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METALLURGY OF
OWEN LAKE DEPOSIT

Prepared for:

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A S S E S S M E N T R E P O R T

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Part 1 of 3

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SECTION 1

SUMMARY

A flowsheet which produces copper, lead and zinc concentrates by differential flotation has been developed for the Owen Lake deposit of Houston Metals Corporation. The flowsheet development was performed with a composite ore sample using batch flotation tests. The viability of the flowsheet was confirmed by means of locked-cycle flotation testing. The results obtained with the composite sample are as follows:

| Product | Cu % | Pb % | Zn % | Au oz/ton | Ag oz/ton |
|-------------|---------|---------|---------|--------------|--------------|
| Copper conc | 27.6 | 5.2 | 8.1 | 0.590 | 301.4 |
| Lead conc | 5.2 | 43.6 | 10.0 | 0.292 | 71.6 |
| Zinc conc | 1.1 | 0.7 | 51.1 | 0.071 | 12.7 |
| Tailing | 0.1 | 0.3 | 0.36 | 0.043 | 2.5 |
| Feed | 1.14 | 1.90 | 7.56 | 0.068 | 14.8 |

| Product | Recovery, % | | | | |
|-------------|-------------|------|------|------|------|
| | Cu | Pb | Zn | Au | Ag |
| Copper conc | 66.5 | 8.3 | 3.5 | 23.1 | 59.5 |
| Lead conc | 13.7 | 76.1 | 4.9 | 12.5 | 15.5 |
| Zinc conc | 12.5 | 4.8 | 87.9 | 13.9 | 11.5 |
| Tailing | 7.3 | 10.8 | 3.7 | 50.4 | 13.5 |

While these results are acceptable, they are not the optimum results achieved in the testwork. During the batch testwork, selective concentrates were produced which are higher in content of the desired metal, and lower in impurities. With optimization of conditions during continuous operation, results which are even better than those presented above should be achievable.

Samples from individual veins show considerable variation in the results obtained, compared to the above results. The reason for this variation is that the composition of these veins varies widely, from almost copper free and high in lead to high in copper and almost lead free. Since the ore is prone to oxidation it cannot be stored after mining in order to carry out blending. The mill will have to accept feed from whatever area is being mined. The mill operators will have to learn to respond to changes in the feed composition as it affects the circuit performance. Although the intended plant is relatively small, the feasibility of installing some degree of on-line process control should be investigated.

The possibility exists to recover additional gold and silver from the flotation tails by cyanidation of a pyrite concentrate produced from these tails. In order to be economically viable, some form of cyanide regeneration would be mandatory. Economic comparisons of cyanide regeneration technologies are required to evaluate this option.

The concentrations of trace metals such as gallium and germanium are too low to result in payment for these metals. They are present in sufficient concentration however that they should contribute to the negotiation of favourable smelter terms.

The present circuit configuration does not provide for regrinding of rougher concentrates prior to cleaning as this did not appear to be required. Provision should be made in the plant layout for the installation of regrind circuits in the event that some areas of the mine require regrinding of the concentrates.

SECTION 2

INTRODUCTION

A metallurgical investigation of samples from the Owen Lake Mine was undertaken by Bacon, Donaldson & Assoc. Ltd. at the request of Mr. W. W. Cummings and Mr. A. A. Petancic of Houston Metals Corp. The scope of the test program initially was to carry out a preliminary metallurgical investigation of samples from several areas of the min. This scope was increased at a later date to include more detailed metallurgical work which would establish a flowsheet capable of producing marketable copper, lead and zinc concentrates.

While it is recognized that the different areas in the mine vary to a considerable degree with regard to Cu-Pb-Zn ratios, much of the detailed testwork was done on a composite sample intended to approximate the mill feed expected during the initial period of operation. Several other samples were tested subsequently to observe the effect of extremes in mineralogy on the results which could be achieved.

SECTION 3 PROCESS DESCRIPTION

The flowsheet proposed for treatment of the Owen Lake deposit is shown in Figure 1. This flowsheet is based on locked cycle testwork included in this report as Test 10F11.

The incoming ore is ground to 70% passing 200 mesh prior to copper-lead bulk flotation. The bulk copper-lead concentrate is cleaned twice with reagent additions to depress sphalerite and pyrite. The cleaned bulk Cu-Pb concentrate is conditioned in two stages to deactivate the lead. The copper is floated off to produce the final copper concentrate while the tails comprise the lead concentrate.

The copper-lead bulk flotation tailings, together with cleaner tailings from the Cu-Pb and Zn circuits are conditioned in two stages to activate the zinc prior to zinc rougher flotation. The zinc rougher concentrate is cleaned twice with depression of pyrite to produce the final zinc concentrate.

The zinc rougher tails form the final plant tails. The production of a pyrite concentrate for gold-silver recovery has not been included at this time. If such a concentrate was to be produced, a short conditioning stage followed by a flotation stage would be introduced prior to discharge of the tails.

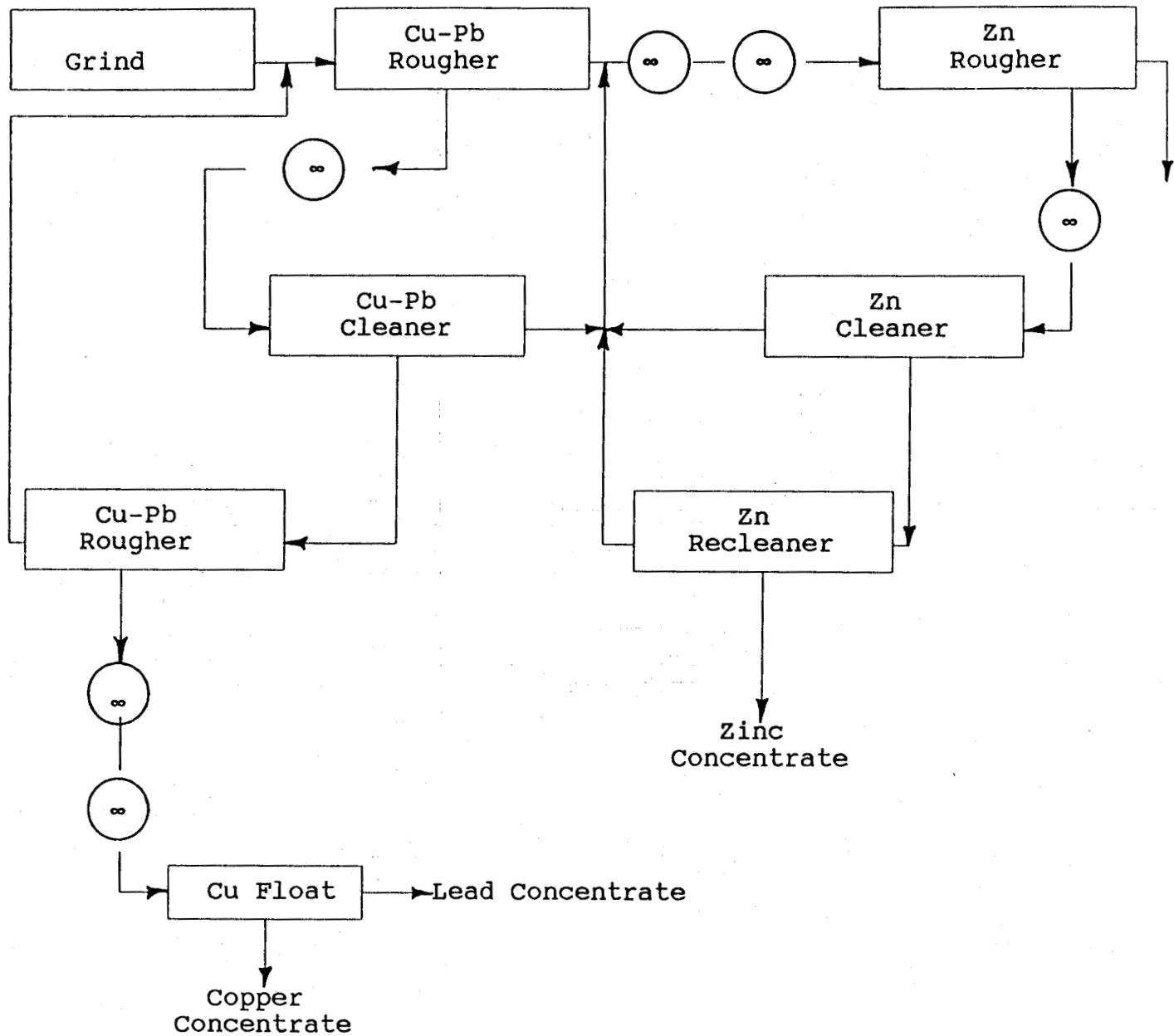


FIGURE 1

PROCESS FLOWSHEET

Residence Times (Batch)

| | |
|------------------------|------------|
| Cu-Pb rougher | 10 minutes |
| Condition | 5 |
| Cu-Pb cleaner | 10 |
| Cu-Pb recleaner | 7 |
| Cu condition - stage 1 | 20 |
| - stage 2 | 20 |
| Cu float | 5 |
| Zn condition - stage 1 | 5 |
| - stage 2 | 5 |
| Zn rougher | 8 |
| Condition | 5 |
| Zn cleaner | 6 |
| Zn recleaner | 5 |

The Cu-Pb rougher flotation time appears to be a critical parameter. While most of the batch tests were done on a 2 kilogram scale, several were done on a 12 kilogram scale. For these larger tests the rougher flotation time had to be increased to 18 minutes while the other times were relatively unchanged.

The copper float time must not be made excessive. With increased flotation time at this stage excessive lead starts to float. It is possible that this problem could be controlled through continued sulphurous acid (SO_2) addition to the flotation cells.

Reagent Consumption

| Reagent | lb/ton | kg/tonne |
|---------------------------------|--------|----------|
| NaCn | 0.65 | 0.33 |
| Na ₂ SO ₃ | 4.0 | 2.0 |
| ZnSO ₄ | 1.5 | 0.75 |
| R-200 | 0.12 | 0.06 |
| Aero 238 | 0.03 | 0.015 |
| MIBC | 0.05 | 0.025 |
| Lime | 7.4 | 2.7 |
| CuSO ₄ | 0.8 | 0.4 |
| Aero 343 | 0.095 | 0.047 |
| DF 1012 | 0.04 | 0.02 |
| Dextrin | 0.11 | 0.06 |
| Sulphurous Acid | 96 | 48 |

In full plant operation it will likely be preferable to replace the sulphurous acid addition with sulphur dioxide.

SECTION 4
SAMPLE DESCRIPTION

The preliminary metallurgical testwork described in the report dated March 12, 1987 by W. G. Bacon, P.Eng., was done on four samples. The descriptions and analyses of these samples are summarized in Table 4.1.

Table 4.1
Analyses of Samples Used for
Preliminary Testwork

| | Vein No.2 | Vein No.5 | High Zn High FeS ₂ | Ruby Vein |
|------------|--------------|--------------|----------------------------------|--------------|
| Cu, % | 0.13 | 1.658 | 0.40 | 3.32 |
| Pb, % | 4.13 | 0.665 | 0.74 | 0.78 |
| Zn, % | 10.99 | 4.369 | 9.80 | 11.40 |
| Fe, % | 7.04 | 7.171 | 10.74 | 20.53 |
| S, % | 8.70 | 7.107 | 16.88 | 56.18 |
| Au, oz/ton | 0.068 | 0.088 | 0.090 | 0.073 |
| Ag, oz/ton | 2.208 | 16.338 | 5.738 | 39.445 |

Prior to the commencement of the detailed flowsheet development, three additional samples were received. The analysis of these samples are summarized in Table 4.2, together with the analysis of a composite sample (composite No. 2) having the following make-up:

| <u>Composite No. 2</u> | <u>Weight %</u> |
|------------------------|-----------------|
| Vein No. 2 | 27.8 |
| Vein No. 5 | 11.1 |
| Footwall Vein | 16.7 |
| Ruby Vein | 22.2 |
| No. 3 Extension | 22.2 |

Table 4.2
Analysis of Samples Used for
Detailed Testwork

| | No. 3 Extension | Switchback Vein | M3 Vein | Composite No. 2 |
|------------|--------------------|--------------------|------------|--------------------|
| Cu, % | 0.86 | 0.10 | 0.61 | 1.20 |
| Pb, % | 0.96 | 4.24 | 0.94 | 2.10 |
| Zn, % | 1.68 | 12.40 | 30.4 | 8.48 |
| Fe, % | 16.30 | 10.92 | 12.95 | 13.13 |
| S, % | 19.59 | 17.00 | 26.74 | 16.75 |
| Au, oz/ton | 0.073 | 0.113 | 0.183 | 0.071 |
| Ag, oz/ton | 10.012 | 1.740 | 24.275 | 14.866 |

Each sample was prepared for testwork by stage crushing to minus 6 mesh prior to 2 kilogram test samples being riffled out.

SECTION 5 DISCUSSION

5.1 Cu-Pb ROUGHER FLOTATION

The conditions for Cu-Pb rougher flotation changed little throughout the test program. Pyrite and zinc depression was achieved through the use of NaCN, Na₂SO₃ and ZnSO₄. Copper and lead activation was achieved with Z-200 (available as reagent 200) and Aerofloat 238.

The pH in the Cu-Pb roughers was allowed to remain at the natural value for the ore. The natural pH varied from 5.1 for the Ruby Vein to 7.9 for the High Zn-High pyrite ore. There was no apparent correlation between the pH during Cu-Pb flotation and the recovery achieved for these metals.

There was some correlation between decreasing feed assay and decreasing recovery for both copper and lead in the rougher concentrate. The recoveries achieved with several samples are summarized in Table 5.1.

Table 5.1
Copper-Lead Rougher Recoveries

| Sample | Head Assay | | Rougher Recovery | |
|------------|------------|------|------------------|------|
| | % Cu | % Pb | Cu | Pb |
| Ruby Vein | 3.32 | 0.78 | 91.8 | 70.1 |
| No. 3 Ext. | 0.86 | 0.96 | 80.6 | 86.2 |
| Switchback | 0.10 | 4.24 | 51.1 | 86.3 |
| M3 | 0.61 | 0.94 | 82.0 | 83.5 |
| Comp. 2 | 1.20 | 2.10 | 90.8 | 90.3 |

It was observed during the testwork that adequate rougher flotation time was important to maintaining high recoveries. For tests which were done on a 2 kilogram scale, a rougher flotation time of 10 minutes proved to be adequate. For tests done on a 12 kilogram scale, this time had to be increased to 18 minutes.

5.2 Cu-Pb CLEANER FLOTATION

The objective of the Cu-Pb cleaner flotation is to maintain the maximum recovery of these elements while at the same time rejecting pyrite and sphalerite.

The initial tests summarized in Table 5.2 used 1.5 lb/ton Na_2SO_3 and 1.0 lb/ton ZnSO_4 for pyrite and sphalerite depression. While these reagents appeared to give acceptable results for some feed materials (ie, No. 3 extension) for other samples, excessive pyrite continued to float.

Table 5.2

Cu-Pb Cleaner Results Without Cyanide Addition

| Test No. | Sample | Cu-Pb Cleaner Concentrate | | | | |
|-------------|------------|---------------------------|------|------|------|------|
| | | % Cu | % Pb | % Zn | % Fe | % S |
| 7F1 | #3 Ext | 14.0 | 18.0 | 7.4 | 15.7 | 31.1 |
| 8F1 | Switchback | 1.1 | 60.0 | 10.8 | 7.1 | 21.0 |
| 9F1 | M3 | 8.6 | 13.2 | 10.4 | 24.4 | 38.2 |

An additional test (7F2) was done on the #3 Extension sample with increased sodium sulphite plus cyanide additions to the cleaners.

The concentrate produced in this test had the following composition:

| | |
|-------|----|
| 20.0% | Cu |
| 30.8% | Pb |
| 5.0% | Zn |
| 6.9% | Fe |
| 24.3% | S |

The concentrate grade was improved over that produced in test 7F1 but both copper and lead recovery decreased by about 30%. A balance has to be achieved therefore between having sufficient cyanide present to depress the pyrite and not having so much that it depresses the copper and lead minerals. While the Cu and Pb concentration in the various test samples varies greatly, the pyrite concentration varies to a lesser degree. Once the appropriate cyanide level is established for a composite samples it should therefore also be suitable for material from the various individual veins.

Following Test 7F2, the remaining development work was done on the composite #2 sample. In Test 10F1, the cyanide addition to the first Cu-Pb cleaner was reduced from 0.2 to 0.1 lb/ton and to the second cleaner it was removed completely. Recoveries were maintained at high levels in this test while at the same time maintaining acceptable concentrate grades. No subsequent changes were made to the reagent additions to the Cu-Pb cleaners.

For most of the testwork the Cu-Pb rougher concentrate was reground prior to cleaning. It was observed that when a porcelain reground mill was used for regrinding, the results appeared to be much better than when a steel mill was used. This was confirmed in Test 10F8. The rougher concentrate was split in

half and one half was reground with porcelain while the other half was reground with steel. The results summarized in Table 5.3 indicate much higher losses when steel was used for regrinding.

Table 5.3

Effect of Grinding Media on Losses to Cleaners

| Media | Cleaner | <u>% losses to tails</u> | |
|-----------|---------|--------------------------|------|
| | | Cu | Pb |
| Steel | 1st | 6.4 | 1.5 |
| | 2nd | 16.3 | 24.9 |
| Porcelain | 1st | 5.0 | 1.6 |
| | 2nd | 7.8 | 5.7 |

It is apparent that the use of steel results in increased losses to the cleaner tails, particularly in the 2nd cleaners. It would therefore be much preferable if the regrind could be eliminated since the need for pebble milling represents an undesirable complication. Test 10F10 was done without regrinding to establish whether it is in fact required. Table 5.4 compares the results of tests with and without regrinding prior to cleaning.

Table 5.4

Cu-Pb Cleaner Concentrate With and Without Regrinding

| Test No. | Regrind | <u>Assays, %</u> | | | | <u>Recovery, %</u> | | | |
|----------|---------|------------------|------|------|-----|--------------------|------|-----|-----|
| | | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| 10F9 | Yes | 14.3 | 26.0 | 6.3 | 8.8 | 69.8 | 83.3 | 4.4 | 4.1 |
| 10F10 | No | 15.9 | 26.2 | 10.0 | 9.6 | 78.3 | 84.9 | 7.6 | 4.6 |

Omitting the regrind does not have a detrimental effect on copper and lead recovery although it does increase the zinc and iron reporting to the bulk concentrate. It appears that for the composite sample, a regrind is not justified.

Tests 4F3 and 8F1 were done on the Ruby vein and Switchback vein respectively, without regrinding of the rougher concentrate. Both tests resulted in acceptable cleaning results, indicating that operation without a regrind will lead to satisfactory concentrate grades and recoveries.

5.3 Cu-Pb SEPARATION

Two copper-lead separation procedures were tested on the concentrate. Conditioning of the bulk concentrate at elevated temperature with starch and sodium bisulphite (Test 10F6) was found to be ineffective.

The separation procedure which has been determined to give good separation results on the composite feed consists of two stages of conditioning followed by flotation of the copper. In the first conditioning step, dextrin and active carbon are added. After a 20 minute conditioning period, sulphurous acid is added to maintain a pH of 4.8 for an additional 20 minutes. At the completion of conditioning, the copper is floated with an addition of Z-200. The separation results achieved in several tests are summarized in Table 5.5.

Table 5.5
Cu-Pb Separation Results for Composite Feed Sample

| Test No. | Dextrin lb/ton | $H_2SO_3^*$ lb/ton | Cu Conc | | | | Pb Conc | | | |
|----------|----------------|--------------------|---------|------|--------|--------|---------|------|--------|--------|
| | | | %Cu | %Pb | Cu Rec | Pb Rec | %Cu | %Pb | Cu Rec | Pb Rec |
| 10F3 | 0.06 | 96 | 33.2 | 9.6 | 34.0 | 6.4 | 1.1 | 64.6 | 1.39 | 52.8 |
| 10F7 | 0.06 | 3 | 19.0 | 36.0 | 66.3 | 58.0 | 9.8 | 16.8 | 4.0 | 3.2 |
| 10F9 | 0.11 | 42 | 18.9 | 27.8 | 64.7 | 62.6 | 3.5 | 21.7 | 5.1 | 20.7 |
| 10F10 | 0.11 | 68 | 26.5 | 6.2 | 74.9 | 11.5 | 1.6 | 52.8 | 3.5 | 73.5 |

* H_2SO_3 addition represents lb/ton of 6% solution

The low recoveries shown for Test 10F3 resulted from losses during bulk concentrate cleaning. This test achieved high grade copper and lead concentrates and demonstrated that a separation could be made. In Tests 10F7, 10F9 and 10F10 the pH during conditioning was in each case maintained at 4.8. However, increasing additions of H_2SO_3 were made at the start of the conditioning period. The results are apparent in Table 5.5 with decreasing lead floating with the copper as the sulphurous acid addition is increased.

During the conditioning with H_2SO_3 the lead is depressed but this depression is not permanent. At the start of the copper flotation this froth is a dull gray as the tetrahedrite-tennantite floats. Once the flotation of the copper minerals is complete, additional flotation time results in lead flotation. This lead flotation is visually apparent as the froth becomes bluish-gray, characteristic of galena flotation. The operators in the plant will have to learn the color differences during flotation so that flotation of lead into the copper concentrate is avoided. Providing for additional SO_2 addition to the flotation cells should help to mitigate this problem.

The results indicate that for a composite sample having an "average" composition a satisfactory separation can be made. The composition of feed to the circuit can be expected to vary widely as feed is derived from predominantly one vein or another. Table 5.6 presents results for the composite sample as well as for samples which represent extremes in composition.

Table 5.6
**Cu-Pb Separation Results for Samples Having
Varying Cu-Pb Ratios**

| Test No. | H ₂ SO ₃ lb/ton | Product | % Cu | % Pb | % Rec Cu | % Rec Pb |
|----------|---------------------------------------|---------|-------|------|----------|----------|
| 10F10 | 68 | Feed | 15.86 | 26.2 | 78.3 | 85.0 |
| | | Cu Conc | 26.5 | 6.2 | 74.9 | 11.5 |
| | | Pb Conc | 1.6 | 52.8 | 3.5 | 73.5 |
| 4F3 | 194 | Feed | 22.3 | 4.4 | 79.5 | 63.0 |
| | | Cu Conc | 24.4 | 3.0 | 78.1 | 39.2 |
| | | Pb Conc | 4.0 | 16.3 | 1.4 | 23.7 |
| 8F2 | 50 | Feed | 0.4 | 56.5 | 17.5 | 56.6 |
| | | Cu Conc | 0.4 | 58.6 | 17.2 | 56.1 |
| | | Pb Conc | 0.14 | 10.4 | 0.2 | 0.5 |

Test 4F3 was conducted on Ruby vein material which contains very little lead. The results indicate that copper flotation was satisfactory and that lead was depressed preferentially. Due to the low lead content of the feed, the lead concentrate has a very low lead content. This situation could not be avoided unless the separation was bypassed when only Ruby vein material was being processed.

Test 8F2 was conducted on Switchback vein material which has negligible copper but is high in lead. With this feed the lead was not adequately depressed and continued to float after conditioning. It was immediately apparent during flotation that

the concentrate consisted almost entirely of galena. With this type of feed the flotation operator would have to visually decide to bypass the separation to the lead concentrate thickener.

5.4 ZINC ROUGHER FLOTATION

The objectives during zinc rougher flotation are to maximize zinc recovery without excessive flotation of iron sulphides and to activate zinc to a sufficient extent that cleaning can be achieved with minimal additional reagent additions. The above objectives were achieved readily with few reagent variations. In Test 10F2 the reagent additions were increased to the following quantities and these were used for all subsequent testwork including the locked-cycle testing:

lime to pH = 10.5
0.6 lb/ton CuSO₄
0.1 lb/ton NaCN
0.03 lb/ton Z-200
0.075 lb/ton Aero 343
Dowfroth 1012

The success of zinc recovery was difficult to judge during batch testing due to flotation of zinc in copper-lead roughers. However, it is significant to note that generally less than 3% of the zinc reported to the final tails. During locked-cycle testing with recirculation of all streams this loss increased to only approximately 3.5%.

5.5 ZINC CLEANER FLOTATION

As for the zinc roughers, the zinc cleaners strive to maintain zinc recovery while achieving maximum rejection of iron sulphides. Sodium cyanide was used to depress the pyrite while Z-200, CuSO₄ and Aero 343 (isopropyl xanthate) were used to maintain zinc activation.

Throughout the test program the variations in reagent addition to the zinc cleaners were minor. The main variation was in the cyanide addition, varying from 0.175 to 0.2 lb/ton. The optimum level for the composite sample appears to be 0.2 lb/ton NaCN. It was found that a true indication for reagent additions to zinc cleaning was only obtained from locked cycle testing (Tests 10F4 and 10F11). During batch testing the effects of recirculating the zinc and pyrite present in the lead cleaner tails do not become apparent. The results of Test 10F4 indicated that a large proportion of the zinc would report to the zinc cleaner tails with the quantities of reagent used in that test (ie, 0.25 lb/ton NaCN, 0.02 lb/ton Z-200). In Test 10F11 it was determined that while an addition of 0.175 oz/ton NaCN resulted in excessive pyrite flotation, increasing the cyanide to 0.2 lb/ton gave zinc concentrates containing 53 to 56% zinc while maintaining recovery.

