



Province of  
British Columbia  
Ministry of  
Energy, Mines and  
Petroleum Resources



**FAME PROGRAM**

(FINANCIAL ASSISTANCE FOR MINERAL EXPLORATION)

**FORM 3**

**APPLICATION FOR PAYMENT**

Grant  
Identification No. 10962-E33 <sup>E34</sup>

**INSTRUCTIONS:**

- Please type or print
- Please submit completed forms, with two copies of the final technical report, to:

*Mailing address:* Manager, FAME, Mineral Resources Division.  
Ministry of Energy, Mines and Petroleum Resources, Parli-  
ament Buildings, Victoria, B.C. V8V 1X4

*Office location:* Manager, FAME, Mineral Resources Division, 300, 756 Fort  
Street, Victoria, B.C.

Date of this Application

February 26, 1988

Applicant: CATHEDRAL GOLD CORPORATION

Address: 800 - 601 West Hastings Street Telephone: (604) 669-8959

City: Vancouver Province: B.C. Postal Code: V6B 5A6

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

Mailing Address (if different from above)

Name: same

Address: \_\_\_\_\_

City: \_\_\_\_\_ Province: \_\_\_\_\_ Postal Code: \_\_\_\_\_

16,743

British Columbia Free Miner Certificate No. 299198

FILMED

I/We, Cathedral Gold Corporation, hereby  
apply for payment of a grant under the FAME (Financial Assistance for Mineral Exploration) Program and declare the information  
given above to be true and accurate.

Peter R. Delancey  
Signature of Applicant or Signing Officer

Peter R. Delancey P. Eng.  
Name (please print)

Senior Geologist  
Title/Occupation (please print)

CUNNINGHAM CREEK  
Project Name (please print)

CATHEDRAL GOLD CORPORATION  
Company (please print)

February 26, 1988  
Date

**EXPENDITURES** (N.B. Please provide actual all-inclusive costs, including salaries and wages, equipment and machinery rental, supplies, services, transportation and accommodation directly attributable to the field program.)

(a) For the following, the full cost (100% of expenditures) are eligible:	Total Eligible Expenses
<b>Geological Surveys, Map and Report Preparation and Related Costs</b>	\$ 35,730.00
<b>Geophysical Surveys (line-kilometres)</b>	
Ground	
Magnetic ..... 9.1 km (10m spacings) ..... \$ 910.00	
Electromagnetic .....	\$
Induced Polarization .....	\$
Radiometric .....	\$
Seismic .....	\$
Other .....	\$
Airborne .....	\$
\$ 910.00	\$ 910.00
<b>Geochemical Surveys (No. of samples analysed for _____)</b>	
Soil ..... 940 for 30 element ICP + Au by AA ..... \$ 20,340.00	
Silt .....	\$
Rock ..... 356 for 30 element ICP + Au by AA ..... \$ 8,717.00	
Other .....	\$
\$ 29,057.00	\$ 29,057.00
<b>Drilling</b>	
Surface ..... 1098.4 ..... m @ \$ 123.79 / m ..... = \$135,967.00	
Underground .....	\$
\$	\$ 135,967.00
<b>Related Technical Surveys</b>	
Sampling/Assaying ..... Core - 128 analyses ..... \$ 3,696.00	
Petrographic .....	\$
Mineralogic .....	\$
Metallurgic .....	\$
\$ 3,696.00	\$ 3,696.00
<b>Preparatory/Physical</b>	
Line/Grid (kilometres) ..... 28 km ..... \$ 4,500.00	
Trenching (metres) .....	\$
\$	\$ 4,500.00
<b>Other Exploration Costs (attach detailed schedules)</b>	
.....	\$
.....	\$
.....	\$
\$	\$
<b>Total Eligible Expenses</b>	<b>\$ 209,860.00</b>

(b) For the following activities only 25% of total costs are eligible:

<b>Tunneling, Drifting, Other Lateral Excavation, Shaft Sinking</b> (25% of total expenses are eligible)	
..... m @ \$ ..... = \$ x 25% = \$	
..... m @ \$ ..... = \$ x 25% = \$	
\$	\$

(c) **TOTAL ELIGIBLE EXPENDITURES:** \$ 209,860.00

**Goods and Services**

Description	Expenditure	
	B.C.	Outside
Meals, Groceries, etc.	\$ 6,960.00	\$
Camping Supplies, Equipment, etc.	3,640.00	
Accommodation	1,000.00	
Transportations — Scheduled Air	2,000.00	
— Air Charter		
— Vehicle Rentals	4,000.00	
— Vehicle O and M Costs	1,000.00	
— Other (specify)		
Equipment Rentals —		
Equipment Rentals — Trenching, etc.		
— Geophysical, etc.		
— Other (specify)		
Contract Drilling	130,967.00	
Consultant Services		
Assays and Analyses	16,753.00	
Communications	500.00	
Other (specify)		
<b>TOTALS:</b>	<b>\$166,820.00</b>	<b>\$</b>

**PACT OF FAME GRANT**

(a) Please indicate what level of **expansion** of your project was attributable to receiving a FAME grant.

\$ 20,000.00

70 person/days employment.

(b) Please indicate what you feel to be the main achievement of this FAME funded program.

Gave additional incentive to drill test deserving targets

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**SUPPLEMENTARY INFORMATION:** The following information is required in order to help us determine the contribution which mineral exploration activity makes to the economy, and relates to the utilization of B.C. vs. outside labour and services. Only figures directly attributable to the funded program should be included (approximate figures acceptable, but please be as accurate as possible).

**(a) Employment, wages and salaries**

Type	No. Employed		No. Person-days		Salaries/Wages Paid	
	B.C.	Outside	B.C.	Outside	B.C.	Outside
Prospectors					\$	\$
Linecutters						
Technicians						
General Labourers						
Drillers/Helpers						
Equipment Operators						
Geologists	4		232		\$ 41,455.00	
Geophysicists	1		3		909.00	
Geochemists						
Engineers						
Supervisory	1		3		1,200.00	
Consulting						
Secretarial						
Managerial						
Legal						
Accounting						
Others (specify)						
Others (specify)						
<b>TOTALS:</b>					\$ 43,564.00	\$



TYPE OF WORK IN THIS REPORT	EXTENT OF WORK (IN METRIC UNITS)	ON WHICH CLAIMS	COST APPORTIONED
f GEOLOGICAL (scale, area) Ground	1:1,000 Lease 32		\$ 37,504
Photo			
GEOPHYSICAL (line-kilometres)			
Ground			
Magnetic	9.1 km		910.00
Electromagnetic			
Induced Polarization			
Radiometric			
Seismic			
Other			
Airborne			
GEOCHEMICAL (number of samples analysed for ....)			
Soil	940	Mineral Lease M32	
Silt			29,057.00
Rock	356	Mineral Lease M32	
Other			
DRILLING (total metres; number of holes, size)			
Core	12 holes totalling 1098.4 m	Mineral Lease M32	135,967.00
Non-core			
RELATED TECHNICAL			
Sampling/analysis core	128		3,696.00
Petrographic			
Mineralogic			
Metallurgic			
PROSPECTING (scale, area)			
PREPARATORY/PHYSICAL			
Legal surveys (scale, area)			
Topographic (scale, area)			
Photogrammetric (scale, area)			
Line/grid (kilometres)	28 km		4,500
Road, local access (kilometres)			
Trench (metres)			
Underground (metres)			
			TOTAL COST 211,634.00

FOR MINISTRY USE ONLY	NAME OF PAC ACCOUNT	DEBIT	CREDIT	REMARKS:
Value work done (from report)				
Value of work approved				
Value claimed (from statement)				
Value credited to PAC account				
Value debited to PAC account				
Accepted	Rept. No.			Information Class
Date				



Province of  
British Columbia

Ministry of  
Energy, Mines and  
Petroleum Resources

ASSESSMENT REPORT  
TITLE PAGE AND SUMMARY

TYPE OF REPORT/SURVEY(S)	TOTAL COST
DRILLING, GEOLOGICAL, GEOCHEMICAL, GEOPHYSICAL	\$211,634.00

AUTHOR(S) PETER R. DELANÇEY, P. ENG. . . . . SIGNATURE(S) *P.R. Delancey*

DATE STATEMENT OF EXPLORATION AND DEVELOPMENT FILED February, 1988 . . . . . YEAR OF WORK 1987

PROPERTY NAME(S) CUNNINGHAM CREEK

COMMODITIES PRESENT Gold

B.C. MINERAL INVENTORY NUMBER(S), IF KNOWN

MINING DIVISION Cariboo . . . . . NTS 93 A 14

LATITUDE 52°55' N . . . . . LONGITUDE 121°21' W

NAMES and NUMBERS of all mineral tenures in good standing (when work was done) that form the property [Examples: TAX 1-4, FIRE 2 (12 units); PHOENIX (Lot 1706); Mineral Lease M 123; Mining or Certified Mining Lease ML 12 (claims involved)]:

Mineral Lease M32, Black Martin 1 & 2, 3 & Fr., Side Winder 1-3, Jim (3 units), Louise (20 units), Donna (12 units)

OWNER(S)

(1) Cathedral Gold Corporation . . . . . (2)

MAILING ADDRESS

Suite 800-601 West Hastings Street  
Vancouver, B.C. V6B 5A6

OPERATOR(S) (that is, Company paying for the work)

(1) Cathedral Gold Corporation . . . . . (2)

MAILING ADDRESS

Suite 800-601 West Hastings Street  
Vancouver, B.C. V6B 5A6

SUMMARY GEOLOGY (lithology, age, structure, alteration, mineralization, size, and attitude):

The Cunningham property is located within the same deformed belt of metasedimentary rocks (Downey Creek: FM. - Mississippian?) hosting the gold deposits at Wells, B.C. . . . . Interbedded quartzites, sericite schists, limestones and chlorite schists strike NW and dip 70-80° NE. Several systems of quartz veins cut these rocks; some veins are gold bearing. . . . . Roughly parallel trending veins-Shasta, Hudson and 605 occupy steeply . . . . . dipping faults. . . . . Gold mineralization is associated with sulphides, mostly pyrite, and is concentrated along steeply plunging ore shoots. Preliminary indications suggest that massive pyritic "replacement" deposits similar to those at Wells, may occur along a limestone horizon.

REFERENCES TO PREVIOUS WORK:

Assessment Report - Geochemical Report on Cunningham Creek Claims, December 1983 by S. Quin. (over)  
Assessment Report - Drilling, Geochemical Report July 1987.

1987 CUNNINGHAM CREEK PROPERTY REPORT

(NTS 93 A,H)

for

IMPERIAL METALS CORPORATION

PETER R. DELANCEY, P. Eng.  
FEBRUARY 1988  
VANCOUVER, BRITISH COLUMBIA

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## 1.0 INTRODUCTION

Cathedral Gold Corporation has a 100% interest in the Cunningham Creek gold property situated 25 km southeast of the towns of Wells and Barkerville, in east-central British Columbia. The property consists of 15 claims and fractions under Mining Lease M32, 7 reverted Crown Granted Claims and 35 MGS units.

The property lies within the Cariboo Gold Belt, one of the major gold producing areas in North America. Placer gold, discovered here in 1859, sparked the great Cariboo gold rush, some 2.5 million ounces of placer gold were recovered. Although extensive exploration for the source of the placer gold was undertaken, it was not until the 1930's that lode production commenced from the Cariboo Gold Quartz and Island Mountain Mines at Wells. Gold bearing quartz veins were discovered on the Cunningham Creek property in the early 1920's but serious work did not commence until 1937. Extensive underground development was carried out on several parallel veins, however, only the Hudson Vein saw production, with 13,000 tons grading 0.40 oz/ton mined and milled. The mine was closed at the outbreak of the World War II.

The Cunningham claims are located within the same belt of rocks hosting the gold deposits at Wells. The Cariboo Gold Quartz, Island Mountain and Mosquito Creek deposits occur along a favourable horizon in highly deformed metasedimentary rocks. The mines have a recorded production of approximately 3 million tons grading 0.40 oz/t. Ore occurs as two distinct types, shallowly plunging sulphide "replacement" bodies and steeply dipping quartz veins. Mosquito Creek Gold Mines is presently carrying out limited mining of replacement ore, to be stockpiled and treated at their 100 tons per day cyanide plant.

Recent exploration of the Cunningham property has focused on drill testing and underground sampling of the Shasta Vein; some 37,000 tons of 0.36 oz/ton gold has been outlined above the 200' level.

The purpose of the 1987 program was to upgrade our understanding of the property prior to drill testing selected targets. Particular emphasis was placed on areas favourable for "replacement" mineralization. Property mapping, fill-in and extension soil surveys, local magnetometer surveys and extensive rock sampling was carried out.

Twelve holes, totalling 1,098m, were drilled to test replacement targets and gold bearing quartz veins (ie 605 Vein).

### 1.1 Location and Access

The Cunningham property is located 25 km southeast of the towns of Wells and Barkerville in east-central British Columbia. The approximate geographic center of the claims is Lat. 52° 55'N, Long. 121° 21'W on NTS Map Sheet 93 A/14 (Figure 1).

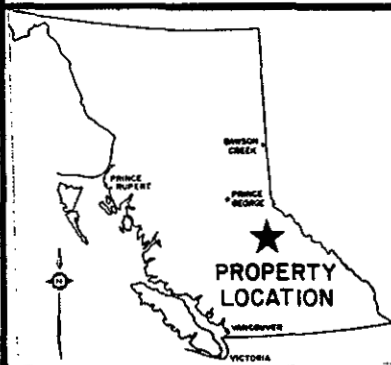
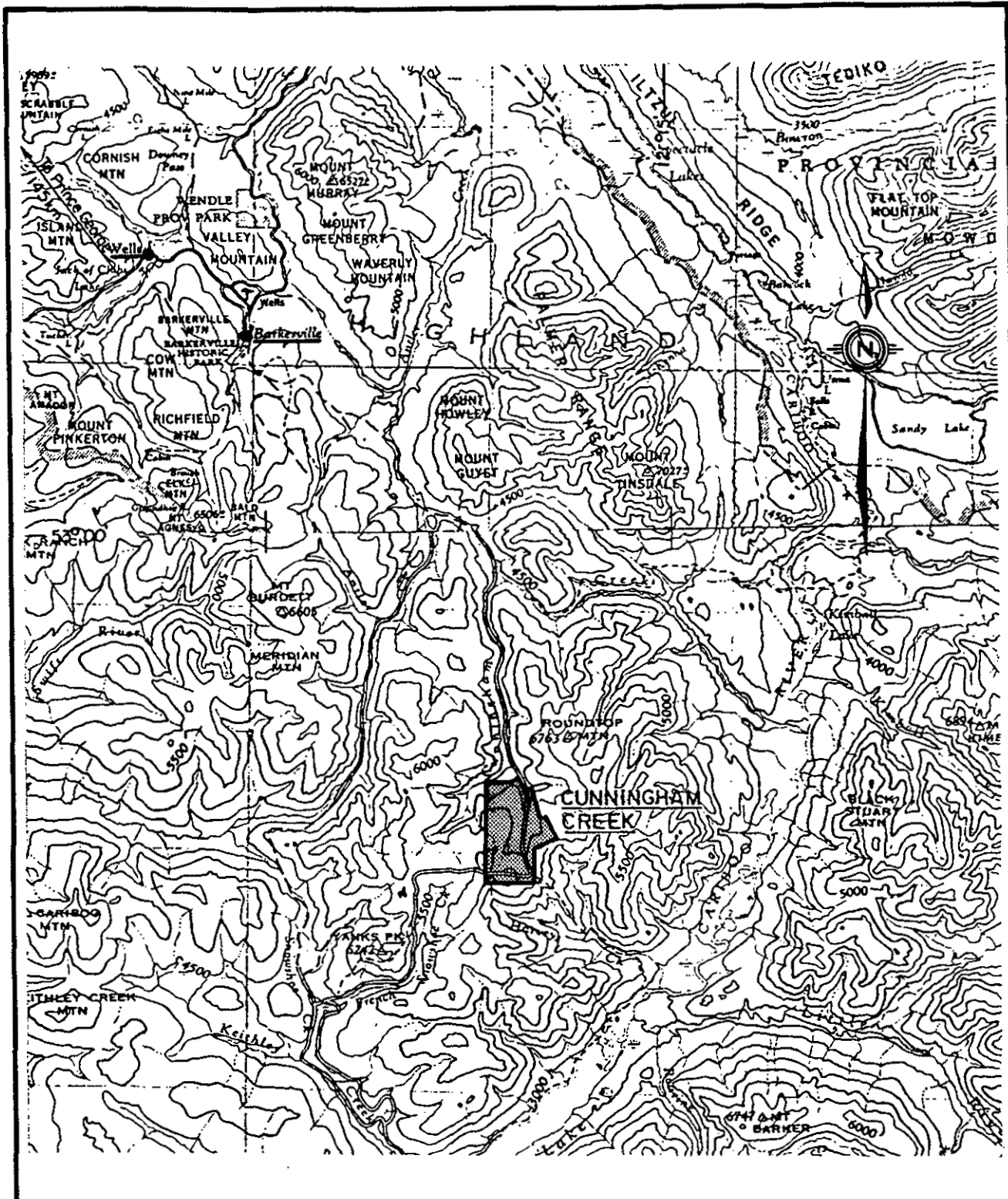
The property is easily accessible by 4-wheel drive vehicle. A well maintained forestry road (Line 3,100) branches off the Wells-Barkerville highway at the Bowron Lake turnoff; at km 17 a secondary road leads up Cunningham Creek past several placer operations to the old Hudson mine workings near the height of land. Further south the road is in poor repair; it eventually links up with logging roads near the town of Likely.

Base camp is located at the junction of Pearce and Peter Creek. Three sturdy wooden buildings provide adequate shelter. Creeks have an ample year round supply of water. All drill core is stored in camp. Although fuel, food and general supplies are available in Wells, a much better selection can be obtained in Quesnel, some 80 km to the west. The Quesnel airport has scheduled flights daily from Vancouver.

### 1.2 Physiography and Climate

The property lies within the transition zone between the rugged Cariboo Mountains to the east and the wooded Fraser Plateau to the west. The claims are centred on the Snowshoe Plateau at an average elevation of 1,370 m. Narrow stream valleys of Peter and Pearce Creeks flow north into Cunningham Creek. The headwaters of Harvey and Sinlock Creeks drain the southern portion of the claim and flow south into Cariboo Lake.





**CATHEDRAL GOLD CORPORATION  
CUNNINGHAM CREEK**

FIGURE 1 N.T.S. 93A, H

**LOCATION MAP**

CARIBOO MINING DIVISION, BRITISH COLUMBIA

km 5 0 5 10 km

SCALE: 1: 250,000

GEOLOGIST: P. DELANCEY

DATE: FEBRUARY, 1988

DRAWN BY: S. HAWORTH

The claims are near timberline, with open park-like meadows occurring at higher elevations. Outcrop is scarce except along creek gullies. Glacial till is common in valleys at lower elevations.

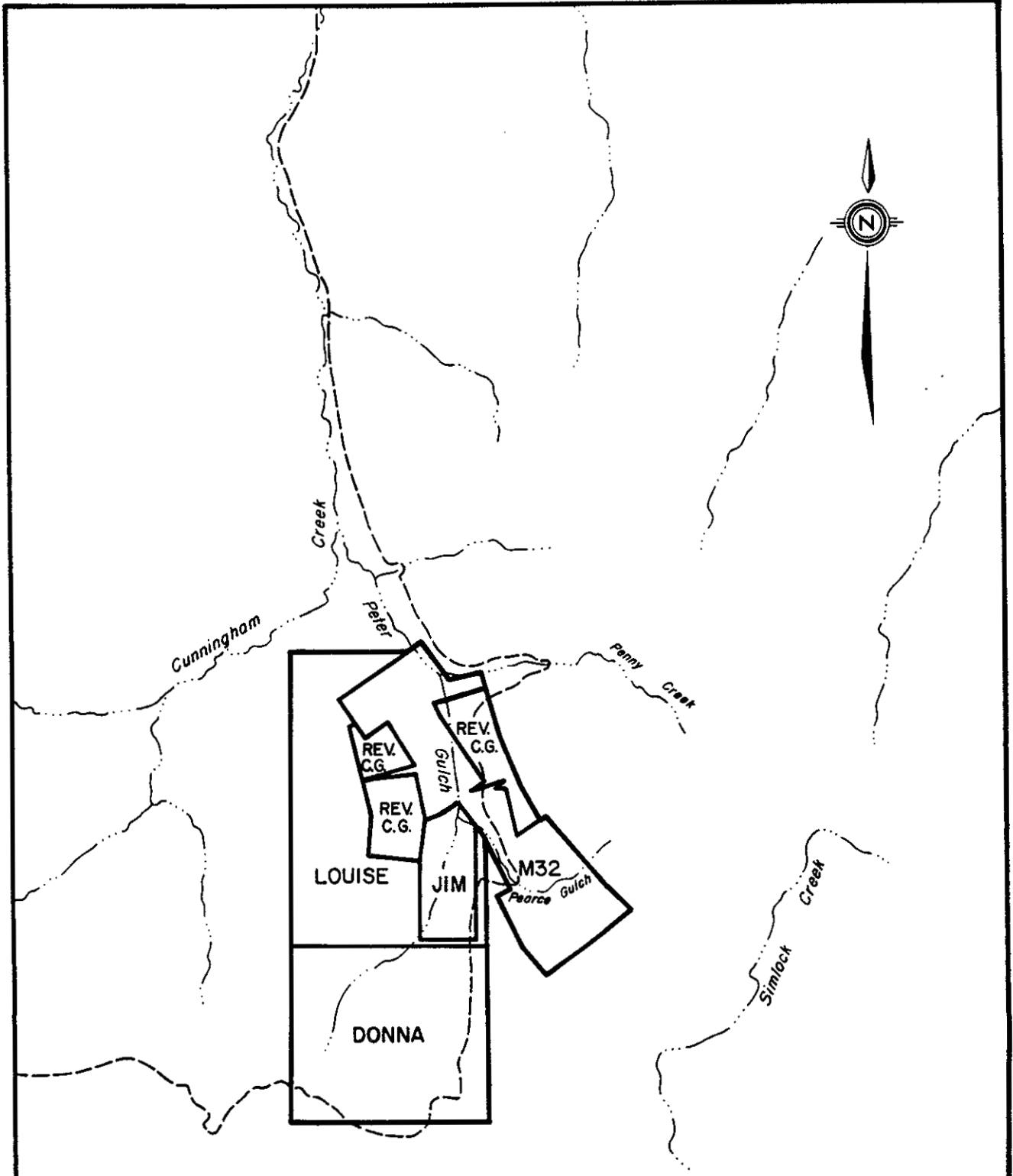
The climate is typically alpine with mild summers and cold winters. Snow accumulation is heavy; most areas are clear of snow by mid June.

### 1.3 Claim Status

The property is owned 100% by Cathedral Gold Corporation. The mineral claims and mineral lease comprising the Cunningham Creek property in the Cariboo Mining District are as follows:

<u>Claim Name</u>	<u>Record No.</u>	<u>Record Date</u>	<u>Expiry</u>
Mineral Lease M32	M32	Jan. 10, 1982	Jan. 10, 1989
Black Martin No. 1 & 2	1129	Aug. 14, 1979	Aug. 14, 1998
Black Martin No. 3 and Black Martin Fraction	1128	Aug. 14, 1979	Aug. 14, 1998
Sidewinder 1	4955	July 11, 1983	July 11, 1998
Sidewinder 2	4956	July 11, 1983	July 11, 1998
Sidewinder 3	4957	July 11, 1983	July 11, 1998
JIM (3 units)	251	Sept. 7, 1976	Sept. 7, 1998
Louise (20 units)	7871	Aug. 19, 1986	Aug. 19, 1998
Donna (12 units)	7955	Sept.18, 1986	Sept.18, 1998

The total area of the property is approximately 800 hectares (2,000 acres). Mineral Lease M32, comprised of 15 Crown Granted claims and fractions, require an annual rental payment of \$952.00. The Black Martin and Sidewinder Claims are reverted Crown Grants and require annual assessment of \$200 per claim. The Jim, Louise and Donna MGS claims, totalling 35 units, require annual assessment work of \$100 to \$200 per unit. All claims are grouped as the Cunningham Creek Group (Figure 2).



**CATHEDRAL GOLD CORPORATION**

**CUNNINGHAM CREEK**

FIGURE 2

N.T.S. 93A/14

**CLAIMS LOCATION MAP**

SCALE: 1:50 000

GEOLOGIST: R.D., M.B.

DATE: FEBRUARY, 1988

DRAWN BY: J. CORKUM

#### 1.4 History of Property

Placer mining has been carried out intermittantly on Cunningham Creek and its tributaries since the famous 1860's Cariboo Gold Rush. The close association of placer gold with seams of detrital pyrite and the presence of quartz crystals with some of the nuggets indicated a nearby source. However, it was not until the 1920's that lode gold was discovered at the head of Pearce Creek. Short adits were driven to explore the gold-bearing Hudson Vein. Full scale development did not commence until 1937 when Cariboo-Hudson Mines Ltd. acquired the property. The following year, 2,440 m of drifting and cross cutting was carried out on 6 levels, with most development on the 200' and 600' levels which were accessed from portals on the hillside. Much of this development work was done to investigate two adjacent veins - the Shasta and 605 Veins. Stoping was carried out on the Hudson Vein between the 250' level and surface. Some 12,938 tons of ore were mined from which 6,186 ounces of gold were recovered using a 100 tpd cyanide mill. The mine was closed in 1939, and in 1948 the mill was dismantled and sold. During the 1940's and 50's, intermittant exploration, including extensive bulldozer trenching, was carried out in the area of the Hudson, Shasta and 605 Veins. Tungsten mineralization was discovered near the junction of Peter and Pearce Creeks in the early 50's. Two adits were driven to test the extent of the tungsten mineralization. To facilitate this exploration several of the remaining Cariboo-Hudson buildings were moved to the junction of Peter and Pearce Creeks (present camp location).

In 1971, the claims reverted to the Crown and were acquired by Resourcex and TVI Mines Ltd. These companies carried out geological, geophysical and geochemical surveys in 1973 and 1976. Five holes were drilled in 1977 to test geochemical anomalies and exposed structures. Invex Resources, a predecessor company of Imperial Metals, acquired the property the following year and in 1979 tested the Shasta Vein with 3 diamond drill holes. Imperial Metals carried out a soil geochemical program in 1983 and continued testing of the Shasta Vein with 12 short holes. In 1984 a fairly major program of drilling, trenching, mine rehabilitation (200' level) and sampling was carried out. Drilling concentrated on the Shasta Vein; 32,000 tons of ore grading 0.36 oz/t were outlined. The 1986 drilling program indicated continuity of the Shasta Vein to a depth of at least 600' below surface. Two encouraging intersections were obtained along the southern extension of 605 Vein and newly discovered "replacement" sulphide body was tested with several short holes. Figure 3 summarizes the recent programs. On July 1, 1987 Imperial Metals Corporation assigned its interest in Cunningham Creek to Cathedral Gold Corporation.

FIGURE 3 - SUMMARY OF RECENT PROGRAMS

YEAR - COMPANY	SUMMARY OF ACTIVITIES	SUMMARY OF RESULTS	REFERENCE
1 9 7 3 - RESOURCEX	<u>Property reconnaissance</u> including soil sampling (310 samples), mag. and altimeter readings on 400' spacing, VLF on 100' interval	5 north - trending anomalous zones through central portion of lease: A - Pearce Creek, B - Hudson, C - Copper Creek, D - Southwest, E - Northeast	Allen, March 1974
1 9 7 6 - RESOURCEX	<u>Detailed soil geochemical surveys</u> (1,306 samples) and prospecting over the 5 anomalous areas outlined in 1973; VLF over grids A and B. Line spacing 100', station intervals 50'	Anomalous zones A, B, C and D confirmed. Co-incident high soils and EM on grid A Drill targets outlined	Allen, May 1977
1 9 7 7 - RESOURCEX	<u>Drilling</u> - 5 holes (totalling 1,512') on principal targets	#77-4 into Shasta Vein was encouraging 12.5' averaging 0.89 oz/t gold	Allen, October 1977
1 9 7 9 - INIVEX	<u>Drilling</u> - 5 holes (totalling 741') tested the Shasta Vein, geological mapping, some trenching	Encouraging results from Shasta Vein 79-1 1.70 m of 0.35 oz/t Au 79-2 0.75 m of 0.06 oz/t Au 79-5 1.50 m of 0.59 oz/t Au	Quinn, B. Sc. Thesis 1980
1 9 8 3 - IMPERIAL	<u>Detail soil geochemical surveys</u> (2,500 samples) covering main mineral occurrence areas. <u>Drilling</u> - 12 holes (totalling 510 m) Shasta Vein	Geochem results indicate drill targets. <u>Drilling</u> Shasta Vein outlined 33,000 tons of 0.39 oz/t Au.	Quinn, December 1983 February 1984
1 9 8 4 - IMPERIAL	<u>Drilling</u> - 16 holes Shasta Vein, 5 holes 605 Vein, 3 holes IP target (totalling 1,132 m) Underground Rehabilitation and sampling 200' level, soil surveys (fill-in and extensions, 711 samples) Extensive trenching showing areas IP over south grid area	Drilling and underground sampling of Shasta Vein generally confirms indicated tonnage and grade, shows erratic nature of mineralization (i.e., ore shoots)	Quinn, August 1984
1 9 8 6 - IMPERIAL	<u>Drilling</u> (totalling 2,327 m) 5 holes to test Shasta Vein below 200' level 5 holes to test IP target area 6 holes to test newly discovered "replacement" zone 2 holes to test S. extension of 605 Vein	Shasta Vein - 7 of 9 holes intersect vein, 2 of these holes intersected ore shoots. I.P. target probably due to graphite "Replacement" body - drilling intersects massive sulphide mineralization, low gold values. Extension of 605 - 0.8 oz/t Au over 2.5m.	Delancey, July 1987
1 9 8 7 - CATHEDRAL	<u>Property Mapping, mag survey</u> soil extensions, <u>rock sampling</u> . <u>Drilling</u> (totalling 1,098 m) 4 holes to test south extension of 605 Vein 2 holes to test anomalous chlorite schist 4 holes to test mag indicated "replacement" targets 1 hole to test Moneta Showing 1 hole to test N extension of Cariboo-Hudson	Several new gold bearing veins discovered, one with visible gold, copper etc. assayed 20 oz/t Au. Drilling indicates the zones are lensey. Detailed mag indicates sulphide or magnetite bodies in limestone, but drilling failed to intersect these bodies. 605 vein extension appears to pinch and swell with erratic gold values.	Delancey, Feb. 1988

### 1.5 Regional Geology

Recent work by Struik of the G.S.C. indicates the geology of south central British Columbia to be composed of four fault separated terranes; from west to east they are, Quesnel, Slide Mtn., Barkerville and Cariboo. The general Wells - Barkerville map area lies within Barkerville terrane and is underlain by a thick package of highly deformed metasedimentary rocks generally referred to as the Snowshoe Group. Age and correlation of rock units within this package is uncertain.

The Wells-Barkerville-Cunningham Creek area is underlain by a north west trending belt of clastic rocks (Snowshoe Group) of the Barkerville Terrane. Further to the east, these rocks are in fault contact with black clastic rocks of the Cariboo Terrane. The immediate Wells - Barkerville - Cunningham Creek mineral properties lie within the Downey Creek formation (Mississippian age?) of phyllites, slates, micaceous quartzites, limestones, marble and green meta-tuffs.

Regionally, the Snowshoe Group rocks have been folded into the Lightning Creek anticlinorium which trends northwest and plunges about 20 degrees north west.

### 1.6 Geology Of The Wells' Gold Deposits

The Mosquito Creek, Island Mountain and Cariboo Gold Quartz deposits at Wells have a recorded production of some 3 million tons grading 0.40 oz/t gold. The gold occurs with pyrite as "replacement" ore bodies and as quartz vein ore bodies, they occur near the contact between sericitic phyllites/limestones (Baker Member) and micaceous quartzites (Rainbow Member). The "replacement" deposits are shallowly plunging pencil shaped bodies in folded limestone. The vein deposits occur as steeply dipping quartz/pyrite filled faults in micaceous quartzites and argillites (Figure 4).

Several theories have been advanced as to the origin of the deposits. One theory suggests that gold-bearing hydrothermal fluids penetrated fractured and folded strata, precipitating quartz and pyrite in the fractures (quartz vein feeders) and "replacing" chemically reactive limestone beds. Some geologists question the "replacement" origin of the massive pyrite bodies, alternatively suggesting them to be of syngenetic origin.

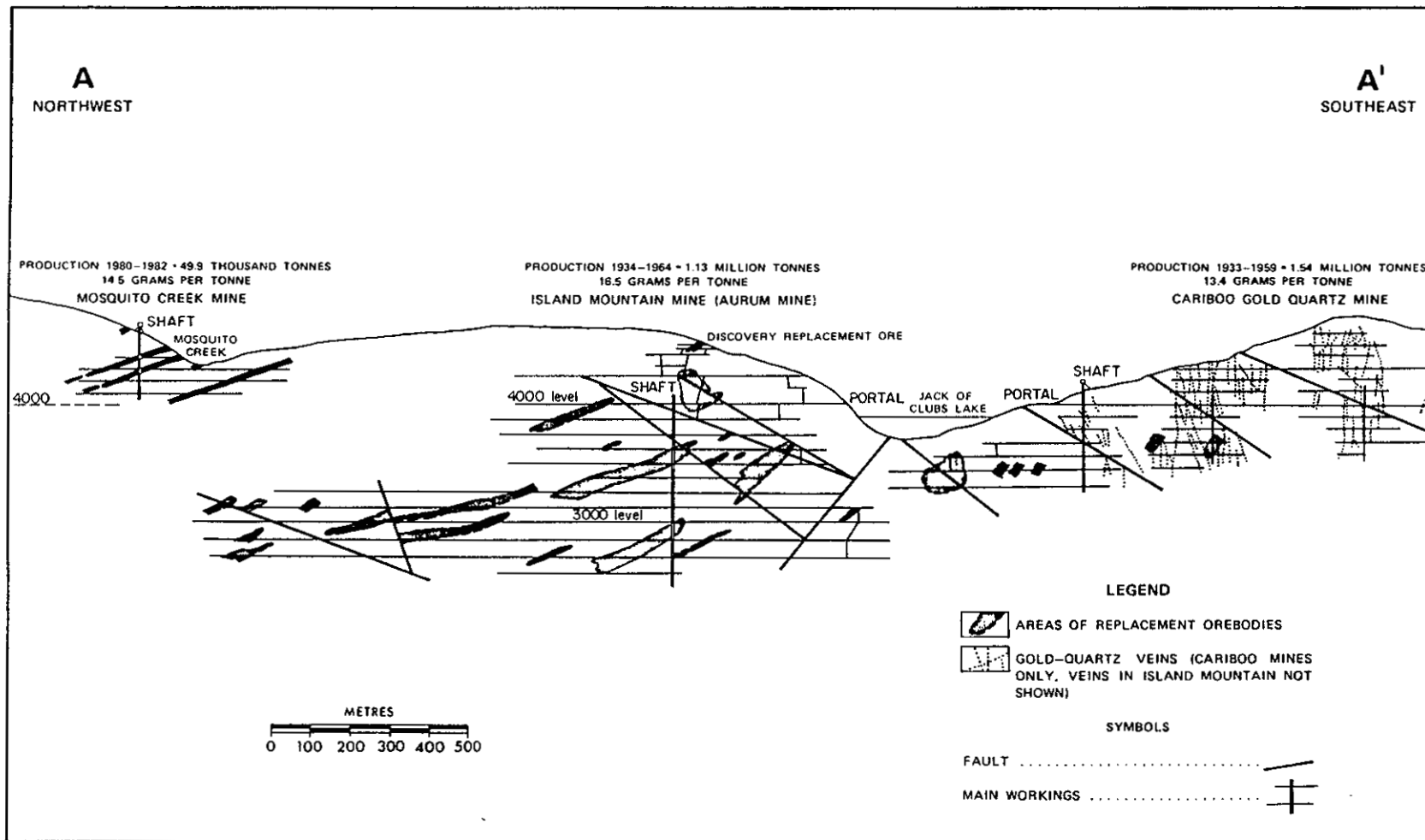


Figure 4. Longitudinal section. Projections of Mosquito Creek, Island Mountain, and Cariboo Gold Quartz mines (From D.J. Aldrick, Paper 1983-1, Ministry of Mines, B.C.)

Mosquito Creek Gold Mining Company is presently mining a limited tonnage of "replacement" type ore and stockpiling it for processing in their 100 ton per day cyanide plant. Geological exploration of the property is continuing and old data is being reevaluated to try to get a better understanding of the geological framework for the location of the ore bodies.

#### 1.7 Summary of Work Done in 1987

The first phase of the 1987 program included:

1. Property mapping of a scale of 1:1,000.
2. Fill-in and extension of soil grids (940 samples).
3. Prospecting and sampling areas of old workings, anomalously high soil samples, geophysical anomalies, or quartz vein/float occurrences, total 356 rock samples.
4. Detailed mag surveys over limestone stratigraphy favourable for "replacement" targets.

The second phase of exploration included twelve NQ drill holes totalling 1098 m. Four holes totalling 487 m tested the southern extension of the 605 Vein; four short holes totalling 176 m tested mag anomalies within the limestone sequence; two holes tested a gold bearing chlorite schist immediately west of the Shata Vein; one hole tested an auriferous galena/quartz vein along the north extension of the Cariboo-Hudson Vein and one hole tested the Moneta Showing (Figure 6). Most exploration was within the M32 Mining Lease.



## 2.0 PROPERTY GEOLOGY

### 2.1 Introduction

Property mapping was mostly carried out at a scale of 1:1000, using grid lines for control (Figures 9, 10, 11, 12). The data was transferred to a 1:5000 scale for presentation purposes (Figure 5).

### 2.2 Lithology

The claim area is underlain by a northwest trending belt of quartzites, sericitic quartzites, sericitic schists, limestones and chlorite schists of the Snowshoe Group. The rock units are frequently intercalated and contacts are often gradational.

Quartzites, sericitic quartzites, sericitic schists: The quartzites are generally massive, light to medium tan grey in colour. The size of the grains is generally less than 2mm; local beds may have grains up to "pea" size. Opalescent pale blue grains are noted locally. Graded bedding or cross bedding is generally indistinct, if present at all. Sericitic quartzite is most common and is frequently gradational to quartzite and sericitic schist. The rocks frequently contain sufficient amounts of ankerite and disseminated pyrite to impart a reddish brown colouration. These rocks are most prominent on the east half of the property and are host to the gold bearing quartz veins.

Limestones, argillites, phyllites, chlorite schists: These lithologies are frequently intercalated. The limestones vary from light grey to black; locally the limestones have sufficient ankerite to weather a buff reddish brown. The unit is relatively continuous and is approximately 400m thick. The argillites are frequently graphitic, particularly where disrupted by faulting. Locally the limestone contains lenses or pods of massive pyrite, pyrrhotite, galena and sphalerite; gold and/or silver accompanies these sulphides locally. Poddy quartz veins, locally containing high gold/silver values cut this limestone sequence.

Chlorite Schists-Meta Tuffs: These rocks are exposed on the west side of the property. Locally these rocks contain disseminations of magnetite. They are probably of volcanic origin. Their relation to the chlorite schists interbedded within the limestone sequence is uncertain.

Diorites: These are the only intrusive rocks in the area. Because of their ankerite content, they weather a buff brown and are sometimes difficult to discern from quartzite outcrops. Their massive, locally cross-cutting nature is evident in creek exposures.

### 2.3 Structure

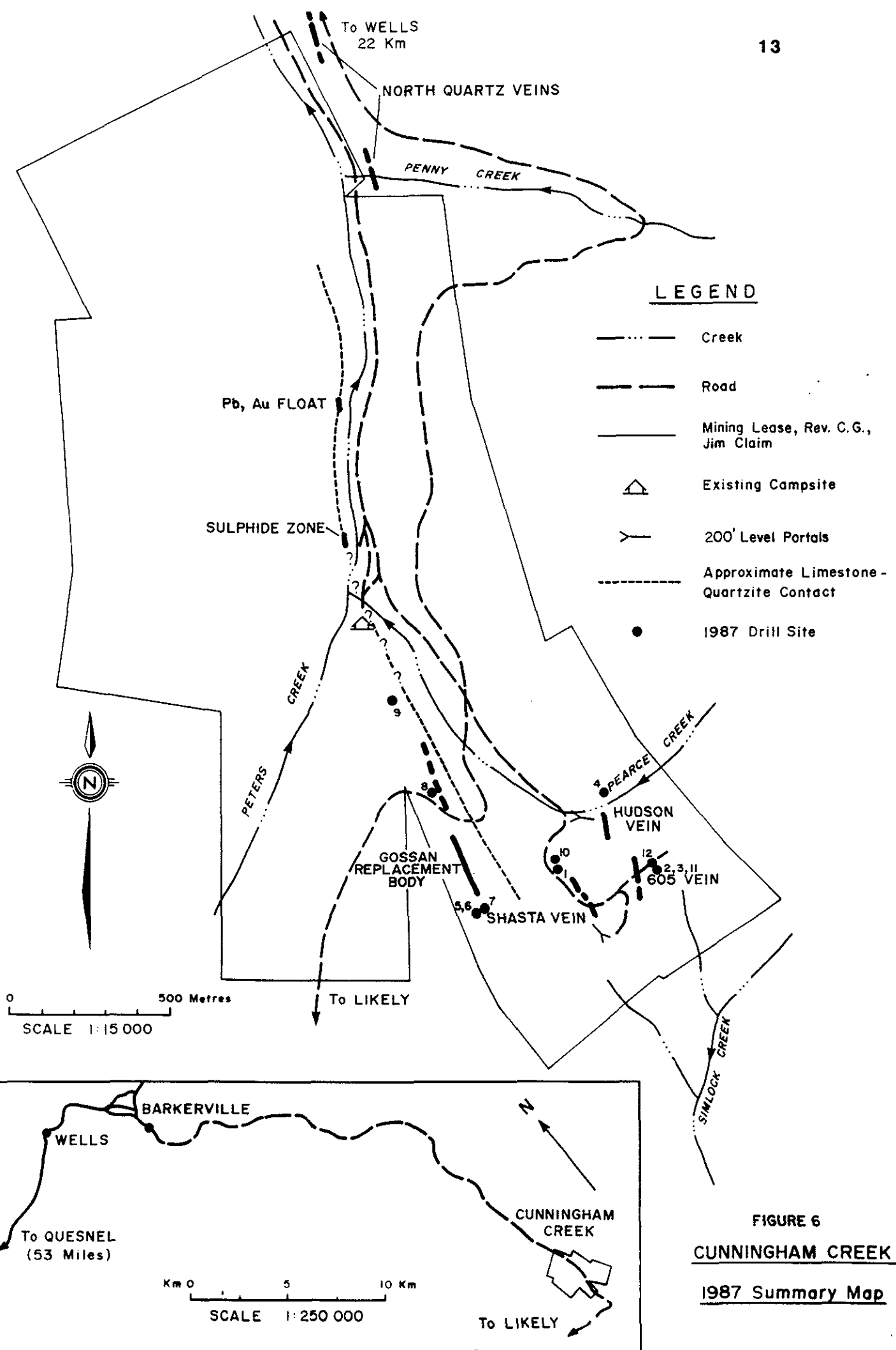
The rocks have a northwest strike of approximately Az. 320° and a dip of 70° to 80° northeast. Regional mapping by government geologists indicates the rocks are isoclinally folded. Foliation, crenulations, and local "kink" or isoclinal folding, and lensing of units, attest to strong structural deformation. Foliation is generally at a slight angle to bedding. Faulting is common. Previous mapping indicated a major fault (Copper Creek fault) cutting across the property. Although no direct evidence was seen for this fault, rock units appear to be slightly offset along this presumed structure. Quartz veins occupy various fracture systems, several veins show evidence of movement along the walls.

## 3. MINERALIZATION

### 3.1 Introduction

The Cunningham Creek property is well mineralized. The most promising showings occur within a belt of quartzite, limestone and argillites trending NNW through the centre of the mining lease. Several types of mineralization are recognized, gold bearing quartz veins are the most prominent. "Replacement" type mineralization is less recognized to date, but is the most important type in the gold mines at Wells. Significant amounts of tungsten mineralization (scheelite) occurs in quartz veins near the junction of Pearce & Peter Creeks.

A 1987 Summary Map showing the location of the more significant gold mineralization, is presented on the following page (Figure 6).



**FIGURE 6**  
**CUNNINGHAM CREEK**  
**1987 Summary Map**

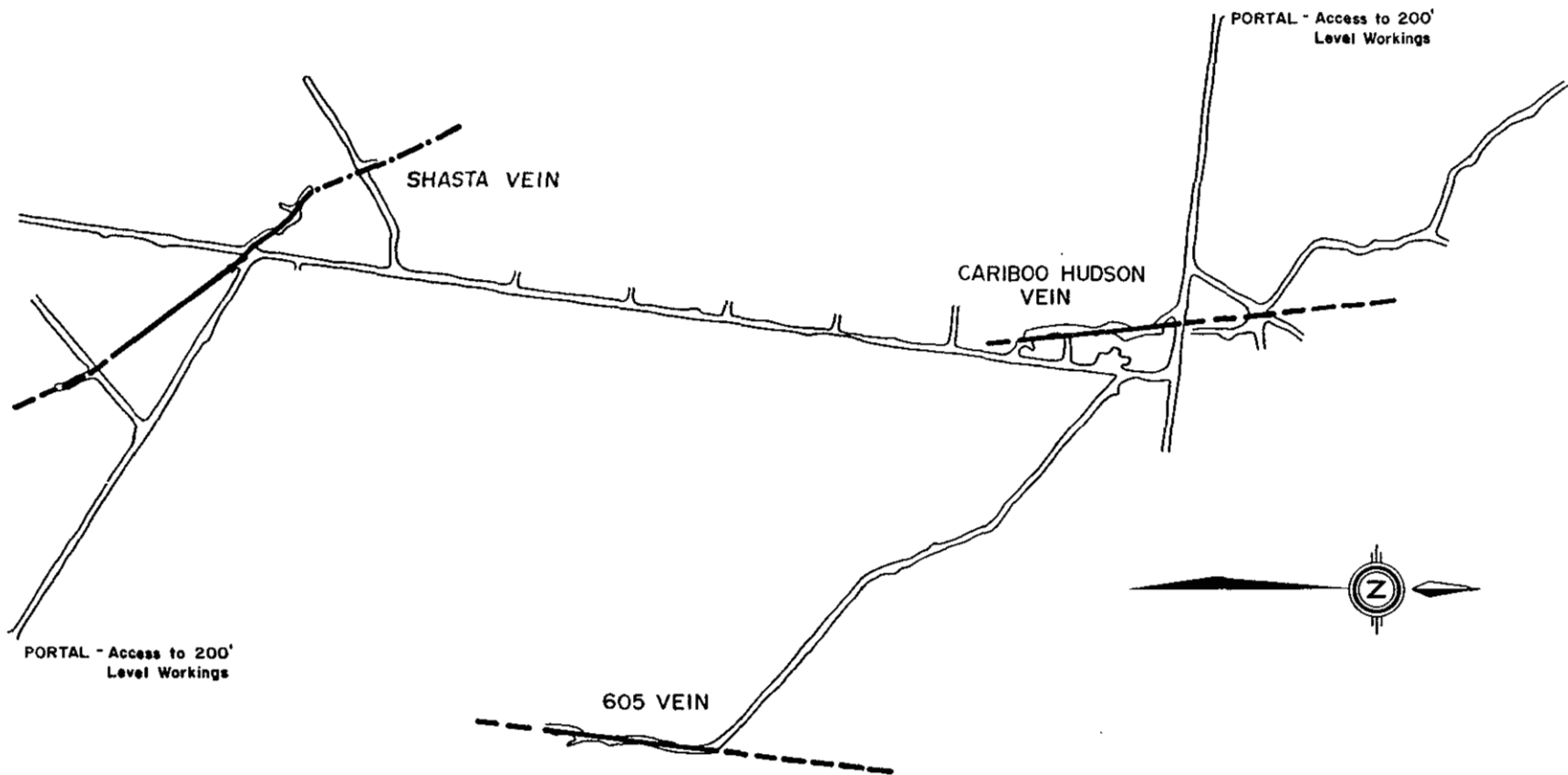
### 3.2 Quartz Veins

Quartz veins are most conspicuous and have been the principal target for gold exploration. The veins range from a few centimeters to few meters wide and from a few meters to several hundreds of meters long. The strike of the veins fall in three main classes - north, northeast and east; veins striking northwesterly along foliation are generally less persistent. The north trending veins are most productive for gold mineralization. These veins, including the Shasta, Hudson and 605 Vein, occupy faults or shears which dip steeply to the east. Branching, splaying, pinching & swelling of the veins are common. These quartz veins are best developed in the more brittle quartzites.

The vein quartz is massive, milky white. Crystal-lined vugs and comb texture indicate relatively open fracture deposition. Ankerite is a common gangue mineral, frequently occurring along the vein walls. Sulphide content of the vein is variable. Pyrite, and less commonly sphalerite, galena and chalcopyrite, occur as irregular masses, bands and disseminations. Pyrite is usually coarsely crystalline and is frequently leached out on surface exposures. Gold mineralization appears to be intimately associated with the sulphides, and a general correlation is noted between the sulphide content and gold content of the vein. Gold bearing ore shoots are associated with concentrations of sulphides within the vein system. The geometry of these steeply plunging shoots is often controlled by the intersection of structures.

### 3.3 Shasta Vein

In 1938 underground exploration workings on the Cariboo Hudson mine were carried through to Simlock Creek to investigate the Shasta Vein, some 150 meters to the west (Figure 7). Interest in the potential of the Shasta Vein was renewed in 1978 when an exploration hole intersected 13 feet averaging 0.89 oz/t Au. Subsequent exploration drilling in 1979, 1983, 1984 and 1986 focused on this vein (see Summary, Figure 3). Approximately 32,000 tons of 0.37 oz/t gold were outlined above the 200' level (S. Quinn 1984); and continuity of the vein was established to 600' below surface. The vein is exposed discontinuously over a strike length of 250 m and dips steeply to the east. The width is extremely variable from less than 0.5 meters to 4.0 meters. The grade of mineralization is equally erratic with the best values accompanying concentrations of sulphide along steeply plunging ore shoots. Trench S-2 exposes a wide lense of quartz with good gold values accompanying concentrations of galena and pyrite. The zone probably extends to the 200 foot level where the workings expose a sulphide-quartz lense. A portion of this ore lens has been displaced some 10 meters by a steeply dipping fault. Some of the better drill intersections appear to have penetrated this shoot.



**LEGEND**

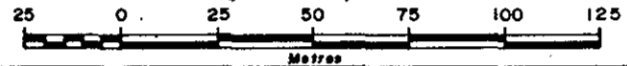
- Intersected Vein: Drilling and Workings
- · - · - Projected Vein: Partially Drilled

**CATHEDRAL GOLD CORPORATION  
CUNNINGHAM CREEK**

FIGURE 7 N.T.S. 93A/14

**200' LEVEL PLAN**

Cariboo Mining Division, British Columbia



SCALE: 1:2000	GEOLOGIST: P. DELANCEY
DATE: FEBRUARY, 1988	DRAWN BY: S. HAWORTH

### 3.4 Hudson Vein

The Hudson Vein strikes approximately N-S and dips approximately 85° to the east. The vein averages 2 to 2.5 m wide and is continuous for approximately 75m before it horsetails, with veins running parallel to foliation. Ore shoots and pods are characterized by irregular masses and bands of sulphides, chiefly pyrite, pyrrhotite and locally sphalerite and galena. In 1938 the vein was extensively explored on four levels down to 600'. Mining was carried out from the 250' level to surface; 12,938 tons of ore were extracted, from which 5,186 oz of gold were recovered before the mine closed in 1939.

### 3.5 605 Vein

The 605 vein lies east of the Hudson and Shasta Veins. The Vein was explored in 1938 by extending the 200' & 600' levels from the Carriboo - Hudson workings. Sampling on the 200' level, at that time, averaged 0.25oz/t Au over 150' drift length. Five drill holes tested the 605 vein during the 1983-84 programs and another two holes, in 1986, tested the south extension. Results are particularly encouraging along the southern extension; DDH 86-20 cut 2.5 meters of quartz/sulphide vein grading 0.8 oz/t Au. 1987 drill testing of this southern extension indicates the vein pinches and swells (two intersections of 5m); best intersection was 0.1 oz/t over 0.4m.

### 3.6 Other Quartz Veins

Numerous other quartz veins transect the area. In the past sampling of veins has been somewhat random and less than thorough. Most veins are barren of mineralization. Anomalously high gold values were obtained from several "newly discovered" veins and other gold bearing veins are suspected in areas of high gold soil anomalies.

A local concentration of pyrite and chalcopyrite was found in lensy quartz veins cutting chlorite schist immediately west of the north end of the Shasta Vein. Assays returned high grade gold values up to 20 oz/t. Subsequent examination indicated considerable visible gold, and some native copper. Drill testing (holes 87-1, 87-10) of this anomalous zone of chlorite schists indicated several sections of  $\pm 0.1$  oz/t Au. (see Figures 19 and 25).

A ± 1m wide quartz vein is exposed in Peters Creek between lines 12+00W and 12+50W. The quartz vein contains banded quartz and pyrite. A grab sample ran 40,900ppb Au (1.2 oz/t). Other grab samples in the same general area are also anomalous. Host rocks are limestones and sericite schists. A drill site was prepared to test this vein but winter conditions prevented completion of the program.

An extensive quartz vein system (Hill Vein) is exposed along the eastern boundary of the claims. The vein is poorly exposed but is well outlined by a soil anomaly. Values up to 3750 ppb Au have been obtained from grab samples. Although a drilling site was spotted, no drill testing of the vein was carried out during the 1987 program.

A quartz vein with local pyrite is exposed in a tributary of Simlock Creek immediately southeast of the 605 Vein; highest gold value is 3485 ppb. Steep topography prevents easy drill testing of this target.

A system of north trending quartz veins with local concentrations of fine banded pyrite are exposed along the north boundary of the property. These veins include two veins previously explored by short adits. Selective samples have values averaging 1.8 oz/t Au.

### 3.7 "Replacement" Type Mineralization

It was not until 1983 that the potential for discovery of "replacement" type gold deposits on the property was recognized. This is the most important type of mineralization at the Island Mt. and Mosquito Creek Mines near Wells. This "replacement" mineralization tends to be high grade (0.7 oz/t Au) and occurs as shallowly plunging pencil-shaped masses of pyrite in limestone (Figure 4). The so-called "sulphide and "IP" showings on the Cunningham property occur within a limestone/argillite unit just north of the junction of Pearce and Peter Creeks. These mineral occurrences are characterized by small pods and irregular masses of pyrrhotite, pyrite and/or galena. High but erratic gold and/or silver values accompany the sulphides. Results suggested the IP anomaly to be due to graphite. North of the Cunningham Claims, similar silver-bearing galena pods have been the target of extensive trenching and drilling (Chaput's Claims).

During the 1986 program, massive gossanous, iron oxide float and outcrop was discovered adjacent to a limestone unit in a narrow north-trending valley west of the Shasta Vein. Samples gave anomalously high gold values up to 4,700 ppb; results from further detail rock sampling in 1987 also were highly anomalous. Drill testing with short holes, (86-14 to 19), proved difficult because the body apparently plunges shallowly northward along topography. However, DDH 86-15 and 16, intersected several feet of semi-massive, weakly banded pyrite and lesser pyrrhotite. Assays results were discouraging. The similarity of this "replacement" body to those of the Wells deposits is striking, and although the lack of gold in this occurrence is disconcerting, the discovery highlights the potential for significant sized replacement bodies on the limestone horizon.

In 1987 detailed magnetometer survey over this body gave a very distinct mag anomaly. Expansion of the survey in other areas where mapping indicated favourable host rocks and alteration, indicated similar anomalies. Several of these targets were tested by shallow drilling; the holes failed to intersect the desired target.

#### 4.0 DRILLING

Drilling programs were conducted in 1977, 1979, 1983, 1984 and 1986 and 1987 totalled 461 m, 726 m, 510 m, 1,132 m, 7,632' and 1,098.4m respectively. Previous drilling focused on exploration of the Shasta Vein. A 1987 drilling summary is presented in Figure 8.

The 1987 drilling was contracted to Paragon Drilling of Kamloops. A Longyear 38 was mobilized to the property on October 14 and demobilized on December 2, 1987.

All core (NQ) for the 1987 program was photographed and logged (Appendix A). Selected intervals, usually with visible sulphides, were split or sawed and sent to Acme Analytical Labs in Vancouver or geochemical analyses. The geochemical certificates are presented in Appendix B. The 1987 drill core is stored in core racks at camp; core from previous drilling is organized and stored in a shelter at camp.



FIGURE 8 - 1987 CUNNINGHAM CREEK DRILLING SUMMARY

HOLE #	COORDINATES	ELEVATION	ATTITUDE	LENGTH	OBJECTIVE	RESULTS			
						From	To	Length	Au ppb
01	2+10E, 1+80S	1715	-45°/261°	175.9	To test at shallow depth quartz veins and pods (up to 20 oz/t Au) in anomalous schists. To intersect source of high mag anomaly in limestones.	16.2 53.6 60.4	18.3  60.9	2.1  0.5	5,390 8,610 1,680
02	4+40E, 1+45N	1740	-43°/271°	93.6	To test 605 vein close to 200' level.	56.3  57.2	61.3  57.6	5.0  0.4	Quartz vein +/- sulphides 3,420
03	4+40E, 0+45N	1740	-60°/225°	149.0	To test 605 vein close to 400' level.	127.8	128.1	0.3	1,440
04	1+45E, 1+30N	1710	-45°/274°	81.4	To test a a shallow depth gold bearing galena quartz vein at north extension of Cariboo Hudson.	No significant values			
05	1+90E, 3+88S	1715	-45°/088°	96.6	To intersect mag anomaly in limestones at a shallow depth.	No significant values			
06	1+90E, 3+88S	1715	-45°/203°	31.1	To test depth extent of sphalerite bands exposed in limestone.	No significant values			
07	2+27E, 3+46S	1715	-45°/273°	32.6	To test mag anomaly in limestone at shallow depth.	No significant values			
08	2+35W, 2+35S	1700?	-45°/190°	16.0	To test mag anomaly in limestone at shallow depth.	No significant values			
09	5+05W, 1+75S	1600	-44°/042°	81.4	To test favourable stratigraphy and galena showing in Moneto area.	Intersected galena but no significant Au values.			
10	1+87E, 1+442S	1715	-45°/285°	96.6	To test chlorite schist which hosts high-grade gold on surface.	34.65	35.15	0.50	4,450
11	4+40E, 0+45N	1740	-53°/241°	131.4	To test 605 vein.	108.5	110.3	1.8	620
12	4+00E, 0+38N	1745	-45°/270°	112.8	To test 605 vein.	26.1  26.1	31.8  27.7	5.7  1.6	Quartz vein +/- sulphides 535

Cross-sections (1:500) for each hole are presented in Figures 19 to 25 (in pocket). Correlation of geology with surface and other holes on the same section is difficult. Major quartz vein intersections, such as the 605 Vein, could generally be correlated from hole to hole but correlation of narrower veins is difficult, if not impossible.

Coordinates of drill holes were measured by chain and compass from grid stations. The position of grid lines and stations is approximate. Elevations of drill collars were approximated from the orthophoto base. A survey tying in all drill hole collars is recommended - particularly if one is attempting to test the projection of specific targets such as plunging ore shoots. A single-shot Sperry-Sun survey was taken at the bottom of each hole. Holes flatten an average of 1° per 100 feet. Core recovery was generally good; drill bit consumption was high.

## 5.0 GEOCHEMISTRY

Several generations of geochemical soil surveys have been carried out over different grids, using various line spacings and sample interval spacings. Samples from the initial programs were not analyzed for gold.

The 1987 program included fill-in line sampling and extension of some grids. Samples were collected at 10m spacing with lines ranging between 25 and 100 meters apart. Some 940 soil samples were collected and analyzed in 1987. Samples of the B horizon were taken, where possible, at a depth of approximately 20-30cm. They were then shipped to Acme Analytical Labs in Vancouver for 30 element ICP and Au by A.A. analyses. Results of the 1984, 1986 and 1987 sampling program for the various grids are presented in Figures 13 to 16. The 1987 geochemical analyses are presented in Appendix B.

