### ARIS SUMMARY SHEET

$\mathbf{O}$	
District Geologist, Prince George Off Confidential: 89.02.19	
ASSESSMENT REPORT 16961 MINING DIVISION: Cariboo	
PROPERTY: Forks LOCATION: LAT 52 22 54 LONG 120 43 18 UTM 10 5805714 655070 NTS 093A07E 093A07W CLAIM(S): Forks 1-4,AR 1-2,Tep 1-3 OPERATOR(S): Armada Gold and Min. AUTHOR(S): Howard, D.A. REPORT YEAR: 1988, 63 Pages COMMODITIES SEARCHED FOR: Gold GEOLOGICAL	
SUMMARY: The property is underlain by a complex suite of black phyllites, tuffs and sediments that have been assigned Middle-Late Triassic age. Structurally, the property covers a segment of the northeast limb of the Eureka Syncline. Gold mineralization (fine gold) is associated with stratabound quartz beds or veins that occur in a distinctive porphyroblastic unit within the black phyllite package.	
WORK DONE: Geological,Geochemical GEOL 4275.0 ha Map(s) - 1; Scale(s) - 1:10 000 LINE 33.7 km ROCK 2 sample(s) ;AU SILT 33 sample(s) ;ME SOIL 935 sample(s) ;ME	



## D.D.H. GEOMANAGEMENT LTD.

LOG NO:	0223	R	D.	
ACTION:				
FILE NO:	and a start of the			

### GEOLOGICAL AND GEOCHEMICAL

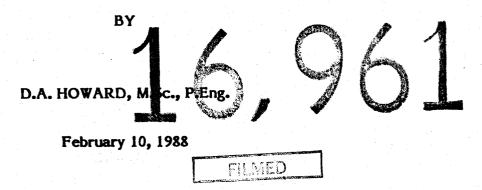
### REPORT

#### ON THE

FORKS 1 - 4, AR 1 - 2, TEP 1 - 3 CLAIMS

Cariboo Mining Division MacKay River Area, British Columbia 52° 23' North / 120° 44' West NTS 93A/7

> GEOLOGICAL BRANCH ASSESSMENT REPORT



422 - 470 Granville Street, Vancouver, B.C. Canada V6C 1V5 • Telephone (604) 681-4413

# TABLE OF CONTENTS

0

 $\bigcirc$ 

O

	· · · · ·
Summary	1
Introduction	2
Location and Access	2
Property and Title	5
History	5
Regional Geological Setting	8
Property Geology	17
(1) General	17
(2) Geological Setting	17
(3) Mineralization	21
Geochemical Survey	22
(1) Geochemical Silt/Soil Survey Results	24
Conclusions	25
Personnel Time Distribution	26
Cost Statement	26
Certification	28
References	29
Appendix A	

Page

V

### LIST OF FIGURES

Figure 1	Regional Location Map	3
Figure 2	Mineral Claim Location Map	4
Figure 3	Claim Map	6
Figure 4	Tectonic Elements of the Cordillera	9
Figure 5	Regional Geology	10
Figure 6	Map Showing Location of Property Relative to the Quesnel/Slide Mountain Terranes	12
Figure 7	Geology of the Quesnel Trough Showing the Relativ Location of Gold Occurrences to the Stratabound Gold Project Area	re 13
Figure 8a	Relative Position in Stratigraphic Column	15
Figure 8b	Position Relative to the East Limb of the Eureka Syncline	15
Figure 9	Generalized Geology of Eureka Peak Area Showing the East Limb Continuity Between Frasergold Creek and Horsefly Lake	16
Figure 10	Geology and Geochemical Map	in pocket
Figure 11	Soil Geochemical Map - Gold	in pocket

### LIST OF TABLES

Table 1A Comparison Between Stream Silt Samples Analyzed<br/>for Gold using -80 mesh and Pulverized -20 mesh<br/>Material

24

### SUMMARY

The Forks 1-4, AR 1-2 and TEP 1-3 mineral claims, held under option by Armada Gold and Minerals Ltd., are located approximately 110 kilometres east of Williams Lake in central British Columbia. The centre of the claim group is situated at the confluence of the North Fork of the Horsefly River and the MacKay River. Coordinates are 52° 23' North, 120° 44' West, N.T.S. 93A/7.

- 1 -

The 171 unit claim block is underlain by a complex suite of black phyllites, tuffs and sediments that have been assigned to the Middle to Late Triassic Quesnel River Group. A distinctive porphyroblastic black phyllite unit, shown to contain a gold bearing horizon, has been mapped across the property. This same porphyroblastic unit is the host rock to the defined gold deposit on the adjoining Eureka Resources, Inc. / Southlands Mining Corp. property. A narrow (25 cm) channel sample collected from the north end of the property in what appears to be in the same stratigraphic position as the Eureka / Southlands deposit assayed 0.065 ounces gold per ton.

During the period 29 July to 24 September 1987, the property was geological mapped, 33.745 kilometers of line and baseline were hand-cut and/or flagged on two grids and soil sampled on 25 or 50 metre spacing. A total of 935 soil samples and 33 silt samples were collected and analyzed by Acme Analytical Laboratories Ltd. of Vancouver, B.C. (30 element I.C.P. plus A.A. gold).

The geochemical survey (Grid 1) defined three discontinuous anomalous zones that warrant trenching and/or diamond drilling to determine their significance.

#### INTRODUCTION

The firm of D.D.H. Geomanagement Ltd. was commissioned in July, 1987 by Mr. A.F. Loo on behalf of Armada Gold and Minerals Ltd. to map the geology and conduct a soil/silt geochemical survey over the Forks 1-4, AR 1-2 and TEP 1-3 mineral claims. The field work upon which this report is based was conducted during the period 29 July to 24 September, 1987 inclusive by the author, Mr. C.E. Gunn and personnel provided by Durfeld Geological of Williams Lake, B.C.

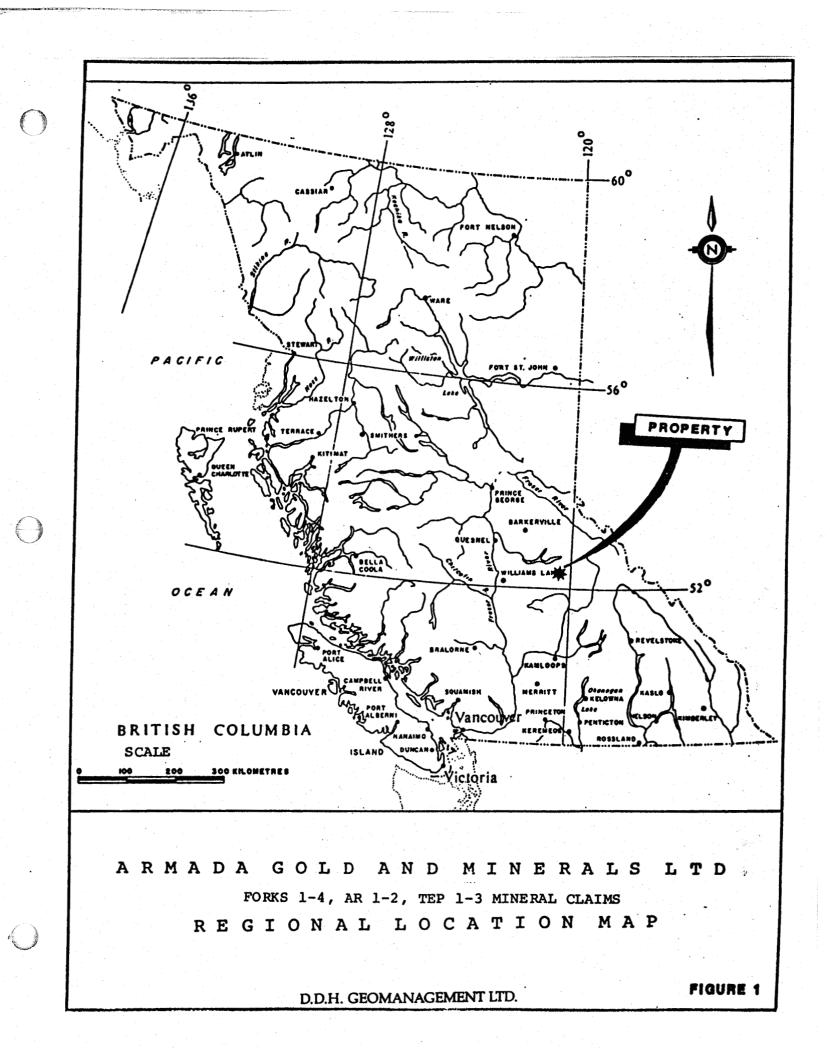
#### LOCATION AND ACCESS

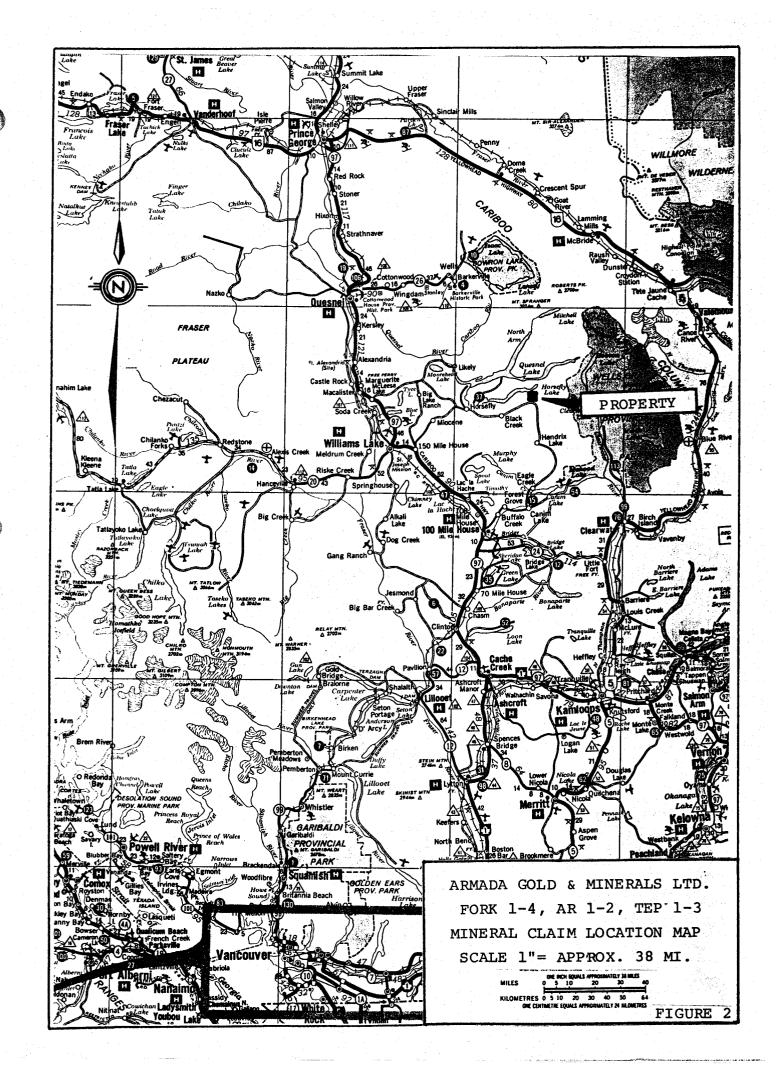
The Forks 1-4, AR 1-2 and TEP 1-3 mineral claims are centred at the confluence of the MacKay River with the north fork of the Horsefly River approximately 110 kilometres east of Williams Lake in Central British Columbia. Coordinates of the confluence of the two rivers is 52° 23' North Latitude and 120° 44' West Longitude. N.T.S. area is 93A/7 (see Figures 1 and 2).

Access to the property is via paved and gravel road, namely 104 kms from 100 Mile House, B.C. or about 90 kms due east of Williams Lake, B.C. Distance along Highway 97 from Vancouver, B.C. to Williams Lake, B.C. is 334 kms. There is scheduled air service between Vancouver and Williams Lake, B.C. Within the project area, logging roads allow two-wheel drive access to most parts of the claim group.

The claims lie along MacKay Creek (elevation 3,400 ft. at a.s.l. - 1,030 m) through Archie Pass (elevation 3,600 ft. a.s.l. - 1,091 m) to Horsefly Lake (elevation 2,580 ft. a.s.l. - 784 m). Local relief is abrupt with Eureka Peak having an elevation of 8,012 feet (2,428 m).

Most of the property has been logged but those areas not yet logged are covered with fir, spruce balsam and thick underbrush.





### **PROPERTY AND TITLE**

The Forks 1-4, AR 1-2 and TEP 1-3 mineral claims are held under option agreement between Armada Gold and Minerals Ltd. and Messers. C.E. Gunn, D.A. Howard and A.D. Drummond.

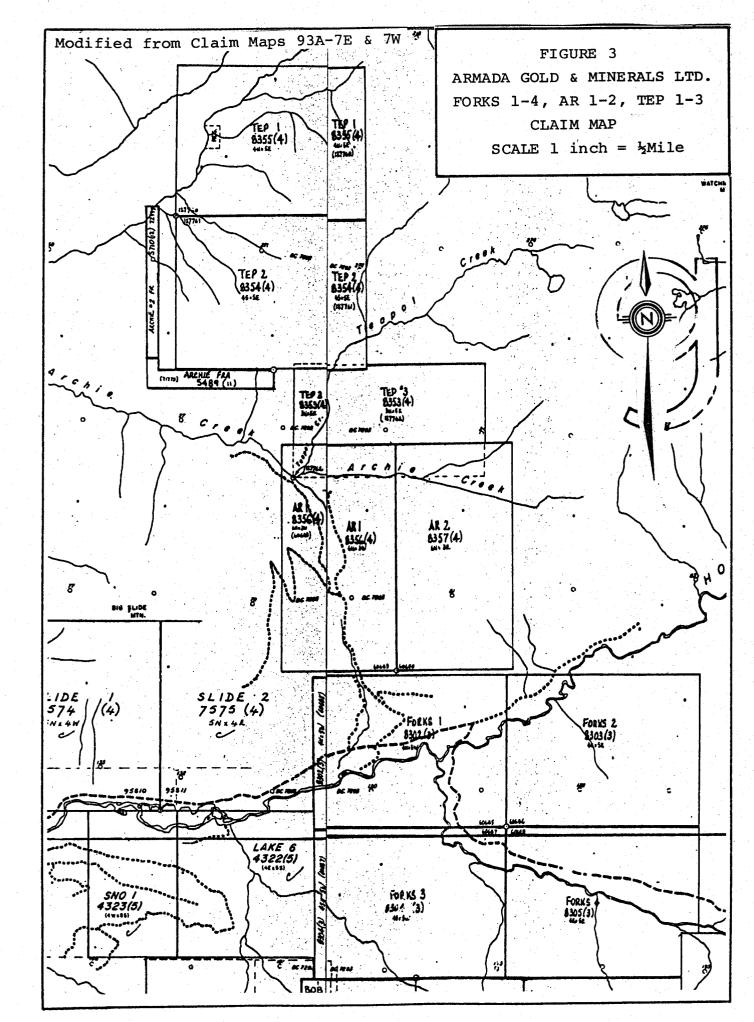
The property is comprised of seven (7) mineral claims containing 171 claim units as follows (see Figure 3).

Claim	No. of Units	Record No.	Date Recorded	Registered* Owner
FORK 1	20	8302	March 19, 1987	D.A. Howard
FORK 2	20	8303	March 19, 1987	D.A. Howard
FORK 3	20	8304	March 19, 1987	D.A. Howard
FORK 4	20	8305	March 19, 1987	D.A. Howard
AR 1	18	8356	April 16, 1987	D.A. Howard
AR 2	18	8357	April 16, 1987	D.A. Howard
TEP 1	20	8355	April 16, 1987	C.E. Gunn
TEP 2	20	8354	April 16, 1987	C.E. Gunn
TEP 3	15	8353	April 16, 1987	C.E. Gunn

\* A bill of sale for 50 percent of the property is held in trust in favour of Armada Gold and Minerals Ltd. subject to completion of the terms as set out in the option agreement.

#### HISTORY

Early work in the MacKay River Valley area dates from 1901 when prospectors panned the creeks for gold. Small operations evaluating the pyrite bearing quartz veins and the gravels on Fraser and Eureka Creek were started in 1902 but discontinued in 1903. Later work in the early 1930's reported placer gold at and below the Forks of the Horsefly River and in the MacKay River - Horsefly River area.



 $\bigcirc$ 

(

.

C

Exploration for copper mineralization in this vicinity was conducted from the mid-1960's to mid - 1970's by such companies as Amax, Union Miniere, Rio Tinto and Helicon Explorations.

The Alpha and Kay claims were staked by C.E. Gunn in 1978 and 1979 on the north side of upper MacKay River valley and on Frasergold Creek. In the fall of 1979 these claims were optioned to Keron Holdings Ltd. who acquired additional claims, conducted soil and rock chip sampling and geological surveys up to 1982 when the claims were transferred to Eureka Resources, Inc. Amoco Canada Petroleum Co. Ltd. optioned the property from Eureka in 1983. Work by Amoco consisted of 2,874.7 meters of NQ diamond drilling (9 holes), grid preparation, soil sampling, magnetometer and electromagnetic surveys. The results of this work to 1984 indicated potential for 3 types of economic deposit: 1) small high-grade types of deposit over widths of 1.5 meters grading 0.2 to 1.50 oz/t gold; 2) medium sized reserves over widths of 3-10 meters grading 0.07 to 0.20 oz/t gold; and 3) large volumes of reserves over widths of 6 - 20 meters grading 0.02 to 0.07 oz/t gold (Eureka Resources, Inc., Annual Report, 1984). Eureka indicated that 1.6 kilometers of strike length of the anomalous zone had been drill tested; the length of the zone is in excess of 4 kilometers. In April, 1985 Eureka Resources, Inc. negotiated an agreement with Amoco Canada to assume total equity interest in the Frasergold property (GCNL, April 10, 1985). On March 30, 1987 Southlands Mining Corporation of Vancouver entered into a joint venture agreement with Eureka Resources, Inc. to earn a 50% working interest in the property by funding a minimum of \$3 million in development of the property. Their news release (Stockwatch, March 30, 1987) noted that:

"Frasergold is an extensive gold project located 100 km east of Williams Lake in central British Columbia. Totalling 27 claims or approximately 8,000 acres, the property features an extensive favourable gold bearing strata, indicated by geochemistry over a strike length of 12 km, and identified in bedrock by drilling over a strike length of 4 km.

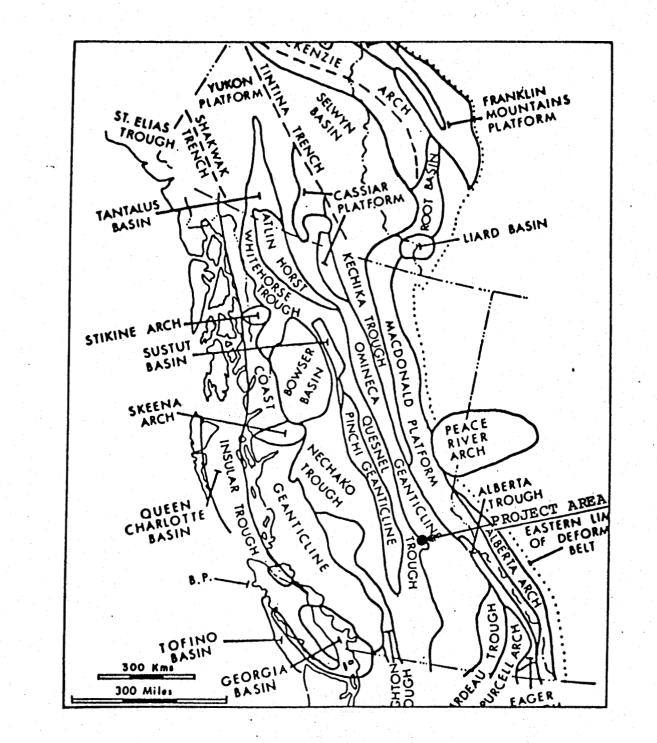
Intensive drilling completed in 1983, 1984 and 1986 over a strike length of 1.5 km has identified the potential of large tonnage open pit reserves of 20 million tons grading 0.06 ounces gold per ton. Also identified is the potential of higher grade underground reserves ranging 1.2 million tons grading 0.40 ounces of gold per ton. Approximately \$1.5 million has been spent on the project to date." The Armada claims adjoin the Eureka/Southland property on the northward onstrike extension of this favourable gold bearing strata. Prior to acquisition by Armada, exploration on this ground was in part conducted by Ripple Resources Ltd. (on Forks 3, 4). The work included soil sampling and one BQ drill hole on the north limb of the Eureka Syncline. The hole was drilled on a low order gold soil anomaly and encountered pyrite, pyrrhotite and chalcopyrite in andesitic tuff (Belik, 1983). In 1982, Dennison Mines Ltd. held the ground presently covered by the area of the L.C.P. of Forks 1, 2, 3 and 4. They completed a geochemical soil survey for copper lead, zinc and silver but not for gold.

On the immediate southeast of Forks 4, the former LL No. 1 claim of Valhalla Minerals Inc. (now Mac 10 of Eureka Resources, Inc.) was the site of a geochemical soil survey which showed spot gold highs adjacent to the project area (Dawson, 1984).

### **REGIONAL GEOLOGICAL SETTING**

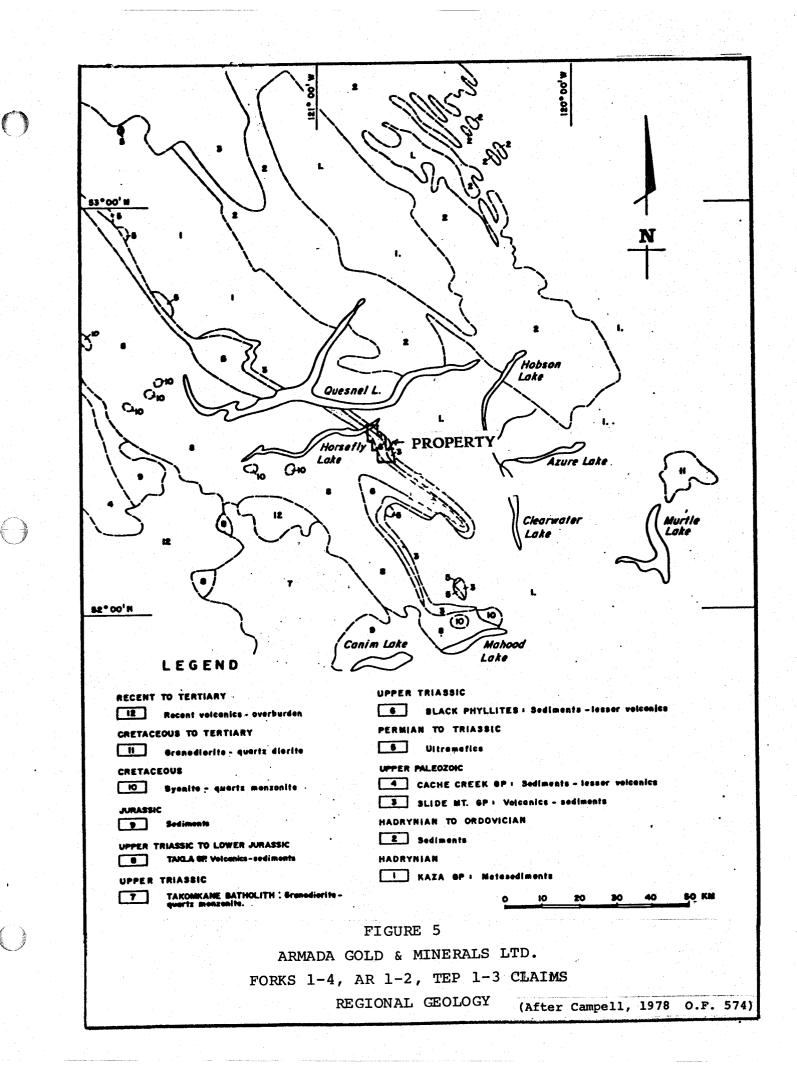
Wheeler et. al. (1972) and others have proposed district groupings of tectonic elements for the Canadian Cordillera. These are outlined in Figure 4. The project area lies along the eastern margin of the Quesnel Trough adjacent to the more easterly Omineca Crystalline Belt (Omineca Geanticline).

Geological compilation of the Quesnel Lake 93A Map Sheet was done by Campbell (1978) and summarized in Figure 5. Highly deformed amphibolite facies rocks of the Kaza Group (Unit 1 in Figure 5) lie to the east of the Pennsylvanian and/or Permian rocks of the Slide Mountain Group (Unit 3). These units form part of the Omineca Crystalline Belt in the project area. To the west lies the Quesnel Trough which at its base has an Upper Triassic phyllitic unit (Unit 6) overlain by Upper Triassic greenstone, augite porphyry breccia, tuff breccia with possible dykes and sills (Unit 8). These latter units are considered to be part of the Takla Group. Intrusive activity has been dated from Upper Triassic (Unit 7) to Cretaceous (Unit 10) to Tertiary (Unit 11).



#### FIGURE 4

ARMADA GOLD & MINERALS LTD. FORKS 1-4, AR 1-2. TEP 1-3 MINERAL CLAIMS TECTONIC ELEMENTS OF THE CORDILLERA (After Wheeler et al., 1972)



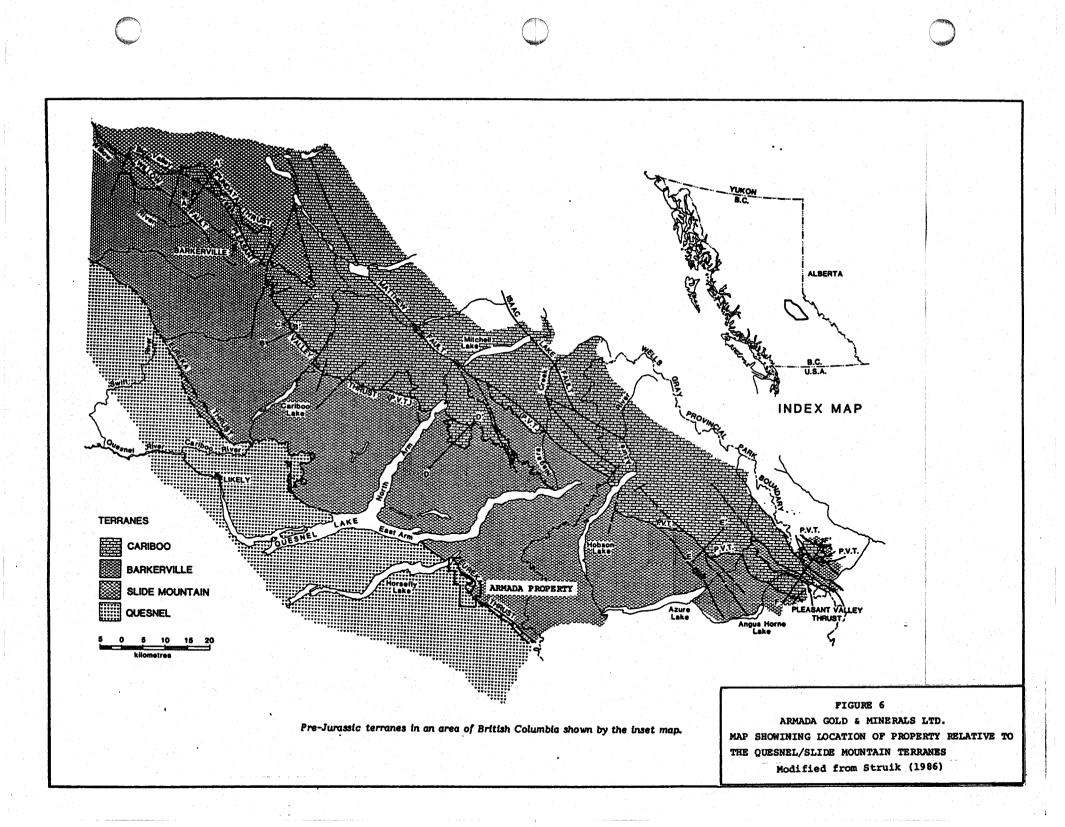
Recent mapping by Struik (1982a,b, 1983a,b, 1985b,c, 1986, 1987) of the Cariboo Mountains and Quesnel Highlands has resulted in a refinement of the divisions previously defined by Monger et. al. (1982) of the area into four stratigraphic and tectonically distinct terranes. Struik (1985) infers that the various terranes were thrust together and metmorphosed during the Jurassic, re-metamorphosed during mid-Cretaceous and subjected to dextrel strike-slip faulting from mid-Cretaceous to early Tertiary. The terranes going from east to west are the Cariboo (continental shelf clastics and carbonates), Barkerville (continental shelf clastics, carbonates and volcanics), Slide Mountain (oceanic rift volcanics, intrusives and clastics) and Quesnel (island arc volcanics and clastics) (Struik, 1986). Figure 6 shows the distribution of the various terranes and how they are structurally related to each other.

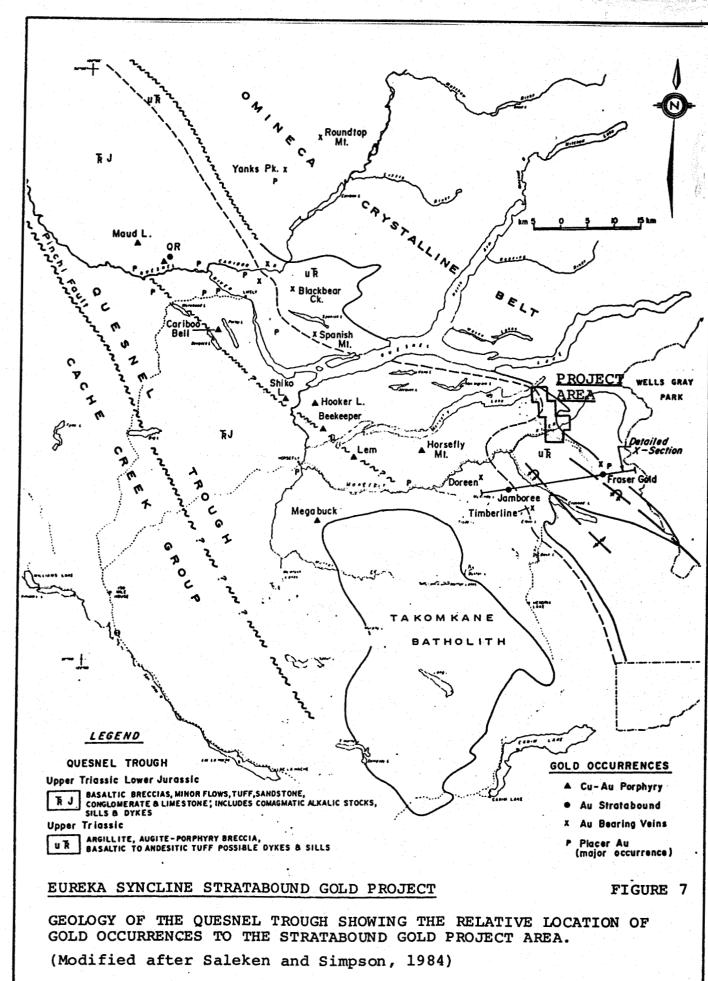
The various terranes are defined by either east dipping or west dipping thrust faults. The Armada property lies along and partially includes a portion of the Eureka Thrust (west dipping) that thrusts Quesnel terrane onto Barkerville.

The gold-bearing occurrences hosted by rocks within the Quesnel Trough are outlined in Figure 7 which also indicates the relative position of the stratabound gold project area. A brief description of the gold occurrences was reported by Saleken and Simpson 1984 and reproduced below:

"In 1964, the Cariboo-Bell deposit was discovered 9 km southwest of Likely. Current drill indicated mineable reserves are 117-million tons grading 0.31% Cu and 0.012 oz/ton Au (including a higher grade zone totalling 30-million tons grading 0.38% Cu and 0.018 oz/ton Au). Mineralization is mainly confined to high level, intrusive breccia zones within an alkalic laccolith of early Jurassic age emplaced at the site of an Upper Triassic eruptive center.

During the early 1970's most of the known Jurassic alkalic plutons in the Likely-Horsefly area were staked and explored for similar coppergold mineralization. Though most were found to contain some auriferous chalcopyrite mineralization in stockwork or disseminated deposits, none proved to be significant in size or grade. It was during the investigation of one of these comagmatic stocks that the QR deposit was discovered in the late 1970's. Gold mineralization was found associated with a pyrite-epidote zone in basaltic breccia flanking





.....

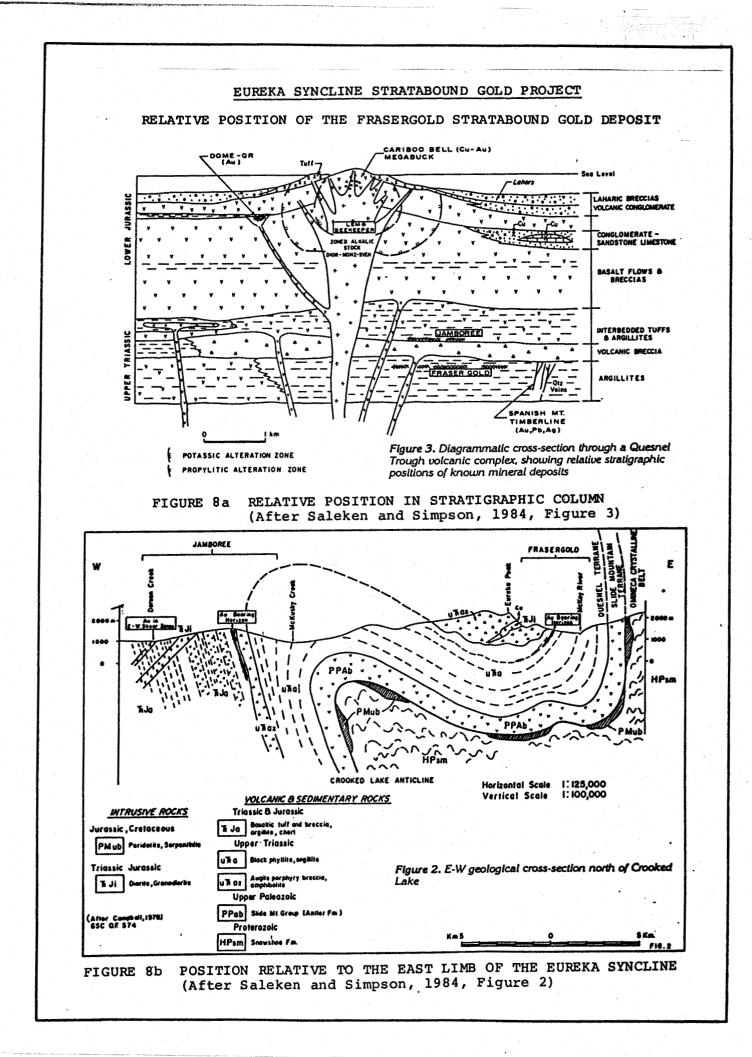
 $\bigcirc$ 

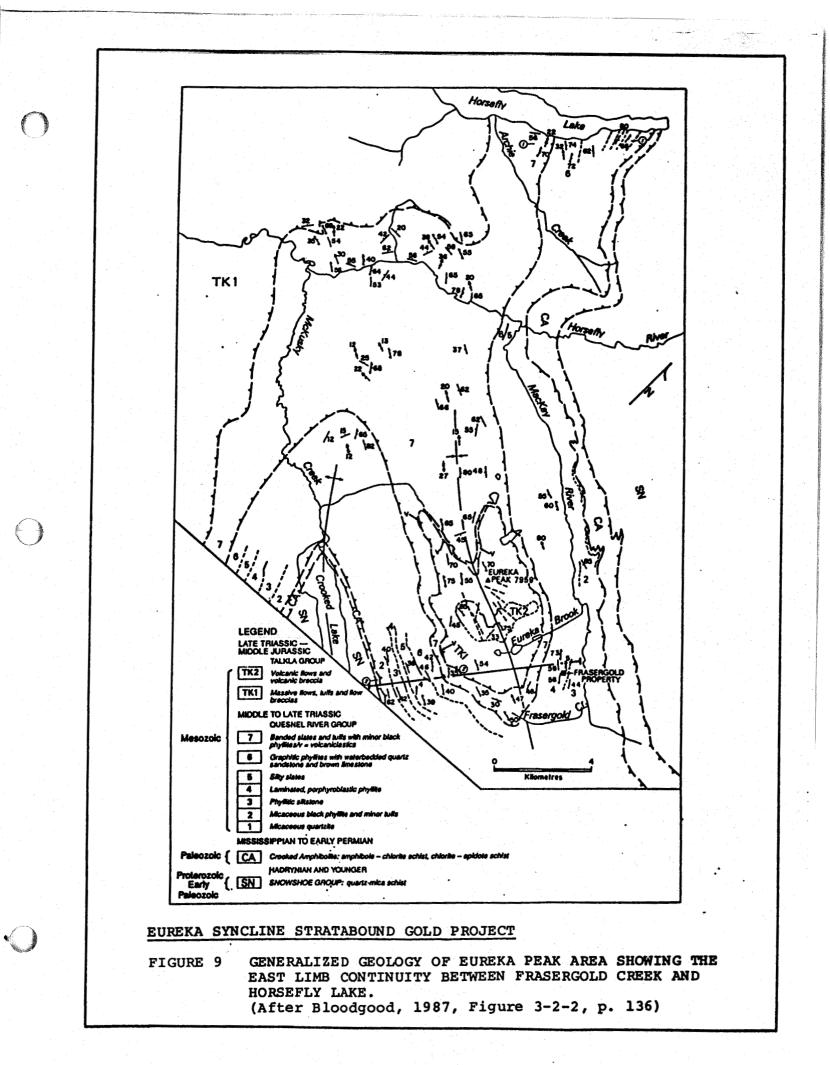
a zoned alkalic stock. The mineralized horizon occurs immediately below a sedimentary contact and above a strongly carbonatized zone (Fox 1983). Drill indicated reserves have been reported as 950,000 tons grading 0.21 oz/ton Au (CMH 1982-83).

