10963 - M3

EQUITY SILVER MINES LIMITED

1

PART 1 OF 3

16770

VOLUME 1 OF 3

FAME GRANT REPORT

FOR

EQUITY SILVER MINES LIMITED

1987 MINESITE EXPLORATION PROGRAMME

ID No. 10963-M3

OMINECA MINING DIVISION

NTS 93 L/1

LATITUDE 54 10' N

LONGITUDE 126 15' W

WORK BY: EQUITY SILVER MINES LIMITED

REPORT BY: R. B. PEASE

FEBRUARY 1988

TABLE OF CONTENTS

FORWARD

In the spring of 1986, the British Columbia government announced a programme, Exploration British Columbia - Financial Assistance for Mineral Exploration (FAME), to promote private sector mineral exploration. One component of the programme, Accelerated Mine Exploration, was to provide grants to mining companies covering up to one-third of eligible exploration expenses at developed mines for the purpose of discovering additional economic reserves. In the spring of 1987 the government announced the programme would be continued in 1987, and shortly afterwards Equity Silver Mines Limited submitted an application for assistance to supplement our 1987 minesite exploration programme.

On July 17, 1987 the Honourable Jack Davis, Minister of Energy, Mines and Petroleum Resources, informed Equity that under the FAME programme, a grant of $ 50,000 had been awarded for the 1987 minesite exploration programme. At the completion of the programme, the grant payment will be pending a successful review of a financial statement and technical data submitted in the format of an Assessment Report by February 28, 1988.

This report has been prepared to present the technical data from Equity's programme.

Respectively Submitted
EQUITY SILVER MINES LIMITED

Robert Pease, B. Sc.
Exploration Geologist

Distribution: Exploration File
B. C. Government (2)

INTRODUCTION

(i) Location and Access

The Equity Silver minesite is located 40 km southeast of the town of Houston, British Columbia (see Figure 1), approximately 575 km by air north-northeast of Vancouver. The town of Houston is serviced by the Canadian National Railway and British Columbia Highway No. 16. Daily jet air service to Vancouver is available from Smithers, a one hour drive northwest of Houston. The minesite lies in the gentle, and occasionally steep, hills of the Nechako Plateau physiographic region. Access is gained to the property by an all-weather gravel road from Houston (see Figures 2 and 3). Access to the drillsites discussed in this report is via numerous minesite roads and recently constructed connecting 4 x 4 trails (see Figure 4).

(ii) Claim Ownership and Status

The Equity minesite property consists of Certified Mining Lease No. 1 and Mining Lease No. 6 surrounded by a block of 289 two-post mineral claims, 7 fractional claims, and 3 modified grid claims (43 units). All of these claims and leases are wholly owned by Equity Silver Mines Limited and are not subject to any vendor agreements. All of the work programme was conducted on these claims and leases. Also contained within the minesite claim block are 19 two-post claims and one fraction, jointly held with Teck Corporation and Pioneer Metals Corporation.

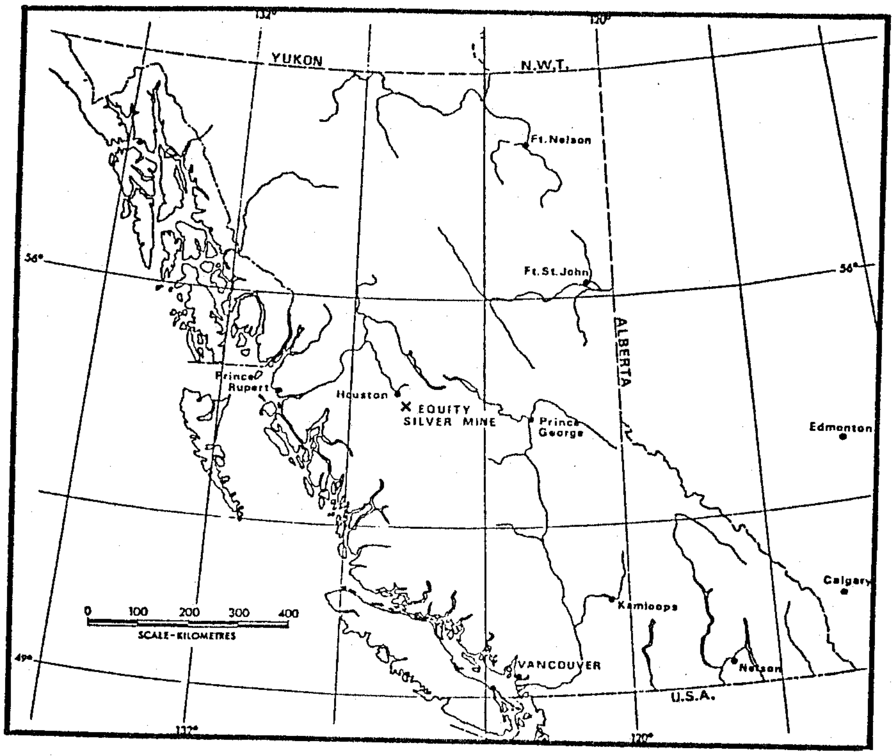


FIGURE 1 - MINESITE LOCATION

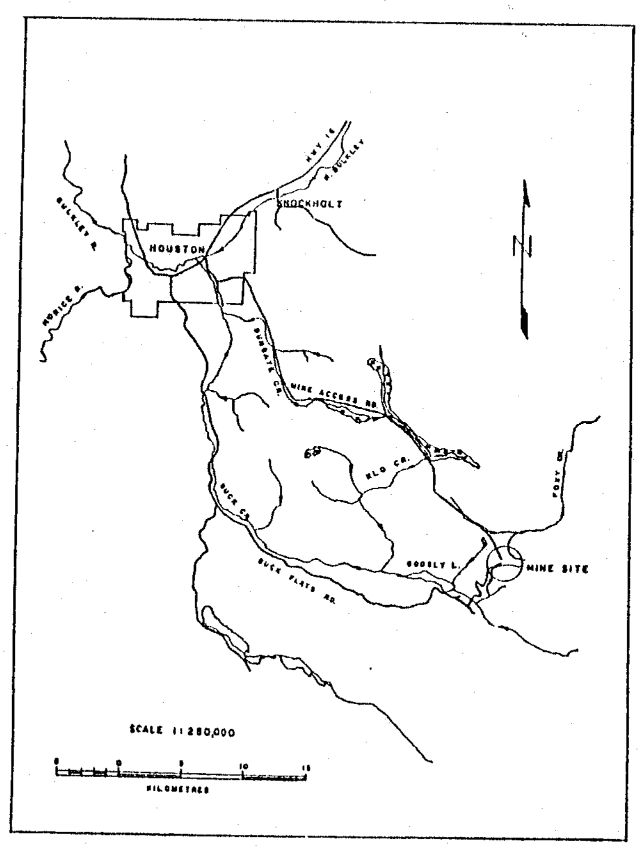


FIGURE 2 - MINESITE ACCESS

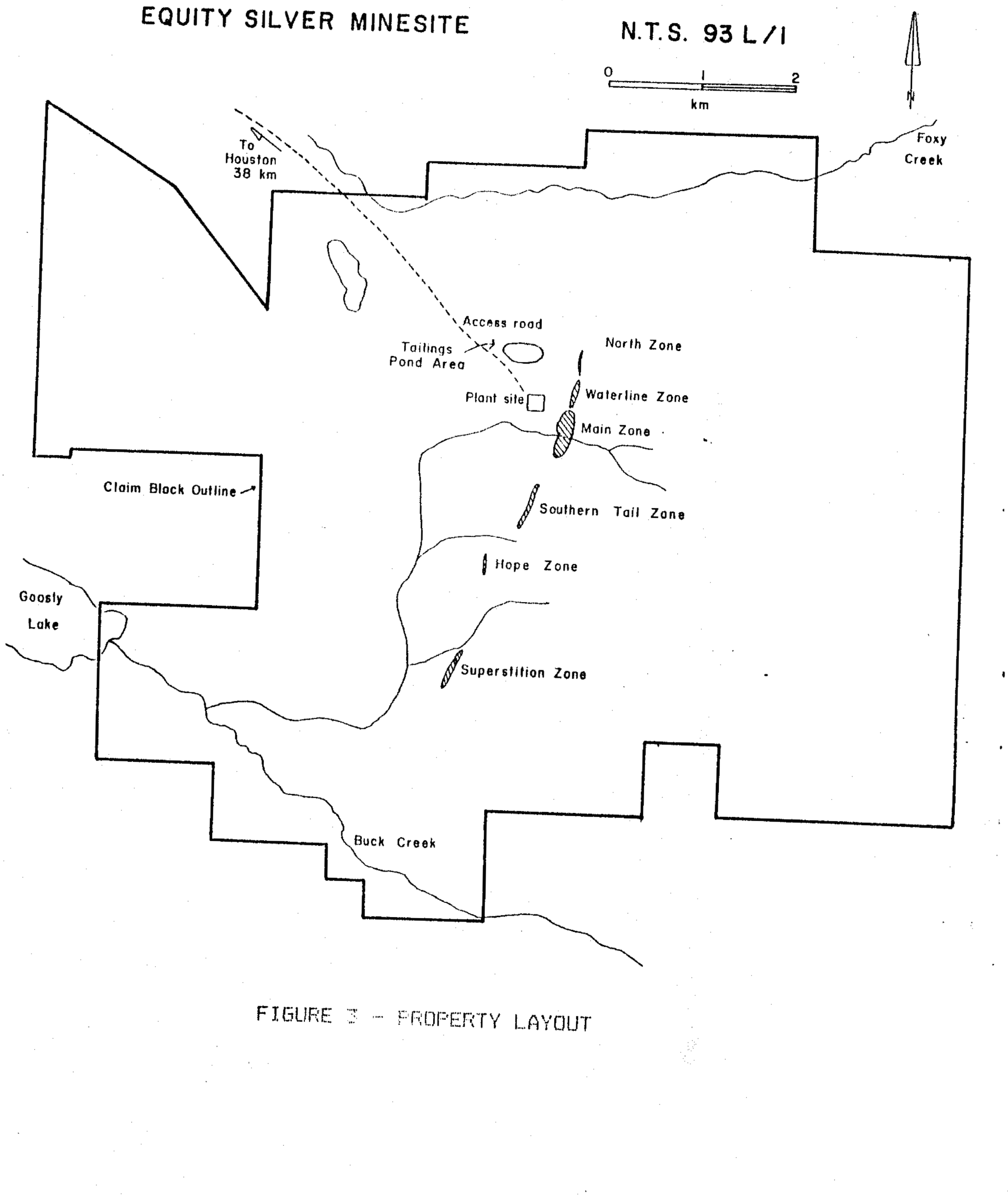


FIGURE 3 - PROPERTY LAYOUT

The company has been continuously operating a 5 500 tpd open pit mining and milling complex at this site since mid 1980. Production was increased to 10 000 tpd in mid 1986. Three ore deposits are known to occur on Certified Mining Lease No. 1. The Southern Tail deposit has been mined out to the economic limit of an open pit, however exploration is continuing on the zone to depth (Southern Tail U/G zone). The Main Zone deposit is currently being mined by an open pit, and the Waterline deposit has yet to be developed. Proven ore reserves, as of January 1988, were approximately 14.7 million tonnes at a grade of 0.26 % copper, 87 g/t silver, and 1.08 g/t gold, based on a 70 g/t silver equivalent* cut-off.

(iii) Purpose

Sixty-two NQ size diamond drillholes, totalling 13,014.3 metres, were drilled to test possible mineralized structures. These holes were spread over six different zones or areas (see Figures 3 and 4). Most of the drilling was confined to the Main, North, and Southern Tail U/G zones.

The Main zone drilling was designed to test possible deeper extensions of the ore zone, as holes were drilled to intersect the mineralized structure approximately 50 to 100 metres down-dip from the deepest previous intersection. The North zone drilling was intended to better delineate the zone by fill-in holes, as well as further explore the zone to depth and to the north. The Southern Tail U/G drilling was designed to explore to depth a relatively narrow, north plunging, high grade mineralized structure.

* g/t silver equivalent = (g/t Ag) + (% Cu X 77) + (g/t Au X 47)

SUMMARY

Deep drilling in the Main zone confirmed the continuation of the mineralized structure to depth, but grades are too low grade to consider deepening designed pit or underground mining.

Drilling in the Southern Tail U/G zone expanded the zone to depth and to the north. Preliminary underground mining feasibility is pending.

Drilling in the North zone expanded and further delineated the reserves. Open pit mining is not feasible, underground methods are being considered.

Drilling in the Waterline zone further delineated the structure, with little net effect on the mining reserve.

Drilling in the Hope zone extended the structure to the north, but low grade, narrow width, and depth of zone are prohibitive to further exploration.

Drilling in the Zest area failed to locate any significant mineralization.

The total expenditures directly related to the programme approached $ 741,000. The FAME grant, if received pending acceptance of this report, will account for $ 50,000 or 6.7 % of the total.

RECOMMENDATIONS

The following are recommendations for future Equity minesite exploration programmes.

1. Diamond drilling programmes are required to test the North, Waterline U/G, and Southern Tail U/G zones to depth.

2. Feasibility studies on underground mining of the North/Waterline U/G and Southern Tail U/G zones are required.

3. No further testing of the Main zone to depth is warrented.

4. No further exploration of the Hope zone or Zest area is warrented.

5. No further delineation of the open pit portion of the Waterline zone is required.

PROPERTY DESCRIPTION

(i) Geology

The geology of the Equity Silver property is briefly described below and illustrated on Figure 5. The reader is referenced to Cyr, et al. (1984) for a more detailed description.

The deposits occur in a homoclinal Upper Jurassic to Cretaceous inlier consisting of sedimentry, pyroclastic, and volcanic rocks flanked by intrusions and surrounded by younger, unconformable Tertiary andesitic to basaltic flows and flow breccias. Four stratigraphic conformable subdivisions, termed the Goosly Sequence, are recognized in the inlier and consist of a basal conglomerate and argillite (clastic division); intercalated sub-aerial tuffs and breccias (pyroclastic division); interbedded volcanic conglomerate, sandstone, and bedded tuff (sedimentry-volcanic division); and andesite and dacite flows (volcanic flow division). The Goosly sequence has an overall strike of 015 and dips generally to the west.

A quartz monzonite stock (58 m.y.) on the west, and a gabbro-monzonite complex (49 m.y.) to the east, intrude the Goosly sequence. Post-mineral andesite and quartz latite dykes (49 m.y.) crosscut the Goosly sequence and the gabbro-monzonite complex.

(ii) Mineralization

Economically significant Cu-Ag-Au mineralization (mineable by open pit) occurs in two distinct zones designated the Main and Waterline orebodies. The Main zone is currently being mined, and development of the Waterline pit is scheduled for early 1988. Cu-Ag-Au mineralization of undetermined economic significance occurs in the

Southern Tail U/G, Superstition, Hope, and North zones (see Figure 3). Of these, the Southern Tail U/G and North zones are the farthest advanced and the feasibility of underground mining of these zones is currently under study.

Pyrite is the most abundant metallic mineral throughout the Goosly sequence regionally, and within the zones of Cu-Ag-Au mineralization in particular. The principal silver mineral is tetrahedrite with minor values contributed by a variety of argentiferous minerals. Chalcopyrite is the principal copper mineral and a smaller but significant portion is in tetrahedrite.

The ore minerals are generally restricted to tabular zones subconcordant to host rock stratigraphy. They occur as disseminations, veins, fracture fillings, and locally as massive pods and matrix material in breccia zones. The primary ore control is structural, since "economic" sulphides tend to be best concentrated in zones of intense fracturing (microveins, stringers) and brecciation.

It is believed the Cu-Ag-Au mineralization is epigenetic in origin. Intrusive activity resulted in the introduction of hydrothermal metal-rich solutions into the pyroclastic division of the Goosly sequence. Sulphides introduced into the more competent and permeable ash and lapilli tuffs of the Main, Waterline, and North zones formed as stringers and disseminations which grade randomly into zones of massive sulphide. In the Southern Tail, Superstition, and Hope zones, sulphides formed as veins, fracture fillings, and breccia zones in the brittle, less permeable fine grained dust tuff. Emplacement of postmineral dykes into all types of sulphide-rich pyroclastic rocks resulted in remobilization and concentration of sulphides adjacent intrusive contacts. Remobilization, concentration, and contact metamorphism of sulphides occurred in the Main and Waterline zones at the contact with the postmineral gabbro-monzonite complex.

(iii) Alteration

Alteration assemblages in the Goosly sequence are characterized by minerals rich in alumina, boron, and phosphorous. The distribution of various alteration zones is illustrated on Figure 6. Four types of alteration are recognized and briefly described below. The reader is referenced to Wojdak and Sinclair (1984) for a more detailed discussion.

1. Aluminous alteration is characterized by a suite of aluminous minerals including analusite, corrundum, pyrophyllite, and scorzalite. These alteration zones show a systematic spatial relationship to areas of mineral deposits.

2. Boron-bearing minerals consisting of tourmaline and dumortierite occur within the ore zones and in the hangingwall section of the Goosly sequence.

3. Phosphorous-bearing minerals including scorzalite, apatite, augelite, and svanbergite occur in the hangingwall zone, immediately above and intimately associated with sulphide minerals - particularly in the Main and Waterline zones.

4. Phyllic alteration is characterized by weak to pervasive sericite-quartz replacement. It appears to envelope zones of intense fracturing, with or without chalcopyrite/tetrahedrite occurences, particularly in Unit 2 dust tuffs.

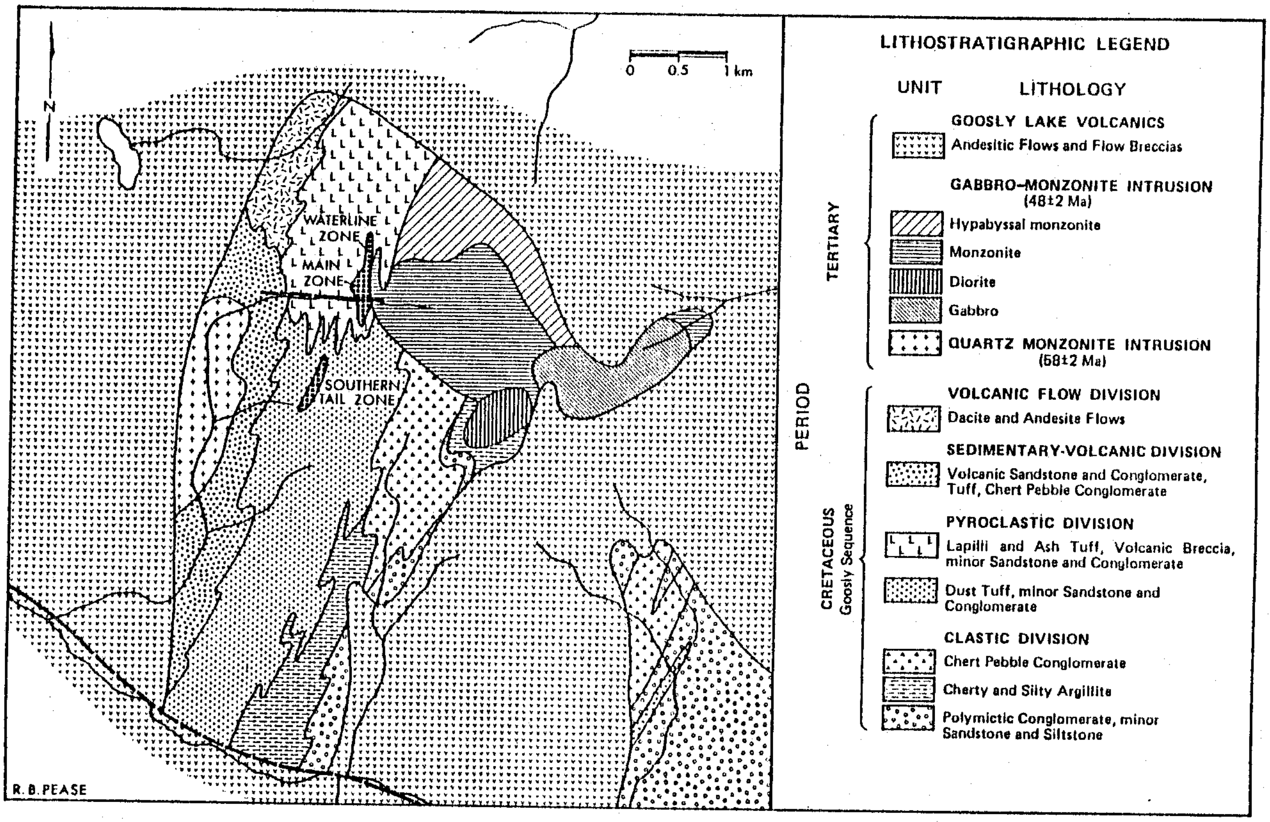


FIGURE 5 - PROPERTY GEOLOGY

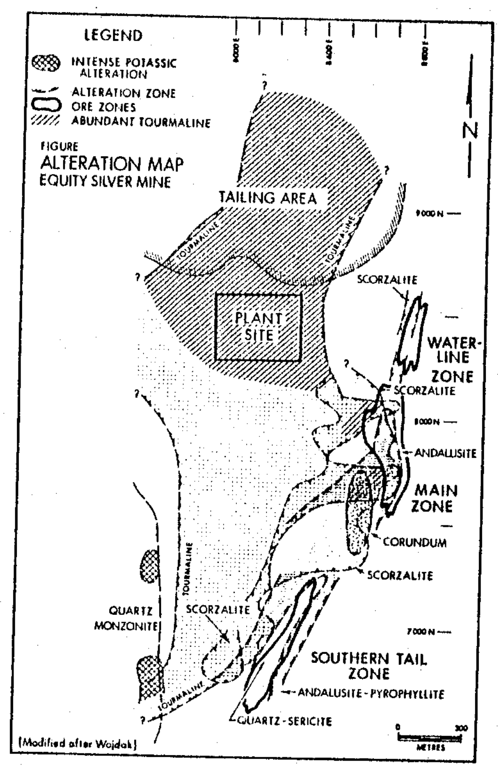


FIGURE 6 - PROPERTY ALTERATION

DRILLING PROGRAMME

The programme consisted of 13,014.3 m of NQ wireline diamond drilling spread over sixty-two (62) holes in six different zones or areas. The collar locations and surface projections of the drillholes are shown on Figure 4.

The drill setup pads and access roads were constructed prior to drill mobilization by a contracted D8 tractor. The drilling commenced on April 27 with drillhole number X87CH310, and was completed on October 21 with drillhole number X87CH371. Drilling was suspended for most of August and September. The drilling contractor was J. T. Thomas Diamond Drilling of Smithers, B. C. A skid-mounted Acker hydraulic wireline drill rig was utilized, and the contractor supplied a tractor to move and assist the drill. An Eastman single shot compass/inclinometer/camera device was used to perform a down-the-hole survey after hole completion.

The core was transported to the logging facilities at the minesite immediately following hole completion. The core logging was divided between six people through the programme; the author (24%), Mr. Darin Labrenz (45%), Mr. Daryl Hanson (12%), Mr. Jim Cyr (2%), Mr. Steve Beneteau (8%), and Mr. Gerry Gagnier (9%). Mr. Labrenz, a geologist temporarily employed by Equity, has REVELANT ? prevalent academic training, holding a B.Sc. degree in geology. Mr. Hanson, a geologist temporarily employed by Equity, has prevalent academic and practical training, holding a B.Sc. degree in geology and having over ten years experience in mineral exploration. Mr. Cyr, Equity's mine geologist, has prevalent academic and practical training, holding a B. Sc. degree in geology and having over ten years experience in mine geology. Mr. Beneteau and Mr. Gagnier, Carleton University geology students temporarily employed by Equity, logged core under the supervision of the author or Mr. Hanson.

Two logging systems were used in the programme. For the holes drilled in the Waterline and Main zones which were logged by Mr. Cyr, a handwritten graphic logging form which he prefers was used. For the balance of the programme, a coded core logging system was utilized mainly to improve the measure of objectivity, consistency, measureability, and readability as compared to handwritten logs. The coding system allows geologic and assay data to be entered into formatted computer data files. These files can be accessed by programs which plot sections and plans, perform statistical analyses, and assist in reserve calculations. An explanation of the logging codes is provided in Appendix I. The drillhole logs are reproduced in Appendix II.

The core was generally sampled top to bottom in approximately 3.0 metre intervals. Barren dyke intersections were generally omitted, as were occasional sections of unaltered and unmineralized core. Sampling was done by a hand operated core splitter. One half was placed in plastic sample bags and delivered to Equity's minesite laboratory for assay, and the other half was returned to the core box for permanent storage. The split core is stored in the facilities at the minesite.

The core samples were assayed for the metals Cu, Ag, Au, Sb, As, Fe, and Zn. In Equity's assay procedure, 1 gram of pulverized material is dissolved in 10 ml of nitric acid and 30 ml of hydrochloric acid. This solution is boiled for fifteen (15) minutes, after which 10 ml of 10 % tartaric acid is added and the sample is returned to the hot plate for five (5) minutes. The solution is allowed to cool and quantitative analysis is done on an atomic absorption machine, except for Au which is fire assayed first.

RESULTS

(i) Main Zone

The Main zone is approximately 700 metres long, up to 90 metres wide, and open to depth on several sections. The zone has an overall orientation of 015 degress and dips 65 degrees to the west. At a 70 g/t silver equivalent cut-off, the grade averages 0.26 % Cu, 94 g/t Ag, and 1.12 g/t Au.

The mineralization is hosted by mainly Unit 2 ash and lapilli tuffs. Several post-mineral dykes cross-cut the orebody. Pyrite, chalcopyrite, and tetrahedrite are the most common sulphides with accessory pyrrhotite, arsenopyrite, sphalerite and galena. These minerals occur mainly as relatively fine-grained disseminations which can locally grade into patches of massive sulphide. The sulphides also occur in irregular microveins and veins. Gold is believed to occur mainly as very fine blebs on tetrahedrite grain boundaries. Pyyrhotite is generally confined within a 70 metre wide zone around the contact with the gabbro-monzonite complex, and is believed to be derived from the conversion of pyrite by contact metamorphism. Magnetite is commonly disseminated throughout the ore zone.

Main zone alteration can be classified as advanced argillic. The zone is enveloped by a varying intensity of chlorite/pyrite lining microfractures and in disseminations. Spatially associated with the ore zone is a suite of aluminous minerals including andalusite, corundum, pyrophyllite, and scorzalite. Ore zones can also be apparently silicified.

Thirteen holes, totalling 4241.4 metres, were drilled in the Main zone. The targets were intersections 50 to 100 metres down-dip of existing drillhole intercepts, generally spread along the strike length of the zone. Prior to the drilling, it was realized that even bonanza results would not justify deepening the designed open pit, but it was hoped that reserves for possible underground mining would be indicated.

The results were discouraging as only relatively low grade intersections were obtained over significant widths (see Table 1). These grades are well below what could be considered for underground mining. The expected rock types, dominantly ash/lapilli tuffs with some dust tuff and minor volcanoclastics, were intersected. All of the holes expect one were anchored into the gabbro complex. The alteration in the mineralized zones was relatively strong as the core was generally silicified and contained scorzalite and magnetite. Chalcopyrite and sphalerite were commonly noted in these intervals. The best intersections were found in the holes toward the southern end of the zone. However, even these are considered to be too low grade for underground mining and no further drilling is anticipated.

(ii) Southern Tail U/G Zone

The Southern Tail U/G zone refers to a relatively high grade mineralized structure below the bottom of the mined-out Southern Tail pit, although it really could be considered part of the same orebody. The U/G zone is approximately 400 metres long, 90 metres wide, and averages about 10 metres thick. It dips 45 degrees to the west and plunges at 35 degrees to the north. The zone is open to depth.

Table 1. Significant Main Zone Intersections

Hole	From	To	Length	Intervals	% Cu	g/t Ag	g/t Au
X87CH310	106.8	122.8	16.0	6	0.11	42	0.31
	211.0	311.0	100.0	35	0.16	18	0.54
X87CH311	3.1	24.7	21.6	9	0.07	35	0.80
	102.0	164.2	62.2	23	0.07	43	1.50
	231.6	281.0	49.4	16	0.20	27	0.52
X87CH312	11.1	42.5	31.4	9	0.04	40	0.44
	94.8	154.0	59.2	21	0.10	32	0.36
	216.4	248.4	32.0	11	0.15	16	0.82
X87CH313	6.1	18.2	12.1	4	0.03	75	0.17
X87CH314	69.1	143.7	74.6	20	0.05	22	0.20
	237.2	309.2	72.0	21	0.07	19	0.35
X87CH315	123.9	141.9	18.0	6	0.04	29	1.55
	219.8	245.1	25.3	8	0.08	33	0.76
X87CH316	146.9	208.6	61.7	19	0.16	15	0.24
	222.3	291.7	69.4	21	0.13	15	0.23
X87CH346	320.1	423.9	103.8	36	0.17	27	0.37
X87CH347	167.1	213.7	46.6	17	0.04	29	0.57
	234.1	246.6	12.5	4	0.30	62	0.66
	287.3	301.0	13.7	7	0.97	92	1.19
X87CH348	3.1	68.5	65.4	22	0.12	59	0.46

The mineralization is hosted by Unit 2 dust tuff with minor ash tuff. Pyrite, chalcopyrite, and tetrahedrite occur in intensely fractured and brecciated zones immediately above a large quartz latite dyke. A broad zone of pervasive quartz-sericite alteration occurs in the hangingwall and mineralized zone. The dyke is unaltered and unmineralized. Minor mineralization is sometimes present below the dyke. The tuffs below the dyke generally display a lower grade chlorite alteration.

Thirteen holes, totalling 2875.6 metres, were drilled to test the zone to depth and to the north. The significant intersections are listed in Table 2.

Table 2. Significant Southern Tail U/G Intersections

Hole	From	To	Length	Intervals	% Cu	g/t Ag	g/t Au
X87CH320	119.2	137.7	18.5	9	0.92	97	1.02
X87CH321	146.8	165.2	18.4	10	0.50	44	0.23
X87CH322	155.6	169.0	13.4	5	0.50	237	0.29
X87CH323	192.9	197.2	4.3	2	0.11	89	1.58
X87CH324	216.6	222.2	5.6	3	0.59	13	0.26
X87CH342	185.3	196.9	11.6	5	1.31	509	6.92
	205.4	207.7	2.3	1	2.00	406	2.03
X87CH343	201.8	210.7	8.9	4	0.42	210	3.12
X87CH361	220.0	237.2	17.2	8	0.97	249	2.80
X87CH362	186.8	208.3	21.5	10	0.57	184	0.37
X87CH363	214.7	216.1	1.4	1	0.06	13	6.85
	224.1	232.4	8.3	4	0.52	14	0.59
X87CH364	190.0	196.9	6.9	3	0.65	184	3.51
	206.4	221.4	15.0	5	0.27	25	0.51
X87CH365	237.5	243.9	6.4	4	0.39	92	2.03

An inferred geological reserve of the Southern Tail U/G zone has been calculated at 924,000 tonnes at a grade of 0.93 % Cu, 266 g/t Ag, and 2.57 g/t Au at a 150 g/t silver equivalent cut-off. A preliminary feasibility study of mining the zone by underground methods is pending. Future delineation drilling will depend on the results of this study, although more drilling is recommended to test the zone further to depth.

(iii) North Zone

The North zone was discovered by diamond drilling in 1986. It has a strike length of approximately 400 metres. The zone has a vertical dip, and strikes north-south. True widths are variable from 1 to 25 metres, but the average is about 8 metres. The zone is open to depth on most sections.

The host rocks are mainly Unit 2 ash and lapilli tuff, with some tuffaceous siltstone in the northern portion. Alteration appears to be confined to, or within a few metres of, the mineralized structure. It consists of an advanced argillic suite (visible scorzalite), silicification, and some phyllic replacement. Magnetite commonly envelops the zone as well. Mineralization occurs as relatively coarse-grained chalcopyrite, sphalerite, arsenopyrite, tetrahedrite, and pyrrhotite in irregular microveins and breccia fillings which can locally grade into massive sulphide, all generally confined to a macrovein-like structure.

Twenty-six holes, totalling 4386.2 metres were drilled to further delineate the zone. The significant intersections are listed in Table 3. The expected rock types were intersected and the style of mineralization and alteration was as expected. Geologic reserves were re-calculated to 545,000 tonnes at 0.62 % Cu, 159 g/t Ag, and 4.16 g/t Au at a 130 g/t silver equivalent cut-off.

Table 3. Significant North Zone Intersections

Hole	From	To	Length	Intervals	% Cu	g/t Ag	g/t Au
X87CH325	216.8	222.9	6.1	2	0.35	52	1.67
	227.2	233.0	5.8	2	0.04	69	0.55
X87CH326	129.1	144.4	15.3	6	0.53	173	5.83
X87CH327	132.1	146.9	14.8	5	1.00	439	3.31
X87CH329	287.9	291.8	3.9	1	0.10	31	1.31
	295.9	299.2	3.3	1	0.01	107	0.06
X87CH331	224.1	226.3	2.2	1	0.74	14	0.02
X87CH333	223.4	239.4	16.0	9	0.93	291	0.98
X87CH334	158.3	180.8	22.5	10	0.15	25	1.19
X87CH335	53.2	61.4	8.2	4	0.13	25	2.25
X87CH336	9.1	13.7	4.6	2	0.25	61	0.24
X87CH349	193.0	196.8	3.8	1	0.63	49	2.83
	223.1	226.4	3.3	1	0.11	79	0.90
X87CH350	205.2	215.2	10.0	4	0.23	92	1.32
X87CH351	178.5	193.5	15.0	5	0.03	17	0.21
X87CH352	214.9	216.4	1.5	1	0.14	119	0.78
X87CH353	130.4	137.5	7.1	4	0.10	42	2.85
X87CH354	79.5	87.8	8.3	3	0.73	218	0.83
	99.1	118.0	18.9	7	1.22	230	5.55
	123.0	133.6	10.6	4	0.78	146	12.27
X87CH355	68.0	71.0	3.0	1	0.08	95	1.06
	95.8	97.5	1.7	1	0.61	520	1.97
X87CH356	45.9	56.5	10.6	3	0.02	28	0.05
X87CH366	116.7	122.1	5.4	2	0.05	45	1.85
X87CH367	48.0	50.8	2.8	1	0.08	102	1.57
	66.0	69.3	3.3	1	Tr	49	0.04
	98.8	102.5	3.7	1	0.05	58	0.40
X87CH369	31.5	33.8	2.3	1	0.29	85	1.77

The feasibility of mining the North zone by an open pit has been analyzed and rejected, due to the low grade and narrow width of the near surface mineralization and the excessive strip ratio. However, the feasibility of mining the zone along with the portion of the Waterline zone below the designed bottom of the open pit (Waterline U/G zone) by underground methods is currently underway, and preliminary results appear to be favourable. Further exploration of these zones to depth is pending the outcome of the underground study.

(iv) Waterline Zone

The style of mineralization/alteration in the Waterline zone is very similiar to the Main zone. The host rocks are mainly Unit 2 ash and lapilli tuff, with some dust tuff and volcanoclastics. Post-mineral quartz latite, andesite and trachyandesite dykes are very common.

The mineralized zone is 375 metres long and averages approximately 40 metres wide. It has a general strike of 010 degrees and dips vertically. The northern half of the zone is open to depth. The minerals chalcopyrite, pryyhotite, sphalerite, tetrahedrite, and arsenopyrite occur mainly as disseminations, which can grade into massive sulphide, and irregular microveins (stringers).

As in the Main zone, alteration can be classified as advanced argillic. Scorzalite is commonly noted close to and within the mineralized zone. Silicification of the mineralized zone and an apparent increase in magnetite are also common.

Five holes, totalling 323.4 metres, were drilled to further delineate some poorly defined areas within the designed open pit portion of the zone. The significant intersections are listed in Table

4. The rock types, alteration and mineralization intersected were consistant with what would be expected in the Waterline zone. The grade and width of the mineralized intersections were disappointing, but they had little effect on the overall mining reserve. This reserve within the Waterline open pit was re-calculated to 2.3 million tonnes at a grade of 0.33 % Cu, 89 g/t Ag, and 1.33 g/t Au at a 70 g/t silver equivalent cut-off. No further drilling in planned within the open pit portion of the Waterline zone, and mining will commence in 1988.

