

GEOLOGY AND GEOCHEMISTRY

on the

TEXADA ISLAND PROPERTY

Nanaimo Mining Division

N.T.S. 92F/10E, 15E

Latitude $49^{\circ} 41.5'$ to $49^{\circ} 46.0'$ N
Longitude 124 30.5' to 124 34.5' W

UTM 388500 E, 5509000 N
(centre of property)

by

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of

Nimbus Management Ltd.

for

Vananda Gold Ltd.

Vancouver, B.C.

February, 1988

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1.0 INTRODUCTION1.1 Location, Access and Topography

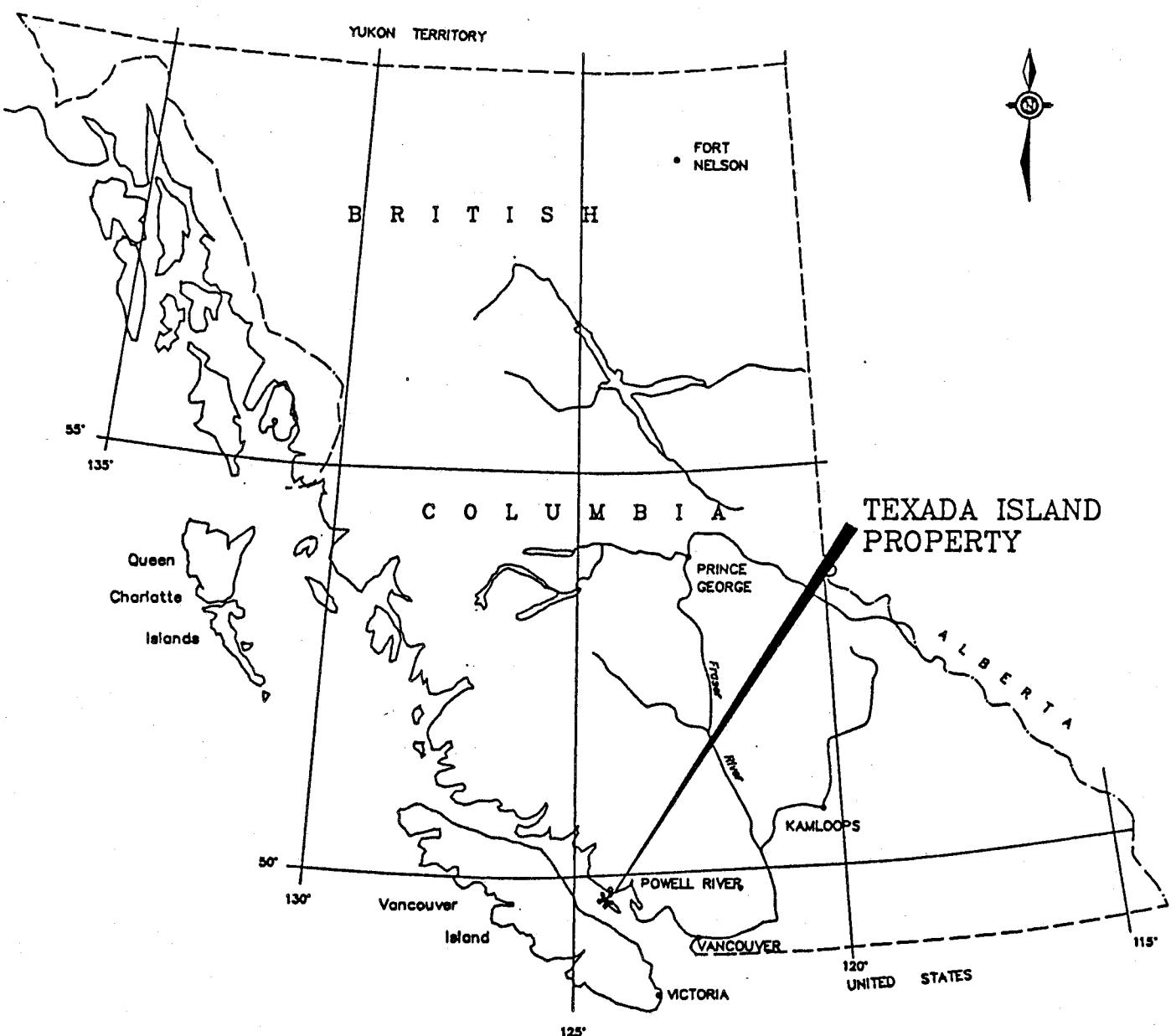
The TEXADA property is located between the villages of Vananda and Gillies Bay, on northern Texada Island, about 80 kilometres northwest of Vancouver (see Figure 1). Access is by highway and ferry to Powell River and then by ferry to Blubber Bay at the north end of the island. Scheduled flight service arrives at the airport at Gillies Bay. Numerous public and private roads provide ready access to most of the property.

Relief on the property is on the order of 250 metres. Forest cover is locally heavy, with considerable second growth. Much of the area of immediate interest lies within and adjacent to the settlement of Vananda, and has suffered some form of cultural disturbance.

1.2 Property Definition and History

The northern portion of Texada Island has been an important mining area, on an intermittent basis, since the late 19th century. The principal periods of activity were: between 1897 and 1919, during which time the gold-copper-silver skarn deposits at Vananda produced about 250,000 tonnes of high-grade ore; from 1948 to 1952, when one of these mines produced 58,000 tonnes of slightly lower grade ore; and from 1952 to 1976, when the large magnetite skarn deposits near Gillies Bay on the west side of the island produced some 10 million tonnes of iron concentrate with byproduct copper, gold and silver. The sites of all these former producers lie within the present Vananda Gold Ltd. property.

More recently apart from a few small programs there was little work in the Vananda Camp until 1970, when the latest phase of property assembly began. Serious ground work, consisting mostly of geophysics and diamond drilling, commenced in 1977, and has continued with some interruptions to the present.



(after Peatfield, 1987)

VANANDA GOLD LTD.

TEXADA ISLAND PROPERTY
NANAIMO, B.C.

LOCATION MAP

DATE: NOV. '86 N.T.S.: 92F/10E, 15E FIGURE: 1

Until the latest phase of work, commissioned by Vananda Gold Ltd., many of the programs were undertaken essentially in isolation, and results have not been compiled in any systematic way.

Prior to the start of the present program in May 1987, Vananda Gold completed: 1:2500 scale mapping of the Florence-Security area, establishment of control grids in strategic locations, collection of about 1300 soil samples of which about 490 were analyzed for Au and other elements. These results are detailed in Peatfield (1987).

1.3 Property and Claim Status

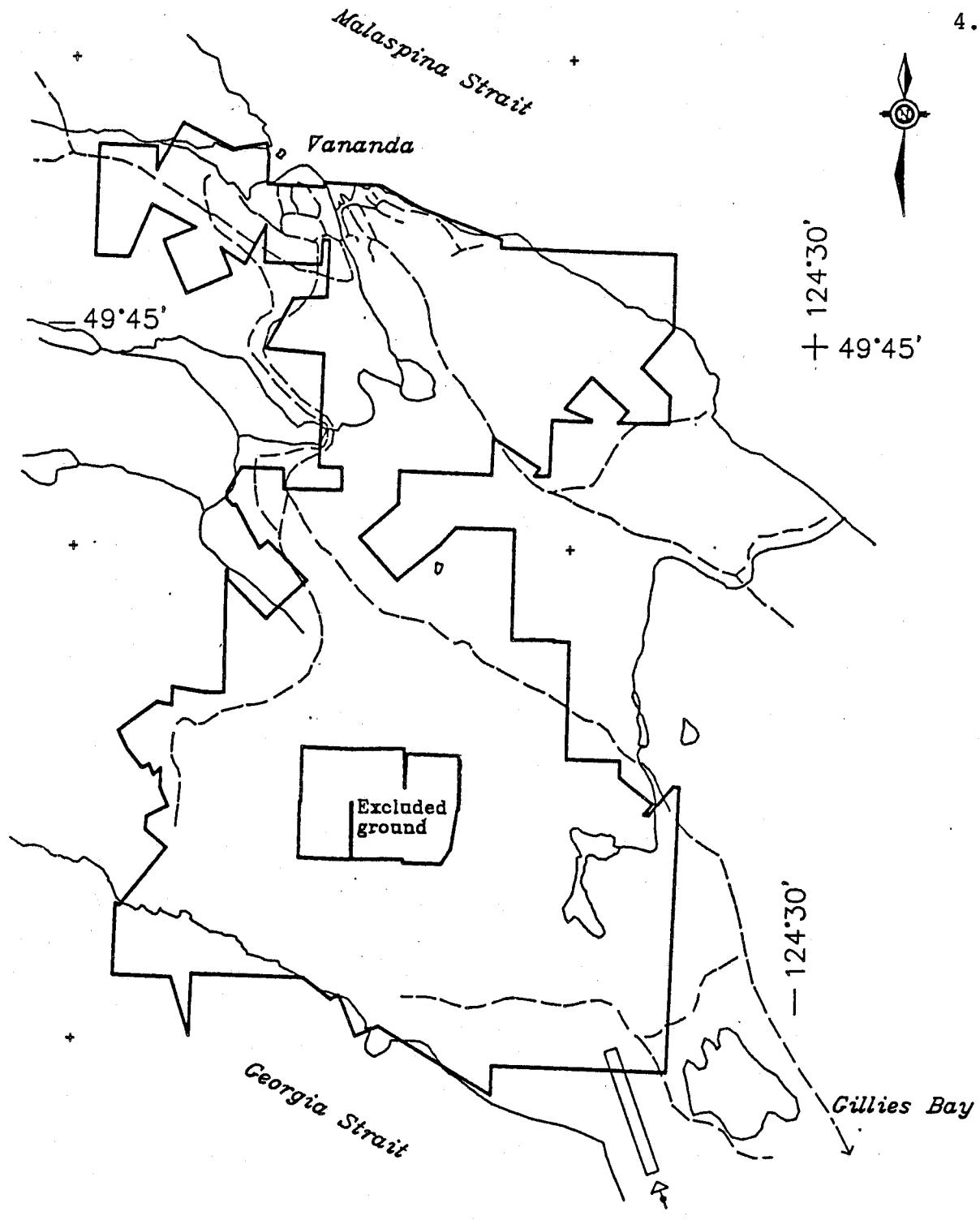
Texada Island is one of the oldest mining camps in the Province, and the property situation is very complex. For some claims separate ownership exists for base and precious metals, and this is complicated further by the presence of the limestone quarries, which do not hold their tenure under the terms of the Mineral Act.

Vananda Gold Ltd.'s property holdings on Texada Island consist of three small mining leases, 31 Crown Granted Claims or Fractional Claims, and 89 located (two post or modified grid) mineral claims or fractional mineral claims. Figure 2 shows a rough outline of the property but it is not based on any comprehensive recent survey and does not show the location of individual claims. Appendix II is a listing of the present property holdings derived from data in the possession of Vananda Gold Ltd.

1.4 Summary of Present Program

The present program consisted of the following: detailed mapping at 1:500 and 1:1000 scale of old showings and workings in the area of Little Billie and Cornell Mines, analysis of about 900 soil samples previously collected, trenching with subsequent 1:1000 and 1:100 scale mapping in the Florence/Security area, S.P. surveying in selected areas and diamond drilling in the area of Florence shaft.

4.



(after Peatfield, 1987)

VANANDA GOLD LTD.

TEXADA ISLAND PROPERTY
NANAIMO, B.C.

PROPERTY OUTLINE

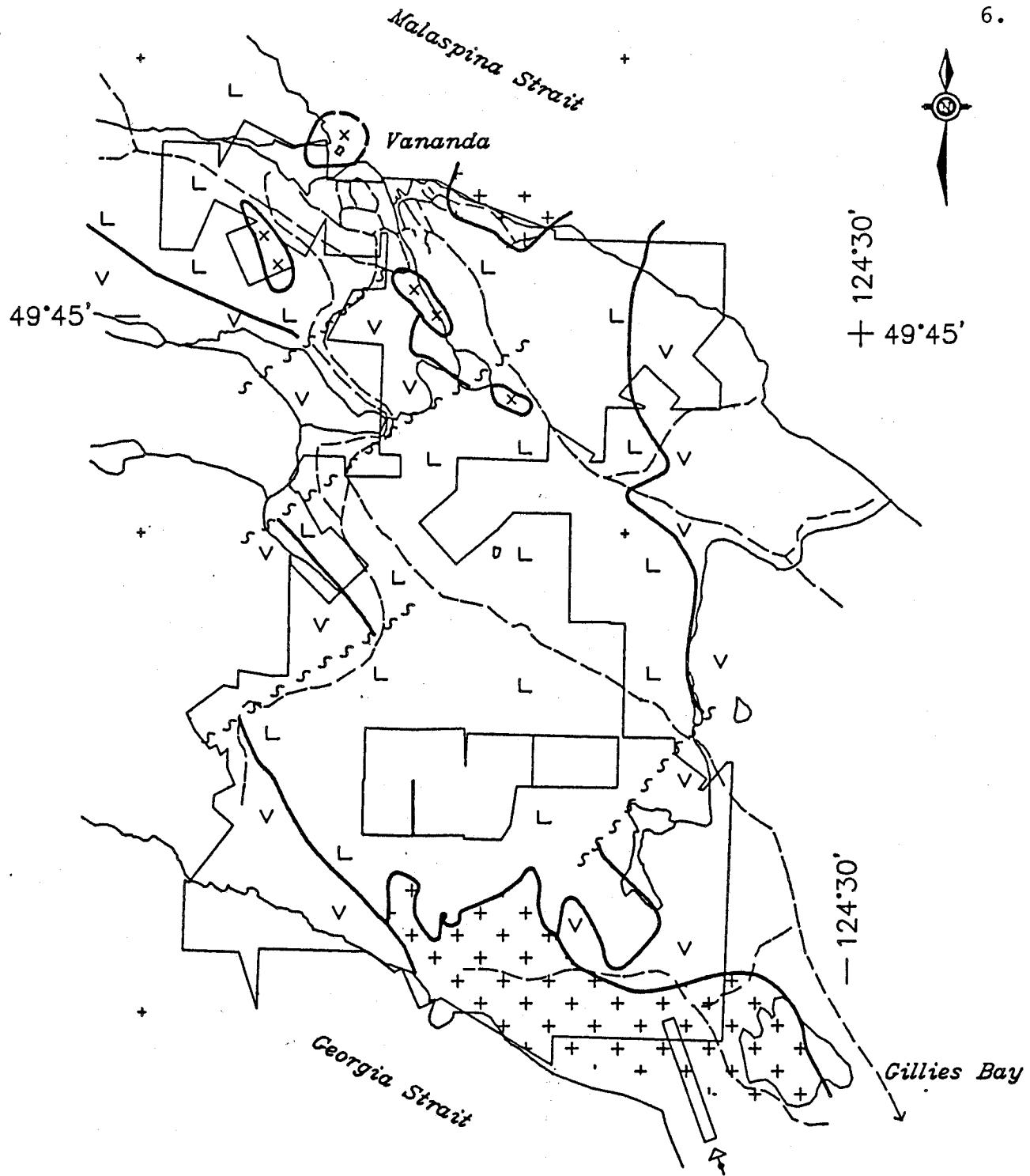
DATE: NOV. '86 N.T.S.: 92F/10E, 15E FIGURE: 2

2.0 GEOLOGY2.1 Regional Geology

The regional geology of Texada Island has not been comprehensively studied since the work of McConnell (1914). Most generally, the Vananda Gold property is underlain by a succession of mid-Mesozoic volcanic and sedimentary strata (see Figure 3), which have been correlated with middle to upper Triassic Karmutsen Group andesites and basalts and overlying upper Triassic Quatsino Formation limestones (Muller 1977). The possibility that Jurassic Bonanza Group volcanic rocks are also present cannot be dismissed.

Both volcanics and sediments are cut by at least two types of intrusive rocks, thought to be of Mesozoic age. The more common, typified by the Gillies Lake Stock in the area of the Texada iron mines, is principally composed of quartz diorite and granodiorite. Near Vananda, closely associated with the gold-copper mines, are smaller bodies of diorite, diorite porphyry, and locally more basic intrusive rock. Numerous dykes, generally porphyritic, may be associated with either intrusive family. The limited studies as have been undertaken suggest that the intrusive rocks are Jurassic or older (Carson, et al., 1971).

6.



- LEGEND
- ⊕ Quartz diorite
 - ✗ Diorite, gabbro
 - ⊓ Quatsino limestone
 - ▽ Karmutsen volcanics
 - 〰 Fault

| | | |
|--------------------------|--|--|
| VANANDA GOLD LTD. | | |
| TEXADA ISLAND PROPERTY | | |
| NANAIMO, B.C. | | |
| PROPERTY GEOLOGY | | |

DATE: NOV. '86 N.T.S.: 92F/10E, 15E FIGURE: 3

2.2

ECONOMIC GEOLOGY

Since the late 1800's several types of deposits have been known on Texada Island. Apart from the limestone quarries, the most important mineralization lies within the Au-Ag-Cu skarn deposits of Vananda and the Fe-Cu skarns near Gillies Bay. Though the Vananda mines have produced generally smaller tonnages, unit values have generally been much greater, and they are presently an attractive exploration target due to their precious metal values.

As summarized from Peatfield (1987), the Vananda gold-copper-silver deposits form narrow relatively short lenses with very substantial down-plunge projections. The larger individual shoots range to 4 x 25 x 150 metres, or about 60,000 tonnes. These lenses or shoots generally consist of bornite and chalcopyrite in a gangue of garnet, epidote, and diopside with lesser amounts of tremolite, wollastonite and other calc-silicate minerals. They are usually associated with local bleaching of the limestone to form "white rock" and most often lie wholly within the massive limestones. Free gold and native silver have been reported, and molybdenite is a widespread but minor constituent. Published reports by McConnell (1914) and Stevenson (1945), provide summaries based on detailed field work.

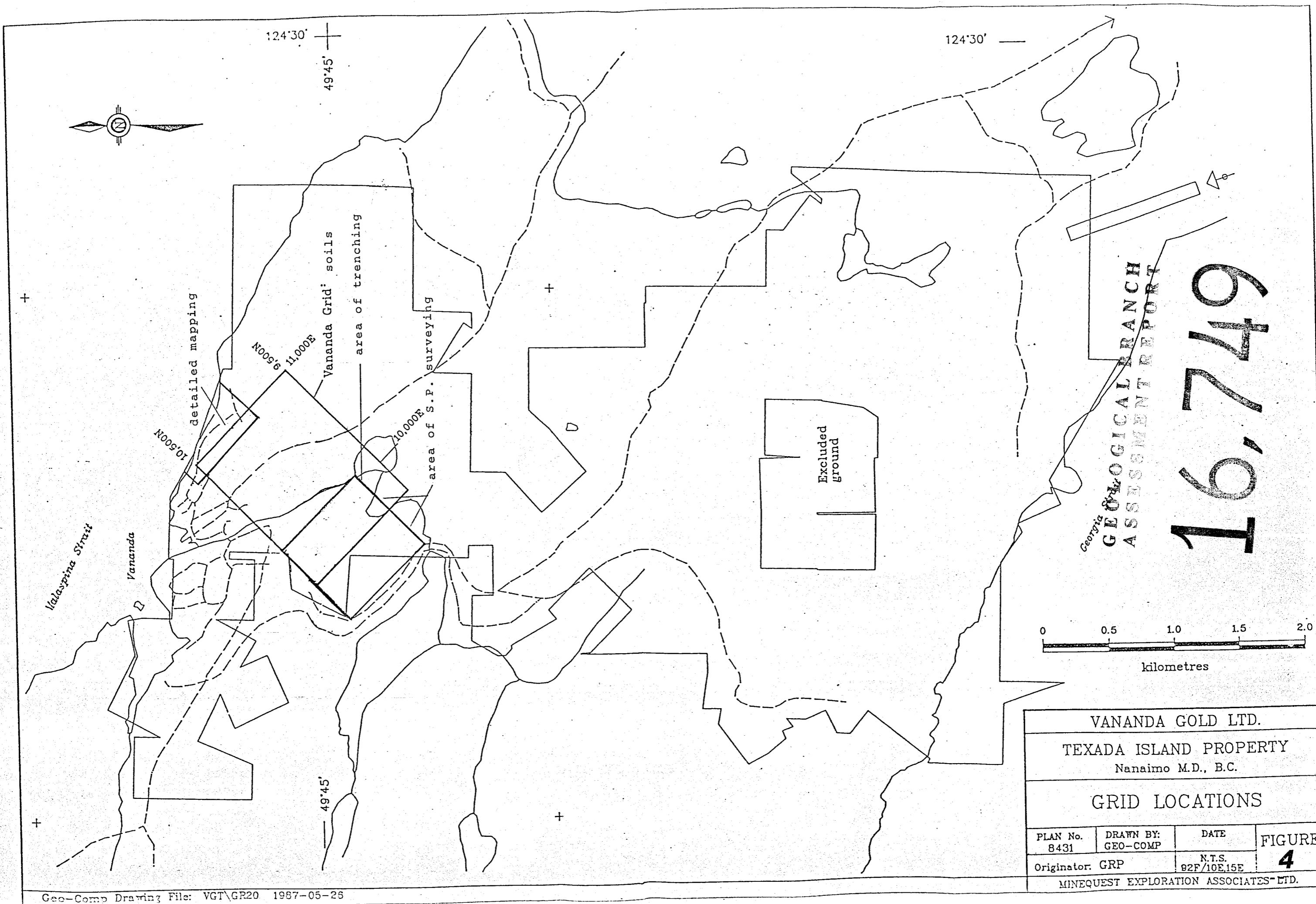
The Texada Iron deposits (see McConnell, 1914; Sangster, 1969; Meinert, 1984) are magnetite-chalcopyrite skarns located near the contacts of limestones, volcanics and quartz diorites. They commonly contain disseminated chalcopyrite, but a few lenses of high-grade copper mineralization, almost exclusively chalcopyrite, are often present.

Numerous showings of gold-silver mineralization in quartz or quartz-carbonate veins and shear-zones in volcanic rocks are present especially on the western side of the limestone belt. Some of these contain locally spectacular gold mineralization. Another occurrence of some considerable interest is the discovery on the Yew claims near Priest Lake, immediately west of the Vananda Gold Ltd. property. A flat-lying limy horizon, less than 50cm thick, within the western volcanic package, contains abundant pyrite, traces of chalcopyrite, and locally significant gold.

Many other mineral showings of various types, mostly copper-gold-silver and zinc or lead, are found in shears, veins and "replacements" on and adjacent to the Vananda Gold property. One of considerable interest consists of an apparently concordant zone within limestone in the Ideal Cement quarry toward the southern end of the property. Mineralization consists of irregular zones of granular semi-massive pyrite and sphalerite. Grab samples collected prior to the present program yielded values up to 6.1 g/t Au and 15.2 g/t Ag. There is a pronounced IP anomaly some distance downdip from the showing; the presumed source lies at no great depth and could easily be tested by a few short vertical drill holes. Native gold has been observed in polished section, as small blebs on pyrite grain boundaries, in association with Pb telluride (altaite?) and Ag telluride (hessite?) (Peatfield, 1987, P.7)

2.3 SIGNIFICANT EXPLORATION RESULTS

The Vananda Gold property has had a long and complex exploration history. Most recently Winter (1985) has summarized previous work and Peatfield (1987, p.10) has isolated significant results from the viewpoint of ongoing exploration:



Geo-Comp Drawing File: VGT\GR20 1987-05-26

- 1) "In the 1920's numerous drill holes in the area of the Vananda mines, especially the Cornell, returned good intersections (Lakes, 1930), which have been only partially followed-up. The best reported intersection, near the Cornell, was 7 metres grading 14.7 g/tonne Au and 11% Cu. The precise location of these holes is not known."
- 2) Toward the end of the second phase of mining at the Little Billie, several underground holes tested the downward extension of the ore-bodies, with attractive intersections (McLean, 1956). One intersection, in a possible new zone, was 5 metres (core length) grading 8.5 g/tonne Au and 2.69% Cu.
- 3) In 1979, Shima Resources drilled several holes in a gravity anomaly southeast of the Little Billie, with some interesting results (Winter, 1985). The best intersection was 2 metres grading 3.5 g/tonne Au and 1.68% Cu, as part of a total intersection of 16 metres grading 1.4 g/tonne Au and 1.31% Cu.
- 4) In 1984, Cartier Resources drilled several holes near the Cornell, with discouraging results, and one hole below the lower workings of the Little Billie, which cut 2.65 metres grading 7.9 g/tonne Au, 29.8 g/tonne Ag, and 1.98% Cu."

3.0 PRESENT PROGRAM

The program described in this report was carried out intermittantly over the period May 1987 to February 1988, by a number of geologists and prospectors working independently. Much of this work is ongoing and the present compilation is of necessity still preliminary. The areas covered are shown at 1:50,000 scale in Figure 4.

3.1 Detailed Geological Mapping

The area around the Cornell, Little Billie gravity anomaly and Little Billie Mine was mapped by L. Lindinger, at 1:500, 1:500 and 1:1000 scales respectively. Mapping as yet is incomplete but the areas covered are shown at 1:5000 scale in Figure 5.

Most of the area is underlain by the Triassic (?) limestones and marbles of the Quatsino Formation. The contact with andesitic volcanic rocks of the Karmutsen Group, is not observed within the areas of detailed mapping. The limestones have been intruded by small stocks of basic intrusive rocks, generally diorite or gabbro, in the area of the Cornell Mine and the Florence and Security showings. In the northeast, near the Little Billie Mine, are numerous exposures of quartz diorite. In contact zones coarsely crystalline garnet-diopside skarn, often with pyrite and chalcopyrite has developed.

Typically the limestone is light grey, massive, relatively finely crystalline rock. Commonly adjacent to intrusive masses and near the old workings, the limestones have been recrystallized and bleached or whitened. These "marbles" appear to be the result of hydrothermal activity related to the intrusive rocks, and probably to the mineralizing events.

The limestones are cut by many steeply dipping dykes of generally basic aspect. For the most part, these are oriented a few degrees north of east, but a few strike very nearly north-south.

Some areas of bleaching or marble are not obviously spatially related to outcropping intrusive bodies, nor associated with copper skarn mineralization. These areas are prime targets for further exploration.

Prominent faulting is present with orientations of 90° , $130-135$; a less obvious set is oriented at 150 . The lack of distinctive lithologic units or marker horizons makes displacements difficult to establish.

LITTLE BILLIE

Around the Little Billie, Lindinger mapped wollastonite (chlorite), garnet - diopside - actinolite, wollastonite - bornite, undifferentiated sulphide, massive magnetitite - chalcopyrite - pyrrhotite and copper (bornite, chalcopyrite) - pyrite-sphalerite-galena-pyrrhotite skarn types. Five types of dykes can be distinguished, sometimes with associated brecciation: diorite (gabbro), post-Vananda stock feldspar, porphyry, quartz diorite, pre-Vananda stock feldspar porphyry and alaskite. Crystal sizes are highly variable. Outcrops of Vananda quartz diorite, Quatsino Formation and Karmutsen Group volcanics are also present. Quatsino rocks can be divided into limestones, undifferentiated marbles, fine to medium crystalline marbles, bleached marbles and megacrystic (>5mm) marbles. Bleaching is particularly common in the area south of the Little Billie.

CORNELL

In the area of the Cornell workings Lindinger identified four map units within the Quatsino Formation. Much of the workings is underlain by bleached marble, which is locally dolomitized crystal size is variable. Diorite, feldspar porphyritic diorite and porphyritic hornblende diorite dykes are present. Near the Cornell Shaft prominent E-W faults appear to be displaced by less continuous $130 - 135^\circ / 70 - 75^\circ$ NE faults.

Both calc-silicate and sulphide skarns are present and often are associated with a diorite dyke stock-work or porphyritic diorite dyking. Disseminated pyrite is also found within some of the coarsely crystalline bleached marbles. Finer crystalline marbles tend to be present at greater distances from presently known workings and showings.

AREA OF LITTLE BILLIE SOUTH GRAVITY ANOMALY

Lindinger's mapping in the area of the Little Billie South gravity anomaly revealed marbles

of various crystal sizes, commonly with considerable amounts of brecciation. Two directions of faulting oriented 90° and 135° do not appear to show an obvious relationship to this brecciation and breccias are not observed adjacent to the quartz diorite and feldspar porphyritic diorite dykes within the map area. In one area possible ankerite was noted. As the mapping was restricted in extent, it is difficult to draw conclusions about the origin of this breccia. Further work is proposed.

3.2 FLORENCE/SECURITY AREA: TRENCHING DETAILED MAPPING
AND ROCK CHIP SAMPLING

The Florence-Security area was cleared and trenched in October to November of 1987 (see Figure 5). As shown in Figure 6, the trenched areas were mapped by S. Crawford at 1:500 and 1:100 scales; subsequently 176 rock chip samples were collected.

Samples were shipped to Acme Analytical Labs Ltd., 852 East Hastings Street, Vancouver V6A 1R6. For each a 31 element ICP analysis was completed and Au was analyzed by fire assay using a half assay ton sample. For the ICP after crushing a .500 gram sample was digested with 3-1-2 HCL-HNO₃-H₂O at 95 degrees Celsius for one hour and was diluted to 10ml with water. Sample descriptions with results are provided in Appendix I and complete analytical results are provided in Appendix III.

Figure 5 summarizes the 1:500 mapping completed to date; compilation of the 1:100 mapping is ongoing. Each sample is described by the prefix FS.87 to designate the year of collection with the following number denoting its location within a specific trench (eg. 87.1 lies within trench 1) and the final number indicating its order within the sampling program.

Crawford distinguished three geologic units: Jurassic diorite, Triassic Marble Bay (Quatsino) Formation marble and Triassic Texada Formation (Karmutsen Group) mafic volcanics. These are described in the legend. Three alteration types are present: garnet skarn, including garnet-pyroxene and garnet-pyroxene-epidote skarn; silicification with 2-20% pyrite and quartz veins and massive magnetite with pyrite, chalcopyrite and limonite boxwork.

Prominent faults are present with orientation of 115° and 150° though this appears to undulate slightly. Magnetite with pyrite, malachite and limonite boxworks appear to be developed along minor splays subparallel to the longer faults. However magnetite is also present where no faulting is recognized. Garnet skarn is particularly widespread in trenches 87.6 and 87.7. Prominent silicification associated with pyritization is developed within the diorite at its contact with the marble near 2+60N on both sides of the base line. Undulations in the diorite/limestone and diorite/volcanic contact, as well as faulting appear to have controlled skarn development.

3.3 VANANDA GRID: ANALYSIS OF SOIL SAMPLES PREVIOUSLY COLLECTED

Peatfield (1987) has described grid establishment and collection of phase II soil samples on the Vananda Grid (see Figure 7). The baseline is oriented at about 045°; lines are run at 100m intervals with stations at 25m spacing. Samples were not collected and lines not completed where cultural disturbances or interferences are present. A total of 628 samples was analyzed.

Sampling Procedure

B horizon was sampled where possible, but at some locations with thin soil cover, considerable C - horizon material was intermixed. Samples were placed in Kraft paper envelopes numbered with grid locations. Phase II sampling was completed in January and February 1987 by personnel experienced in this work.

Analytical Techniques

Soil samples were shipped to Acme Analytical Laboratories Ltd. in Vancouver, for preparation and analysis. There the samples were dried and sieved to minus-80 mesh. They were analyzed for Mo, Cu, Pb, Co, and As as follows: a .500 gram sample was digested with 3ml 3-1-2 HCl-HN03-H20 at 95 degrees Celsius for one hour and was diluted to 10ml with water. Gold analysis was by ignition at 600 C and hot aqua regia leach on a 10 gram sample, MIBK extraction and graphite furnace atomic absorption determination complete analytical results are in Appendix III.

These Au/Cu results are plotted in Figure 7. Statistical assessments have not yet been completed because all anomalies must still be prospected to eliminate any undetected cultural effects.

3.4

S.P. SURVEYING

The self-potential or spontaneous polarization (S.P.) method has been used with good success on Texada to detect gold deposits where some sulphides are present. Figure 4 outlines the general areas covered by the present program of S.P. surveying, shown in Figure 5 in more detail.

Use of S.P. involves measuring voltage potentials produced by electrochemical reactions which arise from differences in the oxidation capacity of waters near the upper and lower surfaces of source bodies. Sources can include pyrite, pyrrhotite, chalcopyrite, galena, graphite, pyrolusite, psilomelane, chalcocite, covellite, magnetite, anthracite coal or cultural artefacts. In this survey, S.P. measures are taken along lines spaced at 100m with 10m stations. One porous pot Cu-CuSO₄ electrode of the voltmetre cable fixed at one corner of the grid and the other is moved to the various points on the grid; a 300m long cable was used. Voltage differences between the grid points and the fixed electrode are recorded. When the cable length is exhausted, a new base station is chosen and its potential with respect to the first base is determined by a few repeated observations or by measuring five or six convenient points from the old as well as the new base. A direct reading millivoltmeter - potentiometer is used to record potentials. Anomaly peaks are detected by

placing the pot directly above the source and moving back and forth until maximum readings are obtained.

The program of S.P. surveying is ongoing and present results are too fragmentary to be meaningful, though strong differentials are recorded in areas of known mineralization.

3.5 DIAMOND DRILLING

A Boyles Brothers X-Ray diamond drill owned by Vananda Gold Ltd. has been mobilized to the Vananda property.

During the month of February a crew of two will have drilled approximately 200m of X-ray size core; to February 15, 1988, 25m has been completed in one hole, on a one shift per day basis. Work was intermittent as variable but sometimes very poor core recoveries necessitated experimenting with several different types of bits. The drill hole location is drawn in Figure 6. At present the first 10m of core is in Vananda's office in Vancouver, while the remainder is stored at the Vananda field office in Gillies Bay. When the hole reaches its expected 35-40m target depth, the core will be logged and due to its small diameter all of the core will be submitted for assay. This will also serve to minimize any nugget effects which may be present. Subsequent holes will lie within a variably spaced grid in the immediate Florence area.

4.0 DISCUSSION

Vananda Gold Ltd. has assembled a land package covering both the Texada iron mines and all of the significant gold-copper-silver mines (former producers) in the Vananda area. These latter deposits produced significant tonnages of good grade ore from elongate, steeply-plunging shoots of skarn mineralization with restricted cross-sectional area but very considerable (250 metres plus) vertical extent. Such shoots were very difficult to explore for, especially in the early days when most exploration was by sinking and drifting. Abundant potential remain for locating more such shoots, both adjacent to old workings and elsewhere.

Although the present program is ongoing, a review of past data and available results indicate that several significant exploration targets are found on the property. There would appear to be excellent potential for the discovery of additional Au-Cu-Ag ore bodies of skarn, vein and/or manto type.

Particular potential exists in the vicinity of old mines, especially below the lower levels of the Little Billie. Based on historical experience individual shoots have possibilities for good depth extent, tonnages up to 200,000 tonnes and grades of 5-12g/tonne Au, 20-100g/tonne Ag and 1.5-3.5% Cu (Peatfield 1987).

