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GEOLOGICAL, GEOCHEMICAL AND GEOPHYSICAL REPORT
ON THE
CASTLE CLAIM GROUP
LIARD MINING DIVISION

104G/16E

57° 48' 30" N

130° 12' 00" W

GEOLOGICAL BRANCH
ASSESSMENT REPORT

BY
P. FOLK, P.ENG.

OF

TECK EXPLORATIONS LIMITED
FOR KAPPA RESOURCE CORPORATION

16,897

FILMED

OCTOBER, 1987

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INTRODUCTION

This report summarizes the results of the 1987 field work on the Castle Claim Group, Liard Mining Division, B.C. The work was done by TECK EXPLORATIONS on behalf of the TECK CORPORATION - KAPPA RESOURCE CORPORATION joint venture.

Location and Access

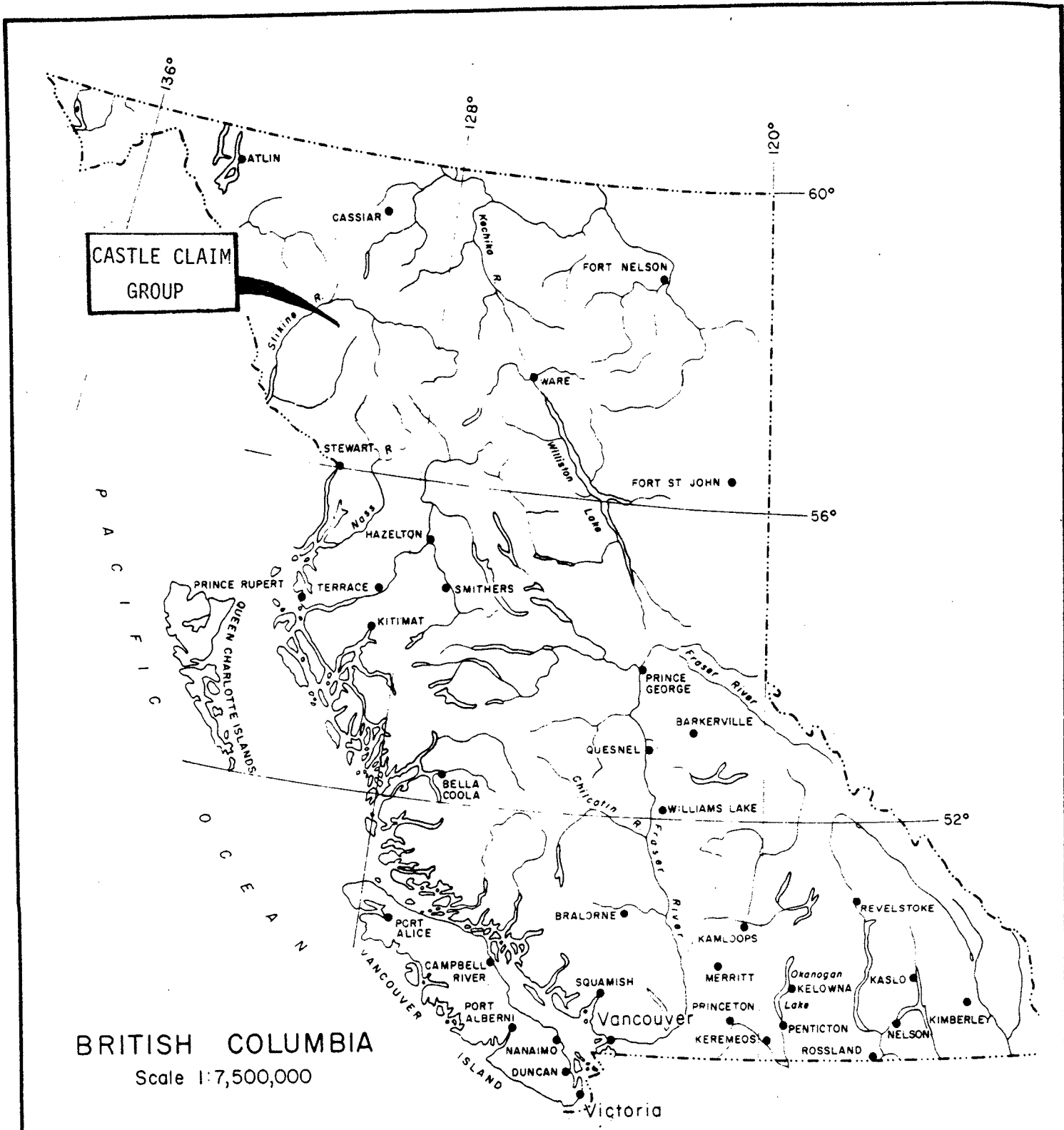
The Castle property is located on the south-west slope of Tsazia Mountain on the Klastline Plateau, northwestern British Columbia. The village of Iskut on the Stewart-Cassiar Highway is 15 km to the east and Dease Lake is about 70 km to the north. Access to the claims is by helicopter from a permanent base at Dease Lake. Excellent radiotelephone communications are available utilizing Northwestel's VHF repeater at Mt. Meehaus.

Physiography

Elevations range from about 1300 m to 2130 m with the camp being situated at 1690 m. The property is entirely above tree-line in rugged, mountainous terrain and alpine meadow-tundra.

The main topographic features of the area are Tuktsayda Mtn. and Mount Edziza located about 5 and 25 km respectively southeast and southwest of the main area of interest. Edziza Peak, in Edziza Park, has been a recently active volcano rising to 2,788 m above sea-level. Smaller coeval black olivine basalt volcanic vents, necks, and flows form distinctive edifices such as Castle Rock on and near the claims.

The area of interest is usually snow-covered between late September and early June. Remnants of glaciers and patches of snow persist the year round on some sheltered, north facing slopes.



BRITISH COLUMBIA
 Scale 1:7,500,000



TECK EXPLORATIONS LIMITED

LOCATION MAP

Fig. 1

History

Sumitomo Metal Mining Canada staked the "JO" group of claims in 1970, and performed a geochemical soil sampling survey for copper in 1971. Later Sumitomo drilled five diamond drill holes totalling about 550 metres and allowed the claims to lapse. The drill core, logs and assays are not available but apparently no gold analysis was completed.

The Castle #1 and Castle #2 claims totalling 27 units were staked by TECK EXPLORATIONS in 1980 as part of a regional program. Limited soil sampling and mapping done in 1980 and 1981 indicated that a substantial area of pyritized volcanics was associated with geochemical anomalies in gold, silver and copper. Assessment was applied on the Castle #2 Claim which contained the anomalies and the Castle #1 was later allowed to lapse. Assessment work in 1985 consisting of hand-trenching and chip sampling, magnetometer, self-potential and VLF-EM surveying yielded positive results. KAPPA RESOURCE CORPORATION entered into a joint venture agreement with TECK CORPORATION in 1987 and funded the work described in this report.

Work Done

Additional claims (CAS 1 - 4) were staked in June and a tent camp was erected in mid-July. A picket grid at 25m intervals was established on lines 50m apart for a total of approximately 14.5 km of line. Soil sampling was completed on the grid and a few silt samples were taken for a total of 545 geochemical samples. Self-potential and magnetometer surveys were carried out over the entire grid and about 10.5 km of IP survey was completed over the main area of interest. A small amount of hand trenching was done and 99 surface rock samples were assayed. A geological map was prepared.

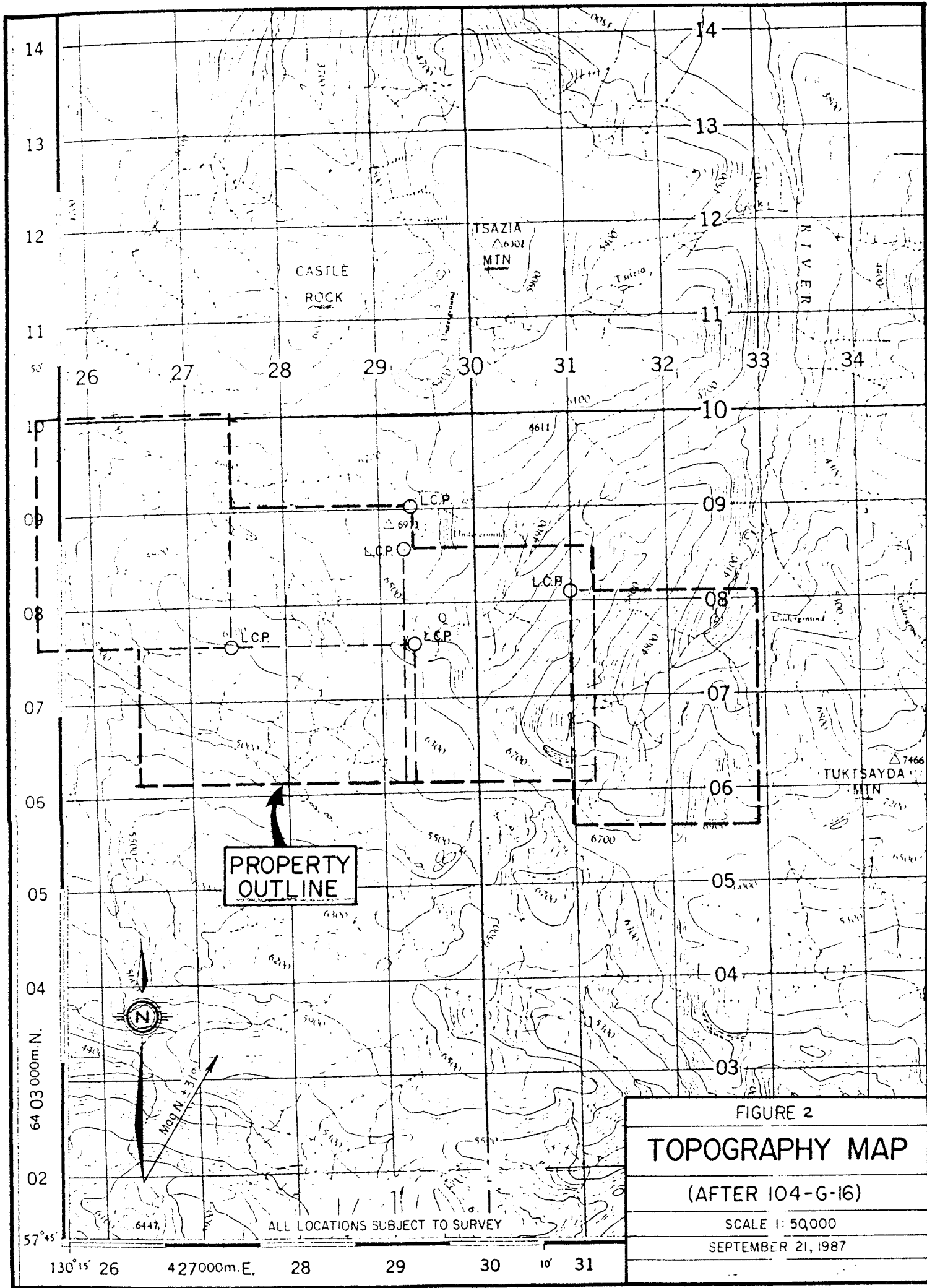
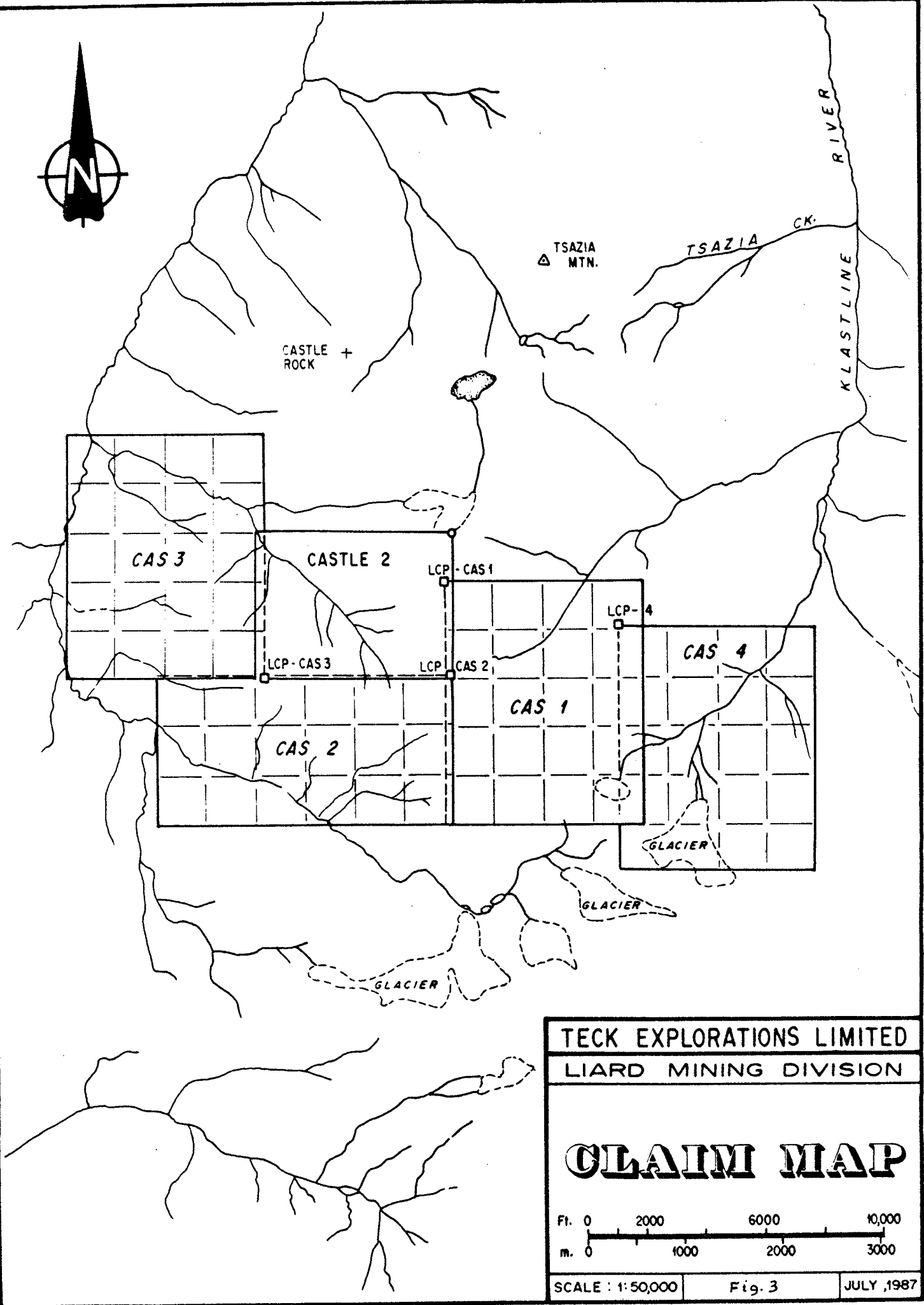
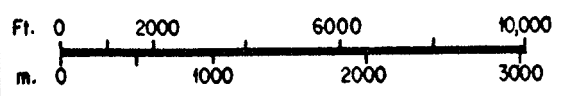


FIGURE 2
TOPOGRAPHY MAP
 (AFTER 104-G-16)
 SCALE 1:50,000
 SEPTEMBER 21, 1987



TECK EXPLORATIONS LIMITED
LIARD MINING DIVISION

CLAIM MAP



SCALE : 1:50,000 Fig. 3 JULY, 1987

Claims

The Castle Claim Group comprising five claims totalling 90 metric claim units is shown on figure 3. Claim data is tabulated below:

| <u>Claim Name</u> | <u>Record No.</u> | <u>Units</u> | <u>Record Data</u> | <u>Recorded Owner</u> |
|-------------------|-------------------|--------------|--------------------|-----------------------|
| CASTLE #2 | 1232(3) | 3S x 4W = 12 | March 26, 1980 | Teck Corporation |
| CAS 1 | 4110(7) | 5S x 4E = 20 | July 6, 1987 | Teck Corporation |
| CAS 2 | 4111(7) | 3S x 6W = 18 | July 6, 1987 | Teck Corporation |
| CAS 3 | 4112(7) | 5N x 4W = 20 | July 6, 1987 | Teck Corporation |
| CAS 4 | 4113(7) | 5S x 4E = 20 | July 6, 1987 | Teck Corporation |
| | | TOTAL | 90 units | |
| | | | ===== | |

