SUMMARY REPORT

1987 EXPLORATION PROGRAM

CRONIN MINE PROJECT

Omineca Mining Division
Latitude 54°55' Longitude 126°50'
NTS Map Sheet 93L/15W

Stephen P. Quin
Mining Geologist

for

SOUTHERN GOLD RESOURCES LTD.
Suite 220 - 145 Chadwick Court
North Vancouver, British Columbia
V7M 3K1

9 November, 1987

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1. INTRODUCTION

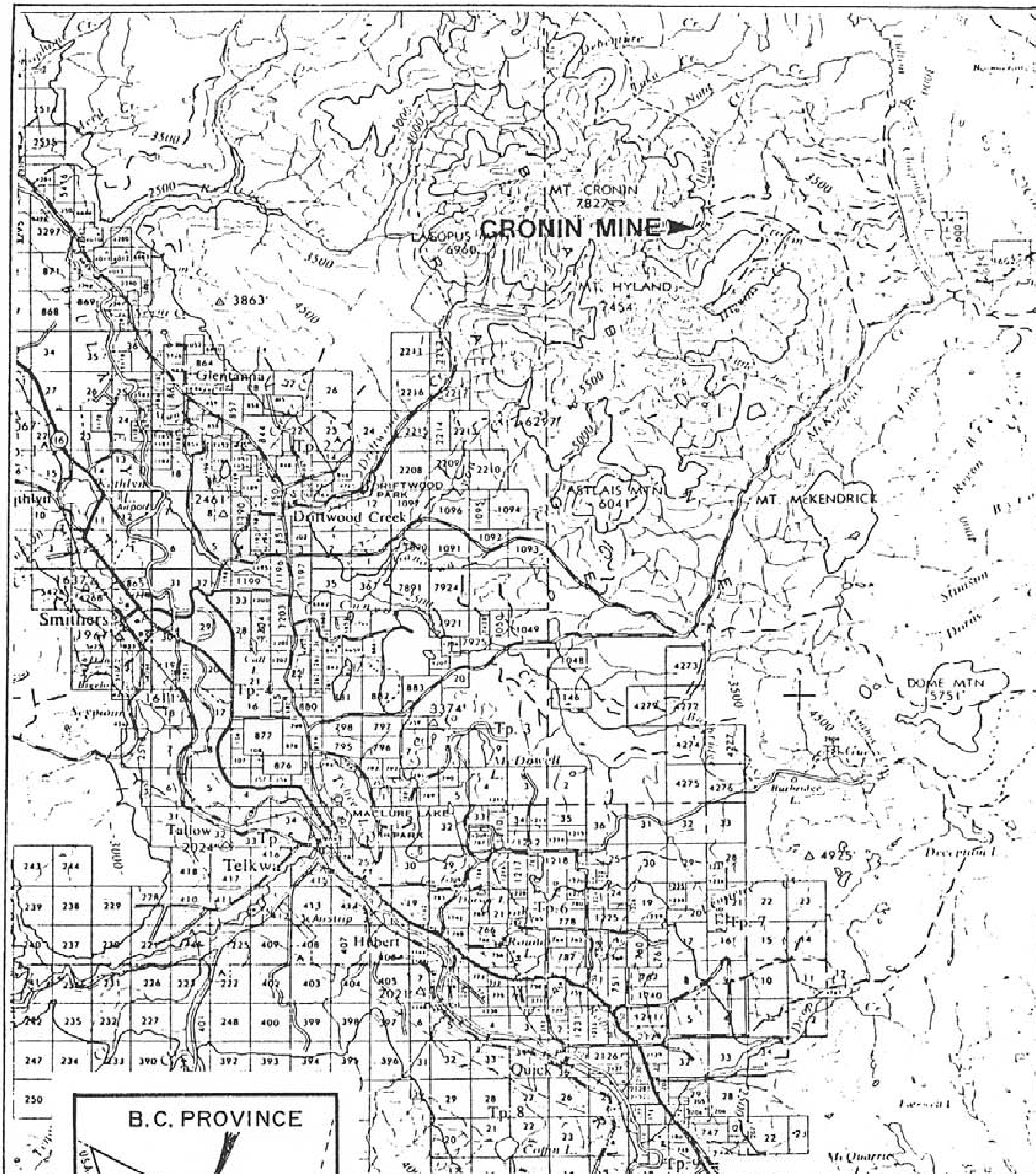
The Cronin Mine property consists of approximately 800 hectares of Crown Grants and located mineral claims 28 kilometers north east of Smithers in central British Columbia. An option on the property was acquired by Southern Gold Resources early in 1987 and a program of exploration was conducted during the months of July and August 1987.

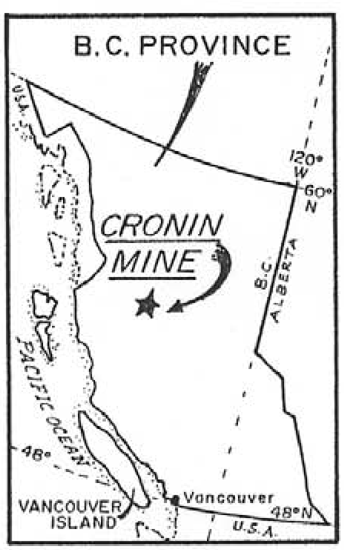
The Cronin Mine is underlain by Jurassic and Cretaceous sediments and intruded by a felsic body dated at 49 ma. Andesitic volcanics of the Brian Boru formation overthrust from the west. Polymetallic sulphide mineralization, principally lead, zinc and silver, lies at the margins of this intrusion and is probably genetically related to it. Sporadic production has occurred from these sulphide bodies since their discovery in 1905 until 1977. The 1987 exploration program was designed to evaluate the potential for hosting economic reserves of mineralization on the property as a whole, utilizing conventional exploration techniques including geology, geophysics and geochemistry.

2. LOCATION & ACCESS

The Cronin Mine lies on the east flanks of Mount Cronin, approximately 28 kilometers northeast of the town of Smithers in central British Columbia. The centre of the property lies at an approximate latitude of 54°55' and a longitude of 126°50' within NTS Map Sheet 93L/15W. Much of the property lies on the northern slopes of the valley drained by Cronin Creek (see Figure 1).

The property is reached via 10 kilometers of 4-wheel drive road that leaves the unpaved Babine Highway at kilometre 32. The Babine Highway leaves Provincial Highway 16 approximately 5 kilometers south of the town of Smithers, B.C. The 4-wheel drive access road required minimal rehabilitation to the mill site, but a large slide had to be cleaned out approximately 1 kilometre above the mill, to give access to the mine site. A small bridge used to cross Cronin Creek at approximately kilometre 10 on the access road is in fairly poor condition and only suitable for light vehicles. A ford adjacent to the bridge was used by heavier equipment, such as the bulldozer. This bridge would have to be replaced to permit heavy vehicles to drive to the mine site.





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CRONIN MINE PROPERTY

LOCATION MAP

SCALE 1:250,000
0 5 10 Km

Work by :		N.T.S. :	93/15
Drawn by :		Date :	OCT. 1987
			FIGURE 1

3. TOPOGRAPHY & CLIMATE

The Cronin Mine property lies on the eastern flanks of the Babine Range, which reach elevations in excess of 2,375 metres in the vicinity of the property. Within the property boundaries, topography is moderately steep, rising from 1,000 metres to alpine flats at 1,700 metres and above. The western end of the property is somewhat more rugged and reaches elevations of 2,100 metres. The majority of the old workings lie between 1,450 metres and 1,600 metres and the mill is at 1,100 metres.

The lower slopes are generally unstable, with extensive evidence for slides, both recent and ancient. Widespread down slope creep appears common. These slopes are heavily forested with spruce, balsam and fir, generally well past maturity, with abundant windfall and snags. The vegetation on the upper slopes consists largely of alpine meadow and patches of juniper, rising to exposed rock and talus at the uppermost elevations of the property. Permanent snow covers some areas and glaciers are found west of the property.

The climate is typical of interior mountain ranges, with heavy winter snowfalls, some persisting into August and September. Spring and early summer tend to be clear and dry while low cloud cover and squalls are not uncommon in the later summer.

4. PROPERTY & OWNERSHIP

The property consists of eight Crown Grants, one reverted Crown Grant, 23 two-post located claims and one modified grid claim. All the Crown Grants and reverted Crown Grants have been surveyed and the data is available in Victoria, B.C. Several claim posts were located in the field. All claims are listed below and shown on Figure 2.

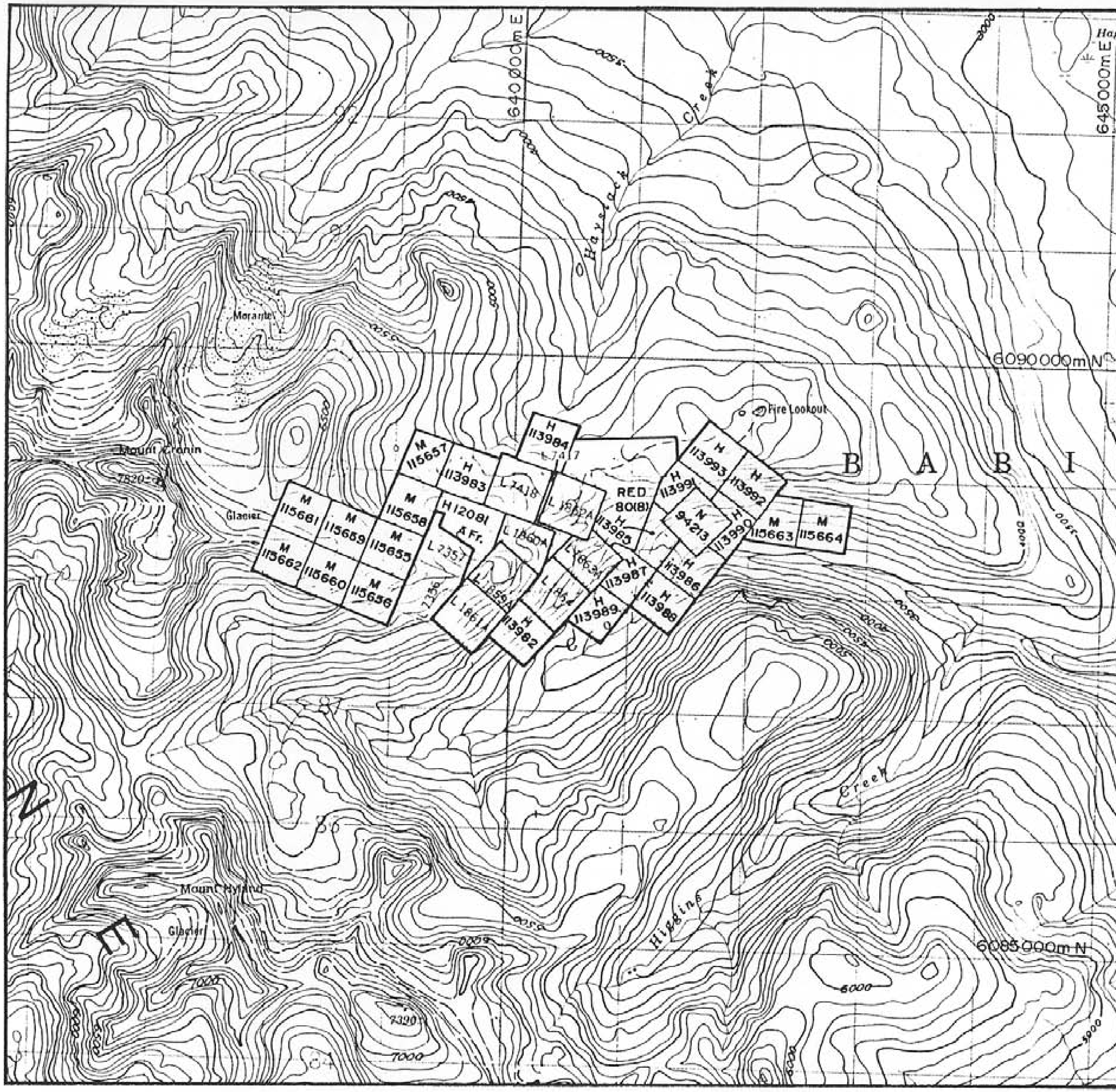
TABLE 1: CLAIM DATA

Claim Name	Type*	Record #	Lot #	Record Date (D-M-Y)
Sunflower	CG	N/A	7418	N/A
Sunflower Fr	CG	N/A	7417	N/A
Homestake	CG	N/A	1859	N/A
Bonanza	CG	N/A	1860	N/A
Eureka	CG	N/A	1861	N/A
Lucky Strike	CG	N/A	1862	N/A
Babine Chief	CG	N/A	1863	N/A
Bulkley Pioneer	CG	N/A	1864	N/A
Sunrise #7	RCG	94213	N/A	30-10-1970
Jim A Fr	2P	12081	N/A	11- 7-1958
Del #1-12	2P	113982-93	N/A	27- 7-1972
View #1-8	2P	115655-62	N/A	6- 9-1972
Mill #1	2P	115663	N/A	6- 9-1972
Mill #2	2P	115664	N/A	6- 9-1972
Red	MG	80	N/A	18- 8-1975

*Types of Claims: CG = Crown Grant
RCG = Reverted Crown Grant
MG = Modified Grid
2P = Two Post

The claims are all grouped together as the Cronin #2 Group. All mineral claims are registered in the name of Southern Gold Resources Ltd., while the Crown Grants are held by Hallmark Resources Ltd., subject to the terms of the option agreement dated April 1, 1987 between Hallmark Resources Ltd., Barnes Resources Inc. and Kindrat Mines Ltd. Under the terms of the agreement Barnes has the sole and exclusive right to earn up to a 51% undiluted interest in the Cronin Property. Barnes assigned its rights under this option agreement to Southern Gold Resources Ltd. in an assignment agreement dated 14 September 1987.

The property lies within the Babine Recreational Area and accordingly a Resource Use Permit must be obtained under the Park Act before commencing work on the property. A Resource Use Permit (#1537) was issued on July 1, 1987 which permits use and maintenance of existing roads, trenching, rehabilitation of old mine portals and geophysical and geochemical work.



TOPOGRAPHICAL BASE FROM 1:50,000 SERIES

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CRONIN MINE PROPERTY

CLAIM MAP

Scale 1:50,000
0 500 1000 2000 3000m

Work by :		N.T.S. :	93 L / 15
Drawn by :	RAM N. GOPAL	Date :	OCTOBER 1987
			FIGURE 2

5. HISTORY

The Cronin Mine has had a fairly extensive history that has been well documented elsewhere (e.g. Livgard 1972, Trenholme 1977) and is summarized below from a variety of sources.

1905 Discovery by prospectors from Hazelton

1908 Property purchased by James Cronin

1908 - 1925 Mr. J. Cronin develops the mine with approximately 4000 feet of lateral workings at a cost of approximately $250,000. Mr. Cronin considered he had the property ready for mill construction at his untimely death in 1925.

1928 The property was obtained from Mr. Cronin's estate and Babine Bonanza Metals Ltd. was formed but the onset of the depression halted further work.

1948 New Cronin Babine Mines Ltd. was formed and constructed a 50 ton per day mill.

1952 Production commenced, producing over 3,000 tons before shutting down due to low metal prices.

1956 Mining and milling resumed, producing over 10,000 tons.

1970 Mr. P. Kindrat purchased the property and continued production.

1971 Property optioned from Kindrat by Messrs. J. Wilson, F. Messner and M. Messner.

1972 The option along with adjoining claims held by the Messners was assigned to Hallmark Resources Ltd.

1973 Hallmark refurbished the mill and camp and placed the property back into production, milling over 1800 tons of ore. Prospecting identified several new veins.

1974 Drifting along the #1 level.

1975 Property optioned to Coca Minerals Ltd. who were looking for bulk tonnage open pittable reserves. They drilled 10 surface diamond holes totalling 1,530 metres into the Wardell Zone identifying a small high grade body of mineralization, but no large tonnage body. The option was terminated.

1977 Underground work on the Cronin Mine, including drifting and raising. Detailed underground mapping and channel sampling and surface mapping completed.

1980 - 1981 Small amount of underground work took place on the #1 level.

1983 Goldsil Mining & Milling Inc. optioned the property. Extensive underground sampling and some surface diamond drilling; 14 holes totalling 1,582 feet. This work confirmed and improved the reserves previously known.

1987 Southern Gold Resources Ltd. acquires an option on the property.

Production is summarized following, based on MINFILE, property reference #093L 127.

TABLE 2: PUBLISHED PRODUCTION DATA

Year	Tonnes Mined	Tonnes Milled	Gold (grams)	Silver (grams)	Copper (Kg)	Lead (Kg)	Zinc (Kg)	Cadmium (Kg)
1917	72	0	0	132,405	0	26,064	0	0
1929	27	0	0	21,368	0	6,214	7,765	0
1951	55	0	93	62,486	0	12,789	16,162	0
1952	3,184	0	871	740,998	0	121,867	128,133	1,702
1956	3,810	3,810	1,244	1,436,554	0	294,727	275,443	3,457
1957	5,368	5,368	1,959	2,072,237	8,092	317,033	384,805	4,891
1958	112	0	187	191,874	0	31,969	30,909	0
1959	907	0	342	302,197	0	49,013	36,910	440
1960	921	0	498	281,607	0	41,603	34,474	430
1961	1102	0	467	360,266	0	53,054	48,364	625
1963	328	328	218	108,798	0	14,037	18,809	255
1964	454	454	249	170,227	0	27,649	41,592	476
1965	703	703	156	379,892	0	63,472	88,967	1,167
1966	907	907	218	312,430	0	50,315	80,396	1,040
1967	680	680	187	145,407	0	33,595	47,523	495
1969	272	272	62	77,291	0	13,066	15,579	155
1970	1,584	1,584	840	367,015	0	50,508	53,243	650
1971	907	907	435	364,869	0	49,183	72,321	855
1972	907	635	311	275,728	0	44,946	47,642	557
1973	2,994	1,814	342	252,712	1,346	42,062	49,530	509
1974	544	544	93	113,557	956	23,212	39,314	308
TOTALS	25,838	18,006	8,772	8,169,918	10,394	1,367,178	1,517,881	18,012
IMPERIAL	28,480	19,800	282	262,672	22,914	3,014,127	3,346,372	39,709

This calculates to a recovered milled grade of 0.5 g/T gold, 454 g/T silver, 7.6% lead and 8.4% zinc.

6. RESERVES

A variety of reserve estimates have been made by several people and are presented below for reference. No attempt was made to evaluate the validity of these reserves during the 1987 field season. However, a brief inspection of the underground workings by the author did indicate significant tonnages are available for mining.

TABLE 3: ORE RESERVE ESTIMATES

Date	Classification	Metric Tons	Total	g/t Au	g/t Ag	%Pb	% Zn
12/1983	Indicated	317,000	317,000	1.7	354.4	8.0	8.0
08/1976	Measured Geological	45,400	45,400	N/A	428.1	8.0	8.0
06/1976	Measured Geological	45,360	45,360	N/A	428.1	7.0	8.0
03/1976	Indicated	42,413 }					
		}	159,901	N/A	428.1	7.11	8.12
05/1974	Inferred	117,448 }					
10/1972	Indicated	42,413 }					
		}	160,349	0.3	428.1	7.11	8.12
	Inferred	117,936 }					

These figures were obtained from MINFILE; property reference #093L 127.

7. GEOLOGY

7.1 Geological Setting

The most recent published mapping in the area was undertaken by T.A. Richards and H.W. Tipper on behalf of the Geological Survey of Canada during the period 1969 - 1971 and is published as GSC Open File #351. A part of this map is reproduced as Figure 3 for ease of reference. The area is currently being remapped by the British Columbia Department of Mines under the supervision of D. MacIntyre.

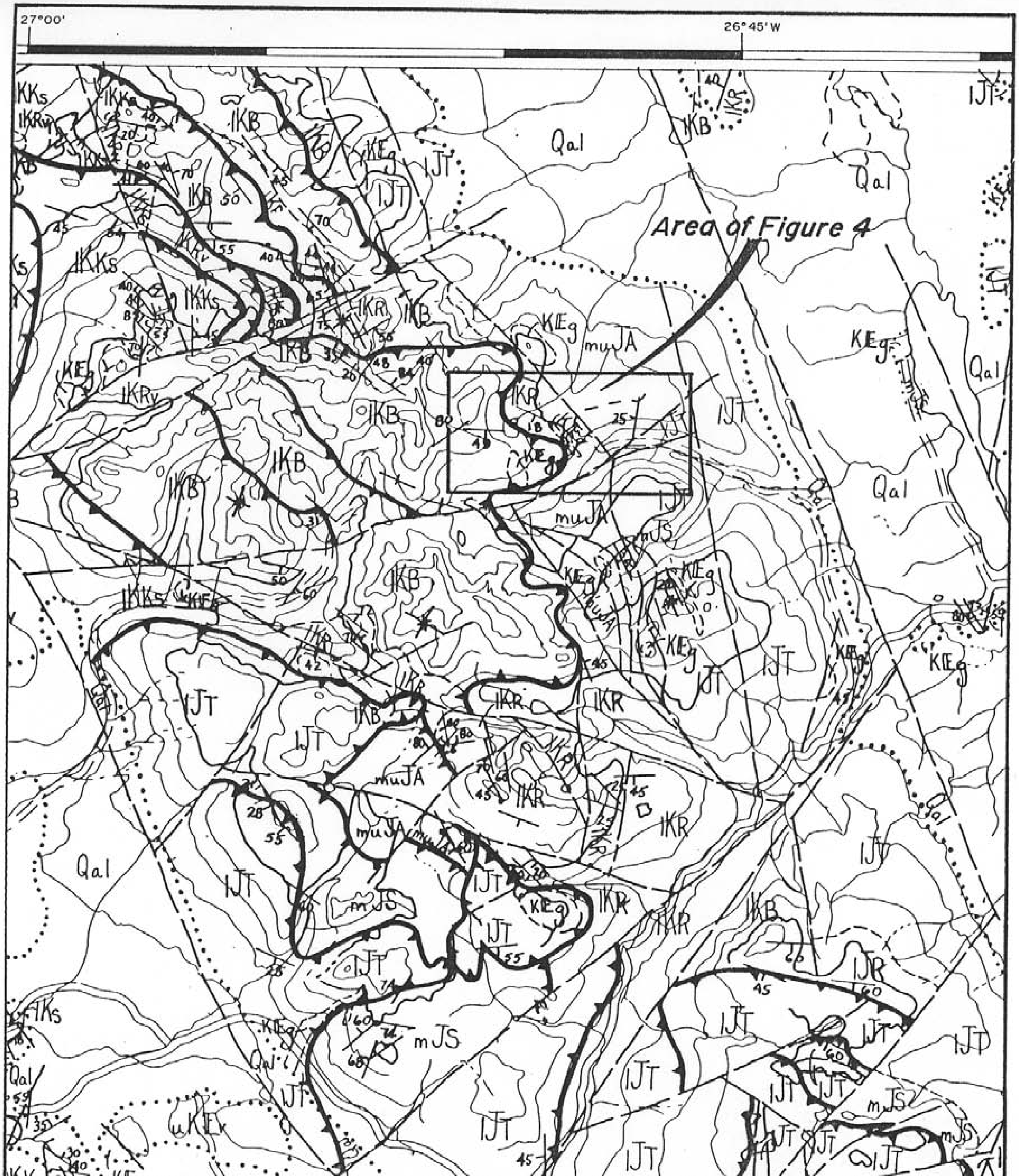
According to Tipper (1972):

> *"The Smithers map area is underlain by the Lower and Middle Jurassic essentially volcanic Hazelton Group, by the Middle and Upper Jurassic mainly sedimentary Bowser Lake Group, by the volcanic and sedimentary Lower Cretaceous Skeena Group, and by the Tertiary Volcanic Endako and Ootsa Lake Groups. The early Jurassic Topley Intrusions cut the lower part of the Hazelton Group and a variety of intermediate to acidic plutons of Late Cretaceous to Eocene age intrude most older units throughout the area. Structurally the area is dominated by a multitude of steep normal faults. Few contacts between map units are unfaulted and these are mainly intrusive or contacts between younger map units. Folding is common only in the few sedimentary units and is spatially and genetically related to the Eocene thrust faults."*

7.2 Property Geology

In the vicinity of the property, the principal rock types consist of the following, using Tipper and Richards nomenclature:

To the east lies the Jurassic Ashman Formation, part of the Bowser Lake Group, considered to be of Upper Bajocian to Lower Oxfordian age, and consisting of dark grey to black shale, quartzose sandstone, greywacke and chert pebble conglomerate. This is overlain to the west by Cretaceous sediments and volcanics of the Skeena Group; including the Red Rose and Brian Boru Formations. The Red Rose Formation is of Middle Albian age and comprises black to dark grey shale, chert pebble conglomerate and minor micaceous greywacke. In the vicinity of the rhyolite intrusives this unit is frequently intensely sericitized and highly foliated. The overlying Brian Boru Formation is overthrust from the west and is considered to be of Albian age or younger. It comprises of vari-coloured porphyritic tuffs, breccias and flows. In the field this unit is quite distinctive as a variety of fresh looking feldspar porphyry andesites, with phenocrysts ranging up to one centimetre, and volcanic agglomerates.



For LEGEND, see Figure

Source: Open File 351

SCALE 1:250,000

Mls 5 0 5 Mls

Kms 5 0 5 Kms

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CRONIN MINE PROPERTY

REGIONAL GEOLOGY

Work by :		N.T.S. :	93 L
Drawn by :		Date :	OCT. 1987
			FIGURE 3

SEDIMENTARY AND VOLCANIC ROCKS

QUATERNARY

PLEISTOCENE AND RECENT

Qal	alluvium, till, gravel

CRETACEOUS AND TERTIARY

OOTSA LAKE GROUP
MAESTRICHTIAN TO EOCENE

uKEv	acidic volcanics undivided; rhyolite and dacite flows, tuffs, and breccias; minor andesite; related felsite and porphyry intrusions

CRETACEOUS

SKEENA GROUP

ALBIAN AND/OR YOUNGER

lKB	lKB: BRIAN BORU FORMATION: vari-coloured porphyritic tuff, breccia, and flows

MIDDLE ALBIAN (mainly or entirely)

lKR / lKs	lKR: RED ROSE FORMATION : black to dark grey shale, chert pebble conglomerate; minor micaceous greywacke. lKs: micaceous greywacke, black to dark grey shale; minor conglomerate and coal

HAUTERIVIAN(?) TO ALBIAN(?)

lKRv	Rocky Ridge volcanics: dark green to rusty brown augite porphyry flows and breccias, rusty red tuff, and breccia, hornblende andesite, aphanitic basic flows

HAUTERIVIAN TO(?) ALBIAN

lKKs	Kitsun Creek sediments: coarse to fine polymictic conglomerate, greywacke, dark grey shale, coal; minor rusty red tuff related to Rocky Ridge volcanics

JURASSIC

BOWSER LAKE GROUP

UPPER BAJOCIAN TO LOWER OXFORDIAN

muJA	ASHMAN FORMATION: dark grey to black shale, quartzose sandstone, greywacke, and chert pebble conglomerate

HAZELTON GROUP

LOWER BAJOCIAN TO LOWER CALLOVIAN

mJs	SMITHERS FORMATION: grey-brown greenish-grey to drab grey greywacke, lithic sandstone, siltstone, shale, tuff breccia, grit, glauconitic sandstone; minor conglomerate

MIDDLE TOARCIAN(?)

lJR	NILKITKWA FORMATION RED TUFF MEMBER: red to brick red, fine-grained, tuff and fine breccia.

SINEMURIAN AND(?) LOWER PLIENSBACHIAN

lJT	TELKWA FORMATION: variegated red, maroon, grey green breccia, tuff, and flows of basaltic to rhyolitic composition

INTRUSIVE ROCKS

LATE CRETACEOUS AND EOCENE

KEg	undivided: quartz diorite, quartz monzonite and granodiorite, in part porphyritic, many small felsite plutons

SYMBOLS

Geological boundary (approximate) - - - - -

Drift boundary . . . .

Bedding (horizontal, inclined, vertical, overturned)

Faults and fault lineaments (approximate)

Thrust fault

Anticline

Syncline

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CRONIN MINE PROPERTY

LEGEND
FOR FIGURE 3

Work by :		N.T.S. :	93 L/15
Drawn by :		Date :	OCT. 1987
			FIGURE

These units are intruded by several high level rhyolite plugs of indeterminate age (See Figure 4). Tipper and Richards (1977) suggest they are Late Cretaceous to Eocene in age and have related rhyolite flows and breccias. Schroeter (1975) distinguishes two phases of rhyolite intrusive:

a) *"RHYOLITE PORPHYRY: Rhyolite porphyry is the most prominent part of the intrusive complex. It is grey, massive, medium to fine-grained porphyry with 20 to 40 per cent one by three-millimetre albite laths in an aphanitic groundmass of quartz, calcite, 'sericite', zoisite, and chloritoid.*

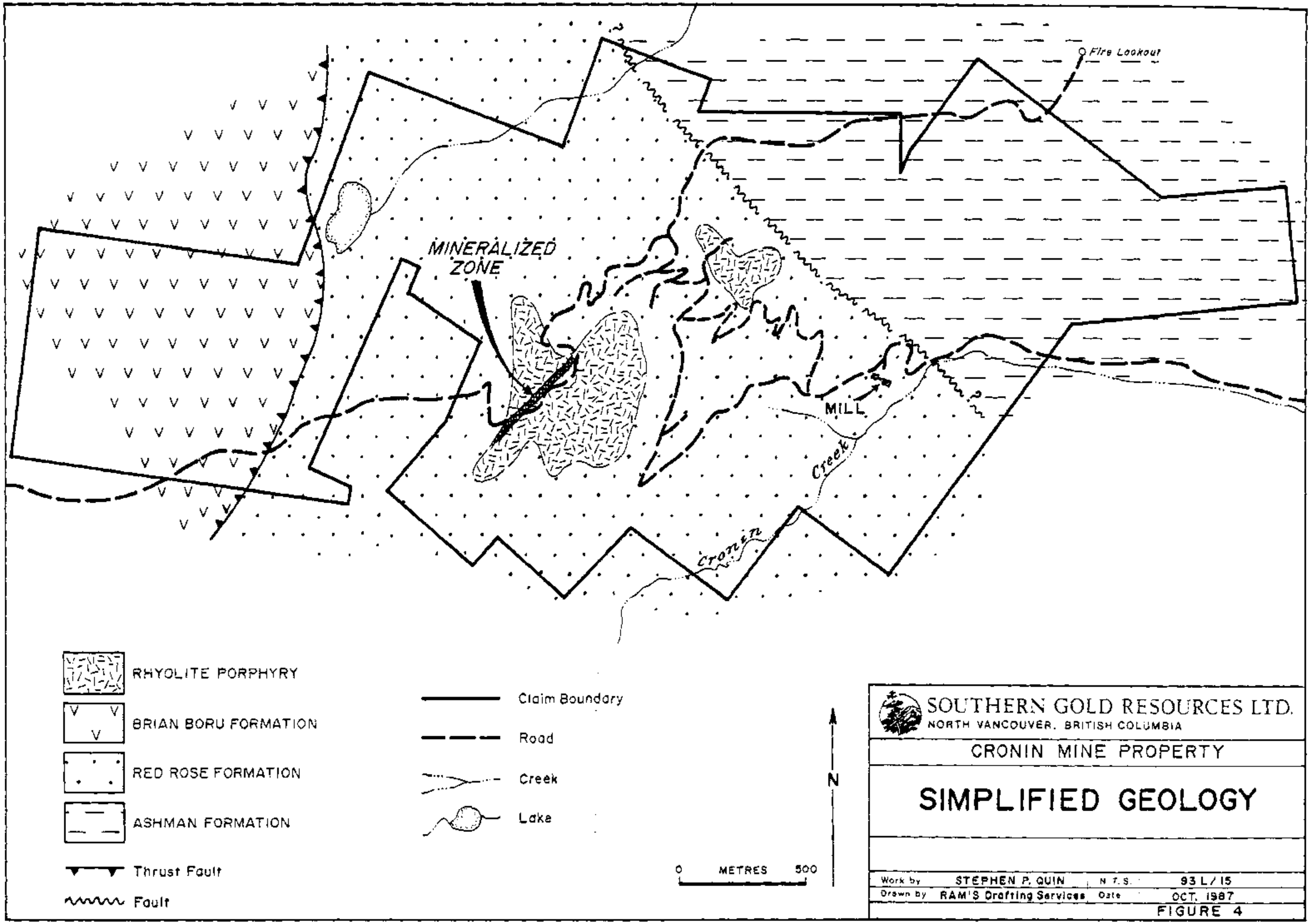
   There is no appreciable chilled margin where this unit is in contact with the sedimentary unit. A quartz stockwork exists within the rhyolite porphyry and this has been intruded by another rhyolite porphyry which has in turn been cut by a second phase of quartz veining. Quartz veinlets average 4 to 20 millimetres in width and carry variable amounts of sphalerite and galena.

   Silicification adjacent to quartz veins is the only significant alteration of this unit."

b) *"RHYOLITE: This strongly altered white to pale yellow unit intrudes the rhyolite porphyry. This unit is aphanitic for the most part, but may contain up to 15 per cent 1 to 2-millimetre quartz phenocrysts. Micro-sized quartz, 'sericite,' and calcite make up the bulk of the rock. Pyrite, sphalerite, and galena occur on dry fractures rather than in a quartz stockwork.*

   Both rhyolite units have undergone low-grade regional metamorphism."

The origin and nature of these rhyolites is a subject of considerable debate and has a bearing on the search for mineralization. Schroeter (1975) considers them intrusive plugs with dyke and sill intrusions into the surrounding sediments. Trenholme (1977) considers that the "rhyolite was intruded into the sedimentary strata during regional folding and that folding generated stresses continued after emplacement and crystallization of the intrusion". Scott and Ikona (1982), however, suggest the sediments are more accurately classified as epiclastic volcanic sediments (volcanic siltstones, sandstones and a sharpstone conglomerate containing fragments of rhyolite porphyry). Further, they suggest that the rhyolitic rocks comprise not only of a massive rhyolite porphyry but also rhyolitic lapilli tuffs and rhyolitic flows (or sills?) intercalated with the sedimentary package on the flanks of the massive rhyolite core. Scott and Ikona conclude that "the presence of the conglomerate and the lapilli tuffs within the epiclastic volcanic package suggests the emplacement of the rhyolite porphyry as a dome and the development of the epiclastic volcanics were contemporaneous. This is also supported by a lack of thermal metamorphism within the epiclastics which would be expected


Fire Lookout
MINERALIZED ZONE
MILL
Cronin
Creek
RHYOLITE PORPHYRY
BRIAN BORU FORMATION
RED ROSE FORMATION
ASHMAN FORMATION
Thrust Fault
Fault
Claim Boundary
Road
Creek
Lake
0 METRES 500
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SOUTHERN GOLD RESOURCES LTD.
NORTH VANCOUVER, BRITISH COLUMBIA
CRONIN MINE PROPERTY
SIMPLIFIED GEOLOGY
Work by STEPHEN P. QUIN N.T.S. 93 L/15
Drawn by RAM'S Drafting Services Date OCT. 1987
FIGURE 4

had the rhyolite porphyry been intruded into the 'sediments' as suggested by previous authors." Vollo (1987) generally supports this latter hypothesis and considers the area "a volcanic complex consisting of extrusive domes, coeval ash flows and synvolcanic intrusions" and "the enclosing sediments are partly of volcanic origin...".

A set of dykes of mixed composition (andesitic, quartz diorite, etc.), variably porphyritic, comprise the final intrusive event. They are post-stockwork and post mineral (Schroeter, 1975).

7.3 Mineralization

There are several types of mineralization on the property, mostly in close proximity to the rhyolite contacts. These types are:

a) Quartz-sulphide veins
b) Massive sulphides associated with a)
c) Breccia Zones
d) Dry fracture fillings (i.e. little or no quartz)
e) Trace dissemination in rhyolite.

Types a) and b) have been the principal sources of mill feed to date while the open pit target was type c). Scott and Ikona (1982) suggest the "overall stockwork appearance is consistent with 'stringer ore' in the feeder zone of a rhyolite dome which may have produced conformable massive sulphide lenses. The presence of the latter have not yet been confirmed as yet but in view of variations in the ore textures seen to date there is a distinct possibility that some of the major mineralized 'veins' may themselves be remobilized conformable massive sulphide lenses." Schroeter (1975) however, considers the sulphide mineralization to be contained in dilatent veins associated with quartz, in quartz stockworks plus types d) and e) mentioned above. He also notes the most common sulphide minerals, in order of abundance are:

Pyrite
Sphalerite
Galena
Chalcopyrite
Boulangerite
Tetrahedrite

Vollo (1987) notes that "most of the productive mineralized veins occur at the rhyolite-shale contact and are essentially conformable with the contact. On the 1st level, where the vein is entirely within rhyolite, it appears to be at the contact between two slightly different rhyolite units, and therefore also conformable. This suggests the 'veins' may be syngenetic, that is, deposited on the surface of the rhyolite and subsequently buried by succeeding flows, tuffs or sediments. They are frequently breccias, with angular fragments of vein material in a similar matrix, the fragments being matrix supported. This suggests that the 'veins' may have resulted *from the collapse of sinter chimneys to form breccia beds. They are also frequently coarsely banded, containing layers of shale or sulfides." The author has observed geological evidence in the field that would support both an intrusive and syngenetic origin for the rhyolites and an exhalative or a fissure vein style of mineralization. These evidences are discussed in more detail in Section 8.2 of this report.*

8. 1987 EXPLORATION PROGRAM

Exploration was conducted on the Cronin Mine property between 24th July and the 20th August 1987 by the author, assisted by two experienced field assistants; James Green and Pierre Mackenzie. This work was not intended to repeat the detailed underground and surface analyses conducted between 1972 and 1983 and extensively reported elsewhere (Livgard 1972, Trenholme 1976, Jones 1977, etc.) Rather, the 1987 exploration program was focussed on identifying new mineralized bodies in the vicinity of the known bodies and in other areas. Hence the program of exploration was conducted 'property wide'.

8.1 Access, Surveys

8.1.1 Road Access.

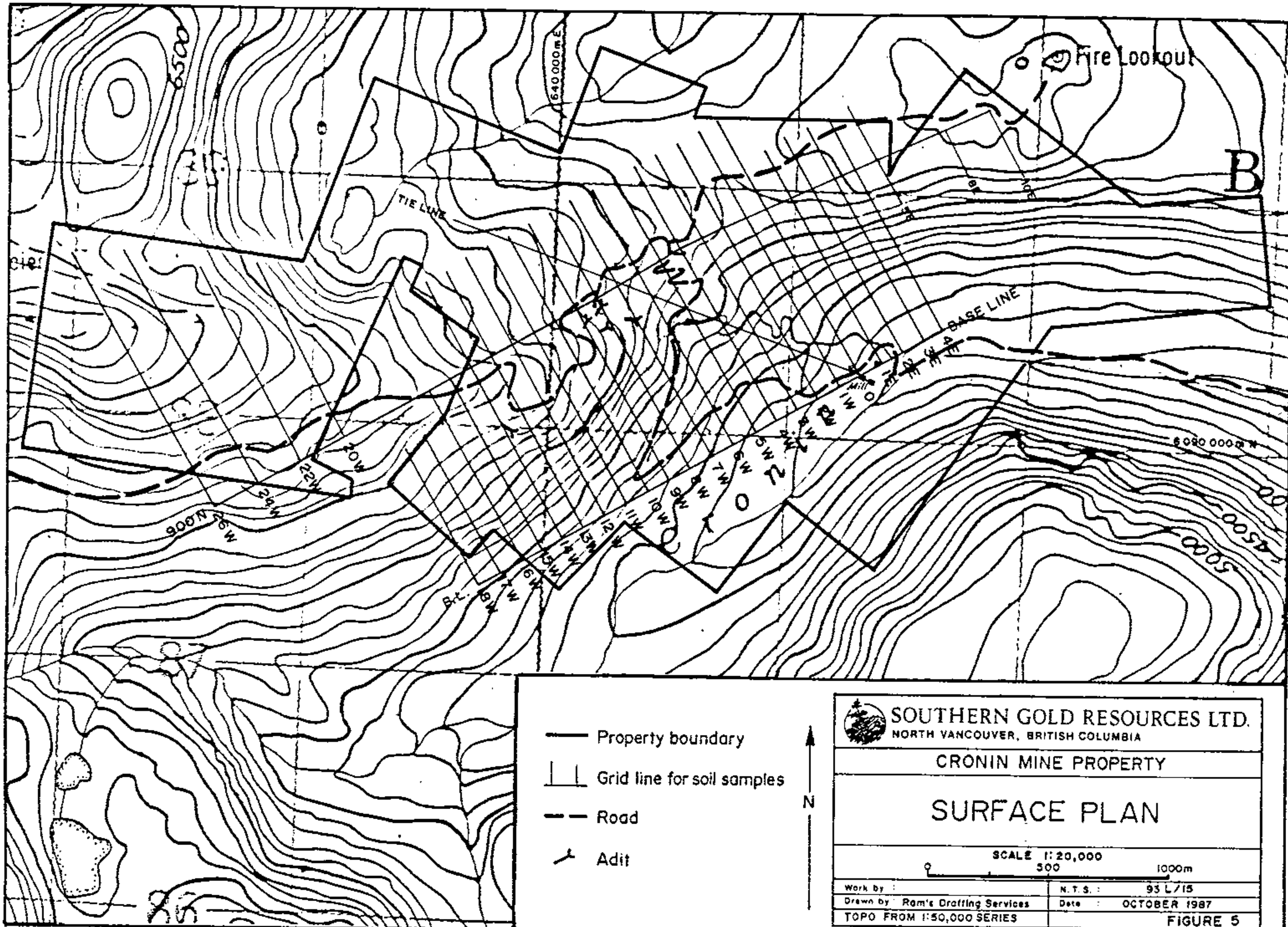
The access road from the Babine Highway to the mill site, a distance of approximately 10 kilometers, was in relatively good condition, if a little rough in places. However, a slide on the road from the mill site to mine site completely blocked access to the upper parts of the property. A D6 Cat bulldozer was contracted to 'clean-up' the main road a little and to regain access to the rest of the property. The bulldozer was required for a total of 46.5 hours.

8.1.2 Base Maps.

In order to have topographic and location control, a 1:5,000 scale topographic contour map and orthophoto base map were prepared by Eagle Mapping of Port Coquitlam, B.C. covering the entire property. Contours were scribed at 20m intervals due to the steep terrain.

8.1.3 Grid.

For greater control in the field a flagged grid was established over much of the property. The base line was run from the north end of the mill building a slope corrected distance of 1,800 metres to 250° and 400 metres to 070°, flagged in orange with 25m stations marked in blue. Cross lines were run every 100 metres and for varying distances to 340°, also flagged in orange with 25m stations marked in blue. Due to topographic constraints not all lines could be run their full distance, hence a second base line was run at 900m north, parallel to the main base line, from line 8+00W to 16+00W. This was later extended a further one kilometre to 26+00W to allow reconnaissance examination of the View Claims. Similarly a few short sections of line were added at 5+00E, 8+00E and 10+00E to allow follow-up work on an observed magnetic anomaly ending on line 4+00E. Total flagged grid exceeded 38 kilometers (see Figure 5).


Fire Lookout
B
TIE LINE
BASE LINE
640 000 m E
6 090 000 m N
6500
5000
4500
Mill
Property boundary
Grid line for soil samples
Road
Adit
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SOUTHERN GOLD RESOURCES LTD.
NORTH VANCOUVER, BRITISH COLUMBIA
CRONIN MINE PROPERTY
SURFACE PLAN
SCALE 1:20,000
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TOPO FROM 1:50,000 SERIES
N.T.S. : 93 L/15
Date : OCTOBER 1987
FIGURE 5

8.2 Geological Mapping

The grid area was reconnaissance mapped at a mapping scale of 1:5,000 utilizing a combination of the established grid and the orthophoto-contour map for orientation. Unfortunately, in several areas outcrop was extremely limited or inaccessible to mapping. These areas included the higher elevation alpine areas east of line 8+00W, the lower slopes of all lines below an elevation of approximately 1,300 metres and the precipitous cliffs of rhyolite porphyry between lines 8+00W and 14+00W. While the major contacts between formations were generally not well exposed, fairly distinct changes in lithology were observed in the field, particularly between the Brian Boru andesite porphyry and the Red Rose altered sediments and intrusive rhyolites. The change between the Red Rose and Ashman Formation sediments was much less distinct, although the Ashman Formation was more obviously sedimentary with evidence of graded bedding, fossils and conglomerates and, further, little or no evidence of the alteration that is common in the Red Rose Formation (see Figure 6).

8.2.1 Brian Boru Formation.

This was found to comprise almost entirely of feldspar porphyritic andesites, with a very fresh, unaltered appearance. They appear to represent a package of 1-10m thick flows at least 100m in total thickness in the grid area. They are generally flat lying to gently dipping southward. The feldspar phenocrysts consist of albite laths of varying sizes and forms that would allow the separation of the various units, if the time were taken to map them out. One unusual flow unit had numerous quartz filled vugs up to 10 cm across and could perhaps be used as a marker horizon in this formation.

8.2.2 Red Rose Formation.

This is the unit in contact with the rhyolite intrusives and hosting the mineralization. Since much of the area mapped that covers this formation was in relatively close proximity to the rhyolite intrusives and hence consisted almost entirely of the altered equivalents of the sedimentary and volcanoclastic lithologies that make up this formation. These were dominantly variously sericitized and chloritized schists. The most intense sericitization was generally in close proximity to the intrusives, but not exclusively so. For example, there are several occurrences of chlorite schists almost entirely enclosed in rhyolite (e.g. on lines 10+00W, 11+00W and 12+00W). The chloritization versus sericitization may therefore indicate original compositional differences or selective alteration in localized areas.

8.2.3 Ashman Formation.

Reportedly separated from the Red Rose Formation to the west by a fault (Tipper 1975). This unit was not entirely as described by previous authors. Much of the formation was clearly of sedimentary origin, mostly comprising of sandstones of a volcanic origin, particularly to the south or older part of the formation. These may represent epiclastic sediments of a more proximal nature than the Red Rose Formation. However, at least one andesitic unit has been identified, apparently striking northeast, with 5-10% 1-2mm feldspar laths. This may represent a conformable flow unit or, alternatively, a sill.

Two types of fossils were noted during mapping, one in outcrop and one in float. Near the fire lookout, on line 10+00E, an area of numerous brachiopods was located, probably a terebratulid such as 'terebratula', in a sandstone host. A piece of float on line 4+00E containing a fairly well preserved near conical belemnite was found in sandstone. Both of these fossils were most abundant in the Cretaceous (Black 1970), though a palaentologist could no doubt be more specific as to precise identification and dating.

8.2.4 Rhyolite.

Most of the rhyolite is massive, coarse grained, unaltered, feldspar porphyry and it outcrops extensively on the cliffs between lines 8+00W and 14+00W. The actual margins of the rhyolite bodies are rarely exposed but near the margins it is frequently interlayered with chlorite and sericite schists (e.g. along base of cliffs and in slide on line 6+00W at 2+00N). The north margin of the main rhyolite body is well-exposed in natural outcrops and recent trenches. This area illustrates the extremely complex nature of the contacts of the rhyolite bodies. This is particularly evident in some of the trenches where sericite schist, rhyolite and chlorite schists are interbanded on as little as a one metre scale (Figure 7). While the rocks in contact with the rhyolite are sericitized or chloritized, there is little evidence of contact metamorphism nor do the rhyolites have chilled margins. This has been suggested by some authors (e.g. Scott 1982) as evidence for the rhyolites being individual flow events, separated by periods of sedimentation. Further evidence for rhyolite flow units is found at the north end of the grid between line 9+00W and 14+00W where a fairly extensive rhyolite flow unit appears to overlie an andesite unit and is in turn overlain by chlorite and sericite schist. Other evidence mentioned above such as the conformity of veins, volcanic breccia units etc. all suggest that the rhyolite represents a fairly high level intrusion with associated flows and/or sills. However, no definite conclusions on its origins can be drawn from the evidence seen to date.