Tests on the composite sample prior to Test 10F10 involved regrinding of the zinc rougher concentrate prior to cleaning. This regrind was eliminated in Tests 10F10 and 10F11. While it is difficult to compare the effects of eliminating the regrind because reagent changes were made at the same time, the results of Test 10F11 (51% Zn at 81.5% recovery) are acceptable indicating that a regrind is not mandatory for this feed material.

Table 5.7 summarizes the results of Ruby vein and Switchback vein material for zinc cleaning without regrinding and with reagent additions at levels developed for the composite sample.

Table 5.7
Zinc Cleaning of Ruby Vein and Switchback
Vein Rougher Concentrates

| Test No. | Sample | Assay | | % Distribution | |
|----------|-----------------------------------|-------|-------|----------------|------|
| | | Zn, % | Fe, % | Zn | Fe |
| 4F3 | Ruby - Rougher - Cleaner | 24.9 | 23.1 | 77.5 | 38.8 |
| | | 33.6 | 17.7 | 26.9 | 7.7 |
| 8F2 | Switchback - Rougher - Cleaner | 33.3 | 11.4 | 79.4 | 30.5 |
| | | 48.7 | 5.3 | 73.5 | 8.9 |

While the results for the switchback vein material are acceptable, the results for the Ruby vein ore are very poor. It is not immediately apparent whether the poor results are due to a lack of regrinding prior to cleaning because the zinc rougher results in Test 4F3 were also poor. The composite #2 sample contains 22.2 weight % Ruby Vein material so regrinding of this material is not a controlling factor when it is being treated together with other materials.

5.6 LOCKED CYCLE TESTING

Test 10F4 was performed as a locked-cycle test. While the Cu-Pb flotation conditions appeared to be adequate, zinc recovery was very poor due to a high circulating load through the zinc cleaner tails. After additional batch testwork, a second locked-cycle test, 10F11, was carried out. A block flowsheet for this test is included as Figure 2. The details of reagent additions and residence times are included in Appendix I.

The average results over the six cycles are presented in Table 5.8.

Table 5.8
Averaged Locked Cycle Results

| Product | Wt% | Assay, % | | | % Distribution | | |
|-------------|------|----------|------|------|----------------|------|------|
| | | Cu | Pb | Zn | Cu | Pb | Zn |
| Cu-Pb conc | 6.5 | 14.1 | 24.7 | 10.0 | 80.2 | 84.4 | 8.4 |
| Zn conc | 13.3 | 1.1 | 0.7 | 51.1 | 12.5 | 4.8 | 87.9 |
| Tail | 80.2 | 0.1 | 0.3 | 0.36 | 7.3 | 10.8 | 3.7 |
| Feed (calc) | | 1.14 | 1.90 | 7.56 | | | |

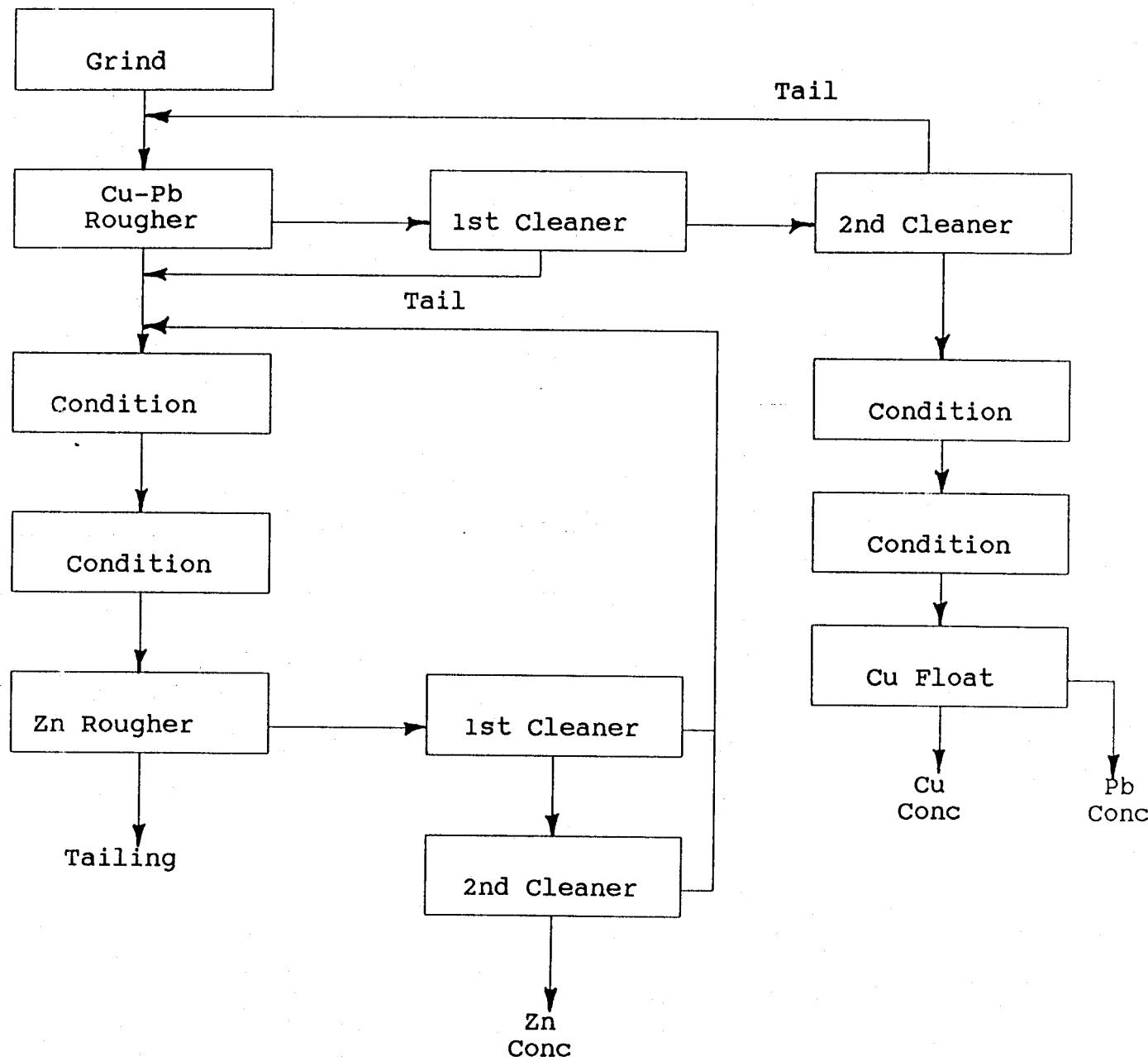


FIGURE 2.

LOCKED-CYCLE TEST BLOCK FLOWSHEET

The Cu-Pb concentrates are reasonably consistent over the six cycles indicating a good reagent balance. The zinc concentrate grade in the first two cycles was judged to be too low because excessive pyrite was visible in the froth. The cyanide addition to the third and subsequent cycle cleaners was increased from 0.175 to 0.2 lb/ton. The improvement in concentrate grade was visually apparent and was confirmed by the assays as the zinc grade went from 46.1% in the second cycle to 53.6% in the third cycle. It is estimated that in continuous operation a zinc grade of 53% Zn could be achieved.

Differential flotation of the bulk Cu-Pb concentrate was performed in the last cycle of the test producing the concentrates summarized in Table 5.9.

Table 5.9
Differential Copper and Lead Concentrates

| Product | Cu % | Pb % | Zn % | Fe % | Au oz/ton | Ag oz/ton |
|---------|---------|---------|---------|---------|--------------|--------------|
| Cu Conc | 27.6 | 5.2 | 8.1 | 12.7 | 0.590 | 301.4 |
| Pb Conc | 5.2 | 43.6 | 10.0 | 8.7 | 0.292 | 71.6 |

The overall locked cycle results compare favorably with those of the batch tests (ie, Test 10F10). This consistency in results indicates that for this composite sample, the reagent additions and residence times are appropriate for continuous operation with recycling of cleaner tails.

5.7 GOLD-SILVER RECOVERY

Batch testing of the composite sample demonstrated that the silver in the feed reports predominantly to the Cu-Pb concentrate. Differential flotation of this product results in a copper concentrate containing most of this silver. Copper concentrates containing in excess of 250 oz/ton Ag were produced.

Approximately 33 to 34% of the gold in the feed reported to the Cu-Pb concentrate. Of this gold, 25% or more follows the copper mineralization resulting in a copper concentrate which contains 0.5 oz/ton Au or more.

The zinc concentrate produced in batch testing (10F10) contained approximately 8% of the silver and 12% of the gold.

The locked-cycle test confirmed the precious metal deportment for the composite sample as summarized in Table 5.10.

Table 5.10
Gold-Silver Distribution in Composite
Sample Locked-Cycle Test

| Product | Assays, oz/ton | | % Distribution | |
|----------------|-----------------------|-----------|-----------------------|-----------|
| | Au | Ag | Au | Ag |
| Cu-Pb Conc | 0.372 | 170.6 | 35.7 | 75.0 |
| Zn conc | 0.071 | 12.7 | 13.9 | 11.5 |
| Tail | 0.043 | 2.5 | 50.4 | 13.5 |
| Feed (calc) | 0.068 | 14.8 | | |

The Cu-Pb concentrate produced in the last cycle of the test was floated differentially to produce copper and lead concentrates. The concentrate grades and calculated recoveries to these products are summarized in Table 5.11.

Table 5.11
**Gold-Silver Distribution in Copper
and Lead Concentrates**

| Product | Assay, oz/ton | | % Distribution | |
|----------------|----------------------|-----------|-----------------------|-----------|
| | Au | Ag | Au | Ag |
| Copper Conc | 0.590 | 301.4 | 23.1 | 59.5 |
| Lead Conc | 0.292 | 71.6 | 12.5 | 15.5 |

Batch testing of samples from the individual veins gave somewhat different results due to the varying mineralogy. These results are summarized in Table 5.12.

Table 5.12
**Gold-Silver Distribution for
Individual Vein Samples**

| Test No. | Vein | Product | Assay, oz/ton | | % Distribution | |
|---------------------|-------------|----------------|----------------------|-----------|-----------------------|-----------|
| | | | Au | Ag | Au | Ag |
| 4F3 | Ruby | Cu-Pb con | 0.125 | 253.9 | 23.8 | 77.8 |
| | | Zn con | 0.060 | 19.2 | 8.1 | 4.2 |
| 7F1 | #3 Ext | Cu-Pb con | 0.228 | 151.1 | 14.4 | 62.8 |
| | | Zn con | 0.286 | 41.5 | 14.9 | 14.2 |
| 8F2 | Switchback | Cu-Pb con | 0.436 | 56.5 | 17.5 | 56.6 |
| | | Zn con | 0.090 | 2.9 | 14.1 | 25.3 |
| 9F1 | M3 | Cu-Pb con | 0.205 | 87.5 | 7.7 | 20.4 |
| | | Zn con | 0.188 | 45.0 | 38.9 | 57.8 |

While it should be noted that several of the tests included in Table 5.12 were done before the reagent additions were finalized and represent products which may be off grade or have low recovery, there are some general trends which are significant. The gold recovery to the combined concentrates is less than 50% in every case and is in most cases near 30%. The total silver recovery is near 80%. The distribution of gold and silver between the two products is not consistent although the Cu-Pb concentrate tends to have a much greater silver content than the Zn concentrate.

Pyrite concentrates were produced in several of the batch tests. The gold and silver content of the pyrite concentrates is misleading in these batch tests because much of the pyrite is contained in the lead and zinc cleaner tails. Table 5.13 summarizes the gold and silver assays of pyrite concentrates produced from several samples.

Table 5.13
Composition of Pyrite Concentrates

| Test No. | Feed | Pyrite Concentrate | |
|----------|------------|--------------------|------------|
| | | Au, oz/ton | Ag, oz/ton |
| 4F3 | Ruby | 0.090 | 8.54 |
| 7F2 | #3 Ext | 0.071 | 4.88 |
| 8F2 | Switchback | 0.180 | 1.96 |
| 10F4 | Composite | 0.110 | 7.20 |

Following the removal of the pyrite concentrates, from 5.58% to 17.12% of the gold in the feed remained in the final tailing.

Table 5.14
Copper Concentrates Trace Element Analyses

| Feed | Cu | Pb | Zn | Hg | As | Cd | Ga | Ge | In |
|-------------|------|-----|------|-------|-------|-----|-----|-----|-----|
| | % | % | % | ppb | % | ppm | ppm | ppm | ppm |
| Ruby Vein | 24.4 | 3.0 | 10.8 | 5125 | 11.72 | 870 | 11 | 233 | 42 |
| Composite 2 | 26.5 | 6.2 | 9.9 | 10875 | 9.66 | 680 | 12 | 192 | 50 |

Table 5.15
Lead Concentrates Trace Element Analyses

| Feed | Cu | Pb | Zn | Hg | As | Cd | Ga | Ge | In |
|-------------|------|------|------|------|------|-----|-----|-----|-----|
| | % | % | % | ppb | % | ppm | ppm | ppm | ppm |
| Ruby Vein | 4.0 | 16.3 | 11.8 | 3125 | 2.09 | 950 | 20 | 157 | 38 |
| Switchback | 0.45 | 58.6 | 4.7 | 1050 | 0.58 | 265 | 1 | 24 | 1 |
| Composite 2 | 0.71 | 56.9 | 8.3 | 4000 | 0.90 | 475 | 11 | 21 | 1 |

Table 5.16
Zinc Concentrates Trace Element Analyses

| Feed | Cu | Pb | Zn | Hg | As | Cd | Ga | Ge | In |
|-------------|------|------|------|------|------|------|-----|-----|-----|
| | % | % | % | ppb | % | ppm | ppm | ppm | ppm |
| Ruby Vein | 1.48 | 0.38 | 33.6 | 6875 | 0.24 | 5400 | 98 | 215 | 132 |
| Switchback | 0.14 | 4.0 | 48.7 | 8000 | 0.15 | 3000 | 34 | 367 | 12 |
| Composite 2 | 0.52 | 0.47 | 48.4 | 9875 | 0.39 | 3375 | 54 | 179 | 108 |

Test 10F4 was a locked-cycle test and it is significant to note that the composition of the pyrite concentrate from this test is in the same range as that of the others. The 10F4 pyrite concentrate was reground to minus 400 mesh and was then cyanided for 48 hours. The test details are included as Appendix II. A gold extraction of 32.8% and a silver extraction of 69.9% was achieved in this test.

Using a gold extraction of 33% and a silver extraction of 70% together with a gold price of \$450 per oz and a silver price of \$7.50 per oz gives recoverable values for the concentrates shown in Table of \$36.14 U.S. to \$58.20 U.S. per ton pyrite. The cyanide consumption in the test was 23.13 kg/tonne (approx. 70 lb/ton) which has a value of approximately \$35. This consumption of cyanide is sufficiently high that some method of cyanide regeneration could be considered. Cyanide regeneration could make the processing of the pyrite concentrate profitable.

5.8 TRACE ELEMENT CONCENTRATION

The Owen Lake deposit is known to contain various impurity elements which may result in penalties or bonus payments at the smelter. The concentration of various elements in copper, lead and zinc concentrates from several feed materials are summarized in Tables 5.14, 5.15 and 5.16. The concentrations of these impurities vary considerably depending on the feed material.

The potential for germanium to generate smelter credits was raised as a consideration early in the test program. Discussions with smelters and concentrate buyers revealed that payment for germanium was unlikely at concentrations less than 1000 ppm. Since the Ge appeared to occur most abundantly in the zinc concentrate, several samples of this product from the composite material were analyzed. Concentrations of Ge of 416 ppm and 506 ppm were determined in zinc concentrate containing 59.2% and

60.0% Zn. Although these concentrations of Ge are lower than those required to obtain payment directly, they could be used as a negotiating point to offset some of the undesirable trace constituents.

APPENDIX I
Flotation Test Details

Summary of Grinds

| Test No. | Cum. % -200 Mesh |
|----------|------------------|
| 4F3 | 75.5 |
| 7F1 | 70.0 |
| 7F2 | 69.4 |
| 8F1 | 72.6 |
| 8F2 | 66.2 |
| 9F1 | 91.4 |
| 10F1 | 76.9 |
| 10F2 | 79.5 |
| 10F3 | 76.5 |
| 10F4 | 74.6 |
| 10F5 | 71.7 |
| 10F6 | 74.0/69.9 |
| 10F7 | 73.4/77.9 |
| 10F8 | 73.3 |
| 10F9 | 76.4 |
| 10F10 | 75.1 |
| 10F11 | 70.1 |

| | |
|-------|-----------|
| 4F3 | 75.5 |
| 7F1 | 70.0 |
| 7F2 | 69.4 |
| 8F1 | 72.6 |
| 8F2 | 66.2 |
| 9F1 | 91.4 |
| 10F1 | 76.9 |
| 10F2 | 79.5 |
| 10F3 | 76.5 |
| 10F4 | 74.6 |
| 10F5 | 71.7 |
| 10F6 | 74.0/69.9 |
| 10F7 | 73.4/77.9 |
| 10F8 | 73.3 |
| 10F9 | 76.4 |
| 10F10 | 75.1 |
| 10F11 | 70.1 |

TESTWORK PROCEDURE

Test No. 6891-4F3

Ruby Vein

| STAGE | TIME (min) | lb/ton | ADDITIONS |
|-----------------------------|---------------|--------------------------------------|--|
| | | | REAGENT |
| GRIND | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ pH = 5.7 ZnSO ₄ Z-200 |
| CU/PB ROUGHER | 10 | 0.03 0.05 | Aero 238 MIBC |
| ZN CONDITION | 5 5 | 2.712 0.6 0.1 0.03 0.075 | Lime to pH = 10.5 CuSO ₄ NaCN Z-200 Aero 343 |
| ZN ROUGHER | 8 | 0.040 | DF1012 |
| PYRITE FLOAT | 9 | 33.0 0.2 0.06 | H ₂ SO ₄ to pH = 6 Aero 350 DF1012 |
| CU/PB CLEANING CONDITION | 5 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| CU/PB CLEANER | 10 | | |
| CU/PB RECLEANER | 7 | 1.0 | Na ₂ SO ₃ |
| ZN CLEANING CONDITION | 5 | 0.40 | Litre to pH = 10.8 |
| ZN CLEANER | 8 | 0.2 0.03 0.30 0.03 | NaCN Z-200 CuSO ₄ Aero 343 |

TESTWORK PROCEDURE

Test No. 6891-4F3

Ruby Vein

| STAGE | TIME (min) | ADDITIONS | |
|-------------------------|---------------|--------------|-----------------------------------|
| | | lb/ton | REAGENT |
| ZN RECLEANER | 5 | 0.35 | Lime to pH = 11.5 |
| CU/PB SEPN CONDITION | 20 | 0.22 0.22 | Dextrin Carbon |
| CONDITION | 20 | 194 ml | 6% sulphurous acid to pH = 4.8 |
| SCREEN OUT CARBON | | | |
| COPPER FLOAT | 10 | 0.02 | Z-200 |

TEST NUMBER: 6891-4F3 FLOTATION OF RUBY VEIN- CU/PB SEPARATION PAGE 2

| PRODUCT | WEIGHT | WEIGHT | ASSAYS | | | | UNITS | | | | % DIST | | | |
|-------------------|--------|--------|--------|--------|--------|--------|---------|--------|----------|----------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| Cu CONC | 398.8 | 10.20 | 24.400 | 3.040 | 10.840 | 11.980 | 248.810 | 30.999 | 110.537 | 122.162 | 78.08 | 39.25 | 10.96 | 6.54 |
| Pb CONC | 44.8 | 1.15 | 4.000 | 16.350 | 11.840 | 18.380 | 4.582 | 18.729 | 13.563 | 21.055 | 1.44 | 23.71 | 1.35 | 1.13 |
| Cu/Pb CONC | 443.6 | 11.34 | 22.340 | 4.384 | 10.341 | 12.826 | 253.392 | 49.729 | 124.100 | 143.216 | 79.52 | 62.96 | 12.31 | 7.67 |
| Cu/Pb 2nd CL TAIL | 46.3 | 1.18 | 18.800 | 1.280 | 18.480 | 9.120 | 22.257 | 1.515 | 19.510 | 10.797 | 6.98 | 1.92 | 1.94 | 0.58 |
| Cu/Pb 1st CL CONC | 489.9 | 12.53 | 22.005 | 4.091 | 11.484 | 12.295 | 275.849 | 51.244 | 143.610 | 154.013 | 86.50 | 64.88 | 14.24 | 8.25 |
| Cu/Pb 1st CL TAIL | 204.9 | 5.24 | 3.200 | 0.790 | 7.980 | 26.000 | 16.765 | 4.139 | 41.704 | 136.219 | 5.26 | 5.24 | 4.14 | 7.29 |
| Cu/Pb RO CONC | 694.8 | 17.77 | 16.459 | 3.117 | 10.431 | 16.337 | 292.415 | 55.363 | 185.314 | 290.233 | 91.76 | 70.12 | 18.38 | 15.54 |
| Zn CONC | 316.1 | 8.08 | 1.480 | 0.360 | 33.600 | 17.700 | 11.962 | 3.071 | 271.573 | 143.061 | 3.75 | 3.89 | 26.93 | 7.66 |
| Zn 2nd CL TAIL | 282.0 | 7.21 | 0.310 | 0.124 | 47.820 | 7.890 | 2.235 | 0.894 | 344.812 | 56.892 | 0.70 | 1.13 | 34.20 | 3.05 |
| Zn 1st CL CONC | 598.1 | 15.29 | 0.928 | 0.259 | 40.305 | 13.075 | 14.197 | 3.965 | 616.385 | 199.353 | 4.48 | 5.02 | 61.13 | 10.71 |
| Zn 1st CL TAIL | 628.0 | 16.06 | 0.280 | 0.232 | 10.260 | 32.720 | 4.496 | 3.725 | 164.752 | 525.407 | 1.41 | 4.72 | 16.34 | 28.13 |
| Zn RO CONC | 1226.1 | 31.35 | 0.596 | 0.245 | 24.916 | 23.137 | 18.694 | 7.691 | 781.137 | 725.360 | 5.87 | 9.74 | 77.47 | 38.84 |
| PYRITE CONC | 403.1 | 10.31 | 0.260 | 0.284 | 2.010 | 38.880 | 2.680 | 2.927 | 20.717 | 400.740 | 0.84 | 3.71 | 2.05 | 21.46 |
| TAIL | 1586.9 | 40.58 | 0.120 | 0.320 | 0.520 | 11.120 | 4.869 | 12.984 | 21.100 | 451.209 | 1.53 | 16.44 | 2.09 | 24.16 |
| CALC HEAD | 3910.9 | 100.0 | 3.187 | 0.790 | 10.083 | 18.875 | 318.857 | 78.985 | 1008.268 | 1867.541 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6891-4F3 FLOTATION OF RUBY VEIN- CU/PB SEPARATION PAGE 1

| PRODUCT | WEIGHT | WEIGHT | Au | Ag | ASSAYS | | UNITS | % DIST | |
|-------------------|--------|--------|--------|---------|--------|----|-------|----------|--------|
| | GMS | % | oz/ton | oz/ton | Au | Ag | | Au | Ag |
| Cu CONC | 398.8 | 10.20 | 0.126 | 272.840 | | | 1.285 | 2782.188 | |
| Pb CONC | 44.8 | 1.15 | 0.116 | 85.360 | | | 0.133 | 97.781 | |
| Cu/Pb CONC | 443.6 | 11.34 | 0.125 | 253.906 | | | 1.418 | 2879.969 | |
| Cu/Pb 2nd CL TAIL | 46.3 | 1.18 | 0.090 | 152.784 | | | 0.107 | 180.853 | |
| Cu/Pb 1st CL CONC | 489.9 | 12.53 | 0.122 | 244.347 | | | 1.524 | 3060.622 | |
| Cu/Pb 1st CL TAIL | 204.9 | 5.24 | 0.080 | 26.232 | | | 0.419 | 137.435 | |
| Cu/Pb RO CONC | 694.8 | 17.77 | 0.103 | 180.024 | | | 1.943 | 3198.257 | |
| Zn CONC | 318.1 | 8.08 | 0.060 | 19.248 | | | 0.485 | 155.573 | |
| Zn 2nd CL TAIL | 282.0 | 7.21 | 0.034 | 5.138 | | | 0.245 | 37.048 | |
| Zn 1st CL CONC | 598.1 | 15.29 | 0.048 | 12.595 | | | 0.730 | 192.621 | |
| Zn 1st CL TAIL | 628.0 | 16.06 | 0.086 | 7.970 | | | 1.381 | 127.980 | |
| Zn RO CONC | 1228.1 | 31.35 | 0.067 | 10.226 | | | 2.111 | 320.601 | |
| PYRITE CONC | 403.1 | 10.31 | 0.090 | 8.540 | | | 0.928 | 88.023 | |
| TAIL | 1586.9 | 40.58 | 0.024 | 2.350 | | | 0.974 | 95.354 | |
| CALC HEAD | 3910.9 | 100.0 | 0.060 | 37.022 | | | 5.958 | 3702.234 | |
| | | | | | | | | 100.00 | 100.00 |