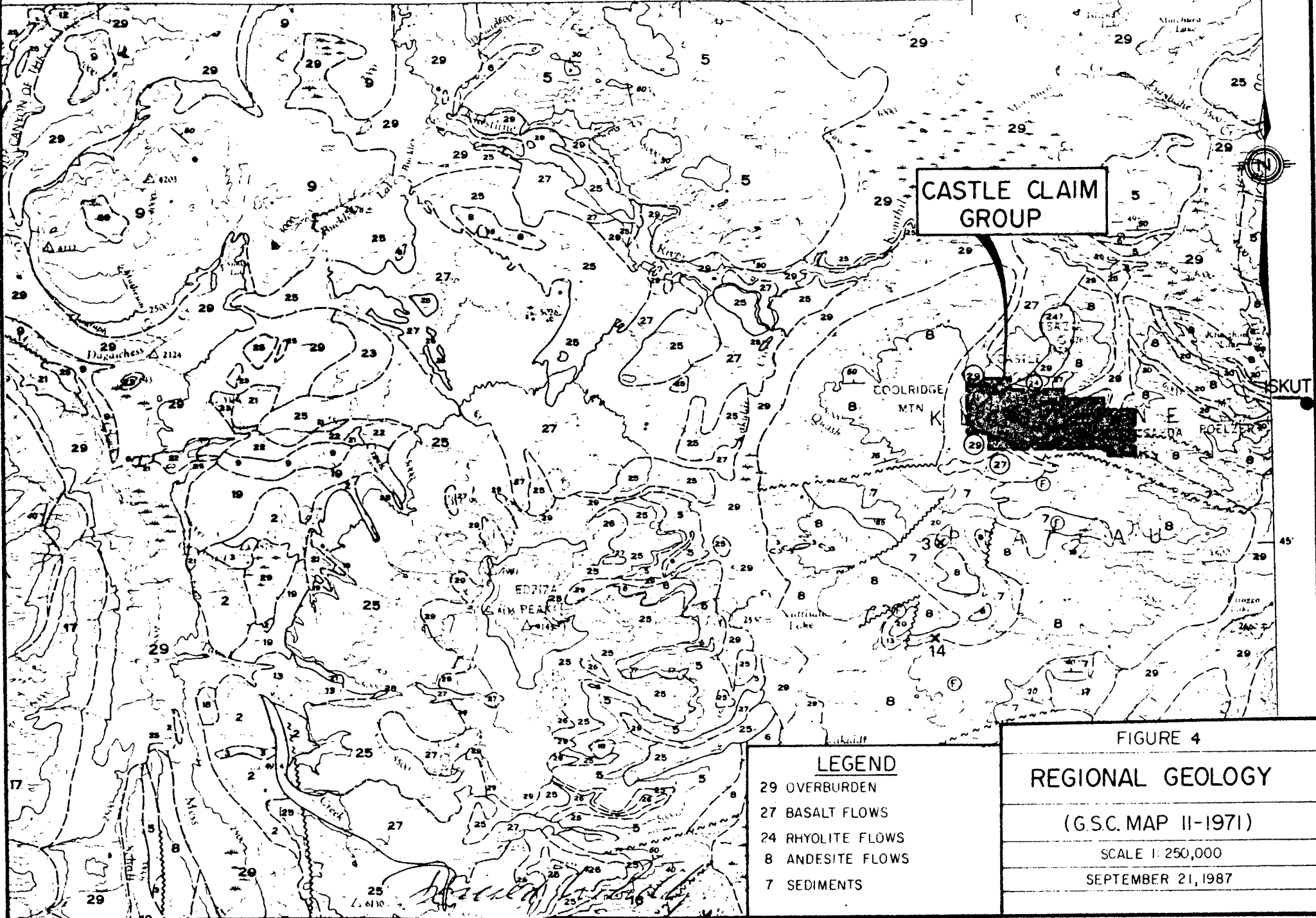
GEOLOGY

Regional Geology

The regional geology of the area taken from G.S.C. Map: 11- 1971 is shown of figure 4. Most of the area is underlain by purple and greenish andesitic flows and pyroclastics of Upper Triassic age. Older black shales and other fine grained sediments are in fault contact with the volcanic units on the southern portion of the claims. Quaternary black olivine basalt tephra outcrops in several places on and near to the claims. A northwest striking, southwest dipping linear gossan up to about 200 m wide which transects most of the claim group is readily visible from the air. This shear (?) zone is mineralized throughout with pyrite and contains chalcopyrite and values in gold and silver on the northwest portion of the property where most of the exploration work has been concentrated.

Property Geology (figure 5.)

Actual outcrops in the grided area are sparse and have suffered such intense fracturing and alteration as to render lithologic identification in hand specimen very difficult. An outcrop map fig. 5, prepared by T. Dey is enclosed.



CASTLE CLAIM GROUP

FIGURE 4

REGIONAL GEOLOGY

(G.S.C. MAP II-1971)

SCALE 1: 250,000

SEPTEMBER 21, 1987

- LEGEND**
- 29 OVERBURDEN
 - 27 BASALT FLOWS
 - 24 RHYOLITE FLOWS
 - 8 ANDESITE FLOWS
 - 7 SEDIMENTS

Lithology

Most of the rocks underlying the grid are fine to coarse grained tuffaceous, epiclastic volcanics from purplish to greenish in color. Some porphyritic volcanics were also noted, some of which may be intrusive in origin.

The lithologies were divided by color, grain size and intensity of alteration into seven separate units the first five of which are predominantly pyroclastic in nature:

1. Medium grained, grey-green volcanics, weakly altered.
2. Coarse grained green volcanics, some porphyritic phases, weakly altered.
3. Medium to coarse grained volcanics with pyrite, moderately altered.
4. Highly altered green volcanics with pyrite and sericite.
5. Purple pyroclastics, unaltered.
6. Light brown volcanic dyke, unaltered.
7. Felsite intrusive.

The felsite intrusive is a tan to orange, fine grained to very weakly porphyritic, feldspar rich, massive body which cuts the volcanic stratigraphy in a northeasterly direction. Except for traces of quartz veining and chalcopyrite and bornite, the felsite is unmineralized and may post-date the main mineralizing event as do a few small brownish volcanic dykes.

Structure

The lithologies strike northwest-southeast (parallel to the base line) and dip 70 to 85 degrees southwest. Much of the quartz-sericite veining and alteration appears to be parallel to the stratigraphy except in the vicinity of fault zones. A fault zone apparently without significant displacement follows the main creek in a NNW direction. This fault and all lithologies and mineralization have been displaced by NNE faults with apparent dextral displacements up to about 50 m.

Alteration

Phyllic and propylitic alteration and attendant mineralization is structurally controlled along: 1) a major northwest trending zone which can be traced for several km. and is parallel to the volcanoclastic stratigraphy. 2) faults which cross-cut the main zone. Propylitic, or moderately altered volcanics are highly fractured and limonitic with pyrite, chlorite, and lesser epidote. Disseminated magnetite found at several locations may be related to the propylitic alteration. Phyllic alteration is represented by assemblages of pyrite-sericite-quartz along relatively narrow structures within the propylitic zone and as a weaker but pervasive alteration product of the host volcanics. The narrow pyrite-sericite-quartz structures (shears?) are very slightly resistant to weathering and are easily recognized in outcrops. They host the gold mineralization.

Mineralization

Pyrite is ubiquitous in a zone (see fig. 5) which has been mapped over an area at least 1.3 km long and up to 200 m wide. The zone continues to the southeast for another one to two km. but terminates at or before the felsite intrusion to the northwest. Pyrite also occurs in and near several cross-cutting fault zones. Generally, the maximum volume of pyrite would be about 5% as disseminations but semi-massive pyrite up to about 15% by volume is found along narrow structures particularly as float near 22 + 00 West, 1 + 25 South.

Malachite, chalcopyrite and traces of bornite are found with pyrite in several locations disseminated in altered volcanics. Although none of the occurrences appear to be of economic grade it was noted that copper occurs adjacent to gold bearing structures in less intensely altered but highly fractured rock.

Visible gold in quartz veinlets within sericitic structures was found near 17 + 00 W, 1 + 00 S and off of the grid at about 1 + 00 W, 1 + 45 N. Both occurrences were not traceable because of overburden. The first is a quite

spectacular occurrence which assayed 0.931 oz Au/T and 4.05 oz Ag/T over 1.0 m with visible gold deliberately omitted from the sample. A selected grab sample of the 5 cm qtz vein in which the native gold occurs assayed 4.03 oz Au/T and 12.66 oz Ag/T (visible gold omitted from the sample). The vein occurs within a sericite-pyrite alteration zone at least 5m wide containing gold values in the 0.01 to 0.02 oz Au/T range. Barite veining was noted nearby.

A second occurrence of native gold is located on the ridge top southwest of the end of the grid and initially assayed 1.156 oz Au/T over 0.4m. Another sample at the same location assayed 0.139 oz Au/T over 0.6m. Visible gold was noted on a 5mm wide quartz veinlet within a pyrite-sericite zone in purple pyroclastics. About 100m. away on strike a sample of float assayed 0.169 oz Au/T.

Several other sericite-pyrite structures were sampled as were most outcrops containing significant quantities of pyrite. All assays are plotted on figure 6 and significant assays are tabulated below:

| Au oz/T | Ag oz/T | Cu % | Sample Width M | Notes |
|------------|------------|---------|-------------------|---------------------|
| 4.030 | 12.66 | .01 | Grab | V.G. omitted |
| 0.931 | 4.05 | .01 | 1.0 M | V.G. omitted |
| 0.109 | 0.74 | .01 | 2.0 M | same area |
| 0.024 | 0.71 | .01 | 1.0 M | same area |
| 0.011 | 0.09 | .03 | 1.5 M | same area |
| 0.029 | 0.22 | .02 | 0.6 M | Mo, Py |
| 0.309 | 0.71 | .01 | 0.3 M | doubtful outcrops |
| 0.022 | 0.07 | .01 | 2.0 M | |
| 0.254 | 0.05 | .01 | 0.9 M | |
| 0.023 | 0.01 | .03 | 1.8 M | repeat of above |
| 0.062 | 0.04 | .04 | 2.5 M | |
| 1.156 | 0.10 | .08 | 0.4 M | |
| 0.139 | 0.17 | .11 | 0.6 M | repeat of above |
| 0.169 | 0.48 | .27 | (F) | same vein as above? |
| 0.062 | 0.15 | .29 | (F) | |

| Au oz/T | Ag oz/T | Cu % | Sample Width M | Notes |
|------------|------------|---------|-------------------|-------------|
| 0.046 | 0.12 | .17 | Grab | |
| 0.062 | 0.31 | .08 | 0.8 M | |
| 0.047 | 0.31 | .01 | (F) | |
| 0.058 | 1.73 | | (F) | Pyrite |
| 0.232 | 1.81 | | (F) | Pyrite |
| 0.033 | 0.20 | .01 | 0.6 M | |
| 0.042 | 0.16 | .02 | 0.5 M | |
| 0.056 | 0.17 | .02 | 0.7 M | |
| 0.029 | 0.02 | .02 | 1.0 M | |
| 0.042 | 0.52 | .01 | 1.3 M | |
| 0.061 | 0.52 | .02 | 0.8 M | |
| 0.042 | 0.25 | .01 | 1.4 M | |
| 0.035 | 0.20 | .02 | 0.4 M) | |
| 0.296 | 1.59 | .70 | 0.3 M) | 0.146/1.3 M |
| 0.144 | 0.52 | .21 | 0.6 M) | |
| 0.055 | 0.67 | .02 | 1.2 M | |

Note: (F) = float

Small barite veins occur sporadically in the area of interest. They appear to be barren of gold mineralization perhaps being associated with a later mineralizing event. Molybdenite and galena in trace amounts were noted.

GEOCHEMISTRY

Soil samples were taken at depths of a few cm. in "B" or "C" horizon material in the poorly developed mountain soils. Many of the samples consisted of talus fines. Overburden is generally not thick but movement down slope has undoubtedly caused transport of anomalies downwards and has also covered mineralized bedrock with barren material. The soil was assayed by ICP techniques at Acme Analytical Labs in Vancouver. Gold analyses were performed by atomic absorption.

Results (Fig. 7,8)

Analyses for Au, Ag and Cu were combined with the 1980 surveys and are plotted on figures 7 and 8. In general gold values greater than 100 PPB, copper greater than 200 PPM and silver greater than 1 PPM are considered anomalous.

Coincidental anomalies in Au, Ag and Cu extend 1.4 km. from line 9 + 50 W to line 23 + 50 W in a zone up to 400 m wide. Peak values are: Au - 1400 PPB, Ag - 13.0 PPM (omitting an erratic high value of 38 PPM), Cu - 5593 PPM. The better values occur near bedrock in creek gullies. A broad anomaly north of the baseline from 15 + 00 W to 22 + 00 W probably represents material which has been transported down-slope from the south. West of line 23 + 00 W all anomalies appear to terminate but this may simply be an effect of deeper overburden since there are a few sporadic highs down slope from projection of the zone.

GEOPHYSICS

Self Potential Survey (Fig. 9)

An S-P survey using porous ceramic pots and a "FLUKE" multimeter was completed with readings at 12.5 M intervals. The corrected results in negative millivolts are plotted on figure 9 which shows three small but distinct anomalies all of which occur adjacent to geochemical anomalies. The positive values on line 19W were checked and have no explanation.

Magnetometer Survey (Fig. 10)

The corrected results of a magnetometer survey utilizing a GEOMETRICS total field proton magnetometer are plotted on Figure 10. The results reflect the fine disseminations of magnetite which were noted in some of the volcanics and have been used to interpret post mineral faulting in the central portion of the grid.

12.5 metre station readings

Regular tie-ins to a base station constituted corrected diurnal variation

Induced Polarization Survey (Fig. 11,12)

Dipole-dipole array

A frequency domain I.P. survey utilizing a dipole spacing of 25 M was conducted by PACIFIC GEOPHYSICAL LIMITED. Remnants of snow interfered with the continuity of the survey at three locations. Results are plotted on figure 11, which is a diagrammatic representation of the anomalies and also on figure 12 which is a contour map of the Fraser Filtered values of percent frequency effect.

A very strong I.P. effect (PFE greater than 10) occurs in a large elongate zone about 1100 M long which corresponds well with the geochemical data except in some instances the geochemical highs are down slope from the I.P. anomaly. This result is consistent with observations of solifluction (soil creep) on the hillsides resulting in the shifting of geochemical anomalies down slope from their source rocks. The visible gold occurrence at 17 + 00 W, 1 + 00 S is within a narrow portion of the I.P. anomaly which is displaced to the south by dextral faulting not far from the occurrence.

To the west the main portion of the I.P. anomaly rapidly dies out but it is probable that the I.P. effect has been masked by deeper overburden and that the mineralized zone does in fact continue for perhaps 200 metres until the felsite contact is reached. It is thought that the felsite contact may be marked by a small creek along line 25 + 50 W.

A very strong I.P. effect (PFE greater than 16) at 1 + 25 S on lines 21 + 50 W to 22 + 50 W occurs in an area of little outcrop. It is likely that the source rock contains a thin band of semi-massive pyrite within the larger pyrite zone. Copper, gold, and silver geochemical anomalies coincide with this strong I.P. anomaly.

DISCUSSION AND CONCLUSIONS

Potentially economic gold and silver values occur in quartz veinlets within shear (?) zones of sericite - pyrite - quartz alteration. Copper

mineralization is often located adjacent to these structures but is not usually within them. Disseminated pyrite, associated with propylitic alteration, yields a pronounced I.P. anomaly and forms a distinctive envelope enclosing the area of interest. The I.P. results can therefore be used to map the surface projection of the zone particularly where outcrops are sparse and the geochemical anomalies have been transported down-slope by erosion and solifluction. Figure 13 is a compilation of the salient geological, geochemical and geophysical features described above and shows the translation of geochemical results down slope from the assumed source areas.

The most significant gold occurrence found to date is near 17 + 00 W, 1 + 00 S where an assay value (omitting any obvious visible gold) of 0.931 oz Au/T, 4.05 oz Ag/T was obtained over a width of 1.0 M. Poor exposures prohibited further sampling along strike. The prospect is within a narrow portion of the I.P. anomaly on the flanks of both a magnetic and a self potential high (see figure 13). An area of structural complication and apparently post-mineral dextral faulting is projected to the east. Several other similar, parallel sericite-pyrite-quartz shear zones within the envelope of pyritization yielded interesting but sub-economic assays.

Narrow, high grade structures are interesting in themselves but for mining purposes a large tonnage, open pittable, lower grade zone should be the target. Such a zone could occur where the generally parallel sericite-pyrite-quartz mineralized structures are intersected by pre-ore structures in other directions. This structural geometry occurs between 15+00 W and 18+50 W south of the baseline where cross-cutting faults and the only exposed northwest-southeast trending sericite-pyrite shear zone are located. Another target area is line 21+50 W to 22+50 W, 1+75 S where a strong I.P. response suggests a narrow but high concentration of sulfides. Geochemical anomalies, pyritic float and sericite-pyrite-quartz altered bedrock are also present nearby. At 13+00 W to 14+00 W, 1+25 S an I.P. anomaly is located up slope from a geochemical high in an area of projected faulting.

RECOMMENDATIONS

The area surrounding the main zone of interest has not been examined and does require preliminary prospecting and reconnaissance geochemical sampling. On the main zone some hand trenching should be carried out where required and feasible but diamond drilling should be the main thrust of the next program. The initial program of NQ drilling should test:

- 1) the area between 15 W and 18 + 50 W south of the baseline.
- 2) between 21 + 50 W and 22 + 50 W, 1 + 75 S.
- 3) near 13 W to 14 W, 1 + 25 S.

Respectfully submitted,



October 28, 1987

P. G. Folk, P.Eng

CERTIFICATE OF QUALIFICATIONS

Peter G. Folk, P.Eng.

I hereby certify that:

1. I graduated from the University of British Columbia in 1971 with a B.A.Sc. degree in geological engineering.
2. I am a member in good standing of the Association of Professional Engineers of the Province of British Columbia.
3. I have worked since graduation as an exploration geologist and mine geologist in Canada and the United States.
4. The work described herein was carried out under my direct supervision.

A handwritten signature in cursive script, appearing to read 'Peter G. Folk', written in dark ink.

