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NEWMONT EXPLORATION OF CANADA LIMITED

GEOLOGICAL AND GEOCHEMICAL REPORT

FILMED

ON THE

OOTSA 1 CLAIM

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

1  
581  
16,581  
1

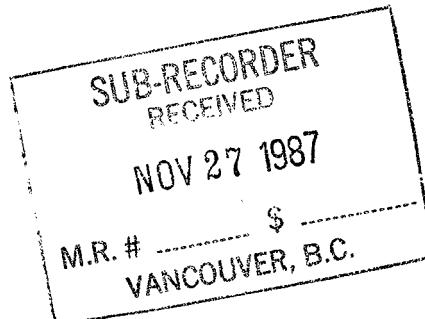
OMINECA MINING DIVISION

NTS 93F/11E

BY

JOHN NEBOCAT

NOVEMBER 25, 1987



LOCATION: Latitude:  $53^{\circ}32'02''$  North Longitude:  $125^{\circ}11'10''$  West

OWNER: NEWMONT EXPLORATION OF CANADA LIMITED

OPERATOR: NEWMONT EXPLORATION OF CANADA LIMITED

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## INTRODUCTION

### Location, Access, Topography

The OOTSA 1 mineral claim is situated in the Nechako Plateau, west-central British Columbia.

The nearest access is from Vanderhoof via the Kenney Dam road, across the dam to Emmett Lake via the Holy Cross road and from there along the Lucas Lake road--a distance of 113 km. The Lucas Lake road is accessible by 4x4 vehicles only, but the others are good quality logging roads.

The claim is typified by gently rolling topography and numerous small lakes and swamps. Relief is generally less than 300m, and on the claim, just over 100m; drainages are rare and for the most part seasonal.

Underbrush is scant, but deadfall is severe in old burns. Tree types consist primarily of jackpine, spruce and aspen.

### History

The OOTSA 1 claim was staked on August 24, 1986 and recorded on September 22, 1986 (record #7931). It is owned and operated by Newmont Exploration of Canada Limited. A fluorite-quartz alteration zone, found by Newmont in August, 1986, is roughly centered within the claim. No signs or records of previous work were found.



NEWMONT EXPLORATION OF CANADA LTD.

OOTSA I CLAIM- INDEX MAP

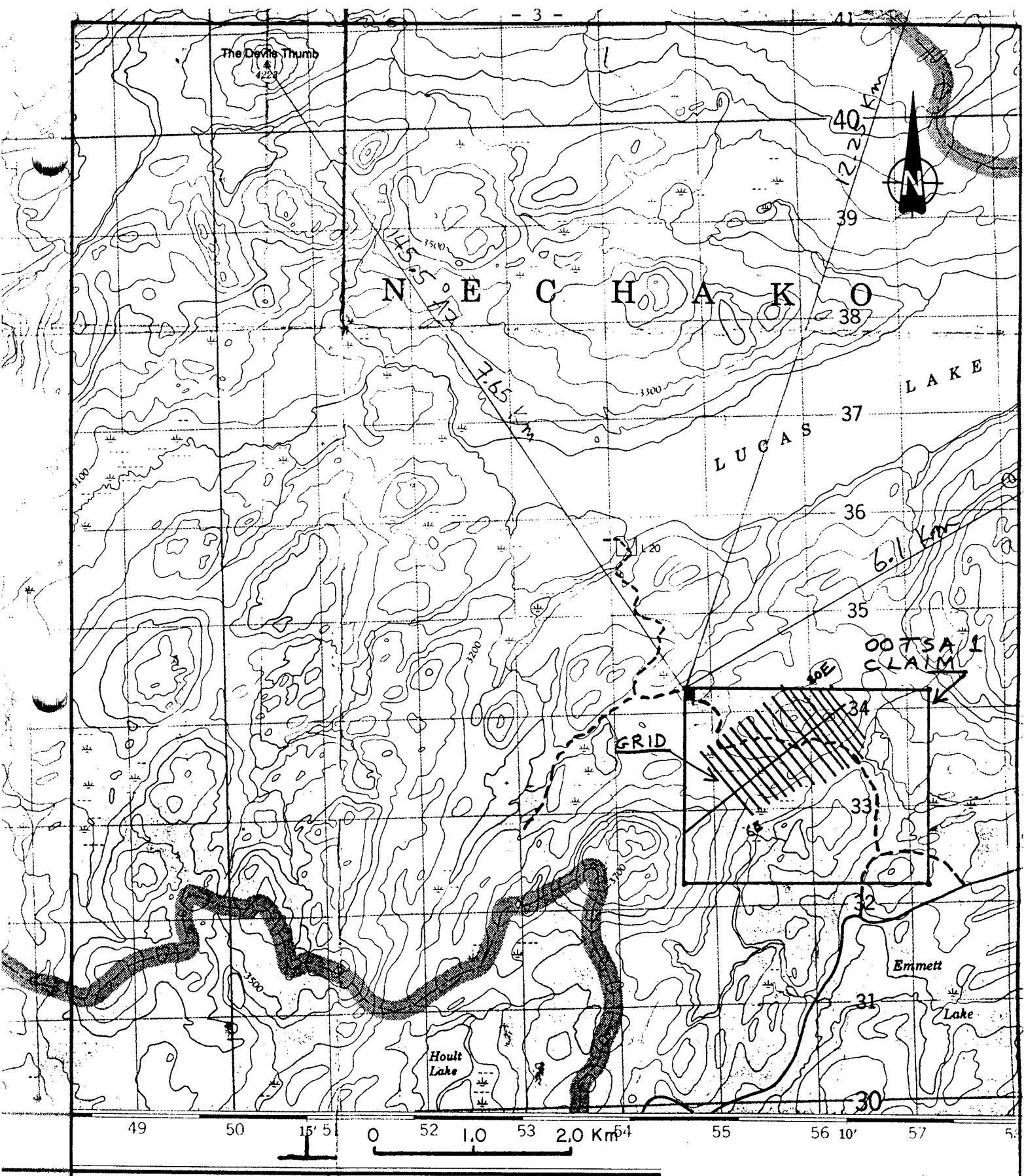
SCALE	LOCATION	DATE
SURVEY BY	DRAWN BY	NO.

93 F / II E

JN

25/11/87

FIGURE I



## CHESLATTA LAKE

COAST LAND DISTRICT RANGE 4

BRITISH COLUMBIA COLOMBIE-BRITANN

Scale 1:50 000 Échelle

0

MILES

1

2

NEWMONT EXPLORATION OF CANADA LTD.

### OOTSA I CLAIM - GRID LOCATION

SCALE	LOCATION	DATE
1 : 50,000	93F/IIE	25/11/87

SURVEY BY	DRAWN BY	NO.
JN	JN	FIGURE 2

### Summary of Work

A geologic sketch map was made in October, 1986, and 15 rock chip samples were taken from the quartz-fluorite showings.

In 1987, 12.675 km of line was cut using a chainsaw and axes; a grid was established on these lines using compasses, chains and pickets. Lines were cut every 100m, and stations were located at 25m intervals along the lines. Four hundred and three soil and five rock samples were collected in 1987.

An area of approximately 1.1 km<sup>2</sup> was geologically mapped at a scale of 1:2500.

### Claims

Newmont Exploration performed the work described within this report on the OOTSA 1 claim; particulars are listed as follows:

<u>Claim Name</u>	<u>Units</u>	<u>Staking Date</u>	<u>Record Date</u>	<u>Record No.</u>
Ootsa 1	20	Aug. 24/86	Sept. 22/86	7931

### GEOLOGY

#### General

The claim is underlain by felsic to intermediate volcanics and small intrusive bodies belonging to the Upper Cretaceous to Eocene Ootsa Lake Group (Tipper, 1963).

Exposure is poor, and outcroppings comprise less than 5% of the claim area. The claim has been extensively glaciated, evidenced by thick till cover and a prominent NE-trending crag and tail pattern seen in landsat images.

### Lithologies

Four lithologic suites were classified on the grid; however, other rock types exist on and around the claim.

Three variations of felsic volcanic were noted. (See Map 1) A pinkish-grey to maroon, glassy to flow-banded rhyolite (unit 1) outcrops along the eastern end of the grid. No internal structures revealed the direction or stratigraphic setting of the flow.

A buff-brown, fine grained, locally porphyritic latite or trachyte (unit 2) lies west of unit 1 and outcrops within an area 500m by 250m. On line 1800E, between 50S and 125S, the latite has been extensively fractured and filled with anastomosing veinlets of hematite; minor hematite veining occurs elsewhere in this unit.

A fine grained, flow-banded and locally brecciated, cream to grey-black rhyolite (unit 3) occurs between lines 1200E and 1500E, near the south end of the grid. The rock can be highly convoluted, and the lighter coloured layers exhibit pull-apart textures. The westernmost outcrop contains breccia and sub-rounded volcanic clasts in a buff to grey matrix. Whether this reflects a basal conglomerate or a fluvial inundation into the volcanic suite is not clear.

Unit 4, a fine grained, equigranular to porphyritic andesite, occupies the bulk of the grid--an area roughly 400m by 1100m. The holocrystalline texture, jointing pattern and spatial setting of the andesite suggests that it is a high-level intrusive. The andesite is in contact with the unit 3 rhyolite at the southern part of the grid and in contact with unit 2 at the north end. No zoning was observed in the stock.

### Structure

The region has been extensively dissected by block and transverse faulting, but this is evident mainly on aerial or landsat photographs. Northwesterly and northerly-trending faults intersect on the claims southwest of the grid; however, smaller, parallel structures pass through the rocks described above. These intersecting faults have helped to prepare the ground for the quartz-fluorite veining, but post-vein faulting has been seen in outcrop.

### Mineralization and Alteration

A zone of quartz-fluorite  $\pm$  potash feldspar  $\pm$  specular hematite alteration and veining occurs within units 3 and 4 near the SW end of the grid. The zone averages 75m -100m in width by 300m in length, and the vein systems trend in various directions. Quartz and fluorite generally occur together in larger veins (>5 cm across) with fluorite occupying the center of the vein. The larger veins generally contain subhedral crystals, but narrow stringers of quartz are generally milky or banded.

Fluorite is either cubic or octahedral, and colours of green, purple and white exist; individual crystals may be up to 2 cm across.

Locally, and usually associated with larger veins displaying breccia or slickenside features, potassic feldspar veins + platy hematite crystals occur.

Other than a minor amount of disseminated pyrite in unit 3 rhyolite, very little sulphide mineralization was seen on the grid.

The host rock andesite takes on a yellow-green to brown colour in the presence of the veins described above - probably due to fine epidote as a result of propylitic alteration. Calcite veins are seen proximal to the quartz-fluorite assemblage, but not within it.

## GEOCHEMISTRY

### Field Procedures

Soil samples were collected along the grid lines every 25m, where possible, and the B horizon, where developed, was sampled at a depth between 10 cm and 20 cm. Glacial "soil," or undeveloped till is common. The soil sample was collected using a mattock and stainless steel trowel and placed in a kraft paper envelope.

The analyses were done by Acme Analytical Laboratories, Vancouver, B.C.

403 soil and 20 rock samples were collected in 1986-1987; the analyses are listed in Appendices "A" and "B".

## Laboratory Procedures

### Soils

The samples are dried and then screened through an 80 mesh sieve; a 0.5 g sample of the -80 mesh material is weighed and digested in 3 ml of 3:1:3 HCl - HNO<sub>3</sub> - H<sub>2</sub>O solvent at 95°C for one hour and is then diluted to 10 ml with water. The digested sample is analyzed for 30 elements using an inductively coupled plasma instrument.

For Hg, a 0.5 g sample is digested with aqua regia and diluted with 20% HCl. Hg in the solution is determined by cold vapour AA using a F & J scientific Hg assembly. An aliquot of the extract is added to a stannous chloride/hydrochloric acid solution. The reduced Hg is swept out of the solution and passed into the Hg cell where it is measured by AA.

A 0.25 g sample is used for F determination. The sample is fused with sodium hydroxide and leached with 10 ml water. The solution is neutralized, buffered, adjusted to pH 7.8 and diluted to 100 ml. Fluorine is determined by Specific Ion Electrode using an Orion Model 404 meter.

For Au, a 10.0 g sample is ignited overnight at 600°C and digested with 30 mls hot dilute aqua regia, and 75 mls of clear solution obtained is extracted with 5 mls Methyl Isobutyl Ketone.

Au is determined in the MIBK extract by Atomic Absorption using background correction.

### Rocks

Rock samples are pulverized to -100 mesh and are analyzed using the same procedures outlined above. Au, however, is preconcentrated using fire assay techniques, then analyzed in the same manner as for soil samples.

## INTERPRETATION

### Soils

The entire 32 element suite was analyzed statistically, and the elements that seemed to have relevance or a significant correlation are plotted on Maps 3-6.

Although other moderate to strong correlations exist between certain lithophile elements, F, Hg, Zn and Ba were chosen as the most important.

### Fluorine

A statistical mean and threshold value (95th %-ile) of 140 ppm and 310 ppm, respectively, was determined.

Fluorine anomalies are spotty but generally coincide with the known fluorite occurrences on the grid, particularly in the andesite porphyry and flow-banded rhyolite between lines 1100E and 1400E. A few single point anomalies exist north of the showing in areas covered by overburden or soil, nonetheless, the anomalous sites are near the porphyry and probably are attributed to some buried veins in these locations.

### Mercury

The mean and threshold for Hg are 35 ppb and 85 ppb, respectively.

Mercury, like fluorine, exhibits a series of spot anomalies, though not generally coincident. In fact, four spot highs ranging from 560 ppb to 3000 ppb (see Map 4) line up in a general north-south direction along the center of the andesite porphyry stock. A fault parallel to this trend is believed to exist 200m west of the Hg anomalies, but no such structure is evident along the trend of the anomalies.

A 9800 ppb anomaly exist in the unit 2 trachyte/latite at L1800E x 100S. Hematite is abundant in the rock here, but no high values in Hg were obtained in the rock samples (discussed in the next section). A fault or fracture may underlie the soil at this site.

### Zinc

Values of 65 ppm and 135 ppm were determined to be the mean and threshold values, respectively, for Zn.

Zinc values are extremely spotty; some coincide with or are near Hg anomalies, but they do not suggest a trend parallel with the Hg. Again, anomalous Zn values coincide with the Hg anomaly on L1800E between 025S and 100S.

### Barium

A mean of 115 ppm Ba and threshold of 250 ppm Ba was determined. Barium follows the Zn highs closely; however, Ba tends to map a larger area and appears to stay within the limits of the andesite porphyry. It is possible that the stock is more alkalic and that the Ba reflects the presence of a Ba-bearing potassic feldspar, or barite associated with widespread calcite. Also, a spot high of 740 ppm occurs at L1800E x 100S.