During the renewed exploration activity in the 1980s other, seemingly stratabound, gold occurrences have been discovered in the eastern Quesnel Trough. Near Frasergold Creek, Eureka Resources has reported drill indicated reserves of 11-million tons grading between 0.04 and 0.05 oz/ton Au (NAGMIN January 15, 1984). Here, gold-pyrite mineralization occurs along an iron-carbonate rich horizon within the Upper Triassic argillite sequence which has been highly deformed and metamorphosed to phyllite (Belik, 1982). The Jamboree property, northwest of Crooked Lake, hosts a stratabound, anomalous gold horizon in tuffaceous phyllite immediately above a contact with the augite porphyry breccia unit.

Saleken and Simpson (1984) in reviewing the gold occurrences of the Quesnel Trough characterize the Eureka Resources / Southlands Mining Corporation. Frasergold deposit which adjoins the Armada property as a stratabound gold deposit. Figure 8a illustrates the relative stratigraphic position while Figure 8b illustrates the relative position within the Eureka syncline of the stratabound gold horizon (Frasergold) the western slope of the MacKay River valley (the crosssection line is indicated in Figure 7).

The geological continuity to the northwest along MacKay River to Horsefly Lake is confirmed by the mapping of Bloodgood (1987) who correlated the stratigraphy of the eastern limb of the Eureka syncline from Frasergold Creek to Horsefly Lake (see Figure 9).





### PROPERTY GEOLOGY

#### (1) General

Regional detailed geologic mapping of the Eureka Peak area by Ms. M.A. Bloodgood in 1984 and 1985 as part of a Masters Thesis / Canada / British Columbia Mineral Development Agreement provided the mapping / conceptual base upon which the present study is based. Bloodgood (1987) inferred that near identical stratigraphy within the black phyllite unit existed along strike from the recent gold discovery of the Frasergold property to the south shore of Horsefly Lake, a distance of approximately 25 kilometres.

Geologic mapping by the writer (geologic map in pocket, Figure 10) is at a scale of 1:10,000. Mapping was done by hip chain and brunten and/or surveyed grid. The formation unit designations are the same as used by Bloodgood (1987) with a few minor changes. In general, the overall distribution of the various black phyllite units are about the same as shown on Bloodgood's map (1987) with the exception of the section along Horsefly Lake and much more detail in areas previously mapped as covered.

### (2) Geologic Setting

The Fork 1-4, AR 1-2 and TEP 1-3 mineral claims are mainly underlain by an unnamed black phyllite formation that have been assayed to the Middle to Late Triassic Quesnel River Group (Tipper, 1978; Campbell, 1978).

The black phyllite formation structurally overlies (thrust fault contact) rocks of the Mississippian to early Permian Crooked Amphibolite (correlative to the Antler Formation of the Slide Mountain Group) and possibly Proterozoic to early Paleozoic Snowshoe Group rocks. The only exposure of Crooked Amphibolite on the property is located approximately 100 metres east of the Carlson Bridge (see Figure 10). At this location the Crooked Amphibolite consists of pale green to gray, fine-grained, banded well foliated biotite-chlorite-quartz schist. Foliation is defined by both the alignment of phyllosilicate minerals and discontinuous quartz/carbonate bands 2-20 mm in width. The contact between the unnamed black phyllite and the Crooked Amphibolite is covered by glacial debris.

Near the northeast end of Horsefly Lake (Figure 10) is an outcrop exposed along a logging road of fine to coarse grained, well-foliated quartz-muscovite schist containing minor biotite and flattened garnets. Bloodgood (1987) appears to have mapped this unit as the basal unit (micaceous quartzite, Unit 1 on Figure 9) of the unnamed black phyllite. The writer believes this unit to be part of the Snowshoe Group based on its higher grade of metamorphism (amphibolite facies) than the overlying black phyllite and the rock type description fits Snowshoe Group rocks. In a discussion with Dr. L.C. Struik (Geol. Surv. Can.) he also felt, based on writer's description of the quartz-mica schist, that it was probably Snowshoe Group.

The unnamed black phyllite formation as defined by Bloodgood (1987a,b) consists of six or seven units depending upon the reference cited. The units from base to top are  $TR_{a1}$  (Unit 1) micaceous quartzite,  $TR_{a2}$  (Unit 2) micaceous black phyllite and tuffs,  $TR_{a3}$  (Unit 3) phyllitic siltstone,  $TR_{a4}$  (Unit 4) laminated phyllite and porphyroblastic phyllite,  $TR_{a5}$  (Unit 5) silty slates and  $TR_{a6}$  (Unit 6) graphitic black phyllites with interbedded quartz sandstone and limestone (Bloodgood, 1987b).

The following description of the various units in the unnamed black phyllite package is based on the writer's observations unless otherwise shown.

### Unit 1 (TR<sub>al</sub>)

The basal unit as defined by Bloodgood (1987a) is in the writer's view not exposed on the claims (see previous discussion regarding Snowshoe Group). Bloodgood (1987a) described Unit 1 as "Buff to rust weathering, pale recrystallized quartz sandstone dominates the unit. Locally the sandstones are dark grey to green in colour. Compositional layering is outlined by alternating quartz rich and mica rich bands. Placer alignment of muscovite defines the schistosity strongly developed parallel to bedding."

### Unit 2 (TR<sub>a2</sub>)

Unit 2 rocks are well exposed along the MacKay River where it passes through Forks 4 (Figure 10). At this location Unit 2 consists of dark grey to silver grey, very fine grained, very siliceous, tightly foliated, locally pyritic and/or graphitic, moderate to high sheen phyllite. Locally the phyllite is poorly laminated, but in general it is impossible to define bedding because of the well developed cleavage/foliation.

### Unit 3 (TR<sub>a</sub>3)

Unit 3 is well exposed along the logging road above Horsefly Lake (TEP 1) and partially exposed in the lower part of No. 1 creek (Forks 4). The lower contact of Unit 3 is not exposed at either of the locations, but it is assumed that the stratigraphically lowest exposure on the Horsefly Lake section is fairly near the base of the unit. Unit 3 on the Horsefly Lake road consists mainly of medium dull gray, very fine grained, locally well laminated, moderately foliated carbonaceous calcareous phyllite containing narrow sections of very siliceous high sheen phyllite. The top of Unit 3 (Horsefly Lake section) is marked by a narrow (3-5 metres) black, very carbonaceous calcareous silty phyllite. In contrast to the Unit 3 in the Horsefly Lake section, Unit 3 at the No. 1 creek location is very siliceous (no carbonate) much more pyritic including bedded pyrite (1 mm beds of very fine grained pyrite) and contains several 1-3 metre beds of white quartzite (almost vein-like except they are conformable to bedding) containing thin bands of very The quartzite-sericite phyllite bands (beds) fine grained sericite phyllite. commonly contain 1-3 percent finely disseminated pyrite and traces of chalcopyrite. A gold assay ran on the above material was negative.

The top of Unit 3 at the No. 1 creek location is marked by a thin unit (5-8 metres) of dark grey, very fine grained, silty, slightly carbonaceous, siliceous, well foliated, high sheen phyllite. Bedding is defined by hairline, highly contorted, white silty beds.

### Unit 4 (TR<sub>au</sub>)

Unit 4 consists of medium grey to silver grey, very fine grained, well laminated, well foliated, tightly folded, siliceous, locally pyritic porphyroblastic (knotted) phyllite. This unit locally contains narrow (1-2 metres) highly contorted, bedded, very fine grained grey limestone beds in the lower part of the unit. Highly deformed (boudinage) quartz veins and/or meta-quartzite beds are common throughout the knotted phyllite unit. The knotted characteristic of Unit 4 makes it one of the most easily identified rock unit in the area. Its appearance is the same at all Unit 4 exposures on the Armada property as well as on the adjoining Eureka Resources Inc./ Southlands Mining Corp. property, which has a published reserve of 20 million tons at a grade of 0.05 to 0.08 ounces gold per ton (George Cross Newsletter, No. 240, December 15, 1987). The Eureka/Southlands deposit is hosted in a quartz-rich horizon within Unit 4. The porphyroblastic appears to be composed of cordierite(?) locally weathered to iron oxides.

### Unit 5 (TR<sub>a5</sub>)

Unit 5 appears to be a very thick unit consisting of medium to dark grey to blue black, very fine grained, siliceous, well foliated locally very graphitic and/or pyritic, locally very well laminated (alternating light coloured, narrow (1-2mm) silty beds and dark phyllite), moderately high sheen phyllite. The unit contains a number of sections of containing interbedded grey micaceous siltstone. Smeared pyrite is locally common on foliation surfaces. Unit 5 commonly breaks out at the outcrop in elongate rod shaped fragments (pensil rock). This is caused by the intense, very tight folding of the foliation in a single direction.

### Unit 6 (TR<sub>a6</sub>)

Unit 6 is very poorly exposed on the Horsefly Lake section therefore the following definition is questionable. Where exposed, Unit 6 consists of medium grey to black, very fine grained, siliceous, blocky, poorly foliated rusty weathering phyllite. The Horsefly Lake section contains mainly grey to pale grey, very fine grained siliceous tuffs which may be part of the overlying unit. No attempt was made to map the

Unit 6 exposed on the Forks claims because it did not appear to host any mineralization. The contacts and attitudes of Unit 6 shown on the Forks claims section of Figure 10 are from mapping by Mary Ann Bloodgood, (1987).

Unit 7 (Bloodgood, 1987a) or Unit TRb (Bloodgood, 1987b) was only mapped on the Horsefly Lake section. At the location (south of TEP 2) the unit consists of mainly grey to pale green, very fine grained siliceous tuffs interbedded with minor dull, dark grey, very fine grained siliceous, blocky meta-siltstones and/or slates. At this same location there is a number of variable width dykes or small stock-like intrusions of dark grey to greenish grey, fine grained, inequigranular, hornblende/augite locally porphyritic diorite. The diorite commonly contains medium grained disseminated, slightly magnetic pyrrhotite.

The possibility of more intrusive activity in the area is suggested from a strong magnetic deflection of the compass in the vicinity of the Legal Corner Post at TEP 1 and 2, although no igneous rock was observed in the immediate area.

Structurally, the Forks, AR and TEP claims cover a segment of the northeast limb of the Eureka Peak syncline. Bedding attitudes are quite variable along strike and range from 30 degrees to vertical with most of the strike direction clustered around 130 degrees ( $\pm$  10 degrees). Most of the Horsefly Lake section dips steeply (70-85 degrees) northeast which suggests some degree of overturning on this segment of the Eureka Peak syncline. All of the black phyllite package appears to exhibit intense isoclinal folding which creates a difficult mapping situation for tracing individual units along strike. Fortunately, for this study the critical unit (Unit 4 - knotted phyllite) is also a very good marker horizon.

### (3) Mineralization

Exploration and sampling by Amoco, Eureka and others have shown that gold mineralization is found in and associated with quartz sweats and/or veins in porphyroblastic black phyllite (Unit 4). The lense, pods and irregular veins of quartz that contain gold are indistinguishable from unmineralized quartz in the same area. It was noted that the mineralized quartz always contained sericite and ankerite or siderite, but barren quartz with the same mineralogy was also sometimes present. A few samples of quartz bearing material found in Unit 4 was sampled by the writer. The one sample contained 0.065 ounces per ton gold (Figure 10, TEP 1) was taken over a 25 centimetre width from a partially exposed boudinaged quartz vein. Thick glacial cover prevented more extensive sampling in the area. The appearance, character and stratigraphic position of the gold bearing sample is identical to the gold bearing outcrop on the Eureka Resources, Inc. property.

#### **GEOCHEMICAL SURVEY**

A silt/soil geochemical survey was conducted over two separate grids on the claim group at various times during the period 29 July to 24 September, 1987 by the writer, Mr. C.E. Gunn and personnel provided by Durfeld Geological of Williams Lake. The sampling of Grid 1 (Figure 11) was done by Mr. Gunn and to a lesser extent by the writer while geologic mapping. Sampling of Grid 2 (Figure 10) (Horsefly Lake section) was mainly done by Durfeld Geological with a minor amount by Mr. Gunn and the writer.

The soil samples were collected along hand-cut and/or flagged north-south (Grid 1) or east-west (Grid 2) lines. Grid 1 contains 12.95 kilometres of line and 2.1 kilometres of baseline and was sampled on 25 metre intervals along the line and 50 metre intervals along the baseline. Grid 2 contains 16.195 kilometres of line 2.5 kilometres of baseline and both the lines and the baseline were sampled on 50 metre intervals. A total of 935 soil samples and 33 silt samples were collected.

Silt samples were collected when any drainage crossed a line and along all of the roads, and occasionally along the coarse of the drainage. Silt sampling results are shown on the geologic map (Figure 10).

The soil sampling method consisted of digging a shallow hole with a grab hoe or shovel and collecting the sample from the "B" horizon. The sample was placed in a Kraft bag and marked as to location. Silt samples were collected with a plastic spoon from several locations at a given sample point and placed in a waterproof Kraft bag the same as the soil samples.

All samples were analyzed by Acme Analytical Laboratories Ltd., 852 East Hastings Street, Vancouver, B.C. V6A 1R6, using 30 element I.C.P. (Inductively Couples Argon Plasm) and an A.A. (Atomic Absorption) for gold.

Soil samples were dried at  $60^{\circ}$  and sieved to -80 mesh and the resultant fraction analyzed. The first batch of silt samples (30) were sieved to -20 mesh and the resultant fraction pulverized prior to analysis. The reason that this method was adapted rather than the normal straight sieving to -80 mesh was that panning of some of the creeks (No. 1 and No. 2) showed free gold coarser than -80 mesh in the pan. It was felt that taking a coarser fraction would pick up this gold. Unfortunately, this reasoning was faulty and as a result the results were much diluted from later check sampling using the -80 mesh fraction for analysis. The following shows the great disparity between the -80 mesh fraction and the pulverized -20 mesh fractions.

#### TABLE I

### A Comparison Between Stream Silt Samples Analyzed for Gold Using -80 mesh and Pulverized -20 mesh Material

Sample No.	-20 mesh (pulverized)	-80 mesh (sieved only)
6	23ppb	2470ppb
7	$\mathbf{I}_{\mathbf{r}}$ , $\mathbf{I}_{\mathbf{r}}$	98
8	102	2820

The laboratory method used to analyze both the soil and silt samples is as follows:

- .500 gram sample is digested with 3 ml solution of 3-1-2, HCL-HNO3-H2O at 95°C for one hour.
- (2) Sample is then diluted to 10 ml with H<sub>2</sub>O. This leach solution is partial for Mn, Fe, Ca, P, Cr, Mg, Ba, Ti, B, Al, Na, K, W, Si, Zn, Ce, Sn, Y, Nb and Ta. Gold detection limit on I.C.P. is 3 ppm, consequently gold was analyzed by

Atomic Absorption (A.A.) from a 10 gram sample which had been ignited overnight at 600°C, digested with hot dilute aqua regia and extracted with methyl isobutyl ketone.

All results are appended (Appendix A).

### (1) Geochemical Silt / Soil Survey Results

The gold geochemical silt and soil results were treated statistically to give the mean, variance and standard deviation. Since by inspection there was no correlation between gold and the other 30 elements that the samples were analyzed for, it was decided that nothing would be gained by statistically analyzing or plotting the results for these elements (see Appendix A for analytical results). Commonly the anomalous values for gold are defined a being the value of the mean plus two standard deviations. The calculated values are given below:

No. of					Standard	Anomalous
Samples	Element	Unit	Mean	Variance	Deviation	Value
935	Au (soil)	ppb	14.079	4011.493	63.336	140.751
30*	Au (silt)	ppb	5.9	352.921	18,786	43.472

\* silt samples that were sieved to -20 mesh and pulverized.

The above statistical approach to determine an anomalous threshold appears to be of little use in dealing with particulate gold. In examining the soil geochemical map (Figure 11) for grid 1 it is very obvious that the background values for the grid area is between 1 and 10 ppb and any value above 50 ppb gold is very anomalous.

Contouring of the plus 50 ppb gold (Grid 1) with an assumed 130 degree trend (most common attitude measured on the gold bearing porphyroblastic black phyllite) defined three possible northwest trending discontinuous anomalous zones. The northern most trend more or less is associated with the knotted phyllite unit as now mapped but because of relatively thick cover the distribution of this unit is questionable in the writer's opinion. The multi-parallel anomalous gold zones could be caused by a repetition of the favourable knotted phyllite due to isoclinal folding, isolated quartz vein systems parallel to the regional trend or glacial smearing. Another factor that may affect the distribution of anomalies is the repeatability of the analysis for particulate gold. A case in point is illustrated on line 12+00E, station 5+25S to 5+75S. At this location duplicate samples were collected after the original sample results showed a very anomalous value (920 ppb). The resampling yielded 23 ppb for a sample site within 5 metres of the original site. Adjoining lower samples gave higher results (9 vs. 32 and 57 vs. 2) (see Figure 11).

The geochemical soil samples from Grid 2 were very low (most in the 1-2 ppb range) due to the extreme thickness of glacial clay in the grid area. Due to their low values it was decided not to make a separate plot but rather just show the higher values on the grid plotted on the geology map (Figure 10). It is interesting to note that a soil sample collected 10 metres for a rock sample site on Grid 2 that contained 0.065 ounces gold per ton was a blank. There apparently has been no mixing of locally derived material with the transported material contained in the glacial debris.

#### CONCLUSIONS

Geologic mapping and soil / silt / rock sampling of the Forks 1-4, AR 1-2 and TEP 1-3 mineral claims has shown that the potentially gold bearing porphyroblastic phyllite unit (Unit 4) is presently under most of the property and it was also shown to contain gold (0.065 opt per 25 cm) at approximately the same stratigraphic horizon as that on the adjoining Eureka Resources, Inc. / Southlands Mining Corp. property. Soil geochemical results were shown to be sometimes helpful in defining potential gold bearing zones, provided that the glacial overburden is not too thick. The geochemical results also showed that the only indicator element for gold was itself.

Further geochemical definition is probably not warranted because of adverse cover conditions so further work will require fairly extensive trenching and/or diamond drilling at those areas now known to be underlain by the porphyroblastic phyllite.

### PERSONNEL TIME DISTRIBUTION

# (Forks 1-4, AR 1-2, TEP 1-3 Mineral Claims

ard, M.Sc., P.Eng. July 29 - August 10, 1987 inclusive August 30 - September 9, 1987 inclusive	24 days
, Professional Prospector July 29 - August 10, 1987 inclusive August 19 - September 14, 1987 inclusive	40 days
eological Staff August 18 - September 23, 1987 Linecutting, sampling contract by the kilometre time not charged	37 days

### COST STATEMENT

### Personnel

4

\$ 9,600.00 6,250.00
12,000.00
28,350.00
15,150.00
10,181.85
3,000.00

### Expenses and Disbursements Continued

Camp operation and travel expenses\$	2,072.95
Flagging, topo string, sample bags	258.96
Telephone	36.82
Sub-total	30,700.58
Report Expenses	
On-Words (typing) Geodrafting Services Ltd. (drafting maps) Xeroxing	123.75 750.00 20.00
Sub-total	893.75
TOTAL	\$59,944.33

Respectfully submitted,

ESSI DAVID A. HOWARD И WH GINEE

D.A. Howard, M.Sc., P.Eng. D.D.H. Geomanagement Ltd.

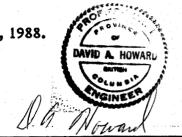
### D.D.H. GEOMANAGEMENT LTD.

### CERTIFICATION

I, David A. Howard, of the City of Vancouver, Province of British Columbia, hereby certify as follows:

- 1. I am a geologist residing at 9040 Glenallan Gate, Richmond, B.C., with an office at 422 470 Granville Street, Vancouver, B.C.
- 2. I am a registered Professional Engineer of the Province of British Columbia. I graduated from Montana State University in 1964 and from the University of Washington in 1967.
- 3. I have practised my profession continuously since June, 1966, with the firm Placer Development Ltd. and since 1981 with D.D.H. Geomanagement Ltd., the latter of which I am a principal.
- 4. I am the author of this report which is based on property work during the period 29 July to September 23, 1987.
- 5. I have a direct interest in the subject property.

Dated at Vancouver, B.C., this /7 # day of February, 1988.



David A. Howard, M.Sc., P.Eng.

#### REFERENCES

- Belik, G.D., 1982: Summary Report on the Frasergold Property, Cariboo Mining Division, British Columbia for Eureka Resources, Inc., Qualifying Report in Eureka Resources, Inc. Prospectus, June 1, 1983.
- Belik, G.D., 1983: Geological, Geochemical and Diamond Drill Report on the Bee Group, Cariboo Mining Division, British Columbia, for Ripple Resources Ltd., Assessment Report. No. 11724.
- Bloodgood, M.A., 1987a: "Geology of the Triassic Black Phyllite in the Eureka Peak Area, Central British Columbia" in Geological Fieldwork, 1986, B.C. Min. of Energy, Mines and Pet. Res., Paper 1987-1.

\_\_\_\_, 1987b: "Geology of the Eureka Peak - MacKay River Area, Central British Columbia, NT.S. 93A/7; Min. of Energy, Mines & Pet. Res. Open File Map 1987-89.

- British Columbia: Annual Report of the Minister of Mines for the years 1901, 1902, 1903, 1910, 1934.
- Campbell, R.B., 1978: Quesnel Lake Map Area, 93A, B.C., Geol. Surv. Can., O.F. 574.
- Dawson, J.M., 1984: Geochemical Report on the LL #1 Claim, Cariboo Mining Division, British Columbia for Valhalla Minerals Inc., Assmt. Rept. No. 12590.

Saleken, L.W. and Simpson, R. G., 1984: "Cariboo-Quesnel Gold Belt: A Geological Overview" in Western Miner, Vol. 57, No. 4, pp. 15-20.

Sketchley, D.A., 1982: Soil Geochemical Report, Hawk 1 Claim, Cariboo Mining Division, for Dennison Mines Limited, Assmt. Rept. No. 10107.

Struik, L.C., 1981: A re-examination of the type area of the Devono-Mississippian Cariboo Orogeny, central British Columbia; Canadian Journal of Earth Sciences, v. 18, p. 1767-1775.

1982a: Snowshoe Formation (1982), central British Columbia; in Current Research, Part B, Geological Survey of Canada, Paper 82-1B, p. 117-124.

\_, 1982b: Bedrock geology of Cariboo Lake (93A/14), Spectacle Lake (93H/3), Swift River (93A/13) and Wells (93H/4) map areas, central British Columbia; Geological Survey of Canada, Open File 858.

1983a: Bedrock geology of Spanish Lake (93A/11) and parts of adjoining map areas, central British Columbia; Geological Survey of Canada, Open File 920. \_, 1983b: Bedrock geology of Quesnel Lake (93A/10) and part of Mitchell Lake (93A/15) map areas, central British Columbia; Geological Survey of Canada, Open File 962.

\_, 1985a: Pre-Cretaceous terranes and their thrust and strike-slip contacts, Prince George east half and McBride west half, British Columbia; in Current Research, Part A, Geological Survey of Canada, Paper 85-1A, p. 267-272.

\_, 1985b: Dextral strike-slip through Wells Gray Provincial Park, British Columbia; <u>in</u> Current Research, Part A, Geological Survey of Canada, Paper 85-1A, p. 305-309.

\_\_, 1985c: Thrust and strike-slip faults bounding tectonostratigraphic terranes, central British Columbia; in Field Guides to Geology and Mineral Deposits in the Southern Canadian Cordillera, ed. D.J. Tempelman-Kluit; Geological Society of America, Cordilleran Section, p. 14.1-14.8.

\_\_\_, 1986: A regional east-dipping thrust places Hadrynian onto probable Paleozoic rocks in Cariboo Mountains, British Columbia; in Current Research, Part A, Geol. Surv. Canada Paper 86-1A, 589-594.

\_, 1986: Imbricated terranes of the Cariboo gold belt with correlation and implications for tectonics in southeastern British Columbia; Can. Jour. of Earth Sciences, v. 23, p. 1047-1061.

Wheeler, J.O. et.al., 1972: "The Cordilleran Structural Province", in Variations in Tectonic Styles in Canada, Geol. Assoc. of Can., Spec. Paper No. 11.

#### Other

G. Cross Newsletter: No. 240, December 15, 1987.

1982 - 1983 Canadian Mines Handbook, p. 116.

1984 - Annual Report, Eureka Resources, Inc.

1986 - Eureka Resources, Inc. Annual Report.

1984 - North American Gold Mining Industry News, Vol. 2, Issue 1, January 15, 1984, p. 1.

1986 - Stockwatch - a publication of Canjex Publishing Ltd., Vancouver, B.C., dated March 30, 1987.

# APPENDIX A

GEOCHEMICAL RESULTS ACME ANALYTICAL LABORATORIES LTD.

DATE RECEIVED ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS, VANCOUVER B.C. PH: (604) 253-3158 COMPUTER LINE: 251-1011 DATE REPORTS MAILED

### ASSAY CERTIFICATE

SAMPLE TYPE : ROCK - CRUSHED AND PULVERIZED TO -100 MESH. AGII & AUII (1A/T) BY FIRE ASSAY Aly DEAN TOYE , CERTIFIED B.C. ASSAYER ASSAYER DDH GEOMANAGEMENT PROJECT ARMADE FILE# 87-3316 SAMPLE Au\*\* Aq \* \* oz/t oz/t

PAGE# 1

B 9867

.13 .003

Nol creek Fork 4 Sericite Phyllite

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE (604)253-3158 FAX (604)253-1716

# GEOCHEMICAL/ASSAY CERTIFICATE

r

(

....

C

ť

1

C

(

C

C

(

(

C

0

(

(

C

.500 GRAM SAMPLE IS DIGESTED WITH 3HL 3-1-2 HCL-HN03-H20 AT 95 DEG.C FOR- DNE HOUR AND IS BILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LINITED FOR NA K AND AL. AU DETECTION LINIT BY ICP IS 3 PPM. - SAMPLE TYPE: Rock Chins A511 BY FIRE ASSAY. AU11 BY FIRE ASSAY

											•		_		· ·																·	
IPLE#	PPN	CU PPN	PB PPN	ZN PPM	A6 PPN	NI PPM	CO PPM	HN PPH	FE		U PPM	au PPN	TH PPN	SR PPM	CD PPH	SB PPN	BI PPM	PPN	CA I	P I	PPN	CR PPH	M6 Z		11 1	PPN	AL I	NA Z	. X		A5\$\$ 02/t	
27028	6	94	661	2236	151.8	15	3	1013	1.74	114	5	ND	2	371	35	52	2		4.50	.023	2	4	.55	16	.01	3	.13	.02	.06			.023
27029	13		1710			.44	11		4.68	247	5	ND		11	17	24		21		.071	25	10				3		.01				.035
27030 27031	15		2138 17		253.2	3 39	2		1.00	262 12	5	ND ND	1 7	2 148	7	15 3	2		.02 5.63	.002	15	23	.01 .80	6 72	.01 .01	2	.03 1.43	.01	.01		7.55	.042
27032	13				36.4	15	2		.90	24	5	ND	1	3	49	11	2	2		.003	2	- 3	.03	2	.01		.06	.01				.030
1																																
7033	2	68	96	41	2.5	32	11	268	2.64	4	5 21	ND	7	21	1	2 16	2	6		.048	13	10	.20	29	.01	2	.62	.04	.08	1	.08	.065
C	18	58	37	132	7.1	67	26	1029	3.97	40	21	1	39	50	17	16	22	56	•49	.084	37	58	.87	177	.08	32	1.84	•08	.14	13	-	-
	- : \																								\$							
		$\mathbf{V}$														1.1		·														
		$\sum$																•														

ACME ANALYTICAL LABORATORIES 852 E.

852 E. HASTINGS ST. VANCUVER B.C. VAA 1R6 PHONE 253-3158

DATA LINE 251-1011

(

C

C

•

£

C

€

C

## GEOCHEMICAL ICP ANALYSIS

#### .500 GRAM SAMPLE IS DIGESTED WITH 3HL 3-1-2 HCL-HN03-H20 AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 HL WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: SILT AUX ANALYSIS BY AA FROM 10 GRAM SAMPLE.

Silt sumple. Pulverized

DATE RECEIVED: AND 14 1987 DATE REPORT MAILED: MIC 24

24/87 ASSAYER. A Mar Dean Toye, CERTIFIED B.C. ASSAYER

D.D.H. GEOMANAGEMENT PROJECT-ARMADA File # 87-3295

	SAMPLE	HO PPM	CU PPM	PB PPM	ZN PPM	A6 Ppn	.NI PPN	CO PPM	MN PPH	FE 2	AS PPM	U PPM	AU Ppm	TH PPN	SR PPN	CD PPM	SB PPM	BI PPM	V PPM	CA Z	P Z	LA PPM	CR PPM	MG %	BA PPM	11 7	B PPM	AL Z	NA Z	K Z	N PPN	AU\$ PPB	
	FORK-1	1	29	12	114	.1	48	13	292	4.15	10	5	ND	2	42	· 1	2	2	75	.50	.036	5	99	.78	48	.10	2	.89	.03	.05	1	1	
	FORK-2	1	29	11	157	.1	54	18		3.21	. 9	5	ND	2	45	1	2	2	54	.56	.046	6	97	.95	59	.08		1.06	.05	.06	1	1	
	FORK-3	. 3	34	12	121	.1	51	16	1424	4.95	8	5	ND	2	39	1	2	2	80	. 44	.037	7	82	.63	93	.09	2	.85	.03	.05	1.	1	
	FORK-4	2	29	10	99	.1	41	11	662	3.11	4	5	ND	2	37	1	3	2	46	.41	.032	6	69	.62	61	.07	2	.79	.03	.05	1	1	
	FORK-5	3	32	10	112	.2	44	11	767	3.32	8	5	ND	2	39	1	2	2	50	.44	.037	8	72	.63	79	.07	.2	.86	.03	.06	1	23	
	FORK-6	3	27	14	94	.2	42	10	583	3.93	7	5	ND	3	35	1	2	2	60	.39	.035	9	71	.59	68	.08	2	.80	.03	.06	1	1	
	FORK-7	- 4	40	13	132	.3	50	12	364	4.16	. 9	5	ND	3	35	1	2	2	60	. 39	.041	7	- 71	.63	52	. 08	2	.82	.03	.05	1	102	
	FORK-8	3	37	13	121	.2	48	12	382	4.02	7 -	5	ND	2	37	- 1	2	2	60	. 41	.039	7	74	.66	52	.08	2	.81	.03	.05	1	2	
	FORK-9	- 3	37	13	114	.2	46	11	323	4.15	. 9.1	5	ND	2	34	1	2	2	63	. 38	.039	7	66	.62	51	.09	5	.80	.04	.04	1	4	
	FORK-10	5	27	14	80	.3	38	11	1052	3.12	4 -	5	ND	2	42	1	2	2	44	.45	.039	8	66	.61	75	.06	4	.90	.04	.05	i	. 1	
	FORK-11	2	28	12	58	.1	35	12	725	3.06	8	5	ND	1	46	1	2	ź	56	.52	.034	6	84	.70	70	.08	2	.90	.03	.06	1	. 1	
	FORK-12	1	24	8	60	.1	33	10		2.78	4	5	ND	2	38	1	2	2	50	.45	.035	5	73	.64	56	.08	5	.77	.03	.04	1	17	
	FORK-13	1	25	10	42	1	- 31	10	367	3.09	5	5	ND	2	40	1	2	2	58	.49	.036	5	79	.66	56	.09	6	.74	.04	.04	t	1	
	FORK-14	.1	18	8	41	.1	27	8	211	2.54	2	. 5	NÐ	1	40	1	2	2	49	.47	.028	3	80	.59	33	.08	2	.64	.03	.04	1	1	
15	FORK-15	- 1	22	6	81	.1	30	8	218	2.11	6	5	ND	1	36 .	1	2	2	36	.43	.033	4	81	.66	46	.08	2	.73	.03	.04	2	1	
	TEP-1	ĩ	26	15	51	.2	26	8	1071	2.29	9	12	NĐ	6	33	1	2	2	24	.35	.032	30	26	. 53	150	. 08	2	1.55	.03	.25	1	1	
	TEP-2	1	18	16	90	.5	27	7			8	5	NĐ	6	25	1	2	2	15	.58	.090	19	15	.40	58	.04	2	.78	.03	.11	1	1	
	TEP-3	1	11	12	53	.2	20	5		1.64	6	5	ND	6	33	1	2	2	13	.30	.028	15	14	.36	51	.05	2	.79	.03	.10	1	2	
	TEP-4	. 4	34	14	128	.6	40	7	544	2.39	9	5	ND	5	27	1	2	2	16	.31	.037	15	16	.40	82	.04	2	.89	.03	.15	1	2	
	TEP-5	2	21	10	69	.3	22	5	313	1.73	8	5	ND	6	20	1	2	2	13	. 28	.040	14	13	.34	45	.04	7	.65	.03	.11	1	1	
	TEP-6	2	25	15	68	.2	24	7	492	2.50	22	5	ND	6	29	1	3	2	15	.31	.043	16	15	.37	67	.04	2	.77	.02	.12	2	1	
	TEP-7	3	25	15	126	.2	34	. 7		2.42	12	9	ND	7	22	1	2	2	13	.29	.049	17	10	.37	53	.03	2	.73	.02	.10	1	1	
	TEP-8	5	29	15	457	.3	89	9	2179		14	5	ND	5	25	3	4	2	16	.27	.041	14	11	.36	99	.03	8	.74	.03	.10	1	2	
	TEP-9	3	25	15	187		-44	7	877	2.13	10	5	ND	5	31	2	2	2	16	.35	.036	15	15	.40	87	.03	. 9	.84	.04	.12	2	1	
	TEP-10	. <b>1</b>	22	15	122	.4	45	. 23	556	2.47	6	5	ND	8	14	1	3	2	19	.18	.043	24	21	.58	79	.05	7	1.14	.03	.18	~ 1	1.	
	TEP-11	3	21	14	99	.2	28	8	381	2.30	3	5	ND	8	20	1	2	2	20	.31	.066	18	23	.53	53	.05	2	. 88	.03	.10	1	2	
	AR-1	4	23	16	108	.3	30	10	716	2.95	. 4.	5	ND	4	20	2	2	2	27	.29	.052	20	26	.62	54	.06	2	1.16	.02	.08	1	1	
	AR-2	9	23	14	237	.5	42	- 8	552	2.99	7	-5	ND	6	33	4	2	2	26	.56	.103	18	23	.58	65	.03	2	. 88	.03	.06	2	1	
	AR-3	5	29	11	145	.3	38	.10	1028	3.05	6	5	ND	5	26	2	2	2	29	.40	.056	15	28	.68	68	.05	3 . 3	1.03	.03	.07	2	° 1	
	AR-4	.3	32	11	91	.4	30	8	361	2.44	5	5	ND	6	- 19	. <b>1</b>	2	- 2	<b>22</b> .	.29	.057	16	20	.58	41	.05	2	.84	.02	.07	1	1.	
- 1	STD C/AU-S	18	58	44	132	7.0	67	26	890	3.99	41	19	7	37	47	18	19	21	55	. 48	.087	35	57	.88	175	.08	32	1.82	.08	.13	12	49	

ACME ANALYTICAL LABORATORIES

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

Grid 1

# GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HN03-H20 AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR NN FE CA P LA CR NG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPN. - SAMPLE TYPE: P1-16 SOIL P17-18 SILT AUX ANALYSIS BY AA FROM 10 GRAM SAMPLE.