TESTWORK PROCEDURE

TEST NO. 6891 - 7F1

DATE _____

No. 3 Ext.

| STAGE | TIME (min.) | ADDITIONS | |
|------------------------|----------------|---------------------------------------|--|
| | | Lb./Ton | REAGENT |
| Grind 55% solids | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ ZnSO ₄ Z-200 pH=6.4 |
| Cu/Pb Rougher | 6 | 0.03 0.050 | AERO 238 pH=6.6 MIBC |
| Zn Condition | 5 5 | 11.89 0.45 0.10 0.02 0.05 | Ca(OH) ₂ to pH-10.5 CuSO ₄ NaCN Z-200 AERO 343 |
| Zn Rougher | 8 | 0.04 | DF 1012 |
| Cu/Pb Cleaning/Regrind | 15 | 1.5 1.0 | Na ₂ SO ₃ ZnSO ₄ |
| Cu/Pb 1st Cleaner | 7 | 0.02 | Z-200 |
| Cu/Pb 2nd Cleaner | 6 | --- | --- |
| Zn Cleaning/Regrind | 15 | 0.10 | CuSO ₄ |
| Condition | 5 | 1.83 | Ca(OH) ₂ to pH=10.8 |
| Zn 1st Cleaner | 6 | 0.25 0.20 0.02 0.05 0.10 | NaCN CuSO ₄ Z-200 AERO 343 CuSO ₄ |
| Zn 2nd Cleaner | 4 | --- | --- |

TEST NUMBER: 6891-7F1 FLOTATION OF #3 EXT. PAGE 2

| PRODUCT | WEIGHT | | WEIGHT | | ASSAYS | | | | | UNITS | | | | | % DIST | | | | |
|-------------------|--------|-------|--------|--------|--------|--------|--------|--------|--------|---------|----------|----------|--------|--------|--------|--------|--------|--|--|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | S% | Cu | Pb | Zn | Fe | S | Cu | Pb | Zn | Fe | S | | |
| Cu/Pb CONC | 88.1 | 4.59 | 14.000 | 18.000 | 7.360 | 15.670 | 31.110 | 64.290 | 82.658 | 33.798 | 71.953 | 142.861 | 79.10 | 83.33 | 21.67 | 4.20 | 7.42 | | |
| Cu/Pb 2nd CL TAIL | 27.8 | 1.45 | 0.470 | 1.320 | 9.600 | 19.800 | 25.810 | 0.581 | 1.913 | 13.311 | 28.691 | 37.400 | 0.84 | 1.93 | 8.92 | 1.68 | 1.94 | | |
| Cu/Pb 1st CL CONC | 115.8 | 6.04 | 10.755 | 13.399 | 7.897 | 16.661 | 29.839 | 64.971 | 84.571 | 47.709 | 100.650 | 180.261 | 79.94 | 85.26 | 30.58 | 5.88 | 9.36 | | |
| Cu/Pb 1st CL TAIL | 101.8 | 5.31 | 0.100 | 0.180 | 9.200 | 7.360 | 10.710 | 0.531 | 0.955 | 48.817 | 39.054 | 56.830 | 0.65 | 0.96 | 31.23 | 2.28 | 2.95 | | |
| Cu/Pb RO CONC | 217.7 | 11.35 | 5.772 | 7.537 | 8.508 | 12.312 | 20.894 | 65.501 | 85.526 | 98.526 | 139.704 | 237.091 | 80.59 | 86.23 | 61.87 | 8.16 | 12.31 | | |
| Zn CONC | 72.4 | 3.77 | 2.320 | 2.080 | 15.200 | 28.620 | 38.690 | 8.755 | 7.849 | 57.361 | 111.779 | 146.008 | 10.77 | 7.91 | 36.77 | 6.53 | 7.58 | | |
| Zn 2nd CL TAIL | 40.8 | 2.13 | 0.360 | 0.200 | 0.150 | 31.630 | 34.220 | 0.766 | 0.425 | 0.319 | 67.266 | 72.774 | 0.84 | 0.43 | 0.20 | 3.93 | 3.78 | | |
| Zn 1st CL CONC | 113.2 | 5.90 | 1.614 | 1.402 | 9.778 | 30.344 | 37.079 | 9.521 | 8.275 | 57.680 | 179.046 | 218.782 | 11.71 | 8.34 | 36.97 | 10.46 | 11.36 | | |
| Zn 1st CL TAIL | 270.3 | 14.09 | 0.200 | 0.090 | 0.030 | 32.460 | 35.720 | 2.818 | 1.268 | 0.423 | 457.333 | 503.264 | 3.47 | 1.28 | 0.27 | 26.71 | 26.13 | | |
| Zn RO CONC | 383.5 | 19.99 | 0.617 | 0.477 | 2.907 | 31.836 | 36.121 | 12.339 | 9.543 | 58.103 | 636.373 | 722.046 | 15.18 | 9.62 | 37.24 | 37.17 | 37.49 | | |
| TAIL | 1317.3 | 68.66 | 0.050 | 0.060 | 0.020 | 13.630 | 14.080 | 3.433 | 4.120 | 1.373 | 935.877 | 966.775 | 4.22 | 4.15 | 0.88 | 54.87 | 50.20 | | |
| CALC HEAD | 1918.5 | 100.0 | 0.813 | 0.392 | 1.560 | 17.120 | 19.259 | 81.273 | 99.189 | 156.003 | 1711.960 | 1925.912 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | | |

TEST NUMBER: 6891-7F1 FLOTATION OF #3 EXT.

| PRODUCT | WEIGHT | | ASSAYS | | UNITS | | % DIST | |
|-------------------|--------|-------|--------|---------|-------|----------|--------|--------|
| | GMS | % | Au | Ag | Au | Ag | Au | Ag |
| Cu/Pb CONC | 88.1 | 4.59 | 0.228 | 151.077 | 1.047 | 893.765 | 14.42 | 62.78 |
| Cu/Pb 2nd CL TAIL | 27.8 | 1.45 | 0.112 | 12.824 | 0.162 | 18.583 | 2.24 | 1.88 |
| Cu/Pb 1st CL CONC | 115.9 | 6.04 | 0.200 | 117.915 | 1.209 | 712.348 | 16.86 | 64.46 |
| Cu/Pb 1st CL TAIL | 101.8 | 5.31 | 0.029 | 2.541 | 0.154 | 13.483 | 2.12 | 1.22 |
| Cu/Pb RO CONC | 217.7 | 11.35 | 0.120 | 63.984 | 1.363 | 725.831 | 18.78 | 55.68 |
| Zn CONC | 72.4 | 3.77 | 0.288 | 41.484 | 1.079 | 158.552 | 14.87 | 14.17 |
| Zn 2nd CL TAIL | 40.8 | 2.13 | 0.135 | 9.363 | 0.287 | 19.912 | 3.96 | 1.80 |
| Zn 1st CL CONC | 113.2 | 5.90 | 0.232 | 29.907 | 1.368 | 176.463 | 18.82 | 15.97 |
| Zn 1st CL TAIL | 270.3 | 14.08 | 0.148 | 5.410 | 2.057 | 76.222 | 28.34 | 6.90 |
| Zn RO CONC | 383.5 | 19.99 | 0.171 | 12.841 | 3.423 | 252.686 | 47.16 | 22.86 |
| TAIL | 1317.3 | 68.88 | 0.038 | 1.844 | 2.472 | 126.615 | 34.05 | 11.46 |
| CALC HEAD | 1918.5 | 100.0 | 0.073 | 11.051 | 7.258 | 1105.131 | 100.00 | 100.00 |

TESTWORK PROCEDURE

TEST NO.

6891 - 7F2

DATE

No. 3 Ext.

| STAGE | TIME (min.) | ADDITIONS | |
|------------------------|----------------|--------------------------------------|--|
| | | Lb./Ton | REAGENT |
| Grind 55% solids | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ ZnSO ₄ Z-200 pH=6.3 |
| Cu/Pb Rougher | 8 | 0.03 0.05 | AERO 238 MIBC pH=6.2 |
| Zn Condition | 5 5 | 3.75 0.45 0.10 0.02 0.05 | Ca(OH) ₂ to pH=10.5 CuSO ₄ NaCN Z-200 AERO 343 |
| Zn Rougher | 8 | 0.04 | DF 1012 |
| Cu/Pb Cleaning/Regrind | 15 | 2.0 1.0 0.2 | Na ₂ SO ₃ ZnSO ₄ NaCN |
| Cu/Pb 1st Cleaner | 6 | 0.02 | Z-200 |
| Condition | 2 | 1.0 0.1 | Na ₂ SO ₃ NaCN |
| Cu/Pb 2nd Cleaner | 5 | --- | --- |
| Zn Cleaning/regrind | 15 | 0.10 | CuSO ₄ |
| Condition | 5 | 1.08 | Ca(OH) ₂ to pH=10.8 |
| Zn 1st Cleaner | 6 | 0.25 0.20 0.02 0.10 | NaCN CuSO ₄ Z-200 CuSO ₄ |
| Zn 2nd Cleaner | 4 | 1.03 | Ca(OH) ₂ to pH=11.5 |
| Pyrite Float | 9 | 6.5 0.2 | H ₂ SO ₄ to pH=6 AERO 350 |

TEST NUMBER: 6891-7F2 FLOTATION OF #3 EXT. PAGE 2

| PRODUCT | WEIGHT | | WEIGHT | | ASSAYS | | | | UNITS | | | | % DIST | | | | |
|-------------------|--------|-------|--------|--------|--------|--------|--------|--------|--------|---------|----------|----------|--------|-------|-------|-------|-------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | S% | Cu | Pb | Zn | Fe | S | Cu | Pb | Zn | Fe | S |
| Cu/Pb CONC | 38.3 | 1.94 | 20.000 | 30.800 | 4.960 | 6.860 | 24.310 | 38.824 | 59.789 | 9.628 | 13.317 | 47.191 | 45.34 | 58.03 | 5.87 | 0.82 | 2.47 |
| Cu/Pb 2nd CL TAIL | 42.1 | 2.13 | 10.240 | 12.880 | 7.440 | 14.480 | 26.810 | 21.850 | 27.483 | 15.876 | 30.855 | 57.207 | 25.52 | 26.68 | 9.87 | 1.90 | 2.99 |
| Cu/Pb 1st CL CONC | 80.4 | 4.08 | 14.883 | 21.417 | 6.259 | 10.840 | 25.619 | 60.674 | 87.273 | 25.504 | 44.172 | 104.398 | 70.86 | 84.71 | 15.54 | 2.72 | 5.46 |
| Cu/Pb 1st CL TAIL | 187.7 | 9.51 | 1.100 | 0.320 | 8.840 | 19.880 | 26.190 | 10.465 | 3.044 | 82.196 | 189.127 | 249.157 | 12.22 | 2.95 | 50.08 | 11.67 | 13.04 |
| Cu/Pb RO CONC | 268.1 | 13.58 | 5.235 | 6.647 | 7.926 | 17.169 | 26.019 | 71.139 | 90.317 | 107.700 | 233.299 | 353.555 | 83.08 | 87.66 | 65.61 | 14.39 | 18.50 |
| Zn CONC | 40.8 | 2.06 | 2.500 | 1.380 | 25.600 | 21.770 | 36.820 | 5.144 | 2.840 | 52.873 | 44.798 | 75.787 | 8.01 | 2.76 | 32.09 | 2.76 | 3.97 |
| Zn 2nd CL TAIL | 25.5 | 1.23 | 0.460 | 0.320 | 0.250 | 30.580 | 34.020 | 0.595 | 0.414 | 0.323 | 39.523 | 43.969 | 0.69 | 0.40 | 0.20 | 2.44 | 2.30 |
| Zn 1st CL CONC | 66.1 | 3.35 | 1.713 | 0.971 | 15.820 | 25.169 | 35.740 | 5.739 | 3.253 | 53.002 | 84.321 | 119.737 | 8.70 | 3.16 | 32.29 | 5.20 | 6.27 |
| Zn 1st CL TAIL | 540.3 | 27.38 | 0.220 | 0.130 | 0.050 | 38.950 | 43.790 | 6.025 | 3.560 | 1.369 | 1066.634 | 1195.176 | 7.04 | 3.46 | 0.83 | 65.80 | 62.76 |
| Zn RO CONC | 606.4 | 30.73 | 0.383 | 0.222 | 1.763 | 37.448 | 42.912 | 11.764 | 8.813 | 54.372 | 1150.955 | 1318.912 | 13.74 | 8.61 | 33.12 | 71.00 | 63.02 |
| PYRITE CONC | 158.8 | 8.05 | 0.220 | 0.200 | 0.080 | 21.710 | 23.560 | 1.772 | 1.611 | 0.644 | 174.846 | 189.746 | 2.07 | 1.56 | 0.39 | 10.79 | 9.93 |
| TAIL | 939.8 | 47.62 | 0.020 | 0.030 | 0.030 | 1.300 | 1.020 | 0.952 | 4.286 | 1.429 | 61.910 | 48.575 | 1.11 | 4.16 | 0.87 | 3.82 | 2.54 |
| CALC HEAD | 1973.0 | 100.0 | 0.856 | 1.030 | 1.841 | 18.210 | 19.108 | 85.6 | 103.0 | 164.1 | 1621.0 | 1910.8 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 |

TEST NUMBER: 6881-7F2 FLOTATION OF #3 EXT. PAGE 1

| PRODUCT | WEIGHT | | WEIGHT | | ASSAYS | | UNITS | | % DIST | |
|-------------------|--------|-------|--------|---------|--------|----|-------|---------|--------|-------|
| | GMS | % | oz/ton | oz/ton | Au | Ag | Au | Ag | Au | Ag |
| Cu/Pb CONC | 38.3 | 1.34 | 0.289 | 256.335 | | | 0.581 | 498.764 | 9.39 | 45.65 |
| Cu/Pb 2nd CL TAIL | 42.1 | 2.13 | 0.119 | 102.098 | | | 0.254 | 217.853 | 4.25 | 19.94 |
| Cu/Pb 1st CL CONC | 80.4 | 4.08 | 0.200 | 175.858 | | | 0.815 | 716.617 | 13.64 | 65.59 |
| Cu/Pb 1st CL TAIL | 187.7 | 9.51 | 0.072 | 10.817 | | | 0.685 | 102.907 | 11.47 | 9.42 |
| Cu/Pb RO CONC | 268.1 | 13.58 | 0.110 | 60.310 | | | 1.500 | 819.524 | 25.11 | 75.01 |
| Zn CONC | 40.8 | 2.06 | 0.191 | 38.533 | | | 0.393 | 79.292 | 6.58 | 7.26 |
| Zn 2nd CL TAIL | 25.5 | 1.29 | 0.148 | 10.034 | | | 0.191 | 12.968 | 3.20 | 1.19 |
| Zn 1st CL CONC | 68.1 | 3.35 | 0.174 | 27.539 | | | 0.584 | 92.261 | 9.78 | 8.44 |
| Zn 1st CL TAIL | 540.3 | 27.38 | 0.109 | 4.407 | | | 2.985 | 120.684 | 49.96 | 11.05 |
| Zn RO CONC | 606.4 | 30.73 | 0.118 | 6.928 | | | 3.569 | 212.945 | 59.74 | 19.49 |
| PYRITE CONC | 158.9 | 8.05 | 0.071 | 4.878 | | | 0.572 | 39.270 | 9.57 | 3.59 |
| TAIL | 939.6 | 47.62 | 0.007 | 0.436 | | | 0.333 | 20.764 | 5.58 | 1.90 |
| CALC HEAD | 1973.0 | 100.0 | 0.060 | 10.925 | | | 8.0 | 1092.5 | 100.0 | 100.0 |

TESTWORK PROCEDURE

Test No. 6891-8F1
Switchback Vein

| STAGE | TIME (min) | ADDITIONS | |
|----------------------------|---------------|--------------------------------------|--|
| | | lb/ton | REAGENT |
| GRIND | 11.5 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ pH = 6.6 ZnSO ₄ Z-200 |
| CU/PB ROUGHER | 7 | 0.03 0.050 | Aero 238 pH = 6.8 MIBC |
| ZN CONDITION | 5 5 | 7.88 0.45 0.10 0.02 0.05 | Ca(OH) ₂ to pH = 10.5 CuSO ₄ NaCN Z-200 Aero 343 |
| ZN ROUGHER | 8 | 0.04 | DF1012 |
| CU/PB CLEANING/ REGRIND | 15 | 1.5 1.0 | Na ₂ SO ₃ ZnSO ₄ |
| CU/PB 1ST CLEANER | 9 | 0.02 | Z-200 |
| CU/PB 2ND CLEANER | 5 | | |
| ZN CLEANING/ REGRIND | 15 | 0.10 | CuSO ₄ |
| CONDITION | 5 | 2.51 | Ca(OH) ₂ to pH = 10.8 |
| ZN 1ST CLEANER | 6 | 0.25 0.20 0.02 0.05 0.10 | NaCN CuSO ₄ Z-200 Aero 343 CuSO ₄ |
| Zn 2ND CLEANER | 5 | | |

TEST NUMBER: 6891-8F1 FLOTATION OF SWITCHBACK VEIN PAGE 2

| PRODUCT | WEIGHT GMS | | WEIGHT % | | ASSAYS | | | | UNITS | | | | % DIST | | | | |
|-------------------|------------|-------|----------|--------|--------|--------|--------|--------|---------|----------|----------|----------|--------|--------|--------|--------|--------|
| | Cu% | Pb% | Zn% | Fe% | S% | Cu | Pb | Zn | Fe | S | Cu | Pb | Zn | Fe | S | | |
| Cu/Pb CONC | 59.8 | 3.15 | 1.100 | 60.000 | 10.800 | 7.070 | 21.010 | 3.464 | 188.959 | 34.013 | 22.266 | 68.167 | 32.66 | 46.22 | 3.06 | 2.02 | 4.03 |
| Cu/Pb 2nd CL TAIL | 34.6 | 1.82 | 0.270 | 35.600 | 24.400 | 7.870 | 24.410 | 0.491 | 64.761 | 44.387 | 14.317 | 44.405 | 4.63 | 15.84 | 3.99 | 1.30 | 2.70 |
| Cu/Pb 1st CL CONC | 54.5 | 4.87 | 0.796 | 51.066 | 15.779 | 7.363 | 22.255 | 3.955 | 253.720 | 78.400 | 38.582 | 110.572 | 37.29 | 62.06 | 7.04 | 3.31 | 6.74 |
| Cu/Pb 1st CL TAIL | 174.3 | 9.16 | 0.180 | 10.800 | 38.800 | 7.890 | 28.650 | 1.466 | 98.972 | 355.565 | 72.304 | 262.550 | 13.82 | 24.21 | 31.95 | 6.55 | 15.99 |
| Cu/Pb RO CONC | 268.8 | 14.13 | 0.384 | 24.956 | 30.707 | 7.705 | 26.402 | 5.422 | 352.692 | 433.964 | 108.887 | 373.122 | 51.11 | 86.27 | 38.99 | 9.86 | 22.73 |
| Zn CONC | 229.1 | 12.05 | 0.180 | 1.360 | 52.000 | 8.470 | 31.680 | 2.168 | 23.609 | 626.351 | 77.933 | 381.592 | 20.44 | 5.77 | 56.27 | 7.06 | 23.24 |
| Zn 2nd CL TAIL | 21.0 | 1.10 | 0.230 | 1.280 | 14.800 | 18.010 | 21.920 | 0.254 | 1.413 | 16.341 | 17.877 | 24.202 | 2.39 | 0.35 | 1.47 | 1.60 | 1.47 |
| Zn 1st CL CONC | 250.1 | 13.15 | 0.184 | 1.903 | 48.876 | 7.271 | 30.880 | 2.422 | 25.022 | 642.692 | 95.609 | 405.794 | 22.83 | 6.12 | 57.74 | 8.66 | 24.72 |
| Zn 1st CL TAIL | 100.6 | 5.29 | 0.140 | 0.530 | 2.160 | 17.360 | 18.180 | 0.740 | 2.803 | 11.425 | 91.820 | 96.157 | 6.98 | 0.69 | 1.03 | 8.32 | 5.86 |
| Zn RO CONC | 350.7 | 18.44 | 0.172 | 1.508 | 35.478 | 10.165 | 27.223 | 3.183 | 27.825 | 854.117 | 187.429 | 501.951 | 29.82 | 6.81 | 58.77 | 16.98 | 30.57 |
| TAIL | 1282.5 | 67.43 | 0.030 | 0.420 | 0.370 | 11.980 | 11.370 | 2.023 | 28.320 | 24.948 | 807.800 | 786.668 | 19.07 | 6.93 | 2.24 | 73.16 | 46.70 |
| CALC HEAD | 1802.0 | 100.0 | 0.108 | 4.088 | 11.130 | 11.041 | 16.417 | 10.607 | 408.837 | 1113.028 | 1104.115 | 1841.741 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 8891-6F1 FLOTATION OF SWITCHBACK VEIN

| PRODUCT | WEIGHT | | ASSAYS | | UNITS | | % DIST | |
|-------------------|--------|-------|--------|--------|--------|---------|--------|--------|
| | GMS | % | Au | Ag | Au | Ag | Au | Ag |
| Cu/Pb CONC | 59.9 | 3.15 | 0.468 | 14.141 | 1.474 | 44.534 | 13.94 | 23.71 |
| Cu/Pb 2nd CL TAIL | 34.6 | 1.82 | 0.106 | 6.452 | 0.193 | 11.737 | 1.82 | 6.25 |
| Cu/Pb 1st CL CONC | 94.5 | 4.97 | 0.335 | 11.328 | 1.867 | 56.272 | 15.77 | 29.96 |
| Cu/Pb 1st CL TAIL | 174.3 | 9.16 | 0.093 | 3.384 | 0.852 | 30.828 | 8.06 | 16.41 |
| Cu/Pb RO CONC | 268.8 | 14.13 | 0.178 | 6.163 | 2.518 | 87.099 | 23.83 | 46.37 |
| Zn CONC | 229.1 | 12.05 | 0.069 | 2.908 | 1.072 | 35.040 | 10.14 | 18.65 |
| Zn 2nd CL TAIL | 21.0 | 1.10 | 0.162 | 2.628 | 0.179 | 2.802 | 1.69 | 1.54 |
| Zn 1st CL CONC | 250.1 | 13.15 | 0.095 | 2.885 | 1.251 | 37.941 | 11.83 | 20.20 |
| Zn 1st CL TAIL | 100.6 | 5.29 | 0.151 | 1.342 | 0.799 | 7.098 | 7.56 | 3.78 |
| Zn RO CONC | 350.7 | 18.44 | 0.111 | 2.443 | 2.050 | 45.039 | 19.39 | 23.98 |
| TAIL | 1282.5 | 67.43 | 0.089 | 0.828 | 6.001 | 55.696 | 56.76 | 29.65 |
| CALC HEAD | 1902.0 | 100.0 | 0.106 | 1.878 | 10.570 | 187.835 | 100.00 | 100.00 |

TESTWORK PROCEDURE

Test No. 6891-8E2

Switchback Vein

| STAGE | TIME (min) | ADDITIONS | |
|----------------------|---------------|-------------------------|---|
| | | lb/ton | REAGENT |
| ZN RECLEANER | 5 | 0.45 | Lime to pH = 11.5 |
| CU/PB SEPN CONDITION | 20 | 0.11 0.11 | Dextrin Carbon |
| CONDITION | 20 | 50 ml | 6% sulphurous acid to pH = 4.8 (pH = 1.2) |
| SCREEN OUT CARBON | | | |
| COPPER FLOAT | 5 | 0.02 | Z-200 |
| CONDITION | 15 | 0.55 0.11 | Dextrin Carbon |
| CONDITION | 5 | 50 ml | 6% sulphurous acid |
| SCREEN OUT CARBON | Pb | floated so didn't float | |

TESTWORK PROCEDURE

Test No. 6891-8F2

Switchback Vein

| STAGE | TIME (min) | ADDITIONS | |
|-----------------------------|---------------|-------------------------------------|--|
| | | lb/ton | REAGENT |
| GRIND | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ pH = 6.9 ZnSO ₄ Z-200 |
| CU/PB ROUGHER | 10 | 0.03 0.05 | Aero 238 pH = 6.4 MIBC |
| ZN CONDITION | 5 5 | 5.46 0.6 0.1 0.03 0.075 | Lime to pH = 10.5 CuSO ₄ NaCN Z-200 Aero 343 |
| ZN ROUGHER | 8 | 0.040 | DF1012 |
| PYRITE FLOAT | 9 | 2 ml 0.2 0.06 | H ₂ SO ₄ to pH = 6 Aero 350 DF1012 |
| CU/PB CLEANING CONDITION | 5 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| CU/PB CLEANER | 10 | | |
| CU/PB RECLEANER | 7 | 1.0 | Na ₂ SO ₃ |
| ZN CLEANING CONDITION | 5 | 0.51 | Lime to pH = 10.8 |
| ZN CLEANER | 8 | 0.2 0.03 0.20 0.02 | NaCN Z-200 CuSO ₄ Aero 343 |