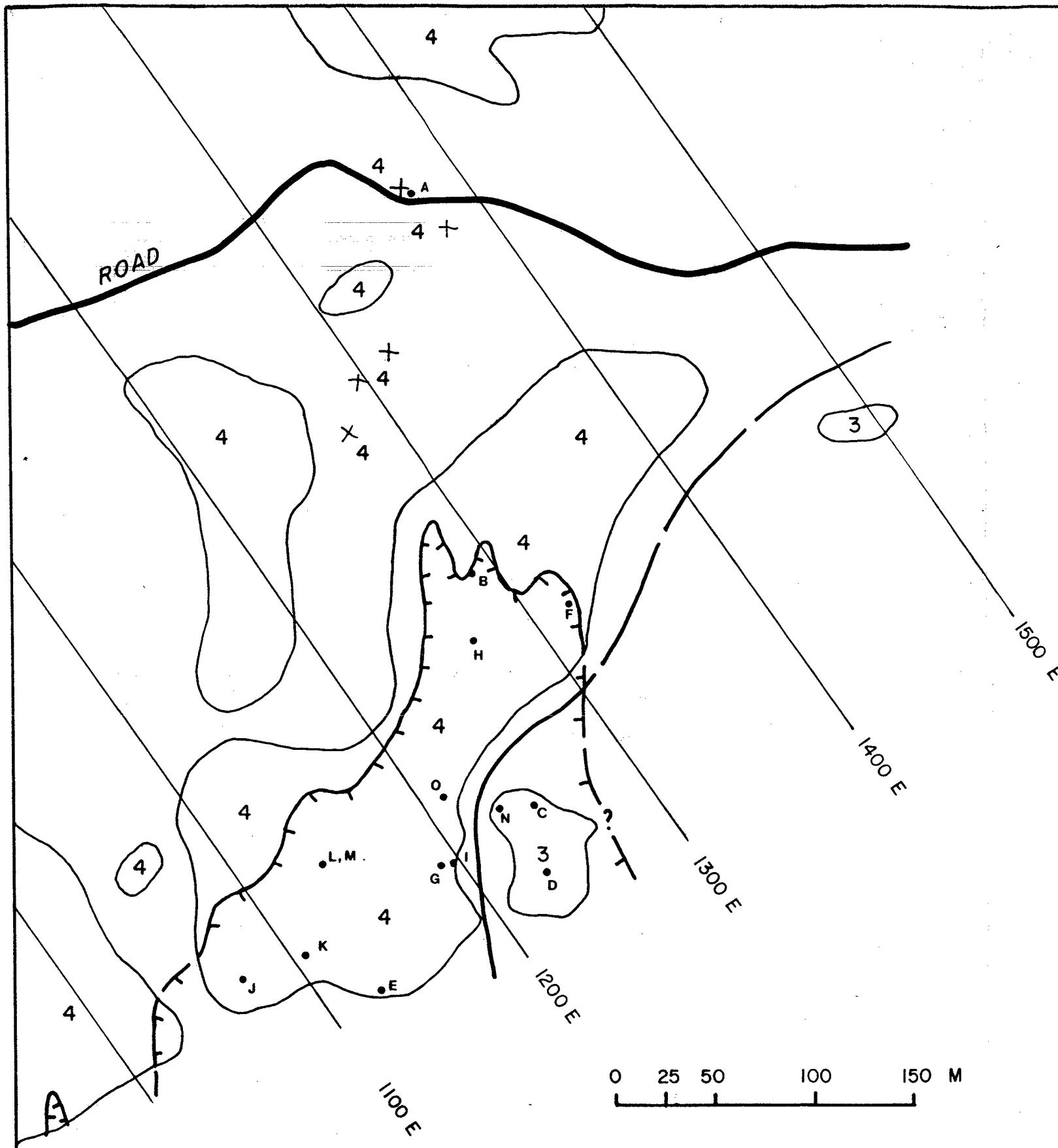
### Rocks

In 1986, the quartz-fluorite system between L1000E and L1300E had 15 rock samples taken from it; no significant precious or base metal values were obtained - the highest value ran 44 ppb Au (see Figure 3).

Arsenic values ranged from 8 ppm to 159 ppm, Hg from 10 ppb to 3300 ppb and F from 130 ppm to 150,000 ppm. In addition, anomalous B values correspond with the highest F values; but Acme Labs informed me that this was due to HF, formed by the digestion of fluorite, attacking boron-bearing analytical glassware.

Five rock samples taken on the grid in 1987 are shown on the geology map (see Map 1); the results are tabulated in Appendix "B".

Elevated values in Fe, Mn, and Hg occur in the latite/trachyte unit where hematite veining was observed; however no anomalous Zn or Ba values occur with them. A high Hg value (3500 ppb) is close to the soil sample which ran 9800 ppb Hg.



SITE	SAMPLE NUMBER	WIDTH (M)	As ppm	B ppm	Au ppb	Hg ppb	F ppm
A	07701	3	33	2	1	3300	630
B	I3180	GRAB	27	2	1	50	39,000
C	I3181	3	102	4	10	100	380
D	I3182	GRAB	8	4	1	200	570
E	I3183	3	13	3	2	250	830
F	I3184	GRAB	113	149	44	70	150,000
G	I3185	GRAB	24	191	1	10	40,000
H	I3188	1.2	14	2	1	130	3500
I	I3094	1.3	15	96	2	90	106,000
J	I3142	6.5	14	2	3	230	970
K	I3143	1.5	24	222	4	100	72,500
L	I3144	3.5	51	4	5	160	1000
M	I3145	4	26	4	2	200	1150
N	I3146	3.5	159	8	2	60	770
O	I3147	2.5	55	3	1	1400	130

4 ANDESITE PORPHYRY

3 FLOW-BANDED RHYOLITE

1 LIMIT OF QUARTZ-FLUORITE ALTERATION

### GEOLOGICAL BRANCH ASSESSMENT REPORT

**16,581**

NEWMONT EXPLORATION OF CANADA LTD.

OOTSA I CLAIM - ROCK SAMPLES

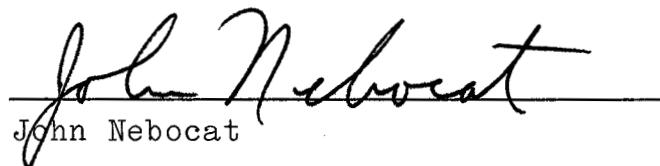
SCALE 1: 2500	LOCATION 93 F/11E	DATE 25/11/87
SURVEY BY JN	DRAWN BY JN	NO. FIGURE 3

### CONCLUSIONS

1. A zone of hydrothermal alteration, accompanied by local, intense quartz-fluorite veining, exists over an area 75m by 300m on the OOTSA 1 claim.
2. The veining appears to be proximal to the intersection of major fault structures.
3. The veining and alteration post-dates the andesite porphyry stock as well as the volcanics it intrudes.
4. The hematite veinlets hosted by the latite/trachyte flow are possibly related to the emplacement of the andesite porphyry stock.
5. No significant precious or base metal values were obtained from the property, where tested.

### RECOMMENDATIONS

1. No further work is recommended in the immediate area of the grid.
2. The presence of quartz/fluorite veining, in conjunction with propylitic alteration and spotty Hg anomalies, warrants further exploration in the area for epithermal, precious metal deposits.

  
John Nebocat

COST STATEMENT

LABOUR

1986

J. Nebocat	(Oct. 4-5)	2 days @ \$134.15/day	\$268.30
H. Klatt	(Oct. 4-5)	2 " @ \$ 94.69/day	189.38

1987

J. Nebocat	(Aug. 21-25)	5 days @ \$153.67/day	768.35
H. Klatt	(Aug. 21-25)	5 " @ 112.14/day	560.70
A. Campbell	(Aug. 21-24)	4 " @ 97.19/day	388.76
K. Atkin	(Aug. 21-24)	4 " @ 124.61/day	<u>498.44</u>
			\$ 2,673.93

CAMP COSTS

\$40/man-day x 20 man-days	800.00
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VEHICLE

1981 Toyota 4x4 \$65/day x 5 days	325.00
-----------------------------------	--------

MISCELLANEOUS

Supplies, fuel, etc	500.00
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GEOCHEMISTRY

1986: 15 rocks for 30 el. ICP, Hg, F, Au @ \$20.50/sample	\$ 307.50
--	-----------

1987: 5 rocks for 30 el. ICP, Hg, F, Au @ \$21.25/sample	106.25
---	--------

403 soils fro 30 el. ICP, Hg, F, Au @ \$17.50/sample	<u>7,052.50</u>	7,466.25
---	-----------------	----------

DRAFTING, COMPUTER TIME, DATA COMPILATION, TYPING	<u>1,500,00</u>
---	-----------------

Total	<u>\$13,265.18</u>
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### STATEMENT OF QUALIFICATIONS

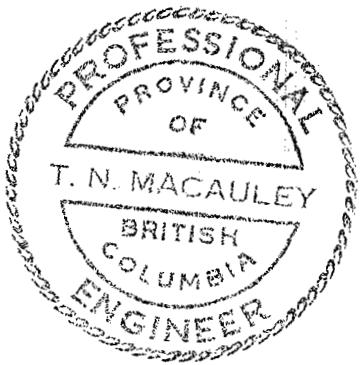
I, John Nebocat, hereby certify that:

1. I am a geologist in the employ of Newmont Exploration of Canada Limited;
2. I am a graduate of the Montana College of Mineral Science and Technology, 1986, Butte, Montana;
3. I am an engineer-in-training with the Association of Professional Engineers of British Columbia;
4. I have performed and supervised the work described in this report.



John Nebocat  
John Nebocat

I hereby certify that the work described in this report was done under my direction.



T.N. Macauley  
T. N. Macauley, P. Eng.  
Exploration Manager-Western Division

Soils for by A.A. 10 gm sample  
Page 2

NEWMONT EXPLORATION PROJECT-337 FILE # 87-3943

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P PPM	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU\$ PPB	HG PPB	F PPM
2995	1	5	11	39	.1	8	3	416	1.62	3	5	ND	3	24	1	2	3	31	.19	.036	12	15	.18	63	.08	4	1.05	.01	.05	1	1	40	100
2996	1	6	8	67	.1	13	5	472	2.25	2	5	ND	3	19	1	2	2	39	.19	.051	13	19	.23	91	.08	2	1.85	.01	.05	1	1	30	100
2997	1	27	6	112	.4	25	10	2373	4.06	2	6	ND	8	138	1	2	3	47	1.49	.080	43	35	.56	237	.02	2	4.67	.02	.21	1	1	90	360
2998	1	5	6	76	.1	10	3	180	1.71	2	5	ND	3	19	1	4	2	29	.17	.059	13	14	.14	76	.06	2	1.19	.01	.05	1	1	30	70
2999	1	5	5	37	.1	6	2	153	1.35	2	5	ND	1	23	1	2	2	24	.22	.016	13	12	.19	57	.08	3	.87	.01	.05	1	1	40	80
3000	1	5	7	35	.1	9	4	243	1.88	3	5	ND	4	18	1	2	2	34	.16	.050	11	16	.17	85	.07	5	1.05	.01	.05	2	1	60	70
3001	1	11	6	59	.1	12	5	245	2.24	6	5	ND	2	22	1	2	2	43	.28	.044	9	17	.29	64	.12	2	1.30	.01	.06	1	1	20	90
3002	1	7	6	43	.1	10	4	224	1.87	4	5	ND	5	27	1	2	2	33	.27	.041	13	14	.23	71	.08	2	.91	.01	.08	2	1	90	120
3003	1	9	7	52	.1	10	3	189	1.94	2	5	ND	3	23	1	2	2	33	.23	.050	13	16	.21	80	.08	6	.96	.02	.07	1	1	70	130
3004	1	4	2	75	.1	8	5	1059	1.83	3	5	ND	2	35	1	2	2	32	.35	.050	12	15	.16	112	.06	4	.91	.01	.09	1	1	60	70
3005	1	9	4	51	.1	10	4	316	1.50	4	5	ND	1	27	1	2	2	26	.24	.031	15	12	.22	65	.08	5	.81	.02	.06	1	1	60	130
3006	1	10	8	48	.1	8	5	235	1.90	3	5	ND	4	27	1	2	2	36	.18	.028	12	17	.20	72	.09	5	.93	.02	.05	1	1	40	80
3007	1	7	14	97	.1	8	4	269	1.95	6	5	ND	3	11	1	2	2	33	.11	.074	12	15	.14	66	.05	4	1.44	.01	.04	1	1	30	70
3008	1	5	6	44	.1	9	3	151	1.31	3	5	ND	1	18	1	3	2	23	.15	.022	11	11	.16	69	.07	2	.85	.01	.05	1	1	110	70
3009	1	10	6	44	.2	10	4	184	1.84	5	7	ND	4	26	1	2	3	35	.24	.032	11	15	.22	75	.09	2	.96	.02	.07	1	1	80	70
3010	1	4	9	62	.2	7	4	494	1.65	2	5	ND	3	22	1	2	2	29	.22	.086	11	14	.13	76	.06	2	1.03	.01	.06	1	2	30	70
3011	1	10	7	48	.1	10	4	178	1.97	4	5	ND	4	25	1	3	2	35	.22	.041	13	16	.22	75	.08	3	1.10	.02	.07	1	1	60	130
3012	1	6	11	36	.1	6	3	165	1.49	2	5	ND	3	24	1	2	2	28	.22	.016	13	13	.20	69	.09	2	.77	.01	.07	2	1	40	70
3013	1	7	12	80	.1	12	4	324	2.06	8	5	ND	4	22	1	2	2	36	.23	.056	12	16	.24	87	.08	2	1.33	.01	.07	1	1	220	110
3014	1	6	3	49	.3	8	3	185	1.49	4	5	ND	4	24	1	2	2	28	.23	.019	12	12	.18	65	.08	7	.74	.01	.07	1	1	40	100
3015	1	6	6	31	.1	8	3	205	1.54	4	5	ND	1	25	1	2	2	31	.20	.016	11	12	.18	77	.07	4	.80	.01	.07	1	1	90	80
3016	2	7	11	77	.1	9	3	521	1.69	4	5	ND	4	19	1	2	2	30	.17	.023	14	12	.19	93	.07	2	1.32	.01	.05	1	1	50	100
3017	2	9	12	67	.1	9	4	496	2.42	3	5	ND	4	19	1	2	2	36	.19	.042	16	17	.21	116	.04	8	1.70	.01	.09	1	1	60	110
3018	8	11	25	164	.2	7	5	2340	2.33	5	5	ND	3	31	1	2	2	26	.25	.065	18	13	.17	180	.02	2	1.56	.01	.06	1	1	70	70
3019	1	36	11	62	.3	23	5	251	2.22	2	5	ND	4	209	1	3	2	25	1.92	.070	50	31	.35	239	.03	2	3.53	.02	.12	1	1	80	180
3020	1	6	10	39	.1	10	4	172	1.71	5	7	ND	3	27	1	2	2	30	.27	.028	15	15	.20	76	.08	2	.91	.01	.07	1	1	20	80
3021	1	7	7	38	.1	8	3	204	1.57	3	5	ND	3	21	1	2	2	29	.19	.018	12	14	.17	60	.08	8	.76	.01	.06	1	1	60	70
STD C/AU-S	19	60	38	134	7.1	72	27	1071	4.01	37	17	8	42	49	18	17	24	56	.50	.083	39	61	.90	179	.08	38	1.86	.06	.12	14	53	1300	-
3022	2	14	17	63	.3	12	10	1392	2.55	6	5	ND	4	42	1	2	2	39	.40	.062	25	19	.36	122	.05	2	1.71	.02	.12	1	1	50	210
3023	1	6	10	38	.1	9	4	212	1.72	5	5	ND	3	20	1	2	2	31	.16	.036	11	15	.19	72	.08	5	1.01	.02	.04	1	1	80	70
3024	1	7	7	35	.2	6	3	249	1.43	5	5	ND	3	25	1	2	2	25	.22	.023	13	12	.20	65	.08	2	.78	.01	.07	2	1	60	80
3025	1	11	9	49	.1	9	4	609	1.68	7	5	ND	3	41	1	2	2	28	.36	.032	20	14	.25	95	.08	3	1.09	.01	.09	1	2	70	100
3026	1	8	10	42	.1	8	4	311	1.53	5	5	ND	4	26	1	2	4	25	.23	.019	15	13	.24	65	.08	2	.93	.01	.07	2	1	50	100
3027	1	7	12	90	.1	6	5	601	2.05	6	5	ND	2	53	1	2	2	32	.55	.127	14	16	.16	130	.06	2	1.26	.01	.11	1	1	60	70
3028	1	6	10	102	.1	5	5	878	1.88	6	5	ND	2	22	1	3	2	34	.19	.042	12	14	.15	94	.06	3	1.29	.01	.05	1	1	30	70
3029	2	7	11	67	.1	9	5	245	2.15	6	5	ND	3	25	1	2	2	38	.26	.016	12	13	.25	114	.08	7	1.13	.01	.05	1	1	40	80
3030	1	7	15	60	.1	7	4	458	1.77	4	6	ND	3	32	1	2	2	35	.25	.027	11	15	.12	97	.06	2	.82	.01	.04	1	1	20	70

