

ARIS SUMMARY SHEET

District Geologist, Kamloops

Off Confidential: 89.04.25

ASSESSMENT REPORT 16985

MINING DIVISION: Similkameen

PROPERTY: Prime  
LOCATION: LAT 49 45 30 LONG 120 29 00  
UTM 10 5514582 681260  
NTS 092H16W  
CLAIM(S): Prime, Prime 1  
OPERATOR(S): Cons. Silver Butte Mines  
AUTHOR(S): Christopher, P.A.  
REPORT YEAR: 1988, 24 Pages

COMMODITIES

SEARCHED FOR: Copper, Gold

GEOLOGICAL

SUMMARY:

The property is underlain by Upper Triassic Nicola Group volcanic rocks that have been intruded by fine-grained feldspar porphyry, diorite and syenite. Copper and gold mineralization occurs in structurally controlled zones with mainly malachite, azurite and neotocite near surface and chalcopryrite plus minor bornite increasing at depth. Pyrite occurs as both fracture and disseminated mineralization with chalcopryrite.

WORK

DONE: Geochemical  
SOIL 224 sample(s) ;ME

RELATED

REPORTS: 06412, 06877, 06900, 07430, 07521, 08241, 08364, 08692, 09649, 13231  
MINFILE: 092HNE055, 092HNE056, 092HNE110

LOG NO: 0502	RD.
ACTION:	
FILE NO:	

GEOCHEMICAL REPORT ON THE PRIME PROPERTY

NICOLA & SIMILKAMEEN MINING DIVISIONS

SUMMERS CREEK, BRITISH COLUMBIA

CLAIMS

PRIME (702), PRIME 1 (323)

LOCATION

N.T.S.: 92H-16W  
 LATITUDE: 49° 45' 40"  
 LONGITUDE: 120° 29' 33"

OPERATOR

CONSOLIDATED SILVER BUTTE MINES LTD.  
 906 - 837 WEST HASTINGS STREET  
 VANCOUVER, B.C. V6C 1B6

OWNER

GIANT PIPER EXPLORATION INC.  
 906-837 WEST HASTINGS STREET  
 VANCOUVER, BRITISH COLUMBIA  
 V6C 1B6

GEOLOGICAL BRANCH  
 ASSESSMENT REPORT  
 16,985

FILMED

BY

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MARCH 7, 1988

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## SUMMARY

The Prime Property, consisting of 2 metric claims totaling 24 units is situated southeast of Missezula Lake and east of Summers Creek. The claims are adjacent to the Missezula Lake Road from kilometers 28 to 30 from Highway 5. The claims were staked to cover copper showings in Nicola Volcanics with renewed interest generated by detection of gold values near the southern boundary of the Prime claim by prospector Ed Mullin in 1978. Previous drilling and surface sampling by Newmont Exploration of Canada Ltd. has indicated a copper zone 200 meters by 15 to 30 meters with a 5 meter section in a trench averaging over 0.25 oz Au/ton. The government mineral inventory 92H-NE 55 and 92H-NE 56 indicates reported reserves of 23,000,000 ton with a 0.20 copper cut-off for the Primer or King George.

The present program consisted of analysis of 224 soil samples by ICP and gold geochemistry to complete analytical work on samples collected during the October 1987 field program. The samples fill-in and extend geochemical coverage reported by Christopher (1987).

Soil geochemical plots were made for gold, copper and molybdenum which showed the most significant responses with gold varying from 1 to 440 ppb, copper from 17 to 1600 ppm and molybdenum from 1 to 58 ppm. Coincident, strong copper, molybdenum and gold values occur together in a northerly trending belt from 7S to 0S with coincident anomalous copper and gold in the area of the old King George workings. The best potential in the area is for a previously unrecognized gold zones associated with known copper mineralization. Potential for by-product molybdenum is suggested by locally strong molybdenum responses.

Since anomalous geochemical values for copper and gold extend to the grid boundaries, extension of the geochemical coverages is warranted. The coincident gold, molybdenum and copper anomaly between line 3S and line 0S warrants trenching.

## INTRODUCTION

The Prime Property consisting of the 24 units is situated in the Nicola and Similkameen Mining Divisions about 30 kilometer north of Princeton, British Columbia. The property has easy road access to the western boundary with two and four-wheel-drive access to the showings. Peter Christopher & Associates Inc. was retained by the management of Giant Piper Exploration Inc. to conduct a geological and geochemical assessment of the Prime Property. The 1987 field program was conducted between October 16, 1987 and October 27, 1987 with 350 soil samples and nine rock samples collected form a grid on the property. A previous report by the writer (Christopher, 1987) summarized the geochemical results obtained from 126 soil samples and 9 rock samples collected. This report summarizes geochemical results for an additional 224 soil samples during the 1987 field program, and provides recommendations for trenching and extension of grid geochemical coverage.

LOCATION AND ACCESS (Figures 1 & 2)

The Prime Property is situated west of Summers Creek and east of Missezula Lake. The western claim boundary extends along the Missezula Lake Road from 28 to 30 kilometers east of Highway 5. The legal corner post for the Prime claim is on the east side of the Missezula Lake road at a bridge crossing of Summers Creek. The area is considered part of the Thompson Plateau of south-central British Columbia. The property is situated at the southwest corner of map sheet 92 H 16W and centers at geographic coordinates of 049° 45' 40" N. latitude and 120° 29' 33" W. longitude.

Access is by the Missezula Lake Road which branches off Highway 5 about 8 kilometers north of Princeton, British Columbia. Missezula Lake is 30 kilometers by good gravel road from Highway 5. The Prime Property can be reached by a 3.5-kilometer of two and 4-wheel-drive road that branches to the east from the main road about 1.5 kilometers south of Missezula Lake. making for slow progress. Elevation vary from 975 meters (3100 feet) in the valley bottom to 1550 meters (5,100') in the eastern claim area.

PROPERTY DEFINITION

The Prime Property, consisting of 24 grid unit is situated in the Nicola and Similkameen Mining Divisions, B.C. The claims were staked using the modified grid system with the Prime claim extending four units north and four units east from a legal corner post situated adjacent to the Missezula Lake Road and the Prime 1 claim extending four units east and 2 units south from a legal corner post situated east of Missezula Lake. The Prime 1 claim was staked by Pat Henry on May 14, 1976 and sold to Piper Petroleums Ltd. on January 5, 1977. The Prime claim was staked on July 28, 1979 by Gordon Gutrath as agent for Piper Petroleums Ltd. The Prime claim was a relocation of the abandoned Prime 47(5) claim.

Table 1 summarizes pertinent claim data and Figure 1 and 2 shows the approximate location of the Prime claims. The legal corner post and the 1E, 2E, 3E and 4E post for the Prime claim were located in the field. The southern boundary of the Prime Claim and was blazed and flagged. The location of the surveyed area is shown on Figure 2.

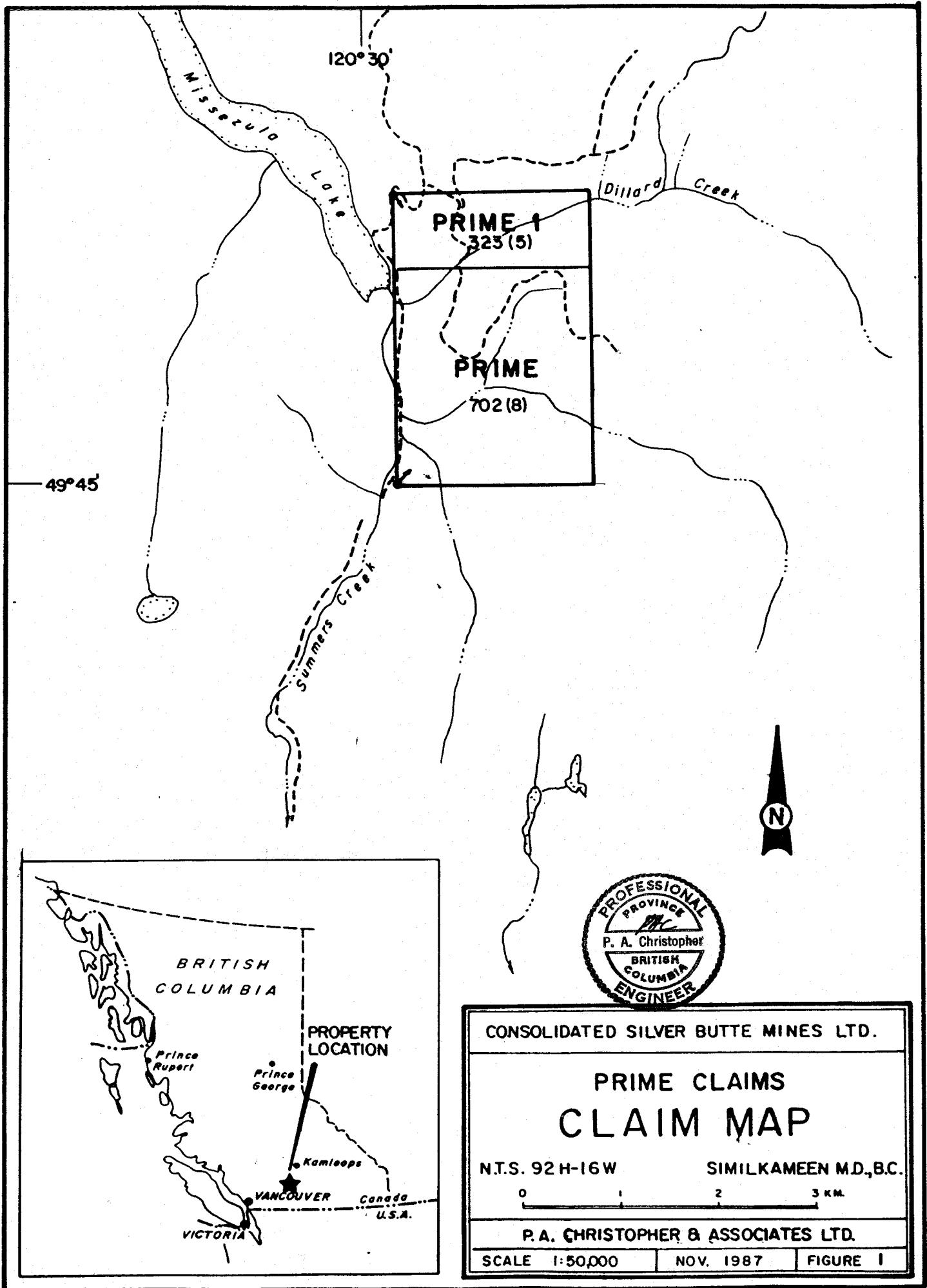
Table I. Pertinent Claim Data For MS Claims.

<u>CLAIM</u>	<u>RECORD #</u>	<u>UNITS/SHAPE</u>	<u>RECORD DATE</u>	<u>EXPIRY*</u>	<u>STAKER</u>
PRIME 1	323(5)	8/2SX4E	MAY 20/86	1990	PAT HENRY
PRIME	702(8)	16/4NX4E	AUG. 21/79	1990	GORDON GUTRATH

\* Before recording work summarized in this report.