Table 4. Significant Waterline Zone Intersections

Hole	From	To	Length	Intervals	% Cu	g/t Ag	g/t Au
X87CH359	24.0	33.0	9.0	3	0.11	93	0.71
	39.0	47.7	8.7	3	0.02	24	0.22
X87CH370	40.9	43.5	2.6	1	0.43	49	4.13
X87CH371	103.5	110.1	6.6	2	0.22	86	1.52

(v) Hope Zone

Two holes, totalling 640.1 metres, were drilled to test the strike extension of the zone to the north. The holes intersected Unit 3 chert pebble conglomerate and sandstone, and Unit 2 dust tuff as expected. Zones of pyrite, chalcopyrite, and trace tetrahedrite mineralization in fracture fillings were intersected at the target depths within an envelope of pervasive quartz-sericite alteration. The style of mineralization most closely resembles the Southern Tail zone. Unfortunately, the first hole (X87CH339) had to be abandoned within the target zone due to caving. The significant intersections are listed in Table 5.

Table 5. Significant Hope Zone Intersections

Hole	From	To	Length	Intervals	% Cu	g/t Ag	g/t Au
X87CH339	278.1	281.3	3.2	1	0.28	141	0.40
X87CH340	315.0	330.3	15.3	6	0.07	77	0.10

The Hope zone is poorly defined. It has been traced for over 400 metres of strike length, but on 100 metre spaced drill sections. The zone appears to dip vertically and have variable widths up to 30 metres. The zone apparently occurs only below a depth of approximately 150 metres below the surface. No reserve data has been calculated due to the wide spaced nature of the drilling. Future drilling in the zone is unlikely due to the relatively low grade and the prohibitive depth of the mineralization.

(vi) Zest Area

Previous drilling in this area had intersected a wide zone (approx. 100 metres) of silicification, relatively heavy diseminated and fracture filling magnetite, and some patchy low grade Cu-Ag-Zn mineralization. Three holes, totalling 547.6 metres, were drilled to further test this zone. The holes intersected mainly Unit 2 dust and ash tuffs with again relatively high magnetite, but unfortunately, no significant mineralization was intersected except for the one interval noted in Table 6. No further drilling is planned in this area.

Table 6. Significant Zest Area Intersection

Hole	From	To	Length	Intervals	% Cu	g/t Ag	g/t Au
X87CH341	179.9	182.0	2.1	1	0.53	20	0.09

TABLE 7

STATEMENT OF EXPENDITURES

1.	Construction of Drillsites and Access Roads	
	D8 Tractor, 129 hours @ 117.50	$ 15,157.50
2.	Diamond Drilling	
	11,076.1 metres @ 44.78/m	495,995.76
	1,938.2 metres @ 51.51/m	99,836.30
	Consumables	22,547.35
	Man and Machine Hours	4,809.00
3.	Sample Assaying	
	3008 drillcore samples @ 17.50/sample	52,640.00
4.	Labour	
	R. Pease; logging and supervision	
	55 days @ 185.00/day	10,175.00
	D. Hanson; logging and supervision	
	17 days @ 165.00/day	2,805.00
	J. Cyr; logging	
	5 days @ 185.00/day	925.00
	D. Labrenz; logging and supervision	
	110 days @ 115.00/day	12,650.00
	G. Gagnier; logging, splitting	
	20 days @ 100.00/day	2,000.00
	S. Beneteau; logging, splitting	
	20 days @ 100.00/day	2,000.00
	C. Mikaelsson; splitting	
	51 days @ 90.00/day	4,590.00
	D. Makowichuk; splitting	
	19 days @ 90.00/day	1,710.00
5.	Vehicle Rental and Fuel	
	110 days @ 50.00/day	5,500.00
6.	Down-hole Survey Camera Rental	3,500.00
7.	Report Preparation	4,000.00
	TOTAL	$ 740,840.91

AUTHOR'S QUALIFICATIONS

I, Robert B. Pease, do hereby certify that:

1. I am a geologist residing at R. R. # 1, Kerr Road, Telkwa, British Columbia.

2. I am a 1981 graduate of the University of Waterloo, Waterloo, Ontario, with an Honours Bachelor of Science degree in Earth Sciences.

3. As a student, I spent some twenty (20) months employed in the mineral exploration field with several mining companies in various regions of Canada.

4. I was employed as an exploration geologist with Duval International Corporation in Vancouver from May 1981 to January 1982.

5. Since February of 1982, I have been continously employed as an exploration geologist with Equity Silver Mines Limited in Houston, British Columbia.

6. I am an Associate Member of the Geological Association of Canada, and a Member of the Canadian Institute of Mining and Metallurgy.

7. I personally supervised the work programmes as described in this report.

R. B. Pease, B.Sc.
Exploration Geologist
EQUITY SILVER MINES LIMITED

REFERENCES

Cyr, J. B.; Pease, R. B.; and Schroeter, T. G. (1984): Geology and Mineralization at Equity Silver Mine. Journal of Econ. Geol., Vol. 79, pp. 947-968.

Wojdak, P. J. and Sinclair, A. J. (1984): Equity Silver Ag-Cu-Au Deposit: Alteration and Fluid Inclusion Studies. Journal of Econ. Geol., Vol. 79, pp. 969-990.

APPENDIX I

Diamond Drillhole Logging Code Explanation

LOGGING CODE EXPLANATION

Column 1 is a key which indicates the type of data or information on each line.

- I - Identity information/data
- S - Survey data
- / - Upper tier geologic data
- L - Lower tier geologic data
- R - Free form remarks
- A - Assay and analysis data

I DATA

Each drillhole has two I lines at the start.

The first line indicates:

Col. 17 to 24 - Drillhole Name
Col. 26 to 27 - Size of Core
Col. 29 to 35 - Day/Month/Year Logged
Col. 36 to 38 - Logger's Initials
Col. 39 to 41 - Helper's Initials (if any)
Col. 42 to 45 - Drilling Contractor
Col. 46 to 50 - Month/Year Hole Drilled
Col. 51 to 53 - Drill Rig Type
Col. 63 to 68 - Grid Azimuth (0.0 if True North)

The second line indicates:

Col. 5 to 45 - Company Name
Col. 46 to 80 - Zone and type of Geocode* used.

NOTE: * Equity uses two types of Geocodes, ST and MN. The ST geocode is used when a hole is drilled south of the Main Zone, and the MN geocode is used to the north of, and including, the Main Zone. This is done to reflect the differing host rock and style of mineralization/alteration between the northern and southern sections of the property.

S DATA

The S000 line is the collar survey data. Subsequent S lines (S001, S002, etc.) are down-the-hole surveys.

Col. 5 to 10 - From (a decimal point is inferred between column 8 and 9)
Col. 11 to 16 - To (a decimal point is inferred between column 14 and 15)
Col. 17 to 18 - Units; MT (metres), FT (feet)
Col. 20 to 26 - Total Length
Col. 27 to 32 - Azimuth
Col. 33 to 38 - Dip
Col. 51 to 60 - Northing
Col. 61 to 70 - Easting
Col. 71 to 80 - Elevation

/ AND L DATA

Disregard the /SCL and LSCL lines, they are only for computer processing. Two lines are available to describe a geologic interval, the upper line (/) and the lower line (L). The /NAM line defines the mineral fields for the upper line, and the LNAM defines the lower line. These mineral fields change according to the type of Geocode (ST or MN) used.

ST Geocode - upper (/NAM) line

Col. 57, 58 MS - Muscovite (sericite)
Col. 59, 60 CL - Chlorite
Col. 61, 62 QZ - Quartz
Col. 63, 64 PY - Pyrite
Col. 65, 66 CP - Chalcopyrite
Col. 67, 68 TT - Tetrahedrite
Col. 69, 70 AS - Arsenopyrite
Col. 71, 72 PR - Pyrrhotite

- lower (LNAM) line

Col. 57, 58 CB - Carbonate
Col. 59, 60 GY - Gypsum
Col. 63, 64 MG - Magnetite
Col. 65, 66 HE - Hematite
Col. 67, 68 SL - Sphalerite
Col. 69, 70 GL - Galena
Col. 71, 72 MO - Molybdenum

MN Geocode - upper (/) line

Col. 57, 58 QZ - Quartz
Col. 59, 60 SZ - Scorzalite
Col. 61, 62 TO - Tourmaline
Col. 63 to 72 - Same as ST Geocode

- lower (L) line

Col. 57, 58 DM - Dumortierite
Col. 59, 60 CB - Carbonate
Col. 61, 62 CL - Chlorite
Col. 63 to 72 - Same as ST Geocode

Upper (/) Geologic Data

Col. 5 to 10 - From (decimal inferred between 8 and 9)
Col. 11 to 16 - To (decimal inferred between 14 and 15)
Col. 17 to 20 - Recovery in Metres (decimal inferred between 18 and 19)
Col. 24 to 27 - Rock Type Code - See Rock Type Chart
Col. 28 to 29 - Typifying Mineral 1 - see Mineral Chart
Col. 30 to 31 - Typifying Mineral 2 - see Mineral Chart
Col. 35 to 36 - Texture 1 - see Texture Chart
Col. 37 to 38 - Texture 2 - see Texture Chart
Col. 47 - Essentially always a "P" which stands for Principle Geologic Interval. If "D", it stands for Ditto Interval which means all of the above interval description applies, except as noted.
Col. 49 to 50 - Structure 1 - see Structure Chart
Col. 55 to 56 - Angle to Core Axis of Structure 1
Col. 57 - Mineral Field, Mode of Occurence - see How Chart
Col. 58 - Mineral Field, Amount of Occurence - see Amount Chart
Col. 59 to 72 - Mineral Fields, same pattern continues (ie. How, Amount) as in columns 57, 58.

Lower (L) Geologic Data

Col. 17 to 20 - RQD in Metres (decimal inferred between 18 and 19)
Col. 28 to 29 - Colour Code - see Colour Chart
Col. 35 to 36 - Typifying Mineral 3 - see Mineral Chart
Col. 37 to 38 - Typifying Mineral 4 - see Mineral Chart
Col. 43 - Count of Fractures at Steep Angle to Core Axis - See Amount Chart
Col. 44 - Count of Fractures at Medium Angle to Core Axis - See Amount Chart
Col. 45 - Count of Fractures at Low Angle to Core Axis - See Amount Chart
Col. 46 - Count of Total Fractures - See Amount Chart

NOTE: Columns 43 to 46 not always used

Col. 49 to 50 - Structure 2 - see Structure Chart
Col. 55 to 56 - Angle to Core Axis of Structure 2
Col. 57 to 72 - Mineral Fields, as in upper (/) Data

R DATA

These are free form remarks written by the logger to further describe the gelogic interval. Note that Rock Type Codes (see Rock Type Charts) are often used.

A DATA

This last type of data lists the assay information for the hole. Note that remarks are also used.

The first line, A001, defines a "set" of assay data. eg. A002 would define a different set, etc. The following lines describe and list the assay data.

ALAB Col. 17 to 80 - Define Laboratory
ATYP Col. 17 to 80 - Define Type of Determination
AMTH Col. 17 to 80 - Define Analytical Method
AUMM Col. 17 to 80 - Define Assay Fields
A001 Col. 5 to 10 - From (decimal inferred between 8 and 9)
Col. 11 to 16 - To (decimal inferred between 18 and 19)
Col. 23 to 26 - Sample Number
Col. 33 to 38 - Percent Copper
Col. 39 to 44 - Grams/Tonne Silver
Col. 45 to 50 - Grams/Tonne Gold
Col. 51 to 56 - Percent Antimony
Col. 57 to 62 - Percent Arsenic
Col. 63 to 68 - Percent Iron
Col. 69 to 74 - Percent Zinc

CHARTS

1. Rock Type Chart

A four digit code is used to describe rock types. The first and second digits are common to both ST and MN Geocodes. The first digit (number) defines stratigraphic unit, and the second digit (letter) defines a lithology unique to the stratigraphic unit. In the ST Geocode, the third digit (number) defines the intensity of fracturing or brecciation, and the fourth digit (number) defines the type and intensity of alteration. In the MN Geocode, the third digit (number) defines the alteration, and the fourth digit (number) defines the mineralization.

One special code, OVBN, is used for overburden.

First Digit	Stratigraphic Unit	Second Digit	Lithology
1	Clastic Division	A	Polymictic Conglomerate
		B	Cherty or Silty Conglomerate
		C	Chert Pebble Conglomerate
		D	Quartz Sandstone
		E	Cherty Argillite
		F	Silty Argillite
2	Pyroclastic Division	A	Flow Breccia
		B	Ash Flow
		C	Dust Tuff
		D	Ash Tuff
		E	Lapilli Tuff
		F	Volcanic Breccia
		G	Volcanic Sandstone
		H	Volcanic Conglomerate
		I	Welded tuff
		J	Interbedded Dust and Ash Tuff
		K	Lahar
		L	Tuffaceous Siltsone
		M	Claystone
3	Sedimentry - Volcanic Division	A	Chert Pebble Conglomerate
		B	Quartz Sandstone
		C	Laminated Dust Tuff
		D	Volcanic Conglomerate
		E	Volcanic Sandstone
		F	Dust Tuff
		G	Ash Tuff
		H	Lapilli Tuff
		I	Volcanic Siltstone
		J	Interbedded Dust and Ash Tuff
		K	Silty Argillite
4	Volcanic Flow Division	A	Andesite Flow
		B	Dacite Flow
6	Quartz Monzonite	A	Fresh Quartz Monzonite
		B	Altered (Potassic) Quartz Monzonite

7	Gabbro-Monzonite Complex	A	Gabbro
		B	Diorite
		C	Monzonite
		D	Hypabyssal Monzonite Prophyry
		E	Gabbro - Monzonite Transition Phase
8	Property Dykes	A	Andesite
		B	Trachyandesite
		C	Quartz Latite
9	Tertiary Volcanics (Goosly Lake Fm)		
		A	Trachyandesite Flow
		B	Amygdaloidal Andesite Flow
		C	Flow Breccia
		D	Reddish-Purple Flow
		E	Massive Andesite Flow
		F	Quartz-eye Porphyry (Latite)
		G	Tuffaceous Sandstone/Siltstone

ST - Geocode

Third Digit	Intensity of Fracturing or Brecciation
0	No Fracturing
1	Weak Fracturing
2	Moderate Fracturing
3	Mod to Strong Fracturing
4	Strong Fracturing
5	Weak Brecciation
6	Weak to Mod Brecciation
7	Moderate Brecciation
8	Mod to Strong Brecciation
9	Strong Brecciation

Fourth Digit	Type and Intensity of Alteration
0	Unaltered
1	Weak Propylitic (CHL - CLAY)
2	Strong Propylitic
3	Weak Phyllic (QTZ - SER.)
4	Moderate Phyllic
5	Pervasive Phyllic
6	Advanced Argillic
7	Weak Potassic
8	Strong Potassic
9	Silicic (QTZ)

MN - Geocode

Third Digit	Alteration
0	Unaltered
1	Propylitic
2	Scorzalite Bearing/Argillic
3	Andalusite Bearing/Argillic
4	Moderate Silicification
5	Strong Silicification
6	Biotite Hornfels
7	Pyrite Porphyroblast Bearing
8	Phyllic (Quartz-Sericite)
9	Quartz - Tourmaline

Fourth Digit	Sulphide Mineralization
0	None
1	Disseminated Pyrite +/- Chalcopyrite
2	Pyrite - Magnetite Intergrowths
3	Sulphide Bearing (CP+/-PY+/-SL) Stringers
4	Sulphide Bearing (CP+/-PY) Patches
5	Massive Sulphide (CP+/-PY+/-TT+/-PO+/-SL) Replacements or Remobilized
6	Grey, "Dusty" Sulphides (fine grained mixture of sulphides and quartz)
7	Sulphides in Breccia Matrix (CP+/-PY+/-TT+/-SL)

2. Mineral Chart (ie. Mineral short-forms)

QZ	Quartz
CL	Chlorite
CY	Clay
CB	Carbonate
PY	Pyrite
MS	Muscovite
CP	Chalcopyrite
TT	Tetrahedrite
AS	Arsenopyrite
PR	Pyrrhotite
MG	Magnetite
HE	Hematite
SL	Sphalerite
GL	Galena
MO	Molybdenite
GY	Gypsum
EP	Epidote
FL	Feldspar
BI	Biotite

3. Texture Chart (ie. Texture Short-Forms)

<<	Micro Veins
MX	Massive
BR	Brecciated
P*	Porphyritic
A*	Amygdaloidal
TC	Trachytic
WP	Wispy
VU	Vugs
AD	Adherring/Pyroclastic
RC	Chilled Rind/Pyroclastic

4. Structure Chart (ie. Structure Short-Forms)

C/	Contact
BD	Bedding
V/	Vein
F/	Fault
BN	Banding
FB	Flow Banding
CU	Upper Contact
CL	Lower Contact
SH	Shear

5. How Chart

Symbol	Most Dominant Mode of Occurence
A	Amygdaloids, cavity fillings
B	Blebs
#	Breccia fillings
C	Coatings & encrustations
*	Clasts
D	Disseminations & scat.x'ls
E	Envelopes
F	Framework crystals
G	Gouge
H	Halos
I	Eyes, augen
J	Interstitial
K	Stockwork
L	Laminated/bedded
M	Massive
N	Nodules
O	Spots
Q	Patches, as in quilts
R	Rosettes & x'tls clusters
S	Selvages
$	Sheeting
T	Stainings, as in tarnish
U	Euhedral crystals

V	Veins
>	Macroveins
<	Microveins
W	Boxwork
X	Massive and/or laminated/bedding
Y	Dalmationite
Z	Fresh, primary rock
+	Flooding

6. Amount Chart

Code	Assigned Value	Range
X	100	100
9	90	85 to 99
8	80	75 to <85
7	70	65 to <75
6	60	55 to <65
5	50	45 to <55
4	40	35 to <45
3	30	25 to <35
2	20	15 to <25
1	10	7 to <15
=	5	4 to < 7
+	3	2 to < 4
)	1	.5 to < 2
*	.3	.2 to <.5
(	.1	.05 to <.2
–	.03	.02 to <.05
.	.01	Trace = <.02
0	0	Nil, Absent
/	.07	Present: Estimate impossible
?	0	Possibly Present

7. Colour Chart

The colour chart can be used in two ways. A lightness can be combined with a colour, or two colours can be combined.

eg. 3U – Dark Brown

or

RU – Reddish Brown

Lightness

Symbol	Value
9	palest

Colour

Symbol	Colour
R	Red

8	pale
7	light
6	lighter
5	medium
4	darker
3	dark
2	very dark
1	darkest

U	brown (Umber)
O	Orange
T	Tan (khaki)
Y	Yellow
L	Lime (Y-G)
G	Green
Q	Aqua (B-P)
B	Blue
V	Violet (B-P)
P	Purple
M	Mauve (P-R)
W	White
A	Gray
N	Black (Noir)

APPENDIX II

Diamond Drillhole Logs

and

Assay Data

Drillholes: X87CH310 to X87CH319

```
IDEN6B0201      X87CH310 NQ    APR87RBP   JTT APR87ACK           0.0
IPRJ         EQUITY SILVER MINES LTD          MAIN ZONE - MN GEOCODE
S000   00   427 MT  368.7 090.0 -65.0                 7560.24   8409.74   1309.69
S001  427  1079     368.7 090.5 -64.0
S002 1079  1689     368.7 090.7 -63.0
S003 1689  2438     368.7 091.2 -64.5
S004 2438  3033     368.7 091.6 -64.5
S005 3033  3383     368.7 091.9 -65.0
S006 3383  3597     368.7 092.0 -65.75
S007 3597  3687     368.7 092.1 -65.0
/SCL        MT.2MT.2
LSCL            MT.2       LCTM
/NAM                                                        QZSZTOPYCPTTASPRGY
LNAM                                                        DMCBCLMGHESLGLMO
/      00     31          OVBN                P
R                :TRICONED - NO CORE
R                :CASING THRU BROKEN ROCK TO 3.1, NO TILL
/      31     69  30     2C11         <<      P BN     55       <)
L                 00          AT                                  <(
R                :LOC 2E
/      69    102  31     2E23     QZ <<       P CU     50  Q*  <+  <?
L                 10          AT                                  <)<(
R                :LOC 2C & 2D, POSSIBLE TT.
/     102    132  29     2D23         <<      PP           Q(  <=  <?
L                 03          TA                                  <*<*
R                :LOC 2C, RARE 2E. 0.2 M OF MASSIVE PY ABOVE DYKE BELOW
/     132    160  27     BA00         <<CM    P CU     30<<    D.
L                 15          BA                CL     60    D*
R                :RARE FELD LATHS
/     160    194  31     2D23         <<VU    P          V+Q-  <+  <*
L                 03          TA                                  <.
R                :LOC 2C23 LARGE QTZ VEINS VUGGY. GOOD GRADE SILVER
/     194    225  28     2E23         <<      P BN     40<(    <*  <.
L                 03          BA                                   <-
R                :LOC 2C & 2D
/     225    258  31     2C11         <<      P BD     55<(Q.  <(
L                 03          AT                                   <.
R                :LOC 2E
/     258    315  53     2E11CL       <<BR    P          <-     <(
L                 10          GA                            <)   <-
/     315    325  10     2E83         <<BR    P                 <*<.<?
L                 03          ga                            <*   <+<?
/     325    437 104     2E11CL       <<BR    P BD     50<.     <*
L                 31          TG                            <)   <(
R                :LOC 2C, MINOR BR.
/     437    457  15     2E81CY       BR<<    P                  ++
L                 00          TG
R                :FAULT ZONE
/     457    482  23     2E11CL       <<RC    P          <-     <)
L                 06          GA                            <)
/     482    508  26     8A00         <<CM    P CU     70<*    D.
L                 18          GA                CL     30    D)  <-
/     508    645 133     2E11CL       <<RC    P         <(     <*
L                 48          TG                            D+   <-
R                :FEW CLAY SEAMS
```

```
/    645   685  37    2C11CL     <<         P         <*     <)
L               10        TA                                   <(
/    685   760  67    2E11CL     <<RC       P         <(     <*
L               15        AG                              <+   <-
/    760   794  32    2E13       <<BR       P         <+     <(  <.
L               03        GA                              <+     <-
R              :SOME CLAY GOUGE
/    794   826  31    2E13       <<BR       P         <)     D*  <.
L               18        GA                              <)
R              :POSSIBLE SILICIFIED
/    826   840  14    8B00       <<CM       P CU    30<*     D.
L               10        2A                  CL    35
R              :ABUN FELD PHENOS
/    840   870  30    2E11       BR<<       P         <*     D)
L               18        GT                              <(
R              :INTENSELY BR'X
/    870   894  24    2E11       BR<<       P         <*     D*
L               10        GT                              <(
R              :AS ABOVE
/    894   943  45    2D11       <<         P         <(     D*
L               08        AT                              <*
R              :LOC 2E11 MINOR OCC OF SOFT LIME GREEN MINERAL IN OPEN SPACE
R              :FILLINGS - POSSIBLY SERICITE
/    943   987  40    2C11       <<         P F/    65<-     D*
L               06        TG                              <)  <.
R              :ABUN SHARDS AT TOP OF INTERVAL WITH SOME 2D
/    987  1017  29    2E11       <<         P         <(     <*
L               15        GT                            <.<-  <-
/   1017  1047  28    2E23       <<         P         <(Q.  <)
L               10        TG                            <-<*<.<(<-
/   1047  1068  20    2E11       <<BR       P         <-     <*
L               06        AT                              <(
/   1068  1097  27    2F14       <<BR       P         <-     D*Q-
L               05        TG                                 D.
R              :CP IN PATCH AT 107.8 WITH PY/MG
/   1097  1113  15    2C11       <<         P         <-     <(
L               08        6G                            <.Q1  <.
R              :ABUN CL SPOTS
/   1113  1143  29    2E12       <<         P         <-     <)<.
L               11        AT                            <.<-<-<(
R              :PY/HE/MG PATCH AT 113.9
/   1143  1173  29    2E14       <<         P         <-     <*<-<?
L               08        TG                              <*  <-
/   1173  1198  24    2E11       <<BR       P         <-     <*
L               10        GA                            <-Q)<.
R              :SOME SHARDS
/   1198  1228  25    2E11       <<BR       P         <-     D(D?
L               00        GA
R              :AS ABOVE
/   1228  1252  23    8A00       <<         P CU    50M-     D.
L               05        5G                              Q*
/   1252  1341  83    2E11       <<RC       P F/    35<(     D*
L               20        BA                              <)  D-
/   1341  1400  56    2C11       <<         P         <-     <*
L               15        TA                              <)  <.
```

```
/    1400   1430   29     2C12         <<          P          <(    Q)
L                  17          GT                                <+D-Q*
R                 :GYPSUM IN <<'S
/    1430   1458   27     2C21         <<          P          <-    Q)
L                  10          GT                                <+D-Q(Q?
R                 :AS ABOVE
/    1458   1525   62     2C11CL       <<          P BD    50<-     <*
L                  23          TG                                <=<.<.
R                 :LOC 2D11, GY IN <<'S
/    1525   1608   78     2C11CL       <<          P          <-    <*
L                  32          TG                                <=<.<-
R                 :AS ABOVE, GY IN <<'S
/    1608   1661   50     2C81CL       <<          P                <*
L                  20          TG                                <=  <.
/    1661   1780  115     2C11CL       <<          P BD    55<(     <*
L                  36          TG                                <=<-<-
R                 :GYPSUM IN <<'S
/    1780   1810   30     2C41         <<          P BD    50<.    <+<.
L                  18          TA                                <-D.
R                 :START OF ALTERNATION ZONE (SILICA)
/    1810   1840   29     2C42         <<          P          <-Q.  D+
L                  13          AT                                <)D*
/    1840   1870   28     2C42         <<BR        P          <-    D)
L                  06          TA                                <)D*
R                 :GYP IN <<'S, SOME BR'X WITH SILICIFICATION
/    1870   1900   30     2C42         <<          P          <-    D)
L                  18          TG                                <+D*
R                 :SOME SERICITE ALT'N
/    1900   1930   30     2C42         <<          P                D+
L                  12          TG                                <(D*
R                 :SOME SER. ALT'N, GYP IN <<'S
/    1930   1960   30     2C82         <<          P                D*
L                  12          TG                                <*D-
R                 :SOME SILIC. GYP IN <<'S
/    1960   1990   30     2C82         <<          P BD    35       D+
L                  18          TG                                <)D(<.
R                 :AS ABOVE
/    1990   2020   30     2E42         <<          P                D+
L                  19          GA                                Q)D)D-
R                 :LAPILLI INDISTINCT IN STRONG SILIFICATION
R                 :GYP IN <<'S, SMALL (0.2 M) BB, GYP <<'S CROSS-CUT BOTH BB + 2E
/    2020   2050   30     2E52         <<          P BN    50       D=
L                  19          GA                                Q*D)<(
R                 :LOC 2C52, GYP IN <<'S
/    2050   2080   30     2C52         <<BR                         D+
L                  21          TG                                <)D)
R                 :SOME MG BANDINGS, GYP IN <<'S
/    2080   2110   29     2C22         <<WP        P            Q-  D)
L                  06          AT                                <+D*
/    2110   2133   23     2C42         BR<<        P                D+
L                  09          TA                                <)D)Q(
R                 :STRONGLY BX'D. GYP IN <<'S
/    2133   2321  184     8C00         P*<<        P BN    40<(     D-
L                 110          YW                    CU    50    <*
R                 :BOTTEM CONTACT GRAD
```

```
/     2321   2339  18    2E52       <<BR         P                D=
L                  12         GA                                <*D)<(
/     2339   2358  19    8A00       <<CM         P CU     60<*
L                  10         4G                   CL     50      D+<.
/     2358   2370  12    2E42       <<BR         P               <(D*<*
L                  03         GA
/     2370   2376  06    8A00       <<CM         P CU     65<-
L                  03         6G                                     D*
R                 :UPPER C/ SHEARED.
/     2376   2385  09    2E52       BR<<         P                D)
L                  03         GA                                Q)
/     2385   2409  24    8A00       <<CM         P CU     60<.
L                  15         6G                   CU     60
R                 :TRACE GYP IN <<'S
/     2409   2440  30    2C42       <<BR         P F/     60      D+<.
L                  06         AT                                <*D-<*
R                 :LOC 2E42, UPPER C/ FAULT BR 0.2 M.
/     2440   2470  29    2E42       <<BR         P BD     40      D+
L                  09         AG                                D-<(
R                 :LOC 2D42
/     2470   2500  30    2D42       <<           P                D)
L                  18         GA                                <)D-
R                 :LOC 2E42
/     2500   2530  30    2E42       <<           P                D)
L                  15         AG                                <)D.<-
R                 :LAPILLI INDISTINCT
/     2530   2560  30    2E42       <<           P BD     35      D+
L                  09         AG                                <)D*<-
R                 :LOC INTERLEVELED 2D42
/     2560   2590  30    2E42       <<BR         PP               D)
L                  11         AG                              <.<*D-<.
R                 :LOC INTERLEV 2D42
/     2590   2614  23    2E42       <<BR         P           <-   D+<.
L                  09         AG                                <)D-
/     2614   2625  11    8A00       <<           P CU     50
L                  06         7G                                     <-
/     2625   2650  25    2E42       <<BR         P BD     55      D+
L                  10         AG                                <)D*
/     2650   2673  22    2E42       <<BR         P           <-   D*
L                  03         GA                                <)D.<.
R                 :LOC 2D42
/     2673   2701  28    8A00       <<CM         P BN     50<-
L                  20         5G                   CL     335     D.
/     2701   2740  37    2E51       <<BR         P           <-   D)
L                  03         GA                                <*
R                 :LAPILLI INDISTINCT
/     2740   2770  29    2E53       <<BR         P           <-   D)<-
L                  03         GA                                <*D(
R                 :LOC 2C
/     2770   2800  30    2E43       <<BR         P             <- D+<(Q?
L                  18         GA                                <*D.
/     2800   2825  25    2E53       <<           P             <( D+<-Q?
L                  19         GA                                <)D.
/     2825   2850  25    2E53       <<BR         P                D+<-
L                  11         GA                                <*
```

```
/   2850  2877  27    2E53       <<          P             Q.  D+D-Q?
L               09        GA                                     Q.
R               :BOTTOM C/ TRANSITIONAL OVER 0.4 M
/   2877  2900  23    8D41       <<MX        P                 D*
L               03        3G                   CL    30        D(<-
R               :STRANGE - POSSIBLY FG ANDESITE FLOW, PRE-MINERAL DYKE?
R               :ABUN. GYP IN <<'S, ABUN SHARDS AND SOME VOLC FRAGS
/   2900  2916  16    2E53       <<BR        P             Q.  D+D.
L               03        GA                                 <*D(
/   2916  2955  38    8D41       <<MX        P                 D)
L               24        GA                                   D-<-
R               :ABUN GYP, IN <<'S, C/ TRANSITIONAL SHARDS?
/   2955  2984  28    8D41       <<MX        P                 D)
L               10        GA                                 Q)D-<-
R               :AS ABOVE, FRAGMENTS OF RELICT LAPILLI? REPLACED BY CL
/   2984  3000  15    2E41       <<          P                 D*
L               00        GA                                 <)
R               :LAPILLI INDISTINCT
/   3000  3013  13    8D41       <<MX        P                 D*
L               06        5G                                     Q-
R               :OCC LAPILLI
/   3013  3023  09    2E41       <<BR        P                 D*
L               00        GA                                 <+
/   3023  3053  30    8D41       <<MX        P                 D)
L               12        4G                                   D-
R               :POSSIBLE DYKE? GYP IN <<'S, SHARDS            D*
/   3053  3081  28    8D41       <<MX        P                 D*
L               15        6G                                 Q)
R               :AS ABOVE, CL REPLACING LAPILLI?
/   3081  3110  28    2E54       <<          P                 D+Q(     <*
L               11        GA                                 <*D*  Q(
R               :SOME ASSIMILATED 8D
/   3110  3148  37    8D41       <<MX          CU    50        D+
L               21        GA                   CL    25      Q)D.<-
R               :GYP IN <<'S
/   3148  3172  24    2E41       <<          P                 D)
L               11        AG                                 <*
R               :LAPILLI INDISTINCT
/   3172  3197  24    2E41       <<          P                 D+D.
L               06        AG                                 <)
R               :AS ABOVE
/   3197  3223  25    8D41       <<MX        P                 D+
L               09        3A                                   D.
R               :GYP IN <,'S
/   3223  3248  25    2E51       <<          P                 D=D.     D.
L               06        GA                                 <)D.
R               :LOC 8D, LAPILLI INDISTINCT
/   3248  3280  31    2E51       <<BR        P                 D+  D?
L               09        GA                                 <+
/   3280  3310  30    2E51       <<BR        P                 D=<.     D.
L               11        GA                                 <+D-
/   3310  3334  24    2E51       <<BR        P                 D+<-     <-
L               06        GA                                 <)D.
/   3334  3363  28    8D44       <<MX        P          <-     D+D.     Q-
L               16        2A                                 <*D-
```

```
R                    :SULPHIDE Q'S INCLUSIONS?
/     3363  3393  30    8D41       <<MX        P          <-    D=
L                 19        2A                                <*D-
R                    :LAPILLI INCLUSIONS
/     3393  3455  62    8B00       <<CM        P CU     20<-    D-
L                 34        6G     P*            CL     40    <*D-
R                    :A REAL DYKE?
/     3455  3480  24    2E41       <<          P                D+
L                 09        GA                                <)D.
R                    :MINOR ASSIMILATED 8B
/     3480  3510  30    2E52       <<BR        P            Q-  D=
L                 11        GA                                <*D(<-
/     3510  3539  28    2E54       <<BR        P          <*    D)Q-<?
L                 09        GA                                <*
/     3539  3571  32    8D41       <<MX        P          <-    D=
L                 10        3A                                <*D-
R                    :CONTAINS LAPILLI FRAG
/     3571  3589  17    2E42       <<          P          <-    D+
L                 03        GA                                <)D(
R                    :GRADES INTO 8D, THEN SHARP INTO GABBRO
/     3589  3687  97    7C01                   P                D(
L                 63        7A                                  D-
R                    :TYPICAL COARSE GRAINED, BIOTITE/FELDSPAR MONZONITE
R                    :END OF HOLE AT 368.7
A001
ALAB                 EQUITY MINESITE LABORATORY
ATYP                 ASSAY
AMTH                 WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM                 RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB   % AS   % FE   % ZN
R       00     31 :TRICONED - NO CORE
R       31     69 :VOLC. - NO CORE
A001    69    102         9381        0.01    24.0 0.54  0.02  0.005 3.96   0.13
A001   102    132         9382        0.02    11.0 0.43  0.05  0.005 9.00   0.05
R      132    160 :DYKE - NO SAMPLE
A001   160    194         9383        0.03    35.0 1.17  0.04  0.01  5.55   0.32
A001   194    225         9384        0.03    11.0 0.38  0.03  0.01  2.63   0.07
A001   225    258         9385        0.02     9.0 0.19  0.03  0.005 3.81   0.06
R      258    315 :VOLC - NO SAMPLE
A001   315    325         9386        0.03    31.0 0.31  0.03  0.01  3.06   0.05
R      325    760 :VOLC - NO SAMPLE
A001   760    794         9387        0.01     5.0 0.12  0.03  0.01  3.07   0.17
A001   794    826         9388        0.02    10.0 0.11  0.03  0.01  3.12   0.03
R      826    840 :DYKE - NO SAMPLE
A001   840    870         9389        0.005    2.0 0.06  0.03  0.005 2.49   0.01
A001   870    894         9390        0.005    1.0 0.07  0.02  0.005 2.71   0.005
R      894    987 :VOLC - NO SAMPLE
A001   987   1017         9391        0.01     3.0 0.04  0.02  0.005 3.03   0.05
A001  1017   1047         9392        0.02    12.0 0.10  0.02  0.005 3.36   0.10
A001  1047   1068         9393        0.02     4.0 0.08  0.04  0.01  4.32   0.02
A001  1068   1097         9394        0.42    62.0 0.15  0.09  0.05  7.73   0.09
R     1097   1113 :VOLC - NO SAMPLE
A001  1113   1143         9395        0.03     7.0 0.08  0.03  0.01  3.92   0.04
A001  1143   1173         9396        0.05    25.0 0.18  0.06  0.06  7.45   0.04
A001  1173   1198         9397        0.06    95.0 0.90  0.05  0.01  3.81   0.03
A001  1198   1228         9398        0.04    53.0 0.52  0.04  0.001 2.83   0.03
```

