hz. Plan. Fig.#5 - Filtered V.L.F. Plan. Fig.#6 - Total Field Magnetic Profiles Plan. Fig.#7 - Total Field Magnetic Contour Plan. Fig.#8 - Gradiometer Profile Plan.

Survey Procedures

Falconbridge Ltd. personnel ensured the grid was established prior to the arrival of the geophysical crew. Grid lines were orientated to the northeast to cross the expected strike of the geology at right angles. Line separation was 100 metres with a station separation of 20 metres horizontal. Portable inclinometers were used to properly slope chain.

Horizontal Co-Planer Loop Survey:

The coil separation was set at 160 metres. Two frequencies, 3555Hz and 888Hz, were used to excite ground conductors. The slope chaining information was subsequently used to keep the coils co-planer and to calculate the slope correction for the in-phase data.

Magnetic and Gradiometer Survey:

A base station was established at the fishing camp located near the west end of Johnson Lake. A base station standard of 57500 nanotesla was assumed for this survey. All of the magnetic data was corrected for the diurnal variation of the earth's magnetic field thru the use of the base station. The base station sampled the magnetic field every 30 seconds.

The gradiometer and magnetic measurements along the survey lines were taken with the sensor 2.5 metres and 3.5 metres above the ground. Readings are accurate to the \pm 1 nanotesla range.

V.L.F. Survey:

Three components of the V.L.F. field were read at each station: the vertical in-phase, vertical quadrature and horizontal field strength.

Data along the cross lines was generally taken using the Annapolis V.L.F. station transmitting at 21.4 khz. The Cutler, Maine station (24.0 khz) was substituted on days when the Annapolis station was off. Both these stations were approximately on strike with the expected northwest strike of the geology and structures. The Seattle station (24.8 khz) was used for the two tie lines, 2000N and 3000N, in an effort to detect any prominent northeast-striking cross structures.

Discussion of the Data

Horizontal Co-Planer Loop Survey:

The large coil separation (160 m) and the two high frequencies, 888 hz and 3555 hz, were used in an effort to look deep (approx. 80 metres) for relatively poor conductors.

A study of the data shows that there is a fair amount of noise in the in-phase data. This noise is more prevalent in the 3555 hz in-phase data. There are two main reasons for this noise: 1) the largest source of noise is due to inaccurate chaining. Chaining error responses are similar in shape and amplitude for both frequencies, thus are easily recognized.

2) geological noise from weakly conducting bedrock and overburden.

The out-of-phase or Quadrature data is generally less noisy and detected several anomalies arising from weak bedrock conductors. The axis of these anomalies, shown as dashed lines on the 3555 hz plot, were best detected by the 3555 hz quadrature data. The lower frequency 888 hz, attenuated the responses. This fact, plus the poor in-phase response, clearly indicates that conductivity is poor at best (approx. 1 mhos). The low amplitude of the responses makes accurate dip and depth determinatations unreliable, however it is clear the conductors are near surface (<15 metres?).

There is no correlation between magnetic anomalies and horizontal loop conductors. This fact indicates conductivity is not due to magnetic minerals such as pyrrhotite.

There is an excellent correlation between strong V.L.F. responses and horizontal loop conductors, however, there remains many V.L.F. responses with no H.L.E.M. response. The H.L.E.M. helps to point out the zones of best conductivity thickness.

The partially covered H.L.E.M. anomaly on the extreme south side of the grid is quite a bit stronger than any of the other H.L.E.M. anomalies. Unfortunately, this conductor could not be completely surveyed due to topography problems.

V.L.F. Survey:

The V.L.F. survey has revealed numerous conductors. The Fraser and Hjelt filters help to understand the spatial position of conductors, both along strike and downdip.

The west central part of the grid has fewer conductors although the conductors present appear stronger and correlate well line to line. The correlation is excellent on the far west side of the grid, where strong V.L.F. responses indicate structures and/or possible sulphide zones.

The numerous V.L.F. conductors on the east central side of the grid makes correlation between lines difficult, except for the strongest anomalies. The most likely reason for the increase in the number of V.L.F. anomalies to the east is a change in the geology to a bedrock lithology that is weakly conducting/and/or badly fractured.

There is a better correlation between V.L.F. anomalies and magnetic anomalies than with the H.L.E.M. and magnetic responses. However, in general, the correlation is still poor. By over-laying the V.L.F. and Magnetic plans, one can see which V.L.F. responses are coincident with magnetic anomalies. The general lack of correlation again suggests conductivity is not related to magnetic minerals. There is one very strong V.L.F. response in the northwest corner of the grid that is coincident with, or flanked by a strong magnetic response (line 39W at 37+40N).

V.L.F. anomalies in areas of felsic volcanics or correlating with geochemical soil anomalies can be examined further by studying the Hjelt filter data. The areas of high current density (highest positive values) should indicate the dip of the conductor. The Fraser filter profile will generally be skewed in the direction of dip, if the dip is less than 75 degrees. In general, dips appear near vertical.

The presentation of the Fraser filter values as a series of stacked profiles, allows one to quickly see which anomalies are continuous and observe the relative strength of anomalies. In conjunction with the other data, one has the best chance of correlating the right anomalies from line to line.

Magnetic Survey:

The magnetic survey has shown that the lithology underlaying the west central part of the grid (near Bay Lake) has a low magnetic susceptibility. Low magnetic susceptibility is typical of felsic volcanic rocks, however is also typical of sediments. The bedrock to the north and south sides of the grid has a low magnetic susceptibility, however appears very amenable to containing numerous narrow magnetic horizons, possible mafic dikes or sills. The lithology to the east side of the grid also has numerous narrow magnetic horizons, but more importantly, contains broad magnetic units that could be andesite flows or gabbro intrusions.

The narrow magnetic responses indicate that the magnetic horizons are thin and near surface. The dip direction of the magnetic horizons is variable, however generally is quite steep.

The magnetic contour patterns, especially the similarity of the pattern to the north and south, suggests the possibility of the same horizon being repeated either thru thrust faulting and/or folding. A copy of the magnetic map on the adjoining property to the west would be helpful, if available.

Gradiometer Survey:

The magnetic gradiometer survey is a useful adjunct to magnetic surveying. The gradiometer acts like a filter, in that it enhances local near surface anomalies at the expense of long wavelength regional anomalies. The rate of fall-off of the magnetic field is much higher for local sources than for regional sources and therefore a higher gradient can be recorded over local sources using sensors one metre vertically apart.

A study of the gradiometer profiles will show an enhancement of the narrow magnetic anomalies. The broad magnetic responses in the east central part of the grid have been descriminated against in the gradiometer data.

A useful feature of the gradiometer data is that it allows a simple calculation to be made for the depth of an anomaly (assuming a dipole field):

d = -3 (total field anomaly)
gradient anomaly

Conclusion and Recommendations

The horizontal co-planer loop and V.L.F. surveys have revealed several interesting bedrock conductors that deserve further follow-up. These conductors should be correlated with the detailed grid geology and geochemistry.

Conductors are generally near enough to surface to expect some success from a trenching program.

The magnetic surveys have given useful information on the nature of the geology underlying the grid. The next step is to fit the magnetic data to the detailed geology of the grid. This step should allow one to extend the mapping into overburden covered areas. The numerous narrow magnetic anomalies have also helped to indicate that the bedrock surface is not deep.

In areas of promising geology and geochemistry, it may help to further evaluate the multiple V.L.F. responses with a limited test I.P. survey to obtain some information on the sulphide content of the conductors. Pyritic argillites may however rule out any hope of discriminating conductors with I.P.

The next phase of exploration should concentrate on finding the sources for the coincident V.L.F. and H.L.E.M. conductors.

Grant A. Hendrickson, P.Geoph.

Statement of Qualification

Grant A. Hendrickson

- B.Science, U.B.C. 1971, Geophysics option.
- For the past 17 years, I have been actively involved in mineral exploration projects throughout Canada and the United States.
- I am a registered Professional Geophysicist with the Association of Professional Engineers, Geologists and Geophysicists of Alberta.
- I am an active member of the S.E.G., E.A.E.G., and B.C.G.S.

Grant A. Hendrickson, P.Geoph.

COST STATEMENT

BAY PROJECT - EXPENDITURES JULY 4 - SEPT.15, 1987.

GEOPHYSICS

<pre>Geophysical Surveys: (Daily rate includes wages for 1 geophysicist, two technicians, 4x4 vehicle, field computer, Maxmin II+, VLF-EM, base station and field magnetometer and gradiometer) Surveys - 18 days @ \$925. 2 Travel Days @ \$647.50. Interpretation & Report: 7 days @ \$300.</pre>	\$ 20,045.
Mobilization & Demobilization: Meals & Gas	\$ 150.
Camp Costs: Cabin(s) at Johnson Lake Fishing Resort for 3 weeks; meals & groceries	\$ 1,720.
Drafting and Maps:	\$ 400.
Total Geophysics:	\$ 22,315.

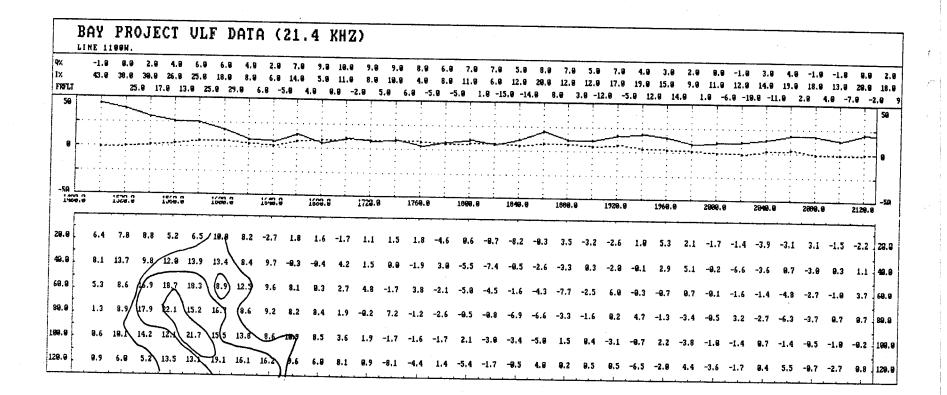
CERTIFICATION

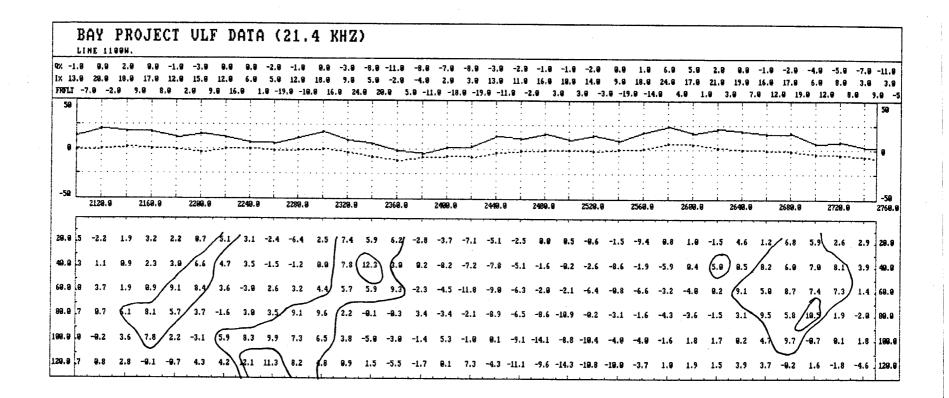
I, Franklin R. Hassard, of Burnaby, British Columbia, do hereby certify that:

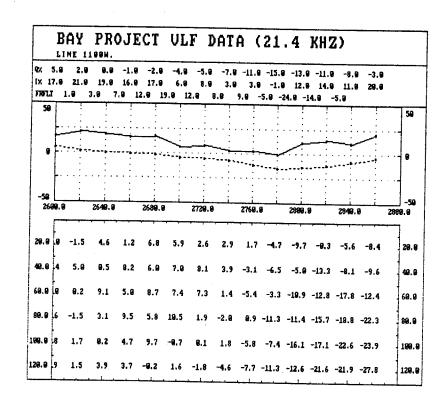
- I am a Senior Exploration Geologist with Falconbridge Limited at #701, 1281 West Georgia Street, Vancouver, B.C., V6E 3J7.
- I am a graduate of the University of British Columbia, B.A. Sc. degree in Geological Engineering 1970.
- 3. I have practiced my profession for over 17 years.
- 4. I am a member of the Association of Professional Engineers of Ontario and a Fellow of the Geological Association of Canada.
- 5. Geophysical exploration during 1987 and the subject of this report by Delta Geoscience Ltd., was carried out under my general direction.
- 6. The costs itemized in the Statement of Expenditures are correct and were incurred on behalf of Kidd Creek Mines Ltd., a division of Falconbridge Limited.

Dated this twenty-fifth day of September, 1987, at.Vancouver, B.C.

Franklin R. Hassan NCE OF O

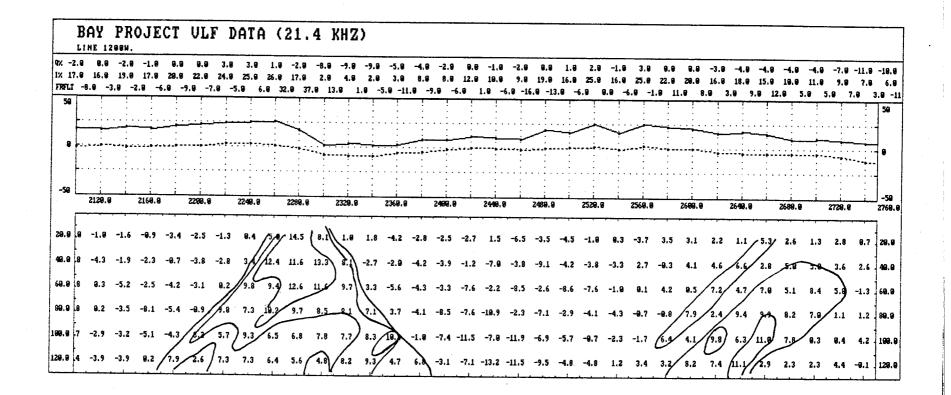


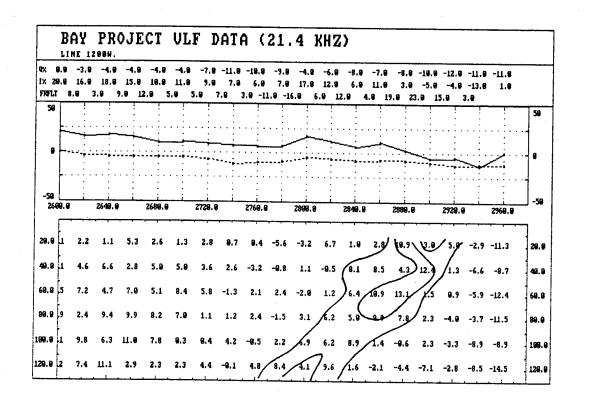


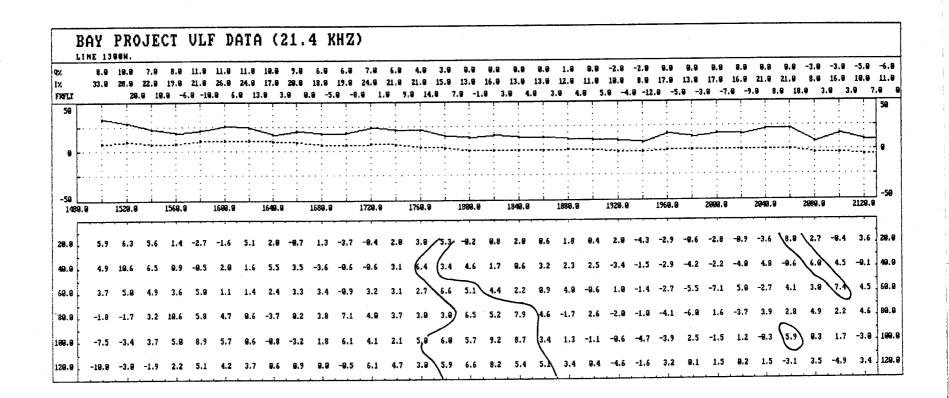


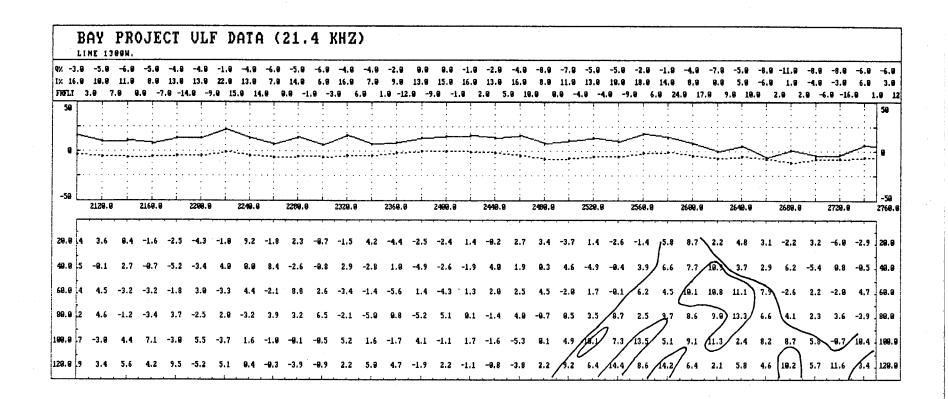
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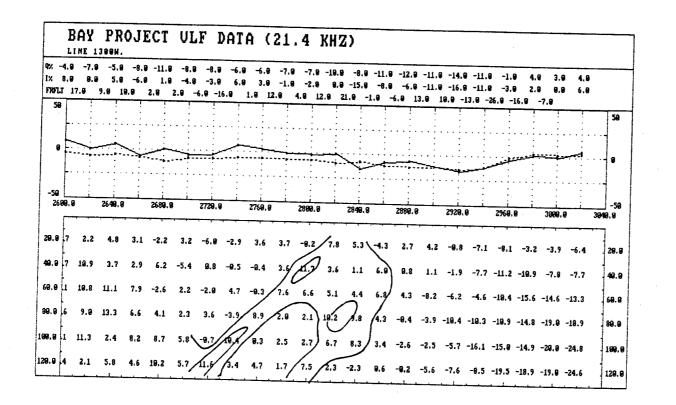
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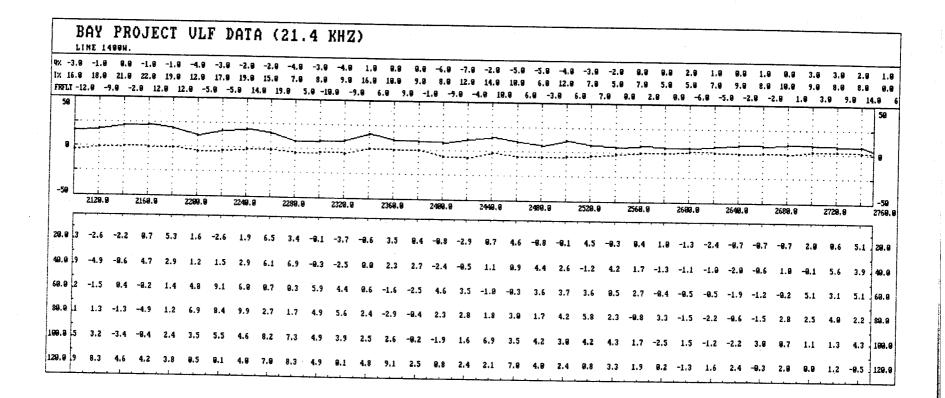


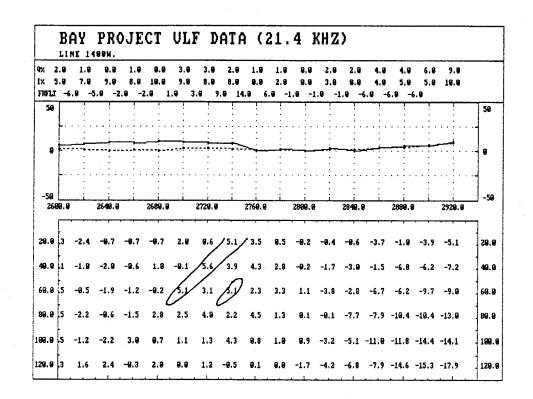




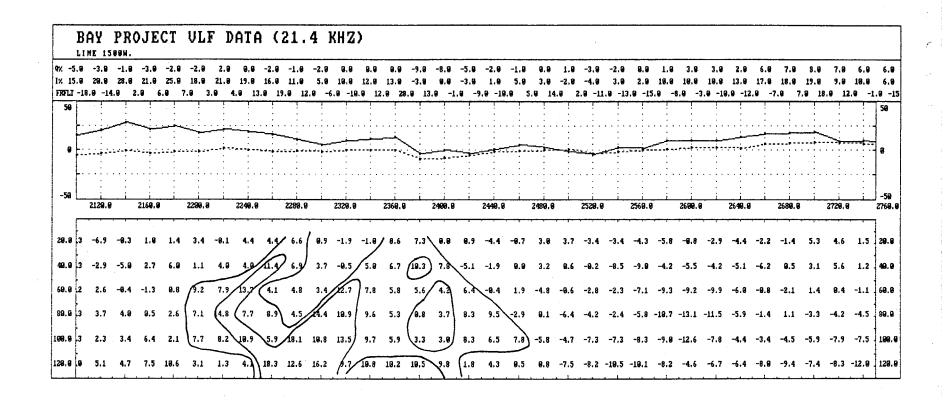


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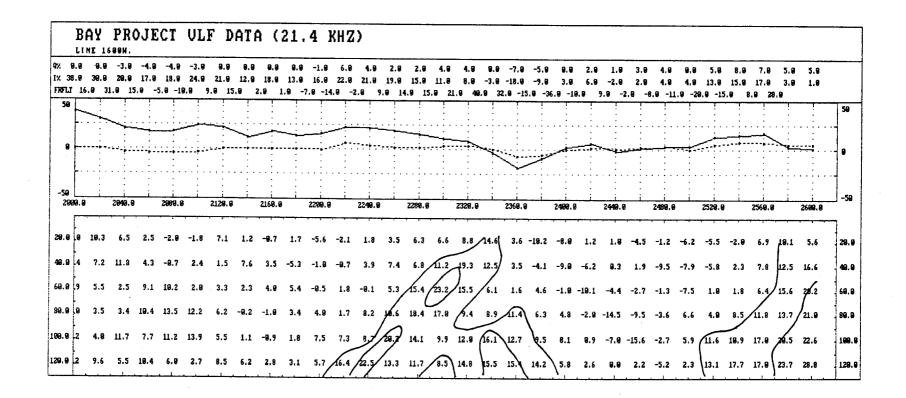