## NEWMONT EXPLORATION PROJECT-337 FILE # 87-3943

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SAMPLE#	MD PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA Z	P PPM	LA PPM	CR PPM	M6 %	BA PPM	TI %	B PPM	AL Z	NA %	K %	W PPM	AU# PPB	HG PPM	F PPM
3031	1	49	14	61	.4	29	7	271	2.28	9	5	ND	11	190	1	4	2	29	1.86	.126	86	28	.37	233	.02	2	4.31	.02	.11	2	1	100	350
3032	3	50	19	53	.6	25	6	718	2.71	10	5	ND	6	155	1	2	2	35	1.55	.087	101	21	.46	190	.02	3	2.64	.01	.19	1	1	180	240
3033	1	6	12	51	.3	9	3	235	1.62	2	5	ND	5	32	1	2	2	33	.34	.036	10	15	.16	63	.08	2	.71	.01	.06	1	1	20	40
3034	1	9	14	33	.2	11	4	204	1.75	4	5	ND	3	26	1	2	2	33	.25	.040	11	16	.18	59	.07	2	.74	.01	.06	1	1	60	90
3035	1	8	14	34	.1	10	4	273	1.62	2	5	ND	4	27	1	2	3	30	.27	.046	11	14	.17	76	.07	3	.75	.01	.10	1	1	40	80
3036	1	6	11	38	.2	6	4	518	1.39	2	5	ND	4	20	1	2	3	26	.22	.042	11	11	.12	84	.06	2	.68	.01	.08	1	1	20	40
3037	1	5	7	48	.1	8	4	315	1.56	2	5	ND	3	27	1	2	2	27	.26	.085	11	14	.16	81	.07	2	.82	.01	.07	1	1	10	70
3038	1	7	14	43	.1	9	4	357	1.72	4	5	ND	3	34	1	2	2	31	.35	.069	12	14	.17	87	.07	2	.84	.01	.11	1	1	30	80
3039	1	7	11	46	.1	12	5	396	1.80	2	5	ND	3	30	1	2	2	33	.27	.056	12	15	.18	80	.07	2	.89	.01	.07	1	1	40	90
3040	1	12	14	41	.1	11	4	265	1.66	2	5	ND	2	32	1	2	2	29	.24	.029	18	13	.25	81	.06	2	1.15	.02	.06	1	1	40	140
3041	1	4	10	39	.1	6	3	290	1.23	2	5	ND	3	22	1	2	2	24	.21	.017	10	9	.15	57	.06	2	.71	.01	.06	1	1	30	60
3042	2	14	18	46	.1	10	6	522	1.98	4	5	ND	2	31	1	2	2	34	.25	.036	16	14	.23	92	.04	2	1.17	.01	.06	1	1	20	130
3043	1	9	13	46	.2	11	4	237	1.70	2	5	ND	4	31	1	2	2	31	.38	.047	13	14	.21	83	.06	4	.87	.01	.13	1	1	40	130
3044	1	6	16	76	.1	8	5	729	1.58	2	5	ND	5	21	1	2	2	29	.18	.025	13	14	.18	89	.07	2	.94	.01	.06	1	1	20	90
3045	1	12	13	69	.1	10	5	942	1.64	5	5	ND	2	65	1	2	2	29	.61	.046	14	14	.23	123	.06	2	1.03	.01	.09	1	1	60	80
3046	1	7	10	38	.1	8	4	351	1.55	3	5	ND	1	23	1	2	2	30	.18	.020	12	14	.21	84	.07	2	.83	.01	.05	1	1	130	100
3047	1	10	14	79	.2	12	5	391	1.70	4	5	ND	2	23	1	2	2	29	.22	.032	11	12	.23	173	.05	2	1.25	.01	.05	1	1	30	80
3048	2	13	22	57	.1	10	5	240	2.56	5	5	ND	3	19	1	2	2	50	.20	.025	11	17	.24	156	.05	2	1.62	.01	.06	1	2	40	110
3049	2	20	15	133	.1	7	8	748	3.22	3	5	ND	2	97	1	2	2	52	.62	.110	10	11	.14	192	.02	5	.82	.01	.09	1	1	250	160
3050	1	8	11	30	.2	9	4	260	1.73	4	5	ND	4	22	1	2	2	35	.17	.019	11	14	.18	70	.06	4	.76	.01	.06	1	1	50	120
3051	1	4	10	54	.1	8	4	353	1.43	2	5	ND	2	20	1	2	2	28	.23	.058	10	13	.16	127	.07	5	.77	.01	.06	1	1	20	120
3052	1	13	17	56	.2	11	6	886	2.30	6	5	ND	3	91	1	2	2	38	.77	.040	18	19	.35	224	.05	2	1.54	.02	.08	1	1	70	190
3053	2	31	21	137	.2	22	8	1151	3.76	3	5	ND	6	158	1	2	2	44	1.29	.042	46	26	.64	506	.03	2	3.41	.02	.14	1	1	110	200
3054	1	10	15	76	.1	9	6	813	2.00	5	5	ND	2	21	1	2	2	38	.18	.066	12	15	.17	142	.06	2	1.34	.01	.09	1	1	30	60
3055	1	7	14	43	.1	6	3	295	1.44	2	5	ND	2	35	1	2	2	31	.43	.024	10	12	.13	95	.05	2	.63	.01	.07	1	2	20	40
3056	2	14	13	38	.1	7	5	195	2.31	4	5	ND	3	18	1	2	3	43	.17	.022	11	16	.19	136	.05	3	.87	.01	.07	1	1	1300	130
3057	1	9	14	53	.1	8	4	446	1.71	3	5	ND	2	26	1	2	2	30	.27	.023	14	13	.22	243	.05	4	1.16	.01	.08	1	1	40	80
3058	2	9	12	41	.1	8	5	551	2.04	4	5	ND	2	26	1	2	2	41	.28	.025	10	13	.19	228	.05	2	1.01	.01	.06	2	1	70	80
STD C/AU-S	20	60	40	127	7.3	69	27	1057	4.02	40	18	8	40	49	18	17	21	56	.46	.089	38	60	.87	173	.07	36	1.94	.06	.12	13	52	1300	-
3059	2	14	15	76	.1	11	8	1641	2.01	2	5	ND	1	47	1	2	2	33	.42	.113	16	17	.16	327	.05	3	1.32	.01	.06	1	1	20	60
3060	1	10	14	56	.1	9	5	302	1.95	2	5	ND	3	20	1	2	2	37	.22	.029	12	15	.22	205	.05	2	1.29	.01	.06	1	1	80	100
3061	1	6	14	48	.1	5	4	201	1.52	2	5	ND	2	17	1	2	2	29	.20	.033	12	12	.14	140	.05	3	.89	.01	.05	1	1	30	70
3062	1	6	12	30	.1	8	4	228	1.44	3	5	ND	3	26	1	2	2	26	.23	.018	16	13	.21	106	.08	4	.90	.01	.06	1	1	70	140
3063	1	6	12	46	.2	10	5	501	1.78	2	5	ND	3	30	1	2	2	33	.28	.031	18	16	.28	128	.07	2	1.14	.01	.07	1	1	40	140
3064	1	7	12	40	.1	7	4	271	1.48	2	5	ND	3	22	1	2	2	27	.21	.023	12	14	.19	72	.06	2	.86	.01	.06	1	1	20	100
3065	1	7	15	40	.1	7	3	250	1.38	2	5	ND	2	22	1	2	2	27	.18	.018	12	12	.20	63	.09	2	.80	.01	.05	1	1	40	100
3066	1	7	10	45	.1	9	4	335	1.62	2	5	ND	2	25	1	2	2	31	.20	.041	12	14	.21	83	.07	6	.93	.01	.06	1	2	30	100

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SAMPLE#	MD PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	ME %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU\$ PPB	HG PPB	F PPM
3067	1	8	10	57	.1	8	4	731	1.55	2	5	ND	2	24	1	2	2	27	.22	.042	12	12	.19	83	.06	3	.89	.01	.06	1	1	60	90
3068	1	8	13	59	.1	9	6	541	1.93	4	5	ND	1	34	1	2	2	33	.31	.034	15	14	.24	100	.05	2	1.15	.01	.08	1	1	30	100
3069	1	6	9	38	.2	8	4	579	1.51	2	5	ND	3	29	1	4	2	28	.24	.022	16	12	.17	86	.06	2	.91	.01	.07	1	2	20	80
3070	1	7	13	39	.1	5	3	270	1.62	2	5	ND	2	29	1	2	2	30	.24	.017	15	13	.23	61	.09	2	.90	.01	.05	2	1	30	120
3071	1	6	10	45	.1	7	4	415	1.57	2	5	ND	1	26	1	2	2	28	.23	.022	16	13	.22	64	.07	2	.91	.01	.05	1	1	30	140
3072	1	3	15	38	.1	6	2	157	1.26	2	5	ND	2	23	1	2	2	25	.21	.013	12	10	.18	54	.08	3	.75	.01	.04	1	19	20	100
3073	1	7	13	42	.1	8	4	177	2.19	4	5	ND	3	23	1	3	2	42	.21	.010	12	15	.24	77	.06	3	.97	.01	.04	1	1	10	70
3074	1	13	19	56	.1	13	6	737	2.72	5	5	ND	4	71	1	2	2	37	.87	.025	23	21	.51	261	.05	3	2.01	.02	.07	1	1	60	200
3075	1	8	18	58	.1	7	6	600	2.03	5	5	ND	2	29	1	2	2	35	.32	.018	11	14	.22	174	.06	4	.99	.01	.07	1	1	20	90
3076	1	6	10	51	.1	7	6	630	2.03	5	5	ND	2	32	1	2	2	36	.39	.022	12	15	.30	96	.08	4	.97	.01	.07	1	1	30	100
3077	2	13	12	60	.1	8	7	725	3.08	6	5	ND	1	33	1	2	2	44	.43	.027	12	13	.21	161	.02	2	1.14	.01	.06	1	1	20	100
3078	1	54	14	98	.2	25	8	1119	3.49	6	7	ND	6	132	1	2	2	37	1.81	.053	59	24	.71	723	.03	4	3.69	.02	.09	1	1	90	120
3079	1	18	15	84	.1	14	9	883	3.06	7	5	ND	4	49	1	2	2	45	.64	.041	39	26	.50	410	.06	3	2.44	.02	.06	1	1	50	150
3080	1	10	18	87	.1	7	6	901	1.98	2	5	ND	2	23	1	2	2	36	.32	.036	16	14	.20	332	.06	4	1.32	.01	.07	1	1	40	110
3081	2	15	20	127	.2	10	10	1990	2.56	4	5	ND	1	34	1	2	2	36	.49	.055	15	14	.25	402	.04	2	1.28	.01	.08	1	1	60	100
3082	1	8	16	43	.1	9	4	221	1.71	4	5	ND	2	23	1	2	2	28	.25	.034	16	12	.21	116	.05	2	.91	.01	.07	2	1	100	140
3083	2	9	12	56	.1	4	4	464	1.57	3	5	ND	1	22	1	2	2	27	.26	.017	12	11	.15	95	.05	2	.81	.01	.05	1	1	30	70
3084	1	13	9	52	.5	5	3	517	.97	2	5	ND	1	39	1	2	2	18	.59	.027	15	7	.11	241	.04	4	.56	.01	.08	1	1	40	40
3085	2	14	16	98	.1	9	6	1808	2.08	3	5	ND	2	30	1	3	2	34	.49	.045	11	14	.17	364	.02	2	1.15	.01	.07	1	2	560	150
3086	2	9	14	94	.1	6	5	1299	1.72	2	5	ND	1	25	1	2	2	29	.36	.046	11	12	.16	198	.04	3	.97	.01	.07	1	3	30	120
3087	2	6	18	93	.1	6	5	890	2.04	4	5	ND	2	17	1	2	2	38	.22	.034	13	14	.18	127	.07	2	1.41	.01	.04	1	1	30	60
3088	1	6	16	68	.2	8	5	685	1.49	2	5	ND	3	20	1	2	2	28	.25	.033	12	12	.19	120	.08	2	.95	.01	.06	1	1	280	60
3089	1	7	12	48	.1	6	4	361	1.60	2	5	ND	2	23	1	2	2	29	.26	.029	13	13	.19	134	.08	4	.88	.01	.05	1	1	120	100
3090	2	7	12	67	.1	8	4	362	2.03	4	5	ND	2	23	1	2	3	35	.30	.039	12	16	.18	160	.04	3	1.12	.01	.06	1	1	110	110
3091	1	7	15	81	.1	7	5	248	1.99	2	5	ND	2	27	1	2	2	37	.31	.039	13	17	.20	110	.09	3	1.14	.01	.05	1	1	20	110
3092	3	11	18	155	.1	13	7	1740	2.77	4	5	ND	3	30	1	2	2	35	.46	.106	14	16	.32	292	.04	3	1.83	.01	.07	1	1	50	200
3093	1	7	18	87	.1	10	4	676	1.63	2	5	ND	2	29	1	2	2	28	.42	.069	12	15	.23	203	.07	5	1.13	.01	.05	1	1	30	70
3094	1	4	13	58	.3	8	3	408	1.56	3	5	ND	2	21	1	2	2	29	.21	.042	12	13	.18	107	.08	6	.94	.01	.09	1	1	20	70
3098	1	6	11	38	.1	5	4	198	1.78	2	5	ND	2	25	1	2	2	36	.20	.012	10	13	.20	63	.08	2	.79	.01	.04	1	1	10	70
3099	1	10	18	74	.1	12	7	402	2.56	5	5	ND	1	25	1	2	2	45	.21	.019	10	18	.31	136	.07	11	1.45	.01	.07	1	1	10	50
STD C/AU-S	20	59	41	135	7.3	65	27	1087	4.13	40	17	8	42	50	18	17	21	56	.50	.089	39	63	.91	184	.08	37	1.88	.06	.12	13	50	1400	-
3100	1	7	16	41	.2	10	6	229	2.09	2	5	ND	4	41	1	2	5	37	.23	.019	14	17	.31	100	.07	3	1.02	.02	.05	2	1	20	140
3101	1	18	13	61	.1	13	6	571	2.25	3	5	ND	3	69	1	2	2	34	.63	.043	24	18	.30	111	.06	2	1.47	.02	.08	1	1	50	130
3102	1	41	19	36	.3	17	6	643	2.66	7	5	ND	6	61	1	2	2	36	.61	.014	35	19	.30	107	.05	2	1.65	.02	.11	1	1	70	120
3103	1	6	11	34	.1	10	4	229	1.74	2	5	ND	4	29	1	2	2	33	.25	.059	10	16	.15	63	.08	10	.80	.01	.09	2	1	20	60
3104	1	7	11	34	.2	7	4	270	1.80	2	5	ND	2	17	1	2	2	33	.14	.047	9	14	.15	62	.06	2	.84	.01	.04	1	1	30	50
3105	1	6	8	31	.1	8	3	141	1.67	2	5	ND	2	16	1	2	2	32	.13	.018	9	14	.15	61	.07	2	.71	.01	.06	1	2	20	40