										-18 SI									1.	1												
DATE REC	CEIVE	D:	SEPT	16 198	97	DAT	E RE	EPOR	T MA	AILE	D: )	Sef	42	9/2	7	ASS	AYER	. A	(c)	kep	1. DE	AN	TOYE	E, C	ERTI	FIE	DB.	с.	ASSA	YER		
		<b>.</b>				D.1	р.н.	GE	0-MA	NAG	EMEN	IT P	ROJE	CT-	ARMA	DA	Fi	le f	# 87	7-42	60	Pé	ağe	1								
SANPLE#	NO PPN	CU PPH	PB PPM	ZN PPM	AG PPN	NI PPN	CO PPM	HN PPM	FE	AS PPM	U PPM	AU - PPN	TH PPN	SR PPN	CD PPM	SB PPM	BI PPM	V PPM	CA Z	P	LA PPM	CR PPM	MG - 7	BA PPN	TI - 7	B PPM	AL I	NA Z	KZ	N PPN	AUX PPB	
0+00 3+75N	. 4	48	÷.	100	.3	33	14	547	3.15	3	- 5	ND	6	23	3	2	5	33	.40	.060	16	45	.60	43	.06	5	.92	.01	.10	1	. 1	
0+00 3+50N	6	109	25	304	1.5	78	23		5.21	15	5	ND	10	36	4	2	2	30	.54	.109	27	40	. 61	41	.04	2	.97	.01	.06	1	3	
0+00 3+25N	11	104	44	426	1.6	93	25	994	6.45	10	5	ND	9	29	3	2	2	27	.44	.101	26	33	•54	43	.03	-6-	.98	.01	.05	1	9	
0+00 3+00N	1	10	2	45	.2	12	3		1.94	4	. 5	ND	2	6	.3	.3	2	28	.03	.062	15	26	.20	36	.01	13	.86	.02	.02	2	9	
0+00 2+75N	5	26	17	150	.7	33	9	602	6.77	- 18	5	ND	<b>4</b> - 	17	1	2	3	. 76	.11	.189	12	77	.39	74	.06	2	1.63	.01	.04	1	1	
0+00 2+50N	15	126	19	354	.9	58	39	1913	17.94	3	5	ND	11	7	4	2	2	15	.13	.255	10	19	.18	43	.01	2	1.16	.01	.02	1	1	
0+00 2+25N	22	160	37	392	2.7	105	22	1057	7.48	10	- 5	ND	8	17	. 3	2	2	31	.19	.112	19	61	.45	65	.03	. 6	1.27	.01	.04	1 -	16	
0+00 2+00N	12	36	21	159	2.8	-34	-11		7.09	- 8	5	ND	6	15	2	2	2	79	.09	.149	. 9	75	• 26	48	• 0H		1.04	.01	.04	1	2	
0+00 1+75N	13	51	24	196	1.7	36	9	1.1.1	6.62	9	5	ND	4	10	1	2	2	59	.06	.209	13	34	-21	54 .	. 05		1.00	.01	.04	1	1	
0+00 1+50N	20	79	22	242	1.5	61	14	458	9.03	9	5	ND	· 5	13	1	2	2	49	.12	.216	-9.	- 95	.32	49	.08	5	1.44	.01	.03	1	5	
0+00 1+25N	7	39	11	156	2.2	34	11	516	5.92	16	5	ND	1	20	1	2	2.	49	.17	.108	14	55	.46	63	. 04	2	1.36	.01	.04	1	2	
0+00 1+00N	6	33	6	129	2.1	31	12	425	5.98	10	5	ND	4	24	1	2	2	81	.19	.106	9	116	.47	61	.09	.2	1.25	.01	.05	1.1	3	
0+00 0+75N	6	44	16	180	2.3	43	12	412	5.80	7	5	ND	- 4	29	3	2	2	71	.21	.058	10	113	.65	98	.09	. 18	1.55	.02	.07	1 -	10	
0+00 0+50N	. 4	32	5	- 75	.4	27	10	401	4.63	9	5	ND	3	-37	1	2	2	85	.29	.038	11	117	.65	119	.13	8	1.39	.02	.08	1	2	
0+00 0+25N	2	34	2	67	.8	27	11	472	2.28	5	5	ND	. 1	38	2	2	2	62	.43	.031	10	107	• • 62	99	.09	10	1.08	.01	.07	1	1	
0+00 0+00N	3	23	2	57	.4	27	10	310	3.80	8	5	ND	1	37	1	2	2	96	.30	.023	. 7	130	.59	97	.13	3	.95	.02	.05	1.	2	
0+00 0+255	2	. 74	10	102	.3	54	20	473	4.49	10	5	ND	3	37	1	2	2	. 74	.48	.056	7	184	.97	83	.10	14	1.61	.02	.10	1	13	
0+00 0+505	2	69	2	113	.6	55	16	234	3.11	. 16 .	5	ND	1	39	1	2	2	75	.41	.054	91	143	.77	104	.08	2	1.43	.01	.10	1	2	
0+00 0+755	5	24	16	59	4.3	19	7	229	3.42	10	5	ND	2	35	. 1	2	2	86	.38	.045	11	96	.29	78	.10	2	.75	.01	.06	1	151	
0+00 1+005	2	30	7	88	.6	33	15	351	5.19	.12	5	ND	- 3	29	- 1	2	2	84	.33	.059	5	145	.62	53	.09	7	1.02	.02	.05	1	2	
 ALAA 11750	•		. g	71	.,	37	. 13	774	3.83	- 6	5	ND	3	34		2	2	67	70	.042	9	114	.68	58	.08	10	1.11	.02	.06	1	3	
0+00 1+255 0+00 1+505	1	46 39	- 8	60	.6 .1	26	- 13	326	3.83 4.34	6	5	ND ND	2	- 38	· I 1	3	2	90	.38 .35	.039	10	114	.00	30 83	.14		1.08	.01	.08	1	7	
0+00 1+355	· · 4	. 92	10	115	.6	57	20		4.32	7	5	ND	2	40	1	2	2	76	.44	.048	12	145	.76	145	.09		1.69	.01	.11	1	6	
0+00 2+005	4	60	13	104	.2	52	21		4,49		5	ND	4	43	3	2	2	81	.44	.042	11	131	.98	107	.12	-	1.65	.02	.09	i	5	
0+00 2+255	4	32	9	76	.4	33	10	328	3.91	4	Š	ND	3	40	Ĩ	2	2	66	.34	.028	12	85	.62	58	.11		1.11	.01	.06	1	26	
• • • • • • • • •	-	•=			•								-			-	-													-		
0+00 2+505	2	30	. 5	75	.8	28	9		3.56	2	5	ND	4	37	1	2	-2	67	. 30	.046	11	94	.64	76	.09		1.20	.01	.07	1	2	
0+00 2+755	4	52	10	75	.6	42	15		4.23	6	5	ND	6	41	4	2	- 2	71	.34	.038	12	96	.73	82	.11		1.40	.02	.07	1	10	
0+00 3+005	1	.63	14	103	.5	53	19		4.29	. 9	5	ND	- 3	43	1	2	2	75	.50	.057	12	138	.87	122	.08		1.57	.02	.12	- 1 -	23	
0+50E 0+00	3	38	1	86	.5	36	12		4.71	7	5	ND	3	38	1	2	2	94	.38	.047	- 8	136	.78	76	.15		1.23	.01	.07	1	2	
1+00E 4+25N	4	65	13	153	.5	46	.16	664	3.72	. 5	6	2	6	30	2	2	2	41	.52	.075	21	57	.78	70	.07	13	1.18	.01	.13	1	1	
1+00E 4+00N	5	74	2	114	.3	41	14	535	3.53	6	5	ND	5	26	1	2	2	42	.39	.076	20	65	.74	72	.07	19	1.20	.01	.10	1 -	1	
1+00E 3+75N	2	66	- 6	93	.4	51	14		3.41	12	5	ND	1	- 41	1	3	2	61	.61	.065	10	104	.67	110	.06	-	1.14	.01	.09	1	- 1	
1+00E 3+50N	9	62	24	156	1.3	42	15		5.06	4	5	ND	7	21	3	2	2	37	.23	.085	17	66	.49	51	.04		1.10	.01	.05	1	9.	
1+00E 3+25N	6	110	19	233	.8	94	25		4.24	4	5	ND	13	19	1	2	2	27	.27	.088	24	73	.59	- 34	.04		1.68	.01	.06	1	31	
1+00E 3+00N	2	21	13	54	.8	17	7	950	2.59	6	5	ND	2	28	1	2	2	70	.13	.061	12	71	.18	58	.11	12	.66	.01	.04	1	17	
1+00E 2+75N	7	53	20	251	.6	64	17	521	4.13	. 4	5	ND	7	21	1	2	2	43	.20	.062	16	70	.53	54	.05	3	1.57	.01	.05	1	11	
STD C/AU-S	19	63	39	129	7.1	68		1032		38	18	7	38	51	17	17	21	59	.48	.087	38	68	.89	177	.08	3.7	1.80	.06	.13	13	50	

Gadi D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260 Page 2 SAMPLE P8 AG 00 MN FE AS AU TH SR CD SB B1 ۷ CA CR 80 CU ZN NI U Ρ LA NG BA TI B AL NA ĸ N AUS PPH PPM PPN PPM PPH PPH PPN PPH 7 PPH PPN PPN PPN PPH PPh PPH PPN PPN 7 2 PPH PPN 7 PPM Z PPM Z Z 7 PPN PPR 1+00E 2+50N 33 12 275 3.64 .23 107 55 2 29 -5 98 .7 -5 ND 4 29 3 2 -65 .036 9 .68 .10 4 1.36 .01 .04 2 8 1+00E 2+25N 15 97 11 303 2.0 73 27 1182 11.31 2 5 NÐ 11 2 2 19 .16 .231 11 23 .18 72 .01 2 .81 .01 .02 6 4 1 1+00E 2+00N 42 2 124 .1 43 16 406 3.46 6 ND 39 3 2 61 .35 .054 14 97 .86 78 7 1.32 .01 .05 2 3 4 4 .11 . .7 12 357 32 .31 .72 93 1+00E 1+75N 3 60 5 107 42 3.78 5 ND 2 2 2 69 .039 11 150 .08 9 1.27 .01 .06 6 1 1 1 1+00E 1+50N 62 2 74 .1 35 11 399 3.40 7 5 NÐ 1 31 2 2 69 .35 .053 10 106 .61 57 .07 .91 .01 .05 2 6 2 1 11 1+00E 1+25N 90 5 96 .3 47 15 707 4.25 36 2 2 78 .40 .079 13 120 .73 95 .06 13 1.23 .01 .08 2 9 -5 NÖ 3 3 2 .73 72 1+00E 1+00N 52 95 .1 46 13 491 3.85 9 8 ND 3 33 2 2 67 .35 .041 10 113 .96 .01 4 6 4 .10 6 .06 1 Q .37 1+00E 0+75N 1 57 9 93 .1 42 11 228 2.39 3 5 NÐ 3 36 2 3 2 58 .052 11 113 .79 102 .08 7 1.26 .01 .08 1 16 28 ND 1+00E 0+50N 74 4 113 1.0 55 1782 3.88 6 5 2 37 3 9 2 80 .40 .056 17 144 .77 161 .07 2 1.75 .01 .11 1 6 1 297 3.35 1+00E 0+25N 3 33 2 61 .4 29 11 8 5 ND 1 32 1 2 2 69 .26 .019 12 102 .72 72 .12 2 1.18 .01 .05 1 16 1+00E 0+00 3 76 7 101 .8 45 15 221 2.99 7 5 NÐ 2 36 2 2 59 .39 .046 13 137 .71 121 .09 4 1.46 .02 ..08 1 1 1 1+00E 0+25S 4 62 9 86 .1 44 15 619 3.88 11 5 NÐ 1 33 4 3 71 .33 .056 9 107 .72 104 .07 2 1.21 .01 .10 - 1 1 1 32 443 10 2 2 81 .26 99 .61 1+00E 0+50S 2 35 9 72 .3 14 4.09 5 NÐ 31 4 .051 10 62 .09 4 1.12 .01 .05 4 1 1 1+00E 0+755 5 70 7 98 .3 45 15 699 3.68 9 5 ND 1 33 3 3 3 69 .31 .065 13 114 .76 115 .06 3 1.35 .01 .10 2 23 7 5 NÐ 2 27 2 76 .22 .036 92 .45 .91 1+00E 1+00S 2 28 5 86 .8 9 464 4.06 3 9 115 .11 7 .01 .04 3 1 1+00E 1+25S 22 17 528 2.70 5 25 2 62 .18 .044 .32 57 .08 . 60 .01 .04 2 20 2 6 46 .1 A -5 ND 2 2 8 81 5 1 1+00E 1+50S 2 55 10 79 .1 37 13 450 3.70 8 5 ND 1 32 2 2 65 .35 .055 8 87 .65 80 .09 17 1.01 .01 .05 1 39 1 7 5 2 28 -3 87 .26 47 2 .81 .01 .03 1+00E 1+75S 2 26 9 67 .1 26 9 218 3.92 MÐ 2 .060 8 87 .49 . 09 1 1 1+00E 2+00S 57 74 .2 -41 14 348 3.63 10 5 NØ 3 33 2 2 56 .32 .064 11 83 .83 61 .08 4 1.26 .01 .05 3 1 3 11 1 357 55 .30 .060 78 .73 10 1.05 .01 1+00E 2+255 74 13 3.46 7 2 31 3 2 10 60 .07 .06 2 53 4 .1 40 6 MÐ 2 1 .08 .29 52 10 1.16 .01 .06 1+00E 2+50S 45 2 70 .1 36 13 357 3.45 4 6 NÐ 3 33 3 3 57 .047 10 81 ..71 1 2 1 1+00E 2+755 149 7 160 2.7 98 27 504 4.44 24 5 ND 2 55 6 2 97 .69 .094 16 230 1.09 285 .07 2 2.83 .01 .23 1 5 8 1 32 70 7 88 .62 85 .87 .01 .08 12 69 .3 14 466 3.52 5 ND 2 5 2 .43 .061 .06 11 3 1+00E 3+00S 2 60 44 8 3 1 1+50E 0+00 147 13 137 2.3 67 13 674 3.39 18 5 ND 2 42 3 4 3 68 .58 .076 23 156 .79 209 .05 2 1.87 .01 .14 1 7 6 2+00E 3+25N 202 1.2 62 19 R 5 NŪ 10 19 5 3 32 .24 .071 32 50 .47 32 .04 .97 .01 .03 1 9 7 77 18 609 4.41 6 12 1.05 38 .33 40 .54 49 .04 .01 .05 2+00E 3+00N 1.7 79 20 564 4.60 7 26 2 -3 .065 66 6 116 16 256 5 8 7 1 5 2+00E 2+75N 67 130 53 15 306 5.17 10 5 ND 2 22 2 3 3 57 .24 .058 9 82 .44 27 .05 2 .89 .01 .03 1 5 10 1.1 1 2+00E 2+50N 27 125 1.8 58 19 595 5.15 11 5 KD 3 23 2 2 66 .24 .057 7 102 . 59 50 .06 6 1.40 .01 .05 1 37 3 49 1 2+00E 2+25N 17 550 3.65 9 5 ND 36 5 3 58 .38 .074 12 94 .87 69 .08 2 1.16 .01 .06 1 2 56 13 105 .1 51 4 1 1 15 445 3.87 11 60 .26 .043 16 97 1.03 71 7 1.61 .01 2+00E 2+00N 3 63 151 .5 58 5 MB 7 34 2 2 2 .12 .08 1 8 4 3707 4.25 77 178 3 1.36 .05 3 2+00E 1+75N 59 23 335 1.2 70 16 5 5 3 24 17 2 2 51 .13 .076 16 .49 .04 .01 1 9 ND 2+00E 1+50N 56 101 .2 52 14 362 3.56 8 5 ND 5 33 2 2 65 .30 .038 12 96 .73 62 .09 9 1.04 .01 .04 .1 185 3 11 2 .95 19 541 5.12 17 7 23 2 2 58 .23 .056 11 88 .60 64 .06 3 .01 .06 1 2+00E 1+25N 93 15 162 .1 70 19 ND 4 2 R 2+00E 1+00N 73 89 .2 53 15 487 3.31 9 5 ND 5 31 2 2 51 .38 .080 12 58 .53 58 .07 14 . 69 .01 .07 1 4 4 6 -1 3 69 .27 .048 11 96 .71 104 3 1.15 .01 .09 7 2+00E 0+75N 3. 52 19 101 .5 40 15 508 3.62 13 6 ND 3 32 2 .07 1 1 22 2+00E 0+50N 68 12 105 .3 47 19 906 3.92 10 5 ND 2 34 2 -2 62 .32 .060 11 94 .76 - 93 .06 2 1.19 .01 .10 1 2 1 27 36 17 38 20 58 .43 .084 38 .86 177 .08 32 1.63 .06 .12 11 50 STD C/AU-S 18 38 132 7.1 68 1022 3.86 7 50 19 16 61 -60

1

C

(

0

ſ

Ċ

(

(

€

(

(

(

C

€

(

C.

6.11 D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260 Page 3 SAMPLE# 10 CU PB ZN AÐ · NE CD **HN** FE AS н Ali TH SR SB BI V CA P LA CR 116 BA TI AL CD 8 NA N. AUS PPM PPN PPN PPM PPN PPN PPM PPN PPN PPN PPN PPM PPH PPN 1 7 PPN PPH X PPN Z z PPH 7 PPN PPN PPN 7 7 PPN 228 2+00E 0+25N 20 701 4.21 .42 .051 .99 5 54 6 107 .7 54 12 5 NÖ 3 39 2 2 75 9 136 105 .09 9 1.49 .02 .08 1 190 1 2+00E 0+00N 97 1.0 59 19 907 3.93 7 5 ND 3 2 2 69 . 49 11 115 .80 .02 5 76 13 37 .065 105 .06 10 1.40 .11 11 1 1 2+00E 0+25S 66 98 1.3 45 9 200 2.92 9 5 ND 40 2 2 64 .52 .058 16 104 .71 112 .05 2 1.39 .01 .08 4 8 1 1 1 2 2+00E 0+50S 57 13 175 2.28 49 .054 .73 71 13 156 1.2 5 5 NÐ 1 37 2 2 .46 16 112 133 .07 2 1.51 4 3 .01 .10 1 2 2+00E 0+75S 89 27 12 3 2 68 .22 .054 15 73 .44 4 -44 9 1.2 8 310 4,94 5 ND 26 3 2 40 .09 2 1.10 .01 .04 1 4 .77 121 .07 2+00E 1+00S 5 78 5 99 1.0 50 17 745 4.32 8 5 2 37 2 2 74 .44 .061 11 111 3 1.52 .01 .11 1 3 617 3.83 68 11 .70 2+00E 1+255 4 62 7 80 .6 44 16 7 5 ND 1 38 3 2 .44 .055 95 96 .06 2 1.36 .01 .09 1 1 1 2+00E 1+50S 23 308 3,04 5 80 .31 8 .33 94 4 36 2 .1 8 ND 31 2 2 .042 86 .12 . 67 .01 .03 60 4 1 1 6 1 4 2+00E 1+75S 4 96 5 57 16 505 3.96 9 5 ND 4 39 6 2 63 .48 .069 13 87 .85 92 .10 4 1.34 .01 .09 88 .1 1 1 10 2 57 .056 13 .63 46 2+00E 2+00S 3 45 5 68 .1 33 12 342 3.24 4 5 ND 41 2 .40 67 .09 2 1.03 .01 .05 1 11 1 1 80 .09 2+00E 2+25S 54 39 12 375 3.63 2 2 64 .41 .046 15 84 .74 2 1.30 .01 .06 2 5 5 83 .2 -5 5 ND 2 41 3 1 22 2 70 12 87 2+00E 2+50S 5 100 2 103 .2 64 516 4.29 6 5 ND 3 39 1 2 .48 .063 130 1:06 .10 2 1.56 .01 .07 1 92 2 2 80 .52 .071 13 95 .98 2+00E 2+75S 4 72 2 100 .6 54 17 621 4.56 5 5 ND 3 43 1 113 .08 9 1.41 .02 .11 1 38 578 3.87 8 5 ND 39 2 2 71 .40 .052 12 93 .75 98 .08 2 1.39 .01 .08 16 2+00E 3+00S 4 60 14 81 .3 43 16 1 1 1 13 .085 12 116 .90 128 21 5 ND 2 2 69 .60 .06 2 1.59 .01 .12 2+50E 0+00 5 100 7 118 .7 63 1018 4.21 1 41 1 1 4 25 .05 .84 .04 15 12 28 .36 .074 31 31 .48 2 .01 3+00E 3+00N 82 13 177 1.2 69 18 491 3.65 3 5 25 2 2 1 ٨ 5 NÐ 2 2 76 .10 .079 7 128 1.48 49 .11 7 2.26 .01 .04 3 3+00E 2+75N 5 -34 11 184 .3 76 16 465 6.68 2 1 10 1 34 35 .27 30 390 95 19 .958 11.67 3 5 ND 6 10 2 2 .08 .175 11 .04 6 1.11 .01 .03 1 15 3+00E 2+50N 22 126 35 3.1 1 7 5 ND 2 2 2 34 .135 10 41 .26 76 .03 11 1.39 .01 .03 1 5 3+00E 2+25N 25 105 31 383 1.1 98 18 721 10.04 10 1 .06 53 .134 57 .40 40 .07 2 1.94 .02 2 3+00E 2+00N 397 1.5 82 19 511 13.75 4 5 ND 6 7 2 2 2 .03 7 .01 3 24 86 48 50 5 2.10 .02 2 .05 .139 9 62 .29 .10 .01 1 3+00E 1+75N 19 63 27 257 2.2 64 18 584 8.90 8 5 M q 2 2 53 .22 33 .02 2 112 18 532 11.38 7 5 ND 3 2 46 .04 .167 9 36 .04 8 1.27 .01 4 3+00E 1+50N 34 113 41 461 1.8 8 2 4 2 2 32 .07 16 49 .38 40 .02 5 2.30 .01 .03 10 399 386 9.28 5 ND 8 11 .118 1 3+00E 1+25N 22 170 44 1.3 81 15 6 1 54 11 42 .38 50 2 1.21 .03 3+00E 1+00N 14 53 14 180 1.1 41 7 343 6.04 2 5 NÐ 4 18 1 2 2 .10 .075 .06 .01 1 1 5 2 43 .087 9 60 .25 35 .08 10 1.40 .01 .02 1 180 12 3 MS 3 11 2 .09 3+00E 0+75N 11 51 17 205 1.4 44 360 6.01 1 .10 .194 .03 14 13 774 7.22 2 2 59 10 65 .33 52 .05 11 1.21 .01 3 3+00E 0+50N 25 231 44 5 5 14 16 46 1.6 6 M -3 46 15 .36 64 .03 3 1.15 .01 .04 5 492 5.40 17 2 2 .082 44 3+00E 0+25N 13 66 29 314 1.2 47 12 7 5 ND 4 .14 1 72 17 .85 137 .08 .01 4 3+00E 0+00N 92 98 61 23 1059 4,30 13 5 MÐ 1 43 2 2 .43 .048 105 8 1.60 .11 1 7 18 .1 1 3 9 5 NÐ 5 42 2 2 67 .39 .044 15 110 1.05 69 .13 2 1.61 .01 .06 1 3+00E 0+25S 2 56 13 202 .4 53 21 459 3.60 1 73 .33 .034 11 102 . 68 101 2 1.46 .01 .07 1 32 3+00E 0+505 42 17 605 3.96 7 5 2 39 2 2 .11 4 54 14 107 .1 ND. .37 .052 10 105 .78 84 .08 10 1.41 .02 .10 1 17 3+00E 0+75S 18 595 4.08 38 2 2 74 3 -74 14 102 .1 45 10 5 ND 1 1 13 .37 2 .2 5 2 2 64 .30 .052 70 .08 , 92 .01 .04 1 10 ND 29 66 3+00E 1+00S ۵ 28 13 82 .4 21 7 292 4.47 1 1 430 3.71 5 ND 33 2 2 89 .23 . 044 10 90 .37 60 .13 6 .92 .01 .05 1 -220 3+00E 1+25S 26 12 20 8 5 1 1 3 61 .3 2 95 .041 7 105 .90 115 .17 11 1.37 .01 .05 2 8 477 11 ND 36 2 2 .36 3+00E 1+50S 4 55 15 106 .6 34 17 5.51 5 1 70 7 87 1.02 74 .17 13 2.31 .01 .14 1 1 3+00E 1+75S 3 80 4 73 .9 32 15 422 4.18 2 5 NÐ 5 28 5 2 3 .43 .047 78 .043 12 149 .97 71 .10 9 1.90 .02 .09 1 3+00E 2+00S 66 7 110 .4 49 21 810 4,65 16 . 5 NĐ 3 33 1 2 2 .26 1 -4 52 38 12 39 39 19 18 21 60 .47 .086 60 .87 178 .08 37 1.83 .06 .13 STD C/AU-S. 19 62 42 132 7.2 68 28 1049 3.96 19 . 7 51



f

r.

f

(

í

Ċ

( )

(

ſ

•

(

(

(

(\_\_\_\_\_

C

6

C

D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260

•																																**	
SAMPLEN	HO Pph	CU PPN	РВ Ргп	ZN PPN	AG PPM	NI PPM	CO PPN	: AN PPR	FE X	AS PPM	U PPN	AU PP <del>N</del>	TH PP <del>N</del>	SR PPN	CD PPM	SB PPh	BI PPN	V PPN	CA Z	P 2	LA PPN	CR PPH	HG 7	BA PPM	TI Z	B PPN	AL Z	NA Z	K Z	N PPN	AU\$		
3+00E 2+258	4	52	2	94	.3	42	14	548	3.53	8	6	ND	5	39	1	2	2	60	.44	.053	10	95	.78	108	.07	2	1.15	.01	.08	1	24		
3+00E 2+505	3	35	2	86	.3	32	14	380	4.55	8	5	ND	4	27	1	2	2	73	.33	.056	- 6	94	.46	71	.07	7	. 82	.01	.04	1	1		
3+00E 2+75S	3	24	2	65	.8	25	7	222	3.97	5	5	ND	8	29	2	2	2	69	.28	.049	8	82	.48	57	.07	. 3	.88	.01	.04	2	1		
3+00E 3+005	2	46	4	75	.9	38	12	428	3.26	3	5	ND	6	. 44	- 3	2	- 2	54	.46	.063	13	67	.71 -	66	.09	- 4	.96	.02	.08	2	23		
3+50E 0+00	9	148	22	441	1.2	<b>98</b>	19	614	7.01	11	6	ND	17	19	5	2	2	33	.18	.076	19	58	.55	78	.03	2	1.76	.01	.05	1 •••	26		
4+00E 3+00N	8	64	18	157	.7	- 44	16	905	5.15	2	5.	NÐ	7	12	1	2	2	29	.09	.062	24	38	.33	25	.03	6	1.15	.01	.02	1	1		
4+00E 2+75N	18	39	19	136	.4	39	13	580	6.78	- 3	5	NĎ	- 6	12	1	2	2	50	.12	.055	9	44	.24	26	.08	2	.79	.01	.03	2	25		
4+00E 2+50N	15	70	20	201	.9	61	12	854	6.94	4	5	ND	4:	12	1	2	2	46	.08	.092	14	38	14	64	.04	. 4	. 88	.01	.03	í	18		
4+00E 2+25N	14	150	34	331	.8	111	20	837	9.82	7	5	NÐ	5	11	2	2	2	23	.12	.152	10	48	.43	44	.02	. 3	1.67	.01	.03	1	580		
4+00E 2+00N	12	60	19	172	2.2	54	10	353	4.96	5	5	ND	4	12	3	2	2	52	.07	.136	11	24	.26	32	.05	3	-61	.01	.04	1	4.		
4+00E 1+75N	97	130	240	526	3.9	207	14	440	10.19	2	5	ND	5	6	2	2	3	27	.05	.179	14	15	.04	27	.01	2	.86	.01	.04	1	94		
4+00E 1+50N	15	67	16	299	2.8	29	16	905	8.41	5	5	ND	3	- <b>4</b>	1	2	2	35	.02	. 183	21	9	.06	43	.01	2	.42	.01	.02	- 1	1		
4+00E 1+25N	33	- 29	31	186	2.0	43	6	321	4.90	3	5	ND	6	4	1	2	2	34	.02	.122	8	17	.07	24	.03	9	.51	.01	.02	2	1		
4+00E 1+00N	10	40	14	116	3.1	36	- 11	1258	3.29	4	5	ND	3	6	2	2	2	29	.02	.049	13	21	.07	61	.02	2	.65	.01	.01	1	5		
STD C/AU-S	19	16	37	134	7.0	- 88	-27-	1054	4.10	- 38		7-	-40-	49-					46-	.085	- 38	60	91	-186-	-80-	- 37	1.73	.06-	13-				
ALAAC ALTER	10			204	1 F	48	9	541	E 14		5	MD	8	10		7	2	44	.13	.128	13	48	.30	74	.04	3	2.23	.01	.05	. 1.	1		
4+00E 0+75N	12 14	56 64	14 24	204 211	1.5	59	-	1831		5	5	ND ND		19 12	1	3 2	2	49	.06	.120	13	40	.22	55	.03	2	.71	.01	.03	1			
4+00E 0+50N	-			324	3.9 2.0	37 73	16		6.43	9 9					1	2	2			.098	17	65	.49	55 65	.05		1.26	.01	.05	1	1		
4+00E 0+25N	12	114	45				15	377	7.04		6	20	8	23	2	2		46	.23		9	- 80	.65	63 95	.03			.01	.05	1	4		
4+00E 0+00	5	57	11	140	1.3	41	12	304	5.49	. 6	° 5 5	ND ND	6	32 40		2	2	64 74	.24	.065		70	.33	131	.08		1.67	.01	.03	2			
4+00E 0+255	10	25	13	66	1.9	22	- 11	240	3.92	•			· •		1		-	. 74	.37	•033	- 14						1.15				1		
4+00E 0+50S	.1	62	4	91	.7	48	8	151	1.85	12	5	ND	3	- 39	· 1	2	2	67	.46	.051	10	90	.78	138	.08	-	1.18	.02	.09	1	610		
4+00E 0+75S	- 3	50	9	. 92	.2	36	17	374	3.42	11	5	ND	4	39	1	2	2	59	.36	.050	14	75	.85	70	.09		1.39	.01	.08	1	16		
4+00E 1+00S	3	42	14	73	.8	39	15	368	3.97	11	5	ND	- 4	33	1	2	2	54	.34	.051	9	78	.58	46	.07	2	.99	.01	.05	1	12		
4+00E 1+255	4	56	- 14	104	1.1	41	15	715	4.38	9	5	ND	5	35	1	2	2	72	•36	.070	15	89	.57	106	.09	2	.98	.01	.06	1	9		
4+00E 1+505	2	39	2	67	1.3	34	11	284	4.01	6	5	ND	4	30	1	2	2	59	.35	.051	8	81	.48	40	.08	2	.85	.01	.04	1	5		
4+00E 1+755	5	72	5	96	1.4	43	19	933	4.65	4	5	ND	3	- 34	1	2	2	64 -	.35	.066	13	102	. 68	117	.08	2	1.41	.01	.09	1	7		
4+00E 2+00S	4	42	9	69	7	30	12	372	5.68	. 8	5	ND	- 24	29	1	2	2	86	.29	.039	8	115	.50	64	.12	- 4	1.10	.01	04	1	<del>98</del>		
4+00E 2+25S	6	48	- 7	78	1.5	32	12	500	4.46	4	5	ND	5	35	1	3	2	75	.31	.036	11	85	.67	125	.13	3	1.32	.01	.08	1	2		
4+00E 2+505	3	63	2	82	.4	41	13	395	3.97	9	5	ND	· 4	39	1	3	2	61	.34	.050	15	80	.78	89	.10	2	1.40	.01	.08	1	5		
4+00E 2+755	4	47	12	105	.4	39	14	517		7	5	ND	3	41	1	2	2	74	.48	.061	11	98	.75	155	.09	2	1.30	.01	.07	1	- 4		
4+00E 3+00S	5	71	12	92	.8	44	18	721		7	5	ND	3	39	2	2	2	68	.37	.049	14	106	.80	119	.09	2	1.51	.01	.10	. 1	32		
4+50E 0+00S	2	7	11	26	1.0	· · 6	2	77	1.02	2	5	ND	2	26	1	2	2	35	.11	.023	13	25	.11	73	.07	2	.65	.01	.03	4.	-11		
5+00E 1+50N	8	70	7	127	.1	53	9	225	7.12	. 6.	5	ND	6	17	1	. 2	2	- 44	.10	.074	16	63	.53	95	.06			.01	.04	<b>1</b> -	2		
5+00E 1+25N	15	70	26	338	.6	30	16	906	10.87	3	5	ND	3	7	· 1	2	2	23	.04	.107	9	12	. 08	óć	.01	2	.64	.01	.02	1	1		сŤ.
5+00E 1+00N	20	46	5	195	.4	31	. <b>8</b> 1	113	3.69	2	5	ND	2	6	1	2	2	37	.03	.038	23	9	.02	33	.02	2	.16	.01	.02	1	1		
5+00E 0+75N	24	120	32	530	3.4	109	25	1150	11.41	10	5	ND	3	14	2	2	2	33	.11	.153	13	40	.31	49	.02	2	1.28	.01	.03	1	8	からつき	
5+00E 0+50N	23	127	39	526	2.0	89	19		12.09	11	5	ND	5	13	3	4	2	40	.08	.092	16	52	.33	56	.05		1.67	.01	.04	1.1	35		
			÷.							- <b>-</b> -			- <b>-</b>		-		-	••												19 L.			25

Grid 1

Page 4

(

1

t

(\_\_

D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260 SAMPLE# 80 CU PB ZN A6 NI CO MN FE AS U AU TH SR CD SÐ ÐI ۷ CA ٩ LA CR MG BA TI ĸ B AL NA N AUI PPM PPH PPB <u>PPB</u> 1111 PPN 22h PPH ž PPH PPN PPM PPN PPH PPh PPN PPN PPM ž 2 PPĦ PPM z PPM z PPM ï Ż Z PPH PPB 5+00E 0+25N 261 3.36 9 35 16 109 .1 23 6 2 -5 5 11 3 2 2 42 .06 .036 14 27 .15 31 .04 4 .58 .01 .02 1 1 5+00E 0+00 3 26 19 7 321 25 2 2 17 .94 1.4 4.24 3 6 ND 4 2 64 .16 .055 9 66 .39 69 .11 9 1.23 .01 .04 1 1 5+00E 0+255 3 38 122 .8 39 9 282 5 32 2 2 54 .29 2 4.16 ND 4 .057 85 .50 89 .01 - 6 3 10 .07 8 1.51 .05 1 1 5+00E 0+50S 2.0 744 33 10 76 28 108 50 28 5.35 15 5 NÐ 3 2 2 2 87 .36 .061 20 138 .88 119 .08 2 2.03 .09 .01 1 1 5+00E 0+75S 188 32 3 74 13 76 33 8 2.23 5 ND 2 .25 77 .6 6 1 ŧ 2 65 .024 13 .46 107 .10 2 1.08 .01 .05 3 1 5+00E 1+00S 74 53 765 123 4 16 92 .4 16 3.57 5 5 43 3 2 2 69 . 49 .043 14 .84 126 :10 3 1.51 .01 .10 1 1 5+00E 1+25S 2 71 12 .1 67 17 466 2.88 5 2 44 2 59 .54 134 1.05 123 115 6 NÐ 1 2 .053 10 .09 2 1.60 .01 .10 1 1 5+00E 1+50S 2 81 7 118 67 14 349 3.12 7 ND 2 40 2 . 48 .058 138 .95 131 2 1.65 .4 64 13 .09 .01 6 1 3 .11 1 2 5+00E 1+75S 5 100 13 122 .1 60 18 828 4.05 12 5 ND 7 34 1 2 2 54 .42 .070 18 67 .73 73 .08 7 1.10 .01 .08 55 1 5+00E 2+00S 1 68 13 88 51 13 418 3.62 5 NÐ 3 36 2 3 2 68 .41 .053 10 119 . 90 75 .08 7. 1.45 .09 .6 6 .01 1 43 5+00E 2+25S 2 63 49 15 479 3.29 40 3 .53 88 9 1.01 6 80 .1 7 -5 ND 4 2 61 .064 9 .69 86 .07 .01 .09 1 28 5+00E 2+50S 50 5 NÐ 2 41 2 70 .52 .061 87 .70 .93 1 61 8 81 .1 :14 466 3.49 8 2 2 9 .08 .01 .08 1 -3 5+00E 2+75S 92 132 82 23 709 4.27 12 5 ND 3 38 77 .35 163 2 13 .1 1 4 4 .054 10 1.31 90 .11 4 2.04 .01 .11 1 3 44 .53 5+00E 3+00S 104 11 141 .5 87 22 703 4.21 17 -5 ND 4 1 2 2 78 .063 10 159 1.28 192 .10 6 1.91 .01 1 .13 1 1 5+50E 0+00S 14 202 22 276 5.9 143 27 2308 6.28 13 5 ND) 10 35 . 2 2 57 .50 .110 115 167 .74 180 .04 2 2.42 .01 .16 22 1 6+00E 2+50N 53 . 35 375 2.58 22 .38 .074 17 39 .58 11 .87 12 3 11 103 .1 9 -5 M 7 4 2 2 .34 .48 .06 .01 .09 1 4 6+00E 2+25N 8 98 27 238 .9 85 21 751 4.31 5 ND 13 19 2 3 2 30 .26 .065 61 37 .65 42 .05 2 1.15 620 2 .01 .04 1 6+00E 2+00N 5 115 45 202 1.7 97 20 788 4.57 4 5 ND 17 18 3 2 2 25 .21 .075 86 36 .58 56 .03 2 1.30 .01 .04 13 1 6+00E 1+75N 39 617 7.03 3 5 ND 5 15 2 3 51 .10 19 55 .44 2 1.44 4 45 23 123 1.5 11 2 ,122 110 .10 .01 .06 1 1 6+00E 1+50N 71 21 196 2.5 59 11 246 5.07 2 5 ND 12 14 4 2 2 -31 .11 .070 19 48 .57 63 .04 2 2.93 .01 .03 1 12 4 6+00E 1+25N 39 219 4.31 36 20 22 40 .14 .073 14 54 .46 70 .06 40 1.20 .01 .08 2 3 3 - 39 5 132 2.5 8 2 MĒ 16 5 2 6+00E 1+00N 27 9 250 5.14 8 ND 29 5 2 2 73 .26 .135 10 65 .49 70 .07 2 1.28 .01 .06 55 41 101 .1 3 6 1 1 6 6+00E 0+75N 35 11 .3 27 8 205 3.70 5 ND 3 25 1 2 2 68 .19 .073 10 57 .38 33 .08 2 .85 .01 .04 1 1 1 107 3 27 2862 12 5 30 9 2 2 56 .37 .128 25 139 .48 245 2 2.06 7 6+00E 0+50N 22 121 35 292 6.8 97 7.50 ND 3 .04 .01 .14 1 6+00E 0+25N 32 .129 38 324 100 13 704 7.64 4 5 ND 5 14 2 2 2 40 .10 .111 15 56 .36 55 .03 2 1.20 .01 .07 1 12 2.0 .23 6+00E 0+00 20 116 29 318 1.8 95 21 894 6.26 10 5 23 5 2 2 42 .081 22 65 .51 76 .04 9 1.37 .01 .07 1 -14 M 6 33 2 73 .35 25 159 .70 2 2.18 6+00E 0+25S 165 ...3 74 25 2487 5.35 16 5 NØ 4 1 2 .080 164 .06 .01 .15 1 1 8 13 163 28 3 2 51 .26 18 3 1.57 .01 .08 5 6+00E 0+505 5 81 11 106 1.0 42 10 411 3.35 7 6 ND 3 4 .067 100 .64 101 .05 1 69 .39 .76 4 1.48 .01 6+00E 0+755 3 751 3.84 12 5 ND 5 38 3 2 2 .051 13 119 104 .09 .10 1 66 17 109 .6 48 16 1 77 .54 47 3 1.21 6+00E 1+005 4 55 11 102 .1 30 11 465 4.62 5 ND 1 36 1 2 2 .20 .035 8 75 .14 .01 .06 1 35 6 6+00E 1+25S 5 83 16 47 18 810 4.00 14 5 38 2 2 2 72 .32 .036 15 121 .71 89 .10 2 1.53 .01 .09 1 116 .1 3 1 32 3 60 .33 .063 16 99 .38 118 .06 2 1.34 .01 .08 6+00E 1+50S 23 110 254 3.1 76 20 1150 6.01 12 5 ND 5 3 2 1-8 34 729 33 2 50 .27 ,041 20 .57 90 3 2.03 .01 .09 15 6+00E 1+75S 21 123 26 247 2.5 91 25 5.80 3 5 ND 5 3 2 110 .07 1 36 3 2 53 .40 18 81 .68 118 .07 8 1.17 .0Ì .08 6+00E 2+00S 104 17 161 69 17 1318 4.73 13 5 ND 2 .067 1 8 14 .1 6 6+00E 2+25S 11 34 2 73 .29 .049 7 122 .75 63 .10 3 1.23 .01 .10 1 2 -54 9 67 .1 44 10 294 3.45 5 ME 3 1 2 1 6+00E 2+505 853 2 69 .55 .054 12 141 1.00 157 .08 2 1.72 .02 .07 -**f** -19 3 89 18 107 .1 69 21 3.72 12 5 ND 2 -44 1 2 37 18 23 38 STD C/AU-S 19 61 38 128 7.0 67 27 1025 3.79 19 8 39 50 22 59 .48 .083 61 .87 177 .08 38 1.76 .06 .13 13 52

#### Grid 1 Page 5

í

1

ί.