P. G. Folk, P.Eng.

APPENDIX I

CERTIFICATE OF QUALIFICATIONS

APPENDIX II

ITEMIZED COST STATEMENT

ITEMIZED COST STATEMENT

P. Folk, P.Eng. Project Manager.

June 30, July 1, July 16 - July 21, July 27 - 30,
Aug 29, 30, Sept. 2 - 3

16 days @ \$230/D = \$ 3,680

J. Bacon, Prospector

June 30, 31 2 days @ \$132/D = \$ 264

J. Simpson, Claim Staker

June 30, 31 2 days @ \$200/D = \$ 400

D. Nikirk, Party Chief

July 16 - Sept. 6 53 days @ \$132/D = \$ 6,996

R. Nikirk, Helper

July 21 - Sept. 6 48 days @ \$93/D = \$ 4,464

T. Dey, Geologist

July 16 - Aug. 13 29 days @ \$132/D = \$ 3,828

I.P. Survey, PACIFIC GEOPHYSICS LIMITED

10.55 km of I.P. survey, Aug. 13 - 30 \$13,054

FRONTIER HELICOPTER, BELL 206 JET RANGER

| Day | Hours | |
|---------------------------------|---------------------------------|------------|
| June 30 | 1.7 | |
| July 17 | 3.3 | |
| July 20 | 0.7 | |
| July 28 | 0.6 | |
| July 29 | 0.6 | |
| Aug. 2 | 0.5 | |
| Aug. 3 | 3.0 | |
| Aug. 10 | 0.5 | |
| Aug. 13 | 0.7 | |
| Aug. 14 | 2.0 | |
| Aug. 15 | 0.5 | |
| Aug. 23 | 0.5 | |
| Aug. 26 | 0.9 | |
| Aug. 29 | 1.5 | |
| Sept. 2 | 5.7 | |
| Sept. 3 | 1.7 | |
| Sept. 4 | <u>0.9</u> | |
| | 25.3 @ 615/hr. including fuel = | \$15,560 |
| Assays and geochemical analyses | | 7,887 |
| Travel and freight | | 3,300 |
| Camp costs, groceries, fuel | | 7,691 |
| Equipment rental | | 214 |
| Drafting and maps | | 2,633 |
| Radiophone | | <u>924</u> |
| | | \$70,895 |

APPENDIX III

ASSAY TECHNIQUES AND RESULTS



ACME ANALYTICAL LABORATORIES LTD.

Assaying & Trace Analysis

852 E. Hastings St., Vancouver, B.C. V6A 1R6

Telephone : 253 - 3158

GEOCHEMICAL LABORATORY METHODOLOGY - 1985

Sample Preparation

1. Soil samples are dried at 60°C and sieved to -80 mesh.
2. Rock samples are pulverized to -100 mesh.

Geochemical Analysis (AA and ICP)

0.5 gram samples are digested in hot dilute aqua regia in a boiling water bath and diluted to 10 ml with demineralized water. Extracted metals are determined by :

A. Atomic Absorption (AA)

Ag*, Bi*, Cd*, Co, Cu, Fe, Ga, In, Mn, Mo, Ni, Pb, Sb*, Tl, V, Zn
(* denotes with background correction.)

B. Inductively Coupled Argon Plasma (ICP)

Ag, Al, As, Au, B, Ba, Bi, Ca, Cd, Co, Cu, Cr, Fe, K, La, Mg, Mn, Mo, Na, Ni, P, Pb, Sb, Sr, Th, Ti, U, V, W, Zn.

Geochemical Analysis for Au*

10.0 gram samples that have been ignited overnight at 600°C are digested with 30 mls hot dilute aqua regia, and 75 mls of clear solution obtained is extracted with 5 mls Methyl Isobutyl Ketone.

Au is determined in the MIBK extract by Atomic Absorption using background correction (Detection Limit = 1 ppb).

Geochemical Analysis for Au**, Pd, Pt, Rh

10.0 - 30.0 gram samples are subjected to Fire Assay preconcentration techniques to produce silver beads.

The silver beads are dissolved and Au, Pd, Pt, and Rh are determined in the solution by graphite furnace Atomic Absorption. Detections - Au=1 ppb; Pd, Pt, Rh=5 ppb

Geochemical Analysis for As

0.5 gram samples are digested with hot dilute aqua regia and diluted to 10 ml. As is determined in the solution by Graphite Furnace Atomic Absorption (AA) or by Inductively Coupled Argon Plasma (ICP).

Geochemical Analysis for Barium

0.25 gram samples are digested with hot NaOH and EDTA solution, and diluted to 20 ml.

Ba is determined in the solution by ICP.

Geochemical Analysis for Tungsten

0.25 gram samples are digested with hot NaOH and EDTA solution, and diluted to 20 ml. W in the solution determined by ICP with a detection of 1 ppm.

Geochemical Analysis for Selenium

0.5 gram samples are digested with hot dilute aqua regia and dilute to 10 ml with H₂O. Se is determined with NaBH₃ with Flameless AA. Detection 0.1 ppm.

ACME ANALYTICAL LABORATORIES
 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
 PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: JUL 31 1987
 DATE REPORT MAILED: *Aug. 10/87.*

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: P1 TO P10-SOIL P11-ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: *D. Toyne* DEAN TOYE, CERTIFIED B.C. ASSAYER

TECK EXPLORATIONS PROJECT-1354 File # 87-2886 Page 1

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L28+00W 0+00S | 38 | .1 | 1 |
| STD C/AU-S | 60 | 7.6 | 48 |
| L28+00W 0+25S | 35 | .3 | 2 |
| L28+00W 0+50S | 49 | .2 | 36 |
| L28+00W 0+75S | 54 | .5 | 6 |
| L28+00W 1+00S | 66 | .3 | 8 |
| L28+00W 1+25S | 40 | .2 | 1 |
| L28+00W 1+50S | 135 | .7 | 780 |
| L28+00W 1+75S | 66 | .5 | 9 |
| L28+00W 2+00S | 44 | .3 | 7 |
| L28+00W 2+25S | 37 | .4 | 1 |
| L28+00W 2+50S | 24 | .1 | 2 |
| L27+50W 1+75N | 117 | .6 | 13 |
| L27+50W 1+50N | 79 | .4 | 16 |
| L27+50W 1+25N | 150 | .4 | 33 |
| L27+50W 1+00N | 64 | .3 | 8 |
| L27+50W 0+75N | 60 | .4 | 7 |
| L27+50W 0+50N | 160 | 1.2 | 12 |
| L27+50W 0+25N | 70 | .4 | 9 |
| L27+50W 0+00N | 58 | .2 | 3 |
| L27+50W 0+25S | 46 | .4 | 1 |
| L27+50W 0+50S | 73 | .4 | 7 |
| L27+50W 0+75S | 30 | .4 | 1 |
| L27+50W 1+00S | 30 | .3 | 1 |
| L27+50W 1+25S | 93 | .5 | 23 |
| L27+50W 1+50S | 181 | .3 | 71 |
| L27+50W 1+75S | 137 | .3 | 34 |
| L27+50W 2+00S | 49 | .6 | 4 |
| L27+50W 2+25S | 49 | .5 | 2 |
| L27+50W 2+50S | 58 | .6 | 2 |
| L26+50W 2+50N | 76 | .2 | 6 |
| L26+50W 2+25N | 76 | .2 | 8 |
| L26+50W 2+00N | 85 | .2 | 10 |
| L26+50W 1+75N | 94 | .5 | 13 |
| L26+50W 1+50N | 121 | .5 | 8 |
| L26+50W 1+25N | 45 | .5 | 1 |
| L26+50W 1+00N | 71 | .4 | 7 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L26+50W 0+75N | 154 | .4 | 34 |
| L26+50W 0+50N | 69 | .4 | 3 |
| L26+50W 0+25N | 96 | .1 | 14 |
| L26+50W 0+25S | 44 | .3 | 5 |
| L26+50W 0+50S | 55 | .3 | 2 |
| L26+50W 0+75S | 51 | .4 | 1 |
| L26+50W 1+00S | 60 | .5 | 6 |
| L26+50W 1+25S | 65 | .2 | 12 |
| L26+50W 1+50S | 95 | .2 | 14 |
| L26+50W 1+75S | 70 | .4 | 3 |
| L26+50W 2+00S | 226 | .5 | 26 |
| L26+50W 2+25S | 69 | .4 | 18 |
| L26+50W 2+50S | 48 | .3 | 1 |
| L25+50W 2+50N | 59 | .6 | 5 |
| L25+50W 2+25N | 383 | .9 | 215 |
| L25+50W 2+00N | 138 | .2 | 36 |
| L25+50W 1+75N | 68 | .1 | 6 |
| L25+50W 1+50N | 79 | .5 | 4 |
| L25+50W 1+25N | 80 | .2 | 14 |
| L25+50W 1+00N | 44 | .3 | 8 |
| L25+50W 0+75N | 53 | .2 | 3 |
| L25+50W 0+50N | 53 | .3 | 12 |
| L25+50W 0+25N | 37 | .1 | 4 |
| L25+50W 0+25S | 203 | .4 | 72 |
| L25+50W 0+50S | 263 | .8 | 44 |
| L25+50W 0+75S | 140 | .7 | 34 |
| L25+50W 1+75S | 76 | .2 | 2 |
| L25+50W 2+00S | 73 | .5 | 1 |
| L25+50W 2+25S | 87 | .2 | 3 |
| L25+50W 2+50S | 74 | .2 | 2 |
| L24+50W 2+50N | 26 | .2 | 5 |
| L24+50W 2+25N | 24 | .2 | 3 |
| L24+50W 2+00N | 65 | .4 | 4 |
| L24+50W 1+75N | 43 | .3 | 1 |
| L24+50W 1+50N | 47 | .3 | 12 |
| L24+50W 1+25N | 414 | .7 | 250 |
| STD C/AU-S | 61 | 7.5 | 48 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L24+50W 1+00N | 113 | .1 | 2 |
| L24+50W 0+75N | 169 | .2 | 51 |
| L24+50W 0+50N | 185 | .4 | 34 |
| L24+50W 0+25S | 72 | .2 | 8 |
| L24+50W 0+50S | 145 | .5 | 15 |
| L24+50W 0+75S | 132 | .1 | 34 |
| L24+50W 1+00S | 183 | .2 | 32 |
| L24+50W 1+25S | 163 | .3 | 40 |
| L24+50W 1+50S | 86 | .1 | 5 |
| L24+50W 1+75S | 58 | .1 | 2 |
| L24+50W 2+00S | 54 | .1 | 1 |
| L24+50W 2+25S | 93 | .1 | 5 |
| L24+50W 2+50S | 97 | .1 | 6 |
| L23+50W 2+50N | 75 | .3 | 5 |
| L23+50W 2+25N | 36 | .1 | 2 |
| L23+50W 2+00N | 24 | .1 | 14 |
| L23+50W 1+75N | 33 | .1 | 18 |
| L23+50W 1+50N | 48 | .1 | 1 |
| L23+50W 1+25N | 278 | .7 | 105 |
| L23+50W 1+00N | 97 | .3 | 16 |
| L23+50W 0+75N | 168 | .4 | 61 |
| L23+50W 0+50N | 296 | .9 | 185 |
| L23+50W 0+25N | 222 | 1.1 | 43 |
| L23+50W 0+25S | 178 | .3 | 48 |
| L23+50W 0+50S | 122 | .3 | 22 |
| L23+50W 0+75S | 400 | 1.0 | 183 |
| L23+50W 1+00S | 272 | .5 | 91 |
| L23+50W 1+25S | 248 | .3 | 37 |
| L23+50W 1+50S | 162 | .3 | 69 |
| L23+50W 1+75S | 91 | .2 | 13 |
| L23+50W 2+00S | 64 | .1 | 1 |
| L23+50W 2+25S | 96 | .1 | 3 |
| L23+50W 2+50S | 64 | .1 | 1 |
| L21+00W 2+50S | 184 | .6 | 47 |
| L21+00W 2+75S | 142 | .3 | 43 |
| L21+00W 3+00S | 65 | .2 | 2 |
| STD C/AU-S | 62 | 7.4 | 49 |

ACME ANALYTICAL LABORATORIES
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011

DATE RECEIVED: JULY 27 1987

DATE REPORT MAILED:

Aug 10/87..

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS -80 MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

TECK EXPLORATION PROJECT-1354 File # 87-2734

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L22+50W 2+50N | 37 | .1 | 4 |
| L22+50W 2+25N | 46 | .1 | 6 |
| L22+50W 2+00N | 41 | .1 | 2 |
| L22+50W 1+75N | 36 | .1 | 7 |
| L22+50W 1+50N | 564 | .8 | 340 |
| L22+50W 1+25N | 306 | .4 | 108 |
| L22+50W 1+00N | 171 | .1 | 113 |
| L22+50W 0+75S | 1160 | .3 | 270 |
| L22+50W 1+00S | 511 | .2 | 121 |
| L22+50W 1+25S | 234 | .2 | 113 |
| L22+50W 1+50S | 314 | .8 | 67 |
| L22+50W 1+75S | 161 | 1.1 | 53 |
| L22+50W 2+00S | 59 | .1 | 5 |
| L22+50W 2+25S | 115 | .1 | 4 |
| L22+50W 2+50S | 106 | .1 | 1 |
| L21+50W 2+50N | 20 | .2 | 3 |
| L21+50W 2+25N | 32 | .4 | 1 |
| L21+50W 2+00N | 56 | .4 | 2 |
| STD C/AU-S | 58 | 7.2 | 47 |
| L21+50W 1+75N | 35 | .1 | 4 |
| L21+50W 1+50N | 534 | 1.1 | 310 |
| L21+50W 0+25S | 403 | .8 | 450 |
| L21+50W 0+50S | 175 | .3 | 36 |
| L21+50W 0+75S | 579 | .7 | 350 |
| L21+50W 1+00S | 233 | .2 | 84 |
| L21+50W 1+25S | 5593 | 2.8 | 1170 |
| L21+50W 1+50S | 95 | .1 | 18 |
| L21+50W 2+25S | 77 | .1 | 9 |
| L21+50W 2+50S | 100 | .4 | 12 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L21+00W 3+25S | 58 | .4 | 4 |
| L21+00W 3+50S | 64 | .5 | 2 |
| L20+50W 2+50N | 65 | .7 | 1 |
| L20+50W 2+25N | 57 | .3 | 4 |
| L20+50W 2+00N | 60 | .4 | 3 |
| L20+50W 1+75N | 62 | .3 | 7 |
| L20+50W 1+50N | 94 | .3 | 16 |
| L20+50W 1+25N | 323 | 1.4 | 290 |
| L20+50W 1+00N | 358 | 1.3 | 187 |
| L20+50W 0+75N | 512 | 1.7 | 164 |
| L20+50W 0+50N | 335 | 1.2 | 230 |
| L20+50W 0+25N | 343 | 1.0 | 310 |
| L20+50W 0+25S | 294 | .8 | 250 |
| L20+50W 0+50S | 130 | .8 | 61 |
| L20+50W 0+75S | 173 | .9 | 47 |
| L20+50W 1+00S | 242 | 1.3 | 260 |
| L20+50W 1+25S | 61 | .6 | 11 |
| L20+50W 1+50S | 310 | .8 | 172 |
| L20+50W 1+75S | 243 | 1.6 | 126 |
| L20+50W 2+00S | 264 | 1.5 | 104 |
| L20+50W 2+25S | 554 | 1.7 | 165 |
| L20+50W 2+50S | 115 | .7 | 10 |
| L20+50W 2+75S | 235 | .7 | 81 |
| L20+50W 3+00S | 127 | .7 | 38 |
| L20+50W 3+25S | 68 | .1 | 6 |
| L20+50W 3+50S | 69 | .5 | 5 |
| L20+00W 2+50S | 53 | .6 | 1 |
| L20+00W 2+75S | 63 | .5 | 1 |
| L20+00W 3+00S | 52 | .5 | 5 |
| L20+00W 3+25S | 72 | .4 | 1 |
| L20+00W 3+50S | 96 | .5 | 7 |
| L19+50W 2+50N | 96 | .6 | 1 |
| L19+50W 2+25N | 88 | .5 | 5 |
| L19+50W 2+00N | 161 | .8 | 9 |
| L19+50W 1+75N | 88 | .3 | 8 |
| L19+50W 1+50N | 92 | .3 | 1 |
| STD C/AU-S | 62 | 7.6 | 49 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L19+50W 1+25N | 94 | .3 | 2 |
| L19+50W 1+00N | 766 | 1.7 | 360 |
| L19+50W 0+75N | 323 | .8 | 121 |
| L19+50W 0+50N | 189 | .7 | 49 |
| L19+50W 0+25N | 336 | .8 | 122 |
| L19+50W 0+25S | 333 | .8 | 41 |
| L19+50W 0+50S | 412 | .9 | 195 |
| L19+50W 0+75S | 235 | .8 | 27 |
| L19+50W 1+00S | 384 | .5 | 265 |
| L19+50W 1+25S | 71 | .5 | 3 |
| L19+50W 1+50S | 81 | .7 | 25 |
| L19+50W 2+00S | 150 | 1.1 | 495 |
| L19+50W 2+25S | 45 | .4 | 195 |
| L19+50W 2+50S | 43 | .4 | 1 |
| L19+50W 2+75S | 50 | .5 | 1 |
| L19+50W 3+00S | 83 | .4 | 1 |
| L19+50W 3+25S | 78 | .4 | 4 |
| L19+50W 3+50S | 65 | .2 | 3 |
| L19+00W 2+50S | 49 | .4 | 1 |
| L19+00W 2+75S | 41 | .4 | 2 |
| L19+00W 3+00S | 50 | .3 | 2 |
| L19+00W 3+25S | 75 | .5 | 1 |
| L19+00W 3+50S | 58 | .4 | 1 |
| L18+50W 2+50N | 64 | .3 | 2 |
| L18+50W 2+25N | 69 | .4 | 4 |
| L18+50W 2+00N | 50 | .2 | 1 |
| L18+50W 1+75N | 58 | .3 | 1 |
| L18+50W 1+50N | 95 | .5 | 2 |
| L18+50W 1+25N | 90 | .4 | 2 |
| L18+50W 1+00N | 66 | .5 | 4 |
| L18+50W 0+75N | 525 | 1.3 | 445 |
| L18+50W 0+50N | 402 | .6 | 225 |
| L18+50W 0+25N | 827 | 1.2 | 450 |
| L18+50W 0+25S | 353 | .8 | 185 |
| L18+50W 0+50S | 1001 | 1.4 | 335 |
| L18+50W 0+75S | 179 | .6 | 3 |
| STD C/AU-S | 64 | 7.1 | 50 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L18+50W 1+00S | 964 | .7 | 480 |
| L18+50W 1+25S | 213 | .1 | 45 |
| L18+50W 1+50S | 109 | .1 | 44 |
| L18+50W 1+75S | 88 | .2 | 25 |
| L18+50W 2+00S | 94 | .1 | 75 |
| L18+50W 2+25S | 48 | .1 | 15 |
| L18+50W 2+50S | 59 | .1 | 5 |
| L18+50W 2+75S | 82 | .1 | 27 |
| L18+50W 3+00S | 91 | .1 | 5 |
| L18+50W 3+25S | 78 | .1 | 6 |
| L18+50W 3+50S | 118 | .1 | 52 |
| L18+00W 2+50S | 74 | .1 | 30 |
| L18+00W 2+75S | 65 | .1 | 10 |
| L18+00W 3+00S | 68 | .1 | 20 |
| L18+00W 3+25S | 77 | .1 | 10 |
| L18+00W 3+50S | 91 | .1 | 6 |
| L17+50W 2+50N | 188 | .3 | 53 |
| L17+50W 2+25N | 53 | .2 | 2 |
| L17+50W 2+00N | 55 | .2 | 4 |
| L17+50W 1+75N | 77 | .1 | 6 |
| L17+50W 1+50N | 46 | .1 | 5 |
| L17+50W 1+25N | 67 | .1 | 3 |
| L17+50W 1+00N | 51 | .5 | 5 |
| L17+50W 0+75N | 86 | .3 | 18 |
| L17+50W 0+50N | 640 | .9 | 240 |
| L17+50W 0+25N | 800 | 1.9 | 250 |
| L17+50W 0+25S | 272 | .8 | 53 |
| L17+50W 0+50S | 267 | .7 | 72 |
| L17+50W 0+75S | 522 | 1.3 | 230 |
| L17+50W 1+00S | 266 | .5 | 61 |
| L17+50W 1+25S | 810 | .7 | 200 |
| L17+50W 1+50S | 330 | .4 | 78 |
| L17+50W 2+25S | 82 | .2 | 15 |
| L17+50W 2+50S | 283 | .4 | 123 |
| L16+50W 2+50N | 67 | .1 | 1 |
| L16+50W 2+25N | 51 | .2 | 2 |
| STD C/AU-S | 61 | 7.6 | 53 |