Previous sample and line spacing was too large, given the lack of significant lateral dispersion and the width of the target sought (approximately 1m). A minimum sample spacing of 10m and line spacing no greater than 25m is recommended. Although other metals such as lead, zinc and silver can locally be good indicator elements; gold analysis is by far the best indicator for gold mineralization.

Soil geochemistry appears to be a reliable and useful exploration tool in the Cunningham Creek area. Superficial cover is generally less than 2m. Soil development is moderate and dispersion restricted. Contamination from previous exploration and mining activities is recognized and is especially a problem in creek valleys that were worked for placer gold.

Prospecting and rock sampling was particularly successful in discovery of new showings. A total of 356 rock samples were collected, their location is indicated on the 1:1,000 Geology and Geochemistry Maps; anomalous values are indicated. Geological analyses are included in Appendix B.

## 6.0 GEOPHYSICS

Significant amounts of pyrrhotite and magnetite were noted in the "replacement target" sulphide intersections in 1986. In 1987 a limited magnetometer survey over the immediate gossanous sulphide body indicate a discrete, elongate mag anomaly reflecting the sulphides and magnetite. Further surveys were carried out on specific grid lines within the favourable limestone package. The work was contracted to a geophysical operator Brian Mullion, using a Scintrex MP 2 instrument. Approximately 9.2 line km were surveyed at a 10 meter station spacing. Although diurnal corrections were made for each survey, no corrections were made between individual surveys. Individual survey results are contoured and presented in Figures 18a to 18f. A summary map showing mag high and lows is presented in Figure 17. Several of the mag anomalies were tested by shallow drilling; results were negative in that no explanation for the anomalies could be seen in the drill core.

## 7.0 DISCUSSION

Several points not apparent or sufficiently emphasized in previous reports are:

- (a) The Cunningham Creek property shows such striking similarities to the deposits at Wells that these better-studied deposits can be used as a "model" to guide exploration at Cunningham Creek.

- (b) None of the veins or "replacement" deposits at Wells would be economic, except for their close spacial distribution. The average cross section of a replacement deposit is 10 square meters; the average dimension of a quartz vein ore shoot is 1.5m x 40m x 30m. Basically, these 2 to 7 thousand ton bodies, are the exploration targets. Exploration at Cunningham Creek must be directed at the discovery and general verification of several mineralized vein/replacement bodies. Encouragingly enough there appears to be several potential quartz veins in the Shasta-Hudson area which have not been adequately tested, or previously recognized. Those that show considerable potential are the 605 Vein(s) and the 635 Vein encountered in the old underground workings, and the Hill and Simlock Creek veins recently recognized on surface. Other, poorly explored veins at the north end of the property show high gold values, (averaging better than .5 oz/t) associated with finely banded pyrite.
- (c) Replacement deposits at Wells are a more attractive target than the vein deposits. There is good reason to believe that the Cunningham property has gold bearing replacement deposits yet to be discovered. The stratigraphy, lithology and setting is very similar to that hosting the Wells "replacement" deposits. Several massive "replacement" deposits containing variable amounts of galena, pyrite, pyrrhotite and magnetite, have been found along the favourable stratigraphy, however no significant "replacement" type gold mineralization has been discovered to date. The sulphides intersected in drilling the auriferous gossanous replacement body discovered in 1986, are typical of the barren bottom on fringes of "replacement deposits. The geometry suggests that this was a large pencil-shaped pyrite-pyrrhotite replacement body which has been mostly eroded. Other indications of yet undiscovered "replacement" mineralization are the presence of typical "halo" signatures such as galena and sphalerite mineralization, mariposite, silicification and ankeritization, together with local elongate magnetite highs presumably reflecting pyrrhotite or magnetite mineralization at depth.
- (d) Where as most of the gold mineralization at Wells is associated with fine grained pyrite, gold mineralization at Cunningham Creek is frequently associated with galena. Active placer workings down drainage show a close association of gold and galena and interestingly enough a spacial association with limestone gravel

lenses. Unfortunately, the galena-gold association is erratic with some galena-quartz veins containing high amount of gold while others are barren; others have high silver values. The relationship between mineralized quartz veins and adjacent "replacement" mineralization is uncertain.

The difficulty in locating quartz-vein ore shoots and/or replacement deposits cannot be overstressed. Detail mapping of the showing areas (including underground) is lacking. Without detailed structural measurement and knowledge of the character of the mineralization, projections and correlation of ore intercepts is difficult and uncertain. Some geological data and assay results is available from old reports; this data must be examined, compiled and integrated with recent exploration data.

Although significant tonnage has been outlined in previous drilling, evaluation of the potential of all gold bearing veins and "replacement" bodies in the immediate area is required before any serious mining developments are considered.

## 8.0 CONCLUSION

The Cunningham Creek property is located along the same belt of rocks hosting the gold deposits at Wells. The immediate geological setting and character of the mineralization is strikingly similar. The overall potential of the Hudson, Shasta and 605 Vein systems is not unlike that of the Cariboo Gold Quartz Mine at Wells, where some 1.5 million tons of 0.4 oz/t gold was mined. The discovery of a "replacement" type sulphides along a favourable limestone unit underlines the potential for "replacement" mineralization similar to that of the Island Mountain and Mosquito Creek deposits where some 1.13 million tons of 0.5 oz/t gold was mined.

## 9.0 RECOMMENDATIONS

The property warrants further exploration. Work should include compilation of all data, a survey of old workings, drill holes, etc., underground rehabilitation and sampling of veins on the 600' level and a minimum of 2000m of drilling to test gold bearing quartz/sulphide veins and "replacement" targets.

10.0

ITEMIZED COST STATEMENT FOR 1987

DATES

August 20 through December 2, 1987.

WAGES

Senior Geologist 82 days at \$265.00/day = \$21,730.00  
Geologist 83 days at \$125.00/day = \$10,375.00  
Geologist 13 days at \$200.00/day = \$ 2,600.00  
Field Assistant 54 days at \$125.00/day = \$ 6,750.00

\$ 41,455.00

MEALS

147 man days at \$30.00/man day =

\$ 4,410.00

TRANSPORTATION

4 months truck rental at \$1,000.00/month = \$ 4,000.00  
Airfare = \$ 2,000.00

\$ 6,000.00

GEOCHEM  
AND ASSAY

128 core samples 30 element ICP  
+ Au at \$13.25 = \$ 1,696.00  
356 rock samples 30 element ICP  
+ Au at \$13.00 = \$ 4,717.00  
940 soil samples 30 element ICP  
+ Au at \$10.00 \$10,340.00

\$ 16,753.00

EQUIPMENT

=

\$ 3,640.00

GEOPHYSICS

9.1 km of proton mag

=

\$ 909.00

DRILLING

1098.4 m NQ drilling  
(includes: Total direct and indirect charges  
camp construction, maintenance and 85 man days  
meals for geological personnel).

\$135,967.00

REPORT  
PREPARATION

Drafting 200 hours at \$15.00/hour = \$ 1,500.00  
Reports = \$ 1,000.00

\$ 2,500.00

TOTAL:

\$211,634.00

11.0

STATEMENT OF QUALIFICATIONS

I, PETER ROSS DELANCEY, of 1748 Dunbar Street, Vancouver, B.C. do hereby certify that:

1. I am a Senior Geologist employed by Imperial Metals Corporation Suite 800 - 601 West Hastings Street, Vancouver, B.C.
2. I have been practising my profession as an exploration geologist since 1967, and have been involved in mining exploration in British Columbia for 17 years.
3. I am a Professional Engineer registered with the Professional Engineering Association of British Columbia.
4. I am a Fellow of The Geological Association of Canada.
5. I obtained my Master of Science Degree from The University of Manitoba, Winnipeg, Manitoba in 1967.

  
Peter R. Delancey

FEBRUARY 1988

12.0      BIBLIOGRAPHY - List of Reports on Cunningham Property

- MARCH 1987      Summary Report of the Cunningham Creek Gold Property  
by P. Delancey
- OCTOBER 1986      Cunningham Creek 1986 Activities and Results  
by P. Delancey
- JANUARY 1985      The Geology and Exploration of the Cunningham Creek Property  
by S. Quin
- AUGUST 1984      Drilling Report on the Cunningham Creek Claim  
by S. Quin
- AUGUST 1984      Logistics Report on Induced Polarization Surveys  
by J. Hawkins (Geoterrex)
- FEBRUARY 1984      Drilling Report on the Cunningham Creek  
by S. Quin
- DECEMBER 1983      Geochemical Report on the Cunningham Creek Claim  
by S. Quin
- SEPTEMBER 1983      A Summary and Evaluation of the Cunningham Creek Property  
with Proposed Exploration for Fall 1983  
by S. Quin
- AUGUST 1980      Geological Report Black Martin Mineral Claim  
by S. Quin
- AUGUST 1980      Prospecting Report Black Martin Mineral Claim  
by S. Quin
- MAY 1979      Report on the Cunningham Creek Property  
by J. Elwell
- OCTOBER 1977      Report on the Cunningham Creek Drilling Project  
by G. Allen
- MAY 1977      Report on Mineral Lease M32 and the Jim Claim  
by G. Allen
- JANUARY 1977      Report of the 1976 Detailed Exploration Program conducted  
on the Cunningham Creek Property  
by G. Allen
- MARCH 1974      Geochemical and Geophysical Report on the Cunningham Creek  
Property  
by G. Allen



A P P E N D I X    A

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DIAMOND DRILL LOGS



CUNNINGHAM CREEK PROPERTY  
CC-87-1  
Page 2 of 6

From Meters	To Meters	Syb	Description	Smp. No.	From To Meters		Lgth.	Rec.	Analysis				
									Au ppb	Ag ppm	Cu ppm	Zn ppm	Pb ppm
			18.30 - 19.30 approx. 30% quartz-ankerite with local pyrite.	353	18.3	19.3	1.0	90%					
			19.30 - 21.90 approx. 3% fig pyrite as wispy bands.	354	19.3	21.9	2.6	90%					
21.90	38.40		<b>Chlorite-Sericite Schist</b> Above grades into more greenish rock which locally shows "plastic" type deformation and local quartz-ankerite segregations locally with some pyrite. Local fine pyrite bands up to 1cm wide noted especially near top of section. Lower section more sericitic.										
			21.90 - 22.00 - piece contains 1cm band of fine pyrite.	355	21.9	22.0	.1	100					
38.40	41.70		<b>Chloritic Quartzite</b> Above interbands gradually with a greyish fine grained micaceous quartzite. Minor pyrite noted as well as v.f. disseminated dark specks. Minor mariposite noted and broken rock at 39.70.										
41.70	49.70		<b>Sericite-Chlorite Schist</b> Similar to 9.10 to 15.90. Lower part shows tiny clay altered grains and rock becomes more quartzitic.										
49.70	54.60		<b>Quartz Vein</b> Coarsely crystalline white quartz vein with local micaceous portions. Ankerite is locally common. Pyrite appears to "replace" a few of the micaceous "inclusions" locally. Pyrite noted at 53.50, 53.60, 52.20. At 53.60 6cm quartz with 10% pyrite.	356	49.70	50.70							
				357	50.70	53.10							
				358	53.10	54.60							
				351	53.60				8610				















































































CUNNINGHAM CREEK PROPERTY  
 DDH-87-10  
 Page 3 of 7

From Meters	To Meters	Syb	Description	Smp. No.	From Meters	To Meters	Lgth.	Rec.	Analysis						
									Au ppb	Ag ppm	Cu ppm	Zn ppm	Pb ppm		
32.90	42.50		<b>Sericite-Chlorite Schist</b> Similar in appearance to the uppermost unit of DDH87-1; light greyish green; finely foliated and laminated; minor kinking; quartz segregations along foliation from 0.20cm to 2cm; occasionally quartz with ankerite and/or pyrite; occasional crush zones (10-20cm) in which rock is soft, broken and highly weathered; overall very light grey colouration would suggest a high proportion of sericite.												
			32.90-35.80m - 2% disseminated pyrite, generally within wispy (1-2mm) concentrations along foliation.	56410	32.90	34.65	1.75		7						
				56411	34.65	35.15	0.50		4450						
				56412	35.15	35.80	0.65		340						
			35.05-35.15m - quartz-ankerite with 5% pyrite.												
			36.50m - foliation at 80° to CA.												
			Beyond 35.80m pyrite is limited to occasional 5cm horizons containing thin wispy pyrite concentrations.												
			38.00-39.10m - abundant quartz segregations with minor pyrite alongside quartz; perhaps 40% quartz.	56413	38.00	39.10	1.1		180						
			39.70-40.20m - medium to dark grey chloritic quartzite.												
			41.50-42.50m - abundant quartz segregations some with pyrite; 2% disseminated pyrite and thin wispy pyrite concentrations.	56414	41.50	42.50	1.0		32						





CUNNINGHAM CREEK PROPERTY  
 DDH-87-10  
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From Meters	To Meters	Syb	Description	Smp. No.	From Meters	To Meters	Lgth.	Rec.	Analysis						
									Au ppb	Ag ppm	Cu ppm	Zn ppm	Pb ppm		
58.40	58.90		<b>Sericite-Chlorite Schist and Quartzite</b> Variably schistose; generally intermixed thin horizons (0.25cm to 2cm) of schist and quartzite; light grey; relatively minor quartz segregations; minor pyrite disseminated along foliation; predominantly quartzite.  60.00m - foliation at 65° to CA.												
58.90	60.20		<b>Sericite-Chlorite Schist</b> Contains 25% quartz segregations; minor disseminated pyrite.	56416	58.90	60.20			12						
60.20	64.00		<b>Sericite-Chlorite Schist and Quartzite</b> Light grey to greenish grey; fine grained quartzite with abundant very, thin, finely laminated layers of sericite-chlorite schist; gives rock a finely laminated appearance; minor quartz segregations.												
64.00	75.10		<b>Sericite-Chlorite Schist</b> Light to medium grey to greenish grey; finely foliated and laminated; minor disseminated pyrite.  68.50-75.10m - abundant light brown ankerite with quartz in segregations and as thin wispy (0.25m) bands along foliation.  69.20-69.70m - small fault??; very broken, weathered core.  70.90-71.10m - small fault??  73.55-74.40m - 20% quartz segregations; minor pyrite.	56417	73.50	74.40	0.9		6						









CUNNINGHAM CREEK PROPERTY  
DDH-87-11  
Page 3 of 5

From Meters	To Meters	Syb	Description	Smp. No.	From To Meters		Lgth.	Rec.	Analysis				
									Au ppb	Ag ppm	Cu ppm	Zn ppm	Pb ppm
			69.30-69.60m - quartz stockwork, 80% quartz.	56435	69.20	69.60	0.40		1				
			75.50m - foliation at 60° to CA.										
			79.50-80.20m - 5-6 quartz veins at 30° to CA; white quartz; minor pyrite; crosscutting foliation.	56436	79.50	80.20	0.70		1				
80.20	101.00		<b>Interbedded Sericite-Quartzite and Phyllite</b> Intermixed light to medium grey, fine grained, sericitic quartzite with lesser dark greenishgrey to black; phyllite; unit is more than 75% quartzite; phyllite generally present as thin, wispy bands 0.25cm to 2cm thick; unit is characterized by abundant whitish to bluish quartz segregations and/or crosscutting quartz veinlets; several horizons have stockwork of quartz veinlets; quartz segregations and veins are generally broken up and brecciated; minor pyrite along some but not all quartz; overall pyrite content is trace but short 5cm-10cm sections have 2% disseminated pyrite generally within more argillitic horizons.										
			80.50-80.60m - 2% disseminated pyrite with quartz.	56437	80.50	80.90	0.40		1				
			83.70-85.10m - 30% quartz; irregular quartz veins and quartz segregations along foliation.	56438	83.70	85.10	1.40		2				
			86.00m - foliation at 50° to CA.										
			90.20m - start of predominantly phyllite unit; greater than 70% phyllite; abundant quartz segregations approx. 1-2 per meter; quartz segregations vary up to 5cm thick; unit is very broken up.	56439	93.00	93.60	0.60		1				



















A P P E N D I X B

GEOCHEMICAL ANALYSES AND ASSAYS

R O C K   A N A L Y S E S



SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
PD-87-1	1	9	2	104	.3	7	17	3672	11.94	17	5	ND	1	122	1	2	2	11	15.27	.070	3	1	.75	29	.01	14	.08	.02	.04	1	1
PD-87-69F	1	19	112	7	.6	4	3	246	1.07	6	5	ND	3	21	1	2	2	1	.58	.006	2	2	.20	4	.01	2	.02	.01	.01	2	3
PD-87-70F	1	614	18	99	.7	18	18	16109	23.89	2	5	ND	2	250	1	2	2	7	11.21	.013	3	2	2.01	10	.01	14	.38	.01	.02	1	2
PD-87-71F	1	1731	38	102	.2	68	66	11895	42.61	8	5	ND	8	85	2	2	11	1	2.36	.016	3	10	.88	17	.01	41	.72	.01	.04	1	7
PD-87-72F	1	620	19	104	.5	19	19	17387	25.62	2	5	ND	2	226	2	2	2	7	9.60	.014	4	3	1.84	14	.01	14	.43	.01	.03	1	3
STD C/AU-R	18	58	40	130	7.1	68	27	997	3.90	38	12	7	37	47	17	17	24	54	.47	.081	36	58	.86	170	.08	35	1.96	.06	.13	12	500

## GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: P1-ROCK P2 TO P11-SOIL AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: SEPT 5 1987

DATE REPORT MAILED: Sept 17/87

ASSAYER: D. Jeps... DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203

File # 87-3946

Page 1

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TJ	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM	
PD-87-2	2	15	16	23	.1	18	7	487	4.06	154	5	ND	7	4	1	2	2	3	.04	.024	12	5	.02	24	.01	17	.22	.02	.09	1	53
PD-87-3	1	7	2	13	.1	7	2	360	1.75	10	5	ND	1	2	1	2	2	1	.04	.010	2	5	.01	8	.01	6	.04	.03	.02	1	1
PD-87-3A	1	5	3	23	.2	8	2	680	2.25	10	5	ND	3	3	1	2	2	2	.16	.006	5	8	.02	11	.01	14	.06	.03	.02	1	1
PD-87-4	1	11	2	24	.1	8	3	284	2.39	6	5	ND	2	1	1	2	2	1	.01	.003	3	6	.02	8	.01	10	.04	.01	.02	1	1
PD-87-5	1	7	5	41	.2	12	3	223	1.41	15	5	ND	4	4	1	2	2	2	.09	.010	8	5	.04	13	.01	13	.14	.02	.04	1	780
PD-87-5A	1	6	9	14	.2	14	5	425	2.33	21	5	ND	4	2	1	2	2	2	.01	.008	8	5	.02	20	.01	8	.10	.01	.06	1	1410
PD-87-6	1	8	9	42	.2	25	7	986	5.00	6	5	ND	7	7	1	2	2	11	.05	.035	13	12	.05	13	.01	2	.25	.06	.02	1	5
PD-87-7	1	14	22	34	1.2	16	6	184	3.59	189	5	3	3	5	1	4	2	3	.01	.012	4	5	.02	15	.01	6	.11	.01	.05	1	3570
PD-87-8	1	9	8	12	.9	8	1	145	1.56	32	5	3	1	4	1	2	2	2	.01	.008	2	6	.01	9	.01	8	.07	.01	.03	1	3160
PD-87-9	5	15	11	39	.1	13	5	842	2.51	10	5	ND	3	6	1	2	2	2	.01	.017	6	5	.02	28	.01	2	.09	.01	.04	1	41
PD-87-10	1	4	3	12	.1	4	1	327	1.42	2	5	ND	1	1	1	2	2	1	.01	.004	2	2	.01	10	.01	4	.05	.01	.03	1	21
PD-87-11	1	3	7263	53	13.0	6	3	1192	3.64	22	5	ND	3	571	1	8	15	2	18.46	.013	4	1	1.50	21	.01	5	.10	.01	.06	1	4
PD-87-12	1	72	25	167	.1	19	12	11549	50.44	11	5	ND	7	18	1	2	3	4	.01	.027	4	1	.08	41	.01	6	.31	.02	.06	1	6
PD-87-13	3	67	15232	101	28.1	4	6	12805	12.31	38	5	ND	2	201	4	31	5	3	15.04	.032	3	1	1.56	10	.01	2	.01	.01	.02	2	28
PD-87-14	3	8	2727	2059	14.9	5	3	5373	6.35	12	5	ND	2	188	23	6	32	3	11.04	.026	2	3	2.46	20	.01	2	.06	.01	.04	12	8
PD-87-15	1	672	120	97	.9	37	11	2621	34.35	23	5	ND	3	27	1	2	3	5	4.47	.007	2	1	.20	10	.01	2	.12	.02	.03	1	12
PD-87-16	1	471	88	139	.7	58	28	2221	38.79	9	5	ND	8	11	1	5	5	16	.45	.011	6	9	.88	7	.01	2	2.84	.02	.02	2	38
PD-87-17	1	88	34	22	.5	9	6	1042	5.27	11	5	ND	2	623	1	2	7	1	26.79	.019	3	3	.14	14	.01	2	.07	.01	.03	1	4
PD-87-18	2	1132	52	104	.1	24	8	4305	48.98	29	5	ND	7	10	1	2	2	13	.06	.045	2	2	.11	59	.01	2	.82	.02	.05	11	49
PD-87-19	2	840	41	110	.3	18	74	1070	51.48	77	5	ND	7	14	1	2	2	7	.29	.063	3	15	.10	10	.01	2	.58	.02	.05	8	250
PD-87-20	34	628	102	334	2.4	129	28	178	8.30	67	10	ND	4	91	4	8	2	54	1.56	.499	5	12	.36	10	.01	7	.66	.02	.18	2	33
TE-87-73F	1	1971	14558	37	226.1	58	115	694	28.39	31	5	ND	3	43	29	227	26	2	1.19	.024	2	1	.13	6	.01	6	.05	.02	.02	12	192
TE-87-74R	1	26	269	19	.5	6	3	517	2.50	13	5	ND	3	1321	1	2	6	1	31.64	.013	3	2	.62	13	.01	2	.06	.02	.03	1	21
TE-87-75F	1	812	2306	138	3.6	18	7	2602	54.68	18	5	ND	5	4	1	3	3	17	.01	.011	2	1	.08	12	.01	2	.40	.02	.05	3	42
TE-87-76R	2	37	248	67	.6	10	5	2485	8.88	11	5	ND	2	679	1	2	4	4	20.00	.022	4	2	3.07	7	.01	2	.02	.01	.02	1	1
TE-87-77R	3	21	48	58	.4	15	7	1536	5.90	16	5	ND	3	564	1	3	3	3	18.48	.026	5	3	2.93	14	.01	2	.08	.01	.04	1	1
TE-87-78R	2	11844	93	613	13.3	23	80	1825	9.83	117	5	ND	1	383	2	2	2	15	17.33	.009	4	1	1.81	11	.01	2	.04	.01	.03	2	138
TE-87-79R	1	86	20021	841	206.5	11	4	197	2.86	50	5	2	1	26	14	136	71	1	.33	.012	2	2	.06	7	.01	5	.05	.02	.02	1	3810
TE-87-80R	1	262	18916	1577	48.0	8	5	331	3.93	131	5	6	2	12	16	20	40	2	.34	.013	4	2	.06	11	.01	5	.08	.01	.04	4	6090
TE-87-81R	1	20	1879	29	2.9	14	5	114	2.08	48	5	ND	1	2	1	2	2	1	.02	.004	2	5	.01	3	.01	10	.03	.01	.01	1	59
TE-87-82F	1	18	518	77	1.2	6	2	111	1.92	93	5	ND	5	8	1	3	2	2	.03	.010	11	7	.01	16	.01	11	.16	.05	.04	1	530
TE-87-83F	1	9	102	58	.2	15	4	573	4.71	16	5	ND	1	3	1	2	2	2	.01	.013	2	2	.03	9	.01	6	.05	.01	.01	10	47
TE-87-84F	3	696	45	90	.6	69	51	7699	18.49	14	5	ND	3	126	1	2	2	2	7.33	.039	2	2	1.89	5	.01	2	.08	.03	.03	1	6
TE-87-85R	2	1630	226	761	5.1	76	39	16002	36.55	55	20	ND	5	52	3	2	12	4	.44	.064	5	1	.26	56	.01	2	.34	.04	.11	2	54
TE-87-86R	1	67	29	27	.5	5	3	1270	2.42	10	5	ND	1	1093	1	2	7	1	31.65	.012	3	1	.41	6	.01	2	.02	.02	.01	1	1
STD C/BU-R	18	58	41	133	7.1	67	27	1040	3.98	37	29	7	38	49	18	17	21	56	.47	.087	37	57	.87	175	.08	36	1.83	.08	.14	11	480

ASSAY REQUIRED FOR

16 > 10,000 PPM  
 0.1 - 75 PPM

ENVIRONMENTAL COPY

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	M	AUT
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
1E-87-87R	1	15	48	20	.4	9	3	408	1.57	2	5	ND	2	3	1	2	2	3	.20	.016	3	5	.14	16	.01	2	.34	.02	.03	1	7
1E-87-88F	1	17	4608	16	8.8	15	5	399	6.64	5034	5	14	1	21	1	7	2	1	.53	.003	2	3	.20	9	.01	2	.06	.02	.05	1	16470
1E-87-89F	1	24	4661	61	35.1	14	5	21	21.07	26560	5	55	2	4	1	11	8	1	.01	.001	2	1	.03	4	.01	4	.01	.01	.02	1	16400
1E-87-90F	1	6	49	10	1.6	14	8	692	3.78	9579	5	7	1	67	1	2	2	1	1.29	.021	2	2	.43	8	.01	4	.05	.02	.04	1	10450
1E-87-91F	1	5	253	9	2.6	13	3	202	2.60	1074	5	12	2	14	1	3	2	1	.29	.030	2	3	.08	9	.01	4	.07	.02	.05	1	10040
1E-87-92F	1	5	80	34	2.2	38	4	2162	6.32	377	5	6	1	8	1	2	2	1	.12	.009	2	3	.15	14	.01	2	.02	.01	.02	2	23500
PD-87-21	1	49	20767	24	339.8	33	3	391	3.69	246	5	ND	1	24	44	222	150	1	.62	.001	2	1	.05	16	.01	2	.04	.05	.01	1	570
PD-87-22	1	6	870	7	3.1	6	2	122	2.40	8643	5	11	1	4	1	3	2	1	.01	.007	2	3	.01	7	.01	12	.05	.01	.03	1	10400
PD-87-23	1	86	6749	112	10.2	15	28	1326	9.38	101	5	ND	4	77	1	4	2	17	2.50	.079	8	2	1.10	41	.01	2	.40	.05	.18	1	86
PD-87-23A	1	5	104	7	.5	2	1	361	1.07	183	5	ND	1	1020	1	2	3	1	19.94	.003	11	1	.18	6	.01	6	.02	.01	.01	1	145
PD-87-23B	1	9	226	14	.5	2	1	439	.93	18	5	ND	1	1469	1	2	6	1	31.40	.008	3	1	.35	8	.01	2	.02	.01	.02	1	15
PD-87-24	10	29	18906	49418	40.4	13	13	853	3.50	57	5	5	1	55	366	27	14	3	2.08	.014	2	2	.33	14	.01	2	.07	.03	.04	1	7710
PD-87-24A	2	18	294	102	.5	11	9	1431	6.63	18	5	ND	6	154	1	2	2	2	8.50	.023	7	1	.59	22	.01	2	.17	.03	.08	1	9
PD-87-25	2	60	499	568	.8	27	10	2952	14.57	19	9	ND	4	297	4	2	2	3	8.64	.010	5	3	1.35	18	.01	2	.13	.02	.06	1	29
PD-87-26	1	9	12250	29	245.7	29	59	70	22.48	320	5	33	2	23	1	5	450	1	.10	.003	2	1	.04	1	.01	2	.01	.01	.03	4	40900
PD-87-28	15	255	17096	92212	187.7	3	17	6353	6.08	25	5	ND	1	102	830	133	29	1	3.73	.057	2	1	.77	10	.01	5	.02	.02	.02	5	2140
PD-87-29	2	25	3558	1596	18.8	12	6	814	3.79	18	5	ND	7	321	17	5	19	3	13.93	.031	5	4	2.10	110	.01	2	.31	.02	.14	278	1680
PD-87-30	3	1663	3317	1764	8.7	30	11	3201	26.23	17	14	ND	3	162	19	4	2	4	6.67	.010	2	1	1.36	8	.01	2	.12	.02	.01	475	5140
STD C/AU-R	18	57	43	132	7.5	70	27	1032	3.93	38	18	8	37	49	18	18	21	58	.47	.086	38	58	.87	175	.07	36	1.81	.06	.15	12	510

ASSAY REQUIRED FOR Pb, As > 10,000 PPM  
 Zn > 20,000 PPM  
 Ag > 35 PPM

SAMPLE#	MO PPH	CU PPH	PB PPH	ZN PPH	AG PPH	NI PPH	CO PPH	MN PPH	FE %	AS PPH	U PPH	AU PPH	TH PPH	SR PPH	CD PPH	SD PPH	BI PPH	V PPH	CA %	P %	LA PPH	CR PPH	MG %	BA PPH	TI %	B PPH	AL %	NA %	K %	M PPH	AU# PPB
JW 87-1F	2	24	6	32	.1	19	12	797	2.92	8	5	ND	4	11	1	2	2	2	.16	.043	7	6	.05	42	.01	2	.12	.05	.02	1	3
JW 87-2 F	1	88	13	237	.6	24	13	3756	29.21	13	5	ND	20	13	1	2	2	10	.02	.031	19	20	.16	70	.01	6	1.05	.02	.10	1	10
JW 87-3 F	1	49	3	9	.2	12	2	867	1.50	33	5	ND	1	8	1	9	3	1	.79	.002	2	5	.02	21	.01	2	.09	.02	.06	1	6
JW 87-4 F	2	155	13	116	.7	7	15	2455	44.69	27	16	ND	4	1	1	2	2	23	.01	.011	2	1	.03	8	.01	2	.20	.01	.03	1	27
JW 87-5 F	1	22	6	37	.2	16	11	1308	3.01	2	5	ND	5	10	1	2	2	5	.28	.051	9	7	.05	25	.01	7	.26	.04	.06	1	1
JW 87-6 R	1	9	2	63	.1	23	11	624	4.18	2	5	ND	2	6	1	4	2	2	.05	.022	4	4	.07	24	.01	2	.28	.02	.06	1	2
JW 87-7 F	1	5	9	91	.2	1	6	7573	14.78	17	5	ND	1	329	2	2	2	10	17.73	.024	3	4	1.82	9	.01	6	.01	.01	.02	1	6
JW 87-8 R	1	4	2	20	.5	10	3	518	2.43	8	5	3	1	4	1	2	2	1	.07	.026	2	2	.03	9	.01	2	.04	.01	.01	1	14840
JW 87-9 F	1	2	2	6	.3	4	1	254	.89	2	5	ND	2	5	1	2	2	1	.24	.004	2	2	.03	4	.01	2	.02	.01	.01	1	8
JW 87-10	1	16	5	59	.1	9	13	5021	28.54	8	5	ND	2	5	1	2	2	3	.04	.017	2	3	.03	56	.01	6	.08	.01	.04	1	18
JW 87-11F	1	2	2	7	.1	5	2	236	.77	2	5	ND	1	1	1	2	2	1	.01	.001	2	2	.01	15	.01	4	.01	.01	.01	1	1
JW 87-12R	1	9	3	28	.2	16	6	586	2.23	7	5	ND	2	6	1	3	2	1	.31	.007	4	2	.03	32	.01	2	.10	.02	.04	1	220
JW 87-13F	3	314	16	88	.5	7	15	1967	41.89	21	5	ND	3	2	1	5	2	25	.01	.013	3	3	.02	42	.01	2	.31	.01	.06	1	31
JW 87-14	3	705	27	101	.7	34	19	2760	44.46	39	5	ND	2	7	2	7	2	24	.01	.020	2	1	.06	28	.01	2	.28	.01	.07	1	44
JW 87-15F	2	452	20	114	.6	27	19	3084	41.36	32	5	ND	4	4	1	10	2	17	.01	.035	4	3	.04	39	.01	2	.21	.01	.05	1	33
JW 87-93R	1	8	2	4	.1	3	1	135	.88	2	5	ND	1	2	1	2	3	1	.01	.007	3	2	.01	4	.01	10	.03	.02	.01	1	6
JW 87-94R	1	10	59	5	.6	14	4	106	2.91	135	5	ND	1	1	1	2	2	1	.01	.002	2	1	.01	6	.01	5	.05	.01	.02	1	995
STD C/AU-R	20	63	40	133	7.3	69	29	1037	3.87	40	18	8	39	52	18	17	20	59	.46	.090	39	61	.84	180	.07	30	1.81	.06	.14	13	480

EXTRA  
COPY

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: Rock Chips AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

EXTRA COPY

DATE RECEIVED: SEPT 16 1987 DATE REPORT MAILED: *Sept 29/87* ASSAYER: *D. J. ...* DEAN TOYE. CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-4280

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPM	
JW-87-16F	1	110	4	101	.1	22	36	1397	9.08	2	5	ND	5	39	1	2	2	75	.25	.088	15	15	.96	58	.01	2	2.47	.06	.05	1	4
JW-87-17F	2	8	2780	47	3.5	23	7	1985	5.38	5	5	ND	1	11	1	2	2	3	.09	.024	3	2	.10	23	.01	2	.10	.02	.02	1	3
JW-87-18F	1	2	96	14	.1	10	2	415	1.27	3	5	ND	1	246	1	2	2	2	5.63	.011	7	2	.07	14	.01	2	.09	.01	.02	1	1
JW-87-19F	1	2	27	12	.1	1	1	354	.63	4	5	ND	1	1475	1	2	6	1	36.06	.013	4	1	.28	9	.01	6	.02	.01	.01	1	1
JW-87-20F	1	509	33	117	.1	20	23	3288	49.25	42	5	ND	3	4	2	2	2	1	.01	.017	2	2	.03	25	.01	4	.23	.01	.05	1	26
JW-87-21	1	24	8	25	.1	5	4	1527	1.75	5	5	ND	1	551	1	2	2	9	9.07	.044	4	2	.29	44	.01	2	.40	.01	.05	1	1
JW-87-22	1	125	11	163	.1	15	28	1680	7.42	34	5	ND	1	199	1	2	2	141	5.58	.064	10	12	2.48	21	.01	4	2.65	.03	.02	1	4
JW-87-23R	1	29	17251	84	24.7	2	7	6330	11.01	33	5	ND	1	352	4	15	2	5	16.67	.030	3	2	2.70	8	.01	6	.03	.01	.02	852	99
JW-87-24R	1	2693	19	132	2.4	8	32	1710	13.46	7	5	ND	1	319	1	2	2	8	11.61	.008	2	3	2.24	12	.01	2	.03	.01	.03	10	142
JW-87-25R	1	138	14	83	.1	16	32	886	7.10	31	5	ND	2	89	1	2	2	41	4.52	.069	7	7	1.42	64	.01	7	.54	.06	.07	1	3
JW-87-26F	1	52	9	22	.1	17	7	613	2.18	2	5	ND	5	29	1	2	2	1	.61	.012	5	3	.18	135	.01	2	.13	.04	.04	1	1
PD-87-31	1	422	30	76	.1	64	28	678	9.85	2	5	ND	3	9	1	2	2	3	.21	.018	4	3	1.74	23	.01	2	.13	.02	.08	11	3
PD-87-32	2	159	20	17	.1	16	5	265	4.49	32	5	ND	1	5	1	2	2	1	.09	.005	3	1	.05	20	.01	3	.09	.01	.04	1	250
PD-87-34A	33	91	30350	54694	509.6	4	3	372	1.34	31	5	ND	1	110	491	51	713	1	.73	.008	2	1	.01	6	.01	3	.02	.01	.01	1	520
PD-87-34B	1	1308	338	267	2.0	4	19	960	53.09	168	5	3	4	4	2	8	17	1	.01	.036	2	2	.05	22	.01	4	.15	.01	.05	127	1880
PD-87-35	30	37	21589	46776	49.0	9	9	4361	10.29	335	5	ND	1	116	605	35	2	4	7.26	.069	3	4	1.07	14	.01	10	.13	.01	.08	1470	2860
PD-87-36	2	294	23762	340	66.8	3	17	1498	48.11	8926	5	ND	1	8	4	27	435	1	.21	.056	2	3	.07	6	.01	5	.18	.01	.04	61	890
PD-87-37	1	22	501	110	1.3	11	8	3190	8.47	153	5	ND	1	280	2	2	2	3	17.33	.013	5	1	4.65	7	.01	5	.04	.01	.03	3	16
TE-87-45R	3	137	22220	831	59.3	11	14	11251	12.13	72	5	ND	1	138	14	54	2	4	10.46	.028	2	3	1.39	21	.01	7	.04	.01	.04	677	60
TE-87-46R	3	63	20323	101	77.1	7	11	13100	11.82	40	5	ND	1	193	8	67	2	4	14.47	.031	2	2	1.47	19	.01	2	.03	.01	.04	220	120
TE-87-97R	1	5	948	10	1.1	2	1	471	.80	9	5	ND	1	931	1	2	5	1	28.05	.012	3	2	.29	6	.01	2	.03	.01	.01	10	1
TE-87-98R	1	810	160	352	1.8	32	24	3934	16.35	80	5	ND	1	411	4	2	2	4	16.02	.008	2	2	1.63	9	.01	2	.01	.01	.01	1	360
TE-87-99R	1	13	45	29	.1	10	5	669	1.85	10	5	ND	1	636	1	2	5	1	26.23	.014	4	1	.29	21	.01	2	.12	.01	.07	1	1
STD C/AU-#	19	59	39	131	7.2	64	28	973	3.52	37	20	8	36	49	18	18	20	55	.47	.084	37	58	.88	177	.06	37	1.90	.06	.13	13	525

✓ Assay required w Pb Zn Ag

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	HG	BA	TI	B	AL	NA	K	W	AUS
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	%	PPM	PPB
JW-87-27R	1	7	76	14	.9	7	1	460	.98	16	5	ND	1	1	1	4	7	1	.01	.003	2	2	.02	11	.01	2	.04	.01	.01	1	560
JW-87-28F	1	3	9	56	.1	7	10	1832	7.13	5	5	ND	1	146	1	2	2	6	10.38	.051	3	1	1.79	5	.01	2	.01	.01	.01	1	3
JW-87-29R	1	2	13	9	.4	1	1	888	1.51	3	5	ND	2	1098	1	2	3	1	32.13	.008	4	1	.99	3	.01	5	.01	.02	.01	1	1
JW-87-30R	1	3	4	30	.1	5	6	1387	5.30	9	5	ND	1	238	1	2	2	16	7.72	.060	2	2	1.60	24	.01	10	.05	.02	.01	1	1
JW-87-31R	1	7	1115	9	23.4	15	18	67	9.20	121	5	4	1	38	1	2	22	1	.87	.002	2	1	.04	4	.01	2	.01	.02	.01	2	4610
JW-87-32R	1	218	25	82	.6	12	15	1029	3.86	25	5	ND	5	635	1	2	2	2	17.41	.024	6	1	1.01	22	.01	2	.10	.01	.06	1	41
JW-87-33R	1	26	35	87	.2	33	20	538	5.15	10	5	ND	9	24	1	3	2	6	.39	.029	9	7	.70	37	.01	3	.26	.04	.10	1	37
JW-87-34R	1	299	49	94	.3	56	39	1462	11.38	170	5	ND	3	29	1	2	2	9	.57	.092	4	1	.09	34	.01	9	.26	.07	.06	1	9
JW-87-35R	1	175	15	69	.4	12	28	1837	7.98	15	5	ND	3	56	1	2	2	12	6.98	.089	5	1	.19	62	.01	6	.29	.03	.08	1	1
JW-87-36R	1	18	24	14	.3	2	2	757	1.40	3	5	ND	2	1348	1	2	2	1	32.80	.012	8	1	.36	16	.01	5	.04	.02	.01	1	1
JW-87-37SC	1	91	108	79	.2	46	16	4514	9.30	35	5	ND	16	24	1	2	2	7	.13	.051	53	10	.10	128	.01	2	.98	.05	.09	1	3
JW-87-38R	3	7	36	69	.6	3	3	18353	15.61	9	11	ND	6	80	1	2	7	3	15.79	.017	5	1	.52	21	.01	2	.04	.01	.03	200	15
JW-87-39R	2	3	1818	163	7.7	8	4	6669	8.32	14	5	ND	4	350	1	2	12	3	18.02	.029	4	2	1.31	49	.01	2	.06	.01	.02	5	6
JW-87-40R	1	12	48	52	.8	15	5	1267	4.48	6	5	ND	3	9	1	2	5	4	.25	.020	5	4	.06	36	.01	2	.17	.03	.03	1	11
JW-87-41R	1	3	50	35	.2	8	6	2269	4.75	10	5	ND	3	570	1	2	2	2	22.71	.011	6	1	2.81	34	.01	2	.07	.01	.04	3	1
JW-87-42F	2	78	21	142	.1	29	19	27261	45.45	9	29	ND	.7	50	1	3	2	4	.04	.027	4	1	.08	81	.01	2	.34	.01	.03	2	2
PD-87-38	1	408	21	109	.8	5	5	1729	52.03	13	5	ND	6	9	1	7	2	4	.24	.009	2	1	.08	12	.01	2	.15	.01	.03	2	9
PD-87-39	1	116	20	220	.4	43	19	2231	29.90	6	5	ND	15	21	1	3	2	5	.13	.020	16	4	.30	23	.01	2	.35	.05	.06	1	1
PD-87-40	2	127	10	70	.1	23	28	1319	8.21	29	5	ND	4	177	1	2	2	17	5.26	.073	9	5	2.35	31	.01	2	.48	.13	.02	1	1
PD-87-41	1	18	2312	2232	3.0	5	4	459	2.32	45	5	ND	1	26	12	2	2	5	.60	.019	3	2	.10	10	.01	2	.10	.04	.03	3	260
TE-87-100R	1	77	10	82	.1	15	30	1221	6.95	5	5	ND	5	221	1	2	2	75	6.61	.071	12	6	1.32	32	.01	2	1.93	.02	.03	1	1
TE-87-101R	1	16	18	41	.2	6	4	2153	4.57	5	5	ND	2	521	1	2	2	3	19.21	.007	6	1	2.86	24	.01	4	.06	.01	.01	2	1
TE-87-102R	3	7	52	87	.3	12	5	10454	41.15	15	5	ND	5	203	1	2	2	3	5.95	.012	2	1	1.11	7	.01	2	.11	.01	.01	2	3
TE-87-103R	1	7	16	37	.3	3	4	1557	3.85	8	5	ND	2	605	1	3	2	3	17.57	.023	2	1	2.01	15	.01	4	.04	.01	.02	2	1
TE-87-104R	1	14	14	9	.3	2	1	983	1.38	3	6	ND	1	1237	1	2	4	1	35.21	.015	4	1	.38	15	.01	9	.02	.02	.01	1	10
TE-87-105R	2	134	15	71	.1	12	16	3065	10.66	8	5	ND	2	501	1	2	2	4	16.29	.025	3	1	2.39	16	.01	2	.29	.01	.01	1	5
TE-87-106R	1	4	20	10	.3	3	1	773	1.21	4	5	ND	2	935	1	2	2	1	30.89	.014	4	1	.24	10	.01	3	.03	.01	.01	1	1
TE-87-107R	1	3	27	20	.3	4	2	1838	2.70	2	5	ND	2	1113	1	2	4	1	34.01	.016	4	1	.56	11	.01	2	.02	.02	.01	1	1
TE-87-108R	2	2	8	23	.2	2	3	3477	4.65	5	5	ND	1	438	1	2	2	2	21.69	.002	4	1	6.62	12	.01	2	.01	.01	.01	1	1
TE-87-109F	1	1269	299	105	4.1	59	263	322	49.65	33	6	ND	5	10	1	3	2	2	.29	.002	2	1	.13	6	.01	2	.06	.01	.01	4	410
TE-87-110R	1	4	4	74	.1	50	17	592	5.21	40	5	ND	7	6	1	2	2	3	.12	.034	10	2	.07	26	.01	6	.25	.02	.12	1	19
TE-87-111R	1	108	29	81	.1	32	17	245	8.09	16	5	ND	12	7	1	3	2	20	.09	.037	9	35	.99	16	.01	2	2.21	.03	.08	1	21
TE-87-112R	1	23	266	119	.5	45	14	1612	5.57	3	5	ND	2	5	1	2	2	15	.07	.015	6	7	.95	12	.01	3	2.05	.02	.03	1	1
TE-87-113R	1	36	10	121	.1	53	24	922	6.85	2	5	ND	11	10	1	2	2	25	.18	.058	21	48	1.38	25	.01	4	3.05	.03	.09	1	1
TE-87-114R	1	10	5	123	.1	50	18	981	6.75	2	5	ND	14	10	1	2	2	25	.12	.038	25	36	1.44	23	.01	2	3.11	.03	.09	1	2
STD C/AU-R	18	58	39	131	7.0	66	27	1027	3.93	37	18	7	38	50	17	18	21	57	.49	.086	38	59	.86	179	.08	38	1.83	.08	.13	12	520

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: Rock Chips AU: ANALYSIS BY AA FROM 10 GRAM SAMPLE.

EXTRA COPY

DATE RECEIVED: SEPT 24 1987 DATE REPORT MAILED: Oct 9/87 ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-4430 Page 1

SAMPLE#	MD	CU	PB	ZN	AS	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BT	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	PPM	PPM	
JW-87-42R	1	10	7	36	.1	13	4	809	3.66	9	5	ND	2	12	1	2	2	.33	.016	2	1	.10	10	.01	2	.04	.02	.01	2	1	
JW-87-43R	1	106	9	101	.3	6	26	1024	8.31	2	5	ND	9	204	1	2	2	184	2.55	.086	22	2	1.89	59	.01	2	3.46	.06	.02	1	1
JW-87-44F	1	8	7	23	.1	7	3	371	2.11	7	5	ND	9	8	1	2	2	6	.10	.019	16	3	.07	14	.01	2	.23	.03	.02	2	1
JW-87-45F	1	5	6	22	.1	9	3	360	1.59	2	5	ND	13	5	1	2	2	4	.04	.021	19	6	.08	22	.01	2	.18	.03	.02	1	1
JW-87-46R	2	31	39	44	.4	8	7	2489	5.52	2	5	ND	1	302	1	2	2	5	10.11	.026	2	1	2.81	13	.01	2	.04	.01	.01	3	11
JW-87-47F	1	8	15	44	.2	9	3	2331	4.17	4	5	ND	2	2	1	2	2	2	.03	.008	4	2	.06	124	.01	2	.06	.01	.01	3	1
JW-87-48F	2	35	14	62	.4	3	3	3952	10.98	6	5	ND	1	464	1	2	2	4	20.53	.006	2	1	.74	10	.01	2	.01	.01	.01	1	2
JW-87-49R	1	171	14	215	.6	25	36	1623	10.95	39	5	ND	5	22	1	2	2	13	1.15	.084	9	1	1.18	57	.01	2	.31	.08	.05	2	1
JW-87-50F	2	4	9	81	.7	18	9	2174	10.20	10	5	ND	3	165	1	2	2	4	16.54	.012	4	1	1.13	20	.01	2	.01	.01	.01	2	1
TE-87-115F	1	8	2476	32	22.4	302	92	1126	18.70	1001	5	4	3	74	1	2	37	2	2.26	.013	2	1	.98	6	.01	2	.01	.03	.01	3	6980
TE-87-116F	2	7	2066	105	2.9	7	5	5204	12.17	75	5	ND	3	237	1	2	2	3	11.12	.039	2	1	2.70	5	.01	2	.01	.01	.01	510	92
TE-87-117F	3	5	9628	613	11.9	4	3	9770	9.63	44	5	ND	4	296	5	5	2	2	14.24	.030	2	1	3.45	11	.01	2	.04	.01	.01	709	520
TE-87-118F	1	14	10668	127	93.1	198	347	1364	23.70	555	5	11	4	59	3	2	180	3	1.90	.148	2	1	.79	6	.01	5	.04	.03	.01	10	19400
TE-87-119R	2	19	150	63	.9	17	6	2123	6.44	6	5	ND	2	348	1	2	2	2	10.53	.031	2	1	3.00	40	.01	2	.10	.01	.04	11	68
TE-87-120R	2	30	144	32	1.3	37	15	979	3.73	5	5	ND	8	169	1	2	2	4	5.04	.036	5	5	1.28	41	.01	3	.33	.03	.09	5	128
TE-87-121F	10	259	29401	40534	61.6	15	21	5240	11.48	48	5	ND	3	81	409	51	2	2	5.14	.029	2	1	1.65	11	.01	4	.07	.03	.03	5	210
TE-87-122F	2	456	15418	215	173.4	31	294	6542	17.49	59	5	ND	3	63	26	186	2	2	4.26	.043	2	1	1.55	5	.01	3	.02	.02	.01	141	710
TE-87-123F	1	9	562	237	.5	9	3	357	1.45	2	5	ND	11	4	2	3	2	1	.08	.011	14	2	.05	28	.01	2	.16	.02	.10	3	6
TE-87-124F	1	10	4330	19	106.2	16	52	60	19.38	241	5	139	3	2	1	2	271	1	.04	.001	2	1	.03	3	.01	2	.01	.01	.01	3	156800
TE-87-125F	1	6	5723	39	7.5	2	2	3906	4.11	4	5	ND	2	68	1	5	2	2	4.74	.022	2	1	.42	7	.01	2	.03	.01	.02	1	118
TE-87-126F	1	198	179	136	1.6	14	17	1459	17.93	11	7	ND	13	55	1	2	2	3	2.26	.025	7	5	1.15	13	.01	2	.19	.04	.08	3	760
TE-87-127F	1	1345	66	27	.9	13	62	508	29.76	30	5	ND	6	4	1	2	2	2	.37	.036	2	1	.05	6	.01	5	.09	.02	.04	6	325
TE-87-128F	2	605	290	103	4.7	7	9	8157	34.36	26	5	ND	4	20	1	2	9	4	.28	.014	2	1	.14	12	.01	2	.03	.01	.01	3	575
TE-87-129F	1	37	58	24	1.0	4	2	1041	3.40	6	5	ND	2	1279	1	2	2	1	25.44	.009	3	1	.24	15	.01	3	.02	.01	.01	2	96
TE-87-130R	1	175	19336	9	338.2	21	34	156	7.31	12	5	ND	2	3	103	656	81	1	.13	.007	2	1	.03	1	.01	13	.01	.01	.01	1	315
TE-87-131R	1	24	2853	103	3.8	3	2	437	1.48	3	5	ND	1	18	1	4	4	1	.32	.001	2	1	.01	7	.01	2	.01	.01	.01	9	49
TE-87-132R	1	11	5139	9	7.3	8	4	394	1.44	15	5	ND	3	1184	1	6	3	1	31.63	.013	3	1	.27	12	.01	2	.05	.01	.02	1	1
TE-87-133R	1	65	131	140	.5	38	12	357	9.46	4	5	ND	11	9	1	2	2	52	.11	.026	12	41	2.05	17	.01	4	4.40	.03	.03	2	8
TE-87-134R	12	150	14273	55239	22.6	12	20	750	3.06	23	5	ND	2	213	633	20	2	1	8.34	.011	3	2	.09	14	.01	2	.09	.01	.01	5	1470
TE-87-135R	1	7	6372	76	23.7	7	2	860	1.62	8	5	ND	1	377	2	5	40	1	10.28	.005	2	2	.12	8	.01	2	.04	.01	.01	1	22
TE-87-136R	6	12	983	357	2.2	10	3	902	1.78	24	5	ND	6	1243	4	2	2	2	25.79	.030	10	2	.18	13	.01	2	.08	.01	.01	1	6
TE-87-137R	1	10	98	63	.9	8	5	749	1.88	2	5	ND	3	1695	1	2	2	1	32.98	.015	4	1	.26	14	.01	2	.07	.01	.03	1	1
TE-87-138R	2	3	127	40	.5	3	2	506	.98	4	5	ND	3	1347	1	2	2	1	27.92	.012	6	1	.20	13	.01	3	.03	.01	.01	1	2
TE-87-139R	1	17	18171	108	179.6	30	17	179	3.23	214	5	6	1	44	1	5	350	1	.60	.005	2	2	.01	3	.01	2	.02	.02	.01	1	4250
TE-87-140R	1	30	992	236	31.5	7	1	56	1.30	138	5	ND	1	18	1	2	80	1	.31	.003	2	1	.01	2	.01	3	.01	.01	.01	1	145
TE-87-141R	1	6	141	25	1.8	5	3	564	1.14	9	5	ND	4	1432	1	2	5	1	34.53	.018	6	1	.27	6	.01	2	.04	.02	.02	1	11
STD C/AU-R	18	58	38	133	7.1	66	26	1034	3.95	37	16	7	38	49	17	17	21	56	.49	.083	36	57	.87	175	.08	32	1.83	.08	.12	13	510

- ASSAY REQUIRED FOR CORRECT RESULT for Cu, Pb > 10,000 ppm Zn > 20,000 ppm

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	V	AU	TH	SR	CD	SB	B1	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU1
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	Z	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	Z	Z	PPM	PPM	Z	PPM	Z	PPM	Z	Z	Z	PPM	PPB
PD-87-42	1	1	19	36	.2	12	6	2722	6.63	21	5	ND	4	359	1	2	2	4	16.86	.012	7	2	3.34	20	.01	2	.13	.01	.06	3	4
PD-87-43	1	3	21	33	.4	5	3	1795	3.98	5	5	ND	2	917	1	2	2	1	20.39	.018	9	2	2.18	12	.01	2	.06	.01	.01	3	25
PD-87-43A	1	2571	258	114	24.3	1089	186	2916	12.06	2361	5	28	1	13	1	5	158	2	.12	.001	2	1	.07	30	.01	2	.01	.01	.01	1	129425
PD-87-44	2	41344	4562	1243	403.8	3025	109	1746	22.47	4779	5	503	2	18	18	28	4923	1	.25	.001	2	1	.07	10	.01	3	.01	.02	.01	1	675010
PD-87-45	2	69	20	78	.8	25	5	4010	12.81	26	5	ND	1	311	1	2	2	7	17.90	.026	2	1	3.02	10	.01	2	.01	.01	.01	2	2345
PD-87-46	1	626	92	47	4.1	58	11	534	4.24	67	5	2	4	7	1	4	73	11	.13	.021	3	13	.72	15	.01	2	1.33	.02	.04	2	4660
PD-87-47	1	20	15	57	.1	42	18	2069	9.95	28	5	ND	2	9	1	2	2	2	.25	.029	3	2	.13	22	.01	7	.10	.02	.03	1	39
PD-87-48	1	192	68	45	.6	31	20	2090	7.75	20	5	ND	3	5	1	2	5	17	.07	.076	10	3	.12	62	.01	4	.38	.07	.04	2	206
PD-87-49	1	39	13	71	.1	14	18	1406	6.21	24	5	ND	2	3	1	2	2	21	.04	.039	4	5	.09	28	.01	2	.21	.03	.03	1	240
PD-87-50	1	16	14	69	.1	39	15	2103	10.00	23	5	ND	4	4	1	2	2	3	.02	.009	9	2	.08	29	.01	2	.10	.01	.05	1	66
PD-87-51	1	10	2380	9	57.3	7	22	147	2.94	1867	5	13	1	5	1	2	112	1	.04	.006	2	3	.01	5	.01	3	.03	.01	.01	1	16225
PD-87-52	1	7	55	129	1.1	16	21	2496	11.87	39	5	ND	1	124	1	2	2	9	6.90	.026	5	1	1.06	30	.01	8	.04	.02	.01	3	230
PD-87-52A	1	6	34	54	.5	32	12	767	4.88	25	5	ND	1	3	1	2	2	2	.05	.016	2	3	.04	35	.01	2	.07	.01	.01	1	76
PD-87-53	1	32	5532	55	105.4	4	1	130	1.24	331	5	ND	1	3	1	2	135	1	.10	.001	2	3	.02	4	.01	2	.01	.01	.01	5	1085
PD-87-54	1	59	27239	178	482.1	7	2	83	.81	51	5	ND	2	11	10	5	1040	1	.01	.003	2	4	.01	5	.01	6	.01	.01	.01	1	73
PD-87-55	2	305	21587	68	393.8	55	47	424	7.28	195	5	15	2	119	49	74	11437	1	.03	.011	4	2	.01	16	.01	3	.02	.01	.01	87	31850
PD-87-56	1	626	2702	80	26.0	48	12	1123	4.53	16	5	ND	1	5	1	2	36	1	.04	.012	2	2	.05	32	.01	2	.09	.02	.02	1	425
PD-87-57	1	17	5220	48	65.0	19	8	3235	7.51	21	5	ND	6	6	1	2	133	1	.03	.026	10	1	.08	23	.01	2	.11	.01	.07	1	645
PD-87-58	1	434	736	63	2.4	42	51	1959	17.44	23	5	ND	3	8	1	2	2	13	.07	.057	2	1	.10	18	.01	7	.16	.04	.01	1	28
PD-87-59	1	97	2345	12	30.4	31	2	396	2.37	5	5	ND	1	2	1	2	71	1	.01	.003	2	4	.05	6	.01	2	.03	.02	.01	1	108
PD-87-60	1	64	321	18	1.1	29	8	198	2.15	9	5	ND	1	1	1	2	2	1	.01	.002	2	4	.02	3	.01	5	.02	.01	.01	1	16
PD-87-61	1	13	391	8	5.7	23	6	59	8.71	332	5	2	1	1	1	5	6	1	.01	.001	2	1	.01	3	.01	3	.01	.01	.01	1	3485
PD-87-62	1	35	4456	7	12.1	31	9	91	4.87	13	5	ND	1	4	1	2	14	1	.01	.001	2	4	.01	35	.01	6	.02	.01	.01	2	62
PD-87-63	1	7	107	4	.9	16	2	83	1.09	44	5	ND	2	1	1	2	2	1	.01	.003	5	3	.01	6	.01	4	.04	.01	.02	1	92
PD-87-64	1	12	67	12	.1	5	2	456	1.63	2	5	ND	1	3	1	2	2	1	.05	.004	2	4	.02	12	.01	2	.03	.01	.01	1	14
PD-87-65	2	105	24	238	.5	41	19	5288	32.98	26	5	ND	17	11	1	2	2	12	.03	.049	23	17	.25	123	.01	2	1.22	.02	.04	7	15
PD-87-66	2	54	29	63	.7	22	8	3899	44.62	227	5	ND	4	7	1	2	2	3	.01	.018	2	1	.07	33	.01	2	.15	.01	.01	3	12310
PD-87-67	2	481	29	63	3.8	26	12	2429	40.30	223	5	20	3	3	1	3	2	3	.01	.044	2	1	.09	10	.01	2	.10	.01	.01	5	35100
PD-87-68	3	74	21	388	.3	36	10	4130	34.62	8	5	ND	15	12	1	2	2	28	.03	.009	20	29	.87	34	.01	2	5.41	.03	.01	1	825
PD-87-69	2	737	38	102	1.7	22	10	3000	43.34	814	5	4	6	2	1	2	2	8	.01	.100	2	1	.06	53	.01	2	.38	.01	.02	6	2580
PD-87-70	2	470	27	118	.6	11	6	3324	37.03	81	5	ND	3	3	1	2	2	9	.01	.027	2	1	.05	13	.01	6	.24	.01	.05	4	1185
PD-87-71	1	510	26	70	.4	5	5	1462	38.01	13	5	ND	3	1	1	2	2	4	.01	.011	2	1	.04	15	.01	2	.17	.01	.01	2	59
PD-87-72	1	285	24	51	.1	8	5	1094	24.24	10	5	ND	4	2	1	2	2	3	.01	.015	3	1	.03	6	.01	7	.30	.01	.01	11	1220
PD-87-73	2	718	38	93	.5	15	45	1921	40.28	12	5	ND	4	3	1	2	2	6	.01	.010	2	1	.06	11	.01	2	.31	.01	.01	2	242
PD-87-74	1	424	19	77	.1	1	5	1304	30.41	11	5	ND	3	1	1	2	2	3	.01	.014	2	1	.03	12	.01	6	.16	.01	.01	2	53
PD-87-75	2	469	26	90	.8	12	7	4015	47.15	54	5	ND	5	4	1	2	2	3	.01	.043	2	1	.11	24	.01	2	.16	.01	.01	3	1320
STD C/AU-R	18	58	38	132	7.2	69	27	1025	3.84	38	24	7	39	51	18	18	21	57	.49	.084	38	58	.86	180	.08	37	1.82	.08	.13	13	520