Further detailed mapping, prospecting and sampling should focus in areas of marbleization or bleaching using guidelines developed from the ongoing detailed mapping, sampling and diamond drilling at the Florence/Security area. The S.P. surveying will no doubt prove a valuable adjunct.

The efficacy of soil sampling in the Vananda grid area remains to be established pending ground truthing of existing anomalies to eliminate cultural disturbances. Further investigation should be carried out to establish whether other elements correlate with gold.

5.0 COST STATEMENT

| | | |
|----|--|------------|
| 1. | Geophysical surveys: including labour, rental of S.P. equipment, etc. | \$ 5,000 |
| 2. | Geochemical Surveys: - Analysis of approximately 600 soil samples. Mo, Cu, Pb, Co, AS and MIBK Au | \$19,900 |
| | - Analysis approximately 200 rock chip samples 31 element ICP, Au by fire assay. | \$ 9,300 |
| 3. | Diamond Drilling: projected to February 28, 1988 200m | \$ 8,000 |
| 4. | Sampling and Assaying: (projected) analysis of drill core above plus labour for all above geochemical sample collection | \$ 7,000 |
| 5. | Trenching: 800m X 15m | \$84,000 |
| 6. | Other Exploration Costs: Vehicle rental and gasoline | \$14,000 |
| | Mapping, surveying | \$ 8,000 |
| | Accomodation | \$ 5,000 |
| | | \$ 160,200 |

6.0 STATEMENT OF QUALIFICATIONS

I, Jenna Hardy, of 535 East Tenth Street,
North Vancouver, B.C. V7L 2E7, state that:

1. I am a geologist with address above, who graduated from the University of Toronto with a B.Sc. (Specialist in Geology) in 1974 and an M.Sc. in 1980.
2. I have practised my profession continuously since 1974 and have worked in the Cordillera since 1976.
3. I have been employed as a full-time project geologist by various companies in Vancouver since 1978.
4. I am a fellow of the Geological Association of Canada, with membership number F2640.
5. I personally reviewed all data in the hands of Vananda Gold Ltd.
6. I have no direct or indirect legal or financial interest in the Vananda Gold Ltd. property described in this report.



February 18, 1988

Jenna Hardy, M.Sc., F.G.A.C.

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APPENDIX I
Rock Chip Sample Descriptions,
Florence/Security Area

Table 1: FLORENCE/SECURITY AREA ROCK CHIP SAMPLES

* All Samples have prefix FS87

| Sample/Assay Number | Description | Length (m) | Results | | |
|---------------------|---|------------|---------|--------|--------|
| | | | Au oz/t | Ag ppm | Cu ppm |
| 6102/1.5* | | 0.7 | 0.004 | 2.3 | 1,155 |
| 6103/1.6 | | 1.2 | 0.003 | 0.9 | 278 |
| 6104/1.7 | | 0.9 | 0.002 | 0.7 | 1,355 |
| 6105/1.8 | cpy-rich | 0.7 | 0.097 | 38.8 | 30,322 |
| 6106/1.9A | mt-py | 1.2 | 0.004 | 2.0 | 811 |
| 6107/1.9B | mt-py-po-gt | 1.0 | 0.006 | 2.0 | 573 |
| 6108/1.10 | skarnified volcanics | 1.6 | 0.004 | 0.7 | 296 |
| 6109/1.11 | skarnified volcanics | 1.0 | 0.003 | 0.3 | 62 |
| 6110/1.12A | skarn | 1.1 | 0.002 | 0.3 | 110 |
| 6111/1.12B | skarn | 1.0 | 0.004 | 0.9 | 371 |
| 6112/1.13A | vein 0.5 m E of mt. vein | Grab | 0.004 | 1.8 | 1,118 |
| 6113/1.13B | mineralized skarn adjacent 13A | Grab | 0.003 | 1.0 | 729 |
| 6114/1.14 | rusty zone; sulphides, quartz, some epidote | Grab | 0.011 | 23.2 | 19,268 |
| 6115/1.15 | rusty zone in epidote skarn | Grab | 0.002 | 9.1 | 6,890 |
| 6116/1.16 | massive sulphide, minor quartz | Grab | 0.004 | 22.7 | 23,516 |
| 6117/2.17 | near massive sulphide W of Shaft #2 | Grab | 0.006 | 0.7 | 1,753 |
| 6118/2.18 | near massive sulphide, some cpy | 1.2 | 0.692 | 29.3 | 15,945 |
| 6119/1.19 | epidote skarn with 10 cm vein | 1.6 | 0.013 | 3.0 | 2,241 |
| 6120/1.20 | silicified grey marble, minor py | 0.6 | 0.005 | 0.6 | 226 |
| 6121/2.21 | mineralized dyke | 1.1 | 0.008 | 2.4 | 2,448 |
| 6122/2.22 | nearly massive sulphide vein | 0.9 | 0.019 | 2.8 | 4,195 |
| 6123/2.23A | cpy-rich shear | 1.4 | 0.526 | 30.7 | 16,181 |
| 6124/2.23B | cpy-rich, mt | 1.7 | 0.219 | 10.0 | 8,782 |
| 6125/3.24 | marble contact with volcanic | 0.7 | 0.071 | 0.3 | 225 |
| 6126/3.25 | clay-like altered volcanic | | 0.003 | 0.2 | 353 |
| 6127/2.26 | iron sulphide zone W side shaft | 1.7 | 0.011 | 1.6 | 4,960 |
| 6128/2.27 | downdip of skarn W of shaft | 1.3 | 0.005 | 0.6 | 577 |
| 6129/2.28 | 2.6 m S of above, skarn | 1.5 | 0.061 | 10.2 | 9,155 |
| 6130/3.29 | 5 cm deep channel in volcanics at marble contact | 0.6 | 0.005 | 1.2 | 396 |
| 6131/2.30 | continuation of 2.28 | 1.5 | 0.002 | 0.5 | 284 |
| 6132/4.31 | sulphide vein | 1.8 | 0.010 | 1.8 | 1,945 |
| 6133/4.32 | vein W of above | 0.7 | 0.004 | 0.8 | 1,288 |
| 6134/4.33A | vein material | 1.6 | 0.017 | 2.3 | 4,190 |
| 6135/4.33B | continuation of above | 1.3 | 0.006 | 0.9 | 877 |
| 6136/4.34A | | 1.25 | 0.004 | 0.6 | 1,523 |
| 6137/4.34B | cpy-rich zone | 1.5 | 0.180 | 16.1 | 15,940 |
| 6138/4.34C | cpy-rich zone | 1.5 | 0.002 | 24.4 | 21,258 |
| 6151/4.35A | skarn | 2.6 | 0.002 | 0.4 | 174 |
| 6152/4.35B | skarn | 1.7 | 0.001 | 0.4 | 78 |
| 6153/4.35C | skarn | 1.7 | 0.001 | 0.5 | 45 |
| 6154/4.36 | a large vein, sooty ?chalcocite | Grab | 0.018 | 0.6 | 2,785 |
| 6155/5.37 | skarn | 2.1 | 0.002 | 0.3 | 179 |

| Sample/Assay Number | Description | Length (m) | Au oz/t | Results Ag ppm | Cu ppm |
|---------------------|--|------------|---------|----------------|--------|
| 6156/5.38A | in vein | 1.8 | 0.010 | 1.3 | 957 |
| 6157/5.38B | in vein | 2.5 | 0.039 | 4.6 | 2,492 |
| 6158/5.39 | ferricrete | Grab | 0.002 | 0.6 | 2,035 |
| 6159/5.40 | massive sulphide on E side of ferricrete | Grab | 0.018 | 2.3 | 4,288 |
| 6160/6.41A | skarn with epidote | 2.5 | 0.005 | 0.6 | 177 |
| 6161/6.41B | copper stained skarn | 2.3 | 0.018 | 1.8 | 1,213 |
| 6161/6.41C | | 2.5 | 0.017 | 1.2 | 451 |
| 6163/6.41D | skarn | 2.2 | 0.005 | 1.0 | 230 |
| 6164/6.42A | garnet skarn | 2.25 | 0.001 | 0.3 | 21 |
| 6165/6.42B | garnet skarn | 2.8 | 0.001 | 0.5 | 27 |
| 6166/6.43A | garnet skarn | 2.4 | 0.001 | 0.4 | 90 |
| 6167/6.43B | garnet skarn | 2.7 | 0.001 | 0.5 | 48 |
| 6168/6.43C | garnet skarn some epidote | 3.1 | 0.001 | 0.1 | 87 |
| 6169/6.43D | garnet-epidote | 2.9 | 0.001 | 0.4 | 28 |
| 6170/5.44 | purple marble | 1.0 | 0.001 | 0.6 | 7 |
| 6171/5.45 | contact of above with skarn | 1.5 | 0.001 | 0.4 | 54 |
| 6172/6.46 | altered intrusive with cpy, py | 1.2 | 0.022 | 2.0 | 2,256 |
| 6173/6.47 | as above | 1.0 | 0.029 | 2.8 | 2,167 |
| 6174/6.48 | marble contact | 2.0 | 0.006 | 0.5 | 157 |
| 6175/7.49A | skarn | 3.3 | 0.001 | 0.3 | 36 |
| 6176/7.49B | skarn | 2.8 | 0.001 | 0.4 | 82 |
| 6177/7.49C | skarn with py | 2.1 | 0.001 | 0.5 | 99 |
| 6178/7.49D | mt with marble | 3.25 | 0.001 | 0.7 | 425 |
| 6179/9.50A | mt, cpy in garnet skarn | 1.8 | 0.004 | 1.6 | 1,013 |
| 6180/9.50B | mt, cpy in epidote-garnet skarn | 2.0 | 0.006 | 4.8 | 6,063 |
| 6181/9.51A | mt, cpy in garnet-epidote skarn | 2.1 | 0.002 | 0.8 | 313 |
| 6182/9.51B | as above | 2.1 | 0.001 | 0.8 | 307 |
| 6183/9.52 | po, py in skarn | 1.25 | 0.001 | 1.5 | 641 |
| 6184/9.53A | massive mt | 1.35 | 0.002 | 0.8 | 104 |
| 6185/9.53B | near massive mt, minor cpy | 1.5 | 0.021 | 4.0 | 3,171 |
| 6186/9.54 | mt + py in altered diorite(?) | 1.6 | 0.001 | 0.7 | 102 |
| 6187/10.55A | rusty skarnified volcanics | 2.0 | 0.001 | 0.8 | 280 |
| 6188/10.55B | as above | 2.15 | 0.001 | 0.3 | 261 |
| 6189/10.56 | as above | 2.0 | 0.001 | 1.5 | 2,061 |
| 6190/10.57 | skarn with cpy | 2.1 | 0.001 | 3.1 | 6,333 |
| 6191/10.58A | as above | 2.2 | 0.001 | 0.9 | 3,093 |
| 6192/10.58B | skarn | 2.65 | 0.001 | 1.0 | 481 |
| 6193/10.58C | skarn | 2.75 | 0.001 | 0.7 | 349 |
| 6194/10.59A | rusty skarnified volcanics | 2.0 | 0.001 | 0.6 | 188 |
| 6195/10.59B | as above | 1.9 | 0.010 | 0.8 | 192 |
| 6196/10.60A | skarn contact with marble, mt, cpy | 2.0 | 0.001 | 1.7 | 1,764 |
| 6197/10.60B | rusty skarnified volcanics | 2.05 | 0.002 | 1.5 | 536 |
| 6198/10.60C | rusty skarnified volcanics | 1.95 | 0.006 | 2.1 | 1,007 |
| 6199/10.60D | as above | 2.0 | 0.012 | 1.0 | 392 |
| 6319/10.61A | skarn | 1.7 | 0.001 | 0.5 | 1,641 |
| 6320/10.61B | rusty skarnified volcanics | 1.7 | 0.001 | 0.2 | 522 |

| Sample/Assay Number | Description | Length (m) | Results | | |
|---------------------|--|------------|---------|--------|--------|
| | | | Au oz/t | Ag ppm | Cu ppm |
| 6321/10.62 | as above | 2.7 | 0.001 | 0.1 | 485 |
| 6322/10.63 | rusty skarnified volcanics | 2.3 | 0.001 | 0.1 | 520 |
| 6251/1.64 | resample FS87.1.14: rusty skarn from which gold panned | 0.8 | 0.001 | 5.1 | 4,953 |
| 6252/1.65A | as above resample 87.1.15 | 1.3 | 0.005 | 4.4 | 4,677 |
| 6253/1.65B | resample 87.1.16 | 1.0 | 0.020 | 3.9 | 2,576 |
| 6254/1.66A | vein S of shaft: py, mt, cpy | 1.55 | 0.042 | 5.5 | 10,566 |
| 6255/1.66B | as above | 1.75 | 0.032 | 5.3 | 10,458 |
| 6298/8.67A | skarn below marble in trench 2, going south | 2.75 | 0.003 | 0.3 | 1,122 |
| 6299/8.67B | as above but contacts marble | 2.7 | 0.008 | 1.5 | 505 |
| 6317/9.68 | skarn | 1.65 | 0.001 | 0.1 | 25 |
| 6318/9.69 | skarn | 2.0 | 0.001 | 0.1 | 33 |
| 6300/8.70 | skarnified volcanics | 2.3 | 0.002 | 0.1 | 505 |
| 6301/8.71 | as above | 2.7 | 0.003 | 0.2 | 653 |
| 6302/8.72 | as above | 2.4 | 0.001 | 0.1 | 345 |
| 6303/8.73 | skarnified volcanics | 2.25 | 0.001 | 0.1 | 370 |
| 6304/8.74 | as above | 2.35 | 0.001 | 0.1 | 329 |
| 6305/8.75 | as above | 2.15 | 0.004 | 0.5 | 799 |
| 6306/8.76 | skarn | 2.2 | 0.001 | 0.1 | 351 |
| 6307/8.77 | skarn/marble contact with Cu stain | 2.5 | 0.002 | 2.2 | 1,298 |
| 6308/8.78 | rusty zone with 7.5 cm quartz vein | 1.4 | 0.001 | 0.4 | 315 |
| 6309/8.79 | vertical sample rusty volcanics | 1.5 | 0.001 | 0.1 | 192 |
| 6310/8.80 | limy clay gouge below rusty volcanics | 2.5 | 0.001 | 0.1 | 112 |
| 6311/8.81 | limy sheared volcanics | 2.4 | 0.001 | 0.1 | 75 |
| 6312/8.82 | rusty skarnified volcanics | 2.2 | 0.001 | 0.1 | 195 |
| 6313/8.83 | as above | 2.3 | 0.001 | 0.1 | 93 |
| 6314/8.84 | rusty skarnified volcanics | 2.15 | 0.001 | 0.1 | 68 |
| 6315/8.85 | as above | 2.15 | 0.001 | 0.1 | 48 |
| 6316/8.86 | as above | 2.1 | 0.001 | 0.1 | 44 |
| 6323/11.87 | sheared volcanic between marble | 1.0 | 0.001 | 0.2 | 140 |
| 6324/11.88 | vertical sample of marble | 1.0 | 0.001 | 0.1 | 40 |
| 6325/11.89 | garnet skarn minor cpy | 1.5 | 0.001 | 0.1 | 16 |
| 6326/11.90 | garnet skarn | 1.2 | 0.001 | 0.1 | 16 |
| 6327/11.91 | skarn, minor cpy | 1.7 | 0.003 | 0.3 | 496 |
| 6328/11.92 | skarn and marble, minor cpy | 1.8 | 0.004 | 0.3 | 570 |
| 6329/11.93 | sheared skarnified volcanics under marble | 1.8 | 0.004 | 0.1 | 60 |
| 6330/11.94 | rusty volcanics | 1.8 | 0.001 | 0.4 | 149 |
| 6331/12.95 | marble contact near ferricrete | 1.3 | 0.004 | 0.4 | 124 |
| 6332/12.96 | some py | 2.5 | 0.001 | 0.2 | 203 |
| 6290/6.97 | hornfels at intrusive contact | 1.2 | 0.001 | 0.1 | 77 |
| 6291/6.98 | vertical sample 3 m S FS87.6.41D | 1.2 | 0.003 | 0.1 | 275 |
| 6292/6.99 | rusty sheared volcanic | 1.6 | 0.001 | 0.1 | 56 |
| 6284/5.100 | rusty volcanic | 1.5 | 0.001 | 0.1 | 47 |
| 6285/5.101 | sheared volcanic | 1.0 | 0.006 | 0.4 | 505 |
| 6286/5.102 | vein material | 1.0 | 0.015 | 1.8 | 1,696 |
| 6278/5.103 | vertical sample in marble at volcanic contact | 1.2 | 0.001 | 0.1 | 2 |

| Sample/Assay Number | Description | Length (m) | Results | | |
|---------------------|---|------------|---------|--------|--------|
| | | | Au oz/t | Ag ppm | Cu ppm |
| 6288/5.104 | vertical sample in andesite | 0.9 | 0.001 | 0.1 | 117 |
| 6272/4.105 | skarn | 1.15 | 0.022 | 0.1 | 79 |
| 6273/4.106 | skarn | 2.1 | 0.001 | 0.1 | 54 |
| 6274/4.107 | skarn | 1.45 | 0.001 | 0.1 | 79 |
| 6289/5.108 | marble contact | 1.35 | 0.001 | 0.1 | 198 |
| 6275/4.109 | skarn | 2.4 | 0.002 | 0.4 | 379 |
| 6276/4.11D | marble | 1.2 | 0.001 | 0.2 | 15 |
| 6277/4.111 | skarn | 1.55 | 0.005 | 0.5 | 632 |
| 6278/4.112 | py, marble contact | 1.25 | 0.021 | 2.8 | 4,280 |
| 6279/4.113 | as above | 2.9 | 0.007 | 1.6 | 2,588 |
| 6280/4.114 | altered marble | 1.0 | 0.001 | 0.1 | 116 |
| 6281/4.115 | sheared skarn | 1.5 | 0.004 | 0.3 | 323 |
| 6282/4.116 | marble | 1.1 | 0.001 | 0.1 | 68 |
| 6283/4.117 | pyrite, marble contact with Cu stain | 1.8 | 0.006 | 2.0 | 1,024 |
| 6256/2.118 | marble, skarn, some cpy | 0.9 | 0.062 | 8.8 | 5,732 |
| 6257/2.119 | mt, cpy in skarn | 0.9 | 0.243 | 23.6 | 18,242 |
| 6258/2.120 | as above | 1.1 | 0.022 | 5.3 | 4,430 |
| 6259/2.121 | marble with skarn inclusions, Cu stain | 1.5 | 0.001 | 2.3 | 3,152 |
| 6260/2.122 | marble | 1.1 | 0.001 | 0.5 | 87 |
| 6261/2.123 | marble with 10 cm quartz vein, Cu stain | 1.3 | 0.002 | 0.3 | 623 |
| 6262/2.124 | marble, py, Cu stain, quartz | 1.15 | 0.003 | 0.7 | 2,336 |
| 6263/2.125 | as above | 1.2 | 0.002 | 0.5 | 1,497 |
| 6264/2.126 | skarn/marble contact | 2.4 | 0.003 | 0.3 | 1,105 |
| 6265/2.27 | skarn, some mt, cpy | 1.6 | 0.022 | 2.9 | 2,297 |
| 6266/2.128 | skarnified sheared marble | 1.7 | 0.001 | 0.3 | 356 |
| 6267/2.129 | marble/skarn contact | 1.5 | 0.003 | 0.3 | 445 |
| 6268/2.130 | skarn | 2.2 | 0.001 | 0.1 | 63 |
| 6269/2.131 | skarn | 1.2 | 0.001 | 0.1 | 82 |
| 6270/2.132 | skarn/marble contact | 1.2 | 0.002 | 0.1 | 409 |
| 6271/3.133 | rusty volcanics | 1.2 | 0.001 | 0.1 | 164 |
| 6295/7.134 | skarn in edge of shaft | 0.8 | 0.236 | 65.7 | 69,215 |
| 6296/7.135 | as above | 1.2 | 0.025 | 4.2 | 2,665 |
| 6297/7.136 | as above | 1.0 | 0.510 | 84.3 | 55,020 |
| 6293/6.137 | top of trench in skarn | 1.2 | 0.001 | 0.1 | 44 |
| 6294/6.138 | as above | 0.7 | 0.001 | 0.1 | 18 |
| 6333/2.139 | silicified diorite | 0.8 | 0.006 | 0.1 | 7 |

APPENDIX II
Property Holdings

APPENDIX II (Continued)

| Name | Record # | Anniversary Date | Expiry Year |
|---------------------|----------|------------------|-------------|
| Ann | 17440 | July 21 | 1996 |
| Ann Fr. | 17441 | July 21 | 1996 |
| True Fr. | 17554 | November 2 | 1991 |
| IC No. 1 | 17608 | February 1 | 1996 |
| IC No. 2 | 17609 | February 1 | 1997 |
| IC No. 3 | 17610 | February 1 | 1997 |
| IC No. 4 | 17611 | February 1 | 1997 |
| I.C. No. 11 | 18126 | August 18 | 1990 |
| I.C. No. 12 | 18127 | August 18 | 1990 |
| I.C. No. 13 | 18128 | August 18 | 1990 |
| I.C. No. 14 | 18129 | August 18 | 1990 |
| I.C. No. 15 | 18130 | August 18 | 1990 |
| I.C. No. 16 | 18131 | August 18 | 1990 |
| MARBLE BAY FRACTION | | | |
| No. 2* | 34423 | October 6 | 1987 |
| STURT BAY NO. 1 | 34424 | October 12 | 1995 |
| STURT BAY NO. 2 | 34425 | October 12 | 1995 |
| VAL Fr | 37436 | March 4 | 1987 |
| NOEX Fr | 37437 | March 4 | 1987 |
| Basic #1 Fr. | 37646 | July 26 | 1991 |
| Basic #2 | 37647 | July 26 | 1991 |
| Basic #3 | 37648 | July 26 | 1991 |
| Basic #4 Fr. | 37649 | July 26 | 1991 |
| Basic #5 | 37650 | July 26 | 1991 |
| Basic #6 Fr. | 37651 | July 26 | 1991 |
| Basic #7 | 37652 | July 26 | 1991 |
| Basic #8 | 37653 | July 26 | 1991 |
| Basic #9 | 37654 | July 26 | 1991 |
| Basic #11 | 37655 | July 26 | 1991 |
| Basic #12 | 37656 | July 26 | 1991 |
| Basic #13 | 37657 | July 26 | 1991 |
| Basic #15 | 37658 | July 26 | 1991 |
| Basic #16 Fr. | 37659 | July 26 | 1991 |
| Basic #19 Fr. | 37661 | July 26 | 1991 |
| Basic #20 Fr. | 37662 | July 26 | 1991 |
| Basic #23 Fr. | 37663 | July 26 | 1991 |
| Basic #24 Fr. | 37664 | July 26 | 1991 |
| IDEAL 10 | 37787 | September 20 | 1995 |
| IDEAL 14 | 37788 | September 20 | 1995 |
| IDEAL 17 Fr. | 37789 | September 20 | 1995 |
| IDEAL 18 Fr. | 37790 | September 20 | 1995 |
| IDEAL 21 Fr. | 37791 | September 20 | 1995 |
| IDEAL 22 Fr. | 37792 | September 20 | 1995 |
| IDEAL 26 Fr. | 37793 | September 20 | 1995 |

* base metal rights only

APPENDIX II (Continued)

| <u>Name</u> | <u>Record #</u> | <u>Anniversary Date</u> | <u>Expiry Year</u> |
|-------------------|-----------------|-------------------------|--------------------|
| BASIC 29 Fr. | 515 | January 23 | 1996 |
| Brownie No. 1 Fr. | 1071 | February 10 | 1997 |
| Brownie #2 Fr. | 1072 | February 10 | 1997 |
| Brownie #3 Fr. | 1147 | April 16 | 1992 |
| B-40878 | 13297 | June 17 | 1990 |
| B 40879 | 13298 | June 17 | 1990 |
| B 40882 | 13301 | June 17 | 1990 |
| B 40884 | 13302 | June 17 | 1990 |
| B 40886 | 13305 | June 17 | 1990 |
| B 40887 | 13306 | June 17 | 1990 |
| B 40888 | 13307 | June 17 | 1990 |
| B 40889 | 13308 | June 17 | 1990 |
| B. 41066 | 13315 | June 24 | 1993 |
| B. 40900 | 13316 | June 24 | 1993 |
| B. 40894 | 13322 | June 24 | 1990 |
| Lime | 13933 | July 13 | 1990 |
| Lime No. 1 Fr. | 13934 | July 13 | 1990 |
| T.M.L. No. 3 | 14306 | May 15 | 1987 |
| Lime No. 10 Fr. | 14518 | June 13 | 1990 |
| Lime No. 11 Fr. | 14519 | June 13 | 1990 |
| Lime No. 12 Fr. | 14524 | July 14 | 1990 |
| Lime No. 13 Fr. | 14585 | November 24 | 1995 |
| Lime 14 | 14586 | November 24 | 1995 |
| Lime 15 Fr | 14587 | November 24 | 1995 |
| Lime 16 Fr | 14588 | November 24 | 1995 |
| T M L #6 Fr | 15326 | April 17 | 1987 |
| T.M.L. #7 Fr. | 15596 | January 17 | 1996 |
| T.M.L. #8 Fr. | 15597 | January 17 | 1996 |
| T.M.L. #9 Fr. | 15598 | January 17 | 1996 |
| T.M.L. #10 Fr. | 15599 | January 17 | 1996 |
| T.M.L. #11 | 15600 | January 17 | 1996 |
| T.M.L. #12 Fr. | 15601 | January 17 | 1996 |
| T.M.L. #13 | 15602 | January 17 | 1996 |
| T.M.L. #14 | 15603 | January 17 | 1996 |
| T.M.L. #15 Fr. | 15604 | January 17 | 1996 |
| TML 36 | 16124 | December 6 | 1995 |
| TML 37 | 16125 | December 6 | 1996 |
| TML 38 | 16126 | December 6 | 1996 |
| TML 39 | 16127 | December 6 | 1996 |
| TML 40 | 16128 | December 6 | 1996 |
| T.M.L. #41 Fr | 16129 | December 6 | 1996 |
| T.M.L. #42 Fr | 16130 | December 6 | 1996 |
| T.M.L. #43 Fr | 16131 | December 6 | 1996 |
| Lime #18 | 17284 | May 7 | 1995 |
| Lime #20 | 17286 | May 14 | 1995 |

APPENDIX II

Property Holdings

| Name | Record # | Anniversary Date | Comments |
|--------------------|----------|------------------|----------------------|
| Cinnabar | M1 | - | Mining Lease |
| Alladin | M10 | - | Mining Lease |
| VanAnda | M15 | - | Mining Lease |
| Copper Queen | L40 | - | CG |
| Eastgate | L53 | - | CG |
| Lucky Jack | L79 | - | CG |
| Volunteer | L131 | - | CG |
| Europe | L133 | - | CG |
| Great Copper Chief | L134 | - | CG |
| Toothpick FR | L140 | - | CG |
| Marble Bay | L154 | - | CG |
| Cameron | L182 | - | CG |
| Cornell | L201 | - | CG |
| Goodall FR | L234 | - | CG |
| Leroi | L264 | - | CG |
| Boulder Nest | L265 | - | CG |
| Jack North | L266 | - | CG |
| Yellow Kid | L267 | - | CG |
| L.M.C. | L268 | - | CG |
| McLeod #3 | L515 | - | CG |
| McLeod #4 | L516 | - | CG |
| McLeod #5 | L517 | - | CG |
| McLeod #6 | L518 | - | CG |
| McLeod #7 | L519 | - | CG |
| McLeod #8 | L520 | - | CG |
| McLeod #1 | L521 | - | CG |
| McLeod #2 FR | L522 | - | CG |
| Lap #1 FR | L523 | - | CG |
| Lap #2 FR | L524 | - | CG |
| Lap #3 FR | L525 | - | CG |
| Lap #4 FR | L526 | - | CG |
| Lap #5 | L527 | - | CG |
| Lap #6 | L528 | - | CG |
| Lap #8 | L530 | - | CG partial ownership |

APPENDIX III

Analytical Results

GEOREMICAL / ASSAY CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML J-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR M6 BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Rock Chips AU#S BY FIRE ASSAY FROM 1/2 A.T.