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P PPM	LA PPM	CR PPM	M6 %	BA PPM	T1 %	B PPM	AL %	NA %	K %	W PPM	AU\$ PPB	H6 PPB	F PPM
3106	1	1	10	33	.2	7	4	209	1.57	2	7	ND	3	23	1	4	2	32	.24	.027	11	13	.15	62	.07	4	.75	.01	.09	1	1	30	120
3107	1	5	10	47	.1	7	5	382	2.11	5	5	ND	4	28	1	4	2	42	.32	.063	11	17	.17	78	.07	18	.82	.01	.11	2	1	20	180
3108	1	4	9	47	.1	7	5	266	1.97	2	5	ND	4	21	1	2	2	42	.24	.043	13	16	.15	48	.08	6	.78	.01	.12	1	31	280	170
3109	1	4	10	39	.1	8	6	355	2.00	3	8	ND	4	38	1	3	2	39	.42	.067	14	17	.16	95	.08	6	.74	.01	.13	1	1	30	150
3110	1	5	12	41	.2	7	5	603	1.98	2	5	ND	3	36	1	2	2	39	.35	.085	13	16	.18	108	.05	3	.93	.01	.11	1	1	50	160
3111	2	6	12	47	.2	8	6	1042	1.85	3	5	ND	4	50	1	3	2	31	.53	.109	15	14	.17	139	.06	7	.94	.01	.11	1	1	20	140
3112	1	1	8	35	.1	7	4	209	1.56	2	5	ND	2	22	1	4	2	33	.25	.025	12	14	.14	57	.08	6	.66	.01	.10	2	1	30	100
3113	1	1	6	36	.1	4	3	269	1.51	2	5	ND	4	20	1	3	2	31	.21	.040	12	16	.12	61	.07	3	.71	.01	.08	1	13	70	120
3114	1	4	8	58	.1	5	4	441	1.55	4	5	ND	4	20	1	5	2	31	.21	.050	12	14	.11	69	.06	4	.79	.01	.08	1	1	40	110
3115	1	1	9	73	.1	5	4	292	1.60	2	5	ND	2	17	1	2	2	31	.15	.058	13	15	.14	64	.07	4	1.07	.01	.07	1	1	10	120
3116	1	4	18	52	.1	10	4	477	1.74	2	5	ND	2	19	1	2	2	35	.16	.031	13	18	.16	70	.08	2	1.18	.01	.06	1	1	20	120
3117	1	9	11	107	.1	11	6	1720	1.46	2	5	ND	3	47	1	2	2	29	.46	.055	15	18	.15	101	.09	7	.91	.02	.09	1	2	10	100
3118	1	4	6	30	.1	9	4	230	1.74	6	5	ND	2	26	1	2	3	37	.25	.020	12	15	.18	43	.09	2	.67	.01	.14	1	1	30	130
3119	1	3	8	58	.2	5	5	392	1.60	2	5	ND	4	26	1	2	2	31	.26	.037	12	13	.17	71	.07	2	.79	.01	.12	1	1	90	110
3120	1	1	6	40	.1	3	4	216	1.51	2	5	ND	1	25	1	2	2	32	.24	.031	12	13	.12	73	.08	2	.65	.01	.13	1	2	20	100
3121	1	7	8	72	.2	6	4	605	1.67	2	5	ND	4	64	1	3	2	31	.59	.114	13	16	.15	140	.08	19	.73	.01	.17	1	1	10	90
3122	1	1	9	27	.1	1	2	260	.94	2	5	ND	1	20	1	2	2	22	.22	.017	12	10	.07	39	.08	3	.36	.01	.10	1	1	5	70
3123	1	1	11	36	.2	7	4	378	1.50	2	5	ND	1	23	1	2	2	30	.23	.028	12	14	.14	69	.08	2	.73	.01	.10	1	2	5	70
3124	1	1	6	35	.1	5	3	265	1.35	2	5	ND	2	21	1	4	2	27	.25	.051	12	12	.11	62	.07	7	.64	.01	.10	1	1	5	70
3125	1	5	9	31	.2	4	5	270	1.89	2	5	ND	4	28	1	2	3	38	.24	.048	12	16	.18	65	.08	2	.65	.01	.10	1	1	60	150
3126	1	7	9	46	.2	8	5	416	1.84	2	5	ND	3	56	1	2	2	36	.50	.019	15	17	.21	81	.07	2	.91	.02	.10	1	1	20	120
3127	1	10	12	41	.1	7	5	343	1.73	2	5	ND	2	48	1	2	2	33	.48	.019	16	14	.17	76	.06	2	.93	.01	.08	1	2	10	140
3128	1	19	15	59	.1	16	7	902	2.80	2	5	ND	3	103	1	2	3	46	.96	.034	36	26	.35	141	.06	7	1.85	.02	.16	1	1	40	180
3129	1	10	12	38	.1	7	4	347	1.99	3	5	ND	3	41	1	3	2	36	.36	.015	14	19	.28	68	.09	3	1.05	.02	.10	1	1	30	140
3130	1	5	7	55	.1	6	4	191	1.62	2	5	ND	2	23	1	2	2	33	.21	.032	12	15	.15	64	.08	5	.85	.01	.07	1	1	5	90
3131	1	10	10	49	.1	7	5	480	1.84	2	5	ND	3	33	1	2	2	35	.27	.039	17	16	.15	82	.09	4	.98	.02	.08	1	1	20	80
3132	1	6	10	32	.1	3	3	157	1.29	2	5	ND	2	29	1	2	2	28	.26	.022	14	12	.16	62	.10	2	.68	.02	.06	1	2	10	120
3133	1	9	10	50	.1	8	4	647	1.61	2	6	ND	1	40	1	2	2	32	.37	.039	17	15	.16	85	.07	2	.86	.01	.09	1	2	50	90
3134	1	4	7	38	.1	5	4	358	1.50	2	5	ND	1	25	1	2	2	32	.21	.038	12	14	.13	77	.08	5	.70	.01	.06	1	1	20	80
3135	1	6	9	68	.2	7	4	355	1.78	2	5	ND	4	30	1	2	2	36	.28	.059	12	16	.17	92	.08	16	.90	.01	.13	1	1	30	60
3136	1	5	9	41	.1	5	3	282	1.23	2	5	ND	1	24	1	2	2	26	.22	.039	11	13	.12	61	.08	10	.59	.01	.09	1	2	10	50
3137	1	6	9	45	.1	4	4	375	1.34	2	5	ND	1	30	1	2	2	29	.29	.020	12	12	.12	70	.07	12	.67	.02	.05	1	1	10	70
3138	1	6	11	37	.1	8	5	318	1.86	2	5	ND	2	27	1	2	2	39	.22	.041	11	16	.17	66	.08	5	.83	.01	.07	1	6	20	70
3139	1	13	12	70	.2	8	5	708	1.63	3	5	ND	1	49	1	2	2	28	.40	.088	13	15	.17	115	.05	2	.96	.01	.15	1	1	40	90
3140	1	8	6	79	.1	5	5	745	1.85	2	5	ND	1	35	1	2	2	33	.33	.073	11	14	.14	120	.07	14	.75	.01	.13	1	1	20	60
3141	1	6	9	33	.1	8	4	219	1.85	2	5	ND	2	24	1	2	2	37	.21	.031	13	18	.17	59	.09	3	.69	.02	.13	1	1	30	110
STD C/AU-S	20	61	43	132	6.9	71	28	1065	4.03	37	21	8	41	52	19	15	20	59	.54	.091	41	65	.83	180	.09	34	1.78	.06	.16	13	50	1400	-

## NEWMONT EXPLORATION PROJECT-337 FILE # B7-3943

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	M6 %	BA PPM	TI %	B PPM	AL %	NA %	K %	N PPM	AU\$ PPB	HG PPM	F PPM
3142	1	8	17	57	.4	5	4	486	1.87	4	8	ND	6	35	1	2	2	37	.32	.048	13	15	.19	129	.08	2	.94	.01	.17	1	1	40	80
3143	1	4	16	50	.2	7	3	489	1.61	5	5	ND	4	18	1	2	2	34	.17	.060	11	13	.12	71	.06	3	.97	.01	.07	1	1	20	70
3144	2	10	29	224	.4	1	4	2564	2.83	6	5	ND	6	95	1	3	2	15	.99	.106	10	8	.11	740	.01	3	1.93	.01	.18	1	1	9800	220
3145	2	14	19	79	.4	5	6	1300	2.38	6	5	ND	5	38	1	2	2	36	.38	.056	17	15	.19	245	.02	2	1.85	.01	.09	1	1	300	250
3146	2	10	29	247	.3	6	6	4462	2.67	4	6	ND	4	67	1	2	2	21	.57	.137	19	11	.17	490	.02	2	2.01	.01	.12	1	1	80	260
3147	2	9	22	156	.1	10	7	1860	1.94	8	5	ND	5	32	1	2	2	36	.26	.051	18	14	.21	179	.06	2	2.02	.01	.07	1	2	50	170
3148	2	21	16	119	.3	15	7	1542	2.57	8	7	ND	6	85	1	2	2	37	.82	.064	27	21	.30	250	.04	2	2.63	.01	.15	1	1	180	210
3149	1	6	15	32	.1	1	3	504	1.17	3	5	ND	2	35	1	2	2	28	.41	.021	13	12	.10	62	.07	2	.57	.01	.10	1	1	20	200
3150	1	6	13	57	.3	6	3	751	1.12	2	5	ND	2	22	1	2	2	25	.18	.040	12	15	.10	78	.06	4	.81	.01	.06	1	1	10	140
3151	2	8	23	120	.2	5	5	2224	1.83	5	5	ND	4	43	1	2	2	34	.32	.074	15	15	.18	229	.06	4	1.25	.01	.09	1	2	20	140
3152	1	5	15	30	.1	2	3	276	1.26	4	5	ND	4	35	1	2	2	28	.31	.016	12	11	.19	55	.10	4	.76	.02	.07	1	1	30	170
3153	1	7	12	57	.3	6	5	897	1.74	3	5	ND	4	38	1	2	2	36	.39	.024	12	15	.19	88	.08	2	.83	.01	.09	1	1	20	100
3154	1	11	13	105	.1	8	5	713	1.92	4	5	ND	3	58	1	2	2	37	.51	.074	12	15	.19	114	.06	7	.94	.01	.16	1	1	30	110
3155	1	20	14	50	.3	16	5	376	2.27	3	5	ND	5	89	1	2	2	38	.56	.023	27	22	.36	149	.05	2	2.23	.02	.14	1	1	30	270
3156	1	4	11	39	.3	1	2	152	1.15	3	5	ND	3	24	1	2	2	26	.21	.012	11	9	.13	44	.08	4	.61	.01	.06	1	1	20	170
3157	1	5	16	58	.1	4	4	391	1.37	2	5	ND	2	26	1	2	2	30	.24	.022	12	12	.14	68	.07	13	.86	.01	.06	1	1	10	80
3158	1	11	19	63	.3	7	5	836	1.73	2	5	ND	2	36	1	2	2	31	.31	.043	15	15	.26	88	.06	2	1.27	.01	.09	1	2	20	190
3159	1	7	11	47	.1	7	3	345	1.57	4	5	ND	3	26	1	2	2	33	.21	.023	12	15	.18	69	.08	2	.89	.01	.09	2	1	10	130
3160	1	7	18	46	.3	7	4	500	1.65	2	5	ND	4	37	1	2	2	34	.34	.031	14	14	.20	73	.08	4	.95	.01	.09	1	1	20	250
3161	1	12	15	58	.1	10	5	852	1.93	6	7	ND	4	47	1	2	2	38	.41	.025	20	19	.26	94	.09	2	1.31	.01	.09	1	1	30	120
3162	1	5	16	50	.1	5	4	447	1.87	2	5	ND	3	30	1	2	2	40	.28	.044	11	17	.18	127	.08	2	1.00	.01	.07	1	1	5	190
3163	1	7	11	73	.3	5	3	429	1.69	3	5	ND	4	30	1	2	2	33	.27	.074	12	15	.19	120	.07	11	1.01	.01	.11	1	1	10	200
3164	1	7	14	45	.2	6	4	468	1.66	4	5	ND	3	26	1	2	2	35	.24	.026	11	15	.17	67	.07	2	.89	.01	.11	1	1	5	180
3165	1	9	12	52	.1	7	5	575	1.97	6	5	ND	2	33	1	2	2	38	.30	.058	11	15	.25	114	.06	13	.97	.01	.10	1	1	30	190
3166	1	14	16	173	.1	7	7	1761	2.13	7	5	ND	3	65	1	2	2	35	.66	.099	16	13	.25	268	.03	3	1.48	.01	.16	1	2	50	180
3167	1	9	12	48	.1	4	4	604	1.47	4	5	ND	3	26	1	2	2	32	.22	.023	11	13	.15	76	.07	13	.81	.01	.08	1	1	30	70
3168	1	9	19	58	.2	5	5	392	1.71	7	5	ND	2	23	1	2	2	32	.20	.027	12	13	.19	68	.05	4	1.36	.01	.07	1	1	5	70
3169	1	7	13	33	.1	5	3	368	1.26	3	5	ND	2	22	1	2	2	29	.18	.018	11	10	.14	57	.06	2	.76	.01	.06	1	1	5	70
3170	1	5	13	77	.1	5	4	317	1.58	3	5	ND	3	16	1	2	2	32	.12	.041	12	13	.13	85	.06	5	1.02	.01	.06	1	1	20	60
3171	1	15	16	75	.1	8	7	655	2.27	3	5	ND	3	58	1	2	2	43	.42	.021	10	15	.22	112	.05	12	1.02	.01	.10	1	1	10	80
3172	1	7	16	73	.2	5	5	318	1.88	7	5	ND	2	30	1	2	2	38	.28	.038	10	14	.19	82	.07	6	.84	.01	.08	1	1	30	120
3173	1	7	15	36	.1	6	4	355	1.58	2	5	ND	4	31	1	2	2	34	.27	.021	13	14	.17	70	.08	5	.69	.01	.11	1	2	30	70
3174	1	7	11	41	.1	8	4	452	1.50	4	5	ND	3	26	1	2	2	31	.22	.026	13	13	.16	60	.08	13	.85	.01	.08	1	1	20	90
3175	1	5	10	73	.1	7	3	499	1.38	4	5	ND	2	21	1	2	2	28	.20	.032	13	13	.13	63	.07	5	.86	.01	.09	1	1	10	80
3176	1	6	16	51	.1	7	4	509	1.58	4	5	ND	3	29	1	2	4	31	.27	.031	16	13	.21	65	.07	2	1.10	.01	.06	1	1	30	110
3177	1	6	13	60	.2	6	4	392	1.38	5	5	ND	3	23	1	2	2	28	.22	.059	12	12	.13	103	.06	2	.95	.01	.09	1	1	20	50
STD C/AU-S	19	58	41	131	7.2	66	26	1046	4.00	37	16	7	40	50	17	17	20	60	.49	.083	37	59	.88	180	.08	35	2.01	.06	.13	13	49	1400	-