1

(

1

(

(

C

€

(

C

(

(

(

C

€

€.

D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260

SAMPLEN	NO PPN	CU PPN	PB PPM	ZN PPN	AG PPM	NI PPN	CO PPM	MN PPH	FE	AS PPN	U PP <del>N</del>	AU Ppr	TH PPN	SR PPM	CD PPH	SB PPM	BI PPN	V PPM	CA X	P X	LA	CR PPN	MG 7	BA PYM	TI Z	B PPN	AL Z	NA Z	K Z	N PPN	aut Ppb	
6+00E 2+75S	3	81	7	91	.3	52	17	533	3.51	12	5	ND	. 1	37	1	3	3	63	.46	.060	12	125	.80	111	.08		1.54	.01	.08	1	95	
6+00E 3+00S	2	53	12	85	.1	- 39	19	1393	4.06	11	5	ND.	1	- 30	1	2	2	69	.26	.080	11	107	.70	81	.07		1.40	.01	.08	1	1	
6+50E 0+00	11	44	15	174	1.2	41	11	858	4.76	8	7	ND	1	23	1	2	2	56	.17	.059	13	64 -	.38	102	.06		1.28	.01	.05	1	. 1	
7+00E 2+00N	15	96	27	212	.1	-71	14	613	5.59	ie . <b>4</b>	5	ND	- 4	17	1	2	2	26	.19	.105	26	30	.41	54	.03	6	.95	.01	.05 .03	1	6 · 7	
7+00E 1+75N	20	80	16	258	1.6	68	12	409	6.88	5	5	ND	5	21	3	2	2	26	.31	.176	- 19	36	.33	64	.02	· 2	1.57	.01	•00	. 1		
7+00E 1+50N	10	65	11	158	1.9	52	13	513	5.98	3	5	ND	4.	13	3	2	2	31	.10	.158	18	36	.34	56	.03		1.25	.01	.03	1	6	
7+00E 1+25N	3	49	19	108	2.7	33	20	2897	6.33	2	5 :	ND	4	10	. 1	2	2	32	.05	.201	22	30	.29	70	.02		1.18	.01	.04	1	4	
7+00E 1+00N	4	28	4	85	1.3	21	6	304	4.71	3	5	ND	1	16	. 1	2	2	42	.09	.066	13	49	.26	57	.06	. 8	1.06	.01	.03	1	1.	
7+00E 0+75N	6	37	13	143	1.3	-32	8	388	6.14	7	5	ND	2	17	1	2	2	45	.14	.123	12	64	-43	63	.06		1.34	.01	.04	1	9.	
7+00E 0+50N	2	47	2	99	.7	41	12	291	3.53	4	5	ND	2	34	1	2	2	51	. 32	.054	13	73	.57	81	.08	2	1.45	.01	.06	1	- <b>-</b>	
7+00E 0+25N	19	59	31	277	4.0	60	11	685	6.40	7	5	ND	4	15	- 1	2	- 2	43	.08	.079	14	49	.30	76	<b>.</b> 04 ·	2	1.41	.01	.04	1	1.	
7+00E 0+00	14	68	33	275	1.6	65	22	1213	12.31	7	. 5	ND	7	10		2	2	22	.13	.194	24	19	.09	- 37	.01	- 4	1.13	.01	.04	1	2	
7+00E 0+25S	32	62	23	170	2.2	55	- 7	135	4.19	- 3	- 5	ND	. 3 .	16	2	2	2	30	.10	.062	13	21	.08	81	.01	8	.41	.01	.04	<b>1</b> .	3	
7+00E 0+50S	13	47	19	110	2.3	31	8	412	3.80	- 5	5	ND	1	18	1	2	2	51	.10	.056	13	45	.14	40	.05	2	.85	.01	.03	1	25	
7+00E 0+75S	7	33	6	161	1.2	. 35	14	643	3.99	. 3	6	ND	3	34	1	2	2	59	.31	.045	12	81	.53	52	.07	13	1.11	.01	.06	1	3	
7+00E 1+00S	4	49	12	m	.6	34	9	320	4.03	7	5	ND	2	24	2	2	2	49	.20	.062	. 14	53	.35	190	.04	2	.97	.01	.04	2	· 4 5	
7+00E 1+25S	5	45	17	121	1.6	28	12	926	4.70	5	5	NÐ	3	22	1	2	2	68	19	.088	13	60	.35	104	.09	_	1.04	.01	.06	1	5	
7+00E 1+50S	. 4	35	22	125	1.0	29	12	515	4.86	6	5	ND	1	24	2	2	2	80	.19	.090	9	72	.31	103	.09	5	.84	.01	.05 .04	1	5	
7+00E 1+75S	6	50	16	187	1.5	41	16	511	5.68	11	5	ND	- 1	27	1	2	2	65	.32	.091	7	89	.55	91	.07	· 4	1.18	.01 .01	.05	2	·	
7+00E 2+00S	7	93	16	173	2.6	61	15	484	4.69	8	5	ND	4	27	2	2	2	32	.27	.089	15	53	.47	115	.03		1.00	. VI	• • •	-		
7+00E 2+25S	6	53	26	172	2.1	44	13	1005	5.10	- 8	6	ND	- 3	27	2	2	2	55	.21	.045	11	73	.40	91	.06	-	1.34	.01	.05	1	8	
7+00E 2+50S	10	50	18	81	2.4	21	7	233	2.90	4	5	ND	2	27	1	2	2	44	.29	.048	14	56	.26	55	.07	2	.80	.01	.05	1	7	
7+00E 2+75S	÷ 4	110	11	113	.4	57	17	617	4.46	26	5	ND	3	- 31	1	3	2	78	.24	.040	11	132	.69	103	.11	10	1.93	.01	.10	1	18	
7+00E 3+005	3	103	6	102	6	63	17	574	3.83	17	5	ND	2	41.	1	2	2	68	.42	.066	14	104	.83	152 28	.08 .02	-2	1.53	.01	.12 .03		2	
7+50E 0+00	16	31	22	139	.9	30	6	194	4.20	3	5	ND	5	6	· 1.	2	2	21	.03	.079	21	14	.09	28	. 42	'	.11	101	. VJ		2	
8+00E 1+75N	18	54	21	132	.9	34	10	. 696	6.41	8	5	ND	3	10	1.	2	3	.24	.09	.169	15	27	.23	49	.02	14	.97	.01	.04	. 1	4	
8+00E 1+50N	19	53	19	149	6	43	9.	490	6.00	. 7	5	ND	1	9	1	2	2	30	.05	.109	15	27	.18	33	.01	2	.91	.01	.03	1		
8+00E 1+25M	38	100	- 48	377	1.8	114	21	1098	7.57	6	5	ND	7	15	. 1	2	2	34	.11	.174	- 17	42	.38	104	.04	3	1.34	.01		. 1	8	
8+00E 1+00N	8	79	21	228	1.9	72	11	400	5.36	6	5	ND	9	19	. 1	2	2	30	.17	.082	17	- 44	.52	74	.05		1.54	.01	.04	1	3	
8+00E 0+75N	9	46	19	200	1.9	42	-11	380	5.73	7	5	NÐ	5.	15	1	3.	2	41	.10	.128	16	52	.44	67	.07	14	1.65	.01	• • • •	<b>1</b> .		
8+00E 0+50N	4	26	14	116	1.5	21	8	1036	4.44	3	5	ND	4	17	2	2	2	54	.08	.145	13	51 17	.27 .08	94 27	.07	2	1.11	.01	.05	1	2	
8+00E 0+25N	12	32	11	114	1.5	41	5	197	2.51	2	5	ND	3	13	3	2	2	. 29 -	.07	.056	14			46	.05	- 6	.96	.01	.04	1	9	
8+00E 0+00	4	28	11	87	1.3	29	. 5	142	3.88	4	5	ND	6	13	1	2	2	-47	.07	.067	15	27 45	.28 .24	64	.03	13	.70	.01	.05	1	3	
8+00E 0+255	10	77	- 28	195	2.5	68	9	594	6.02	् <u>भ</u> 7	5	ND	2	14	2	5	2	36	.13	.090	12 15	40	.24	47	.03	. 6	.81	.01	.03	- i	6	
8+00E 0+50S	12	68	. 16 .	282	7.6	69	9	226	3.59	1	3	ND	3	12	2	2	4	17	.14	.066												
8+00E 0+75S	3	36	17	89	1.3	30	8	361	3.53	9	- 5	ND	4	- 34	1	2	2	- 51	. 30	.065	10	61	.50	92	.07	2		.01	.05	1	3	
STD C/AU-S	18	,62	39	132	7.3	68	28	1023	3.88	39	19	7	38	50	18	16	20	58	.47	.084	38	59	.86	177	.08	36	1.79	.06	.13	13	51	

Grid 1 Page 6

1

ľ

(

£

(

6

€

Ć

0

Ċ

SAMPLE# NÐ CU PB ZN AG NI 60 MN FE AS U AU TH SR CD SB BI CA ρ LA CR MG BA TI U 41 ĸ AUL я . PPN PPH PPN PPM PPH PPM PPH PPh 7 PPN PPH PPH PPH PPN PPN 7 PPH PPN PPN PPN PPN PPN 7 PPN z 1 7 PPM PPB 7 7 8+00E 1+00S 457 3.20 1 71 9 -84 .2 50 13 .38 .53 .98 7 5 ND 6 44 3 2 50 .059 14 63 49 .09 8 .01 .05 1 1 8+00E 1+25S 3 42 19 146 32 13 648 4.81 1.0 8 5 ND 3 25 2 2 67 .19 .118 10 85 .31 171 .06 7 .90 .01 .04 2 1 1 8+00E 1+50S 2 34 185 35 14 665 4.30 11 5 3 27 .23 .080 3 2.0 ND 2 66 10 .41 65 .07 2 1.20 .01 .05 2 3 4 91 15 8+00E 1+75S 3 74 15 128 54 13 539 4.04 5 5 NÐ 5 37 2 2 57 .33 .066 14 .59 80 9 1.17 .6 2 81 .08 .01 .08 1 5 8+00E 2+00S 45 7 101 19 584 3.61 7 5 ND 48 2 2 59 11 72 .53 71 2 .4 36 4 4 .40 .117 .08 4 1.03 .01 .07 1 1 8+00E 2+25S 3 36 12 -95 31 11 303 4.16 77 7 1.41 .8 6 -5 3 37 2 2 .26 .035 10 100 .54 65 .13 .01 .06 2 3 1 8+00E 2+50S 9 76 19 107 .6 49 21 775 4.09 8 5 NÐ -4 41 1 6 3 63 .32 .046 13 99 .61 100 .09 2 1.31 .01 .08 1 1 8+00E 2+75S 7 45 14 80 .8 27 12 643 2.93 8 5 NÐ 4 57 2 5 2 60 .48 .051 10 79 .45 130 .08 18 1.03 .01 .07 2 1 8+00E 3+00S 109 9 59 19 596 4.15 4 5 NÐ 67 2 77 .59 12 .81 15 1.59 1 108 .1 6 1 3 .070 96 166 .14 .02 .19 1 1 34 15 5 NÐ 15 .30 59 .05 8+50E 0+00 2 112 191 1.2 100 890 4.67 5 17 2 30 .11 .054 .04 11 .87 .01 1 4 4 3 36 3 9+00E 1+25N 78 128 308 6.61 5 12 2 23 27 35 30 8 1.30 .01 .03 6 19 .8 49 11 7 2 .11 .081 .31 .02 1 1 6 9+00E 1+00N 85 26 277 .7 79 15 479 6.20 5 12 2 29 23 35 .28 66 .03 6 1.58 .01 .04 31 8 MD . 5 2 .08 .062 1 1 20 19 .25 71 17 1.73 .04 9+00E 0+75N 49 119 36 361 2.1 164 694 7.60 7 5 ND 5 13 2 2 29 .08 .178 36 .02 .01 1 1 6 9+00E 0+50N -34 25 137 2.0 32 7 498 5.65 3 5 ND 11 5 2 52 .05 .150 15 34 .17 81 .05 . 88 .01 .04 1 9 4 5 6 1 9+00E 0+25N 97 150 4.26 54 33 .17 51 12 .82 .01 .03 23 38 8 1.1 31 4 5 NÐ 19 2 2 .10 .064 16 .06 1 1 6 4 4 9+00E 0+00 17 1.31 4 46 128 11 250 7.81 .13 .112 12 83 .30 62 .13 .01 .05 26 1.0 -31 -5 5 NE 6 22 3 3 2 70 1 4 24 .03 34 21 .04 .02 2 .18 .01 1 9+00E 0+25S 2 12 106 .3 39 5 210 2.56 2 5 ND 1 6 3 2 2 .05 .030 9 12 1 9+00E 0+50S 68 132 764 4.53 3 37 70 .30 .061 13 126 .71 168 .07 2 1.64 .01 .10 1 9 4 20 .7 60 19 16 5 ND 5 2 1 25 13 .22 .05 27 23 79 317 3.40 7 5 NÐ 3 2 56 .15 .055 62 49 .08 11 .64 .01 9+00E 0+75S 6 1.6 21 5 5 2 1 10 55 9 .42 89 . 09 6 1.59 .01 .07 1 9+00E 1+00S 6 53 19 143 1.5 45 14 567 5.17 8 5 ND 3 24 2 3 .22 .082 95 61 1 56 6 1.08 9+00E 1+255 34 748 5.33 71 .23 93 .36 .12 .01 .04 1 10 4 6 76 .9 26 15 5 3 30 2 2 2 .043 9 - 6 1 D 633 4.13 62 96 2 1.08 .11 9+00E 1+505 3 108 15 118 .3 63 17 5 ND 46 2 2 2 .45 .073 13 81 .65 .10 .01 1 13 6 6 9+00E 1+75S 58 438 3.98 5 NÐ 3 41 2 2 59 .35 10 84 .52 48 .08 21 1.08 .02 .06 2 18 2 15 105 .7 45 16 6 3 .061 35 11 60 2 .94 .01 .06 1 4 37 10 5 ND 3 2 64 .28 .037 84 .49 .09 9+00E 2+00S 5 18 65 1.4 28 12 438 3.97 4 8 9+00E 2+25S 23 508 3.38 -14 5 MD 3 38 61 . 38 .063 20 191 .57 132 .11 6 1.72 .02 .11 1 20 134 104 5.6 64 14 2 2 2 6 .37 27 9+00E 2+505 -74 128 56 18 601 5.29 14 34 3 73 .053 9 136 .92 89 .14 17 1.69 .01 .09 1 4. 8 2.1 -5 4 3 НĽ 1 9+00E 2+755 17 136 63 21 1219 5.13 8 5 ND 2 27 2 2 53 .21 .071 24 117 .48 91 .05 10 1.62 .01 .08 1 6 9 116 4.1 3 14 2 79 20 .67 127 .07 16 1.73 .01 .10 1 9+00E 3+00S 19 131 1.2 58 27 585 5.87 5 NÐ 38 2 2 2 .36 .065 160 4 11 -84 9+50E 0+00 50 19 146 10 491 6.16 6 5 ND 3 15 2 2 2 49 .06 .066 14 40 .22 44 .07 18 .81 .01 .04 1 - 1 7 1.0 36 22 .071 10 .22 21 .03 9 .54 .01 .02 10+00E 0+75N 10 78 23 163 1.1 44 9 291 4.96 8 5 ND 5 13 4 6 2 .07 28 1 1 10+00E 0+50N 14 15 • 22 .01 .02 1 110 4 33 87 .7 36 234 3.58 10 9 2 58 .03 .057 -14 20 .06 .04 4 8 3 ND 6 2 3 45 .27 44 .05 20 1.03 .01 .03 1 10+00E 0+25N 62 25 165 49 10 441 6.98 ЖÐ 4 16 2 41 .07 .260 12 1 5 1.0 4 5 t 2 29 .131 12 33 .27 44 .03 2 .86 .01 .03 1 1 10+00E 0+00N 6 73 27 212 1.0 63 11 403 6.85 5 5 ND 4 11 4 2 4 .05 .35 67 10+00E 0+25S 4 103 14 202 2.4 99 15 925 4.55 -5 10 ND 4 39 5 2 2 33 . 58 .122 35 86 .03 2 1.07 .01 .04 1 -7 10+00E 0+50S 48 21 110 .8 423 5 ND 2 21 2 2 2 34 .22 .054 16 38 .20 28 .04 11 .62 .01 .04 1. 39 4. 36 9 4.81 6 113 196 17 1033 5.29 23 2 57 .17 .084 17 125 .33 88 .06 2 1.40 .01 : .11 9 10+00E 0+75S .7 . 27 3.5 65 10 5 ND 2 3 2 1 20 39 .81 31 1.67 .05 .13 13 51 7.4 28 1062 3.97 40 52 17 22 60 .44 .097 60 180 ,08 STD C/AU-S 18 64 41 132 71 42 16 8

#### D.D. H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260

# Cill Page 7

Y

ť

(

(

ŧ

C

ť

£

C

ſ

C

C

C

C

C

 $\left( \right)$ 

D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260

																e prove																-
SANPLE#	n0 PPri	CU PPM	PB . PPM	ZN PPM	AG PPM	NI PPN	CO PPM	NN PPN	FE	AS PPn	U PPH	AU PPM	TH PPN	SR PPN	CD PPN	SB PPM	BI PPM	V PPM	CA Z	P	LA PPN	CR PPM	H6 2	BA PPM	TI Z	B PPM	AL Z	NA Z	K Z	W PPN	AUX PPB	
10+00E 1+00S	17	95	33	274	2.5	85	24	1367	7.28	26	5	ND	1	32	1	2	2	46	.47	.099	15	102	.40	79	.02	9	1.30	.01	.05	1	10	
10+00E 1+255	6	67	21	189	3.3	60	11	455	4.78	-14	5	ND	1	43	1	2	2	57	.63	.089		113	.50	112	.05		1.40	.01	.06	i	1	
10+00E 1+50S	4	84	7	98	1.2	49	14	343	4.18	8	5	- ND	3	34	1	2	2	60	.33	.045	10	73	.60	58	.09		1.17	.01	.06	1	2	
10+00E 1+755	8	206	17	117	6.8	70	14	134	3.12	12	5	NÐ	1	28	2	2	2	70	.23	.084	25	148	. 39	107	.07	5	2.24	.01	.07	1	1	
10+00E 2+00S	6	55	29	176	1.3	38	19	738	6.74	19	5	ND	1	23	1.1	2	2	78	.21	.083	7	115	.57	65	.09		1.41	.01	.04	1	1	
						<u>.</u>					_						_															
10+00E 2+25S	8	58	19	131	1.0	36	- 15	775	4.94	11	- 5.	ND	2	23	1	. 2	2	66	.15	.075	12	78	.39	67	.08		1.18	.01	.04	1	3	
10+00E 2+50S	8	69	24	172	3.4	56	22	970	5.50	7	5	ND	. 1	32	1	2	2	53	.30	.067	-11	97	.59	78	.07	24	1.86	.01	.07	1	2	
10+00E 2+75S	10	133	22	281	.8	- 88	24	886 703	4.84	7	5 5	ND		32	1	2	2	56	.32	.069	13	82	.72	. 70	.08		1.67	.01	.07	1	4.	
10+00E 3+00S	44	103 37	59 17	342 76	1.2	110 29	18	438	7.53	12	J 5	ND ND	2	24 25	1	2	2	50 95	.25	.076	11 10	102 77	.47	68 75	.04	6	2.42	.01	.05	1	6	
10+00E 3+25S	•	3/	17	/0	1.1	27	- 11	738	7+21	. *		NU	2	25	. 1	. 4	1	73	•17	.034	10	. 11	.25	- 73	.13	6	. /1	.01	.05	1	1	
10+00E 3+50S	4	63	20	139	1.3	55	18	629	5.38	13	5	ND	2	26	1	2	2	72	.30	.104	8	123	1.02	77	.07	10	1.75	.01	.08	1	8	
10+00E 3+75S	3	37	14	88	1.1	39	14	746	4.47	14	5	ND	- 1	32	· 1	2	2	81	. 39	.055	6	119 -	.73	209	.14	11	1.07	<b>.</b> 01	.06	1	- 1 -	
10+00E 4+00S	4	71	11	115	.6	52	22	865	4.70	18	5	ND	- 2	29	2	2	2	78	.24	.065	13	127	.95	83	.07	12	1.94	.01	.10	1	<u>_</u> +4	
10+00E 4+25S	9	65	15	111	.2	43	.17	747	7.55	: 15	5	NÐ	2	26	. 1	2	5	118	.18	.055	13,	154	.78	58	.17	4	1.78	.01	.09	1.	36	
10+00E 4+50S	9	67	19	148	.5	55	16	558	4.90	8	5	ND	. 3	25	2	2	2	55	.20	.038	16	81	.63	85	.07	8	1.37	.01	.06	1	2	
10+00E 4+75S		70	25	140	.6	81	21	622	4.61	5	5	ND	3	34	1	2	3	59	.34	.045	. 9	88	.87	77	.10	18	1.83	.01	.07	,	4	
10+00E 5+00S	5	42	8	87	1.5	38	10	379	5.30	10	5	NÐ	1	31	÷	2	2	79	.26	.118	. 8	92	.65	45	.08	10	1.40	.01	.06	. 1	39	
10+00E 5+25S	7	62	12	64	.5	35	21		4.26	12	5	ND	2	30	i i	2	2	84	.21	.045	16	107	.47	105	.13		1.19	.01	.05	1	- 1	
10+00E 5+50S	3	32	17	75	.3	26	-13	-531	3.10	- 10 -	5	ND	1	32	1	2	2	67	.26	.056	11	76	.54	97	.07	14	.93	.01	.08	1	62	
10+00E 5+75S	. 6	56	25	92		43	14		4.38	13	5	ND	3	40	1	2	2	67	.32	.037	13	83	.75	108	.11		1.32	.01	.08	1	5	
	-	•••																														
10+00E 6+00S	4	82	16	95	.8	- 47	21	722	4.53	18	5	ND	. 4	30	1	3	2	79	.25	.033	12	117	.85	69	.12		1.56	.01	.07	1	- 5	
10+00E 6+25S	3	- 44	17	66	.7	37	13	352	4.28	12	5	ND	2	34	1	2	2	83	.34	.039	10	96	1.09	- 64	.13	10	1.58	.02	.06	<b>1</b> -	1 - <b>1</b>	
10+00E 6+50S	3	69	6	84	.9	45	20	591	4.04	11	6	ND	7	40	3	2	3	64	.45	.085	16	84	.84	66	.09	7	1.29	.02	.08	1	2	
10+00E 6+75S	· 4 ·	49	16	77	÷.4	39	13	361	3.90	10	5	ND	- 6	36	<b>1</b> .	2	2	62	.31	.041	12	78	.72	73	.09	10	1.32	.02	.06	1	.45	
10+00E 7+00S	6	78	24	124	.9	58	18	577	4.44	.19	.5	ND	6	37	2	2	2	63	.32	.055	16	80	.87	107	.09	2	1.57	.02	.10	1	3	
10+50E 0+00	8	48	34	121	1.4	30	11	322	7.81	8	5	NÐ	6	13	ť	. 4	2	-71	.07	.298	11	56	.31	58	.08	25	1.09	.01	.03	1	1	
10+50E 7+00S	2	59	15	77	3	46	19	511	4.03	11	5	ND	6	41	3	2	2	68	.49	.087	13	88	.94	77	.10	6	1.34	.02	.07	Í	- 1	
11+00E 0+75N	4	58	8	103	.5	36	11	421	3.18	- 6	5	ND	- 3	21	2	2	2	39	.35	.080	18	46	.64	51	.06		1.02	.01	.09	1	1	
11+00E 0+50N	3	77	7	108	.9	69	15	1422	4.40	3	5	ND	6	31	-1	4	2	37	.49	.086	13	51	.74	63	.08	17	.91	.01	.07	1	1	
11+00E 0+25N	4	32	5	107	1.8	34	12	857	5.08	16	5	ND	5	29	1	2	2	92	.23	.122	10	116	. 68	92	11	6	1.11	.01	.06	1	1	
11+00E 0+00	24	122	40	361	1.5	95	14	530	10.18	8	5	ND	6	- 15	1	2	· · · · •	40	.11	.076	. 8	79	.31	47	.07		1.26	.01	.02	1.	5	
11+00E 0+00 A	7	29	19	. 77	1.2	23	12	722	5.03	16	5	- 110	× ×	26	÷	· · 🚡	2	114	.15	.058	. 9	110	.36	57	.17	14	.83	.02	.04	2	112	
11+00E 0+255	6	48	25	115	2.4	- 34	12	913	6.52	13	5	ND	5	21	1	2	3	69	.15	.107	. 7	91	.37	40	.09		1.02	.01	.03	ī	3	
11+00E 0+50S	10	83	25	233	2.2	66	14	598	8.72	.7	5	ND .		13	2	2	- 3	36	.07	.107	12	46	.33	66	.05		1.20	.01	.03	1	16	ana an 20 an
11+00E 0+75S	7	50	29	226	2.4	41			7.12	4	5	ND	- <b>4</b>	15	2	2	2	45	.08	.178	11	44	.23	76	.05	n	.89	.01	.03	1	1	
	_																		A0	004		50		EA	AE	-	1.74	.01	.04		15	
11+00E 1+005	5 18	52	9 38	158 132	1.5	43 68	14 28	358 1034	6.72	- 9 38	21	: QM : 8	42	15 50	2 19	2 18	2 20	37 59	.08 .45	.080	12 38	59 59	.46 :.89	54 180	.05		1.87	.06	.13	1	52	
STD C/AU-S	18	61	20	192	/+0	00	28	1094	3.77	90	- <b>41</b> 3.4.5	0	74	JV	17	10	<b>X</b> V	37	• 40	.vu/	90	47	.07	194			1.01	140	• 4 <b>0</b> 1	44		

ť

1

(

1

C

ŧ

(

C

E

€

(

C

Gill Page B

Gid 1 GEO-MANAGEMENT PROJECT-ARMADA D.D. H. FILE # 87-4260 Page 9 SAMPLE CU PB ZN AG NI 63 MO HH FE AS U AU TH SR CD SB BI v CA Ρ LA CR Π 86 BA AL R NÂ ĸ . Allt PPN PPM PPH PPN PPh PPN PPN PPH 1 PPN PPN PPN PPN PPH PPh PPh PPh PPM 1 2 PPN PPH Z PPN Z 225 1 z Z PPN PPB 11+00E 1+255 4 42 98 .9 28 13 563 5.06 7 -5 24 .25 A 10 f t 2 2 74 .096 4 81 .34 67 .08 2 .74 .01 .03 2 13 11+00E 1+50S 49 34 342 4.99 4 5 164 1.4 11 5 6 NÐ 2 26 2 2 49 .21 .063 7 74 .37 58 .06 2 1.12 4 .01 .04 2 3 11+00E 1+75S 2 42 4 87 .7 30 9 248 3.81 5 MD 1 29 2 2 61 .29 .063 74 .59 49 . 1 6 .08 2 1.11 .01 .04 1 1 11+00E 2+005 2 45 2 72 .5 32 13 301 3.75 5 5 .36 ND 44 2 62 80 .56 1 1 2 .058 8 62 .09 2 1.20 .01 .06 1 1 11+00E 2+255 4 71 17 177 1.1 45 16 646 5.39 M 2 28 5 2 83 .27 .047 11 137 .65 52 2 .17 8 1.74 .01 .06 1 7 11+00E 2+50S 41 20 94 .4 30 9 366 5.00 15 28 .25 .38 6 - 5 M 1 1 2 2 98 .052 6 104 74 .12 2 .75 .01 .05 1 50 11+00E 2+75S 8 90 21 158 .6 57 15 567 4.42 3 5 NÐ 3 27 1 2 2 47 .26 .069 59 .44 61 .06 .97 .01 13 2 .05 1 11 9 121 172 24 1020 5.82 10 22 .23 11+00E 3+00S 15 73 3 5 ND 5 2 34 .48 57 .6 2 .069 18 46 .04 10 .93 .01 .06 2 24 21 .01 11+00E 3+255 8 91 10 171 .8 -67 18 1009 5.51 5 5 NÐ 2 3 2 2 46 .19 .073 11 70 .41 58 .05 2 1.11 .06 2 42 252 48 467 5 NÐ 30 .34 86 2 1.22 11+00E 3+505 12 79 28 .8 10 8.06 6 1 4 2 2 74 .106 9 .36 104 .11 .01 .07 1 4 190 38 11+00E 3+755 4 20 3 67 1.4 14 6 2.23 2 5 30 3 2 2 56 .17 .024 11 .10 48 .09 6 .56 .01 .02 1 3 11+00E 4+00S 27 63 17 190 1.7 45 11 595 5.01 5 2 25 2 2 49 .20 58 .29 92 2 .94 .01 4 .097 8 .04 .06 2 14 2 11+00E 4+25S 3 56 .7 27 11 529 4.07 3 5 ND 26 3 2 71 .44 .064 5 94 1.19 93 .19 2 1.40 .01 .12 5 84 1 2 1 3 11+00E 4+505 3 32 10 69 .4 20 7 267 3.20 2 5 HD. 4 23 3 2 56 .15 .050 17 46 .15 55 11 .45 .01 .04 2 37 2 .06 11+00E 4+755 3 39 7 72 1.3 27 9 353 3.34 :4 5 ND 2 39 2 2 2 61 .29 .043 10 78 .56 53 .09 2 1.32 .01 .05 2 34 11+00E 5+00S 530 2.83 .34 73 2 .95 30 11 60 2.0 26 10 2 -5 ND 37 3 2 2 57 .064 9 .56 82 .08 .01 .07 1 24 1 3 11+00E 5+25S 33 2 .9 26 850 4.08 2 5 ND 31 2 101 .30 97 .57 114 2 1.10 1 66 11 .063 4 .17 .01 .06 1 1 2 1 4 11+00E 5+50S 58 2 125 42 15 466 4.61 2 5 ND 2 52 2 2 70 .50 .067 111 1.29 86 .17 2 2.07 .01 .07 25 1 .6 1 4 1 27 28 217 3 5 NÐ 30 2 89 .27 81 .57 70 2 1.02 11+00E 5+75S 3 2 77 1.7 8 3.72 1 1 2 .061 6 .12 .01 .05 1 43 11+00E 6+00S 4 68 110 .1 53 13 422 4.35 10 5 ND 2 42 2 63 .50 .065 24 103 . 69 103 .07 7 1.48 .01 .09 3 9 1 2 1 11+00E 6+25S .35 46 .03 11 .83 3 40 3 71 2.0 31 6 449 2.47 17 -5 NE 2 26 2 2 2 37 .039 17 .34 50 .01 .03 1 1 37 2 82 91 2.1 48 9 238 2.09 5 ND 1 2 37 . 46 .069 124 .64 90 .05 2 1.74 .01 .09 3 11+00E &+50S 8 7 1 2 26 1 11+00E 6+75S 5 61 .7 32 15 491 5.36 13 5 ND 3 32 3 2 2 96 .30 .055 16 106 .39 66 .14 2 1.22 .01 .06 8 67 1 1 47 565 4.04 12 5 ND 2 40 .36 89 .75 79 2 1.45 32 11+00E 7+00S 5 64 10 97 .1 16 1 2 2 60 .044 15 .07 .01 .08 1 11+50E 0+00 35 12 82 1.3 22 10 784 5.67 8 6 ND 15 2 2 2 83 .08 .197 7 71 .20 57 .11 12 .79 .01 .03 3 4 .4 1 11+50E 7+00S 23 62 75 .67 .05 2 3 .4 18 7 424 3.36 11 5 24 77 .18 .059 12 .30 .09 4 .01 1 -5 68 M 1 1 2 2 5 .37 64 .71 12+00E 0+25M 4 97 11 149 . .9 66 15 280 4.16 3 ND 26 2 2 '44 .072 20 60 .09 2 1.18 .01 .09 1 205 6 1 12+00E 0+00 132 55 15 341 4.34 -5 ЫÐ 5 17 2 43 .22 .052 18 57 .77 59 4 1.45 .08 8 6 RÓ 5 .7 6 1 2 .10 .01 1 5 12+00E 0+255 4 39 115 .5 35 15 331 4.05 5 NÐ 7 15 1 3 2 39 .20 .091 12 41 .37 45 .06 15 .81 .01 .06 1 13 6 12+00E 0+505 322 -69 25 1233 6.04 2 8 NÐ 3 2 38 . 60 24 87 .33 57 12 1.61 .01 .04 10 108 20 4.2 41 8 2 .111 .04 t 3 129 .09 12+00E 0+75S 58 39 831 5.46 20 53 .11 12 51 .20 50 2 . 80 .01 .03 8 17 .6 11 3 -5 NC 3 2 2 2 .058 1 1 714 3.71 94 .39 92 12+00E 1+005 64 7 135 1.1 48 11 12 ND 2 53 5 3 2 52 . 62 .087 15 .04 9 1.09 .01 .07 1 4 6 4 .14 31 .09 28 .08 6 .35 .01 .02 12+00E 1+255 6 45 21 79 29 7 365 2.86 5 ND 18 2 3 2 40 .046 11 1 .1 4 1 1 12+00E 1+50S 7 87 5 92 145 2.9 57 16 741 3.55 ND 43 3 2 2 43 .45 .129 26 112 .39 .03 10 1.28 .01 .07 2 10 4 1 . 1 12+00E 1+75S 3 79 121 .3 53 14 684 3.91 7 NÐ 52 2 2 50 . 58 .068 8 71 .42 55 .05 10 .93 .01 .06 -f 1 6 1 .07 12+00E 2+00S 3 . 94 142 2.3 53 19 719 4.93 7 NO 3 44 3 2 2 54 .47 .064 14 119 .53 84 .07 8 1.51 .01 94 4 5 67 27 1025 3.89 15 39 19 21 58 .43 37 61 .79 175 32 1.62 .06 .13 13 47 STD C/AU-S 18 63 39 131 6.9 36 . 7 49 16 .083 .08