R	1228	1252	:DYKE - NO SAMPLE								
R	1252	1400	:VOLC - NO SAMPLE								
A001	1400	1430		9399	0.04	19.0	0.28	0.03	0.02	3.86	0.08
A001	1430	1458		9400	0.04	24.0	0.49	0.03	0.02	4.19	0.65
R	1458	1780	:VOLC - NO SAMPLE								
A001	1780	1810		9401	0.17	10.0	0.36	0.04	0.01	6.26	0.04
A001	1810	1840		9402	0.02	13.0	0.21	0.02	0.01	3.45	0.01
A001	1840	1870		9403	0.02	6.0	0.10	0.03	0.01	2.98	0.02
A001	1870	1900		9404	0.01	7.0	0.20	0.03	0.01	3.65	0.01
A001	1900	1930		9405	0.07	10.0	0.25	0.04	0.02	4.72	0.05
A001	1930	1960		9406	0.04	10.0	0.18	0.03	0.01	3.44	0.05
A001	1960	1990		9407	0.02	13.0	0.13	0.03	0.02	3.08	0.04
A001	1990	2020		9408	0.07	6.0	0.10	0.04	0.02	5.68	0.03
A001	2020	2050		9409	0.17	10.0	0.15	0.05	0.02	6.33	0.05
A001	2050	2080		9410	0.13	5.0	0.07	0.02	0.005	4.64	0.01
A001	2080	2110		9411	0.01	7.0	0.55	0.01	0.01	1.49	0.01
A001	2110	2133		9412	0.15	21.0	0.27	0.03	0.01	5.41	0.03
R	2133	2321	:DYKE - NO SAMPLE								
A001	2321	2339		9413	0.13	5.0	0.15	0.02	0.01	7.96	0.10
R	2339	2358	:DYKE - NO SAMPLE								
A001	2358	2370		9414	0.14	40.0	0.47	0.01	0.01	5.61	0.05
R	2370	2376	:DYKE - NO SAMPLE								
A001	2376	2385		9415	0.10	24.0	0.43	0.01	0.01	4.14	0.19
R	2385	2409	:DYKE - NO SAMPLE								
A001	2409	2440		9416	0.28	9.0	0.53	0.01	0.01	4.75	0.02
A001	2440	2470		9417	0.19	28.0	0.40	0.02	0.01	5.30	0.06
A001	2470	2500		9418	0.17	32.0	0.54	0.03	0.03	4.68	0.03
A001	2500	2530		9419	0.18	27.0	0.48	0.03	0.03	4.89	0.04
A001	2530	2560		9420	0.26	26.0	0.61	0.03	0.02	6.01	0.15
A001	2560	2590		9621	0.34	25.0	0.55	0.04	0.03	4.15	0.04
A001	2590	2614		9622	0.33	16.0	0.35	0.02	0.01	5.67	0.05
R	2614	2625	:DYKE - NO SAMPLE								
A001	2625	2650		9623	0.20	8.0	0.32	0.01	0.005	3.45	0.04
A001	2650	2673		9624	0.21	16.0	0.38	0.02	0.005	3.40	0.08
R	2673	2701	:DYKE - NO SAMPLE								
A001	2701	2740		9625	0.34	39.0	0.77	0.04	0.02	4.21	0.04
A001	2740	2770		9626	0.34	26.0	0.61	0.02	0.03	2.63	0.04
A001	2770	2800		9627	0.49	23.0	0.84	0.03	0.10	4.98	0.16
A001	2800	2825		9628	0.40	30.0	5.51	0.04	0.09	5.00	0.05
A001	2825	2850		9629	0.46	64.0	1.80	0.07	0.10	4.75	0.07
A001	2850	2877		9630	0.37	66.0	1.48	0.06	0.06	4.54	0.09
A001	2877	2900		9631	0.17	61.0	1.46	0.06	0.02	3.57	0.08
A001	2900	2916		9632	0.27	37.0	0.98	0.03	0.02	5.17	0.45
A001	2916	2955		9633	0.03	12.0	0.31	0.03	0.01	3.54	0.03
A001	2955	2984		9634	0.04	13.0	0.33	0.02	0.02	4.15	0.06
A001	2984	3000		9635	0.15	24.0	0.42	0.02	0.005	4.04	0.23
A001	3000	3013		9636	0.05	12.0	0.30	0.01	0.005	3.85	0.05
A001	3013	3023		9637	0.12	22.0	0.25	0.02	0.005	2.49	0.37
A001	3023	3053		9638	0.03	17.0	0.30	0.02	0.01	4.28	0.03
A001	3053	3081		9639	0.005	4.0	0.04	0.005	0.001	4.12	0.03
A001	3081	3110		9640	0.17	13.0	0.34	0.005	0.03	6.45	0.70
A001	3110	3148		9641	0.02	2.0	0.02	0.005	0.001	4.10	0.05
A001	3148	3172		9642	0.12	9.0	0.07	0.005	0.005	3.62	0.17
A001	3172	3197		9643	0.10	12.0	0.11	0.005	0.02	3.94	0.11
A001	3197	3223		9644	0.02	9.0	0.05	0.005	0.001	4.18	0.03

A001	3223	3248		9645	0.07	9.0	0.11	0.005	0.005	4.39	0.07
A001	3248	3280		9646	0.07	6.0	0.14	0.005	0.005	2.28	0.03
A001	3280	3310		9647	0.11	8.0	0.20	0.005	0.005	2.43	0.04
A001	3310	3334		9648	0.07	6.0	0.15	0.005	0.005	1.82	0.04
A001	3334	3363		9649	0.005	0.5	0.03	0.005	0.005	2.47	0.02
A001	3363	3393		9650	0.02	0.5	0.03	0.005	0.005	3.39	0.03
R	3393	3455	:DYKE - NO SAMPLE								
A001	3455	3480		9651	0.05	5.0	0.25	0.005	0.005	3.92	0.03
A001	3480	3510		9652	0.04	3.0	0.20	0.005	0.005	3.57	0.08
A001	3510	3539		9653	0.07	0.5	0.16	0.005	0.005	2.91	0.12
A001	3539	3571		9654	0.02	0.5	0.02	0.005	0.001	1.81	0.02
A001	3571	3589		9655	0.02	0.5	0.03	0.005	0.001	2.45	0.02
R	3589	3687	:GABBRO - NO SAMPLE								
R			:END OF HOLE AT 368.7 M								

```
IDEN6B0201       X87CH311 NQ    MAY87DJH    JTT MAY87ACK          0.0
IPRJ          EQUITY SILVER MINES LTD        MAIN ZONE - MN GEOCODE
S000   00    320 MT   324.6 090.0 -65.0               7630.15    8438.55    1270.00
S001  320   1006      324.6 090.5 -64.5
S002  1006 1783       324.6 090.9 -65.0
S003  1783 2487       324.6 091.8 -65.0
S004  2487 2944       324.6 092.4 -64.5
S005  2944 3178       324.6 092.5 -65.5
S006  3178 3246       324.6 092.6 -65.0
/SCL          MT.2MT.2
LSCL              MT.2       LCTM
/NAM                                                           QZSZTOPYCPTTASPRGY
LNAM                                                           DMCBCLMGHESLGLMO
/      00     31         OVBN                  P
R                 :TRICONED - NO CORE , BROKEN ROCK - NO TILL
/      31     60  22     2D23SZMS   <<         P          O.   <+
L                 02          6A                               <(  <?
R                 :MASSIVE PY REPLACEMENT @ 5.0 - 5.1 M (40 % PY): LOC 2E
/      60     90  28     2D23SZMS   <<         P          <(O.   <+
L                 05          6A                               <-
R                 :INTO 2C 6.8 - 7.3 M
/      90    120  29     2D83MS     <<BR       P          <(     <+
L                 06          6A                               <-  <?<(<?
R                 :POSS HS (V. FINE GRANINED):V. WEAK LOC BXIA: MASS PY
R                 :REPLACEMENT 10.7 - 10.8 M
/     120    150  29     2D23SZ     <<BR       P           O-   <+
L                 08          GA                                  <?
R                 :V. WEAK LOC BXIA
/     150    169  19     2D23SZ     <<         P          <(O.   <+
L                 06          GA                                  <?
/     169    178  085    2D85PYMS              P          M1     M3
L                 07          6A                                  D?M+
R                 :PALE BROWN SL; PYROCLASTIC FRAGS BECOMING PROGRESSIVELY
R                 :FINER DOWN HOLE - NO LAPILLI
/     178    193  15     2D13       <<BR       P                 <+
L                 03          GA                               <-
R                 :V. WEAK LOCAL BXIA W/VUGGY MATRIX
/     193    213  20     2D13CL     <<         P BD   040      <(
L                 09          GA                               <-
R                 :V. WEAK MS ALT'N ENVS. AROUND PY <<: WEAK CL ALT'N
/     213    247  30     8D13CL     <<P*       P FB   038      <(
L                 00          GA                               <-D-
R                 :CNT ATTITUDES NOT OBSERVED DUE TO HEAVY BROKEN CORE: FB//
R                 :TO CNT?: PRE-MINERAL DYKE
/     247    270  23     2E13CL     <<         P                 <-
L                 04          GA                               <.
R                 :INTO 2D TOWARDS E.O.I.: WEAK MS ALT'N ENV. ON <<: V. WEAK
R                 :CL ALT'N
/     270    300  30     2D13CL     <<         P                 <-
L                 09          GA                               <.
R                 :V. WEAK CL ALT'N: WEAK PATCHY MS ALT'N: INTO 2E TOWARDS EOI
/     300    330  27     2E13CL     <<         P                 <-
L                 15          GA                               <.  <.
R                 :WEAK CL ALT'N
/     330    360  30     2E13CL     <<BR       P                 <-
```

A001	3223	3248	9645	0.07	9.0	0.11	0.005	0.005	4.39	0.07
A001	3248	3280	9646	0.07	6.0	0.14	0.005	0.005	2.28	0.03
A001	3280	3310	9647	0.11	8.0	0.20	0.005	0.005	2.43	0.04
A001	3310	3334	9648	0.07	6.0	0.15	0.005	0.005	1.82	0.04
A001	3334	3363	9649	0.005	0.5	0.03	0.005	0.005	2.47	0.02
A001	3363	3393	9650	0.02	0.5	0.03	0.005	0.005	3.39	0.03
R	3393	3455	:DYKE - NO SAMPLE							
A001	3455	3480	9651	0.05	5.0	0.25	0.005	0.005	3.92	0.03
A001	3480	3510	9652	0.04	3.0	0.20	0.005	0.005	3.57	0.08
A001	3510	3539	9653	0.07	0.5	0.16	0.005	0.005	2.91	0.12
A001	3539	3571	9654	0.02	0.5	0.02	0.005	0.001	1.81	0.02
A001	3571	3589	9655	0.02	0.5	0.03	0.005	0.001	2.45	0.02
R	3589	3687	:GABBRO - NO SAMPLE							
R			:END OF HOLE AT 368.7 M							

```
L                 08        GA                                          <.  <.
R                :WEAK LOCAL BRECCIA (TECTONIC): INTO 2E87 LOC
/    360   391   31    2E23SZMS   <<BR          P              <-O.   <(
L                 11         6T                                             <.
R                :INTO 2D TOWARDS EOI: WEAK LOCAL TECTONIC BRECCIA
/    391   397   06    MSDEPY                   P              M1     M9
L                 06
R                :VEIN? OR LENS
/    397   420   22    2E23SZMS   <<BR          P              <(O.   <(
L                 06         6T
R                :INTO WEAK BXIA LOCALLY
/    420   450   29    2D13CL     <<            P              <+     <-O.
L                 16        GA                                    <(<(
R                :INTO 2E LOCALLY AND TOWARDS EOI: INTO 2D8 LOC
/    450   480   28    2E13CL     <<            P              <(     <-
L                 15        GA                                    <-
R                :INTO 2E8 LOC. - SOME FRAGS ARE MAGNETIC
/    480   497   17    2E13CL     <<            P                     <-
L                 13        GA                                      <(  <-
R                :MS ALT'N ENVS. AROUND <<
/    497   515   17    2E23SZMS   <<            P              <-O.   <(
L                 08        TG
/    515   533   17    2E13CL     <<            P                     <-
L                 12        GA                                      <-  <.
/    533   540   07    8A10CL     P*            P CU   030
L                 07        AG                    CL   028
R                :FLOW BANDED DYKE - LOOKS LIKE A FOLD: V. SMALL ALT'D
R                :PLAG PHENOS - LOOKS MORE LIKE A PRE-MIN DYKE BUT NO
R                :MINERALIZATION
/    540   570   29    2E13CL     <<            P                     <-
L                 12        GA                                    <.<(  <-
R                :INTO 2D8 LOCALLY
/    570   591   18    2E13CL     <<            P                     <-
L                 03        GA                                      <(  <.
R                :INTO 2D8 @ 58.0 TO EOI
/    591   661   70    8A13CL     <<P*          P CU   024        <.
L                 47        AG                                          <.
R                :LOWER CNT SHARP & IRREGULAR: WEAKLY PORPH
/    661   680   19    8C80MS     P*            P
L                 04        8G                                          D.
R                :LOWER CNT SHARP & IRREGULAR
/    680   711   30    8A13CL     P*<<          P                     <.
L                 14        AG                    CL   045   <.<.   <.
R                :WEAK P* TEXT: GOOD SHARP "INTRUSIVE", LOWER CNT
/    711   738   27    2E13CL     <<            P                     <-
L                 03        GA                                <.<-D.<-
R                :DISSEM, MG IN ANDESITIC LAPILLI: ANDESITIC & DACITIC LAPILLI
R                :IN A DACITIC? MATRIX: INTO 2D LOC: MS ALT'N IN DACITE FRAGS
R                :ONLY: NO ALT'N ASSOC W/<<
/    738   756   18    2D83MS     <<            P                     <(
L                 02        TA                                    <(
R                :INTO 2C LOCALLY: LOCALLY STRONG << TEXT (ASSOC W/6T COLOR)
/    756   780   23    2D83MS     <<            P                     <(
L                 02        TA                                <-<(  <(
R                :MASSIVE PY + MG 77.3-77.4 M W/<< OF CB + HS: TO 2C LOC
```

```
/     780    810   29     2E13CL       <<              P                 <(
L                  03          5G                                    <-<(   <-
R                 :INTO 2E83 LOC IN AREAS OF MORE INTENSE <<
/     810    840   29     2E13CL       <<              P            <-     <(
L                  06          5G                                    <-<(D-<.
R                 :DISSEM MG IN ANDESITIC LAPILLI: INTO 2E83 LOC IN AREAS OF MORE
R                 :INTENSE <<: OCCAS VOLC BXIA FRAGS
/     840    870   30     2E13CL       <<              P            <.     <-
L                  08          5G                                    <.<-   <-
R                 :INTO 2D LOCALLY
/     870    900   30     2E23SZCL     <<              P             O-   Q)
L                  09          GA                                      Q)   <-
/     900    930   29     2E23SZCL     <<              P             O.   Q(
L                  00          GA                                      Q(   <-
R                 :INTO 2D LOCALLY
/     930    960   29     2E212CL      <<              P                  Q)
L                  09          AG                                      Q(Q-
R                 :INTO 2E8 LOC
/     960    990   30     2D12CL       <<BR            P             <.   <(<-        <-
L                  06          GA                                      <-   <-
R                 :MASS PY + MG 38.8-38.9 M: V. WEAKLY BRECCIATED LOCALLY
R                 :INTO 2E LOCALLY
/     990   1020          2E23SZCL     <<BR            P            Q(   <)
L                              GA                                      <(   <-
R                 :V. WEAK LOCAL BXIA (TECTONIC)
/    1020   1050   30     2D13CL       <<BR            P                  <(          <+
L                  14          GA                                      <(<.<-
R                 :8A DYKE 104.0-104.1: WEAK LOCAL BR TEXT: INTO 2E LOC
/    1050   1080   30     2D13CL       <<BR            P            <-     <(<.
L                  19          GA                                      <(<.<.
R                 :INTO 2E LOC: WEAK LOCAL BR TEXT                                    <-
/    1080   1089   15     2D13CL       <<BR            P                  <(<.
L                  10          GA                                      <(
R                 :WEAK LOCAL BXIA TEXT (TECTONIC): INTO 2E LOC
/    1089   1099   10     8A10CL       <<P*            P CU    020     <(            <)
L                  08          AG                        CL    035
R                 :WEAK P* TEXT
/    1099   1130   27     2E12CL       <<              P                  Q)          <(
L                  09          GA                                      <(Q)
/    1130   1160   29     2E13CL       <<              P                  <-
L                  22          GA                                      <-
R                 :LOCAL WEAK SILICIFICATION OF MATRIX (MS + QZ?)
/    1160   1190   30     2E23SZCL     <<              P             O-   <(
L                  17          GA                                      <-Q-<-
R                 :LOCAL WEAK SILICIFICATION OF MATRIX (MS + QZ?)
/    1190   1220   29     2E23SZCL     <<              P             O.   <(<.
L                  19          GA                                      <-   <.
R                 :INTO 2D LOCALLY
/    1220   1250   29     2E43QZCL     <<              P                  Q+          <-
L                  18          GA                                      <-Q.<.
R                 :INTO 2D LOCALLY
/    1250   1280   28     2D23SZCL     <<              P            <-O.  <(
L                  23          GA                                      <(       <-
R                 :INTO 2E LOC: MOD. SILICIFICATION LOCALLY
/    1280   1310   29     2E13CL       <<              P                  <(
```

```
L                 17         GA                                  <(
R                :INTO 2C LOC: LOCAL STRON SILICIFICATION (QZ ONLY) - DARK
R                :GREEN COLOR
/     1310  1340  28     2E23SZCL    <<          P             O.  <(
L                 15         GA                                #(<(  <.
R                :STRONG LOCAL SILICIFICATION
/     1340  1352  12     2D23MS      <<          P             O.  <)D(
L                 10         TA                                  <(
/     1352  1386  33     2C83MS      <<BR        P                 <)        <-
L                 14         5T                                  <)
R                :8A 137.5-137.9 M: WEAK LOCAL BXIA TEXT (TECT.)
/     1386  1410  24     2D23SZCL    <<          P           <(O.  <)        <-
L                 09         GA                                  <)
R                :INTO 2E LOCALLY
/     1410  1440  30     2D13CL      <<          P           <.    <)        <-
L                 18         GA                                <.<)
R                :GY STRINGERS X-CUT ALL OTHER STRINGERS & FRACTURE FILLINGS
R                :POSSIBLE 8D DYKE 143.3-144.5
/     1440  1470  30     2D13CL      <<          P                 <+        <-
L                 21         GA                                  <)<-
/     1470  1500  30     2D83MS      <<          P                 <)        <-
L                 07         TA                                  <(<-<.
/     1500  1530  30     2D83MS      <<          P                 <)        <-
L                 19         TA                                  <(<-
R                :LOCAL MOD. SILICIFICATION
/     1530  1560  29     2D83MS      <<          P                 <)<-
L                 05         6T                                  <-<-
/     1560  1590  30     2D82MS      <<<<        P                 <)
L                 21         5T      BR                          <-<(
R                :LOCAL WEAK BXIA TEXT
/     1590  1620  30     2D23CL      <<          P             O-  <(        <.
L                 22         GA                                  <-<-
/     1620  1642  21     2D13CL      <<<<        P                 <(
L                 13         GA                                  <-<)<(
R                :INTO 2D1 LOC: << S/MS ALT'N ENVS.
/     1642  1730  85     8C80MS      P*          P CU   060        D.
L                 72         GW
R                :UPPER CNT SHARP & REGULAR: LOWER CNT GRAD OVER 0.05 M
R                :TYPICAL LATITE
/     1730  1752  22     8A10CL      A*          P
L                 15         4G
R                :LOWER CNT GRAD OVER 0.1 M
/     1752  1821  65     8C80MS      P*FB        P FB   060        D-
L                 47         6A                    CL   060
R                :2 XENOLITHS OF 2DE
/     1821  1850  28     2E12CL      <<<<        P                 Q+        <.
L                 21         GA                                  <(Q(<-
R                :LOCAL SILICIFICATION
/     1850  1878  28     2E12CL      <<<<        P                 <)<.      <-
L                 24         GA                                  <(<(<(
/     1878  1900  22     8D00        P*<<        P CU   030<.    <.
L                 17         VA                                     <?
R                :DACITE COMP?: MINOR MS ALT'N ENVS. ON <<.: UPPER CNT SHARP &
R                :REGULAR: LOWER CNT WEAKLY GRAD
/     1900  1915  15     8D83MS      <<P*        P                 <(        <-
```

```
L                17       5T      BR
R               :ALTERED DACITE (AS ABOVE): MINOR LOCAL BXIA: LOWER CNT
R               :GRAD OVER 0.05 M
/  1915  1940   25    8D00      P*<<       P                   <.      <-
L                17       VA                              <-     <.
R               :AS ABOVE 187.8 - 190.0: INTO 8D8 LOC: MS ALT'N ENVS. OF <<
/  1940  1970   30    8D00      P*<<       P                   <.      <-
L                19       VA                              <-     <.
R               :AS ABOVE W/MS ALT'N ENVS. AND INTO 8D8
/  1970  1994   24    8D00      P*<<       P            <-     <.      <.
L                19       VA                 CL   020   <.<.   <.
R               :AS ABOVE LOWER CNT SHARP & REGULAR: ANDESITE 198.8-199.4
/  1994  2020   26    2D87MS    BR<<       P          #1     #+#.     <-
L                03       6T                                 #(
/  2020  2052   31    2D13CL    <<BR       P                 <(       <)
L                17       GA                               <-<-
R               :INTO 2D87 LOC: 8A - 204.7-205.2 M
/  2052  2064   12    2D87MS    BR<<       P          #1     #(
L                04       6T                               <-
R               :INTO 2D13 LOC
/  2064  2195  131    8A10CLCB  P*         P CU  030
L               111       AG                                 D.
R               :UPPER CNT IRREG (FAIRLY SHARP): LOWER CNT OBSCURRED IN BROKEN
R               :CORE
/  2195  2225   30    2C23MS    <<<<       P           0-    <+
L                05       5T                               <(<-
/  2225  2255   30    2C27MS    BR<<       P          #10-   #+
L                05       AT                               <-
R               :INTO 2D23 LOC
/  2255  2285   30    2C83MS    <<<<       P                 <
L                11       AT                               <(
/  2285  2316   30    2C87MS    BR<<       P          #1     #+
L                19       AT                               <+
/  2316  2346   30    2C87MS    BR<<       P          #1     #+
L                12       TA                               <+
R               :LOCAL SILICIFICATION
/  2346  2377   29    2C83MS    <<BR       P                 <)
L                17       TA                              <(<)
R               :WEAK LOCAL BRECCIA: PATCHY MS ALT'N
/  2377  2407   30    2C13CL    <*BR       P          <-0?   <)
L                03       GA                              <.<(
R               :WEAK TO MED LOCAL BXIA
/  2407  2438   30    2C13CL    <<<<       P                 <)<?
L                08       GA    BR                         <(
R               :V. WEAK LOCAL BXIA
/  2438  2468   30    2C17CL    <<BR       P          #1     #+<?
L                21       GA                               <(#(
R               :LOCAL BXIA TEXT W/QZ+PY+MG MATRIX - V. F. GRAINED
/  2468  2499   30    2C27MS    BR<<       P          #10-   #+<-
L                14       TA                               <(#(
R               :LOCAL BXIA TEXT W/QZ+P+MG MATRIX - V. F. GRAINED
/  2499  2529   30    2C17CL    BR<<       P          #1     #+<(
L                19       GA                               <(
R               :MINOR MS ALT'N: V. F. GRAINED MATRIX IN BXIA
/  2529  2560   30    2C27CL    BR<<       P          #10-   #+<(
```

```
L                  18      GA                                      <-<(#-
R                 :LOCAL BXIA TEXT W/F. GRAINED QZ+PY+MG MATRIX
/    2560   2590  29     2C27MS     BR<<         P            #-O-   #)<(
L                  11      GT                                      <-
R                 :WEAKER << LAST 0.5 M OF INT.
/    2590   2620  30     2C13CL     <<<<         P                      <)
L                  15      GA                                      <)<-
/    2620   2651  30     2C13CL     <<<<         P                      <(
L                  17      GA                                      <)
R                 :INTO 2D LOCALLY: WEAK LOC BXIA
/    2651   2682  31     2C13CL     <<<<         P                      <(
L                  24      GA                                   <(<)
R                 :INTO 2D LOCALLY: WEAK LOC BXIA
/    2682   2712  30     2C13CL     <<<<         P                      <(
L                  21      GA       BR                          <-<)
R                 :INTO 2D LOC: V. WEAK LOCAL BXIA
/    2712   2743  30     2D13CL     <<<<         P                      <(
L                  05      GA       BR                               <)
R                 :V. WEAK LOC BXIA W/PY+CL MATRIX
/    2743   2779  36     2D13CL     <<<<         P                      <(
L                  19      GA                                        <)
/    2779   2810  31     8D11CL     <<           P                      D)        <-
L                  27      AG                                           D-
R                 :SHARP IRREG. UPPER CNT.
/    2810   2840  29     8D11CL     <<P*         P              <.      D)
L                  12      AG                                     <.    D-<.
R                 :TWO SMALL TUFF XENOLITHS: PLAG PHENOS TO 10 X 3 MM
/    2840   2870  30     8D11CL     <<           P                      <(
L                  25      AG                                     <.<(D-
/    2870   2900  30     8D11CL     <<           P                      <.
L                  27      AG                                     <.<.D-
R                 :V. WEAK <<TEXT
/    2900   2930  30     8D11CL     <<           P                      <.
L                  17      AG                                     <-<.D-
R                 :V. WEAK << TEXT
/    2930   2953  23     8D11CL     <<           P                      <.
L                  11      AG                                       <.D-
R                 :TR. EP ALT'N: V. WEAK << TEXT
/    2953   2980  27     2D11CL     <<<<         P                      <.
L                  16      GA                                       <+<)
/    2980   3010  30     2D11CL     <<<<         P                      <.
L                  15      GA                                       <+<)
/    3010   3031  21     2D13CL     <<<<         P                      <(
L                  22      GA                                       <+
R                 :MS ALT'N ENVS. ON <<
/    3031   3053  21     8D13CL     P*<<         P                      <-
L                  09      AG                                     <-<-
R                 :POSSIBLE BA: CNTS V. IRREGULAR - FAIRLY SHARP
/    3053   3078  25     2D13CL     <<<<         P                      <(
L                  13      GA                                     <-<+
/    3078   3108  30     2D13CL     <<<<         P                      <(
L                  22      GA                                     <.<)
R                 :MS ALT'N ENVS. ON <<
/    3108   3139  30     2D23CL     <<<<         P                O-    <(
L                  19      GA                                     <-<)
```

```
/     3139  3165  26     2D13CL      <<<<          P                 <(
L                 14          GA                             <-<)
/     3165  3180  15     7C01                      P                 D(
L                 12          5A                                     D-
R                 :TRANSITION ZONE: UPPER CNT INDISTINCT
/     3180  3246  66     7C00        GT            P
L                 44          5A                                     D(
R                 :GOOD COARSE GRAINED MONZONITE
R                 :EOH @ 324.6 M
A001
ALAB              EQUITY MINESITE LABORATORY
ATYP              ASSAY
AMTH              WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM              RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS  % FE  % ZN
R       00    31  :TRICONED - NO CORE
A001    31    60         9701        0.07    52.0 0.50  0.04  0.001 6.69  0.02
A001    60    90         9702        0.04    29.0 0.91  0.02  0.001 5.43  0.06
A001    90   120         9703        0.08    47.0 1.42  0.05  0.001 9.28  0.49
A001   120   150         9704        0.03    42.0 0.81  0.02  0.001 6.72  0.02
A001   150   169         9705        0.04    38.0 0.70  0.04  0.00110.81  0.32
A001   169   178         9706        0.74    79.0 1.25  0.27  0.06 24.60  4.30
A001   178   193         9707        0.04    16.0 0.33  0.02  0.001 4.86  0.05
A001   193   213         9708        0.02     3.0 0.06  0.005 0.001 1.66  0.02
A001   213   247         9709        0.03    22.0 0.97  0.02  0.001 3.66  0.06
A001   247   270         9710        0.04     0.5 0.05  0.005 0.002 3.30  0.03
A001   270   300         9711        0.005    0.5 0.01  0.005 0.001 2.99  0.005
A001   300   330         9717        0.005    0.5 0.02  0.005 0.001 4.00  0.005
A001   330   360         9713        0.02     4.0 0.13  0.03  0.005 6.89  0.05
A001   360   391         9714        0.04    14.0 0.14  0.03  0.001 8.51  0.37
A001   391   397         9715        0.005    9.0 0.45  0.07  0.00141.30  0.005
A001   397   420         9716        0.05     9.0 0.17  0.03  0.001 6.79  0.05
A001   420   450         9717        0.03     0.5 0.05  0.02  0.001 3.95  0.02
A001   450   480         9718        0.005    0.5 0.05  0.02  0.001 3.66  0.02
A001   480   497         9719        0.02     0.5 0.12  0.005 0.001 2.11  0.02
A001   497   515         9720        0.02     0.5 0.03  0.02  0.001 5.96  0.005
A001   515   533         9721        0.02     0.5 0.04  0.02  0.001 3.06  0.02
R      533   540  :DYKE - NO SAMPLE
A001   540   570         9722        0.005    0.5 0.04  0.005 0.001 2.48  0.005
A001   570   591         9723        0.005    0.5 0.05  0.005 0.001 1.76  0.005
R      591   711  :DYKE - NO SAMPLE
A001   711   738         9724        0.005    0.5 0.04  0.005 0.001 1.92  0.03
A001   738   756         9725        0.005    0.5 0.07  0.005 0.001 2.41  0.03
A001   756   780         9726        0.02     2.0 0.14  0.03  0.001 6.43  0.03
A001   780   810         9727        0.005    0.5 0.14  0.005 0.001 2.13  0.005
A001   810   840         9728        0.06     2.0 0.09  0.02  0.001 2.47  0.02
A001   840   870         9729        0.02     2.0 0.48  0.005 0.001 2.55  0.005
A001   870   900         9730        0.005    3.0 0.05  0.02  0.001 2.93  0.02
A001   900   930         9731        0.005    2.0 0.07  0.02  0.001 2.68  0.02
A001   930   960         9732        0.005    2.0 0.54  0.02  0.001 3.92  0.02
A001   960   990         9733        0.07    11.0 0.08  0.04  0.09  8.54  0.04
A001   990  1020         9734        0.005    2.0 0.11  0.02  0.03  4.05  0.02
A001  1020  1050         9735        0.03    24.0 0.30  0.03  0.005 4.42  0.03
A001  1050  1080         9736        0.06    74.0 0.49  0.04  0.005 4.22  0.04
A001  1080  1089         9737        0.13   139.0 0.79  0.08  0.03  4.54  0.03
R     1089  1099  :DYKE - NO SAMPLE
```

A001	1099	1130	9738	0.15	69.0	0.38	0.07	0.04	7.55	0.04
A001	1130	1160	9799	0.06	100.0	0.57	0.04	0.005	2.97	0.03
A001	1160	1190	9740	0.07	110.0	0.76	0.05	0.03	4.12	0.04
A001	1190	1220	9741	0.11	95.0	0.60	0.05	0.005	3.35	0.05
A001	1220	1250	9742	0.12	110.0	0.62	0.03	0.005	3.74	0.19
A001	1250	1280	9743	0.08	47.0	0.62	0.03	0.04	4.90	0.50
A001	1280	1310	9744	0.05	14.0	0.59	0.02	0.02	4.71	0.07
A001	1310	1340	9745	0.05	22.0	0.55	0.02	0.001	3.02	0.07
A001	1340	1352	9746	0.31	19.0	0.40	0.03	0.02	4.40	0.06
A001	1352	1386	9747	0.06	6.0	0.12	0.02	0.005	2.56	0.02
A001	1386	1410	9748	0.02	6.0	3.10	0.005	0.005	2.45	0.03
A001	1410	1440	9749	0.04	36.0	0.35	0.02	0.005	2.43	0.04
A001	1440	1470	9750	0.04	8.0	0.18	0.02	0.005	3.80	0.05
A001	1470	1500	9751	0.03	10.0	0.37	0.02	0.005	2.44	0.02
A001	1500	1530	9752	0.06	17.0	18.80	0.02	0.006	3.17	0.05
A001	1530	1560	9753	0.11	9.0	1.15	0.02	0.02	4.42	0.10
A001	1560	1590	9759	0.10	39.0	0.57	0.005	0.005	2.50	0.07
A001	1590	1620	9755	0.06	20.0	0.43	0.02	0.02	3.27	0.04
A001	1620	1642	9756	0.08	40.0	1.05	0.02	0.02	2.53	0.04
R	1642	1821	:DYKE - NO SAMPLES							
A001	1821	1850	9757	0.03	11.0	0.10	0.005	0.02	4.32	0.10
A001	1850	1878	9758	0.02	8.0	0.13	0.005	0.005	3.60	0.03
A001	1878	1900	9759	0.005	0.5	0.03	0.005	0.001	1.91	0.01
A001	1900	1915	9760	0.005	2.0	0.10	0.005	0.005	3.29	0.01
A001	1915	1940	9761	0.005	1.0	0.01	0.005	0.005	2.07	0.01
A001	1940	1970	9762	0.005	1.0	0.03	0.005	0.001	1.78	0.01
A001	1970	1994	9763	0.005	0.5	0.02	0.005	0.005	1.92	0.01
A001	1994	2020	9764	0.05	5.0	0.08	0.005	0.005	2.98	0.02
A001	2020	2052	9765	0.04	8.0	0.06	0.02	0.01	4.17	0.04
A001	2052	2064	9766	0.08	5.0	0.12	0.005	0.01	3.47	0.01
R	2064	2195	:DYKE - NO SAMPLES							
A001	2195	2225	9767	0.08	3.0	0.07	0.005	0.005	1.82	0.02
A001	2225	2255	9768	0.10	7.0	0.11	0.005	0.01	2.90	0.03
A001	2255	2285	9769	0.14	11.0	0.16	0.01	0.05	5.40	0.03
A001	2285	2316	9770	0.14	7.0	0.24	0.005	0.04	3.50	0.01
A001	2316	2346	9771	0.33	12.0	0.36	0.02	0.03	4.25	0.03
A001	2346	2377	9772	0.12	5.0	0.16	0.005	0.02	3.88	0.01
A001	2377	2407	9773	0.22	97.0	2.35	0.02	0.03	4.33	0.07
A001	2407	2438	9774	0.20	27.0	0.29	0.03	0.04	3.86	0.03
A001	2438	2468	9775	0.10	5.0	0.11	0.005	0.04	4.35	0.01
A001	2468	2499	9776	0.30	9.0	0.17	0.005	0.06	4.62	0.02
A001	2499	2529	9777	0.38	15.0	0.36	0.02	0.07	4.98	0.02
A001	2529	2560	9778	0.30	12.0	0.24	0.02	0.11	3.98	0.02
A001	2560	2590	9779	0.34	49.0	1.44	0.04	0.14	3.86	0.04
A001	2590	2620	9780	0.25	33.0	0.66	0.04	0.11	3.85	0.02
A001	2620	2651	9821	0.08	28.0	0.33	0.03	0.04	2.40	0.02
A001	2651	2682	9822	0.04	34.0	0.42	0.005	0.02	2.51	0.02
A001	2682	2712	9823	0.03	18.0	0.23	0.005	0.02	3.44	0.02
A001	2712	2743	9824	0.16	32.0	0.48	0.005	0.03	3.02	0.02
A001	2743	2779	9825	0.11	13.0	0.21	0.005	0.04	3.63	0.02
A001	2779	2810	9826	0.22	50.0	0.62	0.005	0.005	2.35	0.02
A001	2810	2840	9827	0.0005	7.0	0.07	0.005	0.005	2.92	0.005
A001	2840	2870	9828	0.02	4.0	0.07	0.005	0.02	4.19	0.03
A001	2870	2900	9829	0.02	3.0	0.03	0.005	0.02	3.91	0.02
A001	2900	2930	9830	0.005	3.0	0.18	0.005	0.005	3.63	0.02