## NEWMONT EXPLORATION PROJECT-337 FILE # 87-3943

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SAMPLE#	MD PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CD PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	Tl PPM	B PPM	AL %	NA %	K %	W PPM	AU** PPB	HG PPB	F PPM
3178	1	2	13	59	.2	4	4	571	1.37	2	5	ND	4	39	1	2	2	27	.38	.040	13	13	.12	91	.07	7	.72	.01	.09	1	1	10	100
3179	1	7	11	35	.1	5	3	320	1.44	2	5	ND	2	25	1	2	4	29	.23	.024	14	13	.16	73	.07	8	.75	.01	.08	2	1	20	150
3180	1	8	16	36	.1	6	4	286	1.84	2	5	ND	2	29	1	2	2	33	.20	.016	13	16	.20	83	.06	3	.83	.01	.08	1	1	30	210
3181	1	8	15	48	.1	4	2	124	1.55	2	5	ND	1	35	1	2	2	34	.23	.018	13	14	.15	68	.07	6	.73	.01	.08	2	2	30	320
3182	1	5	15	45	.1	4	4	377	1.54	2	5	ND	4	26	1	2	2	32	.27	.039	13	14	.22	63	.08	2	.92	.01	.09	2	1	20	190
3183	2	15	27	76	.1	11	5	981	2.23	4	5	ND	3	46	1	2	2	36	.45	.067	22	18	.29	174	.04	5	1.72	.01	.12	1	1	70	220
3184	1	12	20	81	.1	12	7	1217	2.17	5	5	ND	1	34	1	2	2	37	.31	.048	17	19	.29	110	.05	2	1.77	.01	.07	1	1	40	180
3185	1	5	14	86	.1	5	5	1036	1.60	2	6	ND	2	27	1	3	2	31	.28	.057	12	14	.17	115	.07	5	1.02	.01	.08	1	1	20	130
3186	1	4	16	95	.1	9	5	784	1.73	2	5	ND	2	27	1	4	2	33	.27	.052	12	16	.19	124	.07	3	1.01	.01	.07	1	1	30	140
3187	2	12	20	119	.2	6	6	2404	1.90	2	7	ND	2	48	1	2	2	35	.41	.106	13	18	.19	263	.05	3	1.05	.01	.13	1	1	30	110
3188	2	14	19	81	.1	5	6	2165	1.96	4	5	ND	1	41	1	2	4	34	.39	.063	17	17	.21	182	.03	4	1.33	.01	.08	1	1	30	140
3189	1	7	13	42	.2	3	3	436	1.57	2	5	ND	3	29	1	2	3	32	.27	.043	13	18	.16	98	.08	8	.79	.02	.13	2	1	20	100
3190	1	7	14	49	.1	5	4	496	1.97	3	5	ND	2	31	1	3	2	38	.28	.090	14	19	.17	114	.07	4	.94	.01	.08	1	1	60	110
3191	1	5	11	37	.1	4	2	177	1.56	2	5	ND	3	26	1	2	2	32	.22	.044	13	16	.13	80	.07	6	.75	.01	.11	1	1	20	110
3192	1	9	16	65	.2	3	5	487	1.89	3	5	ND	4	26	1	2	2	35	.22	.078	14	17	.16	102	.07	2	.98	.01	.10	1	1	30	110
3193	1	7	8	52	.1	5	4	395	1.67	3	5	ND	2	27	1	2	2	33	.28	.031	17	16	.20	71	.08	3	.90	.01	.08	1	1	10	120
3194	1	8	14	43	.1	7	4	372	1.85	2	5	ND	2	25	1	2	2	39	.27	.040	10	17	.21	70	.12	7	.86	.01	.07	2	1	10	130
3195	1	8	13	48	.2	8	4	1511	1.70	2	5	ND	3	40	1	3	2	33	.39	.066	14	19	.17	169	.07	2	.90	.01	.11	1	1	20	90
3196	1	4	14	44	.1	6	4	300	1.41	2	5	ND	3	23	1	2	2	30	.23	.022	13	16	.18	60	.09	5	.79	.01	.11	1	1	30	100
3197	1	7	15	69	.1	4	5	971	1.74	2	5	ND	2	32	1	2	2	34	.32	.051	13	15	.20	119	.08	3	.97	.01	.07	1	1	20	120
3198	1	9	13	60	.1	5	5	324	1.76	5	5	ND	2	22	1	2	2	33	.27	.026	10	15	.16	155	.03	7	.93	.01	.07	1	1	40	180
3199	3	13	18	84	.1	6	6	1011	2.94	17	5	ND	3	21	1	4	2	39	.38	.042	9	15	.17	384	.01	6	1.76	.01	.10	1	1	80	260
3200	2	14	18	149	.3	11	7	1250	2.72	9	5	ND	3	23	1	4	2	43	.35	.050	12	19	.26	241	.01	3	1.99	.01	.08	1	1	40	220
3201	1	9	18	55	.1	8	5	228	2.07	2	5	ND	3	27	1	2	2	39	.25	.078	15	20	.23	103	.11	9	1.23	.02	.08	1	1	30	140
3202	1	4	8	21	.1	3	2	123	1.11	2	5	ND	3	27	1	2	2	22	.25	.035	12	13	.19	68	.10	3	.70	.02	.06	1	1	20	140
3203	1	8	16	40	.1	6	4	196	1.78	2	5	ND	3	35	1	2	2	35	.30	.049	16	18	.25	88	.10	3	.95	.02	.07	1	5	20	210
3204	1	6	14	49	.2	7	5	209	2.06	2	5	ND	4	27	1	2	2	38	.24	.057	14	17	.24	103	.08	4	1.18	.01	.07	1	1	40	150
3205	1	11	21	39	.1	7	4	344	1.37	4	5	ND	5	30	1	2	2	28	.31	.021	17	18	.25	66	.13	8	.97	.02	.07	1	1	20	160
3206	1	9	14	37	.1	7	4	258	1.80	3	5	ND	3	34	1	2	2	38	.29	.042	15	20	.23	81	.11	8	.90	.02	.07	1	1	30	150
3207	1	10	14	37	.1	7	4	260	1.85	2	5	ND	2	33	1	2	2	38	.32	.037	15	20	.26	76	.14	8	.89	.02	.08	1	1	30	150
3208	1	11	12	38	.2	8	4	213	1.76	2	5	ND	3	33	1	2	3	39	.31	.030	14	19	.24	69	.15	6	.82	.02	.06	1	1	10	90
3209	1	9	13	26	.1	5	4	179	1.40	5	5	ND	3	34	1	2	2	29	.28	.016	13	17	.23	59	.14	2	.76	.02	.07	1	1	40	110
3210	1	9	17	39	.1	7	4	261	1.80	2	5	ND	3	32	1	2	2	37	.31	.023	14	21	.28	55	.16	5	.88	.02	.06	2	1	30	150
3211	1	3	15	30	.5	6	4	175	1.48	2	5	ND	3	37	1	2	2	26	.32	.034	11	16	.31	76	.08	2	1.03	.02	.07	1	43	20	210
3212	1	9	11	26	.2	5	2	173	1.31	2	5	ND	3	29	1	3	3	27	.26	.023	13	15	.22	64	.13	7	.71	.02	.05	1	1	20	90
3213	1	8	13	30	.3	6	3	221	1.53	4	5	ND	3	36	1	2	2	30	.28	.038	14	15	.24	83	.11	2	.80	.02	.06	1	1	220	130
STD C/AU-S	20	63	42	132	7.6	67	28	1122	4.04	36	15	8	40	52	20	15	21	59	.53	.092	40	65	.87	179	.09	37	1.85	.06	.13	12	47	1400	-

## NEWMONT EXPLORATION PROJECT-337 FILE # 87-3943

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	M6 %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU\$ PPB	HG PPB	F PPM
3214	1	5	11	46	.1	8	3	164	1.48	2	5	ND	5	23	1	2	2	30	.25	.033	12	15	.20	55	.11	2	.88	.01	.06	2	1	30	100
3215	1	4	10	61	.1	10	5	252	2.13	4	5	ND	5	28	1	2	2	37	.28	.087	13	18	.28	89	.09	2	1.21	.01	.09	1	1	20	180
3216	1	8	9	36	.1	11	4	202	1.87	3	5	ND	5	28	1	2	2	38	.28	.039	12	19	.26	74	.13	2	.96	.02	.06	1	2	40	160
3217	1	9	11	50	.1	9	4	196	1.91	3	5	ND	5	27	1	2	2	36	.25	.051	13	18	.27	76	.12	2	1.13	.02	.06	1	1	30	170
3218	1	4	15	29	.1	6	3	185	1.37	3	5	ND	7	46	1	2	2	25	.30	.057	15	13	.26	108	.10	2	1.00	.02	.10	1	1	40	210
3219	1	8	16	78	.1	9	5	246	2.19	3	5	ND	5	24	1	2	2	38	.26	.100	14	19	.27	76	.10	2	1.40	.01	.07	1	1	30	180
3220	1	8	13	47	.1	9	4	620	1.54	4	5	ND	5	69	1	2	2	26	.42	.030	22	16	.26	160	.06	2	1.40	.03	.09	1	6	70	180
3221	1	4	16	40	.1	9	4	189	1.80	3	5	ND	4	26	1	2	2	33	.19	.049	14	15	.22	80	.08	2	1.11	.01	.07	1	91	30	140
3222	1	4	16	39	.1	5	3	226	1.51	2	5	ND	4	22	1	2	2	29	.18	.048	13	13	.18	80	.08	2	1.01	.01	.07	1	1	40	140
3223	1	7	19	38	.1	10	3	134	1.42	2	5	ND	2	26	1	2	2	23	.21	.035	14	14	.25	82	.06	2	1.52	.02	.08	1	1	40	210
3224	1	2	14	54	.1	5	3	147	1.46	2	5	ND	5	22	1	2	2	25	.15	.038	12	14	.20	70	.09	2	1.11	.01	.06	1	1	20	110
3225	1	5	19	75	.1	8	4	173	1.79	3	5	ND	5	23	1	3	2	31	.20	.080	13	16	.23	69	.09	2	1.35	.01	.06	1	1	30	140
3226	1	4	12	43	.1	7	3	137	1.32	3	5	ND	3	17	1	2	2	27	.17	.021	11	12	.16	42	.11	12	.76	.02	.05	1	1	10	110
3227	1	7	10	50	.1	10	4	223	1.96	3	5	ND	3	25	1	2	2	37	.23	.037	13	19	.30	61	.13	5	1.09	.02	.05	1	1	10	170
3228	1	8	11	112	.1	8	4	404	1.67	2	5	ND	3	40	1	2	2	25	.40	.077	13	14	.25	111	.07	11	1.20	.02	.08	1	1	30	150
3229	3	11	19	62	.2	8	7	243	3.32	15	5	ND	5	32	1	2	2	33	.44	.046	17	6	.12	149	.01	2	1.15	.01	.08	1	1	40	440
3230	2	6	12	54	.1	7	6	208	3.12	7	5	ND	3	25	1	2	2	38	.58	.068	11	11	.15	165	.01	2	.96	.01	.11	1	1	20	340
3231	1	12	11	55	.1	11	5	279	2.44	6	5	ND	3	22	1	2	2	35	.23	.042	14	14	.25	124	.04	2	1.02	.01	.07	1	1	20	180
3232	1	5	14	43	.1	7	4	257	1.56	2	5	ND	3	25	1	2	2	30	.23	.018	12	15	.21	95	.10	2	.91	.01	.06	1	1	10	120
3233	1	9	13	75	.1	9	5	385	2.05	2	5	ND	4	31	1	2	2	37	.25	.065	14	17	.24	134	.08	2	1.44	.01	.10	1	1	30	150
3234	1	10	15	86	.1	12	6	332	2.29	5	5	ND	2	26	1	2	2	42	.26	.056	12	21	.29	177	.10	2	1.51	.01	.06	1	1	20	230
3235	1	11	11	87	.1	10	5	448	2.28	3	5	ND	3	27	1	2	2	36	.27	.051	13	16	.21	141	.05	8	1.18	.01	.06	1	1	30	180
3236	1	10	18	82	.1	11	6	454	2.52	5	5	ND	3	29	1	2	2	43	.26	.094	14	21	.28	117	.09	2	1.66	.01	.07	1	1	20	140
3237	1	4	8	41	.1	7	4	246	1.62	3	5	ND	4	26	1	2	2	31	.21	.038	13	14	.18	100	.08	2	.98	.01	.09	2	1	10	100
3238	1	14	16	91	.1	12	7	878	2.43	7	5	ND	3	45	1	2	2	38	.53	.060	14	19	.31	234	.07	2	1.57	.01	.08	1	1	40	150
3239	1	6	14	46	.1	7	4	344	1.81	5	5	ND	4	32	1	2	4	35	.23	.032	14	16	.22	96	.09	2	1.08	.01	.06	1	1	30	160
3240	1	5	13	64	.1	8	3	507	1.65	2	5	ND	3	26	1	2	2	30	.24	.076	12	14	.19	106	.08	6	1.14	.01	.09	1	1	20	120
3241	1	8	17	75	.1	11	5	531	2.30	3	5	ND	3	30	1	2	2	36	.28	.128	13	21	.26	210	.07	4	1.76	.01	.06	1	1	20	130
3242	2	11	19	153	.1	13	7	967	3.33	5	5	ND	2	24	1	5	2	46	.35	.081	15	19	.25	349	.05	2	2.04	.01	.06	1	2	50	160
3243	1	6	17	78	.1	9	4	188	1.77	3	5	ND	4	23	1	2	2	31	.22	.042	13	14	.21	115	.07	5	1.38	.01	.04	1	1	20	150
3244	2	13	10	101	.1	7	5	335	2.67	6	5	ND	4	16	1	2	2	42	.21	.047	16	16	.24	168	.03	6	1.77	.01	.08	1	1	30	160
3245	3	9	11	51	.1	9	8	245	4.04	8	5	ND	3	24	1	2	4	41	.37	.048	17	8	.13	107	.01	2	1.10	.01	.07	1	1	30	480
3246	1	5	11	57	.1	8	3	226	1.64	4	5	ND	1	22	1	2	4	30	.19	.016	10	15	.22	75	.07	2	.84	.01	.05	1	1	10	160
3247	1	6	10	52	.1	7	5	312	2.25	8	5	ND	3	26	1	2	5	38	.20	.013	11	17	.23	114	.07	2	.92	.01	.07	1	1	30	140
3248	3	16	10	81	.1	8	7	396	3.55	11	5	ND	3	19	1	2	2	30	.23	.054	10	5	.17	242	.01	2	1.48	.01	.13	1	1	40	370
3249	2	13	15	97	.1	9	6	422	2.45	6	5	ND	3	27	1	2	3	41	.29	.043	14	15	.19	264	.04	10	1.09	.01	.09	1	1	50	150
STD C/AU-S	19	58	39	132	7.4	67	26	1057	4.06	38	18	8	41	50	18	17	19	56	.49	.086	38	60	.89	182	.08	37	1.90	.06	.13	13	50	1300	-