DATE RECEIVED: NOV 13 1987 DATE REPORT MAILED: Nov 30 1987 ASSAYER: DEAN TOYE, CERTIFIED B.C. ASSAYER

| | | VANANDA GOLD | | | | | | | | | | | | File # 87-5763 Page 1 | | | | | | | | | | | | | | | | | | |
|------------|----|--------------|-----|-------|------|-----|-----|------|-------|-----|-----|-----|-----|-----------------------|-----|-----|-----|-----|-------|------|-----|-----|------|-----|-----|-----|------|-----|------|----|------|------|
| SAMPLE# | | MO | CU | PB | ZN | AG | Ni | CO | MN | FE | AS | U | AU | TH | SR | CD | SB | BI | V | CA | P | LA | CR | M6 | BA | TI | B | AL | NA | K | W | AU\$ |
| | | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | OZ/T | | | |
| P 6251 | 9 | 4953 | 8 | 79 | 5.1 | 21 | 97 | 1027 | 9.74 | 47 | 5 | ND | 1 | 45 | 1 | 2 | 2 | 44 | 4.08 | .064 | 2 | 37 | .27 | 24 | .13 | 4 | .95 | .05 | .05 | 4 | .001 | |
| P 6252 | 4 | 4677 | 5 | 72 | 4.4 | 15 | 76 | 724 | 4.46 | 31 | 5 | ND | 1 | 100 | 1 | 2 | 2 | 52 | 2.32 | .091 | 3 | 25 | .47 | 20 | .21 | 5 | 1.37 | .12 | .06 | 1 | .005 | |
| P 6253- | 3 | 2576 | 9 | 69 | 3.9 | 37 | 104 | 419 | 11.17 | 39 | 5 | ND | 1 | 38 | 1 | 2 | 3 | 57 | 1.21 | .039 | 2 | 53 | .32 | 7 | .19 | 2 | .67 | .04 | .03 | 3 | .020 | |
| P 6254- | 1 | 10566 | 9 | 75 | 5.5 | 15 | 211 | 876 | 30.47 | 74 | 5 | ND | 1 | 5 | 1 | 2 | 2 | 19 | 4.39 | .033 | 2 | 6 | .19 | 4 | .03 | 5 | .43 | .02 | .04 | 10 | .042 | |
| P 6255 - | 1 | 10458 | 13 | 103 | 5.3 | 9 | 299 | 762 | 34.54 | 49 | 5 | ND | 1 | 1 | 1 | 2 | 2 | 14 | 4.25 | .017 | 2 | 4 | .05 | 2 | .01 | 7 | .17 | .01 | .03 | 18 | .032 | |
| ✓ P 6256 - | 1 | 5732 | 3 | 100 | 8.8 | 7 | 24 | 927 | 12.35 | 143 | 5 | ND | 1 | 134 | 2 | 2 | 2 | 5 | 20.59 | .005 | 2 | 3 | .21 | 4 | .01 | 2 | .18 | .01 | .01 | 70 | .052 | |
| ✓ P 6257 | 2 | 18242 | 14 | 217 | 23.6 | 19 | 110 | 1129 | 25.99 | 178 | 5 | 7 | 1 | 3 | 3 | 2 | 2 | 10 | 10.38 | .001 | 3 | 3 | .15 | 5 | .01 | 2 | .25 | .01 | .03 | 98 | .243 | |
| ✓ P 6258 | 1 | 4430 | 12 | 480 | 5.3 | 7 | 35 | 1158 | 16.01 | 73 | 5 | ND | 1 | 60 | 6 | 2 | 2 | 25 | 12.08 | .019 | 3 | 10 | 1.08 | 26 | .04 | 2 | 1.08 | .06 | .11 | 19 | .022 | |
| P 6259 | 1 | 3152 | 3 | 459 | 2.3 | 3 | 5 | 685 | 5.42 | 35 | 5 | ND | 1 | 155 | 12 | 2 | 2 | 4 | 26.96 | .010 | 2 | 2 | .44 | 2 | .01 | 2 | .29 | .01 | .01 | 34 | .001 | |
| P 6260 | 1 | 87 | 4 | 332 | .5 | 1 | 1 | 845 | .54 | 6 | 10 | ND | 1 | 417 | 11 | 4 | 7 | 1 | 34.42 | .004 | 2 | 1 | .73 | 19 | .01 | 2 | .04 | .01 | .03 | 1 | .001 | |
| P 6261 | 12 | 623 | 5 | 17163 | .3 | 1 | 4 | 1558 | 2.08 | 37 | 7 | ND | 1 | 372 | 191 | 2 | 4 | 1 | 25.37 | .003 | 2 | 1 | .69 | 19 | .01 | 2 | .14 | .01 | .03 | 1 | .002 | |
| P 6262 | 4 | 2336 | 3 | 6115 | .7 | 1 | 6 | 965 | 4.05 | 27 | 5 | ND | 1 | 235 | 71 | 2 | 3 | 1 | 21.22 | .007 | 2 | 1 | .42 | 5 | .01 | 2 | .21 | .01 | .01 | 1 | .003 | |
| P 6263 | 3 | 1497 | 5 | 3927 | .5 | 2 | 10 | 1471 | 4.24 | 44 | 5 | ND | 1 | 170 | 49 | 2 | 2 | 2 | 14.06 | .009 | 2 | 3 | .35 | 5 | .01 | 2 | .35 | .01 | .01 | 1 | .003 | |
| P 6264 | 1 | 1105 | 10 | 826 | .3 | 13 | 15 | 710 | 2.80 | 43 | 5 | ND | 1 | 158 | 15 | 2 | 2 | 9 | 20.86 | .003 | 4 | 11 | 2.55 | 3 | .08 | 20 | 1.91 | .01 | .01 | 2 | .022 | |
| P 6265 | 1 | 2297 | 10 | 413 | 2.9 | 8 | 32 | 952 | 7.45 | 50 | 5 | 2 | 1 | 48 | 5 | 2 | 4 | 28 | 3.42 | .029 | 4 | 8 | .98 | 21 | .07 | 2 | 1.42 | .07 | .03 | 2 | .022 | |
| P 6266 | 2 | 356 | 7 | 2832 | .3 | 4 | 6 | 1178 | 1.97 | 23 | 5 | ND | 1 | 274 | 46 | 3 | 2 | 28 | 24.84 | .035 | 4 | 1 | 1.53 | 21 | .04 | 4 | 1.19 | .01 | .05 | 1 | .001 | |
| P 6267 | 1 | 445 | 2 | 405 | .3 | 4 | 10 | 833 | 4.73 | 69 | 5 | ND | 1 | 77 | 6 | 2 | 2 | 26 | 15.98 | .025 | 2 | 5 | 2.02 | 43 | .05 | 2 | 1.46 | .02 | .07 | 11 | .003 | |
| P 6268 | 1 | 63 | 5 | 101 | .1 | 7 | 7 | 620 | 2.24 | 29 | 6 | ND | 1 | 78 | 1 | 3 | 2 | 56 | 3.96 | .076 | 4 | 6 | 1.58 | 7 | .13 | 3 | 1.89 | .03 | .03 | 1 | .001 | |
| P 6269 | 1 | 92 | 4 | 54 | .1 | 7 | 5 | 561 | 1.84 | 29 | 5 | ND | 1 | 85 | 1 | 2 | 4 | 62 | 3.64 | .091 | 4 | 6 | 1.00 | 19 | .14 | 4 | 1.72 | .02 | .03 | 1 | .001 | |
| P 6270 | 2 | 409 | 8 | 3326 | .1 | 3 | 6 | 967 | 1.98 | 19 | 5 | ND | 1 | 161 | 26 | 3 | 2 | 25 | 8.12 | .044 | 3 | 4 | 1.15 | 35 | .08 | 3 | 1.58 | .05 | .03 | 1 | .002 | |
| P 6271 | 1 | 164 | 3 | 266 | .1 | 2 | 5 | 564 | 2.33 | 7 | 5 | ND | 1 | 56 | 3 | 5 | 5 | 46 | .79 | .036 | 3 | 5 | 1.59 | 72 | .09 | 2 | 2.29 | .10 | .40 | 1 | .001 | |
| P 6272 | 1 | 79 | 8 | 174 | .1 | 5 | 12 | 794 | 3.01 | 12 | 5 | 2 | 1 | 71 | 1 | 2 | 2 | 27 | 4.59 | .013 | 2 | 4 | 4.78 | 195 | .11 | 2 | 3.32 | .11 | .27 | 1 | .022 | |
| P 6273 | 1 | 54 | 10 | 291 | .1 | 6 | 9 | 648 | 2.33 | 13 | 5 | ND | 1 | 139 | 1 | 2 | 2 | 23 | 3.76 | .016 | 2 | 3 | 3.60 | 305 | .12 | 2 | 3.89 | .21 | .42 | 1 | .001 | |
| P 6274 | 1 | 79 | 12 | 269 | .1 | 4 | 5 | 482 | 1.77 | 15 | 5 | ND | 1 | 160 | 3 | 3 | 2 | 53 | 2.47 | .100 | 4 | 2 | 1.24 | 51 | .15 | 3 | 2.16 | .04 | .10 | 1 | .001 | |
| P 6275 | 3 | 379 | 7 | 559 | .4 | 2 | 9 | 1599 | 5.62 | 22 | 5 | ND | 1 | 6 | 2 | 2 | 2 | 19 | 6.58 | .013 | 2 | 2 | .53 | 9 | .02 | 2 | 1.05 | .01 | .01 | 6 | .002 | |
| P 6276 | 1 | 15 | 5 | 57 | .2 | 2 | 1 | 247 | .25 | 2 | 5 | ND | 1 | 198 | 1 | 2 | 5 | 1 | 26.66 | .002 | 2 | 1 | 2.08 | 2 | .01 | 5 | .04 | .01 | .01 | 1 | .001 | |
| P 6277 | 51 | 632 | 5 | 135 | .5 | 1 | 9 | 1173 | 3.72 | 66 | 5 | ND | 1 | 72 | 2 | 2 | 3 | 39 | 4.92 | .077 | 4 | 1 | .95 | 49 | .06 | 2 | 1.98 | .03 | .08 | 1 | .021 | |
| P 6278 | 7 | 4280 | 19 | 10740 | 2.8 | 7 | 20 | 1156 | 8.41 | 136 | 5 | ND | 1 | 67 | 99 | 2 | 2 | 34 | 5.53 | .039 | 2 | 11 | 2.79 | 34 | .08 | 2 | 2.82 | .17 | .22 | 1 | .007 | |
| P 6279 | 9 | 2588 | 4 | 12658 | 1.6 | 4 | 8 | 275 | 11.34 | 441 | 5 | ND | 1 | 64 | 146 | 2 | 2 | 24 | 5.75 | .011 | 2 | 4 | 1.02 | 8 | .03 | 2 | .84 | .01 | .03 | 1 | .001 | |
| P 6280 | 1 | 115 | 6 | 1218 | .1 | 10 | 8 | 388 | 2.65 | 16 | 5 | ND | 1 | 108 | 28 | 2 | 2 | 17 | 8.84 | .007 | 2 | 16 | 7.02 | 2 | .05 | 13 | 2.47 | .01 | .01 | 1 | .001 | |
| P 6281 | 1 | 323 | 8 | 206 | .3 | 9 | 15 | 890 | 2.95 | 31 | 6 | ND | 1 | 71 | 2 | 2 | 2 | 64 | 4.02 | .054 | 4 | 13 | 3.01 | 31 | .15 | 8 | 3.43 | .11 | .17 | 1 | .004 | |
| P 6282 | 1 | 68 | 2 | 118 | .1 | 1 | 2 | 987 | 1.49 | 7 | 7 | ND | 1 | 399 | 2 | 2 | 3 | 4 | 33.01 | .005 | 2 | 1 | .97 | 18 | .01 | 4 | .40 | .01 | .01 | 1 | .006 | |
| P 6283 | 1 | 1024 | 6 | 1889 | 2.0 | 1 | 6 | 169 | 12.93 | 292 | 5 | ND | 1 | 44 | 24 | 2 | 2 | 7 | 4.99 | .009 | 2 | 2 | .20 | 17 | .01 | 2 | .12 | .01 | .01 | 1 | .001 | |
| P 6284 | 1 | 47 | 3 | 105 | .1 | 8 | 6 | 611 | 2.13 | 10 | 5 | ND | 1 | 76 | 1 | 4 | 2 | 46 | 2.41 | .086 | 7 | 11 | 1.56 | 36 | .12 | 2 | 2.08 | .07 | .07 | 1 | .005 | |
| P 6285 | 2 | 505 | 3 | 181 | .4 | 9 | 23 | 775 | 5.15 | 40 | 5 | ND | 1 | 46 | 1 | 3 | 5 | 58 | 1.61 | .087 | 8 | 12 | 1.66 | 31 | .11 | 2 | 1.64 | .08 | .05 | 1 | .005 | |
| P 6286 | 10 | 1695 | 8 | 9773 | 1.8 | 4 | 82 | 470 | 21.79 | 802 | 5 | ND | 3 | 14 | 106 | 2 | 11 | 38 | .37 | .039 | 3 | 4 | .90 | 9 | .04 | 6 | 1.31 | .06 | .13 | 1 | .015 | |
| STD C | 19 | 61 | 39 | 132 | 7.4 | 71 | 28 | 1044 | 4.11 | 42 | 16 | 8 | 38 | 50 | 18 | 16 | 21 | 57 | .46 | .086 | 38 | 61 | .88 | 179 | .06 | 33 | 1.96 | .06 | .16 | 12 | - | |

- ASSAY REQUIRED FOR CORRECT RESULT

$Cu > 10,000 \text{ ppm}$
 $Po > 35 \text{ ppm}$

VANANDA GOLD

FILE # 87-5763

Page 2

| SAMPLE# | MO PPM | CU PPM | PB PPM | ZN PPM | AG PPM | NI PPM | CD PPM | MN PPM | FE % | AS PPM | U PPM | AU PPM | TH PPM | SR PPM | CD PPM | SB PPM | BI PPM | V PPM | CA PPM | P PPM | LA PPM | CR PPM | MG PPM | BA PPM | TI PPM | B PPM | AL PPM | NA PPM | K PPM | N PPM | AU# OZ/T |
|---------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|----------|----------|-------------|
| P 6287 | 2 | 2 | 3 | 14 | .1 | 1 | 1 | 1757 | .38 | 2 | 5 | ND | 1 | 509 | 1 | 2 | 9 | 4 32.77 | .006 | 3 | 3 | .41 | 5 | .01 | 3 | .23 | .01 | .01 | 1 | .001 | |
| P 6288 | 1 | 117 | 6 | 117 | .1 | 5 | 14 | 392 | 3.96 | 13 | 5 | ND | 1 | 57 | 1 | 2 | 2 | 68 1.10 | .129 | 4 | 15 | 1.25 | 32 | .14 | 5 | 1.75 | .09 | .07 | 1 | .001 | |
| P 6289 | 3 | 199 | 9 | 199 | .1 | 6 | 4 | 507 | 1.61 | 12 | 5 | ND | 1 | 209 | 1 | 2 | 3 | 27 13.49 | .037 | 2 | 14 | 1.54 | 68 | .07 | 8 | 1.86 | .10 | .09 | 1 | .001 | |
| P 6290 | 2 | 77 | 8 | 46 | .1 | 1 | 2 | 233 | .90 | 2 | 5 | ND | 7 | 130 | 1 | 2 | 4 | 10 1.99 | .021 | 12 | 4 | .44 | 81 | .03 | 7 | 2.73 | .19 | .13 | 3 | .001 | |
| P 6291 | 2 | 275 | 7 | 95 | .1 | 11 | 19 | 343 | 2.17 | 19 | 5 | ND | 1 | 255 | 1 | 2 | 2 | 60 3.16 | .147 | 4 | 8 | 2.30 | 122 | .16 | 9 | 4.14 | .11 | .49 | 1 | .003 | |
| P 6292 | 1 | 56 | 9 | 134 | .1 | 3 | 7 | 696 | 2.66 | 2 | 5 | ND | 5 | 30 | 1 | 2 | 2 | 58 1.49 | .119 | 8 | 14 | 5.11 | 17 | .14 | 5 | 3.45 | .06 | .05 | 1 | .001 | |
| P 6293 | 3 | 44 | 6 | 45 | .1 | 2 | 8 | 2207 | 4.30 | 22 | 5 | ND | 4 | 37 | 1 | 2 | 2 | 30 6.33 | .059 | 7 | 4 | .54 | 30 | .07 | 3 | 1.97 | .03 | .03 | 1 | .001 | |
| P 6294 | 5 | 18 | 5 | 42 | .1 | 1 | 6 | 2262 | 4.72 | 19 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 20 7.07 | .050 | 3 | 3 | .46 | 17 | .05 | 2 | 1.81 | .01 | .02 | 3 | .001 | |
| P 6295 | 15 | 69215 | 2 | 655 | 65.7 | 23 | 220 | 859 | 26.08 | 73 | 5 | 4 | 1 | 2 | 5 | 2 | 2 | 8 7.12 | .008 | 3 | 1 | .07 | 2 | .01 | 2 | .32 | .01 | .02 | 41 | .236 | |
| P 6296 | 17 | 2665 | 3 | 71 | 4.2 | 2 | 12 | 1602 | 10.93 | 46 | 5 | ND | 1 | 10 | 1 | 2 | 2 | 35 12.88 | .029 | 4 | 4 | .21 | 4 | .03 | 4 | .82 | .01 | .01 | 178 | .025 | |
| P 6297 | 44 | 55020 | 6 | 311 | 84.3 | 43 | 230 | 746 | 21.01 | 108 | 5 | 12 | 2 | 2 | 4 | 2 | 2 | 10 7.58 | .007 | 5 | 1 | .07 | 3 | .01 | 2 | .54 | .01 | .01 | 98 | .519 | |
| P 6298 | 1 | 545 | 5 | 75 | .3 | 37 | 34 | 945 | 5.08 | 63 | 5 | ND | 1 | 89 | 1 | 2 | 2 | 63 3.56 | .061 | 2 | 47 | 1.19 | 24 | .21 | 5 | 2.29 | .14 | .05 | 1 | .003 | |
| P 6299 | 2 | 1122 | 11 | 91 | 1.5 | 9 | 24 | 2594 | 13.90 | 440 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 23 13.44 | .019 | 2 | 8 | .27 | 8 | .02 | 2 | .72 | .02 | .02 | 6 | .008 | |
| P 6300 | 1 | 505 | 11 | 42 | .1 | 75 | 46 | 446 | 4.55 | 28 | 5 | ND | 1 | 95 | 1 | 2 | 2 | 80 1.54 | .051 | 2 | 78 | .71 | 24 | .31 | 5 | 2.40 | .32 | .04 | 1 | .002 | |
| P 6301 | 1 | 653 | 13 | 55 | .2 | 121 | 93 | 719 | 6.17 | 39 | 5 | ND | 1 | 76 | 1 | 2 | 2 | 79 1.44 | .050 | 2 | 75 | .74 | 18 | .31 | 7 | 2.31 | .31 | .05 | 1 | .003 | |
| P 6302 | 1 | 345 | 2 | 38 | .1 | 99 | 26 | 285 | 3.38 | 22 | 5 | ND | 1 | 179 | 1 | 2 | 2 | 65 1.99 | .055 | 2 | 60 | .48 | 16 | .25 | 3 | 2.47 | .45 | .04 | 1 | .001 | |
| P 6303 | 1 | 370 | 4 | 52 | .1 | 89 | 32 | 356 | 4.92 | 44 | 5 | ND | 1 | 185 | 1 | 2 | 2 | 65 2.33 | .046 | 2 | 64 | .91 | 26 | .21 | 4 | 2.92 | .43 | .08 | 1 | .001 | |
| P 6304 | 1 | 329 | 7 | 54 | .1 | 92 | 36 | 496 | 5.29 | 32 | 5 | ND | 1 | 212 | 1 | 2 | 2 | 88 2.45 | .053 | 2 | 85 | .94 | 45 | .29 | 4 | 3.11 | .45 | .12 | 1 | .001 | |
| P 6305 | 1 | 799 | 5 | 72 | .5 | 103 | 48 | 374 | 6.45 | 28 | 5 | ND | 1 | 147 | 1 | 2 | 3 | 103 2.30 | .060 | 2 | 117 | 1.57 | 46 | .28 | 7 | 3.70 | .39 | .40 | 1 | .004 | |
| P 6306 | 1 | 351 | 9 | 62 | .1 | 71 | 27 | 339 | 4.43 | 30 | 5 | ND | 1 | 164 | 1 | 2 | 2 | 92 3.16 | .070 | 2 | 93 | 1.52 | 50 | .26 | 9 | 4.35 | .24 | .17 | 1 | .001 | |
| P 6307 | 4 | 1298 | 2 | 33 | 2.2 | 11 | 44 | 1168 | 11.23 | 208 | 5 | ND | 1 | 184 | 1 | 2 | 3 | 16 20.47 | .014 | 2 | 6 | .29 | 7 | .02 | 6 | .32 | .01 | .02 | 10 | .002 | |
| P 6308 | 2 | 315 | 3 | 26 | .4 | 7 | 27 | 870 | 4.86 | 14 | 5 | ND | 1 | 166 | 1 | 2 | 2 | 9 19.80 | .013 | 2 | 3 | .34 | 5 | .01 | 3 | .33 | .01 | .01 | 4 | .001 | |
| P 6309 | 1 | 192 | 4 | 91 | .1 | 10 | 20 | 540 | 4.64 | 9 | 5 | ND | 1 | 210 | 1 | 2 | 2 | 138 2.08 | .074 | 3 | 12 | 1.52 | 342 | .27 | 6 | 3.68 | .30 | .44 | 1 | .001 | |
| P 6310 | 1 | 112 | 7 | 86 | .1 | 4 | 11 | 748 | 2.92 | 10 | 5 | ND | 1 | 221 | 1 | 2 | 2 | 60 8.72 | .052 | 3 | 5 | 1.14 | 103 | .15 | 3 | 2.62 | .31 | .07 | 1 | .001 | |
| P 6311 | 2 | 75 | 4 | 261 | .1 | 5 | 12 | 597 | 2.26 | 9 | 5 | ND | 1 | 254 | 3 | 2 | 2 | 67 2.59 | .107 | 4 | 9 | 1.46 | 140 | .14 | 5 | 3.08 | .20 | .12 | 1 | .001 | |
| P 6312 | 1 | 195 | 5 | 177 | .1 | 8 | 17 | 528 | 3.78 | 13 | 5 | ND | 1 | 264 | 1 | 2 | 2 | 78 1.80 | .129 | 3 | 8 | 1.63 | 153 | .16 | 4 | 3.20 | .29 | .12 | 1 | .001 | |
| P 6313 | 2 | 93 | 2 | 48 | .1 | 6 | 14 | 361 | 3.59 | 6 | 5 | ND | 2 | 108 | 1 | 2 | 3 | 73 .89 | .108 | 4 | 9 | 1.01 | 58 | .14 | 4 | 1.76 | .13 | .05 | 2 | .001 | |
| P 6314 | 1 | 68 | 3 | 42 | .1 | 5 | 13 | 431 | 2.96 | 7 | 5 | ND | 1 | 170 | 1 | 2 | 2 | 82 1.50 | .116 | 4 | 5 | 1.03 | 110 | .16 | 4 | 1.99 | .28 | .16 | 1 | .001 | |
| P 6315 | 1 | 48 | 2 | 40 | .1 | 5 | 7 | 642 | 2.04 | 16 | 5 | ND | 1 | 110 | 1 | 2 | 2 | 48 1.94 | .120 | 4 | 5 | .93 | 21 | .13 | 2 | 1.68 | .08 | .05 | 2 | .001 | |
| P 6316 | 1 | 44 | 6 | 53 | .1 | 5 | 6 | 691 | 2.43 | 21 | 5 | ND | 1 | 194 | 1 | 3 | 2 | 48 2.18 | .137 | 3 | 4 | 1.28 | 40 | .12 | 5 | 2.22 | .06 | .04 | 1 | .001 | |
| P 6317 | 1 | 25 | 13 | 54 | .1 | 2 | 1 | 264 | 1.23 | 11 | 5 | ND | 1 | 364 | 1 | 2 | 2 | 28 3.64 | .096 | 3 | 4 | .19 | 40 | .12 | 4 | 4.34 | .58 | .06 | 1 | .001 | |
| P 6318 | 1 | 33 | 7 | 42 | .1 | 2 | 2 | 409 | 1.36 | 14 | 5 | ND | 1 | 426 | 1 | 2 | 2 | 36 4.82 | .103 | 2 | 3 | .27 | 20 | .12 | 5 | 5.14 | .52 | .02 | 2 | .001 | |
| P 6319 | 1 | 1641 | 8 | 196 | .5 | 90 | 101 | 1346 | 7.91 | 6 | 5 | ND | 1 | 94 | 1 | 2 | 2 | 157 .90 | .061 | 3 | 136 | 3.41 | 34 | .16 | 2 | 4.15 | .11 | .05 | 1 | .001 | |
| P 6320 | 1 | 522 | 19 | 136 | .2 | 53 | 57 | 827 | 6.64 | 5 | 5 | ND | 1 | 184 | 1 | 2 | 2 | 156 2.17 | .114 | 5 | 81 | 3.75 | 85 | .16 | 9 | 6.10 | .20 | .07 | 1 | .001 | |
| P 6321 | 1 | 485 | 9 | 138 | .1 | 99 | 47 | 770 | 8.05 | 11 | 5 | ND | 1 | 187 | 1 | 2 | 2 | 158 1.20 | .050 | 2 | 149 | 2.93 | 73 | .22 | 5 | 4.08 | .20 | .03 | 1 | .001 | |
| P 6322 | 1 | 520 | 10 | 241 | .1 | 113 | 73 | 967 | 8.00 | 9 | 5 | ND | 1 | 106 | 1 | 2 | 2 | 184 1.33 | .048 | 2 | 186 | 4.00 | 53 | .19 | 5 | 4.77 | .21 | .03 | 1 | .001 | |
| STD C | 19 | 58 | 36 | 132 | 7.3 | 68 | 29 | 1038 | 4.09 | 39 | 15 | 8 | 38 | 51 | 18 | 16 | 21 | 57 .45 | .089 | 38 | 59 | .86 | 181 | .06 | 35 | 1.95 | .06 | .14 | 11 | - | |

VANANDA GOLD FILE # 87-5763

| SAMPLE# | MO | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SR | CD | SB | BI | V | CA | P | LA | CR | MG | BA | TI | B | AL | NA | K | N | AU88 |
|---------|-----|-----|-----|-----|------|-----|-----|------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|------|-----|-----|------|-----|-----|-----|------|------|-----|---------------|------|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | OZ/T | | | |
| P 6323 | 1 | 140 | 9 | 46 | .2 | 4 | 15 | 430 | 5.36 | 90 | 5 | ND | 3 | 124 | 1 | 2 | 2 | 44 | 3.47 | .114 | 9 | 1 | .93 | 70 | .10 | 2 | 1.80 | .16 | .14 | 3 .001 | |
| P 6324 | 1 | 40 | 2 | 48 | .1 | 3 | 1 | 582 | .92 | 56 | 5 | ND | 1 | 305 | 1 | 2 | 2 | 1 | 29.59 | .069 | 2 | 1 | .03 | 4 | .01 | 7 | .16 | .01 | .04 | 2 .001 | |
| P 6325 | 1 | 16 | 6 | 18 | .1 | 5 | 22 | 1165 | 16.59 | 151 | 5 | ND | 2 | 14 | 1 | 2 | 2 | 5 | 17.56 | .016 | 2 | 2 | .11 | 2 | .01 | 2 | .21 | .01 | .04 | 40 .001 | |
| P 6326 | 1 | 16 | 6 | 16 | .1 | 2 | 6 | 1247 | 13.58 | 88 | 5 | ND | 1 | 10 | 1 | 2 | 2 | 6 | 17.18 | .010 | 2 | 2 | .16 | 2 | .01 | 2 | .29 | .01 | .04 | 21 .001 | |
| P 6327 | 1 | 496 | 2 | 36 | .3 | 6 | 17 | 1079 | 14.13 | 173 | 5 | ND | 1 | 16 | 1 | 2 | 2 | 9 | 14.72 | .035 | 2 | 2 | .16 | 10 | .02 | 4 | .43 | .03 | .05 | 48 .003 | |
| P 6328 | 1 | 570 | 2 | 18 | .3 | 5 | 8 | 898 | 9.37 | 100 | 5 | ND | 1 | 209 | 1 | 2 | 2 | 4 | 23.50 | .024 | 2 | 2 | .12 | 4 | .01 | 4 | .15 | .01 | .04 | 59 .004 | |
| P 6329 | 1 | 60 | 7 | 59 | .1 | 2 | 9 | 296 | 2.84 | 41 | 5 | ND | 1 | 225 | 1 | 2 | 2 | 52 | 3.81 | .130 | 8 | 1 | .90 | 129 | .12 | 3 | 4.90 | .47 | .43 | 1 .004 | |
| P 6330 | 1 | 149 | 7 | 57 | .4 | 68 | 21 | 629 | 4.05 | 34 | 5 | ND | 1 | 183 | 1 | 2 | 2 | 158 | 4.03 | .044 | 2 | 149 | 1.46 | 82 | .14 | 6 | 5.34 | .30 | .43 | 3 .001 | |
| P 6331 | 1 | 124 | 12 | 74 | .4 | 56 | 22 | 915 | 5.22 | 19 | 5 | ND | 1 | 123 | 1 | 2 | 3 | 187 | 17.88 | .068 | 5 | 90 | 1.30 | 18 | .12 | 4 | 2.37 | .01 | .07 | 1 .004 | |
| P 6332 | 1 | 203 | 9 | 104 | .2 | 97 | 44 | 354 | 2.99 | 39 | 5 | ND | 1 | 201 | 1 | 2 | 3 | 136 | 3.20 | .056 | 2 | 145 | 1.09 | 50 | .20 | 4 | 4.04 | .47 | .44 | 1 .001 | |
| P 6333 | 1 | 7 | 4 | 17 | .1 | 3 | 3 | 181 | .94 | 2 | 5 | ND | 8 | 79 | 1 | 2 | 2 | 10 | 1.37 | .015 | 10 | 6 | .30 | 68 | .02 | 2 | 1.76 | .14 | .22 | 1 .006 | |
| P 6334 | 1 | 22 | 4 | 23 | 19.7 | 15 | 11 | 203 | 2.83 | 6 | 5 | 167 | 1 | 114 | 1 | 2 | 2 | 80 | 1.34 | .081 | 4 | 75 | .33 | 36 | .12 | 2 | 1.37 | .25 | .05 | 107.110 ROY'S | |
| STD C | 19 | 59 | 43 | 135 | 7.3 | 69 | 29 | 1065 | 4.02 | 41 | 24 | 7 | 38 | 52 | 18 | 17 | 20 | 60 | .47 | .082 | 39 | 62 | .98 | 181 | .07 | 33 | 1.88 | .06 | .14 | 11 | |

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MM FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: Rock Chips

DATE RECEIVED: NOV 25 1987 DATE REPORT MAILED: Nov 27/87 ASSAYER: D. Toye, DEAN TOYE, CERTIFIED B.C. ASSAYER

VANANDA GOLD LTD. File # 87-5476 Page 1

| SAMPLE | MO | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SR | CD | SB | BI | V | CA | P | LA | CR | MG | BA | TI | B | AL | NA | K | W |
|--------|-----|------|-----|-------|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|------|-----|-----|------|-----|-----|-----|------|-----|-----|----|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | |
| P 8151 | 8 | 174 | 5 | 336 | .4 | 4 | 6 | 732 | 2.42 | 36 | 5 | ND | 2 | 79 | 3 | 2 | 2 | 35 | 2.58 | .087 | 3 | 5 | .73 | 10 | .11 | 2 | 1.01 | .04 | .04 | 1 |
| P 8152 | 1 | 78 | 5 | 390 | .4 | 2 | 4 | 545 | 1.33 | 8 | 5 | ND | 3 | 28 | 2 | 2 | 2 | 19 | 1.34 | .043 | 5 | 3 | .49 | 14 | .10 | 3 | .64 | .07 | .04 | 1 |
| P 8153 | 1 | 45 | 5 | 102 | .5 | 1 | 2 | 455 | 1.34 | 7 | 5 | ND | 5 | 15 | 1 | 2 | 2 | 21 | 1.62 | .048 | 7 | 1 | .23 | 7 | .11 | 2 | .40 | .07 | .02 | 1 |
| P 8154 | 3 | 2785 | 7 | 3473 | .6 | 8 | 11 | 1194 | 3.59 | 27 | 5 | ND | 4 | 19 | 5 | 2 | 2 | 28 | 2.69 | .079 | 4 | 12 | .56 | 24 | .05 | 2 | 1.42 | .04 | .03 | 2 |
| P 8155 | 1 | 179 | 10 | 357 | .3 | 6 | 11 | 597 | 3.70 | 44 | 5 | ND | 2 | 207 | 5 | 3 | 2 | 70 | 2.58 | .085 | 3 | 6 | 1.88 | 145 | .14 | 2 | 3.37 | .22 | .25 | 1 |
| P 8156 | 3 | 957 | 8 | 180 | 1.3 | 1 | 16 | 1304 | 7.72 | 142 | 5 | ND | 2 | 13 | 2 | 2 | 2 | 19 | 2.64 | .013 | 2 | 2 | .61 | 24 | .04 | 2 | 1.14 | .03 | .02 | 1 |
| P 8157 | 9 | 2492 | 13 | 795 | 4.6 | 2 | 23 | 779 | 22.27 | 955 | 5 | ND | 3 | 11 | 14 | 2 | 2 | 27 | .92 | .013 | 2 | 4 | .31 | 19 | .03 | 2 | .66 | .03 | .02 | 1 |
| P 8158 | 1 | 2035 | 2 | 1039 | .6 | 11 | 19 | 706 | 3.16 | 34 | 5 | ND | 3 | 34 | 4 | 2 | 2 | 48 | .69 | .043 | 8 | 13 | .61 | 28 | .10 | 2 | 2.91 | .08 | .05 | 1 |
| P 8159 | 9 | 4289 | 14 | 22340 | 2.3 | 2 | 16 | 69 | 22.06 | 365 | 5 | ND | 3 | 2 | 298 | 2 | 2 | 4 | .07 | .001 | 2 | 5 | .03 | 4 | .01 | 2 | .09 | .01 | .01 | 1 |
| P 8160 | 3 | 177 | 7 | 139 | .6 | 6 | 26 | 493 | 2.49 | 25 | 5 | ND | 3 | 60 | 1 | 7 | 2 | 29 | 2.39 | .082 | 4 | 3 | 3.27 | 423 | .14 | 3 | 3.02 | .07 | .73 | 2 |
| P 8161 | 2 | 1213 | 6 | 551 | 1.8 | 10 | 24 | 437 | 2.56 | 40 | 5 | ND | 2 | 88 | 7 | 2 | 2 | 41 | 2.74 | .125 | 3 | 4 | 1.83 | 188 | .13 | 3 | 1.90 | .11 | .17 | 1 |
| P 8162 | 6 | 451 | 6 | 89 | 1.2 | 7 | 37 | 517 | 2.56 | 32 | 5 | ND | 2 | 79 | 1 | 3 | 2 | 44 | 2.61 | .114 | 4 | 4 | 2.14 | 370 | .15 | 2 | 2.21 | .08 | .34 | 1 |
| P 8163 | 23 | 230 | 4 | 95 | 1.0 | 6 | 19 | 549 | 2.49 | 39 | 5 | ND | 3 | 87 | 1 | 3 | 2 | 45 | 3.01 | .134 | 5 | 5 | 2.06 | 172 | .13 | 4 | 2.24 | .10 | .12 | 1 |
| P 8164 | 8 | 21 | 5 | 17 | .3 | 1 | 2 | 1312 | 3.11 | 9 | 6 | ND | 3 | 4 | 1 | 2 | 2 | 20 | 5.54 | .024 | 2 | 1 | .21 | 3 | .04 | 2 | 1.24 | .01 | .01 | 1 |
| P 8165 | 6 | 27 | 3 | 23 | .5 | 1 | 3 | 1394 | 2.85 | 9 | 5 | ND | 4 | 6 | 1 | 2 | 2 | 15 | 4.75 | .013 | 2 | 1 | .23 | 4 | .03 | 2 | 1.15 | .01 | .01 | 2 |
| P 8166 | 3 | 90 | 4 | 51 | .4 | 3 | 7 | 1558 | 4.31 | 13 | 5 | ND | 3 | 11 | 1 | 2 | 2 | 18 | 6.32 | .028 | 3 | 2 | .98 | 2 | .02 | 2 | 1.63 | .01 | .01 | 1 |
| P 8167 | 8 | 48 | 2 | 24 | .5 | 2 | 4 | 1347 | 2.94 | 10 | 5 | ND | 2 | 11 | 1 | 2 | 2 | 14 | 4.70 | .043 | 4 | 2 | .77 | 3 | .03 | 2 | 1.19 | .01 | .01 | 2 |
| P 8168 | 4 | 87 | 4 | 36 | .1 | 3 | 8 | 1260 | 3.07 | 6 | 5 | ND | 1 | 3 | 1 | 2 | 2 | 18 | 4.25 | .009 | 2 | 2 | .68 | 3 | .02 | 2 | 1.01 | .01 | .01 | 1 |
| P 8169 | 8 | 28 | 2 | 39 | .4 | 2 | 5 | 1228 | 2.34 | 17 | 5 | ND | 3 | 32 | 1 | 2 | 2 | 27 | 3.92 | .089 | 4 | 3 | 1.70 | 5 | .07 | 2 | 1.43 | .02 | .01 | 1 |
| P 8170 | 1 | 7 | 2 | 17 | .6 | 1 | 1 | 1560 | .42 | 2 | 5 | ND | 2 | 373 | 1 | 2 | 2 | 1 | 33.50 | .003 | 2 | 1 | .64 | 3 | .01 | 2 | .09 | .01 | .01 | 1 |
| P 8171 | 2 | 54 | 7 | 223 | .4 | 9 | 16 | 1450 | 4.54 | 26 | 5 | ND | 3 | 207 | 1 | 3 | 2 | 116 | 4.27 | .062 | 3 | 8 | 2.12 | 121 | .19 | 2 | 4.33 | .26 | .14 | 1 |
| P 8172 | 5 | 2256 | 2 | 140 | 2.0 | 15 | 42 | 593 | 2.13 | 27 | 5 | ND | 2 | 30 | 1 | 6 | 2 | 23 | 3.62 | .086 | 3 | 1 | 1.83 | 29 | .10 | 3 | 1.94 | .03 | .11 | 1 |
| P 8173 | 8 | 2167 | 4 | 133 | 2.8 | 6 | 52 | 620 | 2.39 | 34 | 5 | ND | 2 | 51 | 1 | 22 | 2 | 27 | 4.24 | .050 | 5 | 1 | 1.77 | 107 | .13 | 10 | 2.29 | .04 | .15 | 1 |
| P 8174 | 1 | 157 | 7 | 47 | .5 | 3 | 4 | 689 | 1.60 | 11 | 5 | ND | 7 | 110 | 1 | 3 | 2 | 13 | 5.32 | .042 | 8 | 2 | 1.84 | 36 | .04 | 2 | 2.19 | .07 | .07 | 1 |
| P 8175 | 4 | 36 | 3 | 43 | .3 | 3 | 4 | 319 | 1.28 | 3 | 5 | ND | 6 | 67 | 1 | 2 | 2 | 18 | 1.08 | .053 | 6 | 3 | .89 | 38 | .07 | 2 | 1.70 | .10 | .09 | 3 |
| P 8176 | 1 | 82 | 3 | 155 | .4 | 3 | 6 | 297 | 1.54 | 4 | 5 | ND | 6 | 161 | 1 | 2 | 2 | 22 | 1.36 | .039 | 7 | 2 | .85 | 86 | .06 | 2 | 2.36 | .14 | .21 | 1 |
| P 8177 | 1 | 99 | 2 | 105 | .5 | 3 | 8 | 278 | 1.79 | 4 | 5 | ND | 7 | 29 | 1 | 2 | 2 | 19 | .67 | .045 | 9 | 2 | .79 | 22 | .08 | 3 | .93 | .07 | .08 | 1 |
| P 8178 | 3 | 425 | 3 | 160 | .7 | 5 | 14 | 809 | 6.42 | 36 | 5 | ND | 3 | 201 | 1 | 2 | 2 | 15 | 21.71 | .025 | 3 | 3 | .84 | 19 | .02 | 2 | .69 | .01 | .03 | 3 |
| P 8179 | 2 | 1013 | 13 | 107 | 1.6 | 21 | 22 | 1114 | 25.75 | 139 | 5 | ND | 4 | 7 | 1 | 2 | 2 | 14 | 5.86 | .041 | 2 | 1 | .13 | 2 | .01 | 2 | .41 | .01 | .01 | 2 |
| P 8180 | 1 | 6063 | 14 | 306 | 4.8 | 38 | 29 | 725 | 22.79 | 72 | 5 | ND | 3 | 28 | 3 | 2 | 2 | 25 | 2.73 | .015 | 2 | 11 | .39 | 7 | .05 | 2 | .61 | .04 | .01 | 1 |
| P 8181 | 1 | 313 | 11 | 92 | .8 | 22 | 27 | 907 | 27.50 | 51 | 5 | ND | 4 | 5 | 1 | 2 | 2 | 18 | 3.83 | .025 | 2 | 1 | .22 | 2 | .03 | 2 | .40 | .02 | .01 | 1 |
| P 8182 | 3 | 307 | 16 | 126 | .8 | 31 | 35 | 787 | 44.24 | 32 | 5 | ND | 5 | 6 | 1 | 2 | 2 | 18 | 1.29 | .007 | 2 | 6 | .18 | 5 | .03 | 2 | .22 | .02 | .01 | 1 |
| P 8183 | 2 | 641 | 14 | 123 | 1.5 | 35 | 29 | 1666 | 15.79 | 62 | 5 | ND | 3 | 69 | 1 | 2 | 2 | 64 | 5.79 | .042 | 2 | 62 | 2.04 | 7 | .09 | 2 | 2.08 | .02 | .01 | 1 |
| P 8184 | 3 | 104 | 15 | 74 | .8 | 14 | 26 | 761 | 37.37 | 76 | 5 | ND | 4 | 4 | 1 | 2 | 2 | 18 | 1.51 | .017 | 2 | 2 | .12 | 3 | .02 | 2 | .20 | .03 | .02 | 1 |
| P 8185 | 1 | 3171 | 16 | 188 | 4.0 | 31 | 26 | 699 | 30.91 | 34 | 5 | ND | 4 | 4 | 2 | 2 | 2 | 20 | 2.29 | .008 | 2 | 1 | .11 | 4 | .01 | 2 | .21 | .02 | .01 | 2 |
| P 8186 | 1 | 102 | 6 | 37 | .7 | 11 | 15 | 413 | 4.19 | 12 | 5 | ND | 2 | 162 | 1 | 2 | 2 | 110 | 2.06 | .143 | 6 | 12 | .84 | 134 | .17 | 4 | 2.78 | .35 | .26 | 1 |
| GR C | 18 | 57 | 37 | 132 | 7.4 | 68 | 27 | 1032 | 4.05 | 41 | 24 | 7 | 38 | 50 | 18 | 18 | 21 | 56 | .48 | .086 | 37 | 58 | .86 | 178 | .08 | 32 | 1.88 | .09 | .14 | 12 |

VANANDA GOLD LTD.