8.2.5 Mineralization.

Five types of mineralization were noted in Section 6.3 as having been located on the property. Since the focus of the 1987 exploration program was in locating new areas of mineralization and known occurrences have been well-documented elsewhere, little time was spent in the known mineralized areas. However, to assist in recognizing styles of mineralization all mine levels were reconnaissance mapped on a scale of 1:2,000 (Figures 8-10) and several chip channel samples taken for comparison purposes. The table below summarizes these results. All samples are fully described in Appendix 2 and assay certificates enclosed in Appendix 1.

TABLE 4: ROCK SAMPLE ASSAYS (KNOWN ZONES)

SAMPLE #	WIDTH (cm)	LOCATION	CU %	PB %	ZN %	AG oz/t	AU oz/t
CU-1	110	#2 Vein	.57	11.48	8.72	14.18	.038
CU-2	120	#2 Vein	.36	7.50	7.95	26.45	.037
CU-3	80	#1 Vein	.35	4.65	12.26	6.01	.015
CU-4	115	#1 Vein	.01	.62	.56	.85	.014
CU-5	115	#1 Vein	.02	.84	1.07	1.13	.014
CU-6	75	#2 Vein	.06	.80	.29	3.19	.019
CU-7	85	#2 Vein	.03	.22	.26	.93	.044
CU-8	85	#2 Vein	.01	.76	.92	1.30	.037
CU-9	110	#2 Vein	.25	10.19	7.88	11.89	.013
CW-4	80	Cross Vein	.01	4.63	.07	8.92	.189
CW-6	160	Cross Vein	.01	4.13	.06	6.46	.006
CW-8	70	NW Wardell	.01	14.49	.18	12.13	.038
CW-10	100	Wardell Vein	.02	2.06	.24	4.54	.011
CW-11	450	Wardell Vein	.23	12.05	7.60	46.29	.066
CW-12	450	Wardell Vein	.09	3.54	6.37	9.88	.092
CW-13	320	Wardell Vein	.06	6.23	.50	16.90	.044
CW-16	60	Vein above #1 Portal	.35	12.03	1.46	11.66	.007
CW-17	80	Vein above #1 Portal	.05	3.10	2.80	3.43	.033
CW-18	170	Vein above #1 Portal	.25	10.80	.08	19.54	.009
H-1	150	Homestake Adit	.13	7.30	11.43	15.75	.018

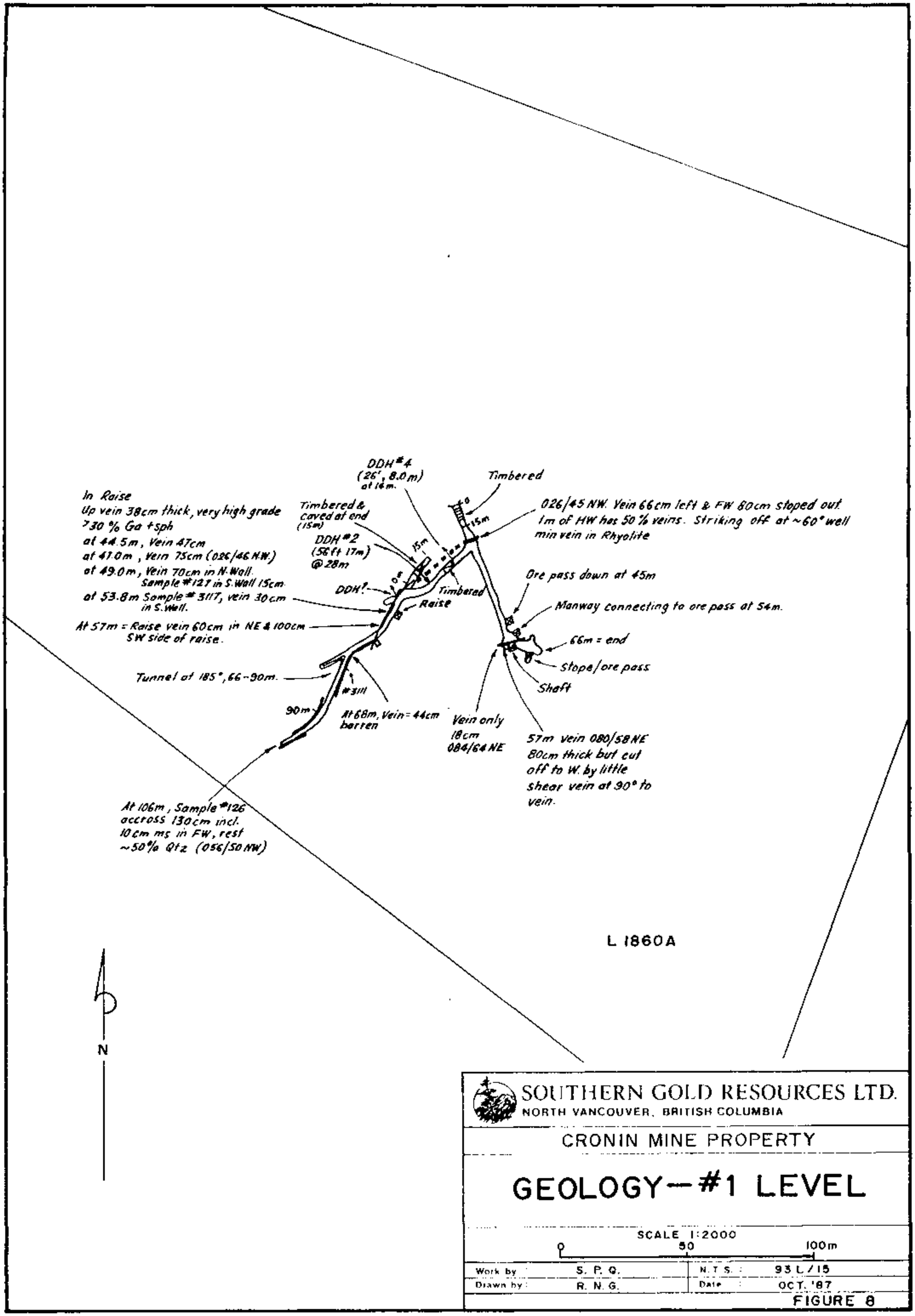
NB: Cu samples collected underground, all others on surface.

This brief reconnaissance did not permit any resolution of the origins of the mineralization, since several conflicting pieces of evidence were observed. For example, on the #5 level (Figure 10) the vein follows the contact between rhyolite and chlorite schist, but there is clearly a minor gouge zone on the hanging wall side of the vein, suggesting a possible fault control. Conversely, in two places on this level it can be determined that this chlorite schist band is only in the order of 1-3m thick with another rhyolite horizon on the hanging wall. This indicates a conformable style of mineralization. Also, this might suggest that there was a lull in volcanic activity leading to a build up of sulphides and deposition of sediments before the onset of renewed volcanism. Shearing may then have selectively occurred in the incompetent sediment layers as opposed to in the more competent rhyolite. However, further west, this vein takes a sharp ninety degree swing away from the main shear and continues southward. This may be a branch off the main trend or a vein following the best developed shears (i.e. line of least resistance). On the #3 level both the #1 and #2 veins are contained entirely within rhyolite, and appear to be shear related (see Figure 9) and cross cutting. On the #1 level the #2 vein is also within rhyolite but in places appears to split into two separate overlapping lenses with no evidence of faulting, again suggesting an exhalative type of origin.

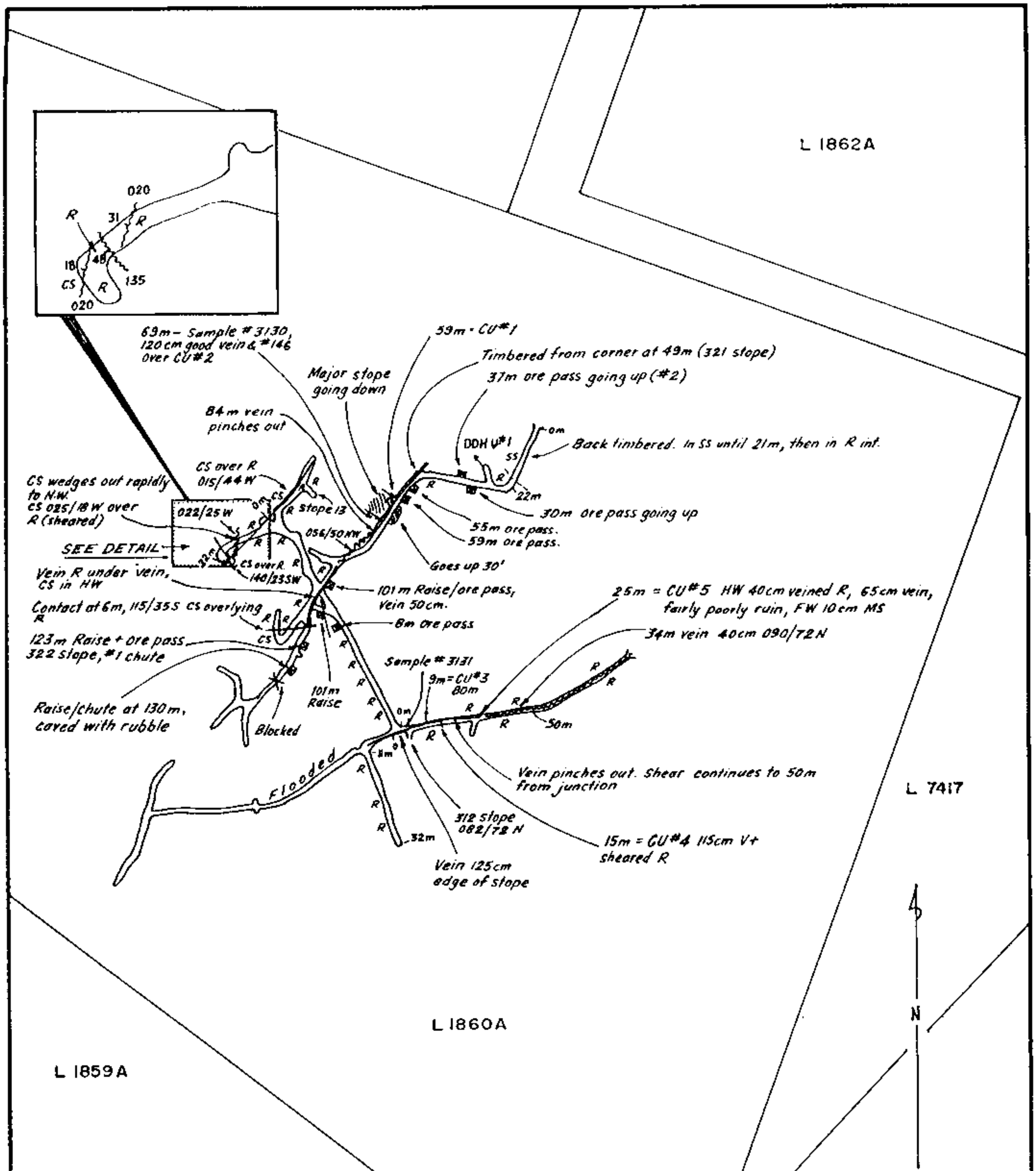
On surface, particularly in the Wardell Zone, a similar picture of conflicting origins is evident. The Wardell vein itself is a heavily mineralized breccia, possibly representing an exhalative collapse breccia. However, it is clearly cross cutting the dominant lithological structure at approximately 90 degrees (see Figure 7). Numerous other quartz and quartz-sulphide veins are orientated in a variety of directions in a coarse stockwork pattern.

These areas, hence, did not allow the author to resolve the debate as to the origin of the mineralization, since conflicting evidences were common not only within the property but even along the same structures. The author, however, still favours a syngenetic origin probably with later remobilization of quartz and sulphides.

Two other areas of interest were noted while mapping. Between line 1+00W and 4+00W, associated with the smaller more easterly rhyolite body, is an extensive area of alteration. This included quartz veining, bleaching and sericitization with associated manganese staining (see Photograph #1). Two grab rock samples from the area (C#6R and C#7R) were slightly anomalous in base metals and gold. The second area was at the north end of L22+00W where an area of large angular boulders was located, all of intensely bleached and stockwork pyrite veined rhyolite. It is the authors opinion that these boulders are very close to outcrop, possibly having only been frost shattered. Three rock



DDH#4
(26', 8.0m)
at 14m.
Timbered
In Raise
Up vein 38cm thick, very high grade
>30 % Ga +sph
at 44.5m, Vein 47cm
at 47.0m, Vein 75cm (026/46 N.W.)
at 49.0m, Vein 70cm in N. Wall.
Sample #127 in S. Wall 15cm
at 53.8m Sample #3117, vein 30cm
in S. Wall.
At 57m = Raise vein 60cm in NE & 100cm
SW side of raise.
Timbered &
caved at end
(15m)
DDH #2
(56ft 17m)
@ 28m
15m
DDH?
Timbered
Raise
026/45 NW. Vein 66cm left & FW 80cm stoped out.
1m of HW has 50% veins. Striking off at ~60° well
min vein in Rhyolite
Ore pass down at 45m
Manway connecting to ore pass at 54m.
66m = end
Stope/ore pass
Shaft
Tunnel at 185°, 66-90m.
#3111
90m
At 68m, Vein = 44cm
barren
Vein only
18cm
084/64 NE
57m vein 080/58 NE
80cm thick but cut
off to W. by little
shear vein at 90° to
vein.
At 106m, Sample #126
accross 130cm incl.
10cm ms in FW, rest
~50% Qtz (056/50 NW)
L 1860A
N
SOUTHERN GOLD RESOURCES LTD.
NORTH VANCOUVER, BRITISH COLUMBIA
CRONIN MINE PROPERTY
GEOLOGY — #1 LEVEL
SCALE 1:2000
0
50
100m
Work by: S. P. Q.
Drawn by: R. N. G.
N.T.S.: 93 L/15
Date: OCT. '87
FIGURE 8



SAMPLE Nos.	Cu (%)	Pb (%)	Zn (%)	Ag (oz/t)	Au (oz/t)
CU 1	0.57	11.48	8.72	14.18	0.038
CU 2	0.36	7.50	7.95	26.45	0.037
CU 3	0.35	4.65	12.26	6.01	0.015
CU 4	0.01	0.62	0.56	0.85	0.014
CU 5	0.02	0.84	1.07	1.13	0.014

SOUTHERN GOLD RESOURCES LTD.
NORTH VANCOUVER, BRITISH COLUMBIA

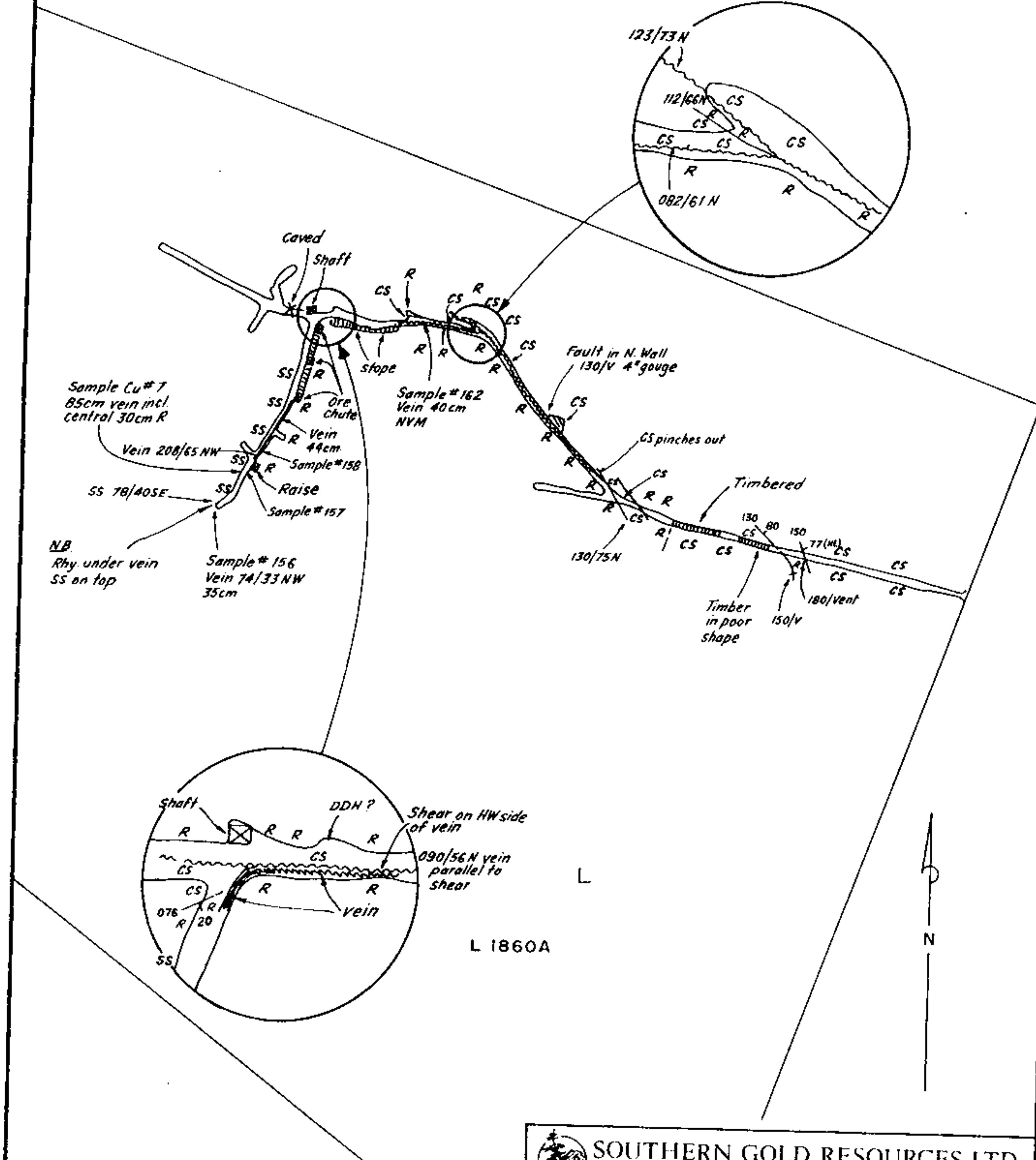
CRONIN MINE PROPERTY

GEOLOGY—# 3 LEVEL

SCALE 1:2000
0 50 100m

Work by:	STEPHEN P QUIN	N.T.S.	93 L/15
Drawn by:	Ram's Drafting Services	Date	OCT. 1987

FIGURE 9



SAMPLE Nos.	Cu (%)	Pb (%)	Zn (%)	Ag (oz/t)	Au (oz/t)
CU 6	0.06	0.80	0.29	3.19	0.019
CU 7	0.03	0.22	0.26	0.93	0.044
CU 8	0.01	0.76	0.92	1.30	0.037
CU 9	0.25	10.19	7.88	11.89	0.013

SOUTHERN GOLD RESOURCES LTD.
NORTH VANCOUVER, BRITISH COLUMBIA

CRONIN MINE PROPERTY

GEOLOGY—#5 LEVEL

SCALE 1:2000
0 50 100 m

Work by	STEPHEN P. QUIN	N.T.S.	93 L / 15
Drawn by	Ram N. Gopal	Date	OCT. '87

FIGURE 10

Photograph 1: Quartz veined & altered zone samples from the area (C#88R1, C#88R2 and C#89R) were variably anomalous in base metals (see Photographs 2 & 3).

TABLE 5: ROCK GEOCHEMISTRY

Sample #	Pb (ppm)	Zn (ppm)	Ag (ppm)	Fe (%)	Au (ppb)
C#6R	198	123	1.5	0.40	12
C#7R	152	820	2.1	0.40	31
C#88R1	157	23	1.5	10.51	11
C#88R2	47	599	0.1	6.19	1
C#89R	26	128	0.4	28.08	1

8.3 Geochemistry

The entire grid area was soil/talus fines sampled at 25m intervals. A total of 1233 samples were collected using a mattock to dig down to the B soil horizon, where such was developed. The 'B' horizon was generally at a depth of 10-30cm and best developed in the upper alpine areas. On the slopes soil horizons were poorly developed, due to the unstable nature of these slopes. In these areas soil samples were collected at depths of approximately 20cm. In some areas, particularly below the rhyolite cliffs between lines 8+00W and 14+00W, only talus fines were available for sampling. All samples were placed in kraft paper bags and air dried before shipping to Acme Analytical Laboratories of Vancouver, B.C. for analysis. All samples were subjected to a 30-element Induced Coupled Plasma (ICP) analysis and also re-analyzed for gold by atomic absorption (AA) for greater sensitivity. The results for six elements (Au & Ag, Pb & Zn, Cu & As) have been computer plotted (Figures 11-13). Figure 14 is a composite anomaly map correlating geochemistry, geophysics and geology. The assay certificates are included as Appendix 1.

The range in geochemical values was much more pronounced than expected. This was particularly so for Pb and Ag, which reached values of over 20,000 ppm and 330 ppm (11 OPT) respectively. Arsenic also proved useful in delineating anomalous areas. Copper was much less anomalous than expected. The range in geochemical values is summarized below.

Photograph 2: View of mineralized area

Photograph 3: Stockwork sulphide veining

TABLE 6: SOIL/TALUS GEOCHEMISTRY

Element	Low (ppm)	High (ppm)
Cu	6	498
Pb	2	20,934
Zn	19	7,578
Ag	0.1	336.6
As	6	20,961
Au	1 ppb	2,920 ppb

8.3.1 Lithological Variations.

As can be seen from all of the maps enclosed, virtually all of the anomalous samples were collected from soils underlain by the Red Rose Formation and rhyolites. The Ashman and Brian Boru Formations are rarely anomalous and can largely be eliminated from future exploration.

8.3.2 Main Zone (Line 7+00W to 15+00W).

This area contains at least 80-90% of all the anomalous values in the grid area. The geochemically anomalous areas for the six elements plotted in figures 11-13 show a fairly close correlation with the outline of the principal rhyolite body, and very closely follow each other. The correlation with the limits of the rhyolite is even closer if the interpreted geophysical limits are used (see section 8.4 below). This shows a sharp cut off of values between lines 7+00W and 6+00W on the east and a northerly limit of around 8+00N on all lines. These two limits, to the north and east, correlate very closely with the projected faults interpreted by Pezzot (1987). As with the geophysical results described below, the geochemistry is not limited to grid south, with highly anomalous values very close to the base line. However, most values are starting to decrease in the last stations and clearly show evidence of downhill spread, for example, the anomalies at the southern ends of lines 7+00W, 8+00W, 11+00W and 12+00W correlate very closely with major talus slides. The western edges of the geochemical anomalies are much more diffuse.

Geochemical delineation of known mineralized zones shows a broad correlation with previously defined trends, but not very continuous or precise. The mine area around 8+00W to 9+00W and at 7+00N to 8+00N is strongly anomalous, probably caused by dump contamination. However, the correlation with outcropping mineralization is not very close, particularly in the Wardell and Homestake areas. Several areas of interest are detailed below:

a) 090° Trend, 13+00W 6+50N to 11+00W 5+50N.
A very definite east-west trend detected by Zn, Pb, Ag, As, Au and possibly by Cu. This cross cuts the Wardell Zone trend at its western end where it is lost, to later reappear in the Homestake area. Several parallel, though less distinct trends are also visible centred on 14+00W 3+25N (As, Cu), 12+00W 4+25N (As) and 12+00W 9+00N (As).

b) 040° Trend, 12+00W 2+25N to 6+00W 5+50N.
A less well delineated trend but noted for the extension of the Pb, Au, Ag, As and Cu anomalies 100m or more further southwest than on the north side of this trend and the alignment of some of the highest Pb values in the area along this trend. There is also a distinct northeastward "bulge" of Cu, Ag, Au, Zn, Pb and As values associated with this area. This "trend" correlates with one of the VLF EM conductors detected both by Hawaii and Annapolis (see section 8.4 below).

c) 040° Trend, 7+00W 2+50N to 6+00W 2+75N.
This correlates with a small vein sampled on surface and is only delineated by Zn.

d) 090° Trend, 16+00W 4+25N to 13+00W 4+00N.
A weak anomaly delineated by Zn and to some extent by Au and correlates closely with a Seattle VLF EM conductor and with a possible magnetically delineated fault zone.

8.3.3 New Anomaly (Line 5+00W to 3+00W at 6+00N to 8+00N).

This anomaly is of limited extent but very strongly anomalous in Au, Ag, As, Pb and Zn and less strongly anomalous in Cu. It appears to be related to the area of bleached and altered rhyolite described at the end of section 8.2.5 and suggests the need for further exploration in this area for polymetallic sulphides as found in the main area of workings.

8.3.4 Miscellaneous Anomalies.

Several other areas have been outlined that are anomalous in one or more of the elements plotted. These include the following.

a) Lines 12+00W to 16+00W between 7+00N and 9+00N.
This area is broadly anomalous in copper and contains several single point anomalies in As and Zn. The area is underlain by rhyolites and altered sediments and hence deserves further attention.

b) Lines 22+00W to 26+00W between 15+00N to 19+00N.
This area is largely covered by coarse moraine and talus but does contain the area of bleached and pyritized rhyolite

float described at the end of section 8.2.5. This area is broadly anomalous in copper, gold, zinc and lead and certainly deserves further attention.

c) Lines 5+00W to 9+00W between 9+00N and 12+00N.
This area lies to the north of the main area of workings and is broadly anomalous in As including one value of 2,568 ppm. This area is alpine meadows and is underlain by rhyolite and altered sediments and should be further investigated.

d) Lines 15+00W to 18+00W between the base line and 2+50N. This southwest corner of the grid is unlikely to be influenced by downhill contamination from the main area and hence represents a valid target. The area is anomalous in As, Cu and Au and overlies an area of sericite schist and rhyolite.

8.4 Geophysics

Southern Gold Resources rented an Integrated Geophysical System (IGS) incorporating a VLF-EM unit and a proton magnetometer from Scintrex. This is a very compact unit comprising of a digital master console, a VLF-EM receiver and a magnetometer. The 'integrated' aspect is electronic hook-up between all these units allowing push button control and digital recording of station and line number and results on the master console's memory. A base station magnetometer, portable computer and plotter completed the package. The two field assistants were trained in its use by the author and conducted the surveys of all of the grid lines. On each line total field magnetic readings were taken and in-phase and quadrature VLF-EM readings for each of the selected frequencies. The three stations selected were Hawaii, Annapolis and Seattle to give omni-directional coverage.

At the end of each day, the base station magnetometer and field unit were connected and the magnetic data corrected for diurnal variation. Then all the data was dumped onto the computer, allowing editing and outputting of profiles on a daily basis. All field data collected was presented to Trent Pezzot of GeoSci Data Analysis Ltd. of Richmond B.C. for final completion and interpretation. The results of his report (Pezzot 1987) are summarized following.

8.4.1 Summary of Results

"Both the magnetic and VLF-Electromagnetic components of this survey have provided useful information for this project.

The magnetometer data appears to outline the area of the rhyolite body mapped by Scott and Ikona as a weak but distinct magnetic high. This zone appears to extend further south than presently mapped. It is highly probable that its' northern limit, the *area of the Cronin Mine is controlled by a fault striking at approximately 075° and that the same geological environment extends for some 500 meters along this structure. Magnetic evidence suggests that the eastern border of the mapped rhyolite body is also fault controlled. The western edge of the rhyolite body is also fault controlled. The western edge of the rhyolite body is less distinct and appears to interfinger with the country rock producing three small outliers of higher susceptibility materials.*

The eastern edge of the survey grid is covered by a large magnetic high, of similar intensity to that associated with the rhyolite body. No geological input for this area is available to the author but the similarity of the magnetic field intensities in this area suggest a similar rhyolitic unit might be present. The same conclusions may be drawn for the western most lines of the survey grid, where "rhyolite" type magnetic highs are observed." (Note by Author: This eastern area closely parallels the limits of the Ashman Formation which may contain some detrital magnetite, since it appears to generally have a higher magnetic intensity.)

"Inphase, quadrature and field strength measurements of three VLF-EM stations were gathered during the course of this survey. A large number of near surface conductive lineations were mapped. Some of these coincide with the outline of the rhyolite but they are indistinguishable from many other anomalies which are believed related to overburden variations. The VLF-EM response associated with the fault immediately north of the Cronin Mine appears to be the most conductive lineation observed within this grid.

The VLF-EM system mapped two major structures which intersect in the general area of the Cronin Mine. One is the above mentioned fault zone. The second approaches the mine site from the southwest and terminates against the fault. The second feature is also reflected as a contact between two distinct surficial conductivity background levels and to a certain degree by the local terrain."

8.4.2 Description of Anomalies

Specific anomalies of interest are detailed below and summarized on Figure 14, the Composite Anomaly Map. More details on these anomalies are given in the report by Pezzot (1987).

a) *Major anomaly parallelling 8+00N from 4+00W to 10+00W.*
This is interpreted by Pezzot (1987) as being a major fault limiting the northerly extent of the rhyolite. It was detected by all VLF-EM frequencies as a strong conductor, but most extensively by Annapolis. Why it is not conductive further west (10+00W to 14+00W) may have economic implications, since there may be sulphides in this part of the zone. The trend may continue weaker all the way to 4+00E intermittently by all three frequencies, but most continuously by Annapolis.

b) *Strong Anomaly at 4+00W and 7+25N.*
Detected by both Hawaii and Annapolis, it parallels (a) above and may possibly represent a faulted off extension of the same, since it lies immediately east of the interpreted 140° fault that limits the eastern edge of the rhyolite. It may be significant that it lies in close proximity to a very strong geochemical anomaly described in section 8.3.3 above.

c) *040° Trend from 16+00W 5+00N to 7+00W 7+75N.*
This series of anomalies is not very strong nor continuous but it closely follows the surface trace of the Wardell trend. It was variously detected by Seattle, Annapolis and Hawaii. The zone is cut off to the north east by the strong 070° "fault zone" described in (a) above.

d) *040° Trend from 11+00W 2+00N to 4+00W 5+75N.*
This is one of several trends parallel to the main mineralized Wardell Zone delineated by Hawaii and to a lesser extent by Annapolis. This trend, however, appears to have some geochemical correlations as noted 8.3.2 (b) above. This is unlikely to be a spurious anomaly caused by topographic effects, since it lies at the base of a cliff where topography should reduce anomalies (Candy C., 1987, Pesonal Communication).

e) *070° Trend from 14+00W 12+00N to 5+00W 12+50N.*
This long continuous VLF EM conductor delineated by the Hawaii and Annapolis frequencies and to a lesser extent by Seattle, appears to correlate with the rhyolite flow unit described in section 8.2.4 above.

9. CONCLUSIONS

The 1987 field season has added significantly to the understanding of the geology and mineralization of the Cronin Mine property. While prospecting/ mapping did not locate any new zones of mineralization, this was not expected because of the long and active exploration history on the property. Mapping of the known mineralized areas did confirm evidences for both a volcanogenic and a fault controlled style of mineralization. An exhalative origin with later remobilization of quartz and sulphides appears to be the most likely origin at this time.

The geophysical survey greatly assisted in delineating the boundaries of the rhyolite intrusives and the Ashman Formation. Further, it clearly indicates fault control of the 'rhyolite' bodies. Significant potential may lie in that part of the 070° fault zone that is most highly conductive. Its conductivity is such that a possible sulphide association is suggested for this section of the fault. Alternatively, there may be a broad alteration zone parallel to the Wardell trend and 200m wide that results in a higher clay content in this part of the 070° fault, making it more conductive (Candy C., 1987, Personal Communication). The main mineralized trend was detected by the survey, though it is not strongly anomalous. Several other trends were also delineated that may be of economic significance. The geochemical survey unfortunately shows widespread dispersion of the elements of interest, which largely masks individual anomalies. However, several zones of interest have been delineated which warrant further investigation. Both geophysics and geochemistry delineated one strong isolated anomaly on line 4+00W which appears to be the best "new area" to be investigated. The very strong geophysical conductor in this area may be a fault offset continuation of the main 070° trend and therefore have the same sulphide potential as indicated for that.

The area covered by line 20+00W to 26+00W has as yet undetermined potential. The rocks discovered there are typical feeder zone altered rhyolites that are found underlying exhalative sulphide deposits. The rocks are only weakly geochemically anomalous and talus samples from the area show a broad copper-lead-zinc anomaly. Geophysics outline one large high intensity magnetic area west of line 24+00W and two smaller high intensity areas, one of which underlies these rocks of interest. Unfortunately the overlying andesites mask any outcrops over almost all of the area so the only exploration would have to be conducted completely "blind".

In conclusion, therefore, the 1987 exploration program was successful in delineating several target areas worthy of further exploration. The geochemical program unfortunately shows widespread contamination that makes discrimination of individual anomalies difficult and somewhat uncertain. The geophysical system used was a reconnaissance tool with shallow penetration and only moderate discriminatory abilities. As a result of these factors and a lack of an outcropping target a more definitive geophysical program of geophysics is recommended to follow-up on the defined targets prior to drilling.

10. RECOMMENDATIONS

A follow-up program to better define the location and nature of the target areas, prior to any physical work such as drilling or trenching, which would be environmentally very sensitive on this property.

STAGE 1: Geophysics

Mobilization/Demobilization	$3,000
Survey (7 days @ $1200)	$8,400
Labour (2 men, 7 days @ $150)	$2,100
Hotel/Meals/Supplies	$2,000
Report, Plotting, etc.	$2,000
	$17,500
Contingency @ 10%	$1,750
TOTAL STAGE 1 EXPENDITURES	$19,250

STAGE 2: Drilling

Road Rehabilitation	$10,000
Geology (30 days @ $300)	$9,000
Assistant (30 days @ $150)	$4,500
Drilling (2,500 feet @ $35)	$87,500
Assaying	$4,000
Camp, Support	$5,000
	$120,000
Contingency @ 10%	$12,000
TOTAL STAGE 2 EXPENDITURES	$132,000

11. STATEMENT OF EXPENSES

1.	Geophysics		
	Equipment 44.24 days @ $170/day		$7,521.33
	Interpretation & Report		$3,442.64
			$10,963.97
2.	Geochemistry		
	Supplies (soil bags, etc.)		$137.80
	1233 Soils - Preparation	@ $0.75	$924.75
	- ICP	@ $6.00	$7,398.00
	- Au by AA	@ $4.25	$5,240.25
	49 Rocks - Preparation	@ $3.00	$147.00
	18 Rocks - ICP	@ $6.00	$108.00
	- Au by AA	@ $4.25	$76.50
	31 Rocks - Au, Ag by FA	@ $11.25	$348.75
	- Cu, Pb, Zn Assay	@ $12.75	$395.25
	Transport		$293.25
	Computer Plotting		$320.00
			$15,389.55
3.	Transportation		
	Air Ticket		$382.40
	Truck 1 month @ $1,000		$1,000.00
			$1,382.40
4.	Physical Work		
	Access - D6 46.5 hrs @ $80		$3,720.00
	- Transport		$260.00
	- Truck		$300.00
			$4,280.00
5.	Base Maps 1:5,000 Scale		$2,835.00
6.	Geological		
	S.P. Quin (Geologist) 28 days @ $300		$8,400.00
	J. Green (Assistant) 30 days @ $150		$4,500.00
	P. Mackenzie (Assistant) 30 days @ $150		$4,500.00
	Camp Support		$7,349.13
	Supplies, Miscellaneous		$1,996.38
			$26,745.51
7.	Report		
	Reproduction		$49.74
	Drafting 82.50 hrs @ $22.00		$1,815.00
	Supplies		$618.54
	S.P. Quin (Geologist) 14 days @ $300		$4,200.00
			$6,683.29
Sub Total			$68,279.72
Administration and Overhead @ 10%			$6,827.97
TOTAL EXPENDITURES			$75,107.69

12. REFERENCES

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Trenholme, L.S. (1976): Report on the Cronin Mine, Hallmark Resources Ltd. October 15, 1976.

Trenholme, L.S. (1977): Report on Properties of Hallmark Resources Ltd. March 23, 1977.

Vollo, N. (1987): Report on the Cronin Mine, Southern Gold Resources Ltd. (Company Report).

13. STATEMENT OF QUALIFICATIONS

I, Stephen P. Quin, do hereby certify that:

1. I am a mining geologist with business address at #220 - 145 Chadwick Court, North Vancouver, B.C., V7M 3K1.

2. I have a Bachelor of Science (Honors) Degree in Mining Geology from the Royal School of Mines in London, England. I am a member of several geological associations.

3. I have worked in mineral exploration since 1981. I have worked in various parts of British Columbia, Europe and the western United States of America.

4. I have based my report on an extensive study of the published data available on the property and on approximately one month spent on the property as detailed in this report.

5. As of August 1986 I have been a Director, Vice-President and Corporate Secretary and a major shareholder of Southern Gold Resources Ltd., a private, non-reporting resource company registered in the province of British Columbia.

6. Between 1981 and 1986 I was a project geologist with Imperial Metals Corporation of Vancouver, B.C.

Signed in North Vancouver this 9th day of November 1987.

Stephen P. Quin, B.Sc., A.R.S.M.

APPENDIX 1

ASSAY CERTIFICATES

ACME ANALYTICAL LABORATORIES
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: AUG 31 1987
DATE REPORT MAILED: Sept 9/87

ASSAY CERTIFICATE

- SAMPLE TYPE: Rock Chips AU** AND AG** BY FIRE ASSAY.

ASSAYER: .... DEAN TOYE, CERTIFIED B.C. ASSAYER

SOUTHERN GOLD PROJECT-121104 File # 87-3784A

SAMPLE#	CU %	PB %	ZN %	AG** OZ/T	AU** OZ/T
CU-1	.57	11.48	8.72	14.18	.038
CU-2	.36	7.50	7.95	26.45	.037
CU-3	.35	4.65	12.26	6.01	.015
CU-4	.01	.62	.56	.85	.014
CU-5	.02	.84	1.07	1.13	.014
CU-6	.06	.80	.29	3.19	.019
CU-7	.03	.22	.26	.93	.044
CU-8	.01	.76	.92	1.30	.037
CU-9	.25	10.19	7.88	11.89	.013
CW-1	.49	14.22	7.46	22.81	.032
CW-2	.04	2.51	.23	8.43	.008
CW-3	.01	.35	.09	.43	.006
CW-4	.01	4.63	.07	8.92	.189
CW-6	.01	4.13	.06	6.46	.006
CW-7	.01	4.21	.31	7.06	.036
CW-8	.01	14.49	.18	12.13	.038
CW-9	.01	.72	.10	2.55	.003
CW-10	.02	2.06	.24	4.54	.011
CW-11	.23	12.05	7.60	46.29	.066
CW-12	.09	3.54	6.37	9.88	.092
CW-13	.06	6.23	.50	16.90	.044
CW-14	.01	.25	.16	1.58	.006
CW-15	.01	.10	.03	.74	.004
CW-16	.35	12.03	1.46	11.66	.007
CW-17	.05	3.10	2.80	3.43	.033
CW-18	.25	10.80	.08	19.54	.009
CW-20	.01	.02	.02	.08	.001
H-1	.13	7.30	11.43	15.75	.018
H-2	.01	1.65	.20	1.87	.002
H-3	.01	.24	.20	.27	.002
H-4	.06	.87	6.68	1.41	.003

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 17 1987 DATE REPORT MAILED: Aug 25/87 ASSAYER. D. Toye ..DEAN TOYE. CERTIFIED B.C. ASSAYER

SOUTHERN GOLD PROJECT-121104 File # 87-3381 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL18W 7+00N	1	23	79	126	.4	17	10	483	4.78	47	5	ND	2	11	1	2	2	33	.07	.121	15	7	.11	77	.01	2	1.16	.01	.04	2	1
CL18W 6+75N	1	35	77	140	.7	16	12	2199	4.25	38	5	ND	2	12	1	3	2	26	.07	.146	15	8	.11	152	.01	6	1.32	.02	.06	1	2
CL18W 6+50N	1	37	80	153	.8	23	15	1132	4.78	42	5	ND	3	15	1	2	2	25	.11	.148	20	10	.19	121	.01	3	1.57	.02	.05	1	1
CL18W 6+25N	1	36	79	149	.7	24	24	2312	5.33	26	5	ND	5	31	1	2	2	22	.24	.141	23	5	.19	233	.01	2	1.21	.02	.06	1	1
CL18W 6+00N	2	42	109	151	.7	25	23	2647	5.96	43	7	ND	4	27	1	2	3	24	.21	.130	26	8	.24	164	.01	2	1.35	.02	.07	3	1
CL18W 5+75N	2	41	132	143	1.0	24	23	2319	5.45	56	6	ND	4	25	1	2	2	22	.18	.133	25	9	.21	137	.01	2	1.23	.02	.05	1	1
CL18W 5+50N	2	37	85	137	.7	23	25	2636	5.57	38	5	ND	5	41	1	2	2	22	.33	.148	24	6	.22	236	.01	2	1.18	.02	.06	1	1
CL18W 5+25N	2	42	151	152	.8	23	19	2100	5.16	61	5	ND	4	27	1	2	2	23	.20	.122	22	8	.24	199	.01	11	1.29	.02	.06	2	1
CL18W 5+00N	2	50	136	163	1.0	23	22	2472	5.83	56	5	ND	4	26	1	2	2	23	.19	.147	24	8	.23	190	.01	2	1.38	.02	.07	2	3
CL18W 4+75N	2	39	116	140	.8	21	17	1875	5.06	57	5	ND	4	17	1	2	2	20	.12	.136	24	10	.20	143	.01	2	1.26	.02	.07	1	1
CL18W 4+50N	1	21	60	84	.4	14	7	805	2.87	38	5	ND	2	14	1	2	2	18	.10	.132	14	9	.15	94	.01	2	1.13	.01	.06	1	2
CL18W 4+25N	2	41	99	164	1.0	32	15	1234	4.98	62	5	ND	4	29	1	2	2	25	.26	.121	21	10	.27	135	.01	2	1.29	.02	.05	2	1
CL18W 4+00N	2	33	82	150	.5	27	16	1407	4.64	60	5	ND	2	21	1	2	2	23	.19	.120	16	9	.23	122	.01	2	1.20	.02	.07	1	1
CL18W 3+75N	3	51	195	236	.8	57	22	2077	5.41	111	5	ND	4	27	1	2	2	21	.19	.111	22	8	.17	157	.01	2	.90	.02	.06	1	2
CL18W 3+50N	2	58	80	164	.4	71	19	1515	5.15	57	5	ND	4	15	1	2	2	21	.11	.074	14	16	.24	120	.01	4	.95	.02	.06	1	3
CL18W 3+25N	1	32	71	119	.5	28	12	886	3.97	47	5	ND	3	18	1	2	2	23	.16	.127	19	11	.24	118	.01	2	1.34	.02	.07	1	1
CL18W 3+00N	2	34	80	114	.6	20	11	1219	4.21	55	5	ND	2	11	1	2	2	25	.07	.143	17	12	.20	135	.01	2	1.37	.02	.06	1	1
CL18W 2+75N	1	35	142	231	.5	35	13	1644	5.22	126	5	ND	3	12	1	2	2	38	.13	.158	12	33	.45	84	.01	3	2.30	.02	.09	1	1
CL18W 2+50N	2	31	111	169	.7	26	12	1171	4.97	97	5	ND	2	10	1	2	2	38	.07	.135	13	24	.35	80	.01	2	2.18	.02	.07	2	4
CL18W 2+25N	4	72	71	209	.3	79	30	3423	6.49	54	5	ND	5	11	1	2	2	35	.02	.092	17	30	.31	225	.01	2	1.88	.02	.05	1	1
CL18W 2+00N	3	54	81	166	.5	49	24	2849	5.05	78	5	ND	4	10	1	2	2	31	.03	.108	18	20	.20	158	.01	2	1.45	.02	.07	1	6
CL18W 1+75N	3	40	102	152	.6	28	18	2465	5.17	69	5	ND	3	13	1	2	2	31	.07	.153	18	15	.26	128	.01	2	1.63	.02	.07	1	1
CL18W 1+50N	3	34	142	218	.5	26	13	3087	4.77	133	5	ND	4	11	1	2	2	22	.07	.129	18	11	.24	168	.01	2	1.66	.02	.07	1	1
CL18W 1+25N	3	37	130	236	.8	27	13	3310	4.72	142	5	ND	5	13	2	2	2	20	.08	.125	19	10	.23	215	.01	2	1.49	.02	.07	1	3
CL18W 1+00N	3	33	82	223	.8	43	14	2661	4.30	134	5	ND	4	14	2	3	2	15	.13	.100	17	6	.18	241	.01	2	1.05	.02	.08	1	1
CL18W 0+75N	2	37	52	192	.5	55	16	1774	4.19	100	5	ND	4	10	1	2	2	14	.11	.065	15	5	.17	192	.01	2	.81	.02	.05	1	1
CL18W 0+50N	3	29	58	210	.7	47	11	1204	4.08	114	5	ND	5	30	1	2	2	12	.23	.058	17	7	.19	169	.01	2	.95	.02	.06	1	5
CL18W 0+25N	4	40	42	348	.8	58	15	1447	4.78	127	5	ND	4	29	2	7	2	13	.33	.069	18	7	.13	134	.01	2	.63	.02	.06	1	5
CL18W 0+00N	3	24	50	157	.7	27	9	3711	3.45	63	5	ND	3	8	1	2	2	14	.04	.108	16	7	.08	217	.01	5	.82	.02	.08	1	1
CL17W 7+00N	3	38	63	191	.7	38	22	1487	6.42	70	5	ND	3	21	1	2	2	37	.23	.140	14	13	.16	163	.01	2	1.40	.02	.05	1	18
CL17W 6+75N	2	22	65	128	.3	19	8	951	3.83	46	5	ND	2	14	1	2	2	35	.13	.121	11	12	.13	117	.01	3	1.34	.02	.04	1	1
CL17W 6+50N	3	42	50	145	.4	43	18	1141	5.30	47	5	ND	3	19	1	2	2	31	.18	.138	14	14	.20	130	.01	2	1.30	.02	.04	2	2
CL17W 6+25N	2	42	42	147	.9	49	19	1063	4.40	55	5	ND	3	19	1	2	2	24	.21	.105	14	10	.11	92	.01	9	.74	.02	.05	2	1
CL17W 6+00N	3	49	54	163	1.2	50	21	1234	5.36	69	5	ND	4	39	1	2	2	27	.35	.119	19	12	.24	144	.01	2	.94	.02	.05	1	2
CL17W 5+75N	2	43	175	195	2.2	38	17	1388	5.20	124	5	ND	4	28	1	2	2	32	.25	.128	18	12	.24	137	.01	5	1.36	.02	.04	1	1
STD C/AU-S	19	58	42	134	7.5	70	28	927	4.09	39	19	8	37	49	19	17	21	57	.49	.090	37	60	.91	171	.08	36	1.91	.08	.14	13	47
CL17W 5+50N	3	37	87	203	1.0	26	16	1552	5.86	49	5	ND	3	23	1	2	2	31	.22	.167	16	10	.23	134	.01	2	1.64	.02	.07	1	1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM
CL17W 5+25N	1	35	92	151	.4	20	16	1683	5.30	56	5	ND	2	25	1
CL17W 5+00N	1	33	74	141	.2	21	15	1467	5.28	45	5	ND	3	21	1
CL17W 4+75N	1	28	67	113	.3	15	12	1692	4.36	38	5	ND	2	15	1
CL17W 4+50N	2	54	64	166	.5	54	23	1725	5.70	40	5	ND	3	25	1
CL17W 4+25N	2	46	125	148	1.3	31	19	1611	5.49	69	5	ND	3	29	1
CL17W 4+00N	2	34	81	145	.2	20	17	7144	4.06	43	5	ND	2	52	1
CL17W 3+75N	2	35	99	140	.2	22	20	3505	4.82	52	5	ND	2	29	1
CL17W 3+50N	1	35	67	129	.1	25	12	1133	4.30	52	5	ND	2	22	1
CL17W 3+25N	2	30	94	162	.2	27	16	3059	3.79	92	5	ND	1	38	3
CL17W 3+00N	3	45	123	183	.2	45	22	3453	4.60	74	5	ND	1	40	2
CL17W 2+75N	2	18	113	82	3.3	21	5	98	3.47	80	5	ND	2	17	1
CL17W 2+50N	1	14	52	52	1.0	13	3	79	1.78	42	5	ND	2	8	1
CL17W 2+25N	3	39	56	150	.4	37	13	872	4.45	49	5	ND	4	26	1
CL17W 2+00N	1	29	45	123	.2	28	13	615	3.85	29	5	ND	4	32	1
CL17W 1+75N	2	55	72	187	.6	70	26	1989	5.55	60	5	ND	6	45	2
CL17W 1+50N	3	82	85	209	1.0	64	22	1808	5.70	431	5	ND	6	36	1
CL17W 1+25N	4	66	122	277	1.3	62	22	2787	6.11	277	5	ND	6	38	2
CL17W 1+00N	6	64	120	321	1.4	58	25	3659	6.62	303	5	ND	5	51	3
CL17W 0+75N	5	58	102	262	1.3	48	22	3109	6.23	220	5	ND	5	45	2
CL17W 0+50N	4	52	75	223	1.1	39	17	2340	5.57	173	5	ND	5	40	2
CL17W 0+25N	2	39	68	212	.5	40	14	1138	4.88	87	5	ND	4	19	1
CL17W 0+00N	4	63	109	249	.4	43	24	4259	5.30	121	5	ND	4	28	2
CL16W 9+00N	2	56	44	160	.5	63	18	1340	5.22	59	5	ND	4	14	1
CL16W 8+75N	3	55	33	167	.3	45	19	1207	7.35	34	5	ND	4	27	1
CL16W 8+50N	2	59	37	150	1.4	65	23	2298	7.12	82	5	ND	3	24	1
CL16W 8+25N	2	56	38	152	.5	79	24	1782	6.79	105	5	ND	3	10	1
CL16W 8+00N	2	49	45	145	.3	62	18	1848	5.63	67	5	ND	2	11	1
CL16W 7+75N	5	57	24	147	.3	105	33	3018	5.26	93	5	ND	3	16	1
CL16W 7+50N	2	49	77	158	.2	74	31	2534	6.14	162	5	ND	3	11	1
CL16W 7+25N	3	54	68	137	.3	49	20	2108	6.38	108	5	ND	2	10	1
CL16W 7+00N	2	42	37	148	.3	40	17	1518	7.56	38	5	ND	3	16	1
CL16W 6+75N	2	35	51	133	.5	25	17	3655	4.89	26	5	ND	3	14	1
CL16W 6+50N	2	29	60	145	.1	22	11	1200	4.62	47	5	ND	2	20	1
CL16W 6+25N	3	49	69	172	.3	44	20	1451	6.27	82	5	ND	3	13	1
CL16W 6+00N	2	41	80	152	.4	41	15	1239	5.12	88	5	ND	3	10	1
CL16W 5+75N	2	35	129	153	2.2	35	15	1377	4.24	119	5	2	2	13	1
STD C/AU-S	18	58	41	131	7.1	68	27	1040	4.06	41	18	8	36	49	19