TEST NUMBER: 6891-8F2 FLOTATION OF SWITCHBACK VEIN- Cu/Pb SEPARATION PAGE 2

| PRODUCT | WEIGHT | | ASSAYS | | | | UNITS | | | | % DIST | | | |
|-------------------|---------|-------|--------|--------|--------|--------|-------|---------|----------|---------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| SEP. CONC | 139.3 | 3.56 | 0.450 | 58.820 | 4.730 | 8.230 | 1.803 | 208.845 | 18.852 | 29.535 | 17.22 | 56.14 | 1.52 | 3.00 |
| SEP. TAIL | 6.5 | 0.17 | 0.140 | 10.360 | 14.340 | 7.180 | 0.023 | 1.722 | 2.384 | 1.194 | 0.25 | 0.46 | 0.22 | 0.12 |
| Cu/Pb CONC | 145.8 | 3.73 | 0.436 | 56.468 | 5.158 | 8.241 | 1.626 | 210.568 | 19.235 | 30.728 | 17.47 | 56.61 | 1.74 | 3.12 |
| Cu/Pb 2nd CL TAIL | 90.6 | 2.32 | 0.490 | 9.380 | 14.780 | 16.580 | 1.135 | 21.735 | 34.248 | 38.419 | 12.20 | 5.84 | 3.10 | 3.90 |
| Cu/Pb 1st CL CONC | 236.4 | 6.05 | 0.457 | 38.422 | 8.846 | 11.437 | 2.782 | 232.302 | 53.483 | 69.147 | 29.87 | 62.45 | 4.84 | 7.02 |
| Cu/Pb 1st CL TAIL | 380.7 | 9.74 | 0.150 | 2.140 | 14.510 | 23.920 | 1.481 | 20.836 | 141.279 | 232.901 | 15.69 | 5.80 | 12.78 | 23.63 |
| Cu/Pb RO CONC | 617.1 | 15.78 | 0.288 | 18.039 | 12.340 | 19.138 | 4.222 | 253.138 | 194.762 | 302.048 | 45.37 | 68.05 | 17.82 | 30.65 |
| Zn CONC | 852.0 | 16.68 | 0.140 | 4.000 | 48.750 | 5.280 | 2.335 | 66.701 | 812.924 | 88.046 | 25.08 | 17.93 | 73.55 | 8.93 |
| Zn 2nd CL TAIL | 46.9 | 1.20 | 0.160 | 1.880 | 15.130 | 13.460 | 0.192 | 2.015 | 18.148 | 16.145 | 2.06 | 0.54 | 1.64 | 1.64 |
| Zn 1st CL CONC | 698.3 | 17.87 | 0.141 | 3.844 | 48.494 | 5.829 | 2.526 | 66.717 | 831.072 | 104.181 | 27.14 | 18.47 | 75.19 | 10.57 |
| Zn 1st CL TAIL | 332.9 | 8.51 | 0.080 | 1.050 | 5.480 | 23.120 | 0.681 | 8.940 | 46.658 | 196.847 | 7.32 | 2.40 | 4.22 | 19.98 |
| Zn RO CONC | 1031.8 | 26.33 | 0.122 | 2.343 | 33.261 | 11.408 | 3.208 | 77.656 | 877.730 | 301.038 | 34.46 | 20.88 | 79.41 | 30.55 |
| PYRITE CONC | 563.8 | 14.42 | 0.070 | 1.140 | 1.310 | 18.540 | 1.009 | 16.438 | 18.890 | 267.339 | 10.84 | 4.42 | 1.71 | 27.13 |
| TAIL | 1697.26 | 43.41 | 0.020 | 0.570 | 0.320 | 2.850 | 0.868 | 24.743 | 13.891 | 115.033 | 9.33 | 6.65 | 1.26 | 11.67 |
| CALC HEAD | 3910.0 | 100.0 | 0.093 | 3.720 | 11.053 | 9.855 | 9.308 | 371.977 | 1105.273 | 365.458 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6881-8F2 FLOTATION OF SWITCHBACK VEIN- Cu/Pb SEPARATION PAGE 1

| PRODUCT | WEIGHT | WEIGHT | Au | Ag | ASSAYS | | UNITS | AU | Ag | % DIST | |
|-------------------|---------|--------|--------|--------|--------|--|--------|---------|----|--------|--------|
| | GMS | % | oz/ton | oz/ton | | | | | | | |
| SEP. CONC | 139.3 | 3.56 | 0.386 | 11.860 | | | 1.375 | 41.541 | | 12.97 | 21.80 |
| SEP. TAIL | 6.5 | 0.17 | 0.245 | 5.314 | | | 0.041 | 0.883 | | 0.38 | 0.46 |
| Cu/Pb CONC | 145.8 | 3.73 | 0.380 | 11.377 | | | 1.416 | 42.424 | | 13.35 | 22.27 |
| Cu/Pb 2nd CL TAIL | 80.6 | 2.32 | 0.162 | 5.044 | | | 0.375 | 11.688 | | 3.54 | 6.13 |
| Cu/Pb 1st CL CONC | 236.4 | 6.05 | 0.298 | 8.950 | | | 1.791 | 54.112 | | 16.89 | 28.40 |
| Cu/Pb 1st CL TAIL | 380.7 | 9.74 | 0.208 | 2.820 | | | 2.006 | 25.510 | | 18.91 | 13.39 |
| Cu/Pb RD CONC | 817.1 | 15.78 | 0.241 | 5.045 | | | 3.797 | 79.622 | | 35.80 | 41.79 |
| Zn CONC | 652.0 | 16.68 | 0.090 | 2.888 | | | 1.501 | 48.125 | | 14.15 | 25.26 |
| Zn 2nd CL TAIL | 48.9 | 1.20 | 0.146 | 3.156 | | | 0.175 | 3.786 | | 1.65 | 1.59 |
| Zn 1st CL CONC | 698.9 | 17.87 | 0.094 | 2.904 | | | 1.676 | 51.911 | | 15.80 | 27.24 |
| Zn 1st CL TAIL | 332.3 | 8.51 | 0.196 | 2.136 | | | 1.663 | 18.186 | | 15.74 | 9.54 |
| Zn RD CONC | 1031.8 | 26.39 | 0.127 | 2.858 | | | 3.345 | 70.097 | | 31.54 | 36.79 |
| PYRITE CONC | 583.8 | 14.42 | 0.180 | 1.958 | | | 2.596 | 28.234 | | 24.47 | 14.82 |
| TAIL | 1897.26 | 43.41 | 0.020 | 0.290 | | | 0.868 | 12.589 | | 8.19 | 6.61 |
| CALC HEAD | 3910.0 | 100.0 | 0.106 | 1.905 | | | 10.605 | 190.541 | | 100.00 | 100.00 |

TESTWORK PROCEDURE

Test No. 6891-9F1
M-3 Vein

| STAGE | TIME (min) | ADDITIONS | |
|----------------------------|---------------|---------------------------------------|--|
| | | 1 b/ton | REAGENT |
| GRIND | 10 | 0.25 1.0 0.5 0.02 | NaCn Na ₂ SO ₃ pH = 6.3 ZnSO ₄ Z-200 |
| CU/PB ROUGHER | 7 | 0.03 0.050 | Aero 238 pH = 6.4 MIBC |
| ZN CONDITION | 5 5 | 12.13 0.45 0.10 0.02 0.05 | Ca(OH) ₂ to pH = 10.5 CuSO ₄ NaCN Z-200 Aero 343 |
| ZN ROUGHER | 8 | 0.04 | DF1012 |
| CU/PB CLEANING/ REGRIND | 15 | 1.5 1.0 | Na ₂ SO ₃ ZNSO ₄ |
| CU/PB 1ST CLEANER | 7 | 0.02 | Z-200 |
| CU/PB 2ND CLEANER | 6 | | |
| ZN CLEANING/ REGRIND | 15 | 0.10 | CUSO ₄ |
| CONDITION | 5 | 1.78 | Ca(OH) ₂ to pH = 10.8 |
| ZN 1ST CLEANER | 9 | 0.25 0.20 0.02 0.05 0.10 | NaCN CuSO ₄ Z-200 Aero 343 CuSO ₄ |
| Zn 2ND CLEANER | 7 | | |

TEST NUMBER: 8881-9F1 FLOTATION OF M-3 VEIN PAGE 2

| PRODUCT | WEIGHT | | WEIGHT | | ASSAYS | | | | UNITS | | | | % DIST | | | | |
|-------------------|--------|-------|--------|--------|--------|--------|--------|--------|--------|----------|----------|----------|--------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | S% | Cu | Pb | Zn | Fe | S | Cu | Pb | Zn | Fe | S |
| Cu/Pb CONC | 111.3 | 5.83 | 8.840 | 13.200 | 10.400 | 24.400 | 38.160 | 50.405 | 77.008 | 60.673 | 142.348 | 222.623 | 78.74 | 79.85 | 2.32 | 11.25 | 8.53 |
| Cu/Pb 2nd CL TAIL | 28.1 | 1.47 | 0.360 | 0.760 | 36.000 | 19.440 | 38.330 | 0.530 | 1.119 | 53.024 | 28.633 | 56.456 | 0.83 | 1.16 | 2.03 | 2.26 | 2.16 |
| Cu/Pb 1st CL CONC | 139.4 | 7.31 | 8.971 | 10.892 | 15.560 | 23.400 | 38.194 | 50.938 | 78.127 | 113.697 | 170.981 | 279.080 | 79.56 | 80.81 | 4.35 | 13.52 | 10.70 |
| Cu/Pb 1st CL TAIL | 168.6 | 8.84 | 0.180 | 0.300 | 50.000 | 8.100 | 31.820 | 1.591 | 2.651 | 441.870 | 71.583 | 281.206 | 2.48 | 2.74 | 16.92 | 5.66 | 10.78 |
| Cu/Pb RO CONC | 308.0 | 16.14 | 3.254 | 5.004 | 34.413 | 15.025 | 34.705 | 52.528 | 80.779 | 555.568 | 242.584 | 580.286 | 82.05 | 83.55 | 21.28 | 19.18 | 21.47 |
| Zn CONC | 613.5 | 32.18 | 0.180 | 0.230 | 62.000 | 2.240 | 32.020 | 5.788 | 7.338 | 1993.762 | 72.033 | 1029.682 | 9.04 | 7.65 | 76.38 | 5.69 | 39.47 |
| Zn 2nd CL TAIL | 23.8 | 1.25 | 0.260 | 0.240 | 12.400 | 17.060 | 23.310 | 0.324 | 0.299 | 15.469 | 21.263 | 29.079 | 0.51 | 0.31 | 0.59 | 1.68 | 1.11 |
| Zn 1st CL CONC | 637.3 | 33.40 | 0.183 | 0.230 | 60.148 | 2.793 | 31.685 | 8.113 | 7.636 | 2009.232 | 93.315 | 1058.761 | 9.55 | 7.96 | 76.95 | 7.38 | 40.58 |
| Zn 1st CL TAIL | 63.7 | 3.34 | 0.200 | 0.200 | 2.560 | 18.180 | 19.670 | 0.668 | 0.668 | 8.548 | 60.702 | 65.677 | 1.04 | 0.69 | 0.33 | 4.80 | 2.52 |
| Zn RO CONC | 701.0 | 38.74 | 0.185 | 0.228 | 54.915 | 4.192 | 30.802 | 8.780 | 8.363 | 2017.779 | 154.017 | 1124.438 | 10.59 | 8.65 | 77.28 | 12.18 | 43.10 |
| TAIL | 898.8 | 47.11 | 0.100 | 0.160 | 0.800 | 18.430 | 19.620 | 4.711 | 7.538 | 37.689 | 868.272 | 924.335 | 7.38 | 7.80 | 1.44 | 68.65 | 35.43 |
| CALC HEAD | 1907.8 | 100.0 | 0.840 | 0.967 | 28.110 | 12.849 | 26.091 | 64.018 | 96.880 | 2611.038 | 1264.853 | 2609.058 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6891-8F1 FLOTATION OF M-3 VEIN

| PRODUCT | WEIGHT | | ASSAYS | | UNITS | | % DIST | |
|-------------------|--------|-------|--------|--------|--------|----------|--------|--------|
| | GMS | % | Au | Ag | Au | Ag | Au | Ag |
| Cu/Pb CONC | 111.3 | 5.83 | 0.205 | 87.515 | 1.196 | 510.558 | 7.70 | 20.37 |
| Cu/Pb 2nd CL TAIL | 28.1 | 1.47 | 0.234 | 37.352 | 0.345 | 55.016 | 2.22 | 2.20 |
| Cu/Pb 1st CL CONC | 139.4 | 7.31 | 0.211 | 77.403 | 1.541 | 565.573 | 9.91 | 22.57 |
| Cu/Pb 1st CL TAIL | 168.6 | 8.84 | 0.183 | 29.414 | 1.617 | 258.943 | 10.41 | 10.37 |
| Cu/Pb RO CONC | 308.0 | 16.14 | 0.196 | 51.134 | 3.158 | 825.517 | 20.32 | 32.94 |
| Zn CONC | 613.5 | 32.16 | 0.188 | 45.054 | 8.046 | 1448.822 | 38.91 | 57.82 |
| Zn 2nd CL TAIL | 23.8 | 1.25 | 0.172 | 10.170 | 0.215 | 12.887 | 1.38 | 0.51 |
| Zn 1st CL CONC | 637.3 | 33.40 | 0.187 | 43.751 | 8.280 | 1461.509 | 40.29 | 58.32 |
| Zn 1st CL TAIL | 63.7 | 3.34 | 0.154 | 5.318 | 0.514 | 17.756 | 3.31 | 0.71 |
| Zn RO CONC | 701.0 | 36.74 | 0.184 | 40.259 | 8.774 | 1479.266 | 43.60 | 59.03 |
| TAIL | 898.8 | 47.11 | 0.119 | 4.289 | 5.806 | 201.121 | 36.08 | 8.03 |
| CALC HEAD | 1907.8 | 100.0 | 0.155 | 25.059 | 15.539 | 2505.903 | 100.00 | 100.00 |

TESTWORK PROCEDURE

TEST NO.

6891 - 10F1

DATE

Composite #2

| STAGE | TIME (min.) | ADDITIONS | |
|------------------------|----------------|--------------------------------------|--|
| | | Lb./Ton | REAGENT |
| Grind | 11 | 0.25 1.0 0.5 0.02 | NaCn Na ₂ SO ₃ ZnSO ₄ Z-200 pH=6.5 |
| Cu/Pb Rougher | 8 | 0.03 0.05 | AERO 238 pH=6.7 MIBC |
| Zn Condition | 5 5 | 8.52 0.45 0.10 0.02 0.05 | Ca(OH) ₂ to pH=10.5 CuSO ₄ NaCN Z-200 AERO 343 |
| Zn Rougher | 8 | 0.04 | DF 1012 |
| Cu/Pb Cleaning/Regrind | 15 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| Cu/Pb 1st Cleaner | 7 | --- | --- |
| Condition | 2 | 1.0 | Na ₂ SO ₃ |
| Cu/Pb 2nd Cleaner | 6 | --- | --- |
| Zn Regrind | 15 | 0.1 | CuSO ₄ |
| Condition | 5 | 0.40 | Ca(OH) ₂ to pH=10.8 |
| Zn 1st Cleaner | 9 | 0.25 0.20 0.02 0.10 | NaCN CuSO ₄ Z-200 CuSO ₄ |
| Zn 2nd Cleaner | 5 | 0.91 | Ca(OH) ₂ to pH=11.5 |

TEST NUMBER: 6891-10F1 FLOTATION OF COMPOSITE ORE #2 PAGE 2

| PRODUCT | WEIGHT | | WEIGHT | | ASSAYS | | | | UNITS | | | | % DIST | | | | |
|-------------------|--------|-------|--------|--------|--------|--------|--------|---------|---------|---------|----------|----------|--------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | S% | Cu | Pb | Zn | Fe | S | Cu | Pb | Zn | Fe | S |
| Cu/Pb CONC | 102.7 | 5.36 | 17.600 | 32.800 | 8.160 | 8.300 | 31.110 | 94.328 | 175.794 | 43.734 | 44.484 | 166.736 | 78.58 | 89.07 | 5.13 | 3.32 | 9.11 |
| Cu/Pb 2nd CL TAIL | 25.3 | 1.32 | 6.720 | 3.800 | 19.200 | 13.000 | 25.810 | 8.873 | 4.753 | 25.350 | 17.270 | 34.077 | 7.39 | 2.41 | 2.97 | 1.29 | 1.86 |
| Cu/Pb 1st CL CONC | 128.0 | 6.68 | 15.450 | 27.028 | 10.342 | 9.245 | 30.062 | 103.201 | 180.547 | 69.084 | 61.754 | 200.814 | 85.97 | 91.48 | 8.10 | 4.61 | 10.98 |
| Cu/Pb 1st CL TAIL | 129.8 | 6.77 | 0.390 | 0.210 | 16.000 | 14.570 | 10.710 | 2.642 | 1.423 | 108.381 | 98.695 | 72.548 | 2.20 | 0.72 | 12.70 | 7.37 | 3.97 |
| Cu/Pb RO CONC | 257.8 | 13.45 | 7.867 | 13.526 | 13.191 | 11.928 | 20.318 | 105.843 | 181.969 | 177.485 | 160.449 | 273.361 | 88.17 | 92.20 | 20.80 | 11.98 | 14.94 |
| Zn CONC | 69.3 | 3.62 | 1.580 | 1.160 | 52.800 | 9.030 | 38.690 | 5.714 | 4.195 | 190.953 | 32.657 | 139.924 | 4.76 | 2.13 | 22.38 | 2.44 | 7.65 |
| Zn 2nd CL TAIL | 106.8 | 5.56 | 0.300 | 0.170 | 58.400 | 4.410 | 34.220 | 1.669 | 0.946 | 324.885 | 24.533 | 190.369 | 1.39 | 0.48 | 38.08 | 1.83 | 10.40 |
| Zn 1st CL CONC | 175.9 | 9.18 | 0.804 | 0.560 | 58.194 | 8.230 | 35.981 | 7.383 | 5.141 | 515.838 | 57.191 | 330.293 | 6.15 | 2.60 | 60.47 | 4.27 | 18.05 |
| Zn 1st CL TAIL | 121.0 | 6.31 | 0.180 | 0.160 | 22.600 | 14.320 | 35.720 | 1.137 | 1.010 | 142.710 | 90.425 | 225.557 | 0.95 | 0.51 | 16.73 | 6.75 | 12.33 |
| Zn RO CONC | 296.9 | 15.49 | 0.550 | 0.397 | 42.503 | 9.527 | 35.875 | 8.520 | 8.151 | 658.547 | 147.615 | 555.850 | 7.10 | 3.12 | 77.20 | 11.02 | 30.38 |
| TAIL | 1361.5 | 71.05 | 0.080 | 0.130 | 0.240 | 14.520 | 14.080 | 5.684 | 9.237 | 17.052 | 1031.676 | 1000.413 | 4.73 | 4.68 | 2.00 | 77.01 | 54.68 |
| CALC HEAD | 1918.2 | 100.0 | 1.200 | 1.974 | 8.531 | 13.397 | 18.296 | 120.047 | 197.357 | 853.065 | 1339.740 | 1829.624 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 8891-10F1 FLOTATION OF ORE COMPOSITE #2 PAGE 1

| PRODUCT | WEIGHT | | ASSAYS | | UNITS | | % DIST | |
|-------------------|--------|-------|--------|---------|-------|----------|--------|--------|
| | GMS | % | Au | Ag | Au | Ag | Au | Ag |
| Cu/Pb CONC | 102.7 | 5.36 | 0.412 | 202.778 | 2.208 | 1086.791 | 30.94 | 73.11 |
| Cu/Pb 2nd CL TAIL | 25.3 | 1.32 | 0.116 | 53.202 | 0.153 | 70.244 | 2.15 | 4.73 |
| Cu/Pb 1st CL CONC | 128.0 | 6.68 | 0.353 | 173.212 | 2.381 | 1157.035 | 33.09 | 77.83 |
| Cu/Pb 1st CL TAIL | 129.8 | 6.77 | 0.066 | 5.647 | 0.447 | 38.252 | 6.26 | 2.57 |
| Cu/Pb RO CONC | 257.8 | 13.45 | 0.203 | 88.844 | 2.808 | 1195.287 | 39.35 | 80.40 |
| Zn CONC | 69.3 | 3.62 | 0.118 | 22.762 | 0.430 | 82.320 | 6.03 | 5.54 |
| Zn 2nd CL TAIL | 106.6 | 5.56 | 0.039 | 4.832 | 0.217 | 25.768 | 3.04 | 1.73 |
| Zn 1st CL CONC | 175.9 | 9.18 | 0.071 | 11.775 | 0.647 | 108.088 | 9.07 | 7.27 |
| Zn 1st CL TAIL | 121.0 | 6.31 | 0.054 | 3.856 | 0.341 | 24.349 | 4.78 | 1.64 |
| Zn RO CONC | 298.9 | 15.49 | 0.064 | 8.548 | 0.988 | 132.437 | 13.85 | 8.91 |
| TAIL | 1361.5 | 71.05 | 0.047 | 2.236 | 3.339 | 158.872 | 46.80 | 10.69 |
| CALC HEAD | 1916.2 | 100.0 | 0.071 | 14.886 | 7.136 | 1488.598 | 100.00 | 100.00 |

TESTWORK PROCEDURE

TEST NO.

6891 - 10F2

DATE

Composite #2

| STAGE | TIME (min.) | ADDITIONS | |
|---------------------|----------------|---------------------------------------|--|
| | | Lb./Ton | REAGENT |
| Grind | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ , ZnSO ₄ Z-200 pH=6.4 |
| Cu/Pb Rougher | 10 | 0.03 0.05 | AERO 238 MIBC pH=6.2 |
| Zn Condition | 5 5 | 6.08 0.60 0.10 0.03 0.075 | Ca(OH) ₂ to pH=10.5 CuSO ₄ NaCN Z-200 AERO 343 |
| Zn Rougher | 8 | 0.04 | DF 1012 |
| Zn Cleaning/Regrind | 15 | 0.10 | CuSO ₄ |
| Condition | 5 | 0.59 | Ca(OH) ₂ to pH=10.8 |
| Zn 1st Cleaner | 3 | 0.25 0.02 0.20 0.02 | NaCN Z-200 CuSO ₄ AERO 343 |
| Zn 2nd Cleaner | 4 | 0.59 | Ca(OH) ₂ to pH=11.5 |

TEST NUMBER: 6891-10F2 FLOTATION OF COMPOSITE ORE #2 PAGE 2

| PRODUCT | WEIGHT | | ASSAYS | | | | UNITS | | | | | % DIST | | | | | |
|----------------|--------|----------|--------|--------|--------|--------|--------|---------|---------|---------|---------|---------|--------|-------|-------|-------|-------|
| | GMS | WEIGHT % | Cu% | Pb% | Zn% | Fe% | S% | Cu | Pb | Zn | Fe | S | Cu | Pb | Zn | Fe | S |
| Cu/Pb RO CONC | 294.4 | 15.08 | 6.960 | 12.320 | 11.800 | 15.690 | 26.230 | 104.981 | 185.829 | 177.985 | 236.660 | 395.641 | 89.03 | 92.85 | 21.43 | 17.60 | 23.67 |
| Zn CONC | 202.4 | 10.37 | 0.620 | 0.390 | 59.200 | 4.850 | 31.910 | 6.429 | 4.044 | 613.899 | 50.294 | 330.904 | 5.45 | 2.02 | 73.93 | 3.74 | 19.80 |
| Zn 2nd CL TAIL | 30.2 | 1.55 | 0.340 | 0.380 | 13.600 | 21.480 | 28.340 | 0.526 | 0.588 | 21.043 | 33.236 | 43.850 | 0.45 | 0.29 | 2.53 | 2.47 | 2.62 |
| Zn 1st CL CONC | 232.6 | 11.92 | 0.584 | 0.389 | 53.279 | 7.009 | 31.446 | 6.955 | 4.632 | 634.942 | 83.530 | 374.754 | 5.90 | 2.31 | 76.46 | 6.21 | 22.42 |
| Zn 1st CL TAIL | 222.3 | 11.39 | 0.200 | 0.200 | 0.840 | 30.420 | 32.190 | 2.278 | 2.278 | 10.706 | 346.468 | 366.628 | 1.93 | 1.14 | 1.29 | 25.77 | 21.94 |
| Zn RO CONC | 454.9 | 23.31 | 0.396 | 0.296 | 27.702 | 18.450 | 31.810 | 9.233 | 6.910 | 645.648 | 429.998 | 741.382 | 7.83 | 3.45 | 77.75 | 31.99 | 44.36 |
| TAIL | 1202.5 | 61.61 | 0.060 | 0.120 | 0.110 | 11.000 | 8.670 | 3.697 | 7.393 | 6.777 | 677.708 | 534.157 | 3.14 | 3.69 | 0.82 | 50.41 | 31.96 |
| CALC HEAD | | 1951.8 | 100.0 | 1.179 | 2.001 | 8.304 | 13.444 | 16.712 | 117.9 | 200.1 | 830.4 | 1344.4 | 1671.2 | 100.0 | 100.0 | 100.0 | 100.0 |

TEST NUMBER: 6891-10F2 FLOTATION OF COMPOSITE ORE #2 PAGE 1

| PRODUCT | WEIGHT | WEIGHT | Au | Ag | ASSAYS | | UNITS | Au | Ag | % DIST | |
|----------------|--------|--------|--------|--------|--------|--|-------|----------|----|--------|-------|
| | GMS | % | oz/ton | oz/ton | | | | | | | |
| Cu/Pb RO CONC | 294.4 | 15.08 | 0.224 | 82.007 | | | 3.379 | 1236.954 | | 48.60 | 82.97 |
| Zn CONC | 202.4 | 10.37 | 0.055 | 9.288 | | | 0.570 | 96.316 | | 8.20 | 6.46 |
| Zn 2nd CL TAIL | 30.2 | 1.55 | 0.090 | 7.128 | | | 0.139 | 11.029 | | 2.00 | 0.74 |
| Zn 1st CL CONC | 232.6 | 11.92 | 0.060 | 9.008 | | | 0.710 | 107.345 | | 10.21 | 7.20 |
| Zn 1st CL TAIL | 222.3 | 11.39 | 0.100 | 5.325 | | | 1.139 | 60.649 | | 16.38 | 4.07 |
| Zn RO CONC | 454.9 | 23.31 | 0.079 | 7.208 | | | 1.849 | 167.994 | | 26.59 | 11.27 |
| TAIL | 1202.5 | 61.61 | 0.028 | 1.395 | | | 1.725 | 85.946 | | 24.81 | 5.76 |
| <hr/> | | | | | | | | | | | |
| CALC HEAD | 1951.8 | 100.0 | 0.070 | 14.909 | | | 7.0 | 1490.9 | | 100.0 | 100.0 |

TESTWORK PROCEDURE

TEST NO.