HISTORY OF THE CLAIMS

The Prime 1 claim was staked by Pat Henry in May 1976 and the Prime claim was staked in July 1979 by Gordon C. Gutrath as agent for



120° 30'

Missezula  
Lake

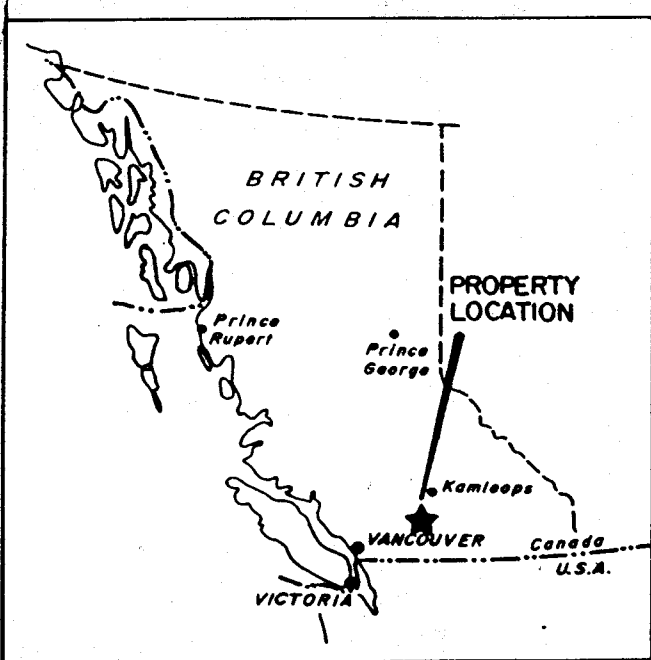
**PRIME 1**  
325 (5)

Dillard  
Creek

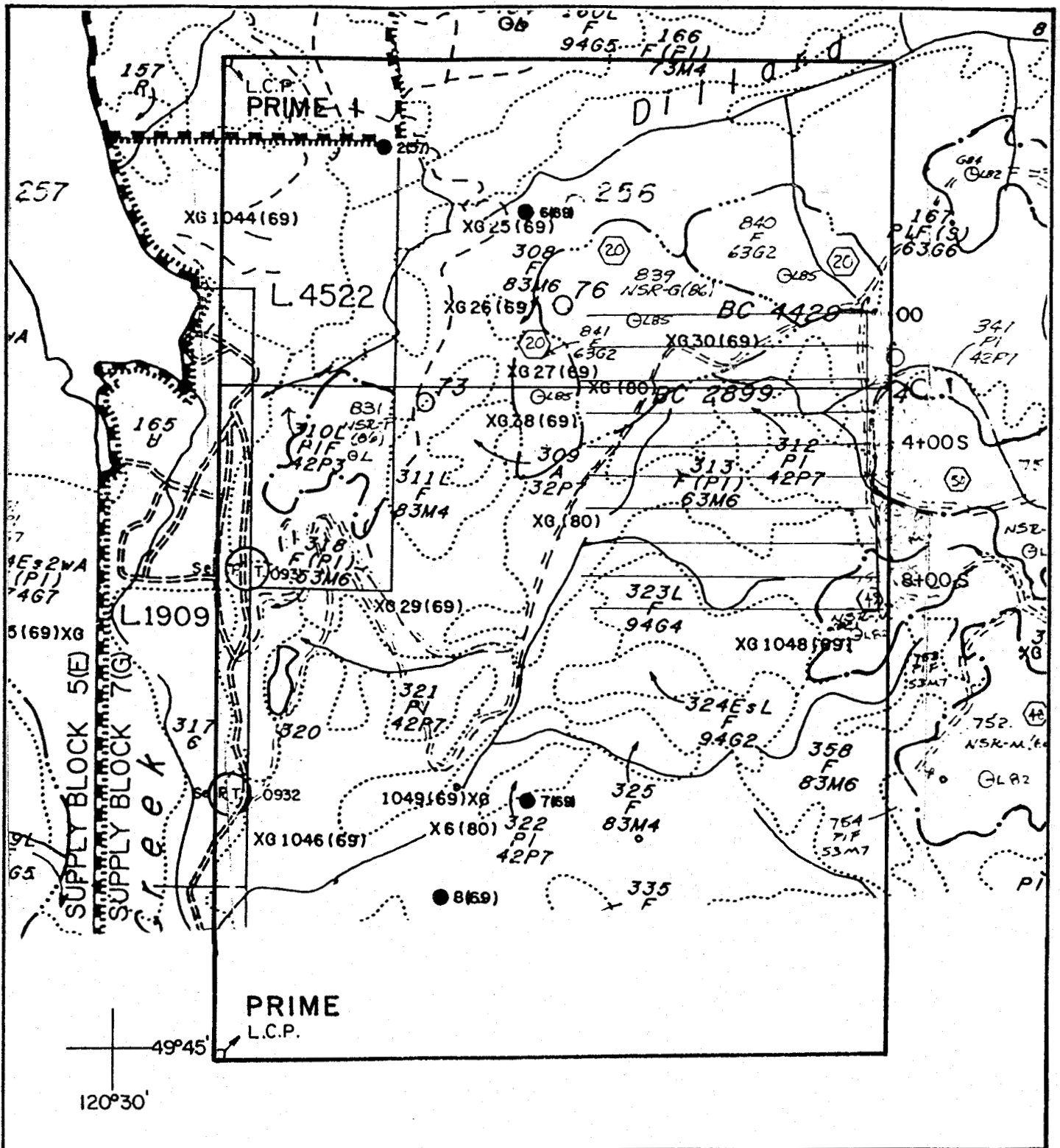
**PRIME**  
702 (8)

49° 45'

Summers  
Creek



CONSOLIDATED SILVER BUTTE MINES LTD.	
<b>PRIME CLAIMS CLAIM MAP</b>	
N.T.S. 92 H-16 W	SIMILKAMEEN M.D., B.C.
P. A. CHRISTOPHER & ASSOCIATES LTD.	
SCALE 1:50,000	NOV. 1987
FIGURE 1	



CONSOLIDATED SILVER BUTTE MINES LTD.

PRIME CLAIMS  
GRID LOCATION

N.T.S. 92H-16W SIMILKAMEEN M.D., B.C.

0 200 400 600 METRES

P.A. CHRISTOPHER & ASSOCIATES LTD.

SCALE

NOV. 1987

FIGURE 2

Piper Petroleums Ltd. (name changed to Giant Piper Petroleum Inc.) to relocated the abandoned Prime 47(5) claim. The claims were staked to cover part of a property known as the King George. The King George was explored by McIntyre Porcupine Mines Limited in 1962 and by Primer Group Minerals between 1963 and 1970 with portions of the claims explored by Perry, Knox, Kaufman, Inc in 1971 and by Belcarra Explorations Ltd. and Riocanex in 1972 and 1973. Exploration included geological mapping, soil geochemical, magnetic, electromagnetic and induced polarization, stripping and trenching surveys with at least 31 percussion holes totaling 4,192 feet and 33 diamond drill holes totaling 13,909 feet. In 1977 and 1978, Piper Petroleums Ltd. explored the property with magnetic, electromagnetic, and geochemical surveys which defined targets for stripping.

In 1978 a group of local prospectors (Edward Mullin, Gerald Burr and William Stevens) found copper showing south of the Prime claim and located the MS and HG claims. In August 1979 they optioned the adjoining Prime claim from Piper Petroleums and optioned the combined property to Newmont Exploration of Canada Ltd. Newmont worked the property between 1979 and 1981. Reports by John Nebocat and Dave Visagie outline geological, geophysical, geochemical, trenching and diamond drilling programs conducted on the property. A total of 12 holes totaling 2,550 meters were drilled by Newmont on a copper-gold zone that straddles the Prime-HG claim boundaries. Newmont reported a copper zone 200 meters long by 10 - 30 meters wide with an average copper content of 0.3 - 0.4%. The highest gold value obtained from the drilling was 3 meters of 0.2 ounces per ton. The potential for small tonnage high grade deposits was not fully tested by Newmont.

The Prime-HG-MS Property was optioned to Peter A. Christopher in 1984 and 1985 with magnetic, electromagnetic, soil geochemical and geological surveys completed before returning the property to the vendors. In 1986 the Prime claim was returned to Giant Piper Exploration Inc.

In October of 1987, Peter Christopher & Associates Inc. was retained by the management of Giant Piper to conduct a geological and geochemical assessment of the Prime Property (Christopher, 1987). This report review of the geochemical results for 224 soil samples collected during the October 1987 field program.

#### WORK PROGRAM

The 1987 work program was conducted by the writer with the assistance of prospectors F. Haidlauf and J. Lissau and assistant C. Reynolds between October 16, 1987 and October 27, 1987 (Christopher, 1987). A total of about 10 line kilometers of grid was chained with 350 stations flagged and soil sampled at 25 meter intervals. Budget restriction restricted analytical work to 124 samples with 224 samples dried and stored for future analytical work. Encouraging results for the initial samples (Christopher, 1987) provided justification for analysis of the 224 additional samples. The grid location is shown on Figure 2 with geochemical values for copper, gold and molybdenum shown on Figure 3 through 5 and analytical data presented in Appendix B. A cost statement for this program is presented as Appendix A.



## REGIONAL GEOLOGY

The Prime Property is situated in the Intermontane Tectonic Belt of the southern Canadian Cordillera. In southern British Columbia the upper Triassic Nicola Group dominates the belt. The Nicola Group consists mainly of alkalic and calc-alkalic volcanic and volcanoclastic rocks that have been divided by Preto (1979) into three north-trending structural belts, bounded by major faults. The Summers Creek fault zone running along the western boundary of the Prime Claim separates rocks of Preto's Central Belt from rocks of the Eastern Belt which underlie the property. Eastern Belt rocks along Summers Creek include both alkalic and calc-alkalic suites derived from comagmatic intrusions and are dominated by extrusive tuffs, lahar deposits, some basaltic flows, and high-level syenitic stocks (Preto, 1979; Christopher, 1973).

The Alleyne-Summers Creek fault system, a major north-south rift system passes along the western boundary of the claim and dominates the tectonic fabric of the property. Local faults generally parallel the northerly trend but N20°W and N40-45°E linears are probably also important fault directions.

Nicola rocks are generally only weakly metamorphosed with maximum regional grade reaching greenschist facies. Locally comagmatic intrusions have produced metasomatic and metamorphic effects with deposits like Ingerbelle, Copper Mountain, Afton, Axe and Craigmont resulting.

## MINERALIZATION

The Prime Property contains a number of structurally controlled copper bearing zones (B.C. Mineral Inventory 92H-NE, 55, 56, 110) with potential for precious metal enhanced 'syenitic' copper deposits. A zone near the southern boundary of the property was explored by Newmont Exploration of Canada Ltd. with a copper zone 200 meters long by 10 to 30 meters wide estimated by Newmont to contain 0.3 to 0.4% copper. The copper mineralization occurs mainly as the secondary minerals malachite, azurite, and neotocite. Chalcopyrite occurs as disseminations in fine alkalic intrusive and as fracture fillings. Pyrite generally occurs with chalcopyrite and minor bornite has been observed in a trench and in core (Nebocat, 1980).

Gold values of up to 3 meters of 0.204 oz Au/ton were intersected in drill hole 80-1 with a 14 meter section in a surface trench averaging 0.104 oz Au/ton. Gold values were reported to occur in fault zones that separated mineralized from fresh, unaltered rock.