SAMPLE#	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL17W 5+25N	2	2	26	.32	.247	16	7	.18	148	.01	2	1.41	.02	.09	1	8
CL17W 5+00N	2	2	27	.21	.215	18	7	.20	119	.01	2	1.56	.02	.08	1	1
CL17W 4+75N	2	2	24	.11	.151	18	5	.13	133	.01	2	1.25	.01	.09	1	1
CL17W 4+50N	2	2	21	.18	.110	21	11	.20	99	.01	2	1.13	.02	.06	1	1
CL17W 4+25N	2	2	23	.19	.119	23	7	.22	88	.01	2	1.55	.02	.07	1	1
CL17W 4+00N	2	2	23	.60	.151	13	6	.09	356	.01	3	1.10	.03	.10	1	4
CL17W 3+75N	2	2	24	.25	.188	15	8	.19	232	.01	2	1.57	.02	.07	1	1
CL17W 3+50N	2	2	24	.18	.146	14	10	.17	104	.01	3	1.19	.02	.08	1	8
CL17W 3+25N	2	2	18	.45	.193	11	7	.13	132	.01	3	.72	.02	.11	1	1
CL17W 3+00N	3	2	19	.45	.214	10	7	.14	114	.01	2	.82	.02	.13	1	1
CL17W 2+75N	3	2	22	.10	.112	12	15	.11	84	.01	2	1.36	.02	.07	1	1
CL17W 2+50N	2	2	18	.02	.083	15	7	.04	47	.01	2	.72	.01	.05	1	2
CL17W 2+25N	3	2	26	.23	.095	20	12	.26	115	.01	9	1.07	.02	.07	1	2
CL17W 2+00N	2	2	27	.30	.119	19	14	.38	108	.02	2	1.44	.02	.08	1	1
CL17W 1+75N	3	2	24	.24	.104	22	16	.26	154	.01	2	1.10	.02	.07	1	3
CL17W 1+50N	2	2	22	.25	.082	21	14	.33	125	.01	4	1.20	.02	.07	1	240
CL17W 1+25N	4	2	27	.26	.081	19	11	.27	219	.01	2	1.04	.02	.07	1	108
CL17W 1+00N	4	2	39	.38	.095	17	8	.28	415	.01	2	.98	.02	.08	1	200
CL17W 0+75N	2	2	36	.36	.110	19	10	.28	363	.01	2	1.00	.02	.08	1	142
CL17W 0+50N	2	2	28	.36	.115	20	8	.26	223	.01	2	.86	.03	.06	1	290
CL17W 0+25N	2	2	28	.15	.094	16	17	.24	141	.01	2	1.30	.02	.07	1	1
CL17W 0+00N	2	2	28	.25	.137	17	14	.25	224	.01	2	1.29	.02	.09	2	50
CL16W 9+00N	2	2	20	.12	.090	16	8	.15	83	.01	7	.79	.02	.07	1	3
CL16W 8+75N	2	2	34	.34	.148	13	10	.18	592	.01	2	.92	.02	.06	1	2
CL16W 8+50N	6	2	26	.15	.170	17	12	.17	156	.01	4	1.19	.02	.07	1	3
CL16W 8+25N	6	2	25	.05	.171	19	17	.13	114	.01	2	1.04	.01	.07	1	4
CL16W 8+00N	5	2	24	.06	.218	13	20	.14	130	.01	2	1.30	.02	.06	1	1
CL16W 7+75N	6	2	21	.05	.099	18	9	.15	403	.01	2	1.15	.02	.07	1	1
CL16W 7+50N	6	2	34	.06	.157	15	19	.40	119	.01	2	1.90	.02	.06	1	6
CL16W 7+25N	5	2	36	.05	.162	13	16	.18	83	.01	2	1.35	.02	.08	1	6
CL16W 7+00N	2	2	45	.07	.180	12	19	.20	107	.01	4	1.85	.02	.06	1	2
CL16W 6+75N	2	3	37	.09	.214	13	15	.16	167	.01	2	1.44	.02	.08	1	11
CL16W 6+50N	2	2	44	.15	.169	12	15	.22	109	.01	2	1.57	.02	.07	1	2
CL16W 6+25N	5	2	31	.05	.147	14	11	.13	147	.01	2	1.14	.01	.05	1	6
CL16W 6+00N	7	2	25	.03	.099	13	11	.09	81	.01	2	.78	.01	.04	1	4
CL16W 5+75N	5	2	23	.11	.104	12	13	.11	76	.01	6	.81	.02	.05	1	9
STD C/AU-S	14	21	56	.49	.089	38	58	.89	175	.08	33	1.86	.08	.14	13	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL16W 5+50N	1	28	144	129	.7	23	12	1443	3.43	98	5	ND	1	12	1	4	2	23	.08	.197	10	11	.09	82	.01	2	.88	.01	.06	1	8
CL16W 5+25N	1	40	67	160	.8	46	16	839	4.57	60	5	ND	3	13	1	2	2	30	.11	.089	13	16	.27	63	.01	2	1.25	.02	.04	1	13
CL16W 5+00N	1	38	280	344	3.8	40	12	752	4.42	170	5	ND	3	13	1	2	2	30	.15	.115	13	20	.28	52	.01	4	1.70	.02	.06	1	17
CL16W 4+75N	1	38	320	307	3.0	40	12	836	4.45	209	5	ND	3	12	1	2	2	29	.13	.101	14	14	.26	55	.01	3	1.36	.02	.06	1	15
CL16W 4+50N	2	15	204	175	2.4	12	4	340	2.40	165	5	ND	2	10	1	3	2	19	.06	.096	15	9	.11	52	.01	2	1.02	.02	.06	1	10
CL16W 4+25N	2	24	498	489	7.0	11	5	909	3.05	429	5	ND	3	12	2	3	2	16	.09	.084	18	9	.15	85	.01	3	1.11	.02	.10	1	41
CL16W 4+00N	2	19	388	415	4.4	11	5	879	2.79	351	5	ND	3	10	1	2	2	19	.08	.087	17	9	.16	66	.01	2	1.44	.02	.09	1	42
CL16W 3+75N	2	22	394	398	1.9	13	7	915	3.05	346	5	ND	3	13	2	3	2	25	.14	.073	16	13	.25	67	.02	3	1.24	.02	.08	1	29
CL16W 3+50N	1	20	335	357	1.9	12	7	999	3.03	275	5	ND	4	16	4	2	2	27	.19	.081	16	14	.25	92	.03	2	.99	.02	.07	1	63
CL16W 3+25N	1	12	85	122	2.8	8	3	131	1.83	68	5	ND	2	9	1	2	2	23	.05	.052	13	9	.16	90	.01	5	1.44	.02	.08	1	16
CL16W 3+00N	1	21	129	240	1.3	19	7	581	3.89	116	5	ND	2	10	1	2	2	35	.08	.090	13	16	.27	84	.01	2	2.01	.02	.09	1	8
CL16W 2+75N	1	15	132	126	1.8	11	3	136	3.18	119	5	ND	1	11	1	2	2	31	.09	.077	12	16	.16	87	.01	2	1.67	.01	.06	1	11
CL16W 2+50N	1	14	96	66	1.6	7	2	62	2.32	55	5	ND	3	9	1	2	2	28	.04	.073	14	15	.13	72	.01	2	1.86	.01	.05	1	1
CL16W 2+25N	2	22	170	175	1.7	16	6	704	4.02	160	5	ND	2	8	1	2	2	35	.04	.109	13	17	.17	61	.01	4	1.52	.01	.06	1	1
CL16W 2+00N	2	33	172	261	1.9	31	13	955	4.27	125	5	ND	3	16	2	3	2	34	.18	.099	15	21	.36	94	.02	7	1.40	.02	.06	1	1
CL16W 1+75N	1	57	104	212	1.1	52	18	1140	5.06	71	5	ND	3	32	1	2	2	30	.33	.107	14	17	.32	127	.01	7	1.02	.03	.05	1	1
CL16W 1+50N	2	70	85	208	1.0	64	24	1876	5.24	64	5	ND	3	24	1	3	2	30	.22	.089	13	17	.34	141	.01	2	1.10	.02	.04	1	1
CL16W 1+25N	2	48	31	147	.6	73	25	1207	4.33	45	5	ND	3	13	1	2	2	20	.14	.054	8	15	.31	70	.01	2	.87	.02	.05	1	1
CL16W 1+00N	2	44	81	212	1.6	48	19	1301	4.36	92	5	ND	2	30	2	5	2	23	.27	.098	13	14	.26	138	.01	2	1.03	.02	.07	1	2
CL16W 0+75N	2	43	72	208	.5	55	22	1422	4.92	107	5	ND	3	20	1	2	2	27	.20	.073	13	16	.29	130	.01	2	1.19	.02	.06	1	2
CL16W 0+50N	2	38	51	162	.5	39	12	459	4.43	92	5	ND	2	12	1	3	2	27	.10	.091	12	13	.20	76	.01	5	1.04	.02	.05	1	7
CL16W 0+25N	2	44	67	185	.6	44	19	1172	4.92	93	5	ND	2	12	1	2	2	28	.10	.094	14	17	.28	113	.01	2	1.26	.02	.05	1	9
CL16W 0+00N	2	44	77	239	1.1	41	12	637	5.10	150	5	ND	3	15	1	3	2	30	.15	.090	14	17	.26	95	.01	2	1.31	.02	.05	1	1
CL15W 9+00N	1	30	46	116	.2	31	8	524	4.53	41	5	ND	1	11	1	2	2	41	.09	.085	9	20	.30	60	.01	2	1.60	.02	.06	1	1
CL15W 8+75N	2	52	67	163	1.1	62	18	1387	4.98	67	5	ND	4	19	1	4	2	20	.10	.084	19	13	.17	90	.01	2	.90	.02	.07	1	3
CL15W 8+50N	2	57	39	159	.6	74	18	960	4.08	71	5	ND	6	38	1	4	2	15	.22	.063	20	13	.15	161	.01	2	.53	.02	.06	1	1
CL15W 8+25N	2	31	53	118	.7	39	9	604	3.65	54	5	ND	3	11	1	2	2	21	.05	.152	17	14	.11	100	.01	2	1.24	.02	.07	1	4
CL15W 8+00N	4	47	36	148	.7	67	12	644	4.59	68	5	ND	5	7	1	2	2	25	.03	.078	23	20	.29	55	.01	8	1.60	.02	.07	1	1
CL15W 7+75N	4	60	81	205	.4	58	25	1931	4.82	89	5	ND	2	14	1	7	2	22	.01	.086	14	10	.08	95	.01	2	.84	.01	.07	1	1
CL15W 7+50N	2	9	91	223	.5	11	3	1547	2.32	40	5	ND	4	12	1	2	2	4	.03	.053	23	3	.05	228	.01	2	1.41	.01	.07	1	1
CL15W 7+25N	2	22	57	151	.4	22	6	1021	3.13	42	5	ND	2	13	1	3	2	19	.06	.148	15	8	.07	113	.01	2	1.29	.01	.07	1	1
CL15W 7+00N	1	18	55	83	.7	18	5	205	2.42	41	5	ND	2	8	1	2	2	24	.02	.121	14	11	.06	56	.01	2	1.13	.01	.06	1	1
CL15W 6+75N	2	38	53	154	.3	39	14	1400	5.62	57	5	ND	2	9	1	2	2	32	.05	.121	9	22	.27	82	.01	2	1.77	.02	.05	1	2
CL15W 6+50N	2	35	110	154	.4	26	10	1749	5.01	84	5	ND	2	9	1	5	2	38	.03	.127	12	19	.13	130	.01	2	1.49	.02	.05	1	2
CL15W 6+25N	1	47	269	212	1.4	39	15	1174	6.74	245	5	ND	2	9	1	3	2	40	.06	.192	10	28	.25	74	.03	2	1.71	.01	.05	1	16
CL15W 6+00N	1	26	91	79	.8	27	9	1171	2.54	73	5	ND	2	13	1	5	2	21	.07	.087	15	12	.07	57	.01	2	.70	.02	.08	1	1
STD C/AU-S	18	58	44	132	7.4	68	27	901	4.00	40	21	7	36	48	18	15	20	56	.48	.089	36	61	.88	171	.08	32	1.84	.08	.13	11	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL15W 5+75N	2	20	485	361	2.8	15	5	2037	3.07	200	5	ND	3	18	3	6	2	14	.09	.092	15	4	.09	64	.01	2	.88	.01	.05	1	43
CL15W 5+50N	4	21	282	309	1.3	14	5	1730	3.04	191	5	ND	2	15	2	9	2	13	.07	.082	17	3	.07	62	.01	2	.78	.01	.05	2	41
CL15W 5+25N	2	28	378	333	2.1	25	8	975	4.02	337	5	ND	3	9	1	9	2	22	.06	.086	16	11	.12	43	.01	2	.92	.01	.05	1	60
CL15W 5+00N	1	23	338	322	2.3	19	6	646	3.47	231	5	ND	2	12	1	7	2	27	.10	.105	13	14	.17	67	.01	2	1.29	.01	.06	1	41
CL15W 4+75N	1	25	346	343	2.7	23	7	558	3.92	280	5	ND	3	12	1	11	2	30	.12	.108	13	15	.22	58	.01	8	2.08	.02	.06	3	28
CL15W 4+50N	2	21	246	243	1.7	18	6	1273	3.57	212	5	ND	2	13	1	7	2	30	.10	.104	13	12	.17	82	.01	4	1.18	.02	.08	2	7
CL15W 4+25N	2	20	246	224	3.3	15	6	775	3.47	218	5	ND	3	9	1	4	2	31	.06	.085	13	16	.16	55	.01	2	1.49	.01	.05	1	19
CL15W 4+00N	2	37	556	548	2.4	28	11	1608	3.85	367	5	ND	4	13	3	9	2	28	.13	.089	15	15	.26	80	.02	5	1.39	.02	.07	1	33
CL15W 3+75N	2	57	585	428	4.8	37	15	1388	4.48	314	5	ND	4	21	4	51	2	27	.22	.107	17	14	.25	137	.01	2	.95	.02	.05	1	29
CL15W 3+50N	1	56	436	347	3.5	40	16	1287	4.54	184	5	ND	2	23	3	13	2	28	.27	.128	16	15	.23	138	.01	2	.85	.02	.05	1	27
CL15W 3+25N	1	52	354	342	3.7	38	16	1267	4.41	163	5	ND	4	21	3	14	2	31	.22	.105	17	18	.30	136	.01	10	1.09	.02	.06	1	18
CL15W 3+00N	1	37	217	301	1.6	31	12	963	3.99	131	5	ND	4	15	2	6	2	31	.18	.095	15	18	.29	111	.01	6	1.33	.02	.06	1	19
CL15W 2+75N	1	45	349	346	4.3	35	13	1220	4.21	190	5	ND	4	14	3	8	2	28	.19	.115	14	17	.23	85	.01	2	1.14	.02	.05	1	18
CL15W 2+50N	1	34	280	296	2.6	29	13	1722	3.71	141	5	ND	3	18	4	6	2	24	.18	.106	15	14	.17	144	.01	2	1.06	.02	.07	1	8
CL15W 2+25N	1	45	117	232	1.4	56	15	842	4.53	110	5	ND	4	22	1	6	2	24	.21	.077	13	12	.19	83	.01	2	.60	.02	.04	1	9
CL15W 2+00N	1	44	134	253	1.3	46	16	1080	4.55	89	7	ND	3	22	2	7	2	36	.24	.096	14	21	.37	119	.01	2	1.04	.02	.07	1	19
CL15W 1+75N	2	34	141	281	.8	30	12	1200	3.84	126	5	ND	2	16	2	2	2	29	.18	.076	12	18	.30	102	.01	2	1.26	.02	.06	1	40
CL15W 1+50N	2	34	178	345	1.4	31	13	1569	3.93	148	5	ND	2	35	3	4	2	29	.37	.093	13	19	.32	160	.01	3	1.37	.03	.08	1	3
CL15W 1+25N	1	40	207	333	2.0	37	13	1129	4.17	136	5	ND	4	22	3	5	2	27	.23	.104	16	14	.25	132	.01	2	.97	.02	.09	1	8
CL15W 1+00N	1	47	202	296	2.0	46	16	1138	4.61	121	5	ND	4	25	3	5	2	33	.30	.103	14	21	.35	144	.01	2	1.06	.03	.07	1	14
CL15W 0+75N	1	45	212	290	2.1	39	14	997	4.42	132	5	ND	3	26	2	7	2	32	.31	.110	16	20	.33	137	.01	12	1.01	.03	.07	1	5
CL15W 0+50N	1	38	188	288	1.3	36	12	988	4.15	128	5	ND	3	21	2	4	2	29	.25	.103	15	16	.25	150	.01	6	1.01	.02	.06	1	10
CL15W 0+25N	1	32	132	241	1.1	33	12	749	3.79	100	5	ND	2	17	1	5	2	24	.19	.100	12	15	.22	70	.01	3	.80	.02	.04	1	5
CL15W 0+00N	1	37	122	225	.8	37	13	804	4.14	90	5	ND	3	21	1	5	2	28	.27	.112	12	18	.28	124	.01	2	.99	.03	.04	1	11
CL14W 13+00N	1	11	35	35	1.2	5	2	46	.93	9	5	ND	1	9	1	2	2	18	.03	.106	9	13	.08	49	.01	2	1.40	.01	.05	1	5
CL14W 12+75N	2	21	36	83	.5	14	7	1518	5.17	28	5	ND	1	9	1	2	2	52	.05	.211	6	17	.25	56	.02	2	1.85	.02	.04	1	1
CL14W 12+50N	1	19	29	73	.4	14	5	288	4.29	24	5	ND	1	11	1	2	2	53	.06	.083	7	15	.22	55	.01	2	1.81	.02	.04	2	1
CL14W 12+25N	2	23	31	85	.4	11	4	941	3.68	21	5	ND	1	10	1	2	2	39	.03	.116	9	16	.12	84	.01	2	1.08	.01	.06	3	1
CL14W 12+00N	2	38	71	205	.6	30	15	1498	4.59	44	5	ND	2	20	1	2	2	34	.19	.122	12	16	.31	117	.01	2	1.48	.02	.07	1	6
CL14W 11+75N	1	42	58	160	.7	26	11	1011	4.14	40	5	ND	2	20	1	3	2	36	.19	.141	12	18	.38	123	.01	2	1.57	.02	.06	1	1
CL14W 11+50N	1	50	49	163	.6	76	24	1916	7.44	25	5	ND	3	75	1	4	2	50	.22	.146	18	48	.85	372	.01	2	2.00	.03	.10	1	3
CL14W 11+25N	1	29	49	103	.8	28	11	1154	3.97	38	5	ND	2	18	1	4	2	36	.14	.117	10	17	.19	151	.01	2	1.48	.02	.06	1	1
CL14W 11+00N	1	21	36	85	.4	17	5	302	3.92	33	5	ND	1	10	1	2	2	44	.06	.212	7	18	.20	61	.01	2	1.61	.02	.06	1	1
CL14W 10+75N	2	20	43	93	.1	16	8	1223	3.45	34	5	ND	2	8	1	2	2	31	.03	.076	9	9	.10	62	.01	2	1.00	.01	.05	1	1
CL14W 10+50N	3	16	58	83	.7	12	8	2220	3.28	31	5	ND	1	15	1	3	2	28	.09	.107	11	8	.07	85	.01	2	1.11	.02	.08	2	2
CL14W 10+25N	1	24	60	106	1.1	18	6	509	4.09	37	5	ND	1	7	1	2	2	35	.03	.103	8	16	.19	50	.01	2	1.88	.01	.03	1	1
STD C/AU-S	18	59	40	133	7.4	69	28	1048	4.02	43	22	8	37	49	18	18	22	57	.49	.091	37	61	.87	176	.08	33	1.83	.08	.14	14	47

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL14W 10+00N	1	30	158	169	2.1	22	8	686	4.11	100	5	ND	1	13	1	2	2	47	.11	.089	9	20	.29	98	.01	2	1.93	.02	.08	2	28
CL14W 9+75N	1	17	25	85	1.5	12	5	453	3.27	18	5	ND	1	11	1	2	2	46	.05	.091	7	18	.20	135	.01	5	1.67	.02	.06	1	1
CL14W 9+50N	1	30	29	150	.6	25	9	710	4.06	21	5	ND	2	93	1	2	2	45	.64	.134	13	23	.50	269	.01	2	2.40	.03	.09	2	1
CL14W 9+25N	1	52	40	137	.5	60	14	877	4.20	36	5	ND	3	23	1	2	2	21	.14	.073	11	14	.18	73	.01	3	.83	.02	.06	1	1
CL14W 9+00N	1	51	59	145	.7	55	16	869	3.52	52	5	ND	3	18	1	2	2	19	.17	.066	16	14	.19	97	.01	3	.82	.02	.07	1	1
CL14W 8+75N	1	54	85	168	1.0	67	17	1085	4.01	76	5	ND	4	19	1	2	2	17	.13	.056	16	13	.20	84	.01	4	.68	.02	.07	1	15
CL14W 8+50N	1	56	41	135	.6	79	18	1032	4.00	46	5	ND	4	16	1	2	2	21	.12	.052	16	19	.28	74	.01	2	.97	.02	.08	1	1
CL14W 8+25N	1	44	46	102	.5	44	11	754	2.58	31	5	ND	2	15	1	2	2	16	.25	.049	14	13	.27	106	.01	2	.72	.02	.06	1	1
CL14W 8+00N	1	40	35	99	.4	43	15	668	3.12	30	5	ND	2	7	1	2	2	12	.08	.044	8	8	.09	40	.01	3	.42	.02	.06	1	2
CL14W 7+75N	3	57	86	341	2.7	55	28	3004	7.89	114	5	ND	3	30	4	2	2	25	.23	.151	21	9	.17	211	.01	11	1.02	.02	.07	1	2
CL14W 7+50N	1	34	41	138	.8	29	9	501	3.86	39	5	ND	1	9	1	2	2	25	.04	.185	8	13	.07	91	.01	2	1.11	.01	.06	1	8
CL14W 7+25N	1	36	39	123	.6	45	14	1064	3.98	49	5	ND	1	11	1	2	2	19	.09	.132	9	13	.08	109	.01	5	.69	.02	.06	1	1
CL14W 7+00N	1	36	106	172	.4	31	13	1858	4.05	45	5	ND	1	14	1	2	2	27	.07	.113	11	10	.08	87	.01	2	.82	.02	.08	1	3
CL14W 6+75N	3	27	53	145	.8	33	10	2118	3.70	56	5	ND	1	20	1	2	2	27	.08	.187	8	13	.07	209	.01	3	1.27	.02	.07	1	1
CL14W 6+50N	1	29	69	89	.2	20	10	3568	3.32	57	5	ND	1	6	1	2	2	29	.01	.094	9	14	.04	81	.01	7	.70	.02	.07	1	11
CL14W 6+25N	1	29	75	87	1.0	18	7	1270	4.87	99	5	ND	1	6	1	2	2	32	.03	.203	7	22	.06	45	.01	3	.91	.01	.06	1	25
CL14W 6+00N	1	45	81	119	.4	36	15	1639	3.65	52	5	ND	1	6	1	2	2	19	.02	.067	5	9	.04	50	.01	2	.41	.01	.04	1	1
CL14W 5+75N	1	17	185	86	1.4	20	6	414	2.39	120	5	ND	1	12	1	6	2	16	.10	.080	5	4	.05	47	.01	2	.59	.02	.06	1	72
CL14W 5+50N	1	25	154	133	.5	28	10	2297	3.27	69	5	ND	2	7	1	6	2	17	.04	.065	10	7	.05	62	.01	2	.49	.01	.06	2	7
CL14W 5+25N	1	19	74	101	.3	35	20	1869	3.75	82	5	ND	2	10	1	2	2	24	.10	.106	5	11	.13	42	.01	2	.89	.02	.06	1	53
CL14W 5+00N	1	21	85	110	.3	31	11	2203	3.58	77	5	ND	1	9	1	3	2	33	.03	.087	14	14	.13	69	.01	2	.83	.01	.05	1	17
CL14W 4+75N	2	27	366	257	2.6	23	13	3266	3.61	114	5	ND	2	80	2	6	2	32	.27	.156	12	15	.20	214	.01	5	1.12	.02	.14	1	5
CL14W 4+50N	18	64	490	1629	3.7	12	8	6795	17.94	176	5	ND	4	32	8	10	2	31	.28	.214	17	7	.26	254	.01	6	1.58	.02	.13	4	3
CL14W 4+25N	3	29	240	499	2.1	15	7	1400	4.29	71	5	ND	2	15	2	3	2	30	.15	.086	14	14	.13	100	.01	2	1.42	.01	.07	2	2
CL14W 4+00N	2	15	217	412	.9	9	6	2282	3.67	379	5	ND	2	10	4	3	2	25	.07	.075	18	6	.09	82	.01	2	.85	.01	.07	2	23
CL14W 3+75N	2	21	207	592	2.2	16	7	1566	3.91	164	5	ND	3	13	4	2	2	29	.10	.083	14	13	.19	133	.01	2	1.57	.01	.07	3	46
CL14W 3+50N	4	80	84	384	.9	71	36	3411	6.38	60	5	ND	4	32	4	2	2	40	.15	.074	23	14	.36	286	.01	2	1.10	.02	.05	1	1
CL14W 3+25N	5	126	96	368	.3	85	45	4770	6.59	91	5	ND	2	40	4	2	2	32	.19	.076	10	23	.31	149	.01	2	1.19	.02	.05	2	2
CL14W 3+00N	4	108	40	323	.3	93	44	3080	5.98	56	5	ND	3	23	3	2	2	28	.06	.041	6	21	.26	128	.01	6	.95	.01	.03	1	1
CL14W 2+75N	4	104	46	358	.5	90	40	2527	6.02	64	5	ND	3	29	5	2	2	29	.11	.064	8	19	.26	106	.01	2	.96	.01	.04	1	1
CL14W 2+50N	1	38	155	280	.9	30	11	1064	3.89	119	5	ND	2	22	1	2	2	29	.17	.094	13	15	.27	103	.01	6	1.32	.02	.06	1	10
CL14W 2+25N	1	30	150	259	.5	33	16	1382	3.92	108	5	ND	3	24	1	2	2	29	.23	.085	16	15	.28	140	.01	10	1.28	.03	.07	1	2
CL14W 2+00N	1	23	104	182	1.9	22	7	398	3.60	78	5	ND	3	10	1	2	2	35	.08	.081	13	16	.19	106	.01	5	1.26	.02	.06	1	13
CL14W 1+75N	1	19	109	125	.9	15	5	223	2.43	71	5	ND	3	8	1	2	2	28	.04	.035	14	9	.12	94	.01	3	1.10	.01	.03	1	11
CL14W 1+50N	2	47	53	162	.4	45	22	1041	6.63	76	5	ND	4	8	1	2	2	49	.04	.085	13	18	.16	77	.01	2	1.18	.01	.05	1	1
CL14W 1+25N	7	53	43	210	.2	83	40	4338	5.39	53	5	ND	3	42	2	2	2	34	.10	.096	10	18	.17	152	.01	2	.76	.01	.06	1	1
STD C/AU-S	18	59	43	132	7.5	69	28	1047	4.01	43	15	8	38	50	18	17	18	58	.48	.092	38	59	.88	180	.08	34	1.84	.09	.14	12	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL14W 1+00N	2	42	75	180	.4	47	17	1683	4.98	49	5	ND	2	11	1	2	2	36	.06	.071	10	21	.29	80	.01	4	1.35	.02	.06	1	1
CL14W 0+75N	2	42	109	187	1.2	44	13	792	4.84	59	5	ND	2	9	1	2	2	34	.05	.069	11	21	.28	68	.01	2	1.27	.01	.05	1	2
CL14W 0+50N	3	28	97	158	.3	29	8	509	4.48	71	5	ND	3	8	1	4	2	33	.05	.098	13	17	.19	46	.01	2	1.11	.01	.05	1	10
CL14W 0+25N	2	39	26	140	.5	38	8	419	3.32	76	5	ND	3	7	1	8	3	23	.07	.050	22	8	.05	55	.01	4	.62	.01	.07	1	1
CL14W 0+00N	3	24	43	142	.5	21	5	324	3.23	186	5	ND	2	6	1	5	2	22	.03	.059	18	5	.06	56	.01	2	.84	.01	.06	1	12
CL13W 13+00N	3	33	47	117	.4	25	13	1426	4.85	45	5	ND	2	14	1	2	2	33	.08	.150	9	14	.20	80	.01	2	1.82	.02	.06	1	1
CL13W 12+75N	1	18	51	97	.1	15	9	1076	4.62	35	5	ND	1	62	1	2	2	55	.37	.106	8	16	.36	74	.01	3	1.63	.03	.05	1	1
CL13W 12+50N	1	7	23	27	.6	4	1	78	.93	9	5	ND	1	9	1	2	2	22	.03	.044	11	9	.09	61	.01	2	1.49	.01	.04	2	1
CL13W 12+25N	1	12	32	66	1.2	12	3	205	2.16	9	5	ND	1	12	1	2	2	40	.03	.095	9	20	.21	143	.01	2	2.93	.02	.08	1	1
CL13W 12+00N	1	12	22	61	.3	9	3	358	2.32	15	5	ND	1	15	1	2	2	41	.10	.072	9	9	.14	92	.01	4	1.22	.02	.05	1	1
CL13W 11+75N	1	16	23	80	.3	9	4	312	2.48	13	5	ND	1	14	1	2	2	53	.09	.071	10	11	.10	96	.01	5	.99	.02	.06	1	1
CL13W 11+50N	2	34	77	180	.6	28	12	1129	4.49	43	5	ND	1	27	1	2	2	34	.26	.116	12	16	.33	117	.01	2	1.52	.02	.07	1	2
CL13W 11+25N	1	30	38	159	.4	23	11	933	4.71	26	5	ND	1	11	1	2	2	51	.06	.113	11	22	.47	87	.02	3	2.69	.02	.08	3	1
CL13W 11+00N	1	13	30	56	.2	9	3	212	2.23	18	5	ND	1	8	1	2	2	35	.03	.090	8	14	.15	61	.01	2	1.44	.01	.04	1	3
CL13W 10+75N	1	21	61	84	1.0	15	6	571	3.57	31	5	ND	1	7	1	2	2	38	.03	.075	8	17	.21	52	.01	3	1.85	.01	.04	2	26
CL13W 10+50N	2	14	59	169	.4	10	3	542	2.77	55	5	ND	1	16	1	2	2	30	.11	.216	10	17	.17	78	.01	2	1.90	.02	.08	1	6
CL13W 10+25N	2	13	38	110	1.4	10	3	320	2.14	22	6	ND	1	17	1	2	2	28	.10	.163	10	14	.14	110	.01	3	1.90	.02	.07	1	1
CL13W 10+00N	2	15	47	96	.9	11	4	463	2.57	16	5	ND	1	10	1	2	2	36	.06	.130	8	16	.22	68	.01	2	2.07	.02	.04	2	1
CL13W 9+75N	1	11	46	61	1.3	5	2	187	1.53	14	5	ND	1	10	1	2	2	75	.03	.085	10	10	.09	88	.01	2	1.66	.01	.05	1	3
CL13W 9+50N	1	14	51	76	.3	8	4	402	2.23	30	5	ND	1	11	1	2	2	42	.07	.053	9	10	.11	58	.01	4	1.00	.02	.06	1	1
CL13W 9+25N	1	10	29	50	.8	6	2	218	1.50	13	5	ND	1	10	1	2	2	28	.03	.091	9	15	.10	75	.01	2	1.40	.01	.04	2	1
CL13W 9+00N	2	45	33	128	.5	47	11	687	4.40	37	5	ND	2	20	1	2	2	25	.11	.126	9	17	.13	91	.01	2	1.05	.02	.05	1	2
CL13W 8+75N	3	46	166	497	1.9	37	16	1280	4.91	54	5	ND	3	30	8	2	2	22	.29	.129	19	8	.10	111	.01	13	.58	.02	.06	1	2
CL13W 8+50N	2	48	56	270	.9	51	19	1182	4.46	42	5	ND	3	34	4	2	2	19	.31	.104	15	11	.15	141	.01	2	.62	.02	.06	1	1
CL13W 8+25N	2	86	55	189	.4	82	26	1390	5.57	34	5	ND	4	14	1	2	2	29	.07	.066	13	28	.44	90	.01	4	1.50	.02	.08	2	9
CL13W 8+00N	7	122	91	220	1.1	176	64	6009	10.19	67	5	ND	8	56	1	3	2	45	.31	.075	29	38	.51	718	.01	6	1.37	.03	.08	1	11
CL13W 7+75N	2	33	43	102	.4	30	9	633	3.19	30	5	ND	2	11	1	2	2	25	.04	.085	13	15	.08	81	.01	4	.84	.02	.07	1	17
CL13W 7+50N	1	19	93	209	.4	30	16	759	7.05	61	5	ND	2	58	1	2	2	137	.43	.207	14	70	1.37	217	.08	6	3.60	.05	.05	2	4
CL13W 7+25N	1	16	78	77	.8	11	2	85	1.67	43	6	ND	2	9	1	3	2	19	.03	.080	17	8	.06	54	.01	2	.93	.01	.04	1	12
CL13W 7+00N	1	20	62	65	.9	14	4	345	2.15	48	5	ND	1	8	1	2	2	25	.03	.084	11	11	.04	44	.01	3	.70	.02	.05	1	2
CL13W 6+75N	2	36	232	124	3.0	14	5	402	3.67	185	5	ND	1	8	1	9	2	46	.02	.096	8	15	.06	42	.01	2	.89	.01	.05	1	37
CL13W 6+50N	1	19	1271	125	3.9	7	2	129	1.35	665	5	ND	2	6	1	13	2	15	.02	.046	15	4	.02	40	.01	2	.63	.01	.04	1	345
CL13W 6+25N	2	35	511	274	4.6	22	10	1585	3.77	168	5	ND	2	19	3	2	2	33	.15	.198	7	16	.14	82	.01	4	1.50	.02	.06	1	6
CL13W 6+00N	2	27	133	101	.7	25	6	724	2.67	67	5	ND	1	11	1	4	2	20	.06	.139	10	6	.06	66	.01	2	.73	.02	.07	1	38
CL13W 5+75N	1	27	91	230	.4	26	7	764	3.91	176	5	ND	1	32	1	2	3	35	.34	.114	10	11	.15	94	.01	2	.87	.02	.08	1	23
CL13W 5+50N	2	13	79	216	.7	8	4	571	3.11	44	5	ND	1	9	1	2	2	50	.04	.069	10	13	.32	64	.01	5	1.90	.02	.05	1	3
CL13W 5+25N	2	15	140	190	.8	10	3	478	2.89	87	5	ND	1	8	1	4	3	39	.03	.072	12	14	.11	60	.01	2	1.43	.01	.04	1	9
STD C/AU-S	18	57	42	132	7.2	68	27	1020	4.02	39	20	7	37	48	18	16	19	55	.49	.088	36	60	.88	171	.08	31	1.83	.08	.14	13	48

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL13W 5+00N	2	21	269	313	3.2	14	6	556	6.00	318	5	ND	3	14	2	7	2	39	.12	.181	10	17	.22	98	.01	2	2.56	.02	.06	1	30
CL13W 4+75N	3	19	331	432	.9	11	7	4196	3.24	369	5	ND	2	11	4	9	2	27	.05	.071	15	9	.10	155	.01	2	1.14	.01	.06	1	1
CL13W 4+50N	3	20	286	401	.9	13	8	3846	3.58	212	5	ND	3	10	3	5	2	29	.06	.092	14	14	.15	163	.01	2	1.43	.01	.07	1	27
CL13W 4+25N	3	21	310	505	1.5	11	6	2772	3.52	432	5	ND	4	12	5	5	2	25	.08	.085	15	12	.16	162	.01	2	1.55	.02	.06	1	53
CL13W 4+00N	3	31	541	1002	5.4	13	8	3283	3.94	778	5	ND	5	30	13	9	2	20	.21	.072	21	12	.20	263	.01	2	1.31	.02	.07	1	63
CL13W 3+75N	2	16	485	767	2.2	11	6	2707	2.35	245	5	ND	6	41	13	3	2	4	.32	.082	20	1	.05	133	.01	2	.34	.01	.05	1	53
CL13W 3+50N	3	29	803	1270	4.6	17	7	3067	3.39	361	5	ND	7	39	19	7	2	6	.31	.090	24	3	.06	156	.01	6	.38	.02	.06	1	60
CL13W 3+00N	2	24	285	594	.8	17	7	1370	3.93	280	6	ND	4	11	3	4	2	23	.10	.078	16	13	.23	151	.01	2	1.02	.02	.06	1	13
CL13W 2+75N	2	18	251	781	1.3	10	4	1930	3.11	376	5	ND	4	16	9	4	2	9	.16	.059	22	2	.10	122	.01	2	.86	.01	.06	1	42
CL13W 2+50N	5	35	262	949	1.8	27	13	3252	5.78	476	5	ND	4	25	10	6	2	22	.18	.092	23	10	.11	151	.01	2	.80	.01	.08	1	33
CL13W 2+25N	4	55	179	529	1.8	113	43	2904	5.84	192	5	ND	4	18	6	2	2	19	.08	.057	17	11	.09	87	.01	2	.56	.01	.05	1	5
CL13W 2+00N	6	46	356	969	2.0	62	31	3536	6.41	342	5	ND	4	21	11	3	2	23	.19	.090	22	9	.12	169	.01	2	1.18	.01	.08	1	8
CL13W 1+75N	4	38	198	485	.9	49	19	1919	5.03	169	5	ND	3	12	4	4	2	20	.08	.071	15	13	.12	86	.01	2	.83	.01	.07	1	24
CL13W 1+50N	5	47	79	613	.5	62	20	1728	6.61	607	5	ND	3	16	6	7	2	19	.05	.050	13	7	.09	73	.01	2	.68	.01	.09	1	25
CL13W 1+25N	4	41	78	301	.1	40	18	1898	5.25	153	5	ND	3	10	1	2	2	23	.03	.083	12	13	.12	67	.01	2	.94	.01	.05	1	9
CL13W 1+00N	5	40	52	276	.6	40	17	1045	5.17	115	5	ND	3	8	1	2	2	25	.03	.079	11	15	.16	51	.01	2	1.12	.01	.04	1	26
CL13W 0+75N	3	53	74	405	.2	48	21	1777	5.39	130	5	ND	3	11	3	3	2	24	.10	.077	10	18	.20	113	.01	2	1.10	.01	.04	1	10
CL13W 0+50N	2	34	110	184	.1	31	11	1648	4.58	67	5	ND	3	11	1	4	2	32	.13	.153	10	17	.22	76	.01	3	1.17	.02	.06	1	1
CL13W 0+25N	2	26	23	133	.2	18	5	203	3.34	51	5	ND	2	7	1	3	2	39	.02	.039	14	7	.06	38	.01	3	.73	.01	.03	1	1
CL13W 0+00N	2	21	48	103	.6	15	6	1023	2.57	45	5	ND	3	10	1	4	2	25	.04	.058	16	8	.07	135	.01	3	.80	.02	.05	1	5
CL12W 13+00N	1	11	22	48	.6	6	2	191	1.82	11	5	ND	1	11	1	3	2	36	.05	.072	8	11	.10	76	.01	2	1.27	.01	.04	3	1
CL12W 12+75N	1	9	16	37	.3	8	2	114	1.22	10	10	ND	1	10	1	3	2	23	.05	.052	10	7	.06	63	.01	2	1.01	.01	.04	1	1
CL12W 12+50N	1	17	25	69	.3	17	5	256	2.66	25	5	ND	1	11	1	4	2	36	.06	.065	9	13	.12	67	.01	2	1.18	.01	.04	1	1
CL12W 12+25N	1	18	29	90	.8	17	5	314	3.04	18	5	ND	1	15	1	3	2	37	.11	.130	7	19	.32	105	.01	3	1.81	.02	.06	1	1
CL12W 12+00N	1	15	21	63	.1	11	4	193	3.48	19	5	ND	1	11	1	2	2	58	.05	.066	5	17	.19	66	.01	2	1.60	.02	.03	1	1
CL12W 11+75N	1	15	22	41	1.2	6	2	85	1.31	8	5	ND	1	9	1	2	2	30	.05	.060	6	13	.17	65	.01	2	2.31	.01	.03	1	3
CL12W 11+50N	2	38	23	198	2.1	31	11	1228	5.40	19	5	ND	2	57	1	2	2	60	.64	.218	10	31	.61	617	.01	2	4.93	.05	.16	1	1
CL12W 11+25N	1	18	25	81	.7	14	5	278	3.07	15	5	ND	1	8	1	2	2	42	.04	.092	6	24	.30	74	.01	4	2.42	.02	.05	1	1
CL12W 11+00N	1	14	26	75	.3	6	3	341	2.58	12	5	ND	1	9	1	2	2	38	.03	.087	10	10	.10	54	.01	2	1.43	.02	.05	1	1
CL12W 10+75N	1	15	39	93	1.5	10	4	233	2.13	15	5	ND	1	13	1	2	2	31	.07	.111	7	16	.22	113	.01	2	2.23	.02	.06	1	1
CL12W 10+50N	1	14	35	92	1.0	14	4	195	2.79	19	7	ND	2	19	1	2	2	43	.15	.065	7	18	.32	155	.01	2	2.30	.02	.06	1	1
CL12W 10+25N	1	16	28	75	.4	17	5	237	2.65	16	5	ND	1	7	1	2	2	33	.03	.078	5	17	.25	68	.01	2	1.71	.02	.03	1	7
CL12W 10+00N	1	8	16	43	1.6	9	3	287	1.26	10	5	ND	2	28	1	2	2	20	.26	.118	9	10	.11	226	.01	2	1.16	.02	.04	2	1
CL12W 9+75N	2	23	30	88	1.7	20	7	884	2.98	21	5	ND	2	12	1	5	2	22	.05	.128	10	9	.08	88	.01	2	1.04	.02	.06	1	1
CL12W 9+50N	2	35	45	120	1.1	32	12	608	3.96	30	5	ND	2	12	1	4	2	26	.05	.089	11	15	.17	69	.01	2	1.23	.02	.05	1	2
CL12W 9+25N	2	25	39	139	.6	31	9	841	3.33	32	5	ND	2	43	1	2	2	21	.34	.082	10	12	.19	145	.01	2	.97	.02	.05	1	1
CL12W 9+00N	2	12	92	507	.4	31	8	543	3.58	125	9	ND	2	26	1	4	2	34	.16	.067	7	21	.46	107	.01	3	1.75	.02	.07	2	6
STD C/AU-S	18	58	41	132	7.2	68	27	1030	4.07	41	21	8	37	48	18	18	18	56	.49	.090	36	59	.90	174	.08	32	1.86	.08	.14	15	52