SAMPLE#	MO PPH	CU PPH	PB PPH	ZN PPH	AG PPH	NI PPH	CO PPH	MN PPH	FE %	AS PPH	U PPH	AU PPH	TH PPH	SR PPH	CD PPH	SB PPH	BI PPH	V PPH	CA %	P %	LA PPH	CR PPH	HG %	BA PPH	TI %	B PPH	AL %	NA %	K %	W PPH	AU# PPB
PD-87-76	16	34	4066	14947	4.9	7	2	1484	2.79	11	5	ND	1	814	47	2	2	26.54	.012	4	1	.92	11	.01	3	.02	.01	.01	1	30	
PD-87-77	17	84	1137	83686	7.5	3	2	557	1.06	22	5	ND	1	734	180	32	3	27.46	.007	2	1	.12	3	.01	2	.01	.01	.01	151	182	
PD-87-78	23	51	20105	81176	46.8	9	2	2480	6.52	25	5	ND	1	220	404	33	3	5.65	.027	2	1	1.10	17	.01	3	.04	.01	.01	91	64	
PD-87-80	2	8	22692	506	59.1	1	3	4353	8.39	26	5	ND	3	252	8	26	71	13.74	.063	3	1	3.29	6	.01	2	.03	.01	.01	705	24	
PD-87-81	2	220	12781	1172	21.7	15	20	2801	11.69	19	5	ND	4	207	15	21	2	9.04	.030	2	3	1.85	7	.01	2	.07	.01	.03	927	18	
PD-87-82	2	232	627	151	1.1	6	10	1867	8.04	5	5	ND	1	265	1	2	2	15.42	.007	2	1	2.07	38	.01	2	.02	.01	.01	46	6	
PD-87-83	5	150	22243	5597	37.6	4	6	12806	10.19	23	5	ND	2	72	60	51	2	9.15	.070	2	1	.30	57	.01	2	.06	.01	.01	73	18	
PD-87-85	1	1717	482	154	.7	27	26	220	50.89	19	5	ND	4	11	1	2	2	.28	.015	2	11	.15	13	.01	2	.08	.02	.01	6	30	
PD-87-86	4	271	834	399	2.0	11	7	6990	25.51	56	12	ND	3	385	4	2	2	10.86	.016	3	1	1.10	8	.01	2	.06	.01	.01	5	148	
STD C/AU-R	18	57	37	130	7.2	68	26	1023	3.97	36	18	7	38	49	18	17	21	.50	.083	37	58	.87	179	.08	32	1.85	.08	.13	12	480	

## GEOCHEMICAL/ASSAY CERTIFICATE

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.  
- SAMPLE TYPE: Core AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: SEPT 24 1987

DATE REPORT MAILED: *Oct 9/87*ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-4430A

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BT	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	CU	PB	ZN	AG	AU			
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	%	PPH	%	%	%	PPH	%	%	%	PPH	PPH	PPH	PPH	PPH
C 4925	6	889	291	99	.7	29	4	8597	30.75	18	5	ND	4	158	1	2	2	4	3.55	.002	2	1	1.37	6	.01	2	1.10	.03	.01	4	-	-	-	.03	.001			
C 4926	3	177	709	80	1.7	18	18	5215	15.66	108	5	ND	3	491	1	2	2	3	16.10	.013	2	1	1.23	15	.01	2	.06	.01	.01	1	-	-	-	.04	.015			
C 4927	3	253	810	744	3.7	35	20	7839	12.84	113	5	ND	2	189	6	23	2	2	9.81	.064	2	1	2.50	6	.01	2	.11	.01	.01	1	-	-	-	.11	.026			
C 4928	4	615	49	73	.8	13	5	11545	17.60	10	5	ND	7	455	1	2	2	20	10.42	.002	2	3	1.84	6	.01	2	.17	.01	.01	1	-	-	-	.03	.004			
C 4929	7	378	16299	32293	40.8	26	34	5338	15.88	35	5	8	3	164	322	48	2	3	7.01	.030	2	1	1.79	11	.01	2	.07	.02	.02	37	-	4.49	3.87	1.25	.122			
C 4930	2	48792	3292	1447	313.2	6256	108	1084	15.97	8229	22	402	2	7	22	42	2972	1	.07	.001	2	1	.05	9	.01	4	.01	.02	.01	1	5.99	-	-	9.18	20.320			
STD C	18	58	40	132	7.1	67	27	1027	3.94	39	18	7	39	49	17	17	22	56	.49	.084	37	60	.87	176	.08	37	1.83	.08	.14	13	-	-	-	-	-			

✓ ASSAY REQUIRED FOR CORRECT RESULT -

**GEOCHEMICAL ICP ANALYSIS**

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: Rock Chips    AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 5 1987    DATE REPORT MAILED: *Oct 13/87*    ASSAYER: *A. J. Toy* ..DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203    File # 87-4630

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
JW87-51F	1	8	12	22	.1	4	2	349	1.72	9	5	ND	1	2	1	2	2	1	.01	.010	2	2	.01	19	.01	2	.06	.01	.02	1	98
JW87-52R	1	9	19	49	.1	32	7	2610	5.93	6	5	ND	1	2	1	3	2	2	.02	.015	6	2	.05	38	.01	2	.09	.01	.02	2	3
JW87-53	1	8	72	10	.3	10	3	1409	3.00	5	5	ND	4	18	1	2	2	1	.44	.013	5	3	.11	19	.01	3	.09	.02	.03	1	2
JW87-54F	2	11	12	47	.1	22	5	3399	9.97	14	5	ND	2	4	1	3	2	5	.01	.012	7	6	.08	53	.01	4	.08	.01	.03	1	31
JW87-55F	1	29	9	57	.1	19	8	3230	4.21	6	5	ND	3	26	1	2	2	6	.54	.029	6	9	.29	52	.01	3	.48	.02	.03	1	1
JW87-56R	1	5	25	15	.1	14	4	1497	4.12	15	5	ND	2	2	1	3	2	2	.01	.011	10	2	.05	20	.01	2	.10	.01	.04	1	1
JW87-57	3	3	10	4	.1	2	1	1511	2.80	2	5	ND	1	1165	1	4	2	1	40.36	.013	2	1	.73	6	.01	2	.01	.01	.01	4	3
JW87-58R	1	4	10	1	.1	7	2	783	1.23	13	5	ND	1	116	1	3	2	1	6.19	.005	2	2	.03	8	.01	3	.01	.01	.02	5	22
PD87-33	1	29	60	8	1.5	17	6	119	3.12	5915	5	7	1	48	1	3	2	1	1.15	.014	2	1	.03	6	.01	3	.02	.01	.02	2	11230
TE87-142F	6	56	25325	17542	141.1	8	11	7656	14.97	105	5	ND	1	150	153	44	199	2	12.21	.006	2	14	1.25	4	.01	3	.01	.01	.01	2	620
TE87-143R	1	74	639	77	1.4	6	9	1976	3.25	34	5	ND	1	1078	1	4	2	1	21.02	.014	2	1	.29	7	.01	3	.21	.01	.01	1	48
TE87-144R	2	185	45	214	.2	27	15	860	19.33	12	8	ND	17	60	2	2	5	39	1.79	.020	22	68	2.35	14	.01	2	6.89	.01	.02	1	2
TE87-145F	1	41	1000	147	1.5	6	4	424	1.31	3	5	ND	2	5	1	2	3	1	.26	.004	3	2	.03	6	.01	4	.06	.01	.01	1	7
TE87-146R	1	167	44	23	1.7	36	53	220	13.29	127	5	6	2	6	1	5	2	1	.09	.001	2	7	.04	7	.01	9	.08	.01	.02	1	4520
TE87-147R	1	15	588	18	4.2	12	8	49	6.21	522	5	2	3	5	1	2	32	2	.05	.002	7	3	.01	22	.01	6	.16	.01	.10	77	2250
TE87-148R	5	25	310	154	2.3	33	17	753	13.69	1218	5	ND	4	41	1	3	26	3	2.10	.016	2	18	.24	16	.01	16	.17	.01	.08	36	780
TE87-149R	1	30	405	218	3.4	35	26	564	18.59	2157	5	2	3	27	4	2	64	2	.89	.009	2	3	.32	8	.01	3	.11	.01	.04	68	3350
STD C/AU-R	18	58	38	132	7.0	67	27	1026	3.96	39	17	7	37	48	18	18	21	57	.45	.084	36	61	.91	173	.08	36	1.84	.05	.12	12	510

*-SE 5/8/87*

*SE 5/8/87*

*TAIL IN DT FROM JOCK O'LEARY*

- ASSAY REQUIRED FOR CORRECT RESULT -

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B M AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: Rock Chips OUR ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 13 1987

DATE REPORT MAILED: Oct 22/87

ASSAYER: *D. J. ...* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-4819 Page 1

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	M	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPM	
JW-87-59R	1	10	9	65	.4	45	13	1334	8.54	48	5	ND	3	7	1	3	3	3	.14	.026	5	4	.12	21	.01	2	.07	.01	.05	1	8
JW-87-60R	1	7	119	80	.6	10	5	43	1.22	110	5	ND	1	2	1	2	2	1	.01	.003	2	2	.01	1	.01	3	.02	.01	.01	12	775
JW-87-60F	1	6	12	10	.2	3	1	124	.81	6	5	ND	1	1	1	2	3	1	.01	.002	2	2	.01	3	.01	3	.01	.01	.01	1	8
JW-87-61R	1	8	3	14	.1	7	3	375	1.48	3	5	ND	3	4	1	2	2	1	.03	.012	9	4	.02	16	.01	2	.09	.02	.03	1	10
JW-87-61F	1	7	4	4	.1	1	1	253	.90	2	5	ND	1	4	1	2	3	1	.06	.029	2	2	.01	5	.01	2	.01	.01	.01	1	1
JW-87-64R	1	7	6	23	.1	5	5	542	2.72	18	5	ND	2	2	1	2	2	1	.01	.008	6	3	.02	12	.01	3	.05	.01	.02	1	35
JW-87-65R	1	7	5	17	.2	6	3	479	2.55	10	5	ND	1	3	1	2	2	1	.02	.003	3	3	.03	9	.01	4	.05	.01	.02	1	155
JW-87-66R	1	12	2	4	.1	1	1	121	.81	2	5	ND	1	1	1	2	2	1	.01	.002	2	3	.01	2	.01	6	.01	.01	.01	1	8
JW-87-67R	1	59	9	46	.3	2	6	6232	10.56	13	6	ND	1	239	2	5	2	3	18.25	.006	3	2	3.69	5	.01	2	.01	.01	.01	1	1
JW-87-68R	1	1	23	12	.2	1	1	972	1.36	2	5	ND	1	977	1	2	6	1	32.81	.020	2	1	1.16	3	.01	6	.01	.01	.01	1	1
JW-87-69F	1	9	10	13	.2	3	2	434	1.71	2	6	ND	1	8	1	2	2	1	.53	.005	2	2	.13	6	.01	3	.03	.01	.02	1	2
JW-87-70R	1	3	3	6	.2	1	1	335	.36	2	5	ND	1	284	1	2	2	1	8.20	.126	2	1	.07	6	.01	13	.08	.07	.01	1	1
JW-87-71R	1	7	8	16	.1	1	1	174	.46	2	5	ND	1	45	1	2	2	1	1.19	.023	2	1	.02	5	.01	2	.01	.01	.01	2	1
JW-87-72F	1	90	19	99	.1	11	19	2009	53.11	5	5	ND	6	7	1	5	2	2	.09	.056	3	8	.08	10	.01	2	.41	.01	.05	1	9
JW-87-73R	1	6	4	1	.1	1	1	57	.32	2	5	ND	1	1	1	2	3	1	.01	.001	2	2	.01	2	.01	2	.01	.01	.01	6	12
JW-87-73F	1	18	21	19	2.6	18	57	352	31.54	598	5	25	2	2	1	5	8	1	.01	.016	2	12	.03	5	.01	8	.03	.01	.02	1	21810
JW-87-74R	1	6	35	6	.5	2	2	435	1.25	11	5	ND	1	30	1	2	2	1	.50	.005	2	4	.01	14	.01	4	.03	.01	.01	188	585
JW-87-75R	1	53	12	39	.1	5	11	1096	4.32	10	5	ND	2	53	1	2	2	20	1.53	.032	3	3	.42	13	.01	2	.49	.02	.03	30	192
PD-87-87	37	136	494	57638	.4	10	7	1285	4.07	19	5	ND	1	449	87	3	2	1	12.74	.034	2	1	1.35	13	.01	3	.08	.01	.05	8	9
PD-87-88	4	379	2	856	.5	15	9	825	2.91	94	5	ND	1	8	1	2	2	1	.16	.003	2	3	.04	11	.01	3	.05	.01	.01	5	310
PD-87-89	2	283	11	849	.5	9	6	5875	9.81	17	5	ND	1	186	3	2	2	2	11.33	.011	2	3	.66	2	.01	2	.01	.01	.01	9	34
PD-87-90	1	85	118	86	.1	49	27	971	5.06	11	5	ND	3	8	1	2	2	12	.23	.035	17	6	.21	15	.01	2	.43	.01	.03	1	6
PD-87-91	1	11	15	109	.1	23	14	989	9.23	3	5	ND	2	8	1	2	3	2	.14	.098	2	3	.08	16	.01	3	.04	.01	.02	2	1
PD-87-92	1	7	25	109	.3	6	7	5352	11.84	25	5	ND	1	232	2	2	2	5	17.41	.073	4	3	1.62	7	.01	2	.03	.01	.06	9	17
PD-87-93	1	10	16	33	.2	6	10	1438	2.74	16	8	ND	1	1197	1	2	2	1	30.14	.017	3	1	.77	5	.01	3	.03	.01	.01	1	2
PD-87-94	1	7	14	44	.1	9	7	1202	3.85	26	5	ND	7	140	1	2	2	2	8.93	.043	12	4	.57	53	.01	5	.35	.06	.13	2	1
PD-87-95	1	79	24	70	.1	17	17	1102	5.31	12	5	ND	2	813	1	3	5	1	22.03	.018	3	2	.74	33	.01	2	.12	.02	.06	1	1
PD-87-96	1	277	40	45	.3	10	27	820	6.29	36	5	ND	1	219	1	3	2	8	7.75	.077	2	1	2.11	35	.01	2	.28	.05	.11	1	1
PD-87-97	1	212	9	68	.2	11	22	965	5.65	43	5	ND	1	284	1	2	2	7	10.06	.076	2	2	3.05	33	.01	6	.24	.03	.11	1	2
TE-87-150R	1	9	19037	36	261.6	1	2	2290	3.52	31	5	ND	1	85	85	1120	3	1	2.48	.003	2	1	.57	2	.01	4	.01	.01	.01	1	124
TE-87-151R	36	40	24257	48188	99.5	2	3	1794	3.10	18	5	ND	2	13	587	97	2	1	.30	.012	2	2	.03	7	.01	6	.06	.01	.02	4	169
TE-87-152R	1	7	173	208	.6	3	5	5426	8.00	16	6	ND	1	295	2	2	3	4	23.96	.010	3	2	2.32	12	.01	2	.03	.01	.01	1	1
TE-87-153R	36	1042	18328	56226	226.9	1	1	278	.91	23	5	ND	1	76	370	1041	2	1	.14	.010	2	1	.02	7	.01	4	.10	.01	.01	1	107
TE-87-154R	9	38	22852	7165	90.0	15	10	1640	5.99	62	5	ND	3	39	111	80	2	2	8.35	.061	3	4	.12	22	.01	6	.13	.01	.06	5	106
TE-87-155R	1	7	1480	165	2.6	3	2	99	1.51	135	5	ND	1	4	2	2	2	1	.13	.004	3	2	.01	5	.01	3	.06	.01	.02	4	325
TE-87-156R	8	251	21643	3310	114.4	139	58	626	22.92	1669	5	4	2	29	20	91	26	4	.05	.013	2	3	.04	11	.01	2	.01	.01	.02	6	5310
STD C/AU-R	20	60	40	132	7.5	69	28	1071	3.97	40	21	8	40	52	18	18	20	60	.47	.092	40	63	.89	179	.07	36	1.85	.06	.14	12	510

- ASSAY REQUIRED FOR CUMULATIVE RESULT *for Pb > 10,000 PPM  
Zn > 20,000 PPM*

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	HG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	Z	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	Z	Z	PPM	PPM	Z	PPM	Z	Z	Z	Z	Z	PPM	PPM
TE-87-157R	48	65	18951	75453	82.1	31	24	10248	25.01	936	5	2	4	17	854	67	2	8	.19	.064	5	1	.04	23	.01	3	.09	.01	.07	5	3520
TE-87-158R	59	73	19963	99999	366.1	4	3	2260	6.48	95	5	ND	1	36	1565	532	7	1	.06	.008	2	1	.04	2	.01	2	.02	.01	.01	5	605
TE-87-159R	28	50	18190	31810	227.9	2	3	514	3.52	2198	5	2	1	18	295	1062	2	1	.06	.032	2	2	.01	3	.01	2	.03	.01	.01	2	820
TE-87-160R	40	51	20109	56716	354.8	2	2	139	2.03	118	5	3	1	5	168	440	2	1	.06	.035	2	1	.01	2	.01	2	.03	.01	.01	3	3460
TE-87-161R	19	135	20282	18484	275.7	1	3	484	4.66	327	5	ND	1	13	161	581	2	1	.02	.069	2	2	.01	7	.01	5	.07	.01	.02	5	750
TE-87-162R	10	14	4142	9499	6.0	19	6	859	1.88	185	5	ND	1	82	34	6	2	1	1.52	.003	5	1	.01	2	.01	9	.02	.01	.01	158	44
TE-87-163R	55	455	18772	98362	258.3	8	6	2978	6.92	256	5	ND	1	63	902	463	196	1	.17	.010	2	2	.03	2	.01	4	.01	.01	.01	3	605
TE-87-164R	11	24	13731	10900	33.2	12	8	3903	6.75	140	5	ND	1	70	138	31	4	2	12.17	.042	4	2	.36	19	.01	5	.10	.01	.06	3	65
TE-87-165R	4	14	5101	2521	11.1	8	4	392	1.45	61	5	ND	1	3	25	10	2	1	.04	.008	2	2	.01	4	.01	2	.01	.01	.01	33	114
TE-87-166R	4	21	21295	2041	88.5	7	8	771	5.00	1150	5	18	1	23	25	68	2	2	1.88	.012	2	3	.05	11	.01	11	.04	.01	.02	29	11980
TE-87-167R	2	5	20774	487	230.1	3	1	160	.45	58	5	ND	1	17	65	854	24	1	.01	.005	2	1	.01	2	.01	7	.01	.01	.01	5	202
TE-87-168R	7	37	21295	4631	74.6	18	12	1545	9.87	510	5	ND	2	21	45	60	18	2	1.49	.031	2	3	.03	4	.01	3	.01	.01	.01	1229	480
TE-87-169R	50	220	19439	87222	408.7	10	23	2000	15.79	268	5	3	3	33	1076	377	32	7	.36	.039	2	1	.04	7	.01	2	.01	.01	.04	1	3360
TE-87-170R	22	40	18656	23407	298.0	10	15	579	5.71	339	5	2	1	31	188	519	367	1	.91	.009	2	2	.06	4	.01	5	.02	.01	.01	2	1965
TE-87-171R	3	21	4630	1244	8.6	8	5	1551	2.43	9	5	ND	1	4	13	7	2	1	.04	.007	2	3	.05	29	.01	4	.14	.01	.02	9	38
TE-87-172R	1	10	1644	353	4.2	26	35	1078	9.15	38	5	ND	3	21	2	2	2	18	.65	.083	8	15	.35	59	.01	7	.68	.04	.08	1	17
TE-87-173R	1	4	474	160	.9	13	4	1445	4.50	11	5	ND	1	11	1	2	2	2	.32	.093	3	4	.06	25	.01	14	.14	.04	.01	5	11
STD C/AU-R	21	61	38	130	7.3	73	28	1114	3.99	42	20	8	40	55	20	18	22	61	.48	.098	42	59	.90	180	.07	37	1.88	.07	.15	12	525

TE-173R ✓  
PAC

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH JML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR HG BA TI V AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: P1-ROCK/CORE P2-ROCK N/A ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 16 1987

DATE REPORT MAILED: Oct 22/87

ASSAYER: D. J. ... DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-4942 Page 1

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	HG	BA	TI	B	AL	NA	K	W	AUX
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
JW87-39R	1	206	2	33	.1	19	25	1316	7.02	9	5	ND	1	175	1	2	3	11	8.95	.074	3	4	1.74	54	.01	6	.32	.04	.14	1	1
JW87-76F	1	6	2	34	.1	13	7	1181	4.78	5	5	ND	1	3	1	2	2	1	.04	.014	2	5	.06	17	.01	2	.07	.01	.03	1	1
JW87-77F	1	1	3	17	.1	3	1	397	1.03	2	5	ND	1	2	1	2	2	1	.01	.007	2	4	.01	9	.01	7	.04	.01	.02	1	1
JW87-78R	1	41	2	21	.1	41	14	480	3.50	5	5	ND	1	5	1	2	2	1	.03	.011	3	3	.03	12	.01	2	.08	.02	.03	1	1
JW87-79F	1	18	27	11	.2	7	3	265	1.01	4	5	ND	1	2	1	2	2	1	.01	.009	2	3	.01	7	.01	3	.06	.01	.02	1	1
JW87-80F	1	4	2	1	.1	1	1	91	.56	2	5	ND	1	1	1	2	2	1	.01	.004	2	1	.01	2	.01	2	.03	.01	.01	1	1
JW87-81R	1	7	5	9	.1	30	7	117	1.74	90	5	ND	5	4	1	2	2	1	.03	.012	18	4	.01	24	.01	2	.20	.02	.09	1	65
JW87-82R	1	6	2	10	.1	16	5	218	1.58	17	5	ND	3	10	1	2	2	1	.29	.012	8	3	.07	16	.01	3	.11	.01	.05	1	18
JW87-83F	1	15	2	12	.1	10	3	600	1.98	2	5	ND	1	7	1	2	2	1	.08	.050	2	3	.12	8	.01	8	.23	.01	.02	1	1
JW87-84R	2	20	1950	821	4.2	13	6	757	2.83	32	5	ND	4	3	1	5	2	1	.02	.012	8	4	.01	9	.01	5	.15	.02	.03	83	99
JW87-85R	1	4	2	3	.1	6	3	449	1.16	9	5	ND	1	1	1	2	2	1	.01	.005	2	2	.01	18	.01	9	.03	.01	.01	1	3
JW87-86R	1	5	23	10	.3	6	1	75	.84	42	5	ND	1	1	1	2	2	1	.01	.004	2	2	.01	3	.01	7	.03	.01	.01	1	260
JW87-87F	1	4	6	10	.1	2	1	1432	2.17	5	5	ND	1	447	1	5	2	1	12.30	.005	3	1	1.17	7	.01	7	.01	.01	.01	1	1
JW87-88R	2	28	9	8	.1	11	4	219	.98	2	5	ND	1	4	1	2	2	15	.06	.014	2	14	.29	7	.01	2	.33	.02	.01	1	5
JW87-89F	1	4	2	1	.2	3	1	177	.66	2	5	ND	1	4	1	2	2	1	.08	.003	2	2	.01	3	.01	6	.03	.01	.01	1	1
PDB7-98	2	48	8	48	.1	55	14	281	3.50	35	5	ND	10	18	1	2	4	2	.36	.034	14	5	.93	32	.01	2	.30	.01	.17	1	1
PDB7-99	2	41	17	55	.1	49	31	566	6.13	105	5	ND	10	19	1	2	2	2	.19	.042	18	5	.96	24	.01	5	.23	.01	.12	1	450
PDB7-100	1	30	32	32	.3	10	7	1968	3.30	25	5	ND	1	1477	1	2	4	1	31.21	.011	2	1	.45	22	.01	3	.05	.01	.02	1	1
PDB7-101	1	1022	15	93	.1	70	16	3988	33.27	10	5	ND	4	247	2	2	2	6	3.30	.012	2	6	1.52	4	.01	2	.27	.01	.03	1	15
PDB7-101 A	1	22	10	26	.1	14	7	1053	3.34	18	5	ND	3	419	1	7	3	1	13.14	.027	7	4	1.25	129	.01	3	.25	.02	.13	1	1
PDB7-102	1	66	74	397	.1	112	18	917	4.23	19	5	ND	1	50	4	2	2	6	1.86	.094	4	14	.16	52	.01	14	.22	.01	.08	1	1
PDB7-102 A	4	167	9	5	.1	45	26	262	3.58	2	5	ND	6	30	1	2	2	1	.81	.036	8	3	.30	28	.01	2	.25	.03	.10	1	4
PDB7-103	1	7	11	10	.2	3	2	749	1.47	6	5	ND	1	1173	1	2	6	1	34.44	.014	4	1	1.23	9	.01	2	.02	.01	.01	1	3
PDB7-103 A	1	95	122	46	.6	48	17	604	3.94	2	5	ND	5	107	1	2	3	4	2.82	.039	7	9	1.10	43	.01	5	.59	.02	.13	1	1
PDB7-104	1	24	19	32	.2	9	5	597	1.82	8	5	ND	3	887	1	2	8	1	25.94	.024	3	1	.65	45	.01	2	.13	.01	.07	1	1
PDB7-105	1	5327	7	101	4.3	49	70	5320	19.42	5	6	ND	1	142	2	2	2	11	9.57	.014	11	6	.35	9	.01	2	.57	.01	.02	6	35
PDB7-106	1	90	13	22	.1	5	8	3730	3.52	3	5	ND	1	1319	1	2	2	1	27.08	.015	3	3	.38	3	.01	2	.32	.01	.01	1	1
PDB7-107	1	650	376	60	2.5	102	15	2746	50.27	2	5	ND	5	11	1	5	6	1	.07	.017	3	9	.18	4	.01	4	1.06	.01	.03	1	6
PDB7-108	1	360	5	60	.3	21	9	510	3.44	2	5	ND	6	5	1	2	2	2	.12	.008	9	8	.48	18	.01	3	.60	.01	.07	1	1
PDB7-109	1	111	10	44	.1	23	12	372	4.17	7	5	ND	9	8	1	2	5	11	.14	.033	21	19	.81	41	.01	3	1.59	.01	.07	1	1
PDB7-501	2	453	142	145	3.1	101	142	319	20.78	140	5	ND	3	17	1	5	6	4	.32	.009	2	2	.09	5	.01	2	.02	.01	.04	1	1
TEB7-174R	1	11	2	1	.1	5	3	91	.64	5	5	ND	1	1	1	2	2	1	.01	.002	2	1	.01	2	.01	2	.02	.01	.01	1	3
TEB7-175F	1	92	2449	32	16.4	178	63	445	7.34	85	5	ND	1	1	1	2	26	1	.01	.004	2	2	.02	5	.01	2	.01	.01	.01	1	115
TEB7-176R	1	47	6	21	.3	9	3	220	1.78	96	5	ND	4	7	1	2	2	1	.19	.012	8	3	.02	15	.01	5	.10	.01	.05	1	940
TEB7-177R	1	11	44	19	.3	8	4	190	1.75	77	5	ND	3	1	1	2	2	1	.01	.005	6	3	.01	16	.01	4	.09	.01	.05	1	13
TEB7-178R	1	4	8	15	.1	38	15	472	2.54	30	5	ND	4	6	1	2	2	1	.04	.026	12	2	.02	18	.01	24	.11	.01	.05	1	16
STD C/AU-R	20	59	42	128	7.5	71	28	1205	4.05	40	18	8	38	54	19	17	20	59	.48	.094	40	63	.90	175	.07	34	1.88	.06	.14	12	510

Sim Lock

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	HG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	%	%	%	%	%	PPH	PPB
TE87-179R	1	4	2653	45	5.0	4	1	50	.70	98	5	ND	1	3	1	2	5	1	.01	.001	2	2	.01	4	.01	2	.03	.01	.02	1	49
TE87-180F	1	3	21	36	.1	6	4	2628	5.47	9	5	ND	1	493	1	4	2	1	17.81	.014	4	3	3.07	6	.01	2	.01	.01	.02	1	1
TE87-181F	2	48	25909	96	117.3	13	2	169	.45	23	5	ND	1	22	10	109	3	1	.39	.015	2	1	.01	3	.01	2	.01	.01	.01	1	4
TE87-182F	1	5	132	2	.3	5	2	53	.61	4	5	ND	1	1	1	2	2	1	.01	.002	2	2	.01	3	.01	4	.02	.01	.01	1	1
TE87-183F	1	8	69	22	.3	6	4	1024	2.69	2	5	ND	1	650	1	2	4	1	27.17	.020	4	3	1.79	4	.01	2	.02	.01	.01	1	1
TE87-184F	1	7	152	79	.2	46	17	2165	7.03	17	5	ND	1	334	1	2	2	14	14.38	.018	2	17	4.10	13	.01	2	.05	.01	.03	1	1
TE87-185F	6	15	149	11	.9	70	47	201	17.90	367	5	ND	1	9	1	2	2	3	.22	.003	2	1	.05	3	.01	2	.01	.01	.01	1	2
TE87-186R	1	229	15	59	.4	13	31	1186	6.71	56	5	ND	3	152	1	2	3	12	4.16	.097	4	2	.99	38	.01	5	.18	.04	.06	1	12
TE87-187R	1	61	12	62	.1	8	14	1172	6.23	29	5	ND	2	307	1	2	2	25	6.79	.115	4	2	1.35	39	.01	3	.13	.03	.05	1	1
TE87-188R	1	99	11	85	.1	8	27	1250	7.99	9	5	ND	4	103	1	2	3	14	3.75	.093	6	1	1.17	29	.01	2	.20	.05	.05	1	1
TE87-189R	1	3	10	38	.2	8	4	1451	3.68	10	5	ND	1	702	1	3	2	1	24.58	.013	5	3	6.52	12	.01	2	.02	.01	.01	1	1
TE87-190R	1	21	23	29	.2	8	4	433	1.45	7	5	ND	2	1190	1	2	6	1	26.59	.015	3	2	.62	29	.01	2	.07	.01	.04	1	42
STD C/AU-R	20	62	37	133	7.6	73	29	1049	4.04	41	20	8	39	55	19	18	18	61	.49	.092	41	58	.90	182	.07	37	1.88	.07	.14	12	485

# GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: ROCK/CORE AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 28 1987 DATE REPORT MAILED: *Nov 4/87* ASSAYER: *[Signature]* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-5248

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM	PPB
JW-87-90F	1	5	13	50	.1	5	2	1042	1.77	11	5	ND	1	22	1	2	2	1	.36	.012	2	3	.10	397	.01	2	.03	.02	.01	2	2
JW-87-91F	2	34	4	70	.7	84	18	852	4.37	5	5	ND	5	269	1	2	2	89	2.88	.215	16	81	3.14	1136	.14	4	1.80	.22	.41	1	3
JW-87-92R	1	4	91	17	.6	4	2	412	1.25	2	5	ND	1	14	1	3	2	1	.49	.010	2	4	.07	20	.01	2	.03	.02	.01	1	2
JW-87-93R	1	3	7	64	.2	10	4	1103	6.53	6	5	ND	2	10	1	2	2	1	.21	.020	2	3	.93	9	.01	3	.01	.02	.01	1	4
JW-87-94R	1	12	8	24	.1	17	5	586	2.47	4	5	ND	8	15	1	2	3	4	.33	.015	10	8	.26	58	.01	2	.23	.04	.03	1	5
JW-87-95R	1	16	2	24	.1	11	4	422	1.96	2	5	ND	13	8	1	2	2	5	.35	.018	12	15	.39	56	.01	2	.43	.04	.01	2	2
JW-87-96R	1	4	2	5	.1	12	3	282	1.25	108	5	ND	1	3	1	2	2	1	.04	.001	2	3	.01	17	.01	2	.02	.01	.01	1	142
JW-87-97F	1	19	81	113	.7	246	13	104	11.28	417	5	ND	1	2	1	2	2	1	.03	.001	2	1	.02	10	.01	2	.01	.01	.01	1	1540
PD-87-110	4	103	24	57	.9	20	18	9177	27.49	38	5	ND	4	64	1	2	2	3	3.69	.010	2	1	1.85	5	.01	2	.15	.01	.03	2	45
PD-87-111	5	83	30	91	.1	33	9	9766	41.96	33	5	ND	5	12	1	2	2	4	.30	.011	2	1	.93	6	.01	2	.26	.03	.03	2	110
PD-87-112	6	160	27	53	1.2	25	7	5924	33.52	3	5	ND	3	164	1	2	2	3	3.66	.004	2	1	1.29	7	.01	2	.16	.02	.01	2	6
PD-87-113	2	188	18	37	1.0	15	7	3099	27.35	4	5	ND	3	69	1	2	3	3	1.68	.002	2	1	.51	7	.01	2	.08	.03	.01	3	5
PD-87-114	4	65	19	131	.7	17	6	5285	22.31	8	5	ND	3	417	1	2	2	12	8.85	.001	2	1	1.48	6	.01	2	1.61	.01	.02	2	19
PD-87-115	1	131	22	40	1.3	2	3	766	32.16	2	5	ND	14	12	1	2	10	4	.04	.010	6	1	.03	7	.01	2	.17	.03	.07	3	9
PD-87-115A	2	15	2	6	.2	5	1	391	2.60	2	12	ND	1	17	1	2	2	1	.36	.001	2	4	.07	2	.01	2	.05	.02	.01	1	34
PD-87-116	2	247	22	49	1.3	22	4	5252	30.08	6	5	ND	5	116	1	2	6	3	3.41	.024	2	2	1.11	5	.01	2	.47	.02	.05	2	8
PD-87-118	4	80	17	56	.7	25	62	8885	23.38	14	5	ND	3	111	1	2	2	2	5.96	.003	2	1	1.92	2	.01	2	.04	.01	.01	2	9
PD-87-119	2	36	15	163	.5	926	96	3130	12.10	1855	5	ND	2	213	1	2	2	18	4.37	.041	3	244	5.05	22	.01	2	.90	.05	.07	2	7
56351	1	199	39	32	2.3	1032	35	1231	4.98	395	5	5	1	47	1	2	26	2	1.62	.001	2	12	.55	5	.01	2	.05	.02	.01	1	8610
STD C/AU-R	19	59	39	132	7.2	68	27	1029	3.97	42	23	7	39	49	17	18	21	56	.47	.087	37	61	.87	176	.08	34	1.78	.08	.13	12	515



S O I L   A N A L Y S E S

Cunningham Creek.

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1 TO P6-SOIL P7-ROCK AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

EXTRA COPY

DATE RECEIVED: AUG 28 1987 DATE REPORT MAILED: Sept 8/87 ASSAYER: D. J. DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-3707 Page 1

Table with columns: SAMPLE#, NO, CU, PB, ZN, AG, NI, CD, MN, FE, AS, U, AU, TH, SR, SB, BI, V, CA, P, LA, CR, MG, BA, TI, B, AL, NA, K, W, AU#, PPB. Rows list various sample IDs and their corresponding element concentrations in PPM and PPB.

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BT	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	%	PPH	%	%	%	PPH	PPB
CC 4+50W 0+50S	1	33	37	79	.1	31	15	434	4.52	35	5	ND	4	7	1	2	2	18	.04	.050	27	21	.46	75	.01	2	1.21	.01	.05	4	29
CC 4+50W 0+60S	1	54	90	127	.4	48	18	981	5.14	21	5	ND	5	18	1	2	2	23	.23	.069	31	25	.53	84	.03	2	1.19	.01	.05	6	18
STD C/AU-S	19	60	38	136	7.4	70	30	1071	4.02	39	23	8	36	49	19	16	20	56	.52	.085	37	61	.93	174	.08	37	1.80	.06	.13	14	48
CC 4+50W 0+70S	2	36	31	98	.1	38	13	319	5.16	21	5	ND	4	5	1	2	2	22	.01	.048	30	37	.59	41	.01	2	1.62	.01	.06	1	25
CC 4+50W 0+80S	1	20	18	41	.3	14	6	253	4.48	12	5	ND	1	5	1	2	2	26	.01	.070	21	27	.25	36	.01	2	1.07	.01	.05	2	32
CC 4+50W 0+90S	1	16	25	46	.1	18	7	163	3.63	11	5	ND	1	4	1	3	2	21	.01	.074	24	27	.30	31	.01	2	.98	.01	.04	1	14
CC 4+50W 1+00S	1	12	19	27	.3	11	4	101	2.72	11	5	ND	1	4	1	2	2	19	.01	.047	21	17	.14	20	.01	16	.74	.01	.02	1	4
CC 4+50W 1+10S	2	29	41	67	.2	25	11	1010	5.23	18	5	ND	1	5	1	3	2	23	.01	.110	26	24	.26	24	.01	2	.89	.01	.04	1	13
CC 4+50W 1+20S	1	17	16	33	.1	5	5	344	2.79	12	5	ND	1	4	1	4	2	16	.01	.068	19	15	.11	22	.01	2	.63	.01	.02	1	21
CC 4+50W 1+30S	1	47	25	80	.6	29	18	1905	5.83	20	5	ND	1	5	1	2	2	24	.02	.078	22	26	.38	43	.01	2	1.13	.01	.03	1	33
CC 4+50W 1+40S	1	18	22	40	.3	11	8	1374	3.54	8	5	ND	1	5	1	2	2	22	.01	.074	21	18	.14	50	.01	3	.80	.01	.04	2	17
CC 4+50W 1+50S	1	12	20	33	.1	7	5	884	2.66	7	5	ND	1	5	1	2	2	25	.01	.049	23	11	.09	37	.01	2	.62	.01	.03	4	400
CC 4+50W 1+60S	1	32	184	240	.3	23	12	577	4.97	16	5	ND	1	6	2	2	2	21	.05	.062	20	23	.29	34	.01	3	1.20	.01	.03	1	10
CC 4+50W 1+70S	1	33	67	125	.2	36	22	1465	9.57	5	5	ND	1	3	1	4	2	10	.01	.090	19	8	.05	21	.01	2	.49	.01	.02	1	1
CC 4+50W 1+80S	1	27	25	50	.1	16	9	490	5.64	10	5	ND	1	3	1	2	2	12	.01	.067	28	8	.04	21	.01	2	.47	.01	.02	1	1
CC 4+50W 1+90S	1	17	34	33	.1	8	5	499	4.03	6	5	ND	1	4	1	2	2	11	.01	.065	22	6	.03	24	.01	2	.38	.01	.03	6	9
CC 4+50W 2+00S	2	71	60	87	.5	23	19	4017	10.11	51	5	ND	1	5	1	2	2	24	.01	.093	14	11	.08	56	.01	4	.65	.01	.03	8	17
CC 4+50W 2+10S	1	27	40	71	.4	16	12	1800	5.88	17	5	ND	1	6	1	2	2	29	.01	.074	19	17	.11	64	.01	2	1.01	.01	.03	3	1
CC 4+50W 2+20S	1	32	44	64	.1	7	10	634	5.58	17	5	ND	1	4	1	2	2	26	.01	.073	11	9	.06	28	.01	2	.55	.01	.01	2	1
CC 4+50W 2+30S	1	36	26	53	.1	9	10	388	5.18	10	5	ND	1	4	1	2	2	20	.01	.064	12	9	.04	26	.01	2	.40	.01	.02	1	1
CC 4+50W 2+40S	1	13	25	66	.1	11	12	958	4.53	6	5	ND	1	14	1	2	2	31	.27	.073	13	22	.15	70	.02	12	.93	.01	.04	1	1
CC 4+50W 2+50S	1	14	11	150	.1	33	18	586	6.31	9	5	ND	1	15	1	2	2	28	.23	.108	18	33	.86	69	.01	2	2.09	.01	.04	1	1
CC 4+50W 2+60S	1	40	28	111	.1	14	15	3474	4.66	7	5	ND	1	28	1	2	2	49	.50	.094	21	21	.48	93	.02	3	1.62	.01	.05	1	1
CC 4+50W 2+70S	1	47	18	78	.2	12	18	838	6.66	10	5	ND	1	14	1	2	3	82	.19	.069	12	18	.85	41	.02	2	1.90	.01	.03	1	1
CC 4+50W 2+80S	1	64	24	86	.1	15	19	1908	6.88	10	5	ND	1	7	1	2	2	44	.06	.102	12	15	.32	56	.01	3	1.14	.01	.03	1	2
CC 4+50W 2+90S	1	22	24	47	.1	14	8	835	4.13	10	5	ND	1	5	1	2	2	28	.01	.080	18	16	.17	38	.01	2	.93	.01	.04	1	1
CC 4+50W 3+00S	1	45	32	76	.4	19	16	1949	5.51	15	5	ND	1	9	1	2	2	28	.10	.087	18	16	.28	59	.01	2	1.04	.01	.03	1	1
CC 3+50W 0+00	2	31	64	220	.6	38	17	1297	4.61	29	5	ND	1	19	2	4	2	14	.29	.089	18	20	.28	45	.01	2	.99	.01	.06	9	45
CC 3+50W 0+10S	1	22	42	86	.6	21	10	459	4.22	25	5	ND	1	9	1	5	2	19	.04	.077	21	18	.16	42	.01	3	.88	.01	.06	5	18
CC 3+50W 0+20S	2	23	41	76	.1	24	11	454	4.89	31	5	ND	1	8	1	2	2	18	.09	.106	22	20	.19	42	.01	2	.86	.01	.05	7	24
CC 3+50W 0+30S	1	16	32	44	.1	16	6	250	3.53	21	5	ND	1	6	1	2	2	20	.03	.067	24	18	.15	34	.01	2	.68	.01	.04	4	33
CC 3+50W 0+40S	2	32	28	88	.7	30	12	728	5.30	26	5	ND	1	9	1	2	3	20	.10	.064	26	27	.27	52	.01	2	1.20	.01	.05	5	12
CC 3+50W 0+50S	2	23	48	85	.6	24	16	1934	3.85	17	5	ND	1	17	1	2	3	23	.15	.099	20	22	.23	94	.01	3	1.16	.01	.08	1	14
CC 3+50W 0+60S	2	32	50	111	.9	36	16	1255	4.70	27	5	ND	1	31	1	2	2	24	.33	.126	20	26	.34	85	.01	3	1.48	.01	.09	1	8
CC 3+50W 0+70S	1	46	30	92	.2	57	20	678	4.98	47	5	ND	6	10	1	3	2	11	.06	.041	34	20	.43	90	.01	7	.99	.01	.06	2	47
CC 3+50W 0+80S	1	77	105	128	.4	47	20	1064	5.62	22	5	ND	4	27	1	2	2	45	.38	.077	24	24	.71	85	.03	4	1.53	.01	.05	7	5
CC 3+50W 0+90S	1	102	65	118	.4	50	23	1475	6.38	11	5	ND	10	30	1	5	2	33	.35	.064	33	24	.95	117	.02	2	1.94	.01	.06	3	8

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	MA	K	W	AU#
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	%	%	%	%	%	PPH	PPB
CC 3+50W 1+00S	3	31	35	95	.3	33	16	620	7.70	23	5	ND	2	4	1	4	3	22	.01	.072	19	33	.39	32	.01	2	1.43	.01	.02	1	10
CC 3+50W 1+10S	2	11	17	35	.3	10	4	176	2.76	6	5	ND	1	5	1	2	3	17	.06	.055	17	16	.17	27	.01	2	.71	.01	.02	3	6
CC 3+50W 1+20S	2	51	58	133	.5	45	21	1657	5.70	21	5	ND	2	34	1	3	2	19	.60	.111	20	23	.51	69	.01	2	1.16	.01	.04	1	15
CC 3+50W 1+30S	1	20	27	45	.4	12	6	374	4.68	14	5	ND	1	7	1	2	2	25	.08	.060	17	18	.17	39	.01	2	.85	.01	.02	2	2
CC 3+50W 1+40S	1	16	20	40	.5	10	5	413	4.06	9	5	ND	1	5	1	2	2	23	.02	.070	18	16	.14	34	.01	2	.79	.01	.03	2	11
CC 3+50W 1+50S	1	16	23	31	.3	6	4	285	3.22	9	5	ND	1	4	1	2	2	21	.01	.060	20	14	.12	28	.01	2	.72	.01	.02	1	27
CC 3+50W 1+60S	1	24	23	38	.3	10	10	930	3.90	15	5	ND	1	4	1	2	2	18	.01	.058	19	11	.12	27	.01	3	.72	.01	.03	1	4
CC 3+50W 1+70S	3	30	144	130	.3	29	18	2198	6.41	18	5	ND	1	10	1	6	2	21	.14	.138	17	19	.28	42	.01	2	1.35	.01	.03	2	14
CC 3+50W 1+80S	2	33	71	138	.2	22	15	3003	5.67	20	5	ND	1	24	1	4	3	19	.34	.157	15	17	.24	73	.01	4	1.24	.01	.03	1	5
CC 3+50W 1+90S	2	42	47	99	.8	24	18	1986	6.34	18	5	ND	1	48	1	2	2	25	.93	.097	12	19	.18	59	.01	2	1.05	.01	.03	1	24
CC 3+50W 2+00S	1	54	35	104	.3	21	15	1076	7.70	13	5	ND	1	6	1	2	2	27	.04	.088	17	16	.23	60	.01	2	1.01	.01	.02	1	8
CC 3+50W 2+10S	2	42	46	82	.4	23	16	1268	6.94	19	5	ND	1	4	1	6	6	21	.02	.077	19	17	.22	48	.01	2	1.06	.01	.02	3	2
CC 3+50W 2+20S	2	45	45	89	.4	24	15	1456	6.84	17	5	ND	1	5	1	5	7	21	.04	.082	18	15	.20	47	.01	4	1.03	.01	.03	1	1
CC 3+50W 2+30S	1	30	21	49	.3	10	8	1394	3.97	9	5	ND	1	4	1	8	2	20	.01	.078	18	13	.12	51	.01	2	.83	.01	.02	1	3
CC 3+50W 2+40S	1	59	51	140	.3	26	21	4578	6.35	15	5	ND	1	32	1	2	2	24	.49	.150	24	21	.29	123	.01	2	1.53	.01	.03	1	2
CC 3+50W 2+50S	1	23	22	68	.3	10	9	520	5.17	10	5	ND	1	5	1	2	2	25	.03	.064	18	15	.13	68	.01	2	.99	.01	.03	2	1
CC 3+50W 2+60S	1	23	28	56	.3	13	8	347	5.06	10	5	ND	1	7	1	2	2	26	.07	.054	17	15	.12	59	.01	2	.92	.01	.02	1	1
CC 3+50W 2+70S	1	41	43	121	.6	20	17	2411	5.67	17	5	ND	1	13	1	2	2	28	.12	.088	17	23	.28	76	.01	2	1.44	.01	.04	1	17
CC 3+50W 2+80S	1	59	98	153	.5	55	23	1761	8.38	26	5	ND	4	14	1	2	2	10	.17	.103	41	14	.17	51	.01	2	1.66	.01	.02	1	3
CC 3+50W 2+90S	1	28	33	75	.5	12	12	750	5.04	13	5	ND	1	6	1	2	2	18	.04	.087	16	11	.10	31	.01	2	.76	.01	.03	1	1
CC 3+50W 3+00S	1	23	47	108	.4	19	12	1805	4.91	14	5	ND	1	16	1	2	2	22	.28	.099	22	16	.17	79	.01	2	1.09	.01	.03	1	2
CC 2+50W 0+00	1	41	43	90	.2	39	22	774	5.59	26	5	ND	2	10	1	2	2	15	.15	.078	22	20	.26	41	.01	2	1.11	.01	.05	1	1
CC 2+50W 0+10S	2	33	90	91	.3	31	22	1826	4.86	33	5	ND	1	10	1	2	2	18	.13	.119	20	18	.24	52	.01	3	1.22	.01	.05	1	10
CC 2+50W 0+20S	4	28	39	90	.1	30	17	1385	5.63	36	5	ND	1	16	1	2	16	8	.30	.107	16	17	.38	42	.01	5	1.04	.01	.01	1	2
CC 2+50W 0+30S	1	29	47	102	.7	30	15	1550	4.33	26	5	ND	2	32	1	2	2	15	.76	.196	27	19	.31	57	.01	3	1.31	.01	.05	1	6
CC 2+50W 0+40S	2	30	46	122	.3	27	19	1885	5.34	31	5	ND	1	16	1	2	2	23	.20	.139	22	25	.31	61	.01	3	1.55	.01	.05	1	1
CC 2+50W 0+50S	1	34	29	86	.1	38	15	465	4.89	56	5	ND	1	7	1	2	2	13	.04	.046	29	21	.36	54	.01	3	1.17	.01	.05	2	19
CC 2+50W 0+60S	1	27	37	104	.4	34	13	928	3.56	32	5	ND	1	26	1	2	2	14	.35	.071	20	18	.33	96	.01	4	.98	.01	.05	1	4
CC 2+50W 0+70S	2	39	56	110	.2	46	20	590	5.26	34	5	ND	2	9	1	5	2	16	.09	.061	30	26	.43	48	.01	2	1.19	.01	.05	2	42
CC 2+50W 0+80S	1	45	44	92	.2	50	20	598	4.95	43	5	ND	4	8	1	2	2	11	.06	.043	31	21	.44	72	.01	2	1.16	.01	.05	3	30
CC 2+50W 0+90S	1	30	69	95	.2	34	16	849	4.60	35	5	ND	2	11	1	3	2	16	.09	.089	21	22	.39	84	.01	2	1.31	.01	.06	1	1
CC 2+50W 1+00S	1	48	49	104	.3	50	19	681	4.72	46	5	ND	4	14	1	2	2	11	.16	.059	24	18	.39	47	.01	3	.89	.01	.05	1	86
CC 2+50W 1+10S	2	16	75	79	.1	21	10	454	4.50	19	5	ND	1	6	1	2	2	18	.02	.066	18	26	.30	36	.01	2	1.09	.01	.04	6	34
CC 2+50W 1+20S	1	32	43	80	.3	19	12	752	5.59	20	5	ND	1	10	1	2	2	22	.13	.085	15	24	.24	51	.01	6	1.03	.01	.04	2	7
CC 2+50W 1+30S	1	42	36	120	1.6	28	15	1926	5.98	23	5	ND	2	52	1	2	2	20	.84	.187	14	24	.31	66	.01	12	1.61	.01	.05	2	8
CC 2+50W 1+40S	1	29	31	76	.4	21	10	529	5.76	23	5	ND	1	9	1	2	2	30	.11	.070	18	26	.22	57	.01	2	1.04	.01	.05	1	11
STD C/AU-S	19	61	42	132	7.4	67	29	1050	4.12	41	24	7	37	49	18	16	21	55	.49	.097	37	60	.90	180	.07	33	1.86	.06	.13	14	51

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TJ	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
CC 2+50W 1+50S	1	42	29	87	.1	23	14	1513	6.71	27	5	ND	2	12	1	6	2	22	.13	.084	15	22	.22	53	.01	3	1.07	.01	.04	6	16
CC 2+50W 1+60S	1	19	26	77	.1	14	8	374	4.85	17	5	ND	1	6	1	2	2	26	.03	.065	19	22	.22	46	.01	2	1.12	.01	.03	1	10
CC 2+50W 1+70S	1	22	21	64	.1	17	8	428	5.62	14	5	ND	1	5	1	2	2	29	.01	.058	17	25	.21	39	.01	2	1.00	.01	.04	1	2
CC 2+50W 1+80S	1	29	130	127	.3	24	13	800	5.53	20	5	ND	1	6	1	6	2	24	.03	.065	18	27	.28	38	.01	2	1.39	.01	.04	1	9
CC 2+50W 1+90S	1	11	15	27	.1	9	4	123	2.66	14	5	ND	1	4	1	3	2	18	.01	.033	20	14	.13	20	.01	3	.76	.01	.02	1	3
STD C/AU-S	19	60	42	130	7.3	71	28	1034	4.03	40	19	8	37	48	19	17	21	56	.49	.083	36	59	.88	175	.08	34	1.80	.06	.12	13	48
CC 2+50W 2+00S	1	30	18	48	.2	15	9	516	5.11	17	5	ND	1	3	1	2	2	20	.01	.058	21	15	.15	22	.01	2	.75	.01	.02	1	7
CC 2+50W 2+10S	1	21	30	45	.1	10	7	931	4.68	17	5	ND	1	4	1	2	2	26	.01	.063	17	13	.09	27	.01	3	.76	.01	.03	9	30
CC 2+50W 2+20S	1	16	16	21	.1	5	3	231	2.30	10	5	ND	1	4	1	4	2	13	.01	.076	19	6	.04	21	.01	3	.47	.01	.03	1	2
CC 2+50W 2+30S	1	23	15	34	.1	11	7	431	4.45	13	5	ND	1	3	1	2	2	14	.01	.060	22	9	.04	22	.01	2	.57	.01	.03	1	1
CC 2+50W 2+40S	1	26	18	39	.1	6	7	476	4.17	12	5	ND	1	4	1	2	2	21	.01	.070	17	12	.09	32	.01	2	.71	.01	.03	2	48
CC 2+50W 2+50S	1	40	174	184	1.4	37	18	10152	9.15	41	11	ND	1	25	3	3	2	21	.30	.176	56	14	.10	131	.02	5	1.60	.01	.04	4	1
CC 2+50W 2+60S	1	31	34	51	.1	15	10	477	6.04	22	5	ND	1	3	1	4	2	25	.01	.073	13	13	.13	36	.01	2	.86	.01	.03	10	12
CC 2+50W 2+70S	1	87	34	124	.1	30	26	2609	8.62	28	5	ND	3	19	2	2	2	22	.25	.082	17	11	.30	61	.01	5	.91	.01	.03	9	25
CC 2+50W 2+80S	1	34	53	137	.1	16	8	318	5.65	24	5	ND	1	21	2	2	2	26	.19	.074	15	23	.26	62	.02	2	1.54	.01	.04	1	9
CC 2+50W 2+90S	1	43	50	168	.2	20	14	2397	4.01	13	5	ND	2	88	2	3	2	19	1.24	.199	14	21	.31	91	.02	2	1.66	.01	.05	1	5
CC 2+50W 3+00S	1	61	45	145	.6	32	20	2550	5.06	19	5	ND	2	76	1	2	2	22	1.12	.142	21	22	.42	95	.02	7	1.91	.01	.06	1	7
CC 1+50W 0+00	1	27	132	92	.4	27	14	1881	3.64	16	5	ND	1	11	1	2	2	24	.12	.060	23	15	.14	161	.01	21	.73	.01	.07	6	2
CC 1+50W 0+10S	1	32	270	107	.5	30	19	2447	4.60	19	5	ND	1	12	1	2	2	22	.15	.102	20	20	.21	76	.01	6	1.08	.01	.08	9	2
CC 1+50W 0+20S	1	24	69	68	.5	21	10	554	3.85	17	5	ND	1	8	1	2	2	22	.06	.073	22	19	.17	49	.01	8	.91	.01	.07	5	1
CC 1+50W 0+30S	1	27	51	76	.1	24	9	481	4.09	18	5	ND	1	8	1	2	2	22	.06	.074	23	19	.18	67	.01	5	.91	.01	.07	7	1
CC 1+50W 0+40S	1	43	79	106	.9	36	19	1856	4.62	27	5	ND	2	19	1	2	2	19	.25	.126	21	23	.27	74	.01	2	1.33	.01	.08	6	3
CC 1+50W 0+50S	1	47	71	119	1.0	38	21	1996	4.56	24	5	ND	2	22	1	2	2	19	.32	.162	23	22	.27	74	.01	4	1.64	.01	.09	3	6
CC 1+50W 0+60S	1	42	51	127	1.1	39	20	1573	4.93	37	5	ND	3	24	1	2	2	17	.31	.154	21	21	.31	66	.01	5	1.59	.01	.07	4	7
CC 1+50W 0+70S	1	40	40	129	.2	41	19	948	4.93	37	5	ND	2	20	1	2	2	18	.25	.114	22	25	.35	63	.01	9	1.42	.01	.07	5	16
CC 1+50W 0+80S	1	42	47	115	.2	44	18	788	4.77	47	5	ND	3	10	1	2	2	15	.09	.068	25	22	.39	62	.01	2	1.24	.01	.07	3	27
CC 1+50W 0+90S	1	41	32	121	.1	40	17	536	4.86	34	5	ND	3	10	1	2	2	18	.09	.054	27	25	.37	60	.01	2	1.21	.01	.08	10	18
CC 1+50W 1+00S	1	18	27	61	.3	19	9	308	2.90	18	5	ND	1	10	1	2	2	18	.07	.072	21	21	.27	93	.01	3	.97	.01	.07	1	51
CC 1+50W 1+10S	1	17	22	60	.1	17	7	278	3.04	24	5	ND	1	8	1	3	2	16	.07	.073	23	20	.26	88	.01	2	.93	.01	.08	1	27
CC 1+50W 1+20S	1	52	72	112	.1	60	24	681	5.35	47	5	ND	13	23	1	2	2	19	.31	.073	36	26	.55	70	.01	5	1.13	.01	.08	1	33
CC 1+50W 1+30S	1	48	47	122	.1	64	24	802	5.42	38	5	ND	13	19	1	5	4	20	.21	.070	40	28	.56	73	.02	3	1.23	.01	.09	1	24
CC 1+50W 1+40S	1	23	44	65	.4	14	8	594	7.35	21	5	ND	2	4	1	2	2	27	.01	.056	17	21	.12	31	.01	3	1.07	.01	.03	1	5
CC 1+50W 1+50S	1	15	15	32	.9	8	4	209	2.95	14	5	ND	1	5	1	2	2	21	.01	.044	26	16	.13	30	.01	2	.83	.01	.05	1	15
CC 1+50W 1+60S	1	10	32	45	1.2	16	5	119	3.70	11	5	ND	1	5	1	2	2	26	.01	.040	27	28	.29	39	.01	2	1.24	.01	.04	1	12
CC 1+50W 1+70S	1	26	202	64	.5	15	12	792	4.57	12	5	ND	1	6	1	2	2	20	.01	.070	18	18	.19	28	.01	2	1.10	.01	.04	1	21
CC 1+50W 1+80S	1	31	34	67	.1	16	10	1086	3.63	17	5	ND	1	6	1	2	2	18	.01	.076	20	20	.22	63	.01	3	1.11	.01	.05	1	38
CC 1+50W 1+90S	1	38	35	99	.3	30	12	1205	4.47	18	5	ND	1	9	1	3	2	21	.04	.084	22	26	.33	61	.01	4	1.23	.01	.05	1	12

IMPERIAL METALS PROJECT-4203 FILE # 87-3707

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU+ PPB
CC 1+50W 2+00S	1	30	30	150	.4	25	11	2277	4.49	20	10	ND	1	37	1	2	2	21	.43	.129	16	23	.23	90	.01	2	1.34	.01	.06	2	29
CC 1+50W 2+10S	1	24	39	110	.2	23	10	2478	4.64	15	5	ND	1	11	1	2	2	23	.07	.103	17	21	.20	77	.01	2	1.27	.01	.06	1	16
CC 1+50W 2+20S	1	56	119	136	.2	40	25	2052	6.97	49	5	ND	2	17	1	2	2	18	.19	.066	26	16	.27	65	.01	2	1.08	.01	.04	10	210
CC 1+50W 2+30S	1	25	34	51	.1	15	6	327	4.91	35	5	ND	1	7	1	2	2	23	.04	.067	20	14	.10	30	.01	2	.92	.01	.04	7	76
CC 1+50W 2+40S	1	39	126	167	1.5	41	16	2873	10.32	63	5	ND	1	50	2	2	2	17	.74	.129	16	17	.18	93	.01	2	1.07	.01	.05	4	360
CC 1+50W 2+50S	1	32	63	223	.6	31	14	6323	5.98	61	5	ND	1	26	2	2	2	20	.62	.187	15	20	.16	128	.01	3	1.45	.01	.06	1	15
CC 1+50W 2+60S	1	23	127	84	.4	13	8	1183	7.18	30	5	ND	1	4	1	2	2	28	.01	.076	21	11	.07	26	.01	2	.71	.01	.02	10	32
CC 1+50W 2+70S	1	13	45	37	.1	9	4	213	2.91	10	5	ND	1	4	1	5	2	11	.01	.087	25	9	.05	28	.01	2	.58	.01	.04	1	5
CC 1+50W 2+80S	1	31	33	77	.1	11	9	819	4.29	14	5	ND	1	6	1	2	2	29	.01	.091	23	17	.20	49	.01	2	1.23	.01	.04	1	12
CC 1+50W 2+90S	1	23	35	100	.1	14	9	983	3.94	16	5	ND	1	6	1	2	2	20	.02	.089	19	16	.17	48	.01	2	.98	.01	.04	1	8
CC 1+50W 3+00S	1	28	53	208	.3	20	15	2929	5.58	18	5	ND	1	24	1	2	2	23	.27	.143	16	16	.20	96	.01	2	1.08	.01	.06	1	26
CC 0+50W 0+00	3	30	54	100	.2	31	16	636	4.32	16	5	ND	1	9	1	2	2	21	.06	.110	23	25	.35	59	.01	2	1.38	.01	.06	1	6
CC 0+50W 0+10S	2	34	71	142	.3	31	20	1158	4.84	20	5	ND	1	12	1	2	2	22	.15	.125	24	25	.37	68	.01	2	1.54	.01	.08	3	3
CC 0+50W 0+20S	2	51	67	132	.1	60	20	658	5.21	39	5	ND	5	9	1	2	2	16	.04	.043	39	26	.52	69	.01	2	1.23	.01	.07	1	36
CC 0+50W 0+30S	3	42	50	147	.1	48	21	992	5.06	25	5	ND	2	11	1	2	2	18	.13	.078	28	28	.50	61	.01	2	1.30	.01	.08	2	35
CC 0+50W 0+40S	3	45	72	197	.1	51	18	707	4.84	33	5	ND	2	10	1	2	3	16	.09	.064	33	26	.48	55	.01	2	1.16	.01	.07	3	36
CC 0+50W 0+50S	3	47	57	202	.1	56	20	673	5.07	32	5	ND	4	10	1	2	11	16	.06	.053	36	29	.54	66	.01	7	1.23	.01	.08	2	52
CC 0+50W 0+60S	3	85	812	1499	.8	56	18	750	5.00	42	5	ND	2	14	4	2	2	15	.21	.065	28	28	.46	95	.01	3	1.14	.01	.09	11	710
CC 0+50W 0+70S	3	42	132	212	.4	52	21	805	4.91	24	5	ND	2	11	1	2	2	18	.13	.064	29	29	.51	56	.01	2	1.29	.01	.07	1	550
CC 0+50W 0+80S	2	39	147	161	.1	45	19	641	4.56	19	5	ND	3	9	1	2	2	17	.07	.044	36	28	.53	50	.01	4	1.15	.01	.07	2	45
CC 0+50W 0+90S	2	20	19573	189	25.1	10	4	99	3.71	254	5	ND	1	13	1	17	14	4	.07	.049	9	9	.08	32	.01	2	.21	.01	.03	212	2010
CC 0+50W 1+00S	1	16	1514	136	3.5	11	4	117	3.63	72	5	ND	1	5	1	4	2	4	.03	.045	12	10	.12	14	.01	2	.30	.01	.04	86	360
CC 0+50W 1+10S	1	23	21	76	.1	20	15	817	3.86	17	5	ND	1	7	1	2	2	23	.02	.089	26	27	.34	58	.01	2	1.35	.01	.07	1	14
CC 0+50W 1+20S	2	22	94	91	.3	32	13	785	3.72	14	5	ND	1	12	1	2	2	27	.11	.072	28	37	.60	78	.01	2	1.27	.01	.06	1	3
CC 0+50W 1+30S	1	15	12	41	.1	13	5	262	3.54	4	5	ND	1	10	1	2	2	21	.10	.048	25	15	.11	41	.01	2	.69	.01	.05	1	6
CC 0+50W 1+40S	1	14	22	63	.1	16	10	401	4.86	13	5	ND	1	6	1	2	2	21	.01	.069	27	20	.20	42	.01	2	.90	.01	.04	1	24
CC 0+50W 1+50S	1	14	11	48	.2	11	8	1402	3.05	11	5	ND	1	11	1	2	2	20	.13	.057	27	14	.15	94	.01	2	.83	.01	.06	1	46
CC 0+50W 1+60S	1	21	9	37	.8	11	7	208	2.92	3	5	ND	1	9	1	2	2	18	.10	.052	27	13	.11	56	.01	2	1.20	.01	.03	1	7
CC 0+50W 1+70S	1	26	46	89	.9	19	9	2085	3.18	14	5	ND	1	23	1	2	2	19	.52	.182	19	16	.25	91	.01	3	1.46	.01	.05	1	1
CC 0+50W 1+80S	1	9	9	27	.1	8	2	39	1.94	6	5	ND	1	4	1	4	5	16	.01	.042	25	10	.08	36	.01	2	.75	.01	.02	1	1
CC 0+50W 1+90S	1	8	4	11	.2	4	1	33	.94	2	5	ND	2	6	1	2	5	6	.01	.041	24	3	.02	23	.01	2	.51	.01	.03	1	1
CC 0+50W 2+00S	1	2	10	23	.1	7	3	204	2.03	5	5	ND	1	4	1	2	2	17	.01	.053	23	11	.03	24	.01	3	.55	.01	.04	1	23
CC 0+50W 2+10S	1	15	68	72	.3	12	9	753	6.61	21	5	ND	1	4	1	2	2	23	.01	.058	18	16	.09	25	.02	3	.96	.01	.03	1	1
CC 0+50W 2+20S	1	18	106	85	.3	19	17	1585	7.62	33	5	ND	1	9	1	2	8	20	.06	.091	19	16	.10	43	.01	2	1.31	.01	.04	3	1
CC 0+50W 2+30S	1	34	58	76	.2	19	9	486	6.99	18	5	ND	1	6	1	2	2	21	.01	.066	25	17	.17	32	.01	2	.99	.01	.03	2	1
CC 0+50W 2+40S	1	23	31	34	.1	9	4	196	3.84	17	5	ND	1	5	1	2	2	20	.01	.044	30	12	.08	27	.01	3	.99	.01	.03	2	12
STD C/AU-S	19	58	37	133	7.1	67	29	1052	4.06	41	19	8	37	49	18	16	22	56	.48	.091	36	59	.89	177	.08	33	1.82	.06	.14	13	52

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
CC 0+50W 2+50S	1	28	23	40	.3	15	6	360	3.40	17	5	ND	4	4	1	2	6	8	.01	.083	30	11	.06	21	.01	4	.53	.01	.02	1	1
CC 0+50W 2+60S	1	173	79	119	.1	42	20	6219	14.68	37	5	ND	5	16	1	2	2	19	.10	.078	29	16	.22	135	.01	2	.97	.01	.06	9	265
CC 0+50W 2+70S	1	19	19	33	.2	8	6	672	3.34	12	5	ND	2	5	1	2	2	17	.01	.060	22	13	.08	34	.01	2	.70	.01	.05	2	6
CC 0+50W 2+80S	1	32	65	72	.4	25	12	672	6.43	22	5	ND	3	5	1	2	2	20	.01	.095	24	18	.23	33	.01	2	.93	.01	.05	3	106
CC 0+50W 2+90S	1	21	51	50	.2	13	7	435	4.07	16	5	ND	3	5	1	2	2	24	.01	.048	25	18	.20	37	.01	2	1.05	.01	.04	1	7
CC 0+50W 3+00S	1	14	32	36	.2	12	4	297	3.62	15	5	ND	2	5	1	2	2	20	.01	.065	26	10	.05	24	.01	2	.67	.01	.05	1	10
STD C/AU-S	20	62	38	133	7.3	73	28	1123	4.19	42	19	8	40	52	18	17	16	61	.50	.091	41	58	.90	182	.08	34	1.84	.07	.16	13	52

GEOCHEMICAL ICP ANALYSIS

KATR A COPY

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR NM FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1 TO P5 SOIL P6 ROCK AUT ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: SEPT 5 1987

DATE REPORT MAILED: Sept 16/87 ASSAYER: DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-3937 Page 1

Table with columns: SAMPLE#, NO, CU, PB, ZN, AG, NI, CD, MN, FE, AS, U, AU, TH, SR, CO, SB, BI, V, CA, P, LA, CR, MG, BA, TI, B, AL, NA, K, W, AU# and corresponding numerical data for various samples.