Previous exploration on the property occurred in structurally controlled copper zones referred to as the King George (Rice, 1960) resulted in reported reserves of 23,000,000 with a copper cut-off of 0.2% (B.C. Mineral Inventory 92H-NE 56). The mineralization is described as occurring in two zones: a zone of silicified Nicola Volcanics with pyrite and chalcopyrite and a zone of minor pyrite and chalcopyrite associated with calcite veinlets and stringers. Little information is available on the precious metal content of the King George copper prospects.

## GEOCHEMICAL SURVEY

Soil samples were collected at 25 meter intervals along cross lines extending at 270° from a base line established near the eastern boundary of the Prime Claim (Figure 2). Soil samples were collected over the area of the old King George workings to test the precious metal potential of the copper bearing zone. A total of 350 soil samples were collected from the B horizon at about 20 cm, placed in craft soil bags and dried. A total of 126 of the soil samples were initially selected for 30 element ICP and atomic absorption gold analyses (Christopher, 1987). The remaining 224 soil samples were analyzed as part of the current program. The B horizon was sampled with a mattock at a depth of about 20 cm. The B horizon is generally greyish brown. Sample stations were chained and flagged with orange and blue flagging.

## RESULTS AND INTERPRETATION

Review of the analytical data for the 30 element ICP indicated that anomalous results were mainly restricted to Mo, Cu and Au. Results for Cu, Au and Mo were plotted and contoured on 1:5,000 scale maps (Figures 3, 4, 5). Background, slightly anomalous and anomalous ranges were based on other surveys conducted over Nicola volcanic terrain. Statistical treatment was not attempted because of the low number of samples. Analytical results are included in the Appendix B at the end of this report.

### Copper

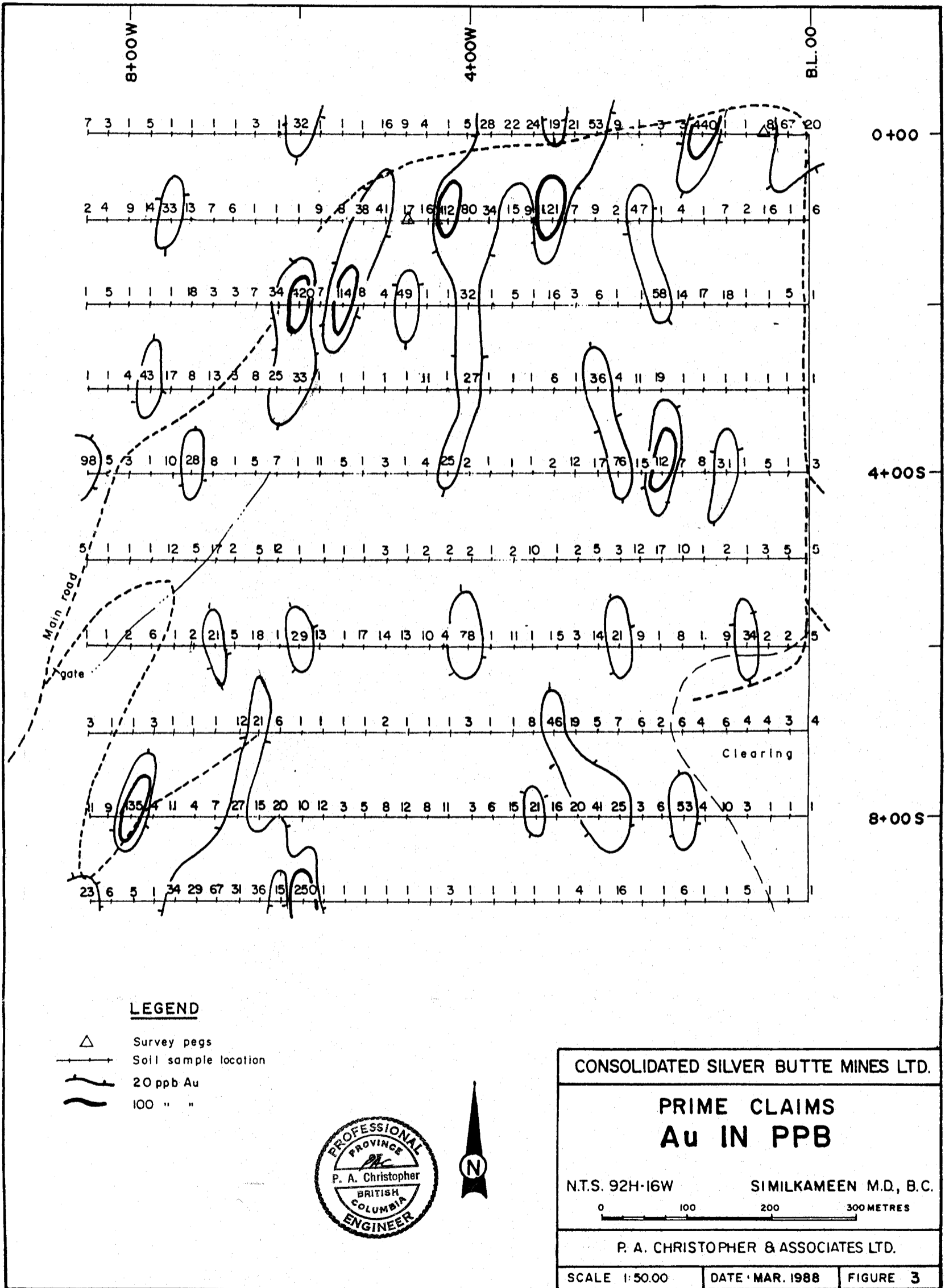
Copper values range from 17 ppm to 1600 ppm with values between 70 and 150 ppm considered weakly anomalous and values over 150 considered anomalous. A total of 97 samples were weakly anomalous or anomalous with 36 of these sample in the anomalous range. About 43% of the samples are at least weakly anomalous in copper with over 16% of the samples anomalous in copper. A strong northeasterly trending zones of anomalous copper values extends to the grid boundaries. Although silver values are not strongly anomalous, the higher silver results occur with the anomalous copper values (ie. all Ag values of 0.7ppm or higher).

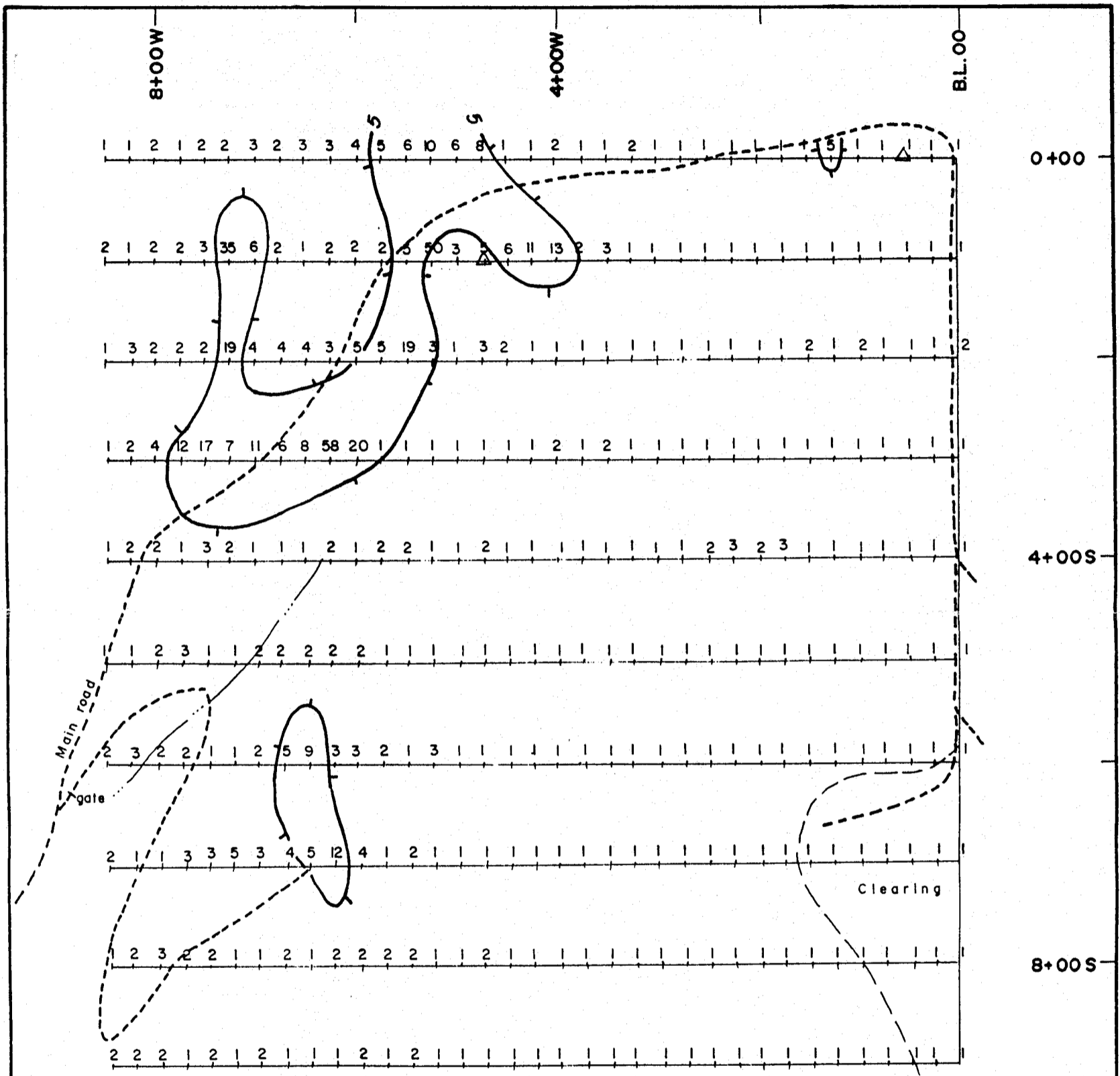
### Silver

Silver ranges from the detection limit of 0.1ppm to 1.7ppm with values between 0.6ppm and 1.7ppm considered weakly anomalous. A total of 6 weakly anomalous values were detected. The strongest silver values of 0.9ppm and 1.7ppm occur with the strong copper and gold on line 4S from 1+75W to 2+25W.


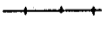

### Gold

Gold ranges from a lower detection limit of 1ppb to 440ppb at line OS 1+25W with values of 20 ppb considered anomalous and values over 99ppb considered strongly anomalous. A total of 36 anomalous values were detected with 5 of the strongly anomalous values. Anomalous gold values generally occur with anomalous copper and/or molybdenum values.