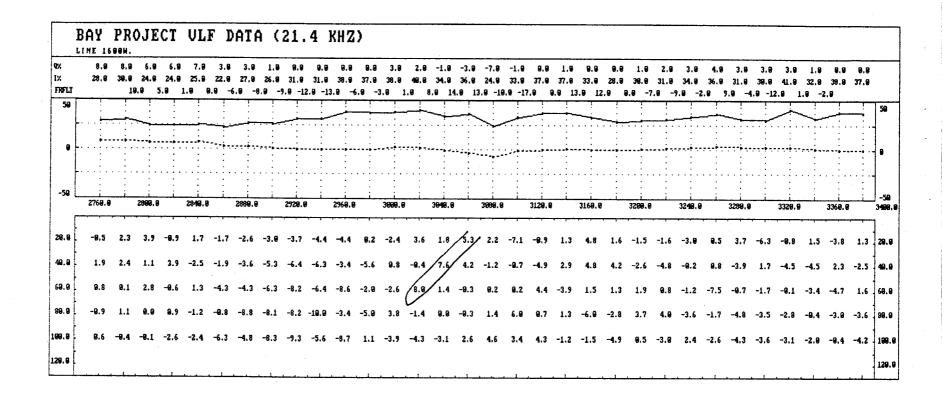
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a.e [1.3	8.9	8.0	7.7	ц.е	5 6.3	3 3.0	1.6	6 -2.9	-9.3	2.3	3.8	-0.6	-2.3	-3.9	-2.6	-3.1	-3.8	-19.9	-19.1	-4.1	-0.7	-4.1	6.0	6.8	1.0	7.8	8.0	5.4	2.8	9.3	-2.9
	4.4	7.3	8.5	12.4	12.3	8.9	9 1.5	9.6	5 4.4	9.1	8.4	-1.2	1.7	8.9	-1.2	-7.3	-5.4	-7.2	-8.8	-8.7	-3.5	-7.5	-9.5	4.6	6.4	4.6	6.6	13.6	4.1	-0.9	3.2	2.6
.9	5.6	6.3	11.4	11.9	9.2	2 7.5	5 6.7	3.8	3 2.2	2.1	-3.8	-9.5	0.3	3.5	9.i	-4.3	-9.2	-19.2	-7.7	-4.5	-12.2	-3.8	9.5	1.1	5.1	12.2	11.7	4.3	7.4	3.3	-8.3	3.7
	26	8.9	9.2	8.1	7.2	5.5	9 9.0	8.8	3.9	-1.3	2.5	-1.4	-1.2	-2.7	1.7	-4.4	-9.8	-9.5	-4.8	-11.4	-4,4	-3.2	-1.8	1.1	7.6	12.3	19,4	4.3	3.2	1	5.3	2.3
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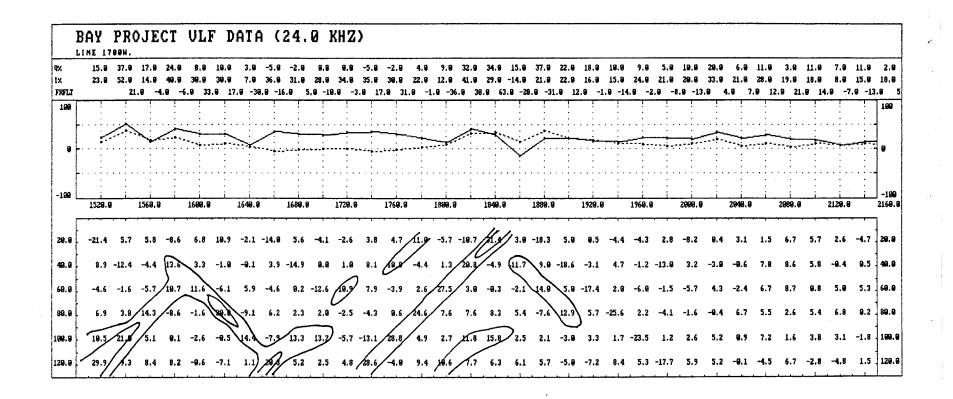


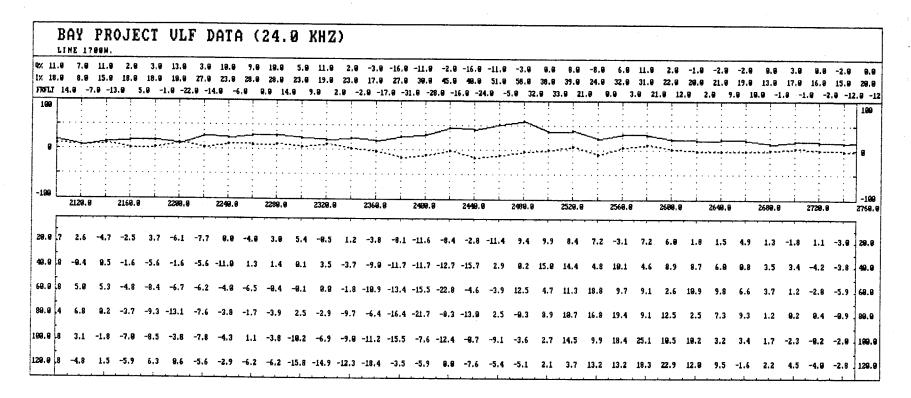
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9,9	34.	.6	1.5	-1.9	-7.8	-4.1	-4.7	-4.3	-3.2	1.6	-1.9	-3,4	-5.2	-3.4	1.5	-4.4	-9.6	-3.1	-4.5	8.9	2.8	9.2	-5.6	-9.4	-2.6	-2.8	3.4	3.4	-9.3	-2.1	218.
1.19	15.	.6	1.2	-5.6	-5.8	-9.5	-7.5	-7.2	-3.1	-4.5	-2.8	-6.8	-7.3	-4.9	-5.3	1.1	-6.7	-6.8	-2.5	-1.1	-9.1	-1.2	-9.5	-8.2	-3.6	1.4	8.9	1.8	1.2	-1.3	49.
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	3 -4.	.2	-4.5	-5.6	-6.9	-12.9	-9.7	-14.8	-19.5	-12.0	-7.8	-6.7	-6.9	-7.4	-13.8	-10.9	-8.5	-0.9	-5.6	-7.5	-3.4	-9.3	-3.9	-1.2	-9.8	-4.9	-3.1	-1.0	-2.4	1.4	89
_	9 -7.	.9	-7.5	-7,4	-7.8	-5.2	-13.1	-13.2	-28.2	-12.4	-12.2	-12,3	-8.0	-9.8	-19.9	-19.8	-6.5	-9.1	-7.7	-7.3	-19.1	-6.8	-6.8	9.1	-1.9	-3.7	-6.4	-3.5	-1.1	-3.4	19
.8																															

TPDIT 23.0 11.0 9.0 4.0 5.0 15.0 -1.0 -9.0 0.0 0.0 -1.0 <th< th=""><th>9% 1% FRFLI</th><th></th><th>7.0 26.9 2</th><th>25.0</th><th>19.0</th><th>21.0</th><th>) -4.0 14.0 4.0 -6</th><th>22.9</th><th>19.0</th><th>12.0</th><th>14.0</th><th>18.6</th><th>17.0</th><th>-5.9 15.9 9.8 -1</th><th>29.9</th><th>25.0</th><th>27.0</th><th>7.9 27.9</th><th>34.8</th><th>39.9</th><th>27 B</th><th>26 8</th><th>27 9</th><th>31 0</th><th>26.0</th><th>20.0</th><th>9,9 38,9</th><th>20.0</th><th>20.0</th><th>-4.0 17.9</th><th>-4.9 18.9</th><th>-3.8 24.8</th><th>1</th></th<>	9% 1% FRFLI		7.0 26.9 2	25.0	19.0	21.0) -4.0 14.0 4.0 -6	22.9	19.0	12.0	14.0	18.6	17.0	-5.9 15.9 9.8 -1	29.9	25.0	27.0	7.9 27.9	34.8	39.9	27 B	26 8	27 9	31 0	26.0	20.0	9,9 38,9	20.0	20.0	-4.0 17.9	-4.9 18.9	-3.8 24.8	1
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	89.9	-7.2	-6.4	-0.2	9.7	14.6	8.8	9.4	1.3	-4.2	-5.9	-10.6	-3.4	-6.8	-7.2	-3.6	-1.3	-4.6	-7.6	-3.0	-9.6	-6.0	-1.4	7.5	6.5	4.2	1.2	4.8	11.7	7.7	11.2	13.9	



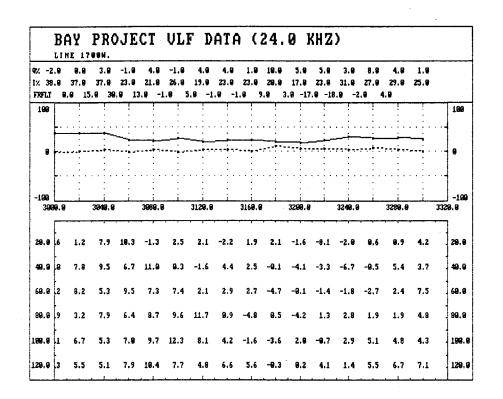


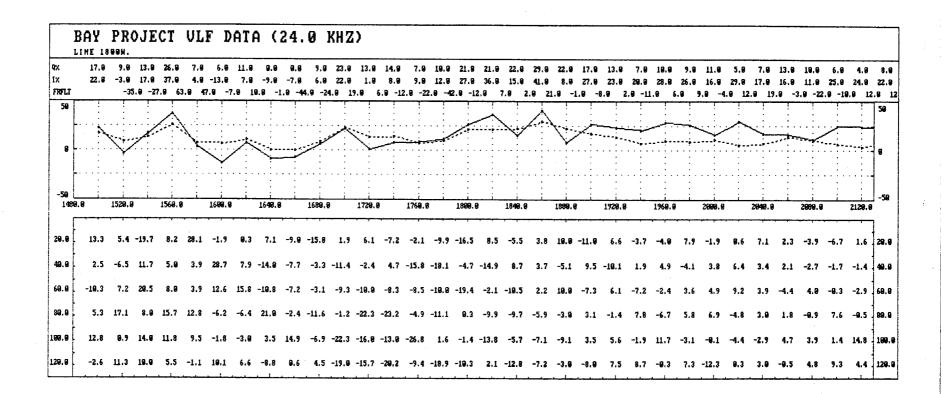


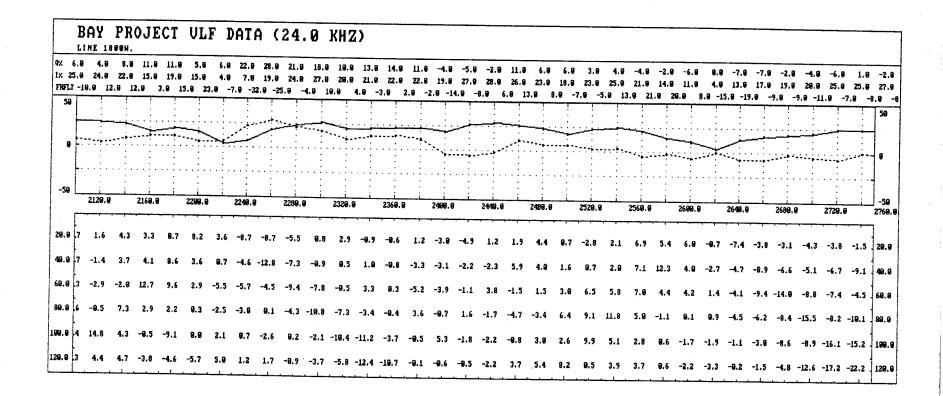


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9.9	A	1.8	1.5	4.9	1.3	-1.8	1.1	-3.0	-4,4	-2.9	0.5	-1.7	-3.0	-9.7	-4.8	-3.3	-1.2	-2.6	-1.8	-2.9	9.6	1.2	7.9	10.3	-1.3	2.5	2.1	-2.2	1.9	2.1	-1.6	-8.1	-2.9	29.
9.9	9	8.7	6.0	9.8	3.5	3.4	-4.2	-3.8	-4.3	-4.2	-4.7	-1.8	-2.9	-7.7	-4.6	-5.0	-5.1	-i.7	-2.3	-2.9	-1.9	7.8	9.5	6.7	11.0	0.3	-1.6	4.4	2.5	-9.1	-4.1	-3.3	-6.7	49.
e.e [61	10.9	9.8	6.6	3.7	1.2	-2.8	-5.9	-2.1	-6.2	-6.1	-4.7	-5.8	-5.7	-6.3	-4.7	-6.5	-6.8	-3.1	-2.6	5.2	8.2	5.3	9.5	7.3	7.4	2.1	2.9	2.7	-4.7	-9.1	-1.4	-1.8	69.
8.8							9.4	-0.9	-4.4	-5.0	-5.9	-77	-5.2	-5.9	-4.7	-8.4	-7.7	-6.9	-6.9	4.4	4.9	3.2	7.9	6.4	8.7	9.6	11.7	8.9	-4.8	8.5	-4.2	1.3	2.8	-
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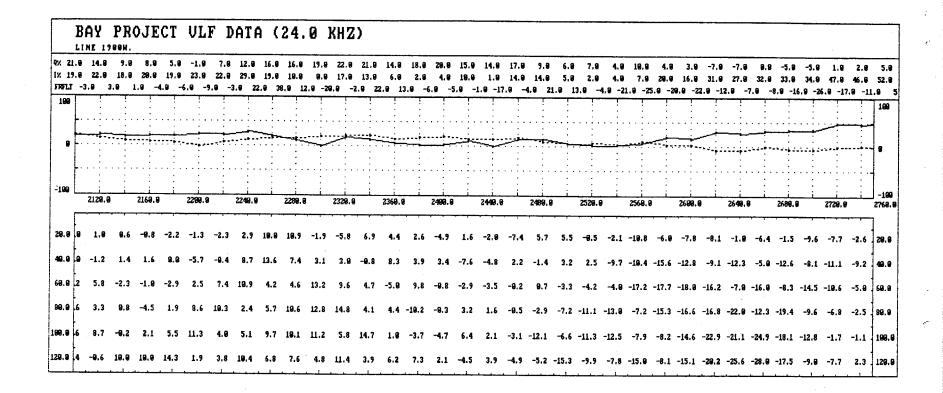


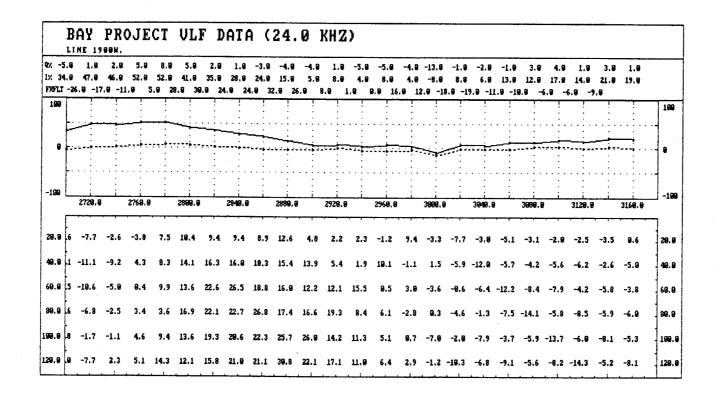


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29.	1]3 -3.	8 -1.	54,8	-2.2	-3.9	-8.4	-4.3	-2.8	2.4	7.8	-9.2	4.2	9.4	4.8	6.8	-3.1	-9.8	1,1	3.5	-8.9	8.7	-4.1	-3.6	-3.1	-6.0	29.6		
49.1	1 -6.	7 -9.	1 -4.2	-6.9	-8.7	-8.6	-9.9	-9.7	5.9	3.3	7.9	5.4	8.6	15.7	3.3	-2.9	-2.8	-4.0	1.3	4.2	-5.1	-5.4	-6.8	-8.1	-7.4	49.0		
69.0	8 -7	4 -4.	5 -9.7	-19.1	-12.1	-9.5	-3.5	-2.9	-3.9	6.5	19.9	14.7	12.6	2.6	4.0	2.8	1.6	-3.0	-5.3	-3.0	1.9	-6.4	-9.2	-12.2	-14.1	69.9		
89.1	5 -8.:	2 -10.	1 -11.2	-19.3	-19,8	-8.6	-4.7	-7.4	-1.1	5.3	11.6	14.9	9.4	1.4	3.8	6.8	9.4	-0.3	-6.9	-8.9	-4.9	-4.0	-19.5	-11.5	-15.1	89.9		
109.0	9 -16.1	1 -15.2	2 -15.3	-14.0	-19,2	-3.9	-7.5	-1.2	1.6	3.5	8.3	6.1	4.2	8.8	5.1	2.3	5.7	-3.9	-4.8	-11.5	-14.6	-19,1	-7.8	-14.0	-16.2	199.0		
129.9	6 -17,2	-22.2	2 -18.7	-12.1	-7.8	-19.5	-2.6	-1.3	3.4	7.5	-9.3	-0.9	6.3	6.6	7.8	4.9	-2.9	2.8	-6.9	-19.7	-16.4	-19.7	-15.3	-13.6	-18.7	129.9		
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X RFLI	35,0	8	16.0		21. 9.9		.3.0 -13.	22.0 0 -1	25.9 .9 2	11.9 2.9 -:	14.9 2.0 -3	24.9 1.9 -1(22.9 8.9 1		27.0 9.0 -28	49.9 1.9 -:	31.0 5.0 -7	41.0 7.0 :	37.9 3.9 7	32.0 .9 4	39.0 10 18		27.9 2.0 -17	48.8 .9 5	39.9).9 13	28.0 3.0 -4	29.0 .0 -1	33.0 .0 15	25.8 .9 18	22.9 .9 19	18.0 19 -1.	19.0 .0 -3	22.8 .0 3	
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9.9	14.1	9	19.5	-1.9	4.	2	8.4	-6.9	5.9	4.4	-6.9	-8.5	-0,4	6.5	-3.0	-13.9	-2.3	-1.6	-5.1	6.9	-1.6	2.9	7.9	-8.9	-0.5	6.1	8.4	-1.3	3.1	6.4	3.8	3.9	-2.9	1.9	29.
9.9	6.	8	12.2	12.2	-5.	8 -	4.9	8.3	2.2	-2.2	-6.8	-6.9	-3.1	-2.0	-3.6	-7.1	-15.2	-4.9	4.3	-5.3	7.2	5.3	-4.5	5.2	8.9	9.9	5.0	4.9	2.9	6.4	9.4	1.9	2.9	-1.2	49.
a.e	-0.	3	7.6	8.8	4.	0	8.9	-1.2	-3.2	-10.6	1.9	5.9	-9.7	-14.5	-4.1	-6.2	-8.5	-9.1	-8.1	6.4	2.9	1.7	3.9	1.6	5.0	-2.8	1.5	11.3	7.7	5.7	3.7	8.7	4.2	5.8	68.
9. G	-1.5	9	-2.4	9.1	13.	3	5.9	-8.9	-19.7	-4.2	-2.1	-1.6	-8.1	-8.8	-13.7	-8.3	-9.6	-8.8	-5.7	9.7	9.7	-9.4	7.2	4.4	-9.5	7.2	9.3	3.8	13.2	5.7	9.6	7.2	8.6	3.3	89.
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8.8	-13.	6 -	-11.9	1.1	5.	6	5.0	-3.8	-7.2	-3,9	-7.3	-18.1	-7.5	-9.8	-13.1	-8.2	-4.9	3.9	-2.9	-12.0	-1.1	5.8	6.3	4,8	2.0	4. (12.8	6.7	6.4	16.6	(10	7.2	4.0	0,1	100

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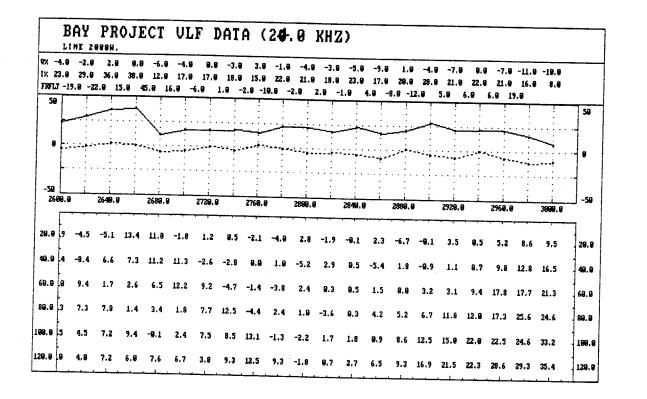


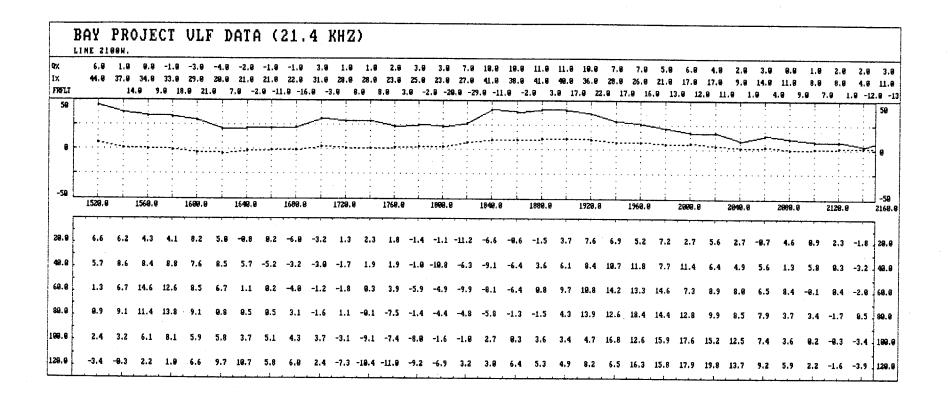


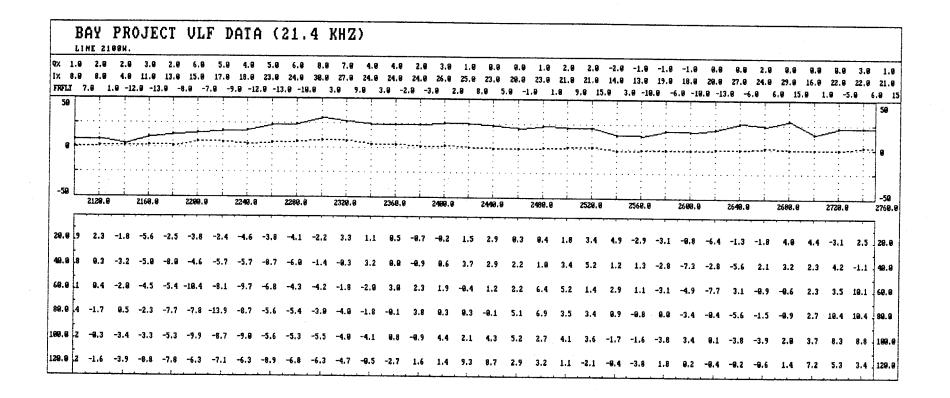
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	-1.3	-2.6	-18.9	-0.6	9.0	3.9	4.6	3.2	-1.7	-6.7	-4.6	-7.2	-7.9	-8.9	-7.6	-4.1	-1.4	3.2	1.0	4.5	5.7	8.6	4.6	19.9	12.5	8.9	14.4	15 9	12.4	3.0	-		
	2.7	-1.1	-4.3	1.6	4.7	12.1	2.0	8.2	-2.2	-2.6	-9.4	-19.6	-19.8	-6.3	-5.3	-8.4	-9.8	2.1	5.7	3.3	19.9	7.5	11.3	11.7	15.8	16.8	17.2	20.0	12 0				ł
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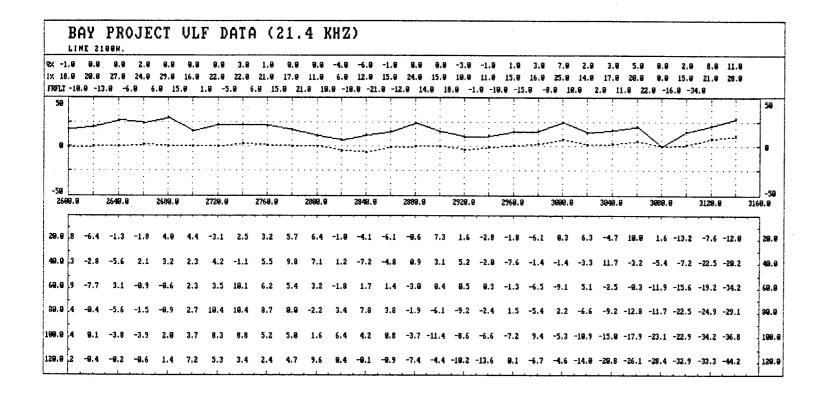
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	.9 -	-0.8	5.8	-1.1	-8.6	8.5	-9.1	-4.7	-4.9	-4.5	-9,4	-4.8	-6.4	5.9	0.8	-4,3	3.4	4.0	-4.3	-9.8	-4.5	-3.8	-2.7	3.4	3.5	-3.9	-4.5	-5.1	13.4	11.8	-1.8	1.2]
.9	2	5.4	-1.6	-2.4	-0.4	-7.4	-5.9	-4.2	-6.7	-6.5	-9.1	-4.8	8.9	-6.2	-1.0	3.5	-1.9	-2.2	-3.0	-7.3	-13.5	-7.3	9.9	3.3	8.5	-3.4	-8.4	6.6	7.3	11.2	ш.з	-2.6	-2.8	-
.0	9	5.2	-3.6	-0.7	-8.9	-2.9	-11.9	-6.1	-3.7	-11.4	-11.9	-4.0	-7.1	-5.9	-2.6	5.3	-9,4	-19.9	-6.8	-8.7	-9.1	-6.4	-0.2	-2.6	-4.2	-5.0	9.4	1.7	2.6	6.5	12.2	9.2	-4.7	69
.9 (1	8	4.8	6.9	-1.8	-3.8	-4.4	-4.9	-9.9	-10.7	-9.1	-7.3	-19.6	-7.9	-1.6	9.4	-8.9	-5.6	-3.3	-12.9	-6.7	-2.4	-6.4	-11.8	-19.1	-6.5	8.3	7.3	7.8	1.4	3.4	1.8	7.7	12.5	89.
^ہ ا	4 1	9,7	7.7	3.6	-7.3	-7.5	-4.7	-11.8	-17.3	-2.9	-5,8	-19.2	-6.1	-1.8	-4.6	-8.9	-8.9	-5.0	-6.2	-9.4	-3,5	-7.1	~15.1	-17.6	4.4	3.5	4.5	7.2	9.4	-9.1	2.4	7.5	8,5	100
	1 6	9.7	6.1	1.2	-2.3	-6.9	-12.8	-9.7	-5.8	-15.0	-9 1	-9.6	-21	-7 9	_0 0									-9,4										1