l

ſ

ť

C

(

C

0

(

ť

C

1

¢

Ć

C

C

€

C,

Gudl D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260 Page 10 SAMPLE MO CU PB Z₩ AG NI 03 -FE HN AS U AU TH SR CD S8 81 v CA ρ LA **C**R #6 BA TI 9 AL NA ĸ .... AUS PPh PPH 7 7 PPN PPN PPN PPH PPH PPN PPN PPH PPH PPN PPĦ PPN PPN PPM PPH 2 PPM PPM 7 PPN 1 PPN 2 7 z PPN PPB 12+00E 2+255 4 66 8 111 .9 44 17 601 4.21 7 5 -ND 3 59 2 2 73 .72 .054 9 104 .56 105 .07 9 1.33 .01 .09 1 17 1 12+00E 2+505 5 157 2 172 81 23 1458 5.34 NÐ 59 74 .75 .101 155 . 67 135 4.7 11 5 4 3 3 2 12 .06 16 2.09 .01 .13 1 . 12+00E 2+755 183 2 155 3.7 67 19 864 5.35 13 .71 12 141 122 6 5 ND 2 63 1 2 2 83 .086 .47 .10 3 1.88 .01 .11 1 4 12+00E 3+005 5 47 72 .2 30 10 296 5.44 5 47 87 .41 .058 95 .42 55 5 5 ND 4 2 10 .14 9 1.13 .01 1 2 .06 1 5 12+00E 3+255 18 54 20 942 4.73 ND 73 113 122 12 1.81 5 80 154 .5 6 5 4 51 2 2 2 .40 .060 11 .64 .08 .01 .10 1 7 12+00E 3+505 26 1062 6.19 87 77 28 2.43 8 79 18 167 .7 66 7 5 ND 7 23 2 2 41 .21 .088 17 .68 .04 .01 .08 10 1 51 536 5.09 39 57 .53 12+00E 3+75S 8 87 8 129 1.5 18 7 5 ND 1 2 2 .41 .041 15 70 90 .07 11 1.60 .01 .08 1 1 86 .080 12+00E 4+00S 14 271 5 197 2.7 85 37 1553 8.27 16 5 ND 6 65 1 9 2 98 .73 18 155 .71 229 .08 8 2.75 .01 .20 1 2 14 59 595 4.93 9 5 ND 61 2 81 .63 .051 11 124 .81 130 .09 10 2.07 12+00E 4+25S 5 100 134 1.2 19 3 1 2 .01 .15 1 3 12+00E 4+50S 72 7 48 31 903 7.03 11 5 NÐ 5 54 2 107 .59 .071 9 144 .77 98 .11 12 2.08 .01 .10 6 147 1.0 1 2 1 7 12+00E 4+755 92 68 24 711 4.61 .50 .070 12 134 .84 118 .07 5 2.05 .01 .10 5 7 134 2.1 -8 5 NI. 1 47 1 2 2 66 1 1 12+00E 5+00S 60 19 379 3.92 59 59 .68 .082 11 124 .80 100 .05 3 1.88 .01 .09 4 64 11 136 1.8 8 5 ND 2 2 1 3 1 4 12+00E 5+25S 7 174 63 21 514 4.51 9 5 ND 3 56 2 60 .72 .089 11 124 .83 95 .05 12 1.66 .01 .09 920 6 - 61 1.3 1 2 1 12+00£ 5+505 4 62 15 150 1.4 78 16 614 3.52 6 5 ND 4 70 2 2 2 55 1.05 .098 10 139 1.02 73 .06 8 1.66 .01 .11 2 9 187 8 2.77 .01 12+00E 5+75S 8 155 9 122 25 2198 5.41 8 5 ND 85 5 2 2 60 1.12 .111 33 181 1.01 .05 .19 1 216 4:1 4 2 12+00E 6+00S .57 6 1.39 8 62 10 152 .1 43 13 389 6.64 14 5 ND 39 2 2 121 .46 .056 12 116 80 .16 .01 .06 1 6 1 12+00E 6+25S 136 23 267 4.7 98 25 1393 4.80 12 5 NÐ 5 73 8 6 2 63 .88 .074 62 102 .78 135 .07 9 2.26 .01 .12 1 2 4 72 2 49 .99 ,080 96 102 .47 87 .08 12 2.33 .01 .05 151 25 163 24 4.58 11 5 ND 15 2 1 12+00E 6+50S 2 752 4.1 1449 8 1 12+00E 6+75S 91 24 419 1.1 105 32 1218 6.74 43 5 ND 6 30 3 2 2 65 .26 .078 37 112 .82 74 .04 7 2.31 .01 .08 1 1100 6 6.53 .21 19 79 .65 178 9 2.07 .01 .08 44 23 656 67 5 ND 60 .095 .06 1 12+00E 7+00S 13 88 349 3.0 89 16 9 31 1 2 4 .12 11 1.15 .01 12+50E 7+005 5 31 12 96 24 9 1198 3.70 12 5 ND 3 23 2 2 2 60 .043 -14 - 54 .39 76 .05 .05 1 1 1.1 13+00E 0+00 5 92 22 169 1.3 48 10 313 4.73 5 5 ND 3 19 2 2 2 54 .20 .038 29 51 .47 57 .12 10 1.34 .01 .04 Ł 1 27 368 .20 .045 44 .48 56 .08 10 1.63 .01 .06 13+00E 0+25S 4 -36 10 137 .8 10 4.59 5 5 ND 4 18 3 2 2 41 11 1 1 13+00E 0+50S 5 61 7 177 .8 63 12 192 3.71 6 5 ND 6 20 3 2 3 39 .35 .077 16 44 .64 52 .11 12 1.05 .01 .07 1 3 14 .74 51 .11 11 1.91 .01 .06 13+00E 0+75S 45 15 534 ND 17 2 43 .19 .037 57 1 5 50 16 168 4.31 5 3 2 1 .1 4 6 2 .92 .01 39 .34 .047 .49 51 .12 .04 13+00E 1+00S 50 11 441 3.99 9 46 6 57 10 194 :.5 6 5 ND 2 21 2 2 2 1 1 2 .93 .01 13+00E 1+25S 9 73 36 162 2.2 50 26 3028 7.12 5 5 ND 2 9 1 2 2 35 .07 .296 10 40 .19 88 .03 .03 1 1 7 1.32 .01 10 92 20 55 21 1431 5.68 5 ND 3 29 2 2 56 .19 .069 12 70 .31 61 .08 .07 1 1 13+00E 1+50S 166 1.5 4 4 72 5.83 .01 .07 13+00E 1+75S 13 81 30 199 2.4 50 15 1131 5.87 5 5 NÐ 2 28 2 2 2 58 .29 .112 9 72 .26 .06 1 1 2 1.36 .01 .05 15 13+00E 2+00S 39 77 27 1697 10.10 10 5 ND 5 19 2 55 .17 .117 10 113 .25 66 .07 1 19 127 274 1.3 2 1 3 124 13 1.07 . 089 20 142 .49 152 .04 5 1.51 .01 .11 9 13+00E 2+255 11 252 262 21 2011 4.37 5 62 5 5 41 15 7.0 MD 4 2 82 .33 93 2 1.27 .01 .06 2 2 13+00E 2+505 115 25 2.5 -54 18 1186 4.41 5 ND 43 3 2 67 .49 .080 13 .06 8 154 9 1 1 .01 .08 1 59 5 5 2 34 2 2 54 .37 .081 11 69 .45 86 .06 5 1.13 1 13+00E 2+75S 11 78 9 195 1.7 14 666 4.66 ND 1 13+00E 3+00S 42 990 5.89 7 5 ND 3 40 7 2 73 .56 .172 6 79 1.06 182 .10 5 1.89 .01 .09 1 9 3 -59 14 229 1.0 21 1 59 2 1.34 .01 1 13+00E 3+255 2 -54 5 36 15 439 3.75 5 жÐ 1 47 2 2 63 .41 .058 8 75 .62 .10 .06 7 4 97 .4 6 4 1.19 .01 12 31 18 1133 5.95 7 4 35 2 89 .32 .094 8 111 .40 66 .11 .06 13+00E 3+509 6 . 58 142 2.0 5 2 2 ME

18 22 59 .48 .086

38 61 .88 176 .08

STD C/AU-S

19 62

39 130 7.1

67

28 1045 3.92

42 20

37 50 17

6

ſ

(

1

ſ

(

•

C

C

£.,

C

(

39 1.80

.06

.13

13 53

Gridl D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260 Page 11 SAMPLE# 10 ល PB A<del>6</del> 8A ZN NI 03 **MN** FE AS AU TH SR CD SB BI Ŷ CA ρ LA CR MG TI. ĸ AUT U 8 AL. NA -₩ PPM 1 PPN PPN PPH PPH PPh 2 ž PPn PPN PPH PPN PPM PPH PPH PPN PPN PPN PPN PPN PPH PPN 2 2 PPN 2 2 z PPH PPB 13+00E 3+755 5 137 13 310 2.1 92 25 1930 5.39 10 5 3 49 2 63 .54 .127 12 141 .80 203 .05 2 2.58 .01 .17 2 £ 10 13+00E 4+00S 87 207 1.69 .50 .080 12 .47 196 .03 2 1.30 2 160 5.4 59 8 5 2 43 4 2 2 26 80 .01 .06 â. 4 ND 1 4 -53 13+00E 4+255 ۵. 67 7 165 .9 54 19 934 5.07 2 5 ND 1 31 1 2 2 .34 .051 15 90 .59 102 .05 2 1.47 .01 .07 1 9 13+00E 4+50S 90 32 14 565 4.08 -5 NÐ 44 2 3 74 .37 .052 9 87 .52 84 10 1.47 5 49 15 .3 -4 1 1 .10 .01 .09 1 4 13+00E 4+75S 4 81 7 81 1.0 40 14 420 4.92 7 5 4 51 2 2 2 86 .56 .053 10 95 .51 88 .12 12 1.35 .01 .08 2 4 13+00E 5+00S 6 120 8 186 1.9 77 28 1889 5.62 5 1 69 2 2 76 .93 .143 9 150 .88 193 .04 9 2.29 .02 .14 1 91 55 13+00E 5+25S 115 8 -74 51 .11 488 3.19 5 2 2 1.34 .078 8 -94 .24 95 .06 2 .93 .01 .04 6 2.6 6 ND 1 84 4 1 17 237 4.46 13+00E 5+505 8 87 12 85 .8 42 9 5 ND 2 2 2 89 .20 .037 14 79 .21 .13 7 .96 .05 5 34 5 116 .01 1 6 13+00E 5+75S 5 95 7 123 63 28 759 5.42 12 5 ND 2 28 2 2 73 .30 . 090 12 147 .72 88 .08 13 2.89 .01 .10 2.1 4 1 6 13+00E 6+00S 3 45 10 49 1.2 24 12 528 3.26 5 2 44 3 2 2 81 .41 .049 9 73 .24 86 .11 8 .73 .01 .05 1 7 4 13+00E 6+25S 5 115 12 205 .8 65 30 2418 4.80 2 2 64 1.17 .212 9 147 .90 173 .04 4 2.24 .02 .13 1 5 1 80 1 3 1 13+00E 6+50S 4 97 11 150 .8 62 25 1005 5.13 7 8 NÐ 3 56 8 2 2 79 .67 .081 11 150 .99 133 .07 13 2.11 .01 .10 1 1 13+00E 6+75S - 74 7 191 .5 62 20 856 4.79 9 5 ND 1 58 2 2 2 70 .80 .077 8 159 1.10 100 .08 6 2.02 .02 .10 1 5 1 .55 2 2.24 13+00E 7+00S 11 222 33 278 8.4 122 29 6583 4.39 6 5 ND 1 74 17 2 2 37 1.01 .151 671 97 154 .04 .01 .06 1 15 13+50E 7+00S 56 63 30 11 351 5.63 7 5 ND 2 37 2 2 97 .39 .061 10 125 .51 71 .13 8 1.26 .01 .05 1 4 11 1.1 6 4 74 .05 2 1.13 .01 .05 2 14+00E 0+50S 89 15 213 1.5 70 17 924 4.34 40 2 2 46 .52 .081 12 67 ,49 1 4 -5 5 NÐ 1 -5 32 2 2 29 .60 .092 13 53 .53 63 .05 2 1.23 .01 .05 1 70 14+00E 0+755 4 90 8 391 3.9 123 17 810 3.32 2 5 ND 3 8 .37 5 19 21 .40 .093 17 30 31 .04 2 .70 .01 .04 1 11 14+00E 1+00S 2 42 2 189 2.1 50 9 264 2.35 2 5 ND 1 6 2 45 63 .21 32 8 1.28 .01 14+00E 1+25S 11 123 17 160 3.7 56 16 769 6.34 4 5 ND 1 16 5 2 2 .12 .058 10 .08 .03 1 9 14+00E 1+50S 49 90 262 4.06 2 ND q 2 34 .08 .033 25 16 .04 30 .04 8 .22 .01 .02 1 - 3 7 19 .2 .27 8 5 3 -5 14+00E 1+75S 50 22 185 42 13 1065 5.95 2 2 47 .15 .087 11 53 .27 48 .07 10 .87 .01 .04 1 7 12 1.1 2 20 5 ND - 3 6 13 15 567 4.18 32 2 2 46 .38 .064 12 62 .28 46 .06 2 .86 .01 .01 1 14+00E 2+00S 6 107 162 .6 59 5 5 MÐ 1 1 6 2 56 .15 76 3 . 36 10. .03 1 33 97 10 556 3.91 5 ND 2 21 2 2 .17 .103 10 41 .06 14+00E 2+25S 6 40 15 1.1 31 3 .30 .05 .01 .03 58 131 15 618 5.14 3 5 ND 1 31 2 2 53 .43 .119 11 52 50 3 . 69 1 41 14+00E 2+50S 7 19 .7 . 44. 4 2 54 .19 .090 14 39 .15 51 .07 8 .44 .01 .04 1 14+00E 2+75S 47 125 37 11 595 4.20 3 5 NÐ 3 24 3 4 6 9 16 .6 14+00E 3+00S 2 53 .37 .071 44 .15 100 .08 2 .49 .01 .04 1 2 19 68 .5 19 695 2.75 2 5 2 34 3 3 9 2 11 8 N 62 .35 91 .53 63 .07 6 1.23 .01 .05 1 4 17 542 4.46 5 ND 3 35 2 2 2 .066 10 14+00E 3+255 5 37 9 118 2.3 37 3 .45 .74 56 .09 3 1.09 .01 .07 1 11 14+00E 3+50S 51 20 511 4.33 3 5 жÐ 2 36 3 2 62 .075 9 67 95 16 140 .1 1 6 224 3.88 NÐ 41 2 2 69 .42 .073 6 78 .59 61 .08 3 .99 .02 .04 1 10 14+00E 3+75S 1 28 10 82 .8 26 9 4 5 1 3 73 .68 52 7 1.12 .01 .06 1 124 366 68 .48 :044 .12 14+00E 4+00S 3 44 7 77 .2 32 14 3.57 3 5 MD 3 49 3 3 2 8 2 1.37 .06 1 13 .42 .052 70 .10 .01 14+00E 4+25S 3 47 2 102 .3 36 -14 365 3.84 -5 3 45 2 2 2 62 10 .60 66 ND 4 .08 1 418 3.85 73 .44 75 .57 65 .12 4 1.27 .01 7 14+00E 4+50S 3 67 15 86 .5 38 13 4 5 NÐ 2 47 1 2 2 . . 044 10 .62 53 8 1.02 .02 13 2 ND 47 2 2 59 .43 .031 12 59 .12 .07 1 11 14+00E 4+75S .3 56 7 94 .3 39 443 3.43 5 4 1 .07 29 80 .070 12 105 .45 77 .11 2 1.45 .02 .1. 14+00E 5+00S 4 140 16 118 1.2 50 20 913 4.89 6 5 NÐ 1 41 1 4 2 .31 . 74 .73 .147 15 116 .54 .04 9 2.06 .01 .15 1 10 14+00E 5+25S 130 21 159 2.9 31 3004 5.76 ND 2 55 7 2 2 169 7 71 5 2 67 .32 .072 66 .29 74 .08 3 .75 .01 .04 31 12 541 -34 .2 14+00E 5+50S 5 + 60 11 75 .8 3.99 6 5 ND -1 1 8 . 89 37 1.83 .06 .13 13 49 39 17 58 .49 .086 36 62 177 .08 STD C/AU-S 18 62 41 131 7.1 68 27 1025 3.96 37 18 9 50 18 22

1

Ċ

€

(

C

Ç

C

C

€

(

C

(

C

(

(

(

D.D.H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260

SAMPLES		NO PPN	UU PPN	р <b>8</b> Гги	ZN PPM	AG PPM	NI PFM	CO PPM	rin Pph	FE 2	AS PPN	U PPN	AU PPN	TH PPN	SR PPM	CD PPM	SB PPM	BI PPN	V PPN	CA Z	Р 1	LA PPM	CR PPM	116 2	BA PPN	11 2	B PPH	AL Z	NA Z	K Z	N PPn	aut PPB	×
14+00E 51	1259	5	134	16	208	2.2	78	26	1919	4.98	13	5	ND		57	7	3	2	64	.69	.117	12	148	. 86	214	.05		2.33	.01	.15	1	4	
14+002 51		7	157	7	194	2.3	87	25	1282	5.00	14	5	ND	2	-55	4	2	2	64	.67	.108	14	224	.71	186	.06		2.33	.01	.13	1	14	
14+00E 64		Ś	49	13	87	.3	35	20	623	5.48	4	5	ND	- 2	36	Ś	2	2	93	.41	.068	6	145	.89	97	.11		1.51	.01	.06	1	1	
14+005 64		2	59	3	55	.4	32	13	446	5.30	6	5	ND	. 4	41	4	2	2	116	.43	.095	7	144	.67	43	.14	2	1.41	.01	.06	1	5	
14+00E 64		2	43	2	66	-1	37	13	390	3.24	2	5	ND	5	50	. <b>1</b>	2	3	62	.48	.039	12	. 67	.64	80	.09	2	1.15	.01	.06	1	3	
14+00E 7+	+00S	2	50	7	137	.6	48	19	548	4.23	. 4	5	ND	3	62	3	2	2	68	.81	.060	8	117	1.01	77	.06	3	1.76	.01	.07	-1	26	
14+50E 7-	+005	2	- 46	6	67	.7	35	17	519	3.94	4	5	ND	4	44	1;	2	2	80	.45	.045	8	111	.77	93	.09		1.44	.01	.06	1	4	
15+00E 14	+005	6	73	15	111	.7	48	12	349		3	5	NÐ	10	22	3	. 4	2	35	.37	.067	22	42	. 66	61	.08		1.00	.02	10	1	2	
15+00E 14		4	27	9	17	.1	29	13		3.76	2	- 5	ND	5	13	1	2 3	2	33	.23	.062	11	30	.35	42	.06	2	.68	.01	.04 .05	1	.54 2	
15+00E 14	+505	10	79	- 18	226	3.1	50	-16	495	2.61	2	5	RU	3	37	17	3	2	27	.65	.145	11	40	.38	111	.03	<b>4</b>	1.01	.01	.03	1	. 4	
15+00E 1-	+755	- 3	168	6	196	2.5	64	: 9	434	2.65	- 2	. 6	ND	. 3	52	5	3	2	34	.87	.155	13	99	.52	71	.05		1.53	.01	.05	1	12	
15+00E 2-	+005	11	116	18	461	7.7	110	27	1179	7.69	4	5	ND	- 4	30	. 11	2	2	38	.36	.091	7	75	.55	47	.06		2.85	.01	.04	1	43	
15+00E 24	+255	9	127	17	275	5.1	101	37			3	- 5	ND	5	28	6	2	2	28	.69	.144	. 9	88	.32	54	.03		2.80	.01	.03	1	15	
15+00E 2	+505	17	73	37	192	1.0	53	19			. 4	5	ND	4	24	. 9	2	2	61	.28	.074	13 -	52	.24	47	.07		1.02	.01	.04	1	1	
15+00E 2-	+755	9	136	10	311	4.4	101	25	1684	5.50	- 5	5	ND	2	44	7	2	. 2	45	.65	.129	12	98	. 38	136	.04	2	1.77	.01	.07	1	- 9	
15+00E 3-	+00S	22	50	17	157	.1	40	15	652	5.84	2	- 5	ND	1	21	2	2	2	55	.16	.070	13	45	.16	45	.07	2	.62	.01	.04	1	1	
15+00E 3-	+255	10	64	-14	109	1.7	36	12	366	4.37	2	5	ND	3	40	3	3	2	56	.57	.066	16	68	.31	55	.06	2	.97	.01	.05	1	7	
15+00E 3-	+505	9	- 99	16	186	1.4	72	21	1877		5	5	ND	- 3	52	2	2	2	<b>47</b> -		.097	10	77	.61	103	.05		1.20	.01	.09	1	6	· · ·
15+00E 34	+755	- 8	118	20	195	2.1	77	21	827		- 14	. 5	ND	5	42	5	2	2	52	.53	.103	14	87	.60	71	.05		1.30	.01	.07	1	9	1 i .
15+00E 4-	+005	6	76	13	106	1.2	38	22	1020	4.69	2	5	ND	5	37	5	2	2	69	.38	.087	12	81	.33	57	.07	. 8	1.25	.01	.06	1	2	
15+00E 4-	+258	3	64	3	90	1.0	29	- 16	589	3.92	2	5	ND	3	44	2	2	2	77	.41	.055	10	80	.42	53	.12		1.34	.01	.06	- 1	3	
15+00E 4	+505	10	151	14	249	1.4	89	113	3125	9.33	- 8	. 5	ND	2	35	10	2	2	124	.39	.102	7	170	.76	150	.12		3.11	.01	.17	1	29	
15+00E 4-	+755	7	70	14	78	1.1	27	8	414	4.29	3	5	ND	5	36	4	5	2	17	.31	.128	11	71	.24	58	.09		1.02	.01	.06	2	60	
15+00E 5	+005	11	218	7	394	2.5	112	- 40		7.15	6	- 5	ND	5	54	8	2	2	78	.67	.170	12	177	.80	223	.06		3.52	.02	.19	. 1	36	
15+00E 5	+255	4	43	12	86	.6	30	12	456	4.53	. 6	5	ND	3	51 -	5	2	4	, <b>17</b> -	.55	.056	8	80	.81	68	.16	2	1.54	.01	.07	1	4	
15+00E 5	+505	5	69	20	73	.6	35	. 9	314	4.01	7	5	ND	2	45	2	2	2	74	.39	.052	9	65	.39	76	.10	2	.89	.01	.06	i	1	
15+00E 5	+755	4	78	8	102	4.0	38	16	767	4.63	2	5	ND	4	40	4	2	2	81	.33	.061	10	95	.38	97	.11	-	1.35	.01	.09	1	1	
15+00t 6	+005	8	55	21	112	1.6	32	13	1084	5.18	6	- 5	ND	- 5	34	6	2	2	52	.41	.082	15	49	.33	74	.06		1.02	.01	.06	<u> </u>	1	
15+00E 6	+255	3	64	16	113	.5	45	18	1048	4.30	3	5	ND	4	39	3	2	2	53	.38	.074	12	93	.57	104	.05		1.34	.02	.08	2	31	
15+00E 6	+505	7	99	26	116	.5	43	10	348	5.24	7	5	ND	3	21	. 4	2	2	57	.13	.078	19	66	.24	54	.07	2	1.34	.01	.04	1	1	
15+00E 6	+755	2	44	7	55	.1	35	11			5	5	ND	2	45	1	2	2	81	.42	.049	8	116	.74	105			1.32	.02	.05	1	5	
15+00E 7-	+005	2	59	13	88	7	38	17	692		3	5	ND	3	57	2	2	2	88	.64	.068	. 8	130	.72	72	.10		1.49	.01	.09	1	1	
15+50E 7	+005	2	79	2	136	1.3	69	22	842		2	9	ND	4	63	- 4	2	2	70		.082	8	153	.90	115	.07		2.02	.02	.08	1	6	
16+00E 1-		5	25	7	35	.7	14	5	190	2.55	2	5	ND	2	22	1	2	2	49	.13	.041	7	32	.16	36	.10	2	.56	.01	.03	1	1 34	
16+00E 1	+505	- 5	33	8	102	- 4	32	19	373	4.64	2	5	ND -	5	14	2	2	2	44	.21	.061	10	41	.36	24	.07	8	.96	.01	.05			
16+00E 1	+755	14	120	22	263	1.0	88	19			5	5	ND	6	12	1	2	2	26	.15	.130	11	31	.36	29	.04	4	.96	.01	.04	17	9	-
STD C/AU	-S	19	61	37	129	7.0	65	27	1004	3.87	39	18	7	38	49	20	18	20	57	.48	.085	36	59	.86	175	.08	3/	1.84	.06	.13	13	50	
						(4) 4. Contract					上にないよう	これ、ス		. 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 197	1.1.1																	a substant of a	

Gill Page 12

(

ſ

£

(

0

(-)

C

C

							Ľ	D.D.	н. 0	5E0-	MANA	GEM	ENT	PRO	JECT	-ARI	MADA	F	ILE	# 83	7-42	:60							Grid	1	P	ace 13	
SAMPLE#	NO PPN	CU PPM	PB PPM	ZN PPM	AG PPR	NI PPN	CO Prn	nn Ppn	FE	AS PPM	U PPN	AU PPM	TH PPN	SR PPN	CD PPM	SB PPM	BI . PPM	V Prii	CA 2	P 2	LA PPM	CR PPM	MG 2	BA PPn	TI Z	B PPN	AL Z	NA Z	K Z	N PPH	aut Ppb		
16+00E 2+00S	8	38	10	101	3.4	37	8	809	4.46	. 4	5	ND	. 4	11	4	3	2	- <b>41</b>	.07	. 162	12	35	.23	48	.04	9	.77	.01	.03	1	3		
16+00E 2+255	1		27	212	7:4	- 91	9	165	1.27	2	. 9.	ND	2	64	6	2	2	25	.79	.123	10	82	.44	216	.03		1.55	.01	.08	. 1	59		
16+00E 2+50S	5	126	12	198	4.0	58	17	1557	3.91	3	5	ND	1	45	3	2	2	44	.55	.175	12	. 97	.40	77	.03		1.65	.01	.06	1	4		
16+00E 2+75S	11	63	11	123	8	33	20	865	6.58	. 6	5 5	ND	1	29	1	2	2	101	.23	.067	. 7	104	.37	47	.18		1.07	.01	.03	1	2		
16+00E 3+00S	23	97	28	197	1.1	47	22	1493	6.87	3	. 3	ND	2	35		2	2	78	.39	.065	13	69	.11	- 60	.16	10	.88	.01	.04	1	3		
16+00E 3+25S	12	67	25	253	.7	63	14	906	5.03	4	5	ND	1	20	1	2	2	44	.15	.077	12	41	.25	56	.03	2	. 66	.01	.03	1	6		
16+00E 3+50S	10	46	16	143	8.1	39	. 7	756	3.43	3	5	ND	1	20	1	2	2	36	.30	.108	11	33	.23	80	.03	2	.46	.01	.04	- 1	25		
16+00E 3+75S	4	40	5	80		32	10	556	3.76	5	5	ND	2	34	2	2	2	74	.30	.054	9	87	.54	60	.11		1.04	.01	.06	1	310	•	
16+00E 4+00S	7	78 70	6 12	137 81	1.0	58 44	26	2165 476	4.41	4	· 5	ND ND	. 3	54 54	2	3	2	51	.58	.096	11	72	.58	91	.07		1.02	.01	.07	1	12		
16+00E 4+25S	2	/v	12	01	•3		17	4/0	3.97	•	3	NV.	1	34	2	3	1	68	.61	.085	9	82	.56	59	.07	2	.82	.01	.07	1	2		
16+00E 4+50S	1	89	5	133	.6	57	15	644	3.76	5	5	ND	1	. 76	1	2	2	59	.97	.082	7	112	.62	122	.06		1.26	.01	.09	. 1	51		
16+90E 4+755	2	-	9	121	.9	48	16	500	4.29	5	5	ND	2	55	2	2	2	71	.51	.053	10	108	.63	100	.08		1.48	.01	.10	1	- 5		
16+00E 5+00S	2		2	136	9	51	20	632		2	. 5	ND	3	61	1	2	2	67	.57	.089	11	114	.73	127	.07		1.52	.02	.12	1	6		
16+00E 5+255	4		8	89	2.2	28	18	989	4.35	5	. 5	ND	2	29	2	5	2	76	.18	.075	- 13	110	.25	65	.09		1.18	.01	.07	1	2		
16+00E 5+50S	3	128	3	185	• •8	77	28	1441	4,89	4	5	ND	3	56	2	2	2	73	.51	.070	12	119	.89	175	.09	3	1.95	.01	.15	· 1	4		
16+00E 5+75S	3	130	7	166	3.0	71	23	1590	5.13	- 8	8	ND .	3	61	3	2	2	76	.59	.120	13	169	.76	177	.05		2.18	.01	. 18	1	15		
16+00E 6+00S	2	- 54	- 3	88	1.0	40	18	587	4.03	7	5	ND	2	48	1	2	2	67	.38	.045	_ 11	103	.58	63	.09		1.27	.01	.08	2	1		
16+00E 6+255	3	48	- 8	<b>6</b> 3	.5	29	18	530	6.30	10	- 5	ND	1	35	1	3	3	90	.42	.151	5	112	.75	48	.12		1.27	.01	.05	· 1	1 -		
16+00E 6+30S	1	54	2	56	1.1	- 30	13	602	5.10	6	- 5	ND	2	39	1	2	2	.99	.37	.234	. 8	134	. 60	77	.11		1.06	.01	.07	. <b>1</b>	1		
16+00E 6+755	2	111	15	110	2.1	70	25	1095	4.53	6	5	⇒ ND	2	48	2	2	5	70	.58	.087	11	147	.86	147	.07	9	1.71	.01	.10	1	5		
16+00E 7+00S	- 5	55	18	84	1.9	32	12	917	4.52	7	5	ND	2	32	1	· · 2	2	94	.23	.047	14	90	.37	173	.13	. 3	.93	.01	.06	1	51		
16+50E 7+00S	7	83	13	17	. 8	38	16	740	7.01	8	6	ND	3.	41	1	2	. 3	137	. 42	.076	8	173	.58	119	.14	- 3 -	1.50	.01	.07	1	10		
17+00E 2+00S	8	43	19	97	1.4	28	6.	348	3.93	3	5	ND	3	13	1	. 2	2	32	.09	.058	10	36	.24	65	.05	2	•78	.01	.03	1	51		
17+00E 2+25S	6	42	10	106	.9	33	7	625	3.90	2	5	ΝÐ	3	. 9	2	- 3	2	31	.04	.032	14	19	.09	. 47	.04	2	.50	.01	.02	1	1		
17+00E 2+50S	6	79	12	147	3.2	. 44	- 11	568	3.50	2	5	ND	. 3	28	1	2	2	33 .	.29	.046	16	38	.22	70	.03	2	.95	.01	.03	1	8		
17+00E 2+75S	.:4	177	15	248	2.8	71	10	192	2.75	9	. 5	ND	2	42	2	2	3	57	.43	.123	15	105	.54	136	.06	2	1.60	.01	.10	1	- 3		
17+00E 3+00S	5	89	14	155	2.6	50	15	859	7.02	8	9	ND	3	36	- 1	3	2	53	.31	.059	7	75	.42	65	.12	. • <b>4</b> °	1.04	.01	04	. 1	4		
17+00E 3+25S	5	101	3	133	.5	51	16	707	4.47	- 4	5	NÐ	- 1	49	1	2	2	69	.44	.070	11	109	.60	100	.07	2	1.40	.01	.09	1.	12		
17+00E 3+50S	7	39	14	73	.1	23	6	214	3.37	- 4	5	ND	- 2	- 33	1	2	2	66	.16	.089	10	47	.12	34	.07	8	.47	.02	.05	1	2		
17+00E 3+75S	12	89	10	224	1.4	70	22	3417	6.03	4 -	10	ND	6	29	8	5	2	43	.28	.158	18	77	.35	103	.03	10	1.19	.01	.07	1	15		
17+00E 4+00S	5	47	2	109	.4	35	14	835	4.26	4	5	ND	3	33	1	2	2	63	.26	.072	· 11	82	.41	65	.06	2	1.04	.01	.08	1	5		
17+00E 4+25S	- 7	28	14	55	.9	15	÷ 4,	147	2.62	3	5	ND	1	29	1	2	2	50	.18	.044	15	42	.14	63	.07	2	.53	.01	.04	2	17		1
17+00E 4+50S	5	31	- 11	83	.2	27	9	594	3.82	5	5	ND	3	36	1.	3	2	69	.28	.050	: 11	62	.25	107	.10	7	.70	.01	.05	1	21		
17+00E 4+75S	4	101	2	113	.6	50	16	486	4.01	5	5	ND	3	47	1	2.	4	60	.50	.081	11	72	.57	68	.09	2	. 98	.02	.10	1	12		235 243 243
17+00E 5+00S	4	72	10	117	1.2	43	10	347	4.48	8	5	ND	3	42	1	2.	2	71	.43	.074	9	98	.50	103	.08	5	1.26	.02	.10	1	37		
17+00E 5+25S	3	53	8	61	.7	30	12	394	3.40	5	5	ND	2	46	1	2	2	64	.42	.069	8	69	.44	69	.11	2	.87	.01	.06	1	18		
STD C/AU-S	18	62	35	132	7.4	68	28	1041	3.94	37	15	1	40	51	16	17	22	59	.44	.087	39	61	.80	181	.08	33	1.66	.06	.13	13	52		
				1.00	1914 - C. M.	インバヤー ひんしょ	1.2 A 1.4 A	1. Sec. 2			1.1		(1) 1. (1) (2) (-1)													1.1.1.4 (1.1.1)						- たうしい おびが 一般学	