A001	2930	2953	9831	0.005	0.5	0.10	0.005	0.005	3.90	0.02
A001	2953	2980	9832	0.005	0.5	0.02	0.005	0.005	4.60	0.005
A001	2980	3010	9833	0.005	0.5	0.02	0.005	0.005	4.37	0.005
A001	3010	3031	9834	0.005	3.0	0.03	0.005	0.005	4.83	0.005
A001	3031	3053	9835	0.005	3.0	0.03	0.005	0.005	4.35	0.02
A001	3053	3078	9836	0.005	2.0	0.47	0.005	0.005	4.23	0.02
A001	3078	3108	9837	0.005	5.0	0.06	0.005	0.005	3.96	0.03
A001	3108	3139	9838	0.02	2.0	0.03	0.005	0.005	2.72	0.03
A001	3139	3165	9839	0.04	7.0	0.07	0.005	0.005	3.30	0.02
A001	3165	3180	9840	0.06	4.0	0.33	0.005	0.005	4.51	0.02
R	3180	3246	:GABBRO - NO SAMPLES							

```
IDEN6B0201       X87CH312 NQ   MAY87RBP   JTT MAY87ACK          0.0
IFRJ            EQUITY SILVER MINES LTD          MAIN ZONE - MN GEOCODE
S000   00    216 MT  350.5 090.0 -70.5                  7690.10   8448.30   1270.20
S001  216    625     350.5 090.9 -71.0
S002  625   1186     350.5 091.8 -71.0
S003 1186   1890     350.5 093.3 -70.5
S004 1890   2484     350.5 094.8 -70.5
S005 2484   3002     350.5 095.9 -70.0
S006 3002   3383     350.5 097.0 -69.5
S007 3383   3505     350.5 097.5 -69.5
/SCL         MT.2MT.2
LSCL             MT.2        LCTM
/NAM                                                            QZSZTOPYCPTTASPRGY
LNAM                                                            DMCBCLMGHESLGLMO
/       00     31          OVBN                  P
R                :TRICONED - NO CORE : BROKEN ROCK TO 3.1, NO TILL
/       31     69  32      2E41        <<        P BD    50<-<-   D=
L                  03          AT
R                :LOC 2C INTERLEVELED
/       69     94  26      2E41        <<BR      P          <-<-   <+
L                  06         7A
R                :LOC 2C + 2F
/       94    111  16      2E41        BR        P          V5     V4
L                  03          YA
R                :ESSENTIALLY ALL QTZ VEIN
/      111    145  32      2E41        <<BR      P          <-     D+   D?
L                  03         5A
R                :FAULT GOUGE AT 12.6 M, LOC 2C41
/      145    177  31      2F41        <<BR      P          <-Q.   D+
L                  09         5A                                   D.Q(
/      177    206  28      2F41        <<BR      P          <-Q-   Q+   <?
L                  09          TA                                  D(D*
/      206    221  14      2F41        <<BR      P            Q.   D(
L                  03         4A       BR
R                :INTENSE BR'X
/      221    288  64      8A00        <<CM      P              <(
L                  09         7G
R                :CONTACTS BROKEN
/      288    326  34      2E41        <<BR      P            Q-   D+   D?
L                  06         6A                                     D(
R                :LOC 2D
/      326    357  30      2E41        <<BR      P                 D)   D?
L                  09         GA                                #*D-D(
R                :LOC 2D & 2F, F/ GOUGE AT 35.0 & 35.6
/      357    388  31      2F41        BR<<      P          #-Q.   D)
L                  09         GA                              <.#)   D-
R                :LOC 2E41
/      388    425  35      2E41        <<BR      P          <-Q.   D)
L                  06         GA                                D*   <(
R                :SOME LAPILLI ALT'N TO SERICITE
/      425    456  15      8B00        P*        P                 D.
L                  03          AG                  CL     15     D+D.
/      456    484  28      2F11        BR<<      P BD    25<(      D*
L                  06         GA                                <*
R                :LOC 2E11, 2C11
```

```
/     484    516   31     2E11         <<RC          P            <-     D)
L                  06          GA                                     <)
R                 :LOC 2E41
/     516    542   27     2E11         <<RC          P            <-     D)
L                  04          AG                                     <)D.<(
R                 :LOC 2E41, 2C11. SOME LAPILLI ALT'N TO SERICITE
/     542    571   29     2E11         <<RC          P            <-     D*
L                  09          AG      AD                             <)  <(
R                 :LOC 2C11, MINOR SILICIFICATION
/     571    604   33     2E12         <<BR          P F/     25<-     D)D.
L                  09          AG                                     <(D-
R                 :LOC 2D, 2C. F/AT 58.8
/     604    621   17     2E11         <<BR          P            <(     D+D.
L                  03          TA                                     <(  D(D-
/     621    638          8B10         <<P*          P CU     20<*     D.
L                              AG                                     D+D.
R                 :CL REPLACING FELD PHENOS
/     638    663   25     2F11         BR<<          P            <-     <)
L                  06          TA                                        D.
/     663    697   30     2C41         <<            P            <*     <+
L                  05          5A                                     <*  <-
R                 :LOST CORE FROM 66.3 TO 66.7
/     697    719   22     2E41         <<            P            <-     <+
L            06           GA                                          <(  <*<-
R                 :SOME LAPILLI ALT'N TO SERICITE
/     719    752   32     2F41         <<BR          P            <-     D)
L                  03          GA                                     <*  <*<-
/     752    791   38     2E42         <<BR          P                   D)
L                  09          TG                                        #*<*
/     791    821   28     2F42         BRBR          P            <-     <*
L                  00          3A                 <<                     #(<-
R                 :VERY BROKEN
/     821    851   29     2F42         BR            P            <*     D*
L                  00          TA                                     #)#+#-
R                 :LAPILLI ALT'D TO SERICITE
/     851    887   20     2E42         <<            P            <-     <*
L                  00          5A                                     <)<(<-
R                 :VERY BROKEN, FEW PIECES OF 8B
/     887    917   29     2F42         BR<<          P            <-     D*
L                  03          GA                                     <)#2<-
R                 :ESSENTIALLY MASSIVE MAGNETITE FROM 90.7 TO 90.9
/     917    948   31     2F42         BR<<          P                   <*        <(
L                  12          AG                                     <(<+<(
/     948    978   30     2E42         <<BR          P BD     60         <*        <-
L                  21          AG                                        <+<-
R                 :LOC 2C42, MINOR BR'N
/     978   1008   30     2F42         BR<<          P               Q.  <)        <.
L                  18          AG                                     <*<+<.
R                 :SOME LAPILLI ALT'D TO SERICITE
/    1008   1035   27     2E42         BR<<          P               Q.  <)Q.Q?    <-
L                  11          TG                                     <)<*
R                 :LOC 2C42
/    1035   1037   02     8A00         CM            P CU     20<-
L                  00          4G                   CL     35
/    1037   1067   30     2F42         BR<<          P               Q.  <+
```

```
L                 12      GA                                         <+<(<-
/    1067  1098   31     2F42      BR<<        P           <-    <+Q.
L                 13      GA                                         <+<-<(
R                :SOME LAPILLI ALT'D TO SERICITE
/    1098  1128   30     2F54      BR<<        P           <-Q-  Q=Q-        <(
L                 09      GA                                         <+Q*
R                :AS ABOVE
/    1128  1158   30     2F54      BR<<        P           <.Q.  <)Q.Q?
L                 11      GA                                         <*<-
R                :AS ABOVE
/    1158  1188   30     2E52      <<BR        P           <*<-  Q+Q.
L                 09      GA                                         <-Q-
R                :MINOR BR'N
/    1188  1218   30     2F41      <<BR        P           <-Q-  <+D.
L                 09      GA                                         <)<-
/    1218  1248   30     2F41      <<BR        P           <-Q.  <)<.        <(
L                 13      GA                                         <*D-
/    1248  1278   30     2E41      <<BR        P           <-    <+          <(
L                 15      GA                                         <)<.
R                :LAPILLI INDISTINCT
/    1278  1308   29     2F11      <<BR        P           <*    <)
L                 09      AG                                         <+<.<(
/    1308  1337   27     2C42      <<BR        P           <-    Q+          <-
L                 06      AG                                         <+Q*<-
R                :LOC 2F42
/    1337  1342   05     8A00      <<          P CU    80                    <*
L                 03      6G                     CL    70    <*  <.
/    1342  1374   32     2F42      <<BR        P           <-Q.  Q_D-        <*
L                 16      GA                                         <)Q*
R                :LOC 2E42
/    1374  1417   42     8B10      <<P*        P CU    35<-                  <*
L                 21      6G                     CL    30    D+D-
R                :FELDSPAR PHENOS ALT'D TO CL
/    1417  1439   21     2C11      BR<<        P                 <*          <-
L                 03      GT                                         <+  <-
/    1439  1473   34     8A00      CM          P CU    20                    <*
L                 19      6G                                             <(
/    1473  1503   30     2C42      <<          P           <-    Q+          <-
L                 09      GA                                         <)Q*<-D-
R                :GRADES INTO 2D
/    1503  1540   36     2D42      <<          P           <-    <+D.
L                 17      GA                                         <*<-<(<<(
/    1540  1568   22     8A11      <<          P                 D(          <-
L                 00      8G                                         <*
R                :VERY BROKEN, POOR RECOV.
/    1568  1603   33     8A11      <<CM        P CU    30      D-
L                 14      TG                     CL    25    <+  <-
R                :BLEACHING ON <<'S
/    1603  1621   16     2D11      <<          P           <-    D*          <-
L                 00      AG                                         <)  <(
/    1621  1635   13     8C01      <<CM        P                 D.
L                 06      AW                     CL    60    <(
R                :UPPER C/ FAULTED
/    1635  1657   20     2D41      BR<<        P           <(    <*          <.
L                 00      GA                                         <*  <-
```

```
R                   :ASSIMILATED BC, BR'D
/    1657   1684   27     2D42        <<BR          P           <-     D+          <(
L                  09        AG                                     <*D-
R                   :MINOR BR'N
/    1684   1733   48     8A00        <<CM          P CU     55<-      D.          <-
L                  32        5G                       CL     45     <(D.
R                   :BOTH C/'S FAULTED
/    1733   1770   33     2D42        <<BR          P           <-Q.   D+          <-
L                  09        GA                                     <*D-D(
/    1770   1803   33     2E52        <<BR          P              Q-  D=          <-
L                  11        AG                                     <(D*
/    1803   1895   90     8A00        <<            P CU     65        D.          <(
L                  38        6G                                         <-
/    1895   1901   06     2F75        <<            P                   D2D)    D=
L                  03        4A                                         D1D+
R                   :SUSPECT XENOLITH IN DYKE, ESSENTIALLY MASSIVE SULPHIDE
/    1901   1937   35     8A00        <<CM          P                                  <*
L                  06        6G                       CL     55
/    1937   1959   21     2E52        <<BR          P                     Q+
L                  09        4A                                     <-D(<-
/    1959   1993   33     2F52        <<BR          P              Q-  D+  D?      <-
L                  07        4A                                     <-D-
R                   :LAST TWO INTERVALS SHOULD CARRY GOOD SILVER
/    1993   2021   28     2D51        <<BR          P                   D)D.        <(
L                  09        4A                                         D.
R                   :GRADES INTO 2F51
/    2021   2045   24     2F52        <<BR          P              Q.  D+          <(
L                  07        TA                                         D(  D.
R                   :LOC 2F56
/    2045   2074   29     2E11        <<            P BD     60<-      D)          <(
L                  11   GA                                          <*
R                   :LOC 2D11
/    2074   2106   32     2E56        <<BR          P           <-     D+Q-        <(
L                  12        GA                                     <*
R                   :LOC 2D51, GRADES INTO 2F AT EOI
/    2106   2140   34     2D52        <<BR          P F/     35   Q.   D+          <-
L                  20        GA                                     <(D-
R                   :F/ GOUGE FROM 210.6 TO 210.9 LOC 2F52
/    2140   2164   24     8D42        <<            P BN     55        D+          <*
L                  11        AG                                     <*D-<(
R                   :SOME CL REPLACING PHENOS
/    2164   2186   22     2E52        <<BR          P           <-Q-   D+D.        <(
L                  09        GA                                     <(D(<-
R                   :MINOR ASSIMILATED 8B, LOC 2D52
/    2186   2257   72     8B00        <<CM          P CU     25<-      D.
L                  49        4G                       CL     30     <-D.
/    2257   2272   15     2E51        <<            P           <-     D+
L                  00        4A                                     <-D.
/    2272   2292   20     8A00        <<            P CU     40<-      D-          <(
L                  06        5G                                     <*D.
R                   :MINOR ASSIMILATED 2E?
/    2292   2322   30     2D52        <<            P           <-     D+D.        <-
L                  06        4A                                     <(D(
R                   :LOC 2E52
/    2322   2353   31     2D53        <<            P           <*     <=<(     <*<.
```

```
L                 09        4A                                      <-<-
R                :LOC 2E53, SHOULD RUN GOOD SILVER
/    2353  2385  31      2D53        <<          P            <-     <+<.     <-
L                 09        4A                                      <-<.  <-
R                :LOC 2C81 TOWARDS EOI
/    2385  2412  26      2C41        <<<<        P                   <)
L                 00        TA                                      <)      <.
/    2412  2435  23      2D53        <<          P                   <+<*<?  <(<-
L                 10        4A                                      <*    <-
R                :LOC 2E53, SHOULD BE GOOD GRADE
/    2435  2461  26      2E53        <<          P BN      40<(      <=Q*     <*
L                 09        3A                                      <*<-<-D.
R                :LAPILLI INDISTINCT
/    2461  2484  23      2C51        <<<<        P            <(     D=
L                 09        4A                                      <)
R                :MINOR 2D
/    2484  2491  06      8B00        <<          P            <-     D.
L                 00        6G                                      <-D.
R                :CONTACTS NOT PRESERVED
/    2491  2511  20      2F53        <<          P            <-     <)
L                 06        6A                                      <*      <(
/    2511  2533  22      2D53        <<BR        P               <+Q.  D+D-     D)
L                 09        3A                                         D-  D-
/    2533  2557  24      2C51        <<          P               <(    <)<.
L                 11        4A                                        <*
/    2557  2560  03      8B00        P*CM        P CU      40
L                 03        3G                     CL      50          D-
/    2560  2567  06      2C51        <<          P               Q(   D)
L                 00        3A
/    2567  2583  15      8B00        <<P*        P CU      30<-
L                 00        6G          CM         CL      20      <)D-<-
/    2583  2613  29      2C51        <<BR        P                   <+,.       <-
L                 03        3A                                      <*D.<.<-
R                :MINOR BR'N
/    2613  2630  10      8B10        P*          P                   D.
L                 00        2G                                      D)D.
R                :VERY BROKEN, POOR RECOV. CL REPLACING FELDSPAR PHENOS
/    2630  2660  29      2C56        <<          P                   D+D-     D.
L                 06        3A                                       D.  D.
/    2660  2694  32      2C53        <<          P            <-     D+D.     D.
L                 16        3A                                      <*<-  D(
R                :LOC 2D53
/    2694  2728  33      2E53        <<BR        P            <(     D+<(     D*
L                 12        3A                                      <*D.  <)
R                :8A FROM 271.2
/    2728  2761  32      2C51        <<                       <*     <+D.<.
L                 18        4A       <<          P                  <*
R                :LOC 2E51
/    2761  2791  30      8A00        <<          P CU      10        D.
L                 11        6G                     CL      10      <-D.
/    2791  2835  42      2C41        <<          P                   <)
L                 18        4A                                      <)
R                :LOC 2E
/    2835  2865  29      2C41        <<          P            <-     <)
L                 09        3A                                      <+<*
```

```
R                :STARTING HEAVY CL-MG <<'ING
/    2865  2895  30    2C41       <<          P                <*
L                06        GA                                 <+<)
R                :AS ABOVE
/    2895  2925  30    2C41       <<<<        P                <(
L                09        3A                                 <)<+
R                :MINOR SERICITE ALT'N ON <<'S
/    2925  2955  30    2C41       <<<<        P          <-    <)
L                11        3A                                 <)<+
R                :AS ABOVE
/    2955  2985  30    2C41       <<<<        P          <*    <)<.     <-
L                11        3A                                 <)<+
R                :GRADES INTO 2D41
/    2985  3016  30    2D43       <<          P          <-    <+<.
L                15        GA                                 <)<*  <-
R                :GRADES INTO 2C41
/    3016  3046  30    2C56       <<          P          <*    D+<-     D*
L                12        3A                                 <(D.  <*
/    3046  3076  30    2E46       <<          P                D+Q-     D*
L                15        3A                                 <(D*  <-
R                :GRADES INTO 2E41
/    3076  3106  30    2E53       <<          P          <-    D+<-     D(
L                16        3A                                 <(<-  <-
/    3106  3131  25    2D51       <<BR        P          <(    Q+D.     D-
L                11        4A                                 <)#1
R                :VERY BR'D
/    3131  3154  22    2D41       <<          P                <)       <.
L                10        GA                                 <+D.
/    3154  3189  35    7C11       <<P*        P          <-    D*D.
L                21        GA                                 <(D.<-
R                :ASSIMILATION OF TUFF AND GABBRO
/    3189  3220  30    2E11       <<          P          <-    D)
L                19        AG                                 <)D.
R                :MINOR 7C11
/    3220  3245  25    2E11       <<          P          <-    D)
L                09        AG                                 <+D.
R                :AS ABOVE
/    3245  3277  31    2E41       <<          P          <(    <*
L                13        AG                                 <+
/    3277  3403 125    8A00       <<CM        P CU   060<-     D.
L                81        7G                   CL   040       D.<-
R                :MINOR XENOLITHS OF 2E11 AT 335.2 AND 339.8 M.
/    3403  3411  08    7C00       P*          P          <-
L                06        AG                                  D-
/    3411  3453  42    2E41       <<          P          <-    D*
L                28        AG                                  D-
R                :ASSIMILATION OF TUFF AND GABBRO - CONTACT HORNFELS
/    3453  3505  52    7C00       P*          P          <-
L                33        AG                                  D-
R                :TYPICAL MEDIUM GRAINED MONZONITE.
R                :END OF HOLE @ 350.5 M.
A001
ALAB             EQUITY MINESITE LABORATORY
ATYP             ASSAY
AMTH             WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
```

AUMM			RCOVSAMPLE	RQD % CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	31	:TRICONED - NO CORE, BROKEN ROCK - NO RECOVERY							
A001	31	69	9656	0.005	4.0	0.13	0.005	0.005	2.88	0.03
A001	69	94	9657	0.001	2.0	0.06	0.005	0.005	4.42	0.005
A001	94	111	9658	0.001	6.0	0.15	0.02	0.005	29.70	0.005
A001	111	145	9659	0.001	28.0	0.29	0.005	0.005	2.71	0.07
A001	145	177	9660	0.02	35.0	0.34	0.005	0.005	3.81	0.03
A001	177	206	9661	0.03	91.0	0.49	0.02	0.005	7.82	0.02
A001	206	221	9662	0.001	3.0	0.25	0.005	0.005	3.69	0.005
R	221	288	:DYKE - NO SAMPLES							
A001	288	326	9663	0.20	111.0	0.84	0.07	0.005	3.54	0.07
A001	326	357	9664	0.04	54.0	1.46	0.02	0.03	5.34	0.12
A001	357	388	9665	0.04	18.0	0.21	0.005	0.005	3.37	0.07
A001	388	425	9666	0.02	32.0	0.39	0.005	0.005	3.53	0.04
R	425	456	:DYKE - NO SAMPLES							
A001	456	484	9667	0.005	0.5	0.04	0.005	0.001	2.86	0.02
A001	484	516	9668	0.005	0.5	0.16	0.005	0.001	2.59	0.02
A001	516	542	9669	0.005	0.5	0.63	0.005	0.001	2.27	0.02
A001	542	571	9670	0.005	0.5	0.07	0.005	0.001	2.18	0.005
A001	571	604	9671	0.005	0.5	0.04	0.005	0.001	2.83	0.02
A001	604	621	9672	0.04	7.0	0.18	0.02	0.005	5.11	0.2
R	621	638	:DYKE - NO SAMPLES							
A001	638	663	9673	0.005	0.5	0.38	0.005	0.005	2.46	0.09
A001	663	697	9674	0.005	5.0	0.19	0.02	0.001	2.26	0.05
A001	697	719	9675	0.005	2.0	0.10	0.005	0.001	2.47	0.20
A001	719	752	9676	0.005	0.5	0.13	0.02	0.001	2.49	0.07
A001	752	791	9677	0.005	0.5	0.71	0.005	0.001	2.91	0.03
A001	791	821	9678	0.005	0.5	0.32	0.005	0.001	3.09	0.03
A001	821	851	9679	0.005	0.5	0.04	0.005	0.001	2.33	0.04
A001	851	887	9680	0.005	3.0	0.76	0.005	0.001	2.15	0.06
A001	887	917	9681	0.005	2.0	0.07	0.02	0.001	4.25	0.04
A001	917	948	9682	0.005	4.0	0.10	0.02	0.02	5.01	0.05
A001	948	978	9683	0.08	40.0	0.87	0.02	0.001	2.76	0.06
A001	978	1008	9684	0.03	8.0	0.12	0.02	0.001	3.14	0.07
A001	1008	1035	9685	0.03	16.0	0.12	0.02	0.001	2.72	0.05
R	1035	1037	:DYKE - NO SAMPLES							
A001	1037	1067	9686	0.005	5.0	0.30	0.02	0.005	3.45	0.04
A001	1067	1098	9687	0.10	35.0	0.27	0.02	0.02	5.82	0.09
A001	1098	1128	9688	0.14	46.0	0.35	0.03	0.005	4.08	0.07
A001	1128	1158	9689	0.07	32.0	0.53	0.03	0.03	4.87	0.09
A001	1158	1188	9690	0.09	29.0	0.17	0.03	0.03	4.94	0.09
A001	1188	1218	9691	0.13	39.0	0.27	0.02	0.09	5.42	0.04
A001	1218	1248	9692	0.08	44.0	0.24	0.02	0.005	3.45	0.37
A001	1248	1278	9693	0.12	31.0	0.32	0.02	0.005	3.85	0.05
A001	1278	1308	9694	0.02	17.0	0.24	0.005	0.005	2.94	0.08
A001	1308	1337	9695	0.14	84.0	1.37	0.005	0.005	4.83	0.18
R	1337	1342	:DYKE - NO SAMPLES							
A001	1342	1374	9696	0.15	46.0	0.26	0.005	0.005	3.66	0.03
R	1374	1417	:DYKE - NO SAMPLES							
A001	1417	1439	9697	0.005	4.0	0.14	0.005	0.005	1.79	0.005
R	1439	1473	:DYKE - NO SAMPLES							
A001	1473	1503	9698	0.14	48.0	1.30	0.005	0.005	2.57	0.19
A001	1503	1540	9699	0.58	80.0	0.30	0.03	0.05	5.79	1.02
R	1540	1603	:DYKE - NO SAMPLES							
A001	1603	1621	9700	0.03	10.0	0.49	0.001	0.005	2.40	0.03

R	1621	1635	:DYKE - NO SAMPLES							
A001	1635	1657	9781	0.02	9.0	0.20	0.005	0.005	2.54	0.03
A001	1657	1684	9782	0.02	8.0	0.12	0.005	0.005	3.10	0.03
R	1684	1733	:DYKE - NO SAMPLES							
A001	1733	1770	9783	0.001	3.0	0.40	0.005	0.02	4.57	0.06
A001	1770	1803	9784	0.005	4.0	0.14	0.005	0.03	4.46	0.05
R	1803	1895	:DYKE - NO SAMPLES							
A001	1895	1901	9785	0.03	5.0	0.60	0.02	0.23	25.40	0.04
R	1901	1937	:DYKE - NO SAMPLES							
A001	1937	1959	9786	0.005	9.0	0.78	0.005	0.02	5.64	0.04
A001	1959	1993	9787	0.005	5.0	0.16	0.005	0.005	2.78	0.04
A001	1993	2021	9788	0.005	6.0	0.52	0.005	0.005	3.16	0.02
A001	2021	2045	9789	0.03	13.0	0.45	0.005	0.005	3.93	0.02
A001	2045	2074	9790	0.02	4.0	0.06	0.005	0.005	3.23	0.06
A001	2074	2106	9791	0.39	9.0	0.38	0.02	0.02	4.98	0.11
A001	2106	2140	9792	0.13	8.0	0.26	0.02	0.05	4.17	0.04
A001	2140	2164	9793	0.03	3.0	0.02	0.02	0.001	2.90	0.02
A001	2164	2186	9794	0.13	10.0	0.23	0.02	0.005	4.35	0.03
R	2186	2257	:DYKE - NO SAMPLES							
A001	2257	2272	9795	0.29	87.0	3.86	0.05	0.07	4.94	0.02
R	2272	2292	:DYKE - NO SAMPLES							
A001	2292	2322	9796	0.08	5.0	0.95	0.03	0.001	2.87	0.04
A001	2322	2353	9797	0.26	9.0	0.31	0.04	0.03	4.25	0.02
A001	2353	2385	9798	0.16	9.0	0.17	0.03	0.005	3.05	0.04
A001	2385	2412	9799	0.12	26.0	0.48	0.02	0.005	2.11	0.05
A001	2412	2435	9800	0.26	38.0	0.21	0.03	0.03	4.12	0.11
A001	2435	2461	9801	0.34	26.0	1.34	0.03	0.04	4.78	0.04
A001	2461	2484	9802	0.27	30.0	4.55	0.05	0.02	4.08	0.05
R	2484	2491	:DYKE - NO SAMPLES							
A001	2491	2511	9803	0.08	8.0	0.36	0.02	0.005	2.14	0.09
A001	2511	2533	9804	0.29	8.0	0.67	0.03	0.07	6.39	0.12
A001	2533	2557	9805	0.09	2.0	0.07	0.005	0.04	2.86	0.02
R	2557	2560	:DYKE - NO SAMPLES							
A001	2560	2567	9806	0.37	25.0	0.89	0.03	0.05	3.37	0.07
R	2567	2583	:DYKE - NO SAMPLES							
A001	2583	2613	9807	0.26	6.0	0.21	0.02	0.03	3.31	0.05
R	2613	2630	:DYKE - NO SAMPLES							
A001	2630	2660	9808	0.25	3.0	0.10	0.02	0.005	3.60	0.03
A001	2660	2694	9809	0.17	5.0	0.07	0.005	0.03	4.04	0.06
A001	2694	2728	9810	0.08	11.0	0.07	0.03	0.02	4.42	0.75
A001	2728	2761	9811	0.06	10.0	0.05	0.02	0.05	4.07	0.04
R	2761	2791	:DYKE - NO SAMPLES							
A001	2791	2835	9812	0.03	9.0	0.03	0.02	.03	4.11	0.02
A001	2835	2865	9813	0.005	0.5	0.11	0.005	0.001	4.82	0.005
A001	2865	2895	9814	0.005	0.5	0.28	0.02	0.001	3.92	0.005
A001	2895	2925	9815	0.005	0.5	0.02	0.005	0.001	2.83	0.001
A001	2925	2955	9816	0.005	0.5	0.01	0.005	0.001	3.06	0.001
A001	2955	2985	9817	0.02	2.0	0.04	0.005	0.02	3.68	0.03
A001	2985	3016	9818	0.005	0.5	0.02	0.005	0.005	3.07	0.005
A001	3016	3046	9819	0.10	13.0	0.10	0.005	0.005	3.40	0.55
A001	3046	3076	9820	0.11	18.0	0.07	0.005	0.02	4.00	0.25
A001	3076	3106	9901	0.06	11.0	0.16	0.005	0.001	3.81	0.04
A001	3106	3131	9902	0.03	9.0	0.03	0.005	0.001	4.47	0.02
A001	3131	3154	9903	0.01	7.0	0.09	0.005	0.001	4.51	0.01
A001	3154	3189	9904	0.04	11.0	0.11	0.005	0.001	2.56	0.02

A001	3189	3220		9905	0.05	15.0	0.05	0.005	0.001	3.87	0.04
A001	3220	3245		9906	0.06	8.0	0.06	0.005	0.001	3.44	0.04
A001	3245	3277		9907	0.02	5.0	0.03	0.005	0.001	4.16	0.03
R	3277	3403	:DYKE - NO SAMPLES								
R	3403	3411	:GABBRO - NO SAMPLES								
A001	3411	3453		9908	0.06	101.0	1.00	0.005	0.001	4.161	0.03
R	3453	3505	:GABBRO - NO SAMPLES								
R			:END OF HOLE @ 350.5								

```
IDEN6B0201      X87CH313 NQ   MAY87RBP   JTT MAY87ACK           0.0
IPRJ           EQUITY SILVER MINES LTD        MAIN ZONE - MN GEOCODE
S000   00    157 MT   52.7 090.0 -60.5              7879.80   8386.70   1270.80
S001  157    527      52.7 090.0 -60.0
/SCL         MT.2MT.2
LSCL            MT.2        LCTM
/NAM                                                       QZSZTOPYCPTTASPRGY
LNAM                                                       DMCBCLMGHESLGLMO
/      00     30         OVBN               P
R                   :TRICONED - NO CORE, CASING THRU BROKEN ROCK
/      30     61         OVBN               P
R                   :CORED BOULDERS
/      61     91    25   2F43        BR<<       P          <)   #2#-
L                   00        6A                              <*     #+
/      91    127    31   2F43        BR<<       P          <)  D*<+
L                   06        GA                              <)     D-
R                   :POSSIBLE MYLONITE?
/     127    152    15   8C00        P*         P          <-   D.
L                   00        AW                              <-
R                   :NO CONTACTS PRESERVED
/     152    182    25   2F41        BR<<       P          #)   <+<.
L                   00        GA                              <*
/     182    212    25   2F41        BR<<       P          <-   D*
L                   00        4A                              <-
R                   :VERY BROKEN, CLAY GOUGE AT 18.9
/     212    242    27   2F41        BR<<       P          <*   D*
L                   00        6A
/     242    272    26   2F41        BR<<       P          <-  D?D*
L                   00        GA                              <(
R                   :TINY BLACK RECTANGLUAR PHENOS TO TO?
/     272    302    27   2F11        BR<<       P          <(   D*
L                   00        6A                              <*
/     302    338    31   2F41        BR<<       P          <-   D*
L                   00        5A                              <(
R                   :CLAY GOUGE AT 30.5 M
R                   :DRILLERS ADVANCED CASING TO 30.5 M
/     338    368    25   2F11        BR<<       P          <-   D*
L                   00        5A                              <(
R                   :LOC 2F41
/     368    396    25   2F11        BR<<       P          <(   D)
L                   00        4A                              <(
R                   :LOC 2F81
/     396    426    27   2F11        BR<<       P          <(   D)
L                   00        4A                              <(
R                   :LOC 2F81, CLAY GOUGE AT 41.1 M
/     426    457    20   2F11        BR<<       P          <-   D*
L                   00        6A                              <-
R                   :CLAY GOUGE AT 46.9 M
/     457    487    22   2F11        BR<<       P          <(   D*
L                   00        6A                                <(
/     487    527    31   2F11        BR<<       P          <-   D*
L                   00        6A                              <(
R                   :LOC 2F41
R                   :DRILLERS ADVANCED CASING TO 45.7 M, BUT THE HOLE CONTINUED TO
R                   :SQUEEZE THE RODS. THEREFORE, HOLE ABANDONED AT 52.7 M
```

R			:END OF HOLE AT 52.7 M								
A001											
ALAB			EQUITY MINESITE LABORATORY								
ATYP			ASSAY								
AMTH			WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST								
AUMM			RCOVSAMPLE	RQD	% CU	G/TAG	G/TAU	% SB	% AS	% FE	% ZN
R	00	30	:TRICONED - NO CORE, CASING THRU BROKEN ROCK								
R	30	61	:CORED BOULDERS, EXTREMELY POOR RECOVERY - NO SAMPLE								
A001	61	91	9909		0.08	75.0	0.40	0.005	0.001	4.55	21.00
A001	91	127	9910		0.005	15.0	0.15	0.005	0.001	4.54	0.15
R	127	152	:DYKE - NO SAMPLE								
A001	152	182	9911		0.05	208.0	0.10	0.03	0.001	5.21	0.06
A001	182	212	9912		0.005	5.0	0.02	0.005	0.001	1.75	0.05
A001	212	242	9913		0.005	3.0	0.32	0.005	0.001	1.44	0.04
A001	242	272	9914		0.005	2.0	0.15	0.005	0.001	1.63	0.06
A001	272	302	9915		0.005	0.5	0.03	0.005	0.001	2.29	0.04
A001	302	338	9916		0.005	2.0	0.04	0.005	0.001	1.34	0.05
A001	338	368	9917		0.005	2.0	0.04	0.005	0.001	1.68	0.03
A001	368	396	9918		0.005	3.0	0.10	0.005	0.001	1.64	0.02
A001	396	426	9919		0.005	0.5	0.05	0.005	0.001	1.93	0.03
A001	426	457	9920		0.005	2.0	0.02	0.005	0.001	1.73	0.40
A001	457	487	9921		0.005	3.0	0.05	0.005	0.001	1.70	0.02
A001	487	527	9922		0.005	2.0	0.05	0.005	0.001	1.65	0.05
R			:END OF HOLE @ 52.7 M								

```
IDEN6B0201       X87CH314 NQ   MAY87RBP   JTT MAY87ACK          0.0
IPRJ           EQUITY SILVER MINES LTD        MAIN ZONE - MN GEOCODE
S000   00    229 MT  320.0 090.0 -71.0              7930.70   8434.00   1260.00
S001  229    625     320.0 090.0 -71.0
S002  625   1140     320.0 090.0 -71.0
S003 1140   1841     320.0 090.0 -72.5
S004 1841   2437     320.0 090.0 -71.0
S005 2437   2848     320.0 090.0 -72.0
S006 2848   3200     320.0 090.0 -71.0
/SCL         MT.2MT.2
LSCL              MT.2       LCTM
/NAM                                                       QZSZTOPYCPTTASPRGY
LNAM                                                       DMCBCLMGHESLGLMO
/      00     91         OVBN                P
R                  :TRICONED - NO CORE, BROKEN ROCK - NO TILL
/      91    140   40    8B80        P*      P          <-
L                  00        5A
R                  :ALL FELDSPAR PHENOS ALT'D TO SERICITE
/     140    143   02    2F11        <<BR    P          <-    D*
L                  00        GA
/     143    183   00    NREC                P
/     183    234   25    2F11        BR<<    P          <(    D(
R                  :CLAY GOUGE AT 20.5 M
/     234    260   20    2G01        <<      P                D(
L                  00        TA
R                  :CLAY GOUGE AT 23.8 M
/     260    300   30    2H01        <<      P          <-    D*
L                  00        6A
/     300    354   32    2F01        <<BR    P          <-    D)
L                  00        4A
/     354    384   30    2H01        <<      P          <*    D*        <*
L                  06        GA                            <-
R                  :LOC 2G11
/     384    414   28    2G01        <<      P          <(    D(        <*
L                  09        GA                            <-
R                  :LOC 2G11
/     414    449   34    2H01        <<      P BD    40<(     D(        <)
L                  09        GA                            <-
R                  :LOC 2G
/     449    480   30    2H01        <<      P BD    35<-    <*         <-
L                  14        4A                            <-
R                  :LOC 2G
/     480    514   33    2H01        <<      P BD    35<-    <*         <(
L                  09        GA
R                  :LOC 2G
/     514    546   31    2H01        <<BR    PP BD   40<-    <(         <*
L                  11        GA                            <*
R                  :LOC 2G, CONSIDERABLE BR'N
/     546    575   28    2E11        <<BR    P          <-    <)
L                  17        AG                            <)
/     575    604   29    2E21        <<BR    P          <(<-  <+
L                  10        AG                            <)
/     604    617   13    8B00        <<P*    P CU    70<-
L                  06        6G      CM        CL    75     D.
/     617    653   35    2E42        <<BR    P          <-Q.  D+        <-
```