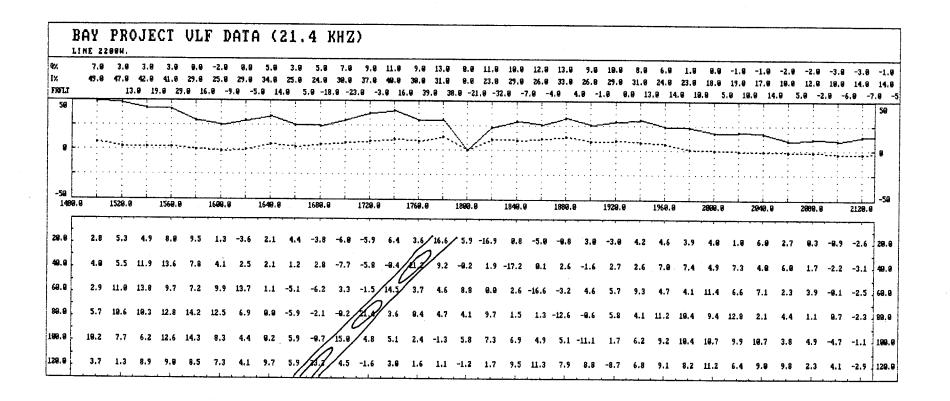
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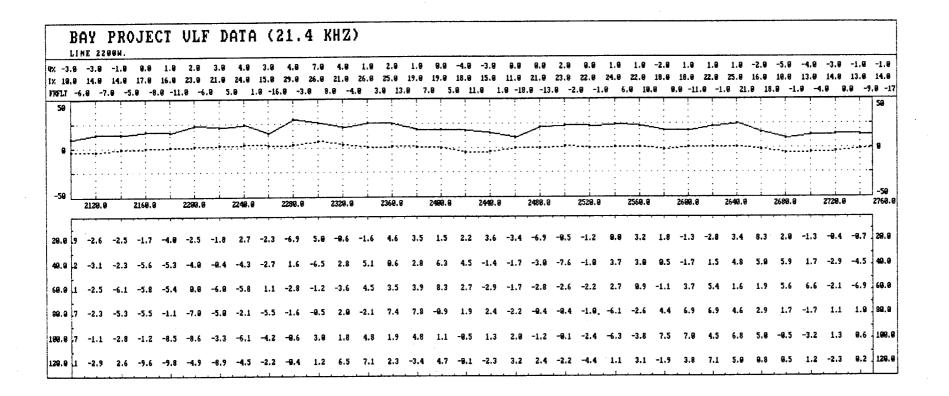


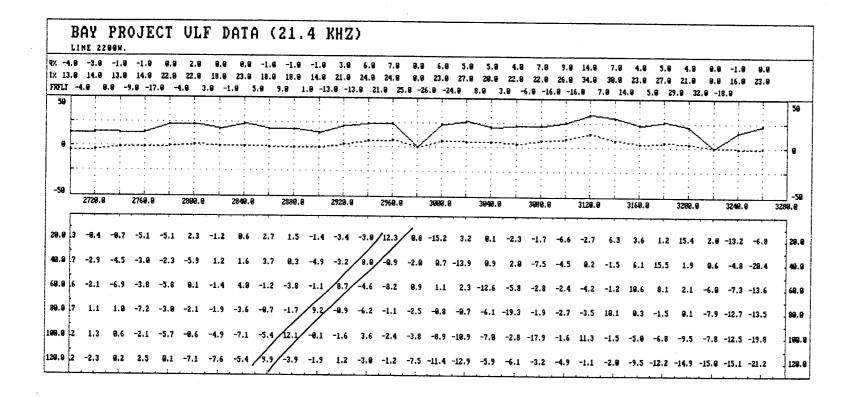




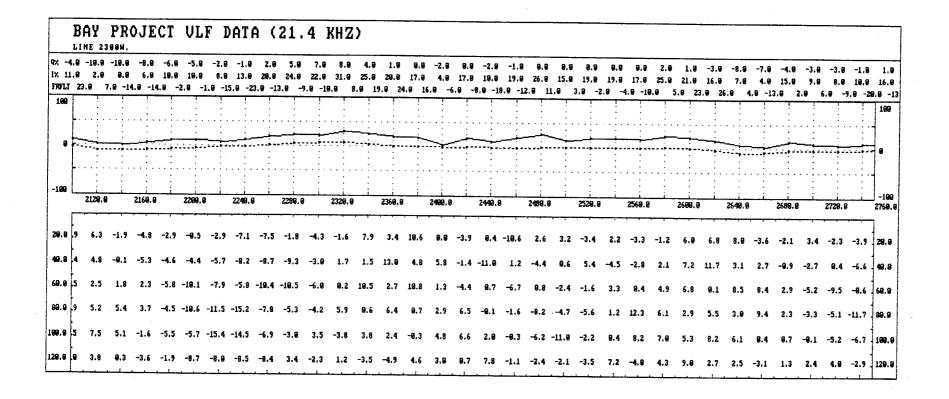


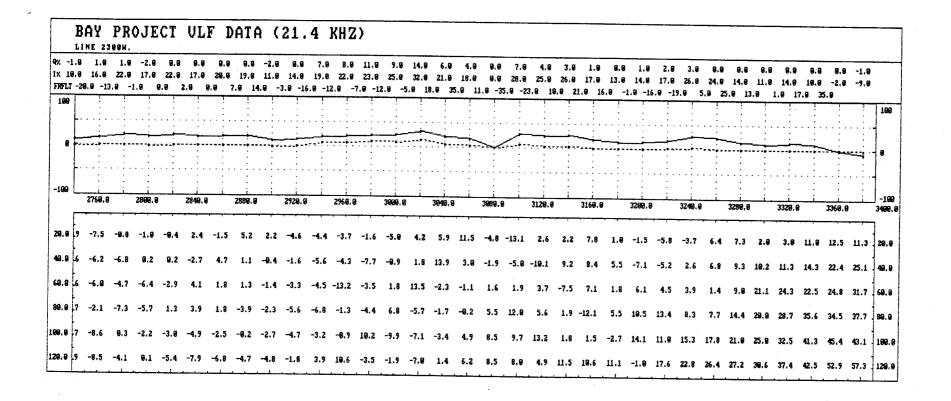


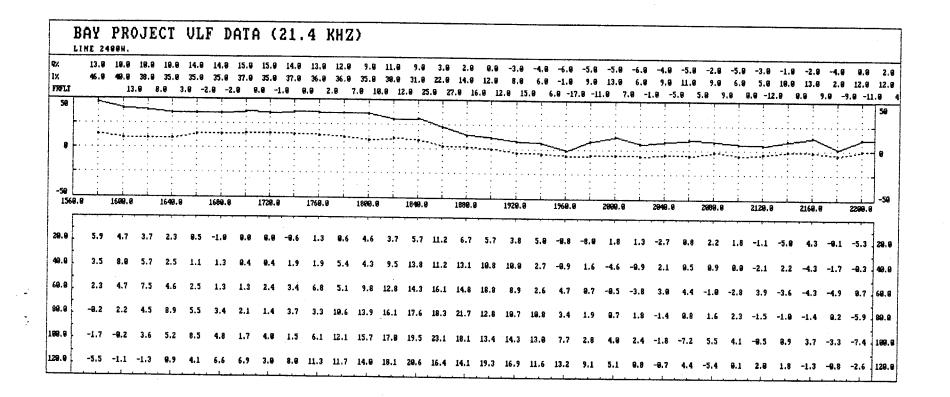


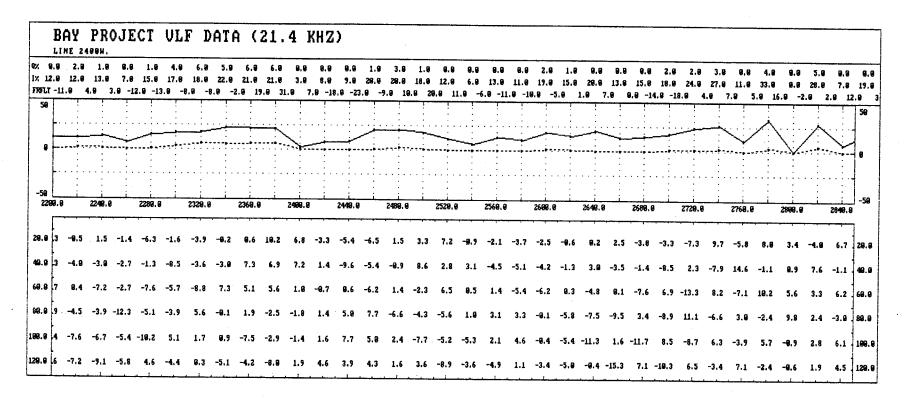


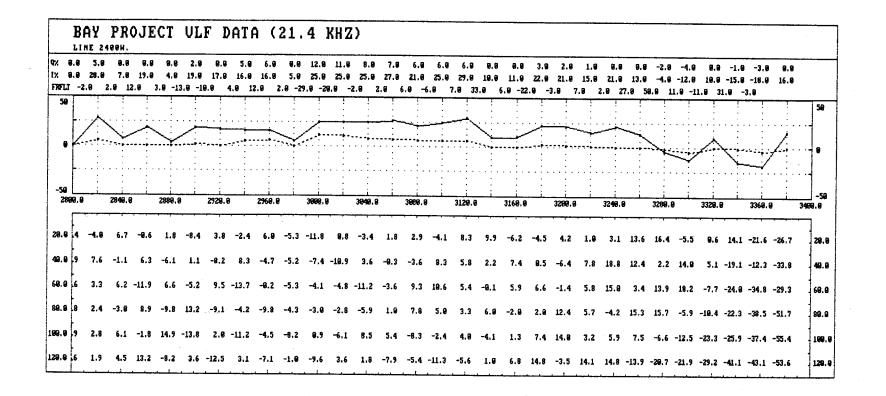
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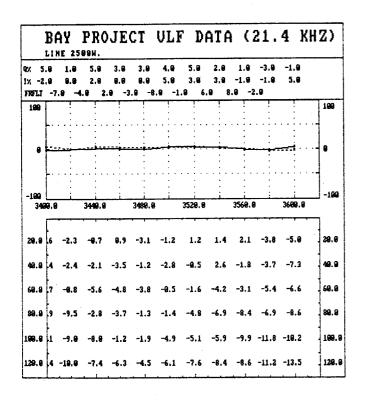


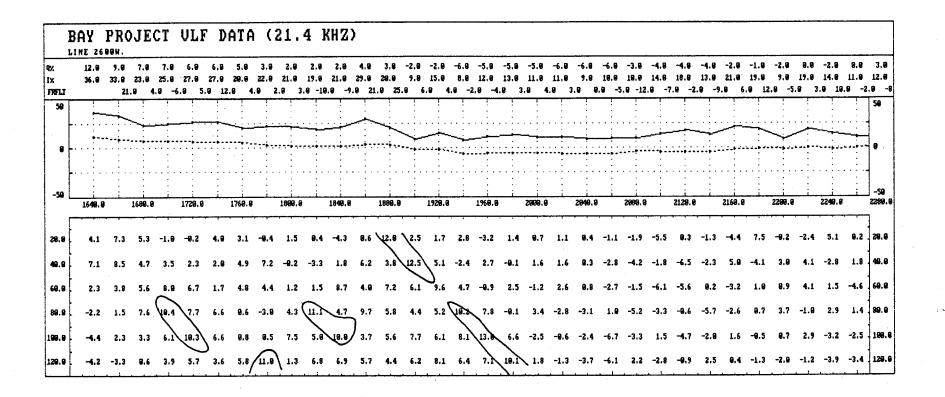


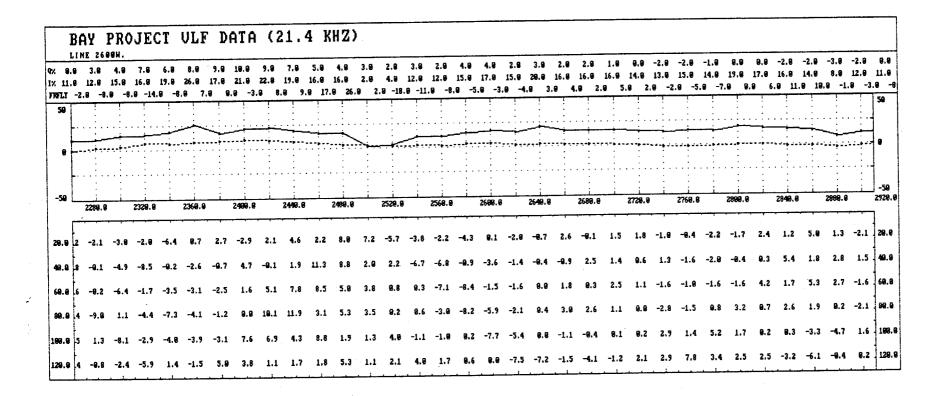
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49:9	5.2	9.9	18.8	3 11.8	19.9	9.6	18.5	12.2	15.5	15.1	-5.6	-1.5	-4.7	-19.8	2.1	8.3	7.6	7.9	1.8	1.8	-2.9	3,8	4.1	2.4	-8.3	-4.1	2.8	3.6	-3.8	2.0	-4.2	-3.9	49.9		
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69.9	5.4	9.9	14.3	12.3	10.1	20.1	16.1	28.6	18.9	9.8	9.1	-4.5	-6.7	-3.7	-4.8	11.3	5.3	3.3	3.9	3.2	5.2	-2.3	-0,3	3.6	٤.٩	2.7	W.1	-9.3	2.7	-2.0	-8.3	-0.3	56.0		
B8.9	1.9	7.7	18.9	13.4	25.5	19.7	23.9	21.8	11.9	10.1	8.3	5.2	-1.4	-0.2	3.1	-3.1	7.5	4.3	7.5	14.9	2.7	2.1	-3,0	-3.3	4.8	4.8	-1.9	-9.7	-1.0	-9.2	-3.6	8.2	89.0		
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88.8	8.3	5.1	9.2	2 25.4	24.7	26.5	24.3	13.3	12.5	16.7	3.8	18.2	8.3	4.7	4.0	-1.6	-3.4	8.7	8.7	8.3	19.2	5.8	3.4	-1.7	1.3	-2.9	2.7	0.4	-2.6	-2.4	8.2	-8.1	198.9		
29.9	1.2	3.6	18.5	5 18.8	25.3	29.5	16.7	15.8	13.2	6.7	12.6	7.9	14.2	11.2	-2.1	8.9	-8.3	1.2	9.1	5.2	9.3	9.8	8.7	8.9	-2.8	2.9	9,8	8.8	-4,4	-7.8	-6.4	-9.8	128.6		

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9.0	1 -	3.6	-2.6	-0,4	-1.5	8.4	-0,4	-6.6	2.9	5.8	5.4	-9,4	-5.2	-1.6	-3.3	-6.3	2.9	-1.1	-9.1	7.4	4.9	1.9	3.0	4.1	-3.6	-6.8	-2.9	5.8	0.5	-4.7	-3.9	-2.3	5.3	29
	9 -	1.0	-4.1	-6.6	8.9	-2.9	-6.3	0.1	-9.3	6.3	4.7	8.7	-3.7	-7. 7	-4.4	8.2	-6.3	8.9	6.3	3.5	5.9	7.4	6.4	-8.2	-2.2	-5.8	-8.9	0,3	2.7	-4.2	-7.9	9.7	1.4	40
.9	5 -	4.3	-3.3	-1.6	-6.8	-6.8	-3.7	-0.4	6.3	-2.6	1.9	4.2	-1.2	-7.4	-5.4	-7.9	-9.7	1.0	5.2	6.4	6.3	11.3	2.3	-2.8	-2.5	5.4	-3.3	-4.1	-4.7	-1.2	2.8	-3.8	-8.9	68
	2 -	8.8	-3.6	-5.8	-10.9	-4.8	-9.4	2.6	9.8	1.4	-2.2	9.4	-0.3	-1.3	-8.9	-7.9	-8.9	3.1	i.i	8.7	19,8	3.7	4.5	1.9	4.2	-9.8	-3.5	-8.9	-7.1	9.1	6.2	2.6	-2.6	88
			-19.6	-11.2	-3.3	-1.5	1.5	-8.5	-8.3	-8.1	-1.3	-7.8	-9.1	-2.2	-1.7	-2.9	-3.2	-9.8	4.7	5.6	5.8	4.1	2.5	19.3	3.1	-2.0	-7.8	-3.4	-2.6	-3.6	-9.2	4.4	4.3	10
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2 14.9	21.0	17.0	11.0	10.0	13.0	11.0	8.0	29.0	16.9	28.6	15.9	13.0	19.0	15.0	15.0	16.0	14.0	4.9	1.9	2.8	2.0	-6.9 - -1.9 -	11.0 -	-16.0 ·	-13.0	-13.9	-11.0	-2.0	-3.8	-2.0	8.8	2.0	8.0	
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2899.		2849.8		2889.0	· · ·	6768.8	, <u>.</u>		, 										,, ·						, <u>, .</u>	, <u>, , , , , , , , , , , , , , , , , , </u>	·				*	• • •	1	
28.8 9	-2.3	5.3	3.8	-8.1	-2.9	3.4	-10.9	-4.2	5.3	-8.6	5.8	2.6	-8.7	-2.5	9.6	9.8	7.2	7.8	2.1	1.7	3.8	7.7	9.1	1.7	-1.6	-1.1	-7,8	-5.2	-0.9	-2.6	-2.3	-9.7	28.9	
40.9	9.7	1.4	4.2	2.7	1.1	-19.4	-8.3	-4.7	-4.5	8.6	3.7	2.8	9.6	9.1	-1.6	7.7	19.9	9.9	7.5	3.8	7.8	10.9	9.4	7.1	-8.2	-7.9	-4.8	-5.2	-7.9	-3.4	-2.4	-2.1	48.9	
69.9	-3.8	-0.9	0.8	8.3	-6.4	-2.9	-7.4	-1.4	9.1	1.3	9.4	1.1	3.9	1.4	7.9	6.8	10.0	8.3	19.4	14.2	11.2	7.8	8.7	8.5	2.1	-3.6	-7.9	-7.4	-7.2	-4.7	-9.8	-5.6	60.9	
98.9 Z	2.6	-2.6	2.9	-9.1	1.6	-1.1	-1.0	9.9	2.6	-2.4	-2.2	9.9	3.9	11.3	9.0	4.7	4.4	8.4	13.9	19.8	16.9	19.6	6.9	2.4	2.7	2.0	-4.3	-8.9	-6.6	-7.9	-9.5	-2.8	89.9	2
99.9 Z	4.4	4.3	-11.0	8.1	-2.0	4.1	3.5	2.1	-1.4	8.6	-8.9	-1.8	13.4	8.4	10.2	8.9	8.3	11.1	17.3	15.2	16.2	13.9	5.8	3.1	3.2	1.1	-2.8	-6.7	-9.8	-19.1	-9.8	-8.8	199.9	
29.9 8	2.6	-5.4	1.6	-5.7	1.7	4.7	8.7	2.9	-0.9	-2.3	-1.1	2.8	3.0	14.9	8.1	11.6	14.4	16.6	14.3	16.0	14.9	9.4	9.5	2.9	-0.3	8.6	9.1	-1.1	-19.0	-11.4	-10.0	-7.4	128.8	
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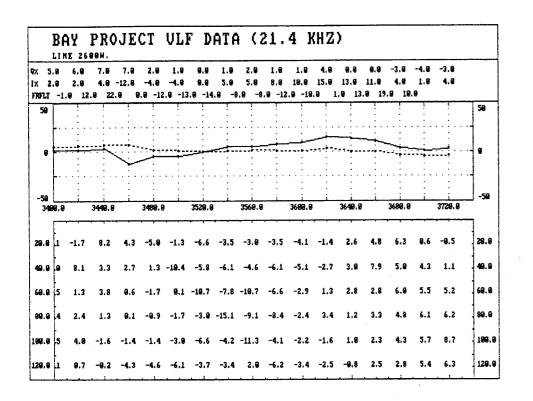