SAMPLE #	ND	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	M	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	PPM	PPM	
CC 6+00W 2+60S	1	19	17	59	.3	17	6	394	4.35	12	8	ND	4	3	1	2	2	23	.02	.058	23	23	.31	37	.01	2	.99	.01	.03	1	4
CC 6+00W 2+70S	1	31	25	77	.6	27	13	946	3.87	12	5	ND	4	23	1	2	2	26	.42	.093	19	27	.37	93	.01	3	1.32	.02	.04	1	1
CC 6+00W 2+80S	1	37	21	83	.1	31	11	371	4.23	18	5	ND	4	8	1	3	2	22	.13	.043	19	25	.40	90	.01	2	1.03	.01	.04	34	3
CC 6+00W 2+90S	1	19	23	52	.2	16	6	273	4.00	12	5	ND	3	5	1	2	2	33	.05	.046	22	28	.21	48	.01	2	.96	.01	.04	2	1
CC 6+00W 3+00S	1	40	33	119	.4	32	18	1015	5.00	17	5	ND	6	17	1	2	2	26	.40	.094	19	29	.45	110	.01	2	1.65	.02	.06	1	1
CC 6+00W 3+10S	1	42	26	91	.4	34	15	1019	4.17	14	5	ND	5	14	1	2	2	19	.32	.077	17	23	.42	87	.01	3	1.17	.01	.05	1	93
CC 6+00W 3+20S	1	41	35	89	.1	31	15	953	4.76	17	5	ND	4	10	1	2	2	25	.13	.079	21	27	.41	95	.01	2	1.43	.01	.05	1	8
CC 6+00W 3+30S	1	37	79	94	.4	25	14	1053	4.99	15	5	ND	3	15	1	2	2	27	.30	.083	22	24	.35	82	.01	2	1.39	.02	.05	1	5
CC 6+00W 3+40S	1	51	39	125	.5	34	18	1520	5.36	19	5	ND	4	22	1	2	2	23	.49	.116	17	24	.46	100	.01	5	1.42	.02	.06	1	4
CC 6+00W 3+50S	1	41	34	95	.6	25	12	574	4.43	14	5	ND	3	19	1	2	2	27	.41	.081	23	25	.30	86	.01	2	1.34	.02	.04	1	3
CC 6+00W 3+60S	1	58	41	127	.6	34	18	1501	4.91	19	6	ND	4	31	1	2	2	22	.80	.147	19	31	.46	113	.01	5	1.52	.02	.05	1	4
CC 6+00W 3+70S	1	43	42	129	.9	31	16	1176	4.54	9	6	ND	4	31	1	2	2	22	.78	.172	20	25	.44	114	.01	2	1.66	.02	.07	1	10
CC 6+00W 3+80S	1	47	38	113	.5	32	16	1056	4.74	16	5	ND	4	17	1	2	2	23	.34	.136	23	29	.41	81	.01	2	1.55	.02	.06	1	16
CC 6+00W 3+90S	1	53	49	132	.7	37	18	1918	5.05	16	5	ND	4	25	1	2	2	23	.51	.188	22	29	.46	121	.01	7	1.70	.02	.06	1	8
CC 6+00W 4+00S	1	48	41	124	.4	43	19	907	5.10	18	5	ND	6	16	1	2	2	26	.28	.083	27	37	.57	87	.01	2	1.51	.02	.05	1	1
CC 6+00W 4+10S	1	45	40	120	.6	32	17	1157	5.23	17	5	ND	3	19	1	2	2	27	.34	.138	22	26	.42	120	.01	4	1.60	.02	.07	1	2
CC 6+00W 4+20S	1	46	45	111	.9	31	18	1591	4.74	14	5	ND	3	22	1	2	2	25	.37	.169	27	29	.41	110	.01	5	1.67	.02	.07	1	4
CC 6+00W 4+30S	2	52	49	137	.8	45	20	1691	5.32	19	5	ND	4	21	1	2	2	25	.33	.186	30	31	.47	112	.01	6	1.80	.02	.07	1	11
CC 6+00W 4+40S	1	38	43	120	.5	30	19	1783	4.75	20	5	ND	3	29	1	2	2	26	.52	.190	20	27	.43	109	.01	2	1.54	.02	.08	1	1
CC 6+00W 4+50S	1	31	34	94	.5	26	13	641	4.10	11	5	ND	3	15	1	2	2	25	.22	.099	24	26	.41	85	.01	2	1.19	.01	.05	1	58
CC 6+00W 4+60S	1	36	42	109	.5	30	16	1210	4.69	14	5	ND	3	20	1	2	2	26	.30	.149	22	26	.44	104	.01	5	1.49	.02	.08	1	5
CC 6+00W 4+70S	1	41	44	112	.4	35	16	997	4.70	16	5	ND	4	21	1	2	2	23	.35	.141	22	31	.48	97	.01	3	1.61	.02	.07	1	3
CC 6+00W 4+80S	1	37	39	123	.7	34	16	1167	4.81	15	5	ND	4	22	1	2	2	23	.36	.147	21	28	.47	99	.01	2	1.56	.02	.06	1	2
CC 6+00W 4+90S	1	41	40	118	.9	35	15	943	4.75	16	5	ND	4	23	1	2	2	23	.39	.157	22	33	.46	114	.01	2	1.58	.02	.07	1	1
CC 6+00W 5+00S	2	30	39	123	.4	29	17	980	4.82	18	5	ND	5	22	1	2	2	23	.40	.125	20	30	.45	154	.01	2	1.42	.02	.06	1	7
CC 2+00W 3+10S	1	27	48	123	.4	19	18	684	5.75	16	5	ND	3	47	1	2	2	28	.64	.075	18	22	.26	46	.02	2	1.70	.02	.04	1	8
CC 2+00W 3+20S	1	26	35	98	.2	18	8	212	6.41	16	5	ND	3	16	1	2	2	29	.21	.051	19	18	.13	38	.01	8	1.05	.01	.03	1	6
CC 2+00W 3+30S	1	22	30	87	.2	19	10	523	4.90	13	5	ND	4	7	1	2	3	23	.03	.065	22	13	.12	29	.01	2	.82	.01	.03	1	2
CC 2+00W 3+40S	1	19	25	78	.2	18	6	377	5.47	15	5	ND	3	4	1	2	2	28	.01	.070	21	17	.14	29	.01	2	.74	.01	.04	1	5
CC 2+00W 3+50S	1	8	12	40	.5	15	4	89	2.42	6	5	ND	3	4	1	2	2	26	.01	.042	19	31	.36	31	.01	5	.98	.01	.02	1	8
CC 2+00W 3+60S	1	18	49	83	.3	19	9	1162	4.89	16	5	ND	2	5	1	2	2	32	.05	.095	17	28	.34	49	.01	2	.89	.01	.04	3	1
CC 2+00W 3+70S	1	13	18	33	.2	9	3	185	2.98	11	5	ND	2	4	1	2	2	23	.01	.058	19	13	.12	35	.01	2	.67	.01	.04	2	39
CC 2+00W 3+80S	1	44	34	80	.3	19	15	2129	4.93	17	5	ND	3	6	1	2	2	25	.04	.087	18	19	.25	66	.01	2	1.35	.01	.05	3	17
CC 2+00W 3+90S	1	31	18	69	.3	19	10	953	3.80	9	5	ND	2	7	1	2	2	28	.07	.061	19	21	.38	63	.02	7	1.40	.01	.05	1	7
CC 2+00W 4+00S	3	43	33	70	.2	18	15	1738	4.23	9	5	ND	2	9	1	2	2	28	.11	.104	15	21	.36	76	.01	2	1.65	.02	.05	1	121
CC 2+00W 4+10S	1	45	37	79	.2	16	12	1558	4.72	12	5	ND	2	9	1	2	2	33	.12	.101	16	22	.32	78	.01	2	1.62	.01	.04	1	16
STD C/AU-S	18	58	42	132	7.2	68	27	1030	3.89	41	23	7	37	49	17	16	20	55	.47	.087	37	58	.85	175	.08	32	1.77	.07	.13	12	49

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	HG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
CC 2+00W 4+20S	1	35	18	51	.2	14	6	166	2.44	5	5	ND	2	8	1	2	2	22	.13	.081	14	10	.38	65	.01	2	1.34	.01	.05	30	1
CC 2+00W 4+30S	1	4	9	30	.2	7	3	76	1.59	3	5	ND	2	5	1	2	2	13	.09	.071	24	15	.15	34	.01	2	.61	.01	.04	1	1
CC 2+00W 4+40S	1	18	35	62	.1	17	7	201	4.18	14	5	ND	2	6	1	2	2	29	.07	.059	20	19	.30	60	.01	2	1.24	.01	.04	1	2
CC 2+00W 4+50S	1	26	17	84	.1	11	7	273	4.30	12	5	ND	2	13	1	2	2	31	.25	.078	16	13	.22	67	.01	4	1.12	.02	.04	1	1
CC 2+00W 4+60S	1	79	18	116	.1	11	29	2312	10.94	4	5	ND	2	4	1	2	2	38	.05	.139	10	11	.22	48	.01	2	1.18	.01	.01	1	3
CC 2+00W 4+70S	1	17	20	36	.1	8	10	1331	2.26	9	5	ND	1	7	1	2	2	24	.09	.074	18	10	.13	49	.01	2	.81	.01	.04	1	8
CC 2+00W 4+80S	1	17	19	41	.1	9	5	413	3.02	9	5	ND	2	5	1	2	2	30	.02	.036	25	12	.13	29	.01	2	.85	.01	.03	3	11
CC 2+00W 4+90S	1	21	43	73	.1	12	12	940	3.93	12	5	ND	2	8	1	2	2	28	.10	.067	18	18	.27	49	.01	3	1.15	.01	.05	1	1
CC 2+00W 5+00S	1	21	101	71	.3	11	22	1579	3.23	16	5	ND	2	9	1	2	2	23	.10	.077	22	12	.20	56	.01	2	.86	.01	.04	1	5
CCA0+00E 0+70S	2	57	125	176	.6	83	25	893	5.06	88	5	ND	7	24	1	2	2	23	.34	.096	31	40	.64	136	.02	6	1.03	.02	.07	5	220
CCA0+00E 0+80S	1	40	3257	259	3.9	33	12	554	5.55	124	5	ND	6	17	1	3	2	16	.25	.080	20	20	.33	71	.01	5	.62	.01	.04	142	540
CCA0+00E 0+90S	1	42	1229	262	2.0	38	14	751	4.83	115	5	ND	5	21	2	4	2	14	.32	.073	19	18	.36	88	.01	2	.56	.01	.03	167	530
CCA0+00E 1+00S	1	54	353	609	1.2	51	19	670	5.15	44	5	ND	6	23	10	2	2	20	.35	.091	23	27	.47	126	.01	7	.82	.02	.03	28	260
CCA0+00E 1+10S	1	53	484	224	1.1	51	26	1034	5.48	88	5	ND	10	17	1	2	2	18	.22	.082	31	29	.41	106	.01	4	.74	.01	.03	180	605
CCA0+00E 1+20S	2	44	81	155	.2	47	19	835	5.09	45	5	ND	5	14	1	2	2	21	.18	.086	20	29	.46	122	.01	11	.76	.02	.03	16	62
CCA0+00E 1+30S	1	37	52	87	.2	22	14	1473	5.18	17	5	ND	4	6	1	2	2	22	.04	.082	20	15	.12	60	.01	7	.94	.01	.05	5	47
CCA0+00E 1+40S	1	17	36	63	.7	11	7	1535	3.30	13	5	ND	2	6	1	2	2	26	.03	.089	19	15	.21	42	.01	2	.77	.01	.04	2	3
CCA0+00E 1+50S	1	14	40	50	.3	8	6	458	3.43	8	5	ND	2	5	1	2	2	37	.02	.048	20	12	.22	35	.01	2	.81	.01	.02	6	24
CCA0+00E 1+60S	1	19	57	69	.5	12	7	652	4.34	14	5	ND	2	5	1	2	2	28	.02	.078	15	17	.19	38	.01	8	.82	.01	.03	2	10
CCA0+00E 1+70S	1	28	65	84	1.0	16	10	914	5.69	19	5	ND	2	5	1	2	2	31	.02	.065	17	18	.21	38	.01	2	.93	.01	.03	4	13
CCA0+00E 1+80S	1	28	87	82	1.0	17	8	435	5.63	20	5	ND	3	5	1	2	2	26	.05	.086	16	18	.26	34	.01	3	1.15	.01	.03	5	45
CCA0+00E 1+90S	1	64	96	105	.2	30	18	824	5.79	21	5	ND	8	10	1	2	2	23	.11	.108	23	15	.40	47	.01	2	1.39	.01	.04	5	157
CCA0+00E 2+00S	1	187	83	227	.8	27	41	6217	10.31	37	5	ND	3	20	1	2	2	35	.40	.188	12	10	.30	185	.01	2	1.08	.02	.03	2	9
CCA0+00E 2+10S	1	28	52	69	.7	15	9	630	5.12	18	5	ND	2	5	1	2	2	26	.02	.115	16	11	.20	39	.01	10	.70	.01	.03	4	38
CCA0+00E 2+20S	1	29	49	76	.9	14	10	1744	4.70	17	5	ND	2	6	1	2	2	32	.04	.136	19	14	.20	41	.01	5	.68	.01	.03	4	23
CCA0+00E 2+30S	1	25	38	66	2.1	15	8	740	3.86	13	5	ND	2	7	1	2	2	27	.11	.122	18	14	.21	44	.01	2	.61	.01	.03	2	17
CCA0+00E 2+40S	1	41	161	137	.9	17	14	1416	7.37	23	5	ND	2	5	1	4	2	32	.03	.120	13	18	.23	31	.01	2	1.06	.01	.03	8	4
CCA0+00E 2+50S	1	23	44	66	.3	13	9	1419	4.61	17	5	ND	2	7	1	2	2	36	.03	.084	19	12	.19	32	.01	2	.75	.01	.03	3	15
CCA0+00E 2+60S	1	24	39	45	1.1	11	6	397	4.10	14	5	ND	2	4	1	2	2	27	.01	.113	19	10	.12	33	.01	2	.55	.01	.02	3	9
CCA0+00E 2+70S	1	17	19	35	.3	8	5	908	2.71	8	5	ND	2	5	1	2	2	24	.05	.126	21	14	.14	31	.01	12	.53	.01	.04	3	51
CCA0+00E 2+80S	1	17	19	51	.5	10	7	1593	3.12	10	5	ND	2	6	1	2	2	29	.05	.118	19	11	.17	49	.01	12	.57	.01	.03	5	7
CCA0+00E 2+90S	1	51	32	78	.5	27	13	803	4.70	15	5	ND	4	6	1	2	2	24	.04	.085	22	22	.33	37	.01	3	1.08	.01	.03	2	4
CCA0+00E 3+00S	1	23	19	48	1.0	13	7	445	3.63	17	5	ND	2	5	1	2	2	35	.02	.104	19	13	.18	39	.01	8	.60	.01	.03	3	36
CCA0+00E 3+10S	1	15	20	50	.5	10	6	817	3.33	8	5	ND	2	7	1	2	2	28	.05	.087	29	11	.14	35	.01	2	.45	.01	.03	29	7
CCA0+00E 3+20S	1	16	20	36	1.2	10	5	222	3.29	11	5	ND	2	5	1	2	2	18	.02	.063	20	10	.11	18	.01	7	.40	.01	.02	3	3
CCA0+00E 3+30S	1	19	21	41	.5	11	5	257	3.61	9	5	ND	3	5	1	2	2	19	.01	.074	22	13	.14	26	.01	7	.62	.01	.03	3	21
SID C/AU-S	18	58	40	132	7.1	69	28	1048	4.01	43	23	7	39	50	19	16	18	57	.48	.091	37	61	.88	178	.08	33	1.84	.08	.13	14	48

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	M6	BA	TI	B	AL	NA	K	M	AUS
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
CCA0+00E 3+40S	1	20	23	44	.6	12	6	455	4.09	17	5	ND	2	5	1	2	2	29	.02	.101	20	18	.13	27	.01	8	.52	.01	.02	3	33
CCA0+00E 3+50S	1	43	44	79	.7	20	13	1075	7.62	16	5	ND	4	9	1	2	2	32	.12	.129	22	22	.29	67	.02	2	1.03	.01	.04	1	1
CCA0+00E 3+60S	1	47	34	74	.6	20	13	850	7.11	16	5	ND	3	5	1	2	3	28	.03	.101	21	23	.29	35	.01	2	.99	.01	.04	1	1
CCA0+00E 3+70S	1	101	60	124	.2	43	25	1516	7.04	18	5	ND	9	9	1	2	2	27	.07	.060	33	22	.51	66	.01	4	1.54	.02	.04	2	1
CCA0+00E 3+80S	1	39	37	77	.4	21	13	1033	6.48	15	5	ND	3	6	1	2	2	27	.04	.128	22	25	.32	37	.01	2	1.12	.01	.03	1	1
CCA0+00E 3+90S	1	36	28	72	.5	19	11	601	6.63	12	5	ND	3	6	1	2	5	33	.03	.121	24	21	.25	33	.01	11	.89	.01	.04	1	1
CCA0+00E 4+00S	1	31	26	72	1.2	16	10	981	5.02	16	5	ND	2	8	1	2	2	37	.06	.098	23	18	.23	43	.01	2	.90	.01	.04	1	1
CCA0+50E 0+60S	1	46	52	168	.4	62	17	577	4.36	48	5	ND	4	28	1	7	3	25	.34	.089	26	43	.54	166	.01	2	1.17	.02	.06	4	28
CCA0+50E 0+70S	1	33	50	179	.3	57	16	761	4.46	36	5	ND	5	20	1	2	2	30	.20	.094	32	54	.58	137	.01	2	1.27	.02	.09	2	6
CCA0+50E 0+80S	2	45	50	212	.3	72	19	655	5.01	41	5	ND	5	23	1	2	4	32	.23	.089	30	62	.70	159	.02	2	1.54	.02	.09	3	9
CCA0+50E 0+90S	1	43	74	185	.6	69	19	708	4.72	48	6	ND	4	23	1	2	3	30	.22	.098	31	53	.65	145	.02	3	1.29	.02	.08	10	925
CCA0+50E 1+00S	1	57	1185	404	2.3	67	28	1956	6.02	190	5	ND	8	20	4	3	2	17	.27	.076	23	19	.49	139	.01	2	.66	.02	.03	205	885
CCA0+50E 1+10S	1	55	2877	546	7.9	40	20	989	7.44	271	5	ND	6	16	4	9	6	13	.25	.062	14	15	.47	47	.01	4	.48	.02	.03	238	1690
CCA0+50E 1+20S	3	64	244	243	1.4	69	27	942	5.92	85	5	ND	8	32	1	5	2	23	.41	.101	27	36	.54	213	.02	2	.82	.02	.04	111	490
CCA0+50E 1+30S	2	67	719	288	1.9	58	24	984	5.98	208	5	ND	8	21	2	4	3	20	.28	.089	29	23	.47	141	.01	3	.83	.02	.05	71	1405
CCA0+50E 1+40S	1	90	82	152	.6	55	25	986	6.19	47	5	ND	12	13	1	2	2	22	.14	.089	41	25	.47	82	.01	2	1.16	.01	.04	4	180
CCA0+50E 1+50S	1	63	123	119	.6	35	17	510	6.13	31	5	ND	7	9	1	2	3	24	.11	.103	27	19	.40	54	.01	9	1.18	.02	.05	13	40
CCA0+50E 1+60S	1	14	36	63	.3	7	5	1047	3.73	10	5	ND	2	7	1	3	2	35	.04	.046	20	15	.13	67	.02	2	.75	.01	.03	49	9
CCA0+50E 1+70S	1	20	74	97	.3	14	8	1126	5.18	16	5	ND	2	9	1	2	2	31	.10	.072	17	23	.19	74	.02	9	.92	.01	.02	3	111
CCA0+50E 1+80S	1	20	42	78	.4	12	6	922	4.83	17	5	ND	1	7	1	2	2	42	.03	.074	18	23	.17	55	.02	2	.73	.01	.04	1	10
CCA0+50E 1+90S	1	18	29	53	.7	9	6	535	2.99	14	5	ND	2	5	1	2	2	23	.04	.059	18	13	.14	40	.01	5	.58	.01	.03	4	5
CCA0+50E 2+00S	1	35	84	115	.2	13	11	2977	8.82	15	5	ND	2	6	1	2	2	34	.02	.117	18	15	.17	85	.01	2	.94	.01	.02	4	6
CCA0+50E 2+10S	1	35	110	92	.6	15	10	967	5.24	16	5	ND	2	7	1	2	2	28	.07	.102	19	16	.23	38	.01	2	.82	.01	.04	2	1
CCA0+50E 2+20S	1	30	83	85	.7	14	10	1271	5.23	14	5	ND	2	8	1	2	2	29	.08	.112	20	18	.20	49	.01	4	.87	.01	.03	2	1
CCA0+50E 2+30S	1	44	37	81	1.0	19	12	955	5.39	16	5	ND	3	6	1	2	2	28	.02	.091	21	17	.31	48	.01	2	1.04	.01	.04	1	4
CCA0+50E 2+40S	1	33	49	97	.5	21	10	1228	4.76	12	5	ND	3	10	1	2	2	23	.11	.141	23	18	.33	128	.01	8	.86	.01	.04	2	3
CCA0+50E 2+50S	1	31	26	59	.7	15	8	408	3.99	11	5	ND	3	5	1	2	2	21	.02	.065	22	12	.22	34	.01	2	.76	.01	.03	1	1
CCA0+50E 2+60S	1	26	53	68	.9	14	8	595	4.28	13	5	ND	2	6	1	2	2	24	.02	.102	20	14	.21	52	.01	2	.69	.01	.03	1	5
CCA0+50E 2+70S	1	44	47	73	.5	17	10	703	5.69	14	5	ND	3	5	1	2	2	26	.03	.101	21	18	.23	34	.01	27	1.01	.02	.03	1	1
CCA0+50E 2+80S	1	38	40	81	.6	19	11	985	5.69	17	5	ND	3	8	1	2	2	27	.11	.160	20	15	.25	34	.01	2	.81	.01	.06	2	1
CCA0+50E 2+90S	1	41	34	73	.4	20	12	840	5.08	12	5	ND	4	7	1	2	2	35	.06	.081	25	16	.42	36	.01	2	1.07	.01	.05	2	1
CCA0+50E 3+00S	1	74	42	91	.4	26	18	813	6.02	17	5	ND	6	10	1	2	2	28	.12	.078	27	16	.41	74	.01	2	1.37	.01	.05	2	31
CCA0+50E 3+10S	1	60	40	87	.5	24	15	951	5.86	15	5	ND	5	8	1	2	2	30	.09	.093	25	14	.36	57	.01	2	1.17	.01	.05	2	8
CCA0+50E 3+20S	1	30	38	54	.5	13	7	301	4.09	16	5	ND	3	5	1	2	3	24	.01	.072	20	14	.22	36	.01	6	.88	.01	.03	1	1
CCA0+50E 3+30S	1	46	62	80	.6	19	13	854	6.04	17	5	ND	4	6	1	2	2	26	.02	.080	23	16	.23	45	.01	2	.97	.01	.04	2	5
CCA0+50E 3+40S	1	41	43	84	.5	19	10	602	6.13	17	5	ND	4	6	1	2	2	30	.01	.096	22	17	.19	39	.01	2	.96	.01	.03	2	6
STD C/AU-S	18	58	43	132	7.4	67	28	1047	3.92	40	24	7	38	50	18	16	20	57	.47	.089	37	58	.87	178	.08	33	1.79	.08	.14	14	47

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	RU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	1	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	2	2	PPM	PPM	1	PPM	1	PPM	1	1	1	PPM	PPB
CCAO+50E 3+50S	1	19	30	41	.2	10	7	1115	4.23	10	5	ND	3	5	1	2	2	28	.02	.105	21	13	.16	41	.01	2	.68	.01	.03	4	2
CCAO+50E 3+60S	1	27	30	64	.2	13	9	1273	5.42	12	5	ND	2	6	1	2	2	35	.03	.105	18	14	.20	58	.01	2	.88	.01	.03	1	1
CCAO+50E 3+70S	1	38	42	75	.2	18	12	926	6.74	10	5	ND	2	6	1	2	2	27	.05	.084	18	17	.27	44	.01	2	.91	.01	.03	1	4
CCAO+50E 3+80S	1	53	59	93	.7	22	16	1238	7.90	15	5	ND	3	7	1	2	2	31	.06	.160	19	17	.29	28	.01	2	1.00	.01	.03	2	5
CCAO+50E 3+90S	1	31	36	62	.3	15	11	1286	5.94	10	5	ND	3	5	1	2	2	31	.01	.147	21	14	.24	39	.01	2	.87	.01	.03	1	8
CCAO+50E 4+00S	1	19	28	39	.5	10	5	199	3.92	9	5	ND	2	4	1	2	2	30	.02	.110	20	13	.16	23	.01	2	.69	.01	.02	2	2

See 1/20

EX-100

SAMPLE#	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUR	
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM	
CC10+S0W 5+00N	1	19	20	56	.3	18	5	121	3.55	22	5	ND	3	6	1	2	20	.09	.048	23	14	.09	34	.01	2	.65	.01	.02	3	23	
CC10+S0W 4+00N	1	13	16	46	.2	13	4	117	2.37	15	5	ND	4	6	1	2	18	.04	.041	24	10	.06	31	.01	2	.64	.01	.02	10	15	
CC10+S0W 4+80N	1	26	36	83	.3	24	13	907	4.70	19	5	ND	4	11	1	4	24	.09	.063	22	21	.22	49	.01	2	1.11	.01	.03	2	8	
CC10+S0W 4+70N	1	36	39	117	.3	36	15	2711	4.17	24	5	ND	4	28	1	2	29	.28	.066	16	22	.37	80	.01	2	1.17	.02	.03	1	13	
CC10+S0W 4+60N	1	38	40	98	.2	39	15	740	4.34	34	5	ND	6	14	1	2	17	.18	.051	24	17	.38	49	.01	7	.91	.02	.03	4	265	
CC10+S0W 4+50N	1	19	11	41	.1	13	5	114	2.10	19	5	ND	2	4	1	2	26	.02	.037	24	11	.04	29	.01	2	.35	.01	.01	4	49	
CC10+S0W 4+40N	1	20	16	55	.2	19	6	223	3.96	55	5	ND	5	4	1	2	25	.03	.051	24	11	.11	42	.01	9	.61	.01	.02	6	38	
CC10+S0W 4+30N	1	13	11	34	.3	12	4	103	2.20	26	5	ND	5	4	1	2	19	.02	.036	24	8	.06	26	.01	2	.44	.01	.02	4	35	
CC10+S0W 4+20N	1	28	38	81	.5	25	9	455	5.53	47	5	ND	6	5	1	2	22	.03	.087	22	19	.16	44	.01	2	1.02	.01	.03	5	32	
CC10+S0W 4+10N	1	12	15	35	.2	11	3	93	2.28	39	5	ND	5	4	1	4	2	.02	.066	20	10	.08	49	.01	2	.53	.01	.02	5	21	
CC10+S0W 4+00N	1	13	20	38	.3	13	4	516	2.87	36	5	ND	4	6	1	5	2	.08	.089	23	10	.09	44	.01	3	.48	.01	.04	3	32	
CC10+S0W 3+90N	1	21	24	64	.4	22	7	368	3.96	35	5	ND	2	5	1	2	2	.06	.105	20	14	.15	64	.01	2	.57	.01	.03	5	13	
CC10+S0W 3+80N	1	25	14	65	.3	28	7	210	3.46	49	5	ND	3	4	1	3	2	.03	.056	23	7	.06	37	.01	2	.48	.01	.02	3	28	
CC10+S0W 3+70N	1	27	23	71	.2	25	8	394	4.52	54	5	ND	4	5	1	3	2	.07	.071	21	12	.12	49	.01	6	.56	.01	.04	5	21	
CC10+S0W 3+60N	1	20	20	58	.2	17	8	567	3.15	39	5	ND	3	6	1	3	2	.07	.074	21	7	.05	61	.01	5	.47	.01	.03	2	12	
CC10+S0W 3+50N	1	25	20	58	.3	19	8	223	3.63	22	5	ND	3	6	1	2	2	.03	.083	18	16	.33	51	.01	2	.92	.01	.04	2	9	
CC10+S0W 3+40N	1	26	26	74	.3	24	10	807	3.48	33	5	ND	3	14	1	2	2	.22	.070	20	12	.25	50	.01	2	.63	.01	.03	1	38	
CC10+S0W 3+30N	1	32	34	77	.4	26	11	631	6.06	38	5	ND	3	5	1	2	2	.02	.072	20	17	.22	45	.01	3	.95	.01	.03	4	32	
CC10+S0W 3+20N	1	33	21	71	.3	18	11	2970	4.60	18	5	ND	3	4	1	2	2	.40	.089	18	12	.26	100	.01	2	.99	.01	.03	1	82	
CC10+S0W 3+10N	1	33	17	58	.4	21	11	1209	4.57	21	5	ND	5	4	1	2	2	.33	.073	25	16	.32	63	.01	2	1.14	.01	.02	1	11	
CC10+S0W 3+00N	1	35	16	66	.7	18	10	1583	3.75	19	5	ND	3	5	1	2	2	.29	.02	.059	23	11	.13	62	.01	4	.67	.01	.03	3	38
CC10+S0W 2+90N	1	41	36	95	.5	26	12	868	5.63	33	5	ND	2	6	1	2	2	.04	.091	18	18	.21	59	.01	7	.87	.01	.03	10	23	
CC10+S0W 2+80N	1	28	21	64	.2	19	7	503	3.98	28	5	ND	3	5	1	2	2	.29	.02	.062	23	12	.12	62	.01	2	.54	.01	.04	2	11
CC10+S0W 2+70N	1	31	30	72	.2	23	9	249	5.48	32	5	ND	3	6	1	2	2	.03	.061	20	16	.19	29	.01	2	.88	.01	.02	3	12	
CC10+S0W 2+60N	1	22	28	106	.2	21	8	423	4.13	23	5	ND	3	24	1	2	2	.19	.32	.069	14	14	.20	26	.01	5	.73	.01	.03	11	14
CC10+S0W 2+50N	1	33	161	180	.7	33	14	928	4.33	25	5	ND	5	27	1	2	2	.44	.066	15	18	.37	33	.01	2	.94	.02	.03	8	41	
CC10+S0W 2+40N	1	25	87	112	.4	23	13	1174	4.30	25	5	ND	3	13	1	2	2	.20	.12	.068	17	15	.24	46	.01	2	.89	.01	.03	7	22
CC10+S0W 2+30N	1	27	50	92	.1	22	11	570	4.53	27	5	ND	3	8	1	2	2	.23	.03	.078	19	17	.20	54	.01	2	.87	.01	.03	7	1
CC10+S0W 2+20N	1	35	33	84	.4	29	12	555	4.84	30	5	ND	3	6	1	2	2	.19	.03	.070	21	18	.21	53	.01	2	.67	.01	.03	6	45
CC10+S0W 2+10N	1	75	114	131	.4	50	26	1045	6.54	35	5	ND	9	9	1	2	2	.17	.09	.065	27	18	.34	40	.01	2	1.05	.01	.03	5	41
CC10+S0W 2+00N	1	51	81	112	.7	33	17	1209	5.51	25	5	ND	4	14	1	2	2	.20	.17	.073	21	16	.30	62	.01	2	1.00	.01	.04	4	32
CC10+S0W 1+90N	1	49	43	129	.3	33	17	1804	4.87	25	5	ND	5	22	1	2	2	.20	.30	.110	16	16	.32	78	.01	2	1.19	.01	.04	3	23
CC10+S0W 1+80N	1	45	47	129	.3	32	16	1718	4.98	27	5	ND	4	22	1	2	2	.20	.32	.115	15	16	.32	75	.01	2	1.09	.01	.05	2	17
CC10+S0W 1+70N	1	25	25	67	.3	21	8	422	4.13	24	5	ND	2	6	1	2	2	.25	.03	.080	19	19	.21	33	.01	2	.76	.01	.03	4	14
CC10+S0W 1+60N	1	28	31	75	.1	24	9	462	5.30	33	5	ND	3	5	1	4	2	.21	.03	.095	18	16	.25	41	.01	2	.81	.01	.03	6	32
CC10+S0W 1+50N	1	98	143	142	.7	44	30	1428	7.23	33	5	ND	9	7	1	3	2	.17	.08	.072	23	17	.37	40	.01	5	1.08	.01	.02	9	109
STD C/AU-S	18	58	40	132	7.2	70	27	1040	3.95	42	25	7	38	49	19	18	22	56	.47	.088	37	59	.87	176	.08	36	1.81	.06	.15	12	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE PPM	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AUX PPB
CC10+50W 1+40N	1	61	233	418	.6	37	27	1702	7.23	29	5	ND	6	40	2	2	2	19	.45	.095	21	27	.42	101	.01	6	1.05	.02	.04	6	25
CC10+50W 1+30N	2	74	570	393	2.2	38	24	1867	6.88	26	5	ND	5	31	3	3	3	20	.49	.093	19	19	.36	90	.01	3	.95	.02	.05	28	85
CC10+50W 1+20N	2	94	229	215	.5	48	29	1355	6.94	29	5	ND	8	34	1	2	2	18	.46	.086	22	15	.41	84	.01	2	.73	.02	.05	10	38
CC10+50W 1+10N	2	56	448	326	1.0	34	19	1966	5.44	23	5	ND	3	37	3	2	2	21	.42	.094	13	23	.30	94	.01	4	.93	.02	.04	36	4
CC10+50W 1+00N	1	63	230	195	.7	29	17	925	6.15	17	5	ND	5	6	1	2	2	22	.09	.067	25	16	.33	53	.01	2	1.15	.01	.04	21	12
CC10+50W 0+90N	1	29	35	76	.6	15	9	934	4.18	14	5	ND	2	4	1	2	2	19	.04	.096	16	12	.20	57	.01	2	.67	.01	.03	1	1
CC10+50W 0+80N	1	47	80	135	.4	22	14	1581	6.49	24	5	ND	3	6	1	2	2	24	.03	.103	25	14	.26	61	.01	2	1.11	.01	.04	7	1
CC10+50W 0+70N	1	35	27	70	.4	17	11	953	4.54	15	5	ND	2	3	1	2	2	21	.03	.099	15	11	.19	32	.01	2	.61	.01	.03	3	1
CC10+50W 0+60N	1	19	53	65	.6	10	6	642	3.33	12	5	ND	2	4	1	2	2	23	.02	.060	19	12	.12	33	.01	2	.49	.01	.04	81	162
CC10+50W 0+50N	1	18	327	143	2.0	11	6	867	3.68	28	5	ND	2	5	1	3	2	19	.03	.099	17	13	.14	26	.01	2	.60	.01	.04	127	24
CC10+50W 0+40N	1	15	15	40	.4	9	5	183	2.43	6	5	ND	2	3	1	2	2	17	.02	.089	19	9	.15	25	.01	2	.52	.01	.03	3	1
CC10+50W 0+30N	1	30	15	59	.4	12	10	730	4.18	13	5	ND	2	4	1	2	2	19	.04	.109	13	10	.15	34	.01	2	.49	.01	.04	15	1
CC10+50W 0+20N	1	7	11	24	.3	6	3	279	1.59	5	5	ND	2	4	1	2	2	24	.02	.061	29	12	.12	29	.02	2	.44	.01	.05	1	1
CC10+50W 0+10N	1	16	14	47	.5	18	7	679	2.53	8	5	ND	2	4	1	2	2	23	.02	.077	18	26	.28	41	.01	2	.68	.01	.04	2	1
CC10+50W 0+00N	1	15	14	49	.3	14	6	498	3.00	7	5	ND	2	5	1	2	2	24	.05	.080	20	20	.25	28	.01	2	.75	.01	.04	1	1
CC10+50W 0+10S	1	35	23	66	.9	15	13	3616	4.00	7	5	ND	2	7	1	2	2	38	.09	.136	15	18	.31	60	.01	3	.87	.01	.05	1	1
CC10+50W 0+20S	1	17	13	49	.4	18	8	1589	2.80	5	5	ND	2	5	1	2	2	24	.07	.079	17	25	.28	66	.01	2	.73	.01	.04	1	4
CC10+50W 0+30S	2	127	21	89	.2	31	15	958	5.83	7	5	ND	6	7	1	2	2	37	.09	.144	20	22	.58	37	.01	2	1.54	.01	.03	1	1
CC10+50W 0+40S	1	11	13	33	.4	19	5	122	2.59	8	5	ND	2	3	1	2	2	42	.01	.054	21	45	.33	20	.01	2	.85	.01	.03	1	1
CC10+50W 0+50S	1	27	19	75	.3	19	10	1161	4.56	9	5	ND	3	4	1	2	2	28	.06	.094	18	17	.36	45	.01	2	1.01	.01	.04	1	1
CC10+50W 0+60S	1	9	13	33	.6	8	3	247	2.08	4	5	ND	4	4	1	2	2	18	.03	.062	27	8	.18	23	.01	2	.70	.01	.04	1	1
CC10+50W 0+70S	1	24	21	66	.2	17	7	329	5.39	10	5	ND	6	3	1	2	2	22	.01	.116	24	18	.33	23	.01	2	1.10	.01	.04	1	1
CC10+50W 0+80S	1	14	15	44	.2	9	4	292	3.39	4	5	ND	4	3	1	2	2	21	.02	.092	18	10	.15	17	.01	2	.61	.01	.03	1	2
CC10+50W 0+90S	1	34	25	77	.1	17	10	1100	4.23	12	5	ND	4	6	1	2	2	21	.11	.103	21	10	.22	30	.01	2	.67	.01	.04	1	1
CC10+50W 1+00S	1	28	22	82	.2	19	8	296	5.73	11	5	ND	7	3	1	2	2	22	.02	.076	22	15	.38	25	.01	2	1.16	.01	.03	1	1
CC9+50W 2+00N	1	27	19	83	.3	19	11	1710	3.83	12	5	ND	3	11	1	2	2	30	.08	.061	18	16	.37	91	.01	2	1.01	.01	.04	1	1
CC9+50W 1+90N	1	16	15	44	.1	12	5	219	2.50	9	5	ND	3	5	1	2	2	23	.02	.058	24	14	.21	37	.01	2	.77	.01	.04	3	1
CC9+50W 1+80N	1	31	23	62	.1	19	9	465	4.59	22	5	ND	4	4	1	2	2	24	.01	.058	25	21	.31	49	.01	2	1.25	.01	.04	2	2
CC9+50W 1+70N	1	47	27	93	.1	36	18	444	5.82	25	5	ND	8	7	1	2	2	22	.04	.054	25	22	.44	51	.01	2	1.72	.01	.04	3	23
CC9+50W 1+60N	1	25	27	93	.1	19	16	1860	4.23	18	5	ND	2	21	1	2	2	23	.30	.105	12	15	.25	99	.01	2	.91	.01	.04	5	1
CC9+50W 1+50N	1	55	43	109	.1	41	21	666	5.55	23	5	ND	8	7	1	3	2	26	.05	.047	27	21	.52	63	.01	2	1.55	.01	.05	2	13
CC9+50W 1+40N	1	73	51	186	.1	44	22	1245	5.90	26	5	ND	9	9	1	2	2	23	.11	.058	30	20	.47	73	.01	2	1.28	.01	.06	1	26
CC9+50W 1+30N	1	21	22	52	.3	16	7	378	3.27	18	5	ND	3	8	1	2	2	21	.07	.057	20	12	.22	62	.01	2	.74	.01	.04	3	62
CC9+50W 1+20N	1	29	29	63	.3	18	9	481	4.55	17	5	ND	3	5	1	2	2	24	.02	.062	19	16	.23	53	.01	3	.87	.01	.03	2	1
CC9+50W 1+10N	1	29	36	73	.1	18	10	756	3.77	12	5	ND	3	14	1	2	2	20	.16	.067	17	14	.24	54	.01	2	.76	.01	.04	2	4
CC9+50W 1+00N	1	14	17	36	.3	12	4	402	2.19	13	5	ND	2	5	1	3	2	20	.02	.046	21	14	.12	46	.01	3	.53	.01	.04	3	138
STD C/AU-S	19	59	41	132	7.3	68	28	1049	3.98	39	24	7	39	50	18	17	20	57	.47	.091	37	60	.87	179	.08	32	1.84	.08	.14	12	51

SAMPLE#	NO	CU	PB	ZN	AS	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
CC9+50W 0+90W	1	27	32	72	.6	17	8	624	4.68	20	5	ND	2	8	1	2	2	26	.09	.062	19	16	.19	38	.01	3	.73	.01	.04	5	18
CC9+50W 0+80W	1	38	41	105	.5	31	15	875	5.19	28	5	ND	4	32	1	2	2	20	.45	.093	20	21	.30	63	.01	2	1.31	.02	.05	3	32
CC9+50W 0+70W	1	70	65	122	.5	49	20	2370	7.20	28	5	ND	9	22	1	2	2	17	.28	.071	30	19	.37	85	.01	7	1.34	.02	.04	3	18
CC9+50W 0+60W	1	63	54	164	.4	35	17	1884	5.46	25	5	ND	4	41	1	2	2	19	.67	.101	16	16	.38	96	.01	4	1.11	.02	.06	3	1
CC9+50W 0+50W	2	168	53	137	1.1	64	35	1739	7.45	47	11	ND	5	41	1	2	2	15	.59	.099	14	12	.31	83	.01	2	.87	.02	.05	3	17
CC9+50W 0+40W	2	95	3336	712	9.2	78	30	1938	12.95	321	5	5	5	19	6	3	4	10	.32	.076	7	5	.21	61	.01	2	.36	.01	.04	961	2160
CC9+50W 0+30W	1	72	173	139	.5	40	25	1411	6.28	28	5	ND	5	22	1	2	2	19	.30	.082	17	16	.34	95	.01	2	.87	.01	.04	12	38
CC9+50W 0+20W	1	48	66	126	.6	29	15	1215	5.16	17	6	ND	4	49	1	2	2	22	.53	.098	14	24	.34	118	.01	2	1.25	.02	.05	3	169
CC9+50W 0+10W	1	54	41	118	.3	30	16	1035	4.99	18	5	ND	6	18	1	2	2	21	.17	.054	21	20	.37	100	.01	2	1.05	.01	.05	2	9
CC9+50W 0+00W	1	18	22	50	.3	8	4	211	3.86	8	5	ND	2	6	1	2	2	34	.04	.045	20	15	.10	50	.01	2	.57	.01	.04	4	1
CC9+50W 0+10S	1	16	20	45	.2	11	5	531	2.66	9	5	ND	2	4	1	2	2	21	.02	.072	18	15	.20	40	.01	2	.68	.01	.05	8	1
CC9+50W 0+20S	1	20	25	59	.3	12	5	169	3.45	6	5	ND	2	4	1	2	2	22	.02	.061	17	19	.23	41	.01	2	.88	.01	.03	2	1
CC9+50W 0+30S	1	11	14	40	.3	8	4	198	2.36	5	5	ND	2	4	1	2	2	21	.04	.069	17	12	.14	31	.01	2	.57	.01	.05	2	1
CC9+50W 0+40S	1	20	29	86	.3	13	11	1096	4.02	10	5	ND	2	6	1	2	2	24	.04	.115	16	17	.25	107	.01	2	.95	.01	.05	2	3
CC9+50W 0+50S	1	34	26	114	.5	20	13	2302	3.97	11	5	ND	3	36	1	2	2	22	.40	.145	12	19	.33	105	.01	5	1.16	.02	.05	1	1
CC9+50W 0+60S	2	30	28	126	.5	20	13	2940	3.87	12	8	ND	3	30	1	2	2	21	.34	.138	12	17	.32	108	.01	3	1.16	.02	.05	3	1
CC9+50W 0+70S	1	12	12	34	.2	8	4	210	2.68	6	7	ND	2	4	1	2	2	21	.02	.058	18	11	.17	24	.01	2	.65	.01	.03	2	2
CC9+50W 0+80S	1	16	15	52	.6	12	6	203	4.08	9	5	ND	3	3	1	2	2	22	.01	.065	19	16	.25	31	.01	2	.94	.01	.04	2	5
CC9+50W 0+90S	1	23	16	61	.4	13	6	353	4.90	12	5	ND	3	3	1	2	2	24	.01	.088	19	17	.23	32	.01	2	.89	.01	.04	1	3
CC9+50W 1+00S	1	17	16	47	.6	10	4	271	4.30	9	5	ND	2	4	1	2	2	23	.05	.067	18	16	.15	26	.01	2	.80	.01	.04	3	4
CC9+50W 1+10S	1	15	16	35	.2	9	4	215	3.21	8	5	ND	2	3	1	2	2	21	.01	.059	19	13	.14	24	.01	4	.73	.01	.04	1	1
CC9+50W 1+20S	1	12	9	29	.2	6	3	238	1.82	5	5	ND	2	4	1	2	2	16	.04	.084	21	8	.08	26	.01	3	.45	.01	.02	1	2
CC9+50W 1+30S	1	17	21	40	.4	9	5	405	3.30	5	5	ND	3	3	1	2	2	19	.01	.078	20	9	.13	28	.01	2	.69	.01	.03	1	1
CC9+50W 1+40S	1	13	13	32	.4	7	3	254	1.79	4	5	ND	3	3	1	2	2	14	.02	.062	21	7	.10	31	.01	4	.53	.01	.04	2	2
CC9+50W 1+50S	1	18	10	38	.1	7	4	161	2.97	7	5	ND	2	3	1	3	2	26	.01	.051	21	7	.09	23	.01	2	.56	.01	.03	1	3
CC9+50W 1+60S	1	28	16	59	.7	13	8	529	4.46	10	5	ND	3	3	1	2	2	26	.01	.087	16	15	.20	32	.01	2	.88	.01	.03	1	1
CC9+50W 1+70S	1	34	18	58	.7	12	8	394	4.44	10	5	ND	2	3	1	2	2	30	.01	.066	19	13	.21	21	.01	3	1.04	.01	.03	1	1
CC9+50W 1+80S	1	19	16	33	1.1	8	4	161	2.36	5	5	ND	3	3	1	2	2	20	.01	.048	21	12	.17	20	.01	2	.76	.01	.03	1	2
CC9+50W 1+90S	1	20	18	46	.2	11	5	549	3.36	6	5	ND	3	4	1	2	2	23	.02	.068	22	14	.18	27	.01	2	.77	.01	.03	2	1
CC9+50W 2+00S	1	19	15	45	.5	11	5	213	3.71	8	5	ND	3	4	1	2	2	31	.02	.070	21	14	.13	34	.01	2	.64	.01	.04	2	1
CC8+50W 1+00W	1	20	20	65	.3	17	8	489	3.73	21	5	ND	2	6	1	2	2	23	.03	.065	21	19	.20	69	.01	2	.73	.01	.04	2	2
CC8+50W 0+90W	1	48	36	107	.3	39	16	542	5.42	34	5	ND	5	6	1	3	2	22	.04	.059	23	20	.40	66	.01	5	1.39	.01	.04	5	22
CC8+50W 0+80W	1	57	37	106	.3	44	19	891	5.32	39	5	ND	9	15	1	2	2	20	.18	.055	29	18	.46	87	.01	2	1.13	.01	.05	3	13
CC8+50W 0+70W	1	25	22	54	.4	19	8	353	3.14	19	5	ND	3	9	1	2	2	20	.09	.079	20	16	.24	61	.01	2	.76	.01	.04	2	1
CC8+50W 0+60W	1	25	21	55	.6	20	8	403	2.88	19	5	ND	3	12	1	2	2	17	.16	.067	22	14	.25	47	.01	2	.71	.01	.05	1	14
CC8+50W 0+50W	1	10	16	34	.1	10	4	241	2.30	11	5	ND	2	5	1	2	2	18	.02	.057	23	15	.18	35	.01	2	.66	.01	.03	1	5
STD C/AU-S	18	58	39	133	7.3	67	27	1041	3.97	41	24	8	38	50	18	14	21	57	.47	.088	37	59	.87	177	.08	32	1.82	.08	.13	14	49

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	N	AUF
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPB
CC8+50W 0+40N	1	24	21	65	.2	21	8	371	3.97	13	5	ND	4	5	1	2	2	19	.04	.067	22	22	.35	47	.01	2	1.09	.01	.04	1	29
CC8+50W 0+30N	1	14	16	45	.2	12	5	828	2.57	11	5	ND	2	4	1	2	2	20	.02	.062	19	14	.16	43	.01	2	.63	.01	.03	2	8
CC8+50W 0+20N	1	22	20	59	.3	20	7	276	2.86	15	5	ND	2	8	1	2	2	17	.10	.064	21	15	.28	47	.01	2	.82	.01	.04	1	4
CC8+50W 0+10N	1	60	42	104	.4	42	18	1123	5.35	27	5	ND	6	7	1	2	2	18	.08	.066	26	25	.39	51	.01	2	1.21	.01	.04	2	32
CC8+50W 0+00N	1	19	16	44	.3	14	6	356	1.83	11	5	ND	3	11	1	2	2	11	.16	.041	25	10	.17	42	.01	2	.60	.01	.02	2	21
CC8+50W 0+10S	1	7	12	28	.5	7	2	97	1.58	9	5	ND	2	4	1	2	2	15	.02	.065	22	12	.13	22	.01	2	.56	.01	.02	1	2
CC8+50W 0+20S	1	12	14	34	.4	11	3	232	2.27	17	5	ND	2	4	1	2	2	15	.02	.050	20	17	.16	39	.01	2	.69	.01	.03	2	44
CC8+50W 0+30S	1	53	60	95	.3	37	18	1246	4.90	34	5	ND	7	14	1	2	2	17	.20	.058	27	17	.36	64	.01	2	.91	.01	.04	2	27
CC8+50W 0+40S	1	31	43	74	.3	20	13	1257	6.28	18	5	ND	3	4	1	2	2	26	.03	.105	17	19	.27	39	.01	2	.90	.01	.02	11	9
CC8+50W 0+50S	1	14	22	32	.5	9	3	159	2.35	10	5	ND	2	7	1	2	2	16	.12	.054	18	14	.18	26	.01	2	.76	.01	.02	8	3
CC8+50W 0+60S	2	47	110	125	.2	29	13	6669	6.56	34	5	ND	3	15	1	2	2	16	.33	.208	15	13	.14	95	.01	5	.82	.01	.04	3	3
CC8+50W 0+70S	1	44	399	280	.9	48	19	669	4.57	60	5	ND	7	22	2	2	2	15	.34	.061	24	16	.45	57	.01	2	.83	.01	.04	31	430
CC8+50W 0+80S	1	46	39	77	.3	15	14	625	4.74	9	5	ND	3	7	1	2	2	16	.05	.072	18	16	.19	37	.01	2	.69	.01	.03	1	2
CC8+50W 0+90S	1	58	32	92	.4	35	17	579	4.89	20	5	ND	6	19	1	2	2	17	.21	.055	21	21	.38	57	.01	2	1.04	.01	.04	1	8
CC8+50W 1+00S	1	41	26	77	.2	25	13	459	4.36	13	5	ND	4	9	1	2	2	17	.10	.056	21	15	.26	19	.01	4	.77	.01	.02	1	4
CC8+50W 1+10S	1	57	30	93	.1	37	17	719	4.57	17	5	ND	10	8	1	2	2	14	.09	.064	29	15	.28	22	.01	12	.74	.01	.02	1	1
CC8+50W 1+20S	1	21	19	53	.1	16	5	116	4.24	11	5	ND	3	5	1	2	2	18	.04	.047	22	15	.17	19	.01	5	.64	.01	.02	1	2
CC8+50W 1+30S	1	15	24	66	.4	14	6	327	3.13	7	5	ND	2	10	1	2	2	26	.08	.049	21	18	.28	59	.01	5	.97	.01	.04	1	1
CC8+50W 1+40S	1	26	36	100	.6	19	10	760	4.09	8	11	ND	2	38	1	2	2	27	.36	.105	14	20	.34	53	.02	2	1.32	.02	.05	1	1
CC8+50W 1+50S	1	42	33	109	.3	29	14	944	4.83	13	8	ND	5	33	1	2	2	23	.40	.097	19	18	.47	48	.02	7	1.14	.02	.03	1	1
CC8+50W 1+60S	1	47	37	124	.5	24	12	1201	3.59	7	22	ND	2	95	1	2	2	18	1.29	.169	9	22	.47	67	.01	5	1.19	.02	.06	2	1
CC8+50W 1+70S	1	46	28	117	.4	24	15	1650	4.55	7	11	ND	2	86	1	2	2	23	1.07	.168	12	23	.44	62	.02	4	1.61	.02	.05	3	1
CC8+50W 1+80S	1	34	44	117	.4	24	14	910	4.86	7	7	ND	4	59	1	2	2	23	.69	.100	14	23	.43	45	.02	2	1.37	.02	.05	1	2
CC8+50W 1+90S	1	29	30	95	.1	21	12	684	3.78	9	5	ND	3	89	1	2	2	18	1.12	.080	10	18	.50	47	.01	2	1.06	.02	.04	1	2
CC8+50W 2+00S	1	38	35	119	.4	26	15	1038	4.55	13	5	ND	4	38	1	2	2	23	.40	.080	17	21	.45	46	.01	2	1.21	.02	.05	2	3
CC7+50W 1+00N	1	18	18	43	.5	15	4	262	2.76	51	5	ND	2	8	1	2	2	20	.11	.080	16	11	.11	54	.01	3	.51	.01	.04	4	8
CC7+50W 0+90N	1	20	25	49	.4	17	5	142	3.85	51	5	ND	3	4	1	5	2	15	.01	.046	17	15	.17	66	.01	2	.73	.01	.03	5	10
CC7+50W 0+80N	1	16	14	45	.2	15	5	1337	2.36	46	5	ND	2	6	1	2	2	16	.09	.062	17	11	.13	97	.01	2	.59	.01	.04	4	9
CC7+50W 0+70N	1	24	23	63	.1	23	7	326	3.73	71	5	ND	3	7	1	3	2	16	.06	.054	20	12	.19	91	.01	2	.71	.01	.04	3	8
CC7+50W 0+60N	1	20	24	55	.2	19	6	145	3.43	57	5	ND	3	4	1	2	2	14	.02	.049	18	14	.20	68	.01	2	.74	.01	.03	3	7
CC7+50W 0+50N	1	26	30	69	.9	24	9	1752	3.89	55	5	ND	2	6	1	3	2	18	.03	.068	17	14	.18	120	.01	2	.70	.01	.04	3	5
CC7+50W 0+40N	1	6	11	27	.5	6	2	96	1.32	22	5	ND	2	5	1	2	2	14	.02	.039	22	10	.08	49	.01	2	.43	.01	.03	2	19
CC7+50W 0+30N	1	44	40	93	.2	43	16	626	4.77	62	5	ND	7	9	1	2	2	16	.09	.049	26	17	.37	80	.01	2	1.03	.01	.04	4	34
CC7+50W 0+20N	1	22	20	64	.7	22	7	301	3.76	43	5	ND	3	7	1	2	2	18	.06	.045	22	17	.21	85	.01	2	.75	.01	.04	2	23
CC7+50W 0+10N	1	27	28	68	.6	23	10	846	3.96	41	5	ND	3	6	1	3	2	16	.06	.054	20	16	.19	110	.01	3	.73	.01	.04	3	64
CC7+50W 0+00N	1	32	29	83	.2	27	10	309	4.62	21	5	ND	5	5	1	2	2	18	.02	.047	23	22	.36	71	.01	2	1.13	.01	.05	2	5
CC7+50W 0+10S	1	24	29	65	.1	22	8	268	3.56	23	5	ND	3	7	1	2	2	18	.07	.054	20	18	.25	76	.01	2	.85	.01	.04	2	28
STD C/AU-S	18	58	40	132	7.1	67	27	1028	3.94	36	24	7	38	50	18	18	21	56	.47	.089	37	58	.87	178	.08	33	1.82	.08	.13	12	52



SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
CC7+50W 0+20S	1	18	22	60	.5	18	8	382	3.25	15	5	ND	4	7	1	3	2	20	.08	.052	23	20	.31	157	.01	2	.97	.01	.05	1	2
CC7+50W 0+30S	1	27	29	69	.5	21	10	465	3.88	19	5	ND	5	5	1	3	2	21	.04	.058	22	22	.35	91	.01	2	1.15	.01	.05	2	9
CC7+50W 0+40S	1	37	181	192	.8	37	21	837	5.16	28	5	ND	10	26	1	4	2	25	.41	.088	37	24	.49	64	.02	2	1.06	.02	.05	46	265
CC7+50W 0+50S	1	55	40	95	.3	38	21	988	5.79	25	5	ND	9	7	1	4	2	17	.08	.060	30	22	.45	39	.01	2	1.04	.01	.03	1	7
CC7+50W 0+60S	1	23	41	57	.7	14	6	237	3.82	9	5	ND	2	22	1	3	2	27	.32	.054	19	21	.25	62	.01	2	1.20	.02	.04	1	5
CC7+50W 0+70S	1	35	47	72	.2	14	6	201	5.02	12	5	ND	3	7	1	2	2	30	.06	.047	20	21	.19	59	.01	3	1.19	.01	.03	2	2
CC7+50W 0+80S	1	25	42	78	.4	17	9	458	4.28	11	5	ND	3	43	1	2	2	29	.59	.056	19	21	.29	69	.01	2	1.39	.02	.04	1	4
CC7+50W 0+90S	1	61	41	122	.3	32	16	977	5.05	13	5	ND	5	40	1	2	2	20	.49	.086	18	23	.43	74	.01	4	1.30	.02	.05	1	10
CC7+50W 1+00S	1	55	49	100	.5	25	13	761	4.32	12	5	ND	4	52	1	2	3	17	.82	.083	17	20	.33	57	.01	2	1.07	.02	.04	7	825
CC7+50W 1+10S	1	29	48	81	.3	19	11	397	4.41	22	5	ND	4	43	1	2	2	21	.67	.073	17	22	.35	52	.01	3	1.26	.02	.05	2	8
CC7+50W 1+20S	1	48	46	90	.5	26	18	754	5.82	25	5	ND	6	34	1	2	2	23	.51	.058	22	19	.40	59	.01	2	1.24	.02	.05	1	13
CC7+50W 1+30S	1	56	44	106	.4	29	17	1251	6.57	16	5	ND	6	12	1	2	2	24	.09	.065	22	22	.39	78	.01	2	1.37	.02	.04	2	38
CC7+50W 1+40S	1	51	37	107	.3	36	17	795	4.84	14	5	ND	8	26	1	2	2	18	.41	.075	29	17	.44	54	.01	2	.95	.02	.04	1	11
CC7+50W 1+50S	1	38	31	89	.4	27	13	761	4.78	9	5	ND	5	35	1	2	2	23	.56	.091	19	23	.40	77	.01	3	1.38	.02	.04	1	8
CC7+50W 1+60S	1	97	38	98	.4	33	17	897	5.35	11	5	ND	6	32	1	3	2	25	.54	.106	23	23	.50	65	.01	3	1.50	.02	.04	1	7
CC7+50W 1+70S	1	36	39	86	.6	24	14	1090	5.02	7	5	ND	5	18	1	5	2	24	.22	.104	17	24	.41	68	.01	5	1.35	.02	.04	1	3
CC7+50W 1+80S	1	25	27	66	.3	18	7	202	4.14	4	5	ND	3	6	1	2	2	28	.03	.058	21	27	.33	53	.01	5	1.28	.01	.03	1	22
CC7+50W 1+90S	1	41	37	101	.5	30	13	767	4.46	12	5	ND	5	42	1	2	2	20	.68	.093	23	24	.42	81	.01	3	1.32	.02	.04	1	4
CC7+50W 2+00S	1	17	27	65	.2	20	6	157	3.31	9	5	ND	4	12	1	2	2	22	.14	.057	22	28	.36	53	.01	2	1.05	.01	.04	1	19
CC6+50W 0+00S	1	39	37	93	.4	39	15	760	4.61	45	5	ND	7	35	1	2	2	16	.49	.063	19	19	.37	87	.01	3	1.12	.02	.06	2	23
CC6+50W 0+10S	1	40	36	94	.2	40	16	669	4.71	40	5	ND	8	20	1	4	2	17	.25	.054	26	23	.42	80	.01	2	1.14	.02	.05	3	28
CC6+50W 0+20S	1	46	38	101	.5	38	16	771	4.91	37	5	ND	7	17	1	2	2	18	.19	.062	26	20	.40	100	.01	2	1.36	.02	.08	4	20
CC6+50W 0+30S	1	46	82	120	.5	37	15	618	4.60	13	5	ND	7	23	1	2	2	21	.26	.055	28	25	.51	82	.01	2	1.26	.02	.07	2	13
CC6+50W 0+40S	1	46	61	123	.4	39	16	657	4.95	13	5	ND	10	18	1	2	2	21	.26	.056	32	26	.53	74	.01	2	1.23	.02	.07	1	37
CC6+50W 0+50S	1	42	236	252	.6	38	16	930	5.48	19	5	ND	7	27	1	2	2	21	.36	.070	27	27	.45	74	.01	2	1.31	.02	.07	4	28
CC6+50W 0+60S	1	28	218	179	.5	24	10	330	4.38	19	5	ND	6	15	1	2	2	20	.17	.055	23	19	.34	42	.01	2	1.09	.01	.05	7	41
CC6+50W 0+70S	1	38	85	145	.6	27	14	1106	4.44	10	5	ND	4	30	1	2	2	18	.46	.082	17	20	.34	58	.01	2	1.19	.02	.03	1	11
CC6+50W 0+80S	1	32	86	231	.4	22	14	1164	6.30	14	5	ND	4	14	2	3	2	24	.09	.068	16	25	.27	81	.02	2	1.30	.02	.05	10	6
CC6+50W 0+90S	1	72	55	152	.3	37	21	1499	6.25	20	5	ND	6	15	1	3	3	17	.14	.069	25	18	.34	95	.01	5	1.03	.02	.05	2	33
CC6+50W 1+00S	1	27	30	85	.3	19	8	328	5.16	8	5	ND	3	6	1	2	2	25	.03	.049	19	22	.27	48	.01	2	1.22	.01	.04	1	2
CC6+50W 1+10S	1	21	19	53	.3	12	7	539	4.22	12	5	ND	3	4	1	3	2	34	.01	.038	22	15	.15	44	.01	2	.90	.01	.02	1	7
CC6+50W 1+20S	1	77	75	117	.4	31	22	2034	6.41	23	5	ND	5	31	1	2	2	12	.81	.088	17	10	.23	72	.01	13	.59	.02	.03	5	6
CC6+50W 1+30S	1	92	38	118	.7	25	25	3538	7.48	28	5	ND	3	49	1	2	2	24	.76	.151	14	16	.27	103	.01	2	1.32	.02	.04	2	7
CC6+50W 1+40S	1	86	24	73	.4	19	14	1313	5.73	11	5	ND	3	52	1	2	2	26	.91	.068	21	16	.28	61	.01	5	1.22	.02	.02	1	3
CC6+50W 1+50S	1	17	10	50	.3	22	12	428	2.99	2	5	ND	6	31	1	2	2	8	.41	.035	14	9	.10	38	.01	3	.66	.02	.03	2	1
CC6+50W 1+60S	1	37	24	90	.4	14	21	868	7.71	7	5	ND	4	24	1	2	2	35	.38	.072	12	21	.36	60	.01	2	1.85	.02	.03	2	1
STD C/AU-S	18	60	42	132	7.3	68	27	1029	4.08	40	19	8	39	50	17	16	20	56	.49	.090	37	59	.90	180	.08	33	1.87	.08	.13	13	42

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	M	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
CC6+S0W 1+70S	1	38	26	105	.2	26	19	712	6.19	16	5	ND	6	8	1	2	2	29	.08	.060	16	24	.39	77	.01	2	1.65	.01	.02	1	24
CC6+S0W 1+80S	1	24	13	44	.1	13	5	234	3.23	10	5	ND	2	26	1	2	2	17	.44	.032	15	9	.11	62	.01	2	.52	.01	.01	2	6
CC6+S0W 1+90S	1	36	34	82	.1	23	10	490	6.78	21	5	ND	4	4	1	2	2	20	.03	.045	19	14	.18	41	.01	2	.92	.01	.01	1	23
CC6+S0W 2+00S	1	30	20	103	.2	22	12	2230	3.98	10	5	ND	3	50	1	2	2	15	1.12	.127	11	14	.32	127	.01	2	.92	.02	.02	1	2
CC6+S0W 2+10S	1	31	28	72	.1	17	13	683	5.00	16	5	ND	3	9	1	2	2	22	.09	.066	19	18	.23	42	.01	2	1.31	.01	.02	1	165
CC6+S0W 2+20S	1	21	29	68	.1	13	7	544	4.35	10	5	ND	2	5	1	3	2	22	.02	.058	15	15	.20	38	.01	2	1.03	.01	.02	1	3
CC6+S0W 2+30S	1	21	14	44	.2	12	7	1666	2.65	7	5	ND	3	4	1	2	2	23	.02	.037	26	13	.11	80	.01	2	.80	.01	.03	2	1
CC6+S0W 2+40S	1	28	39	78	.1	23	9	674	5.06	21	5	ND	2	6	1	2	2	25	.06	.077	15	23	.29	48	.01	2	1.17	.01	.03	1	1
CC6+S0W 2+50S	1	43	23	82	.1	28	12	477	4.31	18	5	ND	4	5	1	2	2	23	.07	.063	16	24	.39	49	.01	2	1.08	.01	.04	1	1
CC6+S0W 2+60S	1	43	22	71	.3	25	12	573	3.92	13	5	ND	4	10	1	2	2	24	.16	.068	17	19	.38	52	.01	6	1.08	.01	.03	1	2
CC6+S0W 2+70S	1	39	30	80	.2	26	14	1263	3.53	7	5	ND	3	15	1	2	2	19	.26	.094	18	16	.31	116	.01	5	1.06	.02	.05	1	1
CC6+S0W 2+80S	1	30	49	75	.1	23	8	433	4.82	14	5	ND	3	7	1	2	2	26	.08	.058	17	26	.30	89	.01	3	1.12	.01	.03	1	24
CC6+S0W 2+90S	1	37	32	98	.2	38	15	1140	4.24	14	5	ND	5	9	1	3	2	24	.09	.083	17	38	.53	86	.01	2	1.40	.01	.04	1	5
CC6+S0W 3+00S	2	25	21	87	.1	23	9	419	3.72	12	5	ND	3	11	1	2	2	24	.19	.052	16	24	.32	117	.01	3	.94	.01	.04	1	3
CC5+00W 2+10S	1	9	13	40	.1	9	4	557	3.53	5	5	ND	2	4	1	2	2	30	.03	.045	22	15	.17	36	.01	4	.91	.01	.02	2	2
CC5+00W 2+20S	1	31	17	59	.1	10	8	669	4.27	10	5	ND	2	6	1	2	2	62	.02	.042	15	12	.29	56	.02	2	1.12	.01	.02	1	1
CC5+00W 2+30S	1	58	21	87	.3	14	15	2189	3.99	13	5	ND	2	52	1	2	2	47	.97	.092	16	13	.42	74	.01	2	1.56	.02	.02	1	5
CC5+00W 2+40S	1	81	21	72	.5	14	9	1051	4.05	13	6	ND	2	36	1	2	2	24	.72	.075	32	14	.19	116	.01	2	1.16	.02	.03	2	11
CC5+00W 2+50S	1	37	38	109	.4	18	11	1136	4.83	18	6	ND	2	38	1	2	2	20	.78	.088	12	17	.20	62	.01	5	1.44	.02	.02	2	6
CC5+00W 2+60S	1	13	20	37	.2	9	4	119	3.13	8	5	ND	3	5	1	3	2	12	.05	.032	19	8	.08	24	.01	2	.52	.01	.02	2	2
CC5+00W 2+70S	1	7	44	114	.3	7	9	1541	13.82	13	5	ND	2	19	1	2	2	29	.38	.120	5	10	.11	21	.01	2	.65	.02	.03	22	24
CC5+00W 2+80S	1	19	48	119	.6	13	10	1505	4.43	13	5	ND	2	48	1	2	2	16	1.10	.112	9	13	.21	57	.01	2	.86	.02	.02	17	3
CC5+00W 2+90S	1	26	27	97	.2	17	11	577	4.37	13	6	ND	3	28	1	2	2	20	.57	.102	16	19	.31	62	.01	4	1.34	.02	.03	1	5
CC5+00W 3+00S	1	20	25	91	.6	15	9	941	4.06	10	5	ND	2	10	1	2	2	24	.06	.069	17	17	.25	75	.01	3	1.26	.01	.04	2	11
CC5+00W 3+10S	1	16	9	38	.1	8	4	168	2.20	7	5	ND	2	6	1	4	2	25	.08	.036	18	9	.08	41	.01	2	.53	.01	.02	2	1
CC5+00W 3+20S	1	85	27	90	.8	21	13	2597	3.55	8	8	ND	2	32	1	2	2	13	.96	.129	19	13	.21	102	.01	2	1.06	.02	.03	1	1
CC5+00W 3+30S	1	31	25	84	.3	19	8	299	5.31	12	5	ND	4	8	1	2	2	24	.17	.045	20	19	.32	67	.01	2	1.09	.01	.03	1	1
CC5+00W 3+40S	1	106	34	116	1.1	34	18	2201	4.56	14	6	ND	3	28	1	2	2	16	.77	.107	13	18	.34	97	.01	2	1.44	.02	.03	1	3
CC5+00W 3+50S	1	29	27	85	.1	18	8	313	4.71	14	5	ND	2	10	1	2	2	22	.14	.060	14	16	.25	56	.01	2	.99	.01	.03	2	3
CC5+00W 3+60S	1	27	24	76	.3	15	8	514	4.18	8	5	ND	2	7	1	3	2	23	.12	.057	19	13	.17	70	.01	2	.80	.01	.03	1	1
CC5+00W 3+70S	1	37	29	96	.6	20	10	587	3.97	13	5	ND	4	21	1	2	2	15	.44	.096	14	11	.24	45	.01	2	1.00	.01	.03	1	6
CC5+00W 3+80S	1	49	39	110	.6	22	13	675	4.71	13	5	ND	5	8	1	2	2	21	.04	.070	25	14	.20	53	.01	2	1.35	.01	.03	1	1
CC5+00W 3+90S	1	57	26	110	.4	17	21	1719	5.89	15	5	ND	2	13	1	3	2	32	.23	.160	10	11	.23	61	.01	2	1.15	.01	.03	1	1
CC5+00W 4+00S	1	51	28	103	.3	20	17	1426	5.25	15	5	ND	2	17	1	2	2	33	.28	.080	19	15	.30	64	.01	3	1.21	.02	.04	1	1
CC5+00W 4+10S	1	60	25	88	.2	20	20	923	6.21	16	5	ND	3	6	1	3	2	28	.04	.088	14	14	.35	48	.01	2	1.23	.01	.04	1	1
CC5+00W 4+20S	1	32	17	76	.1	15	8	620	4.10	14	5	ND	2	10	1	2	2	33	.22	.062	17	15	.20	73	.01	2	.76	.01	.04	1	18
STD C/AU-S	19	58	41	132	6.9	70	26	1029	3.94	40	21	8	37	49	18	15	20	58	.48	.086	38	58	.87	175	.08	36	1.82	.06	.15	13	50

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUT
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
ECS+00M 4+30S	1	57	49	97	.9	33	15	1766	4.08	26	5	ND	3	26	1	2	2	20	.48	.143	23	20	.34	55	.01	4	1.77	.02	.05	1	1
ECS+00M 4+40S	1	51	49	96	.5	31	18	1781	4.69	12	5	ND	3	13	1	2	2	22	.14	.171	23	25	.36	47	.01	3	1.77	.02	.06	1	1
ECS+00M 4+50S	1	64	30	94	.3	30	16	895	6.06	4	5	ND	3	6	1	2	2	45	.06	.089	25	28	.50	67	.01	4	1.56	.01	.05	1	2
ECS+00M 4+60S	1	81	27	80	.3	19	11	529	6.37	3	5	ND	3	6	1	2	2	47	.03	.077	26	23	.31	70	.01	5	1.24	.01	.01	1	24
ECS+00M 4+70S	1	47	30S	117	.4	39	16	1526	5.76	13	5	ND	3	11	1	2	2	43	.15	.121	22	42	.37	165	.01	4	1.16	.01	.06	1	1
ECS+00M 4+80S	1	54	68	102	1.0	41	17	1206	6.27	19	5	ND	3	17	1	2	2	47	.20	.122	28	43	.29	105	.01	4	1.14	.02	.05	1	1
ECS+00M 4+90S	1	31	22	76	.7	31	7	283	4.28	11	5	ND	3	9	1	2	2	40	.16	.112	28	31	.29	68	.01	2	.93	.01	.07	1	2
ECS+00M 5+00S	3	59	29	105	.3	54	16	570	4.85	34	5	ND	9	12	1	2	2	24	.17	.100	40	23	.40	58	.01	7	1.00	.02	.07	1	1
CC4+00M 2+10S	1	35	24	79	.1	8	7	515	5.96	22	5	ND	2	5	1	2	2	21	.03	.084	17	6	.07	31	.01	4	.44	.01	.04	3	1
CC4+00M 2+20S	1	22	22	81	.2	16	8	1166	5.83	15	5	ND	3	8	1	2	2	35	.09	.067	26	20	.19	66	.02	2	1.06	.01	.05	2	11
CC4+00M 2+30S	1	18	17	96	.2	18	13	2899	3.78	2	5	ND	2	23	1	2	2	28	.46	.062	20	24	.33	125	.02	2	1.36	.02	.04	1	1
CC4+00M 2+40S	1	20	15	86	.3	16	8	1289	4.29	2	5	ND	4	15	1	2	2	31	.21	.060	47	21	.29	77	.02	2	1.23	.02	.05	1	2
CC4+00M 2+50S	1	24	13	67	.4	19	9	1109	4.72	2	5	ND	5	12	1	2	2	30	.10	.066	52	20	.40	73	.01	2	1.50	.01	.03	1	1
CC4+00M 2+60S	1	50	24	96	.2	16	14	2002	6.62	2	5	ND	3	17	1	2	2	67	.29	.099	20	20	.87	53	.02	2	2.23	.02	.04	1	1
CC4+00M 2+70S	1	47	16	97	.1	14	13	955	7.70	11	5	ND	2	5	1	2	2	32	.02	.089	23	12	.12	36	.01	3	.73	.01	.04	1	10
CC4+00M 2+80S	1	36	19	82	.2	18	12	1180	5.93	4	5	ND	3	6	1	2	2	38	.06	.094	26	24	.38	44	.01	8	1.60	.02	.04	1	1
CC4+00M 2+90S	1	23	62	151	.1	19	12	7148	7.59	16	5	ND	3	22	1	2	2	29	.27	.135	23	16	.17	118	.01	6	1.43	.02	.05	1	3
CC4+00M 3+00S	1	28	32	77	.2	12	9	988	6.26	8	5	ND	2	6	1	2	2	41	.03	.088	23	17	.17	38	.02	2	.96	.01	.05	3	17
CC4+00M 3+10S	1	29	16	57	.3	10	7	488	5.04	6	5	ND	2	6	1	2	2	41	.03	.096	23	17	.20	40	.01	3	.90	.01	.04	1	9
CC4+00M 3+20S	1	38	19	65	.3	13	7	458	4.83	7	5	ND	2	6	1	2	2	42	.03	.057	26	17	.29	43	.02	2	1.11	.01	.04	1	2
CC4+00M 3+30S	1	80	20	108	.1	14	15	999	10.17	3	5	ND	3	7	1	2	2	47	.10	.077	17	15	.38	71	.02	2	1.66	.01	.04	1	8
CC4+00M 3+40S	1	86	19	103	.5	28	10	346	3.84	6	6	ND	3	15	1	2	2	21	.42	.123	22	24	.48	74	.01	3	1.77	.02	.03	1	2
CC4+00M 3+50S	1	57	27	115	.3	27	15	2897	4.57	11	5	ND	3	20	1	2	2	29	.49	.093	24	26	.47	149	.02	2	1.81	.02	.05	1	1
CC4+00M 3+60S	1	23	17	68	.2	17	7	250	4.65	8	5	ND	5	6	1	2	2	36	.05	.042	34	24	.30	46	.02	2	1.22	.01	.05	1	60
CC4+00M 3+70S	1	19	19	83	.1	20	9	342	5.66	42	5	ND	4	5	1	2	2	29	.03	.074	29	19	.29	42	.01	2	1.46	.01	.04	1	5
CC4+00M 3+80S	1	27	32	98	.2	17	9	835	4.86	122	5	ND	4	6	1	2	2	33	.02	.053	30	17	.19	65	.02	3	1.11	.01	.05	1	2
CC4+00M 3+90S	1	43	54	143	.2	14	9	464	6.60	23	5	ND	2	9	1	2	2	52	.12	.091	19	13	.32	107	.01	2	1.39	.01	.04	1	2
CC4+00M 4+00S	2	41	58	135	.5	23	20	2757	5.58	26	5	ND	3	13	1	2	2	34	.17	.098	24	20	.30	69	.02	2	1.66	.01	.06	1	1
CC4+00M 4+10S	1	21	26	66	.2	13	5	170	4.03	11	5	ND	4	6	1	2	2	28	.08	.055	40	15	.14	54	.01	2	.85	.01	.04	1	16
CC4+00M 4+20S	1	21	38	66	.4	13	5	278	3.86	2	5	ND	4	8	1	2	2	27	.08	.058	37	18	.25	44	.01	2	1.14	.01	.06	1	1
CC4+00M 4+30S	1	33	24	68	.3	14	6	293	4.05	4	5	ND	4	7	1	2	2	30	.05	.060	35	14	.22	33	.01	2	1.03	.01	.05	1	3
CC4+00M 4+40S	2	33	28	72	.4	19	9	513	4.31	6	5	ND	5	6	1	2	2	28	.05	.049	41	13	.11	57	.01	3	.82	.01	.06	1	1
CC4+00M 4+50S	1	25	16	60	.3	16	6	179	2.66	4	5	ND	4	11	1	3	2	29	.14	.043	40	11	.08	48	.01	4	.60	.01	.05	1	4
CC4+00M 4+60S	1	20	22	60	.2	18	7	192	3.98	8	5	ND	3	5	1	2	2	28	.02	.050	35	18	.20	38	.01	3	.85	.01	.04	1	1
CC4+00M 4+70S	1	37	31	72	.3	22	14	704	5.36	10	5	ND	3	11	1	2	2	32	.14	.105	26	21	.26	53	.01	2	1.21	.01	.05	1	1
CC4+00M 4+80S	1	54	37	109	.3	27	25	1784	5.53	16	5	ND	5	8	1	2	2	27	.06	.108	27	17	.39	66	.01	2	1.64	.01	.04	1	1
STD C	18	58	44	132	7.1	68	27	1028	3.96	36	23	8	37	48	18	18	21	55	.48	.086	36	59	.87	171	.08	31	1.82	.07	.14	12	39

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM	
CC4+00W 4400S	1	22	22	56	.3	14	4	123	4.03	14	5	ND	3	4	1	2	2	23	.02	.062	21	17	.25	38	.01	2	.95	.01	.03	1	1
CC4+00W 5400S	1	66	35	121	.5	23	19	2923	5.11	16	5	ND	4	30	1	2	2	26	.71	.200	18	13	.41	77	.01	2	1.69	.02	.05	3	1
CC3+00W 2410S	1	16	11	41	.4	7	4	521	3.27	11	5	ND	2	5	1	2	2	28	.03	.051	21	10	.05	32	.01	2	.48	.01	.03	3	3
CC3+00W 2420S	1	56	29	62	.1	12	9	812	6.91	21	5	ND	3	4	1	2	2	22	.01	.079	16	10	.08	26	.01	5	.61	.01	.02	1	16
CC3+00W 2430S	1	21	46	83	.1	14	11	1767	7.90	15	5	ND	3	4	1	2	2	21	.02	.071	16	13	.14	29	.01	2	.91	.01	.02	6	1
CC3+00W 2440S	1	26	32	99	.1	15	9	1205	6.97	12	5	ND	2	8	1	2	2	30	.09	.078	15	17	.16	68	.01	3	.75	.01	.03	3	11
CC3+00W 2450S	1	29	37	123	.2	21	16	1856	5.85	14	5	ND	2	12	1	2	2	28	.11	.081	16	22	.29	105	.01	2	1.31	.01	.04	2	3
CC3+00W 2460S	1	27	29	86	.1	16	12	1741	4.84	10	5	ND	2	7	1	2	2	26	.05	.071	17	15	.18	66	.01	2	.99	.01	.04	1	7
CC3+00W 2470S	1	49	27	103	.3	22	14	1500	6.20	13	5	ND	3	6	1	2	2	24	.06	.079	16	19	.27	79	.01	2	1.12	.01	.04	2	41
CC3+00W 2480S	1	67	67	149	.2	24	16	2289	9.29	25	5	ND	3	12	1	2	2	25	.14	.104	17	19	.24	91	.01	2	1.12	.01	.05	2	3
CC3+00W 2490S	2	236	50	192	.2	21	20	5188	18.89	28	5	ND	3	13	1	2	2	23	.17	.149	11	12	.19	93	.01	2	.81	.01	.04	1	4
CC3+00W 3400S	1	35	51	134	.4	27	16	1662	6.75	9	5	ND	6	9	1	2	2	23	.08	.086	39	19	.23	65	.01	2	1.29	.01	.04	3	2
CC3+00W 3410S	1	61	34	109	.5	32	20	1440	6.15	9	5	ND	6	11	1	2	2	24	.15	.080	37	22	.38	62	.01	2	1.31	.01	.04	2	3
CC3+00W 3420S	1	26	32	118	.4	21	16	2957	5.47	10	5	ND	2	20	1	2	2	33	.32	.105	16	24	.36	79	.01	2	1.74	.02	.06	1	4
CC3+00W 3430S	1	12	20	62	.2	17	6	338	3.25	6	5	ND	2	8	1	2	2	28	.11	.046	21	20	.28	69	.01	2	1.17	.01	.03	1	1
CC3+00W 3440S	1	19	21	69	.1	18	6	226	4.45	6	5	ND	2	5	1	2	2	27	.03	.055	29	27	.21	47	.01	2	1.31	.01	.03	2	1
CC3+00W 3450S	1	17	19	65	.2	20	8	417	4.87	7	5	ND	2	4	1	2	2	30	.01	.059	16	22	.41	38	.02	4	1.28	.01	.04	1	1
CC3+00W 3460S	1	12	13	42	.2	53	4	291	2.80	4	5	ND	1	4	1	2	2	30	.02	.063	17	19	.21	21	.01	2	.85	.01	.03	3	1
CC3+00W 3470S	1	7	12	27	.2	7	3	262	2.99	6	5	ND	2	3	1	2	2	39	.02	.053	22	13	.11	21	.02	2	.65	.01	.02	1	1
CC3+00W 3480S	1	16	20	49	.2	12	5	345	4.08	8	5	ND	2	4	1	2	2	30	.02	.054	19	18	.19	41	.01	2	1.00	.01	.03	2	1
CC3+00W 3490S	1	64	22	79	.4	18	10	716	4.05	2	5	ND	2	7	1	2	2	31	.07	.062	17	24	.42	73	.01	2	1.84	.01	.04	2	7
CC3+00W 4400S	1	41	16	82	.2	13	10	624	5.01	8	5	ND	2	7	1	2	2	42	.13	.083	15	15	.35	88	.01	2	1.38	.01	.04	1	1
CC3+00W 4410S	1	43	33	100	.3	23	19	1732	4.56	6	5	ND	2	18	1	2	2	29	.51	.127	19	21	.37	114	.01	2	1.53	.02	.05	1	1
CC3+00W 4420S	1	42	27	105	.5	22	12	1932	3.72	10	5	ND	3	30	1	2	2	19	.98	.205	12	19	.33	114	.01	2	1.48	.02	.05	1	1
CC3+00W 4430S	1	29	28	67	.6	21	7	922	3.51	8	5	ND	2	13	1	2	2	22	.25	.163	20	18	.27	45	.01	2	1.43	.01	.04	2	1
CC3+00W 4440S	1	47	39	71	.4	19	12	1600	3.53	8	5	ND	2	12	1	2	2	21	.17	.110	21	16	.22	46	.01	2	1.18	.01	.04	1	1
CC3+00W 4450S	1	65	35	94	.5	19	10	976	3.95	9	5	ND	1	10	1	2	2	24	.15	.121	16	15	.21	47	.01	3	1.43	.01	.04	1	1
CC3+00W 4460S	1	20	21	55	.3	13	6	242	3.52	10	5	ND	2	4	1	2	2	26	.02	.051	20	16	.23	39	.01	3	1.00	.01	.03	1	1
CC3+00W 4470S	1	37	35	84	.3	20	11	519	4.16	8	5	ND	2	8	1	2	2	22	.11	.076	22	20	.34	37	.01	2	1.26	.01	.04	2	3
CC3+00W 4480S	1	22	27	63	.3	11	5	190	3.68	9	5	ND	2	7	1	2	2	29	.07	.061	17	15	.21	50	.01	2	.89	.01	.05	2	1
CC3+00W 4490S	1	38	35	80	.2	18	14	672	4.90	13	5	ND	2	5	1	2	2	31	.02	.085	19	18	.30	38	.01	2	1.28	.01	.05	1	1
CC3+00W 5400S	1	53	51	97	.5	26	18	1995	4.99	11	5	ND	2	15	1	2	2	24	.24	.153	15	20	.32	49	.01	2	1.44	.01	.05	1	13
CC0450E 2400N	1	23	26	77	.3	21	10	689	3.88	11	5	ND	2	12	1	2	2	26	.11	.059	21	21	.33	48	.01	2	1.17	.01	.05	4	6
CC0450E 1490N	1	53	24	90	.3	42	16	887	5.38	13	5	ND	4	9	1	2	2	18	.06	.065	28	26	.50	38	.01	2	1.47	.01	.04	4	10
CC0450E 1480N	1	37	101	82	.3	33	21	2051	4.02	20	5	ND	2	24	1	2	2	21	.17	.118	15	15	.15	54	.01	2	1.18	.01	.06	1	5
CC0450E 1470N	1	35	64	97	.3	43	24	2220	4.40	9	5	ND	2	20	1	2	2	17	.21	.121	13	16	.18	51	.01	2	.89	.01	.06	2	3
STD C/AU-S	18	58	42	132	7.2	68	27	1039	3.99	39	19	7	39	50	19	15	18	57	.48	.089	37	60	.88	177	.08	33	1.83	.08	.13	13	52

SAMPLE#	ND	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUX
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
CC0+50E 1+60N	1	38	32	94	.3	39	17	893	5.07	44	5	ND	3	13	1	2	2	22	.11	.064	20	13	.10	67	.01	2	.71	.01	.04	3	270
CC0+50E 1+50N	1	35	33	94	.1	36	23	1513	4.19	28	5	ND	2	10	1	2	2	21	.11	.078	19	14	.12	69	.01	7	.62	.01	.05	1	46
CC0+50E 1+40N	1	40	193	129	.2	32	23	1496	5.33	19	5	ND	2	12	1	2	2	21	.11	.081	17	13	.14	70	.01	2	.76	.01	.05	1	7
CC0+50E 1+30N	1	27	115	115	.2	31	14	542	4.48	9	5	ND	2	11	1	2	2	22	.12	.063	20	12	.13	49	.01	2	.68	.01	.06	1	1
CC0+50E 1+20H	2	33	191	140	.3	33	20	2872	5.01	9	5	ND	2	23	1	2	2	21	.33	.147	15	20	.26	139	.01	3	1.22	.02	.06	1	2
CC0+50E 1+10N	2	51	103	151	.5	55	27	2312	5.50	24	5	ND	2	20	1	2	2	16	.31	.152	15	18	.26	52	.01	2	1.27	.02	.04	1	49
CC0+50E 1+00N	1	28	33	113	.2	39	15	1156	4.26	21	5	ND	2	17	1	2	2	19	.27	.061	22	17	.21	118	.01	2	.70	.01	.06	1	23
CC0+50E 0+90N	1	36	48	99	.4	45	23	1793	4.59	23	5	ND	3	16	1	2	2	19	.24	.098	18	24	.35	52	.01	4	1.29	.02	.06	1	7
CC0+50E 0+80N	1	29	51	204	.3	35	19	2224	4.31	15	5	ND	2	17	1	2	2	20	.26	.110	17	22	.33	78	.01	2	1.26	.02	.06	1	13
CC0+50E 0+70N	1	32	101	110	.6	34	15	1787	3.93	17	5	ND	2	19	1	2	2	18	.28	.145	15	20	.30	69	.01	2	1.34	.02	.07	1	19
CC0+50E 0+60N	1	28	81	105	.2	31	16	1433	4.33	17	5	ND	2	13	1	2	2	19	.17	.097	18	17	.27	78	.01	2	1.10	.01	.06	1	18
CC0+50E 0+50N	1	52	101	136	.4	37	15	979	4.09	20	5	ND	2	18	1	2	2	18	.28	.091	18	20	.33	65	.01	2	1.18	.02	.06	1	19
CC0+50E 0+40N	1	25	58	91	.3	26	11	636	4.29	17	5	ND	3	10	1	2	2	22	.11	.088	19	19	.25	65	.01	2	1.08	.01	.06	1	41
CC0+50E 0+30N	1	24	51	81	.2	23	10	595	4.00	16	5	ND	2	8	1	2	2	22	.06	.113	20	18	.22	70	.01	2	.99	.01	.06	1	8
CC0+50E 0+20N	1	23	58	86	.7	24	21	1500	3.87	13	5	ND	2	11	1	2	2	22	.14	.127	17	19	.27	67	.01	2	1.23	.01	.07	1	14
CC0+50E 0+10N	2	21	42	96	.4	22	13	860	3.62	12	5	ND	2	11	1	2	2	22	.12	.108	19	18	.27	67	.01	2	1.12	.01	.07	1	59
CC0+50E 0+00N	2	41	73	135	.2	40	14	464	4.66	17	5	ND	4	7	1	2	2	20	.06	.055	26	29	.49	56	.01	2	1.30	.01	.05	2	56
CC1+00E 2+00N	1	22	188	109	.4	27	11	522	3.33	23	5	ND	3	16	1	2	2	25	.10	.044	27	13	.08	52	.01	2	.66	.01	.05	8	21
CC1+00E 1+90N	1	16	45	69	.3	18	6	402	3.25	7	5	ND	3	8	1	2	2	28	.09	.051	26	18	.19	47	.01	2	.88	.01	.05	1	3
CC1+00E 1+80N	1	24	76	76	.4	26	19	1760	3.19	24	5	ND	2	11	1	2	2	23	.07	.064	21	15	.14	54	.01	2	.92	.01	.05	91	80
CC1+00E 1+70N	1	15	52	70	.2	22	7	190	4.39	11	5	ND	3	7	1	2	2	23	.03	.055	22	23	.25	46	.01	2	1.14	.01	.05	1	4
CC1+00E 1+60N	1	25	20	79	.3	32	13	1371	3.71	9	5	ND	2	10	1	2	2	28	.10	.068	20	18	.13	73	.01	3	.76	.01	.05	1	3
CC1+00E 1+50N	1	33	30	84	.2	41	17	694	4.91	25	5	ND	2	9	1	2	2	32	.08	.068	17	33	.32	53	.01	3	1.07	.01	.03	1	52
CC1+00E 1+40N	1	24	46	86	.1	28	12	682	5.01	13	5	ND	2	9	1	2	2	35	.06	.064	20	32	.27	43	.01	2	1.11	.01	.06	1	2
CC1+00E 1+30N	1	27	207	106	.3	29	16	1733	4.34	14	5	ND	2	11	1	2	2	25	.09	.080	19	17	.15	73	.01	5	.96	.01	.05	2	3
CC1+00E 1+20N	1	32	301	139	.3	34	17	1699	4.32	19	5	ND	3	19	1	2	2	25	.27	.074	19	22	.28	51	.01	2	1.21	.02	.06	10	24
CC1+00E 1+10N	1	24	24	73	.2	22	7	223	3.57	22	5	ND	3	10	1	2	2	27	.13	.039	27	15	.14	67	.02	3	.62	.01	.04	1	11
CC1+00E 1+00N	1	35	222	278	.5	51	16	658	4.62	30	5	ND	5	11	1	2	2	22	.12	.048	25	23	.40	33	.02	2	1.12	.01	.04	2	164
CC1+00E 0+90N	1	28	113	96	.6	28	13	1011	4.01	16	5	ND	2	15	1	2	2	24	.20	.062	19	18	.24	96	.01	2	1.08	.01	.05	2	40
CC1+00E 0+80N	1	27	66	85	.3	26	16	1118	4.08	20	5	ND	2	8	1	2	2	21	.08	.075	20	18	.25	57	.01	3	1.14	.01	.05	2	17
CC1+00E 0+70N	1	28	54	75	.6	24	9	468	3.71	16	5	ND	2	8	1	2	2	24	.08	.078	20	19	.24	66	.01	2	1.30	.01	.06	4	4
CC1+00E 0+60N	1	23	32	66	.9	21	9	682	3.49	14	5	ND	2	8	1	2	2	22	.06	.067	21	18	.22	60	.01	2	1.00	.01	.05	4	17
CC1+00E 0+50N	1	24	30	82	.6	20	8	649	2.73	9	5	ND	2	11	1	2	2	19	.14	.097	19	17	.23	88	.01	6	1.01	.01	.07	1	1
CC1+00E 0+40N	1	32	48	132	.3	33	13	725	4.23	20	5	ND	2	12	1	2	2	19	.17	.083	21	23	.37	66	.01	4	1.18	.02	.07	3	18
CC1+00E 0+30N	1	19	27	67	1.0	18	7	347	2.76	6	5	ND	2	7	1	2	2	19	.06	.096	19	19	.28	44	.01	2	1.31	.01	.05	1	21
CC1+00E 0+20N	1	27	35	80	.6	23	10	508	3.55	11	5	ND	2	8	1	2	2	22	.07	.110	20	26	.35	57	.01	2	1.64	.01	.07	2	3
STD C/AU-S	18	59	44	132	7.4	68	27	1054	4.12	40	22	8	39	51	19	14	21	57	.49	.091	38	61	.91	181	.08	33	1.90	.08	.13	12	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
CC1+00E 0+10N	1	24	37	96	.9	26	12	977	3.49	6	5	ND	2	10	1	2	2	22	.10	.106	21	24	.38	68	.01	5	1.37	.01	.07	1	4
CC1+00E 0+00N	2	25	34	118	.5	35	13	718	3.94	11	5	ND	3	13	1	2	2	20	.15	.075	25	32	.43	46	.01	8	1.15	.02	.07	1	8
CC1+50E 2+00N	1	24	28	79	.8	25	12	612	3.69	13	5	ND	2	9	1	2	2	30	.05	.064	22	17	.20	50	.01	2	1.10	.01	.05	1	1
CC1+50E 1+90N	1	22	18	62	.4	21	6	281	3.94	5	5	ND	2	7	1	2	2	31	.05	.051	21	20	.21	48	.01	2	1.03	.01	.05	1	1
CC1+50E 1+80N	1	29	30	72	.5	25	19	1511	3.39	7	5	ND	1	12	1	2	2	25	.13	.107	16	15	.21	42	.01	2	1.12	.01	.06	1	1
CC1+50E 1+70N	1	22	26	74	.4	25	14	2030	3.24	7	5	ND	2	10	1	2	2	25	.09	.074	19	18	.28	59	.01	2	1.11	.01	.05	1	1
CC1+50E 1+60N	1	15	20	55	.5	15	7	650	3.17	9	5	ND	2	7	1	2	2	28	.04	.051	24	18	.20	40	.01	2	1.01	.01	.05	1	1
CC1+50E 1+50N	1	39	27	93	.3	46	15	432	4.55	20	5	ND	7	9	1	2	2	18	.08	.043	31	22	.44	30	.02	2	1.17	.01	.04	7	37
CC1+50E 1+40N	1	18	19	63	.3	20	6	170	4.13	12	5	ND	2	7	1	2	2	22	.08	.053	21	19	.26	31	.01	2	.98	.01	.05	1	8
CC1+50E 1+30N	1	14	21	55	.5	17	6	284	3.27	13	5	ND	2	8	1	2	2	24	.06	.050	26	16	.21	47	.01	6	.82	.01	.04	2	7
CC1+50E 1+20N	1	11	17	41	.4	11	3	105	2.67	10	5	ND	2	7	1	2	2	22	.05	.050	25	12	.13	39	.01	6	.80	.01	.04	2	10
CC1+50E 1+10N	2	22	24	71	.4	25	7	234	5.12	10	5	ND	3	5	1	2	2	27	.02	.058	23	34	.38	33	.01	2	1.32	.01	.04	1	1
CC1+50E 1+00N	1	15	19	41	.6	13	4	111	4.15	14	5	ND	2	5	1	2	3	27	.02	.074	22	19	.16	31	.01	2	.93	.01	.04	2	4
CC1+50E 0+90N	1	20	23	86	.4	23	8	390	3.22	10	5	ND	3	7	1	2	2	24	.05	.064	25	24	.30	42	.01	2	.98	.01	.05	1	12
CC1+50E 0+80N	1	19	28	65	.3	18	6	281	4.30	11	5	ND	2	8	1	2	2	27	.08	.095	18	22	.24	43	.01	2	1.02	.01	.05	1	1
CC1+50E 0+70N	1	36	25	88	.2	40	16	504	4.98	25	5	ND	6	6	1	2	2	18	.03	.044	30	23	.47	35	.02	4	1.28	.01	.05	2	16
CC1+50E 0+60N	1	21	25	73	.5	25	8	304	3.72	12	5	ND	3	6	1	2	2	22	.03	.067	25	27	.35	37	.01	6	1.15	.01	.05	1	1
CC1+50E 0+50N	1	29	37	129	.4	34	11	517	4.62	11	5	ND	3	7	1	2	2	27	.05	.067	27	36	.41	47	.01	2	1.46	.01	.06	1	7
CC1+50E 0+40N	2	38	47	180	.6	38	13	1358	4.43	10	5	ND	3	13	1	2	2	24	.16	.110	25	34	.49	177	.01	2	1.49	.02	.07	1	6
CC1+50E 0+30N	1	27	33	112	.4	33	11	643	3.69	8	5	ND	3	15	1	2	2	23	.16	.071	26	29	.42	74	.01	2	1.11	.01	.06	1	1
CC1+50E 0+20N	1	22	33	91	.6	29	9	807	3.70	8	5	ND	2	11	1	2	2	22	.12	.089	22	29	.41	64	.01	3	1.07	.01	.07	1	4
CC1+50E 0+10N	1	20	34	71	.3	24	6	321	3.14	11	5	ND	2	9	1	2	2	19	.08	.082	22	25	.32	48	.01	5	.93	.01	.05	2	23
CC1+50E 0+00N	2	26	38	92	1.0	30	8	315	3.98	15	5	ND	3	9	1	2	2	19	.09	.094	21	26	.35	42	.01	7	1.08	.01	.06	1	7
STD C/AU-S	18	57	41	131	7.1	67	27	1026	3.98	36	23	8	38	49	18	15	19	55	.48	.087	37	57	.88	173	.08	31	1.82	.08	.13	12	51

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: P1-S SOIL P9-ROCK AU: ANALYSIS BY AA FROM 10 GRAM SAMPLE.

EXTRA CD

DATE RECEIVED: SEPT 15 1987 DATE REPORT MAILED: *Sept 29/87* ASSAYER: *D. Toyer* DEAN TOYE. CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-4221 Page 1

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUR
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
CC 5+25E 2+00N	2	27	12	65	.1	26	11	342	4.45	5	5	ND	1	6	1	2	2	27	.03	.051	21	21	.19	44	.01	3	1.03	.01	.05	1	1
CC 5+25E 1+90N	2	21	11	58	.1	23	11	326	3.59	2	5	ND	3	8	1	2	2	19	.07	.056	22	14	.13	44	.01	2	.93	.01	.05	2	1
CC 5+25E 1+80N	2	37	10	70	.6	27	14	421	4.69	7	5	ND	3	8	1	2	2	22	.07	.071	19	14	.11	51	.01	5	.85	.01	.06	1	1
STD C/AU-S	19	58	41	135	7.1	66	29	997	3.85	37	17	7	38	50	18	18	22	56	.48	.084	38	59	.85	174	.06	37	1.87	.06	.13	14	49
CC 5+25E 1+70N	2	31	14	84	.1	24	14	1278	4.80	6	5	ND	1	7	1	3	2	28	.06	.090	18	15	.20	83	.01	4	.89	.01	.06	1	1
CC 5+25E 1+60N	2	26	17	83	.1	24	10	400	4.02	9	5	ND	2	7	1	2	2	20	.01	.066	30	18	.19	48	.01	4	1.10	.01	.04	1	1
CC 5+25E 1+50N	2	28	22	79	.3	29	11	240	3.52	54	5	ND	4	16	1	3	2	14	.06	.062	23	10	.08	50	.01	11	.70	.01	.06	1	120
CC 5+25E 1+40N	2	18	23	83	.5	20	13	1658	2.79	31	5	ND	2	15	1	3	2	12	.16	.097	14	7	.06	101	.01	3	.54	.01	.08	1	39
CC 5+25E 1+30N	2	17	23	98	.2	22	17	2178	3.64	15	5	ND	1	11	1	2	2	15	.08	.099	16	11	.11	112	.01	5	.72	.03	.07	1	1
CC 5+25E 1+20N	2	25	15	47	.1	18	8	640	2.75	13	5	ND	1	7	1	2	2	15	.03	.059	21	11	.06	41	.01	2	.55	.01	.06	2	54
CC 5+25E 1+10N	2	33	10	79	.2	31	17	2646	2.97	4	5	ND	2	7	1	2	2	7	.08	.078	12	11	.07	120	.01	2	.47	.01	.06	1	1
CC 5+25E 1+00N	1	15	13	58	.2	19	7	183	2.21	19	5	ND	1	6	1	3	2	11	.05	.063	16	7	.04	42	.01	5	.55	.01	.05	1	26
CC 5+25E 0+90N	1	17	24	87	.4	23	13	892	3.57	18	5	ND	2	10	1	2	2	14	.17	.087	11	18	.27	77	.02	4	.91	.01	.06	1	1
CC 5+25E 0+80N	2	35	16	98	.1	40	21	708	4.60	20	5	ND	8	9	1	2	3	14	.08	.069	18	30	.86	51	.01	2	1.81	.01	.05	1	5
CC 5+25E 0+70N	1	20	11	72	.1	43	13	410	4.47	42	5	ND	5	7	1	2	3	22	.04	.055	25	49	.52	39	.01	9	1.36	.01	.05	1	27
CC 5+25E 0+60N	1	12	13	53	.1	23	8	127	3.08	29	5	ND	8	5	1	2	2	15	.04	.035	36	14	.15	39	.01	2	.82	.01	.05	1	310
CC 5+25E 0+50N	2	15	11	67	.1	25	8	172	3.80	25	5	ND	5	5	1	2	2	23	.03	.033	30	20	.22	42	.01	4	1.04	.01	.04	1	5
CC 5+25E 0+40N	2	14	12	70	.1	21	7	202	3.92	17	5	ND	5	11	1	3	2	27	.14	.038	29	20	.20	78	.01	4	.92	.02	.05	1	1
CC 5+25E 0+30N	2	14	8	47	.1	18	7	131	3.34	17	5	ND	9	4	1	2	2	26	.01	.023	30	16	.14	51	.01	6	.90	.01	.04	1	1
CC 5+25E 0+20N	2	18	15	78	.2	28	10	192	4.79	12	5	ND	6	11	1	3	2	25	.14	.033	21	21	.19	45	.01	5	.92	.01	.04	1	2
CC 5+25E 0+10N	2	21	19	60	.1	31	9	163	3.38	12	5	ND	1	7	1	2	2	20	.07	.041	22	9	.05	40	.01	7	.51	.01	.04	1	1
CC 5+25E 0+00N	2	29	79	116	.1	40	21	1815	4.69	24	5	ND	3	18	1	2	2	20	.23	.062	21	20	.29	67	.01	5	1.35	.01	.06	5	15
CC 5+25E 0+10S	1	17	43	88	.1	23	8	276	2.85	30	5	ND	3	6	1	3	2	17	.02	.036	33	9	.04	46	.01	2	.57	.01	.04	1	42
CC 5+25E 0+20S	1	23	33	71	.1	27	8	216	2.63	10	5	ND	2	9	1	2	2	13	.09	.044	27	7	.05	35	.01	6	.42	.01	.06	1	3
CC 5+25E 0+30S	2	46	652	360	2.0	55	13	1052	3.79	20	7	ND	2	31	4	3	2	10	.55	.120	15	17	.26	39	.01	4	1.32	.01	.05	1	28
CC 5+25E 0+40S	2	31	197	268	.8	30	16	1071	4.31	37	5	ND	1	8	2	2	2	19	.04	.078	21	17	.15	42	.01	2	1.00	.01	.05	2	70
CC 5+25E 0+50S	2	16	27	67	.1	21	7	355	2.73	23	5	ND	1	6	1	2	2	19	.03	.049	27	9	.04	43	.01	2	.51	.01	.04	1	24
CC 5+25E 0+60S	2	26	41	97	.3	29	14	761	4.29	30	5	ND	3	6	1	2	2	19	.04	.061	29	19	.17	45	.01	3	1.00	.01	.05	2	8
CC 5+25E 0+70S	2	20	25	74	.2	25	10	305	3.83	25	5	ND	2	6	1	2	2	21	.02	.053	32	17	.20	43	.01	4	1.04	.01	.04	1	21
CC 5+25E 0+80S	2	24	33	84	.1	27	12	730	4.05	29	5	ND	1	7	1	2	2	22	.05	.062	23	17	.16	59	.01	2	.94	.01	.05	1	4
CC 5+25E 0+90S	2	35	19	99	.3	45	32	1819	4.73	34	5	ND	2	12	1	4	2	15	.17	.102	15	27	.28	101	.01	2	1.33	.01	.05	1	1
CC 5+25E 1+00S	2	28	37	110	.3	31	20	1801	3.88	19	5	ND	2	52	1	2	2	19	.85	.096	13	25	.37	110	.01	6	1.41	.01	.06	1	13
CC 5+25E 1+10S	3	35	33	114	.2	56	19	316	5.77	27	5	ND	4	10	1	2	2	25	.12	.061	17	46	.54	61	.01	3	1.96	.01	.04	1	1
CC 5+25E 1+20S	2	33	38	125	.2	37	15	1142	4.97	15	5	ND	3	40	1	2	2	19	.82	.168	18	23	.29	207	.01	2	1.34	.01	.06	1	2
CC 5+25E 1+30S	2	25	46	137	.3	36	20	1091	4.66	15	5	ND	5	17	1	2	2	22	.28	.050	22	25	.44	54	.01	2	1.48	.01	.06	3	13
CC 5+25E 1+40S	2	20	28	74	.3	28	12	525	3.72	18	5	ND	2	8	1	3	2	22	.09	.054	22	14	.10	39	.01	2	.72	.01	.05	1	1
CC 5+25E 1+50S	2	27	13	69	.1	26	10	287	4.04	23	5	ND	1	5	1	2	2	28	.04	.048	23	14	.07	40	.01	2	.69	.01	.03	1	68

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUR
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	PPM	PPM	
CC 5+50E 2+00N	2	26	10	68	.3	25	12	435	4.71	2	5	ND	2	5	1	2	2	24	.03	.044	18	23	.28	38	.01	2	1.38	.01	.02	1	1
CC 5+50E 1+90N	1	24	13	59	.1	21	8	286	3.82	2	5	ND	1	4	1	2	2	20	.03	.053	19	18	.22	41	.01	2	.98	.01	.03	1	1
CC 5+50E 1+80N	2	31	16	67	.1	23	10	245	4.86	2	5	ND	3	6	1	3	2	20	.03	.040	22	18	.20	40	.01	2	1.16	.01	.03	1	1
CC 5+50E 1+70N	2	31	23	104	.3	33	22	1896	4.50	4	5	ND	2	28	1	2	2	16	.38	.083	19	15	.20	82	.01	2	1.22	.01	.06	1	1
CC 5+50E 1+60N	2	24	23	84	.4	24	12	742	3.90	5	5	ND	3	8	1	2	2	20	.04	.045	24	17	.15	108	.01	2	.91	.01	.05	1	1
CC 5+50E 1+50N	2	23	20	57	.3	20	8	156	3.25	2	5	ND	5	5	1	2	2	19	.01	.035	22	12	.10	44	.01	2	.76	.01	.04	1	1
CC 5+50E 1+40N	2	28	16	64	.1	23	9	580	3.23	22	5	ND	1	7	1	2	2	17	.07	.056	19	12	.10	58	.01	2	.71	.01	.03	1	1
CC 5+50E 1+30N	1	25	12	56	.1	21	8	341	2.92	23	5	ND	1	3	1	2	2	12	.01	.048	18	10	.08	42	.01	2	.66	.01	.03	1	1
CC 5+50E 1+20N	1	16	18	56	.3	18	6	475	2.64	9	5	ND	1	5	1	3	2	15	.03	.067	16	13	.09	48	.01	2	.72	.01	.04	1	1
CC 5+50E 1+10N	1	20	17	72	.1	21	10	1114	3.02	4	5	ND	1	6	1	3	2	13	.06	.071	17	14	.13	60	.01	2	.69	.01	.05	1	1
CC 5+50E 1+00N	2	20	19	74	.5	23	9	612	3.27	5	5	ND	1	6	1	2	2	13	.05	.071	16	14	.14	75	.01	2	.71	.01	.04	1	1
CC 5+50E 0+90N	1	17	30	75	.3	18	7	2595	2.23	18	5	ND	1	9	1	2	2	8	.13	.077	15	6	.06	109	.01	2	.38	.01	.06	1	9
CC 5+50E 0+80N	1	21	13	80	.5	25	11	666	4.37	18	5	ND	3	5	1	3	3	15	.04	.098	21	23	.37	42	.01	2	1.17	.01	.05	1	1
CC 5+50E 0+70N	1	13	11	69	.4	21	9	962	2.73	29	5	ND	3	9	1	2	2	12	.22	.094	17	20	.16	63	.01	2	.65	.01	.07	1	1
CC 5+50E 0+60N	1	15	19	69	.1	28	7	266	4.41	33	5	ND	2	3	1	2	3	19	.01	.054	26	32	.33	30	.01	4	1.24	.01	.03	1	136
CC 5+50E 0+50N	1	15	15	49	.1	14	5	137	2.66	100	5	ND	2	6	1	2	2	15	.07	.053	21	10	.09	37	.01	2	.70	.01	.03	1	45
CC 5+50E 0+40N	2	13	9	56	.1	23	6	128	3.83	25	5	ND	4	4	1	2	2	37	.01	.036	26	34	.34	25	.01	2	1.34	.01	.03	1	4
CC 5+50E 0+30N	2	32	16	83	.1	30	11	226	8.95	33	5	ND	4	4	1	2	2	27	.01	.058	24	35	.26	33	.01	2	1.55	.01	.03	1	1
CC 5+50E 0+20N	2	19	13	67	.1	22	8	162	4.14	16	5	ND	7	5	1	2	2	25	.02	.031	30	14	.13	30	.01	2	.69	.01	.04	1	4
CC 5+50E 0+10N	1	20	10	48	.4	19	6	118	2.55	11	5	ND	1	6	1	2	2	25	.08	.041	24	10	.03	34	.01	5	.48	.01	.03	2	5
CC 5+50E 0+00N	2	27	10	78	.1	30	10	228	5.19	14	5	ND	5	5	1	2	2	22	.03	.042	25	19	.20	32	.01	2	1.03	.01	.05	1	1
CC 5+75E 2+00N	2	23	13	50	.5	24	8	171	3.66	4	5	ND	3	4	1	3	2	26	.01	.041	27	17	.11	42	.01	2	.90	.01	.03	2	1
CC 5+75E 1+90N	2	25	10	53	.1	18	7	216	4.02	2	5	ND	1	5	1	2	2	24	.02	.047	28	17	.15	31	.01	2	.97	.01	.03	1	1
CC 5+75E 1+80N	2	43	10	61	.1	33	12	242	4.56	2	5	ND	3	9	1	2	2	17	.04	.036	27	14	.10	28	.01	2	.78	.01	.04	1	1
CC 5+75E 1+70N	1	29	12	66	.1	22	8	173	3.74	8	5	ND	3	11	1	2	2	19	.03	.044	22	14	.08	37	.01	3	.81	.01	.04	1	1
CC 5+75E 1+60N	1	32	30	108	.9	30	13	1727	3.78	8	5	ND	4	54	1	2	2	12	.97	.116	13	15	.27	74	.01	2	1.07	.01	.05	1	1
CC 5+75E 1+50N	2	31	32	116	.1	30	16	966	4.75	7	5	ND	1	13	1	2	2	20	.05	.073	21	18	.16	65	.01	2	1.08	.01	.05	1	1
CC 5+75E 1+40N	2	17	13	56	.5	17	6	198	2.93	3	5	ND	2	9	1	2	2	16	.04	.051	18	11	.07	52	.01	2	.69	.01	.06	1	1
CC 5+75E 1+30N	2	14	13	52	.3	14	5	451	2.09	35	5	ND	1	7	1	2	2	19	.02	.039	27	11	.06	73	.01	3	.65	.01	.04	2	34
CC 5+75E 1+20N	1	15	11	65	.1	19	6	367	2.43	5	5	ND	1	8	1	2	2	9	.09	.046	24	6	.04	41	.01	2	.43	.01	.03	1	1
CC 5+75E 1+10N	1	36	23	72	.1	29	11	436	4.34	3	5	ND	2	5	1	2	2	10	.04	.081	17	18	.26	31	.01	2	1.01	.01	.04	1	1
CC 5+75E 1+00N	2	37	13	75	.3	23	10	317	3.89	3	5	ND	6	4	1	2	2	10	.01	.075	16	15	.30	50	.01	3	1.04	.01	.05	1	1
CC 5+75E 0+90N	1	25	8	65	.3	17	8	373	3.18	2	5	ND	3	5	1	2	2	9	.03	.085	16	17	.30	49	.01	2	1.04	.01	.04	1	1
CC 5+75E 0+80N	1	19	13	87	.1	22	8	509	3.59	2	5	ND	3	10	1	2	2	12	.09	.099	15	19	.27	89	.01	2	.92	.01	.05	1	1
CC 5+75E 0+70N	1	15	16	62	.1	24	9	405	3.31	34	5	ND	2	5	1	2	2	17	.01	.075	25	22	.20	60	.01	4	.81	.01	.06	1	19
CC 5+75E 0+60N	1	24	16	59	.1	24	13	889	3.14	29	5	ND	3	5	1	5	2	10	.01	.083	23	13	.14	70	.01	4	.74	.01	.04	1	26
STD C/AU-S	10	58	35	132	6.8	67	27	943	4.06	37	16	7	36	49	17	18	20	56	.46	.081	36	57	.83	173	.06	32	1.80	.06	.12	12	48



SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	B1	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUX
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
CC 5+75E 0+50N	1	33	26	74	.2	30	13	201	4.06	8	9	ND	6	4	1	3	2	9	.02	.045	35	10	.12	29	.01	2	.70	.01	.04	1	2
CC 5+75E 0+40N	1	13	11	44	.1	16	5	70	1.65	2	5	ND	1	8	1	2	2	14	.09	.052	28	9	.04	50	.01	3	.67	.01	.03	1	13
CC 5+75E 0+30N	1	11	9	43	.1	16	5	82	2.32	17	5	ND	1	6	1	2	2	26	.04	.034	26	12	.07	49	.01	4	.93	.01	.02	1	7
CC 5+75E 0+20N	2	25	25	112	.1	30	11	196	4.73	30	5	ND	7	7	1	2	2	25	.04	.030	29	24	.22	51	.01	4	1.33	.01	.03	1	2
CC 5+75E 0+10N	2	24	15	58	.1	24	8	149	3.99	23	5	ND	1	4	1	2	2	24	.01	.033	30	12	.06	37	.01	7	.76	.01	.02	1	86
CC 5+75E 0+00N	2	24	22	70	.1	24	9	161	4.37	14	5	ND	2	5	1	2	2	22	.03	.042	27	16	.12	34	.01	4	.95	.01	.02	1	11
CC 6+00E 1+00N	2	20	20	65	.1	22	10	637	3.10	5	5	ND	1	9	1	2	2	13	.07	.081	12	14	.14	50	.01	4	.90	.01	.06	1	1
CC 6+00E 0+90N	2	23	21	74	.3	22	10	365	2.82	14	5	ND	2	8	1	2	2	9	.03	.056	17	10	.08	64	.01	2	.75	.01	.05	1	1
CC 6+00E 0+80N	2	22	29	65	.2	21	11	501	2.91	6	8	ND	5	8	1	2	2	8	.03	.054	16	9	.09	36	.01	3	.74	.01	.05	1	2
CC 6+00E 0+70N	2	28	28	146	.5	31	14	1714	2.80	14	9	ND	4	32	1	2	2	6	.63	.063	14	6	.08	147	.01	2	.56	.02	.05	1	10
CC 6+00E 0+60N	1	14	16	58	.1	17	12	850	2.65	10	5	ND	1	7	1	2	2	7	.05	.082	21	6	.07	73	.01	3	.49	.03	.04	1	6
CC 6+00E 0+50N	1	26	12	75	.1	24	11	543	3.05	13	5	ND	2	8	1	2	2	8	.12	.094	17	13	.25	52	.01	4	.79	.03	.05	1	1
CC 6+00E 0+40N	1	37	33	104	.1	41	22	1011	4.30	26	5	ND	5	13	1	2	5	9	.21	.089	15	20	.46	47	.01	2	1.21	.04	.04	1	10
CC 6+00E 0+30N	1	54	39	111	.1	53	25	631	4.09	31	5	ND	3	4	1	3	2	4	.02	.038	32	5	.04	31	.01	2	.47	.02	.03	1	70
CC 6+00E 0+20N	1	48	21	96	.1	51	23	532	4.07	8	5	ND	9	9	1	2	4	9	.16	.044	27	23	.52	34	.01	5	1.29	.02	.06	1	5
CC 6+00E 0+10N	1	30	20	77	.1	38	17	302	4.74	33	5	ND	6	8	1	2	2	17	.12	.063	20	22	.25	41	.01	2	2.17	.03	.05	1	13
CC 6+00E 0+00N	2	26	19	105	.2	30	12	447	4.48	12	5	ND	5	7	1	2	2	20	.03	.040	25	20	.24	60	.01	2	1.29	.06	.04	1	2
CCA 1+00E 1+00S	3	44	71	223	.5	58	18	575	4.69	42	5	ND	2	33	1	2	3	28	.45	.100	24	52	.59	228	.01	2	1.47	.01	.08	3	12
CCA 1+00E 1+10S	3	49	47	166	.1	64	20	650	4.49	43	5	ND	4	25	1	2	2	24	.29	.098	37	40	.48	194	.02	6	1.02	.01	.04	1	17
CCA 1+00E 1+20S	2	51	397	218	.3	54	19	715	4.61	50	5	ND	4	19	1	2	3	21	.26	.085	33	31	.45	144	.02	2	.97	.01	.04	4	159
CCA 1+00E 1+30S	2	58	262	205	.3	36	19	831	5.15	32	5	ND	8	12	2	4	4	18	.14	.062	32	17	.40	52	.01	6	1.04	.01	.04	5	19
CCA 1+00E 1+40S	2	42	664	487	.7	29	15	645	4.57	27	5	ND	1	14	4	3	2	19	.16	.059	22	19	.36	72	.01	2	1.09	.01	.05	2	34
CCA 1+00E 1+50S	1	44	168	91	.5	18	10	427	5.19	17	5	ND	2	7	1	2	3	23	.06	.082	21	17	.28	56	.01	2	1.31	.01	.03	2	16
CCA 1+00E 1+60S	2	38	59	86	.3	16	10	646	4.77	10	5	ND	1	5	1	2	2	26	.04	.072	21	16	.27	46	.01	2	1.14	.01	.04	1	3
CCA 1+00E 1+70S	1	75	94	115	.3	22	16	940	5.50	11	5	ND	2	8	1	2	2	23	.08	.085	33	17	.29	48	.01	2	1.47	.01	.03	1	5
CCA 1+00E 1+80S	1	29	43	75	.1	15	8	505	4.14	8	5	ND	1	6	1	2	2	24	.06	.077	19	15	.25	51	.01	2	.95	.01	.02	1	3
CCA 1+00E 1+90S	2	28	59	79	1.3	14	11	747	5.46	13	5	ND	2	6	1	3	4	27	.06	.140	20	15	.23	37	.01	2	.89	.01	.04	2	4
CCA 1+00E 2+00S	1	39	57	75	.9	13	9	1219	4.09	9	5	ND	1	7	1	2	2	26	.04	.073	26	15	.19	67	.01	6	1.09	.01	.02	1	7
CCA 1+00E 2+10S	1	27	32	75	.4	10	8	481	3.58	8	5	ND	1	16	1	2	2	25	.19	.118	16	11	.19	44	.01	2	.70	.01	.04	1	31
CCA 1+00E 2+20S	1	34	107	94	.5	18	13	697	5.61	13	5	ND	1	12	1	3	2	19	.16	.102	19	15	.27	50	.01	3	.98	.01	.03	1	1
CCA 1+00E 2+30S	2	36	98	85	.5	13	12	1984	4.98	13	5	ND	1	6	1	2	2	22	.03	.099	23	15	.23	71	.01	3	.98	.01	.03	1	1
CCA 1+00E 2+40S	2	45	87	85	.7	16	13	735	5.04	11	5	ND	2	6	1	2	2	21	.06	.103	24	16	.27	28	.01	3	1.23	.01	.03	1	4
CCA 1+00E 2+50S	1	14	17	31	.2	7	4	182	1.94	3	5	ND	1	5	1	2	2	17	.01	.085	22	9	.13	32	.01	3	.57	.01	.02	1	4
CCA 1+00E 2+60S	1	34	35	63	1.2	12	8	462	4.56	10	5	ND	2	4	1	3	2	26	.01	.082	20	14	.23	38	.01	3	.89	.01	.03	1	12
CCA 1+00E 2+70S	1	18	18	39	.8	7	5	168	3.08	6	5	ND	1	4	1	2	2	21	.01	.075	22	13	.20	35	.01	5	.83	.01	.02	1	4
CCA 1+00E 2+80S	1	32	32	63	.3	16	8	328	3.90	11	5	ND	1	4	1	2	2	21	.01	.080	22	14	.26	33	.01	2	.97	.01	.03	1	1
STD C/AU-S	18	57	38	131	6.8	63	27	929	3.70	34	25	7	36	48	17	17	20	55	.46	.080	36	55	.83	175	.06	32	1.89	.06	.12	13	51

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUX
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPB
CCA 1+00E 2+90S	2	48	49	92	.6	19	15	914	6.30	11	5	ND	1	7	1	2	2	25	.07	.114	25	15	.32	34	.01	4	1.14	.01	.04	1	36
CCA 1+00E 3+00S	2	67	92	101	.2	26	18	857	6.66	14	5	ND	3	8	1	2	2	21	.12	.077	24	15	.35	56	.01	4	1.11	.01	.03	1	5
CCA 1+00E 3+10S	2	27	48	60	.6	9	8	1099	4.74	8	5	ND	1	9	1	2	2	30	.07	.074	20	12	.12	59	.01	2	.80	.01	.03	1	4
CCA 1+00E 3+20S	2	55	94	90	.4	22	18	823	7.18	11	5	ND	2	6	1	2	2	25	.04	.073	22	15	.28	47	.01	4	1.24	.01	.03	1	3
CCA 1+00E 3+30S	2	78	83	111	.1	30	21	1591	7.66	18	5	ND	1	6	1	3	2	23	.03	.103	25	19	.28	63	.01	11	1.26	.01	.03	2	1
CCA 1+00E 3+40S	3	47	54	113	1.5	19	16	7949	5.01	11	5	ND	1	9	1	2	3	29	.09	.115	21	14	.20	200	.01	2	.90	.01	.04	1	1
CCA 1+00E 3+50S	2	52	58	77	1.0	17	16	2851	5.61	11	5	ND	1	9	1	3	2	32	.12	.108	21	14	.29	79	.01	2	1.15	.01	.06	1	26
CCA 1+00E 3+60S	2	30	31	60	.2	12	10	1051	5.07	10	5	ND	1	7	1	3	2	32	.06	.101	25	12	.20	62	.01	2	.81	.01	.04	1	3
CCA 1+00E 3+70S	2	37	34	58	.6	13	12	1516	5.14	11	5	ND	1	5	1	2	2	33	.02	.086	23	12	.25	51	.01	3	.91	.01	.03	1	1
CCA 1+00E 3+80S	2	50	35	72	.3	15	14	1049	5.79	10	5	ND	1	5	1	2	2	32	.02	.126	19	13	.22	42	.01	3	.89	.01	.03	1	1
CCA 1+00E 3+90S	2	91	53	112	.1	23	25	1456	8.97	13	5	ND	3	6	1	2	2	37	.04	.127	27	18	.38	51	.01	3	1.79	.01	.04	1	6
CCA 1+00E 4+00S	2	40	33	60	.5	12	10	462	5.77	10	5	ND	1	6	1	2	2	31	.02	.091	25	13	.17	27	.01	2	.78	.01	.03	1	1
CCA 1+50E 1+20S	2	63	1125	234	1.1	44	25	593	6.43	140	5	ND	6	16	1	3	2	18	.20	.082	28	17	.39	86	.01	11	.67	.01	.02	303	1920
CCA 1+50E 1+30S	2	61	1150	261	.5	38	18	806	5.15	44	5	ND	7	16	2	2	2	15	.21	.065	30	12	.31	48	.01	10	.75	.01	.03	12	145
CCA 1+50E 1+40S	2	77	94	119	.1	40	28	618	6.09	27	5	ND	7	19	1	2	2	22	.25	.086	41	12	.52	51	.01	6	1.13	.01	.01	4	73
CCA 1+50E 1+50S	3	47	101	111	.4	33	15	672	10.05	39	5	ND	1	5	1	4	5	42	.04	.110	19	38	.33	45	.01	6	1.14	.01	.03	2	2
CCA 1+50E 1+60S	2	28	42	63	.3	14	8	273	4.98	14	5	ND	2	5	1	2	2	29	.02	.069	27	15	.28	34	.01	5	1.08	.01	.04	6	305
CCA 1+50E 1+70S	2	23	36	68	.1	13	9	839	4.10	9	5	ND	1	6	1	2	2	31	.03	.073	20	20	.18	52	.01	2	.77	.01	.03	14	14
CCA 1+50E 1+80S	2	53	59	142	.7	12	17	2438	8.88	18	5	ND	1	11	1	2	2	36	.12	.151	14	14	.16	153	.01	2	1.09	.01	.02	1	2
STD C/AU-S	20	61	41	128	7.2	70	30	998	3.93	39	20	8	40	50	18	17	18	59	.49	.088	38	58	.89	175	.06	34	1.91	.06	.13	13	51
CCA 1+50E 1+90S	2	35	34	79	1.0	12	13	1091	4.94	9	5	ND	1	6	1	2	2	33	.02	.102	20	13	.27	52	.01	2	1.09	.01	.03	1	34
CCA 1+50E 2+00S	1	15	22	43	.3	8	6	286	3.05	6	5	ND	1	5	1	2	2	29	.02	.063	24	11	.28	35	.01	5	1.04	.01	.03	3	4
CCA 1+50E 2+10S	2	37	46	88	.3	16	14	871	7.12	10	5	ND	1	6	1	2	5	38	.04	.098	20	17	.33	37	.01	2	1.38	.01	.03	1	98
CCA 1+50E 2+20S	2	35	73	111	.4	17	18	2118	6.94	12	7	ND	1	12	1	2	2	33	.21	.123	19	17	.22	64	.01	6	1.04	.01	.05	4	30
CCA 1+50E 2+30S	2	58	86	121	.8	23	17	1092	7.99	13	5	ND	1	8	1	2	2	26	.10	.100	22	17	.28	80	.01	6	1.38	.01	.03	3	14
CCA 1+50E 2+40S	1	15	17	32	.1	9	5	241	2.55	6	5	ND	1	5	1	2	2	22	.01	.045	28	11	.13	43	.01	5	.61	.01	.03	1	25
CCA 1+50E 2+50S	1	19	32	52	.6	9	8	1095	4.08	10	5	ND	1	6	1	2	2	30	.03	.124	22	10	.17	46	.01	3	.76	.01	.03	1	7
CCA 1+50E 2+60S	2	34	39	74	.4	18	12	1410	5.34	9	5	ND	1	5	1	2	2	27	.03	.117	19	18	.27	36	.01	2	1.32	.01	.04	1	3
CCA 1+50E 2+70S	2	38	80	98	.8	18	14	1443	6.29	14	5	ND	1	7	1	2	2	28	.05	.137	21	19	.23	40	.01	5	1.52	.01	.04	8	2
CCA 1+50E 2+80S	2	24	73	64	.9	11	9	621	4.55	12	5	ND	1	5	1	2	2	26	.01	.113	20	11	.18	33	.01	2	.83	.01	.03	1	142
CCA 1+50E 2+90S	2	39	49	64	.5	10	11	2036	4.78	7	5	ND	1	6	1	2	2	33	.01	.109	21	14	.14	71	.01	3	1.25	.01	.04	1	8
CCA 1+50E 3+00S	2	44	58	88	.7	15	12	975	5.03	9	6	ND	2	6	1	2	2	24	.02	.119	23	13	.28	46	.01	7	1.14	.01	.05	1	16
CCA 1+50E 3+10S	2	46	46	92	.1	17	13	1467	5.75	18	5	ND	1	8	1	2	2	33	.04	.120	21	15	.34	114	.01	4	1.28	.01	.04	3	5
CCA 1+50E 3+20S	1	29	27	106	.3	14	9	1100	4.37	13	5	ND	1	18	1	2	2	29	.23	.119	20	12	.21	117	.01	2	.86	.01	.04	1	134
CCA 1+50E 3+30S	2	41	45	77	.3	19	13	812	5.21	15	5	ND	1	7	1	2	2	27	.04	.118	22	15	.23	65	.01	7	1.07	.01	.04	1	4
CCA 1+50E 3+40S	2	39	48	91	.3	16	12	1470	5.63	15	5	ND	1	8	1	2	2	32	.07	.120	20	13	.19	87	.01	2	.86	.01	.04	1	3
CCA 1+50E 3+50S	2	43	57	76	.1	16	13	1040	6.26	14	5	ND	1	7	1	2	2	34	.06	.117	22	12	.23	50	.01	5	.90	.01	.05	1	5

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	X	M	AUX
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
CCA 1+50E 3+60S	1	28	79	55	.1	14	8	204	3.65	13	5	ND	2	5	1	2	2	18	.03	.084	22	11	.22	38	.01	2	.87	.01	.05	1	10
CCA 1+50E 3+70S	1	26	35	61	.2	11	8	465	5.18	14	5	ND	1	5	1	2	2	20	.01	.081	21	14	.17	42	.01	3	.87	.01	.04	1	1
CCA 1+50E 3+80S	1	29	39	59	.4	13	10	849	4.43	19	5	ND	1	4	1	5	2	26	.01	.069	23	17	.22	36	.01	2	1.03	.01	.04	1	1
CCA 1+50E 3+90S	2	40	54	70	.3	18	10	509	6.63	21	5	ND	1	6	1	2	2	22	.03	.078	21	22	.17	29	.01	2	.99	.01	.04	1	1
CCA 1+50E 4+00S	1	48	44	68	.1	19	13	627	5.86	29	5	ND	2	7	1	2	2	27	.01	.054	29	11	.18	29	.01	2	.78	.01	.03	1	1
CCA 2+00E 1+10S	3	48	74	165	.2	64	20	779	5.15	60	5	ND	2	13	1	2	3	26	.14	.075	33	44	.56	154	.01	7	1.49	.01	.06	1	39
CCA 2+00E 1+20S	2	56	74	153	.4	59	22	1279	5.15	57	5	ND	3	18	1	2	2	21	.28	.092	28	34	.50	209	.01	2	1.32	.01	.07	6	32
CCA 2+00E 1+30S	2	53	69	154	.3	55	19	978	4.90	55	5	ND	2	17	1	2	2	21	.23	.096	27	38	.50	197	.01	7	1.27	.01	.07	2	33
CCA 2+00E 1+40S	3	50	223	222	.2	49	20	589	4.84	38	5	ND	4	20	1	2	2	22	.26	.087	29	29	.52	117	.01	5	.97	.01	.04	25	185
CCA 2+00E 1+50S	4	50	199	186	.3	57	25	860	5.40	63	5	ND	4	24	1	3	2	21	.31	.102	23	34	.51	144	.01	5	.83	.01	.04	28	445
CCA 2+00E 1+60S	3	54	869	299	1.4	47	20	942	4.81	67	5	ND	5	18	2	2	2	18	.26	.078	28	20	.44	92	.01	2	.89	.01	.05	57	185
CCA 2+00E 1+70S	2	23	40	59	.3	14	7	328	3.81	23	5	ND	1	7	1	2	2	28	.06	.067	21	13	.12	48	.01	2	.63	.01	.03	12	28
CCA 2+00E 1+80S	1	13	20	41	.2	8	5	267	2.50	15	5	ND	1	5	1	2	2	22	.01	.067	28	11	.13	34	.01	4	.60	.01	.02	5	8
CCA 2+00E 1+90S	1	17	22	32	1.5	7	5	126	2.43	8	5	ND	1	5	1	2	2	22	.01	.061	24	12	.17	30	.01	4	.79	.01	.03	2	6
CCA 2+00E 2+00S	1	29	39	67	1.2	15	10	442	6.60	13	5	ND	2	4	1	2	2	35	.01	.088	21	21	.30	30	.01	2	1.24	.01	.04	2	7
CCA 2+00E 2+10S	1	48	59	83	.4	20	13	576	5.23	15	5	ND	2	5	1	2	2	27	.03	.169	19	16	.34	42	.01	2	1.12	.01	.04	2	96
CCA 2+00E 2+20S	1	38	39	131	1.4	17	15	1203	7.83	11	5	ND	1	10	1	2	2	38	.11	.195	16	20	.38	62	.01	2	1.76	.01	.04	1	5
CCA 2+00E 2+30S	1	63	40	97	.6	19	19	777	6.83	12	5	ND	5	6	1	2	3	56	.07	.136	17	18	.80	35	.01	2	2.24	.01	.03	1	23
CCA 2+00E 2+40S	1	26	30	52	.8	14	8	403	4.53	18	5	ND	1	3	1	2	2	17	.01	.064	24	11	.12	31	.01	2	.66	.01	.03	1	19
CCA 2+00E 2+50S	1	33	49	79	.5	16	11	485	5.27	16	5	ND	1	6	1	2	2	26	.03	.073	19	14	.15	30	.01	3	.86	.01	.03	1	25
CCA 2+00E 2+60S	1	40	58	81	.4	16	13	1500	5.49	13	5	ND	1	5	1	2	2	25	.03	.130	17	14	.23	45	.01	3	.97	.01	.04	28	73
CCA 2+00E 2+70S	1	20	27	41	.6	11	7	255	3.43	11	5	ND	1	4	1	2	2	27	.01	.125	18	11	.14	31	.01	2	.72	.01	.03	6	795
CCA 2+00E 2+80S	1	30	41	58	.5	14	11	1110	4.42	17	5	ND	1	5	1	2	2	25	.01	.094	21	14	.19	40	.01	8	1.04	.01	.04	3	11
CCA 2+00E 2+90S	1	25	44	52	.1	13	8	349	4.81	12	5	ND	1	4	1	2	2	25	.01	.126	23	15	.23	29	.01	2	.97	.01	.04	5	51
CCA 2+00E 3+00S	1	13	34	31	.7	9	3	153	2.51	6	5	ND	1	5	1	2	2	22	.02	.124	22	10	.09	33	.01	2	.57	.01	.04	4	1
CCA 2+00E 3+10S	1	36	28	87	.8	29	13	362	5.47	8	5	ND	4	4	1	2	2	18	.01	.092	24	24	.52	31	.01	3	1.52	.01	.04	1	3
CCA 2+00E 3+20S	1	69	76	98	.3	28	19	961	6.43	17	5	ND	5	5	1	2	2	25	.02	.082	27	17	.36	40	.01	2	1.34	.01	.04	1	2
CCA 2+00E 3+30S	1	52	94	110	.7	19	15	1694	6.33	21	5	ND	1	5	1	2	2	32	.01	.141	24	16	.32	53	.01	3	1.12	.01	.03	3	5
CCA 2+00E 3+40S	1	27	38	51	.2	10	8	505	3.54	8	5	ND	1	6	1	2	2	25	.03	.107	20	11	.20	37	.01	2	.75	.01	.05	3	1
CCA 2+00E 3+50S	1	27	32	50	.1	15	8	359	4.32	13	5	ND	1	6	1	2	2	25	.03	.152	21	11	.15	39	.01	2	.68	.01	.03	3	1
CCA 2+00E 3+60S	2	62	48	75	1.8	21	16	1983	5.65	16	5	ND	2	5	1	2	2	25	.01	.089	29	13	.30	64	.01	2	1.15	.01	.04	1	3
CCA 2+00E 3+70S	1	22	30	46	.1	11	7	750	3.06	8	5	ND	1	5	1	2	2	27	.01	.077	21	10	.15	39	.01	2	.68	.01	.03	2	21
CCA 2+00E 3+80S	1	62	63	93	.4	24	18	789	7.34	16	5	ND	3	5	1	2	2	27	.01	.089	22	19	.36	46	.01	7	1.26	.01	.04	1	10
CCA 2+00E 3+90S	1	30	44	64	.3	14	10	884	4.34	14	5	ND	1	6	1	2	2	28	.01	.105	23	12	.18	36	.01	4	.79	.01	.04	1	1
CCA 2+00E 4+00S	1	54	52	83	.2	23	14	491	6.50	13	5	ND	3	8	1	2	2	27	.08	.186	22	16	.39	37	.01	2	1.19	.01	.06	2	6
CCA 2+50E 1+60S	3	32	199	225	.4	46	16	1023	4.65	34	5	ND	2	50	1	2	2	25	.79	.115	22	39	.61	181	.01	2	1.10	.01	.05	6	24
STD C/AU-S	19	60	41	131	7.3	67	28	1020	3.71	38	18	8	38	52	18	17	20	57	.46	.088	38	59	.91	177	.06	37	1.87	.06	.13	13	53

SAMPLE#	ND	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	NG	BA	TI	B	AL	MA	K	M	AUX
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPM	
CCA 2+50E 1+70S	2	66	54	145	.2	70	22	898	5.35	29	5	ND	13	8	1	3	8	23	.10	.070	37	38	.62	70	.01	3	1.45	.01	.06	2	22
CCA 2+50E 1+80S	3	34	44	93	.5	30	12	398	7.30	33	5	ND	6	5	1	2	2	26	.03	.075	26	34	.37	44	.01	4	1.48	.01	.04	3	13
CCA 2+50E 1+90S	1	29	43	64	.5	17	9	272	5.75	15	5	ND	4	5	1	2	2	21	.06	.106	19	18	.29	33	.01	3	1.07	.01	.04	4	44
CCA 2+50E 2+00S	2	33	31	75	1.1	14	12	619	4.98	9	5	ND	3	5	1	2	2	27	.03	.098	22	22	.29	35	.01	3	1.84	.01	.04	1	150
CCA 2+50E 2+10S	2	25	31	56	.6	14	8	839	4.51	12	5	ND	3	5	1	2	2	21	.03	.094	22	12	.21	30	.01	4	.80	.01	.04	3	31
CCA 2+50E 2+20S	1	5	4	15	.2	2	1	60	.60	3	5	ND	2	5	1	2	2	8	.01	.035	35	5	.08	20	.01	5	.43	.01	.03	1	9
CCA 2+50E 2+30S	2	30	32	65	.9	15	11	797	4.66	11	5	ND	1	5	1	2	2	31	.05	.128	19	13	.34	35	.01	4	1.10	.01	.04	2	10
CCA 2+50E 2+40S	1	54	48	83	1.0	19	14	474	5.88	10	5	ND	5	6	1	2	2	28	.04	.085	17	16	.39	33	.01	3	1.82	.01	.04	3	27
CCA 2+50E 2+50S	1	26	35	57	.9	11	7	378	4.34	15	5	ND	3	5	1	2	2	22	.02	.077	17	13	.18	27	.01	6	.88	.01	.04	4	175
CCA 2+50E 2+60S	1	31	37	59	.8	14	11	792	4.76	14	5	ND	3	4	1	3	2	22	.01	.101	19	13	.19	28	.01	3	.87	.01	.04	12	35
CCA 2+50E 2+70S	1	32	47	69	.7	16	11	556	5.47	19	5	ND	2	5	1	2	2	24	.02	.108	20	14	.21	26	.01	4	.87	.01	.04	8	26
CCA 2+50E 2+80S	1	34	38	79	.8	19	12	718	4.96	14	5	ND	4	7	1	2	2	20	.09	.094	20	14	.29	39	.01	2	1.07	.01	.05	10	20
CCA 2+50E 2+90S	1	36	34	70	.6	16	10	595	5.22	9	5	ND	4	4	1	2	2	24	.02	.107	19	14	.29	39	.01	3	1.18	.01	.04	9	16
CCA 2+50E 3+00S	1	8	13	24	.2	5	2	103	1.53	6	5	ND	1	6	1	2	2	12	.04	.064	19	7	.11	30	.01	4	.53	.01	.03	3	15
CCA 2+50E 3+10S	2	36	50	71	.2	13	9	549	5.56	11	5	ND	1	4	1	2	2	26	.01	.115	18	15	.23	29	.01	10	1.20	.01	.03	17	10
CCA 2+50E 3+20S	1	12	16	34	.3	5	3	100	2.14	2	5	ND	1	4	1	2	2	25	.01	.054	22	10	.18	27	.01	2	.88	.01	.03	1	3
CCA 2+50E 3+30S	1	30	31	62	.4	12	8	457	3.78	9	5	ND	3	8	1	5	2	38	.10	.124	19	14	.36	57	.01	3	1.24	.01	.04	2	16
CCA 2+50E 3+40S	1	30	29	73	.8	12	11	1386	4.14	9	5	ND	2	21	1	2	2	31	.09	.088	18	16	.37	38	.01	6	1.32	.01	.04	1	3
CCA 2+50E 3+50S	1	26	26	49	1.2	11	8	618	4.32	11	5	ND	2	6	1	2	2	29	.03	.120	15	13	.19	65	.01	3	.71	.01	.04	2	17
CCA 2+50E 3+60S	1	44	42	64	.8	17	11	555	4.46	11	5	ND	1	5	1	2	2	24	.03	.088	19	18	.26	47	.01	6	1.10	.01	.04	2	23
CCA 2+50E 3+70S	1	37	46	64	.7	21	11	454	5.45	13	5	ND	1	6	1	2	2	27	.05	.115	20	25	.34	36	.01	2	1.18	.01	.04	4	20
CCA 2+50E 3+80S	1	26	33	45	2.4	10	7	538	4.51	10	5	ND	3	5	1	2	2	26	.03	.158	19	11	.15	42	.01	3	.79	.01	.04	2	21
CCA 2+50E 3+90S	2	36	48	64	.5	14	11	1077	6.70	15	5	ND	1	5	1	2	2	34	.02	.185	18	14	.17	33	.01	4	.91	.01	.03	2	16
CCA 2+50E 4+00S	1	27	39	64	.7	12	9	735	7.29	14	5	ND	1	6	1	2	2	26	.05	.199	17	12	.15	37	.01	6	.80	.01	.04	2	13
CCA 3+00E 1+60S	4	66	74	187	.7	72	24	994	6.65	67	5	ND	6	14	1	2	5	27	.17	.107	32	49	.58	128	.01	6	1.55	.01	.07	4	8
CCA 3+00E 1+70S	2	17	35	53	.4	15	8	638	3.95	21	5	ND	2	5	1	3	2	18	.02	.074	23	17	.17	33	.01	7	.71	.01	.03	13	38
CCA 3+00E 1+80S	2	20	37	54	.4	12	8	336	4.42	18	5	ND	2	5	1	2	2	23	.03	.074	21	17	.19	33	.01	2	.80	.01	.05	4	14
CCA 3+00E 1+90S	1	12	28	47	.3	10	5	360	2.57	11	5	ND	1	5	1	2	2	20	.02	.059	20	14	.19	77	.01	5	.79	.01	.05	4	67
CCA 3+00E 2+00S	1	16	31	63	.7	13	6	462	3.07	13	5	ND	2	6	1	2	2	19	.10	.085	18	14	.22	48	.01	6	.79	.01	.06	4	45
CCA 3+00E 2+10S	1	27	46	75	.6	17	8	309	4.07	14	5	ND	2	7	1	3	2	24	.07	.068	21	18	.28	61	.01	2	1.12	.01	.05	10	18
CCA 3+00E 2+20S	1	40	50	100	.2	24	13	1370	4.79	14	5	ND	1	15	1	2	2	24	.24	.105	21	21	.34	116	.01	2	1.37	.01	.06	3	29
CCA 3+00E 2+30S	1	18	61	82	.6	8	7	562	4.01	12	10	ND	4	6	1	2	2	31	.02	.053	21	12	.14	55	.01	2	.75	.01	.05	5	19
CCA 3+00E 2+40S	1	23	39	56	1.0	9	9	601	3.79	13	5	ND	3	5	1	3	2	30	.03	.052	22	12	.16	44	.01	6	.85	.01	.05	6	23
CCA 3+00E 2+50S	1	23	43	61	.3	11	7	240	3.56	10	5	ND	1	7	1	2	2	23	.10	.059	18	14	.14	46	.01	8	.74	.01	.05	9	42
CCA 3+00E 2+60S	1	31	47	82	.4	13	9	796	4.40	12	5	ND	2	6	1	4	2	28	.02	.068	22	16	.17	81	.01	2	.90	.01	.05	13	37
CCA 3+00E 2+70S	1	28	44	80	.8	14	8	517	5.02	12	5	ND	1	6	1	2	2	26	.05	.070	17	14	.18	63	.01	11	.93	.01	.04	4	14
STD C/AU-S	18	57	37	131	7.3	67	27	1033	3.97	37	18	8	38	49	17	17	21	55	.49	.080	36	56	.89	171	.06	37	1.93	.06	.13	13	51

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
CCA 3+00E 2+80S	1	29	45	68	.2	11	11	817	4.96	12	5	ND	1	4	1	3	2	25	.04	.067	18	14	.15	39	.01	3	.82	.01	.04	72	9
CCA 3+00E 2+90S	1	35	49	82	.6	16	12	849	5.62	12	5	ND	1	7	1	3	2	27	.09	.120	16	21	.22	57	.01	9	1.16	.01	.06	150	4
CCA 3+00E 3+00S	1	26	36	61	.5	10	8	459	4.47	8	5	ND	1	4	1	2	2	23	.02	.097	19	17	.21	33	.01	2	1.02	.01	.04	7	4
CCA 3+00E 3+10S	1	16	27	38	.1	10	5	298	3.24	6	5	ND	1	4	1	2	2	18	.03	.082	24	12	.12	29	.01	3	.69	.01	.05	5	30
CCA 3+00E 3+20S	1	10	8	32	.2	6	4	118	1.76	5	5	ND	1	3	1	2	2	14	.01	.034	33	4	.02	17	.01	2	.26	.01	.02	2	4
CCA 3+00E 3+30S	1	55	88	96	.3	20	15	781	5.59	10	5	ND	4	3	1	2	2	19	.01	.067	30	16	.19	41	.01	3	1.16	.01	.04	2	11
CCA 3+00E 3+40S	1	31	37	67	.1	12	9	603	4.72	8	5	ND	1	4	1	2	2	27	.01	.080	22	14	.21	45	.01	2	1.07	.01	.03	2	4
CCA 3+00E 3+50S	1	32	51	51	.1	11	8	1125	3.89	9	5	ND	1	4	1	2	2	30	.01	.112	20	12	.23	53	.01	4	.97	.01	.03	4	5
CCA 3+00E 3+60S	1	29	47	44	.1	9	6	298	3.86	13	5	ND	1	4	1	4	2	26	.01	.101	19	11	.15	34	.01	2	.94	.01	.03	2	4
CCA 3+00E 3+70S	1	30	33	52	.1	12	8	679	4.72	10	5	ND	1	5	1	2	2	30	.01	.196	21	11	.15	34	.01	2	.74	.01	.04	3	3
CCA 3+00E 3+80S	1	23	39	45	.2	9	7	586	3.69	11	5	ND	1	4	1	2	2	21	.01	.080	19	8	.08	28	.01	2	.62	.01	.03	11	17
CCA 3+00E 3+90S	1	39	37	151	.1	20	12	3261	5.43	16	5	ND	1	18	1	2	2	22	.45	.152	16	11	.11	182	.01	7	.47	.01	.07	1	1
CCA 3+00E 4+00S	1	48	24	72	.3	13	14	1094	5.37	9	5	ND	1	7	1	2	2	51	.07	.095	16	9	.12	38	.01	2	.80	.01	.04	1	3
CCA 3+50E 1+60S	3	57	53	178	.1	61	21	618	4.97	50	5	ND	6	20	1	2	2	18	.26	.093	34	29	.39	135	.01	3	.86	.01	.03	4	21
CCA 3+50E 1+70S	1	16	51	60	.1	15	7	183	4.51	10	5	ND	6	5	1	2	2	20	.03	.052	30	25	.29	38	.01	2	1.08	.01	.03	6	9
CCA 3+50E 1+80S	1	24	24	46	1.2	12	6	292	3.84	12	5	ND	1	4	1	2	2	22	.01	.062	21	14	.12	57	.01	2	.68	.01	.03	4	40
CCA 3+50E 1+90S	1	17	34	54	1.6	11	6	253	3.51	7	5	ND	2	6	1	2	2	26	.06	.050	24	16	.18	49	.01	5	.91	.01	.04	4	17
CCA 3+50E 2+00S	1	11	25	32	.6	8	4	108	2.14	9	5	ND	1	5	1	2	2	22	.01	.043	26	14	.15	50	.01	5	.88	.01	.04	3	32
CCA 3+50E 2+10S	1	29	64	96	.6	15	10	360	4.48	12	5	ND	1	9	1	2	2	27	.12	.067	20	19	.23	64	.01	5	1.25	.01	.05	3	26
CCA 3+50E 2+20S	1	30	52	64	1.5	16	11	355	4.20	15	5	ND	1	5	1	2	2	24	.03	.098	21	14	.23	55	.01	2	.92	.01	.04	4	8
CCA 3+50E 2+30S	1	42	81	99	.4	29	17	641	5.38	22	5	ND	5	9	1	2	2	21	.15	.163	22	18	.38	75	.01	5	1.30	.01	.08	4	10
CCA 3+50E 2+40S	1	25	26	65	.1	17	10	837	3.48	10	5	ND	1	6	1	2	3	23	.04	.066	26	15	.31	70	.01	2	1.12	.01	.05	2	11
CCA 3+50E 2+50S	1	27	43	55	.4	12	9	789	3.62	10	5	ND	1	6	1	2	2	28	.03	.071	23	15	.19	55	.01	2	.98	.01	.04	2	204
CCA 3+50E 2+60S	1	32	58	65	.5	16	11	413	5.45	15	5	ND	1	6	1	2	2	25	.05	.128	20	17	.26	42	.01	2	1.17	.01	.04	4	11
CCA 3+50E 2+70S	1	65	58	91	.1	25	21	807	5.93	10	5	ND	2	6	1	2	2	26	.03	.067	25	18	.30	32	.01	5	1.49	.01	.03	6	24
CCA 3+50E 2+80S	1	26	28	61	.4	14	9	769	4.66	9	5	ND	1	4	1	2	2	28	.01	.129	21	19	.27	37	.01	6	1.25	.01	.04	2	11
CCA 3+50E 2+90S	1	24	13	40	.4	4	6	891	2.23	6	5	ND	1	4	1	2	2	17	.01	.056	21	5	.05	37	.01	5	.40	.01	.03	3	3
CCA 3+50E 3+00S	1	28	40	56	2.6	9	7	379	3.64	10	5	ND	2	4	1	3	2	18	.01	.090	18	13	.19	35	.01	4	1.03	.01	.05	3	7
CCA 3+50E 3+10S	1	23	25	59	.1	7	7	520	2.97	8	5	ND	1	5	1	2	2	21	.03	.087	22	9	.12	35	.01	4	.61	.01	.04	3	8
CCA 3+50E 3+20S	1	12	28	34	.4	8	4	282	2.66	9	5	ND	1	6	1	2	2	22	.02	.138	19	10	.10	50	.01	6	.66	.01	.04	5	3
CCA 3+50E 3+30S	1	19	43	47	.3	9	7	234	4.69	10	5	ND	1	4	1	2	2	28	.01	.175	19	12	.14	24	.01	3	.78	.01	.04	7	6
CCA 3+50E 3+40S	1	34	71	77	.6	17	12	705	5.68	13	5	ND	1	4	1	2	3	23	.01	.135	19	18	.27	44	.01	2	1.28	.01	.04	6	11
CCA 3+50E 3+50S	1	30	47	48	.6	10	8	316	4.43	10	5	ND	1	4	1	2	3	26	.01	.073	22	13	.19	25	.01	3	1.10	.01	.03	3	2
CCA 3+50E 3+60S	1	25	30	75	.1	11	9	718	6.96	13	5	ND	1	6	1	2	2	34	.01	.088	21	11	.14	55	.01	2	.84	.01	.03	1	3
CCA 3+50E 3+70S	1	37	45	81	.5	15	11	681	7.15	10	5	ND	1	8	1	2	2	38	.11	.188	21	15	.18	41	.01	6	.90	.01	.04	3	18
CCA 3+50E 3+80S	1	22	27	54	.1	14	8	428	3.54	7	5	ND	1	7	1	2	2	18	.05	.079	24	10	.15	28	.01	5	.66	.01	.04	1	3
STD C	19	58	39	134	7.0	69	29	969	3.77	37	15	8	37	50	18	15	22	57	.47	.087	37	58	.84	177	.06	33	2.02	.06	.13	10	-

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AUS PPB
CCA 3+50E 3+90S	1	22	52	40	.1	14	7	348	4.69	11	5	ND	1	5	1	2	2	22	.03	.070	18	12	.12	27	.01	4	.63	.01	.02	2	7
CCA 3+50E 4+00S	1	29	71	78	1.1	17	13	847	5.60	14	5	ND	1	8	1	2	2	25	.08	.122	16	19	.20	48	.01	3	1.06	.01	.03	1	3
CCA 4+00E 1+60S	2	47	53	99	.1	49	20	859	4.94	55	5	ND	4	12	1	4	2	13	.14	.063	26	18	.33	80	.01	10	.80	.01	.04	7	27
CCA 4+00E 1+70S	2	19	40	65	.1	23	11	377	5.00	14	5	ND	1	4	1	2	2	19	.02	.068	20	27	.30	25	.01	8	1.16	.01	.03	6	6
CCA 4+00E 1+80S	2	15	113	57	.1	15	11	629	4.02	17	5	ND	1	8	1	2	2	41	.04	.065	21	18	.17	44	.02	3	1.09	.01	.03	2	15
CCA 4+00E 1+90S	2	8	26	41	.3	9	6	305	2.88	12	5	ND	1	6	1	2	2	34	.02	.043	26	15	.11	26	.02	3	.83	.01	.03	4	5
CCA 4+00E 2+00S	2	17	15	44	.1	13	7	302	3.35	24	5	ND	1	5	1	2	2	34	.03	.056	22	13	.13	24	.01	4	.67	.01	.04	2	52
CCA 4+00E 2+10S	2	12	19	43	.3	11	6	269	4.01	15	5	ND	1	4	1	2	2	24	.01	.067	24	14	.12	20	.01	6	.71	.01	.03	4	9
CCA 4+00E 2+20S	2	11	28	36	.1	11	6	679	3.59	12	5	ND	1	4	1	2	2	25	.01	.092	22	14	.13	28	.01	9	.65	.01	.01	3	18
CCA 4+00E 2+30S	1	19	50	47	.4	13	8	420	4.61	14	5	ND	1	4	1	2	2	26	.02	.070	19	17	.17	21	.01	2	.91	.01	.03	9	22
CCA 4+00E 2+40S	1	7	21	29	.1	8	5	177	2.54	8	5	ND	1	4	1	2	2	25	.01	.077	25	11	.17	33	.01	2	.88	.01	.03	5	14
CCA 4+00E 2+50S	1	17	28	51	.1	15	9	475	4.33	17	5	ND	2	4	1	2	2	26	.02	.078	23	16	.32	43	.01	5	1.19	.01	.04	3	30
CCA 4+00E 2+60S	1	12	19	42	.4	10	6	213	3.27	9	5	ND	1	6	1	2	2	30	.03	.075	21	19	.22	35	.01	3	1.18	.01	.05	11	9
CCA 4+00E 2+70S	1	27	36	56	.8	17	12	374	4.36	15	5	ND	1	5	1	2	2	30	.02	.089	19	17	.33	36	.01	3	1.21	.01	.03	4	11
CCA 4+00E 2+80S	2	34	43	66	.1	15	14	1012	6.62	11	5	ND	1	7	1	2	2	31	.01	.080	24	19	.22	47	.01	5	1.38	.01	.03	3	1
CCA 4+00E 2+90S	1	24	33	56	.2	13	10	654	5.29	10	5	ND	1	7	1	2	2	25	.03	.093	22	11	.14	35	.01	2	.82	.01	.05	3	8
CCA 4+00E 3+00S	2	24	34	45	.3	13	9	433	4.91	12	5	ND	1	5	1	2	2	28	.01	.067	22	13	.16	51	.01	2	.84	.01	.03	6	7
CCA 4+00E 3+10S	1	12	27	35	.4	10	6	296	4.48	8	5	ND	1	4	1	2	2	27	.01	.074	20	15	.18	35	.01	2	.89	.01	.03	5	3
CCA 4+00E 3+20S	2	33	64	60	.6	17	12	771	4.94	16	5	ND	1	5	1	2	2	25	.02	.098	18	19	.23	42	.01	2	1.33	.01	.05	7	205
CCA 4+00E 3+30S	1	24	39	51	.2	16	10	329	4.62	16	5	ND	1	4	1	2	2	27	.01	.090	21	14	.22	34	.01	2	.94	.01	.04	7	31
CCA 4+00E 3+40S	1	26	59	58	.1	21	10	220	5.39	26	5	ND	2	4	1	2	2	24	.01	.097	16	20	.30	42	.01	2	1.26	.01	.04	7	10
CCA 4+00E 3+50S	1	14	37	32	.8	9	6	159	3.56	11	5	ND	1	4	1	2	2	22	.01	.056	20	13	.19	26	.01	2	.91	.01	.03	9	40
CCA 4+00E 3+60S	2	20	31	51	.1	14	10	599	6.79	29	5	ND	1	5	1	2	2	27	.01	.099	20	14	.17	32	.01	3	1.01	.01	.04	3	1
CCA 4+00E 3+70S	1	24	30	51	.4	15	9	324	5.34	13	5	ND	1	4	1	2	2	30	.01	.072	19	14	.24	27	.01	3	1.04	.01	.03	3	7
CCA 4+00E 3+80S	1	32	22	66	.1	18	11	600	4.62	8	5	ND	1	5	1	2	3	33	.04	.092	24	17	.43	30	.01	2	1.28	.01	.04	1	1
CCA 4+00E 3+90S	2	53	42	88	.6	17	16	1260	7.71	12	5	ND	1	5	1	2	6	54	.02	.142	15	22	.53	70	.01	3	2.17	.01	.04	3	1
CCA 4+00E 4+00S	2	50	33	67	1.0	14	12	810	5.85	7	5	ND	1	5	1	2	2	39	.04	.116	18	15	.38	42	.01	2	1.34	.01	.04	1	1
STD C/AU-S	19	59	37	128	7.1	68	29	988	3.95	39	17	8	40	51	18	17	19	57	.49	.085	38	61	.88	173	.06	38	1.92	.06	.14	13	52

EXTRA  
COPY

## GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.  
- SAMPLE TYPE: P1-SOIL P2-ROCK AU: ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: SEPT 21 1987

DATE REPORT MAILED: *Oct 1/87*ASSAYER: *N. J. Jones* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-4372 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
CCR 4+25W 2+50S	1	42	22	94	.5	33	22	746	4.66	16	5	ND	15	5	1	2	2	20	.06	.051	36	30	.65	33	.01	2	1.98	.02	.04	1	31
CCR 0+00E 0+90S	1	39	31	112	.2	43	17	800	4.13	14	5	ND	6	12	1	2	2	23	.12	.062	32	29	.53	51	.01	4	1.26	.02	.04	1	71
CCR 1+50E 3+80S	1	46	15	76	.3	13	11	411	5.13	196	5	ND	3	5	1	2	2	35	.06	.099	12	10	.16	47	.01	2	.99	.01	.04	1	142
CCR 2+00E 2+40S	2	23	23	93	.3	52	29	2529	14.52	168	5	ND	4	4	1	2	2	15	.03	.113	16	5	.12	45	.01	2	.45	.01	.04	2	1190
CCR 2+00E 3+30S	1	93	336	233	1.3	35	26	3207	8.09	38	5	ND	3	19	2	2	3	12	.36	.113	15	9	.10	49	.01	3	.91	.02	.03	23	67
CCR 4+00E 3+70S	3	69	47	125	.2	22	16	4834	18.42	301	5	ND	4	9	1	2	2	22	.03	.125	13	11	.16	63	.01	2	.84	.01	.03	5	290
STD C/AU-S	18	59	37	134	7.3	67	27	1035	3.76	39	18	7	39	50	18	17	23	58	.45	.085	38	59	.85	179	.08	36	1.77	.08	.13	12	51

C O R E   A N A L Y S E S



GEOCHEMICAL ANALYSIS CERTIFICATE

DATE RECEIVED: OCT 2 1987 DATE REPORT MAILED: Nov 9/87 ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-5314

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CB	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
E 56352	3	18	31	34	.7	44	19	1059	6.09	287	5	4	8	143	1	2	2	3	3.96	.028	5	8	1.28	22	.01	5	.18	.01	.12	1	5390
E 56353	2	32	14	54	.1	38	16	932	4.37	66	5	ND	10	56	1	2	2	3	1.59	.029	16	8	1.00	21	.01	2	.20	.01	.11	1	21
E 56354	1	39	27	86	.1	42	20	850	5.28	33	5	ND	13	30	1	2	2	5	.72	.036	23	14	1.04	22	.01	3	.49	.01	.14	1	31
E 56355	2	46	48	107	.1	45	26	522	6.05	15	5	ND	11	11	1	2	2	15	.17	.040	15	33	1.08	22	.01	2	1.73	.01	.13	1	11
E 56356	1	18	8	10	.2	15	7	899	2.74	43	5	ND	4	77	1	2	2	2	2.34	.014	6	6	.77	16	.01	3	.13	.01	.07	1	235
E 56357	1	12	6	15	.1	16	4	1121	2.35	23	5	ND	4	54	1	2	2	2	2.21	.013	6	5	.62	13	.01	5	.13	.01	.07	1	126
E 56358	1	16	4	11	.1	22	2	2362	2.77	11	5	ND	1	53	1	2	2	1	3.09	.005	3	6	.73	9	.01	2	.05	.01	.03	1	635
E 56359	1	11	14	16	.1	26	14	1179	3.81	59	5	ND	5	43	1	2	2	2	1.80	.032	6	6	.83	18	.01	2	.20	.01	.13	1	265
E 56360	2	67	7	61	.1	29	20	911	5.70	7	5	ND	6	94	1	2	2	13	3.00	.029	8	14	1.61	20	.01	2	.60	.02	.10	1	1680
E 56361	1	18	3	62	.1	28	13	462	4.58	4	5	ND	5	27	1	2	2	11	1.57	.011	7	10	1.35	505	.01	2	.18	.02	.08	1	89
E 56362	5	156	7	74	.2	28	27	1420	7.96	33	5	ND	2	170	1	2	2	16	5.41	.050	2	13	3.35	25	.01	2	.21	.02	.11	1	1
E 56363	2	88	4	73	.1	32	13	1217	5.10	2	5	ND	6	88	1	2	2	8	2.54	.019	12	10	1.53	92	.01	3	.22	.02	.10	1	1
STD C/AU-R	19	61	38	131	7.5	70	29	1045	4.03	41	18	8	39	53	18	17	19	60	.50	.089	39	59	.89	178	.09	38	1.86	.06	.14	13	480

## GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPB.  
 - SAMPLE TYPE: CORE/ROCK AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 6 1987

DATE REPORT MAILED: Nov 24/87

ASSAYER: D. Toye... DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-5472

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
E 56364	1	26	11	32	.1	18	8	1187	3.15	9	5	ND	1	299	1	2	2	3	5.84	.013	2	6	2.12	7	.01	2	.04	.02	.03	2	1
E 56365	1	29	5	10	.2	7	2	405	1.75	2	5	ND	2	36	1	2	2	1	1.19	.007	3	3	.49	11	.01	2	.09	.02	.05	1	310
E 56366	1	340	5	18	.4	164	10	456	8.42	2	5	ND	3	32	1	2	2	1	.77	.012	2	2	.49	10	.01	2	.06	.01	.05	3	3420
E 56367	1	28	4	16	.1	17	4	792	2.39	2	5	ND	4	102	1	2	2	1	2.20	.031	5	3	.95	18	.01	4	.13	.01	.07	1	1
E 56368	1	305	26	26	.5	63	12	1326	8.31	16	5	ND	7	131	1	2	2	2	3.08	.024	2	4	1.31	26	.01	2	.16	.01	.12	2	19
E 56369	1	22	7	8	.2	6	2	305	1.19	2	5	ND	1	39	1	2	3	1	.83	.007	2	2	.35	11	.01	2	.04	.01	.02	1	1
E 56370	1	72	33	44	.1	66	18	1091	4.96	4	5	ND	7	59	1	2	2	2	.99	.025	6	6	1.13	36	.01	2	.25	.02	.13	2	2
E 56371	1	9	10	21	.1	13	6	1119	3.76	22	5	ND	3	155	1	2	2	1	3.64	.022	4	5	1.60	11	.01	2	.09	.02	.05	1	1
E 56372	1	7	2	13	.2	9	3	503	2.65	7	5	ND	4	58	1	2	2	1	.62	.030	4	4	.72	7	.01	2	.09	.03	.04	2	8
JW-87-98R	1	9	13	24	.1	3	15	732	3.30	45	5	ND	1	765	1	2	2	1	26.21	.018	2	3	.30	11	.01	2	.04	.01	.02	1	65
JW-87-99R	1	135	16	82	.1	14	9	4341	15.36	20	5	ND	1	378	1	2	2	7	16.64	.009	3	1	.92	6	.01	2	.01	.01	.02	1	87
STD C/AU-R	19	60	43	127	7.2	70	29	1040	4.04	40	21	8	37	51	18	18	24	57	.46	.087	39	62	.85	174	.07	34	1.90	.06	.14	12	500

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**GEOCHEMICAL ANALYSIS CERTIFICATE**

ICP - .500 GRAM SAMPLE IS DIGESTED WITH JML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: Core - AUS ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 9 1987

DATE REPORT MAILED: Nov 19/87

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-5526

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUS
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
E 56373	1	113	22	35	.5	33	8	782	3.96	40	10	ND	5	87	1	2	2	2	1.82	.016	6	4	1.03	26	.01	2	.18	.04	.09	1	116
E 56374	1	16	115	31	.3	13	3	339	1.29	2	5	ND	3	48	1	2	2	1	1.18	.013	3	3	.44	8	.01	2	.05	.04	.02	3	1
E 56375	1	34	35	12	.4	16	4	340	1.70	2	5	ND	5	37	1	2	2	1	.92	.013	6	4	.38	8	.01	2	.10	.06	.03	1	1
E 56376	2	13	6	38	.1	34	9	813	3.91	5	5	ND	7	64	1	2	2	3	1.47	.022	7	5	1.18	23	.01	2	.16	.05	.07	1	1
E 56377	1	44	188	53	.5	29	6	1126	3.57	5	5	ND	4	137	1	2	2	2	2.78	.027	4	4	1.26	20	.01	2	.12	.04	.06	1	1
E 56378	1	17	162	43	.2	29	12	917	3.13	43	5	ND	5	152	1	2	2	3	2.49	.027	5	5	1.14	29	.01	2	.19	.04	.08	2	7
E 56379	2	21	8	45	.2	23	7	806	3.24	25	5	ND	4	194	1	2	2	3	3.01	.022	5	4	1.36	16	.01	2	.14	.04	.05	2	6
E 56380	2	6	12	40	.1	31	10	763	4.69	69	5	ND	6	32	1	2	2	2	.50	.026	9	4	1.17	24	.01	4	.20	.03	.09	2	132
E 56381	1	4	33	7	.4	13	3	230	1.81	69	5	ND	3	63	1	2	2	1	.88	.006	3	3	.34	5	.01	3	.05	.03	.02	1	1440
E 56382	1	4	17	4	.1	3	1	262	1.07	3	5	ND	2	23	1	2	2	1	.34	.003	2	3	.24	5	.01	3	.05	.02	.02	1	4
E 56383	2	6	131	32	.5	36	36	792	4.34	135	5	ND	4	77	1	2	2	2	1.09	.013	3	2	.75	12	.01	2	.09	.03	.06	3	510
STD C/AU-R	19	57	38	133	7.4	67	27	1027	4.09	43	25	7	38	30	18	16	20	57	.49	.086	37	58	.85	177	.08	33	1.83	.08	.14	11	520

## GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH JML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: Core AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 16 1987

DATE REPORT MAILED: NOV 23/87

ASSAYER: D. Toyce DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-5667

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
E 56384	1	15	14	57	.3	41	10	1001	7.42	3	5	ND	9	59	1	2	2	3	2.05	.026	7	3	2.03	20	.01	2	.16	.05	.10	1	1
E 56385	8	22	1867	15182	2.9	26	6	597	2.69	7	5	ND	7	97	107	2	2	2	2.27	.021	7	12	.93	25	.01	2	.17	.05	.11	1	1
E 56386	1	29	303	626	.7	40	10	601	4.37	105	5	ND	4	96	4	2	2	2	2.05	.017	3	4	.84	9	.01	3	.06	.04	.03	1	103
E 56387	1	57	874	90	1.4	44	14	1075	4.23	18	5	ND	5	141	1	2	2	3	2.84	.053	3	4	1.29	30	.01	2	.17	.04	.11	1	10
E 56388	2	38	76	2334	.4	95	47	547	5.53	227	5	ND	6	72	15	2	2	3	1.48	.018	5	4	.72	33	.01	2	.20	.05	.12	1	260
E 56389	1	7	7	29	.1	22	6	862	4.69	36	5	ND	5	49	1	2	2	3	.86	.035	7	5	1.42	21	.01	2	.11	.05	.05	1	6
E 56390	1	23	75	74	.4	15	7	652	2.71	4	5	ND	5	857	1	2	2	1	18.07	.029	4	2	.93	20	.01	2	.10	.01	.06	1	1
E 56391	1	74	16	47	.6	11	4	945	5.00	2	5	ND	2	885	1	2	3	1	28.29	.014	2	1	.65	5	.01	2	.02	.01	.01	1	8
E 56392	1	6	3606	736	4.3	3	1	281	.66	8	5	ND	1	907	8	2	3	1	22.92	.041	2	1	.11	8	.01	3	.05	.01	.02	1	1
E 56393	1	6	180	588	.3	6	7	1133	3.66	26	5	ND	2	168	5	2	2	5	6.46	.048	3	2	1.03	17	.01	2	.14	.02	.08	709	22
E 56394	9	30	14177	14844	12.7	18	10	1732	7.61	201	5	ND	3	265	136	14	2	4	10.64	.050	2	16	.96	20	.01	2	.09	.01	.06	577	310
E 56395	2	19	98	128	.2	7	9	3596	7.43	23	5	ND	2	279	1	2	2	6	11.70	.049	2	1	2.54	19	.01	2	.13	.01	.06	3	2
E 56396	1	34	143	99	.3	26	9	873	2.91	72	5	ND	6	71	1	2	2	2	2.98	.026	6	2	.63	31	.01	3	.13	.03	.08	7	1
STD C/AU-R	19	57	38	132	7.1	68	27	1032	4.08	40	20	6	38	51	18	18	20	57	.49	.086	38	59	.89	180	.08	32	1.86	.08	.14	11	485

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: Core AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 18 1987 DATE REPORT MAILED: Nov 27/87 ASSAYER: D. Toyer DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-5768