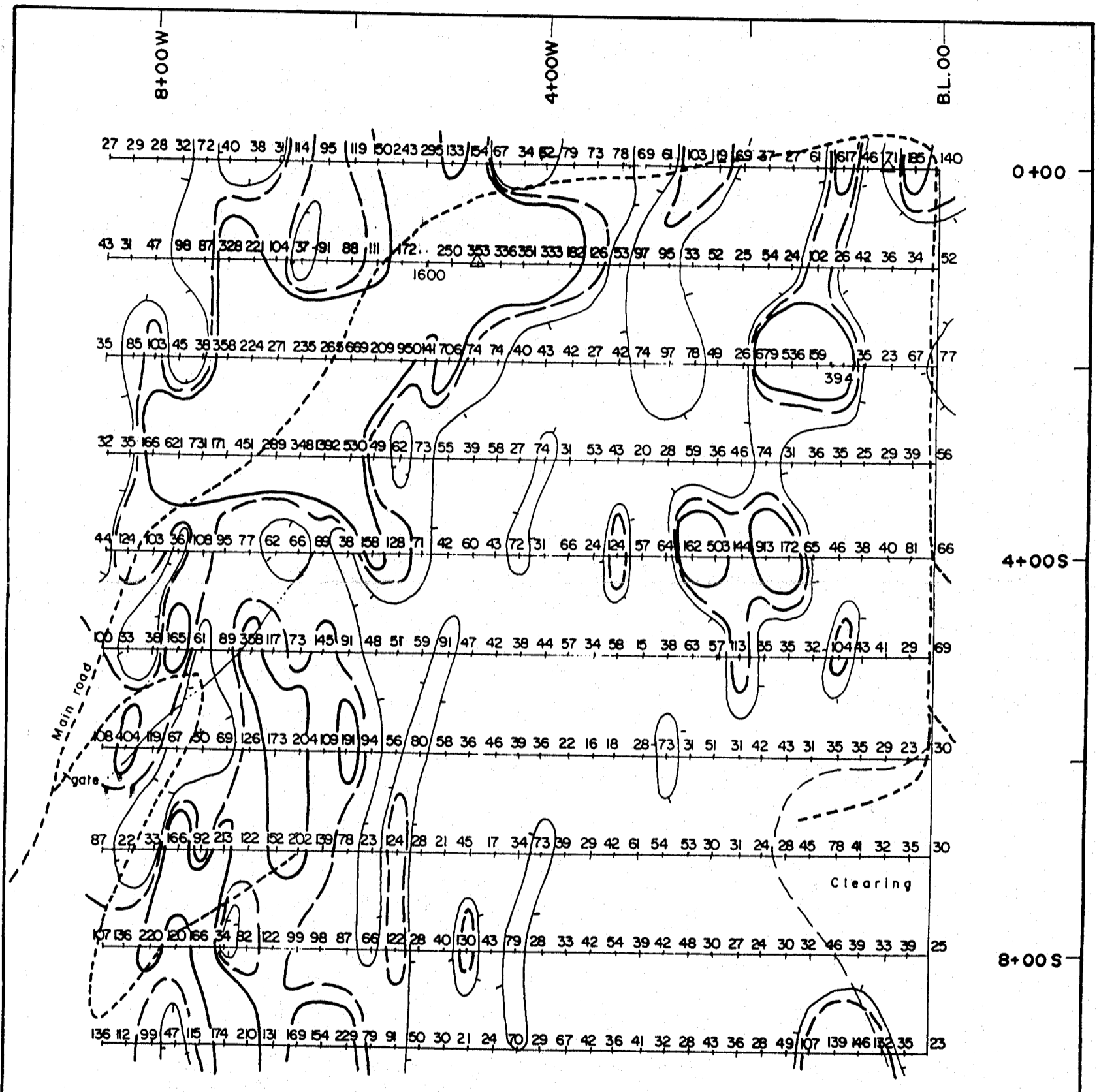


**LEGEND**

-  Survey pegs
-  Soil sample location
-  5 ppm Mo
- 100 " "
- 150 " "

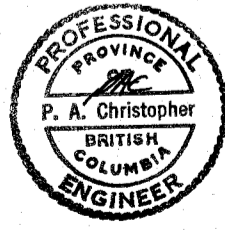


<b>CONSOLIDATED SILVER BUTTE MINES LTD.</b>		
<b>PRIME CLAIMS</b>		
<b>Mo IN PPM</b>		
N.T.S. 92H-16W	SIMILKAMEEN M.D., B.C.	
		
P. A. CHRISTOPHER & ASSOCIATES LTD.		
SCALE 1:50.00	DATE MAR. 1988	FIGURE 4



**LEGEND**

- △ Survey pegs
- +— Soil sample location
- 70 ppm Cu
- 100 " "
- 150 " "



CONSOLIDATED SILVER BUTTE MINES LTD.	
PRIME CLAIMS Cu IN PPM	
N.T.S. 92H-16W	NICOLA M.D., B.C.
P. A. CHRISTOPHER & ASSOCIATES LTD.	
SCALE 1:50,000	DATE MAR. 1988
FIGURE NO. 5	

### Molybdenum

Molybdenum values vary from a lower detection limit of 1ppm to 58ppm with 16 values of 5ppm or greater considered anomalous. The anomalous values for molybdenum are mainly in the northern part of the grid area and occur with anomalous copper and/or gold. The two strongest molybdenum responses of 58ppm and 50ppm occur with the strongest copper responses of 1600ppm and 1392ppm at stations 1S 5+25W and 3S 6+25W.

### CONCLUSIONS AND RECOMMENDATIONS

Soil sampling of part of the old King George showings has indicated the existence of anomalous gold condition in conjunction with northerly and northeasterly anomalous trends for copper and molybdenum. The strongest gold response is 440ppb for a sample at OS 1+25W and 420ppb for a sample at 2S at 6+00W.

Strong geochemical response has been obtained for copper, molybdenum, and gold from a grid covering less than 4 units of the 24 unit Prime Property. Anomalous conditions for copper and gold extend to all grid boundaries with anomalous molybdenum restricted to a northerly, possible mineralized structural trend from line 7S to OS. The strongest coincident copper, gold, and molybdenum anomaly occurs between lines 1S and 3S.

Extension of the geochemical grid is recommended to further define geochemical anomalies. Trenching is recommended to the strong geochemical response extending from 3S 6+25W to 1S 5+25W. Clearing and sampling some of the old King George workings is also recommended.


BIBLIOGRAPHY

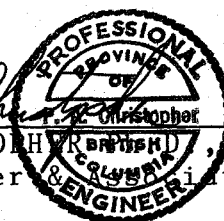
- B.C. Min. Mines. Annual Repts.: 1963 p.57, 1965 p.157, 1966 p. 176, 1968 p. 204, 1969 p. 279, 1971 p. 277, 1972 p. 128, 1973 p. 160; GEM: 1977 p.E137, 1978 p.E154. Exploration in B.C. 1984 p. 199. Government Assessment Reports: 493, 2354, 2344, 2356, 4169, 6412, 6877, 6900, 7340, 7521, 8241, 8364, 8692, 9649, 13231.
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CERTIFICATE

I, Peter A. Christopher, with business address at 3707 West 34th Avenue, Vancouver, British Columbia, do hereby certify that:

- 1) I am a consulting geological engineer registered with the Association of Professional Engineers of British Columbia since 1976.
- 2) I am a Fellow of the Geological Association of Canada and a member of the Society of Economic Geologists.
- 3) I hold a B.Sc. (1966) from the State University of New York at Fredonia, a M.A. (1968) from Dartmouth College and a Ph.D. (1973) from the University of British Columbia.
- 4) I have been practising my profession as a Geologist for over 20 years.
- 5) I have no interest in the properties or securities of Giant Piper Exploration Inc. or Consolidated Silver Butte Mines Ltd.
- 6) I have based this report on a review of available geological data, on several examinations of the property with the most recent examinations on October 16, 24, 25, 1987, and on a geochemical analysis of 224 soil samples collected between October 16, 1987 and October 27, 1987.
- 7) I consent to the use of this report by Consolidated Silver Butte Mines Ltd. or Giant Piper Explorations Inc. for any Filing Statement, Statement of Material Facts or filing Assessment Work.

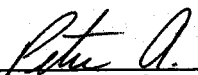
  
PETER A. CHRISTOPHER, P.Eng.  
Peter Christopher Associates Inc.  
March 7, 1988

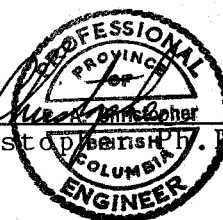




APPENDIX A COST STATEMENT

<u>PERSONNEL</u>		
Peter Christopher	Report Preparation	\$ 600.00
<u>GEOCHEMISTRY</u>		2464.00
<u>DRAFTING</u>	10 HOURS @ 17EA.	170.00
<u>WORD PROCESSING, PRINTING, BINDING, OFFICE</u>		250.00
<u>MANAGEMENT AND OVERHEAD @ 10%</u>		348.40
	TOTAL COSTS	\$ <u>3832.40</u>

  
Peter A. Christopher, P. Eng.  
March 7, 1988



APPENDIX B.

CERTIFICATES OF ANALYSIS

## GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
- SAMPLE TYPE: SOIL AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: FEB 22 1988