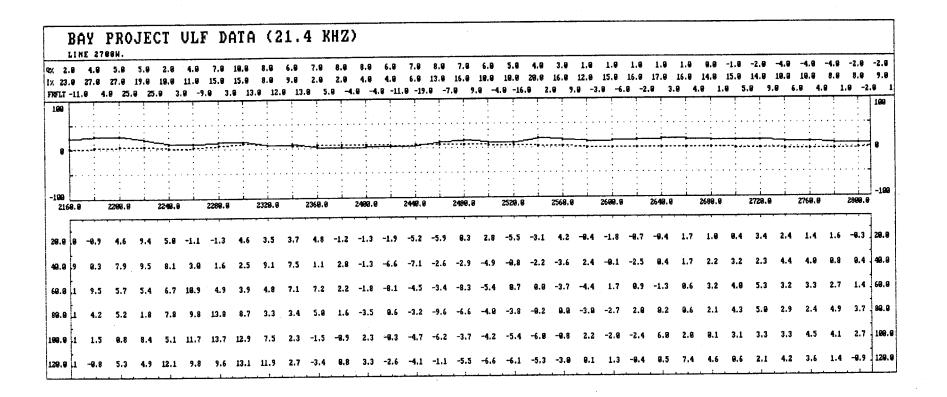


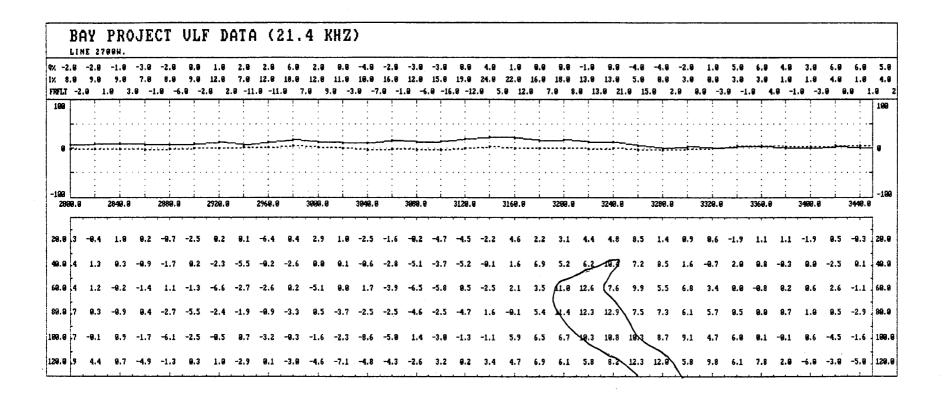
	а а ц		4.8 12.9	5.0 19.0	6.9 22.9	4.0 15.0	9.9 13.9	-1,9 13.9	0.9 17.0	-1.0 13.0	-1.8 6.9	-2.8 17.9	-3.0 11.9	8,0 23.0	-4.0 15.0	-4.6 18.8	-5.8 7.8	-4.0 6.0	-Z.0 13.0	8.9 3.9	0.0 4.9	2.0 4.0	3.0 8.9	1.9 -1.9	2.0 3.0	5.8 2.9	6.8 2.9	7.0 4.0	7.8 -12.9	2.8 -4.9	1.0 -4.9	0.9 8.8	1.9 5.0	2. 5.
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 	292	8.8		2968.0	<u>i</u>	3000.0		3040.0	·····	3080.0	k	3128.0	k	3168.8	ł	3200.0		3248.8		3286.9		3328.0		3368.0		3490.0	.1	3448.8		3480.0		3529.9		3566
9.8 µ	i −8	.2	-4.6	-5.5	2.1	4.2	1.4	-8.7	-9.6	5.6	-3.6	-2.8	-3.3	-2.3	3.7	3.3	8.7	-3.1	2.9	5.6	-8.6	3.0	2.8	-1.6	-1.6	2.1	-1.7	8.2	4.3	-5.0	-1.3	-6.6	-3.5	29.
9.8	i -5	.6	-5.7	-1.6	8.5	2.6	2.6	-9.2	3.8	-1.7	5.0	-4.4	-5.6	0.0	4.9	9.6	1.3	9.1	1.6	2.1	8.4	3.4	1.9	2.2	-9.3	-3.0	8.i	3.3	2.7	1.3	-19.4	-5.8	-6.1	49
e.e (5 -4	l.1	-4.1	-9.4	-2.9	-2.1	3.1	10.4	-0.7	1.9	-5.7	1.4	-1.3	1.1	7.0	-0.6	12.8	6.6	8.3	4.5	5.3	6.3	1.8	1.6	013	6.5	1.3	3.8	0.6	-1.7	0.1	-19.7	-7.8	60.
- F	i -0	1.3	9.2	-3.3	-2.5	9.2	3.5	3.3	7.2	-3.6	9.4	-2.8	5.5	4.2	-3.7	8.6	6.6	i1.9	9.9	11.2	2.1	1.5	4.8	-0.9	8.4	5.4	2.4	1.3	9.1	-9.9	-1.7	-3.9	-15.1	89
9.8 J																																		

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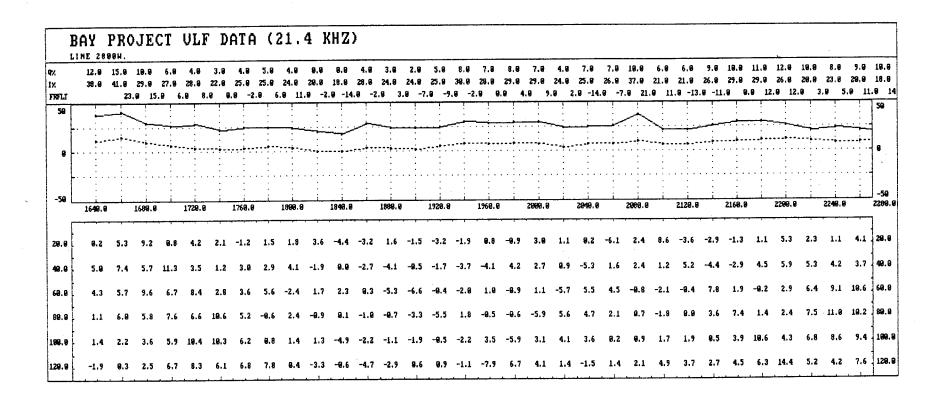
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29.0	4.1	6.4	9.1	6.5	6.7	5.5	2.8	1.4	-8.9	4.2	6.8	3.7	3.4	-8.4	6.8	-8.9	1.4	0.6	-4.2	3.4	-1.9	-2.2	8.7	-1.2	-1.9	-0.7	-3.1	-2.6	0.3	-4.0	-8.9	4.6	29.9
49.0	5.9	11.3	18.9	12.5	11.3	19.9	7.1	3.2	5.9	5.5	7.9	9.0	3.2	2.1	9.2	2.5	-9.2	-1.4	2.6	-4.8	0.4	-1.1	-3.2	-0.8	-1.7	-4.2	-2.4	-9.8	-5.9	-1.9	8.3	7.9	49.8
68.0	4.7	10.4	16.2	16.1	15.2	18.2	6.8	9.4	9.3	9,1	8.6	8.4	9.2	3.7	4.2	-0.6	-1.4	3.2	-2.3	8.9	-4.3	-8.7	-2.2	-3.1	-1.7	-1.7	-2.7	-6.6	-3.8	-1.1	9.5	5.7	68.8
89.0	5.9	19.6	14.5	17.7	14.4	12.9	12.6	10.9	12.4	9.1	8.5	9.8	8.0	12.2	4.2	1.6	2.5	-2.7	-9.3	-2.1	1.1	-2.1	1.1	-2.9	-5.8	-1.7	-6.4	-3.9	9.9	5.1	4.2	5.2	89.9
199.9						17.6																											
ļ																																	
L29.9	1.8	5.9	7.8	8.6	16.3	19.5	19.9	18.8	13.8	11.5	8.5	8.5	4.2	3.9	9.4	8.2	6.3	4.8	2.8	1.7	1.9	-3.0	9.5	-4.4	-3.9	-4.8	-3.5	5,6	2.4	2.1	-0,8	5.3	129.9





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		128.9	0 -3,6	9 -5.	2.	4 -:	8.9 -	3.5	-2.7	-3.3	-1.2	2.3	2.6	6.8	7,8	7.8	3.3	2.9	2.7	6.4	7.3	18.7	9.1	8.6	7.9	5.6	129.0			

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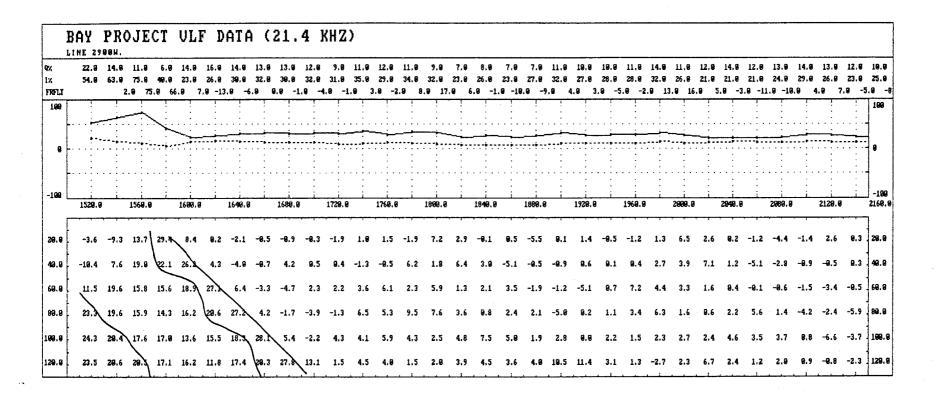
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-58 (_ 2249	i_	2289.	i	2328.1	i_	2368.6	<u>i</u>	2400.0	<u>i</u>	2448.8		2488.9	i_	2529.9	<u>i_</u>	2568.0	<u> </u>	2600.	<u> </u>	2640.9	i	2689.9	i	2729.9	<u>i_</u>	768.8	<u>i_</u>	2898.9	<u> </u>	2849.9	<u>i</u>	2880.9	_]-5 a
Γ			• •••						·	+				· · · ·		÷-,						····			,,				<u>~~ ~ ~</u>	÷	· ,		7
a.e	4.1	3.4	5,6	1.5	-1.7	-6,2	-3,8	-1.3	2.1	0.3	-8.2	-8.1	8,4	-1.4	-1.9	-8.9	-1.1	1.0	3.3	-2.8	-2,3	1.6	4.9	6.9	1.5	3.3	8,3	~3.7	-3.9	8.7	0,7	2.7	29
1.19	3.7	7.6	5.5	3.7	B.9	-3.9	-1.1	9.1	-9.6	1.9	9.1	-9.7	-i.i	-9.3	-2.7	-3.4	8,5	3.9	-9.5	9.2	-1.9	2.1	6.2	6.3	7.8	1.6	-9.1	-2.7	-2.9	-2.4	2.9	9.4	4
.e µ	19,6	4.6	5.4	4.4	1.2	8 .3	-1.7	-1.2	-0.6	0.4	3.1	-9.8	-2.5	-3.2	-1.6	8.1	1.9	-1.4	-8.7	8.9	4.4	3.2	2.7	9.8	6.8	4.5	-2.6	-1.2	-2.2	9.1	-2.5	-0.1	66
1. e [19.2	8.9	4.2	4.8	2.2	1.7	8.9	-1.5	-8.3	0.2	-1.4	2.1	-8.1	-1.4	0.8	1.9	-3.6	-3.3	-1.4	4.2	5.9	6.3	6.1	3.1	3.9	2.5	4.3	-9.4	1.7	-3.9	5.2	-4.2	86
1.0 -(5 9,4	8.8	5.1	3.3	5.7	3,3	2.9	-8.1	-1.4	-1,1	-9.1	-9.2	1.6	8.9	1.3	-2,6	-2.1	-2,0	1.7	4.0	4.7	7,1	6.6	2.1	-1.1	4.6	3.3	5.8	-2.1	-0,9	-2.4	-6.7	10
	7.6	6.7	8.3	6.5	4.3	6.3	4.2	3,8	8.6	-1.3	-2,5	-3,4	-8.1	4.1	-0.9	-1.7	-1.4	3.8	2.8	3.4	5.9	4.9	2.7	1.3	1.7	1.9	8.3	3.8	4.5	-1.3	-3.5	-2.0	112

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: 11.0	5.8	- 13,6	і 1.0 і Ц.0	14.0	18.6	14.0	16.0	16.0	22.0	27.9	- 20.1	8 1.8 8 19.0	16.0	9.1	8 11.0	R 10.0	5	0 4.0	20	1 6		1 1 0								7.9	7.8 9.0	••••	
59			-7.8	-9.9	1.0	2.8	- 9.9	8.0 -1	7.0 -1	5.8 4	1.0 : !	18.9 2	9.0 1	5.8	4.9	5.0	2.9	9.0	6.0	4.8	1.0	-5.0 -:	3.9	8.0	9.9 -1	1.0 -	3.8 4		j.0 -1	10.9 13.9 -4		2.9	6.0
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				شغیب ۱۹۹۰ مرد			÷							÷-		;		:			:					<u>.</u> .						· · · · ·	
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50 (2880.1	<u> </u>	2928.	i. 0	2968.		3899.0	i	319410.	i	3089.0	i_	3120.8	i	3160.	<u>i</u>	3288,		3240.	i	3280.	i	3329.8	i	3360.0			i.		<u>.</u>			<u>.</u>	_] -:
Γ	, . , .	· · · · ·	-, ,		-,,-			,	,	····	, .		,,			-,		;				3328.8	, <i>.</i> -	3308.8	, ,,	3469.6	e 	3440.0	·,	3480.0		3528.6	8 ~~
8.8 7	-1.1	-4.0	-9.1	-5.8	8,8	0,1	-2.2	-3.4	-6.1	-2.1	4.8	5.7	6.5	4.4	9.3	4.5	3.1	7 2.2	2.4	8,3	9.7	-2.7	8.7	3.Z	-3.6	-2.3	9.2	8.5	~4.9	-3.5	1.6	-9.3	28
•												(10.8																		-3.9			
F 1												· · ·	 																	-3.9			
	-2.0	• •										0.0	A0.0	16.1	_	8.8	4,4	1 6.2	6.6	1.5	3.4	1.4	-2.3	-1.7	0.1	2.5	-6.1	-4.7	-1.8	-9.7	1.4	1.9	60
														1			· ·													2.9			
1.8 7	-2.5	-1.3	8.2	-4.8	-6.7	-9,9	-2.8	-3.1	3.3	3.7	2.2	6.1	7.6	4.0	13.6	13.1	18.	5.8	5.7	6.9	2.4	1.1	1.9	2.Z	-2.1	-1.4	-1.4	1.8	-8.1	1.2	8.8	3.9	19
	-5.5	-4.9	-4.9	-5.5	-8.3	-3,3	-4.2	3.3	9.7	2.2	7.7	4.7	7.0	7.8	\ 11.6	45.2	11.3	п.,	9.2	3.2	4.6	4.7	2.9	-1.7	-2.8	-1.6	-2.3	2.2	5.5	-2.9	2.8	4.9	120
	<u>+</u>	<u> </u>	<u></u>			ىا		•l	م يغيب ا	•ł•	4		<u> </u>	<u> </u>	<u> </u>	· /· _	<u> </u>		<u>\.</u>	• l	- -	• - 1		- 4 4		<u> </u>	4 <u>-</u>						

9% 10.0 I% 5.0) 7.0) 3.0			•		-1.1 - 2.1	0 -3.0 0 1.0			-9.0 -1.0		-19.9 -8.9		-9.0 -9.0		-19.0 -13.0								-5.0 -13.0		-4.9 -6.9	
FRELT	-3.0	4.Ø	5.0 -:	L3.8 ·	4.0	2.0	6.0	14.9	2.0 -	4.0 1	1.0 1	7.0 15	.0	3.0 -3								1.0 -				7.0 -8		0,8	
58					!	!	!												!	!	:	:	:		:	:	:	:	50
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-58	; 0	3449.		3489.		3529		3560		3600.		3649.9	i	3680.0		3720.0	i_	3760.0	: i	3899.6		3848.1	: i	3880.0		3928.8	:	3960.0	-50
Г	 ,		· · · · · ·	P-				· • • • •	,,		,	-, -,	····		 ,	,	,		···						,	3766.10	,,	3700.0	
29.9 3	0.3	9.5	-4.0	-3,5	1.6	-0.3	3.1	5.5	i -3.0	2.8	5.5	4.2	5.4	-1,5	1.5	4.4	2.1	-1.1	-1.2	-3.2	-0.6	8.6	-2.6	6.5	4.1	-0.9	-3.9	-1.6	29.0
49.8	-2.3	-2.4	-1.2	-3.9	-3.5	5.4	5.7	8.5	i 5.4	2.7	7.0	10.5	3.5	4.5	2.4	4.1	4.2	0.9	-4.1	-8,9	-1.7	-3.1	0.5	8.9	-0.9	-9.1	-2.6	-6.9	49.8
68.9 5	-6.1	-4.7	-1.8	-8.7	1.4	1.9	1.1	6.3	6.4	19.6	5.6	3.0	10.4	7.7	7.6	1.8	2.3	1.1	2.9	-3.3	-4.4	-2.3	1.3	0.4	-3.0	-2.8	-2.9	-5.1	68.8
89.9												6.9																	89.9
.99.9 4	-1.4	1.9	-0.1	1.2	0.0	3.9	2.6	6.9	19.1	7.9	10.3	12.9	8.3	6.3	9.9	2.2	4.3	-1.5	-1.4	1.4	2.3	-3.3	-4.1	-4.2	-4.1	-3,5	-6,6	-6.7	199.0
	-2.3	2.2	5.5	-2.9	2.6	4.6	9.1	7.9	5.9	п.т	12.6	11.6	19.7	5.8	3.7	8.6	2.0	1.4	-1.6	1.9	8.2	-2.3	-51	-6.3	-5 6	-6.8	-5 8	_0 1	129.6

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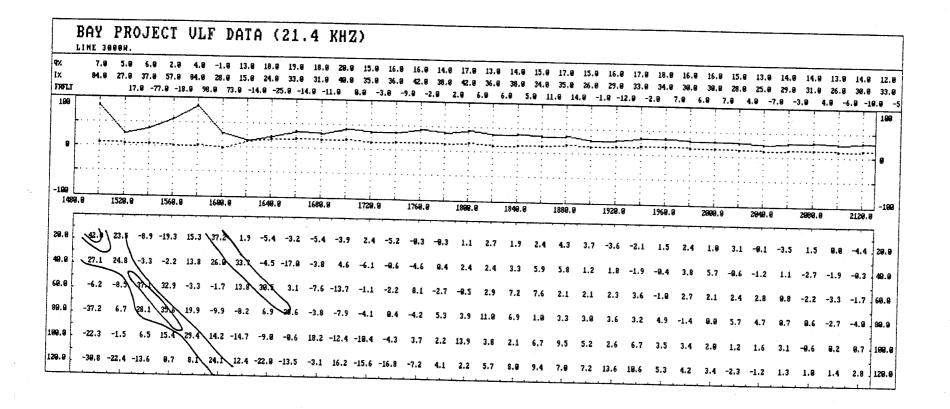
(29.(8 2	6.0	23.0	25.0	29.0	27.0	34.0		26.0	21.0	19.0	19.0	19.8	13.8	11.0	11.0	12.0	13.0	13.9	12.0	17.9		14.0	14.0	18.0	16.0	16.9	19.0	18.0	20.0		19.0	13.0	7.1
199	4.8	7.	.8 -3		8.6	7.8 -1	1.18	0.8 I		1.16				1.18 1.1				3.8 e		5. 0 - 1		1.6 3			, e			3.8 -	s, e -		8.6 7			199
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189		:		:	;		1			i	i	i		i							i					i			i		i			10
	21	28.8		2160.	0	2299.6)	2249.1)	2289.8	1	2320.8		2368.8)	2400.0		2440.0)	2480.0	9	2529,9)	2568.6)	2699.0)	2640.1	}	2689.6	/	2728.0		2760
9.9	4 ;	2.6	9.3	-3.8	-0.8	-2.9	-8.9	5.2	4.4	4.9	2.3	1.1	3.9	4.7	1.3	8.1	-8,9	-1.1	9.5	-2.4	-1.2	1.3	-8.3	-2.8	-1.5	1.6	-2.3	-1.8	-8.7	-8.3	1.5	3.6	7.1	29,1
a a	9 9	8.5	Q.3	-9.3	-6.1	-2.8	2.5	4.3	9.8	6.2	4.3	4.9	5.8	5.8	4.5	8.3	-8.7	8.8	-2.5	-8.7	-8.7	-1.8	-1.9	-1.4	-1.7	-3.2	0.7	-1.2	-1.4	-9.1	2.8	7.4	6.8	49.1
0.0	5 -3	3.4	-8.5	-1.5	-0.5	-1.0	2.7	5.8	4.9	9.2	9.4	8.2	5.5	4.5	4.2	4.6	1.6	-2.6	-1.5	-9.8	-9.4	-2.3	-2.5	9.9	-2.8	-1.4	-3.3	-1.9	-1.8	2.5	7.2	5.7	5.3	68.6
18.9	2 -:	2.4	-5.9	-1.6	3.2	3.9	3.6	4,9	5.0	7.8	13.9	19.4	8.3	4,7	2.9	3.7	1.8	-0.1	-8.3	-8.7	-2.1	9.2	-9.1	-2.5	8.1	-3.4	-2.7	-2.5	2.8	4.9	4.5	5.2	2.5	89.6
18,0	8 -4	6.6	-3.7	-2.7	2.0	6.3	4.7	3.2	7.7	18.8	9.3	12.1	8,6	6.9	4.8	1.5	2.5	3.2	8'8	-1.8	-1.1	-9.1	-1,8	-1.2	-3.2	-8.3	-2,0	1.4	4.3	4.9	2.6	8.6	3.6	199.
18.0 <u> </u>	9 -1	Ø. 8	-2.3	0.9	1.1	3.1	5.0	7.6	8.1	8.3	19.1	8,1	12.5	9.7	5.5	5.0	3.5	3.8	1.3	-19.6	-1,9	-3,5	-2.1	-2.9	-1.2	-1.8	3.1	4.4	3.9	1.7	1.3	1.5	4.2	129.
l-		- b i		**-	سليمغ			- -		A		*		<u></u>					<u> </u>	**					<u> </u>					<u></u>	<u>م</u>			

12 18		59.6	19.0	19.1	13.6	7.9	8.0	10.0	13.0	18.8	7.0	7.0	10.0	12.0	9.0	6.0	15.9	14.9	21.6	8 2.0 9 24.0 29.8 -14	31.8	28.6	18.9	16.0	18.8	11.0	13.8	5.9	3.0		20		2.0	8.0 7.0 9.0 -2		
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-199	L	; 2689.9	i_	2728.		2768.		2899.0	i_	2848.0		2889.0		2928.6	i	2960.0	i	3000.0		3040.0		3060.0	i	3129.9	i	3160.0		3208.0		3248.8		3290.0		-199		
[·	·····			·····			· · · •		·····,						· ·····				, , , , , , , , , , , , , , , , , , ,	,	,,	JI40.0	, , .,		· · · · ·	3606.0		3698.8	, ,,	3,2398.18	,	3328.8 7		
28.9	7	-9.3	1,5	3.6	7.1	2.9	-0.8	-2.8	-0.1	3.0	1.3	-1.2	-2.3	-0.3	2.9	-4.4	-5.8	-4.5	-6.9	-5.1	-2.6	7. 9	6.8	5.3	4.9	-0.8	4.6	5.8	3.3	1.4	-0.3	9.3	-4.5	28.0		
49.8	4	-9.1	2.8	7.4	6.8	5.7	9.1	-1.6	1.4	3.3	1.5	-2.1	-2.3	-8.6	-3.8	-2.0	-6.6	-10.1	-8.4	-7.2	1.9	4.4	12.5	9.8	3.1	7.9	5.9	7.4	7.1	3.5	-9.1	-3.6	9.1	49.9		
69.9	8	2.5	7.2	5.7	5.3	3.6	5.6	3.0	-8.1	-2.2	-1.4	1.4	2.1	-4.2	-3.8	-5.3	-6.2	-11.8	-11.8	-1.3	-0.2	6.9	7.8	19.9	11.7	8.1	8.9	4.3	6.9	8.2	1.7	9.1	-3.6	60.0		
89.9	8	4.9	4.5	5.2	2.5	5.4	5.6	4.9	9.2	-4.4	-0.6	2.8	9.8	-9.1	-6.7	-7,8	-19.9	-8.2	-4.1	-4.7	3.5	1.3	4.4	10.3	14.8	15,6	8.3	8.5	3.8	1.6	6.1	-0.9	-2.9	89.9		
199.0	3	4.9	2.6	8.6	3.6	3.9	5.5	4.8	4.0	2.9	1.6	-2.9	-1.2	-3.3	-6.1	-11.6	-9.4	-3.0	-1.6	-0.2	-3.1	8.4	4.7	18.5	14.1	16.9	15.3	9.3	4.1	1.4	8.4	8.4	-2.8	199.9		
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			۳.۶ - 9.	11.9 9.0			1.0 4.9 -1				13.0 5.0 -10				11.0 3.0 13				11.9 1.0 -4	12.9 1.9 7	7.0 '.0 8.'	9.8 9 17	2.0 .0 14.	-3.0 9 -1.1	0.0 3 -3,	9.8 9 8.	0.0 0 9.	-8.9 .0 -4	-1.0 1.9 -4	-3.0 1.0 -:	-2.0 1.0 -8	-1.8 .9 -15	4.0 .0 -14	8. 4.8
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69 3328	3.9		3368.1		3488.	i	3449.		3499.	ia	3529.6		3569.6		3600.0	i	3648.8		3689.9	i	3729.0		3760.0		899.0		3840.0	i	3889.9	i_	3928.8		3960.0] -1
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.9	.6 -	-9,4	-4.2	-8.4	1.8	4.2	-1.5	-5.0	3.2	-3.1	-6.1	8.8	2.1	0.7	4.6	3.1	-0.1	-2.5	-4.9	2.8	1.9	3.0	7.5	1.3	-9.1	8.8	4.4	8.6	-2.8	8,6	-2.5	-3.7	-5.5	22
	e -	-5.5	-2.8	-0.9	2.2	-9.8	-9.2	9.6	-7.0	-1.8	-9.7	-4.1	-9.1	6.0	4.9	3.2	0.8	-2.8	-9.4	-2.1	5.9	9.4	3.9	4.6	2.9	3.4	0.6	1.9	0.6	-4.6	-2.9	-6.5	-7.9	4
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68.9	4	0.5	-0.6	1.6	1.8	-3.0	-18.3	-7.9	-9.8	-6.9	-19.4	-12.8	-13.9	-16.3	-21,0	-25.9	6	8.9
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29,9	7 3	3.4	-2.4	-4.0	~7.9	-19.1	-8.3	-12.1	-17.1	-24.9	-24.1	-28.7	-31,2	-34,2	-35.5	-36.2	1	29.9