SOUTHERN GOLD PROJECT-121104 FILE # 87-3381

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL12W 8+75N	1	19	159	131	.7	13	5	300	4.77	201	5	ND	1	13	1	2	2	57	.10	.125	7	20	.21	49	.01	5	1.58	.02	.03	2	5
CL12W 8+50N	1	16	129	116	1.5	9	4	2034	2.65	71	5	ND	1	16	2	2	2	47	.11	.102	9	13	.12	122	.01	2	1.40	.01	.07	2	2
CL12W 8+25N	2	59	95	226	.7	72	22	1374	4.97	57	5	ND	4	13	1	2	2	24	.15	.070	19	27	.53	55	.01	2	1.57	.02	.06	2	2
CL12W 8+00N	4	96	90	238	.8	71	34	2604	6.21	72	5	ND	4	14	1	2	2	31	.17	.083	15	25	.51	100	.01	3	1.62	.02	.06	1	8
CL12W 7+75N	3	37	97	111	1.4	22	14	6225	3.64	72	5	ND	2	10	1	2	2	37	.04	.125	14	17	.07	110	.01	2	1.08	.02	.05	1	10
CL12W 7+50N	2	33	61	95	.4	20	8	966	3.19	52	5	ND	2	8	1	2	2	33	.03	.093	18	15	.07	68	.01	2	.84	.02	.07	1	2
CL12W 7+25N	2	29	67	72	.7	18	9	1372	3.20	43	5	ND	1	9	1	2	2	29	.02	.115	13	17	.10	60	.01	4	1.14	.02	.06	1	4
CL12W 7+00N	2	26	161	70	2.0	11	4	818	2.84	101	5	ND	1	8	1	4	2	31	.02	.126	14	18	.07	49	.01	2	1.38	.01	.05	1	11
CL12W 6+75N	2	28	157	85	1.1	21	8	1027	3.62	196	5	ND	1	8	1	2	2	32	.02	.156	13	19	.13	48	.01	6	1.44	.02	.06	1	9
CL12W 6+50N	2	27	120	101	1.1	15	5	962	3.34	84	5	ND	1	8	1	2	2	38	.02	.113	12	14	.13	52	.01	2	1.47	.01	.06	1	10
CL12W 6+25N	1	17	67	67	2.5	11	5	634	1.92	37	5	ND	1	9	1	3	2	22	.03	.113	11	11	.05	55	.01	2	.90	.01	.06	1	14
CL12W 6+00N	2	71	1477	694	13.2	21	8	1106	5.95	1198	5	ND	2	15	4	24	2	36	.15	.197	13	21	.24	86	.01	9	1.98	.02	.05	1	80
CL12W 5+75N	1	14	158	89	1.3	7	2	183	1.74	94	5	ND	1	8	1	5	2	23	.03	.078	13	9	.10	56	.01	2	1.26	.01	.04	1	15
CL12W 5+50N	2	20	598	202	3.2	9	3	882	2.33	426	5	ND	1	10	1	6	2	26	.04	.077	13	10	.07	65	.01	5	.97	.01	.06	1	87
CL12W 5+25N	2	14	330	156	1.1	9	4	5675	2.10	122	5	ND	1	10	1	2	2	26	.08	.071	16	8	.09	206	.01	3	1.27	.02	.08	1	12
CL12W 5+00N	2	17	226	213	1.7	13	6	853	3.73	190	5	ND	1	9	1	3	2	42	.06	.081	11	15	.23	73	.01	3	1.73	.02	.08	3	18
CL12W 4+75N	2	18	289	798	7.2	10	4	2336	3.12	464	5	ND	3	8	4	8	2	13	.10	.153	14	7	.14	116	.01	2	2.28	.01	.08	2	50
CL12W 4+50N	5	20	673	525	.8	11	9	8440	3.80	373	5	ND	3	12	7	7	2	17	.10	.098	17	4	.09	248	.01	2	1.29	.02	.11	3	52
CL12W 4+25N	5	47	2555	954	6.2	10	8	4016	4.91	2201	5	ND	5	25	9	6	2	22	.14	.088	22	6	.10	199	.01	2	1.21	.01	.10	3	40
CL12W 4+00N	3	43	1505	1026	8.8	9	7	3967	4.45	1088	5	ND	4	14	11	6	2	29	.10	.104	21	10	.15	141	.01	2	1.50	.01	.08	4	89
CL12W 3+75N	4	33	212	459	2.5	30	15	2472	7.30	176	5	ND	4	32	4	2	2	42	.18	.114	19	14	.17	249	.01	2	1.86	.02	.10	2	11
CL12W 3+50N	3	55	355	271	2.4	42	15	1018	2.88	37	5	ND	3	11	3	3	2	9	.08	.038	16	5	.04	34	.01	2	.33	.01	.04	1	15
CL12W 3+25N	2	28	162	243	.6	31	15	1517	3.18	84	5	ND	3	10	1	2	2	14	.06	.048	18	5	.06	59	.01	2	.60	.01	.06	1	9
CL12W 3+00N	3	32	219	318	.8	34	19	2890	4.23	142	5	ND	3	15	2	2	2	23	.12	.074	16	13	.13	117	.01	4	1.06	.01	.11	1	14
CL12W 2+75N	3	39	282	333	.9	42	29	4500	4.67	176	5	ND	4	10	2	2	2	25	.06	.076	15	12	.13	106	.01	9	1.00	.02	.08	2	4
CL12W 2+50N	3	108	134	334	.6	72	34	2749	6.30	146	5	ND	4	85	1	2	2	39	.24	.069	14	37	.62	176	.01	2	2.13	.02	.07	1	5
CL12W 2+25N	5	150	2632	1000	13.9	70	25	2975	6.29	1857	5	ND	3	43	17	8	2	22	.44	.086	14	18	.40	120	.01	7	1.10	.03	.08	2	280
CL12W 2+00N	5	62	538	556	3.6	66	26	3106	5.92	316	5	ND	3	65	5	4	2	25	.42	.098	12	18	.28	150	.01	8	1.21	.02	.11	2	49
CL12W 1+75N	5	66	829	553	4.1	56	22	2924	5.55	538	5	ND	3	44	6	4	2	22	.32	.083	14	12	.26	126	.01	2	1.03	.02	.08	1	45
CL12W 1+50N	3	59	250	336	.8	59	21	1838	4.87	217	5	ND	3	20	3	2	2	20	.14	.061	13	22	.34	69	.01	2	1.01	.02	.05	1	18
CL12W 1+25N	3	55	193	340	.7	58	26	2101	5.31	177	5	ND	3	22	2	2	2	23	.21	.084	13	24	.33	87	.01	4	1.08	.02	.07	1	2
CL12W 1+00N	4	80	636	527	3.3	70	27	2655	5.67	521	5	ND	3	31	8	2	2	21	.22	.067	15	17	.29	120	.01	2	.94	.02	.06	2	37
CL12W 0+75N	4	71	111	408	1.3	90	34	2917	6.18	161	5	ND	3	29	4	2	2	22	.12	.049	14	18	.26	157	.01	2	.82	.02	.05	1	6
CL12W 0+50N	4	70	107	403	1.2	89	34	2827	6.06	158	5	ND	3	27	3	2	2	22	.11	.046	14	18	.26	146	.01	2	.85	.02	.06	1	3
CL12W 0+25N	4	59	67	327	.5	71	26	1968	5.88	125	5	ND	3	15	2	2	2	23	.06	.057	11	21	.23	82	.01	2	.89	.01	.05	1	4
CL12W 0+00N	2	23	40	102	.6	16	5	270	2.73	49	5	ND	2	7	1	2	2	30	.02	.046	13	14	.08	50	.01	4	.94	.02	.04	1	1
STD C/AU-S	18	57	38	132	7.2	68	27	1025	3.97	40	17	7	36	48	18	17	19	55	.48	.088	36	57	.87	173	.08	36	1.83	.09	.13	12	53

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL11W 13+00N	2	69	85	215	1.7	37	27	2175	6.76	24	6	ND	4	28	1	6	2	39	.25	.145	16	18	.39	214	.01	2	2.14	.02	.08	3	10
CL11W 12+75N	1	46	47	176	.9	32	15	1226	5.28	17	5	ND	2	25	1	2	2	39	.23	.178	12	13	.29	155	.01	4	2.30	.02	.07	2	7
CL11W 12+50N	1	20	25	95	.5	16	6	366	3.91	13	5	ND	1	12	1	2	2	55	.06	.115	6	18	.38	109	.01	2	2.51	.02	.07	1	1
CL11W 12+25N	1	17	27	64	.1	15	4	320	2.49	23	5	ND	1	10	1	2	2	34	.04	.078	10	11	.07	71	.01	2	1.04	.01	.04	1	7
CL11W 12+00N	1	11	21	87	.1	10	3	289	2.57	11	5	ND	1	28	1	2	2	40	.27	.082	7	13	.22	144	.01	3	1.40	.02	.04	1	3
CL11W 11+75N	1	21	40	109	1.6	18	6	278	4.78	15	5	ND	1	10	1	2	2	44	.08	.121	6	23	.41	84	.01	2	2.89	.02	.05	1	2
CL11W 11+50N	1	12	31	69	1.3	11	3	133	2.06	14	5	ND	1	7	1	2	2	35	.04	.079	6	18	.24	61	.01	2	2.20	.01	.05	1	3
CL11W 11+25N	1	6	35	36	1.6	5	1	42	.92	12	5	ND	1	8	1	2	2	27	.03	.061	8	11	.09	67	.01	2	1.46	.01	.04	1	1
CL11W 11+00N	2	32	68	190	.8	32	10	844	4.13	45	5	ND	1	43	1	4	2	36	.30	.123	10	19	.34	117	.01	2	1.76	.02	.06	2	1
CL11W 10+75N	1	37	47	210	.7	35	10	845	4.81	28	5	ND	2	26	1	2	2	40	.25	.178	8	31	.42	182	.01	2	2.92	.02	.09	1	2
CL11W 10+50N	1	29	35	76	.1	15	16	5262	5.42	12	5	ND	1	5	1	2	2	38	.03	.359	3	27	.15	62	.01	2	1.35	.01	.05	1	4
CL11W 10+25N	2	23	49	99	.2	15	12	2878	5.04	28	5	ND	1	8	1	2	2	43	.03	.256	6	20	.15	51	.01	2	1.82	.01	.07	1	3
CL11W 10+00N	1	13	24	79	.7	11	4	271	2.46	14	5	ND	1	11	1	2	2	38	.06	.104	6	19	.27	95	.01	3	1.85	.02	.05	1	2
CL11W 9+75N	2	21	80	168	1.2	17	7	1768	3.51	62	5	ND	1	44	1	2	2	40	.31	.255	15	16	.30	373	.01	2	2.56	.03	.07	1	1
CL11W 9+50N	1	22	46	108	1.2	21	4	117	1.28	9	14	ND	1	34	1	2	2	20	.31	.087	13	15	.29	227	.01	2	1.54	.03	.05	1	1
CL11W 9+25N	1	7	73	53	2.3	6	2	101	1.02	30	5	ND	1	9	1	2	2	22	.04	.084	8	11	.10	88	.01	2	1.52	.01	.04	1	26
CL11W 9+00N	1	20	83	137	1.8	14	6	635	4.41	81	5	ND	1	12	1	3	2	50	.04	.087	7	19	.19	104	.01	2	1.99	.02	.06	1	1
CL11W 8+75N	1	21	138	146	.9	21	6	368	5.44	115	5	ND	2	8	1	4	2	46	.02	.104	7	14	.17	52	.01	2	1.85	.01	.05	1	1
CL11W 8+50N	1	13	115	126	.9	7	4	264	3.15	142	5	ND	1	7	1	3	2	44	.02	.060	10	9	.15	61	.01	2	1.19	.01	.03	1	2
CL11W 8+25N	1	20	184	252	4.4	15	6	257	5.51	123	5	ND	2	10	1	2	2	51	.05	.074	5	23	.32	67	.02	2	3.37	.02	.03	1	5
CL11W 8+00N	1	17	85	104	1.1	9	3	211	2.71	93	5	ND	1	11	1	5	2	46	.05	.065	9	12	.10	64	.01	2	1.28	.02	.04	1	31
CL11W 7+50N	4	34	1332	1003	11.6	15	6	2725	4.60	648	5	ND	3	17	5	23	2	17	.10	.136	18	10	.15	147	.01	2	1.40	.01	.06	2	95
CL11W 7+25N	2	15	227	203	2.2	7	3	547	2.42	355	5	ND	2	9	2	8	2	24	.03	.084	19	8	.05	69	.01	2	1.09	.01	.05	2	6
CL11W 7+00N	2	18	347	296	11.9	7	3	413	2.25	241	5	ND	2	7	1	6	2	26	.01	.065	18	7	.06	57	.01	6	.95	.01	.03	1	47
CL11W 6+25N	2	19	452	294	4.1	8	3	777	2.49	378	5	ND	2	7	2	35	2	28	.02	.062	19	9	.06	53	.01	2	1.03	.01	.05	1	34
CL11W 6+00N	1	9	101	108	1.1	5	2	119	1.62	75	5	ND	2	5	1	4	2	29	.02	.055	14	9	.12	43	.01	2	1.53	.01	.04	1	17
CL11W 5+75N	2	14	137	140	1.4	7	3	215	3.09	139	5	ND	1	10	1	2	2	43	.05	.080	14	11	.14	54	.01	2	1.83	.02	.05	1	13
CL11W 5+50N	5	56	7245	514	43.3	2	1	196	3.21	1235	5	ND	5	9	1	27	2	9	.01	.104	28	3	.02	49	.01	10	1.01	.02	.04	1	42
CL11W 5+25N	2	13	111	174	.8	6	3	427	2.21	80	5	ND	1	6	1	5	2	26	.03	.064	17	6	.04	56	.01	2	.76	.01	.04	1	22
CL11W 5+00N	6	37	451	653	3.5	10	6	4042	3.44	299	5	ND	3	8	8	8	2	15	.04	.118	18	9	.13	157	.01	5	1.42	.01	.08	3	121
CL11W 4+75N	3	14	278	366	3.7	8	6	3502	2.97	154	5	ND	3	7	3	2	2	23	.03	.111	16	8	.11	162	.01	2	1.75	.01	.07	2	43
CL11W 4+50N	4	19	361	604	2.0	8	7	4271	3.46	363	5	ND	4	12	7	8	2	18	.10	.078	18	5	.09	203	.01	2	1.23	.01	.08	2	129
CL11W 4+25N	3	18	306	672	1.6	7	6	3431	3.45	400	5	ND	5	14	7	6	2	16	.10	.076	20	5	.09	189	.01	2	1.39	.01	.08	2	86
CL11W 4+00N	3	19	340	529	1.4	10	6	3127	3.19	328	5	ND	4	13	5	5	2	17	.07	.073	18	9	.10	214	.01	2	1.16	.01	.10	1	73
CL11W 3+75N	5	30	1004	665	4.1	15	11	6299	5.10	745	5	ND	3	65	6	13	2	23	.34	.090	13	8	.12	212	.01	2	1.26	.02	.09	2	240
CL11W 3+50N	5	43	1335	1558	7.3	17	11	5298	7.14	1511	5	ND	4	70	16	17	2	26	.30	.098	15	11	.26	197	.01	3	1.74	.02	.10	3	168
STD C/AU-S	18	58	42	132	7.1	68	27	916	4.01	44	25	8	36	49	18	17	22	56	.48	.089	36	55	.89	175	.08	33	1.84	.08	.13	14	48

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL11W 3+25N	6	83	1942	1238	66.3	76	32	2611	5.28	1173	5	ND	4	40	16	49	2	19	.28	.063	21	9	.12	116	.01	2	.52	.01	.08	1	146
CL11W 3+00N	3	68	312	341	3.3	79	37	2058	5.79	362	5	ND	3	15	5	8	2	16	.09	.047	6	6	.06	85	.01	7	.35	.01	.07	1	131
CL11W 2+75N	3	57	300	301	1.9	96	43	1411	5.47	319	5	ND	3	11	3	7	2	13	.06	.051	8	7	.06	64	.01	2	.36	.01	.06	1	32
CL11W 2+50N	7	112	3159	1791	27.8	57	27	3800	7.16	2958	5	ND	4	60	41	19	2	16	.31	.095	16	5	.14	227	.01	6	.64	.02	.08	2	230
CL11W 2+25N	7	146	4859	2278	37.7	56	25	3514	7.81	4537	5	ND	4	84	55	27	2	15	.40	.097	15	9	.15	265	.01	2	.59	.02	.10	3	450
CL11W 2+00N	6	95	4927	2359	52.2	38	24	4324	8.10	3664	5	ND	4	52	43	37	2	17	.30	.106	16	6	.15	170	.01	8	.85	.02	.11	4	370
CL11W 1+75N	5	95	4183	2445	50.3	30	17	3822	7.76	3172	5	ND	4	63	41	32	2	17	.43	.092	16	9	.16	175	.01	5	.86	.02	.10	2	194
CL11W 1+50N	6	79	3791	2370	37.6	26	15	3298	7.59	3092	5	ND	4	65	38	32	2	16	.41	.108	17	5	.17	162	.01	8	.91	.02	.10	3	330
CL11W 1+25N	6	88	3743	2561	36.4	28	16	3465	7.73	3163	5	ND	4	60	44	35	2	15	.42	.098	17	5	.18	177	.01	2	.78	.02	.08	3	280
CL11W 1+00N	6	54	2674	1722	15.4	17	12	3391	7.13	1997	5	ND	4	50	28	23	2	17	.37	.099	16	9	.14	128	.01	3	.85	.02	.07	4	280
CL11W 0+75N	6	72	3683	1689	22.7	20	16	4560	7.31	2584	5	ND	3	49	32	29	2	16	.37	.122	14	7	.14	153	.01	2	.86	.02	.07	2	194
CL11W 0+50N	5	70	2694	1841	29.3	19	11	3300	6.79	2263	5	ND	4	58	29	24	2	15	.46	.094	17	6	.15	130	.01	6	.80	.02	.10	2	220
CL11W 0+00N	4	42	369	405	1.6	44	19	2468	4.93	301	5	ND	3	43	4	2	2	19	.40	.090	13	16	.24	84	.01	2	.84	.02	.05	2	19
CL10W 13+00N	1	29	39	118	.4	20	10	834	4.70	26	5	ND	1	11	1	2	2	52	.08	.119	9	24	.41	115	.01	3	2.81	.02	.06	1	2
CL10W 12+75N	1	28	34	118	.5	20	9	800	4.79	24	5	ND	2	19	1	2	2	56	.14	.118	9	25	.43	120	.01	7	2.72	.02	.06	3	1
CL10W 12+50N	1	14	23	52	.2	11	4	169	2.16	13	5	ND	1	11	1	2	2	37	.05	.057	8	12	.20	67	.01	5	1.37	.02	.05	1	2
CL10W 12+25N	1	20	27	61	.6	8	3	356	2.26	18	5	ND	1	10	1	2	2	35	.03	.077	10	14	.07	68	.01	6	1.36	.01	.05	1	4
CL10W 12+00N	1	11	25	44	2.1	7	2	91	1.13	8	5	ND	1	10	1	2	2	26	.03	.094	7	17	.12	71	.01	2	1.75	.01	.04	2	1
CL10W 11+75N	1	20	27	91	1.1	11	4	325	3.45	21	5	ND	1	11	1	2	2	46	.05	.105	6	21	.25	83	.01	6	2.39	.02	.04	1	3
CL10W 11+50N	1	14	29	87	.4	12	4	263	2.45	19	5	ND	1	15	1	2	2	40	.09	.088	8	16	.20	144	.01	2	1.92	.02	.08	1	1
CL10W 11+25N	1	10	29	72	1.2	9	6	502	1.99	10	5	ND	1	21	1	2	2	36	.14	.088	8	14	.17	171	.01	2	1.94	.02	.08	1	54
CL10W 11+00N	1	22	31	101	1.0	15	6	436	3.17	21	5	ND	1	17	1	2	2	41	.12	.119	9	17	.27	124	.01	6	2.16	.02	.05	1	1
CL10W 10+75N	1	20	50	103	1.1	15	6	692	2.95	38	5	ND	1	21	1	2	2	38	.14	.108	9	14	.23	103	.01	2	1.81	.02	.05	1	1
CL10W 10+50N	1	13	24	55	.6	11	3	204	1.93	14	5	ND	1	10	1	3	2	36	.04	.074	7	17	.21	93	.01	2	2.06	.01	.06	1	1
CL10W 10+25N	1	33	64	142	1.3	24	10	622	4.64	49	5	ND	1	9	1	3	2	50	.07	.119	7	29	.45	81	.01	5	2.69	.02	.07	1	1
CL10W 10+00N	2	41	114	147	1.7	34	24	1578	4.04	73	5	ND	3	7	1	3	2	30	.03	.098	12	20	.28	74	.01	2	1.86	.01	.07	1	3
CL10W 9+75N	1	11	62	70	.7	8	4	340	2.08	44	5	ND	1	12	1	3	2	21	.03	.097	13	5	.06	65	.01	2	1.15	.01	.05	1	8
CL10W 9+50N	1	26	165	132	1.1	16	6	723	5.74	198	5	ND	1	10	1	4	2	50	.03	.112	7	19	.12	72	.01	2	1.63	.01	.06	1	4
CL10W 9+25N	1	19	218	197	1.4	14	5	467	3.59	85	5	ND	1	20	1	4	2	43	.14	.110	7	19	.28	147	.01	2	2.34	.02	.08	1	6
CL10W 9+00N	1	18	65	109	.7	12	4	224	3.11	48	5	ND	1	30	1	3	2	49	.26	.060	7	16	.24	149	.01	5	1.59	.02	.05	1	1
CL10W 8+75N	1	8	105	75	2.8	5	2	172	1.31	65	5	ND	1	36	1	2	2	29	.44	.036	10	9	.15	151	.01	2	1.26	.02	.05	1	14
CL10W 8+50N	1	19	141	167	1.0	8	3	681	1.99	75	5	ND	1	46	2	2	2	33	.53	.076	10	14	.21	160	.01	6	1.28	.03	.08	1	2
CL10W 8+25N	1	30	470	270	3.1	16	6	559	6.56	896	5	ND	2	10	2	7	2	47	.10	.096	8	18	.26	50	.01	7	2.28	.02	.03	1	41
CL10W 8+00N	2	40	101	1464	2.2	46	12	861	3.66	289	7	ND	2	76	19	3	2	20	.64	.089	10	17	.26	153	.01	2	1.09	.03	.08	4	4
CL10W 7+75N	1	36	424	336	6.5	32	13	878	5.49	173	5	ND	3	11	1	4	2	43	.12	.088	8	27	.43	61	.01	2	3.40	.02	.05	1	24
STD C/AU-S	18	59	42	132	7.4	68	27	1044	4.05	43	19	7	37	49	18	17	22	57	.49	.089	37	61	.89	178	.08	33	1.86	.08	.14	14	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL10W 7+50N	1	33	475	257	2.6	22	8	945	5.62	393	5	ND	2	8	1	11	2	31	.06	.168	10	15	.15	42	.01	2	1.26	.01	.05	1	32
CL10W 7+25N	1	13	156	91	1.6	4	2	264	1.16	100	5	ND	1	5	1	2	2	14	.02	.056	8	6	.07	37	.01	6	1.06	.01	.04	1	13
CL10W 7+00N	1	17	95	89	1.0	10	4	303	3.86	72	5	ND	1	8	1	2	2	51	.04	.088	8	15	.16	50	.01	2	1.81	.01	.05	1	7
CL10W 6+75N	2	25	784	228	10.8	11	3	266	3.97	661	5	ND	1	7	1	38	2	43	.05	.117	12	12	.13	39	.01	2	1.46	.01	.05	1	117
CL10W 6+25N	1	22	197	259	4.1	10	5	316	6.08	211	5	ND	1	8	1	2	2	68	.05	.112	6	16	.29	56	.02	2	2.74	.01	.04	1	5
CL10W 6+00N	3	62	1672	889	11.1	11	5	606	7.22	1496	5	ND	3	9	5	13	2	40	.09	.160	10	18	.24	63	.01	4	3.38	.02	.04	2	75
CL10W 5+75N	2	20	283	406	3.0	4	2	738	3.37	639	5	ND	1	8	2	9	2	31	.04	.102	15	5	.07	57	.01	4	1.53	.02	.07	1	23
CL10W 5+50N	5	51	2332	711	24.0	4	2	205	3.86	1040	5	ND	3	14	2	10	2	19	.03	.122	20	5	.09	49	.01	4	1.54	.02	.06	1	350
CL10W 5+25N	6	49	2637	1885	12.9	7	7	8053	5.07	736	5	ND	4	27	30	11	2	19	.20	.124	24	9	.11	140	.01	2	1.41	.02	.09	4	380
CL10W 5+00N	9	43	3475	1333	33.8	8	8	3025	5.33	646	5	ND	5	12	8	8	2	14	.09	.121	19	4	.12	111	.01	2	1.66	.02	.09	3	800
CL10W 4+75N	7	73	2537	3688	30.9	9	9	4597	6.70	1203	5	10	5	32	41	7	3	18	.25	.130	24	7	.15	221	.01	2	2.26	.02	.10	2	400
CL10W 4+50N	6	48	1638	2249	13.4	10	6	2839	6.30	882	5	ND	5	24	15	4	2	23	.18	.102	20	9	.20	198	.01	2	2.07	.02	.09	4	270
CL10W 4+25N	4	32	1065	1229	4.7	9	7	3688	5.02	441	5	ND	4	20	9	4	2	23	.15	.086	19	10	.17	211	.01	3	1.70	.02	.09	4	102
CL10W 4+00N	8	21	273	791	4.8	11	6	16304	31.20	253	21	ND	6	31	5	2	2	17	.14	.110	13	3	.36	137	.01	2	1.30	.01	.08	2	52
CL10W 3+75N	5	33	1293	718	10.8	8	6	2986	4.91	805	5	ND	3	10	4	7	2	24	.03	.084	17	12	.10	101	.01	2	1.48	.01	.07	1	104
CL10W 3+25N	19	80	1814	1641	12.7	15	14	5955	6.63	1211	5	ND	4	35	21	15	2	19	.28	.093	26	9	.28	318	.01	5	1.84	.02	.11	3	270
CL10W 3+00N	11	66	1628	1369	12.6	45	21	5744	6.08	1012	5	ND	4	64	20	10	2	18	.46	.096	26	10	.36	382	.01	2	1.46	.02	.14	2	82
CL10W 2+75N	7	58	2090	1113	31.5	28	15	4627	5.27	1066	5	ND	3	57	13	22	2	17	.40	.128	17	11	.23	193	.01	2	1.34	.02	.10	3	125
CL10W 2+25N	2	42	115	435	2.8	47	12	578	5.29	201	5	ND	3	11	1	2	2	31	.06	.079	14	20	.28	127	.01	7	1.90	.02	.07	1	18
CL10W 2+00N	2	25	199	220	.9	20	7	1094	3.11	216	5	ND	2	14	1	3	2	21	.12	.066	13	9	.10	85	.01	2	.76	.01	.08	1	22
CL10W 1+75N	2	26	127	182	.6	20	7	537	3.63	141	5	ND	3	11	1	3	2	29	.05	.075	14	9	.08	93	.01	2	.95	.01	.10	1	10
CL10W 1+50N	3	29	412	301	2.0	24	9	739	3.56	500	5	ND	2	14	2	5	2	22	.10	.079	13	8	.10	59	.01	2	.76	.01	.06	1	50
CL10W 1+25N	4	52	870	713	10.5	46	19	1733	5.42	1049	5	ND	3	16	4	14	2	20	.13	.072	14	13	.10	92	.01	2	.76	.01	.08	1	57
CL10W 1+00N	2	43	239	498	2.3	71	16	1009	4.67	240	5	ND	4	29	3	5	2	22	.19	.066	16	19	.30	170	.01	2	1.88	.02	.10	1	10
CL10W 0+75N	4	37	112	294	1.4	40	9	357	3.94	272	5	ND	3	42	2	5	3	20	.24	.041	14	8	.10	65	.01	6	.65	.02	.08	1	10
CL10W 0+50N	2	45	325	384	3.0	40	13	1419	4.42	229	5	ND	2	26	4	9	2	31	.24	.088	13	22	.39	133	.01	8	1.62	.03	.09	1	17
CL10W 0+25N	1	25	74	204	1.2	24	6	290	5.36	104	5	ND	3	14	1	6	2	36	.08	.078	11	15	.23	76	.01	2	1.38	.02	.04	1	1
CL10W 0+00N	1	28	49	190	.6	26	7	379	4.37	62	5	ND	3	11	1	3	2	30	.07	.049	12	17	.24	61	.01	2	1.35	.02	.05	1	1
CL9W 13+00N	1	33	26	122	.4	20	9	711	5.27	19	5	ND	1	9	1	2	2	55	.08	.097	9	28	.48	93	.01	7	3.24	.02	.07	1	1
CL9W 12+75N	1	16	24	61	1.0	12	4	144	1.92	14	5	ND	1	11	1	2	2	33	.05	.091	7	19	.26	83	.01	3	2.13	.02	.06	1	1
CL9W 12+50N	1	25	38	88	.4	15	7	443	4.76	26	5	ND	1	12	1	2	2	56	.07	.105	7	20	.32	88	.01	2	2.60	.02	.06	1	1
CL9W 12+25N	1	25	44	80	.6	12	4	188	3.89	30	5	ND	1	9	1	2	2	46	.05	.085	8	21	.23	64	.01	3	2.50	.02	.04	1	1
CL9W 12+00N	1	28	32	141	2.3	17	8	1030	4.49	20	5	ND	1	9	1	2	2	53	.04	.130	6	22	.33	93	.01	4	2.39	.02	.06	1	1
CL9W 11+75N	1	26	35	126	1.2	18	7	567	3.80	22	5	ND	1	9	1	2	2	42	.06	.119	7	22	.39	86	.01	3	2.49	.02	.06	1	1
CL9W 11+50N	1	20	33	94	1.3	15	7	516	3.44	25	5	ND	1	9	1	2	2	50	.04	.117	7	22	.36	109	.01	2	2.67	.02	.09	2	1
CL9W 11+25N	1	32	108	196	1.9	22	10	933	4.60	88	5	ND	2	13	1	2	2	48	.09	.158	11	28	.44	151	.01	6	3.37	.03	.09	1	1
STD C/AU-S	18	59	43	132	7.3	68	27	1039	4.07	44	23	8	36	49	18	16	19	56	.49	.090	36	63	.90	175	.08	33	1.86	.08	.13	13	48

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL9W 11+00N	1	37	253	274	5.5	30	13	881	4.23	94	5	ND	2	15	1	8	2	34	.13	.113	10	19	.26	106	.01	2	1.76	.02	.07	1	3
CL9W 10+75N	2	30	244	153	1.7	17	8	1299	5.53	178	5	ND	2	7	1	2	2	44	.04	.136	7	25	.22	44	.01	2	2.04	.02	.04	1	61
CL9W 10+50N	2	24	106	143	5.7	12	6	680	3.67	59	5	ND	1	8	1	2	2	43	.03	.098	8	20	.24	61	.01	4	1.97	.02	.06	1	7
CL9W 10+25N	2	32	199	201	5.7	26	9	1104	4.46	106	5	ND	1	20	1	2	2	37	.16	.139	10	22	.25	94	.01	4	2.05	.02	.06	1	2
CL9W 10+00N	1	17	146	267	.6	17	6	394	3.74	134	5	ND	1	36	1	2	2	50	.36	.075	7	19	.49	228	.01	2	2.07	.03	.06	1	16
CL9W 9+75N	1	20	198	176	.9	10	5	1488	2.54	86	5	ND	1	80	4	2	2	37	.92	.116	8	12	.23	330	.01	6	1.06	.03	.09	1	1
CL9W 9+50N	3	32	309	452	4.5	58	16	5538	5.46	2568	5	ND	3	50	8	2	2	37	.44	.207	15	22	.35	460	.01	2	2.86	.03	.13	1	43
CL9W 9+25N	2	19	102	175	1.0	17	5	771	3.03	118	5	ND	2	31	2	2	2	36	.29	.086	9	13	.19	284	.01	2	1.67	.02	.07	1	1
CL9W 9+00N	1	15	130	173	1.1	10	3	242	2.01	117	5	ND	1	16	1	2	2	31	.12	.101	8	11	.14	144	.01	2	1.53	.02	.08	1	5
CL9W 8+75N	1	7	122	74	.7	5	1	118	.86	71	5	ND	2	8	1	2	2	16	.05	.041	16	7	.04	61	.01	4	.80	.01	.06	1	8
CL9W 8+50N	2	27	974	275	6.8	11	4	259	5.59	1143	8	ND	2	8	1	8	2	46	.04	.106	11	11	.15	66	.01	2	2.07	.01	.06	1	101
CL9W 8+25N	2	37	1673	329	13.9	12	5	449	4.16	1150	5	ND	3	9	2	13	2	27	.07	.134	12	14	.12	50	.01	2	1.73	.01	.05	1	144
CL9W 8+00N	2	25	186	126	4.2	20	7	583	4.21	168	5	ND	3	11	1	2	2	33	.05	.054	10	14	.09	75	.01	2	1.28	.02	.07	1	5
CL9W 7+75N	4	43	4154	797	48.9	11	4	529	4.07	1095	11	ND	2	24	5	63	2	35	.20	.169	12	13	.22	98	.01	2	1.72	.02	.07	1	118
CL9W 7+25N	32	371	14842	1813	132.8	8	3	548	8.78	2546	5	ND	2	14	9	104	2	12	.06	.146	15	4	.05	49	.01	2	.65	.02	.08	4	1050
CL9W 7+00N	47	479	20693	2739	220.8	11	4	1066	10.90	3775	5	ND	2	16	11	136	2	12	.11	.190	13	4	.09	47	.01	2	.84	.02	.10	4	1630
CL9W 6+25N	4	47	1434	585	12.5	6	3	280	3.63	440	5	ND	3	7	5	25	2	42	.03	.064	16	7	.10	50	.01	3	1.49	.01	.04	1	157
CL9W 6+00N	17	33	1352	1070	6.9	6	2	344	3.66	1180	5	ND	2	7	7	9	2	32	.03	.063	17	5	.04	59	.01	2	.89	.01	.05	1	280
CL9W 5+75N	1	8	216	156	1.3	3	1	175	1.52	138	5	ND	1	7	1	2	2	25	.02	.041	15	7	.08	58	.01	2	1.30	.01	.03	1	38
CL9W 5+50N	3	29	1424	656	10.5	8	4	1555	3.89	509	5	ND	3	14	3	7	2	32	.08	.087	18	10	.09	98	.01	3	1.53	.02	.05	2	89
CL9W 3+50N	8	111	4615	2754	34.7	24	16	6171	9.13	3930	5	ND	5	71	49	15	2	15	.42	.112	18	6	.21	302	.01	9	.97	.03	.11	2	470
CL9W 3+25N	9	150	4895	3411	37.8	34	21	8399	11.07	6311	5	ND	5	105	60	22	2	15	.57	.108	21	6	.37	405	.01	10	1.18	.03	.11	1	670
CL9W 3+00N	7	63	1932	1758	13.7	16	10	4020	5.55	934	5	ND	4	52	26	6	3	18	.51	.144	17	9	.21	234	.01	7	1.32	.03	.09	1	117
CL9W 2+75N	6	46	1236	1216	9.0	14	8	2626	4.99	630	5	ND	4	36	11	5	2	20	.38	.124	17	11	.19	202	.01	3	1.41	.02	.09	1	111
CL9W 2+50N	8	140	5160	2124	35.3	22	16	7548	8.18	1713	5	ND	5	31	43	9	2	20	.20	.176	24	6	.22	323	.01	2	1.41	.02	.09	3	230
CL9W 1+25N	2	13	108	78	.8	6	2	195	1.47	49	5	ND	1	18	1	2	2	27	.12	.023	11	8	.04	86	.01	3	.58	.01	.05	1	5
CL9W 1+00N	2	28	62	161	.5	28	8	433	4.41	65	5	ND	3	14	1	2	2	36	.11	.098	12	22	.34	82	.01	6	1.47	.02	.05	1	1
CL9W 0+75N	2	25	77	165	.6	20	7	674	5.01	96	5	ND	2	12	1	2	2	45	.06	.076	11	13	.18	104	.01	6	1.38	.02	.06	1	1
CL9W 0+50N	2	21	41	107	.5	13	4	231	2.93	59	5	ND	3	19	1	2	2	36	.11	.036	13	8	.07	103	.01	3	.79	.01	.07	1	2
CL9W 0+25N	2	28	83	202	.9	23	10	983	4.05	69	5	ND	3	42	1	2	2	37	.24	.061	12	16	.23	201	.01	2	1.51	.02	.09	1	1
CL9W 0+00N	2	29	86	256	.4	19	7	1954	4.12	76	5	ND	2	32	1	6	2	43	.19	.085	11	15	.15	241	.01	2	1.51	.02	.07	1	6
CL8W 13+00N	2	36	38	129	.3	23	9	750	6.21	33	5	ND	2	9	1	2	2	60	.05	.120	6	29	.46	93	.01	3	2.67	.02	.07	1	1
CL8W 12+75N	1	21	34	82	1.1	14	4	251	2.70	25	5	ND	1	10	1	2	2	42	.05	.088	7	18	.29	89	.01	2	2.10	.02	.05	1	1
CL8W 12+50N	1	9	20	29	.2	4	2	457	1.39	12	5	ND	1	9	1	2	2	34	.03	.058	9	12	.08	68	.01	2	1.28	.01	.06	1	5
CL8W 12+25N	1	26	88	116	1.2	18	6	400	4.40	82	5	ND	2	8	1	2	2	49	.05	.109	7	21	.31	66	.01	2	2.53	.02	.05	1	1
CL8W 12+00N	2	24	39	90	.7	13	6	490	5.69	28	5	ND	1	9	1	2	2	50	.04	.123	7	19	.25	77	.01	2	2.80	.02	.04	1	1
STD C/AU-S	18	59	43	132	7.3	67	26	1029	3.98	43	23	7	37	49	18	15	22	56	.48	.088	36	56	.87	178	.08	32	1.82	.09	.14	13	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL8W 11+75N	2	21	35	99	1.1	17	6	347	3.76	15	5	ND	1	11	1	4	2	44	.07	.109	7	23	.39	102	.01	2	2.38	.03	.09	1	1
CL8W 11+50N	2	26	47	119	2.2	23	7	333	4.41	23	5	ND	1	10	1	2	2	51	.07	.083	7	28	.54	124	.01	3	2.97	.03	.11	1	1
CL8W 11+25N	1	8	30	54	.7	7	2	127	1.60	17	5	ND	1	22	1	2	2	29	.17	.056	9	13	.12	134	.01	2	1.15	.02	.09	1	1
CL8W 11+00N	1	17	34	129	.5	15	5	604	3.42	25	5	ND	1	33	1	2	2	46	.32	.101	8	21	.35	214	.01	2	1.84	.02	.08	1	1
CL8W 10+75N	2	16	156	196	.6	12	6	1603	3.09	123	5	ND	1	28	1	2	2	35	.30	.117	9	15	.20	187	.01	5	1.67	.02	.11	1	18
CL8W 10+50N	1	10	174	127	.8	8	3	322	2.04	188	5	ND	1	27	1	5	2	26	.33	.079	10	13	.17	130	.01	2	1.09	.02	.10	1	27
CL8W 10+25N	3	26	257	281	3.5	20	7	635	3.58	110	5	ND	1	18	1	5	2	45	.13	.164	8	22	.40	198	.01	3	3.39	.03	.13	1	2
CL8W 10+00N	2	29	243	337	1.3	25	10	1316	3.63	139	5	ND	1	15	6	5	2	40	.07	.121	10	20	.29	131	.01	2	2.31	.02	.08	1	11
CL8W 9+50N	1	12	249	167	.9	11	4	295	3.26	199	5	ND	1	15	1	4	2	42	.10	.075	9	16	.23	114	.01	3	1.83	.02	.08	1	40
CL8W 9+25N	3	24	310	308	3.1	42	13	2040	4.43	131	5	ND	1	61	7	2	2	39	.62	.183	15	36	.58	315	.01	2	2.16	.04	.12	1	3
CL8W 9+00N	2	29	342	270	2.3	25	8	712	5.57	357	5	ND	2	14	1	6	2	47	.07	.102	9	19	.19	129	.01	2	2.14	.02	.06	1	49
CL8W 8+75N	2	37	197	178	1.5	26	10	1231	7.18	150	5	ND	2	12	1	3	2	61	.05	.106	8	27	.41	109	.01	3	2.92	.02	.07	1	1
CL8W 8+50N	3	36	1743	417	11.7	14	5	422	6.04	1391	5	ND	2	11	2	19	2	40	.12	.136	11	15	.21	60	.01	10	2.72	.02	.05	1	169
CL8W 8+25N	2	23	158	148	2.4	15	6	589	5.16	126	5	ND	1	10	1	5	2	59	.06	.113	8	21	.28	93	.02	3	2.04	.02	.10	1	4
CL8W 8+00N	2	32	933	798	4.6	15	7	1704	3.81	221	5	ND	1	21	8	35	2	43	.20	.127	9	19	.21	114	.01	2	1.64	.02	.10	3	31
CL8W 7+50N	3	99	3263	842	18.6	25	9	902	4.78	290	5	ND	2	9	17	519	2	44	.08	.097	10	18	.30	42	.01	2	2.13	.02	.06	1	106
CL8W 7+25N	2	33	1196	325	16.5	12	5	3126	2.61	296	5	ND	1	17	4	65	5	22	.12	.093	8	6	.09	117	.01	2	1.13	.02	.09	1	95
CL8W 7+00N	12	498	20934	7578	336.6	12	10	6610	16.27	20961	14	3	2	73	242	325	2	10	.30	.151	14	1	.11	226	.01	2	.74	.02	.08	1	2920
CL8W 4+25N	8	50	2140	1317	11.2	18	10	6136	5.79	1555	5	ND	4	100	15	23	2	20	.47	.095	20	11	.23	367	.01	4	1.41	.03	.15	2	280
CL8W 4+00N	9	64	3664	1728	21.8	10	9	6901	5.81	2069	5	ND	4	83	29	62	2	16	.46	.144	18	10	.19	462	.01	2	1.37	.02	.15	2	690
CL8W 1+75N	4	68	1519	1288	15.5	50	20	2399	4.92	885	5	ND	4	24	22	26	2	11	.28	.144	14	5	.13	139	.01	2	.58	.03	.08	2	155
CL8W 1+00N	6	65	2485	1634	32.1	15	6	1835	6.68	2269	5	ND	5	19	10	25	2	17	.15	.193	18	8	.17	133	.01	2	1.77	.02	.10	2	240
CL8W 0+75N	2	7	211	126	2.0	3	1	135	1.00	144	5	ND	5	7	1	5	2	12	.04	.022	23	2	.04	77	.01	2	1.42	.01	.04	1	58
CL8W 0+50N	2	10	324	181	2.4	3	1	143	1.50	262	7	ND	5	6	1	7	3	13	.05	.024	21	4	.07	78	.01	2	1.22	.01	.06	1	57
CL8W 0+25N	3	25	767	624	14.7	7	3	415	3.39	697	5	ND	4	12	2	13	2	19	.10	.059	19	5	.10	105	.01	2	1.12	.01	.08	1	137
CL8W 0+00N	3	21	555	588	3.8	8	3	486	3.02	725	7	ND	4	252	4	4	2	22	.69	.032	16	6	.23	211	.01	3	1.26	.03	.05	1	59
CL7W 13+00N	2	18	70	122	2.5	20	10	998	3.27	37	5	ND	1	14	1	5	2	47	.09	.136	9	32	.48	138	.01	5	2.81	.03	.11	1	2
CL7W 12+75N	1	17	52	110	.9	19	6	228	3.09	28	5	ND	1	11	1	3	2	44	.07	.064	7	21	.46	116	.01	2	2.36	.02	.07	1	1
CL7W 12+50N	1	8	25	33	.6	4	2	98	1.08	6	5	ND	1	11	1	2	2	30	.05	.043	8	16	.17	72	.01	2	1.73	.02	.05	1	2
CL7W 12+25N	1	22	87	112	.5	17	5	350	3.55	84	5	ND	1	10	1	3	2	49	.05	.101	7	20	.35	98	.01	2	2.35	.02	.09	1	1
CL7W 12+00N	1	23	45	110	.7	17	6	329	3.98	28	5	ND	1	9	1	4	2	50	.05	.085	6	23	.41	98	.01	2	2.96	.02	.09	1	1
CL7W 11+75N	1	9	93	38	.9	5	1	77	1.16	53	5	ND	1	9	1	2	2	28	.04	.040	9	11	.10	74	.01	2	1.52	.02	.05	1	4
CL7W 11+50N	1	30	42	124	.6	19	9	905	4.96	32	5	ND	2	11	1	3	2	54	.06	.127	6	28	.38	99	.01	2	2.42	.02	.09	1	2
CL7W 11+25N	2	22	113	171	1.3	12	7	778	3.01	71	5	ND	2	11	1	2	2	43	.06	.114	10	20	.26	119	.01	3	2.08	.03	.08	3	1
CL7W 11+00N	1	26	94	212	.9	22	7	604	4.38	85	5	ND	2	23	1	3	2	50	.21	.112	10	25	.48	227	.01	2	2.74	.03	.09	1	1
CL7W 10+75N	1	25	130	216	1.0	21	7	414	4.57	137	5	ND	1	28	1	4	2	52	.29	.113	8	23	.45	232	.01	5	2.53	.03	.10	1	1
STD C/AU-S	19	59	43	132	7.3	68	27	1039	4.08	44	20	8	37	49	18	15	22	56	.49	.091	37	59	.90	176	.08	33	1.85	.08	.15	12	51