L			11		AG					<)D-Q-	
/	653	661	08	8B00		<<P*	P CU	50<-			
L			03		6G	CM	CL	30		D.	
/	661	691	30	2E42		<<BR	P		<(Q.	<+	<-
L			10		AG					<+Q-Q(	
/	691	717	26	2E12		<<	P		<-	<+D.	<(
L			09		AG					<+D(Q-	
/	717	744	26	2E43		<<	P		<-	D+D(	
L			09		AG					<)D-Q-<(	
R			:LOC 2C83								
/	744	773	29	2E11		<<	P		<-	D+	
L			06		AG					<+ D*	
/	773	800	27	2E11		<<BR	P		<-	D)	<-
L			15		AG					<+	
/	800	830	30	2F12		<<BR	P		<-	D)	<-
L			12		AG					<+D-D-	
/	830	860	30	2F12		BR<<	P		<(	D+	<-
L			15		AG					<+D(<(	
/	860	890	30	2E11		<<	P BN	55<-		D)	<(
L			09		AG					<)	
R			:LOC 2H, 2G								
/	890	920	30	2F11		BR<<	P		<(	<*	<(
L			16		AG					<=	
R			:SOME FRAG UP TO 0.2 M DIAMETER								
/	920	950	30	2F11		BR<<	P		<-	<+	<*
L			12		AG					<)D.D-	
R			:LOC 2F42								
/	950	983	32	2F11		BR<<	P		<-	D)	<(
L			06		AG					<)D.	
R			:CONTAINS TWO 0.2 M 8A'S								
R			:FAULT GOUGE AT 97.4 M								
/	983	1014	10	8A00			P			D.	
L			00		5G					D.	
R			:EXTREMELY BROKEN								
/	1014	1043	27	2F11		BR<<	P		<-	D+	<-
L			06		AG					<+D-D.	
R			:LOC 2F52								
/	1043	1072	27	2F11		BR<<	P		<-	D)	<(
L			09		GA					<) D-	
R			:FAULT GOUGE AT 106.2 M								
/	1072	1101	28	2F12		BR<<	PP		<-	<+	<-
L			06		AG					<+<(<-	
/	1101	1135	33	2F11		BR<<	P		<-	<+<.	<-
L			11		AG					<)D-D-<(	
R			:PATCH OF 2F53 AT 112.8								
/	1135	1170	34	2F12		BR<<	P		<)	Q+Q-	
L			06		GA					<)Q(Q(Q.	
R			:LOC 2F42								
/	1170	1197	20	8A00			P		<-	D-	
L			00		6G					D.	
R			:EXTREMELY BROKEN								
/	1197	1238	40	2F12		BR<<	P		<-	<+	<-
L			11		GA					<*<(	
R			:LOC 2F42								
/	1238	1421	81	8C00		P*CM	P CU	40		D.	

```
L                35       GW                   CL    50
R               :WHITE PLAG PHENOS TO SOME ALT'D TO SERICITE
/    1421  1437  15     2411       <<         P               <-
L                03       GA                                 <*
R               :MINOR 8B INTERCLATED NEAR TOI
/    1437  1470  22     8B10       P*CM       P CU    45      D.
L                09       4G                   CL    50    D-
/    1470  1505  30     2E11       <<         P               D*
L                03       AG                                 <*D.D-
R               :LOC 2E12, MINOR INTERCALATED 8A, VERY BROKEN
/    1505  1524  15     2F12       <<BR       P               D)
L                00       AG                                  D*D(
R               :VERY BROKKEN, MOST PY-MG AT 150.9
/    1524  1554  20     2C11       <<         P               <*
L                00       TA                                 <*
R               :EXTREMELY BROKEN
/    1554  1585  25     2F11       <<BR       P               <*
L                00       6A
R               :EXTREMELY BROKEN, INTERCALATED 8B, LOC 2F41
/    1585  1615  25     2F11       <<         P          <-   D)         <-
L                03       GA                                 <*  Q-
/    1615  1645  29     2C11       <<         P          <(   <*         <-
L                03       TA                                 <)
/    1645  1681  35     2F42       <<BR       P          <-   <+
L                10       GA                                 <)<*<(
/    1681  1691  10     8A00       <<         P BN    40<-
L                06       8G                   C/    40
/    1691  1737  43     2F12       <<BR       P          <(   Q=         <(
L                11       GA                                 <*Q)Q*
/    1737  1810  71     8C00       P*CM       P CU    40      D.
L                25       GW                   CL    50
/    1810  1832  20     8A00       <<CM       P CU    50      D-
L                05       5G                                  D.
/    1832  1862  30     2F12       <<BR       P          <-   <+         <-
L                09       AG                                 <)<-<*
/    1862  1892  30     2E11       <<         P          <-   <)         <*
L                06       AG                                 <+<.<*
R               :LOC 2D11
/    1892  1920  28     2F11       <<BR       P          <-   D*         <(
L                09       AG                                 <+
R               :RELATIVELY COARSE GRAINED
/    1920  1958  37     2E11       <<BR       PP         <(   D*         <*
L                09       AG                                 <+  <.
R               :LOC 2F11
/    1958  1984  25     2F11       <<BR       P          <-   D)         <)
L                06       AG                                 <)<.
R               :INTERCALATED 8B, 50%
/    1984  2027  42     8A00       <<         P CU    50<-    D-         <-
L                21       5G                                  D.
R               :LOWER C/ BR'D
/    2027  2057  30     2F42       <<BR       P          <-   Q+       Q*<*
L                12       AG                                 <)Q-
R               :ALL PR IN Q AT 205.5 M.., SOME INTERCALATED 8A
/    2057  2089  31     2F42       <<BR       P          <(   Q)         <-
L                15       AG                                 <*Q-
```

```
/    2089  2119  30   2F11     <<BR      P          <-    Q+        <-
L                09       AG                              <)
/    2119  2150  31   2F11     <<BR      P          <-    D*        <-
L                15       AG                              <)D.
R                :INTERCALATED 8B, 20%
/    2150  2183  31   2F42     <<BR      P          <-    Q+        <-
L                06       GA                              <(Q(Q-
R                :INTERCALATED 8B, 10%
/    2183  2213  30   2E11     <<BR      P          <-    D(        <*
L                11       GA
/    2213  2256  40   2F11     <<BR      P          <-    D*        <)
L                11       GA                              <(
/    2256  2286  30   2E12     <<        P                Q+        <*
L                12       AG                              <*Q-Q(
R                :LOC 2E42
/    2286  2316  30   2F11     <<BR      P          <-    <*        <*
L                15       AG                              <(
R                :SOME ASSIMILATED 8B
/    2316  2346  29   2E42     <<        P          <-    Q+        <*
L                13       AG                              <*Q(
/    2346  2372  26   2F41     <<BR      P BD   50M(Q.    <)        <*
L                11       AG                              <(Q-
R                :INTERLEVELED 2H
/    2372  2392  20   2F54     <<BR      P                Q1Q)      Q)<(
L                11       4A                              Q)
R                :ALL CP & PR IN Q FROM 237.2 TO 237.6 M
/    2392  2403  11   8A00     <<CM      P CU   50<(      D.        <-
L                11       6G               CL   45        D.
/    2403  2438  34   2F52     <<BR      P          <-Q.  Q1        <-
L                15       4A                              Q*  Q(
/    2438  2469  31   2E52     <<        P          <(    <+        <.
L                10       3A                              <*<-
/    2469  2504  33   2E52     <<        P          <-Q-  <+        <.
L                11       3A                              <(<(
/    2504  2535  31   2E52     <<BR      P BD   50        Q=Q(      Q*<.
L                09       3A                              Q-
/    2535  2569  33   2F52     <<BR      P          <-    Q+        <.
L                19       GA                              Q-
/    2569  2605  35   2E52     <<RC      P          <-Q-  <+<.
L                21       3A                              <*
/    2605  2634  29   8B00     <<P*      P CU   60<-      D.        <*
L                15       5A               CL   55        D*
/    2634  2664  30   2E52     <<BR      P          <*Q.  Q=Q.
L                17       3A                              Q-
/    2664  2687  22   2F53     <<BR      P          <(    <=        <)
L                06       3A                              Q-
/    2687  2694  06   8A00     <<        P CU   45<*
L                00       7G               CL   30        D.
/    2694  2725  30   2E42     <<        P          <*    Q+
L                09       GA                              <*Q-
/    2725  2830  102  8A00     <<        P          <-
L                59       7G                              D.
R                :C/BROKEN
/    2830  2861  31   2E56     <<        P          <-    #2D.
L                12       2A                              #2
```

```
R                    :LAPILLI INDISTINCT
/     2861  2886  25     8B00        <<P*          P            <-    D(         <*
L                 12         4G                                    <-D.
R                    :SOME ASSIMILATED TUFF
/     2886  2922  35     2E42        <<            P            <*    Q+D.       <(
L                 09         GA                                    <(D+
/     2922  2955  35     2E42        <<            P            <(    D+
L                 12         GA                                    <(D*
/     2955  2994  37     2E42        <<            P            <(    Q+         <.
L                 12         5G                                    <+Q-
R                    :LOC 2D42
/     2994  3058  63     8B10        <<            P            <-    D-         <*
L                 24         6G                                  <-   D.
R                    :XENOLITH OF 2E AT 3032
/     3058  3092  33     2E12        <<            P            <-    <*         <-
L                 03         AG                                       <*
/     3092  3113  21     7C00        <<            P                             <(
L                 06         AG                                       D.
/     3113  3141  26     8A00        <<CM          P CU     30                   <*
L                 06         7G                      CL     45        D-
/     3141  3200  57     7C00        <<            P            <-    D.         <(
L                 23         4A                                       D*
R                    :GRAIN SIZE VARIES FROM RELATIVELY FINE TO MEDIUM GRAINED
R                    :END OF HOLE AT 320.0 M
R                    :HOLE 10 FEET LONGER THAN DRILLERS THINK. CORE BLOCK MISTAKE
R                    :AT 900 FEET
A001
ALAB                 EQUITY MINESITE LABORATORY
ATYP                 ASSAY
AMTH                 WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM                 RCOVSAMPLE   RQD % CU   G/TAG G/TAU % SB   % AS   % FE   % ZN
R        00     91 :TRICONED - NO CORE
R        91    140 :DYKE - NO SAMPLE
R       140    143 :TUFF - NO SAMPLE
R       143    183 :NO RECOVERY
A001    183    234         9923        0.005      0.5 0.06  0.005 0.001 2.19   0.02
A001    234    260         9924        0.005      0.5 0.07  0.005 0.001 1.47   0.05
A001    260    300         9925        0.001      0.5 0.04  0.005 0.001 1.71   0.005
A001    300    354         9926        0.001      0.5 0.05  0.005 0.001 2.79   0.005
A001    354    384         9927        0.001      0.5 0.05  0.005 0.001 1.23   0.005
A001    384    414         9928        0.001      0.5 0.78  0.005 0.001 0.97   0.005
A001    414    449         9929        0.001      0.5 0.05  0.005 0.001 1.00   0.005
A001    449    480         9930        0.001      0.5 0.07  0.005 0.001 0.83   0.005
A001    480    514         9931        0.001      0.5 0.04  0.005 0.001 0.74   0.005
A001    514    546         9932        0.001      0.5 0.06  0.005 0.001 0.72   0.005
A001    546    575         9933        0.04      10.0 0.19  0.005 0.02  4.62   0.02
A001    575    604         9934        0.02       7.0 0.16  0.005 0.005 2.72   0.04
R       604    617 :DYKE - NO SAMPLE
A001    617    653         9935        0.001      6.0 0.52  0.005 0.005 3.47   0.02
R       653    661 :DYKE - NO SAMPLE
A001    661    691         9936        0.03      11.0 0.16  0.005 0.005 4.20   0.02
A001    691    717         9937        0.12      26.0 0.56  0.02  0.03  5.84   0.02
A001    717    744         9938        0.26      49.0 0.48  0.04  0.02  4.64   0.25
A001    744    773         9939        0.02      14.0 0.19  0.02  0.005 4.28   0.005
A001    773    800         9940        0.02       9.0 0.12  0.005 0.005 3.83   0.02
```

A001	800	830	9981	0.01	16.0	0.22	0.005	0.02	4.89	0.03
A001	830	860	9982	0.04	22.0	0.22	0.005	0.005	3.90	0.02
A001	860	890	9983	0.005	10.0	0.17	0.005	0.005	3.23	0.02
A001	890	920	9984	0.04	26.0	0.42	0.005	0.005	2.59	0.04
A001	920	950	9985	0.05	36.0	0.17	0.005	0.005	3.04	0.03
A001	950	983	9986	0.03	18.0	0.13	0.005	0.005	4.21	0.03
R	983	1014	:DYKE - NO SAMPLE							
A001	1014	1043	9987	0.005	5.0	0.12	0.005	0.005	3.17	0.10
A001	1043	1072	9988	0.03	8.0	0.16	0.005	0.005	4.03	0.12
A001	1072	1101	9989	0.07	65.0	0.44	0.02	0.005	4.06	0.06
A001	1101	1135	9990	0.21	38.0	0.49	0.02	0.005	7.39	2.20
A001	1135	1170	9991	0.20	70.0	0.39	0.03	0.02	5.16	0.09
R	1170	1197	:DYKE - NO SAMPLE							
A001	1197	1238	9992	0.09	73.0	0.48	0.02	0.02	4.09	0.09
R	1238	1421	:DYKE - NO SAMPLE							
A001	1421	1437	9993	0.02	42.0	0.19	0.005	0.005	3.05	0.02
R	1437	1470	:DYKE - NO SAMPLE							
A001	1470	1505	9994	0.005	4.0	0.07	0.005	0.005	3.29	0.005
A001	1505	1524	9995	0.05	6.0	0.22	0.005	0.01	8.40	0.21
A001	1524	1554	9996	0.005	0.5	0.06	0.005	0.005	1.35	0.03
A001	1554	1585	9997	0.005	1.0	0.07	0.005	0.005	2.37	0.04
A001	1585	1615	9998	0.005	0.5	0.04	0.005	0.005	1.11	0.02
A001	1615	1645	9999	0.005	0.5	0.05	0.005	0.005	0.59	0.005
A001	1645	1681	10000	0.01	2.0	0.05	0.005	0.005	4.40	0.01
R	1681	1691	:DYKE - NO SAMPLE							
A001	1691	1737	1602	0.005	4.0	0.06	0.005	0.02	4.76	0.01
R	1737	1832	:DYKE - NO SAMPLE							
A001	1832	1862	1603	0.02	10.0	0.15	0.005	0.01	2.83	0.01
A001	1862	1892	1604	0.01	4.0	0.08	0.005	0.005	2.10	0.01
A001	1892	1920	1605	0.01	3.0	0.09	0.005	0.005	1.51	0.01
A001	1920	1958	1606	0.005	2.0	0.05	0.005	0.005	1.87	0.005
A001	1958	1984	1607	0.005	4.0	0.73	0.005	0.005	2.89	0.01
R	1984	2027	:DYKE - NO SAMPLE							
A001	2027	2057	1608	0.05	10.0	0.21	0.005	0.21	7.82	0.05
A001	2057	2089	1609	0.005	6.0	0.10	0.005	0.02	3.90	0.02
A001	2089	2119	1610	0.005	2.0	0.55	0.001	0.005	3.00	0.03
A001	2119	2150	1611	0.005	3.0	0.12	0.005	0.03	4.17	0.03
A001	2150	2183	1612	0.02	5.0	0.18	0.005	0.01	2.95	0.02
A001	2183	2213	1613	0.005	2.0	0.11	0.005	0.005	1.12	0.02
A001	2213	2256	1614	0.005	3.0	0.08	0.005	0.005	1.96	0.06
A001	2256	2286	1615	0.005	5.0	0.06	0.005	0.005	1.72	0.08
A001	2286	2316	1616	0.04	25.0	0.20	0.03	0.005	1.87	0.005
A001	2316	2346	1617	0.02	10.0	0.08	0.02	0.01	1.92	0.005
A001	2346	2372	1618	0.03	8.0	0.08	0.01	0.01	2.02	0.005
A001	2372	2392	1619	1.37	270.0	2.25	0.19	0.10	9.48	0.58
R	2392	2403	:DYKE - NO SAMPLE							
A001	2403	2438	1620	0.02	7.0	0.49	0.03	0.02	3.17	0.10
A001	2438	2469	1621	0.02	15.0	0.09	0.03	0.005	2.93	0.09
A001	2469	2504	1622	0.08	26.0	0.24	0.02	0.02	4.41	0.04
A001	2504	2535	1623	0.03	12.0	0.28	0.01	0.02	5.78	0.07
A001	2535	2569	1624	0.005	2.0	0.11	0.005	0.005	2.73	0.01
A001	2569	2605	1625	0.10	35.0	0.49	0.01	0.02	5.93	0.06
R	2605	2634	:DYKE - NO SAMPLE							
A001	2634	2664	1626	0.11	34.0	0.46	0.005	0.10	8.59	0.06
A001	2664	2687	1627	0.20	42.0	3.34	0.01	0.32	15.50	0.12

R	2687	2694	:DYKE - NO SAMPLE								
A001	2694	2725	1628	0.07	23.0	0.58	0.005	0.01	5.66	0.06	
R	2725	2830	:DYKE - NO SAMPLE								
A001	2830	2861	1629	0.02	4.0	0.22	0.005	0.09	10.99	0.04	
R	2861	2886	:DYKE - NO SAMPLE								
A001	2886	2922	1630	0.02	6.0	0.20	0.005	0.05	4.05	0.03	
A001	2922	2955	1631	0.03	8.0	0.13	0.005	0.01	2.44	0.005	
A001	2955	2994	1632	0.04	11.0	0.17	0.005	0.005	2.50	0.01	
R	2994	3058	:DYKE - NO SAMPLE								
A001	3058	3092	1633	0.06	35.0	0.35	0.005	0.005	2.08	0.07	
R	3092	3113	:GABBRO - NO SAMPLE								
R	3113	3141	:DYKE - NO SAMPLE								
R	3141	3200	:GABBRO - NO SAMPLE								
R			:END OF HOLE AT 320.0 M								

```
IDEN6B0201      X87CH315 NQ   MAY87DMLDJHJTT MAY87ACK          0.0
IFRJ           EQUITY SILVER MINES LTD         MAIN ZONE - MN GEOCODE
S000   00    411 MT   353.5 090.0 -70.0              7812.00   8446.50   1260.00
S001  411   1295      353.5 090.8 -70.0
S002 1295   2149      353.5 091.6 -70.0
S003 2149   2880      353.5 092.3 -70.0
S004 2880   3383      353.5 093.0 -71.0
S005 3383   3535      353.5 093.2 -71.0
/SCL          MT.2MT.2
LSCL              MT.2       LCTM
/NAM                                                          QZSZTOPYCPTTASPRGY
LNAM                                                          DMCBCLMGHESLGLMO
/      00    37          OVBN                     P
R                 :TRICONED - NO CORE
/      37    68  26     2D83MS     <<             P           >(    <)
L                00          6T
/      68    91  16     2D31MS                    P                 <(
L                02          5A
R                :.1 M 2D54: CLAY OUGE @ 8.9 M
/      91   122  09     2D31MS                    P                 <(
L                00          5A
R                :0.2 M CLAY GOUGE: INTO 2E LOC
/     122   194  67     8C01PL      P*            P                 D-
L                16          AW                      CL    055
R                :CU OBSCURRED IN BROKEN CORE; 4 CM CLAY GOUGE @ 18.0 M
/     194   225  21     2D31MS      BR            P                 <-
L                00          5A
R                :POST-MIN (FAULT/) BRECCIA W/GOUGE
/     225   252  21     8A00PL      P*            P                 <.
L                02          5A
R                :A FEW XENOLITHS OF 2D31 BXIA: CNTS OBSCURRED IN BROKEN CORE
R                :DACITE?
/     252   305  39     8A00CL      P*            P                 D.
L                09          GA                                <-
R                :0.4 M 2D XENOLITH: INTO 8A AS ABOVE 22.5-25.2 M: LOWER CNT
R                :OBSCURRED IN BROKEN CORE
/     305   341  36     2D43MSQZ   <<             P          <(    <=
L                13          4A                                   <(  <(<-
R                :INTO 2D33 LOC.
/     341   417  65     8A00CL      P*            P CU   050        D.
L                85          GA
R                :CL OBSCURRED IN BROKEN CORE
/     417   435  25     2D33MS     <<             P                 D(
L                02          5A
/     435   472  36     8C01PL      P*            P                 D.
L                06          AW                      CL    040
R                :CU OBSCURRED IN BROKEN CORE
/     472   527  50     2D31MS                    P
L                00          5A
R                :INTO 2E81 (APPROX. .3 M)
/     527   533  05     8A00CL      P*            P                 D.
L                00          GA
R                :CNT OBSCURRED IN BROKEN CORE
/     533   538  04     2D31MS                    P                 <-
L                00          5A
```

```
/    538   563  29    2D13CL                P              <)
L               05          5G                          <(
R              :IN PARTS IS CLOSER TO 2E13
/    563   592  27    2D33MS                P              <)
L               07          5A                                        ?.
R              :CNT 0.5 M OF 2C10
/    592   622  27    2D41MS                P              <)            <)
L               20          5A                                        ?.
R              :CONTAINS OL4 M OF 2D51, CONTAINING ROUNDED FRAGMENTS
/    622   652  28    2D31MS                P              <(            <)
L               16          5A
/    652   679  27    2D31MS                P              <(            <(
L               06          5A
R              :INTO 2E31 IN PLACES
/    679   694  15    2D81MS      <(        P              <+
L               08          GT                             <(<(
R              :CONTAINS 0.5 M OF 2D33
/    694   716  22    2D31MS                P              <+
L               17          5A                             <(<(
/    716   745  29    2D31MS                P              <)            <)
L               09          5A                             <-
R              :CONTAINS 2C81 IN PLACES & ALSO SECONDARY
R              :(<--FELDSPAR IN PLACES)
/    745   771  23    2D11MS                P              <(            <)
L               19          5A                             <-<.
R              :CONTAINS SMALL AMOUNT  2C11
/    771   876  94    8A00PL      P*        P CU   060     D.            <(
L               10          7G
R              :CONTAINS 2 XENOLITHS APPROX. 0.3 M EACH OF 2D20 CONT. PY, HE
R              :SZ, MG: LOWER CONTACT IRREGULAR
/    876   906  25    2D41MSQZ   BR         P          <(     D(
L               60          5A
R              :CONT. .15 M OF 8A00 @ 89.3, BR OCCURS @ 90.4 M
/    906   939  31    2D41MSQZ              P          <)     <)           <(
L               15          4A
/    939   969  28    2E41MSQZ   AD         P          <(     B)
L               18          5A
R              :CONTAINS MINOR 2D41 IN PLACES
/    969   999  27    2E31                  P          <)     D(           <-
L               17          6A
R              :INTO 2E41 W/COLOR = 5A
/    999  1022  23    2E51MSQZ              P          <+     <)
L               08          4A
R              :COLOR TO 5A, SILICIFICATION PREFERENTIALLY OCCURS BETWN GRAINS
/   1022  1048  24    2D11CL                P          <(     D)
L               07          5G                              B1
R              :COLOR TO 6G
/   1048  1068  16    2D11CLMS              P          <*     D)
L               12          6G                              B=   >(
R              :MINOR SILICIFICATION AS WELL AS PHYLLIC ALTERATION
/   1068  1097  25    2E21SZCL   AD         P          <(B)   B+
L               20          5G                              B=        <.
R              :GRADES TO 2E23
/   1097  1122  24    2E21SZCL   AD         P          <(B*   B)
L               18          5G                              B=
```

```
R                  :SILICIFICATION OCCURRING INTERSTITIALLY<(B-  B-
/   1122  1148  25     2D81MS                    P                    B)<)<-
L               15         5T
R               :LOCALLY 2581
/   1148  1167  16     2C81MS                    P                       D-
L               09         6T                                            D.
/   1167  1189  21     2D21SZMS                  P                 B-   D*
L               09         AT                                       B(
R               :LOCALLY TO 2C81 AS ABOVE
/   1189  1211  22     2D11CLMS                  P                      <+
L               11         5G                                       D-       ?-
/   1211  1239  27     2C83MS         <<         P                      <+
R               15         5T                                           <-
/   1239  1268  28     2C83MS         <<         P                      <+
L               12         GT                                       B)
/   1268  1298  24     2D13CL         <<MX       P             <)      QZ        <(
L               11         4G                                       Q1<(
/   1298  1331  28     2C83MS         <<         P             <)      Q1
L               19         AT                                       B)<(
/   1331  1359  27     2C83MS         <<MX       P                     Q1        <)
L               19         5T                                       B)<(<*
/   1359  1389  29     2D51QZ         <<         P             <2B-   Q=         <(
L               19         6A                                       Q)<(D-?)
/   1389  1419  28     2D41QZ         <<<<       P             <1      Q=        >(
L               23         5A                                       Q)<=
/   1419  1433  14     2D51QZCL       <<         P             Q2D-   <=
L               11         4G                                       Q1Q=
/   1433  1455  22     2C11CL         <<         P                      D.          <)
L               19         5G                                       Q1<-
R               :GYPSUM - MAJOR COMPONENT OF MICROVEINS, APPEARANCE OF UNIT
R               :SIMILAR TO 8D
/   1455  1478  21     2C11CL                    P                      D.
L               19         5G         <<                       <)      D-          <)
/   1478  1514  34     2D41QZCL                  P                   Q1
L               27         6A         <<                       Q2      <=
/   1514  1546  29     2C11CL                    P                   <1<)
L               19         5G                                           D.
R               :SIMILAR TO INTERVAL 143.3 - 145.5                  D2  <-
/   1546  1635  81     8C00PL       P*               CU   033
L               32         8G
R               :LOWER CONTACT OBSCURRED IN BROKEN CORE: CLAY GOUGE @
R               :167.5 TO 168.5
/   1635  1670  30     8D11MS                    P                      D-          <-
L               13         7T                                       <-
R               :CONTAINS 1.0 M OF 2D81: CHLORITE ALTERATION OCCURS
R               :PREFERENTIALLY AROUND MICROVEINS
/   1670  1682  11     2D11CLMS                  P                      D(
L               04         5G                                       Q=  <-  ?.
R               :CONTAINS 0.4 M OF 8D81 TO HIGH ALTERATION AROUND VEINS
/   1682  1705  23     8D11MSCL                  P                      D.
L               08         7T                                           <-  ?.
R               :CONTAINS 0.7 M OF 2D11
/   1705  1731         8A00PL                        CU   020
L               02         5G
R               :CONTAINS 0.2 M OF 2D81: LOWER CONTACT IRREGULAR
```

/ 1731 1761 29 2D31MS P <(
L 09 5A <1 <- <-
R :BRECCIATED AND DEFORMED NEAR CONTACT WITH DYKE
/ 1761 1791 28 2E41QZ P Q2 B(
L 15 5A <(<(
/ 1791 1821 29 2E41QZ P Q1 D-
L 16 5A <(<-
/ 1821 1850 27 2D41QZ P Q1 D-
L 14 5A <) <(
/ 1850 1880 29 2D41QZ P Q= D-
L 06 5A <(<(
/ 1880 1911 30 8A00PL P* P CU 040 D-
L 09 5G B1 <(
R :LOWER CONTACT OBSCURRED BY BROKEN CORE
/ 1911 1948 36 2D81CLQZ P <= <1
L 19 5G <-<.
/ 1948 1971 23 8A00PL P* P
L 18 6G <)
R :UPPER CONTACT IRREGULAR: CONTAINS 2C XENOLITH OF APPROX. .15 M
/ 1971 2198 219 8A00PL P* P CU 070
L 73 6G CL 045
/ 2198 2228 28 2D21SZCL P Q1<. <)
L 07 5G <= <(
/ 2228 2258 29 2D41QZCL P Q1<. <)
L 14 5A <= <(
/ 2258 2288 26 2D41QZCL P Q1 D)
L 13 5A <=<(<(<-
R :CONTAINS .20 M OF MX, PY, MG, HE
/ 2288 2318 29 2D41QZCL P Q= <=
L 20 4A <=<-<- <-
/ 2318 2348 30 2D11CL P Q) <*
L 22 4G <1 <)
R :CONTAINS 0.3 M OF INTENSELY << 2C81
/ 2348 2378 28 2D41QZ P Q1 <)
L 12 5A <)<-<- <)
R :CONTAINS 0.3 M OF CHLORITIZED ANDESITE DYKE
/ 2378 2413 32 2D41QZ P Q1 D-
L 20 5A <)<-
/ 2413 2425 11 8A00PL P* P CU 035 D.
L 10 5G CL 040
/ 2425 2451 26 2D11CLQZ P Q1 B)
L 18 Q2<)
R :ZONE SHOWS ALSO MODERATE TO STRONG SILICIFICATION
/ 2451 2588 130 8A00DL P* P CU 030 D-
L 43 5G Q1D=
R :LOWER CONTACT NOT WELL DEFINED, PHENOCRYSTS HAVE
R :RECRYSTALIZED & MINERALIZED
/ 2588 2618 29 2D11CLQZ P Q* D*
L 20 5G Q1<-<- <-
/ 2618 2643 24 2D11C;QZ P Q1 D*
L 10 5G <(<1<) <-
R :CONTAINS FRAGMENTS OF 8D11
/ 2643 2661 16 8D11CL P <)
L 06 4G <(<1<(
R :SHOWS MINOR SILICIFICATION: CONTACTS OBSCURRED: CONTAINS

```
R                    :MINOR 2D11
/     2661  3019 351     8C00PL                     P CU   040       <)
L                169        8G
R                    :CL OBSCURRED BY BROKEN CORE; DYKE SHOWS CHLORITE ALTERATION
R                    :NEAR CONTACTS
/     3019  3048  28     8D51QZPL    P*             P           B3     D-
L                 07        6V                                        <)  <-
/     3048  3078  30     8D41QZPL    P*             P           B2     D.
L                 06        GV                                        <=  <(
/     3078  3094  16     8D41QZ      P*             P           B2     <(
L                 04        GV                                        <)  <-
/     3094  3116  21     8D41QZCL    P*             P           B2     D-
L                 00        7G                                        <=  <(
/     3116  3146  30     8D41QZ      P*             P           B2     D(
L                 03        7V                                        <(
/     3146  3176  28     8D51QZ      P*             P           B2     D.
L                 05        5V                                        B1
/     3176  3206  30     8D51QZ      P*             P           B2     D.
L                 00        6V                                        B1
/     3206  3229  23     8D51QZ      P*             P           B2     D.
L                 16        60                                        B=  <-
/     3229  3259  25     8D51QZ      P*             P           B3
L                 07        7V
/     3259  3385 124     8D51QZ      P*             P           B1     D.
L                 41        5V                                        B1D=
R                    :CONTAINS NUMEROUS XENOLITHS OF 7E
/     3385  3535 146     7E00PL                     P           Q1
L                 70                                                  B1D=
R                    :CONTACT NOT SEEN, ABOUT 1/2 OF THE SECTION IS SIMILAR TO 8D51
R                    :END OF HOLE
A001
ALAB                 EQUITY MINESITE LABORATORY
ATYP                 ASSAY
AMTH                 WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM                 RCOVSAMPLE   RQD % CU   G/TAG G/TAU % SB   % AS   % FE   % ZN
R       00     37 :TRICONED - NO CORE
A001    37     68          9841        0.005    2.0 0.63  0.005 0.005 5.19   0.02
A001    68     91          9842        0.005    1.0 0.06  0.005 0.005 4.10   0.02
A001    91    122          9843        0.005    0.5 0.03  0.005 0.005 1.40   0.02
R      122    194 :DYKE - NO SAMPLE
A001   194    225          9844        0.005    1.0 0.04  0.005 0.005 2.29   0.07
A001   225    252          9845        0.005    0.5 0.05  0.005 0.005 1.41   0.02
R      252    305 :DYKE - NO SAMPLES
A001   305    341          9846        0.005    2.0 0.97  0.005 0.005 4.36   0.06
R      341    417 :DYKE - NO SAMPLES
A001   417    435          9847        0.01     0.5 0.42  0.005 0.005 1.85   0.02
R      435    472 :DYKE - NO SAMPLES
A001   472    500          9848        0.005    0.5 0.06  0.005 0.005 1.51   0.01
A001   500    527          9849        0.005    0.5 0.05  0.005 0.005 1.89   0.01
A001   527    538          9850        0.005    0.5 0.05  0.005 0.005 3.01   0.02
A001   538    563          9851        0.005    0.5 0.06  0.005 0.01  2.52   0.02
A001   563    592          9852        0.005    0.5 0.06  0.005 0.005 1.81   0.04
A001   592    622          9853        0.005    0.4 0.04  0.005 0.001 1.99   0.07
A001   622    652          9854        0.005    0.5 0.05  0.005 0.005 2.06   0.11
A001   652    679          9855        0.005    2.0 0.06  0.005 0.005 2.10   0.10
```

A001	679	694	9856	0.005	3.0	0.08	0.005	0.005	3.02	0.13
A001	694	716	9857	0.005	9.0	0.12	0.02	0.005	2.21	0.06
A001	716	745	9858	0.005	5.0	0.03	0.005	0.005	1.92	0.05
A001	745	771	9859	0.005	3.0	0.17	0.005	0.005	1.43	0.09
R	771	876	:DYKE - NO SAMPLES							
A001	876	906	9860	0.005	5.0	0.05	0.005	0.005	1.89	0.12
A001	906	939	1634	0.03	24.0	0.22	0.06	0.02	2.78	0.09
A001	939	969	1635	0.02	25.0	0.23	0.05	0.01	1.82	0.02
A001	969	999	1636	0.01	2.0	0.03	0.005	0.01	1.92	0.05
A001	999	1022	1637	0.005	3.0	0.09	0.005	0.005	2.76	0.02
A001	1022	1048	1638	0.005	2.0	0.07	0.005	0.005	3.65	0.12
A001	1048	1068	1639	0.02	4.0	0.09	0.005	0.005	3.57	0.19
A001	1068	1097	1640	0.03	8.0	0.26	0.005	0.03	5.52	0.07
A001	1097	1122	2001	0.02	17.0	0.24	0.005	0.09	4.11	0.25
A001	1122	1148	2002	0.01	15.0	0.80	0.005	0.005	3.93	0.03
A001	1148	1167	2003	0.02	3.0	2.10	0.005	0.005	2.34	0.005
A001	1167	1189	2004	0.02	9.0	0.29	0.005	0.01	3.97	0.01
A001	1189	1211	2005	0.01	13.0	0.67	0.005	0.11	6.63	0.02
A001	1211	1239	2006	0.01	9.0	0.50	0.005	0.04	8.80	0.01
A001	1239	1268	2007	0.02	15.0	0.53	0.005	0.06	8.52	0.09
A001	1268	1298	2008	0.04	13.0	0.53	0.02	0.06	17.10	0.02
A001	1298	1331	2009	0.03	49.0	3.64	0.02	0.04	14.5	0.07
A001	1331	1359	2010	0.05	36.0	2.20	0.03	0.05	12.06	0.02
A001	1359	1389	2011	0.04	32.0	1.22	0.005	0.03	10.62	0.02
A001	1389	1419	2012	0.03	26.0	0.97	0.005	0.03	12.65	0.02
A001	1419	1433	2013	0.05	15.0	0.16	0.005	0.05	13.70	0.03
A001	1433	1455	2014	0.005	3.0	0.09	0.005	0.005	3.18	0.01
A001	1455	1478	2015	0.005	3.0	0.05	0.005	0.005	4.01	0.02
A001	1478	1514	2016	0.05	44.0	1.08	0.005	0.005	5.34	0.11
A001	1514	1546	2017	0.005	3.0	0.01	0.005	0.005	3.84	0.02
R	1546	1635	:DYKE - NO SAMPLES							
A001	1635	1670	2018	0.01	7.0	0.14	0.005	0.02	4.40	0.02
A001	1670	1682	2019	0.03	11.0	0.08	0.005	0.02	4.28	0.03
A001	1682	1705	2020	0.005	6.0	0.11	0.005	0.005	3.46	0.02
R	1705	1731	:DYKE - NO SAMPLES							
A001	1731	1761	2021	0.02	5.0	0.08	0.005	0.005	2.31	0.03
A001	1761	1791	2022	0.005	1.0	0.05	0.005	0.005	1.82	0.02
A001	1791	1821	2023	0.005	0.0	0.05	0.005	0.005	1.46	0.02
A001	1821	1850	2024	0.005	0.0	0.04	0.005	0.005	1.07	0.02
A001	1850	1880	2025	0.01	3.0	0.09	0.005	0.01	1.57	0.02
R	1880	1910	:DYKE - NO SAMPLES							
A001	1910	1948	2026	0.11	61.0	3.33	0.03	0.03	3.99	0.15
A001	1948	1971	2027	0.005	3.0	0.11	0.005	0.005	2.89	0.03
R	1971	2198	:DYKE - NO SAMPLES							
A001	2198	2228	2028	0.16	20.0	0.87	0.05	0.01	3.29	0.37
A001	2228	2258	2029	0.13	42.0	1.58	0.03	0.01	2.41	0.33
A001	2258	2288	2030	0.04	7.0	0.57	0.01	0.005	2.68	0.47
A001	2288	2318	2031	0.03	6.0	0.33	0.01	0.005	3.05	0.27
A001	2318	2348	2032	0.05	27.0	0.70	0.01	0.005	2.74	0.24
A001	2348	2378	2033	0.02	20.0	0.57	0.01	0.005	2.45	0.22
A001	2378	2425	1680	0.07	46.0	0.74	0.02	0.005	2.73	0.15
A001	2425	2451	2034	0.19	93.0	0.70	0.09	0.04	3.59	0.10
R	2451	2588	:DYKE - NO SAMPLES							
A001	2588	2618	2035	0.07	17.0	0.28	0.02	0.005	3.37	0.14
A001	2618	2643	2036	0.08	21.0	0.27	0.02	0.005	4.18	0.14