| SAMPLE# | | CU PPM | AG PPM | AU* PPB |
|---------|-------|-----------|-----------|------------|
| L16+50W | 2+00N | 43 | .1 | 1 |
| L16+50W | 1+75N | 50 | .1 | 2 |
| L16+50W | 1+50N | 63 | .4 | 6 |
| L16+50W | 1+25N | 193 | .9 | 23 |
| L16+50W | 1+00N | 111 | .3 | 8 |
| L16+50W | 0+75N | 126 | .2 | 8 |
| L16+50W | 0+50N | 402 | 1.0 | 235 |
| L16+50W | 0+25N | 275 | 1.0 | 215 |
| L16+50W | 0+25S | 112 | .2 | 23 |
| L16+50W | 0+75S | 497 | .9 | 245 |
| L16+50W | 1+00S | 504 | .7 | 85 |
| L16+50W | 2+00S | 155 | .3 | 32 |
| L16+50W | 2+25S | 200 | .6 | 30 |
| L16+50W | 2+50S | 272 | .9 | 62 |
| L15+50W | 2+50N | 48 | .1 | 5 |
| L15+50W | 2+25N | 39 | .1 | 2 |
| L15+50W | 2+00N | 52 | .1 | 3 |
| L15+50W | 1+75N | 63 | .2 | 1 |
| L15+50W | 1+50N | 66 | .3 | 3 |
| L15+50W | 1+25N | 196 | .1 | 85 |
| L15+50W | 1+00N | 90 | .2 | 5 |
| L15+50W | 0+75N | 52 | .1 | 10 |
| L15+50W | 0+50N | 139 | .3 | 13 |
| L15+50W | 0+25N | 269 | .6 | 80 |
| L15+50W | 0+50S | 724 | .5 | 106 |
| L15+50W | 0+75S | 4313 | 1.2 | 1050 |
| L15+50W | 1+00S | 768 | .7 | 215 |
| L15+50W | 1+25S | 1760 | .7 | 345 |
| L15+50W | 1+50S | 1044 | .4 | 195 |
| L15+50W | 1+75S | 224 | .9 | 33 |
| L15+50W | 2+00S | 234 | 2.4 | 68 |
| L15+50W | 2+25S | 133 | .4 | 10 |
| L15+50W | 2+50S | 79 | .2 | 1 |
| L14+50W | 2+50N | 87 | .1 | 1 |
| L14+50W | 2+25N | 66 | .1 | 1 |
| L14+50W | 2+00N | 14 | .1 | 1 |
| STD C | | 62 | 7.6 | 50 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L14+50W 1+75N | 328 | .3 | 15 |
| L14+50W 1+50N | 100 | .6 | 7 |
| L14+50W 1+25N | 61 | .2 | 3 |
| L14+50W 1+00N | 81 | .4 | 5 |
| L14+50W 0+75N | 88 | .6 | 5 |
| L14+50W 0+50N | 46 | .4 | 4 |
| L14+50W 0+25N | 84 | .5 | 11 |
| L14+50W 0+25S | 866 | .8 | 280 |
| L14+50W 0+50S | 451 | .7 | 220 |
| L14+50W 0+75S | 497 | .9 | 144 |
| L14+50W 1+00S | 533 | .6 | 125 |
| L14+50W 1+75S | 98 | .2 | 12 |
| L14+50W 2+00S | 98 | .5 | 6 |
| L14+50W 2+25S | 89 | .1 | 2 |
| L14+50W 2+50S | 42 | .3 | 1 |
| L13+50W 2+50N | 66 | .1 | 1 |
| L13+50W 2+25N | 55 | .3 | 2 |
| L13+50W 2+00N | 126 | .3 | 7 |
| L13+50W 1+75N | 86 | .4 | 9 |
| L13+50W 1+50N | 49 | .4 | 4 |
| L13+50W 1+25N | 52 | .1 | 3 |
| L13+50W 1+00N | 67 | .3 | 4 |
| L13+50W 0+75N | 58 | .3 | 6 |
| L13+50W 0+50N | 88 | .4 | 11 |
| L13+50W 0+25N | 80 | .7 | 31 |
| L13+50W 0+25S | 1317 | 1.0 | 178 |
| L13+50W 0+50S | 715 | 2.8 | 550 |
| L13+50W 1+50S | 45 | .5 | 7 |
| L13+50W 1+75S | 50 | .4 | 3 |
| L13+50W 2+00S | 82 | .4 | 2 |
| L13+50W 2+25S | 61 | .3 | 1 |
| L13+50W 2+50S | 90 | .2 | 4 |
| L12+50W 2+50N | 84 | .3 | 2 |
| L12+50W 2+25N | 90 | .5 | 9 |
| L12+50W 2+00N | 91 | .3 | 7 |
| L12+50W 1+75N | 110 | .3 | 8 |
| STD C/AU-S | 60 | 7.3 | 52 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L12+50W 1+50N | 84 | .5 | 8 |
| L12+50W 1+25N | 180 | .4 | 7 |
| L12+50W 1+00N | 110 | .3 | 12 |
| L12+50W 0+75N | 193 | .7 | 129 |
| L12+50W 0+50N | 167 | 2.9 | 71 |
| L12+50W 0+25S | 259 | .7 | 68 |
| L12+50W 0+50S | 638 | 2.3 | 415 |
| L12+50W 0+75S | 1450 | 1.8 | 535 |
| L12+50W 0+90S | 110 | .8 | 31 |
| L12+50W 1+55S | 119 | .3 | 4 |
| L12+50W 1+75S | 119 | .4 | 1 |
| L12+50W 2+00S | 80 | .4 | 5 |
| L12+50W 2+25S | 76 | .5 | 14 |
| L12+50W 2+50S | 86 | .1 | 160 |
| L11+50W 2+50N | 97 | .4 | 5 |
| L11+50W 2+25N | 133 | .8 | 10 |
| L11+50W 2+00N | 81 | .5 | 1 |
| L11+50W 1+75N | 96 | .4 | 1 |
| L11+50W 1+50N | 56 | .4 | 2 |
| L11+50W 1+25N | 58 | .5 | 1 |
| L11+50W 1+00N | 75 | .4 | 1 |
| L11+50W 0+75N | 55 | .4 | 21 |
| L11+50W 0+50N | 105 | .6 | 180 |
| L11+50W 0+25N | 166 | 1.3 | 665 |
| L11+50W 0+25S | 401 | 3.0 | 695 |
| L11+50W 0+50S | 424 | 1.6 | 495 |
| L11+50W 0+75S | 294 | 1.6 | 290 |
| L11+50W 1+75S | 99 | .4 | 34 |
| L11+50W 2+00S | 82 | .4 | 12 |
| L11+50W 2+25S | 61 | .7 | 1 |
| L11+50W 2+50S | 64 | .4 | 1 |
| L10+50W 2+50N | 119 | .4 | 1 |
| L10+50W 2+25N | 62 | .3 | 3 |
| L10+50W 2+00N | 119 | .3 | 2 |
| L10+50W 1+75N | 75 | .4 | 2 |
| L10+50W 1+50N | 66 | .4 | 1 |
| STD C/AU-S | 60 | 7.3 | 47 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|---------------|-----------|-----------|------------|
| L10+50W 1+25N | 49 | .3 | 5 |
| L10+50W 1+00N | 72 | .2 | 17 |
| L10+50W 0+75N | 58 | .5 | 7 |
| L10+50W 0+50N | 83 | .4 | 750 |
| L10+50W 0+25N | 1256 | 1.3 | 430 |
| L10+50W 0+25S | 367 | 2.8 | 211 |
| L10+50W 0+55S | 1229 | 1.8 | 240 |
| L10+50W 0+75S | 71 | .5 | 93 |
| L10+50W 1+00S | 93 | .7 | 110 |
| L10+50W 1+40S | 249 | 1.1 | 105 |
| L10+50W 2+50S | 138 | .4 | 6 |
| STD C/AU-S | 61 | 7.4 | 50 |

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: P1-3 SOIL P4-ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: *D. Toyer* DEAN TOYE, CERTIFIED B.C. ASSAYER

TECK EXPLORATION PROJECT-1354 File # 87-3651 Page 1

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|--------------|-----------|-----------|------------|
| L9+50W 2+50N | 93 | .1 | 6 |
| L9+50W 2+25N | 94 | .1 | 11 |
| L9+50W 2+00N | 76 | .1 | 5 |
| L9+50W 1+75N | 76 | .1 | 3 |
| L9+50W 1+50N | 58 | .2 | 7 |
| L9+50W 1+25N | 64 | .2 | 3 |
| L9+50W 1+00N | 70 | .2 | 7 |
| L9+50W 0+75N | 84 | .3 | 49 |
| L9+50W 0+50N | 356 | .3 | 34 |
| L9+50W 0+25N | 133 | .4 | 94 |
| L9+50W 0+25S | 174 | 3.2 | 645 |
| L9+50W 0+50S | 896 | 1.0 | 104 |
| L9+50W 1+25S | 137 | .2 | 305 |
| L9+50W 1+50S | 384 | .9 | 151 |
| L9+50W 1+75S | 245 | .6 | 46 |
| L9+50W 2+25S | 108 | .1 | 4 |
| L9+50W 2+50S | 90 | .1 | 2 |
| L9W 2+50N | 90 | .3 | 7 |
| L9W 2+25N | 75 | .1 | 6 |
| L9W 2+00N | 99 | .3 | 5 |
| L9W 1+75N | 53 | .1 | 4 |
| L9W 1+50N | 62 | .1 | 5 |
| L9W 1+25N | 72 | .1 | 43 |
| L9W 1+25S | 129 | .3 | 29 |
| L9W 1+50S | 106 | .3 | 17 |
| L9W 1+75S | 112 | .4 | 6 |
| L9W 2+00S | 161 | .1 | 13 |
| L9W 2+25S | 125 | .1 | 11 |
| L9W 2+50S | 80 | .2 | 3 |
| L8+50W 2+50N | 82 | .1 | 7 |
| L8+50W 2+25N | 75 | .1 | 4 |
| L8+50W 2+00N | 94 | .2 | 14 |
| L8+50W 1+75N | 70 | .1 | 5 |
| L8+50W 1+50N | 85 | .1 | 10 |
| L8+50W 1+00N | 450 | .7 | 67 |
| L8+50W 0+25N | 91 | .2 | 28 |
| STD C/AU-S | 61 | 7.0 | 49 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|--------------|-----------|-----------|------------|
| L8+50W 0+25S | 112 | .9 | 68 |
| L8+50W 1+00S | 161 | .6 | 41 |
| L8+50W 1+25S | 102 | .5 | 12 |
| L8+50W 1+50S | 83 | .3 | 11 |
| L8+50W 1+75S | 122 | .3 | 14 |
| L8+50W 2+00S | 153 | .2 | 11 |
| L8+50W 2+25S | 166 | .3 | 6 |
| L8+50W 2+50S | 112 | .3 | 9 |
| L8+00W 2+50N | 78 | .1 | 25 |
| L8+00W 2+25N | 58 | .2 | 5 |
| L8+00W 2+00N | 60 | .1 | 9 |
| L8+00W 1+25N | 344 | .6 | 132 |
| L8+00W 0+25S | 95 | .3 | 20 |
| L8+00W 0+50S | 101 | .3 | 24 |
| L8+00W 1+00S | 269 | .7 | 73 |
| L8+00W 1+25S | 141 | .3 | 14 |
| L8+00W 1+50S | 149 | .1 | 7 |
| L8+00W 1+75S | 194 | .1 | 5 |
| L8+00W 2+00S | 45 | .1 | 17 |
| L8+00W 2+25S | 118 | .3 | 5 |
| L7+50W 2+50N | 74 | .1 | 6 |
| L7+50W 2+25N | 64 | .2 | 7 |
| L7+50W 2+00N | 72 | .3 | 225 |
| L7+50W 1+75N | 86 | .2 | 24 |
| L7+50W 0+75N | 121 | .4 | 111 |
| L7+50W 0+50N | 112 | .6 | 41 |
| L7+50W 0+25N | 214 | .9 | 102 |
| L7+00W 2+50N | 81 | .3 | 12 |
| L7+00W 2+25N | 89 | .3 | 12 |
| L6+50W 2+50N | 90 | .3 | 28 |
| L6+50W 2+25N | 110 | .2 | 15 |
| L6+50W 2+00N | 98 | .4 | 23 |
| L6+50W 1+00N | 131 | .7 | 31 |
| L6+50W 0+75N | 91 | .6 | 25 |
| L6+50W 0+50N | 60 | .3 | 5 |
| L6+50W 0+25N | 118 | .3 | 14 |
| STD C/AU-S | 61 | 7.1 | 50 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|--------------|-----------|-----------|------------|
| L6+00W 2+50N | 86 | .2 | 11 |
| L6+00W 2+25N | 108 | .5 | 49 |
| L5+50W 2+50N | 77 | .3 | 109 |
| L5+50W 0+50N | 101 | .2 | 12 |
| L5+50W 0+25N | 1181 | .2 | 63 |
| L4+50W 2+50N | 118 | .7 | 50 |
| L4+50W 2+25N | 121 | .9 | 46 |
| L4+50W 2+00N | 198 | 4.4 | 1040 |
| L4+50W 1+75N | 186 | .9 | 310 |
| L4+50W 1+50N | 159 | .5 | 46 |
| L4+50W 1+25N | 111 | .3 | 33 |
| L4+50W 1+00N | 100 | .2 | 68 |
| L4+50W 0+75N | 86 | .2 | 40 |
| L4+50W 0+50N | 292 | .5 | 62 |
| L4+50W 0+25N | 287 | .3 | 13 |
| STD C/AU-S | 61 | 7.0 | 47 |