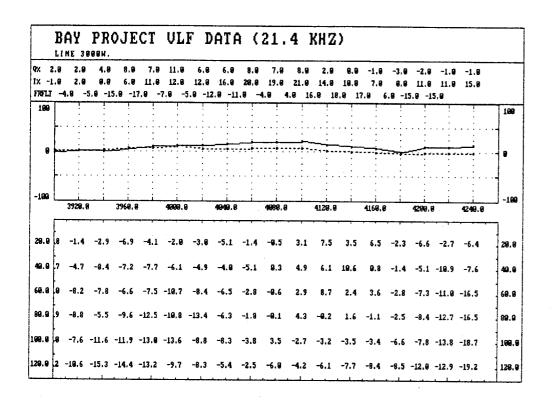
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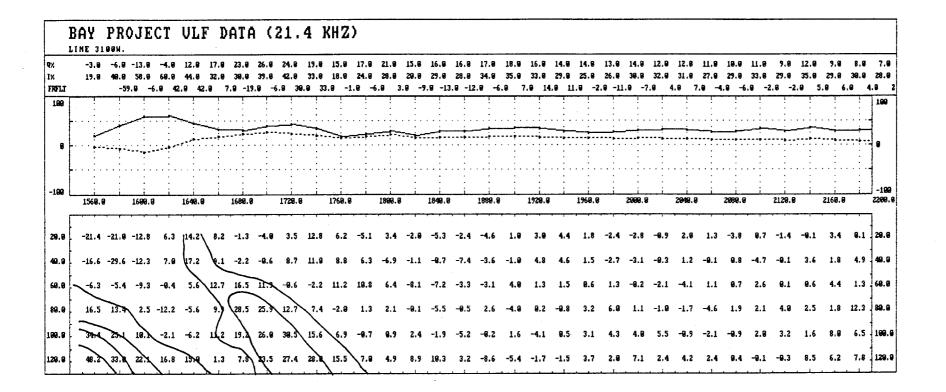


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9. 8	7 -0	.7 -	-1.7	2.4	7.9	9.6	11.9	12.2	9.5	19.3	8.4	6.3	7.9	6.3	6.9	0.1	-1.7	-5.4	-6.1	-6.3	-8.5	-6.5	-3.3	-1.3	-8.7	-2.9	-0.9	1.9	0.9	9.5	9.5	7.7	11.3	68.8
89.Q		. 9	3.9	4.9	8.7	19.7	19.6	11.7	13.4	13.1	11.9	8.1	6.5	6.4	3.8	4.1	-2.4	-4.7	-4.6	-8.3	-8.4	-5.3	-3.2	-1.7	-1.3	-2.4	-1.3	2.9	1.5	-0.2	4.4	5.0	9.3	89.9
9 9.9	79	.5	5.9	8,4	5.8	8.3	18,6	13.3	15.4	15.6	14.9	12.0	8.7	4.0	2.3	-0.9	9.1	-2.7	-5.8	-5.5	-3.8	-4.7	-3.9	-4.1	-5,8	-8.2	1.9	-1.1	8.9	5.0	3.9	6.2	5.8	199.6
	9 T		52	76	9.5	6.1	11.4	14.5	15.1	17.8	16.7	14.4	18.1	5.9	9.3	-9.4	8.3	-1.7	-45	-2.9	-3.6	-3.2	-5.7	-79	-15	-25	-1.4	-1.8	2 0		• 2	4 1	7.9	120.0

% 16,6		17.0	18.9	5.0	3.0	4.0	3.8	1.0		0.0	9.8	16.0	18.8	23.0	23.8	24.0	23.0	22.9	18.9	18.8	28.0	8.0	1.0 -3	.8 -1.	e e.	1.9	9.0	6.0	9.8	19.9	8.8	4.0	
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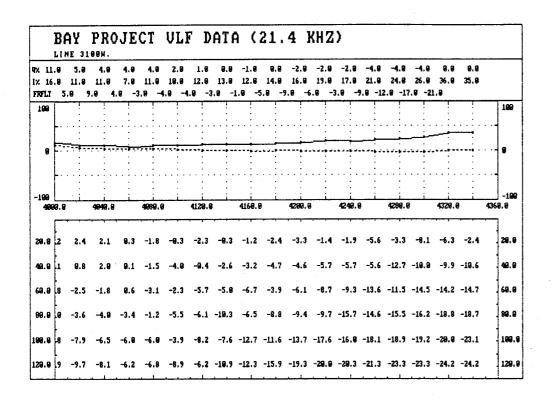
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49.0	9	19.6	i 6.	3 <u>1</u> 1.	1 9.6	3.3	6.3	5.6	6.0	1.3	-2.9	-8.1	-2.9	-12.3	-3.1	-2.0	-7.4	9.5	-8.7	-5.4	-4.8	1.3	1.1	6.2	6.1	3.0	4.1	9.8	12.1	12.4	5.6	3.0	-1.4	49.0
69.9	5	6.1	и.	7 7.	5 10.4	12.1	6.2	7.8	3.5	2.0	-4.1	-8,4	-14.5	-6.8	-7.7	-3.5	-3.8	-5.3	~1.9	-6.2	-1.6	1.9	4.5	0.0	5.9	8.8	9.7	10.2	12.7	19.2	10.8	4.1	-5.3	68.8
89.Q	5	12.9	9.	9 19.	7 11.6	13.9	12.7	5.3	3.7	-3.1	1.3	-8.1	-4.6	-7.1	-6.7	-9.9	-2.6	-4.9	-7.4	4.3	-0.1	-9.7	9.1	-9.2	4.4	13.5	14.5	14.8	8.3	7.5	7.2	3.2	3.3	89.9
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9.9	.8	-8,6	-6.5	-8,5	5.2	-2.8	-6.6	-4.8	-7.8	-3.7	-1.0	-3.9	3.4	-6.6	4.6	17.9	7.4	7.1	6.3	1.3	-1.9	-2.5	-6.9	-1.1	-3.8	-8,9	3.8	-8.3	-0.1	8.2	-3.6	-4.1	-3,4	28.6
. .	4	-7.9	-1.1	-1.1	-3.0	-1.5	-7.4	-13.7	-9.4	-5.9	-3.2	1.1	-8.7	5.7	9.0	11.8	(a.3)	12.1	5.5	3.9	1.2	-5.9	-3.4	-7.5	-1.7	-0.6	-1.9	1.9	-0.1	-3.0	-3.6	-5.7	-5.8	49.6
2.0	3	-2.9	-2.6	-2.1	-5.2	-7.1	-6.1	-8.6	-11.6	-8.6	-4.1	-11.1	5.6	5.8	10.2	11.6	14.2	21.2	19,8) 3.6	-2.2	-1.5	-8.6	-1.9	-5.0	-1.3	0.5	9.9	-1.0	-5.0	-6.7	-4.2	-2.7	68.8
9.0	3	2.6	-4.8	-7.4	-5.6	-9.8	-4.9	-3.1	-9.8	-19.4	-16.8	-3.8	3,3	16.9	18.9	17.1	13.2	12.2	17.)	3.5	1.9	-4.8	-4.6	-5.7	-3.1	-3.1	1.6	-0.3	-2.3	-3.8	-3.6	-4,9	-3.6	80.0
8.8	0	3.6	-2.2	-6.3	-18.2	-7,4	-10.5	-9.2	-3.9	-16.7	-7.3	-8,3	4.8	7.5	ميلا (12.6	14.1	JB-R	6.8	(5.A	0.2	-8.2	-2.1	-3.8	-6.3	-2,1	-5.9	-2,2	-2.5	-9.4	2,6	0.4	-9.4	199.
29.9	.0	6.8	8.2	-8.9	-10,1	-14.4	-11.5	-11.1	-16,6	-8,5	-9,8	8.7	5,5	1.5	∕?ì∖	12.9	8.2	8.3	9.0	4.6	15.3	5.3	1.2	-3.0	-2.6	-9.0	-7.1	-7,9	-2.3	1,6	-9.5	3.9	-	1.8

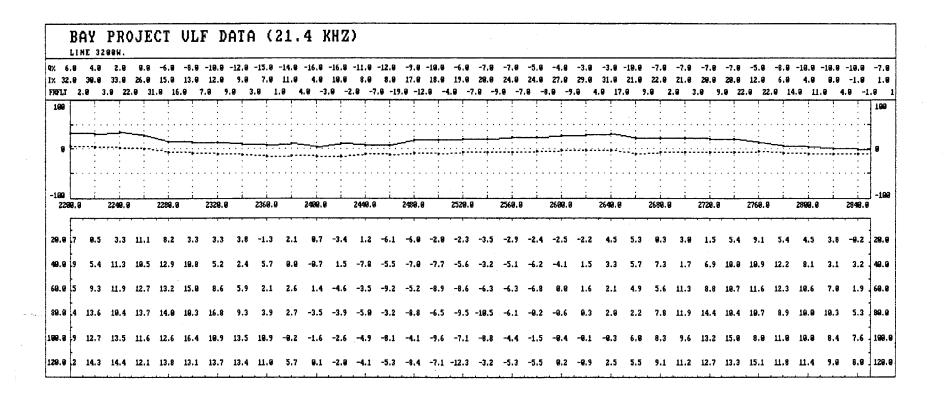
1	3,9	17.8	15,9	12.8	13.9	19,9	18.9	6.0	1.8	7.8	8.8	9.9	-2.8	-15.8	-22.8	-17.9	-18.8	-8.9	-6.8	-18.8	-3.8	-2.8	2.9	8.8	9,6	11.9	16.8	ш.е		7.6	11.8		12.9	
199		,8 3	3.8	7,8	4.8 -3	.8 -1	.9 21	.9 16	5.0 (3, <u>8</u> 6	.8 9	.0 17	1.6 35	.0 2	2.0 -19	.0 -21	1.0 -1	3.8 -1		1.9 -1	1.8 -1	3.8 -1	5.9 -1	7.8 -16	8.8 -1	8.9 -1	1.8 5	5.8 5	1.9 4		3.8 -4	1.0	1.0 -: !	3.0 -
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20 0			2 a	a 2	24	-1.7	, , , , ,	187	 		 		9.6	11.2	15		-4.6	-1.8		-7.6	-5.6	-9.9	-7 0	-5 1	-2.2	-4.7			21		-1.8	-8.3	-2.3	28.8
60, T		-1.0	4.7		4.7	-1.,		10.1		0.6	413	6.6	7.0	14.15	1.0					- 610	214						916]
49.0	8	-0.3	1.3	3.5	-1.8	3.9	7.4	4.2	13.0	4.8	1.7	12.8	14.1	10.3	4.5	-3.6	-9.2	-4.0	-3.6	-4.5	-7.2	-11.8	-7.6	-7.6	-8.8	-3.2	-2.1	6.8	2.0	0.1	-1.5	-4.8	-8.4	48.9
68.8	17	-3.3	1.3	-1.8	8.8	18.2	4.3	7,0	5.4	11.4	13.2	13.7	13.5	5.8	4.5	2.6	-3.2	-11.7	-8.2	-6.3	-7.4	-8.1	-13.1	-13.2	-9.3	-6.1	-8.8	-2.5	-1.8	8.6	-3.1	-2.3	-5.7	68.8
8 8 . 8	6	-1.3	-4.5	4,9	7.8	6,3	8.1	6.7	8.1	13.4	21.6	11.9	5.6	8.3	2.3	5.8	1.2	-6.8	-11.8	-13.8	-11.0	-10.0	-11.6	~11.6	-8.4	-7.3	-8.9	-3.6	-4.9	-3,4	-1.2	-5.5	-6.1	89.9
L 80, Q	4	-5.5	-8,3	1.8	1.2	6,6	9.5	9.1	14.7	18.2	13.7	13,7	6.6	3.2	9.7	1,9	1.7	-1.6	-12.4	-17.3	-15.5	-13.8	-11.2	-9.5	-9.0	-8.5	-7.8	-7.9	-6.5	-6.0	~6.8	-3,9	-8.2	199.0
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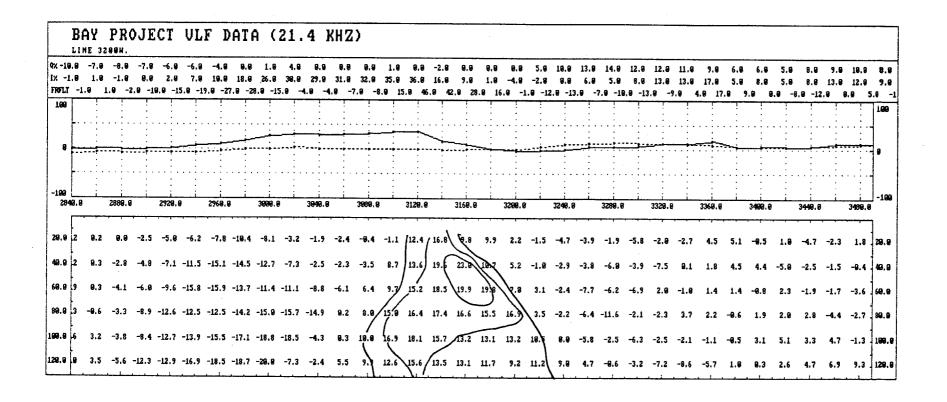
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X	1.0	-11.9	-19.0	-19.8	-2.8	7.9	16.0	22.9	27.8	22.9	23.9	28.8	18.9	18.9	17.8	16.0	14.9	14.9	13.8	13.0	12.0	15.0	14.9	13.0	13.0	10.0	18.9	9.0	9.0	10.0	8.8	6.0	6.0
IX	78.0																														29.8		
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Ē	T.060' 0	• 	1000.	· · · ·	10-90.0	, 	1000.0			, , , , , , , , , , , , , , , , , , , 		, ,,	1000.0	· ·	10-80.0	····		, 		,		, 		,,		, <u> </u>		·		,	, ,	, <u>,</u>	7
28.9	25.5	15.1	-13.1	13.Z	32.1	17.0	2.3	-8.1	-5.9	-4.5	-5.3	1.4	-0.7	-2.3	8.4	-8.7	1,5	-8.9	-8.2	2.9	-4,5	-6.7	1.7	4.7	1.4	8.8	-2.1	1.7	€.6	3.0	1.1	-1.8	28.0
49.9	13.9	8.6	19.1	14,0	26.8	35.7	11.3	-7.8	-11.4	-3.3	0.4	-4.7	-2.8	-8.9	-2.4	-0.3	-2.1	1.8	2.5	-3.7	-4.1	-3.1	-1.6	3.4	5.5	-1.1	-1.0	-0.4	4.9	2.5	2.9	3.6	48.9
69.9	-7.1	16.4	38.8	35.5	11.9	14.6	27.1	8.5	-5.4	-9.4	-7.8	-0.4	1.2	-9.1	-0.7	-5.8	9.8	1.5	-3.6	-5.1	-2.3	2.1	-1.2	-2.3	1.9	6.0	1.1	4.6	e.5	3.7	5.2	3.2	68.0
89.9	2.7	24.9	33.1	35.9	24.3	5.1	9.6	29.7	6.2	-7.7	-11.1	-5.5	-9.1	-0.6	2.3	6.5	1.2	-4.4	-6.8	-2.5	Ũ.3	-8.9	9.3	-2.7	-0.2	4.2	10.5	3.3	3.9	1.7	3.2	6.1	89.9
199.9	9.9	18.4	21.3	21.7	38.2	19.9	-1.8	8.7	18.9	9.5	-11.5	-11.5	-4.8	-2.8	2.9	7.7	-8.6	-3.8	3.6	2.8	-8.9	-1.9	-2.2	3.1	-8.6	3.5	3.9	8.4	3.7	2.1	4.5	12.0	199.9
129.9	3.4	6.8	7.8	14.6	16.2	24.9	19.9	-2.2	5.7	17.3	-0.2	-13.2	-16.6	-5,9	-8.4	-5.1	-1.5	6.4	5.8	4.2	4.2	5.1	4.1	-1.7	4.3	-2.9	9.1	4.9	6.3	5.4	9.9	10.8	129.9

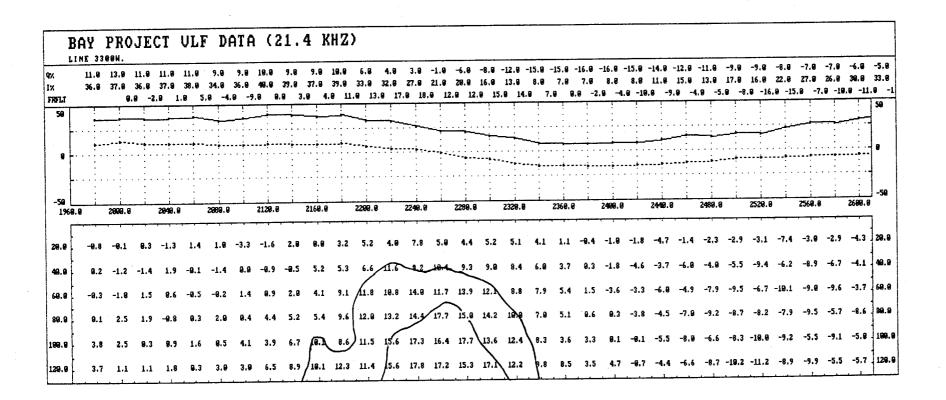


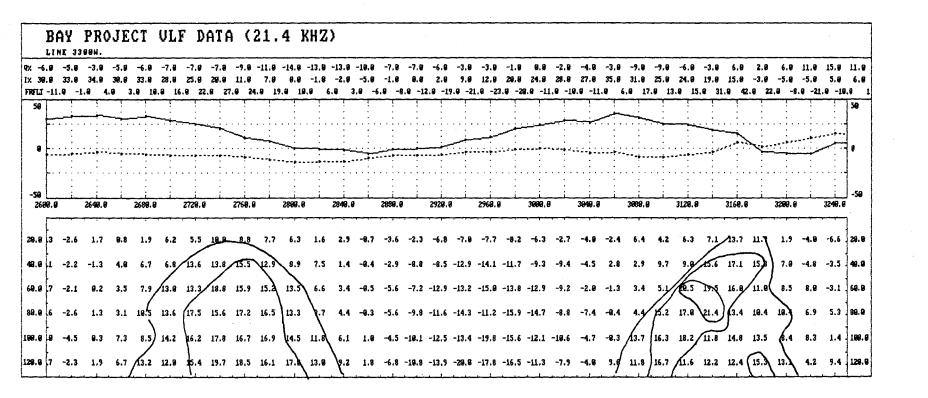


199 9 109 34288,8 3529,8 3568,8 3568,8 3688,8 3728,8 3769,8 3888,8 3849,8 3849,8 3888,8 3928,8 3928,8 3958,8 4000,	199
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9.9 9 9.9 -9.7 -9.1 1.6 3.1 4.8 2.9 -1.5 1.8 9.4 3.9 5.7 5.9 3.8 -3.9 -9.9 -2.6 -4.7 9.3 -5.8 -4.7 -8.8 -4.6 -1.1 -1.9 -9.8 9.8 9.9 1.9 -2.5 -2.9 -1.8	28.9
8.8 4 1.7 9.5 -9.6 2.2 5.6 5.9 3.2 3.6 -9.4 3.9 6.8 7.6 7.5 2.5 1.2 -5.3 -4.1 -2.8 -7.7 -4.7 -5.5 -8.2 -2.7 -4.2 -2.9 -1.5 -8.6 1.4 -2.2 -3.4 -4.2 -1.7	40.0
0.0 6 -1.4 2.8 4.6 4.5 5.9 4.0 5.6 3.0 4.6 3.4 7.7 7.9 5.0 6.6 -0.3 -2.3 -5.3 -0.2 -5.7 -7.0 -6.6 -6.4 -9.5 -4.1 -4.1 -2.5 -0.6 -4.2 -4.3 -5.0 -2.4 -6.5	69.0
9.9 7 -1.7 1.3 7.9 6.4 3.8 5.3 2.7 7.3 6.2 9.1 6.1 3.8 6.6 2.9 3.8 1.1 -5.4 -8.1 -9.8 -9.5 -9.2 -6.9 -6.9 -6.9 -5.6 -5.6 -5.6 -7.5 -1.1 -5.9 -7.7	89.9
8.9 3 9.5 1.4 1.9 3.6 4.9 1.7 6.8 8.5 12.1 8.9 6.1 4.2 1.7 3.7 3.1 -9.7 -3.3 -6.1 -11.3 -19.5 -19.5 -19.5 -7.3 -8.6 -6.2 -7.6 -7.1 -2.1 -6.3 -8.3 -19.4	199.9
8.8 3 2.8 3.9 -1.5 9.8 2.4 5.1 6.6 18.5 11.1 9.6 9.0 5.2 9.9 2.1 -1.6 -1.4 -1.4 -7.5 -7.9 -13.5 -12.3 -11.5 -11.7 -7.2 -18.2 -18.6 -6.9 -4.7 -7.0 -9.2 -19.8 -14.8	129.9

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49.0	5	-0.6	5	1.4	-2.2	-3.4	4 -4	.2	-1.7	-3.3	-5.2	-5.6	-11.	8 -19.	6 -11.9	9 -12.9	-6.4	-6.8	0.5	-1.1	-19.9	-9.8	-12.2	-13.2	-11.3	- 49.0
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68.8	5	-8.1	5 -	4.2	-4,3	-5.	8 -2	.4	-6.5	-7.8	-5.8	-8.4	-11.	5 -19.	6 -17."	7 -11.1	-12.6	-6.8	-9.8	-8.0	-7.8	-13.3	-10.1	-13.1	-17.0	
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89.9	6	~6.	- ·	5.6	-7.5	-1.	1 -3	. 9	-1.1	-8.6	-14.2	-14.1	1/.	a -10.	J -11.1	10.3										
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129.9	6	-6.		4.7	-7.0	~7,	6 -10		TAIL	****			• ••••													