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make

SAMPLE#	NO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUR
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM	PPB
E 56397	1	11	15	16	1.0	10	5	598	2.20	9	12	ND	2	947	1	2	2	2	23.04	.017	3	2	.62	20	.01	2	.12	.01	.05	1	1
E 56398	1	171	7	27	.6	18	19	984	6.27	3	5	ND	2	236	1	2	2	10	7.61	.068	2	1	2.06	59	.01	2	.27	.05	.09	2	1
E 56399	1	34	8805	226	40.4	106	17	1088	2.67	74	5	ND	4	313	3	2	81	1	10.04	.014	4	4	.74	27	.01	2	.15	.01	.09	4	48
E 56400	1	5	526	264	1.4	5	3	876	1.47	10	6	ND	2	1178	4	2	4	1	30.54	.018	4	1	.51	11	.01	3	.06	.01	.03	1	3
E 56401	3	52	11760	1411	18.5	12	9	3376	6.35	25	5	ND	4	524	23	15	2	2	18.08	.052	3	3	2.00	17	.01	2	.11	.01	.06	780	4
E 56402	3	9	8398	444	15.7	21	11	3126	5.40	37	5	ND	7	224	6	10	2	3	11.14	.028	5	5	3.02	16	.01	8	.14	.01	.08	955	6
STD C/AU-R	19	57	38	133	7.1	68	28	1029	4.05	42	21	7	38	49	18	18	19	55	.48	.085	37	58	.87	176	.08	31	1.91	.07	.13	12	500

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: Core. AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 25 1987

DATE REPORT MAILED: Dec 3/87

ASSAYER: *Al. Lopez* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-5892

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
E 56403	1	14	5	44	.5	21	8	927	3.68	13	5	ND	12	631	1	3	2	2	12.60	.018	17	2	1.76	28	.01	2	.19	.02	.11	2	4
E 56404	1	23	8	56	.2	26	10	548	3.15	10	5	ND	14	771	1	5	2	2	14.12	.024	26	3	.94	34	.01	3	.28	.02	.13	1	5
E 56405	1	5	10	69	.1	9	6	2546	5.83	14	5	ND	8	751	1	2	2	2	19.51	.012	19	4	4.32	19	.01	2	.25	.01	.06	1	1
E 56406	1	42	2	83	.2	28	19	974	4.62	9	5	ND	10	91	1	2	2	7	1.17	.031	25	5	1.08	80	.01	2	.40	.02	.14	1	1
E 56407	1	16	4	77	.1	32	17	1350	5.45	4	5	ND	12	81	1	2	2	9	1.15	.032	27	6	1.13	38	.01	3	.28	.01	.14	1	1
E 56408	1	8	2	117	.1	52	19	641	5.79	2	5	ND	13	25	1	2	2	18	.31	.032	26	28	1.53	55	.01	5	2.48	.01	.12	1	1
E 56409	1	29	3	111	.1	40	17	1220	5.39	2	5	ND	11	59	1	2	2	13	.71	.027	25	16	1.47	434	.01	7	1.27	.01	.11	1	2
E 56410	1	46	12	88	.1	36	19	959	4.93	27	5	ND	11	27	1	2	3	4	.43	.031	16	7	1.15	26	.01	7	.49	.02	.13	1	7
E 56411	1	41	24	39	.9	40	14	1014	6.22	156	5	7	7	125	1	2	2	3	2.89	.023	7	5	1.25	26	.01	2	.26	.01	.14	2	4450
E 56412	1	24	6	67	.1	31	15	1158	7.16	72	5	ND	7	124	1	2	2	3	3.84	.020	7	4	1.62	26	.01	2	.21	.01	.15	1	340
E 56413	1	42	22	85	.2	38	24	1058	6.15	71	5	ND	8	80	1	2	2	5	1.82	.044	14	4	1.40	23	.01	2	.29	.01	.14	1	180
E 56414	1	36	11	59	.3	42	20	748	5.82	25	5	ND	12	101	1	2	2	13	2.37	.036	14	19	1.29	33	.01	3	1.58	.01	.13	1	32
E 56415	1	26	59	88	.5	28	13	798	4.71	3	5	ND	7	54	1	2	2	12	1.46	.025	12	16	1.16	23	.01	2	1.62	.01	.12	1	24
E 56416	1	25	2	104	.1	40	18	1007	6.05	2	5	ND	10	56	1	2	2	20	1.49	.031	17	31	1.54	25	.01	2	2.34	.02	.11	1	12
E 56417	1	49	2	75	.1	43	26	680	6.36	56	5	ND	6	33	1	2	2	4	.75	.029	17	3	1.56	29	.01	6	.29	.03	.15	1	6
E 56418	1	9	4	72	.3	33	20	1204	5.70	2	5	ND	3	132	1	2	2	8	3.40	.028	6	3	2.19	19	.01	2	.65	.02	.10	1	1
E 56419	1	7	2	56	.1	35	16	1150	5.11	3	5	ND	6	36	1	2	2	5	.95	.018	12	7	1.29	27	.01	4	.58	.02	.13	1	2
E 56420	1	36	6	78	.1	46	19	825	5.48	16	5	ND	4	40	1	2	2	9	.86	.016	9	5	1.43	146	.01	2	.28	.02	.10	1	1
E 56421	3	49	6	65	.1	42	21	896	5.58	10	5	ND	5	32	1	2	2	5	.69	.030	7	4	1.25	47	.01	6	.26	.03	.13	1	1
E 56422	1	18	2	47	.1	36	16	1057	5.82	27	5	ND	5	45	1	2	2	7	1.03	.016	9	5	1.13	108	.01	3	.29	.02	.14	1	85
E 56423	1	41	3	64	.1	34	15	1067	4.88	2	5	ND	6	41	1	2	3	7	1.11	.022	21	5	1.16	137	.01	4	.30	.02	.12	1	34
E 56424	1	35	6	35	.1	20	8	1134	3.59	8	5	ND	3	66	1	2	2	4	3.25	.013	7	3	1.04	33	.01	5	.20	.01	.10	1	99
E 56425	1	16	2	75	.2	44	18	1035	5.35	6	5	ND	5	37	1	2	2	10	.73	.015	10	5	1.31	495	.01	7	.29	.02	.14	1	4
E 56426	1	90	2	91	.1	38	19	937	4.74	3	5	ND	6	36	1	2	2	9	.50	.018	13	5	1.34	215	.01	7	.33	.02	.14	1	1
STD C/AU-R	19	57	39	131	7.4	67	28	1074	4.14	42	19	7	36	50	18	16	19	56	.46	.084	38	59	.86	177	.06	39	1.87	.06	.14	13	490

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: Core - AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 29 1987

DATE REPORT MAILED: Dec 3/87

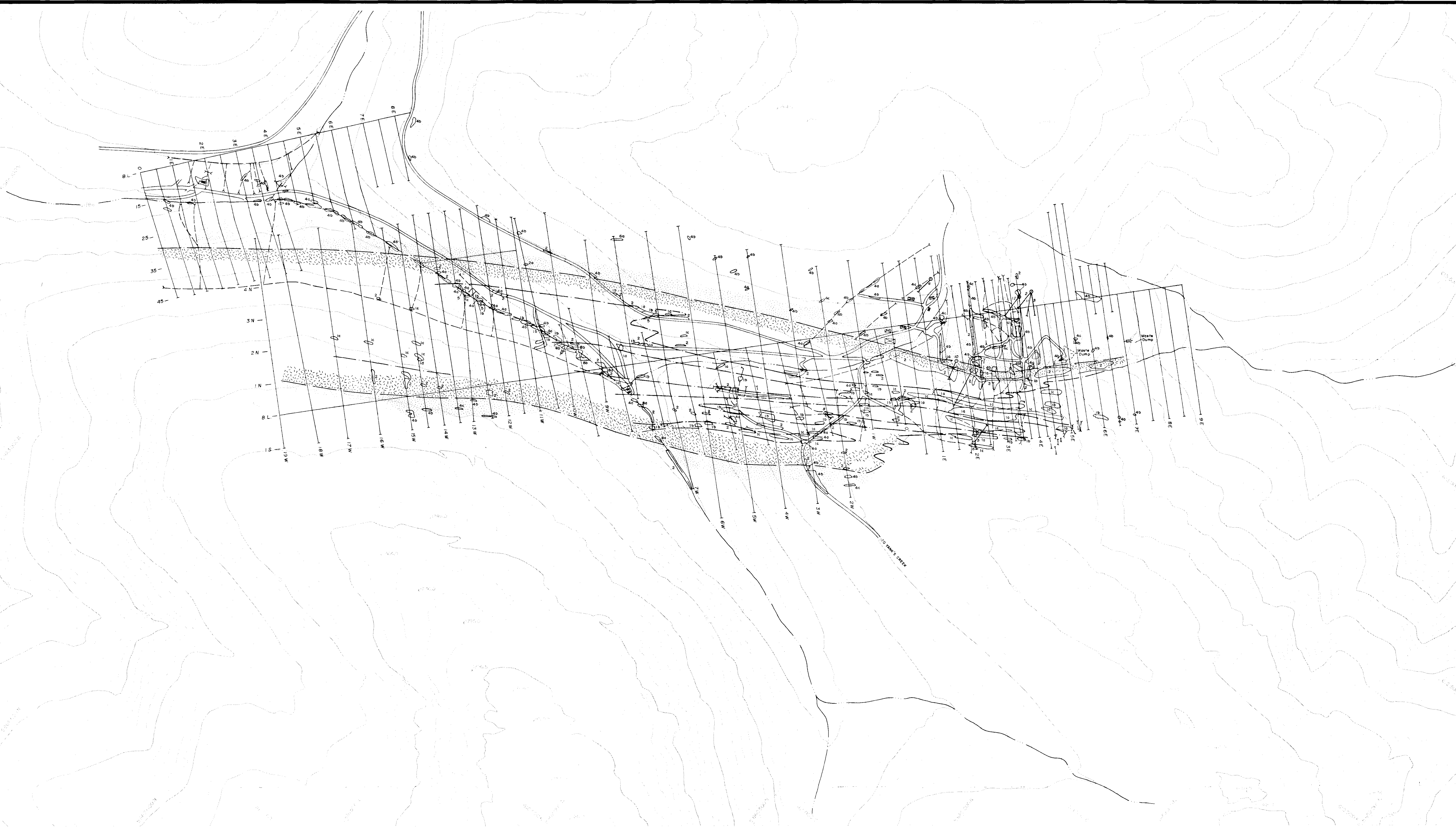
ASSAYER: *D. J. Jepsen* DEAN TOYE, CERTIFIED B.C. ASSAYER

IMPERIAL METALS PROJECT-4203 File # 87-5941 Page 1

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
E 56427	1	39	10	18	.1	46	13	1202	3.34	2	5	ND	11	117	1	2	2	3	3.60	.021	10	9	1.21	28	.01	2	.49	.02	.14	1	5
E 56428	1	29	2	21	.1	35	10	630	2.81	2	5	ND	9	90	1	2	2	3	2.49	.112	7	11	.91	21	.01	10	.59	.03	.13	1	4
E 56429	1	9	2	94	.1	10	4	801	2.12	11	5	ND	4	101	1	2	2	1	3.52	.016	6	2	1.16	15	.01	4	.11	.01	.05	2	7
E 56430	1	50	6	21	.3	18	7	1284	3.34	10	5	ND	3	214	1	2	4	3	5.56	.025	2	7	2.01	13	.01	2	.10	.02	.03	1	5
E 56431	1	19	8	36	.1	23	6	723	2.98	11	5	ND	4	98	1	2	2	1	2.38	.014	6	3	1.07	19	.01	2	.17	.02	.08	1	2
E 56432	1	25	3	31	.1	24	7	910	3.29	2	5	ND	8	39	1	2	4	1	1.01	.018	12	4	.86	25	.01	2	.24	.02	.13	1	3
E 56433	1	27	18	61	.1	39	14	2479	6.04	6	5	ND	7	89	1	2	2	2	1.84	.021	8	4	1.73	20	.01	5	.19	.02	.11	1	1
E 56434	1	21	2	36	.4	19	5	729	2.98	6	5	ND	7	63	1	2	2	1	1.37	.017	12	5	.88	20	.01	4	.16	.02	.07	1	4
E 56435	1	14	5	46	.2	25	9	795	3.36	2	5	ND	12	43	1	3	2	2	1.05	.020	15	5	.89	23	.01	3	.29	.04	.11	1	1
E 56436	1	52	60	45	.3	57	16	1141	5.04	6	5	ND	7	51	1	2	4	2	1.14	.028	10	5	1.27	33	.01	2	.27	.02	.13	1	1
E 56437	1	43	49	72	.2	48	16	1011	4.93	3	5	ND	8	52	1	2	5	2	1.24	.027	11	4	1.38	27	.01	2	.30	.02	.14	2	1
E 56438	1	58	6	98	.1	52	17	797	4.91	2	5	ND	9	28	1	2	2	7	.78	.044	12	23	1.46	31	.01	3	1.12	.04	.14	1	2
E 56439	1	11	2	49	.1	23	8	648	4.08	2	5	ND	7	53	1	2	2	10	1.42	.017	11	25	1.49	11	.01	2	1.33	.03	.07	1	1
E 56440	1	31	8	34	.1	35	11	721	3.89	23	5	ND	8	48	1	2	3	2	1.09	.025	10	6	1.11	31	.01	2	.32	.02	.12	1	10
E 56441	1	14	5	36	.1	28	7	752	3.64	27	5	ND	7	58	1	2	2	2	1.31	.024	9	7	1.07	15	.01	4	.25	.03	.06	1	1
E 56442	1	14	2	113	.1	33	10	507	4.06	40	5	ND	10	56	1	2	7	2	1.02	.029	16	5	1.24	20	.01	5	.28	.02	.10	2	1
E 56443	23	16	8922	32885	9.9	10	11	676	2.89	18	5	ND	4	37	257	5	6	1	.82	.009	3	3	.73	20	.01	4	.09	.01	.05	1	31
E 56444	1	15	6	34	.3	16	5	2005	5.31	5	5	ND	6	36	1	2	7	1	1.11	.016	8	3	1.43	16	.01	2	.14	.01	.09	1	5
E 56445	1	33	41	136	.1	41	12	755	4.15	12	5	ND	3	43	1	2	3	1	1.14	.016	6	4	1.33	26	.01	2	.20	.01	.11	2	1
E 56446	1	34	5	39	.2	61	14	1242	5.11	27	5	ND	10	28	1	2	7	2	.73	.045	14	6	1.42	26	.01	3	.25	.01	.15	1	1
E 56447	1	14	11	26	.1	20	8	822	2.66	20	5	ND	8	92	1	2	2	2	2.44	.030	12	4	1.12	14	.01	2	.23	.01	.08	1	2
E 56448	1	39	1082	183	5.4	56	17	474	11.93	275	5	ND	7	14	1	8	2	3	.26	.020	5	3	1.00	21	.01	2	.27	.02	.13	4	260
E 56449	1	14	25	19	.2	26	11	666	4.12	127	5	ND	3	27	1	3	2	1	.36	.012	5	4	.61	29	.01	3	.10	.01	.07	1	620
E 56450	1	24	4	38	.3	38	13	1076	5.81	69	5	ND	9	40	1	2	3	2	.79	.032	10	4	1.37	24	.01	2	.24	.01	.13	1	590
E 56451	1	81	6	280	.1	37	12	790	6.51	27	6	ND	7	32	1	2	2	3	.78	.028	10	5	1.63	37	.01	5	.21	.01	.10	5	4
E 56452	1	29	7	28	.1	37	12	756	3.96	63	5	ND	7	65	1	2	5	2	1.62	.026	14	4	1.16	22	.01	3	.17	.01	.08	1	6
E 56453	1	29	3	36	.1	20	10	479	2.93	4	5	ND	7	94	1	2	4	3	3.09	.024	7	4	1.08	20	.01	3	.22	.02	.07	1	1
E 56454	1	14	5	16	.1	19	7	313	1.89	25	5	ND	6	81	1	2	2	1	2.25	.009	9	5	.72	21	.01	5	.20	.01	.10	1	9
E 56455	1	9	6	17	.2	49	14	418	3.63	93	5	ND	5	80	1	2	5	1	1.63	.002	4	5	.77	21	.01	8	.16	.01	.09	1	190
E 56456	1	7	2	1	.3	2	1	54	.37	2	10	ND	2	4	1	2	3	1	.05	.001	2	2	.03	1	.01	3	.01	.01	.01	1	5
E 56457	1	14	4	19	.2	23	9	613	2.89	44	5	ND	5	94	1	2	4	2	2.66	.026	10	5	1.15	29	.01	6	.21	.01	.13	1	535
E 56458	1	19	5	22	.2	27	10	635	2.82	38	5	ND	5	107	1	2	3	1	2.97	.032	9	5	1.19	23	.01	4	.21	.01	.11	1	205
E 56459	1	30	9	56	.1	41	14	834	4.92	39	5	ND	7	140	1	2	2	3	3.01	.051	11	4	1.83	31	.01	3	.27	.01	.15	1	25
E 56460	1	9	5	15	.3	23	8	548	3.02	52	5	ND	4	110	1	2	5	1	1.90	.012	8	4	1.11	16	.01	2	.12	.01	.08	1	22
E 56461	1	9	4	31	.1	57	18	719	4.87	137	5	ND	10	60	1	2	2	3	1.04	.028	16	5	1.43	30	.01	2	.27	.01	.15	1	64
E 56462	3	9	3	36	.1	68	19	602	3.70	158	5	ND	7	120	1	4	5	3	1.79	.029	11	5	1.26	33	.01	4	.26	.01	.14	1	58
STD C/AU-R	19	61	38	132	7.4	69	29	1041	4.17	39	19	8	40	51	18	16	23	59	.46	.086	39	61	.89	181	.06	34	1.94	.06	.14	14	480

SAMPLE#	MO	CU	PB	ZN	AG	NZ	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU8
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
E 56463	3	20	12	43	.2	61	20	1011	4.52	112	5	ND	8	152	1	2	2	3	3.33	.021	11	6	2.04	25	.01	2	.19	.01	.13	1	4
E 56464	3	137	9	33	.6	57	21	1002	6.12	96	5	ND	7	97	1	2	2	3	2.42	.025	4	4	1.46	23	.01	2	.17	.01	.12	2	77
E 56465	1	62	8	32	.1	31	11	776	3.12	16	5	ND	8	104	1	2	2	2	2.70	.030	9	4	1.24	26	.01	4	.21	.01	.12	1	6
E 56466	2	31	2	20	.2	27	11	558	2.62	2	5	ND	7	75	1	2	4	1	2.17	.030	7	3	.97	22	.01	2	.17	.01	.10	1	4
E 56467	2	57	4	63	.2	58	17	819	4.29	2	5	ND	9	43	1	2	2	2	1.19	.049	9	4	1.23	27	.01	2	.25	.02	.12	1	1
E 56468	1	27	2	34	.2	45	10	1302	4.28	18	5	ND	7	35	1	2	2	1	1.31	.016	10	3	1.31	18	.01	3	.16	.01	.09	2	6
E 56469	1	16	3	44	.1	29	11	662	3.16	17	5	ND	4	48	1	2	2	1	1.16	.026	6	4	1.03	17	.01	3	.13	.01	.07	1	2
E 56470	1	16	18	41	.1	31	10	924	3.57	41	5	ND	8	20	1	2	4	1	.51	.019	11	4	.90	18	.01	2	.15	.01	.10	1	3
E 56471	1	13	2	20	.1	25	9	1251	3.55	27	5	ND	8	54	1	2	2	1	1.45	.017	11	3	1.10	12	.01	4	.11	.01	.08	1	29
E 56472	1	12	4	61	.2	24	13	3265	6.98	34	5	ND	9	58	1	2	2	1	1.36	.040	13	2	2.11	20	.01	2	.14	.01	.10	1	7
E 56473	1	7	7	37	.1	33	15	1889	4.42	63	5	ND	13	60	1	2	2	1	1.45	.037	23	3	1.59	25	.01	2	.20	.01	.14	1	1
E 56474	1	1	2	3	.1	3	1	348	.83	2	5	ND	4	63	1	2	2	1	1.08	.027	13	3	.36	15	.01	33	.04	.01	.02	1	4
E 56475	1	13	11	41	.3	26	9	1944	5.11	41	5	ND	9	132	1	2	2	1	3.48	.034	9	3	1.76	15	.01	3	.14	.01	.10	1	10
E 56476	1	17	19	54	.2	48	13	673	4.54	24	5	ND	6	60	1	2	2	6	1.98	.036	9	17	1.55	20	.01	5	1.10	.01	.09	1	6
E 56477	1	31	11	39	.3	30	9	552	2.98	58	5	ND	7	69	1	2	2	1	1.20	.023	7	5	.96	20	.01	2	.15	.01	.08	1	73
E 56478	1	17	2	20	.1	53	14	947	3.29	56	5	ND	8	52	1	2	2	1	1.40	.025	10	3	.94	27	.01	2	.19	.01	.12	1	6
STB C/AU-R	19	61	42	132	7.5	69	29	1061	4.05	40	21	8	40	47	18	17	20	60	.46	.087	39	61	.90	179	.06	32	1.90	.06	.14	12	520





**LEGEND**

- [1a] ARGILLACEOUS LIMESTONE  
Thinly laminated black limestone and black limy argillite grading to black phyllitic rock at base of unit. Well developed foliation (subparallel to bedding).
- [1b] BLACK LIMESTONE  
Massive medium grey to black limestone locally containing bleached segregations of white crystalline limestone.
- [1c] WHITE LIMESTONE  
Massive crystalline bleached limestone locally containing segregations of unaltered medium grey to black limestone.
- [1d] SILICIFIED LIMESTONE  
Massive crystalline bleached limestone with local segregations of quartz, and veinlets of quartz.
- [1e] SILICIFIED LIMESTONE BRECCIA  
Brecciated bleached crystalline limestone in silicified matrix.
- [2] CHLORITE SCHIST  
Thinly laminated well foliated, fine to medium grained dark green chlorite schist locally with accessory magnetite, and/or well developed kink bands.
- [3] CHLORITE SERICITE SCHIST  
Thinly laminated yellow-green schist with cleavage parallel to bedding.
- [4a] SERICITE SCHIST  
Very fine grained, thinly laminated, well foliated light grey green schist.
- [4b] SERICITIC QUARTZITE  
Fine grained, laminated, quartzitic siltstone containing at least thirty percent micaceous material.
- [4c] QUARTZITE  
Medium grained massive quartzite with less than thirty percent micaceous material.
- [5] MAFIC DYKES  
Fine grained green dykes locally containing pyroxene phenocrysts, minor olivine, and/or magnetite.

- [1c] QUARTZ VEINS  
No visible mineralization.
- [2] MINERALIZED QUARTZ VEINS  
Veins with sulphide mineralization.
- [3] REPLACEMENT MASS  
Gossanous boulders derived from typical replacement mineralization.
- [4] ARGILLITE  
Very fine grained thinly laminated argillite with well developed foliation.
- [5] GRAPHITIC ARGILLITE  
Fine grained thinly laminated, well foliated, graphitic argillite.

- [6] LIMESTONE, PHYLLITE, CHL. SCHIST, ARGILLITE
- [7] QUARTZITE, SERICITIC QUARTZITE

- CREL -
- RCA -
- TREN -
- ADIT
- BUILDING
- CLAIM POST
- CONTACT
- FAULT
- CLEAVAGE ATTITUDE
- BEDDING ATTITUDE
- MINOR FOLD AXIS
- FAULT ATTITUDE
- SAMPLE LOCATION
- 1987 DDH

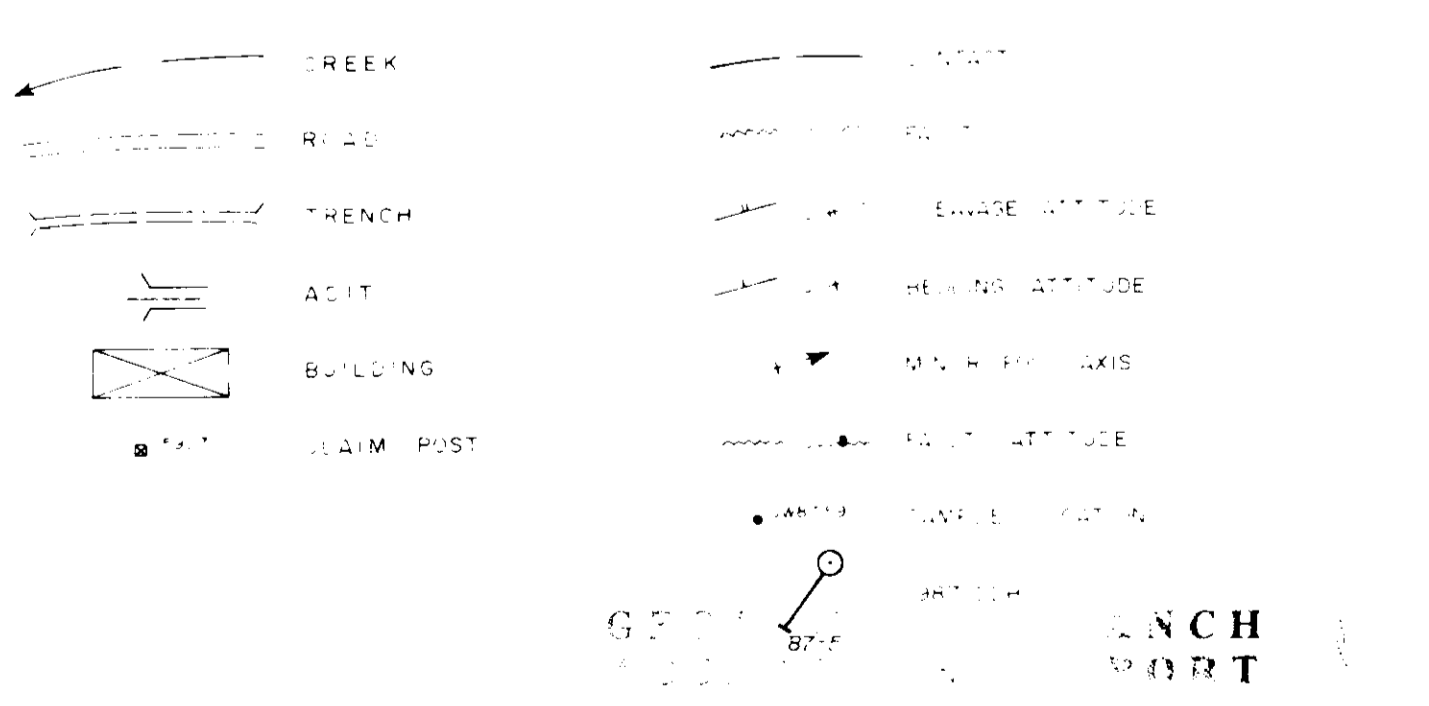
GEOLOGICAL BRANCH  
ASSIGNMENT REPORT

# 16,743

<b>CATHEDRAL GOLD CORPORATION</b>	
<b>CUNNINGHAM CREEK</b>	
FIGURE 5	N.T.S. 93-A/14W
<b>PROPERTY GEOLOGY</b>	
SCALE 1 : 5,000	GEOLOGIST P. DELANEY, J. WALKER
DATE FEBRUARY 1988	DRAWN BY G. I. B. O'S.



- LEGEND**
- 1.0 ARGILLACEOUS LIMESTONE  
Thinly laminated block limestone and block thin argillite grading to block phyllite rock at base of unit. Well developed fracton (subparallel to bedding).
  - 1.1 BLACK LIMESTONE  
Massive medium grained block limestone locally containing lenticled segregations of white crystalline limestone.
  - 1.2 WHITE LIMESTONE  
Massive crystalline block limestone locally containing segregations of unshaded medium grained block limestone.
  - 1.3 SILICIFIED LIMESTONE  
Massive crystalline block limestone with local segregations of quartz and lenses of quartz.
  - 1.4 LENTICLED LIMESTONE BRECCIA  
Brecciated block limestone limestone in crushed form.
  - 2.0 UNBLENDED SCHIST  
Thinly laminated well sorted fine to medium grained dark green chlorite schist locally with locally irregularly bedded well developed thin bands.
  - 2.1 UNBLENDED SERICITE SCHIST  
Thinly laminated well sorted schist with irregularly bedded.
  - 2.2 UNBLENDED SCHIST  
Very fine grained thin bedded well sorted dark green schist.
  - 2.3 SERICITIC QUARTZITE  
Fine grained, laminated, quartz to a matrix containing of well sorted, medium to coarse material.
  - 2.4 QUARTZITE  
Medium grained massive quartzite with well sorted, medium to coarse material.
  - 2.5 MOLT LAYERS  
Fine grained green layers with a laminating structure, translucent, yellow, white, and of magnetite.
  - 2.6 QUARTZ VEINS  
No visible mineralization.
  - 2.7 MINERALIZED QUARTZ VEINS  
Veins with sulphide mineralization.
  - 7 REPLACEMENT ZONATION  
Sedimentary boulders derived from typical replacement zones.
  - 8.0 ANGILITE  
Very fine grained thin bedded argillite with well developed thin bands.
  - 8.1 UNBLENDED ANGILITE  
Fine grained, thin bedded, well sorted, argillite.

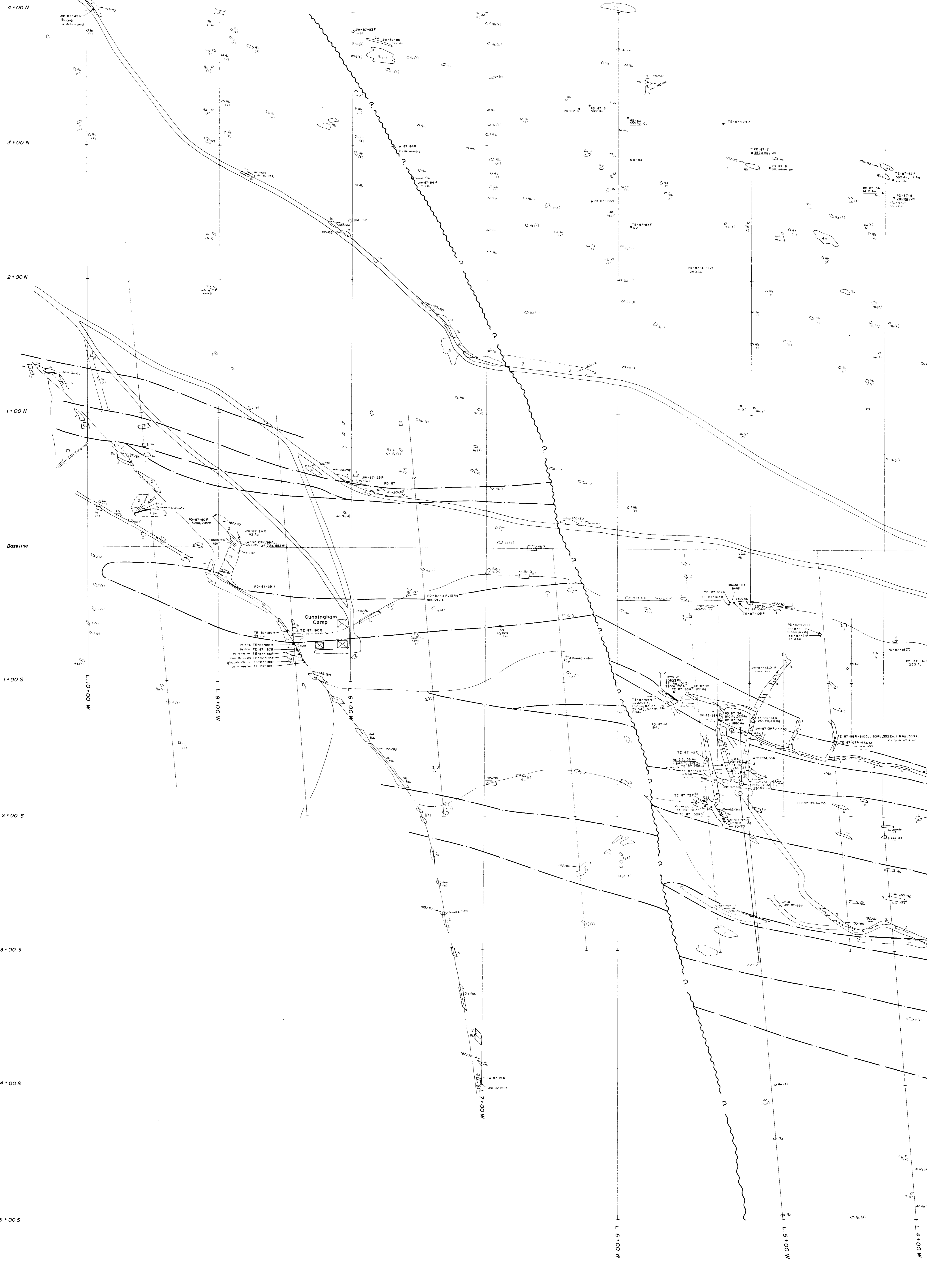


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**CATHEDRAL GOLD CORPORATION**  
**CUNNINGHAM CREEK**  
 FIGURE 9 - Main Grid; SE Area - NTS 93 A/14W  
**GEOLOGY & ROCK GEOCHEMISTRY**

SCALE 1:1,000  
 DATE FEBRUARY 1988  
 GEOLOGIST P. DELANEY, J. WALKER  
 DRAWN BY G. J. & J. W.





4+00 N  
3+00 N  
2+00 N  
1+00 N  
Baseline  
1+00 S  
2+00 S  
3+00 S  
4+00 S  
5+00 S

M 00+01 T

M 00+6 T

M 00+9 T

L 7+00 W

L 6+00 W

L 5+00 W

L 4+00 W

Cunningham Camp

MAGNETITE SAND

Summit cabin

TUNOSTER

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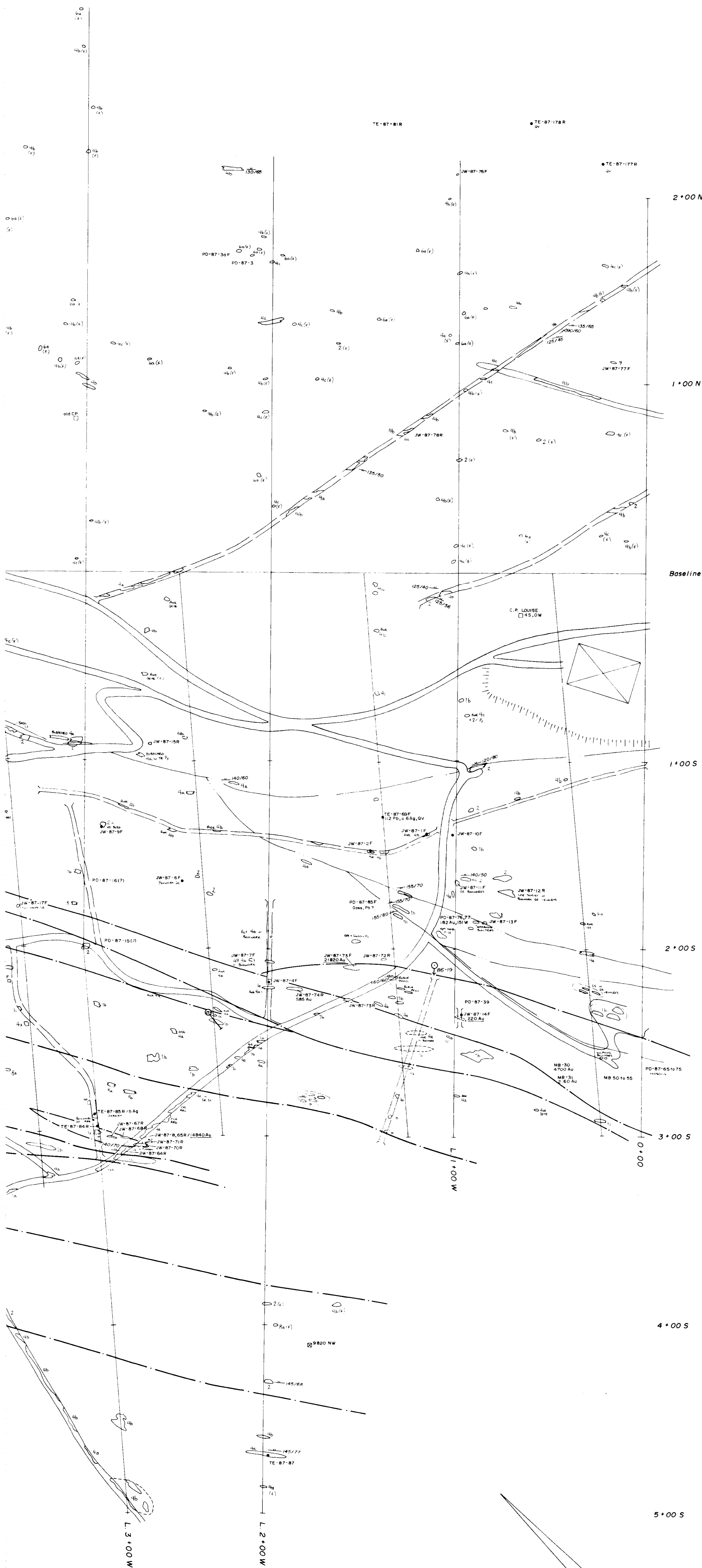
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**LEGEND**

- 1.2 ARTILLACEOUS LIMESTONE  
Thinly laminated black limestone and black limy argillite grading to black cherty rock at base of unit. Well developed fracture subparallel to bedding.
- 1.3 BLACK LIMESTONE  
Massive medium grey to black limestone locally containing bleached segregations of white crystalline limestone.
- 1.4 WHITE LIMESTONE  
Massive crystalline bleached limestone locally containing segregations of unaltered medium grey to black limestone.
- 1.5 SILICIFIED LIMESTONE  
Massive crystalline bleached limestone with local segregations of quartz, and veinlets of quartz.
- 1.6 CLIFFED LIMESTONE BRECCIA  
Brecciated bleached crystalline limestone in silicified matrix.
- 2 CHLORITE SCHIST  
Thinly laminated well foliated, fine to medium grained dark green chloritic schist locally with secondary magnetite, and/or well developed kink bands.
- 3 CHLORITE SERICITE SCHIST  
Thinly laminated yellow-green schist with cleavage parallel to bedding.
- 4a SERICITE SCHIST  
Very fine grained, thinly laminated, well foliated light grey green schist.
- 4b SERICITIC QUARTZITE  
Fine grained, laminated, quartzitic siltstone containing at least thirty percent micaceous material.
- 4c QUARTZITE  
Medium grained massive quartzite with less than thirty percent micaceous material.
- 5 MAFIC DYKES  
Fine grained green dykes locally containing pyroxene phenocrysts, minor biotite, and/or magnetite.
- 5a QUARTZ VENS  
No visible mineralization.
- 5b MINERALIZED QUARTZ VENS  
Vens with sulphide mineralization.
- 7 REPLACEMENT ZONING  
Sossaceous boulders derived from typical replacement mineralization.
- 8a ARGILLITE  
Very fine grained thinly laminated argillite with well developed foliation.
- 8b GRAPHITIC ARGILLITE  
Fine grained, thinly laminated, well foliated, graphitic argillite.

- CREEK
- CONTACT
- RCA
- FAULT
- TRENCH
- CLEAVAGE ATTITUDE
- ADIT
- BEDDING ATTITUDE
- BUILDING
- MINOR FOLD AXIS
- CLAM POST
- FAULT ATTITUDE
- SAMPLE LOCATION
- 1987 DQM

GEOLOGICAL BRANCH  
MINING DEPARTMENT

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<b>CATHEDRAL GOLD CORPORATION</b>	
<b>CUNNINGHAM CREEK</b>	
FIGURE 10 - Main Grid; Central Area -	N.T.S. 93-A/14W
<b>GEOLOGY &amp; <span style="border: 1px solid black; border-radius: 50%; padding: 2px;">3</span></b>	
<b>ROCK GEOCHEMISTRY</b>	
SCALE: 1 : 1,000	GEOLOGIST: P. DELANCEY, J. WALKER
DATE: FEBRUARY 1988	DRAWN BY: g.e.l. & o.s.s.



**LEGEND**

- 1a AMBULLEOUS LIMESTONE  
Thinly laminated black limestone and black limy argill. grading to black phyllitic rock at base of unit. Well developed foliation subparallel to bedding.
- 1b BLACK LIMESTONE  
Massive medium grey to black limestone locally containing bleached segregations of white crystalline limestone.
- 1c WHITE LIMESTONE  
Massive crystalline bleached limestone locally containing segregations of unaltered medium grey to black limestone.
- 1d SLICIFIED LIMESTONE  
Massive crystalline bleached limestone with local segregations of quartz, and lenses of quartz.
- 2 SLICIFIED LIMESTONE BRECCIA  
Brecciated bleached crystalline limestone in slicified matrix.
- 2 CHLORITE SCHIST  
Thinly laminated well foliated, fine to medium grained dark green chloritic schist with accessory magnetite, and/or well developed kink bands.
- 3 CHLORITE SERICITE SCHIST  
Thinly laminated yellow-green schist with cleavage parallel to bedding.
- 4a SERICITE SCHIST  
Very fine grained, thinly laminated, well foliated light grey schist.
- 4b SERICITIC QUARTZITE  
Fine grained, laminated, quartzitic siltstone containing at least thirty percent micaceous material.
- 4c QUARTZITE  
Medium grained massive quartzite with less than thirty percent micaceous material.
- 5 MAFIC DYKES  
Fine grained green dykes locally containing pyroxene phenocrysts, minor pyrite, and/or magnetite. Probably includes basalt D.C.
- 6a QUARTZ VEINS  
To variable mineralization.
- 6b MINERALIZED QUARTZ VEINS  
Veins with sulphide mineralization.
- 7 REPLACEMENT GOSSAN  
Gossanous boulders derived from typical replacement mineralization.
- 8a ARGILLITE  
Very fine grained thinly laminated argillite with well developed foliation.
- 8b GRAPHITIC ARGILLITE  
Fine grained, thinly laminated, well foliated, graphitic argillite.

- CREEK
- ROAD
- TRENCH
- ADIT
- BUILDING
- CLAIM POST
- FLOAT
- CONTACT
- FAULT
- CLEAVAGE ATTITUDE
- BEDDING ATTITUDE
- MINOR FOLD AXIS
- FAULT ATTITUDE
- SAMPLE LOCATION

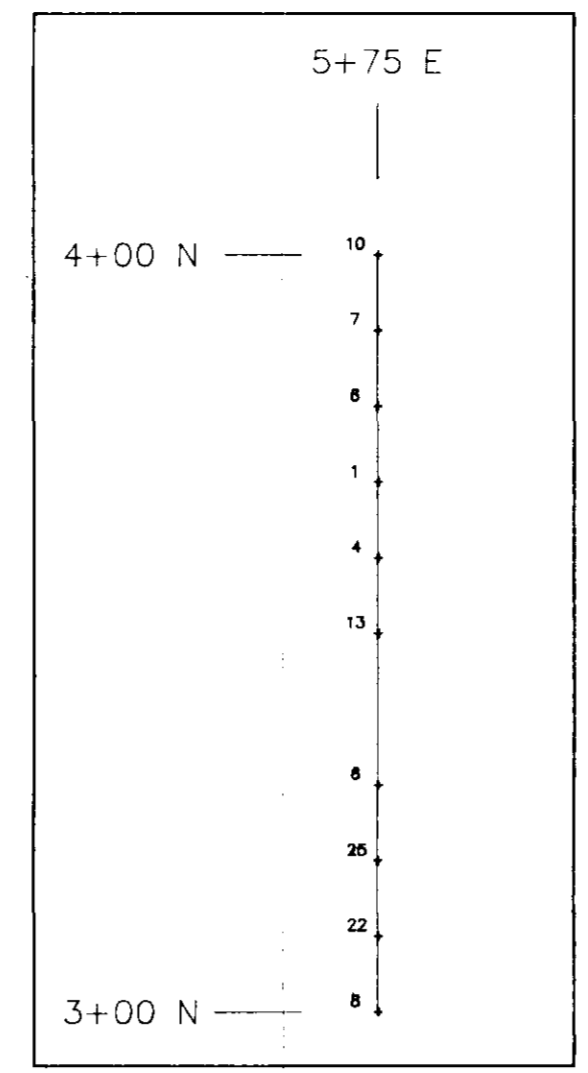
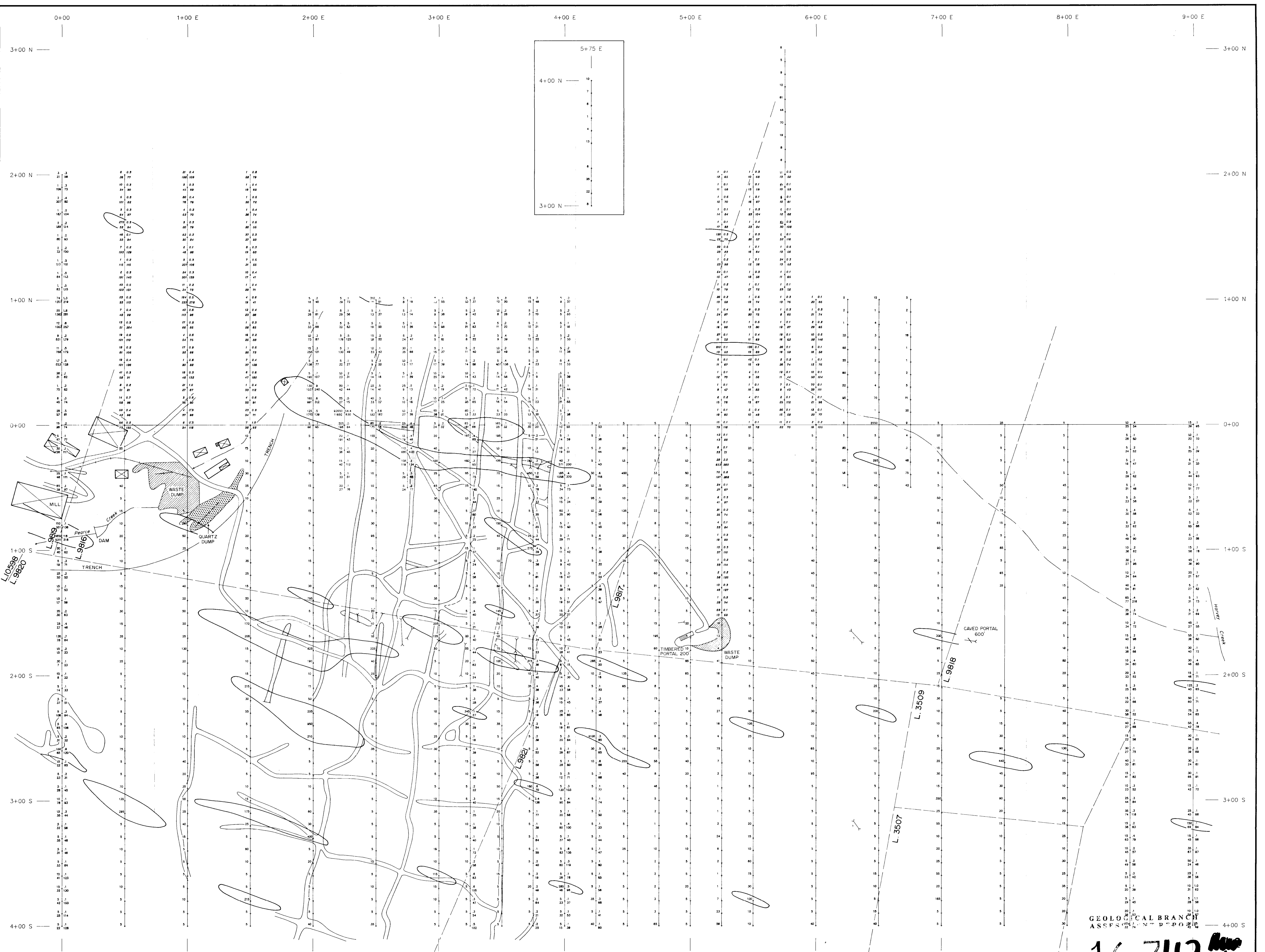
GEOLOGICAL BRANCH  
MINING DEPARTMENT REPORT

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CATHEDRAL GOLD CORPORATION  
CUNNINGHAM CREEK  
FIGURE 11 - Main Grid; NW Area - N.T.S. 93-A/14W  
**GEOLOGY & ROCK GEOCHEMISTRY**  
SCALE: 1:1,000  
DATE: FEBRUARY 1988  
GEOLOGIST: P. DELANEY, J. WALKER  
DRAWN BY: G.E.I. & G.S.S.







LEGEND

- Access Road/Reclaimed Trench
- Creek
- Building
- Railway Track
- Portal
- Trench
- Open Trench
- Soil Sample Line
- Au (ppb) | Ag (ppm)  
Pb (ppm) | Zn (ppm) Geochemistry, 1987
- Au (ppb) | Ag (ppm)  
Pb (ppm) | Zn (ppm) Geochemistry, pre-1987
- Au Value > 100 ppb

**GEOLOGICAL BRANCH**  
ASSESSMENT REPORT

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**CUNNINGHAM CREEK**

FIGURE 13 N.T.S. 93A/14

MAIN GRID (SOUTHEAST AREA)

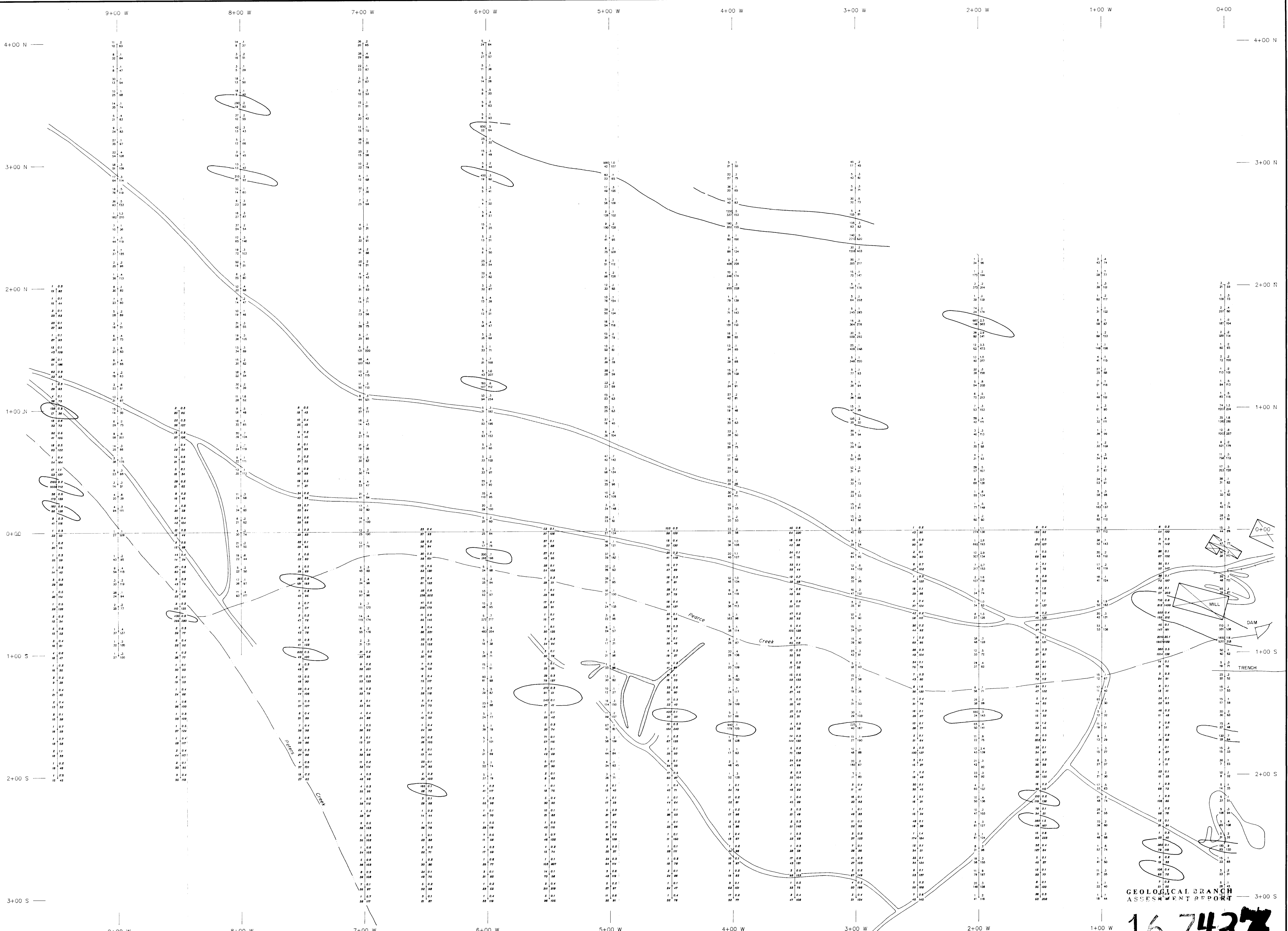
SOIL GEOCHEMISTRY

Metres 0 20 40 60 80 Metres

SCALE: 1:1000 GEOLOGIST: P. DELANCEY

DATE: FEBRUARY 1988 DRAWN BY: S. HAWORTH





LEGEND

	Access Road/Reclaimed Trench		Soil Sample Line
	Creek		Geochemistry, 1987
	Building		Geochemistry, pre-1987
	Railway Track		Au Value > 100 ppb
	Portal		
	Trench		
	Open Trench		

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

167437

CALHEDRA GOLD CORPORATION  
CUNNINGHAM CREEK

FIGURE 14 N.T.S. 93A/14

MAIN GRID (CENTRAL AREA) ⑦

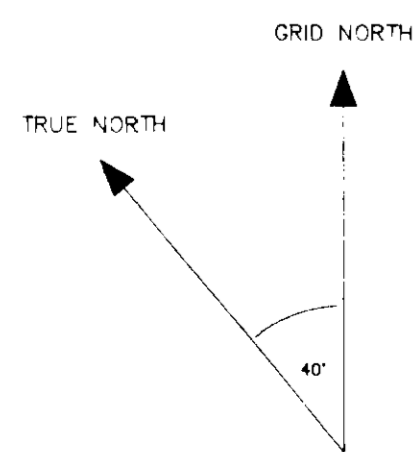
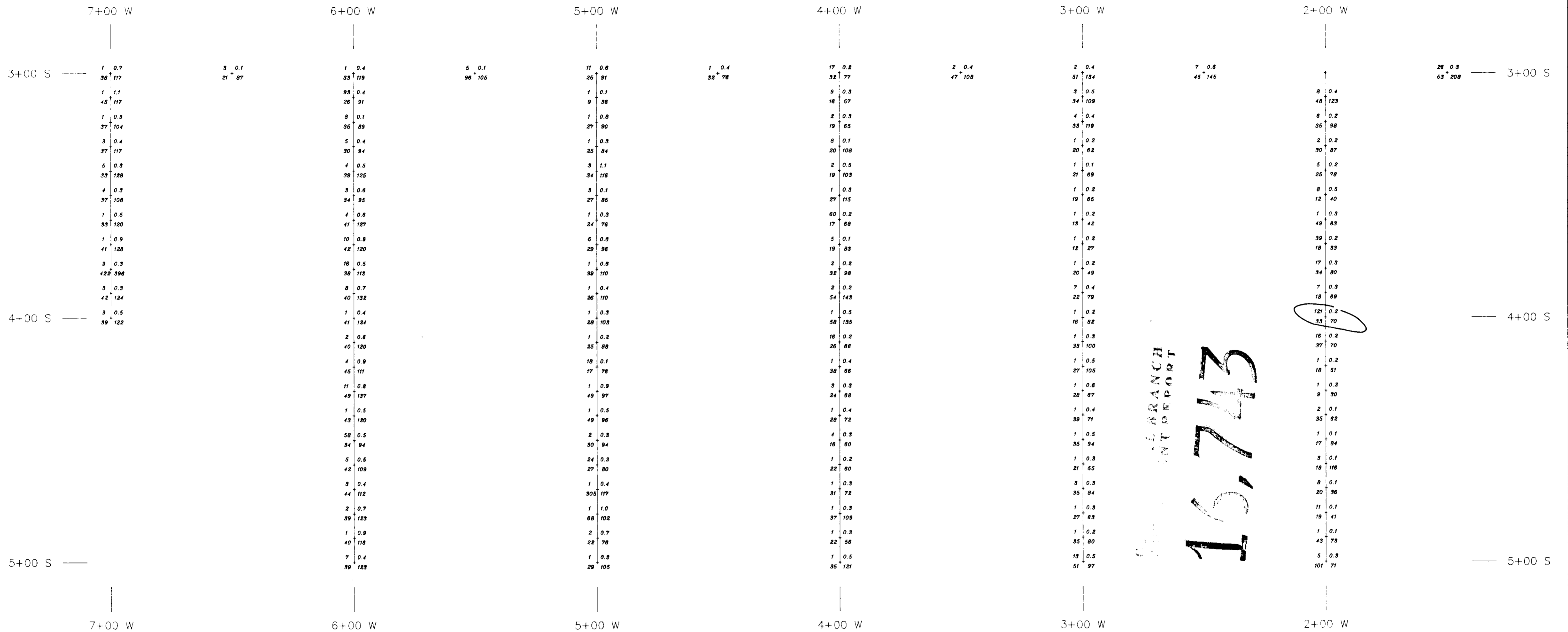
SOIL GEOCHEMISTRY

Metres 20 0 20 40 60 80 Metres

SCALE: 1:1000 GEOLOGIST: P. DELANEY

DATE: FEBRUARY 1998 DRAWN BY: S. HAWORTH





LEGEND

- Access Road/ Reclaimed Trench
- Creek
- Building
- Railway Track
- Portal
- Trench
- Open Trench
- Soil Sample Line
- |          |          |
|----------|----------|
| Au (ppb) | Ag (ppm) |
| Pb (ppm) | Zn (ppm) |

 Geochemistry, 1987
- |          |          |
|----------|----------|
| Au (ppb) | Ag (ppm) |
| Pb (ppm) | Zn (ppm) |

 Geochemistry, pre-1987
- Au Value > 100 ppb

CATHEDRAL GOLD CORPORATION  
CUNNINGHAM CREEK

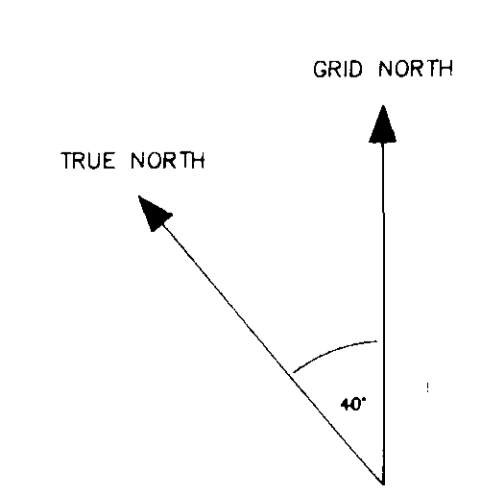
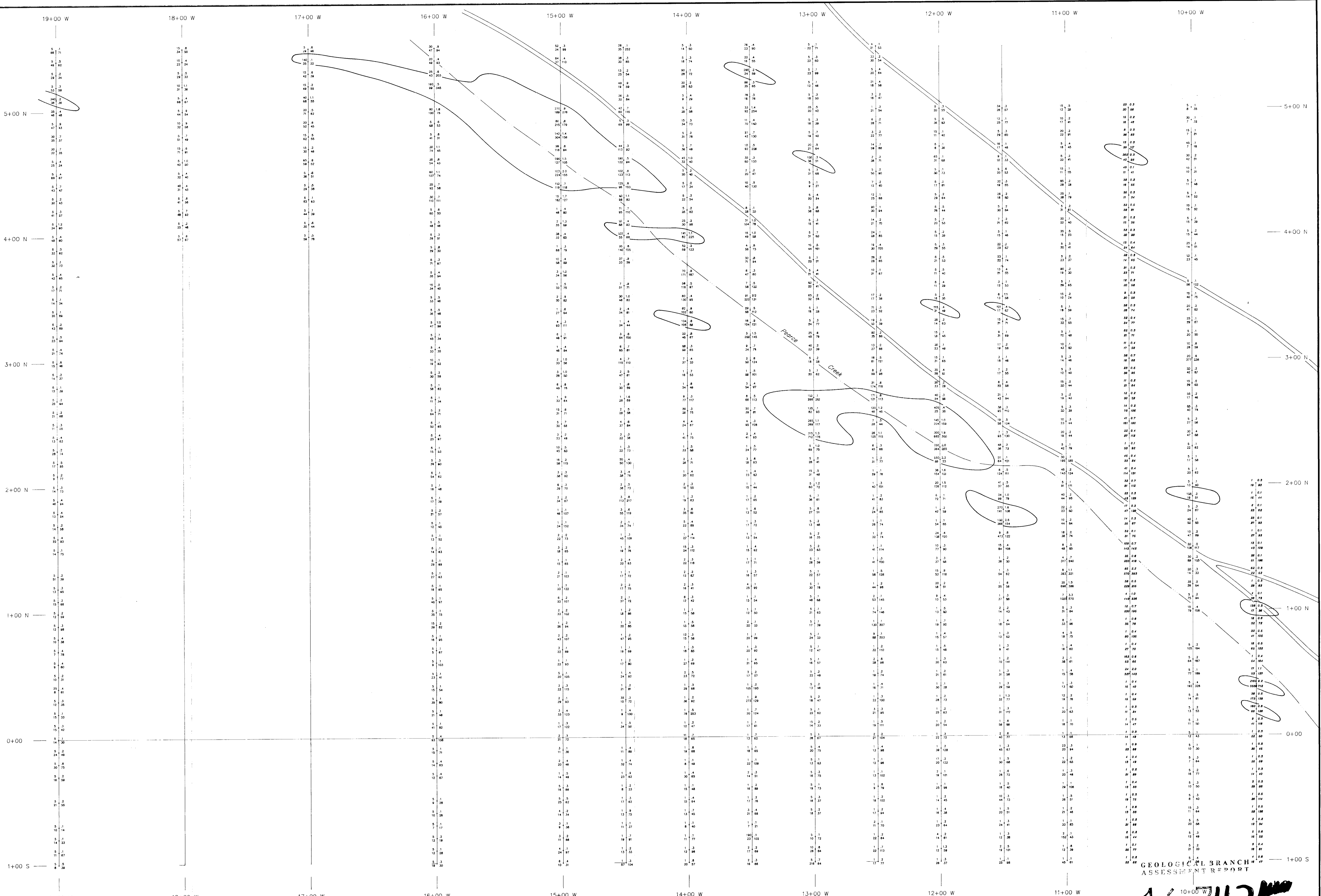
FIGURE 14a N.T.S. 93A/14