SLE # 87-5476

| | NO | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SR | CD | Sb | Bi | V | Ca | P | LA | CR | Mg | BA | Tl | B | Al | Na | K | N |
|--------|-----|------|-----|------|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|------|-----|-----|------|-----|-----|-----|------|-----|-----|----|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | |
| P 6187 | 1 | 280 | 10 | 168 | .8 | 111 | 34 | 769 | 7.42 | 7 | 12 | ND | 2 | 71 | 1 | 2 | 2 | 218 | .62 | .050 | 2 | 239 | 4.67 | 53 | .25 | 3 | 4.63 | .13 | .03 | 1 |
| P 6188 | 1 | 261 | 8 | 179 | .3 | 103 | 32 | 685 | 7.47 | 7 | 5 | ND | 1 | 47 | 1 | 2 | 2 | 193 | .44 | .050 | 2 | 229 | 4.50 | 28 | .21 | 2 | 4.13 | .12 | .03 | 1 |
| P 6189 | 2 | 2061 | 8 | 96 | 1.3 | 49 | 36 | 2342 | 11.27 | 131 | 5 | ND | 2 | 38 | 1 | 2 | 2 | 72 | 7.80 | .018 | 2 | 68 | .76 | 10 | .13 | 2 | 1.36 | .01 | .03 | 4 |
| P 6190 | 1 | 6333 | 7 | 282 | 3.1 | 72 | 45 | 1064 | 7.79 | 63 | 3 | ND | 1 | 63 | 2 | 2 | 2 | 79 | 3.80 | .041 | 2 | 108 | 1.47 | 19 | .27 | 3 | 2.01 | .04 | .05 | 1 |
| P 6191 | 1 | 3093 | 5 | 165 | .9 | 106 | 67 | 991 | 5.92 | 24 | 5 | ND | 1 | 98 | 1 | 2 | 2 | 95 | 2.12 | .051 | 2 | 143 | 1.87 | 32 | .27 | 4 | 2.72 | .17 | .03 | 1 |
| P 6192 | 1 | 481 | 4 | 84 | 1.0 | 49 | 22 | 633 | 3.57 | 64 | 5 | ND | 1 | 137 | 1 | 2 | 2 | 70 | 3.56 | .043 | 2 | 64 | .63 | 16 | .27 | 2 | 2.99 | .26 | .03 | 1 |
| P 6193 | 1 | 349 | 9 | 56 | .7 | 83 | 31 | 292 | 3.53 | 24 | 6 | ND | 1 | 125 | 1 | 2 | 2 | 67 | 2.06 | .047 | 2 | 83 | .82 | 40 | .25 | 2 | 3.48 | .44 | .04 | 1 |
| P 6194 | 1 | 188 | 8 | 194 | .6 | 110 | 35 | 725 | 7.59 | 12 | 5 | ND | 1 | 61 | 1 | 2 | 2 | 169 | .79 | .052 | 2 | 200 | 3.44 | 29 | .23 | 5 | 3.34 | .13 | .02 | 1 |
| P 6195 | 1 | 192 | 7 | 93 | .8 | 90 | 34 | 601 | 6.93 | 12 | 9 | ND | 1 | 93 | 1 | 2 | 2 | 135 | 1.15 | .047 | 2 | 159 | 2.44 | 39 | .35 | 5 | 2.82 | .16 | .03 | 1 |
| P 6196 | 7 | 1764 | 15 | 2390 | 1.7 | 15 | 60 | 1277 | 18.46 | 79 | 5 | ND | 3 | 161 | 21 | 2 | 2 | 54 | 10.37 | .027 | 2 | 38 | .50 | 8 | .10 | 2 | 1.21 | .01 | .01 | 94 |
| P 6197 | 2 | 536 | 9 | 117 | 1.5 | 39 | 24 | 1209 | 10.40 | 44 | 5 | ND | 1 | 108 | 1 | 2 | 2 | 117 | 4.01 | .041 | 2 | 134 | 1.99 | 41 | .22 | 2 | 3.32 | .11 | .04 | 1 |
| P 6198 | 1 | 1007 | 10 | 209 | 2.1 | 126 | 47 | 938 | 8.15 | 29 | 6 | ND | 1 | 129 | 1 | 2 | 2 | 115 | 2.81 | .048 | 2 | 151 | 2.72 | 49 | .25 | 2 | 3.86 | .15 | .05 | 1 |
| P 6199 | 1 | 392 | 6 | 131 | 1.0 | 102 | 37 | 881 | 8.18 | 16 | 6 | ND | 1 | 104 | 1 | 2 | 2 | 161 | 1.49 | .047 | 2 | 172 | 3.41 | 34 | .31 | 2 | 3.63 | .13 | .03 | 1 |
| STD C | 18 | 58 | 40 | 134 | 7.5 | 69 | 27 | 1043 | 4.12 | 40 | 20 | 7 | 39 | 50 | 18 | 18 | 18 | 57 | .49 | .089 | 38 | 59 | .88 | 181 | .08 | 31 | 1.92 | .08 | .14 | 13 |

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: NOV 2 1987
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE (604) 253-3158 FAX (604) 253-1716 DATE REPORT MAILED: Nov 20/87.

ASSAY CERTIFICATE

- SAMPLE TYPE: Rock Chips AU** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

VANANDA GOLD LTD. File # 87-5476 Page 1

| SAMPLE# | AU** oz/t |
|---------|--------------|
|---------|--------------|

| | |
|--------|------|
| P 6151 | .002 |
| P 6152 | .001 |
| P 6153 | .001 |
| P 6154 | .018 |
| P 6155 | .002 |

| | |
|--------|------|
| P 6156 | .010 |
| P 6157 | .039 |
| P 6158 | .002 |
| P 6159 | .018 |
| P 6160 | .005 |

| | |
|--------|------|
| P 6161 | .018 |
| P 6162 | .017 |
| P 6163 | .005 |
| P 6164 | .001 |
| P 6165 | .001 |

| | |
|--------|------|
| P 6166 | .001 |
| P 6167 | .001 |
| P 6168 | .001 |
| P 6169 | .001 |
| P 6170 | .001 |

| | |
|--------|------|
| P 6171 | .001 |
| P 6172 | .022 |
| P 6173 | .029 |
| P 6174 | .006 |
| P 6175 | .001 |

| | |
|--------|------|
| P 6176 | .001 |
| P 6177 | .001 |
| P 6178 | .001 |
| P 6179 | .004 |
| P 6180 | .006 |

| | |
|--------|------|
| P 6181 | .002 |
| P 6182 | .001 |
| P 6183 | .001 |
| P 6184 | .002 |
| P 6185 | .021 |

| | |
|--------|------|
| P 6186 | .001 |
|--------|------|

SAMPLE# AU**
 oz/t

P 6187 .001

P 6188 .001

P 6189 .001

P 6190 .001

P 6191 .001

P 6192 .001

P 6193 .001

P 6194 .001

P 6195 .010

P 6196 .001

P 6197 .002

P 6198 .006

P 6199 .012

ACME ANALYTICAL LABORATORIES
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: AUG 13 1987
DATE REPORT MAILED: Aug. 22/87.

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MB BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1 TO P1B-SOIL P19-ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

P-20 MESH, PULVERIZED

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

VANANDA GOLD LTD. File # 87-3273 Page 1

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 9700E 10075N | 1 | 49 | 19 | 7 | 3 | 15 |
| 9700E 10050N | 1 | 9 | 4 | 3 | 3 | 16 |
| 9700E 10025N | 1 | 92 | 12 | 16 | 9 | 3 |
| 9700E 10000N | 1 | 62 | 13 | 22 | 7 | 2 |
| 9700E 9975N | 1 | 73 | 12 | 14 | 5 | 4 |
| 9700E 9950N | 1 | 50 | 11 | 10 | 5 | 26 |
| 9700E 9925N | 1 | 120 | 9 | 19 | 9 | 9 |
| 9700E 9900N | 1 | 22 | 16 | 13 | 6 | 1 |
| 9700E 9875N | 1 | 24 | 9 | 7 | 4 | 1 |
| 9700E 9825N | 1 | 168 | 9 | 12 | 8 | 16 |
| 9700E 9800N | 2 | 35 | 18 | 10 | 2 | 48 |
| 9700E 9775N | 1 | 217 | 6 | 31 | 7 | 6 |
| 9700E 9750N | 1 | 187 | 12 | 17 | 5 | 17 |
| 9700E 9725N P | 1 | 42 | 10 | 10 | 3 | 7 |
| 9700E 9700N | 1 | 189 | 19 | 34 | 4 | 9 |
| 9700E 9675N | 1 | 95 | 5 | 24 | 2 | 3 |
| 9700E 9650N | 1 | 83 | 8 | 20 | 5 | 2 |
| 9700E 9625N | 2 | 38 | 14 | 21 | 3 | 5 |
| 9700E 9600N | 1 | 26 | 10 | 17 | 2 | 1 |
| 9700E 9575N | 1 | 29 | 11 | 8 | 3 | 22 |
| 9700E 9550N | 1 | 32 | 13 | 9 | 2 | 15 |
| 9700E 9500N | 2 | 133 | 16 | 17 | 14 | 6 |
| 9750E 10475N | 1 | 79 | 14 | 31 | 5 | 2 |
| 9750E 10075N | 2 | 140 | 5 | 31 | 9 | 2 |
| 9750E 10050N | 1 | 87 | 16 | 20 | 9 | 7 |
| 9750E 10025N | 1 | 205 | 12 | 13 | 7 | 9 |
| 9750E 10000N | 1 | 74 | 11 | 10 | 5 | 7 |
| 9750E 9900N | 1 | 55 | 10 | 10 | 7 | 1 |
| 9750E 9875N | 1 | 20 | 13 | 5 | 4 | 1 |
| 9750E 9850N | 1 | 126 | 8 | 9 | 5 | 6 |
| 9750E 9825N | 1 | 162 | 9 | 13 | 3 | 4 |
| 9750E 9800N | 1 | 32 | 9 | 11 | 3 | 1 |
| 9750E 9775N | 1 | 8 | 9 | 3 | 3 | 2 |
| 9750E 9750N | 1 | 43 | 11 | 9 | 6 | 3 |
| 9750E 9725N | 1 | 42 | 12 | 25 | 2 | 5 |
| 9750E 9700N | 1 | 114 | 11 | 30 | 2 | 12 |
| STD C/AU-S | 19 | 60 | 42 | 28 | 39 | 49 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|-----------------|-----------|-----------|-----------|-----------|-----------|------------|
| 9750E 9675N | 1 | 68 | 14 | 21 | 2 | 15 |
| 9750E 9650N | 1 | 151 | 17 | 16 | 27 | 2 |
| 9750E 9625N | 1 | 325 | 12 | 40 | 3 | 11 |
| 9750E 9600N | 1 | 161 | 17 | 29 | 2 | 315 |
| 9750E 9575N | 1 | 204 | 14 | 13 | 4 | 12 |
| 9750E 9550N | 1 | 219 | 16 | 9 | 6 | 10 |
| 9750E 9525N | 1 | 196 | 8 | 32 | 2 | 1 |
| 9750E 9500N | 2 | 192 | 14 | 31 | 2 | 1 |
| 9800E 10475N | 1 | 9 | 12 | 4 | 8 | 25 |
| 9850E 10400N | 1 | 24 | 19 | 8 | 81 | 4 |
| 9850E 9800N | 1 | 29 | 22 | 5 | 10 | 7 |
| 9850E 9775N | 2 | 21 | 19 | 4 | 8 | 2 |
| 9850E 9750N P | 2 | 16 | 33 | 3 | 10 | 4 |
| 9850E 9725N | 1 | 10 | 24 | 3 | 4 | 1 |
| 9850E 9700N | 1 | 25 | 29 | 13 | 8 | 3 |
| 9900E 9750N P | 1 | 184 | 21 | 12 | 10 | 485 |
| 9950E 9750N | 1 | 176 | 19 | 10 | 9 | 70 |
| 10000E 10425N | 1 | 21 | 12 | 6 | 5 | 6 |
| 10050E 10425N P | 1 | 16 | 26 | 3 | 6 | 12 |
| 10050E 9875N | 1 | 19 | 26 | 5 | 7 | 6 |
| 10050E 9850N | 1 | 23 | 85 | 5 | 38 | 143 |
| 10050E 9800N | 5 | 29 | 33 | 8 | 83 | 9 |
| 10050E 9775N | 1 | 35 | 31 | 8 | 36 | 25 |
| 10100E 10450N P | 1 | 74 | 20 | 10 | 31 | 28 |
| 10100E 10425N | 1 | 9 | 11 | 3 | 5 | 102 |
| 10100E 10350N P | 1 | 27 | 31 | 6 | 9 | 57 |
| 10150E 10450N | 1 | 42 | 46 | 6 | 9 | 20 |
| 10150E 10300N | 1 | 36 | 30 | 8 | 6 | 94 |
| 10150E 10225N P | 1 | 35 | 42 | 5 | 38 | 10 |
| 10150E 10200N | 1 | 141 | 24 | 8 | 8 | 29 |
| 10150E 9775N P | 3 | 253 | 28 | 32 | 27 | 55 |
| 10150E 9750N P | 3 | 99 | 22 | 25 | 30 | 59 |
| 10150E 9700N | 1 | 18 | 24 | 7 | 5 | 79 |
| 10150E 9675N | 1 | 34 | 17 | 9 | 5 | 16 |
| 10150E 9650N | 1 | 23 | 48 | 8 | 14 | 2 |
| 10150E 9625N | 1 | 19 | 13 | 6 | 4 | 10 |
| STD C/AU-S | 19 | 60 | 39 | 27 | 39 | 53 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|-----------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10150E 9600N | 1 | 47 | 18 | 7 | 7 | 12 |
| 10150E 9575N | 1 | 82 | 17 | 9 | 7 | 5 |
| 10150E 9550N P | 1 | 41 | 22 | 8 | 6 | 7 |
| 10150E 9525N | 1 | 8884 | 41 | 8 | 6 | 172 |
| 10150E 9500N | 1 | 78 | 13 | 10 | 4 | 4 |
| 10200E 10400N | 1 | 41 | 17 | 7 | 7 | 4 |
| 10200E 10275N P | 5 | 119 | 25 | 12 | 24 | 8 |
| 10200E 10250N | 1 | 40 | 47 | 8 | 9 | 4 |
| 10200E 10225N | 1 | 60 | 38 | 8 | 12 | 5 |
| 10200E 10200N | 1 | 23 | 31 | 3 | 11 | 1 |
| 10200E 10175N | 3 | 67 | 61 | 10 | 29 | 3 |
| 10200E 10150N | 1 | 56 | 17 | 11 | 14 | 1 |
| 10200E 10125N | 2 | 53 | 42 | 11 | 23 | 3 |
| 10200E 10100N | 1 | 20 | 21 | 7 | 4 | 1 |
| 10200E 10075N | 4 | 32 | 37 | 12 | 24 | 2 |
| 10200E 10050N | 2 | 15 | 12 | 6 | 4 | 4 |
| 10200E 10025N | 8 | 33 | 34 | 10 | 9 | 4 |
| 10200E 9975N | 1 | 22 | 43 | 5 | 12 | 1 |
| 10200E 9950N | 1 | 24 | 12 | 5 | 3 | 6 |
| 10200E 9925N | 2 | 27 | 21 | 8 | 8 | 3 |
| 10200E 9900N | 1 | 4 | 8 | 1 | 2 | 1 |
| 10200E 9875N | 2 | 19 | 33 | 3 | 7 | 1 |
| 10200E 9850N | 2 | 24 | 27 | 9 | 11 | 2 |
| 10200E 9825N | 2 | 18 | 31 | 5 | 9 | 1 |
| 10200E 9800N | 1 | 30 | 19 | 7 | 6 | 250 |
| 10200E 9775N | 2 | 18 | 23 | 7 | 63 | 1 |
| 10200E 9750N | 1 | 27 | 14 | 6 | 8 | 3 |
| 10200E 9725N | 1 | 18 | 19 | 6 | 6 | 6 |
| STD C/AU-S | 20 | 62 | 41 | 28 | 39 | 53 |
| 10200E 9700N P | 1 | 17 | 36 | 3 | 6 | 49 |
| 10200E 9675N | 2 | 34 | 48 | 5 | 11 | 1 |
| 10200E 9650N | 1 | 24 | 46 | 8 | 12 | 4 |
| 10200E 9600N | 1 | 9 | 12 | 3 | 2 | 6 |
| 10200E 9575N | 1 | 26 | 25 | 8 | 5 | 1 |
| 10200E 9550N | 1 | 29 | 17 | 7 | 6 | 1 |
| 10200E 9525N | 1 | 15 | 20 | 4 | 3 | 52 |
| 10200E 9500N | 1 | 22 | 16 | 2 | 2 | 2 |

| SAMPLE# | | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|------------|--------|-----------|-----------|-----------|-----------|-----------|------------|
| 10250E | 10450N | 1 | 1030 | 22 | 7 | 2 | 1010 |
| 10250E | 10425N | 1 | 30 | 23 | 4 | 4 | 11 |
| 10250E | 10400N | 1 | 40 | 31 | 7 | 8 | 1 |
| 10250E | 10375N | 17 | 5311 | 50 | 10 | 36 | 795 |
| 10250E | 10350N | 3 | 124 | 100 | 4 | 45 | 1 |
| 10250E | 10325N | 1 | 120 | 104 | 4 | 12 | 15 |
| 10250E | 10300N | 1 | 39 | 28 | 2 | 10 | 1 |
| 10250E | 10275N | 3 | 93 | 131 | 12 | 13 | 103 |
| 10250E | 10250N | 1 | 17 | 45 | 4 | 23 | 1 |
| 10250E | 10225N | 1 | 33 | 18 | 10 | 8 | 1 |
| 10250E | 10200N | 1 | 29 | 17 | 9 | 5 | 1 |
| 10250E | 10175N | 1 | 38 | 30 | 12 | 10 | 1 |
| 10250E | 10150N | 1 | 63 | 14 | 8 | 5 | 73 |
| 10250E | 10125N | 1 | 8 | 11 | 2 | 2 | 185 |
| 10250E | 10100N | 3 | 177 | 17 | 3 | 8 | 1 |
| 10250E | 10075N | 1 | 50 | 35 | 6 | 11 | 2 |
| 10250E | 10000N | 1 | 28 | 35 | 1 | 5 | 1 |
| 10250E | 9975N | 1 | 37 | 20 | 8 | 7 | 1 |
| 10250E | 9950N | 1 | 20 | 19 | 8 | 2 | 2 |
| 10250E | 9925N | 1 | 70 | 2 | 1 | 7 | 1 |
| 10250E | 9900N | 1 | 60 | 11 | 6 | 9 | 2 |
| 10250E | 9875N | 1 | 37 | 26 | 6 | 8 | 1 |
| 10250E | 9850N | 1 | 22 | 19 | 5 | 10 | 2 |
| 10250E | 9775N | 3 | 30 | 50 | 7 | 41 | 2 |
| 10250E | 9750N | 2 | 14 | 35 | 4 | 9 | 1 |
| 10250E | 9725N | 1 | 22 | 15 | 5 | 4 | 2 |
| 10250E | 9700N | 1 | 48 | 13 | 5 | 4 | 1 |
| 10250E | 9675N | 1 | 40 | 18 | 7 | 9 | 1 |
| 10250E | 9650N | 1 | 40 | 28 | 14 | 23 | 6 |
| 10250E | 9625N | 1 | 11 | 15 | 5 | 2 | 1 |
| 10250E | 9600N | 1 | 13 | 18 | 6 | 3 | 2 |
| 10250E | 9575N | 1 | 25 | 14 | 7 | 3 | 1 |
| 10250E | 9550N | 1 | 19 | 15 | 5 | 2 | 2 |
| 10250E | 9525N | 1 | 30 | 13 | 6 | 2 | 1 |
| 10250E | 9500N | 2 | 136 | 35 | 5 | 5 | 2 |
| 10300E | 10600N | 1 | 60 | 59 | 5 | 6 | 2 |
| STD C/AU-S | | 19 | 60 | 42 | 27 | 37 | 47 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10300E 10500N | 1 | 18 | 12 | 4 | 3 | 2 |
| 10300E 10475N | 1 | 66 | 61 | 4 | 12 | 5 |
| 10300E 10450N | 1 | 13 | 15 | 3 | 3 | 1 |
| 10300E 10425N | 1 | 36 | 52 | 3 | 7 | 38 |
| 10300E 10400N | 1 | 26 | 18 | 7 | 2 | 1 |
| 10300E 10375N | 1 | 28 | 39 | 4 | 17 | 86 |
| 10300E 10350N | 1 | 40 | 51 | 13 | 25 | 2 |
| 10300E 10325N | 30 | 4095 | 18 | 6 | 16 | 510 |
| 10300E 10300N | 1 | 59 | 33 | 12 | 23 | 1 |
| 10300E 10275N | 10 | 10651 | 15 | 16 | 23 | 3300 |
| 10300E 10250N | 172 | 248 | 30 | 18 | 52 | 1 |
| 10300E 10225N | 10 | 114 | 65 | 28 | 91 | 1 |
| 10300E 10200N | 4 | 36 | 67 | 11 | 16 | 1 |
| 10300E 10175N | 1 | 18 | 61 | 6 | 11 | 1 |
| 10300E 10150N | 1 | 15 | 15 | 7 | 8 | 1 |
| 10300E 10125N | 7 | 90 | 30 | 26 | 37 | 1 |
| 10300E 10100N | 1 | 56 | 17 | 7 | 5 | 2 |
| 10300E 10075N | 1 | 18 | 16 | 5 | 4 | 1 |
| 10300E 10050N | 2 | 20 | 43 | 6 | 5 | 3 |
| 10300E 10025N | 3 | 117 | 46 | 14 | 19 | 1 |
| 10300E 10000N | 3 | 85 | 43 | 11 | 27 | 2 |
| 10300E 9975N | 2 | 32 | 62 | 9 | 40 | 1 |
| 10300E 9950N | 1 | 24 | 17 | 5 | 8 | 2 |
| 10300E 9925N | 1 | 14 | 15 | 6 | 3 | 1 |
| 10300E 9900N | 1 | 35 | 39 | 10 | 11 | 2 |
| 10300E 9875N | 1 | 25 | 62 | 4 | 12 | 1 |
| 10300E 9850N | 14 | 50 | 58 | 12 | 70 | 2 |
| 10300E 9825N | 2 | 27 | 59 | 7 | 13 | 1 |
| 10300E 9800N | 7 | 47 | 80 | 20 | 42 | 1 |
| 10300E 9775N | 1 | 19 | 28 | 6 | 6 | 2 |
| 10300E 9750N | 1 | 25 | 68 | 8 | 8 | 5 |
| 10300E 9700N | 1 | 25 | 40 | 3 | 14 | 2 |
| 10300E 9675N | 2 | 20 | 40 | 2 | 11 | 1 |
| 10300E 9575N | 1 | 86 | 21 | 7 | 5 | 3 |
| 10300E 9525N | 1 | 28 | 24 | 7 | 8 | 1 |
| 10300E 9500N | 1 | 20 | 26 | 5 | 14 | 2 |
| STD C/AU-S | 18 | 62 | 40 | 28 | 39 | 47 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10350E 10500N | 2 | 57 | 57 | 8 | 29 | 3 |
| 10350E 10475N | 2 | 69 | 53 | 3 | 13 | 1 |
| 10350E 10450N | 2 | 95 | 45 | 2 | 8 | 2 |
| 10350E 10425N | 1 | 39 | 18 | 6 | 17 | 1 |
| 10350E 10400N | 1 | 36 | 13 | 6 | 21 | 1 |
| 10350E 10375N | 1 | 20 | 11 | 5 | 76 | 1 |
| 10350E 10350N | 1 | 18 | 9 | 4 | 10 | 4 |
| 10350E 10325N | 1 | 31 | 19 | 7 | 5 | 1 |
| 10350E 10300N | 1 | 45 | 10 | 4 | 7 | 13 |
| 10350E 10275N | 1 | 39 | 33 | 6 | 10 | 2 |
| 10350E 10250N | 2 | 37 | 41 | 10 | 28 | 1 |
| 10350E 10200N | 3 | 38 | 44 | 14 | 30 | 1 |
| 10350E 10175N | 1 | 34 | 23 | 11 | 10 | 105 |
| 10350E 10150N | 2 | 41 | 48 | 9 | 20 | 1 |
| 10350E 10125N | 2 | 28 | 58 | 6 | 10 | 1 |
| 10350E 10100N | 1 | 15 | 13 | 6 | 5 | 115 |
| 10350E 10075N | 3 | 26 | 39 | 8 | 5 | 3 |
| 10350E 10050N | 2 | 83 | 19 | 7 | 9 | 14 |
| 10350E 10025N | 2 | 24 | 16 | 10 | 15 | 2 |
| 10350E 10000N | 2 | 28 | 38 | 5 | 10 | 1 |
| 10350E 9975N | 1 | 23 | 27 | 8 | 11 | 3 |
| 10350E 9950N | 6 | 32 | 35 | 7 | 29 | 2 |
| 10350E 9925N | 1 | 16 | 14 | 5 | 5 | 1 |
| 10350E 9850N | 1 | 45 | 37 | 9 | 14 | 5 |
| 10350E 9825N | 1 | 62 | 39 | 15 | 38 | 1 |
| 10350E 9800N | 2 | 261 | 860 | 33 | 137 | 1 |
| 10350E 9700N | 1 | 58 | 35 | 6 | 8 | 25 |
| 10350E 9675N | 1 | 27 | 16 | 7 | 5 | 1 |
| 10350E 9650N | 18 | 4823 | 25 | 8 | 12 | 1090 |
| 10350E 9625N | 2 | 52 | 58 | 4 | 8 | 30 |
| 10350E 9500N | 1 | 24 | 25 | 2 | 3 | 10 |
| 10350E 9575N | 2 | 19 | 45 | 3 | 5 | 4 |
| 10350E 9550N | 1 | 26 | 22 | 8 | 3 | 1 |
| 10400E 10500N | 1 | 30 | 25 | 2 | 4 | 2 |
| 10400E 10475N | 3 | 80 | 70 | 3 | 57 | 1 |
| 10400E 10425N | 2 | 81 | 974 | 3 | 15 | 2 |
| 10400E 10400N | 2 | 97 | 178 | 5 | 26 | 1 |
| STD C/AU-S | 19 | 60 | 41 | 27 | 37 | 48 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10400E 10375N | 5 | 48 | 293 | 13 | 147 | 9 |
| 10400E 10350N | 3 | 54 | 80 | 12 | 35 | 4 |
| 10400E 10325N | 1 | 85 | 85 | 3 | 10 | 3 |
| 10400E 10275N | 2 | 21 | 39 | 5 | 13 | 1 |
| 10400E 10250N | 1 | 27 | 33 | 5 | 15 | 2 |
| 10400E 10225N | 3 | 173 | 58 | 9 | 39 | 10 |
| 10400E 10200N | 2 | 41 | 107 | 5 | 16 | 1 |
| 10400E 10175N | 2 | 51 | 15 | 8 | 18 | 3 |
| 10400E 10150N | 1 | 18 | 15 | 6 | 7 | 1 |
| 10400E 10125N | 1 | 18 | 34 | 3 | 12 | 2 |
| 10400E 10100N | 1 | 14 | 15 | 5 | 7 | 4 |
| 10400E 10075N | 1 | 24 | 24 | 9 | 9 | 1 |
| 10400E 10050N | 1 | 17 | 21 | 4 | 4 | 1 |
| 10400E 10025N | 1 | 26 | 50 | 11 | 28 | 1 |
| 10400E 10000N | 1 | 27 | 17 | 8 | 4 | 1 |
| 10400E 9975N | 2 | 35 | 36 | 5 | 8 | 1 |
| 10400E 9950N | 1 | 18 | 15 | 14 | 2 | 1 |
| 10400E 9925N | 1 | 18 | 12 | 6 | 2 | 2 |
| 10400E 9900N | 1 | 24 | 33 | 4 | 5 | 2 |
| 10400E 9825N | 1 | 33 | 65 | 5 | 11 | 1 |
| 10400E 9800N | 1 | 20 | 27 | 2 | 2 | 1 |
| 10400E 9750N | 5 | 455 | 39 | 6 | 9 | 103 |
| 10400E 9725N | 1 | 60 | 37 | 2 | 5 | 2 |
| 10400E 9700N | 1 | 28 | 37 | 7 | 6 | 5 |
| 10400E 9675N | 1 | 10 | 12 | 4 | 2 | 1 |
| STD C/AU-S | 20 | 62 | 40 | 29 | 40 | 49 |
| 10400E 9650N | 1 | 36 | 16 | 7 | 4 | 3 |
| 10400E 9625N | 1 | 24 | 26 | 5 | 3 | 1 |
| 10400E 9600N | 1 | 14 | 49 | 3 | 5 | 1 |
| 10400E 9575N | 1 | 7 | 28 | 2 | 6 | 1 |
| 10400E 9550N | 1 | 11 | 19 | 4 | 2 | 3 |
| 10400E 9525N | 1 | 11 | 15 | 4 | 2 | 2 |
| 10450E 10425N | 1 | 58 | 240 | 13 | 25 | 2 |
| 10450E 10400N | 1 | 68 | 48 | 4 | 33 | 5 |
| 10450E 10375N | 5 | 48 | 568 | 11 | 73 | 4 |
| 10450E 10350N | 4 | 44 | 48 | 14 | 33 | 2 |
| 10450E 10325N | 1 | 64 | 58 | 16 | 58 | 1 |