## NEWMONT EXPLORATION PROJECT-337 FILE # 87-3943

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P PPM	LA PPM	CR PPM	M6 %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU\$ PPB	HG PPM	F PPM
3250	1	8	18	58	.1	12	4	214	1.48	2	5	ND	4	31	1	2	2	31	.31	.019	14	13	.22	92	.11	4	.90	.01	.09	1	1	30	160
3251	2	8	19	109	.1	11	6	389	1.99	3	5	ND	5	23	1	3	2	40	.25	.031	14	14	.18	208	.07	2	1.08	.01	.05	1	1	20	130
3252	2	24	21	87	.2	14	9	1039	3.07	5	5	ND	8	135	1	2	2	38	1.49	.058	35	15	.33	394	.02	2	2.16	.01	.12	1	2	2000	410
3253	2	19	19	62	.1	14	7	742	2.74	3	5	ND	7	78	1	2	2	49	.80	.021	24	22	.39	230	.11	2	1.88	.02	.11	1	1	80	300
3254	1	5	19	61	.1	10	4	204	1.55	3	5	ND	3	28	1	2	2	31	.27	.016	15	13	.22	107	.08	6	1.01	.01	.06	1	1	250	200
3255	1	7	16	53	.1	12	5	305	1.84	2	5	ND	5	28	1	3	2	36	.31	.028	15	14	.24	125	.07	2	1.32	.01	.09	1	1	50	220
3256	1	8	19	49	.1	8	3	253	1.67	5	5	ND	4	30	1	3	2	33	.33	.021	14	13	.28	101	.07	2	1.16	.01	.06	1	1	40	240
3257	2	11	16	63	.1	11	6	417	1.92	4	5	ND	4	31	1	2	2	30	.34	.023	16	12	.27	127	.02	2	1.51	.01	.08	1	1	70	540
3258	4	30	22	102	.4	18	14	865	3.32	27	5	ND	6	36	1	3	2	40	.49	.104	30	18	.44	113	.02	4	2.10	.01	.15	1	1	120	770
3259	1	13	18	57	.1	14	7	545	2.25	6	5	ND	3	34	1	2	2	46	.34	.045	16	21	.29	120	.11	3	1.58	.01	.10	1	1	30	230
3260	2	20	23	116	.1	16	9	895	2.92	9	5	ND	6	49	1	2	2	50	.51	.040	21	21	.37	170	.07	2	1.90	.01	.15	1	1	60	270
3261	2	12	20	35	.1	11	6	263	2.31	3	5	ND	5	48	1	2	2	46	.43	.009	16	20	.31	79	.13	7	1.28	.02	.12	1	1	30	200
3262	3	12	15	49	.1	12	6	494	2.17	7	5	ND	2	44	1	4	2	45	.38	.019	14	18	.26	93	.10	6	1.05	.01	.11	1	1	40	180
3263	3	21	16	120	.1	20	11	1149	2.83	29	5	ND	4	45	1	2	3	40	.59	.070	19	17	.40	206	.02	6	1.59	.01	.17	1	2	70	490
3264	3	33	28	153	.7	23	20	2370	4.27	63	5	ND	5	64	1	2	2	55	.98	.162	32	22	.42	231	.03	3	2.47	.01	.17	1	3	180	580
3265	4	10	14	79	.1	8	6	558	2.40	19	5	ND	3	31	1	4	2	36	.50	.042	9	12	.17	107	.02	6	1.17	.01	.10	1	1	110	170
3266	2	6	13	98	.1	4	7	604	.94	4	5	ND	2	25	1	2	2	19	.29	.028	9	6	.13	108	.01	4	1.43	.01	.07	1	1	20	230
3267	1	11	12	64	.2	9	5	291	1.74	2	5	ND	3	33	1	2	2	35	.36	.028	16	15	.26	84	.11	4	1.05	.01	.08	1	1	40	140
3268	1	172	13	55	.9	58	10	670	3.37	3	13	ND	5	268	1	2	2	45	2.95	.099	213	32	.54	757	.03	5	5.29	.02	.14	1	9	150	570
3269	1	8	17	45	.1	8	4	278	1.42	2	5	ND	4	50	1	2	2	29	.38	.037	16	13	.21	116	.10	2	1.00	.02	.09	2	1	10	160
3270	2	9	17	112	.1	6	6	413	1.28	7	5	ND	2	19	1	2	2	22	.27	.031	10	9	.16	101	.01	2	1.37	.01	.06	1	1	30	280
3271	3	19	19	112	.1	12	8	1324	2.83	2	5	ND	3	34	1	2	2	42	.44	.071	19	16	.33	214	.01	6	2.33	.01	.10	1	1	40	260
3272	1	15	17	65	.2	11	5	430	1.84	4	5	ND	3	29	1	2	4	32	.33	.029	19	14	.25	214	.04	3	1.23	.01	.09	1	2	30	180
3273	2	14	19	173	.1	13	9	1249	2.46	5	5	ND	4	34	1	2	2	40	.55	.060	15	17	.23	338	.02	2	1.34	.01	.13	1	1	100	190
3274	1	11	16	93	.1	17	7	437	2.59	4	5	ND	1	39	1	2	2	45	.43	.033	13	19	.22	176	.05	3	.99	.01	.11	1	1	20	100
3275	1	33	24	167	.2	17	8	1644	2.73	3	5	ND	5	103	1	4	2	38	1.26	.032	28	20	.43	410	.05	8	2.01	.02	.13	1	1	50	170
3276	1	101	18	100	.2	30	6	807	2.23	4	5	ND	4	141	1	2	2	27	1.76	.058	54	17	.43	452	.04	6	1.80	.02	.12	1	1	120	200
3277	1	13	20	48	.1	9	5	567	1.90	2	6	ND	5	43	1	2	2	36	.50	.009	25	15	.22	286	.08	3	1.20	.02	.12	1	1	20	120
3278	1	8	18	39	.1	6	4	629	1.67	2	5	ND	4	48	1	2	2	34	.59	.012	13	15	.21	163	.07	5	.93	.01	.06	1	1	30	120
3279	1	38	19	78	.3	16	7	271	2.90	2	5	ND	7	110	1	3	4	35	1.21	.093	31	20	.56	366	.03	7	1.86	.03	.13	1	1	280	350
3280	1	6	13	33	.1	5	3	140	1.44	2	5	ND	1	21	1	2	2	29	.18	.013	11	11	.11	65	.05	4	.57	.01	.10	1	1	30	80
3281	2	11	17	57	.1	12	6	279	2.31	5	5	ND	2	22	1	2	2	42	.24	.022	13	16	.23	135	.05	2	1.15	.01	.08	1	1	20	140
3282	1	11	9	41	.2	10	5	169	1.83	2	5	ND	5	43	1	2	2	33	.43	.017	17	13	.20	136	.05	2	.96	.01	.14	1	1	30	150
3283	1	10	15	108	.1	11	7	885	2.06	5	5	ND	2	24	1	2	4	37	.30	.051	15	16	.24	182	.04	9	1.67	.01	.09	1	1	20	280
3284	3	22	25	147	.2	14	10	2280	3.72	16	5	ND	4	56	1	7	2	60	.81	.126	17	23	.39	338	.05	5	2.78	.01	.12	1	1	60	250
3285	2	10	20	110	.1	7	9	1871	1.70	2	5	ND	2	36	1	2	2	31	.41	.048	19	14	.20	152	.08	4	1.48	.01	.07	1	1	30	200
STD C/AU-S	20	63	42	132	7.1	73	28	1148	3.97	38	17	9	45	54	20	17	22	61	.54	.095	41	60	.88	181	.09	39	1.77	.06	.15	14	50	1300	-

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SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	Mg	BA	TI	B	Al	NA	K	W	Au\$	Hg	F
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPB	PPB	PPM									
3286	1	10	20	.99	.3	10	6	514	2.67	7	5	ND	6	24	1	3	2	48	.33	.077	14	17	.27	142	.03	4	2.59	.01	.06	1	62	40	280
3287	2	11	21	130	.1	7	6	1005	2.21	8	5	ND	4	25	1	2	2	37	.29	.067	13	16	.24	150	.03	4	1.99	.01	.08	1	1	50	350
3288	4	46	20	202	.4	28	25	3577	5.21	35	5	ND	6	81	1	2	3	79	1.26	.226	39	36	.94	478	.03	6	3.19	.01	.18	1	1	80	1300
3289	1	13	15	116	.1	12	6	578	2.40	2	5	ND	5	45	1	2	4	43	.45	.086	17	20	.31	214	.11	4	1.26	.01	.13	1	1	820	330
3290	2	10	11	45	.1	9	4	410	1.90	2	5	ND	5	32	1	2	2	39	.35	.018	12	16	.21	99	.09	7	.95	.01	.12	2	1	20	90
3291	2	13	15	38	.1	7	4	472	1.95	2	5	ND	3	29	1	2	2	40	.30	.023	11	16	.17	72	.06	7	1.05	.01	.10	1	1	10	100
3292	1	5	11	29	.1	5	4	220	1.56	2	5	ND	4	33	1	2	2	32	.25	.056	12	15	.16	79	.08	2	.83	.01	.10	1	1	10	120
3293	1	8	15	49	.1	7	4	352	1.79	3	5	ND	4	24	1	2	2	33	.28	.028	13	13	.23	100	.03	2	1.24	.01	.09	1	1	20	240
3294	2	32	14	71	.3	18	9	805	3.18	16	5	ND	6	64	1	2	2	38	1.35	.067	60	17	.47	321	.02	4	2.34	.01	.13	1	1	130	700
3295	3	27	19	149	.5	15	13	1659	4.06	14	5	ND	7	123	1	2	2	51	1.14	.081	27	21	.54	354	.01	4	2.95	.01	.20	1	3	100	490
3296	3	14	17	86	.1	11	8	740	2.59	5	5	ND	3	32	1	2	3	44	.38	.024	12	16	.26	201	.03	4	1.31	.01	.13	1	3	50	160
3297	2	24	16	83	.1	11	11	918	3.40	9	5	ND	6	49	1	6	2	50	.76	.038	39	20	.36	468	.03	6	1.93	.01	.18	1	1	90	340
3298	1	7	15	54	.1	9	4	314	1.85	2	5	ND	4	23	1	2	2	39	.28	.011	13	17	.19	114	.10	4	.82	.01	.10	1	1	20	80
3299	1	10	14	54	.1	10	5	464	2.02	2	5	ND	5	32	1	2	4	41	.42	.017	20	17	.26	254	.10	8	1.16	.02	.11	1	1	40	150
3300	2	26	17	83	.2	13	10	905	3.45	4	5	ND	7	50	1	4	2	50	.77	.038	39	22	.37	481	.03	2	1.97	.01	.18	1	1	100	300
3301	1	7	15	30	.3	11	4	165	1.47	2	5	ND	4	28	1	2	2	31	.24	.024	15	13	.22	60	.10	6	.79	.02	.06	1	1	20	150
3302	2	16	20	60	.1	13	7	796	2.51	6	5	ND	4	46	1	2	4	45	.41	.042	25	20	.38	90	.10	9	1.72	.02	.10	1	1	30	260
3303	1	10	16	42	.2	7	5	407	1.69	3	5	ND	5	47	1	2	2	33	.39	.026	27	15	.23	89	.09	4	.95	.02	.11	1	3	20	180
3304	1	6	12	56	.1	8	4	382	1.55	2	5	ND	4	22	1	2	2	31	.21	.020	14	14	.19	56	.09	2	.87	.01	.07	1	1	30	110
3305	1	11	15	37	.1	5	3	178	1.41	2	5	ND	3	24	1	3	2	29	.21	.016	16	12	.18	43	.10	7	.78	.02	.06	1	1	10	110
3306	1	6	13	44	.1	9	4	250	1.35	2	5	ND	4	25	1	2	3	27	.25	.017	15	11	.17	58	.09	4	.76	.02	.06	1	1	20	110
3307	1	11	10	46	.1	10	5	263	1.83	4	5	ND	4	29	1	2	2	39	.29	.018	15	16	.23	61	.11	2	1.04	.02	.05	2	1	20	140
3308	1	11	20	53	.2	13	7	609	2.41	2	5	ND	5	39	1	2	5	47	.37	.029	21	20	.41	70	.14	3	1.47	.02	.07	1	1	30	260
3309	1	7	14	47	.1	7	3	321	1.45	2	5	ND	3	27	1	2	3	32	.25	.018	13	14	.21	51	.12	2	.82	.01	.05	1	6	10	160
3310	1	13	16	56	.1	12	6	454	2.22	2	5	ND	5	35	1	2	3	46	.31	.041	15	18	.35	76	.11	5	1.12	.02	.08	1	1	30	260
3311	2	11	21	92	.1	11	6	532	2.13	3	8	ND	3	33	1	2	2	43	.33	.052	16	16	.31	77	.10	3	1.41	.02	.09	1	1	20	210
3312	1	10	15	63	.2	7	4	358	1.73	2	5	ND	4	28	1	3	2	38	.28	.025	14	17	.26	55	.13	6	1.03	.01	.06	1	1	10	190
3313	1	10	20	51	.1	9	4	535	1.60	2	5	ND	5	30	1	2	2	31	.27	.030	16	13	.23	65	.09	3	1.11	.02	.06	1	1	20	130
3314	1	9	18	61	.1	11	4	400	1.51	2	5	ND	3	32	1	2	2	30	.28	.027	15	13	.22	58	.09	2	1.01	.01	.07	1	1	30	80
3315	1	9	13	59	.1	10	5	454	1.80	3	5	ND	4	27	1	2	2	35	.24	.024	15	14	.22	67	.07	2	1.12	.02	.08	1	1	20	110
3316	2	17	16	85	.1	9	6	1715	1.89	2	5	ND	4	53	1	2	2	32	.43	.067	23	14	.23	113	.06	2	1.52	.02	.14	1	1	30	150
3317	1	7	14	48	.1	8	4	675	1.64	2	5	ND	3	33	1	3	2	32	.27	.026	17	14	.20	70	.09	2	.99	.01	.08	1	1	20	100
3318	1	9	13	33	.2	9	5	277	1.78	3	5	ND	4	39	1	2	2	34	.31	.029	20	15	.23	71	.09	2	.75	.02	.13	1	1	30	210
3319	1	9	9	44	.1	8	5	236	1.68	2	5	ND	3	29	1	2	2	33	.23	.029	15	15	.18	64	.09	4	.75	.02	.09	1	1	10	120
3320	1	6	14	58	.3	5	4	283	1.30	2	5	ND	4	19	1	2	2	26	.17	.025	12	11	.14	58	.08	2	.70	.01	.07	1	2	30	20
3321	1	20	18	41	.1	8	5	387	1.89	3	5	ND	6	54	1	2	3	34	.41	.033	37	16	.30	110	.08	2	.95	.03	.14	1	1	60	160
STD C/RU-S	21	63	41	132	7.1	73	29	1046	4.06	41	15	8	45	55	20	18	21	61	.56	.093	42	61	.91	182	.09	38	1.86	.07	.14	12	47	1300	-