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL7W 10+50N	1	22	397	211	2.2	12	5	642	3.90	400	5	ND	1	13	1	2	4	45	.08	.107	7	16	.19	124	.01	2	1.74	.02	.09	1	44
CL7W 10+25N	1	19	510	202	5.3	9	4	421	3.04	359	5	ND	1	11	1	3	2	47	.06	.101	10	14	.17	99	.01	2	1.89	.02	.07	1	73
CL7W 10+00N	2	22	324	172	3.1	11	4	179	3.24	214	5	ND	1	12	1	2	2	45	.10	.105	7	16	.28	114	.01	2	2.36	.02	.07	1	24
CL7W 9+75N	1	23	284	191	1.3	14	5	240	4.04	229	5	ND	1	10	1	2	2	46	.09	.118	6	20	.34	99	.01	2	2.36	.02	.07	1	18
CL7W 9+50N	1	27	233	254	1.1	15	7	501	4.74	275	5	ND	1	12	1	4	2	58	.08	.093	7	23	.33	117	.01	4	2.12	.02	.08	2	16
CL7W 9+25N	1	12	155	135	.8	8	4	162	3.87	194	5	ND	1	9	1	2	2	54	.05	.062	9	14	.22	70	.03	2	1.63	.02	.06	1	13
CL7W 8+75N	1	28	308	401	1.7	26	8	692	4.54	189	5	ND	2	32	1	3	2	40	.39	.130	8	24	.46	145	.01	3	2.12	.03	.09	1	4
CL7W 8+50N	1	12	72	175	.1	8	5	408	3.23	71	5	ND	1	30	1	2	2	48	.30	.092	8	13	.19	149	.01	2	1.41	.02	.10	1	27
CL7W 8+25N	2	16	65	134	.5	11	5	266	4.24	62	5	ND	1	16	1	2	2	57	.09	.087	8	19	.19	122	.02	2	1.75	.02	.07	1	4
CL7W 8+00N	2	25	203	400	1.4	20	10	2026	3.15	50	5	ND	1	44	7	4	2	31	.51	.111	9	16	.24	293	.01	3	1.76	.03	.11	1	2
CL7W 7+75N	1	14	92	67	2.1	5	3	300	2.27	52	5	ND	1	8	1	2	2	33	.02	.070	9	11	.09	57	.01	2	1.31	.01	.04	1	15
CL7W 7+50N	2	13	155	107	.9	7	3	534	2.58	128	5	ND	1	7	1	2	2	32	.03	.081	11	11	.10	51	.01	2	1.12	.01	.04	1	112
CL7W 7+25N	2	22	239	288	.9	20	6	291	5.27	280	5	ND	3	9	1	2	2	36	.07	.089	10	17	.26	62	.01	2	2.55	.02	.05	1	7
CL7W 7+00N	1	13	157	180	1.1	7	3	137	3.03	220	5	ND	3	8	1	2	2	39	.03	.050	13	12	.10	42	.01	2	1.30	.01	.05	1	20
CL7W 6+75N	1	30	234	346	.8	44	14	535	4.73	198	5	ND	4	8	1	3	2	35	.07	.066	9	20	.31	68	.01	2	1.91	.02	.06	1	43
CL7W 6+50N	2	30	129	197	.9	30	11	498	4.73	86	5	ND	3	10	1	5	2	35	.07	.110	6	14	.22	66	.01	3	1.44	.02	.05	1	6
CL7W 6+25N	2	53	198	293	1.2	46	15	706	5.04	105	5	ND	3	6	1	4	2	25	.05	.084	10	14	.22	56	.01	2	1.10	.02	.05	1	3
CL7W 6+00N	2	38	691	648	7.3	22	10	668	5.55	223	5	ND	2	13	4	19	2	54	.12	.117	12	26	.24	165	.01	2	1.92	.02	.06	1	15
CL7W 5+25N	10	88	7307	1814	52.9	8	7	3573	7.17	2914	5	ND	5	30	14	35	4	18	.12	.144	16	5	.13	163	.01	2	1.43	.03	.09	4	540
CL7W 4+50N	9	64	4409	1119	32.0	14	8	3867	6.45	1911	5	ND	6	20	6	17	5	19	.08	.176	19	9	.18	114	.01	8	1.79	.02	.09	1	290
CL7W 3+50N	2	15	198	146	1.9	11	6	1034	4.39	113	5	ND	1	11	1	2	2	54	.06	.106	8	18	.23	98	.02	9	1.76	.03	.05	1	46
CL7W 3+25N	1	21	105	194	.9	19	7	400	5.60	88	5	ND	3	13	1	2	2	47	.08	.166	9	19	.29	98	.01	2	1.99	.02	.06	1	4
CL7W 3+00N	2	26	88	160	.8	26	8	532	3.96	68	5	ND	4	8	1	2	2	32	.04	.064	14	16	.20	101	.01	2	1.43	.02	.06	1	3
CL7W 2+75N	1	15	58	142	1.6	14	5	340	3.65	58	5	ND	3	12	1	2	2	37	.06	.095	13	15	.15	88	.01	6	1.38	.02	.06	1	9
CL7W 2+50N	2	34	242	477	2.9	40	11	664	4.51	175	5	ND	4	17	3	5	2	25	.14	.089	15	21	.32	115	.01	2	2.37	.02	.06	1	23
CL7W 2+25N	2	29	341	347	1.9	29	7	193	2.88	411	5	ND	4	8	1	5	2	13	.04	.049	16	4	.04	36	.01	2	.76	.01	.04	1	43
CL7W 2+00N	2	31	108	252	2.4	46	10	342	4.04	146	5	ND	3	12	1	7	2	17	.11	.055	14	6	.05	96	.01	3	.74	.02	.07	1	6
CL7W 1+75N	2	39	105	298	.4	62	13	340	4.41	202	5	ND	3	9	1	11	2	17	.05	.052	15	5	.05	34	.01	2	.64	.01	.05	1	12
CL7W 1+50N	5	61	1275	1071	7.6	28	10	2289	5.51	1195	5	ND	5	31	8	49	5	17	.19	.082	20	7	.10	139	.01	2	.88	.02	.09	1	99
CL7W 0+75N	2	21	382	258	2.1	9	4	1100	3.26	298	5	ND	2	11	1	2	2	38	.08	.075	13	10	.10	90	.01	3	.95	.02	.06	1	48
CL7W 0+50N	1	18	76	121	.9	10	4	498	3.26	73	5	ND	1	10	1	2	2	49	.07	.084	10	11	.12	61	.01	4	1.07	.01	.05	1	9
CL7W 0+25N	1	22	83	123	3.2	19	5	320	4.96	68	5	ND	2	17	1	2	2	36	.07	.105	10	18	.16	60	.01	5	1.28	.02	.05	1	1
CL7W 0+00N	7	81	1059	4542	11.9	24	10	7625	3.96	1163	17	ND	3	460	80	5	2	27	1.27	.123	11	18	.34	479	.01	2	1.81	.03	.07	4	49
CL6W 13+00N	1	11	97	79	.4	9	3	228	2.60	79	5	ND	1	11	1	2	2	44	.04	.078	8	16	.20	76	.02	2	1.58	.02	.06	1	4
CL6W 12+75N	1	20	115	129	.8	17	7	567	3.63	100	5	ND	1	10	1	2	2	47	.05	.093	7	26	.39	108	.01	2	2.33	.02	.06	1	7
CL6W 12+50N	1	18	61	102	1.6	14	5	238	3.02	56	5	ND	1	11	1	2	2	48	.05	.082	7	22	.36	120	.01	6	2.58	.02	.08	1	1
STD C/AU-S	18	57	40	133	7.2	70	27	1040	4.00	40	18	8	36	48	18	15	22	58	.48	.090	38	61	.87	174	.08	36	1.82	.06	.14	13	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL6W 12+25N	1	20	88	107	.9	11	6	833	2.92	57	5	ND	1	15	1	2	3	46	.09	.125	8	19	.24	153	.01	2	1.84	.02	.09	2	3
CL6W 12+00N	1	18	65	95	2.1	11	6	496	2.90	52	5	ND	1	11	1	3	2	45	.05	.094	7	20	.25	93	.01	2	2.23	.02	.08	1	2
CL6W 11+75N	1	17	60	138	.5	15	6	814	3.26	51	5	ND	1	17	1	2	2	46	.11	.104	7	17	.35	160	.01	2	2.32	.02	.07	2	1
CL6W 11+50N	1	18	75	154	1.4	17	6	300	3.32	62	5	ND	1	14	1	2	2	45	.07	.105	6	23	.40	152	.01	2	2.56	.02	.09	2	8
CL6W 11+25N	2	30	146	489	4.4	23	7	687	4.02	129	5	ND	2	30	3	2	2	42	.25	.225	13	25	.43	284	.01	5	3.06	.03	.14	2	10
CL6W 11+00N	2	25	158	282	1.0	20	8	1018	4.35	155	5	ND	2	31	2	4	2	48	.27	.167	10	24	.38	292	.01	2	2.53	.03	.11	1	4
CL6W 10+75N	1	21	176	152	3.1	11	4	209	3.21	160	5	ND	1	13	1	2	2	45	.08	.103	8	16	.23	119	.01	4	2.28	.02	.08	1	7
CL6W 10+50N	1	20	130	235	2.7	20	6	359	3.84	139	5	ND	1	22	1	2	2	45	.21	.090	10	24	.47	178	.01	2	2.32	.02	.08	1	2
CL6W 10+25N	1	9	77	55	1.3	5	2	63	1.65	57	7	ND	1	9	1	2	2	25	.04	.047	11	11	.12	78	.01	2	1.79	.01	.04	1	1
CL6W 10+00N	1	19	102	203	.9	16	7	972	3.23	91	5	ND	1	17	1	3	2	39	.13	.102	8	19	.35	177	.01	6	1.99	.03	.09	3	7
CL6W 9+75N	1	8	47	59	.3	7	3	198	1.46	28	5	ND	1	16	1	2	2	30	.10	.049	10	13	.16	154	.01	2	1.41	.02	.04	1	6
CL6W 9+50N	1	15	31	89	.5	13	5	329	3.13	30	5	ND	1	9	1	2	2	52	.04	.072	7	20	.36	106	.01	2	2.13	.02	.05	1	1
CL6W 9+25N	1	19	33	80	.5	10	5	461	3.67	30	5	ND	1	8	1	2	2	53	.03	.083	7	17	.24	87	.01	2	2.04	.02	.06	1	8
CL6W 9+00N	1	16	43	87	1.4	9	4	596	3.62	39	5	ND	1	15	1	2	2	46	.13	.088	9	15	.26	227	.02	3	1.91	.02	.07	1	3
CL6W 8+75N	1	30	79	162	.6	26	12	578	4.77	58	5	ND	3	10	1	2	2	47	.08	.079	8	26	.44	114	.02	2	2.92	.02	.06	1	5
CL6W 8+50N	1	22	48	153	.5	15	7	275	5.65	49	5	ND	3	9	1	2	2	44	.06	.192	9	17	.21	70	.01	3	1.61	.02	.07	2	1
CL6W 8+25N	1	24	58	139	.3	20	8	593	3.86	42	5	ND	2	13	1	5	2	34	.11	.111	10	17	.18	116	.01	2	1.49	.01	.06	1	3
CL6W 8+00N	2	12	51	73	1.0	6	3	218	2.63	24	5	ND	1	11	1	2	2	46	.05	.066	9	14	.11	78	.01	2	1.39	.01	.05	1	3
CL6W 7+75N	1	24	59	114	.8	13	5	209	4.77	51	5	ND	2	10	1	2	2	50	.08	.078	7	14	.19	82	.01	6	1.59	.02	.04	1	1
CL6W 7+50N	2	39	38	135	.4	22	9	596	4.52	38	5	ND	4	7	1	4	2	35	.05	.168	18	16	.08	75	.01	3	.98	.02	.06	3	2
CL6W 7+25N	1	22	60	179	.8	16	8	465	4.80	56	6	ND	2	10	1	3	3	58	.06	.087	9	19	.30	94	.02	2	2.20	.02	.07	1	2
CL6W 7+00N	1	30	50	150	.8	23	11	864	4.94	43	5	ND	3	14	1	4	2	53	.14	.108	8	25	.42	106	.03	2	2.55	.02	.06	2	1
CL6W 6+75N	1	24	42	99	.7	13	6	757	4.34	32	5	ND	1	10	1	2	2	50	.06	.100	7	22	.24	87	.01	6	1.56	.02	.06	1	2
CL6W 6+50N	1	21	60	106	.6	12	5	444	5.52	46	5	ND	1	9	1	2	2	57	.06	.104	9	17	.22	76	.02	2	1.82	.02	.04	1	1
CL6W 6+25N	1	20	107	131	.6	10	5	534	3.99	122	5	ND	2	12	1	3	2	54	.06	.084	10	15	.13	81	.02	2	1.36	.01	.06	1	1
CL6W 6+00N	1	27	91	235	1.1	18	6	663	3.57	88	5	ND	2	195	2	2	2	40	.40	.072	16	18	.33	170	.01	2	1.94	.02	.07	3	4
CL6W 5+75N	2	25	508	378	1.6	16	8	734	5.69	320	5	ND	4	19	2	7	2	34	.14	.136	9	17	.24	91	.01	5	3.58	.02	.04	1	8
CL6W 5+50N	2	25	396	525	3.9	17	18	817	4.29	247	5	ND	3	239	3	5	2	30	.91	.127	8	17	.36	109	.02	3	4.22	.03	.03	1	34
CL6W 5+25N	1	24	129	326	1.0	28	11	617	4.76	112	5	ND	2	89	2	2	2	42	.35	.071	8	22	.43	136	.01	8	2.22	.03	.06	1	7
CL6W 5+00N	1	34	67	875	1.1	32	14	1448	5.28	200	5	ND	3	73	6	2	2	56	.56	.102	13	37	.84	195	.05	9	2.14	.04	.09	1	3
CL6W 4+75N	2	30	127	297	.5	25	9	693	4.39	122	5	ND	3	29	2	2	2	47	.31	.083	9	32	.63	107	.04	3	1.86	.03	.07	2	1
CL6W 4+50N	1	30	26	151	.7	27	11	810	4.27	26	5	ND	3	30	1	2	2	47	.39	.092	9	36	.60	137	.04	2	1.50	.03	.09	2	1
CL6W 4+25N	1	30	35	141	.3	27	13	1158	4.29	31	5	ND	3	27	1	4	2	44	.40	.102	11	27	.54	118	.05	3	1.24	.04	.07	1	1
CL6W 4+00N	1	20	42	98	.7	14	6	242	5.45	42	5	ND	2	10	1	2	2	60	.07	.159	6	22	.27	79	.01	3	1.80	.02	.06	1	1
CL6W 3+75N	2	25	42	138	.6	22	8	424	5.37	41	5	ND	3	11	1	4	2	56	.10	.104	7	34	.43	93	.02	3	2.06	.02	.06	3	2
CL6W 3+50N	1	20	43	104	.4	14	6	301	4.41	35	5	ND	3	9	1	6	2	57	.06	.084	9	20	.26	69	.02	2	1.55	.02	.04	1	1
STD C/AU-S	18	60	44	132	7.6	69	27	1046	4.08	38	18	8	39	51	18	15	22	57	.49	.091	37	60	.90	182	.08	33	1.87	.09	.14	14	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL6W 3+25N	2	39	41	182	.6	42	10	484	4.15	48	5	ND	4	11	1	2	2	24	.10	.098	14	18	.37	93	.01	2	1.63	.02	.06	1	4
CL6W 3+00N	1	29	47	170	.9	26	10	749	4.34	34	5	ND	2	16	1	2	2	44	.16	.077	10	23	.46	145	.02	3	1.96	.02	.07	1	1
CL6W 2+75N	3	72	379	1326	6.4	48	10	2561	3.77	84	9	ND	3	124	26	19	2	29	1.15	.103	24	27	.42	453	.01	2	2.60	.03	.13	4	3
CL6W 2+50N	2	27	52	486	.9	21	6	371	4.57	53	5	ND	2	20	7	6	2	42	.12	.088	10	16	.26	143	.01	5	1.80	.02	.06	1	2
CL6W 2+25N	1	23	58	164	.9	17	5	204	5.30	65	5	ND	3	7	1	3	2	41	.03	.100	8	16	.21	65	.01	4	1.89	.02	.05	1	1
CL6W 2+00N	1	24	44	120	.4	18	5	214	3.89	47	5	ND	2	9	1	2	2	40	.04	.103	9	17	.18	66	.01	2	1.26	.01	.06	1	1
CL6W 1+25N	1	31	57	160	.9	23	7	281	4.68	36	5	ND	1	17	1	2	2	32	.08	.066	6	18	.31	84	.01	2	2.11	.02	.03	1	1
CL6W 1+00N	1	36	44	137	1.4	20	8	427	5.00	46	5	ND	2	7	1	2	2	34	.04	.088	4	16	.29	62	.01	2	1.80	.02	.06	1	2
CL6W 0+75N	1	29	48	145	.8	20	6	285	4.96	40	5	ND	2	24	1	7	2	37	.10	.082	6	19	.30	89	.01	2	1.78	.02	.05	1	1
CL6W 0+50N	2	44	75	1368	1.7	46	13	1835	4.89	47	5	ND	2	172	27	12	2	30	.36	.133	12	21	.43	238	.01	2	1.98	.03	.07	6	6
CL6W 0+25N	1	16	78	159	1.2	12	5	742	2.54	103	5	ND	2	9	1	6	2	25	.05	.064	14	9	.08	48	.01	5	.84	.01	.03	1	3
CL6W 0+00N	1	20	121	211	7.2	12	4	400	3.32	168	5	ND	3	9	1	6	3	26	.04	.068	15	9	.09	92	.01	3	1.30	.01	.05	1	4
CL5W 13+00N	1	21	36	85	1.8	14	5	242	2.60	18	5	ND	1	8	1	2	2	40	.04	.081	6	23	.30	93	.01	2	2.25	.02	.06	1	2
CL5W 12+75N	1	15	122	100	.9	10	4	818	2.04	80	5	ND	1	14	1	2	2	38	.09	.080	7	15	.20	168	.01	2	1.84	.02	.08	1	6
CL5W 12+50N	1	17	106	113	1.9	15	4	230	2.59	85	5	ND	1	10	1	2	2	40	.06	.081	7	20	.35	111	.01	2	2.35	.02	.08	2	14
CL5W 12+25N	1	17	105	110	2.0	14	5	255	2.51	79	5	ND	1	12	1	2	2	41	.08	.088	7	15	.33	104	.01	3	1.86	.02	.07	1	3
CL5W 12+00N	2	26	262	184	3.4	16	10	1424	3.86	206	5	ND	1	18	1	2	3	48	.09	.175	8	22	.29	206	.01	2	2.68	.03	.11	1	11
CL5W 11+75N	1	25	186	195	3.2	18	6	475	3.52	183	5	ND	1	16	1	2	2	45	.09	.153	8	22	.35	208	.01	2	2.83	.02	.09	1	20
CL5W 11+50N	1	9	51	86	2.5	8	3	137	1.80	27	5	ND	1	13	1	2	2	33	.07	.073	6	18	.24	128	.01	2	1.60	.02	.06	1	3
CL5W 11+25N	2	21	208	250	3.7	18	10	1439	3.87	117	5	ND	2	19	1	2	2	48	.15	.121	9	21	.40	181	.01	2	2.65	.02	.08	3	10
CL5W 11+00N	1	27	176	288	3.7	19	8	1142	3.73	107	5	ND	1	33	2	2	2	37	.36	.189	10	24	.38	256	.01	2	2.76	.03	.11	1	9
CL5W 10+75N	1	19	55	154	1.7	15	6	651	3.32	63	5	ND	1	23	1	2	2	42	.22	.127	6	21	.35	166	.01	4	2.18	.02	.11	1	8
CL5W 10+50N	1	14	49	64	.9	8	3	223	1.81	33	5	ND	1	10	1	2	2	38	.05	.070	7	15	.16	105	.01	4	1.80	.02	.08	1	4
CL5W 10+25N	1	17	43	71	1.1	9	4	442	2.89	30	5	ND	1	10	1	2	2	44	.03	.097	7	17	.16	88	.01	2	1.88	.02	.08	1	23
CL5W 10+00N	2	33	43	196	.4	22	9	3804	4.57	22	5	ND	2	19	2	2	2	50	.10	.252	8	26	.43	230	.01	6	3.54	.03	.13	1	1
CL5W 9+75N	2	29	74	441	2.0	21	8	2022	4.10	46	5	ND	3	43	4	2	2	41	.42	.256	18	22	.41	228	.01	3	3.23	.03	.08	1	16
CL5W 9+50N	1	17	23	68	.3	8	4	468	2.58	17	5	ND	1	12	1	2	2	37	.07	.097	7	14	.16	90	.01	3	1.76	.02	.07	1	3
CL5W 9+25N	2	32	28	135	.2	22	8	481	5.40	24	5	ND	1	9	1	2	2	44	.10	.127	8	25	.46	93	.01	2	3.30	.02	.07	2	1
CL5W 9+00N	1	12	45	57	.5	7	2	180	2.38	42	5	ND	1	7	1	2	2	40	.03	.073	7	15	.16	58	.01	2	1.53	.01	.03	1	3
CL5W 8+75N	1	10	23	47	.1	5	2	130	1.80	17	5	ND	1	8	1	3	2	31	.03	.046	9	9	.09	56	.01	2	1.17	.01	.02	1	14
CL5W 8+50N	1	19	71	204	2.4	14	6	359	6.26	84	5	ND	2	7	1	2	2	57	.05	.128	9	21	.23	58	.01	2	2.04	.01	.06	2	3
CL5W 8+25N	3	46	538	873	4.6	29	8	682	6.40	74	5	ND	3	10	3	6	2	41	.07	.135	14	18	.12	58	.01	2	1.26	.01	.06	3	7
CL5W 8+00N	1	26	167	345	6.7	28	8	317	5.26	53	5	ND	3	8	2	3	2	37	.07	.095	9	22	.29	87	.01	3	2.51	.02	.06	1	6
CL5W 7+75N	2	34	94	212	5.2	31	12	499	4.89	34	5	ND	3	16	1	2	2	44	.15	.071	11	26	.49	142	.03	4	3.08	.03	.08	1	5
CL5W 7+50N	1	36	495	584	4.2	13	5	410	2.54	60	5	ND	1	13	9	34	2	34	.14	.044	10	11	.20	79	.02	7	1.03	.02	.05	1	15
CL5W 7+25N	1	28	54	144	.6	18	10	491	5.82	36	5	ND	3	10	1	2	2	44	.10	.122	7	25	.33	95	.03	7	3.80	.02	.04	1	1
STD C/AU-S	19	59	42	132	7.1	67	27	1037	4.05	44	18	8	37	49	18	15	17	56	.49	.089	37	60	.89	178	.08	33	1.87	.08	.14	12	48

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL5W 7+00N	1	24	124	278	1.6	16	7	338	4.95	49	5	ND	1	19	3	2	2	52	.16	.109	7	24	.31	137	.02	2	2.53	.02	.05	1	1
CL5W 6+75N	1	17	48	98	.5	8	4	233	4.50	45	5	ND	1	10	1	2	2	58	.06	.061	8	15	.14	78	.03	2	1.52	.01	.04	1	1
CL5W 6+50N	1	10	36	55	.3	4	2	105	1.79	24	5	ND	1	10	1	2	2	36	.07	.029	9	7	.05	72	.02	2	.87	.02	.03	1	4
CL5W 6+25N	1	21	32	129	.6	22	8	644	3.26	29	5	ND	1	69	1	2	2	35	.60	.072	9	26	.50	173	.02	3	1.72	.03	.05	1	1
CL5W 6+00N	1	19	36	152	.3	16	6	241	4.40	34	5	ND	1	89	1	2	2	57	.55	.080	5	23	.38	188	.02	2	1.99	.03	.05	1	1
CL5W 5+75N	1	29	35	175	.6	27	10	588	4.79	35	5	ND	2	53	1	2	2	49	.35	.083	15	27	.47	223	.01	2	2.95	.03	.06	1	1
CL5W 5+50N	1	24	18	100	.1	24	9	755	4.35	21	5	ND	1	32	1	2	2	45	.36	.070	11	29	.61	164	.06	2	2.00	.03	.05	1	1
CL5W 5+25N	1	20	26	111	.2	26	10	563	3.91	24	5	ND	2	20	1	2	2	43	.23	.060	8	28	.57	160	.03	2	2.19	.03	.06	1	2
CL5W 5+00N	1	31	36	143	.3	33	11	685	4.56	39	5	ND	2	17	1	2	2	44	.17	.071	9	24	.41	113	.02	2	1.86	.02	.07	1	3
CL5W 4+75N	1	40	44	170	.3	45	17	1320	4.59	32	5	ND	3	26	1	2	2	36	.30	.084	12	23	.45	125	.02	2	1.38	.03	.06	2	1
CL5W 4+50N	1	37	43	175	.8	42	13	723	4.40	30	5	ND	2	49	1	2	2	34	.39	.093	12	23	.46	134	.01	2	1.65	.03	.09	1	4
CL5W 4+25N	2	64	81	266	.5	83	30	2981	5.65	82	5	ND	3	23	1	2	2	27	.15	.062	12	28	.59	117	.01	2	1.60	.02	.05	1	7
CL5W 4+00N	1	47	60	219	1.0	58	19	1418	5.04	68	5	ND	3	17	1	2	2	33	.10	.058	11	27	.47	92	.01	2	1.79	.02	.04	1	1
CL5W 3+75N	1	16	66	167	1.0	15	4	173	2.96	99	5	ND	3	6	1	4	2	26	.02	.041	15	7	.10	55	.01	5	1.20	.02	.03	1	2
CL5W 3+50N	1	11	37	62	1.1	8	3	111	2.47	27	5	ND	2	6	1	3	2	40	.03	.031	11	11	.09	40	.02	2	1.08	.01	.02	1	4
CL5W 3+25N	2	28	45	125	.4	42	12	372	4.32	112	5	ND	3	6	1	5	2	29	.02	.056	12	16	.17	56	.01	3	1.40	.01	.04	1	1
CL5W 3+00N	1	29	67	394	.9	36	10	426	5.68	143	5	ND	3	7	1	2	2	48	.04	.092	9	26	.39	78	.01	2	1.64	.02	.05	2	1
CL5W 2+75N	1	24	57	305	.5	36	11	655	5.00	155	5	ND	2	83	1	4	2	43	.35	.100	7	26	.48	141	.01	2	2.42	.03	.08	1	1
CL5W 2+50N	2	18	44	152	.9	18	6	249	4.78	96	5	ND	2	10	1	2	2	48	.04	.084	8	20	.19	56	.01	2	1.73	.02	.06	1	1
CL5W 2+25N	1	20	34	120	1.1	17	6	244	3.90	56	5	ND	2	10	1	2	2	38	.05	.100	12	15	.18	70	.01	2	1.42	.02	.05	1	1
CL5W 2+00N	1	21	42	164	.3	18	7	670	3.42	51	5	ND	1	75	1	4	2	39	.23	.059	10	17	.24	175	.01	4	1.35	.02	.05	1	2
CL5W 1+75N	2	35	63	279	1.1	42	11	1189	3.99	59	6	ND	2	172	2	7	2	35	.36	.073	14	28	.45	211	.01	2	1.96	.03	.09	2	2
CL5W 1+50N	1	22	51	169	.9	21	7	538	5.07	53	5	ND	2	12	1	3	2	41	.08	.098	8	21	.25	88	.01	5	1.77	.02	.05	2	1
CL5W 1+25N	1	36	57	182	.4	30	9	612	5.30	48	5	ND	2	12	1	6	2	41	.07	.082	8	22	.37	87	.01	2	2.00	.02	.04	1	1
CL5W 1+00N	2	24	40	140	.1	18	6	331	5.05	45	5	ND	2	9	1	2	2	41	.03	.068	7	20	.23	84	.01	2	1.70	.02	.04	1	2
CL5W 0+75N	2	27	36	141	.2	23	9	567	4.81	41	5	ND	2	8	1	4	2	41	.04	.085	7	22	.33	72	.01	2	1.71	.02	.06	1	1
CL5W 0+50N	1	24	39	145	.1	21	8	495	5.03	39	5	ND	2	14	1	2	2	40	.10	.089	6	20	.31	120	.01	2	1.68	.02	.04	1	1
CL5W 0+25N	1	30	70	246	.4	26	9	585	4.82	58	5	ND	2	13	1	5	2	40	.08	.097	8	25	.26	129	.01	2	1.84	.02	.08	2	1
CL5W 0+00N	1	24	39	134	.1	15	6	434	5.38	44	5	ND	2	11	1	3	2	48	.08	.067	7	19	.20	74	.01	2	1.63	.02	.07	1	2
CL4W 13+00N	1	10	42	43	.2	6	3	282	2.24	32	5	ND	1	8	1	3	2	44	.03	.066	9	13	.13	55	.01	2	1.48	.02	.06	1	1
CL4W 12+75N	1	27	69	113	.7	17	8	678	3.98	56	5	ND	2	8	1	2	2	44	.04	.107	9	20	.30	91	.01	2	2.06	.02	.06	1	1
CL4W 12+50N	1	19	64	98	1.9	12	5	429	3.50	67	5	ND	1	8	1	2	2	43	.05	.108	8	19	.21	75	.01	4	1.88	.02	.05	1	13
CL4W 12+25N	1	13	28	69	.6	7	3	227	2.80	21	5	ND	1	10	1	2	2	41	.03	.102	9	14	.17	65	.01	2	1.65	.02	.05	1	1
CL4W 12+00N	1	15	27	110	1.6	12	5	516	2.57	14	5	ND	1	17	1	2	2	36	.10	.103	9	17	.23	193	.01	5	2.18	.03	.08	1	1
CL4W 11+75N	1	16	27	105	.9	15	6	249	2.86	21	5	ND	1	13	1	2	2	42	.08	.087	8	16	.36	142	.01	2	2.18	.02	.08	2	1
CL4W 11+50N	1	18	39	136	.7	18	6	275	3.25	34	5	ND	1	17	1	2	2	47	.12	.087	7	21	.48	162	.01	3	2.33	.03	.07	1	1
STD C/AU-S	18	59	41	132	7.3	69	28	1052	3.98	39	18	7	37	50	18	16	18	57	.48	.090	37	61	.86	178	.08	32	1.83	.08	.13	13	51

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL4W 11+25N	1	19	46	119	1.8	15	6	309	3.18	42	5	ND	1	12	1	2	2	40	.08	.088	7	19	.39	109	.01	3	2.12	.02	.06	1	1
CL4W 11+00N	1	16	22	117	1.4	12	5	290	2.63	13	5	ND	1	13	1	2	2	37	.07	.095	7	18	.28	131	.01	2	2.16	.02	.07	1	2
CL4W 10+75N	2	25	101	319	2.1	20	13	1558	4.01	83	5	ND	1	31	3	2	2	43	.30	.175	11	23	.39	223	.01	2	2.44	.03	.10	1	2
CL4W 10+50N	1	30	52	205	2.9	21	12	1476	4.46	48	5	ND	2	17	1	2	2	51	.13	.159	9	27	.39	238	.01	4	3.21	.02	.10	2	1
CL4W 10+25N	1	11	20	65	.9	9	4	215	1.59	8	5	ND	1	13	1	2	2	34	.07	.058	6	15	.23	121	.01	2	1.89	.02	.05	1	1
CL4W 10+00N	1	14	27	75	.3	11	6	676	3.13	17	5	ND	1	11	1	2	2	50	.07	.083	6	20	.29	113	.01	2	1.85	.02	.07	1	2
CL4W 9+75N	1	13	24	82	.5	11	6	1226	2.47	13	5	ND	1	13	1	2	2	41	.11	.062	6	15	.26	140	.01	2	1.58	.02	.07	2	3
CL4W 9+50N	1	22	28	108	.8	17	6	294	3.90	25	5	ND	2	9	1	2	2	41	.06	.074	6	21	.40	71	.01	2	2.17	.02	.05	1	7
CL4W 9+25N	1	21	31	110	.3	14	7	640	4.96	23	5	ND	1	9	1	2	2	61	.05	.086	6	21	.30	112	.02	3	1.70	.02	.07	2	3
CL4W 9+00N	1	18	42	79	.4	8	4	656	2.82	24	5	ND	1	12	1	2	2	58	.06	.109	6	16	.15	116	.01	2	2.11	.02	.11	2	3
CL4W 8+75N	1	12	30	86	.7	12	4	144	2.34	18	5	ND	1	9	1	2	2	37	.06	.047	6	19	.27	116	.01	6	2.25	.02	.07	2	5
CL4W 8+50N	1	30	37	136	1.2	19	9	598	5.02	45	5	ND	1	10	1	2	2	50	.09	.090	6	22	.40	113	.01	3	2.17	.02	.08	1	6
CL4W 8+25N	1	24	39	145	2.2	19	6	240	3.59	30	5	ND	2	9	1	2	2	42	.05	.092	7	23	.37	133	.01	2	2.95	.02	.09	2	1
CL4W 8+00N	5	102	5158	1726	138.5	23	12	2887	6.75	4746	8	ND	4	32	39	59	2	27	.22	.086	11	12	.23	162	.01	2	.83	.02	.07	4	890
CL4W 7+75N	11	98	5906	1649	106.4	24	12	2501	7.12	3999	5	ND	4	29	34	75	4	20	.19	.082	10	8	.17	170	.01	2	.66	.03	.07	2	760
CL4W 7+50N	2	28	149	220	2.9	24	9	519	4.84	102	5	ND	2	9	1	4	2	45	.09	.101	8	20	.34	72	.01	2	2.18	.02	.05	1	8
CL4W 7+25N	1	19	53	143	1.1	13	6	366	5.09	34	5	ND	2	9	1	2	2	50	.07	.108	7	20	.29	64	.02	2	2.26	.02	.05	1	1
CL4W 7+00N	2	47	45	159	1.1	57	21	1299	5.18	54	5	ND	4	35	1	4	2	35	.47	.094	12	19	.50	149	.01	2	1.31	.03	.09	1	3
CL4W 6+75N	1	27	40	169	.6	27	10	667	4.76	29	5	ND	1	17	1	2	2	49	.19	.086	9	28	.54	174	.01	2	2.54	.02	.10	1	1
CL4W 6+50N	1	21	40	148	1.0	17	6	281	4.35	29	5	ND	1	47	1	2	2	46	.45	.076	6	26	.44	111	.01	2	2.61	.03	.06	1	1
CL4W 6+25N	1	20	30	116	.5	18	7	379	5.47	28	5	ND	1	10	1	4	2	57	.07	.081	6	28	.39	90	.02	4	2.06	.02	.06	1	1
CL4W 6+00N	1	22	24	116	.6	21	7	314	5.31	22	5	ND	1	9	1	2	2	55	.08	.076	6	30	.51	103	.03	6	2.43	.02	.07	1	2
CL4W 5+75N	1	20	31	145	.5	20	7	329	5.61	34	5	ND	1	9	1	2	2	51	.08	.073	6	30	.47	108	.03	2	2.78	.02	.07	1	1
CL4W 5+50N	2	31	42	198	.8	31	12	2029	5.14	29	5	ND	2	34	1	5	2	54	.32	.104	11	32	.58	298	.01	2	3.77	.03	.11	1	1
CL4W 5+25N	1	32	31	148	.6	28	13	954	4.56	26	5	ND	2	36	1	4	2	46	.45	.076	10	29	.57	162	.03	2	1.71	.03	.07	1	2
CL4W 5+00N	1	38	38	191	.5	32	10	489	4.72	30	5	ND	3	17	1	2	2	42	.15	.076	10	23	.45	141	.01	2	2.09	.02	.07	1	1
CL4W 4+75N	1	24	32	108	.4	21	7	216	3.74	26	5	ND	2	9	1	2	2	36	.04	.059	11	13	.17	74	.01	2	1.15	.01	.04	1	1
CL4W 4+50N	1	16	35	101	1.0	11	5	706	4.08	32	5	ND	1	10	1	2	2	58	.07	.110	7	19	.20	84	.03	2	1.35	.02	.05	1	1
CL4W 4+25N	2	42	41	191	1.0	51	12	461	5.84	60	5	ND	2	6	1	6	2	29	.02	.107	9	18	.25	64	.01	2	1.40	.01	.06	1	1
CL4W 4+00N	1	37	37	169	1.2	38	12	552	4.91	36	5	ND	3	13	1	3	2	37	.13	.119	10	21	.39	103	.01	2	1.69	.02	.08	1	1
CL4W 3+75N	1	30	38	134	.4	29	8	298	4.46	32	5	ND	2	8	1	2	2	36	.05	.073	9	19	.26	72	.01	2	1.46	.02	.05	1	1
CL4W 3+50N	1	38	42	163	.5	36	9	339	4.84	36	5	ND	2	9	1	2	2	34	.05	.077	9	23	.29	67	.01	2	1.52	.02	.06	1	2
CL4W 3+25N	2	35	40	144	.7	34	10	423	4.67	36	5	ND	2	11	1	2	2	38	.10	.095	10	19	.32	68	.01	4	1.47	.02	.06	1	1
CL4W 3+00N	1	30	34	145	.4	33	10	399	4.51	32	5	ND	2	12	1	2	2	36	.11	.090	9	20	.33	100	.01	2	1.38	.02	.05	1	1
CL4W 2+75N	2	53	45	266	.7	66	16	1010	5.15	39	5	ND	3	22	1	5	2	29	.15	.049	10	27	.48	143	.01	2	1.68	.02	.07	1	1
CL4W 2+50N	1	46	58	232	1.8	58	24	2470	4.89	33	5	ND	2	113	2	3	2	30	.33	.107	10	31	.42	255	.01	2	2.09	.02	.08	2	1
STD C/AU-S	18	59	41	132	7.3	68	28	1036	3.99	41	17	7	36	49	18	14	22	56	.48	.091	37	60	.86	176	.08	32	1.83	.08	.14	14	48

SOUTHERN GOLD PROJECT-121104 FILE # 87-3381

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL4W 2+25N	1	55	47	204	1.0	58	18	1733	5.16	35	5	ND	2	73	1	2	2	31	.36	.087	9	30	.49	145	.01	2	1.77	.03	.07	2	1
CL4W 2+00N	2	49	58	296	2.6	51	14	1591	4.85	58	5	ND	2	135	2	4	2	35	.59	.078	12	31	.52	243	.01	2	2.27	.03	.09	1	1
CL4W 1+75N	1	46	47	183	.4	49	14	912	5.40	34	5	ND	2	76	1	2	2	33	.29	.102	8	29	.47	111	.01	2	1.68	.02	.06	1	1
CL4W 1+50N	1	26	41	124	.7	15	6	238	3.85	67	5	ND	2	12	1	5	2	44	.05	.076	10	16	.11	66	.01	2	1.08	.01	.05	2	21
CL4W 1+25N	1	15	36	104	.9	13	5	264	3.85	34	5	ND	2	10	1	2	2	49	.05	.080	10	15	.17	87	.02	4	1.29	.01	.04	1	1
CL4W 1+00N	1	16	27	90	.2	9	3	131	2.01	37	5	ND	3	11	1	4	2	28	.03	.037	13	4	.06	60	.01	3	1.01	.01	.03	1	7
CL4W 0+75N	1	30	53	179	1.0	26	7	360	4.90	61	5	ND	2	16	1	4	2	36	.09	.095	8	22	.26	116	.01	2	2.00	.02	.04	1	1
CL4W 0+50N	2	40	47	183	1.9	45	11	683	6.48	67	5	ND	2	8	1	3	2	29	.06	.111	8	25	.37	64	.01	2	1.49	.02	.04	1	1
CL4W 0+25N	2	44	113	277	.5	49	20	1298	4.87	90	5	ND	2	24	1	3	2	32	.09	.076	11	21	.31	155	.01	2	1.62	.02	.04	1	1
CL4W 0+00N	2	41	82	279	1.0	48	16	824	5.20	89	5	ND	3	23	2	4	2	30	.23	.088	10	20	.33	106	.01	2	1.37	.02	.04	1	1
CL4E 2+25N	4	29	57	252	.3	32	18	5361	5.47	38	5	ND	1	35	2	2	2	53	.37	.106	9	34	.46	316	.02	2	2.37	.03	.08	1	6
CL4E 2+00N	2	27	44	167	.1	19	8	418	5.57	32	5	ND	2	13	1	3	2	60	.12	.107	8	27	.34	148	.02	5	2.05	.02	.06	1	1
CL4E 1+75N	2	46	53	242	1.6	29	14	2911	4.65	28	5	ND	1	62	3	3	2	45	1.17	.098	17	34	.48	274	.01	2	2.09	.04	.05	1	1
CL4E 1+50N	1	14	28	120	.1	10	5	324	4.03	21	5	ND	2	11	1	2	2	57	.11	.083	9	18	.17	124	.02	2	1.46	.02	.04	1	1
CL4E 1+25N	2	54	42	272	1.7	31	12	2437	4.66	30	5	ND	2	56	4	3	2	45	1.05	.089	20	37	.49	330	.01	2	2.50	.03	.08	1	1
CL4E 1+00N	3	28	61	239	.7	18	13	8199	3.99	39	5	ND	1	50	3	2	2	38	.80	.141	9	16	.23	466	.01	2	1.32	.03	.07	1	1
CL4E 0+75N	2	25	47	198	.3	14	9	989	4.39	34	5	ND	1	35	1	3	2	50	.52	.095	11	18	.21	233	.01	2	1.88	.02	.04	2	14
CL4E 0+50N	2	64	62	262	2.2	36	13	1229	4.87	48	5	ND	2	38	2	2	2	39	.61	.073	18	38	.49	241	.01	2	2.25	.03	.07	1	115
CL4E 0+25N	2	56	107	272	3.5	30	15	1210	4.58	63	5	ND	3	46	3	4	2	34	.67	.089	19	30	.33	229	.01	2	1.82	.03	.07	1	4
CL3W 13+00N	1	24	33	109	1.6	19	6	269	3.47	22	5	ND	1	11	1	4	2	42	.08	.106	8	23	.45	119	.01	7	2.47	.02	.07	1	2
CL3W 12+75N	1	27	64	129	2.5	15	6	636	2.90	42	5	ND	1	21	1	2	2	37	.20	.138	8	19	.33	151	.01	2	2.18	.02	.07	1	1
CL3W 12+50N	1	23	42	147	.6	15	7	636	3.69	34	5	ND	1	15	1	2	2	50	.11	.101	8	21	.37	151	.01	2	2.26	.02	.06	2	3
CL3W 12+25N	1	21	103	133	1.0	13	6	595	6.00	144	5	ND	1	20	1	2	2	57	.21	.215	6	16	.26	124	.01	2	1.77	.02	.05	1	3
CL3W 12+00N	1	21	18	84	1.5	13	4	286	2.69	10	5	ND	1	10	1	3	2	42	.04	.076	7	21	.29	110	.01	4	2.17	.02	.05	1	3
CL3W 11+75N	1	28	21	121	.8	20	7	406	4.76	30	5	ND	1	10	1	2	2	58	.05	.080	7	24	.47	129	.01	2	2.44	.02	.07	1	2
CL3W 11+50N	1	14	33	95	.5	17	5	196	2.81	33	5	ND	1	14	1	2	2	42	.09	.061	6	21	.40	114	.01	2	1.91	.02	.05	2	4
CL3W 11+25N	1	20	25	102	2.0	17	6	289	3.91	15	5	ND	1	14	1	2	2	50	.09	.115	9	26	.43	144	.01	2	2.71	.03	.08	1	2
CL3W 11+00N	1	19	29	115	1.3	17	7	489	3.11	23	5	ND	1	18	1	2	2	46	.11	.103	7	21	.36	171	.01	2	2.48	.02	.07	1	1
CL3W 10+75N	1	12	36	134	.2	15	5	283	2.90	26	5	ND	1	17	1	2	2	45	.12	.053	6	19	.45	153	.01	2	1.96	.02	.04	1	1
CL3W 10+50N	1	15	35	96	.4	11	6	693	2.97	25	5	ND	1	21	1	2	2	44	.17	.080	8	17	.22	214	.01	2	1.41	.02	.05	2	2
CL3W 10+25N	1	16	16	79	.5	9	4	173	2.44	8	5	ND	1	17	1	2	2	40	.10	.070	7	15	.26	120	.01	5	2.01	.02	.04	1	1
CL3W 10+00N	1	22	17	101	1.0	14	7	532	2.89	15	5	ND	1	19	1	2	2	39	.14	.113	8	20	.29	175	.01	2	2.02	.02	.05	1	1
CL3W 9+75N	2	22	21	129	.4	15	7	388	4.37	20	5	ND	1	18	1	2	2	59	.14	.129	7	20	.38	170	.01	2	2.54	.02	.07	1	2
CL3W 9+50N	1	27	34	107	.5	14	7	481	5.16	26	5	ND	1	9	1	3	2	63	.05	.104	7	23	.28	74	.01	2	2.22	.02	.05	1	9
CL3W 9+25N	2	53	33	203	2.9	25	11	3148	4.96	23	5	ND	3	19	1	2	2	50	.07	.235	11	30	.39	276	.01	2	4.17	.02	.11	1	2
CL3W 9+00N	2	21	34	185	1.1	15	7	1380	3.96	37	5	ND	1	85	1	2	2	47	.29	.134	8	19	.32	255	.01	2	2.15	.02	.06	1	1
STD C/AU-S	18	59	42	132	7.1	68	28	1047	4.00	41	18	7	37	50	18	16	21	57	.48	.091	37	61	.88	178	.08	33	1.83	.09	.13	15	53

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
CL3W 8+75N	1	35	30	143	.4	23	10	934	5.69	25	5	ND	2	13	1	2	2	53	.12	.150	7	27	.48	114	.01	3	3.30	.02	.08	1	1
CL3W 8+50N	1	14	32	100	.8	13	5	407	4.55	30	5	ND	1	12	1	2	2	61	.11	.118	7	18	.30	81	.03	2	2.09	.02	.06	1	1
CL3W 1+25N	2	89	75	328	1.4	128	36	1860	6.55	111	5	ND	5	26	1	8	2	21	.31	.095	18	15	.34	72	.01	3	.92	.02	.07	1	3
CL3W 1+00N	2	66	95	303	1.2	91	25	1322	5.61	86	5	ND	3	32	2	6	2	24	.36	.086	13	16	.38	94	.01	2	1.05	.03	.07	1	3
CL3W 0+75N	1	41	87	216	1.1	41	16	1016	4.73	48	5	ND	3	22	1	2	2	35	.24	.094	12	22	.41	105	.01	2	1.44	.02	.06	1	1
CL3W 0+50N	1	75	31	159	.7	93	22	1159	4.99	45	5	ND	1	20	1	4	2	23	.21	.081	3	15	.27	106	.01	2	1.08	.02	.07	1	1
CL3W 0+25N	2	72	36	187	.4	85	19	1229	6.15	46	5	ND	1	15	1	2	2	30	.17	.091	3	21	.34	118	.01	4	1.48	.02	.05	1	2
CL3W 0+00N	1	49	46	191	.5	72	16	800	4.47	36	5	ND	2	41	1	2	2	30	.23	.062	7	22	.37	124	.01	2	1.57	.02	.06	1	1
CL3E 2+25N	3	24	56	200	.9	14	9	1828	3.83	56	5	ND	2	41	2	2	2	39	1.10	.069	11	22	.16	91	.01	2	1.48	.03	.06	1	1
CL3E 2+00N	1	24	57	245	.7	18	7	389	6.25	49	5	ND	2	10	1	2	2	40	.12	.224	8	30	.27	100	.01	2	1.93	.02	.05	1	3
CL3E 1+75N	1	20	55	175	.4	17	6	317	5.75	46	5	ND	2	9	1	2	2	48	.07	.228	9	21	.23	93	.01	2	2.02	.02	.05	1	4
CL3E 1+50N	1	17	34	109	.2	10	4	162	3.37	35	5	ND	2	6	1	3	2	38	.03	.064	11	14	.09	51	.01	2	1.31	.01	.04	1	1
CL3E 1+25N	1	24	55	226	.7	26	9	290	4.57	49	5	ND	2	7	1	2	2	31	.05	.089	10	26	.29	115	.01	2	2.98	.01	.06	1	1
CL3E 1+00N	1	22	44	216	.3	18	7	461	4.90	47	5	ND	2	17	1	2	2	46	.25	.106	10	21	.23	197	.01	2	1.84	.02	.04	1	16
CL3E 0+75N	1	28	71	293	.4	31	12	605	4.83	53	5	ND	2	18	1	2	2	35	.29	.072	9	28	.41	179	.01	4	1.97	.02	.05	1	1
CL3E 0+50N	1	40	97	303	1.2	26	15	524	5.92	52	7	ND	4	23	3	2	2	43	.31	.072	14	29	.23	213	.01	2	3.23	.02	.05	2	2
CL3E 0+00N	1	25	72	179	.9	30	11	194	3.41	34	5	ND	2	29	1	2	2	30	.55	.114	14	29	.44	69	.02	2	1.15	.03	.05	1	1
CL2E 2+50N	1	25	50	202	.4	23	8	308	6.15	45	6	ND	2	9	1	2	2	52	.08	.128	7	24	.38	112	.01	3	2.54	.02	.06	1	2
CL2E 2+25N	2	21	48	135	.4	14	5	218	4.74	38	5	ND	2	11	1	2	2	52	.12	.077	9	18	.19	111	.01	2	1.86	.02	.04	1	1
CL2E 2+00N	1	17	32	99	.3	12	4	207	3.54	27	5	ND	1	9	1	2	2	46	.07	.077	9	15	.13	68	.02	2	1.28	.01	.03	1	1
CL2E 1+75N	1	12	23	92	.3	9	3	167	2.46	23	5	ND	2	13	1	2	2	39	.13	.068	11	13	.12	89	.01	3	1.05	.01	.04	1	2
CL2E 1+50N	1	25	50	135	.2	18	7	726	7.46	51	5	ND	2	8	1	2	2	45	.09	.173	7	26	.46	69	.01	2	2.08	.02	.04	1	1
CL2E 1+25N	2	39	112	269	1.4	34	12	864	4.93	62	5	ND	2	18	1	4	2	32	.33	.101	11	24	.42	108	.01	4	1.80	.02	.08	1	2
CL2E 1+00N	2	39	105	275	1.2	34	12	890	5.00	64	5	ND	2	17	1	2	2	33	.31	.099	11	22	.41	119	.01	2	1.90	.03	.07	2	1
CL2E 0+75N	2	34	105	285	1.1	36	13	1279	4.78	62	5	ND	2	37	2	4	2	32	.67	.088	10	19	.44	153	.01	2	1.73	.03	.06	1	4
CL2E 0+50N	2	33	66	215	1.2	30	12	804	5.75	62	5	ND	2	43	1	3	2	42	.81	.084	9	27	.42	152	.01	2	2.04	.03	.07	1	2
CL2E 0+25N	2	30	64	200	.6	26	9	495	6.52	55	5	ND	2	20	1	2	2	40	.28	.095	7	24	.38	125	.01	2	2.41	.02	.06	1	1
CL2E 0+00N	1	27	40	118	.6	16	7	624	4.90	36	5	ND	1	11	1	2	2	43	.14	.114	7	21	.22	107	.01	2	1.68	.02	.06	1	1
CL1E 2+50N	1	18	46	166	.9	16	8	913	6.08	45	5	ND	1	9	1	2	2	53	.07	.189	8	20	.25	130	.01	2	2.07	.01	.06	1	2
CL1E 2+25N	1	21	54	136	.8	16	6	451	4.63	37	5	ND	2	10	1	2	2	47	.08	.132	9	19	.24	80	.01	2	1.70	.01	.07	1	3
CL1E 2+00N	1	23	60	174	.5	20	8	1078	4.63	47	5	ND	2	14	1	2	2	44	.17	.123	9	23	.30	135	.01	2	1.87	.02	.05	2	2
CL1E 1+75N	1	26	40	128	.9	22	8	445	4.44	26	5	ND	1	14	1	2	2	43	.18	.101	8	23	.39	116	.01	2	1.90	.02	.07	1	4
CL1E 1+50N	1	27	43	138	.6	21	9	904	4.69	31	5	ND	2	20	1	2	2	48	.22	.103	10	26	.35	187	.01	4	2.04	.02	.06	1	1
CL1E 1+25N	1	28	45	149	.9	24	9	553	4.84	37	5	ND	2	16	1	2	2	45	.16	.091	8	27	.38	153	.01	2	1.96	.02	.08	1	1
CL1E 1+00N	2	33	51	115	1.5	14	7	773	5.81	37	5	ND	1	10	1	2	2	48	.11	.223	6	19	.21	93	.01	2	1.49	.02	.07	1	12
CL1E 0+75N	2	27	42	125	.6	18	7	374	5.25	35	5	ND	1	13	1	2	2	50	.10	.081	7	24	.27	97	.01	2	1.93	.02	.07	1	4
CL1E 0+50N	2	40	50	192	2.4	31	12	2110	4.60	35	5	ND	2	50	2	2	2	41	.69	.143	13	27	.44	264	.01	2	2.75	.03	.11	1	2
STD C/AU-S	18	58	43	132	7.3	68	26	1027	3.96	41	24	7	37	47	17	16	21	55	.48	.087	35	58	.87	175	.08	32	1.83	.08	.13	13	52