ः,

C

1

(

(

€

(

C

(

Ç

Gill D.D. H. GEO-MANAGEMENT PROJECT-ARMADA FILE # 87-4260 Page 14 SAMPLE **PB** HO CU ZN AG NI CO HN FE AS U AU TH SR CD SB 91 v CA P LA CR 116 BA TI ĸ 8 AL NA . AUT PPN PPM PPN PPN PPN PPH PPN 7 PPN PP# PPH PPN PPN PPH PPN PPN PPh 7 1 PPN PPN 7 PPN 2 PPN PPN PPN 1 1 7 PPB 17+00E 5+50S 28 584 1 70 15 88 1.0 17 5.95 -5 5 ND 3 35 2 2 92 .46 .082 -5 101 .80 72 .14 10 1.99 .01 .10 1 1 17+00E 5+759 42 434 3.56 73 .52 3 60 17 73 16 5 ND 39 2 60 .40 .067 55 .09 5. .97 . 6 6 6 1 2 10 .02 .07 1 37 17+00E 6+00S 3 149 18 103 2.1 -64 32 1038 4.88 8 5 ND 4 44 1 2 2 77 .49 .066 14 135 .70 149 11 1.98 .10 .01 .13 1 6 17+00E 6+255 3 39 -5 .9 20 185 3.73 2 32 2 89 .27 67 51 6 6 NÐ 4 2 .029 9 .51 59 .19 1 7 1.06 .01 .06 4 1 17+00E 6+50S 2 60 5 -68 5.6 -34 14 504 4,79 7 5 4 37 2 4 84 .26 .057 12 97 .53 53 6 1 .13 2 1.12 .01 .07 3 1 17+00E 6+75S 17 297 1 47 52 .1 28 10 4.78 4 - 5 -3 33 1 2 2 87 .25 .078 9 112 .52 29 .11 2 1.08 .01 .04 2 1 17+00E 7+00S 3 89 9 80 .3 61 14 391 4.78 9 .5 ND 2 29 3 2 81 .25 .030 8 170 1.04 52 .12 2 1.83 .01 1 .06 1 1 59 20 3 37 2 .39 17+50E 7+00S 2 109 10 -111 1.0 665 5 ΗD 2 75 .087 129 .78 120 .07 2 1.60 4.38 6 1 10 .02 .12 1 290 18+00E 2+255 2 105 11 109 .7 54 18 452 3.69 5 -5 NÐ 4 44 1 3 2 46 .47 .069 12 47 .52 54 .09 2 .74 .02 .08 1 52 18+00E 2+505 19 1.2 62 589 43 2 46 .48 .074 13 46 . 58 65 .09 4 .81 .02 3 100 141 18 4.0B \* -5 ND 6 1 2 .09 2 55 .53 18+00E 2+75S 7 5 124 22 226 1.5 113 19 867 3.91 4 -5 10 28 2 2 28 .42 .077 18 -34 32 .06 .66 .02 .08 4 ND 1 1 18+00E 3+00S 4 122 19 163 .9 71 16 481 3.56 3 5 ND 35 1 2 2 40 .37 .067 13 49 .55 48 .08 6 .85 .01 .07 6 1 40 385 3 5 NÐ -1 21 2 -34 .19 .104 45 .45 42 2 .96 18+00E 3+259 4 82 10 169 .4 57 10 3.91 1 2 10 . .04 .01 .05 1 9 32 5 1.11 18+00E 3+50S 3 94 25 159 1.7 68 14 439 3.87 4 5 ND 4 23 1 2 2 .26 .071 12 49 .44 45 .05 .01 .06 7 1 17 1062 4.77 7 ND 45 2 72 .49 .099 14 128 .80 142 2 1.69 .02 18+00E 3+75S 5 129 8 162 114 - 64 5 1 Ť. 2 .06 .13 1 5 692 4.10 2 1.29 18+00E 4+00S 83 2 121 1.0 48 19 42 2 64 .46 .075 10 101 .56 95 .06 .01 .08 41 4 6 5 2 1 2 1 2 65 .27 108 .60 71 2 1.64 18+00E 4+255 87 15 116 .2 43 19 687 4.35 5 ND 33 2 .075 11 .07 .01 .08 1 5 1 6 1 1 18+00E 4+50S 5 41 10 53 1.2 19 182 4.24 5 5 ND 4 -34 2 2 76 .23 .029 8 65 .30 60 .17 . 98 .01 .05 6 1 6 1 4 438 2 28 2 80 .24 .044 8 100 .32 38 15 1.06 18+00E 4+75S 2 12 74 .4 28 14 4.64 -5 ND 2 1 2 .11 .01 .04 1 8 - 60 18+00E 5+00S 5 102 .3 55 17 447 3.99 5 5 5 39 2 2 57 .46 .086 13 61 .56 51 .09 2 . 81 .01 .07 2 27 7 104 1 456 62 .51 .092 13 74 .62 55 .09 13 .89 .01 .06 7 18+00E 5+25S 4 113 93 52 19 4.17 7 -5 5 44 2 2 1 8 .1 1 934 4.15 2 68 .34 .086 9 118 .58 65 .07 15 1.46 .01 .07 5 3 76 .7 40 18 6 5 ND 2 36 2 1 18+00E 5+50S 4 104 1 735 3.62 47 2 63 .61 8 109 .63 104 .06 5 1.29 .01 18+00E 5+755 3 78 2 86 .8 48 17 2 5 ND 1 1 2 .071 .09 1 26 95 16 210 .76 277 .07 2 3.16 .01 29 419 5.68 5 ND 40 2 .41 .122 .24 1 5 18+00E 6+005 8 243 34 190 1.6 100 14 1 1 2 38 2 .37 .052 12 71 .59 88 .09 2 1.08 .01 .08 18+00E 6+25S 3 55 6 85 .6 37 13 490 3.52 3 5 ND 2 t 2 61 1 4 18+00E 6+505 2 32 .2 24 499 2.84 3 .5 33 2 63 .24 .040 11 56 .37 166 .07 8 .76 .01 .06 8 -5 64 9 1 4 32 82 .25 70 .26 46 .12 2 .61 .01 .05 34 · .7 22 237 5 NÐ 2 2 .105 9 3 18+00E 6+75S 3 11 47 6 3.64 3 .1 1 1 33 91 .26 126 .66 62 2 1.37 .02 .07 18+00E 7+00S 2 72 9 69 .1 36 16 575 5.00 4 5 NÐ 1 1 2 .3 .046 8 .13 1 9 .169 18+00E 7+255 3 42 11 22 7 265 4.53 5 5 ND 1 35 1 2 2 93 .29 9 92 .31 -54 .10 2 .80 .01 .08 1 3 6 51 730 42 2 80 .47 .065 9 126 .74 116 .07 2 1.48 .01 .11 14 18+00E 7+505 2 92 2 82 .7 47 20 4.34 7 -5 1 1 2 1 .42 129 .82 .09 2 1.39 .03 .08 18+00E 7+75S 91 11 49 24 743 4.14 38 1 2 2 80 .069 9 104 1 4 1 65 .5 7 5 1 2 79 .83 82 4 1.20 18+00E 8+005 1. 80 2 58 .3 47 18 550 3.99 5 5 ND 2 40 1 2 .47 .066 8 114 .09 .03 .10 2 -5 92 625 5 ND 1 34 2 3 85 .32 .070 14 138 .72 129 .10 2 1.78 .02 .13 1 8 5 13 95 49 19 5.02 4 1 18+50E 7+005 1.2 .34 72 .63 59 62 19+00E 3+00S 75 33 12 405 3.94 3 5 ЖÐ 1 32 1 2 3 62 .063 8 .08 3 .97 .01 .07 1 3 59 10 .1 573 5 ND 45 2 62 .55 .072 85 .61 96 .06 2 1.07 .01 .09 25 19+00E 3+25S 73 1 50 14 3.69 5 1 1 2 8 1 3 109 .6 769 5.49 -30 2 -31 . 38 .089 11 35 .42 52 .04 2 .59 .01 .04 4 20 -5 2 2 1 19+00E 3+505 8 - 92 40 339 2.0 89 -5 1 64 .83 .14 12 51 18 .46 .090 43 180 .08 31 1.73 .06 STD C/AU-S 18 62 36 132 6.9 69 28 1049 4.07 35 15 8 40 51 18 16 61

í

ł

7

C

(

(

1

(

(

(

(

C

£

(

6

C

C

6

D.D.H. GED-MANAGEMENT PROJECT-ARMADA FILE # 87-4260

SAMPLE#	HO PPH	CU PPM	P8 .PPM	ZN PPH	A6 PPM	NI PPM	CO PPM	nn PPn	FE Z	AS PPM	U PP#	AU PPM	TH PPM	SR PPM	CD PPM	SB PPN	8I PPM	V PPN	CA Z	P I	LA PPN	CR PPN	H6 7	BA PPM	TI Z	B PPN	AL Z	NA Z	K Z	N PPN	AUX PPB	
19+00E 3+75S	5	104	9	145	3.6	57	13	436	3.86	10	5	ND	4	30	1	2	2	40	.26	.044	11	51	.62	66	.07	14	1.27	.01	. 06	2	1	
19+00E 4+00S	5	113	1	219	1.2	111	-16	640	4.53	8	5	ND		32	i	2	2	33	.29	.061	12	42	.58	64	.06	5	1.03	.01	.05	-	23	
19+00E 4+25S	6	57		121	1.9	34	16	812	4.99	11	5	ND		31		3	2	57	.30	.050	9	81	.38	59	.09	-	1.22	.01	.04		10	
	-			72		• •	8	255		10	5	ND	2	31		2	2	- 63			•	-		-								
19+00E 4+50S	3	30	. 14	-	.2	-21	-	439	4.34				2			2			.27	.053	6	71	.47	. 69	.11	2	.86	.01	.04	1	- 14	
19+00E 4+75S	9	51	10	133	•1	30	13	437	6.12	12	.9	ND	ు	- 41	1	. <b>4</b>	2	86	.42	.062	y	96	. 58	83	.15	2	1.27	.01	.06	, <b>1</b> ,	8	
									~ ~~	-			-						••				<b>.</b>									
19+00E 5+00S	<u>+</u>	30	10	97	1,1	20	- 9	368	3.78	8	6	ND	3	37	1	2	2	67	.31	•053	. 6	75	.36	88	.12	2	.92	.01	.05	1	. 1	
19+00E 5+25S	3	35	2	49	.2	22	.7	263	3.36	10	- 5-	ND	2	38	1	2	2	65	.34	.041	8	63	.46	62	.10	8	.81	.01	.04	1	2	
19+00E 5+505	2	33	11	59	.5	24	8	254	3.54	9	5	NÐ	. 1	37	1	2	2	77	.34	.033	7	77	.47	80	.10	3	.85	.02	.05	1	260	
19+00E 5+75S	4	62	6	101	•6	43	18	579	4.25	11	5	ND	2	43	1	2	2	73	.44	.071	12	82	.70	85	.09	. 4	1.12	.02	.08	1	13	
19+00E 6+00S	5	78	8	105	.9	41	23	815	4.50	10	5	ND	4	39	1	2	2	76	.36	.040	11	115	.72	89	.10	8	1.51	.01	.08	1	1	
19+00E 6+25S	. 4	59	11	79	1.2	41	17	540	3.75	7	5	ND	2	40	1	2	2	65	.45	.066	- 8-	93	.73	95	.07	5	1.09	.02	.09	1	· 4	
19+00E 6+50S	8	- 50	18	101	1	35	20	933	7.07	-10	7	NÐ	3	30	1	2	3	163	.28	.067	8	124	.42	89	.30	4	1.01	.01	.05	1	23	
14+00E 6+75S	6	86	8	123	.5	40	16	429	4.21	. 8	7	ND	5 3	48	1	2	2	72	.46	.048	12	92	.71	69	.12	1	1.14	.01	.06	1	160	
19+00E 7+00S	2	74	9	89	.2	49	18	631	4.26	14	6	ND	2	39	1	2	2	76	.37	.056	10	109	.76	100	.07	2	1.29	.02	. 08	1	34	
19+00E 7+255	5	103	14	104	.6	52	24	684	6.96	16	.5	ND	- 4	38	3	2	2	101	.43	.069	10	117	.78	118	.12	.9	1.75	.01	.12	1 -	5	
19+00E 7+505	. 1	78	13	. 87	. 6	49	16	588	3.95	10	-5	ND	2	49	1	2	2 -	69	. 52	•064	11	102	.75	117	.07		1.30	.02	.11	1	114	
19+00E 7+755	- 4	78	7	89	- 4	- 49	20	621	4.15	9.	5	NÐ	2	49	1	3	2	73	.53	.066	12	111	. 80	122	• 08	2	1.48	.01	.11	1	10	
19+00E 8+00S	. 3	52	2	32	.9	- 18	6	151	2.68	4	5	ND	3	38	1	2	2	17	.20	.026	12	71	.15	- 38	.13	2	.61	.01	.04	1	2	
19+00E 8+25S	2	32	. 7	51	2.8	22	9	420	4.14	8	5	NÐ	4	37	. 1 -	2	2	84	.26	.096	11	93	.46	36	.12	· 7	.97	.02	.05	-1	. 1	
19+00E 8+50S	3	83	6	95	.1	51	18	576	4.19	11	- 6	NÐ	5	. 49	1	2	2	69	.46	.059	14	82	.86	115	.09	4	1.32	.02	.11	1	3	
																					. • •											
19+00E 8+75S	2	64	6	95	-1	- 44 -	20	486	4.30	9	5	ND	3	57	1	- 2	2	- 75	.66	.051	9	95 .	.80	68	.07	-	1.11	.02	.10	1	1	
19+00E 9+00S	3	67	- 4	100	-4	55	19	525	4.27	14	6	ND	4	- 47	2	2	2	72	.48	.063	13	94	. 88	101	.11	3	1.45	.01	.09	1	20	
19+50E 7+00S	- <b>4</b>	88	2	88	5	- 49	20	728	4.07	8	5	ND	5	48	2	3	2	69	.54	.076	-11	88	. 67	79	.08	7 -	1.11	.01	.09	1	12	
20+00E 3+25S	3	93	5	154	2.2	53	19	516	3.94	8	5	ND	3	47	1	2	2	44	.55	.066	17	84	.72	55	.05	10	1.21	.01	.07	1	41	
20+00E 3+505	8	53	10	123	3.7	- 44	11	525	5.11	8	5	ND	3	14	1	4	3	28	.14	.063	10	- 33	.36	22	.04	2	.92	.01	.04	. 1	1	
20+00E 3+75S	8	110	15	209	3.7	87	15	839	5.75	11	5	ND	.7	·	3		2	23	.09	.070	14	33	. 46	- 39	.02	15	.91	.01	.04	1	10	
20+00E 4+00S	11	45	18	151	1	42	7	423	6.98	18	S	ND	5	16	1	3	2	54	.08	.154	12	33	.28	35	.07	3	.76	.01	.05	1	4	
20+00E 4+25S	13	59		215	2.1	51	. 8	361	6.82	. 9	7	ND	3	17	•	2	2	59	.10	.201	11	42	.31	39	.06	12	.91	.01	.04	1	3	
			28								- 7				4			-				37		55		3	.98	.01	.04	· 1	39	
20+00E 4+50S	7	22	7	64	1.3	15	5	298	4.01	7		ND	. 4	28		2	2.	88	.13	.054	10		-21		.13	-					9	
20+00E 4+75S	, * <b>4</b> ,	63	14	211	1.2	67	14	597	4.17	0	5	ND	5	27	1	5	2	39	.23	.081	13	54	.55	68	.06	3	1.75	.01	.06	<b>1</b>	- <b>7</b>	
20+00E 5+00S	2	50	2	104	.5	36	11	286	4.57	9	5	ND	3	35	1	2	2	66	.27	.045	8	74	.61	75	.11		1.16	.01	.05	1	2	
20+00E 5+255	3	94	2	81	.8	34	7	176	2.16	6	5	ND	3	38	1	2	2	52	. 46	.079	13	73	.55	103	.05		1.03	.01	.06	1	7	
20+00E 5+50S	1	46	8	- 64	.5	25	11	463	3.55	7	5	ND	3	. 41	1	2	2	67	.32	.053	10	- 67 -	.47	56	.08	9	.85	.01	.06	1	84	
20+00E 5+755	3	27	. 7	56	.2	23	L R	203	4.22	3	5	ND	1	44	1	2	2	79	.38	.051	8	73	.59	60	.12	2	1.02	.01	.05	1	1	
20+00E 6+00S	3	35	2	70	.3	25	12	340	4.07	9	5	ND	4	39	1	≦. <b> </b> 4	2	67	.35	.075	8	74	.65	83	.10	2	1.09	.01	.05	1	62	
																					· · · · ·					_						
20+00E 6+25S	3	78	1	78	·	39	16	528	3.74	9	5	ND	5	46	1	2	2	66	47	.076	10	- 74	.72	74	.11		1.07	.01_	.08	1	47	
STD C/AU-S	- 18	57	42	131	6.8	67	27	1027	3.87	39	18	8	38	49	17	17	20	58	44	.084	37	60	.87	176	.08	37	1.65	. 06	.13	14	47	

Grid | Page 15

Ć

1

ſ

(

C

(

C

Ĉ-

(

£

L

and service of the se

							D	D.	H G	EO-M	ANA	GEME	NTH	PROJ	ECT	-ARM	ADA	FI	LE	# 87	-42	50					<i>C</i> ,	, d	1		Pa	ige 16	
SAMPLE#	NO PPN	CU Ppm	PB PPN	ZN PPM	A6 PPM	- NI PPN	CO PPM	nn Ppn	FE	AS PPM	U PP <del>N</del>	AU Ppn	TH PPH	SR PPN	CD PPN	SB PPM	BI PPN	V PPH	CA Z	PI	LA PP#	CR PPN	MG Z	BA PPM	TI Z	B PPM	AL Z	NA Z	K Z	N PPM	AU‡ PPB		
20+00E 6+50S 20+00E 6+75S 20+00E 7+00S	3 1 1	113 148 50	3 5 9	84 52 103	.3 .2 .5	46 45 29	18 19 14	551 444 467	3.98 3.30 5.19	5 2 5	5 5 5	NÐ ND ND	3 2 3	51 50 36	1 1 2	2 2 2	2 4 3	67 80 80	.58 1.05 .30	.090 .122 .053	9 3 7	80 169 95	.74 3.27 .78	80 23 76	.11 .21 .15	2 7 12	1.18 2.36 1.50	.01 .02 .01	.10 .04 .07	1	6 1 1		
20+00E 7+255 20+00E 7+505	2 3	56 60	6 11	72 84	.5 .1	36 36	13 14	419 315	4.37 3.92	6	7 5	ND ND	4	43 39	2	2 2	2 2	.78 73	.38 .31	.031 .041	10 11	85 89	.62 .65	74 82	.12 .10	5	1.29	.01	.07 .08	1 1	7 44		
20+00E 7+755 20+00E 8+005 20+00E 8+255	1 1 2	71 53 36	5 9 9	77 77 74	.1 .1 .2	44 35 28	17 12 13	551 353 460	3.60 3.68 7.08	4 6 6	5 5 6	NÐ ND ND	5 3 3	46 33 26	1 1 2	2 2 2	2 2 2	64 67 100	.42 .28 .22	.050 .052	11 11 6	79 84 124	.68 .61 .44	68 55 47	.12 .08 .15	9	1.15 1.07 1.02	.01 .01 .01	.08 .09 .05	1	30 16 2		
20+00E 8+50S 20+00E 8+75S	2	29 60	9 5	61 74	.1	24 36	10 12	380 467	4.40	12	5	ND ND	23	29 23	1	2	2	72 77	.33 .29	.062	8 13	105	.45	76 95	.09	7	.84	.01	.05	1	3		
20+00E 9+00S 20+00E 9+25S 20+00E 9+50S	4 - 3 - 4	78 78 55	8 7 7	88 89 87	.7 .8 .1	50 50 38	17 15 11	652 536 384	3.73 4.24	7 9 8	55	ND ND ND	3 1 2	45 44 37	1 1 1	2 2 2	2 2 2	79 63 78	.49 .52 .28	.055 .037	10 8 12	98 90 103	.69 .62 .66	121 130 104	.08	5 2	1.33 1.25 1.29	.01 .01 .01	.11 .10 .09	1 1	81 32 16		
20+00E 9+75S 20+00E 10+005	8 - 3 -	118 61	13 . 9	151 89	.9 .2	66 39	19 15	1040 589	4.99 3.84	9	6 5	ND ND	2 3	43 - 34	2 2	2	2 2	77 68	.41 .29	.065	12 12	124 84	.69 .63	172 94	.08		1.83	.01	.14	1 1	26		
STD C/AU-S	19	61	39	133	6.9	67	27	1027	3.94	37	-19	7	39	- 50	18	19	20	58	.45	.085	37	60	.81	177	.08	30	1.67	.05	.13	14	51		

1

6

Ć

C

(

							D.I	э.н.	GEC	)-MA	NAGE	MEN	T PF	OJE		RMA	DA	FIL	E #	87-	4260	>					Grid	2			Page	17
SAMPLES	MU PPN	CU PPM	PB PPM	ZN PPN	46 PPH	NI PPM	CO PPN	MN PPM	FE Z	AS PPM	U PPM	au Ppn	TH PPM	SR PPN	CD PPM	SB PPM	BI PPM	V PPM	CA Z	Р 2	. LA PPN	CR PPN	116 Z	BA PPN	TI Z	B PPM	AL Z	NA Z	K Z	N PPN	aut PPB	
TEP 0+008L TEP 2+00E BL	1	10 20	8	44 55	.1	6 16	3	118 88	2.01	7 7	5 5	ND ND	5	10	1	4	2 2	37 23	.09 .08	.052 .031	. 7 10	18 18	.33	62 54	.10		1.22	.01	.09 .05	1	1	
TEP 2+50E BL TEP 3+00E BL TEP 3+50E BL	333	17 28 27	20 21 17	91 102 123	.1 .1 .7	15 14 26	4 4 7	108 91	2.45 4.18 3.13	12 15 10	5 5 5	ND ND ND	7 7 12	14 10 12	1 1 2	4 2 2	2 3 2	31 39 26	.15 .07	.040 .122 .092	14 12 14	18 25 26	.25 .25 .44	54 57 77	.07 .07 .06	2	1.07 1.47 1.89	.01 .01 .01	.06 .04 .11	1	1 1	
TEP 4+00E BL	5	30	15	86	.3	20	6		3.46	14	5.5	ND	6	11	2	2	2	26	.06	.049	17	23 19	.34	85 41	.05	2	1.28	.01	.09	1 2	1	
TEP 4+50E BL TEP 5+00E BL TEP 5+50 BL		16 21 14	21 12 5	55 67 33	.4	18 12	9	371 138	2.25	7	5 5 5	ND ND ND	8	15 15 10	1	2 3 4 2	2 3 3 2	21 18 18	.14	.030 .043 .022	17 15 10	23 20 15	.47 .45 .26	76 53 59	.06	- 11 2	1.23	.01 .01 .01	.16 .13 .08	2 1 2	1	
TEP 6+00 BL	1	12 16	- <b>6</b>	35 55	.1	10 12	5	91	1.56	- 7	- 5	ND	8	9	1	2	2	40	.08	.092	12	25	.35	62 85	.08	. 2	1.71	.01	.08	1 2	1	
TEP 7+00 BL TEP 7+50 BL TEP 7+90E BL	1 1 3	20 17 37	10 10 2	50 40 96	.1 .2 .2	18 15 33	7 6 8	187 256 493	2.20 1.82 2.32	3 2 10	5 5 5	ND ND ND	8 10 4	18 19 40 9	1	3 3 2 2	2 2 2 4	23 22 18 20	.23 .22 .58 .08	.050 .034 .048 .031	21 17 34 12	24 19 17	.52 .52 .25	84 106 65	.07	18 2	1.17 1.31 1.09	.01 .01 .01	.15	1	1 2 1	
TEP L8+00E 5+45N TEP L8+00E 5+00N	1	20 57	6 12	74 171	.1	42	5	273	1.91	3	5	ND	4	10	1	2	2	20 22 24	.11	.129	10	21 17	.31	107 53	.04	2	1.22	.01	.05 .05	· 1	- 1	
TEP L8+00E 4+50N TEP L8+00E 4+00N TEP L8+00E 3+50N	2 2 2 2	12 30 21	12 14 10	64 111 81	.1 .3 .7	10 20 23	4 10 7 7	145	2.01 2.21 2.30	6 4 2 5	5 5 5 5	ND ND ND ND	6 8 11 6	6 11 26 19	1	5 2 2 2	2 2 3 2	19 31 17	.06 .07 .20 .18	.125	10 12 21 14	16 22 20	.24 .37 .34	85 115 93	.03	6 4	1.17 1.57 1.49	.01	.05 .13 .08	2 1 2	1 1 1	
TEP L8+00E 3+00N TEP L8+00E 2+50N	2	13 19	3	81 99	.5	25 15 8	5		1.90 2.95 1.98	- 5	5	ND ND	· •	13	1	2 2	2	33 29	.11	.051	12 12	22 13	.30	76	.08	9	1.37	.01	.08	2	1	
TEP L8+00E 2+00N TEP L8+00E 1+50N TEP L8+00E 1+00N	2 2 1 27	12 19 11 127	8 19 16 27	61 70 44 693	.1 .3 .3 1.8	14 7 171	5 3 13	134 74 226	3.22	10 6 33	5 5 19	ND ND ND ND	7 7 15	7 10 56	1 1 14	2 2	2 2 2	32 20 67	.05 .08 1.63	.088	13 14 42	21 13 49	.25 .22 .23	63 53 114	.04 .06 .02	10	1.69 .77 1.54	.01 .01 .01	.05 .05 .12	1 1 2	1 1 10	
TEP LB+00E 0+50N	- 1 1	÷	12 13	92 50	.7	19 14	7	336 78	3.29	16	9 5	ND ND ND	12	10 10	1	2	2	24 22	.15	.071	20 12	23 18	.40	64 66	.01		1.36	.01 .01	.07	1	1 3	
TEP 8+50E BL TEP 19+00E 7+00N TEP 19+00E 6+50N	1	10 16 10	15 6 26 14	39 73 35	.1	13 9	5	104 68 129	1.55 3.03 1.57	5 2 3	5	ND ND ND	- 3 10 7	12 9 12	1	2 2 2 2	2 2 2 2 2	18 38 22	.12	.025	12 10 15	19 25 16	.38 .28 .25	51 66 49	.05 .09 .05	2 9 8	2.32	.01 .01 .01	.09 .08 .07	3 1 1	1 6 1	
TEP L9+00E 6+00N TEP L9+00E 6+00N TEP L9+00E 5+50N	I A 2 3	17 19	9	66 102	.1 .5	26 20	6		1.69	9	5	ND	7	56	1 2	2	2	15 23	.56	.079	22 15	19 23	.36	64 88	.05 .05	15 2	.81 1.23	.01	.12 .07	6	1 1	en Gelie Marcale
TEP 19+00E 5+00N TEP 19+00E 5+00N TEP 19+00E 4+65N TEP 19+00E 4+50N	4 4 19	73 46	13 7 23	289 123 387	.5 .5 4.3	91 41 225	9 7	887 484 1269	2.48 2.25 7.87	5 10 55	5 5 5	ND ND ND	6 4 7	15 35 25	1 1 1	2 2 3	2 2 2	17 16 22	.13 .41 .26	.041 .062 .084	14 18 19	19 19 36	.33 .38 .70	131 71 105	.02 .04 .02	3	1.37 .93 1.45	.01 .01 .01	.08 .13 .10	1 1 3	11 55 41	
TEP L9+00E 4+00N STD C/AU-S	1 18	16	9 . 38	69 131	.1 7.0	24 67	9	154 1051	2.20	3 37	5 17	ND 7	9 39	12 50	1 18	2 17	2 19	22 59	.12 .48	.042	16 39	25 60	.49 .88	78 182	.06 .08	. =	1.48 1.81	.01 .06	.11 .13	1 13	1 52	

с. С

6

Ć

4

ť

ſ

(

(

C

Ć

Υ. Υ							D	.D.H	1. GI	E0-M	ANA	SEME	NT	PROJ	ECT	-ARM	IADA	FI	LE	# 87	-42	60						61	d Z	•	Page	18
SAMPLE#	NO PPN	CU PPM	PB PPM	ZN PPH	A6 PPM	NI PPN	CO PPN	NN PPN	FE Z	as Ppn	U PPN	AU PPN	TH PPM	SR PPM	CD PPM	SB PPh	BI PPN	V PPM	CA Z	. Р 1	LA PPM	CR PPN	M <del>G</del> Z	- BA PPN	TI X	B PPM	AL Z	NA Z	K Z	N PPN	AU <b>t</b> PPB	
L9+00E 3+50N	2	19	8	130	.4	18	9		3.27	- 3	6	ND	9	15	1	2	2	30	.13		16	23	.37	78	.07	5	1.89	.01	.08	1	2	
L9+00E 3+00N	3	20	8	133	.1	18	6	136	3.04	2	5	ND	8	12	1	2	2	33	.09	.069	13	20	.31	91	.07		1.67	.01	.07	1	1	
L9+00E 2+50N	5	22	28	139	.8	-17	7.	167	3.94	- 10	5	ND	7	13	2	2	2	41	.09	.079	15	-30	.34	102	.08		3.05	.01	.08	1	2	
L9+00E 2+00N	3	25	-2	113	.6	30	8	142	2.85	6	5	ND	. 8	12	1	2	2	25	.10	.074	15	26	.37	105	.06	- 2	2.05	.01	.09	1	3	
L7+00E 1+50N	. <b>1</b> .	19	2	92	.2	23	7	114	2.29	4	5	NÐ	12	12	3	3	2	20	.13	.057	18	19	.40	82	.06	15	1.60	.01	.09	- 1 -	2	
L9+00E 1+00N	2	13	2	57	.1	18	-4	124	1.70	2	5	ND	8	15	1	7	2	18	.14	.022	18	17	.45	51	.06	5	1.07	.01	.10	1	1 .	
LY+00E 0+50N	-1	7	5	36	.1	. 3	- 3	130	2.19	-2	5	ND	6	13	1	2	2	43	.11	.123	9	19	.35	62	.08	5	1.34	.01	.11	1	2	
19+00E BL	2	5	2	20	.1	4	2	53	1.33	3	5	NÐ	. 6	8	1	3	2	16	.06	.039	12	8	.13	36	.04	4	.76	.01	.03	- 1	1.	
LY+SOE BL	- 1	. 7	4	30	.1	11	5	69	1.80	2	5	ND	6	11	1	2	2	22	.08	.036	13	17	.25	65	.05	4	1.37	.02	.07	1	3	
L10+00E 7+50N	1	4	1	143	.2	15	1	158	1.77	2	5	ND	7	12	4	2	2	20	.11	.055	15	25	.42	82	.07	2	1.08	.02	.09	1	1	
L10+00E 9+00N	1	18	4	126	.3	22	9	203	2.84	2	5	ND	9	13	2	2	2	31	.16	.205	14	20	.42	111	.08	5	1.37	.01	.10	1	2	
L10+00E 8+50N	1	- 9	2	84	.1	9	5	76	2.38	2	5	ND	9	13	1	2	2	32	.12	.122	12	14	.26	71	.07	10	1.38	.02	.05	1	1	
L10+00E 8+00N	3	19	5	123	.5	39	7	77		2	5	ND	7	11	1	2	2	11	.17	.117	21	12	.13	51	.01	2	.77	.01	.04	1 -	1	
L10+00E 7+61N	2	31	24	129	.3	40	. 9	329	2.95	11	5	ND	4	43	1	2	2	15	1.20	.156	29	18	. 38	69	.04	2	.75	.01	.12	1	1.1	
L10+00E 7+50N	4	-86	24	143	2.4	63	25	1511		2	5	ND	9	28	4	2	2	31	.33	.081	23	45	.67	148	.03	4	2.84	.01	.18	1	5	
								1						_	_	_	_						12									
L10+00E 7+00N	1	16	3	68	.3	19	7	132		2	5	ND	8	. 13	. 2	2	2	27	. 14		18	30	.51	100	.07		1.57	.02	.16	1	1	
L10+00E 6+50N	12	17	14	126	.2	39	- 8	449	2.24	- 4	5	ND	- 7	73	1	2	- 2	22	.60	.085	24	20	.36	114	.06		1.25	.02	.07	2	40	
L10+00E 6+00N	1	33	·	73	.8	34	10	484	2.60	10	7	ND	. 9	62	1.	2	2	26	51	.050	67	30	.61	128	.08		1.80	.02	.23	1	4	
L10+00E 5+50N	1.1	8	7	51	.3	12	6	90	1.68	- 3	- 5.	ND	7	16	. 1	4	2	20	.12	.053	15	19	.33	66	.05		1.26	.02	.08	1	1	
L10+00E 5+00N	1	12	7	59	.ó	16	6	76	2.08	2	7	ND	6	10	1	2	2	23	.07	.044	13	17	.27	- 64	.05	. 4	1.47	.02	.07	1	2	
L10+00E 4+50N	2	20	6	88	.1	14	7	286	4.03	6	5	ND	10	12	1	2	2	39	.11	.261	12	28	.35	56	.08	2	2.72	.01	.09	1	1.1	
L10+00E 4+00N	2	18	4	81	.3	24	- 8	148	3.13	6	5	ND	10	15	4	2	2	33	.13	.035	- 15	- 29	.50	. 95	.09	9	1.91	.02	<b>.</b> 14 .	1	1	
L10+00E 3+50N	· 4	36	4	201	.4	52	10	152	3.37	7	5	ND	- 9	12	1	2	2	24	.09	.047	17	30	.46	90	.05	2	2.26	.01	.10	1	3	
L10+00E 3+00N	1	25	13	78	.1	18	7	142	3.38	4	5	ND	7	16	1	2	2	32	.15	.109	15	-24	.49	88	.09	2	1.76	.01	.14	.1	2	
L10+00E 2+50N	3	19	13	118	.8	15	8	194	4.32	5	. 5	ND	11	22	3	2	2	46	.14	.281	16	29	.31	129	.10	2	3.34	.01	.10	1	2	
L10+00E 2+00N	1 -	16	12	58	.3	18	5	138	2.22	. 3	5	ND	9	12	1	2	2	22	.11	.044	14	20	.34	80	.05	2	1.66	.01	.08	1	14	
L10+00E 1+50N	8	50	22	194	. 3.1	32	8	200	6.50	15	5	ND	14	21	6	2	2	53	.11		15	46	.52	173	.13	2	5.94	.02	.21	2	1	
STD C/AU-S	20	62	38	129	7.5	69	29	1051	4.04	- 39	18	7	42	51	22	17	20	60	.45	.089	39	62	.90	174	.08		1.84	07-	-13	-12-	-53	
L10+00E 1+00N	4	27	14	201	.8	21	9	201		7	5	NÐ	10	12	1	3	2	38	.08	.187	15	27	.54	101	.11		2.36	.02	.17	1	1	
L10+00E 0+50N	1	12	13	76	.5	11	4	76	2.42	- 4	5	NĐ	9	9	i	2	2	29	.06	.087	16	19	.29	64	.07		1.52	.02	.07	1	1	
			2 <sup>- 1</sup>							_	_									450	4.4		75					<b>A1</b>	.12		,	
L10+00E BL	1	10	7	37	.1	11	4	111		2	5	ND	5	14	· . <b>I</b> .,	2	2	22	.13		12	17	.35	61	.06	_	1.10				2470	<ul> <li></li></ul>
FORK 6A	. 4	54	13	149	.7	61	17	1357	5.57	8	. 5	ND	3	35	5	. 4	2	88	.40	.059	11	79	.50	109	.07	5	.85	.01	.05			1.1
FORK 7A	· 7	. 74	12	209	.4	78	21	741	7.04	10	5	. ND	4	31	7	2	2	109	.37		8	88	.64	67	.07	2	.87	.01	.05	1	98 วมวก	
FORK BA	7	60	11	158	· • •	63	19	511	8.61	7	5	ND	2	30	10	2	4	162	. 34	.053	. 8	105	.69	50	.10	14	.17	.01	.04	2	2820	

Silt sample - 80 mesh

Grid 2

1

÷

(

(

( . .

6

### GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3HL 3-1-2 HCL-HN03-H20 AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 NL WITH WATER. This leach is partial for MN FE ca P La CR MG ba ti b W and limited for NA K and AL. AU detection limit by ICP is 3 PPN. - Sample type: Soil Aus analysis by an FROM 10 GRAM SAMPLE.