A001	2643	2661	2037	0.07	10.0	0.15	0.01	0.005	3.64	0.08
R	2661	3019	:DYKE - NO SAMPLES							
A001	3019	3049	2038	0.005	0.5	0.04	0.01	0.005	2.23	0.06
A001	3048	3078	2039	0.005	2.0	0.03	0.01	0.005	2.04	0.06
A001	3078	3094	2040	0.005	0.5	0.03	0.005	0.005	2.47	0.06
A001	3094	3116	1641	0.01	8.0	0.04	0.005	0.005	3.01	0.05
A001	3116	3146	1642	0.005	6.0	0.02	0.005	0.005	2.58	0.05
A001	3146	3176	1643	0.005	9.0	0.01	0.005	0.005	2.15	0.04
R	3176	3535	:MIXED DYKE & GABBRO - NO SAMPLES							
R			:END OF HOLE							

```
IDEN6B0201      X87CH316 NQ   MAY87DML   JTT MAY87ACK         0.0
IPRJ          EQUITY SILVER MINES LTD        MAIN ZONE - MN GEOCODE
S000   00   457 MT  329.2 090.0 -70.0          7751.0    8445.5    1260.0
S001  457  1295     329.2 090.0 -70.0
S002 1295  2073     329.2 090.0 -70.0
S003 2073  2743     329.2 090.0 -70.0
S004 2743  3292     329.2 090.0 -70.0
/SCL        MT.2MT.2
LSCL              MT.2       LCTM
/NAM                                                     QZSZTOPYCPTTASPRGY
LNAM                                                     DMCBCLMGHESLGLMO
/      00    91          OVBN               P
R                 :TRICONED - NO CORE
/      91   188  90     8A00PL      P*      P
L                17          6G               CL   055    B(
R                 :CU NOT VISIBLE, LOWER CONTACT ALTERED - DYKE SHOWS QTZ-SERICITE ALT. NE
AR CTCTS.
/     188   213  25     2D13MS              P                 D(
L                00          6A                              B)
R                 :CONTAINS SOME 2C81
/     213   244  30     2D31                P                 B+
L                05          5A                              <(  <)
R                 :CONTAINS 0.4 M OF 8A00 (CONTACT OBSCURRED)
/     244   267  23     2D81MS              P          <(     B+
L                06          5T                                 <-
/     267   288  19     8A00CL      P*      P CU   040       D)
L                00          7G               CL   025    B*
R                 :CONTAINS 0.2 M OF 2D31 CONTAINING PY AND HE
/     288   313  22     2D41QZ              P                <=
L                00           6A                             <(<-
/     313   330  17     2E31MS              P                <(
L                07           6A6A
/     330   348  18     8A00PL     P*       P CU   060       <(
L                02           7G              CL   060
/     348   384  27     2D31                P                <+
L                00          5A                              <-<)
R                 :CLAY GOUGE @ 37.7 M
/     384   406  22     8A00CL      P*      P                D.
L                02          GA               CL   050    <)
R                 :CONTAINS SMALL XENOLITHS OF 2D31: UPPER CONTACT OBSCURRED
R                 :BY BROKEN CORE
/     406   440  31     2D21SZMS            P          B-   <)
L                10           5A                       <(     <(
/     440   474  34     2D21SZ              P                <)
L                06           5A                          <(  <*
/     474   507  31     2D81MS              P                <+<.
L                21           GT                          <((<(<)  <-
R                 :INTO 2E81
/     507   514  07     8A00PL      P*      P CU   070       <-
L                02           7G              CL   010
/     514   539  25     2D81MS              P          B.   <+
L                07             GT                           <((<-
/     539   560  19     2C83SZMS   <<MX     P          B.   >2
L                06           5T                             <((<.
/     560   589  28     2D21SZ     <<MX     P          B-   <1
L                16           5A
```

```
/     589   615   20    2C81MSSZ                 P            B.   D)
L                 00         6T
R                :CONTAINS SOME 2D21 WITH PY STRINGERS & SZ
/     615   645   30    2D21SZ                   P            B-   <=
L                 04         5A
/     645   675   30    2D31MS                   P                 <+
L                 11         5A                                <-
R                :CONTAINS 0.2 M OF 8A00
/     675   705   30    2D21SZ                   P            B.   <+
L                 10
R                :CONTAINS 0.2 M OF 8A00: INTO 2E21 IN PLACES
/     705   731   24    2D31MS                   P                 <)
L                 08          5A                               <-
/     731   765   34    8D81CL       P*          P                 <*          <+
L                 24         6G                                  02
R                :CONTACTS OBSCURRED THROUGH ALTERATION
/     765   785   19    2D41QZ                   P                 <+          <(
L                 19         GA                                  <+
R                :MAY IN PART BE COMPOSED OF 8D81
/     785   817   31    2D31MS                   P                 <=
L                 12         6A                                  <(
R                :LOCALLY INTO 2C31, & LOCALLY SHOWS <<
/     817   847   29    2D81CL                   P                 B+          <)
L                 18         6G                                  B1  <(
/     847   877         2E41                     P
/     877   898   20    2E41QZCL                 P                 B*B.
L                 15         GA                                  B=  <-      <+
/     898   926   28    2D81CL                   P                 <(
L                 15         GA                                  D=
R                :CONTAINS 0.3 M OF 8A00: LOC INTO 2E81
/     926   958   31    2D41QZ                   P          <)   <?<)        <=
L                 19         6A                                     <(
R                :LOC INTO 2E41 (ROCKS MAY BE 2D91)
/     958   980   19    2D41QZ                   P          <*   <?B*        <)
L                 15         6A                                  <-
R                :LOCALLY INTO 2E81: ROCKS MAY POSSIBLY BE 2D91
/     980   1010  30    2C91MS                   P                 <)         <-<(
L                 24         GT                                  <-<-
R                :LOC. INTO 2D41
/     1010  1040  26    2D41QZ                   P          Q=     <(          <*
L                 14         5A                                  B)
/     1040  1070  29    2D41QZ                   P                 <(          <(
L                 16         VA
/     1070  1100  30    2D41QZ                   P          <(     <*          <(
L                 08         5G                                  <)<-<-
R                :LOCALLY INTO 2C41
/     1100  1130  30    2D41QZ                   P                 <*          <(
L                 22         5G                                  <)<-<.
R                :CONTAINS 0.8 M OF 8A00 FROM 110.5 TO 111.3
/     1130  1160  30    2D41QZCL                 P                 <+          <*
L                 22         6G                                  <=<(<-
/     1160  1189  29    2D51QZCL                 P                 <)          <)
L                 15         5G                                  <=<*<-
/     1189  1201  11    8A00PL       P*             CU    050                  <(
L                 09         5G                     CL    070      D*
```

```
/    1201  1223  22     2D41QZCL                  P               <)          <(
L                06        6A                                   <)   <(
/    1223  1266  43     8A00PL      P*            P                D-
L                27        5G                                   <)D)
R               :CONTACT OBSCURRED BY ALTERATION: CONTAINS 0.2M XENOLITH OF 2D41
/    1266  1293  26     2D41QZCL    BR            P               <(          <+
L                16        6A                                   <+
/    1293  1310  17     2D41QZ                    P               <(          <*
L                09        5A                                   <(   <-
/    1310  1322  12     2D41QZCL    BR            P               <(          <(
L                10        7G                                   <=
/    1322  1334  12     8A00PL                    P CU    070      D-          <*
L                10        5G                       CL    070
/    1334  1355  20     2D41QZCL                  P                B(          <*
L                13        5G                                   <)
R               :LOC INTO 8A00
/    1355  1374  19     2D41QZ                    P               <(          <(
L                17        5A                                   <)   <(
/    1374  1469  92     8A00PL      P*            P                            <(
L                51        4G                       CL    065      D)
R               :UPPER CONTACT OBSCURRED BY BROKEN CORE
/    1469  1500  31     2D21SZMG                  P          <(<(   <=       <-
L                06        3N                                   <*<+<(
R               :ALSO SHOWS STRONG SILICIFICATION
/    1500  1529  29     2D21SZ                    P            O-   <*
L                06        5A                                   <(<.
R               :SHOWS MODERATE SILICIFICATION
/    1529  1552  21     2D31MS                    P               <+
L                19        5A                                   <-<-<.
/    1552  1576  23     2D11CL                    P               <(          <)
L                18        5G                                   <=
/    1576  1591  14     2D11CL                    P               <(
L                08        5G                                   <=
R               :CONTAINS 0.4 M OF 8A00
/    1591  1620  24     2D31MS                    P               <(          <-
L                02        6A                                   <+
/    1620  1764 138     8C00PL      P*            P CU    025      D.
L                51        7G
R               :LOWER CONTACT OBSCURRED BY BROKEN CORE: INTO 8A00 NEAR CNTS
/    1764  1786  20     2D41QZ                    P               <*          <(
L                03        6A                                   <*   <(
/    1786  1812  26     2D31MS                    P               <*          <-
L                07        5A                                   <)
R               :SHOWS MNR SILICIFICATION: LOC INTO 2E31
/    1812  1842  30     2D41QZ                    P                B+          <-
L                12        5A
R               :INTO LOC 2C41
/    1842  1872  30     2D41QZ                    P               <)<.        <(
L                03        6A                              <-        <(
R               :CONTAINS 0.3 M XENOLITH OF 8A00
/    1872  1902  30     2D41QZ      <<            P               <)          <(
L                03        5A                                     <+
/    1902  1932  29     2D41QZ      <<            P               <(          <(
L                06        5A
/    1932  1962  28     2D41QZ                    P               <-<.
```

```
                                                              <*
L                  04        4A                               <+        <-
/   1962   1997    34     2D41QZ               P              <(
L                  11        4A                               <*
/   1997   2032    32     2D41QZ               P             <(
L                  10        4A                               <)<)
/   2032   2059    29     2D51QZ     <<        P              <)
L                  19        3N                               <*<(
/   2059   2086    27     2D51QZ     <<        P              <(
L                  11        4N
R                 :CONTAINS 0.3 M OF 8A00
/   2086   2146    60     8A00PL     P*        P CU   025     D-        <)
L                  13        5G                  CL   070     D(
R                 :CONTAINS 2 XENOLITHS OF 2D41 EACH 0.5 M
/   2146   2177    28     2D81MS               P              <)
L                  05        6A                            <+
/   2177   2203    26     2D41QZ               P              <)
L                  15        5A                             <)
/   2203   2223    15     8A00PL     P*        P              D-
L                  00        5G                               D-
R                 :CONTACTS OBSCURRED BY BROKEN CORE
/   2223   2253    30     2D51QZCL   <<        P          <(    <(
L                  18        4N                             <*<(
/   2253   2284    31     2D41QZCL             P              <(
L                  14        4N                             <)<.
/   2284   2314    28     2D41QZ     BR        P              <*<.
L                  21        4N                             <)<-
/   2314   2344    30     2D51QZMG   <<        P              <(<.<(     <-
L                  20        4N                             <(<+
/   2344   2374    30     2D51QZMG   <<        P              <*<*
L                  10        4A                               <+  <(
/   2374   2408    33     2D51QZ,G   <<        P              <*<(
L                  12        4A                               <*  <-
/   2408   2485    77     8A00PL     P*        P CU   080     D.
L                  38        4G                  CL   055     D.
/   2485   2517    29     2D51QZ     <<        P              <(
L                  06        5A                             <)<(  <(
/   2517   2536    23     2D51QZ     <<        P              <*<.
L                  13        4N                             <)<*  <)
/   2536   2555    13     2D51QZ     <<        P              <(<.
L                  08        5N                             <(<(  <)
/   2555   2575    21     2C41QZ               P              <(          <(
L                  14        3N                               <(
/   2575   2596    20     2C51QZ               P              B(
L                  16        2N                               <(
/   2596   2631    31     2D51QZ               P              <(
L                  11        4A                             <-<(  <.
/   2631   2647    16     8A00PL     P*        P              D.
L                  02        6A
/   2647   2682    35     2D51QZ     <<        P              <*<.
L                  08        5N                               <(  <.
/   2682   2717    35     2D41QZSZ             P           B. <(
L                  13        4A                             <(
/   2717   2749    29     2D41QZSZ             P           B. <(
L                  06        5N                             <(
/   2749   2827    75     8A00PL     P*        P CU   055     D.        <(
```

```
L                   53        5G                          CL    068
/    2827  2857     28     2D51QZ      <<          P                  <(    <-
L                   24        4N                                      <)   <-
/    2857  2887     30     2D51QZMG    <<          P                  <*       <(
L                   24        4N                                      <+
/    2887  2917     30     2D51QZMG    <<          P                  <*<.
L                   14        4N                                      <+   <+
/    2917  2947     30     2D51QZMG    <<          P                  <(
L                   23        4N                                      <+   <.
/    2947  2977     29     2D51QZMG    <<          P                  <(
L                   22        4N                                      <+   <(
/    2977  3007     30     2D51QZMG    <<          P                  <(       <(
L                   20        5N                                      <+   <-
/    3007  3037     30     2D51QZMG    <<          P              <.  <*
L                   27        5N                                      <)
/    3037  3067     30     2D41QZ      <<          P                  <(       <-
L                   20        5N                                      <+   <-
R                  :CONTAINS 0.35 M OF 8A00
/    3067  3097     29     2D41QZ      BR          P                  <(<.     <-
L                   23        5N                                    <(<*   <.
R                  :HYDROTHERMAL ALTERATION PREFERENTIAL ALONG BRECCIATION
R                  :FRACTURES: CLAY GOUGE @ 309.5
/    3097  3124     26     2D51QZ      BR          PP                 <(       <-
L                   20        5N                                    <(<*   <.
/    3124  3154     30     2D51QZ      BR          P             <(   <(       <-
L                   28        5A                                    <(<(
/    3154  3184     27     2D51QZ      BR          P                <*<(       <-
L                   22        5A                                      <(   <-
/    3184  3214     30     2D51QZ      BR          P                  <(       <-
L                   26        5A                                      <-   <(
/    3214  3236     21     2D51QZ      BR          P                  <(
L                   15        5A                                      <-   <(
/    3236  3256     14     7C00PL                  P                  D.
L                   07        7V
R                  :FINER GRAINED THAN TYPICAL MONZONITE
/    3256  3292     36     8C00PL      P*          P                  D.
L                   15        8G
R                  :END OF HOLE
A001
ALAB               EQUITY MINESITE LABORATORY
ATYP               ASSAY
AMTH               WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM               RCOVSAMPLE   RQD % CU   G/TAG G/TAU % SB   % AS   % FE   % ZN
R        00     91 :TRICONED - NO CORE
R        91    188 :DYKE - NO SAMPLES
A001   188    213        1644        0.005    0.5 0.04   0.005 0.005 1.79   0.03
A001   213    244        1645        0.005    0.5 0.07   0.005 0.01  2.77   0.03
A001   244    267        1646        0.005    0.5 0.06   0.005 0.005 2.43   0.02
R      267    288 :DYKE - NO SAMPLES
A001   288    313        1647        0.005    4.0 0.11   0.005 0.02  4.80   0.14
A001   313    330        1648        0.005    4.0 0.04   0.005 0.005 2.83   0.05
R      330    348 :DYKE - NO SAMPLES
A001   348    384        1649        0.02    17.0 0.31   0.005 0.04  8.03   0.30
R      384    406 :DYKE - NO SAMPLES
A001   406    440        1650        0.005    3.0 0.10   0.005 0.01  3.55   0.03
```

A001	440	474	1651	0.001	4.0	0.11	0.005	0.02	4.00	0.03
A001	474	507	1652	0.005	20.0	0.44	0.005	0.005	5.59	0.18
R	507	514	:DYKE - NO SAMPLES							
A001	514	539	1653	0.03	22.0	0.33	0.005	0.005	3.61	0.06
A001	539	560	1654	0.03	20.0	0.50	0.03	0.20	29.10	0.29
A001	560	589	1655	0.005	12.0	1.55	0.03	0.005	21.10	0.03
A001	589	615	1656	0.005	6.0	0.10	0.005	0.001	2.69	0.005
A001	615	645	1657	0.005	8.0	0.37	0.005	0.001	3.36	0.02
A001	645	675	1658	0.005	3.0	0.19	0.005	0.001	4.69	0.005
A001	675	705	1659	0.005	2.0	0.04	0.005	0.001	3.41	0.02
A001	705	731	1660	0.005	2.0	0.13	0.005	0.001	4.64	0.02
A001	731	765	1661	0.005	2.0	0.06	0.005	0.001	3.15	0.02
A001	765	785	1662	0.005	0.5	0.01	0.005	0.001	2.04	0.03
A001	785	817	1663	0.005	4.0	0.02	0.005	0.001	2.20	0.19
A001	817	847	1664	0.005	0.5	0.02	0.005	0.001	1.57	0.02
A001	847	877	1665	0.005	2.0	0.03	0.005	0.001	2.36	0.02
A001	877	898	1666	0.005	0.5	0.02	0.005	0.005	1.41	0.01
A001	898	926	1667	0.005	0.5	0.09	0.005	0.005	1.93	0.03
A001	926	959	1668	0.01	1.0	0.14	0.005	0.005	2.10	0.01
A001	959	980	1669	0.005	0.5	0.11	0.005	0.005	1.41	0.01
A001	980	1010	1670	0.005	0.5	0.09	0.005	0.005	2.03	0.005
A001	1010	1040	1671	0.005	0.5	0.03	0.005	0.005	1.75	0.005
A001	1040	1070	1672	0.005	0.5	0.13	0.005	0.01	1.90	0.005
A001	1070	1100	1673	0.005	0.5	0.04	0.005	0.02	1.79	0.005
A001	1100	1130	1674	0.005	2.0	0.03	0.005	0.005	2.19	0.02
A001	1130	1160	1675	0.005	2.0	0.03	0.005	0.001	2.74	0.005
A001	1160	1189	1676	0.005	0.5	0.02	0.005	0.001	2.10	0.005
R	1189	1201	:DYKE - NO SAMPLES							
A001	1201	1223	1677	0.005	0.5	0.03	0.005	0.001	2.33	0.03
R	1223	1266	:DYKE - NO SAMPLES							
A001	1266	1293	1678	0.005	0.5	0.47	0.005	0.001	1.50	0.005
A001	1293	1310	1679	0.005	3.0	0.87	0.005	0.005	1.72	0.005
A001	1310	1322	1761	0.005	0.5	0.05	0.005	0.005	1.66	0.005
R	1322	1334	:DYKE - NO SAMPLES							
A001	1334	1355	1762	0.005	0.5	0.07	0.005	0.005	1.49	0.005
A001	1355	1374	1763	0.005	2.0	0.03	0.005	0.005	1.85	0.005
R	1374	1469	:DYKE - NO SAMPLES							
A001	1469	1500	1764	0.10	39.0	0.21	0.005	0.04	5.48	0.02
A001	1500	1529	1765	0.06	23.0	0.19	0.005	0.03	2.73	0.04
A001	1529	1552	1766	0.06	81.0	0.59	0.02	0.04	4.36	0.03
A001	1552	1576	1767	0.11	43.0	0.55	0.02	0.005	4.12	0.06
A001	1576	1591	1768	0.10	26.0	0.23	0.005	0.005	3.22	0.03
A001	1591	1620	1769	0.06	7.0	0.21	0.005	0.005	2.56	0.08
R	1620	1764	:DYKE - NO SAMPLES							
A001	1764	1786	1770	0.03	10.0	0.11	0.005	0.03	3.69	0.03
A001	1786	1812	1771	0.08	12.0	0.21	0.005	0.02	3.15	0.02
A001	1812	1842	1772	0.34	10.0	0.34	0.005	0.09	3.75	0.04
A001	1842	1872	1773	0.13	13.0	0.31	0.005	0.02	3.29	0.02
A001	1872	1902	1774	0.08	19.0	0.66	0.02	0.005	2.76	0.02
A001	1902	1932	1775	0.19	15.0	0.02	0.02	0.07	3.19	0.03
A001	1932	1962	1776	0.18	14.0	0.41	0.03	0.24	7.35	0.06
A001	1962	1997	1777	0.02	5.0	0.12	0.01	0.005	3.40	0.03
A001	1997	2032	1778	0.18	11.0	0.31	0.03	0.01	5.70	0.04
A001	2032	2059	1771	0.80	13.0	0.36	0.02	0.01	6.60	0.08
A001	2059	2086	1780	1.07	15.0	0.46	0.04	0.01	5.60	0.15

R	2086	2146	:DYKE - NO SAMPLES								
A001	2146	2177		1781	0.10	3.0	0.04	0.01	0.01	4.80	0.16
A001	2177	2203		1782	0.17	9.0	0.15	0.04	0.01	5.90	0.05
R	2203	2223	:DYKE - NO SAMPLES								
A001	2223	2253		1783	0.30	19.0	0.37	0.02	0.05	4.30	0.06
A001	2253	2284		1784	0.12	16.0	0.24	0.03	0.01	3.60	0.05
A001	2284	2314		1785	0.27	47.0	0.96	0.03	0.005	4.30	0.06
A001	2314	2344		1786	0.20	24.0	0.56	0.07	0.03	3.80	0.04
A001	2344	2374		1787	0.25	25.0	0.51	0.06	0.02	4.00	0.05
A001	2374	2408		1788	0.17	8.0	0.11	0.01	0.02	4.10	0.06
R	2408	2485	:DYKE - NO SAMPLES								
A001	2485	2517		1789	0.12	13.0	0.15	0.03	0.02	3.20	0.06
A001	2517	2536		1790	0.22	27.0	0.31	0.04	0.02	5.40	0.46
A001	2536	2555		1791	0.21	20.0	0.15	0.06	0.03	3.90	0.06
A001	2555	2575		1792	0.04	8.0	0.06	0.01	0.02	5.20	0.03
A001	2575	2596		1793	0.08	6.0	0.05	0.03	0.01	7.80	0.04
A001	2596	2631		1794	0.07	8.0	0.03	0.02	0.01	5.00	0.09
R	2631	2647	:DYKE - NO SAMPLES								
A001	2647	2682		1795	0.35	15.0	0.65	0.005	0.03	4.90	0.04
A001	2682	2717		1796	0.18	12.0	0.09	0.005	0.03	5.10	0.04
A001	2717	2749		1797	0.09	23.0	0.04	0.005	0.04	4.10	0.37
R	2749	2827	:DYKE - NO SAMPLES								
A001	2827	2857		1798	0.09	13.0	0.02	0.04	0.02	5.30	0.06
A001	2857	2887		1799	0.15	24.0	0.23	0.06	0.03	4.80	0.09
A001	2887	2917		1800	0.20	41.0	0.83	0.10	0.05	4.80	0.38
A001	2917	2947		1801	0.05	10.0	0.03	0.04	0.04	5.70	0.07
A001	2947	2977		1802	0.03	6.0	0.03	0.01	0.01	4.10	0.05
A001	2977	3007		1803	0.04	8.0	0.04	0.02	0.005	4.20	0.05
A001	3007	3037		1804	0.07	6.0	0.11	0.005	0.03	4.40	0.03
A001	3037	3067		1805	0.07	7.0	0.11	0.005	0.04	4.90	0.02
A001	3067	3097		1806	0.11	10.0	0.24	0.005	0.03	4.90	0.02
A001	3097	3124		1807	0.05	8.0	0.03	0.005	0.11	4.00	0.04
A001	3124	3154		1808	0.03	8.0	0.04	0.005	0.02	3.70	0.04
A001	3154	3184		1809	0.05	17.0	0.04	0.03	0.03	4.12	0.08
A001	3184	3214		1810	0.07	39.0	0.03	0.03	0.02	5.15	0.10
A001	3214	3236		1811	0.04	8.0	0.02	0.03	0.005	3.46	0.10
R	3236	3292	:DYKE OR GABBRO - NO SAMPLES								
R			:END OF HOLE								

```
IDEN6B0201      X87CH317 NQ   MAY87DJH   JTT MAY87ACK          0.0
IPRJ            EQUITY SILVER MINES LTD        MAIN ZONE - MN GEOCODE
S000   00   610 MT  350.5 090.0 -70.0                   7976.69   8419.62   1261.83
S001  610  1600     350.5 095.5 -70.0
S002 1600  2149     350.5 099.0 -70.0
S003 2149  2637     350.5 100.5 -71.0
S004 2637  3139     350.5 102.4 -71.0
S005 3139  3414     350.5 102.4 -71.0
S006 3414  3505     350.5 104.0 -71.0
/SCL          MT.2MT.2
LSCL               MT.2       LCTM
/NAM                                                           QZSZTOPYCPTTASPRGY
LNAM                                                           DMCBCLMGHESLGLMO
/       00   243        OVBN                  P
R                 :TRICONED & CASED - NO CORE :NOT OVERBURDEN
/      243   274  25    8C01PL     P*         P              D-
L                 00         5A
R                 :WHITE, KAOLINITIZED? FELDSPAR PHENOS. (4*2 MM)
/      274   305  27    2E33MSQZ   <<         P         <-    <(
L                 00         TA
R                 :RARE PATCHES OF PY :TAN COLORED LAPILLI, MATRIX SUPPORTED
R                 :RARE BLACK SILICEOUS PATCHES
/      305   317  05    2E31MSQZ              P              D-
L                 00        6A
R                 :V. HEAVILY BROKEN INT. WITH SOME CLAY GOUGE
/      317   448        NREC                  P
R                 :ADVANCED CASING TO 44.8 M
/      448   482  30    2D33MSQZ   <<         P              <)
L                 06         5A
R                 :GOES TO 2E AS ABOVE 27.4 - 30.5 LOCALLY W/ GRAD. CNTS.
/      482   497  14    2C33MSQZ   <<         P              <)
L                 02         6A
R                 :OCCASIONAL PATCHES PY ASS. W/ DARK GREY SILICIFICATION
/      497   518  21    2E45QZMS   <<RC       P         Q=   Q1
L                 02         5A
R                 :2D 50.8-51.8 :MAINLY TAN COLORED LAPILLI IN A GREY SILICIFIED MATRIX
/      518   542  23    2D33MSQZ   <<         P BD   052<-   <)
L                 04         6A                        <.      <-
R                 :2E INTERBEDDED W/PY PATCHES IN MATRIX :2D55 LOC.(MORE SILICA AND PY)
/      542   564  22    2E41QZMS   RC         P              D(
L                 19         TA
R                 :TAN COLORED LAPILLI AND COURSE ASH FRAGS. IN A MED. GRAY
R                 :SIL. MATRIX OF FINER ASH
/      564   583  18    8D31MSQZ   P*FB       P FB   037<(   <-
L                 15         5A
R                 :GOOD SHARP, IRREGULAR CONTACTS :V.WEAKLY PORPHYRITIC:ALTERED DACITE?
/      583   610  26    2D31MSQZ   BR<<       P              <(
L                 04         6A                        <.
R                 :WEAK TECT. BXIA LOC. :V. WEAK << TEXTURE
/      610   640  30    2D33MSQZ   <<BR       P              <(        <-
L                 14         6A                        <-
R                 :2E AND 2C APPEAR LOC. :WEAK TECTONIC BXIA. LOC.
/      640   649  09    2E11CL     P*<<       P CU   040     <(        <)
L                 05         AG                 CL   024     E)
```

```
R                  :ALTERED ANDESITE BRECCIA FRAGMENTS W/ P* TEXTURE.
/     649    670   18     2D31MSQZ    BR<<         P                  J(          <)
L                  11           5A                                  <.
R                  :WEAK LOCAL TECT. BRECCIA W/ PY INFILLING
/     670    695   24     2D33MSQZ    <<           P                 <?<)         <)
L                  18           5A                                  <.
R                  :OCC. << W/ DARK GREY-BLACK HARD MINERAL (TO) : 2E LOC.
/     695    707   12     8D31MS      <<P*         P                  D)          <)
L                  08           4A
R                  :CNTS. SHARP AND IRREGULAR :VAGUE CHILLED MARGINS VISIBLE
/     707    728   19     2C33MS      <<           P                  <)
L                  08           TA
R                  :2D LOC.   :V MINOR 2E
/     728    762   33     2D33MSQZ    <<BR         P                  <+
L                  17           5A                                  <-
R                  :PALE BROWN COLOR TOWARDS E.O.I. :LOC. TECTONIC BXIA. TEXTURE
/     762    796   32     2E31MSQZ    <<RC         P                  <-
L                  19           5A                                  <-
R                  :MOD. << TEXTURE :LOC. TECT. BXIAL TEXT. WITH CL IN MATRIX
/     796   1073  273     8COOMS      P*           P
L                 183           8T
R                  :5% QZ PHENOS :10% ALTERED FELDSPAR PHENOCRYSTS
R                  :UPPER CONTACT NOT OBSERVED DUE TO GOUGE AND BRECCIATION
/    1073   1097   23     2D33MSQZ    <<           P            <)    <=
L                  05           5A                                    <+<-<)
R                  :2E LOC. :WEAK TO MODERATE << TEXTURE
/    1097   1125   26     2D32MSQZ    <<           P            <)    <=
L                  05           5A                                    <+<-<)
R                  :2C LOC.
/    1125   1157   29     2D33MSQZ    <<BR         P            <(    <)          <-
L                  19           4A                                 <-E.
R                  :2E LOC. :WEAK LOCAL TECT. BRECC. W/ CL & PY MATRIX
/    1157   1171   13     2D31MSQZ    BR           P                  I-
L                  06           5A                                  I(
R                  :WEAK LOC. TECTONIC BXIA W/ PY & CL MATRIX
/    1171   1196   25     8A10CL      P*           P CU    032
L                  17           5G                                    D)
R                  :GOOD, SHARP "INTRUSIVE" CNTS: CM @ CV ONLY: NO ATTITUDE @ CL
R                  :DUE TO BROKEN CORE
/    1196   1219   23     2F32MSQZ    RCAD         P            Q-    Q)
L                  07           5A    BR                            I-Q)Q-
R                  :INTO 2F LOC: V. WEAK LOC. TECT. BXIA: V. WEAAK LOCAL TECT.
R                  :BXIA W/PY+CL MATRIX
/    1219   1236   17     2D32MSQZ    <<           P            <)    <)
L                  14           4A                                  <)<-
R                  :WEAK << TEXT
/    1236   1267   33     8A10CL      P*           P
L                  13           5G                 CL    074          D)
R                  :CV V. IRREGULAR: CNTS "INTRUSIVE" (=SHARP W/CHILLED MARGINS)
/    1267   1280   11     2E31MSQZ    <<           P                  D-          <.
L                  04           4A
R                  :INTO 2D LOCALLY: V. WEAK << TEXT
/    1280   1310   30     2F31MSQZ    <<AD         P                  D-          <(
L                  24           4A                                  <(
R                  :INTO 2E & 2D LOC: V. WEAK << TEXT
```

```
/    1310  1341  31    2E32MSQZ   <<BR        P                 <(          <(
L                26         5A                                 <(<-
R               :V. WEAK LOC. TECT. BXIA, W/CL+PY+MG MATRIX
/    1341  1371  30    2E33MSQZ   <<BR        P           <-    <(          <-
L                21         5A                                 <(
R               :CL ALT'N IN SOME LAPILLI: INTO 2D LOC
/    1371  1386  15    2E33MSQZ   <<          P           <-    <(          <-
L                13         GA                                 <(
R               :CL ALT'N IN SOME LAPILLI :LOC 2D
/    1386  1411  25    8A10CL     P*<<        P                             <+
L                22         5G                                    D-
R               :CNT. ANGLES NOT OBSERVED DUE TO MISSING CORE
/    1411  1430  18    2D33MSQZ   <<          P           <-    <(          <-
L                09         5A                                 <(
R               :INTO 2E LOC: TECT BXIA @ LOWER CNT. W/PY+CL MATRIX &
R               :SILIFICATION OF TUFF FRAGS
/    1430  1437  07    8A10CL     <<          P CU   045                    <-
L                07         6G                  CL   030
R               :V. WEAK << TEXT: SHARP "INTRUSIVE" CNTS W/CHILLED MARGIN (WEAK)
/    1437  1463  26    2E33MSQZ   <<          P           <-    <-          <-
L                19         5A                                 <-  <.
R    1437  1463 :INTO 2D LOC.: V. WEAK << TEXT
/    1463  1493  30    2F22MSQZ   <<          P              O.  <-         <-
L                14         5A                                 <-<.<.
R               :WEAK << TEXT: INTO 2E LOC
/    1493  1523  30    2E11CLMS   <<          P                 D-          <-
L                16         GA                                 <-
/    1523  1554  30    2E13CLMS   <<          P VV   063V(      V)          <-
L                21         GA                                  V.V(
/    1554  1584  30    2E13CLMS   <<          P           Q(    Q*          <.
L                14         GA                                  Q.Q(
/    1584  1615  28    2E13CLMS   <<BR        P                 <(          <-
L                20         GA     RC                          <(  <.
R               :WEAK LOC. TEXT BXIA
/    1615  1640  24    2E13CLMS   <<RC        P           <(    <(          <.
L                12         GA     BR                          <(  <.
R               :INTO 2F LOC: V. WEAK LOC. BXIA TEXT
/    1640  1657  17    8A10CL     P*          P CU   054
L                14         5G                  CL   022
R               :V. WEAK P* TEXT: XENOLITH OF 2E (0.1M)
/    1657  1676  17    2E11CLMS   <<          P           I(O.  I(
L                09         GA                                 I(  I.
R               :CL+PY+QZ+HS+trSZ IN MATRIX (REPLACEMENT OF ORIGINAL ASHY
R               :MATRIX)
/    1676  1706  30    2D11CLMS   <<          P                 D(          <)
L                22         GA                                 <-
R               :INTO 2E LOC.
/    1706  1735  29    2E11CLMS   <<          P           D(O.  D(          <)
L                21         GA                                 D(  D-
R               :MATRIX PARTIALLY REPLACED AS ABOVE 165.7-167.6: TR. SZ IN ONE
R               :LAPILLI - NOT IN MATRIX: INTO 2F LOC.
/    1735  1768  32    8A10CL     <<P*        P CU   040                    <)
L                28         6G                  CL   028      D-
R               :STRONG P* TEXT W/PLAG PHENOS TO 20 MM LONG
/    1768  1798  30    2E11CLMS   <<          P           D)    D)          <)
```

```
L                 24       GA                                         D(
R                :INTO 2F LOC: PY+QZ+HE DISSEM IN MATRIX
/    1798  1828  30    2E11CLMS    <<RC         P          D*    D*         <)
L                 22       GA                                         D(
R                :PY+QZ+HS DISSEM IN MATRIX
/    1828  1846  18    2D33MS      <<BR         P          <(    <(
L                 08       5A                                     <-  <(
R                :WEAK LOCAL BXIA TEXT: INTO 2E LOC: NO BY
/    1846  1932  85    8C00        P*           P CU   045
L                 69       9G
R                :CL OBSCURRED IN MISSING CORE: TYPICAL LATITE DYKE: W/15%
R                :ALTERED PLAQ PHENOS
/    1932  1967  35    8A10CL      A*<<         P
L                 30       4G                      CL   035  <-  D.
R                :WEAK ARGILLIC ALT'N FOR FIRST 1.5 M: 3% AMYGDS TO 2 MM DIA (CB
/    1967  1987  19    2D31MS      <<<<         P              D(D(         <+
L                 09       VA                                        <-
R                :UNKNOWN BLACK MIN. IN DISSEMS. W/PY (TO?)
/    1987  2005  17    8D31MS      <<P*         P CU   022       D(
L                 15       6A                                <(     <(
/    2005  2023  17    8D31MS      <<P*         P                D(
L                 11       6A                      CL   065  <(     <(
/    2023  2097  72    8C00        P*           P
L                 52       5A                      CL   030
R                :NOT A TYPICAL PALE GREENISH OR TAN COLORED LATITE DYKE
R                :FAIRLY SILICEOUS
/    2097  2124  27    2E12CLMS    <<           P                Q(         <)
L                 23       GA                                  <-Q(
/    2124  2154  29    2E31MS      <<           P                D(         <(
L                 15       5A                                <(     D(
R                :POST-MIN BXIA & GOUGE FROM 214.0 TO 215.5
/    2154  2174  20    2E31MS      <<           P          D(    D(
L                 08       5A
/    2174  2194  19    8D83MSQZ    <<P*         P          <-    <-         <-
L                 18       6A                                       <-
R                :CV OBSCURRED IN BROKEN CORE
/    2194  2220  25    8D83MSQZ    <<P*         P          <-    <-
L                 24       6A                                 <-
/    2220  2237  17    8D83MSQZ    <<P*         P          <-    <-         <.
L                 14       6A                                 <-
R                :POST-MIN GOUGE & BXIA @ CL
/    2237  2280  40    8A10CL      P*           P
L                 36       5G                      CL   037      D.
R                :WEAK P* TEXT
/    2280  2290  10    2E31MS      <<           P          D(    D(         <-
L                 09       5A
/    2290  2330  38    8A11CL      P*<<         P                D-         <)
L                 33       AG                                 <.<-
/    2330  2347  15    2E32MS      <<           P          Q1    Q1         <-
L                 12       5A                                   Q+Q+Q-
R                :0.3 M 2E52
/    2347  2377  30    2E33MS      <<           P                <)         <-
L                 21       5A                                   <*
R                :INTO 2E43 LOC
/    2377  2408  31    2D21MS      <<BR         P              O.  D)       <-
```

```
L                  23        5A                                 <*
R                 :WEAK LOCAL BXIA TEXT: INTO 2D52 LOC (DARK GREY)
/    2408  2438   30     2D32MS      <<         P                <)        <-
L                  26        5A                                 <-<)<-
R                 :INTO 2D52 (DARK GREY) LOC.: INTO 2E LOC
/    2438  2469   30     2D32MS      <<         P                <)        <-
L                  26        5A                                 <-<)
R                 :INTO 2E LOC: 8A 245.5 - 246.0
/    2469  2496   27     2D32MSQZ    <<         P                Q)        <)
L                  23        6A                                 <(Q*
R                 :INTO 2E LOC
/    2496  2530   33     8A10CL      P*<<       P CU   033                 <)
L                  30        5G                                    D(
R                 :LOWER CNT SHARP & IRREGULAR
/    2530  2560   28     2D32MSQZ    <<BR       P                <)        <-
L                  21        5A                                 <)<*
R                 :WEAK LOCAL BXIA. TEXT W/CL+PY+QZ MATRIX
/    2560  2591   29     2D22MSQZ    <<BR       P           O.   Q=Q)      <-
L                  22        5A                                    Q+
R                 :WEAK LOCAL BXIA TEXT W/PY+QZ MATRIX
/    2591  2621   30     2D12CLMS    <<BR       P         #(     <)        <-
L                  24        GA                                #(<)
R                 :WEAK LOCAL BXIA TEXT W/PY+QZ+CL MATRIX: 0.3 M MASSIVE XTL. TUFF
R                 :INTO 2E LOC.
/    2621  2635   14     2E12CLMS    <<         P                <)
L                  10        GA                                 <-<(
/    2635  2652   16     8A10CL      P*         P CU   080
L                  14        AG                   CL   060
R                 :FAIRLY SHARP CNTS: NO CHILLED MARGINS
/    2652  2682   30     2D12CLMS    BR<<       P         #+      #+       <-
L                  25        AG                                #)#)   #*
R                 :WEAK LOCAL BXIA TEXT W/PY+MG+CL+SL MATRIX AND REPLACEMENTS
R                 :V. WEAK << TEXT
/    2682  2713   29     2D12CLMS    <<<<       P         <(     Q)O.      <-
L                  22        AG      BR                         <(Q*
R                 :WEAK LOCAL BXIA TEXT
/    2713  2743   30     2D12CLMS    <<BR       P         <(     <)        <(
L                  23        AG                                 <(<(
R                 :WEAK LOCAL BXIA TEXT
/    2743  2774   30     2D22MS      <<BR       P                <(        <(
L                  25        5A                                 <-<-
R                 :WEAK LOCAL BXIA TEXT: INTO 2E LOC.
/    2774  2804   30     2D22MS      <<BR       P           <)   Q+        <-
L                  17        5A                                 <-<)Q)
R                 :WEAK BXIA THROUGHOUT INT.: INTO 2E LOC
/    2804  2835   30     2E11CLMS    <<         P         I(     I(        <-
L                  21        GA                                  I(
R                 :PY+CL+QZ IN MATRIX: V. WEAK << TEXT: W/ASH
/    2835  2860   24     2E11CLMS    <<         P         I(     I(        <-
L                  18        GA                                  I(
R                 :TO 2D LOCALLY: V. WEAK << TEXT: AS ABOVE 280.4-283.5
/    2860  2875   15     2E12CLMS    <<         P         I(     I(        <-
L                  14        GA                                  I(I-
R                 :AS ABOVE 280.4-283.5: V. WEAK << TEXT
/    2875  2922   46     8A10CL      P*<<       P CU   035                 <)
```

```
L                  37        AG                      CL    012       D-
R                  :WEAK P* TEXT: SHARP INTRUSIVE CNTS W/CHILLED MARGINS
/     2922  2956   34    2D31MS     <<BR          P            #)     #)
L                  27        5A                                     #(
R                  :WEAK LOCAL BXIA TEXT: 0.3 M 2D54: PY+CL+QZ IN BXIA MATRIX
R                  :0.4 M 8A: INTO 2E LOC
/     2956  2986   30    2D31MS     <<BR          P            Q-     Q(
L                  14        5A                                   <-Q-Q-
R                  :.1 M PATCH OF PY+HE+QZ+MG
/     2986  3017   30    2D11CL     <<            P                   <-        <+
L                  19        5G                                   <-
/     3017  3048   30    2D11CL     <<            P                   D-        <(
L                  24        5G                                 <-
/     3048  3078   30    2D12CL     <<            P                   <(        <(
L                  22        5G                                 <-O-<-
R                  :V. DISTINCTIVE W/ CL+PY SPOTS TO 2 MM DIA (10%) - XTH TUFF?
/     3078  3109   30    2D11CL     <<            P                   O(        <-
L                  22        6G                                 <(O-
R                  :AS ABOVE 304.8-307.8 MINOR PINK CO3
/     3109  3139   30    2D12CL     <<            P                   <(        <-
L                  24        5G                                   <-<-<-
R                  :AS ABOVE 304.8-307.8 TO APPROX 313 M THEN GRADTIONAL CNT TO
R                  :NORMAL 2D
/     3139  3169   30    2E13CLMS   <<            P                   <(        <-
L                  21        GA                                   <-
R                  :INTO 2D41 LOC: INTO 2D LOC
/     3169  3200   30    2D12CLMS   <<BR          P            D(     D(        <-
L                  18        GA                                   <-D-
R                  :INTO 2E LOC: TR. PINK CO3
/     3200  3231   30    2E12CLMS   <<            P                   <(        <-
L                  21        GA                                   <-<-
R                  :INTO 2D LOC
/     3231  3261   30    2E12CL     <<            P            Q-     Q(        <-
L                  18        5G                                   Q-Q)
/     3261  3291   30    2D12CL     <<            P            Q-     Q(        <.
L                  12        5G                                   Q-Q(
R                  :TO 2E LOC
/     3291  3322   29    2D12CL     <<            P            Q-     Q(
L                  19        5G                                   Q-Q(
R                  :TO 2E LOC
/     3322  3352   30    2D32MSKA   <<            P            Q-     Q(        <-
L                  22        GA                                 <(<+Q(
R                  :TO 2E LOC: 0.1 M 7C (SPUR OFF MAIN BODY?)
/     3352  3505         7COOPL     P*<<          P                             <-
L                            4A                                       D)
R                  :SMALL PINKISH APLITE? VNLTS: CNT GRAD OVER 2 CM (ASSIMILATED?)
R                  :EOH @ 350.5 M
A001
ALAB               EQUITY MINESITE LABORATORY
ATYP               ASSAY
AMTH               WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM               RCOVSAMPLE   RQD % CU   G/TAG G/TAU % SB   % AS   % FE   % ZN
R       00    243  :TRICONED AND CASED - NO CORE
A001   243    274       1681       0.01    12.0 0.09   0.03   0.005 2.34   0.02
A001   274    305       1682       0.005    9.0 0.04   0.03   0.005 2.30   0.005
```