DATE REPORT MAILED: Feb 29/88

ASSAYER: *C. Leong* D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

PETER CHRISTOPHER PROJECT-PRIME File # 88-0497 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
OS 8+25W	1	29	4	60	.1	9	9	883	2.61	7	5	ND	1	22	1	2	3	55	.25	.095	3	14	.37	112	.09	3	2.38	.02	.06	1	3
OS 7+75W	1	32	2	55	.1	9	8	647	2.24	4	5	ND	1	16	1	2	2	45	.21	.094	2	10	.23	80	.08	3	2.05	.02	.04	1	5
OS 7+25W	2	40	4	58	.1	12	8	583	2.19	3	5	ND	1	19	1	2	2	48	.26	.055	2	14	.26	82	.09	5	1.83	.02	.06	1	1
OS 6+75W	2	31	4	38	.1	10	6	360	1.87	3	5	ND	1	16	1	2	2	38	.17	.052	3	11	.17	92	.09	6	1.81	.03	.04	1	1
OS 6+25W	3	95	6	70	.1	18	10	531	2.92	6	5	ND	1	22	1	2	2	63	.30	.091	3	18	.47	113	.10	4	2.59	.02	.08	1	1
OS 5+75W	5	150	3	64	.2	14	12	536	2.99	5	5	ND	1	20	1	2	2	55	.23	.136	4	13	.32	98	.11	4	2.75	.03	.05	1	1
OS 5+25W	10	295	11	69	.2	20	19	580	5.84	12	5	ND	2	52	1	2	6	128	.47	.089	7	35	1.13	138	.14	2	3.39	.02	.16	1	1
OS 4+75W	8	154	4	78	.1	18	14	864	4.54	10	5	ND	1	47	1	2	2	97	.40	.096	6	30	.85	153	.11	2	2.96	.03	.14	1	9
OS 4+25W	1	34	2	143	.1	11	7	1119	2.26	5	5	ND	1	19	1	2	2	46	.25	.108	3	16	.30	102	.08	4	1.77	.02	.06	1	1
OS 3+75W	1	79	2	168	.1	19	13	995	3.63	5	5	ND	1	40	1	2	5	80	.43	.080	4	29	.82	135	.11	3	2.80	.03	.14	1	28
OS 3+25W	2	78	7	131	.1	18	12	1266	3.58	6	5	ND	1	39	1	2	5	79	.49	.056	4	28	.79	126	.09	7	2.48	.02	.19	1	24
OS 2+75W	1	61	6	198	.1	17	11	753	3.50	5	5	ND	1	38	1	2	3	75	.40	.061	3	28	.76	123	.09	3	2.34	.02	.13	1	21
OS 2+25W	1	119	3	87	.2	24	14	557	3.78	8	5	ND	1	40	1	2	2	85	.58	.077	6	34	.75	89	.11	6	2.43	.02	.09	1	9
OS 1+75W	1	37	4	60	.1	11	9	454	3.02	6	5	ND	1	22	1	2	2	67	.34	.063	3	20	.48	96	.08	2	1.73	.02	.08	1	3
OS 1+25W	5	61	6	114	.1	7	3	156	.77	5	5	ND	1	111	1	2	4	15	4.16	.071	2	7	.26	53	.02	7	.51	.02	.04	1	440
OS 0+75W	1	46	7	64	.1	13	7	441	2.43	3	5	ND	1	28	1	2	3	56	.47	.067	3	18	.35	111	.09	5	1.96	.02	.07	1	1
OS 0+25W	1	185	3	106	.3	14	12	599	3.74	5	5	ND	1	28	1	2	3	85	.42	.049	5	21	.57	140	.10	2	2.40	.02	.07	1	67
IS 8+25W	1	31	2	44	.1	8	5	535	1.84	4	5	ND	1	17	1	2	2	39	.20	.078	2	10	.19	65	.08	2	1.51	.02	.05	1	4
IS 7+75W	2	98	2	54	.1	15	13	302	3.07	3	5	ND	1	25	1	2	5	76	.37	.039	3	19	.50	72	.11	5	2.14	.02	.06	1	14
IS 7+25W	35	328	3	72	.3	36	13	228	1.26	4	5	ND	1	36	1	3	2	29	1.29	.065	2	10	.22	56	.04	4	.98	.02	.04	1	13
IS 6+75W	2	104	4	65	.1	21	10	468	2.77	2	5	ND	1	23	1	2	4	59	.27	.070	3	24	.48	110	.11	3	2.40	.03	.07	1	6
IS 6+25W	2	91	4	78	.1	17	10	432	2.99	4	5	ND	1	25	1	2	4	65	.29	.085	4	18	.47	116	.11	3	2.61	.03	.07	1	1
IS 5+75W	2	111	4	92	.2	17	11	618	3.27	7	5	ND	1	27	1	2	2	70	.32	.110	5	23	.54	110	.10	4	2.58	.03	.10	1	9
IS 5+25W	50	1600	4	87	.3	26	21	817	7.10	8	5	ND	1	56	1	2	2	174	.47	.179	5	56	1.59	172	.19	6	3.43	.02	.24	1	38
IS 4+75W	5	353	6	94	.3	23	17	578	5.50	7	5	ND	1	49	1	2	5	126	.53	.079	6	36	1.02	128	.15	2	2.81	.02	.33	1	17
IS 4+25W	11	351	7	103	.2	26	23	684	6.60	8	5	ND	1	81	1	2	2	132	.58	.110	7	38	1.06	129	.15	3	3.34	.03	.33	1	112
IS 3+75W	2	182	9	67	.2	19	12	629	4.51	6	5	ND	2	55	1	2	3	113	.81	.085	9	35	.86	88	.14	5	2.50	.02	.22	1	34
IS 3+25W	1	53	8	86	.1	11	8	533	2.79	3	5	ND	1	33	1	2	2	63	.48	.071	5	21	.41	113	.10	6	1.81	.02	.15	1	9
IS 2+75W	1	95	3	58	.1	23	11	532	3.83	6	5	ND	1	51	1	2	2	102	.82	.074	8	40	.77	87	.14	7	2.27	.03	.15	1	7
IS 2+25W	1	52	5	55	.1	15	10	551	3.52	5	5	ND	1	34	1	2	4	89	.50	.026	5	29	.59	104	.12	4	1.71	.02	.16	1	2
IS 1+75W	1	54	5	42	.1	14	8	298	3.42	2	5	ND	1	35	1	2	3	94	.53	.054	5	29	.53	77	.11	4	1.65	.02	.10	1	1
IS 1+25W	1	102	14	71	.1	16	9	902	3.08	2	5	ND	1	43	1	2	2	68	.70	.051	6	24	.41	197	.09	9	2.49	.03	.11	1	1
IS 0+75W	1	42	9	106	.1	11	7	591	2.56	6	5	ND	1	38	1	2	2	52	.60	.189	6	19	.33	204	.08	5	2.40	.03	.06	1	2
IS 0+25W	1	34	8	66	.2	11	8	460	2.91	2	5	ND	1	26	1	2	3	65	.39	.037	4	23	.38	134	.09	2	2.04	.02	.10	2	1
2S 8+25W	3	85	7	58	.1	11	11	1226	2.77	3	5	ND	1	23	1	2	2	55	.26	.090	3	14	.29	111	.09	2	2.02	.02	.05	1	5
2S 7+75W	2	45	7	45	.1	10	6	615	2.05	2	5	ND	1	17	1	2	2	43	.22	.063	2	12	.24	71	.09	4	2.02	.02	.07	2	1
STD C/AU-S	19	58	39	132	7.5	67	29	1122	4.15	41	18	7	37	48	18	20	21	55	.46	.090	39	57	.88	179	.07	31	1.98	.09	.13	12	48