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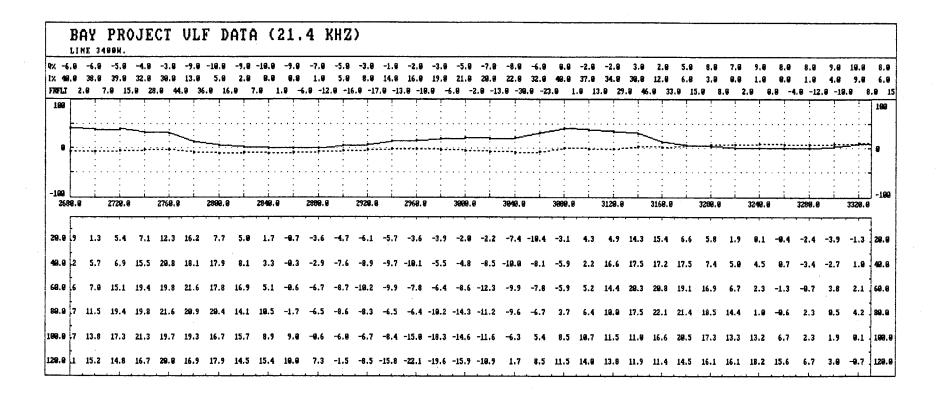


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15.9 5.9 711 -1	16	L.9 5.0 1.1	9.0 4.0 8 -2	8.8 6.9 .9 -11	6.0 6.9	11.0 15.0 1.0	5.0 4.8 5.0 1	9.8 2.9 1.8 -	5.9 3.9 1.0 -f	3.0 4.9	6.9 7.9	7.0 5.0	4.0 5.0 3.0 -6	2.0 10.0	9.9 6.9 3.9 6	-1.9 6.9	-2.9 4.9 8.0 4	-3.9 9.9	-2.9 6.9	-2.0 6.9	-3.0 9.9 9.9	-5.0 3.0	-5.9 2.9 1.8	-3.0 9.0	-2.9 1.9	1.9 3.9	2.0 -4.8	-1.0 -1.0 .0 -:	6,0 -2,8 3,0 -6	8.9 9.9 1.9 -	19.9 3.8 1.0 -3	6.0 0.0	9.0 6.0	1 9.0
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59 3249,	.9	i;	i 3289, 9	i	; 3320.0	i	3360, (i)	3498.0	, <u>i</u>)	; 3440.0	i	3489.9	i	; 3529.0	i	3560.0	i 	3699.8	i	3649.0	i I	3689.9		3728.8	i !	i 3769.0	i	i 3899.0	i	i 3840.0	i	3888.6	
	; ;	9.1	-2.9	-9.5	-4.6	1,9	7.3	-8.2	8.1	-2,2	-1.3	1.2	-3.1	-9.2	2.7	8.4	3.8	-8.5	-3.3	3.7	1,4	-1.0	2.9	1.9	-1.6	3.2	2.1	-1.5	9.2	-3.8	-0.5	-1.9	-6.1	2
	i -3	3.4	1.2	-5.3	-1.3	1.1	1.9	5.7	-1.9	-2.8	-0.8	-1.6	0.4	-1.2	9,8	5.8	9.2	9.1	2.4	-1.3	3.1	4.3	-8.5	-0.4	3.6	1.9	1.1	1.1	-3.9	-1.3	-4.8	-5.3	-2.0	4
.0 [1	-4	4.7	-9.9	2.9	3.9	2.1	0.2	-1.2	5.2	-8.7	-4.6	-2.2	-9.7	2.3	4.2	-8.3	1.8	3.8	2.0	1.6	-8.1	2.6	2.3	2.2	1.8	1.8	-9.8	-1.1	1.2	-6.1	-6.1	-4.4	-6.5]
.8 3					3.3			2.5									3.5									2.0	-1.1	-9.3	-3.1	-4.1	-5.3	-6.8.	-7.3	1
		5.2	-2.3	-3.5	-3.9	8.9	3.2	2.6	1.2	3.9	6.4	1.8	9.8	-2.3	-1.9	3.4	1.3	1.3	5.0	2.7	1.9	3.7	-0.4	3.6	2.5	~1.9	1.3	-2.5	-5.2	-3.8	-4.6	-8.3	-8.7	1

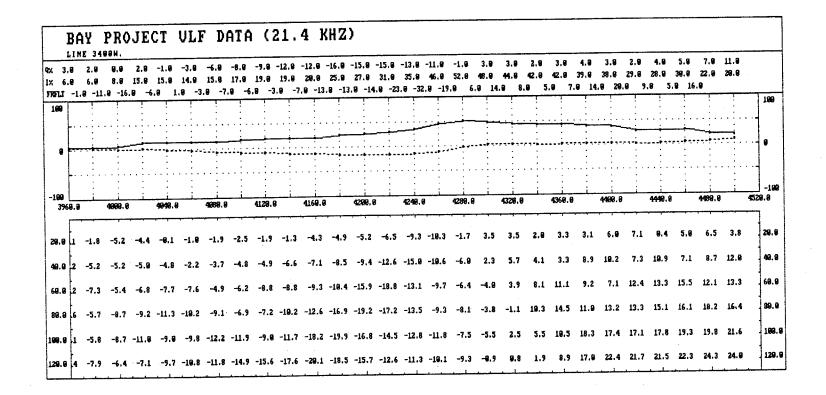
, - CLEMPA, Mercerni, Al, evizari, commu

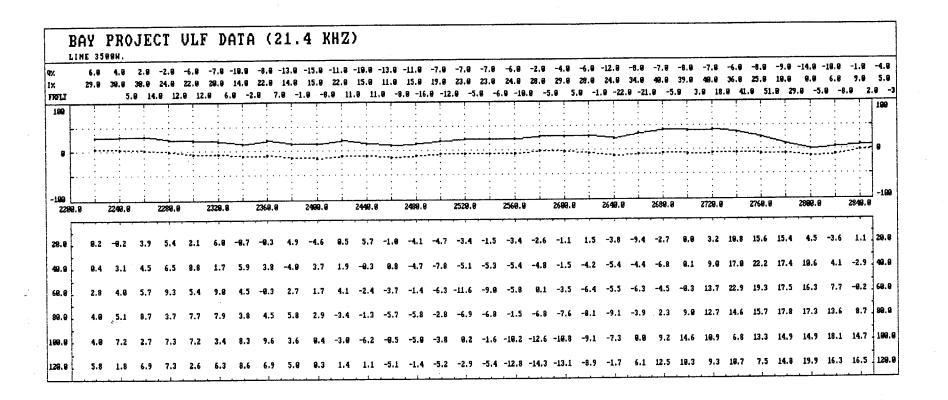
% 6	8	9.8		8.9 11.9 5.9 -		9.0 12.0	5.9 11.9 .0 -1	2.0 12.0				14.0	-5.9 17.9 1.0 -2	14.9	19.0	21.0		31.9	-1.0 39.0 1.8 -16	37.0		39.0	9.9 36.9 1.9 -1		9.9 36.9 1.9 1.	-1.8 40,0 .0 5	-1.9 35.9 .9 5.	-1.0 36.0 a s	2.9 34.0	1.0 29.0 3.0 1	7.0 28.9		11.0 17.0 7.0 -7	28.6
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388	9.0		3928.0	}	3968.6	1	4008.0		4049.8		4999.8	1	4129.9		4169.8		4289.6		4249.0		4289.8		4328.8		10/0.0		4499.9		4449.8		4489.8	1	4529.6	
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9.9	1	8,6	-2.2	-2.6	· · ·	, , . .		, · , -	, ,		, <u>r</u>		,		, ,	, ,	,,		, ,	, <u> </u>	, ,	, ,	,. , .	, ,	9.560.0 0.2			9.7	• •		• •	, ,	-1.6]
	•				-9.5	-1.8	9.1	-1.1	9.9	-1.6	-1.9	-2.3	-0,6	-1.5	-5.4	-2.9	-6.8	-11.7	-3.6	-6.6	-2.2	7.8	-1.6	1.5	,,. ,	8.5	3.2		5.1	4.5	2.6	7.5	• •	29.1
9.9	.a	-6.8	-2.6	-2.2	-9.5 -4.1	-1.8 -1.8	9.1 -2.3	-1.1 -8.3	9.9 ~2.6	-1.6 -2.9	-1. 9 -3.7	-2.3 -2.5	-0,6 -5.1	-1.5 -5.4	-5.4 -5.1	-2.9 -10.9	-6.8 -11.6	-11.7 -19.2	-3.6 -16.1	-6.6 -6.9	-2.2 9.9	7.8 -2.7	-1.6 5.8	1.5 -0.4	8.2	0.5 3.0	3.2 3.9	6.3	5.1 4.4	4.5 8.2	2.6	7.5 2.9	-1.6 5.6	29.1 49.1
9.9 9.9	5	-6.8 -3.9	-2.6	-2.2 -4.2	-9.5 -4.1 -2.6	-1.8 -1.8 -5.2	9.1 -2.3 -2.1	-1.1 -8.3 -4.4	8.8 -2.6 -3.5	-1.6 -2.0 -6.1	-1.9 -3.7 -3.2	-2.3 -2.5 -7.3	-8,6 -5.1 -6.3	-1.5 -5.4 -5.8	-5.4 -5.1 -10.2	-2.9 -10.9 -13.3	-6.8 -11.6 -14.5	-11.7 -18.2 -17.6	-3.6 -16.1 -11.4	-6.6 -6.9 -8.4	-2.2 9.9 -5.6	7.8 -2.7 1.4	-1.6 5.8 -2.8	1.5 -0.4 7.9	0.2 9.8	0.5 3.0 0.6	3.2 3.9 5.6	6.3 6.1	5.1 4.4 18.2	4.5 8.2 12.4	2.6 19.6 6.1	7.5 2.9 9.8	-1.6 5.6 7.8	29. 49.
49.9 69.9 89:9	9 5 3	-6.8 -3.9 -7.3	-2.6 -7.0 -5.2	-2.2 -4.2 -8.9	-9.5 -4.1 -2.6 -4.4	-1.8 -1.8 -5.2 -3.7	9.1 -2.3 -2.1 -8.5	-1.1 -8.3 -4.4 -4.3	9.9 -2.6 -3.5 -8.7	-1.6 -2.0 -6.1 -3.8	-1.9 -3.7 -3.2 -5.8	-2.3 -2.5 -7.3 -7.6	-8,6 -5.1 -6.3 -6.3	-1.5 -5.4 -5.8 -12.2	-5.4 -5.1 -10.2 -15.6	-2.9 -10.9 -13.3 -13.8	-6.8 -11.6 -14.5 -19.1	-11.7 -10.2 -17.6 -14.1	-3.6 -16.1 -11.4 -19.9	-6.6 -6.9 -8.4 -19.6	-2.2 9.9 -5.6 -7.4	7.8 2.7 1.4 -5.8	-1.6 5.8 -2.8 2.2	1.5 -0.4 7.9 9.3	9.2 9.8 9.3	9.5 3.9 9.6 5.3	3.2 3.9 5.6 3.9	6.3 6.1 8.8	5.1 4.4 18.2 9.9	4.5 8.2 12.4 7.5	2.6 19.6 6.1 19.3	7.5 2.9 9.9 11.3	-1.6 5.6 7.8 12.6	

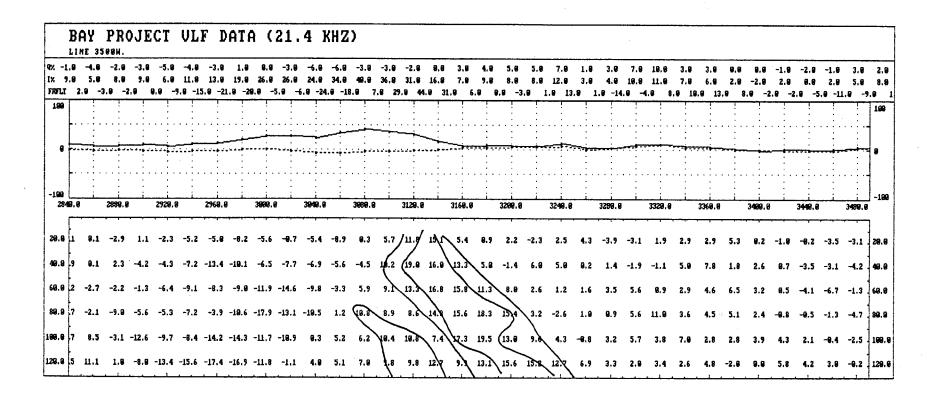
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9% 1%	13 49		14.0 44.9	42.0	48.9	44.8	43.	0 3	2.8	9.8 35.9	3.0 29.0	-3.0	-11.9	13.9	12.8	8.9	7.0	14.8	14.0	-14.9 14.9		-8.0 23.0	-5.9 26.9	-6.9 27.9	-7.9 29.9	-7.8 27.9	-7.9	-6.9 33.0	-6.0 36.0	-4.8 41.8	-5.8 39.0	-6.0 40.0 2.0 2	-6.9 38.9 2.9	39.8	-4.9 32.9 5.9 28
FRFLI 199		:	2.0		.0 -5	1	2.8	13.0	18.		.w .s		5.0	9.8 5		.9 -1	.0 -13			-14	-10			· · · · · ·	·····	1.0 -11									199
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-199 29		2	128.9		2169.8		2296	9.8		2249.0		2289.0	3 	2328.0		2368.9	k 	2499.0	, <u>, , , , , , , , , , , , , , , , , , </u>	2448.6) ,	2489.6	,L., , ,,	2528.6	3	2568.6	 	2699.0	I	2640.0) ,,	2689.6	, , , . ,	2729.0	
29.9	-2	.6	-1.5	2.1	-1.1	-0.9	3.	.8	5.4	7.6	8.8	11.0	6.8	1.4	3.3	2.7	-3.3	-4.1	-8.9	-3.1	-5.7	-5.8	-2.9	-3.1	-8.6	-2.9	-4.4	-1.9	-5.5	-1.8	9.1	8.9	1.3	5.4	29.0
49.9	-9	.5	8.4	-1.9	2.3	3.9	4.	.2	9.5	13.9	16.8	12.9	19.7	9.6	4.2	0.2	-0.5	-3.3	-6.5	-5.4	-7.6	-9.1	-8.6	-3.9	-5.4	-5.0	-5.3	-8.7	-3.4	-3.5	8 .5	3.2	5.7	6.9	48.8
68.0	2	.8	8.8	0.3	2.7	7.0	9.	.3 1	1.2	18.5	17.3	16.0	15.5	12.3	4.5	-8.3	8.9	-1.9	-7.2	-19.5	-8.0	-9.7	-8.3	-19.9	-7.3	-6.6	-8.2	-4.6	-6.9	-1.1	-2.0	3.6	7.0	15.1	68.0
89.9	1	.8	1.7	2.9	3.8	7.7	13.	.61	7.6	15.7	18.1	19.3	17.6	12.9	8.1	4.7	-2.8	-6.2	-7.1	-9.7	-19.8	-6.0	-9.4	-9.6	-8.9	-7.8	-5.Ż	-5.5	-4.6	-6.5	9.1	9.7	11.5	19.4	99.0
100.0	1	.,9	3.6	5.1	7.4	19.9	16.	.2 1	7.8	17.8	18.4	28.9	16.5	13.6	11.8	6.1	-1.3	-8.2	-7.5	-8.2	-9.0	-10,4	-5.2	-7.8	-18.4	-8.1	-7.0	-6.5	-6.9	-2.7	-3.5	8.7	13.8	17.3	199.9
129.9	t.	1.5	5.3	7.7	11.4	16.2	15	2 1	5 0	20 5	19 9		16.9	16.1	12.5	6.5	2 2	-1 6	-7.1		-9.6	-9.7	_11 0	-19.7		-11 5	-9.8	-7.5	-2.8	-2.3	7.6	11.1	15.2	14.8	120.0



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× 19.9	8.0	3.9	3.0	2.0	5.0	3.0	6.8	5.0	3.0	1.0	8.8	0.8	9.9	-1.9	-2.0	-3.0	-1.0	-1.0	-2.9	1.9	9.8	9.8 9.8	1.0	4.9 3.9	6.8 6.8	7.0 3.0		9.0 11.0	7.0 8.0	6.0 4.0	5.9 7.8	3.0 6.0	· •
7. 9.8 7671.1		-1.8 5.0 t		-1.9 3	8.9 .0 -7	3.0 .0 -4	3,9 .9 -2	4.6 :,9 -1	4,8 ,0 -7	4.8 .8 -3	6.0 .9 2	5.W .0 3.	3.6 0 1	18 3. 2.0	2.# ,9 1	3.8 .0 -1	.95		-6.0 .0 -	4.9 1		••••	.8 -9	.8 -6			8 -9		.0 8.				
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29.0	5.6	2.6	9.3	1.1	-2.6	-1.7	-8.8	-1.1	0.0	-1.1	-0.7	1.9	-9.1	0.7	1.3	-0.2	-9.1	3.0	-9,4	-1.6	2.4	-0.3	-1.3	-3.8	-8,7	-0.9	-4.5	-0.6	3.6	8,4	-18.9	A' 1	24.8
49.9	1.4	5.4	2.9	-2.8	-1.4	-2.1	-1.6	-8.8	-1.6	-8.9	9.2	-9.6	2.7	1.1	-9.2	1.5	2.7	-0.7	0.7	1.9	-1.5	-8.3	-2.8	-1.4	-4.4	-4.5	-1.2	-1.2	-1.5	1.9	0.8	-3.2	49.0
	2 1	74	34	1.6	-3.1	-2.1	-3.2	-2.9	9.5	1.1	-8.9	1.1	9.2	1.7	6.9	2.3	0.3	9.1	1.1	1.4	0.4	-4.4	9.8	-3.7	-6.1	-5.6	-1.5	-1.7	-1.9	-9.4	8.2	-5.2	68.8
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.00.9	-19.6	8.9	1.9	4.1	6.8	3.1	-2.8	-8.4	-3,7	-2.8	-9.5	-0.7	-0.5	3,2	8.9	2.7	2.3	1.6	9.4	-3.8	-1.2	-3.3	-5.4	-6.8	-9.8	-4,8	-4.2	-4.9	-3.9	-7.1	~8.9	-7.1	199.0
20 0	-1.5	-1.7	-2.9	R. A	2.8	6.9	4.7	8.9	1.8	-2.2	-2.1	-9.5	2.1	-8.3	1.4	2.2	2.7	9.6	-2.3	-9.4	-4.3	-6.3	-4.2	-1.7	-6.6	-2.9	-4.7	-6.7	-11.6	-10.5	-7.5	-9.4	129.9

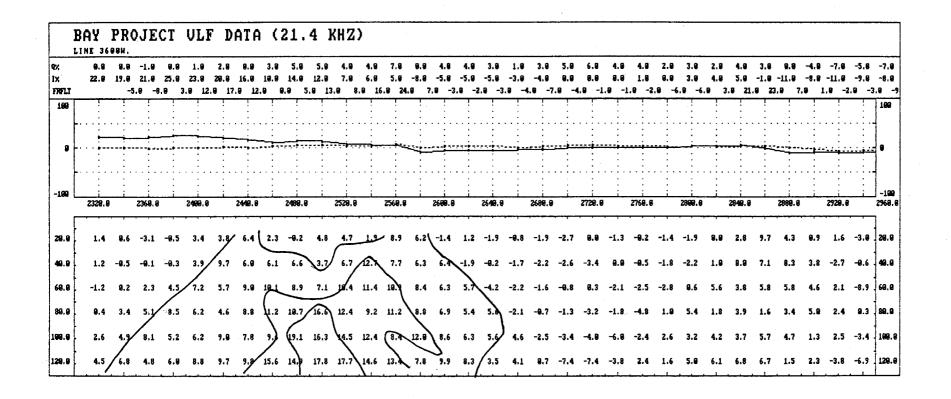






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	8 Z		8.0	8,9	-1.4	9,9 4 0	9.9	W.	88. 14.		8.8	-1'8	-6.8	-1,9	-3.8	-1.6	1.0	•••		6.0	6.8	3.8	1.0							-6.0	-11.0		0 -17.			
IX 5 FRFLI		 1.(-7 10 -2	0.0 2.0 -3	9,8 19 -3	9.9 - 9.8				13.		9.8 8 ~			_(6.0 0.8 -1					19.9 1.9 4	13.8		15.0 1.0 4			15.9 6.9 -			8.8 -	7.6 1 12 -		8 14. _8 8 .			
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-199 348	a. A	i	528.8	Ĺ.	3568.0	i	3609.0	i	364	a. a	;	3689.8	i.	3728.0	i 1	3768.6	<u>i</u> .	3998.6	i	3849.6	i_	i 3680.0	i	3920.0	i	3968.6	i	4998.	<u>i</u>	4949.	<u>.</u>	4008		412	100 29.8	-199
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29.9	1 -2	.4	2.9	-9.5	-1.1	-0.9	-1.7	-2.	1 -3.	3	5.5	1.2	0.8	-2.1	-1.3	0.7	-5.2	9.1	8.3	2,3	-1.1	3.6	-1.8	-1.9	3.5	-5.1	-3.9	1.7	1.7	1.7	-2.3	-3.	4 -2.	5-6	5.8	29.9
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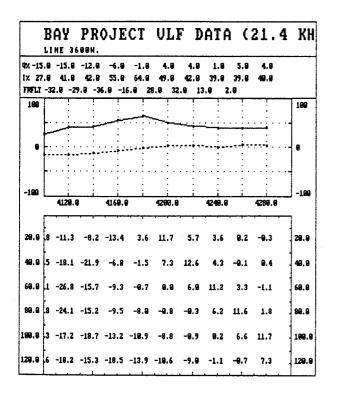
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89.9	6 -	15.4	-23.4	-19.	8 -22.	8 -29.	4 -18	.3 -	19.9	-1.9	5.1	9.1	8.9	9.5	19.2	19.9	6.7	1 89.9
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9.9	7 -	-13.0	-21.6	-29.	6 -1	9.9	-19.7	-:	3.6	-7.8	9.9	-9.	2 6	.7 1	1.9	11.4	8.7	-2.6	0.3	-1.9	6.4	4.7	3.4	2.9	-2.6	9.2	-1.8	-2.4	-3.1	-3.7	-2.1	-1.5	1.4	-2.1	-6.9	9.3	88.9
9.8	5 -	-21.0	-29.6	-22.	8 -2	21.2	-9.8	-11	1.6	-3.9	-7.7	8.	4 3	.9	9.9	19.2	8.6	8.9	-1.6	2.8	-8.1	3.8	2.7	-4.3	-9.5	0.1	8.4	1.8	-1.8	-2.5	-1.3	-3.8	-3.9	-4.1	-1.4	8.4	198.0
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29.9	.8 -2		4.9	9.0	6.5	-0.2	2.2	2.7	0.1	-2.1	-0.6	3.5	0.3	0.9	0.4	-2.8	-3.7	1.2	-9.8	8.3	-1.1	-1.2	-2.8	-10.9	-6.0	-12.8	-11.3	-8.2	-13.4	3.6	11.7	5.7	3.6	29.9
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	-1.8	-0.5	2.6	9.1	2.7	-2.8	-2.9	4.5	3.9	8.6	-1.9	-8.2	-1.2	-6.2	-3.8	-1.5	-2.5	-1.9	3.2	6.1	3.9	8.8	4.5	4.3	6.2	9.0	-5.7	-1.8	-14.7	-6.7	1.4	-19.5	2
a [-1.8	9.9	1.3	5.3	-2.2	-1.5	1.3	1.5	3.2	1.9	-9.8	-4.8	-5.1	-3.2	-6.9	-5.7	-1.7	1.1	3.1	7.1	12.7	6.8	10.4	7.8	4.9	2.2	-2.7	-17.8	-8.4	-10.6	-14.3	-4.6	4
9 [2.1	1.0	2.8	-2.7	1.4	1.5	2.8	-0.5	-1.6	3.6	2.2	-5.0	-5.6	-4.7	-5.4	-6.1	-1.2	3.1	3.7	9.5	6.8	14.1	10.4	9.8	3.1	0.4	-11.5	-6.7	-14.2	-15.8	-14.7	-15.2	6
9	1.6	3.2	-3.3	-í.2	9.9	4.9	1.1	1.2	1.4	-1.9	0.4	-0.6	-4.4	-6.1	-7.9	-2.8	-3.1	-1.8	8.9	6.3	18.9	13.7	12.7	6.6	6.9	-9.7	-4.5	-8.4	-14.4	-17.4	-16.2	-14.8	8
•	3.5	-2.8	-8.9	8.7	4.1	1.4	4.4	3.9	2.4	-2.5	-2.8	-0.4	-3.2	-7.8	-7.6	-3.4	-1.5	1.5	1.8	11.6	19.8	12.2	19.2	12.0	-5.7	2.4	-5.3	-12.3	-14.0	-17.5	-19.5	-16.8	1
	-2.6	8,4	2.8	5.2	2.9	3.2	4.3	5.3	-1.3	-1.4	-4.2	-8.7	-4.4	-2.9	-5,4	-4.4	1.6	2.6	4.6	8.1	11.7	9.1	10.8	-1.6	8.6	-8.9	-5.5	-11.9	-14.8	-14.5	-18.5	-21.6	1