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| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10450E 10300N | 3 | 41 | 42 | 17 | 30 | 3 |
| 10450E 10275N | 2 | 50 | 33 | 24 | 62 | 1 |
| 10450E 10250N | 1 | 123 | 16 | 10 | 42 | 2 |
| 10450E 10225N | 1 | 31 | 33 | 3 | 15 | 2 |
| 10450E 10200N | 2 | 58 | 9 | 18 | 30 | 1 |
| 10450E 10175N | 2 | 18 | 5 | 2 | 9 | 2 |
| 10450E 10150N | 21 | 6945 | 10 | 7 | 19 | 1290 |
| 10450E 10125N | 3 | 592 | 64 | 10 | 16 | 52 |
| 10450E 10100N | 3 | 51 | 55 | 12 | 28 | 1 |
| 10450E 10075N | 2 | 52 | 43 | 6 | 26 | 6 |
| 10450E 10050N | 1 | 38 | 20 | 12 | 37 | 1 |
| 10450E 10025N | 1 | 35 | 14 | 12 | 15 | 1 |
| 10450E 10000N | 7 | 29 | 53 | 8 | 51 | 1 |
| 10450E 9975N | 2 | 35 | 36 | 11 | 51 | 820 |
| 10450E 9900N | 1 | 53 | 28 | 6 | 8 | 4 |
| 10450E 9725N | 1 | 14 | 13 | 5 | 4 | 1 |
| 10450E 9700N | 1 | 30 | 11 | 8 | 6 | 1 |
| 10450E 9675N | 1 | 21 | 11 | 7 | 4 | 4 |
| 10450E 9650N | 1 | 30 | 13 | 7 | 6 | 1 |
| 10450E 9625N | 1 | 17 | 49 | 3 | 6 | 1 |
| 10450E 9600N | 1 | 29 | 21 | 5 | 2 | 1 |
| 10450E 9575N | 1 | 19 | 6 | 7 | 4 | 2 |
| 10450E 9550N | 1 | 20 | 15 | 8 | 10 | 1 |
| 10450E 9525N | 1 | 19 | 13 | 9 | 5 | 1 |
| 10450E 9500N | 1 | 14 | 10 | 3 | 4 | 1 |
| 10500E 10450N | 1 | 64 | 67 | 3 | 10 | 3 |
| 10500E 10425N | 1 | 33 | 19 | 7 | 10 | 1 |
| 10500E 10400N | 2 | 18 | 43 | 1 | 29 | 3 |
| 10500E 10375N | 1 | 26 | 26 | 7 | 13 | 1 |
| 10500E 10350N | 2 | 52 | 31 | 16 | 16 | 3 |
| 10500E 10325N | 2 | 58 | 58 | 7 | 16 | 2 |
| 10500E 10300N | 3 | 41 | 45 | 11 | 13 | 1 |
| 10500E 10275N | 1 | 22 | 27 | 7 | 15 | 1 |
| 10500E 10250N | 1 | 28 | 20 | 8 | 11 | 1 |
| 10500E 10225N | 2 | 32 | 30 | 5 | 13 | 1 |
| 10500E 10200N | 1 | 34 | 14 | 8 | 7 | 2 |
| STD C/AU-S | 18 | 60 | 41 | 29 | 40 | 47 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10500E 10175N | 1 | 24 | 8 | 5 | 7 | 1 |
| 10500E 10150N | 1 | 52 | 46 | 3 | 6 | 2 |
| 10500E 10125N | 2 | 26 | 2 | 1 | 9 | 1 |
| 10500E 10075N | 3 | 59 | 75 | 10 | 39 | 7 |
| 10500E 10050N | 2 | 41 | 9 | 1 | 7 | 1 |
| 10500E 10025N | 1 | 29 | 21 | 5 | 3 | 1 |
| 10500E 10000N | 1 | 21 | 16 | 5 | 3 | 1 |
| 10500E 9975N | 1 | 28 | 16 | 5 | 7 | 2 |
| 10500E 9875N | 3 | 109 | 37 | 9 | 7 | 12 |
| 10500E 9850N | 2 | 55 | 33 | 12 | 32 | 5 |
| 10500E 9825N | 3 | 44 | 309 | 10 | 153 | 3 |
| STD C/AU-S | 19 | 60 | 42 | 28 | 38 | 49 |
| 10500E 9800N | 1 | 18 | 31 | 8 | 15 | 4 |
| 10500E 9775N | 1 | 29 | 21 | 6 | 5 | 1 |
| 10500E 9750N | 1 | 17 | 33 | 7 | 4 | 1 |
| 10500E 9725N | 1 | 27 | 17 | 7 | 8 | 2 |
| 10500E 9675N | 1 | 18 | 13 | 6 | 2 | 1 |
| 10500E 9650N | 1 | 16 | 17 | 7 | 4 | 2 |
| 10500E 9625N | 1 | 13 | 21 | 2 | 5 | 1 |
| 10500E 9600N | 1 | 32 | 11 | 6 | 2 | 1 |
| 10500E 9575N | 1 | 17 | 13 | 6 | 3 | 1 |
| 10500E 9550N | 1 | 18 | 35 | 6 | 4 | 1 |
| 10500E 9525N | 1 | 26 | 11 | 4 | 3 | 1 |
| 10550E 10400N | 2 | 46 | 28 | 4 | 4 | 2 |
| 10550E 10375N | 2 | 82 | 75 | 6 | 12 | 1 |
| 10550E 10350N | 1 | 29 | 25 | 11 | 9 | 2 |
| 10550E 10325N | 5 | 83 | 41 | 23 | 38 | 3 |
| 10550E 10300N | 2 | 51 | 45 | 8 | 23 | 1 |
| 10550E 10275N | 1 | 2 | 2 | 1 | 2 | 2 |
| 10550E 10250N | 1 | 1 | 2 | 1 | 2 | 17 |
| 10550E 10225N | 2 | 47 | 26 | 7 | 5 | 3 |
| 10550E 10200N | 1 | 39 | 23 | 10 | 11 | 1 |
| 10550E 10175N | 3 | 180 | 80 | 9 | 9 | 4 |
| 10550E 10000N | 12 | 119 | 106 | 21 | 51 | 9 |
| 10550E 9975N | 3 | 71 | 40 | 5 | 14 | 7 |
| 10550E 9900N | 2 | 37 | 19 | 11 | 18 | 2 |
| 10550E 9875N | 1 | 47 | 53 | 9 | 11 | 4 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10550E 9850N | 1 | 61 | 192 | 10 | 19 | 14 |
| 10550E 9825N | 2 | 13 | 16 | 2 | 8 | 1 |
| 10550E 9800N | 2 | 18 | 43 | 7 | 11 | 1 |
| 10550E 9775N | 1 | 12 | 19 | 5 | 3 | 1 |
| 10550E 9750N | 1 | 20 | 17 | 7 | 4 | 1 |
| 10550E 9725N | 2 | 56 | 30 | 7 | 146 | 6 |
| 10550E 9675N | 2 | 17 | 31 | 3 | 9 | 1 |
| 10550E 9650N | 4 | 32 | 63 | 10 | 19 | 6 |
| 10550E 9625N | 1 | 14 | 12 | 4 | 2 | 2 |
| 10550E 9600N | 1 | 19 | 36 | 7 | 5 | 2 |
| 10550E 9575N | 1 | 8 | 7 | 3 | 2 | 1 |
| 10550E 9550N | 2 | 17 | 43 | 6 | 8 | 1 |
| 10600E 10425N | 2 | 39 | 111 | 6 | 8 | 5 |
| 10600E 10400N | 2 | 20 | 47 | 4 | 12 | 1 |
| 10600E 10375N | 2 | 58 | 62 | 3 | 10 | 4 |
| 10600E 10350N | 5 | 70 | 54 | 17 | 26 | 3 |
| 10600E 10325N | 2 | 78 | 76 | 5 | 19 | 3 |
| 10600E 10300N | 3 | 90 | 46 | 5 | 18 | 7 |
| 10600E 10275N | 4 | 60 | 63 | 6 | 20 | 3 |
| 10600E 10250N | 5 | 72 | 82 | 12 | 40 | 1 |
| 10600E 10225N | 2 | 37 | 19 | 2 | 10 | 2 |
| 10600E 10200N | 2 | 19 | 20 | 2 | 11 | 1 |
| 10600E 10175N | 3 | 60 | 41 | 13 | 30 | 5 |
| 10600E 10150N | 2 | 93 | 35 | 15 | 34 | 8 |
| 10600E 10125N | 2 | 19 | 12 | 1 | 9 | 1 |
| 10600E 10100N | 5 | 576 | 197 | 3 | 12 | 98 |
| 10600E 10075N | 2 | 122 | 38 | 2 | 8 | 40 |
| 10600E 10050N | 4 | 128 | 43 | 29 | 108 | 8 |
| 10600E 10025N | 6 | 712 | 1122 | 8 | 17 | 157 |
| 10600E 10000N | 1 | 51 | 38 | 7 | 6 | 6 |
| 10600E 9850N | 1 | 63 | 20 | 8 | 14 | 5 |
| 10600E 9825N | 2 | 25 | 26 | 3 | 10 | 1 |
| 10600E 9800N | 3 | 20 | 26 | 6 | 76 | 2 |
| 10600E 9775N | 1 | 40 | 17 | 9 | 9 | 15 |
| 10600E 9750N | 1 | 21 | 13 | 7 | 7 | 1 |
| 10600E 9725N | 1 | 24 | 12 | 8 | 6 | 2 |
| STD C/AU-S | 19 | 63 | 41 | 28 | 40 | 48 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10600E 9700N | 1 | 11 | 11 | 4 | 4 | 1 |
| 10600E 9650N | 2 | 10 | 22 | 1 | 11 | 1 |
| 10600E 9625N | 1 | 12 | 33 | 2 | 10 | 1 |
| 10600E 9600N | 1 | 14 | 14 | 5 | 2 | 1 |
| 10600E 9575N | 1 | 17 | 58 | 3 | 8 | 1 |
| 10600E 9550N | 1 | 16 | 8 | 7 | 2 | 1 |
| 10650E 10425N | 2 | 62 | 39 | 16 | 17 | 1 |
| 10650E 10400N | 1 | 11 | 11 | 2 | 3 | 1 |
| 10650E 10375N | 1 | 38 | 15 | 8 | 2 | 1 |
| 10650E 10350N | 1 | 39 | 65 | 6 | 9 | 2 |
| 10650E 10325N | 2 | 71 | 34 | 15 | 24 | 8 |
| 10650E 10300N | 3 | 35 | 30 | 7 | 14 | 1 |
| 10650E 10275N | 2 | 31 | 49 | 10 | 27 | 1 |
| 10650E 10250N | 1 | 60 | 26 | 6 | 5 | 1 |
| 10650E 10225N | 1 | 25 | 36 | 6 | 7 | 1 |
| 10650E 10200N | 1 | 26 | 17 | 9 | 2 | 5 |
| 10650E 10175N | 1 | 29 | 36 | 3 | 6 | 1 |
| 10650E 10150N | 1 | 28 | 16 | 10 | 3 | 1 |
| 10650E 10125N | 1 | 6 | 7 | 1 | 5 | 1 |
| 10650E 10100N | 4 | 21 | 30 | 3 | 10 | 1 |
| 10650E 10075N | 1 | 36 | 25 | 5 | 15 | 3 |
| 10650E 10050N | 2 | 21 | 18 | 2 | 9 | 1 |
| 10650E 10025N | 1 | 52 | 35 | 5 | 4 | 1 |
| 10650E 10000N | 1 | 41 | 89 | 8 | 8 | 1 |
| 10650E 9975N | 1 | 56 | 35 | 10 | 10 | 5 |
| 10650E 9950N | 1 | 25 | 17 | 10 | 2 | 1 |
| 10650E 9925N | 1 | 30 | 68 | 3 | 15 | 2 |
| 10650E 9900N | 2 | 21 | 51 | 5 | 12 | 1 |
| 10650E 9875N | 1 | 36 | 21 | 11 | 5 | 2 |
| 10650E 9850N | 2 | 12 | 29 | 3 | 13 | 1 |
| 10650E 9825N | 1 | 22 | 15 | 7 | 12 | 1 |
| 10650E 9800N | 2 | 26 | 78 | 11 | 157 | 1 |
| 10650E 9775N | 2 | 14 | 19 | 1 | 12 | 1 |
| 10650E 9750N | 1 | 9 | 28 | 2 | 10 | 1 |
| 10650E 9725N | 1 | 19 | 24 | 10 | 5 | 1 |
| 10650E 9700N | 1 | 29 | 17 | 7 | 3 | 1 |
| STD C/AU-S | 19 | 60 | 41 | 27 | 36 | 52 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10650E 9675N | 1 | 6 | 18 | 1 | 7 | 3 |
| 10650E 9650N | 1 | 19 | 24 | 7 | 10 | 1 |
| 10650E 9625N | 1 | 55 | 11 | 11 | 5 | 1 |
| 10650E 9600N | 1 | 25 | 15 | 8 | 4 | 1 |
| 10650E 9575N | 1 | 22 | 12 | 7 | 2 | 1 |
| 10650E 9550N | 1 | 21 | 75 | 3 | 23 | 4 |
| 10650E 9525N | 1 | 7 | 18 | 3 | 4 | 18 |
| 10650E 9500N | 1 | 17 | 14 | 6 | 4 | 4 |
| 10700E 10500N | 1 | 32 | 70 | 9 | 6 | 3 |
| 10700E 10475N | 1 | 62 | 17 | 13 | 8 | 3 |
| 10700E 10450N | 1 | 57 | 23 | 8 | 9 | 1 |
| 10700E 10425N | 1 | 25 | 23 | 2 | 7 | 1 |
| 10700E 10400N | 4 | 239 | 25 | 38 | 50 | 16 |
| 10700E 10375N | 3 | 50 | 33 | 17 | 26 | 2 |
| 10700E 10350N | 2 | 27 | 35 | 4 | 12 | 1 |
| 10700E 10325N | 1 | 20 | 15 | 7 | 4 | 1 |
| 10700E 10300N | 1 | 17 | 15 | 2 | 3 | 1 |
| 10700E 10275N | 1 | 17 | 17 | 2 | 6 | 4 |
| 10700E 10250N | 1 | 23 | 20 | 1 | 3 | 2 |
| 10700E 10225N | 1 | 15 | 20 | 5 | 4 | 4 |
| 10700E 10200N | 1 | 24 | 58 | 7 | 11 | 1 |
| 10700E 10175N | 1 | 24 | 13 | 1 | 4 | 1 |
| 10700E 10150N | 1 | 22 | 25 | 7 | 9 | 4 |
| 10700E 10125N | 1 | 24 | 18 | 5 | 7 | 3 |
| 10700E 10100N | 1 | 15 | 19 | 3 | 6 | 1 |
| 10700E 10075N | 1 | 25 | 16 | 6 | 5 | 1 |
| 10700E 10050N | 1 | 36 | 24 | 12 | 40 | 1 |
| 10700E 10025N | 4 | 109 | 24 | 22 | 174 | 1 |
| 10700E 10000N | 1 | 46 | 14 | 9 | 15 | 2 |
| 10700E 9975N | 1 | 43 | 14 | 9 | 7 | 2 |
| 10700E 9950N | 1 | 31 | 10 | 10 | 6 | 1 |
| 10700E 9925N | 1 | 29 | 50 | 7 | 16 | 1 |
| 10700E 9900N | 1 | 45 | 194 | 15 | 32 | 1 |
| 10700E 9875N | 2 | 19 | 124 | 4 | 14 | 2 |
| 10700E 9850N | 1 | 10 | 21 | 2 | 7 | 1 |
| 10700E 9825N | 1 | 54 | 14 | 10 | 19 | 2 |
| STD C/AU-S | 19 | 61 | 41 | 27 | 38 | 49 |

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| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10700E 9800N | 1 | 20 | 21 | 6 | 10 | 1 |
| 10700E 9775N | 2 | 31 | 14 | 7 | 11 | 1 |
| 10700E 9750N | 7 | 78 | 11 | 11 | 20 | 1 |
| 10700E 9725N | 1 | 15 | 14 | 7 | 2 | 1 |
| 10700E 9700N | 1 | 6 | 9 | 4 | 2 | 2 |
| 10700E 9675N | 1 | 12 | 16 | 4 | 2 | 1 |
| 10700E 9650N | 1 | 12 | 20 | 6 | 4 | 1 |
| 10700E 9625N | 1 | 12 | 16 | 6 | 4 | 1 |
| 10700E 9600N | 1 | 44 | 4 | 8 | 4 | 2 |
| 10700E 9575N | 1 | 30 | 8 | 9 | 3 | 1 |
| 10700E 9550N | 1 | 21 | 9 | 6 | 2 | 1 |
| 10700E 9525N | 1 | 18 | 15 | 6 | 2 | 2 |
| 10700E 9500N | 1 | 19 | 15 | 8 | 2 | 1 |
| 10750E 10500N | 1 | 17 | 30 | 2 | 5 | 1 |
| 10750E 10475N | 1 | 26 | 43 | 5 | 16 | 1 |
| 10750E 10450N | 1 | 20 | 26 | 4 | 5 | 2 |
| 10750E 10425N | 2 | 23 | 23 | 4 | 6 | 1 |
| 10750E 10400N | 1 | 15 | 12 | 6 | 2 | 1 |
| 10750E 10375N | 1 | 47 | 9 | 3 | 2 | 2 |
| STD C/AU-S | 19 | 60 | 41 | 29 | 38 | 47 |
| 10750E 10350N | 1 | 27 | 29 | 9 | 4 | 1 |
| 10750E 10325N | 1 | 22 | 14 | 6 | 5 | 1 |
| 10750E 10300N | 1 | 15 | 13 | 4 | 15 | 1 |
| 10750E 10275N | 1 | 22 | 13 | 3 | 10 | 1 |
| 10750E 10250N | 2 | 23 | 29 | 5 | 14 | 1 |
| 10750E 10225N | 1 | 22 | 21 | 3 | 17 | 2 |
| 10750E 10200N | 3 | 30 | 46 | 7 | 18 | 4 |
| 10750E 10175N | 1 | 36 | 27 | 2 | 22 | 1 |
| 10750E 10150N | 1 | 32 | 20 | 7 | 26 | 1 |
| 10750E 10125N | 3 | 29 | 31 | 10 | 32 | 1 |
| 10750E 10100N | 2 | 88 | 36 | 24 | 34 | 2 |
| 10750E 10075N | 3 | 47 | 23 | 15 | 37 | 1 |
| 10750E 10050N | 1 | 74 | 24 | 19 | 125 | 2 |
| 10750E 10025N | 1 | 15 | 17 | 2 | 7 | 2 |
| 10750E 10000N | 1 | 19 | 17 | 2 | 24 | 1 |
| 10750E 9975N | 1 | 7 | 8 | 1 | 10 | 1 |
| 10750E 9925N | 1 | 22 | 25 | 12 | 4 | 2 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|-----------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10750E 9900N | 1 | 27 | 13 | 7 | 3 | 1 |
| 10750E 9875N | 1 | 40 | 22 | 8 | 14 | 1 |
| 10750E 9850N | 1 | 36 | 23 | 7 | 25 | 1 |
| STD C/AU-S | 19 | 59 | 38 | 27 | 38 | 48 |
| 10750E 9825N | 1 | 41 | 11 | 7 | 15 | 1 |
| | | | | | | |
| 10750E 9800N | 1 | 22 | 34 | 10 | 14 | 18 |
| 10750E 9775N | 3 | 38 | 12 | 11 | 17 | 1 |
| 10750E 9750N | 2 | 20 | 60 | 7 | 9 | 1 |
| 10750E 9725N | 1 | 24 | 17 | 8 | 4 | 1 |
| 10750E 9700N | 1 | 33 | 43 | 8 | 6 | 1 |
| | | | | | | |
| 10750E 9675N | 1 | 20 | 85 | 3 | 8 | 1 |
| 10750E 9650N | 1 | 18 | 75 | 3 | 9 | 2 |
| 10750E 9625N | 1 | 29 | 12 | 7 | 5 | 1 |
| 10750E 9600N | 1 | 71 | 2 | 9 | 4 | 1 |
| 10750E 9575N | 1 | 19 | 23 | 6 | 6 | 2 |
| | | | | | | |
| 10750E 9550N | 1 | 34 | 13 | 8 | 20 | 1 |
| 10750E 9525N | 1 | 17 | 21 | 6 | 5 | 1 |
| 10750E 9500N | 1 | 18 | 57 | 4 | 13 | 1 |
| 10800E 10500N | 1 | 47 | 27 | 2 | 6 | 1 |
| 10800E 10475N | 1 | 31 | 32 | 6 | 7 | 1 |
| | | | | | | |
| 10800E 10450N | 1 | 40 | 28 | 6 | 9 | 2 |
| 10800E 10425N | 1 | 39 | 33 | 4 | 10 | 1 |
| 10800E 10400N | 1 | 54 | 16 | 8 | 6 | 36 |
| 10800E 10375N | 1 | 22 | 15 | 6 | 4 | 15 |
| 10800E 10350N | 1 | 19 | 12 | 2 | 6 | 2 |
| | | | | | | |
| 10800E 10325N | 4 | 35 | 37 | 4 | 22 | 10 |
| 10800E 10325N A | 1 | 15 | 12 | 3 | 2 | 1 |
| 10800E 10300N | 1 | 43 | 18 | 6 | 6 | 2 |
| 10800E 10250N | 1 | 48 | 28 | 7 | 27 | 1 |
| 10800E 10225N | 1 | 54 | 8 | 7 | 9 | 1 |
| | | | | | | |
| 10800E 10200N | 1 | 39 | 15 | 6 | 8 | 2 |
| 10800E 10175N | 1 | 40 | 11 | 7 | 8 | 1 |
| 10800E 10150N | 1 | 38 | 22 | 8 | 28 | 1 |
| 10800E 10125N | 1 | 13 | 15 | 4 | 7 | 1 |
| 10800E 10100N | 1 | 29 | 61 | 6 | 30 | 1 |
| | | | | | | |
| 10800E 10050N | 2 | 56 | 36 | 14 | 190 | 2 |
| 10800E 10025N | 1 | 22 | 20 | 2 | 7 | 1 |

VANANDA GOLD LTD.

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| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10800E 10000N | 1 | 19 | 45 | 2 | 13 | 4 |
| 10800E 9975N | 1 | 19 | 26 | 2 | 14 | 1 |
| 10800E 9950N | 1 | 11 | 30 | 1 | 9 | 3 |
| 10800E 9925N | 1 | 18 | 32 | 2 | 15 | 2 |
| 10800E 9900N | 1 | 21 | 34 | 3 | 15 | 1 |
| 10800E 9875N | 1 | 27 | 37 | 3 | 12 | 1 |
| 10800E 9850N | 1 | 18 | 29 | 9 | 31 | 1 |
| 10800E 9825N | 1 | 35 | 22 | 12 | 34 | 2 |
| 10800E 9800N | 1 | 51 | 20 | 9 | 18 | 3 |
| 10800E 9775N | 1 | 44 | 17 | 9 | 4 | 1 |
| 10800E 9750N | 1 | 50 | 12 | 8 | 10 | 1 |
| 10800E 9725N | 1 | 28 | 8 | 6 | 2 | 1 |
| 10800E 9700N | 1 | 9 | 55 | 2 | 4 | 2 |
| 10800E 9675N | 1 | 17 | 31 | 2 | 3 | 1 |
| 10800E 9650N | 1 | 12 | 17 | 6 | 3 | 2 |
| 10800E 9625N | 1 | 53 | 98 | 9 | 9 | 2 |
| 10800E 9600N | 1 | 21 | 13 | 7 | 6 | 1 |
| 10800E 9575N | 1 | 28 | 24 | 7 | 19 | 1 |
| 10800E 9550N | 1 | 44 | 11 | 8 | 5 | 3 |
| 10800E 9525N | 1 | 25 | 22 | 8 | 5 | 1 |
| 10800E 9500N | 1 | 16 | 46 | 4 | 8 | 1 |
| 10850E 10375N | 1 | 53 | 24 | 13 | 9 | 1 |
| 10850E 10350N | 1 | 33 | 32 | 2 | 8 | 1 |
| 10850E 10300N | 1 | 36 | 42 | 13 | 53 | 2 |
| 10850E 10275N | 2 | 25 | 41 | 5 | 10 | 1 |
| 10850E 10250N | 1 | 22 | 36 | 2 | 7 | 1 |
| 10850E 10225N | 1 | 21 | 26 | 2 | 9 | 1 |
| 10850E 10200N | 1 | 12 | 13 | 6 | 3 | 1 |
| 10850E 10175N | 1 | 16 | 10 | 2 | 6 | 1 |
| 10850E 10150N | 1 | 27 | 36 | 5 | 10 | 1 |
| 10850E 10125N | 1 | 34 | 13 | 9 | 8 | 2 |
| 10850E 10100N | 1 | 46 | 17 | 7 | 8 | 1 |
| 10850E 10075N | 1 | 41 | 32 | 9 | 42 | 1 |
| 10850E 10000N | 1 | 10 | 23 | 1 | 2 | 1 |
| 10850E 9975N | 1 | 7 | 5 | 1 | 4 | 1 |
| 10850E 9950N | 2 | 89 | 22 | 14 | 231 | 2 |
| STD C/AU-S | 19 | 59 | 42 | 27 | 37 | 49 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10850E 9925N | 1 | 26 | 14 | 9 | 16 | 8 |
| 10850E 9900N | 1 | 10 | 5 | 4 | 8 | 3 |
| 10850E 9875N | 1 | 14 | 110 | 5 | 26 | 2 |
| 10850E 9850N | 1 | 44 | 367 | 3 | 185 | 7 |
| 10850E 9825N | 1 | 9 | 79 | 1 | 29 | 1 |
| 10850E 9800N | 1 | 12 | 49 | 4 | 19 | 2 |
| 10850E 9775N | 1 | 13 | 71 | 2 | 7 | 2 |
| 10850E 9750N | 1 | 9 | 9 | 2 | 2 | 2 |
| 10850E 9725N | 1 | 12 | 41 | 4 | 3 | 4 |
| 10850E 9700N | 1 | 40 | 10 | 12 | 6 | 2 |
| 10850E 9675N | 2 | 37 | 41 | 15 | 20 | 5 |
| STD C/AU-S | 19 | 62 | 41 | 29 | 38 | 47 |
| 10850E 9650N | 1 | 13 | 52 | 7 | 14 | 1 |
| 10850E 9625N | 1 | 14 | 25 | 3 | 9 | 1 |
| 10850E 9600N | 1 | 12 | 63 | 3 | 8 | 3 |
| 10850E 9575N | 1 | 7 | 10 | 1 | 2 | 2 |
| 10850E 9550N | 1 | 32 | 17 | 10 | 4 | 2 |
| 10850E 9525N | 1 | 27 | 159 | 7 | 17 | 2 |
| 10900E 10300N | 1 | 506 | 75 | 7 | 4 | 23 |
| 10900E 10275N | 1 | 60 | 21 | 3 | 3 | 2 |
| 10900E 10250N | 1 | 27 | 35 | 2 | 3 | 1 |
| 10900E 10225N | 1 | 18 | 15 | 3 | 6 | 1 |
| 10900E 10200N | 1 | 32 | 39 | 1 | 3 | 1 |
| 10900E 10150N | 1 | 19 | 34 | 3 | 7 | 1 |
| 10900E 10125N | 1 | 18 | 52 | 3 | 4 | 1 |
| 10900E 10100N | 1 | 8 | 10 | 3 | 2 | 1 |
| 10900E 10075N | 1 | 62 | 18 | 9 | 103 | 3 |
| 10900E 10050N | 3 | 533 | 22 | 5 | 56 | 107 |
| 10900E 10025N | 2 | 118 | 20 | 6 | 13 | 31 |
| 10900E 10000N | 1 | 12 | 19 | 3 | 3 | 6 |
| 10900E 9975N | 1 | 21 | 10 | 9 | 8 | 1 |
| 10900E 9950N | 1 | 14 | 32 | 2 | 5 | 1 |
| 10900E 9925N | 1 | 25 | 38 | 9 | 12 | 7 |
| 10900E 9900N | 1 | 26 | 12 | 6 | 6 | 34 |
| 10900E 9875N | 1 | 38 | 17 | 8 | 76 | 3 |
| 10900E 9850N | 1 | 36 | 8913 | 2 | 228 | 7 |
| 10900E 9825N | 1 | 6 | 85 | 1 | 10 | 1 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 10900E 9800N | 1 | 13 | 69 | 2 | 12 | 1 |
| 10900E 9775N | 1 | 23 | 18 | 6 | 6 | 1 |
| 10950E 10325N | 9 | 535 | 46 | 4 | 5 | 1520 |
| 10950E 10300N | 1 | 40 | 36 | 11 | 30 | 12 |
| 10950E 10275N | 1 | 47 | 20 | 9 | 8 | 1 |
| STD C/AU-S | 18 | 62 | 43 | 29 | 40 | 48 |
| 10950E 10250N | 1 | 46 | 15 | 12 | 5 | 1 |
| 10950E 10225N | 1 | 38 | 15 | 9 | 3 | 1 |
| 10950E 10200N | 1 | 10 | 20 | 1 | 5 | 31 |
| 10950E 10175N | 1 | 19 | 26 | 3 | 4 | 3 |
| 10950E 10150N | 1 | 18 | 25 | 2 | 3 | 1 |
| 10950E 10125N | 1 | 16 | 21 | 3 | 5 | 1 |
| 10950E 10100N | 1 | 22 | 40 | 2 | 5 | 1 |
| 10950E 10075N | 1 | 18 | 16 | 6 | 3 | 1 |
| 10950E 10050N | 1 | 9 | 16 | 4 | 2 | 5 |
| 10950E 10025N | 1 | 30 | 17 | 7 | 5 | 6 |
| 10950E 10000N | 1 | 82 | 17 | 7 | 19 | 2 |
| 10950E 9975N | 1 | 14 | 23 | 3 | 6 | 1 |
| 10950E 9950N | 1 | 11 | 22 | 2 | 2 | 1 |
| 10950E 9925N | 1 | 19 | 57 | 6 | 10 | 5 |
| 10950E 9900N | 1 | 20 | 144 | 6 | 16 | 3 |
| 10950E 9875N | 1 | 51 | 15 | 3 | 11 | 9 |
| 10950E 9850N | 2 | 22 | 373 | 2 | 46 | 10 |
| 10950E 9825N | 1 | 20 | 90 | 2 | 13 | 1 |
| 10950E 9800N | 1 | 9 | 31 | 1 | 3 | 1 |
| 10950E 9775N | 1 | 10 | 133 | 2 | 4 | 1 |
| 10950E 9750N | 1 | 36 | 50 | 8 | 7 | 2 |
| 10950E 9725N | 1 | 27 | 10 | 7 | 4 | 3 |
| 10950E 9700N | 2 | 24 | 17 | 1 | 2 | 5 |
| 11000E 10375N | 1 | 58 | 20 | 2 | 4 | 3 |
| 11000E 10350N | 1 | 46 | 28 | 1 | 3 | 2 |
| 11000E 10325N | 2 | 47 | 26 | 16 | 56 | 1 |
| 11000E 10300N | 1 | 6 | 6 | 1 | 2 | 2 |
| 11000E 10275N | 1 | 32 | 32 | 17 | 20 | 1 |
| 11000E 10250N | 1 | 26 | 22 | 1 | 4 | 2 |
| 11000E 10225N | 1 | 18 | 26 | 2 | 5 | 1 |
| 11000E 10200N | 1 | 13 | 26 | 4 | 2 | 1 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| 11000E 10175N | 1 | 17 | 16 | 8 | 5 | 1 |
| 11000E 10150N | 1 | 20 | 29 | 2 | 6 | 1 |
| 11000E 10125N | 1 | 23 | 37 | 2 | 7 | 1 |
| 11000E 10100N | 1 | 11 | 25 | 4 | 6 | 1 |
| CHECK SAMPLE | 3 | 1256 | 28 | 5 | 8 | 74 |
| STD C | 19 | 59 | 38 | 28 | 38 | - |

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| SAMPLE# | MO PPM | CU PPM | PB PPM | CO PPM | AS PPM | AU* PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|------------|
| PIT ZONE DUMP | 1 | 2160 | 2227 | 13 | 3243 | 9900 |

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR Mn Fe Ca P La Cr Mg Ba Ti B W AND LIMITED FOR Na K AND Al. Au DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: SOIL Au# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 13 1987 DATE REPORT MAILED: Oct 26 1987 ASSAYER... D. J. DEAN TOYE, CERTIFIED B.C. ASSAYER

VANANDA GOLD File # 87-4932

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | SB PPM | Bi PPM | V PPM | Ca % | P PPM | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au# PPB |
|-------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|----------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|------------|
| 9000E 9750N | 1 | 15 | 16 | 72 | .1 | 5 | 3 | 3682 | 1.05 | 14 | 5 | ND | 1 | 185 | 1 | 2 | 2 | 10 19.12 | .085 | 2 | 5 | .59 | 129 | .01 | 11 | .62 | .01 | .02 | 1 | 3 | |
| 9750E 9740N | 1 | 65 | 13 | 99 | .1 | 41 | 14 | 1209 | 2.96 | 15 | 5 | ND | 3 | 60 | 1 | 2 | 2 | 61 6.33 | .048 | 8 | 50 | 2.73 | 116 | .11 | 6 | 1.92 | .02 | .06 | 3 | 23 | |
| 9750E 9615N | 1 | 303 | 16 | 88 | .2 | 122 | 35 | 421 | 5.09 | 2 | 5 | ND | 1 | 36 | 1 | 2 | 2 | 169 .76 | .021 | 2 | 162 | 5.13 | 35 | .38 | 6 | 4.87 | .05 | .12 | 1 | 43 | |
| 9750E 9600N | 1 | 168 | 18 | 95 | .1 | 92 | 30 | 700 | 4.48 | 5 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 145 .54 | .036 | 2 | 142 | 3.12 | 81 | .28 | 9 | 3.24 | .02 | .04 | 2 | 55 | |
| 9750E 9590N | 1 | 50 | 13 | 49 | .1 | 91 | 11 | 266 | 2.56 | 3 | 5 | ND | 2 | 17 | 1 | 2 | 2 | 69 .26 | .026 | 4 | 177 | .77 | 75 | .17 | 4 | 1.34 | .02 | .02 | 1 | 23 | |
| 9760E 9600N | 1 | 14 | 9 | 17 | .1 | 19 | 4 | 383 | 1.68 | 2 | 5 | ND | 1 | 27 | 2 | 2 | 2 | 53 .38 | .010 | 3 | 43 | .35 | 54 | .11 | 3 | .71 | .02 | .02 | 1 | 5 | |
| 9890E 9750N | 1 | 17 | 19 | 81 | .1 | 17 | 6 | 1050 | 2.52 | 6 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 55 .63 | .031 | 4 | 34 | .63 | 46 | .13 | 5 | 1.81 | .02 | .02 | 1 | 1 | |
| 9900E 9725N | 1 | 28 | 20 | 42 | .1 | 19 | 7 | 293 | 2.99 | 3 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 56 .53 | .010 | 7 | 37 | .61 | 43 | .13 | 6 | 2.10 | .02 | .02 | 1 | 85 | |
| 9900E 9760N | 1 | 37 | 24 | 71 | .1 | 15 | 7 | 2973 | 2.76 | 8 | 5 | ND | 2 | 93 | 1 | 2 | 2 | 53 8.39 | .048 | 5 | 28 | 1.32 | 102 | .10 | 5 | 1.80 | .04 | .03 | 1 | 31 | |
| 9900E 9775N | 1 | 21 | 24 | 89 | .1 | 12 | 7 | 1254 | 4.28 | 9 | 5 | ND | 4 | 32 | 1 | 2 | 2 | 56 1.81 | .038 | 10 | 24 | 1.23 | 65 | .13 | 9 | 2.56 | .02 | .04 | 3 | 20 | |
| 9910E 9750N | 1 | 19 | 26 | 66 | .1 | 8 | 8 | 452 | 2.41 | 6 | 5 | ND | 4 | 44 | 1 | 2 | 2 | 42 2.31 | .021 | 8 | 19 | 1.39 | 45 | .13 | 3 | 2.84 | .04 | .04 | 1 | 245 | |
| 10040 9850N | 1 | 26 | 48 | 400 | .3 | 5 | 6 | 10457 | 3.41 | 32 | 5 | ND | 1 | 121 | 2 | 2 | 2 | 31 10.82 | .336 | 8 | 24 | 1.13 | 259 | .04 | 8 | 1.92 | .01 | .03 | 2 | 4 | |
| 10050 9860N | 1 | 29 | 34 | 173 | .2 | 17 | 7 | 1711 | 2.88 | 29 | 5 | ND | 3 | 73 | 2 | 2 | 2 | 37 5.44 | .102 | 7 | 24 | 2.07 | 98 | .05 | 7 | 1.45 | .01 | .05 | 1 | 4 | |
| 10050 9850N | 1 | 30 | 98 | 525 | .3 | 8 | 6 | 1573 | 4.98 | 47 | 5 | ND | 3 | 41 | 1 | 2 | 2 | 61 1.37 | .140 | 6 | 17 | 1.99 | 71 | .09 | 6 | 2.87 | .02 | .03 | 2 | 78 | |
| 10050 9840N | 1 | 12 | 16 | 89 | .1 | 11 | 3 | 894 | 1.59 | 9 | 5 | ND | 1 | 18 | 2 | 2 | 2 | 28 .31 | .124 | 4 | 22 | .23 | 49 | .07 | 3 | .82 | .01 | .01 | 1 | 5 | |
| 10060 9850N | 2 | 24 | 36 | 281 | .5 | 3 | 3 | 9745 | 1.24 | 15 | 5 | ND | 1 | 280 | 1 | 2 | 2 | 9 18.12 | .197 | 3 | 6 | .22 | 214 | .02 | 15 | .78 | .01 | .03 | 2 | 1 | |
| 10190 9800N | 1 | 43 | 45 | 178 | .7 | 23 | 7 | 3162 | 3.01 | 18 | 5 | ND | 3 | 98 | 2 | 2 | 2 | 48 5.19 | .275 | 5 | 46 | 1.86 | 121 | .03 | 4 | 2.58 | .01 | .02 | 2 | 2 | |
| 10200 9800N | 1 | 31 | 26 | 85 | .2 | 19 | 7 | 1031 | 2.41 | 11 | 5 | ND | 3 | 35 | 1 | 3 | 2 | 51 1.84 | .055 | 6 | 36 | .83 | 71 | .11 | 6 | 2.32 | .02 | .03 | 1 | 39 | |
| 10200 9790N | 4 | 46 | 31 | 114 | .1 | 34 | 13 | 1283 | 5.95 | 30 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 67 .68 | .113 | 6 | 41 | 3.22 | 44 | .04 | 6 | 2.60 | .01 | .01 | 1 | 2 | |
| 10210 9800N | 2 | 40 | 39 | 123 | .3 | 33 | 12 | 1149 | 4.73 | 46 | 5 | ND | 3 | 26 | 1 | 2 | 3 | 62 .86 | .115 | 6 | 41 | 3.45 | 51 | .03 | 4 | 3.18 | .01 | .02 | 1 | 2 | |
| STD C/AU-S | 18 | 60 | 42 | 130 | 7.3 | 66 | 28 | 1039 | 3.83 | 40 | 20 | 7 | 38 | 51 | 18 | 17 | 22 | 59 .46 | .091 | 38 | 63 | .87 | 177 | .08 | 37 | 1.77 | .06 | .13 | 12 | 52 | |

GEOCHEMICAL/ASSAY CERTIFICATE

ICP .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: Rock Chips AU\$ BY FIRE ASSAY FROM 1/2 A.T.