| SAMPLE# | MO PPH | CU PPH | PB PPH | ZN PPH | AG PPH | NI PPH | CO PPH | MN PPH | FE % | AS PPH | U PPH | AU PPH | TH PPH | SR PPH | CD PPH | SB PPH | BI PPH | V PPH | CA % | P % | LA PPH | CR PPH | MG % | BA PPH | TI % | B PPH | AL % | NA % | K % | W PPH | AU# PPB |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|------------|
| L22+50W 0+75N | 4 | 316 | 14 | 143 | .6 | 59 | 23 | 1654 | 8.13 | 13 | 5 | ND | 7 | 79 | 2 | 2 | 2 | 82 | .66 | .152 | 27 | 70 | 1.11 | 595 | .61 | 2 | 3.31 | .22 | .15 | 1 | 48 |
| L22+50W 0+50N | 5 | 318 | 28 | 143 | .8 | 51 | 22 | 1031 | 7.97 | 19 | 5 | ND | 8 | 177 | 2 | 2 | 2 | 81 | 1.29 | .145 | 29 | 66 | 1.13 | 542 | .63 | 7 | 3.50 | .48 | .27 | 1 | 85 |
| L22+50W 0+25N | 11 | 327 | 44 | 348 | .9 | 31 | 28 | 3937 | 13.95 | 106 | 5 | ND | 6 | 48 | 3 | 2 | 2 | 49 | .54 | .182 | 29 | 39 | .75 | 629 | .23 | 2 | 1.76 | .08 | .10 | 1 | 55 |
| L22+50W 0+50S | 15 | 583 | 20 | 136 | 1.9 | 54 | 26 | 3604 | 13.87 | 25 | 5 | ND | 7 | 38 | 2 | 2 | 2 | 67 | .43 | .175 | 26 | 55 | 1.05 | 831 | .34 | 2 | 2.09 | .05 | .10 | 1 | 1045 |
| L22+00W 0+25S | 13 | 765 | 19 | 106 | .4 | 36 | 25 | 2667 | 11.64 | 17 | 5 | ND | 6 | 36 | 1 | 2 | 4 | 58 | .32 | .147 | 30 | 45 | .94 | 895 | .26 | 2 | 2.29 | .06 | .10 | 1 | 95 |
| L22+00W 0+25S A | 7 | 358 | 6 | 102 | .7 | 29 | 20 | 2025 | 8.66 | 19 | 5 | ND | 4 | 36 | 1 | 2 | 2 | 63 | .30 | .129 | 24 | 41 | .75 | 994 | .22 | 2 | 2.58 | .02 | .09 | 1 | 79 |
| L22+00W 0+75S | 6 | 570 | 7 | 97 | .8 | 56 | 21 | 1482 | 8.26 | 8 | 5 | ND | 7 | 45 | 3 | 2 | 2 | 83 | .48 | .084 | 36 | 74 | 1.06 | 890 | .58 | 4 | 4.20 | .05 | .10 | 1 | 78 |
| L22+00W 0+75S A | 15 | 360 | 16 | 75 | .7 | 42 | 18 | 1206 | 7.80 | 27 | 5 | ND | 4 | 22 | 2 | 2 | 6 | 54 | .20 | .099 | 16 | 37 | 1.05 | 558 | .14 | 5 | 1.52 | .02 | .09 | 1 | 390 |
| L22+00W 1+25S | 4 | 64 | 32 | 90 | .2 | 39 | 23 | 1263 | 8.16 | 5 | 5 | ND | 7 | 41 | 2 | 2 | 2 | 97 | .33 | .104 | 37 | 67 | .49 | 257 | .66 | 2 | 5.92 | .07 | .05 | 1 | 9 |
| L22+00W 1+25S A | 23 | 1254 | 16 | 111 | 1.8 | 47 | 26 | 3893 | 12.88 | 35 | 5 | ND | 6 | 46 | 1 | 2 | 2 | 58 | .47 | .152 | 31 | 49 | .90 | 540 | .32 | 2 | 2.28 | .11 | .12 | 1 | 590 |
| L22+00W 1+75S | 3 | 219 | 23 | 113 | .9 | 66 | 20 | 1395 | 8.28 | 13 | 5 | ND | 4 | 50 | 1 | 2 | 2 | 76 | .82 | .107 | 36 | 72 | 1.18 | 541 | .46 | 4 | 3.27 | .04 | .07 | 1 | 51 |
| L22+00W 2+25S | 4 | 156 | 13 | 125 | .2 | 68 | 22 | 1530 | 8.34 | 11 | 5 | ND | 5 | 62 | 1 | 2 | 2 | 82 | .82 | .116 | 27 | 67 | 1.33 | 310 | .44 | 3 | 2.99 | .13 | .11 | 1 | 14 |
| L21+50W 1+75S | 3 | 214 | 17 | 133 | .6 | 61 | 20 | 1143 | 8.78 | 9 | 5 | ND | 6 | 80 | 2 | 2 | 2 | 92 | .73 | .142 | 30 | 79 | 1.20 | 292 | .63 | 2 | 4.00 | .19 | .13 | 1 | 59 |
| L21+50W 2+00S | 4 | 313 | 16 | 128 | .8 | 78 | 24 | 1262 | 8.93 | 17 | 5 | ND | 7 | 69 | 1 | 2 | 2 | 85 | .66 | .107 | 23 | 77 | 1.69 | 299 | .57 | 2 | 3.19 | .18 | .12 | 2 | 195 |
| L21+00W 0+75N | 7 | 663 | 24 | 105 | .8 | 32 | 25 | 1834 | 10.37 | 24 | 5 | ND | 5 | 39 | 2 | 2 | 2 | 58 | .50 | .137 | 18 | 35 | .91 | 497 | .18 | 2 | 1.95 | .03 | .13 | 1 | 265 |
| L21+00W 0+25N | 8 | 442 | 24 | 130 | .5 | 48 | 26 | 2783 | 10.31 | 18 | 5 | ND | 6 | 55 | 1 | 3 | 3 | 91 | .41 | .143 | 33 | 68 | .95 | 780 | .50 | 3 | 4.25 | .11 | .11 | 1 | 116 |
| L21+00W 1+75S | 3 | 105 | 28 | 135 | .5 | 64 | 21 | 1045 | 8.51 | 8 | 5 | ND | 7 | 88 | 2 | 2 | 2 | 98 | .71 | .142 | 34 | 84 | 1.28 | 263 | .74 | 3 | 4.59 | .19 | .12 | 1 | 41 |
| L21+00W 2+25S | 4 | 184 | 25 | 102 | .5 | 39 | 20 | 1649 | 7.65 | 8 | 5 | ND | 5 | 73 | 1 | 2 | 2 | 90 | 1.09 | .122 | 32 | 65 | .61 | 292 | .54 | 2 | 4.45 | .05 | .04 | 1 | 91 |
| L20+00W 0+75N | 7 | 495 | 35 | 240 | 2.0 | 35 | 24 | 2877 | 10.20 | 31 | 5 | ND | 4 | 34 | 2 | 2 | 7 | 47 | .30 | .154 | 22 | 35 | .81 | 536 | .19 | 2 | 1.63 | .06 | .10 | 1 | 275 |
| L20+00W 0+25N | 5 | 297 | 18 | 109 | .5 | 65 | 20 | 1308 | 8.74 | 12 | 5 | ND | 6 | 51 | 1 | 2 | 3 | 85 | .45 | .131 | 31 | 68 | 1.28 | 496 | .55 | 3 | 3.82 | .12 | .11 | 1 | 103 |
| L20+00W 0+25S | 5 | 133 | 18 | 102 | .5 | 53 | 20 | 1115 | 7.85 | 8 | 5 | ND | 7 | 37 | 1 | 2 | 2 | 83 | .43 | .099 | 32 | 65 | 1.13 | 541 | .54 | 4 | 4.32 | .05 | .08 | 1 | 30 |
| L20+00W 0+75S | 5 | 151 | 19 | 122 | .4 | 67 | 24 | 1387 | 8.57 | 10 | 5 | ND | 7 | 45 | 2 | 2 | 2 | 92 | .60 | .109 | 34 | 65 | 1.45 | 449 | .60 | 2 | 4.15 | .08 | .08 | 1 | 36 |
| L20+00W 1+25S | 3 | 75 | 8 | 111 | .4 | 69 | 20 | 1149 | 7.03 | 8 | 5 | ND | 6 | 34 | 1 | 2 | 2 | 76 | .44 | .092 | 25 | 61 | 1.37 | 296 | .51 | 3 | 3.27 | .06 | .07 | 1 | 9 |
| L20+00W 1+75S | 6 | 200 | 19 | 114 | .8 | 41 | 25 | 2478 | 11.22 | 21 | 5 | ND | 5 | 39 | 1 | 2 | 5 | 74 | .37 | .154 | 28 | 47 | 1.03 | 319 | .27 | 3 | 2.39 | .07 | .10 | 1 | 42 |
| L20+00W 2+25S | 4 | 438 | 22 | 116 | .8 | 59 | 21 | 1387 | 8.57 | 18 | 5 | ND | 7 | 32 | 1 | 2 | 2 | 90 | .38 | .113 | 36 | 68 | 1.21 | 225 | .54 | 2 | 4.44 | .04 | .07 | 1 | 118 |
| L19+00W 0+25N | 12 | 816 | 6 | 61 | 1.2 | 22 | 21 | 2024 | 10.36 | 28 | 5 | ND | 5 | 26 | 1 | 2 | 2 | 45 | .43 | .126 | 24 | 30 | .68 | 540 | .11 | 2 | 1.63 | .01 | .09 | 1 | 445 |
| L19+00W 0+25S | 4 | 250 | 20 | 88 | .5 | 55 | 22 | 1564 | 7.86 | 13 | 5 | ND | 5 | 40 | 2 | 2 | 2 | 83 | .37 | .108 | 23 | 62 | 1.04 | 868 | .44 | 4 | 3.86 | .03 | .07 | 1 | 62 |
| L19+00W 0+75S | 20 | 515 | 19 | 66 | 2.0 | 24 | 15 | 1434 | 20.84 | 54 | 5 | ND | 6 | 23 | 1 | 2 | 3 | 48 | .09 | .414 | 8 | 25 | .57 | 143 | .16 | 2 | .87 | .02 | .10 | 1 | 405 |
| L19+00W 0+75S A | 10 | 563 | 16 | 82 | 1.1 | 32 | 15 | 1178 | 8.10 | 20 | 5 | ND | 5 | 34 | 1 | 3 | 3 | 65 | .24 | .110 | 18 | 41 | .68 | 559 | .26 | 6 | 2.13 | .03 | .17 | 1 | 220 |
| L19+00W 1+25S | 5 | 84 | 34 | 102 | .3 | 55 | 21 | 1364 | 8.88 | 4 | 5 | ND | 9 | 43 | 2 | 2 | 2 | 105 | .38 | .154 | 39 | 76 | 1.05 | 207 | .77 | 2 | 5.89 | .10 | .08 | 1 | 5 |
| L19+00W 1+75S | 5 | 78 | 25 | 131 | .2 | 66 | 24 | 1440 | 8.98 | 14 | 5 | ND | 8 | 77 | 1 | 2 | 2 | 97 | .76 | .135 | 34 | 80 | 1.39 | 254 | .64 | 3 | 4.56 | .18 | .12 | 1 | 3 |
| L19+00W 2+25S | 4 | 65 | 22 | 117 | .3 | 43 | 21 | 1618 | 7.78 | 5 | 5 | ND | 7 | 32 | 1 | 2 | 2 | 99 | .31 | .124 | 38 | 68 | .73 | 175 | .62 | 4 | 5.61 | .05 | .05 | 1 | 2 |
| L18+00W 0+25N | 8 | 414 | 25 | 106 | 1.0 | 34 | 19 | 1564 | 8.38 | 13 | 5 | ND | 5 | 55 | 1 | 2 | 2 | 79 | .73 | .121 | 34 | 52 | .62 | 707 | .43 | 3 | 3.98 | .05 | .07 | 1 | 136 |
| L18+00W 0+25S | 5 | 197 | 18 | 89 | 1.0 | 44 | 20 | 1494 | 7.60 | 6 | 5 | ND | 7 | 40 | 1 | 2 | 2 | 87 | .44 | .115 | 32 | 62 | .85 | 621 | .49 | 4 | 4.29 | .04 | .05 | 1 | 49 |
| L18+00W 0+75S | 4 | 647 | 17 | 114 | .5 | 55 | 20 | 1258 | 7.66 | 11 | 6 | ND | 7 | 31 | 2 | 4 | 2 | 85 | .39 | .095 | 29 | 66 | 1.09 | 516 | .54 | 2 | 4.27 | .04 | .07 | 1 | 76 |
| L18+00W 1+25S | 5 | 181 | 23 | 113 | .7 | 53 | 23 | 1690 | 8.27 | 11 | 5 | ND | 7 | 42 | 3 | 2 | 2 | 94 | .43 | .136 | 33 | 66 | 1.06 | 351 | .58 | 3 | 4.74 | .09 | .08 | 1 | 32 |
| STD C/AU-S | 18 | 60 | 40 | 132 | 7.2 | 68 | 28 | 1062 | 4.13 | 28 | 22 | 7 | 40 | 52 | 18 | 17 | 19 | 60 | .47 | .086 | 39 | 68 | .85 | 183 | .08 | 37 | 1.78 | .06 | .13 | 12 | 47 |

| SAMPLE# | MO PPM | CU PPM | PB PPM | ZN PPM | AG PPM | NI PPM | CO PPM | MN PPM | FE % | AS PPM | U PPM | AU PPM | TH PPM | SR PPM | CD PPM | SB PPM | BI PPM | V PPM | CA % | P % | LA PPM | CR PPM | MG % | BA PPM | TI % | B PPM | AL % | NA % | K % | W PPM | AU# PPB |
|---------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|------------|
| L18+00W 1+75S | 4 | 119 | 15 | 120 | .3 | 49 | 22 | 1530 | 8.28 | 10 | 5 | ND | 9 | 98 | 2 | 2 | 2 | 91 | .80 | .162 | 33 | 56 | 1.07 | 307 | .60 | 9 | 4.16 | .27 | .17 | 1 | 32 |
| L18+00W 2+25S | 4 | 82 | 11 | 119 | .1 | 51 | 19 | 1187 | 7.65 | 12 | 5 | ND | 9 | 70 | 1 | 2 | 2 | 98 | .56 | .153 | 36 | 56 | 1.06 | 294 | .60 | 3 | 4.78 | .16 | .12 | 1 | 10 |
| STD C/AU-S | 20 | 61 | 39 | 129 | 7.1 | 68 | 29 | 1059 | 4.09 | 40 | 23 | 7 | 45 | 51 | 18 | 17 | 21 | 59 | .48 | .088 | 39 | 58 | .87 | 182 | .07 | 36 | 1.79 | .06 | .12 | 14 | 48 |
| L17+50W 1+75S | 3 | 118 | 15 | 145 | .1 | 50 | 22 | 1089 | 6.99 | 7 | 5 | ND | 8 | 154 | 1 | 2 | 2 | 88 | 1.18 | .148 | 29 | 58 | 1.12 | 353 | .61 | 3 | 4.15 | .49 | .26 | 1 | 28 |
| L17+50W 2+00S | 2 | 96 | 8 | 133 | .1 | 55 | 19 | 1183 | 7.35 | 6 | 5 | ND | 8 | 59 | 1 | 2 | 2 | 92 | .58 | .137 | 32 | 61 | 1.18 | 403 | .52 | 11 | 4.00 | .12 | .11 | 1 | 12 |
| L17+00W 0+25N | 6 | 285 | 10 | 134 | .3 | 74 | 26 | 1672 | 9.22 | 11 | 5 | ND | 8 | 37 | 2 | 2 | 7 | 93 | .37 | .150 | 27 | 60 | 1.63 | 213 | .60 | 4 | 3.51 | .10 | .10 | 1 | 61 |
| L17+00W 0+25S | 6 | 306 | 8 | 145 | .6 | 60 | 24 | 1466 | 8.41 | 17 | 5 | ND | 7 | 81 | 1 | 2 | 2 | 89 | .57 | .163 | 25 | 58 | 1.28 | 318 | .51 | 3 | 3.49 | .25 | .17 | 1 | 57 |
| L17+00W 1+25S | 2 | 207 | 18 | 147 | .2 | 43 | 18 | 1149 | 6.21 | 11 | 5 | ND | 7 | 54 | 1 | 3 | 2 | 81 | .52 | .128 | 32 | 50 | .85 | 442 | .42 | 5 | 3.57 | .11 | .11 | 1 | 31 |
| L17+00W 1+75S | 3 | 145 | 10 | 139 | .1 | 42 | 17 | 1018 | 5.96 | 10 | 5 | ND | 5 | 85 | 1 | 2 | 2 | 77 | .75 | .113 | 26 | 46 | 1.01 | 350 | .36 | 2 | 2.91 | .22 | .15 | 1 | 21 |
| L17+00W 2+25S | 3 | 191 | 14 | 119 | .7 | 34 | 14 | 1064 | 5.69 | 23 | 5 | ND | 6 | 21 | 1 | 2 | 2 | 69 | .25 | .083 | 25 | 39 | .83 | 301 | .21 | 4 | 2.53 | .02 | .06 | 1 | 79 |
| L16+50W 0+50S | 6 | 404 | 17 | 152 | .7 | 51 | 21 | 1136 | 7.17 | 13 | 5 | ND | 7 | 112 | 2 | 2 | 2 | 78 | .95 | .144 | 27 | 53 | 1.12 | 655 | .51 | 9 | 3.37 | .34 | .20 | 1 | 66 |
| L16+00W 0+25N | 8 | 298 | 12 | 106 | .4 | 56 | 24 | 1906 | 9.33 | 13 | 5 | ND | 6 | 43 | 2 | 5 | 2 | 90 | .43 | .136 | 33 | 54 | 1.27 | 318 | .55 | 2 | 4.03 | .11 | .10 | 1 | 137 |
| L16+00W 0+25S | 5 | 262 | 10 | 125 | .1 | 75 | 23 | 1712 | 8.14 | 7 | 5 | ND | 7 | 70 | 1 | 2 | 2 | 80 | .65 | .165 | 28 | 58 | 1.49 | 455 | .56 | 6 | 3.59 | .22 | .17 | 1 | 80 |
| L16+00W 0+75S | 7 | 311 | 31 | 176 | 1.0 | 54 | 25 | 1827 | 8.63 | 19 | 5 | ND | 8 | 99 | 3 | 2 | 3 | 86 | .72 | .165 | 32 | 57 | 1.23 | 756 | .53 | 2 | 3.60 | .31 | .21 | 2 | 85 |
| L16+00W 1+25S | 5 | 272 | 22 | 160 | .1 | 57 | 22 | 856 | 7.20 | 14 | 5 | ND | 5 | 148 | 1 | 3 | 2 | 81 | 1.21 | .144 | 24 | 56 | 1.24 | 455 | .56 | 2 | 3.56 | .48 | .25 | 1 | 29 |
| L16+00W 1+50S | 4 | 146 | 22 | 159 | .5 | 56 | 23 | 974 | 6.69 | 6 | 5 | ND | 6 | 166 | 1 | 2 | 2 | 78 | 1.32 | .130 | 21 | 54 | 1.29 | 313 | .53 | 7 | 3.38 | .56 | .29 | 1 | 22 |
| L16+00W 2+25S | 2 | 79 | 15 | 113 | .1 | 52 | 17 | 935 | 5.85 | 8 | 5 | ND | 5 | 57 | 1 | 2 | 2 | 76 | .52 | .098 | 21 | 48 | 1.19 | 228 | .38 | 4 | 2.73 | .14 | .10 | 1 | 17 |