## NEWMONT EXPLORATION PROJECT-337 FILE # B7-3943

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P PPM	LA PPM	CR %	MG PPM	BA PPM	TI %	B PPM	AL %	NA %	K PPM	W PPM	AU# PPB	HG PPM	F PPM
3322	1	7	6	93	.1	9	5	570	1.81	6	5	ND	6	32	1	3	2	34	.27	.060	15	14	.18	130	.06	2	.83	.01	.17	1	2	20	100
3323	1	9	11	38	.1	5	4	238	1.66	5	5	ND	6	33	1	2	2	34	.28	.030	17	14	.20	65	.07	2	.68	.02	.11	1	1	30	150
3324	1	8	7	63	.1	4	3	206	1.31	5	5	ND	2	24	1	3	2	30	.24	.025	14	10	.17	54	.09	3	.72	.01	.08	1	1	20	80
3325	1	17	14	57	.2	7	5	570	1.60	2	5	ND	5	51	1	2	2	31	.40	.032	33	14	.20	91	.06	2	1.13	.02	.08	1	2	30	110
3326	1	15	10	55	.1	7	5	294	1.89	5	5	ND	5	30	1	3	2	40	.27	.036	16	15	.22	79	.07	4	.96	.02	.10	1	8	20	130
3327	1	13	8	47	.1	5	3	276	1.43	4	5	ND	6	35	1	2	2	31	.25	.020	15	13	.22	59	.09	8	.83	.02	.08	1	9	10	120
3328	1	13	14	58	.1	7	5	356	1.59	5	5	ND	4	36	1	2	2	34	.31	.027	18	12	.23	72	.08	7	1.07	.02	.08	1	1	10	120
3329	1	13	11	73	.1	7	5	353	1.90	2	5	ND	4	32	1	2	2	41	.32	.032	14	14	.22	72	.09	3	1.24	.01	.09	1	1	20	130
3330	1	13	6	46	.1	7	4	424	1.60	6	5	ND	2	38	1	2	3	35	.36	.020	15	14	.21	75	.08	2	.87	.01	.09	1	3	30	90
3331	1	12	10	60	.1	8	6	605	1.88	5	5	ND	3	36	1	3	2	37	.32	.032	19	15	.32	86	.07	4	1.25	.02	.08	1	1	20	180
3332	1	7	8	33	.1	7	4	204	1.68	4	5	ND	3	29	1	2	2	35	.24	.023	14	14	.24	72	.06	2	.82	.02	.08	1	2	30	130
3333	1	7	13	47	.1	6	3	316	1.40	2	5	ND	4	35	1	3	2	28	.29	.022	17	11	.21	79	.06	2	.89	.01	.10	1	3	20	130
3334	2	17	19	72	.1	7	5	359	1.72	3	5	ND	5	31	1	2	2	37	.32	.033	14	15	.31	78	.08	5	1.48	.02	.10	1	2	10	140
3335	1	6	10	35	.2	3	3	163	1.31	4	5	ND	5	26	1	2	2	28	.21	.019	16	11	.19	61	.07	2	.96	.02	.06	1	4	30	100
3336	1	9	10	58	.2	6	4	254	1.59	2	5	ND	5	25	1	2	2	32	.19	.029	17	13	.20	75	.05	3	1.16	.01	.08	1	1	20	140
3337	1	12	16	38	.1	3	3	311	1.18	3	5	ND	5	26	1	2	2	24	.20	.025	17	8	.16	75	.06	6	.92	.02	.08	1	2	20	130
3338	1	9	17	36	.1	8	4	224	1.64	6	5	ND	6	40	1	2	2	32	.31	.040	17	13	.27	78	.07	2	.89	.02	.11	1	1	40	280
3339	1	5	9	70	.1	8	4	329	1.56	6	5	ND	4	24	1	2	2	32	.21	.030	14	13	.16	80	.06	2	1.07	.02	.06	1	3	20	60
3340	1	8	10	56	.1	7	4	723	1.70	6	5	ND	4	38	1	3	2	36	.34	.058	14	15	.20	87	.07	2	.82	.01	.17	1	2	10	120
3341	2	14	17	141	.2	10	6	629	2.37	4	5	ND	4	38	1	5	2	47	.36	.106	14	18	.29	105	.06	3	1.41	.01	.14	1	1	30	110
3342	2	8	9	64	.1	7	4	668	1.57	6	5	ND	4	40	1	4	2	31	.35	.050	15	12	.23	68	.06	2	.96	.01	.19	1	1	20	120
3343	2	17	15	84	.4	11	6	1106	1.92	4	5	ND	6	48	1	2	2	35	.42	.045	25	14	.27	101	.06	3	1.21	.01	.15	1	2	30	200
3344	1	13	6	40	.2	5	4	334	1.35	3	5	ND	6	39	1	2	2	29	.33	.031	18	12	.18	73	.08	6	.75	.02	.10	1	1	10	100
3345	1	12	9	46	.1	5	2	184	1.36	2	5	ND	5	22	1	2	2	32	.25	.013	10	12	.20	33	.12	6	.76	.02	.04	1	2	5	90
3346	1	15	6	70	.2	11	6	615	1.89	2	5	ND	7	49	1	3	2	32	.50	.036	25	15	.27	87	.06	4	1.28	.02	.11	1	3	30	110
3347	1	13	11	40	.1	8	5	338	1.74	4	5	ND	7	27	1	2	2	35	.24	.013	14	15	.19	63	.07	5	.73	.02	.14	1	1	20	70
3348	2	14	5	40	.2	8	5	155	2.09	7	5	ND	4	26	1	4	2	40	.24	.024	10	15	.17	68	.04	6	.83	.01	.07	1	2	40	50
3349	1	12	11	51	.1	3	4	258	1.45	5	5	ND	4	25	1	2	2	30	.20	.018	15	11	.16	65	.05	6	.71	.01	.12	1	1	20	100
3350	2	5	10	54	.1	7	4	167	1.57	4	5	ND	2	21	1	2	2	32	.17	.028	14	13	.15	63	.05	2	.82	.01	.09	1	1	10	70
3351	2	12	12	35	.1	10	6	193	2.16	5	5	ND	7	50	1	3	2	43	.39	.011	20	17	.29	100	.06	2	1.15	.04	.07	1	3	20	100
3352	2	13	8	40	.1	8	4	469	1.59	7	5	ND	6	33	1	2	2	29	.25	.033	18	14	.28	74	.06	6	1.03	.03	.09	1	2	30	180
3353	1	8	9	33	.1	8	4	154	1.41	2	5	ND	5	30	1	2	4	28	.20	.018	14	11	.24	64	.06	2	.82	.02	.08	1	1	20	130
3354	1	7	9	33	.1	5	3	162	1.11	2	5	ND	4	21	1	2	2	24	.18	.011	12	9	.15	42	.07	2	.61	.01	.09	1	1	10	70
3355	1	9	7	40	.2	6	3	154	1.25	2	5	ND	5	26	1	2	2	27	.19	.013	13	11	.19	51	.08	2	.72	.01	.05	1	2	20	100
3356	1	14	12	39	.1	8	3	154	1.45	5	5	ND	5	26	1	2	2	32	.21	.018	15	13	.20	64	.08	9	.82	.02	.06	1	1	20	100
3357	2	13	9	49	.2	9	5	277	1.76	4	5	ND	6	25	1	5	2	38	.22	.022	13	14	.25	56	.09	3	.88	.01	.07	1	1	10	100
STD C/AU-S	21	62	39	133	7.4	70	29	1040	4.12	42	18	8	44	54	18	18	21	61	.51	.089	41	59	.93	180	.07	35	1.78	.06	.14	12	47	1300	-

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU** PPB	HG PPB	F PPM
3358	1	7	11	48	.2	6	3	287	1.47	3	5	ND	3	24	1	2	2	30	.20	.013	15	13	.19	53	.09	2	.81	.02	.07	3	1	30	60
3359	1	7	15	72	.1	4	4	269	1.62	4	5	ND	4	23	1	2	2	30	.20	.028	16	15	.20	60	.08	4	.97	.02	.09	1	1	40	80
3360	1	15	15	77	.2	9	6	635	2.27	5	5	ND	5	34	1	2	2	38	.33	.040	20	20	.30	71	.06	2	1.56	.02	.12	1	1	30	130
3361	1	7	12	64	.1	4	3	200	1.56	2	5	ND	2	23	1	2	2	32	.26	.020	13	14	.20	49	.09	2	.87	.02	.06	1	1	10	30
3362	1	7	16	48	.1	3	4	195	1.69	3	5	ND	2	22	1	2	2	35	.23	.017	13	15	.23	43	.12	3	.82	.02	.06	1	1	20	60
3363	1	7	12	76	.1	6	4	431	1.72	2	5	ND	2	30	1	2	2	33	.35	.032	15	16	.25	61	.09	2	1.04	.01	.11	1	1	20	60
3364	1	9	18	49	.3	8	6	333	2.24	4	5	ND	4	39	1	3	2	43	.32	.046	18	19	.32	102	.10	2	1.00	.02	.12	2	1	30	130
3365	1	16	18	58	.4	9	8	700	2.71	6	5	ND	5	69	1	2	4	46	.79	.023	30	21	.33	161	.06	2	1.94	.02	.14	1	1	40	100
3366	1	7	14	36	.1	4	4	147	1.94	2	5	ND	3	27	1	2	2	41	.26	.011	13	15	.19	77	.08	2	.80	.01	.07	2	1	5	20
3367	1	21	18	102	.2	11	10	2029	3.32	2	5	ND	6	82	1	2	3	41	1.00	.018	23	21	.53	318	.06	2	2.41	.02	.13	1	1	40	90
3368	1	19	22	74	.2	8	10	789	3.91	4	5	ND	5	93	1	3	2	38	1.19	.033	23	17	.43	329	.03	2	2.05	.02	.14	1	1	50	110
3369	1	5	13	28	.3	5	4	232	1.44	2	5	ND	4	31	1	2	2	31	.31	.011	14	13	.17	48	.09	2	.68	.02	.12	1	1	5	30
3370	1	3	13	26	.1	2	4	256	1.54	3	5	ND	2	35	1	2	2	32	.34	.020	13	14	.18	58	.09	2	.69	.01	.14	1	1	5	30
3371	1	7	13	42	.2	6	5	876	1.45	2	5	ND	1	34	1	2	6	29	.35	.040	13	13	.15	83	.08	2	.81	.01	.09	1	1	10	10
3372	1	9	12	57	.1	4	4	820	1.61	2	5	ND	3	29	1	3	2	33	.31	.013	12	14	.17	125	.10	2	.78	.01	.13	1	1	5	10
3373	1	24	22	135	.2	15	13	1333	4.02	7	5	ND	4	54	1	2	2	44	.73	.055	22	20	.38	434	.04	3	2.08	.01	.17	1	1	40	100
3374	1	21	14	104	.3	10	10	801	3.28	8	5	ND	2	38	1	4	2	38	.51	.044	18	18	.28	303	.03	2	1.45	.01	.19	1	1	40	120
3375	1	16	17	82	.4	8	8	1086	2.72	4	5	ND	5	57	1	2	2	46	.68	.036	18	22	.28	328	.07	6	1.51	.01	.15	1	1	30	40
3376	2	48	15	167	.3	13	17	2712	3.93	5	5	ND	4	98	1	3	4	34	1.76	.098	20	13	.22	1167	.02	9	1.27	.01	.22	1	1	90	30
3377	2	30	22	142	.2	11	14	2212	4.08	18	5	ND	2	80	1	3	2	43	1.09	.109	22	17	.23	539	.02	2	1.52	.01	.21	1	1	80	60
3378	1	9	13	45	.1	7	5	558	2.37	5	5	ND	3	31	1	5	2	45	.34	.015	15	19	.24	173	.07	2	1.27	.02	.09	1	1	10	50
3379	1	8	19	67	.1	7	5	411	1.93	4	5	ND	1	26	1	2	2	38	.38	.031	15	18	.24	76	.11	6	1.06	.02	.11	1	1	20	40
3380	1	12	15	93	.3	7	7	689	2.61	2	5	ND	3	54	1	2	2	46	.70	.037	16	22	.25	205	.09	5	1.34	.01	.16	1	1	3000	10
3381	1	11	17	55	.1	6	5	746	2.00	2	5	ND	4	57	1	2	2	34	.71	.015	20	16	.27	239	.08	2	1.41	.02	.10	1	1	50	40
3382	1	14	16	86	.1	8	7	680	2.50	5	5	ND	4	33	1	2	2	46	.42	.046	16	21	.26	205	.10	4	1.26	.01	.13	1	1	130	70
3383	2	61	31	249	.6	17	21	3878	5.90	40	7	ND	5	108	1	7	2	47	1.74	.203	36	19	.25	993	.02	2	1.76	.01	.23	1	1	500	100
3384	1	61	23	186	.6	21	15	2700	4.82	11	7	ND	3	138	1	2	2	50	2.10	.148	64	28	.45	819	.03	8	2.79	.01	.23	2	1	120	100
3385	1	27	13	177	.2	14	8	1526	2.61	4	5	ND	2	60	1	2	2	43	1.05	.095	16	21	.24	519	.07	3	1.35	.01	.17	1	1	40	50
3386	1	15	21	77	.1	8	6	636	2.32	5	5	ND	3	35	1	3	3	39	.41	.046	19	18	.23	243	.07	3	1.08	.01	.17	1	1	50	120
3387	1	21	14	82	.1	9	9	853	3.06	3	5	ND	4	39	1	3	2	46	.60	.057	20	21	.22	329	.04	2	1.42	.01	.12	2	1	70	80
3388	1	12	18	77	.1	8	6	628	2.15	3	5	ND	3	26	1	2	2	43	.34	.031	15	19	.22	205	.11	6	1.21	.02	.12	1	1	20	30
3389	1	8	17	52	.1	9	6	359	2.28	3	5	ND	3	21	1	2	2	46	.30	.017	13	17	.25	151	.11	5	1.08	.01	.14	1	2	30	10
3390	2	19	22	118	.2	17	10	1162	3.35	6	5	ND	4	31	1	4	5	50	.60	.050	20	21	.24	406	.04	4	1.78	.01	.16	1	1	80	60
3391	3	29	23	189	.4	14	16	2657	4.60	4	5	ND	3	47	1	4	2	53	.93	.129	19	17	.26	603	.03	2	1.89	.01	.15	1	1	70	50
3392	2	22	15	95	.1	9	10	1069	3.02	12	5	ND	1	39	1	2	3	35	.49	.059	13	13	.16	345	.02	4	1.15	.01	.15	1	1	40	70
3393	2	24	17	185	.2	9	15	1563	4.60	14	5	ND	2	49	1	5	2	31	.53	.093	16	12	.18	327	.01	2	1.21	.01	.21	1	1	30	160
STD C/AU-S	18	60	40	132	7.5	68	28	1057	4.07	35	21	9	39	50	18	16	20	56	.53	.083	38	59	.86	179	.08	36	1.76	.06	.15	13	50	1300	-

## NEWMONT EXPLORATION PROJECT-337 FILE # 87-3943

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	Mg PPM	BA PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au\$ PPB	Hg PPM	F
3394	2	29	19	127	.1	9	13	1475	4.18	17	5	ND	5	36	1	5	2	33	.47	.078	17	10	.16	222	.01	7	1.20	.01	.18	1	1	20	250
3395	2	26	15	145	.3	12	16	998	4.86	18	5	ND	5	34	1	5	2	41	.47	.118	20	14	.21	264	.01	7	1.71	.01	.16	2	2	50	330
3396	3	63	23	115	.2	14	15	1534	5.35	21	5	ND	6	33	1	8	2	47	.39	.116	16	9	.14	248	.01	3	1.42	.01	.15	1	1	40	460
3397	1	19	16	52	.1	10	8	609	2.74	6	5	ND	4	43	1	2	2	40	.50	.030	18	15	.26	138	.03	3	1.20	.01	.13	1	4	30	190
3398	1	57	16	46	.2	13	6	148	1.89	2	5	ND	3	117	1	2	2	30	1.69	.045	29	15	.41	193	.03	5	1.81	.02	.04	1	1	50	90
3399	1	20	14	76	.1	10	7	1562	2.05	2	5	ND	3	40	1	2	2	41	.38	.031	16	17	.23	126	.08	4	1.19	.02	.06	1	1	30	50
3400	1	7	15	127	.1	9	6	1248	1.95	2	5	ND	3	36	1	2	2	39	.40	.053	11	16	.21	151	.11	2	.90	.01	.08	1	2	20	10
3401	2	22	18	42	.1	8	6	997	2.01	10	5	ND	2	30	1	2	2	29	.41	.063	32	15	.31	62	.07	2	1.45	.09	.08	1	1	40	80
3402	1	16	21	62	.2	11	7	735	2.59	11	5	ND	4	69	1	2	2	43	.83	.062	26	19	.46	91	.09	9	1.64	.05	.10	1	21	50	180
3403	18	23	22	68	.8	15	27	21046	7.78	131	5	ND	5	142	1	2	2	67	1.96	.155	57	19	.42	436	.03	2	2.50	.02	.09	1	1	210	80
3404	2	19	13	65	.4	18	8	1042	2.67	22	5	ND	4	82	1	2	2	38	.95	.080	49	21	.49	135	.05	2	1.93	.02	.10	1	1	80	210
3425	2	22	14	68	.6	23	9	2367	2.82	13	5	ND	3	95	1	3	2	42	1.41	.102	45	25	.51	216	.05	5	2.52	.03	.11	2	1	100	110