6891 - 10F3

DATE

Composite #2 - 12 KG. Feed

| STAGE | TIME (min.) | ADDITIONS | |
|-----------------|----------------|--|--|
| | | Lb./Ton | REAGENT |
| Grind | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ ZnSO ₄ Z-200 |
| Cu/Pb Rougher | 18 | 0.03 0.05 | AERO 238 MIBC |
| Zn Condition | 5 | 27.87 0.45 0.10 0.02 0.05 | Lime to pH=10.5 CuSO ₄ NaCN Z-200 AERO 343 |
| Zn Rougher | 8 | 0.04 | DF 1012 |
| Cu/Pb Regrind | 30 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| Cu/Pb Cleaner | 7 | | |
| Condition | 2 | 1.0 | Na ₂ SO ₃ |
| Cu/Pb recleaner | 6 | | |
| Zinc Regrind | 30 | 0.1 | CuSO ₄ |
| Zn Cleaner | 10 | 1.60 0.25 0.20 0.02 0.04 0.10 | Lime to pH=11 NaCN CuSO ₄ Z-200 AERO 343 CuSO ₄ |
| Zn Recleaner | 5 | 1.20 | Lime to pH=11.5 |

TESTWORK PROCEDURE

TEST NO. 6891 - 10F3 Cont'd DATE _____

Copper-Lead Separation

| STAGE | TIME (min.) | ADDITIONS | |
|-------------------|----------------|--------------|-----------------------------|
| | | Lb./Ton | REAGENT |
| Condition | 20 | 0.06 0.06 | Dextrin Carbon |
| Condition | 20 | 96ml | Sulphuous Acid=6% to pH=4.8 |
| Screen Out Carbon | | | |
| Copper Float | 7 | 0.02 | Z-200 |
| Conc. #2 | 4 | --- | --- |

TEST NUMBER: 8891-10F3 FLOTATION OF COMPOSITE #2 BIG CELL TEST PAGE 2

| PRODUCT | WEIGHT | | WEIGHT | | ASSAYS | | | | UNITS | | | | % DIST | | | | |
|-------------------|---------|-------|--------|--------|--------|--------|--------|---------|---------|---------|----------|----------|--------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | S% | Cu | Pb | Zn | Fe | S | Cu | Pb | Zn | Fe | S |
| Cu CONC | 148.8 | 1.25 | 33.200 | 9.600 | 6.800 | 7.320 | 27.410 | 41.849 | 12.043 | 8.531 | 9.183 | 34.386 | 33.96 | 6.43 | 1.34 | 0.74 | 2.32 |
| Pb CONC | 109.1 | 0.91 | 1.150 | 80.000 | 2.400 | 1.370 | 14.900 | 1.051 | 73.093 | 2.193 | 1.252 | 13.614 | 0.86 | 39.01 | 0.34 | 0.10 | 0.92 |
| Cu/Pb SEP. TAIL | 74.1 | 0.62 | 1.040 | 41.600 | 19.400 | 5.720 | 20.560 | 0.645 | 25.815 | 12.039 | 3.550 | 12.759 | 0.53 | 13.78 | 1.83 | 0.29 | 0.86 |
| Cu/Pb CONC | 333.0 | 2.79 | 15.543 | 39.786 | 8.162 | 5.015 | 21.787 | 43.346 | 110.951 | 22.782 | 13.984 | 60.758 | 35.34 | 59.21 | 3.58 | 1.13 | 4.10 |
| Cu/Pb 2nd CL TAIL | 230.9 | 1.93 | 7.400 | 24.600 | 15.600 | 10.410 | 23.740 | 14.309 | 47.588 | 30.165 | 20.130 | 45.905 | 11.67 | 25.39 | 4.74 | 1.63 | 3.10 |
| Cu/Pb 1st CL CONC | 563.9 | 4.72 | 12.209 | 33.568 | 11.208 | 7.224 | 22.587 | 57.655 | 158.519 | 52.927 | 34.114 | 106.663 | 47.01 | 84.60 | 8.32 | 2.77 | 7.19 |
| Cu/Pb 1st CL TAIL | 1585.0 | 13.11 | 4.400 | 1.440 | 26.800 | 12.810 | 25.590 | 57.667 | 18.873 | 351.244 | 167.889 | 335.385 | 47.02 | 10.07 | 55.21 | 13.62 | 22.61 |
| Cu/Pb RO CONC | 2128.9 | 17.83 | 6.468 | 9.350 | 22.670 | 11.330 | 24.795 | 115.322 | 177.392 | 404.171 | 202.003 | 442.049 | 94.03 | 34.67 | 63.52 | 16.38 | 29.81 |
| Zn CONC | 130.4 | 1.09 | 1.360 | 0.800 | 46.400 | 12.000 | 26.850 | 1.485 | 0.874 | 50.670 | 13.104 | 29.321 | 1.21 | 0.47 | 7.96 | 1.06 | 1.98 |
| Zn 2nd CL TAIL | 331.2 | 2.77 | 0.220 | 0.160 | 54.400 | 5.100 | 29.450 | 0.610 | 0.444 | 150.886 | 14.146 | 81.684 | 0.50 | 0.24 | 23.71 | 1.15 | 5.51 |
| Zn 1st CL CONC | 461.6 | 3.87 | 0.542 | 0.341 | 52.140 | 7.049 | 26.716 | 2.095 | 1.317 | 201.556 | 27.250 | 111.005 | 1.71 | 0.70 | 31.68 | 2.21 | 7.48 |
| Zn 1st CL TAIL | 383.5 | 3.04 | 0.160 | 0.180 | 5.800 | 18.300 | 19.650 | 0.487 | 0.548 | 17.856 | 55.708 | 59.817 | 0.40 | 0.29 | 2.78 | 4.52 | 4.03 |
| Zn RO CONC | 1725.1 | 14.45 | 0.179 | 0.129 | 15.174 | 5.742 | 11.824 | 2.582 | 1.865 | 219.212 | 82.958 | 170.822 | 2.11 | 1.00 | 34.45 | 6.73 | 11.52 |
| TAIL | 8087.0 | 67.72 | 0.070 | 0.120 | 0.190 | 14.000 | 12.850 | 4.741 | 8.127 | 12.868 | 948.145 | 870.262 | 3.87 | 4.34 | 2.02 | 76.89 | 58.88 |
| CALC HEAD | 11941.0 | 100.0 | 1.226 | 1.874 | 6.363 | 12.331 | 14.831 | 122.645 | 187.384 | 636.251 | 1233.106 | 1483.132 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 8891-10F3 FLOTATION OF COMPOSITE #2 BIG CELL TEST PAGE 1

| PRODUCT | WEIGHT | | ASSAYS oz/ton | UNITS | % DIST |
|-------------------|---------|-------|------------------|----------|--------|
| | GMS | % | | | |
| Cu CONC | 149.8 | 1.25 | 458.206 | 574.620 | 41.78 |
| Pb CONC | 109.1 | 0.91 | 54.877 | 50.139 | 3.64 |
| Cu/Pb SEP. TAIL | 74.1 | 0.62 | 45.225 | 28.084 | 2.04 |
| Cu/Pb CONC | 333.0 | 2.79 | 234.167 | 653.023 | 47.46 |
| Cu/Pb 2nd CL TAIL | 230.9 | 1.93 | 91.580 | 177.086 | 12.87 |
| Cu/Pb 1st CL CONC | 563.9 | 4.72 | 175.782 | 830.109 | 60.33 |
| Cu/Pb 1st CL TAIL | 1565.0 | 13.11 | 27.907 | 365.751 | 26.58 |
| Cu/Pb RO CONC | 2128.9 | 17.83 | 87.076 | 1195.860 | 86.91 |
| Zn CONC | 130.4 | 1.09 | 16.547 | 18.070 | 1.31 |
| Zn 2nd CL TAIL | 331.2 | 2.77 | 4.094 | 11.355 | 0.83 |
| Zn 1st CL CONC | 461.6 | 3.87 | 7.612 | 29.425 | 2.14 |
| Zn 1st CL TAIL | 363.5 | 3.04 | 3.398 | 10.344 | 0.75 |
| Zn RO CONC | 1725.1 | 14.45 | 2.753 | 39.769 | 2.89 |
| TAIL | 8087.0 | 67.72 | 2.072 | 140.325 | 10.20 |
| CALC HEAD | 11941.0 | 100.0 | 13.760 | 1375.955 | 100.00 |

TESTWORK PROCEDURE

TEST NO. 6891 - 10F4 DATE _____

Locked Cycle - Composite #2

| STAGE | TIME (min.) | ADDITIONS | |
|-------------------|----------------|------------------------------|--|
| | | Lb./Ton | REAGENT |
| Grind | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ ZnSO ₄ Z-200 |
| Cu/Pb Rougher | 10 | 0.03 0.05 | AERO 238 MIBC |
| Zn Condition | 5 5 | 0.45 0.10 0.02 0.05 | Lime to pH=10.5 CuSO ₄ NaCN Z-200 AERO 343 |
| Zn Rougher | 8 | 0.04 | DF 1012 |
| Cu/Pb Regrind | 15 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaSO ₄ Z-200 |
| Cu/Pb 1st Cleaner | 7 | | |
| Cu/Pb 2nd Cleaner | 6 | 1.0 | Na ₂ SO ₃ |
| Zn Regrind | 15 | 0.10 | CuSO ₄ |
| Condition | 5 | | Ca(OH) ₂ to pH = 10.8 |
| Zn 1st Cleaner | 3 | 0.25 0.02 0.20 0.02 | NaCN Z-200 CuSO ₄ Aero 343 |
| Zn 2nd Cleaner | 4 | | Lime to pH = 11.5 |

TEST NUMBER: 6891-10F4 LOCK CYCLE FLOTATION OF COMPOSITE #2 PAGE 2

| PRODUCT | WEIGHT GMS | | WEIGHT % | | ASSAYS | | | UNITS | | | | % DIST | | | | |
|--------------------|------------|-------|----------|--------|--------|--------|----|---------|---------|---------|----------|--------|--------|--------|--------|--------|
| | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| Cu/Pb CONC #1 | 100.4 | 0.86 | 18.000 | 32.800 | 7.360 | 8.000 | | 15.499 | 28.243 | 8.337 | 7.750 | | 12.93 | 14.42 | 0.76 | 0.58 |
| #2 | 125.8 | 1.08 | 18.000 | 24.800 | 8.980 | 11.110 | | 17.262 | 26.757 | 9.667 | 11.987 | | 14.41 | 13.66 | 1.16 | 0.90 |
| #3 | 100.9 | 0.87 | 16.400 | 32.000 | 7.520 | 9.480 | | 14.192 | 27.691 | 8.507 | 8.204 | | 11.84 | 14.14 | 0.78 | 0.62 |
| #4 | 118.1 | 1.01 | 17.600 | 28.400 | 8.000 | 10.320 | | 17.826 | 28.765 | 8.103 | 10.453 | | 14.88 | 14.69 | 0.97 | 0.79 |
| #5 | 105.0 | 0.90 | 18.000 | 32.800 | 7.360 | 8.580 | | 16.209 | 29.537 | 8.628 | 7.726 | | 13.53 | 15.08 | 0.79 | 0.58 |
| #6 | 107.3 | 0.92 | 17.600 | 32.400 | 7.520 | 8.630 | | 16.196 | 29.816 | 8.920 | 7.942 | | 13.52 | 15.22 | 0.83 | 0.60 |
| TOTAL Cu/Pb CONCS | 657.5 | 5.64 | 17.235 | 30.291 | 7.832 | 9.587 | | 37.185 | 170.809 | 44.163 | 54.061 | | 81.11 | 87.21 | 5.30 | 4.07 |
| Cu/Pb 2nd CL TAIL | 28.8 | 0.23 | 10.400 | 1.840 | 17.600 | 13.700 | | 2.390 | 0.423 | 4.045 | 3.149 | | 1.99 | 0.22 | 0.49 | 0.24 |
| Cu/Pb 1st CL TAIL | 148.7 | 1.26 | 0.920 | 0.880 | 15.200 | 17.180 | | 1.157 | 0.856 | 19.124 | 21.615 | | 0.97 | 0.44 | 2.29 | 1.63 |
| Zn CONC #1 | 80.6 | 0.69 | 1.280 | 1.400 | 57.600 | 4.700 | | 0.885 | 0.968 | 39.816 | 3.249 | | 0.74 | 0.49 | 4.78 | 0.24 |
| #2 | 84.1 | 0.72 | 1.560 | 1.240 | 52.800 | 4.980 | | 1.125 | 0.694 | 38.083 | 3.592 | | 0.94 | 0.46 | 4.57 | 0.27 |
| #3 | 192.9 | 1.85 | 0.960 | 0.830 | 57.800 | 3.570 | | 1.588 | 1.042 | 95.292 | 5.906 | | 1.33 | 0.53 | 11.43 | 0.44 |
| #4 | 148.8 | 1.28 | 1.320 | 0.720 | 57.800 | 3.380 | | 1.685 | 0.919 | 73.507 | 4.313 | | 1.41 | 0.47 | 8.82 | 0.32 |
| #5 | 85.2 | 0.56 | 2.920 | 1.840 | 49.800 | 7.120 | | 1.633 | 1.029 | 27.735 | 3.381 | | 1.36 | 0.53 | 3.33 | 0.30 |
| #6 | 110.5 | 0.35 | 1.520 | 1.040 | 55.200 | 7.140 | | 1.440 | 0.966 | 52.312 | 6.766 | | 1.20 | 0.50 | 6.27 | 0.51 |
| TOTAL Zn CONCS | 682.1 | 5.85 | 1.428 | 0.998 | 55.855 | 4.754 | | 8.356 | 5.838 | 326.745 | 27.806 | | 6.97 | 2.98 | 39.19 | 2.09 |
| Zn 2nd CL TAIL | 237.6 | 2.04 | 0.500 | 0.340 | 58.400 | 5.220 | | 1.019 | 0.693 | 119.004 | 10.637 | | 0.85 | 0.35 | 14.27 | 0.80 |
| Zn 1st CL TAIL | 637.2 | 5.46 | 0.290 | 0.240 | 42.800 | 6.490 | | 1.585 | 1.312 | 233.895 | 35.467 | | 1.32 | 0.67 | 28.05 | 2.67 |
| PYRITE CONC #1 | 348.7 | 2.99 | 0.180 | 0.220 | 0.480 | 38.320 | | 0.538 | 0.858 | 1.435 | 114.598 | | 0.45 | 0.34 | 0.17 | 8.63 |
| #2 | 343.8 | 2.95 | 0.220 | 0.260 | 0.940 | 36.700 | | 0.649 | 0.787 | 2.772 | 108.211 | | 0.54 | 0.38 | 0.33 | 8.15 |
| #3 | 401.4 | 3.44 | 0.240 | 0.280 | 1.730 | 36.680 | | 0.826 | 0.964 | 5.956 | 126.272 | | 0.69 | 0.43 | 0.71 | 9.51 |
| #4 | 346.7 | 2.97 | 0.340 | 0.350 | 1.940 | 30.820 | | 1.011 | 1.041 | 5.768 | 91.641 | | 0.84 | 0.53 | 0.69 | 6.90 |
| #5 | 387.7 | 3.33 | 0.270 | 0.320 | 1.870 | 33.300 | | 0.898 | 1.064 | 6.218 | 110.724 | | 0.75 | 0.54 | 0.75 | 8.34 |
| #6 | 494.2 | 4.24 | 0.260 | 0.340 | 11.400 | 28.200 | | 1.102 | 1.441 | 48.318 | 119.523 | | 0.92 | 0.74 | 5.80 | 9.00 |
| TOTAL PYRITE CONCS | 2322.5 | 19.92 | 0.252 | 0.298 | 3.538 | 33.686 | | 5.024 | 5.934 | 70.487 | 670.970 | | 4.19 | 3.03 | 8.45 | 50.53 |
| TAIL #1 | 1060.4 | 9.09 | 0.040 | 0.120 | 0.320 | 4.980 | | 0.364 | 1.091 | 2.910 | 45.290 | | 0.30 | 0.56 | 0.35 | 3.41 |
| #2 | 1219.0 | 10.45 | 0.050 | 0.120 | 0.270 | 7.940 | | 0.523 | 1.255 | 2.823 | 83.009 | | 0.44 | 0.64 | 0.34 | 6.25 |
| #3 | 1214.4 | 10.42 | 0.050 | 0.180 | 0.250 | 8.320 | | 0.521 | 1.666 | 2.604 | 86.654 | | 0.43 | 0.85 | 0.31 | 6.53 |
| #4 | 1325.1 | 11.36 | 0.060 | 0.160 | 0.260 | 10.110 | | 0.682 | 1.818 | 2.955 | 114.895 | | 0.57 | 0.93 | 0.35 | 8.65 |
| #5 | 1214.9 | 10.42 | 0.060 | 0.280 | 0.240 | 9.830 | | 0.625 | 2.917 | 2.501 | 102.423 | | 0.52 | 1.49 | 0.30 | 7.71 |
| #6 | 915.8 | 7.85 | 0.050 | 0.160 | 0.320 | 9.140 | | 0.393 | 1.257 | 2.513 | 71.787 | | 0.33 | 0.64 | 0.30 | 5.41 |
| TOTAL TAILS | 6949.6 | 59.80 | 0.052 | 0.168 | 0.274 | 8.457 | | 3.107 | 10.005 | 16.305 | 504.057 | | 2.59 | 5.11 | 1.96 | 37.96 |
| CALC HEAD | 11660.0 | 100.0 | 1.198 | 1.959 | 8.337 | 13.278 | | 119.824 | 195.868 | 833.748 | 1327.764 | | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6891-10F4 LOCK CYCLE FLOTATION OF COMPOSITE #2 PAGE 1

| PRODUCT | WEIGHT GMS | WEIGHT % | AU oz/ton | AG oz/ton | ASSAYS | | UNITS | % DIST | | |
|--------------------|------------|----------|-----------|-----------|--------|----|-------|----------|--------|--------|
| | | | | | AU | AG | | AU | AG | |
| Cu/Pb CONC #1 | 100.4 | 0.86 | 0.779 | 200.540 | | | 0.671 | 172.678 | 9.17 | 11.61 |
| | #2 | 125.8 | 1.08 | 0.545 | | | 0.588 | 202.473 | 8.04 | 13.61 |
| | #3 | 100.9 | 0.87 | 0.498 | | | 0.431 | 171.650 | 5.89 | 11.54 |
| | #4 | 118.1 | 1.01 | 0.431 | | | 0.437 | 190.818 | 5.97 | 12.83 |
| | #5 | 105.0 | 0.90 | 0.476 | | | 0.429 | 182.423 | 5.86 | 12.26 |
| | #6 | 107.3 | 0.92 | 0.447 | | | 0.411 | 194.011 | 5.62 | 13.04 |
| TOTAL Cu/Pb CONCS | 657.5 | 5.84 | 0.526 | 197.564 | | | 2.966 | 1114.053 | 40.58 | 74.88 |
| Cu/Pb 2nd CL TAIL | 26.8 | 0.23 | 0.128 | 68.626 | | | 0.029 | 15.773 | 0.40 | 1.06 |
| Cu/Pb 1st CL TAIL | 146.7 | 1.26 | 0.068 | 9.534 | | | 0.086 | 12.071 | 1.17 | 0.81 |
| Zn CONC #1 | 80.8 | 0.69 | 0.132 | 16.634 | | | 0.091 | 11.498 | 1.25 | 0.77 |
| | #2 | 84.1 | 0.72 | 0.144 | | | 0.104 | 14.092 | 1.42 | 0.95 |
| | #3 | 192.9 | 1.85 | 0.061 | | | 0.101 | 19.561 | 1.38 | 1.32 |
| | #4 | 148.8 | 1.28 | 0.055 | | | 0.070 | 18.527 | 0.96 | 1.25 |
| | #5 | 65.2 | 0.56 | 0.100 | | | 0.056 | 17.244 | 0.76 | 1.16 |
| | #6 | 110.5 | 0.95 | 0.070 | | | 0.066 | 16.521 | 0.91 | 1.11 |
| TOTAL Zn CONCS | 682.1 | 5.85 | 0.084 | 16.674 | | | 0.488 | 97.544 | 6.68 | 6.56 |
| Zn 2nd CL TAIL | 237.6 | 2.04 | 0.042 | 8.546 | | | 0.086 | 13.339 | 1.17 | 0.90 |
| Zn 1st CL TAIL | 637.2 | 5.46 | 0.040 | 4.752 | | | 0.219 | 25.369 | 2.99 | 1.75 |
| PYRITE CONC #1 | 348.7 | 2.99 | 0.120 | 6.832 | | | 0.359 | 19.833 | 4.91 | 1.33 |
| | #2 | 343.8 | 2.95 | 0.118 | | | 0.342 | 21.230 | 4.68 | 1.43 |
| | #3 | 401.4 | 3.44 | 0.118 | | | 0.393 | 24.563 | 5.46 | 1.65 |
| | #4 | 346.7 | 2.97 | 0.108 | | | 0.321 | 22.839 | 4.39 | 1.54 |
| | #5 | 387.7 | 3.33 | 0.108 | | | 0.359 | 23.327 | 4.91 | 1.61 |
| | #6 | 494.2 | 4.24 | 0.098 | | | 0.407 | 30.970 | 5.56 | 2.08 |
| TOTAL PYRITE CONCS | 2322.5 | 19.92 | 0.110 | 7.197 | | | 2.187 | 143.361 | 29.91 | 9.64 |
| TAIL #1 | 1060.4 | 9.09 | 0.011 | 0.555 | | | 0.100 | 5.047 | 1.37 | 0.34 |
| | #2 | 1219.0 | 10.45 | 0.021 | | | 0.220 | 12.023 | 3.00 | 0.81 |
| | #3 | 1214.4 | 10.42 | 0.021 | | | 0.219 | 11.623 | 2.99 | 0.78 |
| | #4 | 1325.1 | 11.36 | 0.027 | | | 0.307 | 14.526 | 4.20 | 0.96 |
| | #5 | 1214.9 | 10.42 | 0.021 | | | 0.219 | 12.201 | 2.99 | 0.82 |
| | #6 | 915.8 | 7.85 | 0.024 | | | 0.189 | 10.187 | 2.58 | 0.68 |
| TOTAL TAILS | 6949.6 | 59.80 | 0.021 | 1.102 | | | 1.252 | 65.707 | 17.12 | 4.42 |
| CALC HEAD | 11660.0 | 100.0 | 0.073 | 14.878 | | | 7.314 | 1487.817 | 100.00 | 100.00 |