| SAMPLE# | CU PPM | AG PPM | AU* FPB |
|------------|-----------|-----------|------------|
| 24901 | 77 | 2.5 | 495 |
| 24902 | 99 | .7 | 103 |
| 24903 | 84 | .3 | 110 |
| 24904 | 55 | .3 | 81 |
| 24905 | 109 | .2 | 58 |
| 24906 | 793 | 10.6 | 2440 |
| 24907 | 65 | 6.9 | 1550 |
| 24908 | 114 | 1.0 | 66 |
| 24909 | 182 | 22.9 | 2980 |
| 24910 | 187 | 6.0 | 1350 |
| 24911 | 256 | 5.3 | 1940 |
| 24912 | 160 | 7.6 | 1390 |
| 24913 | 87 | 25.4 | 5030 |
| STD C/AU-R | 59 | 7.3 | 510 |

* HIGHS
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PAGE

ACME ANALYTICAL LABORATORIES LTD.

DATE RECEIVED AUGUST 16 1987

852 E. HASTINGS, VANCOUVER B.C.

PH: (604)253-3158 COMPUTER LINE:251-1011

DATE REPORTS MAILED

Aug 20/87

ASSAY CERTIFICATE

SAMPLE TYPE : PULP
AU** BY FIRE ASSAY

ASSAYER *D. Toye* DEAN TOYE , CERTIFIED B.C. ASSAYER

TECK EXPLORATION PROJECT 1354 FILE# 87-2886 R

PAGE#

| SAMPLE | Au** oz/t |
|--------|--------------|
| 24906 | .062 |
| 24907 | .033 |
| 24909 | .055 |
| 24910 | .056 |
| 24911 | .042 |
| 24912 | .029 |
| 24913 | .109 |

| SAMPLE# | CU PPM | AG PPM | AU* PPB |
|------------|-----------|-----------|------------|
| 24931 | 65 | .1 | 45 |
| 24936 | 59 | .8 | 195 |
| 24937 | 341 | .5 | 225 |
| 24938 | 185 | .5 | 315 |
| 24939 | 582 | .4 | 87 |
| 30565 | 382 | 1.8 | 540 |
| 30566 | 287 | .3 | 150 |
| 30567 | 62 | 1.1 | 93 |
| 30569 | 1338 | .5 | 4 |
| 30570 | 23 | .1 | 9 |
| 30580 | 30 | .2 | 26 |
| 30581 | 164 | .8 | 315 |
| 30582 | 361 | 1.1 | 685 |
| 30583 | 99 | 2.6 | 540 |
| 30584 | 212 | 1.3 | 91 |
| 30585 | 177 | 1.8 | 265 |
| 30586 | 177 | .6 | 72 |
| 30587 | 162 | .7 | 165 |
| STD C/AU-R | 61 | 7.2 | 510 |

ACME ANALYTICAL LABORATORIES
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158

DATE RECEIVED: SEPT 9 1987
DATE REPORT MAILED: *Sept 22/87*

ASSAY CERTIFICATE

- SAMPLE TYPE: Rock Chips

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

TECK EXPLORATIONS LTD. PROJECT-1354 File # 87-4007A

| SAMPLE# | CU % | AG OZ/T | AU* OZ/T |
|------------|---------|------------|-------------|
| CASTLE 1A | .11 | .17 | .139 |
| CASTLE 2A | .27 | .48 | .169 |
| CASTLE 3A | .03 | .01 | .023 |
| CASTLE 4A | .02 | .01 | .019 |
| CASTLE 5A | .03 | .02 | .009 |
| CASTLE 6A | .03 | .09 | .011 |
| CASTLE 7A | .07 | .05 | .007 |
| CASTLE 8A | .01 | .71 | .024 |
| CASTLE 9A | .01 | 4.05 | .931 |
| CASTLE 10A | .01 | .07 | .022 |
| CASTLE 11A | .01 | .03 | .014 |
| CASTLE 12A | .01 | 12.66 | 4.030 |

Plotted

ASSAY CERTIFICATE

- SAMPLE TYPE: ROCK

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

TECK EXPLORATIONS File # 87-3460 Page 1

| SAMPLE# | CU % | AG OZ/T | AU OZ/T |
|---------|---------|------------|------------------|
| 24914 | .03 | .06 | .001 |
| 24915 | .01 | .01 | .001 |
| 24916 | .01 | .08 | .032 |
| 24917 | .01 | .01 | .001 |
| 24918 | .01 | .01 | .001 |
| 24919 | .01 | .01 | .001 |
| 24920 | .01 | .06 | .001 |
| 24921 | .01 | .05 | .001 |
| 24922 | .01 | .02 | .001 |
| 24923 | .01 | .03 | .001 |
| 24924 | .01 | .02 | .001 |
| 24925 | .08 | .10 | 1.156 |
| 24926 | .01 | .01 | .001 |
| 24927 | .08 | .05 | .002 |
| 24928 | .01 | .01 | .001 |
| 24929 | .01 | .03 | .003 |
| 24930 | .04 | .04 | .062 |
| 24932 | .01 | .02 | .001 |
| 24933 | .02 | .03 | .001 |
| 24934 | .01 | .02 | .001 |
| 24935 | .01 | .06 | .004 |
| 24940 | .01 | .04 | .006 |
| 24941 | .01 | .03 | .002 |
| 24942 | .01 | .05 | .254 |
| 24943 | .01 | .03 | .020 |
| 24944 | .01 | .06 | .006 |
| 24945 | .01 | .06 | .006 |
| 24946 | .04 | .04 | .001 |
| 24947 | .07 | .05 | .009 |
| 24948 | .01 | .02 | .005 |
| 24949 | .03 | .06 | .001 |
| 24950 | .01 | .02 | .002 |
| 30551 | .01 | .01 | .001 |
| 30552 | .02 | .04 | .002 |
| 30553 | .04 | .01 | .002 |
| 30554 | .01 | .02 | .002 |

etter

| SAMPLE# | CU % | AG OZ/T | AU OZ/T |
|---------|---------|------------|------------|
| 30555 | .01 | .04 | .010 |
| 30556 | .01 | .02 | .004 |
| 30557 | .01 | .01 | .006 |
| 30558 | .03 | .02 | .002 |
| 30559 | .02 | .01 | .025 |
| 30560 | .01 | .01 | .006 |
| 30561 | .01 | .01 | .005 |
| 30562 | .02 | .01 | .004 |
| 30563 | .03 | .08 | .008 |
| 30564 | .01 | .04 | .006 |
| 30568 | .01 | .01 | .002 |
| 30571 | .01 | .01 | .001 |
| 30572 | .04 | .01 | .001 |
| 30573 | .04 | .04 | .003 |
| 30574 | .03 | .09 | .008 |
| 30575 | .02 | .07 | .005 |
| 30576 | .07 | .01 | .002 |
| 30577 | .12 | .01 | .002 |
| 30578 | .09 | .01 | .004 |
| 30579 | .01 | .01 | .002 |

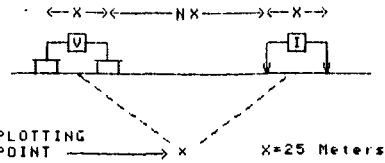
Fraser's technique for filtering induced polarization and resistivity data operates on a pyramid shaped set of readings which include one $n=1$ value, two $n=2$ values, three $n=3$ values, four $n=4$ values, etc. The average of the two $n=2$ readings is added to the average of the three $n=3$ readings, and the average of the four $n=4$ readings, etc. as well as to the single $n=1$ value. The sum of these numbers is then divided by the number of "n" levels used in order to arrive at the final filtered value, which is normally plotted in plan form.

TECK EXPLORATIONS

CASTLE PROPERTY

LIARD M. D. B. C.

LINE NO. -2050H



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
 PROBABLE
 POSSIBLE

FREQUENCY (HERTZ)
4.010.25

DWG. NO. -I P -5892-7

NOTE- CONTOURS
AT LOGARITHMIC
INTERVALS: 1,-1.5
-2,-3,-5,-7.5,-10
PLUS EACH 0.25
FROM 0.5 TO 2.0

DATE SURVEYED: AUG/87
APPROVED: _____
DATE: _____

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY

| TECK EXPLORATIONS CASTLE L2050W | | X=25M RHO (OHM-M) | | | | | | | | | | | | | | | | | | | |
|---------------------------------|------|-------------------|------|------|------|------|------|-----|-----|-----|-----|------|------|------|-----|------|----|----|----|-----|-----|
| DIPOLE NUMBER | | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | |
| COORDINATE | 375S | 325S | 275S | 225S | 175S | 125S | 75S | 25S | 25N | 75N | | | | | | | | | | 75N | |
| INTERPRETATION | | | | | | | | | | | | | | | | | | | | | |
| N=1 | 1265 | 1581 | 1504 | 1363 | 1003 | 1095 | 1791 | 813 | 468 | 586 | 626 | 1187 | 1501 | 1856 | 877 | 1131 | | | | | N=1 |
| N=2 | 1108 | 1759 | 1397 | 916 | 1109 | 985 | 1272 | 591 | 624 | 677 | 638 | 1167 | 1116 | 1093 | 792 | 644 | | | | | N=2 |
| N=3 | 1598 | 1520 | 1019 | 1074 | 1142 | 830 | 742 | 788 | 686 | 778 | 636 | 1059 | 774 | 952 | 518 | 778 | | | | | N=3 |
| N=4 | 1368 | 1139 | 1160 | 1037 | 1149 | 459 | 957 | 851 | 785 | 723 | 588 | 801 | 754 | 613 | 686 | 875 | | | | | N=4 |
| N=5 | | | | | | | | | | | | | | | | | | | | N=5 | |
| N=6 | | | | | | | | | | | | | | | | | | | | N=6 | |

| TECK EXPLORATIONS CASTLE L2050W | | X=25M PFE | | | | | | | | | | | | | | | | | | | |
|---------------------------------|------|-----------|------|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|----|----|-----|-----|
| DIPOLE NUMBER | | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | |
| COORDINATE | 375S | 325S | 275S | 225S | 175S | 125S | 75S | 25S | 25N | 75N | | | | | | | | | | 75N | |
| INTERPRETATION | | | | | | | | | | | | | | | | | | | | | |
| N=1 | 1.5 | 3.1 | 6.6 | 5.5 | 12 | 9.4 | 8.1 | 9.9 | 13 | 14 | 9.6 | 6.6 | 5.8 | 7.8 | 5.7 | 4.3 | | | | | N=1 |
| N=2 | 2.9 | 5.9 | 6.9 | 9.1 | 11 | 13 | 10 | 11 | 14 | 13 | 13 | 8.3 | 7.9 | 6.1 | 6.3 | 8.1 | | | | | N=2 |
| N=3 | 4.9 | 5.1 | 10 | 7.4 | 13 | 14 | 11 | 11 | 13 | 16 | 8.3 | 8.8 | 5 | 8.1 | 9.3 | 6.6 | | | | | N=3 |
| N=4 | 4.5 | 8.3 | 9.1 | 10 | 14 | 15 | 11 | 9.8 | 16 | 16 | 15 | 6.2 | 7.8 | 11 | 6.9 | 7.5 | | | | | N=4 |
| N=5 | | | | | | | | | | | | | | | | | | | | N=5 | |
| N=6 | | | | | | | | | | | | | | | | | | | | N=6 | |

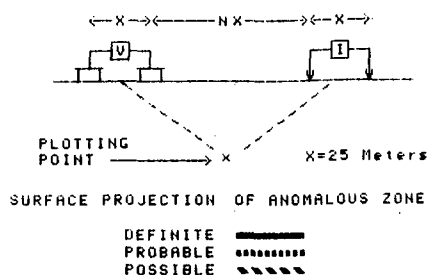
| TECK EXPLORATIONS CASTLE L2050W | | X=25M METAL FACTOR | | | | | | | | | | | | | | | | | | | |
|---------------------------------|------|--------------------|------|------|------|------|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|----|----|----|-----|-----|
| DIPOLE NUMBER | | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | |
| COORDINATE | 375S | 325S | 275S | 225S | 175S | 125S | 75S | 25S | 25N | 75N | | | | | | | | | | 75N | |
| INTERPRETATION | | | | | | | | | | | | | | | | | | | | | |
| N=1 | 1.2 | 2 | 4.4 | 4 | 12 | 8.6 | 4.5 | 12 | 28 | 24 | 15 | 5.6 | 3.9 | 4.2 | 6.5 | 3.8 | | | | | N=1 |
| N=2 | 2.6 | 3.4 | 4.9 | 9.9 | 10 | 13 | 7.9 | 18 | 23 | 19 | 20 | 7.1 | 7.1 | 5.6 | 8 | 13 | | | | | N=2 |
| N=3 | 3.1 | 3.4 | 9.8 | 6.9 | 11 | 16 | 15 | 14 | 19 | 20 | 13 | 8.3 | 6.5 | 8.5 | 18 | 8.5 | | | | | N=3 |
| N=4 | 3.3 | 7.3 | 7.8 | 9.6 | 12 | 34 | 12 | 12 | 22 | 22 | 25 | 7.7 | 10 | 10 | 10 | 9.6 | | | | | N=4 |
| N=5 | | | | | | | | | | | | | | | | | | | | N=5 | |
| N=6 | | | | | | | | | | | | | | | | | | | | N=6 | |

TECK EXPLORATIONS

CASTLE PROPERTY

LIARD M. D. J. B. C.

LINE NO. -1650W



FREQUENCY (HERTZ)
4.010.25

DWG. NO. -I.P.-5892-14

NOTE- CONTOURS
AT LOGARITHMIC
INTERVALS. 1, -1.5
-2, -3, -5, -7.5, -10
PLUS EACH 0.25
FROM 0.5 TO 2.0

DATE SURVEYED: AUG/87
APPROVED: _____
DATE: _____

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY

| TECK EXPLORATIONS CASTLE L1650W X=25M RHO (OHM-M) | | | | | | | | | | | |
|---|-----|------|-----|-----|------|-----|-----|-----|-----|-----|-----|
| DIPOLE NUMBER | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | | |
| COORDINATE | 75S | 25S | 25N | 75N | 125N | | | | | | |
| INTERPRETATION | | | | | | | | | | | |
| N=1 | 760 | 601 | 962 | 594 | 834 | 330 | 440 | 677 | 391 | N=1 | |
| N=2 | 654 | 1076 | 583 | 630 | 385 | 351 | 743 | 372 | N=2 | | |
| N=3 | 980 | 746 | 593 | 284 | 457 | 571 | 443 | N=3 | | | |
| N=4 | 689 | 739 | 269 | 347 | 718 | 361 | N=4 | | | | |
| N=5 | | | | | | | | | | | N=5 |
| N=6 | | | | | | | | | | | N=6 |

| TECK EXPLORATIONS CASTLE L1650W X=25M PFE | | | | | | | | | | | |
|---|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|
| DIPOLE NUMBER | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | | |
| COORDINATE | 75S | 25S | 25N | 75N | 125N | | | | | | |
| INTERPRETATION | | | | | | | | | | | |
| N=1 | 6.2 | 8.5 | 7.6 | 2.3 | 4.2 | 4.8 | 3.2 | 2.2 | 8 | N=1 | |
| N=2 | 6 | 4.3 | 7.7 | 4.4 | 3.9 | 5.1 | 3.4 | 1.6 | N=2 | | |
| N=3 | 3.7 | 6.4 | 9.3 | 4.6 | 3.2 | 4.9 | 3.1 | N=3 | | | |
| N=4 | 6.3 | 8.3 | 9.4 | 3.8 | 3.9 | 4.2 | N=4 | | | | |
| N=5 | | | | | | | | | | | N=5 |
| N=6 | | | | | | | | | | | N=6 |

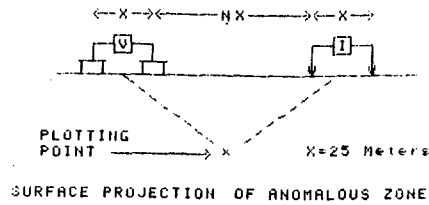
| TECK EXPLORATIONS CASTLE L1650W X=25M METAL FACTOR | | | | | | | | | | | |
|--|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|
| DIPOLE NUMBER | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | | |
| COORDINATE | 75S | 25S | 25N | 75N | 125N | | | | | | |
| INTERPRETATION | | | | | | | | | | | |
| N=1 | 8.2 | 14 | 7.9 | 3.9 | 5 | 15 | 7.3 | 3.2 | 2 | N=1 | |
| N=2 | 9.2 | 4 | 13 | 7 | 10 | 15 | 4.6 | 4.3 | N=2 | | |
| N=3 | 3.8 | 8.6 | 16 | 16 | 7 | 8.6 | 7 | N=3 | | | |
| N=4 | 9.1 | 11 | 35 | 11 | 5.4 | 12 | N=4 | | | | |
| N=5 | | | | | | | | | | | N=5 |
| N=6 | | | | | | | | | | | N=6 |

TECK EXPLORATIONS

CASTLE PROPERTY

LIARD M. D. / B. C.