ACME ANALYTICAL LABORATORIES   852 E. HASTINGS ST. VANCOUVER B.C.   V6A 1R6   PHONE 253-3158   DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-15 SOIL P16 ROCK   AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: AUG 31 1987   DATE REPORT MAILED: Sept 10/87   ASSAYER D. Toye ...DEAN TOYE, CERTIFIED B.C. ASSAYER

SOUTHERN GOLD PROJECT-121104   File # 87-3784   Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
26W 21+00N	1	39	25	129	.1	34	15	1392	4.83	12	5	ND	3	22	1	2	2	62	.26	.210	12	35	.68	143	.03	2	2.88	.01	.06	1	1
26W 20+75N	1	41	15	104	.1	32	12	823	4.71	12	5	ND	1	17	1	2	2	63	.20	.165	11	34	.61	94	.02	2	2.60	.01	.05	1	2
26W 20+50N	1	75	20	143	.4	39	22	2238	5.32	12	5	ND	5	78	1	2	2	77	.69	.121	22	48	1.89	424	.08	3	2.76	.02	.07	1	1
26W 20+25N	1	100	69	207	.5	35	21	1121	5.29	15	5	ND	3	56	1	2	2	48	.47	.129	23	33	.81	233	.04	2	2.58	.01	.08	1	2
26W 20+00N	1	61	25	155	.3	38	18	1310	5.00	16	6	ND	1	30	1	2	2	63	.32	.157	14	39	.87	160	.04	2	2.50	.01	.07	1	1
26W 19+75N	1	78	50	155	1.1	32	23	1580	4.86	10	5	ND	7	107	1	4	2	65	.75	.154	22	40	1.17	402	.12	5	1.92	.02	.08	1	1
26W 19+50N	1	78	29	112	.4	36	23	1191	3.84	9	5	ND	10	70	1	2	2	51	.63	.115	23	32	1.17	343	.08	5	1.74	.01	.14	1	1
26W 19+00N	2	79	62	160	.8	35	31	2177	4.66	16	5	ND	6	51	1	4	2	48	.72	.142	30	40	.96	329	.04	2	1.63	.02	.13	1	1
26W 18+75N	4	65	104	204	1.1	37	31	1616	3.83	21	5	ND	11	59	1	2	2	38	1.34	.114	28	34	.88	322	.02	4	1.49	.02	.15	1	5
26W 18+50N	4	67	134	229	1.1	28	25	1275	3.50	18	5	ND	8	102	1	2	2	31	3.39	.110	25	28	.67	325	.01	7	1.29	.02	.21	1	14
26W 16+00N	2	65	97	161	.4	27	20	4432	4.07	12	5	ND	2	26	1	8	2	38	.15	.261	16	27	.42	246	.01	4	2.60	.01	.09	1	1
26W 15+75N	1	36	484	178	.2	13	16	2841	3.29	14	5	ND	1	18	1	7	2	33	.13	.216	22	17	.23	199	.01	3	2.31	.01	.10	1	1
26W 15+50N	1	41	447	239	.4	20	15	1678	3.19	14	5	ND	2	22	1	4	2	33	.24	.150	19	20	.37	176	.03	4	2.00	.01	.10	1	1
26W 15+25N	1	54	159	197	.6	22	16	2611	4.03	14	6	ND	2	31	2	2	2	38	.29	.183	22	24	.43	232	.03	4	2.28	.01	.11	2	4
26W 15+00N	1	28	37	90	.1	13	7	602	3.18	9	5	ND	1	16	1	2	2	31	.07	.197	14	19	.25	100	.01	5	2.66	.01	.07	1	2
26W 14+75N	1	26	30	92	.2	10	7	1530	2.17	10	5	ND	1	34	1	2	2	25	.21	.203	20	14	.18	258	.01	4	1.82	.01	.09	1	2
26W 14+50N	1	33	30	114	.2	23	17	1380	3.02	10	5	ND	1	45	1	2	2	32	.21	.197	20	23	.41	152	.02	2	2.44	.01	.06	1	1
26W 14+25N	1	35	32	123	.1	38	24	1204	3.28	10	5	ND	2	23	1	2	2	29	.09	.165	20	24	.35	198	.02	3	2.52	.01	.08	1	1
26W 14+00N	1	28	28	117	.1	33	14	562	3.39	14	5	ND	1	24	1	2	2	39	.11	.148	18	26	.41	122	.02	3	2.56	.01	.07	1	7
26W 13+75N	1	25	26	95	.1	20	12	752	3.11	12	5	ND	2	21	1	2	2	34	.16	.134	18	18	.37	119	.02	5	1.94	.01	.07	1	1
26W 13+50N	1	31	30	133	.1	28	14	1091	3.40	17	5	ND	1	31	1	2	2	35	.12	.202	26	23	.43	202	.02	2	2.93	.01	.07	1	1
26W 13+25N	1	28	29	92	.2	22	13	1243	2.53	15	5	ND	1	43	1	2	2	25	.15	.161	20	17	.30	251	.01	2	2.45	.01	.07	1	1
26W 13+00N	2	22	36	102	.5	20	11	1915	2.60	15	5	ND	1	44	1	2	2	27	.18	.221	14	17	.28	198	.01	5	2.22	.01	.07	1	1
26W 12+75N	2	19	27	78	.6	15	15	4248	2.06	11	5	ND	1	40	1	2	2	21	.16	.257	16	13	.19	232	.01	4	1.82	.01	.07	1	1
26W 12+50N	1	32	38	118	.1	22	11	826	3.83	17	5	ND	1	28	1	2	2	39	.14	.133	17	20	.41	140	.02	4	2.23	.01	.06	1	1
26W 12+25N	1	26	34	113	.1	16	10	1347	3.41	18	5	ND	1	18	1	2	2	34	.05	.155	14	16	.29	179	.01	4	1.79	.01	.07	1	1
26W 12+00N	1	31	30	89	.3	17	10	1363	2.81	10	8	ND	1	29	2	2	2	23	.12	.172	17	13	.28	201	.01	7	1.90	.01	.07	1	1
26W 11+75N	1	34	138	109	.4	15	10	1082	2.80	13	5	ND	1	32	1	2	2	23	.16	.175	19	13	.27	193	.01	6	1.93	.01	.08	1	2
26W 11+50N	2	39	44	112	.1	25	14	953	4.34	14	5	ND	3	33	1	2	2	29	.16	.162	20	17	.43	205	.02	2	2.27	.01	.07	1	1
26W 11+25N	1	33	40	106	.1	20	12	900	3.73	12	5	ND	2	21	1	2	2	30	.15	.159	18	16	.37	136	.01	2	2.04	.01	.08	1	1
26W 11+00N	1	34	46	113	.1	19	13	1595	3.84	12	5	ND	4	20	1	2	3	34	.09	.151	20	18	.38	240	.02	2	2.31	.01	.07	1	1
26W 10+75N	1	30	35	102	.1	21	12	903	3.66	15	5	ND	2	24	1	2	2	30	.14	.129	14	17	.39	126	.01	2	1.92	.01	.07	3	1
26W 10+50N	1	41	40	106	.1	24	16	1199	4.38	15	5	ND	2	27	1	2	2	36	.16	.118	17	20	.53	181	.02	4	2.12	.01	.06	1	1
26W 10+25N	1	34	28	100	.1	22	14	1054	4.06	14	5	ND	3	30	1	2	2	34	.17	.140	15	18	.47	225	.01	4	2.12	.01	.07	1	1
26W 10+00N	1	31	36	105	.1	20	12	1027	4.00	14	5	ND	3	20	1	3	2	34	.11	.130	16	18	.43	195	.01	2	2.19	.01	.07	1	3
26W 9+75N	1	38	23	111	.1	26	13	887	4.03	16	5	ND	2	25	1	3	2	30	.18	.129	15	16	.40	164	.01	2	1.98	.01	.06	2	1
STD C/AU-S	18	61	37	131	7.3	72	29	1053	4.06	38	20	8	41	52	18	17	22	60	.46	.095	39	60	.85	178	.08	37	1.78	.06	.14	12	51

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
26W 9+50N	1	36	23	114	.1	24	12	1298	4.31	21	5	ND	4	20	1	2	2	41	.15	.116	15	16	.38	179	.01	2	1.87	.01	.07	1	1
26W 9+25N	5	85	39	151	.1	31	13	2222	4.99	24	5	ND	5	20	1	4	2	34	.12	.172	15	20	.46	236	.01	2	2.49	.01	.08	1	2
26W 9+00N	2	57	46	154	.1	27	15	2834	4.86	25	5	ND	4	34	1	2	2	38	.06	.200	18	21	.49	224	.01	2	2.75	.01	.09	1	2
24W 20+00N	1	41	37	150	.1	23	10	736	3.24	18	5	ND	2	16	1	2	2	44	.12	.181	14	31	.51	95	.01	3	3.75	.01	.05	2	1
24W 19+75N	1	33	25	106	.2	26	11	744	4.03	21	5	ND	2	24	1	3	2	55	.20	.177	13	34	.48	202	.01	2	2.68	.01	.05	1	2
24W 19+50N	6	78	106	187	.7	43	43	2470	4.63	27	6	ND	10	45	1	2	2	45	.53	.123	27	36	.88	451	.02	4	1.77	.02	.16	1	5
24W 19+25N	2	77	68	169	.6	37	21	2100	4.31	18	7	ND	6	60	1	2	2	55	.58	.122	22	51	1.14	280	.07	3	1.85	.02	.11	2	11
24W 19+00N	2	55	52	141	.4	34	20	1527	4.14	16	5	ND	7	44	1	3	3	51	.56	.131	22	48	1.00	190	.08	4	1.57	.02	.10	1	9
24W 18+75N	1	43	28	100	.4	29	15	881	3.81	14	5	ND	6	54	1	2	2	54	.66	.127	18	47	.97	112	.13	2	1.26	.02	.09	1	8
24W 18+50N	1	43	36	111	.4	32	16	854	4.17	15	5	ND	5	43	1	2	2	56	.57	.127	18	49	.92	127	.10	2	1.22	.01	.07	1	76
24W 18+25N	1	53	37	136	.5	29	16	1241	3.94	12	6	ND	7	73	1	2	2	47	1.26	.130	20	38	.78	237	.06	5	1.24	.02	.15	1	31
24W 18+00N	1	58	34	121	.5	30	18	1373	4.09	15	5	ND	7	87	1	3	2	44	1.77	.123	21	36	.83	271	.05	6	1.33	.02	.16	1	25
24W 17+75N	2	60	15	110	.3	31	21	1547	4.44	13	5	ND	7	103	1	2	2	47	2.00	.128	22	33	.86	273	.05	3	1.26	.02	.16	1	103
24W 14+75N	1	28	88	157	.1	11	11	1434	3.67	18	5	ND	4	22	1	2	2	25	.09	.181	22	10	.21	165	.01	2	2.16	.01	.09	2	3
24W 14+50N	1	26	57	103	.1	12	11	1087	3.15	16	5	ND	3	63	1	2	2	25	.15	.158	18	11	.23	180	.01	2	1.91	.01	.08	1	2
24W 14+25N	1	32	48	122	.1	14	11	1129	3.33	16	6	ND	3	15	1	2	2	25	.06	.125	20	13	.30	227	.01	2	2.07	.01	.06	1	2
24W 14+00N	1	33	52	142	.1	19	11	918	3.06	15	5	ND	2	20	1	2	3	33	.07	.122	20	20	.39	124	.03	4	2.46	.01	.08	1	1
24W 13+75N	1	19	61	94	.1	11	8	1411	2.44	13	5	ND	1	15	1	2	2	28	.07	.133	11	11	.22	188	.01	2	1.58	.01	.07	1	2
24W 13+50N	1	23	67	107	.1	13	8	1054	2.32	16	5	ND	1	14	1	2	3	23	.07	.096	15	13	.28	137	.02	2	1.59	.01	.07	1	3
24W 13+25N	1	22	37	93	.1	15	7	529	2.29	13	5	ND	2	14	1	2	2	28	.09	.062	14	18	.32	89	.03	2	1.50	.01	.06	1	4
24W 13+00N	1	18	31	90	.1	12	6	464	2.07	11	5	ND	2	14	1	2	2	24	.08	.078	12	15	.26	86	.02	2	1.33	.01	.06	1	9
24W 12+75N	1	24	44	107	.1	15	8	579	3.11	21	5	ND	2	17	1	2	2	30	.08	.100	15	16	.26	155	.01	2	2.01	.01	.07	1	8
24W 12+50N	1	19	22	84	.1	13	6	366	2.76	18	5	ND	1	12	1	2	2	36	.04	.103	10	15	.23	93	.01	3	1.64	.01	.05	1	1
24W 12+25N	1	28	26	75	.2	11	6	489	2.62	17	5	ND	1	11	1	2	2	36	.03	.154	10	15	.23	81	.01	3	1.93	.01	.06	1	1
24W 12+00N	1	28	27	126	.2	20	9	779	3.21	17	5	ND	1	25	1	2	3	32	.09	.167	13	19	.40	128	.01	2	2.07	.01	.08	1	1
24W 11+75N	1	29	41	110	.1	23	11	597	3.36	17	5	ND	3	26	1	2	2	34	.17	.101	17	23	.48	98	.03	3	1.79	.01	.07	2	2
24W 11+50N	1	29	41	105	.2	16	9	752	3.32	15	5	ND	2	19	1	2	2	29	.07	.123	14	14	.25	119	.01	4	1.57	.01	.08	1	1
24W 11+25N	1	31	37	122	.1	17	10	1087	3.20	15	5	ND	1	44	1	3	2	30	.23	.171	16	16	.30	256	.01	2	1.89	.01	.09	1	2
24W 11+00N	1	25	37	96	.1	17	10	1000	3.27	16	5	ND	2	19	1	2	2	32	.10	.132	14	17	.34	132	.01	2	1.78	.01	.06	1	4
24W 10+75N	1	25	45	111	.2	15	9	624	3.12	16	5	ND	2	13	1	2	3	27	.05	.121	15	14	.31	113	.01	2	1.92	.01	.07	1	1
24W 10+50N	1	31	32	100	.1	18	10	751	3.31	13	5	ND	3	12	1	2	2	27	.04	.109	14	14	.38	123	.01	2	1.82	.01	.06	1	2
24W 10+25N	1	47	42	113	.1	23	16	1450	4.10	17	7	ND	5	16	1	2	2	29	.08	.125	18	17	.57	183	.02	2	2.51	.01	.07	1	1
24W 10+00N	1	40	33	115	.1	22	13	1177	3.81	17	5	ND	5	17	1	2	2	30	.11	.146	19	17	.57	112	.02	2	2.18	.01	.07	1	2
24W 9+75N	1	35	39	115	.1	21	12	765	3.64	20	5	ND	3	16	1	2	2	29	.11	.133	18	17	.47	111	.02	2	1.97	.01	.07	1	1
24W 9+50N	1	24	25	98	.1	16	8	573	3.39	22	5	ND	1	13	1	2	3	38	.09	.135	12	16	.31	76	.01	2	1.74	.01	.06	1	1
24W 9+25N	1	27	33	93	.1	16	7	501	2.84	23	5	ND	1	15	1	2	2	29	.06	.176	13	14	.21	96	.01	3	1.66	.01	.06	1	1
STD C/AU-S	18	62	40	132	7.5	69	28	1047	3.94	40	18	8	38	51	18	18	23	60	.48	.091	38	59	.82	180	.07	39	1.88	.06	.15	12	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
24W 9+00N	1	25	25	96	.4	20	6	346	2.98	20	5	ND	3	10	1	2	2	28	.04	.101	10	14	.18	86	.01	2	1.52	.01	.06	2	2
24W 5+00N	1	31	84	153	.4	11	11	1831	3.57	17	5	ND	4	19	2	2	2	23	.09	.158	23	12	.25	181	.01	5	2.05	.01	.08	1	3
22W 18+00N	8	86	348	622	1.6	59	74	4158	7.86	55	5	ND	10	85	6	4	2	23	.52	.190	32	9	.20	684	.01	5	1.04	.03	.14	1	13
22W 17+75N	4	76	417	532	2.5	32	29	2170	6.03	29	5	ND	6	64	3	4	2	30	.45	.149	27	18	.43	426	.01	3	1.63	.02	.16	1	36
22W 17+50N	5	51	332	524	1.8	18	25	2361	5.62	38	5	ND	10	86	7	5	2	12	.48	.206	33	6	.13	322	.01	3	.91	.03	.12	1	43
22W 17+25N	7	62	304	497	1.7	28	30	2613	6.57	50	5	ND	9	108	4	11	2	12	.46	.206	31	6	.13	304	.01	5	.77	.04	.11	1	33
22W 17+00N	6	67	179	495	1.6	31	31	2444	6.05	48	5	ND	10	101	4	7	2	14	.47	.188	29	9	.23	275	.01	2	.91	.03	.12	1	53
22W 16+75N	4	44	193	421	.8	21	23	1796	5.00	33	5	ND	8	70	3	6	2	16	.50	.191	29	10	.30	226	.01	3	.84	.02	.09	1	22
22W 16+50N	4	47	235	535	1.3	12	24	3354	5.18	27	6	ND	9	91	7	3	2	12	.51	.193	34	6	.22	394	.01	16	1.19	.03	.15	1	28
22W 16+00N	3	48	304	491	1.2	5	17	2791	5.76	20	5	ND	9	72	7	5	2	11	.50	.179	34	4	.11	467	.01	6	.82	.02	.12	1	16
22W 15+75N	5	66	339	537	1.8	8	20	3374	6.31	23	5	ND	8	80	7	5	2	15	.42	.158	32	8	.23	557	.01	4	1.25	.03	.14	1	45
22W 15+50N	4	42	403	446	.7	6	19	3479	5.52	18	5	ND	9	59	10	4	2	12	.41	.161	34	5	.14	418	.01	5	.97	.01	.13	1	25
22W 15+25N	75	88	645	1376	4.6	11	30	7549	8.80	54	8	ND	6	86	18	14	2	18	.27	.179	39	10	.16	876	.01	3	1.26	.01	.08	1	90
22W 15+00N	3	57	99	243	.8	10	20	2739	4.42	16	5	ND	5	50	3	2	2	18	.42	.160	25	8	.22	325	.01	4	1.19	.01	.09	1	15
22W 14+75N	1	27	92	142	.1	8	13	2277	3.56	11	5	ND	3	26	2	2	2	18	.14	.176	15	7	.19	218	.01	2	1.63	.01	.06	1	2
22W 14+50N	1	36	75	141	.1	9	16	2387	3.95	16	5	ND	3	36	1	2	2	20	.19	.199	15	10	.31	253	.01	2	2.30	.01	.07	1	1
22W 14+25N	1	39	100	123	.3	17	23	1602	3.71	16	5	ND	2	10	1	3	2	19	.04	.217	13	10	.20	111	.01	2	1.99	.01	.06	1	1
22W 14+00N	1	23	63	131	.2	16	10	767	3.43	22	5	ND	1	23	1	2	2	34	.14	.121	12	15	.30	169	.01	2	1.92	.01	.05	2	1
22W 13+75N	1	20	28	96	.4	13	6	398	2.75	19	5	ND	1	13	1	2	2	31	.06	.137	10	14	.22	114	.01	2	1.98	.01	.05	1	1
22W 13+50N	1	28	56	138	.6	17	13	1021	3.14	20	5	ND	2	21	2	2	2	26	.09	.112	19	14	.30	227	.01	3	2.37	.01	.08	1	1
22W 13+25N	1	21	19	74	.1	11	5	332	2.33	17	5	ND	1	12	1	2	2	18	.03	.125	12	10	.15	165	.01	3	2.20	.01	.06	1	1
22W 13+00N	1	26	33	105	.1	17	12	1193	3.14	17	5	ND	3	14	1	2	2	27	.10	.116	18	17	.36	108	.01	2	1.90	.01	.07	1	2
22W 12+75N	1	25	42	106	.3	16	9	1010	3.29	19	5	ND	2	18	1	2	2	29	.10	.143	11	17	.33	128	.01	4	2.21	.01	.07	1	1
22W 12+50N	1	27	37	108	.3	18	11	1047	3.79	32	5	ND	2	17	1	2	2	37	.10	.131	13	19	.35	181	.01	3	2.13	.01	.06	1	1
22W 12+25N	1	22	24	80	.1	13	7	801	3.27	20	5	ND	1	17	1	2	2	38	.12	.158	10	16	.28	163	.01	3	2.28	.01	.05	1	1
22W 12+00N	1	44	48	146	1.0	19	13	1157	4.60	23	5	ND	4	34	2	2	2	20	.25	.153	26	11	.26	134	.01	2	1.67	.01	.08	1	1
22W 12+00N A	1	29	9	82	.1	15	9	802	2.80	10	5	ND	2	20	1	2	2	18	.14	.158	14	10	.24	131	.01	5	1.55	.01	.08	1	1
22W 11+75N	1	30	40	116	.1	20	13	946	3.99	27	5	ND	2	21	1	2	2	32	.18	.124	14	14	.29	121	.01	2	1.49	.01	.06	1	2
22W 11+75N A	1	25	33	86	.1	13	10	1248	3.25	16	5	ND	1	18	1	2	2	34	.11	.177	13	13	.27	164	.01	3	2.27	.01	.06	1	1
22W 11+50N	1	23	28	87	.1	15	8	736	3.53	17	5	ND	2	17	1	2	2	39	.12	.122	12	16	.31	109	.01	2	1.80	.01	.05	1	1
22W 11+25N	1	17	23	61	.9	8	4	339	2.17	14	5	ND	1	38	1	2	2	33	.19	.126	15	13	.17	168	.01	5	2.22	.01	.05	1	2
22W 11+00N	1	30	92	161	.2	14	10	704	3.13	14	5	ND	2	20	3	2	2	21	.13	.125	11	9	.26	121	.01	3	1.59	.01	.07	1	1
22W 10+75N	1	21	35	94	.1	12	6	273	2.55	15	5	ND	1	8	1	2	2	24	.03	.086	11	12	.24	81	.01	2	1.93	.01	.04	1	6
22W 10+50N	1	19	15	75	.1	10	5	375	2.59	15	5	ND	1	9	1	2	2	30	.03	.139	10	12	.20	82	.01	2	1.95	.01	.05	1	2
22W 10+25N	1	15	20	74	.1	6	4	539	2.18	14	5	ND	1	11	1	2	2	29	.03	.089	9	11	.09	179	.01	2	1.32	.01	.05	1	1
22W 10+00N	1	26	35	137	.1	14	9	1729	3.49	17	5	ND	1	16	1	2	3	33	.10	.171	8	15	.22	152	.01	2	1.45	.01	.08	1	1
STD C/AU-S	19	58	37	131	7.3	67	27	1012	3.78	40	18	7	38	48	16	17	21	57	.48	.085	36	57	.87	172	.08	35	1.79	.06	.15	13	48

SOUTHERN GOLD PROJECT-121104 FILE # 87-3784

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
22W 9+75N	1	56	54	146	.1	32	18	2288	5.59	17	5	ND	3	23	1	2	2	39	.16	.162	15	17	.36	182	.01	2	1.84	.01	.08	1	1
22W 9+50N	1	67	38	120	.1	30	13	1184	5.48	17	5	ND	3	22	2	3	2	38	.12	.191	16	22	.48	131	.01	2	2.31	.01	.06	1	1
22W 9+25N	1	37	20	97	.1	26	9	604	4.10	21	5	ND	1	13	1	2	2	35	.07	.147	10	16	.21	108	.01	2	1.53	.01	.06	1	1
22W 9+00N	1	48	34	118	.1	32	18	1717	4.85	17	5	ND	3	15	1	2	2	35	.14	.260	19	17	.55	171	.01	6	2.60	.01	.07	1	1
20W 17+00N	6	50	290	484	.6	17	21	1926	5.48	40	5	ND	7	83	5	9	2	15	.56	.248	37	7	.22	245	.01	2	.99	.03	.11	1	53
20W 16+75N	5	60	353	407	1.5	8	22	2728	7.44	36	6	ND	7	79	5	8	2	15	.29	.203	37	2	.12	295	.01	6	.87	.03	.12	1	59
20W 16+50N	5	59	289	407	1.3	7	21	2937	6.68	25	5	ND	9	75	4	4	2	15	.47	.218	36	4	.12	405	.01	8	1.02	.03	.16	1	40
20W 16+25N	4	59	479	576	.9	8	23	3606	7.01	24	5	ND	9	76	6	2	2	16	.52	.213	39	4	.15	534	.01	2	.96	.02	.14	1	35
20W 16+00N	5	65	274	309	.5	23	23	1740	6.11	31	5	ND	9	57	4	4	2	19	.56	.181	41	10	.28	252	.01	3	.99	.01	.14	1	20
20W 15+75N	9	55	286	322	.3	17	24	2724	6.08	31	5	ND	10	61	4	5	2	15	.58	.184	40	6	.24	277	.01	2	.88	.01	.11	1	13
20W 15+50N	5	45	304	321	.3	19	19	1555	4.12	22	5	ND	9	61	4	3	2	11	.49	.160	34	5	.14	178	.01	16	.65	.01	.11	1	9
20W 15+25N	5	88	305	383	1.0	29	30	2866	6.93	26	7	ND	7	59	3	3	2	26	.46	.150	38	11	.30	260	.01	2	1.05	.01	.11	1	13
20W 15+00N	4	105	215	315	1.0	24	29	2492	6.19	20	5	ND	6	52	1	2	2	26	.45	.135	35	12	.37	300	.01	3	1.10	.01	.09	1	2
20W 14+75N	4	76	555	587	3.2	40	41	2212	6.33	50	5	ND	7	57	4	8	2	24	.38	.124	27	10	.25	304	.01	3	1.03	.01	.09	1	3
20W 14+50N	4	67	637	648	3.5	33	35	2546	5.53	55	5	ND	6	56	8	8	2	20	.39	.141	31	8	.21	305	.01	5	.97	.01	.10	1	14
20W 14+25N	7	93	179	307	1.6	34	30	1575	8.54	32	8	ND	5	59	2	2	2	39	.39	.151	37	16	.37	302	.01	2	1.55	.01	.11	1	12
20W 14+00N	2	98	559	663	2.6	38	42	5186	9.50	55	5	ND	7	64	8	2	4	28	.31	.139	30	12	.33	517	.01	2	1.65	.01	.11	1	5
20W 13+75N	3	60	371	547	1.9	25	16	1009	6.50	35	5	ND	4	51	1	4	2	28	.41	.166	31	12	.32	242	.01	2	1.55	.01	.09	1	29
20W 12+25N	1	41	62	133	.1	21	15	1116	5.28	26	5	ND	3	24	1	2	2	36	.20	.164	20	16	.30	165	.01	2	1.91	.01	.07	1	1
20W 11+50N	1	35	48	116	.2	18	13	1313	4.37	20	5	ND	1	43	1	2	2	34	.24	.204	10	14	.28	188	.01	2	1.65	.01	.08	1	2
20W 11+25N	1	34	26	113	.1	22	11	877	4.95	21	5	ND	1	21	1	2	2	54	.15	.120	13	20	.43	161	.02	4	2.10	.01	.06	1	1
20W 11+00N	1	34	54	136	.1	20	11	1047	4.56	19	5	ND	1	19	1	2	2	46	.14	.175	15	19	.41	157	.02	2	2.32	.01	.07	1	1
20W 10+75N	1	28	167	240	.2	13	10	1390	3.39	24	5	ND	1	12	1	2	2	37	.08	.123	11	17	.28	76	.02	5	1.74	.01	.06	1	1
20W 10+50N	1	44	429	502	.8	20	15	1684	5.19	83	5	ND	4	27	4	3	3	40	.16	.130	16	16	.38	228	.02	2	2.25	.01	.07	1	10
20W 10+25N	1	35	54	142	.2	20	14	1358	5.18	27	5	ND	3	23	1	2	2	43	.13	.128	17	16	.39	138	.02	4	1.97	.01	.06	1	1
20W 10+00N	1	35	70	132	.1	18	12	1332	4.24	28	5	ND	2	18	1	2	2	41	.10	.177	14	18	.34	112	.02	5	2.56	.01	.06	1	1
20W 9+75N	1	40	76	156	.2	23	17	1552	5.73	14	5	ND	4	99	1	2	2	31	.48	.081	21	16	.77	305	.01	2	3.17	.01	.05	1	1
20W 9+50N	1	40	35	133	.3	15	10	943	4.67	20	5	ND	4	45	1	2	2	24	.24	.191	18	9	.30	174	.01	3	1.87	.01	.05	1	1
20W 9+25N	2	42	36	119	.1	24	11	806	5.20	48	5	ND	3	14	1	2	3	30	.04	.198	17	15	.30	153	.01	3	2.38	.01	.06	1	1
20W 9+00N	1	30	26	110	.1	16	9	381	4.64	25	5	ND	1	16	1	2	2	39	.07	.155	13	15	.26	141	.01	2	2.32	.01	.05	1	1
STD C/AU-S	18	60	39	127	7.1	68	28	1026	4.05	41	21	7	39	50	20	18	22	59	.47	.089	38	61	.85	176	.08	36	1.74	.06	.13	12	51

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
3W 8+25N	1	35	51	171	1.1	28	10	606	4.70	55	5	ND	3	13	2	2	3	48	.10	.117	10	26	.33	96	.01	4	1.94	.01	.08	2	6
3W 8+00N	1	38	27	160	1.8	34	11	665	4.59	56	5	ND	4	13	2	2	2	45	.09	.088	10	20	.24	102	.01	4	1.58	.01	.07	1	2
3W 7+75N	1	27	27	111	.6	18	8	555	4.84	39	5	ND	2	14	1	2	2	63	.10	.146	8	28	.34	118	.03	4	2.32	.01	.07	1	1
3W 7+50N	1	34	39	155	1.1	28	13	726	4.26	39	5	ND	3	20	1	2	2	42	.18	.124	13	23	.30	121	.03	4	1.98	.01	.07	1	3
3W 7+25N	1	32	58	146	1.1	23	9	366	4.02	49	5	ND	3	15	2	2	3	38	.12	.112	11	19	.24	83	.01	4	1.39	.01	.06	1	7
3W 7+00N	9	81	754	1009	29.7	42	22	4592	6.93	316	6	ND	5	24	15	13	3	15	.19	.120	21	6	.08	147	.01	3	.46	.01	.07	3	139
3W 6+75N	1	44	662	423	12.0	46	18	2275	5.03	181	5	ND	4	21	6	6	2	20	.16	.092	16	11	.11	101	.01	9	.58	.01	.07	2	52
3W 6+50N	1	26	33	131	.2	18	9	607	4.11	34	5	ND	2	13	1	2	2	48	.09	.103	8	21	.30	117	.03	6	2.20	.01	.06	1	1
3W 6+25N	1	36	166	262	1.7	26	11	746	3.42	106	5	ND	2	22	2	2	2	25	.22	.092	14	13	.20	100	.01	2	.82	.01	.06	1	18
3W 6+00N	1	32	2008	1260	7.0	12	5	2050	2.53	638	5	ND	1	9	10	8	2	10	.08	.036	7	7	.09	79	.01	2	.50	.01	.07	5	77
3W 5+75N	1	46	21	156	.1	50	18	1278	4.94	37	5	ND	2	32	1	2	2	47	.46	.080	10	29	.52	131	.04	4	1.31	.03	.08	1	1
3W 5+50N	1	43	33	151	.1	51	15	664	4.12	36	5	ND	2	22	1	2	2	31	.29	.079	10	24	.40	60	.02	2	1.03	.02	.06	1	1
3W 5+25N	5	74	34	228	.5	125	34	1037	6.29	96	5	ND	4	46	1	4	2	14	.48	.057	14	18	.29	67	.01	7	.50	.01	.06	1	1
3W 5+00N	1	49	45	188	.1	50	17	1299	4.42	34	5	ND	4	36	1	2	2	36	.38	.090	13	30	.44	145	.01	2	1.39	.01	.08	1	1
3W 4+75N	1	44	40	184	.2	47	13	702	4.24	44	5	ND	4	16	1	2	2	34	.14	.071	13	24	.35	102	.01	2	1.31	.01	.06	2	1
3W 4+50N	1	48	56	212	.5	51	15	990	4.45	49	5	ND	4	18	2	2	2	31	.16	.063	14	24	.32	154	.01	4	1.30	.01	.07	1	2
3W 4+25N	1	65	26	173	.3	98	22	1012	4.67	41	5	ND	2	24	2	2	2	30	.27	.066	5	34	.46	91	.01	4	1.24	.01	.06	1	1
3W 4+00N	1	56	43	213	.8	82	21	1197	4.69	61	5	ND	2	28	2	4	2	23	.30	.101	10	21	.30	86	.01	3	.91	.02	.10	1	2
3W 3+75N	1	44	31	180	.3	61	16	927	4.56	36	5	ND	2	14	1	2	2	37	.14	.078	9	34	.40	125	.01	2	1.51	.01	.06	1	1
3W 3+50N	1	45	42	198	1.3	30	9	342	4.57	30	5	ND	2	10	1	3	2	48	.06	.084	8	27	.35	92	.01	4	1.98	.01	.06	1	1
3W 3+25N	1	49	70	273	1.0	50	12	623	4.60	54	5	ND	3	29	1	13	2	31	.29	.074	12	27	.38	154	.01	4	1.60	.01	.08	2	2
3W 3+00N	1	39	26	145	.1	35	13	764	4.32	31	5	ND	2	29	1	2	2	44	.38	.080	12	31	.47	136	.03	4	1.53	.02	.10	1	1
3W 2+75N	1	34	54	176	.4	44	17	1365	4.30	39	5	ND	2	17	1	3	2	32	.13	.104	10	23	.29	114	.01	5	1.37	.01	.07	2	1
3W 2+50N	1	34	26	127	.3	30	12	694	3.99	29	5	ND	1	19	1	2	2	43	.24	.096	10	28	.42	193	.03	5	1.49	.02	.07	1	1
3W 2+25N	1	36	20	125	.3	20	9	406	5.30	29	5	ND	2	12	1	2	2	59	.13	.112	7	31	.40	92	.05	9	2.15	.01	.05	1	1
3W 2+00N	1	29	22	106	.6	22	9	329	3.86	26	5	ND	2	21	1	2	2	48	.27	.069	10	29	.42	77	.06	4	1.39	.02	.06	1	1
3W 1+75N	3	54	61	207	.6	57	18	807	4.76	68	5	ND	3	15	2	3	2	26	.12	.105	15	18	.21	66	.01	4	.90	.01	.06	1	4
3W 1+50N	1	60	29	169	.3	66	21	1132	3.84	60	5	ND	2	33	1	7	2	19	.15	.055	10	17	.23	166	.01	5	.93	.01	.06	1	2
2W 13+00N	1	20	15	100	.4	12	5	207	2.78	18	5	ND	1	15	1	2	2	46	.09	.054	7	20	.31	135	.01	3	2.21	.01	.06	1	1
2W 12+75N	1	18	16	106	.6	14	5	294	2.45	21	5	ND	1	19	1	2	2	41	.13	.065	8	21	.35	152	.01	5	1.89	.01	.07	2	1
2W 12+50N	1	20	22	97	.7	15	6	281	3.05	25	5	ND	1	13	1	2	2	45	.06	.045	8	22	.35	104	.02	6	1.95	.01	.05	1	1
2W 12+25N	1	30	19	129	.5	20	7	402	3.51	20	5	ND	1	14	1	2	3	54	.06	.060	8	26	.42	137	.01	5	2.79	.01	.08	1	1
2W 12+00N	1	24	13	108	.3	14	7	1279	3.43	19	5	ND	1	14	1	2	2	57	.06	.091	7	24	.35	128	.01	3	2.10	.01	.08	1	8
2W 11+75N	1	16	25	59	.2	9	9	3048	2.11	14	5	ND	1	12	3	2	2	45	.03	.061	7	17	.18	121	.01	5	1.65	.01	.08	1	1
2W 11+50N	1	32	16	131	.7	28	9	326	4.30	23	5	ND	3	24	1	2	2	58	.19	.064	9	33	.49	202	.02	6	2.68	.01	.11	1	1
2W 11+25N	1	27	10	114	.5	22	8	397	3.41	18	5	ND	1	23	1	2	2	52	.15	.082	8	28	.39	195	.01	5	2.65	.01	.10	1	1
STD C/AU-S	18	61	38	132	6.9	68	28	1042	3.84	43	22	7	40	50	17	18	21	59	.44	.090	38	65	.80	177	.08	31	1.67	.06	.13	12	52

SOUTHERN GOLD PROJECT-121104 FILE # 87-3784

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
2W 11+00N	1	20	16	117	.7	14	9	1539	3.49	21	5	ND	2	24	1	2	2	52	.20	.112	6	18	.32	232	.01	5	1.74	.01	.07	2	10
2W 10+75N	1	19	20	102	.1	15	6	614	3.86	23	5	ND	1	11	1	2	2	55	.07	.076	6	20	.38	182	.02	4	1.74	.01	.06	1	1
2W 10+50N	1	23	23	84	1.7	13	8	990	2.60	13	5	ND	1	16	1	2	2	38	.11	.098	8	16	.28	130	.01	5	2.04	.01	.05	1	1
2W 10+25N	1	30	13	105	.2	16	8	372	4.48	21	5	ND	1	15	1	2	2	59	.11	.064	6	21	.34	152	.01	5	1.80	.01	.05	1	1
2W 10+00N	1	29	12	115	.1	20	10	684	4.10	15	5	ND	1	20	2	2	2	50	.18	.080	7	21	.39	148	.01	6	1.77	.01	.06	1	1
2W 9+75N	1	33	22	122	.1	22	14	1138	4.31	24	5	ND	1	22	1	2	2	51	.23	.084	10	25	.42	147	.02	4	1.44	.01	.07	1	1
2W 9+50N	1	20	32	213	1.6	19	7	561	2.84	29	5	ND	1	49	1	2	2	36	.29	.151	14	19	.28	202	.01	2	2.38	.01	.05	1	1
2W 9+25N	1	23	22	154	1.1	12	6	364	2.90	30	5	ND	1	133	1	2	2	35	.51	.081	10	14	.25	180	.01	3	1.38	.01	.06	1	1
2W 9+00N	1	30	31	148	2.5	19	8	532	3.48	33	5	ND	1	113	1	2	2	38	.43	.089	12	20	.32	182	.01	5	1.80	.01	.05	1	2
2W 8+75N	1	24	29	81	.2	12	6	274	5.02	25	5	ND	1	15	1	2	2	58	.09	.126	6	19	.24	134	.02	5	1.46	.01	.04	1	1
2W 8+50N	1	30	15	106	1.1	14	8	989	4.70	19	5	ND	1	14	1	2	2	58	.15	.167	6	20	.26	99	.01	2	1.57	.01	.08	1	1
2W 8+25N	1	19	36	69	.2	9	5	249	4.03	22	5	ND	1	8	1	2	2	57	.03	.097	8	14	.16	82	.02	4	1.44	.01	.05	1	1
2W 8+00N	1	28	20	120	.8	18	8	406	6.61	28	5	ND	2	10	1	4	2	63	.06	.158	7	25	.42	96	.02	4	2.62	.01	.08	1	1
2W 7+75N	1	38	26	122	.2	28	14	1151	4.81	23	5	ND	2	20	1	2	2	48	.25	.077	11	22	.39	101	.04	4	1.32	.01	.06	1	1
2W 7+50N	1	23	24	117	1.2	13	6	545	4.53	24	5	ND	1	8	1	2	2	56	.04	.102	8	22	.29	81	.01	3	2.22	.01	.05	1	1
2W 7+25N	1	30	31	109	.7	18	8	1038	4.38	29	5	ND	1	10	1	4	2	52	.06	.111	7	17	.21	90	.01	7	1.55	.01	.06	1	1
2W 7+00N	1	16	55	82	1.1	7	4	236	5.01	48	5	ND	1	8	1	3	2	70	.02	.103	10	15	.18	73	.03	2	1.83	.01	.03	1	2
2W 6+75N	1	37	26	160	2.3	35	14	549	5.94	33	5	ND	2	8	1	2	2	52	.03	.098	7	29	.37	92	.02	2	3.74	.01	.05	1	1
2W 6+50N	1	32	29	160	.9	32	10	648	5.80	37	5	ND	2	14	1	2	2	46	.13	.138	7	21	.29	94	.02	4	2.98	.01	.07	1	1
2W 6+25N	1	38	44	165	1.0	49	16	769	4.71	50	5	ND	3	10	1	3	2	32	.05	.086	11	12	.21	63	.01	2	1.27	.01	.05	1	1
2W 6+00N	1	74	27	205	1.6	117	25	1148	6.77	92	5	ND	3	14	1	13	2	15	.13	.055	7	6	.07	71	.01	3	.48	.01	.06	1	1
2W 5+75N	1	41	64	170	3.0	42	17	712	4.80	46	5	ND	3	18	1	2	2	29	.20	.075	11	15	.22	99	.01	2	1.06	.01	.04	1	6
2W 5+50N	1	64	72	262	1.1	90	33	1809	5.65	70	5	ND	1	23	1	6	2	29	.16	.082	7	15	.17	90	.01	2	1.09	.01	.05	1	1
2W 5+25N	2	54	53	360	2.5	69	27	2263	5.64	102	5	ND	3	19	1	8	2	16	.15	.101	20	8	.08	133	.01	3	.48	.01	.07	1	1
STD C/AU-S	18	60	40	132	7.3	70	30	1065	4.06	41	18	8	41	51	19	17	21	61	.48	.090	39	59	.85	169	.08	35	1.78	.06	.13	13	48
2W 5+00N	1	28	23	131	10.1	21	8	314	5.37	26	5	ND	3	9	1	2	2	49	.05	.128	7	23	.32	72	.02	4	3.61	.01	.05	1	1
2W 4+75N	1	32	17	162	1.3	29	12	518	5.07	29	5	ND	3	10	1	3	2	51	.06	.078	8	25	.41	124	.02	6	3.02	.01	.06	1	1
2W 4+50N	1	20	30	113	1.1	16	8	389	4.12	24	5	ND	3	10	1	2	2	51	.04	.097	7	20	.28	84	.02	7	2.56	.01	.05	1	1
2W 4+25N	1	33	19	123	.1	26	11	542	4.55	23	5	ND	2	14	1	2	2	52	.14	.074	9	23	.43	118	.02	4	2.25	.01	.07	1	2
2W 4+00N	1	28	26	119	.3	21	10	505	5.09	27	5	ND	2	15	1	2	2	50	.10	.111	9	23	.33	111	.02	6	2.42	.01	.05	1	1
2W 3+75N	1	20	14	127	.5	17	7	306	4.28	26	5	ND	1	30	1	2	2	51	.14	.075	8	19	.33	111	.02	2	2.31	.01	.05	1	1
2W 3+50N	1	29	23	140	.7	29	10	300	4.50	30	5	ND	2	13	1	2	2	41	.06	.097	8	21	.29	69	.01	4	2.39	.01	.04	1	1
2W 3+25N	1	29	39	176	1.1	24	11	490	5.23	30	5	ND	2	10	1	4	4	50	.05	.139	6	25	.34	107	.01	2	4.09	.01	.05	1	1
2W 3+00N	1	27	42	130	1.3	25	9	537	4.85	31	5	ND	2	13	1	2	4	49	.11	.139	7	26	.36	114	.01	3	2.08	.01	.05	1	1
2W 2+75N	1	27	42	123	.6	21	9	346	4.40	29	5	ND	2	10	1	2	2	46	.05	.080	8	19	.27	84	.01	3	1.91	.01	.06	1	1
2W 2+50N	1	26	24	143	.3	23	9	259	5.05	26	5	ND	3	13	1	2	2	52	.05	.075	7	24	.39	131	.02	5	3.10	.01	.06	1	1
2W 2+25N	1	39	37	167	1.0	33	13	564	5.21	30	5	ND	2	15	1	2	2	53	.10	.086	12	28	.43	131	.01	3	2.78	.01	.06	1	30