DATE RECEIVED: SEPT 25 1987 DATE REPORT MAILED: Oct 7/87 ASSAYER. D. Jugar. DEAN TOYE, CERTIFIED B.C. ASSAYER

D.D.H. GEOMANAGEMENT File # 87-4531 Fage 1

SAMPLE#	ND Pph	CU PPM	PB PPN	ZN PPN	AG PPM	NI PPH	CO PPN	nn PPn	FE	AS PPM	U PPM	au Ppn	TH PPM	SR PPM	CD PPM	SØ PPM	BI PPN	PPN .	CA Z	P Z	LA PPN	CR PPM	M6 7	BA PPH	TI Z	B PPM	AL Z	NA Z	K Z	N PPH	aut PPB	
L10+50E BL	1	9	5	48	.1	12	4	81	1.70	2	5	ND	- 6	11	1	2	2	16	.09	.037	14	16	.37	54	.05	3	1.32	.01	.11	1	· 1	
L11+00E BL	2	8	,	35	.3	8	3	82	1.59	2	5	ND	- 5	11	1	2	2	21	.11	.056	14	12	.26	39	.05	5	.87	.01	.07	- i	;	
L11+50E BL	ī	8	, 1	28	.3	- 5	2	50	1.73	2	5	ND	5	12	3	2	2	24	.11	.061	11	10	.13	42	.05	6	.84	.01	.05		· •	
	:	. 5	5	26		. 9	4	109	1.27	2	5	ND	3	. 9	1	2	2	16	.11	.022	12	13	.26	48	.05	. 4	.88	.01	.06	1	<b>1</b> -	
L12+00E 10+00N	1				-1						-	1.4					2														1	
L12+00E 9+50N	1	. 6	2	18	.1	8	3	75	1.06	2	- 5	ND	•	10	1	2	· 2	15	.11	.020	12	11	.23	33	.04	· 4	.61	.01	.07	1	3	
L12+00E 9+00N	1	3	2	13	.1	5	2	53	1.01	2	- 5	ND	3	8	1	2	2	16	.09	.020	- 11	9	.16	27	.04	2	.60	.01	.04	. 1	1.	
L12+00E 8+50N	1	4	- 5	22	- 1	6	3	65	1.30	2	. 5	ND	3	10	1	2	2	16	.10	.029	. 11	11	. 19	53	.04	5	.82	.01	.05	1	1	
L12+00E 8+00N	7	52	26	350	4.4	74	19	851	6.38	21	<u> </u>	ND	: 6	76	5	2	2	8	2.04	.357	-24	11	.19	87	.01	11	.50	.01	.08	1	4	
L12+00E 7+50N	2	10	8	67	.6	13	. 7	197	1.82	- 3	5	ND	3	27	1	2	2	32	. 38	.045	8	18	.73	145	.10	2	1.10	.01	.24	1	3	
L12+00E 7+00N	i	34	17	137	.6	38	10	573	3.03	2	. 5	ND	6	41	· 1	2	2	22	.94	.074	31	24	.52	142	.07	4	1.50	.01	.18	1	2	
L12+00E 6+50N	1	. 7	7	28	.5	. 6	2	93	1.14	2	5	ND	1	17	1	2	2	16	.23	.028	9	8	.13	55	.03	2	.57	.01	.04	1	- 3	
L12+00E 5+50N	2	27	18	118	.4	30	11		3.78	5	5	ND	10	12	í	2	2	31	.11	.072	14	29	,46	91	.08		2.58	.01	.09	1	1	
L12+00E 5+00N	1	3	. 2	7	.1	3	2	44	.57	2	5	ND	2	10	i	2	2	10	.08	.010	. 8	6	113	24	.03	2	.36	.01	.03	1	;	
	-		. 9	49		-	. 5			- 5	5	ND	5	26	1	2	2	22	.19	.073	10	. 17	.20	74	.04		1.57	.01	.04	- 1	2	
L12+00E 4+50N	-1	9	•		.1	16	_	96	1.80	-							2															
L12+00E 4+00N	1	28	22	83	.2	42	17	159	3.66	9	5	ND	12	24	3	2	4	31	.15	.057	. 17	34	.49	147	.08		2.98	.01	.19	· 1	2	
L12+00E 3+50N	1	10	- 9	36	.3	12	5	103	1.80	- 3	<b>7</b>	ND	6	15	1	2	2	20	.15	.030	12	20	.36	51	.06		1.11	.01	.10	1	1	
L12+00E 3+00N	1	14 -	6	47	.2	17	- 8 -	258	1.95	2	- 5	ND	5	22	1	2	2	22	.24	.027	16	24	.56	62	.07	2	1.18	.01	.18	1	1	
L12+00E 2+50N	1	10	12	55	.1	10	4	90	2.32	3	5	ND	8	14	1	3	2	25	.14	.098	12	19	.33	77	.05	3	1.60	.01	.09	1	1	
L12+00E 2+00N	1	8	2	22	· .1	5	2	224	1.02	2	5	NÐ	. 3	9	1	2	2	13	.06	.022	12	10	.18	45	.04	2	.71	.01	.05	1	. 1	
L12+00E 1+50N	1	11	3	43	.1	25	5	371	1.74	2	5	ND	3	22	1	2	2	20	.29	.037	12	20	.47	106	.06	2	1.03	.01	.21	1	2	
	•									-	·																					
L12+00E 1+00N	2	41	15	194	6	40	10	437	2.56	i 49	5	ND	6	38	4	2	2	26	. 41	.031	- 29	27	.67	136	.07	2	1.90	.01	.33	1	2	
L12+00E 0+50N	1	13	12	46	.3	14	5	109	2.31	- 3	5	ND	8	16	1	2	2	23	.15	.054	14	20	.43	66	.06	2	1.60	.01	.13	. 1	3	
L12+00E BL	6	17	13	42	1	10	2	55	1.44	5	- 5	ND	4	11	. 1	2	2	26	.09	.025	14	10	.19	50	.04	2	. 60	.01	.06	1	2	
L12+00E 0+50S	2	13	. 8	- 57	1.1	12	5	137	2.24	· 4·	5	ND	5	13	2	2	2	22	.10	.027	14	19	.37	68	.06	2	1.19	.01	.11	1	2	
L12+00E 1+005	1	14	14	.47	.1	n	- 5	192	1.94	2	5	ND	5	13	1	2	2	22	.12	.027	14	18	.41	68	.07	3	1.09	.01	.13	1	1	
	•		• 7		••	••		••••		. <b>-</b>			•		-		• • •								• • • •		•					
L12+00E 1+50S	1	8	3	30	.1	8	3	100	1.68	2	5	ND	3	15	2	2	2	23	.12	.032	13	17	.36	63	.06	2	.94	.01	.12	1	1	
L12+00E 2+005	1	14	12	34	.2	12	. 4	102	2.23	2	5	ND	7	14	1	2	3	21	.11	.025	12	22	.44	67	.06	11	1.47	.01	.16	1	1	
L12+00E 2+505	2	11	12	40	.8	13	5	264	1.85	6.	: 5	NÐ	4.	13	. 3	2	2	22	.09	.035	13	18	.29	49	.05	÷ 4	1.14	.01	.10	1	1	
L12+00E 3+005	1	5	12	21	.1	6	2	71	1.55	2	5	ND	2	12	1	2	2	25	.08	.018	12	14	.23	43	.06	2	1.05	.01	.08	- 1	1	1
L12+00E 3+50S	3	10	5	32	.1	8	2	86	1.22	· .	៍ទី	ND	1	- 11	1	2	2	21	.10	.019	11	12	.16	40	.03	2	.31	.01	.05	1	2	
E12400E 34303		10		32	••		۰. •		1144		_ <b>_</b>		<b>.</b>	••	•	•				••••	••	••		an da				•				
L12+00E 4+00S	1	24	. 18	53	.3	.19	. 7	213	2.92	6	° 5	NÐ	4	19	1	3	2	26	.16	.032	18	25	.55	93	.07		1.57	.01	.25	1	1	
L12+00E 4+505	1	25	17	59	.2	19	- 6	163	3.10	5	5	ND	5	10	2	2	2	28	.07	.091	14	26	.55	64	.07	2	1.38	.01	.12	1	1	
L12+00E 5+005	2	13	14	31	.5	7	3	88	2.06	5	5	ND	2	13	2	3	2	27	.12	.045	12	15	.25	56	.05	2	.96	.01	.08	1	1	j. No
L12+00E 5+50S	· ·	36	29	89	1.3	16	- Ā	222	3.90	18	5	ND	3.	14	2	2	2	36	.04	.069	14	19	.30	98	.07	2	.97	.01	.09	1	1	
L12+00E 6+005	- 1 I	13	12	32	1	9	4.	99	1.83	3	5	ND		14	1	2	3	18	.09	.034	15	15	.44	60	.06	2	.94	.01	.17	1	1	׊,
2.2.VVP 6.VVQ	•		••	~*	••										•																	
L12+00E 6+505	1	19	12	41	.1	12	5	149	2.15	2	5	ND	9	. 15	1	2	2	20	.11		19	20	.59	80	.07	· ·	1.28	.01	.28	1	1	
STD C/AU-S	19	59	38	132	7.2	68	27	1024	3.89	37	21	. · · 7	- 38	48	18	17	22	57	.40	.082	36	- 59	.87	175	.08	37	1.84	.05	.12	13	49	

									-							· · · -																	*.
SAMPLE	HQ PPH	CU PPM	PB PPN	ZN PPH	AG PPM	NI PPN	CO PPM	MN PPM	FE Z	AS PPN	U PPN	au Ppn	TH PPM	SR PPN	CD PPN	SB PPM	BI PPN	V PPN	CA Z	P 1	LA PPH	CR Ppn	M6 X	BA PPN	TI Z	B PPM	AL I	NA Z	K Z	N PPN	AUS PPB		
L12+00E 7+00S	5	26	17	57	.4	13	4	172		13	5	ND	3	20	1	2	2	42	.18		14	18	.22	71	.09	3	.78	.01	.10	2	1		
L12+00E 7+50S	2	12 8	7	26	2	9 5	3	75	2.14	2	5	ND	5	16	1	2	2	29	.11	.014	16	19	.32	77	.08	6	.89	.01	.14	1	1		
L12+00E 8+00S L12+00E 8+50S	1	17	8 17	19 27	.3 1.6	- 3 - 36	4	56 89	1.81 4.78	· 6	5	ND	1	6 10	1	2 2	2 2	21 53	.04	.062	13 12	13 120	.14	37 40	.05	2	.68	.01	.07	1	1		
L12+00E 9+00S	1	12	15	36		10	3	101	4.17	7	5	ND	2	8	1	2	2	27	.06	.069	11	25	.28	65	.10		1.20	.01	.09	- 1	1		
	•	••	••		• •		•		70.87	'	<b>-</b>	n.	. *		•	· •	•	<u></u>	. •••				. 29	00		· . •	1.40		••7	•	•		
L12+00E 9+505	2	16	14	40	2.8	8	3	153	5.20	10	5	ND	2	8	1	2	2	45	.04	.098	13	20	.22	41	.05	2	1.21	.01	.05	2	1		
L12+00E 10+00S	- 4	29	6	70	.3	22	2	68	1.46	41	5	ND	1	5	- 1	2	2	25	.02	.028	.17	11	.06	32	.01	2	.54	.01	.03	1	1		
L12+50E BL	1	11	5	37	.3	9	- 3	99	2.31	2	5	ND	7	14	2	3	2	22	. 13	.027	13	20	. 39	70	.06		1.30	.01	.13	- 1	2		
L13+00E BL	1	19	9	41	.1	20	· 7	161	1.75	3	6	ND	11	16	1	2	2	16	.19	.048	23	18	.43	-64	.06		1.22	.01	.18	1	1 .		
L13+50E BL	1	7	4	16	.3	- 4	2	192	.72	2	5	ND	2	23	2	2	2	14	. 30	.012	11	7	.10	50	.03	2	.32	.01	.06	1	1		
L14+00E 10+00N	-1.	9	10	50	.1	12	5	141	1.78	3	6	NÐ	1	12	1	2	2	24	.13	.011	12	21	.39	65	.07	2	.99	.01	.09	1	1 .		
L14+00E 9+50N	1	16	12	70	.2	20	. 8	155	2.47	3	5.	ND	8	16	- 1	2	2	26	.18	.049	12	22	.40	91	.08		1.38	.01	.16	i	1		
L14+00E 9+00N	ī	21	15	50	4	23	. 9	253	2.53	7	5	ND	5	28	1	2	2	29	.32	-	38	30	.58	123	.09		1.73	.01	.22	1	1		
L14+00E 8+50N	1	- 4	2	13	.1	4	2	50	1.03	2	5	ND	1	11	1	2	2	18	.12		8	12	.17	32	.05	- 2	.50	.01	.04	1	1		
L14+00E 8+00N	1.1	9	12	57	1	12	4	87	1.99	2	- 5	ND	141	11	2	2	2	21	.09	.042	11	19	.35	52	.06	2	1.14	.01	.08	Í	1		
	-												•	-		-	-					45											
L14+00E 7+50N	3	20	19	- 84	1.1	14	3	- 94	1.63	6	5	NÐ	. 3	9	1	2	2	18	.07	.044	11	15 25	.13 .32	78 121	.03	2	.79 .93	.01 .01	.04 .08	1 2	- 1		
L14+00E 7+00N L14+00E 6+50N	13 3	44 35	24 20	375 220	2.1	55 41	. 14	442 460	2.78 3.55	17 14	5	ND ND	2 5	20 13	1	2	2	22 31	.33 .18	.179 .038	13	23 34	.32	121	.10		1.56	.01	.15	2	1		
L14+00E 5+00N	14	-33	23	204	1.4	- 55	15	545	5.03	-17	- 5	ND	3	33	·	2	2	- 31 14	.58	.150	16	17	.18	. 77	.03	- 3	.84	.02	.05	2	1		
L14+00E 5+50N	3	29	14	100	1.0	31	7	195	3.89	7	6	ND	- 3	14	1	2	2	30	.14	.046	16	38	.55	79	.06		1.37	.01	.10	1	1		
217.002 0.000	. •	•,	• ·					•••		•			•		•	· • •	•		• • •							-		••••		•	-		
L14+00E 5+00N	3	28	16	105	1.6	32	. 8	202	4.91	- 4	5	ND	6	18	- 1	2	2	19	.37	.268	15	19	.17	64	.04	7	1.31	.01	.06	1	2		
L14+00E 4+50N	2	13	10	42	.2	9	4	148	2.61	. 4	5	ND	4	11	1	2	2	47	.11	.052	13	17	.31	58	.11	5	.86	.01	.08	1	1		
L14+00E 4+00N	1	- 17	13	55	.1	14	6	288	2.58	3	5	ND	6	14	1	2	2	27	.19	.025	15	24	. 40	83	.07	2	1.33	.01	.10	1	1		
L14+00E 3+50N	1	15	14	76	.1	12	- 7	534	2.85	2	5	ND	4	13	1	2	2	27	.18	.028	13	20	.35	86	.05		1.08	.01	.07	1	1		
L14+00E 3+00N	2	19	30	85	.3	. 18	11	1353	3.24	3	5	NÐ	4	14	1	2	2	26	.20	.035	14	20	.24	104	.04	3	.96	.01	.05	1	5		
L14+00E 2+50N	1	14	. 9	50-	.2	12	5	197	2.63	2	5	NÐ	-7	21	Э.	2	2	33	.28	.022	13	20	.34	66	.11	5	1.07	.01	.06	-1	1		
L14+00E 2+00N	3	17	10	64	-1.0	20	5	185	2.85	10	5	ND	6	20	1	2	2	19	.19	.104	15	16	.28	62	.05	6	.94	.01	.07	· 1			
L14+00E 1+50N	1	2	6	5	.1	1	1	- 24	.38	2	5	NÐ		8	1	2	2	6	.06	.006	12	5	.06	28	.02	2	.32	.01	.02	$\sim 1$	1		
L14+00E 1+00N	2	5	3	20	.1	5	ī	58	.94	3	5	NÐ	2	13	. 1	2	2	13	.15	.018	11	7	.10	39	.03	4	.38	.01	.04	- İ	1		
L14+00E 0+50M	1	19	16	40	.4	14	6	304	2.44	3	5	ND	2	21	1	. 3	3	25	.23	.026	21	19	.33	84	.06	8	1.02	.01	.13	1 <b>1</b>	1		4 1 - 1 - 1
																										1997) 1997 - 1997	÷						
L14+00E BL	1	11	14	38	.1	9	3	92	3.16	4	5	ND	2	13	1	2	2	35	.08	.035	13	22	.34	85	.08		1.19	.01	.13	1	1		
L14+00E 0+50S	1	18	12	37	.1	12	4	140	2.42	2	5	ND	1	17	1	2	2	29	.13	.028	11	26	.45	87	.07		1.30	.01	.19	1			Sett
L14+00E 1+00S	1	14	10	20	1.0	7	23	148	1.33	2	6	ND ND	1	22 11	1	2	23	20 26	.24	.022	12	11 18	.14	61 51	.05	2	.49	.01	.09	1	1		
L14+00E 1+50S STD C/AU-S	1	11 58	4	33	1.0	8	27	139 990	2.37	2 38	5 19	<b>RU</b> 7	35	47	-17	2 17	19	26 54	.05 .46	.029	36	18 64	. 27	171	.08		1.79	.05	.13	12	51		
JU 6/80-3	17	10		127	907	66	4	774	7.93	<b></b>	47		<del>.</del> Э	-1/		-17	17		, <del>1</del> 0	• • / •		UT.	100	474	***	74	****** 			••			
L14+00E 2+00S	1	26	16	62	.3	15	6	380	3.00	5	5	ND	3	30	1	2	2	29	.30	.033	19	24	:47	86	.08		1.62	.01	.25	2	1		
L14+00E 2+50S	1	13	10	31	2	9	3	117	1.83	2	5	ND	1	15	1	2	2	20	.13	.039	13	17	.30	60	.05	5	.74	.02	.13	1	1		
			. • .	1 A A A A A A			S. 1997			18 A. M. M.						20 C 10										1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -				1-1977 B. 196	网络拉马斯福州	집 영화가 있을까?	19229

Page 2

(

1

÷,

C

(

C

 $(\cdot$ 

C

(

C

Ċ

C

C

C

6

**C** -

**C**.

C

6, 22

																															•		
SAMPLE	NO PPM	CU PPN	PB PPM	ZN PPM	A6 PPM	NI PPM	CO PPN	nn PPn	FE	AS PPN	U PPN	AU Ppn	TH	SR PPM	CD PPM	SB PPM	BI PPM	V PPN	CA X	P Z	LA PPN	CR PPM	M6 2	BA PPM	TI Z	B PPM	AL Z	NA Z	K Z	N PPN	AUX PPB		
L14+00E 3+00S	2	29	12	66	.9	17	6	218	3.01	2	5	ND	4	22	3	2	2	32	. 18	.032	20	24	.51	109	.09	7	1.75	.01	.31	1	1.		
L14+00E 3+50S	1	15	4	36	1	12	4	140	1.97	2	5	ND	3	18	1	2	2	25	.19	.029	13	17	.51	75	.07	. 2	1.37	.01	.24	1	1		
L14+00E 4+00S	1	12	4	27	-1	10	4	158	1.42	2	5	ND	4	16	1	2	3	18	.16	.036	16	14	. 37	74 5	.05	5	.79	.01	.16	1	1.		
L14+00E 4+50S	1	7	13	22	- 1	5	2	55	2.41	2	5	NÐ	5	8	1	2	2	48	.05	.033	15	13	.25	48	.10	4	.87	.01	.09	2	2		
L14+00E 5+00S	1	9	10	18	.1	5	. 1	40	.96	2	- 5	NÐ	1	10	1	2	2	14	.07	.017	16	9	.15	40	.02	9	.52	.01	.07	2	1		
L14+00E 5+50S	2	. 6	9	14	.1	4	1	39	.76	2	5	ND	1	8	I	2	~ 2	18	.07	.014	11	8	.07	40	.02	2	. 39	.01	.03	1	1		
L14+00E 6+00S	2	8	- 9	19	-1	5	2	57	2.38	2	5	ND	2	8	1	2	2	39	.07	.022	10	11	.19	58	.09	2	.76	.01	.07	1	1		
L14+00E 6+50S	1	3	6	4.	.1	2	1	18	.31	2	5	XD	1	10	1	2	2	8	.08	.007	13	. <u>+</u>	.05	- 34	.02	2	. 35	.01	.03	1	1		
L14+00E 7+00S	4	9	14	23 46	1	5	1 2	142	1.01	4	-5 5	ND	1	14 8-	1	2	2	20	.09	.026	12	8	.08	-64	.02	2	.46	.01	.05	1	. 1 -		
L14+00E 7+50S	8	21	16	70	-,4	. 7	4	171	1.87	16		ND	1.	0	1	2	2	25	.06	.043	14	Ч.	.10	-68	.01	2	.58	.01	.04	1	1		
L14+00E 8+00S	3	23	12	72	.9	18	10	1527	2.13	6	· . 5	ND	2	85	. 4	2	2	23	. 82	.050	18	15	.19	127	.03	4	.87	.01	.06	1	1		
L14+00E 8+50S	1	. 9	8	17	.1	5	2	94	1.02	4	. 5	ND	1	9	÷ 1	2	4	23	.04	.021	22	8	.09	24	.03	2	.40	.01	.03	1	. 1		
L14+00E 9+005	2	9	- 13	17	.2	6	2	105	1.24	4	5	ND	3	6	1	4	2	27	.03	.025	16	7	.09	21	.03	2	.46	.01	.04	. 1	2		
L14+00E 9+50S	5	25	15	175	.3	21	- 14	2290	3.66	13	5	ND	3	89	. 4	2	2	28	.91	.112	16	23	.32	125	.03		1.74	.01	.07	1	1		
L14+00E 10+00S	6	27	10	220	2.0	61	8	3147	2.83	15	9	ND	2	68	32	2	2	21	1.31	.141	15	21	.32	124	.02	4	1.46	.01	.07	1	5		
L14+50E BL	1	17	11	55	.3	14	- 5	173	2.75	3	5	ND	. 4	23	1	2	2	27	.31	.089	13	20	. 40	71	.06	7	1.48	.01	.13	1	1		
LIS+00E BL	2	21	10	51	.2	18	. 7	352	2.18	2	5	ND	3	37	2	2	2	22	.84	.041	24	19	.44	83	.06	2	1.48	.01	.16	1	1		•
L15+50E BL	1	14	- 14	25	.4	8	3	82	1,99	2	5	ND	1	14	1	2	2	27	.09	.026	14	13	.19	47	.05	8	.77	.01	.07	1	1		
L16+00E 10+00N	i, 1	11	12	65	-1	10	7	139	2.17	2	5	ND	. 6	- 14	1	2	2	23	.13	.040	11	17	.27	91	.05	- 3	1.64	01	.12	1	1		
L16+00E 9+50N	1	10	- 7	32	.1	9	14	77	1.63	4	5	ND	4	. 9	1	2	2	17	.10	.036	12	14	.28	38	.05	2	. 98	.01	.09	1	1		
L16+00E 9+00N	1	- 18	15	54	.1	20	. 8	323	2.08	- 34	5	ND	6	17	1	2	2	21	.20	.035	27	21	.46	80	.06	10	1.32	.01	.15	2	1		
L16+00E 8+50N	1 I	13	8	31	.1	13	4	82	1.65	6	5	ND	4	12	. 1	2	2	24	.11	.020	8	17	.34	73	.07	8	.93	.01	. 10	2	1		
L16+00E 8+00N	1	9	7	28	.1	10	4	93	1.99	3	5	ND	6	15	-1	2	2	23	.13	.029	12	16	.41	52	.05	6	.96	.01	.09	1	1		
L16+00E 7+50N	1	20	7	43	.1	18	5	122	2.69	10	. 5	ND	6	13	1.	2	2	30	. 08	.023	11	23	.44	53	.08	4	1.23	.01	.14	1	1		
L16+00E 7+00N	1	14	16	- 38	.1	14	6	188	2.17	- 3	5	ND	- 4	16	1	2	3	25	.17	.020	13	20	.47	71	.08	9	1.12	.01	.23	1	1		
L16+00E 6+50N	1	15	-14	39	.1	12	5	454	1.78	12	5	ND	.4	29	1	2	2	22	.52	.024	22	17	.33	84	.05	6	1.09	.01	.12	.1	1		
L16+00E 6+00N	1	9	. 4	30	1	27	7	322		3	5	ND	3	18	i	2	2	38	.40	.017	9	62	.90	82	.07		1.10	.01	.05	1	-1		
L16+00E 5+50N	i	19	5	50	.3	18	8	390	2.22	10	10	ND	<b>4</b> .	31	1 i	2	2	25	.58	.032	26	23	.51	105	.07		1.59	.01	.23	1	1		
L16+00E 5+00N	1	11	6	22	.1	8	3	73	1.56	2	5	ND	1	11	· 1	2	- Ā	20	.08	.015	11	13	.30	56	.05	-3	.78	.01	.11	1	1		
L16+00E 4+50N	1	24	5	55	.1	17	6	134	3.71	5	5	ND	6	17	1	4	2	34	.14	.058	11.	26	.53	76	.09	11	1.96	.01	.13	1	1		
L15+00E 4+00N	11. J. J. J. 1. J.	27		71		14	. 7	198	3.03		5	MP	•	25	•		2	. 44	.21	.028	13	22	.53	72	.10	10	1.10	.01	.14	100 A	1		
L16+00E 3+50N	- 1	21	6 12	36 45	.1	16 14	- 6	238	3.57	2	5	- XD XD	2	19		2	2	51	.12	.035	13	19	.43	89	.11	5	1.00	.01	.15	1	1		
L16+00E 3+00N	2	14	14	- 34	.6		3	125	3.13	2	5	- ND -	4	17	1	- 3	2	27		.036	13	17	.30	65	.06		1.54	.01	.12	i	t i		
L16+00E 2+50N	1	8	10	19	.2	5	2	57	1.35	2	5	ND	1	10	1	2	2	25	.08	.029	10	.11	.18	48	.07	2	.61	.01	.06	i	1		
L16+00E 2+00N	:	27	24	25	.1	12	3	131	2.83	·	5	i ND	2	14	2	2	2	37	.32	.043	13	18	.18	33	.07	7	.67	.01	.08	2	i		
		•			•••					- <sup>7</sup> .						- <b>-</b>						1.						a a					
L16+00E 1+50W	3	17	12	24	.1	11	3	98	2.27	2	5	ND	3	15	1	2	2	40	.12	.017	14	18	.27	48	.11	6	.88	.01	.17	1	1	196	13.) 13. 13.
STD C/AU-S	10	58	40	130	6.8	68	27	1038	3.96	40	25	. 7	. 38	49	17	17	21	59	.46	.086	37	59	.89	177	.08	37	1.85	.06	.13	13	48		6 d. 1

and the second 
Page 3

(

Ć

*(*...

Ţ

Ç

¢

C

-(°

E

(

(

C

C

(

C

C

C

€

C

Grid 2

SAMPLE	NO PPM	CU PPM	PB PPN	ZN PPM	A6 PPN	- NI PPH	CO PPN	NN PPH	FE Z	AS PPN	U PPN	AU PPN	TH PPM	SR PPM	CD PPN	SB PPM	BI PPN	V PPM	CA Z	P Z	LA PPN	CR PPM	M6 Z	BA PPN	TI. Z	B PPM	AL X	NA	K Z	N PPM	AU# PPB	
L16+00E 1+00N	1	15	8	20	.3	5	2	70	2.44	2	5	ND	4	11	2	2	2	26	.08	.024	14	15	.15	56	.07	7	.93	.01	.08	1	1	
L16+00E 0+50N	1	4	8	10	.1	2	· 1	56	.76	2	5	ND	2	9	· 1	3	2	20	.05	.014	16	7	.07	42	.04	9	.47	.01	.06	1	1	
L16+00E BL	1	13	2	32	.2	8	3	113	2.21	2	5	ND	2	15	-1	2	- 2	26	.10	.049	14	16	.29	64	.06	7	1.08	.01	.12	1	1	
L16+00E 0+50S	41	69	26	178	6.8	97	11	404	5.11	17	5	ND	8	.11	2	2	2	35	.10	.103	23	31	.42	137	.06	5	3.61	.01	.26	. 1	1	
L16+00E 1+00S	1	10	9	25	.1	6	. 3	88	2.37	2	5	ND	2	14	1.	2	2	30	.11	.028	14	17	.29	58	.07	3	1.30	.02	.10	1	1	
L16+00E 1+505	1	16	2	41	.1	12	1.6	202	1.88	2	5	ND	- 5	21	2	2	2	26	. 18	.037	21	22	.56	- 96	. 08		1.33	. 02	. 28	1	1	
L16+00E 2+00S	1	23	7	60	.2	21	9	281	2.30	2	5	ND	6	33	2	2	2	24	.45	.049	45	25	.62	142	.09		1.05	.01	.35	1	. 1	
L16+00E 2+50S	- 1	13	2	47	.2	10	4	108	3.07	2	7	ND ND	5	18	3	2	2	28	.12	.035	15	23	.40	87	.07		1.68	.01	.14	2	1	
L16+00E 3+00S	1	13 19	8	33	.3	10 15	: 4 5	129 155	2.39 2.83	2 2	· 9	ND ND	3	12 15	1	2	2	25 26	.09	.033	16 19	20 25	.41 .59	60	.07	7	1.34	.01	.20	1	1	
L16+00E 3+50S	. 1	17		. 47		IJ	J	100	2.03	. 4	. 1	NU	-	13	•		<b>ک</b>	20	.12	.047	17	23	.37	69	.07	. (	1.49	.01	.25	1	1	
L16+00E 4+00S	1	15	- 4	36	.3	9	- 4	226		2	7	ND	<b>4</b> .	15	2	2	2	26	.08	.032	17	-20	.42	136	.07		1.13	.01	.22	1	1	
L16+00E 4+50S	1	20	12	44	.2	15	5	129	2.84	÷ 4	5	ND	9	12	1	2	2	25	.07	.031	- 19	28	.60	77	.08	2	2.42	.01	.23	1	1	
L16+00E 5+00S	1	13	11	24	.3	. 17	3	92		2	- 5	ND	2	11	1	2	2	34	.08	.065	12	18	.26	57	.07		1.01	.01	.12	1	1	
L16+00E 5+50S	16	24	11	85	1.3	22	4	425	2.81	- 7	5	ND	2	. 0	1	2	2	32	.04	.107	15	13	.13	51	.03	. 7	.73	.01	.06	1	1	
L16+00E 6+00S	2	- 11	15	25	.6	- 6	2	351	1.97	. 3	5	ND	1	· 9	. 3	. 4	2	28	.07	.127	13	11	.10	37	.05	4	.59	.01	.04	1	1	
L16+00E 7+00S	8	15	17	46	.7	11	2	111		14	5	NÐ	2	. 8	2	2	2	32	.03	.047	14	10	.08	39	.03	2	.50	.01	.04	1	. 1	
L16+00E 7+50S	1	15	- 9	39	7	<u> </u>	2	.50	1.56	15	- 5	ND	. 4	4	2	3	2	34	.02	.029	19	8	.06	47	.02	7	. 47	.01	.05	2	1	
L16+00E 8+005	28	31	28	108		13	2	105	3.31	- 69	5	NÐ	4.	. 7.	1	9	2	68	.01	.057	23	11	.03	- 40	.01	. 3	. 48	.01	.03	· .*	4	
L16+00E 8+50S	18	38	16	118	1.9	19	4	103		30	5	ND ND	1	14	2	.3	2	41	.08	.039	18	17	.16	116	.03	6	. 95	.02	.06	- 1	1	
L16+00E 9+005	2	21	14	43	.4	12	3	118	5.27	13	5	NU	4	6	1	2	2	58	.03	.071	18	22	.20	28	.02	7	1.24	.01	.04	1	. 1	
L16+00E 9+50S	3	25	12	52	÷ .4	13	4	258	6.57	10	5	ND	2	7	-1	2	2	53	.02	.053	17	26	.21	41	.03	5	1.28	.02	.04	1	1	
L16+00E 10+00S	6	34	14	75	.4	- 21	7	263	5.62	11	5	ND	2	8 -	- <b>1</b> 1	2	2	44	.05	.066	21	25	.19	58	.02	2	1.18	.02	. 05	-1	12	
L16+50E BL	5	23	11	45	.6	12	5	565	2.20	2	5	ND	3	27	2	2	2	18	. 46	.069	22	16	.23	28	.04	2	1.05	.01	.09	. 1	1	
L17+00E BL	1	20	-9	40	.4	- 14	-4	- 119	2.96	. 2	5	NÐ	3	9	1	2	- 2	36	.04	.032	14	24	.36	- 74	.07	. 6	1.36	.01	.10	1	2	
L17+50E BL	- 1	6	2	s. <b>4</b>	.1	3	1	15	.52	2	5	ND	1	5	1	2	2	13	.05	.009	15	. 4	.01	20	.01	3	.24	.01	.02	. 1	1	
L18+00E 10+00N	1	8	4	11	.1	2	1	55	.75	2	5	NÐ	· . 1 ·	10	1	2	2	18	.10	.013	6	6	.08	35	.03	2	.51	.01	.05	1	1	
L18+00E 9+50N	1	26	15	75	•1.2	17	8	943	1.98	25	. 5	ND	6	57	1	2	2	20	1.31	.064	163	21	.29	92	.05	2	2.82	.01	.16	1	1	
L18+00E 9+00N	1	22	7	- 44	.3	9	2	148	1.05	2	5	ND	1	29	1	- 3	2	23	.37	.019	14	- 10	.07	110	.05	2	.40	.01	.05	3	2	
L18+00E 8+50N	1	15	7	56	.3	16	8	331	2.53	2	5	NÐ	4	19	2	2	2	27	.23	.023	15	26	.50	75	.08	6	1.69	.01	.18	1	9	
L18+00E 8+00N	1	23	9	59	.1	22	10	378	2.97	11	5	ND	10	21	1	2	2	31	.12	.020	42	31	.61	123	.12	- <b>3</b>	2.26	.01	.27	1	1 <b>1</b>	
L18+00E 7+50N	1	16	3	49	.1	13	5	356	1.51	4	6	ND	3	53	1	2	2	17	1.34	.035	40	17	.32	68	.05		1.07	.01	.17	2	1	
L18+00E 7+00N	. 1	- 11	2	33	1	11	4	118	1.92	2	5	ND	.7	13	1	2	3	23	.12	.008	14	17	.42	.59	.08	2	1.10	.01	.16	2	1	
L18+00E 6+50N	1	34	12	56	.9	24	8	681 276	2.66	3	5 5	ND ND	6	19	1	2	2	31 21	.20	.026	25 21	20 18	.27	124 86	.07	2	1.43	.01	.17	1 2	1 1	
L18+00E 6+00N	1	20 9	6	39 24	.3	: 13 8	8		1.91	2	ຸວ 5	ND	4	17 17	1	2	2	21	.17	.024	11	13	. 28	50	.06	2	.91	.01	.10	2	្នុំ	
L18+00E 5+50W	1 <b>1</b> 	<b>7</b>	2		.2		•	221	1.67	2	J	AV			<b>4</b> (	<b>.</b>	4			.020	1					17				6		
L18+00E 5+00N	1	15	6	35	.1	13	7	274	3.06	3	5	MÐ	7	27	2	2	2	26	.40	.029	15	22	.46	70	.10	3	1.31	.01	.20	1	1	
STD C/AU-S	19	62	37	133	7.3	70	29	1061	3.89	41	. 19	. 8	39	51	17	17	22	60	.48	.087	38	61	.88	182	.08	29	1.84	.06	.13	12	52	

Grid 2

f

£.

 $T_{i}^{1}$ 

-

(

C

(

(\*\*

C

C

(

C

C

(

Ç-

6

(

ſ

C

Page 4

Grid Z D.D.H. GEOMANAGEMENT FILE # 87-4531 Page 5 SAMPLER Ctt PB ZN A6 NI 63 FE Ħθ MN AS 11 AU TH SR CD 58 BI CA p LA CR 86 BA ŤΙ AL # AUX B NA ĸ PPH PPH PPH PPM PPH PPN PPN PPN PPH 7 PPM PPH PPN PPH PPN PPH PPH PPN PPN z PPN PPN Z PPH z 2 2 1 z PPM PPR L18+00E 4+50N 18 2 82 .12 6 A .1 5 1.61 2 2 15 27 .017 1 5 2 2 2 9 12 .21 40 - 06 4 .72 .01 . 08 L18+00E 4+00N 29 18 52 10 .5 3 1.41 11 29 4 17 5 NÐ 1 2 2 25 .51 .054 16 16 .16 76 .03 4 . 46 .01 .05 1 L18+00E 3+508 13 34 12 5 232 1.53 1 11 .1 3 5 ND 5 23 2 .44 .034 18 59. 2 14 16 .45 .05 2 .89 Ť .01 .17 5.07 L18+00E 3+00N 38 74 28 7 199 82 13 9 46 1.2 5 ND 6 1 2 3 30 .07 .061 23 22 .43 47 .07 2 1.33 .01 .20 . L18+00E 2+50N 19 19 45 20 111 3.41 17 2 .4 4 5 ND Q 2 2 41 .10 .078 10 42 .44 46 1 .03 2 1.34 .01 .04 ŧ L18+00E 2+00N 2 15 30 .3 12 18 114 3.07 19 5 2 35 .03 .20 32 4 MG 1 2 .060 12 20 .04 2 1.31 .01 .05 4 L18+00E 1+50N 32 12 30 135 1 .3 18 6 2.62 A 5 NÐ R 2 65 .053 24 59 .22 2 . 95 1 .1 3 .16 4 .46 .01 .05 1 1 L18+00E 1+00N 1 13 8 30 .2 9 3 86 3.77 6 5 NÐ R 2 2 45 . 06 .051 4 1 11 21 .28 48 .08 7 1.19 .01 .11 1 1 32 L18+00E 0+50N 13 17 .3 3 81 2.51 5 5 мÐ 2 7 20 1 11 2 2 .04 .039 11 23 .30 37 .06 2 1.19 1 .01 .07 1 1 L18+00E BL 1 7 10 4 .1 3 1 22 .87 2 5 ы 5 2 4 2 19 .02 .019 14 1 .06 19 .03 .35 4 .01 .04 1 L18+00E 0+50S 2 16 12 33 .8 10 3 79 4,56 13 5 2 32 .03 .059 26 36 5 2 10 .26 .11 4 2.05 .01 .08 1 1 L18+00E 1+005 .10 9 18 59 157 1.40 5 NÐ 32 . 06 23 1 .3 4 5 1 7 1 2 2 .018 10 88 .28 .04 2.57 .01 .02 5 1 L18+00E 1+50S 13 9 34 .2 10 . 97 2.31 5 ND 2 5 3 2 17 .02 13 17 .33 t 6 .040 40 .05 2 1.16 .01 .09 1 1 L18+00E 2+005 6 37 .78 3 8 22 .7 5 1 4 6 NÐ 3 5 5 2 2 14 .04 .016 14 6 107 25 .03 6 .28 .01 .04 2 1 L18+00E 2+50S 79 1 10 9 20 .4 4 2 2.38 2 5 MS 1 11 2 2 29 .05 .035 11 14 .22 41 .05 2 .85 .01 .12 t 1 L18+00E 3+005 1 13 12 21 .6 7 2 55 1.92 3 5 10 2 2 26 .08 .028 12 14 .21 42 .06 5 .77 .01 .13 1 .97 L18+00E 3+50S 11 13 .3 3 154 3 17 .05 .024 10 9 38 .05 2 . 48 1 6 1 5 ND 8 2 2 .12 .01 .06 1 1 1 1 L18+00E 4+00S 1 2 13 4 .1 1 1 58 .46 ٦ 5 ND 2 5 2 2 3 16 .03 .021 14 5 .06 22 .06 7 .30 .01 .04 1 1 L18+00E 4+50S 14 15 34 3 235 2.81 5 ND 2 2 29 .03 .077 14 .23 45 .07 2 .75 1 .1 10 4 6 2 18 .01 .07 1 1 1 L18+00E 5+00S 1 4 13 8 .1 3 1 34 .96 3 5 NÐ 3 5 2 2 19 .03 .016 13 7 .10 25 .05 5 .43 .01 .05 1 L18+00E 5+50S 1 2 -5 .1 2 1 45 .29 5 2 2 .03 .009 11 .04 18 .03 2 .23 .01 .02 1 4 2 Q 4 1 1 12 32 .70 5 ND .03 31 .03 2 .52 L18+00E 6+00S 1 5 11 .1 4 1 1 6 2 2 13 .019 11 8 .14 .01 .03 1 1 1 L18+00E 6+50S 3 19 10 61 .5 17 2 303 1.55 9 5 NÐ 2 11 2 2 28 .11 .023 17 11 .07 105 .02 3 .45 .01 .05 Ŧ . 1 L18+00E 7+005 33 29 36 102 19 20 976 2.74 26 6 ND 19 3 2 10 .17 .074 9 9 .06 112 .01 6 .54 .01 .05 14 3.0 1 2 1 L18+00E 7+50S 22 27 14 116 2.8 29 3 60 2.42 8 5 ND 2 2 35 .01 .034 20 12 .04 54 .01 3 .43 .01 .04 2 2 1 . L18+00E 8+00S 23 39 77 .4 19 3 58 2.36 10 2 27 .03 .026 15 8 .03 49 .01 2 .34 .01 .02 1 8 5 ME 5 2 1 1 L18+00E 8+50S 11 36 11 80 113 2.41 12 5 ND 2 33 2 2 27 .37 .035 13 12 113 .02 2 .65 .01 .04 .9 20 3 1 .12 1 1 L18+00E 9+00S 22 185 42 250 8.4 60 18 3403 6.18 44 5 ND 2 94 3 3 2 37 .80 .164 30 36 .46 226 .03 10 2.95 .01 .12 1 - 6 12 32 L18+00E 9+505 18 30 88 3 95 31 5 ND 2 19 .08 .01 2 .71 .01 2 18 .3 16 3.77 1 5 . 1 2 66 .01 .060 .03 1 L18+00E 10+00S 18 23 8 68 .3 20 2 81 2.17 17 5 11 5 3 2 32 .03 .032 15 12 .10 40 .01 2 .52 .01 .03 1 12 1 L18+50E 8L 21 45 216 5.99 2 29 .08 .046 33 .45 34 .11 2 1.77 .01 .10 2 26 .6 14 18 -5 7 2 10 1 4 -5 1 .03 .05 17 .02 3 .51 .02 L19+00E BL -5 13 28 .79 7 ND 2 2 17 .018 10 .01 1 1 6 .2 3 T 4 1 5 3 6 1 L19+50E BL 1 13 10 27 .4 9 2 98 2.86 6 5 ND 1 5 1 2 2 35 .03 .059 8 17 .21 19 .06 2 .93 .01 .07 1 1 37 .52 S L20+00E 10+00N 1. 8 18 38 .2 7 3 101 1.54 2 5 MD 3 7 3 2 2 24 .04 .013 8 8 .11 .04 .01 .03 1 1 L20+00E 9+50N 1 8 12 114 .2 3 162 1.97 3 4 2 2 11 .04 .032 8 .70 40 .09 ..... .92 .01 .25 1 1 1 L20+00E 9+00N .30 1 6 2 8 .1 2 -1 20 . 69 2 5 2 2 18 .01 .010 9 6 .03 16 .02 3 .01 .02 1 1 6 1 36 1.81 STD C/AU-S 18 38 133 66 27 1027 3.85 39 18 37 17 19 57 .48 .082 36 .88 175 .08 .06 .12 12 - 51 60 7.1 7 49 18 61

6

ſ

t

(

€

C

C

C.