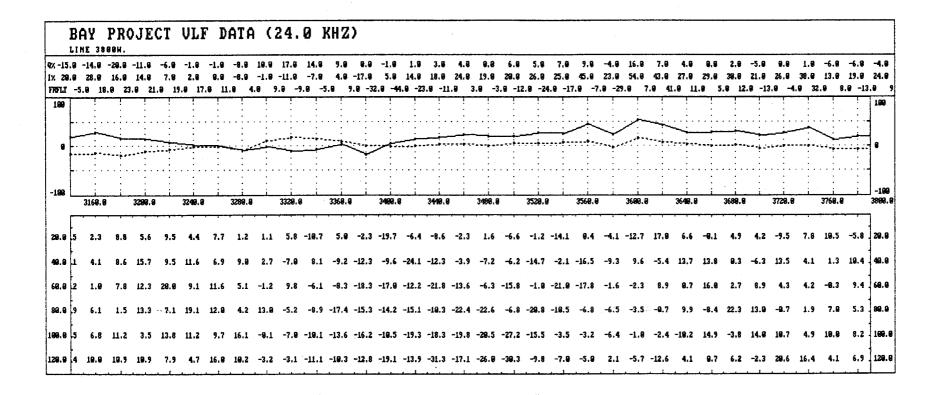
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g 4 - <u>11.8</u> -9.2 -4.8 1.1 3.3 7.8 3.7 7.8 5.6 3.4 4.6 2.7 4.9 5.6 6.4 3.4 -0.9 -3.8 -2.9 -7.6 -6.2 -5.3 -3.4 -2.8 0.4 0.8 -0.1 1.7 3.4 3.9 3.8 5.6		4	-4.2	-1.7	-9.1	ι - ι .	.9	1.1	5.7	3.9	4.4	9.6	-0.2	2.9	8.8	3.8	3.9	0.5	2.1	2.8	-2.2	-3.4	-4.2	-2.8	-3.5	-1.6	0.3	-8.6	9.1	1.7	8.9	-9,1	2.1	3.1	1.6	29
	.9	2	-7.4	-3.8	` -i. !) -9,	.7	2.2	4.5	8.7	5.9	3.6	1.9	1.1	6.0	4.0	3.3	4.6	2.2	-9.5	-1.0	-4.8	-6.1	-6.4	-3.2	-2.9	-2.6	0.1	1.2	8.5	1.4	3.9	2.4	3.8	4.4	49
9 7 -4.6 -9.7 -2.7 1.1 3.7 3.4 4.0 3.5 7.3 6.3 4.7 4.0 4.2 6.9 4.0 3.3 1.4 -2.5 -5.4 -3.9 -7.0 -6.1 -4.6 -1.6 -0.9 -0.4 3.1 3.6 2.7 4.3 4.2 2.1	.0	4 -	·11.8	-9.2	-4.	3 1.	.1	3.3	7.9	3.7	7.8	5.6	3.4	4.6	2.7	4.9	5.6	6.4	3.4	-0.9	-3.8	-2.9	-7.6	-6.2	-5.3	-3.4	-2.0	9.4	8.8	-9.1	1.7	3.4	3.9	3.8	5.6	60
	.0	7	-4.6	-9.7	-2.	71.	.1	3.7	3.4	4.9	3.5	7.3	6.3	4.7	4.9	4.2	6.9	4.0	3.3	1.4	-2.5	-5.4	-3.9	-7.0	-6.1	-4.6	-1.6	-8.9	-9.4	3.1	3.6	2.7	4.3	4.2	2.1	84
		Ł		-19.1			-					6.7	7.3	18.3	8.1	4.9	1.5	-9.2	0.2	-2.8	-9.6				-1.9	-5.1			• •	8,5	3.4	6.1		2 0	2.3	1.

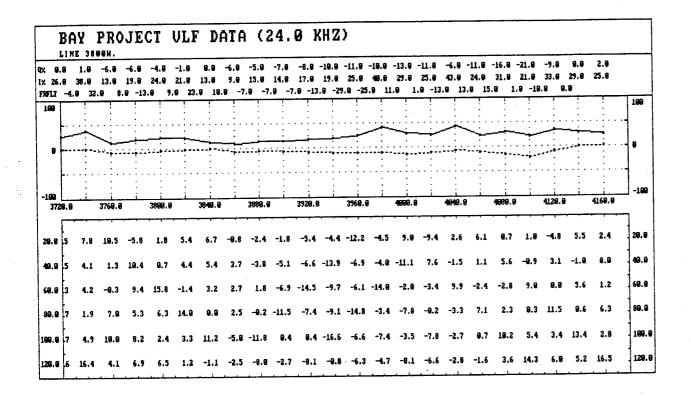
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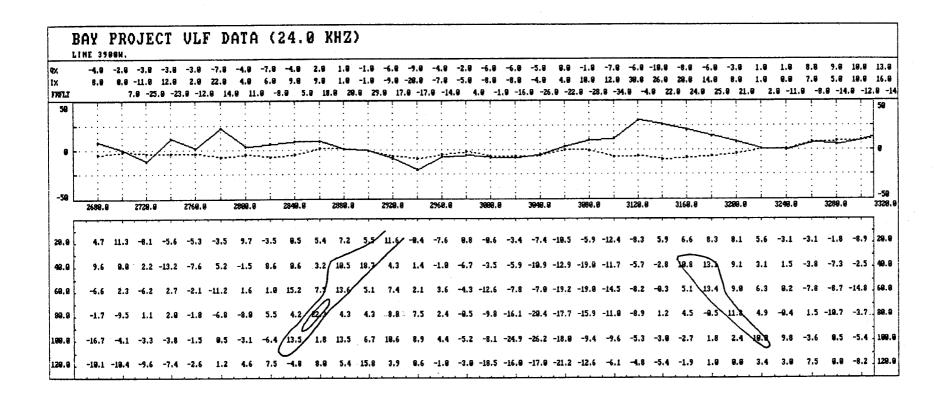
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69.8	8	5.6	3.4	2.1	9.7	3.6	1	7	-9.5	ə.1	-2.9	-2.1	\$ -8.	7 -8	.8 -	8.2 ·	-9.3	-5.8	-19.3	-13.7	-19.6	-24.	3 -13.1	7 -7.5	-3.4	-1.6	1.7	7.2	-8.3	68.9
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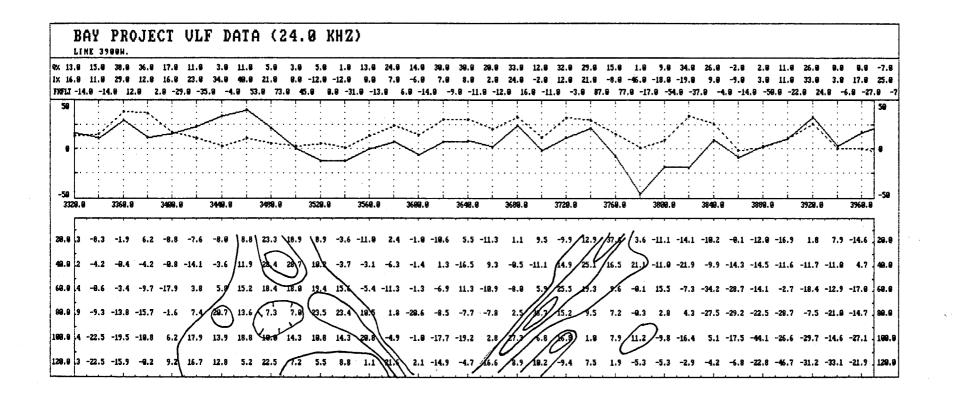
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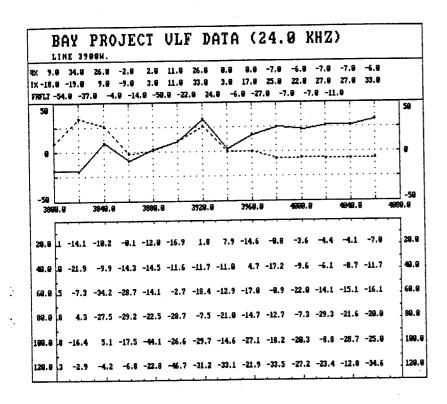
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10.0	2.0	15.3	14.9	1.5	14.9	1.3	-4.8	-4.0	-3.1	2.3	-2.2	-2.5	1.6	4.3	-2.5	19.4	2.9	3.3	-1.8	-4.4	-4.4	-14.8	-4.6	-12.7	-12.8	-2.6	-2.5	-1.6	-7.1	-3.1	4.1	8.6	49.9		
:e.e	4.5	14.9	14.0	15.1	-1.3	7.8	-2.9	-3.2	2.6	-4.9	-2.2	2.7	6.9	-5.2	3.7	2.2	12.7	-6.8	-3.3	2.4	-11.7	-12.8	-19.5	-6.2	-6.2	-9.5	-6.7	-7.8	-0.3	2.2	1.9	7.8	69.9		
×9.0	3.8	3.2	13.7	12.3	7.5	-2.1	6.7	-1.2	-7.6	-5.5	-3.8	5.4	-1.3	6.2	3.7	7.6	-3.9	4.8	-4.1	-19.5	-4.9	-15.4	-11.3	-13.9	-6.3	-19.3	-15.6	-3.9	-1.2	6.9	6.1	1.5	89.9		
19.0	-5.2	2.8	2.9	7.4	9.8	6.4	-8.8	3.1	-11.9	-8.3	8,4	-19,4	4.8	4.6	13.8	-3.1	8,2	2.8	9.1	-9.8	-13.1	-5.4	-18.4	-13.6	-19.3	-12.9	-9.3	-8.8	9.4	4.5	6.8	11.2	198.9		
x9.9	-5.6	-5.9	-4.5	-1.8	6.2	9.1	2.9	-11.4	4.5	-2.3	-14.1	-9.4	-6.5	8.5	-3.7	4.6	4.9	-2.2	-1.1	-3.8	-7.8	-9.5	-9.1	-15.2	-21.9	-29.5	-7.3	-7.8	-4.3	2.4	19.9	10.9	128.9		

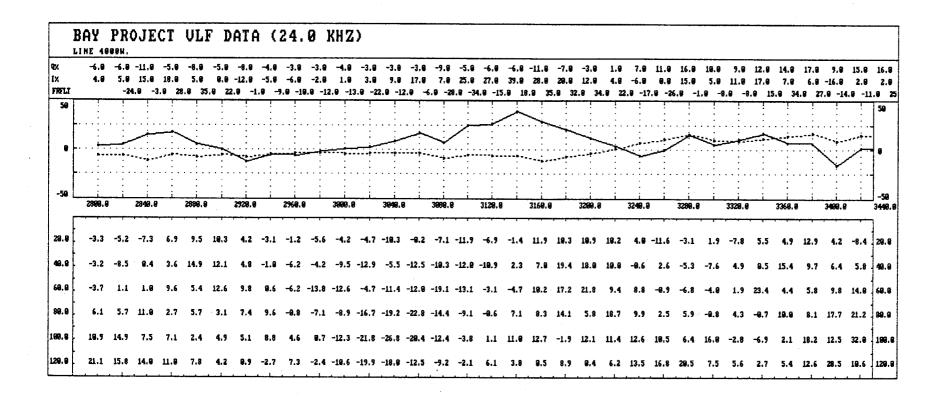


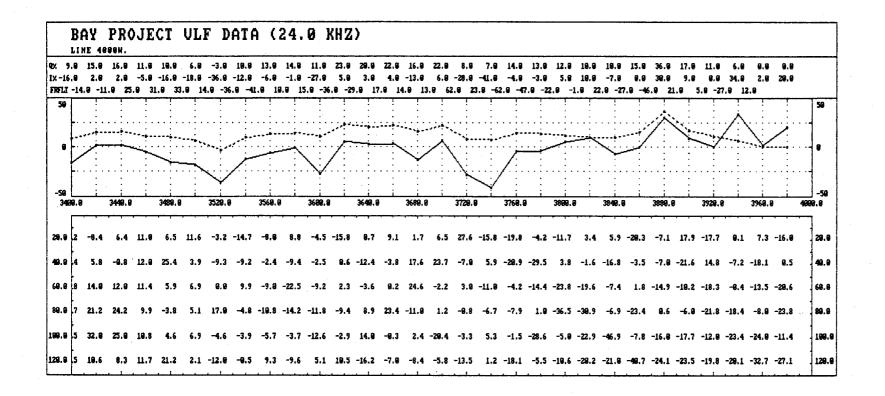


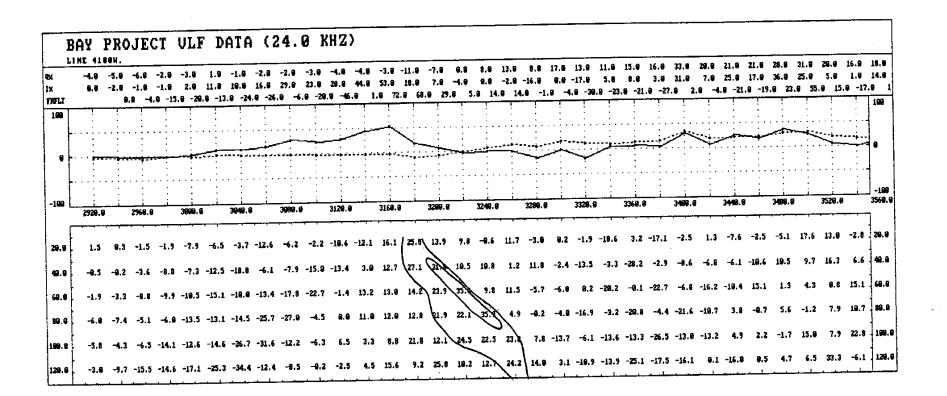




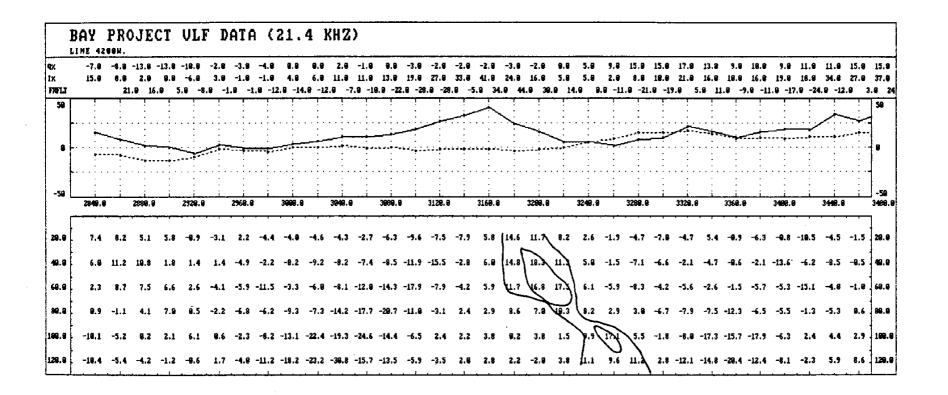




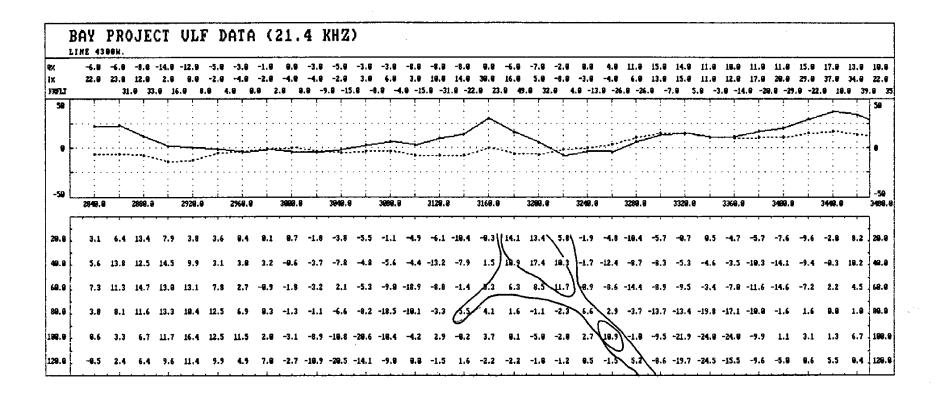


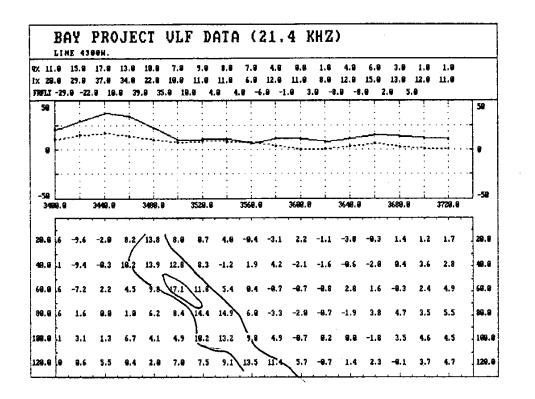


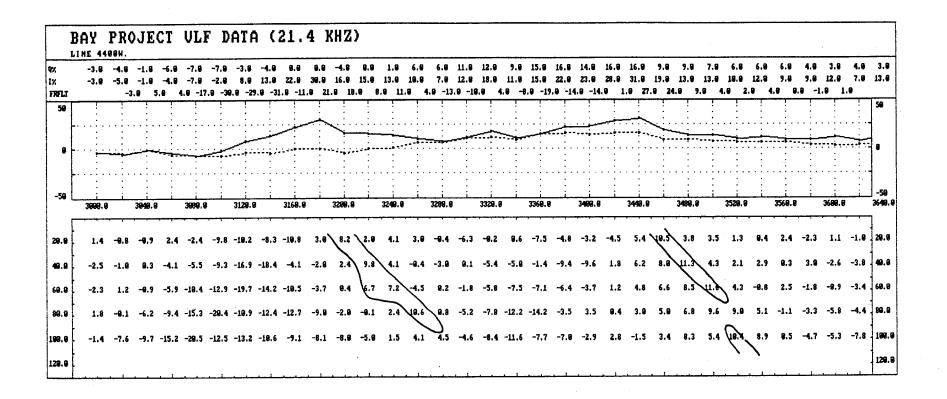
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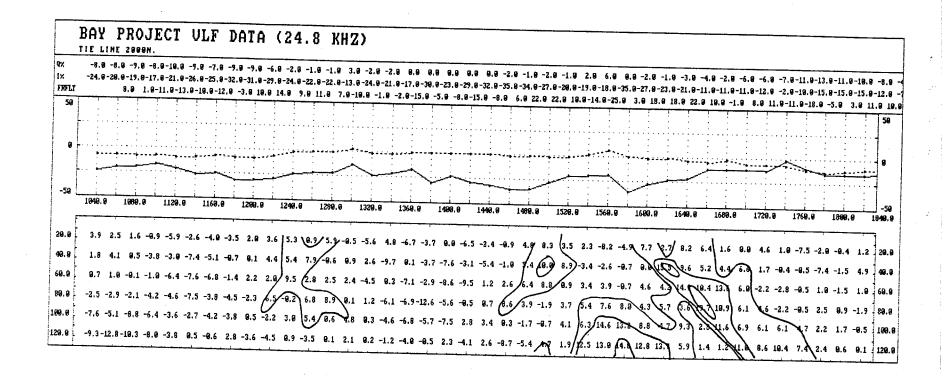


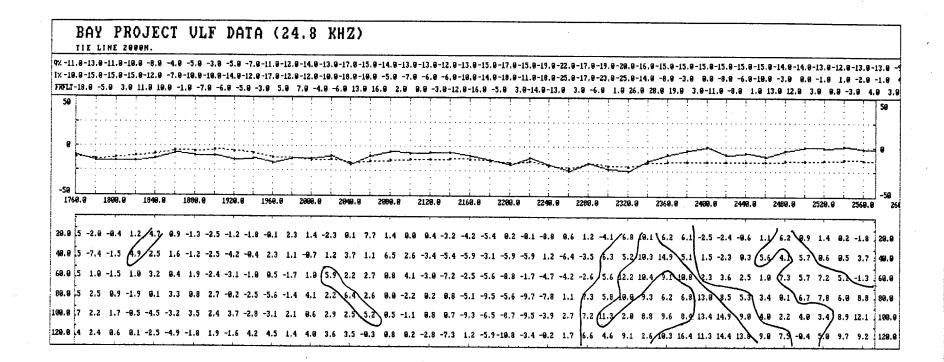
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49.9	6-6	.2	-8.5	-9.5	8.4	7,8	13.9	9,8	7.4	3.5	2.6	-2.6	-5.2	-2.6	-3.9	-8.2	2.3	2.4	2.2	-1.8	9.1		49.9
69.0	3 -15	i.1	-4.0	-1.0	2.6	12.8	13.1	16.3	7.0	5.0	1.4	-1.7	-5.8	-3.3	0.3	8.9	8.9	3.3	8.4	1.5	-2.9		68,9
89.9	.5 -1	.3	-5.3	9.6	2.7	7.3	15.7	19.6	16.9	6.1	-0.4	-1.3	-3.7	-3.5	-1.7	9.7	1.9	9.3	3.6	8.9	1.4	1	99. Q
32. 9	-3 2	.4	4.4	2.9	9.4	8.8	4.7	12.3	8.6	19.3	3.1	2.0	1.1	-1.9	-4.7	~Z.9	-2,1	8.7	-9.2	4.9	1.1	1	199.9
29.8	1 -2	.3	5.9	8.6	4.4	7.0	8.1	5.5	9.2	6.1	19.9	5.1	2.8	1.3	-9.8	-5.7	-5,5	-3.1	-1.9	-1.9	3.5	1	129.6