## NEWMONT EXPLORATION PROJECT - 120 FILE # 86-1547

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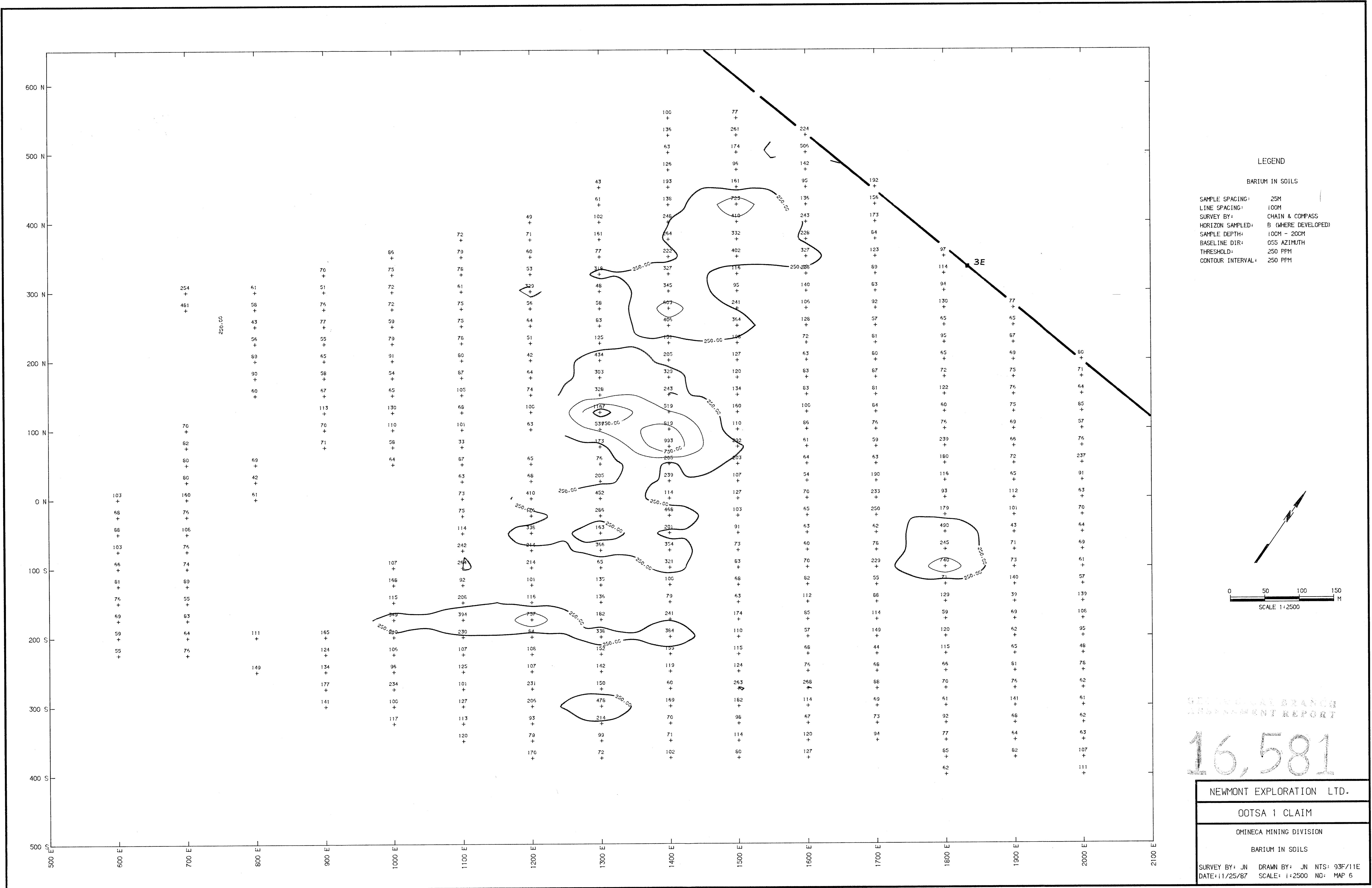
SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P PPM	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na PPM	K %	W PPM	Au#8 PPB	Hg PPB	F PPM
R-07701	1	24	10	60	.3	12	12	735	3.19	33	5	ND	3	64	1	4	2	24	1.38	.128	17	9	.26	231	.01	2	.50	.03	.23	1	1	3300	630
R13094	11	8	2	32	.4	3	2	168	1.20	15	5	ND	3	37	1	2	5	21	7.62	.047	6	9	.20	194	.01	96	2.18	.16	.88	3	2	90	106000
R-13142	3	20	3	62	.1	13	5	200	2.92	28	5	ND	2	14	1	2	2	33	.36	.122	13	11	.35	96	.01	2	1.32	.03	.21	1	3	230	970
R-13143	3	9	4	31	.2	2	2	150	1.50	24	5	ND	3	24	1	2	3	22	6.05	.039	3	8	.35	94	.01	222	2.29	.06	.81	1	4	100	72500
R-13144	4	16	4	57	.2	11	4	203	2.62	51	5	ND	1	8	1	2	2	28	.24	.092	8	9	.53	49	.01	4	1.24	.02	.20	1	5	160	1000
R-13145	3	17	6	55	.1	8	5	187	2.57	26	5	ND	2	9	1	2	2	25	.29	.103	13	7	.48	45	.01	4	1.29	.03	.17	1	2	200	1150
R-13146	7	8	2	67	.3	8	3	180	2.14	159	5	ND	1	32	1	6	2	31	1.18	.055	14	10	.28	156	.01	8	1.69	.04	.50	1	2	60	770
R-13147	11	21	10	61	.3	11	6	139	3.10	55	5	ND	2	11	1	2	2	31	.33	.123	13	10	.43	72	.01	3	1.37	.03	.25	1	1	1400	130
R13180	2	15	14	57	.2	8	7	281	2.30	27	5	ND	3	64	1	2	2	40	3.74	.092	12	13	.71	418	.01	2	2.87	.85	.85	1	1	50	39000
R13181	3	5	7	29	.1	3	1	61	.42	102	5	ND	4	4	1	4	2	.1	.04	.007	25	3	.02	22	.01	4	.30	.01	.17	1	10	100	380
R13182	3	7	5	56	.1	6	3	280	1.32	8	5	ND	4	13	1	2	2	19	.17	.051	22	12	.37	74	.01	4	.80	.01	.24	1	1	200	570
R13183	3	21	2	55	.1	11	7	222	2.85	13	5	ND	2	13	1	2	2	30	.31	.131	15	11	.49	65	.01	3	1.29	.03	.25	1	2	250	830
R13184	9	4	13	58	.7	7	3	116	3.26	113	5	ND	4	40	1	3	5	21	8.09	.021	6	6	.27	90	.01	149	1.32	.15	.29	1	44	70	150000
R13185	2	5	5	12	.1	2	1	65	.57	24	5	ND	1	27	1	3	2	6	3.69	.016	2	4	.06	40	.01	191	.78	.03	.28	1	10	40000	1
R13188	2	22	5	45	.1	9	6	177	1.87	14	5	ND	2	11	1	2	3	27	.61	.118	15	10	.35	98	.01	2	1.40	.03	.30	1	1	130	3500

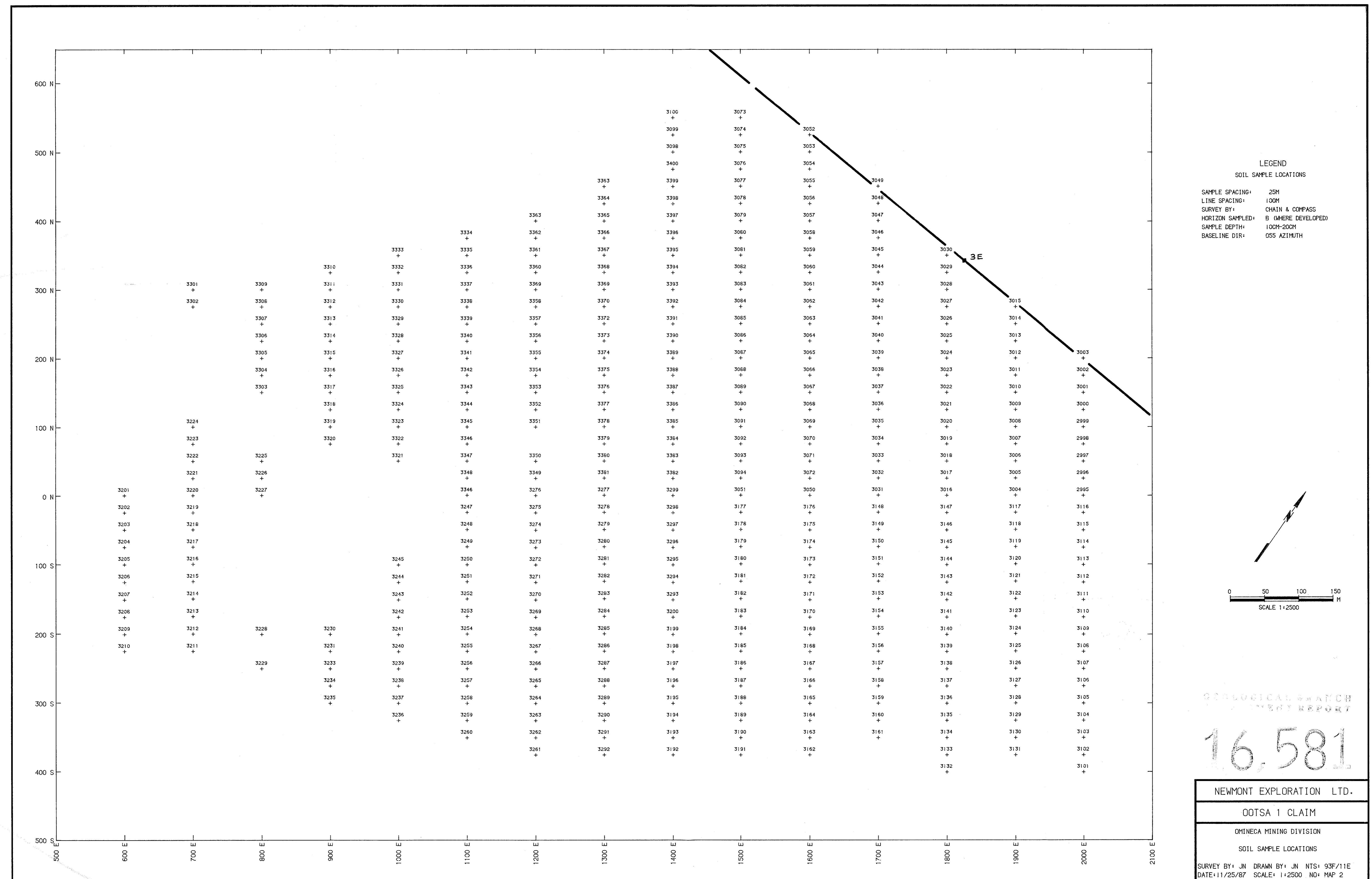
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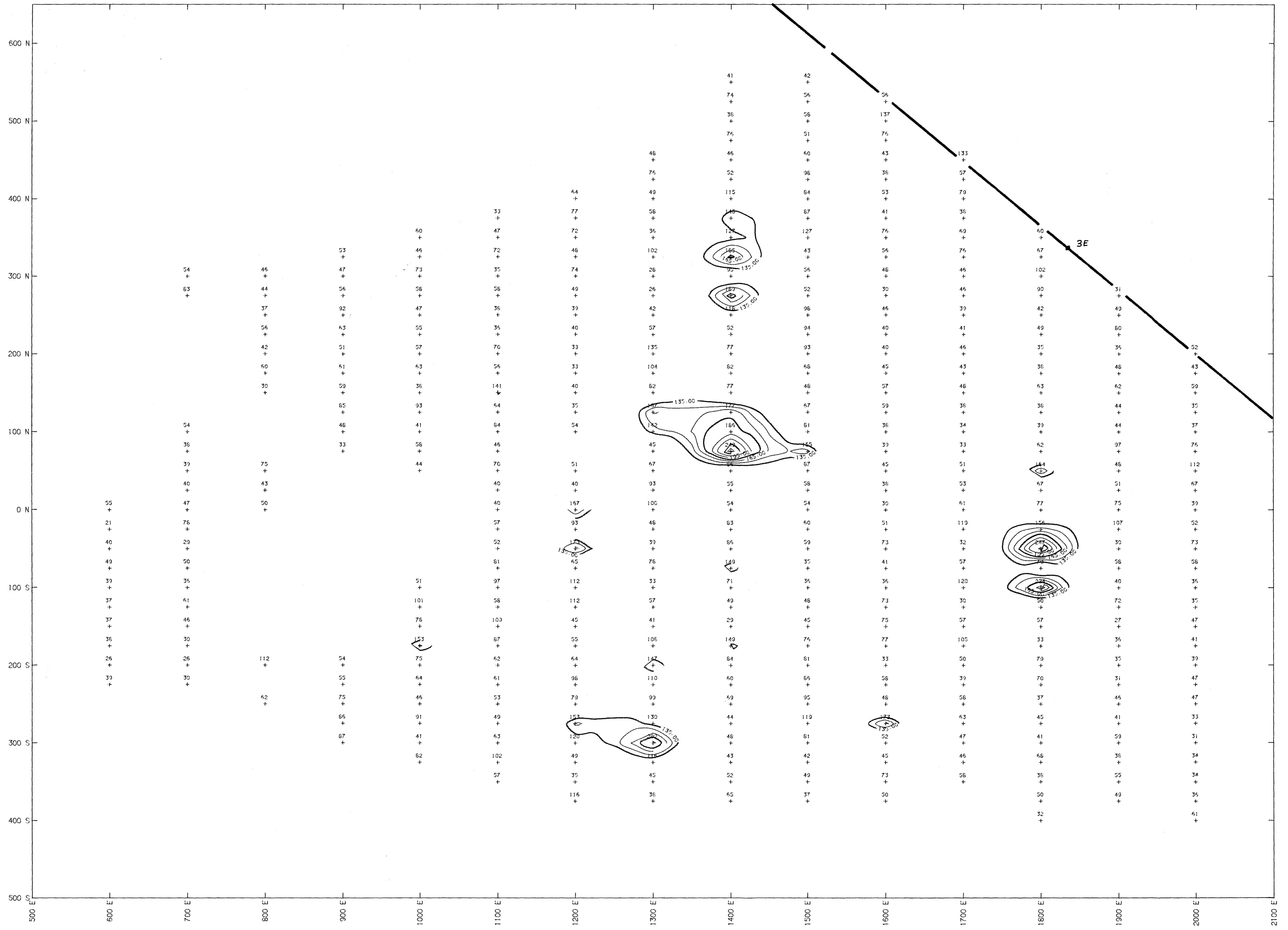
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## NEWMONT EXPLORATION PROJECT-337 File # 87-3943 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P PPM	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na PPM	K %	W PPM	Au#8 PPB	Hg PPB	F PPM
R 14525	2	1	7	82	.2	1	1	2621	1.52	2	5	ND	3	22	1	3	6	1	.13	.007	22	1	.04	124	.01	7	.36	.05	.18	1	1	120	140
R 14527	1	5	6	41	.1	1	1	148	1.28	2	5	ND	2	9	1	2	2	1	.13	.044	7	1	.01	44	.01	11	.24	.05	.19	1	1	3500	130
R 19544	2	4	13	93	.1	1	2	1419	3.81	8	5	ND	1	7	1	2	2	1	.07	.046	7	1	.01	62	.01	16	.32	.04	.16	1	2	350	40
R 19545	1	5	13	90	.1	1	2	2028	4.68	2	5	ND	2	8	1	2	2	1	.09	.046	7	1	.01	66	.01	5	.31	.04	.18	1	1	460	80
R 19546	2	5	12	80	.1	1	2	1852	4.66	2	5	ND	1	8	1	2	2	1	.09	.046	6	1	.01	72	.01	3	.34	.04	.17	1	1	560	100



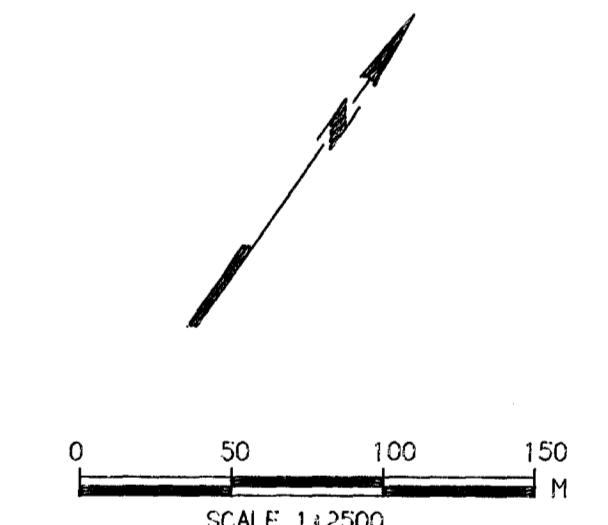




#### LEGEND

#### ZINC IN SOILS

SAMPLE SPACING: 25M  
LINE SPACING: 100M  
SURVEY BY: CHAIN & COMPASS  
HORIZON SAMPLED: B (WHERE DEVELOPED)  
SAMPLE DEPTH: 10CM - 20CM  
BASELINE DIR: 055 AZIMUTH  
THRESHOLD: 135 PPM  
CONTOUR INTERVAL: 15 PPM



GEOLOGICAL BRANCH  
ASSESSMENT REPORT

**16,581**

NEWMONT EXPLORATION LTD.
OOTSA 1 CLAIM
OMINECA MINING DIVISION
ZINC IN SOILS
SURVEY BY: JN DRAWN BY: JN NTS: 93F/11E
DATE: 11/25/87 SCALE: 1:2500 NO: MAP 5