Ć

£

(

#### Grid 2 Fage 6 D.D.H. GEOMANAGEMENT FILE # 87-4531 SAMPLE# MO CU PB ZN AG NI CO HN FE AS TH SR SB CR TI H AU CD 91 CA Ρ LA MG BA B AL NA ĸ ¥. AUX PPN PPH **PPH** PPH PPn PPN PPN PPN 7 PPN PPN PPH PPN PPH PPN PPN PPM PPM PPH 7 PPN PPN 2 1 PPN 7 7 Z PPH. PPB 2 120+00E 8+50N -14 28 2 61 2.49 .08 .033 11 .17 39 .09 2 1 6 •6 - 7 5 -3 10 1 2 2 40 -11 .68 .01 .07 1 f L20+00E 8+00N 14 â 36 .4 12 4 94 4.11 2 5 NÐ 2 12 1 2 2 34 .06 .027 10 23 .40 46 .09 2 1.20 .01 1 .10 1 1 L20+00E 7+50N 2 .1 24 .40 2 5 15 .09 .008 9 5 .03 28 .01 3 .22 1 8 -5 3 1 NÐ 1 1 2 2 10 .01 .02 1 1 L20+00E 7+00N 19 5 33 .2 11 :4 117 2.44 2 5 NÐ 2 12 2 30 .10 .028 34 18 .31 56 .0B 2 1.43 1 1 2 .01 .17 .1 1 .2 L20+00E 6+50N 24 19 272 2.35 13 2 .09 72 22 79 .05 1 8 61 10 5 3 2 23 .050 .47 2 2.72 .01 .19 1 1 1 L20+00E 6+00N 1.99 19 8 -38 .1 12 5 268 22 .14 .040 22 18 .41 .05 4 1.31 .01 3 -5 16 1 2 2 61 .18 1 L20+00E 5+50N 7 2 13 •1 4 1 66 .63 2 5 ND 10 1 2 3 13 .11 .013 13 7 .07 49 .03 2 .33 .01 .05 1 2 1 L20+00E 5+00M 8 75 2 33 7 1 14 18 .1 7 3 2.18 5 NÐ 16 1 2 2 26 .14 .022 18 11 .20 .07 .97 .01 1 .08 1 1 21 L20+00E 4+50N 1 40 15 25 .1 -14-4 89 2.11 2 5 ND 1 1 2 3 16 .21 .080 43 13 .28 64 .02 4 1.58 .01 .12 1 -1 2 L20+00E 4+00M 16 5 35 .1 13 4 115 2.34 5 5 14 1 2 2 21 .13 .023 15 21 .46 56 .07 3 1.44 .01 1 ND .16 1 1 L20+00E 3+50M 1 32 9 26 .2 12 3 86 2.49 - 5 2 16 2 21 .16 .042 27 14 .20 42 .06 2 1.19 .01 .09 1 2 1 58 12 L20+00E 3+00N 14 6 8 .1 2 2 .86 2 5 ND 6 1 2 2 13 .12 .017 4 .02 43 .01 2 .32 .01 .05 1 1 1 1 L20+00E 2+50N 10 10 18 .2 6 2 51 3.02 4 5 NÐ 3 11 2 2 37 .11 .017 12 13 .19 43 .09 4 1.15 .01 .10 1 1 1 - 1 19 27 39 22 15 .08 .043 .52 36 .09 2 2.35 L20+00E 2+00N 1 .64 88 .3 36 9 172 5.12 5 ND 5 1 2 2 34 .01 .11 1 1 5 L20+00E 1+50N 35 10 48 .6 -24 111 4.14 7 5 NÐ 9 2 .151 12 40 .45 66 .11 2 1.34 .01 .10 2 1 1 - 1 L20+00E 1+00M 35 .53 .02 .031 .05 22 .01 2 .47 .01 .02 11 7 7 1 - 5 2 - 8 .1 - 3 1 2 -5 -5 1 2 2 - 1 1.29 .01 13 .09 14 .02 2 5 .3 70 5 3 3 22 .023 9 .44 .01 .02 20 L20+00E 0+50M 1 13 14 9 2 5 1 8 1 1 L20+00E BL - 37 16 32 .3 13 4 123 3.44 19 5 ND 13 2 2 32 .04 .051 20 16 .19 30 .05 2 1.01 .01 .06 1 4 1 1 1 1.08 15 .07 19 .01 3 .50 L20+00E 0+50S 1 11 8 14 .1 7 2 107 4 5 NÐ 1 9 1 2 2 14 .04 .030 8 .01 .04 1 1 L20+00E 1+00S 12 -7 13 3 104 1.42 5 2 16 .06 .038 16 7 .07 33 .01 3 .55 .01 .03 1 1 .1 1 2 1 L20+00E 1+50S 12 .02 18 .30 21 .08 4 .86 .01 11 10 25 .2 3 166 1.94 29 .032 8 .11 1 2 7 2 2 2 58 .02 .022 10 27 .01 2 .54 L20+00E 2+005 7 2 7 .1 . 59 2 -5 ND 2 3 11 6 .06 .01 .02 1 4 1 1 -5 1 1 L20+00E 2+505 10 14 .5 94 1.98 2 5 ND 7 1 2 2 30 .02 .033 12 10 .13 26 .07 4 .71 .01 .06 1 2 4 1 1 6 1 .03 13 10 .17 32 .06 2 .84 L20+00E 3+005 5 5 2 76 1.83 2 5 7 2 2 25 .029 .01 .07 2 1 6 16 .4 ND 1 1 1 L20+00E 3+50S 17 15 41 14 116 3.68 7 2 2 59 .04 .064 14 29 .27 52 .10 2 1.18 ..01 .06 1 3 1.0 4 4 - 6 ND 1 .062 .19 40 .07 2 .78 .01 .05 L20+00E 4+00S 12 23 .3 2 58 2.45 -5 34 .06 13 -14 1 6 - 2 -3 2 2 - 1 1 8 3 2 40 .59 2 .04 .009 10 10 .10 24 .03 .34 .01 .03 L20+00E 4+50S 8 3 2 5 2 15 1 1 1 3 • .1 -1 1 6 1 3 .27 5 2 .01 .010 9 5 .02 19 .01 2 .20 .01 .01 L20+00E 5+00S 5 2 1 .1 1 2 ND 4 1 2 6 1 1 1 1 - 1 33 22 .03 .015 13 .05 .23 .03 9 .23 .01 .02 L20+00E 5+50S 3 18 7 2 1.11 2 5 ND 1 2 2 6 1 1 3 10 .1 1 6 208 12 .06 .026 22 33 .59 143 .13 2 2.56 .01 .26 L20+00E 6+00S 3 36 24 91 1.2 28 10 4.45 7 5 2 2 2 45 4 1 35 .35 89 .07 2 1.42 .01 .13 L20+00E 6+50S 23 18 62 18 864 2.93 25 2 2 .039 20 23 .40 1 1 1 .ŧ -14 :3 2 5 2 22 35 .02 .032 14 16 . 20 36 .08 .64 .01 .05 L20+00E 7+00S 10 68 .2 18 188 3.09 2 2 1 1 6 4 . -5 6 1 31 109 .3 570 2 2 25 .02 .034 15 11 .10 50 .02 2 .58 .01 .04 1 -1 L20+00E 7+50S 7 19 18 9 1.98 5 5 Min 8 3 .28 5 1.37 .03 21 34 .07 .01 .06 2 L20+00E 8+00S 3 32 15 81 ..8 17 5 127 3.68 7 .5 . 7 2 2 25 .050 16 1 1

L20+00E 8+50S

L20+00E 9+00S

STD C/AU-S

10 186

17 67

19

58

22 222

31 121

41 131 7.2

6.1

.9

62 15

26

67

- 8

623 4.45

27 1039 3.86

622 4.43

20

19

39 21

7

5

23

24

1

37 50

8

2

1

17 18 20 59

2

3 2

2 29 .16 .067

> 36 .13 .082

> > .46 .086

31 26 .37

20 21 .28 106 .03

37

60 .86 178 .07

91 .04 2 2.18

3 1.28

36

1.83

.01 .12

.01 .07

.05 .13 1 1

1 . 1

13 48

0

ŧ

1

C

C

Ć

(

€

(

(

(

C

0

(

											•••••					. • •														-		raçe	
SAMPLER	08 1991	CU PPM	PB PPM	ZN PPM	. A5 PPN	NI PPM	CO PPM	HN PPM	FE Z	AS PPM	U PPN	au Pph	TH PPM	SR PPN	CD Pfn	SB PPM	BI PPN	V PPH	CA Z	2	LA PPN	CR PPN	MG - 2	. BA Ppn	TI X	B PPN	AL Z	NA Z	K Z	W PPN	AUX PPB		
L20+00E 9+50S	21	118	41	349	4.3	63	27	6213	5.33	35	5	ND	3	47	5	2	2	31	.42	.215	23	26	.33	124	.02	3	2.43	.01	.09	1	1		
L20+00E 10+005	36	51	18	134	.1	17	3	150	6.79	45	5	ND	4	5	1	5	2	39	.03	.090	13	14	.11	40	.03	2	.61	.01	.04	. 1	1		
L20+50E BL	1	18	20	39	.3	12	3	135	2.91	12	5	ND	1	7	1	2	2	40	.04	.053	9	17	.37	30	.07	- 2	1.08	.01	.07	1	1		
L21+00E BL	1	3	5	5	.1	2	- 1	16	1.36	2	5	ND	1	5	. 1	2	2	26	.02	.025	13	6	.07	23	.05	2	. 63	.01	.04	1	3		
L21+50E BL	1	20	- 6	47	.2	11	. 4	151	2.51	2	5	ND	5	10	2	2	6	22	.06	.040	18	21	.56	70	.06	2	1.67	.01	.21	1	1		
L22+00E 10+00N	1	. 11	13	23	.5	4	2	77	1.51	4		ыñ	•	15	<b>,</b>	•		77	. 11	070		10	17	10		·	E0.		47				
L22+00E 9+50N	1	18	13	54	.3	- 6		136	2.77	5	5	ND ND		15 -11	2	2		23 28	.16	.028 .024	9 14	10 20	.17 .42	40 49	.05	2	.58 1.49	.01	.07	1	1		
L22+00E 9+00N	i		7	26	.1	7	3		2.52	2	- 5	ND	2	13	1	2	2	40	.10	.064	10	15	.28	48	.11	2	.74	.01	.16		2		
L22+00E 8+50N	1	. 11	- 11	31	.2	10	Ă	117	2.29	3	5	ND	2	15	1	3	3	22	.12	.042	13	18	.40	69	.06		1.20	.01	.14	1	· 7		
L22+00E 8+00N	i	21		62	.1	15	7	233	3.18	4	5	ND	- 3	16	i	3	2	35	.09	.024	20	26	.60	96	.11		1.99	.01	.25	1	1		
L22+00E 7+50N	1	7	6	- 14	.2	4	-1	44	.85	2	5	ND	1	13	1	2	2	21	.11	.011	9	6	.13	34	.05	10	.40	.01	.06	2	1		
L22+00E 7+00N	1	20	12	82	.1	21	10	414	2.43	· 4	ć	NÐ	3	52	1	2	2		1.29	.051	18	25	.53	90	.06	7	1.31	.01	.27	1	1		
L22+00E 6+50N	. 1	25	20	95	.2	29	8	261	2.97	7	7	ND	2	59	1	. 2	2		1.65	.048	47	29	.34	53	.06	2	1.39	.01	.11	1	1		
L22+00E 6+00N	1	28	15	50	.5	10	- 4	161	3.64	10	- 6	ND	4	14	1	2	2	29	.20	.040	42	16	.31	36	.11		1.45	.01	.16	1	1		
L22+00E 5+50N	1	18	-17	74	.9	12	5	732	1.85	5	5	ND	4	81	1	2	2	15	3.04	.077	98	. 14	.14	92	.03	. 3	2.15	.01	.06	1	1		
L22+00E 5+00N	1	- 8	9	- 24	.1		1	85	1.11	2	.5	ND	1	10	- 1	. 4	2	27	.13	.017	10	6	.08	46	.04	2	.47	.01	.04	3	2		
L22+00E 4+50N	3	11	26	10	.1	, Å	1	19	.63	2	5	ND	1	9	1	2	2	10	.06	.025	16	4	.03	37	.01	3	.61	.01	.02	1	1		-
L22+00E 4+00N	2	12	9	17	1	3	1	65	.94	2	5	ND	ī	11	1	. 6	2	16	.17	.021	- 9	5	.07	54	.02	3	.42	.01	.04	· 1-	2		
L22+00E 3+50N	2	10	2	7	.3	1	1	33	.71	2	5	ND	-1	- 5	1	2	2	. 9	.03	.026	, 9	2	.03	27	.01	3	.58	.01	.04	i.	2		
L22+00E 3+00N	2	5	2	7	.1	. 3	1	21	.64	2	5	ND	1	- 4	2	2	2	16	.02	.010	8	4	.03	15	.02	4	. 38	.01	.03	1	1		
				× _												1		17 L							·					_			
L22+00E 2+50N	2	6	3	3	1	. 1	1	11	.50	2	-5	ND	- 1	4	1	3	2	10	.02	.012	8	4	.04	17	.01	2	.44	.01	.03	1	1		
L22+00E 2+00N	2	3	2	2	1	11	- 1	25	.29	2	5	ND	1	, <b>, 4</b> ,	-1	2	2	5	.06	.022	8	2	.03	21	.01	2	.47	.01	.02	1	1		
L22+00E 1+50N	2	21	6	11	-1	2	. 2	104	2.71	3	. 5	ND -	3	5	1	- 4	2	29	.04	.024	. 9	5	.11	15	.05	2	.61	.01	.04	1	3		
L22+00E 1+00N	2	3	. 4	3	.1	1	1	24	.52	3	5	ND	. 1	4	1	2	2	13	.01	.011	.12	. 3	.05	17	.02	7	.50	.01	.02	1	2		
L22+00E 0+50N	2	2	2	3	.1	1	- 1	19	.31	2	5	ND	1	3	· 1	2	3	7	.01	.009	- 11	2	.01	13	.01	2	.21	.01	.02	1	1		
L22+00E BL	· 1	13	8	22	.8		2	117	3.37	2	5	ND	3	7	1	2	2	39	.02	.051	12	16	.21	29	.08	3	1.18	.01	.08	ť	1		
L22+00E 0+50S	2	- 6	6	7	· .4	2	- <b>1</b>	36	.86	2	5	ND	1	5		3	3	11	.02	.031	10	5	.10	14	.03	2	.41	.01	.03	ĩ	2		
L22+00E 1+00S	1		. 8	18	.1	10	3	95	1.22	9	5	ND	•	.5	- 1	2	2	27	.01	.019	- 11	10	.13	19	.04	2	.52	.01	.03	3	1		
L22+00E 1+50S	· i	18	19	31		11	. 3	151	3.66	6	5	ND	3	7	1	2	2	33	.04	.047	13	17	.22	29	.07	2	1.05	.01	.06	1	1		
L22+00E 2+00S	1	11	18	26	.1	8	3	79	3.13	5	5	ND		8	2	2	2	42	.04	.053	11	20	.27	56	.07		1.01		.06	· 1	· 1		
L221005 21003	- <b>*</b> .		10	20	• • • •	•	3	·. /7	3.13	3	3		<b>.</b>	•	4		· 4		.00	.035		24				-	1.41			•	۰. •		
L22+00E 2+50S	1	-13	13	31	.2	8	3	82	4.49	6	5	ND	2	10	1	2	2	38	.09	.051	. 11	20	.26	38	.08	2	1.23	.01	.07	1	.1		
L22+00E 3+005	1	8	7	18	.1	31	3	76	2.75	3	5	ND	2	11	1	3	2	50	.10	.023	10	70	.24	50	.07	2	. 68	.01	.05	1	2		
L22+00E 3+505	1	7	11	18	.1	7	2	- 66	1.72	3	5	ND	· ī	. 9	1	2	3	37	,06	.015	10	22	.20	33	.06	2	.58	.01	.03	1	1		
L22+00E 4+00S	2	20	14	20		10	3	73	1.37	4	: 5	ND	ī	13	1	2	2	22	.16	.020	16	13	.22	56	.04	2	.90	.01	.05	1	1		
L22+00E 4+509	1	9	5	30	.1	9	4	137	1.37	2	5	ND	1	13	1	2	2	20	.17	.022	15	15	.39	49	.05	3	1.03	.01	.10	្វ	2		
			-		1					-														taale Al									
L22+00E 5+00S	2	° 1, <b>4</b>	· · · · 7.	7	1	3	1	29	.52	2	5	ND	1	8	. 1 <b>1</b> 1	2	2	13	.05	.007	14	8	.15	27	.07	2	.45	.01	.05	1	_1		
STD C/AU-S	. 19	59	39	135	6.9	69	28	1058	4.03	40	18	9	39	50	18	18	21	59	.49	.094	37	60	.90	178	.08	37	1.82	.06	.13	13	52		
					- No. 1 (S.	2010 BBB							e - 186												11 I I I I I I I I I I I I I I I I I I	1-0.66°,						그 문제 김 씨상	1949

- And Barriel

Page 7

£

2

Е.

C

Ć

C

€.

(

C

(

1

(

(

0

C

(

ŧ

C

Gil Z

· · · · ·									1	D. D.	<b>H.</b> (	SEOM	ANA	SEME	NT	FI	LË	# 87	-45	31							0,7	° -			. 1	Page	8
SAMPLE	- 110 PPH	CU PPM	PB PPN	ZN PPM	AG PPM	NI PPN	CO PPM	HN PPN	FE %	AS PPM	U PPM	AU PPH	TH PPM	SR PPM	CD PPN	SB PPM	BI PPN	V PPM	CA Z	P Z	LA PPM	CR PPN	MG Z	BA Ppm	TI X	B PPH	AL Z	NA Z	K Z	N PPN	AUX PPB		
L22+00E 5+50S	1	- 14	17	27	.2	9	3	117	2.88	2	5	ND	· 4	9	1	2	2	36	.08	.022	12	18	.20	47	.10	2	. 88	.01	.07	· 1	1		
L22+00E 6+00S	3	- 16	. 9	37	.3	12	4	100	3.90	- 4	5	NÐ	5	11	2.	2	2	43	.06	.024	15	26	.41	68	.13	5	1.59	.01	.17	1	1		
L22+00E 6+50S	1	18	10	25	.1	. 9	- 3	67	1.46	2	5	ND.	- 1	9	. 1	2	2	25	.05	.017	17	15	.28	60	.08	2	1.17	.01	.14	1	2	•	
L22+00E 7+00S	5	19	17	48	.1	14 -	- 7	501	2.61	3	5	ND	2	17	2	. 2	2	38	.16	.038	19	22	.35	68	.07	2	1.45	.01	.13	1	1		
L22+00E 7+50S	2	31	17	37	-6	16	. 4	122	3.02	2	- 5	ND	2	18	2	2	2	34	.16	.043	25	20	.29	63	.08	2	1.48	.01	.13	2	1		
L22+00E 8+00S	3	27	17	69	1	21	8	245	3.01	2	5	ND	4	18	1	2	2	34	.17	.033	29	27	.52	90	.09	2	2.03	.01	.21	1	1		
L22+00E 8+50S	1	24	9	68	2	20	- 10	477	2.56	2	5	ND	5	26	2	. 2	2	30	.35	.040	23	25	.60	133	.09	. 7	1.90	.01	.30	1	1		
L22+00E 9+00S	5	- 30	- 15	80	.4	23	- 13	547	3.51	3	5	ND	3	25	1	2	2	42	.21	.060	28	31	.63	135	.08	2	2.53	.01	.26	1.	1		
L22+00E 9+50S	4	39	24	95	• •7	25	- 19	1136	3.80	9	5	ND	3	35	2	2	2	40	. 38	.080	39	32	.61	148	.06	9	2.78	.01	.23	1	1		
L22+00E 10+005	11	39	.44	74	.6	14	4	119	5.02	28	5	ND	14	56	1	2	2	41	.51	.045	24	18	.16	77	. 08	2	1.10	.01	.06	1	3		
L22+50E BL	1	6	8	- 4	-1	2	2	40	.67	2	5	ND	1	3	1	2	2	16	.02	.012	6	4	.04	12	.02	2	.45	.01	.04	1	1		
L23+00E BL	- 1		2	1	.2	2 <b>1</b>	1	80	.23	2	- 5	NÐ	1	3	- 1	2	2	4	.02	.010	13	2	.01	18	.01	- 4	. 38	.01	.02	1	1		
L23+50E BL	1	. 9	13	15	4	. 4	2	· 97	2.79	- 2	5	NÐ	3	7	1, 1	2	2	32	.06	.030	11	15	.14	31	.06	. 4	1.27	.01	.04	1	1		
L24+00E 10+00N	1	20	15	32	.2	. 7	_ 3	55	5.30	3	5	ND	· 8	7	1	2	2	54	. 02	.037	16	24	.27	45	.11	3	1,37	.01	.10	1	1	•	
L24+00E 9+50N	2	16	18	27	-1	6	2	67	4.60	2	5	ND	6	13	-1	2	2	40	.12	.049	14	22	.20	55	.07	2	1.17	.01	.08	. 1	- 1		
124+00E 9+00N	2	22	12	46	.2	11	4	119		, <b>4</b> 1	5	ND	4	17	2	2	2	29	.11	.033	16	26	.35	64	.07		1.64	.01	.13	1	1		
L24+00E 8+50N	. 1	28	17	115	.2	58	: 6	260	2.79	2	- 5	NÐ	3	63	. 1.	2	2	30	.52	.036	29	20	.32	95	.08		1.23	.01	.13	1	1		-
L24+00E 8+00N	2	30	25	73	7	13	- 4	278	4.09	- 4	5	ND	4	16	2	2	3	57	.13	.042	: 15	30	.69	68	.12	5	1.56	.01	.12	1	1		
L24+00E 7+50N	.2	27	39	73	.5	10	4	187	3.39	2	5	ND	1	13	3	2	- 2	. 39	. 11	.043	17	17.	.27	53	.06	2	.98	.01	.08	1.	1		
L24+00E 7+00N	1	25	18	. 84	1	10	2	72	1.96	2	5	ND	1	8	2	3	2	28	.03	.032	11	8	.11	64	.02	2	.80	.01	.04	1	1		
L24+00E 6+50N	1	7	- 17	31	.2	3	1	33	.79	2	. 5	ND	2	. 8	1	3	2	17	.06	.019	11	. 4	.03	41	.01	2	.52	.01	.04	1	1		
L24+00E 6+00N	1	17	120	120	.1	6	· 3	226	2.50	2	5	ND	3	11	. 1	2	2	- 29	. 08	.024	16	- 7	.12	-47	.08	- 4	.61	.01	.09	1	1		
L24+00E 5+50N	1	9	12	. 8	.1	3	1	56	.51	2	.5	ND	1	6	- <b>1</b>	2	2	16	. 05	.014	16	7	.03	45	.03	9	.24	.01	.05	1	1		
L24+00E 5+00N	<u> </u>	. 17	21	30	- 1	9	3	110	1.91	2	. 5	ND	3	18	1	2	2	23	. 05	.038	45	. 14	.20	44	.04	5	. 84	.01	.10	1	1.		
L24+00E 4+50N	3	44.	19	113	1.0	37	7	294	5.56	4	5	ND	. 4	19	1	2	3	72	.07	.055	20	107	1.16	73	.16	2	3.27	.01	.20	1	1		
124+00E 4+00N	2	. 18	12	41	.1	9	. 5	233	3.91	4	5	ND	2	13	.1	2	2	36	.09	.034	14	16	.33	60	.10		1.60	.01	.24	1	1		
L24+00E 3+50N	1	- 4	6	. 4	· .1	2	1	-33	54	. 2	- 5	ND .	2	-4	. 1	2	2	16	.02	.012	10	5	.06	18	.04	10	.58	.01	.04	1	1		
L24+00E 3+00N	1	7.	7	13	.1	• • 4	2	81	.99	2	5	ND	1	6	2	2	· 2	14	.04	.019	7	8	.11	27	.02	- 3	.75	.01	.07	1	2		
L24+00E 2+50N	1 - 1	11	13	20	.1	. 6	2	57	3.26	3	5	ND	4	. 7	. 1	2	2	39	.03	.038	13	16	.19	30	.09	2	.95	101	.07	1.	1		
L24+00E 2+00N	. 1	11.4	. 9	6	.1	1	1	61	.50	2	5	ND	1	5	, <b>1</b>	2	2	13	.03	.016	6	5	.05	27	.02	4	.48	.01	.05	1	- 1-	in de la constante Norma de la constante de la cons	

L24+00E 1+50N

L24+00E 1+00N L24+00E 0+50N

L24+00E 0+50S

L24+00E 1+00S

STD C/AU-S

L24+00E BL

1 3 -5

1 10

1

2 - 9

1

1 9

19 60

10 11

18

2 .1

.1

.1

.2

.3

6.8

21 22

35 .1 11

25

128

17

12 11

8

13 39

46 .19

86 3.60

3 59 2.48 28 1022 3.78

106 3.34 82 3.43

42 2.63

1

2

3

1

4

1

6

6

5

7

69

2

3 5

2

2

2 - 5 ND 3

39 20

-5

5 ND

5 ND

5 ND

> 7 38 49

4 9

3

3

Gridz

2 .56 2 1.27

4 1.17

2 .89 3 1.24

2 1.46

37 1.78

15 .01

47 .08

26 .06

42 .10

.09

.24 39

.86 177 .08

18 13 .23

17 .27

60

.01 .015

.03 .030

.03 .033

.03 .035

.02

.027

44

35

58

2 4

23

2

2 2 41

2 2

2 2 40 .02 .028

2 2

17

2

1

2 2 2 29

2 18

· 6

3 3 .04

13 19

13

12

15 22 .39 41 .08

15

37

.01

.01

.01 .10

.01 .05

.01 .13

.01 .12

.06

.04

.09

.13

1

1

1

2

1

1

1 1

1

1

1.

13 50 (

(

1

Ċ

ť

(

Ç

(

(

C

(

C

C

Ċ

Grid Z Page 9 D. D. H. GEOMANAGEMENT FILE # 87-4531 AUX CA LA CR TI 1 SAMPLE ΗÛ CU PB ZN AG NI CO NN FE ۵G Δti TH SR CD 58 21 υ ø PPN Z 1 PPN PPN 7 PPN 7 PPH 7 z z PPH PPR PPN . 2 PPH PPN PPH PPH PPN PPN PPh PPH PPN. PPH PPM PPN PPM PPH PPH 56 .07 2 1.64 .01 .16 1 .023 .29 1 L24+00E 1+50S 27 79 2.03 5 2 2 2 25 .04 16 19 15 .2 ₹ .0 R 1 16 Q 2 22 .04 -026 14 16 .26 42 .05 2 1.30 .01 .11 1 1 L24+00E 2+00S 14 8 25 .3 8 3 102 2.09 q 5 ND 1 7 -1 2 1 .030 12 14 .26 49 .05 2 1.12 .01 .12 1 1 .05 L24+00E 2+50S 9 20 .3 7 2 63 1.07 5 5 ND 1 A 1 2 2 16 10 1 34 7 2 26 .04 .021 9 8 .10 30 .06 2 .63 .01 .03 1 1 L24+00E 3+005 1 5 ę 8 .1 3 1 1.37 3 5 ND 1 1 2 25 .031 14 19 .40 61 .07 2 1.60 .01 .11 1 L24+00E 3+505 103 2.32 2 5 ND 2 10 2 2 .06 1 15 16 28 .4 10 3 1 .05 .016 13 36 .04 2 .84 .01 .06 1 1 L24+00E 4+00S 49 .82 2 3 14 12 .20 15 2 2 5 9 1 9 13 .4 \* 25 2 .56 12 .08 .03 .01 .03 22 .72 2 2 14 .03 .017 6 1 1 L24+00E 4+50S 5 2 5 ND 7 1 8 5 .3 3 1 ÷t. .1 12 .21 47 .05 2.68 .01 .06 1 . 85 5 ND 13 2 2 13 .08 .030 11 1 L24+00E 5+00S 7 12 11 .1 5 1 56 2 1 1 1 .32 2 1.26 .09 19 48 .05 .01 1 339 1.95 5 NÐ 11 2 2 31 .06 .041 12 1 L24+00E 5+50S 19 13 25 .3 10 5 . 1 1 1 . 09 .028 14 .26 55 .08 2 1.11 .01 .07 1 L24+00E 6+00S 15 29 .2 272 2.12 ٦ 5 мñ 2 13 2 2 31 14 1 1 8 9 . 1 .07 .022 26 .62 82 .08 2 1.85 .01 .16 1 1 L24+00E 6+50S 18 223 2.58 12 2 2 29 19 17 56 .1 7 5 3 1 9 .013 7 .08 31 .07 2 .40 .01 .03 1 1 7 2 2 33 .04 11 L24+00E 7+005 11 2 65 1.18 2 5 ND 2 1 6 9 .1 4 1 23 .07 2 .62 .01 .04 5 2 30 .05 .017 11 9 .12 1 L24+00E 7+50S 10 13 13 .2 2 39 1.60 3 5 ΝÐ 2 9 1 2 t 6 60 .07 3 1.04 .01 .10 1 1 15 2 29 .12 .022 14 20 .42 2 2 L24+00E 8+005 1 13 39 .2 13 4 141 2.13 4 5 ND 1 á 2.86 .05 1 1 .08 .031 16 .23 39 .03 .01 13 364 1.39 5 9 2 21 17 L24+00E 8+50S 3 31 19 49 .5 4 8 ы'n 1 1 \* .01 .08 1 26 .09 .032 17 16 .27 56 .05 2 1.06 L24+00E 9+00S 2 20 17 39 .3 12 -5 228 2.14 5 13 2 2 ŧ 17 50 .05 3 1.17 .01 .10 1 1 25 .07 .026 .36 22 12 32 .3 12 128 2.01 -5 ND 2 11 1 2 2 16 L24+00E 9+50S 4 5 1 .28 56 .08 2 .86 .01 .10 1 Ť 105 2.18 3 2 9 2 2 32 .05 .018 11 15 L24+00E 10+00S 1 15 9 22 .1 8 3 5 ND 1 .05 4 .34 .01 .02 1 .06 16 1 .47 2 5 ЫŊ 2 4 2 2 14 .02 .011 12 4 L24+50E BL 2 17 · 1 1 2 11 2 .1 1 .72 .02 .017 9 .12 29 .08 3 .01 .06 1 1 2 2 26 14 L25+00E BL 10 10 .3 4 41 1.60 2 5 1 6 1 13 52 .06 62 .87 176 .08 37 1.84 .13 STD C/AU-S 27 1028 3.92 -38 18 7 37 49 18 17 20 57 .45 .086 36 18 59 37 131 7.0 88

r

ŕ

į:

.(

í

(

C

Č

C

C

Ċ

(

C

C

C

6

C.

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. VAA 184

PHONE (604) 253-3158 FAX (604) 253-1716

6

ł

1

ť

C

(

t

C

(

(

# GEOCHEMICAL ANALYSIS CERTIFICATE

## ICP - . 500 GRAN SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HHO3-H20 AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR HM FE CA P LA CR HS BA TI B W AND LIMITED FOR WA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-SOIL/SS P2-ROCK AND ANALYSIS BY AN FROM 10 GRAM SAMPLE.

					G	SEC.		HE	:M1	CA	JL.	A	NA		s:	IS		EF	ST.	IF	IC	A	ΓE					,			
				ICP -	.500	GRAM S	AMPLE	IS DI	SESTED	WITH 3	L 3-1	-2 HCL	-HNO3-	H20 AT	95 DEC	C F	OR ONE	HOUR	NIO IS	) )ILUI	ED TO	10 HL	WITH W	ATER.			Ch	pck	An	24/y.	s 03
				this - San	PLE TY	PE: PI	-\$01L/	SS 12-	ROCK	AUX					ed for Gran Si			. AU I	DETECT	10W L1	NIT BY	ICP I	5 3 PP	<b>H.</b>			Gri	d	1		
DATE RECEI	VED	00	T 19 :	1987					Mai	-	N		2/8,	7	AS	SSAY	ER.	A.	Je,	P1.	DEAI	N TC	YE,	CER	TIF	IED	B.C.	. As	SAY	IR	
					S	ANGU	INE	TTI	ENG	INEE	RING	5 PR	OJEC	CT-A	RMAL	A	Fi	le #	87	-503	9	Pa	ge :	Ľ							
SAMPLEN	MO PPM	CU PPM	PB PPN	ZN PPH	AG PPH	NI PPH	CO PPN	IN PPN	FE	AS PPH	U PPH	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPH	CA Z	P Z	LA PPN	CR PPH	NG X	BA PPN	TI Z	B PPN	AL I	NA Z	K I	N PPN	AUX PPB
FORK LS+OOE 3+00N	4	62	6	76	.4	33	14	393	3.12	5	- 5	ND	4	29	ľ	2	2	.34	.36	.051	10	44	.59	38	.06	6	.86	.01	.06	1	2
FORK 15+00E 2+75N	10	84	24	191	.7	63	19	813	5.70	2	5	ND	6	19	1	2	2	27			24	41	.51	46	.04	7	1.06	.01	.04	1	24
FORK LS+00E 2+50N	9	108	19	215	1.2	83	- 23		5.16	- 3	5	ND	9	23	2	2	2	27	.28	.087	45	43	.60	69	.04		1.57	.01	.04	· · 1	11
FORK 15+00E 2+25N	5	42	.15	97	.6	32	- 7	279		1	5	ND	- 3	20	1	2	2	39	.15	.127	16	43	.42	50	.04		1.14	.01	.05	1	4
FORK L5+00E 2+00N	· 8.	65	24	181	1.2	51	16	644	8.12	9	5	ND	2	13	1	2	3	37	.10	.108	16	49	.38	51	.03	5	1.73	.01	.04	- 1	7
FORK 15+00E 1+75N	11	40	17	219	2.1	52	14	399	6.74	4	5	ND	5	17	1.	2	2	42	.10	. 155	16	59	.48	145	.10	7	2.36	.01	.05	1	2
FORK L12+00E 5+255	- 4	65	16	142	.8	35	12	456	3.88	-7	5	ND	3	42	1	2	2	44	.66	. 068	11	60	.50	108	.06	. 6	1.66	.02	.08	1	23
FORK L12+00E 5+50S	5	72	9	151	1.2	80	: 21	748	4.78	1	- 5	ND	3	66	2	2	2	60	. 87	.096	10	159	1.07	- 77	.07		1.91	.02	.08	- 1	32
FORK L12+00E 5+755	6	134	21	206	3.5	110	25		5.48	. 5	. 5	ND	. 3	82	4	2	2		1.00	.101	27	177	1.01	167	.05	7	2.64	.02	.16	1	57
FORK 68 P	4	30	- 4	82	.2	35	10	538	3.07	5	- 5 -	ND	4	24	- 1	2	2	36	.23	.035	10	43	.50	53	.04	9	.72	.02	.05	1	5
FORK 78	6.	44	- 11	120	.4	46	12	587	3.10	5	5	ND	: 3	23	1	2	2	30	.26	.045	9	55	.52	66	.03	6	.73	.01	.06	. 1	
FORK SA P	7	48	10	- 134	.4	49	12	483	3.17	. 6	- 5	ND	4	22	1	2	2	30	.23	.045	. 9	- 46	.51	55	.03	5	.74	.01	.05	. 1	. 3
FORK 9A P	7	59	7	164	.6	57	- 14	662	3.37	4	5	ND	- 4	23	· . 1	2	2	25	.25	.057	10	42	.53	65	.03	8	.80	.01	.06	1	. 1
FORK 105-B Y	6	48	- 8	132	.4	49	12	568		. 5	5 -	ND	4	27	1	2	2	28	.27	.052	10	-55	.60	63	.04	4	- 85 -	.01	.06	1	1
STD C/AU-S	18	59	42	133	7.2	69	28	1030	4.18	39	17	7	28	51	17	18	18	56	.47	. 086	38	60	.88	182	.06	35	1.87	.06	.13	11	50