DATE RECEIVED: OCT 13 1987 DATE REPORT MAILED: Oct 26/87 ASSAYER: *M. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

VANANDA GOLD File # 87-4932A Page 1

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe PPM | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | CD PPM | SB PPM | Bl PPM | V PPM | Ca PPM | P PPM | La PPM | Cr PPM | Mg PPM | Ba PPM | Ti PPM | B PPM | Al PPM | Na PPM | K PPM | W PPM | AU\$ | OZ/T |
|----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|----------|----------|------|------|
| FS87-1-5 | 5 1155 | 6 32 | 2.3 | 20 | 13 1262 | 17.76 | 115 | 5 | ND | 3 2 | 1 | 2 | 2 | 10 18.14 | .001 | 2 | 4 | .06 | 3 | .01 | 2 | .18 | .01 | .01 | 4 | .004 | | | | | | |
| FS87-1-6 | 2 278 | 10 38 | .9 | 26 | 10 1016 | 8.95 | 66 | 5 | ND | 4 58 | 6 | 3 | 2 | 51 12.10 | .034 | 2 | 37 | .22 | 11 | .22 | 10 | 1.05 | .09 | .02 | 19 | .003 | | | | | | |
| FS87-1-7 | 1 1355 | 5 48 | .7 | 60 | 33 227 | 6.93 | 31 | 5 | ND | 2 90 | 1 | 2 | 2 | 85 1.91 | .044 | 2 | 64 | .26 | 17 | .39 | 6 | 1.58 | .23 | .02 | 1 | .002 | | | | | | |
| FS87-1-8 | 2 30322 | 5 465 | 38.8 | 20 | 72 814 | 13.44 | 55 | 5 | ND | 2 27 | 4 | 2 | 2 | 19 11.49 | .033 | 2 | 14 | .19 | 2 | .04 | 2 | .45 | .01 | .01 | 7 | .097 | | | | | | |
| FS87-1-9A | 22 B11 | 10 125 | 2.0 | 70 | 75 2232 | 42.70 | 134 | 5 | ND | 6 30 | 1 | 14 | 2 | 32 5.26 | .025 | 2 | 51 | .23 | 49 | .09 | 24 | .37 | .01 | .02 | 1 | .004 | | | | | | |
| FS87-1-9B | 25 573 | 12 133 | 2.0 | 25 | 44 2227 | 49.23 | 172 | 5 | ND | 6 22 | 1 | 4 | 2 | 24 3.16 | .015 | 2 | 30 | .18 | 71 | .02 | 30 | .17 | .01 | .03 | 1 | .006 | | | | | | |
| FS87-1-10 | 1 296 | 2 75 | .7 | 15 | 21 493 | 4.22 | 13 | 5 | ND | 4 392 | 3 | 3 | 2 | 149 3.68 | .161 | 4 | 20 | 1.52 | 108 | .26 | 10 | 4.93 | .38 | .30 | 1 | .004 | | | | | | |
| FS87-1-11 | 1 62 | 2 57 | .3 | 12 | 12 480 | 4.36 | 10 | 5 | ND | 3 349 | 1 | 2 | 2 | 139 3.14 | .153 | 5 | 26 | 1.53 | 33 | .23 | 4 | 3.73 | .63 | .13 | 1 | .003 | | | | | | |
| FS87-1-12A | 1 110 | 2 23 | .3 | 24 | 10 246 | 1.62 | 18 | 5 | ND | 2 83 | 1 | 2 | 2 | 64 1.99 | .037 | 2 | 48 | .30 | 17 | .43 | 2 | 1.22 | .12 | .06 | 3 | .002 | | | | | | |
| FS87-1-12B | 1 371 | 2 46 | .9 | 44 | 34 308 | 3.24 | 25 | 5 | ND | 3 117 | 3 | 6 | 2 | 75 2.15 | .049 | 2 | 78 | .64 | 17 | .41 | 6 | 1.67 | .26 | .04 | 8 | .004 | | | | | | |
| FS87-1-13A | 1 1118 | 10 60 | 1.8 | 28 | 31 1053 | 19.95 | 22 | 5 | ND | 3 89 | 3 | 2 | 11 | 39 4.34 | .007 | 2 | 9 | 1.19 | 2 | .02 | 2 | .83 | .01 | .01 | 1 | .004 | | | | | | |
| FS87-1-13B | 1 729 | 2 22 | 1.0 | 11 | 7 1250 | 4.54 | 34 | 5 | ND | 1 59 | 3 | 2 | 2 | 31 10.53 | .007 | 2 | 7 | .49 | 2 | .01 | 3 | .53 | .01 | .01 | 4 | .003 | | | | | | |
| FS87-1-18 | 1 15945 | 12 756 | 29.3 | 15 | 310 700 | 19.58 | 201 | 5 | 27 | 4 11 | 10 | 2 | 3 | 10 2.05 | .002 | 2 | 8 | .21 | 2 | .01 | 2 | .34 | .01 | .01 | 1 | .692 | | | | | | |
| FS87-1-19 | 3 2241 | 9 103 | 3.0 | 32 | 141 1137 | 13.07 | 158 | 5 | ND | 2 31 | 3 | 4 | 2 | 64 8.21 | .029 | 2 | 54 | .49 | 4 | .29 | 4 | 1.10 | .03 | .04 | 9 | .013 | | | | | | |
| FS87-1-20 | 2 226 | 2 55 | .6 | 4 | 7 773 | 2.02 | 35 | 38 | ND | 1 531 | 1 | 2 | 2 | 37 24.07 | .068 | 2 | 4 | .74 | 70 | .10 | 12 | 1.57 | .14 | .10 | 2 | .005 | | | | | | |
| FS87-2-21 | 1 2448 | 4 14948 | 2.4 | 2 | 14 717 | 15.56 | 281 | 5 | ND | 2 24 | 175 | 2 | 2 | 10 1.45 | .005 | 2 | 7 | .46 | 15 | .02 | 2 | .53 | .01 | .02 | 2 | .008 | | | | | | |
| FS87-2-22 | 1 4195 | 6 24286 | 2.8 | 4 | 25 530 | 16.09 | 222 | 5 | ND | 3 13 | 256 | 2 | 3 | 8 1.23 | .006 | 2 | 9 | .69 | 6 | .01 | 6 | .79 | .01 | .02 | 1 | .019 | | | | | | |
| FS87-2-23A | 4 16181 | 8 1747 | 30.7 | 8 | 54 1797 | 10.04 | 113 | 5 | 26 | 1 10 | 27 | 3 | 2 | 25 11.74 | .011 | 2 | 9 | .30 | 2 | .02 | 2 | .87 | .01 | .01 | 5 | .526 | | | | | | |
| FS87-2-23B | 4 8782 | 4 372 | 10.0 | 6 | 82 1722 | 10.54 | 153 | 5 | 4 | 1 5 | 6 | 2 | 2 | 22 9.11 | .012 | 2 | 7 | .16 | 2 | .01 | 2 | .45 | .01 | .01 | 2 | .219 | | | | | | |
| FS87-2-26 | 1 4960 | 8 50955 | 1.6 | 2 | 13 312 | 17.80 | 358 | 5 | ND | 2 68 | 619 | 2 | 10 | 44 .18 | .006 | 2 | 5 | .63 | 6 | .01 | 5 | 1.23 | .01 | .05 | 48 | .011 | | | | | | |
| FS87-2-27 | 3 577 | 3 605 | .6 | 7 | 7 1446 | 6.07 | 29 | 5 | ND | 2 63 | 12 | 3 | 2 | 27 13.35 | .020 | 2 | 26 | 1.65 | 86 | .08 | 2 | 1.83 | .03 | .24 | 2 | .005 | | | | | | |
| FS87-2-28 | 5 9155 | 6 412 | 10.2 | 7 | 30 1033 | 12.74 | 154 | 5 | ND | 1 2 | 8 | 2 | 2 | 7 13.89 | .009 | 2 | 10 | .24 | 3 | .01 | 2 | .30 | .01 | .01 | 55 | .061 | | | | | | |
| FS87-2-30 | 1 284 | 2 799 | .5 | 6 | 12 603 | 3.42 | 22 | 5 | ND | 4 130 | 8 | 2 | 2 | 70 1.63 | .076 | 5 | 15 | 2.34 | 78 | .18 | 11 | 2.46 | .16 | .40 | 1 | .002 | | | | | | |
| FS87-3-24 | 1 225 | 6 203 | .3 | 3 | 7 1540 | 5.34 | 26 | 5 | ND | 3 29 | 3 | 2 | 2 | 28 6.09 | .051 | 5 | 10 | 1.95 | 16 | .07 | 2 | 1.34 | .03 | .02 | 3 | .071 | | | | | | |
| FS87-3-25 | 10 353 | 3 185 | .2 | 9 | 12 525 | 3.64 | 13 | 5 | ND | 2 38 | 1 | 2 | 2 | 69 .77 | .040 | 3 | 17 | 2.37 | 58 | .18 | 2 | 2.53 | .05 | .28 | 1 | .003 | | | | | | |
| FS87-3N-29 | 3 396 | 17 970 | 1.2 | 9 | 14 6251 | 6.25 | 19 | 5 | ND | 2 122 | 31 | 2 | 2 | 86 8.84 | .186 | 8 | 16 | 3.02 | 281 | .13 | 8 | 4.69 | .03 | .31 | 1 | .005 | | | | | | |
| FS87-4-31 | 1 1945 | 7 5304 | 1.8 | 4 | 4 135 | 6.29 | 223 | 5 | ND | 1 8 | 74 | 2 | 2 | 9 .23 | .007 | 2 | 3 | .21 | 26 | .02 | 2 | .35 | .01 | .04 | 5 | .010 | | | | | | |
| FS87-4-32 | 1 1288 | 8 6737 | .8 | 2 | 7 597 | 16.02 | 165 | 5 | ND | 3 16 | 85 | 2 | 3 | 17 1.04 | .009 | 2 | 6 | .26 | 23 | .01 | 2 | .46 | .01 | .03 | 3 | .004 | | | | | | |
| FS87-4-33A | 1 4190 | 9 30435 | 2.3 | 3 | 12 556 | 18.08 | 262 | 5 | ND | 3 9 | 352 | 2 | 12 | 38 .50 | .013 | 2 | 7 | 2.14 | 10 | .01 | 2 | 1.85 | .01 | .02 | 1 | .017 | | | | | | |
| FS87-4-33B | 1 877 | 7 3192 | .9 | 2 | 4 144 | 13.42 | 249 | 5 | ND | 2 3 | 35 | 2 | 4 | 7 .26 | .001 | 2 | 4 | .22 | 15 | .01 | 3 | .30 | .01 | .01 | 2 | .006 | | | | | | |
| FS87-4-34A | 4 1523 | 2 4136 | .6 | 9 | 18 1809 | 5.37 | 37 | 5 | ND | 3 57 | 19 | 2 | 2 | 71 3.25 | .073 | 4 | 16 | 3.56 | 60 | .14 | 2 | 3.18 | .05 | .19 | 11 | .004 | | | | | | |
| FS87-4-34B | 1 15940 | 14 6345 | 16.1 | 7 | 22 943 | 5.46 | 57 | 5 | 4 | 3 19 | 63 | 2 | 2 | 15 4.20 | .015 | 4 | 16 | 2.60 | 9 | .04 | 5 | 1.02 | .01 | .02 | 14 | .180 | | | | | | |
| FS87-4-34C | 6 21258 | 15 1578 | 24.4 | 3 | 27 900 | 13.99 | 67 | 5 | 7 | 3 21 | 15 | 3 | 2 | 4 15.52 | .001 | 6 | 10 | .25 | 3 | .01 | 2 | .17 | .01 | .01 | 113 | .293 | | | | | | |
| FS-4-SENTINAL | 1 1071 | 15295 | 9302 | 16.0 | 1 1 | 267 | .24 | 62 | 7 | ND | 1 123 | 145 | 389 | 6 | 2 20.00 | .006 | 2 | 1 | 11.86 | 1 | .01 | 3 | .09 | .01 | .01 | 1 | .002 | | | | | |
| GRAB FS87-1-14 | 4 19268 | 24 383 | 23.2 | 32 | 140 | 169 | 8.64 | 16 | 5 | ND | 2 87 | 2 | 2 | 50 1.11 | .029 | 2 | 46 | .37 | 20 | .21 | 5 | .99 | .06 | .05 | 1 | .011 | | | | | | |
| GRAB FS87-1-15 | 8 6890 | 185 | 182 | 9.1 | 57 | 121 | 183 | 11.12 | 22 | 5 | ND | 3 89 | 3 | 6 | 2 | 51 1.44 | .062 | 2 | 71 | .33 | 9 | .41 | 4 | .75 | .05 | .03 | 1 | .002 | | | | |
| STD C | 19 61 | 37 | 133 | 7.4 | 67 | 28 | 1035 | 3.81 | 40 | 20 | 7 | 40 | 50 | 17 | 17 | 21 | 59 .47 | .088 | 38 | 63 | .87 | 178 | .08 | 37 | 1.78 | .06 | .13 | 13 | - | | | |

- ASSAY REQUIRED FOR CORRECT RESULT for Cu, Pb > 10,000 ppm
 Zn > 20,000 ppm

VANANDA GOLD FILE # 87-4932A

Page 2

| SAMPLE# | MO | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SR | Cu | SB | BI | V | CA | P | LA | CR | Mg | BA | TI | B | AL | NA | K | M | AU88 |
|-----------------|-----|-------|-----|-------|------|-----|-----|------|-------|------|-----|-----|-----|-----|------|-----|-----|-----|-------|------|-----|-----|-----|-----|-----|-----|------|-----|------|----|------|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | DZ/T | | |
| GRAB FS 87-1-16 | 1 | 23516 | 10 | 378 | 22.7 | 28 | 249 | 57 | 20.37 | 22 | 5 | ND | 4 | 6 | 4 | 2 | 3 | 7 | .24 | .010 | 2 | 8 | .05 | 2 | .03 | 2 | .13 | .01 | .01 | 1 | .004 |
| GRAB FS 87-2-17 | 1 | 1753 | 5 | 27473 | .7 | 2 | 15 | 132 | 11.44 | 182 | 5 | ND | 2 | 3 | 322 | 2 | 2 | 4 | .27 | .005 | 2 | 7 | .17 | 4 | .01 | 5 | .15 | .01 | .01 | 1 | .006 |
| MANTO #1 | 3 | 282 | 14 | 14 | .7 | 1 | 3 | 421 | .19 | 3 | 7 | ND | 3 | 512 | 1 | 3 | 2 | 2 | 48.14 | .002 | 2 | 1 | .17 | 1 | .01 | 4 | .06 | .01 | .01 | 1 | .001 |
| MANTO #2 | 3 | 38 | 33 | 896 | 1.0 | 1 | 1 | 5110 | .17 | 15 | 5 | ND | 4 | 601 | 4 | 7 | 2 | 4 | 47.86 | .001 | 2 | 1 | .14 | 1 | .01 | 2 | .01 | .01 | .01 | 1 | .002 |
| MANTO #3 | 3 | 2956 | 87 | 84673 | 21.6 | 1 | 5 | 2192 | 13.46 | 526 | 5 | 6 | 1 | 156 | 1067 | 2 | 2 | 4 | 10.23 | .001 | 2 | 8 | .08 | 2 | .01 | 4 | .01 | .01 | .01 | 1 | .280 |
| MANTO #4 | 1 | 2133 | 100 | 29129 | 15.3 | 1 | 25 | 1082 | 18.02 | 1272 | 5 | ND | 3 | 33 | 225 | 7 | 2 | 3 | 2.71 | .001 | 2 | 1 | .05 | 1 | .01 | 2 | .01 | .01 | .01 | 1 | .220 |
| MANTO #5 | 3 | 1869 | 124 | 32408 | 15.5 | 1 | 28 | 1163 | 17.62 | 967 | 5 | 2 | 2 | 44 | 255 | 5 | 2 | 2 | 2.66 | .001 | 2 | 2 | .05 | 1 | .01 | 2 | .01 | .01 | .01 | 1 | .197 |
| MANTO #6 | 1 | 3995 | 134 | 86410 | 21.6 | 1 | 17 | 995 | 17.81 | 1192 | 5 | ND | 2 | 22 | 902 | 3 | 4 | 2 | 1.58 | .001 | 2 | 1 | .02 | 1 | .01 | 2 | .03 | .01 | .01 | 1 | .237 |
| STD C | 18 | 58 | 37 | 129 | 7.3 | 68 | 28 | 1030 | 3.84 | 39 | 19 | 7 | 39 | 51 | 19 | 18 | 22 | 60 | .46 | .087 | 39 | 58 | .88 | 176 | .08 | 37 | 1.81 | .06 | .14 | 13 | - |

ADDITION TO GEOLOGIC REPORT TEXADA ISLAND PROPERTY
by J.L. Hardy, Nimbus Management Ltd., Feb., 1988

The exploration program described in this report is part of an ongoing project involving additional mapping, rock chip and soil sampling, diamond drilling and S.P. surveying. The present results, however, enable some preliminary conclusions as follows.

1. Areas of Detailed Mapping

Significant untested potential both for Au-Cu veins and skarn-type deposits remains in the area of the Little Billie, Cornell and Little Billie gravity anomaly. The present mapping program has re-discovered old workings, as well as areas of bleaching and garnetite for which detailed sampling is recommended. Areas of brecciation in the area of the Little Billie will require more detailed mapping as well as sampling.

2. Florence/Security Area: Trenching, Detailed Mapping, Rock Chip Sampling

The trenching program exposed an area over 700m of highly prospective ground in the area of the Florence/Security old showings and workings. A total of 176 rock chip samples were collected as shown in Figure 6. Best results obtained were: 1.2m of 0.692 oz/ton Au, 29.3 ppm Ag, 15,945 ppm Cu; 1.5m of 0.180 oz/ton Au, 16.1 ppm Ag, 15,940 ppm Cu; and 0.9m of 0.243 oz/ton Au, 23.6 ppm Ag, 18,242 ppm Cu. Significant gold colours were present in several panned samples which yielded negligible gold on assay, suggesting a possible metallic/gold nugget effect. Additional sampling will be required to resolve this potential problem.

FILMED

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3. Vananda Grid Soil Samples

Soil sample highs up to 3300 ppb Au with 10,651 ppm Cu, 1090 ppb Au with 4823 ppm Cu and 1590 ppb Au with 535 ppm Cu are present in several areas of the grid. While ground truthing is as yet not complete, these results suggest significant potential in areas not known to be previously prospective.

4. S.P. Surveying

Station spacings ranged from 10 to 20 m on lines spaced at 100m. Results as yet are very incomplete; broad but well-defined anomalies appear to be present, trending roughly north-south from anomalous ground owned by others to the west of the Vananda Gold claim boundary. Infill has been completed to cover all of Vananda Gold's ground from Priest Lake in the west to Dismal Swamp in the east. A discrete anomaly on line 2+00N, 3+50W lies wholly within the Karmutsen Group volcanics yet contains limestone as (?) possible cavern infill.

Data?

5. Diamond Drilling

One hole has been drilled to date to an approximate 25m depth. Extremely high sulphide in some sections has created core recovery problems. This has necessitated several shut downs in an attempt to experiment with more favourable bits. When these are obtained, the hole will be deepened to machine limit. To date the hole has intersected several sections of massive pyrite with up to 4% chalcopyrite and intervals of coarsely crystalline white marble. Final logging awaits hole completion.

NOT COMPILED
ON BASEMAP
AT THIS TIME

S.P. SURVEY

VANCOUVER (CONT)

FEB 28/88

START

BASE STATION ON TURTLE LAKE RD. = 0

ST. #2 = -25.

FLORENCE BASELINE

0+00 = 0

0+46 N = 0

0+60 = +8

0+80 = -15

1+00 = -2

1+20 = -9

1+40 = -9

1+60 = -2

1+80 = -10

2+00 = -10

2+20 = -5

(SULPHIDES INPUT FS87-2-23B -90) 2+40 = -12

2+60 = 0

2+80 = -2

3+00 = -6

3+20 = -5

3+40 = -15

3+60 = -23.

3+80 = -35

4+00 = +10

4+20 = -10

4+40 = -10

BASE STATION

1+80 N = 0

(TO SULPHIDES INPUT FS87-2-23B -105) 1+80N / 0+10W = +30

0+20 W = +2

0+30 W = -2

0+40 W = -7

SP SURVEY PAGE 2

(FROM B.S. 1+80N)

$$1+80N / 0+50 = -5$$

$$0+60 = -2$$

$$0+70 = 0$$

$$0+80 = -20$$

$$0+90 = -18$$

$$1+00 = -15$$

$$2+00N / 0+10W = -9$$

$$0+20W = -30$$

$$0+30W = 0$$

$$0+40W = -22$$

$$0+50W = -5$$

$$0+60W = -20$$

$$0+70W = -15$$

$$0+80W = -10$$

$$0+90W = -9$$

$$1+00W = +5$$

$$2+20N / 0+10W = -19$$

$$0+20W = -20$$

$$0+30W = -20$$

$$0+40W = -10$$

$$0+50W = -25$$

$$0+60W = -17$$

$$0+70W = -17$$

$$0+80W = -15$$

$$0+90W = -7$$

$$1+00W = 0$$

$$2+40N / 0+10W = -32$$

$$0+20W = -25$$

$$0+30W = -20$$

$$0+40W = -20$$

(ON ROSKARN LEDGE FS87-2-119 = -35)

(From B.S. +80N)

$$2+40w / 0+50w = -20$$

$$0+60w = -18$$

$$0+70w = -12$$

$$0+80w = -15$$

$$0+90w = +1$$

$$1+00w = 0$$

BASE STATION

$$2+60w / B.L. = 0$$

$$0+10w = 0$$

$$0+20w = -2$$

$$0+30w = -5$$

$$0+40w = -8$$

$$0+50w = -6$$

$$0+60w = -10$$

$$0+70w = 0$$

$$0+80w = -10$$

$$0+90w = +9$$

$$1+00w = +1$$

$$2+80w / 0+10w =$$

$$0+20w = -5$$

$$0+30w = -15$$

$$0+40w = 0$$

$$0+50w = -11$$

$$0+60w = -10$$

$$0+70w = -15$$

$$0+80w = -12$$

$$0+90w = -12$$

$$1+00w = 0$$

$$3+00w / 0+10w = +7$$

$$0+20w = 0$$

S.P. SURVEY page 4

(FROM S.S. 2+60N.)

$$3+00N / 0+30W = 0$$

FLORENCE SHAFT

$$0+40W = -27$$

$$0+50W = -35$$

$$0+60W = -8$$

$$0+70W = 0$$

$$0+80W = -17$$

$$0+90W = -17$$

$$1+00W = -20$$

BASE STATION

$$3+00N / 0+70W = 0$$

$$0+80W = -11$$

$$0+90W = -17$$

$$1+00W = -12$$

$$1+10W = -18$$

$$1+20W = -9$$

$$1+30W = -9$$

$$1+40W = +5$$

$$1+50W = 0$$

$$1+60W = -5$$

IN VOLCANICS

$$1+70W = +6$$

$$1+80W = +22$$

$$1+90W = ?$$

$$2+00W = -3$$

EDGE DISMAL SWAMP

$$2+10W = +25$$

$$2+20W = +1$$

$$2+30W = +10$$

$$2+40W = -5$$

$$2+50W = +15$$

$$2+60W = +15$$

$$2+70W = 0$$

$$2+80W = +18$$

OLD FRENCHS
PARALLELING LINE

S.P. SURVEY page 5.

(from B.S. 3+00N / 0+70W)

3+00N / 2+90W = 0

3+00 W = +1

3+10 W = +1

3+20 W = 0

3+30 W = +20

3+40 W = +5

3+50 W = -10

3+60 W = -18

OLD PIPELINE - ROCKY BLUFF

3+70 W = -20

3+80 W = +7

(4+00W ON OLD L. 3N)

3+90W = +15

4+00W = +8

4+10W = +9

4+20W = 0

(4+30W ON OLD L. 3N)

4+30W = -11

4+40W = -3

4+50W = -40

4+60W = -42

4+70W = -15

4+80W = -40

4+80W = 0

4+90W = -5

-40

-45

BASE STATION (-40)

5+00W = +20

-20

5+10W = +20

-20

5+20W = +20

-20

5+30W = +25

-15

5+40W = +15

-25

(5+50W ON OLD L. 3N)

5+50W = +10

-30

5+60W = -11

-51

5+70W = -52

-92

5+80W = -40

-80

S.P. SURVEY page 20.

(FROM B.S. 3100N / 4+80W)
(-40)

| | | |
|-----------------|-----|------|
| 3100N / 5+90W = | -75 | -115 |
| 6+00 W = | -65 | -105 |
| 6+10 W = | -17 | -57 |
| 6+20 W = | -8 | -48 |
| 6+30 W = | 0 | -40 |
| 6+40 W = | +10 | -30 |
| 6+50 W = | 0 | -40 |

TURN WEST onto RHY. L 390S at 60E

| | | |
|--------------------------|------------|-----|
| L 390S / 45E = | +12 | -28 |
| 30E = | 0 | -40 |
| 15E = | -10 | -50 |
| (RHY. SP. -34) Bl. 390 = | -12 | -52 |
| (" -71) 360S = | -50 | -90 |
| (" -55) 330S = | -45 | -85 |
| (+ -65) 300S = | -45 | -85 |
| ? | 270S = -35 | -75 |

V.G. 4100N crosses B.L. at 267S

TURN E. to 45° down 4100N

| | | |
|-----------------|-----|-----|
| 4100N / 6+30W = | -50 | -90 |
| 6+20W = | -45 | -85 |
| 6+10W = | -35 | -75 |
| 6+00W = | -42 | -82 |
| 5+90W = | -42 | -82 |

BASE STATION (-82)

| | | |
|----------------|-----|-----|
| 4100/N 5+90W = | 0 | -82 |
| 5+80W = | -8 | -90 |
| 5+70W = | 0 | -82 |
| 5+60W = | +5 | -77 |
| 5+50W = | 0 | -82 |
| 5+40W = | +27 | -55 |
| 5+30W = | +23 | -59 |
| 5+20W = | +18 | -64 |

S.P. SURVEY page 7.

| | | |
|------------------------------------|----------------------|-------|
| (FROM B.S. 4+00N / 5+90W) (-82) | 4+00N / 5+10W = -15' | - 97 |
| | 5+00W = +5 | - 77 |
| (TURN TO 135° - EAST) | 3+80N / 5+00W = -10 | - 92 |
| | 3+60N / " = -16 | - 98 |
| | 3+45N / " = -30 | - 112 |
| | 3+20N / " = | |
| <u>BASE STATION</u> (-82) | 4+00N / 5+90W = 0 | - 82 |
| <u>CEMIM POST NE CORNER YEW</u> | 3+80N / 5+30W = -20 | - 108 |
| (ON V.G. GROUND) | 3+55N / 5+30W = -200 | - 282 |
| | 3+60N / " = -129 | - 211 |
| | 3+40N / " = -27 | - 109 |
| | 3+20N / " = 0 | - 92 |
| (2 3+00N OLD GRID) | 3+00N / " = +20 | - 62 |
| ↪ | 2+80N / " = +50 | - 32 |
| (OLD 2 3N / 5+50W IS 5mW.) | 2+80N / 5+40W = +50 | - 32 |
| | 3+00N / " = +30 | - 52 |
| | 3+20N / " = +8 | - 74 |
| | 3+40N / " = -7 | - 89 |
| (CROSS RHY. BOUNDARY AT 3+55N) | 3+60N / " = -5 | - 87 |
| | 3+80N / " = +45 | - 37 |
| | 3+80N / 5+50W = +22 | - 60 |
| | 3+60N / " = +16 | - 66 |
| (CROSS RHY. BOUNDARY) | 3+40N / " = -31 | - 113 |
| | 3+20N / " = +40 | - 42 |
| | 3+00N / " = +45 | - 37 |
| (OLD 2 3N / 5+50W IS 5mE.) | 2+80N / " = +50 | - 32 |
| | 2+80N / 5+20W = +75 | - 7 |
| | 3+00N / 5+20W = +3 | - 79 |
| | 3+20N / " = +15 | - 67 |

S.P. SURVEY page 8.

| | | |
|---------------------------|-----------------------|------|
| (from B.S. 4+00N / 5+90W) | 3+240N / 5+20W = -3 | -85 |
| (-82) | 3+60N / " = -55 | -137 |
| | ~ 3+80N / " = -50 | -132 |
| | 4+00N / " = +18 | -64 |
| | ~ 3+80N / 5+10W = -41 | -123 |
| | 3+60N / " = 0 | -82 |
| | 3+40N / " = +32 | -50 |
| | 3+20N / " = +25 | -57 |
| | 3+00N / " = +68 | -14 |
| | 2+80N / " = +45 | -37 |
| | 2+80N / 5+00W = +45 | -37 |
| | 3+00N / " = +2 | -80 |
| | 3+20N / " = -5 | -87 |

BASE STATION (-30) 3+00N / 5+50 = 0 -30

(on ad logging rd) 123° -20M. st. # 1 = +6 -24

106° - 40M. st. # 2 = +20 -10

106° - 60M " 3 = +20 -10

113° - 80M " 4 = +21 -9

(cross L2N / 5+43W) 127° - 100 " 5 = +25 -5

133° - 120 " 6 = +20 -10

131° - 140 " 7 = +45 +15

93° - 160 " 8 = +40 +10

96° - 180 " 9 = +37 +7

(on L1N at 5+00W) 143° - 200M " 10 = +33 +3

147° - 220M " 11 = +35 +5

155° - 240M " 12 = +45 +15

168° - 260M " 13 = +33 +3

187° - 280M " 14 = +45 +15

167° - 300M " 15 = +45 +15

S.P. SURVEY page 9.

(From B.S. 3+00N / 5+50W) (-30)

$$156^\circ - 320 \text{ m} \text{ St. } *16 = +50 \quad +20$$

$$126^\circ - 340 \text{ " } 17 = +40 \quad +10$$

(350m cross Lon at 5+80W) $108^\circ - 360 \text{ m} \text{ " } 18 = +40 \quad +10$

$$108^\circ - 380 \text{ m} \text{ " } 19 = +50 \quad +20$$

$$128^\circ - 400 \text{ m} \text{ " } 20 = +50 \quad +20$$

$$(CREEK 15M SE) \quad 120^\circ - 420 \text{ m} \text{ " } 21 = +45 \quad +15$$

$$70^\circ - 440 \text{ m} \text{ " } 22 = +50 \quad +20$$

BASE STATION (+15) St. #21 = 0 +15

$$70^\circ - 440 \text{ m} \text{ St. } 22 = +7 \quad +22$$

$$70^\circ - 460 \text{ m} \text{ " } 23 = +22 \quad +37$$

$$72^\circ - 480 \text{ m} \text{ " } 24 = -8 \quad +7$$

$$75^\circ - 500 \text{ m} \text{ " } 25 = -8 \quad +7$$

$$(CREEK at 515m bearing 345^\circ) \quad 77^\circ - 525 \text{ m} \text{ " } 26 = 0 \quad +15$$

$$96^\circ - 540 \text{ m} \text{ " } 27 = -8 \quad +7$$

$$80^\circ - 560 \text{ m} \text{ " } 28 = -8 \quad +7$$

$$40^\circ - 580 \text{ m} \text{ " } 29 = 0 \quad +15$$

$$25^\circ - 600 \text{ m} \text{ " } 30 = 0 \quad +15$$

(END OF LOGGING ROAD) $354^\circ - 620 \text{ m} \text{ " } 31 = +15 \quad +30$

(still volcanics)

$$180^\circ - 550 \text{ m} \text{ " } 32 = -10 \quad +5$$

$$180^\circ - 20 \text{ m} \text{ " } 33 = 0 \quad +15$$

(broken volcanics)

$$180^\circ - 40 \text{ m} \text{ " } 34 = -13 \quad +2$$

$$\text{ " } - 60 \text{ m} \text{ " } 35 = -12 \quad +3$$

(broken grey limestone)

$$\text{ " } - 80 \text{ m} \text{ " } 36 = -20 \quad -5$$

(TOP WHITE MARBLE BLUFF)

$$\text{ " } - 100 \text{ m} \text{ " } 37 = -25 \quad -10$$

$$\text{ " } - 120 \text{ m} \text{ " } 38 = -20 \quad -5$$

$$240^\circ - 140 \text{ m} \text{ " } 39 = -23 \quad -8$$

$$\text{ " } - 160 \text{ m} \text{ " } 40 = -25 \quad -10$$

S.P. SURVEY page 10.

| | | | |
|-----------------|-------------|--------------|-----|
| (FROM B.S. #21) | 240° - 180m | st. 41 = -50 | -35 |
| (+15) | " 190m " | 42 = -25 | -10 |
| | " 200m " | 43 = -18 | -3 |
| | " 220m " | 44 = -18 | -3 |
| | " 240m " | 45 = -22 | -7 |
| | " 250m " | 46 = -23 | -8 |
| | 232° - 270m | " 47 = -18 | -3 |
| | 240° - 290m | " 48 = -10 | +5 |
| | " 310m " | 49 = -15 | 0 |
| | " 330m " | 50 = -12 | +3 |

(LINE DOWN S. SIDE CREEK IN VOLC.) 240° - 30M (between #33 & #34)

TOWARDS PRIEST LAKE

| | | |
|-----------------|------------|------------|
| to 20m | st. 51 = 0 | +15 |
| 214° to 40m | " 52 = 0 | +15 |
| 230° 60m | " 53 = 0 | +15 |
| 230° 80m | " 54 = 0 | +15 |
| 270° 100m | " 55 = 0 | +15 |
| 250° 120m | " 56 = 0 | +15 |
| 248° 140m | " 57 = +10 | +25 |
| 180° 160m | " 58 = +2 | +17 |
| 220° 180m | " 59 = 0 | +15 |
| 220° 200m | " 60 = -2 | +13 |
| 270° 220m | " 61 = 0 | +15 |
| 290° 240m | " 62 = +5 | +20 |
| 280° 260m | " 63 = 0 | +15 |
| (COLD WOOD DAM) | 294° 280m | " 64 = -10 |
| | 235° 290m | " 65 = 0 |

(250M DUE W. TO ROAD AT PRIEST LAKE)

FROM BASE ST #7 = +10

GOING WEST

BL 4+00N = +10 = 0

20 = +2

40 = -27

60 = -72

80 = -35

100 = -22

120 = -14

140 = -1.0

160 = +10 BOTTOM OF CLIFF

180 = +28

200 = +5

220 = +10

240 = +10

260 = 0

280 = -50 VOL. PORPH.