SAMPLE#	MO PPH	CU PPH	PB PPH	ZN PPH	AG PPH	NI PPH	CO PPH	MN PPH	FE %	AS PPH	U PPH	AU PPH	TH PPH	SR PPH	CD PPH	SB PPH	BI PPH	V PPH	CA %	P %	LA PPH	CR PPH	M6 %	BA PPH	TI %	B PPH	AL %	NA %	K %	W PPH	AU# PPB
2S 7+25W	4	358	11	59	.5	17	12	384	3.87	4	6	ND	1	31	1	2	2	91	.35	.058	5	28	.85	159	.13	5	3.03	.02	.07	1	18
2S 6+75W	3	271	8	73	.1	20	13	763	3.48	3	5	ND	1	21	1	2	4	85	.27	.063	3	34	.87	116	.13	7	3.13	.02	.05	1	3
2S 6+25W	5	265	2	66	.2	22	15	543	4.25	7	5	ND	1	30	1	2	5	89	.38	.078	5	27	.93	133	.12	7	2.62	.02	.13	1	34
2S 5+75W	3	209	8	63	.3	19	14	489	3.65	2	5	ND	1	25	1	2	4	86	.26	.044	3	23	.97	140	.13	9	2.62	.02	.12	1	7
2S 5+25W	3	141	7	149	.1	16	14	576	2.41	4	5	ND	1	23	1	2	2	44	.34	.110	3	12	.28	101	.07	7	1.51	.02	.05	1	8
2S 4+75W	1	74	6	120	.3	15	9	379	2.85	2	5	ND	1	26	1	2	2	59	.39	.190	3	20	.45	147	.08	7	2.11	.02	.10	1	49
2S 4+25W	1	40	9	71	.3	13	8	492	2.70	3	5	ND	1	21	1	2	2	61	.27	.095	3	18	.40	85	.09	5	1.86	.02	.06	1	1
2S 3+75W	1	42	3	78	.2	14	8	523	2.85	3	5	ND	1	22	1	2	2	65	.30	.103	3	21	.43	92	.10	4	2.06	.02	.06	1	1
2S 3+25W	1	42	2	74	.2	10	7	520	2.50	4	5	ND	1	20	1	2	2	54	.30	.123	3	16	.35	86	.08	5	1.96	.02	.06	1	1
2S 2+75W	1	97	2	71	.3	13	9	307	3.30	4	5	ND	1	25	1	2	2	80	.39	.068	3	23	.51	93	.08	6	1.84	.02	.07	1	3
2S 2+25W	1	49	5	87	.2	10	6	588	2.26	2	5	ND	1	14	1	2	2	49	.19	.089	2	13	.24	92	.07	8	1.51	.02	.04	2	1
2S 1+75W	1	679	12	213	.5	26	15	1255	4.55	7	5	ND	1	56	1	2	2	74	.93	.071	9	35	.75	354	.07	8	3.29	.03	.11	1	58
2S 1+25W	1	159	6	57	.3	14	10	504	3.49	5	5	ND	1	40	1	2	2	95	.67	.057	6	29	.67	101	.12	11	1.77	.02	.11	1	17
2S 0+75W	1	35	9	51	.1	11	7	448	2.91	2	5	ND	1	29	1	2	2	74	.48	.054	4	23	.46	112	.10	9	1.52	.02	.06	1	1
2S 0+25W	1	67	2	51	.2	16	9	510	3.47	7	5	ND	1	38	1	2	2	89	.57	.044	8	31	.70	107	.11	9	1.91	.02	.09	1	5
3S 8+25W	2	35	6	52	.2	9	6	542	1.96	3	5	ND	1	19	1	2	2	41	.21	.111	2	11	.22	88	.08	5	1.30	.02	.06	1	1
3S 7+75W	12	621	9	46	.4	20	18	587	5.33	6	5	ND	1	49	1	2	2	120	.59	.062	7	36	1.04	147	.14	14	2.39	.02	.25	1	43
3S 7+25W	7	171	5	80	.2	13	8	624	2.91	2	5	ND	1	31	1	2	2	54	.42	.111	4	15	.37	158	.08	5	1.61	.02	.08	2	8
3S 6+75W	6	289	9	96	.2	18	11	1074	3.51	5	5	ND	1	33	1	2	2	74	.40	.059	4	19	.65	190	.10	11	2.46	.03	.13	1	3
3S 6+25W	58	1392	6	107	.6	22	18	808	6.06	20	5	ND	1	47	1	2	3	107	.55	.153	4	21	.68	128	.07	7	2.76	.02	.08	1	25
3S 5+75W	1	49	2	117	.2	10	6	556	2.09	4	5	ND	1	27	1	2	2	40	.48	.034	3	15	.38	89	.08	7	2.00	.04	.06	2	1
3S 5+25W	1	73	12	116	.1	14	8	614	2.70	4	5	ND	1	38	1	2	2	55	.59	.040	4	19	.46	94	.10	7	2.47	.04	.06	1	1
3S 4+75W	1	39	8	73	.1	10	7	384	2.50	5	5	ND	1	23	1	2	2	53	.38	.066	2	16	.34	90	.09	4	1.91	.03	.08	1	1
3S 4+25W	1	27	2	80	.1	12	6	339	2.43	4	5	ND	1	20	1	2	2	50	.37	.105	3	16	.31	86	.09	5	2.19	.03	.07	1	1
3S 3+75W	1	31	5	64	.2	13	8	353	2.92	2	5	ND	1	26	1	2	2	73	.36	.087	3	21	.40	85	.11	6	1.73	.03	.09	1	1
3S 3+25W	1	43	5	62	.1	14	8	517	3.14	6	5	ND	1	41	1	2	2	81	.54	.087	3	25	.47	132	.10	7	1.65	.02	.08	1	1
3S 2+75W	1	28	8	69	.1	12	7	381	2.80	2	5	ND	1	28	1	2	2	69	.40	.097	3	21	.43	99	.10	6	1.71	.02	.07	1	1
3S 2+25W	1	36	7	50	.2	10	7	390	2.54	3	5	ND	1	19	1	2	2	58	.30	.058	2	16	.36	98	.08	4	1.62	.02	.06	2	4
3S 1+75W	1	74	7	110	.3	14	11	555	3.55	8	5	ND	1	24	1	2	2	81	.39	.057	3	22	.58	143	.07	7	1.90	.02	.07	1	19
3S 1+25W	1	36	6	129	.2	10	6	395	2.48	2	5	ND	1	26	1	2	2	53	.42	.032	3	15	.35	155	.06	8	1.75	.03	.06	2	1
3S 0+75W	1	25	7	85	.1	10	6	454	2.57	3	5	ND	1	20	1	2	2	57	.31	.034	3	18	.48	171	.05	6	2.13	.02	.05	1	1
3S 0+25W	1	39	6	56	.1	10	8	508	3.02	2	5	ND	1	18	1	2	2	64	.27	.067	2	25	.66	175	.04	10	1.89	.02	.08	1	1
4S 8+25W	2	124	2	59	.3	18	11	447	4.02	7	5	ND	1	34	1	2	2	97	.48	.047	5	29	.78	89	.10	7	1.86	.02	.14	1	5
4S 7+75W	1	36	7	66	.1	13	8	543	3.03	2	5	ND	1	32	1	2	2	73	.48	.032	4	25	.44	109	.12	6	1.79	.02	.19	1	1
4S 7+25W	2	95	3	62	.1	16	9	417	3.43	6	5	ND	1	35	1	2	2	85	.48	.031	5	31	.61	97	.13	7	1.80	.02	.20	1	28
4S 6+75W	1	62	5	66	.1	14	9	321	3.44	5	5	ND	1	34	1	2	2	89	.46	.035	4	30	.62	90	.13	7	1.87	.02	.15	1	1
STD C/AU-S	18	58	39	132	7.3	68	29	1056	4.16	43	20	7	37	47	18	18	24	55	.46	.088	38	58	.95	176	.07	34	1.94	.09	.14	13	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
4S 6+25W	2	89	5	83	.3	15	9	531	3.27	5	5	ND	1	32	1	2	2	77	.51	.159	4	24	.53	112	.10	4	1.89	.03	.08	1	7
4S 5+75W	2	158	6	52	.3	17	13	429	4.30	5	5	ND	2	43	1	2	6	119	.62	.049	6	36	.89	68	.15	8	1.90	.03	.12	1	11
4S 5+25W	1	71	2	51	.3	15	9	320	3.01	5	5	ND	1	25	1	2	2	69	.39	.076	3	20	.47	98	.11	4	2.35	.03	.07	1	1
4S 4+75W	2	60	2	53	.2	15	8	251	2.86	5	5	ND	1	22	1	2	2	62	.34	.070	4	19	.41	104	.11	3	2.56	.03	.07	1	1
4S 4+25W	1	72	5	36	.1	11	7	249	2.79	4	5	ND	1	25	1	2	2	67	.46	.031	5	17	.44	63	.10	6	1.78	.03	.05	2	25
4S 3+75W	1	66	2	75	.1	15	9	408	3.26	6	5	ND	1	33	1	2	2	80	.50	.110	4	26	.60	105	.12	5	2.18	.03	.09	1	1
4S 3+25W	1	124	6	101	.2	15	10	499	3.17	4	5	ND	2	43	1	2	2	63	.56	.039	5	19	.50	150	.11	7	2.55	.03	.10	1	1
4S 2+75W	1	64	8	81	.2	12	9	318	2.97	5	5	ND	1	24	1	2	2	62	.34	.062	3	19	.43	117	.08	3	1.69	.02	.07	1	12
4S 2+25W	3	503	11	249	.9	31	30	1636	6.32	25	5	ND	2	64	2	2	2	73	4.64	.085	6	35	1.06	175	.01	5	1.64	.01	.09	1	76
4S 1+75W	3	913	15	191	1.7	28	28	1342	7.94	16	5	ND	1	30	1	2	7	107	.65	.073	11	36	1.53	366	.01	6	2.98	.01	.11	1	112
4S 1+25W	1	65	11	85	.4	11	9	700	3.34	6	5	ND	1	17	1	2	5	56	.35	.050	4	16	.56	220	.02	3	1.94	.02	.08	1	8
4S 0+75W	1	38	10	68	.1	9	6	729	2.59	4	5	ND	1	15	1	2	2	49	.26	.088	4	16	.36	212	.07	4	2.42	.02	.06	1	1
4S 0+25W	1	81	6	59	.2	15	10	607	3.61	5	5	ND	1	42	1	2	2	92	.67	.076	8	31	.77	167	.11	6	2.12	.03	.09	1	1
5S 8+25W	1	33	2	74	.1	11	8	730	2.61	4	5	ND	1	27	1	2	2	58	.39	.048	3	22	.40	136	.11	5	1.60	.02	.15	1	1
5S 7+75W	3	165	3	61	.1	13	10	665	3.74	2	5	ND	1	38	1	2	3	90	.55	.042	5	26	.60	102	.12	5	1.61	.02	.19	1	1
5S 7+25W	1	89	2	82	.1	15	11	755	3.38	4	5	ND	1	40	1	2	3	77	.47	.052	5	31	.62	141	.12	5	1.85	.03	.20	1	5
5S 6+75W	2	117	2	70	.1	14	8	533	2.92	2	5	ND	1	26	1	2	2	63	.38	.098	4	21	.42	103	.10	8	2.01	.03	.06	1	2
5S 6+25W	2	145	4	48	.1	13	9	386	3.37	2	5	ND	1	29	1	2	2	81	.41	.051	4	22	.54	88	.11	4	1.92	.02	.05	2	12
5S 5+75W	1	48	4	45	.1	12	8	216	2.61	2	5	ND	1	22	1	2	2	59	.26	.054	2	16	.34	90	.10	3	1.97	.03	.06	2	1
5S 5+25W	1	59	2	51	.1	15	8	325	2.82	2	5	ND	1	28	1	2	2	63	.41	.079	3	20	.48	127	.11	4	2.32	.03	.09	2	1
5S 4+75W	1	47	7	52	.1	14	9	394	2.92	3	5	ND	1	24	1	2	4	64	.34	.063	3	21	.44	91	.11	3	2.16	.03	.07	1	1
5S 4+25W	1	38	3	47	.2	11	7	363	2.48	3	5	ND	1	22	1	2	2	50	.38	.022	3	14	.30	74	.10	4	2.08	.04	.05	2	2
5S 3+75W	1	57	3	57	.2	11	10	392	2.69	5	5	ND	1	20	1	2	3	56	.29	.051	3	15	.39	113	.08	4	2.11	.02	.08	1	1
5S 3+25W	1	58	6	64	.2	14	12	573	3.06	6	5	ND	1	17	1	2	2	55	.22	.032	2	16	.44	162	.07	2	2.20	.02	.07	1	10
5S 2+75W	1	38	3	57	.1	9	10	627	2.47	5	5	ND	1	17	1	2	2	46	.30	.080	2	14	.30	99	.09	3	2.37	.03	.04	1	2
5S 2+25W	1	57	7	96	.2	10	7	846	2.70	8	5	ND	1	14	1	2	2	49	.19	.052	2	16	.34	152	.06	3	1.49	.02	.06	1	3
5S 1+75W	1	35	2	99	.2	10	8	750	2.81	3	5	ND	1	16	1	2	3	47	.26	.077	5	12	.40	200	.04	4	2.01	.02	.07	1	17
5S 1+25W	1	32	2	78	.1	12	7	614	2.58	3	5	ND	1	22	1	2	2	56	.33	.133	3	19	.38	169	.08	4	2.06	.02	.06	1	1
5S 0+75W	1	43	9	76	.2	11	8	552	2.82	3	5	ND	1	18	1	2	2	62	.27	.101	3	21	.50	144	.06	5	2.08	.02	.06	1	1
5S 0+25W	1	29	8	33	.1	9	5	227	2.41	4	5	ND	1	27	1	2	2	57	.41	.017	3	17	.33	90	.09	3	1.70	.02	.07	2	5
6S 8+25W	3	404	4	55	.6	16	8	316	2.89	4	5	ND	1	97	1	2	4	56	2.65	.035	6	20	.57	101	.05	8	1.77	.04	.05	1	1
6S 7+75W	2	67	4	48	.1	13	8	311	2.62	2	5	ND	1	16	1	2	3	54	.20	.103	2	15	.29	76	.09	8	1.76	.02	.04	2	6
6S 7+25W	1	69	4	53	.2	15	9	356	2.58	5	5	ND	1	23	1	2	2	54	.25	.052	3	15	.37	116	.09	3	2.10	.03	.07	1	2
6S 6+75W	5	173	2	50	.2	27	16	846	3.87	5	5	ND	1	31	1	2	5	71	.32	.048	3	30	.65	130	.10	5	2.53	.03	.13	2	5
6S 6+25W	3	109	9	51	.1	21	12	517	3.37	2	5	ND	1	22	1	2	3	75	.32	.028	2	25	.54	89	.09	4	2.18	.02	.09	2	1
6S 5+75W	2	94	5	50	.5	13	9	289	2.62	4	5	ND	1	31	1	2	2	58	.46	.083	3	17	.45	113	.09	4	2.05	.02	.07	2	13
STD C/AU-S	19	59	42	132	7.6	68	29	1121	4.21	41	18	8	37	48	18	19	20	55	.46	.086	39	58	.96	181	.07	32	1.94	.08	.13	12	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AUX PPB
6S 5+25W	3	80	8	51	.2	11	8	364	2.42	2	5	ND	1	24	1	2	2	54	.48	.050	3	15	.35	140	.09	8	2.12	.03	.06	1	17
6S 4+75W	1	36	3	62	.1	13	9	391	2.72	6	5	ND	1	20	1	2	2	59	.27	.119	2	17	.35	117	.10	4	2.06	.02	.06	1	13
6S 4+25W	1	39	4	63	.4	12	8	229	2.97	3	5	ND	1	28	1	2	2	73	.37	.041	3	21	.53	103	.11	8	2.21	.02	.08	1	4
6S 3+75W	1	22	5	40	.1	9	8	559	2.28	4	5	ND	1	17	1	3	2	45	.24	.049	2	11	.28	87	.08	16	2.09	.03	.05	2	1
6S 3+25W	1	18	5	84	.1	9	7	454	2.27	3	5	ND	1	18	1	2	2	47	.26	.065	2	12	.30	93	.07	4	1.74	.03	.07	1	1
6S 2+75W	1	73	3	127	.5	12	10	770	3.70	6	5	ND	1	23	1	2	2	80	.41	.049	2	21	.64	160	.06	7	2.36	.02	.07	1	3
6S 2+25W	1	51	2	105	.1	11	7	502	2.72	4	5	ND	1	20	1	2	2	59	.29	.084	3	18	.48	173	.08	4	2.05	.02	.06	1	21
6S 1+75W	1	42	2	114	.3	12	8	776	2.88	3	5	ND	1	20	1	2	2	64	.32	.088	4	21	.48	144	.08	3	2.24	.02	.07	1	1
6S 1+25W	1	31	6	86	.1	10	7	484	2.65	5	5	ND	1	19	1	2	2	59	.29	.116	3	20	.42	119	.08	3	2.09	.02	.05	1	1
6S 0+75W	1	35	3	80	.3	7	7	694	2.57	5	5	ND	1	14	1	2	2	54	.23	.065	3	16	.38	126	.06	2	2.09	.02	.05	1	34
6S 0+25W	1	23	4	55	.1	9	6	272	2.39	2	5	ND	1	22	1	2	2	53	.35	.101	3	17	.30	92	.09	11	2.00	.03	.04	1	2
7S 8+50W	2	87	2	58	.2	11	10	384	2.93	4	5	ND	1	21	1	2	2	66	.30	.103	3	19	.43	55	.09	5	1.96	.02	.04	1	3
7S 8+25W	1	22	2	45	.3	5	6	284	2.55	2	5	ND	1	16	1	2	2	55	.21	.072	2	11	.14	28	.10	13	1.42	.04	.02	1	1
7S 8+00W	1	33	2	70	.2	11	7	311	2.10	5	5	ND	1	18	1	2	2	43	.20	.107	2	11	.20	63	.09	6	1.73	.03	.05	1	1
7S 7+75W	3	166	3	64	.3	17	11	480	3.63	3	5	ND	1	30	1	2	2	88	.40	.084	3	22	.60	101	.12	8	2.30	.03	.09	1	3
7S 7+50W	3	92	5	46	.1	13	9	249	2.94	2	5	ND	1	31	1	2	2	65	.36	.032	3	17	.52	120	.10	6	2.72	.03	.10	1	1
7S 7+25W	5	213	6	53	.3	21	15	413	4.38	6	5	ND	1	36	1	2	5	98	.43	.048	3	28	.70	110	.13	9	3.12	.03	.16	1	1
7S 7+00W	3	122	2	50	.1	19	13	332	4.00	2	5	ND	1	36	1	2	2	86	.43	.039	3	29	.70	110	.12	12	2.62	.03	.14	1	1
7S 6+75W	4	152	7	61	.1	17	13	419	3.49	4	5	ND	1	23	1	2	3	72	.27	.040	3	17	.45	99	.10	5	2.44	.03	.07	1	12
7S 6+50W	5	202	2	49	.4	12	14	553	4.11	2	5	ND	1	30	1	2	2	67	.35	.046	3	12	.38	70	.10	12	2.33	.03	.08	1	21
7S 6+25W	12	139	12	62	.3	19	18	1111	4.69	6	6	ND	1	33	1	2	5	77	.33	.084	5	18	.58	107	.11	5	3.33	.03	.07	1	6
7S 6+00W	4	78	6	58	.3	17	16	420	4.01	2	5	ND	1	40	1	2	4	75	.42	.050	4	19	.73	174	.11	20	3.63	.04	.12	1	1
7S 5+75W	1	23	2	49	.1	10	10	720	2.36	4	5	ND	1	22	1	2	2	44	.28	.043	3	10	.25	73	.10	5	2.03	.04	.05	2	1
7S 5+50W	2	124	3	68	.4	45	23	485	5.19	4	5	ND	1	43	1	2	4	85	.35	.072	4	61	1.07	170	.10	4	3.75	.03	.09	2	1
7S 5+25W	1	28	6	82	.1	9	8	1330	2.58	6	5	ND	1	22	1	2	2	46	.34	.192	5	12	.27	136	.10	6	3.30	.02	.04	1	1
7S 5+00W	1	21	9	36	.1	6	6	181	2.26	2	5	ND	1	16	1	2	2	41	.24	.053	3	9	.27	179	.04	6	2.40	.03	.05	1	2
7S 4+75W	1	45	2	48	.1	7	7	477	2.30	5	5	ND	1	19	1	2	2	46	.24	.097	4	12	.26	97	.08	7	1.97	.03	.04	1	1
7S 4+50W	1	17	2	41	.1	5	6	212	2.17	2	5	ND	1	14	1	2	2	45	.16	.052	2	8	.14	35	.09	11	1.91	.03	.02	1	1
7S 4+25W	1	34	5	55	.1	10	9	827	2.71	2	5	ND	1	23	1	2	2	55	.29	.068	3	13	.38	119	.08	5	2.57	.03	.06	1	1
7S 4+00W	1	73	2	66	.1	12	11	475	3.40	3	5	ND	1	29	1	2	2	75	.31	.082	2	19	.63	127	.09	3	3.05	.02	.05	1	3
7S 3+75W	1	39	3	82	.1	12	10	387	3.11	5	5	ND	1	21	1	2	2	65	.27	.082	2	18	.50	131	.07	2	2.32	.02	.08	1	1
7S 3+50W	1	29	2	81	.3	10	8	394	2.86	3	5	ND	1	21	1	2	2	63	.31	.046	2	16	.41	112	.06	5	1.84	.03	.08	1	1
7S 3+25W	1	42	3	117	.2	11	8	484	2.74	3	6	ND	1	20	1	2	4	55	.28	.056	2	17	.43	149	.06	2	1.74	.02	.07	1	8
7S 3+00W	1	61	5	80	.5	12	9	353	3.38	3	5	ND	1	24	1	2	5	79	.37	.042	3	21	.59	141	.09	7	2.25	.03	.06	1	46
7S 2+75W	1	54	3	92	.1	12	8	835	3.03	4	5	ND	1	24	1	2	2	70	.37	.034	2	20	.56	211	.08	6	2.10	.03	.13	1	19
7S 2+50W	1	53	4	83	.1	12	7	367	2.60	3	5	ND	1	20	1	2	2	62	.33	.074	2	16	.44	146	.09	3	2.44	.03	.07	1	5
STD C/AU-S	19	58	37	132	7.5	67	29	1061	4.14	44	19	8	37	47	18	17	21	55	.46	.080	38	59	.95	178	.07	37	1.94	.09	.13	12	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU1 PPB
7S 2+25W	1	30	2	77	.3	9	6	457	2.23	2	5	ND	1	18	1	3	2	48	.31	.048	2	13	.33	175	.07	3	1.71	.02	.05	1	7
7S 2+00W	1	31	3	88	.2	9	6	478	2.63	2	5	ND	1	15	1	3	2	56	.25	.052	2	14	.37	176	.08	3	2.05	.02	.05	1	6
7S 1+75W	1	24	5	69	.3	10	6	515	2.13	2	5	ND	1	17	1	2	2	46	.27	.083	2	13	.32	146	.07	6	1.62	.02	.04	1	2
7S 1+50W	1	28	2	88	.2	10	7	476	2.39	2	5	ND	1	18	1	2	2	53	.29	.113	3	16	.37	122	.08	3	1.85	.02	.04	1	6
7S 1+25W	1	45	2	101	.3	9	8	704	3.03	2	5	ND	1	19	1	2	2	65	.31	.066	3	19	.47	143	.07	3	2.17	.02	.05	1	4
7S 1+00W	1	78	7	183	.8	12	8	1977	2.94	23	5	ND	1	130	1	2	5	76	4.22	.290	5	20	.66	538	.07	41	2.35	.14	.52	1	6
7S 0+75W	1	41	5	83	.4	10	8	460	2.87	2	5	ND	1	25	1	2	3	67	.46	.099	4	20	.45	186	.08	6	1.95	.02	.07	1	4
7S 0+50W	1	32	3	64	.2	9	7	464	2.66	2	5	ND	1	18	1	2	2	61	.35	.111	3	17	.42	121	.09	2	2.10	.02	.04	1	4
7S 0+25W	1	35	2	46	.3	11	6	240	2.61	2	5	ND	1	21	1	2	2	61	.33	.054	3	19	.38	128	.09	2	1.89	.02	.04	1	3
7S 0+00W	1	30	7	62	.3	10	6	442	2.52	2	5	ND	1	23	1	2	2	59	.40	.093	3	17	.35	105	.09	6	1.81	.02	.06	1	4
8S 8+50W	1	107	2	73	.3	15	9	401	2.89	2	5	ND	1	26	1	2	2	58	.34	.128	4	16	.45	125	.08	5	2.11	.03	.08	1	11
8S 8+25W	2	136	5	58	.3	17	10	348	3.35	2	5	ND	1	28	1	2	2	74	.37	.085	3	19	.62	130	.11	4	2.64	.02	.10	1	9
8S 8+00W	3	220	2	49	.3	17	13	365	3.93	2	5	ND	1	44	1	2	2	91	.51	.060	4	24	.79	81	.12	3	2.58	.02	.09	2	135
8S 7+75W	2	120	2	64	.3	16	11	576	3.03	2	5	ND	1	24	1	2	5	63	.29	.053	2	19	.51	112	.10	4	2.44	.02	.07	1	4
8S 7+50W	2	166	6	58	.3	18	13	387	3.30	2	5	ND	1	29	1	2	2	59	.35	.087	3	17	.55	160	.08	4	2.76	.02	.10	1	11
8S 7+25W	1	34	5	50	.2	6	6	228	2.11	2	5	ND	1	18	1	2	2	42	.23	.063	2	8	.21	43	.08	4	1.42	.03	.04	1	4
8S 7+00W	1	82	6	84	.2	13	14	1227	3.23	2	5	ND	1	39	1	2	2	59	.50	.056	3	14	.62	115	.10	5	2.38	.02	.12	1	7
8S 6+75W	2	122	9	66	.3	15	14	585	3.54	2	5	ND	1	39	1	2	6	67	.32	.048	3	18	.62	112	.10	3	2.87	.02	.06	1	27
8S 6+50W	1	99	5	69	.4	15	12	686	3.51	3	5	ND	2	31	1	2	2	76	.35	.083	3	22	.62	144	.11	4	2.96	.02	.08	1	15
8S 6+25W	2	98	2	71	.3	13	11	753	3.27	3	5	ND	1	35	1	2	6	72	.43	.082	4	19	.59	135	.10	3	2.62	.02	.09	1	20
8S 6+00W	2	87	8	68	.3	14	11	1152	3.17	2	5	ND	1	31	1	2	2	73	.40	.059	4	20	.59	125	.10	3	2.92	.02	.09	1	10
8S 5+75W	2	66	2	73	.1	12	10	977	2.98	5	5	ND	1	24	1	2	4	66	.30	.095	2	19	.50	125	.10	4	2.42	.02	.06	1	12
8S 5+50W	2	122	4	67	.4	16	11	507	3.38	4	5	ND	1	29	1	2	2	78	.34	.078	3	21	.64	107	.11	6	2.92	.03	.11	1	3
8S 5+25W	1	28	2	62	.1	7	7	761	2.15	6	5	ND	1	22	1	2	2	44	.23	.175	2	10	.24	88	.07	4	1.72	.02	.04	1	5
8S 5+00W	1	40	5	61	.3	9	8	620	2.51	4	5	ND	1	19	1	2	2	52	.23	.113	2	12	.35	89	.09	3	2.46	.02	.05	1	8
8S 4+75W	2	130	3	58	.3	16	16	399	4.40	2	5	ND	2	60	1	2	4	90	.57	.047	5	20	.82	222	.12	5	3.77	.02	.11	1	12
8S 4+50W	1	43	2	61	.3	10	10	796	2.86	4	5	ND	1	30	1	2	2	58	.36	.106	3	13	.46	150	.09	3	2.75	.02	.06	1	8
8S 4+25W	1	79	7	60	.2	12	11	459	3.62	2	5	ND	1	31	1	2	3	84	.40	.031	3	20	.74	107	.10	5	2.78	.02	.08	1	11
8S 4+00W	1	28	2	54	.2	8	6	346	2.08	2	5	ND	1	16	1	2	2	42	.21	.056	2	11	.24	88	.07	2	1.74	.03	.04	1	3
8S 3+75W	1	33	5	65	.3	9	7	627	2.39	2	5	ND	1	18	1	2	2	50	.27	.095	2	12	.32	134	.07	2	1.67	.02	.05	1	6
8S 3+50W	1	42	9	59	.3	9	9	446	3.02	2	5	ND	1	21	1	2	2	64	.29	.038	2	15	.52	115	.09	4	2.21	.02	.07	1	15
8S 3+25W	1	54	8	75	.3	9	8	556	3.00	2	5	ND	1	21	1	2	5	70	.36	.033	3	18	.53	145	.08	3	2.07	.02	.07	1	21
8S 3+00W	1	39	4	80	.4	11	6	444	2.35	2	5	ND	1	21	1	2	2	55	.35	.060	3	14	.38	141	.09	5	1.67	.02	.07	1	16
8S 2+75W	1	42	4	98	.5	9	7	1029	2.51	2	5	ND	1	19	1	2	2	53	.41	.096	2	13	.30	213	.06	3	1.50	.02	.09	1	20
8S 2+50W	1	48	10	92	.6	10	6	394	2.75	2	5	ND	1	15	1	2	2	58	.22	.031	2	15	.52	171	.05	3	1.48	.02	.06	1	41
8S 2+25W	1	30	6	76	.5	13	7	554	2.46	4	5	ND	1	21	1	2	2	53	.34	.088	3	16	.46	175	.07	3	1.78	.02	.09	1	25
STD C/AU-S	19	58	38	132	7.4	68	28	1059	4.22	42	19	8	37	47	18	17	21	55	.47	.086	38	57	.96	179	.07	34	1.95	.09	.14	11	48