A001	305	317	1683	0.005	9.0	0.07	0.01	0.005	1.06	0.005
R	317	448	:NO CORE - CASING ADVANCED TO 44.8 M							
A001	448	482	1684	0.005	10.0	0.04	0.01	0.005	2.41	0.01
A001	482	497	1685	0.005	10.0	0.04	0.04	0.01	8.36	0.02
A001	497	518	1686	0.005	8.0	0.95	0.05	0.03	15.37	0.04
A001	518	542	1687	0.005	10.0	0.07	0.02	0.005	4.45	0.09
A001	542	564	1688	0.02	9.0	0.06	0.005	0.005	1.58	0.005
A001	564	583	1689	0.02	8.0	0.05	0.01	0.005	1.48	0.02
A001	583	610	1690	0.005	10.0	0.06	0.01	0.005	2.11	0.03
A001	610	640	1691	0.01	12.0	0.08	0.01	0.005	2.14	0.03
A001	640	649	1692	0.005	8.0	0.04	0.02	0.005	4.49	0.03
A001	649	670	1693	0.005	11.0	0.05	0.03	0.01	3.64	0.04
A001	670	695	1694	0.005	3.0	0.06	0.02	0.005	3.64	0.03
A001	695	707	1695	0.005	1.0	0.05	0.005	0.005	3.59	0.04
A001	707	728	1696	0.005	0.5	0.04	0.005	0.005	1.79	0.005
A001	728	762	1697	0.005	2.0	0.05	0.005	0.005	3.15	0.01
A001	762	796	1698	0.005	3.0	0.04	0.005	0.005	2.52	0.02
R	796	1073	:DYKE - NO SAMPLES							
A001	1073	1097	1699	0.01	3.0	0.06	0.005	0.005	2.50	0.02
A001	1097	1125	1700	0.01	11.0	0.17	0.005	0.04	5.32	0.91
A001	1125	1157	1701	0.01	0.5	0.08	0.01	0.005	2.04	0.03
A001	1157	1171	1702	0.005	0.5	0.05	0.01	0.005	0.90	0.02
R	1171	1196	:DYKE - NO SAMPLES							
A001	1196	1219	1703	0.005	3.0	0.06	0.005	0.005	2.56	0.02
A001	1219	1236	1704	0.005	0.5	0.05	0.03	0.005	2.97	0.06
R	1236	1267	:DYKE - NO SAMPLES							
A001	1267	1280	1705	0.005	3.0	0.09	0.005	0.005	2.77	0.03
A001	1280	1310	1706	0.03	4.0	0.08	0.01	0.005	2.86	0.03
A001	1310	1341	1707	0.02	6.0	0.08	0.02	0.005	2.09	0.06
A001	1341	1371	1708	0.005	2.0	0.06	0.01	0.005	1.73	0.03
A001	1371	1386	1709	0.005	6.0	0.51	0.01	0.005	2.78	0.02
R	1386	1411	:DYKE - NO SAMPLES							
A001	1411	1430	1710	0.005	3.0	0.07	0.01	0.005	2.15	0.01
R	1430	1437	:DYKE - NO SAMPLE							
A001	1437	1463	1711	0.01	18.0	0.11	0.005	0.005	1.11	0.01
A001	1463	1493	1712	0.03	44.0	0.32	0.005	0.005	2.53	0.02
A001	1493	1523	1713	0.005	2.0	0.42	0.005	0.005	1.48	0.005
A001	1523	1554	1714	0.005	2.0	0.09	0.005	0.005	1.71	0.005
A001	1554	1584	1715	0.005	3.0	0.11	0.005	0.005	2.46	0.005
A001	1584	1615	1716	0.005	2.0	0.18	0.005	0.005	2.32	0.005
A001	1615	1640	1717	0.005	3.0	0.09	0.005	0.005	2.46	0.005
R	1640	1657	:DYKE - NO SAMPLES							
A001	1657	1676	1718	0.005	4.0	0.14	0.005	0.005	3.34	0.005
A001	1676	1706	1719	0.006	2.0	0.05	0.005	0.005	2.13	0.02
A001	1706	1735	1720	0.005	2.0	0.03	0.005	0.005	1.50	0.005
R	1735	1768	:DYKE - NO SAMPLES							
A001	1768	1798	1721	0.005	3.0	0.07	0.005	0.005	1.81	0.005
A001	1798	1828	1722	0.005	2.0	0.05	0.005	0.005	1.72	0.005
A001	1828	1846	1723	0.005	4.0	0.08	0.005	0.005	1.72	0.005
R	1846	1967	:DYKE - NO SAMPLES							
A001	1967	1987	1724	0.005	0.5	0.03	0.005	0.005	1.57	0.005
A001	1987	2005	1725	0.005	0.5	0.05	0.005	0.005	3.26	0.005
A001	2005	2023	1726	0.005	0.5	0.02	0.005	0.005	2.36	0.005
R	2023	2097	:DYKE - NO SAMPLES							
A001	2097	2124	1727	0.06	45.0	0.49	0.005	0.005	1.84	0.04

A001	2124	2155	1728	0.005	7.0	0.19	0.005	0.005	2.30	0.04
A001	2155	2174	1729	0.06	11.0	0.09	0.005	0.005	2.12	0.04
A001	2174	2194	1730	0.005	2.0	0.03	0.005	0.005	2.61	0.005
A001	2194	2220	1731	0.005	0.5	0.05	0.005	0.005	2.93	0.005
A001	2220	2237	1732	0.005	0.5	0.03	0.005	0.005	2.79	0.005
R	2237	2280	:DYKE - NO SAMPLES							
A001	2280	2290	1733	0.005	0.5	0.07	0.005	0.005	1.39	0.005
R	2290	2330	:DYKE - NO SAMPLES							
A001	2330	2347	1734	0.005	3.0	0.24	0.005	0.07	7.93	0.005
A001	2347	2377	1735	0.04	59.0	0.41	0.005	0.005	2.42	0.07
A001	2377	2408	1736	0.02	6.0	0.46	0.005	0.005	2.59	0.005
A001	2408	2438	1737	0.005	2.0	0.12	0.005	0.005	2.10	0.005
A001	2438	2469	1738	0.005	2.0	0.22	0.005	0.005	2.20	0.005
A001	2469	2496	1739	0.02	6.0	0.14	0.005	0.005	2.20	0.02
R	2496	2530	:DYKE - NO SAMPLES							
A001	2530	2560	1740	0.02	4.0	0.13	0.005	0.005	3.17	0.03
A001	2560	2591	1741	0.15	16.0	0.24	0.005	0.005	4.48	0.02
A001	2591	2621	1742	0.06	13.0	0.18	0.005	0.005	3.34	0.03
A001	2621	2635	1743	0.03	9.0	0.29	0.005	0.005	2.98	0.03
R	2635	2652	:DYKE - NO SAMPLE							
A001	2652	2682	1744	0.05	14.0	0.20	0.005	0.005	4.46	0.72
A001	2682	2713	1745	0.04	10.0	0.30	0.005	0.005	3.61	0.02
A001	2713	2743	1746	0.03	5.0	0.12	0.005	0.005	2.24	0.03
A001	2743	2774	1747	0.005	0.5	0.06	0.005	0.005	1.90	0.01
A001	2774	2804	1748	0.01	2.0	0.06	0.005	0.005	2.70	0.01
A001	2804	2835	1749	0.005	0.5	0.05	0.005	0.005	2.40	0.01
A001	2835	2860	1750	0.005	0.5	0.05	0.005	0.005	2.20	0.01
A001	2860	2875	1751	0.005	0.5	0.06	0.005	0.005	2.60	0.01
R	2875	2922	:DYKE - NO SAMPLES							
A001	2922	2956	1752	0.005	0.5	0.02	0.005	0.005	3.10	0.01
A001	2956	2986	1753	0.005	2.0	0.03	0.005	0.005	5.10	0.01
A001	2986	3017	1754	0.01	2.0	0.02	0.005	0.005	2.00	0.01
A001	3017	3048	1755	0.005	0.5	0.02	0.005	0.005	2.00	0.01
A001	3048	3078	1756	0.005	0.5	0.01	0.005	0.005	2.80	0.01
A001	3078	3109	1757	0.005	0.5	0.02	0.005	0.005	2.20	0.01
A001	3109	3139	1758	0.005	0.5	0.03	0.005	0.005	2.60	0.01
A001	3139	3169	1759	0.07	3.0	0.07	0.005	0.005	3.20	0.02
A001	3169	3200	1760	0.01	3.0	0.04	0.005	0.005	2.40	0.01
A001	3200	3231	1841	0.04	5.0	0.09	0.02	0.005	3.00	0.01
A001	3231	3261	1842	0.02	4.0	0.04	0.02	0.005	2.20	0.01
A001	3261	3291	1843	0.02	7.0	0.57	0.02	0.005	2.40	0.02
A001	3291	3322	1844	0.09	9.0	0.06	0.005	0.005	2.20	0.02
A001	3322	3352	1845	0.02	3.0	0.07	0.005	0.005	2.70	0.01
R	3352	3505	:MONZONITE - NO SAMPLES							
R			:EOH @ 350.5 M							

```
IDEN6B0201        X87CH318 NO   MAY87RBP   JTT MAY87ACK         0.0
IPRJ          EQUITY SILVER MINES LTD         MAIN ZONE - MN GEOCODE
S000   00    120 MT   377.9 090.0 -49.5              8118.53   8328.67   1295.17
S001  120    654      377.9 091.0 -49.0
S002  654   1341      377.9 094.6 -44.0
S003 1341   1996      377.9 097.0 -44.0
S004 1996   2606      377.9 100.3 -44.0
S005 2606   3078      377.9 102.3 -44.5
S006 3078   3505      377.9 104.4 -45.0
S007 3505   3734      377.9 106.0 -46.0
S008 3734   3779      377.9 106.0 -46.0
/SCL          MT.2MT.2
LSCL             MT.2       LCTM
/NAM                                                        QZSZTOPYCPTTASPRGY
LNAM                                                        DMCBCLMGHESLGLMO
/       00     91        OVBN               P
R                :TRICONED AND CASED TO 9.1 - NO CORE
/       91    185  83    8COOFL     <<P*    P          I)    D.
L                  20        WA                              D)  D.
R                :LOWER C/ BROKEN, BECOMES DARKER GREY IN LAST 0.5 M
R                :FE STAIN ON <<'S
/      185    237  30    2G31       <<      P          <*    <*
L                  03        6A                                 <-
R                :LOC 2H, VERY BROKEN
/      237    259  20    2H31       <<      P          <(    <)
L                  00        6A
R                :LOC 2G
/      259    287  26    2H31       <<BR    P          <(    <)
L                  00        TA                            <-
/      287    305  17    2G31       <<      P          <(    <*
L                  00        6A                            <-
/      305    362  31    2E31       <<BR    P          <-    <)
L                  00        TA                            <-
R                :LOC 2C 0.2 M OF CORE FROM 31.7 TO 33.8
/      362    446  80    8COOFL     <<P*    P          I(    D.
L                  36        WA                                 <.
R                :C/'S BROKEN
/      446    480  32    2E31       <<      P          <-    <*  <?
L                  06        TA                                 <-
R                :POSSIBLE TT IN << AT 47.0
/      480    490  09    8A00       <<CM    P CU    35<*     D.
L                  03        UG               CL    40       D.
R                :SMALL XENO OF 2C AT 48.3
/      490    515  23    2E31       <<BR    P          <-  D?<)
L                  03        TA                                   D.
R                :F/ GOUGE AT 51.2
/      515    557  40    2F31       BR<<    P              D?<)D.
L                  06        TA                                   D.
R                :ABUN SHARDS
/      557    568  11    8BOOFL     P*      P
L                  00         2A              CL    70       D.
/      568    594  24    8COOFL     P*      P                D.
L                  00        WA
R                :MINOR INTERCALATED 2E.  C/'S BROKEN
/      594    631  35    8A00       <<      P          <-    D.
```

```
L               12        AG                                          D-
R             :RARE FL PHENO, C/ GRADATIONAL
/     631   830 190     8COOFL      <<P*        P           <-       D.
L               15        WA
R             :PATCHES OF DARKER GREY.  VERY BROKEN
/     830   855  24     8AOOFL      <<          P           <*       D.
L               15        4G                     CL     25
R             :MINOR FL PHENOS
/     855   884  28     8BOOFL      <<P*        P           <)     <-
L               16        AG                                      D*
/     884   917  31     2E93        <<BR        P           <)    R-<+D.
L               03        TA                                      <(     D.
R             :TWO 0.1 M INTENSE BR ZONES
/     917   921  04     8B10        P*<<        P CU    50M.     D.
L               03        AG                     CL     35    D=  <-
/     921   950  28     2E91        <<BR        P           <-   R.<+D.
L               03        AT                                      <+
R             :SLIGHT BR'N
/     950   980  29     2E91        BR<<        P           <*   R.<)D.
L               00        AT                                      <(
R             :MORE INTENSE BR'N
/     980  1010  29     2F91        BR<<        P           <(   R(<+
L               03        AT                                      <*
/    1010  1040  28     2F91        BR<<        PP          <-   R-<+<.
L               03        AT                                      <)
/    1040  1070  29     2F91        B4<<        P           <*   R.<)
L               03        AT                                      <*
/    1070  1094  23     2F91        B4<<        P           <-   R.<)
L               03        AT                                      <(
R             :LESS TO, BUT STILL INTENSE BR'N
/    1094  1110  16     8A00        <<          P CU    30<+      D.
L               06        6G                     CL     45     <-D.
R             :XENOLITH OF 2F91 FROM 109.7 TO 109.9 M
/    1110  1140  28     2F91        <<          P           <-Q.R-<)
L               03        AT                                      <*
R             :VERY BROKEN
/    1140  1168  27     2E31        <<          P           <-     <)
L               00        TA                                      <(
/    1168  1193  24     2E31        <<VU        P           <-   <.<+
L               03        TA                                      <*
/    1193  1230  36     2E91        <<          P           <-   R-<)
L               09        BR                                      <.
/    1230  1266  36     2E91        <<          P           <*   D-<+
L               12        TA                                           D-
/    1266  1331  64     8A10        <<CM        P CU    35<-      D.
L               24        6G                     CL     70     D+D-<-
/    1331  1360  28     2E91        <<VU        P           <(   <*<+
L               03        RA                                      <(
R             :F/ GOUGE AT 135.0 M
/    1360  1390  28     2E91        <<VU        P           <*   <*<+
L               00        TA                                      <)
R             :NOT SURE IF ALL << TO IS TO, POSSIBLE CL INTERMIXED
/    1390  1420  29     2E91        <<          P           <-   <-<)
L               09        RA                                      <*
R             :LAPILLI INDISTINCT
```

```
/    1420  1445  25    2E41       <<          P          <-  <.<)        <.
L                11         TA                               <*
R               :MINOR 2I
/    1445  1467  22    2I91       <<          P          <-  <(<)
L                09         TA                               <*
R               :NOT COMPLETELY 2I, SOME 2E
/    1467  1500  32    2I91       <<          P          <(  <(<)        <*
L                06         TA                               <-
R               :SOME 2E
/    1500  1530  30    2I51       <<          P          <-  <)<*        <*
L                19         WA                               <-
R               :SOME 2E
/    1530  1567  36    2I51       <<          P          <-  D?<*        <(
L                15         WA                               <-
R               :ABUN FINE BLACK PHENOS, TO?
/    1567  1607  39    2E91       <<BR        P          <-  <(<)        <-
L                18         TA                               <*
R               :BR'D TOWARDS EOI
/    1607  1639  31    8B10FL     <<P*        P CL    40<-    <.         <)
L                18         6G                               D+   <.
R               :CU BR'D INTO ABOVE INTERVAL
/    1639  1670  30    2E31       <<          P          <*  <?<)        <*
L                09         TA                               <)
/    1670  1688  15    2C81       <<          P          <(  <?<)        <-
L                00         AT                               <*
R               :LOC 2I AT TOI
/    1688  1715  26    2D31       MX          P          <.     Q+
L                06         GA                               D)
/    1715  1742  26    2D31       MX          P          <-     Q)
L                06         GA                               D)
R               :AS ABOVE
/    1742  1770  28    2D31       MX          P          <.     Q+
L                09         GA                               D+
R               :AS ABOVE. LIGHT GREY METALLIC FINELY DISSEM'D
R               :168.8 TO 177.0 COULD BE A VOLCANIC FLOW
/    1770  1853  80    8A00       MXCM        P CU    55<-                 <-
L                32         5G                  CL    70        D.
/    1853  1886  32    2E11CL     <<          P          <-     <)
L                12         AG                               <+  <-
R               :TRANSITION FROM PALE GRAY TUFFS ABOVE INTO TYPICAL TUFF NOW
/    1886  1920  33    2E11CL     <<          P          <-     Q+         <)
L                15         AG                                     Q(
/    1920  1950  30    2E21       <<BR        P          <-Q-   Q+         <-
L                12         AG                               <(  Q-
/    1950  1983  32    2E11       <<BR        P          <-     Q)         <*
L                09         AG                               <(  Q-
/    1983  1990  07    8A00       <<          P CU    50<*
L                06         6G                  CL    60        D.
/    1990  2021  31    2E11CL     <<BR        P          <-     Q+         <-
L                09         AG                                     Q-
/    2021  2050  28    2E12       <<          P          <-     D+         <*
L                11         AG                                  D(Q-
/    2050  2082  31    2E11       <<BR        P                 Q)         <-
L                15         AG                                  D.Q-
/    2082  2104  21    2E11       <<BR        P          <*     <)
```

```
L                 06          AG                                           <*
R                :LOC 2C11
/    2104   2140  35      8B10FL      P*           P CU     70       D.
L                 21          6G                                         D+D.
R                :XENOLITH OF 2E BETWEEN DYKES
/    2140   2219  78      8C10FL      P*CM         P              <-
L                 46          GW                     CL     50
/    2219   2252  31      2E42        <<           P              <-     Q+<(       <-
L                 11          GA                                       <-Q)
R                :LOC 2C
/    2252   2300  47      2E11        <<BR         P              <-     <(         <)
L                 20          AG                                       <)
R                :LOC 2C11
/    2300   2310  10      8A10        <<           P CU     40       D*             <*
L                 06          GT                     CL     50
R                :STRANGE DYKE - POSSIBLE FLOW ?
/    2310   2326  15      2E11        <<BR         P              <-     <(         <)
L                 06          AG
/    2326   2354  27      2E11        <<BR         P              <-     D*         <-
L                 09          AG                                       <)
R                :CLAY IN <<'S
/    2354   2383  28      2E11        <<BR         P              <-     D*
L                 12          AG                                       *)
/    2383   2413  29      2E12        <<BR         P              <-     Q+
L                 03          AG                                       <*Q*Q(
/    2413   2430  16      2E42        <<           P              <)     <+
L                 03          GA                                       <)<-<)
/    2430   2463  31      2E21        <<           P              <*     <)<.
L                 09          GA                                       <)<-<-
R                :LOC 2D41
/    2463   2488  24      2E11        <<           P              <)     <*
L                 11          GA                                       <*  <-
R                :LOC 2E41, SOME 2D
/    2488   2634 143      8B00FL      <<P*         P              <-
L                 39          6G                                       D*D.
R                :FINER GRAINED NEAR BOTTOM
/    2634   2660  24      2E43        <<           P              <(     <)
L                 03          GA                                       <-  <*<.
/    2660   2687  26      2E21        <<           P              <-Q(   <+
L                 00          GA                                       <)  <*
/    2687   2706  18      2E52        <<MX         P                     Q2
L                 06          2G                                       <)Q+Q)
/    2706   2743  36      2E22        <<           P              <-Q.   <)
L                 09          GA                                       <)<*
/    2743   2763  20      8A00        <<CM         P CU     55<*                    <-
L                 12          2G                     CL     50       D.
/    2763   2796  33      2E41        <<BR         P              <)     <+<.       <-
L                 16          GA                                       <(  <*
R                :LOC 2C, LOC 2E51
/    2796   2819  23      2E11        <<           P              <-     <)<.       <.
L                 00          GA                                       <-
R                :LOC 2C
/    2819   2846  27      2E41        <<BR         P              <)     D)         <-
L                 06          AG                                       <)  <-
/    2846   2876  30      2E51        <<BR         P              <-     D)         <-
```

```
                    09        AG                                  Q?  <)
L                  :RARE LAVENDER SPOTS, DM ?
R    2876  2908    32     2E11       <<          P          <-     Q*          <)
/                  19         GA                                 <)<_<(
L                  :LOC 2D
R    2908  2926    18     2E41       <<          P          <(     <(          <(
/                  06         GA                               <*
L    2926  2956    30     2E42       <<          P          <-     Q=D.        <-
/                  18         GA                               <)Q(   <(
L                  :LOC 2C
R    2956  2985    29     2E42       <<          P          <-Q.   D+          <(
/                  16         GA                               <(D-
L                  :VERY MINOR SZ
R    2985  3052    65     8A00       <<VU        P CU   55<-                   <-
/                  28         6G     CM                            D.D-
L    3052  3078    26     2E11       <<          P          <-     D)          <+
/                  12         AG                               <)
L                  :F/ GOUGE ON UPPER CONTACT
R    3078  3109    31     2E42       <<          P          <-     D+          <(
/                  16         GA                               <+D(
L                  :LOC 2D42
R    3109  3139    30     2E11       <<          P          <-     <*          <+
/                  09         AG                               <)
L    3139  3170    31     2E11       <<          P          <(     <(          <)
/                  11         AG                               <)
L    3170  3200    30     2E11       <<          P          <-     Q*          <*
/                  16         AG                               <+  D-
L    3200  3235    34     2D11       <<          P          <-     Q(          <(
/                  12         7G                               <)
L                  :LOC 2E
R    3235  3304    68     8B00FL     <<CM        P CU   50<-                   <*
/                  41         4G     P*            CL   40     D+D.
L                  :FINER GRAINED TOWARDS EOI
R    3304  3322    18     2E11       <<          P          <-     D*          <-
/                  03         AG                               <+  <-
L    3322  3352    30     2E11       <<          P          <(                 <-
/                  09         AG                               <)D+
L                  :LOC 2D
R    3352  3383    31     2D11       <<          P          <(     D*
/                  12         5G                               <+
L                  :LOC 2C
R    3383  3413    30     2E14       <<          P          <-     D+D.     D*
/                  15         AG                               <)
L                  :PATCH OF PR-CP AT 341.0
R    3413  3450    36     2E44       <<          P          <(     D=D*     D+
/                  12         AG                               <-
L                  :SOME QZ-MS ALT'N OF LAPILLI
R    3450  3486    36     2E21       <<          P          <-Q.   D)          <-
/                  16         UG                               <*
L                  :SOME 2D11
R    3486  3509    23     8C00       <<P*        P CU   65<-   D.
/                  12         GW     CM            CL   60
L    3509  3520    11     8A00       MXCM        P                 D.
/                  03         6G                   CL   55         D.
L    3520  3529    09     2E41       <<BR        P          <-     D+
/
```

```
L                 06        AG                                      <-
/    3529  3543   14      BA00        <<            P  CU     50<*
L                 06        7G                         CL     70    <-D.
/    3543  3566   23      2E11        <<            P           <-     D*
L                 12        AG                                      <+
/    3566  3596   30      2E22        <<            P           <-Q.   D+
L                 12        AG                                      <)D(
R                 :QZ-MS ALT'N OF SOME LAPILLI
/    3596  3626   30      2E11        <<BR          P           <-     D)
L                 15        AG                                      <*D.
/    3626  3657   30      2E11        <<            P           <.     D*
L                 09        GA                                      <)D.
/    3657  3687   30      2E11        <<BR          P           <*     D(
L                 11        GA                                      <+D.<.R
R                 :0.3 M OF 8A AT EOI
/    3687  3718   30      2E41        <<            P           <-     D*
L                 15        GA                                      <+  <(
R                 :LOC 2E11
/    3718  3748   30      2E42        <<            P           <-     D+        D.
L                 17        GA                                      <)D-
R                 ::OC 2E11
/    3748  3779   31      2E41        <<            P           <-     D)
L                 18        GA                                      <+D.
R                 :LOC 2D
R                 :MAYBE HOLE SHOULD HAVE CONTINUED
R                 :END OF HOLE 377.9
A001
ALAB              EQUITY MINESITE LABORATORY
ATYP              ASSAY
AMTH              WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM              RCOVSAMPLE   RQD % CU   G/TAG G/TAU % SB   % AS   % FE   % ZN
R       00    91  :TRICONED - NO CORE
R       91   185  :DYKE - NO SAMPLE
A001   185   237        1881       0.06     3.0 0.11  0.02  0.005 3.10   0.16
A001   237   259        1882       0.02     7.0 0.04  0.02  0.005 1.90   0.04
A001   259   287        1883       0.01     4.0 0.05  0.02  0.005 3.40   0.18
A001   287   305        1884       0.005    3.0 0.04  0.02  0.01   2.50  0.12
A001   305   362        1885       0.005    0.5 0.01  0.005 0.01   1.70  0.03
R      362   446  :DYKE - NO SAMPLE
A001   446   480        1886       0.03    34.0 0.11  0.07  0.03   2.30  0.10
R      480   490  :DYKE - NO SAMPLE
A001   490   515        1887       0.005    6.0 0.13  0.03  0.01   5.60  0.08
A001   515   557        1888       0.005    3.0 0.07  0.005 0.01   2.10  0.04
R      557   884  :DYKES - NO SAMPLES
A001   884   917        1889       0.01    18.0 0.13  0.04  0.005 2.50   0.07
R      917   921  :DYKE - NO SAMPLE
A001   921   950        1890       0.005    3.0 0.24  0.005 0.02   5.80  0.09
A001   950   980        1891       0.005    3.0 0.02  0.005 0.005 2.20   0.09
A001   980  1010        1892       0.005    2.0 0.04  0.005 0.005 3.20   0.13
A001  1010  1040        1893       0.005    2.0 0.02  0.005 0.005 2.80   0.19
A001  1040  1070        1894       0.02    13.0 0.20  0.005 0.005 4.10   0.21
A001  1070  1094        1895       0.005    1.0 0.01  0.005 0.005 0.80   0.14
R     1094  1110  :DYKE - NO SAMPLE
A001  1110  1140        1896       0.001    0.5 0.09  0.005 0.02   2.05  0.02
A001  1140  1168        1897       0.005    0.5 0.05  0.005 0.02   2.66  0.02
```

A001	1168	1193	1898	0.001	0.5	0.67	0.005	0.02	2.06	0.11
A001	1193	1230	1899	0.001	0.5	0.03	0.005	0.005	1.41	0.03
A001	1230	1266	1900	0.001	0.5	0.15	0.03	0.005	1.76	0.06
R	1266	1331	:DYKE - NO SAMPLE							
A001	1331	1360	1901	0.001	0.5	0.02	0.03	0.03	1.24	0.07
A001	1360	1390	1902	0.005	1.0	0.005	0.005	0.005	3.50	0.06
A001	1390	1420	1903	0.005	0.5	0.005	0.005	0.005	1.30	0.02
A001	1420	1445	1904	0.005	0.5	0.005	0.005	0.005	0.40	0.005
A001	1445	1467	1905	0.005	0.5	0.005	0.005	0.005	1.10	0.005
A001	1467	1500	1906	0.005	0.5	0.005	0.005	0.005	0.40	0.005
A001	1500	1530	1907	0.005	0.5	0.19	0.005	0.005	0.50	0.005
A001	1530	1567	1908	0.005	0.5	0.01	0.005	0.005	0.70	0.005
A001	1567	1607	1909	0.005	0.5	0.005	0.005	0.005	1.50	0.005
R	1607	1639	:DYKE - NO SAMPLE							
A001	1639	1670	1910	0.005	0.5	0.005	0.005	0.005	0.50	0.005
A001	1670	1688	1911	0.005	0.5	0.01	0.005	0.005	1.90	0.005
A001	1688	1715	1912	0.005	0.5	0.005	0.005	0.005	2.40	0.005
A001	1715	1742	1913	0.005	0.5	0.01	0.005	0.05	1.40	0.01
A001	1742	1770	1914	0.005	0.5	0.005	0.005	0.05	1.40	0.01
R	1770	1853	:DYKE - NO SAMPLE							
A001	1853	1886	1915	0.005	4.0	0.005	0.005	0.01	3.30	0.005
A001	1886	1920	1916	0.01	6.0	0.09	0.005	0.005	3.70	0.02
A001	1920	1950	1917	0.04	9.0	0.17	0.005	0.005	3.50	0.03
A001	1950	1982	1918	0.005	4.0	0.06	0.005	0.005	3.10	0.02
R	1983	1990	:DYKE - NO SAMPLE							
A001	1990	2021	1919	0.005	4.0	0.12	0.005	0.005	3.40	0.01
A001	2021	2050	1920	0.02	10.0	0.15	0.005	0.02	4.20	0.02
A001	2050	2082	1961	0.005	3.0	0.07	0.005	0.01	3.20	0.01
A001	2082	2104	1962	0.005	3.0	0.13	0.005	0.005	2.10	0.03
R	2104	2219	:DYKE - NO SAMPLE							
A001	2219	2252	1963	0.005	0.5	0.36	0.005	0.01	2.60	0.02
A001	2252	2300	1964	0.005	0.5	0.09	0.005	0.005	1.40	0.04
R	2300	2310	:DYKE - NO SAMPLE							
A001	2310	2326	1965	0.005	0.5	0.23	0.005	0.005	1.00	0.01
A001	2326	2354	1966	0.005	0.5	0.11	0.005	0.005	2.90	0.02
A001	2354	2383	1967	0.03	3.0	0.20	0.005	0.005	3.30	0.03
A001	2383	2413	1968	0.09	20.0	0.49	0.005	0.02	4.70	0.05
A001	2413	2430	1969	0.005	1.0	0.06	0.005	0.01	6.70	0.02
A001	2430	2463	1970	0.02	3.0	0.08	0.005	0.01	3.10	0.03
A001	2463	2488	1971	0.005	2.0	0.08	0.005	0.02	3.60	0.02
R	2488	2634	:DYKE - NO SAMPLE							
A001	2634	2660	1972	0.01	0.5	0.04	0.005	0.005	1.90	0.05
A001	2660	2687	1973	0.005	3.0	0.005	0.01	0.005	3.00	0.02
A001	2687	2706	1974	0.06	21.0	0.18	0.01	0.07	13.90	0.02
A001	2706	2743	1975	0.02	7.0	0.08	0.005	0.005	3.30	0.02
R	2743	2763	:DYKE - NO SAMPLE							
A001	2763	2796	1976	0.08	56.0	0.19	0.04	0.01	3.30	0.03
A001	2796	2819	1977	0.01	4.0	0.06	0.005	0.005	2.80	0.02
A001	2819	2846	1978	0.005	4.0	0.03	0.005	0.005	2.30	0.06
A001	2846	2876	1979	0.005	0.5	0.02	0.005	0.005	1.90	0.02
A001	2876	2908	1980	0.01	14.0	0.08	0.005	0.02	3.50	0.04
A001	2908	2926	1981	0.005	11.0	0.05	0.005	0.005	2.60	0.03
A001	2926	2956	1982	0.01	5.0	0.13	0.005	0.005	5.10	0.20
A001	2956	2985	1983	0.03	21.0	0.11	0.005	0.005	4.20	0.04
R	2985	3052	:DYKE - NO SAMPLE							