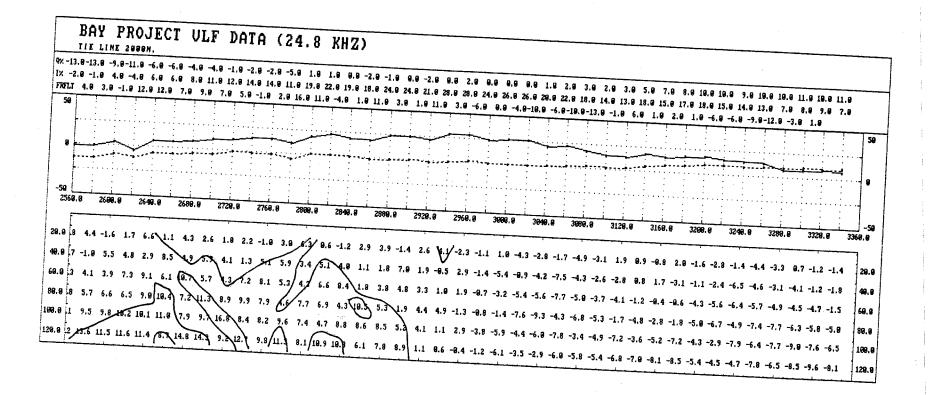


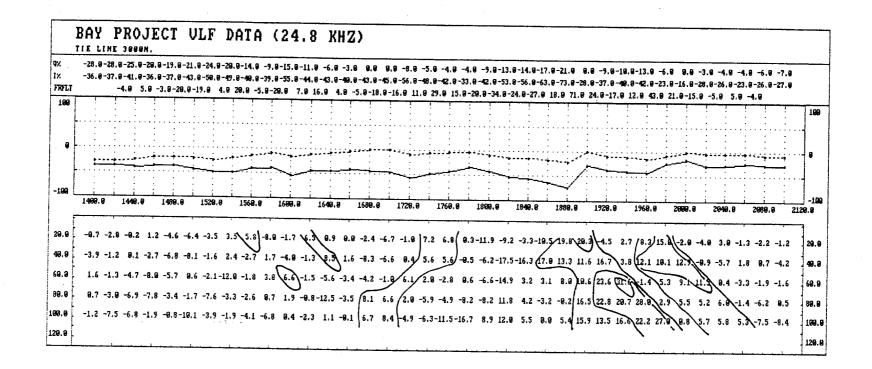


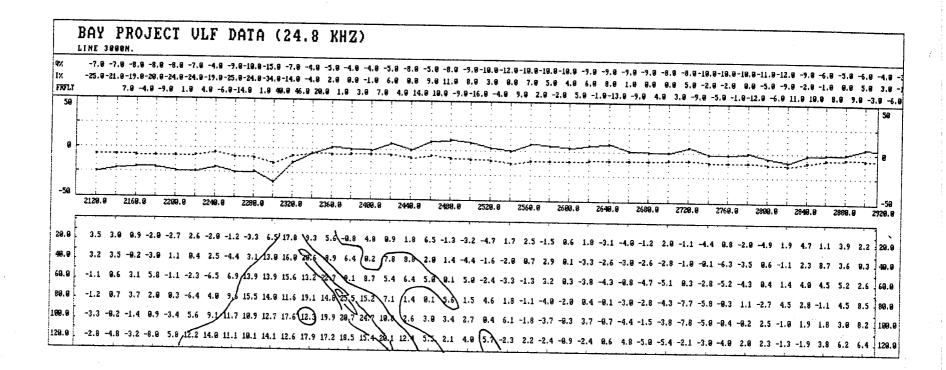


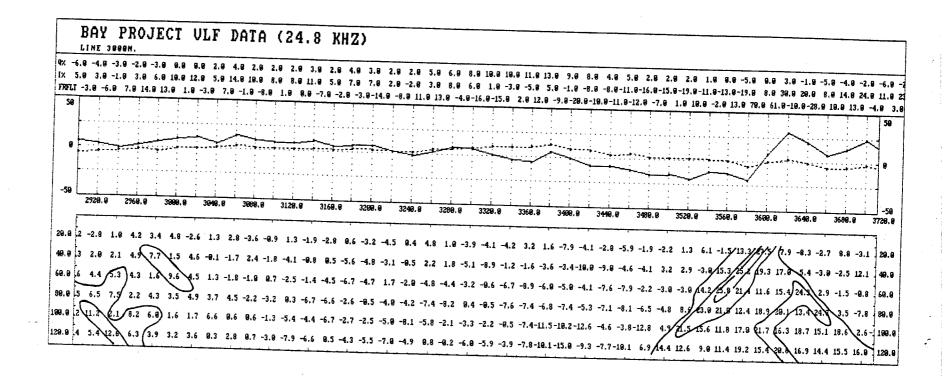


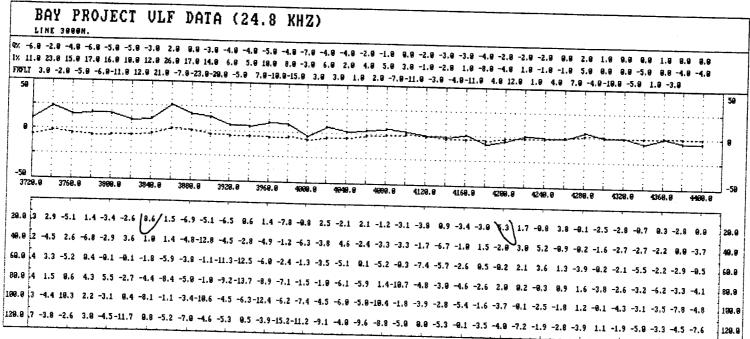










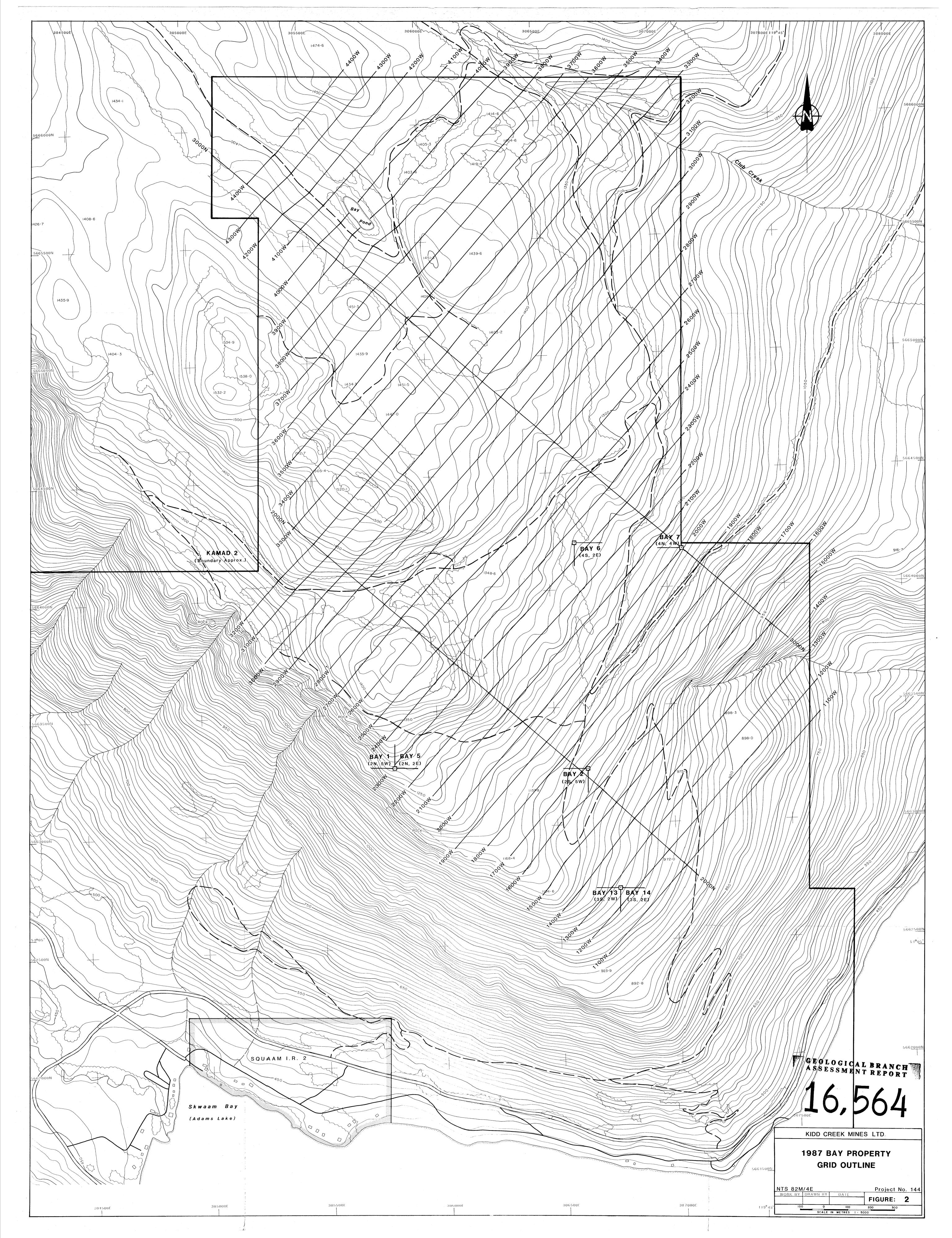


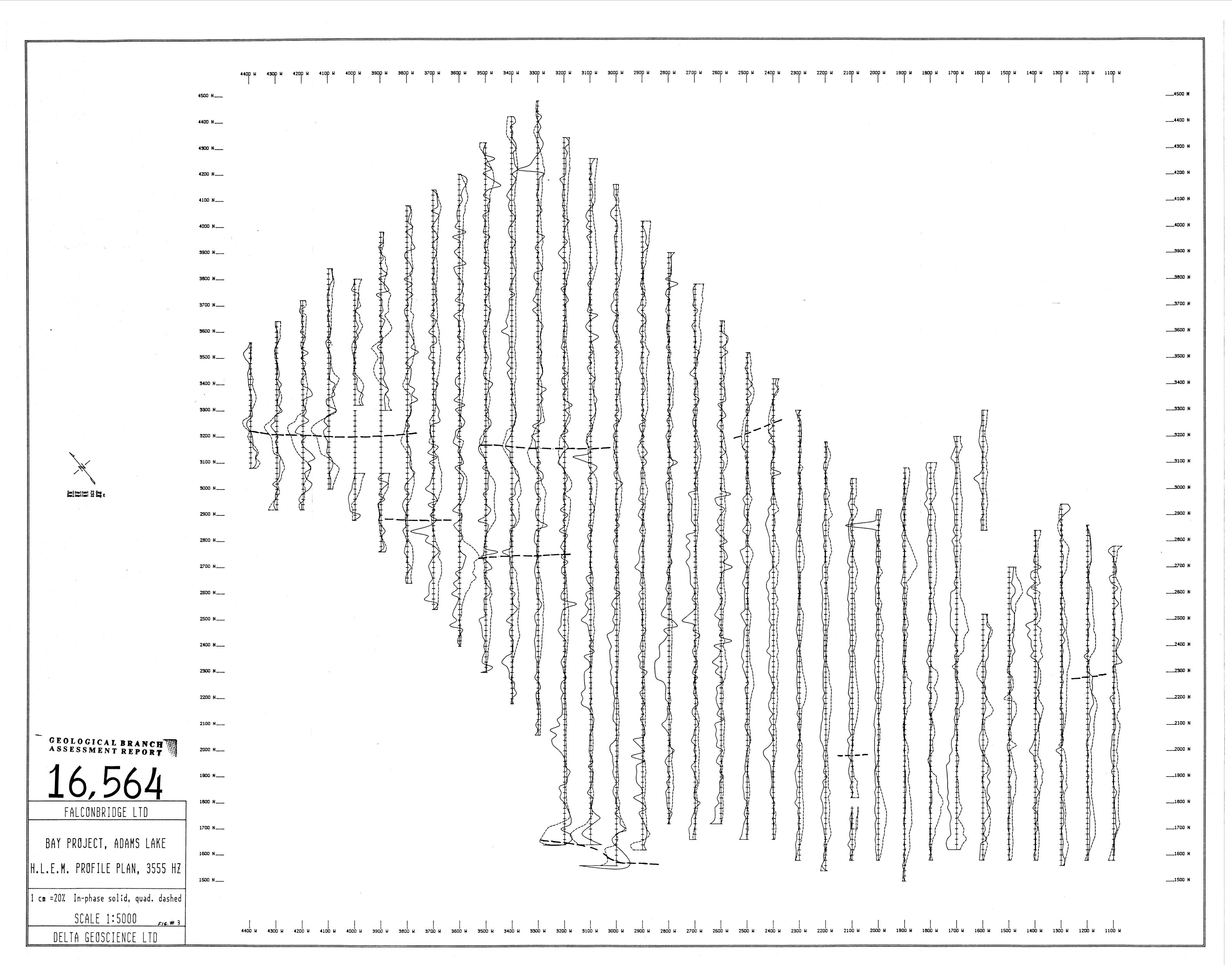
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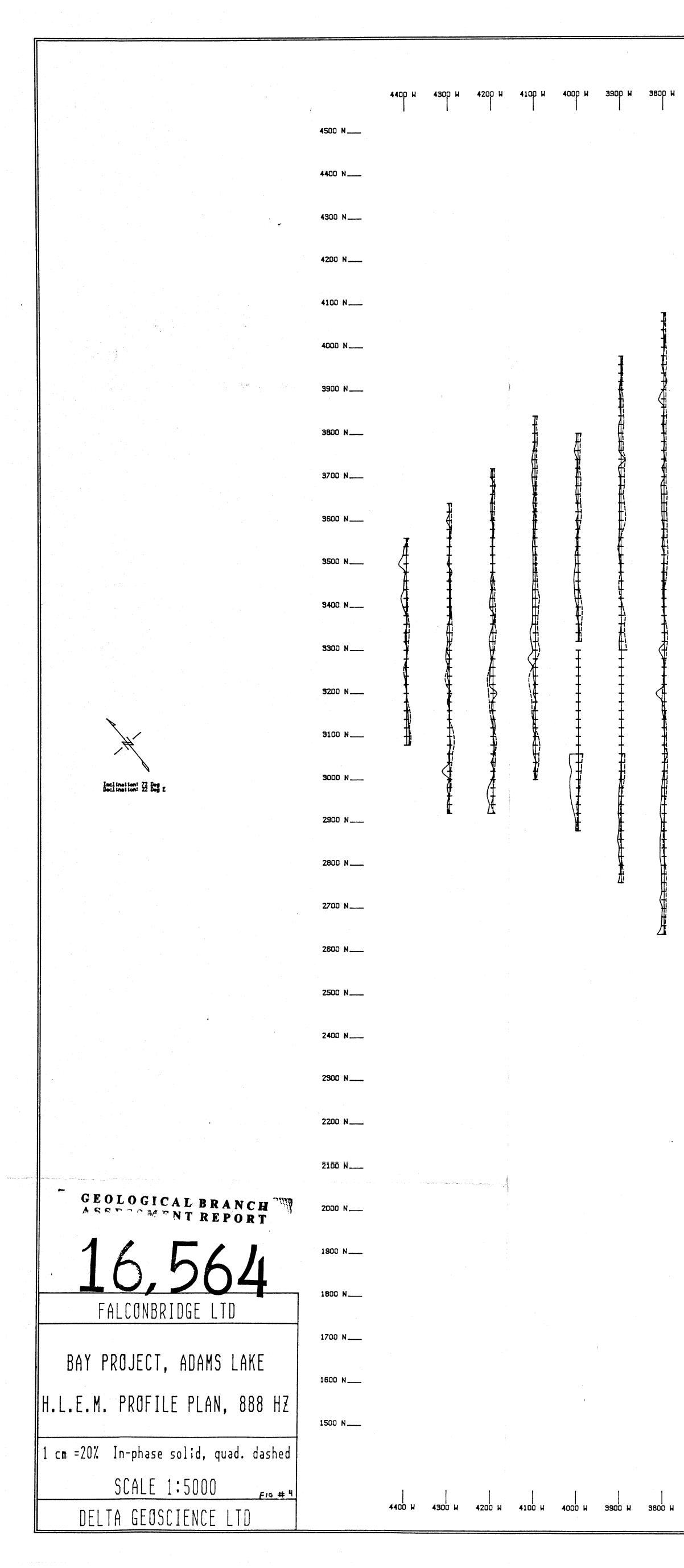
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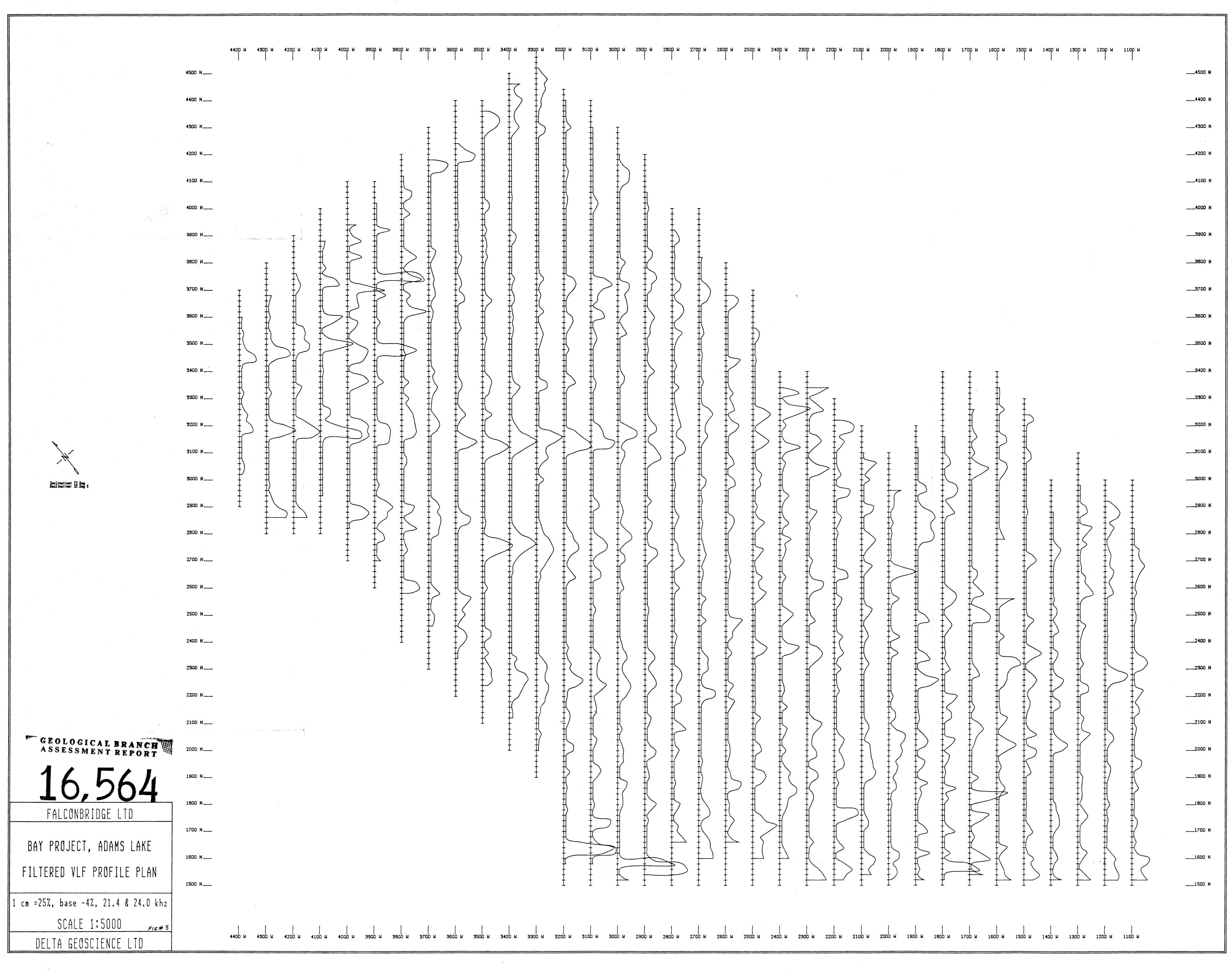


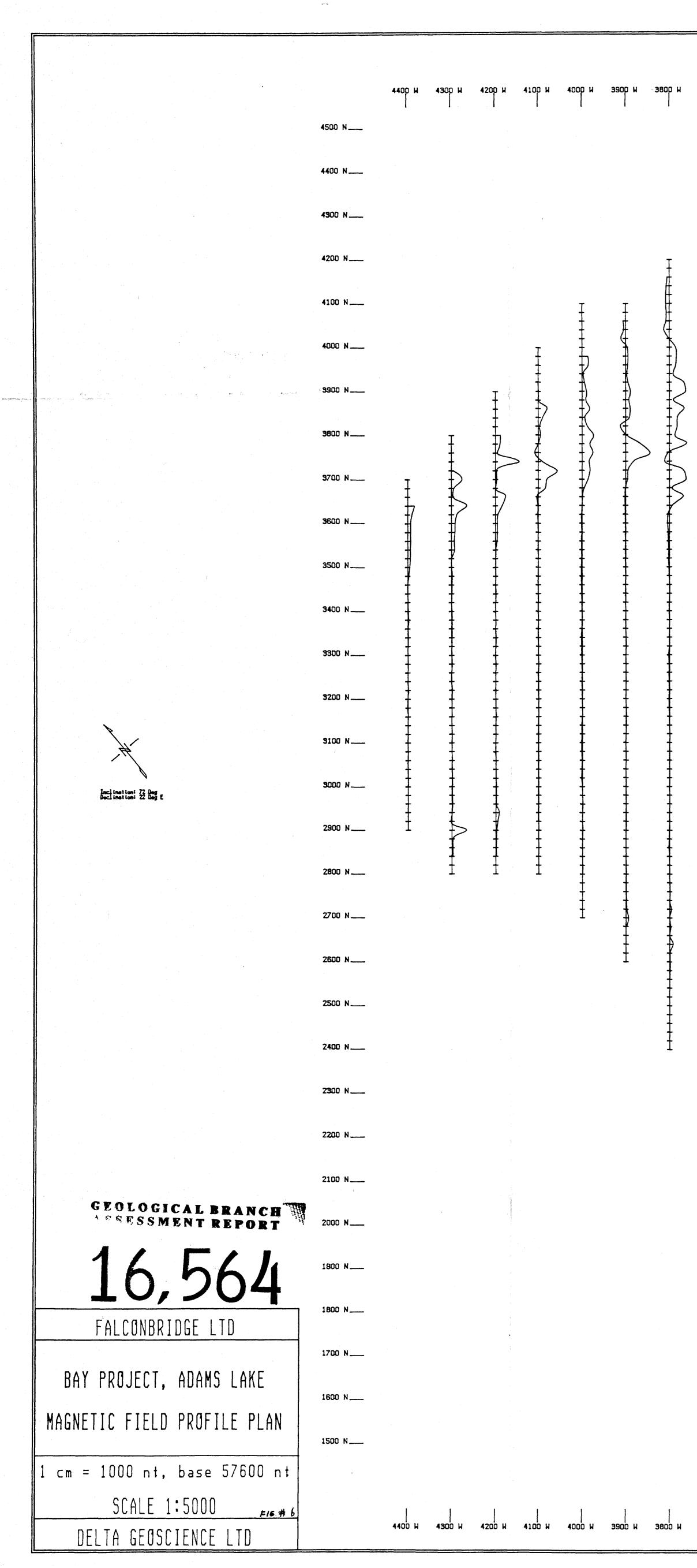




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							H H			₩.	, 	1600 N 1500 N





1300 H 1200 H 1100 H 1500 W 3500 W 3400 W 3300 W 3200 W 3000 H 2900 H 2500 1 2300 W 2200 W 2000 W 1900 W 1800 W 1700 W 1600 W 1400 W 3700 3100 W 2600 W 2400 W 2100 W ____4500 N . ____4400 N ____4300 N ____4200 N ____4100 N ----4000 N ____3900 N ____3800 N ____3700 N ____3600 N ____3500 N ____3400 N ___3300 N ____3200 N ____9100 N ____9000 N ____2900 N \$ ____2800 N ____2700 N ____2600 N ____2500 N f >.___2400 N +>____2300 N $^+$ > ____2200 N 1 ____2100 N +. $+ \rightarrow$ \triangleright ____2000 N ----- \rightarrow \downarrow ____1900 N ____1800 N Ţ \mathbf{F} \mathbf{r} ___1700 N \mathbb{P} \rightarrow \downarrow $\frac{1}{2}$ \geq ____1600 N ___1500 N 1200 W 1100 W 2200 W 2700 W 2500 W 2400 W 2100 W 2000 W 1800 W 1700 H 3200 H 2800 H 1900 W 1400 W