300 = -32

320 = 0

340 = -5

360 = 0 ← PIPELINE

380 = -75

400 = -110 CLIFF AREA

420 = -69

440 = +83

460 = +40

480 = -45

500 = +2

BL 5+00N = -30 = 0

10 = -20

30 = -35

30 = -55 NEAR SHAFT

40 = -24 AREA

50 = -16

60 = -2

70 = +12

80 = -20

100 = -30

120 = -15

140 = -18

160 = -10

180 = -12

200 = -15

220 = -16

240 = -12

260 = -10

280 = -16

300 = -0) SWAMP

320 = +8) AREA

340 = -15

360 = -60) CLIFF AREA

380 = -40

400 = -20

FROM BASE ST #7 = +10
GOING WEST

BL 6+00 N = -15 = 0 BL 7+00 N = -25 = 0

10 = -14

10 = -17

20 = -15

20 = -5

30 = -21

30 = -5

40 = -36

40 = +3

50 = -27

50 = -15

60 = -25

60 = -3

70 = -35

70 = -11

80 = -12

80 = -47

90 = -25

90 = -27

100 = -24

100 = -43

110 = -5

110 = -165

120 = -30

120 = -95

130 = -10

130 = -40

140 = -11

140 = -33

150 = -25

150 = -23

160 = -20

160 = -5

170 = -40

170 = -5

180 = -50

180 = -7

190 = -43

190 = -26

200 = -55

200 = -15

210 = -30

210 = -33

SWAMP AREA

CLIFF AREA

CONTINUATION
OF TRENCH
#10?

SWAMP
AREA

CLIFF
AREA

FROM BASE ST. #1 = 0
GOING WEST

| LINE 0+00 | LINE 1+00 | LINE 2+00 |
|----------------|------------------|------------------|
| ST. 0 = 0 | ST. 0 = 0 | ST. 0 = 0 |
| 20 = 0 | 20 = 0 | 10 = +11 |
| 40 = -5 | 40 = -29 | 20 = +8 |
| 60 = 0 | 50 = -30 | 30 = +18 |
| 80 = 0 | 60 = -10 | 40 = 0 |
| <u>100 = 0</u> | <u>80 = 0</u> | <u>60 = +5</u> |
| EAST SIDE | 100 = -10 | 80 = 0 |
| OF SWAMP | 110 = 0 | 100 = 0 |
| | <u>120 = +18</u> | <u>120 = +4</u> |
| | EAST SIDE | |
| | OF SWAMP | <u>140 = +12</u> |
| | | EAST SIDE |
| | | OF SWAMP |

FROM BASE ST "4 = -40
GOING EAST

LINE 2+00

160]
180] SWAMP
200] AREA
220]

240 = +7

250 = -4

260 = -50

270 = -28 CREEK

280 = -25

300 = -23

320 = -36

340 = -50

350 = -151 CREEK

360 = -88 NOTE EXPOSURE

380 = -20 OF MARBLE IN

400 = -32 CREEK

420 = -19

440 = -23

460 = -18

480 = -2

500 = -12

FROM BASE ST # 6 = -30

GOING WEST

LINE 2+00 BASE ST # 11 = +25 = -5 = 0

520 = -14

540 = -15 ROAD

560 = -15

580 = +4

600 = -19

620 = -25

640 = -30

660 = -25 E. SIDE OF SWAMP

680 = -33 W. ~ ~ ~

700 = -26

720 = -27 EDGE OF SWAMP NEAR HWY

FROM BASE ST. +11 = +25 - -5 = 0
GOING EAST

LINE 1+00 SWAMP 40 m WIDE
 $160 = +15$ WEST SIDE OF SWAMP
 $180 = +4$
 $200 = +13$
 $220 = -5$
 $240 = -5$
 $260 = +3$
 $280 = +4$ CREEK
 $300 = +6$
 $320 = +2$
 $340 = +10$ CREEK
 $360 = -5$ PIPELINE
 $380 = -5$
 $400 = -1$ CLIFF
 $420 = +1$
 $440 = -5$
 $460 = -5$
 $480 = -5$

1340E + 11° 11' = +20 = -5 = 0

GOING WEST

LINE 1+00

500 = -1 ROAD

520 = -8

540 = -17

560 = -16

580 = -5 SWAMP

600 = -13

620 = -18 S. END OF A SWAMP

640 = -27

660 = -24

680 = -31

700 = -30

720 = -25 NEAR HWY.

BASE ST. 11 = +25 = -5 = 0

GOING WEST

LINE 0+00

580 = +10

600 = -20

620 = -9

640 = -12

680 = +3

700 = -5

720 = -5

740 = -14

760 = -2

780 = +28 EDGE OF CREEK NEAR HWY.

BASE ST. #12 = +15 = +10 = 0
GOING EAST

LINE 0+00

120 =



140 =

160 = W. SIDE OF SWAMP

180 = +45

200 = +30

220 = +37

240 = +35

260 = +22

280 = +10

300 = +25

320 = +5

340 = +25

360 = +26

CREEK

380 = +29

400 = +37

PIPELINE

420 = +31

440 = +23

460 = +22

480 = +25

500 = +38

520 = +10

DACITE DYKE

540 = +25

560 = +17

BASE LINE

↑
E

W
↓

BL 7+00 BL 6+00 BL 5+00 BL 4+00 2+60 N
BASE ST. BASE ST. BASE ST. BASE ST.
 $\#10 = -25$ $\#9 = -15$ $\#8 = -30$ $\#7 = +10$ $\#2 = 0$

BASE ST.
 $\#1 = 0$

SW in P

3+70 W
BASE ST.
 $\#3 = 0$

4+80 W
BASE ST.
 $\#4 = -40$
5+90 W
BASE ST.
 $\#5 = -41$

5+40 W
BASE ST.
 $\#11 = +25$
5+50 W
BASE ST.
 $\#6 = +10$

5+80 W
BASE ST.
 $\#12 = +15$

LEGEND

RECENT

Qal Recent Sediments

JURASSIC

MIDDLE TO UPPER JURASSIC - ISLAND INTRUSIONS

JD DIORITE

JHPD PORPHYRITIC HORNBLENDE DIORITE

JFPD FELDSPAR PORPHYRY DIORITE

JQD QUARTZ DIORITE

TRIASSIC

UPPER TRIASSIC - QUATSINO (MARBLE BAY) LIMESTONE

TQL LIMESTONE Dark grey to black, massive

TQM MARBLE Dark to pale grey, banding rare

TQM_b BLEACHED MARBLE Ivory to white

TQM_{bd} BLEACHED MARBLE Dolomitized

UPPER TRIASSIC AND OLDER - KARMUTSEN VOLCANICS

TKB PILLOW BASALT Related breccia & tuff

TKFa FLOW BASALT Amygdaloidal

TKC CALCARENITE

MINERALIZATION

SKCs CALC SILICATE SKARN

SKs SULPHIDE SKARN

QV QUARTZ VEIN

BO BORNITE

PY PYRITE

PO PYRRHOTITE

CPY CHALCOPYRITE

ZnS SPHALERITE

SYMBOLS

GEOLOGIC CONTACT DEFINED, APPROXIMATE, ASSUMED

FAULT DEFINED, APPROXIMATE, ASSUMED

LIMIT OF OUTCROP

CLIFF DEFINED, APPROXIMATE

DRILLHOLE

SURVEY MONUMENT

SHAFT, PIT

ADIT

TRACK, TRAIL, ROAD

SHORELINE DEFINED, APPROXIMATE

SAMPLE SOIL, ROCK

GRID NORTH

315° AZ.

H6 I6 J6
H7 I7 J7
H8 I8 J8

GEOLOGICAL BRANCH

REPORT

16,749

SCALE 1:1000

20 0 10 20 40 60 80 100 METRES

VANANDA GOLD LTD.

TEXADA ISLAND B.C.

SURFACE GEOLOGY

GRAVITY HIGH SOUTH OF LITTLE

BILLIE AREA BLOCK I7

MINING DISTRICT NANAIMO LAT. LONG.

L LINDINGER NTS DATE

REV.

FIG. DWG. REV.



LEGEND

RECENT

Qal Recent Sediments

JURASSIC

MIDDLE TO UPPER JURASSIC - ISLAND INTRUSIONS

JD DIORITE

JHPD PORPHYRITIC HORNBLENDE DIORITE

JFPD FELDSPAR PORPHYRY DIORITE

JQD QUARTZ DIORITE

SUFFIX TO LITHOLOGIES

V VITREOUS f FINE GRAINED <1mm e MEGACRYSTIC >5mm

m MEDIUM GRAINED 1-2mm c COARSE GRAINED 2-4mm

TRIASSIC

UPPER TRIASSIC - QUATSINO (MARBLE BAY) LIMESTONE

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TKFa FLOW BASALT Amygdaloidal

TKC CALCARENITE

MINERALIZATION

SKcs CALC SILICATE SKARN

SKs SULPHIDE SKARN

QV QUARTZ VEIN PY PYRITE PO PYRRHOTITE CPY CHALCOPYRITE

ZnS SPHALERITE

S Y M B O L S

GEOLOGIC CONTACT DEFINED, APPROXIMATE, ASSUMED

METAMORPHIC ISOGRAD

FAULT DEFINED, APPROXIMATE, ASSUMED

LIMIT OF OUTCROP

CLIFF DEFINED, APPROXIMATE

DRILLHOLE

SURVEY MONUMENT

SHAFT, PIT

ADIT

TRENCH

TRACK, TRAIL, ROAD

SAMPLE

SOIL, ROCK

SHORELINE DEFINED, APPROXIMATE

GRID NORTH

315° AZ.

GEOLOGICAL BRANCH

ASSESSMENT REPORT

SCALE 1:500

METRES

16,749

10 0 10 20 30 40 50

8800 N 8900 N 9000 N 9100 N 9200 E 9300 E 9400 E 9500 E 9600 E 9700 E 9800 E 9900 E

9850 E 9900 E

9800 E 9900 E

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9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

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8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

8600 N 8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

8550 N 8600 N 8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

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8150 N 8200 N 8250 N 8300 N 8350 N 8400 N 8450 N 8500 N 8550 N 8600 N 8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

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8050 N 8100 N 8150 N 8200 N 8250 N 8300 N 8350 N 8400 N 8450 N 8500 N 8550 N 8600 N 8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

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777 8050 N 8100 N 8150 N 8200 N 8250 N 8300 N 8350 N 8400 N 8450 N 8500 N 8550 N 8600 N 8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

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777 777 8000 N 8050 N 8100 N 8150 N 8200 N 8250 N 8300 N 8350 N 8400 N 8450 N 8500 N 8550 N 8600 N 8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

777 777 777 8000 N 8050 N 8100 N 8150 N 8200 N 8250 N 8300 N 8350 N 8400 N 8450 N 8500 N 8550 N 8600 N 8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

777 777 777 777 8000 N 8050 N 8100 N 8150 N 8200 N 8250 N 8300 N 8350 N 8400 N 8450 N 8500 N 8550 N 8600 N 8650 N 8700 N 8750 N 8800 N 8850 N 8900 N 8950 N 9000 N 9050 N 9100 N 9200 N 9300 N 9400 N 9500 N 9600 N 9700 N 9800 N 9900 N

LEGEND

JURASSIC

- JDD DIORITE (GABBRO) DYES
- JFPD POST VANANDA STOCK FELDSPAR PORPHYRY DYES
- JQD(0) VANANDA QUARTZ DIORITE AND DYES
- JFPD PRE VANANDA STOCK FELDSPAR PORPHYRY DYES (OPEN HORNFELSED)
- JAD ALASKITE DYES
- CRYSTAL SIZE IN ALL DYES HIGHLY VARIABLE
- (f) FINE GRAINED 1MM
- (m) MEDIUM GRAINED 1-2MM
- (c) COARSE GRAINED > 2MM
- (p) DEGEMATITE

TRIASSIC

MARBLE BAY LIMESTONE

- RLST LIMESTONE
- RM MARBLE UNDIFF
- TM_a(f)(m)(c) " FINE, MEDIUM, COARSE 1MM 1-2MM > 2MM BLEACHED
- TM_b " "
- TM_e " MEGACRYSTIC > 5MM

KARMUTSEN ? VOLCANICS

- RV

MINERALIZATION

- SK₁ WOLLASTONITE (CHLORITE) SKARN
- SK₂ GARNET + DIOPSID + ACTINOLITE SKARN
- SK₃ WOLLASTONITE BORNITE SKARN

- SK₅ SULPHIDE SKARN UNDIFF

- SK₆ COPPER SKARN (BORNITE, CPO, PY, ZnS, PPS) PO

- SK₁₀ MASSIVE MAGNETITE SKARN
ICPO, PO,

VEIN AND MANTO MINERALIZATION

- QU QUARTZ VEINING
- CV CALCITE VEINING
- STK STOCKWORK
- PY PYRITAE
- PO PYRPHOTITE
- CP CHALCOPYRITE
- ZnS SPHALERITE
- PBS GALENA
- T? TELLURIODES?

SYMBOLS

- GEOLOGIC CONTACT DEFINED APPROX ASSUMED
- FAULT DEFINED, APPROXIMATE
- STRIKE & DIP SYMBOL LIMIT OF OUT CROP
- CLIFF DEFINED, APPROXIMATE
- BRECCIA FRAGMENTS
- SHAFT, PIT
- DEPRESSION
- FLOAT OR SUBCROP
- DIAMOND DRILL HOLE
- DUMP
- PAVED ROAD
- SHORELINE DEFINED APPROXIMATE

16,749
GEOLOGICAL BRANCH
ASSESSMENT REPORT

VANANDA GOLD LTD

PRELIMINARY GEOLOGY

LITTLE BILLIE MINE AREA

TEXADA ISLAND B.C.

LAT 49°45'30"N LONG 124°23'00"E

0 20 40 60 80 100 METRES

SCALE 1:1000

L LINDINGER

JUNE 11 1987

LEGEND

RECENT

Qal Recent Sediments

JURASSIC

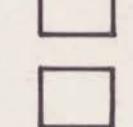
MIDDLE TO UPPER JURASSIC - ISLAND INTRUSIONS

JD DIORITE

JHPD PORPHYRITIC HORNBLENDE DIORITE

JFPD FELDSPAR PORPHYRY DIORITE

JQD QUARTZ DIORITE



SUFFIX TO LITHOLOGIES

V VITREOUS f FINE GRAINED <1mm e MEGACRYSTIC >5mm
m MEDIUM GRAINED 1-2mm. c COARSE GRAINED 2-4mm

TRIASSIC

UPPER TRIASSIC - QUATSINO (MARBLE BAY) LIMESTONE

TQL LIMESTONE Dark grey to black, massive

TQM MARBLE Dark to pale grey, banding rare

TQM_b BLEACHED MARBLE Ivory to white

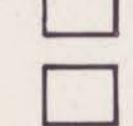
TQMbd BLEACHED MARBLE Dolomitized

UPPER TRIASSIC AND OLDER - KARMUTSEN VOLCANICS

TKB PILLOW BASALT Related breccia & tuff

TKFa FLOW BASALT Amygdaloidal

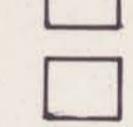
TKC CALCARENITE



MINERALIZATION

SKcs CALC SILICATE SKARN

SKs SULPHIDE SKARN



QV QUARTZ VEIN

BO BORNITE

EPI EPIDOTE

PY PYRITE

PO PYRRHOTITE

ZnS SPHALERITE

Cpy CHALCOPYRITE

Mag MAGNETITE

Wol WOLLASTONITE

SYMBOLS

GEOLIC CONTACT DEFINED, APPROXIMATE, ASSUMED
METAMORPHIC ISograd

FAULT DEFINED, APPROXIMATE, ASSUMED

LIMIT OF OUTCROP CLIFF DEFINED, APPROXIMATE

DRILLHOLE SURVEY MONUMENT

SHAFT, PIT ADIT

TRACK, TRAIL, ROAD SAMPLE SOIL, ROCK

SHORELINE DEFINED, APPROXIMATE

H9 NW NE I9
H9 SW SE
H10 I10

GEOLOGICAL BRANCH ASSESSMENT REPORT

GRID NORTH 315° AZ.

SCALE 1:500

16,749

METRES

VANANDA GOLD LTD.

TEXADA ISLAND B. C.

SURFACE GEOLOGY

CORNELL MINE AREA

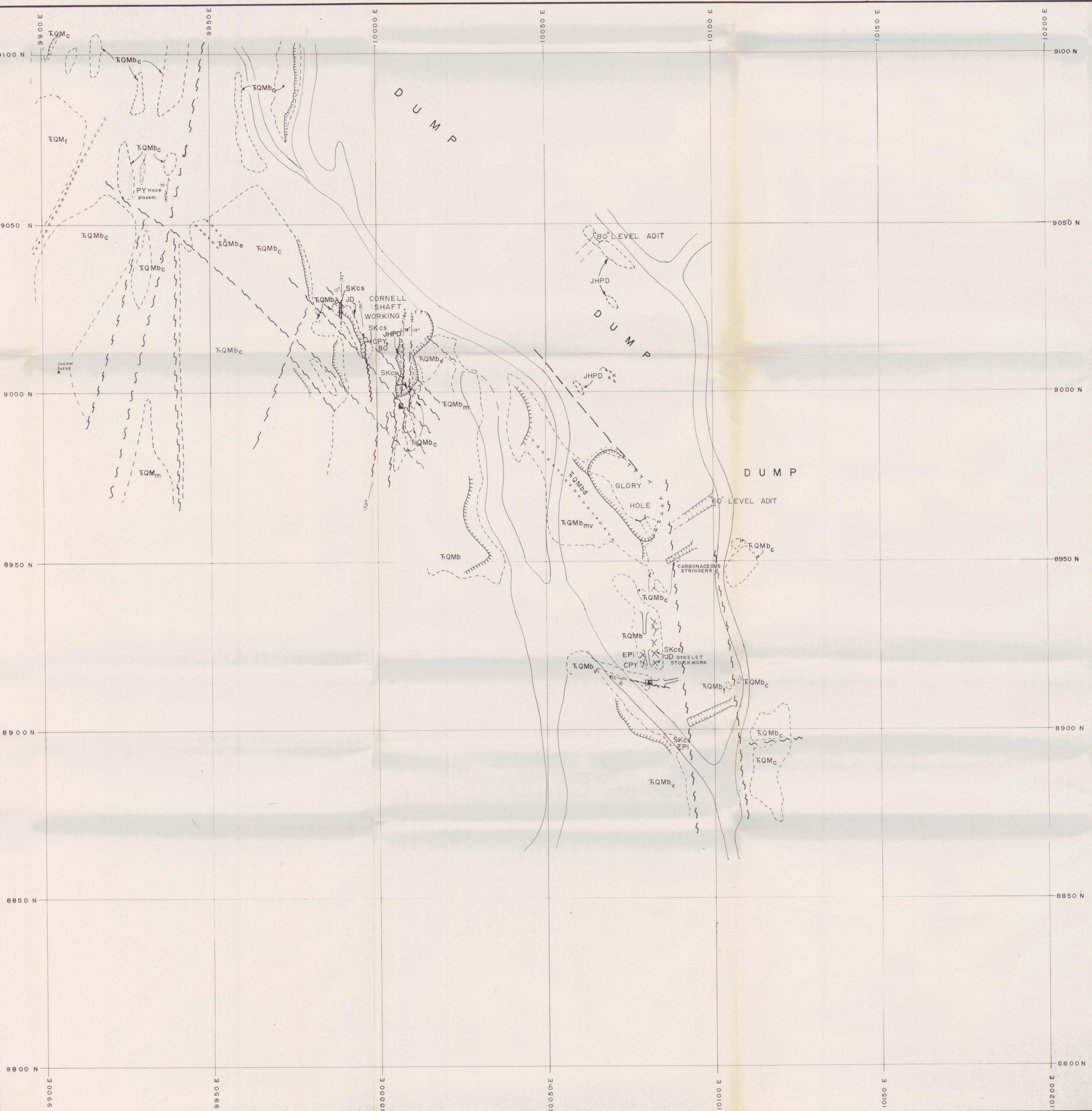
BLOCK H9 SE

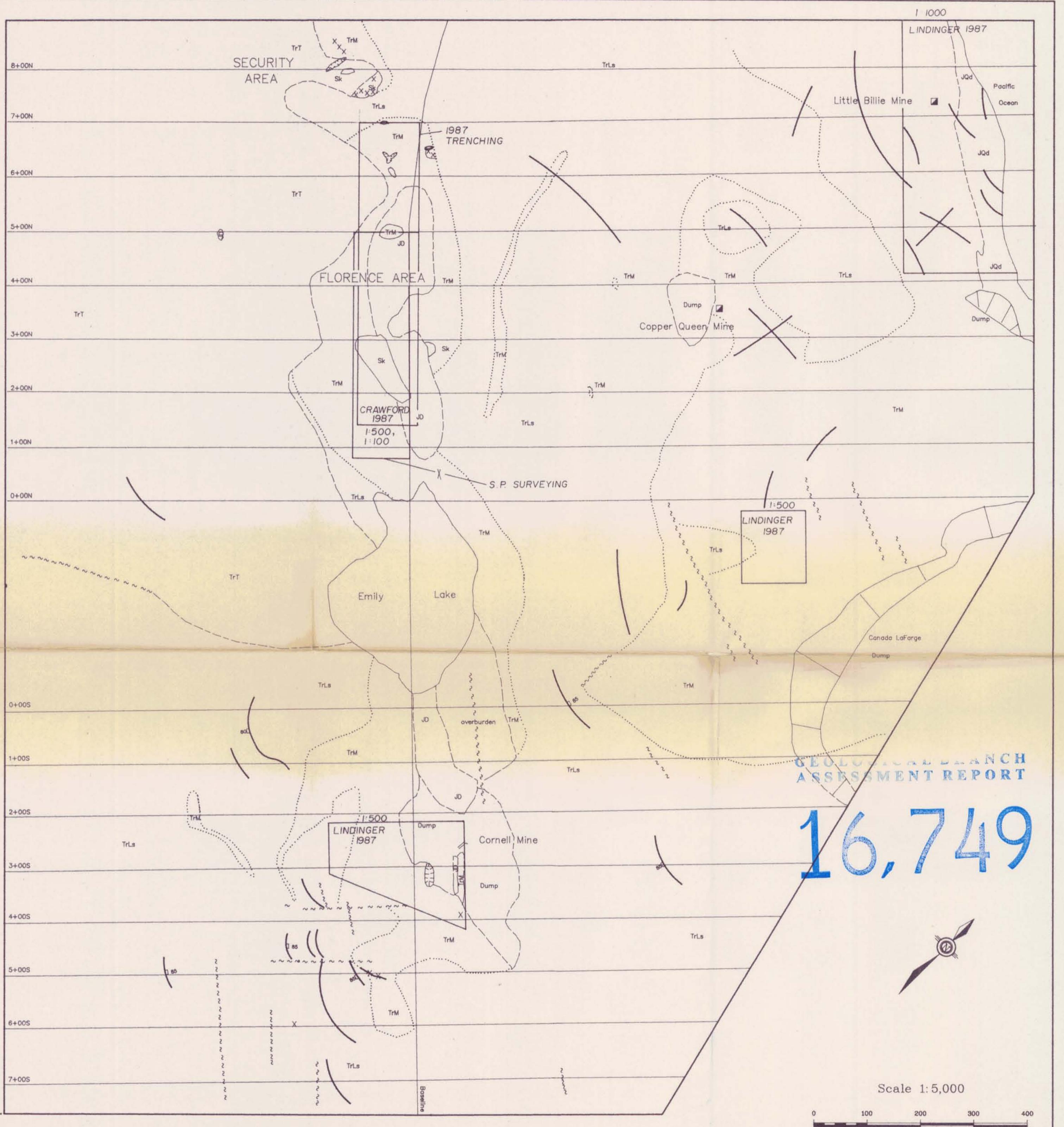
MINING DISTRICT NANAIMO LAT. LONG.

L LINDINGER NTS DATE

FIG. DWG. REV.

FIG. DWG. REV.





Middle-Upper Triassic

LEGEND

Middle-Upper Jurassic

JD Diorite-gabbro Intrusions

JQd Quartz dioritic Intrusions

Marble Bay Marble, recrystallized/bleached limestone

TrLs Marble Bay Limestone

TrT Texada Formation: Undifferentiated Basaltic/andesitic tuffs and flows

Sk Skarn: diopside-garnet replacement of marble or intrusive (epidote) with marble/diorite remnants

Mine waste

Marble contact: Between light/dark grey massive limestone and recrystallized limestone to white/dark grey granular marble

Undifferentiated dikes—generally dioritic-gabbroic, minor granitic phase

Inferred fault

X Prospect pit

Glory hole or large pit

Adit □ Shaft

○ Lithologic contact—Inferred

— Area of detailed mapping

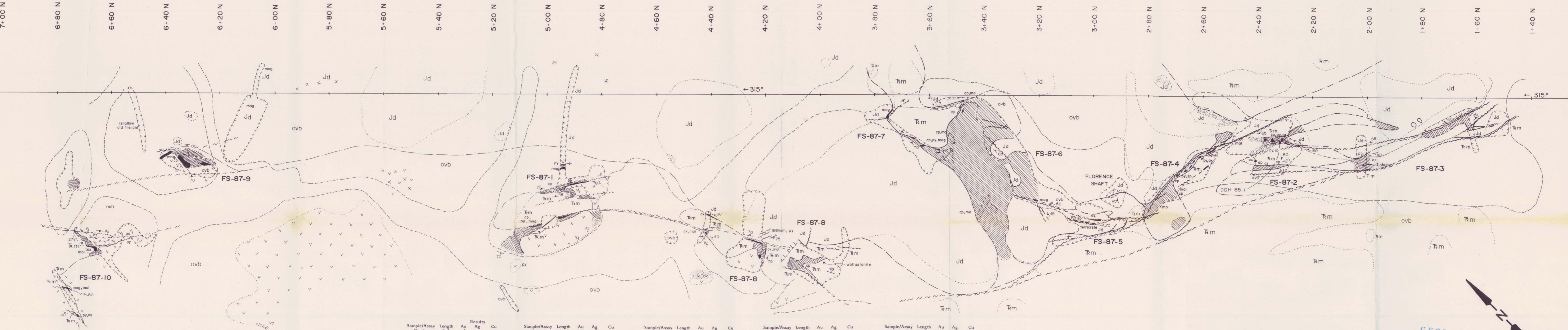
VANANDA GOLD LTD.

TEXADA ISLAND PROPERTY
NANAIMO, M.D., B.C.

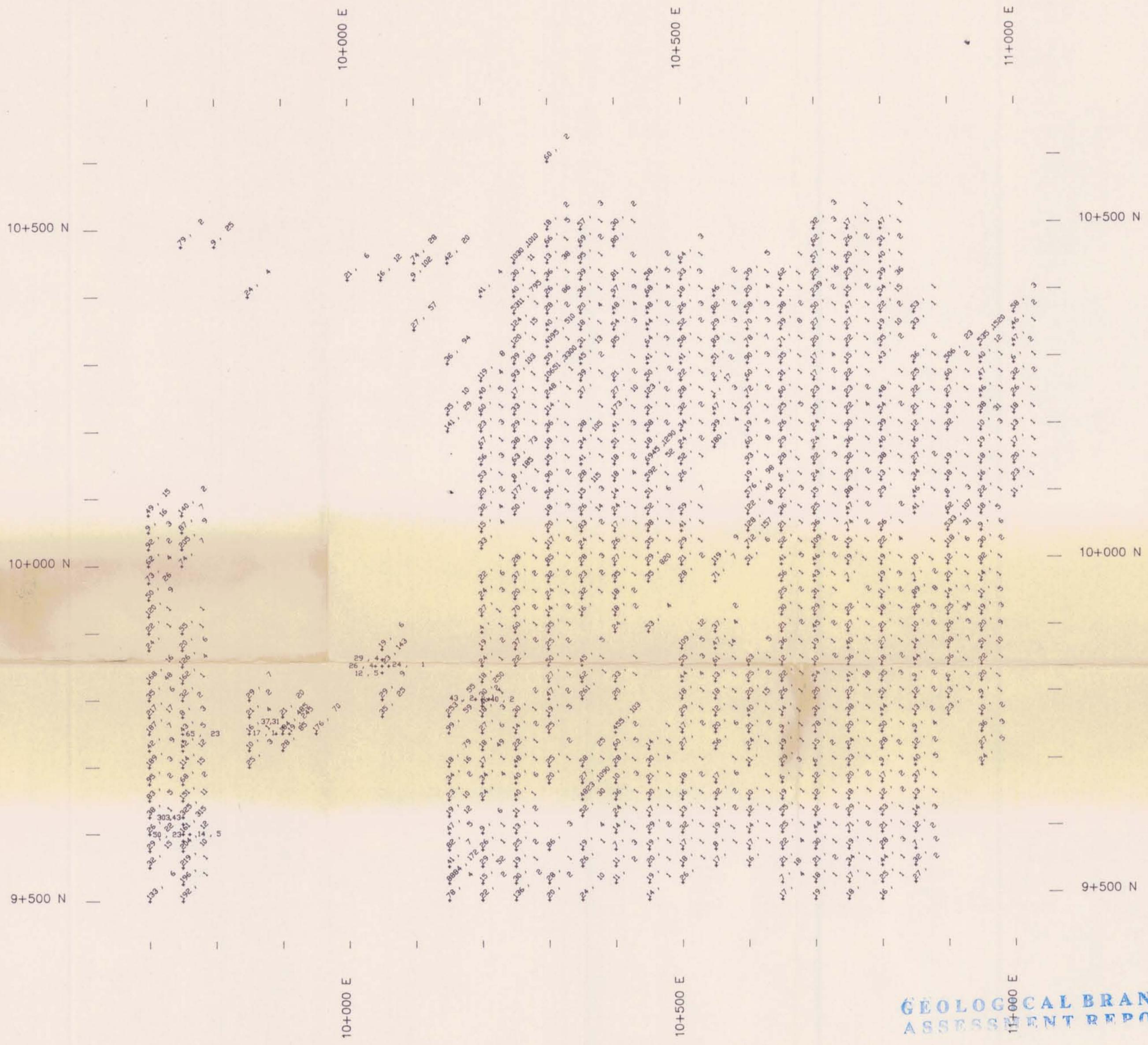
GEOLOGY MAP

| Original | Drawn | Date | PLAN No. | FIGURE |
|----------|-------|------------------|-------------|--------|
| Original | AE | Geo-Comp May '87 | | |
| Revision | | | N.T.S. | |
| Revision | | | 92F/10E,15E | 5 |

MINEQUEST EXPLORATION ASSOCIATES LTD.