SOUTHERN GOLD PROJECT-121104 FILE # 87-3784

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU† PPB
2W 2+00N	1	44	26	139	.3	35	14	689	4.55	31	5	ND	5	22	1	2	2	45	.20	.073	11	23	.46	150	.02	6	1.97	.01	.05	1	3
2W 1+75N	1	31	56	134	1.5	20	9	285	4.62	40	5	ND	3	10	1	2	2	44	.06	.100	9	16	.22	93	.01	4	1.64	.01	.04	1	1
2W 1+50N	1	43	83	191	.7	40	14	443	3.97	47	5	ND	4	18	2	2	2	24	.21	.105	15	11	.22	69	.01	5	.83	.01	.04	1	8
2W 1+25N	1	41	110	212	.4	36	13	553	4.08	55	5	ND	3	12	1	2	2	31	.13	.068	13	14	.28	77	.01	3	1.16	.01	.04	2	12
2W 1+00N	1	33	71	204	.8	27	11	495	4.01	41	5	ND	2	17	2	3	2	40	.19	.082	10	21	.37	99	.01	6	1.52	.01	.05	1	2
2W 0+75N	1	43	81	175	1.3	33	13	778	4.65	40	5	ND	2	22	1	2	2	46	.27	.073	11	24	.50	127	.04	4	1.44	.01	.05	1	3
2W 0+50N	1	56	145	240	.6	66	20	1001	4.85	70	5	ND	2	15	1	2	2	32	.17	.079	8	23	.38	73	.01	5	1.26	.01	.04	2	6
2W 0+25N	1	50	293	349	3.4	50	18	952	4.75	81	5	ND	2	22	3	6	2	32	.21	.095	12	18	.33	98	.01	3	1.50	.01	.05	1	10
2W 0+00N	1	58	74	206	1.1	68	25	1460	5.19	62	5	ND	2	24	1	4	2	21	.23	.088	8	16	.29	92	.01	5	.92	.01	.04	1	3
1W 13+00N	1	9	19	24	.3	4	2	55	1.44	12	5	ND	1	8	1	2	2	31	.04	.044	5	9	.12	53	.01	6	1.39	.01	.02	1	2
1W 12+75N	1	12	14	19	.2	3	2	40	1.75	11	5	ND	1	7	1	2	2	41	.02	.026	6	7	.09	52	.01	4	1.18	.01	.02	1	2
1W 12+50N	1	37	21	123	.4	23	8	446	3.48	14	5	ND	1	13	1	2	2	44	.08	.072	11	22	.37	252	.01	2	3.61	.01	.07	1	1
1W 12+25N	1	23	30	125	.5	10	6	345	6.10	36	5	ND	2	9	1	2	2	81	.05	.159	6	19	.25	71	.02	5	2.38	.01	.03	2	17
1W 12+00N	1	31	14	125	.3	19	7	394	4.44	21	5	ND	1	22	1	2	2	48	.19	.110	12	22	.34	224	.01	3	3.30	.02	.07	1	2
1W 11+75N	1	18	12	75	.3	12	5	161	3.24	14	5	ND	1	20	1	2	2	50	.15	.060	7	14	.27	175	.01	4	1.88	.01	.04	1	1
1W 11+50N	1	22	17	59	.2	9	4	159	5.02	20	5	ND	1	7	1	2	2	66	.01	.066	6	15	.17	76	.01	6	1.92	.01	.03	1	1
1W 11+25N	1	25	23	97	.4	12	6	247	5.57	26	5	ND	1	16	1	2	2	53	.15	.104	6	17	.25	99	.02	3	2.50	.01	.04	1	1
1W 11+00N	1	28	13	127	.8	21	9	569	4.24	18	5	ND	1	19	1	2	2	54	.12	.100	7	22	.42	185	.01	2	2.94	.01	.07	1	1
1W 10+75N	1	27	13	142	.3	24	8	269	4.46	18	5	ND	2	17	1	2	2	58	.12	.054	6	23	.47	211	.01	5	2.88	.01	.07	1	5
1W 10+50N	1	13	7	54	.1	6	4	151	3.35	16	5	ND	1	11	1	2	2	55	.05	.044	6	11	.14	79	.02	4	1.38	.01	.03	1	1
1W 10+25N	1	19	18	92	.2	10	4	182	5.73	23	5	ND	1	10	1	2	2	79	.04	.084	6	17	.26	107	.03	2	1.91	.01	.04	1	1
1W 10+00N	1	19	20	66	.1	10	5	182	4.56	19	5	ND	1	8	1	2	2	69	.02	.086	7	15	.19	59	.02	4	1.67	.01	.03	1	1
1W 9+75N	1	24	22	140	.1	16	6	266	4.74	28	5	ND	1	15	1	2	3	55	.09	.097	7	17	.31	120	.02	7	2.26	.01	.05	1	1
1W 9+50N	1	20	17	101	.1	12	6	282	6.01	24	5	ND	1	15	1	2	2	70	.07	.095	6	17	.29	90	.04	3	1.94	.01	.03	1	1
1W 9+25N	1	18	17	75	.1	9	4	191	4.62	23	5	ND	1	9	1	2	2	64	.02	.055	6	15	.21	71	.02	2	2.00	.01	.03	1	1
1W 9+00N	1	18	17	79	.1	9	5	236	3.32	17	5	ND	1	12	1	2	2	49	.05	.059	7	12	.20	105	.01	3	1.81	.01	.04	1	8
1W 8+75N	1	18	19	65	.4	8	4	192	5.14	27	5	ND	1	6	1	2	2	75	.01	.068	6	14	.15	49	.04	2	1.46	.01	.02	1	2
1W 8+50N	1	27	25	98	.6	11	6	269	6.41	28	5	ND	2	8	1	3	2	59	.02	.087	6	20	.25	58	.03	6	2.32	.01	.03	1	2
1W 8+25N	1	23	22	84	.4	14	6	320	6.07	27	5	ND	1	7	1	2	2	63	.01	.108	5	20	.29	76	.03	2	1.79	.01	.04	1	1
1W 8+00N	1	19	22	85	.4	14	5	237	4.04	19	5	ND	1	9	3	2	2	50	.02	.070	6	18	.29	94	.01	5	1.87	.01	.05	1	2
1W 7+75N	1	30	37	132	.8	18	7	410	7.53	31	5	ND	1	9	2	2	2	56	.07	.142	6	23	.28	99	.02	2	2.66	.01	.04	1	2
1W 7+50N	1	28	32	112	.9	15	6	244	6.01	30	5	ND	1	9	1	2	2	59	.06	.225	5	22	.27	81	.02	3	1.70	.01	.05	1	1
1W 7+25N	1	32	34	127	.4	20	8	350	4.38	29	5	ND	2	20	1	2	2	52	.20	.081	8	18	.36	90	.03	2	1.51	.01	.04	1	3
1W 7+00N	1	27	44	141	.3	20	8	316	5.36	30	5	ND	3	10	1	2	3	57	.08	.137	7	25	.37	135	.01	2	2.59	.01	.04	1	1
1W 6+75N	1	33	54	147	1.0	22	10	318	4.90	35	5	ND	3	16	1	2	2	44	.15	.191	9	21	.33	84	.01	7	1.96	.01	.04	1	5
STD C/AU-S	19	62	37	131	7.2	71	29	1056	4.02	40	24	7	39	50	18	18	24	60	.45	.090	39	57	.85	170	.08	34	1.74	.06	.13	14	50
1W 6+50N	1	15	36	72	.1	10	4	268	1.88	24	5	ND	3	8	1	2	2	23	.02	.037	12	5	.04	86	.01	3	.80	.01	.03	1	-

SOUTHERN GOLD PROJECT-121104 FILE # 87-3784

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
1W 6+25N	1	42	76	207	.8	53	19	1366	4.49	38	5	ND	3	25	2	4	2	30	.20	.087	6	21	.34	197	.01	5	1.12	.01	.04	1	19
1W 6+00N	1	57	310	384	6.4	65	18	1011	4.60	61	5	ND	3	25	4	5	2	19	.21	.073	7	13	.23	136	.01	2	.82	.01	.05	1	17
1W 5+75N	1	64	56	258	.2	91	39	3212	6.33	48	5	ND	4	21	2	4	2	23	.12	.078	5	24	.50	120	.01	2	1.25	.01	.05	1	3
1W 5+50N	1	53	55	221	.8	58	22	963	5.70	65	5	ND	3	17	2	6	2	26	.10	.059	6	20	.34	93	.01	2	1.24	.01	.04	1	5
1W 5+25N	1	36	39	152	1.2	46	13	605	4.93	37	5	ND	3	30	1	2	2	41	.16	.120	8	19	.33	128	.01	2	2.15	.01	.05	1	15
1W 5+00N	1	35	30	156	1.4	34	14	449	4.45	28	5	ND	3	11	1	2	3	44	.08	.095	7	23	.42	128	.02	6	2.68	.01	.05	1	1
1W 4+75N	2	50	31	180	.3	65	24	1578	4.70	34	5	ND	3	31	2	2	2	21	.26	.073	6	15	.33	99	.01	2	.89	.01	.04	1	2
1W 4+50N	1	60	39	255	.5	89	38	2885	5.98	44	5	ND	3	40	2	5	2	22	.26	.078	6	23	.46	146	.01	7	1.14	.01	.04	1	3
1W 4+25N	1	47	25	94	.7	21	16	652	4.75	43	5	ND	1	12	1	6	2	21	.15	.068	3	6	.11	94	.01	2	.75	.01	.04	1	1
1W 4+00N	1	44	32	193	.4	59	20	1018	5.58	55	5	ND	3	18	1	4	2	20	.17	.093	5	20	.38	109	.01	2	1.01	.01	.04	1	1
1W 3+75N	1	37	39	153	1.2	22	8	291	5.22	52	5	ND	3	17	1	6	2	31	.12	.166	7	12	.18	84	.01	2	1.26	.01	.05	1	3
1W 3+50N	1	22	47	108	1.0	15	6	203	4.41	38	5	ND	2	12	1	2	2	51	.12	.084	8	17	.26	85	.02	5	1.53	.01	.04	1	2
1W 3+25N	1	30	46	188	.6	30	9	317	5.62	35	5	ND	3	15	2	2	2	55	.13	.072	6	28	.47	132	.01	2	2.66	.01	.07	2	1
1W 3+00N	2	58	34	226	.6	69	23	1035	6.08	64	5	ND	4	11	1	8	2	27	.05	.067	12	20	.34	70	.01	2	1.13	.01	.04	1	3
1W 2+75N	1	52	31	207	.9	69	19	1317	5.56	51	5	ND	2	14	1	9	2	20	.11	.094	7	11	.18	73	.01	2	.70	.01	.05	1	2
1W 2+50N	5	51	56	274	2.9	61	14	789	4.99	71	5	ND	3	6	2	8	2	23	.01	.060	14	9	.12	60	.01	2	.78	.01	.04	2	2
1W 2+25N	1	39	740	376	3.9	34	10	533	4.78	49	5	ND	3	66	2	92	2	38	.40	.090	9	16	.33	149	.01	5	1.46	.01	.06	1	5
1W 2+00N	1	54	80	227	1.4	69	24	1401	5.12	56	5	ND	3	23	2	6	2	18	.18	.072	6	18	.36	78	.01	4	.84	.01	.05	1	2
1W 1+75N	1	55	79	249	.8	86	23	1371	4.65	72	5	ND	3	35	3	4	2	21	.35	.084	9	15	.38	90	.01	2	.75	.01	.05	1	1
1W 1+50N	1	41	44	149	.4	37	12	487	4.53	40	5	ND	3	16	1	3	2	41	.16	.076	11	23	.42	79	.02	3	1.29	.02	.05	1	1
1W 1+25N	1	44	31	147	.4	57	18	892	3.61	46	5	ND	2	17	1	2	2	21	.25	.075	7	12	.21	89	.01	2	.79	.01	.05	1	2
1W 1+00N	1	42	62	158	1.9	60	18	1451	3.44	57	5	ND	2	18	1	3	2	14	.22	.061	8	7	.11	96	.01	2	.55	.01	.05	1	210
1W 0+75N	1	30	82	182	1.1	25	9	492	4.57	40	5	ND	2	16	1	2	2	51	.09	.099	9	22	.34	120	.02	3	2.02	.01	.05	1	1
1W 0+50N	1	51	214	315	1.5	47	15	735	4.83	75	5	ND	3	15	3	2	2	33	.15	.077	11	19	.34	96	.01	2	1.24	.01	.04	1	1
1W 0+25N	1	49	60	204	.7	50	14	638	4.46	60	5	ND	3	17	2	2	2	25	.14	.098	12	16	.27	107	.01	2	.98	.01	.05	1	1
1W 0+00N	10	57	111	874	1.1	60	14	1843	6.80	145	5	ND	3	8	2	19	2	22	.01	.096	16	7	.06	53	.01	6	.73	.01	.03	2	3
00 13+00N	1	21	16	90	.2	13	5	207	4.14	20	5	ND	1	8	1	2	2	48	.03	.062	5	19	.32	84	.01	3	2.04	.01	.04	1	1
00 12+75N	1	13	15	39	.3	5	3	115	2.45	18	5	ND	1	8	1	2	2	59	.01	.035	6	11	.09	42	.02	4	1.08	.01	.03	3	1
00 12+50N	1	23	17	72	.1	13	6	423	4.00	17	5	ND	1	7	2	2	2	57	.01	.092	6	19	.27	51	.01	3	1.61	.01	.05	2	2
00 12+25N	1	17	7	41	.4	7	3	288	2.38	13	5	ND	1	8	1	2	2	44	.01	.075	7	13	.12	60	.01	7	1.16	.01	.06	1	1
00 12+00N	1	35	13	132	1.5	23	8	335	4.53	18	5	ND	1	14	1	2	2	53	.08	.097	7	28	.49	165	.01	2	3.30	.02	.08	1	1
00 11+75N	1	20	18	95	.3	15	6	342	2.92	12	5	ND	1	12	1	2	2	49	.08	.068	8	19	.44	107	.01	7	2.22	.01	.06	1	1
00 11+50N	1	24	7	113	1.4	20	5	271	2.67	11	5	ND	1	9	2	2	2	36	.04	.092	7	23	.38	144	.01	4	3.10	.01	.07	1	2
00 11+25N	1	26	20	129	.3	14	7	420	5.06	21	5	ND	1	7	1	2	2	51	.03	.108	6	21	.30	76	.02	2	2.20	.01	.03	1	1
00 11+00N	1	16	19	64	.1	9	4	184	5.33	18	5	ND	1	6	1	2	2	62	.01	.092	5	17	.21	56	.02	2	1.66	.01	.04	1	2
00 10+75N	1	15	16	75	.3	14	5	187	2.40	15	5	ND	1	10	1	2	2	39	.04	.046	7	18	.37	93	.01	2	1.86	.01	.05	1	1
STD C/AU-S	19	61	41	129	7.0	69	28	1032	3.94	38	20	7	38	51	17	18	22	59	.45	.092	38	58	.91	125	.08	35	1.79	.06	.13	13	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
00 10+50N	1	23	17	93	.7	12	6	229	5.24	24	5	ND	3	10	1	2	2	66	.06	.077	7	22	.29	97	.03	2	2.02	.01	.05	2	2
00 10+25N	1	17	14	77	.7	12	5	188	3.18	21	5	ND	1	13	1	2	2	61	.10	.057	6	18	.32	108	.02	3	1.82	.01	.05	1	1
00 10+00N	1	18	14	118	.9	14	7	622	2.68	16	5	ND	1	28	1	3	2	44	.25	.082	8	18	.34	228	.01	2	2.25	.01	.07	1	35
00 9+75N	1	25	18	123	.5	12	5	276	3.72	23	5	ND	1	18	1	3	2	53	.12	.082	8	17	.24	187	.01	2	2.49	.01	.06	1	1
00 9+50N	1	18	16	89	.2	10	5	217	3.04	14	5	ND	1	25	1	2	2	54	.19	.049	7	15	.23	207	.02	2	1.65	.01	.05	1	2
00 9+25N	1	25	20	85	.4	12	5	219	4.24	21	5	ND	1	14	1	2	3	61	.11	.063	6	19	.26	117	.02	2	1.77	.01	.05	3	1
00 9+00N	1	34	28	180	.3	19	9	4603	4.05	17	5	ND	2	40	1	5	2	53	.30	.138	13	24	.42	451	.01	2	3.16	.02	.10	1	2
00 8+75N	1	23	22	99	.9	11	6	447	4.74	26	5	ND	2	9	1	2	2	58	.05	.091	7	19	.22	92	.02	2	1.99	.01	.06	1	1
00 8+50N	1	27	17	122	.7	14	7	322	6.40	28	5	ND	1	15	1	2	3	77	.07	.113	6	23	.30	190	.03	2	2.18	.01	.06	1	2
00 8+25N	1	23	23	86	.8	25	9	300	4.50	26	5	ND	1	19	1	7	2	72	.11	.103	9	49	.54	138	.05	2	1.85	.02	.04	2	28
00 8+00N	1	23	25	113	.6	15	7	327	4.47	27	5	ND	1	10	1	2	2	48	.09	.097	6	22	.32	67	.03	2	2.50	.01	.04	2	2
00 7+75N	1	32	30	141	.5	17	9	1709	5.08	29	5	ND	2	8	1	2	2	64	.03	.092	5	25	.33	116	.01	2	2.82	.01	.11	1	1
00 7+50N	1	32	21	135	.1	19	10	557	4.94	29	5	ND	3	13	1	3	2	59	.10	.111	7	25	.41	114	.02	2	2.30	.01	.06	1	1
00 7+25N	1	38	38	160	.3	30	13	844	4.43	34	5	ND	3	26	1	3	2	46	.37	.101	12	24	.44	136	.03	2	1.44	.01	.08	1	2
00 7+00N	1	38	31	162	1.0	27	10	361	5.67	35	5	ND	3	20	1	2	3	53	.25	.167	8	31	.45	169	.02	2	2.30	.01	.05	1	6
00 6+75N	1	32	40	145	.3	26	13	753	4.66	33	5	ND	3	18	1	2	3	45	.22	.114	10	25	.38	133	.02	2	1.50	.01	.05	1	1
00 6+50N	1	25	42	109	.2	16	6	251	3.42	35	5	ND	1	10	1	2	2	40	.08	.130	9	15	.16	74	.01	2	1.12	.01	.05	1	2
00 6+25N	1	25	36	137	.7	20	11	1549	3.87	24	5	ND	1	44	1	2	2	41	.75	.107	12	21	.39	246	.01	2	1.77	.01	.07	1	1
00 6+00N	1	34	30	148	.6	24	11	604	4.41	29	5	ND	3	28	1	3	2	50	.34	.076	12	28	.44	194	.02	2	2.27	.01	.07	1	2
00 5+75N	1	28	38	168	.5	23	11	877	4.67	29	5	ND	3	20	1	2	2	53	.18	.064	11	26	.40	287	.01	2	2.44	.01	.06	1	1
00 5+50N	1	33	33	132	.6	22	10	616	4.54	34	5	ND	3	16	1	3	2	49	.15	.105	10	23	.31	238	.01	2	1.90	.01	.06	2	2
00 5+25N	1	39	52	188	1.3	29	10	360	6.61	47	5	ND	3	11	1	2	2	53	.08	.113	9	32	.41	131	.01	2	2.83	.01	.07	1	1
00 5+00N	1	32	31	158	.6	25	12	974	4.52	36	5	ND	2	58	1	2	2	53	.70	.074	11	34	.43	249	.01	2	2.40	.02	.09	1	2
00 4+75N	3	39	38	157	1.5	28	14	3958	7.04	86	5	ND	2	95	1	2	2	51	1.11	.076	12	37	.38	353	.01	2	2.50	.01	.09	1	4
00 4+50N	1	52	68	177	.3	38	14	852	4.80	47	5	ND	3	34	1	2	2	40	.42	.073	13	26	.46	129	.01	2	1.69	.01	.06	1	2
00 4+25N	1	32	40	174	.2	23	10	464	4.86	43	5	ND	2	14	1	2	2	50	.12	.086	9	23	.37	98	.01	2	1.81	.01	.06	2	1
00 4+00N	1	42	54	178	.3	34	11	660	4.60	46	5	ND	3	17	1	2	2	40	.19	.069	12	23	.41	118	.01	2	1.84	.01	.06	1	2
00 3+75N	1	31	47	161	.6	25	10	860	4.32	36	5	ND	2	20	1	3	2	47	.22	.107	9	27	.39	152	.01	2	1.94	.01	.07	2	1
00 3+50N	1	29	34	131	.9	20	8	446	4.36	31	5	ND	1	11	1	2	2	49	.09	.099	8	24	.32	105	.01	3	1.95	.01	.06	1	1
00 3+25N	1	33	39	171	.9	29	12	996	4.05	30	5	ND	3	58	1	2	2	41	.83	.081	10	28	.44	244	.01	2	1.98	.01	.08	1	1
00 3+00N	1	34	34	156	.3	27	11	611	4.69	30	5	ND	2	44	1	3	2	48	.53	.075	8	33	.48	174	.02	2	1.89	.01	.05	1	2
00 2+75N	1	30	35	135	.2	20	9	551	4.12	31	5	ND	1	25	1	2	2	47	.34	.078	7	23	.29	119	.01	2	1.56	.01	.06	1	1
00 2+50N	1	36	34	151	.6	29	12	1068	4.62	36	5	ND	3	38	1	3	2	45	.52	.086	11	27	.40	187	.01	2	1.77	.01	.07	1	2
00 2+25N	1	69	30	148	.5	48	22	1294	6.42	54	5	ND	3	42	1	2	3	45	.64	.127	14	22	.50	204	.01	2	1.44	.02	.06	1	1
00 2+00N	1	41	50	184	.8	29	13	1035	4.03	46	5	ND	2	67	1	4	2	33	1.04	.107	12	21	.34	202	.01	2	1.39	.02	.07	2	2
00 1+75N	1	40	51	168	.5	31	12	810	4.33	42	5	ND	2	47	1	2	2	39	.64	.091	12	23	.37	171	.01	2	1.44	.02	.06	1	5
STD C/AU-S	18	62	41	132	7.2	68	28	1052	3.96	40	19	8	38	50	18	18	21	59	.48	.091	38	61	.83	178	.07	39	1.71	.06	.15	12	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM
00 1+50N	1	42	41	156	.7	32	12	809	4.28	45	5	ND	4	20	1	2	2
00 1+25N	1	57	28	188	.5	55	20	1081	5.17	57	5	ND	4	17	1	2	2
00 1+00N	1	48	25	182	.6	57	14	440	5.12	73	5	ND	4	9	1	7	2
00 0+75N	1	60	41	209	.5	75	24	1450	5.17	66	5	ND	3	31	1	5	2
00 0+50N	1	51	32	195	.7	59	17	959	5.08	63	5	ND	3	16	1	6	2
00 0+25N	3	54	41	143	1.5	39	17	1043	5.31	51	5	ND	2	24	1	3	2
1E 11+25N	1	28	20	112	.6	15	6	215	3.74	19	5	ND	1	8	1	2	2
1E 11+00N	1	25	11	78	.1	11	4	191	4.30	18	5	ND	2	8	1	2	2
1E 10+75N	1	21	16	72	.2	11	5	308	5.89	21	5	ND	1	8	1	2	2
1E 10+50N	1	26	23	83	.2	14	6	261	6.62	28	5	ND	2	8	1	2	2
1E 10+25N	1	24	19	87	.2	14	6	264	5.37	23	5	ND	1	7	1	2	2
1E 10+00N	1	12	9	44	.3	6	3	153	2.64	15	5	ND	1	8	1	2	2
1E 9+75N	1	29	24	108	.2	17	7	372	5.54	27	5	ND	1	8	1	3	2
1E 9+50N	1	18	30	91	.1	10	5	225	4.53	21	5	ND	1	9	1	2	2
1E 9+25N	1	27	18	115	.4	19	9	591	4.67	25	5	ND	1	12	1	2	2
1E 9+00N	1	38	20	234	1.2	28	12	2340	4.96	16	5	ND	3	21	1	2	2
1E 8+75N	1	27	9	122	.1	21	7	337	4.06	20	5	ND	1	16	1	2	3
1E 8+50N	1	22	16	105	.6	15	5	238	3.33	20	5	ND	1	14	1	2	2
1E 8+25N	1	19	20	67	.2	7	4	147	3.76	27	5	ND	1	13	1	2	2
1E 8+00N	1	22	15	134	.1	24	7	492	3.79	21	5	ND	1	38	1	2	2
1E 7+75N	1	22	28	122	.1	14	7	313	4.77	26	5	ND	2	11	1	4	2
1E 7+50N	1	28	29	165	.1	21	11	385	4.92	30	5	ND	2	11	1	3	2
1E 7+25N	1	32	20	130	.1	21	10	307	4.92	31	5	ND	3	12	1	2	2
1E 7+00N	1	28	25	117	.5	19	8	467	4.32	25	5	ND	2	14	1	2	2
1E 6+75N	1	29	16	110	.1	19	9	431	4.95	24	5	ND	2	16	1	2	2
1E 6+50N	1	13	11	94	.1	12	6	385	2.49	7	5	ND	2	12	3	2	2
1E 6+25N	1	27	21	120	.1	20	9	710	4.03	22	5	ND	1	28	1	2	2
1E 6+00N	2	43	27	160	.1	33	13	476	6.22	29	5	ND	2	10	1	2	3
1E 5+75N	1	42	64	182	.2	28	11	311	4.49	41	5	ND	4	17	1	2	2
1E 5+50N	1	18	73	174	.1	15	7	376	3.26	35	5	ND	2	12	1	2	2
1E 5+25N	1	31	54	219	.3	36	12	448	5.13	46	5	ND	3	10	1	2	2
1E 5+00N	1	18	36	184	.5	22	8	443	4.16	35	5	ND	3	11	1	2	2
1E 4+75N	1	22	44	166	.7	19	7	226	4.27	41	5	ND	3	9	1	2	3
1E 4+50N	1	36	58	217	.5	37	12	531	4.63	54	5	ND	3	13	1	2	2
1E 4+25N	1	49	111	503	1.1	44	13	786	4.63	61	5	ND	3	38	5	9	2
1E 4+00N	1	37	99	236	.2	34	13	593	4.72	55	5	ND	2	20	1	6	3
STD C/AU-S	18	63	42	132	7.2	72	27	1055	4.00	41	18	8	41	52	19	16	22

SAMPLE#	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
00 1+50N	33	.12	.077	9	18	.22	149	.01	2	1.35	.01	.05	1	2
00 1+25N	27	.18	.070	12	19	.36	108	.01	2	1.03	.01	.05	1	1
00 1+00N	26	.05	.084	9	9	.06	68	.01	2	.75	.01	.05	1	4
00 0+75N	23	.20	.067	12	18	.24	170	.01	2	.99	.01	.04	1	2
00 0+50N	25	.10	.072	10	18	.23	120	.01	2	.95	.01	.04	2	1
00 0+25N	25	.27	.117	11	14	.19	132	.01	2	.91	.01	.05	1	1
1E 11+25N	48	.07	.076	8	21	.28	77	.01	2	3.01	.01	.03	1	1
1E 11+00N	47	.05	.078	5	22	.20	60	.02	2	3.15	.01	.02	1	1
1E 10+75N	62	.02	.109	5	23	.23	49	.03	2	1.87	.01	.03	1	1
1E 10+50N	71	.04	.127	5	25	.28	50	.02	3	1.84	.01	.04	2	1
1E 10+25N	58	.04	.120	6	25	.30	60	.02	2	2.21	.01	.05	1	1
1E 10+00N	50	.02	.055	6	12	.14	56	.02	2	1.24	.01	.03	2	82
1E 9+75N	62	.03	.105	6	25	.31	76	.02	2	2.00	.01	.04	1	4
1E 9+50N	64	.03	.088	6	17	.21	93	.02	2	2.17	.01	.04	1	8
1E 9+25N	50	.11	.116	7	26	.39	110	.02	2	1.86	.01	.06	1	1
1E 9+00N	56	.12	.110	9	32	.47	323	.01	2	4.03	.02	.13	1	1
1E 8+75N	56	.07	.088	6	27	.41	161	.01	2	2.36	.01	.08	1	2
1E 8+50N	48	.08	.084	7	21	.30	115	.01	2	2.34	.01	.07	1	1
1E 8+25N	70	.06	.085	6	16	.15	121	.02	2	1.55	.01	.03	2	1
1E 8+00N	57	.32	.097	8	29	.47	253	.02	4	1.82	.02	.09	1	1
1E 7+75N	51	.09	.128	6	23	.29	91	.02	5	2.67	.01	.04	1	1
1E 7+50N	57	.07	.102	7	25	.38	123	.04	2	2.47	.01	.04	2	1
1E 7+25N	57	.08	.079	7	25	.37	129	.03	2	2.52	.01	.05	1	1
1E 7+00N	53	.15	.088	8	26	.37	114	.03	4	1.70	.01	.05	1	1
1E 6+75N	57	.17	.135	7	28	.39	128	.03	2	1.84	.01	.06	1	1
1E 6+50N	33	.12	.039	5	15	.26	99	.01	2	1.17	.01	.04	1	1
1E 6+25N	52	.41	.083	8	26	.38	155	.02	2	1.89	.01	.06	1	1
1E 6+00N	63	.08	.069	7	40	.55	144	.01	3	3.09	.01	.07	1	1
1E 5+75N	41	.17	.092	14	22	.32	90	.02	2	1.36	.01	.06	1	2
1E 5+50N	35	.07	.077	11	14	.16	134	.01	2	1.20	.01	.05	1	1
1E 5+25N	39	.06	.067	9	24	.43	107	.01	2	2.44	.01	.06	1	1
1E 5+00N	46	.09	.092	11	22	.27	92	.01	2	1.74	.01	.06	1	1
1E 4+75N	44	.03	.090	11	17	.23	80	.01	2	1.54	.01	.07	1	1
1E 4+50N	35	.14	.071	12	21	.39	65	.01	2	1.55	.01	.07	1	1
1E 4+25N	27	.81	.094	12	21	.39	80	.01	4	1.27	.01	.06	1	1
1E 4+00N	36	.21	.072	11	22	.37	66	.01	5	1.54	.01	.05	1	1
STD C/AU-S	58	.46	.091	40	62	.84	179	.07	39	1.88	.06	.14	13	50

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU! PPB
1E 3+75N	1	28	55	194	.5	23	8	351	4.24	50	5	ND	4	12	1	3	2	36	.12	.044	10	17	.30	100	.01	2	1.69	.01	.05	2	1
1E 3+50N	1	35	84	236	.7	30	12	1014	4.80	67	7	ND	2	22	1	9	2	33	.36	.080	13	19	.39	97	.01	7	1.85	.01	.06	2	1
1E 3+25N	1	36	86	227	.8	31	11	706	4.43	61	5	ND	3	20	2	8	2	31	.25	.093	11	19	.33	85	.01	2	1.49	.01	.05	2	1
1E 3+00N	1	32	42	133	.2	19	7	486	4.02	43	5	ND	1	11	1	4	2	39	.14	.125	8	21	.22	68	.01	2	1.30	.01	.04	1	1
1E 2+75N	1	16	26	86	.4	8	4	228	2.90	23	5	ND	1	11	1	2	2	41	.14	.074	10	11	.10	71	.01	2	1.19	.01	.04	1	1
2E 11+25N	1	14	23	52	.4	7	3	161	2.84	18	5	ND	1	8	1	2	2	53	.04	.142	7	22	.21	56	.01	3	2.09	.01	.04	2	1
2E 11+00N	1	19	16	61	1.2	8	4	272	3.64	20	5	ND	1	9	1	3	2	57	.03	.095	7	17	.17	68	.01	2	2.10	.01	.03	3	2
2E 10+75N	1	24	25	85	.4	14	6	295	6.09	29	6	ND	1	10	1	4	2	70	.04	.101	6	25	.30	65	.02	3	2.39	.01	.04	1	2
2E 10+50N	1	13	16	41	.3	5	3	156	2.26	22	5	ND	1	11	1	2	2	38	.06	.069	7	10	.11	56	.01	4	1.33	.01	.04	1	3
2E 10+25N	1	23	51	83	.6	12	6	264	5.78	45	6	ND	1	8	1	4	2	68	.04	.117	5	22	.30	55	.02	3	2.31	.01	.04	1	1
2E 10+00N	1	21	26	71	.1	11	5	449	4.87	28	6	ND	1	8	1	2	2	65	.04	.124	7	19	.22	51	.02	3	1.95	.01	.05	1	1
2E 9+75N	2	23	37	126	.2	28	8	400	8.31	38	5	ND	1	14	1	6	2	118	.06	.112	6	62	.54	351	.05	2	2.54	.01	.06	1	1
2E 9+50N	1	28	29	176	1.6	21	9	572	3.98	25	7	ND	1	88	1	2	2	50	.70	.059	10	31	.45	363	.01	2	2.18	.02	.07	1	1
2E 9+25N	1	24	11	131	.3	20	8	538	4.05	21	5	ND	1	53	1	2	2	48	.48	.072	10	26	.54	289	.02	2	2.04	.01	.07	1	2
2E 9+00N	1	20	16	114	.2	17	7	464	3.68	20	5	ND	1	45	1	2	2	44	.42	.071	9	24	.48	209	.02	2	1.89	.01	.08	1	1
2E 8+75N	1	19	15	103	.2	15	7	360	4.05	24	5	ND	1	23	1	2	2	54	.21	.086	7	23	.41	205	.02	3	2.02	.01	.06	1	1
2E 8+50N	1	26	21	96	.6	14	7	617	3.30	18	5	ND	1	16	1	3	2	48	.08	.106	11	23	.29	166	.01	4	3.20	.02	.09	2	1
2E 8+25N	1	12	12	78	.2	9	5	398	2.17	13	5	ND	1	20	1	2	3	37	.16	.047	9	16	.26	152	.01	3	1.90	.01	.05	1	2
2E 8+00N	1	26	18	133	1.0	24	9	520	4.13	18	5	ND	1	19	1	3	2	50	.14	.107	10	33	.48	195	.01	4	3.94	.02	.09	2	1
2E 7+75N	1	32	21	125	.7	24	11	535	5.20	27	5	ND	1	12	1	2	2	56	.10	.078	10	29	.51	116	.03	5	2.79	.01	.07	1	2
2E 7+50N	1	35	17	114	.4	26	12	600	4.68	25	5	ND	2	21	1	2	2	51	.23	.071	14	31	.50	162	.02	3	2.53	.02	.07	1	1
2E 7+25N	1	21	26	130	.4	14	7	291	6.23	27	5	ND	2	9	1	2	2	60	.04	.102	7	27	.28	101	.03	3	3.84	.01	.05	1	1
2E 7+00N	1	38	29	181	.9	28	12	308	5.85	28	5	ND	2	9	1	4	2	56	.05	.139	6	31	.40	135	.02	2	4.71	.01	.06	2	1
2E 6+75N	1	42	16	127	.1	25	12	648	4.89	26	5	ND	2	14	1	5	2	51	.12	.059	13	29	.45	135	.03	2	1.89	.01	.07	3	1
2E 6+50N	1	26	21	143	.2	21	9	317	5.08	25	5	ND	3	8	1	3	2	57	.06	.076	7	27	.42	80	.03	4	2.26	.01	.05	1	1
2E 6+25N	1	14	20	76	.1	10	5	294	3.46	19	5	ND	1	10	1	3	2	52	.10	.086	8	19	.20	94	.03	3	1.45	.01	.06	1	1
2E 6+00N	1	16	22	81	.5	14	5	194	3.39	24	5	ND	2	8	2	2	2	56	.07	.063	8	27	.24	65	.03	6	1.45	.01	.05	1	2
2E 5+75N	1	18	20	130	.3	16	7	242	4.67	27	5	ND	2	9	1	2	2	60	.08	.107	8	33	.34	92	.02	3	2.10	.01	.05	1	1
2E 5+50N	1	27	41	157	.6	27	10	748	4.36	53	5	ND	2	34	1	2	2	36	.84	.073	11	25	.27	88	.01	2	1.97	.01	.06	1	1
2E 5+25N	1	25	32	182	.4	26	8	299	5.45	61	5	ND	2	9	1	2	2	38	.05	.066	9	28	.34	99	.01	2	2.38	.01	.07	2	1
2E 5+00N	1	15	18	108	.4	14	6	301	2.99	32	5	ND	2	13	1	2	3	38	.07	.062	10	26	.22	116	.01	7	1.38	.01	.09	1	2
2E 4+75N	1	18	25	111	.5	14	5	220	4.01	43	5	ND	2	6	1	2	2	33	.02	.077	10	16	.19	64	.01	2	1.45	.01	.06	1	1
2E 4+50N	1	29	45	172	.5	24	8	345	3.98	49	5	ND	4	7	1	2	2	33	.02	.078	10	17	.18	72	.01	4	1.36	.01	.04	1	1
2E 4+25N	1	21	43	130	.4	16	6	244	3.64	38	5	ND	3	8	1	2	2	39	.03	.056	10	16	.13	91	.01	2	1.39	.01	.05	1	2
2E 4+00N	1	26	51	245	.4	17	8	486	5.72	47	5	ND	3	12	1	6	2	45	.16	.164	9	21	.25	117	.01	2	2.00	.01	.08	2	2
2E 3+75N	1	20	19	102	.2	18	7	298	4.53	21	5	ND	2	10	1	2	2	63	.09	.093	7	32	.32	90	.02	4	1.81	.01	.05	1	1
STD C/AU-S	18	60	40	127	7.1	69	27	1036	3.99	39	21	8	40	50	17	17	23	59	.46	.089	38	61	.84	173	.08	38	1.89	.06	.13	13	49

SOUTHERN GOLD PROJECT-121104 FILE # 87-3784

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
2E 3+50N	1	24	22	151	.2	17	7	287	4.11	25	5	ND	3	16	1	2	2	48	.14	.073	9	19	.28	128	.02	2	1.49	.01	.06	3	10
2E 3+25N	1	27	33	150	.3	21	7	312	5.03	35	5	ND	3	12	1	3	2	54	.12	.105	9	23	.31	104	.02	5	1.61	.01	.06	1	1
2E 3+00N	1	25	24	134	.8	14	7	249	5.01	32	5	ND	2	15	1	3	2	59	.16	.117	7	22	.25	121	.02	2	1.62	.01	.07	1	1
2E 2+75N	1	23	30	135	.2	13	6	240	4.85	29	5	ND	1	10	1	2	2	59	.10	.076	9	17	.21	96	.01	2	1.79	.01	.05	1	2
3E 11+50N	1	10	27	44	.6	5	2	80	1.22	12	5	ND	1	13	1	2	2	32	.07	.064	7	13	.15	86	.01	5	1.76	.01	.05	1	3
3E 11+25N	1	27	34	88	.4	17	6	239	3.84	26	5	ND	1	11	1	2	2	49	.09	.085	8	23	.34	85	.01	3	2.60	.01	.06	1	3
3E 11+00N	1	28	20	101	.3	19	7	276	5.08	23	5	ND	1	11	1	2	2	64	.06	.072	7	27	.39	90	.01	2	2.58	.01	.09	2	1
3E 10+75N	1	22	11	83	.3	14	5	187	3.25	18	5	ND	1	13	1	2	2	46	.07	.060	7	19	.29	108	.01	4	2.06	.01	.06	1	1
3E 10+50N	1	23	14	97	.3	19	8	557	3.46	15	5	ND	1	18	1	2	2	49	.13	.082	7	23	.40	129	.01	4	2.20	.01	.09	1	1
3E 10+25N	1	18	14	99	.1	16	7	491	3.09	15	5	ND	1	21	1	2	2	52	.16	.068	8	22	.41	203	.01	2	2.26	.01	.10	1	1
3E 10+00N	1	24	16	132	.3	19	9	1473	3.88	16	5	ND	1	29	1	2	2	57	.26	.084	9	26	.47	238	.01	2	2.48	.01	.12	1	8
3E 9+75N	1	28	17	122	.6	21	11	634	3.83	12	5	ND	2	19	1	2	2	52	.12	.112	9	27	.42	177	.01	3	2.92	.01	.12	1	1
3E 9+50N	1	26	7	119	.3	21	7	312	4.58	19	5	ND	1	13	1	2	2	56	.07	.056	9	27	.48	122	.01	4	2.79	.01	.10	1	1
3E 9+25N	1	23	19	95	.2	18	7	275	4.58	18	5	ND	1	13	1	2	2	60	.06	.096	7	25	.40	107	.01	5	2.48	.01	.09	1	1
3E 9+00N	1	29	20	136	.1	22	9	352	5.51	20	5	ND	3	10	1	2	2	57	.06	.086	7	30	.43	94	.02	3	3.61	.01	.07	1	1
3E 8+75N	1	23	21	92	.4	14	6	247	6.49	30	5	ND	2	10	1	2	2	81	.04	.111	7	23	.28	71	.02	2	2.65	.01	.06	1	1
3E 8+50N	1	16	24	66	.3	9	4	201	4.09	25	5	ND	2	9	1	2	2	73	.03	.076	8	18	.20	71	.02	5	1.76	.01	.05	2	2
3E 8+25N	1	24	27	110	.4	17	7	520	5.49	30	5	ND	2	9	1	2	2	66	.07	.126	8	27	.37	79	.03	2	2.13	.01	.07	1	1
3E 8+00N	1	26	40	112	.3	18	7	353	7.01	24	5	ND	2	9	1	2	2	69	.04	.113	7	29	.39	92	.03	2	3.06	.01	.06	1	1
3E 7+75N	1	24	24	119	.3	16	7	307	5.76	21	5	ND	2	11	1	3	2	67	.08	.105	8	27	.38	79	.04	3	2.74	.01	.06	1	1
3E 7+50N	1	11	18	46	.1	5	3	123	2.19	14	5	ND	1	10	1	2	2	52	.05	.035	10	13	.10	53	.03	2	1.30	.01	.03	2	1
3E 7+25N	1	18	18	100	.1	10	5	317	4.77	25	5	ND	2	11	1	2	2	71	.09	.119	10	19	.21	95	.03	2	1.93	.01	.05	1	1
3E 7+00N	1	23	32	123	.4	15	7	257	6.14	34	5	ND	3	9	1	2	3	68	.05	.127	6	23	.29	81	.04	3	2.46	.01	.07	2	1
3E 6+75N	1	24	23	175	.4	18	9	701	5.22	29	5	ND	2	11	1	2	2	62	.08	.086	8	22	.36	82	.02	6	2.83	.01	.08	1	1
3E 6+50N	2	31	21	214	.1	24	13	818	5.46	34	5	ND	2	12	1	2	3	59	.13	.070	9	25	.45	99	.02	2	3.17	.01	.08	2	1
3E 6+25N	2	42	27	194	.1	30	18	922	6.22	38	5	ND	3	12	1	2	2	43	.14	.058	9	24	.62	83	.04	3	3.34	.01	.06	2	1
3E 6+00N	1	46	35	182	.2	39	16	572	5.84	42	5	ND	3	12	1	2	2	47	.17	.051	10	38	.74	65	.05	2	3.05	.01	.06	1	1
3E 5+75N	1	19	11	81	.1	15	7	298	3.79	29	5	ND	2	5	1	2	2	40	.07	.026	9	25	.42	26	.01	3	1.58	.01	.04	1	1
3E 5+50N	1	31	33	177	.1	30	18	1394	5.47	68	5	ND	2	17	1	2	2	42	.36	.077	14	44	.75	63	.02	3	2.52	.01	.08	2	1
3E 5+25N	1	32	28	177	.2	42	15	694	5.80	51	5	ND	2	16	1	2	2	48	.36	.113	10	57	.94	61	.03	4	2.78	.01	.07	1	2
3E 5+00N	2	39	23	159	.1	32	16	782	5.85	39	5	ND	2	12	1	2	2	46	.31	.077	9	42	.80	49	.06	2	2.41	.01	.05	1	1
3E 4+75N	1	44	28	172	.2	35	17	1988	6.04	41	5	ND	3	14	1	2	2	52	.38	.085	13	47	.93	52	.09	3	2.41	.01	.06	2	1
3E 4+50N	2	47	34	186	.2	48	17	878	6.88	44	5	ND	4	13	1	2	2	60	.39	.098	9	68	1.17	61	.08	7	2.96	.01	.08	2	1
3E 4+25N	1	40	33	172	.1	31	19	3166	6.17	41	5	ND	2	17	1	2	2	50	.59	.106	11	45	.85	53	.07	2	2.37	.01	.06	1	1
3E 4+00N	1	37	34	179	.5	31	18	1323	5.41	49	5	ND	2	25	1	2	4	48	.73	.154	8	52	.68	80	.02	2	2.14	.01	.14	1	2
3E 3+75N	1	31	49	168	.4	46	21	2424	5.16	26	5	ND	2	19	1	2	2	75	.43	.140	10	112	.98	201	.03	2	2.26	.01	.09	1	1
STD C/AU-S	18	62	39	131	7.4	72	29	1051	4.07	40	17	8	41	51	17	17	19	60	.46	.091	40	58	.85	177	.08	36	1.76	.06	.14	13	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
3E 3+50N	1	28	28	116	.1	21	7	412	3.49	24	5	ND	2	16	2	2	2	52	.25	.099	8	48	.40	124	.03	4	1.43	.01	.07	1	1
3E 3+25N	1	26	30	158	.1	21	8	338	4.41	30	5	ND	1	11	1	2	2	53	.13	.104	7	30	.39	147	.02	2	1.78	.01	.05	1	1
3E 3+00N	1	29	34	145	.2	24	12	1057	4.38	37	5	ND	2	16	2	2	2	57	.27	.094	8	59	.56	146	.02	4	2.19	.01	.05	1	2
3E 2+75N	1	97	45	264	2.6	52	21	3287	5.30	89	5	ND	2	84	2	2	2	42	2.00	.145	19	80	.67	236	.01	2	3.79	.01	.12	1	1
4E 12+00N	1	25	10	90	.1	13	5	218	3.06	15	5	ND	1	9	1	2	2	47	.05	.053	6	18	.30	89	.01	3	2.18	.01	.06	1	2
4E 11+75N	1	23	13	102	.1	18	6	339	3.59	17	5	ND	1	11	1	2	3	54	.06	.061	7	24	.43	123	.01	4	2.53	.01	.08	1	1
4E 11+50N	1	23	10	104	.1	21	7	337	3.81	21	5	ND	1	12	1	2	2	51	.07	.067	7	28	.50	139	.01	2	2.63	.01	.06	1	2
4E 11+25N	1	19	42	90	.2	15	8	354	2.64	25	5	ND	1	14	1	2	2	42	.08	.065	8	20	.37	145	.01	4	2.34	.01	.06	1	1
4E 11+00N	1	39	14	119	.4	21	8	377	3.75	20	5	ND	1	18	1	2	2	51	.13	.077	8	24	.50	168	.01	5	2.60	.02	.07	1	1
4E 10+75N	1	30	5	108	.1	19	7	343	3.66	18	5	ND	1	14	2	2	2	52	.08	.082	7	26	.47	140	.01	4	2.66	.01	.08	1	2
4E 10+50N	1	25	9	95	.1	16	6	482	3.39	17	5	ND	1	13	1	2	2	51	.06	.081	7	23	.36	132	.01	4	2.31	.01	.07	1	1
4E 10+25N	1	32	27	103	.1	16	7	304	5.92	28	5	ND	2	10	1	2	2	57	.05	.097	5	22	.33	68	.02	3	2.37	.01	.05	1	2
4E 10+00N	1	37	15	283	.5	26	9	1637	4.71	22	5	ND	2	18	2	3	2	51	.22	.155	11	29	.46	255	.01	7	3.16	.01	.09	1	1
4E 9+75N	1	29	23	114	.1	15	8	470	6.84	29	5	ND	1	11	2	3	2	66	.06	.101	6	24	.34	84	.02	4	2.47	.01	.06	1	2
4E 9+50N	1	24	22	117	.1	14	6	287	4.63	25	5	ND	1	8	1	2	2	63	.03	.066	6	20	.32	73	.02	2	2.75	.01	.05	1	1
4E 9+25N	1	24	34	87	.3	14	6	374	4.82	34	5	ND	1	8	2	3	2	59	.03	.081	6	22	.32	57	.02	2	2.14	.01	.04	1	2
4E 9+00N	1	17	40	59	.3	9	4	209	3.42	32	5	ND	1	8	1	2	2	62	.02	.060	7	17	.19	61	.02	3	1.63	.01	.03	1	1
4E 8+75N	1	25	9	94	.2	16	6	288	4.14	18	5	ND	1	9	2	2	2	58	.05	.063	7	24	.38	84	.04	2	3.16	.01	.05	1	2
4E 8+50N	1	24	17	77	.2	12	5	230	5.62	29	5	ND	1	8	1	3	2	74	.03	.065	6	21	.26	57	.04	2	2.65	.01	.04	1	2
4E 8+25N	1	24	15	86	.1	14	6	322	5.55	23	5	ND	1	7	1	4	2	60	.03	.088	6	25	.31	62	.03	2	2.54	.01	.04	1	1
4E 8+00N	1	22	12	79	.1	12	6	484	4.76	20	5	ND	1	9	1	2	2	64	.05	.108	6	20	.26	59	.03	3	1.97	.01	.04	1	2
4E 7+75N	1	18	20	71	.1	8	4	227	4.60	24	5	ND	2	9	1	2	2	71	.05	.095	8	17	.18	58	.04	2	1.91	.01	.04	1	2
4E 7+50N	1	24	22	123	.5	12	6	443	5.14	30	5	ND	1	10	1	4	2	62	.08	.113	7	20	.28	77	.03	4	2.03	.01	.05	1	1
4E 7+25N	1	25	23	85	.4	11	5	245	4.42	26	5	ND	2	11	2	5	2	62	.05	.120	6	18	.22	80	.02	5	1.71	.01	.04	1	2
4E 7+00N	1	27	30	108	.1	19	9	252	4.79	31	5	ND	2	13	1	2	2	60	.10	.052	6	22	.36	108	.03	6	3.29	.01	.05	1	2
4E 6+75N	3	28	16	156	.1	22	15	2198	6.93	13	5	ND	3	32	1	2	2	58	.91	.044	13	28	.74	248	.12	6	4.74	.03	.11	1	1
4E 6+50N	3	28	17	246	.1	17	13	708	7.52	23	5	ND	2	16	1	3	2	60	.20	.029	6	21	.48	144	.09	2	3.87	.01	.09	1	2
4E 6+25N	2	25	12	207	.1	15	13	1423	5.73	22	5	ND	1	16	1	2	2	46	.25	.132	5	19	.42	116	.08	6	2.78	.01	.10	1	1
4E 6+00N	1	36	47	216	.1	56	15	548	6.28	48	5	ND	2	14	1	3	2	71	.20	.080	7	88	1.03	103	.08	2	3.10	.01	.07	1	2
4E 5+75N	1	25	39	221	.1	36	13	926	5.37	43	5	ND	1	14	1	2	2	56	.21	.103	6	59	.70	104	.04	4	2.59	.01	.08	1	1
4E 5+50N	1	31	51	279	.1	35	12	674	5.54	43	5	ND	2	11	1	5	2	54	.14	.108	8	50	.60	109	.04	6	2.45	.01	.07	1	2
4E 5+25N	1	32	26	189	.7	36	11	360	5.03	41	5	ND	2	11	1	3	2	46	.17	.057	7	40	.54	92	.07	2	2.31	.01	.08	1	1
4E 5+00N	1	45	60	266	.2	42	17	548	5.18	67	5	ND	2	19	1	2	2	56	.25	.041	14	47	.66	119	.07	3	2.66	.01	.12	1	2
4E 4+75N	2	33	60	201	.1	29	16	754	5.76	60	5	ND	3	25	1	2	2	74	.66	.038	9	39	.51	180	.04	4	2.65	.02	.07	1	1
4E 4+50N	2	31	47	207	.3	33	14	768	5.96	58	5	ND	2	14	1	2	2	71	.16	.074	8	48	.61	137	.04	3	2.46	.01	.07	1	2
4E 4+25N	1	28	58	186	.5	30	12	940	4.46	43	5	ND	2	22	1	6	2	46	.34	.077	10	22	.42	131	.01	3	1.80	.01	.11	1	1
STD C/AU-S	18	59	39	128	7.3	69	28	1019	3.90	40	21	8	38	50	18	18	20	58	.45	.091	38	60	.91	173	.09	36	1.86	.06	.13	13	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
4E 4+00N	1	28	45	157	.1	26	9	428	4.16	40	5	ND	4	13	1	4	2	52	.19	.061	8	35	.41	77	.02	2	1.79	.01	.07	1	2
4E 3+75N	1	30	50	189	.4	23	12	649	4.13	42	5	ND	3	14	1	7	2	51	.18	.060	9	26	.35	140	.02	2	1.68	.01	.07	1	4
4E 3+50N	1	29	38	166	.3	19	9	653	4.17	31	5	ND	3	13	2	4	2	50	.14	.107	8	23	.32	160	.02	6	1.60	.01	.06	1	1
4E 3+25N	1	21	29	203	.1	14	8	688	4.18	26	5	ND	1	12	1	2	2	59	.11	.071	9	26	.28	182	.02	2	1.86	.01	.06	1	2
4E 3+00N	1	48	53	259	.4	22	13	1799	4.38	41	5	ND	2	61	2	5	2	49	1.20	.089	9	33	.25	201	.01	5	2.14	.02	.07	1	2
4E 2+75N	1	30	41	137	.1	16	6	312	3.71	35	5	ND	1	15	1	7	2	54	.24	.087	8	23	.20	90	.02	5	1.32	.01	.05	1	1
4E 2+50N	1	31	48	226	.1	39	13	475	5.42	32	5	ND	2	19	1	3	3	76	.27	.054	8	75	.68	116	.05	2	2.85	.01	.07	1	4
5E 12+00N	1	21	31	74	.5	12	5	328	4.01	29	5	ND	2	9	2	4	2	59	.04	.085	7	20	.24	53	.01	2	2.00	.01	.05	1	2
5E 11+75N	1	25	15	82	.5	15	5	241	2.48	19	8	ND	2	10	1	4	2	44	.04	.069	11	20	.29	126	.01	3	2.50	.01	.07	1	1
5E 11+50N	1	21	52	73	.3	10	5	251	4.32	38	5	ND	1	9	3	2	2	59	.03	.056	7	20	.21	71	.02	2	1.98	.01	.04	1	10
5E 11+25N	1	33	30	111	.4	25	9	547	4.61	27	5	ND	2	8	1	4	2	59	.04	.084	6	36	.44	87	.02	2	2.58	.01	.06	1	2
5E 11+00N	1	26	33	84	.5	16	7	374	4.04	29	5	ND	1	9	2	5	3	56	.04	.092	6	24	.30	69	.01	6	2.08	.01	.06	2	2
5E 10+75N	1	22	10	90	.3	19	6	251	3.19	19	5	ND	2	10	2	2	3	50	.05	.052	6	25	.42	106	.01	4	2.51	.01	.08	1	1
5E 10+50N	1	14	55	46	.4	7	3	106	2.84	34	7	ND	3	9	2	4	2	54	.03	.053	7	15	.15	52	.01	5	1.59	.01	.04	1	2
5E 10+25N	1	25	32	101	.2	19	7	256	4.09	30	5	ND	2	12	2	3	2	54	.08	.075	8	24	.38	109	.01	4	2.64	.01	.07	1	3
5E 10+00N	1	39	14	154	1.3	25	7	299	3.80	9	5	ND	2	16	1	2	2	54	.07	.102	9	32	.46	246	.01	3	5.19	.02	.13	1	2
5E 9+75N	1	24	20	73	3.0	15	13	946	2.22	13	5	ND	1	14	1	2	2	46	.05	.121	8	23	.27	180	.01	5	3.38	.02	.12	1	1
5E 9+50N	1	20	33	77	.4	14	5	228	3.65	33	5	ND	1	10	1	3	2	51	.05	.078	7	24	.31	54	.02	2	2.55	.01	.05	1	2
5E 9+25N	1	23	66	91	.4	14	5	370	4.14	49	5	ND	1	8	2	3	2	56	.05	.089	7	24	.30	63	.02	2	2.35	.01	.04	1	2
5E 9+00N	1	20	15	64	.1	12	5	406	3.93	24	5	ND	2	9	1	2	2	51	.04	.094	7	20	.26	66	.02	2	2.10	.01	.06	1	1
5E 8+75N	1	24	10	81	.2	16	6	219	3.37	20	5	ND	1	9	1	2	2	47	.06	.088	7	26	.34	102	.01	2	3.24	.01	.06	1	2
5E 8+50N	1	22	12	83	.2	15	6	318	3.58	19	5	ND	1	9	1	2	2	52	.02	.077	7	23	.29	93	.01	2	2.65	.01	.07	1	1
5E 8+25N	1	32	11	101	.5	20	6	269	3.50	14	6	ND	1	12	1	2	2	49	.05	.102	9	28	.38	126	.01	4	3.33	.01	.10	1	2
5E 8+00N	1	24	22	154	.8	23	8	1159	3.51	23	5	ND	1	22	1	2	2	47	.30	.159	10	26	.43	180	.01	3	2.54	.01	.09	1	2
5E 7+75N	1	34	31	162	.4	21	9	421	5.05	30	5	ND	2	14	1	2	2	66	.04	.091	13	29	.37	219	.01	2	3.75	.01	.09	1	1
5E 7+50N	1	29	25	92	.1	18	7	254	8.00	31	5	ND	2	9	1	2	2	86	.04	.159	6	35	.35	83	.02	2	2.62	.01	.05	1	2
9E 9+00N	1	20	18	107	.2	10	5	230	4.30	20	5	ND	2	9	1	2	2	56	.03	.083	6	18	.26	61	.01	5	2.83	.01	.05	1	1
9E 8+75N	1	19	2	89	.1	12	5	226	3.06	18	5	ND	1	6	1	4	2	47	.01	.067	8	19	.29	71	.01	2	2.74	.01	.06	1	2
9E 8+50N	1	38	19	158	.3	28	12	750	5.01	29	5	ND	2	10	3	4	3	62	.01	.083	7	31	.47	162	.01	2	3.74	.01	.10	1	1
9E 8+25N	2	19	10	83	.1	15	7	391	2.82	19	5	ND	2	22	1	2	2	47	.26	.076	11	21	.26	180	.01	2	2.20	.01	.06	1	2
8E 8+00N	1	21	16	82	.1	17	6	182	3.79	19	5	ND	2	14	1	2	2	51	.08	.053	9	26	.31	102	.01	2	3.45	.01	.05	1	1
8E 7+75N	1	25	23	74	.6	17	6	192	3.72	18	5	ND	2	9	1	2	2	50	.04	.093	11	28	.33	89	.01	4	4.10	.01	.05	1	2
8E 7+50N	1	24	33	91	.2	14	6	267	6.59	26	5	ND	2	9	1	2	2	74	.02	.115	8	26	.28	69	.02	2	2.82	.01	.05	1	1
8E 7+25N	1	24	24	87	.1	15	6	264	7.68	29	5	ND	3	9	1	4	2	85	.03	.137	8	29	.29	66	.02	2	2.90	.01	.05	1	2
8E 7+00N	1	23	21	94	.1	18	7	263	6.45	22	5	ND	3	9	2	2	2	77	.03	.149	8	31	.35	71	.02	2	2.77	.01	.06	1	1
8E 6+75N	1	17	13	84	.5	11	5	237	4.02	19	5	ND	3	10	1	2	2	65	.04	.090	8	21	.21	58	.03	2	1.98	.01	.05	1	2
STD C/AU-S	18	62	38	132	7.3	72	29	1056	4.04	42	24	8	41	52	18	18	22	61	.46	.092	40	61	.85	179	.07	2	1.76	.06	.15	12	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
10E 9+00N	1	32	18	118	.6	16	7	577	4.21	18	5	ND	3	10	1	2	2	62	.04	.130	8	25	.37	89	.01	2	3.34	.01	.07	1	2
10E 8+75N	1	26	17	108	.8	19	6	309	3.56	19	5	ND	2	10	1	2	2	57	.06	.090	7	25	.42	119	.01	2	3.41	.01	.06	2	6
10E 8+50N	1	27	9	129	1.3	21	6	281	3.30	9	5	ND	2	20	2	2	2	56	.23	.136	10	30	.47	244	.01	2	4.24	.02	.10	1	1
10E 8+25N	1	15	10	48	.2	8	3	156	2.74	12	5	ND	1	12	1	3	2	53	.04	.069	6	16	.18	87	.01	5	2.06	.02	.05	4	4
10E 8+00N	1	15	8	44	.1	8	4	142	3.05	18	5	ND	1	11	1	2	2	60	.04	.059	7	14	.18	94	.01	2	1.84	.01	.04	2	2
10E 7+75N	1	27	13	91	.5	18	6	286	2.92	11	5	ND	2	11	1	2	2	52	.05	.082	10	24	.40	162	.01	5	3.21	.02	.07	1	3
10E 7+50N	1	29	15	105	1.6	18	8	392	4.51	21	5	ND	1	9	1	2	2	60	.03	.087	7	23	.36	131	.01	2	2.31	.02	.06	1	1
10E 7+25N	2	34	36	257	.8	29	13	679	4.64	12	5	ND	2	22	1	2	2	62	.23	.138	9	33	.53	305	.01	2	4.76	.02	.12	1	1
10E 7+00N	1	11	14	36	.2	6	3	115	2.08	10	5	ND	1	10	1	2	2	54	.03	.066	7	13	.12	65	.01	2	1.32	.01	.04	1	1
10E 6+75N	1	25	19	101	.2	19	7	264	4.24	18	5	ND	2	14	1	2	2	63	.11	.081	6	25	.40	135	.01	18	2.57	.03	.07	1	1
10E 6+50N	1	26	32	84	.2	13	6	325	4.04	27	5	ND	2	10	1	2	2	65	.03	.088	7	19	.23	76	.01	2	2.09	.01	.05	1	2
10E 6+25N	1	16	19	63	.1	8	4	191	3.74	19	5	ND	2	9	1	2	2	69	.03	.085	8	16	.22	60	.02	2	2.07	.01	.06	1	2
10E 6+00N	1	17	23	60	.1	9	5	280	3.85	20	5	ND	2	9	1	2	2	61	.02	.073	9	19	.22	74	.02	4	2.77	.02	.06	1	2
STD C/AU-S	17	58	37	128	7.0	68	28	1024	3.71	39	27	7	37	50	17	17	20	59	.42	.091	38	61	.90	176	.08	38	1.85	.06	.13	14	50