TESTWORK PROCEDURE

TEST NO. 6891 - 10F5

DATE _____

Composite #2 - 12 KG. Test

| STAGE | TIME (min.) | ADDITIONS | |
|---------------------|----------------|---------------------------------------|--|
| | | Lb./Ton | REAGENT |
| Grind | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ ZnSO ₄ Z-200 pH=6.4 |
| Cu/Pb Rougher | 15 | 0.03 0.05 | AERO 238 MIBC pH=6.2 |
| Zn Condition | 5 5 | 9.33 0.60 0.10 0.03 0.075 | Ca(OH) ₂ to pH=10.5 CuSO ₄ NaCN Z-200 AERO 343 |
| Zn Rougher | 8 | 0.04 | DF 1012 |
| Zn Cleaning/Regrind | 30 | 0.10 | CuSO ₄ |
| Condition | 5 | 0.79 | Ca(OH) ₂ to pH=10.8 |
| Zn 1st Cleaner | 6 | 0.25 0.02 0.20 0.02 | NaCN Z-200 CuSO ₄ AERO 343 |
| Zn 2nd Cleaner | 5 | 0.79 | Ca(OH) ₂ pH=11.5 |
| Cu/Pb Regrind | 30 | 2.0 1.0 0.1 | Na ₂ SO ₃ ZnSO ₄ NaCN |
| Cu/Pb 1st Cleaner | 7 | 0.02 | Z-200 |
| Condition | 2 | 1.0 | Na ₂ SO ₃ |
| Cu/Pb 2nd Cleaner | ---- | ---- | NO FLOAT |

TEST NUMBER: 6891-10F5 FLOTATION OF COMPOSITE #2 BIG CELL TEST #2 PAGE 2

| PRODUCT | WEIGHT | | WEIGHT | | ASSAYS | | | | UNITS | | | | % DIST | | | |
|-------------------|---------|-------|--------|--------|--------|--------|---------|---------|---------|----------|--------|--------|--------|--------|--|--|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe | | |
| Cu/Pb 1st CL CONC | 513.0 | 4.29 | 10.000 | 32.000 | 7.800 | 10.890 | 42.870 | 137.183 | 33.438 | 46.885 | 39.17 | 78.34 | 4.16 | 3.54 | | |
| Cu/Pb 1st CL TAIL | 1245.2 | 10.41 | 5.300 | 2.200 | 19.400 | 16.320 | 55.150 | 22.893 | 201.871 | 169.821 | 50.39 | 13.07 | 25.10 | 12.86 | | |
| Cu/Pb RO CONC | 1758.2 | 14.89 | 6.671 | 10.895 | 16.015 | 14.736 | 98.020 | 160.076 | 235.309 | 216.506 | 89.57 | 91.42 | 29.25 | 16.40 | | |
| Zn CONC | 915.0 | 7.65 | 0.570 | 0.350 | 60.000 | 4.280 | 4.358 | 2.676 | 458.781 | 32.726 | 3.98 | 1.53 | 57.03 | 2.48 | | |
| Zn 2nd CL TAIL | 175.1 | 1.46 | 0.270 | 0.280 | 34.000 | 12.980 | 0.395 | 0.410 | 49.751 | 18.993 | 0.36 | 0.23 | 6.18 | 1.44 | | |
| Zn 1st CL CONC | 1090.1 | 9.11 | 0.522 | 0.339 | 55.824 | 5.677 | 4.753 | 3.086 | 508.531 | 51.719 | 4.34 | 1.76 | 63.22 | 3.92 | | |
| Zn 1st CL TAIL | 682.8 | 5.71 | 0.180 | 0.240 | 7.900 | 16.270 | 1.027 | 1.369 | 45.077 | 92.835 | 0.94 | 0.78 | 5.60 | 7.03 | | |
| Zn RO CONC | 1772.9 | 14.82 | 0.390 | 0.301 | 37.367 | 9.757 | 5.781 | 4.455 | 553.608 | 144.555 | 5.28 | 2.54 | 68.82 | 10.35 | | |
| TAIL | 8435.4 | 70.49 | 0.080 | 0.150 | 0.220 | 13.610 | 5.639 | 10.574 | 15.508 | 959.393 | 5.15 | 6.04 | 1.93 | 72.66 | | |
| CALC HEAD | 11966.5 | 100.0 | 1.094 | 1.751 | 8.044 | 13.205 | 109.440 | 175.105 | 804.426 | 1320.454 | 100.00 | 100.00 | 100.00 | 100.00 | | |

TEST NUMBER: 6891-10F5 FLOTATION OF COMPOSITE #2 BIG CELL TEST #2 PAGE 1

| PRODUCT | WEIGHT | WEIGHT | Au | Ag | ASSAYS | UNITS | % DIST | |
|-------------------|---------|--------|--------|---------|--------|--------|----------|---------------|
| | GMS | % | oz/ton | oz/ton | | | Au | Ag |
| Cu/Pb 1st CL CONC | 513.0 | 4.29 | 1.146 | 190.110 | | 4.913 | 814.395 | 35.56 57.44 |
| Cu/Pb 1st CL TAIL | 1245.2 | 10.41 | 0.248 | 36.338 | | 2.581 | 378.102 | 18.68 26.65 |
| Cu/Pb RO CONC | 1758.2 | 14.89 | 0.510 | 81.204 | | 7.493 | 1193.098 | 54.24 84.09 |
| Zn CONC | 915.0 | 7.65 | 0.358 | 7.374 | | 2.737 | 56.384 | 19.82 3.97 |
| Zn 2nd CL TAIL | 175.1 | 1.46 | 0.076 | 5.268 | | 0.111 | 7.708 | 0.81 0.54 |
| Zn 1st CL CONC | 1090.1 | 9.11 | 0.313 | 7.036 | | 2.849 | 64.093 | 20.62 4.52 |
| Zn 1st CL TAIL | 682.8 | 5.71 | 0.102 | 3.844 | | 0.582 | 21.934 | 4.21 1.55 |
| Zn RO CONC | 1772.9 | 14.82 | 0.232 | 5.806 | | 3.431 | 86.026 | 24.83 6.06 |
| TAIL | 8435.4 | 70.49 | 0.041 | 1.981 | | 2.890 | 139.644 | 20.92 9.84 |
| CALC HEAD | 11966.5 | 100.0 | 0.138 | 14.188 | | 13.814 | 1418.768 | 100.00 100.00 |

TESTWORK PROCEDURE

TEST NO.

6891 - 10F6

DATE

| STAGE | TIME (min.) | ADDITIONS | |
|------------------------|----------------|----------------------------|---|
| | | Lb./Ton | REAGENT |
| Grind | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ ZnSO ₄ Z-200 |
| Cu/Pb Rougher | 10 | 0.03 0.05 | AERO 238 MIBC |
| Cu/Pb Cleaning/Regrind | 15 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| Cu/Pb 1st Cleaner | 7 | --- | --- |
| Condition | 2 | 1.0 | Na ₂ SO ₃ |
| Cu/Pb 2nd Cleaner | 6 | --- | --- |
| Cu/Pb Separation | | | |
| Condition | 20 | 0.05 0.1 | 60°C Staley Starch NaHSO ₃ |
| Cu Float | 5 | 0.02 | Z-200 |

TEST NUMBER: 6891-10F8 PAGE 2

| PRODUCT | WEIGHT | | ASSAYS | | | UNITS | | | | % DIST | | | | |
|-------------------|--------|-------|--------|-------|-------|-------|---------|---------|---------|----------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| Cu Conc | 144.3 | 3.74 | 23.20 | 32.00 | 5.80 | 8.61 | 86.777 | 119.652 | 21.894 | 24.724 | 72.25 | 81.84 | 2.61 | 1.91 |
| Pb Conc | 43.0 | 1.11 | 4.00 | 42.40 | 12.00 | 11.94 | 4.458 | 47.259 | 13.375 | 13.308 | 3.71 | 24.42 | 1.61 | 1.03 |
| Cu/Pb 2ND CL CONC | 187.3 | 4.85 | 18.79 | 34.39 | 7.22 | 7.83 | 91.235 | 166.951 | 35.069 | 38.032 | 75.97 | 85.26 | 4.23 | 2.94 |
| Cu/Pb 2nd CL Tail | 42.4 | 1.10 | 10.40 | 4.80 | 18.00 | 14.43 | 11.430 | 5.275 | 19.783 | 15.925 | 9.52 | 2.73 | 2.38 | 1.23 |
| Cu/Pb 1ST CL CONC | 229.7 | 5.95 | 17.24 | 28.93 | 9.21 | 9.08 | 102.665 | 172.226 | 54.852 | 53.357 | 85.48 | 88.98 | 6.61 | 4.16 |
| Cu/Pb 1st CL Tail | 242.2 | 6.28 | 0.88 | 0.48 | 17.20 | 18.83 | 4.269 | 2.888 | 107.982 | 118.215 | 3.55 | 1.49 | 13.01 | 9.12 |
| Cu/Pb RO CONC | 471.9 | 12.23 | 8.74 | 14.32 | 13.31 | 14.08 | 106.934 | 175.114 | 162.834 | 172.173 | 89.04 | 90.48 | 19.62 | 13.29 |
| Tail | 3386.0 | 87.77 | 0.15 | 0.21 | 7.60 | 12.80 | 13.165 | 18.431 | 867.036 | 1123.430 | 10.96 | 9.52 | 80.38 | 86.71 |
| CALC HEAD | 3857.9 | 100.0 | 1.20 | 1.94 | 8.30 | 12.96 | 120.099 | 193.548 | 829.871 | 1295.602 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6891-10F6 PAGE 1

| PRODUCT | WEIGHTS | | | | ASSAYS | | UNITS | | % DIST | | |
|-------------------|---------|-------|-----------|-----------|--------|-------|--------|----------|----------|--------|--------|
| | GMS | % | Au oz/ton | Ag oz/ton | | | Au | Ag | Au | Ag | |
| Cu Concentrate | 144.3 | 3.74 | 0.890 | 242.255 | | | 2.581 | 906.125 | 32.81 | 63.47 | |
| Pb Concentrate | 43.0 | 1.11 | 0.212 | 93.916 | | | 0.236 | 104.878 | 3.00 | 7.33 | |
| Cu/Pb 2ND CL CONC | 187.3 | 4.85 | 0.580 | 208.200 | | | 2.817 | 1010.803 | 35.82 | 70.81 | |
| Cu/Pb 2nd CL Tail | 42.4 | 1.10 | 0.200 | 77.893 | | | 0.220 | 85.608 | 2.79 | 6.00 | |
| Cu/Pb 1ST CL CONC | 229.7 | 5.95 | 0.510 | 184.146 | | | 3.037 | 1096.411 | 38.81 | 78.80 | |
| Cu/Pb 1st CL Tail | 242.2 | 6.28 | 0.084 | 8.347 | | | 0.527 | 52.403 | 6.71 | 3.67 | |
| Cu/Pb RO CONC | 471.9 | 12.23 | 0.291 | 93.918 | | | 3.584 | 1148.814 | 45.32 | 80.47 | |
| Tail | 3388.0 | 87.77 | 0.049 | 3.176 | | | 4.301 | 278.751 | 54.68 | 19.53 | |
| CALC HEAD | | | | 3857.9 | 100.0 | 0.079 | 14.276 | 7.865 | 1427.585 | 100.00 | 100.00 |

TESTWORK PROCEDURE

TEST NO. 6891 - 10F7

DATE _____

| STAGE | TIME (min.) | ADDITIONS | |
|-------------------|----------------|----------------------------|---|
| | | Lb./Ton | REAGENT |
| Grind | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ ZnSO ₄ Z-200 |
| Cu/Pb Rougher | 10 | 0.03 0.05 | AERO 238 MIBC |
| Cu/Pb Regrind | 15 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| Cu/Pb 1st Cleaner | 7 | --- | --- |
| Condition | 2 | 1.0 | Na ₂ SO ₃ |
| Cu/Pb 2nd Cleaner | 6 | --- | --- |
| Cu/Pb Separation | | | |
| Condition | 20 | 0.06 0.06 | DEX-TRIN CARBON (-6#+16#) |
| Condition | 20 | 3ml (6%) | Sulphurous Acid to Ph=4.8 |
| Screen Out Carbon | | | |
| Cu Float | 5 | 0.02 | Z-200 |

TEST NUMBER: 6891-10F7 PAGE 2

| PRODUCT | WEIGHT | | ASSAYS | | | | UNITS | | | | % DIST | | | |
|-------------------|--------|-------|--------|-------|-------|-------|---------|---------|---------|----------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| Cu Conc | 165.5 | 4.25 | 19.00 | 36.00 | 7.80 | 13.34 | 80.674 | 152.855 | 33.119 | 56.641 | 66.30 | 58.00 | 3.94 | 4.10 |
| Pb Conc | 19.4 | 0.50 | 9.80 | 18.80 | 9.60 | 19.01 | 4.878 | 8.362 | 4.778 | 9.462 | 4.01 | 3.17 | 0.57 | 0.69 |
| Cu/Pb 2ND CL CONC | 184.9 | 4.74 | 18.03 | 33.99 | 7.89 | 13.93 | 85.551 | 161.217 | 37.897 | 66.103 | 70.31 | 61.17 | 4.50 | 4.79 |
| Cu/Pb 2nd CL Tail | 46.9 | 1.20 | 12.70 | 16.20 | 13.90 | 18.21 | 15.281 | 19.493 | 16.725 | 21.911 | 12.56 | 7.40 | 1.99 | 1.59 |
| Cu/Pb 1ST CL CONC | 231.8 | 5.95 | 16.86 | 30.39 | 8.18 | 14.80 | 100.833 | 180.710 | 54.622 | 88.014 | 82.87 | 68.58 | 6.49 | 8.37 |
| Cu/Pb 1st CL Tail | 254.0 | 6.52 | 1.05 | 0.49 | 14.80 | 20.81 | 6.842 | 3.193 | 95.141 | 135.608 | 5.62 | 1.21 | 11.31 | 9.82 |
| Cu/Pb RO CONC | 485.0 | 12.46 | 8.84 | 14.78 | 12.02 | 17.94 | 107.675 | 183.303 | 149.763 | 223.822 | 88.49 | 69.78 | 17.80 | 18.19 |
| Tail | 3412.0 | 87.54 | 0.16 | 0.91 | 7.90 | 13.22 | 14.006 | 79.658 | 691.539 | 1157.233 | 11.51 | 30.22 | 82.20 | 83.81 |
| CALC HEAD | 3897.8 | 100.0 | 1.22 | 2.64 | 8.41 | 13.81 | 121.681 | 263.561 | 841.302 | 1380.856 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6891-10F7 PAGE 1

| PRODUCT | WEIGHT | | WEIGHT | | ASSAYS | | UNITS | | % DIST | |
|-------------------|--------|-------|--------|---------|--------|----|-------|----------|--------|--------|
| | GMS | % | oz/ton | oz/ton | Au | Ag | Au | Ag | Au | Ag |
| Cu Conc | 185.5 | 4.25 | 0.526 | 224.898 | | | 2.233 | 954.914 | 29.79 | 63.64 |
| Pb Conc | 19.4 | 0.50 | 0.437 | 118.151 | | | 0.218 | 58.806 | 2.90 | 3.92 |
| Cu/Pb 2ND CL CONC | 184.9 | 4.74 | 0.517 | 213.698 | | | 2.451 | 1013.719 | 32.63 | 67.56 |
| Cu/Pb 2nd CL Tail | 48.9 | 1.20 | 0.152 | 89.716 | | | 0.183 | 107.950 | 2.44 | 7.19 |
| Cu/Pb 1ST CL CONC | 231.8 | 5.95 | 0.443 | 188.613 | | | 2.634 | 1121.669 | 35.13 | 74.75 |
| Cu/Pb 1st CL Tail | 254.0 | 6.52 | 0.088 | 9.832 | | | 0.573 | 64.722 | 7.65 | 4.31 |
| Cu/Pb RG CONC | 485.8 | 12.46 | 0.257 | 95.190 | | | 3.207 | 1186.391 | 42.78 | 79.07 |
| Tail | 3412.0 | 87.54 | 0.049 | 3.588 | | | 4.289 | 314.081 | 57.22 | 20.93 |
| <hr/> | | | | | | | | | | |
| CALC HEAD | 3897.8 | 100.0 | 0.075 | 15.005 | | | 7.497 | 1500.472 | 100.00 | 100.00 |

TESTWORK PROCEDURE

Test No. 6891-10F8

Comp. #2

| STAGE | TIME (min) | ADDITIONS | |
|--|---------------|-------------------------------------|--|
| | | lb/ton | REAGENT |
| GRIND | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ pH = 5.3 ZnSO ₄ Z-200 |
| CU/PB ROUGHER | 18 | 1.63 0.03 0.05 | Na ₂ CO ₃ to pH = 6.5 Aero 238 MIBC pH = 6.5 |
| ZN CONDITION | 5 5 | 8.84 0.6 0.1 0.03 0.075 | Lime to pH = 10.5 CuSO ₄ NaCN Z-200 Aero 343 |
| ZN ROUGHER | 8 | 0.04 | DF1012 |
| Note: Cu/Pb Rougher conc split and 1/2 reground with steel, 1/2 with porcelain | | | |
| CU/PB REGRIND | 15 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| CU/PB 1ST CLEANER | 9 | | |
| CU/PB 2ND CLEANER | 8 | 1.0 | Na ₂ SO ₃ |
| ZN REGRIND | 30 | 0.1 | CuSO ₄ |
| CONDITION | 5 | 1.18 | Lime to pH 10.8 |
| ZN CLEANER | 8 | 0.25 0.03 0.20 0.02 | NaCN Z-200 CuSO ₄ Aero 343 |
| ZN 2ND CLEANER | 6 | 0.94 | Lime to pH 11.5 |

TEST NUMBER: 6891-10F8 FLOTATION OF COMPOSITE #2 BIG CELL FLOAT #3 PAGE 2

| PRODUCT | WEIGHT GMS | | WEIGHT % | | ASSAYS | | | | UNITS | | | | % DIST | | | |
|----------------------|------------|-------|----------|--------|--------|--------|---------|---------|---------|----------|--------|--------|--------|--------|----|----|
| | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| #1 Cu/Pb CONC | 136.4 | 1.15 | 22.640 | 27.380 | 5.870 | 8.830 | 25.932 | 31.338 | 8.494 | 10.114 | 21.24 | 17.68 | 0.80 | 0.75 | | |
| #1 Cu/Pb 2nd CL TAIL | 190.0 | 1.80 | 12.480 | 27.640 | 10.910 | 11.950 | 19.912 | 44.099 | 17.407 | 19.066 | 16.31 | 24.88 | 2.14 | 1.42 | | |
| #1 Cu/Pb 1st CL CONC | 326.4 | 2.74 | 16.726 | 27.523 | 8.720 | 10.646 | 45.843 | 75.437 | 23.901 | 29.180 | 37.55 | 42.57 | 2.94 | 2.17 | | |
| #1 Cu/Pb 1st CL TAIL | 257.5 | 2.18 | 3.640 | 1.220 | 13.560 | 22.280 | 7.871 | 2.638 | 29.321 | 48.176 | 6.45 | 1.49 | 3.60 | 3.58 | | |
| #1 Cu/Pb RO CONC | 583.9 | 4.90 | 10.955 | 15.923 | 10.855 | 15.777 | 53.714 | 78.075 | 53.222 | 77.356 | 43.93 | 44.06 | 6.54 | 5.74 | | |
| #2 Cu/Pb CONC | 247.3 | 2.08 | 18.880 | 32.980 | 8.880 | 8.080 | 38.792 | 68.446 | 14.246 | 18.738 | 31.77 | 38.62 | 1.75 | 1.24 | | |
| #2 Cu/Pb 2nd CL TAIL | 94.7 | 0.80 | 11.960 | 12.740 | 15.420 | 10.830 | 9.511 | 10.131 | 12.262 | 8.812 | 7.79 | 5.72 | 1.51 | 0.84 | | |
| #2 Cu/Pb 1st CL CONC | 342.0 | 2.87 | 18.619 | 27.361 | 9.230 | 8.827 | 48.303 | 78.578 | 26.508 | 25.350 | 39.56 | 44.34 | 3.26 | 1.88 | | |
| #2 Cu/Pb 1st CL TAIL | 223.5 | 1.88 | 3.230 | 1.510 | 14.260 | 17.100 | 6.062 | 2.834 | 26.763 | 32.093 | 4.97 | 1.80 | 3.29 | 2.38 | | |
| #2 Cu/Pb RO CONC | 585.5 | 4.75 | 11.448 | 17.144 | 11.218 | 12.097 | 54.365 | 81.412 | 53.271 | 57.443 | 44.53 | 45.94 | 6.54 | 4.27 | | |
| COMB Cu/Pb RO CONC | 1149.4 | 8.65 | 11.198 | 16.524 | 11.033 | 13.966 | 108.079 | 159.487 | 108.493 | 134.799 | 88.52 | 90.00 | 13.08 | 10.01 | | |
| Zn CONC | 149.8 | 1.26 | 3.710 | 1.800 | 42.520 | 10.010 | 4.867 | 2.013 | 53.487 | 12.592 | 3.82 | 1.14 | 6.57 | 0.93 | | |
| Zn 2nd CL TAIL | 637.0 | 5.35 | 0.340 | 0.200 | 54.240 | 5.550 | 1.819 | 1.070 | 290.134 | 29.887 | 1.49 | 0.80 | 35.84 | 2.20 | | |
| Zn 1st CL CONC | 788.8 | 6.81 | 0.982 | 0.487 | 52.009 | 6.399 | 6.486 | 3.082 | 343.820 | 42.279 | 5.31 | 1.74 | 42.21 | 3.14 | | |
| Zn 1st CL TAIL | 1215.5 | 10.21 | 0.190 | 0.210 | 34.080 | 13.310 | 1.933 | 2.143 | 347.851 | 135.854 | 1.59 | 1.21 | 42.73 | 10.09 | | |
| Zn RO CONC | 2002.3 | 18.81 | 0.501 | 0.311 | 41.125 | 10.594 | 8.425 | 5.226 | 691.472 | 178.133 | 8.90 | 2.95 | 84.93 | 13.23 | | |
| TAIL | 8756.9 | 73.53 | 0.076 | 0.170 | 0.220 | 14.080 | 5.589 | 12.501 | 18.178 | 1033.892 | 4.58 | 7.05 | 1.99 | 76.77 | | |
| CALC HEAD | 11908.8 | 100.0 | 1.221 | 1.772 | 8.141 | 13.468 | 122.092 | 177.213 | 814.143 | 1346.824 | 100.00 | 100.00 | 100.00 | 100.00 | | |

TEST NUMBER: 6891-10F8 FLOTATION OF COMPOSITE #2 BIG CELL FLOAT #3 PAGE 1

| PRODUCT | WEIGHT | WEIGHT | AU | Ag | ASSAYS | UNITS | % DIST | |
|----------------------|---------|--------|--------|---------|--------|--------|----------|---------------|
| | GMS | % | oz/ton | oz/ton | | | Au | Ag |
| #1 Cu/Pb CONC | 136.4 | 1.15 | 0.995 | 278.140 | | 1.140 | 318.579 | 9.24 22.87 |
| #1 Cu/Pb 2nd CL TAIL | 190.0 | 1.60 | 0.101 | 108.959 | | 0.161 | 173.843 | 1.31 12.48 |
| #1 Cu/Pb 1st CL CONC | 326.4 | 2.74 | 0.475 | 179.658 | | 1.301 | 492.421 | 10.55 35.35 |
| #1 Cu/Pb 1st CL TAIL | 257.5 | 2.16 | 0.097 | 27.857 | | 0.210 | 60.235 | 1.70 4.32 |
| #1 Cu/Pb RO CONC | 583.9 | 4.90 | 0.308 | 112.714 | | 1.511 | 552.657 | 12.25 39.67 |
| #2 Cu/Pb CONC | 247.3 | 2.08 | 1.579 | 212.762 | | 3.279 | 441.832 | 26.58 31.72 |
| #2 Cu/Pb 2nd CL TAIL | 94.7 | 0.80 | 0.160 | 101.291 | | 0.127 | 80.549 | 1.03 5.78 |
| #2 Cu/Pb 1st CL CONC | 342.0 | 2.87 | 1.188 | 181.898 | | 3.406 | 522.381 | 27.62 37.50 |
| #2 Cu/Pb 1st CL TAIL | 223.5 | 1.88 | 0.536 | 24.318 | | 1.006 | 46.766 | 8.16 3.36 |
| #2 Cu/Pb RO CONC | 565.5 | 4.75 | 0.929 | 119.854 | | 4.412 | 589.147 | 35.77 40.86 |
| COMB CU/Pb RO CONC | 1149.4 | 9.65 | 0.614 | 118.227 | | 5.923 | 1121.804 | 48.02 80.53 |
| Zn CONC | 149.8 | 1.26 | 0.589 | 38.888 | | 0.741 | 48.915 | 6.01 3.51 |
| Zn 2nd CL TAIL | 637.0 | 5.35 | 0.079 | 8.843 | | 0.423 | 35.534 | 3.43 2.55 |
| Zn 1st CL CONC | 786.8 | 6.81 | 0.091 | 4.476 | | 1.163 | 84.449 | 9.43 6.06 |
| Zn 1st CL TAIL | 1215.5 | 10.21 | 0.190 | 0.210 | | 1.939 | 2.143 | 15.72 0.15 |
| Zn RO CONC | 2002.3 | 16.81 | 0.185 | 5.150 | | 3.103 | 86.583 | 25.16 6.22 |
| TAIL | 8756.3 | 73.53 | 0.045 | 2.511 | | 3.309 | 184.845 | 26.83 13.25 |
| CALC HEAD | 11908.6 | 100.0 | 0.123 | 13.830 | | 12.335 | 1393.041 | 100.00 100.00 |