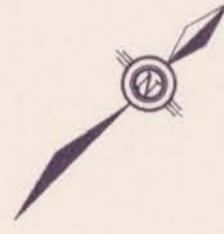
| Sample/Assay Number | Length (m) | Au oz/t | Ag ppm | Cu ppm | Sample/Assay Number | Length (m) | Au oz/t | Ag ppm | Cu ppm | Sample/Assay Number | Length (m) | Au oz/t | Ag ppm | Cu ppm | Sample/Assay Number | Length (m) | Au oz/t | Ag ppm | Cu ppm | Sample/Assay Number | Length (m) | Au oz/t | Ag ppm | Cu ppm |
|---------------------|------------|---------|--------|--------|---------------------|------------|---------|--------|------------|---------------------|------------|---------|--------|-----------|---------------------|------------|---------|--------|------------|---------------------|------------|---------|--------|--------|
| 6102/1.5* | 0.7 | 0.006 | 2.3 | 1,155 | 6126/3.25 | 0.003 | 0.2 | 353 | 6175/7.49A | 3.3 | 0.001 | 0.3 | 36 | 6317/9.68 | 0.9 | 0.001 | 0.1 | 25 | 6288/5.10A | 0.9 | 0.001 | 0.1 | 117 | |
| 6103/1.6 | 1.2 | 0.003 | 0.9 | 273 | 6127/2.26 | 1.7 | 0.011 | 0.4 | 4,960 | 6176/7.49B | 2.8 | 0.001 | 0.4 | 82 | 6318/9.69 | 2.0 | 0.001 | 0.1 | 33 | 6272/4.103 | 1.15 | 0.022 | 0.1 | 79 |
| 6104/1.7 | 0.9 | 0.002 | 0.7 | 1,155 | 6128/2.27 | 1.3 | 0.005 | 0.6 | 77 | 6177/7.49C | 2.1 | 0.001 | 0.5 | 99 | 6300/8.70 | 2.3 | 0.002 | 0.1 | 505 | 6273/4.106 | 0.92 | 0.021 | 0.1 | 54 |
| 6105/1.8 | 0.7 | 0.007 | 38.8 | 30,322 | 6129/2.28 | 1.5 | 0.061 | 10.2 | 9,155 | 6178/7.49D | 3.25 | 0.001 | 0.7 | 235 | 6301/8.71 | 2.7 | 0.003 | 0.2 | 633 | 6274/4.107 | 1.45 | 0.001 | 0.1 | 79 |
| 6106/1.9A | 1.2 | 0.004 | 2.0 | 811 | 6130/3.29 | 0.6 | 0.005 | 1.2 | 396 | 6179/9.50A | 1.8 | 0.006 | 0.6 | 1,013 | 6302/3.72 | 2.6 | 0.001 | 0.1 | 345 | 6275/4.108 | 1.35 | 0.001 | 0.1 | 198 |
| 6107/1.9B | 1.0 | 0.006 | 2.0 | 573 | 6131/2.20 | 1.5 | 0.002 | 0.5 | 284 | 6180/9.50B | 2.0 | 0.001 | 0.1 | 370 | 6303/8.73 | 2.4 | 0.002 | 0.4 | 379 | 6276/4.109 | 0.9 | 0.001 | 0.1 | 117 |
| 6108/1.9C | 1.0 | 0.002 | 0.7 | 296 | 6132/2.21 | 1.8 | 0.010 | 1.8 | 1,945 | 6181/9.51A | 2.1 | 0.002 | 0.8 | 313 | 6304/8.74 | 2.35 | 0.001 | 0.1 | 329 | 6277/4.110 | 1.2 | 0.001 | 0.2 | 15 |
| 6109/1.11 | 1.0 | 0.003 | 0.3 | 62 | 6133/4.32 | 0.7 | 0.009 | 1.2 | 1,238 | 6182/9.51B | 2.1 | 0.002 | 0.8 | 307 | 6305/8.75 | 2.15 | 0.004 | 0.5 | 799 | 6278/4.111 | 1.35 | 0.002 | 0.5 | 632 |
| 6110/1.12A | 1.1 | 0.002 | 0.3 | 110 | 6134/4.33A | 1.6 | 0.017 | 2.3 | 1,190 | 6183/9.52 | 1.25 | 0.001 | 0.5 | 441 | 6306/8.76 | 2.2 | 0.001 | 0.1 | 331 | 6278/4.112 | 1.25 | 0.021 | 2.8 | 9,280 |
| 6111/1.12B | 1.0 | 0.004 | 0.9 | 371 | 6135/4.33B | 1.3 | 0.006 | 0.9 | 877 | 6184/9.53A | 1.35 | 0.002 | 0.8 | 106 | 6307/8.77 | 2.5 | 0.002 | 2.2 | 1,298 | 6279/4.113 | 2.9 | 0.007 | 1.6 | 5,888 |
| 6112/1.13A | Grab | 0.904 | 1.8 | 1,118 | 6135/4.34A | 1.25 | 0.004 | 0.6 | 1,523 | 6185/9.53B | 1.9 | 0.021 | 4.0 | 3,171 | 6308/8.78 | 1.4 | 0.001 | 0.1 | 315 | 6280/4.114 | 1.0 | 0.001 | 0.1 | 116 |
| 6113/1.13B | Grab | 0.003 | 1.0 | 729 | 6136/4.34B | 0.9 | 0.004 | 0.8 | 1,180 | 6186/9.54 | 1.6 | 0.001 | 0.7 | 102 | 6309/8.79 | 1.5 | 0.001 | 0.1 | 192 | 6281/4.115 | 1.5 | 0.004 | 0.3 | 323 |
| 6114/1.14 | Grab | 0.003 | 1.3 | 19,668 | 6138/9.54C | 1.5 | 0.189 | 16.1 | 15,940 | 6187/9.55A | 2.0 | 0.001 | 0.8 | 280 | 6310/8.80 | 2.1 | 0.001 | 0.1 | 112 | 6282/4.116 | 0.9 | 0.001 | 0.1 | 68 |
| 6115/1.15 | Grab | 0.002 | 9.1 | 6,899 | 6139/4.35A | 2.6 | 0.002 | 0.4 | 179 | 6188/9.55B | 2.15 | 0.001 | 0.3 | 261 | 6311/8.81 | 2.4 | 0.001 | 0.1 | 73 | 6283/4.117 | 1.8 | 0.006 | 2.0 | 1,028 |
| 6116/1.16 | Grab | 0.004 | 22.7 | 23,316 | 6132/4.35B | 1.7 | 0.001 | 0.4 | 78 | 6189/9.56 | 2.0 | 0.001 | 0.1 | 195 | 6312/8.82 | 2.2 | 0.001 | 0.1 | 195 | 6286/4.118 | 0.9 | 0.002 | 3.8 | 5,732 |
| 6117/2.17 | Grab | 0.006 | 0.7 | 1,753 | 6133/4.35C | 1.7 | 0.001 | 0.5 | 45 | 6190/10.57 | 2.1 | 0.001 | 3.1 | 3,333 | 6313/8.83 | 2.3 | 0.001 | 0.1 | 93 | 6287/2.119 | 0.9 | 0.243 | 23.4 | 15,242 |
| 6118/2.18 | 1.2 | 0.002 | 29.3 | 15,945 | 6134/4.36 | Grab | 0.018 | 0.6 | 2,785 | 6191/10.58A | 2.2 | 0.001 | 0.9 | 3,093 | 6314/8.84 | 2.15 | 0.001 | 0.1 | 68 | 6288/2.120 | 1.1 | 0.022 | 5.3 | 4,430 |
| 6119/2.19 | 1.6 | 0.002 | 3.6 | 2,261 | 6135/4.37 | 2.1 | 0.002 | 0.3 | 179 | 6192/10.58B | 2.65 | 0.001 | 1.0 | 981 | 6315/8.85 | 2.15 | 0.001 | 0.1 | 48 | 6289/2.121 | 1.5 | 0.001 | 2.4 | 3,152 |
| 6120/2.20 | 0.6 | 0.003 | 0.6 | 2,261 | 6136/4.38A | 1.8 | 0.002 | 0.3 | 937 | 6193/10.58C | 2.75 | 0.001 | 0.7 | 349 | 6316/8.86 | 2.1 | 0.001 | 0.1 | 44 | 6290/2.122 | 1.1 | 0.001 | 0.5 | 37 |
| 6121/2.21 | 1.1 | 0.008 | 2.4 | 2,488 | 6137/4.38B | 2.3 | 0.039 | 4.6 | 2,492 | 6194/10.59A | 2.0 | 0.001 | 0.6 | 146 | 6317/11.87 | 1.0 | 0.001 | 0.2 | 140 | 6291/2.123 | 1.3 | 0.002 | 0.3 | 623 |
| 6122/2.22 | 0.9 | 0.019 | 2.8 | 4,195 | 6138/4.39A | Grab | 0.002 | 0.8 | 2,035 | 6195/10.59B | 1.9 | 0.010 | 0.8 | 192 | 6318/11.88 | 1.0 | 0.001 | 0.1 | 40 | 6292/2.124 | 1.15 | 0.003 | 0.7 | 2,336 |
| 6123/2.23A | 1.4 | 0.526 | 30.7 | 16,181 | 6139/4.39B | Grab | 0.018 | 2.3 | 4,288 | 6196/10.60A | 2.0 | 0.001 | 1.7 | 1,764 | 6325/11.89 | 1.5 | 0.001 | 0.1 | 16 | 6293/2.125 | 1.2 | 0.002 | 0.5 | 1,497 |
| 6123/2.23B | 1.7 | 0.219 | 10.0 | 8,752 | 6140/4.39C | Grab | 0.002 | 0.6 | 177 | 6197/10.60B | 2.05 | 0.002 | 1.5 | 336 | 6326/11.90 | 1.2 | 0.001 | 0.1 | 16 | 6294/2.126 | 2.4 | 0.003 | 0.1 | 1,105 |
| 6124/3.24 | 0.7 | 0.071 | 0.3 | 225 | 6141/4.40A | 2.3 | 0.002 | 1.3 | 1,213 | 6198/10.60C | 1.95 | 0.006 | 2.1 | 1,007 | 6327/11.91 | 1.2 | 0.003 | 0.3 | 995 | 6295/2.127 | 1.6 | 0.022 | 2.8 | 2,297 |
| 6125/4.41C | 2.5 | 0.017 | 1.3 | 1,591 | 6142/4.40B | 2.0 | 0.001 | 1.0 | 1,292 | 6199/10.61A | 2.0 | 0.001 | 1.0 | 92 | 6328/11.92 | 1.8 | 0.001 | 0.3 | 570 | 6296/2.128 | 1.5 | 0.003 | 0.3 | 576 |
| 6126/4.42A | 2.2 | 0.005 | 0.1 | 230 | 6143/4.41A | 2.8 | 0.001 | 0.5 | 27 | 6200/10.61B | 1.7 | 0.001 | 0.2 | 522 | 6330/11.94 | 1.8 | 0.001 | 0.1 | 149 | 6297/2.129 | 1.5 | 0.003 | 0.3 | 445 |
| 6127/4.42B | 2.25 | 0.001 | 0.3 | 21 | 6144/4.41B | 2.0 | 0.001 | 0.2 | 1,642 | 6201/10.61C | 1.7 | 0.001 | 0.2 | 522 | 6331/12.95 | 1.3 | 0.009 | 0.1 | 124 | 6298/2.130 | 1.2 | 0.001 | 0.1 | 63 |
| 6128/4.43A | 2.4 | 0.001 | 0.5 | 43 | 6145/4.42A | 2.7 | 0.001 | 0.5 | 43 | 6202/10.62 | 2.7 | 0.001 | 0.1 | 485 | 6332/12.96 | 2.5 | 0.002 | 0.2 | 203 | 6299/2.131 | 1.2 | 0.001 | | |



**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

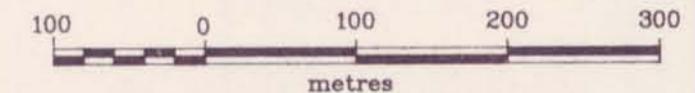
16,749

LEGEND



8884, 172
Cu ppm, Au ppb

Scale 1:5000



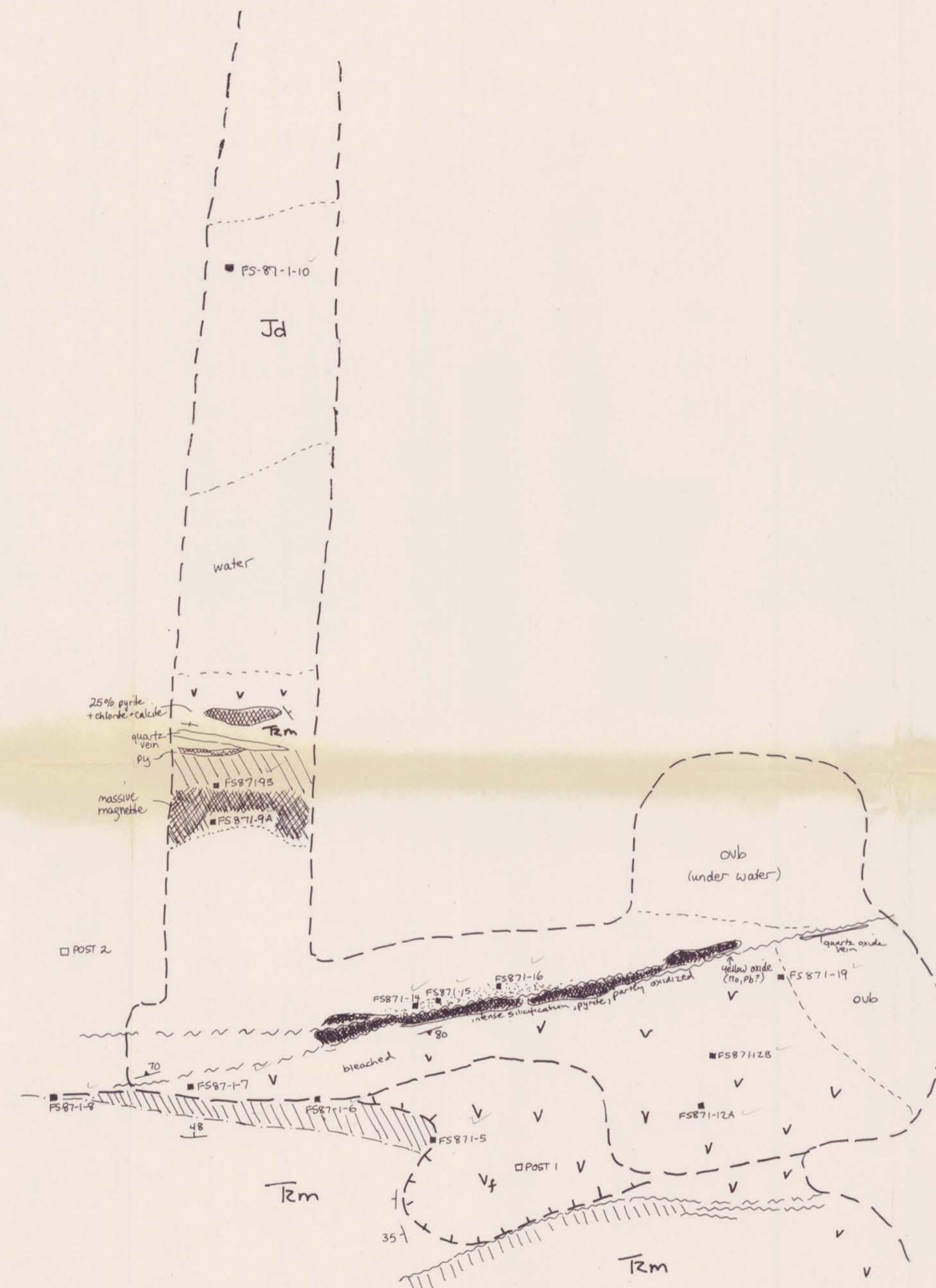
VANANDA GOLD LTD.

TEXADA ISLAND PROPERTY
NANAIMO, M.D., B.C.

GEOCHEMICAL SURVEY
COPPER & GOLD

| Originator | Drawn | Date | PLAN No. | FIGURE |
|------------|----------|---------|-------------|--------|
| Original | Geo-Comp | FEB '88 | | |
| Revision | | | N.T.S. | |
| Revision | | | 92F/10E,15E | 7 |

MINEQUEST EXPLORATION ASSOCIATES LTD.



LEGEND

Geological Formations

| | | |
|-------|---|--|
| [Jd] | diorite (Jurassic) | diorite, gabbro; coarse to fine grained, magnetic, locally altered to pyrite, epidote |
| [Trm] | marble (Triassic Marble Bay Formation) | white marble, coarse to fine crystalline, grey and laminated in shear zones |
| [V/V] | mafic volcanics (Triassic Texada Formation) | dark green fine grained to ophiitic flows or hypabyssal intrusions, 1-5% pyrite, locally magnetic V _f : aquogene tuff; lapilli sized fragments |

Alteration

| | | |
|------------------|--------------|--|
| [diagonal lines] | garnet skarn | Includes garnet-pyroxene and garnet-pyroxene-epidote skarn |
| [cross-hatch] | silification | 2-20% pyrite, includes quartz veins |
| [wavy lines] | mag py cp ox | massive magnetite, pyrite, chalcopyrite; limonite boxwork |

Symbols

| | |
|-------------------|--|
| — — — | geological contact; observed, inferred |
| ~~~~~ | fault; observed, inferred |
| ○○○ | outcrop |
| x x | suboutcrop |
| T T | trench |
| FS-87-5 | road |
| Y Y ₆₈ | bedding, fracture, mineralized fracture dip in degrees |
| oub | overburden |
| mag | magnetite |
| py | pyrite |
| po | pyrrhotite |
| sp | sphalerite |
| cp | chalcopyrite |
| mo | molybdenite |
| mal | malachite |
| az | azurite |
| ox | iron oxides |

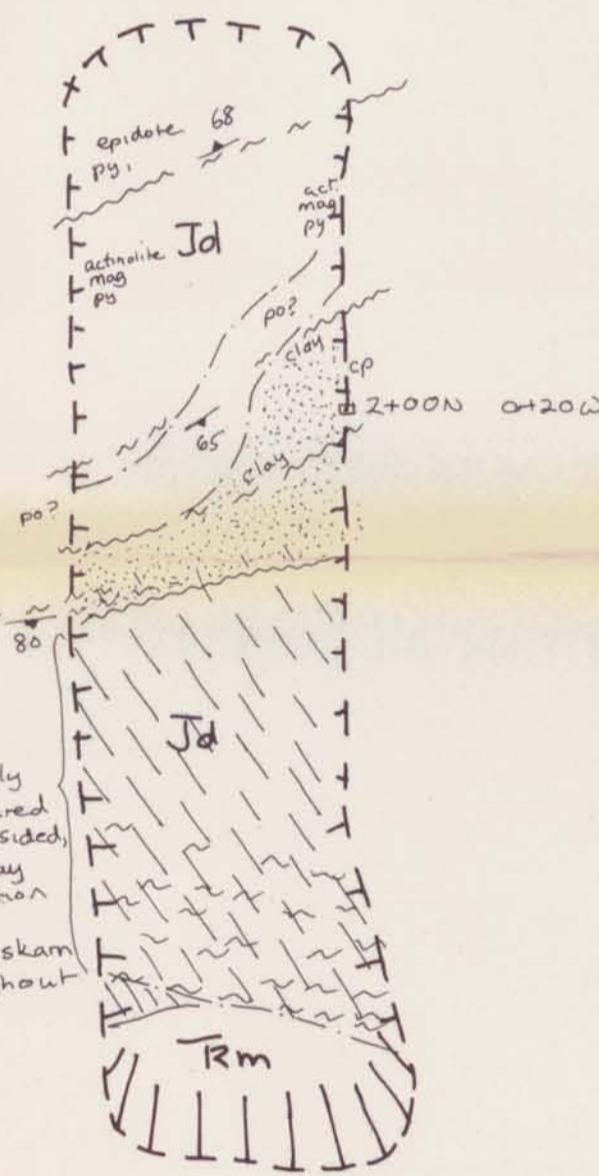
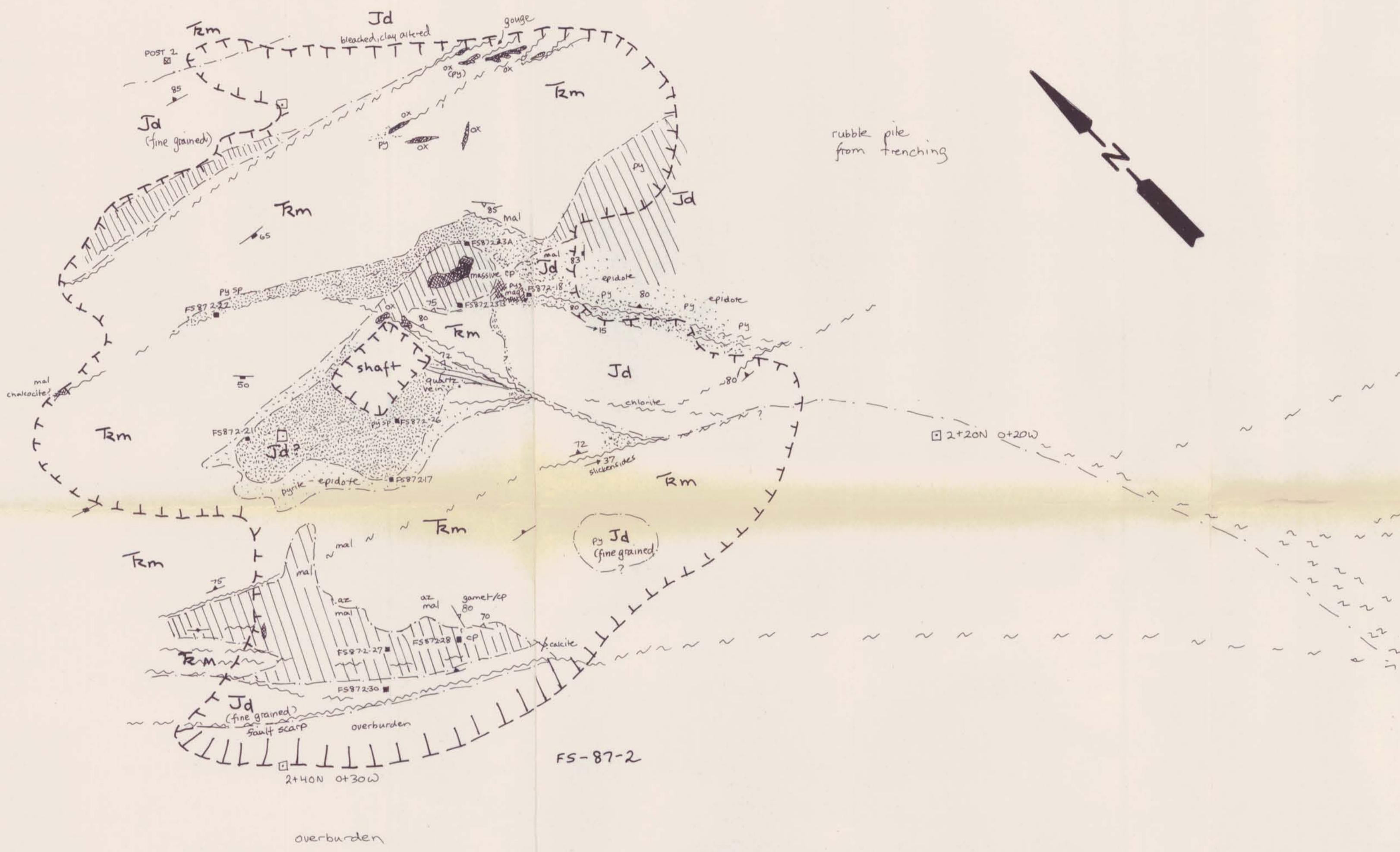
GEOLOGICAL BRANCH ASSESSMENT REPORT

16,749

10962-E 107

GEOLOGY FS. 87-1

| | | |
|----------------------------|-------------|----------------|
| SCALE: 1:100 | APPROVED BY | DRAWN BY |
| DATE: 2-88 | | SC |
| FLORENCE SECURITY PROPERTY | | DRAWING NUMBER |



GEOLOGICAL BRANCH ASSESSMENT REPORT

16,749

LEGEND

Geological Formations

- [Jd] diorite (Jurassic) diorite, gabbro: coarse to fine grained, magnetic, locally altered to pyrite, epidote
- [Trm] marble (Triassic Marble Bay Formation) white marble, coarse to fine crystalline, grey and laminated in shear zones
- [Vv] mafic volcanics (Triassic Texada Formation) dark green fine grained to ophiitic flows or hypabyssal intrusions; 5% pyrite, locally magnetic. V: aquogene tuff; lapilli sized fragments

Alteration

- [diagonal lines] garnet skarn includes garnet-pyroxene and garnet-pyroxene-epidote skarn
- [cross-hatch] silicification 2-20% pyrite, includes quartz veins
- [wavy line] massive magnetite, pyrite, chalcopyrite; limonite boxwork

0 1 2 3
metres

Symbols

- geological contact ; observed, inferred
- ~~~ fault ; observed, inferred
- outcrop
- × suboutcrop
- trench
- FS-87-5 road
- bedding, fracture, mineralized fracture dip in degrees
- ovb overburden
- mag magnetite sp sphalerite mal malachite
- py pyrite cp chalcopyrite az azurite
- po pyrrhotite mo molybdenite ox iron oxides

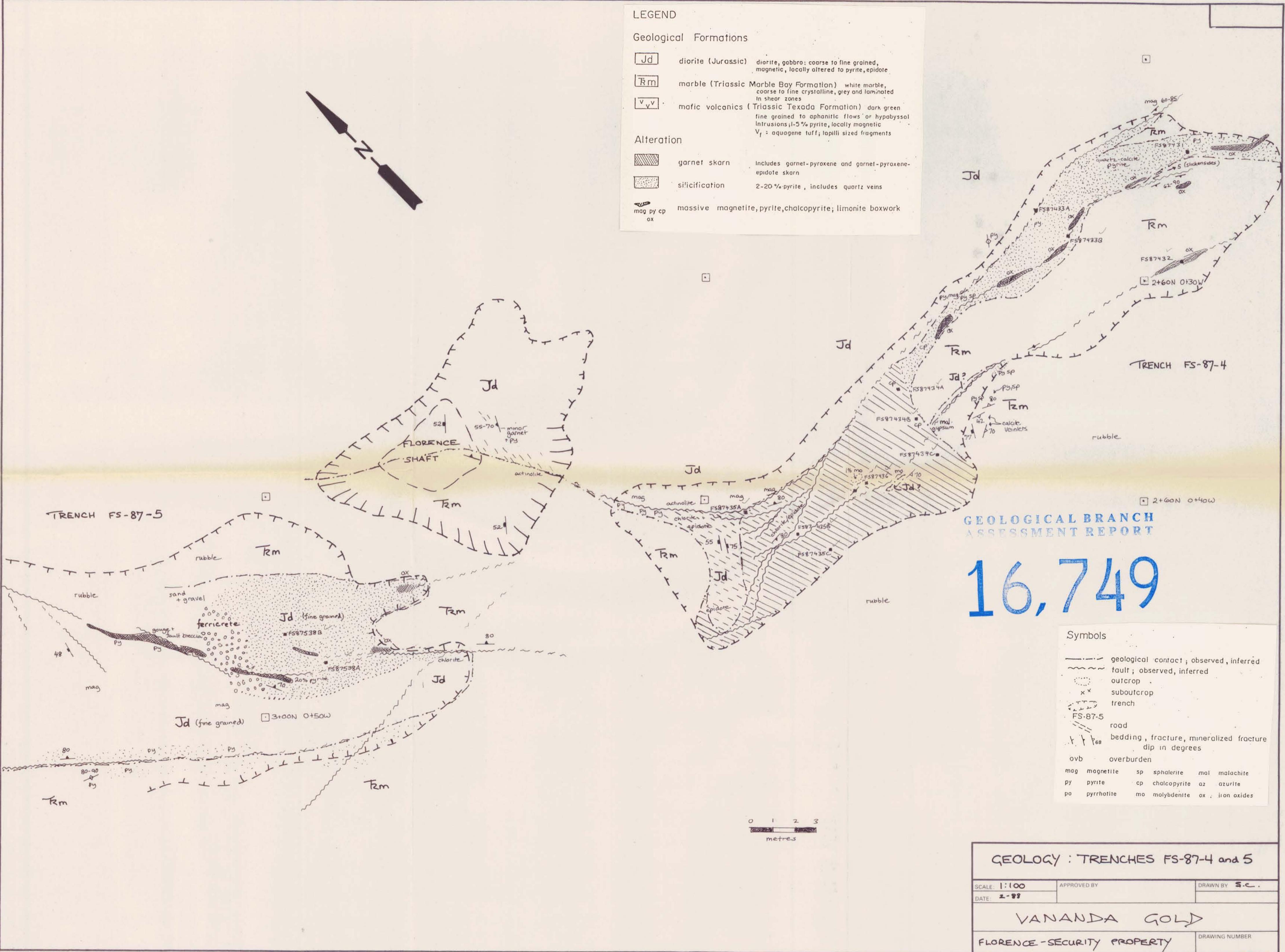
GEOLOGY : TRENCH 87-FS2

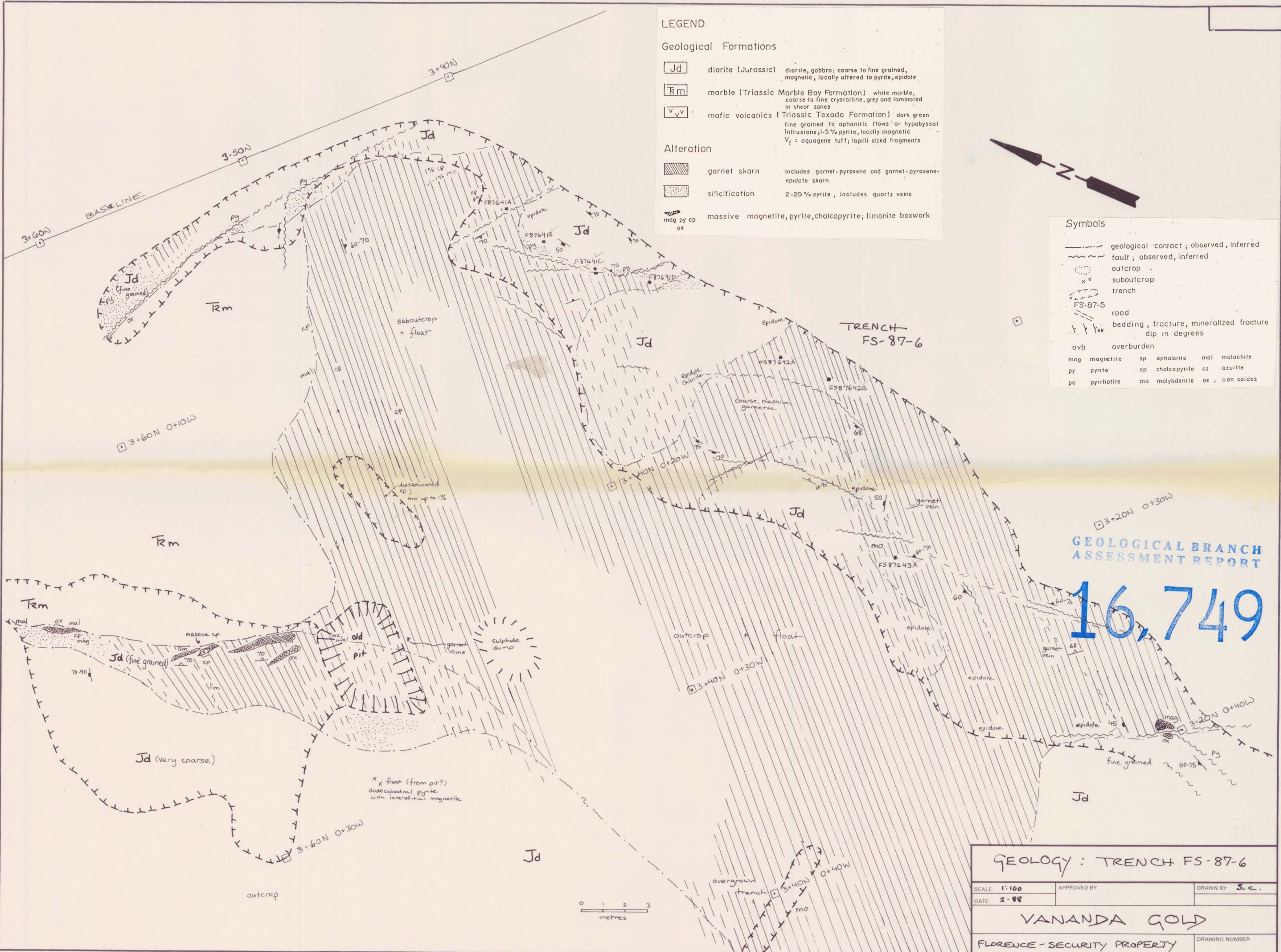
| | |
|--------------|-------------|
| SCALE: 1:100 | APPROVED BY |
|--------------|-------------|

| | |
|------------|---------------|
| DATE: 2-88 | DRAWN BY S.C. |
|------------|---------------|

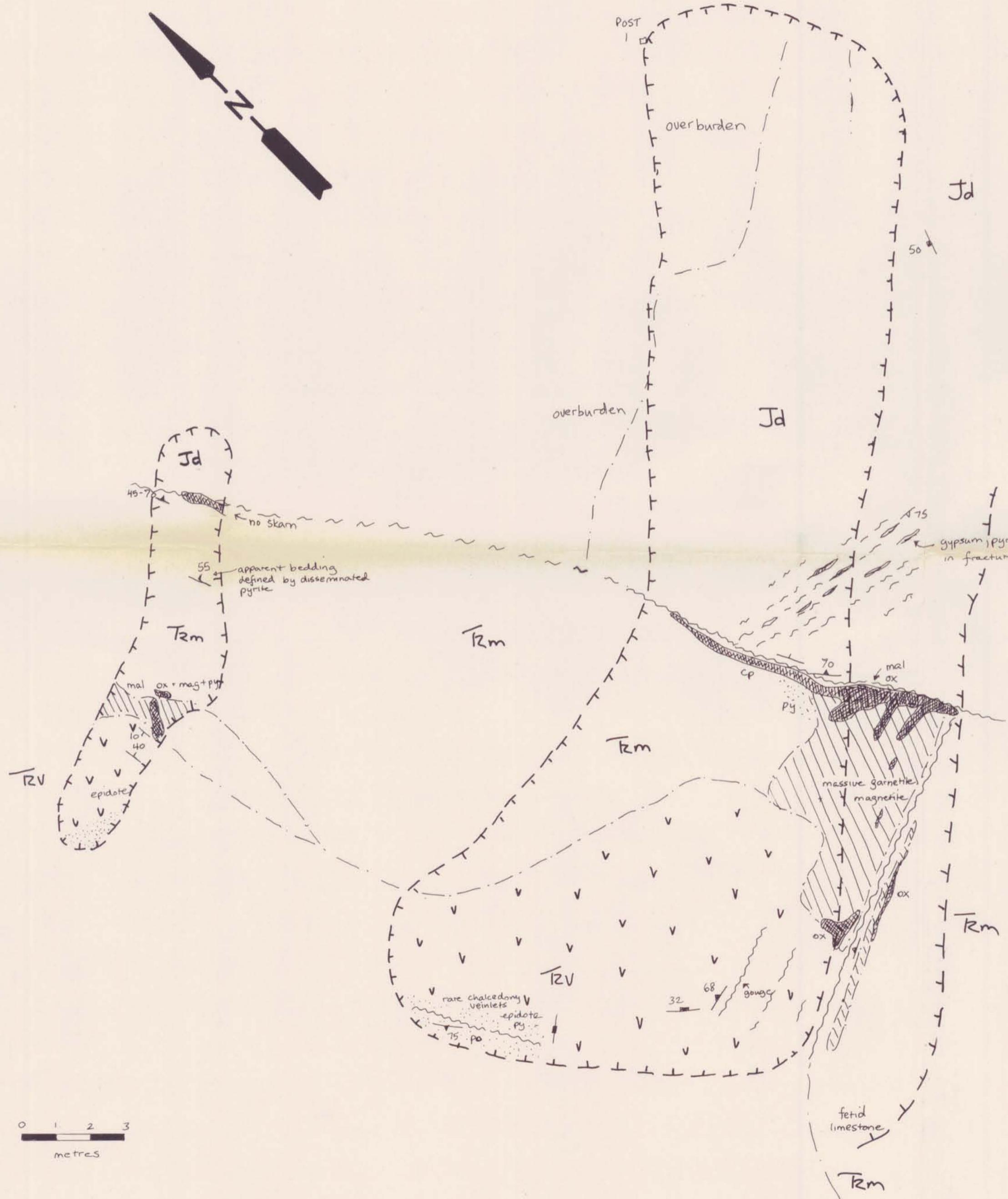
VANANDA GOLD

FLORENCE SECURITY PROPERTY DRAWING NUMBER





4+60N 0+40W
(nearest standing post)



LEGEND

Geological Formations

| | | |
|----|---|--|
| Jd | diorite (Jurassic) | diorite, gabbro; coarse to fine grained, magnetic, locally altered to pyrite, epidote |
| Tm | marble (Triassic Marble Bay Formation) | white marble, coarse to fine crystalline, grey and laminated in shear zones |
| VV | mafic volcanics (Triassic Texada Formation) | dark green fine grained to ophiitic flows or hypabyssal Intrusions; 1-5% pyrite, locally magnetic Vf = aquagene tuff; lapilli sized fragments |

Alteration

| | | |
|--|----------------|--|
| | garnet skarn | Includes garnet-pyroxene and garnet-pyroxene-epidote skarn |
| | silicification | 2-20% pyrite, includes quartz veins |
| | mag py cp ox | massive magnetite, pyrite, chalcopyrite; limonite boxwork |

GEOLOGICAL BRANCH ASSESSMENT REPORT

16,749

TRENCH FS-87-8

Symbols

| | |
|-----|--|
| | geological contact; observed, inferred |
| | fault; observed, inferred |
| | outcrop |
| | suboutcrop |
| | trench |
| | FS-87-5 |
| | road |
| | dip in degrees |
| | overburden |
| mag | magnetite |
| py | pyrite |
| po | pyrrhotite |
| sp | sphalerite |
| mo | molybdenite |
| mal | malachite |
| oz | azurite |
| ox | iron oxides |

GEOLOGY TRENCH FS-87-8

| | | |
|------------------------------|-------------|---------------|
| SCALE: 1:100 | APPROVED BY | DRAWN BY S.C. |
| DATE: 2-88 | | |
| VANANDA GOLD | | |
| FLORENCE - SECURITY PROPERTY | | |