SOUTHERN GOLD PROJECT-121104 FILE # 87-3784

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
C# 1R	1	18	44	145	.3	6	7	734	3.82	30	5	ND	2	50	1	2	2	31	1.09	.053	7	12	.60	98	.01	7	1.18	.05	.15	1	1
C# 2R	1	35	19	90	.1	8	12	924	5.38	20	5	ND	1	38	1	2	2	56	1.63	.056	5	21	.99	53	.21	8	2.22	.07	.13	1	1
C# 3R	3	53	9	70	.3	55	25	693	6.64	10	5	ND	2	105	1	2	2	179	2.60	.108	9	74	3.11	59	.65	15	3.13	.27	.05	1	1
C# 4R	1	34	8	107	.1	37	6	1260	3.63	35	5	ND	1	206	1	2	2	10	4.08	.035	2	14	1.69	26	.01	2	.35	.02	.08	1	1
C# 5R	4	20	3	59	.1	49	12	1826	6.19	41	5	ND	1	475	1	6	2	22	10.44	.067	3	20	3.65	20	.01	5	.41	.03	.08	3	1
C# 6R	1	4	198	123	1.5	1	1	283	.40	39	5	ND	2	2	1	3	2	1	.01	.004	2	2	.01	33	.01	4	.34	.03	.20	1	12
C# 7R	1	3	152	820	2.1	4	1	2998	.40	138	5	ND	1	9	16	3	2	1	.05	.002	2	1	.02	108	.01	2	.25	.02	.19	2	31
C# 8R	2	5	433	75	3.5	1	1	50	.56	101	5	ND	1	2	1	3	2	1	.01	.001	2	1	.01	33	.01	4	.22	.01	.19	2	40
C# 9R	1	11	256	1279	.9	2	1	1050	1.49	383	5	ND	6	14	16	5	2	2	.10	.043	20	1	.02	107	.01	6	.35	.03	.14	3	29
C# 10R	1	42	11	103	.1	56	18	1189	5.17	47	5	ND	4	15	1	8	2	47	.23	.132	11	30	.50	99	.01	2	1.26	.04	.10	1	1
C# 11R	1	7	16	111	.2	3	4	816	1.77	10	5	ND	4	66	1	2	2	16	1.02	.067	16	5	.26	616	.01	10	.60	.06	.18	1	1
C# 84R	1	2	108	109	.1	1	1	364	.31	2	5	ND	2	4	1	3	3	1	.01	.003	3	1	.03	56	.01	2	.36	.04	.16	2	1
C# 88R1	76	24	157	23	1.5	23	9	32	10.51	180	5	ND	4	13	1	13	2	3	.01	.021	8	1	.02	4	.01	10	.24	.03	.19	1	11
C# 88R2	19	25	47	599	.1	26	15	559	6.19	84	5	ND	7	26	4	7	2	6	.32	.148	18	2	.03	12	.01	4	.57	.04	.23	2	1
C# 89R	11	31	26	128	.4	20	22	9946	28.08	39	5	ND	5	152	1	2	2	104	.32	.083	13	11	.63	537	.02	9	3.60	.02	.06	1	1
C# 103R	2	29	24	166	.2	28	10	2415	2.90	7	5	ND	8	69	1	6	2	22	2.83	.097	21	21	.33	95	.01	2	.85	.02	.25	1	1
C# 117R	3	13	35	253	.4	10	6	847	2.36	42	5	ND	4	148	3	3	2	6	2.42	.068	7	6	.47	111	.01	8	.29	.02	.15	1	1
C# 124R	1	16	9	111	.2	23	10	824	6.06	21	5	ND	2	21	1	2	2	81	.89	.050	6	38	1.35	29	.26	10	2.24	.05	.04	1	2
STD C/AU-R	19	60	39	129	7.0	67	27	1030	3.85	41	24	7	38	49	17	18	19	59	.45	.097	37	59	.89	174	.08	22	1.69	.06	.13	13	495

APPENDIX 2

SAMPLE DESCRIPTIONS

Sample #	Description	Cu(%)	Pb(%)	Zn(%)	Ag(OPT)	Au(OPT)
SURFACE GRAB SAMPLES						
C#1R	Location: L4E 4+75N Type: Chip sample of outcrop Fsp. porphyry andesite with laths up to 2mm. Also blebs of disseminated pyrite up to 3mm, 2-3%.	18*	44*	145*	0.3*	1**
C#2R	Location: L4E 5+50N Type: Chip sample of outcrop Very fine grained dark grey metasediment with 2-3% fine disseminated pyrite.	35*	19*	90*	0.1*	1**
C#3R	Location: L4E 6+20N Type: Chip sample of outcrop Fine grained andesitic tuff with rounded disseminations of pyrite (1-2%).	53*	9*	70*	0.3*	1**
C#4R	Location: L4E 5+00 - 5+50N Type: Grab sample Chloritic quartz-calcite veined phyllite.	34*	8*	107*	0.1*	1**
C#5R	Location: L4E ST00N - 5+50N Type: Grab sample Sericitic quartz calcite veined schist	20*	3*	59*	0.1*	1**
C#6R	Location: L5W 8+00N Type: Chip sample Very fine grained siliceous rhyolite, pale (white) with dendritic manganese stain on fractures.	4*	198*	123*	1.5*	12**
C#7R	Location: L4W 8+00N - 7+75N Type: Grab sample Massive to slightly sericitized & foliated rhyolite, weathered yellow, locally bleached white. Manganese stained.	3*	152*	820*	2.1*	31**
C#8R	Location: Trench Type: Grab Iron stained & bleached rhyolite	5*	433*	75*	3.5*	40**

Note: * Indicates values in ppm ** Indicates values in ppb

Sample #	Description	Cu(%)	Pb(%)	Zn(%)	Ag(OPT)	Au(OPT
C#9R	Location: L10W 6100N Type: Grab from trench Porphyritic iron stained rhyolite with quartz diorite dyke to N.E.	11*	256*	1279*	0.9*	29**
C#10R	Location: L9W 10+85N Type: Grab Iron stained feldspar porphyry rhyolite in 2m band over & underlain by choritic phyllite.	42*	11*	103*	0.1*	1**
?	Location: L11W 6 + 50N Type: Chip across 130 cm FW 30 cm quartz breccia vein with less than 5% Ga + Sph in blebs & disseminations. 25 cm quartz diorite dyke 35 cm massive white quartz vein with blebs & dissemination of Ga + Sph.					
C#11R	Location: L11+50W 7+75N Type: Grab sample Two to three metre quartz diorite dyke with 1-2% pyrite.	7*	16*	111*	0.2*	1**
C#84R	Location: L22W 11+25N Type: Grab sample from pit Bleached feldspar porphyry with fine disseminated pyrite & galena.	2*	108*	109*	0.1*	1**
C#88R1	Location: L22+30W 16+50N Type: Grab sample Bleached rhyolite with stockwork sulphide veining with 10-15% fine pyrite.	24*	157*	23*	1.5*	11**
C#88R2	Location: L22 +30W 16+50N Type: Grab sample of float Feldspar porphyry andesite with 10% disseminated pyrite.	25*	47*	599*	0.1*	1**

Note: * Indicates values in ppm ** Indicates values in ppb

Sample #	Description	Cu(%)	Pb(%)	Zn(%)	Ag(OPT)	Au(OPT)
C#89R	Location: L22W 16+50N Type: Grab sample of float Massive dense haematite altered volcanic breccia.	31*	26*	128*	0.4*	1**
C#103R	Location: C26W 16+20N Type: Grab sample Strongly iron stained, moderately foliated rhyolite with minor disseminated pyrite.	29*	24*	166*	0.2*	1**
C#117R	Location: L9W 3+50N Type: Chip across 400 cm FW 200 cm band of very fine grained cherty rhyolite with 1-2% dissem. Pyrite. HW 200 cm quartz veined rhyolite.	13*	35*	253*	0.4*	1**
C#124R	Location: Type: Grab sample Grit with 3-4% disseminated very fine grained pyrite.	16*	9*	111*	0.2*	1**
HOMESTAKE ADIT						
H#1	Location: Homestake adit in small raise Type: Chip sample across 150 cm Quartz vein with locally massive blebs of Galena and sphalerite.	0.13	7.30	11.43	15.75	0.018
H#2	Location: Homestake adit in wall south of shaft Type: Chip sample across 115 cm Quartz vein with minor disseminated Galena & Sphalerite.	0.01	1.65	0.20	1.87	0.002
H#3	Location: Homestake adit Type: Chip sample	0.01	0.24	0.20	0.27	0.002
H#4	Location: Homestake adit Type: Chip sample	0.06	0.87	6.68	1.41	0.003

Note: * Indicates values in ppm ** Indicates values in ppb

Sample #	Description	Cu(%)	Pb(%)	Zn(%)	Ag(OPT)	Au(OPT
UNDERGROUND SAMPLES, MAIN WORKINGS						
CU#1	Location: #3 level @ 59m from North portal Type: Chip sample across 110 cm of #2 vein. Quartz vein with abundant sulphides, 20% + Ga & Sph.	0.57	11.48	8.72	14.18	0.038
CU#2	Location: #3 level @ 69m from north portal Type: Chip sample across 120 cm of #2 vein. Quartz vein with abundant sulphides 20-25% Ga & Sph.	0.36	7.50	7.95	26.45	0.037
CU#3	Location: #3 level @ 77m from south portal Type: Chip sample across 80 cm of #1 vein. Quartz vein with abundant sulphides, principally sphalerite (20-25%) & Galena (10%).	0.35	4.65	12.26	6.01	0.015
CU#4	Location: #3 level @ 71m from south portal Type: Chip sample across 115 cm #1 vein Largely barren quartz vein & sheared rhyolite.	0.01	0.62	0.56	0.85	0.014
CU#5	Location: #3 level @ 61m from south portal Type: Chip sample across 115 cm of #1 vein HW 40 cm quartz veined rhyolite 65 cm poorly mineralized quartz vein FW 10 cm sulphide rich vein (Ga + Sph).	0.02	0.84	1.07	1.13	0.014
CU#6	Location: #5 level @ 294m from portal Type: Chip sample across 75 cm of #2 vein Fairly poorly mineralized quartz vein with only 3-4% sulphides, principally Ga + Sph.	0.06	0.80	0.29	3.19	0.019
CU#7	Location: #5 level @ 311m from portal Type: Chip sample across 85 cm of #2 vein Poorly mineralized vein enclosing 30 cm of barren rhyolite.	0.03	0.22	0.26	0.93	0.044
CU#8	Location: #5 level, 266m from portal Type: Chip across 85 cm of #2 vein Poorly mineralized vein between ore chutes.	0.01	0.76	0.92	1.30	0.037

Note: * Indicates values in ppm ** Indicates values in ppb

Sample #	Description	Cu(%)	Pb(%)	Zn(%)	Ag(OPT)	Au(OPT)
CU#9	Location: #5 level, 251m from portal Type: Chip sample across 110 cm of #2 vein Very well mineralized quartz vein with abundant sulphides including >20% Galena & 15-20% sphalerite.	0.25	10.19	7.88	11.89	0.013

WARDELL ZONE SAMPLES

Sample #	Description	Cu(%)	Pb(%)	Zn(%)	Ag(OPT)	Au(OPT)
CW#1	Location: Homestake adit dump Type: Grab of coarse dump material Large pieces of quartz vein with 30% + Galena, Sphalerit & pyrite.	0.49	14.22	7.46	22.81	0.032
CW#2	Location: Trench at west end of zone Type: Chip across 1m Quartz vein with 3-4% Galena	0.04	2.51	0.23	8.43	0.008
CW#3	Location: Small trench near west end of zone Type: Chip across 1m Very poorly mineralized quartz veined rhyolite.	0.01	0.35	0.09	0.43	0.006
CW#4	Location: Pit near west end of zone Type: Chip across 80 cm Small cross cutting quartz vein at 110 /80N HW 30 cm quartz vein 20 cm Rhyolite dyke 30 cm quartz vein with 10% Galena	0.01	4.63	0.07	8.92	0.189
CW#6	Location: Trench along strike to NW of CW#4 Type: Chip across 160 cm Cross cutting quartz vein with 5-10% disseminated Galena.	0.01	4.13	0.06	6.46	0.006
CW#7	Location: Trench near west end of zone Type: Chip across 45 cm vein Possible extension of Wardell Zone with 10% disseminated Galena.	0.01	4.21	0.31	7.06	0.036

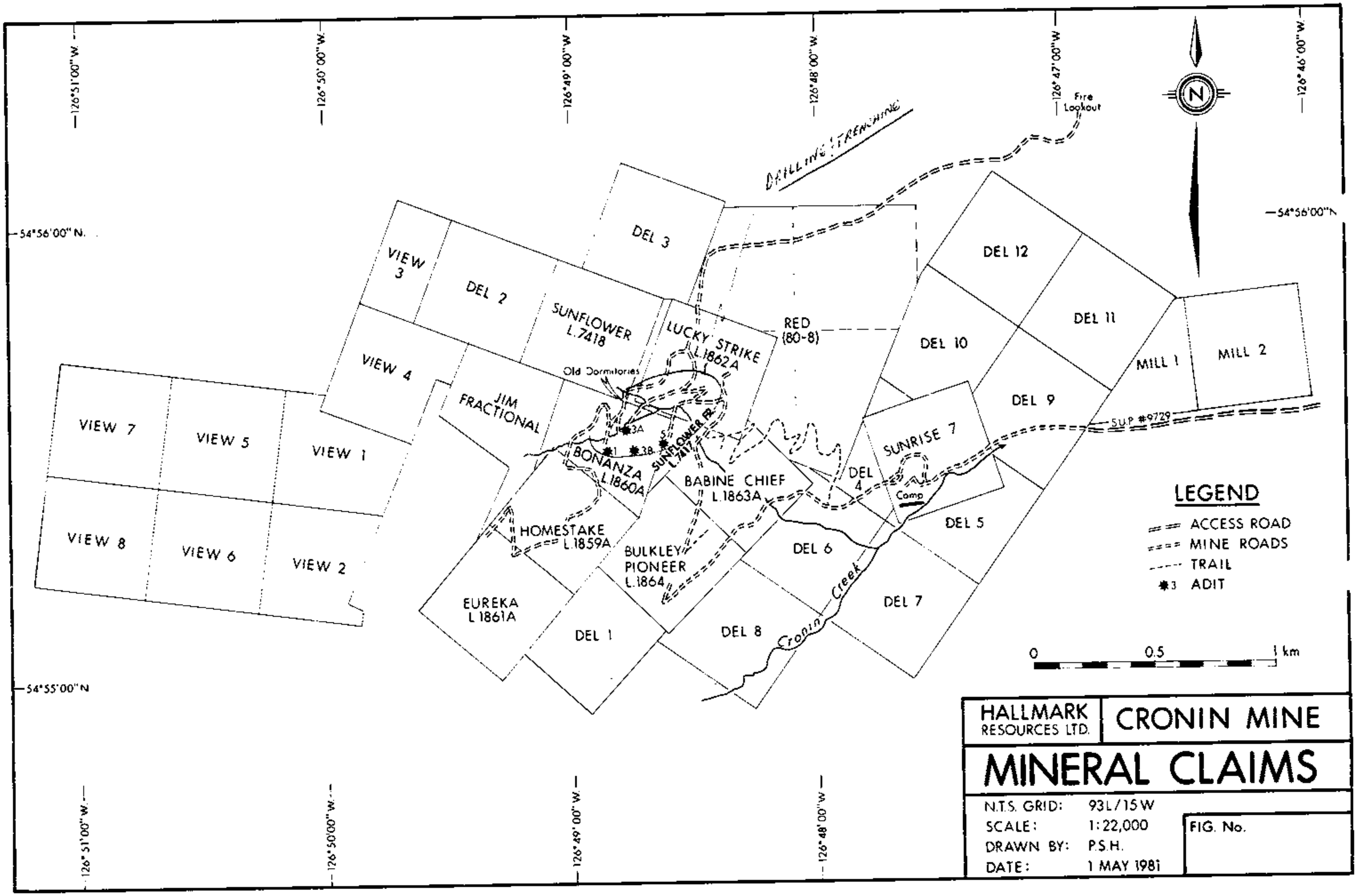
Note: * Indicates values in ppm ** Indicates values in ppb

Sample #	Description	Cu(%)	Pb(%)	Zn(%)	Ag(OPT)	Au(OPT
CW#8	Location: NW end of Wardell Zone Type: Chip across 70 cm Quartz vein with abundant Galena (30%+).	0.01	14.49	0.18	12.13	0.038
CW#9	Location: West end of Wardell vein Type: Chip across 35 cm Wardell vein ends & narrow 35 cm quartz vein splays off at 120 to main trend with minor disseminated Galena.	0.01	0.72	0.10	2.55	0.003
CW#10	Location: Main Wardell vein, western end Type: Chip across 100 cm Poorly exposed Wardell vein with minor Galena (<5%).	0.02	2.06	0.24	4.54	0.011
CW#11	Location: Wardell shafts, immediately east of. Type: Chip across 450 cm Very wide section of Wardell vein, quartz vein & altered/veined rhyolite with abundant sulphides; 30% Ga, 20% Sph.	0.23	12.05	7.60	46.29	0.066
CW#12	Location: Wardell shafts, immediately west of. Type: Chip across 450 cm Main section of Wardell Zone with abundant sulphides very similar to CW#11.	0.09	3.54	6.37	9.88	0.092
CW#13	Location: 2m east of CW#11 Type: Chip across 320 cm Probably footwall section of Wardell vein, with richest part trenched out.	0.06	6.23	0.50	16.90	0.044
CW#14	Location: East of #2 Shaft Type: Chip across 50 cm Nearly barren massive white quartz vein	0.01	0.25	0.16	1.58	0.006
CW#15	Location: East of #2 shaft & CW#14 Type: Chip across 40 cm Same vein as CW#14, barren white quartz	0.01	0.10	0.03	0.74	0.004

Note: * Indicates values in ppm ** Indicates values in ppb

Sample #	Description	Cu(%)	Pb(%)	Zn(%)	Ag(OPT)	Au(OPT
CW#16	Location: Above #1 Portal near 8+50W 7+00N Type: Chip across 60 cm Includes 20 cm of quartz vein with blebs of massive Galena & minor Sphalerite.	0.35	12.03	1.46	11.66	0.007
CW#17	Location: Above #1 Portal Type: Chip across 80 cm Includes 35 cm of quartz vein with 5% Galena & 5% Sphalerite.	0.05	3.10	2.80	3.43	0.033
CW#18	Location: Above #1 Portal near 8+50W 7+00N Type: Chip across 170 cm Irregularly quartz veined & brecciated zone with massive blebs of Galena (~25%).	0.25	10.80	0.08	19.54	0.009
CW#20	Location: Above #1 Portal near 8+50W 7+00N Type: Chip across 65 cm Mostly barren quartz vein with minor Ga + Sph.	0.01	0.02	0.02	0.08	0.001

Note: * Indicates values in ppm ** Indicates values in ppb



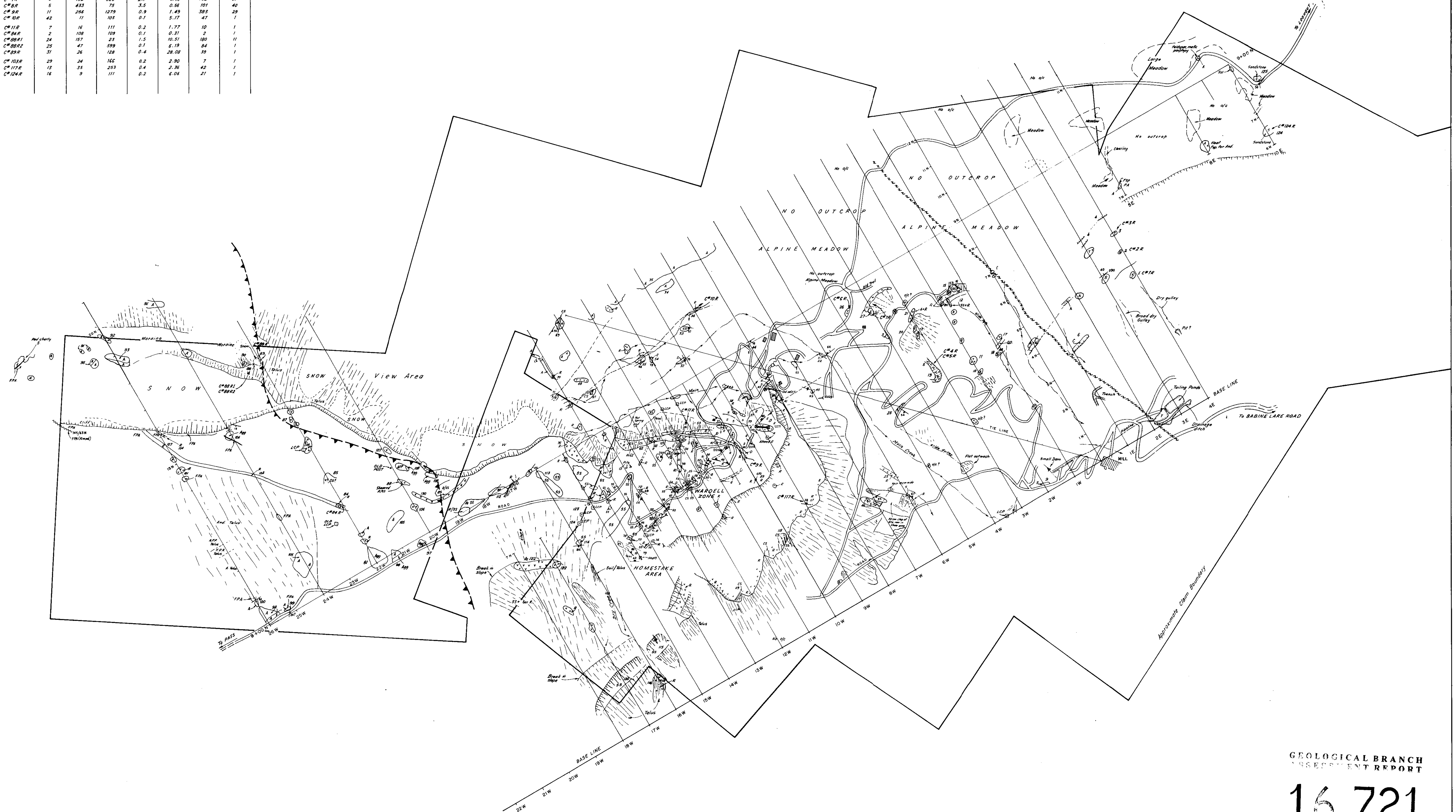
HALLMARK RESOURCES LTD.	CRONIN MINE

MINERAL CLAIMS

N.T.S. GRID: 93L/15W
SCALE: 1:22,000
DRAWN BY: P.S.H.
DATE: 1 MAY 1981

FIG. No.

SAMPLE Nos.	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Fe (ppm)	As (ppm)	Au (ppb)
87– C# 1R	18	44	145	0.3	3.82	30	1
C# 2R	35	19	90	0.1	5.38	20	1
C# 3R	53	9	70	0.3	6.64	10	1
C# 4R	34	8	107	0.1	3.63	35	1
C# 5R	20	3	59	0.1	6.19	41	1
C# 6R	4	198	123	1.5	0.40	39	12
C# 7R	3	152	820	2.1	0.40	138	31
C# 8R	5	433	75	3.5	0.56	101	40
C# 9R	11	256	1279	0.9	1.49	383	29
C# 10R	42	11	103	0.1	5.17	47	1
C# 11R	7	16	111	0.2	1.77	10	1
C# 84R	2	108	109	0.1	0.31	2	1
C# 88R1	24	157	23	1.5	10.51	180	11
C# 88R2	25	47	599	0.1	6.19	84	1
C# 89R	31	26	128	0.4	28.08	39	1
C# 103R	29	24	166	0.2	2.90	7	1
C# 117R	13	35	253	0.4	2.36	42	1
C# 124R	16	9	111	0.2	6.06	21	1



NOTE: Slope distances are not corrected along the direction of Grid Lines N.W. to S.E.

LEGEND

SEDIMENTARY & VOLCANIC ROCKS

BRIAN BORU FORMATION
Principally porphyritic andesite flows (A) & andesitic agglomerates (Agg)

RED ROSE FORMATION
Black to dark grey shale (cs), chert pebble conglomerate micaceous greywacke. Altered to sericite schist (ss) in vicinity of rhyolite intrusives

ASHMAN FORMATION
Dark grey to black shale, sandstone & chert pebble conglomerate

INTRUSIVE ROCKS

Dykes — Quartz Diorite (QD), Diorite (D)
Porphyritic Rhyolite
Indeterminate Granitic intrusive

Fault
Fault, interpreted
Thrust Fault, interpreted
Bedding, inclined
Foliation, inclined, vertical
Vein

D.D.H. *Diamond Drill Hole*
Shaft
Adit
Trench
92 *Field Note Reference*
C#6R *Rock sample number*

Road
Creek
LCP *Legal Corner Post*

N

SOUTHERN GOLD RESOURCES LTD.
NORTH VANCOUVER, BRITISH COLUMBIA

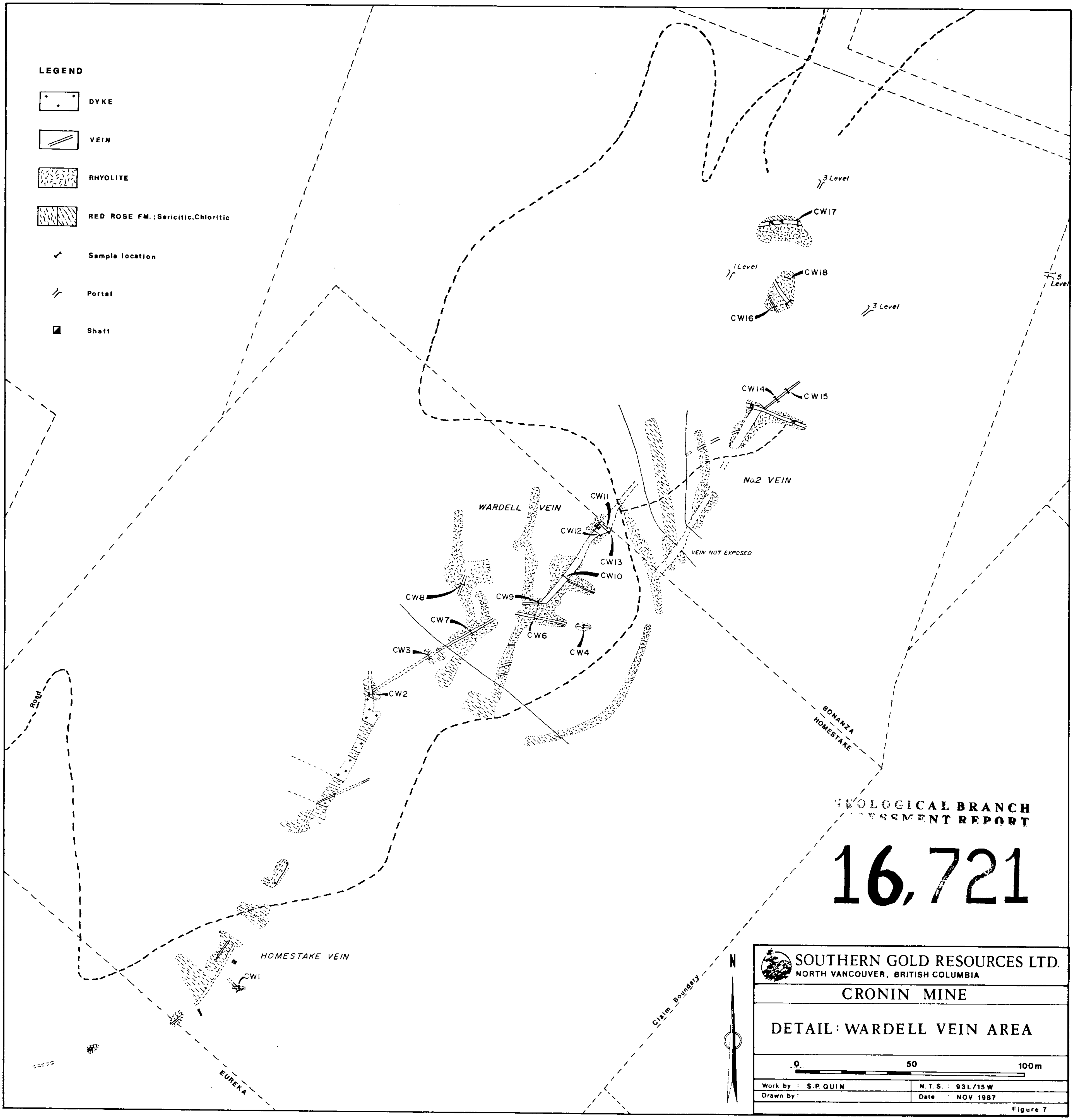
CRONIN MINE PROPERTY

FIELD GEOLOGY

SCALE 1:5000
METRES 100 50 0 100 200 300 400 METRES

Work by : STEPHEN P. QUIN	N.T.S. : 93 L / 15
Drawn by : RAM N. GOPAL	Date : SEPTEMBER, 1987

FIGURE 6



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,721

SOUTHERN GOLD RESOURCES LTD.
NORTH VANCOUVER, BRITISH COLUMBIA

CRONIN MINE

DETAIL: WARDELL VEIN AREA

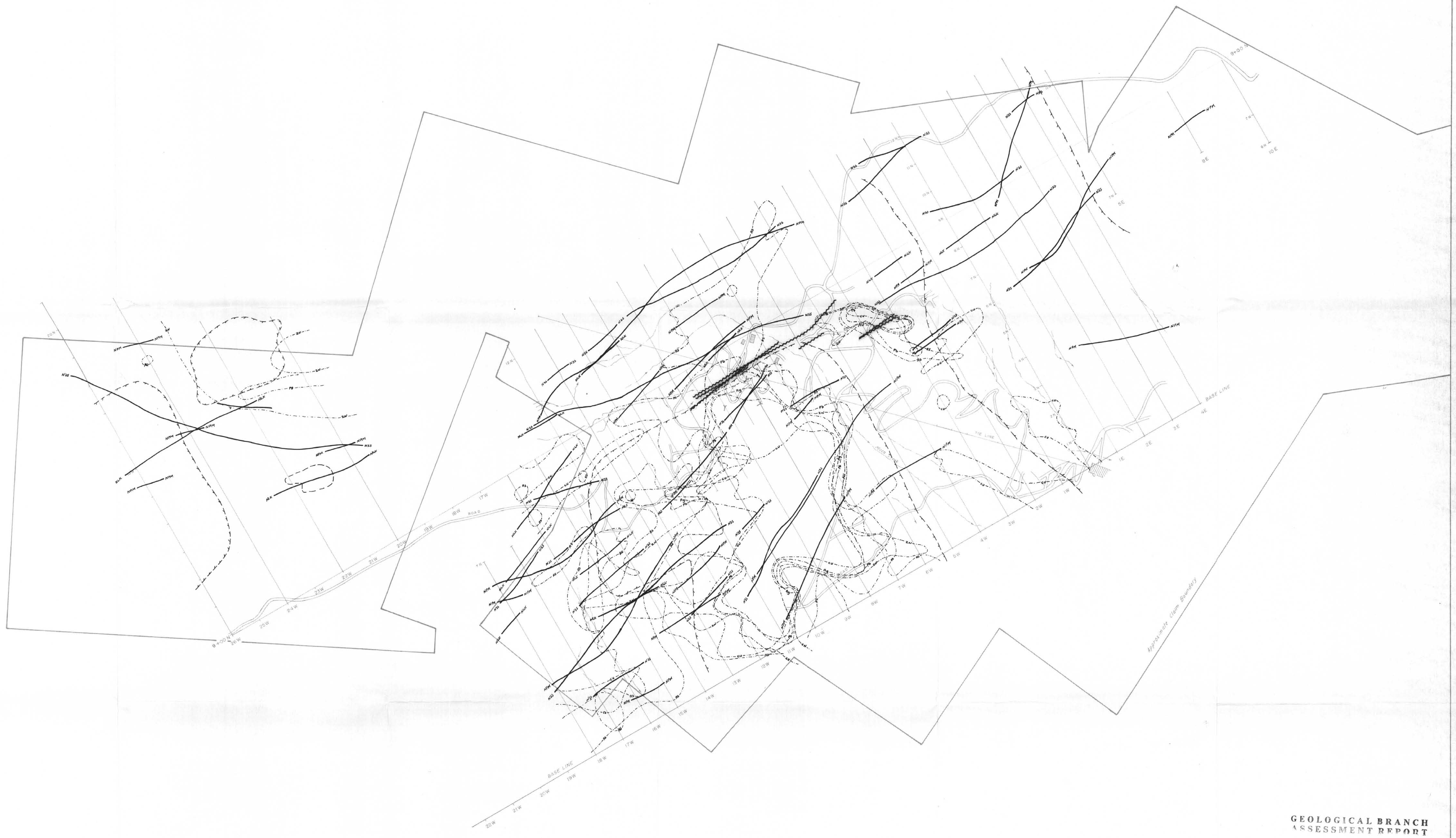
0 50 100m

Work by : S.P. QUIN	N.T.S. : 93L/15W
Drawn by :	Date : NOV 1987
	Figure 7

GEOLOGICAL BRANCH
ASSESSMENT REPORT
16,721
LEGEND
Ag ppm Au ppb
15 + 34
APPROXIMATE CLAIM BOUNDARY
metres
SOUTHERN GOLD RESOURCES LTD.
CRONIN MINE PROPERTY
AG & AU GEOCHEMISTRY
SCALE: 1:5000
DATE: Sept.'87
N.T.S. 93L/15W
DRAWN BY GEO-COMP
FIGURE 11

SOUTHERN GOLD RESOURCES LTD.
CRONIN MINE PROPERTY
PB & ZN GEOCHEMISTRY
SCALE: 1:5000
DATE: Sept.'87
N.T.S. 93L/15W
DRAWN BY GEO-COMP
FIGURE 12
GEOLOGICAL BRANCH
ASSESSMENT REPORT
16,721
0 100 200 300 400
metres
LEGEND
Pb ppm Zn ppm
158 + 34
APPROXIMATE CLAIM BOUNDARY
BASE LINE
2100N
2000N
1900N
1800N
1700N
1600N
1500N
1400N
1300N
1200N
1100N
1000N
900N
800N
700N
600N
500N
400N
300N
200N
100N
00
26W
24W
22W
20W
18W
17W
16W
15W
14W
13W
12W
11W
10W
9W
8W
7W
6W
5W
4W
3W
2W
1W
0
1E
2E
3E
4E
5E
8E
9E
10E


APPROXIMATE CLAIM BOUNDARY
2100N
2000N
1900N
1800N
1700N
1600N
1500N
1400N
1300N
1200N
1100N
1000N
900N
800N
700N
600N
500N
400N
300N
200N
100N
BASE LINE
00
26W
24W
22W
20W
18W
17W
16W
15W
14W
13W
12W
11W
10W
9W
8W
7W
6W
5W
4W
3W
2W
1W
0
1E
2E
3E
4E
5E
8E
9E
10E
LEGEND
As ppm Cu ppm
158 + 34
GEOLOGICAL BRANCH
ASSESSMENT REPORT
16,721
0 100 200 300 400
metres
SOUTHERN GOLD RESOURCES LTD.
CRONIN MINE PROPERTY
AS & CU GEOCHEMISTRY
SCALE: 1:5000
DATE: Sept.'87
N.T.S. 93I/15W
DRAWN BY GEO-COMP
FIGURE 13



Mag High

STRONG — VLF EM Conductors
NPM – HAWAII
NSS – ANNAPOLIS
WEAK — NLK – SEATLE

Geochemically Anomalous Areas

Au	Gold
Cu	Copper
Pb	Lead
As	Arsenic
Ag	Silver
Zn	Zinc

Road
Creek

N

SOUTHERN GOLD RESOURCES LTD.
NORTH VANCOUVER, BRITISH COLUMBIA

CRONIN MINE PROPERTY

COMPOSITE ANOMALY MAP

SCALE 1:5000
METRES 100 50 0 100 200 300 400 METRES

Work by : STEPHEN P. QUIN	N.T.S. : 93 L / 15 (N.W.)
Drawn by : Ram N. Gopal	Date : SEPTEMBER, 1987

FIGURE 14