MAIN GRID (CENTRAL AREA - SOUTH)

SOIL GEOCHEMISTRY 8

Metres 20 0 20 40 60 80 Metres

SCALE: 1:1000	GEOLOGIST: P. DELANCEY
DATE: FEBRUARY 1988	DRAWN BY: S. HAWORTH



LEGEND

	Access Road/ Reclaimed Trench		Soil Sample Line
	Building		Geochemistry, 1987
	Railway Track		Geochemistry, pre-1987
	Partial		Au Value > 100 ppb
	Trench		
	Open Trench		

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

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CUNNINGHAM CREEK

FIGURE 15 N.T.S. 93A/14

MAIN GRID (NORTHWEST AREA) 9

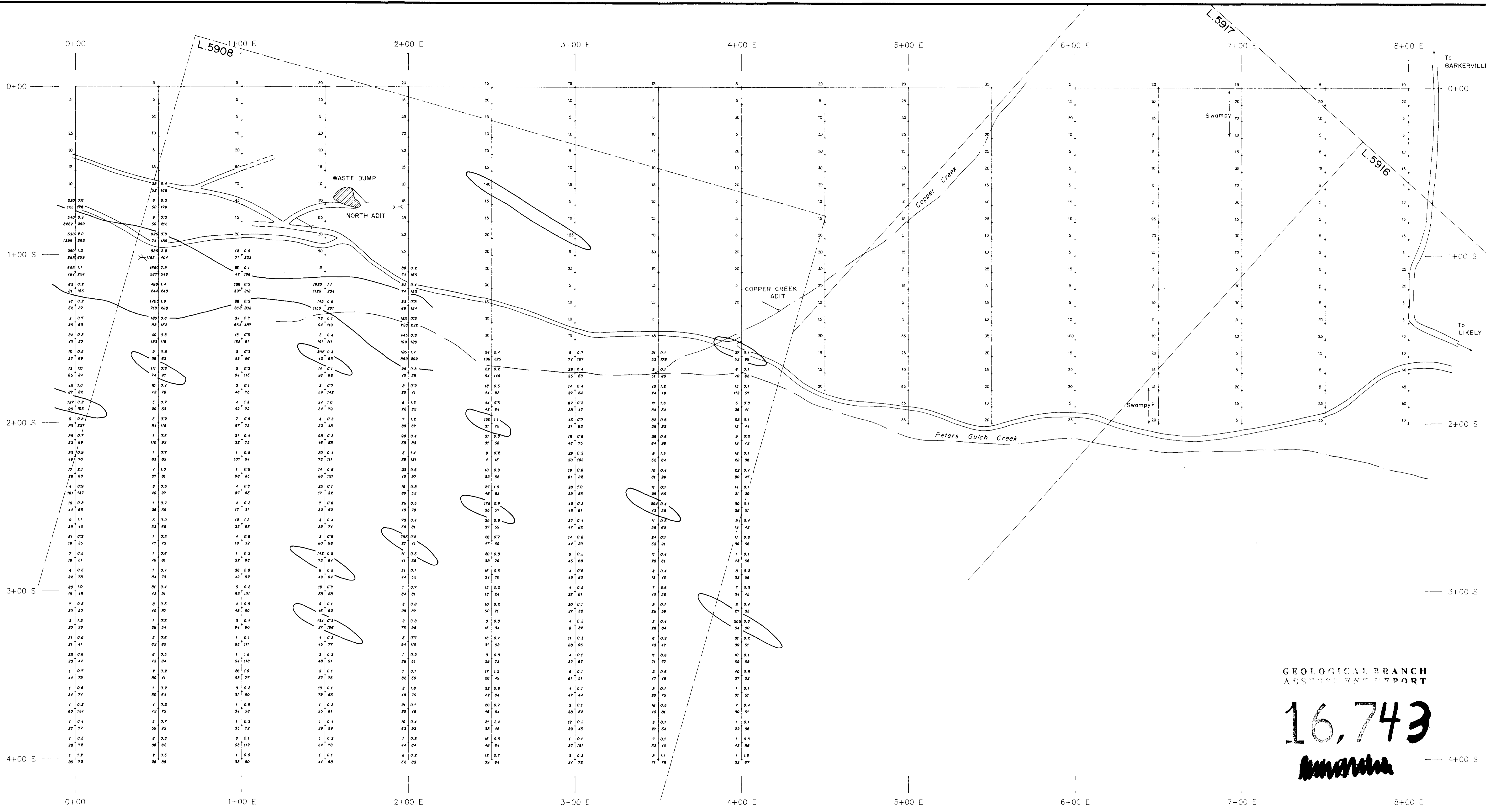
SOIL GEOCHEMISTRY

Metres 20 0 20 40 60 80 Metres

SCALE: 1:1000

DATE: FEBRUARY 1988

GEOLGIST: P. DELANCEY  
DRAWN BY: S. HAWORTH



GEOLOGICAL BRANCH  
ASSESSMENT REPORT

**16,743**  
*S. Haworth*

- LEGEND
- Access Road/Reclaimed Trench Creek
  - Building
  - Railway Track
  - Portal
  - Trench
  - Open Trench
  - Soil Sample Line
  - |          |          |                    |
|----------|----------|--------------------|
| Au (ppb) | Ag (ppm) | Geochemistry, 1987 |
| Pb (ppm) | Zn (ppm) |                    |
  - |          |          |                        |
|----------|----------|------------------------|
| Au (ppb) | Ag (ppm) | Geochemistry, pre-1987 |
| Pb (ppm) | Zn (ppm) |                        |
  - Au Value > 100 ppb

CATHEDRAL GOLD CORPORATION  
CUNNINGHAM CREEK

FIGURE 16 N.T.S. 93A/14

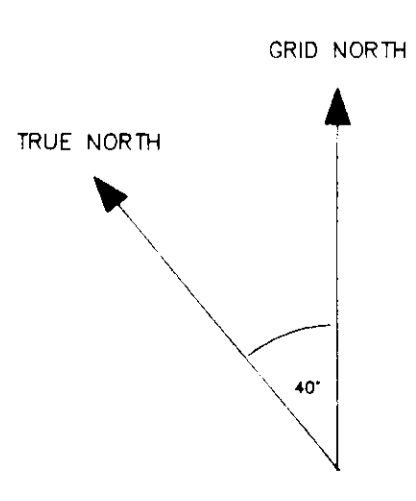
NORTH GRID (10)

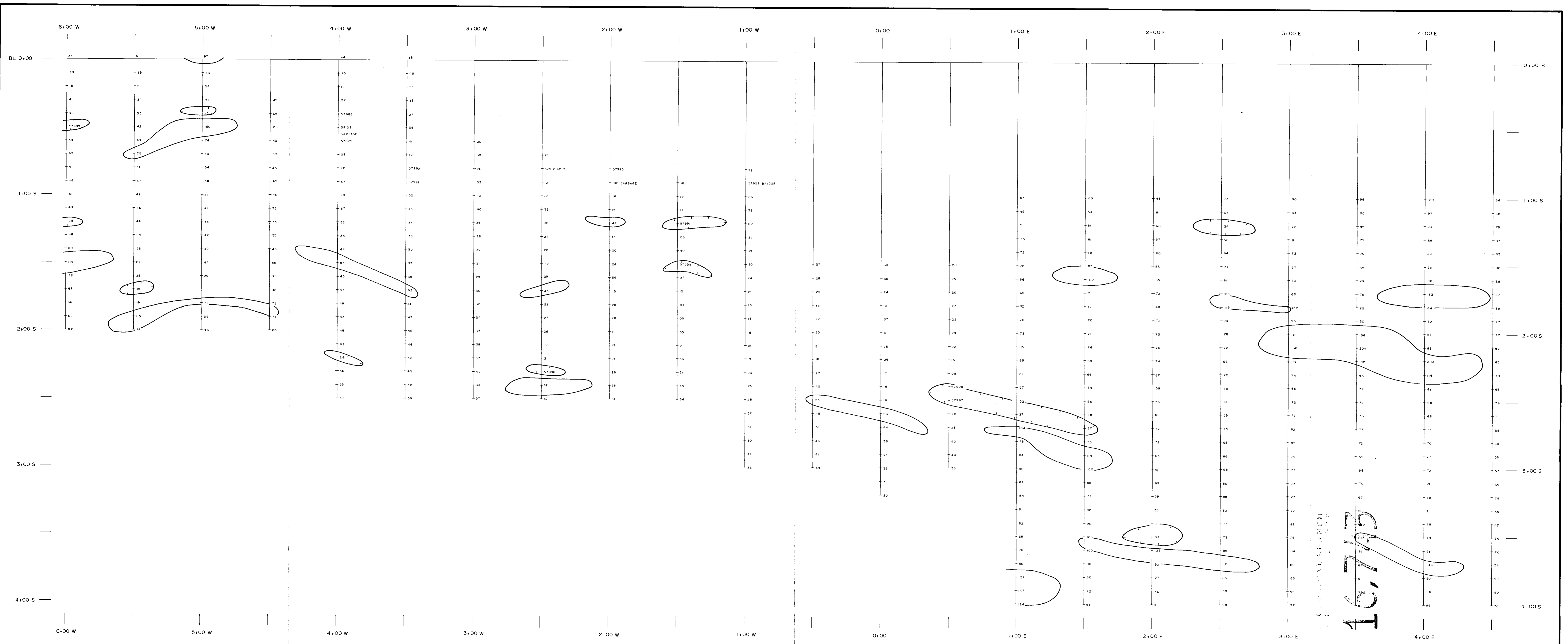
**SOIL GEOCHEMISTRY**

Metres 0 20 40 60 80 Metres



SCALE: 1:1000 GEOLOGIST: P. DELANCEY

DATE: FEBRUARY 1988 DRAWN BY: S. HAWORTH






**LEGEND**

-  Magnetic High
-  Magnetic Low

76 Gamma Reading  
 NB All readings are 580.0 unless otherwise noted.

**NOTES**  
 1. Compilation of several surveys. See individual maps for detail.  
 2. Instrument: Scintrex MP2  
 Geophysicist: B.T. Muloin

**CATHEDRAL GOLD CORPORATION**  
**CUNNINGHAM CREEK**  
 FIGURE 17 N.T.S. 93A/14W  
 MAIN GRID (SOUTHEAST & CENTRAL AREAS)   
 SUMMARY MAGNETOMETER SURVEY

Metres 25 0 25 50 75 Metres

SCALE: 1:1000  
 DATE: FEBRUARY 1988

GEOLOGIST: P. DELANCEY  
 DRAWN BY: S. HAWORTH

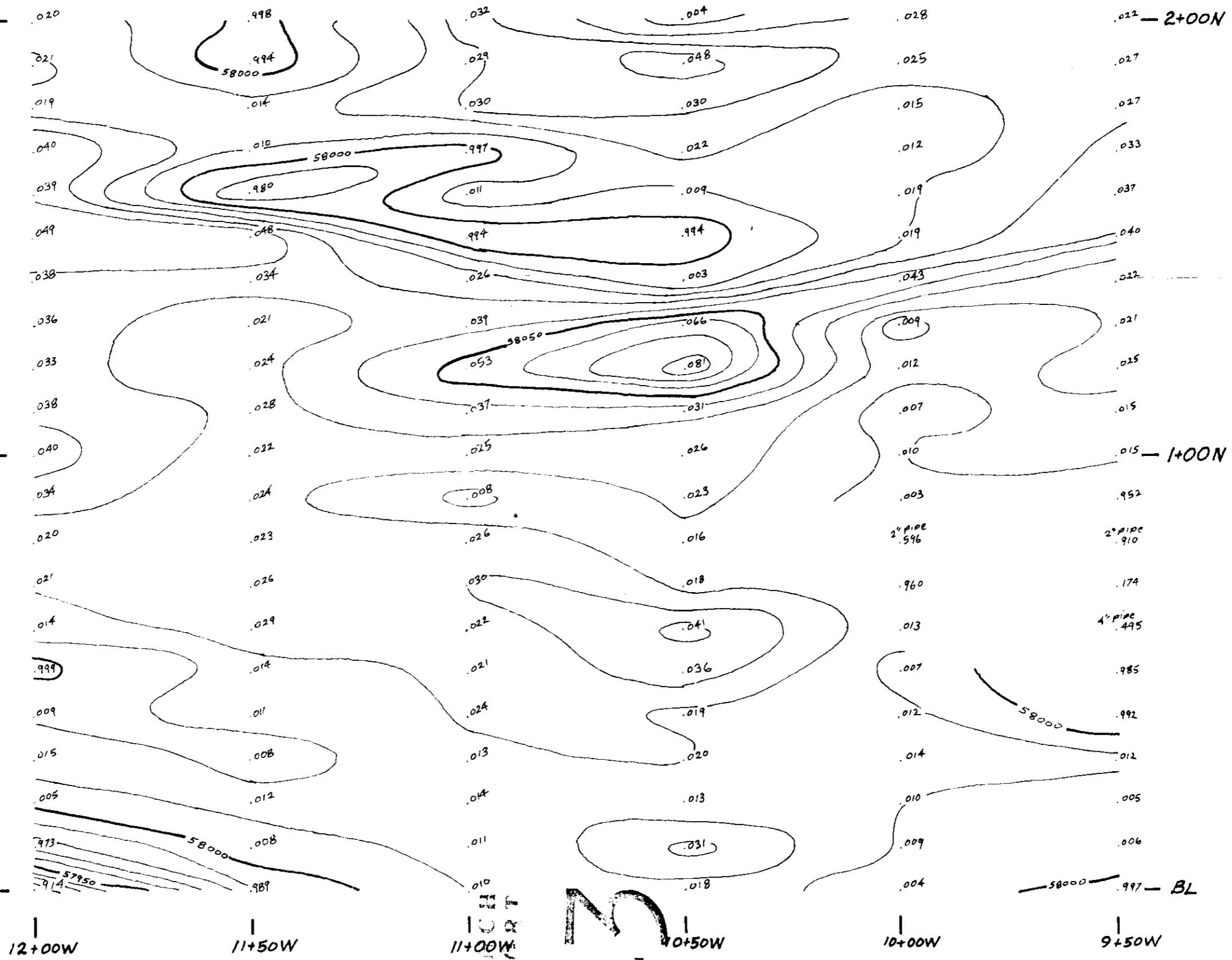
2+00N -

.022 - 2+00N

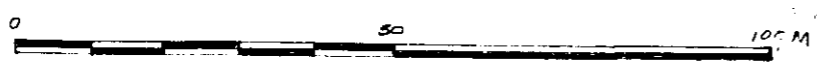
1+00N -

.015 - 1+00N

BL -



SULPHIDE



IMPERIAL METALS CORPORATION  
CUNNINGHAM CREEK  
FIGURE 18a  
MAGNETOMETER SURVEY

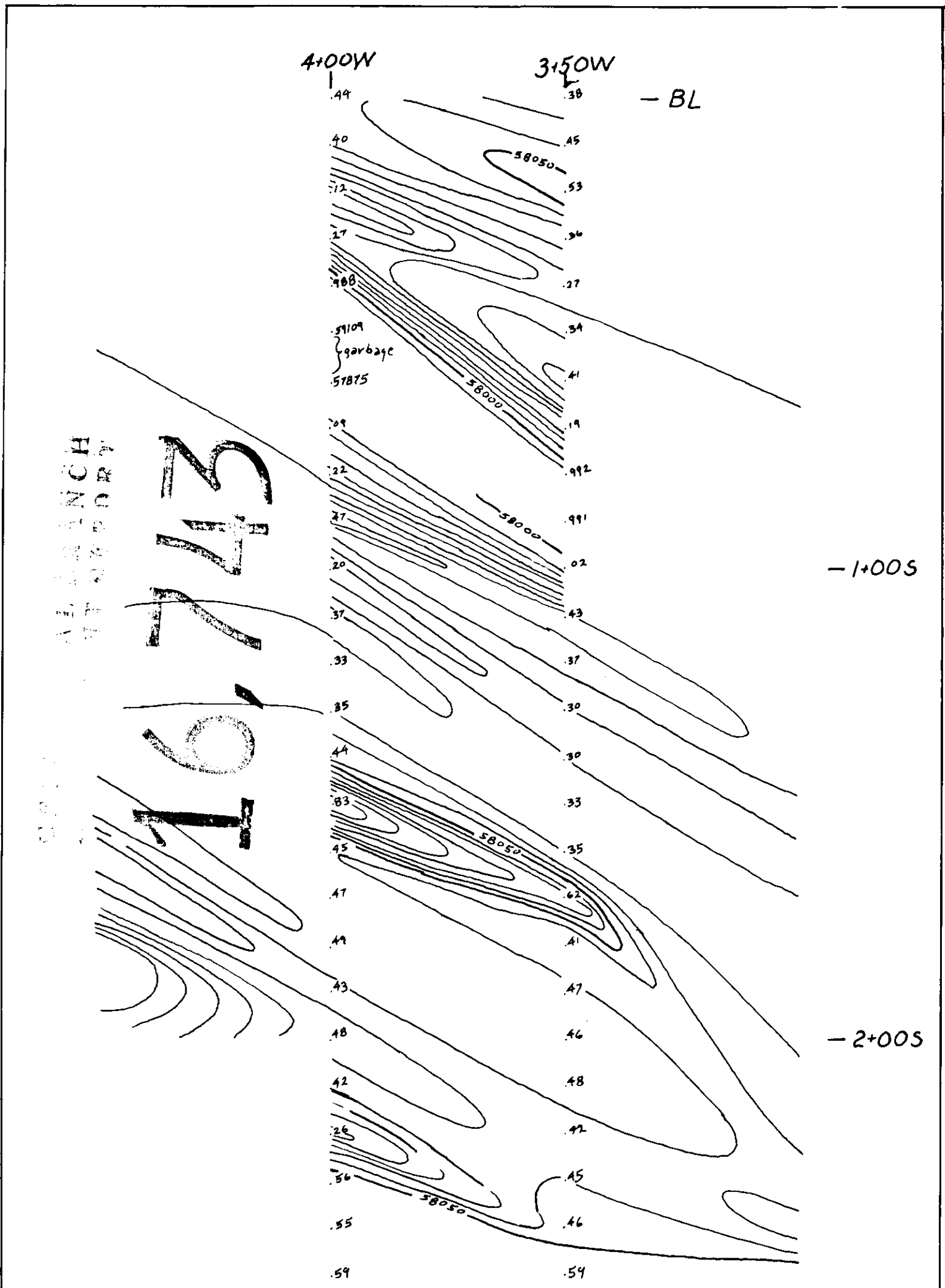
16712

IMPERIAL METALS CORPORATION  
 CUNNINGHAM CREEK  
 FIGURE 18a  
 N.T.S. 93A/14W  
 MAGNETOMETER SURVEY

12

INSTRUMENT: SCINTREX MP 2  
 SCALE: 1 : 1000  
 DATE: OCT, 1987  
 GEOPHYSICIST: B.T. MULOIN  
 DRAWN BY: B.T. MULOIN





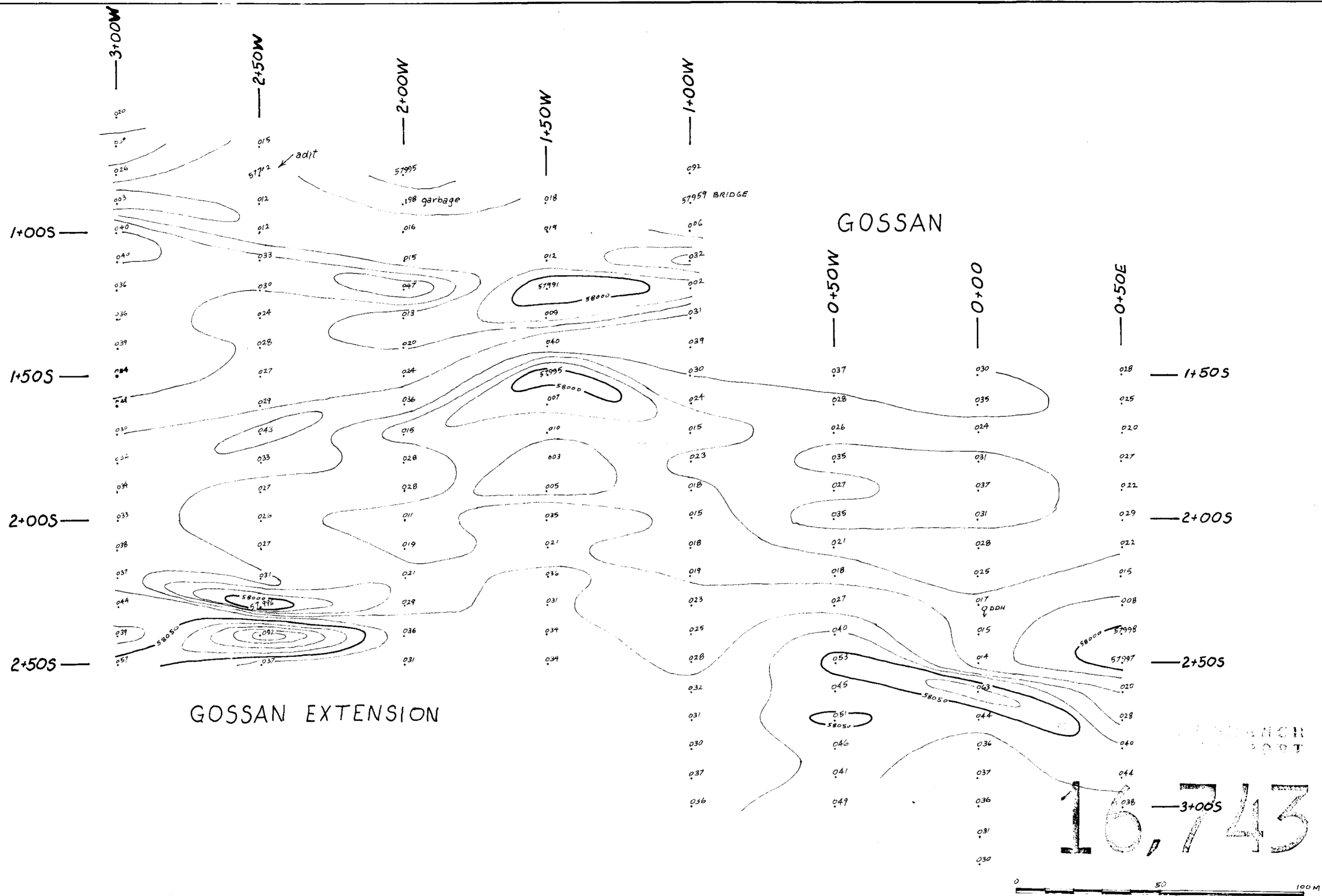
MAGNETOMETER SURVEY; MONETA-GOSSAN GAP

FIGURE 18c

14

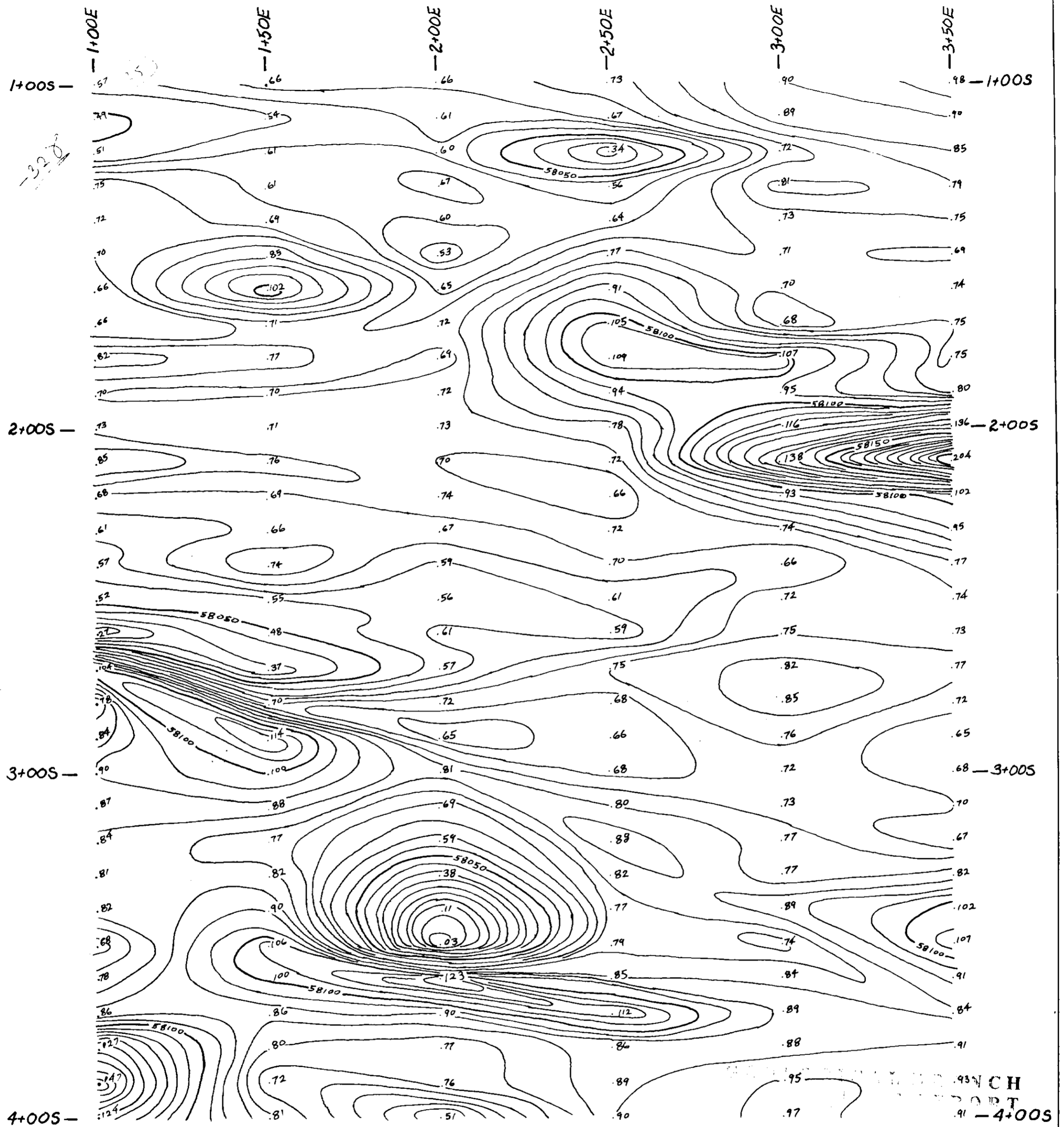
B.T. MULDOIN 10/87





IMPERIAL METALS CORPORATION  
 CUNNINGHAM CREEK  
 FIGURE 18d N.T.S. 93A/14W  
 MAGNETOMETER SURVEY  
 (15)  
 INSTRUMENT: SCINTREX MP2  
 SCALE: 1:1000 GEOPHYICIST: B.T. MULOIN  
 DATE: SEPT, 1987 DRAWN BY: B.T. MULOIN





South Gossan Extension

16,743



IMPERIAL METALS

Cunningham Creek  
Magnetometer Survey

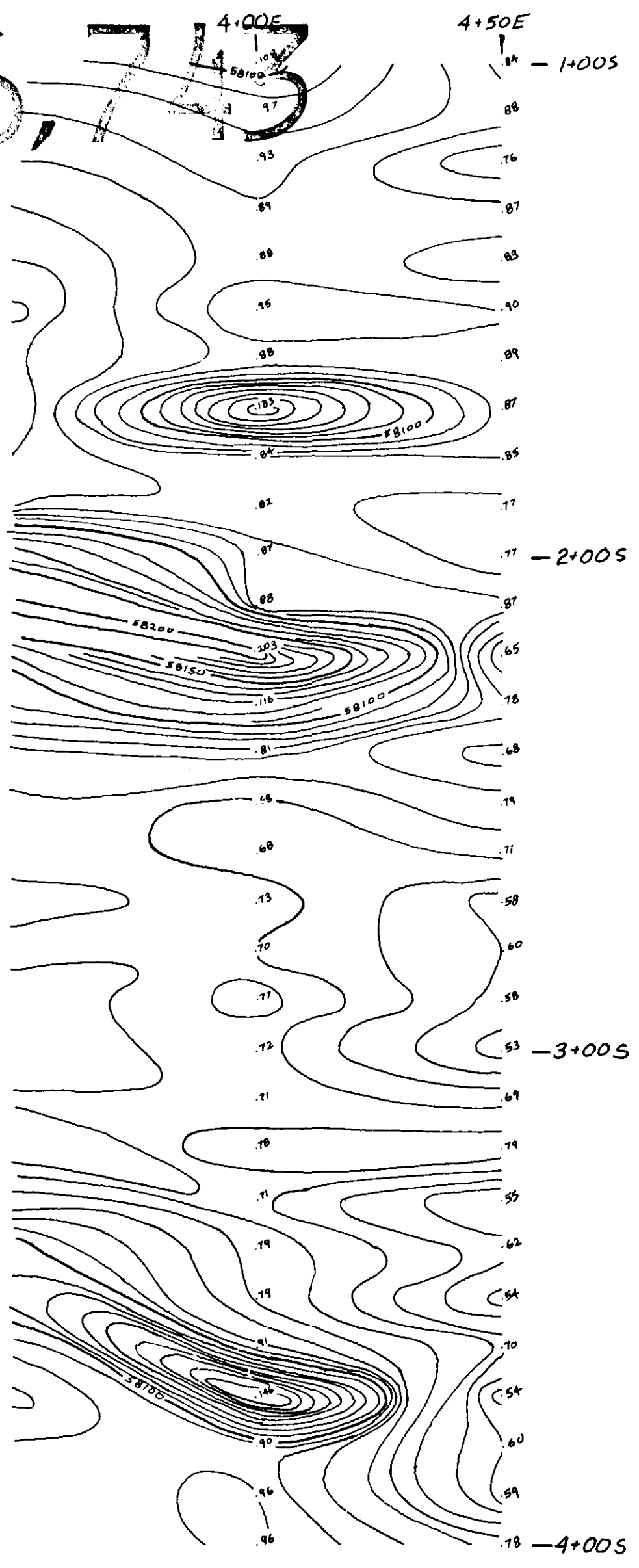
instrument: Scintrex MP2  
operator: Bryan T. Muloin B.Sc. B.Ed.

FIGURE 18e

16

10/87

16,743



SOUTH GOSSAN MAGNETOMETER SURVEY

FIGURE 18f

(17)

B.T.MULDIN  
10/87

elevation above m.s.l.  
(metres)

2+10 E, 1+80 S  
-45°/261°

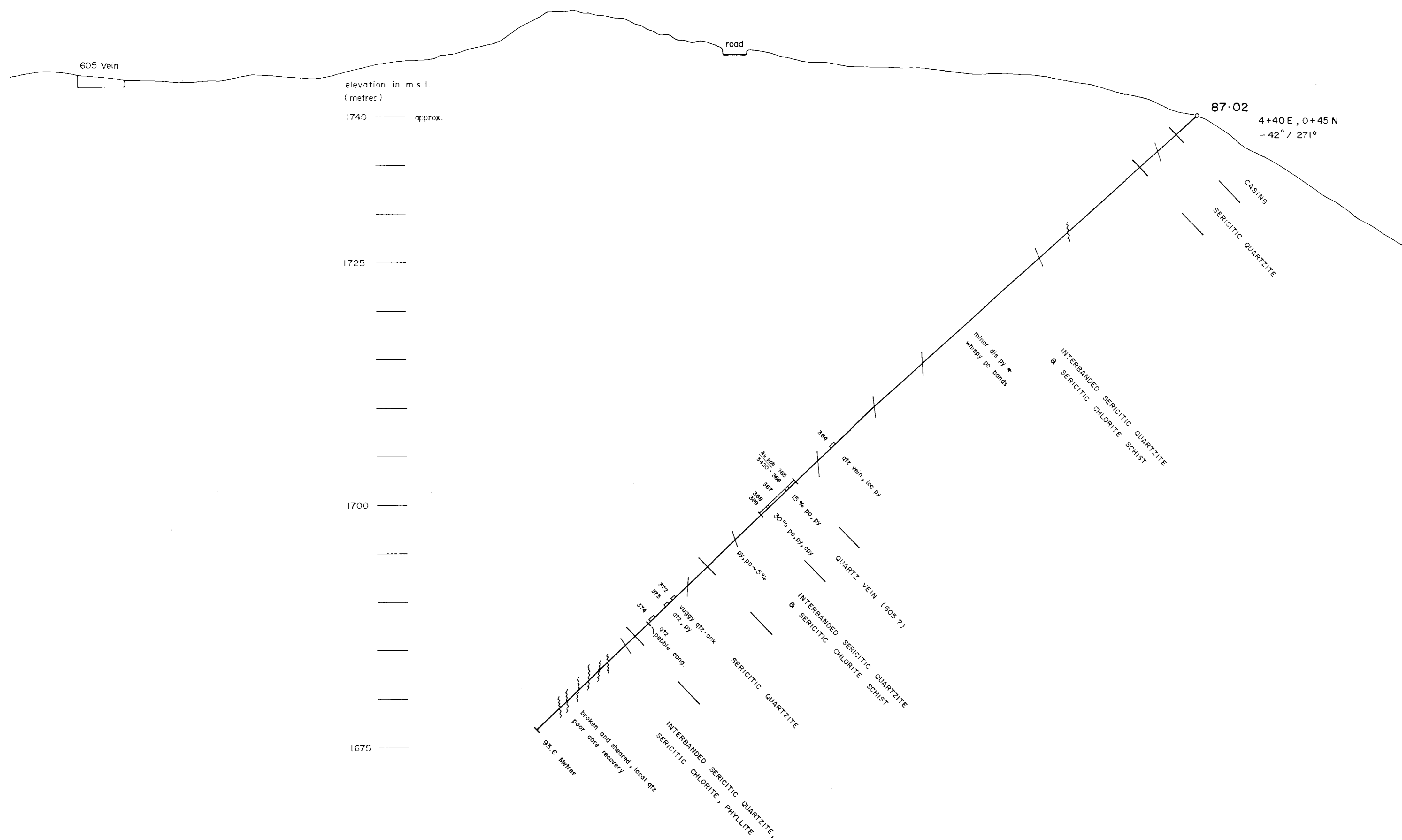


Fault or shear  
53478 Sample interval, assay tag #  
Angle of bedding or foliation to core axis (degrees)  
Geological contact

GEOLOGICAL BRANCH  
ASSIGNMENT REPORT

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CATHEDRAL GOLD CORPORATION	
CUNNINGHAM CREEK	
FIGURE 19	N.T.S. 93-A/14W
DDH 87-01 (18)	
5 0 5 10 15 20 Metres	
SCALE: 1:250	GEOLOGIST: P. DELANCEY / J. WALKER
DATE: FEBRUARY 1988	DRAWN BY: g.e.l.



- Fault or shear
- Sample interval, assay tag #
- Angle of bedding or foliation to core axis
- Geological contact

MINERAL SERVICES  
 1100 BAYVIEW AVENUE  
 SCARBOROUGH, ONTARIO M1S 5B7  
 TEL: (416) 291-1100  
 FAX: (416) 291-1101

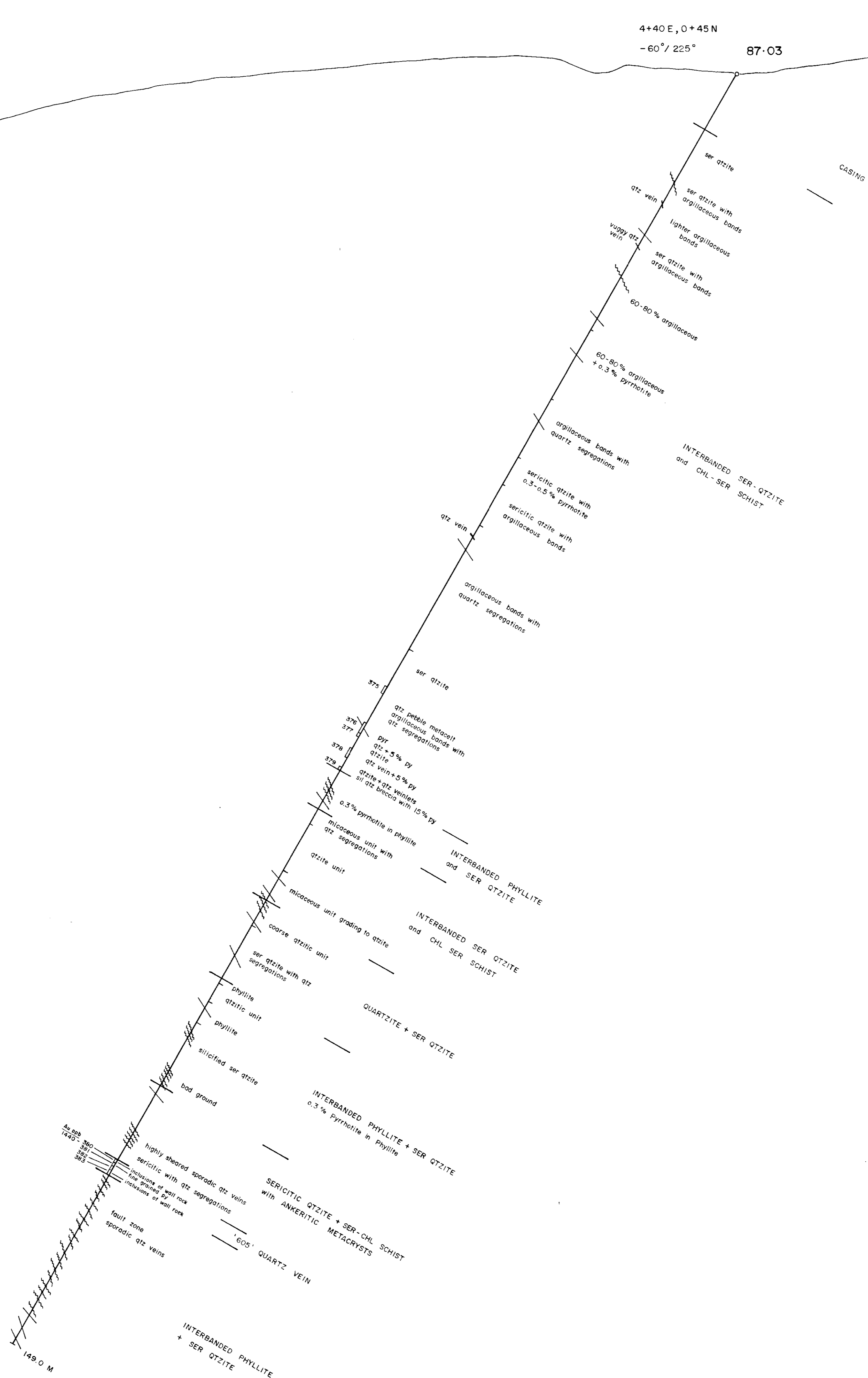
16,743

CATHEDRAL GOLD CORPORATION	
CUNNINGHAM CREEK	
FIGURE 20	N.T.S. 93-A/14W
DDH 87-02	
SCALE: 1:250	GEOLOGIST: P. DELANCEY / J. WALKER
DATE: FEBRUARY 1988	DRAWN BY: [Signature]

elevation above m.s.l.  
(metres)

1750  
1725  
1700  
1675  
1650  
1625

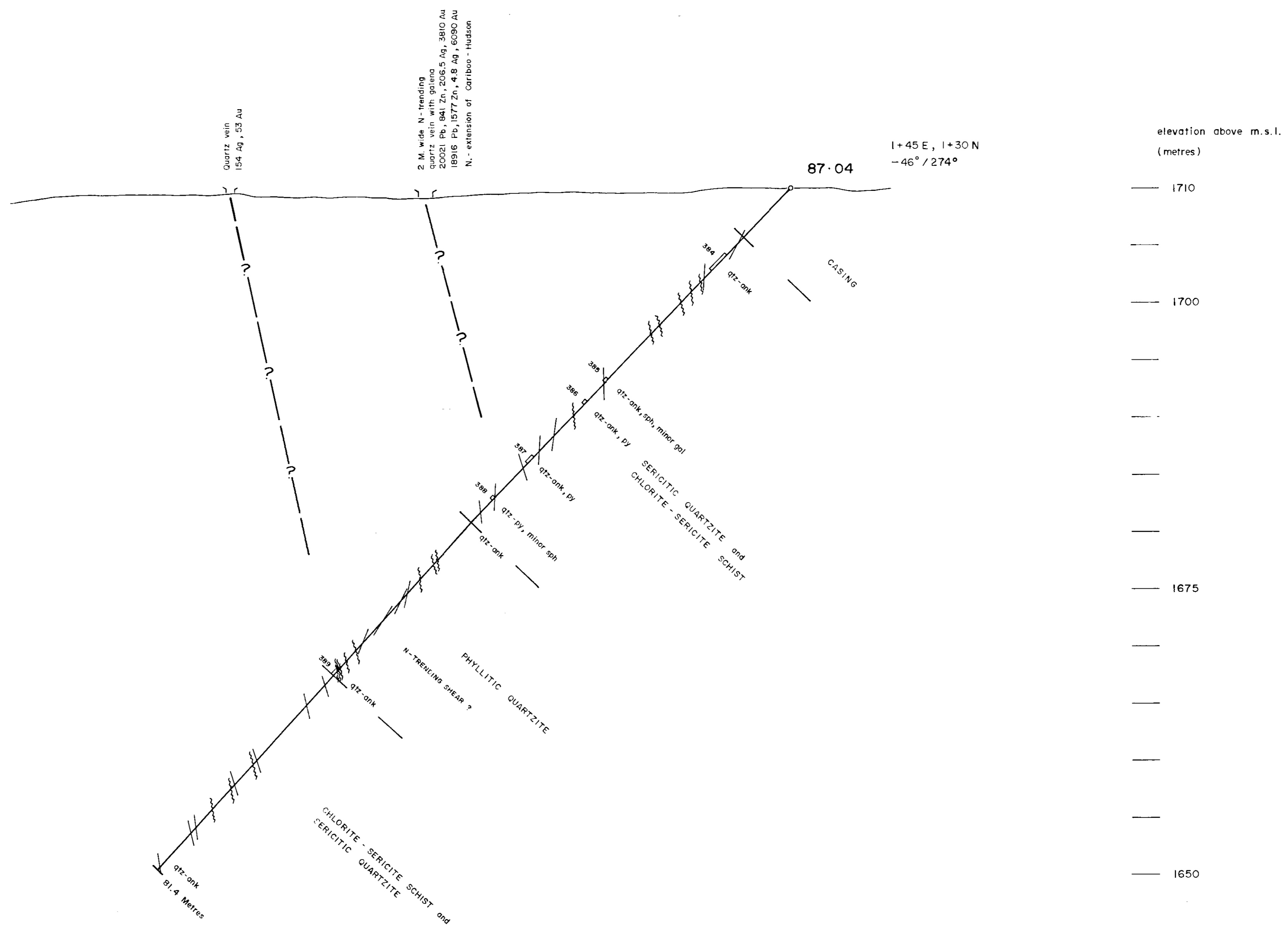
4+40 E, 0+45 N  
-60° / 225° 87-03



- Fault or shear
- 55478 Sample interval, assay tag #
- Angle of bedding or foliation to core axis
- Geological contact

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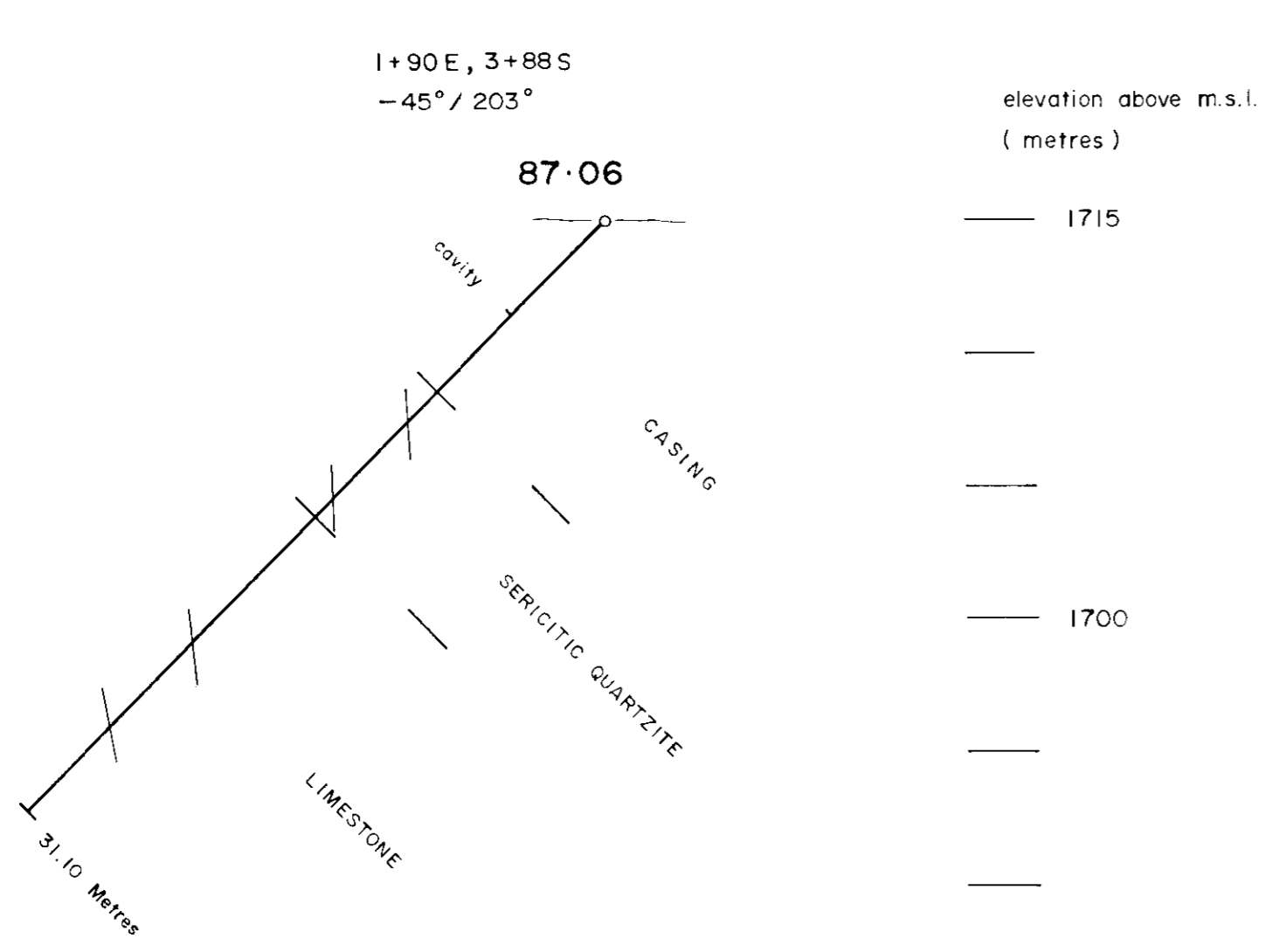
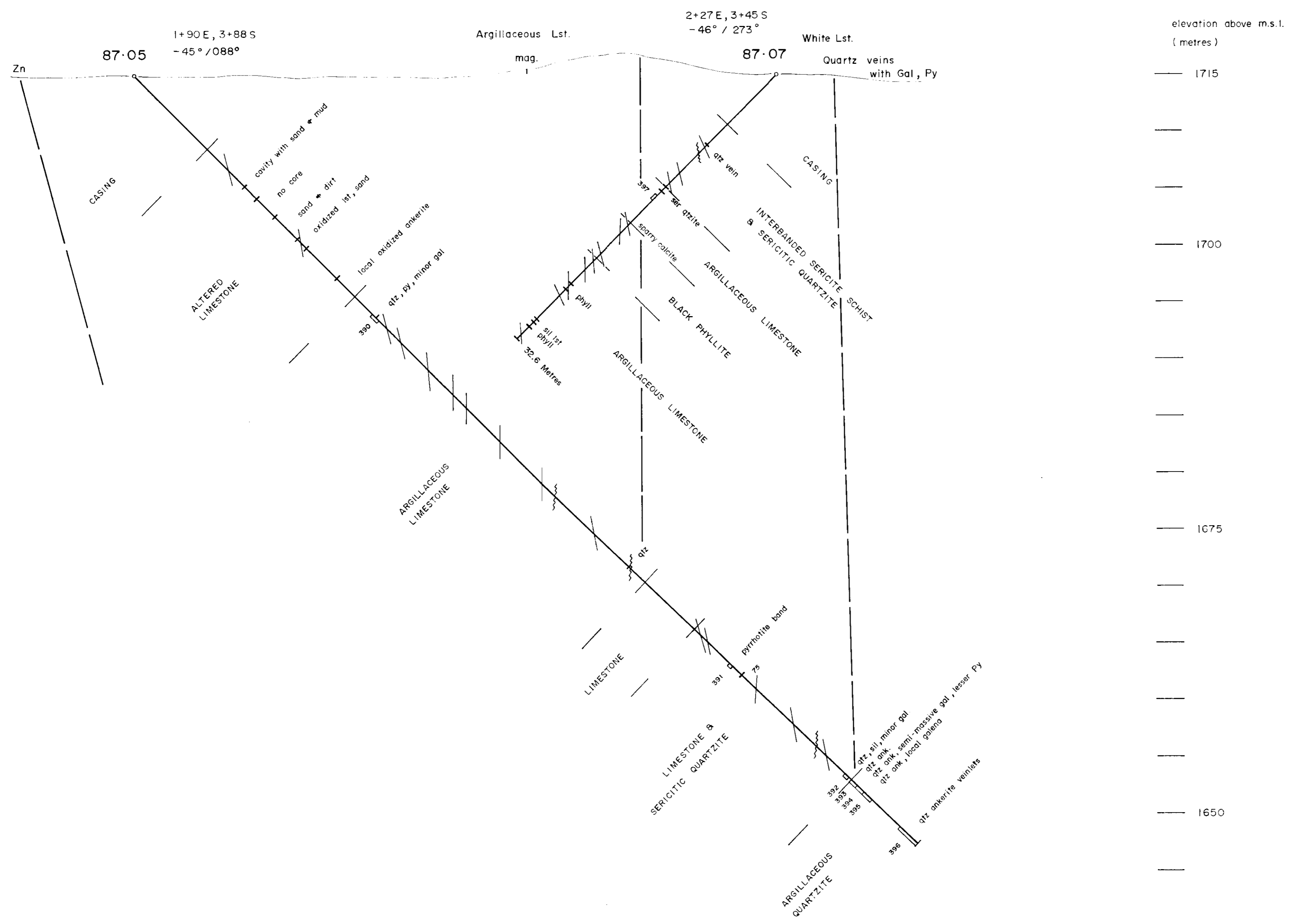
CATHEDRAL GOLD CORPORATION  
CUNNINGHAM CREEK  
FIGURE 21 N.T.S. 93-A/14W  
DDH 87-03 (20)  
SCALE: 1:250  
DATE: 1993  
GEOLOGIST: P. DELANCEY / J. WALKER  
DRAWN BY:



- Fault or shear
- Sample interval, assay tag #
- Angle of bedding or foliation to core axis
- Geological contact

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CATHEDRAL GOLD CORPORATION	
CUNNINGHAM CREEK	
FIGURE 22	N.T.S. 93-A/14W
DDH 87.04 <span style="border: 1px solid black; border-radius: 50%; padding: 2px;">21</span>	
SCALE: 1:250	GEOLOGIST: P. DELANCEY / J. WALKER
DATE: FEBRUARY 1988	DRAWN BY: g.e.l.



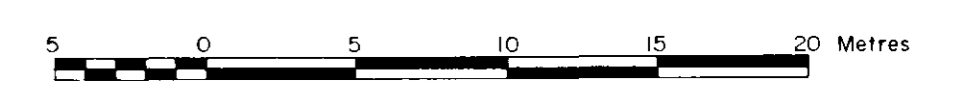
- Fault or shear
- Sample interval, assay tag #
- Angle of bedding or foliation to core axis
- Geological contact

16,743

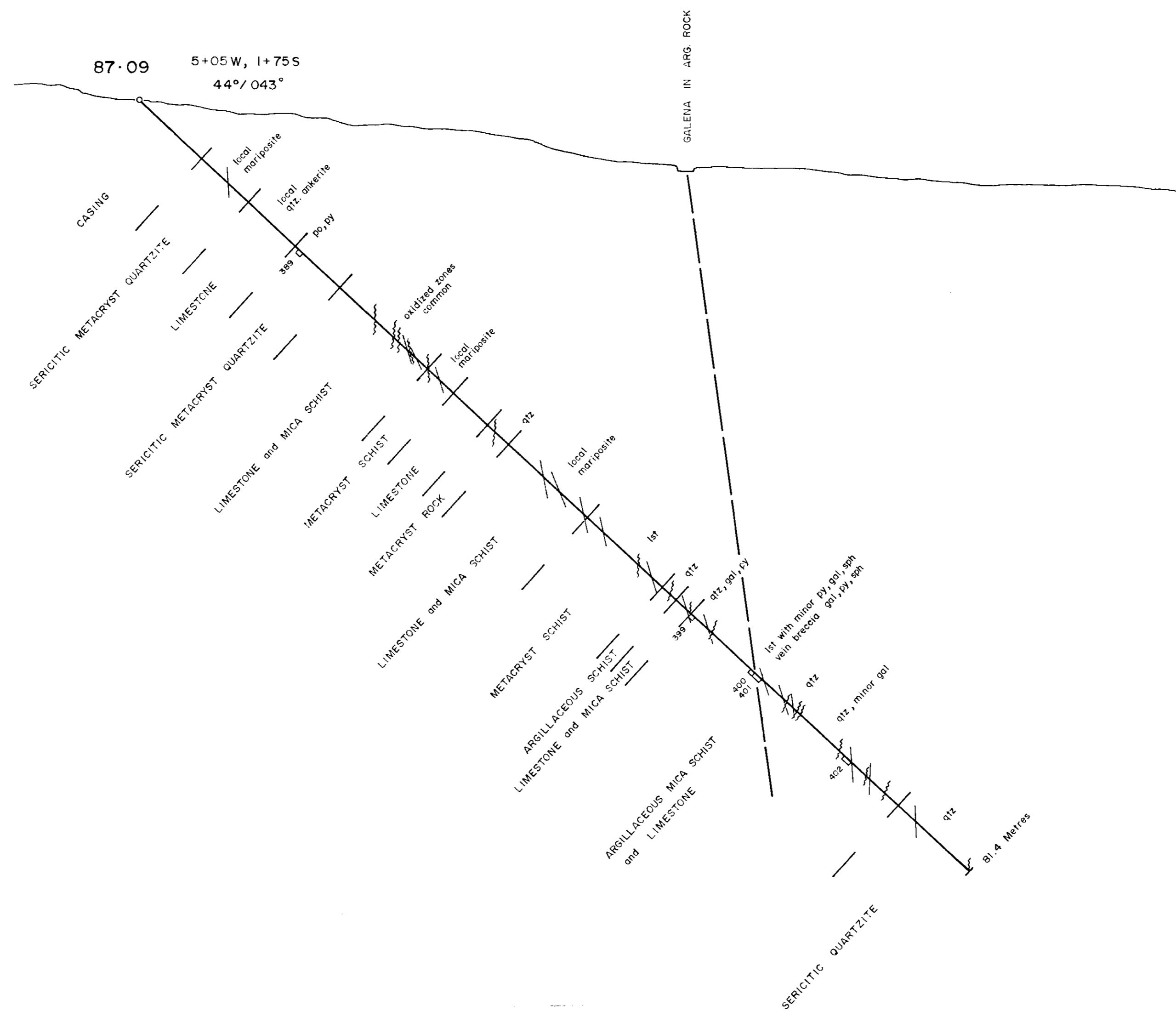
CATHEDRAL GOLD CORPORATION  
CUNNINGHAM CREEK

FIGURE 23 N.T.S. 93-A/14W

DDH's 87-05,06 + 07



SCALE: 1:250 GEOLOGIST: P. DELANCEY / J. WALKER  
DATE: FEBRUARY 1988 DRAWN BY: g.e.l.

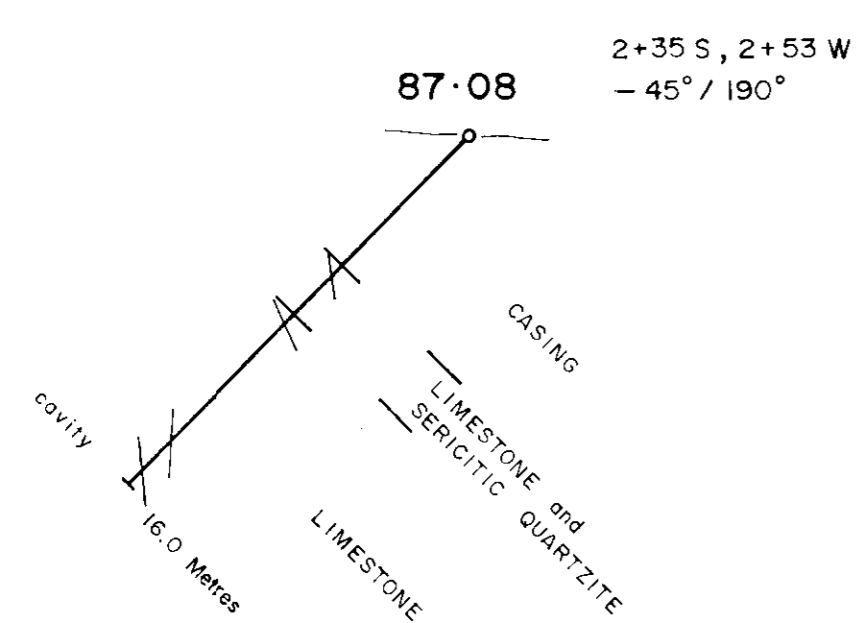


elevation above m.s.l.  
(metres)

1600

1575

1550



- Fault or shear
- Sample interval, assay tag #
- Angle of bedding or foliation to core axis
- Geological contact

GEOLOGICAL BRANCH  
MINING DEPARTMENT REPORT

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CATHEDRAL GOLD CORPORATION

CUNNINGHAM CREEK

FIGURE 24

N.T.S. 93-A/14W

DDH's 87-08,09

23

5 0 5 10 15 20 Metres

SCALE: 1 : 250

GEOLOGIST: P. DELANCEY / J. WALKER

DATE: FEBRUARY 1988

DRAWN BY: G.E.I.



elevation above m.s.l.  
(metres)



GEOLOGICAL BRANCH  
 REPORT  
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CATHEDRAL GOLD CORPORATION  
 CUNNINGHAM CREEK

FIGURE 25 N.T.S. 93-A/14 W

DDH's 87-10, 11 + 12

SCALE: 1:250

DATE: FEBRUARY 1988  
 GEOLOGIST: P. DELANEY / D. GORE  
 DRAWN BY: g.e.l.