A001	3052	3078		1984	0.005	5.0	0.12	0.005	0.005	3.00	0.08
A001	3078	3109		1985	0.16	15.0	0.19	0.03	0.18	5.60	0.05
A001	3109	3139		1986	0.005	0.5	0.02	0.005	0.001	2.10	0.005
A001	3139	3170		1987	0.005	0.5	0.04	0.005	0.001	2.10	0.02
A001	3170	3200		1988	0.005	0.5	0.03	0.005	0.001	2.00	0.01
A001	3200	3235		1989	0.005	2.0	0.02	0.005	0.001	1.10	0.005
R	3235	3304	:DYKE - NO SAMPLE								
A001	3304	3322		1990	0.005	4.0	0.07	0.005	0.001	2.90	0.07
A001	3322	3352		1991	0.005	3.0	0.03	0.005	0.001	3.10	0.03
A001	3352	3383		1992	0.005	2.0	0.02	0.005	0.001	1.70	0.01
A001	3383	3413		1993	0.005	4.0	0.11	0.005	0.001	4.80	0.02
A001	3413	3450		1994	0.005	3.0	0.12	0.005	0.001	4.10	0.005
A001	3450	3486		1995	0.005	3.0	0.09	0.005	0.001	3.20	0.03
R	3486	3520	:DYKE - NO SAMPLE								
A001	3520	3529		1996	0.005	3.0	0.08	0.005	0.001	3.30	0.02
R	3529	3543	:DYKE - NO SAMPLE								
A001	3543	3566		1997	0.005	3.0	0.14	0.005	0.001	2.10	0.03
A001	3566	3596		1998	0.005	3.0	0.12	0.005	0.001	2.40	0.01
A001	3596	3626		1999	0.005	0.5	0.06	0.005	0.001	2.10	0.01
A001	3626	3657		2000	0.005	2.0	0.07	0.005	0.001	2.00	0.04
A001	3657	3687		1812	0.01	2.0	0.08	0.01	0.005	2.40	0.02
A001	3687	3718		1813	0.02	4.0	0.09	0.005	0.10	2.10	0.04
A001	3718	3748		1814	0.04	10.0	0.10	0.005	0.005	1.70	0.03
A001	3748	3779		1815	0.04	11.0	0.11	0.005	0.03	2.40	0.03
R			:END OF HOLE @ 377.9								

```
IDEN6B0201      X87CH319 NQ   MAY87DMLDJHJTT MAY87ACK          0.0
IPRJ               EQUITY SILVER MINES LTD          MAIN ZONE - MN GEOCODE
S000   00    229 MT  387.1 090.0 -51.0                   8024.65   8325.92   1285.70
S001  229    884     387.1 090.6 -51.0
S002  884   1631     387.1 091.7 -51.0
S003 1631   2286     387.1 092.6 -50.5
S004 2286   2972     387.1 093.4 -50.5
S005 2972   3566     387.1 094.4 -50.0
S006 3566   3840     387.1 095.0 -51.0
S007 3840   3871     387.1 095.1 -51.0
/SCL           MT.2MT.2
LSCL              MT.2        LCTM
/NAM                                                          QZSZTOPYCPTTASPRGY
LNAM                                                          DMCBCLMGHESLGLMO
/      00    183         OVBN                 P
R                :TRICONED - NO CORE
/     183    213  20     2D31MS      BD       P                D-
L                 00        7A
R                :VERY MINOR DARK GREY 2D53 :VERY WEAK BEDDING :OCC. SPOTTED
R                 TEXT WITH ANDALUSITE? SPOTS UP TO 2 MM
/     213    244  27     2D31MS      BDWL     P BD    055     D?D-
L                           7A
R                :AS ABOVE 18.3 - 21.3 W/0.4 M 8A: 0.2 M 2D53 (DARK GREY)
R                :LOCAL 2L TEXT
/     244    274  18     2D31MS      <<       P                D-
L                 00        7A
R                :0.1 M 2D53 (DARK GREY): TO 2C LOC.: TR PY IN <<
/     274    302  24     2E31MS      <<       P                D-
L                 00        7A
R                :V. WEAK << TEXT. W/ TR PY
/     302    350  46     8A10CL      P*<<     P          <-
/                 31        5G                  CL    034
R                :V. WEAK << TEXT W/QZ: CU OBSCURRED IN BROKEN CORE
/     350    366  13     2D31MS               P                D.
L                 00        7A
/     366    396  30     2D31MS      BD<<     P BD    050      D.
L                 02        7A
R                :LOCAL SPOTTED TEXT (ADALUSITE?): TO 2C LOC: V. WEAK <<TEXT W/PY
/     396    419  21     2D31MS      BD       P                D.
L                 02        7A
R                :0.5 M 2E INTERLEVED. LOCAL SPOTTED TEXT (ANDALUSITE?):
R                :0.03 M 2D53 (DARK GREY)
/     419    443  24     8A10CL      P*<<     P
L                 18        AG                            <)
R                :DAK GREY ALT'N ENVS. ALONG <<
/     443    457  13     2D93TOMS    <<BR     P               D-<)
L                 00        5T
R                :0.5 M POST-MIN BXIA W/SOME GOUGE
/     457    487  20     2D93TOMS    <<       P          <)   <(<)
L                 00        5T
R                :TO+PY+QZ AS <<?
/     487    518  27     2D93TOMS    <<       P          <)   <(<)
L                 00        5T
R                :AS ABOVE 45.7 - 48.7
/     518    548  27     2D83MSQZ    <<BR     P          <)   <?<)
```

```
L                03        7A
R               :TO 2C LOCALLY NO TO XTLS VISIBLE: LOCAL BXIA ZONES
/   548   581   32    2D93MSQZ   <<BR          P           <)   <(<)
L               02        7A
R               :WEAK LOCAL BXIA TEXT: TO 2E LOCALLY
/   581   610   27    8D13CLCY   <<P*          P CU   025       <(
L               02        AG                     CL   060
/   610   615   05    2D31MSQZ                 P                     D(
L               00        5A
R               :POSSIBLE XENOLITH
/   615   629   13    8A10CLEP   A*            P
L               05        AG
R               :CNTS NOT OBSERVED DUE TO BROKEN CORE
/   629   719   90    8C00MS     D*            P
L               75        GT                     CL   060
R               :LOWER CNT SHARP
/   719   734   12    8A10CL     A*            P
L               10        AG                     CL   070
R               :LOWER CNT SHARP
/   734   749   15    8C00MS     P*            P
L               04        7A
R               :LOWER CNT NOT OBSERVED DUE TO GOUGE
/   749   756   07    2D31MS                   P                     D-
L               02        5A
R               :POSSIBLE XENOLITH
/   756   844   88    8C00MS     P*            P
L               74        GT                     CL   060
R               :QZ+FL PHENOS
/   844   860   16    2D31MSQZ                 P                     D)
L               05        5A
/   860   884   24    2D33MSQZ   <<            P           <(     <(
L               20        5A
R               :V. PALE BROWNISH COLOR LOCALLY
/   884   914   30    2D33MSQZ   <<            P           <(     <)
L               14        5A
R               :TO 2E LOCALLY: TR POST-MIN BXIA & GOUGE
/   914   945   30    2D93TOMS   <<<<          P           <)   R-<+
L               18        5A                                        <)
/   945   975   30    2D93TOMS   <<            P           <)   R-<=
L               15        5A
/   975  1006   31    2D93TOMS   <<            P           <)   R-<=
L               17        5A
/  1006  1036   30    2D93TOMS   <<            P           <-   R-<)
L               00        5A
/  1036  1051   15    8A10CL     A*            P
L               07        5G                     CL   065
R               :CU OBSCURRED IN BROKEN CORE: LOWER CNT W/WEAK CM TEXT - SHARP
R               :& IRREGULAR
/  1051  1069   18    2D93TOMS   <<            P           <-   R-<)
L               03        5A
R               :0.7 M (2 SECTIONS) OF 8A
/  1069  1097   26    2D93TOMS   <<            P           <-   R-<)        <-
L               18        5A
/  1097  1127   30    2D93TOMS   <<            P           <-   R-<*        <-
L               09        5A
```

```
R                  :TO 2C LOCALLY
/    1127  1158  31     2D83MS      <<WL          P WL   063<-    <*
L                08          5A
R                  :LOCALLY WELDED TEXT
/    1158  1189  30     2D83MS      <<            P          <)   <?<+
L                02          5A
R                  :TO 2C LOC.
/    1189  1219  30     2D83MS      <<2L          P WL   070<-     <)
L                00          5A
R                  :MINOR CLAY GOUGE (FAULT?)
/    1219  1249  30     2D83MS      <<WL          P WL   065<-  <?<)         <.
L                09          5A
R                  :TO 2C LOC.
/    1249  1280  30     2D93TOMS    <<BD          P BD   067<+Q-R(<)          <)
L                22          5A
/    1280  1310  30     2D23SZMS    <<WL          P WL   072  0.  <)
L                11          5A        BR
R                  :WEAK LOCAL BXIA TEXT: TO 2C LOC.
/    1310  1341  30     2D83MSQZ    <<BR         P                D?<)
L                17          5A
R                  :0.3 M 2D53 AND 0.1 M 8A: STRONG LOCAL BXIA ZONES
/    1341  1369  27     2D37MS      BR            P                  #)
L                00          5A                          Q?
R                  :0.3 M BXIA TEXT: SAMPLE TAKEN TO TEST FOR DM (PALE PURPLE COLOR
/    1369  1402  30     2D31MS                    P F/   010       D(
L                03          5A
R                  :0.4 M 8A: POST-MIN GOUGE & BXIA RELATED TO FAULT
/    1402  1433  28     2D33MS      <<            P                 <+
L                04          5A
R                  :0.4 M 8A: LOTS OF POST-MIN BXIA & GOUGE (RELATED TO DYKES?)
/    1433  1450  16     2D33MS      <,            P                 <)
L                03          5A
R                  :POST-MIN GOUGE & BXIA AS ABOVE 2 INTS
/    1450  1593 142     8A10CL      P*            P CU   085
L                45          5G                     CL   050       D.
R                  :CU SHARP W/WEAK CHILLED MARGIN (& CL)
/    1593  1622  26     2D33MS      <<MX          P                 <1       <*
L                12          5A                                   <(<-
R                  :MX PYRITE TO ASS. W/0.6 M OF DARK BRECCIATED ROCK W/MINOR
R                  :SILIFICATION
/    1622  1641  18     8A00PL      P*            P CU   055
L                15          5G                     CU   070
R                  :CU SHARP - WK CHILLED MARG. CL IRREGULAR - STRONG CHILLED MARG.
R                  :CONTAINS 0.5 M OF 2D
/    1641  1675  33     2D21MSSZ    <<            P          <(<-  <(
L                10                                            <(  <-
R                  :LOCAL BXIA & GOUGE
/    1675  1709  33     2D31MS                    P                 <+       <(
L                10          5A                                      <)
R                  :CONTAINS 0.1 M OF MASSIVE SULPHIDE
/    1709  1750  40     8D11CL      <<P*          P CU   075       <(       <*
L                30          5G                                  <)
R                  :LOWER CONTACT DESTROYED BY POST-MINERAL DYKE
/    1750  1776  25     8A00PL      P*            P                          <(
L                15          6G
```

```
R                    :CL & CU IRREGULAR, OBSCURRED IN BROKEN CORE
/    1776  1832  56      8D11CL      P*<<         P                   D(          <)
L                23         5G                                     <)D-
R                    :CL & CU IRREGULAR
/    1832  1998 164      8D11CL      <<P*         P                   D-          <)
L               111         5G                                     <)
R                    :CU OBSCURRED BY BROKEN CORE: CL IS IRREGULAR
/    1998  2011  13      2D31MS                   P                   D.
L                00         5A                                     <(
R                    :TO 2E LOCALLY
/    2011  2040  29      2D33MS      BR           P                   <=          <*
L                26         5A                                     <)<)<(
R                    :PY OCCURS MAINLY IN 0.2 M OF MASSIVE PY, MG, HE
/    2040  2069  29      2D31MS                   P                Q(  <(<-       <(
L                16         5A                                     <(
R                    :CP OCCURS ONLY IN .1 M OF 2D23 W/10% SZ: MINOR BXIA
/    2069  2092  23      2D31MS      BR           P                   <(          <(
L                04         5A                                     <(
R                    :BRECCIATION OCCURS PROXIMAL TO DYKE (POSSIBLE RESPONSE)
/    2092  2132  38      8C00PL      P*           P CU   060
L                04         8G                      CL   035
/    2132  2163  31      8A00PL      P*           P CU   035                      <(
L                18         5A
R                    :CL IRREGULAR
/    2163  2220  53      8C00PL      P*           P
L                05         8G                      CL   080
R                    :CU IRREGULAR:A ROCK SIMILAR TO 8C ABOVE (209.2-213.2)
/    2220  2245  25      2D31MS      BR           P                   <)
L                05         5A                                     <(<-<-
R                    :BXIA IS POST-MINERAL  DUE TO PROXIMITY TO DYKE
/    2245  2270  23      2D31MS      BR           P                   <(
L                02         5A
R                    :CONTAINS 0.4 M OF 8A00
/    2270  2302  33      8D11CL      P*           P                   <)          <(
L                08         5G                                     B+
R                    :CU IRREGUULAR, CLOBSCURRED BY BROKEN CORE
/    2302  2332  30      2D33MS      <<MX         P                   Q1
L                08         5A                                        Q+Q(Q(
R                    :ZONE SHOWS LOCAL SILICIFICATION ESP. WHERE MX PYRITE OCCURS
/    2332  2361  24      2D31MS                   P                   <(
L                10         5A                                     B(
/    2361  2392  30      2D33MS      MX           P                   Q=          <)
L                12         5A                                        D(Q(Q(
R                    :MINERALIZATION OCCURS IN MASSIVE ZONE OF 0.3M (2361-2364)
/    2392  2413  20      8A00CL      P*           P CU   080          D.          <(
L                11         6A                      CL   050     B)
R                    :CONTAINS 2 0.2 M XENOLITHS OF 2D31 AS ABOVE: CONTACTS SHARP
/    2413  2443  29      2D31MS      BR           P                   <(          <(
L                21         6A                                     <(  <-
/    2443  2473  30      2D33MS      BR           P            <(     Q=          <(
L                15         5A                                     <*D(<)
R                    :MINERALIZATION & BR OCCUR IN MX ZONE 0.5 MW/STRONG SILIFICATION
/    2473  2499  25      2D31MS      BR           P            <(     Q+
L                07         5A                                     <)<(<(<-
R                    :MIN. OCCURS IN SILICIFIED ZONE: WHOLE ZONES SHOWS INTENSE
```

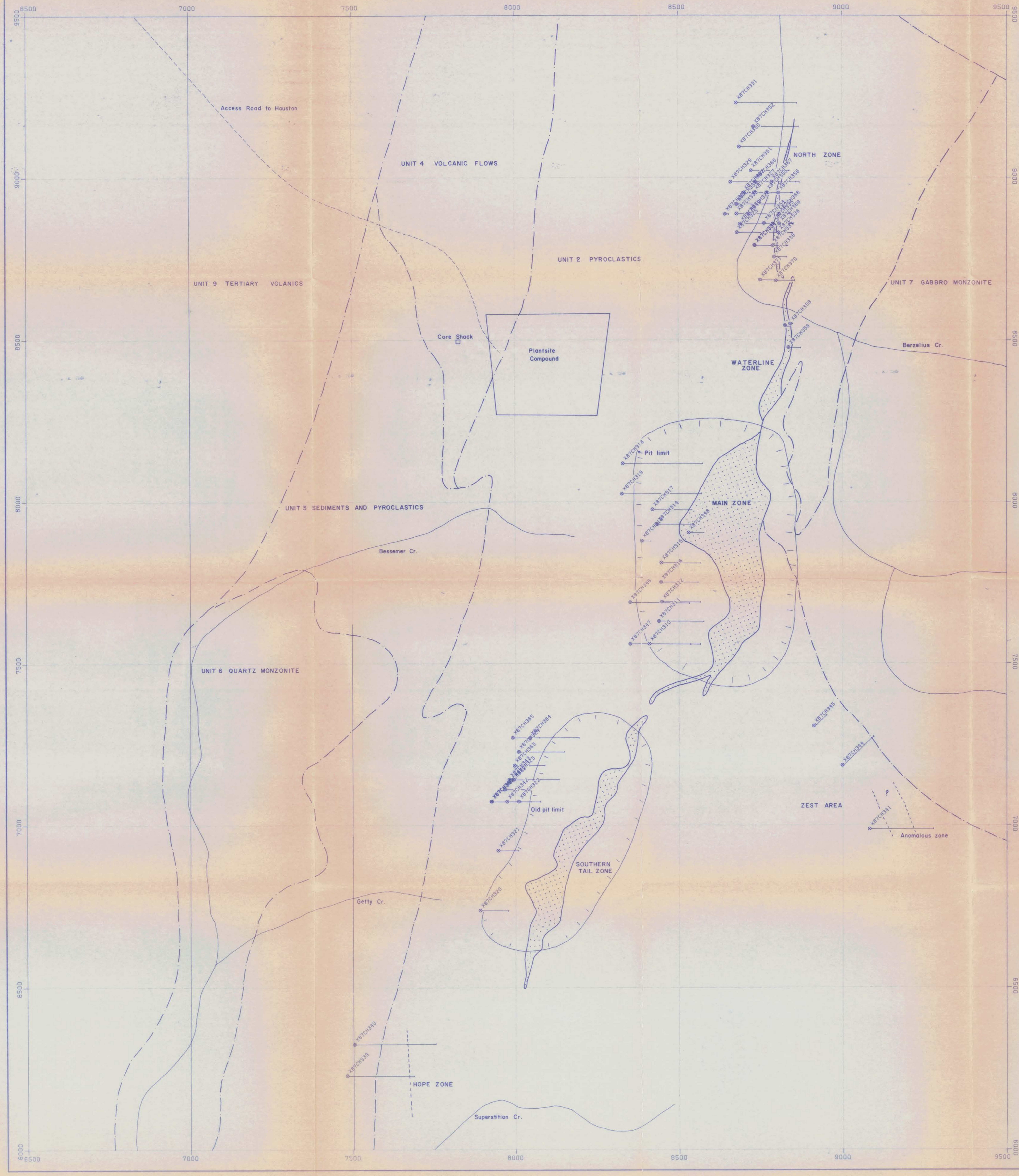
```
R                 :TECTONIC DEFORMATION
/    2499  2532  32     2E31MS                    P                  <)         <(
L                17          5A                                    B*<(<(
R                 :TO 2D LOC.: ZONE SHOWS MODERATE SILICIFICATION IN PLACES
/    2532  2564  32     2D11CL                    P            <(     B)        <(
L                19          5G                                    <+
R                 :MODERATE SILICIFICATION IN PLACES: TO 2E LOC
/    2564  2587  23     2E31MS     BR             P                  <(         <)
L                17          5A                                    B*
/    2587  2617  30     2D11CL                    P                  B*         <*
L                28          4G                                    Q=
R                 :TO 2E LOC: SHOWS MINOR - MODERATE SILICIFICATION
/    2617  2650  33     2D11CL                    P              B.  <(         <(
L                16          4G                                    Q+
R                 :TO 2E LOC
/    2650  2684  33     2E31MSSZ   BR             P              B.  <(         <(
L                23                                                Q)  D.
R                 :BR OCCURS NEAR 268.2 M & IS ASSOCIATED W/CLAY GOUGE
/    2684  2714  30     2D31MS                    P                  <(
L                23          5A                                    <)  <-
R                 :SOME MODERATE SILICIFICATION LOC.
/    2714  2748  34     2D31MS                    P                  <(         <(
L                18          5A                                    <(
/    2748  2782  33     2E41QZ                    P                  <*         <(
L                25          6A                                    <)  <(
R                 :LOC. INTO 2D31
/    2782  2834  51     8C00PL     P*             P CU   045         D.
L                22          7G
R                 :CONTACTS SHARP - LOWER CONTACTS IRREGULAR
/    2834  2848  13     2D31MS     BR             P                  D(
L                00          5A                                    <(
R                 :UNIT IS HIGH BRECCIATED W/GOUGE (POST-MIN DUE TO PROXIMITY TO
R                 :TWO DYKES)
/    2848  2871  23     8A00PL     P*             P CU   005
L                07          5G
R                 :CL OBSCURRED BY BROKEN CORE - CU SHARP W/WEAK CHILLED MARGIN
/    2871  2901  30     2D31MS                    P            <(     D)
L                16          6A                                    <(<(<-
R                 :ALSO SHOWS MINOR SILIFICATION
/    2901  2932  30     2D31MS                    P                  <*         <-
L                18          6A                                    <*
R                 :TO 2E IN PLACES
/    2932  2951  18     2D41QZ     BR             P                  <-
L                03          7A
/    2951  2970  19     2D41QZ     BR             P                  <-         <*
L                14          7A
R                 :TO 2E IN PLACES
/    2970  3004  34     2D11CL                    P                  B+         <*
L                13          4G                                    Q+<(<-
R                 :INTO ARGILLIC ALTERATION LOCALLY
/    3004  3060  56     8A00PL     P*             P                  <-         <*
L                39          55                      CL   055
R                 :INTO CU IRREGULAR CL SHARP W/WEAK CHILLED MARGIN
/    3060  3089  28     2E31MS     BR             P                  <(         <(
L                19          5A                                    <(
```

```
/    3089  3120   31   2D31MS     <<            P                       <(        <*
L                 10         4A                                       <)
R                 :INTO 2D11 LOC.
/    3120  3145   25   2D31MS                   P                       <(        <(
L                 06         5A                                       <(
/    3145  3170   25   2D41QZCL   <<            P                       <)        <-
L                 12         4G                                       B)<*
/    3170  3195   25   2D11CL                   P                       <)        <(
L                 16         4G                                       <*D)
R                 :ZONE SHOWS MINOR SILICIFICATION
/    3195  3228   30   2D31MS     <<            P                       <(        <(
L                 25         5A                                       <+
/    3228  3258   30   2D31MS                   P                       B(        <-
L                 16         5A                                       <*
R                 :MODERATE SILICIFICATION LOC. TO 2E LOC.
/    3258  3284   26   2D31MS                   P           Q(     Q+           <-
L                 14         4A                                       <*<(
R                 :SILICIFICATION AND << LOC.
/    3284  3314   30   2D31MS     BR            P                       D(        <*
L                 08         6A                                       <)
/    3314  3336   21   2D41QZCL                 P                       D(
L                 13         4A                                       <*          <-
R                 :TOO 2E LOC.
/    3336  3358   23   2D51QZ                   P                       Q+
L                 09         6A                                       <*<(
/    3358  3389   31   2E31MS                   P                       Q=<?
L                 24         5A                                       <)
/    3389  3419   30   2E11CL                   P                       <)        <-
L                 13         4G                                       <=<-
R                 :LOC. SHOWS MODERATE TO STRONG SILICIFICATION
/    3419  3455   36   2E11CL     BR            P                       B*        <-
L                 17         5G                                       <+<)
R                 :LOC - QTZ-SER. OR SILICIC ALTERATION
/    3455  3490   35   2D41QZCL                 P                       <(
L                 17         5G                                       <(<(
/    3490  3600  110   8COOPL     P*            P CL    050             D.        <.
L                 67         7G                                         D(
R                 :CL OBSCURRED BY BROKEN CORE: GRADES TO 8A00 OCCURRING FROM
R                 :349.0 - 350.8 AND 355.8 - 357.3
/    3600  3620   20   2D31MS                   P             <*      B*          <-
L                 06         5A                                       D)
R                 :MINOR SILICIFICATION: TO 2E LOC.
/    3620  3640   19   2E41QZ                   P             <+      B(          <-
L                 02         6A                                       <(
R                 :POST MINERAL BRECCIATION & GOUGE PROXIMAL TO DYKE
/    3640  3653   13   8A00PL     P*            P
L                 11         5G                   CL    035
R                 :CU OBSCURRED BY BROKEN CORE
/    3653  3683   29   2E11CLQZ                 P             <+      Q)
L                 04         5G                                       Q+<(
R                 :TO 2D LOC: MATRIX IS SILICIFIED: CONT. 0.2 M OF 8A00
/    3683  3709   24   2D41QZ                   P             Q)      <)
L                 04         5G                                       <*<*<(
/    3709  3724   15   8A00CL     P*            P
L                 04         4G
```

```
R                  :CONTACTS OBSCURRED BY BROKEN CORE
/    3724  3742   18      2D51QZ                    P               <*
L                 06         6A                                  <(<*<-<-
/    3742  3761   20      2D41QZ                    P               <(
L                 10         GA                                   <(
/    3761  3777   16      8A00PL       P*           P CU   030
L                 10         5G                       CL   050
/    3777  3794   17      2D53QZ                    P               <+        <-
L                 05         GA                                   <*<(<(<-
/    3794  3817   22      2E51QZ                    P               <(
L                 07         5A                                   Q+<-
/    3817  3871   54      7A00PL       P*           P
L                 24         4G
R                  :END OF HOLE @ 387.1 M
A001
ALAB               EQUITY MINESITE LABORATORY
ATYP               ASSAY
AMTH               WET EXTRACTION A.A. - AU FIRE ASSAYED FIRST
AUMM               RCOVSAMPLE   RQD % CU  G/TAG G/TAU % SB  % AS   % FE  % ZN
R      00    183 :TRICONED - NO CORE
A001  183    213        1846        0.005    0.5 0.02  0.02  0.005 2.37  0.03
A001  213    244        1847        0.005    0.5 0.05  0.03  0.005 2.59  0.04
A001  244    274        1848        0.001    0.5 0.02  0.005 0.005 3.72  0.005
A001  274    302        1849        0.001    0.5 0.03  0.005 0.005 1.73  0.02
R     302    350 :DYKE - NO SAMPLES
A001  350    366        1850        0.001    0.5 0.02  0.005 0.005 0.60  0.005
A001  366    396        1851        0.001    0.5 0.03  0.005 0.005 0.68  0.13
A001  396    419        1852        0.001    0.5 0.02  0.005 0.005 1.12  0.005
A001  419    443        1853        0.001    0.5 0.04  0.04  0.02  4.49  0.03
A001  443    457        1854        0.001    0.5 0.02  0.03  0.02  2.11  0.005
A001  457    487        1855        0.001    0.5 0.04  0.005 0.005 2.14  0.03
A001  487    518        1856        0.005    0.5 0.06  0.005 0.005 3.81  0.07
A001  518    548        1857        0.005    0.5 0.04  0.005 0.005 1.53  0.05
A001  548    581        1858        0.005    0.5 0.04  0.005 0.005 1.84  0.05
R     581    844 :DYKE - NO SAMPLES
A001  844    860        1959        0.005    0.5 0.01  0.005 0.005 3.00  0.005
A001  860    884        1860        0.005    0.5 0.01  0.005 0.005 3.10  0.005
A001  884    914        1861        0.02     0.5 0.08  0.005 0.005 3.00  0.005
A001  914    945        1862        0.005    0.5 0.11  0.005 0.005 2.69  0.005
A001  945    975        1863        0.05     8.0 0.54  0.005 0.005 9.30  0.07
A001  975   1006        1864        0.005    0.5 0.04  0.005 0.005 3.00  0.005
A001 1006   1036        1865        0.005    0.5 0.03  0.005 0.005 1.70  0.005
R    1036   1051 :DYKE - NO SAMPLE
A001 1051   1069        1866        0.005    0.5 0.01  0.005 0.005 2.70  0.01
A001 1069   1097        1867        0.005    0.5 0.05  0.005 0.005 1.70  0.005
A001 1097   1127        1868        0.005    0.5 0.005 0.005 0.005 0.90  0.07
A001 1127   1158        1869        0.005    0.5 0.05  0.005 0.005 1.80  0.03
A001 1158   1189        1870        0.005    0.5 0.07  0.005 0.005 4.60  0.01
A001 1189   1219        1871        0.005    0.5 0.05  0.005 0.005 1.70  0.01
A001 1219   1249        1872        0.005    0.5 0.02  0.005 0.005 0.90  0.005
A001 1249   1280        1873        0.005    0.5 0.20  0.005 0.005 0.90  0.005
A001 1280   1310        1874        0.005    0.5 0.01  0.005 0.005 1.00  0.005
A001 1310   1341        1875        0.005    0.5 0.01  0.005 0.005 2.20  0.005
A001 1341   1369        1876        0.005    9.0 0.03  0.005 0.005 0.80  0.005
A001 1369   1402        1877        0.02     9.0 0.16  0.005 0.005 2.20  0.01
```

A001	1402	1433	1878	0.005	0.5	0.17	0.005	0.005	4.60	0.03
A001	1433	1450	1879	0.01	2.0	0.02	0.005	0.005	1.70	0.005
R	1450	1593	:DYKE - NO SAMPLE							
A001	1593	1622	1880	0.005	2.0	0.11	0.005	0.005	6.80	0.005
R	1622	1641	:DYKE - NO SAMPLE							
A001	1641	1675	1921	0.005	2.0	0.36	0.005	0.005	2.00	0.005
A001	1675	1709	1922	0.005	3.0	0.01	0.005	0.005	4.40	0.02
R	1709	1998	:DYKES - NO SAMPLES							
A001	1998	2011	1923	0.02	7.0	0.06	0.005	0.005	1.70	0.02
A001	2011	2040	1924	0.01	7.0	0.02	0.005	0.02	3.90	0.01
A001	2040	2069	1925	0.02	6.0	0.12	0.005	0.05	2.00	0.02
A001	2069	2092	1926	0.005	2.0	0.02	0.005	0.005	2.30	0.02
R	2092	2220	:DYKES - NO SAMPLES							
A001	2220	2245	1927	0.005	3.0	0.03	0.005	0.005	2.90	0.01
A001	2245	2270	1928	0.005	4.0	0.02	0.005	0.005	3.20	0.01
R	2270	2302	:DYKE - NO SAMPLE							
A001	2302	2332	1929	0.02	6.0	0.27	0.005	0.03	7.40	0.04
A001	2332	2361	1930	0.05	3.0	0.03	0.005	0.005	1.90	0.02
A001	2361	2392	1931	0.05	4.0	0.63	0.005	0.05	8.60	0.41
R	2392	2413	:DYKE - NO SAMPLE							
A001	2413	2443	1932	0.05	5.0	0.14	0.005	0.005	3.00	0.03
A001	2443	2473	1933	0.01	5.0	0.15	0.005	0.03	4.80	0.02
A001	2473	2499	1934	0.01	4.0	0.07	0.005	0.005	2.30	0.02
A001	2499	2532	1935	0.005	3.0	0.07	0.005	0.005	2.10	0.005
A001	2532	2564	1936	0.005	3.0	0.10	0.005	0.02	2.80	0.01
A001	2564	2587	1937	0.005	2.0	0.06	0.005	0.005	1.10	0.01
A001	2587	2617	1938	0.07	90.0	0.24	0.02	0.01	3.60	0.03
A001	2617	2650	1939	0.02	10.0	0.14	0.005	0.01	3.30	0.04
A001	2650	2684	1940	0.01	48.0	0.30	0.005	0.005	2.70	0.02
A001	2684	2714	1941	0.005	3.0	0.03	0.005	0.005	2.70	0.01
A001	2714	2748	1942	0.005	0.5	0.05	0.005	0.01	2.20	0.01
A001	2748	2782	1943	0.03	6.0	0.13	0.005	0.005	4.00	0.14
R	2782	2834	:DYKE - NO SAMPLE							
A001	2834	2848	1944	0.005	5.0	0.09	0.005	0.01	2.80	0.01
R	2848	2871	:DYKE - NO SAMPLE							
A001	2871	2901	1945	0.01	3.0	0.16	0.005	0.02	5.60	0.07
A001	2901	2932	1946	0.02	3.0	0.04	0.005	0.02	3.90	0.02
A001	2932	2951	1947	0.005	2.0	0.04	0.005	0.005	0.70	0.04
A001	2951	2970	1948	0.005	3.0	0.05	0.005	0.01	3.00	0.01
A001	2970	3004	1949	0.005	3.0	0.08	0.005	0.005	2.70	0.005
R	3004	3060	:DYKE - NO SAMPLE							
A001	3060	3089	1950	0.005	0.5	0.16	0.005	0.005	0.60	0.01
A001	3089	3120	1951	0.005	2.0	0.32	0.005	0.005	1.20	0.02
A001	3120	3145	1952	0.005	3.0	0.74	0.005	0.005	2.40	0.02
A001	3145	3170	1953	0.01	1.0	0.15	0.005	0.01	4.90	0.02
A001	3170	3195	1954	0.005	0.5	0.02	0.005	0.005	2.60	0.01
A001	3195	3228	1955	0.005	2.0	0.57	0.005	0.005	1.90	0.01
A001	3228	3258	1956	0.01	2.0	0.15	0.005	0.005	2.80	0.01
A001	3258	3284	1957	0.005	2.0	0.32	0.005	0.01	6.60	0.01
A001	3284	3314	1958	0.01	0.5	0.03	0.005	0.005	1.70	0.01
A001	3314	3336	1959	0.005	2.0	0.12	0.005	0.005	1.90	0.005
A001	3336	3358	1960	0.01	2.0	0.13	0.005	0.005	4.40	0.05
A001	3358	3389	3700	0.01	3.0	0.14	0.005	0.07	5.70	0.01
A001	3389	3419	3701	0.02	3.0	0.07	0.005	0.005	3.20	0.03
A001	3419	3455	3702	0.02	3.0	0.005	0.005	0.005	1.80	0.01

A001	3455	3490		3703	0.02	3.0	0.06	0.005	0.005	2.50	0.03
R	3490	3600	:DYKE - NO SAMPLE								
A001	3600	3620		3704	0.02	7.0	0.09	0.005	0.01	3.70	0.06
A001	3620	3640		3705	0.07	42.0	0.62	0.005	0.005	3.20	0.09
R	3640	3653	:DYKE - NO SAMPLE								
A001	3653	3683		3706	0.03	6.0	0.12	0.005	0.005	3.10	0.02
A001	3683	3709		3707	0.03	4.0	0.15	0.005	0.01	3.20	0.03
R	3709	3724	:DYKE - NO SAMPLE								
A001	3724	3742		3708	0.02	5.0	0.18	0.005	0.005	2.60	0.01
A001	3742	3761		3709	0.02	5.0	0.11	0.005	0.005	2.30	0.02
R	3761	3777	:DYKE - NO SAMPLE								
A001	3777	3794		3710	0.04	0.5	0.02	0.005	0.005	5.00	0.04
A001	3794	3817		3711	0.03	17.0	0.17	0.005	0.005	2.70	0.03
R	3817	3871	:GABBRO - NO SAMPLE								
R			:END OF HOLE @ 387.1 M								



LEGEND

Geologic Contact
Road
General Surface Projection of Mineralization

DATA PLOTTED ON THIS MAP:
DIRECTORY: /EQUITY OD/USR/GL-DDH

FIELD FILE
• POINTS: HOLE DHLIST87

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,770

part 1 of 3

0 125 250 375 500
METRES

EQUITY SILVER MINES LIMITED

DRAWN DPS	FIGURE 4. DRILLHOLE LOCATIONS. GEOLOGY
DATE 88:01:28	
SCALE 1:5000	
NO.	PLATE