TESTWORK PROCEDURE

Test No. 6891-10F9

Comp. #2

| STAGE | TIME (min) | lb/ton | ADDITIONS |
|----------------------|---------------|--------------------------------------|--|
| | | | REAGENT |
| GRIND | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ pH = 6.3 ZnSO ₄ Z-200 |
| CU/PB ROUGHER | 10 | 0.03 0.05 | Aero 238 MIBC pH = 6.0 |
| ZN CONDITION | 5 5 | 10.95 0.6 0.1 0.03 0.075 | Lime to pH = 10.5 CuSO ₄ NaCN Z-200 Aero 343 |
| ZN ROUGHER | 8 | 0.04 | DF1012 |
| CU/PB REGRIND | 15 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| CU/PB 1ST CLEANER | 9 | | |
| CU/PB 2ND CLEANER | 8 | 1.0 | Na ₂ SO ₃ |
| ZN REGRIND | 15 | 0.010 | CuSO ₄ |
| CONDITION | 5 | 0.42 | Lime to pH 10.8 |
| ZN 1ST CLEANER | 6 | 0.25 0.03 0.20 0.02 | NaCN Z-200 CuSO ₄ Aero 343 |
| ZN 2ND CLEANER | 5 | 0.78 | Lime to pH 11.5 |

TESTWORK PROCEDURE

Test No. 6891-10F9

| STAGE | TIME (min) | ADDITIONS | |
|----------------------|---------------|---------------|------------------------|
| | | lb/ton | REAGENT |
| CONDITION | 20 | 0.11 0.11 | Dextrin Carbon |
| CONDITION | 20 | 42 ml (6%) | Sulphurous to pH = 4.8 |
| SCREEN OUT CARBON | | | 6.0-4.8 |
| COPPER FLOAT | 1.5 | 0.02 | Z-200 |
| #2 CU FLOAT | 5.5 | | |

TEST NUMBER: 6891-10FS FLOTATION OF COMPOSITE ORE - Cu/Pb SEPARATION PAGE 2

| PRODUCT | WEIGHT | | ASSAYS | | | | UNITS | | | | % DIST | | | |
|---------------------|--------|-------|--------|--------|--------|--------|---------|---------|---------|----------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| Cu CONC | 144.3 | 3.83 | 18.920 | 27.800 | 5.280 | 6.490 | 65.896 | 102.701 | 19.508 | 23.376 | 64.68 | 62.81 | 2.59 | 2.14 |
| Pb CONC | 39.5 | 1.01 | 2.730 | 14.310 | 7.800 | 18.330 | 2.749 | 14.411 | 7.855 | 16.445 | 2.54 | 8.79 | 1.04 | 1.47 |
| Pb TAIL | 21.8 | 0.56 | 5.030 | 35.200 | 10.290 | 10.250 | 2.798 | 19.564 | 5.719 | 5.697 | 2.59 | 11.93 | 0.78 | 0.51 |
| COMP Pb CONC & TAIL | 81.3 | 1.56 | 3.548 | 21.739 | 8.686 | 14.168 | 5.545 | 33.975 | 13.574 | 22.142 | 5.13 | 20.71 | 1.80 | 1.97 |
| Cu/Pb CONC | 208.2 | 5.26 | 14.350 | 25.998 | 6.292 | 8.772 | 75.441 | 136.677 | 33.080 | 46.118 | 88.81 | 83.32 | 4.40 | 4.11 |
| Cu/Pb 2nd CL TAIL | 48.4 | 1.23 | 10.630 | 4.500 | 13.340 | 13.170 | 13.117 | 5.553 | 16.461 | 16.252 | 12.14 | 3.39 | 2.19 | 1.45 |
| Cu/Pb 1st CL CONC | 254.6 | 6.49 | 13.643 | 21.911 | 7.632 | 9.608 | 88.558 | 142.229 | 49.541 | 62.370 | 81.95 | 86.71 | 6.58 | 5.56 |
| Cu/Pb 1st CL TAIL | 241.8 | 6.16 | 1.180 | 0.410 | 13.050 | 18.190 | 7.274 | 2.528 | 80.451 | 112.138 | 6.73 | 1.54 | 10.69 | 9.99 |
| Cu/Pb RO CONC | 496.4 | 12.66 | 7.572 | 11.438 | 10.271 | 13.789 | 95.833 | 144.757 | 129.992 | 174.508 | 88.68 | 88.25 | 17.28 | 15.55 |
| Zn CONC | 371.1 | 9.46 | 0.580 | 0.540 | 52.360 | 5.430 | 5.488 | 5.109 | 495.397 | 51.375 | 5.08 | 3.11 | 85.84 | 4.58 |
| Zn 2nd CL TAIL | 48.8 | 1.19 | 0.350 | 0.500 | 18.630 | 12.970 | 0.416 | 0.594 | 19.758 | 15.409 | 0.38 | 0.36 | 2.63 | 1.37 |
| Zn 1st CL CONC | 417.7 | 10.65 | 0.554 | 0.536 | 48.374 | 6.271 | 5.903 | 5.703 | 515.155 | 88.785 | 5.46 | 3.48 | 68.47 | 5.95 |
| Zn 1st CL TAIL | 210.4 | 5.36 | 0.170 | 0.270 | 18.410 | 13.400 | 0.912 | 1.448 | 88.027 | 71.881 | 0.84 | 0.88 | 11.70 | 6.41 |
| Zn RO CONC | 628.1 | 18.01 | 0.426 | 0.447 | 37.667 | 8.659 | 8.815 | 7.152 | 603.182 | 138.665 | 8.31 | 4.36 | 80.16 | 12.36 |
| TAIL | 2797.8 | 71.33 | 0.078 | 0.170 | 0.270 | 11.340 | 5.421 | 12.126 | 19.259 | 808.888 | 5.02 | 7.39 | 2.56 | 72.09 |
| CALC HEAD | 3922.3 | 100.0 | 1.081 | 1.840 | 7.524 | 11.221 | 108.089 | 164.035 | 752.433 | 1122.059 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6891-10FS FLOTATION OF COMPOSITE ORE -Cu/Pb SEPARATION PAGE 1

| PRODUCT | WEIGHT | WEIGHT | Au | Ag | ASSAYS | UNITS | Au | Ag | % DIST | |
|---------------------|--------|--------|--------|---------|--------|-------|----------|----|--------|--------|
| | GMS | % | oz/ton | oz/ton | | | | | Au | Ag |
| Cu CONC | 144.9 | 3.69 | 0.495 | 227.052 | | 1.829 | 838.796 | | 23.45 | 58.80 |
| Pb CONC | 21.8 | 0.56 | 0.392 | 86.142 | | 0.218 | 47.878 | | 2.79 | 3.36 |
| Pb TAIL | 38.5 | 1.01 | 0.390 | 113.189 | | 0.393 | 113.989 | | 5.04 | 7.99 |
| COMP Pb CONC & TAIL | 81.3 | 1.56 | 0.391 | 103.570 | | 0.611 | 161.867 | | 7.83 | 11.35 |
| Cu/Pb CONC | 206.2 | 5.26 | 0.464 | 190.343 | | 2.439 | 1000.663 | | 31.28 | 70.15 |
| Cu/Pb 2nd CL TAIL | 48.4 | 1.23 | 0.124 | 88.508 | | 0.153 | 103.218 | | 1.96 | 7.66 |
| Cu/Pb 1st CL CONC | 254.8 | 6.49 | 0.399 | 170.984 | | 2.592 | 1109.881 | | 33.24 | 77.80 |
| Cu/Pb 1st CL TAIL | 241.8 | 6.16 | 0.076 | 10.834 | | 0.469 | 86.789 | | 6.01 | 4.68 |
| Cu/Pb RO CONC | 496.4 | 12.68 | 0.242 | 92.974 | | 3.061 | 1176.670 | | 39.25 | 82.48 |
| Zn CONC | 371.1 | 9.48 | 0.070 | 8.252 | | 0.862 | 78.075 | | 8.49 | 5.47 |
| Zn 2nd CL TAIL | 46.8 | 1.19 | 0.070 | 7.730 | | 0.083 | 9.184 | | 1.07 | 0.64 |
| Zn 1st CL CONC | 417.7 | 10.85 | 0.070 | 8.194 | | 0.745 | 87.259 | | 9.56 | 8.12 |
| Zn 1st CL TAIL | 210.4 | 5.36 | 0.066 | 4.050 | | 0.354 | 21.725 | | 4.54 | 1.52 |
| Zn RO CONC | 628.1 | 16.01 | 0.069 | 6.806 | | 1.100 | 108.984 | | 14.10 | 7.64 |
| TAIL | 2797.8 | 71.33 | 0.051 | 1.975 | | 3.638 | 140.877 | | 46.65 | 9.88 |
| CALC HEAD | 3922.3 | 100.0 | 0.078 | 14.285 | | 7.798 | 1426.532 | | 100.00 | 100.00 |

TESTWORK PROCEDURE

Test No. 6891-10F10

Comp. #2

| STAGE | TIME (min) | lb/ton | ADDITIONS |
|----------------------|---------------|--------------------------------------|--|
| | | | REAGENT |
| GRIND | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ pH = 6.2 ZnSO ₄ Z-200 |
| CU/PB ROUGHER | 10 | 0.03 0.05 | Aero 238 MIBC pH = 5.7 |
| ZN CONDITION | 5 5 | 14.05 0.6 0.1 0.03 0.075 | Lime to pH = 10.5 CuSO ₄ NaCN Z-200 Aero 343 |
| ZN ROUGHER | 8 | 0.04 | DF1012 |
| CONDITION | 5 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| CU/PB 1ST CLEANER | 10 | | |
| CU/PB 2ND CLEANER | 7 | 1.0 | Na ₂ SO ₃ |
| CONDTION | 5 | 0.66 | Lime to pH 10.8 |
| ZN 1ST CLEANER | 6 | 0.175 0.03 0.20 0.02 | NaCN Z-200 CuSO ₄ Aero 343 |
| ZN 2ND CLEANER | 5 | 0.69 | Lime to pH 11.5 |

TESTWORK PROCEDURE

Test No. 6891-10F10

Cu/Pb Separation

| STAGE | TIME (min) | ADDITIONS | |
|----------------------|---------------|---------------|-----------------------------------|
| | | lb/ton | REAGENT |
| CONDITION | 20 | 0.11 0.11 | Dextrin Carbon |
| CONDITION | 20 | 68 ml (6%) | Sulphurous to pH = 4.8 6.1-4.8 |
| SCREEN OUT CARBON | | | |
| COPPER FLOAT | 3.5 | 0.02 | Z-200 |
| #2 CU FLOAT | 4.5 | | |

TEST NUMBER: 6891-10F10 FLOTATION OF COMPOSITE ORE WITHOUT REGRIND - CU/PB SEPARATION PAGE 2

| PRODUCT | WEIGHT | | ASSAYS | | | UNITS | | | | % DIST | | | | |
|---------------------|--------|-------|--------|--------|--------|--------|---------|---------|---------|----------|--------|--------|--------|--------|
| | GMS | % | Cu% | Pb% | Zn% | Fe% | Cu | Pb | Zn | Fe | Cu | Pb | Zn | Fe |
| Cu CONC | 134.9 | 3.44 | 26.520 | 8.180 | 9.930 | 11.540 | 91.330 | 21.283 | 34.197 | 39.741 | 74.87 | 11.48 | 4.35 | 3.13 |
| Pb CONC | 30.1 | 0.77 | 3.820 | 43.080 | 13.970 | 7.900 | 2.935 | 33.103 | 10.735 | 6.070 | 2.41 | 17.85 | 1.37 | 0.48 |
| Pb TAIL | 71.0 | 1.81 | 0.710 | 58.920 | 8.330 | 6.790 | 1.287 | 103.169 | 15.098 | 12.307 | 1.05 | 55.63 | 1.92 | 0.97 |
| COMP Pb CONC & TAIL | 101.1 | 2.58 | 1.836 | 52.198 | 10.008 | 7.120 | 4.222 | 136.272 | 25.833 | 18.378 | 3.46 | 73.48 | 3.29 | 1.45 |
| Cu/Pb CONC | 236.0 | 6.02 | 15.860 | 26.151 | 9.984 | 9.647 | 95.552 | 157.555 | 60.030 | 58.119 | 78.33 | 84.95 | 7.64 | 4.57 |
| Cu/Pb 2nd CL TAIL | 28.3 | 0.72 | 7.650 | 7.650 | 13.940 | 11.090 | 5.871 | 5.527 | 10.071 | 8.012 | 4.65 | 2.98 | 1.28 | 0.63 |
| Cu/Pb 1st CL CONC | 264.3 | 6.75 | 15.002 | 24.170 | 10.380 | 9.801 | 101.223 | 163.082 | 70.101 | 66.131 | 82.98 | 87.93 | 8.93 | 5.20 |
| Cu/Pb 1st CL TAIL | 213.5 | 5.45 | 1.760 | 0.800 | 14.440 | 18.280 | 9.593 | 4.360 | 78.703 | 99.632 | 7.86 | 2.35 | 10.02 | 7.84 |
| Cu/Pb RO CONC | 477.8 | 12.20 | 9.085 | 13.728 | 12.200 | 13.590 | 110.816 | 167.442 | 148.804 | 165.783 | 90.85 | 90.28 | 18.95 | 13.04 |
| Zn CONC | 497.4 | 12.70 | 0.520 | 0.470 | 48.480 | 8.380 | 6.803 | 5.968 | 615.595 | 106.155 | 5.41 | 3.22 | 78.40 | 8.35 |
| Zn 2nd CL TAIL | 68.7 | 1.70 | 0.260 | 0.350 | 0.860 | 34.320 | 0.443 | 0.596 | 1.464 | 58.439 | 0.36 | 0.32 | 0.19 | 4.60 |
| Zn 1st CL CONC | 564.1 | 14.40 | 0.489 | 0.456 | 42.849 | 11.430 | 7.046 | 6.564 | 617.059 | 164.593 | 5.78 | 3.54 | 78.58 | 12.94 |
| Zn 1st CL TAIL | 160.4 | 4.08 | 0.160 | 0.260 | 0.500 | 23.520 | 0.855 | 1.065 | 2.047 | 98.309 | 0.54 | 0.57 | 0.26 | 7.57 |
| Zn RO CONC | 724.5 | 18.50 | 0.416 | 0.412 | 33.473 | 14.106 | 7.701 | 7.829 | 619.106 | 260.902 | 6.31 | 4.11 | 78.84 | 20.52 |
| TAIL | 2714.9 | 69.31 | 0.050 | 0.150 | 0.250 | 12.190 | 3.485 | 10.396 | 17.327 | 844.852 | 2.84 | 5.61 | 2.21 | 86.44 |
| CALC HEAD | 3917.2 | 100.0 | 1.220 | 1.855 | 7.852 | 12.715 | 121.982 | 165.467 | 785.237 | 1271.518 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6881-10F10 FLOTATION OF COMPOSITE ORE WITHOUT REGRIND - Cu/Pb SEPARATION PAGE 1

| PRODUCT | WEIGHT | WEIGHT | AU | AG | ASSAYS | | UNITS | % DIST | |
|---------------------|--------|--------|--------|---------|--------|----|-------|----------|--------|
| | GMS | % | oz/ton | oz/ton | AU | AG | | AU | AG |
| Cu CONC | 134.8 | 3.44 | 0.572 | 269.642 | | | 1.970 | 928.594 | |
| Pb CONC | 30.1 | 0.77 | 0.246 | 85.804 | | | 0.189 | 85.779 | |
| Pb TAIL | 71.0 | 1.81 | 0.150 | 29.200 | | | 0.272 | 52.926 | |
| COMP Pb CONC & TAIL | 101.1 | 2.58 | 0.179 | 45.993 | | | 0.461 | 118.705 | |
| Cu/Pb CONC | 236.0 | 6.02 | 0.403 | 173.833 | | | 2.431 | 1047.299 | |
| Cu/Pb 2nd CL TAIL | 28.3 | 0.72 | 0.134 | 81.474 | | | 0.097 | 58.862 | |
| Cu/Pb 1st CL CONC | 264.3 | 6.75 | 0.375 | 163.944 | | | 2.528 | 1106.161 | |
| Cu/Pb 1st CL TAIL | 213.5 | 5.45 | 0.092 | 19.622 | | | 0.501 | 106.947 | |
| Cu/Pb RO CONC | 477.8 | 12.20 | 0.248 | 99.455 | | | 3.029 | 1213.107 | |
| Zn CONC | 497.4 | 12.70 | 0.070 | 8.278 | | | 0.889 | 117.811 | |
| Zn 2nd CL TAIL | 86.7 | 1.76 | 0.144 | 8.790 | | | 0.245 | 14.967 | |
| Zn 1st CL CONC | 564.1 | 14.40 | 0.073 | 9.220 | | | 1.134 | 132.778 | |
| Zn 1st CL TAIL | 160.4 | 4.08 | 0.078 | 4.274 | | | 0.319 | 17.501 | |
| Zn RO CONC | 724.5 | 18.50 | 0.079 | 8.125 | | | 1.453 | 150.280 | |
| TAIL | 2714.9 | 69.31 | 0.040 | 1.868 | | | 2.772 | 129.465 | |
| CALC HEAD | 3917.2 | 100.0 | 0.073 | 14.928 | | | 7.255 | 1492.852 | |
| | | | | | | | | 100.00 | 100.00 |

TESTWORK PROCEDURE

Test No. 6891-10F11

Locked Cycle

| STAGE | TIME (min) | ADDITIONS | |
|---|---------------|-------------------------------------|--|
| | | lb/ton | REAGENT |
| GRIND | 11 | 0.25 1.0 0.5 0.02 | NaCN Na ₂ SO ₃ pH = 6.2 ZnSO ₄ Z-200 |
| RECYLE CU/PB 2ND CLEANER TAIL | | | |
| CU/PB ROUGHER | 10 | 0.03 0.05 | Aero 238 MIBC pH = 5.7 |
| RECYLE CU/PB 1ST & 2ND CLEANER TAIL | | | |
| ZN CONDITION | 5 5 | 6.67 0.6 0.1 0.03 0.075 | Lime to pH = 10.5 CuSO ₄ NaCN Z-200 Aero 343 |
| ZN ROUGHER | 8 | 0.04 | DF1012 |
| CU/PB CONDITION | 5 | 2.0 1.0 0.1 0.02 | Na ₂ SO ₃ ZnSO ₄ NaCN Z-200 |
| CU/PB 1ST CLEANER | 10 | | |
| CU/PB 2ND CLEANER | 7 | 1.0 | Na ₂ SO ₃ |
| ZN CONDITIONS | 5 | 0.36 | Lime to pH 10.8 |
| ZN 1ST CLEANER | 6 | 0.175 0.03 0.20 0.02 | NaCN Z-200 CuSO ₄ Aero 343 |
| ZN 2ND CLEANER | 5 | 0.38 | Lime to pH 11.5 |

TESTWORK PROCEDURE

Test No. 6891-10F11

Cu/Pb Separation

| STAGE | TIME (min) | ADDITIONS | |
|----------------------|---------------|---------------|------------------------|
| | | lb/ton | REAGENT |
| CONDITION | 20 | 0.11 0.11 | Dextrin Carbon |
| CONDITION | 20 | 60 ml (6%) | Sulphurous to pH = 4.8 |
| SCREEN OUT CARBON | | | |
| COPPER FLOAT | 5 | 0.02 | Z-200 |

TEST NUMBER: 6891-10F11 FLOTATION OF COMPOSITE #2 - LOCKED CYCLE PAGE 2

| PRODUCT | WEIGHT GMS | WEIGHT % | ASSAYS | | | | | % DIST | | | | |
|-------------------|------------|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | Cu% | Pb% | Zn% | Fe% | Insol% | Cu | Pb | Zn | Fe | Insol |
| Cu/Pb CONC #1 | 115.1 | 0.96 | 13.450 | 22.740 | 10.360 | 10.380 | | 11.01 | 11.63 | 1.23 | 0.78 | |
| Cu/Pb CONC #2 | 92.1 | 0.77 | 13.760 | 22.960 | 8.110 | 11.490 | | 9.01 | 9.39 | 0.77 | 0.69 | |
| Cu/Pb CONC #3 | 163.1 | 1.36 | 13.600 | 26.400 | 8.800 | 10.100 | | 15.78 | 19.13 | 1.48 | 1.08 | |
| Cu/Pb CONC #4 | 122.0 | 1.02 | 14.560 | 26.240 | 13.440 | 12.900 | | 12.64 | 14.22 | 1.70 | 1.03 | |
| Cu/Pb CONC #5 | 147.0 | 1.22 | 13.440 | 23.520 | 10.240 | 13.000 | | 14.05 | 15.36 | 1.56 | 1.25 | |
| Cu CONC #6 | 53.7 | 0.45 | 27.600 | 5.200 | 8.080 | 12.700 | | 10.54 | 1.24 | 0.45 | 0.45 | |
| Pb CONC #6 | 58.9 | 0.49 | 5.200 | 43.600 | 10.000 | 8.700 | | 2.18 | 11.41 | 0.61 | 0.34 | |
| Cu/Pb CONCS | 112.6 | 0.94 | 15.863 | 25.287 | 9.084 | 10.608 | | 12.72 | 12.65 | 1.06 | 0.78 | |
| TOTAL Cu/Pb CONCS | 751.9 | 6.26 | 14.063 | 24.663 | 10.031 | 11.410 | | 75.21 | 82.38 | 7.80 | 5.63 | |
| Cu/Pb 2nd CL TAIL | 39.0 | 0.32 | 9.200 | 8.600 | 13.200 | 12.100 | | 2.55 | 1.49 | 0.53 | 0.31 | |
| Cu/Pb 1st CL TAIL | 90.4 | 0.75 | 4.640 | 0.800 | 17.120 | 10.700 | | 2.98 | 0.32 | 1.60 | 0.63 | |
| Zn CONC #1 | 229.9 | 1.92 | 0.700 | 0.630 | 47.220 | 7.830 | 3.480 | 1.14 | 0.64 | 11.23 | 1.18 | 11.26 |
| Zn CONC #2 | 279.6 | 2.33 | 0.830 | 0.730 | 46.130 | 7.600 | 3.920 | 1.65 | 0.91 | 13.34 | 1.39 | 15.43 |
| Zn CONC #3 | 267.8 | 2.23 | 1.120 | 0.760 | 53.600 | 6.400 | 3.660 | 2.13 | 0.90 | 14.85 | 1.12 | 13.80 |
| Zn CONC #4 | 228.6 | 1.90 | 1.240 | 0.680 | 48.800 | 6.000 | 8.840 | 2.02 | 0.69 | 11.54 | 0.90 | 28.44 |
| Zn CONC #5 | 310.6 | 2.59 | 1.120 | 0.520 | 56.000 | 5.200 | 3.900 | 2.47 | 0.72 | 17.99 | 1.06 | 17.05 |
| Zn CONC #6 | 226.5 | 1.89 | 1.440 | 0.800 | 53.600 | 6.700 | 4.400 | 2.32 | 0.81 | 12.56 | 1.00 | 14.03 |
| TOTAL Zn CONCS | 1543.0 | 12.86 | 1.070 | 0.681 | 51.068 | 6.574 | 4.605 | 11.74 | 4.67 | 81.52 | 6.66 | 100.00 |
| Zn 2nd CL TAIL | 63.5 | 0.53 | 0.560 | 0.600 | 27.200 | 9.400 | | 0.25 | 0.17 | 1.79 | 0.39 | |
| Zn 1st CL TAIL | 245.6 | 2.05 | 0.220 | 0.370 | 12.960 | 11.200 | | 0.38 | 0.40 | 3.29 | 1.80 | |
| TAIL #1 | 1441.3 | 12.01 | 0.100 | 0.270 | 0.220 | 14.470 | | 1.03 | 1.73 | 0.33 | 13.68 | |
| TAIL #2 | 1528.9 | 12.74 | 0.096 | 0.280 | 0.310 | 13.320 | | 1.04 | 1.90 | 0.49 | 13.36 | |
| TAIL #3 | 1608.6 | 13.40 | 0.100 | 0.270 | 0.500 | 13.200 | | 1.14 | 1.93 | 0.83 | 13.93 | |
| TAIL #4 | 1459.6 | 12.16 | 0.120 | 0.240 | 0.450 | 14.400 | | 1.25 | 1.56 | 0.68 | 13.79 | |
| TAIL #5 | 1644.5 | 13.70 | 0.110 | 0.250 | 0.340 | 14.900 | | 1.29 | 1.83 | 0.58 | 16.08 | |
| TAIL #6 | 1585.5 | 13.21 | 0.100 | 0.230 | 0.340 | 13.200 | | 1.13 | 1.62 | 0.56 | 13.73 | |
| TOTAL TAILS | 9268.4 | 77.22 | 0.104 | 0.257 | 0.361 | 13.908 | | 6.87 | 10.56 | 3.47 | 84.58 | |
| CALC HEAD | 12001.8 | 100.0 | 1.171 | 1.875 | 8.054 | 12.699 | 0.592 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6891-10F11 FLOTATION OF COMPOSITE #2 - LOCKED CYCLE PAGE 1