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AUX PPB
BS 2+00W	1	27	2	78	.1	10	6	508	2.37	2	5	ND	1	15	1	2	2	51	.24	.060	2	16	.41	120	.06	13	1.38	.03	.06	1	3
BS 1+75W	1	24	6	71	.1	8	5	425	2.17	2	5	ND	1	16	1	2	2	46	.24	.077	2	13	.36	114	.08	8	1.63	.03	.06	1	6
BS 1+50W	1	30	8	80	.2	11	7	580	2.44	2	5	ND	1	21	1	2	2	56	.34	.067	3	17	.44	124	.08	10	1.79	.02	.05	1	53
BS 1+25W	1	32	14	89	.2	10	7	504	2.58	3	5	ND	1	19	1	2	2	57	.29	.060	3	16	.40	135	.08	3	2.01	.02	.05	1	4
BS 1+00W	1	46	5	105	.1	9	8	819	3.13	4	5	ND	1	17	1	2	2	60	.34	.046	3	16	.43	208	.05	7	1.85	.02	.09	1	10
BS 0+75W	1	39	4	93	.1	11	8	540	3.07	4	5	ND	1	21	1	2	2	68	.36	.062	3	22	.55	149	.07	7	2.11	.02	.07	1	3
BS 0+50W	1	33	10	68	.1	10	7	442	2.66	3	5	ND	1	20	1	2	2	62	.38	.043	3	21	.55	146	.07	7	1.91	.02	.08	1	1
BS 0+25W	1	39	8	78	.1	14	8	745	3.11	2	5	ND	1	20	1	2	2	75	.33	.054	3	26	.64	173	.07	4	2.16	.02	.06	1	1
BS 0+00W	1	25	9	77	.1	11	6	556	2.46	2	5	ND	1	19	1	2	2	57	.30	.051	3	19	.47	154	.08	7	1.94	.02	.08	1	1
9S 8+50W	2	136	6	61	.2	17	12	770	4.40	4	5	ND	1	60	1	2	2	91	.54	.068	4	23	.85	121	.12	13	2.81	.02	.18	1	23
9S 8+25W	2	112	9	53	.2	14	10	422	3.52	5	5	ND	1	40	1	2	2	82	.51	.045	4	22	.66	87	.13	14	2.23	.03	.13	1	6
9S 8+00W	2	99	8	56	.1	15	10	361	3.26	4	5	ND	1	37	1	2	2	64	.45	.052	4	21	.55	116	.10	9	2.41	.03	.10	1	5
9S 7+75W	1	47	10	71	.2	12	8	516	2.33	2	5	ND	1	29	1	2	2	42	.32	.095	3	12	.34	98	.08	10	1.86	.03	.09	1	1
9S 7+50W	2	115	5	70	.2	16	19	1433	4.89	3	5	ND	1	70	1	3	3	89	.70	.046	4	23	1.02	92	.12	12	2.91	.02	.20	1	34
9S 7+25W	1	174	9	79	.2	17	19	1272	5.00	3	5	ND	1	56	1	2	2	79	.55	.036	5	18	.72	89	.11	5	3.36	.03	.15	1	29
9S 7+00W	2	210	16	108	.5	16	20	757	5.37	7	5	ND	1	58	1	2	2	96	.63	.066	4	23	1.39	91	.10	11	3.23	.03	.27	1	67
9S 6+75W	1	131	14	66	.1	13	26	698	4.46	3	6	ND	1	88	1	2	2	81	.86	.049	4	20	1.01	79	.13	12	3.66	.05	.14	1	31
9S 6+50W	1	169	7	60	.5	22	29	760	5.02	6	5	ND	1	65	1	2	6	78	.57	.049	6	26	.89	89	.10	6	2.65	.02	.33	1	36
9S 6+25W	1	154	14	54	.3	18	20	512	4.37	5	5	ND	1	98	1	2	4	93	1.07	.041	5	23	.98	91	.12	12	4.66	.03	.17	1	15
9S 6+00W	2	229	13	64	.3	18	20	721	5.16	11	6	ND	1	114	1	2	4	109	1.04	.054	5	22	.96	110	.13	11	4.07	.03	.17	1	250
9S 5+75W	1	79	9	54	.1	13	14	1105	3.73	20	5	ND	1	57	1	2	2	84	.80	.035	6	22	.65	109	.11	10	2.48	.02	.19	1	1
9S 5+50W	2	91	9	49	.1	13	12	504	3.70	10	5	ND	1	47	1	2	2	84	.61	.033	4	20	.69	112	.13	5	2.66	.02	.16	1	1
9S 5+25W	1	50	2	80	.1	14	9	292	3.04	6	5	ND	1	27	1	2	2	62	.35	.139	3	19	.49	171	.09	5	2.49	.02	.07	1	1
9S 5+00W	1	30	7	86	.2	10	7	396	2.67	2	5	ND	1	30	1	2	2	59	.37	.086	3	17	.38	107	.10	5	1.93	.03	.09	1	1
9S 4+75W	1	21	8	55	.1	8	6	400	2.13	2	5	ND	1	18	1	2	2	42	.23	.143	2	11	.29	104	.08	8	1.84	.02	.06	1	1
9S 4+50W	1	24	6	52	.1	8	6	334	2.10	5	5	ND	1	15	1	2	2	43	.20	.081	2	10	.21	79	.08	4	1.62	.03	.05	1	1
9S 4+25W	1	70	8	59	.2	11	10	455	3.52	3	5	ND	1	27	1	2	2	81	.42	.044	2	20	.68	106	.09	7	2.35	.02	.11	1	3
9S 4+00W	1	29	3	39	.1	7	7	281	2.57	2	5	ND	1	14	1	2	2	31	.22	.019	2	9	.21	171	.04	6	1.38	.02	.08	1	1
9S 3+75W	1	67	11	64	.2	10	8	373	2.33	3	5	ND	1	17	1	2	2	45	.26	.058	3	12	.25	113	.08	4	2.22	.03	.07	1	1
9S 3+50W	1	42	11	72	.2	12	8	652	3.17	2	5	ND	1	28	1	3	2	77	.38	.038	3	20	.59	148	.10	8	2.23	.02	.08	1	1
9S 3+25W	1	36	8	80	.1	11	7	469	2.88	2	5	ND	1	20	1	2	2	64	.29	.038	2	19	.59	123	.08	7	2.15	.03	.07	1	1
9S 3+00W	1	41	12	141	.2	14	7	612	2.96	3	5	ND	1	24	1	2	4	66	.35	.037	2	26	.68	162	.08	12	2.20	.03	.09	1	1
9S 2+75W	1	32	5	140	.3	10	6	537	2.55	2	5	ND	1	22	1	2	2	59	.26	.046	2	20	.52	139	.08	3	1.59	.02	.08	1	4
9S 2+50W	1	28	6	137	.2	9	7	477	2.60	2	5	ND	1	18	1	2	2	59	.26	.059	2	19	.46	119	.08	9	2.04	.03	.07	1	1
9S 2+25W	1	43	5	152	.3	10	6	864	2.53	2	5	ND	1	33	1	3	2	60	.37	.048	2	18	.49	189	.09	3	1.95	.02	.07	1	16
9S 2+00W	1	36	9	93	.2	9	7	483	2.77	2	5	ND	1	24	1	2	2	66	.35	.060	3	17	.47	145	.09	6	1.71	.03	.08	1	1
STD C/AU-S	18	57	39	131	7.2	67	28	1061	4.12	39	22	8	36	47	17	20	20	54	.46	.088	37	57	.94	174	.07	33	1.91	.09	.14	11	48



SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
9S 1+75W	1	28	5	84	.2	9	7	435	2.75	2	5	ND	1	26	1	2	2	64	.41	.055	3	19	.41	146	.09	3	1.71	.02	.07	1	1
9S 1+50W	1	49	6	55	.1	11	9	462	3.60	2	5	ND	1	33	1	2	5	100	.56	.021	3	25	.66	138	.12	3	1.68	.02	.10	1	6
9S 1+25W	1	107	10	73	.2	15	12	843	4.14	3	5	ND	1	33	1	2	3	98	.69	.038	7	35	.79	231	.11	6	2.66	.02	.25	1	1
9S 1+00W	1	139	16	119	.3	25	17	1384	5.17	4	5	ND	1	28	1	2	3	97	1.20	.047	6	50	.87	283	.03	5	2.08	.01	.20	1	1
9S 0+75W	1	146	11	87	.2	17	14	1015	4.83	8	5	ND	1	25	1	2	7	110	.57	.029	6	34	1.01	200	.04	4	2.24	.02	.16	1	5
9S 0+50W	1	132	7	87	.2	21	14	1245	4.77	2	5	ND	1	19	1	2	4	114	.46	.036	5	38	1.43	292	.04	4	2.67	.02	.21	1	1
9S 0+25W	1	35	7	64	.1	13	9	352	3.79	2	5	ND	1	26	1	2	3	89	.50	.023	4	26	.78	244	.10	3	2.23	.02	.08	1	1
9S 0+00W	1	23	6	80	.1	8	8	529	2.88	2	5	ND	1	17	1	2	2	63	.31	.033	2	19	.51	157	.06	2	1.47	.02	.09	1	1
STD C/AU-S	19	59	38	132	7.6	67	30	1096	4.21	44	18	8	37	49	19	21	22	57	.47	.083	40	58	.90	179	.07	36	1.81	.08	.13	11	47

# ACME ANALYTICAL LABORATORIES LTD.

PHONE: 253-3158

852 East Hastings St., Vancouver, B.C. V6A 1R6

File: BB-0497

Date: FEB 29 1988

PETER CHRISTOPHER & ASSOC.  
3707 W. 34TH AVE  
VANCOUVER, BC  
V6N 2K9

TERMS:  
NET TWO WEEKS -  
1½% PER MONTH CHARGED ON  
OVERDUE ACCOUNTS.

NUMBER	ASSAY	PRICE	AMOUNT
	PROJECT : PRIME		
224	ICP ANALYSIS @	6.00	1344.00
224	GEOCHEM AU ASSAY @	4.25	952.00
224	SOIL SAMPLE PREPARATION @	0.75	168.00
	TOTAL		2464.00

PLEASE PAY LAST AMOUNT 