LINE NO. -1200W



DEFINITE 
 PROBABLE 
 POSSIBLE 

FREQUENCY (HERTZ)
4.0; 0.25

DWG. NO. -I.P.-5892-23

NOTE- CONTOURS
AT LOGARITHMIC
INTERVALS. 1, -1.5
-2, -3, -5, -7.5, -10
PLUS EACH 0.25
FROM 0.5 TO 2.0

DATE SURVEYED: AUG/87

APPROVED: _____

DATE: _____

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY

| TECK EXPLORATIONS CASTLE L1200W X=25M RHO (OHM-M) | | | | | | | | | | | | | | | | |
|---|------|------|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|--|--|--|
| DIPOLE NUMBER | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | | | | |
| COORDINATE | 200S | 150S | 100S | 50S | 0 | 50N | 100N | | | | | | | | | |
| INTERPRETATION | | | | | | | | | | | | | | | | |
| N=1 | 3534 | 1498 | 678 | 688 | 340 | 388 | 562 | 440 | 568 | 829 | 1050 | 986 | N=1 | | | |
| N=2 | 2865 | 1200 | 842 | 789 | 356 | 267 | 722 | 573 | 423 | 642 | 792 | 971 | N=2 | | | |
| N=3 | 2258 | 1223 | 1115 | 1188 | 409 | 246 | 448 | 660 | 562 | 456 | 829 | 848 | N=3 | | | |
| N=4 | 2667 | 1235 | 1278 | 1500 | 665 | 264 | 357 | 401 | 601 | 595 | 610 | 920 | N=4 | | | |
| N=5 | | | | | | | | | | | | N=5 | | | | |
| N=6 | | | | | | | | | | | | N=6 | | | | |

| TECK EXPLORATIONS CASTLE L1200W X=25M PFE | | | | | | | | | | | | | | | | |
|---|------|------|------|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|--|--|--|
| DIPOLE NUMBER | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | | | | |
| COORDINATE | 200S | 150S | 100S | 50S | 0 | 50N | 100N | | | | | | | | | |
| INTERPRETATION | | | | | | | | | | | | | | | | |
| N=1 | 1 | 3 | 7.1 | 8.9 | 8.3 | 6.4 | 6.3 | 4 | 4.6 | 4.4 | 2 | 1.7 | N=1 | | | |
| N=2 | 1.3 | 4.4 | 7.4 | 7.9 | 8.7 | 8.6 | 8.1 | 5.8 | 5 | 5 | 2.9 | 2.3 | N=2 | | | |
| N=3 | 1.7 | 4.9 | 6.9 | 7 | 8.7 | 9.6 | 9.2 | 7.3 | 7.1 | 5.5 | 3.1 | 2.8 | N=3 | | | |
| N=4 | 2.3 | 5.3 | 6.8 | 6.6 | 8.3 | 9.6 | 10 | 8.3 | 9.1 | 7.3 | 3.7 | 3 | N=4 | | | |
| N=5 | | | | | | | | | | | | N=5 | | | | |
| N=6 | | | | | | | | | | | | N=6 | | | | |

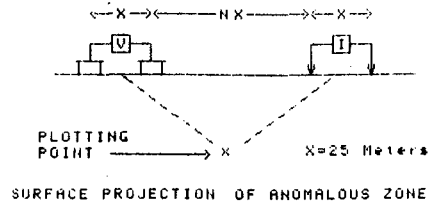
| TECK EXPLORATIONS CASTLE L1200W X=25M METAL FACTOR | | | | | | | | | | | | | | | | |
|--|------|------|------|-----|----|-----|------|-----|-----|-----|-----|-----|-----|--|--|--|
| DIPOLE NUMBER | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | | | | |
| COORDINATE | 200S | 150S | 100S | 50S | 0 | 50N | 100N | | | | | | | | | |
| INTERPRETATION | | | | | | | | | | | | | | | | |
| N=1 | .3 | 2 | 11 | 15 | 24 | 16 | 11 | 9.1 | 8.1 | 5.3 | 1.9 | 1.7 | N=1 | | | |
| N=2 | .5 | 3.7 | 8.8 | 11 | 24 | 32 | 11 | 10 | 12 | 7.8 | 3.7 | 2.4 | N=2 | | | |
| N=3 | .8 | 4 | 6.2 | 5.9 | 21 | 39 | 21 | 11 | 13 | 12 | 3.7 | 3.3 | N=3 | | | |
| N=4 | .9 | 4.3 | 5.3 | 4.4 | 12 | 36 | 28 | 21 | 15 | 12 | 6.1 | 3.3 | N=4 | | | |
| N=5 | | | | | | | | | | | | N=5 | | | | |
| N=6 | | | | | | | | | | | | N=6 | | | | |




TECK EXPLORATIONS

CASTLE PROPERTY

LIARD N. D. B. C.

LINE NO. -1000N



DEFINITE 
 PROBABLE 
 POSSIBLE 

FREQUENCY (HERTZ)
4.0; 0.25

DWG. NO. -I.P. -5892-27

NOTE- CONTOURS
AT LOGARITHMIC
INTERVALS 1.-1.5
-2.-3.-5.-7.5.-10
PLUS EACH 0.25
FROM 0.5 TO 2.0

DATE SURVEYED-AUG/87
APPROVED _____
DATE _____

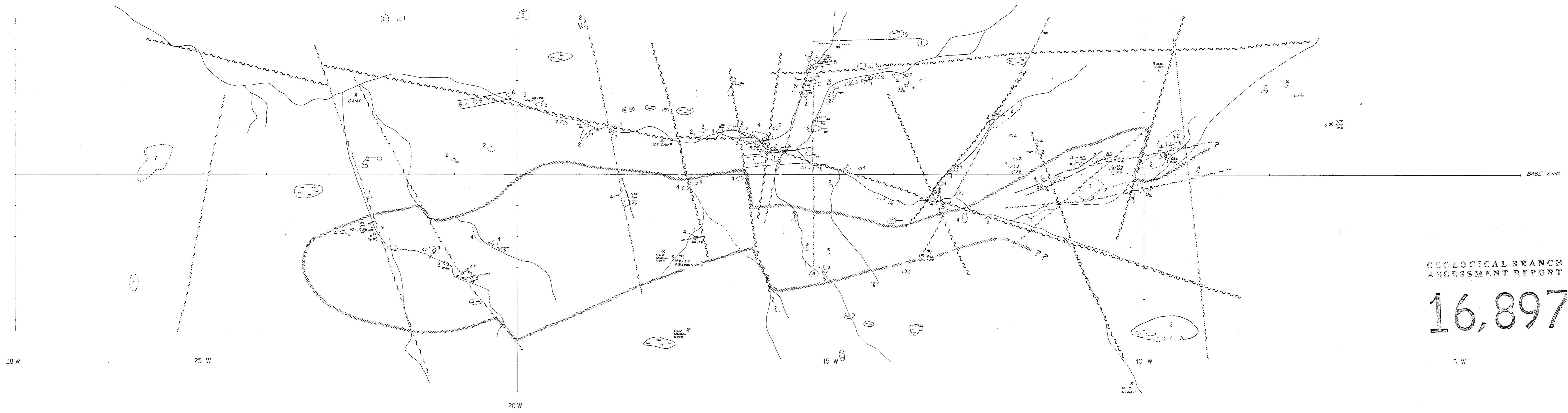
PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY

| TECK EXPLORATIONS CASTLE L1000N X=25M RHO (OHM-M) | | | | | | | | | | |
|---|------|------|------|------|-----|-----|------|-----|-----|--|
| DIPOLE NUMBER | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| COORDINATE | 125S | 75S | 25S | 25N | 75N | | | | | |
| INTERPRETATION | | | | | | | | | | |
| N=1 | 254 | 2663 | 605 | 650 | 382 | 809 | 1216 | 861 | N=1 | |
| N=2 | | 585 | 1324 | 721 | 360 | 473 | 910 | 676 | N=2 | |
| N=3 | | | 775 | 1485 | 358 | 407 | 589 | 301 | N=3 | |
| N=4 | | | | 959 | 712 | 372 | 497 | 572 | N=4 | |
| N=5 | | | | | | | | | N=5 | |
| N=6 | | | | | | | | | N=6 | |

| TECK EXPLORATIONS CASTLE L1000N X=25M PFE | | | | | | | | | | |
|---|------|-----|-----|-----|-----|-----|-----|-----|-----|--|
| DIPOLE NUMBER | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| COORDINATE | 125S | 75S | 25S | 25N | 75N | | | | | |
| INTERPRETATION | | | | | | | | | | |
| N=1 | 7.8 | 7.8 | 4.7 | 6.4 | 4.1 | 2.6 | 2.8 | 2.9 | N=1 | |
| N=2 | | 7.8 | 5.3 | 4.3 | 4.5 | 4.5 | 3.3 | 2.1 | N=2 | |
| N=3 | | | 6.7 | 4.9 | 4.3 | 5.5 | 5.1 | 3.5 | N=3 | |
| N=4 | | | | 6.6 | 4.5 | 5.6 | 5.7 | 4.5 | N=4 | |
| N=5 | | | | | | | | | N=5 | |
| N=6 | | | | | | | | | N=6 | |

| TECK EXPLORATIONS CASTLE L1000N X=25M METAL FACTOR | | | | | | | | | | |
|--|------|-----|-----|-----|-----|-----|-----|-----|-----|--|
| DIPOLE NUMBER | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | |
| COORDINATE | 125S | 75S | 25S | 25N | 75N | | | | | |
| INTERPRETATION | | | | | | | | | | |
| N=1 | 31 | 2.9 | 7.8 | 9.9 | 11 | 3.2 | 2.3 | 3.4 | N=1 | |
| N=2 | | 13 | 4 | 6 | 13 | 9.5 | 3.6 | 3.1 | N=2 | |
| N=3 | | | 8.6 | 3.3 | 12 | 14 | 8.7 | 4.4 | N=3 | |
| N=4 | | | | 6.9 | 6.3 | 15 | 11 | 7.9 | N=4 | |
| N=5 | | | | | | | | | N=5 | |
| N=6 | | | | | | | | | N=6 | |



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,897

5 W

LEGEND

- | | |
|--|---|
| <ul style="list-style-type: none"> 1 MEDIUM GRAINED, GREY-GREEN VOLCANICS 2 COARSE GRAINED GREEN VOLCANICS (PORPHYRY) 3 MED. ALTERED (PROPYLITIC) MED. TO COARSE GRAINED VOLC. PYRITIC 4 HIGHLY ALTERED (PHYLIC) GREEN VOLCANICS. SERICITE, PYRITE. 5 PURPLE PYROCLASTICS 6 LIGHT BROWN VOLCANIC DYKE 7 FELSITE | <ul style="list-style-type: none"> ZONE OF CONSISTENT PY ALTERATION (INTERPRETED) --- VEINS (SER, QZ, BAR, PY) — LITHOLOGIC CONTACT ~ ~ ~ POSSIBLE FAULT ~ ~ ~ PROBABLE FAULT x (f) FLOAT |
|--|---|

| | |
|--------------------------------------|-------------------------------|
| TECK EXPLORATIONS LIMITED | |
| CASTLE GOLD | |
| GEOLOGY | |
| | |
| COMPILED: T. DEY DRAWN: WE DATE: | SCALE: 1:2500 NTS: FIG. 5 |

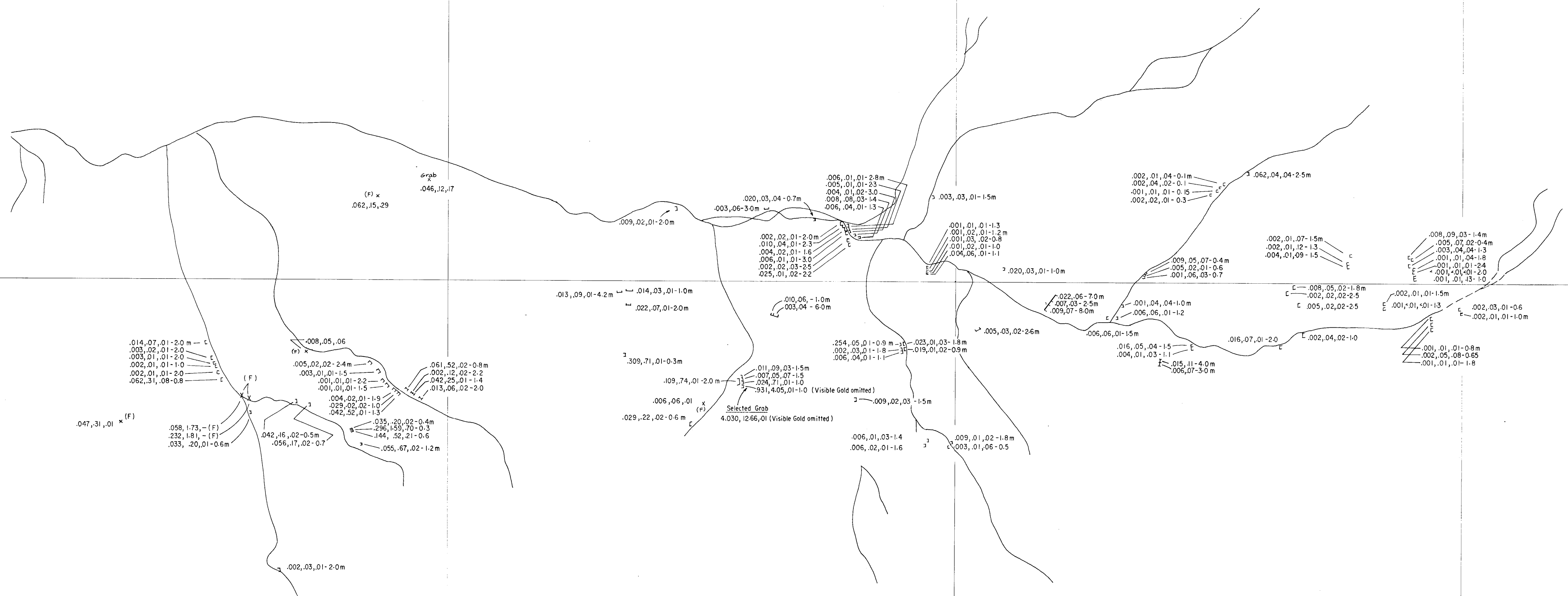
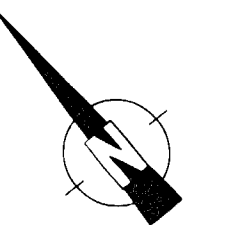
25 W

20 W

15 W

10 W

5 W



(resample) .139,17,11-0.6m
1.156,10,08-0.4m

(F)
x
.169,48,27

BASE LINE

GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,897

ASSAY RESULTS

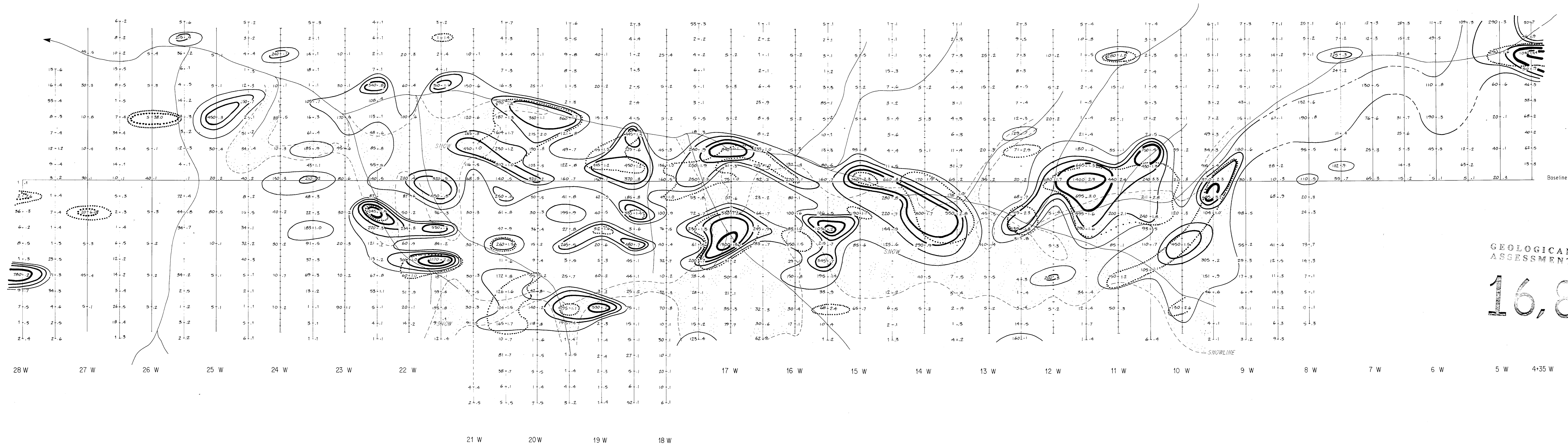
| Au-oz/t | Ag-oz/t | Cu-% | Length in metres |
|---------|---------|------|------------------|
| .041 | .22 | .02 | 0.6 m |