| PRODUCT | WEIGHT GMS | WEIGHT % | Au oz/ton | Ag oz/ton | ASSAYS | | Z DIST |
|--------------------|---------------|-------------|--------------|--------------|--------|----|---------------|
| | | | | | Au | Ag | |
| Cu/Pb CONC #1 | 115.1 | 0.96 | 0.476 | 173.384 | | | 6.72 11.21 |
| Cu/Pb CONC #2 | 92.1 | 0.77 | 0.478 | 195.250 | | | 5.40 10.11 |
| TCu/Pb CONC #3 | 163.1 | 1.36 | 0.262 | 160.944 | | | 5.24 14.75 |
| TCu/Pb CONC #4 | 122.0 | 1.02 | 0.282 | 171.164 | | | 4.22 11.73 |
| Cu/Pb CONC #5 | 147.0 | 1.22 | 0.374 | 155.350 | | | 6.75 12.83 |
| Cu CONC #6 | 53.7 | 0.45 | 0.590 | 301.446 | | | 3.89 9.10 |
| Pb CONC #6 | 58.9 | 0.49 | 0.292 | 71.568 | | | 2.11 2.37 |
| Cu/Pb CONC #6 | 112.6 | 0.94 | 0.434 | 181.199 | | | 6.00 11.47 |
| TOTAL Cu/Pb CONCS | 751.9 | 6.26 | 0.372 | 170.648 | | | 34.34 72.10 |
| TCu/Pb 2nd CL TAIL | 39.0 | 0.32 | 0.184 | 84.860 | | | 0.88 1.86 |
| Cu/Pb 1st CL TAIL | 90.4 | 0.75 | 0.058 | 20.910 | | | 0.54 1.06 |
| Zn CONC #1 | 229.9 | 1.92 | 0.098 | 9.910 | | | 2.77 1.29 |
| Zn CONC #2 | 279.6 | 2.33 | 0.084 | 11.454 | | | 2.88 1.80 |
| Zn CONC #3 | 267.8 | 2.23 | 0.074 | 13.624 | | | 2.43 2.05 |
| Zn CONC #4 | 226.6 | 1.90 | 0.052 | 13.366 | | | 1.46 1.72 |
| Zn CONC #5 | 310.6 | 2.59 | 0.052 | 12.216 | | | 1.98 2.13 |
| Zn CONC #6 | 226.5 | 1.89 | 0.068 | 16.138 | | | 1.89 2.05 |
| TOTAL Zn CONCS | 1543.0 | 12.86 | 0.071 | 12.725 | | | 13.41 11.03 |
| 2nd CL TAIL | 63.5 | 0.53 | 0.060 | 8.708 | | | 0.47 0.31 |
| Zn 1st CL TAIL | 245.6 | 2.05 | 0.056 | 4.236 | | | 1.69 0.58 |
| TAIL #1 | 1441.3 | 12.01 | 0.041 | 2.224 | | | 7.25 1.80 |
| TAIL #2 | 1528.9 | 12.74 | 0.040 | 2.208 | | | 7.51 1.90 |
| TAIL #3 | 1608.6 | 13.40 | 0.044 | 2.671 | | | 8.69 2.41 |
| TAIL #4 | 1459.6 | 12.16 | 0.044 | 2.738 | | | 7.88 2.25 |
| TAIL #5 | 1644.5 | 13.70 | 0.042 | 2.562 | | | 8.48 2.37 |
| TAIL #6 | 1585.5 | 13.21 | 0.045 | 2.605 | | | 8.76 2.32 |
| TOTAL TAILS | 9268.4 | 77.22 | 0.043 | 2.505 | | | 48.56 13.05 |
| ALC HEAD | 12001.8 | 100.0 | 0.068 | 14.827 | | | 100.00 100.00 |

TEST NUMBER: 6891-10F11 FLOTATION OF COMPOSITE #2 - LOCKED CYCLE PAGE 2

| PRODUCT | WEIGHT GMS | WEIGHT % | ASSAYS | | | | | % DIST | | | | |
|-------------------|------------|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | Cu% | Pb% | Zn% | Fe% | Insol% | Cu | Pb | Zn | Fe | Insol |
| Cu/Pb CONC #1 | 115.1 | 1.00 | 13.450 | 22.740 | 10.360 | 10.380 | | 11.74 | 11.91 | 1.33 | 0.81 | 0.00 |
| Cu/Pb CONC #2 | 92.1 | 0.80 | 13.760 | 22.960 | 8.110 | 11.490 | | 9.61 | 9.62 | 0.83 | 0.72 | 0.00 |
| Cu/Pb CONC #3 | 163.1 | 1.41 | 13.600 | 26.400 | 8.800 | 10.100 | | 16.82 | 19.60 | 1.60 | 1.12 | 0.00 |
| Cu/Pb CONC #4 | 122.0 | 1.06 | 14.560 | 26.240 | 13.440 | 12.900 | | 13.47 | 14.57 | 1.83 | 1.07 | 0.00 |
| Cu/Pb CONC #5 | 147.0 | 1.27 | 13.440 | 23.520 | 10.240 | 13.000 | | 14.98 | 15.74 | 1.68 | 1.29 | 0.00 |
| Cu CONC #6 | 53.7 | 0.46 | 27.600 | 5.200 | 8.080 | 12.700 | | 11.24 | 1.27 | 0.48 | 0.46 | 0.00 |
| Tb CONC #6 | 58.9 | 0.51 | 5.200 | 43.600 | 10.000 | 8.700 | | 2.32 | 11.69 | 0.66 | 0.35 | 0.00 |
| Cu/Pb CONC #6 | 112.6 | 0.97 | 15.883 | 25.287 | 9.084 | 10.608 | | 13.56 | 12.96 | 1.14 | 0.81 | 0.00 |
| TOTAL Cu/Pb CONCS | 751.9 | 6.50 | 14.063 | 24.663 | 10.031 | 11.410 | | 80.16 | 84.40 | 8.41 | 5.81 | 0.00 |
| Zn CONC #1 | 229.9 | 1.99 | 0.700 | 0.630 | 47.220 | 7.830 | 3.480 | 1.22 | 0.66 | 12.10 | 1.22 | 11.26 |
| Zn CONC #2 | 279.6 | 2.42 | 0.830 | 0.730 | 46.130 | 7.600 | 3.920 | 1.76 | 0.93 | 14.38 | 1.44 | 15.43 |
| Zn CONC #3 | 267.8 | 2.32 | 1.120 | 0.760 | 53.600 | 6.400 | 3.660 | 2.27 | 0.93 | 16.00 | 1.16 | 13.80 |
| Zn CONC #4 | 228.6 | 1.98 | 1.240 | 0.680 | 48.800 | 6.000 | 8.840 | 2.15 | 0.71 | 12.44 | 0.93 | 28.44 |
| Zn CONC #5 | 310.6 | 2.69 | 1.120 | 0.520 | 56.000 | 5.200 | 3.900 | 2.64 | 0.74 | 19.39 | 1.09 | 17.05 |
| Zn CONC #6 | 226.5 | 1.96 | 1.440 | 0.800 | 53.600 | 6.700 | 4.400 | 2.47 | 0.82 | 13.54 | 1.03 | 14.03 |
| TOTAL Zn CONCS | 1543.0 | 13.34 | 1.070 | 0.681 | 51.068 | 6.574 | 4.605 | 12.51 | 4.78 | 87.86 | 6.87 | 100.00 |
| TAIL #1 | 1441.3 | 12.46 | 0.100 | 0.270 | 0.220 | 14.470 | | 1.09 | 1.77 | 0.35 | 14.13 | |
| TAIL #2 | 1528.9 | 13.22 | 0.096 | 0.280 | 0.310 | 13.320 | | 1.11 | 1.95 | 0.53 | 13.79 | |
| TAIL #3 | 1608.6 | 13.91 | 0.100 | 0.270 | 0.500 | 13.200 | | 1.22 | 1.98 | 0.90 | 14.38 | |
| TAIL #4 | 1459.6 | 12.62 | 0.120 | 0.240 | 0.450 | 14.400 | | 1.33 | 1.59 | 0.73 | 14.24 | |
| TAIL #5 | 1644.5 | 14.22 | 0.110 | 0.250 | 0.340 | 14.900 | | 1.37 | 1.87 | 0.62 | 16.60 | |
| TAIL #6 | 1585.5 | 13.71 | 0.100 | 0.230 | 0.340 | 13.200 | | 1.20 | 1.66 | 0.60 | 14.18 | |
| TOTAL TAILS | 9268.4 | 80.15 | 0.104 | 0.257 | 0.361 | 13.908 | | 7.33 | 10.82 | 3.74 | 87.32 | |
| CALC HEAD | 11563.3 | 100.0 | 1.141 | 1.900 | 7.757 | 12.767 | 0.614 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |

TEST NUMBER: 6891-10F11 FLOTATION OF COMPOSITE #2 - LOCKED CYCLE PAGE 1

| PRODUCT | WEIGHT | WEIGHT% | Au | Ag | ASSAYS | | Au | Ag | % BIST |
|-------------------|---------|---------|--------|---------|--------|--|--------|--------|--------|
| | GMS | % | oz/ton | oz/ton | | | | | |
| Cu/Pb CONC #1 | 115.1 | 1.00 | 0.476 | 173.364 | | | 6.98 | 11.66 | |
| Cu/Pb CONC #2 | 92.1 | 0.80 | 0.478 | 195.250 | | | 5.61 | 10.51 | |
| Cu/Pb CONC #3 | 163.1 | 1.41 | 0.262 | 160.944 | | | 5.45 | 15.34 | |
| Cu/Pb CONC #4 | 122.0 | 1.06 | 0.282 | 171.164 | | | 4.38 | 12.20 | |
| Cu/Pb CONC #5 | 147.0 | 1.27 | 0.374 | 155.350 | | | 7.01 | 13.34 | |
| Cu CONC #6 | 53.7 | 0.46 | 0.590 | 301.446 | | | 4.04 | 9.46 | |
| Pb CONC #6 | 53.9 | 0.51 | 0.292 | 71.568 | | | 2.19 | 2.46 | |
| Cu/Pb CONC #6 | 112.6 | 0.97 | 0.434 | 181.199 | | | 6.23 | 11.92 | |
| TOTAL Cu/Pb CONCS | 751.9 | 6.50 | 0.372 | 170.648 | | | 35.66 | 74.96 | |
| Zn CONC #1 | 229.9 | 1.99 | 0.098 | 9.910 | | | 2.87 | 1.33 | |
| Zn CONC #2 | 279.6 | 2.42 | 0.084 | 11.454 | | | 2.99 | 1.87 | |
| Zn CONC #3 | 267.8 | 2.32 | 0.074 | 13.624 | | | 2.53 | 2.13 | |
| Zn CONC #4 | 228.6 | 1.98 | 0.052 | 13.366 | | | 1.51 | 1.79 | |
| Zn CONC #5 | 310.6 | 2.69 | 0.052 | 12.216 | | | 2.06 | 2.22 | |
| Zn CONC #6 | 226.5 | 1.96 | 0.068 | 16.138 | | | 1.96 | 2.14 | |
| TOTAL Zn CONCS | 1543.0 | 13.34 | 0.071 | 12.725 | | | 13.92 | 11.47 | |
| TAIL #1 | 1441.3 | 12.46 | 0.041 | 2.224 | | | 7.53 | 1.87 | |
| TAIL #2 | 1528.9 | 13.22 | 0.040 | 2.208 | | | 7.79 | 1.97 | |
| TAIL #3 | 1608.6 | 13.91 | 0.044 | 2.671 | | | 9.02 | 2.51 | |
| TAIL #4 | 1459.6 | 12.62 | 0.044 | 2.738 | | | 8.18 | 2.33 | |
| TAIL #5 | 1644.5 | 14.22 | 0.042 | 2.562 | | | 8.80 | 2.46 | |
| TAIL #6 | 1585.5 | 13.71 | 0.045 | 2.605 | | | 9.09 | 2.41 | |
| TOTAL TAILS | 9268.4 | 80.15 | 0.043 | 2.505 | | | 50.42 | 13.56 | |
| CALC HEAD | 11563.3 | 100.0 | 0.068 | 14.802 | | | 100.00 | 100.00 | |

APPENDIX II

Cyanidation Test of Pyrite Concentrate

CYANIDATION REPORT

Feed Description: File No.: 6891
 6891-10F4 Cycles 1-5 Test No.: 6891-C1
 Pyrite Conc Composite after
 regrinding to -400 mesh

Starting Conditions:

912 dry g. of feed
 1.368 ml. of water
 40 % solids
 2 gpl NaCN
 10.5 pH target

Test Progress:

| Time hr | NaCN | | Ca(OH) ₂ | | pH | O ₂ ppm |
|------------|-------------|---------------|---------------------|--------------------|----|-----------------------|
| | Conc g/l | Addition g | Conc g/l | Addition ml 10% | | |
| 0 | 2.00 | 2.74 | | | 10 | 9.5-10.6 |
| 0.5 | 0.00 | 2.74 | | | | 10.6 |
| 1 | 0.28 | 2.74 | | | | 11.6 |
| 2.5 | 0.10 | 6.84 | | | | |
| 4 | 0.45 | 6.22 | | | | |
| 5 | 3.38 | 2.22 | | | | |
| 6 | 4.20 | 1.09 | | | | |
| 20 | 2.88 | | | | | |
| 24 | 3.16 | | | | | |
| 48 | 2.56 | | 0.30 | | 41 | 11.2 |

Reagent Consumption: NaCN = 23.13 kg/t
 Lime = 0.65 kg/t

Reducing Power: RP = 2880 ml of N/10 KMnO₄ per
 1000 ml solution

Assay Results:

| Sample Time hr | Solids Assay | | Liquid Assay | | Extraction | |
|----------------------|--------------|-------------------------|--------------|--------|------------|-------------|
| | Gold g/t | Silver | Gold mg/l | Silver | Gold % | Silver % |
| 6 | | | 0.76 | 56.2 | 26.2 | 33.8 |
| 24 | | | 0.84 | 104.2 | 28.9 | 62.1 |
| 48 | | | 0.96 | 117.72 | 32.8 | 69.9 |
| Tail | 2.43 | 62.61 | | | 67.2 | 30.1 |
| Head | 3.65 | 207.74 (.106 oz/ton) | | | | |



PHONE (705) 652-3341
TELEX NO. 06962842
FACSIMILE NO. (705) 652-6365

October 30, 1987

Houston Metals Corporation
Suite 910-800 West Pender Street
Vancouver, B.C.
V6C 2X6

Attn: Mr. Adolf A. Petancic:

Enclosed please find the minutes of the meeting held at Lakefield with Mr. E.W.S. Ward and Mr. N.C. Croome. During the meeting the metallurgical results were reviewed and the final phase of the testwork proposed. So far we have defined a process by which separate copper, lead and zinc concentrates can be produced. Further work would be concentrated to optimize the results and to perform continuous locked cycle tests in order to generate data for a feasibility study, and to determine the effect of intermediate product recirculation on concentrates, grades and recoveries.

Mr. Croome pointed out that this testwork is not being performed on a representative sample (i.e. does not include vein No. 3 ore) and therefore standard tests should be carried out to define metallurgy on individual samples.

To date we have conducted 27 batch flotation tests at the total cost of \$22,000. In order to complete all metallurgical testing we would need an additional \$30,000. Please let me know if the budget for this testwork represents any problems.

Regards

LAKEFIELD RESEARCH

S. Bulatovic, P. Eng.
Chief Development Engineer

SB:jm

Encl.

c.c. Norman C. Croome
E.W.S. Ward

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,715

PART 1 OF 3

185 CONCESSION STREET, P.O. BOX 430 LAKEFIELD, ONTARIO, CANADA K0L 2H0

FILMED

MINUTES OF MEETING

Purpose: Silver Queen Metallurgy Review

- Present:
1. N.C. Croome, P. Eng., President
N.C. Croome and Associates Ltd.
on behalf of James Wade Engineering
 2. E.W.S. Ward, Metallurgical Consultant
on behalf of James Wade Engineering
 3. S.M. Bulatovic, P. Eng.
Lakefield Research

1. Testwork Review

1.1 Ore Samples

All laboratory testwork was carried out on the composite sample consisting of the following individual samples:

- a) No. 2 Vein = 3 parts
- b) F.W. Vein - 2750 Level = 2 parts
- c) F.W. Vein - 2600 Level = 1 part
- d) No. 3 extension = 2 parts
- e) No. 5 Vein = 1 part
- f) S.B. Vein = 1 part

The head assays of the composite sample were as follows:

| | |
|----------------|------------|
| Copper (Cu) | 1.60% |
| Lead (Pb) | 0.96% |
| Zinc (Zn) | 7.75% |
| Iron (Fe) | 16.20% |
| Sulphur (S) | 21.90% |
| Gallium (Ga) | 0.0018% |
| Germanium (Ge) | 0.0115% |
| Arsenic (As) | 0.66% |
| Gold (Au) | 2.16 g/t |
| Silver (Ag) | 546.00 g/t |

Mr. N.C. Croome and Mr. E. Ward pointed out that the composite sample on which laboratory testwork is being done is not representative because it does not include vein No. 3 ore which represents about 80% of the ore body. It was suggested that additional tests should be performed on individual samples. The individual samples from which the composite is prepared are still available. The weights of the individual samples remaining are as follows:

| | |
|----------------------|-------|
| No. 2 Vein | 96 kg |
| F.W. Vein 2750 Level | 52 kg |
| F.W. Vein 2600 Level | 21 kg |
| No. 3 Extension | 3 kg |
| No. 5 Vein | 20 kg |
| SB Vein | 49 kg |

1.2 Laboratory Testwork

A total of 27 laboratory tests were performed in which different treatment processes applicable to Silver Queen ore were examined.

This includes:

- a) Cu-Pb bulk flotation followed by Cu-Pb separation
- b) Cu-Pb-Zn bulk flotation and separation
- c) Sequential Cu-Pb-Zn flotation

Cu-Pb Bulk Flotation. Although good metallurgical bulk flotation results were obtained using this method the Cu-Pb separation represents a problem because of the presence of secondary copper minerals. Separation may only be possible with the use of extremely high dosages of lead depressant. Even under these conditions sharpness of separation is poor.

Sequential Cu-Pb-Zn Flotation. This method is more suitable for treatment of the Silver Queen ore and would provide a more stable circuit for the future plant. Using this method the following metallurgical results were obtained.

Metallurgical Results

| Product | Assays % | | | | | Cu | % Distribution | Pb | Zn |
|----------------|----------|-----|------|-------|------|------|----------------|-----|----|
| | Cu | Pb | Zn | Au | Ag | | | | |
| Cu Concentrate | 26.4 | 2.1 | 7.1 | 12.0 | 5617 | 76.0 | 10.0 | 4.0 | |
| Pb Concentrate | 1.2 | 5.5 | 6.0 | 115.0 | 5400 | 3.0 | 54.0 | 1.0 | |
| Zn Concentrate | 0.3 | 0.2 | 60.0 | 1.5 | 500 | 0.5 | 0.5 | 85 | |

The gold recovery in the copper plus lead concentrates was about 50%. Extra gold, about 15% was recovered in a germanium concentrate after zinc flotation. The remaining gold, about 35% is enclosed within pyrite. The silver recovery in the combined copper and lead concentrate was over 85%. 10% of the Ag reports to the zinc concentrate.

2. Gallium and Germanium Distribution

Most of the recoverable gallium reported to the copper lead and zinc concentrates (about 50%) the remaining 50% of the gallium reports to the zinc tailing. Germanium, however, is not associated with either copper or zinc minerals and 85% of the germanium reports to the zinc tailing. We have conducted germanium occurrence tests to determine if germanium is associated with pyrite or is a separate mineral. This data is not available yet. However, the germanium concentrate assayed 10.0 g/t gold and 2000 g/t silver. If germanium is not associated with pyrite it may be possible to recover germanium in a separate concentrate with extra gold and silver recovery.

3. Further Testwork

In order to optimize the treatment method and further improve metallurgical results the following work would be required.

1. Conduct 5 batch tests on the composite to optimize the reagent scheme and flowsheet.
2. Conduct 15 tests on individual samples using the developed procedure to determine the metallurgical responses of the individual samples to the standard procedure developed.
3. Conduct two locked cycle tests to determine the effect of intermediate product recirculation and to generate data for feasibility.
4. Conduct preliminary roasting tests on copper concentrate to determine if the arsenic can be removed from the concentrate along with mercury.

Minutes of Meeting Lakefield Research, October 25, 1987

| | | |
|----------------|-----------------------------|--|
| Those present: | S. Bulatovic, P.Eng. | Chief Development Engineer Lakefield Research |
| | R. S. (Bob) Salter, PhD. | General Manager, Lakefield Research |
| | E. W. S. Ward | Metallurgist, James Wade Engineering |
| | N. C. Croome | Project Manager, James Wade Engineering |

The testwork to be conducted by Lakefield Research:

- (1) to develop a process by which separate Copper, Lead and Zinc concentrates can be produced
- (2) maximize Germanium and Gallium recoveries in either the copper concentrate or zinc concentrate.

A series of tests have been conducted to optimize:

- (1) Different treatment processes, ie. bulk float, sequential flotating minerals
- (2) reagent consumption and material balances
- (3) grinding characteristics.

A total of 27 tests have been completed to date and it was determined that sequential flotation was possible, as a separation of copper lead float was not recommended, a copper concentrate, lead concentrate and a zinc concentrate was possible.

Approximate results were:

Copper Concentrate containing:

26 percent copper
2.2 percent lead
with a 75 percent recovery.

Lead Concentrate containing:

45-65 percent lead, expected to average
55% with a 50 percent recovery

Zinc Concentrate containing:

62-63 percent zinc with a plus 80% recovery.

Approximately 70 percent the precious metals Gold and Silver report to the Copper and Lead concentrates.

S. Bulatovic, of Lakefield Research, is of the opinion that a germanium concentrate, which contains a large percentage of the remaining precious metals, can be produced from the remaining pyrite tails. Very preliminary testing indicates that the germanium can be floated and a separate germanium concentrate can be prepared. While the quantity of concentrate is relatively small, preliminary testing shows it to contain up to 5 Troy ounces per ton Gold and 10 Troy ounces per ton Silver. The present price of germanium is approximately \$140 U.S. per pound. World scarcity and demand indicates an increase in its value which would add materially to the overall value of the Silver Queen ore.

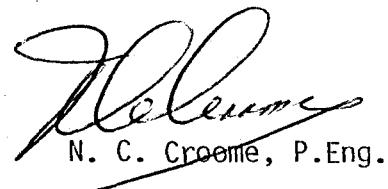
The arsenic reports to the copper concentrate giving up to 8 percent. There are several methods for roasting the copper concentrates to rid them of the arsenic. The economics of inclusion of a small roasting circuit is doubtful when consideration of the tonnages and capital costs involved.

Lakefield suggests additional flotation tests to optimize the results of the flotation tests to date, which would include an additional 15 tests and 2 locked-cycle tests. The preliminary testing program will be completed by mid December. However, the sample being used by Lakefield does not contain any ore from the No. 3 Vein and hence cannot be considered as truly representative of the average grade of ore in the mine as a large percentage of the proven and probable ore is in

the No. 3 Vein. In order to get a more representative sample for testing, it will be necessary to ship from the mine 20 kilos of average ore from No. 3 Vein and 20 kilos of ore which will have an average grade similar to that of the ore reserves. If these samples can be shipped by air freight to Lakefield in the near future, the information obtained from this testing can be included in the overall results for the mid December report. The data obtained will approximate that which can be anticipated for the treatment of ores from the mine.

For the purposes of a pre-feasibility study, these results can be averaged and projected to give a reasonable degree of confidence for the ultimate results.

For the Phase II Detailed Feasibility Study, it is recommended that Lakefield Research conduct a pilot plant study, treating 200 tons of ore from the Silver Queen property. The estimated cost of the program is estimated at \$340,000 plus cost of mining and rail freight.



N. C. Croome, P.Eng.