TECK EXPLORATIONS LIMITED
CASTLE GOLD

SURFACE SAMPLES



Compiled: Drawn: wE Date: Sept. '87 Scale: 1:2500 FIG. 6



GEOLOGICAL BRANCH
ASSESSMENT REPORT

16,897

LEGEND

Au (ppb) 5-1
27-1 Ag (ppm)

CONTOURS

Au - ppb Ag - ppm
 10010.....
 2005.0.....
 300
 500
 >1000

TECK EXPLORATIONS LIMITED
CASTLE GOLD

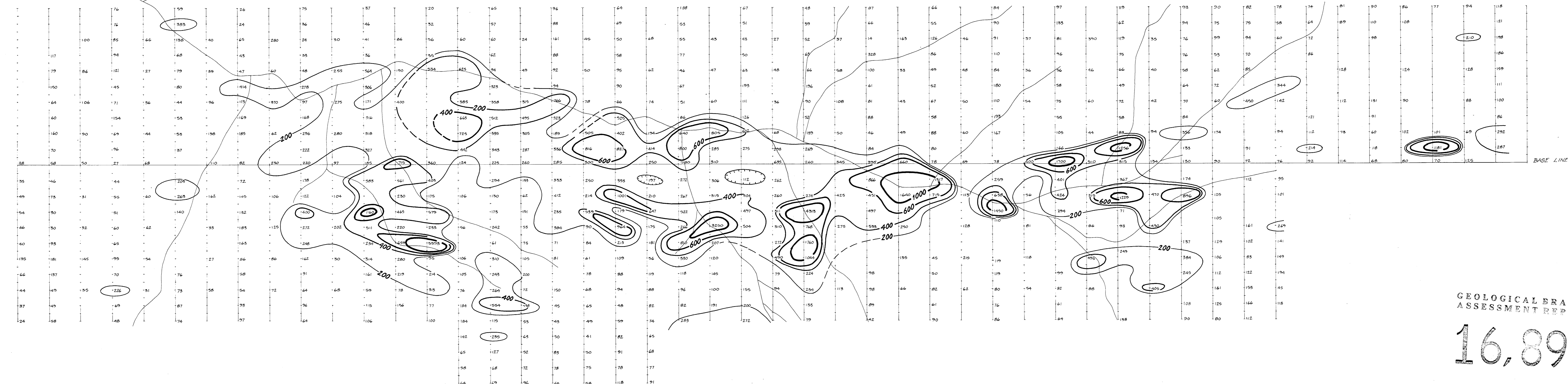
SOIL GEOCHEMISTRY
Au (ppb) - Ag (ppm)

50 0 50 100 200
METRES

COMPILED: DRAWN: WE DATE: SCALE: 1:2500 NTS: FIG. 7



28 W 26 W 24 W 22 W 20 W 18 W 16 W 14 W 12 W 10 W 8 W 6 W 4 W



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LEGEND

200 Cu (ppm)
272

CONTOURS
Cu - ppm

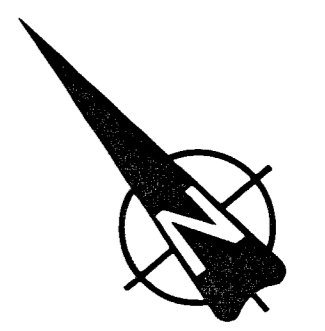
- 200 —
- 400 —
- 600 —
- >1000 —

TECK EXPLORATIONS LIMITED
CASTLE PROJECT

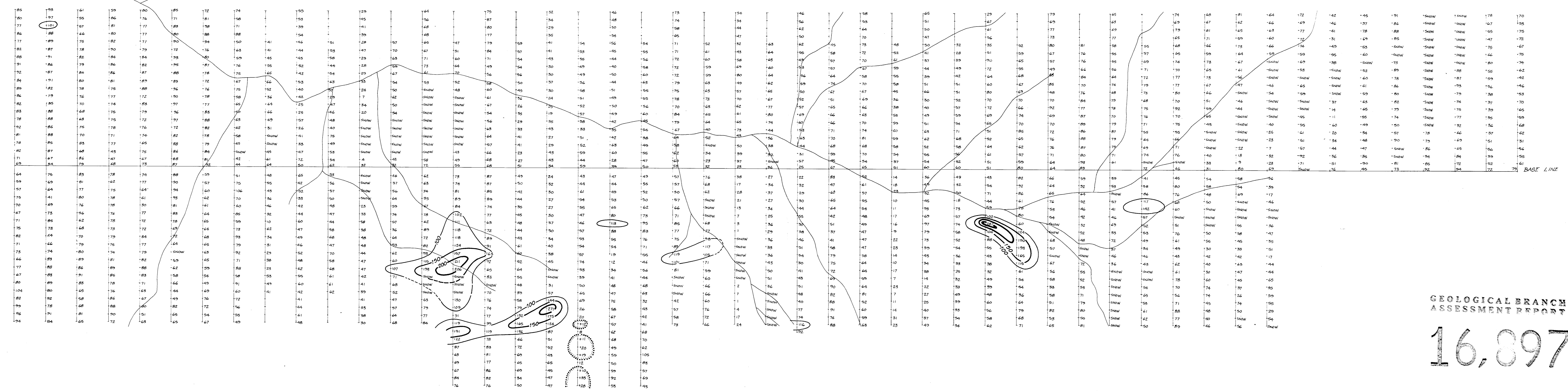
SOIL GEOCHEMISTRY
(Cu - ppm)

50 0 50 100 200
METRES

COMPILED: _____ DRAWN: _____ DATE: _____ SCALE: 1:2500 MTS: _____ FIG. 8



28 W 26 W 24 W 22 W 20 W 18 W 16 W 14 W 12 W 10 W 8 W 6 W 4 W



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| CONTOURS | POSTINGS |
|--|-------------------|
| — 100 — | 22 |
| — 150 — | 27 |
| — 200 — | 25 (MILLI VOLTS) |
| — 250 — | 40 |
| ***** POSITIVE VALUES | 37 |
| | 49 |
| ALL VALUES ARE NEGATIVE | |
| * USEFUL MEASUREMENTS NOT OBTAINED IN AREAS COVERED BY OLD SNOW. | OPERATORS: |
| * POSITIVE VALUES DOUBLE CHECKED | D. NIKIRK |
| | R. NIKIRK |
| | T. DEY |

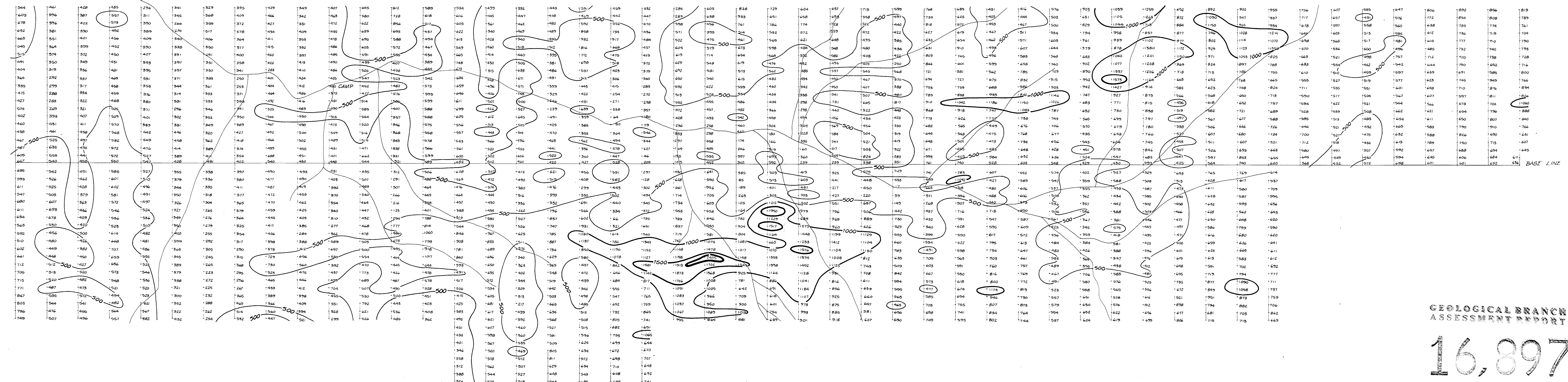
TECK EXPLORATIONS LIMITED
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SELF - POTENTIAL SURVEY

COMPILED: _____ DRAWN: # _____ DATE: _____ SCALE: 1:2500 NTS: _____ FIG. 9



28 W 26 W 24 W 22 W 20 W 18 W 16 W 14 W 12 W 10 W 8 W 6 W 4 W



GEOLOGICAL BRANCH
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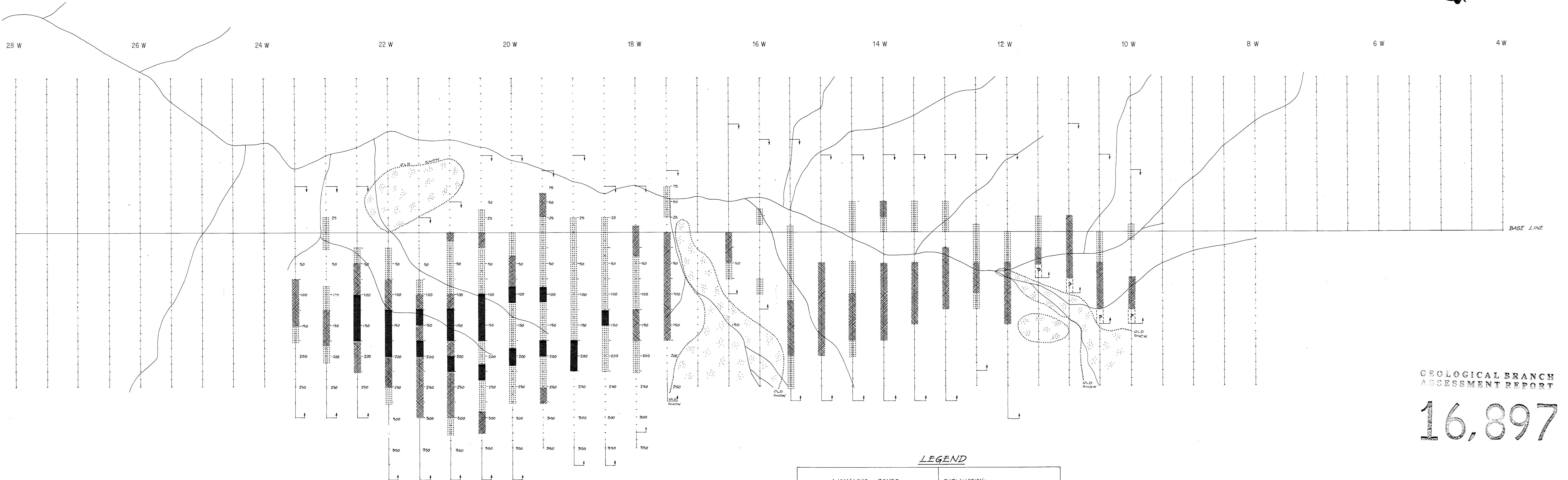
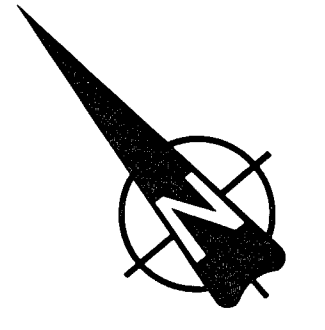
| CONTOURS | POSTINGS |
|---|----------------------|
| — 500 — | 611 |
| — 1000 — | 659 (GAMMAS) |
| — 1500 — | 647 |
| — 2000 — | 581 |
| (GAMMAS) | 607 |
| | DATUM: 57,500 GAMMAS |
| INSTRUMENT: | OPERATOR: |
| E.G.G. GEOMETRICS PORTABLE PROTON MAGNETOMETER, MODEL G816/826A SERIAL N ^o 6663 | D. NIKIRK |
| (TOTAL FIELD) | |

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MAGNETOMETER SURVEY

50 0 50 100 200
METRES

COMPILED: DRAWN: # DATE: SCALE: 1:2500 NTS: FIG. 10



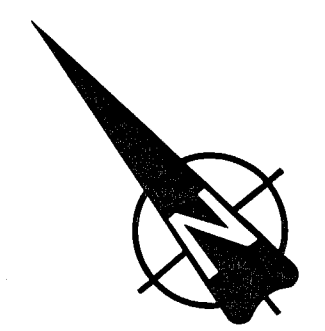
GEOLOGICAL BRANCH
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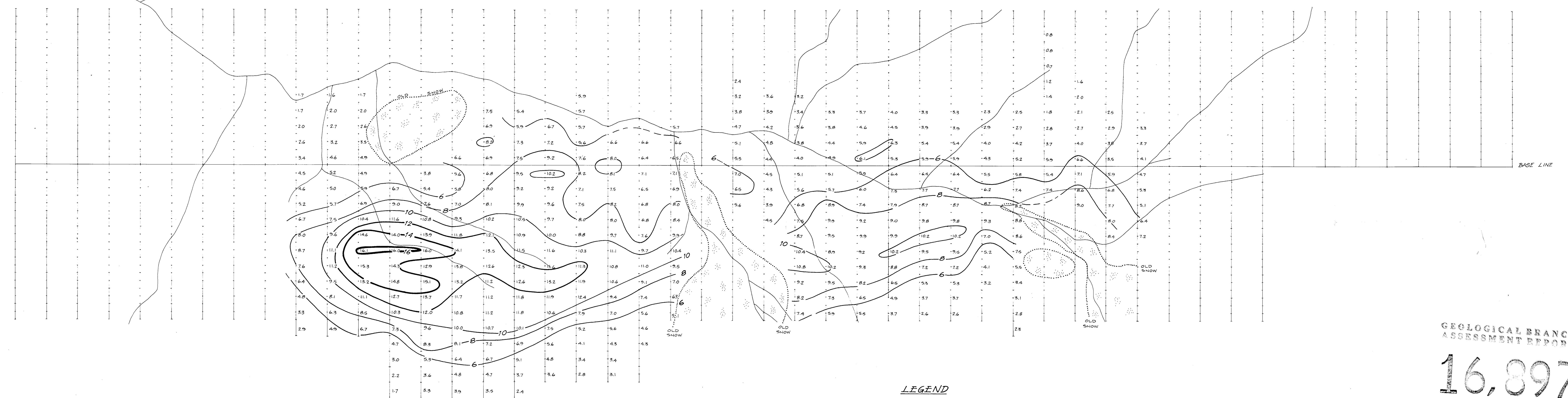
LEGEND

| <u>ANOMALOUS ZONES</u> | | <u>EXPLANATION:</u> |
|------------------------|-------------------|---|
| | DEFINITE | USEFUL DATA NOT OBTAINED IN AREAS COVERED BY OLD SNOW |
| | PROBABLE | |
| | POSSIBLE | LINE 17 W NOT SURVEYED DUE TO LOCATIONS OF OLD SNOW. |
| | SURVEY BOUNDARIES | |
| | | <u>OPERATORS:</u> |
| | | MIKE CORMIER DOUG NIKIRK RAY NIKIRK |
| | | <u>CONDUCTED BY:</u> |
| | | PACIFIC GEOPHYSICAL LTD. AUG. 1987 |

| | | | |
|---------------------------|-----------|-------|----------------------------|
| TECK EXPLORATIONS LIMITED | | | |
| CASTLE GOLD | | | |
| <i>I.P. SURVEY</i> | | | |
| | | | |
| COMPILED: | DRAWN: MR | DATE: | SCALE: 1:2500 NTS: FIG. 11 |



28 W 26 W 24 W 22 W 20 W 18 W 16 W 14 W 12 W 10 W 8 W 6 W 4 W



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LEGEND

| | |
|---|---|
| <p><u>POSTINGS</u></p> <p>8.8 6.5 4.9 3.7</p> <p>FRASER FILTER PFE VALUES</p> | <p><u>CONTOURS</u></p> <p>6 8 10 12 14 16</p> |
| <p><u>EXPLANATION:</u></p> <p>USEFUL DATA NOT OBTAINED IN AREAS COVERED BY OLD SNOW</p> <p>L 17 W NOT SURVEYED DUE TO LOCATIONS OF OLD SNOW</p> | <p><u>OPERATORS:</u></p> <p>MIKE CORMIER DOUG NIKIRK RAY NIKIRK</p> <p><u>CONDUCTED BY:</u></p> <p>PACIFIC GEOPHYSICAL LTD. AUG. 1987</p> |

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I.P. SURVEY



